LIBERO CONSORZIO COMUNALE DI AGRIGENTO

(L.R.15/2015)

ex Provincia Regionale di Agrigento

Settore Infrastrutture stradali

Edilizia scolastica Patrimonio e Manutenzione

Aggiornamento ed adeguamento alla normativa vigente del progetto esecutivo relativo ai lavori di costruzione dell'Istituto Tecnico per il Commercio in Campobello di Licata. Completamento.

PROGETTO ESECUTIVO

Procedura di affidamento ai sensi dell'art. 50 comma 1 lett.b) del D.lgs n.36/2023 a conferma dell'art. 1 comma 2 lett.a) del D.L. 16 Luglio 2020 n.76. D.Lgs. 50/2016 in deroga all'art. 36 comma 2,lett.a) del D.Lgs. 50/2016 come mod dall'art.1 della L.n.78 21 giugno 2022, (G.U. n. 77 del 31 marzo 2023 - S.O. n. 12) - CIG: A0374BAA46 -

N. Elaborato:	Titolo elaborato:
5.9	5 - IMPIANTO SPORTIVO: STRUTTURALI Tabelle Pilastri

Il Responsabile Unico del Procedimento
(Arch. Alfonso Giulio)

Il progettista
Delta Ingegneria
Ing. Desiderio Carlino

Sez. A
N. A 1984
Ordine degli Ingegneri della Provincia di Agrigento
Dott. Ing.
Desiderio Carlino
settori civile ambientale, industriale, dell'informazione

REV.	DATA	DESCRIZIONE	REDATTO	
A	Luglio 2024	Emissione	*Ing. Desiderio Carlino*	

Delta Ingegneria srl
via Artemide 3 92100 Agrigento - tel 0922 402212
email - g.ferraro@deltaingegneria.it

Lavoro: **D2403a** Intestazione lavoro: **Palestra Campobello**
Elemento: **PILASTRO** Gruppo: **2** Tabella: **Tabella pilastri**
Descrizione: **Pilastri**
Rck: **350.00** daN/cm² fyk: **4580.0** daN/cm² Copriferro di calcolo: **5.0** cm Copriferro di disegno: **4.0** cm
Verifica in ottemperanza alle NTC2018
Per le combinazioni sismiche la capacità è valutata in campo elastico o sostanzialmente elastico(§7.4.1 NTC2018)
Diametro staffe: **8** mm Numero braccia: **2**
ρ min.: **1.000** % Passo max. armatura longitudinale: **50.0** cm
Progettazione in capacità (NTC 2018): **Limitazione della domanda di resistenza al caso NON dissipativo**

ASTA NUM. 1 NI 32 NF 26 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 32C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice resistenza			aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-272	1215	608	0	1306	-1491	6.28	6.28	9.42	9.42	3	0.18	0.03	0.15	0.00	0.00	24.0
2	0	-380	933	409	0	950	-1129	6.28	6.28	9.42	9.42	2	0.18	0.02	0.12	0.00	0.00	24.0
3	0	-395	940	424	0	1010	-1136	6.28	6.28	9.42	9.42	2	0.18	0.02	0.12	0.00	0.00	24.0
4	0	-23	928	512	0	1000	-1157	6.28	6.28	9.42	9.42	2	0.18	0.02	0.12	0.00	0.00	24.0
5	0	-38	935	527	0	1060	-1165	6.28	6.28	9.42	9.42	2	0.19	0.02	0.12	0.00	0.00	24.0
6	0	-238	923	428	0	896	-1130	6.28	6.28	9.42	9.42	2	0.17	0.02	0.12	0.00	0.00	24.0
7	0	-287	947	477	0	1099	-1155	6.28	6.28	9.42	9.42	2	0.19	0.02	0.12	0.00	0.00	24.0
8	0	-131	922	459	0	911	-1138	6.28	6.28	9.42	9.42	2	0.18	0.02	0.12	0.00	0.00	24.0
9	0	-180	945	508	0	1114	-1164	6.28	6.28	9.42	9.42	2	0.19	0.02	0.12	0.00	0.00	24.0
10	0	-380	933	409	0	950	-1129	6.28	6.28	9.42	9.42	2	0.18	0.02	0.12	0.00	0.00	24.0
11	0	-395	940	424	0	1010	-1136	6.28	6.28	9.42	9.42	2	0.18	0.02	0.12	0.00	0.00	24.0
12	0	-23	928	512	0	1000	-1157	6.28	6.28	9.42	9.42	2	0.18	0.02	0.12	0.00	0.00	24.0
13	0	-38	935	527	0	1060	-1165	6.28	6.28	9.42	9.42	2	0.19	0.02	0.12	0.00	0.00	24.0
14	0	-238	923	428	0	896	-1130	6.28	6.28	9.42	9.42	2	0.17	0.02	0.12	0.00	0.00	24.0
15	0	-287	947	477	0	1099	-1155	6.28	6.28	9.42	9.42	2	0.19	0.02	0.12	0.00	0.00	24.0
16	0	-131	922	459	0	911	-1138	6.28	6.28	9.42	9.42	2	0.18	0.02	0.12	0.00	0.00	24.0
17	0	-180	945	508	0	1114	-1164	6.28	6.28	9.42	9.42	2	0.19	0.02	0.12	0.00	0.00	24.0
18	0	-1795	1326	183	0	1102	-1248	6.28	6.28	9.42	9.42	3	0.15	0.03	0.16	0.00	0.00	24.0
19	0	-1253	1132	802	0	1413	-1497	6.28	6.28	9.42	9.42	3	0.18	0.03	0.14	0.00	0.00	24.0
20	0	-703	1257	1065	0	1559	-1411	6.28	6.28	9.42	9.42	3	0.17	0.03	0.15	0.00	0.00	24.0
37	0	-1584	1388	15	0	1014	-1205	6.28	6.28	9.42	9.42	3	0.14	0.04	0.17	0.00	0.00	24.0
38	0	-681	1065	1046	0	1533	-1621	6.28	6.28	9.42	9.42	3	0.19	0.03	0.14	0.00	0.00	24.0
39	0	237	1273	1485	0	1776	-1478	6.28	6.28	9.42	9.42	3	0.18	0.04	0.21	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	83	211	1215	608	0	804	-489	6.28	6.28	9.42	9.42	3	0.06	0.03	0.13	0.00	0.00	24.0
2	83	-9	933	409	0	612	-359	6.28	6.28	9.42	9.42	2	0.07	0.02	0.10	0.00	0.00	24.0
3	83	-23	940	424	0	661	-360	6.28	6.28	9.42	9.42	2	0.07	0.02	0.10	0.00	0.00	24.0
4	83	348	928	512	0	577	-391	6.28	6.28	9.42	9.42	2	0.07	0.02	0.10	0.00	0.00	24.0
5	83	333	935	527	0	625	-393	6.28	6.28	9.42	9.42	2	0.08	0.02	0.10	0.00	0.00	24.0
6	83	133	923	428	0	543	-368	6.28	6.28	9.42	9.42	2	0.07	0.02	0.10	0.00	0.00	24.0
7	83	85	947	477	0	706	-374	6.28	6.28	9.42	9.42	2	0.08	0.02	0.10	0.00	0.00	24.0
8	83	240	922	459	0	532	-378	6.28	6.28	9.42	9.42	2	0.07	0.02	0.10	0.00	0.00	24.0
9	83	192	945	508	0	695	-384	6.28	6.28	9.42	9.42	2	0.08	0.02	0.10	0.00	0.00	24.0
10	83	-9	933	409	0	612	-359	6.28	6.28	9.42	9.42	2	0.07	0.02	0.10	0.00	0.00	24.0
11	83	-23	940	424	0	661	-360	6.28	6.28	9.42	9.42	2	0.07	0.02	0.10	0.00	0.00	24.0
12	83	348	928	512	0	577	-391	6.28	6.28	9.42	9.42	2	0.07	0.02	0.10	0.00	0.00	24.0
13	83	333	935	527	0	625	-393	6.28	6.28	9.42	9.42	2	0.08	0.02	0.10	0.00	0.00	24.0
14	83	133	923	428	0	543	-368	6.28	6.28	9.42	9.42	2	0.07	0.02	0.10	0.00	0.00	24.0
15	83	85	947	477	0	706	-374	6.28	6.28	9.42	9.42	2	0.08	0.02	0.10	0.00	0.00	24.0
16	83	240	922	459	0	532	-378	6.28	6.28	9.42	9.42	2	0.07	0.02	0.10	0.00	0.00	24.0
17	83	192	945	508	0	695	-384	6.28	6.28	9.42	9.42	2	0.08	0.02	0.10	0.00	0.00	24.0
18	83	-1312	1223	183	0	951	-197	6.28	6.28	9.42	9.42	3	0.05	0.03	0.13	0.00	0.00	24.0
19	83	-770	1235	802	0	752	-520	6.28	6.28	9.42	9.42	3	0.06	0.03	0.13	0.00	0.00	24.0
20	83	-220	1257	837	0	774	-374	6.28	6.28	9.42	9.42	3	0.05	0.03	0.14	0.00	0.00	24.0
37	83	-1101	1216	15	0	1002	-131	6.28	6.28	9.42	9.42	3	0.05	0.03	0.13	0.00	0.00	24.0
38	83	-198	1237	1046	0	670	-672	6.28	6.28	9.42	9.42	3	0.08	0.03	0.16	0.00	0.00	24.0
39	83	719	1273	1104	0	708	-428	6.28	6.28	9.42	9.42	3	0.06	0.03	0.15	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	165	694	1215	608	0	302	513	6.28	6.28	9.42	9.42	3	0.06	0.03	0.15	0.00	0.00	24.0
2	165	362	933	409	0	275	411	6.28	6.28	9.42	9.42	2	0.06	0.02	0.12	0.00	0.00	24.0
3	165	348	940	424	0	311	416	6.28	6.28	9.42	9.42	2	0.06	0.02	0.12	0.00	0.00	24.0
4	165	719	928	512	0	154	374	6.28	6.28	9.42	9.42	2	0.05	0.02	0.12	0.00	0.00	24.0
5	165	705	935	527	0	190	379	6.28	6.28	9.42	9.42	2	0.05	0.02	0.12	0.00	0.00	24.0
6	165	504	923	428	0	190	394	6.28	6.28	9.42	9.42	2	0.06	0.02	0.12	0.00	0.00	24.0
7	165	456	947	477	0	312	407	6.28	6.28	9.42	9.42	2	0.06	0.02	0.12	0.00	0.00	24.0
8	165	611	922	459	0	154	382	6.28	6.28	9.42	9.42	2	0.05	0.02	0.12	0.00	0.00	24.0
9	165	563	945	508	0	276	396	6.28	6.28	9.42	9.42	2	0.06	0.02	0.12	0.00	0.00	24.0
10	165	362	933	409	0	275	411	6.28	6.28	9.42	9.42	2	0.06	0.02	0.12	0.00	0.00	24.0
11	165	348	940	424	0	311	416	6.28	6.28	9.42	9.42	2	0.06	0.02	0.12	0.00	0.00	24.0
12	165	719	928	512	0	154	374	6.28	6.28	9.42	9.42	2	0.05	0.02	0.12	0.00	0.00	24.0
13	165	705	935	527	0	190	379	6.28	6.28	9.42	9.42	2	0.05	0.02	0.12	0.00	0.00	24.0
14	165	504	923	428	0	190	394	6.28	6.28	9.42	9.42	2	0.06	0.02	0.12	0.00	0.00	24.0
15	165	456	947	477	0	312	407	6.28	6.28	9.42	9.42	2	0.06	0.02	0.12	0.00	0.00	24.0
16	165	611	922	459	0	154	382	6.28	6.28	9.42	9.42	2	0.05	0.02	0.12	0.00	0.00	24.0
17	165	563	945	508	0	276	396	6.28	6.28	9.42	9.42	2	0.06	0.02	0.12	0.00	0.00	24.0
18	165	-830	1120	183	0	799	769	6.28	6.28	9.42	9.42	3	0.09	0.03	0.12	0.00	0.00	24.0
19	165	-288	1338	802	0	90	542	6.28	6.28	9.42	9.42	3	0.06	0.03	0.17	0.00	0.00	24.0
20	165	263	1257	608	0	178	663	6.28	6.28	9.42	9.42	3	0.08	0.03	0.16	0.00	0.00	24.0
37	165	-619	1044	15	0	989	800	6.28	6.28	9.42	9.42	3	0.10	0.03	0.11	0.00	0.00	24.0
38	165	285	1409	1046	0	-193	420	6.28	6.28	9.42	9.42	3	0.05	0.04	0.18	0.00	0.00	24.0
39	165	1202	1273	723	0	-46	623	6.28	6.28	9.42	9.42	3	0.07	0.03	0.16	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	248	1176	1215	608	0	-199	1516	6.28	6.28	9.42	9.42	3	0.18	0.03	0.15	0.00	0.00	24.0
2	248	734	933	409	0	-62	1181	6.28	6.28	9.42	9.42	2	0.15	0.02	0.12	0.00	0.00	24.0

3	248	719	940	424	0	-38	1191	6.28	6.28	9.42	9.42	2	0.15	0.02	0.12	0.00	0.00	24.0
4	248	1091	928	512	0	-269	1140	6.28	6.28	9.42	9.42	2	0.15	0.02	0.12	0.00	0.00	24.0
5	248	1076	935	527	0	-244	1150	6.28	6.28	9.42	9.42	2	0.15	0.02	0.12	0.00	0.00	24.0
6	248	876	923	428	0	-163	1155	6.28	6.28	9.42	9.42	2	0.15	0.02	0.12	0.00	0.00	24.0
7	248	827	947	477	0	-81	1189	6.28	6.28	9.42	9.42	2	0.15	0.02	0.12	0.00	0.00	24.0
8	248	983	922	459	0	-225	1143	6.28	6.28	9.42	9.42	2	0.15	0.02	0.12	0.00	0.00	24.0
9	248	934	945	508	0	-143	1176	6.28	6.28	9.42	9.42	2	0.15	0.02	0.12	0.00	0.00	24.0
10	248	734	933	409	0	-62	1181	6.28	6.28	9.42	9.42	2	0.15	0.02	0.12	0.00	0.00	24.0
11	248	719	940	424	0	-38	1191	6.28	6.28	9.42	9.42	2	0.15	0.02	0.12	0.00	0.00	24.0
12	248	1091	928	512	0	-269	1140	6.28	6.28	9.42	9.42	2	0.15	0.02	0.12	0.00	0.00	24.0
13	248	1076	935	527	0	-244	1150	6.28	6.28	9.42	9.42	2	0.15	0.02	0.12	0.00	0.00	24.0
14	248	876	923	428	0	-163	1155	6.28	6.28	9.42	9.42	2	0.15	0.02	0.12	0.00	0.00	24.0
15	248	827	947	477	0	-81	1189	6.28	6.28	9.42	9.42	2	0.15	0.02	0.12	0.00	0.00	24.0
16	248	983	922	459	0	-225	1143	6.28	6.28	9.42	9.42	2	0.15	0.02	0.12	0.00	0.00	24.0
17	248	934	945	508	0	-143	1176	6.28	6.28	9.42	9.42	2	0.15	0.02	0.12	0.00	0.00	24.0
18	248	-347	1016	183	0	648	1650	6.28	6.28	9.42	9.42	3	0.19	0.03	0.13	0.00	0.00	24.0
19	248	195	1442	802	0	-572	1689	6.28	6.28	9.42	9.42	3	0.20	0.04	0.18	0.00	0.00	24.0
20	248	745	1257	380	0	-229	1701	6.28	6.28	9.42	9.42	3	0.20	0.03	0.16	0.00	0.00	24.0
37	248	-136	872	15	0	977	1590	6.28	6.28	9.42	9.42	3	0.19	0.02	0.11	0.00	0.00	24.0
38	248	767	1581	1046	0	-1056	1653	6.28	6.28	9.42	9.42	3	0.20	0.04	0.20	0.00	0.00	24.0
39	248	1684	1273	342	0	-485	1674	6.28	6.28	9.42	9.42	3	0.20	0.03	0.16	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	330	1659	1215	608	0	-701	2518	6.28	6.28	9.42	9.42	3	0.30	0.03	0.15	0.00	0.00	24.0
2	330	1105	933	409	0	-399	1951	6.28	6.28	9.42	9.42	2	0.26	0.02	0.12	0.00	0.00	24.0
3	330	1090	940	424	0	-387	1967	6.28	6.28	9.42	9.42	2	0.26	0.02	0.12	0.00	0.00	24.0
4	330	1462	928	512	0	-692	1906	6.28	6.28	9.42	9.42	2	0.26	0.02	0.12	0.00	0.00	24.0
5	330	1447	935	527	0	-679	1922	6.28	6.28	9.42	9.42	2	0.27	0.02	0.12	0.00	0.00	24.0
6	330	1247	923	428	0	-516	1917	6.28	6.28	9.42	9.42	2	0.26	0.02	0.12	0.00	0.00	24.0
7	330	1198	947	477	0	-475	1970	6.28	6.28	9.42	9.42	2	0.26	0.02	0.12	0.00	0.00	24.0
8	330	1354	922	459	0	-604	1903	6.28	6.28	9.42	9.42	2	0.26	0.02	0.12	0.00	0.00	24.0
9	330	1305	945	508	0	-562	1956	6.28	6.28	9.42	9.42	2	0.27	0.02	0.12	0.00	0.00	24.0
10	330	1105	933	409	0	-399	1951	6.28	6.28	9.42	9.42	2	0.26	0.02	0.12	0.00	0.00	24.0
11	330	1090	940	424	0	-387	1967	6.28	6.28	9.42	9.42	2	0.26	0.02	0.12	0.00	0.00	24.0
12	330	1462	928	512	0	-692	1906	6.28	6.28	9.42	9.42	2	0.26	0.02	0.12	0.00	0.00	24.0
13	330	1447	935	527	0	-679	1922	6.28	6.28	9.42	9.42	2	0.27	0.02	0.12	0.00	0.00	24.0
14	330	1247	923	428	0	-516	1917	6.28	6.28	9.42	9.42	2	0.26	0.02	0.12	0.00	0.00	24.0
15	330	1198	947	477	0	-475	1970	6.28	6.28	9.42	9.42	2	0.26	0.02	0.12	0.00	0.00	24.0
16	330	1354	922	459	0	-604	1903	6.28	6.28	9.42	9.42	2	0.26	0.02	0.12	0.00	0.00	24.0
17	330	1305	945	508	0	-562	1956	6.28	6.28	9.42	9.42	2	0.27	0.02	0.12	0.00	0.00	24.0
18	330	135	913	183	0	497	2446	6.28	6.28	9.42	9.42	3	0.28	0.02	0.11	0.00	0.00	24.0
19	330	677	1545	802	0	-1233	2921	6.28	6.28	9.42	9.42	3	0.34	0.04	0.19	0.00	0.00	24.0
20	330	1228	1257	151	0	-448	2738	6.28	6.28	9.42	9.42	3	0.32	0.03	0.16	0.00	0.00	24.0
37	330	346	700	15	0	965	2238	6.28	6.28	9.42	9.42	3	0.26	0.02	0.09	0.00	0.00	24.0
38	330	1250	1753	1046	0	-1919	3028	6.28	6.28	9.42	9.42	3	0.36	0.05	0.22	0.00	0.00	24.0
39	330	2167	1273	-38	0	-611	2724	6.28	6.28	9.42	9.42	3	0.32	0.03	0.16	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

VERIFICA NODO IN TESTA AL PILASTRO, NODO NUM. 26 NON CONFINATO

(par.7.2.2 NTC2018 "La domanda di resistenza valutata con i criteri della progettazione in capacità può essere assunta non superiore alla domanda di resistenza valutata per il caso di comportamento strutturale non dissipativo.")

PROGETTAZIONE IN CAPACITA'

Asse loc. pilastro y nodo ESTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 45.0 cm, hjc= 20.0 cm
Asse loc. pilastro z nodo ESTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 30.0 cm, hjc= 50.0 cm

FxMin,inf	FxMin,sup	FxMax,sup	FySup	FzSup	Vjbdy	Vjbdz	Vres,y	Vres,z	I.R.compr.	Ashy	Ashz	PASSO	Nota
daN					daN		daN			cmq		cm	
-10000000150474662198766888550 40		1	-0	0	0	17616	17616	63005	105009	0.28	7.07	--	6.63

VERIFICA DI RESISTENZA CON SOLLECITAZIONI COMPORTAMENTO NON DISSIPATIVO

Asse loc. pilastro y nodo ESTERNO: Hjw= 40.0 cm, bj= 45.0 cm, hjc= 20.0 cm, db1= 45.0 cm

NC	Fx,sup	Fx,inf	Mb	Vb	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-0	-0	1091	945	0	2693	63005	0.04	0.00	40.00	
3	-0	-0	1112	939	0	2746	63005	0.04	0.00	40.00	
4	-0	-0	985	973	0	2431	63005	0.04	0.00	40.00	
5	-0	-0	1006	967	0	2484	63005	0.04	0.00	40.00	
6	-0	-0	1029	962	0	2540	63005	0.04	0.00	40.00	
7	-0	-0	1100	941	0	2715	63005	0.04	0.00	40.00	
8	-0	-0	997	971	0	2462	63005	0.04	0.00	40.00	
9	-0	-0	1068	950	0	2636	63005	0.04	0.00	40.00	
10	-0	-0	1091	945	0	2693	63005	0.04	0.00	40.00	
11	-0	-0	1112	939	0	2746	63005	0.04	0.00	40.00	
12	-0	-0	985	973	0	2431	63005	0.04	0.00	40.00	
13	-0	-0	1006	967	0	2484	63005	0.04	0.00	40.00	
14	-0	-0	1029	962	0	2540	63005	0.04	0.00	40.00	
15	-0	-0	1100	941	0	2715	63005	0.04	0.00	40.00	
16	-0	-0	997	971	0	2462	63005	0.04	0.00	40.00	
17	-0	-0	1068	950	0	2636	63005	0.04	0.00	40.00	

Asse loc. pilastro z nodo ESTERNO: Hjw= 40.0 cm, bj= 30.0 cm, hjc= 50.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb	Vb	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-0	-0	-1575	1535	0	3889	105009	0.04	0.00	40.00	
3	-0	-0	-1791	1599	0	4422	105009	0.04	0.00	40.00	
4	-0	-0	-1449	1507	0	3578	105009	0.03	0.00	40.00	
5	-0	-0	-1664	1572	0	4109	105009	0.04	0.00	40.00	
6	-0	-0	-1279	1450	0	3158	105009	0.03	0.00	40.00	
7	-0	-0	-1998	1665	0	4933	105009	0.05	0.00	40.00	
8	-0	-0	-1241	1442	0	3064	105009	0.03	0.00	40.00	
9	-0	-0	-1960	1657	0	4840	105009	0.05	0.00	40.00	
10	-0	-0	-1575	1535	0	3889	105009	0.04	0.00	40.00	
11	-0	-0	-1791	1599	0	4422	105009	0.04	0.00	40.00	
12	-0	-0	-1449	1507	0	3578	105009	0.03	0.00	40.00	
13	-0	-0	-1664	1572	0	4109	105009	0.04	0.00	40.00	
14	-0	-0	-1279	1450	0	3158	105009	0.03	0.00	40.00	

15	-0	-0	-1998	1665	0	4933	105009	0.05	0.00	40.00
16	-0	-0	-1241	1442	0	3064	105009	0.03	0.00	40.00
17	-0	-0	-1960	1657	0	4840	105009	0.05	0.00	40.00

CONFRONTO E SINTESI CONCLUSIVE (si assume in ogni caso passo <= 15 cm)

I.R.compr.	Ashy	Ashz	PASSO	Nota
	cmq		cm	
0.05	--	--	15.00	**VERIFICATO**

ASTA NUM. 2 NI 33 NF 32 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 32B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-7991	73	248	0	157	-122	6.28	6.28	9.42	9.42	3	0.01	0.01	0.03	0.00	0.00	24.0
2	0	-6293	47	162	0	22	-79	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
3	0	-6365	45	230	0	230	-74	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
4	0	-5930	67	151	0	12	-114	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
5	0	-6001	65	219	0	220	-110	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
6	0	-6082	56	79	0	-224	-97	6.28	6.28	9.42	9.42	2	0.02	0.00	0.01	0.00	0.00	24.0
7	0	-6321	50	306	0	469	-81	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
8	0	-5973	62	75	0	-227	-107	6.28	6.28	9.42	9.42	2	0.02	0.00	0.01	0.00	0.00	24.0
9	0	-6212	56	302	0	466	-92	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
10	0	-6293	47	162	0	22	-79	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
11	0	-6365	45	230	0	230	-74	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
12	0	-5930	67	151	0	12	-114	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
13	0	-6001	65	219	0	220	-110	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
14	0	-6082	56	79	0	-224	-97	6.28	6.28	9.42	9.42	2	0.02	0.00	0.01	0.00	0.00	24.0
15	0	-6321	50	306	0	469	-81	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
16	0	-5973	62	75	0	-227	-107	6.28	6.28	9.42	9.42	2	0.02	0.00	0.01	0.00	0.00	24.0
17	0	-6212	56	302	0	466	-92	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
18	0	-9536	213	213	0	-39	-166	6.28	6.28	9.42	9.42	3	0.02	0.01	0.03	0.00	0.00	24.0
19	0	-9072	-229	215	0	73	193	6.28	6.28	9.42	9.42	3	0.02	0.01	0.03	0.00	0.00	24.0
20	0	-8559	-17	946	0	748	41	6.28	6.28	9.42	9.42	3	0.04	0.02	0.11	0.00	0.00	24.0
37	0	-9281	387	224	0	-28	-329	6.28	6.28	9.42	9.42	3	0.03	0.01	0.04	0.00	0.00	24.0
38	0	-8507	-350	228	0	159	268	6.28	6.28	9.42	9.42	3	0.03	0.01	0.04	0.00	0.00	24.0
39	0	-7652	2	1446	0	1285	16	6.28	6.28	9.42	9.42	3	0.06	0.03	0.18	0.00	0.00	24.0
apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0																		
1	110	-7348	73	248	0	-115	-42	6.28	6.28	9.42	9.42	3	0.01	0.01	0.03	0.00	0.00	24.0
2	110	-5798	47	162	0	-156	-27	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
3	110	-5870	45	230	0	-24	-25	6.28	6.28	9.42	9.42	2	0.00	0.01	0.03	0.00	0.00	24.0
4	110	-5435	67	151	0	-153	-41	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
5	110	-5506	65	219	0	-21	-38	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
6	110	-5587	56	79	0	-310	-35	6.28	6.28	9.42	9.42	2	0.02	0.00	0.01	0.00	0.00	24.0
7	110	-5826	50	306	0	132	-26	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
8	110	-5478	62	75	0	-309	-39	6.28	6.28	9.42	9.42	2	0.02	0.00	0.01	0.00	0.00	24.0
9	110	-5717	56	302	0	133	-30	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
10	110	-5798	47	162	0	-156	-27	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
11	110	-5870	45	230	0	-24	-25	6.28	6.28	9.42	9.42	2	0.00	0.01	0.03	0.00	0.00	24.0
12	110	-5435	67	151	0	-153	-41	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
13	110	-5506	65	219	0	-21	-38	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
14	110	-5587	56	79	0	-310	-35	6.28	6.28	9.42	9.42	2	0.02	0.00	0.01	0.00	0.00	24.0
15	110	-5826	50	306	0	132	-26	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
16	110	-5478	62	75	0	-309	-39	6.28	6.28	9.42	9.42	2	0.02	0.00	0.01	0.00	0.00	24.0
17	110	-5717	56	302	0	133	-30	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
18	110	-8892	109	213	0	-273	12	6.28	6.28	9.42	9.42	3	0.01	0.00	0.03	0.00	0.00	24.0
19	110	-8428	-125	215	0	-164	-2	6.28	6.28	9.42	9.42	3	0.01	0.00	0.03	0.00	0.00	24.0
20	110	-7916	-17	641	0	-124	22	6.28	6.28	9.42	9.42	3	0.01	0.01	0.08	0.00	0.00	24.0
37	110	-8638	213	224	0	-274	1	6.28	6.28	9.42	9.42	3	0.01	0.01	0.03	0.00	0.00	24.0
38	110	-7864	-177	228	0	-92	-21	6.28	6.28	9.42	9.42	3	0.00	0.01	0.03	0.00	0.00	24.0
39	110	-7008	2	938	0	-26	19	6.28	6.28	9.42	9.42	3	0.00	0.02	0.12	0.00	0.00	24.0
apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0																		
1	220	-6704	73	248	0	-387	38	6.28	6.28	9.42	9.42	3	0.02	0.01	0.03	0.00	0.00	24.0
2	220	-5303	47	162	0	-334	25	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
3	220	-5375	45	230	0	-277	25	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
4	220	-4940	67	151	0	-319	33	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
5	220	-5011	65	219	0	-261	34	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
6	220	-5092	56	79	0	-397	27	6.28	6.28	9.42	9.42	2	0.03	0.00	0.01	0.00	0.00	24.0
7	220	-5331	50	306	0	-204	28	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
8	220	-4983	62	75	0	-392	30	6.28	6.28	9.42	9.42	2	0.03	0.00	0.01	0.00	0.00	24.0
9	220	-5222	56	302	0	-199	31	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
10	220	-5303	47	162	0	-334	25	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
11	220	-5375	45	230	0	-277	25	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
12	220	-4940	67	151	0	-319	33	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
13	220	-5011	65	219	0	-261	34	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
14	220	-5092	56	79	0	-397	27	6.28	6.28	9.42	9.42	2	0.03	0.00	0.01	0.00	0.00	24.0
15	220	-5331	50	306	0	-204	28	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
16	220	-4983	62	75	0	-392	30	6.28	6.28	9.42	9.42	2	0.03	0.00	0.01	0.00	0.00	24.0
17	220	-5222	56	302	0	-199	31	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
18	220	-8249	5	213	0	-507	75	6.28	6.28	9.42	9.42	3	0.02	0.00	0.03	0.00	0.00	24.0
19	220	-7785	-21	215	0	-400	-82	6.28	6.28	9.42	9.42	3	0.02	0.00	0.03	0.00	0.00	24.0
20	220	-7272	-17	336	0	-662	3	6.28	6.28	9.42	9.42	3	0.03	0.01	0.04	0.00	0.00	24.0
37	220	-7994	40	224	0	-521	140	6.28	6.28	9.42	9.42	3	0.03	0.01	0.03	0.00	0.00	24.0
38	220	-7220	-4	228	0	-342	-120	6.28	6.28	9.42	9.42	3	0.02	0.01	0.03	0.00	0.00	24.0
39	220	-6365	2	430	0	-779	21	6.28	6.28	9.42	9.42	3	0.04	0.01	0.05	0.00	0.00	24.0
apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0																		
1	330	-6060	73	248	0	-659	118	6.28	6.28	9.42	9.42	3	0.03	0.01	0.03	0.00	0.00	24.0
2	330	-4808	47	162	0	-513	77	6.28	6.28	9.42	9.42	2	0.04	0.00	0.02	0.00	0.00	24.0
3	330	-4880	45	230	0	-530	75	6.28	6.28	9.42	9.42	2	0.04	0.01	0.03	0.00	0.00	24.0
4	330	-4445	67	151	0	-485	107	6.28	6.28	9.42	9.42	2	0.04	0.00	0.02	0.00	0.00	24.0
5	330	-4516	65	219	0	-502	105	6.28	6.28	9.42	9.42	2	0.04	0.01	0.03	0.00	0.00	24.0
6	330	-4597	56	79	0	-483	89	6.28	6.28	9.42	9.42	2	0.04	0.00	0.01	0.00	0.00	24.0
7	330	-4836	50	306	0	-540	83	6.28	6.28	9.42	9.42	2	0.04	0.01	0.04	0.00	0.00	24.0
8	330	-4488	62	75	0	-475	99	6.28	6.28	9.42	9.42	2	0.04	0.00	0.01	0.00	0.00	24.0

9	330	-4727	56	302	0	-531	92	6.28	6.28	9.42	9.42	2	0.04	0.01	0.04	0.00	0.00	24.0
10	330	-4808	47	162	0	-513	77	6.28	6.28	9.42	9.42	2	0.04	0.00	0.02	0.00	0.00	24.0
11	330	-4880	45	230	0	-530	75	6.28	6.28	9.42	9.42	2	0.04	0.01	0.03	0.00	0.00	24.0
12	330	-4445	67	151	0	-485	107	6.28	6.28	9.42	9.42	2	0.04	0.00	0.02	0.00	0.00	24.0
13	330	-4516	65	219	0	-502	105	6.28	6.28	9.42	9.42	2	0.04	0.01	0.03	0.00	0.00	24.0
14	330	-4597	56	79	0	-483	89	6.28	6.28	9.42	9.42	2	0.04	0.00	0.01	0.00	0.00	24.0
15	330	-4836	50	306	0	-540	83	6.28	6.28	9.42	9.42	2	0.04	0.01	0.04	0.00	0.00	24.0
16	330	-4488	62	75	0	-475	99	6.28	6.28	9.42	9.42	2	0.04	0.00	0.01	0.00	0.00	24.0
17	330	-4727	56	302	0	-531	92	6.28	6.28	9.42	9.42	2	0.04	0.01	0.04	0.00	0.00	24.0
18	330	-7606	-99	213	0	-741	23	6.28	6.28	9.42	9.42	3	0.04	0.00	0.03	0.00	0.00	24.0
19	330	-7142	83	215	0	-636	-48	6.28	6.28	9.42	9.42	3	0.03	0.00	0.03	0.00	0.00	24.0
20	330	-6628	-17	32	0	-865	-16	6.28	6.28	9.42	9.42	3	0.04	0.00	0.00	0.00	0.00	24.0
37	330	-7350	-133	224	0	-767	89	6.28	6.28	9.42	9.42	3	0.04	0.01	0.03	0.00	0.00	24.0
38	330	-6576	170	228	0	-592	-29	6.28	6.28	9.42	9.42	3	0.03	0.01	0.03	0.00	0.00	24.0
39	330	-5722	2	-78	0	-973	24	6.28	6.28	9.42	9.42	3	0.05	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	440	-5417	73	248	0	-932	198	6.28	6.28	9.42	9.42	3	0.05	0.01	0.03	0.00	0.00	24.0
2	440	-4313	47	162	0	-691	129	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
3	440	-4385	45	230	0	-783	124	6.28	6.28	9.42	9.42	2	0.06	0.01	0.03	0.00	0.00	24.0
4	440	-3950	67	151	0	-651	181	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
5	440	-4021	65	219	0	-743	177	6.28	6.28	9.42	9.42	2	0.06	0.01	0.03	0.00	0.00	24.0
6	440	-4102	56	79	0	-570	152	6.28	6.28	9.42	9.42	2	0.05	0.00	0.01	0.00	0.00	24.0
7	440	-4341	50	306	0	-876	138	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
8	440	-3993	62	75	0	-557	167	6.28	6.28	9.42	9.42	2	0.05	0.00	0.01	0.00	0.00	24.0
9	440	-4232	56	302	0	-864	154	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
10	440	-4313	47	162	0	-691	129	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
11	440	-4385	45	230	0	-783	124	6.28	6.28	9.42	9.42	2	0.06	0.01	0.03	0.00	0.00	24.0
12	440	-3950	67	151	0	-651	181	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
13	440	-4021	65	219	0	-743	177	6.28	6.28	9.42	9.42	2	0.06	0.01	0.03	0.00	0.00	24.0
14	440	-4102	56	79	0	-570	152	6.28	6.28	9.42	9.42	2	0.05	0.00	0.01	0.00	0.00	24.0
15	440	-4341	50	306	0	-876	138	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
16	440	-3993	62	75	0	-557	167	6.28	6.28	9.42	9.42	2	0.05	0.00	0.01	0.00	0.00	24.0
17	440	-4232	56	302	0	-864	154	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
18	440	-6962	-203	213	0	-975	-143	6.28	6.28	9.42	9.42	3	0.05	0.01	0.03	0.00	0.00	24.0
19	440	-6498	187	215	0	-873	101	6.28	6.28	9.42	9.42	3	0.04	0.00	0.03	0.00	0.00	24.0
20	440	-5985	-17	-273	0	-732	-35	6.28	6.28	9.42	9.42	3	0.04	0.01	0.03	0.00	0.00	24.0
37	440	-6707	-306	224	0	-1014	-153	6.28	6.28	9.42	9.42	3	0.05	0.01	0.03	0.00	0.00	24.0
38	440	-5933	343	228	0	-843	253	6.28	6.28	9.42	9.42	3	0.05	0.01	0.03	0.00	0.00	24.0
39	440	-5078	2	-586	0	-608	27	6.28	6.28	9.42	9.42	3	0.03	0.01	0.07	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

VERIFICA NODO IN TESTA AL PILASTRO, NODO NUM. 32 NON CONFINATO

(par.7.2.2 NTC2018 "La domanda di resistenza valutata con i criteri della progettazione in capacità può essere assunta non superiore alla domanda di resistenza valutata per il caso di comportamento strutturale non dissipativo.")

PROGETTAZIONE IN CAPACITA'

Asse loc. pilastro y nodo ESTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 45.0 cm, hjc= 20.0 cm
Asse loc. pilastro z nodo ESTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 30.0 cm, hjc= 50.0 cm

FxMin,inf	FxMin,sup	FxMax,sup	FySup	FzSup	Vjbdy	Vjbdz	Vres,y	Vres,z	I.R.compr.	Ashy	Ashz	PASSO	Nota
daN					daN		daN			cmq		cm	
-3950	-23	-395	922	409	16695	17208	62907	104844	0.27	4.38	--	11.93	

VERIFICA DI RESISTENZA CON SOLLECITAZIONI COMPORTAMENTO NON DISSIPATIVO

Asse loc. pilastro y nodo ESTERNO: Hjw= 40.0 cm, bj= 45.0 cm, hjc= 20.0 cm, db1= 45.0 cm

NC	Fx,sup	Fx,inf	Mb	Vb	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-380	-4313	-1918	1981	933	3802	62910	0.06	0.00	40.00	
3	-395	-4385	-1912	1979	940	3780	62907	0.06	0.00	40.00	
4	-23	-3950	-1868	1971	928	3684	63000	0.06	0.00	40.00	
5	-38	-4021	-1862	1969	935	3662	62996	0.06	0.00	40.00	
6	-238	-4102	-1906	1980	923	3783	62946	0.06	0.00	40.00	
7	-287	-4341	-1889	1973	947	3717	62934	0.06	0.00	40.00	
8	-131	-3993	-1891	1977	922	3747	62973	0.06	0.00	40.00	
9	-180	-4232	-1874	1970	945	3682	62960	0.06	0.00	40.00	
10	-380	-4313	-1918	1981	933	3802	62910	0.06	0.00	40.00	
11	-395	-4385	-1912	1979	940	3780	62907	0.06	0.00	40.00	
12	-23	-3950	-1868	1971	928	3684	63000	0.06	0.00	40.00	
13	-38	-4021	-1862	1969	935	3662	62996	0.06	0.00	40.00	
14	-238	-4102	-1906	1980	923	3783	62946	0.06	0.00	40.00	
15	-287	-4341	-1889	1973	947	3717	62934	0.06	0.00	40.00	
16	-131	-3993	-1891	1977	922	3747	62973	0.06	0.00	40.00	
17	-180	-4232	-1874	1970	945	3682	62960	0.06	0.00	40.00	

Asse loc. pilastro z nodo ESTERNO: Hjw= 40.0 cm, bj= 30.0 cm, hjc= 50.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb	Vb	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-380	-4313	-1677	1952	409	3732	104850	0.04	0.00	40.00	
3	-395	-4385	-1860	2011	424	4169	104844	0.04	0.00	40.00	
4	-23	-3950	-1688	1955	512	3655	104999	0.03	0.00	40.00	
5	-38	-4021	-1870	2014	527	4090	104993	0.04	0.00	40.00	
6	-238	-4102	-1469	1884	428	3199	104910	0.03	0.00	40.00	
7	-287	-4341	-2076	2081	477	4649	104889	0.04	0.00	40.00	
8	-131	-3993	-1472	1885	459	3175	104954	0.03	0.00	40.00	
9	-180	-4232	-2079	2082	508	4625	104934	0.04	0.00	40.00	
10	-380	-4313	-1677	1952	409	3732	104850	0.04	0.00	40.00	
11	-395	-4385	-1860	2011	424	4169	104844	0.04	0.00	40.00	
12	-23	-3950	-1688	1955	512	3655	104999	0.03	0.00	40.00	
13	-38	-4021	-1870	2014	527	4090	104993	0.04	0.00	40.00	
14	-238	-4102	-1469	1884	428	3199	104910	0.03	0.00	40.00	
15	-287	-4341	-2076	2081	477	4649	104889	0.04	0.00	40.00	
16	-131	-3993	-1472	1885	459	3175	104954	0.03	0.00	40.00	
17	-180	-4232	-2079	2082	508	4625	104934	0.04	0.00	40.00	

CONFRONTO E SINTESI CONCLUSIVE (si assume in ogni caso passo <= 15 cm)

I.R.compr.	Ashy	Ashz	PASSO	Nota
	cmq		cm	
0.06	--	--	15.00	**VERIFICATO**

ASTA NUM. 3 NI 27 NF 25 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 7C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	5881	-1011	834	0	1410	1440	6.28	6.28	9.42	9.42	3	0.19	0.03	0.13	0.00	0.00	24.0
2	0	4546	-778	607	0	1083	1122	6.28	6.28	9.42	9.42	2	0.19	0.02	0.10	0.00	0.00	24.0
3	0	4598	-783	689	0	1127	1128	6.28	6.28	9.42	9.42	2	0.20	0.02	0.10	0.00	0.00	24.0
4	0	4450	-772	593	0	1043	1087	6.28	6.28	9.42	9.42	2	0.19	0.02	0.10	0.00	0.00	24.0
5	0	4502	-777	675	0	1087	1093	6.28	6.28	9.42	9.42	2	0.19	0.02	0.10	0.00	0.00	24.0
6	0	4451	-770	507	0	1018	1103	6.28	6.28	9.42	9.42	2	0.19	0.02	0.10	0.00	0.00	24.0
7	0	4626	-787	780	0	1164	1122	6.28	6.28	9.42	9.42	2	0.20	0.02	0.11	0.00	0.00	24.0
8	0	4422	-768	502	0	1006	1093	6.28	6.28	9.42	9.42	2	0.19	0.02	0.10	0.00	0.00	24.0
9	0	4597	-785	776	0	1152	1112	6.28	6.28	9.42	9.42	2	0.20	0.02	0.11	0.00	0.00	24.0
10	0	4546	-778	607	0	1083	1122	6.28	6.28	9.42	9.42	2	0.19	0.02	0.10	0.00	0.00	24.0
11	0	4598	-783	689	0	1127	1128	6.28	6.28	9.42	9.42	2	0.20	0.02	0.10	0.00	0.00	24.0
12	0	4450	-772	593	0	1043	1087	6.28	6.28	9.42	9.42	2	0.19	0.02	0.10	0.00	0.00	24.0
13	0	4502	-777	675	0	1087	1093	6.28	6.28	9.42	9.42	2	0.19	0.02	0.10	0.00	0.00	24.0
14	0	4451	-770	507	0	1018	1103	6.28	6.28	9.42	9.42	2	0.19	0.02	0.10	0.00	0.00	24.0
15	0	4626	-787	780	0	1164	1122	6.28	6.28	9.42	9.42	2	0.20	0.02	0.11	0.00	0.00	24.0
16	0	4422	-768	502	0	1006	1093	6.28	6.28	9.42	9.42	2	0.19	0.02	0.10	0.00	0.00	24.0
17	0	4597	-785	776	0	1152	1112	6.28	6.28	9.42	9.42	2	0.20	0.02	0.11	0.00	0.00	24.0
18	0	6459	-690	1063	0	1523	1324	6.28	6.28	9.42	9.42	3	0.17	0.03	0.15	0.00	0.00	24.0
19	0	5906	-1271	777	0	1266	1368	6.28	6.28	9.42	9.42	3	0.18	0.03	0.16	0.00	0.00	24.0
20	0	7095	-1007	1512	0	1580	1374	6.28	6.28	9.42	9.42	3	0.18	0.04	0.21	0.00	0.00	24.0
37	0	6513	-509	1129	0	1614	1343	6.28	6.28	9.42	9.42	3	0.18	0.03	0.16	0.00	0.00	24.0
38	0	5592	-1478	652	0	1184	1416	6.28	6.28	9.42	9.42	3	0.18	0.04	0.19	0.00	0.00	24.0
39	0	7574	-1039	1877	0	1709	1427	6.28	6.28	9.42	9.42	3	0.19	0.04	0.26	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	83	6364	-1011	834	0	723	606	6.28	6.28	9.42	9.42	3	0.08	0.03	0.12	0.00	0.00	24.0
2	83	4917	-778	607	0	582	480	6.28	6.28	9.42	9.42	2	0.09	0.02	0.09	0.00	0.00	24.0
3	83	4969	-783	689	0	558	482	6.28	6.28	9.42	9.42	2	0.09	0.02	0.10	0.00	0.00	24.0
4	83	4821	-772	593	0	554	450	6.28	6.28	9.42	9.42	2	0.08	0.02	0.08	0.00	0.00	24.0
5	83	4873	-777	675	0	530	452	6.28	6.28	9.42	9.42	2	0.08	0.02	0.09	0.00	0.00	24.0
6	83	4822	-770	507	0	600	467	6.28	6.28	9.42	9.42	2	0.09	0.02	0.08	0.00	0.00	24.0
7	83	4997	-787	780	0	520	473	6.28	6.28	9.42	9.42	2	0.09	0.02	0.11	0.00	0.00	24.0
8	83	4793	-768	502	0	591	459	6.28	6.28	9.42	9.42	2	0.09	0.02	0.08	0.00	0.00	24.0
9	83	4968	-785	776	0	512	464	6.28	6.28	9.42	9.42	2	0.08	0.02	0.11	0.00	0.00	24.0
10	83	4917	-778	607	0	582	480	6.28	6.28	9.42	9.42	2	0.09	0.02	0.09	0.00	0.00	24.0
11	83	4969	-783	689	0	558	482	6.28	6.28	9.42	9.42	2	0.09	0.02	0.10	0.00	0.00	24.0
12	83	4821	-772	593	0	554	450	6.28	6.28	9.42	9.42	2	0.08	0.02	0.08	0.00	0.00	24.0
13	83	4873	-777	675	0	530	452	6.28	6.28	9.42	9.42	2	0.08	0.02	0.09	0.00	0.00	24.0
14	83	4822	-770	507	0	600	467	6.28	6.28	9.42	9.42	2	0.09	0.02	0.08	0.00	0.00	24.0
15	83	4997	-787	780	0	520	473	6.28	6.28	9.42	9.42	2	0.09	0.02	0.11	0.00	0.00	24.0
16	83	4793	-768	502	0	591	459	6.28	6.28	9.42	9.42	2	0.09	0.02	0.08	0.00	0.00	24.0
17	83	4968	-785	776	0	512	464	6.28	6.28	9.42	9.42	2	0.08	0.02	0.11	0.00	0.00	24.0
18	83	6942	-878	1063	0	646	677	6.28	6.28	9.42	9.42	3	0.09	0.03	0.15	0.00	0.00	24.0
19	83	6388	-1082	777	0	625	397	6.28	6.28	9.42	9.42	3	0.05	0.03	0.12	0.00	0.00	24.0
20	83	7578	-1007	1284	0	427	543	6.28	6.28	9.42	9.42	3	0.07	0.03	0.18	0.00	0.00	24.0
37	83	6996	-823	1129	0	682	793	6.28	6.28	9.42	9.42	3	0.10	0.03	0.16	0.00	0.00	24.0
38	83	6074	-1164	652	0	646	327	6.28	6.28	9.42	9.42	3	0.05	0.03	0.13	0.00	0.00	24.0
39	83	8057	-1039	1496	0	317	570	6.28	6.28	9.42	9.42	3	0.07	0.04	0.21	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	165	6846	-1011	834	0	35	-228	6.28	6.28	9.42	9.42	3	0.03	0.03	0.13	0.00	0.00	24.0
2	165	5288	-778	607	0	81	-162	6.28	6.28	9.42	9.42	2	0.02	0.02	0.10	0.00	0.00	24.0
3	165	5340	-783	689	0	-10	-165	6.28	6.28	9.42	9.42	2	0.02	0.02	0.10	0.00	0.00	24.0
4	165	5192	-772	593	0	64	-186	6.28	6.28	9.42	9.42	2	0.03	0.02	0.10	0.00	0.00	24.0
5	165	5244	-777	675	0	-27	-189	6.28	6.28	9.42	9.42	2	0.03	0.02	0.10	0.00	0.00	24.0
6	165	5194	-770	507	0	182	-168	6.28	6.28	9.42	9.42	2	0.03	0.02	0.08	0.00	0.00	24.0
7	165	5368	-787	780	0	-123	-176	6.28	6.28	9.42	9.42	2	0.03	0.02	0.11	0.00	0.00	24.0
8	165	5164	-768	502	0	177	-175	6.28	6.28	9.42	9.42	2	0.03	0.02	0.08	0.00	0.00	24.0
9	165	5340	-785	776	0	-128	-183	6.28	6.28	9.42	9.42	2	0.03	0.02	0.11	0.00	0.00	24.0
10	165	5288	-778	607	0	81	-162	6.28	6.28	9.42	9.42	2	0.02	0.02	0.10	0.00	0.00	24.0
11	165	5340	-783	689	0	-10	-165	6.28	6.28	9.42	9.42	2	0.02	0.02	0.10	0.00	0.00	24.0
12	165	5192	-772	593	0	64	-186	6.28	6.28	9.42	9.42	2	0.03	0.02	0.10	0.00	0.00	24.0
13	165	5244	-777	675	0	-27	-189	6.28	6.28	9.42	9.42	2	0.03	0.02	0.10	0.00	0.00	24.0
14	165	5194	-770	507	0	182	-168	6.28	6.28	9.42	9.42	2	0.03	0.02	0.08	0.00	0.00	24.0
15	165	5368	-787	780	0	-123	-176	6.28	6.28	9.42	9.42	2	0.03	0.02	0.11	0.00	0.00	24.0
16	165	5164	-768	502	0	177	-175	6.28	6.28	9.42	9.42	2	0.03	0.02	0.08	0.00	0.00	24.0
17	165	5340	-785	776	0	-128	-183	6.28	6.28	9.42	9.42	2	0.03	0.02	0.11	0.00	0.00	24.0
18	165	7424	-1067	1063	0	-231	-125	6.28	6.28	9.42	9.42	3	0.02	0.03	0.15	0.00	0.00	24.0
19	165	6871	-894	777	0	-16	-418	6.28	6.28	9.42	9.42	3	0.05	0.02	0.11	0.00	0.00	24.0
20	165	8060	-1007	1055	0	-538	-288	6.28	6.28	9.42	9.42	3	0.04	0.03	0.15	0.00	0.00	24.0
37	165	7478	-1137	1129	0	-250	-15	6.28	6.28	9.42	9.42	3	0.01	0.03	0.16	0.00	0.00	24.0
38	165	6557	-849	652	0	108	-504	6.28	6.28	9.42	9.42	3	0.06	0.02	0.11	0.00	0.00	24.0
39	165	8540	-1039	1115	0	-760	-287	6.28	6.28	9.42	9.42	3	0.05	0.03	0.16	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	248	7329	-1011	834	0	-653	-1062	6.28	6.28	9.42	9.42	3	0.14	0.03	0.13	0.00	0.00	24.0
2	248	5660	-778	607	0	-420	-804	6.28	6.28	9.42	9.42	2	0.12	0.02	0.10	0.00	0.00	24.0
3	248	5712	-783	689	0	-579	-811	6.28	6.28	9.42	9.42	2	0.13	0.02	0.10	0.00	0.00	24.0
4	248	5564	-772	593	0	-425	-823	6.28	6.28	9.42	9.42	2	0.13	0.02	0.10	0.00	0.00	24.0
5	248	5616	-777	675	0	-584	-829	6.28	6.28	9.42	9.42	2	0.14	0.02	0.10	0.00	0.00	24.0
6	248	5565	-770	507	0	-236	-804	6.28	6.28	9.42	9.42	2	0.12	0.02	0.10	0.00	0.00	24.0
7	248	5740	-787	780	0	-766	-825	6.28	6.28	9.42	9.42	2	0.14	0.02	0.11	0.00	0.00	24.0
8	248	5536	-768	502	0	-238	-809	6.28	6.28	9.42	9.42	2	0.12	0.02	0.10	0.00	0.00	24.0
9	248	5711	-785	776	0	-767	-831	6.28	6.28	9.42	9.42	2	0.14	0.02	0.11	0.00	0.00	24.0
10	248	5660	-778	607	0	-420	-804	6.28	6.28	9.42	9.42	2	0.12	0.02	0.10	0.00	0.00	24.0
11	248	5712	-783	689	0	-579	-811	6.28	6.28	9.42	9.42	2	0.13	0.02	0.10	0.00	0.00	24.0
12	248	5564	-772	593	0	-425	-823	6.28	6.28	9.42	9.42	2	0.13	0.02	0.10	0.00	0.00	24.0
13	248	5616	-777	675	0	-584	-829	6.28	6.28	9.42	9.42	2	0.14	0.02	0.10	0.00	0.00	24.0
14	248	5565	-770	507	0	-236	-804	6.28	6.28	9.42	9.42	2	0.12	0.02	0.10	0.00	0.00	24.0

15	248	5740	-787	780	0	-766	-825	6.28	6.28	9.42	9.42	2	0.14	0.02	0.11	0.00	0.00	24.0
16	248	5536	-768	502	0	-238	-809	6.28	6.28	9.42	9.42	2	0.12	0.02	0.10	0.00	0.00	24.0
17	248	5711	-785	776	0	-767	-831	6.28	6.28	9.42	9.42	2	0.14	0.02	0.11	0.00	0.00	24.0
18	248	7906	-1255	1063	0	-1109	-1083	6.28	6.28	9.42	9.42	3	0.14	0.03	0.15	0.00	0.00	24.0
19	248	7354	-705	777	0	-658	-1077	6.28	6.28	9.42	9.42	3	0.14	0.02	0.11	0.00	0.00	24.0
20	248	8543	-1007	826	0	-1314	-1119	6.28	6.28	9.42	9.42	3	0.15	0.03	0.12	0.00	0.00	24.0
37	248	7961	-1452	1129	0	-1181	-1084	6.28	6.28	9.42	9.42	3	0.14	0.04	0.16	0.00	0.00	24.0
38	248	7040	-535	652	0	-430	-1074	6.28	6.28	9.42	9.42	3	0.14	0.02	0.09	0.00	0.00	24.0
39	248	9022	-1039	735	0	-1524	-1144	6.28	6.28	9.42	9.42	3	0.16	0.03	0.11	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	330	7812	-1011	834	0	-1340	-1896	6.28	6.28	9.42	9.42	3	0.25	0.03	0.13	0.00	0.00	24.0
2	330	6031	-778	607	0	-921	-1446	6.28	6.28	9.42	9.42	2	0.23	0.02	0.10	0.00	0.00	24.0
3	330	6083	-783	689	0	-1148	-1457	6.28	6.28	9.42	9.42	2	0.25	0.02	0.10	0.00	0.00	24.0
4	330	5935	-772	593	0	-914	-1460	6.28	6.28	9.42	9.42	2	0.23	0.02	0.10	0.00	0.00	24.0
5	330	5987	-777	675	0	-1141	-1470	6.28	6.28	9.42	9.42	2	0.25	0.02	0.10	0.00	0.00	24.0
6	330	5936	-770	507	0	-654	-1439	6.28	6.28	9.42	9.42	2	0.22	0.02	0.10	0.00	0.00	24.0
7	330	6111	-787	780	0	-1410	-1474	6.28	6.28	9.42	9.42	2	0.26	0.02	0.11	0.00	0.00	24.0
8	330	5907	-768	502	0	-652	-1443	6.28	6.28	9.42	9.42	2	0.22	0.02	0.10	0.00	0.00	24.0
9	330	6082	-785	776	0	-1407	-1478	6.28	6.28	9.42	9.42	2	0.26	0.02	0.11	0.00	0.00	24.0
10	330	6031	-778	607	0	-921	-1446	6.28	6.28	9.42	9.42	2	0.23	0.02	0.10	0.00	0.00	24.0
11	330	6083	-783	689	0	-1148	-1457	6.28	6.28	9.42	9.42	2	0.25	0.02	0.10	0.00	0.00	24.0
12	330	5935	-772	593	0	-914	-1460	6.28	6.28	9.42	9.42	2	0.23	0.02	0.10	0.00	0.00	24.0
13	330	5987	-777	675	0	-1141	-1470	6.28	6.28	9.42	9.42	2	0.25	0.02	0.10	0.00	0.00	24.0
14	330	5936	-770	507	0	-654	-1439	6.28	6.28	9.42	9.42	2	0.22	0.02	0.10	0.00	0.00	24.0
15	330	6111	-787	780	0	-1410	-1474	6.28	6.28	9.42	9.42	2	0.26	0.02	0.11	0.00	0.00	24.0
16	330	5907	-768	502	0	-652	-1443	6.28	6.28	9.42	9.42	2	0.22	0.02	0.10	0.00	0.00	24.0
17	330	6082	-785	776	0	-1407	-1478	6.28	6.28	9.42	9.42	2	0.26	0.02	0.11	0.00	0.00	24.0
18	330	8389	-1444	1063	0	-1986	-2197	6.28	6.28	9.42	9.42	3	0.29	0.04	0.18	0.00	0.00	24.0
19	330	7836	-517	777	0	-1299	-1581	6.28	6.28	9.42	9.42	3	0.21	0.02	0.11	0.00	0.00	24.0
20	330	9026	-1007	598	0	-1901	-1950	6.28	6.28	9.42	9.42	3	0.26	0.03	0.13	0.00	0.00	24.0
37	330	8444	-1766	1129	0	-2113	-2411	6.28	6.28	9.42	9.42	3	0.32	0.05	0.22	0.00	0.00	24.0
38	330	7522	-220	652	0	-968	-1386	6.28	6.28	9.42	9.42	3	0.18	0.02	0.09	0.00	0.00	24.0
39	330	9505	-1039	354	0	-1973	-2001	6.28	6.28	9.42	9.42	3	0.27	0.03	0.13	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

VERIFICA NODO IN TESTA AL PILASTRO, NODO NUM. 25 NON CONFINATO

(par.7.2.2 NTC2018 "La domanda di resistenza valutata con i criteri della progettazione in capacità può essere assunta non superiore alla domanda di resistenza valutata per il caso di comportamento strutturale non dissipativo.")

PROGETTAZIONE IN CAPACITA'

Asse loc. pilastro y nodo ESTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 45.0 cm, hjc= 20.0 cm
Asse loc. pilastro z nodo ESTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 30.0 cm, hjc= 50.0 cm

FxMin,inf	FxMin,sup	FxMax,sup	FySup	FzSup	Vjbdy	Vjbdz	Vres,y	Vres,z	I.R.compr.	Ashy	Ashz	PASSO	Nota
daN					daN		daN			cmq		cm	
-10000000150474662198766888550 40		1		-0	0	0	17616	17616	63005	105009	0.28	7.07	-- 6.63

VERIFICA DI RESISTENZA CON SOLLECITAZIONI COMPORTAMENTO NON DISSIPATIVO

Asse loc. pilastro y nodo ESTERNO: Hjw= 40.0 cm, bj= 45.0 cm, hjc= 20.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb	Vb	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m			daN			cmq	cm	
2	-0	-0	-692	1303	0	1708	63005	0.03	0.00	40.00	
3	-0	-0	-677	1299	0	1671	63005	0.03	0.00	40.00	
4	-0	-0	-650	1297	0	1606	63005	0.03	0.00	40.00	
5	-0	-0	-635	1293	0	1569	63005	0.02	0.00	40.00	
6	-0	-0	-695	1306	0	1716	63005	0.03	0.00	40.00	
7	-0	-0	-644	1292	0	1591	63005	0.03	0.00	40.00	
8	-0	-0	-683	1304	0	1686	63005	0.03	0.00	40.00	
9	-0	-0	-632	1290	0	1560	63005	0.02	0.00	40.00	
10	-0	-0	-692	1303	0	1708	63005	0.03	0.00	40.00	
11	-0	-0	-677	1299	0	1671	63005	0.03	0.00	40.00	
12	-0	-0	-650	1297	0	1606	63005	0.03	0.00	40.00	
13	-0	-0	-635	1293	0	1569	63005	0.02	0.00	40.00	
14	-0	-0	-695	1306	0	1716	63005	0.03	0.00	40.00	
15	-0	-0	-644	1292	0	1591	63005	0.03	0.00	40.00	
16	-0	-0	-683	1304	0	1686	63005	0.03	0.00	40.00	
17	-0	-0	-632	1290	0	1560	63005	0.02	0.00	40.00	

Asse loc. pilastro z nodo ESTERNO: Hjw= 40.0 cm, bj= 30.0 cm, hjc= 50.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb	Vb	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m			daN			cmq	cm	
2	-0	-0	-1616	1557	0	3990	105009	0.04	0.00	40.00	
3	-0	-0	-1674	1583	0	4133	105009	0.04	0.00	40.00	
4	-0	-0	-1532	1522	0	3783	105009	0.04	0.00	40.00	
5	-0	-0	-1591	1548	0	3928	105009	0.04	0.00	40.00	
6	-0	-0	-1519	1514	0	3751	105009	0.04	0.00	40.00	
7	-0	-0	-1713	1601	0	4230	105009	0.04	0.00	40.00	
8	-0	-0	-1494	1503	0	3689	105009	0.04	0.00	40.00	
9	-0	-0	-1688	1591	0	4168	105009	0.04	0.00	40.00	
10	-0	-0	-1616	1557	0	3990	105009	0.04	0.00	40.00	
11	-0	-0	-1674	1583	0	4133	105009	0.04	0.00	40.00	
12	-0	-0	-1532	1522	0	3783	105009	0.04	0.00	40.00	
13	-0	-0	-1591	1548	0	3928	105009	0.04	0.00	40.00	
14	-0	-0	-1519	1514	0	3751	105009	0.04	0.00	40.00	
15	-0	-0	-1713	1601	0	4230	105009	0.04	0.00	40.00	
16	-0	-0	-1494	1503	0	3689	105009	0.04	0.00	40.00	
17	-0	-0	-1688	1591	0	4168	105009	0.04	0.00	40.00	

CONFRONTO E SINTESI CONCLUSIVE (si assume in ogni caso passo <= 15 cm)

I.R.compr.	Ashy	Ashz	PASSO	Nota
	cmq		cm	
0.04	--	--	15.00	**VERIFICATO**

ASTA NUM. 4 NI 23 NF 27 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 7B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-2013	-204	386	0	530	398	6.28	6.28	9.42	9.42	3	0.05	0.01	0.05	0.00	0.00	24.0
2	0	-1498	-163	264	0	320	315	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
3	0	-1496	-162	332	0	525	312	6.28	6.28	9.42	9.42	2	0.06	0.01	0.05	0.00	0.00	24.0
4	0	-1601	-152	261	0	291	300	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
5	0	-1600	-151	330	0	496	298	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
6	0	-1535	-160	183	0	71	312	6.28	6.28	9.42	9.42	2	0.04	0.00	0.02	0.00	0.00	24.0
7	0	-1531	-157	411	0	754	304	6.28	6.28	9.42	9.42	2	0.07	0.01	0.06	0.00	0.00	24.0
8	0	-1566	-157	182	0	62	308	6.28	6.28	9.42	9.42	2	0.04	0.00	0.02	0.00	0.00	24.0
9	0	-1562	-154	410	0	745	300	6.28	6.28	9.42	9.42	2	0.07	0.01	0.06	0.00	0.00	24.0
10	0	-1498	-163	264	0	320	315	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
11	0	-1496	-162	332	0	525	312	6.28	6.28	9.42	9.42	2	0.06	0.01	0.05	0.00	0.00	24.0
12	0	-1601	-152	261	0	291	300	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
13	0	-1600	-151	330	0	496	298	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
14	0	-1535	-160	183	0	71	312	6.28	6.28	9.42	9.42	2	0.04	0.00	0.02	0.00	0.00	24.0
15	0	-1531	-157	411	0	754	304	6.28	6.28	9.42	9.42	2	0.07	0.01	0.06	0.00	0.00	24.0
16	0	-1566	-157	182	0	62	308	6.28	6.28	9.42	9.42	2	0.04	0.00	0.02	0.00	0.00	24.0
17	0	-1562	-154	410	0	745	300	6.28	6.28	9.42	9.42	2	0.07	0.01	0.06	0.00	0.00	24.0
18	0	-1623	241	458	0	709	31	6.28	6.28	9.42	9.42	3	0.04	0.01	0.06	0.00	0.00	24.0
19	0	-2016	-566	349	0	335	655	6.28	6.28	9.42	9.42	3	0.07	0.01	0.07	0.00	0.00	24.0
20	0	-967	-155	1148	0	1260	324	6.28	6.28	9.42	9.42	3	0.07	0.03	0.16	0.00	0.00	24.0
37	0	-1588	496	489	0	836	-158	6.28	6.28	9.42	9.42	3	0.04	0.01	0.07	0.00	0.00	24.0
38	0	-2243	-848	306	0	212	882	6.28	6.28	9.42	9.42	3	0.10	0.02	0.10	0.00	0.00	24.0
39	0	-495	-164	1639	0	1754	331	6.28	6.28	9.42	9.42	3	0.09	0.04	0.23	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	110	-1370	-204	386	0	106	174	6.28	6.28	9.42	9.42	3	0.02	0.01	0.05	0.00	0.00	24.0
2	110	-1003	-163	264	0	30	136	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
3	110	-1001	-162	332	0	159	134	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
4	110	-1106	-152	261	0	4	133	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
5	110	-1105	-151	330	0	133	132	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
6	110	-1040	-160	183	0	-131	136	6.28	6.28	9.42	9.42	2	0.02	0.00	0.03	0.00	0.00	24.0
7	110	-1036	-157	411	0	302	132	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
8	110	-1071	-157	182	0	-139	135	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
9	110	-1067	-154	410	0	294	131	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
10	110	-1003	-163	264	0	30	136	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
11	110	-1001	-162	332	0	159	134	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
12	110	-1106	-152	261	0	4	133	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
13	110	-1105	-151	330	0	133	132	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
14	110	-1040	-160	183	0	-131	136	6.28	6.28	9.42	9.42	2	0.02	0.00	0.03	0.00	0.00	24.0
15	110	-1036	-157	411	0	302	132	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
16	110	-1071	-157	182	0	-139	135	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
17	110	-1067	-154	410	0	294	131	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
18	110	-980	51	458	0	205	192	6.28	6.28	9.42	9.42	3	0.02	0.01	0.06	0.00	0.00	24.0
19	110	-1373	-376	349	0	-49	137	6.28	6.28	9.42	9.42	3	0.02	0.01	0.05	0.00	0.00	24.0
20	110	-324	-155	843	0	165	154	6.28	6.28	9.42	9.42	3	0.02	0.02	0.12	0.00	0.00	24.0
37	110	-945	180	489	0	298	214	6.28	6.28	9.42	9.42	3	0.03	0.01	0.07	0.00	0.00	24.0
38	110	-1599	-532	306	0	-125	122	6.28	6.28	9.42	9.42	3	0.01	0.01	0.06	0.00	0.00	24.0
39	110	149	-164	1131	0	231	150	6.28	6.28	9.42	9.42	3	0.02	0.03	0.16	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	220	-726	-204	386	0	-318	-50	6.28	6.28	9.42	9.42	3	0.02	0.01	0.05	0.00	0.00	24.0
2	220	-508	-163	264	0	-260	-43	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
3	220	-506	-162	332	0	-206	-44	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
4	220	-611	-152	261	0	-284	-34	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
5	220	-610	-151	330	0	-230	-34	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
6	220	-545	-160	183	0	-332	-40	6.28	6.28	9.42	9.42	2	0.03	0.00	0.03	0.00	0.00	24.0
7	220	-541	-157	411	0	-151	-41	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
8	220	-576	-157	182	0	-339	-37	6.28	6.28	9.42	9.42	2	0.03	0.00	0.03	0.00	0.00	24.0
9	220	-572	-154	410	0	-158	-38	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
10	220	-508	-163	264	0	-260	-43	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
11	220	-506	-162	332	0	-206	-44	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
12	220	-611	-152	261	0	-284	-34	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
13	220	-610	-151	330	0	-230	-34	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
14	220	-545	-160	183	0	-332	-40	6.28	6.28	9.42	9.42	2	0.03	0.00	0.03	0.00	0.00	24.0
15	220	-541	-157	411	0	-151	-41	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
16	220	-576	-157	182	0	-339	-37	6.28	6.28	9.42	9.42	2	0.03	0.00	0.03	0.00	0.00	24.0
17	220	-572	-154	410	0	-158	-38	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
18	220	-336	-139	458	0	-299	144	6.28	6.28	9.42	9.42	3	0.02	0.01	0.06	0.00	0.00	24.0
19	220	-729	-185	349	0	-433	-171	6.28	6.28	9.42	9.42	3	0.03	0.01	0.05	0.00	0.00	24.0
20	220	320	-155	539	0	-595	-17	6.28	6.28	9.42	9.42	3	0.03	0.01	0.08	0.00	0.00	24.0
37	220	-301	-137	489	0	-239	237	6.28	6.28	9.42	9.42	3	0.03	0.01	0.07	0.00	0.00	24.0
38	220	-956	-215	306	0	-461	-288	6.28	6.28	9.42	9.42	3	0.04	0.01	0.04	0.00	0.00	24.0
39	220	792	-164	623	0	-734	-31	6.28	6.28	9.42	9.42	3	0.04	0.01	0.09	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	330	-83	-204	386	0	-743	-274	6.28	6.28	9.42	9.42	3	0.05	0.01	0.05	0.00	0.00	24.0
2	330	-13	-163	264	0	-550	-223	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
3	330	-11	-162	332	0	-571	-222	6.28	6.28	9.42	9.42	2	0.06	0.01	0.05	0.00	0.00	24.0
4	330	-116	-152	261	0	-572	-200	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
5	330	-115	-151	330	0	-592	-200	6.28	6.28	9.42	9.42	2	0.06	0.01	0.05	0.00	0.00	24.0
6	330	-50	-160	183	0	-533	-216	6.28	6.28	9.42	9.42	2	0.05	0.00	0.03	0.00	0.00	24.0
7	330	-46	-157	411	0	-603	-213	6.28	6.28	9.42	9.42	2	0.06	0.01	0.06	0.00	0.00	24.0
8	330	-81	-157	182	0	-540	-209	6.28	6.28	9.42	9.42	2	0.05	0.00	0.03	0.00	0.00	24.0
9	330	-77	-154	410	0	-609	-206	6.28	6.28	9.42	9.42	2	0.06	0.01	0.06	0.00	0.00	24.0
10	330	-13	-163	264	0	-550	-223	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
11	330	-11	-162	332	0	-571	-222	6.28	6.28	9.42	9.42	2	0.06	0.01	0.05	0.00	0.00	24.0
12	330	-116	-152	261	0	-572	-200	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
13	330	-115	-151	330	0	-592	-200	6.28	6.28	9.42	9.42	2	0.06	0.01	0.05	0.00	0.00	24.0
14	330	-50	-160	183	0	-533	-216	6.28	6.28	9.42	9.42	2	0.05	0.00	0.03	0.00	0.00	24.0
15	330	-46	-157	411	0	-603	-213	6.28	6.28	9.42	9.42	2	0.06	0.01	0.06	0.00	0.00	24.0
16	330	-81	-157	182	0	-540	-209	6.28	6.28	9.42	9.42	2	0.05	0.00	0.03	0.00	0.00	24.0
17	330	-77	-154	410	0	-609	-206	6.28	6.28	9.42	9.42	2	0.06	0.01	0.06	0.00	0.00	24.0
18	330	307	-329	458	0	-803	-113	6.28	6.28	9.42	9.42	3	0.04	0.01	0.06	0.00	0.00	24.0
19	330	-86	5	349	0	-816	-271	6.28	6.28	9.42	9.42	3	0.05	0.01	0.05	0.00	0.00	24.0
20	330	963	-155	234	0	-1020	-188	6.28	6.28	9.42	9.42	3	0.06	0.01	0.03	0.00	0.00	24.0

37	330	342	-454	489	0	-777	-88	6.28	6.28	9.42	9.42	3	0.04	0.01	0.07	0.00	0.00	24.0
38	330	-312	102	306	0	-798	-350	6.28	6.28	9.42	9.42	3	0.05	0.01	0.04	0.00	0.00	24.0
39	330	1436	-164	115	0	-1140	-212	6.28	6.28	9.42	9.42	3	0.06	0.00	0.02	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	440	561	-204	386	0	-1167	-498	6.28	6.28	9.42	9.42	3	0.08	0.01	0.05	0.00	0.00	24.0
2	440	482	-163	264	0	-840	-402	6.28	6.28	9.42	9.42	2	0.09	0.01	0.04	0.00	0.00	24.0
3	440	484	-162	332	0	-936	-400	6.28	6.28	9.42	9.42	2	0.10	0.01	0.05	0.00	0.00	24.0
4	440	379	-152	261	0	-859	-367	6.28	6.28	9.42	9.42	2	0.09	0.01	0.04	0.00	0.00	24.0
5	440	380	-151	330	0	-955	-365	6.28	6.28	9.42	9.42	2	0.09	0.01	0.05	0.00	0.00	24.0
6	440	445	-160	183	0	-735	-392	6.28	6.28	9.42	9.42	2	0.08	0.00	0.03	0.00	0.00	24.0
7	440	449	-157	411	0	-1055	-386	6.28	6.28	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
8	440	414	-157	182	0	-740	-381	6.28	6.28	9.42	9.42	2	0.08	0.00	0.03	0.00	0.00	24.0
9	440	418	-154	410	0	-1061	-375	6.28	6.28	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
10	440	482	-163	264	0	-840	-402	6.28	6.28	9.42	9.42	2	0.09	0.01	0.04	0.00	0.00	24.0
11	440	484	-162	332	0	-936	-400	6.28	6.28	9.42	9.42	2	0.10	0.01	0.05	0.00	0.00	24.0
12	440	379	-152	261	0	-859	-367	6.28	6.28	9.42	9.42	2	0.09	0.01	0.04	0.00	0.00	24.0
13	440	380	-151	330	0	-955	-365	6.28	6.28	9.42	9.42	2	0.09	0.01	0.05	0.00	0.00	24.0
14	440	445	-160	183	0	-735	-392	6.28	6.28	9.42	9.42	2	0.08	0.00	0.03	0.00	0.00	24.0
15	440	449	-157	411	0	-1055	-386	6.28	6.28	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
16	440	414	-157	182	0	-740	-381	6.28	6.28	9.42	9.42	2	0.08	0.00	0.03	0.00	0.00	24.0
17	440	418	-154	410	0	-1061	-375	6.28	6.28	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
18	440	951	-519	458	0	-1307	-580	6.28	6.28	9.42	9.42	3	0.09	0.01	0.06	0.00	0.00	24.0
19	440	558	195	349	0	-1200	-161	6.28	6.28	9.42	9.42	3	0.06	0.01	0.05	0.00	0.00	24.0
20	440	1607	-155	-71	0	-1110	-359	6.28	6.28	9.42	9.42	3	0.07	0.00	0.02	0.00	0.00	24.0
37	440	986	-771	489	0	-1315	-761	6.28	6.28	9.42	9.42	3	0.10	0.02	0.08	0.00	0.00	24.0
38	440	331	419	306	0	-1135	-64	6.28	6.28	9.42	9.42	3	0.06	0.01	0.05	0.00	0.00	24.0
39	440	2079	-164	-393	0	-987	-393	6.28	6.28	9.42	9.42	3	0.07	0.01	0.05	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

VERIFICA NODO IN TESTA AL PILASTRO, NODO NUM. 27 NON CONFINATO
(par.7.2.2 NTC2018 "La domanda di resistenza valutata con i criteri della progettazione in capacità può essere assunta non superiore alla domanda di resistenza valutata per il caso di comportamento strutturale non dissipativo.")

PROGETTAZIONE IN CAPACITA'
Asse loc. pilastro y nodo ESTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 45.0 cm, hjc= 20.0 cm
Asse loc. pilastro z nodo ESTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 30.0 cm, hjc= 50.0 cm

FxMin,inf	FxMin,sup	FxMax,sup	FySup	FzSup	Vjbdy	Vjbdz	Vres,y	Vres,z	I.R.compr.	Ashy	Ashz	PASSO	Nota
daN					daN		daN			cmq		cm	
-10000000150474662198766888550 40	1	-0	768	502	16848	17114	63005	105009	0.27	5.96	--	8.12	

VERIFICA DI RESISTENZA CON SOLLECITAZIONI COMPORTAMENTO NON DISSIPATIVO

Asse loc. pilastro y nodo ESTERNO: Hjw= 40.0 cm, bj= 45.0 cm, hjc= 20.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb	Vb	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-0	-0	-1935	2017	778	3999	63005	0.06	0.00	40.00	
3	-0	-0	-1931	2015	783	3985	63005	0.06	0.00	40.00	
4	-0	-0	-2000	2032	772	4167	63005	0.07	0.00	40.00	
5	-0	-0	-1996	2031	777	4152	63005	0.07	0.00	40.00	
6	-0	-0	-1962	2024	770	4074	63005	0.06	0.00	40.00	
7	-0	-0	-1949	2019	787	4026	63005	0.06	0.00	40.00	
8	-0	-0	-1982	2028	768	4126	63005	0.07	0.00	40.00	
9	-0	-0	-1968	2023	785	4075	63005	0.06	0.00	40.00	
10	-0	-0	-1935	2017	778	3999	63005	0.06	0.00	40.00	
11	-0	-0	-1931	2015	783	3985	63005	0.06	0.00	40.00	
12	-0	-0	-2000	2032	772	4167	63005	0.07	0.00	40.00	
13	-0	-0	-1996	2031	777	4152	63005	0.07	0.00	40.00	
14	-0	-0	-1962	2024	770	4074	63005	0.06	0.00	40.00	
15	-0	-0	-1949	2019	787	4026	63005	0.06	0.00	40.00	
16	-0	-0	-1982	2028	768	4126	63005	0.07	0.00	40.00	
17	-0	-0	-1968	2023	785	4075	63005	0.06	0.00	40.00	

Asse loc. pilastro z nodo ESTERNO: Hjw= 40.0 cm, bj= 30.0 cm, hjc= 50.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb	Vb	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-0	-0	-1963	2047	607	4240	105009	0.04	0.00	40.00	
3	-0	-0	-2131	2099	689	4573	105009	0.04	0.00	40.00	
4	-0	-0	-1939	2039	593	4195	105009	0.04	0.00	40.00	
5	-0	-0	-2107	2091	675	4527	105009	0.04	0.00	40.00	
6	-0	-0	-1758	1983	507	3834	105009	0.04	0.00	40.00	
7	-0	-0	-2319	2158	780	4946	105009	0.05	0.00	40.00	
8	-0	-0	-1751	1980	502	3821	105009	0.04	0.00	40.00	
9	-0	-0	-2312	2155	776	4933	105009	0.05	0.00	40.00	
10	-0	-0	-1963	2047	607	4240	105009	0.04	0.00	40.00	
11	-0	-0	-2131	2099	689	4573	105009	0.04	0.00	40.00	
12	-0	-0	-1939	2039	593	4195	105009	0.04	0.00	40.00	
13	-0	-0	-2107	2091	675	4527	105009	0.04	0.00	40.00	
14	-0	-0	-1758	1983	507	3834	105009	0.04	0.00	40.00	
15	-0	-0	-2319	2158	780	4946	105009	0.05	0.00	40.00	
16	-0	-0	-1751	1980	502	3821	105009	0.04	0.00	40.00	
17	-0	-0	-2312	2155	776	4933	105009	0.05	0.00	40.00	

CONFRONTO E SINTESI CONCLUSIVE (si assume in ogni caso passo <= 15 cm)

I.R.compr.	Ashy	Ashz	PASSO	Nota
	cmq		cm	
0.07	--	--	15.00	**VERIFICATO**

ASTA NUM. 5 NI 34 NF 35 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 12C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-10780	-333	239	0	-337	487	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
2	0	-8317	-266	170	0	-332	379	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
3	0	-8328	-265	206	0	-230	378	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
4	0	-8260	-248	162	0	-288	371	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
5	0	-8271	-247	198	0	-186	370	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
6	0	-8284	-261	127	0	-436	378	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
7	0	-8321	-257	244	0	-96	374	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
8	0	-8267	-256	124	0	-422	376	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
9	0	-8303	-252	241	0	-82	371	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
10	0	-8317	-266	170	0	-332	379	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
11	0	-8328	-265	206	0	-230	378	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
12	0	-8260	-248	162	0	-288	371	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
13	0	-8271	-247	198	0	-186	370	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
14	0	-8284	-261	127	0	-436	378	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
15	0	-8321	-257	244	0	-96	374	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
16	0	-8267	-256	124	0	-422	376	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
17	0	-8303	-252	241	0	-82	371	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
18	0	-13820	-618	649	0	-990	999	6.28	6.28	12.57	12.57	3	0.06	0.01	0.06	0.00	0.00	24.0
19	0	-12090	-160	402	0	-544	224	6.28	6.28	12.57	12.57	3	0.02	0.01	0.04	0.00	0.00	24.0
20	0	-12540	-369	1281	0	-5833	574	6.28	6.28	12.57	12.57	3	0.21	0.02	0.12	0.00	0.00	24.0
37	0	-13800	-754	640	0	-1000	1218	6.28	6.28	12.57	12.57	3	0.07	0.01	0.07	0.00	0.00	24.0
38	0	-10900	10	227	0	-258	-74	6.28	6.28	12.57	12.57	3	0.01	0.00	0.02	0.00	0.00	24.0
39	0	-11670	-338	1693	0	-9072	509	6.28	6.28	12.57	12.57	3	0.33	0.03	0.16	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	83	-10137	-333	239	0	-534	212	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
2	83	-7822	-266	170	0	-473	160	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
3	83	-7833	-265	206	0	-400	160	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
4	83	-7765	-248	162	0	-422	167	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
5	83	-7776	-247	198	0	-349	166	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
6	83	-7789	-261	127	0	-540	163	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
7	83	-7826	-257	244	0	-297	162	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
8	83	-7772	-256	124	0	-525	165	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
9	83	-7808	-252	241	0	-281	164	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
10	83	-7822	-266	170	0	-473	160	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
11	83	-7833	-265	206	0	-400	160	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
12	83	-7765	-248	162	0	-422	167	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
13	83	-7776	-247	198	0	-349	166	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
14	83	-7789	-261	127	0	-540	163	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
15	83	-7826	-257	244	0	-297	162	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
16	83	-7772	-256	124	0	-525	165	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
17	83	-7808	-252	241	0	-281	164	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
18	83	-13178	-618	649	0	-1525	489	6.28	6.28	12.57	12.57	3	0.06	0.01	0.06	0.00	0.00	24.0
19	83	-11446	-160	402	0	-876	92	6.28	6.28	12.57	12.57	3	0.03	0.01	0.04	0.00	0.00	24.0
20	83	-11898	-369	828	0	-6703	270	6.28	6.28	12.57	12.57	3	0.24	0.01	0.08	0.00	0.00	24.0
37	83	-13158	-754	640	0	-1527	596	6.28	6.28	12.57	12.57	3	0.06	0.01	0.06	0.00	0.00	24.0
38	83	-10258	10	227	0	-445	-66	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
39	83	-11026	-338	938	0	-10157	230	6.28	6.28	12.57	12.57	3	0.36	0.02	0.09	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	165	-9494	-333	239	0	-731	-63	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
2	165	-7327	-266	170	0	-613	-60	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
3	165	-7338	-265	206	0	-569	-59	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
4	165	-7270	-248	162	0	-556	-38	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
5	165	-7281	-247	198	0	-512	-37	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
6	165	-7294	-261	127	0	-644	-53	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
7	165	-7331	-257	244	0	-498	-51	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
8	165	-7277	-256	124	0	-627	-46	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
9	165	-7313	-252	241	0	-481	-44	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
10	165	-7327	-266	170	0	-613	-60	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
11	165	-7338	-265	206	0	-569	-59	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
12	165	-7270	-248	162	0	-556	-38	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
13	165	-7281	-247	198	0	-512	-37	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
14	165	-7294	-261	127	0	-644	-53	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
15	165	-7331	-257	244	0	-498	-51	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
16	165	-7277	-256	124	0	-627	-46	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
17	165	-7313	-252	241	0	-481	-44	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
18	165	-12535	-618	649	0	-2061	-21	6.28	6.28	12.57	12.57	3	0.07	0.01	0.06	0.00	0.00	24.0
19	165	-10802	-160	402	0	-1208	-40	6.28	6.28	12.57	12.57	3	0.04	0.01	0.04	0.00	0.00	24.0
20	165	-11256	-369	375	0	-7200	-34	6.28	6.28	12.57	12.57	3	0.26	0.01	0.04	0.00	0.00	24.0
37	165	-12515	-754	640	0	-2055	-26	6.28	6.28	12.57	12.57	3	0.07	0.01	0.06	0.00	0.00	24.0
38	165	-9615	10	227	0	-633	-58	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
39	165	-10382	-338	183	0	-10620	-49	6.28	6.28	12.57	12.57	3	0.38	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	248	-8851	-333	239	0	-929	-338	6.28	6.28	12.57	12.57	3	0.04	0.01	0.03	0.00	0.00	24.0
2	248	-6832	-266	170	0	-754	-279	6.28	6.28	12.57	12.57	2	0.05	0.00	0.02	0.00	0.00	24.0
3	248	-6843	-265	206	0	-739	-277	6.28	6.28	12.57	12.57	2	0.05	0.00	0.02	0.00	0.00	24.0
4	248	-6775	-248	162	0	-690	-242	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
5	248	-6786	-247	198	0	-675	-241	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
6	248	-6799	-261	127	0	-749	-268	6.28	6.28	12.57	12.57	2	0.05	0.00	0.02	0.00	0.00	24.0
7	248	-6836	-257	244	0	-699	-263	6.28	6.28	12.57	12.57	2	0.05	0.00	0.03	0.00	0.00	24.0
8	248	-6782	-256	124	0	-730	-257	6.28	6.28	12.57	12.57	2	0.05	0.00	0.02	0.00	0.00	24.0
9	248	-6818	-252	241	0	-680	-252	6.28	6.28	12.57	12.57	2	0.04	0.00	0.03	0.00	0.00	24.0
10	248	-6832	-266	170	0	-754	-279	6.28	6.28	12.57	12.57	2	0.05	0.00	0.02	0.00	0.00	24.0
11	248	-6843	-265	206	0	-739	-277	6.28	6.28	12.57	12.57	2	0.05	0.00	0.02	0.00	0.00	24.0
12	248	-6775	-248	162	0	-690	-242	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
13	248	-6786	-247	198	0	-675	-241	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
14	248	-6799	-261	127	0	-749	-268	6.28	6.28	12.57	12.57	2	0.05	0.00	0.02	0.00	0.00	24.0
15	248	-6836	-257	244	0	-699	-263	6.28	6.28	12.57	12.57	2	0.05	0.00	0.03	0.00	0.00	24.0
16	248	-6782	-256	124	0	-730	-257	6.28	6.28	12.57	12.57	2	0.05	0.00	0.02	0.00	0.00	24.0
17	248	-6818	-252	241	0	-680	-252	6.28	6.28	12.57	12.57	2	0.04	0.00	0.03	0.00	0.00	24.0
18	248	-11892	-618	649	0	-2596	-531	6.28	6.28	12.57	12.57	3	0.10	0.01	0.06	0.00	0.00	24.0
19	248	-10157	-160	402	0	-1539	-171	6.28	6.28	12.57	12.57	3	0.06	0.01	0.04	0.00	0.00	24.0
20	248	-10613	-369	-78	0	-7322	-338	6.28	6.28	12.57	12.57	3	0.27	0.01	0.03	0.00	0.00	24.0
37	248	-11872	-754	640	0	-2582	-648	6.28	6.28	12.57	12.57	3	0.10	0.01	0.06	0.00	0.00	24.0
38	248	-8972	10	227	0	-820	-50	6.28	6.28	12.57	12.57	3	0.03	0.00	0.02	0.00	0.00	24.0
39	248	-9737	-338	-572	0	-10459	-328	6.28	6.28	12.57	12.57	3	0.38	0.01	0.06	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	330	-8208	-333	239	0	-1126	-613	6.28	6.28	12.57	12.57	3	0.05	0.01	0.03	0.00	0.00	24.0
2	330	-6337	-266	170	0	-894	-498	6.28	6.28	12.57	12.57	2	0.07	0.00	0.02	0.00	0.00	24.0
3	330	-6348	-265	206	0	-908	-496	6.28	6.28	12.57	12.57	2	0.07	0.00	0.02	0.00	0.00	24.0
4	330	-6280	-248	162	0	-824	-447	6.28	6.28	12.57	12.57	2	0.06	0.00	0.02	0.00	0.00	24.0
5	330	-6291	-247	198	0	-838	-444	6.28	6.28	12.57	12.57	2	0.06	0.00	0.02	0.00	0.00	24.0
6	330	-6304	-261	127	0	-853	-484	6.28	6.28	12.57	12.57	2	0.06	0.00	0.02	0.00	0.00	24.0
7	330	-6341	-257	244	0	-900	-475	6.28	6.28	12.57	12.57	2	0.06	0.00	0.03	0.00	0.00	24.0
8	330	-6287	-256	124	0	-832	-468	6.28	6.28	12.57	12.57	2	0.06	0.00	0.02	0.00	0.00	24.0
9	330	-6323	-252	241	0	-879	-459	6.28	6.28	12.57	12.57	2	0.06	0.00	0.03	0.00	0.00	24.0
10	330	-6337	-266	170	0	-894	-498	6.28	6.28	12.57	12.57	2	0.07	0.00	0.02	0.00	0.00	24.0
11	330	-6348	-265	206	0	-908	-496	6.28	6.28	12.57	12.57	2	0.07	0.00	0.02	0.00	0.00	24.0
12	330	-6280	-248	162	0	-824	-447	6.28	6.28	12.57	12.57	2	0.06	0.00	0.02	0.00	0.00	24.0
13	330	-6291	-247	198	0	-838	-444	6.28	6.28	12.57	12.57	2	0.06	0.00	0.02	0.00	0.00	24.0
14	330	-6304	-261	127	0	-853	-484	6.28	6.28	12.57	12.57	2	0.06	0.00	0.02	0.00	0.00	24.0
15	330	-6341	-257	244	0	-900	-475	6.28	6.28	12.57	12.57	2	0.06	0.00	0.03	0.00	0.00	24.0
16	330	-6287	-256	124	0	-832	-468	6.28	6.28	12.57	12.57	2	0.06	0.00	0.02	0.00	0.00	24.0
17	330	-6323	-252	241	0	-879	-459	6.28	6.28	12.57	12.57	2	0.06	0.00	0.03	0.00	0.00	24.0
18	330	-11250	-618	649	0	-3132	-1041	6.28	6.28	12.57	12.57	3	0.13	0.01	0.06	0.00	0.00	24.0
19	330	-9513	-160	402	0	-1871	-303	6.28	6.28	12.57	12.57	3	0.07	0.01	0.04	0.00	0.00	24.0
20	330	-9971	-369	-531	0	-7071	-642	6.28	6.28	12.57	12.57	3	0.26	0.01	0.05	0.00	0.00	24.0
37	330	-11230	-754	640	0	-3110	-1270	6.28	6.28	12.57	12.57	3	0.13	0.01	0.06	0.00	0.00	24.0
38	330	-8330	10	227	0	-1008	-41	6.28	6.28	12.57	12.57	3	0.04	0.00	0.02	0.00	0.00	24.0
39	330	-9093	-338	-1327	0	-9676	-607	6.28	6.28	12.57	12.57	3	0.36	0.02	0.13	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

VERIFICA NODO IN TESTA AL PILASTRO, NODO NUM. 35 NON CONFINATO

(par.7.2.2 NTC2018 "La domanda di resistenza valutata con i criteri della progettazione in capacità può essere assunta non superiore alla domanda di resistenza valutata per il caso di comportamento strutturale non dissipativo.")

PROGETTAZIONE IN CAPACITA'

Asse loc. pilastro y nodo INTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 50.0 cm, hjc= 30.0 cm
Asse loc. pilastro z nodo: --

FxMin,inf	FxMin,sup	FxMax,sup	FySup	FzSup	Vjbdy	Vjbdz	Vres,y	Vres,z	I.R.compr.	Ashy	Ashz	PASSO	Nota
daN					daN		daN			cmq		cm	
-6280	-3514	-3613	759	282	34474	--	130127	--	0.26	8.78	--	5.17	

VERIFICA DI RESISTENZA CON SOLLECITAZIONI COMPORTAMENTO NON DISSIPATIVO

Asse loc. pilastro y nodo INTERNO: Hjw= 40.0 cm, bj= 50.0 cm, hjc= 30.0 cm, db1= 45.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb,1	Mb,2	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-3607	-6337	-1529	-902	847	702	130129	0.01	0.00	40.00	
3	-3613	-6348	-1537	-904	850	713	130127	0.01	0.00	40.00	
4	-3514	-6280	-1522	-983	759	571	130158	0.00	0.00	40.00	
5	-3520	-6291	-1530	-986	762	582	130157	0.00	0.00	40.00	
6	-3567	-6304	-1517	-928	812	643	130142	0.00	0.00	40.00	
7	-3588	-6341	-1544	-935	823	680	130135	0.01	0.00	40.00	
8	-3539	-6287	-1515	-952	786	604	130151	0.00	0.00	40.00	
9	-3560	-6323	-1542	-960	797	641	130144	0.00	0.00	40.00	
10	-3607	-6337	-1529	-902	847	702	130129	0.01	0.00	40.00	
11	-3613	-6348	-1537	-904	850	713	130127	0.01	0.00	40.00	
12	-3514	-6280	-1522	-983	759	571	130158	0.00	0.00	40.00	
13	-3520	-6291	-1530	-986	762	582	130157	0.00	0.00	40.00	
14	-3567	-6304	-1517	-928	812	643	130142	0.00	0.00	40.00	
15	-3588	-6341	-1544	-935	823	680	130135	0.01	0.00	40.00	
16	-3539	-6287	-1515	-952	786	604	130151	0.00	0.00	40.00	
17	-3560	-6323	-1542	-960	797	641	130144	0.00	0.00	40.00	

CONFRONTO E SINTESI CONCLUSIVE (si assume in ogni caso passo <= 15 cm)

I.R.compr.	Ashy	Ashz	PASSO	Nota
	cmq		cm	
0.01	--	--	15.00	**VERIFICATO**

ASTA NUM. 6 NI 36 NF 37 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 17C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-10930	-289	303	0	-741	306	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
2	0	-8410	-235	223	0	-618	246	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
3	0	-8456	-236	244	0	-512	246	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
4	0	-8360	-209	222	0	-628	225	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
5	0	-8405	-209	243	0	-521	226	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
6	0	-8340	-226	198	0	-746	238	6.28	6.28	12.57	12.57	2	0.05	0.00	0.02	0.00	0.00	24.0
7	0	-8490	-227	268	0	-391	239	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
8	0	-8325	-218	198	0	-749	232	6.28	6.28	12.57	12.57	2	0.05	0.00	0.02	0.00	0.00	24.0
9	0	-8475	-219	268	0	-394	233	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
10	0	-8410	-235	223	0	-618	246	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
11	0	-8456	-236	244	0	-512	246	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
12	0	-8360	-209	222	0	-628	225	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
13	0	-8405	-209	243	0	-521	226	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
14	0	-8340	-226	198	0	-746	238	6.28	6.28	12.57	12.57	2	0.05	0.00	0.02	0.00	0.00	24.0
15	0	-8490	-227	268	0	-391	239	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
16	0	-8325	-218	198	0	-749	232	6.28	6.28	12.57	12.57	2	0.05	0.00	0.02	0.00	0.00	24.0
17	0	-8475	-219	268	0	-394	233	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
18	0	-14320	-559	710	0	-1636	735	6.28	6.28	12.57	12.57	3	0.07	0.01	0.07	0.00	0.00	24.0
19	0	-13140	-98	598	0	-1504	4	6.28	6.28	12.57	12.57	3	0.05	0.01	0.06	0.00	0.00	24.0
20	0	-13390	-324	1662	0	-7429	361	6.28	6.28	12.57	12.57	3	0.26	0.03	0.16	0.00	0.00	24.0
37	0	-13840	-700	635	0	-1412	957	6.28	6.28	12.57	12.57	3	0.07	0.01	0.06	0.00	0.00	24.0
38	0	-11870	69	446	0	-1192	-261	6.28	6.28	12.57	12.57	3	0.05	0.01	0.04	0.00	0.00	24.0
39	0	-12290	-308	2221	0	-11070	334	6.28	6.28	12.57	12.57	3	0.39	0.04	0.21	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	83	-10286	-289	303	0	-991	68	6.28	6.28	12.57	12.57	3	0.04	0.01	0.03	0.00	0.00	24.0
2	83	-7915	-235	223	0	-802	52	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
3	83	-7961	-236	244	0	-713	52	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
4	83	-7865	-209	222	0	-811	53	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
5	83	-7910	-209	243	0	-722	53	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
6	83	-7845	-226	198	0	-909	52	6.28	6.28	12.57	12.57	2	0.05	0.00	0.02	0.00	0.00	24.0
7	83	-7995	-227	268	0	-612	52	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
8	83	-7830	-218	198	0	-912	52	6.28	6.28	12.57	12.57	2	0.05	0.00	0.02	0.00	0.00	24.0
9	83	-7980	-219	268	0	-615	53	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
10	83	-7915	-235	223	0	-802	52	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
11	83	-7961	-236	244	0	-713	52	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
12	83	-7865	-209	222	0	-811	53	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
13	83	-7910	-209	243	0	-722	53	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
14	83	-7845	-226	198	0	-909	52	6.28	6.28	12.57	12.57	2	0.05	0.00	0.02	0.00	0.00	24.0
15	83	-7995	-227	268	0	-612	52	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
16	83	-7830	-218	198	0	-912	52	6.28	6.28	12.57	12.57	2	0.05	0.00	0.02	0.00	0.00	24.0
17	83	-7980	-219	268	0	-615	53	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
18	83	-13678	-559	710	0	-2222	274	6.28	6.28	12.57	12.57	3	0.08	0.01	0.07	0.00	0.00	24.0
19	83	-12498	-98	598	0	-1997	-77	6.28	6.28	12.57	12.57	3	0.07	0.01	0.06	0.00	0.00	24.0
20	83	-12748	-324	1209	0	-8614	94	6.28	6.28	12.57	12.57	3	0.31	0.02	0.12	0.00	0.00	24.0
37	83	-13195	-700	635	0	-1936	380	6.28	6.28	12.57	12.57	3	0.07	0.01	0.06	0.00	0.00	24.0
38	83	-11226	69	446	0	-1560	-205	6.28	6.28	12.57	12.57	3	0.06	0.01	0.04	0.00	0.00	24.0
39	83	-11648	-308	1466	0	-12589	80	6.28	6.28	12.57	12.57	3	0.45	0.03	0.14	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	165	-9643	-289	303	0	-1241	-170	6.28	6.28	12.57	12.57	3	0.05	0.01	0.03	0.00	0.00	24.0
2	165	-7420	-235	223	0	-986	-143	6.28	6.28	12.57	12.57	2	0.06	0.00	0.02	0.00	0.00	24.0
3	165	-7466	-236	244	0	-914	-143	6.28	6.28	12.57	12.57	2	0.05	0.00	0.03	0.00	0.00	24.0
4	165	-7370	-209	222	0	-995	-119	6.28	6.28	12.57	12.57	2	0.06	0.00	0.02	0.00	0.00	24.0
5	165	-7415	-209	243	0	-923	-119	6.28	6.28	12.57	12.57	2	0.05	0.00	0.03	0.00	0.00	24.0
6	165	-7350	-226	198	0	-1073	-134	6.28	6.28	12.57	12.57	2	0.06	0.00	0.02	0.00	0.00	24.0
7	165	-7500	-227	268	0	-833	-135	6.28	6.28	12.57	12.57	2	0.05	0.00	0.03	0.00	0.00	24.0
8	165	-7335	-218	198	0	-1075	-127	6.28	6.28	12.57	12.57	2	0.06	0.00	0.02	0.00	0.00	24.0
9	165	-7485	-219	268	0	-836	-128	6.28	6.28	12.57	12.57	2	0.05	0.00	0.03	0.00	0.00	24.0
10	165	-7420	-235	223	0	-986	-143	6.28	6.28	12.57	12.57	2	0.06	0.00	0.02	0.00	0.00	24.0
11	165	-7466	-236	244	0	-914	-143	6.28	6.28	12.57	12.57	2	0.05	0.00	0.03	0.00	0.00	24.0
12	165	-7370	-209	222	0	-995	-119	6.28	6.28	12.57	12.57	2	0.06	0.00	0.02	0.00	0.00	24.0
13	165	-7415	-209	243	0	-923	-119	6.28	6.28	12.57	12.57	2	0.05	0.00	0.03	0.00	0.00	24.0
14	165	-7350	-226	198	0	-1073	-134	6.28	6.28	12.57	12.57	2	0.06	0.00	0.02	0.00	0.00	24.0
15	165	-7500	-227	268	0	-833	-135	6.28	6.28	12.57	12.57	2	0.05	0.00	0.03	0.00	0.00	24.0
16	165	-7335	-218	198	0	-1075	-127	6.28	6.28	12.57	12.57	2	0.06	0.00	0.02	0.00	0.00	24.0
17	165	-7485	-219	268	0	-836	-128	6.28	6.28	12.57	12.57	2	0.05	0.00	0.03	0.00	0.00	24.0
18	165	-13035	-559	710	0	-2808	-188	6.28	6.28	12.57	12.57	3	0.10	0.01	0.07	0.00	0.00	24.0
19	165	-11855	-98	598	0	-2490	-158	6.28	6.28	12.57	12.57	3	0.09	0.01	0.06	0.00	0.00	24.0
20	165	-12105	-324	756	0	-9425	-173	6.28	6.28	12.57	12.57	3	0.34	0.01	0.07	0.00	0.00	24.0
37	165	-12550	-700	635	0	-2459	-198	6.28	6.28	12.57	12.57	3	0.09	0.01	0.06	0.00	0.00	24.0
38	165	-10582	69	446	0	-1928	-148	6.28	6.28	12.57	12.57	3	0.07	0.01	0.04	0.00	0.00	24.0
39	165	-11005	-308	711	0	-13486	-174	6.28	6.28	12.57	12.57	3	0.48	0.01	0.07	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	248	-9000	-289	303	0	-1491	-408	6.28	6.28	12.57	12.57	3	0.06	0.01	0.03	0.00	0.00	24.0
2	248	-6925	-235	223	0	-1170	-337	6.28	6.28	12.57	12.57	2	0.07	0.00	0.02	0.00	0.00	24.0
3	248	-6971	-236	244	0	-1115	-337	6.28	6.28	12.57	12.57	2	0.07	0.00	0.03	0.00	0.00	24.0
4	248	-6875	-209	222	0	-1178	-291	6.28	6.28	12.57	12.57	2	0.07	0.00	0.02	0.00	0.00	24.0
5	248	-6920	-209	243	0	-1123	-292	6.28	6.28	12.57	12.57	2	0.07	0.00	0.03	0.00	0.00	24.0
6	248	-6855	-226	198	0	-1236	-320	6.28	6.28	12.57	12.57	2	0.08	0.00	0.02	0.00	0.00	24.0
7	248	-7005	-227	268	0	-1055	-322	6.28	6.28	12.57	12.57	2	0.07	0.00	0.03	0.00	0.00	24.0
8	248	-6840	-218	198	0	-1239	-307	6.28	6.28	12.57	12.57	2	0.08	0.00	0.02	0.00	0.00	24.0
9	248	-6990	-219	268	0	-1057	-308	6.28	6.28	12.57	12.57	2	0.07	0.00	0.03	0.00	0.00	24.0
10	248	-6925	-235	223	0	-1170	-337	6.28	6.28	12.57	12.57	2	0.07	0.00	0.02	0.00	0.00	24.0
11	248	-6971	-236	244	0	-1115	-337	6.28	6.28	12.57	12.57	2	0.07	0.00	0.03	0.00	0.00	24.0
12	248	-6875	-209	222	0	-1178	-291	6.28	6.28	12.57	12.57	2	0.07	0.00	0.02	0.00	0.00	24.0
13	248	-6920	-209	243	0	-1123	-292	6.28	6.28	12.57	12.57	2	0.07	0.00	0.03	0.00	0.00	24.0
14	248	-6855	-226	198	0	-1236	-320	6.28	6.28	12.57	12.57	2	0.08	0.00	0.02	0.00	0.00	24.0
15	248	-7005	-227	268	0	-1055	-322	6.28	6.28	12.57	12.57	2	0.07	0.00	0.03	0.00	0.00	24.0
16	248	-6840	-218	198	0	-1239	-307	6.28	6.28	12.57	12.57	2	0.08	0.00	0.02	0.00	0.00	24.0
17	248	-6990	-219	268	0	-1057	-308	6.28	6.28	12.57	12.57	2	0.07	0.00	0.03	0.00	0.00	24.0
18	248	-12392	-559	710	0	-3395	-649	6.28	6.28	12.57	12.57	3	0.13	0.01	0.07	0.00	0.00	24.0
19	248	-11212	-98	598	0	-2983	-239	6.28	6.28	12.57	12.57	3	0.11	0.01	0.06	0.00	0.00	24.0
20	248	-11462	-324	303	0	-9862	-440	6.28	6.28	12.57	12.57	3	0.35	0.01	0.03	0.00	0.00	24.0
37	248	-11905	-700	635	0	-2982	-775	6.28	6.28	12.57	12.57	3	0.12	0.01	0.06	0.00	0.00	24.0
38	248	-9939	69	446	0	-2297	-91	6.28	6.28	12.57	12.57	3	0.08	0.01	0.04	0.00	0.00	24.0
39	248	-10362	-308	-44	0	-13759	-427	6.28	6.28	12.57	12.57	3	0.50	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	330	-8356	-289	303	0	-1741	-647	6.28	6.28	12.57	12.57	3	0.07	0.01	0.03	0.00	0.00	24.0
2	330	-6430	-235	223	0	-1354	-531	6.28	6.28	12.57	12.57	2	0.09	0.00	0.02	0.00	0.00	24.0
3	330	-6476	-236	244	0	-1316	-531	6.28	6.28	12.57	12.57	2	0.09	0.00	0.03	0.00	0.00	24.0
4	330	-6380	-209	222	0	-1362	-463	6.28	6.28	12.57	12.57	2	0.09	0.00	0.02	0.00	0.00	24.0
5	330	-6425	-209	243	0	-1324	-464	6.28	6.28	12.57	12.57	2	0.09	0.00	0.03	0.00	0.00	24.0
6	330	-6360	-226	198	0	-1400	-506	6.28	6.28	12.57	12.57	2	0.09	0.00	0.02	0.00	0.00	24.0
7	330	-6510	-227	268	0	-1276	-509	6.28	6.28	12.57	12.57	2	0.09	0.00	0.03	0.00	0.00	24.0
8	330	-6345	-218	198	0	-1402	-486	6.28	6.28	12.57	12.57	2	0.09	0.00	0.02	0.00	0.00	24.0
9	330	-6495	-219	268	0	-1278	-488	6.28	6.28	12.57	12.57	2	0.08	0.00	0.03	0.00	0.00	24.0
10	330	-6430	-235	223	0	-1354	-531	6.28	6.28	12.57	12.57	2	0.09	0.00	0.02	0.00	0.00	24.0
11	330	-6476	-236	244	0	-1316	-531	6.28	6.28	12.57	12.57	2	0.09	0.00	0.03	0.00	0.00	24.0
12	330	-6380	-209	222	0	-1362	-463	6.28	6.28	12.57	12.57	2	0.09	0.00	0.02	0.00	0.00	24.0
13	330	-6425	-209	243	0	-1324	-464	6.28	6.28	12.57	12.57	2	0.09	0.00	0.03	0.00	0.00	24.0
14	330	-6360	-226	198	0	-1400	-506	6.28	6.28	12.57	12.57	2	0.09	0.00	0.02	0.00	0.00	24.0
15	330	-6510	-227	268	0	-1276	-509	6.28	6.28	12.57	12.57	2	0.09	0.00	0.03	0.00	0.00	24.0
16	330	-6345	-218	198	0	-1402	-486	6.28	6.28	12.57	12.57	2	0.09	0.00	0.02	0.00	0.00	24.0
17	330	-6495	-219	268	0	-1278	-488	6.28	6.28	12.57	12.57	2	0.08	0.00	0.03	0.00	0.00	24.0
18	330	-11750	-559	710	0	-3981	-1110	6.28	6.28	12.57	12.57	3	0.16	0.01	0.07	0.00	0.00	24.0
19	330	-10570	-98	598	0	-3476	-319	6.28	6.28	12.57	12.57	3	0.13	0.01	0.06	0.00	0.00	24.0
20	330	-10820	-324	-150	0	-9925	-707	6.28	6.28	12.57	12.57	3	0.36	0.01	0.03	0.00	0.00	24.0
37	330	-11260	-700	635	0	-3506	-1353	6.28	6.28	12.57	12.57	3	0.15	0.01	0.06	0.00	0.00	24.0
38	330	-9295	69	446	0	-2665	-35	6.28	6.28	12.57	12.57	3	0.10	0.01	0.04	0.00	0.00	24.0
39	330	-9720	-308	-800	0	-13410	-681	6.28	6.28	12.57	12.57	3	0.49	0.01	0.08	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

VERIFICA NODO IN TESTA AL PILASTRO, NODO NUM. 37 NON CONFINATO

(par.7.2.2 NTC2018 "La domanda di resistenza valutata con i criteri della progettazione in capacità può essere assunta non superiore alla domanda di resistenza valutata per il caso di comportamento strutturale non dissipativo.")

PROGETTAZIONE IN CAPACITA'
Asse loc. pilastro y nodo INTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 50.0 cm, hjc= 30.0 cm
Asse loc. pilastro z nodo: --

FxMin,inf	FxMin,sup	FxMax,sup	FySup	FzSup	Vjbdy	Vjbdz	Vres,y	Vres,z	I.R.compr.	Ashy	Ashz	PASSO	Nota
daN					daN		daN			cmq		cm	
-6345	-3446	-3617	81	187	35152	--	130126	--	0.27	8.78	--	5.17	

VERIFICA DI RESISTENZA CON SOLLECITAZIONI COMPORTAMENTO NON DISSIPATIVO

Asse loc. pilastro y nodo INTERNO: Hjw= 40.0 cm, bj= 50.0 cm, hjc= 30.0 cm, db1= 45.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb,1	Mb,2	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-3534	-6430	-1179	-1417	236	351	130152	0.00	0.00	40.00	
3	-3581	-6476	-1179	-1416	237	348	130137	0.00	0.00	40.00	
4	-3482	-6380	-1093	-1508	81	944	130169	0.01	0.00	40.00	
5	-3528	-6425	-1092	-1506	81	941	130154	0.01	0.00	40.00	
6	-3462	-6360	-1150	-1451	182	562	130175	0.00	0.00	40.00	
7	-3617	-6510	-1147	-1446	183	555	130126	0.00	0.00	40.00	
8	-3446	-6345	-1124	-1478	135	739	130180	0.01	0.00	40.00	
9	-3601	-6495	-1122	-1473	136	731	130131	0.01	0.00	40.00	
10	-3534	-6430	-1179	-1417	236	351	130152	0.00	0.00	40.00	
11	-3581	-6476	-1179	-1416	237	348	130137	0.00	0.00	40.00	
12	-3482	-6380	-1093	-1508	81	944	130169	0.01	0.00	40.00	
13	-3528	-6425	-1092	-1506	81	941	130154	0.01	0.00	40.00	
14	-3462	-6360	-1150	-1451	182	562	130175	0.00	0.00	40.00	
15	-3617	-6510	-1147	-1446	183	555	130126	0.00	0.00	40.00	
16	-3446	-6345	-1124	-1478	135	739	130180	0.01	0.00	40.00	
17	-3601	-6495	-1122	-1473	136	731	130131	0.01	0.00	40.00	

CONFRONTO E SINTESI CONCLUSIVE (si assume in ogni caso passo <= 15 cm)

I.R.compr.	Ashy	Ashz	PASSO	Nota
	cmq		cm	
0.01	--	--	15.00	**VERIFICATO**

ASTA NUM. 7 NI 38 NF 39 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 22C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-13170	63	248	0	-147	-102	6.28	6.28	12.57	12.57	3	0.01	0.00	0.02	0.00	0.00	24.0
2	0	-10120	35	170	0	-128	-68	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
3	0	-10160	31	201	0	3	-64	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
4	0	-10100	65	180	0	-229	-92	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
5	0	-10140	62	211	0	-98	-89	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
6	0	-10070	50	138	0	-317	-81	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
7	0	-10190	37	240	0	121	-69	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
8	0	-10060	59	141	0	-347	-88	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
9	0	-10190	47	243	0	91	-76	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
10	0	-10120	35	170	0	-128	-68	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
11	0	-10160	31	201	0	3	-64	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
12	0	-10100	65	180	0	-229	-92	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
13	0	-10140	62	211	0	-98	-89	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
14	0	-10070	50	138	0	-317	-81	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
15	0	-10190	37	240	0	121	-69	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
16	0	-10060	59	141	0	-347	-88	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
17	0	-10190	47	243	0	91	-76	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
18	0	-15710	-239	470	0	-199	323	6.28	6.28	12.57	12.57	3	0.02	0.01	0.04	0.00	0.00	24.0
19	0	-16520	246	632	0	-640	-455	6.28	6.28	12.57	12.57	3	0.03	0.01	0.06	0.00	0.00	24.0
20	0	-15740	-15	1217	0	-5425	-41	6.28	6.28	12.57	12.57	3	0.19	0.02	0.11	0.00	0.00	24.0
37	0	-14520	-380	318	0	35	569	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
38	0	-15880	428	588	0	-699	-729	6.28	6.28	12.57	12.57	3	0.04	0.01	0.05	0.00	0.00	24.0
39	0	-14570	-6	1563	0	-8675	-38	6.28	6.28	12.57	12.57	3	0.30	0.03	0.15	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	83	-12525	63	248	0	-351	-50	6.28	6.28	12.57	12.57	3	0.01	0.00	0.02	0.00	0.00	24.0
2	83	-9624	35	170	0	-269	-39	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
3	83	-9664	31	201	0	-163	-39	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
4	83	-9604	65	180	0	-378	-38	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
5	83	-9644	62	211	0	-272	-38	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
6	83	-9574	50	138	0	-431	-39	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
7	83	-9696	37	240	0	-77	-38	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
8	83	-9565	59	141	0	-463	-39	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
9	83	-9694	47	243	0	-110	-38	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
10	83	-9624	35	170	0	-269	-39	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
11	83	-9664	31	201	0	-163	-39	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
12	83	-9604	65	180	0	-378	-38	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
13	83	-9644	62	211	0	-272	-38	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
14	83	-9574	50	138	0	-431	-39	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
15	83	-9696	37	240	0	-77	-38	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
16	83	-9565	59	141	0	-463	-39	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
17	83	-9694	47	243	0	-110	-38	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
18	83	-15065	-239	470	0	-587	126	6.28	6.28	12.57	12.57	3	0.02	0.01	0.04	0.00	0.00	24.0
19	83	-15878	246	632	0	-1161	-253	6.28	6.28	12.57	12.57	3	0.04	0.01	0.06	0.00	0.00	24.0
20	83	-15098	-15	764	0	-6242	-53	6.28	6.28	12.57	12.57	3	0.22	0.01	0.07	0.00	0.00	24.0
37	83	-13878	-380	318	0	-228	255	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
38	83	-15235	428	588	0	-1184	-375	6.28	6.28	12.57	12.57	3	0.05	0.01	0.05	0.00	0.00	24.0
39	83	-13928	-6	808	0	-9653	-43	6.28	6.28	12.57	12.57	3	0.34	0.01	0.08	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	165	-11880	63	248	0	-556	2	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
2	165	-9129	35	170	0	-409	-10	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0

3	165	-9168	31	201	0	-328	-13	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
4	165	-9109	65	180	0	-527	15	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
5	165	-9148	62	211	0	-446	13	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
6	165	-9078	50	138	0	-544	2	6.28	6.28	12.57	12.57	2	0.03	0.00	0.01	0.00	0.00	24.0
7	165	-9202	37	240	0	-275	-7	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
8	165	-9070	59	141	0	-579	9	6.28	6.28	12.57	12.57	2	0.03	0.00	0.01	0.00	0.00	24.0
9	165	-9198	47	243	0	-311	1	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
10	165	-9129	35	170	0	-409	-10	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
11	165	-9168	31	201	0	-328	-13	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
12	165	-9109	65	180	0	-527	15	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
13	165	-9148	62	211	0	-446	13	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
14	165	-9078	50	138	0	-544	2	6.28	6.28	12.57	12.57	2	0.03	0.00	0.01	0.00	0.00	24.0
15	165	-9202	37	240	0	-275	-7	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
16	165	-9070	59	141	0	-579	9	6.28	6.28	12.57	12.57	2	0.03	0.00	0.01	0.00	0.00	24.0
17	165	-9198	47	243	0	-311	1	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
18	165	-14420	-239	470	0	-975	-72	6.28	6.28	12.57	12.57	3	0.03	0.01	0.04	0.00	0.00	24.0
19	165	-15235	246	632	0	-1682	-50	6.28	6.28	12.57	12.57	3	0.06	0.01	0.06	0.00	0.00	24.0
20	165	-14455	-15	311	0	-6686	-66	6.28	6.28	12.57	12.57	3	0.23	0.01	0.03	0.00	0.00	24.0
37	165	-13235	-380	318	0	-490	-58	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
38	165	-14590	428	588	0	-1669	-22	6.28	6.28	12.57	12.57	3	0.06	0.01	0.06	0.00	0.00	24.0
39	165	-13285	-6	52	0	-10007	-48	6.28	6.28	12.57	12.57	3	0.35	0.00	0.00	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	248	-11235	63	248	0	-760	53	6.28	6.28	12.57	12.57	3	0.03	0.00	0.02	0.00	0.00	24.0
2	248	-8634	35	170	0	-549	19	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
3	248	-8672	31	201	0	-494	13	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
4	248	-8614	65	180	0	-675	69	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
5	248	-8652	62	211	0	-620	64	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
6	248	-8583	50	138	0	-658	43	6.28	6.28	12.57	12.57	2	0.04	0.00	0.01	0.00	0.00	24.0
7	248	-8707	37	240	0	-474	24	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
8	248	-8576	59	141	0	-696	58	6.28	6.28	12.57	12.57	2	0.04	0.00	0.01	0.00	0.00	24.0
9	248	-8703	47	243	0	-512	39	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
10	248	-8634	35	170	0	-549	19	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
11	248	-8672	31	201	0	-494	13	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
12	248	-8614	65	180	0	-675	69	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
13	248	-8652	62	211	0	-620	64	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
14	248	-8583	50	138	0	-658	43	6.28	6.28	12.57	12.57	2	0.04	0.00	0.01	0.00	0.00	24.0
15	248	-8707	37	240	0	-474	24	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
16	248	-8576	59	141	0	-696	58	6.28	6.28	12.57	12.57	2	0.04	0.00	0.01	0.00	0.00	24.0
17	248	-8703	47	243	0	-512	39	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
18	248	-13775	-239	470	0	-1363	-269	6.28	6.28	12.57	12.57	3	0.05	0.01	0.04	0.00	0.00	24.0
19	248	-14592	246	632	0	-2204	153	6.28	6.28	12.57	12.57	3	0.08	0.01	0.06	0.00	0.00	24.0
20	248	-13812	-15	-142	0	-6755	-78	6.28	6.28	12.57	12.57	3	0.24	0.00	0.01	0.00	0.00	24.0
37	248	-12592	-380	318	0	-753	-371	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
38	248	-13945	428	588	0	-2154	332	6.28	6.28	12.57	12.57	3	0.08	0.01	0.06	0.00	0.00	24.0
39	248	-12642	-6	-703	0	-9739	-53	6.28	6.28	12.57	12.57	3	0.34	0.01	0.07	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	330	-10590	63	248	0	-964	105	6.28	6.28	12.57	12.57	3	0.04	0.00	0.02	0.00	0.00	24.0
2	330	-8138	35	170	0	-689	47	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
3	330	-8176	31	201	0	-660	39	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
4	330	-8118	65	180	0	-824	123	6.28	6.28	12.57	12.57	2	0.05	0.00	0.02	0.00	0.00	24.0
5	330	-8156	62	211	0	-794	115	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
6	330	-8087	50	138	0	-771	84	6.28	6.28	12.57	12.57	2	0.04	0.00	0.01	0.00	0.00	24.0
7	330	-8213	37	240	0	-672	55	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
8	330	-8081	59	141	0	-812	107	6.28	6.28	12.57	12.57	2	0.05	0.00	0.01	0.00	0.00	24.0
9	330	-8207	47	243	0	-712	78	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
10	330	-8138	35	170	0	-689	47	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
11	330	-8176	31	201	0	-660	39	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
12	330	-8118	65	180	0	-824	123	6.28	6.28	12.57	12.57	2	0.05	0.00	0.02	0.00	0.00	24.0
13	330	-8156	62	211	0	-794	115	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
14	330	-8087	50	138	0	-771	84	6.28	6.28	12.57	12.57	2	0.04	0.00	0.01	0.00	0.00	24.0
15	330	-8213	37	240	0	-672	55	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
16	330	-8081	59	141	0	-812	107	6.28	6.28	12.57	12.57	2	0.05	0.00	0.01	0.00	0.00	24.0
17	330	-8207	47	243	0	-712	78	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
18	330	-13130	-239	470	0	-1751	-466	6.28	6.28	12.57	12.57	3	0.07	0.01	0.04	0.00	0.00	24.0
19	330	-13950	246	632	0	-2725	355	6.28	6.28	12.57	12.57	3	0.10	0.01	0.06	0.00	0.00	24.0
20	330	-13170	-15	-595	0	-6451	-90	6.28	6.28	12.57	12.57	3	0.23	0.01	0.06	0.00	0.00	24.0
37	330	-11950	-380	318	0	-1015	-684	6.28	6.28	12.57	12.57	3	0.05	0.01	0.03	0.00	0.00	24.0
38	330	-13300	428	588	0	-2639	685	6.28	6.28	12.57	12.57	3	0.10	0.01	0.06	0.00	0.00	24.0
39	330	-12000	-6	-1458	0	-8848	-58	6.28	6.28	12.57	12.57	3	0.31	0.03	0.14	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

VERIFICA NODO IN TESTA AL PILASTRO, NODO NUM. 39 NON CONFINATO

(par.7.2.2 NTC2018 "La domanda di resistenza valutata con i criteri della progettazione in capacità può essere assunta non superiore alla domanda di resistenza valutata per il caso di comportamento strutturale non dissipativo.")

PROGETTAZIONE IN CAPACITA'

Asse loc. pilastro y nodo INTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 50.0 cm, hjc= 30.0 cm

Asse loc. pilastro z nodo: --

FxMin,inf	FxMin,sup	FxMax,sup	FySup	FzSup	Vjbdy	Vjbdz	Vres,y	Vres,z	I.R.compr.	Ashy	Ashz	PASSO	Nota
daN					daN		daN			cmq		cm	
-8081	-4171	-4284	675	351	34558	--	129916	--	0.27	8.77	--	5.18	

VERIFICA DI RESISTENZA CON SOLLECITAZIONI COMPORTAMENTO NON DISSIPATIVO

Asse loc. pilastro y nodo INTERNO: Hjw= 40.0 cm, bj= 50.0 cm, hjc= 30.0 cm, db1= 45.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb,1	Mb,2	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m			daN			cmq	cm	
2	-4192	-8138	-1901	-2246	677	175	129945	0.00	0.00	40.00	
3	-4223	-8176	-1905	-2257	675	194	129935	0.00	0.00	40.00	
4	-4233	-8118	-1810	-2208	727	256	129932	0.00	0.00	40.00	
5	-4263	-8156	-1814	-2219	726	275	129922	0.00	0.00	40.00	
6	-4171	-8087	-1863	-2220	696	185	129951	0.00	0.00	40.00	
7	-4272	-8213	-1879	-2257	691	243	129919	0.00	0.00	40.00	
8	-4183	-8081	-1836	-2208	712	207	129947	0.00	0.00	40.00	
9	-4284	-8207	-1851	-2245	706	267	129916	0.00	0.00	40.00	
10	-4192	-8138	-1901	-2246	677	175	129945	0.00	0.00	40.00	
11	-4223	-8176	-1905	-2257	675	194	129935	0.00	0.00	40.00	
12	-4233	-8118	-1810	-2208	727	256	129932	0.00	0.00	40.00	

13	-4263	-8156	-1814	-2219	726	275	129922	0.00	0.00	40.00
14	-4171	-8087	-1863	-2220	696	185	129951	0.00	0.00	40.00
15	-4272	-8213	-1879	-2257	691	243	129919	0.00	0.00	40.00
16	-4183	-8081	-1836	-2208	712	207	129947	0.00	0.00	40.00
17	-4284	-8207	-1851	-2245	706	267	129916	0.00	0.00	40.00

CONFRONTO E SINTESI CONCLUSIVE (si assume in ogni caso passo <= 15 cm)

I.R.compr.	Ashy	Ashz	PASSO	Nota
	cmq		cm	
0.00	--	--	15.00	**VERIFICATO**

ASTA NUM. 8 NI 40 NF 34 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 12B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-19200	-153	123	0	160	403	6.28	6.28	12.57	12.57	3	0.02	0.00	0.01	0.00	0.00	24.0
2	0	-14800	-110	94	0	54	295	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
3	0	-14810	-109	126	0	272	293	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
4	0	-14730	-126	64	0	-26	327	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
5	0	-14740	-125	96	0	193	325	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
6	0	-14760	-117	46	0	-229	309	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
7	0	-14800	-113	152	0	500	301	6.28	6.28	12.57	12.57	2	0.03	0.00	0.01	0.00	0.00	24.0
8	0	-14740	-122	37	0	-253	319	6.28	6.28	12.57	12.57	2	0.03	0.00	0.01	0.00	0.00	24.0
9	0	-14780	-118	144	0	476	311	6.28	6.28	12.57	12.57	2	0.03	0.00	0.01	0.00	0.00	24.0
10	0	-14800	-110	94	0	54	295	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
11	0	-14810	-109	126	0	272	293	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
12	0	-14730	-126	64	0	-26	327	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
13	0	-14740	-125	96	0	193	325	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
14	0	-14760	-117	46	0	-229	309	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
15	0	-14800	-113	152	0	500	301	6.28	6.28	12.57	12.57	2	0.03	0.00	0.01	0.00	0.00	24.0
16	0	-14740	-122	37	0	-253	319	6.28	6.28	12.57	12.57	2	0.03	0.00	0.01	0.00	0.00	24.0
17	0	-14780	-118	144	0	476	311	6.28	6.28	12.57	12.57	2	0.03	0.00	0.01	0.00	0.00	24.0
18	0	-22150	-22	413	0	738	138	6.28	6.28	12.57	12.57	3	0.03	0.01	0.04	0.00	0.00	24.0
19	0	-20450	-305	128	0	3	710	6.28	6.28	12.57	12.57	3	0.04	0.01	0.03	0.00	0.00	24.0
20	0	-20910	-148	3182	0	2738	386	6.28	6.28	12.57	12.57	3	0.10	0.05	0.28	0.00	0.00	24.0
37	0	-22140	76	461	0	917	-58	6.28	6.28	12.57	12.57	3	0.03	0.01	0.04	0.00	0.00	24.0
38	0	-19300	-397	-14	0	-308	895	6.28	6.28	12.57	12.57	3	0.05	0.01	0.03	0.00	0.00	24.0
39	0	-20070	-134	5075	0	4251	354	6.28	6.28	12.57	12.57	3	0.15	0.09	0.44	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	110	-18342	-153	123	0	25	235	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
2	110	-14140	-110	94	0	-49	174	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
3	110	-14150	-109	126	0	134	173	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
4	110	-14070	-126	64	0	-96	189	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
5	110	-14080	-125	96	0	87	187	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
6	110	-14100	-117	46	0	-280	181	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
7	110	-14140	-113	152	0	332	177	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
8	110	-14080	-122	37	0	-294	185	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
9	110	-14120	-118	144	0	318	181	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
10	110	-14140	-110	94	0	-49	174	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
11	110	-14150	-109	126	0	134	173	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
12	110	-14070	-126	64	0	-96	189	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
13	110	-14080	-125	96	0	87	187	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
14	110	-14100	-117	46	0	-280	181	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
15	110	-14140	-113	152	0	332	177	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
16	110	-14080	-122	37	0	-294	185	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
17	110	-14120	-118	144	0	318	181	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
18	110	-21292	-22	413	0	283	115	6.28	6.28	12.57	12.57	3	0.01	0.01	0.04	0.00	0.00	24.0
19	110	-19592	-305	128	0	-138	375	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
20	110	-20052	-148	2578	0	-430	223	6.28	6.28	12.57	12.57	3	0.02	0.04	0.23	0.00	0.00	24.0
37	110	-21282	76	461	0	409	26	6.28	6.28	12.57	12.57	3	0.01	0.01	0.04	0.00	0.00	24.0
38	110	-18442	-397	-14	0	-293	459	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
39	110	-19212	-134	4068	0	-778	207	6.28	6.28	12.57	12.57	3	0.03	0.07	0.36	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	220	-17485	-153	123	0	-111	67	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
2	220	-13480	-110	94	0	-153	53	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
3	220	-13490	-109	126	0	-4	53	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
4	220	-13410	-126	64	0	-167	50	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
5	220	-13420	-125	96	0	-18	50	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
6	220	-13440	-117	46	0	-331	52	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
7	220	-13480	-113	152	0	164	52	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
8	220	-13420	-122	37	0	-335	51	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
9	220	-13460	-118	144	0	160	51	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
10	220	-13480	-110	94	0	-153	53	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
11	220	-13490	-109	126	0	-4	53	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
12	220	-13410	-126	64	0	-167	50	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
13	220	-13420	-125	96	0	-18	50	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
14	220	-13440	-117	46	0	-331	52	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
15	220	-13480	-113	152	0	164	52	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
16	220	-13420	-122	37	0	-335	51	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
17	220	-13460	-118	144	0	160	51	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
18	220	-20435	-22	413	0	-171	91	6.28	6.28	12.57	12.57	3	0.01	0.01	0.04	0.00	0.00	24.0
19	220	-18735	-305	128	0	-279	39	6.28	6.28	12.57	12.57	3	0.01	0.01	0.02	0.00	0.00	24.0
20	220	-19195	-148	1974	0	-2933	61	6.28	6.28	12.57	12.57	3	0.10	0.03	0.17	0.00	0.00	24.0
37	220	-20425	76	461	0	-98	109	6.28	6.28	12.57	12.57	3	0.01	0.01	0.04	0.00	0.00	24.0
38	220	-17585	-397	-14	0	-277	22	6.28	6.28	12.57	12.57	3	0.01	0.01	0.03	0.00	0.00	24.0
39	220	-18355	-134	3062	0	-4700	59	6.28	6.28	12.57	12.57	3	0.16	0.05	0.27	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	330	-16628	-153	123	0	-247	-101	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
2	330	-12820	-110	94	0	-256	-68	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
3	330	-12830	-109	126	0	-142	-67	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
4	330	-12750	-126	64	0	-238	-88	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
5	330	-12760	-125	96	0	-124	-87	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
6	330	-12780	-117	46	0	-382	-76	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0

7	330	-12820	-113	152	0	-3	-73	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
8	330	-12760	-122	37	0	-377	-82	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
9	330	-12800	-118	144	0	2	-79	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
10	330	-12820	-110	94	0	-256	-68	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
11	330	-12830	-109	126	0	-142	-67	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
12	330	-12750	-126	64	0	-238	-88	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
13	330	-12760	-125	96	0	-124	-87	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
14	330	-12780	-117	46	0	-382	-76	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
15	330	-12820	-113	152	0	-3	-73	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
16	330	-12760	-122	37	0	-377	-82	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
17	330	-12800	-118	144	0	2	-79	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
18	330	-19578	-22	413	0	-626	67	6.28	6.28	12.57	12.57	3	0.02	0.01	0.04	0.00	0.00	24.0
19	330	-17878	-305	128	0	-420	-297	6.28	6.28	12.57	12.57	3	0.02	0.01	0.02	0.00	0.00	24.0
20	330	-18338	-148	1369	0	-4771	-101	6.28	6.28	12.57	12.57	3	0.16	0.02	0.12	0.00	0.00	24.0
37	330	-19568	76	461	0	-606	192	6.28	6.28	12.57	12.57	3	0.02	0.01	0.04	0.00	0.00	24.0
38	330	-16728	-397	-14	0	-262	-414	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
39	330	-17498	-134	2055	0	-7514	-88	6.28	6.28	12.57	12.57	3	0.26	0.04	0.19	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	440	-15770	-153	123	0	-383	-269	6.28	6.28	12.57	12.57	3	0.02	0.00	0.01	0.00	0.00	24.0
2	440	-12160	-110	94	0	-359	-189	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
3	440	-12170	-109	126	0	-281	-187	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
4	440	-12090	-126	64	0	-308	-227	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
5	440	-12100	-125	96	0	-230	-225	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
6	440	-12120	-117	46	0	-433	-204	6.28	6.28	12.57	12.57	2	0.03	0.00	0.01	0.00	0.00	24.0
7	440	-12160	-113	152	0	-171	-198	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
8	440	-12100	-122	37	0	-418	-216	6.28	6.28	12.57	12.57	2	0.03	0.00	0.01	0.00	0.00	24.0
9	440	-12140	-118	144	0	-156	-209	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
10	440	-12160	-110	94	0	-359	-189	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
11	440	-12170	-109	126	0	-281	-187	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
12	440	-12090	-126	64	0	-308	-227	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
13	440	-12100	-125	96	0	-230	-225	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
14	440	-12120	-117	46	0	-433	-204	6.28	6.28	12.57	12.57	2	0.03	0.00	0.01	0.00	0.00	24.0
15	440	-12160	-113	152	0	-171	-198	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
16	440	-12100	-122	37	0	-418	-216	6.28	6.28	12.57	12.57	2	0.03	0.00	0.01	0.00	0.00	24.0
17	440	-12140	-118	144	0	-156	-209	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
18	440	-18720	-22	413	0	-1080	43	6.28	6.28	12.57	12.57	3	0.04	0.01	0.04	0.00	0.00	24.0
19	440	-17020	-305	128	0	-561	-632	6.28	6.28	12.57	12.57	3	0.04	0.01	0.03	0.00	0.00	24.0
20	440	-17480	-148	765	0	-5945	-264	6.28	6.28	12.57	12.57	3	0.21	0.01	0.07	0.00	0.00	24.0
37	440	-18710	76	461	0	-1113	276	6.28	6.28	12.57	12.57	3	0.04	0.01	0.04	0.00	0.00	24.0
38	440	-15870	-397	-14	0	-247	-850	6.28	6.28	12.57	12.57	3	0.05	0.01	0.03	0.00	0.00	24.0
39	440	-16640	-134	1048	0	-9221	-236	6.28	6.28	12.57	12.57	3	0.32	0.02	0.10	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

VERIFICA NODO IN TESTA AL PILASTRO, NODO NUM. 34 NON CONFINATO

(par.7.2.2 NTC2018 "La domanda di resistenza valutata con i criteri della progettazione in capacità può essere assunta non superiore alla domanda di resistenza valutata per il caso di comportamento strutturale non dissipativo.")

PROGETTAZIONE IN CAPACITA'

Asse loc. pilastro y nodo INTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 50.0 cm, hjc= 30.0 cm
Asse loc. pilastro z nodo: --

FxMin,inf	FxMin,sup	FxMax,sup	FySup	FzSup	Vjbdy	Vjbdz	Vres,y	Vres,z	I.R.compr.	Ashy	Ashz	PASSO	Nota
daN					daN		daN			cmq		cm	
-12090	-8260	-8328	247	124	34986	--	128632	--	0.27	8.70	--	5.23	

VERIFICA DI RESISTENZA CON SOLLECITAZIONI COMPORTAMENTO NON DISSIPATIVO

Asse loc. pilastro y nodo INTERNO: Hjw= 40.0 cm, bj= 50.0 cm, hjc= 30.0 cm, db1= 45.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb,1	Mb,2	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-8317	-12160	-1443	-2012	266	1139	128636	0.01	0.00	40.00	
3	-8328	-12170	-1447	-2012	265	1130	128632	0.01	0.00	40.00	
4	-8260	-12090	-1421	-2019	248	1229	128654	0.01	0.00	40.00	
5	-8271	-12100	-1425	-2019	247	1220	128651	0.01	0.00	40.00	
6	-8284	-12120	-1431	-2013	261	1176	128646	0.01	0.00	40.00	
7	-8321	-12160	-1444	-2015	257	1153	128635	0.01	0.00	40.00	
8	-8267	-12100	-1424	-2015	256	1204	128652	0.01	0.00	40.00	
9	-8303	-12140	-1437	-2018	252	1183	128640	0.01	0.00	40.00	
10	-8317	-12160	-1443	-2012	266	1139	128636	0.01	0.00	40.00	
11	-8328	-12170	-1447	-2012	265	1130	128632	0.01	0.00	40.00	
12	-8260	-12090	-1421	-2019	248	1229	128654	0.01	0.00	40.00	
13	-8271	-12100	-1425	-2019	247	1220	128651	0.01	0.00	40.00	
14	-8284	-12120	-1431	-2013	261	1176	128646	0.01	0.00	40.00	
15	-8321	-12160	-1444	-2015	257	1153	128635	0.01	0.00	40.00	
16	-8267	-12100	-1424	-2015	256	1204	128652	0.01	0.00	40.00	
17	-8303	-12140	-1437	-2018	252	1183	128640	0.01	0.00	40.00	

CONFRONTO E SINTESI CONCLUSIVE (si assume in ogni caso passo <= 15 cm)

I.R.compr.	Ashy	Ashz	PASSO	Nota
	cmq		cm	
0.01	--	--	15.00	**VERIFICATO**

ASTA NUM. 9 NI 41 NF 36 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 17B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza	aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m	cm
1	0	-19280	7	300	0	521	13	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
2	0	-14830	14	219	0	305	-11	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
3	0	-14880	14	243	0	508	-9	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
4	0	-14780	-3	218	0	293	29	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0

5	0	-14830	-4	242	0	497	30	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
6	0	-14760	9	190	0	63	2	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
7	0	-14910	7	271	0	742	6	6.28	6.28	12.57	12.57	2	0.04	0.00	0.03	0.00	0.00	24.0
8	0	-14740	4	190	0	60	13	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
9	0	-14900	1	271	0	738	18	6.28	6.28	12.57	12.57	2	0.04	0.00	0.03	0.00	0.00	24.0
10	0	-14830	14	219	0	305	-11	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
11	0	-14880	14	243	0	508	-9	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
12	0	-14780	-3	218	0	293	29	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
13	0	-14830	-4	242	0	497	30	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
14	0	-14760	9	190	0	63	2	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
15	0	-14910	7	271	0	742	6	6.28	6.28	12.57	12.57	2	0.04	0.00	0.03	0.00	0.00	24.0
16	0	-14740	4	190	0	60	13	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
17	0	-14900	1	271	0	738	18	6.28	6.28	12.57	12.57	2	0.04	0.00	0.03	0.00	0.00	24.0
18	0	-22660	195	698	0	1293	-375	6.28	6.28	12.57	12.57	3	0.05	0.01	0.06	0.00	0.00	24.0
19	0	-21490	-134	606	0	1053	302	6.28	6.28	12.57	12.57	3	0.04	0.01	0.05	0.00	0.00	24.0
20	0	-21750	22	3951	0	4181	-19	6.28	6.28	12.57	12.57	3	0.14	0.07	0.34	0.00	0.00	24.0
37	0	-22180	297	614	0	1163	-585	6.28	6.28	12.57	12.57	3	0.05	0.01	0.05	0.00	0.00	24.0
38	0	-20220	-252	462	0	763	544	6.28	6.28	12.57	12.57	3	0.04	0.01	0.04	0.00	0.00	24.0
39	0	-20660	9	6037	0	5976	9	6.28	6.28	12.57	12.57	3	0.20	0.10	0.52	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	110	-18420	7	300	0	191	20	6.28	6.28	12.57	12.57	3	0.01	0.01	0.03	0.00	0.00	24.0
2	110	-14170	14	219	0	64	5	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
3	110	-14220	14	243	0	241	6	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
4	110	-14120	-3	218	0	53	25	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
5	110	-14170	-4	242	0	230	26	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
6	110	-14100	9	190	0	-146	11	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
7	110	-14250	7	271	0	444	14	6.28	6.28	12.57	12.57	2	0.02	0.00	0.03	0.00	0.00	24.0
8	110	-14080	4	190	0	-149	17	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
9	110	-14240	1	271	0	440	20	6.28	6.28	12.57	12.57	2	0.02	0.00	0.03	0.00	0.00	24.0
10	110	-14170	14	219	0	64	5	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
11	110	-14220	14	243	0	241	6	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
12	110	-14120	-3	218	0	53	25	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
13	110	-14170	-4	242	0	230	26	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
14	110	-14100	9	190	0	-146	11	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
15	110	-14250	7	271	0	444	14	6.28	6.28	12.57	12.57	2	0.02	0.00	0.03	0.00	0.00	24.0
16	110	-14080	4	190	0	-149	17	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
17	110	-14240	1	271	0	440	20	6.28	6.28	12.57	12.57	2	0.02	0.00	0.03	0.00	0.00	24.0
18	110	-21802	195	698	0	526	-161	6.28	6.28	12.57	12.57	3	0.02	0.01	0.06	0.00	0.00	24.0
19	110	-20632	-134	606	0	386	154	6.28	6.28	12.57	12.57	3	0.02	0.01	0.05	0.00	0.00	24.0
20	110	-20892	22	3347	0	167	5	6.28	6.28	12.57	12.57	3	0.01	0.06	0.29	0.00	0.00	24.0
37	110	-21320	297	614	0	487	-259	6.28	6.28	12.57	12.57	3	0.02	0.01	0.05	0.00	0.00	24.0
38	110	-19362	-252	462	0	254	267	6.28	6.28	12.57	12.57	3	0.02	0.01	0.04	0.00	0.00	24.0
39	110	-19800	9	5030	0	-112	19	6.28	6.28	12.57	12.57	3	0.00	0.09	0.44	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	220	-17560	7	300	0	-138	28	6.28	6.28	12.57	12.57	3	0.01	0.01	0.03	0.00	0.00	24.0
2	220	-13510	14	219	0	-176	21	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
3	220	-13560	14	243	0	-26	21	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
4	220	-13460	-3	218	0	-187	22	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
5	220	-13510	-4	242	0	-37	22	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
6	220	-13440	9	190	0	-355	21	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
7	220	-13590	7	271	0	146	21	6.28	6.28	12.57	12.57	2	0.01	0.00	0.03	0.00	0.00	24.0
8	220	-13420	4	190	0	-359	21	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
9	220	-13580	1	271	0	142	21	6.28	6.28	12.57	12.57	2	0.01	0.00	0.03	0.00	0.00	24.0
10	220	-13510	14	219	0	-176	21	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
11	220	-13560	14	243	0	-26	21	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
12	220	-13460	-3	218	0	-187	22	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
13	220	-13510	-4	242	0	-37	22	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
14	220	-13440	9	190	0	-355	21	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
15	220	-13590	7	271	0	146	21	6.28	6.28	12.57	12.57	2	0.01	0.00	0.03	0.00	0.00	24.0
16	220	-13420	4	190	0	-359	21	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
17	220	-13580	1	271	0	142	21	6.28	6.28	12.57	12.57	2	0.01	0.00	0.03	0.00	0.00	24.0
18	220	-20945	195	698	0	-242	53	6.28	6.28	12.57	12.57	3	0.01	0.01	0.06	0.00	0.00	24.0
19	220	-19775	-134	606	0	-281	7	6.28	6.28	12.57	12.57	3	0.01	0.01	0.05	0.00	0.00	24.0
20	220	-20035	22	2743	0	-3183	30	6.28	6.28	12.57	12.57	3	0.11	0.05	0.24	0.00	0.00	24.0
37	220	-20460	297	614	0	-189	68	6.28	6.28	12.57	12.57	3	0.01	0.01	0.05	0.00	0.00	24.0
38	220	-18505	-252	462	0	-254	-9	6.28	6.28	12.57	12.57	3	0.01	0.01	0.04	0.00	0.00	24.0
39	220	-18940	9	4024	0	-5092	29	6.28	6.28	12.57	12.57	3	0.17	0.07	0.36	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	330	-16700	7	300	0	-468	35	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
2	330	-12850	14	219	0	-417	37	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
3	330	-12900	14	243	0	-293	36	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
4	330	-12800	-3	218	0	-427	18	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
5	330	-12850	-4	242	0	-303	17	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
6	330	-12780	9	190	0	-565	31	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
7	330	-12930	7	271	0	-152	29	6.28	6.28	12.57	12.57	2	0.01	0.00	0.03	0.00	0.00	24.0
8	330	-12760	4	190	0	-568	25	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
9	330	-12920	1	271	0	-155	23	6.28	6.28	12.57	12.57	2	0.01	0.00	0.03	0.00	0.00	24.0
10	330	-12850	14	219	0	-417	37	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
11	330	-12900	14	243	0	-293	36	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
12	330	-12800	-3	218	0	-427	18	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
13	330	-12850	-4	242	0	-303	17	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
14	330	-12780	9	190	0	-565	31	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
15	330	-12930	7	271	0	-152	29	6.28	6.28	12.57	12.57	2	0.01	0.00	0.03	0.00	0.00	24.0
16	330	-12760	4	190	0	-568	25	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
17	330	-12920	1	271	0	-155	23	6.28	6.28	12.57	12.57	2	0.01	0.00	0.03	0.00	0.00	24.0
18	330	-20088	195	698	0	-1009	267	6.28	6.28	12.57	12.57	3	0.04	0.01	0.06	0.00	0.00	24.0
19	330	-18918	-134	606	0	-948	-141	6.28	6.28	12.57	12.57	3	0.03	0.01	0.05	0.00	0.00	24.0
20	330	-19178	22	2139	0	-5868	54	6.28	6.28	12.57	12.57	3	0.20	0.04	0.19	0.00	0.00	24.0
37	330	-19600	297	614	0	-864	394	6.28	6.28	12.57	12.57	3	0.04	0.01	0.05	0.00	0.00	24.0
38	330	-17648	-252	462	0	-762	-286	6.28	6.28	12.57	12.57	3	0.03	0.01	0.04	0.00	0.00	24.0
39	330	-18080	9	3017	0	-8965	38	6.28	6.28	12.57	12.57	3	0.31	0.05	0.27	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	440	-15840	7	300	0	-798	43	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
2	440	-12190	14	219	0	-657	53	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
3	440	-12240	14	243	0	-560	52	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
4	440	-12140	-3	218	0	-667	14	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
5	440	-12190	-4	242	0	-570	13	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
6	440	-12120	9	190	0	-774	41	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
7	440	-12270	7	271	0	-450	36	6.28	6.28	12.57	12.57	2	0.02	0.00	0.03	0.00	0.00	24.0
8	440	-12100	4	190	0	-777	29	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
9	440	-12260	1	271	0	-453	25	6.28	6.28	12.57	12.57	2	0.02	0.00	0.03	0.00	0.00	24.0
10	440	-12190	14	219	0	-657	53	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0

11	440	-12240	14	243	0	-560	52	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
12	440	-12140	-3	218	0	-667	14	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
13	440	-12190	-4	242	0	-570	13	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
14	440	-12120	9	190	0	-774	41	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
15	440	-12270	7	271	0	-450	36	6.28	6.28	12.57	12.57	2	0.02	0.00	0.03	0.00	0.00	24.0
16	440	-12100	4	190	0	-777	29	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
17	440	-12260	1	271	0	-453	25	6.28	6.28	12.57	12.57	2	0.02	0.00	0.03	0.00	0.00	24.0
18	440	-19230	195	698	0	-1776	482	6.28	6.28	12.57	12.57	3	0.07	0.01	0.06	0.00	0.00	24.0
19	440	-18060	-134	606	0	-1615	-289	6.28	6.28	12.57	12.57	3	0.06	0.01	0.05	0.00	0.00	24.0
20	440	-18320	22	1535	0	-7889	78	6.28	6.28	12.57	12.57	3	0.27	0.03	0.14	0.00	0.00	24.0
37	440	-18740	297	614	0	-1540	721	6.28	6.28	12.57	12.57	3	0.07	0.01	0.05	0.00	0.00	24.0
38	440	-16790	-252	462	0	-1271	-563	6.28	6.28	12.57	12.57	3	0.05	0.01	0.04	0.00	0.00	24.0
39	440	-17220	9	2010	0	-11730	48	6.28	6.28	12.57	12.57	3	0.40	0.03	0.18	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

VERIFICA NODO IN TESTA AL PILASTRO, NODO NUM. 36 NON CONFINATO

(par.7.2.2 NTC2018 "La domanda di resistenza valutata con i criteri della progettazione in capacità può essere assunta non superiore alla domanda di resistenza valutata per il caso di comportamento strutturale non dissipativo.")

PROGETTAZIONE IN CAPACITA'

Asse loc. pilastro y nodo INTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 50.0 cm, hjc= 30.0 cm
Asse loc. pilastro z nodo: --

FxMin,inf	FxMin,sup	FxMax,sup	FySup	FzSup	Vjbdy	Vjbdz	Vres,y	Vres,z	I.R.compr.	Ashy	Ashz	PASSO	Nota
daN					daN		daN			cmq		cm	
-12100	-8325	-8490	209	198	35024	--	128581	--	0.27	8.70	--	5.23	

VERIFICA DI RESISTENZA CON SOLLECITAZIONI COMPORTAMENTO NON DISSIPATIVO

Asse loc. pilastro y nodo INTERNO: Hjw= 40.0 cm, bj= 50.0 cm, hjc= 30.0 cm, db1= 45.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb,1	Mb,2	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-8410	-12190	-1613	-1806	235	241	128606	0.00	0.00	40.00	
3	-8456	-12240	-1613	-1808	236	246	128592	0.00	0.00	40.00	
4	-8360	-12140	-1604	-1815	209	312	128622	0.00	0.00	40.00	
5	-8405	-12190	-1604	-1817	209	317	128608	0.00	0.00	40.00	
6	-8340	-12120	-1610	-1807	226	261	128629	0.00	0.00	40.00	
7	-8490	-12270	-1610	-1813	227	275	128581	0.00	0.00	40.00	
8	-8325	-12100	-1607	-1809	218	281	128633	0.00	0.00	40.00	
9	-8475	-12260	-1607	-1816	219	297	128585	0.00	0.00	40.00	
10	-8410	-12190	-1613	-1806	235	241	128606	0.00	0.00	40.00	
11	-8456	-12240	-1613	-1808	236	246	128592	0.00	0.00	40.00	
12	-8360	-12140	-1604	-1815	209	312	128622	0.00	0.00	40.00	
13	-8405	-12190	-1604	-1817	209	317	128608	0.00	0.00	40.00	
14	-8340	-12120	-1610	-1807	226	261	128629	0.00	0.00	40.00	
15	-8490	-12270	-1610	-1813	227	275	128581	0.00	0.00	40.00	
16	-8325	-12100	-1607	-1809	218	281	128633	0.00	0.00	40.00	
17	-8475	-12260	-1607	-1816	219	297	128585	0.00	0.00	40.00	

CONFRONTO E SINTESI CONCLUSIVE (si assume in ogni caso passo <= 15 cm)

I.R.compr.	Ashy	Ashz	PASSO	Nota
	cmq		cm	
0.00	--	--	15.00	**VERIFICATO**

ASTA NUM. 10 NI 42 NF 38 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 22B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-21560	98	28	0	-56	-249	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
2	0	-16570	83	-11	0	-187	-207	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
3	0	-16610	81	13	0	26	-202	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
4	0	-16560	69	30	0	-112	-181	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
5	0	-16600	67	55	0	101	-176	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
6	0	-16520	81	-25	0	-410	-204	6.28	6.28	12.57	12.57	2	0.03	0.00	0.01	0.00	0.00	24.0
7	0	-16650	74	56	0	301	-187	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
8	0	-16520	77	-13	0	-387	-196	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
9	0	-16650	70	68	0	324	-179	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
10	0	-16570	83	-11	0	-187	-207	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
11	0	-16610	81	13	0	26	-202	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
12	0	-16560	69	30	0	-112	-181	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
13	0	-16600	67	55	0	101	-176	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
14	0	-16520	81	-25	0	-410	-204	6.28	6.28	12.57	12.57	2	0.03	0.00	0.01	0.00	0.00	24.0
15	0	-16650	74	56	0	301	-187	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
16	0	-16520	77	-13	0	-387	-196	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
17	0	-16650	70	68	0	324	-179	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
18	0	-24050	296	-21	0	-283	-640	6.28	6.28	12.57	12.57	3	0.03	0.01	0.02	0.00	0.00	24.0
19	0	-24840	-5	245	0	363	-37	6.28	6.28	12.57	12.57	3	0.01	0.00	0.02	0.00	0.00	24.0
20	0	-24090	117	2968	0	2256	-272	6.28	6.28	12.57	12.57	3	0.08	0.05	0.25	0.00	0.00	24.0
37	0	-22890	380	-136	0	-528	-811	6.28	6.28	12.57	12.57	3	0.04	0.01	0.03	0.00	0.00	24.0
38	0	-24210	-121	308	0	550	194	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
39	0	-22950	82	4845	0	3705	-198	6.28	6.28	12.57	12.57	3	0.12	0.08	0.41	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	110	-20702	98	28	0	-87	-141	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
2	110	-15910	83	-11	0	-175	-116	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
3	110	-15950	81	13	0	12	-113	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
4	110	-15900	69	30	0	-145	-104	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
5	110	-15940	67	55	0	41	-102	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
6	110	-15860	81	-25	0	-382	-115	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
7	110	-15990	74	56	0	240	-106	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
8	110	-15860	77	-13	0	-373	-112	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0

9	110	-15990	70	68	0	249	-102	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
10	110	-15910	83	-11	0	-175	-116	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
11	110	-15950	81	13	0	12	-113	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
12	110	-15900	69	30	0	-145	-104	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
13	110	-15940	67	55	0	41	-102	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
14	110	-15860	81	-25	0	-382	-115	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
15	110	-15990	74	56	0	240	-106	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
16	110	-15860	77	-13	0	-373	-112	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
17	110	-15990	70	68	0	249	-102	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
18	110	-23190	296	-21	0	-260	-314	6.28	6.28	12.57	12.57	3	0.02	0.01	0.02	0.00	0.00	24.0
19	110	-23982	-5	245	0	93	-42	6.28	6.28	12.57	12.57	3	0.00	0.00	0.02	0.00	0.00	24.0
20	110	-23230	117	2364	0	-677	-143	6.28	6.28	12.57	12.57	3	0.02	0.04	0.20	0.00	0.00	24.0
37	110	-22032	380	-136	0	-378	-393	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
38	110	-23352	-121	308	0	211	61	6.28	6.28	12.57	12.57	3	0.01	0.01	0.03	0.00	0.00	24.0
39	110	-22092	82	3838	0	-1071	-108	6.28	6.28	12.57	12.57	3	0.04	0.06	0.33	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	220	-19845	98	28	0	-118	-34	6.28	6.28	12.57	12.57	3	0.00	0.00	0.01	0.00	0.00	24.0
2	220	-15250	83	-11	0	-163	-24	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
3	220	-15290	81	13	0	-3	-24	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
4	220	-15240	69	30	0	-178	-28	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
5	220	-15280	67	55	0	-19	-28	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
6	220	-15200	81	-25	0	-355	-26	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
7	220	-15330	74	56	0	178	-25	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
8	220	-15200	77	-13	0	-359	-27	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
9	220	-15330	70	68	0	173	-26	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
10	220	-15250	83	-11	0	-163	-24	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
11	220	-15290	81	13	0	-3	-24	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
12	220	-15240	69	30	0	-178	-28	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
13	220	-15280	67	55	0	-19	-28	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
14	220	-15200	81	-25	0	-355	-26	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
15	220	-15330	74	56	0	178	-25	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
16	220	-15200	77	-13	0	-359	-27	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
17	220	-15330	70	68	0	173	-26	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
18	220	-22330	296	-21	0	-237	11	6.28	6.28	12.57	12.57	3	0.01	0.01	0.02	0.00	0.00	24.0
19	220	-23125	-5	245	0	-177	-48	6.28	6.28	12.57	12.57	3	0.01	0.00	0.02	0.00	0.00	24.0
20	220	-22370	117	1760	0	-2945	-15	6.28	6.28	12.57	12.57	3	0.10	0.03	0.15	0.00	0.00	24.0
37	220	-21175	380	-136	0	-228	25	6.28	6.28	12.57	12.57	3	0.01	0.01	0.03	0.00	0.00	24.0
38	220	-22495	-121	308	0	-128	-72	6.28	6.28	12.57	12.57	3	0.01	0.01	0.03	0.00	0.00	24.0
39	220	-21235	82	2831	0	-4740	-18	6.28	6.28	12.57	12.57	3	0.16	0.05	0.24	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	330	-18988	98	28	0	-149	74	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
2	330	-14590	83	-11	0	-151	67	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
3	330	-14630	81	13	0	-17	66	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
4	330	-14580	69	30	0	-212	48	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
5	330	-14620	67	55	0	-79	46	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
6	330	-14540	81	-25	0	-327	63	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
7	330	-14670	74	56	0	116	57	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
8	330	-14540	77	-13	0	-346	57	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
9	330	-14670	70	68	0	98	51	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
10	330	-14590	83	-11	0	-151	67	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
11	330	-14630	81	13	0	-17	66	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
12	330	-14580	69	30	0	-212	48	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
13	330	-14620	67	55	0	-79	46	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
14	330	-14540	81	-25	0	-327	63	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
15	330	-14670	74	56	0	116	57	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
16	330	-14540	77	-13	0	-346	57	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
17	330	-14670	70	68	0	98	51	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
18	330	-21470	296	-21	0	-214	336	6.28	6.28	12.57	12.57	3	0.02	0.01	0.02	0.00	0.00	24.0
19	330	-22268	-5	245	0	-447	-53	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
20	330	-21510	117	1156	0	-4548	114	6.28	6.28	12.57	12.57	3	0.15	0.02	0.10	0.00	0.00	24.0
37	330	-20318	380	-136	0	-78	443	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
38	330	-21638	-121	308	0	-466	-206	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
39	330	-20378	82	1825	0	-7301	73	6.28	6.28	12.57	12.57	3	0.25	0.03	0.16	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	440	-18130	98	28	0	-180	182	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
2	440	-13930	83	-11	0	-138	159	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
3	440	-13970	81	13	0	-32	155	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
4	440	-13920	69	30	0	-245	125	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
5	440	-13960	67	55	0	-138	120	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
6	440	-13880	81	-25	0	-300	152	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
7	440	-14010	74	56	0	55	138	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
8	440	-13880	77	-13	0	-332	142	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
9	440	-14010	70	68	0	23	127	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
10	440	-13930	83	-11	0	-138	159	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
11	440	-13970	81	13	0	-32	155	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
12	440	-13920	69	30	0	-245	125	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
13	440	-13960	67	55	0	-138	120	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
14	440	-13880	81	-25	0	-300	152	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
15	440	-14010	74	56	0	55	138	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
16	440	-13880	77	-13	0	-332	142	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
17	440	-14010	70	68	0	23	127	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
18	440	-20610	296	-21	0	-190	661	6.28	6.28	12.57	12.57	3	0.03	0.01	0.02	0.00	0.00	24.0
19	440	-21410	-5	245	0	-717	-59	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
20	440	-20650	117	552	0	-5487	242	6.28	6.28	12.57	12.57	3	0.19	0.01	0.05	0.00	0.00	24.0
37	440	-19460	380	-136	0	72	861	6.28	6.28	12.57	12.57	3	0.05	0.01	0.03	0.00	0.00	24.0
38	440	-20780	-121	308	0	-805	-339	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
39	440	-19520	82	818	0	-8754	163	6.28	6.28	12.57	12.57	3	0.30	0.01	0.07	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

VERIFICA NODO IN TESTA AL PILASTRO, NODO NUM. 38 NON CONFINATO

(par.7.2.2 NTC2018 "La domanda di resistenza valutata con i criteri della progettazione in capacità può essere assunta non superiore alla domanda di resistenza valutata per il caso di comportamento strutturale non dissipativo.")

PROGETTAZIONE IN CAPACITA'

Asse loc. pilastro y nodo INTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 50.0 cm, hjc= 30.0 cm

Asse loc. pilastro z nodo: --

FxMin,inf	FxMin,sup	FxMax,sup	FySup	FzSup	Vjbdy	Vjbdz	Vres,y	Vres,z	I.R.compr.	Ashy	Ashz	PASSO	Nota
daN					daN		daN			cmq		cm	
-13880	-10060	-10190	31	138	35202	--	128037	--	0.27	8.67	--	5.25	

VERIFICA DI RESISTENZA CON SOLLECITAZIONI COMPORTAMENTO NON DISSIPATIVO

Asse loc. pilastro y nodo INTERNO: Hjw= 40.0 cm, bj= 50.0 cm, hjc= 30.0 cm, db1= 45.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb,1	Mb,2	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-10120	-13930	-1855	-1627	35	528	128060	0.00	0.00	40.00	
3	-10160	-13970	-1853	-1634	31	510	128047	0.00	0.00	40.00	
4	-10100	-13920	-1848	-1631	65	470	128066	0.00	0.00	40.00	
5	-10140	-13960	-1846	-1637	62	454	128053	0.00	0.00	40.00	
6	-10070	-13880	-1854	-1621	50	525	128076	0.00	0.00	40.00	
7	-10190	-14010	-1849	-1642	37	474	128037	0.00	0.00	40.00	
8	-10060	-13880	-1852	-1622	59	509	128079	0.00	0.00	40.00	
9	-10190	-14010	-1847	-1643	47	457	128037	0.00	0.00	40.00	
10	-10120	-13930	-1855	-1627	35	528	128060	0.00	0.00	40.00	
11	-10160	-13970	-1853	-1634	31	510	128047	0.00	0.00	40.00	
12	-10100	-13920	-1848	-1631	65	470	128066	0.00	0.00	40.00	
13	-10140	-13960	-1846	-1637	62	454	128053	0.00	0.00	40.00	
14	-10070	-13880	-1854	-1621	50	525	128076	0.00	0.00	40.00	
15	-10190	-14010	-1849	-1642	37	474	128037	0.00	0.00	40.00	
16	-10060	-13880	-1852	-1622	59	509	128079	0.00	0.00	40.00	
17	-10190	-14010	-1847	-1643	47	457	128037	0.00	0.00	40.00	

CONFRONTO E SINTESI CONCLUSIVE (si assume in ogni caso passo <= 15 cm)

I.R.compr.	Ashy	Ashz	PASSO	Nota
	cmq		cm	
0.00	--	--	15.00	**VERIFICATO**

ASTA NUM. 11 NI 48 NF 49 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 31B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-22650	446	-27	0	-37	-6598	15.71	15.71	9.42	9.42	3	0.12	0.01	0.03	0.00	0.00	24.0
2	0	-17320	414	-59	0	-126	-5637	15.71	15.71	9.42	9.42	2	0.14	0.01	0.03	0.00	0.00	24.0
3	0	-17270	398	16	0	78	-5517	15.71	15.71	9.42	9.42	2	0.14	0.01	0.03	0.00	0.00	24.0
4	0	-17580	289	-57	0	-135	-4634	15.71	15.71	9.42	9.42	2	0.12	0.00	0.02	0.00	0.00	24.0
5	0	-17530	272	19	0	69	-4514	15.71	15.71	9.42	9.42	2	0.11	0.00	0.02	0.00	0.00	24.0
6	0	-17470	390	-146	0	-367	-5425	15.71	15.71	9.42	9.42	2	0.14	0.00	0.03	0.00	0.00	24.0
7	0	-17300	334	105	0	313	-5027	15.71	15.71	9.42	9.42	2	0.13	0.00	0.03	0.00	0.00	24.0
8	0	-17550	352	-146	0	-370	-5124	15.71	15.71	9.42	9.42	2	0.13	0.00	0.03	0.00	0.00	24.0
9	0	-17380	296	106	0	310	-4726	15.71	15.71	9.42	9.42	2	0.12	0.00	0.02	0.00	0.00	24.0
10	0	-17320	414	-59	0	-126	-5637	15.71	15.71	9.42	9.42	2	0.14	0.01	0.03	0.00	0.00	24.0
11	0	-17270	398	16	0	78	-5517	15.71	15.71	9.42	9.42	2	0.14	0.01	0.03	0.00	0.00	24.0
12	0	-17580	289	-57	0	-135	-4634	15.71	15.71	9.42	9.42	2	0.12	0.00	0.02	0.00	0.00	24.0
13	0	-17530	272	19	0	69	-4514	15.71	15.71	9.42	9.42	2	0.11	0.00	0.02	0.00	0.00	24.0
14	0	-17470	390	-146	0	-367	-5425	15.71	15.71	9.42	9.42	2	0.14	0.00	0.03	0.00	0.00	24.0
15	0	-17300	334	105	0	313	-5027	15.71	15.71	9.42	9.42	2	0.13	0.00	0.03	0.00	0.00	24.0
16	0	-17550	352	-146	0	-370	-5124	15.71	15.71	9.42	9.42	2	0.13	0.00	0.03	0.00	0.00	24.0
17	0	-17380	296	106	0	310	-4726	15.71	15.71	9.42	9.42	2	0.12	0.00	0.02	0.00	0.00	24.0
18	0	-25950	2116	-126	0	-218	-14790	15.71	15.71	9.42	9.42	3	0.26	0.03	0.15	0.00	0.00	24.0
19	0	-30690	-158	-50	0	-116	-10190	15.71	15.71	9.42	9.42	3	0.17	0.00	0.01	0.00	0.00	24.0
20	0	-27590	805	180	0	495	-11480	15.71	15.71	9.42	9.42	3	0.20	0.01	0.06	0.00	0.00	24.0
37	0	-22560	2698	-131	0	-206	-14400	15.71	15.71	9.42	9.42	3	0.25	0.03	0.19	0.00	0.00	24.0
38	0	-30460	-1092	-3	0	-37	-6724	15.71	15.71	9.42	9.42	3	0.11	0.01	0.07	0.00	0.00	24.0
39	0	-25290	514	379	0	982	-8886	15.71	15.71	9.42	9.42	3	0.16	0.01	0.04	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	110	-21505	446	-27	0	-8	-6107	15.71	15.71	9.42	9.42	3	0.11	0.01	0.03	0.00	0.00	24.0
2	110	-16440	414	-59	0	-60	-5181	15.71	15.71	9.42	9.42	2	0.13	0.01	0.03	0.00	0.00	24.0
3	110	-16390	398	16	0	61	-5080	15.71	15.71	9.42	9.42	2	0.13	0.01	0.03	0.00	0.00	24.0
4	110	-16700	289	-57	0	-73	-4316	15.71	15.71	9.42	9.42	2	0.11	0.00	0.02	0.00	0.00	24.0
5	110	-16650	272	19	0	48	-4215	15.71	15.71	9.42	9.42	2	0.10	0.00	0.02	0.00	0.00	24.0
6	110	-16590	390	-146	0	-206	-4996	15.71	15.71	9.42	9.42	2	0.13	0.00	0.03	0.00	0.00	24.0
7	110	-16420	334	105	0	198	-4660	15.71	15.71	9.42	9.42	2	0.12	0.00	0.03	0.00	0.00	24.0
8	110	-16670	352	-146	0	-210	-4736	15.71	15.71	9.42	9.42	2	0.12	0.00	0.03	0.00	0.00	24.0
9	110	-16500	296	106	0	194	-4400	15.71	15.71	9.42	9.42	2	0.11	0.00	0.02	0.00	0.00	24.0
10	110	-16440	414	-59	0	-60	-5181	15.71	15.71	9.42	9.42	2	0.13	0.01	0.03	0.00	0.00	24.0
11	110	-16390	398	16	0	61	-5080	15.71	15.71	9.42	9.42	2	0.13	0.01	0.03	0.00	0.00	24.0
12	110	-16700	289	-57	0	-73	-4316	15.71	15.71	9.42	9.42	2	0.11	0.00	0.02	0.00	0.00	24.0
13	110	-16650	272	19	0	48	-4215	15.71	15.71	9.42	9.42	2	0.10	0.00	0.02	0.00	0.00	24.0
14	110	-16590	390	-146	0	-206	-4996	15.71	15.71	9.42	9.42	2	0.13	0.00	0.03	0.00	0.00	24.0
15	110	-16420	334	105	0	198	-4660	15.71	15.71	9.42	9.42	2	0.12	0.00	0.03	0.00	0.00	24.0
16	110	-16670	352	-146	0	-210	-4736	15.71	15.71	9.42	9.42	2	0.12	0.00	0.03	0.00	0.00	24.0
17	110	-16500	296	106	0	194	-4400	15.71	15.71	9.42	9.42	2	0.11	0.00	0.02	0.00	0.00	24.0
18	110	-24805	1908	-126	0	-79	-12578	15.71	15.71	9.42	9.42	3	0.22	0.02	0.13	0.00	0.00	24.0
19	110	-29545	49	-50	0	-61	-10250	15.71	15.71	9.42	9.42	3	0.17	0.00	0.00	0.00	0.00	24.0
20	110	-26445	805	180	0	298	-10596	15.71	15.71	9.42	9.42	3	0.18	0.01	0.06	0.00	0.00	24.0
37	110	-21415	2352	-131	0	-63	-11622	15.71	15.71	9.42	9.42	3	0.20	0.03	0.17	0.00	0.00	24.0
38	110	-29315	-745	-3	0	-34	-7734	15.71	15.71	9.42	9.42	3	0.13	0.01	0.05	0.00	0.00	24.0
39	110	-24148	514	379	0	564	-8321	15.71	15.71	9.42	9.42	3	0.15	0.01	0.04	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	220	-20360	446	-27	0	21	-5617	15.71	15.71	9.42	9.42	3	0.10	0.01	0.03	0.00	0.00	24.0
2	220	-15560	414	-59	0	5	-4725	15.71	15.71	9.42	9.42	2	0.12	0.01	0.03	0.00	0.00	24.0
3	220	-15510	398	16	0	43	-4642	15.71	15.71	9.42	9.42	2	0.12	0.01	0.03	0.00	0.00	24.0
4	220	-15820	289	-57	0	-10	-3999	15.71	15.71	9.42	9.42	2	0.10	0.00	0.02	0.00	0.00	24.0
5	220	-15770	272	19	0	28	-3916	15.71	15.71	9.42	9.42	2	0.10	0.00	0.02	0.00	0.00	24.0
6	220	-15710	390	-146	0	-45	-4567	15.71	15.71	9.42	9.42	2	0.11	0.00	0.03	0.00	0.00	24.0
7	220	-15540	334	105	0	82	-4292	15.71	15.71	9.42	9.42	2	0.11	0.00	0.03	0.00	0.00	24.0
8	220	-15790	352	-146	0	-50	-4349	15.71	15.71	9.42	9.42	2	0.11	0.00	0.03	0.00	0.00	24.0
9	220	-15620	296	106	0	78	-4074	15.71	15.71	9.42	9.42	2	0.10	0.00	0.02	0.00	0.00	24.0
10	220	-15560	414	-59	0	5	-4725	15.71	15.71	9.42	9.42	2	0.12	0.01	0.03	0.00	0.00	24.0
11	220	-15510	398	16	0	43	-4642	15.71	15.71	9.42	9.42	2	0.12	0.01	0.03	0.00	0.00	24.0
12	220	-15820	289	-57	0	-10	-3999	15.71	15.71	9.42	9.42	2	0.10	0.00	0.02	0.00	0.00	24.0

13	220	-15770	272	19	0	28	-3916	15.71	15.71	9.42	9.42	2	0.10	0.00	0.02	0.00	0.00	24.0
14	220	-15710	390	-146	0	-45	-4567	15.71	15.71	9.42	9.42	2	0.11	0.00	0.03	0.00	0.00	24.0
15	220	-15540	334	105	0	82	-4292	15.71	15.71	9.42	9.42	2	0.11	0.00	0.03	0.00	0.00	24.0
16	220	-15790	352	-146	0	-50	-4349	15.71	15.71	9.42	9.42	2	0.11	0.00	0.03	0.00	0.00	24.0
17	220	-15620	296	106	0	78	-4074	15.71	15.71	9.42	9.42	2	0.10	0.00	0.02	0.00	0.00	24.0
18	220	-23660	1700	-126	0	60	-10595	15.71	15.71	9.42	9.42	3	0.18	0.02	0.12	0.00	0.00	24.0
19	220	-28400	257	-50	0	-6	-10080	15.71	15.71	9.42	9.42	3	0.17	0.00	0.02	0.00	0.00	24.0
20	220	-25300	805	180	0	100	-9712	15.71	15.71	9.42	9.42	3	0.17	0.01	0.06	0.00	0.00	24.0
37	220	-20270	2005	-131	0	81	-9226	15.71	15.71	9.42	9.42	3	0.16	0.03	0.15	0.00	0.00	24.0
38	220	-28170	-399	-3	0	-30	-8363	15.71	15.71	9.42	9.42	3	0.14	0.00	0.03	0.00	0.00	24.0
39	220	-23005	514	379	0	147	-7756	15.71	15.71	9.42	9.42	3	0.14	0.01	0.04	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	330	-19215	446	-27	0	51	-5126	15.71	15.71	9.42	9.42	3	0.09	0.01	0.03	0.00	0.00	24.0
2	330	-14680	414	-59	0	70	-4269	15.71	15.71	9.42	9.42	2	0.11	0.01	0.03	0.00	0.00	24.0
3	330	-14630	398	16	0	26	-4204	15.71	15.71	9.42	9.42	2	0.10	0.01	0.03	0.00	0.00	24.0
4	330	-14940	289	-57	0	52	-3681	15.71	15.71	9.42	9.42	2	0.09	0.00	0.02	0.00	0.00	24.0
5	330	-14890	272	19	0	7	-3617	15.71	15.71	9.42	9.42	2	0.09	0.00	0.02	0.00	0.00	24.0
6	330	-14830	390	-146	0	116	-4138	15.71	15.71	9.42	9.42	2	0.10	0.00	0.03	0.00	0.00	24.0
7	330	-14660	334	105	0	-33	-3924	15.71	15.71	9.42	9.42	2	0.10	0.00	0.03	0.00	0.00	24.0
8	330	-14910	352	-146	0	111	-3962	15.71	15.71	9.42	9.42	2	0.10	0.00	0.03	0.00	0.00	24.0
9	330	-14740	296	106	0	-38	-3748	15.71	15.71	9.42	9.42	2	0.09	0.00	0.02	0.00	0.00	24.0
10	330	-14680	414	-59	0	70	-4269	15.71	15.71	9.42	9.42	2	0.11	0.01	0.03	0.00	0.00	24.0
11	330	-14630	398	16	0	26	-4204	15.71	15.71	9.42	9.42	2	0.10	0.01	0.03	0.00	0.00	24.0
12	330	-14940	289	-57	0	52	-3681	15.71	15.71	9.42	9.42	2	0.09	0.00	0.02	0.00	0.00	24.0
13	330	-14890	272	19	0	7	-3617	15.71	15.71	9.42	9.42	2	0.09	0.00	0.02	0.00	0.00	24.0
14	330	-14830	390	-146	0	116	-4138	15.71	15.71	9.42	9.42	2	0.10	0.00	0.03	0.00	0.00	24.0
15	330	-14660	334	105	0	-33	-3924	15.71	15.71	9.42	9.42	2	0.10	0.00	0.03	0.00	0.00	24.0
16	330	-14910	352	-146	0	111	-3962	15.71	15.71	9.42	9.42	2	0.10	0.00	0.03	0.00	0.00	24.0
17	330	-14740	296	106	0	-38	-3748	15.71	15.71	9.42	9.42	2	0.09	0.00	0.02	0.00	0.00	24.0
18	330	-22515	1492	-126	0	199	-8840	15.71	15.71	9.42	9.42	3	0.16	0.02	0.11	0.00	0.00	24.0
19	330	-27255	465	-50	0	49	-9683	15.71	15.71	9.42	9.42	3	0.17	0.01	0.03	0.00	0.00	24.0
20	330	-24155	805	180	0	-98	-8828	15.71	15.71	9.42	9.42	3	0.15	0.01	0.06	0.00	0.00	24.0
37	330	-19125	1658	-131	0	225	-7210	15.71	15.71	9.42	9.42	3	0.13	0.02	0.12	0.00	0.00	24.0
38	330	-27025	-52	-3	0	-26	-8611	15.71	15.71	9.42	9.42	3	0.15	0.00	0.00	0.00	0.00	24.0
39	330	-21862	514	379	0	-270	-7190	15.71	15.71	9.42	9.42	3	0.13	0.01	0.04	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	440	-18070	446	-27	0	80	-4635	15.71	15.71	9.42	9.42	3	0.08	0.01	0.03	0.00	0.00	24.0
2	440	-13800	414	-59	0	136	-3813	15.71	15.71	9.42	9.42	2	0.10	0.01	0.03	0.00	0.00	24.0
3	440	-13750	398	16	0	8	-3767	15.71	15.71	9.42	9.42	2	0.09	0.01	0.03	0.00	0.00	24.0
4	440	-14060	289	-57	0	115	-3364	15.71	15.71	9.42	9.42	2	0.09	0.00	0.02	0.00	0.00	24.0
5	440	-14010	272	19	0	-13	-3318	15.71	15.71	9.42	9.42	2	0.08	0.00	0.02	0.00	0.00	24.0
6	440	-13950	390	-146	0	277	-3709	15.71	15.71	9.42	9.42	2	0.10	0.00	0.03	0.00	0.00	24.0
7	440	-13780	334	105	0	-148	-3557	15.71	15.71	9.42	9.42	2	0.09	0.00	0.03	0.00	0.00	24.0
8	440	-14030	352	-146	0	271	-3574	15.71	15.71	9.42	9.42	2	0.09	0.00	0.03	0.00	0.00	24.0
9	440	-13860	296	106	0	-154	-3422	15.71	15.71	9.42	9.42	2	0.09	0.00	0.02	0.00	0.00	24.0
10	440	-13800	414	-59	0	136	-3813	15.71	15.71	9.42	9.42	2	0.10	0.01	0.03	0.00	0.00	24.0
11	440	-13750	398	16	0	8	-3767	15.71	15.71	9.42	9.42	2	0.09	0.01	0.03	0.00	0.00	24.0
12	440	-14060	289	-57	0	115	-3364	15.71	15.71	9.42	9.42	2	0.09	0.00	0.02	0.00	0.00	24.0
13	440	-14010	272	19	0	-13	-3318	15.71	15.71	9.42	9.42	2	0.08	0.00	0.02	0.00	0.00	24.0
14	440	-13950	390	-146	0	277	-3709	15.71	15.71	9.42	9.42	2	0.10	0.00	0.03	0.00	0.00	24.0
15	440	-13780	334	105	0	-148	-3557	15.71	15.71	9.42	9.42	2	0.09	0.00	0.03	0.00	0.00	24.0
16	440	-14030	352	-146	0	271	-3574	15.71	15.71	9.42	9.42	2	0.09	0.00	0.03	0.00	0.00	24.0
17	440	-13860	296	106	0	-154	-3422	15.71	15.71	9.42	9.42	2	0.09	0.00	0.02	0.00	0.00	24.0
18	440	-21370	1284	-126	0	338	-7314	15.71	15.71	9.42	9.42	3	0.13	0.02	0.09	0.00	0.00	24.0
19	440	-26110	673	-50	0	104	-9056	15.71	15.71	9.42	9.42	3	0.16	0.01	0.05	0.00	0.00	24.0
20	440	-23010	805	180	0	-295	-7944	15.71	15.71	9.42	9.42	3	0.14	0.01	0.06	0.00	0.00	24.0
37	440	-17980	1312	-131	0	368	-5576	15.71	15.71	9.42	9.42	3	0.10	0.02	0.10	0.00	0.00	24.0
38	440	-25880	294	-3	0	-22	-8478	15.71	15.71	9.42	9.42	3	0.15	0.00	0.02	0.00	0.00	24.0
39	440	-20720	514	379	0	-688	-6625	15.71	15.71	9.42	9.42	3	0.12	0.01	0.04	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 12 NI 91 NF 92 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 30B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-24430	1145	-62	0	-171	-12730	15.71	15.71	9.42	9.42	3	0.22	0.01	0.08	0.00	0.00	24.0
2	0	-18780	1059	-82	0	-223	-11270	15.71	15.71	9.42	9.42	2	0.28	0.01	0.08	0.00	0.00	24.0
3	0	-18820	1056	-5	0	-14	-11290	15.71	15.71	9.42	9.42	2	0.27	0.01	0.08	0.00	0.00	24.0
4	0	-18770	705	-90	0	-249	-8292	15.71	15.71	9.42	9.42	2	0.21	0.01	0.05	0.00	0.00	24.0
5	0	-18810	702	-13	0	-40	-8316	15.71	15.71	9.42	9.42	2	0.20	0.01	0.05	0.00	0.00	24.0
6	0	-18740	938	-175	0	-476	-10200	15.71	15.71	9.42	9.42	2	0.26	0.01	0.07	0.00	0.00	24.0
7	0	-18850	929	82	0	221	-10280	15.71	15.71	9.42	9.42	2	0.25	0.01	0.07	0.00	0.00	24.0
8	0	-18740	832	-177	0	-484	-9307	15.71	15.71	9.42	9.42	2	0.23	0.01	0.06	0.00	0.00	24.0
9	0	-18850	823	80	0	213	-9386	15.71	15.71	9.42	9.42	2	0.23	0.01	0.06	0.00	0.00	24.0
10	0	-18780	1059	-82	0	-223	-11270	15.71	15.71	9.42	9.42	2	0.28	0.01	0.08	0.00	0.00	24.0
11	0	-18820	1056	-5	0	-14	-11290	15.71	15.71	9.42	9.42	2	0.27	0.01	0.08	0.00	0.00	24.0
12	0	-18770	705	-90	0	-249	-8292	15.71	15.71	9.42	9.42	2	0.21	0.01	0.05	0.00	0.00	24.0
13	0	-18810	702	-13	0	-40	-8316	15.71	15.71	9.42	9.42	2	0.20	0.01	0.05	0.00	0.00	24.0
14	0	-18740	938	-175	0	-476	-10200	15.71	15.71	9.42	9.42	2	0.26	0.01	0.07	0.00	0.00	24.0
15	0	-18850	929	82	0	221	-10280	15.71	15.71	9.42	9.42	2	0.25	0.01	0.07	0.00	0.00	24.0
16	0	-18740	832	-177	0	-484	-9307	15.71	15.71	9.42	9.42	2	0.23	0.01	0.06	0.00	0.00	24.0
17	0	-18850	823	80	0	213	-9386	15.71	15.71	9.42	9.42	2	0.23	0.01	0.06	0.00	0.00	24.0
18	0	-30020	3933	-149	0	-378	-30130	15.71	15.71	9.42	9.42	3	0.51	0.05	0.26	0.00	0.00	24.0
19	0	-33660	823	-135	0	-376	-18650	15.71	15.71	9.42	9.42	3	0.31	0.01	0.05	0.00	0.00	24.0
20	0	-30770	2207	137	0	311	-22800	15.71	15.71	9.42	9.42	3	0.39	0.03	0.15	0.00	0.00	24.0
37	0	-26430	4566	-126	0	-308	-30150	15.71	15.71	9.42	9.42	3	0.52	0.06	0.32	0.00	0.00	24.0
38	0	-32500	-617	-103	0	-305	-11020	15.71	15.71	9.42	9.42	3	0.19	0.01	0.04	0.00	0.00	24.0
39	0	-27670	1690	350	0	839	-17940	15.71	15.71	9.42	9.42	3	0.31	0.02	0.12	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	110	-23288	1145	-62	0	-103	-11471	15.71	15.71	9.42	9.42	3	0.20	0.01	0.08	0.00	0.00	24.0
2	110	-17900	1059	-82	0	-133	-10106	15.71	15.71	9.42	9.42	2	0.25	0.01	0.08	0.00	0.00	24.0
3	110	-17940	1056	-5	0	-9	-10130	15.71	15.71	9.42	9.42	2	0.25	0.01	0.08	0.00	0.00	24.0
4	110	-17890	705	-90	0	-150	-7517	15.71	15.71	9.42	9.42	2	0.19	0.01	0.05	0.00	0.00	24.0
5	110	-17930	702	-13	0	-26	-7544	15.71	15.71	9.42	9.42	2	0.18	0.01	0.05	0.00	0.00	24.0
6	110	-17860	938	-175	0	-284	-9168	15.71	15.71	9.42	9.42	2	0.23	0.01	0.07	0.00	0.00	24.0
7	110	-17970	929	82	0	131	-9258	15.71	15.71	9.42	9.42	2	0.23	0.01	0.07	0.00	0.00	24.0
8	110	-17860	832	-177	0	-289	-8392	15.71	15.71	9.42	9.42	2	0.21	0.01	0.06	0.00	0.00	24.0

9	110	-17970	823	80	0	126	-8481	15.71	15.71	9.42	9.42	2	0.21	0.01	0.06	0.00	0.00	24.0
10	110	-17900	1059	-82	0	-133	-10106	15.71	15.71	9.42	9.42	2	0.25	0.01	0.08	0.00	0.00	24.0
11	110	-17940	1056	-5	0	-9	-10130	15.71	15.71	9.42	9.42	2	0.25	0.01	0.08	0.00	0.00	24.0
12	110	-17890	705	-90	0	-150	-7517	15.71	15.71	9.42	9.42	2	0.19	0.01	0.05	0.00	0.00	24.0
13	110	-17930	702	-13	0	-26	-7544	15.71	15.71	9.42	9.42	2	0.18	0.01	0.05	0.00	0.00	24.0
14	110	-17860	938	-175	0	-284	-9168	15.71	15.71	9.42	9.42	2	0.23	0.01	0.07	0.00	0.00	24.0
15	110	-17970	929	82	0	131	-9258	15.71	15.71	9.42	9.42	2	0.23	0.01	0.07	0.00	0.00	24.0
16	110	-17860	832	-177	0	-289	-8392	15.71	15.71	9.42	9.42	2	0.21	0.01	0.06	0.00	0.00	24.0
17	110	-17970	823	80	0	126	-8481	15.71	15.71	9.42	9.42	2	0.21	0.01	0.06	0.00	0.00	24.0
18	110	-28878	3725	-149	0	-214	-25919	15.71	15.71	9.42	9.42	3	0.44	0.05	0.25	0.00	0.00	24.0
19	110	-32518	1031	-135	0	-228	-17631	15.71	15.71	9.42	9.42	3	0.30	0.01	0.07	0.00	0.00	24.0
20	110	-29625	2207	137	0	160	-20372	15.71	15.71	9.42	9.42	3	0.35	0.03	0.15	0.00	0.00	24.0
37	110	-25288	4220	-126	0	-169	-25318	15.71	15.71	9.42	9.42	3	0.44	0.05	0.30	0.00	0.00	24.0
38	110	-31355	-271	-103	0	-192	-11509	15.71	15.71	9.42	9.42	3	0.20	0.00	0.02	0.00	0.00	24.0
39	110	-26528	1690	350	0	454	-16080	15.71	15.71	9.42	9.42	3	0.28	0.02	0.12	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	220	-22145	1145	-62	0	-35	-10212	15.71	15.71	9.42	9.42	3	0.18	0.01	0.08	0.00	0.00	24.0
2	220	-17020	1059	-82	0	-42	-8942	15.71	15.71	9.42	9.42	2	0.22	0.01	0.08	0.00	0.00	24.0
3	220	-17060	1056	-5	0	-3	-8969	15.71	15.71	9.42	9.42	2	0.22	0.01	0.08	0.00	0.00	24.0
4	220	-17010	705	-90	0	-51	-6742	15.71	15.71	9.42	9.42	2	0.17	0.01	0.05	0.00	0.00	24.0
5	220	-17050	702	-13	0	-11	-6771	15.71	15.71	9.42	9.42	2	0.17	0.01	0.05	0.00	0.00	24.0
6	220	-16980	938	-175	0	-91	-8137	15.71	15.71	9.42	9.42	2	0.20	0.01	0.07	0.00	0.00	24.0
7	220	-17090	929	82	0	40	-8235	15.71	15.71	9.42	9.42	2	0.20	0.01	0.07	0.00	0.00	24.0
8	220	-16980	832	-177	0	-94	-7478	15.71	15.71	9.42	9.42	2	0.18	0.01	0.06	0.00	0.00	24.0
9	220	-17090	823	80	0	38	-7576	15.71	15.71	9.42	9.42	2	0.19	0.01	0.06	0.00	0.00	24.0
10	220	-17020	1059	-82	0	-42	-8942	15.71	15.71	9.42	9.42	2	0.22	0.01	0.08	0.00	0.00	24.0
11	220	-17060	1056	-5	0	-3	-8969	15.71	15.71	9.42	9.42	2	0.22	0.01	0.08	0.00	0.00	24.0
12	220	-17010	705	-90	0	-51	-6742	15.71	15.71	9.42	9.42	2	0.17	0.01	0.05	0.00	0.00	24.0
13	220	-17050	702	-13	0	-11	-6771	15.71	15.71	9.42	9.42	2	0.17	0.01	0.05	0.00	0.00	24.0
14	220	-16980	938	-175	0	-91	-8137	15.71	15.71	9.42	9.42	2	0.20	0.01	0.07	0.00	0.00	24.0
15	220	-17090	929	82	0	40	-8235	15.71	15.71	9.42	9.42	2	0.20	0.01	0.07	0.00	0.00	24.0
16	220	-16980	832	-177	0	-94	-7478	15.71	15.71	9.42	9.42	2	0.18	0.01	0.06	0.00	0.00	24.0
17	220	-17090	823	80	0	38	-7576	15.71	15.71	9.42	9.42	2	0.19	0.01	0.06	0.00	0.00	24.0
18	220	-27735	3517	-149	0	-50	-21938	15.71	15.71	9.42	9.42	3	0.38	0.04	0.24	0.00	0.00	24.0
19	220	-31375	1239	-135	0	-80	-16382	15.71	15.71	9.42	9.42	3	0.28	0.02	0.08	0.00	0.00	24.0
20	220	-28480	2207	137	0	9	-17945	15.71	15.71	9.42	9.42	3	0.31	0.03	0.15	0.00	0.00	24.0
37	220	-24145	3873	-126	0	-30	-20868	15.71	15.71	9.42	9.42	3	0.36	0.05	0.28	0.00	0.00	24.0
38	220	-30210	76	-103	0	-79	-11617	15.71	15.71	9.42	9.42	3	0.20	0.00	0.01	0.00	0.00	24.0
39	220	-25385	1690	350	0	69	-14220	15.71	15.71	9.42	9.42	3	0.25	0.02	0.12	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	330	-21002	1145	-62	0	33	-8954	15.71	15.71	9.42	9.42	3	0.16	0.01	0.08	0.00	0.00	24.0
2	330	-16140	1059	-82	0	48	-7777	15.71	15.71	9.42	9.42	2	0.19	0.01	0.08	0.00	0.00	24.0
3	330	-16180	1056	-5	0	3	-7808	15.71	15.71	9.42	9.42	2	0.19	0.01	0.08	0.00	0.00	24.0
4	330	-16130	705	-90	0	48	-5966	15.71	15.71	9.42	9.42	2	0.15	0.01	0.05	0.00	0.00	24.0
5	330	-16170	702	-13	0	3	-5998	15.71	15.71	9.42	9.42	2	0.15	0.01	0.05	0.00	0.00	24.0
6	330	-16100	938	-175	0	101	-7106	15.71	15.71	9.42	9.42	2	0.18	0.01	0.07	0.00	0.00	24.0
7	330	-16210	929	82	0	-50	-7213	15.71	15.71	9.42	9.42	2	0.18	0.01	0.07	0.00	0.00	24.0
8	330	-16100	832	-177	0	101	-6563	15.71	15.71	9.42	9.42	2	0.16	0.01	0.06	0.00	0.00	24.0
9	330	-16210	823	80	0	-50	-6670	15.71	15.71	9.42	9.42	2	0.16	0.01	0.06	0.00	0.00	24.0
10	330	-16140	1059	-82	0	48	-7777	15.71	15.71	9.42	9.42	2	0.19	0.01	0.08	0.00	0.00	24.0
11	330	-16180	1056	-5	0	3	-7808	15.71	15.71	9.42	9.42	2	0.19	0.01	0.08	0.00	0.00	24.0
12	330	-16130	705	-90	0	48	-5966	15.71	15.71	9.42	9.42	2	0.15	0.01	0.05	0.00	0.00	24.0
13	330	-16170	702	-13	0	3	-5998	15.71	15.71	9.42	9.42	2	0.15	0.01	0.05	0.00	0.00	24.0
14	330	-16100	938	-175	0	101	-7106	15.71	15.71	9.42	9.42	2	0.18	0.01	0.07	0.00	0.00	24.0
15	330	-16210	929	82	0	-50	-7213	15.71	15.71	9.42	9.42	2	0.18	0.01	0.07	0.00	0.00	24.0
16	330	-16100	832	-177	0	101	-6563	15.71	15.71	9.42	9.42	2	0.16	0.01	0.06	0.00	0.00	24.0
17	330	-16210	823	80	0	-50	-6670	15.71	15.71	9.42	9.42	2	0.16	0.01	0.06	0.00	0.00	24.0
18	330	-26592	3309	-149	0	113	-18184	15.71	15.71	9.42	9.42	3	0.31	0.04	0.23	0.00	0.00	24.0
19	330	-30232	1447	-135	0	68	-14906	15.71	15.71	9.42	9.42	3	0.25	0.02	0.10	0.00	0.00	24.0
20	330	-27335	2207	137	0	-141	-15518	15.71	15.71	9.42	9.42	3	0.27	0.03	0.15	0.00	0.00	24.0
37	330	-23002	3527	-126	0	109	-16798	15.71	15.71	9.42	9.42	3	0.29	0.04	0.25	0.00	0.00	24.0
38	330	-29065	422	-103	0	34	-11344	15.71	15.71	9.42	9.42	3	0.19	0.01	0.03	0.00	0.00	24.0
39	330	-24242	1690	350	0	-316	-12360	15.71	15.71	9.42	9.42	3	0.22	0.02	0.12	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	440	-19860	1145	-62	0	101	-7695	15.71	15.71	9.42	9.42	3	0.14	0.01	0.09	0.00	0.00	24.0
2	440	-15260	1059	-82	0	139	-6613	15.71	15.71	9.42	9.42	2	0.17	0.01	0.08	0.00	0.00	24.0
3	440	-15300	1056	-5	0	8	-6648	15.71	15.71	9.42	9.42	2	0.16	0.01	0.08	0.00	0.00	24.0
4	440	-15250	705	-90	0	147	-5191	15.71	15.71	9.42	9.42	2	0.13	0.01	0.05	0.00	0.00	24.0
5	440	-15290	702	-13	0	17	-5226	15.71	15.71	9.42	9.42	2	0.13	0.01	0.05	0.00	0.00	24.0
6	440	-15220	938	-175	0	294	-6074	15.71	15.71	9.42	9.42	2	0.16	0.01	0.07	0.00	0.00	24.0
7	440	-15330	929	82	0	-141	-6191	15.71	15.71	9.42	9.42	2	0.16	0.01	0.07	0.00	0.00	24.0
8	440	-15220	832	-177	0	296	-5648	15.71	15.71	9.42	9.42	2	0.15	0.01	0.06	0.00	0.00	24.0
9	440	-15330	823	80	0	-138	-5765	15.71	15.71	9.42	9.42	2	0.14	0.01	0.06	0.00	0.00	24.0
10	440	-15260	1059	-82	0	139	-6613	15.71	15.71	9.42	9.42	2	0.17	0.01	0.08	0.00	0.00	24.0
11	440	-15300	1056	-5	0	8	-6648	15.71	15.71	9.42	9.42	2	0.16	0.01	0.08	0.00	0.00	24.0
12	440	-15250	705	-90	0	147	-5191	15.71	15.71	9.42	9.42	2	0.13	0.01	0.05	0.00	0.00	24.0
13	440	-15290	702	-13	0	17	-5226	15.71	15.71	9.42	9.42	2	0.13	0.01	0.05	0.00	0.00	24.0
14	440	-15220	938	-175	0	294	-6074	15.71	15.71	9.42	9.42	2	0.16	0.01	0.07	0.00	0.00	24.0
15	440	-15330	929	82	0	-141	-6191	15.71	15.71	9.42	9.42	2	0.16	0.01	0.07	0.00	0.00	24.0
16	440	-15220	832	-177	0	296	-5648	15.71	15.71	9.42	9.42	2	0.15	0.01	0.06	0.00	0.00	24.0
17	440	-15330	823	80	0	-138	-5765	15.71	15.71	9.42	9.42	2	0.14	0.01	0.06	0.00	0.00	24.0
18	440	-25450	3101	-149	0	277	-14660	15.71	15.71	9.42	9.42	3	0.25	0.04	0.22	0.00	0.00	24.0
19	440	-29090	1655	-135	0	216	-13200	15.71	15.71	9.42	9.42	3	0.23	0.02	0.11	0.00	0.00	24.0
20	440	-26190	2207	137	0	-292	-13090	15.71	15.71	9.42	9.42	3	0.23	0.03	0.15	0.00	0.00	24.0
37	440	-21860	3180	-126	0	248	-13110	15.71	15.71	9.42	9.42	3	0.23	0.04	0.23	0.00	0.00	24.0
38	440	-27920	769	-103	0	147	-10690	15.71	15.71	9.42	9.42	3	0.18	0.01	0.05	0.00	0.00	24.0
39	440	-23100	1690	350	0	-701	-10500	15.71	15.71	9.42	9.42	3	0.19	0.02	0.12	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 13 NI 134 NF 135 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 29B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-24440	1290	-128	0	-359	-13500	15.71	15.71	9.42	9.42	3	0.24	0.02	0.09	0.00	0.00	24.0
2	0	-18760	1202	-135	0	-377	-12040	15.71	15.71	9.42	9.42	2	0.30	0.02	0.09	0.00	0.00	24.0
3	0	-18730	1191	-61	0	-173	-11940	15.71	15.71	9.42	9.42	2	0.29	0.02	0.09	0.00	0.00	24.0
4	0	-18870	793	-136	0	-379	-8827	15.71	15.71	9.42	9.42	2	0.22	0.01	0.06	0.00	0.00	24.0

5	0	-18830	782	-61	0	-175	-8720	15.71	15.71	9.42	9.42	2	0.21	0.01	0.06	0.00	0.00	24.0
6	0	-18840	1071	-222	0	-616	-11040	15.71	15.71	9.42	9.42	2	0.28	0.01	0.08	0.00	0.00	24.0
7	0	-18720	1036	26	0	64	-10690	15.71	15.71	9.42	9.42	2	0.26	0.01	0.08	0.00	0.00	24.0
8	0	-18870	948	-222	0	-616	-10080	15.71	15.71	9.42	9.42	2	0.26	0.01	0.07	0.00	0.00	24.0
9	0	-18760	913	25	0	64	-9721	15.71	15.71	9.42	9.42	2	0.24	0.01	0.07	0.00	0.00	24.0
10	0	-18760	1202	-135	0	-377	-12040	15.71	15.71	9.42	9.42	2	0.30	0.02	0.09	0.00	0.00	24.0
11	0	-18730	1191	-61	0	-173	-11940	15.71	15.71	9.42	9.42	2	0.29	0.02	0.09	0.00	0.00	24.0
12	0	-18870	793	-136	0	-379	-8827	15.71	15.71	9.42	9.42	2	0.22	0.01	0.06	0.00	0.00	24.0
13	0	-18830	782	-61	0	-175	-8720	15.71	15.71	9.42	9.42	2	0.21	0.01	0.06	0.00	0.00	24.0
14	0	-18840	1071	-222	0	-616	-11040	15.71	15.71	9.42	9.42	2	0.28	0.01	0.08	0.00	0.00	24.0
15	0	-18720	1036	26	0	64	-10690	15.71	15.71	9.42	9.42	2	0.26	0.01	0.08	0.00	0.00	24.0
16	0	-18870	948	-222	0	-616	-10080	15.71	15.71	9.42	9.42	2	0.26	0.01	0.07	0.00	0.00	24.0
17	0	-18760	913	25	0	64	-9721	15.71	15.71	9.42	9.42	2	0.24	0.01	0.07	0.00	0.00	24.0
18	0	-29840	4309	-271	0	-753	-32030	15.71	15.71	9.42	9.42	3	0.55	0.05	0.29	0.00	0.00	24.0
19	0	-33840	1011	-226	0	-647	-19760	15.71	15.71	9.42	9.42	3	0.33	0.01	0.07	0.00	0.00	24.0
20	0	-30620	2433	3	0	-64	-23820	15.71	15.71	9.42	9.42	3	0.40	0.03	0.16	0.00	0.00	24.0
37	0	-26130	4961	-245	0	-674	-32080	15.71	15.71	9.42	9.42	3	0.56	0.06	0.35	0.00	0.00	24.0
38	0	-32800	-536	-170	0	-497	-11620	15.71	15.71	9.42	9.42	3	0.20	0.01	0.04	0.00	0.00	24.0
39	0	-27430	1833	211	0	473	-18380	15.71	15.71	9.42	9.42	3	0.32	0.02	0.13	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	110	-23295	1290	-128	0	-219	-12081	15.71	15.71	9.42	9.42	3	0.21	0.02	0.09	0.00	0.00	24.0
2	110	-17880	1202	-135	0	-229	-10719	15.71	15.71	9.42	9.42	2	0.26	0.02	0.09	0.00	0.00	24.0
3	110	-17850	1191	-61	0	-106	-10629	15.71	15.71	9.42	9.42	2	0.26	0.02	0.09	0.00	0.00	24.0
4	110	-17990	793	-136	0	-230	-7955	15.71	15.71	9.42	9.42	2	0.20	0.01	0.06	0.00	0.00	24.0
5	110	-17950	782	-61	0	-107	-7860	15.71	15.71	9.42	9.42	2	0.19	0.01	0.06	0.00	0.00	24.0
6	110	-17960	1071	-222	0	-372	-9862	15.71	15.71	9.42	9.42	2	0.25	0.01	0.08	0.00	0.00	24.0
7	110	-17840	1036	26	0	36	-9550	15.71	15.71	9.42	9.42	2	0.23	0.01	0.08	0.00	0.00	24.0
8	110	-17990	948	-222	0	-372	-9036	15.71	15.71	9.42	9.42	2	0.23	0.01	0.07	0.00	0.00	24.0
9	110	-17880	913	25	0	36	-8717	15.71	15.71	9.42	9.42	2	0.21	0.01	0.07	0.00	0.00	24.0
10	110	-17880	1202	-135	0	-229	-10719	15.71	15.71	9.42	9.42	2	0.26	0.02	0.09	0.00	0.00	24.0
11	110	-17850	1191	-61	0	-106	-10629	15.71	15.71	9.42	9.42	2	0.26	0.02	0.09	0.00	0.00	24.0
12	110	-17990	793	-136	0	-230	-7955	15.71	15.71	9.42	9.42	2	0.20	0.01	0.06	0.00	0.00	24.0
13	110	-17950	782	-61	0	-107	-7860	15.71	15.71	9.42	9.42	2	0.19	0.01	0.06	0.00	0.00	24.0
14	110	-17960	1071	-222	0	-372	-9862	15.71	15.71	9.42	9.42	2	0.25	0.01	0.08	0.00	0.00	24.0
15	110	-17840	1036	26	0	36	-9550	15.71	15.71	9.42	9.42	2	0.23	0.01	0.08	0.00	0.00	24.0
16	110	-17990	948	-222	0	-372	-9036	15.71	15.71	9.42	9.42	2	0.23	0.01	0.07	0.00	0.00	24.0
17	110	-17880	913	25	0	36	-8717	15.71	15.71	9.42	9.42	2	0.21	0.01	0.07	0.00	0.00	24.0
18	110	-28695	4101	-271	0	-455	-27404	15.71	15.71	9.42	9.42	3	0.47	0.05	0.28	0.00	0.00	24.0
19	110	-32695	1219	-226	0	-398	-18533	15.71	15.71	9.42	9.42	3	0.31	0.01	0.08	0.00	0.00	24.0
20	110	-29475	2433	3	0	-67	-21142	15.71	15.71	9.42	9.42	3	0.36	0.03	0.16	0.00	0.00	24.0
37	110	-24985	4614	-245	0	-404	-26813	15.71	15.71	9.42	9.42	3	0.47	0.06	0.33	0.00	0.00	24.0
38	110	-31655	-190	-170	0	-310	-12019	15.71	15.71	9.42	9.42	3	0.20	0.00	0.01	0.00	0.00	24.0
39	110	-26285	1833	211	0	241	-16365	15.71	15.71	9.42	9.42	3	0.28	0.02	0.13	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	220	-22150	1290	-128	0	-78	-10661	15.71	15.71	9.42	9.42	3	0.19	0.02	0.09	0.00	0.00	24.0
2	220	-17000	1202	-135	0	-80	-9398	15.71	15.71	9.42	9.42	2	0.23	0.02	0.09	0.00	0.00	24.0
3	220	-16970	1191	-61	0	-39	-9318	15.71	15.71	9.42	9.42	2	0.23	0.02	0.09	0.00	0.00	24.0
4	220	-17110	793	-136	0	-81	-7083	15.71	15.71	9.42	9.42	2	0.17	0.01	0.06	0.00	0.00	24.0
5	220	-17070	782	-61	0	-40	-7000	15.71	15.71	9.42	9.42	2	0.17	0.01	0.06	0.00	0.00	24.0
6	220	-17080	1071	-222	0	-128	-8685	15.71	15.71	9.42	9.42	2	0.21	0.01	0.08	0.00	0.00	24.0
7	220	-16960	1036	26	0	8	-8409	15.71	15.71	9.42	9.42	2	0.20	0.01	0.08	0.00	0.00	24.0
8	220	-17110	948	-222	0	-128	-7992	15.71	15.71	9.42	9.42	2	0.20	0.01	0.07	0.00	0.00	24.0
9	220	-17000	913	25	0	8	-7713	15.71	15.71	9.42	9.42	2	0.19	0.01	0.07	0.00	0.00	24.0
10	220	-17000	1202	-135	0	-80	-9398	15.71	15.71	9.42	9.42	2	0.23	0.02	0.09	0.00	0.00	24.0
11	220	-16970	1191	-61	0	-39	-9318	15.71	15.71	9.42	9.42	2	0.23	0.02	0.09	0.00	0.00	24.0
12	220	-17110	793	-136	0	-81	-7083	15.71	15.71	9.42	9.42	2	0.17	0.01	0.06	0.00	0.00	24.0
13	220	-17070	782	-61	0	-40	-7000	15.71	15.71	9.42	9.42	2	0.17	0.01	0.06	0.00	0.00	24.0
14	220	-17080	1071	-222	0	-128	-8685	15.71	15.71	9.42	9.42	2	0.21	0.01	0.08	0.00	0.00	24.0
15	220	-16960	1036	26	0	8	-8409	15.71	15.71	9.42	9.42	2	0.20	0.01	0.08	0.00	0.00	24.0
16	220	-17110	948	-222	0	-128	-7992	15.71	15.71	9.42	9.42	2	0.20	0.01	0.07	0.00	0.00	24.0
17	220	-17000	913	25	0	8	-7713	15.71	15.71	9.42	9.42	2	0.19	0.01	0.07	0.00	0.00	24.0
18	220	-27550	3893	-271	0	-157	-23008	15.71	15.71	9.42	9.42	3	0.39	0.05	0.27	0.00	0.00	24.0
19	220	-31550	1427	-226	0	-150	-17077	15.71	15.71	9.42	9.42	3	0.29	0.02	0.09	0.00	0.00	24.0
20	220	-28330	2433	3	0	-71	-18465	15.71	15.71	9.42	9.42	3	0.32	0.03	0.17	0.00	0.00	24.0
37	220	-23840	4268	-245	0	-135	-21928	15.71	15.71	9.42	9.42	3	0.38	0.05	0.30	0.00	0.00	24.0
38	220	-30510	157	-170	0	-122	-12037	15.71	15.71	9.42	9.42	3	0.20	0.00	0.01	0.00	0.00	24.0
39	220	-25140	1833	211	0	10	-14350	15.71	15.71	9.42	9.42	3	0.25	0.02	0.13	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	330	-21005	1290	-128	0	62	-9241	15.71	15.71	9.42	9.42	3	0.16	0.02	0.09	0.00	0.00	24.0
2	330	-16120	1202	-135	0	68	-8076	15.71	15.71	9.42	9.42	2	0.20	0.02	0.09	0.00	0.00	24.0
3	330	-16090	1191	-61	0	27	-8006	15.71	15.71	9.42	9.42	2	0.20	0.02	0.09	0.00	0.00	24.0
4	330	-16230	793	-136	0	69	-6211	15.71	15.71	9.42	9.42	2	0.15	0.01	0.06	0.00	0.00	24.0
5	330	-16190	782	-61	0	28	-6139	15.71	15.71	9.42	9.42	2	0.15	0.01	0.06	0.00	0.00	24.0
6	330	-16200	1071	-222	0	116	-7507	15.71	15.71	9.42	9.42	2	0.19	0.01	0.08	0.00	0.00	24.0
7	330	-16080	1036	26	0	-20	-7269	15.71	15.71	9.42	9.42	2	0.18	0.01	0.08	0.00	0.00	24.0
8	330	-16230	948	-222	0	116	-6948	15.71	15.71	9.42	9.42	2	0.17	0.01	0.07	0.00	0.00	24.0
9	330	-16120	913	25	0	-20	-6709	15.71	15.71	9.42	9.42	2	0.16	0.01	0.07	0.00	0.00	24.0
10	330	-16120	1202	-135	0	68	-8076	15.71	15.71	9.42	9.42	2	0.20	0.02	0.09	0.00	0.00	24.0
11	330	-16090	1191	-61	0	27	-8006	15.71	15.71	9.42	9.42	2	0.20	0.02	0.09	0.00	0.00	24.0
12	330	-16230	793	-136	0	69	-6211	15.71	15.71	9.42	9.42	2	0.15	0.01	0.06	0.00	0.00	24.0
13	330	-16190	782	-61	0	28	-6139	15.71	15.71	9.42	9.42	2	0.15	0.01	0.06	0.00	0.00	24.0
14	330	-16200	1071	-222	0	116	-7507	15.71	15.71	9.42	9.42	2	0.19	0.01	0.08	0.00	0.00	24.0
15	330	-16080	1036	26	0	-20	-7269	15.71	15.71	9.42	9.42	2	0.18	0.01	0.08	0.00	0.00	24.0
16	330	-16230	948	-222	0	116	-6948	15.71	15.71	9.42	9.42	2	0.17	0.01	0.07	0.00	0.00	24.0
17	330	-16120	913	25	0	-20	-6709	15.71	15.71	9.42	9.42	2	0.16	0.01	0.07	0.00	0.00	24.0
18	330	-26405	3686	-271	0	141	-18839	15.71	15.71	9.42	9.42	3	0.32	0.05	0.26	0.00	0.00	24.0
19	330	-30405	1635	-226	0	99	-15393	15.71	15.71	9.42	9.42	3	0.26	0.02	0.11	0.00	0.00	24.0
20	330	-27185	2433	3	0	-74	-15787	15.71	15.71	9.42	9.42	3	0.27	0.03	0.17	0.00	0.00	24.0
37	330	-22695	3922	-245	0	135	-17423	15.71	15.71	9.42	9.42	3	0.30	0.05	0.28	0.00	0.00	24.0
38	330	-29365	503	-170	0	66	-11674	15.71	15.71	9.42	9.42	3	0.20	0.01	0.03	0.00	0.00	24.0
39	330	-23995	1833	211	0	-222	-12335	15.71	15.71	9.42	9.42	3	0.22	0.02	0.13	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	440	-19860	1290	-128	0	203	-7822	15.71	15.71	9.42	9.42	3	0.14	0.02	0.10	0.00	0.00	24.0
2	440	-15240	1202	-135	0	216	-6755	15.71	15.71	9.42	9.42	2	0.17	0.02	0.09	0.00	0.00	24.0
3	440	-15210	1191	-61	0	94	-6695	15.71	15.71	9.42	9.42	2	0.17	0.02	0.09	0.00	0.00	24.0
4	440	-15350	793	-136	0	218	-5339	15.71	15.71	9.42	9.42	2	0.14	0.01	0.06	0.00	0.00	24.0
5	440	-15310	782	-61	0	95	-5279	15.71	15.71	9.42	9.42	2	0.13	0.01	0.06	0.00	0.00	24.0
6	440	-15320	1071	-222	0	360	-6329	15.71	15.71	9.42	9.42	2	0.16	0.01	0.08	0.00	0.00	24.0
7	440	-15200	1036	26	0	-48	-6129	15.71	15.71	9.42	9.42	2	0.15	0.01	0.08	0.00	0.00	24.0
8	440	-15350	948	-222	0	360	-5904	15.71	15.71	9.42	9.42	2	0.15	0.01	0.07	0.00	0.00	24.0
9	440	-15240	913	25	0	-48	-5705	15.71	15.71	9.42	9.42	2	0.14	0.01	0.07	0.00	0.00	24.0
10	440	-15240	1202	-135	0	216	-6755	15.71	15.71	9.42	9.42	2	0.17	0.02	0.09	0.00	0.00	24.0

11	440	-15210	1191	-61	0	94	-6695	15.71	15.71	9.42	9.42	2	0.17	0.02	0.09	0.00	0.00	24.0
12	440	-15350	793	-136	0	218	-5339	15.71	15.71	9.42	9.42	2	0.14	0.01	0.06	0.00	0.00	24.0
13	440	-15310	782	-61	0	95	-5279	15.71	15.71	9.42	9.42	2	0.13	0.01	0.06	0.00	0.00	24.0
14	440	-15320	1071	-222	0	360	-6329	15.71	15.71	9.42	9.42	2	0.16	0.01	0.08	0.00	0.00	24.0
15	440	-15200	1036	26	0	-48	-6129	15.71	15.71	9.42	9.42	2	0.15	0.01	0.08	0.00	0.00	24.0
16	440	-15350	948	-222	0	360	-5904	15.71	15.71	9.42	9.42	2	0.15	0.01	0.07	0.00	0.00	24.0
17	440	-15240	913	25	0	-48	-5705	15.71	15.71	9.42	9.42	2	0.14	0.01	0.07	0.00	0.00	24.0
18	440	-25260	3478	-271	0	439	-14900	15.71	15.71	9.42	9.42	3	0.26	0.04	0.24	0.00	0.00	24.0
19	440	-29260	1843	-226	0	348	-13480	15.71	15.71	9.42	9.42	3	0.23	0.02	0.12	0.00	0.00	24.0
20	440	-26040	2433	3	0	-77	-13110	15.71	15.71	9.42	9.42	3	0.23	0.03	0.17	0.00	0.00	24.0
37	440	-21550	3575	-245	0	405	-13300	15.71	15.71	9.42	9.42	3	0.24	0.04	0.26	0.00	0.00	24.0
38	440	-28220	850	-170	0	253	-10930	15.71	15.71	9.42	9.42	3	0.19	0.01	0.06	0.00	0.00	24.0
39	440	-22850	1833	211	0	-454	-10320	15.71	15.71	9.42	9.42	3	0.18	0.02	0.13	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 14 NI 177 NF 178 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 28B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-24340	1147	-144	0	-457	-12500	15.71	15.71	9.42	9.42	3	0.22	0.01	0.08	0.00	0.00	24.0
2	0	-18710	1088	-146	0	-455	-11290	15.71	15.71	9.42	9.42	2	0.28	0.01	0.08	0.00	0.00	24.0
3	0	-18710	1088	-76	0	-258	-11290	15.71	15.71	9.42	9.42	2	0.28	0.01	0.08	0.00	0.00	24.0
4	0	-18730	677	-145	0	-445	-7941	15.71	15.71	9.42	9.42	2	0.20	0.01	0.05	0.00	0.00	24.0
5	0	-18740	677	-75	0	-248	-7941	15.71	15.71	9.42	9.42	2	0.20	0.01	0.05	0.00	0.00	24.0
6	0	-18710	944	-227	0	-682	-10120	15.71	15.71	9.42	9.42	2	0.26	0.01	0.07	0.00	0.00	24.0
7	0	-18720	944	6	0	-24	-10120	15.71	15.71	9.42	9.42	2	0.24	0.01	0.07	0.00	0.00	24.0
8	0	-18720	821	-227	0	-679	-9112	15.71	15.71	9.42	9.42	2	0.23	0.01	0.06	0.00	0.00	24.0
9	0	-18730	820	6	0	-21	-9113	15.71	15.71	9.42	9.42	2	0.22	0.01	0.06	0.00	0.00	24.0
10	0	-18710	1088	-146	0	-455	-11290	15.71	15.71	9.42	9.42	2	0.28	0.01	0.08	0.00	0.00	24.0
11	0	-18710	1088	-76	0	-258	-11290	15.71	15.71	9.42	9.42	2	0.28	0.01	0.08	0.00	0.00	24.0
12	0	-18730	677	-145	0	-445	-7941	15.71	15.71	9.42	9.42	2	0.20	0.01	0.05	0.00	0.00	24.0
13	0	-18740	677	-75	0	-248	-7941	15.71	15.71	9.42	9.42	2	0.20	0.01	0.05	0.00	0.00	24.0
14	0	-18710	944	-227	0	-682	-10120	15.71	15.71	9.42	9.42	2	0.26	0.01	0.07	0.00	0.00	24.0
15	0	-18720	944	6	0	-24	-10120	15.71	15.71	9.42	9.42	2	0.24	0.01	0.07	0.00	0.00	24.0
16	0	-18720	821	-227	0	-679	-9112	15.71	15.71	9.42	9.42	2	0.23	0.01	0.06	0.00	0.00	24.0
17	0	-18730	820	6	0	-21	-9113	15.71	15.71	9.42	9.42	2	0.22	0.01	0.06	0.00	0.00	24.0
18	0	-29740	4051	-327	0	-1008	-30460	15.71	15.71	9.42	9.42	3	0.52	0.05	0.27	0.00	0.00	24.0
19	0	-33540	757	-271	0	-837	-17830	15.71	15.71	9.42	9.42	3	0.30	0.01	0.05	0.00	0.00	24.0
20	0	-30520	2220	-69	0	-319	-22430	15.71	15.71	9.42	9.42	3	0.38	0.03	0.15	0.00	0.00	24.0
37	0	-26130	4738	-295	0	-911	-30870	15.71	15.71	9.42	9.42	3	0.54	0.06	0.33	0.00	0.00	24.0
38	0	-32460	-752	-201	0	-626	-9824	15.71	15.71	9.42	9.42	3	0.17	0.01	0.05	0.00	0.00	24.0
39	0	-27440	1686	136	0	237	-17480	15.71	15.71	9.42	9.42	3	0.30	0.02	0.12	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	110	-23195	1147	-144	0	-299	-11238	15.71	15.71	9.42	9.42	3	0.20	0.01	0.08	0.00	0.00	24.0
2	110	-17830	1088	-146	0	-295	-10093	15.71	15.71	9.42	9.42	2	0.25	0.01	0.08	0.00	0.00	24.0
3	110	-17830	1088	-76	0	-175	-10093	15.71	15.71	9.42	9.42	2	0.25	0.01	0.08	0.00	0.00	24.0
4	110	-17850	677	-145	0	-286	-7197	15.71	15.71	9.42	9.42	2	0.18	0.01	0.05	0.00	0.00	24.0
5	110	-17860	677	-75	0	-165	-7197	15.71	15.71	9.42	9.42	2	0.18	0.01	0.05	0.00	0.00	24.0
6	110	-17830	944	-227	0	-433	-9081	15.71	15.71	9.42	9.42	2	0.23	0.01	0.07	0.00	0.00	24.0
7	110	-17840	944	6	0	-31	-9081	15.71	15.71	9.42	9.42	2	0.22	0.01	0.07	0.00	0.00	24.0
8	110	-17840	821	-227	0	-430	-8210	15.71	15.71	9.42	9.42	2	0.21	0.01	0.06	0.00	0.00	24.0
9	110	-17850	820	6	0	-28	-8211	15.71	15.71	9.42	9.42	2	0.20	0.01	0.06	0.00	0.00	24.0
10	110	-17830	1088	-146	0	-295	-10093	15.71	15.71	9.42	9.42	2	0.25	0.01	0.08	0.00	0.00	24.0
11	110	-17830	1088	-76	0	-175	-10093	15.71	15.71	9.42	9.42	2	0.25	0.01	0.08	0.00	0.00	24.0
12	110	-17850	677	-145	0	-286	-7197	15.71	15.71	9.42	9.42	2	0.18	0.01	0.05	0.00	0.00	24.0
13	110	-17860	677	-75	0	-165	-7197	15.71	15.71	9.42	9.42	2	0.18	0.01	0.05	0.00	0.00	24.0
14	110	-17830	944	-227	0	-433	-9081	15.71	15.71	9.42	9.42	2	0.23	0.01	0.07	0.00	0.00	24.0
15	110	-17840	944	6	0	-31	-9081	15.71	15.71	9.42	9.42	2	0.22	0.01	0.07	0.00	0.00	24.0
16	110	-17840	821	-227	0	-430	-8210	15.71	15.71	9.42	9.42	2	0.21	0.01	0.06	0.00	0.00	24.0
17	110	-17850	820	6	0	-28	-8211	15.71	15.71	9.42	9.42	2	0.20	0.01	0.06	0.00	0.00	24.0
18	110	-28595	3843	-327	0	-648	-26119	15.71	15.71	9.42	9.42	3	0.45	0.05	0.26	0.00	0.00	24.0
19	110	-32395	965	-271	0	-538	-16883	15.71	15.71	9.42	9.42	3	0.29	0.01	0.06	0.00	0.00	24.0
20	110	-29378	2220	-69	0	-243	-19988	15.71	15.71	9.42	9.42	3	0.34	0.03	0.15	0.00	0.00	24.0
37	110	-24985	4392	-295	0	-587	-25848	15.71	15.71	9.42	9.42	3	0.45	0.05	0.31	0.00	0.00	24.0
38	110	-31318	-406	-201	0	-405	-10460	15.71	15.71	9.42	9.42	3	0.18	0.00	0.03	0.00	0.00	24.0
39	110	-26295	1686	136	0	87	-15625	15.71	15.71	9.42	9.42	3	0.27	0.02	0.12	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	220	-22050	1147	-144	0	-141	-9976	15.71	15.71	9.42	9.42	3	0.18	0.01	0.08	0.00	0.00	24.0
2	220	-16950	1088	-146	0	-135	-8896	15.71	15.71	9.42	9.42	2	0.22	0.01	0.08	0.00	0.00	24.0
3	220	-16950	1088	-76	0	-91	-8896	15.71	15.71	9.42	9.42	2	0.22	0.01	0.08	0.00	0.00	24.0
4	220	-16970	677	-145	0	-126	-6452	15.71	15.71	9.42	9.42	2	0.16	0.01	0.05	0.00	0.00	24.0
5	220	-16980	677	-75	0	-83	-6452	15.71	15.71	9.42	9.42	2	0.16	0.01	0.05	0.00	0.00	24.0
6	220	-16950	944	-227	0	-183	-8042	15.71	15.71	9.42	9.42	2	0.20	0.01	0.07	0.00	0.00	24.0
7	220	-16960	944	6	0	-37	-8043	15.71	15.71	9.42	9.42	2	0.20	0.01	0.07	0.00	0.00	24.0
8	220	-16960	821	-227	0	-180	-7307	15.71	15.71	9.42	9.42	2	0.18	0.01	0.06	0.00	0.00	24.0
9	220	-16970	820	6	0	-35	-7308	15.71	15.71	9.42	9.42	2	0.18	0.01	0.06	0.00	0.00	24.0
10	220	-16950	1088	-146	0	-135	-8896	15.71	15.71	9.42	9.42	2	0.22	0.01	0.08	0.00	0.00	24.0
11	220	-16950	1088	-76	0	-91	-8896	15.71	15.71	9.42	9.42	2	0.22	0.01	0.08	0.00	0.00	24.0
12	220	-16970	677	-145	0	-126	-6452	15.71	15.71	9.42	9.42	2	0.16	0.01	0.05	0.00	0.00	24.0
13	220	-16980	677	-75	0	-83	-6452	15.71	15.71	9.42	9.42	2	0.16	0.01	0.05	0.00	0.00	24.0
14	220	-16950	944	-227	0	-183	-8042	15.71	15.71	9.42	9.42	2	0.20	0.01	0.07	0.00	0.00	24.0
15	220	-16960	944	6	0	-37	-8043	15.71	15.71	9.42	9.42	2	0.20	0.01	0.07	0.00	0.00	24.0
16	220	-16960	821	-227	0	-180	-7307	15.71	15.71	9.42	9.42	2	0.18	0.01	0.06	0.00	0.00	24.0
17	220	-16970	820	6	0	-35	-7308	15.71	15.71	9.42	9.42	2	0.18	0.01	0.06	0.00	0.00	24.0
18	220	-27450	3635	-327	0	-288	-22008	15.71	15.71	9.42	9.42	3	0.38	0.05	0.25	0.00	0.00	24.0
19	220	-31250	1173	-271	0	-240	-15707	15.71	15.71	9.42	9.42	3	0.27	0.01	0.08	0.00	0.00	24.0
20	220	-28235	2220	-69	0	-167	-17545	15.71	15.71	9.42	9.42	3	0.30	0.03	0.15	0.00	0.00	24.0
37	220	-23840	4045	-295	0	-263	-21208	15.71	15.71	9.42	9.42	3	0.37	0.05	0.29	0.00	0.00	24.0
38	220	-30175	-59	-201	0	-184	-10714	15.71	15.71	9.42	9.42	3	0.18	0.00	0.01	0.00	0.00	24.0
39	220	-25150	1686	136	0	-62	-13770	15.71	15.71	9.42	9.42	3	0.24	0.02	0.12	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	330	-20905	1147	-144	0	16	-8715	15.71	15.71	9.42	9.42	3	0.15	0.01	0.08	0.00	0.00	24.0
2	330	-16070	1088	-146	0	25	-7699	15.71	15.71	9.42	9.42	2	0.19	0.01	0.08	0.00	0.00	24.0
3	330	-16070	1088	-76	0	-8	-7700	15.71	15.71	9.42	9.42	2	0.19	0.01	0.08	0.00	0.00	24.0
4	330	-16090	677	-145	0	33	-5708	15.71	15.71	9.42	9.42	2	0.14	0.01	0.05	0.00	0.00	24.0
5	330	-16100	677	-75	0	-0	-5708	15.71	15.71	9.42	9.42	2	0.14	0.01	0.05	0.00	0.00	24.0
6	330	-16070	944	-227	0	67	-7002	15.71	15.71	9.42	9.42	2	0.17	0.01	0.07	0.00	0.00	24.0

7	330	-16080	944	6	0	-44	-7004	15.71	15.71	9.42	9.42	2	0.17	0.01	0.07	0.00	0.00	24.0
8	330	-16080	821	-227	0	69	-6404	15.71	15.71	9.42	9.42	2	0.16	0.01	0.06	0.00	0.00	24.0
9	330	-16090	820	6	0	-42	-6406	15.71	15.71	9.42	9.42	2	0.16	0.01	0.06	0.00	0.00	24.0
10	330	-16070	1088	-146	0	25	-7699	15.71	15.71	9.42	9.42	2	0.19	0.01	0.08	0.00	0.00	24.0
11	330	-16070	1088	-76	0	-8	-7700	15.71	15.71	9.42	9.42	2	0.19	0.01	0.08	0.00	0.00	24.0
12	330	-16090	677	-145	0	33	-5708	15.71	15.71	9.42	9.42	2	0.14	0.01	0.05	0.00	0.00	24.0
13	330	-16100	677	-75	0	-0	-5708	15.71	15.71	9.42	9.42	2	0.14	0.01	0.05	0.00	0.00	24.0
14	330	-16070	944	-227	0	67	-7002	15.71	15.71	9.42	9.42	2	0.17	0.01	0.07	0.00	0.00	24.0
15	330	-16080	944	6	0	-44	-7004	15.71	15.71	9.42	9.42	2	0.17	0.01	0.07	0.00	0.00	24.0
16	330	-16080	821	-227	0	69	-6404	15.71	15.71	9.42	9.42	2	0.16	0.01	0.06	0.00	0.00	24.0
17	330	-16090	820	6	0	-42	-6406	15.71	15.71	9.42	9.42	2	0.16	0.01	0.06	0.00	0.00	24.0
18	330	-26305	3428	-327	0	73	-18124	15.71	15.71	9.42	9.42	3	0.31	0.04	0.24	0.00	0.00	24.0
19	330	-30105	1381	-271	0	59	-14303	15.71	15.71	9.42	9.42	3	0.24	0.02	0.09	0.00	0.00	24.0
20	330	-27092	2220	-69	0	-91	-15102	15.71	15.71	9.42	9.42	3	0.26	0.03	0.15	0.00	0.00	24.0
37	330	-22695	3698	-295	0	61	-16948	15.71	15.71	9.42	9.42	3	0.30	0.05	0.27	0.00	0.00	24.0
38	330	-29032	287	-201	0	37	-10588	15.71	15.71	9.42	9.42	3	0.18	0.00	0.02	0.00	0.00	24.0
39	330	-24005	1686	136	0	-212	-11915	15.71	15.71	9.42	9.42	3	0.21	0.02	0.12	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	440	-19760	1147	-144	0	174	-7453	15.71	15.71	9.42	9.42	3	0.13	0.01	0.09	0.00	0.00	24.0
2	440	-15190	1088	-146	0	186	-6502	15.71	15.71	9.42	9.42	2	0.16	0.01	0.08	0.00	0.00	24.0
3	440	-15190	1088	-76	0	75	-6503	15.71	15.71	9.42	9.42	2	0.16	0.01	0.08	0.00	0.00	24.0
4	440	-15210	677	-145	0	192	-4964	15.71	15.71	9.42	9.42	2	0.13	0.01	0.05	0.00	0.00	24.0
5	440	-15220	677	-75	0	82	-4964	15.71	15.71	9.42	9.42	2	0.12	0.01	0.05	0.00	0.00	24.0
6	440	-15190	944	-227	0	317	-5963	15.71	15.71	9.42	9.42	2	0.15	0.01	0.07	0.00	0.00	24.0
7	440	-15200	944	6	0	-51	-5965	15.71	15.71	9.42	9.42	2	0.15	0.01	0.07	0.00	0.00	24.0
8	440	-15200	821	-227	0	319	-5502	15.71	15.71	9.42	9.42	2	0.14	0.01	0.06	0.00	0.00	24.0
9	440	-15210	820	6	0	-49	-5503	15.71	15.71	9.42	9.42	2	0.14	0.01	0.06	0.00	0.00	24.0
10	440	-15190	1088	-146	0	186	-6502	15.71	15.71	9.42	9.42	2	0.16	0.01	0.08	0.00	0.00	24.0
11	440	-15190	1088	-76	0	75	-6503	15.71	15.71	9.42	9.42	2	0.16	0.01	0.08	0.00	0.00	24.0
12	440	-15210	677	-145	0	192	-4964	15.71	15.71	9.42	9.42	2	0.13	0.01	0.05	0.00	0.00	24.0
13	440	-15220	677	-75	0	82	-4964	15.71	15.71	9.42	9.42	2	0.12	0.01	0.05	0.00	0.00	24.0
14	440	-15190	944	-227	0	317	-5963	15.71	15.71	9.42	9.42	2	0.15	0.01	0.07	0.00	0.00	24.0
15	440	-15200	944	6	0	-51	-5965	15.71	15.71	9.42	9.42	2	0.15	0.01	0.07	0.00	0.00	24.0
16	440	-15200	821	-227	0	319	-5502	15.71	15.71	9.42	9.42	2	0.14	0.01	0.06	0.00	0.00	24.0
17	440	-15210	820	6	0	-49	-5503	15.71	15.71	9.42	9.42	2	0.14	0.01	0.06	0.00	0.00	24.0
18	440	-25160	3220	-327	0	433	-14470	15.71	15.71	9.42	9.42	3	0.25	0.04	0.23	0.00	0.00	24.0
19	440	-28960	1589	-271	0	357	-12670	15.71	15.71	9.42	9.42	3	0.22	0.02	0.11	0.00	0.00	24.0
20	440	-25950	2220	-69	0	-15	-12660	15.71	15.71	9.42	9.42	3	0.22	0.03	0.16	0.00	0.00	24.0
37	440	-21550	3352	-295	0	385	-13070	15.71	15.71	9.42	9.42	3	0.23	0.04	0.24	0.00	0.00	24.0
38	440	-27890	634	-201	0	258	-10080	15.71	15.71	9.42	9.42	3	0.17	0.01	0.04	0.00	0.00	24.0
39	440	-22860	1686	136	0	-362	-10060	15.71	15.71	9.42	9.42	3	0.18	0.02	0.12	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 15 NI 220 NF 221 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 27B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-21240	-483	-309	0	-602	-5870	15.71	15.71	9.42	9.42	3	0.11	0.01	0.04	0.00	0.00	24.0
2	0	-16180	-340	-263	0	-541	-5753	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
3	0	-16330	-342	-194	0	-352	-5866	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
4	0	-16350	-401	-281	0	-575	-3164	15.71	15.71	9.42	9.42	2	0.09	0.01	0.03	0.00	0.00	24.0
5	0	-16500	-403	-212	0	-385	-3277	15.71	15.71	9.42	9.42	2	0.09	0.01	0.03	0.00	0.00	24.0
6	0	-16070	-359	-350	0	-775	-4716	15.71	15.71	9.42	9.42	2	0.13	0.00	0.03	0.00	0.00	24.0
7	0	-16550	-366	-119	0	-142	-5092	15.71	15.71	9.42	9.42	2	0.13	0.00	0.03	0.00	0.00	24.0
8	0	-16120	-377	-356	0	-785	-3939	15.71	15.71	9.42	9.42	2	0.12	0.00	0.03	0.00	0.00	24.0
9	0	-16610	-384	-125	0	-152	-4315	15.71	15.71	9.42	9.42	2	0.11	0.00	0.03	0.00	0.00	24.0
10	0	-16180	-340	-263	0	-541	-5753	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
11	0	-16330	-342	-194	0	-352	-5866	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
12	0	-16350	-401	-281	0	-575	-3164	15.71	15.71	9.42	9.42	2	0.09	0.01	0.03	0.00	0.00	24.0
13	0	-16500	-403	-212	0	-385	-3277	15.71	15.71	9.42	9.42	2	0.09	0.01	0.03	0.00	0.00	24.0
14	0	-16070	-359	-350	0	-775	-4716	15.71	15.71	9.42	9.42	2	0.13	0.00	0.03	0.00	0.00	24.0
15	0	-16550	-366	-119	0	-142	-5092	15.71	15.71	9.42	9.42	2	0.13	0.00	0.03	0.00	0.00	24.0
16	0	-16120	-377	-356	0	-785	-3939	15.71	15.71	9.42	9.42	2	0.12	0.00	0.03	0.00	0.00	24.0
17	0	-16610	-384	-125	0	-152	-4315	15.71	15.71	9.42	9.42	2	0.11	0.00	0.03	0.00	0.00	24.0
18	0	-24610	218	-431	0	-1041	-16730	15.71	15.71	9.42	9.42	3	0.30	0.01	0.02	0.00	0.00	24.0
19	0	-28990	-1598	-464	0	-1059	-7230	15.71	15.71	9.42	9.42	3	0.13	0.02	0.11	0.00	0.00	24.0
20	0	-26340	-672	-225	0	-480	-11370	15.71	15.71	9.42	9.42	3	0.20	0.01	0.05	0.00	0.00	24.0
37	0	-21370	890	-376	0	-890	-17900	15.71	15.71	9.42	9.42	3	0.32	0.01	0.07	0.00	0.00	24.0
38	0	-28670	-2135	-430	0	-920	-2068	15.71	15.71	9.42	9.42	3	0.05	0.03	0.15	0.00	0.00	24.0
39	0	-24270	-593	-32	0	44	-8970	15.71	15.71	9.42	9.42	3	0.16	0.01	0.04	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	110	-20095	-483	-309	0	-262	-6401	15.71	15.71	9.42	9.42	3	0.11	0.01	0.04	0.00	0.00	24.0
2	110	-15300	-340	-263	0	-252	-6127	15.71	15.71	9.42	9.42	2	0.16	0.00	0.03	0.00	0.00	24.0
3	110	-15450	-342	-194	0	-138	-6242	15.71	15.71	9.42	9.42	2	0.16	0.00	0.03	0.00	0.00	24.0
4	110	-15470	-401	-281	0	-266	-3605	15.71	15.71	9.42	9.42	2	0.09	0.01	0.03	0.00	0.00	24.0
5	110	-15620	-403	-212	0	-152	-3720	15.71	15.71	9.42	9.42	2	0.09	0.01	0.03	0.00	0.00	24.0
6	110	-15190	-359	-350	0	-389	-5111	15.71	15.71	9.42	9.42	2	0.13	0.00	0.03	0.00	0.00	24.0
7	110	-15670	-366	-119	0	-10	-5494	15.71	15.71	9.42	9.42	2	0.14	0.00	0.03	0.00	0.00	24.0
8	110	-15240	-377	-356	0	-393	-4354	15.71	15.71	9.42	9.42	2	0.12	0.00	0.03	0.00	0.00	24.0
9	110	-15730	-384	-125	0	-15	-4737	15.71	15.71	9.42	9.42	2	0.12	0.00	0.03	0.00	0.00	24.0
10	110	-15300	-340	-263	0	-252	-6127	15.71	15.71	9.42	9.42	2	0.16	0.00	0.03	0.00	0.00	24.0
11	110	-15450	-342	-194	0	-138	-6242	15.71	15.71	9.42	9.42	2	0.16	0.00	0.03	0.00	0.00	24.0
12	110	-15470	-401	-281	0	-266	-3605	15.71	15.71	9.42	9.42	2	0.09	0.01	0.03	0.00	0.00	24.0
13	110	-15620	-403	-212	0	-152	-3720	15.71	15.71	9.42	9.42	2	0.09	0.01	0.03	0.00	0.00	24.0
14	110	-15190	-359	-350	0	-389	-5111	15.71	15.71	9.42	9.42	2	0.13	0.00	0.03	0.00	0.00	24.0
15	110	-15670	-366	-119	0	-10	-5494	15.71	15.71	9.42	9.42	2	0.14	0.00	0.03	0.00	0.00	24.0
16	110	-15240	-377	-356	0	-393	-4354	15.71	15.71	9.42	9.42	2	0.12	0.00	0.03	0.00	0.00	24.0
17	110	-15730	-384	-125	0	-15	-4737	15.71	15.71	9.42	9.42	2	0.12	0.00	0.03	0.00	0.00	24.0
18	110	-23465	10	-431	0	-567	-16604	15.71	15.71	9.42	9.42	3	0.29	0.01	0.03	0.00	0.00	24.0
19	110	-27845	-1390	-464	0	-549	-8873	15.71	15.71	9.42	9.42	3	0.15	0.02	0.10	0.00	0.00	24.0
20	110	-25198	-672	-225	0	-232	-12110	15.71	15.71	9.42	9.42	3	0.21	0.01	0.05	0.00	0.00	24.0
37	110	-20228	543	-376	0	-477	-17111	15.71	15.71	9.42	9.42	3	0.30	0.01	0.04	0.00	0.00	24.0
38	110	-27528	-1789	-430	0	-447	-4226	15.71	15.71	9.42	9.42	3	0.08	0.02	0.12	0.00	0.00	24.0
39	110	-23125	-593	-32	0	79	-9622	15.71	15.71	9.42	9.42	3	0.17	0.01	0.04	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	220	-18950	-483	-309	0	77	-6932	15.71	15.71	9.42	9.42	3	0.12	0.01	0.04	0.00	0.00	24.0
2	220	-14420	-340	-263	0	38	-6501	15.71	15.71	9.42	9.42	2	0.16	0.00	0.03	0.00	0.00	24.0

3	220	-14570	-342	-194	0	75	-6618	15.71	15.71	9.42	9.42	2	0.17	0.00	0.03	0.00	0.00	24.0
4	220	-14590	-401	-281	0	44	-4046	15.71	15.71	9.42	9.42	2	0.10	0.01	0.03	0.00	0.00	24.0
5	220	-14740	-403	-212	0	81	-4164	15.71	15.71	9.42	9.42	2	0.10	0.01	0.03	0.00	0.00	24.0
6	220	-14310	-359	-350	0	-4	-5506	15.71	15.71	9.42	9.42	2	0.14	0.00	0.03	0.00	0.00	24.0
7	220	-14790	-366	-119	0	121	-5896	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
8	220	-14360	-377	-356	0	-2	-4769	15.71	15.71	9.42	9.42	2	0.12	0.00	0.03	0.00	0.00	24.0
9	220	-14850	-384	-125	0	123	-5159	15.71	15.71	9.42	9.42	2	0.13	0.00	0.03	0.00	0.00	24.0
10	220	-14420	-340	-263	0	38	-6501	15.71	15.71	9.42	9.42	2	0.16	0.00	0.03	0.00	0.00	24.0
11	220	-14570	-342	-194	0	75	-6618	15.71	15.71	9.42	9.42	2	0.17	0.00	0.03	0.00	0.00	24.0
12	220	-14590	-401	-281	0	44	-4046	15.71	15.71	9.42	9.42	2	0.10	0.01	0.03	0.00	0.00	24.0
13	220	-14740	-403	-212	0	81	-4164	15.71	15.71	9.42	9.42	2	0.10	0.01	0.03	0.00	0.00	24.0
14	220	-14310	-359	-350	0	-4	-5506	15.71	15.71	9.42	9.42	2	0.14	0.00	0.03	0.00	0.00	24.0
15	220	-14790	-366	-119	0	121	-5896	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
16	220	-14360	-377	-356	0	-2	-4769	15.71	15.71	9.42	9.42	2	0.12	0.00	0.03	0.00	0.00	24.0
17	220	-14850	-384	-125	0	123	-5159	15.71	15.71	9.42	9.42	2	0.13	0.00	0.03	0.00	0.00	24.0
18	220	-22320	-198	-431	0	-92	-16708	15.71	15.71	9.42	9.42	3	0.29	0.01	0.03	0.00	0.00	24.0
19	220	-26700	-1182	-464	0	-38	-10287	15.71	15.71	9.42	9.42	3	0.18	0.01	0.08	0.00	0.00	24.0
20	220	-24055	-672	-225	0	15	-12850	15.71	15.71	9.42	9.42	3	0.22	0.01	0.05	0.00	0.00	24.0
37	220	-19085	197	-376	0	-64	-16703	15.71	15.71	9.42	9.42	3	0.30	0.01	0.02	0.00	0.00	24.0
38	220	-26385	-1442	-430	0	26	-6003	15.71	15.71	9.42	9.42	3	0.10	0.02	0.10	0.00	0.00	24.0
39	220	-21980	-593	-32	0	115	-10275	15.71	15.71	9.42	9.42	3	0.18	0.01	0.04	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	330	-17805	-483	-309	0	417	-7464	15.71	15.71	9.42	9.42	3	0.14	0.01	0.04	0.00	0.00	24.0
2	330	-13540	-340	-263	0	327	-6875	15.71	15.71	9.42	9.42	2	0.18	0.00	0.03	0.00	0.00	24.0
3	330	-13690	-342	-194	0	288	-6994	15.71	15.71	9.42	9.42	2	0.18	0.00	0.03	0.00	0.00	24.0
4	330	-13710	-401	-281	0	353	-4488	15.71	15.71	9.42	9.42	2	0.12	0.01	0.03	0.00	0.00	24.0
5	330	-13860	-403	-212	0	314	-4607	15.71	15.71	9.42	9.42	2	0.12	0.01	0.03	0.00	0.00	24.0
6	330	-13430	-359	-350	0	381	-5900	15.71	15.71	9.42	9.42	2	0.16	0.00	0.03	0.00	0.00	24.0
7	330	-13910	-366	-119	0	252	-6298	15.71	15.71	9.42	9.42	2	0.16	0.00	0.03	0.00	0.00	24.0
8	330	-13480	-377	-356	0	389	-5184	15.71	15.71	9.42	9.42	2	0.14	0.00	0.03	0.00	0.00	24.0
9	330	-13970	-384	-125	0	260	-5582	15.71	15.71	9.42	9.42	2	0.14	0.00	0.03	0.00	0.00	24.0
10	330	-13540	-340	-263	0	327	-6875	15.71	15.71	9.42	9.42	2	0.18	0.00	0.03	0.00	0.00	24.0
11	330	-13690	-342	-194	0	288	-6994	15.71	15.71	9.42	9.42	2	0.18	0.00	0.03	0.00	0.00	24.0
12	330	-13710	-401	-281	0	353	-4488	15.71	15.71	9.42	9.42	2	0.12	0.01	0.03	0.00	0.00	24.0
13	330	-13860	-403	-212	0	314	-4607	15.71	15.71	9.42	9.42	2	0.12	0.01	0.03	0.00	0.00	24.0
14	330	-13430	-359	-350	0	381	-5900	15.71	15.71	9.42	9.42	2	0.16	0.00	0.03	0.00	0.00	24.0
15	330	-13910	-366	-119	0	252	-6298	15.71	15.71	9.42	9.42	2	0.16	0.00	0.03	0.00	0.00	24.0
16	330	-13480	-377	-356	0	389	-5184	15.71	15.71	9.42	9.42	2	0.14	0.00	0.03	0.00	0.00	24.0
17	330	-13970	-384	-125	0	260	-5582	15.71	15.71	9.42	9.42	2	0.14	0.00	0.03	0.00	0.00	24.0
18	330	-21175	-406	-431	0	382	-17039	15.71	15.71	9.42	9.42	3	0.30	0.01	0.03	0.00	0.00	24.0
19	330	-25555	-974	-464	0	472	-11473	15.71	15.71	9.42	9.42	3	0.20	0.01	0.07	0.00	0.00	24.0
20	330	-22912	-672	-225	0	263	-13590	15.71	15.71	9.42	9.42	3	0.24	0.01	0.05	0.00	0.00	24.0
37	330	-17942	-150	-376	0	350	-16676	15.71	15.71	9.42	9.42	3	0.30	0.01	0.02	0.00	0.00	24.0
38	330	-25242	-1096	-430	0	499	-7399	15.71	15.71	9.42	9.42	3	0.13	0.01	0.08	0.00	0.00	24.0
39	330	-20835	-593	-32	0	150	-10928	15.71	15.71	9.42	9.42	3	0.19	0.01	0.04	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	440	-16660	-483	-309	0	756	-7995	15.71	15.71	9.42	9.42	3	0.15	0.01	0.04	0.00	0.00	24.0
2	440	-12660	-340	-263	0	616	-7249	15.71	15.71	9.42	9.42	2	0.20	0.00	0.03	0.00	0.00	24.0
3	440	-12810	-342	-194	0	501	-7370	15.71	15.71	9.42	9.42	2	0.20	0.00	0.03	0.00	0.00	24.0
4	440	-12830	-401	-281	0	662	-4929	15.71	15.71	9.42	9.42	2	0.14	0.01	0.03	0.00	0.00	24.0
5	440	-12980	-403	-212	0	547	-5051	15.71	15.71	9.42	9.42	2	0.14	0.01	0.03	0.00	0.00	24.0
6	440	-12550	-359	-350	0	767	-6295	15.71	15.71	9.42	9.42	2	0.18	0.00	0.03	0.00	0.00	24.0
7	440	-13030	-366	-119	0	383	-6700	15.71	15.71	9.42	9.42	2	0.18	0.00	0.03	0.00	0.00	24.0
8	440	-12600	-377	-356	0	780	-5599	15.71	15.71	9.42	9.42	2	0.16	0.00	0.03	0.00	0.00	24.0
9	440	-13090	-384	-125	0	397	-6004	15.71	15.71	9.42	9.42	2	0.16	0.00	0.03	0.00	0.00	24.0
10	440	-12660	-340	-263	0	616	-7249	15.71	15.71	9.42	9.42	2	0.20	0.00	0.03	0.00	0.00	24.0
11	440	-12810	-342	-194	0	501	-7370	15.71	15.71	9.42	9.42	2	0.20	0.00	0.03	0.00	0.00	24.0
12	440	-12830	-401	-281	0	662	-4929	15.71	15.71	9.42	9.42	2	0.14	0.01	0.03	0.00	0.00	24.0
13	440	-12980	-403	-212	0	547	-5051	15.71	15.71	9.42	9.42	2	0.14	0.01	0.03	0.00	0.00	24.0
14	440	-12550	-359	-350	0	767	-6295	15.71	15.71	9.42	9.42	2	0.18	0.00	0.03	0.00	0.00	24.0
15	440	-13030	-366	-119	0	383	-6700	15.71	15.71	9.42	9.42	2	0.18	0.00	0.03	0.00	0.00	24.0
16	440	-12600	-377	-356	0	780	-5599	15.71	15.71	9.42	9.42	2	0.16	0.00	0.03	0.00	0.00	24.0
17	440	-13090	-384	-125	0	397	-6004	15.71	15.71	9.42	9.42	2	0.16	0.00	0.03	0.00	0.00	24.0
18	440	-20030	-614	-431	0	857	-17600	15.71	15.71	9.42	9.42	3	0.32	0.01	0.05	0.00	0.00	24.0
19	440	-24410	-766	-464	0	983	-12430	15.71	15.71	9.42	9.42	3	0.22	0.01	0.05	0.00	0.00	24.0
20	440	-21770	-672	-225	0	511	-14330	15.71	15.71	9.42	9.42	3	0.25	0.01	0.05	0.00	0.00	24.0
37	440	-16800	-496	-376	0	763	-17030	15.71	15.71	9.42	9.42	3	0.31	0.01	0.04	0.00	0.00	24.0
38	440	-24100	-749	-430	0	973	-8414	15.71	15.71	9.42	9.42	3	0.15	0.01	0.05	0.00	0.00	24.0
39	440	-19690	-593	-32	0	186	-11580	15.71	15.71	9.42	9.42	3	0.21	0.01	0.04	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 16 NI 263 NF 264 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 25B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-21630	95	-159	0	-499	86	6.28	6.28	9.42	9.42	3	0.02	0.00	0.02	0.00	0.00	24.0
2	0	-17810	227	-189	0	-538	-265	6.28	6.28	9.42	9.42	2	0.05	0.01	0.02	0.00	0.00	24.0
3	0	-17630	226	-80	0	-286	-264	6.28	6.28	9.42	9.42	2	0.04	0.01	0.02	0.00	0.00	24.0
4	0	-15650	-81	-164	0	-483	396	6.28	6.28	9.42	9.42	2	0.06	0.00	0.02	0.00	0.00	24.0
5	0	-15470	-81	-55	0	-230	397	6.28	6.28	9.42	9.42	2	0.05	0.00	0.01	0.00	0.00	24.0
6	0	-17260	120	-308	0	-813	-34	6.28	6.28	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
7	0	-16670	118	56	0	28	-31	6.28	6.28	9.42	9.42	2	0.00	0.00	0.01	0.00	0.00	24.0
8	0	-16610	28	-300	0	-796	164	6.28	6.28	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
9	0	-16020	26	64	0	45	167	6.28	6.28	9.42	9.42	2	0.02	0.00	0.01	0.00	0.00	24.0
10	0	-17810	227	-189	0	-538	-265	6.28	6.28	9.42	9.42	2	0.05	0.01	0.02	0.00	0.00	24.0
11	0	-17630	226	-80	0	-286	-264	6.28	6.28	9.42	9.42	2	0.04	0.01	0.02	0.00	0.00	24.0
12	0	-15650	-81	-164	0	-483	396	6.28	6.28	9.42	9.42	2	0.06	0.00	0.02	0.00	0.00	24.0
13	0	-15470	-81	-55	0	-230	397	6.28	6.28	9.42	9.42	2	0.05	0.00	0.01	0.00	0.00	24.0
14	0	-17260	120	-308	0	-813	-34	6.28	6.28	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
15	0	-16670	118	56	0	28	-31	6.28	6.28	9.42	9.42	2	0.00	0.00	0.01	0.00	0.00	24.0
16	0	-16610	28	-300	0	-796	164	6.28	6.28	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
17	0	-16020	26	64	0	45	167	6.28	6.28	9.42	9.42	2	0.02	0.00	0.01	0.00	0.00	24.0
18	0	-26780	715	-546	0	-1362	-911	6.28	6.28	9.42	9.42	3	0.10	0.02	0.06	0.00	0.00	24.0
19	0	-22340	-581	-418	0	-1070	1271	6.28	6.28	9.42	9.42	3	0.12	0.01	0.05	0.00	0.00	24.0
20	0	-23840	75	-369	0	-590	158	6.28	6.28	9.42	9.42	3	0.03	0.01	0.04	0.00	0.00	24.0
37	0	-27190	1156	-487	0	-1232	-1668	6.28	6.28	9.42	9.42	3	0.15	0.03	0.10	0.00	0.00	24.0
38	0	-19780	-1005	-273	0	-745	1968	6.28	6.28	9.42	9.42	3	0.19	0.02	0.10	0.00	0.00	24.0
39	0	-22280	90	-192	0	54	112	6.28	6.28	9.42	9.42	3	0.01	0.00	0.02	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	97	-21060	95	-159	0	-345	179	6.28	6.28	9.42	9.42	3	0.02	0.00	0.02	0.00	0.00	24.0
2	97	-17370	227	-189	0	-354	-43	6.28	6.28	9.42	9.42	2	0.02	0.01	0.02	0.00	0.00	24.0
3	97	-17192	226	-80	0	-208	-43	6.28	6.28	9.42	9.42	2	0.01	0.01	0.02	0.00	0.00	24.0
4	97	-15210	-81	-164	0	-323	318	6.28	6.28	9.42	9.42	2	0.04	0.00	0.02	0.00	0.00	24.0
5	97	-15030	-81	-55	0	-177	318	6.28	6.28	9.42	9.42	2	0.04	0.00	0.01	0.00	0.00	24.0
6	97	-16820	120	-308	0	-513	82	6.28	6.28	9.42	9.42	2	0.03	0.01	0.03	0.00	0.00	24.0
7	97	-16232	118	56	0	-26	84	6.28	6.28	9.42	9.42	2	0.01	0.00	0.01	0.00	0.00	24.0
8	97	-16170	28	-300	0	-504	191	6.28	6.28	9.42	9.42	2	0.04	0.01	0.03	0.00	0.00	24.0
9	97	-15582	26	64	0	-17	192	6.28	6.28	9.42	9.42	2	0.02	0.00	0.01	0.00	0.00	24.0
10	97	-17370	227	-189	0	-354	-43	6.28	6.28	9.42	9.42	2	0.02	0.01	0.02	0.00	0.00	24.0
11	97	-17192	226	-80	0	-208	-43	6.28	6.28	9.42	9.42	2	0.01	0.01	0.02	0.00	0.00	24.0
12	97	-15210	-81	-164	0	-323	318	6.28	6.28	9.42	9.42	2	0.04	0.00	0.02	0.00	0.00	24.0
13	97	-15030	-81	-55	0	-177	318	6.28	6.28	9.42	9.42	2	0.04	0.00	0.01	0.00	0.00	24.0
14	97	-16820	120	-308	0	-513	82	6.28	6.28	9.42	9.42	2	0.03	0.01	0.03	0.00	0.00	24.0
15	97	-16232	118	56	0	-26	84	6.28	6.28	9.42	9.42	2	0.01	0.00	0.01	0.00	0.00	24.0
16	97	-16170	28	-300	0	-504	191	6.28	6.28	9.42	9.42	2	0.04	0.01	0.03	0.00	0.00	24.0
17	97	-15582	26	64	0	-17	192	6.28	6.28	9.42	9.42	2	0.02	0.00	0.01	0.00	0.00	24.0
18	97	-26210	623	-546	0	-829	-259	6.28	6.28	9.42	9.42	3	0.04	0.01	0.05	0.00	0.00	24.0
19	97	-21770	-489	-418	0	-663	749	6.28	6.28	9.42	9.42	3	0.07	0.01	0.05	0.00	0.00	24.0
20	97	-23270	75	-239	0	-295	231	6.28	6.28	9.42	9.42	3	0.02	0.01	0.02	0.00	0.00	24.0
37	97	-26618	1002	-487	0	-757	-616	6.28	6.28	9.42	9.42	3	0.06	0.02	0.08	0.00	0.00	24.0
38	97	-19210	-851	-273	0	-479	1063	6.28	6.28	9.42	9.42	3	0.10	0.02	0.08	0.00	0.00	24.0
39	97	-21710	90	25	0	133	200	6.28	6.28	9.42	9.42	3	0.02	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	195	-20490	95	-159	0	-190	271	6.28	6.28	9.42	9.42	3	0.03	0.00	0.02	0.00	0.00	24.0
2	195	-16930	227	-189	0	-170	178	6.28	6.28	9.42	9.42	2	0.02	0.01	0.02	0.00	0.00	24.0
3	195	-16755	226	-80	0	-130	178	6.28	6.28	9.42	9.42	2	0.02	0.01	0.02	0.00	0.00	24.0
4	195	-14770	-81	-164	0	-163	239	6.28	6.28	9.42	9.42	2	0.03	0.00	0.02	0.00	0.00	24.0
5	195	-14590	-81	-55	0	-123	239	6.28	6.28	9.42	9.42	2	0.03	0.00	0.01	0.00	0.00	24.0
6	195	-16380	120	-308	0	-213	199	6.28	6.28	9.42	9.42	2	0.03	0.01	0.03	0.00	0.00	24.0
7	195	-15795	118	56	0	-81	199	6.28	6.28	9.42	9.42	2	0.02	0.00	0.01	0.00	0.00	24.0
8	195	-15730	28	-300	0	-211	218	6.28	6.28	9.42	9.42	2	0.03	0.01	0.03	0.00	0.00	24.0
9	195	-15145	26	64	0	-79	218	6.28	6.28	9.42	9.42	2	0.02	0.00	0.01	0.00	0.00	24.0
10	195	-16930	227	-189	0	-170	178	6.28	6.28	9.42	9.42	2	0.02	0.01	0.02	0.00	0.00	24.0
11	195	-16755	226	-80	0	-130	178	6.28	6.28	9.42	9.42	2	0.02	0.01	0.02	0.00	0.00	24.0
12	195	-14770	-81	-164	0	-163	239	6.28	6.28	9.42	9.42	2	0.03	0.00	0.02	0.00	0.00	24.0
13	195	-14590	-81	-55	0	-123	239	6.28	6.28	9.42	9.42	2	0.03	0.00	0.01	0.00	0.00	24.0
14	195	-16380	120	-308	0	-213	199	6.28	6.28	9.42	9.42	2	0.03	0.01	0.03	0.00	0.00	24.0
15	195	-15795	118	56	0	-81	199	6.28	6.28	9.42	9.42	2	0.02	0.00	0.01	0.00	0.00	24.0
16	195	-15730	28	-300	0	-211	218	6.28	6.28	9.42	9.42	2	0.03	0.01	0.03	0.00	0.00	24.0
17	195	-15145	26	64	0	-79	218	6.28	6.28	9.42	9.42	2	0.02	0.00	0.01	0.00	0.00	24.0
18	195	-25640	531	-546	0	-297	304	6.28	6.28	9.42	9.42	3	0.03	0.01	0.05	0.00	0.00	24.0
19	195	-21200	-397	-418	0	-255	317	6.28	6.28	9.42	9.42	3	0.03	0.01	0.04	0.00	0.00	24.0
20	195	-22700	75	-127	0	-119	305	6.28	6.28	9.42	9.42	3	0.03	0.00	0.01	0.00	0.00	24.0
37	195	-26045	849	-487	0	-281	286	6.28	6.28	9.42	9.42	3	0.03	0.02	0.08	0.00	0.00	24.0
38	195	-18640	-698	-273	0	-212	308	6.28	6.28	9.42	9.42	3	0.03	0.02	0.07	0.00	0.00	24.0
39	195	-21140	90	212	0	15	287	6.28	6.28	9.42	9.42	3	0.03	0.00	0.02	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	292	-19920	95	-159	0	-36	363	6.28	6.28	9.42	9.42	3	0.03	0.00	0.02	0.00	0.00	24.0
2	292	-16490	227	-189	0	14	399	6.28	6.28	9.42	9.42	2	0.04	0.01	0.02	0.00	0.00	24.0
3	292	-16318	226	-80	0	-52	399	6.28	6.28	9.42	9.42	2	0.04	0.01	0.02	0.00	0.00	24.0
4	292	-14330	-81	-164	0	-3	160	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
5	292	-14150	-81	-55	0	-69	160	6.28	6.28	9.42	9.42	2	0.02	0.00	0.01	0.00	0.00	24.0
6	292	-15940	120	-308	0	86	316	6.28	6.28	9.42	9.42	2	0.03	0.01	0.03	0.00	0.00	24.0
7	292	-15358	118	56	0	-136	314	6.28	6.28	9.42	9.42	2	0.04	0.00	0.01	0.00	0.00	24.0
8	292	-15290	28	-300	0	81	245	6.28	6.28	9.42	9.42	2	0.03	0.01	0.03	0.00	0.00	24.0
9	292	-14708	26	64	0	-141	243	6.28	6.28	9.42	9.42	2	0.03	0.00	0.01	0.00	0.00	24.0
10	292	-16490	227	-189	0	14	399	6.28	6.28	9.42	9.42	2	0.04	0.01	0.02	0.00	0.00	24.0
11	292	-16318	226	-80	0	-52	399	6.28	6.28	9.42	9.42	2	0.04	0.01	0.02	0.00	0.00	24.0
12	292	-14330	-81	-164	0	-3	160	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
13	292	-14150	-81	-55	0	-69	160	6.28	6.28	9.42	9.42	2	0.02	0.00	0.01	0.00	0.00	24.0
14	292	-15940	120	-308	0	86	316	6.28	6.28	9.42	9.42	2	0.03	0.01	0.03	0.00	0.00	24.0
15	292	-15358	118	56	0	-136	314	6.28	6.28	9.42	9.42	2	0.04	0.00	0.01	0.00	0.00	24.0
16	292	-15290	28	-300	0	81	245	6.28	6.28	9.42	9.42	2	0.03	0.01	0.03	0.00	0.00	24.0
17	292	-14708	26	64	0	-141	243	6.28	6.28	9.42	9.42	2	0.03	0.00	0.01	0.00	0.00	24.0
18	292	-25070	439	-546	0	236	776	6.28	6.28	9.42	9.42	3	0.07	0.01	0.05	0.00	0.00	24.0
19	292	-20630	-305	-418	0	152	-25	6.28	6.28	9.42	9.42	3	0.01	0.01	0.04	0.00	0.00	24.0
20	292	-22130	75	-34	0	-42	378	6.28	6.28	9.42	9.42	3	0.03	0.00	0.01	0.00	0.00	24.0
37	292	-25472	695	-487	0	194	1038	6.28	6.28	9.42	9.42	3	0.09	0.02	0.06	0.00	0.00	24.0
38	292	-18070	-544	-273	0	54	-298	6.28	6.28	9.42	9.42	3	0.03	0.01	0.05	0.00	0.00	24.0
39	292	-20570	90	367	0	-270	375	6.28	6.28	9.42	9.42	3	0.04	0.01	0.04	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	390	-19350	95	-159	0	119	456	6.28	6.28	9.42	9.42	3	0.04	0.00	0.02	0.00	0.00	24.0
2	390	-16050	227	-189	0	199	620	6.28	6.28	9.42	9.42	2	0.07	0.01	0.02	0.00	0.00	24.0
3	390	-15880	226	-80	0	26	619	6.28	6.28	9.42	9.42	2	0.06	0.01	0.02	0.00	0.00	24.0
4	390	-13890	-81	-164	0	158	82	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
5	390	-13710	-81	-55	0	-16	81	6.28	6.28	9.42	9.42	2	0.01	0.00	0.01	0.00	0.00	24.0
6	390	-15500	120	-308	0	386	433	6.28	6.28	9.42	9.42	2	0.06	0.01	0.03	0.00	0.00	24.0
7	390	-14920	118	56	0	-191	430	6.28	6.28	9.42	9.42	2	0.05	0.00	0.01	0.00	0.00	24.0
8	390	-14850	28	-300	0	374	272	6.28	6.28	9.42	9.42	2	0.04	0.01	0.03	0.00	0.00	24.0
9	390	-14270	26	64	0	-203	268	6.28	6.28	9.42	9.42	2	0.03	0.00	0.01	0.00	0.00	24.0
10	390	-16050	227	-189	0	199	620	6.28	6.28	9.42	9.42	2	0.07	0.01	0.02	0.00	0.00	24.0
11	390	-15880	226	-80	0	26	619	6.28	6.28	9.42	9.42	2	0.06	0.01	0.02	0.00	0.00	24.0
12	390	-13890	-81	-164	0	158	82	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
13	390	-13710	-81	-55	0	-16	81	6.28	6.28	9.42	9.42	2	0.01	0.00	0.01	0.00	0.00	24.0
14	390	-15500	120	-308	0	386	433	6.28	6.28	9.42	9.42	2	0.06	0.01	0.03	0.00	0.00	24.0
15	390	-14920	118	56	0	-191	430	6.28	6.28	9.42	9.42	2	0.05	0.00	0.01	0.00	0.00	24.0
16	390	-14850	28	-300	0	374	272	6.28	6.28	9.42	9.42	2	0.04	0.01	0.03	0.00	0.00	24.0
17	390	-14270	26	64	0	-203	268	6.28	6.28	9.42	9.42	2	0.03	0.00	0.01	0.00	0.00	24.0
18	390	-24500	346	-546	0	769	1159	6.28	6.28	9.42	9.42	3	0.11	0.01	0.05	0.00	0.00	24.0
19	390	-20060	-213	-418	0	559	-278	6.28	6.28	9.42	9.42	3	0.03	0.01	0.04	0.00	0.00	24.0
20	390	-21560	75	41	0	-47	452	6.28	6.28	9.42	9.42	3	0.04	0.00	0.01	0.00	0.00	24.0
37	390	-24900	542	-487	0	669	1641	6.28	6.28	9.42	9.42	3	0.15	0.01	0.05	0.00	0.00	24.0
38	390	-17500	-391	-273	0	320	-753	6.28	6.28	9.42	9.42	3	0.07	0.01	0.04	0.00	0.00	24.0
39	390	-20000	90	491	0	-690	462	6.28	6.28	9.42	9.42	3	0.05	0.01	0.05	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

VERIFICA NODO IN TESTA AL PILASTRO, NODO NUM. 264 NON CONFINATO

(par.7.2.2 NTC2018 "La domanda di resistenza valutata con i criteri della progettazione in capacità può essere assunta non superiore alla domanda di resistenza valutata per il caso di comportamento strutturale non dissipativo.")

PROGETTAZIONE IN CAPACITA'
Asse loc. pilastro y nodo ESTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 45.0 cm, hjc= 20.0 cm
Asse loc. pilastro z nodo INTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 30.0 cm, hjc= 50.0 cm

FxMin,inf	FxMin,sup	FxMax,sup	FySup	FzSup	Vjbdy	Vjbdz	Vres,y	Vres,z	I.R.compr.	Ashy	Ashz	PASSO	Nota
daN					daN		daN			cmq		cm	
-13710	-5873	-7790	45	169	17571	35064	61027	127974	0.29	4.26	5.97	8.10	

VERIFICA DI RESISTENZA CON SOLLECITAZIONI COMPORTAMENTO NON DISSIPATIVO

Asse loc. pilastro y nodo ESTERNO: Hjw= 40.0 cm, bj= 45.0 cm, hjc= 20.0 cm, db1= 45.0 cm

NC	Fx,sup	Fx,inf	Mb	Vb	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-7790	-16050	-1724	1988	297	3960	61027	0.06	0.00	40.00	
3	-7657	-15880	-1722	1987	298	3954	61061	0.06	0.00	40.00	
4	-6006	-13890	-382	1500	46	896	61486	0.01	0.00	40.00	
5	-5873	-13710	-380	1499	45	892	61520	0.01	0.00	40.00	
6	-7321	-15500	-1256	1818	176	2926	61148	0.05	0.00	40.00	
7	-6878	-14920	-1250	1815	179	2908	61262	0.05	0.00	40.00	
8	-6786	-14850	-853	1672	73	2034	61285	0.03	0.00	40.00	
9	-6342	-14270	-847	1669	76	2016	61399	0.03	0.00	40.00	
10	-7790	-16050	-1724	1988	297	3960	61027	0.06	0.00	40.00	
11	-7657	-15880	-1722	1987	298	3954	61061	0.06	0.00	40.00	
12	-6006	-13890	-382	1500	46	896	61486	0.01	0.00	40.00	
13	-5873	-13710	-380	1499	45	892	61520	0.01	0.00	40.00	
14	-7321	-15500	-1256	1818	176	2926	61148	0.05	0.00	40.00	
15	-6878	-14920	-1250	1815	179	2908	61262	0.05	0.00	40.00	
16	-6786	-14850	-853	1672	73	2034	61285	0.03	0.00	40.00	
17	-6342	-14270	-847	1669	76	2016	61399	0.03	0.00	40.00	

Asse loc. pilastro z nodo INTERNO: Hjw= 40.0 cm, bj= 30.0 cm, hjc= 50.0 cm, db1= 45.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb,1	Mb,2	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-7790	-16050	-2069	-1098	379	2018	127974	0.02	0.00	40.00	
3	-7657	-15880	-1839	-1295	282	1061	128031	0.01	0.00	40.00	
4	-6006	-13890	-2142	-1224	382	1884	128734	0.01	0.00	40.00	
5	-5873	-13710	-1912	-1421	285	927	128791	0.01	0.00	40.00	
6	-7321	-15500	-2362	-913	494	3085	128175	0.02	0.00	40.00	
7	-6878	-14920	-1597	-1568	169	98	128363	0.00	0.00	40.00	
8	-6786	-14850	-2384	-950	495	3045	128403	0.02	0.00	40.00	
9	-6342	-14270	-1619	-1606	170	138	128592	0.00	0.00	40.00	
10	-7790	-16050	-2069	-1098	379	2018	127974	0.02	0.00	40.00	
11	-7657	-15880	-1839	-1295	282	1061	128031	0.01	0.00	40.00	
12	-6006	-13890	-2142	-1224	382	1884	128734	0.01	0.00	40.00	
13	-5873	-13710	-1912	-1421	285	927	128791	0.01	0.00	40.00	
14	-7321	-15500	-2362	-913	494	3085	128175	0.02	0.00	40.00	
15	-6878	-14920	-1597	-1568	169	98	128363	0.00	0.00	40.00	
16	-6786	-14850	-2384	-950	495	3045	128403	0.02	0.00	40.00	
17	-6342	-14270	-1619	-1606	170	138	128592	0.00	0.00	40.00	

CONFRONTO E SINTESI CONCLUSIVE (si assume in ogni caso passo <= 15 cm)

I.R.compr.	Ashy	Ashz	PASSO	Nota
	cmq		cm	
0.06	--	--	15.00	**VERIFICATO**

ASTA NUM. 17 NI 49 NF 51 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 31C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-12680	573	-74	0	-138	-3711	15.71	15.71	9.42	9.42	3	0.07	0.01	0.05	0.00	0.00	24.0
2	0	-9644	507	-107	0	-192	-3084	15.71	15.71	9.42	9.42	2	0.08	0.01	0.04	0.00	0.00	24.0
3	0	-9591	488	42	0	40	-3021	15.71	15.71	9.42	9.42	2	0.08	0.01	0.04	0.00	0.00	24.0
4	0	-9920	394	-155	0	-253	-2688	15.71	15.71	9.42	9.42	2	0.07	0.01	0.03	0.00	0.00	24.0
5	0	-9867	375	-6	0	-21	-2625	15.71	15.71	9.42	9.42	2	0.07	0.00	0.03	0.00	0.00	24.0
6	0	-9802	490	-298	0	-484	-3019	15.71	15.71	9.42	9.42	2	0.09	0.01	0.04	0.00	0.00	24.0
7	0	-9626	426	199	0	289	-2809	15.71	15.71	9.42	9.42	2	0.08	0.01	0.04	0.00	0.00	24.0
8	0	-9885	456	-313	0	-502	-2900	15.71	15.71	9.42	9.42	2	0.09	0.01	0.04	0.00	0.00	24.0
9	0	-9709	392	185	0	271	-2690	15.71	15.71	9.42	9.42	2	0.08	0.01	0.03	0.00	0.00	24.0
10	0	-9644	507	-107	0	-192	-3084	15.71	15.71	9.42	9.42	2	0.08	0.01	0.04	0.00	0.00	24.0
11	0	-9591	488	42	0	40	-3021	15.71	15.71	9.42	9.42	2	0.08	0.01	0.04	0.00	0.00	24.0
12	0	-9920	394	-155	0	-253	-2688	15.71	15.71	9.42	9.42	2	0.07	0.01	0.03	0.00	0.00	24.0
13	0	-9867	375	-6	0	-21	-2625	15.71	15.71	9.42	9.42	2	0.07	0.00	0.03	0.00	0.00	24.0
14	0	-9802	490	-298	0	-484	-3019	15.71	15.71	9.42	9.42	2	0.09	0.01	0.04	0.00	0.00	24.0
15	0	-9626	426	199	0	289	-2809	15.71	15.71	9.42	9.42	2	0.08	0.01	0.04	0.00	0.00	24.0
16	0	-9885	456	-313	0	-502	-2900	15.71	15.71	9.42	9.42	2	0.09	0.01	0.04	0.00	0.00	24.0
17	0	-9709	392	185	0	271	-2690	15.71	15.71	9.42	9.42	2	0.08	0.01	0.03	0.00	0.00	24.0
18	0	-15950	1558	-16	0	-46	-6387	15.71	15.71	9.42	9.42	3	0.11	0.02	0.12	0.00	0.00	24.0
19	0	-20800	923	-140	0	-223	-8292	15.71	15.71	9.42	9.42	3	0.15	0.01	0.07	0.00	0.00	24.0
20	0	-17600	1192	121	0	94	-7058	15.71	15.71	9.42	9.42	3	0.13	0.02	0.09	0.00	0.00	24.0
37	0	-12510	1550	28	0	13	-4568	15.71	15.71	9.42	9.42	3	0.08	0.02	0.12	0.00	0.00	24.0
38	0	-20600	491	-178	0	-281	-7742	15.71	15.71	9.42	9.42	3	0.14	0.01	0.04	0.00	0.00	24.0
39	0	-15270	940	256	0	248	-5685	15.71	15.71	9.42	9.42	3	0.10	0.01	0.07	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	83	-11822	573	-74	0	-78	-3238	15.71	15.71	9.42	9.42	3	0.06	0.01	0.05	0.00	0.00	24.0
2	83	-8984	507	-107	0	-104	-2666	15.71	15.71	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
3	83	-8931	488	42	0	5	-2619	15.71	15.71	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
4	83	-9260	394	-155	0	-125	-2362	15.71	15.71	9.42	9.42	2	0.06	0.01	0.03	0.00	0.00	24.0

5	83	-9207	375	-6	0	-16	-2315	15.71	15.71	9.42	9.42	2	0.06	0.00	0.03	0.00	0.00	24.0
6	83	-9142	490	-298	0	-238	-2615	15.71	15.71	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
7	83	-8966	426	199	0	125	-2457	15.71	15.71	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
8	83	-9225	456	-313	0	-244	-2524	15.71	15.71	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
9	83	-9049	392	185	0	118	-2366	15.71	15.71	9.42	9.42	2	0.06	0.01	0.03	0.00	0.00	24.0
10	83	-8984	507	-107	0	-104	-2666	15.71	15.71	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
11	83	-8931	488	42	0	5	-2619	15.71	15.71	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
12	83	-9260	394	-155	0	-125	-2362	15.71	15.71	9.42	9.42	2	0.06	0.01	0.03	0.00	0.00	24.0
13	83	-9207	375	-6	0	-16	-2315	15.71	15.71	9.42	9.42	2	0.06	0.00	0.03	0.00	0.00	24.0
14	83	-9142	490	-298	0	-238	-2615	15.71	15.71	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
15	83	-8966	426	199	0	125	-2457	15.71	15.71	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
16	83	-9225	456	-313	0	-244	-2524	15.71	15.71	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
17	83	-9049	392	185	0	118	-2366	15.71	15.71	9.42	9.42	2	0.06	0.01	0.03	0.00	0.00	24.0
18	83	-15090	1352	-16	0	-33	-5187	15.71	15.71	9.42	9.42	3	0.09	0.02	0.11	0.00	0.00	24.0
19	83	-19942	1129	-140	0	-108	-7445	15.71	15.71	9.42	9.42	3	0.13	0.01	0.08	0.00	0.00	24.0
20	83	-16742	1192	121	0	-5	-6074	15.71	15.71	9.42	9.42	3	0.11	0.02	0.09	0.00	0.00	24.0
37	83	-11652	1206	28	0	-10	-3431	15.71	15.71	9.42	9.42	3	0.06	0.02	0.10	0.00	0.00	24.0
38	83	-19742	836	-178	0	-134	-7195	15.71	15.71	9.42	9.42	3	0.13	0.01	0.06	0.00	0.00	24.0
39	83	-14412	940	256	0	36	-4909	15.71	15.71	9.42	9.42	3	0.09	0.01	0.07	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	165	-10965	573	-74	0	-17	-2764	15.71	15.71	9.42	9.42	3	0.05	0.01	0.05	0.00	0.00	24.0
2	165	-8324	507	-107	0	-15	-2247	15.71	15.71	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
3	165	-8271	488	42	0	-29	-2216	15.71	15.71	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
4	165	-8600	394	-155	0	4	-2037	15.71	15.71	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
5	165	-8547	375	-6	0	-11	-2006	15.71	15.71	9.42	9.42	2	0.05	0.00	0.03	0.00	0.00	24.0
6	165	-8482	490	-298	0	8	-2211	15.71	15.71	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
7	165	-8306	426	199	0	-40	-2106	15.71	15.71	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
8	165	-8565	456	-313	0	14	-2148	15.71	15.71	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
9	165	-8389	392	185	0	-34	-2043	15.71	15.71	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
10	165	-8324	507	-107	0	-15	-2247	15.71	15.71	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
11	165	-8271	488	42	0	-29	-2216	15.71	15.71	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
12	165	-8600	394	-155	0	4	-2037	15.71	15.71	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
13	165	-8547	375	-6	0	-11	-2006	15.71	15.71	9.42	9.42	2	0.05	0.00	0.03	0.00	0.00	24.0
14	165	-8482	490	-298	0	8	-2211	15.71	15.71	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
15	165	-8306	426	199	0	-40	-2106	15.71	15.71	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
16	165	-8565	456	-313	0	14	-2148	15.71	15.71	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
17	165	-8389	392	185	0	-34	-2043	15.71	15.71	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
18	165	-14230	1145	-16	0	-20	-4156	15.71	15.71	9.42	9.42	3	0.08	0.01	0.09	0.00	0.00	24.0
19	165	-19085	1336	-140	0	8	-6429	15.71	15.71	9.42	9.42	3	0.11	0.02	0.10	0.00	0.00	24.0
20	165	-15885	1192	121	0	-105	-5090	15.71	15.71	9.42	9.42	3	0.09	0.02	0.09	0.00	0.00	24.0
37	165	-10794	862	28	0	-33	-2577	15.71	15.71	9.42	9.42	3	0.05	0.01	0.07	0.00	0.00	24.0
38	165	-18885	1180	-178	0	13	-6364	15.71	15.71	9.42	9.42	3	0.11	0.01	0.09	0.00	0.00	24.0
39	165	-13555	940	256	0	-175	-4133	15.71	15.71	9.42	9.42	3	0.08	0.01	0.07	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	248	-10108	573	-74	0	44	-2291	15.71	15.71	9.42	9.42	3	0.04	0.01	0.05	0.00	0.00	24.0
2	248	-7664	507	-107	0	74	-1829	15.71	15.71	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
3	248	-7611	488	42	0	-64	-1814	15.71	15.71	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
4	248	-7940	394	-155	0	132	-1712	15.71	15.71	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
5	248	-7887	375	-6	0	-6	-1696	15.71	15.71	9.42	9.42	2	0.04	0.00	0.03	0.00	0.00	24.0
6	248	-7822	490	-298	0	255	-1806	15.71	15.71	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
7	248	-7646	426	199	0	-204	-1754	15.71	15.71	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
8	248	-7905	456	-313	0	272	-1771	15.71	15.71	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
9	248	-7729	392	185	0	-187	-1719	15.71	15.71	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
10	248	-7664	507	-107	0	74	-1829	15.71	15.71	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
11	248	-7611	488	42	0	-64	-1814	15.71	15.71	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
12	248	-7940	394	-155	0	132	-1712	15.71	15.71	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
13	248	-7887	375	-6	0	-6	-1696	15.71	15.71	9.42	9.42	2	0.04	0.00	0.03	0.00	0.00	24.0
14	248	-7822	490	-298	0	255	-1806	15.71	15.71	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
15	248	-7646	426	199	0	-204	-1754	15.71	15.71	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
16	248	-7905	456	-313	0	272	-1771	15.71	15.71	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
17	248	-7729	392	185	0	-187	-1719	15.71	15.71	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
18	248	-13370	939	-16	0	-6	-3297	15.71	15.71	9.42	9.42	3	0.06	0.01	0.07	0.00	0.00	24.0
19	248	-18228	1542	-140	0	123	-5241	15.71	15.71	9.42	9.42	3	0.09	0.02	0.12	0.00	0.00	24.0
20	248	-15028	1192	121	0	-205	-4107	15.71	15.71	9.42	9.42	3	0.08	0.02	0.09	0.00	0.00	24.0
37	248	-9935	518	28	0	-55	-2008	15.71	15.71	9.42	9.42	3	0.04	0.01	0.04	0.00	0.00	24.0
38	248	-18028	1524	-178	0	160	-5249	15.71	15.71	9.42	9.42	3	0.09	0.02	0.12	0.00	0.00	24.0
39	248	-12698	940	256	0	-386	-3358	15.71	15.71	9.42	9.42	3	0.06	0.01	0.08	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	330	-9250	573	-74	0	105	-1818	15.71	15.71	9.42	9.42	3	0.03	0.01	0.05	0.00	0.00	24.0
2	330	-7004	507	-107	0	162	-1411	15.71	15.71	9.42	9.42	2	0.04	0.01	0.04	0.00	0.00	24.0
3	330	-6951	488	42	0	-98	-1411	15.71	15.71	9.42	9.42	2	0.04	0.01	0.04	0.00	0.00	24.0
4	330	-7280	394	-155	0	260	-1386	15.71	15.71	9.42	9.42	2	0.04	0.01	0.03	0.00	0.00	24.0
5	330	-7227	375	-6	0	-1	-1386	15.71	15.71	9.42	9.42	2	0.04	0.00	0.03	0.00	0.00	24.0
6	330	-7162	490	-298	0	501	-1402	15.71	15.71	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
7	330	-6986	426	199	0	-368	-1403	15.71	15.71	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
8	330	-7245	456	-313	0	530	-1395	15.71	15.71	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
9	330	-7069	392	185	0	-339	-1395	15.71	15.71	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
10	330	-7004	507	-107	0	162	-1411	15.71	15.71	9.42	9.42	2	0.04	0.01	0.04	0.00	0.00	24.0
11	330	-6951	488	42	0	-98	-1411	15.71	15.71	9.42	9.42	2	0.04	0.01	0.04	0.00	0.00	24.0
12	330	-7280	394	-155	0	260	-1386	15.71	15.71	9.42	9.42	2	0.04	0.01	0.03	0.00	0.00	24.0
13	330	-7227	375	-6	0	-1	-1386	15.71	15.71	9.42	9.42	2	0.04	0.00	0.03	0.00	0.00	24.0
14	330	-7162	490	-298	0	501	-1402	15.71	15.71	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
15	330	-6986	426	199	0	-368	-1403	15.71	15.71	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
16	330	-7245	456	-313	0	530	-1395	15.71	15.71	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
17	330	-7069	392	185	0	-339	-1395	15.71	15.71	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
18	330	-12510	733	-16	0	7	-2607	15.71	15.71	9.42	9.42	3	0.05	0.01	0.06	0.00	0.00	24.0
19	330	-17370	1749	-140	0	239	-3884	15.71	15.71	9.42	9.42	3	0.07	0.02	0.13	0.00	0.00	24.0
20	330	-14170	1192	121	0	-305	-3123	15.71	15.71	9.42	9.42	3	0.06	0.02	0.09	0.00	0.00	24.0
37	330	-9077	174	28	0	-78	-1722	15.71	15.71	9.42	9.42	3	0.03	0.00	0.01	0.00	0.00	24.0
38	330	-17170	1868	-178	0	308	-3850	15.71	15.71	9.42	9.42	3	0.07	0.02	0.14	0.00	0.00	24.0
39	330	-11840	940	256	0	-598	-2582	15.71	15.71	9.42	9.42	3	0.05	0.01	0.08	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 18 NI 92 NF 94 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 30C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm

1	0	-14610	1354	-173	0	-271	-7137	15.71	15.71	9.42	9.42	3	0.13	0.02	0.11	0.00	0.00	24.0
2	0	-11230	1249	-197	0	-309	-6247	15.71	15.71	9.42	9.42	2	0.17	0.02	0.10	0.00	0.00	24.0
3	0	-11270	1261	-50	0	-73	-6298	15.71	15.71	9.42	9.42	2	0.16	0.02	0.10	0.00	0.00	24.0
4	0	-11210	822	-216	0	-343	-4682	15.71	15.71	9.42	9.42	2	0.13	0.01	0.07	0.00	0.00	24.0
5	0	-11240	834	-70	0	-107	-4733	15.71	15.71	9.42	9.42	2	0.12	0.01	0.07	0.00	0.00	24.0
6	0	-11180	1085	-374	0	-596	-5639	15.71	15.71	9.42	9.42	2	0.16	0.01	0.09	0.00	0.00	24.0
7	0	-11300	1126	113	0	190	-5810	15.71	15.71	9.42	9.42	2	0.15	0.01	0.09	0.00	0.00	24.0
8	0	-11170	957	-380	0	-606	-5170	15.71	15.71	9.42	9.42	2	0.15	0.01	0.08	0.00	0.00	24.0
9	0	-11290	998	107	0	180	-5340	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
10	0	-11230	1249	-197	0	-309	-6247	15.71	15.71	9.42	9.42	2	0.17	0.02	0.10	0.00	0.00	24.0
11	0	-11270	1261	-50	0	-73	-6298	15.71	15.71	9.42	9.42	2	0.16	0.02	0.10	0.00	0.00	24.0
12	0	-11210	822	-216	0	-343	-4682	15.71	15.71	9.42	9.42	2	0.13	0.01	0.07	0.00	0.00	24.0
13	0	-11240	834	-70	0	-107	-4733	15.71	15.71	9.42	9.42	2	0.12	0.01	0.07	0.00	0.00	24.0
14	0	-11180	1085	-374	0	-596	-5639	15.71	15.71	9.42	9.42	2	0.16	0.01	0.09	0.00	0.00	24.0
15	0	-11300	1126	113	0	190	-5810	15.71	15.71	9.42	9.42	2	0.15	0.01	0.09	0.00	0.00	24.0
16	0	-11170	957	-380	0	-606	-5170	15.71	15.71	9.42	9.42	2	0.15	0.01	0.08	0.00	0.00	24.0
17	0	-11290	998	107	0	180	-5340	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
18	0	-20290	3636	-297	0	-437	-14830	15.71	15.71	9.42	9.42	3	0.26	0.05	0.27	0.00	0.00	24.0
19	0	-23870	1922	-356	0	-560	-12830	15.71	15.71	9.42	9.42	3	0.23	0.02	0.14	0.00	0.00	24.0
20	0	-21010	2597	-100	0	-183	-12960	15.71	15.71	9.42	9.42	3	0.23	0.03	0.19	0.00	0.00	24.0
37	0	-16700	3742	-226	0	-320	-13320	15.71	15.71	9.42	9.42	3	0.24	0.05	0.29	0.00	0.00	24.0
38	0	-22670	884	-325	0	-525	-9982	15.71	15.71	9.42	9.42	3	0.18	0.01	0.06	0.00	0.00	24.0
39	0	-17900	2010	103	0	104	-10190	15.71	15.71	9.42	9.42	3	0.18	0.03	0.15	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	83	-13752	1354	-173	0	-127	-6020	15.71	15.71	9.42	9.42	3	0.11	0.02	0.11	0.00	0.00	24.0
2	83	-10571	1249	-197	0	-147	-5216	15.71	15.71	9.42	9.42	2	0.14	0.02	0.10	0.00	0.00	24.0
3	83	-10610	1261	-50	0	-32	-5258	15.71	15.71	9.42	9.42	2	0.13	0.02	0.10	0.00	0.00	24.0
4	83	-10549	822	-216	0	-164	-4004	15.71	15.71	9.42	9.42	2	0.11	0.01	0.07	0.00	0.00	24.0
5	83	-10580	834	-70	0	-49	-4045	15.71	15.71	9.42	9.42	2	0.10	0.01	0.07	0.00	0.00	24.0
6	83	-10520	1085	-374	0	-287	-4744	15.71	15.71	9.42	9.42	2	0.13	0.01	0.09	0.00	0.00	24.0
7	83	-10641	1126	113	0	96	-4881	15.71	15.71	9.42	9.42	2	0.13	0.01	0.09	0.00	0.00	24.0
8	83	-10511	957	-380	0	-292	-4381	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
9	83	-10631	998	107	0	91	-4517	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
10	83	-10571	1249	-197	0	-147	-5216	15.71	15.71	9.42	9.42	2	0.14	0.02	0.10	0.00	0.00	24.0
11	83	-10610	1261	-50	0	-32	-5258	15.71	15.71	9.42	9.42	2	0.13	0.02	0.10	0.00	0.00	24.0
12	83	-10549	822	-216	0	-164	-4004	15.71	15.71	9.42	9.42	2	0.11	0.01	0.07	0.00	0.00	24.0
13	83	-10580	834	-70	0	-49	-4045	15.71	15.71	9.42	9.42	2	0.10	0.01	0.07	0.00	0.00	24.0
14	83	-10520	1085	-374	0	-287	-4744	15.71	15.71	9.42	9.42	2	0.13	0.01	0.09	0.00	0.00	24.0
15	83	-10641	1126	113	0	96	-4881	15.71	15.71	9.42	9.42	2	0.13	0.01	0.09	0.00	0.00	24.0
16	83	-10511	957	-380	0	-292	-4381	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
17	83	-10631	998	107	0	91	-4517	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
18	83	-19432	3430	-297	0	-192	-11916	15.71	15.71	9.42	9.42	3	0.21	0.04	0.26	0.00	0.00	24.0
19	83	-23012	2128	-356	0	-266	-11159	15.71	15.71	9.42	9.42	3	0.20	0.03	0.15	0.00	0.00	24.0
20	83	-20152	2597	-100	0	-100	-10817	15.71	15.71	9.42	9.42	3	0.19	0.03	0.19	0.00	0.00	24.0
37	83	-15842	3398	-226	0	-134	-10375	15.71	15.71	9.42	9.42	3	0.19	0.04	0.26	0.00	0.00	24.0
38	83	-21812	1229	-325	0	-256	-9110	15.71	15.71	9.42	9.42	3	0.16	0.02	0.09	0.00	0.00	24.0
39	83	-17040	2010	103	0	19	-8533	15.71	15.71	9.42	9.42	3	0.15	0.03	0.15	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	165	-12895	1354	-173	0	16	-4903	15.71	15.71	9.42	9.42	3	0.09	0.02	0.11	0.00	0.00	24.0
2	165	-9912	1249	-197	0	15	-4186	15.71	15.71	9.42	9.42	2	0.11	0.02	0.10	0.00	0.00	24.0
3	165	-9950	1261	-50	0	10	-4217	15.71	15.71	9.42	9.42	2	0.11	0.02	0.10	0.00	0.00	24.0
4	165	-9888	822	-216	0	14	-3326	15.71	15.71	9.42	9.42	2	0.09	0.01	0.07	0.00	0.00	24.0
5	165	-9921	834	-70	0	9	-3357	15.71	15.71	9.42	9.42	2	0.09	0.01	0.07	0.00	0.00	24.0
6	165	-9860	1085	-374	0	22	-3849	15.71	15.71	9.42	9.42	2	0.10	0.01	0.09	0.00	0.00	24.0
7	165	-9982	1126	113	0	3	-3952	15.71	15.71	9.42	9.42	2	0.10	0.01	0.09	0.00	0.00	24.0
8	165	-9852	957	-380	0	21	-3591	15.71	15.71	9.42	9.42	2	0.09	0.01	0.08	0.00	0.00	24.0
9	165	-9972	998	107	0	2	-3694	15.71	15.71	9.42	9.42	2	0.09	0.01	0.08	0.00	0.00	24.0
10	165	-9912	1249	-197	0	15	-4186	15.71	15.71	9.42	9.42	2	0.11	0.02	0.10	0.00	0.00	24.0
11	165	-9950	1261	-50	0	10	-4217	15.71	15.71	9.42	9.42	2	0.11	0.02	0.10	0.00	0.00	24.0
12	165	-9888	822	-216	0	14	-3326	15.71	15.71	9.42	9.42	2	0.09	0.01	0.07	0.00	0.00	24.0
13	165	-9921	834	-70	0	9	-3357	15.71	15.71	9.42	9.42	2	0.09	0.01	0.07	0.00	0.00	24.0
14	165	-9860	1085	-374	0	22	-3849	15.71	15.71	9.42	9.42	2	0.10	0.01	0.09	0.00	0.00	24.0
15	165	-9982	1126	113	0	3	-3952	15.71	15.71	9.42	9.42	2	0.10	0.01	0.09	0.00	0.00	24.0
16	165	-9852	957	-380	0	21	-3591	15.71	15.71	9.42	9.42	2	0.09	0.01	0.08	0.00	0.00	24.0
17	165	-9972	998	107	0	2	-3694	15.71	15.71	9.42	9.42	2	0.09	0.01	0.08	0.00	0.00	24.0
18	165	-18575	3223	-297	0	53	-9172	15.71	15.71	9.42	9.42	3	0.16	0.04	0.24	0.00	0.00	24.0
19	165	-22155	2334	-356	0	28	-9318	15.71	15.71	9.42	9.42	3	0.16	0.03	0.17	0.00	0.00	24.0
20	165	-19295	2597	-100	0	-18	-8673	15.71	15.71	9.42	9.42	3	0.15	0.03	0.19	0.00	0.00	24.0
37	165	-14985	3054	-226	0	53	-7714	15.71	15.71	9.42	9.42	3	0.14	0.04	0.24	0.00	0.00	24.0
38	165	-20955	1573	-325	0	12	-7955	15.71	15.71	9.42	9.42	3	0.14	0.02	0.12	0.00	0.00	24.0
39	165	-16180	2010	103	0	-65	-6877	15.71	15.71	9.42	9.42	3	0.12	0.03	0.16	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	248	-12038	1354	-173	0	159	-3786	15.71	15.71	9.42	9.42	3	0.07	0.02	0.11	0.00	0.00	24.0
2	248	-9252	1249	-197	0	178	-3156	15.71	15.71	9.42	9.42	2	0.08	0.02	0.10	0.00	0.00	24.0
3	248	-9290	1261	-50	0	51	-3177	15.71	15.71	9.42	9.42	2	0.08	0.02	0.11	0.00	0.00	24.0
4	248	-9227	822	-216	0	192	-2648	15.71	15.71	9.42	9.42	2	0.07	0.01	0.07	0.00	0.00	24.0
5	248	-9262	834	-70	0	66	-2669	15.71	15.71	9.42	9.42	2	0.07	0.01	0.07	0.00	0.00	24.0
6	248	-9201	1085	-374	0	330	-2953	15.71	15.71	9.42	9.42	2	0.08	0.01	0.09	0.00	0.00	24.0
7	248	-9322	1126	113	0	-90	-3024	15.71	15.71	9.42	9.42	2	0.08	0.01	0.09	0.00	0.00	24.0
8	248	-9192	957	-380	0	334	-2802	15.71	15.71	9.42	9.42	2	0.08	0.01	0.08	0.00	0.00	24.0
9	248	-9314	998	107	0	-86	-2872	15.71	15.71	9.42	9.42	2	0.08	0.01	0.08	0.00	0.00	24.0
10	248	-9252	1249	-197	0	178	-3156	15.71	15.71	9.42	9.42	2	0.08	0.02	0.10	0.00	0.00	24.0
11	248	-9290	1261	-50	0	51	-3177	15.71	15.71	9.42	9.42	2	0.08	0.02	0.11	0.00	0.00	24.0
12	248	-9227	822	-216	0	192	-2648	15.71	15.71	9.42	9.42	2	0.07	0.01	0.07	0.00	0.00	24.0
13	248	-9262	834	-70	0	66	-2669	15.71	15.71	9.42	9.42	2	0.07	0.01	0.07	0.00	0.00	24.0
14	248	-9201	1085	-374	0	330	-2953	15.71	15.71	9.42	9.42	2	0.08	0.01	0.09	0.00	0.00	24.0
15	248	-9322	1126	113	0	-90	-3024	15.71	15.71	9.42	9.42	2	0.08	0.01	0.09	0.00	0.00	24.0
16	248	-9192	957	-380	0	334	-2802	15.71	15.71	9.42	9.42	2	0.08	0.01	0.08	0.00	0.00	24.0
17	248	-9314	998	107	0	-86	-2872	15.71	15.71	9.42	9.42	2	0.08	0.01	0.08	0.00	0.00	24.0
18	248	-17718	3016	-297	0	298	-6599	15.71	15.71	9.42	9.42	3	0.12	0.04	0.23	0.00	0.00	24.0
19	248	-21298	2541	-356	0	322	-7307	15.71	15.71	9.42	9.42	3	0.13	0.03	0.19	0.00	0.00	24.0
20	248	-18438	2597	-100	0	65	-6530	15.71	15.71	9.42	9.42	3	0.12	0.03	0.20	0.00	0.00	24.0
37	248	-14128	2710	-226	0	239	-5337	15.71	15.71	9.42	9.42	3	0.10	0.03	0.21	0.00	0.00	24.0
38	248	-20098	1917	-325	0	280	-6515	15.71	15.71	9.42	9.42	3	0.12	0.02	0.14	0.00	0.00	24.0
39	248	-15320	2010	103	0	-150	-5220	15.71	15.71	9.42	9.42	3	0.09	0.03	0.16	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	330	-11180	1354	-173	0	302	-2669	15.71	15.71	9.42	9.42	3	0.05	0.02	0.11	0.00	0.00	24.0
2	330	-8593	1249	-197	0	340	-2125	15.71	15.71	9.42	9.42	2	0.06	0.02	0.11	0.00	0.00	24.0
3	330	-8630	1261	-50	0	93	-2136	15.71	15.71	9.42	9.42	2	0.06	0.02	0.11	0.00	0.00	24.0
4	330	-8566	822	-216	0	371	-1970	15.71	15.71	9.42	9.42	2	0.06	0.01	0.07	0.00	0.00	24.0
5	330	-8602	834	-70	0	124	-1981	15.71	15.71	9.42	9.42	2	0.05	0.01	0.07	0.00	0.00	24.0
6	330	-8541	1085	-374	0	639	-2058	15.71	15.71	9.42	9.42	2	0.07	0.01	0.09	0.00	0.00	24.0

7	330	-8663	1126	113	0	-184	-2095	15.71	15.71	9.42	9.42	2	0.06	0.01	0.09	0.00	0.00	24.0
8	330	-8533	957	-380	0	648	-2012	15.71	15.71	9.42	9.42	2	0.07	0.01	0.08	0.00	0.00	24.0
9	330	-8655	998	107	0	-175	-2049	15.71	15.71	9.42	9.42	2	0.06	0.01	0.08	0.00	0.00	24.0
10	330	-8593	1249	-197	0	340	-2125	15.71	15.71	9.42	9.42	2	0.06	0.02	0.11	0.00	0.00	24.0
11	330	-8630	1261	-50	0	93	-2136	15.71	15.71	9.42	9.42	2	0.06	0.02	0.11	0.00	0.00	24.0
12	330	-8566	822	-216	0	371	-1970	15.71	15.71	9.42	9.42	2	0.06	0.01	0.07	0.00	0.00	24.0
13	330	-8602	834	-70	0	124	-1981	15.71	15.71	9.42	9.42	2	0.05	0.01	0.07	0.00	0.00	24.0
14	330	-8541	1085	-374	0	639	-2058	15.71	15.71	9.42	9.42	2	0.07	0.01	0.09	0.00	0.00	24.0
15	330	-8663	1126	113	0	-184	-2095	15.71	15.71	9.42	9.42	2	0.06	0.01	0.09	0.00	0.00	24.0
16	330	-8533	957	-380	0	648	-2012	15.71	15.71	9.42	9.42	2	0.07	0.01	0.08	0.00	0.00	24.0
17	330	-8655	998	107	0	-175	-2049	15.71	15.71	9.42	9.42	2	0.06	0.01	0.08	0.00	0.00	24.0
18	330	-16860	2810	-297	0	543	-4196	15.71	15.71	9.42	9.42	3	0.08	0.04	0.22	0.00	0.00	24.0
19	330	-20440	2747	-356	0	616	-5125	15.71	15.71	9.42	9.42	3	0.09	0.03	0.20	0.00	0.00	24.0
20	330	-17580	2597	-100	0	147	-4387	15.71	15.71	9.42	9.42	3	0.08	0.03	0.20	0.00	0.00	24.0
37	330	-13270	2366	-226	0	425	-3244	15.71	15.71	9.42	9.42	3	0.06	0.03	0.19	0.00	0.00	24.0
38	330	-19240	2261	-325	0	548	-4792	15.71	15.71	9.42	9.42	3	0.09	0.03	0.17	0.00	0.00	24.0
39	330	-14460	2010	103	0	-235	-3563	15.71	15.71	9.42	9.42	3	0.07	0.03	0.16	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 19 NI 135 NF 137 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 29C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-14570	1322	-308	0	-490	-7061	15.71	15.71	9.42	9.42	3	0.13	0.02	0.10	0.00	0.00	24.0
2	0	-11170	1228	-315	0	-502	-6203	15.71	15.71	9.42	9.42	2	0.17	0.02	0.10	0.00	0.00	24.0
3	0	-11140	1207	-163	0	-253	-6127	15.71	15.71	9.42	9.42	2	0.16	0.02	0.10	0.00	0.00	24.0
4	0	-11280	826	-311	0	-501	-4736	15.71	15.71	9.42	9.42	2	0.13	0.01	0.07	0.00	0.00	24.0
5	0	-11240	806	-159	0	-253	-4660	15.71	15.71	9.42	9.42	2	0.12	0.01	0.07	0.00	0.00	24.0
6	0	-11260	1111	-491	0	-791	-5779	15.71	15.71	9.42	9.42	2	0.17	0.01	0.09	0.00	0.00	24.0
7	0	-11130	1043	15	0	37	-5524	15.71	15.71	9.42	9.42	2	0.14	0.01	0.09	0.00	0.00	24.0
8	0	-11290	990	-490	0	-791	-5339	15.71	15.71	9.42	9.42	2	0.15	0.01	0.08	0.00	0.00	24.0
9	0	-11160	922	16	0	37	-5084	15.71	15.71	9.42	9.42	2	0.13	0.01	0.08	0.00	0.00	24.0
10	0	-11170	1228	-315	0	-502	-6203	15.71	15.71	9.42	9.42	2	0.17	0.02	0.10	0.00	0.00	24.0
11	0	-11140	1207	-163	0	-253	-6127	15.71	15.71	9.42	9.42	2	0.16	0.02	0.10	0.00	0.00	24.0
12	0	-11280	826	-311	0	-501	-4736	15.71	15.71	9.42	9.42	2	0.13	0.01	0.07	0.00	0.00	24.0
13	0	-11240	806	-159	0	-253	-4660	15.71	15.71	9.42	9.42	2	0.12	0.01	0.07	0.00	0.00	24.0
14	0	-11260	1111	-491	0	-791	-5779	15.71	15.71	9.42	9.42	2	0.17	0.01	0.09	0.00	0.00	24.0
15	0	-11130	1043	15	0	37	-5524	15.71	15.71	9.42	9.42	2	0.14	0.01	0.09	0.00	0.00	24.0
16	0	-11290	990	-490	0	-791	-5339	15.71	15.71	9.42	9.42	2	0.15	0.01	0.08	0.00	0.00	24.0
17	0	-11160	922	16	0	37	-5084	15.71	15.71	9.42	9.42	2	0.13	0.01	0.08	0.00	0.00	24.0
18	0	-20010	3533	-612	0	-951	-14530	15.71	15.71	9.42	9.42	3	0.26	0.04	0.26	0.00	0.00	24.0
19	0	-24000	1911	-592	0	-939	-12880	15.71	15.71	9.42	9.42	3	0.23	0.02	0.14	0.00	0.00	24.0
20	0	-20780	2470	-327	0	-540	-12540	15.71	15.71	9.42	9.42	3	0.22	0.03	0.18	0.00	0.00	24.0
37	0	-16290	3616	-521	0	-804	-12920	15.71	15.71	9.42	9.42	3	0.24	0.05	0.28	0.00	0.00	24.0
38	0	-22950	912	-489	0	-785	-10160	15.71	15.71	9.42	9.42	3	0.18	0.01	0.07	0.00	0.00	24.0
39	0	-17570	1843	-46	0	-121	-9609	15.71	15.71	9.42	9.42	3	0.17	0.02	0.14	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	83	-13712	1322	-308	0	-236	-5971	15.71	15.71	9.42	9.42	3	0.11	0.02	0.10	0.00	0.00	24.0
2	83	-10511	1228	-315	0	-242	-5190	15.71	15.71	9.42	9.42	2	0.14	0.02	0.10	0.00	0.00	24.0
3	83	-10479	1207	-163	0	-119	-5131	15.71	15.71	9.42	9.42	2	0.13	0.02	0.10	0.00	0.00	24.0
4	83	-10620	826	-311	0	-244	-4055	15.71	15.71	9.42	9.42	2	0.11	0.01	0.07	0.00	0.00	24.0
5	83	-10580	806	-159	0	-121	-3995	15.71	15.71	9.42	9.42	2	0.10	0.01	0.07	0.00	0.00	24.0
6	83	-10599	1111	-491	0	-386	-4862	15.71	15.71	9.42	9.42	2	0.13	0.01	0.09	0.00	0.00	24.0
7	83	-10470	1043	15	0	24	-4664	15.71	15.71	9.42	9.42	2	0.12	0.01	0.09	0.00	0.00	24.0
8	83	-10629	990	-490	0	-387	-4522	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
9	83	-10500	922	16	0	23	-4323	15.71	15.71	9.42	9.42	2	0.11	0.01	0.08	0.00	0.00	24.0
10	83	-10511	1228	-315	0	-242	-5190	15.71	15.71	9.42	9.42	2	0.14	0.02	0.10	0.00	0.00	24.0
11	83	-10479	1207	-163	0	-119	-5131	15.71	15.71	9.42	9.42	2	0.13	0.02	0.10	0.00	0.00	24.0
12	83	-10620	826	-311	0	-244	-4055	15.71	15.71	9.42	9.42	2	0.11	0.01	0.07	0.00	0.00	24.0
13	83	-10580	806	-159	0	-121	-3995	15.71	15.71	9.42	9.42	2	0.10	0.01	0.07	0.00	0.00	24.0
14	83	-10599	1111	-491	0	-386	-4862	15.71	15.71	9.42	9.42	2	0.13	0.01	0.09	0.00	0.00	24.0
15	83	-10470	1043	15	0	24	-4664	15.71	15.71	9.42	9.42	2	0.12	0.01	0.09	0.00	0.00	24.0
16	83	-10629	990	-490	0	-387	-4522	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
17	83	-10500	922	16	0	23	-4323	15.71	15.71	9.42	9.42	2	0.11	0.01	0.08	0.00	0.00	24.0
18	83	-19152	3326	-612	0	-446	-11700	15.71	15.71	9.42	9.42	3	0.21	0.04	0.25	0.00	0.00	24.0
19	83	-23142	2118	-592	0	-450	-11217	15.71	15.71	9.42	9.42	3	0.20	0.03	0.15	0.00	0.00	24.0
20	83	-19920	2470	-327	0	-271	-10503	15.71	15.71	9.42	9.42	3	0.19	0.03	0.18	0.00	0.00	24.0
37	83	-15432	3272	-521	0	-375	-10078	15.71	15.71	9.42	9.42	3	0.18	0.04	0.25	0.00	0.00	24.0
38	83	-22090	1257	-489	0	-382	-9266	15.71	15.71	9.42	9.42	3	0.16	0.02	0.09	0.00	0.00	24.0
39	83	-16712	1843	-46	0	-83	-8088	15.71	15.71	9.42	9.42	3	0.15	0.02	0.14	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	165	-12855	1322	-308	0	18	-4880	15.71	15.71	9.42	9.42	3	0.09	0.02	0.11	0.00	0.00	24.0
2	165	-9852	1228	-315	0	18	-4178	15.71	15.71	9.42	9.42	2	0.11	0.02	0.10	0.00	0.00	24.0
3	165	-9818	1207	-163	0	16	-4135	15.71	15.71	9.42	9.42	2	0.11	0.02	0.10	0.00	0.00	24.0
4	165	-9960	826	-311	0	12	-3374	15.71	15.71	9.42	9.42	2	0.09	0.01	0.07	0.00	0.00	24.0
5	165	-9921	806	-159	0	10	-3330	15.71	15.71	9.42	9.42	2	0.09	0.01	0.07	0.00	0.00	24.0
6	165	-9938	1111	-491	0	18	-3946	15.71	15.71	9.42	9.42	2	0.10	0.01	0.09	0.00	0.00	24.0
7	165	-9810	1043	15	0	11	-3803	15.71	15.71	9.42	9.42	2	0.10	0.01	0.09	0.00	0.00	24.0
8	165	-9968	990	-490	0	17	-3705	15.71	15.71	9.42	9.42	2	0.09	0.01	0.08	0.00	0.00	24.0
9	165	-9840	922	16	0	10	-3562	15.71	15.71	9.42	9.42	2	0.09	0.01	0.08	0.00	0.00	24.0
10	165	-9852	1228	-315	0	18	-4178	15.71	15.71	9.42	9.42	2	0.11	0.02	0.10	0.00	0.00	24.0
11	165	-9818	1207	-163	0	16	-4135	15.71	15.71	9.42	9.42	2	0.11	0.02	0.10	0.00	0.00	24.0
12	165	-9960	826	-311	0	12	-3374	15.71	15.71	9.42	9.42	2	0.09	0.01	0.07	0.00	0.00	24.0
13	165	-9921	806	-159	0	10	-3330	15.71	15.71	9.42	9.42	2	0.09	0.01	0.07	0.00	0.00	24.0
14	165	-9938	1111	-491	0	18	-3946	15.71	15.71	9.42	9.42	2	0.10	0.01	0.09	0.00	0.00	24.0
15	165	-9810	1043	15	0	11	-3803	15.71	15.71	9.42	9.42	2	0.10	0.01	0.09	0.00	0.00	24.0
16	165	-9968	990	-490	0	17	-3705	15.71	15.71	9.42	9.42	2	0.09	0.01	0.08	0.00	0.00	24.0
17	165	-9840	922	16	0	10	-3562	15.71	15.71	9.42	9.42	2	0.09	0.01	0.08	0.00	0.00	24.0
18	165	-18295	3120	-612	0	59	-9040	15.71	15.71	9.42	9.42	3	0.16	0.04	0.24	0.00	0.00	24.0
19	165	-22285	2324	-592	0	39	-9384	15.71	15.71	9.42	9.42	3	0.16	0.03	0.17	0.00	0.00	24.0
20	165	-19060	2470	-327	0	-2	-8467	15.71	15.71	9.42	9.42	3	0.15	0.03	0.19	0.00	0.00	24.0
37	165	-14575	2928	-521	0	55	-7520	15.71	15.71	9.42	9.42	3	0.14	0.04	0.23	0.00	0.00	24.0
38	165	-21230	1601	-489	0	22	-8088	15.71	15.71	9.42	9.42	3	0.14	0.02	0.12	0.00	0.00	24.0
39	165	-15855	1843	-46	0	-45	-6568	15.71	15.71	9.42	9.42	3	0.12	0.02	0.14	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	248	-11998	1322	-308	0	273	-3790	15.71	15.71	9.42	9.42	3	0.07	0.02	0.11	0.00	0.00	24.0
2	248	-9193	1228	-315	0	278	-3165	15.71	15.71	9.42	9.42	2	0.09	0.02	0.10	0.00	0.00	24.0

3	248	-9157	1207	-163	0	150	-3139	15.71	15.71	9.42	9.42	2	0.08	0.02	0.10	0.00	0.00	24.0
4	248	-9300	826	-311	0	269	-2692	15.71	15.71	9.42	9.42	2	0.08	0.01	0.07	0.00	0.00	24.0
5	248	-9262	806	-159	0	142	-2666	15.71	15.71	9.42	9.42	2	0.07	0.01	0.07	0.00	0.00	24.0
6	248	-9276	1111	-491	0	423	-3030	15.71	15.71	9.42	9.42	2	0.09	0.01	0.09	0.00	0.00	24.0
7	248	-9149	1043	15	0	-1	-2943	15.71	15.71	9.42	9.42	2	0.08	0.01	0.09	0.00	0.00	24.0
8	248	-9308	990	-490	0	421	-2888	15.71	15.71	9.42	9.42	2	0.08	0.01	0.08	0.00	0.00	24.0
9	248	-9181	922	16	0	-4	-2801	15.71	15.71	9.42	9.42	2	0.07	0.01	0.08	0.00	0.00	24.0
10	248	-9193	1228	-315	0	278	-3165	15.71	15.71	9.42	9.42	2	0.09	0.02	0.10	0.00	0.00	24.0
11	248	-9157	1207	-163	0	150	-3139	15.71	15.71	9.42	9.42	2	0.08	0.02	0.10	0.00	0.00	24.0
12	248	-9300	826	-311	0	269	-2692	15.71	15.71	9.42	9.42	2	0.08	0.01	0.07	0.00	0.00	24.0
13	248	-9262	806	-159	0	142	-2666	15.71	15.71	9.42	9.42	2	0.07	0.01	0.07	0.00	0.00	24.0
14	248	-9276	1111	-491	0	423	-3030	15.71	15.71	9.42	9.42	2	0.09	0.01	0.09	0.00	0.00	24.0
15	248	-9149	1043	15	0	-1	-2943	15.71	15.71	9.42	9.42	2	0.08	0.01	0.09	0.00	0.00	24.0
16	248	-9308	990	-490	0	421	-2888	15.71	15.71	9.42	9.42	2	0.08	0.01	0.08	0.00	0.00	24.0
17	248	-9181	922	16	0	-4	-2801	15.71	15.71	9.42	9.42	2	0.07	0.01	0.08	0.00	0.00	24.0
18	248	-17438	2914	-612	0	563	-6551	15.71	15.71	9.42	9.42	3	0.12	0.04	0.22	0.00	0.00	24.0
19	248	-21428	2530	-592	0	527	-7380	15.71	15.71	9.42	9.42	3	0.13	0.03	0.18	0.00	0.00	24.0
20	248	-18200	2470	-327	0	268	-6430	15.71	15.71	9.42	9.42	3	0.12	0.03	0.19	0.00	0.00	24.0
37	248	-13718	2584	-521	0	485	-5246	15.71	15.71	9.42	9.42	3	0.10	0.03	0.21	0.00	0.00	24.0
38	248	-20370	1945	-489	0	425	-6626	15.71	15.71	9.42	9.42	3	0.12	0.02	0.14	0.00	0.00	24.0
39	248	-14998	1843	-46	0	-7	-5047	15.71	15.71	9.42	9.42	3	0.09	0.02	0.14	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	330	-11140	1322	-308	0	527	-2700	15.71	15.71	9.42	9.42	3	0.05	0.02	0.11	0.00	0.00	24.0
2	330	-8534	1228	-315	0	537	-2152	15.71	15.71	9.42	9.42	2	0.07	0.02	0.10	0.00	0.00	24.0
3	330	-8496	1207	-163	0	285	-2143	15.71	15.71	9.42	9.42	2	0.06	0.02	0.10	0.00	0.00	24.0
4	330	-8640	826	-311	0	526	-2011	15.71	15.71	9.42	9.42	2	0.07	0.01	0.07	0.00	0.00	24.0
5	330	-8602	806	-159	0	273	-2001	15.71	15.71	9.42	9.42	2	0.06	0.01	0.07	0.00	0.00	24.0
6	330	-8615	1111	-491	0	828	-2113	15.71	15.71	9.42	9.42	2	0.08	0.01	0.09	0.00	0.00	24.0
7	330	-8489	1043	15	0	-14	-2082	15.71	15.71	9.42	9.42	2	0.05	0.01	0.09	0.00	0.00	24.0
8	330	-8647	990	-490	0	825	-2071	15.71	15.71	9.42	9.42	2	0.08	0.01	0.08	0.00	0.00	24.0
9	330	-8521	922	16	0	-17	-2040	15.71	15.71	9.42	9.42	2	0.05	0.01	0.08	0.00	0.00	24.0
10	330	-8534	1228	-315	0	537	-2152	15.71	15.71	9.42	9.42	2	0.07	0.02	0.10	0.00	0.00	24.0
11	330	-8496	1207	-163	0	285	-2143	15.71	15.71	9.42	9.42	2	0.06	0.02	0.10	0.00	0.00	24.0
12	330	-8640	826	-311	0	526	-2011	15.71	15.71	9.42	9.42	2	0.07	0.01	0.07	0.00	0.00	24.0
13	330	-8602	806	-159	0	273	-2001	15.71	15.71	9.42	9.42	2	0.06	0.01	0.07	0.00	0.00	24.0
14	330	-8615	1111	-491	0	828	-2113	15.71	15.71	9.42	9.42	2	0.08	0.01	0.09	0.00	0.00	24.0
15	330	-8489	1043	15	0	-14	-2082	15.71	15.71	9.42	9.42	2	0.05	0.01	0.09	0.00	0.00	24.0
16	330	-8647	990	-490	0	825	-2071	15.71	15.71	9.42	9.42	2	0.08	0.01	0.08	0.00	0.00	24.0
17	330	-8521	922	16	0	-17	-2040	15.71	15.71	9.42	9.42	2	0.05	0.01	0.08	0.00	0.00	24.0
18	330	-16580	2707	-612	0	1068	-4232	15.71	15.71	9.42	9.42	3	0.09	0.03	0.21	0.00	0.00	24.0
19	330	-20570	2737	-592	0	1016	-5206	15.71	15.71	9.42	9.42	3	0.10	0.03	0.20	0.00	0.00	24.0
20	330	-17340	2470	-327	0	537	-4394	15.71	15.71	9.42	9.42	3	0.08	0.03	0.19	0.00	0.00	24.0
37	330	-12860	2240	-521	0	915	-3256	15.71	15.71	9.42	9.42	3	0.07	0.03	0.18	0.00	0.00	24.0
38	330	-19510	2289	-489	0	828	-4880	15.71	15.71	9.42	9.42	3	0.09	0.03	0.17	0.00	0.00	24.0
39	330	-14140	1843	-46	0	31	-3526	15.71	15.71	9.42	9.42	3	0.06	0.02	0.15	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 20 NI 178 NF 180 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 28C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-14360	1241	-350	0	-546	-6781	15.71	15.71	9.42	9.42	3	0.13	0.02	0.10	0.00	0.00	24.0
2	0	-11030	1170	-348	0	-551	-6026	15.71	15.71	9.42	9.42	2	0.17	0.01	0.10	0.00	0.00	24.0
3	0	-11030	1169	-183	0	-281	-6026	15.71	15.71	9.42	9.42	2	0.16	0.01	0.10	0.00	0.00	24.0
4	0	-11060	740	-354	0	-559	-4407	15.71	15.71	9.42	9.42	2	0.13	0.01	0.06	0.00	0.00	24.0
5	0	-11060	740	-190	0	-289	-4407	15.71	15.71	9.42	9.42	2	0.12	0.01	0.06	0.00	0.00	24.0
6	0	-11030	1021	-543	0	-869	-5460	15.71	15.71	9.42	9.42	2	0.16	0.01	0.08	0.00	0.00	24.0
7	0	-11050	1018	7	0	32	-5459	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
8	0	-11040	892	-545	0	-872	-4974	15.71	15.71	9.42	9.42	2	0.15	0.01	0.07	0.00	0.00	24.0
9	0	-11060	889	5	0	30	-4973	15.71	15.71	9.42	9.42	2	0.13	0.01	0.07	0.00	0.00	24.0
10	0	-11030	1170	-348	0	-551	-6026	15.71	15.71	9.42	9.42	2	0.17	0.01	0.10	0.00	0.00	24.0
11	0	-11030	1169	-183	0	-281	-6026	15.71	15.71	9.42	9.42	2	0.16	0.01	0.10	0.00	0.00	24.0
12	0	-11060	740	-354	0	-559	-4407	15.71	15.71	9.42	9.42	2	0.13	0.01	0.06	0.00	0.00	24.0
13	0	-11060	740	-190	0	-289	-4407	15.71	15.71	9.42	9.42	2	0.12	0.01	0.06	0.00	0.00	24.0
14	0	-11030	1021	-543	0	-869	-5460	15.71	15.71	9.42	9.42	2	0.16	0.01	0.08	0.00	0.00	24.0
15	0	-11050	1018	7	0	32	-5459	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
16	0	-11040	892	-545	0	-872	-4974	15.71	15.71	9.42	9.42	2	0.15	0.01	0.07	0.00	0.00	24.0
17	0	-11060	889	5	0	30	-4973	15.71	15.71	9.42	9.42	2	0.13	0.01	0.07	0.00	0.00	24.0
18	0	-19770	3445	-707	0	-1150	-14340	15.71	15.71	9.42	9.42	3	0.26	0.04	0.26	0.00	0.00	24.0
19	0	-23600	1738	-719	0	-1156	-12210	15.71	15.71	9.42	9.42	3	0.22	0.02	0.12	0.00	0.00	24.0
20	0	-20570	2389	-390	0	-661	-12300	15.71	15.71	9.42	9.42	3	0.22	0.03	0.18	0.00	0.00	24.0
37	0	-16140	3573	-584	0	-949	-12930	15.71	15.71	9.42	9.42	3	0.24	0.05	0.28	0.00	0.00	24.0
38	0	-22520	728	-604	0	-958	-9385	15.71	15.71	9.42	9.42	3	0.17	0.01	0.05	0.00	0.00	24.0
39	0	-17480	1812	-56	0	-134	-9543	15.71	15.71	9.42	9.42	3	0.17	0.02	0.14	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	83	-13502	1241	-350	0	-257	-5757	15.71	15.71	9.42	9.42	3	0.11	0.02	0.10	0.00	0.00	24.0
2	83	-10369	1170	-348	0	-264	-5060	15.71	15.71	9.42	9.42	2	0.13	0.01	0.10	0.00	0.00	24.0
3	83	-10370	1169	-183	0	-130	-5061	15.71	15.71	9.42	9.42	2	0.13	0.01	0.10	0.00	0.00	24.0
4	83	-10400	740	-354	0	-266	-3796	15.71	15.71	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
5	83	-10401	740	-190	0	-132	-3797	15.71	15.71	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
6	83	-10371	1021	-543	0	-421	-4618	15.71	15.71	9.42	9.42	2	0.13	0.01	0.08	0.00	0.00	24.0
7	83	-10390	1018	7	0	26	-4619	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
8	83	-10381	892	-545	0	-422	-4238	15.71	15.71	9.42	9.42	2	0.12	0.01	0.07	0.00	0.00	24.0
9	83	-10399	889	5	0	25	-4240	15.71	15.71	9.42	9.42	2	0.11	0.01	0.07	0.00	0.00	24.0
10	83	-10369	1170	-348	0	-264	-5060	15.71	15.71	9.42	9.42	2	0.13	0.01	0.10	0.00	0.00	24.0
11	83	-10370	1169	-183	0	-130	-5061	15.71	15.71	9.42	9.42	2	0.13	0.01	0.10	0.00	0.00	24.0
12	83	-10400	740	-354	0	-266	-3796	15.71	15.71	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
13	83	-10401	740	-190	0	-132	-3797	15.71	15.71	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
14	83	-10371	1021	-543	0	-421	-4618	15.71	15.71	9.42	9.42	2	0.13	0.01	0.08	0.00	0.00	24.0
15	83	-10390	1018	7	0	26	-4619	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
16	83	-10381	892	-545	0	-422	-4238	15.71	15.71	9.42	9.42	2	0.12	0.01	0.07	0.00	0.00	24.0
17	83	-10399	889	5	0	25	-4240	15.71	15.71	9.42	9.42	2	0.11	0.01	0.07	0.00	0.00	24.0
18	83	-18912	3239	-707	0	-567	-11582	15.71	15.71	9.42	9.42	3	0.21	0.04	0.24	0.00	0.00	24.0
19	83	-22740	1944	-719	0	-563	-10690	15.71	15.71	9.42	9.42	3	0.19	0.02	0.14	0.00	0.00	24.0
20	83	-19712	2389	-390	0	-339	-10330	15.71	15.71	9.42	9.42	3	0.18	0.03	0.18	0.00	0.00	24.0
37	83	-15282	3229	-584	0	-467	-10125	15.71	15.71	9.42	9.42	3	0.18	0.04	0.25	0.00	0.00	24.0
38	83	-21662	1072	-604	0	-460	-8642	15.71	15.71	9.42	9.42	3	0.15	0.01	0.08	0.00	0.00	24.0
39	83	-16622	1812	-56	0	-88	-8048	15.71	15.71	9.42	9.42	3	0.14	0.02	0.14	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	165	-12645	1241	-350	0	31	-4733	15.71	15.71	9.42	9.42	3	0.09	0.02	0.10	0.00	0.00	24.0
2	165	-9708	1170	-348	0	23	-4095	15.71	15.71	9.42	9.42	2	0.10	0.01	0.10	0.00	0.00	24.0
3	165	-9711	1169	-183	0	21	-4096	15.71	15.71	9.42	9.42	2	0.10	0.01	0.10	0.00	0.00	24.0
4	165	-9740	740	-354	0	26	-3186	15.71	15.71	9.42	9.42	2	0.08	0.01	0.06	0.00	0.00	24.0
5	165	-9742	740	-190	0	24	-3187	15.71	15.71	9.42	9.42	2	0.08	0.01	0.06	0.00	0.00	24.0
6	165	-9712	1021	-543	0	26	-3776	15.71	15.71	9.42	9.42	2	0.10	0.01	0.08	0.00	0.00	24.0
7	165	-9729	1018	7	0	20	-3780	15.71	15.71	9.42	9.42	2	0.10	0.01	0.08	0.00	0.00	24.0
8	165	-9722	892	-545	0	27	-3502	15.71	15.71	9.42	9.42	2	0.09	0.01	0.07	0.00	0.00	24.0
9	165	-9738	889	5	0	21	-3507	15.71	15.71	9.42	9.42	2	0.09	0.01	0.07	0.00	0.00	24.0
10	165	-9708	1170	-348	0	23	-4095	15.71	15.71	9.42	9.42	2	0.10	0.01	0.10	0.00	0.00	24.0
11	165	-9711	1169	-183	0	21	-4096	15.71	15.71	9.42	9.42	2	0.10	0.01	0.10	0.00	0.00	24.0
12	165	-9740	740	-354	0	26	-3186	15.71	15.71	9.42	9.42	2	0.08	0.01	0.06	0.00	0.00	24.0
13	165	-9742	740	-190	0	24	-3187	15.71	15.71	9.42	9.42	2	0.08	0.01	0.06	0.00	0.00	24.0
14	165	-9712	1021	-543	0	26	-3776	15.71	15.71	9.42	9.42	2	0.10	0.01	0.08	0.00	0.00	24.0
15	165	-9729	1018	7	0	20	-3780	15.71	15.71	9.42	9.42	2	0.10	0.01	0.08	0.00	0.00	24.0
16	165	-9722	892	-545	0	27	-3502	15.71	15.71	9.42	9.42	2	0.09	0.01	0.07	0.00	0.00	24.0
17	165	-9738	889	5	0	21	-3507	15.71	15.71	9.42	9.42	2	0.09	0.01	0.07	0.00	0.00	24.0
18	165	-18055	3032	-707	0	16	-8994	15.71	15.71	9.42	9.42	3	0.16	0.04	0.23	0.00	0.00	24.0
19	165	-21880	2151	-719	0	31	-9000	15.71	15.71	9.42	9.42	3	0.16	0.03	0.16	0.00	0.00	24.0
20	165	-18855	2389	-390	0	-17	-8360	15.71	15.71	9.42	9.42	3	0.15	0.03	0.18	0.00	0.00	24.0
37	165	-14425	2885	-584	0	14	-7604	15.71	15.71	9.42	9.42	3	0.14	0.04	0.23	0.00	0.00	24.0
38	165	-20805	1416	-604	0	38	-7616	15.71	15.71	9.42	9.42	3	0.13	0.02	0.10	0.00	0.00	24.0
39	165	-15765	1812	-56	0	-42	-6553	15.71	15.71	9.42	9.42	3	0.12	0.02	0.14	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	248	-11788	1241	-350	0	319	-3709	15.71	15.71	9.42	9.42	3	0.07	0.02	0.10	0.00	0.00	24.0
2	248	-9048	1170	-348	0	311	-3129	15.71	15.71	9.42	9.42	2	0.09	0.02	0.10	0.00	0.00	24.0
3	248	-9052	1169	-183	0	173	-3132	15.71	15.71	9.42	9.42	2	0.08	0.01	0.10	0.00	0.00	24.0
4	248	-9079	740	-354	0	319	-2575	15.71	15.71	9.42	9.42	2	0.07	0.01	0.06	0.00	0.00	24.0
5	248	-9082	740	-190	0	181	-2577	15.71	15.71	9.42	9.42	2	0.07	0.01	0.06	0.00	0.00	24.0
6	248	-9052	1021	-543	0	474	-2933	15.71	15.71	9.42	9.42	2	0.09	0.01	0.09	0.00	0.00	24.0
7	248	-9068	1018	7	0	14	-2940	15.71	15.71	9.42	9.42	2	0.08	0.01	0.09	0.00	0.00	24.0
8	248	-9062	892	-545	0	477	-2767	15.71	15.71	9.42	9.42	2	0.08	0.01	0.07	0.00	0.00	24.0
9	248	-9078	889	5	0	17	-2773	15.71	15.71	9.42	9.42	2	0.07	0.01	0.07	0.00	0.00	24.0
10	248	-9048	1170	-348	0	311	-3129	15.71	15.71	9.42	9.42	2	0.09	0.02	0.10	0.00	0.00	24.0
11	248	-9052	1169	-183	0	173	-3132	15.71	15.71	9.42	9.42	2	0.08	0.01	0.10	0.00	0.00	24.0
12	248	-9079	740	-354	0	319	-2575	15.71	15.71	9.42	9.42	2	0.07	0.01	0.06	0.00	0.00	24.0
13	248	-9082	740	-190	0	181	-2577	15.71	15.71	9.42	9.42	2	0.07	0.01	0.06	0.00	0.00	24.0
14	248	-9052	1021	-543	0	474	-2933	15.71	15.71	9.42	9.42	2	0.09	0.01	0.09	0.00	0.00	24.0
15	248	-9068	1018	7	0	14	-2940	15.71	15.71	9.42	9.42	2	0.08	0.01	0.09	0.00	0.00	24.0
16	248	-9062	892	-545	0	477	-2767	15.71	15.71	9.42	9.42	2	0.08	0.01	0.07	0.00	0.00	24.0
17	248	-9078	889	5	0	17	-2773	15.71	15.71	9.42	9.42	2	0.07	0.01	0.07	0.00	0.00	24.0
18	248	-17198	2826	-707	0	600	-6577	15.71	15.71	9.42	9.42	3	0.12	0.04	0.22	0.00	0.00	24.0
19	248	-21020	2358	-719	0	624	-7140	15.71	15.71	9.42	9.42	3	0.13	0.03	0.17	0.00	0.00	24.0
20	248	-17998	2389	-390	0	305	-6390	15.71	15.71	9.42	9.42	3	0.12	0.03	0.18	0.00	0.00	24.0
37	248	-13568	2541	-584	0	496	-5367	15.71	15.71	9.42	9.42	3	0.10	0.03	0.20	0.00	0.00	24.0
38	248	-19948	1760	-604	0	536	-6306	15.71	15.71	9.42	9.42	3	0.11	0.02	0.13	0.00	0.00	24.0
39	248	-14908	1812	-56	0	4	-5058	15.71	15.71	9.42	9.42	3	0.09	0.02	0.14	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	330	-10930	1241	-350	0	608	-2685	15.71	15.71	9.42	9.42	3	0.06	0.02	0.10	0.00	0.00	24.0
2	330	-8387	1170	-348	0	598	-2164	15.71	15.71	9.42	9.42	2	0.07	0.02	0.10	0.00	0.00	24.0
3	330	-8392	1169	-183	0	324	-2167	15.71	15.71	9.42	9.42	2	0.06	0.02	0.10	0.00	0.00	24.0
4	330	-8419	740	-354	0	611	-1964	15.71	15.71	9.42	9.42	2	0.07	0.01	0.06	0.00	0.00	24.0
5	330	-8423	740	-190	0	337	-1967	15.71	15.71	9.42	9.42	2	0.06	0.01	0.06	0.00	0.00	24.0
6	330	-8393	1021	-543	0	922	-2091	15.71	15.71	9.42	9.42	2	0.08	0.01	0.09	0.00	0.00	24.0
7	330	-8408	1018	7	0	9	-2100	15.71	15.71	9.42	9.42	2	0.05	0.01	0.09	0.00	0.00	24.0
8	330	-8403	892	-545	0	926	-2031	15.71	15.71	9.42	9.42	2	0.08	0.01	0.08	0.00	0.00	24.0
9	330	-8417	889	5	0	13	-2040	15.71	15.71	9.42	9.42	2	0.05	0.01	0.07	0.00	0.00	24.0
10	330	-8387	1170	-348	0	598	-2164	15.71	15.71	9.42	9.42	2	0.07	0.02	0.10	0.00	0.00	24.0
11	330	-8392	1169	-183	0	324	-2167	15.71	15.71	9.42	9.42	2	0.06	0.02	0.10	0.00	0.00	24.0
12	330	-8419	740	-354	0	611	-1964	15.71	15.71	9.42	9.42	2	0.07	0.01	0.06	0.00	0.00	24.0
13	330	-8423	740	-190	0	337	-1967	15.71	15.71	9.42	9.42	2	0.06	0.01	0.06	0.00	0.00	24.0
14	330	-8393	1021	-543	0	922	-2091	15.71	15.71	9.42	9.42	2	0.08	0.01	0.09	0.00	0.00	24.0
15	330	-8408	1018	7	0	9	-2100	15.71	15.71	9.42	9.42	2	0.05	0.01	0.09	0.00	0.00	24.0
16	330	-8403	892	-545	0	926	-2031	15.71	15.71	9.42	9.42	2	0.08	0.01	0.08	0.00	0.00	24.0
17	330	-8417	889	5	0	13	-2040	15.71	15.71	9.42	9.42	2	0.05	0.01	0.07	0.00	0.00	24.0
18	330	-16340	2620	-707	0	1183	-4330	15.71	15.71	9.42	9.42	3	0.09	0.03	0.20	0.00	0.00	24.0
19	330	-20160	2564	-719	0	1217	-5109	15.71	15.71	9.42	9.42	3	0.10	0.03	0.19	0.00	0.00	24.0
20	330	-17140	2389	-390	0	627	-4420	15.71	15.71	9.42	9.42	3	0.08	0.03	0.18	0.00	0.00	24.0
37	330	-12710	2197	-584	0	977	-3414	15.71	15.71	9.42	9.42	3	0.07	0.03	0.18	0.00	0.00	24.0
38	330	-19090	2104	-604	0	1034	-4712	15.71	15.71	9.42	9.42	3	0.09	0.03	0.16	0.00	0.00	24.0
39	330	-14050	1812	-56	0	50	-3563	15.71	15.71	9.42	9.42	3	0.06	0.02	0.14	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 21 NI 221 NF 223 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 27C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-13240	1663	-1012	0	-2027	-8053	15.71	15.71	9.42	9.42	3	0.17	0.02	0.13	0.00	0.00	24.0
2	0	-10110	1614	-905	0	-1787	-7420	15.71	15.71	9.42	9.42	2	0.24	0.02	0.13	0.00	0.00	24.0
3	0	-10180	1648	-724	0	-1476	-7549	15.71	15.71	9.42	9.42	2	0.23	0.02	0.14	0.00	0.00	24.0
4	0	-10190	910	-833	0	-1643	-4839	15.71	15.71	9.42	9.42	2	0.17	0.01	0.08	0.00	0.00	24.0
5	0	-10260	945	-652	0	-1332	-4969	15.71	15.71	9.42	9.42	2	0.16	0.01	0.08	0.00	0.00	24.0
6	0	-10060	1328	-1091	0	-2099	-6366	15.71	15.71	9.42	9.42	2	0.22	0.02	0.11	0.00	0.00	24.0
7	0	-10290	1442	-488	0	-1063	-6797	15.71	15.71	9.42	9.42	2	0.20	0.02	0.12	0.00	0.00	24.0
8	0	-10090	1117	-1070	0	-2056	-5592	15.71	15.71	9.42	9.42	2	0.20	0.01	0.09	0.00	0.00	24.0
9	0	-10310	1231	-466	0	-1020	-6023	15.71	15.71	9.42	9.42	2	0.18	0.02	0.10	0.00	0.00	24.0
10	0	-10110	1614	-905	0	-1787	-7420	15.71	15.71	9.42	9.42	2	0.24	0.02	0.13	0.00	0.00	24.0
11	0	-10180	1648	-724	0	-1476	-7549	15.71	15.71	9.42	9.42	2	0.23	0.02	0.14	0.00	0.00	24.0
12	0	-10190	910	-833	0	-1643	-4839	15.71	15.71	9.42	9.42	2	0.17	0.01	0.08	0.00	0.00	24.0
13	0	-10260	945	-652	0	-1332	-4969	15.71	15.71	9.42	9.42	2	0.16	0.01	0.08	0.00	0.00	24.0
14	0	-10060	1328	-1091	0	-2099	-6366	15.71	15.71	9.42	9.42	2	0.22	0.02	0.11	0.00	0.00	24.0
15	0	-10290	1442	-488	0	-1063	-6797	15.71	15.71	9.42	9.42	2	0.20	0.02	0.12	0.00	0.00	24.0
16	0	-10090	1117	-1070	0	-2056	-5592	15.71	15.71	9.42	9.42	2	0.20	0.01	0.09	0.00	0.00	24.0
17	0	-10310	1231	-466	0	-1020	-6023	15.71	15.71	9.42	9.42	2	0.18	0.02	0.10	0.00	0.00	24.0
18	0	-17290	4822	-1991	0	-3679	-18810	15.71	15.71	9.42	9.42	3	0.37	0.06	0.37	0.00	0.00	24.0
19	0	-21500	2026	-1909	0	-3344	-12820	15.71	15.71	9.42	9.42	3	0.26	0.03	0.15	0.00	0.00	24.0
20	0	-18640	3261	-1510	0	-2784	-15040	15.71	15.71	9.42	9.42	3	0.29	0.04	0.25	0.00	0.00	24.0

37	0	-13920	5177	-1712	0	-3305	-18270	15.71	15.71	9.42	9.42	3	0.36	0.07	0.41	0.00	0.00	24.0
38	0	-20930	517	-1575	0	-2747	-8292	15.71	15.71	9.42	9.42	3	0.18	0.02	0.09	0.00	0.00	24.0
39	0	-16160	2575	-911	0	-1814	-11980	15.71	15.71	9.42	9.42	3	0.23	0.03	0.20	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	83	-12383	1663	-1012	0	-1192	-6681	15.71	15.71	9.42	9.42	3	0.13	0.02	0.13	0.00	0.00	24.0
2	83	-9451	1614	-905	0	-1040	-6088	15.71	15.71	9.42	9.42	2	0.18	0.02	0.13	0.00	0.00	24.0
3	83	-9520	1648	-724	0	-879	-6190	15.71	15.71	9.42	9.42	2	0.18	0.02	0.14	0.00	0.00	24.0
4	83	-9531	910	-833	0	-956	-4088	15.71	15.71	9.42	9.42	2	0.13	0.01	0.08	0.00	0.00	24.0
5	83	-9600	945	-652	0	-794	-4190	15.71	15.71	9.42	9.42	2	0.13	0.01	0.08	0.00	0.00	24.0
6	83	-9401	1328	-1091	0	-1199	-5270	15.71	15.71	9.42	9.42	2	0.17	0.02	0.11	0.00	0.00	24.0
7	83	-9629	1442	-488	0	-661	-5608	15.71	15.71	9.42	9.42	2	0.16	0.02	0.12	0.00	0.00	24.0
8	83	-9430	1117	-1070	0	-1174	-4670	15.71	15.71	9.42	9.42	2	0.15	0.01	0.09	0.00	0.00	24.0
9	83	-9650	1231	-466	0	-636	-5008	15.71	15.71	9.42	9.42	2	0.14	0.02	0.10	0.00	0.00	24.0
10	83	-9451	1614	-905	0	-1040	-6088	15.71	15.71	9.42	9.42	2	0.18	0.02	0.13	0.00	0.00	24.0
11	83	-9520	1648	-724	0	-879	-6190	15.71	15.71	9.42	9.42	2	0.18	0.02	0.14	0.00	0.00	24.0
12	83	-9531	910	-833	0	-956	-4088	15.71	15.71	9.42	9.42	2	0.13	0.01	0.08	0.00	0.00	24.0
13	83	-9600	945	-652	0	-794	-4190	15.71	15.71	9.42	9.42	2	0.13	0.01	0.08	0.00	0.00	24.0
14	83	-9401	1328	-1091	0	-1199	-5270	15.71	15.71	9.42	9.42	2	0.17	0.02	0.11	0.00	0.00	24.0
15	83	-9629	1442	-488	0	-661	-5608	15.71	15.71	9.42	9.42	2	0.16	0.02	0.12	0.00	0.00	24.0
16	83	-9430	1117	-1070	0	-1174	-4670	15.71	15.71	9.42	9.42	2	0.15	0.01	0.09	0.00	0.00	24.0
17	83	-9650	1231	-466	0	-636	-5008	15.71	15.71	9.42	9.42	2	0.14	0.02	0.10	0.00	0.00	24.0
18	83	-16432	4616	-1991	0	-2036	-14917	15.71	15.71	9.42	9.42	3	0.28	0.06	0.36	0.00	0.00	24.0
19	83	-20642	2232	-1909	0	-1769	-11064	15.71	15.71	9.42	9.42	3	0.21	0.03	0.16	0.00	0.00	24.0
20	83	-17782	3261	-1510	0	-1538	-12349	15.71	15.71	9.42	9.42	3	0.23	0.04	0.25	0.00	0.00	24.0
37	83	-13062	4833	-1712	0	-1892	-14140	15.71	15.71	9.42	9.42	3	0.27	0.06	0.39	0.00	0.00	24.0
38	83	-20072	861	-1575	0	-1448	-7723	15.71	15.71	9.42	9.42	3	0.15	0.02	0.09	0.00	0.00	24.0
39	83	-15302	2575	-911	0	-1062	-9856	15.71	15.71	9.42	9.42	3	0.19	0.03	0.20	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	165	-11526	1663	-1012	0	-357	-5309	15.71	15.71	9.42	9.42	3	0.10	0.02	0.14	0.00	0.00	24.0
2	165	-8792	1614	-905	0	-293	-4757	15.71	15.71	9.42	9.42	2	0.13	0.02	0.14	0.00	0.00	24.0
3	165	-8861	1648	-724	0	-281	-4830	15.71	15.71	9.42	9.42	2	0.13	0.02	0.14	0.00	0.00	24.0
4	165	-8872	910	-833	0	-268	-3337	15.71	15.71	9.42	9.42	2	0.09	0.01	0.08	0.00	0.00	24.0
5	165	-8940	945	-652	0	-256	-3410	15.71	15.71	9.42	9.42	2	0.09	0.01	0.08	0.00	0.00	24.0
6	165	-8742	1328	-1091	0	-298	-4175	15.71	15.71	9.42	9.42	2	0.11	0.02	0.11	0.00	0.00	24.0
7	165	-8968	1442	-488	0	-259	-4418	15.71	15.71	9.42	9.42	2	0.12	0.02	0.12	0.00	0.00	24.0
8	165	-8769	1117	-1070	0	-291	-3749	15.71	15.71	9.42	9.42	2	0.10	0.01	0.09	0.00	0.00	24.0
9	165	-8990	1231	-466	0	-251	-3992	15.71	15.71	9.42	9.42	2	0.11	0.02	0.10	0.00	0.00	24.0
10	165	-8792	1614	-905	0	-293	-4757	15.71	15.71	9.42	9.42	2	0.13	0.02	0.14	0.00	0.00	24.0
11	165	-8861	1648	-724	0	-281	-4830	15.71	15.71	9.42	9.42	2	0.13	0.02	0.14	0.00	0.00	24.0
12	165	-8872	910	-833	0	-268	-3337	15.71	15.71	9.42	9.42	2	0.09	0.01	0.08	0.00	0.00	24.0
13	165	-8940	945	-652	0	-256	-3410	15.71	15.71	9.42	9.42	2	0.09	0.01	0.08	0.00	0.00	24.0
14	165	-8742	1328	-1091	0	-298	-4175	15.71	15.71	9.42	9.42	2	0.11	0.02	0.11	0.00	0.00	24.0
15	165	-8968	1442	-488	0	-259	-4418	15.71	15.71	9.42	9.42	2	0.12	0.02	0.12	0.00	0.00	24.0
16	165	-8769	1117	-1070	0	-291	-3749	15.71	15.71	9.42	9.42	2	0.10	0.01	0.09	0.00	0.00	24.0
17	165	-8990	1231	-466	0	-251	-3992	15.71	15.71	9.42	9.42	2	0.11	0.02	0.10	0.00	0.00	24.0
18	165	-15575	4409	-1991	0	-394	-11193	15.71	15.71	9.42	9.42	3	0.20	0.06	0.34	0.00	0.00	24.0
19	165	-19785	2438	-1909	0	-195	-9138	15.71	15.71	9.42	9.42	3	0.16	0.03	0.18	0.00	0.00	24.0
20	165	-16925	3261	-1510	0	-292	-9658	15.71	15.71	9.42	9.42	3	0.17	0.04	0.25	0.00	0.00	24.0
37	165	-12205	4489	-1712	0	-479	-10294	15.71	15.71	9.42	9.42	3	0.19	0.06	0.36	0.00	0.00	24.0
38	165	-19215	1205	-1575	0	-149	-6871	15.71	15.71	9.42	9.42	3	0.12	0.02	0.09	0.00	0.00	24.0
39	165	-14445	2575	-911	0	-310	-7733	15.71	15.71	9.42	9.42	3	0.14	0.03	0.20	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	248	-10669	1663	-1012	0	478	-3937	15.71	15.71	9.42	9.42	3	0.08	0.02	0.14	0.00	0.00	24.0
2	248	-8134	1614	-905	0	453	-3426	15.71	15.71	9.42	9.42	2	0.10	0.02	0.14	0.00	0.00	24.0
3	248	-8202	1648	-724	0	316	-3471	15.71	15.71	9.42	9.42	2	0.10	0.02	0.14	0.00	0.00	24.0
4	248	-8213	910	-833	0	419	-2586	15.71	15.71	9.42	9.42	2	0.08	0.01	0.08	0.00	0.00	24.0
5	248	-8281	945	-652	0	281	-2631	15.71	15.71	9.42	9.42	2	0.07	0.01	0.08	0.00	0.00	24.0
6	248	-8083	1328	-1091	0	602	-3080	15.71	15.71	9.42	9.42	2	0.10	0.02	0.11	0.00	0.00	24.0
7	248	-8308	1442	-488	0	143	-3228	15.71	15.71	9.42	9.42	2	0.09	0.02	0.12	0.00	0.00	24.0
8	248	-8108	1117	-1070	0	592	-2828	15.71	15.71	9.42	9.42	2	0.09	0.01	0.09	0.00	0.00	24.0
9	248	-8331	1231	-466	0	133	-2976	15.71	15.71	9.42	9.42	2	0.08	0.02	0.10	0.00	0.00	24.0
10	248	-8134	1614	-905	0	453	-3426	15.71	15.71	9.42	9.42	2	0.10	0.02	0.14	0.00	0.00	24.0
11	248	-8202	1648	-724	0	316	-3471	15.71	15.71	9.42	9.42	2	0.10	0.02	0.14	0.00	0.00	24.0
12	248	-8213	910	-833	0	419	-2586	15.71	15.71	9.42	9.42	2	0.08	0.01	0.08	0.00	0.00	24.0
13	248	-8281	945	-652	0	281	-2631	15.71	15.71	9.42	9.42	2	0.07	0.01	0.08	0.00	0.00	24.0
14	248	-8083	1328	-1091	0	602	-3080	15.71	15.71	9.42	9.42	2	0.10	0.02	0.11	0.00	0.00	24.0
15	248	-8308	1442	-488	0	143	-3228	15.71	15.71	9.42	9.42	2	0.09	0.02	0.12	0.00	0.00	24.0
16	248	-8108	1117	-1070	0	592	-2828	15.71	15.71	9.42	9.42	2	0.09	0.01	0.09	0.00	0.00	24.0
17	248	-8331	1231	-466	0	133	-2976	15.71	15.71	9.42	9.42	2	0.08	0.02	0.10	0.00	0.00	24.0
18	248	-14718	4202	-1991	0	1249	-7641	15.71	15.71	9.42	9.42	3	0.15	0.05	0.33	0.00	0.00	24.0
19	248	-18928	2645	-1909	0	1380	-7041	15.71	15.71	9.42	9.42	3	0.14	0.03	0.20	0.00	0.00	24.0
20	248	-16068	3261	-1510	0	954	-6968	15.71	15.71	9.42	9.42	3	0.13	0.04	0.25	0.00	0.00	24.0
37	248	-11348	4145	-1712	0	933	-6732	15.71	15.71	9.42	9.42	3	0.13	0.05	0.34	0.00	0.00	24.0
38	248	-18358	1549	-1575	0	1150	-5735	15.71	15.71	9.42	9.42	3	0.11	0.02	0.12	0.00	0.00	24.0
39	248	-13588	2575	-911	0	441	-5609	15.71	15.71	9.42	9.42	3	0.10	0.03	0.20	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	330	-9812	1663	-1012	0	1313	-2565	15.71	15.71	9.42	9.42	3	0.07	0.02	0.14	0.00	0.00	24.0
2	330	-7475	1614	-905	0	1200	-2094	15.71	15.71	9.42	9.42	2	0.09	0.02	0.14	0.00	0.00	24.0
3	330	-7542	1648	-724	0	913	-2111	15.71	15.71	9.42	9.42	2	0.08	0.02	0.14	0.00	0.00	24.0
4	330	-7554	910	-833	0	1106	-1835	15.71	15.71	9.42	9.42	2	0.08	0.01	0.08	0.00	0.00	24.0
5	330	-7621	945	-652	0	819	-1851	15.71	15.71	9.42	9.42	2	0.07	0.01	0.08	0.00	0.00	24.0
6	330	-7424	1328	-1091	0	1502	-1984	15.71	15.71	9.42	9.42	2	0.10	0.02	0.11	0.00	0.00	24.0
7	330	-7647	1442	-488	0	546	-2039	15.71	15.71	9.42	9.42	2	0.07	0.02	0.12	0.00	0.00	24.0
8	330	-7448	1117	-1070	0	1474	-1906	15.71	15.71	9.42	9.42	2	0.10	0.01	0.10	0.00	0.00	24.0
9	330	-7671	1231	-466	0	517	-1961	15.71	15.71	9.42	9.42	2	0.06	0.02	0.10	0.00	0.00	24.0
10	330	-7475	1614	-905	0	1200	-2094	15.71	15.71	9.42	9.42	2	0.09	0.02	0.14	0.00	0.00	24.0
11	330	-7542	1648	-724	0	913	-2111	15.71	15.71	9.42	9.42	2	0.08	0.02	0.14	0.00	0.00	24.0
12	330	-7554	910	-833	0	1106	-1835	15.71	15.71	9.42	9.42	2	0.08	0.01	0.08	0.00	0.00	24.0
13	330	-7621	945	-652	0	819	-1851	15.71	15.71	9.42	9.42	2	0.07	0.01	0.08	0.00	0.00	24.0
14	330	-7424	1328	-1091	0	1502	-1984	15.71	15.71	9.42	9.42	2	0.10	0.02	0.11	0.00	0.00	24.0
15	330	-7647	1442	-488	0	546	-2039	15.71	15.71	9.42	9.42	2	0.07	0.02	0.12	0.00	0.00	24.0
16	330	-7448	1117	-1070	0	1474	-1906	15.71	15.71	9.42	9.42	2	0.10	0.01	0.10	0.00	0.00	24.0
17	330	-7671	1231	-466	0	517	-1961	15.71	15.71	9.42	9.42	2	0.06	0.02	0.10	0.00	0.00	24.0
18	330	-13860	3996	-1991	0	2892	-4258	15.71	15.71	9.42	9.42	3	0.13	0.05	0.32	0.00	0.00	24.0
19	330	-18070	2851	-1909	0	2954	-4774	15.71	15.71	9.42	9.42	3	0.14	0.04	0.22	0.00	0.00	24.0
20	330	-15210	3261	-1510	0	2200	-4277	15.71	15.71	9.42	9.42	3	0.11	0.04	0.25	0.00	0.00	24.0
37	330	-10490	3801	-1712	0	2346	-3454	15.71	15.71	9.42	9.42	3	0.11	0.05	0.31	0.00	0.00	24.0
38	330	-17500	1893	-1575	0	2449	-4315	15.71	15.71	9.42	9.42	3	0.12	0.02	0.14	0.00	0.00	24.0
39	330	-12730	2575	-911	0	1193	-3486	15.71	15.71	9.42	9.42	3	0.08	0.03	0.21	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 22 NI 264 NF 266 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 25C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-8881	164	-432	0	-812	-532	6.28	6.28	9.42	9.42	3	0.06	0.01	0.05	0.00	0.00	24.0
2	0	-7790	297	-379	0	-756	-823	6.28	6.28	9.42	9.42	2	0.12	0.01	0.05	0.00	0.00	24.0
3	0	-7657	298	-282	0	-507	-821	6.28	6.28	9.42	9.42	2	0.11	0.01	0.03	0.00	0.00	24.0
4	0	-6006	-46	-382	0	-743	2	6.28	6.28	9.42	9.42	2	0.05	0.01	0.05	0.00	0.00	24.0
5	0	-5873	-45	-285	0	-494	4	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
6	0	-7321	176	-494	0	-1042	-536	6.28	6.28	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
7	0	-6878	179	-169	0	-212	-530	6.28	6.28	9.42	9.42	2	0.07	0.00	0.02	0.00	0.00	24.0
8	0	-6786	73	-495	0	-1038	-289	6.28	6.28	9.42	9.42	2	0.08	0.01	0.06	0.00	0.00	24.0
9	0	-6342	76	-170	0	-208	-283	6.28	6.28	9.42	9.42	2	0.04	0.00	0.02	0.00	0.00	24.0
10	0	-7790	297	-379	0	-756	-823	6.28	6.28	9.42	9.42	2	0.12	0.01	0.05	0.00	0.00	24.0
11	0	-7657	298	-282	0	-507	-821	6.28	6.28	9.42	9.42	2	0.11	0.01	0.03	0.00	0.00	24.0
12	0	-6006	-46	-382	0	-743	2	6.28	6.28	9.42	9.42	2	0.05	0.01	0.05	0.00	0.00	24.0
13	0	-5873	-45	-285	0	-494	4	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
14	0	-7321	176	-494	0	-1042	-536	6.28	6.28	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
15	0	-6878	179	-169	0	-212	-530	6.28	6.28	9.42	9.42	2	0.07	0.00	0.02	0.00	0.00	24.0
16	0	-6786	73	-495	0	-1038	-289	6.28	6.28	9.42	9.42	2	0.08	0.01	0.06	0.00	0.00	24.0
17	0	-6342	76	-170	0	-208	-283	6.28	6.28	9.42	9.42	2	0.04	0.00	0.02	0.00	0.00	24.0
18	0	-12750	612	-422	0	-1276	-1394	6.28	6.28	9.42	9.42	3	0.15	0.02	0.06	0.00	0.00	24.0
19	0	-9477	-774	-247	0	-1082	995	6.28	6.28	9.42	9.42	3	0.11	0.02	0.08	0.00	0.00	24.0
20	0	-10520	-43	-392	0	-808	-249	6.28	6.28	9.42	9.42	3	0.04	0.01	0.05	0.00	0.00	24.0
37	0	-13120	1156	-513	0	-1222	-2301	6.28	6.28	9.42	9.42	3	0.23	0.03	0.12	0.00	0.00	24.0
38	0	-7669	-1154	-221	0	-899	1682	6.28	6.28	9.42	9.42	3	0.18	0.03	0.13	0.00	0.00	24.0
39	0	-9403	65	-463	0	-441	-392	6.28	6.28	9.42	9.42	3	0.04	0.01	0.05	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	95	-8325	164	-432	0	-402	-377	6.28	6.28	9.42	9.42	3	0.04	0.01	0.05	0.00	0.00	24.0
2	95	-7362	297	-379	0	-395	-540	6.28	6.28	9.42	9.42	2	0.07	0.01	0.05	0.00	0.00	24.0
3	95	-7230	298	-282	0	-239	-538	6.28	6.28	9.42	9.42	2	0.07	0.01	0.03	0.00	0.00	24.0
4	95	-5578	-46	-382	0	-380	-42	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
5	95	-5446	-45	-285	0	-224	-39	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
6	95	-6894	176	-494	0	-573	-369	6.28	6.28	9.42	9.42	2	0.06	0.01	0.06	0.00	0.00	24.0
7	95	-6450	179	-169	0	-51	-360	6.28	6.28	9.42	9.42	2	0.04	0.00	0.02	0.00	0.00	24.0
8	95	-6358	73	-495	0	-568	-220	6.28	6.28	9.42	9.42	2	0.05	0.01	0.06	0.00	0.00	24.0
9	95	-5914	76	-170	0	-46	-210	6.28	6.28	9.42	9.42	2	0.03	0.00	0.02	0.00	0.00	24.0
10	95	-7362	297	-379	0	-395	-540	6.28	6.28	9.42	9.42	2	0.07	0.01	0.05	0.00	0.00	24.0
11	95	-7230	298	-282	0	-239	-538	6.28	6.28	9.42	9.42	2	0.07	0.01	0.03	0.00	0.00	24.0
12	95	-5578	-46	-382	0	-380	-42	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
13	95	-5446	-45	-285	0	-224	-39	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
14	95	-6894	176	-494	0	-573	-369	6.28	6.28	9.42	9.42	2	0.06	0.01	0.06	0.00	0.00	24.0
15	95	-6450	179	-169	0	-51	-360	6.28	6.28	9.42	9.42	2	0.04	0.00	0.02	0.00	0.00	24.0
16	95	-6358	73	-495	0	-568	-220	6.28	6.28	9.42	9.42	2	0.05	0.01	0.06	0.00	0.00	24.0
17	95	-5914	76	-170	0	-46	-210	6.28	6.28	9.42	9.42	2	0.03	0.00	0.02	0.00	0.00	24.0
18	95	-12192	493	-422	0	-875	-869	6.28	6.28	9.42	9.42	3	0.09	0.01	0.05	0.00	0.00	24.0
19	95	-8921	-655	-247	0	-848	317	6.28	6.28	9.42	9.42	3	0.05	0.02	0.06	0.00	0.00	24.0
20	95	-9964	-43	-265	0	-497	-290	6.28	6.28	9.42	9.42	3	0.04	0.01	0.03	0.00	0.00	24.0
37	95	-12562	958	-513	0	-734	-1297	6.28	6.28	9.42	9.42	3	0.13	0.02	0.10	0.00	0.00	24.0
38	95	-7113	-956	-221	0	-689	680	6.28	6.28	9.42	9.42	3	0.08	0.02	0.10	0.00	0.00	24.0
39	95	-8847	65	-251	0	-105	-331	6.28	6.28	9.42	9.42	3	0.03	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	190	-7770	164	-432	0	8	-221	6.28	6.28	9.42	9.42	3	0.02	0.01	0.05	0.00	0.00	24.0
2	190	-6935	297	-379	0	-35	-258	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
3	190	-6802	298	-282	0	29	-255	6.28	6.28	9.42	9.42	2	0.03	0.01	0.03	0.00	0.00	24.0
4	190	-5151	-46	-382	0	-17	-86	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
5	190	-5018	-45	-285	0	47	-82	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
6	190	-6466	176	-494	0	-104	-202	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
7	190	-6023	179	-169	0	110	-190	6.28	6.28	9.42	9.42	2	0.03	0.00	0.02	0.00	0.00	24.0
8	190	-5931	73	-495	0	-98	-151	6.28	6.28	9.42	9.42	2	0.02	0.01	0.06	0.00	0.00	24.0
9	190	-5487	76	-170	0	116	-138	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
10	190	-6935	297	-379	0	-35	-258	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
11	190	-6802	298	-282	0	29	-255	6.28	6.28	9.42	9.42	2	0.03	0.01	0.03	0.00	0.00	24.0
12	190	-5151	-46	-382	0	-17	-86	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
13	190	-5018	-45	-285	0	47	-82	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
14	190	-6466	176	-494	0	-104	-202	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
15	190	-6023	179	-169	0	110	-190	6.28	6.28	9.42	9.42	2	0.03	0.00	0.02	0.00	0.00	24.0
16	190	-5931	73	-495	0	-98	-151	6.28	6.28	9.42	9.42	2	0.02	0.01	0.06	0.00	0.00	24.0
17	190	-5487	76	-170	0	116	-138	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
18	190	-11635	374	-422	0	-474	-458	6.28	6.28	9.42	9.42	3	0.05	0.01	0.05	0.00	0.00	24.0
19	190	-8366	-537	-247	0	-613	-250	6.28	6.28	9.42	9.42	3	0.04	0.01	0.05	0.00	0.00	24.0
20	190	-9407	-43	-156	0	-299	-330	6.28	6.28	9.42	9.42	3	0.04	0.00	0.02	0.00	0.00	24.0
37	190	-12005	760	-513	0	-247	-481	6.28	6.28	9.42	9.42	3	0.05	0.02	0.08	0.00	0.00	24.0
38	190	-6558	-758	-221	0	-479	-134	6.28	6.28	9.42	9.42	3	0.03	0.02	0.08	0.00	0.00	24.0
39	190	-8292	65	-69	0	45	-269	6.28	6.28	9.42	9.42	3	0.03	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	285	-7214	164	-432	0	418	-66	6.28	6.28	9.42	9.42	3	0.02	0.01	0.05	0.00	0.00	24.0
2	285	-6508	297	-379	0	325	24	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
3	285	-6374	298	-282	0	297	28	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
4	285	-4724	-46	-382	0	346	-130	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
5	285	-4590	-45	-285	0	318	-125	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
6	285	-6038	176	-494	0	365	-35	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
7	285	-5596	179	-169	0	271	-20	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
8	285	-5504	73	-495	0	372	-82	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
9	285	-5060	76	-170	0	277	-66	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
10	285	-6508	297	-379	0	325	24	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
11	285	-6374	298	-282	0	297	28	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
12	285	-4724	-46	-382	0	346	-130	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
13	285	-4590	-45	-285	0	318	-125	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
14	285	-6038	176	-494	0	365	-35	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
15	285	-5596	179	-169	0	271	-20	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
16	285	-5504	73	-495	0	372	-82	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
17	285	-5060	76	-170	0	277	-66	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
18	285	-11078	255	-422	0	-73	-159	6.28	6.28	9.42	9.42	3	0.02	0.01	0.05	0.00	0.00	24.0
19	285	-7810	-418	-247	0	-379	-703	6.28	6.28	9.42	9.42	3	0.08	0.01	0.05	0.00	0.00	24.0
20	285	-8850	-43	-65	0	-196	-371	6.28	6.28	9.42	9.42	3	0.04	0.00	0.01	0.00	0.00	24.0
37	285	-11448	562	-513	0	241	146	6.28	6.28	9.42	9.42	3	0.02	0.01	0.06	0.00	0.00	24.0
38	285	-6002	-560	-221	0	-269	-760	6.28	6.28	9.42	9.42	3	0.08	0.01	0.06	0.00	0.00	24.0

39	285	-7736	65	82	0	37	-207	6.28	6.28	9.42	9.42	3	0.02	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	380	-6658	164	-432	0	828	89	6.28	6.28	9.42	9.42	3	0.04	0.01	0.05	0.00	0.00	24.0
2	380	-6080	297	-379	0	685	306	6.28	6.28	9.42	9.42	2	0.06	0.01	0.05	0.00	0.00	24.0
3	380	-5947	298	-282	0	564	312	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
4	380	-4296	-46	-382	0	709	-174	6.28	6.28	9.42	9.42	2	0.06	0.01	0.05	0.00	0.00	24.0
5	380	-4163	-45	-285	0	588	-169	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
6	380	-5611	176	-494	0	834	132	6.28	6.28	9.42	9.42	2	0.06	0.01	0.06	0.00	0.00	24.0
7	380	-5168	179	-169	0	432	150	6.28	6.28	9.42	9.42	2	0.04	0.00	0.02	0.00	0.00	24.0
8	380	-5076	73	-495	0	842	-13	6.28	6.28	9.42	9.42	2	0.05	0.01	0.06	0.00	0.00	24.0
9	380	-4632	76	-170	0	439	6	6.28	6.28	9.42	9.42	2	0.03	0.00	0.02	0.00	0.00	24.0
10	380	-6080	297	-379	0	685	306	6.28	6.28	9.42	9.42	2	0.06	0.01	0.05	0.00	0.00	24.0
11	380	-5947	298	-282	0	564	312	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
12	380	-4296	-46	-382	0	709	-174	6.28	6.28	9.42	9.42	2	0.06	0.01	0.05	0.00	0.00	24.0
13	380	-4163	-45	-285	0	588	-169	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
14	380	-5611	176	-494	0	834	132	6.28	6.28	9.42	9.42	2	0.06	0.01	0.06	0.00	0.00	24.0
15	380	-5168	179	-169	0	432	150	6.28	6.28	9.42	9.42	2	0.04	0.00	0.02	0.00	0.00	24.0
16	380	-5076	73	-495	0	842	-13	6.28	6.28	9.42	9.42	2	0.05	0.01	0.06	0.00	0.00	24.0
17	380	-4632	76	-170	0	439	6	6.28	6.28	9.42	9.42	2	0.03	0.00	0.02	0.00	0.00	24.0
18	380	-10520	136	-422	0	328	27	6.28	6.28	9.42	9.42	3	0.02	0.01	0.05	0.00	0.00	24.0
19	380	-7254	-299	-247	0	-144	-1043	6.28	6.28	9.42	9.42	3	0.11	0.01	0.03	0.00	0.00	24.0
20	380	-8294	-43	8	0	-170	-412	6.28	6.28	9.42	9.42	3	0.04	0.00	0.00	0.00	0.00	24.0
37	380	-10890	364	-513	0	729	586	6.28	6.28	9.42	9.42	3	0.06	0.01	0.06	0.00	0.00	24.0
38	380	-5446	-362	-221	0	-59	-1198	6.28	6.28	9.42	9.42	3	0.13	0.01	0.04	0.00	0.00	24.0
39	380	-7180	65	203	0	-101	-145	6.28	6.28	9.42	9.42	3	0.02	0.00	0.02	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

VERIFICA NODO IN TESTA AL PILASTRO, NODO NUM. 266 NON CONFINATO

(par.7.2.2 NTC2018 "La domanda di resistenza valutata con i criteri della progettazione in capacità può essere assunta non superiore alla domanda di resistenza valutata per il caso di comportamento strutturale non dissipativo.")

PROGETTAZIONE IN CAPACITA'

Asse loc. pilastro y nodo ESTERNO: As2(inf)= 4.02, As1(sup)= 6.03, Hjw= 40.0 cm, bj= 45.0 cm, hjc= 20.0 cm
Asse loc. pilastro z nodo ESTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 30.0 cm, hjc= 50.0 cm

FxMin,inf	FxMin,sup	FxMax,sup	FySup	FzSup	Vjbdy	Vjbdz	Vres,y	Vres,z	I.R.compr.	Ashy	Ashz	PASSO	Nota
daN					daN		daN			cmq		cm	
-4163	1	-0	0	0	26425	17616	63005	105009	0.42	4.37	--	11.94	

VERIFICA DI RESISTENZA CON SOLLECITAZIONI COMPORTAMENTO NON DISSIPATIVO

Asse loc. pilastro y nodo ESTERNO: Hjw= 40.0 cm, bj= 45.0 cm, hjc= 20.0 cm, db1= 45.0 cm

NC	Fx,sup	Fx,inf	Mb	Vb	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-0	-6080	-2673	1806	0	6600	63005	0.10	0.00	40.00	
3	-0	-5947	-2651	1800	0	6546	63005	0.10	0.00	40.00	
4	-0	-4296	-462	1135	0	1142	63005	0.02	0.00	40.00	
5	-0	-4163	-440	1129	0	1086	63005	0.02	0.00	40.00	
6	-0	-5611	-1925	1579	0	4753	63005	0.08	0.00	40.00	
7	-0	-5168	-1851	1558	0	4570	63005	0.07	0.00	40.00	
8	-0	-5076	-1262	1377	0	3116	63005	0.05	0.00	40.00	
9	-0	-4632	-1188	1357	0	2933	63005	0.05	0.00	40.00	
10	-0	-6080	-2673	1806	0	6600	63005	0.10	0.00	40.00	
11	-0	-5947	-2651	1800	0	6546	63005	0.10	0.00	40.00	
12	-0	-4296	-462	1135	0	1142	63005	0.02	0.00	40.00	
13	-0	-4163	-440	1129	0	1086	63005	0.02	0.00	40.00	
14	-0	-5611	-1925	1579	0	4753	63005	0.08	0.00	40.00	
15	-0	-5168	-1851	1558	0	4570	63005	0.07	0.00	40.00	
16	-0	-5076	-1262	1377	0	3116	63005	0.05	0.00	40.00	
17	-0	-4632	-1188	1357	0	2933	63005	0.05	0.00	40.00	

Asse loc. pilastro z nodo ESTERNO: Hjw= 40.0 cm, bj= 30.0 cm, hjc= 50.0 cm, db1= 45.0 cm

NC	Fx,sup	Fx,inf	Mb	Vb	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-0	-6080	-2200	1743	0	5432	105009	0.05	0.00	40.00	
3	-0	-5947	-1953	1666	0	4822	105009	0.05	0.00	40.00	
4	-0	-4296	-2128	1720	0	5254	105009	0.05	0.00	40.00	
5	-0	-4163	-1881	1643	0	4644	105009	0.04	0.00	40.00	
6	-0	-5611	-2463	1825	0	6081	105009	0.06	0.00	40.00	
7	-0	-5168	-1640	1568	0	4049	105009	0.04	0.00	40.00	
8	-0	-5076	-2441	1818	0	6027	105009	0.06	0.00	40.00	
9	-0	-4632	-1618	1561	0	3995	105009	0.04	0.00	40.00	
10	-0	-6080	-2200	1743	0	5432	105009	0.05	0.00	40.00	
11	-0	-5947	-1953	1666	0	4822	105009	0.05	0.00	40.00	
12	-0	-4296	-2128	1720	0	5254	105009	0.05	0.00	40.00	
13	-0	-4163	-1881	1643	0	4644	105009	0.04	0.00	40.00	
14	-0	-5611	-2463	1825	0	6081	105009	0.06	0.00	40.00	
15	-0	-5168	-1640	1568	0	4049	105009	0.04	0.00	40.00	
16	-0	-5076	-2441	1818	0	6027	105009	0.06	0.00	40.00	
17	-0	-4632	-1618	1561	0	3995	105009	0.04	0.00	40.00	

CONFRONTO E SINTESI CONCLUSIVE (si assume in ogni caso passo <= 15 cm)

I.R.compr.	Ashy	Ashz	PASSO	Nota
	cmq		cm	
0.10	--	--	15.00	**VERIFICATO**

ASTA NUM. 23 NI 298 NF 271 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 20C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice resistenza	aswta	aswto	PASSO

	--																	
	cm	daN				daN*m		cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-12630	-165	-95	0	-1302	434	6.28	6.28	12.57	12.57	3	0.05	0.00	0.01	0.00	0.00	24.0
2	0	-9499	556	-125	0	-1380	-901	6.28	6.28	12.57	12.57	2	0.10	0.01	0.05	0.00	0.00	24.0
3	0	-9473	550	-0	0	-591	-889	6.28	6.28	12.57	12.57	2	0.07	0.01	0.05	0.00	0.00	24.0
4	0	-9963	-804	-146	0	-1413	1556	6.28	6.28	12.57	12.57	2	0.14	0.01	0.08	0.00	0.00	24.0
5	0	-9937	-811	-21	0	-624	1568	6.28	6.28	12.57	12.57	2	0.11	0.01	0.08	0.00	0.00	24.0
6	0	-9691	88	-278	0	-2313	-56	6.28	6.28	12.57	12.57	2	0.12	0.00	0.03	0.00	0.00	24.0
7	0	-9605	66	138	0	319	-15	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
8	0	-9830	-320	-284	0	-2323	682	6.28	6.28	12.57	12.57	2	0.14	0.01	0.03	0.00	0.00	24.0
9	0	-9745	-342	132	0	309	723	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
10	0	-9499	556	-125	0	-1380	-901	6.28	6.28	12.57	12.57	2	0.10	0.01	0.05	0.00	0.00	24.0
11	0	-9473	550	-0	0	-591	-889	6.28	6.28	12.57	12.57	2	0.07	0.01	0.05	0.00	0.00	24.0
12	0	-9963	-804	-146	0	-1413	1556	6.28	6.28	12.57	12.57	2	0.14	0.01	0.08	0.00	0.00	24.0
13	0	-9937	-811	-21	0	-624	1568	6.28	6.28	12.57	12.57	2	0.11	0.01	0.08	0.00	0.00	24.0
14	0	-9691	88	-278	0	-2313	-56	6.28	6.28	12.57	12.57	2	0.12	0.00	0.03	0.00	0.00	24.0
15	0	-9605	66	138	0	319	-15	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
16	0	-9830	-320	-284	0	-2323	682	6.28	6.28	12.57	12.57	2	0.14	0.01	0.03	0.00	0.00	24.0
17	0	-9745	-342	132	0	309	723	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
18	0	-14210	1398	-185	0	-2837	-2291	6.28	6.28	12.57	12.57	3	0.15	0.03	0.11	0.00	0.00	24.0
19	0	-16260	-2093	-314	0	-3092	3923	6.28	6.28	12.57	12.57	3	0.23	0.04	0.18	0.00	0.00	24.0
20	0	-14710	-321	-765	0	-1754	763	6.28	6.28	12.57	12.57	3	0.07	0.01	0.07	0.00	0.00	24.0
37	0	-12730	2620	-92	0	-2214	-4485	6.28	6.28	12.57	12.57	3	0.25	0.05	0.24	0.00	0.00	24.0
38	0	-16150	-3199	-307	0	-2638	5872	6.28	6.28	12.57	12.57	3	0.32	0.06	0.28	0.00	0.00	24.0
39	0	-13560	-246	-1059	0	-409	606	6.28	6.28	12.57	12.57	3	0.03	0.02	0.10	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	95	-11890	-165	-95	0	-1212	277	6.28	6.28	12.57	12.57	3	0.05	0.00	0.01	0.00	0.00	24.0
2	95	-8929	556	-125	0	-1261	-373	6.28	6.28	12.57	12.57	2	0.08	0.01	0.05	0.00	0.00	24.0
3	95	-8903	550	-0	0	-590	-367	6.28	6.28	12.57	12.57	2	0.04	0.01	0.05	0.00	0.00	24.0
4	95	-9393	-804	-146	0	-1275	792	6.28	6.28	12.57	12.57	2	0.09	0.01	0.07	0.00	0.00	24.0
5	95	-9367	-811	-21	0	-604	798	6.28	6.28	12.57	12.57	2	0.07	0.01	0.08	0.00	0.00	24.0
6	95	-9121	88	-278	0	-2049	28	6.28	6.28	12.57	12.57	2	0.11	0.00	0.03	0.00	0.00	24.0
7	95	-9035	66	138	0	187	48	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
8	95	-9260	-320	-284	0	-2053	378	6.28	6.28	12.57	12.57	2	0.12	0.01	0.03	0.00	0.00	24.0
9	95	-9175	-342	132	0	183	397	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
10	95	-8929	556	-125	0	-1261	-373	6.28	6.28	12.57	12.57	2	0.08	0.01	0.05	0.00	0.00	24.0
11	95	-8903	550	-0	0	-590	-367	6.28	6.28	12.57	12.57	2	0.04	0.01	0.05	0.00	0.00	24.0
12	95	-9393	-804	-146	0	-1275	792	6.28	6.28	12.57	12.57	2	0.09	0.01	0.07	0.00	0.00	24.0
13	95	-9367	-811	-21	0	-604	798	6.28	6.28	12.57	12.57	2	0.07	0.01	0.08	0.00	0.00	24.0
14	95	-9121	88	-278	0	-2049	28	6.28	6.28	12.57	12.57	2	0.11	0.00	0.03	0.00	0.00	24.0
15	95	-9035	66	138	0	187	48	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
16	95	-9260	-320	-284	0	-2053	378	6.28	6.28	12.57	12.57	2	0.12	0.01	0.03	0.00	0.00	24.0
17	95	-9175	-342	132	0	183	397	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
18	95	-13470	1398	-185	0	-2661	-963	6.28	6.28	12.57	12.57	3	0.11	0.03	0.11	0.00	0.00	24.0
19	95	-15520	-2093	-314	0	-2793	1935	6.28	6.28	12.57	12.57	3	0.14	0.04	0.17	0.00	0.00	24.0
20	95	-13970	-321	-513	0	-1150	458	6.28	6.28	12.57	12.57	3	0.05	0.01	0.05	0.00	0.00	24.0
37	95	-11989	2620	-92	0	-2126	-1996	6.28	6.28	12.57	12.57	3	0.13	0.05	0.22	0.00	0.00	24.0
38	95	-15408	-3199	-307	0	-2346	2833	6.28	6.28	12.57	12.57	3	0.17	0.06	0.28	0.00	0.00	24.0
39	95	-12820	-246	-638	0	393	372	6.28	6.28	12.57	12.57	3	0.02	0.01	0.06	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	190	-11150	-165	-95	0	-1122	120	6.28	6.28	12.57	12.57	3	0.04	0.00	0.01	0.00	0.00	24.0
2	190	-8359	556	-125	0	-1143	156	6.28	6.28	12.57	12.57	2	0.06	0.01	0.05	0.00	0.00	24.0
3	190	-8333	550	-0	0	-590	156	6.28	6.28	12.57	12.57	2	0.04	0.01	0.05	0.00	0.00	24.0
4	190	-8823	-804	-146	0	-1137	28	6.28	6.28	12.57	12.57	2	0.06	0.01	0.07	0.00	0.00	24.0
5	190	-8797	-811	-21	0	-585	28	6.28	6.28	12.57	12.57	2	0.03	0.01	0.07	0.00	0.00	24.0
6	190	-8551	88	-278	0	-1785	112	6.28	6.28	12.57	12.57	2	0.10	0.00	0.03	0.00	0.00	24.0
7	190	-8465	66	138	0	56	110	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
8	190	-8690	-320	-284	0	-1784	74	6.28	6.28	12.57	12.57	2	0.09	0.01	0.03	0.00	0.00	24.0
9	190	-8605	-342	132	0	58	72	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
10	190	-8359	556	-125	0	-1143	156	6.28	6.28	12.57	12.57	2	0.06	0.01	0.05	0.00	0.00	24.0
11	190	-8333	550	-0	0	-590	156	6.28	6.28	12.57	12.57	2	0.04	0.01	0.05	0.00	0.00	24.0
12	190	-8823	-804	-146	0	-1137	28	6.28	6.28	12.57	12.57	2	0.06	0.01	0.07	0.00	0.00	24.0
13	190	-8797	-811	-21	0	-585	28	6.28	6.28	12.57	12.57	2	0.03	0.01	0.07	0.00	0.00	24.0
14	190	-8551	88	-278	0	-1785	112	6.28	6.28	12.57	12.57	2	0.10	0.00	0.03	0.00	0.00	24.0
15	190	-8465	66	138	0	56	110	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
16	190	-8690	-320	-284	0	-1784	74	6.28	6.28	12.57	12.57	2	0.09	0.01	0.03	0.00	0.00	24.0
17	190	-8605	-342	132	0	58	72	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
18	190	-12730	1398	-185	0	-2485	366	6.28	6.28	12.57	12.57	3	0.09	0.03	0.11	0.00	0.00	24.0
19	190	-14780	-2093	-314	0	-2494	-54	6.28	6.28	12.57	12.57	3	0.09	0.04	0.17	0.00	0.00	24.0
20	190	-13230	-321	-297	0	-768	153	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
37	190	-11248	2620	-92	0	-2038	492	6.28	6.28	12.57	12.57	3	0.08	0.05	0.22	0.00	0.00	24.0
38	190	-14665	-3199	-307	0	-2054	-207	6.28	6.28	12.57	12.57	3	0.07	0.06	0.26	0.00	0.00	24.0
39	190	-12080	-246	-278	0	823	138	6.28	6.28	12.57	12.57	3	0.03	0.00	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	285	-10409	-165	-95	0	-1033	-37	6.28	6.28	12.57	12.57	3	0.04	0.00	0.01	0.00	0.00	24.0
2	285	-7789	556	-125	0	-1024	684	6.28	6.28	12.57	12.57	2	0.08	0.01	0.05	0.00	0.00	24.0
3	285	-7763	550	-0	0	-590	678	6.28	6.28	12.57	12.57	2	0.06	0.01	0.05	0.00	0.00	24.0
4	285	-8253	-804	-146	0	-998	-735	6.28	6.28	12.57	12.57	2	0.08	0.01	0.07	0.00	0.00	24.0
5	285	-8227	-811	-21	0	-565	-742	6.28	6.28	12.57	12.57	2	0.06	0.01	0.08	0.00	0.00	24.0
6	285	-7981	88	-278	0	-1521	196	6.28	6.28	12.57	12.57	2	0.09	0.00	0.03	0.00	0.00	24.0
7	285	-7895	66	138	0	-75	173	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
8	285	-8120	-320	-284	0	-1514	-230	6.28	6.28	12.57	12.57	2	0.09	0.01	0.03	0.00	0.00	24.0
9	285	-8035	-342	132	0	-68	-253	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
10	285	-7789	556	-125	0	-1024	684	6.28	6.28	12.57	12.57	2	0.08	0.01	0.05	0.00	0.00	24.0
11	285	-7763	550	-0	0	-590	678	6.28	6.28	12.57	12.57	2	0.06	0.01	0.05	0.00	0.00	24.0
12	285	-8253	-804	-146	0	-998	-735	6.28	6.28	12.57	12.57	2	0.08	0.01	0.07	0.00	0.00	24.0
13	285	-8227	-811	-21	0	-565	-742	6.28	6.28	12.57	12.57	2	0.06	0.01	0.08	0.00	0.00	24.0
14	285	-7981	88	-278	0	-1521	196	6.28	6.28	12.57	12.57	2	0.09	0.00	0.03	0.00	0.00	24.0
15	285	-7895	66	138	0	-75	173	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
16	285	-8120	-320	-284	0	-1514	-230	6.28	6.28	12.57	12.57	2	0.09	0.01	0.03	0.00	0.00	24.0
17	285	-8035	-342	132	0	-68	-253	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
18	285	-11990	1398	-185	0	-2309	1694	6.28	6.28	12.57	12.57	3	0.12	0.03	0.12	0.00	0.00	24.0
19	285	-14040	-2093	-314	0	-2196	-2042	6.28	6.28	12.57	12.57	3	0.13	0.04	0.17	0.00	0.00	24.0
20	285	-12490	-321	-117	0	-574	-152	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
37	285	-10508	2620	-92	0	-1951	2981	6.28	6.28	12.57	12.57	3	0.17	0.05	0.25	0.00	0.00	24.0
38	285	-13922	-3199	-307	0	-1762	-3246	6.28	6.28	12.57	12.57	3	0.18	0.06	0.29	0.00	0.00	24.0
39	285	-11340	-246	22	0	940	-96	6.28	6.28	12.57	12.57	3	0.03	0.00	0.02	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	380	-9669	-165	-95	0	-943	-194	6.28	6.28	12.57	12.57	3	0.04	0.00	0.01	0.00	0.00	24.0
2	380	-7219	556	-125	0	-905	1213	6.28	6.28	12.57	12.57	2	0.10	0.01	0.05	0.00	0.00	24.0

3	380	-7193	550	-0	0	-590	1200	6.28	6.28	12.57	12.57	2	0.09	0.01	0.05	0.00	0.00	24.0
4	380	-7683	-804	-146	0	-860	-1499	6.28	6.28	12.57	12.57	2	0.12	0.01	0.08	0.00	0.00	24.0
5	380	-7657	-811	-21	0	-545	-1512	6.28	6.28	12.57	12.57	2	0.11	0.01	0.08	0.00	0.00	24.0
6	380	-7411	88	-278	0	-1257	279	6.28	6.28	12.57	12.57	2	0.07	0.00	0.03	0.00	0.00	24.0
7	380	-7325	66	138	0	-207	235	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
8	380	-7550	-320	-284	0	-1244	-534	6.28	6.28	12.57	12.57	2	0.08	0.01	0.03	0.00	0.00	24.0
9	380	-7465	-342	132	0	-193	-578	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
10	380	-7219	556	-125	0	-905	1213	6.28	6.28	12.57	12.57	2	0.10	0.01	0.05	0.00	0.00	24.0
11	380	-7193	550	-0	0	-590	1200	6.28	6.28	12.57	12.57	2	0.09	0.01	0.05	0.00	0.00	24.0
12	380	-7683	-804	-146	0	-860	-1499	6.28	6.28	12.57	12.57	2	0.12	0.01	0.08	0.00	0.00	24.0
13	380	-7657	-811	-21	0	-545	-1512	6.28	6.28	12.57	12.57	2	0.11	0.01	0.08	0.00	0.00	24.0
14	380	-7411	88	-278	0	-1257	279	6.28	6.28	12.57	12.57	2	0.07	0.00	0.03	0.00	0.00	24.0
15	380	-7325	66	138	0	-207	235	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
16	380	-7550	-320	-284	0	-1244	-534	6.28	6.28	12.57	12.57	2	0.08	0.01	0.03	0.00	0.00	24.0
17	380	-7465	-342	132	0	-193	-578	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
18	380	-11250	1398	-185	0	-2133	3023	6.28	6.28	12.57	12.57	3	0.18	0.03	0.13	0.00	0.00	24.0
19	380	-13300	-2093	-314	0	-1897	-4030	6.28	6.28	12.57	12.57	3	0.23	0.04	0.19	0.00	0.00	24.0
20	380	-11750	-321	27	0	-534	-458	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
37	380	-9767	2620	-92	0	-1863	5470	6.28	6.28	12.57	12.57	3	0.31	0.05	0.25	0.00	0.00	24.0
38	380	-13180	-3199	-307	0	-1470	-6285	6.28	6.28	12.57	12.57	3	0.35	0.06	0.29	0.00	0.00	24.0
39	380	-10600	-246	261	0	801	-330	6.28	6.28	12.57	12.57	3	0.03	0.00	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

VERIFICA NODO IN TESTA AL PILASTRO, NODO NUM. 271 NON CONFINATO

(par.7.2.2 NTC2018 "La domanda di resistenza valutata con i criteri della progettazione in capacità può essere assunta non superiore alla domanda di resistenza valutata per il caso di comportamento strutturale non dissipativo.")

PROGETTAZIONE IN CAPACITA'

Asse loc. pilastro y nodo INTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 50.0 cm, hjc= 30.0 cm
Asse loc. pilastro z nodo: --

FxMin,inf	FxMin,sup	FxMax,sup	FySup	FzSup	Vjbdy	Vjbdz	Vres,y	Vres,z	I.R.compr.	Ashy	Ashz	PASSO	Nota
daN					daN		daN			cmq		cm	
-7193	-3996	-4233	131	96	35102	--	129932	--	0.27	8.78	--	5.18	

VERIFICA DI RESISTENZA CON SOLLECITAZIONI COMPORTAMENTO NON DISSIPATIVO

Asse loc. pilastro y nodo INTERNO: Hjw= 40.0 cm, bj= 50.0 cm, hjc= 30.0 cm, db1= 45.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb,1	Mb,2	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-4026	-7219	-2256	-665	144	3783	129997	0.03	0.00	40.00	
3	-3996	-7193	-2248	-677	142	3737	130006	0.03	0.00	40.00	
4	-4233	-7683	-1097	-2247	134	2706	129932	0.02	0.00	40.00	
5	-4204	-7657	-1090	-2259	131	2755	129941	0.02	0.00	40.00	
6	-4133	-7411	-1858	-1206	143	1467	129963	0.01	0.00	40.00	
7	-4035	-7325	-1835	-1244	136	1323	129994	0.01	0.00	40.00	
8	-4195	-7550	-1511	-1680	140	278	129944	0.00	0.00	40.00	
9	-4097	-7465	-1487	-1719	133	440	129975	0.00	0.00	40.00	
10	-4026	-7219	-2256	-665	144	3783	129997	0.03	0.00	40.00	
11	-3996	-7193	-2248	-677	142	3737	130006	0.03	0.00	40.00	
12	-4233	-7683	-1097	-2247	134	2706	129932	0.02	0.00	40.00	
13	-4204	-7657	-1090	-2259	131	2755	129941	0.02	0.00	40.00	
14	-4133	-7411	-1858	-1206	143	1467	129963	0.01	0.00	40.00	
15	-4035	-7325	-1835	-1244	136	1323	129994	0.01	0.00	40.00	
16	-4195	-7550	-1511	-1680	140	278	129944	0.00	0.00	40.00	
17	-4097	-7465	-1487	-1719	133	440	129975	0.00	0.00	40.00	

CONFRONTO E SINTESI CONCLUSIVE (si assume in ogni caso passo <= 15 cm)

I.R.compr.	Ashy	Ashz	PASSO	Nota
	cmq		cm	
0.03	--	--	15.00	**VERIFICATO**

ASTA NUM. 24 NI 78 NF 77 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 6B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-23970	-814	36	0	66	10330	15.71	15.71	9.42	9.42	3	0.18	0.01	0.06	0.00	0.00	24.0
2	0	-18560	-519	-8	0	-37	6966	15.71	15.71	9.42	9.42	2	0.17	0.01	0.04	0.00	0.00	24.0
3	0	-18540	-494	80	0	180	6821	15.71	15.71	9.42	9.42	2	0.17	0.01	0.04	0.00	0.00	24.0
4	0	-18330	-759	-25	0	-78	9068	15.71	15.71	9.42	9.42	2	0.22	0.01	0.06	0.00	0.00	24.0
5	0	-18310	-734	62	0	139	8923	15.71	15.71	9.42	9.42	2	0.22	0.01	0.06	0.00	0.00	24.0
6	0	-18510	-631	-116	0	-304	7871	15.71	15.71	9.42	9.42	2	0.20	0.01	0.05	0.00	0.00	24.0
7	0	-18430	-550	176	0	418	7387	15.71	15.71	9.42	9.42	2	0.19	0.01	0.04	0.00	0.00	24.0
8	0	-18440	-703	-121	0	-317	8502	15.71	15.71	9.42	9.42	2	0.21	0.01	0.05	0.00	0.00	24.0
9	0	-18360	-622	171	0	406	8018	15.71	15.71	9.42	9.42	2	0.20	0.01	0.05	0.00	0.00	24.0
10	0	-18560	-519	-8	0	-37	6966	15.71	15.71	9.42	9.42	2	0.17	0.01	0.04	0.00	0.00	24.0
11	0	-18540	-494	80	0	180	6821	15.71	15.71	9.42	9.42	2	0.17	0.01	0.04	0.00	0.00	24.0
12	0	-18330	-759	-25	0	-78	9068	15.71	15.71	9.42	9.42	2	0.22	0.01	0.06	0.00	0.00	24.0
13	0	-18310	-734	62	0	139	8923	15.71	15.71	9.42	9.42	2	0.22	0.01	0.06	0.00	0.00	24.0
14	0	-18510	-631	-116	0	-304	7871	15.71	15.71	9.42	9.42	2	0.20	0.01	0.05	0.00	0.00	24.0
15	0	-18430	-550	176	0	418	7387	15.71	15.71	9.42	9.42	2	0.19	0.01	0.04	0.00	0.00	24.0
16	0	-18440	-703	-121	0	-317	8502	15.71	15.71	9.42	9.42	2	0.21	0.01	0.05	0.00	0.00	24.0
17	0	-18360	-622	171	0	406	8018	15.71	15.71	9.42	9.42	2	0.20	0.01	0.05	0.00	0.00	24.0
18	0	-34830	577	70	0	111	14750	15.71	15.71	9.42	9.42	3	0.25	0.01	0.04	0.00	0.00	24.0
19	0	-27250	-3632	-64	0	-179	22290	15.71	15.71	9.42	9.42	3	0.38	0.05	0.25	0.00	0.00	24.0
20	0	-30120	-1271	294	0	660	16950	15.71	15.71	9.42	9.42	3	0.29	0.02	0.09	0.00	0.00	24.0
37	0	-35100	2213	126	0	241	9572	15.71	15.71	9.42	9.42	3	0.16	0.03	0.14	0.00	0.00	24.0
38	0	-22470	-4802	-98	0	-242	22140	15.71	15.71	9.42	9.42	3	0.39	0.06	0.35	0.00	0.00	24.0
39	0	-27250	-868	499	0	1156	13240	15.71	15.71	9.42	9.42	3	0.23	0.01	0.06	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	110	-22825	-814	36	0	27	9434	15.71	15.71	9.42	9.42	3	0.16	0.01	0.06	0.00	0.00	24.0
2	110	-17680	-519	-8	0	-29	6395	15.71	15.71	9.42	9.42	2	0.16	0.01	0.04	0.00	0.00	24.0
3	110	-17660	-494	80	0	92	6277	15.71	15.71	9.42	9.42	2	0.15	0.01	0.04	0.00	0.00	24.0
4	110	-17450	-759	-25	0	-50	8234	15.71	15.71	9.42	9.42	2	0.20	0.01	0.06	0.00	0.00	24.0
5	110	-17430	-734	62	0	70	8115	15.71	15.71	9.42	9.42	2	0.20	0.01	0.06	0.00	0.00	24.0
6	110	-17630	-631	-116	0	-177	7177	15.71	15.71	9.42	9.42	2	0.18	0.01	0.05	0.00	0.00	24.0
7	110	-17550	-550	176	0	225	6782	15.71	15.71	9.42	9.42	2	0.17	0.01	0.04	0.00	0.00	24.0
8	110	-17560	-703	-121	0	-183	7729	15.71	15.71	9.42	9.42	2	0.19	0.01	0.05	0.00	0.00	24.0
9	110	-17480	-622	171	0	218	7334	15.71	15.71	9.42	9.42	2	0.18	0.01	0.05	0.00	0.00	24.0
10	110	-17680	-519	-8	0	-29	6395	15.71	15.71	9.42	9.42	2	0.16	0.01	0.04	0.00	0.00	24.0
11	110	-17660	-494	80	0	92	6277	15.71	15.71	9.42	9.42	2	0.15	0.01	0.04	0.00	0.00	24.0
12	110	-17450	-759	-25	0	-50	8234	15.71	15.71	9.42	9.42	2	0.20	0.01	0.06	0.00	0.00	24.0
13	110	-17430	-734	62	0	70	8115	15.71	15.71	9.42	9.42	2	0.20	0.01	0.06	0.00	0.00	24.0
14	110	-17630	-631	-116	0	-177	7177	15.71	15.71	9.42	9.42	2	0.18	0.01	0.05	0.00	0.00	24.0
15	110	-17550	-550	176	0	225	6782	15.71	15.71	9.42	9.42	2	0.17	0.01	0.04	0.00	0.00	24.0
16	110	-17560	-703	-121	0	-183	7729	15.71	15.71	9.42	9.42	2	0.19	0.01	0.05	0.00	0.00	24.0
17	110	-17480	-622	171	0	218	7334	15.71	15.71	9.42	9.42	2	0.18	0.01	0.05	0.00	0.00	24.0
18	110	-33688	197	70	0	34	15177	15.71	15.71	9.42	9.42	3	0.25	0.00	0.01	0.00	0.00	24.0
19	110	-26108	-3252	-64	0	-109	18506	15.71	15.71	9.42	9.42	3	0.32	0.04	0.23	0.00	0.00	24.0
20	110	-28975	-1271	294	0	337	15552	15.71	15.71	9.42	9.42	3	0.27	0.02	0.09	0.00	0.00	24.0
37	110	-33958	1579	126	0	103	11657	15.71	15.71	9.42	9.42	3	0.20	0.02	0.10	0.00	0.00	24.0
38	110	-21328	-4168	-98	0	-135	17207	15.71	15.71	9.42	9.42	3	0.30	0.05	0.30	0.00	0.00	24.0
39	110	-26105	-868	499	0	608	12285	15.71	15.71	9.42	9.42	3	0.21	0.01	0.06	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	220	-21680	-814	36	0	-12	8537	15.71	15.71	9.42	9.42	3	0.15	0.01	0.06	0.00	0.00	24.0
2	220	-16800	-519	-8	0	-20	5825	15.71	15.71	9.42	9.42	2	0.14	0.01	0.04	0.00	0.00	24.0
3	220	-16780	-494	80	0	4	5734	15.71	15.71	9.42	9.42	2	0.14	0.01	0.04	0.00	0.00	24.0
4	220	-16570	-759	-25	0	-23	7399	15.71	15.71	9.42	9.42	2	0.18	0.01	0.06	0.00	0.00	24.0
5	220	-16550	-734	62	0	1	7307	15.71	15.71	9.42	9.42	2	0.18	0.01	0.06	0.00	0.00	24.0
6	220	-16750	-631	-116	0	-49	6482	15.71	15.71	9.42	9.42	2	0.16	0.01	0.05	0.00	0.00	24.0
7	220	-16670	-550	176	0	31	6178	15.71	15.71	9.42	9.42	2	0.15	0.01	0.04	0.00	0.00	24.0
8	220	-16680	-703	-121	0	-50	6955	15.71	15.71	9.42	9.42	2	0.17	0.01	0.05	0.00	0.00	24.0
9	220	-16600	-622	171	0	31	6650	15.71	15.71	9.42	9.42	2	0.16	0.01	0.05	0.00	0.00	24.0
10	220	-16800	-519	-8	0	-20	5825	15.71	15.71	9.42	9.42	2	0.14	0.01	0.04	0.00	0.00	24.0
11	220	-16780	-494	80	0	4	5734	15.71	15.71	9.42	9.42	2	0.14	0.01	0.04	0.00	0.00	24.0
12	220	-16570	-759	-25	0	-23	7399	15.71	15.71	9.42	9.42	2	0.18	0.01	0.06	0.00	0.00	24.0
13	220	-16550	-734	62	0	1	7307	15.71	15.71	9.42	9.42	2	0.18	0.01	0.06	0.00	0.00	24.0
14	220	-16750	-631	-116	0	-49	6482	15.71	15.71	9.42	9.42	2	0.16	0.01	0.05	0.00	0.00	24.0
15	220	-16670	-550	176	0	31	6178	15.71	15.71	9.42	9.42	2	0.15	0.01	0.04	0.00	0.00	24.0
16	220	-16680	-703	-121	0	-50	6955	15.71	15.71	9.42	9.42	2	0.17	0.01	0.05	0.00	0.00	24.0
17	220	-16600	-622	171	0	31	6650	15.71	15.71	9.42	9.42	2	0.16	0.01	0.05	0.00	0.00	24.0
18	220	-32545	-183	70	0	-43	15186	15.71	15.71	9.42	9.42	3	0.26	0.00	0.01	0.00	0.00	24.0
19	220	-24965	-2872	-64	0	-38	15140	15.71	15.71	9.42	9.42	3	0.26	0.04	0.20	0.00	0.00	24.0
20	220	-27830	-1271	294	0	14	14155	15.71	15.71	9.42	9.42	3	0.24	0.02	0.09	0.00	0.00	24.0
37	220	-32815	946	126	0	-35	13045	15.71	15.71	9.42	9.42	3	0.22	0.01	0.06	0.00	0.00	24.0
38	220	-20185	-3535	-98	0	-27	12972	15.71	15.71	9.42	9.42	3	0.23	0.04	0.26	0.00	0.00	24.0
39	220	-24960	-868	499	0	59	11330	15.71	15.71	9.42	9.42	3	0.20	0.01	0.06	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	330	-20535	-814	36	0	-51	7640	15.71	15.71	9.42	9.42	3	0.13	0.01	0.06	0.00	0.00	24.0
2	330	-15920	-519	-8	0	-12	5254	15.71	15.71	9.42	9.42	2	0.13	0.01	0.04	0.00	0.00	24.0
3	330	-15900	-494	80	0	-84	5190	15.71	15.71	9.42	9.42	2	0.13	0.01	0.04	0.00	0.00	24.0
4	330	-15690	-759	-25	0	5	6565	15.71	15.71	9.42	9.42	2	0.16	0.01	0.06	0.00	0.00	24.0
5	330	-15670	-734	62	0	-67	6500	15.71	15.71	9.42	9.42	2	0.16	0.01	0.06	0.00	0.00	24.0
6	330	-15870	-631	-116	0	78	5788	15.71	15.71	9.42	9.42	2	0.14	0.01	0.05	0.00	0.00	24.0
7	330	-15790	-550	176	0	-162	5573	15.71	15.71	9.42	9.42	2	0.14	0.01	0.04	0.00	0.00	24.0
8	330	-15800	-703	-121	0	83	6182	15.71	15.71	9.42	9.42	2	0.15	0.01	0.05	0.00	0.00	24.0
9	330	-15720	-622	171	0	-157	5966	15.71	15.71	9.42	9.42	2	0.15	0.01	0.05	0.00	0.00	24.0
10	330	-15920	-519	-8	0	-12	5254	15.71	15.71	9.42	9.42	2	0.13	0.01	0.04	0.00	0.00	24.0
11	330	-15900	-494	80	0	-84	5190	15.71	15.71	9.42	9.42	2	0.13	0.01	0.04	0.00	0.00	24.0
12	330	-15690	-759	-25	0	5	6565	15.71	15.71	9.42	9.42	2	0.16	0.01	0.06	0.00	0.00	24.0
13	330	-15670	-734	62	0	-67	6500	15.71	15.71	9.42	9.42	2	0.16	0.01	0.06	0.00	0.00	24.0
14	330	-15870	-631	-116	0	78	5788	15.71	15.71	9.42	9.42	2	0.14	0.01	0.05	0.00	0.00	24.0
15	330	-15790	-550	176	0	-162	5573	15.71	15.71	9.42	9.42	2	0.14	0.01	0.04	0.00	0.00	24.0
16	330	-15800	-703	-121	0	83	6182	15.71	15.71	9.42	9.42	2	0.15	0.01	0.05	0.00	0.00	24.0
17	330	-15720	-622	171	0	-157	5966	15.71	15.71	9.42	9.42	2	0.15	0.01	0.05	0.00	0.00	24.0
18	330	-31402	-563	70	0	-120	14777	15.71	15.71	9.42	9.42	3	0.25	0.01	0.04	0.00	0.00	24.0
19	330	-23822	-2491	-64	0	32	12192	15.71	15.71	9.42	9.42	3	0.21	0.03	0.18	0.00	0.00	24.0
20	330	-26685	-1271	294	0	-310	12758	15.71	15.71	9.42	9.42	3	0.22	0.02	0.09	0.00	0.00	24.0
37	330	-31672	312	126	0	-174	13736	15.71	15.71	9.42	9.42	3	0.23	0.00	0.02	0.00	0.00	24.0
38	330	-19042	-2901	-98	0	80	9433	15.71	15.71	9.42	9.42	3	0.17	0.04	0.22	0.00	0.00	24.0
39	330	-23815	-868	499	0	-489	10374	15.71	15.71	9.42	9.42	3	0.18	0.01	0.06	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	440	-19390	-814	36	0	-90	6744	15.71	15.71	9.42	9.42	3	0.12	0.01	0.06	0.00	0.00	24.0
2	440	-15040	-519	-8	0	-3	4684	15.71	15.71	9.42	9.42	2	0.12	0.01	0.04	0.00	0.00	24.0
3	440	-15020	-494	80	0	-171	4646	15.71	15.71	9.42	9.42	2	0.12	0.01	0.04	0.00	0.00	24.0
4	440	-14810	-759	-25	0	32	5730	15.71	15.71	9.42	9.42	2	0.14	0.01	0.06	0.00	0.00	24.0
5	440	-14790	-734	62	0	-136	5692	15.71	15.71	9.42	9.42	2	0.14	0.01	0.06	0.00	0.00	24.0
6	440	-14990	-631	-116	0	206	5094	15.71	15.71	9.42	9.42	2	0.13	0.01	0.05	0.00	0.00	24.0
7	440	-14910	-550	176	0	-356	4968	15.71	15.71	9.42	9.42	2	0.13	0.01	0.04	0.00	0.00	24.0
8	440	-14920	-703	-121	0	216	5408	15.71	15.71	9.42	9.42	2	0.14	0.01	0.06	0.00	0.00	24.0
9	440	-14840	-622	171	0	-345	5282	15.71	15.71	9.42	9.42	2	0.14	0.01	0.05	0.00	0.00	24.0
10	440	-15040	-519	-8	0	-3	4684	15.71	15.71	9.42	9.42	2	0.12	0.01	0.04	0.00	0.00	24.0
11	440	-15020	-494	80	0	-171	4646	15.71	15.71	9.42	9.42	2	0.12	0.01	0.04	0.00	0.00	24.0
12	440	-14810	-759	-25	0	32	5730	15.71	15.71	9.42	9.42	2	0.14	0.01	0.06	0.00	0.00	24.0
13	440	-14790	-734	62	0	-136	5692	15.71	15.71	9.42	9.42	2	0.14	0.01	0.06	0.00	0.00	24.0
14	440	-14990	-631	-116	0	206	5094	15.71	15.71	9.42	9.42	2	0.13	0.01	0.05	0.00	0.00	24.0
15	440	-14910	-550	176	0	-356	4968	15.71	15.71	9.42	9.42	2	0.13	0.01	0.04	0.00	0.00	24.0
16	440	-14920	-703	-121	0	216	5408	15.71	15.71	9.42	9.42	2	0.14	0.01	0.06	0.00	0.00	24.0
17	440	-14840	-622	171	0	-345	5282	15.71	15.71	9.42	9.42	2	0.14	0.01	0.05	0.00	0.00	24.0
18	440	-30260	-943	70	0	-197	13950	15.71	15.71	9.42	9.42	3	0.24	0.01	0.06	0.00	0.00	24.0
19	440	-22680	-2111	-64	0	102	9662	15.71	15.71	9.42	9.42	3	0.17	0.03	0.15	0.00	0.00	24.0
20	440	-25540	-1271	294	0	-633	11360	15.71	15.71	9.42	9.42	3	0.20	0.02	0.09	0.00	0.00	24.0
37	440	-30530	-321	126	0	-312	13730	15.71	15.71	9.42	9.42	3	0.23	0.00	0.02	0.00	0.00	24.0
38	440	-17900	-2267	-98	0	188	6591	15.71	15.71	9.42	9.42	3	0.12	0.03	0.17	0.00	0.00	24.0
39	440	-22670	-868	499	0	-1038	9419	15.71	15.71	9.42	9.42	3	0.17	0.01	0.06	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 25 NI 121 NF 120 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 5B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice resistenza	aswta	aswto	PASSO

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	cm	daN			daN*m		cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-25740	-1465	-53	0	-142	16830	15.71	15.71	9.42	9.42	3	0.29	0.02	0.10	0.00	0.00	24.0
2	0	-19760	-872	-78	0	-206	10560	15.71	15.71	9.42	9.42	2	0.26	0.01	0.06	0.00	0.00	24.0
3	0	-19800	-867	7	0	9	10580	15.71	15.71	9.42	9.42	2	0.25	0.01	0.06	0.00	0.00	24.0
4	0	-19800	-1387	-88	0	-229	15320	15.71	15.71	9.42	9.42	2	0.37	0.02	0.10	0.00	0.00	24.0
5	0	-19830	-1382	-3	0	-14	15330	15.71	15.71	9.42	9.42	2	0.37	0.02	0.10	0.00	0.00	24.0
6	0	-19730	-1058	-180	0	-465	12210	15.71	15.71	9.42	9.42	2	0.30	0.01	0.08	0.00	0.00	24.0
7	0	-19860	-1042	102	0	252	12260	15.71	15.71	9.42	9.42	2	0.30	0.01	0.08	0.00	0.00	24.0
8	0	-19740	-1212	-183	0	-472	13640	15.71	15.71	9.42	9.42	2	0.34	0.02	0.09	0.00	0.00	24.0
9	0	-19870	-1196	99	0	245	13680	15.71	15.71	9.42	9.42	2	0.33	0.02	0.09	0.00	0.00	24.0
10	0	-19760	-872	-78	0	-206	10560	15.71	15.71	9.42	9.42	2	0.26	0.01	0.06	0.00	0.00	24.0
11	0	-19800	-867	7	0	9	10580	15.71	15.71	9.42	9.42	2	0.25	0.01	0.06	0.00	0.00	24.0
12	0	-19800	-1387	-88	0	-229	15320	15.71	15.71	9.42	9.42	2	0.37	0.02	0.10	0.00	0.00	24.0
13	0	-19830	-1382	-3	0	-14	15330	15.71	15.71	9.42	9.42	2	0.37	0.02	0.10	0.00	0.00	24.0
14	0	-19730	-1058	-180	0	-465	12210	15.71	15.71	9.42	9.42	2	0.30	0.01	0.08	0.00	0.00	24.0
15	0	-19860	-1042	102	0	252	12260	15.71	15.71	9.42	9.42	2	0.30	0.01	0.08	0.00	0.00	24.0
16	0	-19740	-1212	-183	0	-472	13640	15.71	15.71	9.42	9.42	2	0.34	0.02	0.09	0.00	0.00	24.0
17	0	-19870	-1196	99	0	245	13680	15.71	15.71	9.42	9.42	2	0.33	0.02	0.09	0.00	0.00	24.0
18	0	-37980	-389	-98	0	-279	24230	15.71	15.71	9.42	9.42	3	0.40	0.00	0.02	0.00	0.00	24.0
19	0	-30730	-5350	-137	0	-354	38370	15.71	15.71	9.42	9.42	3	0.65	0.07	0.36	0.00	0.00	24.0
20	0	-33070	-2663	181	0	389	29180	15.71	15.71	9.42	9.42	3	0.49	0.03	0.17	0.00	0.00	24.0
37	0	-37650	1723	-63	0	-196	14810	15.71	15.71	9.42	9.42	3	0.25	0.02	0.11	0.00	0.00	24.0
38	0	-25560	-6546	-128	0	-321	38390	15.71	15.71	9.42	9.42	3	0.66	0.08	0.46	0.00	0.00	24.0
39	0	-29460	-2067	402	0	918	23070	15.71	15.71	9.42	9.42	3	0.40	0.03	0.14	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	110	-24595	-1465	-53	0	-85	15220	15.71	15.71	9.42	9.42	3	0.26	0.02	0.10	0.00	0.00	24.0
2	110	-18880	-872	-78	0	-120	9602	15.71	15.71	9.42	9.42	2	0.23	0.01	0.07	0.00	0.00	24.0
3	110	-18920	-867	7	0	2	9625	15.71	15.71	9.42	9.42	2	0.23	0.01	0.07	0.00	0.00	24.0
4	110	-18920	-1387	-88	0	-132	13795	15.71	15.71	9.42	9.42	2	0.33	0.02	0.10	0.00	0.00	24.0
5	110	-18950	-1382	-3	0	-10	13811	15.71	15.71	9.42	9.42	2	0.33	0.02	0.10	0.00	0.00	24.0
6	110	-18850	-1058	-180	0	-267	11047	15.71	15.71	9.42	9.42	2	0.27	0.01	0.08	0.00	0.00	24.0
7	110	-18980	-1042	102	0	140	11113	15.71	15.71	9.42	9.42	2	0.27	0.01	0.08	0.00	0.00	24.0
8	110	-18860	-1212	-183	0	-270	12307	15.71	15.71	9.42	9.42	2	0.30	0.02	0.09	0.00	0.00	24.0
9	110	-18990	-1196	99	0	137	12365	15.71	15.71	9.42	9.42	2	0.30	0.02	0.09	0.00	0.00	24.0
10	110	-18880	-872	-78	0	-120	9602	15.71	15.71	9.42	9.42	2	0.23	0.01	0.07	0.00	0.00	24.0
11	110	-18920	-867	7	0	2	9625	15.71	15.71	9.42	9.42	2	0.23	0.01	0.07	0.00	0.00	24.0
12	110	-18920	-1387	-88	0	-132	13795	15.71	15.71	9.42	9.42	2	0.33	0.02	0.10	0.00	0.00	24.0
13	110	-18950	-1382	-3	0	-10	13811	15.71	15.71	9.42	9.42	2	0.33	0.02	0.10	0.00	0.00	24.0
14	110	-18850	-1058	-180	0	-267	11047	15.71	15.71	9.42	9.42	2	0.27	0.01	0.08	0.00	0.00	24.0
15	110	-18980	-1042	102	0	140	11113	15.71	15.71	9.42	9.42	2	0.27	0.01	0.08	0.00	0.00	24.0
16	110	-18860	-1212	-183	0	-270	12307	15.71	15.71	9.42	9.42	2	0.30	0.02	0.09	0.00	0.00	24.0
17	110	-18990	-1196	99	0	137	12365	15.71	15.71	9.42	9.42	2	0.30	0.02	0.09	0.00	0.00	24.0
18	110	-36838	-769	-98	0	-172	23592	15.71	15.71	9.42	9.42	3	0.39	0.01	0.05	0.00	0.00	24.0
19	110	-29588	-4970	-137	0	-203	32695	15.71	15.71	9.42	9.42	3	0.56	0.06	0.34	0.00	0.00	24.0
20	110	-31925	-2663	181	0	190	26252	15.71	15.71	9.42	9.42	3	0.44	0.03	0.18	0.00	0.00	24.0
37	110	-36505	1089	-63	0	-127	16355	15.71	15.71	9.42	9.42	3	0.27	0.01	0.07	0.00	0.00	24.0
38	110	-24415	-5912	-128	0	-180	31537	15.71	15.71	9.42	9.42	3	0.55	0.07	0.42	0.00	0.00	24.0
39	110	-28315	-2067	402	0	476	20795	15.71	15.71	9.42	9.42	3	0.36	0.03	0.14	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	220	-23450	-1465	-53	0	-27	13610	15.71	15.71	9.42	9.42	3	0.24	0.02	0.10	0.00	0.00	24.0
2	220	-18000	-872	-78	0	-35	8643	15.71	15.71	9.42	9.42	2	0.21	0.01	0.07	0.00	0.00	24.0
3	220	-18040	-867	7	0	-6	8670	15.71	15.71	9.42	9.42	2	0.21	0.01	0.07	0.00	0.00	24.0
4	220	-18040	-1387	-88	0	-35	12270	15.71	15.71	9.42	9.42	2	0.30	0.02	0.11	0.00	0.00	24.0
5	220	-18070	-1382	-3	0	-6	12291	15.71	15.71	9.42	9.42	2	0.30	0.02	0.10	0.00	0.00	24.0
6	220	-17970	-1058	-180	0	-69	9885	15.71	15.71	9.42	9.42	2	0.24	0.01	0.08	0.00	0.00	24.0
7	220	-18100	-1042	102	0	28	9966	15.71	15.71	9.42	9.42	2	0.24	0.01	0.08	0.00	0.00	24.0
8	220	-17980	-1212	-183	0	-69	10974	15.71	15.71	9.42	9.42	2	0.27	0.02	0.09	0.00	0.00	24.0
9	220	-18110	-1196	99	0	28	11050	15.71	15.71	9.42	9.42	2	0.27	0.02	0.09	0.00	0.00	24.0
10	220	-18000	-872	-78	0	-35	8643	15.71	15.71	9.42	9.42	2	0.21	0.01	0.07	0.00	0.00	24.0
11	220	-18040	-867	7	0	-6	8670	15.71	15.71	9.42	9.42	2	0.21	0.01	0.07	0.00	0.00	24.0
12	220	-18040	-1387	-88	0	-35	12270	15.71	15.71	9.42	9.42	2	0.30	0.02	0.11	0.00	0.00	24.0
13	220	-18070	-1382	-3	0	-6	12291	15.71	15.71	9.42	9.42	2	0.30	0.02	0.10	0.00	0.00	24.0
14	220	-17970	-1058	-180	0	-69	9885	15.71	15.71	9.42	9.42	2	0.24	0.01	0.08	0.00	0.00	24.0
15	220	-18100	-1042	102	0	28	9966	15.71	15.71	9.42	9.42	2	0.24	0.01	0.08	0.00	0.00	24.0
16	220	-17980	-1212	-183	0	-69	10974	15.71	15.71	9.42	9.42	2	0.27	0.02	0.09	0.00	0.00	24.0
17	220	-18110	-1196	99	0	28	11050	15.71	15.71	9.42	9.42	2	0.27	0.02	0.09	0.00	0.00	24.0
18	220	-35695	-1150	-98	0	-64	22536	15.71	15.71	9.42	9.42	3	0.37	0.01	0.07	0.00	0.00	24.0
19	220	-28445	-4590	-137	0	-53	27439	15.71	15.71	9.42	9.42	3	0.47	0.06	0.31	0.00	0.00	24.0
20	220	-30780	-2663	181	0	-9	23325	15.71	15.71	9.42	9.42	3	0.40	0.03	0.18	0.00	0.00	24.0
37	220	-35360	456	-63	0	-58	17204	15.71	15.71	9.42	9.42	3	0.29	0.01	0.03	0.00	0.00	24.0
38	220	-23270	-5279	-128	0	-38	25381	15.71	15.71	9.42	9.42	3	0.44	0.07	0.38	0.00	0.00	24.0
39	220	-27170	-2067	402	0	34	18520	15.71	15.71	9.42	9.42	3	0.32	0.03	0.14	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	330	-22305	-1465	-53	0	31	12000	15.71	15.71	9.42	9.42	3	0.21	0.02	0.11	0.00	0.00	24.0
2	330	-17120	-872	-78	0	51	7684	15.71	15.71	9.42	9.42	2	0.19	0.01	0.07	0.00	0.00	24.0
3	330	-17160	-867	7	0	-13	7716	15.71	15.71	9.42	9.42	2	0.19	0.01	0.07	0.00	0.00	24.0
4	330	-17160	-1387	-88	0	61	10744	15.71	15.71	9.42	9.42	2	0.26	0.02	0.11	0.00	0.00	24.0
5	330	-17190	-1382	-3	0	-3	10772	15.71	15.71	9.42	9.42	2	0.26	0.02	0.11	0.00	0.00	24.0
6	330	-17090	-1058	-180	0	129	8722	15.71	15.71	9.42	9.42	2	0.22	0.01	0.08	0.00	0.00	24.0
7	330	-17220	-1042	102	0	-84	8820	15.71	15.71	9.42	9.42	2	0.22	0.01	0.08	0.00	0.00	24.0
8	330	-17100	-1212	-183	0	132	9640	15.71	15.71	9.42	9.42	2	0.24	0.02	0.09	0.00	0.00	24.0
9	330	-17230	-1196	99	0	-81	9736	15.71	15.71	9.42	9.42	2	0.24	0.02	0.09	0.00	0.00	24.0
10	330	-17120	-872	-78	0	51	7684	15.71	15.71	9.42	9.42	2	0.19	0.01	0.07	0.00	0.00	24.0
11	330	-17160	-867	7	0	-13	7716	15.71	15.71	9.42	9.42	2	0.19	0.01	0.07	0.00	0.00	24.0
12	330	-17160	-1387	-88	0	61	10744	15.71	15.71	9.42	9.42	2	0.26	0.02	0.11	0.00	0.00	24.0
13	330	-17190	-1382	-3	0	-3	10772	15.71	15.71	9.42	9.42	2	0.26	0.02	0.11	0.00	0.00	24.0
14	330	-17090	-1058	-180	0	129	8722	15.71	15.71	9.42	9.42	2	0.22	0.01	0.08	0.00	0.00	24.0
15	330	-17220	-1042	102	0	-84	8820	15.71	15.71	9.42	9.42	2	0.22	0.01	0.08	0.00	0.00	24.0
16	330	-17100	-1212	-183	0	132	9640	15.71	15.71	9.42	9.42	2	0.24	0.02	0.09	0.00	0.00	24.0
17	330	-17230	-1196	99	0	-81	9736	15.71	15.71	9.42	9.42	2	0.24	0.02	0.09	0.00	0.00	24.0
18	330	-34552	-1530	-98	0	43	21062	15.71	15.71	9.42	9.42	3	0.35	0.02	0.10	0.00	0.00	24.0
19	330	-27302	-4210	-137	0	98	22600	15.71	15.71	9.42	9.42	3	0.39	0.05	0.29	0.00	0.00	24.0
20	330	-29635	-2663	181	0	-209	20397	15.71	15.71	9.42	9.42	3	0.35	0.03	0.18	0.00	0.00	24.0
37	330	-34215	-178	-63	0	12	17355	15.71	15.71	9.42	9.42	3	0.29	0.00	0.01	0.00	0.00	24.0
38	330	-22125	-4646	-128	0	103	19922	15.71	15.71	9.42	9.42	3	0.35	0.06	0.34	0.00	0.00	24.0
39	330	-26025	-2067	402	0	-408	16245	15.71	15.71	9.42	9.42	3	0.28	0.03	0.14	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	440	-21160	-1465	-53	0	89	10390	15.71	15.71	9.42	9.42	3	0.18	0.02	0.11	0.00	0.00	24.0
2	440	-16240	-872	-78	0	136	6726	15.71	15.71	9.42	9.42	2	0.17	0.01	0.07	0.00	0.00	24.0

3	440	-16280	-867	7	0	-21	6761	15.71	15.71	9.42	9.42	2	0.17	0.01	0.07	0.00	0.00	24.0
4	440	-16280	-1387	-88	0	158	9219	15.71	15.71	9.42	9.42	2	0.23	0.02	0.11	0.00	0.00	24.0
5	440	-16310	-1382	-3	0	1	9253	15.71	15.71	9.42	9.42	2	0.23	0.02	0.11	0.00	0.00	24.0
6	440	-16210	-1058	-180	0	327	7559	15.71	15.71	9.42	9.42	2	0.19	0.01	0.08	0.00	0.00	24.0
7	440	-16340	-1042	102	0	-197	7673	15.71	15.71	9.42	9.42	2	0.19	0.01	0.08	0.00	0.00	24.0
8	440	-16220	-1212	-183	0	333	8307	15.71	15.71	9.42	9.42	2	0.21	0.02	0.09	0.00	0.00	24.0
9	440	-16350	-1196	99	0	-190	8421	15.71	15.71	9.42	9.42	2	0.21	0.02	0.09	0.00	0.00	24.0
10	440	-16240	-872	-78	0	136	6726	15.71	15.71	9.42	9.42	2	0.17	0.01	0.07	0.00	0.00	24.0
11	440	-16280	-867	7	0	-21	6761	15.71	15.71	9.42	9.42	2	0.17	0.01	0.07	0.00	0.00	24.0
12	440	-16280	-1387	-88	0	158	9219	15.71	15.71	9.42	9.42	2	0.23	0.02	0.11	0.00	0.00	24.0
13	440	-16310	-1382	-3	0	1	9253	15.71	15.71	9.42	9.42	2	0.23	0.02	0.11	0.00	0.00	24.0
14	440	-16210	-1058	-180	0	327	7559	15.71	15.71	9.42	9.42	2	0.19	0.01	0.08	0.00	0.00	24.0
15	440	-16340	-1042	102	0	-197	7673	15.71	15.71	9.42	9.42	2	0.19	0.01	0.08	0.00	0.00	24.0
16	440	-16220	-1212	-183	0	333	8307	15.71	15.71	9.42	9.42	2	0.21	0.02	0.09	0.00	0.00	24.0
17	440	-16350	-1196	99	0	-190	8421	15.71	15.71	9.42	9.42	2	0.21	0.02	0.09	0.00	0.00	24.0
18	440	-33410	-1910	-98	0	151	19170	15.71	15.71	9.42	9.42	3	0.32	0.02	0.12	0.00	0.00	24.0
19	440	-26160	-3830	-137	0	248	18180	15.71	15.71	9.42	9.42	3	0.31	0.05	0.27	0.00	0.00	24.0
20	440	-28490	-2663	181	0	-408	17470	15.71	15.71	9.42	9.42	3	0.30	0.03	0.18	0.00	0.00	24.0
37	440	-33070	-812	-63	0	81	16810	15.71	15.71	9.42	9.42	3	0.28	0.01	0.05	0.00	0.00	24.0
38	440	-20980	-4012	-128	0	244	15160	15.71	15.71	9.42	9.42	3	0.27	0.05	0.29	0.00	0.00	24.0
39	440	-24880	-2067	402	0	-850	13970	15.71	15.71	9.42	9.42	3	0.25	0.03	0.15	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 26 NI 164 NF 163 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 4B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-25890	-1674	-65	0	-178	18350	15.71	15.71	9.42	9.42	3	0.32	0.02	0.12	0.00	0.00	24.0
2	0	-19950	-980	-89	0	-236	11460	15.71	15.71	9.42	9.42	2	0.28	0.01	0.07	0.00	0.00	24.0
3	0	-19920	-974	-6	0	-24	11370	15.71	15.71	9.42	9.42	2	0.27	0.01	0.07	0.00	0.00	24.0
4	0	-19910	-1602	-94	0	-250	16860	15.71	15.71	9.42	9.42	2	0.41	0.02	0.12	0.00	0.00	24.0
5	0	-19880	-1596	-12	0	-38	16770	15.71	15.71	9.42	9.42	2	0.40	0.02	0.12	0.00	0.00	24.0
6	0	-19980	-1205	-187	0	-488	13460	15.71	15.71	9.42	9.42	2	0.33	0.02	0.09	0.00	0.00	24.0
7	0	-19870	-1184	88	0	218	13150	15.71	15.71	9.42	9.42	2	0.32	0.01	0.09	0.00	0.00	24.0
8	0	-19960	-1392	-189	0	-493	15080	15.71	15.71	9.42	9.42	2	0.37	0.02	0.10	0.00	0.00	24.0
9	0	-19860	-1371	86	0	214	14770	15.71	15.71	9.42	9.42	2	0.36	0.02	0.10	0.00	0.00	24.0
10	0	-19950	-980	-89	0	-236	11460	15.71	15.71	9.42	9.42	2	0.28	0.01	0.07	0.00	0.00	24.0
11	0	-19920	-974	-6	0	-24	11370	15.71	15.71	9.42	9.42	2	0.27	0.01	0.07	0.00	0.00	24.0
12	0	-19910	-1602	-94	0	-250	16860	15.71	15.71	9.42	9.42	2	0.41	0.02	0.12	0.00	0.00	24.0
13	0	-19880	-1596	-12	0	-38	16770	15.71	15.71	9.42	9.42	2	0.40	0.02	0.12	0.00	0.00	24.0
14	0	-19980	-1205	-187	0	-488	13460	15.71	15.71	9.42	9.42	2	0.33	0.02	0.09	0.00	0.00	24.0
15	0	-19870	-1184	88	0	218	13150	15.71	15.71	9.42	9.42	2	0.32	0.01	0.09	0.00	0.00	24.0
16	0	-19960	-1392	-189	0	-493	15080	15.71	15.71	9.42	9.42	2	0.37	0.02	0.10	0.00	0.00	24.0
17	0	-19860	-1371	86	0	214	14770	15.71	15.71	9.42	9.42	2	0.36	0.02	0.10	0.00	0.00	24.0
18	0	-38400	-663	-110	0	-327	26390	15.71	15.71	9.42	9.42	3	0.44	0.01	0.04	0.00	0.00	24.0
19	0	-30870	-5896	-134	0	-363	42120	15.71	15.71	9.42	9.42	3	0.71	0.07	0.39	0.00	0.00	24.0
20	0	-33200	-3022	145	0	295	31640	15.71	15.71	9.42	9.42	3	0.53	0.04	0.20	0.00	0.00	24.0
37	0	-38110	1604	-83	0	-260	15980	15.71	15.71	9.42	9.42	3	0.26	0.02	0.10	0.00	0.00	24.0
38	0	-25570	-7117	-123	0	-319	42190	15.71	15.71	9.42	9.42	3	0.73	0.09	0.50	0.00	0.00	24.0
39	0	-29450	-2327	341	0	778	24720	15.71	15.71	9.42	9.42	3	0.42	0.03	0.16	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	110	-24748	-1674	-65	0	-106	16508	15.71	15.71	9.42	9.42	3	0.29	0.02	0.12	0.00	0.00	24.0
2	110	-19070	-980	-89	0	-139	10382	15.71	15.71	9.42	9.42	2	0.25	0.01	0.07	0.00	0.00	24.0
3	110	-19040	-974	-6	0	-17	10298	15.71	15.71	9.42	9.42	2	0.25	0.01	0.07	0.00	0.00	24.0
4	110	-19030	-1602	-94	0	-146	15099	15.71	15.71	9.42	9.42	2	0.37	0.02	0.12	0.00	0.00	24.0
5	110	-19000	-1596	-12	0	-25	15015	15.71	15.71	9.42	9.42	2	0.36	0.02	0.12	0.00	0.00	24.0
6	110	-19100	-1205	-187	0	-283	12135	15.71	15.71	9.42	9.42	2	0.30	0.02	0.09	0.00	0.00	24.0
7	110	-18990	-1184	88	0	122	11847	15.71	15.71	9.42	9.42	2	0.29	0.01	0.09	0.00	0.00	24.0
8	110	-19080	-1392	-189	0	-285	13550	15.71	15.71	9.42	9.42	2	0.33	0.02	0.10	0.00	0.00	24.0
9	110	-18980	-1371	86	0	119	13263	15.71	15.71	9.42	9.42	2	0.32	0.02	0.10	0.00	0.00	24.0
10	110	-19070	-980	-89	0	-139	10382	15.71	15.71	9.42	9.42	2	0.25	0.01	0.07	0.00	0.00	24.0
11	110	-19040	-974	-6	0	-17	10298	15.71	15.71	9.42	9.42	2	0.25	0.01	0.07	0.00	0.00	24.0
12	110	-19030	-1602	-94	0	-146	15099	15.71	15.71	9.42	9.42	2	0.37	0.02	0.12	0.00	0.00	24.0
13	110	-19000	-1596	-12	0	-25	15015	15.71	15.71	9.42	9.42	2	0.36	0.02	0.12	0.00	0.00	24.0
14	110	-19100	-1205	-187	0	-283	12135	15.71	15.71	9.42	9.42	2	0.30	0.02	0.09	0.00	0.00	24.0
15	110	-18990	-1184	88	0	122	11847	15.71	15.71	9.42	9.42	2	0.29	0.01	0.09	0.00	0.00	24.0
16	110	-19080	-1392	-189	0	-285	13550	15.71	15.71	9.42	9.42	2	0.33	0.02	0.10	0.00	0.00	24.0
17	110	-18980	-1371	86	0	119	13263	15.71	15.71	9.42	9.42	2	0.32	0.02	0.10	0.00	0.00	24.0
18	110	-37255	-1043	-110	0	-206	25452	15.71	15.71	9.42	9.42	3	0.42	0.01	0.07	0.00	0.00	24.0
19	110	-29728	-5516	-134	0	-216	35845	15.71	15.71	9.42	9.42	3	0.61	0.07	0.37	0.00	0.00	24.0
20	110	-32058	-3022	145	0	136	28315	15.71	15.71	9.42	9.42	3	0.48	0.04	0.20	0.00	0.00	24.0
37	110	-36968	970	-83	0	-168	17395	15.71	15.71	9.42	9.42	3	0.29	0.01	0.06	0.00	0.00	24.0
38	110	-24425	-6484	-123	0	-184	34710	15.71	15.71	9.42	9.42	3	0.60	0.08	0.46	0.00	0.00	24.0
39	110	-28308	-2327	341	0	403	22160	15.71	15.71	9.42	9.42	3	0.38	0.03	0.16	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	220	-23605	-1674	-65	0	-34	14665	15.71	15.71	9.42	9.42	3	0.26	0.02	0.12	0.00	0.00	24.0
2	220	-18190	-980	-89	0	-41	9304	15.71	15.71	9.42	9.42	2	0.23	0.01	0.07	0.00	0.00	24.0
3	220	-18160	-974	-6	0	-10	9226	15.71	15.71	9.42	9.42	2	0.22	0.01	0.07	0.00	0.00	24.0
4	220	-18150	-1602	-94	0	-42	13338	15.71	15.71	9.42	9.42	2	0.32	0.02	0.12	0.00	0.00	24.0
5	220	-18120	-1596	-12	0	-12	13260	15.71	15.71	9.42	9.42	2	0.32	0.02	0.12	0.00	0.00	24.0
6	220	-18220	-1205	-187	0	-77	10809	15.71	15.71	9.42	9.42	2	0.26	0.02	0.09	0.00	0.00	24.0
7	220	-18110	-1184	88	0	25	10545	15.71	15.71	9.42	9.42	2	0.26	0.01	0.09	0.00	0.00	24.0
8	220	-18200	-1392	-189	0	-78	12020	15.71	15.71	9.42	9.42	2	0.29	0.02	0.11	0.00	0.00	24.0
9	220	-18100	-1371	86	0	25	11755	15.71	15.71	9.42	9.42	2	0.28	0.02	0.10	0.00	0.00	24.0
10	220	-18190	-980	-89	0	-41	9304	15.71	15.71	9.42	9.42	2	0.23	0.01	0.07	0.00	0.00	24.0
11	220	-18160	-974	-6	0	-10	9226	15.71	15.71	9.42	9.42	2	0.22	0.01	0.07	0.00	0.00	24.0
12	220	-18150	-1602	-94	0	-42	13338	15.71	15.71	9.42	9.42	2	0.32	0.02	0.12	0.00	0.00	24.0
13	220	-18120	-1596	-12	0	-12	13260	15.71	15.71	9.42	9.42	2	0.32	0.02	0.12	0.00	0.00	24.0
14	220	-18220	-1205	-187	0	-77	10809	15.71	15.71	9.42	9.42	2	0.26	0.02	0.09	0.00	0.00	24.0
15	220	-18110	-1184	88	0	25	10545	15.71	15.71	9.42	9.42	2	0.26	0.01	0.09	0.00	0.00	24.0
16	220	-18200	-1392	-189	0	-78	12020	15.71	15.71	9.42	9.42	2	0.29	0.02	0.11	0.00	0.00	24.0
17	220	-18100	-1371	86	0	25	11755	15.71	15.71	9.42	9.42	2	0.28	0.02	0.10	0.00	0.00	24.0
18	220	-36110	-1424	-110	0	-85	24096	15.71	15.71	9.42	9.42	3	0.40	0.02	0.09	0.00	0.00	24.0
19	220	-28585	-5136	-134	0	-69	29989	15.71	15.71	9.42	9.42	3	0.51	0.06	0.35	0.00	0.00	24.0
20	220	-30915	-3022	145	0	-23	24990	15.71	15.71	9.42	9.42	3	0.42	0.04	0.20	0.00	0.00	24.0
37	220	-35825	337	-83	0	-76	18114	15.71	15.71	9.42	9.42	3	0.30	0.00	0.02	0.00	0.00	24.0
38	220	-23280	-5850	-123	0	-49	27926	15.71	15.71	9.42	9.42	3	0.49	0.07	0.42	0.00	0.00	24.0
39	220	-27165	-2327	341	0	27	19600	15.71	15.71	9.42	9.42	3	0.34	0.03	0.16	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	330	-22462	-1674	-65	0	38	12822	15.71	15.71	9.42	9.42	3	0.22	0.02	0.12	0.00	0.00	24.0
2	330	-17310	-980	-89	0	57	8227	15.71	15.71	9.42	9.42	2	0.20	0.01	0.07	0.00	0.00	24.0
3	330	-17280	-974	-6	0	-3	8155	15.71	15.71	9.42	9.42	2	0.20	0.01	0.07	0.00	0.00	24.0
4	330	-17270	-1602	-94	0	62	11577	15.71	15.71	9.42	9.42	2	0.28	0.02	0.12	0.00	0.00	24.0
5	330	-17240	-1596	-12	0	2	11505	15.71	15.71	9.42	9.42	2	0.28	0.02	0.12	0.00	0.00	24.0
6	330	-17340	-1205	-187	0	128	9484	15.71	15.71	9.42	9.42	2	0.23	0.02	0.09	0.00	0.00	24.0
7	330	-17230	-1184	88	0	-72	9242	15.71	15.71	9.42	9.42	2	0.23	0.01	0.09	0.00	0.00	24.0
8	330	-17320	-1392	-189	0	130	10490	15.71	15.71	9.42	9.42	2	0.26	0.02	0.11	0.00	0.00	24.0
9	330	-17220	-1371	86	0	-70	10247	15.71	15.71	9.42	9.42	2	0.25	0.02	0.10	0.00	0.00	24.0
10	330	-17310	-980	-89	0	57	8227	15.71	15.71	9.42	9.42	2	0.20	0.01	0.07	0.00	0.00	24.0
11	330	-17280	-974	-6	0	-3	8155	15.71	15.71	9.42	9.42	2	0.20	0.01	0.07	0.00	0.00	24.0
12	330	-17270	-1602	-94	0	62	11577	15.71	15.71	9.42	9.42	2	0.28	0.02	0.12	0.00	0.00	24.0
13	330	-17240	-1596	-12	0	2	11505	15.71	15.71	9.42	9.42	2	0.28	0.02	0.12	0.00	0.00	24.0
14	330	-17340	-1205	-187	0	128	9484	15.71	15.71	9.42	9.42	2	0.23	0.02	0.09	0.00	0.00	24.0
15	330	-17230	-1184	88	0	-72	9242	15.71	15.71	9.42	9.42	2	0.23	0.01	0.09	0.00	0.00	24.0
16	330	-17320	-1392	-189	0	130	10490	15.71	15.71	9.42	9.42	2	0.26	0.02	0.11	0.00	0.00	24.0
17	330	-17220	-1371	86	0	-70	10247	15.71	15.71	9.42	9.42	2	0.25	0.02	0.10	0.00	0.00	24.0
18	330	-34965	-1804	-110	0	36	22322	15.71	15.71	9.42	9.42	3	0.37	0.02	0.12	0.00	0.00	24.0
19	330	-27442	-4756	-134	0	78	24550	15.71	15.71	9.42	9.42	3	0.42	0.06	0.33	0.00	0.00	24.0
20	330	-29772	-3022	145	0	-182	21665	15.71	15.71	9.42	9.42	3	0.37	0.04	0.20	0.00	0.00	24.0
37	330	-34682	-297	-83	0	16	18135	15.71	15.71	9.42	9.42	3	0.30	0.00	0.02	0.00	0.00	24.0
38	330	-22135	-5216	-123	0	86	21840	15.71	15.71	9.42	9.42	3	0.38	0.07	0.38	0.00	0.00	24.0
39	330	-26022	-2327	341	0	-348	17040	15.71	15.71	9.42	9.42	3	0.30	0.03	0.16	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	440	-21320	-1674	-65	0	110	10980	15.71	15.71	9.42	9.42	3	0.19	0.02	0.12	0.00	0.00	24.0
2	440	-16430	-980	-89	0	154	7149	15.71	15.71	9.42	9.42	2	0.18	0.01	0.08	0.00	0.00	24.0
3	440	-16400	-974	-6	0	4	7083	15.71	15.71	9.42	9.42	2	0.17	0.01	0.08	0.00	0.00	24.0
4	440	-16390	-1602	-94	0	165	9816	15.71	15.71	9.42	9.42	2	0.24	0.02	0.12	0.00	0.00	24.0
5	440	-16360	-1596	-12	0	15	9750	15.71	15.71	9.42	9.42	2	0.24	0.02	0.12	0.00	0.00	24.0
6	440	-16460	-1205	-187	0	334	8159	15.71	15.71	9.42	9.42	2	0.21	0.02	0.09	0.00	0.00	24.0
7	440	-16350	-1184	88	0	-168	7939	15.71	15.71	9.42	9.42	2	0.20	0.01	0.09	0.00	0.00	24.0
8	440	-16440	-1392	-189	0	337	8960	15.71	15.71	9.42	9.42	2	0.23	0.02	0.11	0.00	0.00	24.0
9	440	-16340	-1371	86	0	-165	8740	15.71	15.71	9.42	9.42	2	0.22	0.02	0.11	0.00	0.00	24.0
10	440	-16430	-980	-89	0	154	7149	15.71	15.71	9.42	9.42	2	0.18	0.01	0.08	0.00	0.00	24.0
11	440	-16400	-974	-6	0	4	7083	15.71	15.71	9.42	9.42	2	0.17	0.01	0.08	0.00	0.00	24.0
12	440	-16390	-1602	-94	0	165	9816	15.71	15.71	9.42	9.42	2	0.24	0.02	0.12	0.00	0.00	24.0
13	440	-16360	-1596	-12	0	15	9750	15.71	15.71	9.42	9.42	2	0.24	0.02	0.12	0.00	0.00	24.0
14	440	-16460	-1205	-187	0	334	8159	15.71	15.71	9.42	9.42	2	0.21	0.02	0.09	0.00	0.00	24.0
15	440	-16350	-1184	88	0	-168	7939	15.71	15.71	9.42	9.42	2	0.20	0.01	0.09	0.00	0.00	24.0
16	440	-16440	-1392	-189	0	337	8960	15.71	15.71	9.42	9.42	2	0.23	0.02	0.11	0.00	0.00	24.0
17	440	-16340	-1371	86	0	-165	8740	15.71	15.71	9.42	9.42	2	0.22	0.02	0.11	0.00	0.00	24.0
18	440	-33820	-2184	-110	0	157	20130	15.71	15.71	9.42	9.42	3	0.34	0.03	0.14	0.00	0.00	24.0
19	440	-26300	-4376	-134	0	225	19530	15.71	15.71	9.42	9.42	3	0.34	0.05	0.30	0.00	0.00	24.0
20	440	-28630	-3022	145	0	-341	18340	15.71	15.71	9.42	9.42	3	0.31	0.04	0.21	0.00	0.00	24.0
37	440	-33540	-930	-83	0	107	17460	15.71	15.71	9.42	9.42	3	0.29	0.01	0.06	0.00	0.00	24.0
38	440	-20990	-4583	-123	0	221	16450	15.71	15.71	9.42	9.42	3	0.29	0.06	0.34	0.00	0.00	24.0
39	440	-24880	-2327	341	0	-724	14480	15.71	15.71	9.42	9.42	3	0.25	0.03	0.16	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 27 NI 207 NF 206 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 3B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-25550	-1476	-79	0	-200	16740	15.71	15.71	9.42	9.42	3	0.29	0.02	0.10	0.00	0.00	24.0
2	0	-19650	-844	-99	0	-256	10230	15.71	15.71	9.42	9.42	2	0.25	0.01	0.06	0.00	0.00	24.0
3	0	-19650	-845	-20	0	-48	10240	15.71	15.71	9.42	9.42	2	0.25	0.01	0.06	0.00	0.00	24.0
4	0	-19650	-1426	-101	0	-260	15500	15.71	15.71	9.42	9.42	2	0.38	0.02	0.11	0.00	0.00	24.0
5	0	-19660	-1427	-22	0	-52	15520	15.71	15.71	9.42	9.42	2	0.37	0.02	0.11	0.00	0.00	24.0
6	0	-19640	-1046	-192	0	-500	12060	15.71	15.71	9.42	9.42	2	0.30	0.01	0.08	0.00	0.00	24.0
7	0	-19660	-1050	72	0	194	12100	15.71	15.71	9.42	9.42	2	0.29	0.01	0.08	0.00	0.00	24.0
8	0	-19640	-1221	-193	0	-501	13640	15.71	15.71	9.42	9.42	2	0.34	0.02	0.09	0.00	0.00	24.0
9	0	-19660	-1225	71	0	193	13690	15.71	15.71	9.42	9.42	2	0.33	0.02	0.09	0.00	0.00	24.0
10	0	-19650	-844	-99	0	-256	10230	15.71	15.71	9.42	9.42	2	0.25	0.01	0.06	0.00	0.00	24.0
11	0	-19650	-845	-20	0	-48	10240	15.71	15.71	9.42	9.42	2	0.25	0.01	0.06	0.00	0.00	24.0
12	0	-19650	-1426	-101	0	-260	15500	15.71	15.71	9.42	9.42	2	0.38	0.02	0.11	0.00	0.00	24.0
13	0	-19660	-1427	-22	0	-52	15520	15.71	15.71	9.42	9.42	2	0.37	0.02	0.11	0.00	0.00	24.0
14	0	-19640	-1046	-192	0	-500	12060	15.71	15.71	9.42	9.42	2	0.30	0.01	0.08	0.00	0.00	24.0
15	0	-19660	-1050	72	0	194	12100	15.71	15.71	9.42	9.42	2	0.29	0.01	0.08	0.00	0.00	24.0
16	0	-19640	-1221	-193	0	-501	13640	15.71	15.71	9.42	9.42	2	0.34	0.02	0.09	0.00	0.00	24.0
17	0	-19660	-1225	71	0	193	13690	15.71	15.71	9.42	9.42	2	0.33	0.02	0.09	0.00	0.00	24.0
18	0	-37720	-339	-134	0	-369	23490	15.71	15.71	9.42	9.42	3	0.39	0.00	0.02	0.00	0.00	24.0
19	0	-30370	-5474	-138	0	-362	38990	15.71	15.71	9.42	9.42	3	0.66	0.07	0.37	0.00	0.00	24.0
20	0	-32740	-2697	109	0	234	29080	15.71	15.71	9.42	9.42	3	0.49	0.03	0.18	0.00	0.00	24.0
37	0	-37450	1839	-114	0	-317	13600	15.71	15.71	9.42	9.42	3	0.23	0.02	0.12	0.00	0.00	24.0
38	0	-25210	-6719	-120	0	-304	39440	15.71	15.71	9.42	9.42	3	0.68	0.08	0.47	0.00	0.00	24.0
39	0	-29150	-2090	291	0	688	22920	15.71	15.71	9.42	9.42	3	0.39	0.03	0.14	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	110	-24405	-1476	-79	0	-114	15115	15.71	15.71	9.42	9.42	3	0.26	0.02	0.10	0.00	0.00	24.0
2	110	-18770	-844	-99	0	-147	9302	15.71	15.71	9.42	9.42	2	0.23	0.01	0.06	0.00	0.00	24.0
3	110	-18770	-845	-20	0	-26	9311	15.71	15.71	9.42	9.42	2	0.22	0.01	0.06	0.00	0.00	24.0
4	110	-18770	-1426	-101	0	-149	13933	15.71	15.71	9.42	9.42	2	0.34	0.02	0.11	0.00	0.00	24.0
5	110	-18780	-1427	-22	0	-28	13950	15.71	15.71	9.42	9.42	2	0.34	0.02	0.11	0.00	0.00	24.0
6	110	-18760	-1046	-192	0	-289	10910	15.71	15.71	9.42	9.42	2	0.27	0.01	0.08	0.00	0.00	24.0
7	110	-18780	-1050	72	0	115	10946	15.71	15.71	9.42	9.42	2	0.27	0.01	0.08	0.00	0.00	24.0
8	110	-18760	-1221	-193	0	-290	12298	15.71	15.71	9.42	9.42	2	0.30	0.02	0.09	0.00	0.00	24.0
9	110	-18780	-1225	71	0	114	12342	15.71	15.71	9.42	9.42	2	0.30	0.02	0.09	0.00	0.00	24.0
10	110	-18770	-844	-99	0	-147	9302	15.71	15.71	9.42	9.42	2	0.23	0.01	0.06	0.00	0.00	24.0
11	110	-18770	-845	-20	0	-26	9311	15.71	15.71	9.42	9.42	2	0.22	0.01	0.06	0.00	0.00	24.0
12	110	-18770	-1426	-101	0	-149	13933	15.71	15.71	9.42	9.42	2	0.34	0.02	0.11	0.00	0.00	24.0
13	110	-18780	-1427	-22	0	-28	13950	15.71	15.71	9.42	9.42	2	0.34	0.02	0.11	0.00	0.00	24.0
14	110	-18760	-1046	-192	0	-289	10910	15.71	15.71	9.42	9.42	2	0.27	0.01	0.08	0.00	0.00	24.0
15	110	-18780	-1050	72	0	115	10946	15.71	15.71	9.42	9.42	2	0.27	0.01	0.08	0.00	0.00	24.0
16	110	-18760	-1221	-193	0	-290	12298	15.71	15.71	9.42	9.42	2	0.30	0.02	0.09	0.00	0.00	24.0
17	110	-18780	-1225	71	0	114	12342	15.71	15.71	9.42	9.42	2	0.30	0.02	0.09	0.00	0.00	24.0
18	110	-36575	-719	-134	0	-222	22907	15.71	15.71	9.42	9.42	3	0.38	0.01	0.05	0.00	0.00	24.0
19	110	-29228	-5094	-138	0	-210	33178	15.71	15.71	9.42	9.42	3	0.57	0.06	0.34	0.00	0.00	24.0
20	110	-31595	-2697	109	0	114	26113	15.71	15.71	9.42	9.42	3	0.44	0.03	0.18	0.00	0.00	24.0

37	110	-36305	1205	-114	0	-192	15275	15.71	15.71	9.42	9.42	3	0.25	0.01	0.08	0.00	0.00	24.0
38	110	-24065	-6086	-120	0	-172	32397	15.71	15.71	9.42	9.42	3	0.56	0.08	0.43	0.00	0.00	24.0
39	110	-28005	-2090	291	0	368	20623	15.71	15.71	9.42	9.42	3	0.35	0.03	0.14	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	220	-23260	-1476	-79	0	-27	13490	15.71	15.71	9.42	9.42	3	0.24	0.02	0.11	0.00	0.00	24.0
2	220	-17890	-844	-99	0	-38	8373	15.71	15.71	9.42	9.42	2	0.20	0.01	0.06	0.00	0.00	24.0
3	220	-17890	-845	-20	0	-4	8382	15.71	15.71	9.42	9.42	2	0.20	0.01	0.06	0.00	0.00	24.0
4	220	-17890	-1426	-101	0	-38	12366	15.71	15.71	9.42	9.42	2	0.30	0.02	0.11	0.00	0.00	24.0
5	220	-17900	-1427	-22	0	-4	12379	15.71	15.71	9.42	9.42	2	0.30	0.02	0.11	0.00	0.00	24.0
6	220	-17880	-1046	-192	0	-78	9759	15.71	15.71	9.42	9.42	2	0.24	0.01	0.08	0.00	0.00	24.0
7	220	-17900	-1050	72	0	36	9791	15.71	15.71	9.42	9.42	2	0.24	0.01	0.08	0.00	0.00	24.0
8	220	-17880	-1221	-193	0	-78	10956	15.71	15.71	9.42	9.42	2	0.27	0.02	0.09	0.00	0.00	24.0
9	220	-17900	-1225	71	0	36	10993	15.71	15.71	9.42	9.42	2	0.27	0.02	0.09	0.00	0.00	24.0
10	220	-17890	-844	-99	0	-38	8373	15.71	15.71	9.42	9.42	2	0.20	0.01	0.06	0.00	0.00	24.0
11	220	-17890	-845	-20	0	-4	8382	15.71	15.71	9.42	9.42	2	0.20	0.01	0.06	0.00	0.00	24.0
12	220	-17890	-1426	-101	0	-38	12366	15.71	15.71	9.42	9.42	2	0.30	0.02	0.11	0.00	0.00	24.0
13	220	-17900	-1427	-22	0	-4	12379	15.71	15.71	9.42	9.42	2	0.30	0.02	0.11	0.00	0.00	24.0
14	220	-17880	-1046	-192	0	-78	9759	15.71	15.71	9.42	9.42	2	0.24	0.01	0.08	0.00	0.00	24.0
15	220	-17900	-1050	72	0	36	9791	15.71	15.71	9.42	9.42	2	0.24	0.01	0.08	0.00	0.00	24.0
16	220	-17880	-1221	-193	0	-78	10956	15.71	15.71	9.42	9.42	2	0.27	0.02	0.09	0.00	0.00	24.0
17	220	-17900	-1225	71	0	36	10993	15.71	15.71	9.42	9.42	2	0.27	0.02	0.09	0.00	0.00	24.0
18	220	-35430	-1100	-134	0	-74	21906	15.71	15.71	9.42	9.42	3	0.36	0.01	0.07	0.00	0.00	24.0
19	220	-28085	-4714	-138	0	-58	27784	15.71	15.71	9.42	9.42	3	0.48	0.06	0.32	0.00	0.00	24.0
20	220	-30450	-2697	109	0	-5	23145	15.71	15.71	9.42	9.42	3	0.39	0.03	0.18	0.00	0.00	24.0
37	220	-35160	572	-114	0	-66	16254	15.71	15.71	9.42	9.42	3	0.27	0.01	0.04	0.00	0.00	24.0
38	220	-22920	-5452	-120	0	-40	26051	15.71	15.71	9.42	9.42	3	0.46	0.07	0.39	0.00	0.00	24.0
39	220	-26860	-2090	291	0	48	18325	15.71	15.71	9.42	9.42	3	0.32	0.03	0.14	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	330	-22115	-1476	-79	0	59	11865	15.71	15.71	9.42	9.42	3	0.21	0.02	0.11	0.00	0.00	24.0
2	330	-17010	-844	-99	0	71	7445	15.71	15.71	9.42	9.42	2	0.18	0.01	0.06	0.00	0.00	24.0
3	330	-17010	-845	-20	0	18	7453	15.71	15.71	9.42	9.42	2	0.18	0.01	0.06	0.00	0.00	24.0
4	330	-17010	-1426	-101	0	73	10798	15.71	15.71	9.42	9.42	2	0.26	0.02	0.11	0.00	0.00	24.0
5	330	-17020	-1427	-22	0	20	10809	15.71	15.71	9.42	9.42	2	0.26	0.02	0.11	0.00	0.00	24.0
6	330	-17000	-1046	-192	0	134	8609	15.71	15.71	9.42	9.42	2	0.21	0.01	0.08	0.00	0.00	24.0
7	330	-17020	-1050	72	0	-43	8637	15.71	15.71	9.42	9.42	2	0.21	0.01	0.08	0.00	0.00	24.0
8	330	-17000	-1221	-193	0	134	9615	15.71	15.71	9.42	9.42	2	0.24	0.02	0.09	0.00	0.00	24.0
9	330	-17020	-1225	71	0	-43	9644	15.71	15.71	9.42	9.42	2	0.24	0.02	0.09	0.00	0.00	24.0
10	330	-17010	-844	-99	0	71	7445	15.71	15.71	9.42	9.42	2	0.18	0.01	0.06	0.00	0.00	24.0
11	330	-17010	-845	-20	0	18	7453	15.71	15.71	9.42	9.42	2	0.18	0.01	0.06	0.00	0.00	24.0
12	330	-17010	-1426	-101	0	73	10798	15.71	15.71	9.42	9.42	2	0.26	0.02	0.11	0.00	0.00	24.0
13	330	-17020	-1427	-22	0	20	10809	15.71	15.71	9.42	9.42	2	0.26	0.02	0.11	0.00	0.00	24.0
14	330	-17000	-1046	-192	0	134	8609	15.71	15.71	9.42	9.42	2	0.21	0.01	0.08	0.00	0.00	24.0
15	330	-17020	-1050	72	0	-43	8637	15.71	15.71	9.42	9.42	2	0.21	0.01	0.08	0.00	0.00	24.0
16	330	-17000	-1221	-193	0	134	9615	15.71	15.71	9.42	9.42	2	0.24	0.02	0.09	0.00	0.00	24.0
17	330	-17020	-1225	71	0	-43	9644	15.71	15.71	9.42	9.42	2	0.24	0.02	0.09	0.00	0.00	24.0
18	330	-34285	-1480	-134	0	74	20487	15.71	15.71	9.42	9.42	3	0.34	0.02	0.10	0.00	0.00	24.0
19	330	-26942	-4333	-138	0	94	22808	15.71	15.71	9.42	9.42	3	0.39	0.05	0.30	0.00	0.00	24.0
20	330	-29305	-2697	109	0	-125	20177	15.71	15.71	9.42	9.42	3	0.34	0.03	0.18	0.00	0.00	24.0
37	330	-34015	-62	-114	0	59	16535	15.71	15.71	9.42	9.42	3	0.28	0.00	0.01	0.00	0.00	24.0
38	330	-21775	-4818	-120	0	93	20402	15.71	15.71	9.42	9.42	3	0.36	0.06	0.35	0.00	0.00	24.0
39	330	-25715	-2090	291	0	-273	16028	15.71	15.71	9.42	9.42	3	0.28	0.03	0.15	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	440	-20970	-1476	-79	0	146	10240	15.71	15.71	9.42	9.42	3	0.18	0.02	0.11	0.00	0.00	24.0
2	440	-16130	-844	-99	0	180	6517	15.71	15.71	9.42	9.42	2	0.16	0.01	0.07	0.00	0.00	24.0
3	440	-16130	-845	-20	0	40	6524	15.71	15.71	9.42	9.42	2	0.16	0.01	0.07	0.00	0.00	24.0
4	440	-16130	-1426	-101	0	184	9231	15.71	15.71	9.42	9.42	2	0.23	0.02	0.11	0.00	0.00	24.0
5	440	-16140	-1427	-22	0	44	9238	15.71	15.71	9.42	9.42	2	0.23	0.02	0.11	0.00	0.00	24.0
6	440	-16120	-1046	-192	0	345	7459	15.71	15.71	9.42	9.42	2	0.19	0.01	0.08	0.00	0.00	24.0
7	440	-16140	-1050	72	0	-122	7482	15.71	15.71	9.42	9.42	2	0.19	0.01	0.08	0.00	0.00	24.0
8	440	-16120	-1221	-193	0	346	8273	15.71	15.71	9.42	9.42	2	0.21	0.02	0.09	0.00	0.00	24.0
9	440	-16140	-1225	71	0	-121	8296	15.71	15.71	9.42	9.42	2	0.21	0.02	0.09	0.00	0.00	24.0
10	440	-16130	-844	-99	0	180	6517	15.71	15.71	9.42	9.42	2	0.16	0.01	0.07	0.00	0.00	24.0
11	440	-16130	-845	-20	0	40	6524	15.71	15.71	9.42	9.42	2	0.16	0.01	0.07	0.00	0.00	24.0
12	440	-16130	-1426	-101	0	184	9231	15.71	15.71	9.42	9.42	2	0.23	0.02	0.11	0.00	0.00	24.0
13	440	-16140	-1427	-22	0	44	9238	15.71	15.71	9.42	9.42	2	0.23	0.02	0.11	0.00	0.00	24.0
14	440	-16120	-1046	-192	0	345	7459	15.71	15.71	9.42	9.42	2	0.19	0.01	0.08	0.00	0.00	24.0
15	440	-16140	-1050	72	0	-122	7482	15.71	15.71	9.42	9.42	2	0.19	0.01	0.08	0.00	0.00	24.0
16	440	-16120	-1221	-193	0	346	8273	15.71	15.71	9.42	9.42	2	0.21	0.02	0.09	0.00	0.00	24.0
17	440	-16140	-1225	71	0	-121	8296	15.71	15.71	9.42	9.42	2	0.21	0.02	0.09	0.00	0.00	24.0
18	440	-33140	-1860	-134	0	222	18650	15.71	15.71	9.42	9.42	3	0.31	0.02	0.12	0.00	0.00	24.0
19	440	-25800	-3953	-138	0	247	18250	15.71	15.71	9.42	9.42	3	0.32	0.05	0.28	0.00	0.00	24.0
20	440	-28160	-2697	109	0	-244	17210	15.71	15.71	9.42	9.42	3	0.30	0.03	0.18	0.00	0.00	24.0
37	440	-32870	-695	-114	0	184	16120	15.71	15.71	9.42	9.42	3	0.27	0.01	0.05	0.00	0.00	24.0
38	440	-20630	-4185	-120	0	225	15450	15.71	15.71	9.42	9.42	3	0.27	0.05	0.31	0.00	0.00	24.0
39	440	-24570	-2090	291	0	-593	13730	15.71	15.71	9.42	9.42	3	0.24	0.03	0.15	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 28 NI 250 NF 249 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 2B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-24510	-776	-34	0	-149	10630	15.71	15.71	9.42	9.42	3	0.18	0.01	0.06	0.00	0.00	24.0
2	0	-18880	-352	-74	0	-241	6047	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
3	0	-18940	-362	4	0	-37	6178	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
4	0	-18760	-833	-56	0	-193	10170	15.71	15.71	9.42	9.42	2	0.25	0.01	0.06	0.00	0.00	24.0
5	0	-18830	-842	22	0	11	10300	15.71	15.71	9.42	9.42	2	0.25	0.01	0.06	0.00	0.00	24.0
6	0	-18760	-510	-159	0	-462	7337	15.71	15.71	9.42	9.42	2	0.19	0.01	0.04	0.00	0.00	24.0
7	0	-18970	-541	101	0	218	7776	15.71	15.71	9.42	9.42	2	0.19	0.01	0.04	0.00	0.00	24.0
8	0	-18730	-654	-154	0	-448	8574	15.71	15.71	9.42	9.42	2	0.22	0.01	0.05	0.00	0.00	24.0
9	0	-18940	-685	107	0	233	9014	15.71	15.71	9.42	9.42	2	0.22	0.01	0.05	0.00	0.00	24.0
10	0	-18880	-352	-74	0	-241	6047	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
11	0	-18940	-362	4	0	-37	6178	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
12	0	-18760	-833	-56	0	-193	10170	15.71	15.71	9.42	9.42	2	0.25	0.01	0.06	0.00	0.00	24.0
13	0	-18830	-842	22	0	11	10300	15.71	15.71	9.42	9.42	2	0.25	0.01	0.06	0.00	0.00	24.0
14	0	-18760	-510	-159	0	-462	7337	15.71	15.71	9.42	9.42	2	0.19	0.01	0.04	0.00	0.00	24.0
15	0	-18970	-541	101	0	218	7776	15.71	15.71	9.42	9.42	2	0.19	0.01	0.04	0.00	0.00	24.0
16	0	-18730	-654	-154	0	-448	8574	15.71	15.71	9.42	9.42	2	0.22	0.01	0.05	0.00	0.00	24.0

17	0	-18940	-685	107	0	233	9014	15.71	15.71	9.42	9.42	2	0.22	0.01	0.05	0.00	0.00	24.0
18	0	-35620	933	-45	0	-328	12930	15.71	15.71	9.42	9.42	3	0.22	0.01	0.06	0.00	0.00	24.0
19	0	-28150	-3962	-15	0	-158	25990	15.71	15.71	9.42	9.42	3	0.45	0.05	0.27	0.00	0.00	24.0
20	0	-30910	-1416	202	0	326	18430	15.71	15.71	9.42	9.42	3	0.31	0.02	0.09	0.00	0.00	24.0
37	0	-35760	2806	-56	0	-354	5698	15.71	15.71	9.42	9.42	3	0.10	0.03	0.18	0.00	0.00	24.0
38	0	-23310	-5353	-7	0	-71	27460	15.71	15.71	9.42	9.42	3	0.48	0.07	0.38	0.00	0.00	24.0
39	0	-27910	-1109	355	0	735	14870	15.71	15.71	9.42	9.42	3	0.26	0.01	0.08	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	110	-23365	-776	-34	0	-112	9775	15.71	15.71	9.42	9.42	3	0.17	0.01	0.06	0.00	0.00	24.0
2	110	-18000	-352	-74	0	-159	5660	15.71	15.71	9.42	9.42	2	0.14	0.00	0.03	0.00	0.00	24.0
3	110	-18060	-362	4	0	-41	5780	15.71	15.71	9.42	9.42	2	0.14	0.00	0.03	0.00	0.00	24.0
4	110	-17880	-833	-56	0	-131	9254	15.71	15.71	9.42	9.42	2	0.23	0.01	0.06	0.00	0.00	24.0
5	110	-17950	-842	22	0	-13	9374	15.71	15.71	9.42	9.42	2	0.23	0.01	0.06	0.00	0.00	24.0
6	110	-17880	-510	-159	0	-287	6776	15.71	15.71	9.42	9.42	2	0.17	0.01	0.04	0.00	0.00	24.0
7	110	-18090	-541	101	0	107	7181	15.71	15.71	9.42	9.42	2	0.18	0.01	0.04	0.00	0.00	24.0
8	110	-17850	-654	-154	0	-279	7855	15.71	15.71	9.42	9.42	2	0.20	0.01	0.05	0.00	0.00	24.0
9	110	-18060	-685	107	0	116	8260	15.71	15.71	9.42	9.42	2	0.20	0.01	0.05	0.00	0.00	24.0
10	110	-18000	-352	-74	0	-159	5660	15.71	15.71	9.42	9.42	2	0.14	0.00	0.03	0.00	0.00	24.0
11	110	-18060	-362	4	0	-41	5780	15.71	15.71	9.42	9.42	2	0.14	0.00	0.03	0.00	0.00	24.0
12	110	-17880	-833	-56	0	-131	9254	15.71	15.71	9.42	9.42	2	0.23	0.01	0.06	0.00	0.00	24.0
13	110	-17950	-842	22	0	-13	9374	15.71	15.71	9.42	9.42	2	0.23	0.01	0.06	0.00	0.00	24.0
14	110	-17880	-510	-159	0	-287	6776	15.71	15.71	9.42	9.42	2	0.17	0.01	0.04	0.00	0.00	24.0
15	110	-18090	-541	101	0	107	7181	15.71	15.71	9.42	9.42	2	0.18	0.01	0.04	0.00	0.00	24.0
16	110	-17850	-654	-154	0	-279	7855	15.71	15.71	9.42	9.42	2	0.20	0.01	0.05	0.00	0.00	24.0
17	110	-18060	-685	107	0	116	8260	15.71	15.71	9.42	9.42	2	0.20	0.01	0.05	0.00	0.00	24.0
18	110	-34475	553	-45	0	-278	13747	15.71	15.71	9.42	9.42	3	0.23	0.01	0.04	0.00	0.00	24.0
19	110	-27005	-3582	-15	0	-142	21840	15.71	15.71	9.42	9.42	3	0.38	0.04	0.25	0.00	0.00	24.0
20	110	-29768	-1416	202	0	104	16873	15.71	15.71	9.42	9.42	3	0.29	0.02	0.10	0.00	0.00	24.0
37	110	-34615	2172	-56	0	-292	8436	15.71	15.71	9.42	9.42	3	0.14	0.03	0.14	0.00	0.00	24.0
38	110	-22165	-4720	-7	0	-64	21921	15.71	15.71	9.42	9.42	3	0.38	0.06	0.34	0.00	0.00	24.0
39	110	-26765	-1109	355	0	345	13651	15.71	15.71	9.42	9.42	3	0.24	0.01	0.08	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	220	-22220	-776	-34	0	-74	8920	15.71	15.71	9.42	9.42	3	0.16	0.01	0.06	0.00	0.00	24.0
2	220	-17120	-352	-74	0	-78	5272	15.71	15.71	9.42	9.42	2	0.13	0.00	0.03	0.00	0.00	24.0
3	220	-17180	-362	4	0	-46	5383	15.71	15.71	9.42	9.42	2	0.13	0.00	0.03	0.00	0.00	24.0
4	220	-17000	-833	-56	0	-69	8338	15.71	15.71	9.42	9.42	2	0.20	0.01	0.06	0.00	0.00	24.0
5	220	-17070	-842	22	0	-36	8448	15.71	15.71	9.42	9.42	2	0.21	0.01	0.06	0.00	0.00	24.0
6	220	-17000	-510	-159	0	-113	6215	15.71	15.71	9.42	9.42	2	0.15	0.01	0.04	0.00	0.00	24.0
7	220	-17210	-541	101	0	-4	6586	15.71	15.71	9.42	9.42	2	0.16	0.01	0.04	0.00	0.00	24.0
8	220	-16970	-654	-154	0	-110	7136	15.71	15.71	9.42	9.42	2	0.18	0.01	0.05	0.00	0.00	24.0
9	220	-17180	-685	107	0	-2	7507	15.71	15.71	9.42	9.42	2	0.18	0.01	0.05	0.00	0.00	24.0
10	220	-17120	-352	-74	0	-78	5272	15.71	15.71	9.42	9.42	2	0.13	0.00	0.03	0.00	0.00	24.0
11	220	-17180	-362	4	0	-46	5383	15.71	15.71	9.42	9.42	2	0.13	0.00	0.03	0.00	0.00	24.0
12	220	-17000	-833	-56	0	-69	8338	15.71	15.71	9.42	9.42	2	0.20	0.01	0.06	0.00	0.00	24.0
13	220	-17070	-842	22	0	-36	8448	15.71	15.71	9.42	9.42	2	0.21	0.01	0.06	0.00	0.00	24.0
14	220	-17000	-510	-159	0	-113	6215	15.71	15.71	9.42	9.42	2	0.15	0.01	0.04	0.00	0.00	24.0
15	220	-17210	-541	101	0	-4	6586	15.71	15.71	9.42	9.42	2	0.16	0.01	0.04	0.00	0.00	24.0
16	220	-16970	-654	-154	0	-110	7136	15.71	15.71	9.42	9.42	2	0.18	0.01	0.05	0.00	0.00	24.0
17	220	-17180	-685	107	0	-2	7507	15.71	15.71	9.42	9.42	2	0.18	0.01	0.05	0.00	0.00	24.0
18	220	-33330	173	-45	0	-229	14146	15.71	15.71	9.42	9.42	3	0.24	0.00	0.01	0.00	0.00	24.0
19	220	-25860	-3202	-15	0	-125	18109	15.71	15.71	9.42	9.42	3	0.31	0.04	0.22	0.00	0.00	24.0
20	220	-28625	-1416	202	0	-119	15315	15.71	15.71	9.42	9.42	3	0.26	0.02	0.10	0.00	0.00	24.0
37	220	-33470	1539	-56	0	-230	10478	15.71	15.71	9.42	9.42	3	0.18	0.02	0.10	0.00	0.00	24.0
38	220	-21020	-4086	-7	0	-57	17079	15.71	15.71	9.42	9.42	3	0.30	0.05	0.30	0.00	0.00	24.0
39	220	-25620	-1109	355	0	-45	12432	15.71	15.71	9.42	9.42	3	0.21	0.01	0.08	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	330	-21075	-776	-34	0	-37	8066	15.71	15.71	9.42	9.42	3	0.14	0.01	0.06	0.00	0.00	24.0
2	330	-16240	-352	-74	0	3	4885	15.71	15.71	9.42	9.42	2	0.12	0.00	0.03	0.00	0.00	24.0
3	330	-16300	-362	4	0	-50	4985	15.71	15.71	9.42	9.42	2	0.12	0.00	0.03	0.00	0.00	24.0
4	330	-16120	-833	-56	0	-7	7422	15.71	15.71	9.42	9.42	2	0.18	0.01	0.06	0.00	0.00	24.0
5	330	-16190	-842	22	0	-60	7523	15.71	15.71	9.42	9.42	2	0.19	0.01	0.07	0.00	0.00	24.0
6	330	-16120	-510	-159	0	62	5655	15.71	15.71	9.42	9.42	2	0.14	0.01	0.04	0.00	0.00	24.0
7	330	-16330	-541	101	0	-116	5992	15.71	15.71	9.42	9.42	2	0.15	0.01	0.04	0.00	0.00	24.0
8	330	-16090	-654	-154	0	59	6416	15.71	15.71	9.42	9.42	2	0.16	0.01	0.05	0.00	0.00	24.0
9	330	-16300	-685	107	0	-119	6754	15.71	15.71	9.42	9.42	2	0.17	0.01	0.05	0.00	0.00	24.0
10	330	-16240	-352	-74	0	3	4885	15.71	15.71	9.42	9.42	2	0.12	0.00	0.03	0.00	0.00	24.0
11	330	-16300	-362	4	0	-50	4985	15.71	15.71	9.42	9.42	2	0.12	0.00	0.03	0.00	0.00	24.0
12	330	-16120	-833	-56	0	-7	7422	15.71	15.71	9.42	9.42	2	0.18	0.01	0.06	0.00	0.00	24.0
13	330	-16190	-842	22	0	-60	7523	15.71	15.71	9.42	9.42	2	0.19	0.01	0.07	0.00	0.00	24.0
14	330	-16120	-510	-159	0	62	5655	15.71	15.71	9.42	9.42	2	0.14	0.01	0.04	0.00	0.00	24.0
15	330	-16330	-541	101	0	-116	5992	15.71	15.71	9.42	9.42	2	0.15	0.01	0.04	0.00	0.00	24.0
16	330	-16090	-654	-154	0	59	6416	15.71	15.71	9.42	9.42	2	0.16	0.01	0.05	0.00	0.00	24.0
17	330	-16300	-685	107	0	-119	6754	15.71	15.71	9.42	9.42	2	0.17	0.01	0.05	0.00	0.00	24.0
18	330	-32185	-207	-45	0	-180	14127	15.71	15.71	9.42	9.42	3	0.24	0.00	0.01	0.00	0.00	24.0
19	330	-24715	-2822	-15	0	-109	14795	15.71	15.71	9.42	9.42	3	0.26	0.04	0.20	0.00	0.00	24.0
20	330	-27482	-1416	202	0	-341	13758	15.71	15.71	9.42	9.42	3	0.24	0.02	0.10	0.00	0.00	24.0
37	330	-32325	905	-56	0	-168	11822	15.71	15.71	9.42	9.42	3	0.20	0.01	0.06	0.00	0.00	24.0
38	330	-19875	-3452	-7	0	-50	12934	15.71	15.71	9.42	9.42	3	0.23	0.04	0.26	0.00	0.00	24.0
39	330	-24475	-1109	355	0	-436	11214	15.71	15.71	9.42	9.42	3	0.20	0.01	0.08	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	440	-19930	-776	-34	0	0	7211	15.71	15.71	9.42	9.42	3	0.13	0.01	0.06	0.00	0.00	24.0
2	440	-15360	-352	-74	0	85	4497	15.71	15.71	9.42	9.42	2	0.11	0.00	0.03	0.00	0.00	24.0
3	440	-15420	-362	4	0	-54	4588	15.71	15.71	9.42	9.42	2	0.11	0.00	0.03	0.00	0.00	24.0
4	440	-15240	-833	-56	0	55	6506	15.71	15.71	9.42	9.42	2	0.16	0.01	0.07	0.00	0.00	24.0
5	440	-15310	-842	22	0	-84	6597	15.71	15.71	9.42	9.42	2	0.16	0.01	0.07	0.00	0.00	24.0
6	440	-15240	-510	-159	0	237	5094	15.71	15.71	9.42	9.42	2	0.13	0.01	0.04	0.00	0.00	24.0
7	440	-15450	-541	101	0	-227	5397	15.71	15.71	9.42	9.42	2	0.14	0.01	0.04	0.00	0.00	24.0
8	440	-15210	-654	-154	0	228	5697	15.71	15.71	9.42	9.42	2	0.15	0.01	0.05	0.00	0.00	24.0
9	440	-15420	-685	107	0	-236	6000	15.71	15.71	9.42	9.42	2	0.15	0.01	0.05	0.00	0.00	24.0
10	440	-15360	-352	-74	0	85	4497	15.71	15.71	9.42	9.42	2	0.11	0.00	0.03	0.00	0.00	24.0
11	440	-15420	-362	4	0	-54	4588	15.71	15.71	9.42	9.42	2	0.11	0.00	0.03	0.00	0.00	24.0
12	440	-15240	-833	-56	0	55	6506	15.71	15.71	9.42	9.42	2	0.16	0.01	0.07	0.00	0.00	24.0
13	440	-15310	-842	22	0	-84	6597	15.71	15.71	9.42	9.42	2	0.16	0.01	0.07	0.00	0.00	24.0
14	440	-15240	-510	-159	0	237	5094	15.71	15.71	9.42	9.42	2	0.13	0.01	0.04	0.00	0.00	24.0
15	440	-15450	-541	101	0	-227	5397	15.71	15.71	9.42	9.42	2	0.14	0.01	0.04	0.00	0.00	24.0
16	440	-15210	-654	-154	0	228	5697	15.71	15.71	9.42	9.42	2	0.15	0.01	0.05	0.00	0.00	24.0
17	440	-15420	-685	107	0	-236	6000	15.71	15.71	9.42	9.42	2	0.15	0.01	0.05	0.00	0.00	24.0
18	440	-31040	-587	-45	0	-131	13690	15.71	15.71	9.42	9.42	3	0.23	0.01	0.04	0.00	0.00	24.0
19	440	-23570	-2442	-15	0	-93	11900	15.71	15.71	9.42	9.42	3	0.21	0.03	0.17	0.00	0.00	24.0
20	440	-26340	-1416	202	0	-563	12200	15.71	15.71	9.42	9.42	3	0.21	0.02	0.10	0.00	0.00	24.0
37	440	-31180	272	-56	0	-107	12470	15.71	15.71	9.42	9.42	3	0.21	0.00	0.02	0.00	0.00	24.0
38	440	-18730	-2819	-7	0	-42	9486	15.71	15.71	9.42	9.42	3	0.17	0.04	0.21	0.00	0.00	24.0

39	440	-23330	-1109	355	0	-826	9995	15.71	15.71	9.42	9.42	3	0.18	0.01	0.08	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 29 NI 293 NF 292 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 1B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-17260	-97	-328	0	-347	54	6.28	6.28	9.42	9.42	3	0.02	0.01	0.03	0.00	0.00	24.0
2	0	-12590	84	-302	0	-432	-355	6.28	6.28	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
3	0	-12410	82	-238	0	-230	-348	6.28	6.28	9.42	9.42	2	0.04	0.01	0.03	0.00	0.00	24.0
4	0	-14150	-231	-267	0	-304	432	6.28	6.28	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
5	0	-13970	-234	-203	0	-102	439	6.28	6.28	9.42	9.42	2	0.05	0.01	0.02	0.00	0.00	24.0
6	0	-13340	-24	-365	0	-623	-87	6.28	6.28	9.42	9.42	2	0.04	0.01	0.04	0.00	0.00	24.0
7	0	-12740	-31	-151	0	50	-65	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
8	0	-13810	-118	-354	0	-585	149	6.28	6.28	9.42	9.42	2	0.04	0.01	0.04	0.00	0.00	24.0
9	0	-13210	-126	-140	0	88	171	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
10	0	-12590	84	-302	0	-432	-355	6.28	6.28	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
11	0	-12410	82	-238	0	-230	-348	6.28	6.28	9.42	9.42	2	0.04	0.01	0.03	0.00	0.00	24.0
12	0	-14150	-231	-267	0	-304	432	6.28	6.28	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
13	0	-13970	-234	-203	0	-102	439	6.28	6.28	9.42	9.42	2	0.05	0.01	0.02	0.00	0.00	24.0
14	0	-13340	-24	-365	0	-623	-87	6.28	6.28	9.42	9.42	2	0.04	0.01	0.04	0.00	0.00	24.0
15	0	-12740	-31	-151	0	50	-65	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
16	0	-13810	-118	-354	0	-585	149	6.28	6.28	9.42	9.42	2	0.04	0.01	0.04	0.00	0.00	24.0
17	0	-13210	-126	-140	0	88	171	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
18	0	-19570	845	-599	0	-933	-1552	6.28	6.28	9.42	9.42	3	0.15	0.02	0.08	0.00	0.00	24.0
19	0	-21160	-915	-374	0	-337	1423	6.28	6.28	9.42	9.42	3	0.13	0.02	0.09	0.00	0.00	24.0
20	0	-19550	-43	-512	0	-171	-48	6.28	6.28	9.42	9.42	3	0.01	0.01	0.05	0.00	0.00	24.0
37	0	-18020	1413	-623	0	-1039	-2506	6.28	6.28	9.42	9.42	3	0.24	0.03	0.14	0.00	0.00	24.0
38	0	-20670	-1522	-248	0	-45	2453	6.28	6.28	9.42	9.42	3	0.23	0.04	0.14	0.00	0.00	24.0
39	0	-17990	-67	-478	0	231	1	6.28	6.28	9.42	9.42	3	0.01	0.01	0.05	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	97	-16690	-97	-328	0	-27	-40	6.28	6.28	9.42	9.42	3	0.00	0.01	0.03	0.00	0.00	24.0
2	97	-12150	84	-302	0	-137	-273	6.28	6.28	9.42	9.42	2	0.03	0.01	0.03	0.00	0.00	24.0
3	97	-11970	82	-238	0	2	-269	6.28	6.28	9.42	9.42	2	0.03	0.01	0.03	0.00	0.00	24.0
4	97	-13710	-231	-267	0	-44	206	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
5	97	-13530	-234	-203	0	95	211	6.28	6.28	9.42	9.42	2	0.03	0.01	0.02	0.00	0.00	24.0
6	97	-12902	-24	-365	0	-267	-111	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
7	97	-12302	-31	-151	0	197	-95	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
8	97	-13370	-118	-354	0	-239	33	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
9	97	-12772	-126	-140	0	225	48	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
10	97	-12150	84	-302	0	-137	-273	6.28	6.28	9.42	9.42	2	0.03	0.01	0.03	0.00	0.00	24.0
11	97	-11970	82	-238	0	2	-269	6.28	6.28	9.42	9.42	2	0.03	0.01	0.03	0.00	0.00	24.0
12	97	-13710	-231	-267	0	-44	206	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
13	97	-13530	-234	-203	0	95	211	6.28	6.28	9.42	9.42	2	0.03	0.01	0.02	0.00	0.00	24.0
14	97	-12902	-24	-365	0	-267	-111	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
15	97	-12302	-31	-151	0	197	-95	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
16	97	-13370	-118	-354	0	-239	33	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
17	97	-12772	-126	-140	0	225	48	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
18	97	-19000	677	-599	0	-349	-810	6.28	6.28	9.42	9.42	3	0.08	0.02	0.07	0.00	0.00	24.0
19	97	-20590	-747	-374	0	28	613	6.28	6.28	9.42	9.42	3	0.06	0.02	0.07	0.00	0.00	24.0
20	97	-18980	-43	-381	0	263	-90	6.28	6.28	9.42	9.42	3	0.01	0.01	0.04	0.00	0.00	24.0
37	97	-17450	1132	-623	0	-431	-1266	6.28	6.28	9.42	9.42	3	0.12	0.03	0.11	0.00	0.00	24.0
38	97	-20100	-1241	-248	0	197	1106	6.28	6.28	9.42	9.42	3	0.10	0.03	0.12	0.00	0.00	24.0
39	97	-17420	-67	-260	0	588	-65	6.28	6.28	9.42	9.42	3	0.03	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	195	-16120	-97	-328	0	293	-135	6.28	6.28	9.42	9.42	3	0.02	0.01	0.04	0.00	0.00	24.0
2	195	-11710	84	-302	0	158	-191	6.28	6.28	9.42	9.42	2	0.03	0.01	0.03	0.00	0.00	24.0
3	195	-11530	82	-238	0	234	-189	6.28	6.28	9.42	9.42	2	0.03	0.01	0.03	0.00	0.00	24.0
4	195	-13270	-231	-267	0	217	-19	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
5	195	-13090	-234	-203	0	293	-17	6.28	6.28	9.42	9.42	2	0.02	0.01	0.02	0.00	0.00	24.0
6	195	-12465	-24	-365	0	89	-134	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
7	195	-11865	-31	-151	0	344	-126	6.28	6.28	9.42	9.42	2	0.03	0.00	0.02	0.00	0.00	24.0
8	195	-12930	-118	-354	0	107	-82	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
9	195	-12335	-126	-140	0	362	-74	6.28	6.28	9.42	9.42	2	0.03	0.00	0.02	0.00	0.00	24.0
10	195	-11710	84	-302	0	158	-191	6.28	6.28	9.42	9.42	2	0.03	0.01	0.03	0.00	0.00	24.0
11	195	-11530	82	-238	0	234	-189	6.28	6.28	9.42	9.42	2	0.03	0.01	0.03	0.00	0.00	24.0
12	195	-13270	-231	-267	0	217	-19	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
13	195	-13090	-234	-203	0	293	-17	6.28	6.28	9.42	9.42	2	0.02	0.01	0.02	0.00	0.00	24.0
14	195	-12465	-24	-365	0	89	-134	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
15	195	-11865	-31	-151	0	344	-126	6.28	6.28	9.42	9.42	2	0.03	0.00	0.02	0.00	0.00	24.0
16	195	-12930	-118	-354	0	107	-82	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
17	195	-12335	-126	-140	0	362	-74	6.28	6.28	9.42	9.42	2	0.03	0.00	0.02	0.00	0.00	24.0
18	195	-18430	508	-599	0	235	-232	6.28	6.28	9.42	9.42	3	0.02	0.01	0.06	0.00	0.00	24.0
19	195	-20020	-578	-374	0	393	-33	6.28	6.28	9.42	9.42	3	0.02	0.01	0.05	0.00	0.00	24.0
20	195	-18410	-43	-270	0	579	-131	6.28	6.28	9.42	9.42	3	0.03	0.01	0.03	0.00	0.00	24.0
37	195	-16880	851	-623	0	176	-299	6.28	6.28	9.42	9.42	3	0.03	0.02	0.08	0.00	0.00	24.0
38	195	-19530	-960	-248	0	438	33	6.28	6.28	9.42	9.42	3	0.02	0.02	0.08	0.00	0.00	24.0
39	195	-16850	-67	-73	0	748	-130	6.28	6.28	9.42	9.42	3	0.04	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	292	-15550	-97	-328	0	613	-230	6.28	6.28	9.42	9.42	3	0.03	0.01	0.04	0.00	0.00	24.0
2	292	-11270	84	-302	0	452	-109	6.28	6.28	9.42	9.42	2	0.03	0.01	0.03	0.00	0.00	24.0
3	292	-11090	82	-238	0	466	-109	6.28	6.28	9.42	9.42	2	0.03	0.01	0.03	0.00	0.00	24.0
4	292	-12830	-231	-267	0	477	-245	6.28	6.28	9.42	9.42	2	0.04	0.01	0.03	0.00	0.00	24.0
5	292	-12650	-234	-203	0	491	-244	6.28	6.28	9.42	9.42	2	0.04	0.01	0.02	0.00	0.00	24.0
6	292	-12028	-24	-365	0	445	-157	6.28	6.28	9.42	9.42	2	0.04	0.01	0.04	0.00	0.00	24.0
7	292	-11428	-31	-151	0	491	-156	6.28	6.28	9.42	9.42	2	0.04	0.00	0.02	0.00	0.00	24.0
8	292	-12490	-118	-354	0	452	-197	6.28	6.28	9.42	9.42	2	0.04	0.01	0.04	0.00	0.00	24.0
9	292	-11898	-126	-140	0	498	-197	6.28	6.28	9.42	9.42	2	0.04	0.00	0.02	0.00	0.00	24.0
10	292	-11270	84	-302	0	452	-109	6.28	6.28	9.42	9.42	2	0.03	0.01	0.03	0.00	0.00	24.0
11	292	-11090	82	-238	0	466	-109	6.28	6.28	9.42	9.42	2	0.03	0.01	0.03	0.00	0.00	24.0
12	292	-12830	-231	-267	0	477	-245	6.28	6.28	9.42	9.42	2	0.04	0.01	0.03	0.00	0.00	24.0
13	292	-12650	-234	-203	0	491	-244	6.28	6.28	9.42	9.42	2	0.04	0.01	0.02	0.00	0.00	24.0
14	292	-12028	-24	-365	0	445	-157	6.28	6.28	9.42	9.42	2	0.04	0.01	0.04	0.00	0.00	24.0
15	292	-11428	-31	-151	0	491	-156	6.28	6.28	9.42	9.42	2	0.04	0.00	0.02	0.00	0.00	24.0
16	292	-12490	-118	-354	0	452	-197	6.28	6.28	9.42	9.42	2	0.04	0.01	0.04	0.00	0.00	24.0
17	292	-11898	-126	-140	0	498	-197	6.28	6.28	9.42	9.42	2	0.04	0.00	0.02	0.00	0.00	24.0
18	292	-17860	340	-599	0	820	181	6.28	6.28	9.42	9.42	3	0.04	0.01	0.06	0.00	0.00	24.0

19	292	-19450	-410	-374	0	757	-515	6.28	6.28	9.42	9.42	3	0.06	0.01	0.04	0.00	0.00	24.0
20	292	-17840	-43	-176	0	795	-173	6.28	6.28	9.42	9.42	3	0.04	0.00	0.02	0.00	0.00	24.0
37	292	-16310	570	-623	0	783	393	6.28	6.28	9.42	9.42	3	0.05	0.01	0.07	0.00	0.00	24.0
38	292	-18960	-680	-248	0	679	-766	6.28	6.28	9.42	9.42	3	0.08	0.02	0.07	0.00	0.00	24.0
39	292	-16280	-67	82	0	741	-196	6.28	6.28	9.42	9.42	3	0.04	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	390	-14980	-97	-328	0	933	-325	6.28	6.28	9.42	9.42	3	0.05	0.01	0.04	0.00	0.00	24.0
2	390	-10830	84	-302	0	747	-27	6.28	6.28	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
3	390	-10650	82	-238	0	698	-29	6.28	6.28	9.42	9.42	2	0.04	0.01	0.03	0.00	0.00	24.0
4	390	-12390	-231	-267	0	737	-470	6.28	6.28	9.42	9.42	2	0.08	0.01	0.03	0.00	0.00	24.0
5	390	-12210	-234	-203	0	689	-472	6.28	6.28	9.42	9.42	2	0.08	0.01	0.02	0.00	0.00	24.0
6	390	-11590	-24	-365	0	801	-180	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
7	390	-10990	-31	-151	0	638	-187	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
8	390	-12050	-118	-354	0	798	-313	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
9	390	-11460	-126	-140	0	635	-320	6.28	6.28	9.42	9.42	2	0.06	0.00	0.02	0.00	0.00	24.0
10	390	-10830	84	-302	0	747	-27	6.28	6.28	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
11	390	-10650	82	-238	0	698	-29	6.28	6.28	9.42	9.42	2	0.04	0.01	0.03	0.00	0.00	24.0
12	390	-12390	-231	-267	0	737	-470	6.28	6.28	9.42	9.42	2	0.08	0.01	0.03	0.00	0.00	24.0
13	390	-12210	-234	-203	0	689	-472	6.28	6.28	9.42	9.42	2	0.08	0.01	0.02	0.00	0.00	24.0
14	390	-11590	-24	-365	0	801	-180	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
15	390	-10990	-31	-151	0	638	-187	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
16	390	-12050	-118	-354	0	798	-313	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
17	390	-11460	-126	-140	0	635	-320	6.28	6.28	9.42	9.42	2	0.06	0.00	0.02	0.00	0.00	24.0
18	390	-17290	171	-599	0	1404	430	6.28	6.28	9.42	9.42	3	0.07	0.01	0.06	0.00	0.00	24.0
19	390	-18880	-241	-374	0	1122	-832	6.28	6.28	9.42	9.42	3	0.09	0.01	0.04	0.00	0.00	24.0
20	390	-17270	-43	-102	0	929	-214	6.28	6.28	9.42	9.42	3	0.05	0.00	0.01	0.00	0.00	24.0
37	390	-15740	289	-623	0	1391	812	6.28	6.28	9.42	9.42	3	0.10	0.01	0.07	0.00	0.00	24.0
38	390	-18390	-399	-248	0	921	-1292	6.28	6.28	9.42	9.42	3	0.13	0.01	0.04	0.00	0.00	24.0
39	390	-15710	-67	206	0	598	-262	6.28	6.28	9.42	9.42	3	0.04	0.00	0.02	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 30 NI 77 NF 76 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 6C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-14090	-874	149	0	71	5896	15.71	15.71	9.42	9.42	3	0.11	0.01	0.07	0.00	0.00	24.0
2	0	-10970	-567	52	0	-20	4059	15.71	15.71	9.42	9.42	2	0.10	0.01	0.05	0.00	0.00	24.0
3	0	-10950	-546	124	0	105	4006	15.71	15.71	9.42	9.42	2	0.10	0.01	0.04	0.00	0.00	24.0
4	0	-10730	-799	105	0	4	5066	15.71	15.71	9.42	9.42	2	0.13	0.01	0.07	0.00	0.00	24.0
5	0	-10710	-778	177	0	129	5012	15.71	15.71	9.42	9.42	2	0.13	0.01	0.06	0.00	0.00	24.0
6	0	-10910	-673	-14	0	-157	4474	15.71	15.71	9.42	9.42	2	0.12	0.01	0.06	0.00	0.00	24.0
7	0	-10840	-602	227	0	259	4295	15.71	15.71	9.42	9.42	2	0.11	0.01	0.05	0.00	0.00	24.0
8	0	-10830	-742	2	0	-150	4776	15.71	15.71	9.42	9.42	2	0.12	0.01	0.06	0.00	0.00	24.0
9	0	-10770	-672	242	0	267	4597	15.71	15.71	9.42	9.42	2	0.12	0.01	0.06	0.00	0.00	24.0
10	0	-10970	-567	52	0	-20	4059	15.71	15.71	9.42	9.42	2	0.10	0.01	0.05	0.00	0.00	24.0
11	0	-10950	-546	124	0	105	4006	15.71	15.71	9.42	9.42	2	0.10	0.01	0.04	0.00	0.00	24.0
12	0	-10730	-799	105	0	4	5066	15.71	15.71	9.42	9.42	2	0.13	0.01	0.07	0.00	0.00	24.0
13	0	-10710	-778	177	0	129	5012	15.71	15.71	9.42	9.42	2	0.13	0.01	0.06	0.00	0.00	24.0
14	0	-10910	-673	-14	0	-157	4474	15.71	15.71	9.42	9.42	2	0.12	0.01	0.06	0.00	0.00	24.0
15	0	-10840	-602	227	0	259	4295	15.71	15.71	9.42	9.42	2	0.11	0.01	0.05	0.00	0.00	24.0
16	0	-10830	-742	2	0	-150	4776	15.71	15.71	9.42	9.42	2	0.12	0.01	0.06	0.00	0.00	24.0
17	0	-10770	-672	242	0	267	4597	15.71	15.71	9.42	9.42	2	0.12	0.01	0.06	0.00	0.00	24.0
18	0	-25080	-1078	238	0	134	13290	15.71	15.71	9.42	9.42	3	0.23	0.01	0.08	0.00	0.00	24.0
19	0	-17360	-2293	295	0	107	8851	15.71	15.71	9.42	9.42	3	0.16	0.03	0.17	0.00	0.00	24.0
20	0	-20260	-1583	330	0	139	10580	15.71	15.71	9.42	9.42	3	0.19	0.02	0.12	0.00	0.00	24.0
37	0	-25380	-408	181	0	127	13090	15.71	15.71	9.42	9.42	3	0.23	0.01	0.03	0.00	0.00	24.0
38	0	-12510	-2432	276	0	83	5689	15.71	15.71	9.42	9.42	3	0.10	0.03	0.20	0.00	0.00	24.0
39	0	-17350	-1249	335	0	135	8574	15.71	15.71	9.42	9.42	3	0.15	0.02	0.10	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	83	-13232	-874	149	0	-51	5175	15.71	15.71	9.42	9.42	3	0.09	0.01	0.07	0.00	0.00	24.0
2	83	-10309	-567	52	0	-63	3591	15.71	15.71	9.42	9.42	2	0.09	0.01	0.05	0.00	0.00	24.0
3	83	-10289	-546	124	0	3	3556	15.71	15.71	9.42	9.42	2	0.09	0.01	0.05	0.00	0.00	24.0
4	83	-10070	-799	105	0	-82	4407	15.71	15.71	9.42	9.42	2	0.11	0.01	0.07	0.00	0.00	24.0
5	83	-10050	-778	177	0	-17	4370	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
6	83	-10249	-673	-14	0	-146	3919	15.71	15.71	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
7	83	-10180	-602	227	0	72	3798	15.71	15.71	9.42	9.42	2	0.10	0.01	0.05	0.00	0.00	24.0
8	83	-10171	-742	2	0	-152	4164	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
9	83	-10110	-672	242	0	67	4043	15.71	15.71	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
10	83	-10309	-567	52	0	-63	3591	15.71	15.71	9.42	9.42	2	0.09	0.01	0.05	0.00	0.00	24.0
11	83	-10289	-546	124	0	3	3556	15.71	15.71	9.42	9.42	2	0.09	0.01	0.05	0.00	0.00	24.0
12	83	-10070	-799	105	0	-82	4407	15.71	15.71	9.42	9.42	2	0.11	0.01	0.07	0.00	0.00	24.0
13	83	-10050	-778	177	0	-17	4370	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
14	83	-10249	-673	-14	0	-146	3919	15.71	15.71	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
15	83	-10180	-602	227	0	72	3798	15.71	15.71	9.42	9.42	2	0.10	0.01	0.05	0.00	0.00	24.0
16	83	-10171	-742	2	0	-152	4164	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
17	83	-10110	-672	242	0	67	4043	15.71	15.71	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
18	83	-24222	-1455	238	0	-63	12246	15.71	15.71	9.42	9.42	3	0.21	0.02	0.10	0.00	0.00	24.0
19	83	-16502	-1916	295	0	-136	7115	15.71	15.71	9.42	9.42	3	0.13	0.02	0.15	0.00	0.00	24.0
20	83	-19402	-1583	330	0	-134	9275	15.71	15.71	9.42	9.42	3	0.16	0.02	0.12	0.00	0.00	24.0
37	83	-24522	-1037	181	0	-22	12495	15.71	15.71	9.42	9.42	3	0.22	0.01	0.07	0.00	0.00	24.0
38	83	-11653	-1803	276	0	-145	3942	15.71	15.71	9.42	9.42	3	0.07	0.02	0.15	0.00	0.00	24.0
39	83	-16492	-1249	335	0	-141	7544	15.71	15.71	9.42	9.42	3	0.14	0.02	0.10	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	165	-12375	-874	149	0	-174	4454	15.71	15.71	9.42	9.42	3	0.08	0.01	0.07	0.00	0.00	24.0
2	165	-9648	-567	52	0	-105	3124	15.71	15.71	9.42	9.42	2	0.08	0.01	0.05	0.00	0.00	24.0
3	165	-9628	-546	124	0	-99	3105	15.71	15.71	9.42	9.42	2	0.08	0.01	0.05	0.00	0.00	24.0
4	165	-9409	-799	105	0	-168	3748	15.71	15.71	9.42	9.42	2	0.10	0.01	0.07	0.00	0.00	24.0
5	165	-9389	-778	177	0	-163	3729	15.71	15.71	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
6	165	-9588	-673	-14	0	-134	3364	15.71	15.71	9.42	9.42	2	0.09	0.01	0.06	0.00	0.00	24.0
7	165	-9520	-602	227	0	-115	3302	15.71	15.71	9.42	9.42	2	0.09	0.01	0.05	0.00	0.00	24.0
8	165	-9512	-742	2	0	-153	3552	15.71	15.71	9.42	9.42	2	0.09	0.01	0.06	0.00	0.00	24.0
9	165	-9450	-672	242	0	-133	3489	15.71	15.71	9.42	9.42	2	0.09	0.01	0.06	0.00	0.00	24.0
10	165	-9648	-567	52	0	-105	3124	15.71	15.71	9.42	9.42	2	0.08	0.01	0.05	0.00	0.00	24.0
11	165	-9628	-546	124	0	-99	3105	15.71	15.71	9.42	9.42	2	0.08	0.01	0.05	0.00	0.00	24.0
12	165	-9409	-799	105	0	-168	3748	15.71	15.71	9.42	9.42	2	0.10	0.01	0.07	0.00	0.00	24.0
13	165	-9389	-778	177	0	-163	3729	15.71	15.71	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
14	165	-9588	-673	-14	0	-134	3364	15.71	15.71	9.42	9.42	2	0.09	0.01	0.06	0.00	0.00	24.0

15	165	-9520	-602	227	0	-115	3302	15.71	15.71	9.42	9.42	2	0.09	0.01	0.05	0.00	0.00	24.0
16	165	-9512	-742	2	0	-153	3552	15.71	15.71	9.42	9.42	2	0.09	0.01	0.06	0.00	0.00	24.0
17	165	-9450	-672	242	0	-133	3489	15.71	15.71	9.42	9.42	2	0.09	0.01	0.06	0.00	0.00	24.0
18	165	-23365	-1832	238	0	-259	10890	15.71	15.71	9.42	9.42	3	0.19	0.02	0.13	0.00	0.00	24.0
19	165	-15645	-1538	295	0	-380	5691	15.71	15.71	9.42	9.42	3	0.10	0.02	0.12	0.00	0.00	24.0
20	165	-18545	-1583	330	0	-406	7970	15.71	15.71	9.42	9.42	3	0.14	0.02	0.12	0.00	0.00	24.0
37	165	-23665	-1666	181	0	-171	11381	15.71	15.71	9.42	9.42	3	0.20	0.02	0.12	0.00	0.00	24.0
38	165	-10796	-1175	276	0	-373	2714	15.71	15.71	9.42	9.42	3	0.05	0.02	0.10	0.00	0.00	24.0
39	165	-15635	-1249	335	0	-417	6514	15.71	15.71	9.42	9.42	3	0.12	0.02	0.10	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	248	-11518	-874	149	0	-297	3734	15.71	15.71	9.42	9.42	3	0.07	0.01	0.07	0.00	0.00	24.0
2	248	-8987	-567	52	0	-148	2656	15.71	15.71	9.42	9.42	2	0.07	0.01	0.05	0.00	0.00	24.0
3	248	-8968	-546	124	0	-202	2655	15.71	15.71	9.42	9.42	2	0.07	0.01	0.05	0.00	0.00	24.0
4	248	-8748	-799	105	0	-255	3089	15.71	15.71	9.42	9.42	2	0.09	0.01	0.07	0.00	0.00	24.0
5	248	-8728	-778	177	0	-308	3087	15.71	15.71	9.42	9.42	2	0.09	0.01	0.07	0.00	0.00	24.0
6	248	-8927	-673	-14	0	-123	2810	15.71	15.71	9.42	9.42	2	0.07	0.01	0.06	0.00	0.00	24.0
7	248	-8860	-602	227	0	-302	2805	15.71	15.71	9.42	9.42	2	0.08	0.01	0.05	0.00	0.00	24.0
8	248	-8853	-742	2	0	-155	2939	15.71	15.71	9.42	9.42	2	0.08	0.01	0.06	0.00	0.00	24.0
9	248	-8789	-672	242	0	-334	2934	15.71	15.71	9.42	9.42	2	0.08	0.01	0.06	0.00	0.00	24.0
10	248	-8987	-567	52	0	-148	2656	15.71	15.71	9.42	9.42	2	0.07	0.01	0.05	0.00	0.00	24.0
11	248	-8968	-546	124	0	-202	2655	15.71	15.71	9.42	9.42	2	0.07	0.01	0.05	0.00	0.00	24.0
12	248	-8748	-799	105	0	-255	3089	15.71	15.71	9.42	9.42	2	0.09	0.01	0.07	0.00	0.00	24.0
13	248	-8728	-778	177	0	-308	3087	15.71	15.71	9.42	9.42	2	0.09	0.01	0.07	0.00	0.00	24.0
14	248	-8927	-673	-14	0	-123	2810	15.71	15.71	9.42	9.42	2	0.07	0.01	0.06	0.00	0.00	24.0
15	248	-8860	-602	227	0	-302	2805	15.71	15.71	9.42	9.42	2	0.08	0.01	0.05	0.00	0.00	24.0
16	248	-8853	-742	2	0	-155	2939	15.71	15.71	9.42	9.42	2	0.08	0.01	0.06	0.00	0.00	24.0
17	248	-8789	-672	242	0	-334	2934	15.71	15.71	9.42	9.42	2	0.08	0.01	0.06	0.00	0.00	24.0
18	248	-22508	-2210	238	0	-455	9224	15.71	15.71	9.42	9.42	3	0.16	0.03	0.16	0.00	0.00	24.0
19	248	-14788	-1161	295	0	-623	4577	15.71	15.71	9.42	9.42	3	0.09	0.01	0.09	0.00	0.00	24.0
20	248	-17688	-1583	330	0	-679	6664	15.71	15.71	9.42	9.42	3	0.12	0.02	0.12	0.00	0.00	24.0
37	248	-22808	-2294	181	0	-321	9748	15.71	15.71	9.42	9.42	3	0.17	0.03	0.17	0.00	0.00	24.0
38	248	-9940	-546	276	0	-600	2004	15.71	15.71	9.42	9.42	3	0.04	0.01	0.05	0.00	0.00	24.0
39	248	-14778	-1249	335	0	-693	5483	15.71	15.71	9.42	9.42	3	0.10	0.02	0.10	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	330	-10660	-874	149	0	-419	3013	15.71	15.71	9.42	9.42	3	0.06	0.01	0.07	0.00	0.00	24.0
2	330	-8326	-567	52	0	-191	2189	15.71	15.71	9.42	9.42	2	0.06	0.01	0.05	0.00	0.00	24.0
3	330	-8307	-546	124	0	-304	2205	15.71	15.71	9.42	9.42	2	0.06	0.01	0.05	0.00	0.00	24.0
4	330	-8088	-799	105	0	-341	2430	15.71	15.71	9.42	9.42	2	0.07	0.01	0.07	0.00	0.00	24.0
5	330	-8068	-778	177	0	-454	2446	15.71	15.71	9.42	9.42	2	0.07	0.01	0.07	0.00	0.00	24.0
6	330	-8266	-673	-14	0	-112	2255	15.71	15.71	9.42	9.42	2	0.06	0.01	0.06	0.00	0.00	24.0
7	330	-8200	-602	227	0	-489	2308	15.71	15.71	9.42	9.42	2	0.07	0.01	0.05	0.00	0.00	24.0
8	330	-8194	-742	2	0	-157	2327	15.71	15.71	9.42	9.42	2	0.06	0.01	0.06	0.00	0.00	24.0
9	330	-8129	-672	242	0	-534	2380	15.71	15.71	9.42	9.42	2	0.08	0.01	0.06	0.00	0.00	24.0
10	330	-8326	-567	52	0	-191	2189	15.71	15.71	9.42	9.42	2	0.06	0.01	0.05	0.00	0.00	24.0
11	330	-8307	-546	124	0	-304	2205	15.71	15.71	9.42	9.42	2	0.06	0.01	0.05	0.00	0.00	24.0
12	330	-8088	-799	105	0	-341	2430	15.71	15.71	9.42	9.42	2	0.07	0.01	0.07	0.00	0.00	24.0
13	330	-8068	-778	177	0	-454	2446	15.71	15.71	9.42	9.42	2	0.07	0.01	0.07	0.00	0.00	24.0
14	330	-8266	-673	-14	0	-112	2255	15.71	15.71	9.42	9.42	2	0.06	0.01	0.06	0.00	0.00	24.0
15	330	-8200	-602	227	0	-489	2308	15.71	15.71	9.42	9.42	2	0.07	0.01	0.05	0.00	0.00	24.0
16	330	-8194	-742	2	0	-157	2327	15.71	15.71	9.42	9.42	2	0.06	0.01	0.06	0.00	0.00	24.0
17	330	-8129	-672	242	0	-534	2380	15.71	15.71	9.42	9.42	2	0.08	0.01	0.06	0.00	0.00	24.0
18	330	-21650	-2587	238	0	-652	7246	15.71	15.71	9.42	9.42	3	0.13	0.03	0.19	0.00	0.00	24.0
19	330	-13930	-784	295	0	-866	3775	15.71	15.71	9.42	9.42	3	0.08	0.01	0.06	0.00	0.00	24.0
20	330	-16830	-1583	330	0	-951	5359	15.71	15.71	9.42	9.42	3	0.10	0.02	0.12	0.00	0.00	24.0
37	330	-21950	-2923	181	0	-470	7597	15.71	15.71	9.42	9.42	3	0.14	0.04	0.21	0.00	0.00	24.0
38	330	-9083	83	276	0	-828	1813	15.71	15.71	9.42	9.42	3	0.05	0.00	0.02	0.00	0.00	24.0
39	330	-13920	-1249	335	0	-969	4453	15.71	15.71	9.42	9.42	3	0.09	0.02	0.10	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 31 NI 120 NF 119 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 5C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-15880	-1569	49	0	-47	9639	15.71	15.71	9.42	9.42	3	0.17	0.02	0.12	0.00	0.00	24.0
2	0	-12180	-919	-20	0	-120	6078	15.71	15.71	9.42	9.42	2	0.16	0.01	0.07	0.00	0.00	24.0
3	0	-12210	-926	60	0	23	6128	15.71	15.71	9.42	9.42	2	0.15	0.01	0.07	0.00	0.00	24.0
4	0	-12220	-1489	15	0	-96	8701	15.71	15.71	9.42	9.42	2	0.22	0.02	0.12	0.00	0.00	24.0
5	0	-12260	-1495	95	0	47	8750	15.71	15.71	9.42	9.42	2	0.22	0.02	0.12	0.00	0.00	24.0
6	0	-12150	-1112	-102	0	-279	6938	15.71	15.71	9.42	9.42	2	0.18	0.01	0.09	0.00	0.00	24.0
7	0	-12270	-1132	167	0	198	7104	15.71	15.71	9.42	9.42	2	0.18	0.01	0.09	0.00	0.00	24.0
8	0	-12160	-1283	-92	0	-271	7725	15.71	15.71	9.42	9.42	2	0.20	0.02	0.10	0.00	0.00	24.0
9	0	-12290	-1303	177	0	206	7890	15.71	15.71	9.42	9.42	2	0.20	0.02	0.11	0.00	0.00	24.0
10	0	-12180	-919	-20	0	-120	6078	15.71	15.71	9.42	9.42	2	0.16	0.01	0.07	0.00	0.00	24.0
11	0	-12210	-926	60	0	23	6128	15.71	15.71	9.42	9.42	2	0.15	0.01	0.07	0.00	0.00	24.0
12	0	-12220	-1489	15	0	-96	8701	15.71	15.71	9.42	9.42	2	0.22	0.02	0.12	0.00	0.00	24.0
13	0	-12260	-1495	95	0	47	8750	15.71	15.71	9.42	9.42	2	0.22	0.02	0.12	0.00	0.00	24.0
14	0	-12150	-1112	-102	0	-279	6938	15.71	15.71	9.42	9.42	2	0.18	0.01	0.09	0.00	0.00	24.0
15	0	-12270	-1132	167	0	198	7104	15.71	15.71	9.42	9.42	2	0.18	0.01	0.09	0.00	0.00	24.0
16	0	-12160	-1283	-92	0	-271	7725	15.71	15.71	9.42	9.42	2	0.20	0.02	0.10	0.00	0.00	24.0
17	0	-12290	-1303	177	0	206	7890	15.71	15.71	9.42	9.42	2	0.20	0.02	0.11	0.00	0.00	24.0
18	0	-28160	-2045	-26	0	-231	18560	15.71	15.71	9.42	9.42	3	0.32	0.03	0.14	0.00	0.00	24.0
19	0	-20910	-4104	107	0	-87	17910	15.71	15.71	9.42	9.42	3	0.32	0.05	0.30	0.00	0.00	24.0
20	0	-23250	-2858	106	0	-77	17010	15.71	15.71	9.42	9.42	3	0.30	0.04	0.21	0.00	0.00	24.0
37	0	-27810	-868	-66	0	-242	15990	15.71	15.71	9.42	9.42	3	0.27	0.01	0.06	0.00	0.00	24.0
38	0	-15730	-4300	155	0	-1	14900	15.71	15.71	9.42	9.42	3	0.27	0.05	0.33	0.00	0.00	24.0
39	0	-19630	-2224	152	0	15	13400	15.71	15.71	9.42	9.42	3	0.24	0.03	0.17	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	83	-15022	-1569	49	0	-88	8344	15.71	15.71	9.42	9.42	3	0.15	0.02	0.12	0.00	0.00	24.0
2	83	-11519	-919	-20	0	-103	5320	15.71	15.71	9.42	9.42	2	0.14	0.01	0.07	0.00	0.00	24.0
3	83	-11551	-926	60	0	-27	5365	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
4	83	-11560	-1489	15	0	-108	7472	15.71	15.71	9.42	9.42	2	0.19	0.02	0.12	0.00	0.00	24.0
5	83	-11599	-1495	95	0	-31	7516	15.71	15.71	9.42	9.42	2	0.19	0.02	0.12	0.00	0.00	24.0
6	83	-11490	-1112	-102	0	-194	6021	15.71	15.71	9.42	9.42	2	0.16	0.01	0.09	0.00	0.00	24.0
7	83	-11610	-1132	167	0	61	6170	15.71	15.71	9.42	9.42	2	0.16	0.01	0.09	0.00	0.00	24.0
8	83	-11500	-1283	-92	0	-196	6667	15.71	15.71	9.42	9.42	2	0.17	0.02	0.10	0.00	0.00	24.0
9	83	-11629	-1303	177	0	59	6815	15.71	15.71	9.42	9.42	2	0.17	0.02	0.11	0.00	0.00	24.0
10	83	-11519	-919	-20	0	-103	5320	15.71	15.71	9.42	9.42	2	0.14	0.01	0.07	0.00	0.00	24.0

11	83	-11551	-926	60	0	-27	5365	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
12	83	-11560	-1489	15	0	-108	7472	15.71	15.71	9.42	9.42	2	0.19	0.02	0.12	0.00	0.00	24.0
13	83	-11599	-1495	95	0	-31	7516	15.71	15.71	9.42	9.42	2	0.19	0.02	0.12	0.00	0.00	24.0
14	83	-11490	-1112	-102	0	-194	6021	15.71	15.71	9.42	9.42	2	0.16	0.01	0.09	0.00	0.00	24.0
15	83	-11610	-1132	167	0	61	6170	15.71	15.71	9.42	9.42	2	0.16	0.01	0.09	0.00	0.00	24.0
16	83	-11500	-1283	-92	0	-196	6667	15.71	15.71	9.42	9.42	2	0.17	0.02	0.10	0.00	0.00	24.0
17	83	-11629	-1303	177	0	59	6815	15.71	15.71	9.42	9.42	2	0.17	0.02	0.11	0.00	0.00	24.0
18	83	-27300	-2422	-26	0	-210	16717	15.71	15.71	9.42	9.42	3	0.29	0.03	0.17	0.00	0.00	24.0
19	83	-20052	-3727	107	0	-175	14678	15.71	15.71	9.42	9.42	3	0.26	0.05	0.28	0.00	0.00	24.0
20	83	-22392	-2858	106	0	-165	14652	15.71	15.71	9.42	9.42	3	0.26	0.04	0.21	0.00	0.00	24.0
37	83	-26950	-1497	-66	0	-187	15014	15.71	15.71	9.42	9.42	3	0.26	0.02	0.10	0.00	0.00	24.0
38	83	-14872	-3672	155	0	-129	11611	15.71	15.71	9.42	9.42	3	0.21	0.05	0.29	0.00	0.00	24.0
39	83	-18772	-2224	152	0	-111	11566	15.71	15.71	9.42	9.42	3	0.21	0.03	0.17	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	165	-14165	-1569	49	0	-128	7049	15.71	15.71	9.42	9.42	3	0.13	0.02	0.12	0.00	0.00	24.0
2	165	-10858	-919	-20	0	-87	4561	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
3	165	-10892	-926	60	0	-77	4601	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
4	165	-10900	-1489	15	0	-120	6244	15.71	15.71	9.42	9.42	2	0.16	0.02	0.12	0.00	0.00	24.0
5	165	-10938	-1495	95	0	-110	6283	15.71	15.71	9.42	9.42	2	0.16	0.02	0.12	0.00	0.00	24.0
6	165	-10829	-1112	-102	0	-110	5104	15.71	15.71	9.42	9.42	2	0.13	0.01	0.09	0.00	0.00	24.0
7	165	-10951	-1132	167	0	-77	5236	15.71	15.71	9.42	9.42	2	0.13	0.01	0.09	0.00	0.00	24.0
8	165	-10840	-1283	-92	0	-120	5609	15.71	15.71	9.42	9.42	2	0.14	0.02	0.11	0.00	0.00	24.0
9	165	-10968	-1303	177	0	-87	5740	15.71	15.71	9.42	9.42	2	0.15	0.02	0.11	0.00	0.00	24.0
10	165	-10858	-919	-20	0	-87	4561	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
11	165	-10892	-926	60	0	-77	4601	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
12	165	-10900	-1489	15	0	-120	6244	15.71	15.71	9.42	9.42	2	0.16	0.02	0.12	0.00	0.00	24.0
13	165	-10938	-1495	95	0	-110	6283	15.71	15.71	9.42	9.42	2	0.16	0.02	0.12	0.00	0.00	24.0
14	165	-10829	-1112	-102	0	-110	5104	15.71	15.71	9.42	9.42	2	0.13	0.01	0.09	0.00	0.00	24.0
15	165	-10951	-1132	167	0	-77	5236	15.71	15.71	9.42	9.42	2	0.13	0.01	0.09	0.00	0.00	24.0
16	165	-10840	-1283	-92	0	-120	5609	15.71	15.71	9.42	9.42	2	0.14	0.02	0.11	0.00	0.00	24.0
17	165	-10968	-1303	177	0	-87	5740	15.71	15.71	9.42	9.42	2	0.15	0.02	0.11	0.00	0.00	24.0
18	165	-26440	-2800	-26	0	-189	14562	15.71	15.71	9.42	9.42	3	0.25	0.03	0.19	0.00	0.00	24.0
19	165	-19195	-3350	107	0	-264	11758	15.71	15.71	9.42	9.42	3	0.21	0.04	0.25	0.00	0.00	24.0
20	165	-21535	-2858	106	0	-252	12293	15.71	15.71	9.42	9.42	3	0.22	0.04	0.21	0.00	0.00	24.0
37	165	-26090	-2126	-66	0	-133	13519	15.71	15.71	9.42	9.42	3	0.23	0.03	0.15	0.00	0.00	24.0
38	165	-14015	-3043	155	0	-257	8841	15.71	15.71	9.42	9.42	3	0.16	0.04	0.24	0.00	0.00	24.0
39	165	-17915	-2224	152	0	-236	9733	15.71	15.71	9.42	9.42	3	0.17	0.03	0.17	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	248	-13308	-1569	49	0	-168	5754	15.71	15.71	9.42	9.42	3	0.11	0.02	0.13	0.00	0.00	24.0
2	248	-10197	-919	-20	0	-70	3802	15.71	15.71	9.42	9.42	2	0.10	0.01	0.08	0.00	0.00	24.0
3	248	-10232	-926	60	0	-126	3837	15.71	15.71	9.42	9.42	2	0.10	0.01	0.08	0.00	0.00	24.0
4	248	-10240	-1489	15	0	-132	5015	15.71	15.71	9.42	9.42	2	0.13	0.02	0.12	0.00	0.00	24.0
5	248	-10278	-1495	95	0	-189	5050	15.71	15.71	9.42	9.42	2	0.13	0.02	0.12	0.00	0.00	24.0
6	248	-10168	-1112	-102	0	-26	4187	15.71	15.71	9.42	9.42	2	0.11	0.01	0.09	0.00	0.00	24.0
7	248	-10292	-1132	167	0	-214	4302	15.71	15.71	9.42	9.42	2	0.11	0.01	0.09	0.00	0.00	24.0
8	248	-10181	-1283	-92	0	-44	4551	15.71	15.71	9.42	9.42	2	0.12	0.02	0.11	0.00	0.00	24.0
9	248	-10306	-1303	177	0	-233	4666	15.71	15.71	9.42	9.42	2	0.12	0.02	0.11	0.00	0.00	24.0
10	248	-10197	-919	-20	0	-70	3802	15.71	15.71	9.42	9.42	2	0.10	0.01	0.08	0.00	0.00	24.0
11	248	-10232	-926	60	0	-126	3837	15.71	15.71	9.42	9.42	2	0.10	0.01	0.08	0.00	0.00	24.0
12	248	-10240	-1489	15	0	-132	5015	15.71	15.71	9.42	9.42	2	0.13	0.02	0.12	0.00	0.00	24.0
13	248	-10278	-1495	95	0	-189	5050	15.71	15.71	9.42	9.42	2	0.13	0.02	0.12	0.00	0.00	24.0
14	248	-10168	-1112	-102	0	-26	4187	15.71	15.71	9.42	9.42	2	0.11	0.01	0.09	0.00	0.00	24.0
15	248	-10292	-1132	167	0	-214	4302	15.71	15.71	9.42	9.42	2	0.11	0.01	0.09	0.00	0.00	24.0
16	248	-10181	-1283	-92	0	-44	4551	15.71	15.71	9.42	9.42	2	0.12	0.02	0.11	0.00	0.00	24.0
17	248	-10306	-1303	177	0	-233	4666	15.71	15.71	9.42	9.42	2	0.12	0.02	0.11	0.00	0.00	24.0
18	248	-25580	-3177	-26	0	-168	12097	15.71	15.71	9.42	9.42	3	0.21	0.04	0.22	0.00	0.00	24.0
19	248	-18338	-2973	107	0	-352	9148	15.71	15.71	9.42	9.42	3	0.16	0.04	0.22	0.00	0.00	24.0
20	248	-20678	-2858	106	0	-339	9934	15.71	15.71	9.42	9.42	3	0.18	0.04	0.21	0.00	0.00	24.0
37	248	-25230	-2754	-66	0	-78	11506	15.71	15.71	9.42	9.42	3	0.20	0.03	0.19	0.00	0.00	24.0
38	248	-13158	-2414	155	0	-384	6590	15.71	15.71	9.42	9.42	3	0.12	0.03	0.19	0.00	0.00	24.0
39	248	-17058	-2224	152	0	-362	7899	15.71	15.71	9.42	9.42	3	0.14	0.03	0.17	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	330	-12450	-1569	49	0	-208	4459	15.71	15.71	9.42	9.42	3	0.08	0.02	0.13	0.00	0.00	24.0
2	330	-9536	-919	-20	0	-53	3044	15.71	15.71	9.42	9.42	2	0.08	0.01	0.08	0.00	0.00	24.0
3	330	-9573	-926	60	0	-176	3074	15.71	15.71	9.42	9.42	2	0.08	0.01	0.08	0.00	0.00	24.0
4	330	-9580	-1489	15	0	-144	3787	15.71	15.71	9.42	9.42	2	0.10	0.02	0.12	0.00	0.00	24.0
5	330	-9617	-1495	95	0	-268	3816	15.71	15.71	9.42	9.42	2	0.10	0.02	0.12	0.00	0.00	24.0
6	330	-9508	-1112	-102	0	59	3270	15.71	15.71	9.42	9.42	2	0.08	0.01	0.09	0.00	0.00	24.0
7	330	-9632	-1132	167	0	-352	3368	15.71	15.71	9.42	9.42	2	0.09	0.01	0.09	0.00	0.00	24.0
8	330	-9521	-1283	-92	0	31	3493	15.71	15.71	9.42	9.42	2	0.09	0.02	0.11	0.00	0.00	24.0
9	330	-9645	-1303	177	0	-379	3591	15.71	15.71	9.42	9.42	2	0.10	0.02	0.11	0.00	0.00	24.0
10	330	-9536	-919	-20	0	-53	3044	15.71	15.71	9.42	9.42	2	0.08	0.01	0.08	0.00	0.00	24.0
11	330	-9573	-926	60	0	-176	3074	15.71	15.71	9.42	9.42	2	0.08	0.01	0.08	0.00	0.00	24.0
12	330	-9580	-1489	15	0	-144	3787	15.71	15.71	9.42	9.42	2	0.10	0.02	0.12	0.00	0.00	24.0
13	330	-9617	-1495	95	0	-268	3816	15.71	15.71	9.42	9.42	2	0.10	0.02	0.12	0.00	0.00	24.0
14	330	-9508	-1112	-102	0	59	3270	15.71	15.71	9.42	9.42	2	0.08	0.01	0.09	0.00	0.00	24.0
15	330	-9632	-1132	167	0	-352	3368	15.71	15.71	9.42	9.42	2	0.09	0.01	0.09	0.00	0.00	24.0
16	330	-9521	-1283	-92	0	31	3493	15.71	15.71	9.42	9.42	2	0.09	0.02	0.11	0.00	0.00	24.0
17	330	-9645	-1303	177	0	-379	3591	15.71	15.71	9.42	9.42	2	0.10	0.02	0.11	0.00	0.00	24.0
18	330	-24720	-3554	-26	0	-147	9320	15.71	15.71	9.42	9.42	3	0.16	0.04	0.25	0.00	0.00	24.0
19	330	-17480	-2596	107	0	-440	6850	15.71	15.71	9.42	9.42	3	0.12	0.03	0.20	0.00	0.00	24.0
20	330	-19820	-2858	106	0	-426	7576	15.71	15.71	9.42	9.42	3	0.14	0.04	0.21	0.00	0.00	24.0
37	330	-24370	-3383	-66	0	-23	8974	15.71	15.71	9.42	9.42	3	0.16	0.04	0.24	0.00	0.00	24.0
38	330	-12300	-1786	155	0	-512	4857	15.71	15.71	9.42	9.42	3	0.09	0.02	0.14	0.00	0.00	24.0
39	330	-16200	-2224	152	0	-488	6066	15.71	15.71	9.42	9.42	3	0.11	0.03	0.17	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 32 NI 163 NF 162 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 4C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-16000	-1695	-138	0	-196	10120	15.71	15.71	9.42	9.42	3	0.18	0.02	0.13	0.00	0.00	24.0
2	0	-12340	-1005	-141	0	-230	6466	15.71	15.71	9.42	9.42	2	0.17	0.01	0.08	0.00	0.00	24.0
3	0	-12310	-990	-54	0	-68	6386	15.71	15.71	9.42	9.42	2	0.16	0.01	0.08	0.00	0.00	24.0
4	0	-12300	-1617	-158	0	-234	9183	15.71	15.71	9.42	9.42	2	0.24	0.02	0.13	0.00	0.00	24.0
5	0	-12260	-1602	-71	0	-72	9102	15.71	15.71	9.42	9.42	2	0.23	0.02	0.13	0.00	0.00	24.0
6	0	-12370	-1236	-249	0	-420	7511	15.71	15.71	9.42	9.42	2	0.20	0.02	0.10	0.00	0.00	24.0

7	0	-12250	-1187	41	0	119	7243	15.71	15.71	9.42	9.42	2	0.18	0.02	0.10	0.00	0.00	24.0
8	0	-12360	-1420	-254	0	-421	8326	15.71	15.71	9.42	9.42	2	0.22	0.02	0.11	0.00	0.00	24.0
9	0	-12240	-1371	36	0	118	8058	15.71	15.71	9.42	9.42	2	0.20	0.02	0.11	0.00	0.00	24.0
10	0	-12340	-1005	-141	0	-230	6466	15.71	15.71	9.42	9.42	2	0.17	0.01	0.08	0.00	0.00	24.0
11	0	-12310	-990	-54	0	-68	6386	15.71	15.71	9.42	9.42	2	0.16	0.01	0.08	0.00	0.00	24.0
12	0	-12300	-1617	-158	0	-234	9183	15.71	15.71	9.42	9.42	2	0.24	0.02	0.13	0.00	0.00	24.0
13	0	-12260	-1602	-71	0	-72	9102	15.71	15.71	9.42	9.42	2	0.23	0.02	0.13	0.00	0.00	24.0
14	0	-12370	-1236	-249	0	-420	7511	15.71	15.71	9.42	9.42	2	0.20	0.02	0.10	0.00	0.00	24.0
15	0	-12250	-1187	41	0	119	7243	15.71	15.71	9.42	9.42	2	0.18	0.02	0.10	0.00	0.00	24.0
16	0	-12360	-1420	-254	0	-421	8326	15.71	15.71	9.42	9.42	2	0.22	0.02	0.11	0.00	0.00	24.0
17	0	-12240	-1371	36	0	118	8058	15.71	15.71	9.42	9.42	2	0.20	0.02	0.11	0.00	0.00	24.0
18	0	-28510	-2237	-360	0	-538	19390	15.71	15.71	9.42	9.42	3	0.33	0.03	0.15	0.00	0.00	24.0
19	0	-20970	-4397	-302	0	-394	18910	15.71	15.71	9.42	9.42	3	0.33	0.06	0.32	0.00	0.00	24.0
20	0	-23310	-3040	-205	0	-300	17610	15.71	15.71	9.42	9.42	3	0.31	0.04	0.22	0.00	0.00	24.0
37	0	-28230	-988	-316	0	-498	16620	15.71	15.71	9.42	9.42	3	0.29	0.01	0.07	0.00	0.00	24.0
38	0	-15670	-4588	-219	0	-257	15820	15.71	15.71	9.42	9.42	3	0.29	0.06	0.36	0.00	0.00	24.0
39	0	-19550	-2326	-57	0	-100	13640	15.71	15.71	9.42	9.42	3	0.24	0.03	0.17	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	83	-15140	-1695	-138	0	-82	8722	15.71	15.71	9.42	9.42	3	0.16	0.02	0.13	0.00	0.00	24.0
2	83	-11681	-1005	-141	0	-114	5637	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
3	83	-11650	-990	-54	0	-24	5569	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
4	83	-11640	-1617	-158	0	-103	7849	15.71	15.71	9.42	9.42	2	0.20	0.02	0.13	0.00	0.00	24.0
5	83	-11601	-1602	-71	0	-13	7780	15.71	15.71	9.42	9.42	2	0.20	0.02	0.13	0.00	0.00	24.0
6	83	-11710	-1236	-249	0	-215	6491	15.71	15.71	9.42	9.42	2	0.17	0.02	0.10	0.00	0.00	24.0
7	83	-11591	-1187	41	0	85	6263	15.71	15.71	9.42	9.42	2	0.16	0.02	0.10	0.00	0.00	24.0
8	83	-11699	-1420	-254	0	-212	7155	15.71	15.71	9.42	9.42	2	0.19	0.02	0.12	0.00	0.00	24.0
9	83	-11580	-1371	36	0	88	6927	15.71	15.71	9.42	9.42	2	0.18	0.02	0.11	0.00	0.00	24.0
10	83	-11681	-1005	-141	0	-114	5637	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
11	83	-11650	-990	-54	0	-24	5569	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
12	83	-11640	-1617	-158	0	-103	7849	15.71	15.71	9.42	9.42	2	0.20	0.02	0.13	0.00	0.00	24.0
13	83	-11601	-1602	-71	0	-13	7780	15.71	15.71	9.42	9.42	2	0.20	0.02	0.13	0.00	0.00	24.0
14	83	-11710	-1236	-249	0	-215	6491	15.71	15.71	9.42	9.42	2	0.17	0.02	0.10	0.00	0.00	24.0
15	83	-11591	-1187	41	0	85	6263	15.71	15.71	9.42	9.42	2	0.16	0.02	0.10	0.00	0.00	24.0
16	83	-11699	-1420	-254	0	-212	7155	15.71	15.71	9.42	9.42	2	0.19	0.02	0.12	0.00	0.00	24.0
17	83	-11580	-1371	36	0	88	6927	15.71	15.71	9.42	9.42	2	0.18	0.02	0.11	0.00	0.00	24.0
18	83	-27652	-2614	-360	0	-241	17390	15.71	15.71	9.42	9.42	3	0.30	0.03	0.18	0.00	0.00	24.0
19	83	-20112	-4020	-302	0	-145	15438	15.71	15.71	9.42	9.42	3	0.27	0.05	0.30	0.00	0.00	24.0
20	83	-22450	-3040	-205	0	-131	15101	15.71	15.71	9.42	9.42	3	0.26	0.04	0.22	0.00	0.00	24.0
37	83	-27372	-1617	-316	0	-237	15546	15.71	15.71	9.42	9.42	3	0.27	0.02	0.11	0.00	0.00	24.0
38	83	-14810	-3960	-219	0	-77	12293	15.71	15.71	9.42	9.42	3	0.22	0.05	0.31	0.00	0.00	24.0
39	83	-18692	-2326	-57	0	-53	11721	15.71	15.71	9.42	9.42	3	0.21	0.03	0.17	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	165	-14280	-1695	-138	0	32	7324	15.71	15.71	9.42	9.42	3	0.13	0.02	0.13	0.00	0.00	24.0
2	165	-11022	-1005	-141	0	3	4808	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
3	165	-10990	-990	-54	0	21	4752	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
4	165	-10980	-1617	-158	0	28	6515	15.71	15.71	9.42	9.42	2	0.17	0.02	0.13	0.00	0.00	24.0
5	165	-10942	-1602	-71	0	46	6458	15.71	15.71	9.42	9.42	2	0.16	0.02	0.13	0.00	0.00	24.0
6	165	-11050	-1236	-249	0	-10	5471	15.71	15.71	9.42	9.42	2	0.14	0.02	0.10	0.00	0.00	24.0
7	165	-10932	-1187	41	0	51	5284	15.71	15.71	9.42	9.42	2	0.13	0.02	0.10	0.00	0.00	24.0
8	165	-11038	-1420	-254	0	-3	5984	15.71	15.71	9.42	9.42	2	0.15	0.02	0.12	0.00	0.00	24.0
9	165	-10920	-1371	36	0	59	5796	15.71	15.71	9.42	9.42	2	0.15	0.02	0.11	0.00	0.00	24.0
10	165	-11022	-1005	-141	0	3	4808	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
11	165	-10990	-990	-54	0	21	4752	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
12	165	-10980	-1617	-158	0	28	6515	15.71	15.71	9.42	9.42	2	0.17	0.02	0.13	0.00	0.00	24.0
13	165	-10942	-1602	-71	0	46	6458	15.71	15.71	9.42	9.42	2	0.16	0.02	0.13	0.00	0.00	24.0
14	165	-11050	-1236	-249	0	-10	5471	15.71	15.71	9.42	9.42	2	0.14	0.02	0.10	0.00	0.00	24.0
15	165	-10932	-1187	41	0	51	5284	15.71	15.71	9.42	9.42	2	0.13	0.02	0.10	0.00	0.00	24.0
16	165	-11038	-1420	-254	0	-3	5984	15.71	15.71	9.42	9.42	2	0.15	0.02	0.12	0.00	0.00	24.0
17	165	-10920	-1371	36	0	59	5796	15.71	15.71	9.42	9.42	2	0.15	0.02	0.11	0.00	0.00	24.0
18	165	-26795	-2991	-360	0	56	15078	15.71	15.71	9.42	9.42	3	0.26	0.04	0.21	0.00	0.00	24.0
19	165	-19255	-3642	-302	0	104	12277	15.71	15.71	9.42	9.42	3	0.22	0.05	0.27	0.00	0.00	24.0
20	165	-21590	-3040	-205	0	38	12592	15.71	15.71	9.42	9.42	3	0.22	0.04	0.22	0.00	0.00	24.0
37	165	-26515	-2246	-316	0	24	13953	15.71	15.71	9.42	9.42	3	0.24	0.03	0.16	0.00	0.00	24.0
38	165	-13950	-3331	-219	0	104	9285	15.71	15.71	9.42	9.42	3	0.17	0.04	0.26	0.00	0.00	24.0
39	165	-17835	-2326	-57	0	-6	9803	15.71	15.71	9.42	9.42	3	0.17	0.03	0.18	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	248	-13420	-1695	-138	0	146	5926	15.71	15.71	9.42	9.42	3	0.11	0.02	0.13	0.00	0.00	24.0
2	248	-10363	-1005	-141	0	119	3979	15.71	15.71	9.42	9.42	2	0.10	0.01	0.08	0.00	0.00	24.0
3	248	-10329	-990	-54	0	66	3935	15.71	15.71	9.42	9.42	2	0.10	0.01	0.08	0.00	0.00	24.0
4	248	-10319	-1617	-158	0	158	5182	15.71	15.71	9.42	9.42	2	0.14	0.02	0.13	0.00	0.00	24.0
5	248	-10283	-1602	-71	0	105	5137	15.71	15.71	9.42	9.42	2	0.13	0.02	0.13	0.00	0.00	24.0
6	248	-10389	-1236	-249	0	195	4452	15.71	15.71	9.42	9.42	2	0.12	0.02	0.10	0.00	0.00	24.0
7	248	-10272	-1187	41	0	17	4304	15.71	15.71	9.42	9.42	2	0.11	0.02	0.10	0.00	0.00	24.0
8	248	-10377	-1420	-254	0	207	4812	15.71	15.71	9.42	9.42	2	0.13	0.02	0.12	0.00	0.00	24.0
9	248	-10259	-1371	36	0	29	4665	15.71	15.71	9.42	9.42	2	0.12	0.02	0.11	0.00	0.00	24.0
10	248	-10363	-1005	-141	0	119	3979	15.71	15.71	9.42	9.42	2	0.10	0.01	0.08	0.00	0.00	24.0
11	248	-10329	-990	-54	0	66	3935	15.71	15.71	9.42	9.42	2	0.10	0.01	0.08	0.00	0.00	24.0
12	248	-10319	-1617	-158	0	158	5182	15.71	15.71	9.42	9.42	2	0.14	0.02	0.13	0.00	0.00	24.0
13	248	-10283	-1602	-71	0	105	5137	15.71	15.71	9.42	9.42	2	0.13	0.02	0.13	0.00	0.00	24.0
14	248	-10389	-1236	-249	0	195	4452	15.71	15.71	9.42	9.42	2	0.12	0.02	0.10	0.00	0.00	24.0
15	248	-10272	-1187	41	0	17	4304	15.71	15.71	9.42	9.42	2	0.11	0.02	0.10	0.00	0.00	24.0
16	248	-10377	-1420	-254	0	207	4812	15.71	15.71	9.42	9.42	2	0.13	0.02	0.12	0.00	0.00	24.0
17	248	-10259	-1371	36	0	29	4665	15.71	15.71	9.42	9.42	2	0.12	0.02	0.11	0.00	0.00	24.0
18	248	-25938	-3368	-360	0	353	12455	15.71	15.71	9.42	9.42	3	0.22	0.04	0.24	0.00	0.00	24.0
19	248	-18398	-3265	-302	0	353	9427	15.71	15.71	9.42	9.42	3	0.17	0.04	0.25	0.00	0.00	24.0
20	248	-20730	-3040	-205	0	207	10083	15.71	15.71	9.42	9.42	3	0.18	0.04	0.22	0.00	0.00	24.0
37	248	-25658	-2874	-316	0	285	11841	15.71	15.71	9.42	9.42	3	0.21	0.04	0.20	0.00	0.00	24.0
38	248	-13090	-2702	-219	0	284	6795	15.71	15.71	9.42	9.42	3	0.12	0.03	0.22	0.00	0.00	24.0
39	248	-16978	-2326	-57	0	41	7884	15.71	15.71	9.42	9.42	3	0.14	0.03	0.18	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	330	-12560	-1695	-138	0	260	4528	15.71	15.71	9.42	9.42	3	0.08	0.02	0.14	0.00	0.00	24.0
2	330	-9704	-1005	-141	0	236	3150	15.71	15.71	9.42	9.42	2	0.09	0.01	0.08	0.00	0.00	24.0
3	330	-9669	-990	-54	0	110	3118	15.71	15.71	9.42	9.42	2	0.08	0.01	0.08	0.00	0.00	24.0
4	330	-9659	-1617	-158	0	289	3848	15.71	15.71	9.42	9.42	2	0.11	0.02	0.13	0.00	0.00	24.0
5	330	-9624	-1602	-71	0	164	3815	15.71	15.71	9.42	9.42	2	0.10	0.02	0.13	0.00	0.00	24.0
6	330	-9729	-1236	-249	0	400	3432	15.71	15.71	9.42	9.42	2	0.10	0.02	0.10	0.00	0.00	24.0
7	330	-9613	-1187	41	0	-17	3324	15.71	15.71	9.42	9.42	2	0.09	0.02	0.10	0.00	0.00	24.0
8	330	-9716	-1420	-254	0	416	3641	15.71	15.71	9.42	9.42	2	0.10	0.02	0.12	0.00	0.00	24.0
9	330	-9599	-1371	36	0	-1	3534	15.71	15.71	9.42	9.42	2	0.09	0.02	0.11	0.00	0.00	24.0
10	330	-9704	-1005	-141	0	236	3150	15.71	15.71	9.42	9.42	2	0.09	0.01	0.08	0.00	0.00	24.0
11	330	-9669	-990	-54	0	110	3118	15.71	15.71	9.42	9.42	2	0.08	0.01	0.08	0.00	0.00	24.0
12	330	-9659	-1617	-158	0	289	3848	15.71	15.71	9.42	9.42	2	0.11	0.02	0.13	0.00	0.00	24.0

13	330	-9624	-1602	-71	0	164	3815	15.71	15.71	9.42	9.42	2	0.10	0.02	0.13	0.00	0.00	24.0
14	330	-9729	-1236	-249	0	400	3432	15.71	15.71	9.42	9.42	2	0.10	0.02	0.10	0.00	0.00	24.0
15	330	-9613	-1187	41	0	-17	3324	15.71	15.71	9.42	9.42	2	0.09	0.02	0.10	0.00	0.00	24.0
16	330	-9716	-1420	-254	0	416	3641	15.71	15.71	9.42	9.42	2	0.10	0.02	0.12	0.00	0.00	24.0
17	330	-9599	-1371	36	0	-1	3534	15.71	15.71	9.42	9.42	2	0.09	0.02	0.11	0.00	0.00	24.0
18	330	-25080	-3745	-360	0	651	9521	15.71	15.71	9.42	9.42	3	0.17	0.05	0.26	0.00	0.00	24.0
19	330	-17540	-2888	-302	0	602	6889	15.71	15.71	9.42	9.42	3	0.13	0.04	0.22	0.00	0.00	24.0
20	330	-19870	-3040	-205	0	376	7574	15.71	15.71	9.42	9.42	3	0.14	0.04	0.23	0.00	0.00	24.0
37	330	-24800	-3503	-316	0	546	9211	15.71	15.71	9.42	9.42	3	0.16	0.04	0.25	0.00	0.00	24.0
38	330	-12230	-2074	-219	0	464	4824	15.71	15.71	9.42	9.42	3	0.09	0.03	0.17	0.00	0.00	24.0
39	330	-16120	-2326	-57	0	88	5966	15.71	15.71	9.42	9.42	3	0.11	0.03	0.18	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 33 NI 206 NF 205 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 3C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-15680	-1547	-227	0	-271	9453	15.71	15.71	9.42	9.42	3	0.17	0.02	0.12	0.00	0.00	24.0
2	0	-12060	-883	-214	0	-307	5873	15.71	15.71	9.42	9.42	2	0.15	0.01	0.07	0.00	0.00	24.0
3	0	-12070	-884	-106	0	-117	5879	15.71	15.71	9.42	9.42	2	0.15	0.01	0.07	0.00	0.00	24.0
4	0	-12060	-1497	-243	0	-301	8663	15.71	15.71	9.42	9.42	2	0.22	0.02	0.12	0.00	0.00	24.0
5	0	-12070	-1498	-136	0	-111	8669	15.71	15.71	9.42	9.42	2	0.22	0.02	0.12	0.00	0.00	24.0
6	0	-12060	-1097	-349	0	-526	6843	15.71	15.71	9.42	9.42	2	0.18	0.01	0.09	0.00	0.00	24.0
7	0	-12070	-1100	8	0	107	6863	15.71	15.71	9.42	9.42	2	0.17	0.01	0.09	0.00	0.00	24.0
8	0	-12060	-1281	-358	0	-524	7680	15.71	15.71	9.42	9.42	2	0.21	0.02	0.10	0.00	0.00	24.0
9	0	-12070	-1284	-1	0	109	7700	15.71	15.71	9.42	9.42	2	0.20	0.02	0.10	0.00	0.00	24.0
10	0	-12060	-883	-214	0	-307	5873	15.71	15.71	9.42	9.42	2	0.15	0.01	0.07	0.00	0.00	24.0
11	0	-12070	-884	-106	0	-117	5879	15.71	15.71	9.42	9.42	2	0.15	0.01	0.07	0.00	0.00	24.0
12	0	-12060	-1497	-243	0	-301	8663	15.71	15.71	9.42	9.42	2	0.22	0.02	0.12	0.00	0.00	24.0
13	0	-12070	-1498	-136	0	-111	8669	15.71	15.71	9.42	9.42	2	0.22	0.02	0.12	0.00	0.00	24.0
14	0	-12060	-1097	-349	0	-526	6843	15.71	15.71	9.42	9.42	2	0.18	0.01	0.09	0.00	0.00	24.0
15	0	-12070	-1100	8	0	107	6863	15.71	15.71	9.42	9.42	2	0.17	0.01	0.09	0.00	0.00	24.0
16	0	-12060	-1281	-358	0	-524	7680	15.71	15.71	9.42	9.42	2	0.21	0.02	0.10	0.00	0.00	24.0
17	0	-12070	-1284	-1	0	109	7700	15.71	15.71	9.42	9.42	2	0.20	0.02	0.10	0.00	0.00	24.0
18	0	-27920	-1959	-541	0	-768	18040	15.71	15.71	9.42	9.42	3	0.31	0.02	0.13	0.00	0.00	24.0
19	0	-20530	-4131	-483	0	-526	17830	15.71	15.71	9.42	9.42	3	0.32	0.05	0.30	0.00	0.00	24.0
20	0	-22910	-2821	-323	0	-398	16650	15.71	15.71	9.42	9.42	3	0.29	0.04	0.20	0.00	0.00	24.0
37	0	-27660	-746	-467	0	-726	15360	15.71	15.71	9.42	9.42	3	0.27	0.01	0.05	0.00	0.00	24.0
38	0	-15340	-4367	-370	0	-321	15000	15.71	15.71	9.42	9.42	3	0.27	0.06	0.34	0.00	0.00	24.0
39	0	-19310	-2183	-104	0	-108	13050	15.71	15.71	9.42	9.42	3	0.23	0.03	0.16	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	83	-14822	-1547	-227	0	-84	8176	15.71	15.71	9.42	9.42	3	0.15	0.02	0.12	0.00	0.00	24.0
2	83	-11400	-883	-214	0	-130	5144	15.71	15.71	9.42	9.42	2	0.13	0.01	0.07	0.00	0.00	24.0
3	83	-11409	-884	-106	0	-29	5150	15.71	15.71	9.42	9.42	2	0.13	0.01	0.07	0.00	0.00	24.0
4	83	-11401	-1497	-243	0	-100	7429	15.71	15.71	9.42	9.42	2	0.19	0.02	0.12	0.00	0.00	24.0
5	83	-11410	-1498	-136	0	1	7434	15.71	15.71	9.42	9.42	2	0.19	0.02	0.12	0.00	0.00	24.0
6	83	-11399	-1097	-349	0	-238	5938	15.71	15.71	9.42	9.42	2	0.16	0.01	0.09	0.00	0.00	24.0
7	83	-11411	-1100	8	0	100	5956	15.71	15.71	9.42	9.42	2	0.15	0.01	0.09	0.00	0.00	24.0
8	83	-11399	-1281	-358	0	-229	6623	15.71	15.71	9.42	9.42	2	0.17	0.02	0.10	0.00	0.00	24.0
9	83	-11411	-1284	-1	0	109	6641	15.71	15.71	9.42	9.42	2	0.17	0.02	0.10	0.00	0.00	24.0
10	83	-11400	-883	-214	0	-130	5144	15.71	15.71	9.42	9.42	2	0.13	0.01	0.07	0.00	0.00	24.0
11	83	-11409	-884	-106	0	-29	5150	15.71	15.71	9.42	9.42	2	0.13	0.01	0.07	0.00	0.00	24.0
12	83	-11401	-1497	-243	0	-100	7429	15.71	15.71	9.42	9.42	2	0.19	0.02	0.12	0.00	0.00	24.0
13	83	-11410	-1498	-136	0	1	7434	15.71	15.71	9.42	9.42	2	0.19	0.02	0.12	0.00	0.00	24.0
14	83	-11399	-1097	-349	0	-238	5938	15.71	15.71	9.42	9.42	2	0.16	0.01	0.09	0.00	0.00	24.0
15	83	-11411	-1100	8	0	100	5956	15.71	15.71	9.42	9.42	2	0.15	0.01	0.09	0.00	0.00	24.0
16	83	-11399	-1281	-358	0	-229	6623	15.71	15.71	9.42	9.42	2	0.17	0.02	0.10	0.00	0.00	24.0
17	83	-11411	-1284	-1	0	109	6641	15.71	15.71	9.42	9.42	2	0.17	0.02	0.10	0.00	0.00	24.0
18	83	-27062	-2336	-541	0	-322	16268	15.71	15.71	9.42	9.42	3	0.28	0.03	0.16	0.00	0.00	24.0
19	83	-19672	-3754	-483	0	-127	14576	15.71	15.71	9.42	9.42	3	0.26	0.05	0.28	0.00	0.00	24.0
20	83	-22052	-2821	-323	0	-131	14324	15.71	15.71	9.42	9.42	3	0.25	0.04	0.20	0.00	0.00	24.0
37	83	-26800	-1375	-467	0	-341	14484	15.71	15.71	9.42	9.42	3	0.25	0.02	0.10	0.00	0.00	24.0
38	83	-14482	-3738	-370	0	-16	11657	15.71	15.71	9.42	9.42	3	0.21	0.05	0.29	0.00	0.00	24.0
39	83	-18452	-2183	-104	0	-22	11248	15.71	15.71	9.42	9.42	3	0.20	0.03	0.16	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	165	-13965	-1547	-227	0	104	6900	15.71	15.71	9.42	9.42	3	0.13	0.02	0.12	0.00	0.00	24.0
2	165	-10740	-883	-214	0	46	4416	15.71	15.71	9.42	9.42	2	0.11	0.01	0.07	0.00	0.00	24.0
3	165	-10748	-884	-106	0	59	4420	15.71	15.71	9.42	9.42	2	0.11	0.01	0.07	0.00	0.00	24.0
4	165	-10742	-1497	-243	0	101	6194	15.71	15.71	9.42	9.42	2	0.16	0.02	0.12	0.00	0.00	24.0
5	165	-10750	-1498	-136	0	114	6199	15.71	15.71	9.42	9.42	2	0.16	0.02	0.12	0.00	0.00	24.0
6	165	-10738	-1097	-349	0	50	5033	15.71	15.71	9.42	9.42	2	0.13	0.01	0.09	0.00	0.00	24.0
7	165	-10752	-1100	8	0	93	5048	15.71	15.71	9.42	9.42	2	0.13	0.01	0.09	0.00	0.00	24.0
8	165	-10738	-1281	-358	0	66	5566	15.71	15.71	9.42	9.42	2	0.14	0.02	0.11	0.00	0.00	24.0
9	165	-10752	-1284	-1	0	110	5582	15.71	15.71	9.42	9.42	2	0.14	0.02	0.11	0.00	0.00	24.0
10	165	-10740	-883	-214	0	46	4416	15.71	15.71	9.42	9.42	2	0.11	0.01	0.07	0.00	0.00	24.0
11	165	-10748	-884	-106	0	59	4420	15.71	15.71	9.42	9.42	2	0.11	0.01	0.07	0.00	0.00	24.0
12	165	-10742	-1497	-243	0	101	6194	15.71	15.71	9.42	9.42	2	0.16	0.02	0.12	0.00	0.00	24.0
13	165	-10750	-1498	-136	0	114	6199	15.71	15.71	9.42	9.42	2	0.16	0.02	0.12	0.00	0.00	24.0
14	165	-10738	-1097	-349	0	50	5033	15.71	15.71	9.42	9.42	2	0.13	0.01	0.09	0.00	0.00	24.0
15	165	-10752	-1100	8	0	93	5048	15.71	15.71	9.42	9.42	2	0.13	0.01	0.09	0.00	0.00	24.0
16	165	-10738	-1281	-358	0	66	5566	15.71	15.71	9.42	9.42	2	0.14	0.02	0.11	0.00	0.00	24.0
17	165	-10752	-1284	-1	0	110	5582	15.71	15.71	9.42	9.42	2	0.14	0.02	0.11	0.00	0.00	24.0
18	165	-26205	-2714	-541	0	124	14185	15.71	15.71	9.42	9.42	3	0.24	0.03	0.19	0.00	0.00	24.0
19	165	-18815	-3376	-483	0	271	11634	15.71	15.71	9.42	9.42	3	0.21	0.04	0.25	0.00	0.00	24.0
20	165	-21195	-2821	-323	0	136	11997	15.71	15.71	9.42	9.42	3	0.21	0.04	0.21	0.00	0.00	24.0
37	165	-25940	-2004	-467	0	45	13090	15.71	15.71	9.42	9.42	3	0.23	0.02	0.14	0.00	0.00	24.0
38	165	-13625	-3110	-370	0	289	8832	15.71	15.71	9.42	9.42	3	0.16	0.04	0.25	0.00	0.00	24.0
39	165	-17595	-2183	-104	0	64	9447	15.71	15.71	9.42	9.42	3	0.17	0.03	0.17	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	248	-13108	-1547	-227	0	291	5624	15.71	15.71	9.42	9.42	3	0.10	0.02	0.12	0.00	0.00	24.0
2	248	-10081	-883	-214	0	222	3687	15.71	15.71	9.42	9.42	2	0.10	0.01	0.07	0.00	0.00	24.0
3	248	-10087	-884	-106	0	146	3691	15.71	15.71	9.42	9.42	2	0.10	0.01	0.07	0.00	0.00	24.0
4	248	-10083	-1497	-243	0	301	4960	15.71	15.71	9.42	9.42	2	0.13	0.02	0.12	0.00	0.00	24.0
5	248	-10090	-1498	-136	0	226	4963	15.71	15.71	9.42	9.42	2	0.13	0.02	0.12	0.00	0.00	24.0
6	248	-10077	-1097	-349	0	338	4129	15.71	15.71	9.42	9.42	2	0.11	0.01	0.09	0.00	0.00	24.0
7	248	-10092	-1100	8	0	86	4141	15.71	15.71	9.42	9.42	2	0.11	0.01	0.09	0.00	0.00	24.0
8	248	-10078	-1281	-358	0	362	4510	15.71	15.71	9.42	9.42	2	0.12	0.02	0.11	0.00	0.00	24.0

9	248	-10093	-1284	-1	0	110	4522	15.71	15.71	9.42	9.42	2	0.12	0.02	0.11	0.00	0.00	24.0
10	248	-10081	-883	-214	0	222	3687	15.71	15.71	9.42	9.42	2	0.10	0.01	0.07	0.00	0.00	24.0
11	248	-10087	-884	-106	0	146	3691	15.71	15.71	9.42	9.42	2	0.10	0.01	0.07	0.00	0.00	24.0
12	248	-10083	-1497	-243	0	301	4960	15.71	15.71	9.42	9.42	2	0.13	0.02	0.12	0.00	0.00	24.0
13	248	-10090	-1498	-136	0	226	4963	15.71	15.71	9.42	9.42	2	0.13	0.02	0.12	0.00	0.00	24.0
14	248	-10077	-1097	-349	0	338	4129	15.71	15.71	9.42	9.42	2	0.11	0.01	0.09	0.00	0.00	24.0
15	248	-10092	-1100	8	0	86	4141	15.71	15.71	9.42	9.42	2	0.11	0.01	0.09	0.00	0.00	24.0
16	248	-10078	-1281	-358	0	362	4510	15.71	15.71	9.42	9.42	2	0.12	0.02	0.11	0.00	0.00	24.0
17	248	-10093	-1284	-1	0	110	4522	15.71	15.71	9.42	9.42	2	0.12	0.02	0.11	0.00	0.00	24.0
18	248	-25348	-3091	-541	0	571	11791	15.71	15.71	9.42	9.42	3	0.21	0.04	0.22	0.00	0.00	24.0
19	248	-17958	-2999	-483	0	669	9002	15.71	15.71	9.42	9.42	3	0.16	0.04	0.23	0.00	0.00	24.0
20	248	-20338	-2821	-323	0	402	9670	15.71	15.71	9.42	9.42	3	0.17	0.04	0.21	0.00	0.00	24.0
37	248	-25080	-2632	-467	0	430	11177	15.71	15.71	9.42	9.42	3	0.20	0.03	0.19	0.00	0.00	24.0
38	248	-12768	-2482	-370	0	594	6526	15.71	15.71	9.42	9.42	3	0.12	0.03	0.20	0.00	0.00	24.0
39	248	-16738	-2183	-104	0	150	7645	15.71	15.71	9.42	9.42	3	0.14	0.03	0.17	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	330	-12250	-1547	-227	0	479	4347	15.71	15.71	9.42	9.42	3	0.08	0.02	0.12	0.00	0.00	24.0
2	330	-9421	-883	-214	0	398	2959	15.71	15.71	9.42	9.42	2	0.09	0.01	0.07	0.00	0.00	24.0
3	330	-9426	-884	-106	0	234	2962	15.71	15.71	9.42	9.42	2	0.08	0.01	0.07	0.00	0.00	24.0
4	330	-9424	-1497	-243	0	502	3725	15.71	15.71	9.42	9.42	2	0.11	0.02	0.12	0.00	0.00	24.0
5	330	-9430	-1498	-136	0	338	3728	15.71	15.71	9.42	9.42	2	0.10	0.02	0.12	0.00	0.00	24.0
6	330	-9416	-1097	-349	0	626	3224	15.71	15.71	9.42	9.42	2	0.10	0.01	0.09	0.00	0.00	24.0
7	330	-9433	-1100	8	0	79	3234	15.71	15.71	9.42	9.42	2	0.08	0.01	0.09	0.00	0.00	24.0
8	330	-9417	-1281	-358	0	657	3453	15.71	15.71	9.42	9.42	2	0.11	0.02	0.11	0.00	0.00	24.0
9	330	-9434	-1284	-1	0	110	3463	15.71	15.71	9.42	9.42	2	0.09	0.02	0.11	0.00	0.00	24.0
10	330	-9421	-883	-214	0	398	2959	15.71	15.71	9.42	9.42	2	0.09	0.01	0.07	0.00	0.00	24.0
11	330	-9426	-884	-106	0	234	2962	15.71	15.71	9.42	9.42	2	0.08	0.01	0.07	0.00	0.00	24.0
12	330	-9424	-1497	-243	0	502	3725	15.71	15.71	9.42	9.42	2	0.11	0.02	0.12	0.00	0.00	24.0
13	330	-9430	-1498	-136	0	338	3728	15.71	15.71	9.42	9.42	2	0.10	0.02	0.12	0.00	0.00	24.0
14	330	-9416	-1097	-349	0	626	3224	15.71	15.71	9.42	9.42	2	0.10	0.01	0.09	0.00	0.00	24.0
15	330	-9433	-1100	8	0	79	3234	15.71	15.71	9.42	9.42	2	0.08	0.01	0.09	0.00	0.00	24.0
16	330	-9417	-1281	-358	0	657	3453	15.71	15.71	9.42	9.42	2	0.11	0.02	0.11	0.00	0.00	24.0
17	330	-9434	-1284	-1	0	110	3463	15.71	15.71	9.42	9.42	2	0.09	0.02	0.11	0.00	0.00	24.0
18	330	-24490	-3468	-541	0	1017	9085	15.71	15.71	9.42	9.42	3	0.16	0.04	0.25	0.00	0.00	24.0
19	330	-17100	-2622	-483	0	1067	6682	15.71	15.71	9.42	9.42	3	0.13	0.03	0.20	0.00	0.00	24.0
20	330	-19480	-2821	-323	0	669	7344	15.71	15.71	9.42	9.42	3	0.13	0.04	0.21	0.00	0.00	24.0
37	330	-24220	-3261	-467	0	815	8745	15.71	15.71	9.42	9.42	3	0.16	0.04	0.23	0.00	0.00	24.0
38	330	-11910	-1853	-370	0	900	4739	15.71	15.71	9.42	9.42	3	0.10	0.02	0.15	0.00	0.00	24.0
39	330	-15880	-2183	-104	0	236	5843	15.71	15.71	9.42	9.42	3	0.11	0.03	0.17	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 34 NI 249 NF 248 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 2C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza			aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx		cmq/m		cm
1	0	-14490	-884	-442	0	-381	6441	15.71	15.71	9.42	9.42	3	0.12	0.01	0.07	0.00	0.00	24.0
2	0	-11180	-432	-378	0	-401	3857	15.71	15.71	9.42	9.42	2	0.11	0.01	0.04	0.00	0.00	24.0
3	0	-11240	-452	-280	0	-209	3962	15.71	15.71	9.42	9.42	2	0.10	0.01	0.04	0.00	0.00	24.0
4	0	-11060	-907	-400	0	-377	5947	15.71	15.71	9.42	9.42	2	0.16	0.01	0.07	0.00	0.00	24.0
5	0	-11120	-927	-302	0	-186	6052	15.71	15.71	9.42	9.42	2	0.16	0.01	0.08	0.00	0.00	24.0
6	0	-11070	-574	-500	0	-616	4466	15.71	15.71	9.42	9.42	2	0.13	0.01	0.05	0.00	0.00	24.0
7	0	-11270	-642	-174	0	22	4817	15.71	15.71	9.42	9.42	2	0.12	0.01	0.05	0.00	0.00	24.0
8	0	-11030	-717	-507	0	-609	5093	15.71	15.71	9.42	9.42	2	0.14	0.01	0.06	0.00	0.00	24.0
9	0	-11230	-785	-180	0	29	5443	15.71	15.71	9.42	9.42	2	0.14	0.01	0.06	0.00	0.00	24.0
10	0	-11180	-432	-378	0	-401	3857	15.71	15.71	9.42	9.42	2	0.11	0.01	0.04	0.00	0.00	24.0
11	0	-11240	-452	-280	0	-209	3962	15.71	15.71	9.42	9.42	2	0.10	0.01	0.04	0.00	0.00	24.0
12	0	-11060	-907	-400	0	-377	5947	15.71	15.71	9.42	9.42	2	0.16	0.01	0.07	0.00	0.00	24.0
13	0	-11120	-927	-302	0	-186	6052	15.71	15.71	9.42	9.42	2	0.16	0.01	0.08	0.00	0.00	24.0
14	0	-11070	-574	-500	0	-616	4466	15.71	15.71	9.42	9.42	2	0.13	0.01	0.05	0.00	0.00	24.0
15	0	-11270	-642	-174	0	22	4817	15.71	15.71	9.42	9.42	2	0.12	0.01	0.05	0.00	0.00	24.0
16	0	-11030	-717	-507	0	-609	5093	15.71	15.71	9.42	9.42	2	0.14	0.01	0.06	0.00	0.00	24.0
17	0	-11230	-785	-180	0	29	5443	15.71	15.71	9.42	9.42	2	0.14	0.01	0.06	0.00	0.00	24.0
18	0	-25650	-815	-1529	0	-1559	13030	15.71	15.71	9.42	9.42	3	0.24	0.02	0.09	0.00	0.00	24.0
19	0	-18100	-2709	-954	0	-839	11400	15.71	15.71	9.42	9.42	3	0.21	0.03	0.20	0.00	0.00	24.0
20	0	-20890	-1681	-1039	0	-906	11640	15.71	15.71	9.42	9.42	3	0.21	0.02	0.12	0.00	0.00	24.0
37	0	-25810	103	-1459	0	-1531	11690	15.71	15.71	9.42	9.42	3	0.21	0.02	0.08	0.00	0.00	24.0
38	0	-13240	-3053	-500	0	-331	8983	15.71	15.71	9.42	9.42	3	0.16	0.04	0.24	0.00	0.00	24.0
39	0	-17890	-1340	-642	0	-443	9367	15.71	15.71	9.42	9.42	3	0.17	0.02	0.10	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	83	-13632	-884	-442	0	-16	5712	15.71	15.71	9.42	9.42	3	0.10	0.01	0.07	0.00	0.00	24.0
2	83	-10520	-432	-378	0	-89	3501	15.71	15.71	9.42	9.42	2	0.09	0.01	0.04	0.00	0.00	24.0
3	83	-10580	-452	-280	0	22	3589	15.71	15.71	9.42	9.42	2	0.09	0.01	0.04	0.00	0.00	24.0
4	83	-10399	-907	-400	0	-47	5199	15.71	15.71	9.42	9.42	2	0.13	0.01	0.07	0.00	0.00	24.0
5	83	-10459	-927	-302	0	64	5287	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
6	83	-10410	-574	-500	0	-203	3992	15.71	15.71	9.42	9.42	2	0.11	0.01	0.05	0.00	0.00	24.0
7	83	-10609	-642	-174	0	165	4287	15.71	15.71	9.42	9.42	2	0.11	0.01	0.05	0.00	0.00	24.0
8	83	-10370	-717	-507	0	-191	4502	15.71	15.71	9.42	9.42	2	0.12	0.01	0.06	0.00	0.00	24.0
9	83	-10570	-785	-180	0	178	4796	15.71	15.71	9.42	9.42	2	0.13	0.01	0.06	0.00	0.00	24.0
10	83	-10520	-432	-378	0	-89	3501	15.71	15.71	9.42	9.42	2	0.09	0.01	0.04	0.00	0.00	24.0
11	83	-10580	-452	-280	0	22	3589	15.71	15.71	9.42	9.42	2	0.09	0.01	0.04	0.00	0.00	24.0
12	83	-10399	-907	-400	0	-47	5199	15.71	15.71	9.42	9.42	2	0.13	0.01	0.07	0.00	0.00	24.0
13	83	-10459	-927	-302	0	64	5287	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
14	83	-10410	-574	-500	0	-203	3992	15.71	15.71	9.42	9.42	2	0.11	0.01	0.05	0.00	0.00	24.0
15	83	-10609	-642	-174	0	165	4287	15.71	15.71	9.42	9.42	2	0.11	0.01	0.05	0.00	0.00	24.0
16	83	-10370	-717	-507	0	-191	4502	15.71	15.71	9.42	9.42	2	0.12	0.01	0.06	0.00	0.00	24.0
17	83	-10570	-785	-180	0	178	4796	15.71	15.71	9.42	9.42	2	0.13	0.01	0.06	0.00	0.00	24.0
18	83	-24790	-1192	-1529	0	-298	12202	15.71	15.71	9.42	9.42	3	0.21	0.02	0.09	0.00	0.00	24.0
19	83	-17242	-2332	-954	0	-52	9322	15.71	15.71	9.42	9.42	3	0.17	0.03	0.18	0.00	0.00	24.0
20	83	-20032	-1681	-1039	0	-49	10252	15.71	15.71	9.42	9.42	3	0.18	0.02	0.12	0.00	0.00	24.0
37	83	-24952	-525	-1459	0	-328	11517	15.71	15.71	9.42	9.42	3	0.20	0.02	0.08	0.00	0.00	24.0
38	83	-12381	-2424	-500	0	82	6724	15.71	15.71	9.42	9.42	3	0.12	0.03	0.20	0.00	0.00	24.0
39	83	-17030	-1340	-642	0	87	8262	15.71	15.71	9.42	9.42	3	0.15	0.02	0.10	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	165	-12775	-884	-442	0	348	4983	15.71	15.71	9.42	9.42	3	0.09	0.01	0.07	0.00	0.00	24.0
2	165	-9861	-432	-378	0	223	3144	15.71	15.71	9.42	9.42	2	0.09	0.01	0.04	0.00	0.00	24.0
3	165	-9920	-452	-280	0	253	3216	15.71	15.71	9.42	9.42	2	0.09	0.01	0.04	0.00	0.00	24.0
4	165	-9738	-907	-400	0	283	4450	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0

5	165	-9798	-927	-302	0	313	4522	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
6	165	-9750	-574	-500	0	209	3518	15.71	15.71	9.42	9.42	2	0.09	0.01	0.05	0.00	0.00	24.0
7	165	-9948	-642	-174	0	309	3757	15.71	15.71	9.42	9.42	2	0.10	0.01	0.05	0.00	0.00	24.0
8	165	-9710	-717	-507	0	227	3910	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
9	165	-9910	-785	-180	0	327	4148	15.71	15.71	9.42	9.42	2	0.11	0.01	0.07	0.00	0.00	24.0
10	165	-9861	-432	-378	0	223	3144	15.71	15.71	9.42	9.42	2	0.09	0.01	0.04	0.00	0.00	24.0
11	165	-9920	-452	-280	0	253	3216	15.71	15.71	9.42	9.42	2	0.09	0.01	0.04	0.00	0.00	24.0
12	165	-9738	-907	-400	0	283	4450	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
13	165	-9798	-927	-302	0	313	4522	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
14	165	-9750	-574	-500	0	209	3518	15.71	15.71	9.42	9.42	2	0.09	0.01	0.05	0.00	0.00	24.0
15	165	-9948	-642	-174	0	309	3757	15.71	15.71	9.42	9.42	2	0.10	0.01	0.05	0.00	0.00	24.0
16	165	-9710	-717	-507	0	227	3910	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
17	165	-9910	-785	-180	0	327	4148	15.71	15.71	9.42	9.42	2	0.11	0.01	0.07	0.00	0.00	24.0
18	165	-23930	-1570	-1529	0	964	11063	15.71	15.71	9.42	9.42	3	0.20	0.02	0.11	0.00	0.00	24.0
19	165	-16385	-1954	-954	0	735	7555	15.71	15.71	9.42	9.42	3	0.14	0.02	0.15	0.00	0.00	24.0
20	165	-19175	-1681	-1039	0	809	8864	15.71	15.71	9.42	9.42	3	0.16	0.02	0.13	0.00	0.00	24.0
37	165	-24095	-1154	-1459	0	876	10825	15.71	15.71	9.42	9.42	3	0.19	0.02	0.08	0.00	0.00	24.0
38	165	-11522	-1796	-500	0	494	4983	15.71	15.71	9.42	9.42	3	0.09	0.02	0.15	0.00	0.00	24.0
39	165	-16170	-1340	-642	0	617	7156	15.71	15.71	9.42	9.42	3	0.13	0.02	0.10	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	248	-11918	-884	-442	0	713	4254	15.71	15.71	9.42	9.42	3	0.08	0.01	0.07	0.00	0.00	24.0
2	248	-9202	-432	-378	0	535	2788	15.71	15.71	9.42	9.42	2	0.09	0.01	0.04	0.00	0.00	24.0
3	248	-9261	-452	-280	0	484	2843	15.71	15.71	9.42	9.42	2	0.09	0.01	0.04	0.00	0.00	24.0
4	248	-9077	-907	-400	0	613	3702	15.71	15.71	9.42	9.42	2	0.11	0.01	0.08	0.00	0.00	24.0
5	248	-9137	-927	-302	0	562	3757	15.71	15.71	9.42	9.42	2	0.11	0.01	0.08	0.00	0.00	24.0
6	248	-9089	-574	-500	0	622	3044	15.71	15.71	9.42	9.42	2	0.09	0.01	0.05	0.00	0.00	24.0
7	248	-9288	-642	-174	0	452	3227	15.71	15.71	9.42	9.42	2	0.09	0.01	0.05	0.00	0.00	24.0
8	248	-9051	-717	-507	0	645	3318	15.71	15.71	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
9	248	-9249	-785	-180	0	476	3501	15.71	15.71	9.42	9.42	2	0.10	0.01	0.07	0.00	0.00	24.0
10	248	-9202	-432	-378	0	535	2788	15.71	15.71	9.42	9.42	2	0.09	0.01	0.04	0.00	0.00	24.0
11	248	-9261	-452	-280	0	484	2843	15.71	15.71	9.42	9.42	2	0.09	0.01	0.04	0.00	0.00	24.0
12	248	-9077	-907	-400	0	613	3702	15.71	15.71	9.42	9.42	2	0.11	0.01	0.08	0.00	0.00	24.0
13	248	-9137	-927	-302	0	562	3757	15.71	15.71	9.42	9.42	2	0.11	0.01	0.08	0.00	0.00	24.0
14	248	-9089	-574	-500	0	622	3044	15.71	15.71	9.42	9.42	2	0.09	0.01	0.05	0.00	0.00	24.0
15	248	-9288	-642	-174	0	452	3227	15.71	15.71	9.42	9.42	2	0.09	0.01	0.05	0.00	0.00	24.0
16	248	-9051	-717	-507	0	645	3318	15.71	15.71	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
17	248	-9249	-785	-180	0	476	3501	15.71	15.71	9.42	9.42	2	0.10	0.01	0.07	0.00	0.00	24.0
18	248	-23070	-1947	-1529	0	2226	9613	15.71	15.71	9.42	9.42	3	0.19	0.02	0.14	0.00	0.00	24.0
19	248	-15528	-1577	-954	0	1523	6099	15.71	15.71	9.42	9.42	3	0.13	0.02	0.12	0.00	0.00	24.0
20	248	-18318	-1681	-1039	0	1666	7476	15.71	15.71	9.42	9.42	3	0.15	0.02	0.13	0.00	0.00	24.0
37	248	-23238	-1782	-1459	0	2079	9615	15.71	15.71	9.42	9.42	3	0.19	0.02	0.13	0.00	0.00	24.0
38	248	-10664	-1167	-500	0	907	3761	15.71	15.71	9.42	9.42	3	0.08	0.01	0.10	0.00	0.00	24.0
39	248	-15310	-1340	-642	0	1147	6051	15.71	15.71	9.42	9.42	3	0.12	0.02	0.10	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	330	-11060	-884	-442	0	1078	3525	15.71	15.71	9.42	9.42	3	0.08	0.01	0.07	0.00	0.00	24.0
2	330	-8542	-432	-378	0	846	2432	15.71	15.71	9.42	9.42	2	0.09	0.01	0.04	0.00	0.00	24.0
3	330	-8601	-452	-280	0	715	2470	15.71	15.71	9.42	9.42	2	0.08	0.01	0.04	0.00	0.00	24.0
4	330	-8416	-907	-400	0	944	2954	15.71	15.71	9.42	9.42	2	0.10	0.01	0.08	0.00	0.00	24.0
5	330	-8476	-927	-302	0	812	2992	15.71	15.71	9.42	9.42	2	0.10	0.01	0.08	0.00	0.00	24.0
6	330	-8429	-574	-500	0	1034	2570	15.71	15.71	9.42	9.42	2	0.10	0.01	0.05	0.00	0.00	24.0
7	330	-8627	-642	-174	0	595	2697	15.71	15.71	9.42	9.42	2	0.08	0.01	0.05	0.00	0.00	24.0
8	330	-8391	-717	-507	0	1063	2727	15.71	15.71	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
9	330	-8589	-785	-180	0	624	2853	15.71	15.71	9.42	9.42	2	0.09	0.01	0.07	0.00	0.00	24.0
10	330	-8542	-432	-378	0	846	2432	15.71	15.71	9.42	9.42	2	0.09	0.01	0.04	0.00	0.00	24.0
11	330	-8601	-452	-280	0	715	2470	15.71	15.71	9.42	9.42	2	0.08	0.01	0.04	0.00	0.00	24.0
12	330	-8416	-907	-400	0	944	2954	15.71	15.71	9.42	9.42	2	0.10	0.01	0.08	0.00	0.00	24.0
13	330	-8476	-927	-302	0	812	2992	15.71	15.71	9.42	9.42	2	0.10	0.01	0.08	0.00	0.00	24.0
14	330	-8429	-574	-500	0	1034	2570	15.71	15.71	9.42	9.42	2	0.10	0.01	0.05	0.00	0.00	24.0
15	330	-8627	-642	-174	0	595	2697	15.71	15.71	9.42	9.42	2	0.08	0.01	0.05	0.00	0.00	24.0
16	330	-8391	-717	-507	0	1063	2727	15.71	15.71	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
17	330	-8589	-785	-180	0	624	2853	15.71	15.71	9.42	9.42	2	0.09	0.01	0.07	0.00	0.00	24.0
18	330	-22210	-2324	-1529	0	3487	7852	15.71	15.71	9.42	9.42	3	0.19	0.03	0.17	0.00	0.00	24.0
19	330	-14670	-1200	-954	0	2310	4955	15.71	15.71	9.42	9.42	3	0.13	0.02	0.09	0.00	0.00	24.0
20	330	-17460	-1681	-1039	0	2524	6088	15.71	15.71	9.42	9.42	3	0.15	0.02	0.13	0.00	0.00	24.0
37	330	-22380	-2411	-1459	0	3283	7886	15.71	15.71	9.42	9.42	3	0.19	0.03	0.17	0.00	0.00	24.0
38	330	-9805	-538	-500	0	1320	3057	15.71	15.71	9.42	9.42	3	0.08	0.01	0.04	0.00	0.00	24.0
39	330	-14450	-1340	-642	0	1677	4946	15.71	15.71	9.42	9.42	3	0.11	0.02	0.11	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 35 NI 302 NF 291 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 1D
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-9624	-125	-429	0	-1283	650	6.28	6.28	9.42	9.42	3	0.09	0.01	0.05	0.00	0.00	24.0
2	0	-6990	108	-345	0	-1046	66	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
3	0	-6862	98	-317	0	-957	75	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
4	0	-7944	-291	-343	0	-1018	925	6.28	6.28	9.42	9.42	2	0.14	0.01	0.04	0.00	0.00	24.0
5	0	-7816	-300	-315	0	-928	935	6.28	6.28	9.42	9.42	2	0.14	0.01	0.04	0.00	0.00	24.0
6	0	-7473	-21	-377	0	-1140	355	6.28	6.28	9.42	9.42	2	0.09	0.01	0.05	0.00	0.00	24.0
7	0	-7046	-52	-283	0	-843	387	6.28	6.28	9.42	9.42	2	0.08	0.01	0.03	0.00	0.00	24.0
8	0	-7759	-140	-376	0	-1132	613	6.28	6.28	9.42	9.42	2	0.11	0.01	0.05	0.00	0.00	24.0
9	0	-7333	-172	-283	0	-834	645	6.28	6.28	9.42	9.42	2	0.10	0.01	0.03	0.00	0.00	24.0
10	0	-6990	108	-345	0	-1046	66	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
11	0	-6862	98	-317	0	-957	75	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
12	0	-7944	-291	-343	0	-1018	925	6.28	6.28	9.42	9.42	2	0.14	0.01	0.04	0.00	0.00	24.0
13	0	-7816	-300	-315	0	-928	935	6.28	6.28	9.42	9.42	2	0.14	0.01	0.04	0.00	0.00	24.0
14	0	-7473	-21	-377	0	-1140	355	6.28	6.28	9.42	9.42	2	0.09	0.01	0.05	0.00	0.00	24.0
15	0	-7046	-52	-283	0	-843	387	6.28	6.28	9.42	9.42	2	0.08	0.01	0.03	0.00	0.00	24.0
16	0	-7759	-140	-376	0	-1132	613	6.28	6.28	9.42	9.42	2	0.11	0.01	0.05	0.00	0.00	24.0
17	0	-7333	-172	-283	0	-834	645	6.28	6.28	9.42	9.42	2	0.10	0.01	0.03	0.00	0.00	24.0
18	0	-12570	1140	522	0	-1048	-943	6.28	6.28	9.42	9.42	3	0.10	0.03	0.11	0.00	0.00	24.0
19	0	-12550	-821	-86	0	-1122	1805	6.28	6.28	9.42	9.42	3	0.18	0.02	0.09	0.00	0.00	24.0
20	0	-11880	108	-7	0	-1209	469	6.28	6.28	9.42	9.42	3	0.07	0.00	0.01	0.00	0.00	24.0
37	0	-11610	1694	512	0	-1088	-1783	6.28	6.28	9.42	9.42	3	0.18	0.04	0.18	0.00	0.00	24.0
38	0	-11580	-1574	-502	0	-1212	2797	6.28	6.28	9.42	9.42	3	0.29	0.04	0.17	0.00	0.00	24.0
39	0	-10470	-26	-370	0	-1357	569	6.28	6.28	9.42	9.42	3	0.08	0.01	0.04	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	83	-9141	-125	-429	0	-929	547	6.28	6.28	9.42	9.42	3	0.07	0.01	0.05	0.00	0.00	24.0
2	83	-6619	108	-345	0	-761	155	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
3	83	-6491	98	-317	0	-695	156	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
4	83	-7573	-291	-343	0	-735	685	6.28	6.28	9.42	9.42	2	0.10	0.01	0.04	0.00	0.00	24.0
5	83	-7445	-300	-315	0	-669	687	6.28	6.28	9.42	9.42	2	0.10	0.01	0.04	0.00	0.00	24.0
6	83	-7102	-21	-377	0	-829	338	6.28	6.28	9.42	9.42	2	0.07	0.01	0.05	0.00	0.00	24.0
7	83	-6675	-52	-283	0	-609	344	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
8	83	-7388	-140	-376	0	-822	497	6.28	6.28	9.42	9.42	2	0.09	0.01	0.05	0.00	0.00	24.0
9	83	-6962	-172	-283	0	-601	503	6.28	6.28	9.42	9.42	2	0.08	0.01	0.03	0.00	0.00	24.0
10	83	-6619	108	-345	0	-761	155	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
11	83	-6491	98	-317	0	-695	156	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
12	83	-7573	-291	-343	0	-735	685	6.28	6.28	9.42	9.42	2	0.10	0.01	0.04	0.00	0.00	24.0
13	83	-7445	-300	-315	0	-669	687	6.28	6.28	9.42	9.42	2	0.10	0.01	0.04	0.00	0.00	24.0
14	83	-7102	-21	-377	0	-829	338	6.28	6.28	9.42	9.42	2	0.07	0.01	0.05	0.00	0.00	24.0
15	83	-6675	-52	-283	0	-609	344	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
16	83	-7388	-140	-376	0	-822	497	6.28	6.28	9.42	9.42	2	0.09	0.01	0.05	0.00	0.00	24.0
17	83	-6962	-172	-283	0	-601	503	6.28	6.28	9.42	9.42	2	0.08	0.01	0.03	0.00	0.00	24.0
18	83	-12088	951	522	0	-1479	-80	6.28	6.28	9.42	9.42	3	0.07	0.02	0.09	0.00	0.00	24.0
19	83	-12068	-632	-86	0	-1051	1206	6.28	6.28	9.42	9.42	3	0.13	0.02	0.07	0.00	0.00	24.0
20	83	-11398	108	104	0	-1250	558	6.28	6.28	9.42	9.42	3	0.08	0.00	0.01	0.00	0.00	24.0
37	83	-11128	1380	512	0	-1511	-515	6.28	6.28	9.42	9.42	3	0.09	0.03	0.13	0.00	0.00	24.0
38	83	-11098	-1260	-502	0	-798	1628	6.28	6.28	9.42	9.42	3	0.17	0.03	0.13	0.00	0.00	24.0
39	83	-9987	-26	-186	0	-1130	548	6.28	6.28	9.42	9.42	3	0.07	0.00	0.02	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	165	-8658	-125	-429	0	-576	444	6.28	6.28	9.42	9.42	3	0.05	0.01	0.05	0.00	0.00	24.0
2	165	-6248	108	-345	0	-477	244	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
3	165	-6120	98	-317	0	-434	237	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
4	165	-7202	-291	-343	0	-452	445	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
5	165	-7074	-300	-315	0	-409	439	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
6	165	-6730	-21	-377	0	-518	321	6.28	6.28	9.42	9.42	2	0.06	0.01	0.05	0.00	0.00	24.0
7	165	-6304	-52	-283	0	-375	301	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
8	165	-7016	-140	-376	0	-511	382	6.28	6.28	9.42	9.42	2	0.06	0.01	0.05	0.00	0.00	24.0
9	165	-6590	-172	-283	0	-368	361	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
10	165	-6248	108	-345	0	-477	244	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
11	165	-6120	98	-317	0	-434	237	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
12	165	-7202	-291	-343	0	-452	445	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
13	165	-7074	-300	-315	0	-409	439	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
14	165	-6730	-21	-377	0	-518	321	6.28	6.28	9.42	9.42	2	0.06	0.01	0.05	0.00	0.00	24.0
15	165	-6304	-52	-283	0	-375	301	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
16	165	-7016	-140	-376	0	-511	382	6.28	6.28	9.42	9.42	2	0.06	0.01	0.05	0.00	0.00	24.0
17	165	-6590	-172	-283	0	-368	361	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
18	165	-11605	763	522	0	-1910	627	6.28	6.28	9.42	9.42	3	0.11	0.02	0.07	0.00	0.00	24.0
19	165	-11585	-443	-86	0	-980	762	6.28	6.28	9.42	9.42	3	0.08	0.01	0.04	0.00	0.00	24.0
20	165	-10916	108	198	0	-1376	647	6.28	6.28	9.42	9.42	3	0.09	0.00	0.02	0.00	0.00	24.0
37	165	-10645	1065	512	0	-1934	493	6.28	6.28	9.42	9.42	3	0.10	0.03	0.10	0.00	0.00	24.0
38	165	-10616	-945	-502	0	-384	719	6.28	6.28	9.42	9.42	3	0.07	0.02	0.10	0.00	0.00	24.0
39	165	-9504	-26	-28	0	-1043	527	6.28	6.28	9.42	9.42	3	0.07	0.00	0.00	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	248	-8176	-125	-429	0	-222	340	6.28	6.28	9.42	9.42	3	0.04	0.01	0.05	0.00	0.00	24.0
2	248	-5876	108	-345	0	-192	333	6.28	6.28	9.42	9.42	2	0.04	0.01	0.04	0.00	0.00	24.0
3	248	-5748	98	-317	0	-172	319	6.28	6.28	9.42	9.42	2	0.04	0.01	0.04	0.00	0.00	24.0
4	248	-6830	-291	-343	0	-170	205	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
5	248	-6702	-300	-315	0	-150	191	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
6	248	-6359	-21	-377	0	-208	305	6.28	6.28	9.42	9.42	2	0.04	0.01	0.05	0.00	0.00	24.0
7	248	-5932	-52	-283	0	-141	257	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
8	248	-6645	-140	-376	0	-201	266	6.28	6.28	9.42	9.42	2	0.04	0.01	0.05	0.00	0.00	24.0
9	248	-6219	-172	-283	0	-135	219	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
10	248	-5876	108	-345	0	-192	333	6.28	6.28	9.42	9.42	2	0.04	0.01	0.04	0.00	0.00	24.0
11	248	-5748	98	-317	0	-172	319	6.28	6.28	9.42	9.42	2	0.04	0.01	0.04	0.00	0.00	24.0
12	248	-6830	-291	-343	0	-170	205	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
13	248	-6702	-300	-315	0	-150	191	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
14	248	-6359	-21	-377	0	-208	305	6.28	6.28	9.42	9.42	2	0.04	0.01	0.05	0.00	0.00	24.0
15	248	-5932	-52	-283	0	-141	257	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
16	248	-6645	-140	-376	0	-201	266	6.28	6.28	9.42	9.42	2	0.04	0.01	0.05	0.00	0.00	24.0
17	248	-6219	-172	-283	0	-135	219	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
18	248	-11122	574	522	0	-2341	1178	6.28	6.28	9.42	9.42	3	0.15	0.01	0.06	0.00	0.00	24.0
19	248	-11102	-255	-86	0	-909	474	6.28	6.28	9.42	9.42	3	0.06	0.01	0.02	0.00	0.00	24.0
20	248	-10434	108	277	0	-1573	736	6.28	6.28	9.42	9.42	3	0.10	0.01	0.03	0.00	0.00	24.0
37	248	-10162	751	512	0	-2356	1242	6.28	6.28	9.42	9.42	3	0.16	0.02	0.07	0.00	0.00	24.0
38	248	-10133	-631	-502	0	30	69	6.28	6.28	9.42	9.42	3	0.01	0.02	0.07	0.00	0.00	24.0
39	248	-9020	-26	104	0	-1076	505	6.28	6.28	9.42	9.42	3	0.07	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	330	-7693	-125	-429	0	131	237	6.28	6.28	9.42	9.42	3	0.03	0.01	0.05	0.00	0.00	24.0
2	330	-5505	108	-345	0	92	422	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
3	330	-5377	98	-317	0	89	400	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
4	330	-6459	-291	-343	0	113	-35	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
5	330	-6331	-300	-315	0	110	-57	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
6	330	-5988	-21	-377	0	103	288	6.28	6.28	9.42	9.42	2	0.04	0.01	0.05	0.00	0.00	24.0
7	330	-5561	-52	-283	0	92	214	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
8	330	-6274	-140	-376	0	110	151	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
9	330	-5848	-172	-283	0	99	77	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
10	330	-5505	108	-345	0	92	422	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
11	330	-5377	98	-317	0	89	400	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
12	330	-6459	-291	-343	0	113	-35	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
13	330	-6331	-300	-315	0	110	-57	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
14	330	-5988	-21	-377	0	103	288	6.28	6.28	9.42	9.42	2	0.04	0.01	0.05	0.00	0.00	24.0
15	330	-5561	-52	-283	0	92	214	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
16	330	-6274	-140	-376	0	110	151	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
17	330	-5848	-172	-283	0	99	77	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
18	330	-10640	386	522	0	-2772	1574	6.28	6.28	9.42	9.42	3	0.19	0.01	0.06	0.00	0.00	24.0
19	330	-10620	-66	-86	0	-838	342	6.28	6.28	9.42	9.42	3	0.05	0.00	0.01	0.00	0.00	24.0
20	330	-9952	108	340	0	-1829	826	6.28	6.28	9.42	9.42	3	0.12	0.01	0.04	0.00	0.00	24.0
37	330	-9680	436	512	0	-2779	1732	6.28	6.28	9.42	9.42	3	0.20	0.01	0.06	0.00	0.00	24.0
38	330	-9651	-316	-502	0	445	-322	6.28	6.28	9.42	9.42	3	0.04	0.01	0.06	0.00	0.00	24.0
39	330	-8537	-26	208	0	-1207	484	6.28	6.28	9.42	9.42	3	0.07	0.00	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

VERIFICA NODO IN TESTA AL PILASTRO, NODO NUM. 291 NON CONFINATO

(par.7.2.2 NTC2018 "La domanda di resistenza valutata con i criteri della progettazione in capacità può essere assunta non superiore alla domanda di resistenza valutata per il caso di comportamento strutturale non dissipativo.")

PROGETTAZIONE IN CAPACITA'

Asse loc. pilastro y nodo ESTERNO: As2(inf)= 4.02, As1(sup)= 6.03, Hjw= 40.0 cm, bj= 45.0 cm, hjc= 20.0 cm

Asse loc. pilastro z nodo ESTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 30.0 cm, hjc= 50.0 cm

FxMin,inf	FxMin,sup	FxMax,sup	FySup	FzSup	Vjbdy	Vjbdz	Vres,y	Vres,z	I.R.compr.	Ashy	Ashz	PASSO	Nota
daN					daN		daN			cmq		cm	
-5377	1	-0	0	0	26425	17616	63005	105009	0.42	4.36	--	11.99	

VERIFICA DI RESISTENZA CON SOLLECITAZIONI COMPORTAMENTO NON DISSIPATIVO

Asse loc. pilastro y nodo ESTERNO: Hjw= 40.0 cm, bj= 45.0 cm, hjc= 20.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb	Vb	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m			daN			cmq	cm	
2	-0	-5505	-1329	1376	0	3281	63005	0.05	0.00	40.00	
3	-0	-5377	-1314	1373	0	3244	63005	0.05	0.00	40.00	
4	-0	-6459	-3671	2093	0	9064	63005	0.14	0.00	40.00	
5	-0	-6331	-3656	2090	0	9027	63005	0.14	0.00	40.00	
6	-0	-5988	-2166	1631	0	5348	63005	0.08	0.00	40.00	
7	-0	-5561	-2116	1621	0	5225	63005	0.08	0.00	40.00	
8	-0	-6274	-2868	1846	0	7081	63005	0.11	0.00	40.00	
9	-0	-5848	-2819	1836	0	6960	63005	0.11	0.00	40.00	
10	-0	-5505	-1329	1376	0	3281	63005	0.05	0.00	40.00	
11	-0	-5377	-1314	1373	0	3244	63005	0.05	0.00	40.00	
12	-0	-6459	-3671	2093	0	9064	63005	0.14	0.00	40.00	
13	-0	-6331	-3656	2090	0	9027	63005	0.14	0.00	40.00	
14	-0	-5988	-2166	1631	0	5348	63005	0.08	0.00	40.00	
15	-0	-5561	-2116	1621	0	5225	63005	0.08	0.00	40.00	
16	-0	-6274	-2868	1846	0	7081	63005	0.11	0.00	40.00	
17	-0	-5848	-2819	1836	0	6960	63005	0.11	0.00	40.00	

Asse loc. pilastro z nodo ESTERNO: Hjw= 40.0 cm, bj= 30.0 cm, hjc= 50.0 cm, db1= 45.0 cm

NC	Fx,sup	Fx,inf	Mb	Vb	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m			daN			cmq	cm	
2	-0	-5505	-1979	1626	0	4886	105009	0.05	0.00	40.00	
3	-0	-5377	-1724	1544	0	4257	105009	0.04	0.00	40.00	
4	-0	-6459	-1862	1583	0	4598	105009	0.04	0.00	40.00	
5	-0	-6331	-1607	1501	0	3968	105009	0.04	0.00	40.00	
6	-0	-5988	-2237	1706	0	5523	105009	0.05	0.00	40.00	
7	-0	-5561	-1384	1433	0	3417	105009	0.03	0.00	40.00	
8	-0	-6274	-2202	1693	0	5437	105009	0.05	0.00	40.00	
9	-0	-5848	-1349	1420	0	3331	105009	0.03	0.00	40.00	
10	-0	-5505	-1979	1626	0	4886	105009	0.05	0.00	40.00	
11	-0	-5377	-1724	1544	0	4257	105009	0.04	0.00	40.00	
12	-0	-6459	-1862	1583	0	4598	105009	0.04	0.00	40.00	
13	-0	-6331	-1607	1501	0	3968	105009	0.04	0.00	40.00	
14	-0	-5988	-2237	1706	0	5523	105009	0.05	0.00	40.00	
15	-0	-5561	-1384	1433	0	3417	105009	0.03	0.00	40.00	
16	-0	-6274	-2202	1693	0	5437	105009	0.05	0.00	40.00	
17	-0	-5848	-1349	1420	0	3331	105009	0.03	0.00	40.00	

CONFRONTO E SINTESI CONCLUSIVE (si assume in ogni caso passo <= 15 cm)

I.R.compr.	Ashy	Ashz	PASSO	Nota
	cmq		cm	
0.14	--	--	15.00	**VERIFICATO**

ASTA NUM. 36 NI 325 NF 295 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 10D
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-10780	-98	-148	0	-1393	-75	6.28	6.28	12.57	12.57	3	0.05	0.00	0.01	0.00	0.00	24.0
2	0	-8475	655	-172	0	-1386	-1107	6.28	6.28	12.57	12.57	2	0.11	0.01	0.06	0.00	0.00	24.0
3	0	-8468	647	-63	0	-734	-1097	6.28	6.28	12.57	12.57	2	0.09	0.01	0.06	0.00	0.00	24.0
4	0	-8113	-798	-166	0	-1410	981	6.28	6.28	12.57	12.57	2	0.11	0.01	0.07	0.00	0.00	24.0
5	0	-8107	-806	-57	0	-757	991	6.28	6.28	12.57	12.57	2	0.08	0.01	0.08	0.00	0.00	24.0
6	0	-8356	156	-297	0	-2155	-389	6.28	6.28	12.57	12.57	2	0.12	0.01	0.03	0.00	0.00	24.0
7	0	-8334	129	67	0	19	-354	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
8	0	-8247	-280	-295	0	-2162	238	6.28	6.28	12.57	12.57	2	0.12	0.01	0.03	0.00	0.00	24.0
9	0	-8226	-307	69	0	12	273	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
10	0	-8475	655	-172	0	-1386	-1107	6.28	6.28	12.57	12.57	2	0.11	0.01	0.06	0.00	0.00	24.0
11	0	-8468	647	-63	0	-734	-1097	6.28	6.28	12.57	12.57	2	0.09	0.01	0.06	0.00	0.00	24.0
12	0	-8113	-798	-166	0	-1410	981	6.28	6.28	12.57	12.57	2	0.11	0.01	0.07	0.00	0.00	24.0
13	0	-8107	-806	-57	0	-757	991	6.28	6.28	12.57	12.57	2	0.08	0.01	0.08	0.00	0.00	24.0
14	0	-8356	156	-297	0	-2155	-389	6.28	6.28	12.57	12.57	2	0.12	0.01	0.03	0.00	0.00	24.0
15	0	-8334	129	67	0	19	-354	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
16	0	-8247	-280	-295	0	-2162	238	6.28	6.28	12.57	12.57	2	0.12	0.01	0.03	0.00	0.00	24.0
17	0	-8226	-307	69	0	12	273	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
18	0	-13210	1398	-422	0	-3412	-2061	6.28	6.28	12.57	12.57	3	0.16	0.03	0.11	0.00	0.00	24.0
19	0	-11070	-2173	-237	0	-2557	2860	6.28	6.28	12.57	12.57	3	0.17	0.04	0.20	0.00	0.00	24.0
20	0	-11800	-347	-785	0	-1743	332	6.28	6.28	12.57	12.57	3	0.07	0.01	0.08	0.00	0.00	24.0
37	0	-13610	2686	-426	0	-3183	-3862	6.28	6.28	12.57	12.57	3	0.23	0.05	0.24	0.00	0.00	24.0
38	0	-10040	-3265	-117	0	-1758	4340	6.28	6.28	12.57	12.57	3	0.25	0.06	0.31	0.00	0.00	24.0
39	0	-11250	-222	-1031	0	-401	126	6.28	6.28	12.57	12.57	3	0.02	0.02	0.10	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	83	-10136	-98	-148	0	-1271	-156	6.28	6.28	12.57	12.57	3	0.05	0.00	0.01	0.00	0.00	24.0
2	83	-7980	655	-172	0	-1244	-566	6.28	6.28	12.57	12.57	2	0.08	0.01	0.06	0.00	0.00	24.0
3	83	-7973	647	-63	0	-682	-563	6.28	6.28	12.57	12.57	2	0.06	0.01	0.06	0.00	0.00	24.0
4	83	-7618	-798	-166	0	-1273	322	6.28	6.28	12.57	12.57	2	0.08	0.01	0.07	0.00	0.00	24.0
5	83	-7612	-806	-57	0	-711	326	6.28	6.28	12.57	12.57	2	0.05	0.01	0.07	0.00	0.00	24.0
6	83	-7861	156	-297	0	-1910	-260	6.28	6.28	12.57	12.57	2	0.11	0.01	0.03	0.00	0.00	24.0

7	83	-7839	129	67	0	-36	-247	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
8	83	-7752	-280	-295	0	-1918	6	6.28	6.28	12.57	12.57	2	0.10	0.01	0.03	0.00	0.00	24.0
9	83	-7731	-307	69	0	-45	20	6.28	6.28	12.57	12.57	2	0.00	0.01	0.03	0.00	0.00	24.0
10	83	-7980	655	-172	0	-1244	-566	6.28	6.28	12.57	12.57	2	0.08	0.01	0.06	0.00	0.00	24.0
11	83	-7973	647	-63	0	-682	-563	6.28	6.28	12.57	12.57	2	0.06	0.01	0.06	0.00	0.00	24.0
12	83	-7618	-798	-166	0	-1273	322	6.28	6.28	12.57	12.57	2	0.08	0.01	0.07	0.00	0.00	24.0
13	83	-7612	-806	-57	0	-711	326	6.28	6.28	12.57	12.57	2	0.05	0.01	0.07	0.00	0.00	24.0
14	83	-7861	156	-297	0	-1910	-260	6.28	6.28	12.57	12.57	2	0.11	0.01	0.03	0.00	0.00	24.0
15	83	-7839	129	67	0	-36	-247	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
16	83	-7752	-280	-295	0	-1918	6	6.28	6.28	12.57	12.57	2	0.10	0.01	0.03	0.00	0.00	24.0
17	83	-7731	-307	69	0	-45	20	6.28	6.28	12.57	12.57	2	0.00	0.01	0.03	0.00	0.00	24.0
18	83	-12568	1398	-422	0	-3063	-908	6.28	6.28	12.57	12.57	3	0.12	0.03	0.11	0.00	0.00	24.0
19	83	-10427	-2173	-237	0	-2361	1067	6.28	6.28	12.57	12.57	3	0.10	0.04	0.18	0.00	0.00	24.0
20	83	-11156	-347	-566	0	-1188	45	6.28	6.28	12.57	12.57	3	0.04	0.01	0.06	0.00	0.00	24.0
37	83	-12965	2686	-426	0	-2832	-1646	6.28	6.28	12.57	12.57	3	0.13	0.05	0.22	0.00	0.00	24.0
38	83	-9396	-3265	-117	0	-1661	1646	6.28	6.28	12.57	12.57	3	0.10	0.06	0.28	0.00	0.00	24.0
39	83	-10606	-222	-666	0	295	-57	6.28	6.28	12.57	12.57	3	0.01	0.01	0.07	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	165	-9492	-98	-148	0	-1148	-237	6.28	6.28	12.57	12.57	3	0.04	0.00	0.01	0.00	0.00	24.0
2	165	-7485	655	-172	0	-1102	-26	6.28	6.28	12.57	12.57	2	0.06	0.01	0.06	0.00	0.00	24.0
3	165	-7478	647	-63	0	-630	-28	6.28	6.28	12.57	12.57	2	0.03	0.01	0.06	0.00	0.00	24.0
4	165	-7123	-798	-166	0	-1136	-337	6.28	6.28	12.57	12.57	2	0.07	0.01	0.07	0.00	0.00	24.0
5	165	-7117	-806	-57	0	-664	-339	6.28	6.28	12.57	12.57	2	0.05	0.01	0.07	0.00	0.00	24.0
6	165	-7366	156	-297	0	-1665	-132	6.28	6.28	12.57	12.57	2	0.09	0.01	0.03	0.00	0.00	24.0
7	165	-7344	129	67	0	-91	-140	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
8	165	-7257	-280	-295	0	-1675	-225	6.28	6.28	12.57	12.57	2	0.09	0.01	0.03	0.00	0.00	24.0
9	165	-7236	-307	69	0	-101	-233	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
10	165	-7485	655	-172	0	-1102	-26	6.28	6.28	12.57	12.57	2	0.06	0.01	0.06	0.00	0.00	24.0
11	165	-7478	647	-63	0	-630	-28	6.28	6.28	12.57	12.57	2	0.03	0.01	0.06	0.00	0.00	24.0
12	165	-7123	-798	-166	0	-1136	-337	6.28	6.28	12.57	12.57	2	0.07	0.01	0.07	0.00	0.00	24.0
13	165	-7117	-806	-57	0	-664	-339	6.28	6.28	12.57	12.57	2	0.05	0.01	0.07	0.00	0.00	24.0
14	165	-7366	156	-297	0	-1665	-132	6.28	6.28	12.57	12.57	2	0.09	0.01	0.03	0.00	0.00	24.0
15	165	-7344	129	67	0	-91	-140	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
16	165	-7257	-280	-295	0	-1675	-225	6.28	6.28	12.57	12.57	2	0.09	0.01	0.03	0.00	0.00	24.0
17	165	-7236	-307	69	0	-101	-233	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
18	165	-11925	1398	-422	0	-2715	246	6.28	6.28	12.57	12.57	3	0.10	0.03	0.12	0.00	0.00	24.0
19	165	-9784	-2173	-237	0	-2166	-726	6.28	6.28	12.57	12.57	3	0.09	0.04	0.18	0.00	0.00	24.0
20	165	-10512	-347	-378	0	-800	-241	6.28	6.28	12.57	12.57	3	0.03	0.01	0.04	0.00	0.00	24.0
37	165	-12320	2686	-426	0	-2480	570	6.28	6.28	12.57	12.57	3	0.10	0.05	0.22	0.00	0.00	24.0
38	165	-8753	-3265	-117	0	-1564	-1048	6.28	6.28	12.57	12.57	3	0.08	0.06	0.28	0.00	0.00	24.0
39	165	-9962	-222	-353	0	712	-241	6.28	6.28	12.57	12.57	3	0.03	0.01	0.04	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	248	-8848	-98	-148	0	-1026	-318	6.28	6.28	12.57	12.57	3	0.04	0.00	0.02	0.00	0.00	24.0
2	248	-6990	655	-172	0	-961	515	6.28	6.28	12.57	12.57	2	0.07	0.01	0.06	0.00	0.00	24.0
3	248	-6983	647	-63	0	-578	506	6.28	6.28	12.57	12.57	2	0.05	0.01	0.06	0.00	0.00	24.0
4	248	-6628	-798	-166	0	-1000	-995	6.28	6.28	12.57	12.57	2	0.09	0.01	0.07	0.00	0.00	24.0
5	248	-6622	-806	-57	0	-617	-1004	6.28	6.28	12.57	12.57	2	0.08	0.01	0.08	0.00	0.00	24.0
6	248	-6871	156	-297	0	-1420	-3	6.28	6.28	12.57	12.57	2	0.07	0.01	0.03	0.00	0.00	24.0
7	248	-6849	129	67	0	-146	-33	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
8	248	-6762	-280	-295	0	-1432	-456	6.28	6.28	12.57	12.57	2	0.09	0.01	0.03	0.00	0.00	24.0
9	248	-6741	-307	69	0	-158	-486	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
10	248	-6990	655	-172	0	-961	515	6.28	6.28	12.57	12.57	2	0.07	0.01	0.06	0.00	0.00	24.0
11	248	-6983	647	-63	0	-578	506	6.28	6.28	12.57	12.57	2	0.05	0.01	0.06	0.00	0.00	24.0
12	248	-6628	-798	-166	0	-1000	-995	6.28	6.28	12.57	12.57	2	0.09	0.01	0.07	0.00	0.00	24.0
13	248	-6622	-806	-57	0	-617	-1004	6.28	6.28	12.57	12.57	2	0.08	0.01	0.08	0.00	0.00	24.0
14	248	-6871	156	-297	0	-1420	-3	6.28	6.28	12.57	12.57	2	0.07	0.01	0.03	0.00	0.00	24.0
15	248	-6849	129	67	0	-146	-33	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
16	248	-6762	-280	-295	0	-1432	-456	6.28	6.28	12.57	12.57	2	0.09	0.01	0.03	0.00	0.00	24.0
17	248	-6741	-307	69	0	-158	-486	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
18	248	-11282	1398	-422	0	-2367	1399	6.28	6.28	12.57	12.57	3	0.11	0.03	0.12	0.00	0.00	24.0
19	248	-9142	-2173	-237	0	-1970	-2518	6.28	6.28	12.57	12.57	3	0.15	0.04	0.21	0.00	0.00	24.0
20	248	-9868	-347	-222	0	-554	-527	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
37	248	-11675	2686	-426	0	-2128	2786	6.28	6.28	12.57	12.57	3	0.16	0.05	0.25	0.00	0.00	24.0
38	248	-8110	-3265	-117	0	-1468	-3742	6.28	6.28	12.57	12.57	3	0.22	0.06	0.31	0.00	0.00	24.0
39	248	-9319	-222	-92	0	892	-424	6.28	6.28	12.57	12.57	3	0.04	0.00	0.02	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	330	-8204	-98	-148	0	-903	-399	6.28	6.28	12.57	12.57	3	0.04	0.00	0.02	0.00	0.00	24.0
2	330	-6495	655	-172	0	-819	1056	6.28	6.28	12.57	12.57	2	0.09	0.01	0.06	0.00	0.00	24.0
3	330	-6488	647	-63	0	-527	1040	6.28	6.28	12.57	12.57	2	0.08	0.01	0.06	0.00	0.00	24.0
4	330	-6133	-798	-166	0	-863	-1654	6.28	6.28	12.57	12.57	2	0.13	0.01	0.08	0.00	0.00	24.0
5	330	-6127	-806	-57	0	-571	-1669	6.28	6.28	12.57	12.57	2	0.12	0.01	0.08	0.00	0.00	24.0
6	330	-6376	156	-297	0	-1175	126	6.28	6.28	12.57	12.57	2	0.07	0.01	0.03	0.00	0.00	24.0
7	330	-6354	129	67	0	-201	73	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
8	330	-6267	-280	-295	0	-1188	-687	6.28	6.28	12.57	12.57	2	0.09	0.01	0.03	0.00	0.00	24.0
9	330	-6246	-307	69	0	-215	-739	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
10	330	-6495	655	-172	0	-819	1056	6.28	6.28	12.57	12.57	2	0.09	0.01	0.06	0.00	0.00	24.0
11	330	-6488	647	-63	0	-527	1040	6.28	6.28	12.57	12.57	2	0.08	0.01	0.06	0.00	0.00	24.0
12	330	-6133	-798	-166	0	-863	-1654	6.28	6.28	12.57	12.57	2	0.13	0.01	0.08	0.00	0.00	24.0
13	330	-6127	-806	-57	0	-571	-1669	6.28	6.28	12.57	12.57	2	0.12	0.01	0.08	0.00	0.00	24.0
14	330	-6376	156	-297	0	-1175	126	6.28	6.28	12.57	12.57	2	0.07	0.01	0.03	0.00	0.00	24.0
15	330	-6354	129	67	0	-201	73	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
16	330	-6267	-280	-295	0	-1188	-687	6.28	6.28	12.57	12.57	2	0.09	0.01	0.03	0.00	0.00	24.0
17	330	-6246	-307	69	0	-215	-739	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
18	330	-10640	1398	-422	0	-2018	2552	6.28	6.28	12.57	12.57	3	0.15	0.03	0.13	0.00	0.00	24.0
19	330	-8499	-2173	-237	0	-1774	-4311	6.28	6.28	12.57	12.57	3	0.25	0.04	0.21	0.00	0.00	24.0
20	330	-9224	-347	-97	0	-424	-814	6.28	6.28	12.57	12.57	3	0.05	0.01	0.03	0.00	0.00	24.0
37	330	-11030	2686	-426	0	-1777	5002	6.28	6.28	12.57	12.57	3	0.28	0.05	0.25	0.00	0.00	24.0
38	330	-7466	-3265	-117	0	-1371	-6436	6.28	6.28	12.57	12.57	3	0.37	0.06	0.32	0.00	0.00	24.0
39	330	-8675	-222	116	0	879	-608	6.28	6.28	12.57	12.57	3	0.05	0.00	0.02	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

VERIFICA NODO IN TESTA AL PILASTRO, NODO NUM. 295 NON CONFINATO

(par.7.2.2 NTC2018 "La domanda di resistenza valutata con i criteri della progettazione in capacità può essere assunta non superiore alla domanda di resistenza valutata per il caso di comportamento strutturale non dissipativo.")

PROGETTAZIONE IN CAPACITA'

Asse loc. pilastro y nodo INTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 50.0 cm, hjc= 30.0 cm

Asse loc. pilastro z nodo: --

FxMin,inf	FxMin,sup	FxMax,sup	FySup	FzSup	Vjbdy	Vjbdz	Vres,y	Vres,z	I.R.compr.	Ashy	Ashz	PASSO	Nota
daN					daN		daN			cmq		cm	

-6127	-3123	-3219	193	92	35040	--	130251	--	0.27	8.79	--	5.17							

VERIFICA DI RESISTENZA CON SOLLECITAZIONI COMPORTAMENTO NON DISSIPATIVO

Asse loc. pilastro y nodo INTERNO: Hjw= 40.0 cm, bj= 50.0 cm, hjc= 30.0 cm, db1= 45.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb,1	Mb,2	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-3219	-6495	-1751	-1260	200	1012	130251	0.01	0.00	40.00	
3	-3210	-6488	-1753	-1257	193	1032	130254	0.01	0.00	40.00	
4	-3131	-6133	-43	-2512	290	5807	130279	0.04	0.00	40.00	
5	-3123	-6127	-45	-2509	282	5802	130282	0.04	0.00	40.00	
6	-3198	-6376	-1150	-1701	240	1120	130258	0.01	0.00	40.00	
7	-3169	-6354	-1158	-1692	216	1103	130267	0.01	0.00	40.00	
8	-3172	-6267	-638	-2077	267	3286	130266	0.03	0.00	40.00	
9	-3143	-6246	-646	-2067	242	3267	130275	0.03	0.00	40.00	
10	-3219	-6495	-1751	-1260	200	1012	130251	0.01	0.00	40.00	
11	-3210	-6488	-1753	-1257	193	1032	130254	0.01	0.00	40.00	
12	-3131	-6133	-43	-2512	290	5807	130279	0.04	0.00	40.00	
13	-3123	-6127	-45	-2509	282	5802	130282	0.04	0.00	40.00	
14	-3198	-6376	-1150	-1701	240	1120	130258	0.01	0.00	40.00	
15	-3169	-6354	-1158	-1692	216	1103	130267	0.01	0.00	40.00	
16	-3172	-6267	-638	-2077	267	3286	130266	0.03	0.00	40.00	
17	-3143	-6246	-646	-2067	242	3267	130275	0.03	0.00	40.00	

CONFRONTO E SINTESI CONCLUSIVE (si assume in ogni caso passo <= 15 cm)

I.R.compr.	Ashy	Ashz	PASSO	Nota
	cmq		cm	
0.04	--	--	15.00	**VERIFICATO**

ASTA NUM. 37 NI 296 NF 297 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 15C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-15400	-162	-359	0	-1334	343	6.28	6.28	12.57	12.57	3	0.05	0.01	0.03	0.00	0.00	24.0
2	0	-11530	546	-328	0	-1404	-975	6.28	6.28	12.57	12.57	2	0.11	0.01	0.05	0.00	0.00	24.0
3	0	-11450	540	-224	0	-650	-964	6.28	6.28	12.57	12.57	2	0.08	0.01	0.05	0.00	0.00	24.0
4	0	-12250	-790	-329	0	-1402	1492	6.28	6.28	12.57	12.57	2	0.13	0.01	0.07	0.00	0.00	24.0
5	0	-12160	-796	-225	0	-648	1503	6.28	6.28	12.57	12.57	2	0.11	0.01	0.07	0.00	0.00	24.0
6	0	-11880	86	-450	0	-2283	-125	6.28	6.28	12.57	12.57	2	0.12	0.01	0.04	0.00	0.00	24.0
7	0	-11600	65	-102	0	231	-87	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
8	0	-12100	-315	-451	0	-2282	615	6.28	6.28	12.57	12.57	2	0.13	0.01	0.04	0.00	0.00	24.0
9	0	-11810	-336	-102	0	231	653	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
10	0	-11530	546	-328	0	-1404	-975	6.28	6.28	12.57	12.57	2	0.11	0.01	0.05	0.00	0.00	24.0
11	0	-11450	540	-224	0	-650	-964	6.28	6.28	12.57	12.57	2	0.08	0.01	0.05	0.00	0.00	24.0
12	0	-12250	-790	-329	0	-1402	1492	6.28	6.28	12.57	12.57	2	0.13	0.01	0.07	0.00	0.00	24.0
13	0	-12160	-796	-225	0	-648	1503	6.28	6.28	12.57	12.57	2	0.11	0.01	0.07	0.00	0.00	24.0
14	0	-11880	86	-450	0	-2283	-125	6.28	6.28	12.57	12.57	2	0.12	0.01	0.04	0.00	0.00	24.0
15	0	-11600	65	-102	0	231	-87	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
16	0	-12100	-315	-451	0	-2282	615	6.28	6.28	12.57	12.57	2	0.13	0.01	0.04	0.00	0.00	24.0
17	0	-11810	-336	-102	0	231	653	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
18	0	-19790	1342	-862	0	-3341	-2350	6.28	6.28	12.57	12.57	3	0.16	0.02	0.10	0.00	0.00	24.0
19	0	-20030	-2105	-767	0	-2849	3930	6.28	6.28	12.57	12.57	3	0.22	0.04	0.18	0.00	0.00	24.0
20	0	-19000	-352	-1532	0	-2371	730	6.28	6.28	12.57	12.57	3	0.09	0.03	0.14	0.00	0.00	24.0
37	0	-18250	2564	-748	0	-2937	-4592	6.28	6.28	12.57	12.57	3	0.25	0.05	0.22	0.00	0.00	24.0
38	0	-18640	-3181	-588	0	-2117	5874	6.28	6.28	12.57	12.57	3	0.31	0.06	0.27	0.00	0.00	24.0
39	0	-16930	-259	-1864	0	-1319	540	6.28	6.28	12.57	12.57	3	0.05	0.03	0.17	0.00	0.00	24.0
apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0																		
1	95	-14660	-162	-359	0	-993	189	6.28	6.28	12.57	12.57	3	0.04	0.01	0.03	0.00	0.00	24.0
2	95	-10961	546	-328	0	-1092	-457	6.28	6.28	12.57	12.57	2	0.07	0.01	0.05	0.00	0.00	24.0
3	95	-10880	540	-224	0	-437	-451	6.28	6.28	12.57	12.57	2	0.04	0.01	0.05	0.00	0.00	24.0
4	95	-11679	-790	-329	0	-1089	742	6.28	6.28	12.57	12.57	2	0.08	0.01	0.07	0.00	0.00	24.0
5	95	-11590	-796	-225	0	-434	747	6.28	6.28	12.57	12.57	2	0.06	0.01	0.07	0.00	0.00	24.0
6	95	-11311	86	-450	0	-1855	-44	6.28	6.28	12.57	12.57	2	0.09	0.01	0.04	0.00	0.00	24.0
7	95	-11029	65	-102	0	328	-25	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
8	95	-11530	-315	-451	0	-1854	316	6.28	6.28	12.57	12.57	2	0.10	0.01	0.04	0.00	0.00	24.0
9	95	-11240	-336	-102	0	329	334	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
10	95	-10961	546	-328	0	-1092	-457	6.28	6.28	12.57	12.57	2	0.07	0.01	0.05	0.00	0.00	24.0
11	95	-10880	540	-224	0	-437	-451	6.28	6.28	12.57	12.57	2	0.04	0.01	0.05	0.00	0.00	24.0
12	95	-11679	-790	-329	0	-1089	742	6.28	6.28	12.57	12.57	2	0.08	0.01	0.07	0.00	0.00	24.0
13	95	-11590	-796	-225	0	-434	747	6.28	6.28	12.57	12.57	2	0.06	0.01	0.07	0.00	0.00	24.0
14	95	-11311	86	-450	0	-1855	-44	6.28	6.28	12.57	12.57	2	0.09	0.01	0.04	0.00	0.00	24.0
15	95	-11029	65	-102	0	328	-25	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
16	95	-11530	-315	-451	0	-1854	316	6.28	6.28	12.57	12.57	2	0.10	0.01	0.04	0.00	0.00	24.0
17	95	-11240	-336	-102	0	329	334	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
18	95	-19048	1342	-862	0	-2522	-1075	6.28	6.28	12.57	12.57	3	0.10	0.02	0.10	0.00	0.00	24.0
19	95	-19288	-2105	-767	0	-2121	1930	6.28	6.28	12.57	12.57	3	0.12	0.04	0.16	0.00	0.00	24.0
20	95	-18260	-352	-1280	0	-1038	396	6.28	6.28	12.57	12.57	3	0.04	0.02	0.11	0.00	0.00	24.0
37	95	-17510	2564	-748	0	-2227	-2156	6.28	6.28	12.57	12.57	3	0.13	0.05	0.20	0.00	0.00	24.0
38	95	-17900	-3181	-588	0	-1558	2852	6.28	6.28	12.57	12.57	3	0.16	0.06	0.27	0.00	0.00	24.0
39	95	-16190	-259	-1443	0	247	295	6.28	6.28	12.57	12.57	3	0.02	0.02	0.13	0.00	0.00	24.0
apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0																		
1	190	-13920	-162	-359	0	-651	35	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
2	190	-10392	546	-328	0	-781	62	6.28	6.28	12.57	12.57	2	0.04	0.01	0.05	0.00	0.00	24.0
3	190	-10309	540	-224	0	-225	61	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
4	190	-11108	-790	-329	0	-776	-9	6.28	6.28	12.57	12.57	2	0.04	0.01	0.07	0.00	0.00	24.0
5	190	-11020	-796	-225	0	-221	-9	6.28	6.28	12.57	12.57	2	0.01	0.01	0.07	0.00	0.00	24.0
6	190	-10742	86	-450	0	-1427	38	6.28	6.28	12.57	12.57	2	0.07	0.01	0.04	0.00	0.00	24.0
7	190	-10458	65	-102	0	424	37	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
8	190	-10959	-315	-451	0	-1426	17	6.28	6.28	12.57	12.57	2	0.07	0.01	0.04	0.00	0.00	24.0
9	190	-10670	-336	-102	0	426	15	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
10	190	-10392	546	-328	0	-781	62	6.28	6.28	12.57	12.57	2	0.04	0.01	0.05	0.00	0.00	24.0

11	190	-10309	540	-224	0	-225	61	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
12	190	-11108	-790	-329	0	-776	-9	6.28	6.28	12.57	12.57	2	0.04	0.01	0.07	0.00	0.00	24.0
13	190	-11020	-796	-225	0	-221	-9	6.28	6.28	12.57	12.57	2	0.01	0.01	0.07	0.00	0.00	24.0
14	190	-10742	86	-450	0	-1427	38	6.28	6.28	12.57	12.57	2	0.07	0.01	0.04	0.00	0.00	24.0
15	190	-10458	65	-102	0	424	37	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
16	190	-10959	-315	-451	0	-1426	17	6.28	6.28	12.57	12.57	2	0.07	0.01	0.04	0.00	0.00	24.0
17	190	-10670	-336	-102	0	426	15	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
18	190	-18305	1342	-862	0	-1703	201	6.28	6.28	12.57	12.57	3	0.06	0.02	0.10	0.00	0.00	24.0
19	190	-18545	-2105	-767	0	-1393	-70	6.28	6.28	12.57	12.57	3	0.05	0.04	0.16	0.00	0.00	24.0
20	190	-17520	-352	-1064	0	72	61	6.28	6.28	12.57	12.57	3	0.00	0.02	0.10	0.00	0.00	24.0
37	190	-16770	2564	-748	0	-1517	280	6.28	6.28	12.57	12.57	3	0.06	0.05	0.20	0.00	0.00	24.0
38	190	-17160	-3181	-588	0	-1000	-170	6.28	6.28	12.57	12.57	3	0.04	0.06	0.25	0.00	0.00	24.0
39	190	-15450	-259	-1083	0	1443	49	6.28	6.28	12.57	12.57	3	0.05	0.02	0.10	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	285	-13180	-162	-359	0	-310	-120	6.28	6.28	12.57	12.57	3	0.01	0.01	0.03	0.00	0.00	24.0
2	285	-9824	546	-328	0	-469	581	6.28	6.28	12.57	12.57	2	0.05	0.01	0.05	0.00	0.00	24.0
3	285	-9738	540	-224	0	-13	574	6.28	6.28	12.57	12.57	2	0.03	0.01	0.05	0.00	0.00	24.0
4	285	-10538	-790	-329	0	-464	-759	6.28	6.28	12.57	12.57	2	0.06	0.01	0.07	0.00	0.00	24.0
5	285	-10450	-796	-225	0	-7	-765	6.28	6.28	12.57	12.57	2	0.05	0.01	0.07	0.00	0.00	24.0
6	285	-10174	86	-450	0	-999	119	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
7	285	-9888	65	-102	0	521	98	6.28	6.28	12.57	12.57	2	0.03	0.00	0.01	0.00	0.00	24.0
8	285	-10388	-315	-451	0	-998	-282	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
9	285	-10100	-336	-102	0	523	-303	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
10	285	-9824	546	-328	0	-469	581	6.28	6.28	12.57	12.57	2	0.05	0.01	0.05	0.00	0.00	24.0
11	285	-9738	540	-224	0	-13	574	6.28	6.28	12.57	12.57	2	0.03	0.01	0.05	0.00	0.00	24.0
12	285	-10538	-790	-329	0	-464	-759	6.28	6.28	12.57	12.57	2	0.06	0.01	0.07	0.00	0.00	24.0
13	285	-10450	-796	-225	0	-7	-765	6.28	6.28	12.57	12.57	2	0.05	0.01	0.07	0.00	0.00	24.0
14	285	-10174	86	-450	0	-999	119	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
15	285	-9888	65	-102	0	521	98	6.28	6.28	12.57	12.57	2	0.03	0.00	0.01	0.00	0.00	24.0
16	285	-10388	-315	-451	0	-998	-282	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
17	285	-10100	-336	-102	0	523	-303	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
18	285	-17562	1342	-862	0	-883	1476	6.28	6.28	12.57	12.57	3	0.08	0.02	0.12	0.00	0.00	24.0
19	285	-17802	-2105	-767	0	-664	-2069	6.28	6.28	12.57	12.57	3	0.11	0.04	0.18	0.00	0.00	24.0
20	285	-16780	-352	-884	0	995	-273	6.28	6.28	12.57	12.57	3	0.04	0.02	0.08	0.00	0.00	24.0
37	285	-16030	2564	-748	0	-806	2716	6.28	6.28	12.57	12.57	3	0.15	0.05	0.22	0.00	0.00	24.0
38	285	-16420	-3181	-588	0	-441	-3192	6.28	6.28	12.57	12.57	3	0.17	0.06	0.28	0.00	0.00	24.0
39	285	-14710	-259	-783	0	2324	-197	6.28	6.28	12.57	12.57	3	0.08	0.01	0.07	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	380	-12440	-162	-359	0	32	-274	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
2	380	-9255	546	-328	0	-157	1100	6.28	6.28	12.57	12.57	2	0.07	0.01	0.05	0.00	0.00	24.0
3	380	-9168	540	-224	0	200	1087	6.28	6.28	12.57	12.57	2	0.07	0.01	0.05	0.00	0.00	24.0
4	380	-9967	-790	-329	0	-151	-1509	6.28	6.28	12.57	12.57	2	0.09	0.01	0.07	0.00	0.00	24.0
5	380	-9880	-796	-225	0	206	-1521	6.28	6.28	12.57	12.57	2	0.10	0.01	0.08	0.00	0.00	24.0
6	380	-9605	86	-450	0	-572	201	6.28	6.28	12.57	12.57	2	0.04	0.01	0.05	0.00	0.00	24.0
7	380	-9317	65	-102	0	618	160	6.28	6.28	12.57	12.57	2	0.04	0.00	0.01	0.00	0.00	24.0
8	380	-9818	-315	-451	0	-570	-582	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
9	380	-9530	-336	-102	0	620	-622	6.28	6.28	12.57	12.57	2	0.06	0.01	0.03	0.00	0.00	24.0
10	380	-9255	546	-328	0	-157	1100	6.28	6.28	12.57	12.57	2	0.07	0.01	0.05	0.00	0.00	24.0
11	380	-9168	540	-224	0	200	1087	6.28	6.28	12.57	12.57	2	0.07	0.01	0.05	0.00	0.00	24.0
12	380	-9967	-790	-329	0	-151	-1509	6.28	6.28	12.57	12.57	2	0.09	0.01	0.07	0.00	0.00	24.0
13	380	-9880	-796	-225	0	206	-1521	6.28	6.28	12.57	12.57	2	0.10	0.01	0.08	0.00	0.00	24.0
14	380	-9605	86	-450	0	-572	201	6.28	6.28	12.57	12.57	2	0.04	0.01	0.05	0.00	0.00	24.0
15	380	-9317	65	-102	0	618	160	6.28	6.28	12.57	12.57	2	0.04	0.00	0.01	0.00	0.00	24.0
16	380	-9818	-315	-451	0	-570	-582	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
17	380	-9530	-336	-102	0	620	-622	6.28	6.28	12.57	12.57	2	0.06	0.01	0.03	0.00	0.00	24.0
18	380	-16820	1342	-862	0	-64	2751	6.28	6.28	12.57	12.57	3	0.15	0.02	0.12	0.00	0.00	24.0
19	380	-17060	-2105	-767	0	64	-4069	6.28	6.28	12.57	12.57	3	0.22	0.04	0.18	0.00	0.00	24.0
20	380	-16040	-352	-740	0	1763	-607	6.28	6.28	12.57	12.57	3	0.07	0.01	0.07	0.00	0.00	24.0
37	380	-15290	2564	-748	0	-96	5152	6.28	6.28	12.57	12.57	3	0.28	0.05	0.23	0.00	0.00	24.0
38	380	-15680	-3181	-588	0	117	-6214	6.28	6.28	12.57	12.57	3	0.33	0.06	0.28	0.00	0.00	24.0
39	380	-13970	-259	-544	0	2950	-443	6.28	6.28	12.57	12.57	3	0.11	0.01	0.05	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

VERIFICA NODO IN TESTA AL PILASTRO, NODO NUM. 297 NON CONFINATO

(par.7.2.2 NTC2018 "La domanda di resistenza valutata con i criteri della progettazione in capacità può essere assunta non superiore alla domanda di resistenza valutata per il caso di comportamento strutturale non dissipativo.")

PROGETTAZIONE IN CAPACITA'

Asse loc. pilastro y nodo INTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 50.0 cm, hjc= 30.0 cm
Asse loc. pilastro z nodo: --

FxMin,inf	FxMin,sup	FxMax,sup	FySup	FzSup	Vjbdy	Vjbdz	Vres,y	Vres,z	I.R.compr.	Ashy	Ashz	PASSO	Nota
daN					daN		daN			cmq		cm	
-9168	-5460	-6290	1	20	35232	--	129281	--	0.27	8.75	--	5.19	

VERIFICA DI RESISTENZA CON SOLLECITAZIONI COMPORTAMENTO NON DISSIPATIVO

Asse loc. pilastro y nodo INTERNO: Hjw= 40.0 cm, bj= 50.0 cm, hjc= 30.0 cm, db1= 45.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb,1	Mb,2	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-5550	-9255	-2125	-1159	33	2352	129515	0.02	0.00	40.00	
3	-5460	-9168	-2126	-1165	31	2341	129544	0.02	0.00	40.00	
4	-6290	-9967	-874	-2343	10	3616	129281	0.03	0.00	40.00	
5	-6201	-9880	-875	-2349	12	3627	129309	0.03	0.00	40.00	
6	-5913	-9605	-1686	-1566	20	276	129400	0.00	0.00	40.00	
7	-5615	-9317	-1689	-1587	14	238	129495	0.00	0.00	40.00	
8	-6136	-9818	-1311	-1921	7	1499	129329	0.01	0.00	40.00	
9	-5837	-9530	-1314	-1942	1	1549	129424	0.01	0.00	40.00	
10	-5550	-9255	-2125	-1159	33	2352	129515	0.02	0.00	40.00	
11	-5460	-9168	-2126	-1165	31	2341	129544	0.02	0.00	40.00	
12	-6290	-9967	-874	-2343	10	3616	129281	0.03	0.00	40.00	
13	-6201	-9880	-875	-2349	12	3627	129309	0.03	0.00	40.00	
14	-5913	-9605	-1686	-1566	20	276	129400	0.00	0.00	40.00	
15	-5615	-9317	-1689	-1587	14	238	129495	0.00	0.00	40.00	
16	-6136	-9818	-1311	-1921	7	1499	129329	0.01	0.00	40.00	
17	-5837	-9530	-1314	-1942	1	1549	129424	0.01	0.00	40.00	

CONFRONTO E SINTESI CONCLUSIVE (si assume in ogni caso passo <= 15 cm)

I.R.compr.	Ashy	Ashz	PASSO	Nota
	cmq		cm	
0.03	--	--	15.00	**VERIFICATO**

ASTA NUM. 38 NI 299 NF 294 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 10B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-27370	-31	286	0	183	31	6.28	6.28	12.57	12.57	3	0.01	0.00	0.02	0.00	0.00	24.0
2	0	-21210	326	236	0	95	-827	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
3	0	-21190	321	188	0	130	-814	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
4	0	-20920	-369	252	0	152	862	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
5	0	-20900	-374	204	0	187	875	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
6	0	-21130	89	297	0	73	-251	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
7	0	-21070	72	139	0	192	-208	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
8	0	-21040	-120	302	0	90	256	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
9	0	-20980	-137	143	0	209	298	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
10	0	-21210	326	236	0	95	-827	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
11	0	-21190	321	188	0	130	-814	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
12	0	-20920	-369	252	0	152	862	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
13	0	-20900	-374	204	0	187	875	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
14	0	-21130	89	297	0	73	-251	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
15	0	-21070	72	139	0	192	-208	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
16	0	-21040	-120	302	0	90	256	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
17	0	-20980	-137	143	0	209	298	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
18	0	-30330	1173	524	0	193	-2779	6.28	6.28	12.57	12.57	3	0.13	0.02	0.09	0.00	0.00	24.0
19	0	-28540	-1074	501	0	428	2568	6.28	6.28	12.57	12.57	3	0.13	0.02	0.08	0.00	0.00	24.0
20	0	-29110	41	193	0	-149	-92	6.28	6.28	12.57	12.57	3	0.01	0.00	0.02	0.00	0.00	24.0
37	0	-30240	1896	455	0	66	-4518	6.28	6.28	12.57	12.57	3	0.22	0.03	0.14	0.00	0.00	24.0
38	0	-27250	-1848	417	0	458	4393	6.28	6.28	12.57	12.57	3	0.22	0.03	0.14	0.00	0.00	24.0
39	0	-28200	10	-97	0	-504	-40	6.28	6.28	12.57	12.57	3	0.02	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	97	-26610	-31	286	0	-96	1	6.28	6.28	12.57	12.57	3	0.00	0.00	0.02	0.00	0.00	24.0
2	97	-20625	326	236	0	-135	-509	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
3	97	-20605	321	188	0	-53	-501	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
4	97	-20335	-369	252	0	-94	502	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
5	97	-20315	-374	204	0	-12	510	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
6	97	-20545	89	297	0	-216	-164	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
7	97	-20485	72	139	0	57	-138	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
8	97	-20455	-120	302	0	-204	139	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
9	97	-20395	-137	143	0	69	165	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
10	97	-20625	326	236	0	-135	-509	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
11	97	-20605	321	188	0	-53	-501	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
12	97	-20335	-369	252	0	-94	502	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
13	97	-20315	-374	204	0	-12	510	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
14	97	-20545	89	297	0	-216	-164	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
15	97	-20485	72	139	0	57	-138	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
16	97	-20455	-120	302	0	-204	139	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
17	97	-20395	-137	143	0	69	165	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
18	97	-29570	1173	524	0	-318	-1636	6.28	6.28	12.57	12.57	3	0.08	0.02	0.09	0.00	0.00	24.0
19	97	-27778	-1074	501	0	-60	1521	6.28	6.28	12.57	12.57	3	0.07	0.02	0.08	0.00	0.00	24.0
20	97	-28350	41	193	0	-337	-52	6.28	6.28	12.57	12.57	3	0.01	0.00	0.02	0.00	0.00	24.0
37	97	-29480	1896	455	0	-377	-2670	6.28	6.28	12.57	12.57	3	0.13	0.03	0.14	0.00	0.00	24.0
38	97	-26490	-1848	417	0	52	2592	6.28	6.28	12.57	12.57	3	0.13	0.03	0.14	0.00	0.00	24.0
39	97	-27440	10	-97	0	-410	-30	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	195	-25850	-31	286	0	-375	-30	6.28	6.28	12.57	12.57	3	0.01	0.00	0.02	0.00	0.00	24.0
2	195	-20040	326	236	0	-366	-192	6.28	6.28	12.57	12.57	2	0.02	0.01	0.02	0.00	0.00	24.0
3	195	-20020	321	188	0	-237	-189	6.28	6.28	12.57	12.57	2	0.02	0.01	0.02	0.00	0.00	24.0
4	195	-19750	-369	252	0	-339	142	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
5	195	-19730	-374	204	0	-211	145	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
6	195	-19960	89	297	0	-506	-78	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
7	195	-19900	72	139	0	-78	-68	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
8	195	-19870	-120	302	0	-498	22	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
9	195	-19810	-137	143	0	-70	32	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
10	195	-20040	326	236	0	-366	-192	6.28	6.28	12.57	12.57	2	0.02	0.01	0.02	0.00	0.00	24.0
11	195	-20020	321	188	0	-237	-189	6.28	6.28	12.57	12.57	2	0.02	0.01	0.02	0.00	0.00	24.0
12	195	-19750	-369	252	0	-339	142	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
13	195	-19730	-374	204	0	-211	145	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
14	195	-19960	89	297	0	-506	-78	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
15	195	-19900	72	139	0	-78	-68	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
16	195	-19870	-120	302	0	-498	22	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
17	195	-19810	-137	143	0	-70	32	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
18	195	-28810	1173	524	0	-829	-492	6.28	6.28	12.57	12.57	3	0.04	0.02	0.08	0.00	0.00	24.0
19	195	-27015	-1074	501	0	-549	475	6.28	6.28	12.57	12.57	3	0.03	0.02	0.08	0.00	0.00	24.0
20	195	-27590	41	193	0	-525	-12	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
37	195	-28720	1896	455	0	-821	-821	6.28	6.28	12.57	12.57	3	0.05	0.03	0.14	0.00	0.00	24.0
38	195	-25730	-1848	417	0	-354	790	6.28	6.28	12.57	12.57	3	0.04	0.03	0.15	0.00	0.00	24.0
39	195	-26680	10	-97	0	-315	-20	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	292	-25090	-31	286	0	-654	-61	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
2	292	-19455	326	236	0	-596	126	6.28	6.28	12.57	12.57	2	0.03	0.01	0.02	0.00	0.00	24.0
3	292	-19435	321	188	0	-421	124	6.28	6.28	12.57	12.57	2	0.02	0.01	0.02	0.00	0.00	24.0
4	292	-19165	-369	252	0	-585	-218	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
5	292	-19145	-374	204	0	-410	-219	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
6	292	-19375	89	297	0	-795	8	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
7	292	-19315	72	139	0	-213	2	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
8	292	-19285	-120	302	0	-792	-95	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
9	292	-19225	-137	143	0	-210	-101	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
10	292	-19455	326	236	0	-596	126	6.28	6.28	12.57	12.57	2	0.03	0.01	0.02	0.00	0.00	24.0
11	292	-19435	321	188	0	-421	124	6.28	6.28	12.57	12.57	2	0.02	0.01	0.02	0.00	0.00	24.0
12	292	-19165	-369	252	0	-585	-218	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
13	292	-19145	-374	204	0	-410	-219	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
14	292	-19375	89	297	0	-795	8	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0

15	292	-19315	72	139	0	-213	2	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
16	292	-19285	-120	302	0	-792	-95	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
17	292	-19225	-137	143	0	-210	-101	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
18	292	-28050	1173	524	0	-1340	651	6.28	6.28	12.57	12.57	3	0.05	0.02	0.08	0.00	0.00	24.0
19	292	-26252	-1074	501	0	-1037	-572	6.28	6.28	12.57	12.57	3	0.04	0.02	0.08	0.00	0.00	24.0
20	292	-26830	41	193	0	-714	29	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
37	292	-27960	1896	455	0	-1264	1027	6.28	6.28	12.57	12.57	3	0.06	0.03	0.13	0.00	0.00	24.0
38	292	-24970	-1848	417	0	-761	-1011	6.28	6.28	12.57	12.57	3	0.05	0.03	0.15	0.00	0.00	24.0
39	292	-25920	10	-97	0	-220	-10	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	390	-24330	-31	286	0	-933	-91	6.28	6.28	12.57	12.57	3	0.03	0.00	0.02	0.00	0.00	24.0
2	390	-18870	326	236	0	-826	444	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
3	390	-18850	321	188	0	-605	437	6.28	6.28	12.57	12.57	2	0.04	0.01	0.02	0.00	0.00	24.0
4	390	-18580	-369	252	0	-830	-578	6.28	6.28	12.57	12.57	2	0.06	0.01	0.03	0.00	0.00	24.0
5	390	-18560	-374	204	0	-609	-584	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
6	390	-18790	89	297	0	-1085	94	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
7	390	-18730	72	139	0	-349	72	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
8	390	-18700	-120	302	0	-1086	-212	6.28	6.28	12.57	12.57	2	0.06	0.01	0.03	0.00	0.00	24.0
9	390	-18640	-137	143	0	-350	-234	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
10	390	-18870	326	236	0	-826	444	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
11	390	-18850	321	188	0	-605	437	6.28	6.28	12.57	12.57	2	0.04	0.01	0.02	0.00	0.00	24.0
12	390	-18580	-369	252	0	-830	-578	6.28	6.28	12.57	12.57	2	0.06	0.01	0.03	0.00	0.00	24.0
13	390	-18560	-374	204	0	-609	-584	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
14	390	-18790	89	297	0	-1085	94	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
15	390	-18730	72	139	0	-349	72	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
16	390	-18700	-120	302	0	-1086	-212	6.28	6.28	12.57	12.57	2	0.06	0.01	0.03	0.00	0.00	24.0
17	390	-18640	-137	143	0	-350	-234	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
18	390	-27290	1173	524	0	-1851	1794	6.28	6.28	12.57	12.57	3	0.10	0.02	0.08	0.00	0.00	24.0
19	390	-25490	-1074	501	0	-1526	-1619	6.28	6.28	12.57	12.57	3	0.09	0.02	0.08	0.00	0.00	24.0
20	390	-26070	41	193	0	-902	69	6.28	6.28	12.57	12.57	3	0.03	0.00	0.02	0.00	0.00	24.0
37	390	-27200	1896	455	0	-1708	2876	6.28	6.28	12.57	12.57	3	0.15	0.03	0.15	0.00	0.00	24.0
38	390	-24210	-1848	417	0	-1167	-2813	6.28	6.28	12.57	12.57	3	0.14	0.03	0.15	0.00	0.00	24.0
39	390	-25160	10	-97	0	-126	-0	6.28	6.28	12.57	12.57	3	0.00	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

VERIFICA NODO IN TESTA AL PILASTRO, NODO NUM. 294 NON CONFINATO

(par.7.2.2 NTC2018 "La domanda di resistenza valutata con i criteri della progettazione in capacità può essere assunta non superiore alla domanda di resistenza valutata per il caso di comportamento strutturale non dissipativo.")

PROGETTAZIONE IN CAPACITA'

Asse loc. pilastro y nodo ESTERNO: As2(inf)= 4.02, As1(sup)= 6.03, Hjw= 40.0 cm, bj= 50.0 cm, hjc= 30.0 cm
Asse loc. pilastro z nodo INTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 40.0 cm, hjc= 50.0 cm

FxMin,inf	FxMin,sup	FxMax,sup	FySup	FzSup	Vjbdy	Vjbdz	Vres,y	Vres,z	I.R.compr.	Ashy	Ashz	PASSO	Nota
daN					daN		daN			cmq		cm	
-18560	-10090	-11090	14	2	26411	35231	101484	170331	0.26	2.26	1.81	32.06	

VERIFICA DI RESISTENZA CON SOLLECITAZIONI COMPORTAMENTO NON DISSIPATIVO

Asse loc. pilastro y nodo ESTERNO: Hjw= 40.0 cm, bj= 50.0 cm, hjc= 30.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb	Vb	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-11090	-18870	-847	1621	540	1550	101484	0.02	0.00	40.00	
3	-11080	-18850	-852	1622	523	1581	101487	0.02	0.00	40.00	
4	-10110	-18580	-2677	2240	1021	5589	101801	0.05	0.00	40.00	
5	-10090	-18560	-2683	2242	1038	5587	101807	0.05	0.00	40.00	
6	-10760	-18790	-1481	1835	14	3643	101591	0.04	0.00	40.00	
7	-10720	-18730	-1499	1841	43	3658	101604	0.04	0.00	40.00	
8	-10470	-18700	-2030	2021	455	4558	101684	0.04	0.00	40.00	
9	-10420	-18640	-2048	2027	512	4545	101701	0.04	0.00	40.00	
10	-11090	-18870	-847	1621	540	1550	101484	0.02	0.00	40.00	
11	-11080	-18850	-852	1622	523	1581	101487	0.02	0.00	40.00	
12	-10110	-18580	-2677	2240	1021	5589	101801	0.05	0.00	40.00	
13	-10090	-18560	-2683	2242	1038	5587	101807	0.05	0.00	40.00	
14	-10760	-18790	-1481	1835	14	3643	101591	0.04	0.00	40.00	
15	-10720	-18730	-1499	1841	43	3658	101604	0.04	0.00	40.00	
16	-10470	-18700	-2030	2021	455	4558	101684	0.04	0.00	40.00	
17	-10420	-18640	-2048	2027	512	4545	101701	0.04	0.00	40.00	

Asse loc. pilastro z nodo INTERNO: Hjw= 40.0 cm, bj= 40.0 cm, hjc= 50.0 cm, db1= 45.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb,1	Mb,2	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-11090	-18870	-1776	-1215	144	1241	170331	0.01	0.00	40.00	
3	-11080	-18850	-1535	-1453	23	180	170336	0.00	0.00	40.00	
4	-10110	-18580	-1858	-1283	123	1297	170750	0.01	0.00	40.00	
5	-10090	-18560	-1617	-1522	2	233	170759	0.00	0.00	40.00	
6	-10760	-18790	-2086	-961	278	2501	170473	0.01	0.00	40.00	
7	-10720	-18730	-1283	-1755	126	1040	170490	0.01	0.00	40.00	
8	-10470	-18700	-2111	-982	271	2517	170597	0.01	0.00	40.00	
9	-10420	-18640	-1307	-1775	132	1023	170618	0.01	0.00	40.00	
10	-11090	-18870	-1776	-1215	144	1241	170331	0.01	0.00	40.00	
11	-11080	-18850	-1535	-1453	23	180	170336	0.00	0.00	40.00	
12	-10110	-18580	-1858	-1283	123	1297	170750	0.01	0.00	40.00	
13	-10090	-18560	-1617	-1522	2	233	170759	0.00	0.00	40.00	
14	-10760	-18790	-2086	-961	278	2501	170473	0.01	0.00	40.00	
15	-10720	-18730	-1283	-1755	126	1040	170490	0.01	0.00	40.00	
16	-10470	-18700	-2111	-982	271	2517	170597	0.01	0.00	40.00	
17	-10420	-18640	-1307	-1775	132	1023	170618	0.01	0.00	40.00	

CONFRONTO E SINTESI CONCLUSIVE (si assume in ogni caso passo <= 15 cm)

I.R.compr.	Ashy	Ashz	PASSO	Nota
	cmq		cm	
0.05	--	--	15.00	**VERIFICATO**

ASTA NUM. 39 NI 300 NF 296 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 15B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-37050	142	578	0	698	-198	6.28	6.28	12.57	12.57	3	0.02	0.01	0.04	0.00	0.00	24.0
2	0	-28250	360	462	0	514	-662	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
3	0	-28150	359	423	0	552	-660	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
4	0	-28850	-141	467	0	522	355	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
5	0	-28760	-142	428	0	560	357	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
6	0	-28570	186	509	0	471	-309	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
7	0	-28250	182	380	0	600	-301	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
8	0	-28750	36	510	0	474	-4	6.28	6.28	12.57	12.57	2	0.02	0.01	0.04	0.00	0.00	24.0
9	0	-28430	32	381	0	603	4	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
10	0	-28250	360	462	0	514	-662	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
11	0	-28150	359	423	0	552	-660	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
12	0	-28850	-141	467	0	522	355	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
13	0	-28760	-142	428	0	560	357	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
14	0	-28570	186	509	0	471	-309	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
15	0	-28250	182	380	0	600	-301	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
16	0	-28750	36	510	0	474	-4	6.28	6.28	12.57	12.57	2	0.02	0.01	0.04	0.00	0.00	24.0
17	0	-28430	32	381	0	603	4	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
18	0	-42800	1007	708	0	628	-1833	6.28	6.28	12.57	12.57	3	0.08	0.02	0.07	0.00	0.00	24.0
19	0	-42790	-638	694	0	671	1355	6.28	6.28	12.57	12.57	3	0.06	0.01	0.05	0.00	0.00	24.0
20	0	-41960	182	413	0	270	-240	6.28	6.28	12.57	12.57	3	0.01	0.01	0.03	0.00	0.00	24.0
37	0	-40670	1541	664	0	615	-2883	6.28	6.28	12.57	12.57	3	0.13	0.03	0.11	0.00	0.00	24.0
38	0	-40660	-1200	640	0	687	2430	6.28	6.28	12.57	12.57	3	0.11	0.02	0.08	0.00	0.00	24.0
39	0	-39280	167	172	0	19	-227	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	97	-36290	142	578	0	134	-60	6.28	6.28	12.57	12.57	3	0.01	0.01	0.04	0.00	0.00	24.0
2	97	-27665	360	462	0	63	-311	6.28	6.28	12.57	12.57	2	0.02	0.01	0.04	0.00	0.00	24.0
3	97	-27565	359	423	0	140	-309	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
4	97	-28265	-141	467	0	67	217	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
5	97	-28175	-142	428	0	143	219	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
6	97	-27985	186	509	0	-25	-128	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
7	97	-27665	182	380	0	230	-123	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
8	97	-28165	36	510	0	-24	31	6.28	6.28	12.57	12.57	2	0.00	0.01	0.04	0.00	0.00	24.0
9	97	-27845	32	381	0	231	35	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
10	97	-27665	360	462	0	63	-311	6.28	6.28	12.57	12.57	2	0.02	0.01	0.04	0.00	0.00	24.0
11	97	-27565	359	423	0	140	-309	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
12	97	-28265	-141	467	0	67	217	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
13	97	-28175	-142	428	0	143	219	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
14	97	-27985	186	509	0	-25	-128	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
15	97	-27665	182	380	0	230	-123	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
16	97	-28165	36	510	0	-24	31	6.28	6.28	12.57	12.57	2	0.00	0.01	0.04	0.00	0.00	24.0
17	97	-27845	32	381	0	231	35	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
18	97	-42040	1007	708	0	-62	-852	6.28	6.28	12.57	12.57	3	0.04	0.02	0.07	0.00	0.00	24.0
19	97	-42030	-638	694	0	-5	732	6.28	6.28	12.57	12.57	3	0.03	0.01	0.05	0.00	0.00	24.0
20	97	-41200	182	413	0	-133	-62	6.28	6.28	12.57	12.57	3	0.01	0.01	0.03	0.00	0.00	24.0
37	97	-39910	1541	664	0	-33	-1380	6.28	6.28	12.57	12.57	3	0.06	0.03	0.11	0.00	0.00	24.0
38	97	-39900	-1200	640	0	64	1260	6.28	6.28	12.57	12.57	3	0.06	0.02	0.08	0.00	0.00	24.0
39	97	-38518	167	172	0	-149	-65	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	195	-35530	142	578	0	-430	78	6.28	6.28	12.57	12.57	3	0.01	0.01	0.04	0.00	0.00	24.0
2	195	-27080	360	462	0	-387	40	6.28	6.28	12.57	12.57	2	0.02	0.01	0.04	0.00	0.00	24.0
3	195	-26980	359	423	0	-273	41	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
4	195	-27680	-141	467	0	-389	80	6.28	6.28	12.57	12.57	2	0.02	0.01	0.04	0.00	0.00	24.0
5	195	-27590	-142	428	0	-274	80	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
6	195	-27400	186	509	0	-521	54	6.28	6.28	12.57	12.57	2	0.02	0.01	0.04	0.00	0.00	24.0
7	195	-27080	182	380	0	-140	55	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
8	195	-27580	36	510	0	-521	66	6.28	6.28	12.57	12.57	2	0.02	0.01	0.04	0.00	0.00	24.0
9	195	-27260	32	381	0	-141	67	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
10	195	-27080	360	462	0	-387	40	6.28	6.28	12.57	12.57	2	0.02	0.01	0.04	0.00	0.00	24.0
11	195	-26980	359	423	0	-273	41	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
12	195	-27680	-141	467	0	-389	80	6.28	6.28	12.57	12.57	2	0.02	0.01	0.04	0.00	0.00	24.0
13	195	-27590	-142	428	0	-274	80	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
14	195	-27400	186	509	0	-521	54	6.28	6.28	12.57	12.57	2	0.02	0.01	0.04	0.00	0.00	24.0
15	195	-27080	182	380	0	-140	55	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
16	195	-27580	36	510	0	-521	66	6.28	6.28	12.57	12.57	2	0.02	0.01	0.04	0.00	0.00	24.0
17	195	-27260	32	381	0	-141	67	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
18	195	-41280	1007	708	0	-753	130	6.28	6.28	12.57	12.57	3	0.02	0.02	0.06	0.00	0.00	24.0
19	195	-41270	-638	694	0	-681	110	6.28	6.28	12.57	12.57	3	0.02	0.01	0.05	0.00	0.00	24.0
20	195	-40440	182	413	0	-535	115	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
37	195	-39150	1541	664	0	-681	123	6.28	6.28	12.57	12.57	3	0.02	0.03	0.10	0.00	0.00	24.0
38	195	-39140	-1200	640	0	-560	90	6.28	6.28	12.57	12.57	3	0.02	0.02	0.08	0.00	0.00	24.0
39	195	-37755	167	172	0	-317	98	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	292	-34770	142	578	0	-994	216	6.28	6.28	12.57	12.57	3	0.03	0.01	0.04	0.00	0.00	24.0
2	292	-26495	360	462	0	-838	392	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
3	292	-26395	359	423	0	-685	391	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
4	292	-27095	-141	467	0	-844	-58	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
5	292	-27005	-142	428	0	-692	-59	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
6	292	-26815	186	509	0	-1017	235	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
7	292	-26495	182	380	0	-510	233	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
8	292	-26995	36	510	0	-1019	100	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
9	292	-26675	32	381	0	-512	98	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
10	292	-26495	360	462	0	-838	392	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
11	292	-26395	359	423	0	-685	391	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
12	292	-27095	-141	467	0	-844	-58	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
13	292	-27005	-142	428	0	-692	-59	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
14	292	-26815	186	509	0	-1017	235	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
15	292	-26495	182	380	0	-510	233	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
16	292	-26995	36	510	0	-1019	100	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
17	292	-26675	32	381	0	-512	98	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
18	292	-40520	1007	708	0	-1444	1111	6.28	6.28	12.57	12.57	3	0.07	0.02	0.06	0.00	0.00	24.0
19	292	-40510	-638	694	0	-1357	-512	6.28	6.28	12.57	12.57	3	0.05	0.01	0.05	0.00	0.00	24.0
20	292	-39680	182	413	0	-938	292	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0

37	292	-38390	1541	664	0	-1328	1626	6.28	6.28	12.57	12.57	3	0.08	0.03	0.11	0.00	0.00	24.0
38	292	-38380	-1200	640	0	-1183	-1080	6.28	6.28	12.57	12.57	3	0.06	0.02	0.08	0.00	0.00	24.0
39	292	-36992	167	172	0	-485	261	6.28	6.28	12.57	12.57	3	0.02	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	390	-34010	142	578	0	-1558	354	6.28	6.28	12.57	12.57	3	0.05	0.01	0.04	0.00	0.00	24.0
2	390	-25910	360	462	0	-1288	743	6.28	6.28	12.57	12.57	2	0.08	0.01	0.04	0.00	0.00	24.0
3	390	-25810	359	423	0	-1098	741	6.28	6.28	12.57	12.57	2	0.07	0.01	0.03	0.00	0.00	24.0
4	390	-26510	-141	467	0	-1299	-196	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
5	390	-26420	-142	428	0	-1109	-198	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
6	390	-26230	186	509	0	-1513	416	6.28	6.28	12.57	12.57	2	0.08	0.01	0.04	0.00	0.00	24.0
7	390	-25910	182	380	0	-880	410	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
8	390	-26410	36	510	0	-1516	135	6.28	6.28	12.57	12.57	2	0.07	0.01	0.04	0.00	0.00	24.0
9	390	-26090	32	381	0	-884	129	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
10	390	-25910	360	462	0	-1288	743	6.28	6.28	12.57	12.57	2	0.08	0.01	0.04	0.00	0.00	24.0
11	390	-25810	359	423	0	-1098	741	6.28	6.28	12.57	12.57	2	0.07	0.01	0.03	0.00	0.00	24.0
12	390	-26510	-141	467	0	-1299	-196	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
13	390	-26420	-142	428	0	-1109	-198	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
14	390	-26230	186	509	0	-1513	416	6.28	6.28	12.57	12.57	2	0.08	0.01	0.04	0.00	0.00	24.0
15	390	-25910	182	380	0	-880	410	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
16	390	-26410	36	510	0	-1516	135	6.28	6.28	12.57	12.57	2	0.07	0.01	0.04	0.00	0.00	24.0
17	390	-26090	32	381	0	-884	129	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
18	390	-39760	1007	708	0	-2134	2093	6.28	6.28	12.57	12.57	3	0.12	0.02	0.06	0.00	0.00	24.0
19	390	-39750	-638	694	0	-2033	-1135	6.28	6.28	12.57	12.57	3	0.08	0.01	0.05	0.00	0.00	24.0
20	390	-38920	182	413	0	-1341	470	6.28	6.28	12.57	12.57	3	0.05	0.01	0.03	0.00	0.00	24.0
37	390	-37630	1541	664	0	-1976	3129	6.28	6.28	12.57	12.57	3	0.15	0.03	0.11	0.00	0.00	24.0
38	390	-37620	-1200	640	0	-1807	-2250	6.28	6.28	12.57	12.57	3	0.12	0.02	0.08	0.00	0.00	24.0
39	390	-36230	167	172	0	-653	423	6.28	6.28	12.57	12.57	3	0.03	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

VERIFICA NODO IN TESTA AL PILASTRO, NODO NUM. 296 NON CONFINATO

(par.7.2.2 NTC2018 "La domanda di resistenza valutata con i criteri della progettazione in capacità può essere assunta non superiore alla domanda di resistenza valutata per il caso di comportamento strutturale non dissipativo.")

PROGETTAZIONE IN CAPACITA'

Asse loc. pilastro y nodo INTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 50.0 cm, hjc= 30.0 cm
Asse loc. pilastro z nodo INTERNO: As2(inf)= 6.03, As1(sup)= 6.03, Hjw= 40.0 cm, bj= 40.0 cm, hjc= 50.0 cm

FxMin,inf	FxMin,sup	FxMax,sup	FySup	FzSup	Vjbdy	Vjbdz	Vres,y	Vres,z	I.R.compr.	Ashy	Ashz	PASSO	Nota
daN					daN		daN			cmq		cm	
-25810	-11450	-12250	65	102	35168	52747	127376	169834	0.31	8.64	10.18	4.39	

VERIFICA DI RESISTENZA CON SOLLECITAZIONI COMPORTAMENTO NON DISSIPATIVO

Asse loc. pilastro y nodo INTERNO: Hjw= 40.0 cm, bj= 50.0 cm, hjc= 30.0 cm, db1= 45.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb,1	Mb,2	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-11530	-25910	-2591	-888	546	3658	127607	0.03	0.00	40.00	
3	-11450	-25810	-2587	-896	540	3636	127633	0.03	0.00	40.00	
4	-12250	-26510	-923	-2419	790	2903	127376	0.02	0.00	40.00	
5	-12160	-26420	-919	-2427	796	2928	127405	0.02	0.00	40.00	
6	-11880	-26230	-2012	-1415	86	1388	127495	0.01	0.00	40.00	
7	-11600	-25910	-1998	-1441	65	1310	127585	0.01	0.00	40.00	
8	-12100	-26410	-1512	-1875	315	581	127424	0.00	0.00	40.00	
9	-11810	-26090	-1498	-1900	336	657	127517	0.01	0.00	40.00	
10	-11530	-25910	-2591	-888	546	3658	127607	0.03	0.00	40.00	
11	-11450	-25810	-2587	-896	540	3636	127633	0.03	0.00	40.00	
12	-12250	-26510	-923	-2419	790	2903	127376	0.02	0.00	40.00	
13	-12160	-26420	-919	-2427	796	2928	127405	0.02	0.00	40.00	
14	-11880	-26230	-2012	-1415	86	1388	127495	0.01	0.00	40.00	
15	-11600	-25910	-1998	-1441	65	1310	127585	0.01	0.00	40.00	
16	-12100	-26410	-1512	-1875	315	581	127424	0.00	0.00	40.00	
17	-11810	-26090	-1498	-1900	336	657	127517	0.01	0.00	40.00	

Asse loc. pilastro z nodo INTERNO: Hjw= 40.0 cm, bj= 40.0 cm, hjc= 50.0 cm, db1= 45.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb,1	Mb,2	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-11530	-25910	-2584	-2484	328	81	170143	0.00	0.00	40.00	
3	-11450	-25810	-2298	-2766	224	932	170177	0.01	0.00	40.00	
4	-12250	-26510	-2535	-2452	329	124	169834	0.00	0.00	40.00	
5	-12160	-26420	-2250	-2733	225	968	169873	0.01	0.00	40.00	
6	-11880	-26230	-2900	-2145	450	1414	169993	0.01	0.00	40.00	
7	-11600	-25910	-1948	-3083	102	2700	170113	0.02	0.00	40.00	
8	-12100	-26410	-2885	-2135	451	1401	169898	0.01	0.00	40.00	
9	-11810	-26090	-1934	-3073	102	2710	170023	0.02	0.00	40.00	
10	-11530	-25910	-2584	-2484	328	81	170143	0.00	0.00	40.00	
11	-11450	-25810	-2298	-2766	224	932	170177	0.01	0.00	40.00	
12	-12250	-26510	-2535	-2452	329	124	169834	0.00	0.00	40.00	
13	-12160	-26420	-2250	-2733	225	968	169873	0.01	0.00	40.00	
14	-11880	-26230	-2900	-2145	450	1414	169993	0.01	0.00	40.00	
15	-11600	-25910	-1948	-3083	102	2700	170113	0.02	0.00	40.00	
16	-12100	-26410	-2885	-2135	451	1401	169898	0.01	0.00	40.00	
17	-11810	-26090	-1934	-3073	102	2710	170023	0.02	0.00	40.00	

CONFRONTO E SINTESI CONCLUSIVE (si assume in ogni caso passo <= 15 cm)

I.R.compr.	Ashy	Ashz	PASSO	Nota
	cmq		cm	
0.03	--	--	15.00	**VERIFICATO**

ASTA NUM. 40 NI 301 NF 298 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 20B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-34870	124	713	0	921	-261	6.28	6.28	12.57	12.57	3	0.03	0.01	0.05	0.00	0.00	24.0
2	0	-26650	323	578	0	705	-688	6.28	6.28	12.57	12.57	2	0.06	0.01	0.05	0.00	0.00	24.0
3	0	-26610	322	547	0	761	-685	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
4	0	-27040	-131	550	0	655	284	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
5	0	-27000	-132	520	0	711	287	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
6	0	-26840	165	604	0	622	-351	6.28	6.28	12.57	12.57	2	0.04	0.01	0.05	0.00	0.00	24.0
7	0	-26690	162	502	0	809	-342	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
8	0	-26960	29	595	0	607	-59	6.28	6.28	12.57	12.57	2	0.03	0.01	0.05	0.00	0.00	24.0
9	0	-26810	26	494	0	794	-50	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
10	0	-26650	323	578	0	705	-688	6.28	6.28	12.57	12.57	2	0.06	0.01	0.05	0.00	0.00	24.0
11	0	-26610	322	547	0	761	-685	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
12	0	-27040	-131	550	0	655	284	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
13	0	-27000	-132	520	0	711	287	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
14	0	-26840	165	604	0	622	-351	6.28	6.28	12.57	12.57	2	0.04	0.01	0.05	0.00	0.00	24.0
15	0	-26690	162	502	0	809	-342	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
16	0	-26960	29	595	0	607	-59	6.28	6.28	12.57	12.57	2	0.03	0.01	0.05	0.00	0.00	24.0
17	0	-26810	26	494	0	794	-50	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
18	0	-37980	932	1006	0	1184	-1869	6.28	6.28	12.57	12.57	3	0.09	0.02	0.07	0.00	0.00	24.0
19	0	-39820	-585	902	0	981	1207	6.28	6.28	12.57	12.57	3	0.06	0.01	0.06	0.00	0.00	24.0
20	0	-38380	173	704	0	829	-331	6.28	6.28	12.57	12.57	3	0.03	0.01	0.05	0.00	0.00	24.0
37	0	-35830	1420	952	0	1184	-2869	6.28	6.28	12.57	12.57	3	0.14	0.02	0.10	0.00	0.00	24.0
38	0	-38900	-1108	779	0	846	2257	6.28	6.28	12.57	12.57	3	0.11	0.02	0.08	0.00	0.00	24.0
39	0	-36500	155	450	0	592	-306	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	97	-34110	124	713	0	225	-139	6.28	6.28	12.57	12.57	3	0.01	0.01	0.05	0.00	0.00	24.0
2	97	-26065	323	578	0	141	-373	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
3	97	-26025	322	547	0	227	-371	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
4	97	-26455	-131	550	0	119	157	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
5	97	-26415	-132	520	0	205	159	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
6	97	-26255	165	604	0	33	-190	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
7	97	-26105	162	502	0	319	-183	6.28	6.28	12.57	12.57	2	0.02	0.01	0.04	0.00	0.00	24.0
8	97	-26375	29	595	0	27	-31	6.28	6.28	12.57	12.57	2	0.00	0.01	0.05	0.00	0.00	24.0
9	97	-26225	26	494	0	312	-25	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
10	97	-26065	323	578	0	141	-373	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
11	97	-26025	322	547	0	227	-371	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
12	97	-26455	-131	550	0	119	157	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
13	97	-26415	-132	520	0	205	159	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
14	97	-26255	165	604	0	33	-190	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
15	97	-26105	162	502	0	319	-183	6.28	6.28	12.57	12.57	2	0.02	0.01	0.04	0.00	0.00	24.0
16	97	-26375	29	595	0	27	-31	6.28	6.28	12.57	12.57	2	0.00	0.01	0.05	0.00	0.00	24.0
17	97	-26225	26	494	0	312	-25	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
18	97	-37220	932	1006	0	204	-960	6.28	6.28	12.57	12.57	3	0.04	0.02	0.07	0.00	0.00	24.0
19	97	-39060	-585	902	0	102	637	6.28	6.28	12.57	12.57	3	0.03	0.01	0.06	0.00	0.00	24.0
20	97	-37620	173	704	0	143	-162	6.28	6.28	12.57	12.57	3	0.01	0.01	0.05	0.00	0.00	24.0
37	97	-35070	1420	952	0	255	-1484	6.28	6.28	12.57	12.57	3	0.07	0.02	0.10	0.00	0.00	24.0
38	97	-38140	-1108	779	0	86	1177	6.28	6.28	12.57	12.57	3	0.05	0.02	0.08	0.00	0.00	24.0
39	97	-35740	155	450	0	154	-154	6.28	6.28	12.57	12.57	3	0.01	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	195	-33350	124	713	0	-471	-18	6.28	6.28	12.57	12.57	3	0.01	0.01	0.05	0.00	0.00	24.0
2	195	-25480	323	578	0	-422	-58	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
3	195	-25440	322	547	0	-306	-57	6.28	6.28	12.57	12.57	2	0.02	0.01	0.04	0.00	0.00	24.0
4	195	-25870	-131	550	0	-418	29	6.28	6.28	12.57	12.57	2	0.02	0.01	0.04	0.00	0.00	24.0
5	195	-25830	-132	520	0	-302	30	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
6	195	-25670	165	604	0	-555	-29	6.28	6.28	12.57	12.57	2	0.03	0.01	0.05	0.00	0.00	24.0
7	195	-25520	162	502	0	-171	-25	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
8	195	-25790	29	595	0	-553	-3	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
9	195	-25640	26	494	0	-169	1	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
10	195	-25480	323	578	0	-422	-58	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
11	195	-25440	322	547	0	-306	-57	6.28	6.28	12.57	12.57	2	0.02	0.01	0.04	0.00	0.00	24.0
12	195	-25870	-131	550	0	-418	29	6.28	6.28	12.57	12.57	2	0.02	0.01	0.04	0.00	0.00	24.0
13	195	-25830	-132	520	0	-302	30	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
14	195	-25670	165	604	0	-555	-29	6.28	6.28	12.57	12.57	2	0.03	0.01	0.05	0.00	0.00	24.0
15	195	-25520	162	502	0	-171	-25	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
16	195	-25790	29	595	0	-553	-3	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
17	195	-25640	26	494	0	-169	1	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
18	195	-36460	932	1006	0	-777	-52	6.28	6.28	12.57	12.57	3	0.02	0.02	0.07	0.00	0.00	24.0
19	195	-38300	-585	902	0	-777	67	6.28	6.28	12.57	12.57	3	0.02	0.01	0.06	0.00	0.00	24.0
20	195	-36860	173	704	0	-543	6	6.28	6.28	12.57	12.57	3	0.02	0.01	0.05	0.00	0.00	24.0
37	195	-34310	1420	952	0	-674	-100	6.28	6.28	12.57	12.57	3	0.02	0.02	0.09	0.00	0.00	24.0
38	195	-37380	-1108	779	0	-673	97	6.28	6.28	12.57	12.57	3	0.02	0.02	0.07	0.00	0.00	24.0
39	195	-34980	155	450	0	-284	-3	6.28	6.28	12.57	12.57	3	0.01	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	292	-32590	124	713	0	-1166	103	6.28	6.28	12.57	12.57	3	0.04	0.01	0.05	0.00	0.00	24.0
2	292	-24895	323	578	0	-985	257	6.28	6.28	12.57	12.57	2	0.05	0.01	0.05	0.00	0.00	24.0
3	292	-24855	322	547	0	-840	258	6.28	6.28	12.57	12.57	2	0.04	0.01	0.05	0.00	0.00	24.0
4	292	-25285	-131	550	0	-954	-99	6.28	6.28	12.57	12.57	2	0.04	0.01	0.05	0.00	0.00	24.0
5	292	-25245	-132	520	0	-809	-99	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
6	292	-25085	165	604	0	-1144	132	6.28	6.28	12.57	12.57	2	0.05	0.01	0.05	0.00	0.00	24.0
7	292	-24935	162	502	0	-660	133	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
8	292	-25205	29	595	0	-1134	25	6.28	6.28	12.57	12.57	2	0.05	0.01	0.05	0.00	0.00	24.0
9	292	-25055	26	494	0	-651	26	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
10	292	-24895	323	578	0	-985	257	6.28	6.28	12.57	12.57	2	0.05	0.01	0.05	0.00	0.00	24.0
11	292	-24855	322	547	0	-840	258	6.28	6.28	12.57	12.57	2	0.04	0.01	0.05	0.00	0.00	24.0
12	292	-25285	-131	550	0	-954	-99	6.28	6.28	12.57	12.57	2	0.04	0.01	0.05	0.00	0.00	24.0
13	292	-25245	-132	520	0	-809	-99	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
14	292	-25085	165	604	0	-1144	132	6.28	6.28	12.57	12.57	2	0.05	0.01	0.05	0.00	0.00	24.0
15	292	-24935	162	502	0	-660	133	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
16	292	-25205	29	595	0	-1134	25	6.28	6.28	12.57	12.57	2	0.05	0.01	0.05	0.00	0.00	24.0
17	292	-25055	26	494	0	-651	26	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
18	292	-35700	932	1006	0	-1757	856	6.28	6.28	12.57	12.57	3	0.07	0.02	0.07	0.00	0.00	24.0
19	292	-37540	-585	902	0	-1656	-504	6.28	6.28	12.57	12.57	3	0.06	0.01	0.07	0.00	0.00	24.0
20	292	-36100	173	704	0	-1230	175	6.28	6.28	12.57	12.57	3	0.04	0.01	0.05	0.00	0.00	24.0
37	292	-33550	1420	952	0	-1602	1285	6.28	6.28	12.57	12.57	3	0.08	0.02	0.09	0.00	0.00	24.0
38	292	-36620	-1108	779	0	-1433	-983	6.28	6.28	12.57	12.57	3	0.06	0.02	0.07	0.00	0.00	24.0
39	292	-34220	155	450	0	-723	149	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	390	-31830	124	713	0	-1862	224	6.28	6.28	12.57	12.57	3	0.06	0.01	0.05	0.00	0.00	24.0
2	390	-24310	323	578	0	-1548	573	6.28	6.28	12.57	12.57	2	0.09	0.01	0.05	0.00	0.00	24.0
3	390	-24270	322	547	0	-1373	572	6.28	6.28	12.57	12.57	2	0.08	0.01	0.05	0.00	0.00	24.0
4	390	-24700	-131	550	0	-1491	-227	6.28	6.28	12.57	12.57	2	0.07	0.01	0.05	0.00	0.00	24.0
5	390	-24660	-132	520	0	-1316	-228	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
6	390	-24500	165	604	0	-1732	293	6.28	6.28	12.57	12.57	2	0.09	0.01	0.05	0.00	0.00	24.0
7	390	-24350	162	502	0	-1150	292	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
8	390	-24620	29	595	0	-1714	53	6.28	6.28	12.57	12.57	2	0.08	0.01	0.05	0.00	0.00	24.0
9	390	-24470	26	494	0	-1133	52	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
10	390	-24310	323	578	0	-1548	573	6.28	6.28	12.57	12.57	2	0.09	0.01	0.05	0.00	0.00	24.0
11	390	-24270	322	547	0	-1373	572	6.28	6.28	12.57	12.57	2	0.08	0.01	0.05	0.00	0.00	24.0
12	390	-24700	-131	550	0	-1491	-227	6.28	6.28	12.57	12.57	2	0.07	0.01	0.05	0.00	0.00	24.0
13	390	-24660	-132	520	0	-1316	-228	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
14	390	-24500	165	604	0	-1732	293	6.28	6.28	12.57	12.57	2	0.09	0.01	0.05	0.00	0.00	24.0
15	390	-24350	162	502	0	-1150	292	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
16	390	-24620	29	595	0	-1714	53	6.28	6.28	12.57	12.57	2	0.08	0.01	0.05	0.00	0.00	24.0
17	390	-24470	26	494	0	-1133	52	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
18	390	-34940	932	1006	0	-2738	1765	6.28	6.28	12.57	12.57	3	0.12	0.02	0.07	0.00	0.00	24.0
19	390	-36780	-585	902	0	-2535	-1074	6.28	6.28	12.57	12.57	3	0.10	0.01	0.07	0.00	0.00	24.0
20	390	-35340	173	704	0	-1916	343	6.28	6.28	12.57	12.57	3	0.06	0.01	0.05	0.00	0.00	24.0
37	390	-32790	1420	952	0	-2531	2670	6.28	6.28	12.57	12.57	3	0.15	0.02	0.10	0.00	0.00	24.0
38	390	-35860	-1108	779	0	-2192	-2063	6.28	6.28	12.57	12.57	3	0.12	0.02	0.07	0.00	0.00	24.0
39	390	-33460	155	450	0	-1161	300	6.28	6.28	12.57	12.57	3	0.04	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

VERIFICA NODO IN TESTA AL PILASTRO, NODO NUM. 298 NON CONFINATO

(par.7.2.2 NTC2018 "La domanda di resistenza valutata con i criteri della progettazione in capacità può essere assunta non superiore alla domanda di resistenza valutata per il caso di comportamento strutturale non dissipativo.")

PROGETTAZIONE IN CAPACITA'

Asse loc. pilastro y nodo INTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 50.0 cm, hjc= 30.0 cm
Asse loc. pilastro z nodo INTERNO: As2(inf)= 6.03, As1(sup)= 6.03, Hjw= 40.0 cm, bj= 40.0 cm, hjc= 50.0 cm

FxMin,inf	FxMin,sup	FxMax,sup	FySup	FzSup	Vjbdy	Vjbdz	Vres,y	Vres,z	I.R.compr.	Ashy	Ashz	PASSO	Nota
daN					daN		daN			cmq		cm	
-24270	-9473	-9963	66	0	35167	52849	128110	170813	0.31	8.68	10.98	4.03	

VERIFICA DI RESISTENZA CON SOLLECITAZIONI COMPORTAMENTO NON DISSIPATIVO

Asse loc. pilastro y nodo INTERNO: Hjw= 40.0 cm, bj= 50.0 cm, hjc= 30.0 cm, db1= 45.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb,1	Mb,2	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-9499	-24310	-2841	-1393	556	3019	128258	0.02	0.00	40.00	
3	-9473	-24270	-2832	-1396	550	2996	128267	0.02	0.00	40.00	
4	-9963	-24700	-1261	-2810	804	3021	128110	0.02	0.00	40.00	
5	-9937	-24660	-1253	-2813	811	3041	128118	0.02	0.00	40.00	
6	-9691	-24500	-2297	-1886	88	927	128197	0.01	0.00	40.00	
7	-9605	-24350	-2270	-1896	66	858	128224	0.01	0.00	40.00	
8	-9830	-24620	-1823	-2311	320	885	128152	0.01	0.00	40.00	
9	-9745	-24470	-1796	-2321	342	954	128180	0.01	0.00	40.00	
10	-9499	-24310	-2841	-1393	556	3019	128258	0.02	0.00	40.00	
11	-9473	-24270	-2832	-1396	550	2996	128267	0.02	0.00	40.00	
12	-9963	-24700	-1261	-2810	804	3021	128110	0.02	0.00	40.00	
13	-9937	-24660	-1253	-2813	811	3041	128118	0.02	0.00	40.00	
14	-9691	-24500	-2297	-1886	88	927	128197	0.01	0.00	40.00	
15	-9605	-24350	-2270	-1896	66	858	128224	0.01	0.00	40.00	
16	-9830	-24620	-1823	-2311	320	885	128152	0.01	0.00	40.00	
17	-9745	-24470	-1796	-2321	342	954	128180	0.01	0.00	40.00	

Asse loc. pilastro z nodo INTERNO: Hjw= 40.0 cm, bj= 40.0 cm, hjc= 50.0 cm, db1= 45.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb,1	Mb,2	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-9499	-24310	-2564	-2745	125	322	171011	0.00	0.00	40.00	
3	-9473	-24270	-2252	-3043	0	1953	171022	0.01	0.00	40.00	
4	-9963	-24700	-2597	-2688	146	79	170813	0.00	0.00	40.00	
5	-9937	-24660	-2285	-2986	21	1710	170824	0.01	0.00	40.00	
6	-9691	-24500	-2940	-2378	278	1110	170929	0.01	0.00	40.00	
7	-9605	-24350	-1900	-3371	138	3494	170966	0.02	0.00	40.00	
8	-9830	-24620	-2949	-2361	284	1168	170870	0.01	0.00	40.00	
9	-9745	-24470	-1910	-3354	132	3433	170906	0.02	0.00	40.00	
10	-9499	-24310	-2564	-2745	125	322	171011	0.00	0.00	40.00	
11	-9473	-24270	-2252	-3043	0	1953	171022	0.01	0.00	40.00	
12	-9963	-24700	-2597	-2688	146	79	170813	0.00	0.00	40.00	
13	-9937	-24660	-2285	-2986	21	1710	170824	0.01	0.00	40.00	
14	-9691	-24500	-2940	-2378	278	1110	170929	0.01	0.00	40.00	
15	-9605	-24350	-1900	-3371	138	3494	170966	0.02	0.00	40.00	
16	-9830	-24620	-2949	-2361	284	1168	170870	0.01	0.00	40.00	
17	-9745	-24470	-1910	-3354	132	3433	170906	0.02	0.00	40.00	

CONFRONTO E SINTESI CONCLUSIVE (si assume in ogni caso passo <= 15 cm)

I.R.compr.	Ashy	Ashz	PASSO	Nota
	cmq		cm	
0.02	--	--	15.00	**VERIFICATO**

ASTA NUM. 41 NI 35 NF 31 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 12D
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm

1	0	-4632	1046	416	0	-1107	-1374	6.28	6.28	12.57	12.57	3	0.09	0.02	0.11	0.00	0.00	24.0
2	0	-3607	847	302	0	-903	-1126	6.28	6.28	12.57	12.57	2	0.10	0.02	0.09	0.00	0.00	24.0
3	0	-3613	850	324	0	-879	-1129	6.28	6.28	12.57	12.57	2	0.10	0.02	0.09	0.00	0.00	24.0
4	0	-3514	759	316	0	-824	-986	6.28	6.28	12.57	12.57	2	0.09	0.01	0.08	0.00	0.00	24.0
5	0	-3520	762	338	0	-801	-989	6.28	6.28	12.57	12.57	2	0.09	0.01	0.08	0.00	0.00	24.0
6	0	-3567	812	282	0	-903	-1073	6.28	6.28	12.57	12.57	2	0.10	0.02	0.08	0.00	0.00	24.0
7	0	-3588	823	354	0	-824	-1084	6.28	6.28	12.57	12.57	2	0.09	0.02	0.08	0.00	0.00	24.0
8	0	-3539	786	286	0	-879	-1031	6.28	6.28	12.57	12.57	2	0.09	0.01	0.08	0.00	0.00	24.0
9	0	-3560	797	358	0	-801	-1041	6.28	6.28	12.57	12.57	2	0.09	0.01	0.08	0.00	0.00	24.0
10	0	-3607	847	302	0	-903	-1126	6.28	6.28	12.57	12.57	2	0.10	0.02	0.09	0.00	0.00	24.0
11	0	-3613	850	324	0	-879	-1129	6.28	6.28	12.57	12.57	2	0.10	0.02	0.09	0.00	0.00	24.0
12	0	-3514	759	316	0	-824	-986	6.28	6.28	12.57	12.57	2	0.09	0.01	0.08	0.00	0.00	24.0
13	0	-3520	762	338	0	-801	-989	6.28	6.28	12.57	12.57	2	0.09	0.01	0.08	0.00	0.00	24.0
14	0	-3567	812	282	0	-903	-1073	6.28	6.28	12.57	12.57	2	0.10	0.02	0.08	0.00	0.00	24.0
15	0	-3588	823	354	0	-824	-1084	6.28	6.28	12.57	12.57	2	0.09	0.02	0.08	0.00	0.00	24.0
16	0	-3539	786	286	0	-879	-1031	6.28	6.28	12.57	12.57	2	0.09	0.01	0.08	0.00	0.00	24.0
17	0	-3560	797	358	0	-801	-1041	6.28	6.28	12.57	12.57	2	0.09	0.01	0.08	0.00	0.00	24.0
18	0	-7784	918	1006	0	-3143	-1401	6.28	6.28	12.57	12.57	3	0.14	0.02	0.10	0.00	0.00	24.0
19	0	-5865	844	759	0	-1844	-1054	6.28	6.28	12.57	12.57	3	0.09	0.02	0.08	0.00	0.00	24.0
20	0	-6372	978	-100	0	-7385	-1322	6.28	6.28	12.57	12.57	3	0.29	0.02	0.09	0.00	0.00	24.0
37	0	-7815	1007	938	0	-3131	-1576	6.28	6.28	12.57	12.57	3	0.14	0.02	0.10	0.00	0.00	24.0
38	0	-4615	883	526	0	-966	-999	6.28	6.28	12.57	12.57	3	0.06	0.02	0.09	0.00	0.00	24.0
39	0	-5461	1106	-906	0	-10200	-1445	6.28	6.28	12.57	12.57	3	0.40	0.02	0.10	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	58	-4181	1046	416	0	-1348	-769	6.28	6.28	12.57	12.57	3	0.07	0.02	0.09	0.00	0.00	24.0
2	58	-3260	847	302	0	-1078	-636	6.28	6.28	12.57	12.57	2	0.08	0.02	0.08	0.00	0.00	24.0
3	58	-3266	850	324	0	-1066	-637	6.28	6.28	12.57	12.57	2	0.08	0.02	0.08	0.00	0.00	24.0
4	58	-3167	759	316	0	-1007	-547	6.28	6.28	12.57	12.57	2	0.08	0.01	0.07	0.00	0.00	24.0
5	58	-3173	762	338	0	-996	-548	6.28	6.28	12.57	12.57	2	0.08	0.01	0.07	0.00	0.00	24.0
6	58	-3220	812	282	0	-1066	-603	6.28	6.28	12.57	12.57	2	0.08	0.02	0.07	0.00	0.00	24.0
7	58	-3241	823	354	0	-1029	-608	6.28	6.28	12.57	12.57	2	0.08	0.02	0.08	0.00	0.00	24.0
8	58	-3192	786	286	0	-1045	-577	6.28	6.28	12.57	12.57	2	0.08	0.01	0.07	0.00	0.00	24.0
9	58	-3213	797	358	0	-1008	-580	6.28	6.28	12.57	12.57	2	0.08	0.01	0.07	0.00	0.00	24.0
10	58	-3260	847	302	0	-1078	-636	6.28	6.28	12.57	12.57	2	0.08	0.02	0.08	0.00	0.00	24.0
11	58	-3266	850	324	0	-1066	-637	6.28	6.28	12.57	12.57	2	0.08	0.02	0.08	0.00	0.00	24.0
12	58	-3167	759	316	0	-1007	-547	6.28	6.28	12.57	12.57	2	0.08	0.01	0.07	0.00	0.00	24.0
13	58	-3173	762	338	0	-996	-548	6.28	6.28	12.57	12.57	2	0.08	0.01	0.07	0.00	0.00	24.0
14	58	-3220	812	282	0	-1066	-603	6.28	6.28	12.57	12.57	2	0.08	0.02	0.07	0.00	0.00	24.0
15	58	-3241	823	354	0	-1029	-608	6.28	6.28	12.57	12.57	2	0.08	0.02	0.08	0.00	0.00	24.0
16	58	-3192	786	286	0	-1045	-577	6.28	6.28	12.57	12.57	2	0.08	0.01	0.07	0.00	0.00	24.0
17	58	-3213	797	358	0	-1008	-580	6.28	6.28	12.57	12.57	2	0.08	0.01	0.07	0.00	0.00	24.0
18	58	-7333	918	1006	0	-3725	-870	6.28	6.28	12.57	12.57	3	0.15	0.02	0.10	0.00	0.00	24.0
19	58	-5414	844	759	0	-2283	-566	6.28	6.28	12.57	12.57	3	0.09	0.02	0.08	0.00	0.00	24.0
20	58	-5921	978	-418	0	-7235	-757	6.28	6.28	12.57	12.57	3	0.28	0.02	0.09	0.00	0.00	24.0
37	58	-7364	1007	938	0	-3674	-994	6.28	6.28	12.57	12.57	3	0.15	0.02	0.10	0.00	0.00	24.0
38	58	-4164	883	526	0	-1270	-488	6.28	6.28	12.57	12.57	3	0.06	0.02	0.08	0.00	0.00	24.0
39	58	-5010	1106	-1435	0	-9523	-805	6.28	6.28	12.57	12.57	3	0.36	0.03	0.15	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	116	-3730	1046	416	0	-1588	-165	6.28	6.28	12.57	12.57	3	0.06	0.02	0.09	0.00	0.00	24.0
2	116	-2913	847	302	0	-1252	-146	6.28	6.28	12.57	12.57	2	0.07	0.02	0.08	0.00	0.00	24.0
3	116	-2919	850	324	0	-1254	-146	6.28	6.28	12.57	12.57	2	0.07	0.02	0.08	0.00	0.00	24.0
4	116	-2820	759	316	0	-1190	-108	6.28	6.28	12.57	12.57	2	0.07	0.01	0.07	0.00	0.00	24.0
5	116	-2826	762	338	0	-1191	-107	6.28	6.28	12.57	12.57	2	0.07	0.01	0.07	0.00	0.00	24.0
6	116	-2873	812	282	0	-1229	-134	6.28	6.28	12.57	12.57	2	0.07	0.02	0.07	0.00	0.00	24.0
7	116	-2894	823	354	0	-1233	-132	6.28	6.28	12.57	12.57	2	0.07	0.02	0.08	0.00	0.00	24.0
8	116	-2845	786	286	0	-1210	-122	6.28	6.28	12.57	12.57	2	0.07	0.01	0.07	0.00	0.00	24.0
9	116	-2866	797	358	0	-1214	-120	6.28	6.28	12.57	12.57	2	0.07	0.01	0.07	0.00	0.00	24.0
10	116	-2913	847	302	0	-1252	-146	6.28	6.28	12.57	12.57	2	0.07	0.02	0.08	0.00	0.00	24.0
11	116	-2919	850	324	0	-1254	-146	6.28	6.28	12.57	12.57	2	0.07	0.02	0.08	0.00	0.00	24.0
12	116	-2820	759	316	0	-1190	-108	6.28	6.28	12.57	12.57	2	0.07	0.01	0.07	0.00	0.00	24.0
13	116	-2826	762	338	0	-1191	-107	6.28	6.28	12.57	12.57	2	0.07	0.01	0.07	0.00	0.00	24.0
14	116	-2873	812	282	0	-1229	-134	6.28	6.28	12.57	12.57	2	0.07	0.02	0.07	0.00	0.00	24.0
15	116	-2894	823	354	0	-1233	-132	6.28	6.28	12.57	12.57	2	0.07	0.02	0.08	0.00	0.00	24.0
16	116	-2845	786	286	0	-1210	-122	6.28	6.28	12.57	12.57	2	0.07	0.01	0.07	0.00	0.00	24.0
17	116	-2866	797	358	0	-1214	-120	6.28	6.28	12.57	12.57	2	0.07	0.01	0.07	0.00	0.00	24.0
18	116	-6882	918	1006	0	-4307	-339	6.28	6.28	12.57	12.57	3	0.16	0.02	0.10	0.00	0.00	24.0
19	116	-4963	844	759	0	-2722	-78	6.28	6.28	12.57	12.57	3	0.10	0.02	0.08	0.00	0.00	24.0
20	116	-5470	978	-736	0	-6902	-191	6.28	6.28	12.57	12.57	3	0.26	0.02	0.09	0.00	0.00	24.0
37	116	-6912	1007	938	0	-4216	-412	6.28	6.28	12.57	12.57	3	0.16	0.02	0.10	0.00	0.00	24.0
38	116	-3713	883	526	0	-1574	23	6.28	6.28	12.57	12.57	3	0.06	0.02	0.08	0.00	0.00	24.0
39	116	-4558	1106	-1965	0	-8540	-165	6.28	6.28	12.57	12.57	3	0.32	0.03	0.21	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	173	-3279	1046	416	0	-1829	440	6.28	6.28	12.57	12.57	3	0.08	0.02	0.10	0.00	0.00	24.0
2	173	-2566	847	302	0	-1427	343	6.28	6.28	12.57	12.57	2	0.09	0.02	0.08	0.00	0.00	24.0
3	173	-2572	850	324	0	-1441	346	6.28	6.28	12.57	12.57	2	0.09	0.02	0.08	0.00	0.00	24.0
4	173	-2473	759	316	0	-1372	331	6.28	6.28	12.57	12.57	2	0.09	0.01	0.07	0.00	0.00	24.0
5	173	-2479	762	338	0	-1386	334	6.28	6.28	12.57	12.57	2	0.09	0.01	0.07	0.00	0.00	24.0
6	173	-2526	812	282	0	-1393	336	6.28	6.28	12.57	12.57	2	0.09	0.02	0.07	0.00	0.00	24.0
7	173	-2547	823	354	0	-1438	345	6.28	6.28	12.57	12.57	2	0.09	0.02	0.08	0.00	0.00	24.0
8	173	-2498	786	286	0	-1376	332	6.28	6.28	12.57	12.57	2	0.09	0.01	0.07	0.00	0.00	24.0
9	173	-2519	797	358	0	-1421	341	6.28	6.28	12.57	12.57	2	0.09	0.01	0.07	0.00	0.00	24.0
10	173	-2566	847	302	0	-1427	343	6.28	6.28	12.57	12.57	2	0.09	0.02	0.08	0.00	0.00	24.0
11	173	-2572	850	324	0	-1441	346	6.28	6.28	12.57	12.57	2	0.09	0.02	0.08	0.00	0.00	24.0
12	173	-2473	759	316	0	-1372	331	6.28	6.28	12.57	12.57	2	0.09	0.01	0.07	0.00	0.00	24.0
13	173	-2479	762	338	0	-1386	334	6.28	6.28	12.57	12.57	2	0.09	0.01	0.07	0.00	0.00	24.0
14	173	-2526	812	282	0	-1393	336	6.28	6.28	12.57	12.57	2	0.09	0.02	0.07	0.00	0.00	24.0
15	173	-2547	823	354	0	-1438	345	6.28	6.28	12.57	12.57	2	0.09	0.02	0.08	0.00	0.00	24.0
16	173	-2498	786	286	0	-1376	332	6.28	6.28	12.57	12.57	2	0.09	0.01	0.07	0.00	0.00	24.0
17	173	-2519	797	358	0	-1421	341	6.28	6.28	12.57	12.57	2	0.09	0.01	0.07	0.00	0.00	24.0
18	173	-6431	918	1006	0	-4889	192	6.28	6.28	12.57	12.57	3	0.18	0.02	0.11	0.00	0.00	24.0
19	173	-4512	844	759	0	-3161	410	6.28	6.28	12.57	12.57	3	0.12	0.02	0.08	0.00	0.00	24.0
20	173	-5019	978	-1053	0	-6385	374	6.28	6.28	12.57	12.57	3	0.24	0.02	0.11	0.00	0.00	24.0
37	173	-6461	1007	938	0	-4758	170	6.28	6.28	12.57	12.57	3	0.18	0.02	0.10	0.00	0.00	24.0
38	173	-3262	883	526	0	-1878	534	6.28	6.28	12.57	12.57	3	0.08	0.02	0.08	0.00	0.00	24.0
39	173	-4107	1106	-2494	0	-7250	474	6.28	6.28	12.57	12.57	3	0.28	0.04	0.27	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	231	-2828	1046	416	0	-2069	1045	6.28	6.28	12.57	12.57	3	0.10	0.02	0.10	0.00	0.00	24.0
2	231	-2219	847	302	0	-1602	833	6.28	6.28	12.57	12.57	2	0.12	0.02	0.08	0.00	0.00	24.0
3	231	-2225	850	324	0	-1628	838	6.28	6.28	12.57	12.57	2	0.12	0.02	0.08	0.00	0.00	24.0
4	231	-2126	759	316	0	-1555	770	6.28	6.28	12.57	12.57	2	0.12	0.01	0.07	0.00	0.00	24.0
5	231	-2132	762	338	0	-1581	774	6.28	6.28	12.57	12.57	2	0.12	0.01	0.07	0.00	0.00	24.0
6	231	-2179	812	282	0	-1556	806	6.28	6.28	12.57	12.57	2	0.12	0.02	0.07	0.00	0.00	24.0

7	231	-2200	823	354	0	-1642	821	6.28	6.28	12.57	12.57	2	0.12	0.02	0.08	0.00	0.00	24.0
8	231	-2151	786	286	0	-1542	787	6.28	6.28	12.57	12.57	2	0.12	0.01	0.07	0.00	0.00	24.0
9	231	-2172	797	358	0	-1628	802	6.28	6.28	12.57	12.57	2	0.12	0.01	0.07	0.00	0.00	24.0
10	231	-2219	847	302	0	-1602	833	6.28	6.28	12.57	12.57	2	0.12	0.02	0.08	0.00	0.00	24.0
11	231	-2225	850	324	0	-1628	838	6.28	6.28	12.57	12.57	2	0.12	0.02	0.08	0.00	0.00	24.0
12	231	-2126	759	316	0	-1555	770	6.28	6.28	12.57	12.57	2	0.12	0.01	0.07	0.00	0.00	24.0
13	231	-2132	762	338	0	-1581	774	6.28	6.28	12.57	12.57	2	0.12	0.01	0.07	0.00	0.00	24.0
14	231	-2179	812	282	0	-1556	806	6.28	6.28	12.57	12.57	2	0.12	0.02	0.07	0.00	0.00	24.0
15	231	-2200	823	354	0	-1642	821	6.28	6.28	12.57	12.57	2	0.12	0.02	0.08	0.00	0.00	24.0
16	231	-2151	786	286	0	-1542	787	6.28	6.28	12.57	12.57	2	0.12	0.01	0.07	0.00	0.00	24.0
17	231	-2172	797	358	0	-1628	802	6.28	6.28	12.57	12.57	2	0.12	0.01	0.07	0.00	0.00	24.0
18	231	-5980	918	1006	0	-5471	723	6.28	6.28	12.57	12.57	3	0.21	0.02	0.11	0.00	0.00	24.0
19	231	-4061	844	759	0	-3600	898	6.28	6.28	12.57	12.57	3	0.15	0.02	0.08	0.00	0.00	24.0
20	231	-4568	978	-1371	0	-5684	939	6.28	6.28	12.57	12.57	3	0.23	0.02	0.15	0.00	0.00	24.0
37	231	-6010	1007	938	0	-5301	753	6.28	6.28	12.57	12.57	3	0.21	0.02	0.10	0.00	0.00	24.0
38	231	-2811	883	526	0	-2182	1045	6.28	6.28	12.57	12.57	3	0.10	0.02	0.08	0.00	0.00	24.0
39	231	-3656	1106	-3023	0	-5655	1114	6.28	6.28	12.57	12.57	3	0.23	0.05	0.33	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 42 NI 37 NF 43 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 17D
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-4591	206	282	0	-1806	-223	6.28	6.28	12.57	12.57	3	0.07	0.00	0.03	0.00	0.00	24.0
2	0	-3534	236	208	0	-1411	-293	6.28	6.28	12.57	12.57	2	0.09	0.00	0.02	0.00	0.00	24.0
3	0	-3581	237	225	0	-1363	-294	6.28	6.28	12.57	12.57	2	0.08	0.00	0.02	0.00	0.00	24.0
4	0	-3482	81	208	0	-1415	-49	6.28	6.28	12.57	12.57	2	0.08	0.00	0.02	0.00	0.00	24.0
5	0	-3528	81	226	0	-1366	-50	6.28	6.28	12.57	12.57	2	0.08	0.00	0.02	0.00	0.00	24.0
6	0	-3462	182	187	0	-1470	-206	6.28	6.28	12.57	12.57	2	0.09	0.00	0.02	0.00	0.00	24.0
7	0	-3617	183	246	0	-1307	-210	6.28	6.28	12.57	12.57	2	0.08	0.00	0.03	0.00	0.00	24.0
8	0	-3446	135	187	0	-1471	-132	6.28	6.28	12.57	12.57	2	0.08	0.00	0.02	0.00	0.00	24.0
9	0	-3601	136	246	0	-1308	-137	6.28	6.28	12.57	12.57	2	0.08	0.00	0.03	0.00	0.00	24.0
10	0	-3534	236	208	0	-1411	-293	6.28	6.28	12.57	12.57	2	0.09	0.00	0.02	0.00	0.00	24.0
11	0	-3581	237	225	0	-1363	-294	6.28	6.28	12.57	12.57	2	0.08	0.00	0.02	0.00	0.00	24.0
12	0	-3482	81	208	0	-1415	-49	6.28	6.28	12.57	12.57	2	0.08	0.00	0.02	0.00	0.00	24.0
13	0	-3528	81	226	0	-1366	-50	6.28	6.28	12.57	12.57	2	0.08	0.00	0.02	0.00	0.00	24.0
14	0	-3462	182	187	0	-1470	-206	6.28	6.28	12.57	12.57	2	0.09	0.00	0.02	0.00	0.00	24.0
15	0	-3617	183	246	0	-1307	-210	6.28	6.28	12.57	12.57	2	0.08	0.00	0.03	0.00	0.00	24.0
16	0	-3446	135	187	0	-1471	-132	6.28	6.28	12.57	12.57	2	0.08	0.00	0.02	0.00	0.00	24.0
17	0	-3601	136	246	0	-1308	-137	6.28	6.28	12.57	12.57	2	0.08	0.00	0.03	0.00	0.00	24.0
18	0	-8060	573	682	0	-4104	-813	6.28	6.28	12.57	12.57	3	0.16	0.01	0.07	0.00	0.00	24.0
19	0	-6842	-51	535	0	-3578	174	6.28	6.28	12.57	12.57	3	0.13	0.01	0.06	0.00	0.00	24.0
20	0	-7106	255	74	0	-9972	-314	6.28	6.28	12.57	12.57	3	0.37	0.00	0.02	0.00	0.00	24.0
37	0	-7568	769	624	0	-3621	-1117	6.28	6.28	12.57	12.57	3	0.15	0.01	0.07	0.00	0.00	24.0
38	0	-5538	-272	379	0	-2744	527	6.28	6.28	12.57	12.57	3	0.11	0.01	0.04	0.00	0.00	24.0
39	0	-5978	238	-389	0	-13400	-285	6.28	6.28	12.57	12.57	3	0.50	0.01	0.04	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	88	-3901	206	282	0	-2055	-40	6.28	6.28	12.57	12.57	3	0.08	0.00	0.03	0.00	0.00	24.0
2	88	-3003	236	208	0	-1595	-83	6.28	6.28	12.57	12.57	2	0.09	0.00	0.02	0.00	0.00	24.0
3	88	-3050	237	225	0	-1562	-84	6.28	6.28	12.57	12.57	2	0.09	0.00	0.02	0.00	0.00	24.0
4	88	-2951	81	208	0	-1599	23	6.28	6.28	12.57	12.57	2	0.09	0.00	0.02	0.00	0.00	24.0
5	88	-2997	81	226	0	-1566	22	6.28	6.28	12.57	12.57	2	0.09	0.00	0.02	0.00	0.00	24.0
6	88	-2931	182	187	0	-1636	-45	6.28	6.28	12.57	12.57	2	0.09	0.00	0.02	0.00	0.00	24.0
7	88	-3086	183	246	0	-1525	-48	6.28	6.28	12.57	12.57	2	0.08	0.00	0.03	0.00	0.00	24.0
8	88	-2915	135	187	0	-1637	-13	6.28	6.28	12.57	12.57	2	0.09	0.00	0.02	0.00	0.00	24.0
9	88	-3070	136	246	0	-1526	-17	6.28	6.28	12.57	12.57	2	0.08	0.00	0.03	0.00	0.00	24.0
10	88	-3003	236	208	0	-1595	-83	6.28	6.28	12.57	12.57	2	0.09	0.00	0.02	0.00	0.00	24.0
11	88	-3050	237	225	0	-1562	-84	6.28	6.28	12.57	12.57	2	0.09	0.00	0.02	0.00	0.00	24.0
12	88	-2951	81	208	0	-1599	23	6.28	6.28	12.57	12.57	2	0.09	0.00	0.02	0.00	0.00	24.0
13	88	-2997	81	226	0	-1566	22	6.28	6.28	12.57	12.57	2	0.09	0.00	0.02	0.00	0.00	24.0
14	88	-2931	182	187	0	-1636	-45	6.28	6.28	12.57	12.57	2	0.09	0.00	0.02	0.00	0.00	24.0
15	88	-3086	183	246	0	-1525	-48	6.28	6.28	12.57	12.57	2	0.08	0.00	0.03	0.00	0.00	24.0
16	88	-2915	135	187	0	-1637	-13	6.28	6.28	12.57	12.57	2	0.09	0.00	0.02	0.00	0.00	24.0
17	88	-3070	136	246	0	-1526	-17	6.28	6.28	12.57	12.57	2	0.08	0.00	0.03	0.00	0.00	24.0
18	88	-7370	573	682	0	-4708	-305	6.28	6.28	12.57	12.57	3	0.18	0.01	0.07	0.00	0.00	24.0
19	88	-6152	-51	535	0	-4051	129	6.28	6.28	12.57	12.57	3	0.15	0.01	0.06	0.00	0.00	24.0
20	88	-6416	255	-412	0	-9822	-88	6.28	6.28	12.57	12.57	3	0.36	0.01	0.04	0.00	0.00	24.0
37	88	-6878	769	624	0	-4174	-436	6.28	6.28	12.57	12.57	3	0.16	0.01	0.07	0.00	0.00	24.0
38	88	-4848	-272	379	0	-3080	287	6.28	6.28	12.57	12.57	3	0.12	0.01	0.04	0.00	0.00	24.0
39	88	-5288	238	-1199	0	-12697	-75	6.28	6.28	12.57	12.57	3	0.48	0.02	0.13	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	177	-3210	206	282	0	-2304	143	6.28	6.28	12.57	12.57	3	0.09	0.00	0.03	0.00	0.00	24.0
2	177	-2472	236	208	0	-1778	126	6.28	6.28	12.57	12.57	2	0.10	0.00	0.02	0.00	0.00	24.0
3	177	-2519	237	225	0	-1762	125	6.28	6.28	12.57	12.57	2	0.10	0.00	0.02	0.00	0.00	24.0
4	177	-2420	81	208	0	-1783	94	6.28	6.28	12.57	12.57	2	0.10	0.00	0.02	0.00	0.00	24.0
5	177	-2466	81	226	0	-1766	93	6.28	6.28	12.57	12.57	2	0.10	0.00	0.03	0.00	0.00	24.0
6	177	-2400	182	187	0	-1801	116	6.28	6.28	12.57	12.57	2	0.10	0.00	0.02	0.00	0.00	24.0
7	177	-2555	183	246	0	-1742	113	6.28	6.28	12.57	12.57	2	0.10	0.00	0.03	0.00	0.00	24.0
8	177	-2384	135	187	0	-1802	106	6.28	6.28	12.57	12.57	2	0.10	0.00	0.02	0.00	0.00	24.0
9	177	-2539	136	246	0	-1744	104	6.28	6.28	12.57	12.57	2	0.10	0.00	0.03	0.00	0.00	24.0
10	177	-2472	236	208	0	-1778	126	6.28	6.28	12.57	12.57	2	0.10	0.00	0.02	0.00	0.00	24.0
11	177	-2519	237	225	0	-1762	125	6.28	6.28	12.57	12.57	2	0.10	0.00	0.02	0.00	0.00	24.0
12	177	-2420	81	208	0	-1783	94	6.28	6.28	12.57	12.57	2	0.10	0.00	0.02	0.00	0.00	24.0
13	177	-2466	81	226	0	-1766	93	6.28	6.28	12.57	12.57	2	0.10	0.00	0.03	0.00	0.00	24.0
14	177	-2400	182	187	0	-1801	116	6.28	6.28	12.57	12.57	2	0.10	0.00	0.02	0.00	0.00	24.0
15	177	-2555	183	246	0	-1742	113	6.28	6.28	12.57	12.57	2	0.10	0.00	0.03	0.00	0.00	24.0
16	177	-2384	135	187	0	-1802	106	6.28	6.28	12.57	12.57	2	0.10	0.00	0.02	0.00	0.00	24.0
17	177	-2539	136	246	0	-1744	104	6.28	6.28	12.57	12.57	2	0.10	0.00	0.03	0.00	0.00	24.0
18	177	-6680	573	682	0	-5311	202	6.28	6.28	12.57	12.57	3	0.20	0.01	0.07	0.00	0.00	24.0
19	177	-5462	-51	535	0	-4525	84	6.28	6.28	12.57	12.57	3	0.17	0.01	0.06	0.00	0.00	24.0
20	177	-5726	255	-898	0	-9242	137	6.28	6.28	12.57	12.57	3	0.35	0.02	0.09	0.00	0.00	24.0
37	177	-6188	769	624	0	-4726	244	6.28	6.28	12.57	12.57	3	0.18	0.01	0.07	0.00	0.00	24.0
38	177	-4158	-272	379	0	-3415	47	6.28	6.28	12.57	12.57	3	0.13	0.01	0.04	0.00	0.00	24.0
39	177	-4598	238	-2009	0	-11278	136	6.28	6.28	12.57	12.57	3	0.43	0.04	0.22	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	266	-2520	206	282	0	-2553	325	6.28	6.28	12.57	12.57	3	0.10	0.00	0.03	0.00	0.00	24.0
2	266	-1941	236	208	0	-1962	335	6.28	6.28	12.57	12.57	2	0.12	0.00	0.02	0.00	0.00	24.0

3	266	-1988	237	225	0	-1961	335	6.28	6.28	12.57	12.57	2	0.12	0.00	0.03	0.00	0.00	24.0
4	266	-1889	81	208	0	-1967	165	6.28	6.28	12.57	12.57	2	0.11	0.00	0.02	0.00	0.00	24.0
5	266	-1935	81	226	0	-1965	165	6.28	6.28	12.57	12.57	2	0.11	0.00	0.03	0.00	0.00	24.0
6	266	-1869	182	187	0	-1966	276	6.28	6.28	12.57	12.57	2	0.12	0.00	0.02	0.00	0.00	24.0
7	266	-2024	183	246	0	-1960	275	6.28	6.28	12.57	12.57	2	0.12	0.00	0.03	0.00	0.00	24.0
8	266	-1853	135	187	0	-1968	225	6.28	6.28	12.57	12.57	2	0.12	0.00	0.02	0.00	0.00	24.0
9	266	-2008	136	246	0	-1961	224	6.28	6.28	12.57	12.57	2	0.12	0.00	0.03	0.00	0.00	24.0
10	266	-1941	236	208	0	-1962	335	6.28	6.28	12.57	12.57	2	0.12	0.00	0.02	0.00	0.00	24.0
11	266	-1988	237	225	0	-1961	335	6.28	6.28	12.57	12.57	2	0.12	0.00	0.03	0.00	0.00	24.0
12	266	-1889	81	208	0	-1967	165	6.28	6.28	12.57	12.57	2	0.11	0.00	0.02	0.00	0.00	24.0
13	266	-1935	81	226	0	-1965	165	6.28	6.28	12.57	12.57	2	0.11	0.00	0.03	0.00	0.00	24.0
14	266	-1869	182	187	0	-1966	276	6.28	6.28	12.57	12.57	2	0.12	0.00	0.02	0.00	0.00	24.0
15	266	-2024	183	246	0	-1960	275	6.28	6.28	12.57	12.57	2	0.12	0.00	0.03	0.00	0.00	24.0
16	266	-1853	135	187	0	-1968	225	6.28	6.28	12.57	12.57	2	0.12	0.00	0.02	0.00	0.00	24.0
17	266	-2008	136	246	0	-1961	224	6.28	6.28	12.57	12.57	2	0.12	0.00	0.03	0.00	0.00	24.0
18	266	-5989	573	682	0	-5914	710	6.28	6.28	12.57	12.57	3	0.23	0.01	0.07	0.00	0.00	24.0
19	266	-4771	-51	535	0	-4998	38	6.28	6.28	12.57	12.57	3	0.19	0.01	0.06	0.00	0.00	24.0
20	266	-5035	255	-1384	0	-8232	362	6.28	6.28	12.57	12.57	3	0.31	0.02	0.15	0.00	0.00	24.0
37	266	-5497	769	624	0	-5278	924	6.28	6.28	12.57	12.57	3	0.21	0.01	0.07	0.00	0.00	24.0
38	266	-3467	-272	379	0	-3750	-194	6.28	6.28	12.57	12.57	3	0.14	0.01	0.04	0.00	0.00	24.0
39	266	-3907	238	-2819	0	-9141	346	6.28	6.28	12.57	12.57	3	0.35	0.05	0.31	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	354	-1830	206	282	0	-2802	508	6.28	6.28	12.57	12.57	3	0.11	0.00	0.03	0.00	0.00	24.0
2	354	-1410	236	208	0	-2146	545	6.28	6.28	12.57	12.57	2	0.14	0.00	0.02	0.00	0.00	24.0
3	354	-1457	237	225	0	-2160	545	6.28	6.28	12.57	12.57	2	0.14	0.00	0.03	0.00	0.00	24.0
4	354	-1358	81	208	0	-2151	237	6.28	6.28	12.57	12.57	2	0.13	0.00	0.02	0.00	0.00	24.0
5	354	-1404	81	226	0	-2165	237	6.28	6.28	12.57	12.57	2	0.13	0.00	0.03	0.00	0.00	24.0
6	354	-1338	182	187	0	-2132	437	6.28	6.28	12.57	12.57	2	0.13	0.00	0.02	0.00	0.00	24.0
7	354	-1493	183	246	0	-2178	437	6.28	6.28	12.57	12.57	2	0.14	0.00	0.03	0.00	0.00	24.0
8	354	-1322	135	187	0	-2134	344	6.28	6.28	12.57	12.57	2	0.13	0.00	0.02	0.00	0.00	24.0
9	354	-1477	136	246	0	-2179	344	6.28	6.28	12.57	12.57	2	0.13	0.00	0.03	0.00	0.00	24.0
10	354	-1410	236	208	0	-2146	545	6.28	6.28	12.57	12.57	2	0.14	0.00	0.02	0.00	0.00	24.0
11	354	-1457	237	225	0	-2160	545	6.28	6.28	12.57	12.57	2	0.14	0.00	0.03	0.00	0.00	24.0
12	354	-1358	81	208	0	-2151	237	6.28	6.28	12.57	12.57	2	0.13	0.00	0.02	0.00	0.00	24.0
13	354	-1404	81	226	0	-2165	237	6.28	6.28	12.57	12.57	2	0.13	0.00	0.03	0.00	0.00	24.0
14	354	-1338	182	187	0	-2132	437	6.28	6.28	12.57	12.57	2	0.13	0.00	0.02	0.00	0.00	24.0
15	354	-1493	183	246	0	-2178	437	6.28	6.28	12.57	12.57	2	0.14	0.00	0.03	0.00	0.00	24.0
16	354	-1322	135	187	0	-2134	344	6.28	6.28	12.57	12.57	2	0.13	0.00	0.02	0.00	0.00	24.0
17	354	-1477	136	246	0	-2179	344	6.28	6.28	12.57	12.57	2	0.13	0.00	0.03	0.00	0.00	24.0
18	354	-5299	573	682	0	-6518	1217	6.28	6.28	12.57	12.57	3	0.26	0.01	0.07	0.00	0.00	24.0
19	354	-4081	-51	535	0	-5471	-7	6.28	6.28	12.57	12.57	3	0.21	0.01	0.06	0.00	0.00	24.0
20	354	-4345	255	-1870	0	-6792	588	6.28	6.28	12.57	12.57	3	0.26	0.03	0.20	0.00	0.00	24.0
37	354	-4807	769	624	0	-5831	1605	6.28	6.28	12.57	12.57	3	0.24	0.01	0.07	0.00	0.00	24.0
38	354	-2777	-272	379	0	-4086	-434	6.28	6.28	12.57	12.57	3	0.16	0.01	0.04	0.00	0.00	24.0
39	354	-3217	238	-3629	0	-6288	556	6.28	6.28	12.57	12.57	3	0.24	0.06	0.40	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 43 NI 39 NF 44 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 22D
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-5496	-911	533	0	-959	593	6.28	6.28	12.57	12.57	3	0.05	0.02	0.08	0.00	0.00	24.0
2	0	-4192	-677	407	0	-700	393	6.28	6.28	12.57	12.57	2	0.05	0.01	0.06	0.00	0.00	24.0
3	0	-4223	-675	440	0	-641	391	6.28	6.28	12.57	12.57	2	0.05	0.01	0.06	0.00	0.00	24.0
4	0	-4233	-727	380	0	-835	521	6.28	6.28	12.57	12.57	2	0.07	0.01	0.07	0.00	0.00	24.0
5	0	-4263	-726	414	0	-776	519	6.28	6.28	12.57	12.57	2	0.06	0.01	0.07	0.00	0.00	24.0
6	0	-4171	-696	359	0	-816	441	6.28	6.28	12.57	12.57	2	0.06	0.01	0.06	0.00	0.00	24.0
7	0	-4272	-691	470	0	-619	433	6.28	6.28	12.57	12.57	2	0.05	0.01	0.06	0.00	0.00	24.0
8	0	-4183	-712	351	0	-857	479	6.28	6.28	12.57	12.57	2	0.06	0.01	0.06	0.00	0.00	24.0
9	0	-4284	-706	462	0	-660	472	6.28	6.28	12.57	12.57	2	0.05	0.01	0.06	0.00	0.00	24.0
10	0	-4192	-677	407	0	-700	393	6.28	6.28	12.57	12.57	2	0.05	0.01	0.06	0.00	0.00	24.0
11	0	-4223	-675	440	0	-641	391	6.28	6.28	12.57	12.57	2	0.05	0.01	0.06	0.00	0.00	24.0
12	0	-4233	-727	380	0	-835	521	6.28	6.28	12.57	12.57	2	0.07	0.01	0.07	0.00	0.00	24.0
13	0	-4263	-726	414	0	-776	519	6.28	6.28	12.57	12.57	2	0.06	0.01	0.07	0.00	0.00	24.0
14	0	-4171	-696	359	0	-816	441	6.28	6.28	12.57	12.57	2	0.06	0.01	0.06	0.00	0.00	24.0
15	0	-4272	-691	470	0	-619	433	6.28	6.28	12.57	12.57	2	0.05	0.01	0.06	0.00	0.00	24.0
16	0	-4183	-712	351	0	-857	479	6.28	6.28	12.57	12.57	2	0.06	0.01	0.06	0.00	0.00	24.0
17	0	-4284	-706	462	0	-660	472	6.28	6.28	12.57	12.57	2	0.05	0.01	0.06	0.00	0.00	24.0
18	0	-7809	-693	1074	0	-1781	130	6.28	6.28	12.57	12.57	3	0.07	0.02	0.11	0.00	0.00	24.0
19	0	-8832	-944	1135	0	-2750	727	6.28	6.28	12.57	12.57	3	0.11	0.02	0.11	0.00	0.00	24.0
20	0	-7916	-851	-3	0	-6808	470	6.28	6.28	12.57	12.57	3	0.25	0.02	0.07	0.00	0.00	24.0
37	0	-6591	-647	869	0	-1036	-8	6.28	6.28	12.57	12.57	3	0.04	0.02	0.09	0.00	0.00	24.0
38	0	-8296	-1064	969	0	-2652	985	6.28	6.28	12.57	12.57	3	0.11	0.02	0.10	0.00	0.00	24.0
39	0	-6769	-911	-926	0	-9415	558	6.28	6.28	12.57	12.57	3	0.35	0.02	0.10	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	53	-5084	-911	533	0	-1242	111	6.28	6.28	12.57	12.57	3	0.05	0.02	0.08	0.00	0.00	24.0
2	53	-3875	-677	407	0	-915	35	6.28	6.28	12.57	12.57	2	0.05	0.01	0.06	0.00	0.00	24.0
3	53	-3906	-675	440	0	-873	34	6.28	6.28	12.57	12.57	2	0.05	0.01	0.06	0.00	0.00	24.0
4	53	-3916	-727	380	0	-1037	137	6.28	6.28	12.57	12.57	2	0.06	0.01	0.07	0.00	0.00	24.0
5	53	-3946	-726	414	0	-995	136	6.28	6.28	12.57	12.57	2	0.06	0.01	0.07	0.00	0.00	24.0
6	53	-3854	-696	359	0	-1006	73	6.28	6.28	12.57	12.57	2	0.06	0.01	0.06	0.00	0.00	24.0
7	53	-3955	-691	470	0	-868	68	6.28	6.28	12.57	12.57	2	0.05	0.01	0.06	0.00	0.00	24.0
8	53	-3866	-712	351	0	-1042	103	6.28	6.28	12.57	12.57	2	0.06	0.01	0.06	0.00	0.00	24.0
9	53	-3967	-706	462	0	-904	99	6.28	6.28	12.57	12.57	2	0.05	0.01	0.06	0.00	0.00	24.0
10	53	-3875	-677	407	0	-915	35	6.28	6.28	12.57	12.57	2	0.05	0.01	0.06	0.00	0.00	24.0
11	53	-3906	-675	440	0	-873	34	6.28	6.28	12.57	12.57	2	0.05	0.01	0.06	0.00	0.00	24.0
12	53	-3916	-727	380	0	-1037	137	6.28	6.28	12.57	12.57	2	0.06	0.01	0.07	0.00	0.00	24.0
13	53	-3946	-726	414	0	-995	136	6.28	6.28	12.57	12.57	2	0.06	0.01	0.07	0.00	0.00	24.0
14	53	-3854	-696	359	0	-1006	73	6.28	6.28	12.57	12.57	2	0.06	0.01	0.06	0.00	0.00	24.0
15	53	-3955	-691	470	0	-868	68	6.28	6.28	12.57	12.57	2	0.05	0.01	0.06	0.00	0.00	24.0
16	53	-3866	-712	351	0	-1042	103	6.28	6.28	12.57	12.57	2	0.06	0.01	0.06	0.00	0.00	24.0
17	53	-3967	-706	462	0	-904	99	6.28	6.28	12.57	12.57	2	0.05	0.01	0.06	0.00	0.00	24.0
18	53	-7396	-693	1074	0	-2349	-236	6.28	6.28	12.57	12.57	3	0.09	0.02	0.11	0.00	0.00	24.0
19	53	-8420	-944	1135	0	-3350	228	6.28	6.28	12.57	12.57	3	0.12	0.02	0.12	0.00	0.00	24.0
20	53	-7504	-851	-293	0	-6730	20	6.28	6.28	12.57	12.57	3	0.25	0.02	0.07	0.00	0.00	24.0
37	53	-6178	-647	869	0	-1495	-350	6.28	6.28	12.57	12.57	3	0.06	0.02	0.09	0.00	0.00	24.0
38	53	-7884	-1064	969	0	-3164	422	6.28	6.28	12.57	12.57	3	0.12	0.02	0.10	0.00	0.00	24.0
39	53	-6356	-911	-1410	0	-8797	76	6.28	6.28	12.57	12.57	3	0.33	0.02	0.15	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	106	-4671	-911	533	0	-1524	-371	6.28	6.28	12.57	12.57	3	0.06	0.02	0.08	0.00	0.00	24.0
2	106	-3558	-677	407	0	-1130	-322	6.28	6.28	12.57	12.57	2	0.07	0.01	0.06	0.00	0.00	24.0
3	106	-3588	-675	440	0	-1106	-323	6.28	6.28	12.57	12.57	2	0.07	0.01	0.06	0.00	0.00	24.0
4	106	-3598	-727	380	0	-1238	-248	6.28	6.28	12.57	12.57	2	0.08	0.01	0.07	0.00	0.00	24.0
5	106	-3628	-726	414	0	-1214	-248	6.28	6.28	12.57	12.57	2	0.07	0.01	0.07	0.00	0.00	24.0
6	106	-3536	-696	359	0	-1195	-296	6.28	6.28	12.57	12.57	2	0.08	0.01	0.06	0.00	0.00	24.0
7	106	-3638	-691	470	0	-1116	-297	6.28	6.28	12.57	12.57	2	0.07	0.01	0.06	0.00	0.00	24.0
8	106	-3548	-712	351	0	-1228	-273	6.28	6.28	12.57	12.57	2	0.08	0.01	0.06	0.00	0.00	24.0
9	106	-3650	-706	462	0	-1149	-275	6.28	6.28	12.57	12.57	2	0.07	0.01	0.06	0.00	0.00	24.0
10	106	-3558	-677	407	0	-1130	-322	6.28	6.28	12.57	12.57	2	0.07	0.01	0.06	0.00	0.00	24.0
11	106	-3588	-675	440	0	-1106	-323	6.28	6.28	12.57	12.57	2	0.07	0.01	0.06	0.00	0.00	24.0
12	106	-3598	-727	380	0	-1238	-248	6.28	6.28	12.57	12.57	2	0.08	0.01	0.07	0.00	0.00	24.0
13	106	-3628	-726	414	0	-1214	-248	6.28	6.28	12.57	12.57	2	0.07	0.01	0.07	0.00	0.00	24.0
14	106	-3536	-696	359	0	-1195	-296	6.28	6.28	12.57	12.57	2	0.08	0.01	0.06	0.00	0.00	24.0
15	106	-3638	-691	470	0	-1116	-297	6.28	6.28	12.57	12.57	2	0.07	0.01	0.06	0.00	0.00	24.0
16	106	-3548	-712	351	0	-1228	-273	6.28	6.28	12.57	12.57	2	0.08	0.01	0.06	0.00	0.00	24.0
17	106	-3650	-706	462	0	-1149	-275	6.28	6.28	12.57	12.57	2	0.07	0.01	0.06	0.00	0.00	24.0
18	106	-6984	-693	1074	0	-2917	-603	6.28	6.28	12.57	12.57	3	0.12	0.02	0.11	0.00	0.00	24.0
19	106	-8008	-944	1135	0	-3950	-271	6.28	6.28	12.57	12.57	3	0.15	0.02	0.12	0.00	0.00	24.0
20	106	-7091	-851	-583	0	-6499	-430	6.28	6.28	12.57	12.57	3	0.24	0.02	0.07	0.00	0.00	24.0
37	106	-5766	-647	869	0	-1954	-693	6.28	6.28	12.57	12.57	3	0.08	0.02	0.09	0.00	0.00	24.0
38	106	-7471	-1064	969	0	-3676	-140	6.28	6.28	12.57	12.57	3	0.14	0.02	0.10	0.00	0.00	24.0
39	106	-5944	-911	-1894	0	-7924	-405	6.28	6.28	12.57	12.57	3	0.30	0.03	0.20	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	159	-4259	-911	533	0	-1806	-853	6.28	6.28	12.57	12.57	3	0.08	0.02	0.08	0.00	0.00	24.0
2	159	-3240	-677	407	0	-1345	-680	6.28	6.28	12.57	12.57	2	0.10	0.01	0.06	0.00	0.00	24.0
3	159	-3271	-675	440	0	-1339	-680	6.28	6.28	12.57	12.57	2	0.10	0.01	0.06	0.00	0.00	24.0
4	159	-3281	-727	380	0	-1439	-632	6.28	6.28	12.57	12.57	2	0.10	0.01	0.07	0.00	0.00	24.0
5	159	-3311	-726	414	0	-1433	-631	6.28	6.28	12.57	12.57	2	0.10	0.01	0.07	0.00	0.00	24.0
6	159	-3219	-696	359	0	-1385	-664	6.28	6.28	12.57	12.57	2	0.10	0.01	0.06	0.00	0.00	24.0
7	159	-3320	-691	470	0	-1365	-663	6.28	6.28	12.57	12.57	2	0.10	0.01	0.06	0.00	0.00	24.0
8	159	-3231	-712	351	0	-1413	-650	6.28	6.28	12.57	12.57	2	0.10	0.01	0.06	0.00	0.00	24.0
9	159	-3332	-706	462	0	-1393	-648	6.28	6.28	12.57	12.57	2	0.10	0.01	0.06	0.00	0.00	24.0
10	159	-3240	-677	407	0	-1345	-680	6.28	6.28	12.57	12.57	2	0.10	0.01	0.06	0.00	0.00	24.0
11	159	-3271	-675	440	0	-1339	-680	6.28	6.28	12.57	12.57	2	0.10	0.01	0.06	0.00	0.00	24.0
12	159	-3281	-727	380	0	-1439	-632	6.28	6.28	12.57	12.57	2	0.10	0.01	0.07	0.00	0.00	24.0
13	159	-3311	-726	414	0	-1433	-631	6.28	6.28	12.57	12.57	2	0.10	0.01	0.07	0.00	0.00	24.0
14	159	-3219	-696	359	0	-1385	-664	6.28	6.28	12.57	12.57	2	0.10	0.01	0.06	0.00	0.00	24.0
15	159	-3320	-691	470	0	-1365	-663	6.28	6.28	12.57	12.57	2	0.10	0.01	0.06	0.00	0.00	24.0
16	159	-3231	-712	351	0	-1413	-650	6.28	6.28	12.57	12.57	2	0.10	0.01	0.06	0.00	0.00	24.0
17	159	-3332	-706	462	0	-1393	-648	6.28	6.28	12.57	12.57	2	0.10	0.01	0.06	0.00	0.00	24.0
18	159	-6572	-693	1074	0	-3485	-969	6.28	6.28	12.57	12.57	3	0.14	0.02	0.11	0.00	0.00	24.0
19	159	-7595	-944	1135	0	-4550	-770	6.28	6.28	12.57	12.57	3	0.18	0.02	0.12	0.00	0.00	24.0
20	159	-6678	-851	-874	0	-6114	-880	6.28	6.28	12.57	12.57	3	0.24	0.02	0.09	0.00	0.00	24.0
37	159	-5354	-647	869	0	-2414	-1035	6.28	6.28	12.57	12.57	3	0.11	0.02	0.09	0.00	0.00	24.0
38	159	-7059	-1064	969	0	-4189	-703	6.28	6.28	12.57	12.57	3	0.16	0.02	0.10	0.00	0.00	24.0
39	159	-5532	-911	-2378	0	-6794	-887	6.28	6.28	12.57	12.57	3	0.26	0.04	0.25	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	211	-3846	-911	533	0	-2088	-1335	6.28	6.28	12.57	12.57	3	0.11	0.02	0.08	0.00	0.00	24.0
2	211	-2923	-677	407	0	-1560	-1038	6.28	6.28	12.57	12.57	2	0.13	0.01	0.06	0.00	0.00	24.0
3	211	-2954	-675	440	0	-1572	-1037	6.28	6.28	12.57	12.57	2	0.13	0.01	0.06	0.00	0.00	24.0
4	211	-2964	-727	380	0	-1640	-1017	6.28	6.28	12.57	12.57	2	0.13	0.01	0.07	0.00	0.00	24.0
5	211	-2994	-726	414	0	-1652	-1015	6.28	6.28	12.57	12.57	2	0.13	0.01	0.07	0.00	0.00	24.0
6	211	-2902	-696	359	0	-1575	-1032	6.28	6.28	12.57	12.57	2	0.13	0.01	0.06	0.00	0.00	24.0
7	211	-3003	-691	470	0	-1613	-1028	6.28	6.28	12.57	12.57	2	0.13	0.01	0.06	0.00	0.00	24.0
8	211	-2914	-712	351	0	-1599	-1026	6.28	6.28	12.57	12.57	2	0.13	0.01	0.07	0.00	0.00	24.0
9	211	-3015	-706	462	0	-1637	-1021	6.28	6.28	12.57	12.57	2	0.13	0.01	0.06	0.00	0.00	24.0
10	211	-2923	-677	407	0	-1560	-1038	6.28	6.28	12.57	12.57	2	0.13	0.01	0.06	0.00	0.00	24.0
11	211	-2954	-675	440	0	-1572	-1037	6.28	6.28	12.57	12.57	2	0.13	0.01	0.06	0.00	0.00	24.0
12	211	-2964	-727	380	0	-1640	-1017	6.28	6.28	12.57	12.57	2	0.13	0.01	0.07	0.00	0.00	24.0
13	211	-2994	-726	414	0	-1652	-1015	6.28	6.28	12.57	12.57	2	0.13	0.01	0.07	0.00	0.00	24.0
14	211	-2902	-696	359	0	-1575	-1032	6.28	6.28	12.57	12.57	2	0.13	0.01	0.06	0.00	0.00	24.0
15	211	-3003	-691	470	0	-1613	-1028	6.28	6.28	12.57	12.57	2	0.13	0.01	0.06	0.00	0.00	24.0
16	211	-2914	-712	351	0	-1599	-1026	6.28	6.28	12.57	12.57	2	0.13	0.01	0.07	0.00	0.00	24.0
17	211	-3015	-706	462	0	-1637	-1021	6.28	6.28	12.57	12.57	2	0.13	0.01	0.06	0.00	0.00	24.0
18	211	-6159	-693	1074	0	-4053	-1336	6.28	6.28	12.57	12.57	3	0.17	0.02	0.11	0.00	0.00	24.0
19	211	-7183	-944	1135	0	-5150	-1269	6.28	6.28	12.57	12.57	3	0.21	0.02	0.12	0.00	0.00	24.0
20	211	-6266	-851	-1164	0	-5575	-1330	6.28	6.28	12.57	12.57	3	0.23	0.02	0.12	0.00	0.00	24.0
37	211	-4941	-647	869	0	-2873	-1377	6.28	6.28	12.57	12.57	3	0.13	0.02	0.09	0.00	0.00	24.0
38	211	-6646	-1064	969	0	-4701	-1266	6.28	6.28	12.57	12.57	3	0.19	0.02	0.10	0.00	0.00	24.0
39	211	-5119	-911	-2862	0	-5409	-1368	6.28	6.28	12.57	12.57	3	0.22	0.05	0.31	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 44 NI 295 NF 261 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 10E
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-4122	-314	-385	0	-1084	884	6.28	6.28	12.57	12.57	3	0.06	0.01	0.04	0.00	0.00	24.0
2	0	-3219	-200	-347	0	-978	564	6.28	6.28	12.57	12.57	2	0.08	0.01	0.04	0.00	0.00	24.0
3	0	-3210	-193	-226	0	-638	543	6.28	6.28	12.57	12.57	2	0.06	0.00	0.02	0.00	0.00	24.0
4	0	-3131	-290	-366	0	-1029	816	6.28	6.28	12.57	12.57	2	0.09	0.01	0.04	0.00	0.00	24.0
5	0	-3123	-282	-245	0	-689	795	6.28	6.28	12.57	12.57	2	0.07	0.01	0.03	0.00	0.00	24.0
6	0	-3198	-240	-495	0	-1393	677	6.28	6.28	12.57	12.57	2	0.10	0.01	0.05	0.00	0.00	24.0
7	0	-3169	-216	-92	0	-259	607	6.28	6.28	12.57	12.57	2	0.05	0.00	0.02	0.00	0.00	24.0
8	0	-3172	-267	-500	0	-1408	752	6.28	6.28	12.57	12.57	2	0.11	0.01	0.05	0.00	0.00	24.0
9	0	-3143	-242	-97	0	-274	682	6.28	6.28	12.57	12.57	2	0.05	0.00	0.02	0.00	0.00	24.0
10	0	-3219	-200	-347	0	-978	564	6.28	6.28	12.57	12.57	2	0.08	0.01	0.04	0.00	0.00	24.0
11	0	-3210	-193	-226	0	-638	543	6.28	6.28	12.57	12.57	2	0.06	0.00	0.02	0.00	0.00	24.0
12	0	-3131	-290	-366	0	-1029	816	6.28	6.28	12.57	12.57	2	0.09	0.01	0.04	0.00	0.00	24.0
13	0	-3123	-282	-245	0	-689	795	6.28	6.28	12.57	12.57	2	0.07	0.01	0.03	0.00	0.00	24.0
14	0	-3198	-240	-495	0	-1393	677	6.28	6.28	12.57	12.57	2	0.10	0.01	0.05	0.00	0.00	24.0
15	0	-3169	-216	-92	0	-259	607	6.28	6.28	12.57	12.57	2	0.05	0.00	0.02	0.00	0.00	24.0
16	0	-3172	-267	-500	0	-1408	752	6.28	6.28	12.57	12.57	2	0.11	0.01	0.05	0.00	0.00	24.0
17	0	-3143	-242	-97	0	-274	682	6.28	6.28	12.57	12.57	2	0.05	0.00	0.02	0.00	0.00	24.0
18	0	-6568	-511	-831	0	-2340	1439	6.28	6.28	12.57	12.57	3	0.12	0.01	0.09	0.00	0.00	24.0
19	0	-4957	-613	-732	0	-2061	1726	6.28	6.28	12.57	12.57	3	0.12	0.01	0.08	0.00	0.00	24.0
20	0	-5368	-516	-511	0	-571	1452	6.28	6.28	12.57	12.57	3	0.09	0.01	0.05	0.00	0.00	24.0

37	0	-6691	-390	-735	0	-2071	1095	6.28	6.28	12.57	12.57	3	0.10	0.01	0.08	0.00	0.00	24.0
38	0	-4005	-559	-571	0	-1607	1573	6.28	6.28	12.57	12.57	3	0.10	0.01	0.06	0.00	0.00	24.0
39	0	-4690	-397	-202	0	876	1117	6.28	6.28	12.57	12.57	3	0.07	0.01	0.04	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	58	-3671	-314	-385	0	-861	702	6.28	6.28	12.57	12.57	3	0.05	0.01	0.04	0.00	0.00	24.0
2	58	-2872	-200	-347	0	-777	448	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
3	58	-2863	-193	-226	0	-507	432	6.28	6.28	12.57	12.57	2	0.05	0.00	0.02	0.00	0.00	24.0
4	58	-2784	-290	-366	0	-818	648	6.28	6.28	12.57	12.57	2	0.07	0.01	0.04	0.00	0.00	24.0
5	58	-2776	-282	-245	0	-548	632	6.28	6.28	12.57	12.57	2	0.06	0.01	0.03	0.00	0.00	24.0
6	58	-2851	-240	-495	0	-1107	538	6.28	6.28	12.57	12.57	2	0.08	0.01	0.05	0.00	0.00	24.0
7	58	-2822	-216	-92	0	-206	482	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
8	58	-2825	-267	-500	0	-1119	598	6.28	6.28	12.57	12.57	2	0.08	0.01	0.06	0.00	0.00	24.0
9	58	-2796	-242	-97	0	-218	542	6.28	6.28	12.57	12.57	2	0.04	0.00	0.03	0.00	0.00	24.0
10	58	-2872	-200	-347	0	-777	448	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
11	58	-2863	-193	-226	0	-507	432	6.28	6.28	12.57	12.57	2	0.05	0.00	0.02	0.00	0.00	24.0
12	58	-2784	-290	-366	0	-818	648	6.28	6.28	12.57	12.57	2	0.07	0.01	0.04	0.00	0.00	24.0
13	58	-2776	-282	-245	0	-548	632	6.28	6.28	12.57	12.57	2	0.06	0.01	0.03	0.00	0.00	24.0
14	58	-2851	-240	-495	0	-1107	538	6.28	6.28	12.57	12.57	2	0.08	0.01	0.05	0.00	0.00	24.0
15	58	-2822	-216	-92	0	-206	482	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
16	58	-2825	-267	-500	0	-1119	598	6.28	6.28	12.57	12.57	2	0.08	0.01	0.06	0.00	0.00	24.0
17	58	-2796	-242	-97	0	-218	542	6.28	6.28	12.57	12.57	2	0.04	0.00	0.03	0.00	0.00	24.0
18	58	-6117	-511	-831	0	-1859	1143	6.28	6.28	12.57	12.57	3	0.09	0.01	0.09	0.00	0.00	24.0
19	58	-4506	-613	-732	0	-1638	1371	6.28	6.28	12.57	12.57	3	0.09	0.01	0.08	0.00	0.00	24.0
20	58	-4917	-516	-357	0	-321	1154	6.28	6.28	12.57	12.57	3	0.07	0.01	0.05	0.00	0.00	24.0
37	58	-6240	-390	-735	0	-1646	870	6.28	6.28	12.57	12.57	3	0.08	0.01	0.08	0.00	0.00	24.0
38	58	-3554	-559	-571	0	-1277	1250	6.28	6.28	12.57	12.57	3	0.08	0.01	0.06	0.00	0.00	24.0
39	58	-4239	-397	54	0	918	887	6.28	6.28	12.57	12.57	3	0.06	0.01	0.04	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	116	-3220	-314	-385	0	-639	520	6.28	6.28	12.57	12.57	3	0.04	0.01	0.04	0.00	0.00	24.0
2	116	-2525	-200	-347	0	-576	332	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
3	116	-2516	-193	-226	0	-376	320	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
4	116	-2437	-290	-366	0	-606	481	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
5	116	-2429	-282	-245	0	-406	468	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
6	116	-2504	-240	-495	0	-821	399	6.28	6.28	12.57	12.57	2	0.06	0.01	0.05	0.00	0.00	24.0
7	116	-2476	-216	-92	0	-152	357	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
8	116	-2478	-267	-500	0	-830	443	6.28	6.28	12.57	12.57	2	0.06	0.01	0.06	0.00	0.00	24.0
9	116	-2449	-242	-97	0	-162	402	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
10	116	-2525	-200	-347	0	-576	332	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
11	116	-2516	-193	-226	0	-376	320	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
12	116	-2437	-290	-366	0	-606	481	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
13	116	-2429	-282	-245	0	-406	468	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
14	116	-2504	-240	-495	0	-821	399	6.28	6.28	12.57	12.57	2	0.06	0.01	0.05	0.00	0.00	24.0
15	116	-2476	-216	-92	0	-152	357	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
16	116	-2478	-267	-500	0	-830	443	6.28	6.28	12.57	12.57	2	0.06	0.01	0.06	0.00	0.00	24.0
17	116	-2449	-242	-97	0	-162	402	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
18	116	-5666	-511	-831	0	-1379	847	6.28	6.28	12.57	12.57	3	0.07	0.01	0.09	0.00	0.00	24.0
19	116	-4054	-613	-732	0	-1214	1017	6.28	6.28	12.57	12.57	3	0.07	0.01	0.08	0.00	0.00	24.0
20	116	-4466	-516	-226	0	-154	855	6.28	6.28	12.57	12.57	3	0.05	0.01	0.05	0.00	0.00	24.0
37	116	-5789	-390	-735	0	-1220	645	6.28	6.28	12.57	12.57	3	0.06	0.01	0.08	0.00	0.00	24.0
38	116	-3103	-559	-571	0	-947	927	6.28	6.28	12.57	12.57	3	0.06	0.01	0.06	0.00	0.00	24.0
39	116	-3788	-397	273	0	821	658	6.28	6.28	12.57	12.57	3	0.05	0.01	0.04	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	173	-2769	-314	-385	0	-416	339	6.28	6.28	12.57	12.57	3	0.02	0.01	0.04	0.00	0.00	24.0
2	173	-2178	-200	-347	0	-375	216	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
3	173	-2169	-193	-226	0	-245	208	6.28	6.28	12.57	12.57	2	0.02	0.00	0.03	0.00	0.00	24.0
4	173	-2090	-290	-366	0	-395	313	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
5	173	-2082	-282	-245	0	-265	305	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
6	173	-2157	-240	-495	0	-535	260	6.28	6.28	12.57	12.57	2	0.04	0.01	0.06	0.00	0.00	24.0
7	173	-2129	-216	-92	0	-99	233	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
8	173	-2131	-267	-500	0	-541	289	6.28	6.28	12.57	12.57	2	0.04	0.01	0.06	0.00	0.00	24.0
9	173	-2102	-242	-97	0	-105	262	6.28	6.28	12.57	12.57	2	0.02	0.00	0.03	0.00	0.00	24.0
10	173	-2178	-200	-347	0	-375	216	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
11	173	-2169	-193	-226	0	-245	208	6.28	6.28	12.57	12.57	2	0.02	0.00	0.03	0.00	0.00	24.0
12	173	-2090	-290	-366	0	-395	313	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
13	173	-2082	-282	-245	0	-265	305	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
14	173	-2157	-240	-495	0	-535	260	6.28	6.28	12.57	12.57	2	0.04	0.01	0.06	0.00	0.00	24.0
15	173	-2129	-216	-92	0	-99	233	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
16	173	-2131	-267	-500	0	-541	289	6.28	6.28	12.57	12.57	2	0.04	0.01	0.06	0.00	0.00	24.0
17	173	-2102	-242	-97	0	-105	262	6.28	6.28	12.57	12.57	2	0.02	0.00	0.03	0.00	0.00	24.0
18	173	-5215	-511	-831	0	-898	552	6.28	6.28	12.57	12.57	3	0.05	0.01	0.09	0.00	0.00	24.0
19	173	-3603	-613	-732	0	-791	662	6.28	6.28	12.57	12.57	3	0.05	0.01	0.08	0.00	0.00	24.0
20	173	-4015	-516	-116	0	-56	557	6.28	6.28	12.57	12.57	3	0.03	0.01	0.05	0.00	0.00	24.0
37	173	-5338	-390	-735	0	-795	420	6.28	6.28	12.57	12.57	3	0.04	0.01	0.08	0.00	0.00	24.0
38	173	-2652	-559	-571	0	-617	604	6.28	6.28	12.57	12.57	3	0.04	0.01	0.06	0.00	0.00	24.0
39	173	-3337	-397	456	0	609	428	6.28	6.28	12.57	12.57	3	0.03	0.01	0.05	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	231	-2318	-314	-385	0	-193	157	6.28	6.28	12.57	12.57	3	0.01	0.01	0.04	0.00	0.00	24.0
2	231	-1831	-200	-347	0	-175	100	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
3	231	-1822	-193	-226	0	-114	97	6.28	6.28	12.57	12.57	2	0.01	0.00	0.03	0.00	0.00	24.0
4	231	-1743	-290	-366	0	-184	146	6.28	6.28	12.57	12.57	2	0.02	0.01	0.04	0.00	0.00	24.0
5	231	-1735	-282	-245	0	-123	142	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
6	231	-1810	-240	-495	0	-249	121	6.28	6.28	12.57	12.57	2	0.02	0.01	0.06	0.00	0.00	24.0
7	231	-1782	-216	-92	0	-46	108	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
8	231	-1784	-267	-500	0	-251	134	6.28	6.28	12.57	12.57	2	0.02	0.01	0.06	0.00	0.00	24.0
9	231	-1755	-242	-97	0	-49	122	6.28	6.28	12.57	12.57	2	0.01	0.00	0.03	0.00	0.00	24.0
10	231	-1831	-200	-347	0	-175	100	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
11	231	-1822	-193	-226	0	-114	97	6.28	6.28	12.57	12.57	2	0.01	0.00	0.03	0.00	0.00	24.0
12	231	-1743	-290	-366	0	-184	146	6.28	6.28	12.57	12.57	2	0.02	0.01	0.04	0.00	0.00	24.0
13	231	-1735	-282	-245	0	-123	142	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
14	231	-1810	-240	-495	0	-249	121	6.28	6.28	12.57	12.57	2	0.02	0.01	0.06	0.00	0.00	24.0
15	231	-1782	-216	-92	0	-46	108	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
16	231	-1784	-267	-500	0	-251	134	6.28	6.28	12.57	12.57	2	0.02	0.01	0.06	0.00	0.00	24.0
17	231	-1755	-242	-97	0	-49	122	6.28	6.28	12.57	12.57	2	0.01	0.00	0.03	0.00	0.00	24.0
18	231	-4764	-511	-831	0	-418	256	6.28	6.28	12.57	12.57	3	0.02	0.01	0.09	0.00	0.00	24.0
19	231	-3152	-613	-732	0	-368	308	6.28	6.28	12.57	12.57	3	0.02	0.01	0.08	0.00	0.00	24.0
20	231	-3564	-516	-29	0	-15	259	6.28	6.28	12.57	12.57	3	0.02	0.01	0.05	0.00	0.00	24.0
37	231	-4887	-390	-735	0	-370	194	6.28	6.28	12.57	12.57	3	0.02	0.01	0.08	0.00	0.00	24.0
38	231	-2201	-559	-571	0	-287	281	6.28	6.28	12.57	12.57	3	0.02	0.01	0.06	0.00	0.00	24.0
39	231	-2886	-397	602	0	301	199	6.28	6.28	12.57	12.57	3	0.02	0.01	0.07	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 45 NI 297 NF 260 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 15D
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-7638	-14	30	0	122	56	6.28	6.28	12.57	12.57	3	0.01	0.00	0.00	0.00	0.00	24.0
2	0	-5550	-33	-22	0	-91	134	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
3	0	-5460	-31	67	0	271	127	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
4	0	-6290	10	-20	0	-83	-40	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
5	0	-6201	12	69	0	279	-47	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
6	0	-5913	-20	-126	0	-510	80	6.28	6.28	12.57	12.57	2	0.03	0.00	0.01	0.00	0.00	24.0
7	0	-5615	-14	172	0	696	58	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
8	0	-6136	-7	-125	0	-508	28	6.28	6.28	12.57	12.57	2	0.03	0.00	0.01	0.00	0.00	24.0
9	0	-5837	-1	173	0	698	6	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
10	0	-5550	-33	-22	0	-91	134	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
11	0	-5460	-31	67	0	271	127	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
12	0	-6290	10	-20	0	-83	-40	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
13	0	-6201	12	69	0	279	-47	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
14	0	-5913	-20	-126	0	-510	80	6.28	6.28	12.57	12.57	2	0.03	0.00	0.01	0.00	0.00	24.0
15	0	-5615	-14	172	0	696	58	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
16	0	-6136	-7	-125	0	-508	28	6.28	6.28	12.57	12.57	2	0.03	0.00	0.01	0.00	0.00	24.0
17	0	-5837	-1	173	0	698	6	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
18	0	-12110	-102	31	0	126	414	6.28	6.28	12.57	12.57	3	0.02	0.00	0.01	0.00	0.00	24.0
19	0	-12370	34	62	0	248	-136	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
20	0	-11310	-30	21	0	1921	122	6.28	6.28	12.57	12.57	3	0.07	0.00	0.00	0.00	0.00	24.0
37	0	-10530	-140	16	0	64	564	6.28	6.28	12.57	12.57	3	0.03	0.00	0.01	0.00	0.00	24.0
38	0	-10960	87	66	0	268	-352	6.28	6.28	12.57	12.57	3	0.02	0.00	0.01	0.00	0.00	24.0
39	0	-9203	-19	-1	0	3056	78	6.28	6.28	12.57	12.57	3	0.11	0.00	0.00	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	88	-6948	-14	30	0	95	44	6.28	6.28	12.57	12.57	3	0.00	0.00	0.00	0.00	0.00	24.0
2	88	-5019	-33	-22	0	-71	104	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
3	88	-4929	-31	67	0	212	99	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
4	88	-5759	10	-20	0	-65	-32	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
5	88	-5670	12	69	0	218	-37	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
6	88	-5382	-20	-126	0	-399	63	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
7	88	-5084	-14	172	0	544	45	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
8	88	-5605	-7	-125	0	-397	22	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
9	88	-5306	-1	173	0	545	4	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
10	88	-5019	-33	-22	0	-71	104	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
11	88	-4929	-31	67	0	212	99	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
12	88	-5759	10	-20	0	-65	-32	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
13	88	-5670	12	69	0	218	-37	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
14	88	-5382	-20	-126	0	-399	63	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
15	88	-5084	-14	172	0	544	45	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
16	88	-5605	-7	-125	0	-397	22	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
17	88	-5306	-1	173	0	545	4	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
18	88	-11418	-102	31	0	98	323	6.28	6.28	12.57	12.57	3	0.02	0.00	0.01	0.00	0.00	24.0
19	88	-11678	34	62	0	193	-106	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
20	88	-10620	-30	256	0	1796	95	6.28	6.28	12.57	12.57	3	0.07	0.00	0.03	0.00	0.00	24.0
37	88	-9838	-140	16	0	50	441	6.28	6.28	12.57	12.57	3	0.02	0.00	0.01	0.00	0.00	24.0
38	88	-10269	87	66	0	209	-275	6.28	6.28	12.57	12.57	3	0.02	0.00	0.01	0.00	0.00	24.0
39	88	-8512	-19	391	0	2879	61	6.28	6.28	12.57	12.57	3	0.11	0.01	0.04	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	177	-6258	-14	30	0	68	32	6.28	6.28	12.57	12.57	3	0.00	0.00	0.00	0.00	0.00	24.0
2	177	-4488	-33	-22	0	-51	75	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
3	177	-4398	-31	67	0	152	71	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
4	177	-5228	10	-20	0	-47	-23	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
5	177	-5139	12	69	0	157	-26	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
6	177	-4851	-20	-126	0	-287	45	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
7	177	-4553	-14	172	0	391	33	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
8	177	-5074	-7	-125	0	-286	16	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
9	177	-4775	-1	173	0	392	3	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
10	177	-4488	-33	-22	0	-51	75	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
11	177	-4398	-31	67	0	152	71	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
12	177	-5228	10	-20	0	-47	-23	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
13	177	-5139	12	69	0	157	-26	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
14	177	-4851	-20	-126	0	-287	45	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
15	177	-4553	-14	172	0	391	33	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
16	177	-5074	-7	-125	0	-286	16	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
17	177	-4775	-1	173	0	392	3	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
18	177	-10727	-102	31	0	70	233	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
19	177	-10987	34	62	0	139	-76	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
20	177	-9930	-30	458	0	1477	69	6.28	6.28	12.57	12.57	3	0.05	0.01	0.05	0.00	0.00	24.0
37	177	-9147	-140	16	0	36	317	6.28	6.28	12.57	12.57	3	0.02	0.00	0.01	0.00	0.00	24.0
38	177	-9578	87	66	0	150	-197	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
39	177	-7822	-19	727	0	2380	44	6.28	6.28	12.57	12.57	3	0.09	0.01	0.07	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	266	-5567	-14	30	0	42	19	6.28	6.28	12.57	12.57	3	0.00	0.00	0.00	0.00	0.00	24.0
2	266	-3957	-33	-22	0	-32	46	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
3	266	-3867	-31	67	0	93	43	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
4	266	-4697	10	-20	0	-29	-14	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
5	266	-4608	12	69	0	95	-16	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
6	266	-4320	-20	-126	0	-176	28	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
7	266	-4022	-14	172	0	239	20	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
8	266	-4543	-7	-125	0	-175	10	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
9	266	-4244	-1	173	0	240	2	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
10	266	-3957	-33	-22	0	-32	46	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
11	266	-3867	-31	67	0	93	43	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
12	266	-4697	10	-20	0	-29	-14	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
13	266	-4608	12	69	0	95	-16	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
14	266	-4320	-20	-126	0	-176	28	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
15	266	-4022	-14	172	0	239	20	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
16	266	-4543	-7	-125	0	-175	10	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
17	266	-4244	-1	173	0	240	2	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
18	266	-10036	-102	31	0	42	142	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
19	266	-10296	34	62	0	84	-46	6.28	6.28	12.57	12.57	3	0.00	0.00	0.01	0.00	0.00	24.0
20	266	-9241	-30	625	0	995	42	6.28	6.28	12.57	12.57	3	0.04	0.01	0.06	0.00	0.00	24.0
37	266	-8456	-140	16	0	21	193	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
38	266	-8888	87	66	0	91	-120	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0

39	266	-7132	-19	1006	0	1609	27	6.28	6.28	12.57	12.57	3	0.06	0.02	0.10	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	354	-4877	-14	30	0	15	7	6.28	6.28	12.57	12.57	3	0.00	0.00	0.00	0.00	0.00	24.0
2	354	-3426	-33	-22	0	-12	16	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
3	354	-3336	-31	67	0	33	16	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
4	354	-4166	10	-20	0	-11	-5	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
5	354	-4077	12	69	0	34	-6	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
6	354	-3789	-20	-126	0	-64	10	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
7	354	-3491	-14	172	0	86	7	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
8	354	-4012	-7	-125	0	-64	4	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
9	354	-3713	-1	173	0	87	1	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
10	354	-3426	-33	-22	0	-12	16	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
11	354	-3336	-31	67	0	33	16	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
12	354	-4166	10	-20	0	-11	-5	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
13	354	-4077	12	69	0	34	-6	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
14	354	-3789	-20	-126	0	-64	10	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
15	354	-3491	-14	172	0	86	7	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
16	354	-4012	-7	-125	0	-64	4	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
17	354	-3713	-1	173	0	87	1	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
18	354	-9344	-102	31	0	14	51	6.28	6.28	12.57	12.57	3	0.00	0.00	0.01	0.00	0.00	24.0
19	354	-9604	34	62	0	30	-16	6.28	6.28	12.57	12.57	3	0.00	0.00	0.01	0.00	0.00	24.0
20	354	-8551	-30	759	0	380	15	6.28	6.28	12.57	12.57	3	0.01	0.01	0.08	0.00	0.00	24.0
37	354	-7764	-140	16	0	7	70	6.28	6.28	12.57	12.57	3	0.00	0.00	0.01	0.00	0.00	24.0
38	354	-8197	87	66	0	32	-43	6.28	6.28	12.57	12.57	3	0.00	0.00	0.01	0.00	0.00	24.0
39	354	-6441	-19	1229	0	616	10	6.28	6.28	12.57	12.57	3	0.02	0.02	0.13	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 46 NI 271 NF 259 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 20D
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-5349	179	-438	0	-1146	-468	6.28	6.28	12.57	12.57	3	0.05	0.01	0.05	0.00	0.00	24.0
2	0	-4026	144	-416	0	-1090	-377	6.28	6.28	12.57	12.57	2	0.07	0.01	0.05	0.00	0.00	24.0
3	0	-3996	142	-273	0	-715	-372	6.28	6.28	12.57	12.57	2	0.05	0.00	0.03	0.00	0.00	24.0
4	0	-4233	134	-400	0	-1048	-349	6.28	6.28	12.57	12.57	2	0.07	0.01	0.04	0.00	0.00	24.0
5	0	-4204	131	-257	0	-673	-344	6.28	6.28	12.57	12.57	2	0.05	0.00	0.03	0.00	0.00	24.0
6	0	-4133	143	-578	0	-1512	-374	6.28	6.28	12.57	12.57	2	0.09	0.01	0.06	0.00	0.00	24.0
7	0	-4035	136	-100	0	-263	-356	6.28	6.28	12.57	12.57	2	0.03	0.00	0.01	0.00	0.00	24.0
8	0	-4195	140	-573	0	-1499	-365	6.28	6.28	12.57	12.57	2	0.09	0.01	0.06	0.00	0.00	24.0
9	0	-4097	133	-96	0	-250	-347	6.28	6.28	12.57	12.57	2	0.03	0.00	0.01	0.00	0.00	24.0
10	0	-4026	144	-416	0	-1090	-377	6.28	6.28	12.57	12.57	2	0.07	0.01	0.05	0.00	0.00	24.0
11	0	-3996	142	-273	0	-715	-372	6.28	6.28	12.57	12.57	2	0.05	0.00	0.03	0.00	0.00	24.0
12	0	-4233	134	-400	0	-1048	-349	6.28	6.28	12.57	12.57	2	0.07	0.01	0.04	0.00	0.00	24.0
13	0	-4204	131	-257	0	-673	-344	6.28	6.28	12.57	12.57	2	0.05	0.00	0.03	0.00	0.00	24.0
14	0	-4133	143	-578	0	-1512	-374	6.28	6.28	12.57	12.57	2	0.09	0.01	0.06	0.00	0.00	24.0
15	0	-4035	136	-100	0	-263	-356	6.28	6.28	12.57	12.57	2	0.03	0.00	0.01	0.00	0.00	24.0
16	0	-4195	140	-573	0	-1499	-365	6.28	6.28	12.57	12.57	2	0.09	0.01	0.06	0.00	0.00	24.0
17	0	-4097	133	-96	0	-250	-347	6.28	6.28	12.57	12.57	2	0.03	0.00	0.01	0.00	0.00	24.0
18	0	-7388	312	-938	0	-2456	-816	6.28	6.28	12.57	12.57	3	0.10	0.02	0.10	0.00	0.00	24.0
19	0	-8868	335	-864	0	-2261	-875	6.28	6.28	12.57	12.57	3	0.10	0.02	0.09	0.00	0.00	24.0
20	0	-7573	298	-553	0	-704	-780	6.28	6.28	12.57	12.57	3	0.05	0.01	0.06	0.00	0.00	24.0
37	0	-6034	256	-813	0	-2127	-670	6.28	6.28	12.57	12.57	3	0.09	0.01	0.09	0.00	0.00	24.0
38	0	-8501	294	-688	0	-1802	-768	6.28	6.28	12.57	12.57	3	0.08	0.01	0.07	0.00	0.00	24.0
39	0	-6342	233	-171	0	794	-610	6.28	6.28	12.57	12.57	3	0.04	0.00	0.02	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	53	-4937	179	-438	0	-914	-374	6.28	6.28	12.57	12.57	3	0.04	0.01	0.05	0.00	0.00	24.0
2	53	-3709	144	-416	0	-870	-301	6.28	6.28	12.57	12.57	2	0.06	0.01	0.05	0.00	0.00	24.0
3	53	-3679	142	-273	0	-570	-297	6.28	6.28	12.57	12.57	2	0.04	0.00	0.03	0.00	0.00	24.0
4	53	-3916	134	-400	0	-836	-278	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
5	53	-3887	131	-257	0	-537	-274	6.28	6.28	12.57	12.57	2	0.04	0.00	0.03	0.00	0.00	24.0
6	53	-3816	143	-578	0	-1207	-298	6.28	6.28	12.57	12.57	2	0.08	0.01	0.06	0.00	0.00	24.0
7	53	-3718	136	-100	0	-210	-284	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
8	53	-3878	140	-573	0	-1196	-291	6.28	6.28	12.57	12.57	2	0.07	0.01	0.06	0.00	0.00	24.0
9	53	-3780	133	-96	0	-200	-277	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
10	53	-3709	144	-416	0	-870	-301	6.28	6.28	12.57	12.57	2	0.06	0.01	0.05	0.00	0.00	24.0
11	53	-3679	142	-273	0	-570	-297	6.28	6.28	12.57	12.57	2	0.04	0.00	0.03	0.00	0.00	24.0
12	53	-3916	134	-400	0	-836	-278	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
13	53	-3887	131	-257	0	-537	-274	6.28	6.28	12.57	12.57	2	0.04	0.00	0.03	0.00	0.00	24.0
14	53	-3816	143	-578	0	-1207	-298	6.28	6.28	12.57	12.57	2	0.08	0.01	0.06	0.00	0.00	24.0
15	53	-3718	136	-100	0	-210	-284	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
16	53	-3878	140	-573	0	-1196	-291	6.28	6.28	12.57	12.57	2	0.07	0.01	0.06	0.00	0.00	24.0
17	53	-3780	133	-96	0	-200	-277	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
18	53	-6976	312	-938	0	-1960	-651	6.28	6.28	12.57	12.57	3	0.08	0.02	0.10	0.00	0.00	24.0
19	53	-8456	335	-864	0	-1804	-698	6.28	6.28	12.57	12.57	3	0.08	0.02	0.09	0.00	0.00	24.0
20	53	-7160	298	-413	0	-449	-622	6.28	6.28	12.57	12.57	3	0.04	0.01	0.04	0.00	0.00	24.0
37	53	-5622	256	-813	0	-1697	-534	6.28	6.28	12.57	12.57	3	0.07	0.01	0.09	0.00	0.00	24.0
38	53	-8088	294	-688	0	-1438	-613	6.28	6.28	12.57	12.57	3	0.06	0.01	0.07	0.00	0.00	24.0
39	53	-5930	233	64	0	820	-487	6.28	6.28	12.57	12.57	3	0.04	0.00	0.02	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	106	-4524	179	-438	0	-683	-279	6.28	6.28	12.57	12.57	3	0.03	0.01	0.05	0.00	0.00	24.0
2	106	-3392	144	-416	0	-650	-225	6.28	6.28	12.57	12.57	2	0.04	0.01	0.05	0.00	0.00	24.0
3	106	-3362	142	-273	0	-426	-221	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
4	106	-3598	134	-400	0	-625	-208	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
5	106	-3570	131	-257	0	-401	-205	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
6	106	-3498	143	-578	0	-901	-223	6.28	6.28	12.57	12.57	2	0.06	0.01	0.06	0.00	0.00	24.0
7	106	-3400	136	-100	0	-157	-212	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
8	106	-3560	140	-573	0	-894	-217	6.28	6.28	12.57	12.57	2	0.06	0.01	0.06	0.00	0.00	24.0
9	106	-3462	133	-96	0	-149	-207	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
10	106	-3392	144	-416	0	-650	-225	6.28	6.28	12.57	12.57	2	0.04	0.01	0.05	0.00	0.00	24.0
11	106	-3362	142	-273	0	-426	-221	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
12	106	-3598	134	-400	0	-625	-208	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
13	106	-3570	131	-257	0	-401	-205	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
14	106	-3498	143	-578	0	-901	-223	6.28	6.28	12.57	12.57	2	0.06	0.01	0.06	0.00	0.00	24.0
15	106	-3400	136	-100	0	-157	-212	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
16	106	-3560	140	-573	0	-894	-217	6.28	6.28	12.57	12.57	2	0.06	0.01	0.06	0.00	0.00	24.0
17	106	-3462	133	-96	0	-149	-207	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
18	106	-6564	312	-938	0	-1464	-486	6.28	6.28	12.57	12.57	3	0.06	0.02	0.10	0.00	0.00	24.0

19	106	-8044	335	-864	0	-1348	-521	6.28	6.28	12.57	12.57	3	0.06	0.02	0.09	0.00	0.00	24.0
20	106	-6748	298	-292	0	-264	-465	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
37	106	-5209	256	-813	0	-1268	-399	6.28	6.28	12.57	12.57	3	0.05	0.01	0.09	0.00	0.00	24.0
38	106	-7676	294	-688	0	-1074	-457	6.28	6.28	12.57	12.57	3	0.05	0.01	0.07	0.00	0.00	24.0
39	106	-5517	233	264	0	732	-363	6.28	6.28	12.57	12.57	3	0.03	0.00	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	159	-4112	179	-438	0	-451	-184	6.28	6.28	12.57	12.57	3	0.02	0.01	0.05	0.00	0.00	24.0
2	159	-3074	144	-416	0	-429	-148	6.28	6.28	12.57	12.57	2	0.03	0.01	0.05	0.00	0.00	24.0
3	159	-3044	142	-273	0	-282	-146	6.28	6.28	12.57	12.57	2	0.02	0.00	0.03	0.00	0.00	24.0
4	159	-3281	134	-400	0	-413	-137	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
5	159	-3252	131	-257	0	-265	-135	6.28	6.28	12.57	12.57	2	0.02	0.00	0.03	0.00	0.00	24.0
6	159	-3181	143	-578	0	-596	-147	6.28	6.28	12.57	12.57	2	0.04	0.01	0.06	0.00	0.00	24.0
7	159	-3083	136	-100	0	-103	-140	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
8	159	-3243	140	-573	0	-591	-144	6.28	6.28	12.57	12.57	2	0.04	0.01	0.06	0.00	0.00	24.0
9	159	-3145	133	-96	0	-99	-137	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
10	159	-3074	144	-416	0	-429	-148	6.28	6.28	12.57	12.57	2	0.03	0.01	0.05	0.00	0.00	24.0
11	159	-3044	142	-273	0	-282	-146	6.28	6.28	12.57	12.57	2	0.02	0.00	0.03	0.00	0.00	24.0
12	159	-3281	134	-400	0	-413	-137	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
13	159	-3252	131	-257	0	-265	-135	6.28	6.28	12.57	12.57	2	0.02	0.00	0.03	0.00	0.00	24.0
14	159	-3181	143	-578	0	-596	-147	6.28	6.28	12.57	12.57	2	0.04	0.01	0.06	0.00	0.00	24.0
15	159	-3083	136	-100	0	-103	-140	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
16	159	-3243	140	-573	0	-591	-144	6.28	6.28	12.57	12.57	2	0.04	0.01	0.06	0.00	0.00	24.0
17	159	-3145	133	-96	0	-99	-137	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
18	159	-6151	312	-938	0	-968	-321	6.28	6.28	12.57	12.57	3	0.04	0.02	0.10	0.00	0.00	24.0
19	159	-7631	335	-864	0	-891	-344	6.28	6.28	12.57	12.57	3	0.04	0.02	0.09	0.00	0.00	24.0
20	159	-6336	298	-192	0	-137	-307	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
37	159	-4797	256	-813	0	-838	-264	6.28	6.28	12.57	12.57	3	0.04	0.01	0.09	0.00	0.00	24.0
38	159	-7264	294	-688	0	-710	-302	6.28	6.28	12.57	12.57	3	0.03	0.01	0.07	0.00	0.00	24.0
39	159	-5105	233	431	0	547	-240	6.28	6.28	12.57	12.57	3	0.02	0.01	0.05	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	211	-3700	179	-438	0	-220	-90	6.28	6.28	12.57	12.57	3	0.01	0.01	0.05	0.00	0.00	24.0
2	211	-2757	144	-416	0	-209	-72	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
3	211	-2727	142	-273	0	-137	-71	6.28	6.28	12.57	12.57	2	0.01	0.00	0.03	0.00	0.00	24.0
4	211	-2964	134	-400	0	-201	-67	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
5	211	-2935	131	-257	0	-129	-66	6.28	6.28	12.57	12.57	2	0.01	0.00	0.03	0.00	0.00	24.0
6	211	-2864	143	-578	0	-290	-72	6.28	6.28	12.57	12.57	2	0.02	0.01	0.06	0.00	0.00	24.0
7	211	-2766	136	-100	0	-50	-68	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
8	211	-2926	140	-573	0	-288	-70	6.28	6.28	12.57	12.57	2	0.02	0.01	0.06	0.00	0.00	24.0
9	211	-2828	133	-96	0	-48	-66	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
10	211	-2757	144	-416	0	-209	-72	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
11	211	-2727	142	-273	0	-137	-71	6.28	6.28	12.57	12.57	2	0.01	0.00	0.03	0.00	0.00	24.0
12	211	-2964	134	-400	0	-201	-67	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
13	211	-2935	131	-257	0	-129	-66	6.28	6.28	12.57	12.57	2	0.01	0.00	0.03	0.00	0.00	24.0
14	211	-2864	143	-578	0	-290	-72	6.28	6.28	12.57	12.57	2	0.02	0.01	0.06	0.00	0.00	24.0
15	211	-2766	136	-100	0	-50	-68	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
16	211	-2926	140	-573	0	-288	-70	6.28	6.28	12.57	12.57	2	0.02	0.01	0.06	0.00	0.00	24.0
17	211	-2828	133	-96	0	-48	-66	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
18	211	-5739	312	-938	0	-472	-157	6.28	6.28	12.57	12.57	3	0.02	0.02	0.10	0.00	0.00	24.0
19	211	-7219	335	-864	0	-434	-167	6.28	6.28	12.57	12.57	3	0.02	0.02	0.09	0.00	0.00	24.0
20	211	-5923	298	-112	0	-57	-149	6.28	6.28	12.57	12.57	3	0.01	0.01	0.03	0.00	0.00	24.0
37	211	-4384	256	-813	0	-408	-129	6.28	6.28	12.57	12.57	3	0.02	0.01	0.09	0.00	0.00	24.0
38	211	-6851	294	-688	0	-346	-146	6.28	6.28	12.57	12.57	3	0.02	0.01	0.07	0.00	0.00	24.0
39	211	-4692	233	564	0	283	-117	6.28	6.28	12.57	12.57	3	0.01	0.01	0.06	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 47 NI 129 NF 124 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 9B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-12030	-19	-76	0	-138	-50	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
2	0	-9293	57	-128	0	-238	-295	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
3	0	-9227	56	-37	0	-68	-291	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
4	0	-9287	-86	-80	0	-143	214	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
5	0	-9222	-87	11	0	26	218	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
6	0	-9367	9	-216	0	-403	-121	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
7	0	-9149	5	85	0	163	-108	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
8	0	-9366	-34	-202	0	-374	31	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
9	0	-9147	-38	100	0	191	44	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
10	0	-9293	57	-128	0	-238	-295	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
11	0	-9227	56	-37	0	-68	-291	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
12	0	-9287	-86	-80	0	-143	214	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
13	0	-9222	-87	11	0	26	218	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
14	0	-9367	9	-216	0	-403	-121	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
15	0	-9149	5	85	0	163	-108	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
16	0	-9366	-34	-202	0	-374	31	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
17	0	-9147	-38	100	0	191	44	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
18	0	-13110	167	-346	0	-635	-731	6.28	6.28	12.57	12.57	3	0.04	0.01	0.03	0.00	0.00	24.0
19	0	-12980	-266	-55	0	-77	804	6.28	6.28	12.57	12.57	3	0.04	0.00	0.02	0.00	0.00	24.0
20	0	-12940	-47	-316	0	-618	30	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
37	0	-12680	321	-408	0	-757	-1271	6.28	6.28	12.57	12.57	3	0.07	0.01	0.04	0.00	0.00	24.0
38	0	-12470	-400	79	0	172	1287	6.28	6.28	12.57	12.57	3	0.07	0.01	0.04	0.00	0.00	24.0
39	0	-12390	-36	-356	0	-729	-3	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	97	-11270	-19	-76	0	-64	-69	6.28	6.28	12.57	12.57	3	0.00	0.00	0.01	0.00	0.00	24.0
2	97	-8708	57	-128	0	-113	-239	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
3	97	-8642	56	-37	0	-32	-236	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
4	97	-8702	-86	-80	0	-66	131	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
5	97	-8637	-87	11	0	16	133	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
6	97	-8782	9	-216	0	-192	-113	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
7	97	-8564	5	85	0	80	-103	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
8	97	-8781	-34	-202	0	-177	-2	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
9	97	-8562	-38	100	0	94	8	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
10	97	-8708	57	-128	0	-113	-239	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
11	97	-8642	56	-37	0	-32	-236	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
12	97	-8702	-86	-80	0	-66	131	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
13	97	-8637	-87	11	0	16	133	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
14	97	-8782	9	-216	0	-192	-113	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0

15	97	-8564	5	85	0	80	-103	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
16	97	-8781	-34	-202	0	-177	-2	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
17	97	-8562	-38	100	0	94	8	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
18	97	-12350	167	-346	0	-297	-568	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
19	97	-12220	-266	-55	0	-24	545	6.28	6.28	12.57	12.57	3	0.03	0.00	0.02	0.00	0.00	24.0
20	97	-12178	-47	-316	0	-311	-16	6.28	6.28	12.57	12.57	3	0.01	0.01	0.03	0.00	0.00	24.0
37	97	-11920	321	-408	0	-359	-958	6.28	6.28	12.57	12.57	3	0.05	0.01	0.04	0.00	0.00	24.0
38	97	-11708	-400	79	0	96	897	6.28	6.28	12.57	12.57	3	0.05	0.01	0.04	0.00	0.00	24.0
39	97	-11630	-36	-356	0	-382	-38	6.28	6.28	12.57	12.57	3	0.01	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	195	-10511	-19	-76	0	10	-87	6.28	6.28	12.57	12.57	3	0.00	0.00	0.01	0.00	0.00	24.0
2	195	-8123	57	-128	0	11	-183	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
3	195	-8057	56	-37	0	4	-181	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
4	195	-8117	-86	-80	0	12	47	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
5	195	-8052	-87	11	0	5	49	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
6	195	-8197	9	-216	0	19	-105	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
7	195	-7979	5	85	0	-4	-98	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
8	195	-8196	-34	-202	0	20	-36	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
9	195	-7977	-38	100	0	-3	-29	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
10	195	-8123	57	-128	0	11	-183	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
11	195	-8057	56	-37	0	4	-181	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
12	195	-8117	-86	-80	0	12	47	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
13	195	-8052	-87	11	0	5	49	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
14	195	-8197	9	-216	0	19	-105	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
15	195	-7979	5	85	0	-4	-98	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
16	195	-8196	-34	-202	0	20	-36	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
17	195	-7977	-38	100	0	-3	-29	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
18	195	-11590	167	-346	0	41	-405	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
19	195	-11460	-266	-55	0	29	286	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
20	195	-11417	-47	-316	0	-3	-62	6.28	6.28	12.57	12.57	3	0.00	0.01	0.03	0.00	0.00	24.0
37	195	-11159	321	-408	0	38	-645	6.28	6.28	12.57	12.57	3	0.04	0.01	0.04	0.00	0.00	24.0
38	195	-10947	-400	79	0	19	508	6.28	6.28	12.57	12.57	3	0.03	0.01	0.04	0.00	0.00	24.0
39	195	-10869	-36	-356	0	-35	-73	6.28	6.28	12.57	12.57	3	0.00	0.01	0.04	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	292	-9752	-19	-76	0	84	-106	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
2	292	-7538	57	-128	0	136	-127	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
3	292	-7472	56	-37	0	40	-126	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
4	292	-7532	-86	-80	0	89	-36	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
5	292	-7467	-87	11	0	-6	-35	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
6	292	-7612	9	-216	0	230	-96	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
7	292	-7394	5	85	0	-87	-94	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
8	292	-7611	-34	-202	0	217	-69	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
9	292	-7392	-38	100	0	-101	-66	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
10	292	-7538	57	-128	0	136	-127	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
11	292	-7472	56	-37	0	40	-126	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
12	292	-7532	-86	-80	0	89	-36	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
13	292	-7467	-87	11	0	-6	-35	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
14	292	-7612	9	-216	0	230	-96	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
15	292	-7394	5	85	0	-87	-94	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
16	292	-7611	-34	-202	0	217	-69	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
17	292	-7392	-38	100	0	-101	-66	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
18	292	-10830	167	-346	0	379	-242	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
19	292	-10699	-266	-55	0	82	27	6.28	6.28	12.57	12.57	3	0.00	0.00	0.02	0.00	0.00	24.0
20	292	-10656	-47	-316	0	305	-108	6.28	6.28	12.57	12.57	3	0.01	0.01	0.03	0.00	0.00	24.0
37	292	-10398	321	-408	0	436	-331	6.28	6.28	12.57	12.57	3	0.02	0.01	0.04	0.00	0.00	24.0
38	292	-10186	-400	79	0	-58	118	6.28	6.28	12.57	12.57	3	0.01	0.01	0.04	0.00	0.00	24.0
39	292	-10108	-36	-356	0	313	-108	6.28	6.28	12.57	12.57	3	0.01	0.01	0.04	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	390	-8992	-19	-76	0	158	-124	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
2	390	-6953	57	-128	0	260	-71	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
3	390	-6887	56	-37	0	77	-71	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
4	390	-6947	-86	-80	0	167	-120	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
5	390	-6882	-87	11	0	-17	-120	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
6	390	-7027	9	-216	0	442	-88	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
7	390	-6809	5	85	0	-170	-89	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
8	390	-7026	-34	-202	0	414	-102	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
9	390	-6807	-38	100	0	-198	-103	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
10	390	-6953	57	-128	0	260	-71	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
11	390	-6887	56	-37	0	77	-71	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
12	390	-6947	-86	-80	0	167	-120	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
13	390	-6882	-87	11	0	-17	-120	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
14	390	-7027	9	-216	0	442	-88	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
15	390	-6809	5	85	0	-170	-89	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
16	390	-7026	-34	-202	0	414	-102	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
17	390	-6807	-38	100	0	-198	-103	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
18	390	-10070	167	-346	0	716	-79	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
19	390	-9939	-266	-55	0	136	-231	6.28	6.28	12.57	12.57	3	0.01	0.00	0.03	0.00	0.00	24.0
20	390	-9894	-47	-316	0	612	-154	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
37	390	-9638	321	-408	0	833	-18	6.28	6.28	12.57	12.57	3	0.03	0.01	0.04	0.00	0.00	24.0
38	390	-9424	-400	79	0	-135	-272	6.28	6.28	12.57	12.57	3	0.02	0.01	0.04	0.00	0.00	24.0
39	390	-9348	-36	-356	0	660	-143	6.28	6.28	12.57	12.57	3	0.03	0.01	0.04	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

VERIFICA NODO IN TESTA AL PILASTRO, NODO NUM. 124 NON CONFINATO

(par.7.2.2 NTC2018 "La domanda di resistenza valutata con i criteri della progettazione in capacità può essere assunta non superiore alla domanda di resistenza valutata per il caso di comportamento strutturale non dissipativo.")

PROGETTAZIONE IN CAPACITA'

Asse loc. pilastro y nodo: --

Asse loc. pilastro z nodo INTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 40.0 cm, hjc= 50.0 cm

FxMin,inf	FxMin,sup	FxMax,sup	FySup	FzSup	Vjbdy	Vjbdz	Vres,y	Vres,z	I.R.compr.	Ashy	Ashz	PASSO	Nota
	daN				daN		daN			cmq		cm	
-6807	1	-0	0	0	--	35233	--	175015	0.20	--	4.08	13.08	

VERIFICA DI RESISTENZA CON SOLLECITAZIONI COMPORTAMENTO NON DISSIPATIVO

Asse loc. pilastro z nodo INTERNO: Hjw= 40.0 cm, bj= 40.0 cm, hjc= 50.0 cm, db1= 45.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb,1	Mb,2	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota

	daN		daN*m		daN			cmq	cm
2	-0	-6953	-2489	-2229	0	642	175015	0.00	0.00	40.00
3	-0	-6887	-2358	-2281	0	190	175015	0.00	0.00	40.00
4	-0	-6947	-2441	-2274	0	412	175015	0.00	0.00	40.00
5	-0	-6882	-2309	-2326	0	42	175015	0.00	0.00	40.00
6	-0	-7027	-2626	-2185	0	1089	175015	0.01	0.00	40.00
7	-0	-6809	-2187	-2357	0	420	175015	0.00	0.00	40.00
8	-0	-7026	-2612	-2198	0	1022	175015	0.01	0.00	40.00
9	-0	-6807	-2173	-2371	0	489	175015	0.00	0.00	40.00
10	-0	-6953	-2489	-2229	0	642	175015	0.00	0.00	40.00
11	-0	-6887	-2358	-2281	0	190	175015	0.00	0.00	40.00
12	-0	-6947	-2441	-2274	0	412	175015	0.00	0.00	40.00
13	-0	-6882	-2309	-2326	0	42	175015	0.00	0.00	40.00
14	-0	-7027	-2626	-2185	0	1089	175015	0.01	0.00	40.00
15	-0	-6809	-2187	-2357	0	420	175015	0.00	0.00	40.00
16	-0	-7026	-2612	-2198	0	1022	175015	0.01	0.00	40.00
17	-0	-6807	-2173	-2371	0	489	175015	0.00	0.00	40.00

CONFRONTO E SINTESI CONCLUSIVE (si assume in ogni caso passo <= 15 cm)

I.R.compr.	Ashy	Ashz	PASSO	Nota
	cmq		cm	
0.01	--	--	15.00	**VERIFICATO**

ASTA NUM. 48 NI 128 NF 125 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 14B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-19220	18	-360	0	-636	-21	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
2	0	-14820	92	-308	0	-534	-231	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
3	0	-14740	91	-237	0	-431	-230	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
4	0	-14840	-63	-318	0	-548	197	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
5	0	-14750	-63	-246	0	-445	199	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
6	0	-14920	38	-395	0	-660	-83	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
7	0	-14650	36	-156	0	-316	-78	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
8	0	-14920	-8	-398	0	-663	45	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
9	0	-14660	-10	-159	0	-320	51	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
10	0	-14820	92	-308	0	-534	-231	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
11	0	-14740	91	-237	0	-431	-230	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
12	0	-14840	-63	-318	0	-548	197	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
13	0	-14750	-63	-246	0	-445	199	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
14	0	-14920	38	-395	0	-660	-83	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
15	0	-14650	36	-156	0	-316	-78	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
16	0	-14920	-8	-398	0	-663	45	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
17	0	-14660	-10	-159	0	-320	51	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
18	0	-21140	242	-666	0	-1097	-628	6.28	6.28	12.57	12.57	3	0.05	0.01	0.06	0.00	0.00	24.0
19	0	-21090	-241	-612	0	-1019	677	6.28	6.28	12.57	12.57	3	0.05	0.01	0.05	0.00	0.00	24.0
20	0	-21000	5	-799	0	-1345	13	6.28	6.28	12.57	12.57	3	0.05	0.01	0.07	0.00	0.00	24.0
37	0	-20260	409	-595	0	-987	-1079	6.28	6.28	12.57	12.57	3	0.06	0.01	0.05	0.00	0.00	24.0
38	0	-20180	-396	-506	0	-857	1098	6.28	6.28	12.57	12.57	3	0.06	0.01	0.04	0.00	0.00	24.0
39	0	-20030	14	-817	0	-1399	-9	6.28	6.28	12.57	12.57	3	0.05	0.01	0.07	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	97	-18460	18	-360	0	-285	-3	6.28	6.28	12.57	12.57	3	0.01	0.01	0.03	0.00	0.00	24.0
2	97	-14235	92	-308	0	-234	-142	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
3	97	-14155	91	-237	0	-200	-141	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
4	97	-14255	-63	-318	0	-238	136	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
5	97	-14165	-63	-246	0	-205	137	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
6	97	-14335	38	-395	0	-274	-46	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
7	97	-14065	36	-156	0	-163	-42	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
8	97	-14335	-8	-398	0	-275	38	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
9	97	-14075	-10	-159	0	-164	41	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
10	97	-14235	92	-308	0	-234	-142	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
11	97	-14155	91	-237	0	-200	-141	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
12	97	-14255	-63	-318	0	-238	136	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
13	97	-14165	-63	-246	0	-205	137	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
14	97	-14335	38	-395	0	-274	-46	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
15	97	-14065	36	-156	0	-163	-42	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
16	97	-14335	-8	-398	0	-275	38	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
17	97	-14075	-10	-159	0	-164	41	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
18	97	-20378	242	-666	0	-448	-392	6.28	6.28	12.57	12.57	3	0.02	0.01	0.06	0.00	0.00	24.0
19	97	-20330	-241	-612	0	-422	443	6.28	6.28	12.57	12.57	3	0.03	0.01	0.05	0.00	0.00	24.0
20	97	-20240	5	-799	0	-566	18	6.28	6.28	12.57	12.57	3	0.02	0.01	0.07	0.00	0.00	24.0
37	97	-19498	409	-595	0	-406	-680	6.28	6.28	12.57	12.57	3	0.04	0.01	0.05	0.00	0.00	24.0
38	97	-19420	-396	-506	0	-364	712	6.28	6.28	12.57	12.57	3	0.04	0.01	0.04	0.00	0.00	24.0
39	97	-19270	14	-817	0	-602	5	6.28	6.28	12.57	12.57	3	0.02	0.01	0.07	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	195	-17700	18	-360	0	67	15	6.28	6.28	12.57	12.57	3	0.00	0.01	0.03	0.00	0.00	24.0
2	195	-13650	92	-308	0	67	-52	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
3	195	-13570	91	-237	0	30	-52	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
4	195	-13670	-63	-318	0	72	75	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
5	195	-13580	-63	-246	0	35	76	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
6	195	-13750	38	-395	0	112	-8	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
7	195	-13480	36	-156	0	-11	-7	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
8	195	-13750	-8	-398	0	113	30	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
9	195	-13490	-10	-159	0	-9	31	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
10	195	-13650	92	-308	0	67	-52	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
11	195	-13570	91	-237	0	30	-52	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
12	195	-13670	-63	-318	0	72	75	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
13	195	-13580	-63	-246	0	35	76	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
14	195	-13750	38	-395	0	112	-8	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
15	195	-13480	36	-156	0	-11	-7	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
16	195	-13750	-8	-398	0	113	30	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
17	195	-13490	-10	-159	0	-9	31	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
18	195	-19615	242	-666	0	201	-156	6.28	6.28	12.57	12.57	3	0.01	0.01	0.06	0.00	0.00	24.0

19	195	-19570	-241	-612	0	174	208	6.28	6.28	12.57	12.57	3	0.01	0.01	0.05	0.00	0.00	24.0
20	195	-19480	5	-799	0	213	24	6.28	6.28	12.57	12.57	3	0.01	0.01	0.07	0.00	0.00	24.0
37	195	-18735	409	-595	0	174	-281	6.28	6.28	12.57	12.57	3	0.02	0.01	0.05	0.00	0.00	24.0
38	195	-18660	-396	-506	0	129	326	6.28	6.28	12.57	12.57	3	0.02	0.01	0.04	0.00	0.00	24.0
39	195	-18510	14	-817	0	195	18	6.28	6.28	12.57	12.57	3	0.01	0.01	0.07	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	292	-16940	18	-360	0	418	33	6.28	6.28	12.57	12.57	3	0.01	0.01	0.03	0.00	0.00	24.0
2	292	-13065	92	-308	0	368	37	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
3	292	-12985	91	-237	0	261	37	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
4	292	-13085	-63	-318	0	382	14	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
5	292	-12995	-63	-246	0	275	14	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
6	292	-13165	38	-395	0	497	29	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
7	292	-12895	36	-156	0	142	29	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
8	292	-13165	-8	-398	0	501	22	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
9	292	-12905	-10	-159	0	146	22	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
10	292	-13065	92	-308	0	368	37	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
11	292	-12985	91	-237	0	261	37	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
12	292	-13085	-63	-318	0	382	14	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
13	292	-12995	-63	-246	0	275	14	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
14	292	-13165	38	-395	0	497	29	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
15	292	-12895	36	-156	0	142	29	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
16	292	-13165	-8	-398	0	501	22	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
17	292	-12905	-10	-159	0	146	22	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
18	292	-18852	242	-666	0	851	80	6.28	6.28	12.57	12.57	3	0.03	0.01	0.06	0.00	0.00	24.0
19	292	-18810	-241	-612	0	771	-27	6.28	6.28	12.57	12.57	3	0.03	0.01	0.05	0.00	0.00	24.0
20	292	-18720	5	-799	0	993	29	6.28	6.28	12.57	12.57	3	0.03	0.01	0.07	0.00	0.00	24.0
37	292	-17972	409	-595	0	754	117	6.28	6.28	12.57	12.57	3	0.03	0.01	0.05	0.00	0.00	24.0
38	292	-17900	-396	-506	0	622	-60	6.28	6.28	12.57	12.57	3	0.02	0.01	0.05	0.00	0.00	24.0
39	292	-17750	14	-817	0	991	32	6.28	6.28	12.57	12.57	3	0.03	0.01	0.07	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	390	-16180	18	-360	0	769	51	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
2	390	-12480	92	-308	0	669	126	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
3	390	-12400	91	-237	0	492	126	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
4	390	-12500	-63	-318	0	692	-47	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
5	390	-12410	-63	-246	0	515	-48	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
6	390	-12580	38	-395	0	883	67	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
7	390	-12310	36	-156	0	294	64	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
8	390	-12580	-8	-398	0	890	15	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
9	390	-12320	-10	-159	0	301	12	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
10	390	-12480	92	-308	0	669	126	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
11	390	-12400	91	-237	0	492	126	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
12	390	-12500	-63	-318	0	692	-47	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
13	390	-12410	-63	-246	0	515	-48	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
14	390	-12580	38	-395	0	883	67	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
15	390	-12310	36	-156	0	294	64	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
16	390	-12580	-8	-398	0	890	15	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
17	390	-12320	-10	-159	0	301	12	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
18	390	-18090	242	-666	0	1500	316	6.28	6.28	12.57	12.57	3	0.06	0.01	0.06	0.00	0.00	24.0
19	390	-18050	-241	-612	0	1368	-262	6.28	6.28	12.57	12.57	3	0.05	0.01	0.05	0.00	0.00	24.0
20	390	-17960	5	-799	0	1772	34	6.28	6.28	12.57	12.57	3	0.06	0.01	0.07	0.00	0.00	24.0
37	390	-17210	409	-595	0	1334	516	6.28	6.28	12.57	12.57	3	0.05	0.01	0.05	0.00	0.00	24.0
38	390	-17140	-396	-506	0	1115	-446	6.28	6.28	12.57	12.57	3	0.05	0.01	0.05	0.00	0.00	24.0
39	390	-16990	14	-817	0	1788	46	6.28	6.28	12.57	12.57	3	0.06	0.01	0.07	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

VERIFICA NODO IN TESTA AL PILASTRO, NODO NUM. 125 NON CONFINATO

(par.7.2.2 NTC2018 "La domanda di resistenza valutata con i criteri della progettazione in capacità può essere assunta non superiore alla domanda di resistenza valutata per il caso di comportamento strutturale non dissipativo.")

PROGETTAZIONE IN CAPACITA'

Asse loc. pilastro y nodo: --

Asse loc. pilastro z nodo INTERNO: As2(inf)= 6.03, As1(sup)= 6.03, Hjw= 40.0 cm, bj= 40.0 cm, hjc= 50.0 cm

FxMin,inf	FxMin,sup	FxMax,sup	FySup	FzSup	Vjbdy	Vjbdz	Vres,y	Vres,z	I.R.compr.	Ashy	Ashz	PASSO	Nota
daN					daN		daN			cmq		cm	
-12310	1	-0	0	0	--	52849	--	175015	0.30	--	13.27	3.28	

VERIFICA DI RESISTENZA CON SOLLECITAZIONI COMPORTAMENTO NON DISSIPATIVO

Asse loc. pilastro z nodo INTERNO: Hjw= 40.0 cm, bj= 40.0 cm, hjc= 50.0 cm, db1= 45.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb,1	Mb,2	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-0	-12480	-4325	-3657	0	1649	175015	0.01	0.00	40.00	
3	-0	-12400	-4188	-3696	0	1215	175015	0.01	0.00	40.00	
4	-0	-12500	-4350	-3658	0	1709	175015	0.01	0.00	40.00	
5	-0	-12410	-4213	-3698	0	1272	175015	0.01	0.00	40.00	
6	-0	-12580	-4494	-3611	0	2180	175015	0.01	0.00	40.00	
7	-0	-12310	-4037	-3743	0	726	175015	0.00	0.00	40.00	
8	-0	-12580	-4501	-3612	0	2195	175015	0.01	0.00	40.00	
9	-0	-12320	-4044	-3744	0	741	175015	0.00	0.00	40.00	
10	-0	-12480	-4325	-3657	0	1649	175015	0.01	0.00	40.00	
11	-0	-12400	-4188	-3696	0	1215	175015	0.01	0.00	40.00	
12	-0	-12500	-4350	-3658	0	1709	175015	0.01	0.00	40.00	
13	-0	-12410	-4213	-3698	0	1272	175015	0.01	0.00	40.00	
14	-0	-12580	-4494	-3611	0	2180	175015	0.01	0.00	40.00	
15	-0	-12310	-4037	-3743	0	726	175015	0.00	0.00	40.00	
16	-0	-12580	-4501	-3612	0	2195	175015	0.01	0.00	40.00	
17	-0	-12320	-4044	-3744	0	741	175015	0.00	0.00	40.00	

CONFRONTO E SINTESI CONCLUSIVE (si assume in ogni caso passo <= 15 cm)

I.R.compr.	Ashy	Ashz	PASSO	Nota
	cmq		cm	
0.01	--	--	15.00	**VERIFICATO**

ASTA NUM. 49 NI 127 NF 126 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 19B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	--												Fx,M	Bielle	V,Mx			
	cm		daN			daN*m				cmq						cmq/m		cm
1	0	-19010	11	-184	0	-316	-61	6.28	6.28	12.57	12.57	3	0.01	0.00	0.02	0.00	0.00	24.0
2	0	-14660	78	-168	0	-279	-253	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
3	0	-14580	77	-86	0	-159	-251	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
4	0	-14670	-61	-198	0	-327	157	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
5	0	-14590	-62	-116	0	-207	160	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
6	0	-14750	31	-274	0	-436	-113	6.28	6.28	12.57	12.57	2	0.02	0.00	0.03	0.00	0.00	24.0
7	0	-14490	27	0	0	-36	-104	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
8	0	-14760	-11	-284	0	-451	10	6.28	6.28	12.57	12.57	2	0.02	0.00	0.03	0.00	0.00	24.0
9	0	-14490	-14	-9	0	-51	19	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
10	0	-14660	78	-168	0	-279	-253	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
11	0	-14580	77	-86	0	-159	-251	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
12	0	-14670	-61	-198	0	-327	157	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
13	0	-14590	-62	-116	0	-207	160	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
14	0	-14750	31	-274	0	-436	-113	6.28	6.28	12.57	12.57	2	0.02	0.00	0.03	0.00	0.00	24.0
15	0	-14490	27	0	0	-36	-104	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
16	0	-14760	-11	-284	0	-451	10	6.28	6.28	12.57	12.57	2	0.02	0.00	0.03	0.00	0.00	24.0
17	0	-14490	-14	-9	0	-51	19	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
18	0	-20790	228	-254	0	-402	-680	6.28	6.28	12.57	12.57	3	0.04	0.00	0.02	0.00	0.00	24.0
19	0	-20870	-205	-384	0	-605	559	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
20	0	-20680	13	-383	0	-637	-66	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
37	0	-19890	372	-170	0	-276	-1093	6.28	6.28	12.57	12.57	3	0.06	0.01	0.03	0.00	0.00	24.0
38	0	-20030	-350	-385	0	-614	973	6.28	6.28	12.57	12.57	3	0.05	0.01	0.03	0.00	0.00	24.0
39	0	-19710	14	-384	0	-668	-69	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	97	-18250	11	-184	0	-137	-50	6.28	6.28	12.57	12.57	3	0.01	0.00	0.02	0.00	0.00	24.0
2	97	-14075	78	-168	0	-116	-177	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
3	97	-13995	77	-86	0	-76	-175	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
4	97	-14085	-61	-198	0	-134	98	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
5	97	-14005	-62	-116	0	-95	99	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
6	97	-14165	31	-274	0	-169	-83	6.28	6.28	12.57	12.57	2	0.01	0.00	0.03	0.00	0.00	24.0
7	97	-13905	27	0	0	-36	-77	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
8	97	-14175	-11	-284	0	-174	-0	6.28	6.28	12.57	12.57	2	0.01	0.00	0.03	0.00	0.00	24.0
9	97	-13905	-14	-9	0	-42	5	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
10	97	-14075	78	-168	0	-116	-177	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
11	97	-13995	77	-86	0	-76	-175	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
12	97	-14085	-61	-198	0	-134	98	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
13	97	-14005	-62	-116	0	-95	99	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
14	97	-14165	31	-274	0	-169	-83	6.28	6.28	12.57	12.57	2	0.01	0.00	0.03	0.00	0.00	24.0
15	97	-13905	27	0	0	-36	-77	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
16	97	-14175	-11	-284	0	-174	-0	6.28	6.28	12.57	12.57	2	0.01	0.00	0.03	0.00	0.00	24.0
17	97	-13905	-14	-9	0	-42	5	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
18	97	-20030	228	-254	0	-154	-458	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
19	97	-20110	-205	-384	0	-231	359	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
20	97	-19920	13	-383	0	-264	-53	6.28	6.28	12.57	12.57	3	0.01	0.01	0.03	0.00	0.00	24.0
37	97	-19130	372	-170	0	-110	-731	6.28	6.28	12.57	12.57	3	0.04	0.01	0.03	0.00	0.00	24.0
38	97	-19268	-350	-385	0	-238	632	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
39	97	-18948	14	-384	0	-293	-55	6.28	6.28	12.57	12.57	3	0.01	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	195	-17490	11	-184	0	43	-40	6.28	6.28	12.57	12.57	3	0.00	0.00	0.02	0.00	0.00	24.0
2	195	-13490	78	-168	0	48	-100	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
3	195	-13410	77	-86	0	7	-100	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
4	195	-13500	-61	-198	0	59	38	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
5	195	-13420	-62	-116	0	18	39	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
6	195	-13580	31	-274	0	99	-53	6.28	6.28	12.57	12.57	2	0.01	0.00	0.03	0.00	0.00	24.0
7	195	-13320	27	0	0	-36	-50	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
8	195	-13590	-11	-284	0	102	-11	6.28	6.28	12.57	12.57	2	0.01	0.00	0.03	0.00	0.00	24.0
9	195	-13320	-14	-9	0	-33	-9	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
10	195	-13490	78	-168	0	48	-100	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
11	195	-13410	77	-86	0	7	-100	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
12	195	-13500	-61	-198	0	59	38	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
13	195	-13420	-62	-116	0	18	39	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
14	195	-13580	31	-274	0	99	-53	6.28	6.28	12.57	12.57	2	0.01	0.00	0.03	0.00	0.00	24.0
15	195	-13320	27	0	0	-36	-50	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
16	195	-13590	-11	-284	0	102	-11	6.28	6.28	12.57	12.57	2	0.01	0.00	0.03	0.00	0.00	24.0
17	195	-13320	-14	-9	0	-33	-9	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
18	195	-19270	228	-254	0	94	-236	6.28	6.28	12.57	12.57	3	0.01	0.00	0.02	0.00	0.00	24.0
19	195	-19350	-205	-384	0	143	159	6.28	6.28	12.57	12.57	3	0.01	0.01	0.03	0.00	0.00	24.0
20	195	-19160	13	-383	0	109	-40	6.28	6.28	12.57	12.57	3	0.00	0.01	0.03	0.00	0.00	24.0
37	195	-18370	372	-170	0	56	-368	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
38	195	-18505	-350	-385	0	137	291	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
39	195	-18185	14	-384	0	81	-41	6.28	6.28	12.57	12.57	3	0.00	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	292	-16730	11	-184	0	223	-30	6.28	6.28	12.57	12.57	3	0.01	0.00	0.02	0.00	0.00	24.0
2	292	-12905	78	-168	0	212	-24	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
3	292	-12825	77	-86	0	91	-24	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
4	292	-12915	-61	-198	0	252	-21	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
5	292	-12835	-62	-116	0	131	-22	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
6	292	-12995	31	-274	0	367	-23	6.28	6.28	12.57	12.57	2	0.02	0.00	0.03	0.00	0.00	24.0
7	292	-12735	27	0	0	-36	-24	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
8	292	-13005	-11	-284	0	379	-22	6.28	6.28	12.57	12.57	2	0.02	0.00	0.03	0.00	0.00	24.0
9	292	-12735	-14	-9	0	-24	-23	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
10	292	-12905	78	-168	0	212	-24	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
11	292	-12825	77	-86	0	91	-24	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
12	292	-12915	-61	-198	0	252	-21	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
13	292	-12835	-62	-116	0	131	-22	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
14	292	-12995	31	-274	0	367	-23	6.28	6.28	12.57	12.57	2	0.02	0.00	0.03	0.00	0.00	24.0
15	292	-12735	27	0	0	-36	-24	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
16	292	-13005	-11	-284	0	379	-22	6.28	6.28	12.57	12.57	2	0.02	0.00	0.03	0.00	0.00	24.0
17	292	-12735	-14	-9	0	-24	-23	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
18	292	-18510	228	-254	0	342	-14	6.28	6.28	12.57	12.57	3	0.01	0.00	0.02	0.00	0.00	24.0
19	292	-18590	-205	-384	0	517	-41	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
20	292	-18400	13	-383	0	483	-27	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
37	292	-17610	372	-170	0	221	-6	6.28	6.28	12.57	12.57	3	0.01	0.01	0.03	0.00	0.00	24.0
38	292	-17742	-350	-385	0	513	-50	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0

39	292	-17422	14	-384	0	456	-27	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	390	-15970	11	-184	0	402	-19	6.28	6.28	12.57	12.57	3	0.01	0.00	0.02	0.00	0.00	24.0
2	390	-12320	78	-168	0	375	53	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
3	390	-12240	77	-86	0	174	51	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
4	390	-12330	-61	-198	0	445	-81	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
5	390	-12250	-62	-116	0	243	-82	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
6	390	-12410	31	-274	0	634	7	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
7	390	-12150	27	0	0	-36	3	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
8	390	-12420	-11	-284	0	655	-33	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
9	390	-12150	-14	-9	0	-16	-37	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
10	390	-12320	78	-168	0	375	53	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
11	390	-12240	77	-86	0	174	51	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
12	390	-12330	-61	-198	0	445	-81	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
13	390	-12250	-62	-116	0	243	-82	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
14	390	-12410	31	-274	0	634	7	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
15	390	-12150	27	0	0	-36	3	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
16	390	-12420	-11	-284	0	655	-33	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
17	390	-12150	-14	-9	0	-16	-37	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
18	390	-17750	228	-254	0	590	208	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
19	390	-17830	-205	-384	0	891	-240	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
20	390	-17640	13	-383	0	856	-14	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
37	390	-16850	372	-170	0	387	356	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
38	390	-16980	-350	-385	0	888	-391	6.28	6.28	12.57	12.57	3	0.04	0.01	0.03	0.00	0.00	24.0
39	390	-16660	14	-384	0	830	-14	6.28	6.28	12.57	12.57	3	0.03	0.01	0.04	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

VERIFICA NODO IN TESTA AL PILASTRO, NODO NUM. 126 NON CONFINATO

(par.7.2.2 NTC2018 "La domanda di resistenza valutata con i criteri della progettazione in capacità può essere assunta non superiore alla domanda di resistenza valutata per il caso di comportamento strutturale non dissipativo.")

PROGETTAZIONE IN CAPACITA'

Asse loc. pilastro y nodo: --

Asse loc. pilastro z nodo INTERNO: As2(inf)= 6.03, As1(sup)= 6.03, Hjw= 40.0 cm, bj= 40.0 cm, hjc= 50.0 cm

FxMin,inf	FxMin,sup	FxMax,sup	FySup	FzSup	Vjbdy	Vjbdz	Vres,y	Vres,z	I.R.compr.	Ashy	Ashz	PASSO	Nota
daN					daN		daN			cmq		cm	
-12150	1	-0	0	0	--	52849	--	175015	0.30	--	13.27	3.28	

VERIFICA DI RESISTENZA CON SOLLECITAZIONI COMPORTAMENTO NON DISSIPATIVO

Asse loc. pilastro z nodo INTERNO: Hjw= 40.0 cm, bj= 40.0 cm, hjc= 50.0 cm, db1= 45.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb,1	Mb,2	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-0	-12320	-4058	-3682	0	928	175015	0.01	0.00	40.00	
3	-0	-12240	-3909	-3735	0	430	175015	0.00	0.00	40.00	
4	-0	-12330	-4108	-3663	0	1099	175015	0.01	0.00	40.00	
5	-0	-12250	-3959	-3716	0	600	175015	0.00	0.00	40.00	
6	-0	-12410	-4249	-3614	0	1568	175015	0.01	0.00	40.00	
7	-0	-12150	-3753	-3789	0	89	175015	0.00	0.00	40.00	
8	-0	-12420	-4264	-3609	0	1617	175015	0.01	0.00	40.00	
9	-0	-12150	-3768	-3784	0	40	175015	0.00	0.00	40.00	
10	-0	-12320	-4058	-3682	0	928	175015	0.01	0.00	40.00	
11	-0	-12240	-3909	-3735	0	430	175015	0.00	0.00	40.00	
12	-0	-12330	-4108	-3663	0	1099	175015	0.01	0.00	40.00	
13	-0	-12250	-3959	-3716	0	600	175015	0.00	0.00	40.00	
14	-0	-12410	-4249	-3614	0	1568	175015	0.01	0.00	40.00	
15	-0	-12150	-3753	-3789	0	89	175015	0.00	0.00	40.00	
16	-0	-12420	-4264	-3609	0	1617	175015	0.01	0.00	40.00	
17	-0	-12150	-3768	-3784	0	40	175015	0.00	0.00	40.00	

CONFRONTO E SINTESI CONCLUSIVE (si assume in ogni caso passo <= 15 cm)

I.R.compr.	Ashy	Ashz	PASSO	Nota
	cmq		cm	
0.01	--	--	15.00	**VERIFICATO**

ASTA NUM. 50 NI 166 NF 167 SEZ. Rp B= 0.400 H= 0.600 (pilastro)
PIL. NUM. 26B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-10450	-502	-6	0	-215	1352	12.57	12.57	6.28	6.28	3	0.05	0.01	0.05	0.00	0.00	24.0
2	0	-8280	-219	-50	0	-256	583	12.57	12.57	6.28	6.28	2	0.04	0.00	0.02	0.00	0.00	24.0
3	0	-8279	-223	44	0	-65	584	12.57	12.57	6.28	6.28	2	0.03	0.00	0.02	0.00	0.00	24.0
4	0	-7803	-550	-53	0	-266	1497	12.57	12.57	6.28	6.28	2	0.09	0.01	0.06	0.00	0.00	24.0
5	0	-7802	-554	40	0	-75	1498	12.57	12.57	6.28	6.28	2	0.08	0.01	0.06	0.00	0.00	24.0
6	0	-8113	-331	-160	0	-482	902	12.57	12.57	6.28	6.28	2	0.06	0.01	0.03	0.00	0.00	24.0
7	0	-8112	-343	152	0	154	904	12.57	12.57	6.28	6.28	2	0.05	0.01	0.04	0.00	0.00	24.0
8	0	-7970	-430	-161	0	-485	1176	12.57	12.57	6.28	6.28	2	0.08	0.01	0.04	0.00	0.00	24.0
9	0	-7969	-442	151	0	151	1178	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
10	0	-8280	-219	-50	0	-256	583	12.57	12.57	6.28	6.28	2	0.04	0.00	0.02	0.00	0.00	24.0
11	0	-8279	-223	44	0	-65	584	12.57	12.57	6.28	6.28	2	0.03	0.00	0.02	0.00	0.00	24.0
12	0	-7803	-550	-53	0	-266	1497	12.57	12.57	6.28	6.28	2	0.09	0.01	0.06	0.00	0.00	24.0
13	0	-7802	-554	40	0	-75	1498	12.57	12.57	6.28	6.28	2	0.08	0.01	0.06	0.00	0.00	24.0
14	0	-8113	-331	-160	0	-482	902	12.57	12.57	6.28	6.28	2	0.06	0.01	0.03	0.00	0.00	24.0
15	0	-8112	-343	152	0	154	904	12.57	12.57	6.28	6.28	2	0.05	0.01	0.04	0.00	0.00	24.0
16	0	-7970	-430	-161	0	-485	1176	12.57	12.57	6.28	6.28	2	0.08	0.01	0.04	0.00	0.00	24.0
17	0	-7969	-442	151	0	151	1178	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
18	0	-12160	-515	-331	0	-847	696	12.57	12.57	6.28	6.28	3	0.05	0.01	0.05	0.00	0.00	24.0
19	0	-10840	-1411	-287	0	-775	3246	12.57	12.57	6.28	6.28	3	0.13	0.02	0.14	0.00	0.00	24.0
20	0	-11390	-910	-70	0	-302	1889	12.57	12.57	6.28	6.28	3	0.07	0.02	0.09	0.00	0.00	24.0

37	0	-12200	-67	-253	0	-686	-355	12.57	12.57	6.28	6.28	3	0.04	0.00	0.02	0.00	0.00	24.0
38	0	-9997	-1559	-180	0	-566	3894	12.57	12.57	6.28	6.28	3	0.15	0.03	0.16	0.00	0.00	24.0
39	0	-10930	-725	182	0	222	1632	12.57	12.57	6.28	6.28	3	0.06	0.01	0.07	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	97	-9690	-502	-6	0	-209	862	12.57	12.57	6.28	6.28	3	0.03	0.01	0.05	0.00	0.00	24.0
2	97	-7695	-219	-50	0	-208	369	12.57	12.57	6.28	6.28	2	0.03	0.00	0.02	0.00	0.00	24.0
3	97	-7694	-223	44	0	-108	366	12.57	12.57	6.28	6.28	2	0.02	0.00	0.02	0.00	0.00	24.0
4	97	-7218	-550	-53	0	-214	961	12.57	12.57	6.28	6.28	2	0.06	0.01	0.06	0.00	0.00	24.0
5	97	-7217	-554	40	0	-115	958	12.57	12.57	6.28	6.28	2	0.05	0.01	0.06	0.00	0.00	24.0
6	97	-7528	-331	-160	0	-326	580	12.57	12.57	6.28	6.28	2	0.04	0.01	0.03	0.00	0.00	24.0
7	97	-7527	-343	152	0	6	570	12.57	12.57	6.28	6.28	2	0.03	0.01	0.04	0.00	0.00	24.0
8	97	-7385	-430	-161	0	-328	757	12.57	12.57	6.28	6.28	2	0.05	0.01	0.04	0.00	0.00	24.0
9	97	-7384	-442	151	0	4	747	12.57	12.57	6.28	6.28	2	0.04	0.01	0.05	0.00	0.00	24.0
10	97	-7695	-219	-50	0	-208	369	12.57	12.57	6.28	6.28	2	0.03	0.00	0.02	0.00	0.00	24.0
11	97	-7694	-223	44	0	-108	366	12.57	12.57	6.28	6.28	2	0.02	0.00	0.02	0.00	0.00	24.0
12	97	-7218	-550	-53	0	-214	961	12.57	12.57	6.28	6.28	2	0.06	0.01	0.06	0.00	0.00	24.0
13	97	-7217	-554	40	0	-115	958	12.57	12.57	6.28	6.28	2	0.05	0.01	0.06	0.00	0.00	24.0
14	97	-7528	-331	-160	0	-326	580	12.57	12.57	6.28	6.28	2	0.04	0.01	0.03	0.00	0.00	24.0
15	97	-7527	-343	152	0	6	570	12.57	12.57	6.28	6.28	2	0.03	0.01	0.04	0.00	0.00	24.0
16	97	-7385	-430	-161	0	-328	757	12.57	12.57	6.28	6.28	2	0.05	0.01	0.04	0.00	0.00	24.0
17	97	-7384	-442	151	0	4	747	12.57	12.57	6.28	6.28	2	0.04	0.01	0.05	0.00	0.00	24.0
18	97	-11400	-515	-331	0	-524	194	12.57	12.57	6.28	6.28	3	0.03	0.01	0.05	0.00	0.00	24.0
19	97	-10078	-1411	-287	0	-495	1871	12.57	12.57	6.28	6.28	3	0.07	0.02	0.14	0.00	0.00	24.0
20	97	-10630	-910	-70	0	-234	1002	12.57	12.57	6.28	6.28	3	0.04	0.02	0.09	0.00	0.00	24.0
37	97	-11440	-67	-253	0	-439	-420	12.57	12.57	6.28	6.28	3	0.03	0.00	0.02	0.00	0.00	24.0
38	97	-9236	-1559	-180	0	-390	2374	12.57	12.57	6.28	6.28	3	0.09	0.03	0.16	0.00	0.00	24.0
39	97	-10168	-725	182	0	45	925	12.57	12.57	6.28	6.28	3	0.03	0.01	0.07	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	195	-8930	-502	-6	0	-204	372	12.57	12.57	6.28	6.28	3	0.02	0.01	0.05	0.00	0.00	24.0
2	195	-7110	-219	-50	0	-159	156	12.57	12.57	6.28	6.28	2	0.01	0.00	0.02	0.00	0.00	24.0
3	195	-7109	-223	44	0	-151	149	12.57	12.57	6.28	6.28	2	0.01	0.00	0.02	0.00	0.00	24.0
4	195	-6633	-550	-53	0	-162	424	12.57	12.57	6.28	6.28	2	0.03	0.01	0.06	0.00	0.00	24.0
5	195	-6632	-554	40	0	-154	418	12.57	12.57	6.28	6.28	2	0.03	0.01	0.06	0.00	0.00	24.0
6	195	-6943	-331	-160	0	-170	257	12.57	12.57	6.28	6.28	2	0.02	0.01	0.03	0.00	0.00	24.0
7	195	-6942	-343	152	0	-142	236	12.57	12.57	6.28	6.28	2	0.02	0.01	0.04	0.00	0.00	24.0
8	195	-6800	-430	-161	0	-171	337	12.57	12.57	6.28	6.28	2	0.02	0.01	0.04	0.00	0.00	24.0
9	195	-6799	-442	151	0	-143	316	12.57	12.57	6.28	6.28	2	0.02	0.01	0.05	0.00	0.00	24.0
10	195	-7110	-219	-50	0	-159	156	12.57	12.57	6.28	6.28	2	0.01	0.00	0.02	0.00	0.00	24.0
11	195	-7109	-223	44	0	-151	149	12.57	12.57	6.28	6.28	2	0.01	0.00	0.02	0.00	0.00	24.0
12	195	-6633	-550	-53	0	-162	424	12.57	12.57	6.28	6.28	2	0.03	0.01	0.06	0.00	0.00	24.0
13	195	-6632	-554	40	0	-154	418	12.57	12.57	6.28	6.28	2	0.03	0.01	0.06	0.00	0.00	24.0
14	195	-6943	-331	-160	0	-170	257	12.57	12.57	6.28	6.28	2	0.02	0.01	0.03	0.00	0.00	24.0
15	195	-6942	-343	152	0	-142	236	12.57	12.57	6.28	6.28	2	0.02	0.01	0.04	0.00	0.00	24.0
16	195	-6800	-430	-161	0	-171	337	12.57	12.57	6.28	6.28	2	0.02	0.01	0.04	0.00	0.00	24.0
17	195	-6799	-442	151	0	-143	316	12.57	12.57	6.28	6.28	2	0.02	0.01	0.05	0.00	0.00	24.0
18	195	-10639	-515	-331	0	-201	-308	12.57	12.57	6.28	6.28	3	0.02	0.01	0.05	0.00	0.00	24.0
19	195	-9317	-1411	-287	0	-215	495	12.57	12.57	6.28	6.28	3	0.02	0.02	0.14	0.00	0.00	24.0
20	195	-9870	-910	-70	0	-166	115	12.57	12.57	6.28	6.28	3	0.01	0.02	0.09	0.00	0.00	24.0
37	195	-10681	-67	-253	0	-192	-486	12.57	12.57	6.28	6.28	3	0.02	0.00	0.02	0.00	0.00	24.0
38	195	-8476	-1559	-180	0	-215	854	12.57	12.57	6.28	6.28	3	0.03	0.03	0.16	0.00	0.00	24.0
39	195	-9407	-725	182	0	-132	219	12.57	12.57	6.28	6.28	3	0.01	0.01	0.07	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	292	-8171	-502	-6	0	-198	-117	12.57	12.57	6.28	6.28	3	0.01	0.01	0.05	0.00	0.00	24.0
2	292	-6525	-219	-50	0	-111	-58	12.57	12.57	6.28	6.28	2	0.01	0.00	0.02	0.00	0.00	24.0
3	292	-6524	-223	44	0	-194	-68	12.57	12.57	6.28	6.28	2	0.01	0.00	0.02	0.00	0.00	24.0
4	292	-6048	-550	-53	0	-110	-112	12.57	12.57	6.28	6.28	2	0.01	0.01	0.06	0.00	0.00	24.0
5	292	-6047	-554	40	0	-193	-122	12.57	12.57	6.28	6.28	2	0.02	0.01	0.06	0.00	0.00	24.0
6	292	-6358	-331	-160	0	-14	-66	12.57	12.57	6.28	6.28	2	0.00	0.01	0.03	0.00	0.00	24.0
7	292	-6357	-343	152	0	-291	-99	12.57	12.57	6.28	6.28	2	0.02	0.01	0.04	0.00	0.00	24.0
8	292	-6215	-430	-161	0	-13	-82	12.57	12.57	6.28	6.28	2	0.00	0.01	0.05	0.00	0.00	24.0
9	292	-6214	-442	151	0	-290	-115	12.57	12.57	6.28	6.28	2	0.02	0.01	0.05	0.00	0.00	24.0
10	292	-6525	-219	-50	0	-111	-58	12.57	12.57	6.28	6.28	2	0.01	0.00	0.02	0.00	0.00	24.0
11	292	-6524	-223	44	0	-194	-68	12.57	12.57	6.28	6.28	2	0.01	0.00	0.02	0.00	0.00	24.0
12	292	-6048	-550	-53	0	-110	-112	12.57	12.57	6.28	6.28	2	0.01	0.01	0.06	0.00	0.00	24.0
13	292	-6047	-554	40	0	-193	-122	12.57	12.57	6.28	6.28	2	0.02	0.01	0.06	0.00	0.00	24.0
14	292	-6358	-331	-160	0	-14	-66	12.57	12.57	6.28	6.28	2	0.00	0.01	0.03	0.00	0.00	24.0
15	292	-6357	-343	152	0	-291	-99	12.57	12.57	6.28	6.28	2	0.02	0.01	0.04	0.00	0.00	24.0
16	292	-6215	-430	-161	0	-13	-82	12.57	12.57	6.28	6.28	2	0.00	0.01	0.05	0.00	0.00	24.0
17	292	-6214	-442	151	0	-290	-115	12.57	12.57	6.28	6.28	2	0.02	0.01	0.05	0.00	0.00	24.0
18	292	-9878	-515	-331	0	121	-811	12.57	12.57	6.28	6.28	3	0.03	0.01	0.05	0.00	0.00	24.0
19	292	-8556	-1411	-287	0	64	-880	12.57	12.57	6.28	6.28	3	0.03	0.02	0.14	0.00	0.00	24.0
20	292	-9111	-910	-70	0	-97	-773	12.57	12.57	6.28	6.28	3	0.03	0.02	0.09	0.00	0.00	24.0
37	292	-9922	-67	-253	0	55	-551	12.57	12.57	6.28	6.28	3	0.02	0.00	0.02	0.00	0.00	24.0
38	292	-7716	-1559	-180	0	-40	-667	12.57	12.57	6.28	6.28	3	0.02	0.03	0.16	0.00	0.00	24.0
39	292	-8646	-725	182	0	-309	-488	12.57	12.57	6.28	6.28	3	0.02	0.01	0.07	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	390	-7411	-502	-6	0	-192	-607	12.57	12.57	6.28	6.28	3	0.03	0.01	0.05	0.00	0.00	24.0
2	390	-5940	-219	-50	0	-63	-272	12.57	12.57	6.28	6.28	2	0.02	0.00	0.02	0.00	0.00	24.0
3	390	-5939	-223	44	0	-237	-285	12.57	12.57	6.28	6.28	2	0.02	0.00	0.02	0.00	0.00	24.0
4	390	-5463	-550	-53	0	-58	-649	12.57	12.57	6.28	6.28	2	0.04	0.01	0.06	0.00	0.00	24.0
5	390	-5462	-554	40	0	-232	-662	12.57	12.57	6.28	6.28	2	0.04	0.01	0.06	0.00	0.00	24.0
6	390	-5773	-331	-160	0	143	-388	12.57	12.57	6.28	6.28	2	0.03	0.01	0.03	0.00	0.00	24.0
7	390	-5772	-343	152	0	-439	-433	12.57	12.57	6.28	6.28	2	0.04	0.01	0.04	0.00	0.00	24.0
8	390	-5630	-430	-161	0	144	-501	12.57	12.57	6.28	6.28	2	0.03	0.01	0.05	0.00	0.00	24.0
9	390	-5629	-442	151	0	-438	-546	12.57	12.57	6.28	6.28	2	0.05	0.01	0.05	0.00	0.00	24.0
10	390	-5940	-219	-50	0	-63	-272	12.57	12.57	6.28	6.28	2	0.02	0.00	0.02	0.00	0.00	24.0
11	390	-5939	-223	44	0	-237	-285	12.57	12.57	6.28	6.28	2	0.02	0.00	0.02	0.00	0.00	24.0
12	390	-5463	-550	-53	0	-58	-649	12.57	12.57	6.28	6.28	2	0.04	0.01	0.06	0.00	0.00	24.0
13	390	-5462	-554	40	0	-232	-662	12.57	12.57	6.28	6.28	2	0.04	0.01	0.06	0.00	0.00	24.0
14	390	-5773	-331	-160	0	143	-388	12.57	12.57	6.28	6.28	2	0.03	0.01	0.03	0.00	0.00	24.0
15	390	-5772	-343	152	0	-439	-433	12.57	12.57	6.28	6.28	2	0.04	0.01	0.04	0.00	0.00	24.0
16	390	-5630	-430	-161	0	144	-501	12.57	12.57	6.28	6.28	2	0.03	0.01	0.05	0.00	0.00	24.0
17	390	-5629	-442	151	0	-438	-546	12.57	12.57	6.28	6.28	2	0.05	0.01	0.05	0.00	0.00	24.0
18	390	-9118	-515	-331	0	444	-1313	12.57	12.57	6.28	6.28	3	0.05	0.01	0.05	0.00	0.00	24.0
19	390	-7794	-1411	-287	0	344	-2255	12.57	12.57	6.28	6.28	3	0.09	0.02	0.14	0.00	0.00	24.0
20	390	-8351	-910	-70	0	-29	-1660	12.57	12.57	6.28	6.28	3	0.06	0.02	0.09	0.00	0.00	24.0
37	390	-9162	-67	-253	0	302	-616	12.57	12.57	6.28	6.28	3	0.03	0.00	0.02	0.00	0.00	24.0
38	390	-6955	-1559	-180	0	136	-2187	12.57	12.57	6.28	6.28	3	0.08	0.03	0.16	0.00	0.00	24.0
39	390	-7884	-725	182	0	-487	-1195	12.57	12.57	6.28	6.28	3	0.05	0.01	0.07	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

VERIFICA NODO IN TESTA AL PILASTRO, NODO NUM. 167 NON CONFINATO
(par.7.2.2 NTC2018 "La domanda di resistenza valutata con i criteri della progettazione in capacità può essere assunta non superiore alla domanda di resistenza valutata per il caso di comportamento strutturale non dissipativo.")

PROGETTAZIONE IN CAPACITA'
Asse loc. pilastro y nodo ESTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 40.0 cm, hjc= 50.0 cm
Asse loc. pilastro z nodo ESTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 50.0 cm, hjc= 30.0 cm

FxMin,inf	FxMin,sup	FxMax,sup	FySup	FzSup	Vjbdy	Vjbdz	Vres,y	Vres,z	I.R.compr.	Ashy	Ashz	PASSO	Nota
daN					daN		daN			cmq		cm	
-5462	-1499	-1990	1402	99	16214	17517	139180	104385	0.17	--	--	40.00	

VERIFICA DI RESISTENZA CON SOLLECITAZIONI COMPORTAMENTO NON DISSIPATIVO

Asse loc. pilastro y nodo ESTERNO: Hjw= 40.0 cm, bj= 40.0 cm, hjc= 50.0 cm, db1= 45.0 cm

NC	Fx,sup	Fx,inf	Mb	Vb	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-1857	-5940	-1717	1304	2062	2178	139236	0.02	0.00	40.00	
3	-1718	-5939	-1729	1307	2087	2182	139294	0.02	0.00	40.00	
4	-1772	-5463	-665	960	1402	240	139272	0.00	0.00	40.00	
5	-1632	-5462	-677	964	1428	244	139330	0.00	0.00	40.00	
6	-1990	-5773	-1335	1179	1801	1495	139180	0.01	0.00	40.00	
7	-1524	-5772	-1375	1191	1886	1509	139375	0.01	0.00	40.00	
8	-1965	-5630	-1019	1076	1603	913	139191	0.01	0.00	40.00	
9	-1499	-5629	-1060	1088	1688	929	139386	0.01	0.00	40.00	
10	-1857	-5940	-1717	1304	2062	2178	139236	0.02	0.00	40.00	
11	-1718	-5939	-1729	1307	2087	2182	139294	0.02	0.00	40.00	
12	-1772	-5463	-665	960	1402	240	139272	0.00	0.00	40.00	
13	-1632	-5462	-677	964	1428	244	139330	0.00	0.00	40.00	
14	-1990	-5773	-1335	1179	1801	1495	139180	0.01	0.00	40.00	
15	-1524	-5772	-1375	1191	1886	1509	139375	0.01	0.00	40.00	
16	-1965	-5630	-1019	1076	1603	913	139191	0.01	0.00	40.00	
17	-1499	-5629	-1060	1088	1688	929	139386	0.01	0.00	40.00	

Asse loc. pilastro z nodo ESTERNO: Hjw= 40.0 cm, bj= 50.0 cm, hjc= 30.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb	Vb	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-1857	-5940	-1021	2779	759	1762	104427	0.02	0.00	40.00	
3	-1718	-5939	-1213	2915	380	2615	104471	0.03	0.00	40.00	
4	-1772	-5463	-947	2731	652	1685	104454	0.02	0.00	40.00	
5	-1632	-5462	-1138	2867	274	2536	104498	0.02	0.00	40.00	
6	-1990	-5773	-771	2603	1164	740	104385	0.01	0.00	40.00	
7	-1524	-5772	-1411	3057	99	3385	104532	0.03	0.00	40.00	
8	-1965	-5630	-749	2589	1132	717	104393	0.01	0.00	40.00	
9	-1499	-5629	-1388	3042	131	3296	104539	0.03	0.00	40.00	
10	-1857	-5940	-1021	2779	759	1762	104427	0.02	0.00	40.00	
11	-1718	-5939	-1213	2915	380	2615	104471	0.03	0.00	40.00	
12	-1772	-5463	-947	2731	652	1685	104454	0.02	0.00	40.00	
13	-1632	-5462	-1138	2867	274	2536	104498	0.02	0.00	40.00	
14	-1990	-5773	-771	2603	1164	740	104385	0.01	0.00	40.00	
15	-1524	-5772	-1411	3057	99	3385	104532	0.03	0.00	40.00	
16	-1965	-5630	-749	2589	1132	717	104393	0.01	0.00	40.00	
17	-1499	-5629	-1388	3042	131	3296	104539	0.03	0.00	40.00	

CONFRONTO E SINTESI CONCLUSIVE (si assume in ogni caso passo <= 15 cm)

I.R.compr.	Ashy	Ashz	PASSO	Nota
	cmq		cm	
0.03	--	--	15.00	**VERIFICATO**

ASTA NUM. 51 NI 168 NF 169 SEZ. Rp B= 0.400 H= 0.600 (pilastro)
PIL. NUM. 11B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-7652	488	440	0	393	-1659	12.57	12.57	6.28	6.28	3	0.07	0.01	0.05	0.00	0.00	24.0
2	0	-5694	642	337	0	307	-1876	12.57	12.57	6.28	6.28	2	0.11	0.01	0.07	0.00	0.00	24.0
3	0	-5798	645	370	0	348	-1885	12.57	12.57	6.28	6.28	2	0.11	0.01	0.07	0.00	0.00	24.0
4	0	-5973	106	307	0	256	-668	12.57	12.57	6.28	6.28	2	0.04	0.01	0.03	0.00	0.00	24.0
5	0	-6078	110	340	0	298	-677	12.57	12.57	6.28	6.28	2	0.05	0.01	0.03	0.00	0.00	24.0
6	0	-5669	450	288	0	241	-1442	12.57	12.57	6.28	6.28	2	0.08	0.01	0.05	0.00	0.00	24.0
7	0	-6018	462	398	0	378	-1473	12.57	12.57	6.28	6.28	2	0.09	0.01	0.05	0.00	0.00	24.0
8	0	-5753	289	279	0	226	-1080	12.57	12.57	6.28	6.28	2	0.06	0.01	0.03	0.00	0.00	24.0
9	0	-6102	302	389	0	363	-1110	12.57	12.57	6.28	6.28	2	0.07	0.01	0.03	0.00	0.00	24.0
10	0	-5694	642	337	0	307	-1876	12.57	12.57	6.28	6.28	2	0.11	0.01	0.07	0.00	0.00	24.0
11	0	-5798	645	370	0	348	-1885	12.57	12.57	6.28	6.28	2	0.11	0.01	0.07	0.00	0.00	24.0
12	0	-5973	106	307	0	256	-668	12.57	12.57	6.28	6.28	2	0.04	0.01	0.03	0.00	0.00	24.0
13	0	-6078	110	340	0	298	-677	12.57	12.57	6.28	6.28	2	0.05	0.01	0.03	0.00	0.00	24.0
14	0	-5669	450	288	0	241	-1442	12.57	12.57	6.28	6.28	2	0.08	0.01	0.05	0.00	0.00	24.0
15	0	-6018	462	398	0	378	-1473	12.57	12.57	6.28	6.28	2	0.09	0.01	0.05	0.00	0.00	24.0
16	0	-5753	289	279	0	226	-1080	12.57	12.57	6.28	6.28	2	0.06	0.01	0.03	0.00	0.00	24.0
17	0	-6102	302	389	0	363	-1110	12.57	12.57	6.28	6.28	2	0.07	0.01	0.03	0.00	0.00	24.0
18	0	-7109	1768	502	0	509	-4493	12.57	12.57	6.28	6.28	3	0.17	0.03	0.18	0.00	0.00	24.0
19	0	-8122	-2	427	0	363	-514	12.57	12.57	6.28	6.28	3	0.03	0.01	0.04	0.00	0.00	24.0
20	0	-7644	830	419	0	344	-2387	12.57	12.57	6.28	6.28	3	0.09	0.01	0.09	0.00	0.00	24.0
37	0	-6735	2229	516	0	542	-5542	12.57	12.57	6.28	6.28	3	0.21	0.04	0.23	0.00	0.00	24.0
38	0	-8423	-721	390	0	300	1088	12.57	12.57	6.28	6.28	3	0.04	0.01	0.07	0.00	0.00	24.0
39	0	-7626	665	378	0	267	-2034	12.57	12.57	6.28	6.28	3	0.08	0.01	0.07	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	97	-6892	488	440	0	-36	-1183	12.57	12.57	6.28	6.28	3	0.04	0.01	0.05	0.00	0.00	24.0
2	97	-5109	642	337	0	-22	-1251	12.57	12.57	6.28	6.28	2	0.07	0.01	0.07	0.00	0.00	24.0
3	97	-5213	645	370	0	-13	-1256	12.57	12.57	6.28	6.28	2	0.07	0.01	0.07	0.00	0.00	24.0
4	97	-5388	106	307	0	-43	-564	12.57	12.57	6.28	6.28	2	0.03	0.01	0.03	0.00	0.00	24.0
5	97	-5493	110	340	0	-34	-569	12.57	12.57	6.28	6.28	2	0.03	0.01	0.03	0.00	0.00	24.0
6	97	-5084	450	288	0	-39	-1003	12.57	12.57	6.28	6.28	2	0.05	0.01	0.05	0.00	0.00	24.0
7	97	-5433	462	398	0	-10	-1022	12.57	12.57	6.28	6.28	2	0.05	0.01	0.05	0.00	0.00	24.0
8	97	-5168	289	279	0	-46	-798	12.57	12.57	6.28	6.28	2	0.04	0.01	0.03	0.00	0.00	24.0
9	97	-5517	302	389	0	-16	-816	12.57	12.57	6.28	6.28	2	0.04	0.01	0.03	0.00	0.00	24.0
10	97	-5109	642	337	0	-22	-1251	12.57	12.57	6.28	6.28	2	0.07	0.01	0.07	0.00	0.00	24.0
11	97	-5213	645	370	0	-13	-1256	12.57	12.57	6.28	6.28	2	0.07	0.01	0.07	0.00	0.00	24.0
12	97	-5388	106	307	0	-43	-564	12.57	12.57	6.28	6.28	2	0.03	0.01	0.03	0.00	0.00	24.0
13	97	-5493	110	340	0	-34	-569	12.57	12.57	6.28	6.28	2	0.03	0.01	0.03	0.00	0.00	24.0
14	97	-5084	450	288	0	-39	-1003	12.57	12.57	6.28	6.28	2	0.05	0.01	0.05	0.00	0.00	24.0
15	97	-5433	462	398	0	-10	-1022	12.57	12.57	6.28	6.28	2	0.05	0.01	0.05	0.00	0.00	24.0
16	97	-5168	289	279	0	-46	-798	12.57	12.57	6.28	6.28	2	0.04	0.01	0.03	0.00	0.00	24.0
17	97	-5517	302	389	0	-16	-816	12.57	12.57	6.28	6.28	2	0.04	0.01	0.03	0.00	0.00	24.0
18	97	-6348	1768	502	0	19	-2769	12.57	12.57	6.28	6.28	3	0.10	0.03	0.19	0.00	0.00	24.0
19	97	-7362	-2	427	0	-53	-516	12.57	12.57	6.28	6.28	3	0.02	0.01	0.04	0.00	0.00	24.0
20	97	-6884	830	419	0	-64	-1578	12.57	12.57	6.28	6.28	3	0.06	0.01	0.09	0.00	0.00	24.0
37	97	-5974	2229	516	0	39	-3369	12.57	12.57	6.28	6.28	3	0.13	0.04	0.23	0.00	0.00	24.0
38	97	-7662	-721	390	0	-81	386	12.57	12.57	6.28	6.28	3	0.02	0.01	0.07	0.00	0.00	24.0
39	97	-6866	665	378	0	-101	-1385	12.57	12.57	6.28	6.28	3	0.05	0.01	0.07	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	195	-6131	488	440	0	-465	-706	12.57	12.57	6.28	6.28	3	0.04	0.01	0.05	0.00	0.00	24.0
2	195	-4524	642	337	0	-350	-625	12.57	12.57	6.28	6.28	2	0.05	0.01	0.07	0.00	0.00	24.0
3	195	-4628	645	370	0	-374	-627	12.57	12.57	6.28	6.28	2	0.05	0.01	0.07	0.00	0.00	24.0
4	195	-4803	106	307	0	-342	-460	12.57	12.57	6.28	6.28	2	0.04	0.01	0.03	0.00	0.00	24.0
5	195	-4908	110	340	0	-366	-462	12.57	12.57	6.28	6.28	2	0.04	0.01	0.03	0.00	0.00	24.0
6	195	-4499	450	288	0	-320	-565	12.57	12.57	6.28	6.28	2	0.04	0.01	0.05	0.00	0.00	24.0
7	195	-4848	462	398	0	-398	-572	12.57	12.57	6.28	6.28	2	0.05	0.01	0.05	0.00	0.00	24.0
8	195	-4583	289	279	0	-318	-516	12.57	12.57	6.28	6.28	2	0.04	0.01	0.03	0.00	0.00	24.0
9	195	-4932	302	389	0	-396	-522	12.57	12.57	6.28	6.28	2	0.04	0.01	0.03	0.00	0.00	24.0
10	195	-4524	642	337	0	-350	-625	12.57	12.57	6.28	6.28	2	0.05	0.01	0.07	0.00	0.00	24.0
11	195	-4628	645	370	0	-374	-627	12.57	12.57	6.28	6.28	2	0.05	0.01	0.07	0.00	0.00	24.0
12	195	-4803	106	307	0	-342	-460	12.57	12.57	6.28	6.28	2	0.04	0.01	0.03	0.00	0.00	24.0
13	195	-4908	110	340	0	-366	-462	12.57	12.57	6.28	6.28	2	0.04	0.01	0.03	0.00	0.00	24.0
14	195	-4499	450	288	0	-320	-565	12.57	12.57	6.28	6.28	2	0.04	0.01	0.05	0.00	0.00	24.0
15	195	-4848	462	398	0	-398	-572	12.57	12.57	6.28	6.28	2	0.05	0.01	0.05	0.00	0.00	24.0
16	195	-4583	289	279	0	-318	-516	12.57	12.57	6.28	6.28	2	0.04	0.01	0.03	0.00	0.00	24.0
17	195	-4932	302	389	0	-396	-522	12.57	12.57	6.28	6.28	2	0.04	0.01	0.03	0.00	0.00	24.0
18	195	-5588	1768	502	0	-470	-1045	12.57	12.57	6.28	6.28	3	0.05	0.03	0.19	0.00	0.00	24.0
19	195	-6601	-2	427	0	-469	-518	12.57	12.57	6.28	6.28	3	0.03	0.01	0.04	0.00	0.00	24.0
20	195	-6123	830	419	0	-473	-769	12.57	12.57	6.28	6.28	3	0.04	0.01	0.09	0.00	0.00	24.0
37	195	-5214	2229	516	0	-465	-1195	12.57	12.57	6.28	6.28	3	0.05	0.04	0.24	0.00	0.00	24.0
38	195	-6902	-721	390	0	-462	-317	12.57	12.57	6.28	6.28	3	0.03	0.01	0.07	0.00	0.00	24.0
39	195	-6105	665	378	0	-469	-736	12.57	12.57	6.28	6.28	3	0.04	0.01	0.07	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	292	-5370	488	440	0	-894	-230	12.57	12.57	6.28	6.28	3	0.05	0.01	0.05	0.00	0.00	24.0
2	292	-3939	642	337	0	-679	0	12.57	12.57	6.28	6.28	2	0.04	0.01	0.07	0.00	0.00	24.0
3	292	-4043	645	370	0	-734	2	12.57	12.57	6.28	6.28	2	0.05	0.01	0.07	0.00	0.00	24.0
4	292	-4218	106	307	0	-642	-357	12.57	12.57	6.28	6.28	2	0.05	0.01	0.03	0.00	0.00	24.0
5	292	-4323	110	340	0	-697	-355	12.57	12.57	6.28	6.28	2	0.05	0.01	0.03	0.00	0.00	24.0
6	292	-3914	450	288	0	-601	-126	12.57	12.57	6.28	6.28	2	0.04	0.01	0.05	0.00	0.00	24.0
7	292	-4263	462	398	0	-786	-121	12.57	12.57	6.28	6.28	2	0.05	0.01	0.05	0.00	0.00	24.0
8	292	-3998	289	279	0	-590	-234	12.57	12.57	6.28	6.28	2	0.04	0.01	0.03	0.00	0.00	24.0
9	292	-4347	302	389	0	-775	-228	12.57	12.57	6.28	6.28	2	0.05	0.01	0.04	0.00	0.00	24.0
10	292	-3939	642	337	0	-679	0	12.57	12.57	6.28	6.28	2	0.04	0.01	0.07	0.00	0.00	24.0
11	292	-4043	645	370	0	-734	2	12.57	12.57	6.28	6.28	2	0.05	0.01	0.07	0.00	0.00	24.0
12	292	-4218	106	307	0	-642	-357	12.57	12.57	6.28	6.28	2	0.05	0.01	0.03	0.00	0.00	24.0
13	292	-4323	110	340	0	-697	-355	12.57	12.57	6.28	6.28	2	0.05	0.01	0.03	0.00	0.00	24.0
14	292	-3914	450	288	0	-601	-126	12.57	12.57	6.28	6.28	2	0.04	0.01	0.05	0.00	0.00	24.0
15	292	-4263	462	398	0	-786	-121	12.57	12.57	6.28	6.28	2	0.05	0.01	0.05	0.00	0.00	24.0
16	292	-3998	289	279	0	-590	-234	12.57	12.57	6.28	6.28	2	0.04	0.01	0.03	0.00	0.00	24.0
17	292	-4347	302	389	0	-775	-228	12.57	12.57	6.28	6.28	2	0.05	0.01	0.04	0.00	0.00	24.0
18	292	-4828	1768	502	0	-960	679	12.57	12.57	6.28	6.28	3	0.06	0.03	0.19	0.00	0.00	24.0
19	292	-5840	-2	427	0	-885	-520	12.57	12.57	6.28	6.28	3	0.05	0.01	0.04	0.00	0.00	24.0
20	292	-5362	830	419	0	-882	40	12.57	12.57	6.28	6.28	3	0.05	0.01	0.09	0.00	0.00	24.0
37	292	-4454	2229	516	0	-968	978	12.57	12.57	6.28	6.28	3	0.06	0.04	0.24	0.00	0.00	24.0
38	292	-6142	-721	390	0	-842	-1019	12.57	12.57	6.28	6.28	3	0.06	0.01	0.08	0.00	0.00	24.0
39	292	-5344	665	378	0	-838	-88	12.57	12.57	6.28	6.28	3	0.05	0.01	0.07	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	390	-4610	488	440	0	-1323	246	12.57	12.57	6.28	6.28	3	0.08	0.01	0.05	0.00	0.00	24.0
2	390	-3354	642	337	0	-1007	626	12.57	12.57	6.28	6.28	2	0.08	0.01	0.07	0.00	0.00	24.0
3	390	-3458	645	370	0	-1095	631	12.57	12.57	6.28	6.28	2	0.09	0.01	0.07	0.00	0.00	24.0
4	390	-3633	106	307	0	-941	-253	12.57	12.57	6.28	6.28	2	0.07	0.01	0.03	0.00	0.00	24.0
5	390	-3738	110	340	0	-1029	-248	12.57	12.57	6.28	6.28	2	0.07	0.01	0.03	0.00	0.00	24.0
6	390	-3329	450	288	0	-881	312	12.57	12.57	6.28	6.28	2	0.06	0.01	0.05	0.00	0.00	24.0
7	390	-3678	462	398	0	-1174	330	12.57	12.57	6.28	6.28	2	0.08	0.01	0.05	0.00	0.00	24.0
8	390	-3413	289	279	0	-862	48	12.57	12.57	6.28	6.28	2	0.06	0.01	0.03	0.00	0.00	24.0
9	390	-3762	302	389	0	-1155	66	12.57	12.57	6.28	6.28	2	0.07	0.01	0.04	0.00	0.00	24.0
10	390	-3354	642	337	0	-1007	626	12.57	12.57	6.28	6.28	2	0.08	0.01	0.07	0.00	0.00	24.0
11	390	-3458	645	370	0	-1095	631	12.57	12.57	6.28	6.28	2	0.09	0.01	0.07	0.00	0.00	24.0
12	390	-3633	106	307	0	-941	-253	12.57	12.57	6.28	6.28	2	0.07	0.01	0.03	0.00	0.00	24.0
13	390	-3738	110	340	0	-1029	-248	12.57	12.57	6.28	6.28	2	0.07	0.01	0.03	0.00	0.00	24.0
14	390	-3329	450	288	0	-881	312	12.57	12.57	6.28	6.28	2	0.06	0.01	0.05	0.00	0.00	24.0
15	390	-3678	462	398	0	-1174	330	12.57	12.57	6.28	6.28	2	0.08	0.01	0.05	0.00	0.00	24.0
16	390	-3413	289	279	0	-862	48	12.57	12.57	6.28	6.28	2	0.06	0.01	0.03	0.00	0.00	24.0
17	390	-3762	302	389	0	-1155	66	12.57	12.57	6.28	6.28	2	0.07	0.01	0.04	0.00	0.00	24.0
18	390	-4067	1768	502	0	-1449	2403	12.57	12.57	6.28	6.28	3	0.12	0.03	0.19	0.00	0.00	24.0
19	390	-5080	-2	427	0	-1301	-521	12.57	12.57	6.28	6.28	3	0.08	0.01	0.04	0.00	0.00	24.0
20	390	-4602	830	419	0	-1290	849	12.57	12.57	6.28	6.28	3	0.08	0.01	0.09	0.00	0.00	24.0
37	390	-3693	2229	516	0	-1471	3152	12.57	12.57	6.28	6.28	3	0.14	0.04	0.24	0.00	0.00	24.0
38	390	-5381	-721	390	0	-1223	-1722	12.57	12.57	6.28	6.28	3	0.09	0.01	0.08	0.00	0.00	24.0
39	390	-4584	665	378	0	-1206	561	12.57	12.57	6.28	6.28	3	0.07	0.01	0.07	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

VERIFICA NODO IN TESTA AL PILASTRO, NODO NUM. 169 NON CONFINATO

(par.7.2.2 NTC2018 "La domanda di resistenza valutata con i criteri della progettazione in capacità può essere assunta non superiore alla domanda di resistenza valutata per il caso di comportamento strutturale non dissipativo.")

PROGETTAZIONE IN CAPACITA'

Asse loc. pilastro y nodo ESTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 40.0 cm, hjc= 50.0 cm

Asse loc. pilastro z nodo ESTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 50.0 cm, hjc= 30.0 cm

FxMin,inf	FxMin,sup	FxMax,sup	FySup	FzSup	Vjbdy	Vjbdz	Vres,y	Vres,z	I.R.compr.	Ashy	Ashz	PASSO	Nota
daN					daN		daN			cmq		cm	
-3329	1	-0	0	0	17616	17616	140012	105009	0.17	--	--	40.00	

VERIFICA DI RESISTENZA CON SOLLECITAZIONI COMPORTAMENTO NON DISSIPATIVO

Asse loc. pilastro y nodo ESTERNO: Hjw= 40.0 cm, bj= 40.0 cm, hjc= 50.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb	Vb	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m			daN			cmq	cm	
2	-0	-3354	850	571	0	2099	140012	0.01	0.00	40.00	
3	-0	-3458	854	569	0	2108	140012	0.02	0.00	40.00	
4	-0	-3633	-421	900	0	1040	140012	0.01	0.00	40.00	
5	-0	-3738	-417	898	0	1030	140012	0.01	0.00	40.00	
6	-0	-3329	561	687	0	1384	140012	0.01	0.00	40.00	
7	-0	-3678	572	683	0	1412	140012	0.01	0.00	40.00	
8	-0	-3413	-82	786	0	202	140012	0.00	0.00	40.00	
9	-0	-3762	-69	782	0	170	140012	0.00	0.00	40.00	
10	-0	-3354	850	571	0	2099	140012	0.01	0.00	40.00	
11	-0	-3458	854	569	0	2108	140012	0.02	0.00	40.00	
12	-0	-3633	-421	900	0	1040	140012	0.01	0.00	40.00	
13	-0	-3738	-417	898	0	1030	140012	0.01	0.00	40.00	
14	-0	-3329	561	687	0	1384	140012	0.01	0.00	40.00	
15	-0	-3678	572	683	0	1412	140012	0.01	0.00	40.00	
16	-0	-3413	-82	786	0	202	140012	0.00	0.00	40.00	
17	-0	-3762	-69	782	0	170	140012	0.00	0.00	40.00	

Asse loc. pilastro z nodo ESTERNO: Hjw= 40.0 cm, bj= 50.0 cm, hjc= 30.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb	Vb	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m			daN			cmq	cm	
2	-0	-3354	-965	2783	0	2383	105009	0.02	0.00	40.00	
3	-0	-3458	-1053	2889	0	2600	105009	0.02	0.00	40.00	
4	-0	-3633	-894	2734	0	2207	105009	0.02	0.00	40.00	
5	-0	-3738	-981	2840	0	2423	105009	0.02	0.00	40.00	
6	-0	-3329	-838	2642	0	2070	105009	0.02	0.00	40.00	
7	-0	-3678	-1130	2995	0	2790	105009	0.03	0.00	40.00	
8	-0	-3413	-817	2627	0	2017	105009	0.02	0.00	40.00	
9	-0	-3762	-1108	2980	0	2736	105009	0.03	0.00	40.00	
10	-0	-3354	-965	2783	0	2383	105009	0.02	0.00	40.00	
11	-0	-3458	-1053	2889	0	2600	105009	0.02	0.00	40.00	
12	-0	-3633	-894	2734	0	2207	105009	0.02	0.00	40.00	
13	-0	-3738	-981	2840	0	2423	105009	0.02	0.00	40.00	
14	-0	-3329	-838	2642	0	2070	105009	0.02	0.00	40.00	
15	-0	-3678	-1130	2995	0	2790	105009	0.03	0.00	40.00	
16	-0	-3413	-817	2627	0	2017	105009	0.02	0.00	40.00	
17	-0	-3762	-1108	2980	0	2736	105009	0.03	0.00	40.00	

CONFRONTO E SINTESI CONCLUSIVE (si assume in ogni caso passo <= 15 cm)

I.R.compr.	Ashy	Ashz	PASSO	Nota
	cmq		cm	
0.03	--	--	15.00	**VERIFICATO**

ASTA NUM. 52 NI 170 NF 171 SEZ. Rp B= 0.400 H= 0.600 (pilastro)
PIL. NUM. 16B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-11920	820	695	0	680	-1397	12.57	12.57	6.28	6.28	3	0.06	0.01	0.08	0.00	0.00	24.0
2	0	-9106	1020	512	0	496	-1810	12.57	12.57	6.28	6.28	2	0.11	0.02	0.10	0.00	0.00	24.0
3	0	-9229	1021	547	0	538	-1812	12.57	12.57	6.28	6.28	2	0.11	0.02	0.10	0.00	0.00	24.0
4	0	-9105	240	522	0	508	-337	12.57	12.57	6.28	6.28	2	0.04	0.01	0.05	0.00	0.00	24.0
5	0	-9229	242	556	0	550	-339	12.57	12.57	6.28	6.28	2	0.04	0.01	0.05	0.00	0.00	24.0
6	0	-8961	745	476	0	451	-1292	12.57	12.57	6.28	6.28	2	0.08	0.01	0.08	0.00	0.00	24.0
7	0	-9373	750	590	0	592	-1299	12.57	12.57	6.28	6.28	2	0.09	0.01	0.08	0.00	0.00	24.0
8	0	-8961	512	478	0	454	-850	12.57	12.57	6.28	6.28	2	0.06	0.01	0.05	0.00	0.00	24.0
9	0	-9373	516	593	0	596	-857	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
10	0	-9106	1020	512	0	496	-1810	12.57	12.57	6.28	6.28	2	0.11	0.02	0.10	0.00	0.00	24.0
11	0	-9229	1021	547	0	538	-1812	12.57	12.57	6.28	6.28	2	0.11	0.02	0.10	0.00	0.00	24.0
12	0	-9105	240	522	0	508	-337	12.57	12.57	6.28	6.28	2	0.04	0.01	0.05	0.00	0.00	24.0
13	0	-9229	242	556	0	550	-339	12.57	12.57	6.28	6.28	2	0.04	0.01	0.05	0.00	0.00	24.0
14	0	-8961	745	476	0	451	-1292	12.57	12.57	6.28	6.28	2	0.08	0.01	0.08	0.00	0.00	24.0
15	0	-9373	750	590	0	592	-1299	12.57	12.57	6.28	6.28	2	0.09	0.01	0.08	0.00	0.00	24.0
16	0	-8961	512	478	0	454	-850	12.57	12.57	6.28	6.28	2	0.06	0.01	0.05	0.00	0.00	24.0
17	0	-9373	516	593	0	596	-857	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
18	0	-12340	2690	704	0	675	-4863	12.57	12.57	6.28	6.28	3	0.18	0.05	0.26	0.00	0.00	24.0
19	0	-12350	104	729	0	704	-12	12.57	12.57	6.28	6.28	3	0.04	0.01	0.07	0.00	0.00	24.0
20	0	-12270	1319	625	0	532	-2298	12.57	12.57	6.28	6.28	3	0.09	0.02	0.13	0.00	0.00	24.0
37	0	-12090	3363	679	0	654	-6140	12.57	12.57	6.28	6.28	3	0.23	0.06	0.33	0.00	0.00	24.0
38	0	-12120	-946	720	0	702	1944	12.57	12.57	6.28	6.28	3	0.08	0.02	0.09	0.00	0.00	24.0
39	0	-11980	1078	547	0	415	-1865	12.57	12.57	6.28	6.28	3	0.07	0.02	0.10	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	97	-11159	820	695	0	3	-597	12.57	12.57	6.28	6.28	3	0.02	0.01	0.08	0.00	0.00	24.0
2	97	-8521	1020	512	0	-3	-816	12.57	12.57	6.28	6.28	2	0.04	0.02	0.10	0.00	0.00	24.0
3	97	-8644	1021	547	0	5	-816	12.57	12.57	6.28	6.28	2	0.04	0.02	0.10	0.00	0.00	24.0
4	97	-8520	240	522	0	-1	-102	12.57	12.57	6.28	6.28	2	0.01	0.01	0.04	0.00	0.00	24.0
5	97	-8644	242	556	0	8	-103	12.57	12.57	6.28	6.28	2	0.01	0.01	0.05	0.00	0.00	24.0
6	97	-8376	745	476	0	-13	-566	12.57	12.57	6.28	6.28	2	0.03	0.01	0.08	0.00	0.00	24.0

7	97	-8788	750	590	0	16	-568	12.57	12.57	6.28	6.28	2	0.03	0.01	0.08	0.00	0.00	24.0
8	97	-8376	512	478	0	-12	-351	12.57	12.57	6.28	6.28	2	0.02	0.01	0.05	0.00	0.00	24.0
9	97	-8788	516	593	0	17	-354	12.57	12.57	6.28	6.28	2	0.02	0.01	0.05	0.00	0.00	24.0
10	97	-8521	1020	512	0	-3	-816	12.57	12.57	6.28	6.28	2	0.04	0.02	0.10	0.00	0.00	24.0
11	97	-8644	1021	547	0	5	-816	12.57	12.57	6.28	6.28	2	0.04	0.02	0.10	0.00	0.00	24.0
12	97	-8520	240	522	0	-1	-102	12.57	12.57	6.28	6.28	2	0.01	0.01	0.04	0.00	0.00	24.0
13	97	-8644	242	556	0	8	-103	12.57	12.57	6.28	6.28	2	0.01	0.01	0.05	0.00	0.00	24.0
14	97	-8376	745	476	0	-13	-566	12.57	12.57	6.28	6.28	2	0.03	0.01	0.08	0.00	0.00	24.0
15	97	-8788	750	590	0	16	-568	12.57	12.57	6.28	6.28	2	0.03	0.01	0.08	0.00	0.00	24.0
16	97	-8376	512	478	0	-12	-351	12.57	12.57	6.28	6.28	2	0.02	0.01	0.05	0.00	0.00	24.0
17	97	-8788	516	593	0	17	-354	12.57	12.57	6.28	6.28	2	0.02	0.01	0.05	0.00	0.00	24.0
18	97	-11578	2690	704	0	-11	-2241	12.57	12.57	6.28	6.28	3	0.08	0.05	0.26	0.00	0.00	24.0
19	97	-11590	104	729	0	-7	89	12.57	12.57	6.28	6.28	3	0.00	0.01	0.06	0.00	0.00	24.0
20	97	-11509	1319	625	0	-78	-1012	12.57	12.57	6.28	6.28	3	0.04	0.02	0.13	0.00	0.00	24.0
37	97	-11329	3363	679	0	-8	-2861	12.57	12.57	6.28	6.28	3	0.10	0.06	0.33	0.00	0.00	24.0
38	97	-11358	-946	720	0	-1	1022	12.57	12.57	6.28	6.28	3	0.04	0.02	0.09	0.00	0.00	24.0
39	97	-11218	1078	547	0	-119	-814	12.57	12.57	6.28	6.28	3	0.03	0.02	0.11	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	195	-10398	820	695	0	-675	202	12.57	12.57	6.28	6.28	3	0.04	0.01	0.08	0.00	0.00	24.0
2	195	-7936	1020	512	0	-503	178	12.57	12.57	6.28	6.28	2	0.04	0.02	0.10	0.00	0.00	24.0
3	195	-8059	1021	547	0	-528	179	12.57	12.57	6.28	6.28	2	0.04	0.02	0.10	0.00	0.00	24.0
4	195	-7935	240	522	0	-510	132	12.57	12.57	6.28	6.28	2	0.03	0.01	0.05	0.00	0.00	24.0
5	195	-8059	242	556	0	-534	133	12.57	12.57	6.28	6.28	2	0.04	0.01	0.05	0.00	0.00	24.0
6	195	-7791	745	476	0	-477	161	12.57	12.57	6.28	6.28	2	0.03	0.01	0.08	0.00	0.00	24.0
7	195	-8203	750	590	0	-559	164	12.57	12.57	6.28	6.28	2	0.04	0.01	0.08	0.00	0.00	24.0
8	195	-7791	512	478	0	-478	147	12.57	12.57	6.28	6.28	2	0.03	0.01	0.05	0.00	0.00	24.0
9	195	-8203	516	593	0	-561	150	12.57	12.57	6.28	6.28	2	0.04	0.01	0.06	0.00	0.00	24.0
10	195	-7936	1020	512	0	-503	178	12.57	12.57	6.28	6.28	2	0.04	0.02	0.10	0.00	0.00	24.0
11	195	-8059	1021	547	0	-528	179	12.57	12.57	6.28	6.28	2	0.04	0.02	0.10	0.00	0.00	24.0
12	195	-7935	240	522	0	-510	132	12.57	12.57	6.28	6.28	2	0.03	0.01	0.05	0.00	0.00	24.0
13	195	-8059	242	556	0	-534	133	12.57	12.57	6.28	6.28	2	0.04	0.01	0.05	0.00	0.00	24.0
14	195	-7791	745	476	0	-477	161	12.57	12.57	6.28	6.28	2	0.03	0.01	0.08	0.00	0.00	24.0
15	195	-8203	750	590	0	-559	164	12.57	12.57	6.28	6.28	2	0.04	0.01	0.08	0.00	0.00	24.0
16	195	-7791	512	478	0	-478	147	12.57	12.57	6.28	6.28	2	0.03	0.01	0.05	0.00	0.00	24.0
17	195	-8203	516	593	0	-561	150	12.57	12.57	6.28	6.28	2	0.04	0.01	0.06	0.00	0.00	24.0
18	195	-10816	2690	704	0	-698	382	12.57	12.57	6.28	6.28	3	0.04	0.05	0.26	0.00	0.00	24.0
19	195	-10830	104	729	0	-718	191	12.57	12.57	6.28	6.28	3	0.04	0.01	0.07	0.00	0.00	24.0
20	195	-10748	1319	625	0	-687	274	12.57	12.57	6.28	6.28	3	0.04	0.02	0.13	0.00	0.00	24.0
37	195	-10568	3363	679	0	-670	418	12.57	12.57	6.28	6.28	3	0.04	0.06	0.33	0.00	0.00	24.0
38	195	-10597	-946	720	0	-704	99	12.57	12.57	6.28	6.28	3	0.04	0.02	0.09	0.00	0.00	24.0
39	195	-10457	1078	547	0	-652	237	12.57	12.57	6.28	6.28	3	0.04	0.02	0.11	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	292	-9636	820	695	0	-1352	1001	12.57	12.57	6.28	6.28	3	0.08	0.01	0.08	0.00	0.00	24.0
2	292	-7351	1020	512	0	-1002	1173	12.57	12.57	6.28	6.28	2	0.10	0.02	0.11	0.00	0.00	24.0
3	292	-7474	1021	547	0	-1061	1174	12.57	12.57	6.28	6.28	2	0.10	0.02	0.11	0.00	0.00	24.0
4	292	-7350	240	522	0	-1018	366	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
5	292	-7474	242	556	0	-1077	368	12.57	12.57	6.28	6.28	2	0.08	0.01	0.05	0.00	0.00	24.0
6	292	-7206	745	476	0	-940	887	12.57	12.57	6.28	6.28	2	0.09	0.01	0.08	0.00	0.00	24.0
7	292	-7618	750	590	0	-1135	895	12.57	12.57	6.28	6.28	2	0.10	0.01	0.08	0.00	0.00	24.0
8	292	-7206	512	478	0	-945	646	12.57	12.57	6.28	6.28	2	0.08	0.01	0.05	0.00	0.00	24.0
9	292	-7618	516	593	0	-1140	653	12.57	12.57	6.28	6.28	2	0.09	0.01	0.06	0.00	0.00	24.0
10	292	-7351	1020	512	0	-1002	1173	12.57	12.57	6.28	6.28	2	0.10	0.02	0.11	0.00	0.00	24.0
11	292	-7474	1021	547	0	-1061	1174	12.57	12.57	6.28	6.28	2	0.10	0.02	0.11	0.00	0.00	24.0
12	292	-7350	240	522	0	-1018	366	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
13	292	-7474	242	556	0	-1077	368	12.57	12.57	6.28	6.28	2	0.08	0.01	0.05	0.00	0.00	24.0
14	292	-7206	745	476	0	-940	887	12.57	12.57	6.28	6.28	2	0.09	0.01	0.08	0.00	0.00	24.0
15	292	-7618	750	590	0	-1135	895	12.57	12.57	6.28	6.28	2	0.10	0.01	0.08	0.00	0.00	24.0
16	292	-7206	512	478	0	-945	646	12.57	12.57	6.28	6.28	2	0.08	0.01	0.05	0.00	0.00	24.0
17	292	-7618	516	593	0	-1140	653	12.57	12.57	6.28	6.28	2	0.09	0.01	0.06	0.00	0.00	24.0
18	292	-10055	2690	704	0	-1384	3005	12.57	12.57	6.28	6.28	3	0.13	0.05	0.27	0.00	0.00	24.0
19	292	-10070	104	729	0	-1429	292	12.57	12.57	6.28	6.28	3	0.08	0.01	0.07	0.00	0.00	24.0
20	292	-9987	1319	625	0	-1297	1559	12.57	12.57	6.28	6.28	3	0.09	0.02	0.13	0.00	0.00	24.0
37	292	-9808	3363	679	0	-1332	3697	12.57	12.57	6.28	6.28	3	0.15	0.06	0.34	0.00	0.00	24.0
38	292	-9836	-946	720	0	-1406	-823	12.57	12.57	6.28	6.28	3	0.08	0.02	0.09	0.00	0.00	24.0
39	292	-9696	1078	547	0	-1185	1289	12.57	12.57	6.28	6.28	3	0.08	0.02	0.11	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	390	-8875	820	695	0	-2029	1801	12.57	12.57	6.28	6.28	3	0.13	0.01	0.08	0.00	0.00	24.0
2	390	-6766	1020	512	0	-1502	2167	12.57	12.57	6.28	6.28	2	0.17	0.02	0.11	0.00	0.00	24.0
3	390	-6889	1021	547	0	-1594	2170	12.57	12.57	6.28	6.28	2	0.18	0.02	0.11	0.00	0.00	24.0
4	390	-6765	240	522	0	-1527	601	12.57	12.57	6.28	6.28	2	0.11	0.01	0.05	0.00	0.00	24.0
5	390	-6889	242	556	0	-1619	604	12.57	12.57	6.28	6.28	2	0.12	0.01	0.05	0.00	0.00	24.0
6	390	-6621	745	476	0	-1404	1614	12.57	12.57	6.28	6.28	2	0.14	0.01	0.08	0.00	0.00	24.0
7	390	-7033	750	590	0	-1710	1626	12.57	12.57	6.28	6.28	2	0.16	0.01	0.08	0.00	0.00	24.0
8	390	-6621	512	478	0	-1411	1145	12.57	12.57	6.28	6.28	2	0.12	0.01	0.05	0.00	0.00	24.0
9	390	-7033	516	593	0	-1718	1156	12.57	12.57	6.28	6.28	2	0.14	0.01	0.06	0.00	0.00	24.0
10	390	-6766	1020	512	0	-1502	2167	12.57	12.57	6.28	6.28	2	0.17	0.02	0.11	0.00	0.00	24.0
11	390	-6889	1021	547	0	-1594	2170	12.57	12.57	6.28	6.28	2	0.18	0.02	0.11	0.00	0.00	24.0
12	390	-6765	240	522	0	-1527	601	12.57	12.57	6.28	6.28	2	0.11	0.01	0.05	0.00	0.00	24.0
13	390	-6889	242	556	0	-1619	604	12.57	12.57	6.28	6.28	2	0.12	0.01	0.05	0.00	0.00	24.0
14	390	-6621	745	476	0	-1404	1614	12.57	12.57	6.28	6.28	2	0.14	0.01	0.08	0.00	0.00	24.0
15	390	-7033	750	590	0	-1710	1626	12.57	12.57	6.28	6.28	2	0.16	0.01	0.08	0.00	0.00	24.0
16	390	-6621	512	478	0	-1411	1145	12.57	12.57	6.28	6.28	2	0.12	0.01	0.05	0.00	0.00	24.0
17	390	-7033	516	593	0	-1718	1156	12.57	12.57	6.28	6.28	2	0.14	0.01	0.06	0.00	0.00	24.0
18	390	-9293	2690	704	0	-2071	5627	12.57	12.57	6.28	6.28	3	0.24	0.05	0.27	0.00	0.00	24.0
19	390	-9310	104	729	0	-2140	394	12.57	12.57	6.28	6.28	3	0.12	0.01	0.07	0.00	0.00	24.0
20	390	-9226	1319	625	0	-1906	2845	12.57	12.57	6.28	6.28	3	0.14	0.02	0.13	0.00	0.00	24.0
37	390	-9047	3363	679	0	-1994	6976	12.57	12.57	6.28	6.28	3	0.28	0.06	0.34	0.00	0.00	24.0
38	390	-9074	-946	720	0	-2109	-1746	12.57	12.57	6.28	6.28	3	0.13	0.02	0.10	0.00	0.00	24.0
39	390	-8934	1078	547	0	-1718	2340	12.57	12.57	6.28	6.28	3	0.12	0.02	0.11	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

VERIFICA NODO IN TESTA AL PILASTRO, NODO NUM. 171 NON CONFINATO

(par.7.2.2 NTC2018 "La domanda di resistenza valutata con i criteri della progettazione in capacità può essere assunta non superiore alla domanda di resistenza valutata per il caso di comportamento strutturale non dissipativo.")

PROGETTAZIONE IN CAPACITA'

Asse loc. pilastro y nodo INTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 40.0 cm, hjc= 50.0 cm
Asse loc. pilastro z nodo ESTERNO: As2(inf)= 6.03, As1(sup)= 6.03, Hjw= 40.0 cm, bj= 60.0 cm, hjc= 30.0 cm

FxMin,inf	FxMin,sup	FxMax,sup	FySup	FzSup	Vjbdy	Vjbdz	Vres,y	Vres,z	I.R.compr.	Ashy	Ashz	PASSO	Nota
daN					daN		daN			cmq		cm	

-6621	1	-0	0	0	35233	26425	175015	126011	0.21	4.08	1.81	13.08

VERIFICA DI RESISTENZA CON SOLLECITAZIONI COMPORTAMENTO NON DISSIPATIVO

Asse loc. pilastro y nodo INTERNO: Hjw= 40.0 cm, bj= 40.0 cm, hjc= 50.0 cm, db1= 45.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb,1	Mb,2	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m			daN			cmq	cm	
2	-0	-6766	-2200	-45	0	5321	175015	0.03	0.00	40.00	
3	-0	-6889	-2203	-46	0	5327	175015	0.03	0.00	40.00	
4	-0	-6765	-1323	-895	0	1058	175015	0.01	0.00	40.00	
5	-0	-6889	-1326	-896	0	1063	175015	0.01	0.00	40.00	
6	-0	-6621	-1889	-341	0	3821	175015	0.02	0.00	40.00	
7	-0	-7033	-1900	-344	0	3841	175015	0.02	0.00	40.00	
8	-0	-6621	-1626	-596	0	2543	175015	0.01	0.00	40.00	
9	-0	-7033	-1637	-599	0	2563	175015	0.01	0.00	40.00	
10	-0	-6766	-2200	-45	0	5321	175015	0.03	0.00	40.00	
11	-0	-6889	-2203	-46	0	5327	175015	0.03	0.00	40.00	
12	-0	-6765	-1323	-895	0	1058	175015	0.01	0.00	40.00	
13	-0	-6889	-1326	-896	0	1063	175015	0.01	0.00	40.00	
14	-0	-6621	-1889	-341	0	3821	175015	0.02	0.00	40.00	
15	-0	-7033	-1900	-344	0	3841	175015	0.02	0.00	40.00	
16	-0	-6621	-1626	-596	0	2543	175015	0.01	0.00	40.00	
17	-0	-7033	-1637	-599	0	2563	175015	0.01	0.00	40.00	

Asse loc. pilastro z nodo ESTERNO: Hjw= 40.0 cm, bj= 60.0 cm, hjc= 30.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb	Vb	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m			daN			cmq	cm	
2	-0	-6766	-1551	4514	0	3830	126011	0.03	0.00	40.00	
3	-0	-6889	-1644	4636	0	4059	126011	0.03	0.00	40.00	
4	-0	-6765	-1583	4540	0	3909	126011	0.03	0.00	40.00	
5	-0	-6889	-1676	4662	0	4138	126011	0.03	0.00	40.00	
6	-0	-6621	-1454	4381	0	3590	126011	0.03	0.00	40.00	
7	-0	-7033	-1763	4788	0	4353	126011	0.03	0.00	40.00	
8	-0	-6621	-1464	4389	0	3615	126011	0.03	0.00	40.00	
9	-0	-7033	-1773	4795	0	4378	126011	0.03	0.00	40.00	
10	-0	-6766	-1551	4514	0	3830	126011	0.03	0.00	40.00	
11	-0	-6889	-1644	4636	0	4059	126011	0.03	0.00	40.00	
12	-0	-6765	-1583	4540	0	3909	126011	0.03	0.00	40.00	
13	-0	-6889	-1676	4662	0	4138	126011	0.03	0.00	40.00	
14	-0	-6621	-1454	4381	0	3590	126011	0.03	0.00	40.00	
15	-0	-7033	-1763	4788	0	4353	126011	0.03	0.00	40.00	
16	-0	-6621	-1464	4389	0	3615	126011	0.03	0.00	40.00	
17	-0	-7033	-1773	4795	0	4378	126011	0.03	0.00	40.00	

CONFRONTO E SINTESI CONCLUSIVE (si assume in ogni caso passo <= 15 cm)

I.R.compr.	Ashy	Ashz	PASSO	Nota
	cmq		cm	
0.03	--	--	15.00	**VERIFICATO**

ASTA NUM. 53 NI 172 NF 185 SEZ. Rp B= 0.400 H= 0.600 (pilastro)
PIL. NUM. 21B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-11950	668	718	0	731	-1355	12.57	12.57	6.28	6.28	3	0.06	0.01	0.06	0.00	0.00	24.0
2	0	-9113	905	539	0	548	-1791	12.57	12.57	6.28	6.28	2	0.11	0.02	0.09	0.00	0.00	24.0
3	0	-9246	909	580	0	600	-1796	12.57	12.57	6.28	6.28	2	0.11	0.02	0.09	0.00	0.00	24.0
4	0	-9133	120	526	0	524	-289	12.57	12.57	6.28	6.28	2	0.04	0.01	0.05	0.00	0.00	24.0
5	0	-9266	123	566	0	576	-294	12.57	12.57	6.28	6.28	2	0.04	0.01	0.05	0.00	0.00	24.0
6	0	-8964	626	487	0	479	-1260	12.57	12.57	6.28	6.28	2	0.08	0.01	0.06	0.00	0.00	24.0
7	0	-9408	638	622	0	653	-1276	12.57	12.57	6.28	6.28	2	0.09	0.01	0.06	0.00	0.00	24.0
8	0	-8971	391	483	0	472	-809	12.57	12.57	6.28	6.28	2	0.06	0.01	0.04	0.00	0.00	24.0
9	0	-9415	402	618	0	646	-825	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
10	0	-9113	905	539	0	548	-1791	12.57	12.57	6.28	6.28	2	0.11	0.02	0.09	0.00	0.00	24.0
11	0	-9246	909	580	0	600	-1796	12.57	12.57	6.28	6.28	2	0.11	0.02	0.09	0.00	0.00	24.0
12	0	-9133	120	526	0	524	-289	12.57	12.57	6.28	6.28	2	0.04	0.01	0.05	0.00	0.00	24.0
13	0	-9266	123	566	0	576	-294	12.57	12.57	6.28	6.28	2	0.04	0.01	0.05	0.00	0.00	24.0
14	0	-8964	626	487	0	479	-1260	12.57	12.57	6.28	6.28	2	0.08	0.01	0.06	0.00	0.00	24.0
15	0	-9408	638	622	0	653	-1276	12.57	12.57	6.28	6.28	2	0.09	0.01	0.06	0.00	0.00	24.0
16	0	-8971	391	483	0	472	-809	12.57	12.57	6.28	6.28	2	0.06	0.01	0.04	0.00	0.00	24.0
17	0	-9415	402	618	0	646	-825	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
18	0	-12360	2609	820	0	876	-5012	12.57	12.57	6.28	6.28	3	0.19	0.05	0.25	0.00	0.00	24.0
19	0	-12410	-38	759	0	771	24	12.57	12.57	6.28	6.28	3	0.04	0.01	0.07	0.00	0.00	24.0
20	0	-12450	1202	749	0	742	-2338	12.57	12.57	6.28	6.28	3	0.09	0.02	0.12	0.00	0.00	24.0
37	0	-12100	3288	807	0	872	-6316	12.57	12.57	6.28	6.28	3	0.23	0.06	0.32	0.00	0.00	24.0
38	0	-12190	-1124	706	0	697	2078	12.57	12.57	6.28	6.28	3	0.08	0.02	0.11	0.00	0.00	24.0
39	0	-12240	942	690	0	649	-1859	12.57	12.57	6.28	6.28	3	0.08	0.02	0.09	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	97	-11188	668	718	0	31	-703	12.57	12.57	6.28	6.28	3	0.03	0.01	0.07	0.00	0.00	24.0
2	97	-8528	905	539	0	22	-908	12.57	12.57	6.28	6.28	2	0.05	0.02	0.09	0.00	0.00	24.0
3	97	-8661	909	580	0	35	-910	12.57	12.57	6.28	6.28	2	0.05	0.02	0.09	0.00	0.00	24.0
4	97	-8548	120	526	0	12	-172	12.57	12.57	6.28	6.28	2	0.01	0.01	0.05	0.00	0.00	24.0
5	97	-8681	123	566	0	25	-174	12.57	12.57	6.28	6.28	2	0.01	0.01	0.05	0.00	0.00	24.0
6	97	-8379	626	487	0	4	-649	12.57	12.57	6.28	6.28	2	0.03	0.01	0.06	0.00	0.00	24.0
7	97	-8823	638	622	0	46	-654	12.57	12.57	6.28	6.28	2	0.04	0.01	0.06	0.00	0.00	24.0
8	97	-8386	391	483	0	1	-428	12.57	12.57	6.28	6.28	2	0.02	0.01	0.04	0.00	0.00	24.0
9	97	-8830	402	618	0	43	-433	12.57	12.57	6.28	6.28	2	0.02	0.01	0.05	0.00	0.00	24.0
10	97	-8528	905	539	0	22	-908	12.57	12.57	6.28	6.28	2	0.05	0.02	0.09	0.00	0.00	24.0
11	97	-8661	909	580	0	35	-910	12.57	12.57	6.28	6.28	2	0.05	0.02	0.09	0.00	0.00	24.0
12	97	-8548	120	526	0	12	-172	12.57	12.57	6.28	6.28	2	0.01	0.01	0.05	0.00	0.00	24.0

13	97	-8681	123	566	0	25	-174	12.57	12.57	6.28	6.28	2	0.01	0.01	0.05	0.00	0.00	24.0
14	97	-8379	626	487	0	4	-649	12.57	12.57	6.28	6.28	2	0.03	0.01	0.06	0.00	0.00	24.0
15	97	-8823	638	622	0	46	-654	12.57	12.57	6.28	6.28	2	0.04	0.01	0.06	0.00	0.00	24.0
16	97	-8386	391	483	0	1	-428	12.57	12.57	6.28	6.28	2	0.02	0.01	0.04	0.00	0.00	24.0
17	97	-8830	402	618	0	43	-433	12.57	12.57	6.28	6.28	2	0.02	0.01	0.05	0.00	0.00	24.0
18	97	-11600	2609	820	0	76	-2468	12.57	12.57	6.28	6.28	3	0.09	0.05	0.25	0.00	0.00	24.0
19	97	-11651	-38	759	0	31	-14	12.57	12.57	6.28	6.28	3	0.00	0.01	0.07	0.00	0.00	24.0
20	97	-11688	1202	749	0	12	-1166	12.57	12.57	6.28	6.28	3	0.04	0.02	0.12	0.00	0.00	24.0
37	97	-11340	3288	807	0	85	-3110	12.57	12.57	6.28	6.28	3	0.11	0.06	0.32	0.00	0.00	24.0
38	97	-11428	-1124	706	0	9	982	12.57	12.57	6.28	6.28	3	0.04	0.02	0.11	0.00	0.00	24.0
39	97	-11479	942	690	0	-23	-940	12.57	12.57	6.28	6.28	3	0.03	0.02	0.09	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	195	-10427	668	718	0	-670	-51	12.57	12.57	6.28	6.28	3	0.04	0.01	0.07	0.00	0.00	24.0
2	195	-7943	905	539	0	-503	-26	12.57	12.57	6.28	6.28	2	0.03	0.02	0.09	0.00	0.00	24.0
3	195	-8076	909	580	0	-530	-24	12.57	12.57	6.28	6.28	2	0.03	0.02	0.09	0.00	0.00	24.0
4	195	-7963	120	526	0	-500	-55	12.57	12.57	6.28	6.28	2	0.03	0.01	0.05	0.00	0.00	24.0
5	195	-8096	123	566	0	-527	-54	12.57	12.57	6.28	6.28	2	0.03	0.01	0.05	0.00	0.00	24.0
6	195	-7794	626	487	0	-472	-38	12.57	12.57	6.28	6.28	2	0.03	0.01	0.06	0.00	0.00	24.0
7	195	-8238	638	622	0	-560	-33	12.57	12.57	6.28	6.28	2	0.03	0.01	0.06	0.00	0.00	24.0
8	195	-7801	391	483	0	-471	-47	12.57	12.57	6.28	6.28	2	0.03	0.01	0.05	0.00	0.00	24.0
9	195	-8245	402	618	0	-559	-41	12.57	12.57	6.28	6.28	2	0.03	0.01	0.06	0.00	0.00	24.0
10	195	-7943	905	539	0	-503	-26	12.57	12.57	6.28	6.28	2	0.03	0.02	0.09	0.00	0.00	24.0
11	195	-8076	909	580	0	-530	-24	12.57	12.57	6.28	6.28	2	0.03	0.02	0.09	0.00	0.00	24.0
12	195	-7963	120	526	0	-500	-55	12.57	12.57	6.28	6.28	2	0.03	0.01	0.05	0.00	0.00	24.0
13	195	-8096	123	566	0	-527	-54	12.57	12.57	6.28	6.28	2	0.03	0.01	0.05	0.00	0.00	24.0
14	195	-7794	626	487	0	-472	-38	12.57	12.57	6.28	6.28	2	0.03	0.01	0.06	0.00	0.00	24.0
15	195	-8238	638	622	0	-560	-33	12.57	12.57	6.28	6.28	2	0.03	0.01	0.06	0.00	0.00	24.0
16	195	-7801	391	483	0	-471	-47	12.57	12.57	6.28	6.28	2	0.03	0.01	0.05	0.00	0.00	24.0
17	195	-8245	402	618	0	-559	-41	12.57	12.57	6.28	6.28	2	0.03	0.01	0.06	0.00	0.00	24.0
18	195	-10840	2609	820	0	-723	76	12.57	12.57	6.28	6.28	3	0.04	0.05	0.26	0.00	0.00	24.0
19	195	-10892	-38	759	0	-709	-51	12.57	12.57	6.28	6.28	3	0.04	0.01	0.07	0.00	0.00	24.0
20	195	-10927	1202	749	0	-719	5	12.57	12.57	6.28	6.28	3	0.04	0.02	0.12	0.00	0.00	24.0
37	195	-10579	3288	807	0	-702	97	12.57	12.57	6.28	6.28	3	0.04	0.06	0.32	0.00	0.00	24.0
38	195	-10667	-1124	706	0	-679	-114	12.57	12.57	6.28	6.28	3	0.04	0.02	0.11	0.00	0.00	24.0
39	195	-10718	942	690	0	-696	-21	12.57	12.57	6.28	6.28	3	0.04	0.02	0.09	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	292	-9666	668	718	0	-1370	600	12.57	12.57	6.28	6.28	3	0.08	0.01	0.07	0.00	0.00	24.0
2	292	-7358	905	539	0	-1029	857	12.57	12.57	6.28	6.28	2	0.09	0.02	0.09	0.00	0.00	24.0
3	292	-7491	909	580	0	-1096	862	12.57	12.57	6.28	6.28	2	0.09	0.02	0.09	0.00	0.00	24.0
4	292	-7378	120	526	0	-1013	62	12.57	12.57	6.28	6.28	2	0.06	0.01	0.05	0.00	0.00	24.0
5	292	-7511	123	566	0	-1079	66	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
6	292	-7209	626	487	0	-947	573	12.57	12.57	6.28	6.28	2	0.07	0.01	0.06	0.00	0.00	24.0
7	292	-7653	638	622	0	-1167	589	12.57	12.57	6.28	6.28	2	0.09	0.01	0.07	0.00	0.00	24.0
8	292	-7216	391	483	0	-942	334	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
9	292	-7660	402	618	0	-1162	351	12.57	12.57	6.28	6.28	2	0.08	0.01	0.06	0.00	0.00	24.0
10	292	-7358	905	539	0	-1029	857	12.57	12.57	6.28	6.28	2	0.09	0.02	0.09	0.00	0.00	24.0
11	292	-7491	909	580	0	-1096	862	12.57	12.57	6.28	6.28	2	0.09	0.02	0.09	0.00	0.00	24.0
12	292	-7378	120	526	0	-1013	62	12.57	12.57	6.28	6.28	2	0.06	0.01	0.05	0.00	0.00	24.0
13	292	-7511	123	566	0	-1079	66	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
14	292	-7209	626	487	0	-947	573	12.57	12.57	6.28	6.28	2	0.07	0.01	0.06	0.00	0.00	24.0
15	292	-7653	638	622	0	-1167	589	12.57	12.57	6.28	6.28	2	0.09	0.01	0.07	0.00	0.00	24.0
16	292	-7216	391	483	0	-942	334	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
17	292	-7660	402	618	0	-1162	351	12.57	12.57	6.28	6.28	2	0.08	0.01	0.06	0.00	0.00	24.0
18	292	-10081	2609	820	0	-1522	2619	12.57	12.57	6.28	6.28	3	0.13	0.05	0.26	0.00	0.00	24.0
19	292	-10132	-38	759	0	-1449	-88	12.57	12.57	6.28	6.28	3	0.08	0.01	0.07	0.00	0.00	24.0
20	292	-10166	1202	749	0	-1449	1176	12.57	12.57	6.28	6.28	3	0.09	0.02	0.12	0.00	0.00	24.0
37	292	-9818	3288	807	0	-1489	3303	12.57	12.57	6.28	6.28	3	0.15	0.06	0.33	0.00	0.00	24.0
38	292	-9906	-1124	706	0	-1368	-1210	12.57	12.57	6.28	6.28	3	0.08	0.02	0.11	0.00	0.00	24.0
39	292	-9958	942	690	0	-1368	898	12.57	12.57	6.28	6.28	3	0.08	0.02	0.09	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	390	-8904	668	718	0	-2071	1252	12.57	12.57	6.28	6.28	3	0.12	0.01	0.07	0.00	0.00	24.0
2	390	-6773	905	539	0	-1555	1740	12.57	12.57	6.28	6.28	2	0.16	0.02	0.09	0.00	0.00	24.0
3	390	-6906	909	580	0	-1661	1748	12.57	12.57	6.28	6.28	2	0.16	0.02	0.09	0.00	0.00	24.0
4	390	-6793	120	526	0	-1525	178	12.57	12.57	6.28	6.28	2	0.10	0.01	0.05	0.00	0.00	24.0
5	390	-6926	123	566	0	-1631	186	12.57	12.57	6.28	6.28	2	0.10	0.01	0.06	0.00	0.00	24.0
6	390	-6624	626	487	0	-1422	1184	12.57	12.57	6.28	6.28	2	0.12	0.01	0.07	0.00	0.00	24.0
7	390	-7068	638	622	0	-1773	1211	12.57	12.57	6.28	6.28	2	0.14	0.01	0.07	0.00	0.00	24.0
8	390	-6631	391	483	0	-1413	715	12.57	12.57	6.28	6.28	2	0.11	0.01	0.05	0.00	0.00	24.0
9	390	-7075	402	618	0	-1764	742	12.57	12.57	6.28	6.28	2	0.13	0.01	0.06	0.00	0.00	24.0
10	390	-6773	905	539	0	-1555	1740	12.57	12.57	6.28	6.28	2	0.16	0.02	0.09	0.00	0.00	24.0
11	390	-6906	909	580	0	-1661	1748	12.57	12.57	6.28	6.28	2	0.16	0.02	0.09	0.00	0.00	24.0
12	390	-6793	120	526	0	-1525	178	12.57	12.57	6.28	6.28	2	0.10	0.01	0.05	0.00	0.00	24.0
13	390	-6926	123	566	0	-1631	186	12.57	12.57	6.28	6.28	2	0.10	0.01	0.06	0.00	0.00	24.0
14	390	-6624	626	487	0	-1422	1184	12.57	12.57	6.28	6.28	2	0.12	0.01	0.07	0.00	0.00	24.0
15	390	-7068	638	622	0	-1773	1211	12.57	12.57	6.28	6.28	2	0.14	0.01	0.07	0.00	0.00	24.0
16	390	-6631	391	483	0	-1413	715	12.57	12.57	6.28	6.28	2	0.11	0.01	0.05	0.00	0.00	24.0
17	390	-7075	402	618	0	-1764	742	12.57	12.57	6.28	6.28	2	0.13	0.01	0.06	0.00	0.00	24.0
18	390	-9321	2609	820	0	-2321	5163	12.57	12.57	6.28	6.28	3	0.23	0.05	0.26	0.00	0.00	24.0
19	390	-9373	-38	759	0	-2189	-126	12.57	12.57	6.28	6.28	3	0.12	0.01	0.07	0.00	0.00	24.0
20	390	-9404	1202	749	0	-2179	2348	12.57	12.57	6.28	6.28	3	0.14	0.02	0.12	0.00	0.00	24.0
37	390	-9058	3288	807	0	-2276	6509	12.57	12.57	6.28	6.28	3	0.27	0.06	0.33	0.00	0.00	24.0
38	390	-9144	-1124	706	0	-2056	-2306	12.57	12.57	6.28	6.28	3	0.13	0.02	0.11	0.00	0.00	24.0
39	390	-9197	942	690	0	-2040	1817	12.57	12.57	6.28	6.28	3	0.13	0.02	0.09	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

VERIFICA NODO IN TESTA AL PILASTRO, NODO NUM. 185 NON CONFINATO

(par.7.2.2 NTC2018 "La domanda di resistenza valutata con i criteri della progettazione in capacità può essere assunta non superiore alla domanda di resistenza valutata per il caso di comportamento strutturale non dissipativo.")

PROGETTAZIONE IN CAPACITA'

Asse loc. pilastro y nodo INTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 40.0 cm, hjc= 50.0 cm
Asse loc. pilastro z nodo ESTERNO: As2(inf)= 6.03, As1(sup)= 6.03, Hjw= 40.0 cm, bj= 60.0 cm, hjc= 30.0 cm

FxMin,inf	FxMin,sup	FxMax,sup	FySup	FzSup	Vjbdy	Vjbdz	Vres,y	Vres,z	I.R.compr.	Ashy	Ashz	PASSO	Nota
daN					daN		daN			cmq		cm	
-6624	1	-0	0	0	35233	26425	175015	126011	0.21	4.08	1.81	13.08	

VERIFICA DI RESISTENZA CON SOLLECITAZIONI COMPORTAMENTO NON DISSIPATIVO

Asse loc. pilastro y nodo INTERNO: Hjw= 40.0 cm, bj= 40.0 cm, hjc= 50.0 cm, db1= 45.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb,1	Mb,2	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m			daN			cmq	cm	
2	-0	-6773	-2057	-337	0	4247	175015	0.02	0.00	40.00	
3	-0	-6906	-2056	-329	0	4264	175015	0.02	0.00	40.00	
4	-0	-6793	-1197	-1227	0	74	175015	0.00	0.00	40.00	
5	-0	-6926	-1196	-1219	0	57	175015	0.00	0.00	40.00	
6	-0	-6624	-1757	-658	0	2715	175015	0.02	0.00	40.00	
7	-0	-7068	-1753	-631	0	2770	175015	0.02	0.00	40.00	
8	-0	-6631	-1499	-924	0	1419	175015	0.01	0.00	40.00	
9	-0	-7075	-1495	-898	0	1474	175015	0.01	0.00	40.00	
10	-0	-6773	-2057	-337	0	4247	175015	0.02	0.00	40.00	
11	-0	-6906	-2056	-329	0	4264	175015	0.02	0.00	40.00	
12	-0	-6793	-1197	-1227	0	74	175015	0.00	0.00	40.00	
13	-0	-6926	-1196	-1219	0	57	175015	0.00	0.00	40.00	
14	-0	-6624	-1757	-658	0	2715	175015	0.02	0.00	40.00	
15	-0	-7068	-1753	-631	0	2770	175015	0.02	0.00	40.00	
16	-0	-6631	-1499	-924	0	1419	175015	0.01	0.00	40.00	
17	-0	-7075	-1495	-898	0	1474	175015	0.01	0.00	40.00	

Asse loc. pilastro z nodo ESTERNO: Hjw= 40.0 cm, bj= 60.0 cm, hjc= 30.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb	Vb	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-0	-6773	-1618	4542	0	3995	126011	0.03	0.00	40.00	
3	-0	-6906	-1731	4679	0	4274	126011	0.03	0.00	40.00	
4	-0	-6793	-1588	4522	0	3921	126011	0.03	0.00	40.00	
5	-0	-6926	-1701	4659	0	4200	126011	0.03	0.00	40.00	
6	-0	-6624	-1476	4375	0	3644	126011	0.03	0.00	40.00	
7	-0	-7068	-1853	4832	0	4575	126011	0.04	0.00	40.00	
8	-0	-6631	-1466	4369	0	3620	126011	0.03	0.00	40.00	
9	-0	-7075	-1843	4826	0	4551	126011	0.04	0.00	40.00	
10	-0	-6773	-1618	4542	0	3995	126011	0.03	0.00	40.00	
11	-0	-6906	-1731	4679	0	4274	126011	0.03	0.00	40.00	
12	-0	-6793	-1588	4522	0	3921	126011	0.03	0.00	40.00	
13	-0	-6926	-1701	4659	0	4200	126011	0.03	0.00	40.00	
14	-0	-6624	-1476	4375	0	3644	126011	0.03	0.00	40.00	
15	-0	-7068	-1853	4832	0	4575	126011	0.04	0.00	40.00	
16	-0	-6631	-1466	4369	0	3620	126011	0.03	0.00	40.00	
17	-0	-7075	-1843	4826	0	4551	126011	0.04	0.00	40.00	

CONFRONTO E SINTESI CONCLUSIVE (si assume in ogni caso passo <= 15 cm)

I.R.compr.	Ashy	Ashz	PASSO	Nota
	cmq		cm	
0.04	--	--	15.00	**VERIFICATO**

ASTA NUM. 54 NI 167 NF 208 SEZ. Rp B= 0.400 H= 0.600 (pilastro)
PIL. NUM. 26C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-2268	2268	-671	0	1309	-2459	12.57	12.57	6.28	6.28	3	0.12	0.04	0.25	0.00	0.00	24.0
2	0	-1857	2062	-759	0	1029	-2211	12.57	12.57	6.28	6.28	2	0.16	0.04	0.23	0.00	0.00	24.0
3	0	-1718	2087	-380	0	1054	-2238	12.57	12.57	6.28	6.28	2	0.16	0.04	0.23	0.00	0.00	24.0
4	0	-1772	1402	-652	0	959	-1545	12.57	12.57	6.28	6.28	2	0.12	0.02	0.16	0.00	0.00	24.0
5	0	-1632	1428	-274	0	985	-1573	12.57	12.57	6.28	6.28	2	0.13	0.03	0.16	0.00	0.00	24.0
6	0	-1990	1801	-1164	0	975	-1946	12.57	12.57	6.28	6.28	2	0.15	0.03	0.20	0.00	0.00	24.0
7	0	-1524	1886	99	0	1059	-2037	12.57	12.57	6.28	6.28	2	0.15	0.03	0.21	0.00	0.00	24.0
8	0	-1965	1603	-1132	0	954	-1746	12.57	12.57	6.28	6.28	2	0.13	0.03	0.18	0.00	0.00	24.0
9	0	-1499	1688	131	0	1039	-1837	12.57	12.57	6.28	6.28	2	0.14	0.03	0.19	0.00	0.00	24.0
10	0	-1857	2062	-759	0	1029	-2211	12.57	12.57	6.28	6.28	2	0.16	0.04	0.23	0.00	0.00	24.0
11	0	-1718	2087	-380	0	1054	-2238	12.57	12.57	6.28	6.28	2	0.16	0.04	0.23	0.00	0.00	24.0
12	0	-1772	1402	-652	0	959	-1545	12.57	12.57	6.28	6.28	2	0.12	0.02	0.16	0.00	0.00	24.0
13	0	-1632	1428	-274	0	985	-1573	12.57	12.57	6.28	6.28	2	0.13	0.03	0.16	0.00	0.00	24.0
14	0	-1990	1801	-1164	0	975	-1946	12.57	12.57	6.28	6.28	2	0.15	0.03	0.20	0.00	0.00	24.0
15	0	-1524	1886	99	0	1059	-2037	12.57	12.57	6.28	6.28	2	0.15	0.03	0.21	0.00	0.00	24.0
16	0	-1965	1603	-1132	0	954	-1746	12.57	12.57	6.28	6.28	2	0.13	0.03	0.18	0.00	0.00	24.0
17	0	-1499	1688	131	0	1039	-1837	12.57	12.57	6.28	6.28	2	0.14	0.03	0.19	0.00	0.00	24.0
18	0	-3099	5715	-1844	0	1787	-5930	12.57	12.57	6.28	6.28	3	0.25	0.10	0.63	0.00	0.00	24.0
19	0	-2925	2992	-1624	0	1637	-3367	12.57	12.57	6.28	6.28	3	0.16	0.05	0.33	0.00	0.00	24.0
20	0	-2560	4130	-170	0	1890	-4406	12.57	12.57	6.28	6.28	3	0.20	0.07	0.46	0.00	0.00	24.0
37	0	-2912	5941	-1569	0	1701	-6069	12.57	12.57	6.28	6.28	3	0.26	0.10	0.65	0.00	0.00	24.0
38	0	-2623	1403	-1204	0	1449	-1797	12.57	12.57	6.28	6.28	3	0.10	0.02	0.16	0.00	0.00	24.0
39	0	-2014	3299	1219	0	1872	-3528	12.57	12.57	6.28	6.28	3	0.17	0.06	0.37	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	12	-2170	2268	-671	0	1393	-2175	12.57	12.57	6.28	6.28	3	0.11	0.04	0.25	0.00	0.00	24.0
2	12	-1782	2062	-759	0	1124	-1953	12.57	12.57	6.28	6.28	2	0.15	0.04	0.23	0.00	0.00	24.0
3	12	-1643	2087	-380	0	1102	-1977	12.57	12.57	6.28	6.28	2	0.15	0.04	0.23	0.00	0.00	24.0
4	12	-1697	1402	-652	0	1041	-1370	12.57	12.57	6.28	6.28	2	0.12	0.02	0.16	0.00	0.00	24.0
5	12	-1557	1428	-274	0	1019	-1394	12.57	12.57	6.28	6.28	2	0.12	0.03	0.16	0.00	0.00	24.0
6	12	-1915	1801	-1164	0	1120	-1721	12.57	12.57	6.28	6.28	2	0.14	0.03	0.20	0.00	0.00	24.0
7	12	-1449	1886	99	0	1047	-1801	12.57	12.57	6.28	6.28	2	0.14	0.03	0.21	0.00	0.00	24.0
8	12	-1890	1603	-1132	0	1096	-1546	12.57	12.57	6.28	6.28	2	0.13	0.03	0.18	0.00	0.00	24.0
9	12	-1424	1688	131	0	1023	-1626	12.57	12.57	6.28	6.28	2	0.13	0.03	0.19	0.00	0.00	24.0
10	12	-1782	2062	-759	0	1124	-1953	12.57	12.57	6.28	6.28	2	0.15	0.04	0.23	0.00	0.00	24.0
11	12	-1643	2087	-380	0	1102	-1977	12.57	12.57	6.28	6.28	2	0.15	0.04	0.23	0.00	0.00	24.0
12	12	-1697	1402	-652	0	1041	-1370	12.57	12.57	6.28	6.28	2	0.12	0.02	0.16	0.00	0.00	24.0
13	12	-1557	1428	-274	0	1019	-1394	12.57	12.57	6.28	6.28	2	0.12	0.03	0.16	0.00	0.00	24.0
14	12	-1915	1801	-1164	0	1120	-1721	12.57	12.57	6.28	6.28	2	0.14	0.03	0.20	0.00	0.00	24.0
15	12	-1449	1886	99	0	1047	-1801	12.57	12.57	6.28	6.28	2	0.14	0.03	0.21	0.00	0.00	24.0
16	12	-1890	1603	-1132	0	1096	-1546	12.57	12.57	6.28	6.28	2	0.13	0.03	0.18	0.00	0.00	24.0
17	12	-1424	1688	131	0	1023	-1626	12.57	12.57	6.28	6.28	2	0.13	0.03	0.19	0.00	0.00	24.0
18	12	-3002	5715	-1844	0	2018	-5216	12.57	12.57	6.28	6.28	3	0.23	0.10	0.63	0.00	0.00	24.0

19	12	-2828	2992	-1624	0	1840	-2993	12.57	12.57	6.28	6.28	3	0.15	0.05	0.33	0.00	0.00	24.0
20	12	-2462	4130	-170	0	1911	-3890	12.57	12.57	6.28	6.28	3	0.18	0.07	0.46	0.00	0.00	24.0
37	12	-2814	5941	-1569	0	1897	-5326	12.57	12.57	6.28	6.28	3	0.23	0.10	0.66	0.00	0.00	24.0
38	12	-2526	1403	-1204	0	1600	-1622	12.57	12.57	6.28	6.28	3	0.11	0.02	0.16	0.00	0.00	24.0
39	12	-1916	3299	1219	0	1720	-3116	12.57	12.57	6.28	6.28	3	0.15	0.06	0.37	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-2073	2268	-671	0	1477	-1892	12.57	12.57	6.28	6.28	3	0.11	0.04	0.25	0.00	0.00	24.0
2	25	-1707	2062	-759	0	1219	-1696	12.57	12.57	6.28	6.28	2	0.14	0.04	0.23	0.00	0.00	24.0
3	25	-1568	2087	-380	0	1149	-1716	12.57	12.57	6.28	6.28	2	0.14	0.04	0.23	0.00	0.00	24.0
4	25	-1622	1402	-652	0	1123	-1195	12.57	12.57	6.28	6.28	2	0.12	0.02	0.16	0.00	0.00	24.0
5	25	-1482	1428	-274	0	1053	-1216	12.57	12.57	6.28	6.28	2	0.11	0.03	0.16	0.00	0.00	24.0
6	25	-1840	1801	-1164	0	1266	-1496	12.57	12.57	6.28	6.28	2	0.14	0.03	0.20	0.00	0.00	24.0
7	25	-1374	1886	99	0	1034	-1565	12.57	12.57	6.28	6.28	2	0.13	0.03	0.21	0.00	0.00	24.0
8	25	-1815	1603	-1132	0	1237	-1345	12.57	12.57	6.28	6.28	2	0.13	0.03	0.18	0.00	0.00	24.0
9	25	-1349	1688	131	0	1006	-1415	12.57	12.57	6.28	6.28	2	0.12	0.03	0.19	0.00	0.00	24.0
10	25	-1707	2062	-759	0	1219	-1696	12.57	12.57	6.28	6.28	2	0.14	0.04	0.23	0.00	0.00	24.0
11	25	-1568	2087	-380	0	1149	-1716	12.57	12.57	6.28	6.28	2	0.14	0.04	0.23	0.00	0.00	24.0
12	25	-1622	1402	-652	0	1123	-1195	12.57	12.57	6.28	6.28	2	0.12	0.02	0.16	0.00	0.00	24.0
13	25	-1482	1428	-274	0	1053	-1216	12.57	12.57	6.28	6.28	2	0.11	0.03	0.16	0.00	0.00	24.0
14	25	-1840	1801	-1164	0	1266	-1496	12.57	12.57	6.28	6.28	2	0.14	0.03	0.20	0.00	0.00	24.0
15	25	-1374	1886	99	0	1034	-1565	12.57	12.57	6.28	6.28	2	0.13	0.03	0.21	0.00	0.00	24.0
16	25	-1815	1603	-1132	0	1237	-1345	12.57	12.57	6.28	6.28	2	0.13	0.03	0.18	0.00	0.00	24.0
17	25	-1349	1688	131	0	1006	-1415	12.57	12.57	6.28	6.28	2	0.12	0.03	0.19	0.00	0.00	24.0
18	25	-2904	5715	-1844	0	2248	-4501	12.57	12.57	6.28	6.28	3	0.21	0.10	0.63	0.00	0.00	24.0
19	25	-2730	2992	-1624	0	2043	-2619	12.57	12.57	6.28	6.28	3	0.15	0.05	0.33	0.00	0.00	24.0
20	25	-2365	4130	-170	0	1933	-3374	12.57	12.57	6.28	6.28	3	0.17	0.07	0.46	0.00	0.00	24.0
37	25	-2717	5941	-1569	0	2093	-4583	12.57	12.57	6.28	6.28	3	0.21	0.11	0.66	0.00	0.00	24.0
38	25	-2428	1403	-1204	0	1750	-1446	12.57	12.57	6.28	6.28	3	0.11	0.02	0.16	0.00	0.00	24.0
39	25	-1819	3299	1219	0	1567	-2703	12.57	12.57	6.28	6.28	3	0.14	0.06	0.37	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-1976	2268	-671	0	1560	-1609	12.57	12.57	6.28	6.28	3	0.10	0.04	0.25	0.00	0.00	24.0
2	38	-1632	2062	-759	0	1313	-1438	12.57	12.57	6.28	6.28	2	0.14	0.04	0.23	0.00	0.00	24.0
3	38	-1493	2087	-380	0	1196	-1455	12.57	12.57	6.28	6.28	2	0.13	0.04	0.23	0.00	0.00	24.0
4	38	-1547	1402	-652	0	1204	-1019	12.57	12.57	6.28	6.28	2	0.11	0.02	0.16	0.00	0.00	24.0
5	38	-1407	1428	-274	0	1088	-1037	12.57	12.57	6.28	6.28	2	0.11	0.03	0.16	0.00	0.00	24.0
6	38	-1765	1801	-1164	0	1412	-1270	12.57	12.57	6.28	6.28	2	0.13	0.03	0.20	0.00	0.00	24.0
7	38	-1299	1886	99	0	1022	-1330	12.57	12.57	6.28	6.28	2	0.12	0.03	0.21	0.00	0.00	24.0
8	38	-1740	1603	-1132	0	1379	-1145	12.57	12.57	6.28	6.28	2	0.13	0.03	0.18	0.00	0.00	24.0
9	38	-1274	1688	131	0	990	-1204	12.57	12.57	6.28	6.28	2	0.11	0.03	0.19	0.00	0.00	24.0
10	38	-1632	2062	-759	0	1313	-1438	12.57	12.57	6.28	6.28	2	0.14	0.04	0.23	0.00	0.00	24.0
11	38	-1493	2087	-380	0	1196	-1455	12.57	12.57	6.28	6.28	2	0.13	0.04	0.23	0.00	0.00	24.0
12	38	-1547	1402	-652	0	1204	-1019	12.57	12.57	6.28	6.28	2	0.11	0.02	0.16	0.00	0.00	24.0
13	38	-1407	1428	-274	0	1088	-1037	12.57	12.57	6.28	6.28	2	0.11	0.03	0.16	0.00	0.00	24.0
14	38	-1765	1801	-1164	0	1412	-1270	12.57	12.57	6.28	6.28	2	0.13	0.03	0.20	0.00	0.00	24.0
15	38	-1299	1886	99	0	1022	-1330	12.57	12.57	6.28	6.28	2	0.12	0.03	0.21	0.00	0.00	24.0
16	38	-1740	1603	-1132	0	1379	-1145	12.57	12.57	6.28	6.28	2	0.13	0.03	0.18	0.00	0.00	24.0
17	38	-1274	1688	131	0	990	-1204	12.57	12.57	6.28	6.28	2	0.11	0.03	0.19	0.00	0.00	24.0
18	38	-2806	5715	-1844	0	2478	-3786	12.57	12.57	6.28	6.28	3	0.20	0.10	0.63	0.00	0.00	24.0
19	38	-2632	2992	-1624	0	2246	-2245	12.57	12.57	6.28	6.28	3	0.15	0.05	0.33	0.00	0.00	24.0
20	38	-2268	4130	-170	0	1954	-2857	12.57	12.57	6.28	6.28	3	0.15	0.07	0.46	0.00	0.00	24.0
37	38	-2620	5941	-1569	0	2289	-3841	12.57	12.57	6.28	6.28	3	0.19	0.11	0.66	0.00	0.00	24.0
38	38	-2330	1403	-1204	0	1900	-1270	12.57	12.57	6.28	6.28	3	0.12	0.02	0.16	0.00	0.00	24.0
39	38	-1722	3299	1219	0	1414	-2291	12.57	12.57	6.28	6.28	3	0.12	0.06	0.37	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-1878	2268	-671	0	1644	-1325	12.57	12.57	6.28	6.28	3	0.11	0.04	0.25	0.00	0.00	24.0
2	50	-1557	2062	-759	0	1408	-1180	12.57	12.57	6.28	6.28	2	0.13	0.04	0.23	0.00	0.00	24.0
3	50	-1418	2087	-380	0	1244	-1194	12.57	12.57	6.28	6.28	2	0.12	0.04	0.24	0.00	0.00	24.0
4	50	-1472	1402	-652	0	1286	-844	12.57	12.57	6.28	6.28	2	0.11	0.02	0.16	0.00	0.00	24.0
5	50	-1332	1428	-274	0	1122	-859	12.57	12.57	6.28	6.28	2	0.10	0.03	0.16	0.00	0.00	24.0
6	50	-1690	1801	-1164	0	1557	-1045	12.57	12.57	6.28	6.28	2	0.13	0.03	0.20	0.00	0.00	24.0
7	50	-1224	1886	99	0	1010	-1094	12.57	12.57	6.28	6.28	2	0.11	0.03	0.21	0.00	0.00	24.0
8	50	-1665	1603	-1132	0	1520	-945	12.57	12.57	6.28	6.28	2	0.13	0.03	0.18	0.00	0.00	24.0
9	50	-1199	1688	131	0	973	-993	12.57	12.57	6.28	6.28	2	0.10	0.03	0.19	0.00	0.00	24.0
10	50	-1557	2062	-759	0	1408	-1180	12.57	12.57	6.28	6.28	2	0.13	0.04	0.23	0.00	0.00	24.0
11	50	-1418	2087	-380	0	1244	-1194	12.57	12.57	6.28	6.28	2	0.12	0.04	0.24	0.00	0.00	24.0
12	50	-1472	1402	-652	0	1286	-844	12.57	12.57	6.28	6.28	2	0.11	0.02	0.16	0.00	0.00	24.0
13	50	-1332	1428	-274	0	1122	-859	12.57	12.57	6.28	6.28	2	0.10	0.03	0.16	0.00	0.00	24.0
14	50	-1690	1801	-1164	0	1557	-1045	12.57	12.57	6.28	6.28	2	0.13	0.03	0.20	0.00	0.00	24.0
15	50	-1224	1886	99	0	1010	-1094	12.57	12.57	6.28	6.28	2	0.11	0.03	0.21	0.00	0.00	24.0
16	50	-1665	1603	-1132	0	1520	-945	12.57	12.57	6.28	6.28	2	0.13	0.03	0.18	0.00	0.00	24.0
17	50	-1199	1688	131	0	973	-993	12.57	12.57	6.28	6.28	2	0.10	0.03	0.19	0.00	0.00	24.0
18	50	-2709	5715	-1844	0	2709	-3072	12.57	12.57	6.28	6.28	3	0.19	0.10	0.63	0.00	0.00	24.0
19	50	-2535	2992	-1624	0	2449	-1871	12.57	12.57	6.28	6.28	3	0.16	0.05	0.33	0.00	0.00	24.0
20	50	-2170	4130	-170	0	1975	-2341	12.57	12.57	6.28	6.28	3	0.14	0.07	0.46	0.00	0.00	24.0
37	50	-2522	5941	-1569	0	2485	-3098	12.57	12.57	6.28	6.28	3	0.18	0.11	0.66	0.00	0.00	24.0
38	50	-2233	1403	-1204	0	2051	-1095	12.57	12.57	6.28	6.28	3	0.13	0.02	0.16	0.00	0.00	24.0
39	50	-1624	3299	1219	0	1262	-1879	12.57	12.57	6.28	6.28	3	0.10	0.06	0.37	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

VERIFICA NODO IN TESTA AL PILASTRO, NODO NUM. 208 NON CONFINATO

(par.7.2.2 NTC2018 "La domanda di resistenza valutata con i criteri della progettazione in capacità può essere assunta non superiore alla domanda di resistenza valutata per il caso di comportamento strutturale non dissipativo.")

PROGETTAZIONE IN CAPACITA'

Asse loc. pilastro y nodo: --

Asse loc. pilastro z nodo ESTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 50.0 cm, hjc= 30.0 cm

FxMin,inf	FxMin,sup	FxMax,sup	FySup	FzSup	Vjbdy	Vjbdz	Vres,y	Vres,z	I.R.compr.	Ashy	Ashz	PASSO	Nota
daN					daN		daN			cmq		cm	
-1199	1	-0	0	0	--	17616	--	105009	0.17	--	--	40.00	

VERIFICA DI RESISTENZA CON SOLLECITAZIONI COMPORTAMENTO NON DISSIPATIVO

Asse loc. pilastro z nodo ESTERNO: Hjw= 40.0 cm, bj= 50.0 cm, hjc= 30.0 cm, db1= 45.0 cm

NC	Fx,sup	Fx,inf	Mb	Vb	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m	daN					cmq	cm	
2	-0	-1557	-1408	1557	0	3477	105009	0.03	0.00	40.00	

3	-0	-1418	-1244	1418	0	3072	105009	0.03	0.00	40.00
4	-0	-1472	-1286	1472	0	3175	105009	0.03	0.00	40.00
5	-0	-1332	-1122	1332	0	2770	105009	0.03	0.00	40.00
6	-0	-1690	-1557	1690	0	3844	105009	0.04	0.00	40.00
7	-0	-1224	-1010	1224	0	2494	105009	0.02	0.00	40.00
8	-0	-1665	-1520	1665	0	3753	105009	0.04	0.00	40.00
9	-0	-1199	-973	1199	0	2403	105009	0.02	0.00	40.00
10	-0	-1557	-1408	1557	0	3477	105009	0.03	0.00	40.00
11	-0	-1418	-1244	1418	0	3072	105009	0.03	0.00	40.00
12	-0	-1472	-1286	1472	0	3175	105009	0.03	0.00	40.00
13	-0	-1332	-1122	1332	0	2770	105009	0.03	0.00	40.00
14	-0	-1690	-1557	1690	0	3844	105009	0.04	0.00	40.00
15	-0	-1224	-1010	1224	0	2494	105009	0.02	0.00	40.00
16	-0	-1665	-1520	1665	0	3753	105009	0.04	0.00	40.00
17	-0	-1199	-973	1199	0	2403	105009	0.02	0.00	40.00

CONFRONTO E SINTESI CONCLUSIVE (si assume in ogni caso passo <= 15 cm)

I.R.compr.	Ashy	Ashz	PASSO	Nota
	cmq		cm	
0.04	--	--	15.00	**VERIFICATO**

ASTA NUM. 55 NI 122 NF 165 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 24B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-11440	1	-410	0	-809	132	6.28	6.28	9.42	9.42	3	0.04	0.01	0.05	0.00	0.00	24.0
2	0	-8824	50	-420	0	-824	-39	6.28	6.28	9.42	9.42	2	0.05	0.01	0.05	0.00	0.00	24.0
3	0	-8809	49	-275	0	-540	-38	6.28	6.28	9.42	9.42	2	0.03	0.01	0.03	0.00	0.00	24.0
4	0	-8784	-47	-356	0	-705	240	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
5	0	-8770	-48	-210	0	-421	242	6.28	6.28	9.42	9.42	2	0.04	0.00	0.03	0.00	0.00	24.0
6	0	-8828	17	-568	0	-1114	56	6.28	6.28	9.42	9.42	2	0.07	0.01	0.07	0.00	0.00	24.0
7	0	-8778	14	-82	0	-167	62	6.28	6.28	9.42	9.42	2	0.01	0.00	0.01	0.00	0.00	24.0
8	0	-8816	-12	-549	0	-1079	140	6.28	6.28	9.42	9.42	2	0.07	0.01	0.07	0.00	0.00	24.0
9	0	-8766	-15	-62	0	-131	146	6.28	6.28	9.42	9.42	2	0.02	0.00	0.01	0.00	0.00	24.0
10	0	-8824	50	-420	0	-824	-39	6.28	6.28	9.42	9.42	2	0.05	0.01	0.05	0.00	0.00	24.0
11	0	-8809	49	-275	0	-540	-38	6.28	6.28	9.42	9.42	2	0.03	0.01	0.03	0.00	0.00	24.0
12	0	-8784	-47	-356	0	-705	240	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
13	0	-8770	-48	-210	0	-421	242	6.28	6.28	9.42	9.42	2	0.04	0.00	0.03	0.00	0.00	24.0
14	0	-8828	17	-568	0	-1114	56	6.28	6.28	9.42	9.42	2	0.07	0.01	0.07	0.00	0.00	24.0
15	0	-8778	14	-82	0	-167	62	6.28	6.28	9.42	9.42	2	0.01	0.00	0.01	0.00	0.00	24.0
16	0	-8816	-12	-549	0	-1079	140	6.28	6.28	9.42	9.42	2	0.07	0.01	0.07	0.00	0.00	24.0
17	0	-8766	-15	-62	0	-131	146	6.28	6.28	9.42	9.42	2	0.02	0.00	0.01	0.00	0.00	24.0
18	0	-12390	130	-887	0	-1733	-229	6.28	6.28	9.42	9.42	3	0.08	0.02	0.10	0.00	0.00	24.0
19	0	-12290	-164	-650	0	-1285	610	6.28	6.28	9.42	9.42	3	0.08	0.01	0.07	0.00	0.00	24.0
20	0	-12310	-15	-384	0	-757	183	6.28	6.28	9.42	9.42	3	0.04	0.01	0.04	0.00	0.00	24.0
37	0	-11980	234	-850	0	-1655	-528	6.28	6.28	9.42	9.42	3	0.09	0.02	0.10	0.00	0.00	24.0
38	0	-11820	-257	-455	0	-909	870	6.28	6.28	9.42	9.42	3	0.09	0.01	0.05	0.00	0.00	24.0
39	0	-11850	-8	-12	0	-29	159	6.28	6.28	9.42	9.42	3	0.02	0.00	0.00	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	97	-10868	1	-410	0	-410	133	6.28	6.28	9.42	9.42	3	0.02	0.01	0.05	0.00	0.00	24.0
2	97	-8385	50	-420	0	-414	9	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
3	97	-8370	49	-275	0	-272	10	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
4	97	-8345	-47	-356	0	-358	194	6.28	6.28	9.42	9.42	2	0.04	0.01	0.04	0.00	0.00	24.0
5	97	-8331	-48	-210	0	-216	195	6.28	6.28	9.42	9.42	2	0.03	0.00	0.03	0.00	0.00	24.0
6	97	-8389	17	-568	0	-560	73	6.28	6.28	9.42	9.42	2	0.04	0.01	0.07	0.00	0.00	24.0
7	97	-8339	14	-82	0	-87	76	6.28	6.28	9.42	9.42	2	0.01	0.00	0.01	0.00	0.00	24.0
8	97	-8377	-12	-549	0	-544	128	6.28	6.28	9.42	9.42	2	0.04	0.01	0.07	0.00	0.00	24.0
9	97	-8327	-15	-62	0	-70	131	6.28	6.28	9.42	9.42	2	0.02	0.00	0.01	0.00	0.00	24.0
10	97	-8385	50	-420	0	-414	9	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
11	97	-8370	49	-275	0	-272	10	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
12	97	-8345	-47	-356	0	-358	194	6.28	6.28	9.42	9.42	2	0.04	0.01	0.04	0.00	0.00	24.0
13	97	-8331	-48	-210	0	-216	195	6.28	6.28	9.42	9.42	2	0.03	0.00	0.03	0.00	0.00	24.0
14	97	-8389	17	-568	0	-560	73	6.28	6.28	9.42	9.42	2	0.04	0.01	0.07	0.00	0.00	24.0
15	97	-8339	14	-82	0	-87	76	6.28	6.28	9.42	9.42	2	0.01	0.00	0.01	0.00	0.00	24.0
16	97	-8377	-12	-549	0	-544	128	6.28	6.28	9.42	9.42	2	0.04	0.01	0.07	0.00	0.00	24.0
17	97	-8327	-15	-62	0	-70	131	6.28	6.28	9.42	9.42	2	0.02	0.00	0.01	0.00	0.00	24.0
18	97	-11820	130	-887	0	-868	-102	6.28	6.28	9.42	9.42	3	0.04	0.02	0.10	0.00	0.00	24.0
19	97	-11720	-164	-650	0	-651	450	6.28	6.28	9.42	9.42	3	0.05	0.01	0.07	0.00	0.00	24.0
20	97	-11740	-15	-384	0	-382	168	6.28	6.28	9.42	9.42	3	0.02	0.01	0.04	0.00	0.00	24.0
37	97	-11411	234	-850	0	-826	-300	6.28	6.28	9.42	9.42	3	0.05	0.02	0.10	0.00	0.00	24.0
38	97	-11250	-257	-455	0	-465	620	6.28	6.28	9.42	9.42	3	0.06	0.01	0.05	0.00	0.00	24.0
39	97	-11280	-8	-12	0	-17	151	6.28	6.28	9.42	9.42	3	0.02	0.00	0.00	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	195	-10297	1	-410	0	-10	134	6.28	6.28	9.42	9.42	3	0.01	0.01	0.05	0.00	0.00	24.0
2	195	-7946	50	-420	0	-4	58	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
3	195	-7932	49	-275	0	-4	58	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
4	195	-7906	-47	-356	0	-12	148	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
5	195	-7892	-48	-210	0	-12	148	6.28	6.28	9.42	9.42	2	0.02	0.00	0.03	0.00	0.00	24.0
6	195	-7950	17	-568	0	-7	89	6.28	6.28	9.42	9.42	2	0.01	0.01	0.07	0.00	0.00	24.0
7	195	-7900	14	-82	0	-7	90	6.28	6.28	9.42	9.42	2	0.01	0.00	0.01	0.00	0.00	24.0
8	195	-7938	-12	-549	0	-9	116	6.28	6.28	9.42	9.42	2	0.01	0.01	0.07	0.00	0.00	24.0
9	195	-7888	-15	-62	0	-10	117	6.28	6.28	9.42	9.42	2	0.01	0.00	0.01	0.00	0.00	24.0
10	195	-7946	50	-420	0	-4	58	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
11	195	-7932	49	-275	0	-4	58	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
12	195	-7906	-47	-356	0	-12	148	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
13	195	-7892	-48	-210	0	-12	148	6.28	6.28	9.42	9.42	2	0.02	0.00	0.03	0.00	0.00	24.0
14	195	-7950	17	-568	0	-7	89	6.28	6.28	9.42	9.42	2	0.01	0.01	0.07	0.00	0.00	24.0
15	195	-7900	14	-82	0	-7	90	6.28	6.28	9.42	9.42	2	0.01	0.00	0.01	0.00	0.00	24.0
16	195	-7938	-12	-549	0	-9	116	6.28	6.28	9.42	9.42	2	0.01	0.01	0.07	0.00	0.00	24.0
17	195	-7888	-15	-62	0	-10	117	6.28	6.28	9.42	9.42	2	0.01	0.00	0.01	0.00	0.00	24.0
18	195	-11250	130	-887	0	-3	25	6.28	6.28	9.42	9.42	3	0.00	0.02	0.10	0.00	0.00	24.0
19	195	-11150	-164	-650	0	-17	289	6.28	6.28	9.42	9.42	3	0.03	0.01	0.07	0.00	0.00	24.0
20	195	-11170	-15	-384	0	-7	153	6.28	6.28	9.42	9.42	3	0.02	0.01	0.04	0.00	0.00	24.0
37	195	-10842	234	-850	0	3	-71	6.28	6.28	9.42	9.42	3	0.01	0.02	0.10	0.00	0.00	24.0
38	195	-10680	-257	-455	0	-21	370	6.28	6.28	9.42	9.42	3	0.04	0.01	0.05	0.00	0.00	24.0

39	195	-10711	-8	-12	0	-5	143	6.28	6.28	9.42	9.42	3	0.01	0.00	0.00	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	292	-9726	1	-410	0	389	135	6.28	6.28	9.42	9.42	3	0.02	0.01	0.05	0.00	0.00	24.0
2	292	-7508	50	-420	0	406	106	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
3	292	-7493	49	-275	0	263	106	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
4	292	-7468	-47	-356	0	335	102	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
5	292	-7454	-48	-210	0	193	101	6.28	6.28	9.42	9.42	2	0.02	0.00	0.03	0.00	0.00	24.0
6	292	-7512	17	-568	0	547	105	6.28	6.28	9.42	9.42	2	0.04	0.01	0.07	0.00	0.00	24.0
7	292	-7462	14	-82	0	73	103	6.28	6.28	9.42	9.42	2	0.01	0.00	0.01	0.00	0.00	24.0
8	292	-7500	-12	-549	0	526	104	6.28	6.28	9.42	9.42	2	0.04	0.01	0.07	0.00	0.00	24.0
9	292	-7450	-15	-62	0	51	102	6.28	6.28	9.42	9.42	2	0.01	0.00	0.01	0.00	0.00	24.0
10	292	-7508	50	-420	0	406	106	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
11	292	-7493	49	-275	0	263	106	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
12	292	-7468	-47	-356	0	335	102	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
13	292	-7454	-48	-210	0	193	101	6.28	6.28	9.42	9.42	2	0.02	0.00	0.03	0.00	0.00	24.0
14	292	-7512	17	-568	0	547	105	6.28	6.28	9.42	9.42	2	0.04	0.01	0.07	0.00	0.00	24.0
15	292	-7462	14	-82	0	73	103	6.28	6.28	9.42	9.42	2	0.01	0.00	0.01	0.00	0.00	24.0
16	292	-7500	-12	-549	0	526	104	6.28	6.28	9.42	9.42	2	0.04	0.01	0.07	0.00	0.00	24.0
17	292	-7450	-15	-62	0	51	102	6.28	6.28	9.42	9.42	2	0.01	0.00	0.01	0.00	0.00	24.0
18	292	-10680	130	-887	0	863	151	6.28	6.28	9.42	9.42	3	0.04	0.02	0.10	0.00	0.00	24.0
19	292	-10580	-164	-650	0	617	129	6.28	6.28	9.42	9.42	3	0.03	0.01	0.08	0.00	0.00	24.0
20	292	-10600	-15	-384	0	368	138	6.28	6.28	9.42	9.42	3	0.02	0.01	0.04	0.00	0.00	24.0
37	292	-10272	234	-850	0	832	157	6.28	6.28	9.42	9.42	3	0.04	0.02	0.10	0.00	0.00	24.0
38	292	-10109	-257	-455	0	423	120	6.28	6.28	9.42	9.42	3	0.02	0.01	0.05	0.00	0.00	24.0
39	292	-10142	-8	-12	0	7	135	6.28	6.28	9.42	9.42	3	0.01	0.00	0.00	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	390	-9154	1	-410	0	789	136	6.28	6.28	9.42	9.42	3	0.04	0.01	0.05	0.00	0.00	24.0
2	390	-7069	50	-420	0	816	155	6.28	6.28	9.42	9.42	2	0.06	0.01	0.05	0.00	0.00	24.0
3	390	-7054	49	-275	0	531	153	6.28	6.28	9.42	9.42	2	0.04	0.01	0.03	0.00	0.00	24.0
4	390	-7029	-47	-356	0	682	56	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
5	390	-7015	-48	-210	0	397	55	6.28	6.28	9.42	9.42	2	0.03	0.00	0.03	0.00	0.00	24.0
6	390	-7073	17	-568	0	1101	122	6.28	6.28	9.42	9.42	2	0.08	0.01	0.07	0.00	0.00	24.0
7	390	-7023	14	-82	0	152	117	6.28	6.28	9.42	9.42	2	0.02	0.00	0.01	0.00	0.00	24.0
8	390	-7061	-12	-549	0	1061	92	6.28	6.28	9.42	9.42	2	0.07	0.01	0.07	0.00	0.00	24.0
9	390	-7011	-15	-62	0	112	88	6.28	6.28	9.42	9.42	2	0.01	0.00	0.01	0.00	0.00	24.0
10	390	-7069	50	-420	0	816	155	6.28	6.28	9.42	9.42	2	0.06	0.01	0.05	0.00	0.00	24.0
11	390	-7054	49	-275	0	531	153	6.28	6.28	9.42	9.42	2	0.04	0.01	0.03	0.00	0.00	24.0
12	390	-7029	-47	-356	0	682	56	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
13	390	-7015	-48	-210	0	397	55	6.28	6.28	9.42	9.42	2	0.03	0.00	0.03	0.00	0.00	24.0
14	390	-7073	17	-568	0	1101	122	6.28	6.28	9.42	9.42	2	0.08	0.01	0.07	0.00	0.00	24.0
15	390	-7023	14	-82	0	152	117	6.28	6.28	9.42	9.42	2	0.02	0.00	0.01	0.00	0.00	24.0
16	390	-7061	-12	-549	0	1061	92	6.28	6.28	9.42	9.42	2	0.07	0.01	0.07	0.00	0.00	24.0
17	390	-7011	-15	-62	0	112	88	6.28	6.28	9.42	9.42	2	0.01	0.00	0.01	0.00	0.00	24.0
18	390	-10110	130	-887	0	1728	278	6.28	6.28	9.42	9.42	3	0.08	0.02	0.10	0.00	0.00	24.0
19	390	-10010	-164	-650	0	1251	-31	6.28	6.28	9.42	9.42	3	0.06	0.01	0.08	0.00	0.00	24.0
20	390	-10030	-15	-384	0	742	123	6.28	6.28	9.42	9.42	3	0.04	0.01	0.05	0.00	0.00	24.0
37	390	-9703	234	-850	0	1661	385	6.28	6.28	9.42	9.42	3	0.09	0.02	0.10	0.00	0.00	24.0
38	390	-9539	-257	-455	0	867	-130	6.28	6.28	9.42	9.42	3	0.04	0.01	0.05	0.00	0.00	24.0
39	390	-9572	-8	-12	0	19	126	6.28	6.28	9.42	9.42	3	0.01	0.00	0.00	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

VERIFICA NODO IN TESTA AL PILASTRO, NODO NUM. 165 NON CONFINATO

(par.7.2.2 NTC2018 "La domanda di resistenza valutata con i criteri della progettazione in capacità può essere assunta non superiore alla domanda di resistenza valutata per il caso di comportamento strutturale non dissipativo.")

PROGETTAZIONE IN CAPACITA'

Asse loc. pilastro y nodo: --

Asse loc. pilastro z nodo INTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 30.0 cm, hjc= 50.0 cm

FxMin,inf	FxMin,sup	FxMax,sup	FySup	FzSup	Vjbdy	Vjbdz	Vres,y	Vres,z	I.R.compr.	Ashy	Ashz	PASSO	Nota
daN					daN		daN			cmq		cm	
-7011	1	-0	0	0	--	35233	--	131261	0.27	--	8.55	5.33	

VERIFICA DI RESISTENZA CON SOLLECITAZIONI COMPORTAMENTO NON DISSIPATIVO

Asse loc. pilastro z nodo INTERNO: Hjw= 40.0 cm, bj= 30.0 cm, hjc= 50.0 cm, db1= 45.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb,1	Mb,2	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-0	-7069	-2799	-1984	0	2012	131261	0.02	0.00	40.00	
3	-0	-7054	-2645	-2114	0	1311	131261	0.01	0.00	40.00	
4	-0	-7029	-2695	-2013	0	1684	131261	0.01	0.00	40.00	
5	-0	-7015	-2541	-2144	0	980	131261	0.01	0.00	40.00	
6	-0	-7073	-2943	-1842	0	2719	131261	0.02	0.00	40.00	
7	-0	-7023	-2429	-2277	0	375	131261	0.00	0.00	40.00	
8	-0	-7061	-2912	-1851	0	2620	131261	0.02	0.00	40.00	
9	-0	-7011	-2398	-2285	0	279	131261	0.00	0.00	40.00	
10	-0	-7069	-2799	-1984	0	2012	131261	0.02	0.00	40.00	
11	-0	-7054	-2645	-2114	0	1311	131261	0.01	0.00	40.00	
12	-0	-7029	-2695	-2013	0	1684	131261	0.01	0.00	40.00	
13	-0	-7015	-2541	-2144	0	980	131261	0.01	0.00	40.00	
14	-0	-7073	-2943	-1842	0	2719	131261	0.02	0.00	40.00	
15	-0	-7023	-2429	-2277	0	375	131261	0.00	0.00	40.00	
16	-0	-7061	-2912	-1851	0	2620	131261	0.02	0.00	40.00	
17	-0	-7011	-2398	-2285	0	279	131261	0.00	0.00	40.00	

CONFRONTO E SINTESI CONCLUSIVE (si assume in ogni caso passo <= 15 cm)

I.R.compr.	Ashy	Ashz	PASSO	Nota
	cmq		cm	
0.02	--	--	15.00	**VERIFICATO**

ASTA NUM. 56 NI 209 NF 210 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 23B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza			aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx		cmq/m		cm
1	0	-7554	114	-861	0	-1182	-53	6.28	6.28	9.42	9.42	3	0.06	0.02	0.11	0.00	0.00		24.0
2	0	-5899	117	-731	0	-1064	-105	6.28	6.28	9.42	9.42	2	0.07	0.02	0.09	0.00	0.00		24.0
3	0	-5822	120	-628	0	-832	-111	6.28	6.28	9.42	9.42	2	0.06	0.01	0.08	0.00	0.00		24.0
4	0	-5800	55	-697	0	-986	30	6.28	6.28	9.42	9.42	2	0.06	0.02	0.09	0.00	0.00		24.0
5	0	-5723	58	-594	0	-754	24	6.28	6.28	9.42	9.42	2	0.05	0.01	0.07	0.00	0.00		24.0
6	0	-5954	92	-839	0	-1307	-51	6.28	6.28	9.42	9.42	2	0.09	0.02	0.11	0.00	0.00		24.0
7	0	-5697	102	-496	0	-535	-71	6.28	6.28	9.42	9.42	2	0.04	0.01	0.06	0.00	0.00		24.0
8	0	-5924	74	-829	0	-1284	-10	6.28	6.28	9.42	9.42	2	0.08	0.02	0.10	0.00	0.00		24.0
9	0	-5667	83	-486	0	-511	-30	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00		24.0
10	0	-5899	117	-731	0	-1064	-105	6.28	6.28	9.42	9.42	2	0.07	0.02	0.09	0.00	0.00		24.0
11	0	-5822	120	-628	0	-832	-111	6.28	6.28	9.42	9.42	2	0.06	0.01	0.08	0.00	0.00		24.0
12	0	-5800	55	-697	0	-986	30	6.28	6.28	9.42	9.42	2	0.06	0.02	0.09	0.00	0.00		24.0
13	0	-5723	58	-594	0	-754	24	6.28	6.28	9.42	9.42	2	0.05	0.01	0.07	0.00	0.00		24.0
14	0	-5954	92	-839	0	-1307	-51	6.28	6.28	9.42	9.42	2	0.09	0.02	0.11	0.00	0.00		24.0
15	0	-5697	102	-496	0	-535	-71	6.28	6.28	9.42	9.42	2	0.04	0.01	0.06	0.00	0.00		24.0
16	0	-5924	74	-829	0	-1284	-10	6.28	6.28	9.42	9.42	2	0.08	0.02	0.10	0.00	0.00		24.0
17	0	-5667	83	-486	0	-511	-30	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00		24.0
18	0	-8255	190	-1227	0	-1936	-219	6.28	6.28	9.42	9.42	3	0.09	0.03	0.15	0.00	0.00		24.0
19	0	-7930	10	-1088	0	-1620	175	6.28	6.28	9.42	9.42	3	0.08	0.03	0.13	0.00	0.00		24.0
20	0	-7895	114	-882	0	-1163	-50	6.28	6.28	9.42	9.42	3	0.06	0.02	0.11	0.00	0.00		24.0
37	0	-8123	254	-1167	0	-1836	-360	6.28	6.28	9.42	9.42	3	0.09	0.03	0.14	0.00	0.00		24.0
38	0	-7581	-45	-935	0	-1309	295	6.28	6.28	9.42	9.42	3	0.07	0.02	0.11	0.00	0.00		24.0
39	0	-7524	128	-592	0	-547	-80	6.28	6.28	9.42	9.42	3	0.03	0.01	0.07	0.00	0.00		24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	97	-6984	114	-861	0	-342	58	6.28	6.28	9.42	9.42	3	0.02	0.02	0.11	0.00	0.00		24.0
2	97	-5460	117	-731	0	-351	9	6.28	6.28	9.42	9.42	2	0.02	0.02	0.09	0.00	0.00		24.0
3	97	-5383	120	-628	0	-220	6	6.28	6.28	9.42	9.42	2	0.01	0.01	0.08	0.00	0.00		24.0
4	97	-5361	55	-697	0	-306	84	6.28	6.28	9.42	9.42	2	0.02	0.02	0.09	0.00	0.00		24.0
5	97	-5284	58	-594	0	-175	81	6.28	6.28	9.42	9.42	2	0.02	0.01	0.08	0.00	0.00		24.0
6	97	-5515	92	-839	0	-489	39	6.28	6.28	9.42	9.42	2	0.03	0.02	0.11	0.00	0.00		24.0
7	97	-5258	102	-496	0	-51	28	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00		24.0
8	97	-5485	74	-829	0	-476	62	6.28	6.28	9.42	9.42	2	0.03	0.02	0.10	0.00	0.00		24.0
9	97	-5228	83	-486	0	-37	51	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00		24.0
10	97	-5460	117	-731	0	-351	9	6.28	6.28	9.42	9.42	2	0.02	0.02	0.09	0.00	0.00		24.0
11	97	-5383	120	-628	0	-220	6	6.28	6.28	9.42	9.42	2	0.01	0.01	0.08	0.00	0.00		24.0
12	97	-5361	55	-697	0	-306	84	6.28	6.28	9.42	9.42	2	0.02	0.02	0.09	0.00	0.00		24.0
13	97	-5284	58	-594	0	-175	81	6.28	6.28	9.42	9.42	2	0.02	0.01	0.08	0.00	0.00		24.0
14	97	-5515	92	-839	0	-489	39	6.28	6.28	9.42	9.42	2	0.03	0.02	0.11	0.00	0.00		24.0
15	97	-5258	102	-496	0	-51	28	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00		24.0
16	97	-5485	74	-829	0	-476	62	6.28	6.28	9.42	9.42	2	0.03	0.02	0.10	0.00	0.00		24.0
17	97	-5228	83	-486	0	-37	51	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00		24.0
18	97	-7684	190	-1227	0	-740	-33	6.28	6.28	9.42	9.42	3	0.04	0.03	0.15	0.00	0.00		24.0
19	97	-7360	10	-1088	0	-559	185	6.28	6.28	9.42	9.42	3	0.03	0.03	0.13	0.00	0.00		24.0
20	97	-7325	114	-882	0	-302	61	6.28	6.28	9.42	9.42	3	0.02	0.02	0.11	0.00	0.00		24.0
37	97	-7552	254	-1167	0	-699	-112	6.28	6.28	9.42	9.42	3	0.03	0.03	0.14	0.00	0.00		24.0
38	97	-7011	-45	-935	0	-398	251	6.28	6.28	9.42	9.42	3	0.03	0.02	0.12	0.00	0.00		24.0
39	97	-6954	128	-592	0	30	44	6.28	6.28	9.42	9.42	3	0.00	0.01	0.07	0.00	0.00		24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	195	-6413	114	-861	0	498	169	6.28	6.28	9.42	9.42	3	0.03	0.02	0.11	0.00	0.00		24.0
2	195	-5022	117	-731	0	362	123	6.28	6.28	9.42	9.42	2	0.03	0.02	0.09	0.00	0.00		24.0
3	195	-4944	120	-628	0	392	123	6.28	6.28	9.42	9.42	2	0.03	0.01	0.08	0.00	0.00		24.0
4	195	-4922	55	-697	0	373	138	6.28	6.28	9.42	9.42	2	0.03	0.02	0.09	0.00	0.00		24.0
5	195	-4846	58	-594	0	404	137	6.28	6.28	9.42	9.42	2	0.04	0.01	0.08	0.00	0.00		24.0
6	195	-5076	92	-839	0	329	129	6.28	6.28	9.42	9.42	2	0.03	0.02	0.11	0.00	0.00		24.0
7	195	-4820	102	-496	0	433	127	6.28	6.28	9.42	9.42	2	0.04	0.01	0.06	0.00	0.00		24.0
8	195	-5046	74	-829	0	332	133	6.28	6.28	9.42	9.42	2	0.03	0.02	0.11	0.00	0.00		24.0
9	195	-4790	83	-486	0	436	132	6.28	6.28	9.42	9.42	2	0.04	0.01	0.06	0.00	0.00		24.0
10	195	-5022	117	-731	0	362	123	6.28	6.28	9.42	9.42	2	0.03	0.02	0.09	0.00	0.00		24.0
11	195	-4944	120	-628	0	392	123	6.28	6.28	9.42	9.42	2	0.03	0.01	0.08	0.00	0.00		24.0
12	195	-4922	55	-697	0	373	138	6.28	6.28	9.42	9.42	2	0.03	0.02	0.09	0.00	0.00		24.0
13	195	-4846	58	-594	0	404	137	6.28	6.28	9.42	9.42	2	0.04	0.01	0.08	0.00	0.00		24.0
14	195	-5076	92	-839	0	329	129	6.28	6.28	9.42	9.42	2	0.03	0.02	0.11	0.00	0.00		24.0
15	195	-4820	102	-496	0	433	127	6.28	6.28	9.42	9.42	2	0.04	0.01	0.06	0.00	0.00		24.0
16	195	-5046	74	-829	0	332	133	6.28	6.28	9.42	9.42	2	0.03	0.02	0.11	0.00	0.00		24.0
17	195	-4790	83	-486	0	436	132	6.28	6.28	9.42	9.42	2	0.04	0.01	0.06	0.00	0.00		24.0
18	195	-7114	190	-1227	0	457	152	6.28	6.28	9.42	9.42	3	0.03	0.03	0.15	0.00	0.00		24.0
19	195	-6789	10	-1088	0	502	195	6.28	6.28	9.42	9.42	3	0.03	0.03	0.13	0.00	0.00		24.0
20	195	-6754	114	-882	0	558	171	6.28	6.28	9.42	9.42	3	0.03	0.02	0.11	0.00	0.00		24.0
37	195	-6982	254	-1167	0	439	136	6.28	6.28	9.42	9.42	3	0.03	0.03	0.14	0.00	0.00		24.0
38	195	-6440	-45	-935	0	514	208	6.28	6.28	9.42	9.42	3	0.03	0.02	0.12	0.00	0.00		24.0
39	195	-6383	128	-592	0	607	169	6.28	6.28	9.42	9.42	3	0.03	0.01	0.07	0.00	0.00		24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	292	-5842	114	-861	0	1337	280	6.28	6.28	9.42	9.42	3	0.07	0.02	0.11	0.00	0.00		24.0
2	292	-4583	117	-731	0	1074	237	6.28	6.28	9.42	9.42	2	0.08	0.02	0.09	0.00	0.00		24.0
3	292	-4506	120	-628	0	1005	239	6.28	6.28	9.42	9.42	2	0.08	0.01	0.08	0.00	0.00		24.0
4	292	-4484	55	-697	0	1053	192	6.28	6.28	9.42	9.42	2	0.08	0.02	0.09	0.00	0.00		24.0
5	292	-4407	58	-594	0	984	194	6.28	6.28	9.42	9.42	2	0.08	0.01	0.08	0.00	0.00		24.0
6	292	-4638	92	-839	0	1148	219	6.28	6.28	9.42	9.42	2	0.09	0.02	0.11	0.00	0.00		24.0
7	292	-4381	102	-496	0	916	226	6.28	6.28	9.42	9.42	2	0.07	0.01	0.06	0.00	0.00		24.0
8	292	-4608	74	-829	0	1141	205	6.28	6.28	9.42	9.42	2	0.09	0.02	0.11	0.00	0.00		24.0
9	292	-4351	83	-486	0	910	212	6.28	6.28	9.42	9.42	2	0.07	0.01	0.06	0.00	0.00		24.0
10	292	-4583	117	-731	0	1074	237	6.28	6.28	9.42	9.42	2	0.08	0.02	0.09	0.00	0.00		24.0
11	292	-4506	120	-628	0	1005	239	6.28	6.28	9.42	9.42	2	0.08	0.01	0.08	0.00	0.00		24.0
12	292	-4484	55	-697	0	1053	192	6.28	6.28	9.42	9.42	2	0.08	0.02	0.09	0.00	0.00		24.0
13	292	-4407	58	-594	0	984	194	6.28	6.28	9.42	9.42	2	0.08	0.01	0.08	0.00	0.00		24.0
14	292	-4638	92	-839	0	1148	219	6.28	6.28	9.42	9.42	2	0.09	0.02	0.11	0.00	0.00		24.0
15	292	-4381	102	-496	0	916	226	6.28	6.28	9.42	9.42	2	0.07	0.01	0.06	0.00	0.00		24.0
16	292	-4608	74	-829	0	1141	205	6.28	6.28	9.42	9.42	2	0.09	0.02	0.11	0.00	0.00		24.0
17	292	-4351	83	-486	0	910	212	6.28	6.28	9.42	9.42	2	0.07	0.01	0.06	0.00	0.00		24.0
18	292	-6544	190	-1227	0	1654	337	6.28	6.28	9.42	9.42	3	0.09	0.03	0.15	0.00	0.00		24.0
19	292	-6218	10	-1088	0	1564	205	6.28	6.28	9.42	9.42	3	0.08	0.03	0.14	0.00	0.00		24.0
20	292	-6184	114	-882	0	1418	282	6.28	6.28	9.42	9.42	3	0.07	0.02	0.11	0.00	0.00		24.0
37	292	-6412	254	-1167	0	1576	384	6.28	6.28	9.42	9.42	3	0.09	0.03	0.15	0.00	0.00		24.0
38	292	-5870	-45	-935	0	1426	164	6.28	6.28	9.42	9.42	3	0.07	0.02	0.12	0.00	0.00		24.0
39	292	-5812	128	-592	0	1183	293	6.28	6.28	9.42	9.42	3	0.06	0.01	0.07	0.00	0.00		24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	390	-5272	114	-861	0	2177	391	6.28	6.28	9.42	9.42	3	0.11	0.02	0.11	0.00	0.00	24.0
2	390	-4144	117	-731	0	1787	351	6.28	6.28	9.42	9.42	2	0.14	0.02	0.09	0.00	0.00	24.0
3	390	-4067	120	-628	0	1617	356	6.28	6.28	9.42	9.42	2	0.13	0.01	0.08	0.00	0.00	24.0
4	390	-4045	55	-697	0	1733	245	6.28	6.28	9.42	9.42	2	0.13	0.02	0.09	0.00	0.00	24.0
5	390	-3968	58	-594	0	1563	250	6.28	6.28	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
6	390	-4199	92	-839	0	1966	308	6.28	6.28	9.42	9.42	2	0.15	0.02	0.11	0.00	0.00	24.0
7	390	-3942	102	-496	0	1400	325	6.28	6.28	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
8	390	-4169	74	-829	0	1949	277	6.28	6.28	9.42	9.42	2	0.14	0.02	0.11	0.00	0.00	24.0
9	390	-3912	83	-486	0	1384	293	6.28	6.28	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
10	390	-4144	117	-731	0	1787	351	6.28	6.28	9.42	9.42	2	0.14	0.02	0.09	0.00	0.00	24.0
11	390	-4067	120	-628	0	1617	356	6.28	6.28	9.42	9.42	2	0.13	0.01	0.08	0.00	0.00	24.0
12	390	-4045	55	-697	0	1733	245	6.28	6.28	9.42	9.42	2	0.13	0.02	0.09	0.00	0.00	24.0
13	390	-3968	58	-594	0	1563	250	6.28	6.28	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
14	390	-4199	92	-839	0	1966	308	6.28	6.28	9.42	9.42	2	0.15	0.02	0.11	0.00	0.00	24.0
15	390	-3942	102	-496	0	1400	325	6.28	6.28	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
16	390	-4169	74	-829	0	1949	277	6.28	6.28	9.42	9.42	2	0.14	0.02	0.11	0.00	0.00	24.0
17	390	-3912	83	-486	0	1384	293	6.28	6.28	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
18	390	-5973	190	-1227	0	2850	522	6.28	6.28	9.42	9.42	3	0.15	0.03	0.15	0.00	0.00	24.0
19	390	-5648	10	-1088	0	2625	215	6.28	6.28	9.42	9.42	3	0.13	0.03	0.14	0.00	0.00	24.0
20	390	-5614	114	-882	0	2279	393	6.28	6.28	9.42	9.42	3	0.12	0.02	0.11	0.00	0.00	24.0
37	390	-5841	254	-1167	0	2713	632	6.28	6.28	9.42	9.42	3	0.15	0.03	0.15	0.00	0.00	24.0
38	390	-5300	-45	-935	0	2337	121	6.28	6.28	9.42	9.42	3	0.11	0.02	0.12	0.00	0.00	24.0
39	390	-5242	128	-592	0	1760	417	6.28	6.28	9.42	9.42	3	0.10	0.01	0.08	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

VERIFICA NODO IN TESTA AL PILASTRO, NODO NUM. 210 NON CONFINATO

(par.7.2.2 NTC2018 "La domanda di resistenza valutata con i criteri della progettazione in capacità può essere assunta non superiore alla domanda di resistenza valutata per il caso di comportamento strutturale non dissipativo.")

PROGETTAZIONE IN CAPACITA'

Asse loc. pilastro y nodo ESTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 45.0 cm, hjc= 20.0 cm
Asse loc. pilastro z nodo ESTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 30.0 cm, hjc= 50.0 cm

FxMin,inf	FxMin,sup	FxMax,sup	FySup	FzSup	Vjbdy	Vjbdz	Vres,y	Vres,z	I.R.compr.	Ashy	Ashz	PASSO	Nota
daN					daN		daN			cmq		cm	
-3912	1	-0	0	0	17616	17616	63005	105009	0.28	4.38	--	11.93	

VERIFICA DI RESISTENZA CON SOLLECITAZIONI COMPORTAMENTO NON DISSIPATIVO

Asse loc. pilastro y nodo ESTERNO: Hjw= 40.0 cm, bj= 45.0 cm, hjc= 20.0 cm, db1= 45.0 cm

NC	Fx,sup	Fx,inf	Mb	Vb	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-0	-4144	-447	934	0	1103	63005	0.02	0.00	40.00	
3	-0	-4067	-451	935	0	1114	63005	0.02	0.00	40.00	
4	-0	-4045	-231	856	0	570	63005	0.01	0.00	40.00	
5	-0	-3968	-235	858	0	581	63005	0.01	0.00	40.00	
6	-0	-4199	-366	905	0	904	63005	0.01	0.00	40.00	
7	-0	-3942	-381	910	0	940	63005	0.01	0.00	40.00	
8	-0	-4169	-301	882	0	744	63005	0.01	0.00	40.00	
9	-0	-3912	-316	887	0	780	63005	0.01	0.00	40.00	
10	-0	-4144	-447	934	0	1103	63005	0.02	0.00	40.00	
11	-0	-4067	-451	935	0	1114	63005	0.02	0.00	40.00	
12	-0	-4045	-231	856	0	570	63005	0.01	0.00	40.00	
13	-0	-3968	-235	858	0	581	63005	0.01	0.00	40.00	
14	-0	-4199	-366	905	0	904	63005	0.01	0.00	40.00	
15	-0	-3942	-381	910	0	940	63005	0.01	0.00	40.00	
16	-0	-4169	-301	882	0	744	63005	0.01	0.00	40.00	
17	-0	-3912	-316	887	0	780	63005	0.01	0.00	40.00	

Asse loc. pilastro z nodo ESTERNO: Hjw= 40.0 cm, bj= 30.0 cm, hjc= 50.0 cm, db1= 45.0 cm

NC	Fx,sup	Fx,inf	Mb	Vb	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-0	-4144	-1740	3210	0	4296	105009	0.04	0.00	40.00	
3	-0	-4067	-1575	3132	0	3889	105009	0.04	0.00	40.00	
4	-0	-4045	-1687	3188	0	4165	105009	0.04	0.00	40.00	
5	-0	-3968	-1523	3110	0	3760	105009	0.04	0.00	40.00	
6	-0	-4199	-1914	3294	0	4726	105009	0.05	0.00	40.00	
7	-0	-3942	-1365	3032	0	3370	105009	0.03	0.00	40.00	
8	-0	-4169	-1898	3288	0	4686	105009	0.04	0.00	40.00	
9	-0	-3912	-1349	3025	0	3331	105009	0.03	0.00	40.00	
10	-0	-4144	-1740	3210	0	4296	105009	0.04	0.00	40.00	
11	-0	-4067	-1575	3132	0	3889	105009	0.04	0.00	40.00	
12	-0	-4045	-1687	3188	0	4165	105009	0.04	0.00	40.00	
13	-0	-3968	-1523	3110	0	3760	105009	0.04	0.00	40.00	
14	-0	-4199	-1914	3294	0	4726	105009	0.05	0.00	40.00	
15	-0	-3942	-1365	3032	0	3370	105009	0.03	0.00	40.00	
16	-0	-4169	-1898	3288	0	4686	105009	0.04	0.00	40.00	
17	-0	-3912	-1349	3025	0	3331	105009	0.03	0.00	40.00	

CONFRONTO E SINTESI CONCLUSIVE (si assume in ogni caso passo <= 15 cm)

I.R.compr.	Ashy	Ashz	PASSO	Nota
	cmq		cm	
0.05	--	--	15.00	**VERIFICATO**

ASTA NUM. 57 NI 142 NF 123 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 18B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m	cm

1	0	-13300	-97	-1214	0	-1201	129	6.28	6.28	12.57	12.57	3	0.04	0.02	0.12	0.00	0.00	24.0
2	0	-10250	-7	-953	0	-967	-50	6.28	6.28	12.57	12.57	2	0.05	0.02	0.09	0.00	0.00	24.0
3	0	-10200	-5	-900	0	-851	-54	6.28	6.28	12.57	12.57	2	0.04	0.02	0.09	0.00	0.00	24.0
4	0	-10260	-144	-969	0	-996	252	6.28	6.28	12.57	12.57	2	0.06	0.02	0.10	0.00	0.00	24.0
5	0	-10220	-142	-915	0	-881	248	6.28	6.28	12.57	12.57	2	0.05	0.02	0.09	0.00	0.00	24.0
6	0	-10300	-58	-1021	0	-1112	61	6.28	6.28	12.57	12.57	2	0.06	0.02	0.10	0.00	0.00	24.0
7	0	-10160	-50	-842	0	-727	47	6.28	6.28	12.57	12.57	2	0.04	0.01	0.08	0.00	0.00	24.0
8	0	-10310	-99	-1026	0	-1121	151	6.28	6.28	12.57	12.57	2	0.06	0.02	0.10	0.00	0.00	24.0
9	0	-10170	-91	-847	0	-736	137	6.28	6.28	12.57	12.57	2	0.04	0.01	0.08	0.00	0.00	24.0
10	0	-10250	-7	-953	0	-967	-50	6.28	6.28	12.57	12.57	2	0.05	0.02	0.09	0.00	0.00	24.0
11	0	-10200	-5	-900	0	-851	-54	6.28	6.28	12.57	12.57	2	0.04	0.02	0.09	0.00	0.00	24.0
12	0	-10260	-144	-969	0	-996	252	6.28	6.28	12.57	12.57	2	0.06	0.02	0.10	0.00	0.00	24.0
13	0	-10220	-142	-915	0	-881	248	6.28	6.28	12.57	12.57	2	0.05	0.02	0.09	0.00	0.00	24.0
14	0	-10300	-58	-1021	0	-1112	61	6.28	6.28	12.57	12.57	2	0.06	0.02	0.10	0.00	0.00	24.0
15	0	-10160	-50	-842	0	-727	47	6.28	6.28	12.57	12.57	2	0.04	0.01	0.08	0.00	0.00	24.0
16	0	-10310	-99	-1026	0	-1121	151	6.28	6.28	12.57	12.57	2	0.06	0.02	0.10	0.00	0.00	24.0
17	0	-10170	-91	-847	0	-736	137	6.28	6.28	12.57	12.57	2	0.04	0.01	0.08	0.00	0.00	24.0
18	0	-14090	80	-1383	0	-1431	-267	6.28	6.28	12.57	12.57	3	0.05	0.02	0.13	0.00	0.00	24.0
19	0	-14160	-323	-1454	0	-1570	623	6.28	6.28	12.57	12.57	3	0.07	0.02	0.14	0.00	0.00	24.0
20	0	-14190	-104	-1496	0	-1649	143	6.28	6.28	12.57	12.57	3	0.06	0.03	0.14	0.00	0.00	24.0
37	0	-13660	222	-1271	0	-1266	-579	6.28	6.28	12.57	12.57	3	0.05	0.02	0.12	0.00	0.00	24.0
38	0	-13790	-450	-1390	0	-1497	904	6.28	6.28	12.57	12.57	3	0.07	0.02	0.13	0.00	0.00	24.0
39	0	-13840	-85	-1460	0	-1630	104	6.28	6.28	12.57	12.57	3	0.06	0.03	0.14	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	97	-12540	-97	-1214	0	-17	34	6.28	6.28	12.57	12.57	3	0.00	0.02	0.12	0.00	0.00	24.0
2	97	-9664	-7	-953	0	-37	-57	6.28	6.28	12.57	12.57	2	0.00	0.02	0.10	0.00	0.00	24.0
3	97	-9616	-5	-900	0	26	-59	6.28	6.28	12.57	12.57	2	0.00	0.02	0.09	0.00	0.00	24.0
4	97	-9676	-144	-969	0	-52	111	6.28	6.28	12.57	12.57	2	0.01	0.02	0.10	0.00	0.00	24.0
5	97	-9636	-142	-915	0	11	110	6.28	6.28	12.57	12.57	2	0.01	0.02	0.09	0.00	0.00	24.0
6	97	-9715	-58	-1021	0	-116	4	6.28	6.28	12.57	12.57	2	0.01	0.02	0.10	0.00	0.00	24.0
7	97	-9576	-50	-842	0	95	-2	6.28	6.28	12.57	12.57	2	0.00	0.01	0.08	0.00	0.00	24.0
8	97	-9724	-99	-1026	0	-121	55	6.28	6.28	12.57	12.57	2	0.01	0.02	0.10	0.00	0.00	24.0
9	97	-9584	-91	-847	0	90	48	6.28	6.28	12.57	12.57	2	0.01	0.01	0.08	0.00	0.00	24.0
10	97	-9664	-7	-953	0	-37	-57	6.28	6.28	12.57	12.57	2	0.00	0.02	0.10	0.00	0.00	24.0
11	97	-9616	-5	-900	0	26	-59	6.28	6.28	12.57	12.57	2	0.00	0.02	0.09	0.00	0.00	24.0
12	97	-9676	-144	-969	0	-52	111	6.28	6.28	12.57	12.57	2	0.01	0.02	0.10	0.00	0.00	24.0
13	97	-9636	-142	-915	0	11	110	6.28	6.28	12.57	12.57	2	0.01	0.02	0.09	0.00	0.00	24.0
14	97	-9715	-58	-1021	0	-116	4	6.28	6.28	12.57	12.57	2	0.01	0.02	0.10	0.00	0.00	24.0
15	97	-9576	-50	-842	0	95	-2	6.28	6.28	12.57	12.57	2	0.00	0.01	0.08	0.00	0.00	24.0
16	97	-9724	-99	-1026	0	-121	55	6.28	6.28	12.57	12.57	2	0.01	0.02	0.10	0.00	0.00	24.0
17	97	-9584	-91	-847	0	90	48	6.28	6.28	12.57	12.57	2	0.01	0.01	0.08	0.00	0.00	24.0
18	97	-13330	80	-1383	0	-83	-189	6.28	6.28	12.57	12.57	3	0.01	0.02	0.13	0.00	0.00	24.0
19	97	-13400	-323	-1454	0	-152	308	6.28	6.28	12.57	12.57	3	0.02	0.03	0.14	0.00	0.00	24.0
20	97	-13430	-104	-1496	0	-190	42	6.28	6.28	12.57	12.57	3	0.01	0.03	0.14	0.00	0.00	24.0
37	97	-12900	222	-1271	0	-27	-362	6.28	6.28	12.57	12.57	3	0.02	0.02	0.12	0.00	0.00	24.0
38	97	-13028	-450	-1390	0	-142	465	6.28	6.28	12.57	12.57	3	0.03	0.02	0.13	0.00	0.00	24.0
39	97	-13078	-85	-1460	0	-207	22	6.28	6.28	12.57	12.57	3	0.01	0.03	0.14	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	195	-11780	-97	-1214	0	1167	-60	6.28	6.28	12.57	12.57	3	0.04	0.02	0.12	0.00	0.00	24.0
2	195	-9078	-7	-953	0	892	-64	6.28	6.28	12.57	12.57	2	0.05	0.02	0.10	0.00	0.00	24.0
3	195	-9032	-5	-900	0	903	-64	6.28	6.28	12.57	12.57	2	0.05	0.02	0.09	0.00	0.00	24.0
4	195	-9092	-144	-969	0	893	-29	6.28	6.28	12.57	12.57	2	0.05	0.02	0.10	0.00	0.00	24.0
5	195	-9052	-142	-915	0	904	-28	6.28	6.28	12.57	12.57	2	0.05	0.02	0.09	0.00	0.00	24.0
6	195	-9130	-58	-1021	0	879	-52	6.28	6.28	12.57	12.57	2	0.05	0.02	0.10	0.00	0.00	24.0
7	195	-8991	-50	-842	0	916	-51	6.28	6.28	12.57	12.57	2	0.05	0.01	0.08	0.00	0.00	24.0
8	195	-9138	-99	-1026	0	879	-41	6.28	6.28	12.57	12.57	2	0.05	0.02	0.10	0.00	0.00	24.0
9	195	-8999	-91	-847	0	916	-41	6.28	6.28	12.57	12.57	2	0.05	0.01	0.09	0.00	0.00	24.0
10	195	-9078	-7	-953	0	892	-64	6.28	6.28	12.57	12.57	2	0.05	0.02	0.10	0.00	0.00	24.0
11	195	-9032	-5	-900	0	903	-64	6.28	6.28	12.57	12.57	2	0.05	0.02	0.09	0.00	0.00	24.0
12	195	-9092	-144	-969	0	893	-29	6.28	6.28	12.57	12.57	2	0.05	0.02	0.10	0.00	0.00	24.0
13	195	-9052	-142	-915	0	904	-28	6.28	6.28	12.57	12.57	2	0.05	0.02	0.09	0.00	0.00	24.0
14	195	-9130	-58	-1021	0	879	-52	6.28	6.28	12.57	12.57	2	0.05	0.02	0.10	0.00	0.00	24.0
15	195	-8991	-50	-842	0	916	-51	6.28	6.28	12.57	12.57	2	0.05	0.01	0.08	0.00	0.00	24.0
16	195	-9138	-99	-1026	0	879	-41	6.28	6.28	12.57	12.57	2	0.05	0.02	0.10	0.00	0.00	24.0
17	195	-8999	-91	-847	0	916	-41	6.28	6.28	12.57	12.57	2	0.05	0.01	0.09	0.00	0.00	24.0
18	195	-12570	80	-1383	0	1265	-111	6.28	6.28	12.57	12.57	3	0.05	0.02	0.13	0.00	0.00	24.0
19	195	-12640	-323	-1454	0	1265	-7	6.28	6.28	12.57	12.57	3	0.04	0.03	0.14	0.00	0.00	24.0
20	195	-12670	-104	-1496	0	1268	-59	6.28	6.28	12.57	12.57	3	0.05	0.03	0.14	0.00	0.00	24.0
37	195	-12140	222	-1271	0	1212	-146	6.28	6.28	12.57	12.57	3	0.04	0.02	0.12	0.00	0.00	24.0
38	195	-12265	-450	-1390	0	1213	27	6.28	6.28	12.57	12.57	3	0.04	0.02	0.13	0.00	0.00	24.0
39	195	-12315	-85	-1460	0	1217	-60	6.28	6.28	12.57	12.57	3	0.04	0.03	0.14	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	292	-11020	-97	-1214	0	2351	-154	6.28	6.28	12.57	12.57	3	0.09	0.02	0.12	0.00	0.00	24.0
2	292	-8491	-7	-953	0	1822	-71	6.28	6.28	12.57	12.57	2	0.10	0.02	0.10	0.00	0.00	24.0
3	292	-8447	-5	-900	0	1780	-69	6.28	6.28	12.57	12.57	2	0.09	0.02	0.09	0.00	0.00	24.0
4	292	-8509	-144	-969	0	1837	-169	6.28	6.28	12.57	12.57	2	0.10	0.02	0.10	0.00	0.00	24.0
5	292	-8467	-142	-915	0	1796	-167	6.28	6.28	12.57	12.57	2	0.10	0.02	0.09	0.00	0.00	24.0
6	292	-8546	-58	-1021	0	1875	-108	6.28	6.28	12.57	12.57	2	0.10	0.02	0.10	0.00	0.00	24.0
7	292	-8406	-50	-842	0	1738	-100	6.28	6.28	12.57	12.57	2	0.09	0.01	0.09	0.00	0.00	24.0
8	292	-8553	-99	-1026	0	1880	-138	6.28	6.28	12.57	12.57	2	0.10	0.02	0.10	0.00	0.00	24.0
9	292	-8414	-91	-847	0	1742	-129	6.28	6.28	12.57	12.57	2	0.09	0.01	0.09	0.00	0.00	24.0
10	292	-8491	-7	-953	0	1822	-71	6.28	6.28	12.57	12.57	2	0.10	0.02	0.10	0.00	0.00	24.0
11	292	-8447	-5	-900	0	1780	-69	6.28	6.28	12.57	12.57	2	0.09	0.02	0.09	0.00	0.00	24.0
12	292	-8509	-144	-969	0	1837	-169	6.28	6.28	12.57	12.57	2	0.10	0.02	0.10	0.00	0.00	24.0
13	292	-8467	-142	-915	0	1796	-167	6.28	6.28	12.57	12.57	2	0.10	0.02	0.09	0.00	0.00	24.0
14	292	-8546	-58	-1021	0	1875	-108	6.28	6.28	12.57	12.57	2	0.10	0.02	0.10	0.00	0.00	24.0
15	292	-8406	-50	-842	0	1738	-100	6.28	6.28	12.57	12.57	2	0.09	0.01	0.09	0.00	0.00	24.0
16	292	-8553	-99	-1026	0	1880	-138	6.28	6.28	12.57	12.57	2	0.10	0.02	0.10	0.00	0.00	24.0
17	292	-8414	-91	-847	0	1742	-129	6.28	6.28	12.57	12.57	2	0.09	0.01	0.09	0.00	0.00	24.0
18	292	-11810	80	-1383	0	2614	-33	6.28	6.28	12.57	12.57	3	0.09	0.02	0.13	0.00	0.00	24.0
19	292	-11880	-323	-1454	0	2683	-322	6.28	6.28	12.57	12.57	3	0.10	0.03	0.14	0.00	0.00	24.0
20	292	-11910	-104	-1496	0	2727	-161	6.28	6.28	12.57	12.57	3	0.10	0.03	0.15	0.00	0.00	24.0
37	292	-11380	222	-1271	0	2451	71	6.28	6.28	12.57	12.57	3	0.09	0.02	0.12	0.00	0.00	24.0
38	292	-11502	-450	-1390	0	2567	-411	6.28	6.28	12.57	12.57	3	0.10	0.02	0.14	0.00	0.00	24.0
39	292	-11552	-85	-1460	0	2640	-143	6.28	6.28	12.57	12.57	3	0.10	0.03	0.14	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	390	-10260	-97	-1214	0	3535	-249	6.28	6.28	12.57	12.57	3	0.13	0.02	0.12	0.00	0.00	24.0
2	390	-7905	-7	-953	0	2751	-78	6.28	6.28	12.57	12.57	2	0.15	0.02	0.10	0.00	0.00	24.0
3	390	-7863	-5	-900	0	2657	-74	6.28	6.28	12.57	12.57	2	0.14	0.02	0.09	0.00	0.00	24.0
4	390	-7925	-144	-969	0	2782	-309	6.28	6.28	12.57	12.57	2	0.15	0.02	0.10	0.00	0.00	24.0
5	390	-7883	-142	-915	0	2688	-305	6.28	6.28	12.57	12.57	2	0.15	0.02	0.09	0.00	0.00	24.0
6	390	-7961	-58	-1021	0	2871	-165	6.28	6.28	12.57	12.57	2	0.15	0.02	0.10	0.00	0.00	24.0

7	390	-7822	-50	-842	0	2559	-149	6.28	6.28	12.57	12.57	2	0.14	0.01	0.09	0.00	0.00	24.0
8	390	-7967	-99	-1026	0	2880	-234	6.28	6.28	12.57	12.57	2	0.16	0.02	0.10	0.00	0.00	24.0
9	390	-7828	-91	-847	0	2568	-218	6.28	6.28	12.57	12.57	2	0.14	0.01	0.09	0.00	0.00	24.0
10	390	-7905	-7	-953	0	2751	-78	6.28	6.28	12.57	12.57	2	0.15	0.02	0.10	0.00	0.00	24.0
11	390	-7863	-5	-900	0	2657	-74	6.28	6.28	12.57	12.57	2	0.14	0.02	0.09	0.00	0.00	24.0
12	390	-7925	-144	-969	0	2782	-309	6.28	6.28	12.57	12.57	2	0.15	0.02	0.10	0.00	0.00	24.0
13	390	-7883	-142	-915	0	2688	-305	6.28	6.28	12.57	12.57	2	0.15	0.02	0.09	0.00	0.00	24.0
14	390	-7961	-58	-1021	0	2871	-165	6.28	6.28	12.57	12.57	2	0.15	0.02	0.10	0.00	0.00	24.0
15	390	-7822	-50	-842	0	2559	-149	6.28	6.28	12.57	12.57	2	0.14	0.01	0.09	0.00	0.00	24.0
16	390	-7967	-99	-1026	0	2880	-234	6.28	6.28	12.57	12.57	2	0.16	0.02	0.10	0.00	0.00	24.0
17	390	-7828	-91	-847	0	2568	-218	6.28	6.28	12.57	12.57	2	0.14	0.01	0.09	0.00	0.00	24.0
18	390	-11050	80	-1383	0	3962	46	6.28	6.28	12.57	12.57	3	0.14	0.02	0.14	0.00	0.00	24.0
19	390	-11120	-323	-1454	0	4101	-637	6.28	6.28	12.57	12.57	3	0.15	0.03	0.14	0.00	0.00	24.0
20	390	-11150	-104	-1496	0	4186	-262	6.28	6.28	12.57	12.57	3	0.15	0.03	0.15	0.00	0.00	24.0
37	390	-10620	222	-1271	0	3690	288	6.28	6.28	12.57	12.57	3	0.14	0.02	0.13	0.00	0.00	24.0
38	390	-10740	-450	-1390	0	3922	-849	6.28	6.28	12.57	12.57	3	0.15	0.02	0.14	0.00	0.00	24.0
39	390	-10790	-85	-1460	0	4064	-225	6.28	6.28	12.57	12.57	3	0.15	0.03	0.14	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

VERIFICA NODO IN TESTA AL PILASTRO, NODO NUM. 123 NON CONFINATO

(par.7.2.2 NTC2018 "La domanda di resistenza valutata con i criteri della progettazione in capacità può essere assunta non superiore alla domanda di resistenza valutata per il caso di comportamento strutturale non dissipativo.")

PROGETTAZIONE IN CAPACITA'

Asse loc. pilastro y nodo INTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 50.0 cm, hjc= 30.0 cm
Asse loc. pilastro z nodo ESTERNO: As2(inf)= 6.03, As1(sup)= 6.03, Hjw= 40.0 cm, bj= 40.0 cm, hjc= 50.0 cm

FxMin,inf	FxMin,sup	FxMax,sup	FySup	FzSup	Vjbdy	Vjbdz	Vres,y	Vres,z	I.R.compr.	Ashy	Ashz	PASSO	Nota
daN					daN		daN			cmq		cm	
-7822	1	-0	0	0	35233	26425	131261	140012	0.27	8.85	--	5.13	

VERIFICA DI RESISTENZA CON SOLLECITAZIONI COMPORTAMENTO NON DISSIPATIVO

Asse loc. pilastro y nodo INTERNO: Hjw= 40.0 cm, bj= 50.0 cm, hjc= 30.0 cm, db1= 45.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb,1	Mb,2	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-0	-7905	-1177	-1156	0	52	131261	0.00	0.00	40.00	
3	-0	-7863	-1176	-1152	0	59	131261	0.00	0.00	40.00	
4	-0	-7925	-962	-1378	0	1026	131261	0.01	0.00	40.00	
5	-0	-7883	-961	-1374	0	1019	131261	0.01	0.00	40.00	
6	-0	-7961	-1103	-1239	0	336	131261	0.00	0.00	40.00	
7	-0	-7822	-1100	-1224	0	306	131261	0.00	0.00	40.00	
8	-0	-7967	-1039	-1306	0	659	131261	0.01	0.00	40.00	
9	-0	-7828	-1035	-1291	0	632	131261	0.00	0.00	40.00	
10	-0	-7905	-1177	-1156	0	52	131261	0.00	0.00	40.00	
11	-0	-7863	-1176	-1152	0	59	131261	0.00	0.00	40.00	
12	-0	-7925	-962	-1378	0	1026	131261	0.01	0.00	40.00	
13	-0	-7883	-961	-1374	0	1019	131261	0.01	0.00	40.00	
14	-0	-7961	-1103	-1239	0	336	131261	0.00	0.00	40.00	
15	-0	-7822	-1100	-1224	0	306	131261	0.00	0.00	40.00	
16	-0	-7967	-1039	-1306	0	659	131261	0.01	0.00	40.00	
17	-0	-7828	-1035	-1291	0	632	131261	0.00	0.00	40.00	

Asse loc. pilastro z nodo ESTERNO: Hjw= 40.0 cm, bj= 40.0 cm, hjc= 50.0 cm, db1= 45.0 cm

NC	Fx,sup	Fx,inf	Mb	Vb	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-0	-7905	-2787	5625	0	6881	140012	0.05	0.00	40.00	
3	-0	-7863	-2690	5585	0	6642	140012	0.05	0.00	40.00	
4	-0	-7925	-2816	5638	0	6953	140012	0.05	0.00	40.00	
5	-0	-7883	-2719	5598	0	6714	140012	0.05	0.00	40.00	
6	-0	-7961	-2911	5676	0	7188	140012	0.05	0.00	40.00	
7	-0	-7822	-2586	5543	0	6385	140012	0.05	0.00	40.00	
8	-0	-7967	-2920	5680	0	7210	140012	0.05	0.00	40.00	
9	-0	-7828	-2595	5547	0	6407	140012	0.05	0.00	40.00	
10	-0	-7905	-2787	5625	0	6881	140012	0.05	0.00	40.00	
11	-0	-7863	-2690	5585	0	6642	140012	0.05	0.00	40.00	
12	-0	-7925	-2816	5638	0	6953	140012	0.05	0.00	40.00	
13	-0	-7883	-2719	5598	0	6714	140012	0.05	0.00	40.00	
14	-0	-7961	-2911	5676	0	7188	140012	0.05	0.00	40.00	
15	-0	-7822	-2586	5543	0	6385	140012	0.05	0.00	40.00	
16	-0	-7967	-2920	5680	0	7210	140012	0.05	0.00	40.00	
17	-0	-7828	-2595	5547	0	6407	140012	0.05	0.00	40.00	

CONFRONTO E SINTESI CONCLUSIVE (si assume in ogni caso passo <= 15 cm)

I.R.compr.	Ashy	Ashz	PASSO	Nota
	cmq		cm	
0.05	--	--	15.00	**VERIFICATO**

ASTA NUM. 58 NI 211 NF 212 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 13B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-12490	57	-1205	0	-1344	-79	6.28	6.28	9.42	9.42	3	0.06	0.03	0.14	0.00	0.00	24.0
2	0	-9624	82	-946	0	-1075	-140	6.28	6.28	9.42	9.42	2	0.07	0.02	0.11	0.00	0.00	24.0
3	0	-9593	82	-906	0	-992	-138	6.28	6.28	9.42	9.42	2	0.07	0.02	0.11	0.00	0.00	24.0
4	0	-9625	6	-948	0	-1076	16	6.28	6.28	9.42	9.42	2	0.07	0.02	0.11	0.00	0.00	24.0
5	0	-9593	5	-908	0	-993	18	6.28	6.28	9.42	9.42	2	0.06	0.02	0.11	0.00	0.00	24.0
6	0	-9662	56	-994	0	-1172	-87	6.28	6.28	9.42	9.42	2	0.08	0.02	0.12	0.00	0.00	24.0

7	0	-9556	54	-860	0	-896	-82	6.28	6.28	9.42	9.42	2	0.06	0.02	0.10	0.00	0.00	24.0
8	0	-9662	33	-994	0	-1172	-40	6.28	6.28	9.42	9.42	2	0.07	0.02	0.12	0.00	0.00	24.0
9	0	-9556	31	-860	0	-896	-35	6.28	6.28	9.42	9.42	2	0.06	0.02	0.10	0.00	0.00	24.0
10	0	-9624	82	-946	0	-1075	-140	6.28	6.28	9.42	9.42	2	0.07	0.02	0.11	0.00	0.00	24.0
11	0	-9593	82	-906	0	-992	-138	6.28	6.28	9.42	9.42	2	0.07	0.02	0.11	0.00	0.00	24.0
12	0	-9625	6	-948	0	-1076	16	6.28	6.28	9.42	9.42	2	0.07	0.02	0.11	0.00	0.00	24.0
13	0	-9593	5	-908	0	-993	18	6.28	6.28	9.42	9.42	2	0.06	0.02	0.11	0.00	0.00	24.0
14	0	-9662	56	-994	0	-1172	-87	6.28	6.28	9.42	9.42	2	0.08	0.02	0.12	0.00	0.00	24.0
15	0	-9556	54	-860	0	-896	-82	6.28	6.28	9.42	9.42	2	0.06	0.02	0.10	0.00	0.00	24.0
16	0	-9662	33	-994	0	-1172	-40	6.28	6.28	9.42	9.42	2	0.07	0.02	0.12	0.00	0.00	24.0
17	0	-9556	31	-860	0	-896	-35	6.28	6.28	9.42	9.42	2	0.06	0.02	0.10	0.00	0.00	24.0
18	0	-13370	158	-1497	0	-1823	-286	6.28	6.28	9.42	9.42	3	0.09	0.03	0.17	0.00	0.00	24.0
19	0	-13340	-70	-1460	0	-1745	177	6.28	6.28	9.42	9.42	3	0.08	0.03	0.16	0.00	0.00	24.0
20	0	-13490	49	-1609	0	-2041	-63	6.28	6.28	9.42	9.42	3	0.09	0.04	0.18	0.00	0.00	24.0
37	0	-12970	238	-1400	0	-1686	-448	6.28	6.28	9.42	9.42	3	0.09	0.03	0.16	0.00	0.00	24.0
38	0	-12920	-142	-1339	0	-1556	323	6.28	6.28	9.42	9.42	3	0.08	0.03	0.15	0.00	0.00	24.0
39	0	-13160	56	-1588	0	-2049	-76	6.28	6.28	9.42	9.42	3	0.09	0.04	0.18	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	97	-11920	57	-1205	0	-169	-24	6.28	6.28	9.42	9.42	3	0.01	0.03	0.14	0.00	0.00	24.0
2	97	-9185	82	-946	0	-152	-59	6.28	6.28	9.42	9.42	2	0.01	0.02	0.11	0.00	0.00	24.0
3	97	-9154	82	-906	0	-108	-58	6.28	6.28	9.42	9.42	2	0.01	0.02	0.11	0.00	0.00	24.0
4	97	-9186	6	-948	0	-152	22	6.28	6.28	9.42	9.42	2	0.01	0.02	0.11	0.00	0.00	24.0
5	97	-9154	5	-908	0	-109	22	6.28	6.28	9.42	9.42	2	0.01	0.02	0.11	0.00	0.00	24.0
6	97	-9223	56	-994	0	-203	-32	6.28	6.28	9.42	9.42	2	0.01	0.02	0.12	0.00	0.00	24.0
7	97	-9117	54	-860	0	-57	-29	6.28	6.28	9.42	9.42	2	0.01	0.02	0.10	0.00	0.00	24.0
8	97	-9223	33	-994	0	-203	-8	6.28	6.28	9.42	9.42	2	0.01	0.02	0.12	0.00	0.00	24.0
9	97	-9117	31	-860	0	-57	-5	6.28	6.28	9.42	9.42	2	0.00	0.02	0.10	0.00	0.00	24.0
10	97	-9185	82	-946	0	-152	-59	6.28	6.28	9.42	9.42	2	0.01	0.02	0.11	0.00	0.00	24.0
11	97	-9154	82	-906	0	-108	-58	6.28	6.28	9.42	9.42	2	0.01	0.02	0.11	0.00	0.00	24.0
12	97	-9186	6	-948	0	-152	22	6.28	6.28	9.42	9.42	2	0.01	0.02	0.11	0.00	0.00	24.0
13	97	-9154	5	-908	0	-109	22	6.28	6.28	9.42	9.42	2	0.01	0.02	0.11	0.00	0.00	24.0
14	97	-9223	56	-994	0	-203	-32	6.28	6.28	9.42	9.42	2	0.01	0.02	0.12	0.00	0.00	24.0
15	97	-9117	54	-860	0	-57	-29	6.28	6.28	9.42	9.42	2	0.01	0.02	0.10	0.00	0.00	24.0
16	97	-9223	33	-994	0	-203	-8	6.28	6.28	9.42	9.42	2	0.01	0.02	0.12	0.00	0.00	24.0
17	97	-9117	31	-860	0	-57	-5	6.28	6.28	9.42	9.42	2	0.00	0.02	0.10	0.00	0.00	24.0
18	97	-12800	158	-1497	0	-364	-132	6.28	6.28	9.42	9.42	3	0.02	0.03	0.17	0.00	0.00	24.0
19	97	-12770	-70	-1460	0	-322	109	6.28	6.28	9.42	9.42	3	0.02	0.03	0.16	0.00	0.00	24.0
20	97	-12920	49	-1609	0	-472	-16	6.28	6.28	9.42	9.42	3	0.02	0.04	0.18	0.00	0.00	24.0
37	97	-12400	238	-1400	0	-321	-216	6.28	6.28	9.42	9.42	3	0.02	0.03	0.16	0.00	0.00	24.0
38	97	-12350	-142	-1339	0	-250	185	6.28	6.28	9.42	9.42	3	0.02	0.03	0.15	0.00	0.00	24.0
39	97	-12590	56	-1588	0	-501	-22	6.28	6.28	9.42	9.42	3	0.02	0.04	0.18	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	195	-11350	57	-1205	0	1006	31	6.28	6.28	9.42	9.42	3	0.05	0.03	0.14	0.00	0.00	24.0
2	195	-8746	82	-946	0	771	21	6.28	6.28	9.42	9.42	2	0.05	0.02	0.11	0.00	0.00	24.0
3	195	-8716	82	-906	0	776	21	6.28	6.28	9.42	9.42	2	0.05	0.02	0.11	0.00	0.00	24.0
4	195	-8748	6	-948	0	771	27	6.28	6.28	9.42	9.42	2	0.05	0.02	0.11	0.00	0.00	24.0
5	195	-8716	5	-908	0	776	27	6.28	6.28	9.42	9.42	2	0.05	0.02	0.11	0.00	0.00	24.0
6	195	-8784	56	-994	0	765	23	6.28	6.28	9.42	9.42	2	0.05	0.02	0.12	0.00	0.00	24.0
7	195	-8678	54	-860	0	781	23	6.28	6.28	9.42	9.42	2	0.05	0.02	0.10	0.00	0.00	24.0
8	195	-8784	33	-994	0	766	25	6.28	6.28	9.42	9.42	2	0.05	0.02	0.12	0.00	0.00	24.0
9	195	-8678	31	-860	0	781	25	6.28	6.28	9.42	9.42	2	0.05	0.02	0.10	0.00	0.00	24.0
10	195	-8746	82	-946	0	771	21	6.28	6.28	9.42	9.42	2	0.05	0.02	0.11	0.00	0.00	24.0
11	195	-8716	82	-906	0	776	21	6.28	6.28	9.42	9.42	2	0.05	0.02	0.11	0.00	0.00	24.0
12	195	-8748	6	-948	0	771	27	6.28	6.28	9.42	9.42	2	0.05	0.02	0.11	0.00	0.00	24.0
13	195	-8716	5	-908	0	776	27	6.28	6.28	9.42	9.42	2	0.05	0.02	0.11	0.00	0.00	24.0
14	195	-8784	56	-994	0	765	23	6.28	6.28	9.42	9.42	2	0.05	0.02	0.12	0.00	0.00	24.0
15	195	-8678	54	-860	0	781	23	6.28	6.28	9.42	9.42	2	0.05	0.02	0.10	0.00	0.00	24.0
16	195	-8784	33	-994	0	766	25	6.28	6.28	9.42	9.42	2	0.05	0.02	0.12	0.00	0.00	24.0
17	195	-8678	31	-860	0	781	25	6.28	6.28	9.42	9.42	2	0.05	0.02	0.10	0.00	0.00	24.0
18	195	-12230	158	-1497	0	1096	22	6.28	6.28	9.42	9.42	3	0.05	0.03	0.17	0.00	0.00	24.0
19	195	-12200	-70	-1460	0	1102	41	6.28	6.28	9.42	9.42	3	0.05	0.03	0.17	0.00	0.00	24.0
20	195	-12350	49	-1609	0	1097	32	6.28	6.28	9.42	9.42	3	0.05	0.04	0.18	0.00	0.00	24.0
37	195	-11830	238	-1400	0	1045	16	6.28	6.28	9.42	9.42	3	0.05	0.03	0.16	0.00	0.00	24.0
38	195	-11780	-142	-1339	0	1055	47	6.28	6.28	9.42	9.42	3	0.05	0.03	0.15	0.00	0.00	24.0
39	195	-12020	56	-1588	0	1048	32	6.28	6.28	9.42	9.42	3	0.05	0.04	0.18	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	292	-10780	57	-1205	0	2180	87	6.28	6.28	9.42	9.42	3	0.10	0.03	0.14	0.00	0.00	24.0
2	292	-8308	82	-946	0	1693	101	6.28	6.28	9.42	9.42	2	0.11	0.02	0.11	0.00	0.00	24.0
3	292	-8277	82	-906	0	1659	100	6.28	6.28	9.42	9.42	2	0.11	0.02	0.11	0.00	0.00	24.0
4	292	-8309	6	-948	0	1695	33	6.28	6.28	9.42	9.42	2	0.11	0.02	0.11	0.00	0.00	24.0
5	292	-8277	5	-908	0	1661	32	6.28	6.28	9.42	9.42	2	0.10	0.02	0.11	0.00	0.00	24.0
6	292	-8346	56	-994	0	1734	78	6.28	6.28	9.42	9.42	2	0.11	0.02	0.12	0.00	0.00	24.0
7	292	-8240	54	-860	0	1620	75	6.28	6.28	9.42	9.42	2	0.10	0.02	0.10	0.00	0.00	24.0
8	292	-8346	33	-994	0	1735	58	6.28	6.28	9.42	9.42	2	0.11	0.02	0.12	0.00	0.00	24.0
9	292	-8240	31	-860	0	1620	55	6.28	6.28	9.42	9.42	2	0.10	0.02	0.10	0.00	0.00	24.0
10	292	-8308	82	-946	0	1693	101	6.28	6.28	9.42	9.42	2	0.11	0.02	0.11	0.00	0.00	24.0
11	292	-8277	82	-906	0	1659	100	6.28	6.28	9.42	9.42	2	0.11	0.02	0.11	0.00	0.00	24.0
12	292	-8309	6	-948	0	1695	33	6.28	6.28	9.42	9.42	2	0.11	0.02	0.11	0.00	0.00	24.0
13	292	-8277	5	-908	0	1661	32	6.28	6.28	9.42	9.42	2	0.10	0.02	0.11	0.00	0.00	24.0
14	292	-8346	56	-994	0	1734	78	6.28	6.28	9.42	9.42	2	0.11	0.02	0.12	0.00	0.00	24.0
15	292	-8240	54	-860	0	1620	75	6.28	6.28	9.42	9.42	2	0.10	0.02	0.10	0.00	0.00	24.0
16	292	-8346	33	-994	0	1735	58	6.28	6.28	9.42	9.42	2	0.11	0.02	0.12	0.00	0.00	24.0
17	292	-8240	31	-860	0	1620	55	6.28	6.28	9.42	9.42	2	0.10	0.02	0.10	0.00	0.00	24.0
18	292	-11660	158	-1497	0	2555	177	6.28	6.28	9.42	9.42	3	0.12	0.03	0.17	0.00	0.00	24.0
19	292	-11630	-70	-1460	0	2525	-27	6.28	6.28	9.42	9.42	3	0.11	0.03	0.17	0.00	0.00	24.0
20	292	-11780	49	-1609	0	2666	79	6.28	6.28	9.42	9.42	3	0.12	0.04	0.18	0.00	0.00	24.0
37	292	-11260	238	-1400	0	2410	248	6.28	6.28	9.42	9.42	3	0.11	0.03	0.16	0.00	0.00	24.0
38	292	-11210	-142	-1339	0	2361	-91	6.28	6.28	9.42	9.42	3	0.11	0.03	0.15	0.00	0.00	24.0
39	292	-11450	56	-1588	0	2596	86	6.28	6.28	9.42	9.42	3	0.12	0.04	0.18	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	390	-10210	57	-1205	0	3355	142	6.28	6.28	9.42	9.42	3	0.16	0.03	0.14	0.00	0.00	24.0
2	390	-7869	82	-946	0	2616	182	6.28	6.28	9.42	9.42	2	0.17	0.02	0.11	0.00	0.00	24.0
3	390	-7838	82	-906	0	2543	180	6.28	6.28	9.42	9.42	2	0.17	0.02	0.11	0.00	0.00	24.0
4	390	-7870	6	-948	0	2619	38	6.28	6.28	9.42	9.42	2	0.16	0.02	0.11	0.00	0.00	24.0
5	390	-7838	5	-908	0	2546	37	6.28	6.28	9.42	9.42	2	0.16	0.02	0.11	0.00	0.00	24.0
6	390	-7907	56	-994	0	2703	133	6.28	6.28	9.42	9.42	2	0.17	0.02	0.12	0.00	0.00	24.0
7	390	-7801	54	-860	0	2458	128	6.28	6.28	9.42	9.42	2	0.16	0.02	0.10	0.00	0.00	24.0
8	390	-7907	33	-994	0	2704	90	6.28	6.28	9.42	9.42	2	0.17	0.02	0.12	0.00	0.00	24.0
9	390	-7801	31	-860	0	2459	85	6.28	6.28	9.42	9.42	2	0.16	0.02	0.10	0.00	0.00	24.0
10	390	-7869	82	-946	0	2616	182	6.28	6.28	9.42	9.42	2	0.17	0.02	0.11	0.00	0.00	24.0
11	390	-7838	82	-906	0	2543	180	6.28	6.28	9.42	9.42	2	0.17	0.02	0.11	0.00	0.00	24.0
12	390	-7870	6	-948	0	2619	38	6.28	6.28	9.42	9.42	2	0.16	0.02	0.11	0.00	0.00	24.0

13	390	-7838	5	-908	0	2546	37	6.28	6.28	9.42	9.42	2	0.16	0.02	0.11	0.00	0.00	24.0
14	390	-7907	56	-994	0	2703	133	6.28	6.28	9.42	9.42	2	0.17	0.02	0.12	0.00	0.00	24.0
15	390	-7801	54	-860	0	2458	128	6.28	6.28	9.42	9.42	2	0.16	0.02	0.10	0.00	0.00	24.0
16	390	-7907	33	-994	0	2704	90	6.28	6.28	9.42	9.42	2	0.17	0.02	0.12	0.00	0.00	24.0
17	390	-7801	31	-860	0	2459	85	6.28	6.28	9.42	9.42	2	0.16	0.02	0.10	0.00	0.00	24.0
18	390	-11090	158	-1497	0	4014	331	6.28	6.28	9.42	9.42	3	0.19	0.03	0.17	0.00	0.00	24.0
19	390	-11060	-70	-1460	0	3948	-95	6.28	6.28	9.42	9.42	3	0.18	0.03	0.17	0.00	0.00	24.0
20	390	-11210	49	-1609	0	4235	126	6.28	6.28	9.42	9.42	3	0.19	0.04	0.18	0.00	0.00	24.0
37	390	-10690	238	-1400	0	3775	481	6.28	6.28	9.42	9.42	3	0.18	0.03	0.16	0.00	0.00	24.0
38	390	-10640	-142	-1339	0	3666	-230	6.28	6.28	9.42	9.42	3	0.17	0.03	0.16	0.00	0.00	24.0
39	390	-10880	56	-1588	0	4145	140	6.28	6.28	9.42	9.42	3	0.19	0.04	0.18	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

VERIFICA NODO IN TESTA AL PILASTRO, NODO NUM. 212 NON CONFINATO

(par.7.2.2 NTC2018 "La domanda di resistenza valutata con i criteri della progettazione in capacità può essere assunta non superiore alla domanda di resistenza valutata per il caso di comportamento strutturale non dissipativo.")

PROGETTAZIONE IN CAPACITA'

Asse loc. pilastro y nodo INTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 45.0 cm, hjc= 20.0 cm
Asse loc. pilastro z nodo ESTERNO: As2(inf)= 6.03, As1(sup)= 6.03, Hjw= 40.0 cm, bj= 40.0 cm, hjc= 50.0 cm

FxMin,inf	FxMin,sup	FxMax,sup	FySup	FzSup	Vjbdy	Vjbdz	Vres,y	Vres,z	I.R.compr.	Ashy	Ashz	PASSO	Nota
daN					daN		daN			cmq		cm	
-7801	1	-0	0	0	35233	26425	78757	140012	0.45	8.85	--	5.13	

VERIFICA DI RESISTENZA CON SOLLECITAZIONI COMPORTAMENTO NON DISSIPATIVO

Asse loc. pilastro y nodo INTERNO: Hjw= 40.0 cm, bj= 45.0 cm, hjc= 20.0 cm, db1= 45.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb,1	Mb,2	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-0	-7869	-1310	-975	0	827	78757	0.01	0.00	40.00	
3	-0	-7838	-1307	-975	0	820	78757	0.01	0.00	40.00	
4	-0	-7870	-1130	-1158	0	69	78757	0.00	0.00	40.00	
5	-0	-7838	-1126	-1157	0	77	78757	0.00	0.00	40.00	
6	-0	-7907	-1251	-1040	0	521	78757	0.01	0.00	40.00	
7	-0	-7801	-1240	-1038	0	499	78757	0.01	0.00	40.00	
8	-0	-7907	-1197	-1094	0	254	78757	0.00	0.00	40.00	
9	-0	-7801	-1186	-1093	0	230	78757	0.00	0.00	40.00	
10	-0	-7869	-1310	-975	0	827	78757	0.01	0.00	40.00	
11	-0	-7838	-1307	-975	0	820	78757	0.01	0.00	40.00	
12	-0	-7870	-1130	-1158	0	69	78757	0.00	0.00	40.00	
13	-0	-7838	-1126	-1157	0	77	78757	0.00	0.00	40.00	
14	-0	-7907	-1251	-1040	0	521	78757	0.01	0.00	40.00	
15	-0	-7801	-1240	-1038	0	499	78757	0.01	0.00	40.00	
16	-0	-7907	-1197	-1094	0	254	78757	0.00	0.00	40.00	
17	-0	-7801	-1186	-1093	0	230	78757	0.00	0.00	40.00	

Asse loc. pilastro z nodo ESTERNO: Hjw= 40.0 cm, bj= 40.0 cm, hjc= 50.0 cm, db1= 45.0 cm

NC	Fx,sup	Fx,inf	Mb	Vb	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-0	-7869	-2672	5601	0	6598	140012	0.05	0.00	40.00	
3	-0	-7838	-2596	5570	0	6410	140012	0.05	0.00	40.00	
4	-0	-7870	-2675	5601	0	6605	140012	0.05	0.00	40.00	
5	-0	-7838	-2599	5571	0	6417	140012	0.05	0.00	40.00	
6	-0	-7907	-2761	5637	0	6817	140012	0.05	0.00	40.00	
7	-0	-7801	-2509	5535	0	6195	140012	0.04	0.00	40.00	
8	-0	-7907	-2762	5637	0	6820	140012	0.05	0.00	40.00	
9	-0	-7801	-2510	5535	0	6198	140012	0.04	0.00	40.00	
10	-0	-7869	-2672	5601	0	6598	140012	0.05	0.00	40.00	
11	-0	-7838	-2596	5570	0	6410	140012	0.05	0.00	40.00	
12	-0	-7870	-2675	5601	0	6605	140012	0.05	0.00	40.00	
13	-0	-7838	-2599	5571	0	6417	140012	0.05	0.00	40.00	
14	-0	-7907	-2761	5637	0	6817	140012	0.05	0.00	40.00	
15	-0	-7801	-2509	5535	0	6195	140012	0.04	0.00	40.00	
16	-0	-7907	-2762	5637	0	6820	140012	0.05	0.00	40.00	
17	-0	-7801	-2510	5535	0	6198	140012	0.04	0.00	40.00	

CONFRONTO E SINTESI CONCLUSIVE (si assume in ogni caso passo <= 15 cm)

I.R.compr.	Ashy	Ashz	PASSO	Nota
	cmq		cm	
0.05	--	--	15.00	**VERIFICATO**

ASTA NUM. 59 NI 213 NF 214 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 8B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-7262	-108	-607	0	-645	42	6.28	6.28	9.42	9.42	3	0.03	0.01	0.07	0.00	0.00	24.0
2	0	-5580	-52	-505	0	-583	-39	6.28	6.28	9.42	9.42	2	0.04	0.01	0.06	0.00	0.00	24.0
3	0	-5548	-53	-460	0	-480	-35	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
4	0	-5624	-114	-473	0	-512	100	6.28	6.28	9.42	9.42	2	0.04	0.01	0.06	0.00	0.00	24.0
5	0	-5592	-115	-428	0	-409	104	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
6	0	-5633	-71	-547	0	-679	5	6.28	6.28	9.42	9.42	2	0.04	0.01	0.07	0.00	0.00	24.0
7	0	-5526	-77	-396	0	-335	18	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
8	0	-5646	-90	-537	0	-657	47	6.28	6.28	9.42	9.42	2	0.04	0.01	0.07	0.00	0.00	24.0
9	0	-5540	-96	-386	0	-314	60	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
10	0	-5580	-52	-505	0	-583	-39	6.28	6.28	9.42	9.42	2	0.04	0.01	0.06	0.00	0.00	24.0
11	0	-5548	-53	-460	0	-480	-35	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
12	0	-5624	-114	-473	0	-512	100	6.28	6.28	9.42	9.42	2	0.04	0.01	0.06	0.00	0.00	24.0

13	0	-5592	-115	-428	0	-409	104	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
14	0	-5633	-71	-547	0	-679	5	6.28	6.28	9.42	9.42	2	0.04	0.01	0.07	0.00	0.00	24.0
15	0	-5526	-77	-396	0	-335	18	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
16	0	-5646	-90	-537	0	-657	47	6.28	6.28	9.42	9.42	2	0.04	0.01	0.07	0.00	0.00	24.0
17	0	-5540	-96	-386	0	-314	60	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
18	0	-7633	-23	-800	0	-1016	-151	6.28	6.28	9.42	9.42	3	0.05	0.02	0.10	0.00	0.00	24.0
19	0	-7713	-209	-632	0	-639	266	6.28	6.28	9.42	9.42	3	0.04	0.01	0.08	0.00	0.00	24.0
20	0	-7754	-112	-804	0	-1020	50	6.28	6.28	9.42	9.42	3	0.05	0.02	0.10	0.00	0.00	24.0
37	0	-7408	41	-812	0	-1074	-295	6.28	6.28	9.42	9.42	3	0.06	0.02	0.10	0.00	0.00	24.0
38	0	-7543	-268	-532	0	-447	401	6.28	6.28	9.42	9.42	3	0.05	0.01	0.06	0.00	0.00	24.0
39	0	-7610	-108	-818	0	-1081	40	6.28	6.28	9.42	9.42	3	0.05	0.02	0.10	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	97	-6692	-108	-607	0	-53	-64	6.28	6.28	9.42	9.42	3	0.01	0.01	0.08	0.00	0.00	24.0
2	97	-5141	-52	-505	0	-91	-90	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
3	97	-5109	-53	-460	0	-32	-87	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
4	97	-5185	-114	-473	0	-51	-11	6.28	6.28	9.42	9.42	2	0.00	0.01	0.06	0.00	0.00	24.0
5	97	-5153	-115	-428	0	8	-8	6.28	6.28	9.42	9.42	2	0.00	0.01	0.05	0.00	0.00	24.0
6	97	-5194	-71	-547	0	-146	-64	6.28	6.28	9.42	9.42	2	0.01	0.01	0.07	0.00	0.00	24.0
7	97	-5087	-77	-396	0	51	-57	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
8	97	-5207	-90	-537	0	-133	-41	6.28	6.28	9.42	9.42	2	0.01	0.01	0.07	0.00	0.00	24.0
9	97	-5101	-96	-386	0	63	-34	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
10	97	-5141	-52	-505	0	-91	-90	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
11	97	-5109	-53	-460	0	-32	-87	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
12	97	-5185	-114	-473	0	-51	-11	6.28	6.28	9.42	9.42	2	0.00	0.01	0.06	0.00	0.00	24.0
13	97	-5153	-115	-428	0	8	-8	6.28	6.28	9.42	9.42	2	0.00	0.01	0.05	0.00	0.00	24.0
14	97	-5194	-71	-547	0	-146	-64	6.28	6.28	9.42	9.42	2	0.01	0.01	0.07	0.00	0.00	24.0
15	97	-5087	-77	-396	0	51	-57	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
16	97	-5207	-90	-537	0	-133	-41	6.28	6.28	9.42	9.42	2	0.01	0.01	0.07	0.00	0.00	24.0
17	97	-5101	-96	-386	0	63	-34	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
18	97	-7062	-23	-800	0	-236	-174	6.28	6.28	9.42	9.42	3	0.02	0.02	0.10	0.00	0.00	24.0
19	97	-7143	-209	-632	0	-22	63	6.28	6.28	9.42	9.42	3	0.01	0.01	0.08	0.00	0.00	24.0
20	97	-7184	-112	-804	0	-236	-60	6.28	6.28	9.42	9.42	3	0.01	0.02	0.10	0.00	0.00	24.0
37	97	-6838	41	-812	0	-283	-255	6.28	6.28	9.42	9.42	3	0.03	0.02	0.10	0.00	0.00	24.0
38	97	-6973	-268	-532	0	72	140	6.28	6.28	9.42	9.42	3	0.02	0.01	0.07	0.00	0.00	24.0
39	97	-7040	-108	-818	0	-284	-65	6.28	6.28	9.42	9.42	3	0.02	0.02	0.10	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	195	-6122	-108	-607	0	538	-170	6.28	6.28	9.42	9.42	3	0.03	0.01	0.08	0.00	0.00	24.0
2	195	-4702	-52	-505	0	402	-140	6.28	6.28	9.42	9.42	2	0.04	0.01	0.06	0.00	0.00	24.0
3	195	-4670	-53	-460	0	417	-139	6.28	6.28	9.42	9.42	2	0.04	0.01	0.06	0.00	0.00	24.0
4	195	-4746	-114	-473	0	411	-121	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
5	195	-4714	-115	-428	0	426	-121	6.28	6.28	9.42	9.42	2	0.04	0.01	0.05	0.00	0.00	24.0
6	195	-4756	-71	-547	0	388	-134	6.28	6.28	9.42	9.42	2	0.03	0.01	0.07	0.00	0.00	24.0
7	195	-4648	-77	-396	0	437	-132	6.28	6.28	9.42	9.42	2	0.04	0.01	0.05	0.00	0.00	24.0
8	195	-4768	-90	-537	0	390	-128	6.28	6.28	9.42	9.42	2	0.03	0.01	0.07	0.00	0.00	24.0
9	195	-4662	-96	-386	0	440	-127	6.28	6.28	9.42	9.42	2	0.04	0.01	0.05	0.00	0.00	24.0
10	195	-4702	-52	-505	0	402	-140	6.28	6.28	9.42	9.42	2	0.04	0.01	0.06	0.00	0.00	24.0
11	195	-4670	-53	-460	0	417	-139	6.28	6.28	9.42	9.42	2	0.04	0.01	0.06	0.00	0.00	24.0
12	195	-4746	-114	-473	0	411	-121	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
13	195	-4714	-115	-428	0	426	-121	6.28	6.28	9.42	9.42	2	0.04	0.01	0.05	0.00	0.00	24.0
14	195	-4756	-71	-547	0	388	-134	6.28	6.28	9.42	9.42	2	0.03	0.01	0.07	0.00	0.00	24.0
15	195	-4648	-77	-396	0	437	-132	6.28	6.28	9.42	9.42	2	0.04	0.01	0.05	0.00	0.00	24.0
16	195	-4768	-90	-537	0	390	-128	6.28	6.28	9.42	9.42	2	0.03	0.01	0.07	0.00	0.00	24.0
17	195	-4662	-96	-386	0	440	-127	6.28	6.28	9.42	9.42	2	0.04	0.01	0.05	0.00	0.00	24.0
18	195	-6492	-23	-800	0	544	-196	6.28	6.28	9.42	9.42	3	0.03	0.02	0.10	0.00	0.00	24.0
19	195	-6572	-209	-632	0	595	-141	6.28	6.28	9.42	9.42	3	0.03	0.01	0.08	0.00	0.00	24.0
20	195	-6613	-112	-804	0	548	-170	6.28	6.28	9.42	9.42	3	0.03	0.02	0.10	0.00	0.00	24.0
37	195	-6268	41	-812	0	508	-215	6.28	6.28	9.42	9.42	3	0.03	0.02	0.10	0.00	0.00	24.0
38	195	-6402	-268	-532	0	591	-122	6.28	6.28	9.42	9.42	3	0.03	0.01	0.07	0.00	0.00	24.0
39	195	-6470	-108	-818	0	513	-170	6.28	6.28	9.42	9.42	3	0.03	0.02	0.10	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	292	-5551	-108	-607	0	1130	-275	6.28	6.28	9.42	9.42	3	0.06	0.01	0.08	0.00	0.00	24.0
2	292	-4264	-52	-505	0	894	-190	6.28	6.28	9.42	9.42	2	0.07	0.01	0.07	0.00	0.00	24.0
3	292	-4232	-53	-460	0	865	-191	6.28	6.28	9.42	9.42	2	0.07	0.01	0.06	0.00	0.00	24.0
4	292	-4308	-114	-473	0	872	-232	6.28	6.28	9.42	9.42	2	0.07	0.01	0.06	0.00	0.00	24.0
5	292	-4276	-115	-428	0	843	-233	6.28	6.28	9.42	9.42	2	0.07	0.01	0.06	0.00	0.00	24.0
6	292	-4317	-71	-547	0	921	-203	6.28	6.28	9.42	9.42	2	0.07	0.01	0.07	0.00	0.00	24.0
7	292	-4210	-77	-396	0	823	-208	6.28	6.28	9.42	9.42	2	0.07	0.01	0.05	0.00	0.00	24.0
8	292	-4330	-90	-537	0	914	-216	6.28	6.28	9.42	9.42	2	0.07	0.01	0.07	0.00	0.00	24.0
9	292	-4224	-96	-386	0	816	-220	6.28	6.28	9.42	9.42	2	0.07	0.01	0.05	0.00	0.00	24.0
10	292	-4264	-52	-505	0	894	-190	6.28	6.28	9.42	9.42	2	0.07	0.01	0.07	0.00	0.00	24.0
11	292	-4232	-53	-460	0	865	-191	6.28	6.28	9.42	9.42	2	0.07	0.01	0.06	0.00	0.00	24.0
12	292	-4308	-114	-473	0	872	-232	6.28	6.28	9.42	9.42	2	0.07	0.01	0.06	0.00	0.00	24.0
13	292	-4276	-115	-428	0	843	-233	6.28	6.28	9.42	9.42	2	0.07	0.01	0.06	0.00	0.00	24.0
14	292	-4317	-71	-547	0	921	-203	6.28	6.28	9.42	9.42	2	0.07	0.01	0.07	0.00	0.00	24.0
15	292	-4210	-77	-396	0	823	-208	6.28	6.28	9.42	9.42	2	0.07	0.01	0.05	0.00	0.00	24.0
16	292	-4330	-90	-537	0	914	-216	6.28	6.28	9.42	9.42	2	0.07	0.01	0.07	0.00	0.00	24.0
17	292	-4224	-96	-386	0	816	-220	6.28	6.28	9.42	9.42	2	0.07	0.01	0.05	0.00	0.00	24.0
18	292	-5922	-23	-800	0	1325	-219	6.28	6.28	9.42	9.42	3	0.07	0.02	0.10	0.00	0.00	24.0
19	292	-6002	-209	-632	0	1211	-344	6.28	6.28	9.42	9.42	3	0.07	0.01	0.08	0.00	0.00	24.0
20	292	-6042	-112	-804	0	1332	-279	6.28	6.28	9.42	9.42	3	0.07	0.02	0.10	0.00	0.00	24.0
37	292	-5697	41	-812	0	1299	-175	6.28	6.28	9.42	9.42	3	0.06	0.02	0.10	0.00	0.00	24.0
38	292	-5832	-268	-532	0	1110	-384	6.28	6.28	9.42	9.42	3	0.07	0.01	0.07	0.00	0.00	24.0
39	292	-5899	-108	-818	0	1311	-275	6.28	6.28	9.42	9.42	3	0.07	0.02	0.10	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	390	-4981	-108	-607	0	1721	-381	6.28	6.28	9.42	9.42	3	0.09	0.01	0.08	0.00	0.00	24.0
2	390	-3825	-52	-505	0	1387	-241	6.28	6.28	9.42	9.42	2	0.10	0.01	0.07	0.00	0.00	24.0
3	390	-3793	-53	-460	0	1314	-243	6.28	6.28	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
4	390	-3869	-114	-473	0	1334	-343	6.28	6.28	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
5	390	-3837	-115	-428	0	1260	-346	6.28	6.28	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
6	390	-3878	-71	-547	0	1454	-273	6.28	6.28	9.42	9.42	2	0.11	0.01	0.07	0.00	0.00	24.0
7	390	-3771	-77	-396	0	1209	-283	6.28	6.28	9.42	9.42	2	0.10	0.01	0.05	0.00	0.00	24.0
8	390	-3891	-90	-537	0	1438	-304	6.28	6.28	9.42	9.42	2	0.11	0.01	0.07	0.00	0.00	24.0
9	390	-3785	-96	-386	0	1193	-313	6.28	6.28	9.42	9.42	2	0.10	0.01	0.05	0.00	0.00	24.0
10	390	-3825	-52	-505	0	1387	-241	6.28	6.28	9.42	9.42	2	0.10	0.01	0.07	0.00	0.00	24.0
11	390	-3793	-53	-460	0	1314	-243	6.28	6.28	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
12	390	-3869	-114	-473	0	1334	-343	6.28	6.28	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
13	390	-3837	-115	-428	0	1260	-346	6.28	6.28	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
14	390	-3878	-71	-547	0	1454	-273	6.28	6.28	9.42	9.42	2	0.11	0.01	0.07	0.00	0.00	24.0
15	390	-3771	-77	-396	0	1209	-283	6.28	6.28	9.42	9.42	2	0.10	0.01	0.05	0.00	0.00	24.0
16	390	-3891	-90	-537	0	1438	-304	6.28	6.28	9.42	9.42	2	0.11	0.01	0.07	0.00	0.00	24.0
17	390	-3785	-96	-386	0	1193	-313	6.28	6.28	9.42	9.42	2	0.10	0.01	0.05	0.00	0.00	24.0
18	390	-5351	-23	-800	0	2105	-242	6.28	6.28	9.42	9.42	3	0.10	0.02	0.10	0.00	0.00	24.0

19	390	-5432	-209	-632	0	1828	-548	6.28	6.28	9.42	9.42	3	0.10	0.01	0.08	0.00	0.00	24.0
20	390	-5472	-112	-804	0	2116	-388	6.28	6.28	9.42	9.42	3	0.11	0.02	0.10	0.00	0.00	24.0
37	390	-5127	41	-812	0	2090	-136	6.28	6.28	9.42	9.42	3	0.10	0.02	0.10	0.00	0.00	24.0
38	390	-5262	-268	-532	0	1629	-645	6.28	6.28	9.42	9.42	3	0.10	0.01	0.07	0.00	0.00	24.0
39	390	-5329	-108	-818	0	2108	-380	6.28	6.28	9.42	9.42	3	0.11	0.02	0.10	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

VERIFICA NODO IN TESTA AL PILASTRO, NODO NUM. 214 NON CONFINATO
(par.7.2.2 NTC2018 "La domanda di resistenza valutata con i criteri della progettazione in capacità può essere assunta non superiore alla domanda di resistenza valutata per il caso di comportamento strutturale non dissipativo.")

PROGETTAZIONE IN CAPACITA'
Asse loc. pilastro y nodo ESTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 45.0 cm, hjc= 20.0 cm
Asse loc. pilastro z nodo ESTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 30.0 cm, hjc= 50.0 cm

FxMin,inf	FxMin,sup	FxMax,sup	FySup	FzSup	Vjbdy	Vjbdz	Vres,y	Vres,z	I.R.compr.	Ashy	Ashz	PASSO	Nota
daN					daN		daN			cmq		cm	
-3771	1	-0	0	0	17616	17616	63005	105009	0.28	4.38	--	11.92	

VERIFICA DI RESISTENZA CON SOLLECITAZIONI COMPORTAMENTO NON DISSIPATIVO

Asse loc. pilastro y nodo ESTERNO: Hjw= 40.0 cm, bj= 45.0 cm, hjc= 20.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb	Vb	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m			daN			cmq	cm	
2	-0	-3825	-264	874	0	651	63005	0.01	0.00	40.00	
3	-0	-3793	-267	875	0	660	63005	0.01	0.00	40.00	
4	-0	-3869	-478	944	0	1181	63005	0.02	0.00	40.00	
5	-0	-3837	-482	945	0	1190	63005	0.02	0.00	40.00	
6	-0	-3878	-335	897	0	827	63005	0.01	0.00	40.00	
7	-0	-3771	-346	901	0	855	63005	0.01	0.00	40.00	
8	-0	-3891	-399	918	0	986	63005	0.02	0.00	40.00	
9	-0	-3785	-411	922	0	1014	63005	0.02	0.00	40.00	
10	-0	-3825	-264	874	0	651	63005	0.01	0.00	40.00	
11	-0	-3793	-267	875	0	660	63005	0.01	0.00	40.00	
12	-0	-3869	-478	944	0	1181	63005	0.02	0.00	40.00	
13	-0	-3837	-482	945	0	1190	63005	0.02	0.00	40.00	
14	-0	-3878	-335	897	0	827	63005	0.01	0.00	40.00	
15	-0	-3771	-346	901	0	855	63005	0.01	0.00	40.00	
16	-0	-3891	-399	918	0	986	63005	0.02	0.00	40.00	
17	-0	-3785	-411	922	0	1014	63005	0.02	0.00	40.00	

Asse loc. pilastro z nodo ESTERNO: Hjw= 40.0 cm, bj= 30.0 cm, hjc= 50.0 cm, db1= 45.0 cm

NC	Fx,sup	Fx,inf	Mb	Vb	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m			daN			cmq	cm	
2	-0	-3825	-1341	2951	0	3311	105009	0.03	0.00	40.00	
3	-0	-3793	-1269	2918	0	3133	105009	0.03	0.00	40.00	
4	-0	-3869	-1289	2925	0	3183	105009	0.03	0.00	40.00	
5	-0	-3837	-1217	2892	0	3005	105009	0.03	0.00	40.00	
6	-0	-3878	-1408	2981	0	3477	105009	0.03	0.00	40.00	
7	-0	-3771	-1166	2870	0	2879	105009	0.03	0.00	40.00	
8	-0	-3891	-1392	2973	0	3437	105009	0.03	0.00	40.00	
9	-0	-3785	-1150	2863	0	2840	105009	0.03	0.00	40.00	
10	-0	-3825	-1341	2951	0	3311	105009	0.03	0.00	40.00	
11	-0	-3793	-1269	2918	0	3133	105009	0.03	0.00	40.00	
12	-0	-3869	-1289	2925	0	3183	105009	0.03	0.00	40.00	
13	-0	-3837	-1217	2892	0	3005	105009	0.03	0.00	40.00	
14	-0	-3878	-1408	2981	0	3477	105009	0.03	0.00	40.00	
15	-0	-3771	-1166	2870	0	2879	105009	0.03	0.00	40.00	
16	-0	-3891	-1392	2973	0	3437	105009	0.03	0.00	40.00	
17	-0	-3785	-1150	2863	0	2840	105009	0.03	0.00	40.00	

CONFRONTO E SINTESI CONCLUSIVE (si assume in ogni caso passo <= 15 cm)

I.R.compr.	Ashy	Ashz	PASSO	Nota
	cmq		cm	
0.03	--	--	15.00	**VERIFICATO**

ASTA NUM. 60 NI 292 NF 302 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 1C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-14980	-97	-328	0	933	-325	6.28	6.28	9.42	9.42	3	0.05	0.01	0.04	0.00	0.00	24.0
2	0	-10830	84	-302	0	747	-27	6.28	6.28	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
3	0	-10650	82	-238	0	698	-29	6.28	6.28	9.42	9.42	2	0.04	0.01	0.03	0.00	0.00	24.0
4	0	-12390	-231	-267	0	737	-470	6.28	6.28	9.42	9.42	2	0.08	0.01	0.03	0.00	0.00	24.0
5	0	-12210	-234	-203	0	689	-472	6.28	6.28	9.42	9.42	2	0.08	0.01	0.02	0.00	0.00	24.0
6	0	-11590	-24	-365	0	801	-180	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
7	0	-10990	-31	-151	0	638	-187	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
8	0	-12050	-118	-354	0	798	-313	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
9	0	-11460	-126	-140	0	635	-320	6.28	6.28	9.42	9.42	2	0.06	0.00	0.02	0.00	0.00	24.0
10	0	-10830	84	-302	0	747	-27	6.28	6.28	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
11	0	-10650	82	-238	0	698	-29	6.28	6.28	9.42	9.42	2	0.04	0.01	0.03	0.00	0.00	24.0
12	0	-12390	-231	-267	0	737	-470	6.28	6.28	9.42	9.42	2	0.08	0.01	0.03	0.00	0.00	24.0
13	0	-12210	-234	-203	0	689	-472	6.28	6.28	9.42	9.42	2	0.08	0.01	0.02	0.00	0.00	24.0
14	0	-11590	-24	-365	0	801	-180	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
15	0	-10990	-31	-151	0	638	-187	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
16	0	-12050	-118	-354	0	798	-313	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
17	0	-11460	-126	-140	0	635	-320	6.28	6.28	9.42	9.42	2	0.06	0.00	0.02	0.00	0.00	24.0
18	0	-17290	171	-599	0	1404	430	6.28	6.28	9.42	9.42	3	0.07	0.01	0.06	0.00	0.00	24.0

19	0	-18880	-241	-374	0	1122	-832	6.28	6.28	9.42	9.42	3	0.09	0.01	0.04	0.00	0.00	24.0
20	0	-17270	-43	-102	0	929	-214	6.28	6.28	9.42	9.42	3	0.05	0.00	0.01	0.00	0.00	24.0
37	0	-15740	289	-623	0	1391	812	6.28	6.28	9.42	9.42	3	0.10	0.01	0.07	0.00	0.00	24.0
38	0	-18390	-399	-248	0	921	-1292	6.28	6.28	9.42	9.42	3	0.13	0.01	0.04	0.00	0.00	24.0
39	0	-15710	-67	206	0	598	-262	6.28	6.28	9.42	9.42	3	0.04	0.00	0.02	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-14908	-97	-328	0	974	-337	6.28	6.28	9.42	9.42	3	0.05	0.01	0.04	0.00	0.00	24.0
2	12	-10775	84	-302	0	785	-17	6.28	6.28	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
3	12	-10595	82	-238	0	728	-19	6.28	6.28	9.42	9.42	2	0.04	0.01	0.03	0.00	0.00	24.0
4	12	-12335	-231	-267	0	771	-499	6.28	6.28	9.42	9.42	2	0.08	0.01	0.03	0.00	0.00	24.0
5	12	-12155	-234	-203	0	714	-501	6.28	6.28	9.42	9.42	2	0.08	0.01	0.02	0.00	0.00	24.0
6	12	-11532	-24	-365	0	846	-183	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
7	12	-10932	-31	-151	0	657	-190	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
8	12	-11995	-118	-354	0	842	-328	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
9	12	-11402	-126	-140	0	653	-335	6.28	6.28	9.42	9.42	2	0.06	0.00	0.02	0.00	0.00	24.0
10	12	-10775	84	-302	0	785	-17	6.28	6.28	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
11	12	-10595	82	-238	0	728	-19	6.28	6.28	9.42	9.42	2	0.04	0.01	0.03	0.00	0.00	24.0
12	12	-12335	-231	-267	0	771	-499	6.28	6.28	9.42	9.42	2	0.08	0.01	0.03	0.00	0.00	24.0
13	12	-12155	-234	-203	0	714	-501	6.28	6.28	9.42	9.42	2	0.08	0.01	0.02	0.00	0.00	24.0
14	12	-11532	-24	-365	0	846	-183	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
15	12	-10932	-31	-151	0	657	-190	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
16	12	-11995	-118	-354	0	842	-328	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
17	12	-11402	-126	-140	0	653	-335	6.28	6.28	9.42	9.42	2	0.06	0.00	0.02	0.00	0.00	24.0
18	12	-17218	143	-599	0	1479	450	6.28	6.28	9.42	9.42	3	0.08	0.01	0.06	0.00	0.00	24.0
19	12	-18805	-213	-374	0	1169	-860	6.28	6.28	9.42	9.42	3	0.09	0.01	0.04	0.00	0.00	24.0
20	12	-17198	-43	-85	0	940	-220	6.28	6.28	9.42	9.42	3	0.05	0.00	0.01	0.00	0.00	24.0
37	12	-15668	242	-623	0	1469	846	6.28	6.28	9.42	9.42	3	0.10	0.01	0.07	0.00	0.00	24.0
38	12	-18318	-351	-248	0	951	-1339	6.28	6.28	9.42	9.42	3	0.13	0.01	0.03	0.00	0.00	24.0
39	12	-15638	-67	234	0	571	-270	6.28	6.28	9.42	9.42	3	0.04	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-14835	-97	-328	0	1015	-349	6.28	6.28	9.42	9.42	3	0.06	0.01	0.04	0.00	0.00	24.0
2	25	-10720	84	-302	0	823	-6	6.28	6.28	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
3	25	-10540	82	-238	0	758	-9	6.28	6.28	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
4	25	-12280	-231	-267	0	804	-528	6.28	6.28	9.42	9.42	2	0.09	0.01	0.03	0.00	0.00	24.0
5	25	-12100	-234	-203	0	739	-531	6.28	6.28	9.42	9.42	2	0.08	0.01	0.02	0.00	0.00	24.0
6	25	-11475	-24	-365	0	892	-186	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
7	25	-10875	-31	-151	0	676	-194	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
8	25	-11940	-118	-354	0	886	-342	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
9	25	-11345	-126	-140	0	670	-351	6.28	6.28	9.42	9.42	2	0.06	0.00	0.02	0.00	0.00	24.0
10	25	-10720	84	-302	0	823	-6	6.28	6.28	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
11	25	-10540	82	-238	0	758	-9	6.28	6.28	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
12	25	-12280	-231	-267	0	804	-528	6.28	6.28	9.42	9.42	2	0.09	0.01	0.03	0.00	0.00	24.0
13	25	-12100	-234	-203	0	739	-531	6.28	6.28	9.42	9.42	2	0.08	0.01	0.02	0.00	0.00	24.0
14	25	-11475	-24	-365	0	892	-186	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
15	25	-10875	-31	-151	0	676	-194	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
16	25	-11940	-118	-354	0	886	-342	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
17	25	-11345	-126	-140	0	670	-351	6.28	6.28	9.42	9.42	2	0.06	0.00	0.02	0.00	0.00	24.0
18	25	-17145	114	-599	0	1554	466	6.28	6.28	9.42	9.42	3	0.08	0.01	0.06	0.00	0.00	24.0
19	25	-18730	-184	-374	0	1216	-885	6.28	6.28	9.42	9.42	3	0.09	0.01	0.04	0.00	0.00	24.0
20	25	-17125	-43	-71	0	950	-225	6.28	6.28	9.42	9.42	3	0.05	0.00	0.01	0.00	0.00	24.0
37	25	-15595	194	-623	0	1546	873	6.28	6.28	9.42	9.42	3	0.10	0.01	0.07	0.00	0.00	24.0
38	25	-18245	-303	-248	0	982	-1379	6.28	6.28	9.42	9.42	3	0.13	0.01	0.03	0.00	0.00	24.0
39	25	-15565	-67	258	0	540	-279	6.28	6.28	9.42	9.42	3	0.03	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-14762	-97	-328	0	1056	-361	6.28	6.28	9.42	9.42	3	0.06	0.01	0.04	0.00	0.00	24.0
2	38	-10665	84	-302	0	861	4	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
3	38	-10485	82	-238	0	788	2	6.28	6.28	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
4	38	-12225	-231	-267	0	838	-557	6.28	6.28	9.42	9.42	2	0.09	0.01	0.03	0.00	0.00	24.0
5	38	-12045	-234	-203	0	765	-560	6.28	6.28	9.42	9.42	2	0.09	0.01	0.02	0.00	0.00	24.0
6	38	-11418	-24	-365	0	938	-189	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
7	38	-10818	-31	-151	0	694	-198	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
8	38	-11885	-118	-354	0	931	-357	6.28	6.28	9.42	9.42	2	0.08	0.01	0.04	0.00	0.00	24.0
9	38	-11288	-126	-140	0	688	-367	6.28	6.28	9.42	9.42	2	0.07	0.00	0.02	0.00	0.00	24.0
10	38	-10665	84	-302	0	861	4	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
11	38	-10485	82	-238	0	788	2	6.28	6.28	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
12	38	-12225	-231	-267	0	838	-557	6.28	6.28	9.42	9.42	2	0.09	0.01	0.03	0.00	0.00	24.0
13	38	-12045	-234	-203	0	765	-560	6.28	6.28	9.42	9.42	2	0.09	0.01	0.02	0.00	0.00	24.0
14	38	-11418	-24	-365	0	938	-189	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
15	38	-10818	-31	-151	0	694	-198	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
16	38	-11885	-118	-354	0	931	-357	6.28	6.28	9.42	9.42	2	0.08	0.01	0.04	0.00	0.00	24.0
17	38	-11288	-126	-140	0	688	-367	6.28	6.28	9.42	9.42	2	0.07	0.00	0.02	0.00	0.00	24.0
18	38	-17072	86	-599	0	1629	479	6.28	6.28	9.42	9.42	3	0.09	0.01	0.06	0.00	0.00	24.0
19	38	-18655	-156	-374	0	1262	-907	6.28	6.28	9.42	9.42	3	0.10	0.01	0.04	0.00	0.00	24.0
20	38	-17052	-43	-59	0	958	-230	6.28	6.28	9.42	9.42	3	0.05	0.00	0.01	0.00	0.00	24.0
37	38	-15522	147	-623	0	1624	894	6.28	6.28	9.42	9.42	3	0.11	0.01	0.07	0.00	0.00	24.0
38	38	-18172	-256	-248	0	1013	-1414	6.28	6.28	9.42	9.42	3	0.14	0.01	0.03	0.00	0.00	24.0
39	38	-15492	-67	278	0	506	-287	6.28	6.28	9.42	9.42	3	0.03	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-14690	-97	-328	0	1097	-373	6.28	6.28	9.42	9.42	3	0.06	0.01	0.04	0.00	0.00	24.0
2	50	-10610	84	-302	0	898	15	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
3	50	-10430	82	-238	0	817	12	6.28	6.28	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
4	50	-12170	-231	-267	0	871	-586	6.28	6.28	9.42	9.42	2	0.09	0.01	0.03	0.00	0.00	24.0
5	50	-11990	-234	-203	0	790	-589	6.28	6.28	9.42	9.42	2	0.09	0.01	0.02	0.00	0.00	24.0
6	50	-11360	-24	-365	0	983	-192	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
7	50	-10760	-31	-151	0	713	-202	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
8	50	-11830	-118	-354	0	975	-372	6.28	6.28	9.42	9.42	2	0.08	0.01	0.04	0.00	0.00	24.0
9	50	-11230	-126	-140	0	705	-382	6.28	6.28	9.42	9.42	2	0.07	0.00	0.02	0.00	0.00	24.0
10	50	-10610	84	-302	0	898	15	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
11	50	-10430	82	-238	0	817	12	6.28	6.28	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
12	50	-12170	-231	-267	0	871	-586	6.28	6.28	9.42	9.42	2	0.09	0.01	0.03	0.00	0.00	24.0
13	50	-11990	-234	-203	0	790	-589	6.28	6.28	9.42	9.42	2	0.09	0.01	0.02	0.00	0.00	24.0
14	50	-11360	-24	-365	0	983	-192	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
15	50	-10760	-31	-151	0	713	-202	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
16	50	-11830	-118	-354	0	975	-372	6.28	6.28	9.42	9.42	2	0.08	0.01	0.04	0.00	0.00	24.0
17	50	-11230	-126	-140	0	705	-382	6.28	6.28	9.42	9.42	2	0.07	0.00	0.02	0.00	0.00	24.0
18	50	-17000	57	-599	0	1704	488	6.28	6.28	9.42	9.42	3	0.09	0.01	0.06	0.00	0.00	24.0
19	50	-18580	-127	-374	0	1309	-924	6.28	6.28	9.42	9.42	3	0.10	0.01	0.04	0.00	0.00	24.0
20	50	-16980	-43	-49	0	965	-236	6.28	6.28	9.42	9.42	3	0.05	0.00	0.01	0.00	0.00	24.0
37	50	-15450	99	-623	0	1702	909	6.28	6.28	9.42	9.42	3	0.11	0.01	0.07	0.00	0.00	24.0
38	50	-18100	-208	-248	0	1044	-1443	6.28	6.28	9.42	9.42	3	0.14	0.01	0.03	0.00	0.00	24.0
39	50	-15420	-67	294	0	471	-296	6.28	6.28	9.42	9.42	3	0.03	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

VERIFICA NODO IN TESTA AL PILASTRO, NODO NUM. 302 NON CONFINATO
(par.7.2.2 NTC2018 "La domanda di resistenza valutata con i criteri della progettazione in capacità può essere assunta non superiore alla domanda di resistenza valutata per il caso di comportamento strutturale non dissipativo.")

PROGETTAZIONE IN CAPACITA'
Asse loc. pilastro y nodo ESTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 45.0 cm, hjc= 20.0 cm
Asse loc. pilastro z nodo ESTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 30.0 cm, hjc= 50.0 cm

FxMin,inf	FxMin,sup	FxMax,sup	FySup	FzSup	Vjbdy	Vjbdz	Vres,y	Vres,z	I.R.compr.	Ashy	Ashz	PASSO	Nota
daN					daN		daN			cmq		cm	
-10430	-6862	-7944	21	283	17596	17334	60987	101645	0.29	4.13	--	12.87	

VERIFICA DI RESISTENZA CON SOLLECITAZIONI COMPORTAMENTO NON DISSIPATIVO

Asse loc. pilastro y nodo ESTERNO: Hjw= 40.0 cm, bj= 45.0 cm, hjc= 20.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb	Vb	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m			daN			cmq	cm	
2	-6990	-10610	-494	1542	108	1112	61233	0.02	0.00	40.00	
3	-6862	-10430	-514	1549	98	1171	61266	0.02	0.00	40.00	
4	-7944	-12170	-2121	2165	291	4946	60987	0.08	0.00	40.00	
5	-7816	-11990	-2141	2171	300	4986	61020	0.08	0.00	40.00	
6	-7473	-11360	-1040	1752	21	2547	61109	0.04	0.00	40.00	
7	-7046	-10760	-1107	1775	52	2681	61219	0.04	0.00	40.00	
8	-7759	-11830	-1528	1939	140	3633	61035	0.06	0.00	40.00	
9	-7333	-11230	-1595	1961	172	3766	61145	0.06	0.00	40.00	
10	-6990	-10610	-494	1542	108	1112	61233	0.02	0.00	40.00	
11	-6862	-10430	-514	1549	98	1171	61266	0.02	0.00	40.00	
12	-7944	-12170	-2121	2165	291	4946	60987	0.08	0.00	40.00	
13	-7816	-11990	-2141	2171	300	4986	61020	0.08	0.00	40.00	
14	-7473	-11360	-1040	1752	21	2547	61109	0.04	0.00	40.00	
15	-7046	-10760	-1107	1775	52	2681	61219	0.04	0.00	40.00	
16	-7759	-11830	-1528	1939	140	3633	61035	0.06	0.00	40.00	
17	-7333	-11230	-1595	1961	172	3766	61145	0.06	0.00	40.00	

Asse loc. pilastro z nodo ESTERNO: Hjw= 40.0 cm, bj= 30.0 cm, hjc= 50.0 cm, db1= 45.0 cm

NC	Fx,sup	Fx,inf	Mb	Vb	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m			daN			cmq	cm	
2	-6990	-10610	-2028	2074	345	4663	102055	0.05	0.00	40.00	
3	-6862	-10430	-1846	2017	317	4241	102110	0.04	0.00	40.00	
4	-7944	-12170	-1973	2057	343	4529	101645	0.04	0.00	40.00	
5	-7816	-11990	-1791	2000	315	4108	101700	0.04	0.00	40.00	
6	-7473	-11360	-2220	2136	377	5105	101848	0.05	0.00	40.00	
7	-7046	-10760	-1615	1943	283	3704	102031	0.04	0.00	40.00	
8	-7759	-11830	-2203	2131	376	5063	101725	0.05	0.00	40.00	
9	-7333	-11230	-1599	1938	283	3665	101908	0.04	0.00	40.00	
10	-6990	-10610	-2028	2074	345	4663	102055	0.05	0.00	40.00	
11	-6862	-10430	-1846	2017	317	4241	102110	0.04	0.00	40.00	
12	-7944	-12170	-1973	2057	343	4529	101645	0.04	0.00	40.00	
13	-7816	-11990	-1791	2000	315	4108	101700	0.04	0.00	40.00	
14	-7473	-11360	-2220	2136	377	5105	101848	0.05	0.00	40.00	
15	-7046	-10760	-1615	1943	283	3704	102031	0.04	0.00	40.00	
16	-7759	-11830	-2203	2131	376	5063	101725	0.05	0.00	40.00	
17	-7333	-11230	-1599	1938	283	3665	101908	0.04	0.00	40.00	

CONFRONTO E SINTESI CONCLUSIVE (si assume in ogni caso passo <= 15 cm)

I.R.compr.	Ashy	Ashz	PASSO	Nota
	cmq		cm	
0.08	--	--	15.00	**VERIFICATO**

ASTA NUM. 61 NI 294 NF 325 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 10C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-13770	-324	-95	0	-1339	2335	6.28	6.28	12.57	12.57	3	0.13	0.01	0.03	0.00	0.00	24.0
2	0	-11090	540	-144	0	-1374	1307	6.28	6.28	12.57	12.57	2	0.12	0.01	0.04	0.00	0.00	24.0
3	0	-11080	523	-23	0	-673	1308	6.28	6.28	12.57	12.57	2	0.10	0.01	0.05	0.00	0.00	24.0
4	0	-10110	-1021	-123	0	-1387	2284	6.28	6.28	12.57	12.57	2	0.18	0.02	0.10	0.00	0.00	24.0
5	0	-10090	-1038	-2	0	-686	2284	6.28	6.28	12.57	12.57	2	0.15	0.02	0.10	0.00	0.00	24.0
6	0	-10760	14	-278	0	-2197	1649	6.28	6.28	12.57	12.57	2	0.17	0.00	0.03	0.00	0.00	24.0
7	0	-10720	-43	126	0	141	1650	6.28	6.28	12.57	12.57	2	0.10	0.00	0.01	0.00	0.00	24.0
8	0	-10470	-455	-271	0	-2201	1942	6.28	6.28	12.57	12.57	2	0.19	0.01	0.04	0.00	0.00	24.0
9	0	-10420	-512	132	0	138	1943	6.28	6.28	12.57	12.57	2	0.12	0.01	0.05	0.00	0.00	24.0
10	0	-11090	540	-144	0	-1374	1307	6.28	6.28	12.57	12.57	2	0.12	0.01	0.04	0.00	0.00	24.0
11	0	-11080	523	-23	0	-673	1308	6.28	6.28	12.57	12.57	2	0.10	0.01	0.05	0.00	0.00	24.0
12	0	-10110	-1021	-123	0	-1387	2284	6.28	6.28	12.57	12.57	2	0.18	0.02	0.10	0.00	0.00	24.0
13	0	-10090	-1038	-2	0	-686	2284	6.28	6.28	12.57	12.57	2	0.15	0.02	0.10	0.00	0.00	24.0
14	0	-10760	14	-278	0	-2197	1649	6.28	6.28	12.57	12.57	2	0.17	0.00	0.03	0.00	0.00	24.0
15	0	-10720	-43	126	0	141	1650	6.28	6.28	12.57	12.57	2	0.10	0.00	0.01	0.00	0.00	24.0
16	0	-10470	-455	-271	0	-2201	1942	6.28	6.28	12.57	12.57	2	0.19	0.01	0.04	0.00	0.00	24.0
17	0	-10420	-512	132	0	138	1943	6.28	6.28	12.57	12.57	2	0.12	0.01	0.05	0.00	0.00	24.0
18	0	-17020	2114	-361	0	-3403	1611	6.28	6.28	12.57	12.57	3	0.15	0.04	0.17	0.00	0.00	24.0
19	0	-13130	-3343	-77	0	-2454	3956	6.28	6.28	12.57	12.57	3	0.23	0.06	0.30	0.00	0.00	24.0
20	0	-14730	-601	-740	0	-1915	2723	6.28	6.28	12.57	12.57	3	0.16	0.01	0.07	0.00	0.00	24.0
37	0	-18010	4024	-416	0	-3206	680	6.28	6.28	12.57	12.57	3	0.12	0.07	0.31	0.00	0.00	24.0
38	0	-11540	-5071	57	0	-1624	4586	6.28	6.28	12.57	12.57	3	0.26	0.09	0.47	0.00	0.00	24.0
39	0	-14210	-500	-1048	0	-726	2532	6.28	6.28	12.57	12.57	3	0.14	0.02	0.10	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-13672	-324	-95	0	-1327	2295	6.28	6.28 12.57 12.57	3	0.13	0.01	0.03	0.00	0.00	24.0
2	12	-11015	540	-144	0	-1356	1375	6.28	6.28 12.57 12.57	2	0.12	0.01	0.05	0.00	0.00	24.0
3	12	-11005	523	-23	0	-670	1373	6.28	6.28 12.57 12.57	2	0.10	0.01	0.05	0.00	0.00	24.0
4	12	-10034	-1021	-123	0	-1372	2156	6.28	6.28 12.57 12.57	2	0.17	0.02	0.10	0.00	0.00	24.0
5	12	-10016	-1038	-2	0	-685	2154	6.28	6.28 12.57 12.57	2	0.15	0.02	0.10	0.00	0.00	24.0
6	12	-10685	14	-278	0	-2163	1651	6.28	6.28 12.57 12.57	2	0.17	0.00	0.03	0.00	0.00	24.0
7	12	-10645	-43	126	0	126	1645	6.28	6.28 12.57 12.57	2	0.10	0.00	0.01	0.00	0.00	24.0
8	12	-10395	-455	-271	0	-2167	1885	6.28	6.28 12.57 12.57	2	0.18	0.01	0.04	0.00	0.00	24.0
9	12	-10345	-512	132	0	121	1879	6.28	6.28 12.57 12.57	2	0.11	0.01	0.05	0.00	0.00	24.0
10	12	-11015	540	-144	0	-1356	1375	6.28	6.28 12.57 12.57	2	0.12	0.01	0.05	0.00	0.00	24.0
11	12	-11005	523	-23	0	-670	1373	6.28	6.28 12.57 12.57	2	0.10	0.01	0.05	0.00	0.00	24.0
12	12	-10034	-1021	-123	0	-1372	2156	6.28	6.28 12.57 12.57	2	0.17	0.02	0.10	0.00	0.00	24.0
13	12	-10016	-1038	-2	0	-685	2154	6.28	6.28 12.57 12.57	2	0.15	0.02	0.10	0.00	0.00	24.0
14	12	-10685	14	-278	0	-2163	1651	6.28	6.28 12.57 12.57	2	0.17	0.00	0.03	0.00	0.00	24.0
15	12	-10645	-43	126	0	126	1645	6.28	6.28 12.57 12.57	2	0.10	0.00	0.01	0.00	0.00	24.0
16	12	-10395	-455	-271	0	-2167	1885	6.28	6.28 12.57 12.57	2	0.18	0.01	0.04	0.00	0.00	24.0
17	12	-10345	-512	132	0	121	1879	6.28	6.28 12.57 12.57	2	0.11	0.01	0.05	0.00	0.00	24.0
18	12	-16922	2114	-361	0	-3358	1875	6.28	6.28 12.57 12.57	3	0.15	0.04	0.17	0.00	0.00	24.0
19	12	-13032	-3343	-77	0	-2444	3538	6.28	6.28 12.57 12.57	3	0.20	0.06	0.30	0.00	0.00	24.0
20	12	-14632	-601	-707	0	-1825	2648	6.28	6.28 12.57 12.57	3	0.15	0.01	0.07	0.00	0.00	24.0
37	12	-17912	4024	-416	0	-3154	1182	6.28	6.28 12.57 12.57	3	0.13	0.07	0.31	0.00	0.00	24.0
38	12	-11442	-5071	57	0	-1631	3952	6.28	6.28 12.57 12.57	3	0.22	0.09	0.47	0.00	0.00	24.0
39	12	-14112	-500	-993	0	-599	2469	6.28	6.28 12.57 12.57	3	0.14	0.02	0.09	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-13575	-324	-95	0	-1316	2254	6.28	6.28 12.57 12.57	3	0.13	0.01	0.03	0.00	0.00	24.0
2	25	-10940	540	-144	0	-1338	1442	6.28	6.28 12.57 12.57	2	0.13	0.01	0.05	0.00	0.00	24.0
3	25	-10930	523	-23	0	-667	1438	6.28	6.28 12.57 12.57	2	0.10	0.01	0.05	0.00	0.00	24.0
4	25	-9959	-1021	-123	0	-1357	2028	6.28	6.28 12.57 12.57	2	0.16	0.02	0.10	0.00	0.00	24.0
5	25	-9942	-1038	-2	0	-685	2025	6.28	6.28 12.57 12.57	2	0.14	0.02	0.10	0.00	0.00	24.0
6	25	-10610	14	-278	0	-2128	1652	6.28	6.28 12.57 12.57	2	0.17	0.00	0.03	0.00	0.00	24.0
7	25	-10570	-43	126	0	110	1639	6.28	6.28 12.57 12.57	2	0.10	0.00	0.01	0.00	0.00	24.0
8	25	-10320	-455	-271	0	-2133	1828	6.28	6.28 12.57 12.57	2	0.18	0.01	0.04	0.00	0.00	24.0
9	25	-10270	-512	132	0	104	1815	6.28	6.28 12.57 12.57	2	0.11	0.01	0.05	0.00	0.00	24.0
10	25	-10940	540	-144	0	-1338	1442	6.28	6.28 12.57 12.57	2	0.13	0.01	0.05	0.00	0.00	24.0
11	25	-10930	523	-23	0	-667	1438	6.28	6.28 12.57 12.57	2	0.10	0.01	0.05	0.00	0.00	24.0
12	25	-9959	-1021	-123	0	-1357	2028	6.28	6.28 12.57 12.57	2	0.16	0.02	0.10	0.00	0.00	24.0
13	25	-9942	-1038	-2	0	-685	2025	6.28	6.28 12.57 12.57	2	0.14	0.02	0.10	0.00	0.00	24.0
14	25	-10610	14	-278	0	-2128	1652	6.28	6.28 12.57 12.57	2	0.17	0.00	0.03	0.00	0.00	24.0
15	25	-10570	-43	126	0	110	1639	6.28	6.28 12.57 12.57	2	0.10	0.00	0.01	0.00	0.00	24.0
16	25	-10320	-455	-271	0	-2133	1828	6.28	6.28 12.57 12.57	2	0.18	0.01	0.04	0.00	0.00	24.0
17	25	-10270	-512	132	0	104	1815	6.28	6.28 12.57 12.57	2	0.11	0.01	0.05	0.00	0.00	24.0
18	25	-16825	2114	-361	0	-3312	2139	6.28	6.28 12.57 12.57	3	0.16	0.04	0.17	0.00	0.00	24.0
19	25	-12935	-3343	-77	0	-2434	3120	6.28	6.28 12.57 12.57	3	0.18	0.06	0.30	0.00	0.00	24.0
20	25	-14535	-601	-679	0	-1738	2572	6.28	6.28 12.57 12.57	3	0.15	0.01	0.06	0.00	0.00	24.0
37	25	-17815	4024	-416	0	-3102	1685	6.28	6.28 12.57 12.57	3	0.14	0.07	0.31	0.00	0.00	24.0
38	25	-11345	-5071	57	0	-1639	3318	6.28	6.28 12.57 12.57	3	0.19	0.09	0.47	0.00	0.00	24.0
39	25	-14015	-500	-945	0	-478	2406	6.28	6.28 12.57 12.57	3	0.13	0.02	0.09	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-13478	-324	-95	0	-1304	2214	6.28	6.28 12.57 12.57	3	0.13	0.01	0.03	0.00	0.00	24.0
2	38	-10865	540	-144	0	-1320	1510	6.28	6.28 12.57 12.57	2	0.13	0.01	0.05	0.00	0.00	24.0
3	38	-10855	523	-23	0	-664	1504	6.28	6.28 12.57 12.57	2	0.11	0.01	0.05	0.00	0.00	24.0
4	38	-9884	-1021	-123	0	-1341	1901	6.28	6.28 12.57 12.57	2	0.15	0.02	0.10	0.00	0.00	24.0
5	38	-9868	-1038	-2	0	-685	1895	6.28	6.28 12.57 12.57	2	0.13	0.02	0.10	0.00	0.00	24.0
6	38	-10535	14	-278	0	-2094	1654	6.28	6.28 12.57 12.57	2	0.17	0.00	0.03	0.00	0.00	24.0
7	38	-10495	-43	126	0	94	1634	6.28	6.28 12.57 12.57	2	0.10	0.00	0.01	0.00	0.00	24.0
8	38	-10245	-455	-271	0	-2100	1771	6.28	6.28 12.57 12.57	2	0.18	0.01	0.04	0.00	0.00	24.0
9	38	-10195	-512	132	0	88	1751	6.28	6.28 12.57 12.57	2	0.11	0.01	0.05	0.00	0.00	24.0
10	38	-10865	540	-144	0	-1320	1510	6.28	6.28 12.57 12.57	2	0.13	0.01	0.05	0.00	0.00	24.0
11	38	-10855	523	-23	0	-664	1504	6.28	6.28 12.57 12.57	2	0.11	0.01	0.05	0.00	0.00	24.0
12	38	-9884	-1021	-123	0	-1341	1901	6.28	6.28 12.57 12.57	2	0.15	0.02	0.10	0.00	0.00	24.0
13	38	-9868	-1038	-2	0	-685	1895	6.28	6.28 12.57 12.57	2	0.13	0.02	0.10	0.00	0.00	24.0
14	38	-10535	14	-278	0	-2094	1654	6.28	6.28 12.57 12.57	2	0.17	0.00	0.03	0.00	0.00	24.0
15	38	-10495	-43	126	0	94	1634	6.28	6.28 12.57 12.57	2	0.10	0.00	0.01	0.00	0.00	24.0
16	38	-10245	-455	-271	0	-2100	1771	6.28	6.28 12.57 12.57	2	0.18	0.01	0.04	0.00	0.00	24.0
17	38	-10195	-512	132	0	88	1751	6.28	6.28 12.57 12.57	2	0.11	0.01	0.05	0.00	0.00	24.0
18	38	-16728	2114	-361	0	-3267	2404	6.28	6.28 12.57 12.57	3	0.17	0.04	0.17	0.00	0.00	24.0
19	38	-12838	-3343	-77	0	-2425	2702	6.28	6.28 12.57 12.57	3	0.16	0.06	0.30	0.00	0.00	24.0
20	38	-14438	-601	-655	0	-1655	2497	6.28	6.28 12.57 12.57	3	0.14	0.01	0.06	0.00	0.00	24.0
37	38	-17718	4024	-416	0	-3050	2188	6.28	6.28 12.57 12.57	3	0.15	0.07	0.31	0.00	0.00	24.0
38	38	-11248	-5071	57	0	-1646	2685	6.28	6.28 12.57 12.57	3	0.16	0.09	0.47	0.00	0.00	24.0
39	38	-13918	-500	-906	0	-362	2344	6.28	6.28 12.57 12.57	3	0.13	0.02	0.09	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-13380	-324	-95	0	-1292	2173	6.28	6.28 12.57 12.57	3	0.12	0.01	0.03	0.00	0.00	24.0
2	50	-10790	540	-144	0	-1302	1577	6.28	6.28 12.57 12.57	2	0.13	0.01	0.05	0.00	0.00	24.0
3	50	-10780	523	-23	0	-661	1569	6.28	6.28 12.57 12.57	2	0.11	0.01	0.05	0.00	0.00	24.0
4	50	-9808	-1021	-123	0	-1326	1773	6.28	6.28 12.57 12.57	2	0.15	0.02	0.10	0.00	0.00	24.0
5	50	-9794	-1038	-2	0	-685	1765	6.28	6.28 12.57 12.57	2	0.12	0.02	0.10	0.00	0.00	24.0
6	50	-10460	14	-278	0	-2059	1655	6.28	6.28 12.57 12.57	2	0.17	0.00	0.03	0.00	0.00	24.0
7	50	-10420	-43	126	0	78	1628	6.28	6.28 12.57 12.57	2	0.10	0.00	0.01	0.00	0.00	24.0
8	50	-10170	-455	-271	0	-2066	1714	6.28	6.28 12.57 12.57	2	0.17	0.01	0.04	0.00	0.00	24.0
9	50	-10120	-512	132	0	71	1687	6.28	6.28 12.57 12.57	2	0.10	0.01	0.05	0.00	0.00	24.0
10	50	-10790	540	-144	0	-1302	1577	6.28	6.28 12.57 12.57	2	0.13	0.01	0.05	0.00	0.00	24.0
11	50	-10780	523	-23	0	-661	1569	6.28	6.28 12.57 12.57	2	0.11	0.01	0.05	0.00	0.00	24.0
12	50	-9808	-1021	-123	0	-1326	1773	6.28	6.28 12.57 12.57	2	0.15	0.02	0.10	0.00	0.00	24.0
13	50	-9794	-1038	-2	0	-685	1765	6.28	6.28 12.57 12.57	2	0.12	0.02	0.10	0.00	0.00	24.0
14	50	-10460	14	-278	0	-2059	1655	6.28	6.28 12.57 12.57	2	0.17	0.00	0.03	0.00	0.00	24.0
15	50	-10420	-43	126	0	78	1628	6.28	6.28 12.57 12.57	2	0.10	0.00	0.01	0.00	0.00	24.0
16	50	-10170	-455	-271	0	-2066	1714	6.28	6.28 12.57 12.57	2	0.17	0.01	0.04	0.00	0.00	24.0
17	50	-10120	-512	132	0	71	1687	6.28	6.28 12.57 12.57	2	0.10	0.01	0.05	0.00	0.00	24.0
18	50	-16630	2114	-361	0	-3222	2668	6.28	6.28 12.57 12.57	3	0.17	0.04	0.17	0.00	0.00	24.0
19	50	-12740	-3343	-77	0	-2415	2284	6.28	6.28 12.57 12.57	3	0.14	0.06	0.27	0.00	0.00	24.0
20	50	-14340	-601	-636	0	-1574	2422	6.28	6.28 12.57 12.57	3	0.14	0.01	0.06	0.00	0.00	24.0
37	50	-17620	4024	-416	0	-2998	2691	6.28	6.28 12.57 12.57	3	0.17	0.07	0.31	0.00	0.00	24.0
38	50	-11150	-5071	57	0	-1653	2051	6.28	6.28 12.57 12.57	3	0.12	0.09	0.47	0.00	0.00	24.0
39	50	-13820	-500	-875	0	-251	2281	6.28	6.28 12.57 12.57	3	0.12	0.02	0.08	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

VERIFICA NODO IN TESTA AL PILASTRO, NODO NUM. 325 NON CONFINATO

(par.7.2.2 NTC2018 "La domanda di resistenza valutata con i criteri della progettazione in capacità può essere assunta non superiore alla domanda di resistenza valutata per il caso di comportamento strutturale non dissipativo.")

PROGETTAZIONE IN CAPACITA'
Asse loc. pilastro y nodo ESTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 50.0 cm, hjc= 30.0 cm
Asse loc. pilastro z nodo: --

FxMin,inf	FxMin,sup	FxMax,sup	FySup	FzSup	Vjbdy	Vjbdz	Vres,y	Vres,z	I.R.compr.	Ashy	Ashz	PASSO	Nota
daN					daN		daN			cmq		cm	
-9794	-8107	-8475	129	57	17487	--	102326	--	0.17	--	--	40.00	

VERIFICA DI RESISTENZA CON SOLLECITAZIONI COMPORTAMENTO NON DISSIPATIVO

Asse loc. pilastro y nodo ESTERNO: Hjw= 40.0 cm, bj= 50.0 cm, hjc= 30.0 cm, db1= 45.0 cm

NC	Fx,sup	Fx,inf	Mb	Vb	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-8475	-10790	-2685	2317	655	5974	102326	0.06	0.00	40.00	
3	-8468	-10780	-2666	2310	647	5935	102328	0.06	0.00	40.00	
4	-8113	-9808	-793	1694	798	1159	102442	0.01	0.00	40.00	
5	-8107	-9794	-774	1688	806	1105	102444	0.01	0.00	40.00	
6	-8356	-10460	-2044	2107	156	4891	102364	0.05	0.00	40.00	
7	-8334	-10420	-1982	2084	129	4764	102371	0.05	0.00	40.00	
8	-8247	-10170	-1477	1920	280	3367	102399	0.03	0.00	40.00	
9	-8226	-10120	-1414	1898	307	3185	102406	0.03	0.00	40.00	
10	-8475	-10790	-2685	2317	655	5974	102326	0.06	0.00	40.00	
11	-8468	-10780	-2666	2310	647	5935	102328	0.06	0.00	40.00	
12	-8113	-9808	-793	1694	798	1159	102442	0.01	0.00	40.00	
13	-8107	-9794	-774	1688	806	1105	102444	0.01	0.00	40.00	
14	-8356	-10460	-2044	2107	156	4891	102364	0.05	0.00	40.00	
15	-8334	-10420	-1982	2084	129	4764	102371	0.05	0.00	40.00	
16	-8247	-10170	-1477	1920	280	3367	102399	0.03	0.00	40.00	
17	-8226	-10120	-1414	1898	307	3185	102406	0.03	0.00	40.00	

CONFRONTO E SINTESI CONCLUSIVE (si assume in ogni caso passo <= 15 cm)

I.R.compr.	Ashy	Ashz	PASSO	Nota
	cmq		cm	
0.06	--	--	15.00	**VERIFICATO**

ASTA NUM. 62 NI 1543 NF 1542 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 6
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-3786	122	-531	0	-310	5086	15.71	15.71	9.42	9.42	3	0.10	0.01	0.04	0.00	0.00	24.0
2	0	-3979	101	-251	0	-171	3235	15.71	15.71	9.42	9.42	2	0.09	0.00	0.02	0.00	0.00	24.0
3	0	-4114	88	-356	0	-168	3143	15.71	15.71	9.42	9.42	2	0.09	0.00	0.02	0.00	0.00	24.0
4	0	-1711	100	-461	0	-310	4681	15.71	15.71	9.42	9.42	2	0.13	0.01	0.03	0.00	0.00	24.0
5	0	-1846	88	-566	0	-307	4590	15.71	15.71	9.42	9.42	2	0.13	0.01	0.04	0.00	0.00	24.0
6	0	-3027	115	-202	0	-223	3848	15.71	15.71	9.42	9.42	2	0.11	0.00	0.01	0.00	0.00	24.0
7	0	-3478	74	-551	0	-213	3542	15.71	15.71	9.42	9.42	2	0.10	0.01	0.04	0.00	0.00	24.0
8	0	-2347	115	-266	0	-265	4282	15.71	15.71	9.42	9.42	2	0.12	0.00	0.02	0.00	0.00	24.0
9	0	-2797	73	-614	0	-254	3976	15.71	15.71	9.42	9.42	2	0.11	0.01	0.04	0.00	0.00	24.0
10	0	-3979	101	-251	0	-171	3235	15.71	15.71	9.42	9.42	2	0.09	0.00	0.02	0.00	0.00	24.0
11	0	-4114	88	-356	0	-168	3143	15.71	15.71	9.42	9.42	2	0.09	0.00	0.02	0.00	0.00	24.0
12	0	-1711	100	-461	0	-310	4681	15.71	15.71	9.42	9.42	2	0.13	0.01	0.03	0.00	0.00	24.0
13	0	-1846	88	-566	0	-307	4590	15.71	15.71	9.42	9.42	2	0.13	0.01	0.04	0.00	0.00	24.0
14	0	-3027	115	-202	0	-223	3848	15.71	15.71	9.42	9.42	2	0.11	0.00	0.01	0.00	0.00	24.0
15	0	-3478	74	-551	0	-213	3542	15.71	15.71	9.42	9.42	2	0.10	0.01	0.04	0.00	0.00	24.0
16	0	-2347	115	-266	0	-265	4282	15.71	15.71	9.42	9.42	2	0.12	0.00	0.02	0.00	0.00	24.0
17	0	-2797	73	-614	0	-254	3976	15.71	15.71	9.42	9.42	2	0.11	0.01	0.04	0.00	0.00	24.0
18	0	-6179	948	-707	0	-418	6268	15.71	15.71	9.42	9.42	3	0.12	0.01	0.08	0.00	0.00	24.0
19	0	7432	-322	-1434	0	-910	13630	15.71	15.71	9.42	9.42	3	0.28	0.02	0.10	0.00	0.00	24.0
20	0	-467	304	-1343	0	-630	8926	15.71	15.71	9.42	9.42	3	0.18	0.02	0.10	0.00	0.00	24.0
37	0	-12180	1309	-289	0	-138	2228	15.71	15.71	9.42	9.42	3	0.04	0.02	0.11	0.00	0.00	24.0
38	0	10510	-809	-1501	0	-959	14500	15.71	15.71	9.42	9.42	3	0.30	0.02	0.11	0.00	0.00	24.0
39	0	-2661	236	-1349	0	-492	6658	15.71	15.71	9.42	9.42	3	0.13	0.02	0.09	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
1	12	-3656	122	-531	0	-244	5101	15.71	15.71	9.42	9.42	3	0.10	0.01	0.04	0.00	0.00	24.0
2	12	-3879	101	-251	0	-140	3248	15.71	15.71	9.42	9.42	2	0.09	0.00	0.02	0.00	0.00	24.0
3	12	-4014	88	-356	0	-123	3154	15.71	15.71	9.42	9.42	2	0.09	0.00	0.02	0.00	0.00	24.0
4	12	-1611	100	-461	0	-252	4694	15.71	15.71	9.42	9.42	2	0.13	0.01	0.03	0.00	0.00	24.0
5	12	-1746	88	-566	0	-236	4601	15.71	15.71	9.42	9.42	2	0.13	0.01	0.04	0.00	0.00	24.0
6	12	-2927	115	-202	0	-198	3862	15.71	15.71	9.42	9.42	2	0.11	0.00	0.01	0.00	0.00	24.0
7	12	-3378	74	-551	0	-144	3551	15.71	15.71	9.42	9.42	2	0.10	0.01	0.04	0.00	0.00	24.0
8	12	-2247	115	-266	0	-232	4296	15.71	15.71	9.42	9.42	2	0.12	0.00	0.02	0.00	0.00	24.0
9	12	-2697	73	-614	0	-177	3985	15.71	15.71	9.42	9.42	2	0.11	0.01	0.04	0.00	0.00	24.0
10	12	-3879	101	-251	0	-140	3248	15.71	15.71	9.42	9.42	2	0.09	0.00	0.02	0.00	0.00	24.0
11	12	-4014	88	-356	0	-123	3154	15.71	15.71	9.42	9.42	2	0.09	0.00	0.02	0.00	0.00	24.0
12	12	-1611	100	-461	0	-252	4694	15.71	15.71	9.42	9.42	2	0.13	0.01	0.03	0.00	0.00	24.0
13	12	-1746	88	-566	0	-236	4601	15.71	15.71	9.42	9.42	2	0.13	0.01	0.04	0.00	0.00	24.0
14	12	-2927	115	-202	0	-198	3862	15.71	15.71	9.42	9.42	2	0.11	0.00	0.01	0.00	0.00	24.0
15	12	-3378	74	-551	0	-144	3551	15.71	15.71	9.42	9.42	2	0.10	0.01	0.04	0.00	0.00	24.0
16	12	-2247	115	-266	0	-232	4296	15.71	15.71	9.42	9.42	2	0.12	0.00	0.02	0.00	0.00	24.0
17	12	-2697	73	-614	0	-177	3985	15.71	15.71	9.42	9.42	2	0.11	0.01	0.04	0.00	0.00	24.0
18	12	-6049	948	-707	0	-330	6386	15.71	15.71	9.42	9.42	3	0.12	0.01	0.08	0.00	0.00	24.0
19	12	7562	-322	-1434	0	-731	13590	15.71	15.71	9.42	9.42	3	0.28	0.02	0.10	0.00	0.00	24.0
20	12	-337	304	-1343	0	-462	8964	15.71	15.71	9.42	9.42	3	0.18	0.02	0.10	0.00	0.00	24.0
37	12	-12050	1309	-289	0	-102	2392	15.71	15.71	9.42	9.42	3	0.04	0.02	0.11	0.00	0.00	24.0
38	12	10640	-809	-1501	0	-771	14397	15.71	15.71	9.42	9.42	3	0.30	0.02	0.11	0.00	0.00	24.0
39	12	-2531	236	-1349	0	-324	6688	15.71	15.71	9.42	9.42	3	0.13	0.02	0.09	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
1	25	-3526	122	-531	0	-178	5116	15.71	15.71	9.42	9.42	3	0.10	0.01	0.04	0.00	0.00	24.0
2	25	-3779	101	-251	0	-108	3260	15.71	15.71	9.42	9.42	2	0.09	0.00	0.02	0.00	0.00	24.0

3	25	-3914	88	-356	0	-79	3165	15.71	15.71	9.42	9.42	2	0.09	0.00	0.02	0.00	0.00	24.0
4	25	-1511	100	-461	0	-194	4706	15.71	15.71	9.42	9.42	2	0.13	0.01	0.03	0.00	0.00	24.0
5	25	-1646	88	-566	0	-165	4612	15.71	15.71	9.42	9.42	2	0.13	0.01	0.04	0.00	0.00	24.0
6	25	-2827	115	-202	0	-173	3876	15.71	15.71	9.42	9.42	2	0.11	0.00	0.01	0.00	0.00	24.0
7	25	-3278	74	-551	0	-75	3561	15.71	15.71	9.42	9.42	2	0.10	0.01	0.04	0.00	0.00	24.0
8	25	-2147	115	-266	0	-198	4310	15.71	15.71	9.42	9.42	2	0.12	0.00	0.02	0.00	0.00	24.0
9	25	-2597	73	-614	0	-101	3994	15.71	15.71	9.42	9.42	2	0.11	0.01	0.04	0.00	0.00	24.0
10	25	-3779	101	-251	0	-108	3260	15.71	15.71	9.42	9.42	2	0.09	0.00	0.02	0.00	0.00	24.0
11	25	-3914	88	-356	0	-79	3165	15.71	15.71	9.42	9.42	2	0.09	0.00	0.02	0.00	0.00	24.0
12	25	-1511	100	-461	0	-194	4706	15.71	15.71	9.42	9.42	2	0.13	0.01	0.03	0.00	0.00	24.0
13	25	-1646	88	-566	0	-165	4612	15.71	15.71	9.42	9.42	2	0.13	0.01	0.04	0.00	0.00	24.0
14	25	-2827	115	-202	0	-173	3876	15.71	15.71	9.42	9.42	2	0.11	0.00	0.01	0.00	0.00	24.0
15	25	-3278	74	-551	0	-75	3561	15.71	15.71	9.42	9.42	2	0.10	0.01	0.04	0.00	0.00	24.0
16	25	-2147	115	-266	0	-198	4310	15.71	15.71	9.42	9.42	2	0.12	0.00	0.02	0.00	0.00	24.0
17	25	-2597	73	-614	0	-101	3994	15.71	15.71	9.42	9.42	2	0.11	0.01	0.04	0.00	0.00	24.0
18	25	-5919	948	-707	0	-241	6505	15.71	15.71	9.42	9.42	3	0.12	0.01	0.08	0.00	0.00	24.0
19	25	7692	-322	-1434	0	-552	13550	15.71	15.71	9.42	9.42	3	0.28	0.02	0.10	0.00	0.00	24.0
20	25	-207	304	-1343	0	-295	9002	15.71	15.71	9.42	9.42	3	0.18	0.02	0.10	0.00	0.00	24.0
37	25	-11920	1309	-289	0	-66	2556	15.71	15.71	9.42	9.42	3	0.05	0.02	0.11	0.00	0.00	24.0
38	25	10770	-809	-1501	0	-584	14295	15.71	15.71	9.42	9.42	3	0.30	0.02	0.11	0.00	0.00	24.0
39	25	-2401	236	-1349	0	-155	6717	15.71	15.71	9.42	9.42	3	0.13	0.02	0.09	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-3396	122	-531	0	-111	5132	15.71	15.71	9.42	9.42	3	0.10	0.01	0.04	0.00	0.00	24.0
2	38	-3679	101	-251	0	-77	3273	15.71	15.71	9.42	9.42	2	0.09	0.00	0.02	0.00	0.00	24.0
3	38	-3814	88	-356	0	-35	3176	15.71	15.71	9.42	9.42	2	0.09	0.00	0.02	0.00	0.00	24.0
4	38	-1411	100	-461	0	-137	4718	15.71	15.71	9.42	9.42	2	0.13	0.01	0.03	0.00	0.00	24.0
5	38	-1546	88	-566	0	-94	4622	15.71	15.71	9.42	9.42	2	0.13	0.01	0.04	0.00	0.00	24.0
6	38	-2727	115	-202	0	-147	3891	15.71	15.71	9.42	9.42	2	0.11	0.00	0.01	0.00	0.00	24.0
7	38	-3178	74	-551	0	-6	3570	15.71	15.71	9.42	9.42	2	0.10	0.01	0.04	0.00	0.00	24.0
8	38	-2047	115	-266	0	-165	4325	15.71	15.71	9.42	9.42	2	0.12	0.00	0.02	0.00	0.00	24.0
9	38	-2497	73	-614	0	-24	4004	15.71	15.71	9.42	9.42	2	0.11	0.01	0.04	0.00	0.00	24.0
10	38	-3679	101	-251	0	-77	3273	15.71	15.71	9.42	9.42	2	0.09	0.00	0.02	0.00	0.00	24.0
11	38	-3814	88	-356	0	-35	3176	15.71	15.71	9.42	9.42	2	0.09	0.00	0.02	0.00	0.00	24.0
12	38	-1411	100	-461	0	-137	4718	15.71	15.71	9.42	9.42	2	0.13	0.01	0.03	0.00	0.00	24.0
13	38	-1546	88	-566	0	-94	4622	15.71	15.71	9.42	9.42	2	0.13	0.01	0.04	0.00	0.00	24.0
14	38	-2727	115	-202	0	-147	3891	15.71	15.71	9.42	9.42	2	0.11	0.00	0.01	0.00	0.00	24.0
15	38	-3178	74	-551	0	-6	3570	15.71	15.71	9.42	9.42	2	0.10	0.01	0.04	0.00	0.00	24.0
16	38	-2047	115	-266	0	-165	4325	15.71	15.71	9.42	9.42	2	0.12	0.00	0.02	0.00	0.00	24.0
17	38	-2497	73	-614	0	-24	4004	15.71	15.71	9.42	9.42	2	0.11	0.01	0.04	0.00	0.00	24.0
18	38	-5789	948	-707	0	-153	6623	15.71	15.71	9.42	9.42	3	0.12	0.01	0.08	0.00	0.00	24.0
19	38	7822	-322	-1434	0	-373	13510	15.71	15.71	9.42	9.42	3	0.27	0.02	0.10	0.00	0.00	24.0
20	38	-77	304	-1343	0	-127	9040	15.71	15.71	9.42	9.42	3	0.17	0.02	0.10	0.00	0.00	24.0
37	38	-11790	1309	-289	0	-30	2719	15.71	15.71	9.42	9.42	3	0.05	0.02	0.11	0.00	0.00	24.0
38	38	10900	-809	-1501	0	-396	14193	15.71	15.71	9.42	9.42	3	0.29	0.02	0.11	0.00	0.00	24.0
39	38	-2271	236	-1349	0	14	6746	15.71	15.71	9.42	9.42	3	0.13	0.02	0.09	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-3266	122	-531	0	-45	5147	15.71	15.71	9.42	9.42	3	0.10	0.01	0.04	0.00	0.00	24.0
2	50	-3579	101	-251	0	-46	3285	15.71	15.71	9.42	9.42	2	0.09	0.00	0.02	0.00	0.00	24.0
3	50	-3714	88	-356	0	10	3187	15.71	15.71	9.42	9.42	2	0.08	0.00	0.02	0.00	0.00	24.0
4	50	-1311	100	-461	0	-79	4731	15.71	15.71	9.42	9.42	2	0.13	0.01	0.03	0.00	0.00	24.0
5	50	-1446	88	-566	0	-23	4633	15.71	15.71	9.42	9.42	2	0.13	0.01	0.04	0.00	0.00	24.0
6	50	-2627	115	-202	0	-122	3905	15.71	15.71	9.42	9.42	2	0.11	0.00	0.01	0.00	0.00	24.0
7	50	-3078	74	-551	0	63	3579	15.71	15.71	9.42	9.42	2	0.10	0.01	0.04	0.00	0.00	24.0
8	50	-1947	115	-266	0	-132	4339	15.71	15.71	9.42	9.42	2	0.12	0.00	0.02	0.00	0.00	24.0
9	50	-2397	73	-614	0	53	4013	15.71	15.71	9.42	9.42	2	0.11	0.01	0.04	0.00	0.00	24.0
10	50	-3579	101	-251	0	-46	3285	15.71	15.71	9.42	9.42	2	0.09	0.00	0.02	0.00	0.00	24.0
11	50	-3714	88	-356	0	10	3187	15.71	15.71	9.42	9.42	2	0.08	0.00	0.02	0.00	0.00	24.0
12	50	-1311	100	-461	0	-79	4731	15.71	15.71	9.42	9.42	2	0.13	0.01	0.03	0.00	0.00	24.0
13	50	-1446	88	-566	0	-23	4633	15.71	15.71	9.42	9.42	2	0.13	0.01	0.04	0.00	0.00	24.0
14	50	-2627	115	-202	0	-122	3905	15.71	15.71	9.42	9.42	2	0.11	0.00	0.01	0.00	0.00	24.0
15	50	-3078	74	-551	0	63	3579	15.71	15.71	9.42	9.42	2	0.10	0.01	0.04	0.00	0.00	24.0
16	50	-1947	115	-266	0	-132	4339	15.71	15.71	9.42	9.42	2	0.12	0.00	0.02	0.00	0.00	24.0
17	50	-2397	73	-614	0	53	4013	15.71	15.71	9.42	9.42	2	0.11	0.01	0.04	0.00	0.00	24.0
18	50	-5659	948	-707	0	-65	6742	15.71	15.71	9.42	9.42	3	0.13	0.01	0.08	0.00	0.00	24.0
19	50	7952	-322	-1434	0	-193	13470	15.71	15.71	9.42	9.42	3	0.27	0.02	0.10	0.00	0.00	24.0
20	50	53	304	-1343	0	41	9078	15.71	15.71	9.42	9.42	3	0.18	0.02	0.10	0.00	0.00	24.0
37	50	-11660	1309	-289	0	6	2883	15.71	15.71	9.42	9.42	3	0.05	0.02	0.11	0.00	0.00	24.0
38	50	11030	-809	-1501	0	-209	14090	15.71	15.71	9.42	9.42	3	0.29	0.02	0.11	0.00	0.00	24.0
39	50	-2141	236	-1349	0	182	6776	15.71	15.71	9.42	9.42	3	0.13	0.02	0.09	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 63 NI 1542 NF 78 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 6A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-8461	1257	-222	0	-45	6050	15.71	15.71	9.42	9.42	3	0.11	0.02	0.11	0.00	0.00	24.0
2	0	-7430	820	-17	0	-46	3959	15.71	15.71	9.42	9.42	2	0.10	0.01	0.07	0.00	0.00	24.0
3	0	-7543	796	-340	0	10	3859	15.71	15.71	9.42	9.42	2	0.10	0.01	0.07	0.00	0.00	24.0
4	0	-5475	1138	-2	0	-79	5449	15.71	15.71	9.42	9.42	2	0.14	0.01	0.10	0.00	0.00	24.0
5	0	-5588	1115	-325	0	-23	5349	15.71	15.71	9.42	9.42	2	0.14	0.01	0.10	0.00	0.00	24.0
6	0	-6613	959	365	0	-122	4597	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
7	0	-6990	880	-711	0	63	4264	15.71	15.71	9.42	9.42	2	0.11	0.01	0.08	0.00	0.00	24.0
8	0	-6027	1055	369	0	-132	5044	15.71	15.71	9.42	9.42	2	0.14	0.01	0.09	0.00	0.00	24.0
9	0	-6404	975	-706	0	53	4711	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
10	0	-7430	820	-17	0	-46	3959	15.71	15.71	9.42	9.42	2	0.10	0.01	0.07	0.00	0.00	24.0
11	0	-7543	796	-340	0	10	3859	15.71	15.71	9.42	9.42	2	0.10	0.01	0.07	0.00	0.00	24.0
12	0	-5475	1138	-2	0	-79	5449	15.71	15.71	9.42	9.42	2	0.14	0.01	0.10	0.00	0.00	24.0
13	0	-5588	1115	-325	0	-23	5349	15.71	15.71	9.42	9.42	2	0.14	0.01	0.10	0.00	0.00	24.0
14	0	-6613	959	365	0	-122	4597	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
15	0	-6990	880	-711	0	63	4264	15.71	15.71	9.42	9.42	2	0.11	0.01	0.08	0.00	0.00	24.0
16	0	-6027	1055	369	0	-132	5044	15.71	15.71	9.42	9.42	2	0.14	0.01	0.09	0.00	0.00	24.0
17	0	-6404	975	-706	0	53	4711	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
18	0	-12590	2682	-352	0	-65	8115	15.71	15.71	9.42	9.42	3	0.15	0.03	0.22	0.00	0.00	24.0
19	0	-186	2326	-29	0	-193	14690	15.71	15.71	9.42	9.42	3	0.28	0.03	0.22	0.00	0.00	24.0
20	0	-7145	2311	-1238	0	41	10330	15.71	15.71	9.42	9.42	3	0.19	0.03	0.20	0.00	0.00	24.0
37	0	-17430	2395	-471	0	6	4181	15.71	15.71	9.42	9.42	3	0.07	0.03	0.18	0.00	0.00	24.0
38	0	3238	1801	67	0	-209	15130	15.71	15.71	9.42	9.42	3	0.30	0.02	0.17	0.00	0.00	24.0
39	0	-8360	1776	-1948	0	182	7874	15.71	15.71	9.42	9.42	3	0.15	0.03	0.15	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-8331	1257	-222	0	-17	6207	15.71	15.71	9.42	9.42	3	0.12	0.02	0.11	0.00	0.00	24.0
2	12	-7330	820	-17	0	-43	4061	15.71	15.71	9.42	9.42	2	0.11	0.01	0.07	0.00	0.00	24.0
3	12	-7443	796	-340	0	52	3958	15.71	15.71	9.42	9.42	2	0.10	0.01	0.07	0.00	0.00	24.0
4	12	-5375	1138	-2	0	-79	5591	15.71	15.71	9.42	9.42	2	0.15	0.01	0.10	0.00	0.00	24.0
5	12	-5488	1115	-325	0	17	5488	15.71	15.71	9.42	9.42	2	0.14	0.01	0.10	0.00	0.00	24.0
6	12	-6513	959	365	0	-168	4717	15.71	15.71	9.42	9.42	2	0.13	0.01	0.08	0.00	0.00	24.0
7	12	-6890	880	-711	0	152	4374	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
8	12	-5927	1055	369	0	-178	5176	15.71	15.71	9.42	9.42	2	0.14	0.01	0.09	0.00	0.00	24.0
9	12	-6304	975	-706	0	141	4833	15.71	15.71	9.42	9.42	2	0.13	0.01	0.08	0.00	0.00	24.0
10	12	-7330	820	-17	0	-43	4061	15.71	15.71	9.42	9.42	2	0.11	0.01	0.07	0.00	0.00	24.0
11	12	-7443	796	-340	0	52	3958	15.71	15.71	9.42	9.42	2	0.10	0.01	0.07	0.00	0.00	24.0
12	12	-5375	1138	-2	0	-79	5591	15.71	15.71	9.42	9.42	2	0.15	0.01	0.10	0.00	0.00	24.0
13	12	-5488	1115	-325	0	17	5488	15.71	15.71	9.42	9.42	2	0.14	0.01	0.10	0.00	0.00	24.0
14	12	-6513	959	365	0	-168	4717	15.71	15.71	9.42	9.42	2	0.13	0.01	0.08	0.00	0.00	24.0
15	12	-6890	880	-711	0	152	4374	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
16	12	-5927	1055	369	0	-178	5176	15.71	15.71	9.42	9.42	2	0.14	0.01	0.09	0.00	0.00	24.0
17	12	-6304	975	-706	0	141	4833	15.71	15.71	9.42	9.42	2	0.13	0.01	0.08	0.00	0.00	24.0
18	12	-12460	2682	-352	0	-21	8450	15.71	15.71	9.42	9.42	3	0.15	0.03	0.22	0.00	0.00	24.0
19	12	-56	2326	-29	0	-190	14980	15.71	15.71	9.42	9.42	3	0.29	0.03	0.22	0.00	0.00	24.0
20	12	-7015	2311	-1238	0	196	10620	15.71	15.71	9.42	9.42	3	0.20	0.03	0.20	0.00	0.00	24.0
37	12	-17300	2395	-471	0	65	4480	15.71	15.71	9.42	9.42	3	0.08	0.03	0.18	0.00	0.00	24.0
38	12	3368	1801	67	0	-217	15355	15.71	15.71	9.42	9.42	3	0.30	0.02	0.17	0.00	0.00	24.0
39	12	-8230	1776	-1948	0	426	8096	15.71	15.71	9.42	9.42	3	0.15	0.03	0.15	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-8201	1257	-222	0	11	6364	15.71	15.71	9.42	9.42	3	0.12	0.02	0.11	0.00	0.00	24.0
2	25	-7230	820	-17	0	-41	4164	15.71	15.71	9.42	9.42	2	0.11	0.01	0.07	0.00	0.00	24.0
3	25	-7343	796	-340	0	95	4058	15.71	15.71	9.42	9.42	2	0.11	0.01	0.07	0.00	0.00	24.0
4	25	-5275	1138	-2	0	-79	5734	15.71	15.71	9.42	9.42	2	0.15	0.01	0.10	0.00	0.00	24.0
5	25	-5388	1115	-325	0	58	5627	15.71	15.71	9.42	9.42	2	0.15	0.01	0.10	0.00	0.00	24.0
6	25	-6413	959	365	0	-213	4837	15.71	15.71	9.42	9.42	2	0.13	0.01	0.08	0.00	0.00	24.0
7	25	-6790	880	-711	0	241	4484	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
8	25	-5827	1055	369	0	-224	5308	15.71	15.71	9.42	9.42	2	0.14	0.01	0.09	0.00	0.00	24.0
9	25	-6204	975	-706	0	230	4954	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
10	25	-7230	820	-17	0	-41	4164	15.71	15.71	9.42	9.42	2	0.11	0.01	0.07	0.00	0.00	24.0
11	25	-7343	796	-340	0	95	4058	15.71	15.71	9.42	9.42	2	0.11	0.01	0.07	0.00	0.00	24.0
12	25	-5275	1138	-2	0	-79	5734	15.71	15.71	9.42	9.42	2	0.15	0.01	0.10	0.00	0.00	24.0
13	25	-5388	1115	-325	0	58	5627	15.71	15.71	9.42	9.42	2	0.15	0.01	0.10	0.00	0.00	24.0
14	25	-6413	959	365	0	-213	4837	15.71	15.71	9.42	9.42	2	0.13	0.01	0.08	0.00	0.00	24.0
15	25	-6790	880	-711	0	241	4484	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
16	25	-5827	1055	369	0	-224	5308	15.71	15.71	9.42	9.42	2	0.14	0.01	0.09	0.00	0.00	24.0
17	25	-6204	975	-706	0	230	4954	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
18	25	-12330	2682	-352	0	23	8786	15.71	15.71	9.42	9.42	3	0.16	0.03	0.22	0.00	0.00	24.0
19	25	74	2326	-29	0	-186	15270	15.71	15.71	9.42	9.42	3	0.30	0.03	0.22	0.00	0.00	24.0
20	25	-6885	2311	-1238	0	351	10910	15.71	15.71	9.42	9.42	3	0.21	0.03	0.20	0.00	0.00	24.0
37	25	-17170	2395	-471	0	124	4780	15.71	15.71	9.42	9.42	3	0.09	0.03	0.18	0.00	0.00	24.0
38	25	3498	1801	67	0	-225	15580	15.71	15.71	9.42	9.42	3	0.31	0.02	0.17	0.00	0.00	24.0
39	25	-8100	1776	-1948	0	669	8318	15.71	15.71	9.42	9.42	3	0.16	0.03	0.15	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-8071	1257	-222	0	38	6522	15.71	15.71	9.42	9.42	3	0.12	0.02	0.11	0.00	0.00	24.0
2	38	-7130	820	-17	0	-39	4267	15.71	15.71	9.42	9.42	2	0.11	0.01	0.07	0.00	0.00	24.0
3	38	-7243	796	-340	0	137	4157	15.71	15.71	9.42	9.42	2	0.11	0.01	0.07	0.00	0.00	24.0
4	38	-5175	1138	-2	0	-78	5876	15.71	15.71	9.42	9.42	2	0.16	0.01	0.10	0.00	0.00	24.0
5	38	-5288	1115	-325	0	98	5767	15.71	15.71	9.42	9.42	2	0.15	0.01	0.10	0.00	0.00	24.0
6	38	-6313	959	365	0	-259	4956	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
7	38	-6690	880	-711	0	330	4593	15.71	15.71	9.42	9.42	2	0.13	0.01	0.08	0.00	0.00	24.0
8	38	-5727	1055	369	0	-271	5439	15.71	15.71	9.42	9.42	2	0.15	0.01	0.09	0.00	0.00	24.0
9	38	-6104	975	-706	0	318	5076	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
10	38	-7130	820	-17	0	-39	4267	15.71	15.71	9.42	9.42	2	0.11	0.01	0.07	0.00	0.00	24.0
11	38	-7243	796	-340	0	137	4157	15.71	15.71	9.42	9.42	2	0.11	0.01	0.07	0.00	0.00	24.0
12	38	-5175	1138	-2	0	-78	5876	15.71	15.71	9.42	9.42	2	0.16	0.01	0.10	0.00	0.00	24.0
13	38	-5288	1115	-325	0	98	5767	15.71	15.71	9.42	9.42	2	0.15	0.01	0.10	0.00	0.00	24.0
14	38	-6313	959	365	0	-259	4956	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
15	38	-6690	880	-711	0	330	4593	15.71	15.71	9.42	9.42	2	0.13	0.01	0.08	0.00	0.00	24.0
16	38	-5727	1055	369	0	-271	5439	15.71	15.71	9.42	9.42	2	0.15	0.01	0.09	0.00	0.00	24.0
17	38	-6104	975	-706	0	318	5076	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
18	38	-12200	2682	-352	0	67	9121	15.71	15.71	9.42	9.42	3	0.17	0.03	0.22	0.00	0.00	24.0
19	38	204	2326	-29	0	-182	15560	15.71	15.71	9.42	9.42	3	0.30	0.03	0.22	0.00	0.00	24.0
20	38	-6755	2311	-1238	0	506	11200	15.71	15.71	9.42	9.42	3	0.21	0.03	0.20	0.00	0.00	24.0
37	38	-17040	2395	-471	0	182	5079	15.71	15.71	9.42	9.42	3	0.09	0.03	0.18	0.00	0.00	24.0
38	38	3628	1801	67	0	-234	15805	15.71	15.71	9.42	9.42	3	0.31	0.02	0.17	0.00	0.00	24.0
39	38	-7970	1776	-1948	0	913	8539	15.71	15.71	9.42	9.42	3	0.17	0.03	0.15	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-7941	1257	-222	0	66	6679	15.71	15.71	9.42	9.42	3	0.12	0.02	0.11	0.00	0.00	24.0
2	50	-7030	820	-17	0	-37	4369	15.71	15.71	9.42	9.42	2	0.11	0.01	0.07	0.00	0.00	24.0
3	50	-7143	796	-340	0	180	4257	15.71	15.71	9.42	9.42	2	0.11	0.01	0.07	0.00	0.00	24.0
4	50	-5075	1138	-2	0	-78	6018	15.71	15.71	9.42	9.42	2	0.16	0.01	0.10	0.00	0.00	24.0
5	50	-5188	1115	-325	0	139	5906	15.71	15.71	9.42	9.42	2	0.16	0.01	0.10	0.00	0.00	24.0
6	50	-6213	959	365	0	-304	5076	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
7	50	-6590	880	-711	0	418	4703	15.71	15.71	9.42	9.42	2	0.13	0.01	0.08	0.00	0.00	24.0
8	50	-5627	1055	369	0	-317	5571	15.71	15.71	9.42	9.42	2	0.15	0.01	0.09	0.00	0.00	24.0
9	50	-6004	975	-706	0	406	5198	15.71	15.71	9.42	9.42	2	0.15	0.01	0.08	0.00	0.00	24.0
10	50	-7030	820	-17	0	-37	4369	15.71	15.71	9.42	9.42	2	0.11	0.01	0.07	0.00	0.00	24.0
11	50	-7143	796	-340	0	180	4257	15.71	15.71	9.42	9.42	2	0.11	0.01	0.07	0.00	0.00	24.0
12	50	-5075	1138	-2	0	-78	6018	15.71	15.71	9.42	9.42	2	0.16	0.01	0.10	0.00	0.00	24.0
13	50	-5188	1115	-325	0	139	5906	15.71	15.71	9.42	9.42	2	0.16	0.01	0.10	0.00	0.00	24.0
14	50	-6213	959	365	0	-304	5076	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
15	50	-6590	880	-711	0	418	4703	15.71	15.71	9.42	9.42	2	0.13	0.01	0.08	0.00	0.00	24.0
16	50	-5627	1055	369	0	-317	5571	15.71	15.71	9.42	9.42	2	0.15	0.01	0.09	0.00	0.00	24.0
17	50	-6004	975	-706	0	406	5198	15.71	15.71	9.42	9.42	2	0.15	0.01	0.08	0.00	0.00	24.0
18	50	-12070	2682	-352	0	111	9456	15.71	15.71	9.42	9.42	3	0.17	0.03	0.22	0.00	0.00	24.0
19	50	334	2326	-29	0	-179	15850	15.71	15.71	9.42	9.42	3	0.31	0.03	0.22	0.00	0.00	24.0
20	50	-6625	2311	-1238	0	660	11490	15.71	15.71	9.42	9.42	3	0.22	0.03	0.20	0.00	0.00	24.0
37	50	-16910	2395	-471	0	241	5378	15.71	15.71	9.42	9.42	3	0.10	0.03	0.18	0.00	0.00	24.0
38	50	3758	1801	67	0	-242	16030	15.71	15.71	9.42	9.42	3	0.32	0.02	0.17	0.00	0.00	24.0
39	50	-7840	1776	-1948	0	1156	8761	15.71	15.71	9.42	9.42	3	0.17	0.03	0.15	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 64 NI 1581 NF 121 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 5A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-4292	2409	161	0	-62	10480	15.71	15.71	9.42	9.42	3	0.20	0.03	0.21	0.00	0.00	24.0
2	0	-5317	1457	279	0	-66	6400	15.71	15.71	9.42	9.42	2	0.17	0.02	0.13	0.00	0.00	24.0
3	0	-5333	1465	-38	0	-9	6404	15.71	15.71	9.42	9.42	2	0.17	0.02	0.13	0.00	0.00	24.0
4	0	-1271	2241	285	0	-86	9712	15.71	15.71	9.42	9.42	2	0.26	0.03	0.21	0.00	0.00	24.0
5	0	-1286	2250	-31	0	-29	9717	15.71	15.71	9.42	9.42	2	0.26	0.03	0.21	0.00	0.00	24.0
6	0	-3883	1722	651	0	-139	7554	15.71	15.71	9.42	9.42	2	0.20	0.02	0.15	0.00	0.00	24.0
7	0	-3934	1749	-405	0	50	7568	15.71	15.71	9.42	9.42	2	0.20	0.02	0.16	0.00	0.00	24.0
8	0	-2669	1957	653	0	-145	8548	15.71	15.71	9.42	9.42	2	0.23	0.03	0.18	0.00	0.00	24.0
9	0	-2720	1985	-403	0	44	8562	15.71	15.71	9.42	9.42	2	0.23	0.03	0.18	0.00	0.00	24.0
10	0	-5317	1457	279	0	-66	6400	15.71	15.71	9.42	9.42	2	0.17	0.02	0.13	0.00	0.00	24.0
11	0	-5333	1465	-38	0	-9	6404	15.71	15.71	9.42	9.42	2	0.17	0.02	0.13	0.00	0.00	24.0
12	0	-1271	2241	285	0	-86	9712	15.71	15.71	9.42	9.42	2	0.26	0.03	0.21	0.00	0.00	24.0
13	0	-1286	2250	-31	0	-29	9717	15.71	15.71	9.42	9.42	2	0.26	0.03	0.21	0.00	0.00	24.0
14	0	-3883	1722	651	0	-139	7554	15.71	15.71	9.42	9.42	2	0.20	0.02	0.15	0.00	0.00	24.0
15	0	-3934	1749	-405	0	50	7568	15.71	15.71	9.42	9.42	2	0.20	0.02	0.16	0.00	0.00	24.0
16	0	-2669	1957	653	0	-145	8548	15.71	15.71	9.42	9.42	2	0.23	0.03	0.18	0.00	0.00	24.0
17	0	-2720	1985	-403	0	44	8562	15.71	15.71	9.42	9.42	2	0.23	0.03	0.18	0.00	0.00	24.0
18	0	-6983	4381	351	0	-104	14530	15.71	15.71	9.42	9.42	3	0.27	0.06	0.38	0.00	0.00	24.0
19	0	11010	4994	386	0	-161	25710	15.71	15.71	9.42	9.42	3	0.53	0.07	0.47	0.00	0.00	24.0
20	0	1126	4367	-661	0	59	18700	15.71	15.71	9.42	9.42	3	0.36	0.06	0.41	0.00	0.00	24.0
37	0	-15070	3436	270	0	-62	7666	15.71	15.71	9.42	9.42	3	0.14	0.04	0.27	0.00	0.00	24.0
38	0	14930	4457	329	0	-156	26300	15.71	15.71	9.42	9.42	3	0.55	0.06	0.42	0.00	0.00	24.0
39	0	-1552	3411	-1417	0	209	14620	15.71	15.71	9.42	9.42	3	0.28	0.04	0.31	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-4162	2409	161	0	-82	10780	15.71	15.71	9.42	9.42	3	0.20	0.03	0.21	0.00	0.00	24.0
2	12	-5217	1457	279	0	-101	6582	15.71	15.71	9.42	9.42	2	0.18	0.02	0.13	0.00	0.00	24.0
3	12	-5233	1465	-38	0	-5	6587	15.71	15.71	9.42	9.42	2	0.17	0.02	0.13	0.00	0.00	24.0
4	12	-1171	2241	285	0	-122	9992	15.71	15.71	9.42	9.42	2	0.27	0.03	0.21	0.00	0.00	24.0
5	12	-1186	2250	-31	0	-25	9998	15.71	15.71	9.42	9.42	2	0.27	0.03	0.21	0.00	0.00	24.0
6	12	-3783	1722	651	0	-221	7769	15.71	15.71	9.42	9.42	2	0.21	0.02	0.15	0.00	0.00	24.0
7	12	-3834	1749	-405	0	100	7787	15.71	15.71	9.42	9.42	2	0.21	0.02	0.16	0.00	0.00	24.0
8	12	-2569	1957	653	0	-227	8793	15.71	15.71	9.42	9.42	2	0.24	0.03	0.18	0.00	0.00	24.0
9	12	-2620	1985	-403	0	94	8810	15.71	15.71	9.42	9.42	2	0.24	0.03	0.18	0.00	0.00	24.0
10	12	-5217	1457	279	0	-101	6582	15.71	15.71	9.42	9.42	2	0.18	0.02	0.13	0.00	0.00	24.0
11	12	-5233	1465	-38	0	-5	6587	15.71	15.71	9.42	9.42	2	0.17	0.02	0.13	0.00	0.00	24.0
12	12	-1171	2241	285	0	-122	9992	15.71	15.71	9.42	9.42	2	0.27	0.03	0.21	0.00	0.00	24.0
13	12	-1186	2250	-31	0	-25	9998	15.71	15.71	9.42	9.42	2	0.27	0.03	0.21	0.00	0.00	24.0
14	12	-3783	1722	651	0	-221	7769	15.71	15.71	9.42	9.42	2	0.21	0.02	0.15	0.00	0.00	24.0
15	12	-3834	1749	-405	0	100	7787	15.71	15.71	9.42	9.42	2	0.21	0.02	0.16	0.00	0.00	24.0
16	12	-2569	1957	653	0	-227	8793	15.71	15.71	9.42	9.42	2	0.24	0.03	0.18	0.00	0.00	24.0
17	12	-2620	1985	-403	0	94	8810	15.71	15.71	9.42	9.42	2	0.24	0.03	0.18	0.00	0.00	24.0
18	12	-6853	4381	351	0	-148	15078	15.71	15.71	9.42	9.42	3	0.28	0.06	0.38	0.00	0.00	24.0
19	12	11140	4994	386	0	-209	26335	15.71	15.71	9.42	9.42	3	0.54	0.07	0.47	0.00	0.00	24.0
20	12	1256	4367	-661	0	141	19247	15.71	15.71	9.42	9.42	3	0.37	0.06	0.41	0.00	0.00	24.0
37	12	-14940	3436	270	0	-95	8096	15.71	15.71	9.42	9.42	3	0.15	0.04	0.27	0.00	0.00	24.0
38	12	15060	4457	329	0	-197	26858	15.71	15.71	9.42	9.42	3	0.57	0.06	0.42	0.00	0.00	24.0
39	12	-1422	3411	-1417	0	386	15045	15.71	15.71	9.42	9.42	3	0.29	0.04	0.31	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-4032	2409	161	0	-102	11080	15.71	15.71	9.42	9.42	3	0.21	0.03	0.21	0.00	0.00	24.0
2	25	-5117	1457	279	0	-136	6764	15.71	15.71	9.42	9.42	2	0.18	0.02	0.13	0.00	0.00	24.0
3	25	-5133	1465	-38	0	0	6770	15.71	15.71	9.42	9.42	2	0.18	0.02	0.13	0.00	0.00	24.0
4	25	-1071	2241	285	0	-157	10271	15.71	15.71	9.42	9.42	2	0.28	0.03	0.21	0.00	0.00	24.0
5	25	-1086	2250	-31	0	-21	10278	15.71	15.71	9.42	9.42	2	0.28	0.03	0.21	0.00	0.00	24.0
6	25	-3683	1722	651	0	-302	7984	15.71	15.71	9.42	9.42	2	0.22	0.02	0.15	0.00	0.00	24.0
7	25	-3734	1749	-405	0	151	8006	15.71	15.71	9.42	9.42	2	0.22	0.02	0.16	0.00	0.00	24.0
8	25	-2469	1957	653	0	-308	9038	15.71	15.71	9.42	9.42	2	0.25	0.03	0.18	0.00	0.00	24.0
9	25	-2520	1985	-403	0	145	9058	15.71	15.71	9.42	9.42	2	0.25	0.03	0.18	0.00	0.00	24.0
10	25	-5117	1457	279	0	-136	6764	15.71	15.71	9.42	9.42	2	0.18	0.02	0.13	0.00	0.00	24.0
11	25	-5133	1465	-38	0	0	6770	15.71	15.71	9.42	9.42	2	0.18	0.02	0.13	0.00	0.00	24.0
12	25	-1071	2241	285	0	-157	10271	15.71	15.71	9.42	9.42	2	0.28	0.03	0.21	0.00	0.00	24.0
13	25	-1086	2250	-31	0	-21	10278	15.71	15.71	9.42	9.42	2	0.28	0.03	0.21	0.00	0.00	24.0
14	25	-3683	1722	651	0	-302	7984	15.71	15.71	9.42	9.42	2	0.22	0.02	0.15	0.00	0.00	24.0
15	25	-3734	1749	-405	0	151	8006	15.71	15.71	9.42	9.42	2	0.22	0.02	0.16	0.00	0.00	24.0
16	25	-2469	1957	653	0	-308	9038	15.71	15.71	9.42	9.42	2	0.25	0.03	0.18	0.00	0.00	24.0
17	25	-2520	1985	-403	0	145	9058	15.71	15.71	9.42	9.42	2	0.25	0.03	0.18	0.00	0.00	24.0
18	25	-6723	4381	351	0	-191	15625	15.71	15.71	9.42	9.42	3	0.29	0.06	0.38	0.00	0.00	24.0
19	25	11270	4994	386	0	-257	26960	15.71	15.71	9.42	9.42	3	0.56	0.07	0.47	0.00	0.00	24.0
20	25	1386	4367	-661	0	224	19795	15.71	15.71	9.42	9.42	3	0.39	0.06	0.41	0.00	0.00	24.0
37	25	-14810	3436	270	0	-129	8525	15.71	15.71	9.42	9.42	3	0.15	0.04	0.27	0.00	0.00	24.0
38	25	15190	4457	329	0	-239	27415	15.71	15.71	9.42	9.42	3	0.58	0.06	0.42	0.00	0.00	24.0
39	25	-1292	3411	-1417	0	564	15470	15.71	15.71	9.42	9.42	3	0.30	0.04	0.31	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-3902	2409	161	0	-122	11380	15.71	15.71	9.42	9.42	3	0.22	0.03	0.21	0.00	0.00	24.0
2	38	-5017	1457	279	0	-171	6946	15.71	15.71	9.42	9.42	2	0.19	0.02	0.13	0.00	0.00	24.0
3	38	-5033	1465	-38	0	5	6954	15.71	15.71	9.42	9.42	2	0.18	0.02	0.13	0.00	0.00	24.0
4	38	-971	2241	285	0	-193	10551	15.71	15.71	9.42	9.42	2	0.29	0.03	0.21	0.00	0.00	24.0
5	38	-986	2250	-31	0	-18	10559	15.71	15.71	9.42	9.42	2	0.29	0.03	0.21	0.00	0.00	24.0
6	38	-3583	1722	651	0	-383	8200	15.71	15.71	9.42	9.42	2	0.23	0.02	0.15	0.00	0.00	24.0
7	38	-3634	1749	-405	0	202	8224	15.71	15.71	9.42	9.42	2	0.22	0.02	0.16	0.00	0.00	24.0
8	38	-2369	1957	653	0	-390	9282	15.71	15.71	9.42	9.42	2	0.26	0.03	0.18	0.00	0.00	24.0
9	38	-2420	1985	-403	0	195	9306	15.71	15.71	9.42	9.42	2	0.25	0.03	0.18	0.00	0.00	24.0
10	38	-5017	1457	279	0	-171	6946	15.71	15.71	9.42	9.42	2	0.19	0.02	0.13	0.00	0.00	24.0
11	38	-5033	1465	-38	0	5	6954	15.71	15.71	9.42	9.42	2	0.18	0.02	0.13	0.00	0.00	24.0
12	38	-971	2241	285	0	-193	10551	15.71	15.71	9.42	9.42	2	0.29	0.03	0.21	0.00	0.00	24.0
13	38	-986	2250	-31	0	-18	10559	15.71	15.71	9.42	9.42	2	0.29	0.03	0.21	0.00	0.00	24.0
14	38	-3583	1722	651	0	-383	8200	15.71	15.71	9.42	9.42	2	0.23	0.02	0.15	0.00	0.00	24.0
15	38	-3634	1749	-405	0	202	8224	15.71	15.71	9.42	9.42	2	0.22	0.02	0.16	0.00	0.00	24.0
16	38	-2369	1957	653	0	-390	9282	15.71	15.71	9.42	9.42	2	0.26	0.03	0.18	0.00	0.00	24.0
17	38	-2420	1985	-403	0	195	9306	15.71	15.71	9.42	9.42	2	0.25	0.03	0.18	0.00	0.00	24.0
18	38	-6593	4381	351	0	-235	16172	15.71	15.71	9.42	9.42	3	0.30	0.06	0.38	0.00	0.00	24.0
19	38	11400	4994	386	0	-305	27585	15.71	15.71	9.42	9.42	3	0.57	0.07	0.47	0.00	0.00	24.0
20	38	1516	4367	-661	0	307	20342	15.71	15.71	9.42	9.42	3	0.40	0.06	0.41	0.00	0.00	24.0
37	38	-14680	3436	270	0	-163	8955	15.71	15.71	9.42	9.42	3	0.16	0.04	0.27	0.00	0.00	24.0
38	38	15320	4457	329	0	-280	27973	15.71	15.71	9.42	9.42	3	0.59	0.06	0.42	0.00	0.00	24.0
39	38	-1162	3411	-1417	0	741	15895	15.71	15.71	9.42	9.42	3	0.31	0.04	0.31	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-3772	2409	161	0	-142	11680	15.71	15.71	9.42	9.42	3	0.22	0.03	0.22	0.00	0.00	24.0
2	50	-4917	1457	279	0	-206	7128	15.71	15.71	9.42	9.42	2	0.19	0.02	0.13	0.00	0.00	24.0
3	50	-4933	1465	-38	0	9	7137	15.71	15.71	9.42	9.42	2	0.19	0.02	0.13	0.00	0.00	24.0
4	50	-870	2241	285	0	-229	10830	15.71	15.71	9.42	9.42	2	0.30	0.03	0.21	0.00	0.00	24.0
5	50	-886	2250	-31	0	-14	10840	15.71	15.71	9.42	9.42	2	0.29	0.03	0.21	0.00	0.00	24.0
6	50	-3483	1722	651	0	-465	8415	15.71	15.71	9.42	9.42	2	0.24	0.02	0.15	0.00	0.00	24.0
7	50	-3534	1749	-405	0	252	8443	15.71	15.71	9.42	9.42	2	0.23	0.02	0.16	0.00	0.00	24.0
8	50	-2269	1957	653	0	-472	9527	15.71	15.71	9.42	9.42	2	0.27	0.03	0.18	0.00	0.00	24.0
9	50	-2320	1985	-403	0	245	9554	15.71	15.71	9.42	9.42	2	0.26	0.03	0.18	0.00	0.00	24.0
10	50	-4917	1457	279	0	-206	7128	15.71	15.71	9.42	9.42	2	0.19	0.02	0.13	0.00	0.00	24.0
11	50	-4933	1465	-38	0	9	7137	15.71	15.71	9.42	9.42	2	0.19	0.02	0.13	0.00	0.00	24.0
12	50	-870	2241	285	0	-229	10830	15.71	15.71	9.42	9.42	2	0.30	0.03	0.21	0.00	0.00	24.0
13	50	-886	2250	-31	0	-14	10840	15.71	15.71	9.42	9.42	2	0.29	0.03	0.21	0.00	0.00	24.0
14	50	-3483	1722	651	0	-465	8415	15.71	15.71	9.42	9.42	2	0.24	0.02	0.15	0.00	0.00	24.0
15	50	-3534	1749	-405	0	252	8443	15.71	15.71	9.42	9.42	2	0.23	0.02	0.16	0.00	0.00	24.0
16	50	-2269	1957	653	0	-472	9527	15.71	15.71	9.42	9.42	2	0.27	0.03	0.18	0.00	0.00	24.0
17	50	-2320	1985	-403	0	245	9554	15.71	15.71	9.42	9.42	2	0.26	0.03	0.18	0.00	0.00	24.0
18	50	-6463	4381	351	0	-279	16720	15.71	15.71	9.42	9.42	3	0.31	0.06	0.38	0.00	0.00	24.0
19	50	11530	4994	386	0	-354	28210	15.71	15.71	9.42	9.42	3	0.58	0.07	0.47	0.00	0.00	24.0
20	50	1646	4367	-661	0	389	20890	15.71	15.71	9.42	9.42	3	0.41	0.06	0.41	0.00	0.00	24.0
37	50	-14550	3436	270	0	-196	9384	15.71	15.71	9.42	9.42	3	0.17	0.04	0.27	0.00	0.00	24.0
38	50	15450	4457	329	0	-321	28530	15.71	15.71	9.42	9.42	3	0.60	0.06	0.42	0.00	0.00	24.0
39	50	-1032	3411	-1417	0	918	16320	15.71	15.71	9.42	9.42	3	0.32	0.04	0.32	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 65 NI 1601 NF 164 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 4A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-3131	2618	266	0	-45	11550	15.71	15.71	9.42	9.42	3	0.22	0.03	0.24	0.00	0.00	24.0
2	0	-4713	1598	352	0	-60	7025	15.71	15.71	9.42	9.42	2	0.19	0.02	0.14	0.00	0.00	24.0
3	0	-4771	1578	40	0	-4	6964	15.71	15.71	9.42	9.42	2	0.18	0.02	0.14	0.00	0.00	24.0
4	0	-46	2449	369	0	-66	10810	15.71	15.71	9.42	9.42	2	0.30	0.03	0.23	0.00	0.00	24.0
5	0	-104	2430	57	0	-10	10750	15.71	15.71	9.42	9.42	2	0.29	0.03	0.23	0.00	0.00	24.0
6	0	-3012	1918	722	0	-127	8422	15.71	15.71	9.42	9.42	2	0.23	0.02	0.17	0.00	0.00	24.0
7	0	-3205	1854	-318	0	59	8217	15.71	15.71	9.42	9.42	2	0.22	0.02	0.17	0.00	0.00	24.0
8	0	-1612	2174	727	0	-129	9557	15.71	15.71	9.42	9.42	2	0.26	0.03	0.20	0.00	0.00	24.0
9	0	-1805	2109	-313	0	58	9352	15.71	15.71	9.42	9.42	2	0.25	0.03	0.19	0.00	0.00	24.0
10	0	-4713	1598	352	0	-60	7025	15.71	15.71	9.42	9.42	2	0.19	0.02	0.14	0.00	0.00	24.0
11	0	-4771	1578	40	0	-4	6964	15.71	15.71	9.42	9.42	2	0.18	0.02	0.14	0.00	0.00	24.0
12	0	-46	2449	369	0	-66	10810	15.71	15.71	9.42	9.42	2	0.30	0.03	0.23	0.00	0.00	24.0
13	0	-104	2430	57	0	-10	10750	15.71	15.71	9.42	9.42	2	0.29	0.03	0.23	0.00	0.00	24.0
14	0	-3012	1918	722	0	-127	8422	15.71	15.71	9.42	9.42	2	0.23	0.02	0.17	0.00	0.00	24.0
15	0	-3205	1854	-318	0	59	8217	15.71	15.71	9.42	9.42	2	0.22	0.02	0.17	0.00	0.00	24.0
16	0	-1612	2174	727	0	-129	9557	15.71	15.71	9.42	9.42	2	0.26	0.03	0.20	0.00	0.00	24.0
17	0	-1805	2109	-313	0	58	9352	15.71	15.71	9.42	9.42	2	0.25	0.03	0.19	0.00	0.00	24.0
18	0	-5489	4708	494	0	-81	16050	15.71	15.71	9.42	9.42	3	0.30	0.06	0.41	0.00	0.00	24.0
19	0	14130	5445	536	0	-95	28410	15.71	15.71	9.42	9.42	3	0.60	0.07	0.51	0.00	0.00	24.0
20	0	3093	4660	-428	0	81	20470	15.71	15.71	9.42	9.42	3	0.40	0.06	0.44	0.00	0.00	24.0
37	0	-14480	3662	397	0	-61	8458	15.71	15.71	9.42	9.42	3	0.15	0.05	0.29	0.00	0.00	24.0
38	0	18210	4891	467	0	-86	29050	15.71	15.71	9.42	9.42	3	0.63	0.06	0.46	0.00	0.00	24.0
39	0	-180	3582	-1139	0	208	15830	15.71	15.71	9.42	9.42	3	0.31	0.05	0.33	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-3001	2618	266	0	-79	11877	15.71	15.71	9.42	9.42	3	0.23	0.03	0.24	0.00	0.00	24.0
2	12	-4613	1598	352	0	-104	7225	15.71	15.71	9.42	9.42	2	0.19	0.02	0.14	0.00	0.00	24.0
3	12	-4671	1578	40	0	-9	7161	15.71	15.71	9.42	9.42	2	0.19	0.02	0.14	0.00	0.00	24.0
4	12	54	2449	369	0	-112	11115	15.71	15.71	9.42	9.42	2	0.31	0.03	0.23	0.00	0.00	24.0
5	12	-4	2430	57	0	-17	11052	15.71	15.71	9.42	9.42	2	0.30	0.03	0.23	0.00	0.00	24.0
6	12	-2912	1918	722	0	-218	8662	15.71	15.71	9.42	9.42	2	0.24	0.02	0.17	0.00	0.00	24.0
7	12	-3105	1854	-318	0	99	8448	15.71	15.71	9.42	9.42	2	0.23	0.02	0.17	0.00	0.00	24.0
8	12	-1512	2174	727	0	-220	9828	15.71	15.71	9.42	9.42	2	0.27	0.03	0.20	0.00	0.00	24.0
9	12	-1705	2109	-313	0	97	9616	15.71	15.71	9.42	9.42	2	0.26	0.03	0.19	0.00	0.00	24.0
10	12	-4613	1598	352	0	-104	7225	15.71	15.71	9.42	9.42	2	0.19	0.02	0.14	0.00	0.00	24.0
11	12	-4671	1578	40	0	-9	7161	15.71	15.71	9.42	9.42	2	0.19	0.02	0.14	0.00	0.00	24.0
12	12	54	2449	369	0	-112	11115	15.71	15.71	9.42	9.42	2	0.31	0.03	0.23	0.00	0.00	24.0
13	12	-4	2430	57	0	-17	11052	15.71	15.71	9.42	9.42	2	0.30	0.03	0.23	0.00	0.00	24.0
14	12	-2912	1918	722	0	-218	8662	15.71	15.71	9.42	9.42	2	0.24	0.02	0.17	0.00	0.00	24.0
15	12	-3105	1854	-318	0	99	8448	15.71	15.71	9.42	9.42	2	0.23	0.02	0.17	0.00	0.00	24.0
16	12	-1512	2174	727	0	-220	9828	15.71	15.71	9.42	9.42	2	0.27	0.03	0.20	0.00	0.00	24.0
17	12	-1705	2109	-313	0	97	9616	15.71	15.71	9.42	9.42	2	0.26	0.03	0.19	0.00	0.00	24.0
18	12	-5359	4708	494	0	-142	16637	15.71	15.71	9.42	9.42	3	0.31	0.06	0.41	0.00	0.00	24.0
19	12	14260	5445	536	0	-162	29090	15.71	15.71	9.42	9.42	3	0.61	0.07	0.51	0.00	0.00	24.0
20	12	3223	4660	-428	0	135	21052	15.71	15.71	9.42	9.42	3	0.41	0.06	0.44	0.00	0.00	24.0
37	12	-14350	3662	397	0	-111	8916	15.71	15.71	9.42	9.42	3	0.16	0.05	0.29	0.00	0.00	24.0
38	12	18340	4891	467	0	-144	29662	15.71	15.71	9.42	9.42	3	0.64	0.06	0.42	0.00	0.00	24.0
39	12	-50	3582	-1139	0	351	16277	15.71	15.71	9.42	9.42	3	0.32	0.05	0.34	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-2871	2618	266	0	-112	12205	15.71	15.71	9.42	9.42	3	0.23	0.03	0.24	0.00	0.00	24.0
2	25	-4513	1598	352	0	-148	7424	15.71	15.71	9.42	9.42	2	0.20	0.02	0.14	0.00	0.00	24.0
3	25	-4571	1578	40	0	-14	7358	15.71	15.71	9.42	9.42	2	0.19	0.02	0.14	0.00	0.00	24.0
4	25	154	2449	369	0	-158	11420	15.71	15.71	9.42	9.42	2	0.32	0.03	0.23	0.00	0.00	24.0
5	25	96	2430	57	0	-24	11355	15.71	15.71	9.42	9.42	2	0.31	0.03	0.23	0.00	0.00	24.0
6	25	-2812	1918	722	0	-308	8901	15.71	15.71	9.42	9.42	2	0.25	0.02	0.17	0.00	0.00	24.0
7	25	-3005	1854	-318	0	139	8680	15.71	15.71	9.42	9.42	2	0.24	0.02	0.17	0.00	0.00	24.0
8	25	-1412	2174	727	0	-311	10098	15.71	15.71	9.42	9.42	2	0.28	0.03	0.20	0.00	0.00	24.0
9	25	-1605	2109	-313	0	136	9881	15.71	15.71	9.42	9.42	2	0.27	0.03	0.19	0.00	0.00	24.0
10	25	-4513	1598	352	0	-148	7424	15.71	15.71	9.42	9.42	2	0.20	0.02	0.14	0.00	0.00	24.0
11	25	-4571	1578	40	0	-14	7358	15.71	15.71	9.42	9.42	2	0.19	0.02	0.14	0.00	0.00	24.0
12	25	154	2449	369	0	-158	11420	15.71	15.71	9.42	9.42	2	0.32	0.03	0.23	0.00	0.00	24.0
13	25	96	2430	57	0	-24	11355	15.71	15.71	9.42	9.42	2	0.31	0.03	0.23	0.00	0.00	24.0
14	25	-2812	1918	722	0	-308	8901	15.71	15.71	9.42	9.42	2	0.25	0.02	0.17	0.00	0.00	24.0
15	25	-3005	1854	-318	0	139	8680	15.71	15.71	9.42	9.42	2	0.24	0.02	0.17	0.00	0.00	24.0
16	25	-1412	2174	727	0	-311	10098	15.71	15.71	9.42	9.42	2	0.28	0.03	0.20	0.00	0.00	24.0
17	25	-1605	2109	-313	0	136	9881	15.71	15.71	9.42	9.42	2	0.27	0.03	0.19	0.00	0.00	24.0
18	25	-5229	4708	494	0	-204	17225	15.71	15.71	9.42	9.42	3	0.32	0.06	0.41	0.00	0.00	24.0
19	25	14390	5445	536	0	-229	29770	15.71	15.71	9.42	9.42	3	0.63	0.07	0.51	0.00	0.00	24.0
20	25	3353	4660	-428	0	188	21635	15.71	15.71	9.42	9.42	3	0.42	0.06	0.44	0.00	0.00	24.0
37	25	-14220	3662	397	0	-161	9374	15.71	15.71	9.42	9.42	3	0.17	0.05	0.29	0.00	0.00	24.0
38	25	18470	4891	467	0	-203	30275	15.71	15.71	9.42	9.42	3	0.65	0.06	0.42	0.00	0.00	24.0

39	25	80	3582	-1139	0	493	16725	15.71	15.71	9.42	9.42	3	0.33	0.05	0.34	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-2741	2618	266	0	-145	12532	15.71	15.71	9.42	9.42	3	0.24	0.03	0.24	0.00	0.00	24.0
2	38	-4413	1598	352	0	-192	7624	15.71	15.71	9.42	9.42	2	0.21	0.02	0.14	0.00	0.00	24.0
3	38	-4471	1578	40	0	-19	7556	15.71	15.71	9.42	9.42	2	0.20	0.02	0.14	0.00	0.00	24.0
4	38	254	2449	369	0	-204	11725	15.71	15.71	9.42	9.42	2	0.33	0.03	0.23	0.00	0.00	24.0
5	38	196	2430	57	0	-31	11658	15.71	15.71	9.42	9.42	2	0.32	0.03	0.23	0.00	0.00	24.0
6	38	-2712	1918	722	0	-398	9141	15.71	15.71	9.42	9.42	2	0.25	0.02	0.17	0.00	0.00	24.0
7	38	-2905	1854	-318	0	179	8912	15.71	15.71	9.42	9.42	2	0.24	0.02	0.17	0.00	0.00	24.0
8	38	-1312	2174	727	0	-402	10369	15.71	15.71	9.42	9.42	2	0.29	0.03	0.20	0.00	0.00	24.0
9	38	-1505	2109	-313	0	175	10146	15.71	15.71	9.42	9.42	2	0.28	0.03	0.19	0.00	0.00	24.0
10	38	-4413	1598	352	0	-192	7624	15.71	15.71	9.42	9.42	2	0.21	0.02	0.14	0.00	0.00	24.0
11	38	-4471	1578	40	0	-19	7556	15.71	15.71	9.42	9.42	2	0.20	0.02	0.14	0.00	0.00	24.0
12	38	254	2449	369	0	-204	11725	15.71	15.71	9.42	9.42	2	0.33	0.03	0.23	0.00	0.00	24.0
13	38	196	2430	57	0	-31	11658	15.71	15.71	9.42	9.42	2	0.32	0.03	0.23	0.00	0.00	24.0
14	38	-2712	1918	722	0	-398	9141	15.71	15.71	9.42	9.42	2	0.25	0.02	0.17	0.00	0.00	24.0
15	38	-2905	1854	-318	0	179	8912	15.71	15.71	9.42	9.42	2	0.24	0.02	0.17	0.00	0.00	24.0
16	38	-1312	2174	727	0	-402	10369	15.71	15.71	9.42	9.42	2	0.29	0.03	0.20	0.00	0.00	24.0
17	38	-1505	2109	-313	0	175	10146	15.71	15.71	9.42	9.42	2	0.28	0.03	0.19	0.00	0.00	24.0
18	38	-5099	4708	494	0	-266	17812	15.71	15.71	9.42	9.42	3	0.34	0.06	0.41	0.00	0.00	24.0
19	38	14520	5445	536	0	-296	30450	15.71	15.71	9.42	9.42	3	0.64	0.07	0.51	0.00	0.00	24.0
20	38	3483	4660	-428	0	242	22217	15.71	15.71	9.42	9.42	3	0.44	0.06	0.44	0.00	0.00	24.0
37	38	-14090	3662	397	0	-210	9832	15.71	15.71	9.42	9.42	3	0.18	0.05	0.29	0.00	0.00	24.0
38	38	18600	4891	467	0	-261	30887	15.71	15.71	9.42	9.42	3	0.67	0.06	0.42	0.00	0.00	24.0
39	38	210	3582	-1139	0	636	17173	15.71	15.71	9.42	9.42	3	0.34	0.05	0.34	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-2611	2618	266	0	-178	12860	15.71	15.71	9.42	9.42	3	0.25	0.03	0.24	0.00	0.00	24.0
2	50	-4313	1598	352	0	-236	7824	15.71	15.71	9.42	9.42	2	0.21	0.02	0.14	0.00	0.00	24.0
3	50	-4371	1578	40	0	-24	7753	15.71	15.71	9.42	9.42	2	0.21	0.02	0.14	0.00	0.00	24.0
4	50	354	2449	369	0	-250	12030	15.71	15.71	9.42	9.42	2	0.34	0.03	0.23	0.00	0.00	24.0
5	50	296	2430	57	0	-38	11960	15.71	15.71	9.42	9.42	2	0.33	0.03	0.23	0.00	0.00	24.0
6	50	-2612	1918	722	0	-488	9381	15.71	15.71	9.42	9.42	2	0.26	0.02	0.17	0.00	0.00	24.0
7	50	-2805	1854	-318	0	218	9143	15.71	15.71	9.42	9.42	2	0.25	0.02	0.17	0.00	0.00	24.0
8	50	-1212	2174	727	0	-493	10640	15.71	15.71	9.42	9.42	2	0.30	0.03	0.20	0.00	0.00	24.0
9	50	-1405	2109	-313	0	214	10410	15.71	15.71	9.42	9.42	2	0.29	0.03	0.19	0.00	0.00	24.0
10	50	-4313	1598	352	0	-236	7824	15.71	15.71	9.42	9.42	2	0.21	0.02	0.14	0.00	0.00	24.0
11	50	-4371	1578	40	0	-24	7753	15.71	15.71	9.42	9.42	2	0.21	0.02	0.14	0.00	0.00	24.0
12	50	354	2449	369	0	-250	12030	15.71	15.71	9.42	9.42	2	0.34	0.03	0.23	0.00	0.00	24.0
13	50	296	2430	57	0	-38	11960	15.71	15.71	9.42	9.42	2	0.33	0.03	0.23	0.00	0.00	24.0
14	50	-2612	1918	722	0	-488	9381	15.71	15.71	9.42	9.42	2	0.26	0.02	0.17	0.00	0.00	24.0
15	50	-2805	1854	-318	0	218	9143	15.71	15.71	9.42	9.42	2	0.25	0.02	0.17	0.00	0.00	24.0
16	50	-1212	2174	727	0	-493	10640	15.71	15.71	9.42	9.42	2	0.30	0.03	0.20	0.00	0.00	24.0
17	50	-1405	2109	-313	0	214	10410	15.71	15.71	9.42	9.42	2	0.29	0.03	0.19	0.00	0.00	24.0
18	50	-4969	4708	494	0	-327	18400	15.71	15.71	9.42	9.42	3	0.35	0.06	0.41	0.00	0.00	24.0
19	50	14650	5445	536	0	-363	31130	15.71	15.71	9.42	9.42	3	0.66	0.07	0.47	0.00	0.00	24.0
20	50	3613	4660	-428	0	295	22800	15.71	15.71	9.42	9.42	3	0.45	0.06	0.44	0.00	0.00	24.0
37	50	-13960	3662	397	0	-260	10290	15.71	15.71	9.42	9.42	3	0.19	0.05	0.29	0.00	0.00	24.0
38	50	18730	4891	467	0	-319	31500	15.71	15.71	9.42	9.42	3	0.68	0.06	0.42	0.00	0.00	24.0
39	50	340	3582	-1139	0	778	17620	15.71	15.71	9.42	9.42	3	0.35	0.05	0.34	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 66 NI 1621 NF 207 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 3A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-4262	2383	344	0	-28	10430	15.71	15.71	9.42	9.42	3	0.20	0.03	0.21	0.00	0.00	24.0
2	0	-5537	1406	411	0	-51	6175	15.71	15.71	9.42	9.42	2	0.16	0.02	0.12	0.00	0.00	24.0
3	0	-5531	1408	101	0	3	6183	15.71	15.71	9.42	9.42	2	0.16	0.02	0.12	0.00	0.00	24.0
4	0	-1026	2259	428	0	-46	9859	15.71	15.71	9.42	9.42	2	0.27	0.03	0.21	0.00	0.00	24.0
5	0	-1020	2261	118	0	8	9867	15.71	15.71	9.42	9.42	2	0.27	0.03	0.21	0.00	0.00	24.0
6	0	-3966	1702	778	0	-111	7454	15.71	15.71	9.42	9.42	2	0.20	0.02	0.15	0.00	0.00	24.0
7	0	-3945	1709	-254	0	67	7483	15.71	15.71	9.42	9.42	2	0.20	0.02	0.15	0.00	0.00	24.0
8	0	-2612	1958	783	0	-110	8559	15.71	15.71	9.42	9.42	2	0.23	0.03	0.18	0.00	0.00	24.0
9	0	-2592	1965	-249	0	68	8588	15.71	15.71	9.42	9.42	2	0.23	0.03	0.18	0.00	0.00	24.0
10	0	-5537	1406	411	0	-51	6175	15.71	15.71	9.42	9.42	2	0.16	0.02	0.12	0.00	0.00	24.0
11	0	-5531	1408	101	0	3	6183	15.71	15.71	9.42	9.42	2	0.16	0.02	0.12	0.00	0.00	24.0
12	0	-1026	2259	428	0	-46	9859	15.71	15.71	9.42	9.42	2	0.27	0.03	0.21	0.00	0.00	24.0
13	0	-1020	2261	118	0	8	9867	15.71	15.71	9.42	9.42	2	0.27	0.03	0.21	0.00	0.00	24.0
14	0	-3966	1702	778	0	-111	7454	15.71	15.71	9.42	9.42	2	0.20	0.02	0.15	0.00	0.00	24.0
15	0	-3945	1709	-254	0	67	7483	15.71	15.71	9.42	9.42	2	0.20	0.02	0.15	0.00	0.00	24.0
16	0	-2612	1958	783	0	-110	8559	15.71	15.71	9.42	9.42	2	0.23	0.03	0.18	0.00	0.00	24.0
17	0	-2592	1965	-249	0	68	8588	15.71	15.71	9.42	9.42	2	0.23	0.03	0.18	0.00	0.00	24.0
18	0	-7458	4259	621	0	-59	14040	15.71	15.71	9.42	9.42	3	0.26	0.05	0.36	0.00	0.00	24.0
19	0	11770	5049	641	0	-41	26190	15.71	15.71	9.42	9.42	3	0.54	0.07	0.47	0.00	0.00	24.0
20	0	1233	4316	-265	0	101	18680	15.71	15.71	9.42	9.42	3	0.36	0.06	0.40	0.00	0.00	24.0
37	0	-15990	3257	520	0	-57	6834	15.71	15.71	9.42	9.42	3	0.12	0.04	0.25	0.00	0.00	24.0
38	0	16060	4573	552	0	-28	27090	15.71	15.71	9.42	9.42	3	0.57	0.06	0.43	0.00	0.00	24.0
39	0	-1506	3351	-957	0	210	14560	15.71	15.71	9.42	9.42	3	0.28	0.04	0.31	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-4132	2383	344	0	-71	10728	15.71	15.71	9.42	9.42	3	0.20	0.03	0.21	0.00	0.00	24.0
2	12	-5437	1406	411	0	-102	6351	15.71	15.71	9.42	9.42	2	0.17	0.02	0.12	0.00	0.00	24.0
3	12	-5431	1408	101	0	-10	6359	15.71	15.71	9.42	9.42	2	0.17	0.02	0.12	0.00	0.00	24.0
4	12	-926	2259	428	0	-99	10142	15.71	15.71	9.42	9.42	2	0.28	0.03	0.21	0.00	0.00	24.0
5	12	-920	2261	118	0	-7	10150	15.71	15.71	9.42	9.42	2	0.28	0.03	0.21	0.00	0.00	24.0
6	12	-3866	1702	778	0	-209	7667	15.71	15.71	9.42	9.42	2	0.21	0.02	0.15	0.00	0.00	24.0
7	12	-3845	1709	-254	0	98	7696	15.71	15.71	9.42	9.42	2	0.21	0.02	0.15	0.00	0.00	24.0
8	12	-2512	1958	783	0	-208	8804	15.71	15.71	9.42	9.42	2	0.24	0.03	0.18	0.00	0.00	24.0
9	12	-2492	1965	-249	0	99	8834	15.71	15.71	9.42	9.42	2	0.24	0.03	0.18	0.00	0.00	24.0
10	12	-5437	1406	411	0	-102	6351	15.71	15.71	9.42	9.42	2	0.17	0.02	0.12	0.00	0.00	24.0
11	12	-5431	1408	101	0	-10	6359	15.71	15.71	9.42	9.42	2	0.17	0.02	0.12	0.00	0.00	24.0
12	12	-926	2259	428	0	-99	10142	15.71	15.71	9.42	9.42	2	0.28	0.03	0.21	0.00	0.00	24.0
13	12	-920	2261	118	0	-7	10150	15.71	15.71	9.42	9.42	2	0.28	0.03	0.21	0.00	0.00	24.0
14	12	-3866	1702	778	0	-209	7667	15.71	15.71	9.42	9.42	2	0.21	0.02	0.15	0.00	0.00	24.0
15	12	-3845	1709	-254	0	98	7696	15.71	15.71	9.42	9.42	2	0.21	0.02	0.15	0.00	0.00	24.0
16	12	-2512	1958	783	0	-208	8804	15.71	15.71	9.42	9.42	2	0.24	0.03	0.18	0.00	0.00	24.0
17	12	-2492	1965	-249	0	99	8834	15.71	15.71	9.42	9.42	2	0.24	0.03	0.18	0.00	0.00	24.0
18	12	-7328	4259	621	0	-136	14572	15.71	15.71	9.42	9.42	3	0.27	0.05	0.36	0.00	0.00	24.0

19	12	11900	5049	641	0	-121	26822	15.71	15.71	9.42	9.42	3	0.55	0.07	0.47	0.00	0.00	24.0
20	12	1363	4316	-265	0	134	19217	15.71	15.71	9.42	9.42	3	0.37	0.06	0.40	0.00	0.00	24.0
37	12	-15860	3257	520	0	-122	7241	15.71	15.71	9.42	9.42	3	0.13	0.04	0.25	0.00	0.00	24.0
38	12	16190	4573	552	0	-97	27662	15.71	15.71	9.42	9.42	3	0.59	0.06	0.43	0.00	0.00	24.0
39	12	-1376	3351	-957	0	329	14980	15.71	15.71	9.42	9.42	3	0.29	0.04	0.31	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-4002	2383	344	0	-114	11025	15.71	15.71	9.42	9.42	3	0.21	0.03	0.21	0.00	0.00	24.0
2	25	-5337	1406	411	0	-153	6526	15.71	15.71	9.42	9.42	2	0.18	0.02	0.12	0.00	0.00	24.0
3	25	-5331	1408	101	0	-23	6536	15.71	15.71	9.42	9.42	2	0.17	0.02	0.12	0.00	0.00	24.0
4	25	-826	2259	428	0	-153	10425	15.71	15.71	9.42	9.42	2	0.29	0.03	0.21	0.00	0.00	24.0
5	25	-820	2261	118	0	-22	10434	15.71	15.71	9.42	9.42	2	0.28	0.03	0.21	0.00	0.00	24.0
6	25	-3766	1702	778	0	-306	7880	15.71	15.71	9.42	9.42	2	0.22	0.02	0.15	0.00	0.00	24.0
7	25	-3745	1709	-254	0	130	7910	15.71	15.71	9.42	9.42	2	0.21	0.02	0.15	0.00	0.00	24.0
8	25	-2412	1958	783	0	-306	9048	15.71	15.71	9.42	9.42	2	0.25	0.03	0.18	0.00	0.00	24.0
9	25	-2392	1965	-249	0	130	9079	15.71	15.71	9.42	9.42	2	0.25	0.03	0.18	0.00	0.00	24.0
10	25	-5337	1406	411	0	-153	6526	15.71	15.71	9.42	9.42	2	0.18	0.02	0.12	0.00	0.00	24.0
11	25	-5331	1408	101	0	-23	6536	15.71	15.71	9.42	9.42	2	0.17	0.02	0.12	0.00	0.00	24.0
12	25	-826	2259	428	0	-153	10425	15.71	15.71	9.42	9.42	2	0.29	0.03	0.21	0.00	0.00	24.0
13	25	-820	2261	118	0	-22	10434	15.71	15.71	9.42	9.42	2	0.28	0.03	0.21	0.00	0.00	24.0
14	25	-3766	1702	778	0	-306	7880	15.71	15.71	9.42	9.42	2	0.22	0.02	0.15	0.00	0.00	24.0
15	25	-3745	1709	-254	0	130	7910	15.71	15.71	9.42	9.42	2	0.21	0.02	0.15	0.00	0.00	24.0
16	25	-2412	1958	783	0	-306	9048	15.71	15.71	9.42	9.42	2	0.25	0.03	0.18	0.00	0.00	24.0
17	25	-2392	1965	-249	0	130	9079	15.71	15.71	9.42	9.42	2	0.25	0.03	0.18	0.00	0.00	24.0
18	25	-7198	4259	621	0	-214	15105	15.71	15.71	9.42	9.42	3	0.28	0.05	0.36	0.00	0.00	24.0
19	25	12030	5049	641	0	-201	27455	15.71	15.71	9.42	9.42	3	0.57	0.07	0.47	0.00	0.00	24.0
20	25	1493	4316	-265	0	167	19755	15.71	15.71	9.42	9.42	3	0.38	0.06	0.40	0.00	0.00	24.0
37	25	-15730	3257	520	0	-187	7648	15.71	15.71	9.42	9.42	3	0.14	0.04	0.25	0.00	0.00	24.0
38	25	16320	4573	552	0	-166	28235	15.71	15.71	9.42	9.42	3	0.60	0.06	0.43	0.00	0.00	24.0
39	25	-1246	3351	-957	0	449	15400	15.71	15.71	9.42	9.42	3	0.30	0.04	0.31	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-3872	2383	344	0	-157	11322	15.71	15.71	9.42	9.42	3	0.21	0.03	0.21	0.00	0.00	24.0
2	38	-5237	1406	411	0	-205	6702	15.71	15.71	9.42	9.42	2	0.18	0.02	0.12	0.00	0.00	24.0
3	38	-5231	1408	101	0	-35	6712	15.71	15.71	9.42	9.42	2	0.18	0.02	0.12	0.00	0.00	24.0
4	38	-726	2259	428	0	-206	10707	15.71	15.71	9.42	9.42	2	0.30	0.03	0.21	0.00	0.00	24.0
5	38	-720	2261	118	0	-37	10717	15.71	15.71	9.42	9.42	2	0.29	0.03	0.21	0.00	0.00	24.0
6	38	-3666	1702	778	0	-403	8092	15.71	15.71	9.42	9.42	2	0.23	0.02	0.15	0.00	0.00	24.0
7	38	-3645	1709	-254	0	162	8124	15.71	15.71	9.42	9.42	2	0.22	0.02	0.15	0.00	0.00	24.0
8	38	-2312	1958	783	0	-404	9293	15.71	15.71	9.42	9.42	2	0.26	0.03	0.18	0.00	0.00	24.0
9	38	-2292	1965	-249	0	161	9324	15.71	15.71	9.42	9.42	2	0.25	0.03	0.18	0.00	0.00	24.0
10	38	-5237	1406	411	0	-205	6702	15.71	15.71	9.42	9.42	2	0.18	0.02	0.12	0.00	0.00	24.0
11	38	-5231	1408	101	0	-35	6712	15.71	15.71	9.42	9.42	2	0.18	0.02	0.12	0.00	0.00	24.0
12	38	-726	2259	428	0	-206	10707	15.71	15.71	9.42	9.42	2	0.30	0.03	0.21	0.00	0.00	24.0
13	38	-720	2261	118	0	-37	10717	15.71	15.71	9.42	9.42	2	0.29	0.03	0.21	0.00	0.00	24.0
14	38	-3666	1702	778	0	-403	8092	15.71	15.71	9.42	9.42	2	0.23	0.02	0.15	0.00	0.00	24.0
15	38	-3645	1709	-254	0	162	8124	15.71	15.71	9.42	9.42	2	0.22	0.02	0.15	0.00	0.00	24.0
16	38	-2312	1958	783	0	-404	9293	15.71	15.71	9.42	9.42	2	0.26	0.03	0.18	0.00	0.00	24.0
17	38	-2292	1965	-249	0	161	9324	15.71	15.71	9.42	9.42	2	0.25	0.03	0.18	0.00	0.00	24.0
18	38	-7068	4259	621	0	-292	15638	15.71	15.71	9.42	9.42	3	0.29	0.05	0.37	0.00	0.00	24.0
19	38	12160	5049	641	0	-282	28088	15.71	15.71	9.42	9.42	3	0.58	0.07	0.47	0.00	0.00	24.0
20	38	1623	4316	-265	0	201	20293	15.71	15.71	9.42	9.42	3	0.40	0.06	0.40	0.00	0.00	24.0
37	38	-15600	3257	520	0	-252	8056	15.71	15.71	9.42	9.42	3	0.15	0.04	0.25	0.00	0.00	24.0
38	38	16450	4573	552	0	-235	28808	15.71	15.71	9.42	9.42	3	0.61	0.06	0.43	0.00	0.00	24.0
39	38	-1116	3351	-957	0	569	15820	15.71	15.71	9.42	9.42	3	0.31	0.04	0.31	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-3742	2383	344	0	-200	11620	15.71	15.71	9.42	9.42	3	0.22	0.03	0.21	0.00	0.00	24.0
2	50	-5137	1406	411	0	-256	6878	15.71	15.71	9.42	9.42	2	0.19	0.02	0.12	0.00	0.00	24.0
3	50	-5131	1408	101	0	-48	6888	15.71	15.71	9.42	9.42	2	0.18	0.02	0.12	0.00	0.00	24.0
4	50	-626	2259	428	0	-260	10990	15.71	15.71	9.42	9.42	2	0.30	0.03	0.21	0.00	0.00	24.0
5	50	-620	2261	118	0	-52	11000	15.71	15.71	9.42	9.42	2	0.30	0.03	0.21	0.00	0.00	24.0
6	50	-3566	1702	778	0	-500	8305	15.71	15.71	9.42	9.42	2	0.23	0.02	0.15	0.00	0.00	24.0
7	50	-3545	1709	-254	0	194	8337	15.71	15.71	9.42	9.42	2	0.23	0.02	0.15	0.00	0.00	24.0
8	50	-2212	1958	783	0	-501	9538	15.71	15.71	9.42	9.42	2	0.27	0.03	0.18	0.00	0.00	24.0
9	50	-2192	1965	-249	0	193	9570	15.71	15.71	9.42	9.42	2	0.26	0.03	0.18	0.00	0.00	24.0
10	50	-5137	1406	411	0	-256	6878	15.71	15.71	9.42	9.42	2	0.19	0.02	0.12	0.00	0.00	24.0
11	50	-5131	1408	101	0	-48	6888	15.71	15.71	9.42	9.42	2	0.18	0.02	0.12	0.00	0.00	24.0
12	50	-626	2259	428	0	-260	10990	15.71	15.71	9.42	9.42	2	0.30	0.03	0.21	0.00	0.00	24.0
13	50	-620	2261	118	0	-52	11000	15.71	15.71	9.42	9.42	2	0.30	0.03	0.21	0.00	0.00	24.0
14	50	-3566	1702	778	0	-500	8305	15.71	15.71	9.42	9.42	2	0.23	0.02	0.15	0.00	0.00	24.0
15	50	-3545	1709	-254	0	194	8337	15.71	15.71	9.42	9.42	2	0.23	0.02	0.15	0.00	0.00	24.0
16	50	-2212	1958	783	0	-501	9538	15.71	15.71	9.42	9.42	2	0.27	0.03	0.18	0.00	0.00	24.0
17	50	-2192	1965	-249	0	193	9570	15.71	15.71	9.42	9.42	2	0.26	0.03	0.18	0.00	0.00	24.0
18	50	-6938	4259	621	0	-369	16170	15.71	15.71	9.42	9.42	3	0.30	0.05	0.37	0.00	0.00	24.0
19	50	12290	5049	641	0	-362	28720	15.71	15.71	9.42	9.42	3	0.60	0.07	0.47	0.00	0.00	24.0
20	50	1753	4316	-265	0	234	20830	15.71	15.71	9.42	9.42	3	0.41	0.06	0.40	0.00	0.00	24.0
37	50	-15470	3257	520	0	-317	8463	15.71	15.71	9.42	9.42	3	0.15	0.04	0.25	0.00	0.00	24.0
38	50	16580	4573	552	0	-304	29380	15.71	15.71	9.42	9.42	3	0.63	0.06	0.43	0.00	0.00	24.0
39	50	-986	3351	-957	0	688	16240	15.71	15.71	9.42	9.42	3	0.32	0.04	0.31	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 67 NI 1641 NF 250 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 2A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-8739	1306	366	0	34	6251	15.71	15.71	9.42	9.42	3	0.12	0.02	0.11	0.00	0.00	24.0
2	0	-8538	641	462	0	-10	3324	15.71	15.71	9.42	9.42	2	0.09	0.01	0.05	0.00	0.00	24.0
3	0	-8466	669	161	0	44	3409	15.71	15.71	9.42	9.42	2	0.09	0.01	0.06	0.00	0.00	24.0
4	0	-4979	1341	403	0	9	6209	15.71	15.71	9.42	9.42	2	0.16	0.02	0.12	0.00	0.00	24.0
5	0	-4907	1368	102	0	62	6294	15.71	15.71	9.42	9.42	2	0.17	0.02	0.12	0.00	0.00	24.0
6	0	-7376	854	793	0	-66	4234	15.71	15.71	9.42	9.42	2	0.11	0.01	0.07	0.00	0.00	24.0
7	0	-7136	946	-212	0	112	4518	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
8	0	-6309	1064	776	0	-60	5100	15.71	15.71	9.42	9.42	2	0.13	0.01	0.09	0.00	0.00	24.0
9	0	-6068	1156	-230	0	118	5383	15.71	15.71	9.42	9.42	2	0.14	0.01	0.10	0.00	0.00	24.0
10	0	-8538	641	462	0	-10	3324	15.71	15.71	9.42	9.42	2	0.09	0.01	0.05	0.00	0.00	24.0
11	0	-8466	669	161	0	44	3409	15.71	15.71	9.42	9.42	2	0.09	0.01	0.06	0.00	0.00	24.0
12	0	-4979	1341	403	0	9	6209	15.71	15.71	9.42	9.42	2	0.16	0.02	0.12	0.00	0.00	24.0
13	0	-4907	1368	102	0	62	6294	15.71	15.71	9.42	9.42	2	0.17	0.02	0.12	0.00	0.00	24.0
14	0	-7376	854	793	0	-66	4234	15.71	15.71	9.42	9.42	2	0.11	0.01	0.07	0.00	0.00	24.0

15	0	-7136	946	-212	0	112	4518	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
16	0	-6309	1064	776	0	-60	5100	15.71	15.71	9.42	9.42	2	0.13	0.01	0.09	0.00	0.00	24.0
17	0	-6068	1156	-230	0	118	5383	15.71	15.71	9.42	9.42	2	0.14	0.01	0.10	0.00	0.00	24.0
18	0	-14860	2337	756	0	51	6833	15.71	15.71	9.42	9.42	3	0.12	0.03	0.18	0.00	0.00	24.0
19	0	2099	3025	506	0	95	17210	15.71	15.71	9.42	9.42	3	0.34	0.04	0.28	0.00	0.00	24.0
20	0	-6570	2542	-223	0	214	11350	15.71	15.71	9.42	9.42	3	0.21	0.03	0.22	0.00	0.00	24.0
37	0	-21320	1658	754	0	23	1492	15.71	15.71	9.42	9.42	3	0.03	0.02	0.12	0.00	0.00	24.0
38	0	6950	2805	336	0	97	18790	15.71	15.71	9.42	9.42	3	0.38	0.04	0.26	0.00	0.00	24.0
39	0	-7499	2000	-878	0	296	9016	15.71	15.71	9.42	9.42	3	0.17	0.03	0.17	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-8609	1306	366	0	-12	6415	15.71	15.71	9.42	9.42	3	0.12	0.02	0.11	0.00	0.00	24.0
2	12	-8438	641	462	0	-68	3404	15.71	15.71	9.42	9.42	2	0.09	0.01	0.05	0.00	0.00	24.0
3	12	-8366	669	161	0	24	3492	15.71	15.71	9.42	9.42	2	0.09	0.01	0.06	0.00	0.00	24.0
4	12	-4879	1341	403	0	-42	6376	15.71	15.71	9.42	9.42	2	0.17	0.02	0.12	0.00	0.00	24.0
5	12	-4807	1368	102	0	49	6465	15.71	15.71	9.42	9.42	2	0.17	0.02	0.12	0.00	0.00	24.0
6	12	-7276	854	793	0	-165	4341	15.71	15.71	9.42	9.42	2	0.12	0.01	0.07	0.00	0.00	24.0
7	12	-7036	946	-212	0	139	4636	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
8	12	-6209	1064	776	0	-157	5233	15.71	15.71	9.42	9.42	2	0.14	0.01	0.09	0.00	0.00	24.0
9	12	-5968	1156	-230	0	147	5528	15.71	15.71	9.42	9.42	2	0.15	0.01	0.10	0.00	0.00	24.0
10	12	-8438	641	462	0	-68	3404	15.71	15.71	9.42	9.42	2	0.09	0.01	0.05	0.00	0.00	24.0
11	12	-8366	669	161	0	24	3492	15.71	15.71	9.42	9.42	2	0.09	0.01	0.06	0.00	0.00	24.0
12	12	-4879	1341	403	0	-42	6376	15.71	15.71	9.42	9.42	2	0.17	0.02	0.12	0.00	0.00	24.0
13	12	-4807	1368	102	0	49	6465	15.71	15.71	9.42	9.42	2	0.17	0.02	0.12	0.00	0.00	24.0
14	12	-7276	854	793	0	-165	4341	15.71	15.71	9.42	9.42	2	0.12	0.01	0.07	0.00	0.00	24.0
15	12	-7036	946	-212	0	139	4636	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
16	12	-6209	1064	776	0	-157	5233	15.71	15.71	9.42	9.42	2	0.14	0.01	0.09	0.00	0.00	24.0
17	12	-5968	1156	-230	0	147	5528	15.71	15.71	9.42	9.42	2	0.15	0.01	0.10	0.00	0.00	24.0
18	12	-14730	2337	756	0	-44	7125	15.71	15.71	9.42	9.42	3	0.13	0.03	0.18	0.00	0.00	24.0
19	12	2229	3025	506	0	32	17588	15.71	15.71	9.42	9.42	3	0.34	0.04	0.28	0.00	0.00	24.0
20	12	-6440	2542	-223	0	242	11667	15.71	15.71	9.42	9.42	3	0.22	0.03	0.22	0.00	0.00	24.0
37	12	-21190	1658	754	0	-71	1699	15.71	15.71	9.42	9.42	3	0.03	0.02	0.12	0.00	0.00	24.0
38	12	7080	2805	336	0	55	19140	15.71	15.71	9.42	9.42	3	0.38	0.04	0.26	0.00	0.00	24.0
39	12	-7369	2000	-878	0	406	9267	15.71	15.71	9.42	9.42	3	0.17	0.03	0.17	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-8479	1306	366	0	-58	6578	15.71	15.71	9.42	9.42	3	0.12	0.02	0.11	0.00	0.00	24.0
2	25	-8338	641	462	0	-125	3484	15.71	15.71	9.42	9.42	2	0.09	0.01	0.05	0.00	0.00	24.0
3	25	-8266	669	161	0	4	3576	15.71	15.71	9.42	9.42	2	0.09	0.01	0.06	0.00	0.00	24.0
4	25	-4779	1341	403	0	-92	6544	15.71	15.71	9.42	9.42	2	0.17	0.02	0.12	0.00	0.00	24.0
5	25	-4707	1368	102	0	37	6636	15.71	15.71	9.42	9.42	2	0.18	0.02	0.12	0.00	0.00	24.0
6	25	-7176	854	793	0	-264	4448	15.71	15.71	9.42	9.42	2	0.12	0.01	0.07	0.00	0.00	24.0
7	25	-6936	946	-212	0	165	4754	15.71	15.71	9.42	9.42	2	0.13	0.01	0.08	0.00	0.00	24.0
8	25	-6109	1064	776	0	-254	5366	15.71	15.71	9.42	9.42	2	0.15	0.01	0.09	0.00	0.00	24.0
9	25	-5868	1156	-230	0	175	5672	15.71	15.71	9.42	9.42	2	0.15	0.01	0.10	0.00	0.00	24.0
10	25	-8338	641	462	0	-125	3484	15.71	15.71	9.42	9.42	2	0.09	0.01	0.05	0.00	0.00	24.0
11	25	-8266	669	161	0	4	3576	15.71	15.71	9.42	9.42	2	0.09	0.01	0.06	0.00	0.00	24.0
12	25	-4779	1341	403	0	-92	6544	15.71	15.71	9.42	9.42	2	0.17	0.02	0.12	0.00	0.00	24.0
13	25	-4707	1368	102	0	37	6636	15.71	15.71	9.42	9.42	2	0.18	0.02	0.12	0.00	0.00	24.0
14	25	-7176	854	793	0	-264	4448	15.71	15.71	9.42	9.42	2	0.12	0.01	0.07	0.00	0.00	24.0
15	25	-6936	946	-212	0	165	4754	15.71	15.71	9.42	9.42	2	0.13	0.01	0.08	0.00	0.00	24.0
16	25	-6109	1064	776	0	-254	5366	15.71	15.71	9.42	9.42	2	0.15	0.01	0.09	0.00	0.00	24.0
17	25	-5868	1156	-230	0	175	5672	15.71	15.71	9.42	9.42	2	0.15	0.01	0.10	0.00	0.00	24.0
18	25	-14600	2337	756	0	-138	7418	15.71	15.71	9.42	9.42	3	0.13	0.03	0.18	0.00	0.00	24.0
19	25	2359	3025	506	0	-32	17965	15.71	15.71	9.42	9.42	3	0.35	0.04	0.28	0.00	0.00	24.0
20	25	-6310	2542	-223	0	270	11985	15.71	15.71	9.42	9.42	3	0.23	0.03	0.22	0.00	0.00	24.0
37	25	-21060	1658	754	0	-165	1906	15.71	15.71	9.42	9.42	3	0.03	0.02	0.12	0.00	0.00	24.0
38	25	7210	2805	336	0	13	19490	15.71	15.71	9.42	9.42	3	0.39	0.04	0.26	0.00	0.00	24.0
39	25	-7239	2000	-878	0	515	9518	15.71	15.71	9.42	9.42	3	0.18	0.03	0.17	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-8349	1306	366	0	-103	6742	15.71	15.71	9.42	9.42	3	0.13	0.02	0.11	0.00	0.00	24.0
2	38	-8238	641	462	0	-183	3565	15.71	15.71	9.42	9.42	2	0.10	0.01	0.05	0.00	0.00	24.0
3	38	-8166	669	161	0	-17	3660	15.71	15.71	9.42	9.42	2	0.09	0.01	0.06	0.00	0.00	24.0
4	38	-4679	1341	403	0	-142	6712	15.71	15.71	9.42	9.42	2	0.18	0.02	0.12	0.00	0.00	24.0
5	38	-4607	1368	102	0	24	6807	15.71	15.71	9.42	9.42	2	0.18	0.02	0.12	0.00	0.00	24.0
6	38	-7076	854	793	0	-363	4554	15.71	15.71	9.42	9.42	2	0.13	0.01	0.07	0.00	0.00	24.0
7	38	-6836	946	-212	0	192	4873	15.71	15.71	9.42	9.42	2	0.13	0.01	0.08	0.00	0.00	24.0
8	38	-6009	1064	776	0	-351	5499	15.71	15.71	9.42	9.42	2	0.15	0.01	0.09	0.00	0.00	24.0
9	38	-5768	1156	-230	0	204	5816	15.71	15.71	9.42	9.42	2	0.16	0.01	0.10	0.00	0.00	24.0
10	38	-8238	641	462	0	-183	3565	15.71	15.71	9.42	9.42	2	0.10	0.01	0.05	0.00	0.00	24.0
11	38	-8166	669	161	0	-17	3660	15.71	15.71	9.42	9.42	2	0.09	0.01	0.06	0.00	0.00	24.0
12	38	-4679	1341	403	0	-142	6712	15.71	15.71	9.42	9.42	2	0.18	0.02	0.12	0.00	0.00	24.0
13	38	-4607	1368	102	0	24	6807	15.71	15.71	9.42	9.42	2	0.18	0.02	0.12	0.00	0.00	24.0
14	38	-7076	854	793	0	-363	4554	15.71	15.71	9.42	9.42	2	0.13	0.01	0.07	0.00	0.00	24.0
15	38	-6836	946	-212	0	192	4873	15.71	15.71	9.42	9.42	2	0.13	0.01	0.08	0.00	0.00	24.0
16	38	-6009	1064	776	0	-351	5499	15.71	15.71	9.42	9.42	2	0.15	0.01	0.09	0.00	0.00	24.0
17	38	-5768	1156	-230	0	204	5816	15.71	15.71	9.42	9.42	2	0.16	0.01	0.10	0.00	0.00	24.0
18	38	-14470	2337	756	0	-233	7710	15.71	15.71	9.42	9.42	3	0.14	0.03	0.18	0.00	0.00	24.0
19	38	2489	3025	506	0	-95	18343	15.71	15.71	9.42	9.42	3	0.36	0.04	0.28	0.00	0.00	24.0
20	38	-6180	2542	-223	0	298	12303	15.71	15.71	9.42	9.42	3	0.23	0.03	0.22	0.00	0.00	24.0
37	38	-20930	1658	754	0	-259	2114	15.71	15.71	9.42	9.42	3	0.04	0.02	0.12	0.00	0.00	24.0
38	38	7340	2805	336	0	-29	19840	15.71	15.71	9.42	9.42	3	0.40	0.04	0.26	0.00	0.00	24.0
39	38	-7109	2000	-878	0	625	9769	15.71	15.71	9.42	9.42	3	0.19	0.03	0.17	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-8219	1306	366	0	-149	6905	15.71	15.71	9.42	9.42	3	0.13	0.02	0.11	0.00	0.00	24.0
2	50	-8138	641	462	0	-241	3645	15.71	15.71	9.42	9.42	2	0.10	0.01	0.05	0.00	0.00	24.0
3	50	-8066	669	161	0	-37	3743	15.71	15.71	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
4	50	-4579	1341	403	0	-193	6879	15.71	15.71	9.42	9.42	2	0.19	0.02	0.12	0.00	0.00	24.0
5	50	-4507	1368	102	0	11	6978	15.71	15.71	9.42	9.42	2	0.18	0.02	0.12	0.00	0.00	24.0
6	50	-6976	854	793	0	-462	4661	15.71	15.71	9.42	9.42	2	0.13	0.01	0.07	0.00	0.00	24.0
7	50	-6736	946	-212	0	218	4991	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
8	50	-5909	1064	776	0	-448	5632	15.71	15.71	9.42	9.42	2	0.16	0.01	0.09	0.00	0.00	24.0
9	50	-5668	1156	-230	0	233	5961	15.71	15.71	9.42	9.42	2	0.16	0.01	0.10	0.00	0.00	24.0
10	50	-8138	641	462	0	-241	3645	15.71	15.71	9.42	9.42	2	0.10	0.01	0.05	0.00	0.00	24.0
11	50	-8066	669	161	0	-37	3743	15.71	15.71	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
12	50	-4579	1341	403	0	-193	6879	15.71	15.71	9.42	9.42	2	0.19	0.02	0.12	0.00	0.00	24.0
13	50	-4507	1368	102	0	11	6978	15.71	15.71	9.42	9.42	2	0.18	0.02	0.12	0.00	0.00	24.0
14	50	-6976	854	793	0	-462	4661	15.71	15.71	9.42	9.42	2	0.13	0.01	0.07	0.00	0.00	24.0
15	50	-6736	946	-212	0	218	4991	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
16	50	-5909	1064	776	0	-448	5632	15.71	15.71	9.42	9.42	2	0.16	0.01	0.09	0.00	0.00	24.0
17	50	-5668	1156	-230	0	233	5961	15.71	15.71	9.42	9.42	2	0.16	0.01	0.10	0.00	0.00	24.0
18	50	-14340	2337	756	0	-328	8002	15.71	15.71	9.42	9.42	3	0.15	0.03	0.18	0.00	0.00	24.0
19	50	2619	3025	506	0	-158	18720	15.71	15.71	9.42	9.42	3	0.37	0.04	0.28	0.00	0.00	24.0
20	50	-6050	2542	-223	0	326	12620	15.71	15.71	9.42	9.42	3	0.24	0.03	0.22	0.00	0.00	24.0

37	50	-20800	1658	754	0	-354	2321	15.71	15.71	9.42	9.42	3	0.04	0.02	0.12	0.00	0.00	24.0
38	50	7470	2805	336	0	-71	20190	15.71	15.71	9.42	9.42	3	0.41	0.04	0.26	0.00	0.00	24.0
39	50	-6979	2000	-878	0	735	10020	15.71	15.71	9.42	9.42	3	0.19	0.03	0.17	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 68 NI 1580 NF 1581 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 5
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	1474	544	-253	0	-188	9137	15.71	15.71	9.42	9.42	3	0.18	0.01	0.05	0.00	0.00	24.0
2	0	-1255	337	-72	0	-102	5465	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
3	0	-1266	348	-174	0	-97	5463	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
4	0	3533	488	-214	0	-193	8595	15.71	15.71	9.42	9.42	2	0.25	0.01	0.05	0.00	0.00	24.0
5	0	3522	500	-317	0	-188	8592	15.71	15.71	9.42	9.42	2	0.25	0.01	0.05	0.00	0.00	24.0
6	0	434	376	-1	0	-140	6564	15.71	15.71	9.42	9.42	2	0.18	0.00	0.04	0.00	0.00	24.0
7	0	397	415	-345	0	-122	6554	15.71	15.71	9.42	9.42	2	0.18	0.01	0.04	0.00	0.00	24.0
8	0	1870	422	-44	0	-167	7503	15.71	15.71	9.42	9.42	2	0.21	0.01	0.04	0.00	0.00	24.0
9	0	1834	460	-387	0	-150	7493	15.71	15.71	9.42	9.42	2	0.21	0.01	0.04	0.00	0.00	24.0
10	0	-1255	337	-72	0	-102	5465	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
11	0	-1266	348	-174	0	-97	5463	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
12	0	3533	488	-214	0	-193	8595	15.71	15.71	9.42	9.42	2	0.25	0.01	0.05	0.00	0.00	24.0
13	0	3522	500	-317	0	-188	8592	15.71	15.71	9.42	9.42	2	0.25	0.01	0.05	0.00	0.00	24.0
14	0	434	376	-1	0	-140	6564	15.71	15.71	9.42	9.42	2	0.18	0.00	0.04	0.00	0.00	24.0
15	0	397	415	-345	0	-122	6554	15.71	15.71	9.42	9.42	2	0.18	0.01	0.04	0.00	0.00	24.0
16	0	1870	422	-44	0	-167	7503	15.71	15.71	9.42	9.42	2	0.21	0.01	0.04	0.00	0.00	24.0
17	0	1834	460	-387	0	-150	7493	15.71	15.71	9.42	9.42	2	0.21	0.01	0.04	0.00	0.00	24.0
18	0	1051	1648	-295	0	-251	12090	15.71	15.71	9.42	9.42	3	0.24	0.02	0.15	0.00	0.00	24.0
19	0	21480	356	-705	0	-513	23890	15.71	15.71	9.42	9.42	3	0.53	0.01	0.05	0.00	0.00	24.0
20	0	9869	963	-786	0	-334	16680	15.71	15.71	9.42	9.42	3	0.34	0.01	0.09	0.00	0.00	24.0
37	0	-8970	1931	-79	0	-101	5277	15.71	15.71	9.42	9.42	3	0.10	0.02	0.16	0.00	0.00	24.0
38	0	25080	-224	-762	0	-537	24940	15.71	15.71	9.42	9.42	3	0.56	0.01	0.05	0.00	0.00	24.0
39	0	5726	789	-897	0	-239	12910	15.71	15.71	9.42	9.42	3	0.26	0.01	0.07	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	1604	544	-253	0	-157	9205	15.71	15.71	9.42	9.42	3	0.18	0.01	0.05	0.00	0.00	24.0
2	12	-1155	337	-72	0	-93	5507	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
3	12	-1166	348	-174	0	-75	5506	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
4	12	3633	488	-214	0	-166	8656	15.71	15.71	9.42	9.42	2	0.25	0.01	0.05	0.00	0.00	24.0
5	12	3622	500	-317	0	-148	8655	15.71	15.71	9.42	9.42	2	0.25	0.01	0.05	0.00	0.00	24.0
6	12	534	376	-1	0	-140	6611	15.71	15.71	9.42	9.42	2	0.18	0.00	0.04	0.00	0.00	24.0
7	12	497	415	-345	0	-79	6606	15.71	15.71	9.42	9.42	2	0.18	0.01	0.04	0.00	0.00	24.0
8	12	1970	422	-44	0	-162	7556	15.71	15.71	9.42	9.42	2	0.21	0.01	0.04	0.00	0.00	24.0
9	12	1934	460	-387	0	-101	7551	15.71	15.71	9.42	9.42	2	0.21	0.01	0.04	0.00	0.00	24.0
10	12	-1155	337	-72	0	-93	5507	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
11	12	-1166	348	-174	0	-75	5506	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
12	12	3633	488	-214	0	-166	8656	15.71	15.71	9.42	9.42	2	0.25	0.01	0.05	0.00	0.00	24.0
13	12	3622	500	-317	0	-148	8655	15.71	15.71	9.42	9.42	2	0.25	0.01	0.05	0.00	0.00	24.0
14	12	534	376	-1	0	-140	6611	15.71	15.71	9.42	9.42	2	0.18	0.00	0.04	0.00	0.00	24.0
15	12	497	415	-345	0	-79	6606	15.71	15.71	9.42	9.42	2	0.18	0.01	0.04	0.00	0.00	24.0
16	12	1970	422	-44	0	-162	7556	15.71	15.71	9.42	9.42	2	0.21	0.01	0.04	0.00	0.00	24.0
17	12	1934	460	-387	0	-101	7551	15.71	15.71	9.42	9.42	2	0.21	0.01	0.04	0.00	0.00	24.0
18	12	1181	1648	-295	0	-214	12297	15.71	15.71	9.42	9.42	3	0.24	0.02	0.15	0.00	0.00	24.0
19	12	21610	356	-705	0	-425	23935	15.71	15.71	9.42	9.42	3	0.53	0.01	0.05	0.00	0.00	24.0
20	12	9999	963	-786	0	-236	16800	15.71	15.71	9.42	9.42	3	0.34	0.01	0.09	0.00	0.00	24.0
37	12	-8840	1931	-79	0	-91	5518	15.71	15.71	9.42	9.42	3	0.10	0.02	0.16	0.00	0.00	24.0
38	12	25210	-224	-762	0	-442	24913	15.71	15.71	9.42	9.42	3	0.56	0.01	0.05	0.00	0.00	24.0
39	12	5856	789	-897	0	-127	13010	15.71	15.71	9.42	9.42	3	0.26	0.01	0.07	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	1734	544	-253	0	-125	9273	15.71	15.71	9.42	9.42	3	0.18	0.01	0.05	0.00	0.00	24.0
2	25	-1055	337	-72	0	-84	5549	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
3	25	-1066	348	-174	0	-53	5550	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
4	25	3733	488	-214	0	-140	8717	15.71	15.71	9.42	9.42	2	0.25	0.01	0.05	0.00	0.00	24.0
5	25	3722	500	-317	0	-109	8717	15.71	15.71	9.42	9.42	2	0.25	0.01	0.05	0.00	0.00	24.0
6	25	634	376	-1	0	-140	6658	15.71	15.71	9.42	9.42	2	0.19	0.00	0.04	0.00	0.00	24.0
7	25	597	415	-345	0	-36	6658	15.71	15.71	9.42	9.42	2	0.18	0.01	0.04	0.00	0.00	24.0
8	25	2070	422	-44	0	-156	7609	15.71	15.71	9.42	9.42	2	0.21	0.01	0.04	0.00	0.00	24.0
9	25	2034	460	-387	0	-53	7609	15.71	15.71	9.42	9.42	2	0.21	0.01	0.04	0.00	0.00	24.0
10	25	-1055	337	-72	0	-84	5549	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
11	25	-1066	348	-174	0	-53	5550	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
12	25	3733	488	-214	0	-140	8717	15.71	15.71	9.42	9.42	2	0.25	0.01	0.05	0.00	0.00	24.0
13	25	3722	500	-317	0	-109	8717	15.71	15.71	9.42	9.42	2	0.25	0.01	0.05	0.00	0.00	24.0
14	25	634	376	-1	0	-140	6658	15.71	15.71	9.42	9.42	2	0.19	0.00	0.04	0.00	0.00	24.0
15	25	597	415	-345	0	-36	6658	15.71	15.71	9.42	9.42	2	0.18	0.01	0.04	0.00	0.00	24.0
16	25	2070	422	-44	0	-156	7609	15.71	15.71	9.42	9.42	2	0.21	0.01	0.04	0.00	0.00	24.0
17	25	2034	460	-387	0	-53	7609	15.71	15.71	9.42	9.42	2	0.21	0.01	0.04	0.00	0.00	24.0
18	25	1311	1648	-295	0	-178	12505	15.71	15.71	9.42	9.42	3	0.24	0.02	0.15	0.00	0.00	24.0
19	25	21740	356	-705	0	-337	23980	15.71	15.71	9.42	9.42	3	0.53	0.01	0.05	0.00	0.00	24.0
20	25	10130	963	-786	0	-138	16920	15.71	15.71	9.42	9.42	3	0.35	0.01	0.09	0.00	0.00	24.0
37	25	-8710	1931	-79	0	-81	5759	15.71	15.71	9.42	9.42	3	0.11	0.02	0.16	0.00	0.00	24.0
38	25	25340	-224	-762	0	-347	24885	15.71	15.71	9.42	9.42	3	0.56	0.01	0.05	0.00	0.00	24.0
39	25	5986	789	-897	0	-15	13110	15.71	15.71	9.42	9.42	3	0.26	0.01	0.07	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	1864	544	-253	0	-94	9341	15.71	15.71	9.42	9.42	3	0.18	0.01	0.05	0.00	0.00	24.0
2	38	-955	337	-72	0	-75	5592	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
3	38	-966	348	-174	0	-31	5594	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
4	38	3833	488	-214	0	-113	8778	15.71	15.71	9.42	9.42	2	0.25	0.01	0.05	0.00	0.00	24.0
5	38	3822	500	-317	0	-69	8780	15.71	15.71	9.42	9.42	2	0.25	0.01	0.05	0.00	0.00	24.0
6	38	734	376	-1	0	-139	6705	15.71	15.71	9.42	9.42	2	0.19	0.00	0.04	0.00	0.00	24.0
7	38	697	415	-345	0	7	6710	15.71	15.71	9.42	9.42	2	0.18	0.01	0.04	0.00	0.00	24.0
8	38	2170	422	-44	0	-151	7661	15.71	15.71	9.42	9.42	2	0.22	0.01	0.04	0.00	0.00	24.0
9	38	2134	460	-387	0	-5	7666	15.71	15.71	9.42	9.42	2	0.21	0.01	0.04	0.00	0.00	24.0
10	38	-955	337	-72	0	-75	5592	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
11	38	-966	348	-174	0	-31	5594	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
12	38	3833	488	-214	0	-113	8778	15.71	15.71	9.42	9.42	2	0.25	0.01	0.05	0.00	0.00	24.0
13	38	3822	500	-317	0	-69	8780	15.71	15.71	9.42	9.42	2	0.25	0.01	0.05	0.00	0.00	24.0
14	38	734	376	-1	0	-139	6705	15.71	15.71	9.42	9.42	2	0.19	0.00	0.04	0.00	0.00	24.0
15	38	697	415	-345	0	7	6710	15.71	15.71	9.42	9.42	2	0.18	0.01	0.04	0.00	0.00	24.0
16	38	2170	422	-44	0	-151	7661	15.71	15.71	9.42	9.42	2	0.22	0.01	0.04	0.00	0.00	24.0

17	38	2134	460	-387	0	-5	7666	15.71	15.71	9.42	9.42	2	0.21	0.01	0.04	0.00	0.00	24.0
18	38	1441	1648	-295	0	-141	12712	15.71	15.71	9.42	9.42	3	0.25	0.02	0.15	0.00	0.00	24.0
19	38	21870	356	-705	0	-249	24025	15.71	15.71	9.42	9.42	3	0.53	0.01	0.05	0.00	0.00	24.0
20	38	10260	963	-786	0	-39	17040	15.71	15.71	9.42	9.42	3	0.35	0.01	0.09	0.00	0.00	24.0
37	38	-8580	1931	-79	0	-71	6001	15.71	15.71	9.42	9.42	3	0.11	0.02	0.16	0.00	0.00	24.0
38	38	25470	-224	-762	0	-252	24857	15.71	15.71	9.42	9.42	3	0.56	0.01	0.05	0.00	0.00	24.0
39	38	6116	789	-897	0	97	13210	15.71	15.71	9.42	9.42	3	0.26	0.01	0.07	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	1994	544	-253	0	-62	9409	15.71	15.71	9.42	9.42	3	0.18	0.01	0.05	0.00	0.00	24.0
2	50	-855	337	-72	0	-66	5634	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
3	50	-866	348	-174	0	-9	5637	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
4	50	3933	488	-214	0	-86	8839	15.71	15.71	9.42	9.42	2	0.25	0.01	0.05	0.00	0.00	24.0
5	50	3922	500	-317	0	-29	8842	15.71	15.71	9.42	9.42	2	0.25	0.01	0.05	0.00	0.00	24.0
6	50	834	376	-1	0	-139	6752	15.71	15.71	9.42	9.42	2	0.19	0.00	0.04	0.00	0.00	24.0
7	50	797	415	-345	0	50	6762	15.71	15.71	9.42	9.42	2	0.19	0.01	0.04	0.00	0.00	24.0
8	50	2270	422	-44	0	-145	7714	15.71	15.71	9.42	9.42	2	0.22	0.01	0.04	0.00	0.00	24.0
9	50	2234	460	-387	0	44	7724	15.71	15.71	9.42	9.42	2	0.22	0.01	0.04	0.00	0.00	24.0
10	50	-855	337	-72	0	-66	5634	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
11	50	-866	348	-174	0	-9	5637	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
12	50	3933	488	-214	0	-86	8839	15.71	15.71	9.42	9.42	2	0.25	0.01	0.05	0.00	0.00	24.0
13	50	3922	500	-317	0	-29	8842	15.71	15.71	9.42	9.42	2	0.25	0.01	0.05	0.00	0.00	24.0
14	50	834	376	-1	0	-139	6752	15.71	15.71	9.42	9.42	2	0.19	0.00	0.04	0.00	0.00	24.0
15	50	797	415	-345	0	50	6762	15.71	15.71	9.42	9.42	2	0.19	0.01	0.04	0.00	0.00	24.0
16	50	2270	422	-44	0	-145	7714	15.71	15.71	9.42	9.42	2	0.22	0.01	0.04	0.00	0.00	24.0
17	50	2234	460	-387	0	44	7724	15.71	15.71	9.42	9.42	2	0.22	0.01	0.04	0.00	0.00	24.0
18	50	1571	1648	-295	0	-104	12920	15.71	15.71	9.42	9.42	3	0.25	0.02	0.15	0.00	0.00	24.0
19	50	22000	356	-705	0	-161	24070	15.71	15.71	9.42	9.42	3	0.53	0.01	0.05	0.00	0.00	24.0
20	50	10390	963	-786	0	59	17160	15.71	15.71	9.42	9.42	3	0.35	0.01	0.09	0.00	0.00	24.0
37	50	-8450	1931	-79	0	-62	6242	15.71	15.71	9.42	9.42	3	0.12	0.02	0.16	0.00	0.00	24.0
38	50	25600	-224	-762	0	-156	24830	15.71	15.71	9.42	9.42	3	0.56	0.01	0.05	0.00	0.00	24.0
39	50	6246	789	-897	0	209	13310	15.71	15.71	9.42	9.42	3	0.27	0.01	0.07	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 69 NI 1600 NF 1601 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 4
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	2931	531	84	0	-3	10180	15.71	15.71	9.42	9.42	3	0.20	0.01	0.05	0.00	0.00	24.0
2	0	-471	362	126	0	3	6052	15.71	15.71	9.42	9.42	2	0.16	0.00	0.03	0.00	0.00	24.0
3	0	-545	351	25	0	8	5999	15.71	15.71	9.42	9.42	2	0.16	0.00	0.03	0.00	0.00	24.0
4	0	5055	466	104	0	-14	9663	15.71	15.71	9.42	9.42	2	0.27	0.01	0.04	0.00	0.00	24.0
5	0	4981	455	3	0	-8	9609	15.71	15.71	9.42	9.42	2	0.27	0.01	0.04	0.00	0.00	24.0
6	0	1549	411	237	0	-9	7378	15.71	15.71	9.42	9.42	2	0.20	0.01	0.04	0.00	0.00	24.0
7	0	1303	375	-101	0	9	7200	15.71	15.71	9.42	9.42	2	0.20	0.00	0.04	0.00	0.00	24.0
8	0	3207	442	230	0	-14	8461	15.71	15.71	9.42	9.42	2	0.24	0.01	0.04	0.00	0.00	24.0
9	0	2961	406	-108	0	4	8283	15.71	15.71	9.42	9.42	2	0.23	0.01	0.04	0.00	0.00	24.0
10	0	-471	362	126	0	3	6052	15.71	15.71	9.42	9.42	2	0.16	0.00	0.03	0.00	0.00	24.0
11	0	-545	351	25	0	8	5999	15.71	15.71	9.42	9.42	2	0.16	0.00	0.03	0.00	0.00	24.0
12	0	5055	466	104	0	-14	9663	15.71	15.71	9.42	9.42	2	0.27	0.01	0.04	0.00	0.00	24.0
13	0	4981	455	3	0	-8	9609	15.71	15.71	9.42	9.42	2	0.27	0.01	0.04	0.00	0.00	24.0
14	0	1549	411	237	0	-9	7378	15.71	15.71	9.42	9.42	2	0.20	0.01	0.04	0.00	0.00	24.0
15	0	1303	375	-101	0	9	7200	15.71	15.71	9.42	9.42	2	0.20	0.00	0.04	0.00	0.00	24.0
16	0	3207	442	230	0	-14	8461	15.71	15.71	9.42	9.42	2	0.24	0.01	0.04	0.00	0.00	24.0
17	0	2961	406	-108	0	4	8283	15.71	15.71	9.42	9.42	2	0.23	0.01	0.04	0.00	0.00	24.0
18	0	2976	1685	188	0	13	13530	15.71	15.71	9.42	9.42	3	0.27	0.02	0.16	0.00	0.00	24.0
19	0	25330	190	130	0	-30	26570	15.71	15.71	9.42	9.42	3	0.60	0.00	0.02	0.00	0.00	24.0
20	0	12310	848	-148	0	8	18440	15.71	15.71	9.42	9.42	3	0.38	0.01	0.08	0.00	0.00	24.0
37	0	-8149	2051	182	0	30	5972	15.71	15.71	9.42	9.42	3	0.11	0.03	0.17	0.00	0.00	24.0
38	0	29100	-440	86	0	-43	27700	15.71	15.71	9.42	9.42	3	0.65	0.01	0.04	0.00	0.00	24.0
39	0	7411	657	-377	0	20	14150	15.71	15.71	9.42	9.42	3	0.28	0.01	0.06	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	3061	531	84	0	-14	10248	15.71	15.71	9.42	9.42	3	0.20	0.01	0.05	0.00	0.00	24.0
2	12	-371	362	126	0	-13	6097	15.71	15.71	9.42	9.42	2	0.17	0.00	0.03	0.00	0.00	24.0
3	12	-445	351	25	0	5	6043	15.71	15.71	9.42	9.42	2	0.16	0.00	0.03	0.00	0.00	24.0
4	12	5155	466	104	0	-27	9721	15.71	15.71	9.42	9.42	2	0.28	0.01	0.04	0.00	0.00	24.0
5	12	5081	455	3	0	-9	9666	15.71	15.71	9.42	9.42	2	0.27	0.01	0.04	0.00	0.00	24.0
6	12	1649	411	237	0	-39	7430	15.71	15.71	9.42	9.42	2	0.21	0.01	0.04	0.00	0.00	24.0
7	12	1403	375	-101	0	21	7247	15.71	15.71	9.42	9.42	2	0.20	0.00	0.04	0.00	0.00	24.0
8	12	3307	442	230	0	-43	8516	15.71	15.71	9.42	9.42	2	0.24	0.01	0.04	0.00	0.00	24.0
9	12	3061	406	-108	0	17	8334	15.71	15.71	9.42	9.42	2	0.23	0.01	0.04	0.00	0.00	24.0
10	12	-371	362	126	0	-13	6097	15.71	15.71	9.42	9.42	2	0.17	0.00	0.03	0.00	0.00	24.0
11	12	-445	351	25	0	5	6043	15.71	15.71	9.42	9.42	2	0.16	0.00	0.03	0.00	0.00	24.0
12	12	5155	466	104	0	-27	9721	15.71	15.71	9.42	9.42	2	0.28	0.01	0.04	0.00	0.00	24.0
13	12	5081	455	3	0	-9	9666	15.71	15.71	9.42	9.42	2	0.27	0.01	0.04	0.00	0.00	24.0
14	12	1649	411	237	0	-39	7430	15.71	15.71	9.42	9.42	2	0.21	0.01	0.04	0.00	0.00	24.0
15	12	1403	375	-101	0	21	7247	15.71	15.71	9.42	9.42	2	0.20	0.00	0.04	0.00	0.00	24.0
16	12	3307	442	230	0	-43	8516	15.71	15.71	9.42	9.42	2	0.24	0.01	0.04	0.00	0.00	24.0
17	12	3061	406	-108	0	17	8334	15.71	15.71	9.42	9.42	2	0.23	0.01	0.04	0.00	0.00	24.0
18	12	3106	1685	188	0	-10	13740	15.71	15.71	9.42	9.42	3	0.27	0.02	0.16	0.00	0.00	24.0
19	12	25460	190	130	0	-47	26593	15.71	15.71	9.42	9.42	3	0.60	0.00	0.02	0.00	0.00	24.0
20	12	12440	848	-148	0	26	18545	15.71	15.71	9.42	9.42	3	0.38	0.01	0.08	0.00	0.00	24.0
37	12	-8019	2051	182	0	7	6228	15.71	15.71	9.42	9.42	3	0.12	0.03	0.17	0.00	0.00	24.0
38	12	29230	-440	86	0	-54	27645	15.71	15.71	9.42	9.42	3	0.65	0.01	0.04	0.00	0.00	24.0
39	12	7541	657	-377	0	67	14232	15.71	15.71	9.42	9.42	3	0.29	0.01	0.06	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	3191	531	84	0	-24	10315	15.71	15.71	9.42	9.42	3	0.20	0.01	0.05	0.00	0.00	24.0
2	25	-271	362	126	0	-29	6142	15.71	15.71	9.42	9.42	2	0.17	0.00	0.03	0.00	0.00	24.0
3	25	-345	351	25	0	2	6086	15.71	15.71	9.42	9.42	2	0.17	0.00	0.03	0.00	0.00	24.0
4	25	5255	466	104	0	-40	9780	15.71	15.71	9.42	9.42	2	0.28	0.01	0.04	0.00	0.00	24.0
5	25	5181	455	3	0	-9	9723	15.71	15.71	9.42	9.42	2	0.28	0.01	0.04	0.00	0.00	24.0
6	25	1749	411	237	0	-68	7481	15.71	15.71	9.42	9.42	2	0.21	0.01	0.04	0.00	0.00	24.0
7	25	1503	375	-101	0	34	7294	15.71	15.71	9.42	9.42	2	0.20	0.00	0.04	0.00	0.00	24.0
8	25	3407	442	230	0	-72	8571	15.71	15.71	9.42	9.42	2	0.24	0.01	0.04	0.00	0.00	24.0
9	25	3161	406	-108	0	31	8385	15.71	15.71	9.42	9.42	2	0.23	0.01	0.04	0.00	0.00	24.0
10	25	-271	362	126	0	-29	6142	15.71	15.71	9.42	9.42	2	0.17	0.00	0.03	0.00	0.00	24.0
11	25	-345	351	25	0	2	6086	15.71	15.71	9.42	9.42	2	0.17	0.00	0.03	0.00	0.00	24.0
12	25	5255	466	104	0	-40	9780	15.71	15.71	9.42	9.42	2	0.28	0.01	0.04	0.00	0.00	24.0

13	25	5181	455	3	0	-9	9723	15.71	15.71	9.42	9.42	2	0.28	0.01	0.04	0.00	0.00	24.0
14	25	1749	411	237	0	-68	7481	15.71	15.71	9.42	9.42	2	0.21	0.01	0.04	0.00	0.00	24.0
15	25	1503	375	-101	0	34	7294	15.71	15.71	9.42	9.42	2	0.20	0.00	0.04	0.00	0.00	24.0
16	25	3407	442	230	0	-72	8571	15.71	15.71	9.42	9.42	2	0.24	0.01	0.04	0.00	0.00	24.0
17	25	3161	406	-108	0	31	8385	15.71	15.71	9.42	9.42	2	0.23	0.01	0.04	0.00	0.00	24.0
18	25	3236	1685	188	0	-34	13950	15.71	15.71	9.42	9.42	3	0.27	0.02	0.16	0.00	0.00	24.0
19	25	25590	190	130	0	-63	26615	15.71	15.71	9.42	9.42	3	0.60	0.00	0.02	0.00	0.00	24.0
20	25	12570	848	-148	0	44	18650	15.71	15.71	9.42	9.42	3	0.39	0.01	0.08	0.00	0.00	24.0
37	25	-7889	2051	182	0	-16	6484	15.71	15.71	9.42	9.42	3	0.12	0.03	0.17	0.00	0.00	24.0
38	25	29360	-440	86	0	-65	27590	15.71	15.71	9.42	9.42	3	0.64	0.01	0.04	0.00	0.00	24.0
39	25	7671	657	-377	0	114	14315	15.71	15.71	9.42	9.42	3	0.29	0.01	0.06	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	3321	531	84	0	-35	10383	15.71	15.71	9.42	9.42	3	0.20	0.01	0.05	0.00	0.00	24.0
2	38	-171	362	126	0	-44	6188	15.71	15.71	9.42	9.42	2	0.17	0.00	0.03	0.00	0.00	24.0
3	38	-245	351	25	0	-1	6130	15.71	15.71	9.42	9.42	2	0.17	0.00	0.03	0.00	0.00	24.0
4	38	5355	466	104	0	-53	9838	15.71	15.71	9.42	9.42	2	0.28	0.01	0.04	0.00	0.00	24.0
5	38	5281	455	3	0	-9	9780	15.71	15.71	9.42	9.42	2	0.28	0.01	0.04	0.00	0.00	24.0
6	38	1849	411	237	0	-98	7532	15.71	15.71	9.42	9.42	2	0.21	0.01	0.04	0.00	0.00	24.0
7	38	1603	375	-101	0	47	7340	15.71	15.71	9.42	9.42	2	0.20	0.00	0.04	0.00	0.00	24.0
8	38	3507	442	230	0	-100	8627	15.71	15.71	9.42	9.42	2	0.24	0.01	0.04	0.00	0.00	24.0
9	38	3261	406	-108	0	44	8435	15.71	15.71	9.42	9.42	2	0.24	0.01	0.04	0.00	0.00	24.0
10	38	-171	362	126	0	-44	6188	15.71	15.71	9.42	9.42	2	0.17	0.00	0.03	0.00	0.00	24.0
11	38	-245	351	25	0	-1	6130	15.71	15.71	9.42	9.42	2	0.17	0.00	0.03	0.00	0.00	24.0
12	38	5355	466	104	0	-53	9838	15.71	15.71	9.42	9.42	2	0.28	0.01	0.04	0.00	0.00	24.0
13	38	5281	455	3	0	-9	9780	15.71	15.71	9.42	9.42	2	0.28	0.01	0.04	0.00	0.00	24.0
14	38	1849	411	237	0	-98	7532	15.71	15.71	9.42	9.42	2	0.21	0.01	0.04	0.00	0.00	24.0
15	38	1603	375	-101	0	47	7340	15.71	15.71	9.42	9.42	2	0.20	0.00	0.04	0.00	0.00	24.0
16	38	3507	442	230	0	-100	8627	15.71	15.71	9.42	9.42	2	0.24	0.01	0.04	0.00	0.00	24.0
17	38	3261	406	-108	0	44	8435	15.71	15.71	9.42	9.42	2	0.24	0.01	0.04	0.00	0.00	24.0
18	38	3366	1685	188	0	-57	14160	15.71	15.71	9.42	9.42	3	0.28	0.02	0.16	0.00	0.00	24.0
19	38	25720	190	130	0	-79	26638	15.71	15.71	9.42	9.42	3	0.61	0.00	0.02	0.00	0.00	24.0
20	38	12700	848	-148	0	63	18755	15.71	15.71	9.42	9.42	3	0.39	0.01	0.08	0.00	0.00	24.0
37	38	-7759	2051	182	0	-39	6741	15.71	15.71	9.42	9.42	3	0.13	0.03	0.17	0.00	0.00	24.0
38	38	29490	-440	86	0	-75	27535	15.71	15.71	9.42	9.42	3	0.64	0.01	0.04	0.00	0.00	24.0
39	38	7801	657	-377	0	161	14397	15.71	15.71	9.42	9.42	3	0.29	0.01	0.06	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	3451	531	84	0	-45	10450	15.71	15.71	9.42	9.42	3	0.21	0.01	0.05	0.00	0.00	24.0
2	50	-71	362	126	0	-60	6233	15.71	15.71	9.42	9.42	2	0.17	0.00	0.03	0.00	0.00	24.0
3	50	-145	351	25	0	-4	6174	15.71	15.71	9.42	9.42	2	0.17	0.00	0.03	0.00	0.00	24.0
4	50	5455	466	104	0	-66	9896	15.71	15.71	9.42	9.42	2	0.28	0.01	0.04	0.00	0.00	24.0
5	50	5381	455	3	0	-10	9837	15.71	15.71	9.42	9.42	2	0.28	0.01	0.04	0.00	0.00	24.0
6	50	1949	411	237	0	-127	7584	15.71	15.71	9.42	9.42	2	0.21	0.01	0.04	0.00	0.00	24.0
7	50	1703	375	-101	0	59	7387	15.71	15.71	9.42	9.42	2	0.21	0.00	0.04	0.00	0.00	24.0
8	50	3607	442	230	0	-129	8682	15.71	15.71	9.42	9.42	2	0.25	0.01	0.04	0.00	0.00	24.0
9	50	3361	406	-108	0	58	8486	15.71	15.71	9.42	9.42	2	0.24	0.01	0.04	0.00	0.00	24.0
10	50	-71	362	126	0	-60	6233	15.71	15.71	9.42	9.42	2	0.17	0.00	0.03	0.00	0.00	24.0
11	50	-145	351	25	0	-4	6174	15.71	15.71	9.42	9.42	2	0.17	0.00	0.03	0.00	0.00	24.0
12	50	5455	466	104	0	-66	9896	15.71	15.71	9.42	9.42	2	0.28	0.01	0.04	0.00	0.00	24.0
13	50	5381	455	3	0	-10	9837	15.71	15.71	9.42	9.42	2	0.28	0.01	0.04	0.00	0.00	24.0
14	50	1949	411	237	0	-127	7584	15.71	15.71	9.42	9.42	2	0.21	0.01	0.04	0.00	0.00	24.0
15	50	1703	375	-101	0	59	7387	15.71	15.71	9.42	9.42	2	0.21	0.00	0.04	0.00	0.00	24.0
16	50	3607	442	230	0	-129	8682	15.71	15.71	9.42	9.42	2	0.25	0.01	0.04	0.00	0.00	24.0
17	50	3361	406	-108	0	58	8486	15.71	15.71	9.42	9.42	2	0.24	0.01	0.04	0.00	0.00	24.0
18	50	3496	1685	188	0	-81	14370	15.71	15.71	9.42	9.42	3	0.28	0.02	0.16	0.00	0.00	24.0
19	50	25850	190	130	0	-95	26660	15.71	15.71	9.42	9.42	3	0.61	0.00	0.02	0.00	0.00	24.0
20	50	12830	848	-148	0	81	18860	15.71	15.71	9.42	9.42	3	0.39	0.01	0.08	0.00	0.00	24.0
37	50	-7629	2051	182	0	-61	6997	15.71	15.71	9.42	9.42	3	0.13	0.03	0.17	0.00	0.00	24.0
38	50	29620	-440	86	0	-86	27480	15.71	15.71	9.42	9.42	3	0.64	0.01	0.04	0.00	0.00	24.0
39	50	7931	657	-377	0	208	14480	15.71	15.71	9.42	9.42	3	0.29	0.01	0.06	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 70 NI 1620 NF 1621 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 3
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	1495	524	392	0	168	9102	15.71	15.71	9.42	9.42	3	0.18	0.01	0.05	0.00	0.00	24.0
2	0	-1528	336	317	0	108	5250	15.71	15.71	9.42	9.42	2	0.14	0.00	0.03	0.00	0.00	24.0
3	0	-1521	336	211	0	108	5257	15.71	15.71	9.42	9.42	2	0.14	0.00	0.03	0.00	0.00	24.0
4	0	3820	469	393	0	151	8746	15.71	15.71	9.42	9.42	2	0.25	0.01	0.04	0.00	0.00	24.0
5	0	3828	470	286	0	151	8754	15.71	15.71	9.42	9.42	2	0.25	0.01	0.04	0.00	0.00	24.0
6	0	334	382	468	0	123	6464	15.71	15.71	9.42	9.42	2	0.18	0.01	0.04	0.00	0.00	24.0
7	0	361	384	113	0	123	6490	15.71	15.71	9.42	9.42	2	0.18	0.01	0.04	0.00	0.00	24.0
8	0	1939	422	491	0	136	7513	15.71	15.71	9.42	9.42	2	0.21	0.01	0.04	0.00	0.00	24.0
9	0	1965	424	136	0	136	7539	15.71	15.71	9.42	9.42	2	0.21	0.01	0.04	0.00	0.00	24.0
10	0	-1528	336	317	0	108	5250	15.71	15.71	9.42	9.42	2	0.14	0.00	0.03	0.00	0.00	24.0
11	0	-1521	336	211	0	108	5257	15.71	15.71	9.42	9.42	2	0.14	0.00	0.03	0.00	0.00	24.0
12	0	3820	469	393	0	151	8746	15.71	15.71	9.42	9.42	2	0.25	0.01	0.04	0.00	0.00	24.0
13	0	3828	470	286	0	151	8754	15.71	15.71	9.42	9.42	2	0.25	0.01	0.04	0.00	0.00	24.0
14	0	334	382	468	0	123	6464	15.71	15.71	9.42	9.42	2	0.18	0.01	0.04	0.00	0.00	24.0
15	0	361	384	113	0	123	6490	15.71	15.71	9.42	9.42	2	0.18	0.01	0.04	0.00	0.00	24.0
16	0	1939	422	491	0	136	7513	15.71	15.71	9.42	9.42	2	0.21	0.01	0.04	0.00	0.00	24.0
17	0	1965	424	136	0	136	7539	15.71	15.71	9.42	9.42	2	0.21	0.01	0.04	0.00	0.00	24.0
18	0	449	1633	655	0	269	11630	15.71	15.71	9.42	9.42	3	0.23	0.02	0.15	0.00	0.00	24.0
19	0	22360	288	887	0	402	24390	15.71	15.71	9.42	9.42	3	0.54	0.01	0.06	0.00	0.00	24.0
20	0	9953	895	420	0	311	16690	15.71	15.71	9.42	9.42	3	0.34	0.01	0.08	0.00	0.00	24.0
37	0	-10110	1939	454	0	170	4474	15.71	15.71	9.42	9.42	3	0.08	0.02	0.16	0.00	0.00	24.0
38	0	26410	-302	841	0	392	25750	15.71	15.71	9.42	9.42	3	0.59	0.01	0.06	0.00	0.00	24.0
39	0	5733	710	63	0	241	12910	15.71	15.71	9.42	9.42	3	0.26	0.01	0.07	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	1625	524	392	0	119	9168	15.71	15.71	9.42	9.42	3	0.18	0.01	0.05	0.00	0.00	24.0
2	12	-1428	336	317	0	68	5292	15.71	15.71	9.42	9.42	2	0.14	0.00	0.03	0.00	0.00	24.0
3	12	-1421	336	211	0	82	5299	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
4	12	3920	469	393	0	101	8805	15.71	15.71	9.42	9.42	2	0.25	0.01	0.04	0.00	0.00	24.0
5	12	3928	470	286	0	115	8812	15.71	15.71	9.42	9.42	2	0.25	0.01	0.04	0.00	0.00	24.0
6	12	434	382	468	0	64	6512	15.71	15.71	9.42	9.42	2	0.18	0.01	0.04	0.00	0.00	24.0
7	12	461	384	113	0	109	6538	15.71	15.71	9.42	9.42	2	0.18	0.01	0.04	0.00	0.00	24.0
8	12	2039	422	491	0	74	7566	15.71	15.71	9.42	9.42	2	0.21	0.01	0.04	0.00	0.00	24.0

9	12	2065	424	136	0	119	7592	15.71	15.71	9.42	9.42	2	0.21	0.01	0.04	0.00	0.00	24.0
10	12	-1428	336	317	0	68	5292	15.71	15.71	9.42	9.42	2	0.14	0.00	0.03	0.00	0.00	24.0
11	12	-1421	336	211	0	82	5299	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
12	12	3920	469	393	0	101	8805	15.71	15.71	9.42	9.42	2	0.25	0.01	0.04	0.00	0.00	24.0
13	12	3928	470	286	0	115	8812	15.71	15.71	9.42	9.42	2	0.25	0.01	0.04	0.00	0.00	24.0
14	12	434	382	468	0	64	6512	15.71	15.71	9.42	9.42	2	0.18	0.01	0.04	0.00	0.00	24.0
15	12	461	384	113	0	109	6538	15.71	15.71	9.42	9.42	2	0.18	0.01	0.04	0.00	0.00	24.0
16	12	2039	422	491	0	74	7566	15.71	15.71	9.42	9.42	2	0.21	0.01	0.04	0.00	0.00	24.0
17	12	2065	424	136	0	119	7592	15.71	15.71	9.42	9.42	2	0.21	0.01	0.04	0.00	0.00	24.0
18	12	579	1633	655	0	187	11835	15.71	15.71	9.42	9.42	3	0.23	0.02	0.15	0.00	0.00	24.0
19	12	22490	288	887	0	291	24428	15.71	15.71	9.42	9.42	3	0.54	0.01	0.06	0.00	0.00	24.0
20	12	10082	895	420	0	259	16802	15.71	15.71	9.42	9.42	3	0.34	0.01	0.08	0.00	0.00	24.0
37	12	-9979	1939	454	0	113	4716	15.71	15.71	9.42	9.42	3	0.09	0.02	0.16	0.00	0.00	24.0
38	12	26540	-302	841	0	287	25710	15.71	15.71	9.42	9.42	3	0.59	0.01	0.06	0.00	0.00	24.0
39	12	5863	710	63	0	233	12998	15.71	15.71	9.42	9.42	3	0.26	0.01	0.07	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	1755	524	392	0	70	9233	15.71	15.71	9.42	9.42	3	0.18	0.01	0.05	0.00	0.00	24.0
2	25	-1328	336	317	0	29	5333	15.71	15.71	9.42	9.42	2	0.14	0.00	0.03	0.00	0.00	24.0
3	25	-1321	336	211	0	55	5342	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
4	25	4020	469	393	0	52	8863	15.71	15.71	9.42	9.42	2	0.25	0.01	0.04	0.00	0.00	24.0
5	25	4028	470	286	0	79	8871	15.71	15.71	9.42	9.42	2	0.25	0.01	0.04	0.00	0.00	24.0
6	25	534	382	468	0	6	6560	15.71	15.71	9.42	9.42	2	0.18	0.01	0.04	0.00	0.00	24.0
7	25	561	384	113	0	95	6586	15.71	15.71	9.42	9.42	2	0.18	0.01	0.04	0.00	0.00	24.0
8	25	2139	422	491	0	13	7618	15.71	15.71	9.42	9.42	2	0.21	0.01	0.04	0.00	0.00	24.0
9	25	2165	424	136	0	102	7645	15.71	15.71	9.42	9.42	2	0.21	0.01	0.04	0.00	0.00	24.0
10	25	-1328	336	317	0	29	5333	15.71	15.71	9.42	9.42	2	0.14	0.00	0.03	0.00	0.00	24.0
11	25	-1321	336	211	0	55	5342	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
12	25	4020	469	393	0	52	8863	15.71	15.71	9.42	9.42	2	0.25	0.01	0.04	0.00	0.00	24.0
13	25	4028	470	286	0	79	8871	15.71	15.71	9.42	9.42	2	0.25	0.01	0.04	0.00	0.00	24.0
14	25	534	382	468	0	6	6560	15.71	15.71	9.42	9.42	2	0.18	0.01	0.04	0.00	0.00	24.0
15	25	561	384	113	0	95	6586	15.71	15.71	9.42	9.42	2	0.18	0.01	0.04	0.00	0.00	24.0
16	25	2139	422	491	0	13	7618	15.71	15.71	9.42	9.42	2	0.21	0.01	0.04	0.00	0.00	24.0
17	25	2165	424	136	0	102	7645	15.71	15.71	9.42	9.42	2	0.21	0.01	0.04	0.00	0.00	24.0
18	25	709	1633	655	0	105	12040	15.71	15.71	9.42	9.42	3	0.23	0.02	0.15	0.00	0.00	24.0
19	25	22620	288	887	0	180	24465	15.71	15.71	9.42	9.42	3	0.54	0.01	0.06	0.00	0.00	24.0
20	25	10212	895	420	0	206	16915	15.71	15.71	9.42	9.42	3	0.35	0.01	0.08	0.00	0.00	24.0
37	25	-9848	1939	454	0	56	4958	15.71	15.71	9.42	9.42	3	0.09	0.02	0.16	0.00	0.00	24.0
38	25	26670	-302	841	0	182	25670	15.71	15.71	9.42	9.42	3	0.59	0.01	0.06	0.00	0.00	24.0
39	25	5993	710	63	0	225	13085	15.71	15.71	9.42	9.42	3	0.26	0.01	0.07	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	1885	524	392	0	21	9298	15.71	15.71	9.42	9.42	3	0.18	0.01	0.05	0.00	0.00	24.0
2	38	-1228	336	317	0	-11	5375	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
3	38	-1221	336	211	0	29	5384	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
4	38	4120	469	393	0	3	8922	15.71	15.71	9.42	9.42	2	0.25	0.01	0.04	0.00	0.00	24.0
5	38	4128	470	286	0	43	8930	15.71	15.71	9.42	9.42	2	0.25	0.01	0.04	0.00	0.00	24.0
6	38	634	382	468	0	-53	6607	15.71	15.71	9.42	9.42	2	0.18	0.01	0.04	0.00	0.00	24.0
7	38	661	384	113	0	81	6634	15.71	15.71	9.42	9.42	2	0.18	0.01	0.04	0.00	0.00	24.0
8	38	2239	422	491	0	-48	7671	15.71	15.71	9.42	9.42	2	0.21	0.01	0.04	0.00	0.00	24.0
9	38	2265	424	136	0	85	7698	15.71	15.71	9.42	9.42	2	0.22	0.01	0.04	0.00	0.00	24.0
10	38	-1228	336	317	0	-11	5375	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
11	38	-1221	336	211	0	29	5384	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
12	38	4120	469	393	0	3	8922	15.71	15.71	9.42	9.42	2	0.25	0.01	0.04	0.00	0.00	24.0
13	38	4128	470	286	0	43	8930	15.71	15.71	9.42	9.42	2	0.25	0.01	0.04	0.00	0.00	24.0
14	38	634	382	468	0	-53	6607	15.71	15.71	9.42	9.42	2	0.18	0.01	0.04	0.00	0.00	24.0
15	38	661	384	113	0	81	6634	15.71	15.71	9.42	9.42	2	0.18	0.01	0.04	0.00	0.00	24.0
16	38	2239	422	491	0	-48	7671	15.71	15.71	9.42	9.42	2	0.21	0.01	0.04	0.00	0.00	24.0
17	38	2265	424	136	0	85	7698	15.71	15.71	9.42	9.42	2	0.22	0.01	0.04	0.00	0.00	24.0
18	38	839	1633	655	0	23	12245	15.71	15.71	9.42	9.42	3	0.24	0.02	0.15	0.00	0.00	24.0
19	38	22750	288	887	0	70	24502	15.71	15.71	9.42	9.42	3	0.54	0.01	0.06	0.00	0.00	24.0
20	38	10341	895	420	0	154	17027	15.71	15.71	9.42	9.42	3	0.35	0.01	0.08	0.00	0.00	24.0
37	38	-9717	1939	454	0	-0	5201	15.71	15.71	9.42	9.42	3	0.10	0.02	0.16	0.00	0.00	24.0
38	38	26800	-302	841	0	77	25630	15.71	15.71	9.42	9.42	3	0.59	0.01	0.06	0.00	0.00	24.0
39	38	6123	710	63	0	218	13173	15.71	15.71	9.42	9.42	3	0.26	0.01	0.07	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	2015	524	392	0	-28	9364	15.71	15.71	9.42	9.42	3	0.18	0.01	0.05	0.00	0.00	24.0
2	50	-1128	336	317	0	-51	5417	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
3	50	-1121	336	211	0	3	5426	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
4	50	4220	469	393	0	-46	8980	15.71	15.71	9.42	9.42	2	0.25	0.01	0.04	0.00	0.00	24.0
5	50	4228	470	286	0	8	8988	15.71	15.71	9.42	9.42	2	0.25	0.01	0.04	0.00	0.00	24.0
6	50	734	382	468	0	-111	6655	15.71	15.71	9.42	9.42	2	0.19	0.01	0.04	0.00	0.00	24.0
7	50	761	384	113	0	67	6682	15.71	15.71	9.42	9.42	2	0.18	0.01	0.04	0.00	0.00	24.0
8	50	2339	422	491	0	-110	7724	15.71	15.71	9.42	9.42	2	0.22	0.01	0.04	0.00	0.00	24.0
9	50	2365	424	136	0	68	7751	15.71	15.71	9.42	9.42	2	0.22	0.01	0.04	0.00	0.00	24.0
10	50	-1128	336	317	0	-51	5417	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
11	50	-1121	336	211	0	3	5426	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
12	50	4220	469	393	0	-46	8980	15.71	15.71	9.42	9.42	2	0.25	0.01	0.04	0.00	0.00	24.0
13	50	4228	470	286	0	8	8988	15.71	15.71	9.42	9.42	2	0.25	0.01	0.04	0.00	0.00	24.0
14	50	734	382	468	0	-111	6655	15.71	15.71	9.42	9.42	2	0.19	0.01	0.04	0.00	0.00	24.0
15	50	761	384	113	0	67	6682	15.71	15.71	9.42	9.42	2	0.18	0.01	0.04	0.00	0.00	24.0
16	50	2339	422	491	0	-110	7724	15.71	15.71	9.42	9.42	2	0.22	0.01	0.04	0.00	0.00	24.0
17	50	2365	424	136	0	68	7751	15.71	15.71	9.42	9.42	2	0.22	0.01	0.04	0.00	0.00	24.0
18	50	969	1633	655	0	-59	12450	15.71	15.71	9.42	9.42	3	0.24	0.02	0.15	0.00	0.00	24.0
19	50	22880	288	887	0	-41	24540	15.71	15.71	9.42	9.42	3	0.55	0.01	0.06	0.00	0.00	24.0
20	50	10470	895	420	0	101	17140	15.71	15.71	9.42	9.42	3	0.35	0.01	0.08	0.00	0.00	24.0
37	50	-9586	1939	454	0	-57	5443	15.71	15.71	9.42	9.42	3	0.10	0.02	0.16	0.00	0.00	24.0
38	50	26930	-302	841	0	-28	25590	15.71	15.71	9.42	9.42	3	0.59	0.01	0.06	0.00	0.00	24.0
39	50	6253	710	63	0	210	13260	15.71	15.71	9.42	9.42	3	0.27	0.01	0.07	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 71 NI 1640 NF 1641 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 2
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-3955	88	539	0	304	5279	15.71	15.71	9.42	9.42	3	0.10	0.01	0.04	0.00	0.00	24.0
2	0	-5168	-37	375	0	178	2671	15.71	15.71	9.42	9.42	2	0.07	0.01	0.03	0.00	0.00	24.0
3	0	-5072	-20	280	0	184	2743	15.71	15.71	9.42	9.42	2	0.08	0.00	0.02	0.00	0.00	24.0
4	0	-1012	155	549	0	283	5378	15.71	15.71	9.42	9.42	2	0.15	0.01	0.04	0.00	0.00	24.0

5	0	-916	173	454	0	289	5451	15.71	15.71	9.42	9.42	2	0.16	0.01	0.03	0.00	0.00	24.0
6	0	-3826	10	547	0	208	3534	15.71	15.71	9.42	9.42	2	0.10	0.01	0.04	0.00	0.00	24.0
7	0	-3506	68	230	0	228	3775	15.71	15.71	9.42	9.42	2	0.11	0.00	0.02	0.00	0.00	24.0
8	0	-2579	68	599	0	239	4346	15.71	15.71	9.42	9.42	2	0.12	0.01	0.04	0.00	0.00	24.0
9	0	-2259	126	282	0	259	4587	15.71	15.71	9.42	9.42	2	0.13	0.00	0.02	0.00	0.00	24.0
10	0	-5168	-37	375	0	178	2671	15.71	15.71	9.42	9.42	2	0.07	0.01	0.03	0.00	0.00	24.0
11	0	-5072	-20	280	0	184	2743	15.71	15.71	9.42	9.42	2	0.08	0.00	0.02	0.00	0.00	24.0
12	0	-1012	155	549	0	283	5378	15.71	15.71	9.42	9.42	2	0.15	0.01	0.04	0.00	0.00	24.0
13	0	-916	173	454	0	289	5451	15.71	15.71	9.42	9.42	2	0.16	0.01	0.03	0.00	0.00	24.0
14	0	-3826	10	547	0	208	3534	15.71	15.71	9.42	9.42	2	0.10	0.01	0.04	0.00	0.00	24.0
15	0	-3506	68	230	0	228	3775	15.71	15.71	9.42	9.42	2	0.11	0.00	0.02	0.00	0.00	24.0
16	0	-2579	68	599	0	239	4346	15.71	15.71	9.42	9.42	2	0.12	0.01	0.04	0.00	0.00	24.0
17	0	-2259	126	282	0	259	4587	15.71	15.71	9.42	9.42	2	0.13	0.00	0.02	0.00	0.00	24.0
18	0	-8597	686	813	0	457	5116	15.71	15.71	9.42	9.42	3	0.10	0.01	0.06	0.00	0.00	24.0
19	0	10320	-25	1516	0	853	15910	15.71	15.71	9.42	9.42	3	0.33	0.02	0.11	0.00	0.00	24.0
20	0	356	336	812	0	620	9889	15.71	15.71	9.42	9.42	3	0.20	0.01	0.06	0.00	0.00	24.0
37	0	-16500	842	374	0	210	-191	15.71	15.71	9.42	9.42	3	0.01	0.01	0.06	0.00	0.00	24.0
38	0	15030	-342	1546	0	870	17800	15.71	15.71	9.42	9.42	3	0.38	0.02	0.11	0.00	0.00	24.0
39	0	-1574	260	372	0	482	7764	15.71	15.71	9.42	9.42	3	0.15	0.01	0.03	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-3825	88	539	0	236	5290	15.71	15.71	9.42	9.42	3	0.10	0.01	0.04	0.00	0.00	24.0
2	12	-5068	-37	375	0	131	2666	15.71	15.71	9.42	9.42	2	0.07	0.01	0.03	0.00	0.00	24.0
3	12	-4972	-20	280	0	149	2740	15.71	15.71	9.42	9.42	2	0.08	0.00	0.02	0.00	0.00	24.0
4	12	-912	155	549	0	215	5398	15.71	15.71	9.42	9.42	2	0.15	0.01	0.04	0.00	0.00	24.0
5	12	-816	173	454	0	232	5473	15.71	15.71	9.42	9.42	2	0.15	0.01	0.03	0.00	0.00	24.0
6	12	-3726	10	547	0	139	3535	15.71	15.71	9.42	9.42	2	0.10	0.01	0.04	0.00	0.00	24.0
7	12	-3406	68	230	0	199	3783	15.71	15.71	9.42	9.42	2	0.11	0.00	0.02	0.00	0.00	24.0
8	12	-2479	68	599	0	164	4354	15.71	15.71	9.42	9.42	2	0.12	0.01	0.04	0.00	0.00	24.0
9	12	-2159	126	282	0	224	4603	15.71	15.71	9.42	9.42	2	0.13	0.00	0.02	0.00	0.00	24.0
10	12	-5068	-37	375	0	131	2666	15.71	15.71	9.42	9.42	2	0.07	0.01	0.03	0.00	0.00	24.0
11	12	-4972	-20	280	0	149	2740	15.71	15.71	9.42	9.42	2	0.08	0.00	0.02	0.00	0.00	24.0
12	12	-912	155	549	0	215	5398	15.71	15.71	9.42	9.42	2	0.15	0.01	0.04	0.00	0.00	24.0
13	12	-816	173	454	0	232	5473	15.71	15.71	9.42	9.42	2	0.15	0.01	0.03	0.00	0.00	24.0
14	12	-3726	10	547	0	139	3535	15.71	15.71	9.42	9.42	2	0.10	0.01	0.04	0.00	0.00	24.0
15	12	-3406	68	230	0	199	3783	15.71	15.71	9.42	9.42	2	0.11	0.00	0.02	0.00	0.00	24.0
16	12	-2479	68	599	0	164	4354	15.71	15.71	9.42	9.42	2	0.12	0.01	0.04	0.00	0.00	24.0
17	12	-2159	126	282	0	224	4603	15.71	15.71	9.42	9.42	2	0.13	0.00	0.02	0.00	0.00	24.0
18	12	-8467	686	813	0	356	5202	15.71	15.71	9.42	9.42	3	0.10	0.01	0.06	0.00	0.00	24.0
19	12	10450	-25	1516	0	663	15908	15.71	15.71	9.42	9.42	3	0.33	0.02	0.11	0.00	0.00	24.0
20	12	486	336	812	0	519	9932	15.71	15.71	9.42	9.42	3	0.20	0.01	0.06	0.00	0.00	24.0
37	12	-16370	842	374	0	164	-86	15.71	15.71	9.42	9.42	3	0.01	0.01	0.06	0.00	0.00	24.0
38	12	15160	-342	1546	0	677	17758	15.71	15.71	9.42	9.42	3	0.38	0.02	0.11	0.00	0.00	24.0
39	12	-1444	260	372	0	436	7796	15.71	15.71	9.42	9.42	3	0.15	0.01	0.03	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-3695	88	539	0	169	5301	15.71	15.71	9.42	9.42	3	0.10	0.01	0.04	0.00	0.00	24.0
2	25	-4968	-37	375	0	84	2661	15.71	15.71	9.42	9.42	2	0.07	0.01	0.03	0.00	0.00	24.0
3	25	-4872	-20	280	0	114	2738	15.71	15.71	9.42	9.42	2	0.07	0.00	0.02	0.00	0.00	24.0
4	25	-812	155	549	0	146	5417	15.71	15.71	9.42	9.42	2	0.15	0.01	0.04	0.00	0.00	24.0
5	25	-716	173	454	0	176	5494	15.71	15.71	9.42	9.42	2	0.15	0.01	0.03	0.00	0.00	24.0
6	25	-3626	10	547	0	71	3537	15.71	15.71	9.42	9.42	2	0.10	0.01	0.04	0.00	0.00	24.0
7	25	-3306	68	230	0	170	3792	15.71	15.71	9.42	9.42	2	0.11	0.00	0.02	0.00	0.00	24.0
8	25	-2379	68	599	0	90	4363	15.71	15.71	9.42	9.42	2	0.12	0.01	0.04	0.00	0.00	24.0
9	25	-2059	126	282	0	189	4618	15.71	15.71	9.42	9.42	2	0.13	0.00	0.02	0.00	0.00	24.0
10	25	-4968	-37	375	0	84	2661	15.71	15.71	9.42	9.42	2	0.07	0.01	0.03	0.00	0.00	24.0
11	25	-4872	-20	280	0	114	2738	15.71	15.71	9.42	9.42	2	0.07	0.00	0.02	0.00	0.00	24.0
12	25	-812	155	549	0	146	5417	15.71	15.71	9.42	9.42	2	0.15	0.01	0.04	0.00	0.00	24.0
13	25	-716	173	454	0	176	5494	15.71	15.71	9.42	9.42	2	0.15	0.01	0.03	0.00	0.00	24.0
14	25	-3626	10	547	0	71	3537	15.71	15.71	9.42	9.42	2	0.10	0.01	0.04	0.00	0.00	24.0
15	25	-3306	68	230	0	170	3792	15.71	15.71	9.42	9.42	2	0.11	0.00	0.02	0.00	0.00	24.0
16	25	-2379	68	599	0	90	4363	15.71	15.71	9.42	9.42	2	0.12	0.01	0.04	0.00	0.00	24.0
17	25	-2059	126	282	0	189	4618	15.71	15.71	9.42	9.42	2	0.13	0.00	0.02	0.00	0.00	24.0
18	25	-8337	686	813	0	254	5288	15.71	15.71	9.42	9.42	3	0.10	0.01	0.06	0.00	0.00	24.0
19	25	10580	-25	1516	0	474	15905	15.71	15.71	9.42	9.42	3	0.33	0.02	0.11	0.00	0.00	24.0
20	25	616	336	812	0	417	9975	15.71	15.71	9.42	9.42	3	0.20	0.01	0.06	0.00	0.00	24.0
37	25	-16240	842	374	0	117	19	15.71	15.71	9.42	9.42	3	0.00	0.01	0.07	0.00	0.00	24.0
38	25	15290	-342	1546	0	483	17715	15.71	15.71	9.42	9.42	3	0.38	0.02	0.11	0.00	0.00	24.0
39	25	-1314	260	372	0	389	7829	15.71	15.71	9.42	9.42	3	0.15	0.01	0.03	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-3565	88	539	0	101	5312	15.71	15.71	9.42	9.42	3	0.10	0.01	0.04	0.00	0.00	24.0
2	38	-4868	-37	375	0	37	2657	15.71	15.71	9.42	9.42	2	0.07	0.01	0.03	0.00	0.00	24.0
3	38	-4772	-20	280	0	79	2736	15.71	15.71	9.42	9.42	2	0.07	0.00	0.02	0.00	0.00	24.0
4	38	-712	155	549	0	77	5437	15.71	15.71	9.42	9.42	2	0.15	0.01	0.04	0.00	0.00	24.0
5	38	-616	173	454	0	119	5516	15.71	15.71	9.42	9.42	2	0.15	0.01	0.03	0.00	0.00	24.0
6	38	-3526	10	547	0	3	3538	15.71	15.71	9.42	9.42	2	0.09	0.01	0.04	0.00	0.00	24.0
7	38	-3206	68	230	0	141	3801	15.71	15.71	9.42	9.42	2	0.10	0.00	0.02	0.00	0.00	24.0
8	38	-2279	68	599	0	15	4372	15.71	15.71	9.42	9.42	2	0.12	0.01	0.04	0.00	0.00	24.0
9	38	-1959	126	282	0	153	4634	15.71	15.71	9.42	9.42	2	0.13	0.00	0.02	0.00	0.00	24.0
10	38	-4868	-37	375	0	37	2657	15.71	15.71	9.42	9.42	2	0.07	0.01	0.03	0.00	0.00	24.0
11	38	-4772	-20	280	0	79	2736	15.71	15.71	9.42	9.42	2	0.07	0.00	0.02	0.00	0.00	24.0
12	38	-712	155	549	0	77	5437	15.71	15.71	9.42	9.42	2	0.15	0.01	0.04	0.00	0.00	24.0
13	38	-616	173	454	0	119	5516	15.71	15.71	9.42	9.42	2	0.15	0.01	0.03	0.00	0.00	24.0
14	38	-3526	10	547	0	3	3538	15.71	15.71	9.42	9.42	2	0.09	0.01	0.04	0.00	0.00	24.0
15	38	-3206	68	230	0	141	3801	15.71	15.71	9.42	9.42	2	0.10	0.00	0.02	0.00	0.00	24.0
16	38	-2279	68	599	0	15	4372	15.71	15.71	9.42	9.42	2	0.12	0.01	0.04	0.00	0.00	24.0
17	38	-1959	126	282	0	153	4634	15.71	15.71	9.42	9.42	2	0.13	0.00	0.02	0.00	0.00	24.0
18	38	-8207	686	813	0	152	5373	15.71	15.71	9.42	9.42	3	0.10	0.01	0.06	0.00	0.00	24.0
19	38	10710	-25	1516	0	284	15902	15.71	15.71	9.42	9.42	3	0.33	0.02	0.11	0.00	0.00	24.0
20	38	746	336	812	0	316	10017	15.71	15.71	9.42	9.42	3	0.20	0.01	0.06	0.00	0.00	24.0
37	38	-16110	842	374	0	70	125	15.71	15.71	9.42	9.42	3	0.00	0.01	0.07	0.00	0.00	24.0
38	38	15420	-342	1546	0	290	17672	15.71	15.71	9.42	9.42	3	0.37	0.02	0.11	0.00	0.00	24.0
39	38	-1184	260	372	0	342	7862	15.71	15.71	9.42	9.42	3	0.15	0.01	0.03	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-3435	88	539	0	34	5323	15.71	15.71	9.42	9.42	3	0.10	0.01	0.04	0.00	0.00	24.0
2	50	-4768	-37	375	0	-10	2652	15.71	15.71	9.42	9.42	2	0.07	0.01	0.03	0.00	0.00	24.0
3	50	-4672	-20	280	0	44	2733	15.71	15.71	9.42	9.42	2	0.07	0.00	0.02	0.00	0.00	24.0
4	50	-612	155	549	0	9	5456	15.71	15.71	9.42	9.42	2	0.15	0.01	0.04	0.00	0.00	24.0
5	50	-516	173	454	0	62	5537	15.71	15.71	9.42	9.42	2	0.15	0.01	0.03	0.00	0.00	24.0
6	50	-3426	10	547	0	-66	3539	15.71	15.71	9.42	9.42	2	0.10	0.01	0.04	0.00	0.00	24.0
7	50	-3106	68	230	0	112	3809	15.71	15.71	9.42	9.42	2	0.10	0.00	0.02	0.00	0.00	24.0
8	50	-2179	68	599	0	-60	4380	15.71	15.71	9.42	9.42	2	0.12	0.01	0.04	0.00	0.00	24.0
9	50	-1859	126	282	0	118	4650	15.71	15.71	9.42	9.42	2	0.13	0.00	0.02	0.00	0.00	24.0
10	50	-4768	-37	375	0	-10	2652	15.71	15.71	9.42	9.42	2	0.07	0.01	0.03	0.00	0.00	24.0

11	50	-4672	-20	280	0	44	2733	15.71	15.71	9.42	9.42	2	0.07	0.00	0.02	0.00	0.00	24.0
12	50	-612	155	549	0	9	5456	15.71	15.71	9.42	9.42	2	0.15	0.01	0.04	0.00	0.00	24.0
13	50	-516	173	454	0	62	5537	15.71	15.71	9.42	9.42	2	0.15	0.01	0.03	0.00	0.00	24.0
14	50	-3426	10	547	0	-66	3539	15.71	15.71	9.42	9.42	2	0.10	0.01	0.04	0.00	0.00	24.0
15	50	-3106	68	230	0	112	3809	15.71	15.71	9.42	9.42	2	0.10	0.00	0.02	0.00	0.00	24.0
16	50	-2179	68	599	0	-60	4380	15.71	15.71	9.42	9.42	2	0.12	0.01	0.04	0.00	0.00	24.0
17	50	-1859	126	282	0	118	4650	15.71	15.71	9.42	9.42	2	0.13	0.00	0.02	0.00	0.00	24.0
18	50	-8077	686	813	0	51	5459	15.71	15.71	9.42	9.42	3	0.10	0.01	0.06	0.00	0.00	24.0
19	50	10840	-25	1516	0	95	15900	15.71	15.71	9.42	9.42	3	0.33	0.02	0.11	0.00	0.00	24.0
20	50	876	336	812	0	214	10060	15.71	15.71	9.42	9.42	3	0.20	0.01	0.06	0.00	0.00	24.0
37	50	-15980	842	374	0	23	230	15.71	15.71	9.42	9.42	3	0.00	0.01	0.07	0.00	0.00	24.0
38	50	15550	-342	1546	0	97	17630	15.71	15.71	9.42	9.42	3	0.37	0.02	0.11	0.00	0.00	24.0
39	50	-1054	260	372	0	296	7894	15.71	15.71	9.42	9.42	3	0.15	0.01	0.03	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 72 NI 1663 NF 1664 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 31
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-6035	-401	-1747	0	-941	-2303	15.71	15.71	9.42	9.42	3	0.06	0.02	0.12	0.00	0.00	24.0
2	0	-3934	-305	-1515	0	-843	-2150	15.71	15.71	9.42	9.42	2	0.08	0.02	0.10	0.00	0.00	24.0
3	0	-4032	-283	-1605	0	-835	-2087	15.71	15.71	9.42	9.42	2	0.08	0.02	0.11	0.00	0.00	24.0
4	0	-5252	-334	-1082	0	-613	-1456	15.71	15.71	9.42	9.42	2	0.06	0.01	0.07	0.00	0.00	24.0
5	0	-5351	-312	-1172	0	-605	-1394	15.71	15.71	9.42	9.42	2	0.05	0.02	0.08	0.00	0.00	24.0
6	0	-4281	-342	-1259	0	-771	-1980	15.71	15.71	9.42	9.42	2	0.08	0.02	0.09	0.00	0.00	24.0
7	0	-4608	-267	-1558	0	-745	-1771	15.71	15.71	9.42	9.42	2	0.07	0.02	0.11	0.00	0.00	24.0
8	0	-4676	-350	-1129	0	-702	-1772	15.71	15.71	9.42	9.42	2	0.07	0.02	0.08	0.00	0.00	24.0
9	0	-5004	-276	-1428	0	-676	-1563	15.71	15.71	9.42	9.42	2	0.06	0.02	0.10	0.00	0.00	24.0
10	0	-3934	-305	-1515	0	-843	-2150	15.71	15.71	9.42	9.42	2	0.08	0.02	0.10	0.00	0.00	24.0
11	0	-4032	-283	-1605	0	-835	-2087	15.71	15.71	9.42	9.42	2	0.08	0.02	0.11	0.00	0.00	24.0
12	0	-5252	-334	-1082	0	-613	-1456	15.71	15.71	9.42	9.42	2	0.06	0.01	0.07	0.00	0.00	24.0
13	0	-5351	-312	-1172	0	-605	-1394	15.71	15.71	9.42	9.42	2	0.05	0.02	0.08	0.00	0.00	24.0
14	0	-4281	-342	-1259	0	-771	-1980	15.71	15.71	9.42	9.42	2	0.08	0.02	0.09	0.00	0.00	24.0
15	0	-4608	-267	-1558	0	-745	-1771	15.71	15.71	9.42	9.42	2	0.07	0.02	0.11	0.00	0.00	24.0
16	0	-4676	-350	-1129	0	-702	-1772	15.71	15.71	9.42	9.42	2	0.07	0.02	0.08	0.00	0.00	24.0
17	0	-5004	-276	-1428	0	-676	-1563	15.71	15.71	9.42	9.42	2	0.06	0.02	0.10	0.00	0.00	24.0
18	0	1859	-428	-4237	0	-2310	-7597	15.71	15.71	9.42	9.42	3	0.18	0.06	0.30	0.00	0.00	24.0
19	0	-7023	-978	-2334	0	-1281	-3457	15.71	15.71	9.42	9.42	3	0.08	0.03	0.16	0.00	0.00	24.0
20	0	-3315	-610	-3365	0	-1672	-4960	15.71	15.71	9.42	9.42	3	0.12	0.05	0.23	0.00	0.00	24.0
37	0	3667	-145	-4370	0	-2373	-7919	15.71	15.71	9.42	9.42	3	0.19	0.06	0.31	0.00	0.00	24.0
38	0	-11140	-1062	-1199	0	-659	-1019	15.71	15.71	9.42	9.42	3	0.03	0.02	0.09	0.00	0.00	24.0
39	0	-4957	-448	-2916	0	-1310	-3524	15.71	15.71	9.42	9.42	3	0.08	0.04	0.20	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-5905	-401	-1747	0	-723	-2353	15.71	15.71	9.42	9.42	3	0.05	0.02	0.12	0.00	0.00	24.0
2	12	-3834	-305	-1515	0	-653	-2188	15.71	15.71	9.42	9.42	2	0.08	0.02	0.10	0.00	0.00	24.0
3	12	-3932	-283	-1605	0	-634	-2122	15.71	15.71	9.42	9.42	2	0.07	0.02	0.11	0.00	0.00	24.0
4	12	-5152	-334	-1082	0	-478	-1498	15.71	15.71	9.42	9.42	2	0.05	0.01	0.07	0.00	0.00	24.0
5	12	-5251	-312	-1172	0	-458	-1433	15.71	15.71	9.42	9.42	2	0.05	0.02	0.08	0.00	0.00	24.0
6	12	-4181	-342	-1259	0	-614	-2023	15.71	15.71	9.42	9.42	2	0.07	0.02	0.09	0.00	0.00	24.0
7	12	-4508	-267	-1558	0	-550	-1804	15.71	15.71	9.42	9.42	2	0.06	0.02	0.11	0.00	0.00	24.0
8	12	-4576	-350	-1129	0	-561	-1816	15.71	15.71	9.42	9.42	2	0.06	0.02	0.08	0.00	0.00	24.0
9	12	-4904	-276	-1428	0	-498	-1598	15.71	15.71	9.42	9.42	2	0.06	0.02	0.10	0.00	0.00	24.0
10	12	-3834	-305	-1515	0	-653	-2188	15.71	15.71	9.42	9.42	2	0.08	0.02	0.10	0.00	0.00	24.0
11	12	-3932	-283	-1605	0	-634	-2122	15.71	15.71	9.42	9.42	2	0.07	0.02	0.11	0.00	0.00	24.0
12	12	-5152	-334	-1082	0	-478	-1498	15.71	15.71	9.42	9.42	2	0.05	0.01	0.07	0.00	0.00	24.0
13	12	-5251	-312	-1172	0	-458	-1433	15.71	15.71	9.42	9.42	2	0.05	0.02	0.08	0.00	0.00	24.0
14	12	-4181	-342	-1259	0	-614	-2023	15.71	15.71	9.42	9.42	2	0.07	0.02	0.09	0.00	0.00	24.0
15	12	-4508	-267	-1558	0	-550	-1804	15.71	15.71	9.42	9.42	2	0.06	0.02	0.11	0.00	0.00	24.0
16	12	-4576	-350	-1129	0	-561	-1816	15.71	15.71	9.42	9.42	2	0.06	0.02	0.08	0.00	0.00	24.0
17	12	-4904	-276	-1428	0	-498	-1598	15.71	15.71	9.42	9.42	2	0.06	0.02	0.10	0.00	0.00	24.0
18	12	1989	-428	-4237	0	-1780	-7651	15.71	15.71	9.42	9.42	3	0.17	0.06	0.30	0.00	0.00	24.0
19	12	-6893	-978	-2334	0	-989	-3579	15.71	15.71	9.42	9.42	3	0.08	0.03	0.16	0.00	0.00	24.0
20	12	-3185	-610	-3365	0	-1251	-5036	15.71	15.71	9.42	9.42	3	0.11	0.05	0.23	0.00	0.00	24.0
37	12	3797	-145	-4370	0	-1827	-7937	15.71	15.71	9.42	9.42	3	0.18	0.06	0.31	0.00	0.00	24.0
38	12	-11010	-1062	-1199	0	-509	-1152	15.71	15.71	9.42	9.42	3	0.03	0.02	0.09	0.00	0.00	24.0
39	12	-4827	-448	-2916	0	-945	-3580	15.71	15.71	9.42	9.42	3	0.08	0.04	0.20	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-5775	-401	-1747	0	-504	-2403	15.71	15.71	9.42	9.42	3	0.05	0.02	0.12	0.00	0.00	24.0
2	25	-3734	-305	-1515	0	-464	-2226	15.71	15.71	9.42	9.42	2	0.07	0.02	0.10	0.00	0.00	24.0
3	25	-3832	-283	-1605	0	-433	-2157	15.71	15.71	9.42	9.42	2	0.07	0.02	0.11	0.00	0.00	24.0
4	25	-5052	-334	-1082	0	-342	-1540	15.71	15.71	9.42	9.42	2	0.05	0.01	0.07	0.00	0.00	24.0
5	25	-5151	-312	-1172	0	-312	-1472	15.71	15.71	9.42	9.42	2	0.05	0.02	0.08	0.00	0.00	24.0
6	25	-4081	-342	-1259	0	-457	-2066	15.71	15.71	9.42	9.42	2	0.07	0.02	0.09	0.00	0.00	24.0
7	25	-4408	-267	-1558	0	-355	-1838	15.71	15.71	9.42	9.42	2	0.06	0.02	0.11	0.00	0.00	24.0
8	25	-4476	-350	-1129	0	-420	-1860	15.71	15.71	9.42	9.42	2	0.06	0.02	0.08	0.00	0.00	24.0
9	25	-4804	-276	-1428	0	-319	-1632	15.71	15.71	9.42	9.42	2	0.05	0.02	0.10	0.00	0.00	24.0
10	25	-3734	-305	-1515	0	-464	-2226	15.71	15.71	9.42	9.42	2	0.07	0.02	0.10	0.00	0.00	24.0
11	25	-3832	-283	-1605	0	-433	-2157	15.71	15.71	9.42	9.42	2	0.07	0.02	0.11	0.00	0.00	24.0
12	25	-5052	-334	-1082	0	-342	-1540	15.71	15.71	9.42	9.42	2	0.05	0.01	0.07	0.00	0.00	24.0
13	25	-5151	-312	-1172	0	-312	-1472	15.71	15.71	9.42	9.42	2	0.05	0.02	0.08	0.00	0.00	24.0
14	25	-4081	-342	-1259	0	-457	-2066	15.71	15.71	9.42	9.42	2	0.07	0.02	0.09	0.00	0.00	24.0
15	25	-4408	-267	-1558	0	-355	-1838	15.71	15.71	9.42	9.42	2	0.06	0.02	0.11	0.00	0.00	24.0
16	25	-4476	-350	-1129	0	-420	-1860	15.71	15.71	9.42	9.42	2	0.06	0.02	0.08	0.00	0.00	24.0
17	25	-4804	-276	-1428	0	-319	-1632	15.71	15.71	9.42	9.42	2	0.05	0.02	0.10	0.00	0.00	24.0
18	25	2119	-428	-4237	0	-1251	-7704	15.71	15.71	9.42	9.42	3	0.16	0.06	0.30	0.00	0.00	24.0
19	25	-6763	-978	-2334	0	-697	-3702	15.71	15.71	9.42	9.42	3	0.08	0.03	0.16	0.00	0.00	24.0
20	25	-3055	-610	-3365	0	-831	-5113	15.71	15.71	9.42	9.42	3	0.10	0.05	0.23	0.00	0.00	24.0
37	25	3927	-145	-4370	0	-1281	-7955	15.71	15.71	9.42	9.42	3	0.17	0.06	0.31	0.00	0.00	24.0
38	25	-10880	-1062	-1199	0	-359	-1285	15.71	15.71	9.42	9.42	3	0.03	0.02	0.09	0.00	0.00	24.0
39	25	-4697	-448	-2916	0	-581	-3636	15.71	15.71	9.42	9.42	3	0.07	0.04	0.20	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-5645	-401	-1747	0	-286	-2454	15.71	15.71	9.42	9.42	3	0.05	0.02	0.12	0.00	0.00	24.0
2	38	-3634	-305	-1515	0	-274	-2264	15.71	15.71	9.42	9.42	2	0.07	0.02	0.10	0.00	0.00	24.0
3	38	-3732	-283	-1605	0	-233	-2193	15.71	15.71	9.42	9.42	2	0.06	0.02	0.11	0.00	0.00	24.0
4	38	-4952	-334	-1082	0	-207	-1582	15.71	15.71	9.42	9.42	2	0.05	0.01	0.07	0.00	0.00	24.0
5	38	-5051	-312	-1172	0	-165	-1511	15.71	15.71	9.42	9.42	2	0.04	0.02	0.08	0.00	0.00	24.0
6	38	-3981	-342	-1259	0	-299	-2108	15.71	15.71	9.42	9.42	2	0.06	0.02	0.09	0.00	0.00	24.0

7	38	-4308	-267	-1558	0	-161	-1871	15.71	15.71	9.42	9.42	2	0.05	0.02	0.11	0.00	0.00	24.0
8	38	-4376	-350	-1129	0	-279	-1904	15.71	15.71	9.42	9.42	2	0.06	0.02	0.08	0.00	0.00	24.0
9	38	-4704	-276	-1428	0	-140	-1666	15.71	15.71	9.42	9.42	2	0.05	0.02	0.10	0.00	0.00	24.0
10	38	-3634	-305	-1515	0	-274	-2264	15.71	15.71	9.42	9.42	2	0.07	0.02	0.10	0.00	0.00	24.0
11	38	-3732	-283	-1605	0	-233	-2193	15.71	15.71	9.42	9.42	2	0.06	0.02	0.11	0.00	0.00	24.0
12	38	-4952	-334	-1082	0	-207	-1582	15.71	15.71	9.42	9.42	2	0.05	0.01	0.07	0.00	0.00	24.0
13	38	-5051	-312	-1172	0	-165	-1511	15.71	15.71	9.42	9.42	2	0.04	0.02	0.08	0.00	0.00	24.0
14	38	-3981	-342	-1259	0	-299	-2108	15.71	15.71	9.42	9.42	2	0.06	0.02	0.09	0.00	0.00	24.0
15	38	-4308	-267	-1558	0	-161	-1871	15.71	15.71	9.42	9.42	2	0.05	0.02	0.11	0.00	0.00	24.0
16	38	-4376	-350	-1129	0	-279	-1904	15.71	15.71	9.42	9.42	2	0.06	0.02	0.08	0.00	0.00	24.0
17	38	-4704	-276	-1428	0	-140	-1666	15.71	15.71	9.42	9.42	2	0.05	0.02	0.10	0.00	0.00	24.0
18	38	2249	-428	-4237	0	-721	-7757	15.71	15.71	9.42	9.42	3	0.16	0.06	0.30	0.00	0.00	24.0
19	38	-6633	-978	-2334	0	-406	-3824	15.71	15.71	9.42	9.42	3	0.07	0.03	0.16	0.00	0.00	24.0
20	38	-2925	-610	-3365	0	-410	-5189	15.71	15.71	9.42	9.42	3	0.10	0.05	0.23	0.00	0.00	24.0
37	38	4057	-145	-4370	0	-735	-7973	15.71	15.71	9.42	9.42	3	0.16	0.06	0.31	0.00	0.00	24.0
38	38	-10750	-1062	-1199	0	-209	-1417	15.71	15.71	9.42	9.42	3	0.03	0.02	0.09	0.00	0.00	24.0
39	38	-4567	-448	-2916	0	-216	-3692	15.71	15.71	9.42	9.42	3	0.07	0.04	0.20	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-5515	-401	-1747	0	-67	-2504	15.71	15.71	9.42	9.42	3	0.05	0.02	0.12	0.00	0.00	24.0
2	50	-3534	-305	-1515	0	-85	-2302	15.71	15.71	9.42	9.42	2	0.06	0.02	0.10	0.00	0.00	24.0
3	50	-3632	-283	-1605	0	-32	-2228	15.71	15.71	9.42	9.42	2	0.06	0.02	0.11	0.00	0.00	24.0
4	50	-4852	-334	-1082	0	-72	-1624	15.71	15.71	9.42	9.42	2	0.04	0.01	0.07	0.00	0.00	24.0
5	50	-4951	-312	-1172	0	-19	-1550	15.71	15.71	9.42	9.42	2	0.04	0.02	0.08	0.00	0.00	24.0
6	50	-3881	-342	-1259	0	-142	-2151	15.71	15.71	9.42	9.42	2	0.06	0.02	0.09	0.00	0.00	24.0
7	50	-4208	-267	-1558	0	34	-1905	15.71	15.71	9.42	9.42	2	0.05	0.02	0.11	0.00	0.00	24.0
8	50	-4276	-350	-1129	0	-138	-1948	15.71	15.71	9.42	9.42	2	0.06	0.02	0.08	0.00	0.00	24.0
9	50	-4604	-276	-1428	0	38	-1701	15.71	15.71	9.42	9.42	2	0.05	0.02	0.10	0.00	0.00	24.0
10	50	-3534	-305	-1515	0	-85	-2302	15.71	15.71	9.42	9.42	2	0.06	0.02	0.10	0.00	0.00	24.0
11	50	-3632	-283	-1605	0	-32	-2228	15.71	15.71	9.42	9.42	2	0.06	0.02	0.11	0.00	0.00	24.0
12	50	-4852	-334	-1082	0	-72	-1624	15.71	15.71	9.42	9.42	2	0.04	0.01	0.07	0.00	0.00	24.0
13	50	-4951	-312	-1172	0	-19	-1550	15.71	15.71	9.42	9.42	2	0.04	0.02	0.08	0.00	0.00	24.0
14	50	-3881	-342	-1259	0	-142	-2151	15.71	15.71	9.42	9.42	2	0.06	0.02	0.09	0.00	0.00	24.0
15	50	-4208	-267	-1558	0	34	-1905	15.71	15.71	9.42	9.42	2	0.05	0.02	0.11	0.00	0.00	24.0
16	50	-4276	-350	-1129	0	-138	-1948	15.71	15.71	9.42	9.42	2	0.06	0.02	0.08	0.00	0.00	24.0
17	50	-4604	-276	-1428	0	38	-1701	15.71	15.71	9.42	9.42	2	0.05	0.02	0.10	0.00	0.00	24.0
18	50	2379	-428	-4237	0	-191	-7811	15.71	15.71	9.42	9.42	3	0.15	0.06	0.30	0.00	0.00	24.0
19	50	-6503	-978	-2334	0	-114	-3946	15.71	15.71	9.42	9.42	3	0.07	0.03	0.16	0.00	0.00	24.0
20	50	-2795	-610	-3365	0	11	-5265	15.71	15.71	9.42	9.42	3	0.10	0.05	0.23	0.00	0.00	24.0
37	50	4187	-145	-4370	0	-188	-7991	15.71	15.71	9.42	9.42	3	0.16	0.06	0.31	0.00	0.00	24.0
38	50	-10620	-1062	-1199	0	-60	-1550	15.71	15.71	9.42	9.42	3	0.03	0.02	0.09	0.00	0.00	24.0
39	50	-4437	-448	-2916	0	148	-3748	15.71	15.71	9.42	9.42	3	0.07	0.04	0.20	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 73 NI 1664 NF 48 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 31A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-10540	-852	-61	0	-67	-3398	15.71	15.71	9.42	9.42	3	0.06	0.01	0.07	0.00	0.00	24.0
2	0	-7533	-741	82	0	-85	-3011	15.71	15.71	9.42	9.42	2	0.08	0.01	0.06	0.00	0.00	24.0
3	0	-7609	-715	-221	0	-32	-2934	15.71	15.71	9.42	9.42	2	0.08	0.01	0.06	0.00	0.00	24.0
4	0	-8610	-596	128	0	-72	-2294	15.71	15.71	9.42	9.42	2	0.06	0.01	0.05	0.00	0.00	24.0
5	0	-8685	-571	-175	0	-19	-2217	15.71	15.71	9.42	9.42	2	0.06	0.01	0.05	0.00	0.00	24.0
6	0	-7822	-720	451	0	-142	-2850	15.71	15.71	9.42	9.42	2	0.08	0.01	0.06	0.00	0.00	24.0
7	0	-8074	-635	-558	0	34	-2593	15.71	15.71	9.42	9.42	2	0.07	0.01	0.05	0.00	0.00	24.0
8	0	-8145	-676	464	0	-138	-2635	15.71	15.71	9.42	9.42	2	0.07	0.01	0.06	0.00	0.00	24.0
9	0	-8397	-592	-544	0	38	-2378	15.71	15.71	9.42	9.42	2	0.06	0.01	0.05	0.00	0.00	24.0
10	0	-7533	-741	82	0	-85	-3011	15.71	15.71	9.42	9.42	2	0.08	0.01	0.06	0.00	0.00	24.0
11	0	-7609	-715	-221	0	-32	-2934	15.71	15.71	9.42	9.42	2	0.08	0.01	0.06	0.00	0.00	24.0
12	0	-8610	-596	128	0	-72	-2294	15.71	15.71	9.42	9.42	2	0.06	0.01	0.05	0.00	0.00	24.0
13	0	-8685	-571	-175	0	-19	-2217	15.71	15.71	9.42	9.42	2	0.06	0.01	0.05	0.00	0.00	24.0
14	0	-7822	-720	451	0	-142	-2850	15.71	15.71	9.42	9.42	2	0.08	0.01	0.06	0.00	0.00	24.0
15	0	-8074	-635	-558	0	34	-2593	15.71	15.71	9.42	9.42	2	0.07	0.01	0.05	0.00	0.00	24.0
16	0	-8145	-676	464	0	-138	-2635	15.71	15.71	9.42	9.42	2	0.07	0.01	0.06	0.00	0.00	24.0
17	0	-8397	-592	-544	0	38	-2378	15.71	15.71	9.42	9.42	2	0.06	0.01	0.05	0.00	0.00	24.0
18	0	-5392	-1825	53	0	-191	-9083	15.71	15.71	9.42	9.42	3	0.17	0.02	0.16	0.00	0.00	24.0
19	0	-13180	-1822	5	0	-114	-5215	15.71	15.71	9.42	9.42	3	0.10	0.02	0.15	0.00	0.00	24.0
20	0	-9738	-1666	-969	0	11	-6497	15.71	15.71	9.42	9.42	3	0.12	0.02	0.14	0.00	0.00	24.0
37	0	-3236	-1508	36	0	-188	-9143	15.71	15.71	9.42	9.42	3	0.17	0.02	0.14	0.00	0.00	24.0
38	0	-16220	-1502	-44	0	-60	-2696	15.71	15.71	9.42	9.42	3	0.05	0.02	0.12	0.00	0.00	24.0
39	0	-10480	-1243	-1668	0	148	-4833	15.71	15.71	9.42	9.42	3	0.09	0.02	0.11	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-10410	-852	-61	0	-60	-3504	15.71	15.71	9.42	9.42	3	0.06	0.01	0.07	0.00	0.00	24.0
2	12	-7433	-741	82	0	-95	-3104	15.71	15.71	9.42	9.42	2	0.08	0.01	0.06	0.00	0.00	24.0
3	12	-7509	-715	-221	0	-4	-3023	15.71	15.71	9.42	9.42	2	0.08	0.01	0.06	0.00	0.00	24.0
4	12	-8510	-596	128	0	-88	-2368	15.71	15.71	9.42	9.42	2	0.06	0.01	0.05	0.00	0.00	24.0
5	12	-8585	-571	-175	0	3	-2288	15.71	15.71	9.42	9.42	2	0.06	0.01	0.05	0.00	0.00	24.0
6	12	-7722	-720	451	0	-198	-2940	15.71	15.71	9.42	9.42	2	0.08	0.01	0.06	0.00	0.00	24.0
7	12	-7974	-635	-558	0	104	-2673	15.71	15.71	9.42	9.42	2	0.07	0.01	0.05	0.00	0.00	24.0
8	12	-8045	-676	464	0	-196	-2720	15.71	15.71	9.42	9.42	2	0.07	0.01	0.06	0.00	0.00	24.0
9	12	-8297	-592	-544	0	106	-2452	15.71	15.71	9.42	9.42	2	0.07	0.01	0.05	0.00	0.00	24.0
10	12	-7433	-741	82	0	-95	-3104	15.71	15.71	9.42	9.42	2	0.08	0.01	0.06	0.00	0.00	24.0
11	12	-7509	-715	-221	0	-4	-3023	15.71	15.71	9.42	9.42	2	0.08	0.01	0.06	0.00	0.00	24.0
12	12	-8510	-596	128	0	-88	-2368	15.71	15.71	9.42	9.42	2	0.06	0.01	0.05	0.00	0.00	24.0
13	12	-8585	-571	-175	0	3	-2288	15.71	15.71	9.42	9.42	2	0.06	0.01	0.05	0.00	0.00	24.0
14	12	-7722	-720	451	0	-198	-2940	15.71	15.71	9.42	9.42	2	0.08	0.01	0.06	0.00	0.00	24.0
15	12	-7974	-635	-558	0	104	-2673	15.71	15.71	9.42	9.42	2	0.07	0.01	0.05	0.00	0.00	24.0
16	12	-8045	-676	464	0	-196	-2720	15.71	15.71	9.42	9.42	2	0.07	0.01	0.06	0.00	0.00	24.0
17	12	-8297	-592	-544	0	106	-2452	15.71	15.71	9.42	9.42	2	0.07	0.01	0.05	0.00	0.00	24.0
18	12	-5262	-1825	53	0	-198	-9311	15.71	15.71	9.42	9.42	3	0.18	0.02	0.16	0.00	0.00	24.0
19	12	-13050	-1822	5	0	-114	-5443	15.71	15.71	9.42	9.42	3	0.10	0.02	0.15	0.00	0.00	24.0
20	12	-9608	-1666	-969	0	132	-6705	15.71	15.71	9.42	9.42	3	0.12	0.02	0.14	0.00	0.00	24.0
37	12	-3106	-1508	36	0	-193	-9332	15.71	15.71	9.42	9.42	3	0.18	0.02	0.14	0.00	0.00	24.0
38	12	-16090	-1502	-44	0	-54	-2884	15.71	15.71	9.42	9.42	3	0.05	0.02	0.12	0.00	0.00	24.0
39	12	-10350	-1243	-1668	0	356	-4988	15.71	15.71	9.42	9.42	3	0.09	0.02	0.11	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-10280	-852	-61	0	-52	-3611	15.71	15.71	9.42	9.42	3	0.07	0.01	0.07	0.00	0.00	24.0
2	25	-7333	-741	82	0	-105	-3196	15.71	15.71	9.42	9.42	2	0.09	0.01	0.06	0.00	0.00	24.0

3	25	-7409	-715	-221	0	23	-3112	15.71	15.71	9.42	9.42	2	0.08	0.01	0.06	0.00	0.00	24.0
4	25	-8410	-596	128	0	-104	-2443	15.71	15.71	9.42	9.42	2	0.07	0.01	0.05	0.00	0.00	24.0
5	25	-8485	-571	-175	0	25	-2360	15.71	15.71	9.42	9.42	2	0.06	0.01	0.05	0.00	0.00	24.0
6	25	-7622	-720	451	0	-254	-3030	15.71	15.71	9.42	9.42	2	0.08	0.01	0.06	0.00	0.00	24.0
7	25	-7874	-635	-558	0	174	-2752	15.71	15.71	9.42	9.42	2	0.08	0.01	0.05	0.00	0.00	24.0
8	25	-7945	-676	464	0	-254	-2804	15.71	15.71	9.42	9.42	2	0.08	0.01	0.06	0.00	0.00	24.0
9	25	-8197	-592	-544	0	174	-2526	15.71	15.71	9.42	9.42	2	0.07	0.01	0.05	0.00	0.00	24.0
10	25	-7333	-741	82	0	-105	-3196	15.71	15.71	9.42	9.42	2	0.09	0.01	0.06	0.00	0.00	24.0
11	25	-7409	-715	-221	0	23	-3112	15.71	15.71	9.42	9.42	2	0.08	0.01	0.06	0.00	0.00	24.0
12	25	-8410	-596	128	0	-104	-2443	15.71	15.71	9.42	9.42	2	0.07	0.01	0.05	0.00	0.00	24.0
13	25	-8485	-571	-175	0	25	-2360	15.71	15.71	9.42	9.42	2	0.06	0.01	0.05	0.00	0.00	24.0
14	25	-7622	-720	451	0	-254	-3030	15.71	15.71	9.42	9.42	2	0.08	0.01	0.06	0.00	0.00	24.0
15	25	-7874	-635	-558	0	174	-2752	15.71	15.71	9.42	9.42	2	0.08	0.01	0.05	0.00	0.00	24.0
16	25	-7945	-676	464	0	-254	-2804	15.71	15.71	9.42	9.42	2	0.08	0.01	0.06	0.00	0.00	24.0
17	25	-8197	-592	-544	0	174	-2526	15.71	15.71	9.42	9.42	2	0.07	0.01	0.05	0.00	0.00	24.0
18	25	-5132	-1825	53	0	-204	-9540	15.71	15.71	9.42	9.42	3	0.18	0.02	0.16	0.00	0.00	24.0
19	25	-12920	-1822	5	0	-115	-5671	15.71	15.71	9.42	9.42	3	0.10	0.02	0.15	0.00	0.00	24.0
20	25	-9478	-1666	-969	0	253	-6914	15.71	15.71	9.42	9.42	3	0.13	0.02	0.14	0.00	0.00	24.0
37	25	-2976	-1508	36	0	-197	-9520	15.71	15.71	9.42	9.42	3	0.18	0.02	0.14	0.00	0.00	24.0
38	25	-15960	-1502	-44	0	-48	-3072	15.71	15.71	9.42	9.42	3	0.06	0.02	0.12	0.00	0.00	24.0
39	25	-10220	-1243	-1668	0	565	-5144	15.71	15.71	9.42	9.42	3	0.10	0.02	0.11	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-10150	-852	-61	0	-45	-3717	15.71	15.71	9.42	9.42	3	0.07	0.01	0.07	0.00	0.00	24.0
2	38	-7233	-741	82	0	-115	-3288	15.71	15.71	9.42	9.42	2	0.09	0.01	0.06	0.00	0.00	24.0
3	38	-7309	-715	-221	0	51	-3202	15.71	15.71	9.42	9.42	2	0.08	0.01	0.06	0.00	0.00	24.0
4	38	-8310	-596	128	0	-120	-2517	15.71	15.71	9.42	9.42	2	0.07	0.01	0.05	0.00	0.00	24.0
5	38	-8385	-571	-175	0	47	-2431	15.71	15.71	9.42	9.42	2	0.06	0.01	0.05	0.00	0.00	24.0
6	38	-7522	-720	451	0	-311	-3119	15.71	15.71	9.42	9.42	2	0.09	0.01	0.06	0.00	0.00	24.0
7	38	-7774	-635	-558	0	243	-2832	15.71	15.71	9.42	9.42	2	0.08	0.01	0.05	0.00	0.00	24.0
8	38	-7845	-676	464	0	-312	-2889	15.71	15.71	9.42	9.42	2	0.08	0.01	0.06	0.00	0.00	24.0
9	38	-8097	-592	-544	0	242	-2600	15.71	15.71	9.42	9.42	2	0.07	0.01	0.05	0.00	0.00	24.0
10	38	-7233	-741	82	0	-115	-3288	15.71	15.71	9.42	9.42	2	0.09	0.01	0.06	0.00	0.00	24.0
11	38	-7309	-715	-221	0	51	-3202	15.71	15.71	9.42	9.42	2	0.08	0.01	0.06	0.00	0.00	24.0
12	38	-8310	-596	128	0	-120	-2517	15.71	15.71	9.42	9.42	2	0.07	0.01	0.05	0.00	0.00	24.0
13	38	-8385	-571	-175	0	47	-2431	15.71	15.71	9.42	9.42	2	0.06	0.01	0.05	0.00	0.00	24.0
14	38	-7522	-720	451	0	-311	-3119	15.71	15.71	9.42	9.42	2	0.09	0.01	0.06	0.00	0.00	24.0
15	38	-7774	-635	-558	0	243	-2832	15.71	15.71	9.42	9.42	2	0.08	0.01	0.05	0.00	0.00	24.0
16	38	-7845	-676	464	0	-312	-2889	15.71	15.71	9.42	9.42	2	0.08	0.01	0.06	0.00	0.00	24.0
17	38	-8097	-592	-544	0	242	-2600	15.71	15.71	9.42	9.42	2	0.07	0.01	0.05	0.00	0.00	24.0
18	38	-5002	-1825	53	0	-211	-9768	15.71	15.71	9.42	9.42	3	0.18	0.02	0.16	0.00	0.00	24.0
19	38	-12790	-1822	5	0	-116	-5898	15.71	15.71	9.42	9.42	3	0.11	0.02	0.15	0.00	0.00	24.0
20	38	-9348	-1666	-969	0	374	-7122	15.71	15.71	9.42	9.42	3	0.13	0.02	0.14	0.00	0.00	24.0
37	38	-2846	-1508	36	0	-202	-9708	15.71	15.71	9.42	9.42	3	0.19	0.02	0.14	0.00	0.00	24.0
38	38	-15830	-1502	-44	0	-43	-3259	15.71	15.71	9.42	9.42	3	0.06	0.02	0.12	0.00	0.00	24.0
39	38	-10089	-1243	-1668	0	773	-5299	15.71	15.71	9.42	9.42	3	0.10	0.02	0.11	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-10020	-852	-61	0	-37	-3824	15.71	15.71	9.42	9.42	3	0.07	0.01	0.07	0.00	0.00	24.0
2	50	-7133	-741	82	0	-126	-3381	15.71	15.71	9.42	9.42	2	0.09	0.01	0.06	0.00	0.00	24.0
3	50	-7209	-715	-221	0	78	-3291	15.71	15.71	9.42	9.42	2	0.09	0.01	0.06	0.00	0.00	24.0
4	50	-8210	-596	128	0	-135	-2592	15.71	15.71	9.42	9.42	2	0.07	0.01	0.05	0.00	0.00	24.0
5	50	-8285	-571	-175	0	69	-2502	15.71	15.71	9.42	9.42	2	0.07	0.01	0.05	0.00	0.00	24.0
6	50	-7422	-720	451	0	-367	-3209	15.71	15.71	9.42	9.42	2	0.09	0.01	0.06	0.00	0.00	24.0
7	50	-7674	-635	-558	0	313	-2911	15.71	15.71	9.42	9.42	2	0.08	0.01	0.05	0.00	0.00	24.0
8	50	-7745	-676	464	0	-370	-2973	15.71	15.71	9.42	9.42	2	0.09	0.01	0.06	0.00	0.00	24.0
9	50	-7997	-592	-544	0	310	-2674	15.71	15.71	9.42	9.42	2	0.08	0.01	0.05	0.00	0.00	24.0
10	50	-7133	-741	82	0	-126	-3381	15.71	15.71	9.42	9.42	2	0.09	0.01	0.06	0.00	0.00	24.0
11	50	-7209	-715	-221	0	78	-3291	15.71	15.71	9.42	9.42	2	0.09	0.01	0.06	0.00	0.00	24.0
12	50	-8210	-596	128	0	-135	-2592	15.71	15.71	9.42	9.42	2	0.07	0.01	0.05	0.00	0.00	24.0
13	50	-8285	-571	-175	0	69	-2502	15.71	15.71	9.42	9.42	2	0.07	0.01	0.05	0.00	0.00	24.0
14	50	-7422	-720	451	0	-367	-3209	15.71	15.71	9.42	9.42	2	0.09	0.01	0.06	0.00	0.00	24.0
15	50	-7674	-635	-558	0	313	-2911	15.71	15.71	9.42	9.42	2	0.08	0.01	0.05	0.00	0.00	24.0
16	50	-7745	-676	464	0	-370	-2973	15.71	15.71	9.42	9.42	2	0.09	0.01	0.06	0.00	0.00	24.0
17	50	-7997	-592	-544	0	310	-2674	15.71	15.71	9.42	9.42	2	0.08	0.01	0.05	0.00	0.00	24.0
18	50	-4872	-1825	53	0	-218	-9996	15.71	15.71	9.42	9.42	3	0.19	0.02	0.16	0.00	0.00	24.0
19	50	-12660	-1822	5	0	-116	-6126	15.71	15.71	9.42	9.42	3	0.11	0.02	0.15	0.00	0.00	24.0
20	50	-9218	-1666	-969	0	495	-7330	15.71	15.71	9.42	9.42	3	0.14	0.02	0.14	0.00	0.00	24.0
37	50	-2716	-1508	36	0	-206	-9897	15.71	15.71	9.42	9.42	3	0.19	0.02	0.14	0.00	0.00	24.0
38	50	-15700	-1502	-44	0	-37	-3447	15.71	15.71	9.42	9.42	3	0.06	0.02	0.12	0.00	0.00	24.0
39	50	-9959	-1243	-1668	0	982	-5454	15.71	15.71	9.42	9.42	3	0.11	0.02	0.11	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 74 NI 1667 NF 1665 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 30
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-441	-1050	-904	0	-519	-5837	15.71	15.71	9.42	9.42	3	0.12	0.01	0.10	0.00	0.00	24.0
2	0	1300	-910	-796	0	-479	-5404	15.71	15.71	9.42	9.42	2	0.16	0.01	0.09	0.00	0.00	24.0
3	0	1298	-923	-894	0	-472	-5408	15.71	15.71	9.42	9.42	2	0.16	0.01	0.09	0.00	0.00	24.0
4	0	-1976	-692	-497	0	-326	-3572	15.71	15.71	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
5	0	-1978	-705	-595	0	-320	-3576	15.71	15.71	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
6	0	156	-818	-578	0	-433	-4758	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
7	0	148	-862	-903	0	-412	-4772	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
8	0	-827	-753	-488	0	-387	-4208	15.71	15.71	9.42	9.42	2	0.12	0.01	0.07	0.00	0.00	24.0
9	0	-834	-797	-814	0	-366	-4222	15.71	15.71	9.42	9.42	2	0.12	0.01	0.07	0.00	0.00	24.0
10	0	1300	-910	-796	0	-479	-5404	15.71	15.71	9.42	9.42	2	0.16	0.01	0.09	0.00	0.00	24.0
11	0	1298	-923	-894	0	-472	-5408	15.71	15.71	9.42	9.42	2	0.16	0.01	0.09	0.00	0.00	24.0
12	0	-1976	-692	-497	0	-326	-3572	15.71	15.71	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
13	0	-1978	-705	-595	0	-320	-3576	15.71	15.71	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
14	0	156	-818	-578	0	-433	-4758	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
15	0	148	-862	-903	0	-412	-4772	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
16	0	-827	-753	-488	0	-387	-4208	15.71	15.71	9.42	9.42	2	0.12	0.01	0.07	0.00	0.00	24.0
17	0	-834	-797	-814	0	-366	-4222	15.71	15.71	9.42	9.42	2	0.12	0.01	0.07	0.00	0.00	24.0
18	0	16240	-1968	-2270	0	-1293	-16510	15.71	15.71	9.42	9.42	3	0.36	0.03	0.18	0.00	0.00	24.0
19	0	333	-1924	-1125	0	-687	-8280	15.71	15.71	9.42	9.42	3	0.17	0.03	0.18	0.00	0.00	24.0
20	0	7128	-1853	-1894	0	-903	-11490	15.71	15.71	9.42	9.42	3	0.24	0.03	0.17	0.00	0.00	24.0
37	0	18670	-1691	-2394	0	-1342	-17110	15.71	15.71	9.42	9.42	3	0.38	0.03	0.17	0.00	0.00	24.0
38	0	-7839	-1618	-486	0	-331	-3394	15.71	15.71	9.42	9.42	3	0.07	0.02	0.14	0.00	0.00	24.0
39	0	3485	-1499	-1767	0	-691	-8737	15.71	15.71	9.42	9.42	3	0.18	0.02	0.14	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-311	-1050	-904	0	-406	-5968	15.71	15.71	9.42	9.42	3	0.12	0.01	0.10	0.00	0.00	24.0
2	12	1400	-910	-796	0	-379	-5518	15.71	15.71	9.42	9.42	2	0.16	0.01	0.09	0.00	0.00	24.0
3	12	1398	-923	-894	0	-361	-5524	15.71	15.71	9.42	9.42	2	0.16	0.01	0.09	0.00	0.00	24.0
4	12	-1876	-692	-497	0	-264	-3658	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
5	12	-1878	-705	-595	0	-245	-3664	15.71	15.71	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
6	12	256	-818	-578	0	-360	-4860	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
7	12	248	-862	-903	0	-299	-4880	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
8	12	-727	-753	-488	0	-326	-4302	15.71	15.71	9.42	9.42	2	0.13	0.01	0.07	0.00	0.00	24.0
9	12	-734	-797	-814	0	-264	-4322	15.71	15.71	9.42	9.42	2	0.12	0.01	0.07	0.00	0.00	24.0
10	12	1400	-910	-796	0	-379	-5518	15.71	15.71	9.42	9.42	2	0.16	0.01	0.09	0.00	0.00	24.0
11	12	1398	-923	-894	0	-361	-5524	15.71	15.71	9.42	9.42	2	0.16	0.01	0.09	0.00	0.00	24.0
12	12	-1876	-692	-497	0	-264	-3658	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
13	12	-1878	-705	-595	0	-245	-3664	15.71	15.71	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
14	12	256	-818	-578	0	-360	-4860	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
15	12	248	-862	-903	0	-299	-4880	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
16	12	-727	-753	-488	0	-326	-4302	15.71	15.71	9.42	9.42	2	0.13	0.01	0.07	0.00	0.00	24.0
17	12	-734	-797	-814	0	-264	-4322	15.71	15.71	9.42	9.42	2	0.12	0.01	0.07	0.00	0.00	24.0
18	12	16370	-1968	-2270	0	-1009	-16755	15.71	15.71	9.42	9.42	3	0.36	0.03	0.18	0.00	0.00	24.0
19	12	463	-1924	-1125	0	-546	-8520	15.71	15.71	9.42	9.42	3	0.17	0.03	0.18	0.00	0.00	24.0
20	12	7258	-1853	-1894	0	-666	-11720	15.71	15.71	9.42	9.42	3	0.24	0.03	0.17	0.00	0.00	24.0
37	12	18800	-1691	-2394	0	-1043	-17320	15.71	15.71	9.42	9.42	3	0.38	0.03	0.17	0.00	0.00	24.0
38	12	-7709	-1618	-486	0	-270	-3596	15.71	15.71	9.42	9.42	3	0.07	0.02	0.14	0.00	0.00	24.0
39	12	3615	-1499	-1767	0	-470	-8925	15.71	15.71	9.42	9.42	3	0.18	0.02	0.14	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-181	-1050	-904	0	-293	-6100	15.71	15.71	9.42	9.42	3	0.12	0.01	0.10	0.00	0.00	24.0
2	25	1500	-910	-796	0	-279	-5632	15.71	15.71	9.42	9.42	2	0.16	0.01	0.09	0.00	0.00	24.0
3	25	1498	-923	-894	0	-249	-5639	15.71	15.71	9.42	9.42	2	0.16	0.01	0.09	0.00	0.00	24.0
4	25	-1776	-692	-497	0	-202	-3745	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
5	25	-1778	-705	-595	0	-171	-3753	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
6	25	356	-818	-578	0	-288	-4963	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
7	25	348	-862	-903	0	-186	-4988	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
8	25	-627	-753	-488	0	-265	-4396	15.71	15.71	9.42	9.42	2	0.13	0.01	0.07	0.00	0.00	24.0
9	25	-634	-797	-814	0	-162	-4421	15.71	15.71	9.42	9.42	2	0.12	0.01	0.07	0.00	0.00	24.0
10	25	1500	-910	-796	0	-279	-5632	15.71	15.71	9.42	9.42	2	0.16	0.01	0.09	0.00	0.00	24.0
11	25	1498	-923	-894	0	-249	-5639	15.71	15.71	9.42	9.42	2	0.16	0.01	0.09	0.00	0.00	24.0
12	25	-1776	-692	-497	0	-202	-3745	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
13	25	-1778	-705	-595	0	-171	-3753	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
14	25	356	-818	-578	0	-288	-4963	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
15	25	348	-862	-903	0	-186	-4988	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
16	25	-627	-753	-488	0	-265	-4396	15.71	15.71	9.42	9.42	2	0.13	0.01	0.07	0.00	0.00	24.0
17	25	-634	-797	-814	0	-162	-4421	15.71	15.71	9.42	9.42	2	0.12	0.01	0.07	0.00	0.00	24.0
18	25	16500	-1968	-2270	0	-726	-17000	15.71	15.71	9.42	9.42	3	0.37	0.03	0.18	0.00	0.00	24.0
19	25	593	-1924	-1125	0	-405	-8761	15.71	15.71	9.42	9.42	3	0.17	0.03	0.18	0.00	0.00	24.0
20	25	7388	-1853	-1894	0	-429	-11950	15.71	15.71	9.42	9.42	3	0.24	0.03	0.17	0.00	0.00	24.0
37	25	18930	-1691	-2394	0	-743	-17530	15.71	15.71	9.42	9.42	3	0.38	0.03	0.17	0.00	0.00	24.0
38	25	-7579	-1618	-486	0	-209	-3798	15.71	15.71	9.42	9.42	3	0.07	0.02	0.14	0.00	0.00	24.0
39	25	3745	-1499	-1767	0	-249	-9112	15.71	15.71	9.42	9.42	3	0.18	0.02	0.14	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-51	-1050	-904	0	-180	-6231	15.71	15.71	9.42	9.42	3	0.12	0.01	0.10	0.00	0.00	24.0
2	38	1600	-910	-796	0	-180	-5745	15.71	15.71	9.42	9.42	2	0.16	0.01	0.09	0.00	0.00	24.0
3	38	1598	-923	-894	0	-137	-5755	15.71	15.71	9.42	9.42	2	0.16	0.01	0.09	0.00	0.00	24.0
4	38	-1676	-692	-497	0	-139	-3831	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
5	38	-1678	-705	-595	0	-97	-3841	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
6	38	456	-818	-578	0	-216	-5065	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
7	38	448	-862	-903	0	-73	-5095	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
8	38	-527	-753	-488	0	-204	-4490	15.71	15.71	9.42	9.42	2	0.13	0.01	0.07	0.00	0.00	24.0
9	38	-534	-797	-814	0	-61	-4521	15.71	15.71	9.42	9.42	2	0.12	0.01	0.07	0.00	0.00	24.0
10	38	1600	-910	-796	0	-180	-5745	15.71	15.71	9.42	9.42	2	0.16	0.01	0.09	0.00	0.00	24.0
11	38	1598	-923	-894	0	-137	-5755	15.71	15.71	9.42	9.42	2	0.16	0.01	0.09	0.00	0.00	24.0
12	38	-1676	-692	-497	0	-139	-3831	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
13	38	-1678	-705	-595	0	-97	-3841	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
14	38	456	-818	-578	0	-216	-5065	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
15	38	448	-862	-903	0	-73	-5095	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
16	38	-527	-753	-488	0	-204	-4490	15.71	15.71	9.42	9.42	2	0.13	0.01	0.07	0.00	0.00	24.0
17	38	-534	-797	-814	0	-61	-4521	15.71	15.71	9.42	9.42	2	0.12	0.01	0.07	0.00	0.00	24.0
18	38	16630	-1968	-2270	0	-442	-17245	15.71	15.71	9.42	9.42	3	0.37	0.03	0.18	0.00	0.00	24.0
19	38	723	-1924	-1125	0	-265	-9002	15.71	15.71	9.42	9.42	3	0.18	0.03	0.18	0.00	0.00	24.0
20	38	7518	-1853	-1894	0	-193	-12180	15.71	15.71	9.42	9.42	3	0.25	0.03	0.17	0.00	0.00	24.0
37	38	19060	-1691	-2394	0	-444	-17740	15.71	15.71	9.42	9.42	3	0.39	0.03	0.17	0.00	0.00	24.0
38	38	-7449	-1618	-486	0	-148	-4000	15.71	15.71	9.42	9.42	3	0.08	0.02	0.14	0.00	0.00	24.0
39	38	3875	-1499	-1767	0	-28	-9300	15.71	15.71	9.42	9.42	3	0.18	0.02	0.14	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	79	-1050	-904	0	-67	-6362	15.71	15.71	9.42	9.42	3	0.12	0.01	0.10	0.00	0.00	24.0
2	50	1700	-910	-796	0	-80	-5859	15.71	15.71	9.42	9.42	2	0.16	0.01	0.09	0.00	0.00	24.0
3	50	1698	-923	-894	0	-25	-5870	15.71	15.71	9.42	9.42	2	0.16	0.01	0.09	0.00	0.00	24.0
4	50	-1576	-692	-497	0	-77	-3918	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
5	50	-1578	-705	-595	0	-22	-3929	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
6	50	556	-818	-578	0	-144	-5167	15.71	15.71	9.42	9.42	2	0.15	0.01	0.08	0.00	0.00	24.0
7	50	548	-862	-903	0	40	-5203	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
8	50	-427	-753	-488	0	-143	-4584	15.71	15.71	9.42	9.42	2	0.13	0.01	0.07	0.00	0.00	24.0
9	50	-434	-797	-814	0	41	-4621	15.71	15.71	9.42	9.42	2	0.13	0.01	0.07	0.00	0.00	24.0
10	50	1700	-910	-796	0	-80	-5859	15.71	15.71	9.42	9.42	2	0.16	0.01	0.09	0.00	0.00	24.0
11	50	1698	-923	-894	0	-25	-5870	15.71	15.71	9.42	9.42	2	0.16	0.01	0.09	0.00	0.00	24.0
12	50	-1576	-692	-497	0	-77	-3918	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
13	50	-1578	-705	-595	0	-22	-3929	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
14	50	556	-818	-578	0	-144	-5167	15.71	15.71	9.42	9.42	2	0.15	0.01	0.08	0.00	0.00	24.0
15	50	548	-862	-903	0	40	-5203	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
16	50	-427	-753	-488	0	-143	-4584	15.71	15.71	9.42	9.42	2	0.13	0.01	0.07	0.00	0.00	24.0
17	50	-434	-797	-814	0	41	-4621	15.71	15.71	9.42	9.42	2	0.13	0.01	0.07	0.00	0.00	24.0
18	50	16760	-1968	-2270	0	-158	-17490	15.71	15.71	9.42	9.42	3	0.37	0.03	0.18	0.00	0.00	24.0
19	50	853	-1924	-1125	0	-124	-9242	15.71	15.71	9.42	9.42	3	0.18	0.03	0.18	0.00	0.00	24.0
20	50	7648	-1853	-1894	0	44	-12410	15.71	15.71	9.42	9.42	3	0.25	0.03	0.17	0.00	0.00	24.0
37	50	19190	-1691	-2394	0	-144	-17950	15.71	15.71	9.42	9.42	3	0.39	0.03	0.17	0.00	0.00	24.0
38	50	-7319	-1618	-486	0	-88	-4202	15.71	15.71	9.42	9.42	3	0.08	0.02	0.14	0.00	0.00	24.0
39	50	4005	-1499	-1767	0	193	-9487	15.71	15.71	9.42	9.42	3	0.19	0.02	0.14	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 75 NI 1684 NF 1683 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 29
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	528	-949	260	0	42	-6407	15.71	15.71	9.42	9.42	3	0.12	0.01	0.09	0.00	0.00	24.0
2	0	2282	-826	234	0	23	-5970	15.71	15.71	9.42	9.42	2	0.17	0.01	0.08	0.00	0.00	24.0
3	0	2192	-808	134	0	27	-5913	15.71	15.71	9.42	9.42	2	0.16	0.01	0.08	0.00	0.00	24.0
4	0	-1379	-652	266	0	39	-3944	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
5	0	-1469	-634	167	0	43	-3887	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
6	0	1106	-786	361	0	23	-5328	15.71	15.71	9.42	9.42	2	0.15	0.01	0.07	0.00	0.00	24.0
7	0	805	-726	30	0	37	-5137	15.71	15.71	9.42	9.42	2	0.14	0.01	0.07	0.00	0.00	24.0
8	0	8	-734	371	0	28	-4720	15.71	15.71	9.42	9.42	2	0.13	0.01	0.07	0.00	0.00	24.0
9	0	-293	-674	40	0	42	-4529	15.71	15.71	9.42	9.42	2	0.12	0.01	0.06	0.00	0.00	24.0
10	0	2282	-826	234	0	23	-5970	15.71	15.71	9.42	9.42	2	0.17	0.01	0.08	0.00	0.00	24.0
11	0	2192	-808	134	0	27	-5913	15.71	15.71	9.42	9.42	2	0.16	0.01	0.08	0.00	0.00	24.0
12	0	-1379	-652	266	0	39	-3944	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
13	0	-1469	-634	167	0	43	-3887	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
14	0	1106	-786	361	0	23	-5328	15.71	15.71	9.42	9.42	2	0.15	0.01	0.07	0.00	0.00	24.0
15	0	805	-726	30	0	37	-5137	15.71	15.71	9.42	9.42	2	0.14	0.01	0.07	0.00	0.00	24.0
16	0	8	-734	371	0	28	-4720	15.71	15.71	9.42	9.42	2	0.13	0.01	0.07	0.00	0.00	24.0
17	0	-293	-674	40	0	42	-4529	15.71	15.71	9.42	9.42	2	0.12	0.01	0.06	0.00	0.00	24.0
18	0	18800	-1699	522	0	75	-17950	15.71	15.71	9.42	9.42	3	0.39	0.02	0.16	0.00	0.00	24.0
19	0	1572	-1847	514	0	99	-9052	15.71	15.71	9.42	9.42	3	0.18	0.02	0.17	0.00	0.00	24.0
20	0	8582	-1610	192	0	91	-12320	15.71	15.71	9.42	9.42	3	0.25	0.02	0.15	0.00	0.00	24.0
37	0	21370	-1382	439	0	52	-18600	15.71	15.71	9.42	9.42	3	0.41	0.02	0.13	0.00	0.00	24.0
38	0	-7345	-1628	426	0	92	-3768	15.71	15.71	9.42	9.42	3	0.07	0.02	0.14	0.00	0.00	24.0
39	0	4338	-1234	-112	0	79	-9219	15.71	15.71	9.42	9.42	3	0.18	0.02	0.12	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	658	-949	260	0	10	-6526	15.71	15.71	9.42	9.42	3	0.13	0.01	0.09	0.00	0.00	24.0
2	12	2382	-826	234	0	-7	-6073	15.71	15.71	9.42	9.42	2	0.17	0.01	0.08	0.00	0.00	24.0
3	12	2292	-808	134	0	10	-6014	15.71	15.71	9.42	9.42	2	0.17	0.01	0.08	0.00	0.00	24.0
4	12	-1279	-652	266	0	5	-4025	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
5	12	-1369	-634	167	0	22	-3966	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
6	12	1206	-786	361	0	-22	-5426	15.71	15.71	9.42	9.42	2	0.15	0.01	0.07	0.00	0.00	24.0
7	12	905	-726	30	0	33	-5228	15.71	15.71	9.42	9.42	2	0.14	0.01	0.07	0.00	0.00	24.0
8	12	108	-734	371	0	-18	-4812	15.71	15.71	9.42	9.42	2	0.13	0.01	0.07	0.00	0.00	24.0
9	12	-193	-674	40	0	37	-4613	15.71	15.71	9.42	9.42	2	0.13	0.01	0.06	0.00	0.00	24.0
10	12	2382	-826	234	0	-7	-6073	15.71	15.71	9.42	9.42	2	0.17	0.01	0.08	0.00	0.00	24.0
11	12	2292	-808	134	0	10	-6014	15.71	15.71	9.42	9.42	2	0.17	0.01	0.08	0.00	0.00	24.0
12	12	-1279	-652	266	0	5	-4025	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
13	12	-1369	-634	167	0	22	-3966	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
14	12	1206	-786	361	0	-22	-5426	15.71	15.71	9.42	9.42	2	0.15	0.01	0.07	0.00	0.00	24.0
15	12	905	-726	30	0	33	-5228	15.71	15.71	9.42	9.42	2	0.14	0.01	0.07	0.00	0.00	24.0
16	12	108	-734	371	0	-18	-4812	15.71	15.71	9.42	9.42	2	0.13	0.01	0.07	0.00	0.00	24.0
17	12	-193	-674	40	0	37	-4613	15.71	15.71	9.42	9.42	2	0.13	0.01	0.06	0.00	0.00	24.0
18	12	18930	-1699	522	0	9	-18163	15.71	15.71	9.42	9.42	3	0.39	0.02	0.16	0.00	0.00	24.0
19	12	1702	-1847	514	0	34	-9283	15.71	15.71	9.42	9.42	3	0.18	0.02	0.17	0.00	0.00	24.0
20	12	8712	-1610	192	0	67	-12522	15.71	15.71	9.42	9.42	3	0.25	0.02	0.15	0.00	0.00	24.0
37	12	21500	-1382	439	0	-3	-18772	15.71	15.71	9.42	9.42	3	0.41	0.02	0.13	0.00	0.00	24.0
38	12	-7215	-1628	426	0	39	-3971	15.71	15.71	9.42	9.42	3	0.07	0.02	0.14	0.00	0.00	24.0
39	12	4468	-1234	-112	0	93	-9373	15.71	15.71	9.42	9.42	3	0.19	0.02	0.12	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	788	-949	260	0	-23	-6644	15.71	15.71	9.42	9.42	3	0.13	0.01	0.09	0.00	0.00	24.0
2	25	2482	-826	234	0	-36	-6176	15.71	15.71	9.42	9.42	2	0.17	0.01	0.08	0.00	0.00	24.0
3	25	2392	-808	134	0	-7	-6115	15.71	15.71	9.42	9.42	2	0.17	0.01	0.08	0.00	0.00	24.0
4	25	-1179	-652	266	0	-28	-4107	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
5	25	-1269	-634	167	0	1	-4046	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
6	25	1306	-786	361	0	-67	-5524	15.71	15.71	9.42	9.42	2	0.15	0.01	0.07	0.00	0.00	24.0
7	25	1005	-726	30	0	30	-5318	15.71	15.71	9.42	9.42	2	0.15	0.01	0.07	0.00	0.00	24.0
8	25	208	-734	371	0	-64	-4904	15.71	15.71	9.42	9.42	2	0.14	0.01	0.07	0.00	0.00	24.0
9	25	-93	-674	40	0	32	-4697	15.71	15.71	9.42	9.42	2	0.13	0.01	0.06	0.00	0.00	24.0
10	25	2482	-826	234	0	-36	-6176	15.71	15.71	9.42	9.42	2	0.17	0.01	0.08	0.00	0.00	24.0
11	25	2392	-808	134	0	-7	-6115	15.71	15.71	9.42	9.42	2	0.17	0.01	0.08	0.00	0.00	24.0
12	25	-1179	-652	266	0	-28	-4107	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
13	25	-1269	-634	167	0	1	-4046	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
14	25	1306	-786	361	0	-67	-5524	15.71	15.71	9.42	9.42	2	0.15	0.01	0.07	0.00	0.00	24.0
15	25	1005	-726	30	0	30	-5318	15.71	15.71	9.42	9.42	2	0.15	0.01	0.07	0.00	0.00	24.0
16	25	208	-734	371	0	-64	-4904	15.71	15.71	9.42	9.42	2	0.14	0.01	0.07	0.00	0.00	24.0
17	25	-93	-674	40	0	32	-4697	15.71	15.71	9.42	9.42	2	0.13	0.01	0.06	0.00	0.00	24.0
18	25	19060	-1699	522	0	-56	-18375	15.71	15.71	9.42	9.42	3	0.40	0.02	0.16	0.00	0.00	24.0
19	25	1832	-1847	514	0	-30	-9513	15.71	15.71	9.42	9.42	3	0.19	0.02	0.17	0.00	0.00	24.0
20	25	8842	-1610	192	0	43	-12725	15.71	15.71	9.42	9.42	3	0.26	0.02	0.15	0.00	0.00	24.0
37	25	21630	-1382	439	0	-58	-18945	15.71	15.71	9.42	9.42	3	0.42	0.02	0.13	0.00	0.00	24.0
38	25	-7085	-1628	426	0	-14	-4175	15.71	15.71	9.42	9.42	3	0.08	0.02	0.14	0.00	0.00	24.0
39	25	4598	-1234	-112	0	107	-9528	15.71	15.71	9.42	9.42	3	0.19	0.02	0.12	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	918	-949	260	0	-55	-6763	15.71	15.71	9.42	9.42	3	0.13	0.01	0.09	0.00	0.00	24.0
2	38	2582	-826	234	0	-65	-6280	15.71	15.71	9.42	9.42	2	0.18	0.01	0.08	0.00	0.00	24.0
3	38	2492	-808	134	0	-24	-6216	15.71	15.71	9.42	9.42	2	0.17	0.01	0.08	0.00	0.00	24.0
4	38	-1079	-652	266	0	-61	-4189	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
5	38	-1169	-634	167	0	-20	-4125	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
6	38	1406	-786	361	0	-112	-5623	15.71	15.71	9.42	9.42	2	0.16	0.01	0.07	0.00	0.00	24.0
7	38	1105	-726	30	0	26	-5409	15.71	15.71	9.42	9.42	2	0.15	0.01	0.07	0.00	0.00	24.0
8	38	308	-734	371	0	-111	-4995	15.71	15.71	9.42	9.42	2	0.14	0.01	0.07	0.00	0.00	24.0
9	38	7	-674	40	0	27	-4782	15.71	15.71	9.42	9.42	2	0.13	0.01	0.06	0.00	0.00	24.0
10	38	2582	-826	234	0	-65	-6280	15.71	15.71	9.42	9.42	2	0.18	0.01	0.08	0.00	0.00	24.0
11	38	2492	-808	134	0	-24	-6216	15.71	15.71	9.42	9.42	2	0.17	0.01	0.08	0.00	0.00	24.0
12	38	-1079	-652	266	0	-61	-4189	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
13	38	-1169	-634	167	0	-20	-4125	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
14	38	1406	-786	361	0	-112	-5623	15.71	15.71	9.42	9.42	2	0.16	0.01	0.07	0.00	0.00	24.0
15	38	1105	-726	30	0	26	-5409	15.71	15.71	9.42	9.42	2	0.15	0.01	0.07	0.00	0.00	24.0
16	38	308	-734	371	0	-111	-4995	15.71	15.71	9.42	9.42	2	0.14	0.01	0.07	0.00	0.00	24.0
17	38	7	-674	40	0	27	-4782	15.71	15.71	9.42	9.42	2	0.13	0.01	0.06	0.00	0.00	24.0
18	38	19190	-1699	522	0	-121	-18587	15.71	15.71	9.42	9.42	3	0.40	0.02	0.16	0.00	0.00	24.0
19	38	1962	-1847	514	0	-94	-9744	15.71	15.71	9.42	9.42	3	0.19	0.02	0.17	0.00	0.00	24.0
20	38	8972	-1610	192	0	19	-12927	15.71	15.71	9.42	9.42	3	0.26	0.02	0.15	0.00	0.00	24.0
37	38	21760	-1382	439	0	-112	-19118	15.71	15.71	9.42	9.42	3	0.42	0.02	0.13	0.00	0.00	24.0
38	38	-6955	-1628	426	0	-68	-4378	15.71	15.71	9.42	9.42	3	0.08	0.02	0.14	0.00	0.00	24.0
39	38	4728	-1234	-112	0	121	-9682	15.71	15.71	9.42	9.42	3	0.19	0.02	0.12	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	1048	-949	260	0	-88	-6881	15.71	15.71	9.42	9.42	3	0.13	0.01	0.09	0.00	0.00	24.0
2	50	2682	-826	234	0	-94	-6383	15.71	15.71	9.42	9.42	2	0.18	0.01	0.08	0.00	0.00	24.0
3	50	2592	-808	134	0	-40	-6317	15.71	15.71	9.42	9.42	2	0.18	0.01	0.08	0.00	0.00	24.0
4	50	-979	-652	266	0	-94	-4270	15.71	15.71	9.42	9.42	2	0.12	0.01	0.06	0.00	0.00	24.0
5	50	-1069	-634	167	0	-41	-4204	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
6	50	1506	-786	361	0	-157	-5721	15.71	15.71	9.42	9.42	2	0.16	0.01	0.07	0.00	0.00	24.0
7	50	1205	-726	30	0	22	-5500	15.71	15.71	9.42	9.42	2	0.15	0.01	0.07	0.00	0.00	24.0
8	50	408	-734	371	0	-157	-5087	15.71	15.71	9.42	9.42	2	0.14	0.01	0.07	0.00	0.00	24.0
9	50	107	-674	40	0	22	-4866	15.71	15.71	9.42	9.42	2	0.13	0.01	0.06	0.00	0.00	24.0
10	50	2682	-826	234	0	-94	-6383	15.71	15.71	9.42	9.42	2	0.18	0.01	0.08	0.00	0.00	24.0
11	50	2592	-808	134	0	-40	-6317	15.71	15.71	9.42	9.42	2	0.18	0.01	0.08	0.00	0.00	24.0
12	50	-979	-652	266	0	-94	-4270	15.71	15.71	9.42	9.42	2	0.12	0.01	0.06	0.00	0.00	24.0
13	50	-1069	-634	167	0	-41	-4204	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
14	50	1506	-786	361	0	-157	-5721	15.71	15.71	9.42	9.42	2	0.16	0.01	0.07	0.00	0.00	24.0
15	50	1205	-726	30	0	22	-5500	15.71	15.71	9.42	9.42	2	0.15	0.01	0.07	0.00	0.00	24.0
16	50	408	-734	371	0	-157	-5087	15.71	15.71	9.42	9.42	2	0.14	0.01	0.07	0.00	0.00	24.0
17	50	107	-674	40	0	22	-4866	15.71	15.71	9.42	9.42	2	0.13	0.01	0.06	0.00	0.00	24.0
18	50	19320	-1699	522	0	-186	-18800	15.71	15.71	9.42	9.42	3	0.41	0.02	0.16	0.00	0.00	24.0
19	50	2092	-1847	514	0	-159	-9975	15.71	15.71	9.42	9.42	3	0.20	0.02	0.17	0.00	0.00	24.0
20	50	9102	-1610	192	0	-5	-13130	15.71	15.71	9.42	9.42	3	0.27	0.02	0.15	0.00	0.00	24.0
37	50	21890	-1382	439	0	-167	-19290	15.71	15.71	9.42	9.42	3	0.43	0.02	0.13	0.00	0.00	24.0
38	50	-6825	-1628	426	0	-121	-4582	15.71	15.71	9.42	9.42	3	0.09	0.02	0.14	0.00	0.00	24.0
39	50	4858	-1234	-112	0	135	-9836	15.71	15.71	9.42	9.42	3	0.20	0.02	0.12	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 76 NI 1692 NF 1691 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 28
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-745	-1104	1370	0	589	-5681	15.71	15.71	9.42	9.42	3	0.11	0.02	0.10	0.00	0.00	24.0
2	0	1257	-988	1225	0	513	-5395	15.71	15.71	9.42	9.42	2	0.16	0.02	0.09	0.00	0.00	24.0
3	0	1250	-993	1118	0	509	-5393	15.71	15.71	9.42	9.42	2	0.16	0.02	0.09	0.00	0.00	24.0
4	0	-2397	-706	990	0	398	-3347	15.71	15.71	9.42	9.42	2	0.10	0.01	0.07	0.00	0.00	24.0
5	0	-2404	-710	882	0	394	-3344	15.71	15.71	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
6	0	-13	-884	1268	0	477	-4681	15.71	15.71	9.42	9.42	2	0.14	0.02	0.09	0.00	0.00	24.0
7	0	-38	-900	911	0	465	-4673	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
8	0	-1109	-799	1197	0	442	-4066	15.71	15.71	9.42	9.42	2	0.12	0.02	0.08	0.00	0.00	24.0
9	0	-1134	-815	840	0	430	-4059	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
10	0	1257	-988	1225	0	513	-5395	15.71	15.71	9.42	9.42	2	0.16	0.02	0.09	0.00	0.00	24.0
11	0	1250	-993	1118	0	509	-5393	15.71	15.71	9.42	9.42	2	0.16	0.02	0.09	0.00	0.00	24.0
12	0	-2397	-706	990	0	398	-3347	15.71	15.71	9.42	9.42	2	0.10	0.01	0.07	0.00	0.00	24.0
13	0	-2404	-710	882	0	394	-3344	15.71	15.71	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
14	0	-13	-884	1268	0	477	-4681	15.71	15.71	9.42	9.42	2	0.14	0.02	0.09	0.00	0.00	24.0
15	0	-38	-900	911	0	465	-4673	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
16	0	-1109	-799	1197	0	442	-4066	15.71	15.71	9.42	9.42	2	0.12	0.02	0.08	0.00	0.00	24.0
17	0	-1134	-815	840	0	430	-4059	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
18	0	16410	-2309	3290	0	1423	-16610	15.71	15.71	9.42	9.42	3	0.36	0.05	0.23	0.00	0.00	24.0
19	0	-610	-1973	2100	0	870	-7747	15.71	15.71	9.42	9.42	3	0.16	0.03	0.18	0.00	0.00	24.0
20	0	6630	-1999	2209	0	1055	-11220	15.71	15.71	9.42	9.42	3	0.23	0.03	0.19	0.00	0.00	24.0
37	0	19250	-2084	3253	0	1425	-17440	15.71	15.71	9.42	9.42	3	0.39	0.05	0.23	0.00	0.00	24.0
38	0	-9129	-1523	1271	0	505	-2668	15.71	15.71	9.42	9.42	3	0.05	0.02	0.13	0.00	0.00	24.0
39	0	2939	-1566	1452	0	813	-8452	15.71	15.71	9.42	9.42	3	0.17	0.02	0.15	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-615	-1104	1370	0	418	-5819	15.71	15.71	9.42	9.42	3	0.11	0.02	0.10	0.00	0.00	24.0
2	12	1357	-988	1225	0	360	-5519	15.71	15.71	9.42	9.42	2	0.16	0.02	0.09	0.00	0.00	24.0
3	12	1350	-993	1118	0	370	-5517	15.71	15.71	9.42	9.42	2	0.16	0.02	0.09	0.00	0.00	24.0
4	12	-2297	-706	990	0	274	-3435	15.71	15.71	9.42	9.42	2	0.10	0.01	0.07	0.00	0.00	24.0
5	12	-2304	-710	882	0	284	-3433	15.71	15.71	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
6	12	87	-884	1268	0	318	-4792	15.71	15.71	9.42	9.42	2	0.14	0.02	0.09	0.00	0.00	24.0
7	12	62	-900	911	0	351	-4786	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
8	12	-1009	-799	1197	0	292	-4166	15.71	15.71	9.42	9.42	2	0.12	0.02	0.08	0.00	0.00	24.0
9	12	-1034	-815	840	0	325	-4161	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
10	12	1357	-988	1225	0	360	-5519	15.71	15.71	9.42	9.42	2	0.16	0.02	0.09	0.00	0.00	24.0
11	12	1350	-993	1118	0	370	-5517	15.71	15.71	9.42	9.42	2	0.16	0.02	0.09	0.00	0.00	24.0
12	12	-2297	-706	990	0	274	-3435	15.71	15.71	9.42	9.42	2	0.10	0.01	0.07	0.00	0.00	24.0
13	12	-2304	-710	882	0	284	-3433	15.71	15.71	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
14	12	87	-884	1268	0	318	-4792	15.71	15.71	9.42	9.42	2	0.14	0.02	0.09	0.00	0.00	24.0
15	12	62	-900	911	0	351	-4786	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
16	12	-1009	-799	1197	0	292	-4166	15.71	15.71	9.42	9.42	2	0.12	0.02	0.08	0.00	0.00	24.0
17	12	-1034	-815	840	0	325	-4161	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
18	12	16540	-2309	3290	0	1012	-16900	15.71	15.71	9.42	9.42	3	0.37	0.05	0.23	0.00	0.00	24.0
19	12	-481	-1973	2100	0	608	-7994	15.71	15.71	9.42	9.42	3	0.16	0.03	0.18	0.00	0.00	24.0
20	12	6760	-1999	2209	0	779	-11470	15.71	15.71	9.42	9.42	3	0.24	0.03	0.19	0.00	0.00	24.0
37	12	19380	-2084	3253	0	1018	-17700	15.71	15.71	9.42	9.42	3	0.39	0.05	0.23	0.00	0.00	24.0
38	12	-8999	-1523	1271	0	346	-2858	15.71	15.71	9.42	9.42	3	0.06	0.02	0.13	0.00	0.00	24.0
39	12	3069	-1566	1452	0	631	-8648	15.71	15.71	9.42	9.42	3	0.17	0.02	0.15	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-485	-1104	1370	0	247	-5957	15.71	15.71	9.42	9.42	3	0.12	0.02	0.10	0.00	0.00	24.0
2	25	1457	-988	1225	0	207	-5642	15.71	15.71	9.42	9.42	2	0.16	0.02	0.09	0.00	0.00	24.0
3	25	1450	-993	1118	0	230	-5642	15.71	15.71	9.42	9.42	2	0.16	0.02	0.09	0.00	0.00	24.0
4	25	-2197	-706	990	0	150	-3523	15.71	15.71	9.42	9.42	2	0.10	0.01	0.07	0.00	0.00	24.0
5	25	-2204	-710	882	0	173	-3522	15.71	15.71	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
6	25	187	-884	1268	0	160	-4902	15.71	15.71	9.42	9.42	2	0.14	0.02	0.09	0.00	0.00	24.0
7	25	162	-900	911	0	237	-4898	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
8	25	-909	-799	1197	0	143	-4266	15.71	15.71	9.42	9.42	2	0.12	0.02	0.08	0.00	0.00	24.0
9	25	-934	-815	840	0	220	-4262	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
10	25	1457	-988	1225	0	207	-5642	15.71	15.71	9.42	9.42	2	0.16	0.02	0.09	0.00	0.00	24.0
11	25	1450	-993	1118	0	230	-5642	15.71	15.71	9.42	9.42	2	0.16	0.02	0.09	0.00	0.00	24.0
12	25	-2197	-706	990	0	150	-3523	15.71	15.71	9.42	9.42	2	0.10	0.01	0.07	0.00	0.00	24.0
13	25	-2204	-710	882	0	173	-3522	15.71	15.71	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
14	25	187	-884	1268	0	160	-4902	15.71	15.71	9.42	9.42	2	0.14	0.02	0.09	0.00	0.00	24.0
15	25	162	-900	911	0	237	-4898	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
16	25	-909	-799	1197	0	143	-4266	15.71	15.71	9.42	9.42	2	0.12	0.02	0.08	0.00	0.00	24.0
17	25	-934	-815	840	0	220	-4262	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
18	25	16670	-2309	3290	0	600	-17190	15.71	15.71	9.42	9.42	3	0.37	0.05	0.23	0.00	0.00	24.0
19	25	-351	-1973	2100	0	346	-8240	15.71	15.71	9.42	9.42	3	0.16	0.03	0.18	0.00	0.00	24.0
20	25	6890	-1999	2209	0	503	-11720	15.71	15.71	9.42	9.42	3	0.24	0.03	0.19	0.00	0.00	24.0
37	25	19510	-2084	3253	0	612	-17960	15.71	15.71	9.42	9.42	3	0.39	0.05	0.23	0.00	0.00	24.0
38	25	-8869	-1523	1271	0	187	-3048	15.71	15.71	9.42	9.42	3	0.06	0.02	0.13	0.00	0.00	24.0

39	25	3199	-1566	1452	0	450	-8844	15.71	15.71	9.42	9.42	3	0.18	0.02	0.15	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-355	-1104	1370	0	76	-6095	15.71	15.71	9.42	9.42	3	0.12	0.02	0.10	0.00	0.00	24.0
2	38	1557	-988	1225	0	53	-5766	15.71	15.71	9.42	9.42	2	0.16	0.02	0.09	0.00	0.00	24.0
3	38	1550	-993	1118	0	90	-5766	15.71	15.71	9.42	9.42	2	0.16	0.02	0.09	0.00	0.00	24.0
4	38	-2097	-706	990	0	26	-3611	15.71	15.71	9.42	9.42	2	0.10	0.01	0.07	0.00	0.00	24.0
5	38	-2104	-710	882	0	63	-3610	15.71	15.71	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
6	38	287	-884	1268	0	1	-5012	15.71	15.71	9.42	9.42	2	0.14	0.02	0.09	0.00	0.00	24.0
7	38	262	-900	911	0	123	-5011	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
8	38	-809	-799	1197	0	-7	-4366	15.71	15.71	9.42	9.42	2	0.12	0.02	0.08	0.00	0.00	24.0
9	38	-834	-815	840	0	115	-4364	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
10	38	1557	-988	1225	0	53	-5766	15.71	15.71	9.42	9.42	2	0.16	0.02	0.09	0.00	0.00	24.0
11	38	1550	-993	1118	0	90	-5766	15.71	15.71	9.42	9.42	2	0.16	0.02	0.09	0.00	0.00	24.0
12	38	-2097	-706	990	0	26	-3611	15.71	15.71	9.42	9.42	2	0.10	0.01	0.07	0.00	0.00	24.0
13	38	-2104	-710	882	0	63	-3610	15.71	15.71	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
14	38	287	-884	1268	0	1	-5012	15.71	15.71	9.42	9.42	2	0.14	0.02	0.09	0.00	0.00	24.0
15	38	262	-900	911	0	123	-5011	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
16	38	-809	-799	1197	0	-7	-4366	15.71	15.71	9.42	9.42	2	0.12	0.02	0.08	0.00	0.00	24.0
17	38	-834	-815	840	0	115	-4364	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
18	38	16800	-2309	3290	0	189	-17480	15.71	15.71	9.42	9.42	3	0.37	0.05	0.23	0.00	0.00	24.0
19	38	-221	-1973	2100	0	83	-8487	15.71	15.71	9.42	9.42	3	0.16	0.03	0.18	0.00	0.00	24.0
20	38	7020	-1999	2209	0	227	-11970	15.71	15.71	9.42	9.42	3	0.24	0.03	0.19	0.00	0.00	24.0
37	38	19640	-2084	3253	0	205	-18220	15.71	15.71	9.42	9.42	3	0.40	0.05	0.23	0.00	0.00	24.0
38	38	-8739	-1523	1271	0	28	-3239	15.71	15.71	9.42	9.42	3	0.06	0.02	0.13	0.00	0.00	24.0
39	38	3329	-1566	1452	0	268	-9039	15.71	15.71	9.42	9.42	3	0.18	0.02	0.15	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-225	-1104	1370	0	-96	-6233	15.71	15.71	9.42	9.42	3	0.12	0.02	0.10	0.00	0.00	24.0
2	50	1657	-988	1225	0	-100	-5890	15.71	15.71	9.42	9.42	2	0.17	0.02	0.09	0.00	0.00	24.0
3	50	1650	-993	1118	0	-50	-5890	15.71	15.71	9.42	9.42	2	0.16	0.02	0.09	0.00	0.00	24.0
4	50	-1997	-706	990	0	-97	-3699	15.71	15.71	9.42	9.42	2	0.10	0.01	0.07	0.00	0.00	24.0
5	50	-2004	-710	882	0	-47	-3699	15.71	15.71	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
6	50	387	-884	1268	0	-157	-5123	15.71	15.71	9.42	9.42	2	0.14	0.02	0.09	0.00	0.00	24.0
7	50	362	-900	911	0	9	-5123	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
8	50	-709	-799	1197	0	-156	-4466	15.71	15.71	9.42	9.42	2	0.13	0.02	0.08	0.00	0.00	24.0
9	50	-734	-815	840	0	10	-4466	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
10	50	1657	-988	1225	0	-100	-5890	15.71	15.71	9.42	9.42	2	0.17	0.02	0.09	0.00	0.00	24.0
11	50	1650	-993	1118	0	-50	-5890	15.71	15.71	9.42	9.42	2	0.16	0.02	0.09	0.00	0.00	24.0
12	50	-1997	-706	990	0	-97	-3699	15.71	15.71	9.42	9.42	2	0.10	0.01	0.07	0.00	0.00	24.0
13	50	-2004	-710	882	0	-47	-3699	15.71	15.71	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
14	50	387	-884	1268	0	-157	-5123	15.71	15.71	9.42	9.42	2	0.14	0.02	0.09	0.00	0.00	24.0
15	50	362	-900	911	0	9	-5123	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
16	50	-709	-799	1197	0	-156	-4466	15.71	15.71	9.42	9.42	2	0.13	0.02	0.08	0.00	0.00	24.0
17	50	-734	-815	840	0	10	-4466	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
18	50	16930	-2309	3290	0	-222	-17770	15.71	15.71	9.42	9.42	3	0.38	0.05	0.23	0.00	0.00	24.0
19	50	-91	-1973	2100	0	-180	-8733	15.71	15.71	9.42	9.42	3	0.17	0.03	0.18	0.00	0.00	24.0
20	50	7150	-1999	2209	0	-49	-12220	15.71	15.71	9.42	9.42	3	0.25	0.03	0.19	0.00	0.00	24.0
37	50	19770	-2084	3253	0	-201	-18480	15.71	15.71	9.42	9.42	3	0.40	0.05	0.23	0.00	0.00	24.0
38	50	-8609	-1523	1271	0	-131	-3429	15.71	15.71	9.42	9.42	3	0.06	0.02	0.13	0.00	0.00	24.0
39	50	3459	-1566	1452	0	87	-9235	15.71	15.71	9.42	9.42	3	0.18	0.02	0.15	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 77 NI 1700 NF 1699 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 27
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-6958	-807	2375	0	1124	-1534	15.71	15.71	9.42	9.42	3	0.05	0.03	0.16	0.00	0.00	24.0
2	0	-4085	-833	2152	0	1011	-1873	15.71	15.71	9.42	9.42	2	0.08	0.03	0.15	0.00	0.00	24.0
3	0	-4058	-862	2065	0	1018	-1916	15.71	15.71	9.42	9.42	2	0.08	0.03	0.14	0.00	0.00	24.0
4	0	-6647	-380	1589	0	711	-444	15.71	15.71	9.42	9.42	2	0.04	0.02	0.12	0.00	0.00	24.0
5	0	-6620	-408	1502	0	718	-487	15.71	15.71	9.42	9.42	2	0.04	0.02	0.11	0.00	0.00	24.0
6	0	-5014	-640	2056	0	898	-1322	15.71	15.71	9.42	9.42	2	0.06	0.03	0.14	0.00	0.00	24.0
7	0	-4923	-737	1767	0	921	-1466	15.71	15.71	9.42	9.42	2	0.07	0.02	0.12	0.00	0.00	24.0
8	0	-5783	-504	1888	0	808	-893	15.71	15.71	9.42	9.42	2	0.05	0.03	0.13	0.00	0.00	24.0
9	0	-5691	-601	1598	0	831	-1038	15.71	15.71	9.42	9.42	2	0.06	0.02	0.11	0.00	0.00	24.0
10	0	-4085	-833	2152	0	1011	-1873	15.71	15.71	9.42	9.42	2	0.08	0.03	0.15	0.00	0.00	24.0
11	0	-4058	-862	2065	0	1018	-1916	15.71	15.71	9.42	9.42	2	0.08	0.03	0.14	0.00	0.00	24.0
12	0	-6647	-380	1589	0	711	-444	15.71	15.71	9.42	9.42	2	0.04	0.02	0.12	0.00	0.00	24.0
13	0	-6620	-408	1502	0	718	-487	15.71	15.71	9.42	9.42	2	0.04	0.02	0.11	0.00	0.00	24.0
14	0	-5014	-640	2056	0	898	-1322	15.71	15.71	9.42	9.42	2	0.06	0.03	0.14	0.00	0.00	24.0
15	0	-4923	-737	1767	0	921	-1466	15.71	15.71	9.42	9.42	2	0.07	0.02	0.12	0.00	0.00	24.0
16	0	-5783	-504	1888	0	808	-893	15.71	15.71	9.42	9.42	2	0.05	0.03	0.13	0.00	0.00	24.0
17	0	-5691	-601	1598	0	831	-1038	15.71	15.71	9.42	9.42	2	0.06	0.02	0.11	0.00	0.00	24.0
18	0	2146	-2258	5956	0	2910	-7544	15.71	15.71	9.42	9.42	3	0.19	0.08	0.42	0.00	0.00	24.0
19	0	-10180	-1076	3299	0	1534	-1329	15.71	15.71	9.42	9.42	3	0.06	0.05	0.24	0.00	0.00	24.0
20	0	-4381	-1615	4061	0	2077	-4120	15.71	15.71	9.42	9.42	3	0.11	0.06	0.28	0.00	0.00	24.0
37	0	5277	-2369	6107	0	3010	-8665	15.71	15.71	9.42	9.42	3	0.21	0.09	0.43	0.00	0.00	24.0
38	0	-15270	-399	1679	0	717	1694	15.71	15.71	9.42	9.42	3	0.04	0.02	0.10	0.00	0.00	24.0
39	0	-5601	-1297	2948	0	1622	-2958	15.71	15.71	9.42	9.42	3	0.08	0.04	0.20	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-6828	-807	2375	0	827	-1635	15.71	15.71	9.42	9.42	3	0.04	0.03	0.16	0.00	0.00	24.0
2	12	-3985	-833	2152	0	742	-1977	15.71	15.71	9.42	9.42	2	0.07	0.03	0.15	0.00	0.00	24.0
3	12	-3958	-862	2065	0	760	-2024	15.71	15.71	9.42	9.42	2	0.08	0.03	0.14	0.00	0.00	24.0
4	12	-6547	-380	1589	0	512	-491	15.71	15.71	9.42	9.42	2	0.03	0.02	0.12	0.00	0.00	24.0
5	12	-6520	-408	1502	0	530	-538	15.71	15.71	9.42	9.42	2	0.03	0.02	0.10	0.00	0.00	24.0
6	12	-4914	-640	2056	0	641	-1402	15.71	15.71	9.42	9.42	2	0.06	0.03	0.14	0.00	0.00	24.0
7	12	-4823	-737	1767	0	700	-1558	15.71	15.71	9.42	9.42	2	0.06	0.02	0.12	0.00	0.00	24.0
8	12	-5683	-504	1888	0	572	-956	15.71	15.71	9.42	9.42	2	0.04	0.03	0.13	0.00	0.00	24.0
9	12	-5591	-601	1598	0	631	-1113	15.71	15.71	9.42	9.42	2	0.05	0.02	0.11	0.00	0.00	24.0
10	12	-3985	-833	2152	0	742	-1977	15.71	15.71	9.42	9.42	2	0.07	0.03	0.15	0.00	0.00	24.0
11	12	-3958	-862	2065	0	760	-2024	15.71	15.71	9.42	9.42	2	0.08	0.03	0.14	0.00	0.00	24.0
12	12	-6547	-380	1589	0	512	-491	15.71	15.71	9.42	9.42	2	0.03	0.02	0.12	0.00	0.00	24.0
13	12	-6520	-408	1502	0	530	-538	15.71	15.71	9.42	9.42	2	0.03	0.02	0.10	0.00	0.00	24.0
14	12	-4914	-640	2056	0	641	-1402	15.71	15.71	9.42	9.42	2	0.06	0.03	0.14	0.00	0.00	24.0
15	12	-4823	-737	1767	0	700	-1558	15.71	15.71	9.42	9.42	2	0.06	0.02	0.12	0.00	0.00	24.0
16	12	-5683	-504	1888	0	572	-956	15.71	15.71	9.42	9.42	2	0.04	0.03	0.13	0.00	0.00	24.0
17	12	-5591	-601	1598	0	631	-1113	15.71	15.71	9.42	9.42	2	0.05	0.02	0.11	0.00	0.00	24.0
18	12	2276	-2258	5956	0	2165	-7826	15.71	15.71	9.42	9.42	3	0.18	0.08	0.42	0.00	0.00	24.0

19	12	-10050	-1076	3299	0	1122	-1463	15.71	15.71	9.42	9.42	3	0.05	0.05	0.21	0.00	0.00	24.0
20	12	-4251	-1615	4061	0	1569	-4322	15.71	15.71	9.42	9.42	3	0.10	0.06	0.28	0.00	0.00	24.0
37	12	5407	-2369	6107	0	2247	-8961	15.71	15.71	9.42	9.42	3	0.20	0.09	0.43	0.00	0.00	24.0
38	12	-15140	-399	1679	0	507	1644	15.71	15.71	9.42	9.42	3	0.04	0.02	0.10	0.00	0.00	24.0
39	12	-5471	-1297	2948	0	1253	-3120	15.71	15.71	9.42	9.42	3	0.08	0.04	0.20	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-6698	-807	2375	0	530	-1736	15.71	15.71	9.42	9.42	3	0.04	0.03	0.16	0.00	0.00	24.0
2	25	-3885	-833	2152	0	473	-2081	15.71	15.71	9.42	9.42	2	0.07	0.03	0.15	0.00	0.00	24.0
3	25	-3858	-862	2065	0	502	-2132	15.71	15.71	9.42	9.42	2	0.07	0.03	0.14	0.00	0.00	24.0
4	25	-6447	-380	1589	0	314	-539	15.71	15.71	9.42	9.42	2	0.02	0.02	0.11	0.00	0.00	24.0
5	25	-6420	-408	1502	0	342	-589	15.71	15.71	9.42	9.42	2	0.03	0.02	0.10	0.00	0.00	24.0
6	25	-4814	-640	2056	0	384	-1482	15.71	15.71	9.42	9.42	2	0.05	0.03	0.14	0.00	0.00	24.0
7	25	-4723	-737	1767	0	479	-1651	15.71	15.71	9.42	9.42	2	0.06	0.02	0.12	0.00	0.00	24.0
8	25	-5583	-504	1888	0	336	-1019	15.71	15.71	9.42	9.42	2	0.04	0.03	0.13	0.00	0.00	24.0
9	25	-5491	-601	1598	0	431	-1188	15.71	15.71	9.42	9.42	2	0.04	0.02	0.11	0.00	0.00	24.0
10	25	-3885	-833	2152	0	473	-2081	15.71	15.71	9.42	9.42	2	0.07	0.03	0.15	0.00	0.00	24.0
11	25	-3858	-862	2065	0	502	-2132	15.71	15.71	9.42	9.42	2	0.07	0.03	0.14	0.00	0.00	24.0
12	25	-6447	-380	1589	0	314	-539	15.71	15.71	9.42	9.42	2	0.02	0.02	0.11	0.00	0.00	24.0
13	25	-6420	-408	1502	0	342	-589	15.71	15.71	9.42	9.42	2	0.03	0.02	0.10	0.00	0.00	24.0
14	25	-4814	-640	2056	0	384	-1482	15.71	15.71	9.42	9.42	2	0.05	0.03	0.14	0.00	0.00	24.0
15	25	-4723	-737	1767	0	479	-1651	15.71	15.71	9.42	9.42	2	0.06	0.02	0.12	0.00	0.00	24.0
16	25	-5583	-504	1888	0	336	-1019	15.71	15.71	9.42	9.42	2	0.04	0.03	0.13	0.00	0.00	24.0
17	25	-5491	-601	1598	0	431	-1188	15.71	15.71	9.42	9.42	2	0.04	0.02	0.11	0.00	0.00	24.0
18	25	2406	-2258	5956	0	1421	-8109	15.71	15.71	9.42	9.42	3	0.17	0.08	0.42	0.00	0.00	24.0
19	25	-9921	-1076	3299	0	709	-1598	15.71	15.71	9.42	9.42	3	0.04	0.05	0.21	0.00	0.00	24.0
20	25	-4121	-1615	4061	0	1062	-4523	15.71	15.71	9.42	9.42	3	0.10	0.06	0.28	0.00	0.00	24.0
37	25	5537	-2369	6107	0	1483	-9258	15.71	15.71	9.42	9.42	3	0.20	0.09	0.43	0.00	0.00	24.0
38	25	-15010	-399	1679	0	297	1594	15.71	15.71	9.42	9.42	3	0.03	0.02	0.10	0.00	0.00	24.0
39	25	-5341	-1297	2948	0	885	-3282	15.71	15.71	9.42	9.42	3	0.07	0.04	0.20	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-6568	-807	2375	0	233	-1836	15.71	15.71	9.42	9.42	3	0.04	0.03	0.16	0.00	0.00	24.0
2	38	-3785	-833	2152	0	204	-2185	15.71	15.71	9.42	9.42	2	0.06	0.03	0.15	0.00	0.00	24.0
3	38	-3758	-862	2065	0	244	-2239	15.71	15.71	9.42	9.42	2	0.07	0.03	0.14	0.00	0.00	24.0
4	38	-6347	-380	1589	0	115	-586	15.71	15.71	9.42	9.42	2	0.02	0.02	0.11	0.00	0.00	24.0
5	38	-6320	-408	1502	0	154	-640	15.71	15.71	9.42	9.42	2	0.02	0.02	0.10	0.00	0.00	24.0
6	38	-4714	-640	2056	0	127	-1562	15.71	15.71	9.42	9.42	2	0.04	0.03	0.14	0.00	0.00	24.0
7	38	-4623	-737	1767	0	258	-1743	15.71	15.71	9.42	9.42	2	0.05	0.02	0.12	0.00	0.00	24.0
8	38	-5483	-504	1888	0	100	-1082	15.71	15.71	9.42	9.42	2	0.03	0.03	0.13	0.00	0.00	24.0
9	38	-5391	-601	1598	0	232	-1263	15.71	15.71	9.42	9.42	2	0.04	0.02	0.11	0.00	0.00	24.0
10	38	-3785	-833	2152	0	204	-2185	15.71	15.71	9.42	9.42	2	0.06	0.03	0.15	0.00	0.00	24.0
11	38	-3758	-862	2065	0	244	-2239	15.71	15.71	9.42	9.42	2	0.07	0.03	0.14	0.00	0.00	24.0
12	38	-6347	-380	1589	0	115	-586	15.71	15.71	9.42	9.42	2	0.02	0.02	0.11	0.00	0.00	24.0
13	38	-6320	-408	1502	0	154	-640	15.71	15.71	9.42	9.42	2	0.02	0.02	0.10	0.00	0.00	24.0
14	38	-4714	-640	2056	0	127	-1562	15.71	15.71	9.42	9.42	2	0.04	0.03	0.14	0.00	0.00	24.0
15	38	-4623	-737	1767	0	258	-1743	15.71	15.71	9.42	9.42	2	0.05	0.02	0.12	0.00	0.00	24.0
16	38	-5483	-504	1888	0	100	-1082	15.71	15.71	9.42	9.42	2	0.03	0.03	0.13	0.00	0.00	24.0
17	38	-5391	-601	1598	0	232	-1263	15.71	15.71	9.42	9.42	2	0.04	0.02	0.11	0.00	0.00	24.0
18	38	2536	-2258	5956	0	676	-8391	15.71	15.71	9.42	9.42	3	0.17	0.08	0.42	0.00	0.00	24.0
19	38	-9792	-1076	3299	0	297	-1732	15.71	15.71	9.42	9.42	3	0.03	0.05	0.21	0.00	0.00	24.0
20	38	-3991	-1615	4061	0	554	-4725	15.71	15.71	9.42	9.42	3	0.09	0.06	0.28	0.00	0.00	24.0
37	38	5667	-2369	6107	0	720	-9554	15.71	15.71	9.42	9.42	3	0.20	0.09	0.43	0.00	0.00	24.0
38	38	-14880	-399	1679	0	87	1544	15.71	15.71	9.42	9.42	3	0.03	0.02	0.10	0.00	0.00	24.0
39	38	-5211	-1297	2948	0	516	-3444	15.71	15.71	9.42	9.42	3	0.07	0.04	0.20	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-6438	-807	2375	0	-64	-1937	15.71	15.71	9.42	9.42	3	0.04	0.03	0.16	0.00	0.00	24.0
2	50	-3685	-833	2152	0	-65	-2289	15.71	15.71	9.42	9.42	2	0.06	0.03	0.15	0.00	0.00	24.0
3	50	-3658	-862	2065	0	-15	-2347	15.71	15.71	9.42	9.42	2	0.06	0.03	0.14	0.00	0.00	24.0
4	50	-6247	-380	1589	0	-84	-633	15.71	15.71	9.42	9.42	2	0.02	0.02	0.11	0.00	0.00	24.0
5	50	-6220	-408	1502	0	-33	-691	15.71	15.71	9.42	9.42	2	0.02	0.02	0.10	0.00	0.00	24.0
6	50	-4614	-640	2056	0	-130	-1642	15.71	15.71	9.42	9.42	2	0.05	0.03	0.14	0.00	0.00	24.0
7	50	-4523	-737	1767	0	38	-1835	15.71	15.71	9.42	9.42	2	0.05	0.02	0.12	0.00	0.00	24.0
8	50	-5383	-504	1888	0	-136	-1145	15.71	15.71	9.42	9.42	2	0.03	0.03	0.13	0.00	0.00	24.0
9	50	-5291	-601	1598	0	32	-1338	15.71	15.71	9.42	9.42	2	0.04	0.02	0.11	0.00	0.00	24.0
10	50	-3685	-833	2152	0	-65	-2289	15.71	15.71	9.42	9.42	2	0.06	0.03	0.15	0.00	0.00	24.0
11	50	-3658	-862	2065	0	-15	-2347	15.71	15.71	9.42	9.42	2	0.06	0.03	0.14	0.00	0.00	24.0
12	50	-6247	-380	1589	0	-84	-633	15.71	15.71	9.42	9.42	2	0.02	0.02	0.11	0.00	0.00	24.0
13	50	-6220	-408	1502	0	-33	-691	15.71	15.71	9.42	9.42	2	0.02	0.02	0.10	0.00	0.00	24.0
14	50	-4614	-640	2056	0	-130	-1642	15.71	15.71	9.42	9.42	2	0.05	0.03	0.14	0.00	0.00	24.0
15	50	-4523	-737	1767	0	38	-1835	15.71	15.71	9.42	9.42	2	0.05	0.02	0.12	0.00	0.00	24.0
16	50	-5383	-504	1888	0	-136	-1145	15.71	15.71	9.42	9.42	2	0.03	0.03	0.13	0.00	0.00	24.0
17	50	-5291	-601	1598	0	32	-1338	15.71	15.71	9.42	9.42	2	0.04	0.02	0.11	0.00	0.00	24.0
18	50	2666	-2258	5956	0	-68	-8673	15.71	15.71	9.42	9.42	3	0.17	0.08	0.42	0.00	0.00	24.0
19	50	-9662	-1076	3299	0	-116	-1867	15.71	15.71	9.42	9.42	3	0.04	0.05	0.22	0.00	0.00	24.0
20	50	-3861	-1615	4061	0	47	-4927	15.71	15.71	9.42	9.42	3	0.09	0.06	0.28	0.00	0.00	24.0
37	50	5797	-2369	6107	0	-44	-9850	15.71	15.71	9.42	9.42	3	0.20	0.09	0.43	0.00	0.00	24.0
38	50	-14750	-399	1679	0	-122	1494	15.71	15.71	9.42	9.42	3	0.03	0.02	0.10	0.00	0.00	24.0
39	50	-5081	-1297	2948	0	148	-3606	15.71	15.71	9.42	9.42	3	0.07	0.04	0.20	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 78 NI 1665 NF 91 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 30A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-6363	-2026	209	0	-67	-7473	15.71	15.71	9.42	9.42	3	0.14	0.03	0.18	0.00	0.00	24.0
2	0	-3573	-1824	286	0	-80	-6762	15.71	15.71	9.42	9.42	2	0.18	0.02	0.16	0.00	0.00	24.0
3	0	-3578	-1835	-22	0	-25	-6774	15.71	15.71	9.42	9.42	2	0.18	0.02	0.16	0.00	0.00	24.0
4	0	-6212	-1282	344	0	-77	-4724	15.71	15.71	9.42	9.42	2	0.13	0.02	0.11	0.00	0.00	24.0
5	0	-6217	-1292	35	0	-22	-4736	15.71	15.71	9.42	9.42	2	0.12	0.02	0.11	0.00	0.00	24.0
6	0	-4490	-1623	666	0	-144	-6035	15.71	15.71	9.42	9.42	2	0.16	0.02	0.14	0.00	0.00	24.0
7	0	-4508	-1656	-362	0	40	-6074	15.71	15.71	9.42	9.42	2	0.16	0.02	0.15	0.00	0.00	24.0
8	0	-5282	-1460	683	0	-143	-5424	15.71	15.71	9.42	9.42	2	0.15	0.02	0.13	0.00	0.00	24.0
9	0	-5300	-1494	-344	0	41	-5463	15.71	15.71	9.42	9.42	2	0.14	0.02	0.13	0.00	0.00	24.0
10	0	-3573	-1824	286	0	-80	-6762	15.71	15.71	9.42	9.42	2	0.18	0.02	0.16	0.00	0.00	24.0
11	0	-3578	-1835	-22	0	-25	-6774	15.71	15.71	9.42	9.42	2	0.18	0.02	0.16	0.00	0.00	24.0
12	0	-6212	-1282	344	0	-77	-4724	15.71	15.71	9.42	9.42	2	0.13	0.02	0.11	0.00	0.00	24.0
13	0	-6217	-1292	35	0	-22	-4736	15.71	15.71	9.42	9.42	2	0.12	0.02	0.11	0.00	0.00	24.0
14	0	-4490	-1623	666	0	-144	-6035	15.71	15.71	9.42	9.42	2	0.16	0.02	0.14	0.00	0.00	24.0

15	0	-4508	-1656	-362	0	40	-6074	15.71	15.71	9.42	9.42	2	0.16	0.02	0.15	0.00	0.00	24.0
16	0	-5282	-1460	683	0	-143	-5424	15.71	15.71	9.42	9.42	2	0.15	0.02	0.13	0.00	0.00	24.0
17	0	-5300	-1494	-344	0	41	-5463	15.71	15.71	9.42	9.42	2	0.14	0.02	0.13	0.00	0.00	24.0
18	0	5399	-4707	439	0	-158	-19310	15.71	15.71	9.42	9.42	3	0.38	0.06	0.44	0.00	0.00	24.0
19	0	-7824	-3448	503	0	-124	-10820	15.71	15.71	9.42	9.42	3	0.20	0.04	0.29	0.00	0.00	24.0
20	0	-1861	-3811	-533	0	44	-14030	15.71	15.71	9.42	9.42	3	0.27	0.05	0.35	0.00	0.00	24.0
37	0	8098	-4457	328	0	-144	-19660	15.71	15.71	9.42	9.42	3	0.40	0.06	0.42	0.00	0.00	24.0
38	0	-13940	-2359	435	0	-88	-5506	15.71	15.71	9.42	9.42	3	0.10	0.03	0.19	0.00	0.00	24.0
39	0	-4002	-2964	-1293	0	193	-10850	15.71	15.71	9.42	9.42	3	0.21	0.04	0.26	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-6233	-2026	209	0	-93	-7726	15.71	15.71	9.42	9.42	3	0.14	0.03	0.18	0.00	0.00	24.0
2	12	-3473	-1824	286	0	-116	-6990	15.71	15.71	9.42	9.42	2	0.19	0.02	0.16	0.00	0.00	24.0
3	12	-3478	-1835	-22	0	-22	-7003	15.71	15.71	9.42	9.42	2	0.19	0.02	0.16	0.00	0.00	24.0
4	12	-6112	-1282	344	0	-120	-4884	15.71	15.71	9.42	9.42	2	0.13	0.02	0.11	0.00	0.00	24.0
5	12	-6117	-1292	35	0	-27	-4898	15.71	15.71	9.42	9.42	2	0.13	0.02	0.11	0.00	0.00	24.0
6	12	-4390	-1623	666	0	-227	-6238	15.71	15.71	9.42	9.42	2	0.17	0.02	0.14	0.00	0.00	24.0
7	12	-4408	-1656	-362	0	85	-6281	15.71	15.71	9.42	9.42	2	0.17	0.02	0.15	0.00	0.00	24.0
8	12	-5182	-1460	683	0	-228	-5606	15.71	15.71	9.42	9.42	2	0.15	0.02	0.13	0.00	0.00	24.0
9	12	-5200	-1494	-344	0	84	-5650	15.71	15.71	9.42	9.42	2	0.15	0.02	0.13	0.00	0.00	24.0
10	12	-3473	-1824	286	0	-116	-6990	15.71	15.71	9.42	9.42	2	0.19	0.02	0.16	0.00	0.00	24.0
11	12	-3478	-1835	-22	0	-22	-7003	15.71	15.71	9.42	9.42	2	0.19	0.02	0.16	0.00	0.00	24.0
12	12	-6112	-1282	344	0	-120	-4884	15.71	15.71	9.42	9.42	2	0.13	0.02	0.11	0.00	0.00	24.0
13	12	-6117	-1292	35	0	-27	-4898	15.71	15.71	9.42	9.42	2	0.13	0.02	0.11	0.00	0.00	24.0
14	12	-4390	-1623	666	0	-227	-6238	15.71	15.71	9.42	9.42	2	0.17	0.02	0.14	0.00	0.00	24.0
15	12	-4408	-1656	-362	0	85	-6281	15.71	15.71	9.42	9.42	2	0.17	0.02	0.15	0.00	0.00	24.0
16	12	-5182	-1460	683	0	-228	-5606	15.71	15.71	9.42	9.42	2	0.15	0.02	0.13	0.00	0.00	24.0
17	12	-5200	-1494	-344	0	84	-5650	15.71	15.71	9.42	9.42	2	0.15	0.02	0.13	0.00	0.00	24.0
18	12	5529	-4707	439	0	-213	-19900	15.71	15.71	9.42	9.42	3	0.40	0.06	0.44	0.00	0.00	24.0
19	12	-7694	-3448	503	0	-187	-11250	15.71	15.71	9.42	9.42	3	0.21	0.04	0.29	0.00	0.00	24.0
20	12	-1731	-3811	-533	0	111	-14505	15.71	15.71	9.42	9.42	3	0.28	0.05	0.35	0.00	0.00	24.0
37	12	8228	-4457	328	0	-186	-20218	15.71	15.71	9.42	9.42	3	0.41	0.06	0.42	0.00	0.00	24.0
38	12	-13810	-2359	435	0	-142	-5801	15.71	15.71	9.42	9.42	3	0.11	0.03	0.19	0.00	0.00	24.0
39	12	-3872	-2964	-1293	0	354	-11223	15.71	15.71	9.42	9.42	3	0.21	0.04	0.26	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-6103	-2026	209	0	-119	-7980	15.71	15.71	9.42	9.42	3	0.15	0.03	0.18	0.00	0.00	24.0
2	25	-3373	-1824	286	0	-152	-7218	15.71	15.71	9.42	9.42	2	0.20	0.02	0.16	0.00	0.00	24.0
3	25	-3378	-1835	-22	0	-20	-7232	15.71	15.71	9.42	9.42	2	0.19	0.02	0.16	0.00	0.00	24.0
4	25	-6012	-1282	344	0	-163	-5044	15.71	15.71	9.42	9.42	2	0.14	0.02	0.11	0.00	0.00	24.0
5	25	-6017	-1292	35	0	-31	-5059	15.71	15.71	9.42	9.42	2	0.13	0.02	0.11	0.00	0.00	24.0
6	25	-4290	-1623	666	0	-310	-6440	15.71	15.71	9.42	9.42	2	0.18	0.02	0.14	0.00	0.00	24.0
7	25	-4308	-1656	-362	0	131	-6488	15.71	15.71	9.42	9.42	2	0.17	0.02	0.15	0.00	0.00	24.0
8	25	-5082	-1460	683	0	-313	-5789	15.71	15.71	9.42	9.42	2	0.16	0.02	0.13	0.00	0.00	24.0
9	25	-5100	-1494	-344	0	127	-5836	15.71	15.71	9.42	9.42	2	0.16	0.02	0.13	0.00	0.00	24.0
10	25	-3373	-1824	286	0	-152	-7218	15.71	15.71	9.42	9.42	2	0.20	0.02	0.16	0.00	0.00	24.0
11	25	-3378	-1835	-22	0	-20	-7232	15.71	15.71	9.42	9.42	2	0.19	0.02	0.16	0.00	0.00	24.0
12	25	-6012	-1282	344	0	-163	-5044	15.71	15.71	9.42	9.42	2	0.14	0.02	0.11	0.00	0.00	24.0
13	25	-6017	-1292	35	0	-31	-5059	15.71	15.71	9.42	9.42	2	0.13	0.02	0.11	0.00	0.00	24.0
14	25	-4290	-1623	666	0	-310	-6440	15.71	15.71	9.42	9.42	2	0.18	0.02	0.14	0.00	0.00	24.0
15	25	-4308	-1656	-362	0	131	-6488	15.71	15.71	9.42	9.42	2	0.17	0.02	0.15	0.00	0.00	24.0
16	25	-5082	-1460	683	0	-313	-5789	15.71	15.71	9.42	9.42	2	0.16	0.02	0.13	0.00	0.00	24.0
17	25	-5100	-1494	-344	0	127	-5836	15.71	15.71	9.42	9.42	2	0.16	0.02	0.13	0.00	0.00	24.0
18	25	5659	-4707	439	0	-268	-20490	15.71	15.71	9.42	9.42	3	0.41	0.06	0.44	0.00	0.00	24.0
19	25	-7564	-3448	503	0	-250	-11680	15.71	15.71	9.42	9.42	3	0.22	0.04	0.29	0.00	0.00	24.0
20	25	-1601	-3811	-533	0	177	-14980	15.71	15.71	9.42	9.42	3	0.29	0.05	0.35	0.00	0.00	24.0
37	25	8358	-4457	328	0	-226	-20775	15.71	15.71	9.42	9.42	3	0.42	0.06	0.42	0.00	0.00	24.0
38	25	-13680	-2359	435	0	-196	-6096	15.71	15.71	9.42	9.42	3	0.11	0.03	0.19	0.00	0.00	24.0
39	25	-3742	-2964	-1293	0	516	-11595	15.71	15.71	9.42	9.42	3	0.22	0.04	0.26	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-5973	-2026	209	0	-145	-8233	15.71	15.71	9.42	9.42	3	0.15	0.03	0.18	0.00	0.00	24.0
2	38	-3273	-1824	286	0	-188	-7446	15.71	15.71	9.42	9.42	2	0.20	0.02	0.16	0.00	0.00	24.0
3	38	-3278	-1835	-22	0	-17	-7462	15.71	15.71	9.42	9.42	2	0.20	0.02	0.16	0.00	0.00	24.0
4	38	-5912	-1282	344	0	-206	-5205	15.71	15.71	9.42	9.42	2	0.14	0.02	0.11	0.00	0.00	24.0
5	38	-5917	-1292	35	0	-35	-5221	15.71	15.71	9.42	9.42	2	0.14	0.02	0.11	0.00	0.00	24.0
6	38	-4190	-1623	666	0	-393	-6643	15.71	15.71	9.42	9.42	2	0.19	0.02	0.14	0.00	0.00	24.0
7	38	-4208	-1656	-362	0	176	-6695	15.71	15.71	9.42	9.42	2	0.18	0.02	0.15	0.00	0.00	24.0
8	38	-4982	-1460	683	0	-399	-5972	15.71	15.71	9.42	9.42	2	0.17	0.02	0.13	0.00	0.00	24.0
9	38	-5000	-1494	-344	0	170	-6023	15.71	15.71	9.42	9.42	2	0.16	0.02	0.13	0.00	0.00	24.0
10	38	-3273	-1824	286	0	-188	-7446	15.71	15.71	9.42	9.42	2	0.20	0.02	0.16	0.00	0.00	24.0
11	38	-3278	-1835	-22	0	-17	-7462	15.71	15.71	9.42	9.42	2	0.20	0.02	0.16	0.00	0.00	24.0
12	38	-5912	-1282	344	0	-206	-5205	15.71	15.71	9.42	9.42	2	0.14	0.02	0.11	0.00	0.00	24.0
13	38	-5917	-1292	35	0	-35	-5221	15.71	15.71	9.42	9.42	2	0.14	0.02	0.11	0.00	0.00	24.0
14	38	-4190	-1623	666	0	-393	-6643	15.71	15.71	9.42	9.42	2	0.19	0.02	0.14	0.00	0.00	24.0
15	38	-4208	-1656	-362	0	176	-6695	15.71	15.71	9.42	9.42	2	0.18	0.02	0.15	0.00	0.00	24.0
16	38	-4982	-1460	683	0	-399	-5972	15.71	15.71	9.42	9.42	2	0.17	0.02	0.13	0.00	0.00	24.0
17	38	-5000	-1494	-344	0	170	-6023	15.71	15.71	9.42	9.42	2	0.16	0.02	0.13	0.00	0.00	24.0
18	38	5789	-4707	439	0	-323	-21080	15.71	15.71	9.42	9.42	3	0.42	0.06	0.44	0.00	0.00	24.0
19	38	-7434	-3448	503	0	-313	-12110	15.71	15.71	9.42	9.42	3	0.23	0.04	0.29	0.00	0.00	24.0
20	38	-1471	-3811	-533	0	244	-15455	15.71	15.71	9.42	9.42	3	0.30	0.05	0.35	0.00	0.00	24.0
37	38	8488	-4457	328	0	-268	-21332	15.71	15.71	9.42	9.42	3	0.43	0.06	0.42	0.00	0.00	24.0
38	38	-13550	-2359	435	0	-251	-6391	15.71	15.71	9.42	9.42	3	0.12	0.03	0.19	0.00	0.00	24.0
39	38	-3612	-2964	-1293	0	677	-11967	15.71	15.71	9.42	9.42	3	0.23	0.04	0.27	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-5843	-2026	209	0	-171	-8486	15.71	15.71	9.42	9.42	3	0.16	0.03	0.18	0.00	0.00	24.0
2	50	-3173	-1824	286	0	-223	-7674	15.71	15.71	9.42	9.42	2	0.21	0.02	0.16	0.00	0.00	24.0
3	50	-3178	-1835	-22	0	-14	-7691	15.71	15.71	9.42	9.42	2	0.21	0.02	0.17	0.00	0.00	24.0
4	50	-5812	-1282	344	0	-249	-5365	15.71	15.71	9.42	9.42	2	0.15	0.02	0.11	0.00	0.00	24.0
5	50	-5817	-1292	35	0	-40	-5382	15.71	15.71	9.42	9.42	2	0.14	0.02	0.11	0.00	0.00	24.0
6	50	-4090	-1623	666	0	-476	-6846	15.71	15.71	9.42	9.42	2	0.19	0.02	0.14	0.00	0.00	24.0
7	50	-4108	-1656	-362	0	221	-6902	15.71	15.71	9.42	9.42	2	0.19	0.02	0.15	0.00	0.00	24.0
8	50	-4882	-1460	683	0	-484	-6154	15.71	15.71	9.42	9.42	2	0.17	0.02	0.13	0.00	0.00	24.0
9	50	-4900	-1494	-344	0	213	-6210	15.71	15.71	9.42	9.42	2	0.17	0.02	0.13	0.00	0.00	24.0
10	50	-3173	-1824	286	0	-223	-7674	15.71	15.71	9.42	9.42	2	0.21	0.02	0.16	0.00	0.00	24.0
11	50	-3178	-1835	-22	0	-14	-7691	15.71	15.71	9.42	9.42	2	0.21	0.02	0.17	0.00	0.00	24.0
12	50	-5812	-1282	344	0	-249	-5365	15.71	15.71	9.42	9.42	2	0.15	0.02	0.11	0.00	0.00	24.0
13	50	-5817	-1292	35	0	-40	-5382	15.71	15.71	9.42	9.42	2	0.14	0.02	0.11	0.00	0.00	24.0
14	50	-4090	-1623	666	0	-476	-6846	15.71	15.71	9.42	9.42	2	0.19	0.02	0.14	0.00	0.00	24.0
15	50	-4108	-1656	-362	0	221	-6902	15.71	15.71	9.42	9.42	2	0.19	0.02	0.15	0.00	0.00	24.0
16	50	-4882	-1460	683	0	-484	-6154	15.71	15.71	9.42	9.42	2	0.17	0.02	0.13	0.00	0.00	24.0
17	50	-4900	-1494	-344	0	213	-6210	15.71	15.71	9.42	9.42	2	0.17	0.02	0.13	0.00	0.00	24.0
18	50	5919	-4707	439	0	-378	-21670	15.71	15.71	9.42	9.42	3	0.43	0.06	0.44	0.00	0.00	24.0
19	50	-7304	-3448	503	0	-376	-12540	15.71	15.71	9.42	9.42	3	0.24	0.04	0.29	0.00	0.00	24.0
20	50	-1341	-3811	-533	0	311	-15930	15.71	15.71	9.42	9.42	3	0.31	0.05	0.35	0.00	0.00	24.0

37	50	8618	-4457	328	0	-308	-21890	15.71	15.71	9.42	9.42	3	0.44	0.06	0.42	0.00	0.00	24.0
38	50	-13420	-2359	435	0	-305	-6686	15.71	15.71	9.42	9.42	3	0.12	0.03	0.19	0.00	0.00	24.0
39	50	-3482	-2964	-1293	0	839	-12340	15.71	15.71	9.42	9.42	3	0.24	0.04	0.27	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 79 NI 1683 NF 134 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 29A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-5666	-2083	542	0	-88	-8034	15.71	15.71	9.42	9.42	3	0.15	0.03	0.18	0.00	0.00	24.0
2	0	-2849	-1891	566	0	-94	-7324	15.71	15.71	9.42	9.42	2	0.20	0.02	0.17	0.00	0.00	24.0
3	0	-2919	-1867	265	0	-40	-7254	15.71	15.71	9.42	9.42	2	0.19	0.02	0.17	0.00	0.00	24.0
4	0	-5799	-1338	569	0	-94	-5105	15.71	15.71	9.42	9.42	2	0.14	0.02	0.12	0.00	0.00	24.0
5	0	-5868	-1314	269	0	-41	-5035	15.71	15.71	9.42	9.42	2	0.13	0.02	0.11	0.00	0.00	24.0
6	0	-3801	-1725	918	0	-157	-6628	15.71	15.71	9.42	9.42	2	0.18	0.02	0.15	0.00	0.00	24.0
7	0	-4032	-1646	-84	0	22	-6397	15.71	15.71	9.42	9.42	2	0.17	0.02	0.15	0.00	0.00	24.0
8	0	-4686	-1559	919	0	-157	-5963	15.71	15.71	9.42	9.42	2	0.16	0.02	0.14	0.00	0.00	24.0
9	0	-4916	-1480	-83	0	22	-5731	15.71	15.71	9.42	9.42	2	0.15	0.02	0.13	0.00	0.00	24.0
10	0	-2849	-1891	566	0	-94	-7324	15.71	15.71	9.42	9.42	2	0.20	0.02	0.17	0.00	0.00	24.0
11	0	-2919	-1867	265	0	-40	-7254	15.71	15.71	9.42	9.42	2	0.19	0.02	0.17	0.00	0.00	24.0
12	0	-5799	-1338	569	0	-94	-5105	15.71	15.71	9.42	9.42	2	0.14	0.02	0.12	0.00	0.00	24.0
13	0	-5868	-1314	269	0	-41	-5035	15.71	15.71	9.42	9.42	2	0.13	0.02	0.11	0.00	0.00	24.0
14	0	-3801	-1725	918	0	-157	-6628	15.71	15.71	9.42	9.42	2	0.18	0.02	0.15	0.00	0.00	24.0
15	0	-4032	-1646	-84	0	22	-6397	15.71	15.71	9.42	9.42	2	0.17	0.02	0.15	0.00	0.00	24.0
16	0	-4686	-1559	919	0	-157	-5963	15.71	15.71	9.42	9.42	2	0.16	0.02	0.14	0.00	0.00	24.0
17	0	-4916	-1480	-83	0	22	-5731	15.71	15.71	9.42	9.42	2	0.15	0.02	0.13	0.00	0.00	24.0
18	0	7305	-4839	1133	0	-186	-20710	15.71	15.71	9.42	9.42	3	0.42	0.06	0.45	0.00	0.00	24.0
19	0	-6958	-3563	976	0	-159	-11610	15.71	15.71	9.42	9.42	3	0.22	0.05	0.31	0.00	0.00	24.0
20	0	-810	-3835	119	0	-5	-14800	15.71	15.71	9.42	9.42	3	0.28	0.05	0.36	0.00	0.00	24.0
37	0	10130	-4573	1014	0	-167	-21100	15.71	15.71	9.42	9.42	3	0.43	0.06	0.43	0.00	0.00	24.0
38	0	-13650	-2447	753	0	-121	-5917	15.71	15.71	9.42	9.42	3	0.11	0.03	0.19	0.00	0.00	24.0
39	0	-3398	-2900	-676	0	135	-11240	15.71	15.71	9.42	9.42	3	0.21	0.04	0.26	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-5536	-2083	542	0	-155	-8294	15.71	15.71	9.42	9.42	3	0.16	0.03	0.18	0.00	0.00	24.0
2	12	-2749	-1891	566	0	-165	-7560	15.71	15.71	9.42	9.42	2	0.21	0.02	0.17	0.00	0.00	24.0
3	12	-2819	-1867	265	0	-74	-7487	15.71	15.71	9.42	9.42	2	0.20	0.02	0.17	0.00	0.00	24.0
4	12	-5699	-1338	569	0	-166	-5272	15.71	15.71	9.42	9.42	2	0.14	0.02	0.12	0.00	0.00	24.0
5	12	-5768	-1314	269	0	-74	-5199	15.71	15.71	9.42	9.42	2	0.14	0.02	0.11	0.00	0.00	24.0
6	12	-3701	-1725	918	0	-272	-6844	15.71	15.71	9.42	9.42	2	0.19	0.02	0.15	0.00	0.00	24.0
7	12	-3932	-1646	-84	0	33	-6603	15.71	15.71	9.42	9.42	2	0.18	0.02	0.15	0.00	0.00	24.0
8	12	-4586	-1559	919	0	-272	-6158	15.71	15.71	9.42	9.42	2	0.17	0.02	0.14	0.00	0.00	24.0
9	12	-4816	-1480	-83	0	33	-5916	15.71	15.71	9.42	9.42	2	0.16	0.02	0.13	0.00	0.00	24.0
10	12	-2749	-1891	566	0	-165	-7560	15.71	15.71	9.42	9.42	2	0.21	0.02	0.17	0.00	0.00	24.0
11	12	-2819	-1867	265	0	-74	-7487	15.71	15.71	9.42	9.42	2	0.20	0.02	0.17	0.00	0.00	24.0
12	12	-5699	-1338	569	0	-166	-5272	15.71	15.71	9.42	9.42	2	0.14	0.02	0.12	0.00	0.00	24.0
13	12	-5768	-1314	269	0	-74	-5199	15.71	15.71	9.42	9.42	2	0.14	0.02	0.11	0.00	0.00	24.0
14	12	-3701	-1725	918	0	-272	-6844	15.71	15.71	9.42	9.42	2	0.19	0.02	0.15	0.00	0.00	24.0
15	12	-3932	-1646	-84	0	33	-6603	15.71	15.71	9.42	9.42	2	0.18	0.02	0.15	0.00	0.00	24.0
16	12	-4586	-1559	919	0	-272	-6158	15.71	15.71	9.42	9.42	2	0.17	0.02	0.14	0.00	0.00	24.0
17	12	-4816	-1480	-83	0	33	-5916	15.71	15.71	9.42	9.42	2	0.16	0.02	0.13	0.00	0.00	24.0
18	12	7435	-4839	1133	0	-328	-21315	15.71	15.71	9.42	9.42	3	0.43	0.06	0.45	0.00	0.00	24.0
19	12	-6828	-3563	976	0	-281	-12055	15.71	15.71	9.42	9.42	3	0.23	0.05	0.31	0.00	0.00	24.0
20	12	-680	-3835	119	0	-20	-15280	15.71	15.71	9.42	9.42	3	0.29	0.05	0.36	0.00	0.00	24.0
37	12	10260	-4573	1014	0	-294	-21670	15.71	15.71	9.42	9.42	3	0.44	0.06	0.43	0.00	0.00	24.0
38	12	-13520	-2447	753	0	-215	-6223	15.71	15.71	9.42	9.42	3	0.11	0.03	0.19	0.00	0.00	24.0
39	12	-3268	-2900	-676	0	220	-11602	15.71	15.71	9.42	9.42	3	0.22	0.04	0.26	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-5406	-2083	542	0	-223	-8554	15.71	15.71	9.42	9.42	3	0.16	0.03	0.18	0.00	0.00	24.0
2	25	-2649	-1891	566	0	-236	-7796	15.71	15.71	9.42	9.42	2	0.21	0.02	0.17	0.00	0.00	24.0
3	25	-2719	-1867	265	0	-107	-7721	15.71	15.71	9.42	9.42	2	0.21	0.02	0.17	0.00	0.00	24.0
4	25	-5599	-1338	569	0	-237	-5440	15.71	15.71	9.42	9.42	2	0.15	0.02	0.12	0.00	0.00	24.0
5	25	-5668	-1314	269	0	-108	-5363	15.71	15.71	9.42	9.42	2	0.14	0.02	0.11	0.00	0.00	24.0
6	25	-3601	-1725	918	0	-386	-7060	15.71	15.71	9.42	9.42	2	0.20	0.02	0.15	0.00	0.00	24.0
7	25	-3832	-1646	-84	0	43	-6808	15.71	15.71	9.42	9.42	2	0.18	0.02	0.15	0.00	0.00	24.0
8	25	-4486	-1559	919	0	-387	-6352	15.71	15.71	9.42	9.42	2	0.18	0.02	0.14	0.00	0.00	24.0
9	25	-4716	-1480	-83	0	43	-6101	15.71	15.71	9.42	9.42	2	0.16	0.02	0.13	0.00	0.00	24.0
10	25	-2649	-1891	566	0	-236	-7796	15.71	15.71	9.42	9.42	2	0.21	0.02	0.17	0.00	0.00	24.0
11	25	-2719	-1867	265	0	-107	-7721	15.71	15.71	9.42	9.42	2	0.21	0.02	0.17	0.00	0.00	24.0
12	25	-5599	-1338	569	0	-237	-5440	15.71	15.71	9.42	9.42	2	0.15	0.02	0.12	0.00	0.00	24.0
13	25	-5668	-1314	269	0	-108	-5363	15.71	15.71	9.42	9.42	2	0.14	0.02	0.11	0.00	0.00	24.0
14	25	-3601	-1725	918	0	-386	-7060	15.71	15.71	9.42	9.42	2	0.20	0.02	0.15	0.00	0.00	24.0
15	25	-3832	-1646	-84	0	43	-6808	15.71	15.71	9.42	9.42	2	0.18	0.02	0.15	0.00	0.00	24.0
16	25	-4486	-1559	919	0	-387	-6352	15.71	15.71	9.42	9.42	2	0.18	0.02	0.14	0.00	0.00	24.0
17	25	-4716	-1480	-83	0	43	-6101	15.71	15.71	9.42	9.42	2	0.16	0.02	0.13	0.00	0.00	24.0
18	25	7565	-4839	1133	0	-470	-21920	15.71	15.71	9.42	9.42	3	0.44	0.06	0.45	0.00	0.00	24.0
19	25	-6698	-3563	976	0	-403	-12500	15.71	15.71	9.42	9.42	3	0.24	0.05	0.31	0.00	0.00	24.0
20	25	-550	-3835	119	0	-35	-15760	15.71	15.71	9.42	9.42	3	0.30	0.05	0.36	0.00	0.00	24.0
37	25	10390	-4573	1014	0	-421	-22240	15.71	15.71	9.42	9.42	3	0.46	0.06	0.43	0.00	0.00	24.0
38	25	-13390	-2447	753	0	-309	-6529	15.71	15.71	9.42	9.42	3	0.12	0.03	0.19	0.00	0.00	24.0
39	25	-3138	-2900	-676	0	304	-11965	15.71	15.71	9.42	9.42	3	0.23	0.04	0.26	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-5276	-2083	542	0	-291	-8815	15.71	15.71	9.42	9.42	3	0.17	0.03	0.18	0.00	0.00	24.0
2	38	-2549	-1891	566	0	-306	-8033	15.71	15.71	9.42	9.42	2	0.22	0.02	0.17	0.00	0.00	24.0
3	38	-2619	-1867	265	0	-140	-7954	15.71	15.71	9.42	9.42	2	0.22	0.02	0.17	0.00	0.00	24.0
4	38	-5499	-1338	569	0	-308	-5607	15.71	15.71	9.42	9.42	2	0.15	0.02	0.12	0.00	0.00	24.0
5	38	-5568	-1314	269	0	-141	-5528	15.71	15.71	9.42	9.42	2	0.15	0.02	0.11	0.00	0.00	24.0
6	38	-3501	-1725	918	0	-501	-7275	15.71	15.71	9.42	9.42	2	0.21	0.02	0.15	0.00	0.00	24.0
7	38	-3732	-1646	-84	0	54	-7014	15.71	15.71	9.42	9.42	2	0.19	0.02	0.15	0.00	0.00	24.0
8	38	-4386	-1559	919	0	-502	-6547	15.71	15.71	9.42	9.42	2	0.19	0.02	0.14	0.00	0.00	24.0
9	38	-4616	-1480	-83	0	53	-6286	15.71	15.71	9.42	9.42	2	0.17	0.02	0.13	0.00	0.00	24.0
10	38	-2549	-1891	566	0	-306	-8033	15.71	15.71	9.42	9.42	2	0.22	0.02	0.17	0.00	0.00	24.0
11	38	-2619	-1867	265	0	-140	-7954	15.71	15.71	9.42	9.42	2	0.22	0.02	0.17	0.00	0.00	24.0
12	38	-5499	-1338	569	0	-308	-5607	15.71	15.71	9.42	9.42	2	0.15	0.02	0.12	0.00	0.00	24.0
13	38	-5568	-1314	269	0	-141	-5528	15.71	15.71	9.42	9.42	2	0.15	0.02	0.11	0.00	0.00	24.0
14	38	-3501	-1725	918	0	-501	-7275	15.71	15.71	9.42	9.42	2	0.21	0.02	0.15	0.00	0.00	24.0
15	38	-3732	-1646	-84	0	54	-7014	15.71	15.71	9.42	9.42	2	0.19	0.02	0.15	0.00	0.00	24.0
16	38	-4386	-1559	919	0	-502	-6547	15.71	15.71	9.42	9.42	2	0.19	0.02	0.14	0.00	0.00	24.0

17	38	-4616	-1480	-83	0	53	-6286	15.71	15.71	9.42	9.42	2	0.17	0.02	0.13	0.00	0.00	24.0
18	38	7695	-4839	1133	0	-611	-22525	15.71	15.71	9.42	9.42	3	0.46	0.06	0.45	0.00	0.00	24.0
19	38	-6568	-3563	976	0	-525	-12945	15.71	15.71	9.42	9.42	3	0.24	0.05	0.31	0.00	0.00	24.0
20	38	-420	-3835	119	0	-50	-16240	15.71	15.71	9.42	9.42	3	0.31	0.05	0.36	0.00	0.00	24.0
37	38	10520	-4573	1014	0	-547	-22810	15.71	15.71	9.42	9.42	3	0.47	0.06	0.43	0.00	0.00	24.0
38	38	-13260	-2447	753	0	-403	-6834	15.71	15.71	9.42	9.42	3	0.13	0.03	0.20	0.00	0.00	24.0
39	38	-3008	-2900	-676	0	389	-12327	15.71	15.71	9.42	9.42	3	0.24	0.04	0.26	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-5146	-2083	542	0	-359	-9075	15.71	15.71	9.42	9.42	3	0.17	0.03	0.18	0.00	0.00	24.0
2	50	-2449	-1891	566	0	-377	-8269	15.71	15.71	9.42	9.42	2	0.23	0.02	0.17	0.00	0.00	24.0
3	50	-2519	-1867	265	0	-173	-8188	15.71	15.71	9.42	9.42	2	0.22	0.02	0.17	0.00	0.00	24.0
4	50	-5399	-1338	569	0	-379	-5774	15.71	15.71	9.42	9.42	2	0.16	0.02	0.12	0.00	0.00	24.0
5	50	-5468	-1314	269	0	-175	-5692	15.71	15.71	9.42	9.42	2	0.15	0.02	0.11	0.00	0.00	24.0
6	50	-3401	-1725	918	0	-616	-7491	15.71	15.71	9.42	9.42	2	0.22	0.02	0.15	0.00	0.00	24.0
7	50	-3632	-1646	-84	0	64	-7220	15.71	15.71	9.42	9.42	2	0.19	0.02	0.15	0.00	0.00	24.0
8	50	-4286	-1559	919	0	-616	-6742	15.71	15.71	9.42	9.42	2	0.19	0.02	0.14	0.00	0.00	24.0
9	50	-4516	-1480	-83	0	64	-6471	15.71	15.71	9.42	9.42	2	0.17	0.02	0.13	0.00	0.00	24.0
10	50	-2449	-1891	566	0	-377	-8269	15.71	15.71	9.42	9.42	2	0.23	0.02	0.17	0.00	0.00	24.0
11	50	-2519	-1867	265	0	-173	-8188	15.71	15.71	9.42	9.42	2	0.22	0.02	0.17	0.00	0.00	24.0
12	50	-5399	-1338	569	0	-379	-5774	15.71	15.71	9.42	9.42	2	0.16	0.02	0.12	0.00	0.00	24.0
13	50	-5468	-1314	269	0	-175	-5692	15.71	15.71	9.42	9.42	2	0.15	0.02	0.11	0.00	0.00	24.0
14	50	-3401	-1725	918	0	-616	-7491	15.71	15.71	9.42	9.42	2	0.22	0.02	0.15	0.00	0.00	24.0
15	50	-3632	-1646	-84	0	64	-7220	15.71	15.71	9.42	9.42	2	0.19	0.02	0.15	0.00	0.00	24.0
16	50	-4286	-1559	919	0	-616	-6742	15.71	15.71	9.42	9.42	2	0.19	0.02	0.14	0.00	0.00	24.0
17	50	-4516	-1480	-83	0	64	-6471	15.71	15.71	9.42	9.42	2	0.17	0.02	0.13	0.00	0.00	24.0
18	50	7825	-4839	1133	0	-753	-23130	15.71	15.71	9.42	9.42	3	0.47	0.06	0.45	0.00	0.00	24.0
19	50	-6438	-3563	976	0	-647	-13390	15.71	15.71	9.42	9.42	3	0.25	0.05	0.31	0.00	0.00	24.0
20	50	-290	-3835	119	0	-64	-16720	15.71	15.71	9.42	9.42	3	0.32	0.05	0.36	0.00	0.00	24.0
37	50	10650	-4573	1014	0	-674	-23380	15.71	15.71	9.42	9.42	3	0.48	0.06	0.43	0.00	0.00	24.0
38	50	-13130	-2447	753	0	-497	-7140	15.71	15.71	9.42	9.42	3	0.13	0.03	0.20	0.00	0.00	24.0
39	50	-2878	-2900	-676	0	473	-12690	15.71	15.71	9.42	9.42	3	0.24	0.04	0.26	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 80 NI 1691 NF 177 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 28A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-6576	-2007	723	0	-96	-7326	15.71	15.71	9.42	9.42	3	0.14	0.03	0.17	0.00	0.00	24.0
2	0	-3573	-1854	711	0	-100	-6781	15.71	15.71	9.42	9.42	2	0.18	0.02	0.17	0.00	0.00	24.0
3	0	-3577	-1856	416	0	-50	-6781	15.71	15.71	9.42	9.42	2	0.18	0.02	0.17	0.00	0.00	24.0
4	0	-6539	-1232	696	0	-97	-4490	15.71	15.71	9.42	9.42	2	0.12	0.02	0.11	0.00	0.00	24.0
5	0	-6544	-1234	401	0	-47	-4489	15.71	15.71	9.42	9.42	2	0.12	0.02	0.11	0.00	0.00	24.0
6	0	-4606	-1634	1050	0	-157	-5980	15.71	15.71	9.42	9.42	2	0.16	0.02	0.14	0.00	0.00	24.0
7	0	-4620	-1640	67	0	9	-5978	15.71	15.71	9.42	9.42	2	0.16	0.02	0.14	0.00	0.00	24.0
8	0	-5496	-1447	1045	0	-156	-5292	15.71	15.71	9.42	9.42	2	0.14	0.02	0.13	0.00	0.00	24.0
9	0	-5510	-1454	62	0	10	-5290	15.71	15.71	9.42	9.42	2	0.14	0.02	0.13	0.00	0.00	24.0
10	0	-3573	-1854	711	0	-100	-6781	15.71	15.71	9.42	9.42	2	0.18	0.02	0.17	0.00	0.00	24.0
11	0	-3577	-1856	416	0	-50	-6781	15.71	15.71	9.42	9.42	2	0.18	0.02	0.17	0.00	0.00	24.0
12	0	-6539	-1232	696	0	-97	-4490	15.71	15.71	9.42	9.42	2	0.12	0.02	0.11	0.00	0.00	24.0
13	0	-6544	-1234	401	0	-47	-4489	15.71	15.71	9.42	9.42	2	0.12	0.02	0.11	0.00	0.00	24.0
14	0	-4606	-1634	1050	0	-157	-5980	15.71	15.71	9.42	9.42	2	0.16	0.02	0.14	0.00	0.00	24.0
15	0	-4620	-1640	67	0	9	-5978	15.71	15.71	9.42	9.42	2	0.16	0.02	0.14	0.00	0.00	24.0
16	0	-5496	-1447	1045	0	-156	-5292	15.71	15.71	9.42	9.42	2	0.14	0.02	0.13	0.00	0.00	24.0
17	0	-5510	-1454	62	0	10	-5290	15.71	15.71	9.42	9.42	2	0.14	0.02	0.13	0.00	0.00	24.0
18	0	5727	-4880	1572	0	-222	-19540	15.71	15.71	9.42	9.42	3	0.39	0.06	0.46	0.00	0.00	24.0
19	0	-8526	-3338	1314	0	-180	-10270	15.71	15.71	9.42	9.42	3	0.19	0.04	0.28	0.00	0.00	24.0
20	0	-2143	-3803	540	0	-49	-13790	15.71	15.71	9.42	9.42	3	0.26	0.05	0.35	0.00	0.00	24.0
37	0	8763	-4708	1420	0	-201	-20160	15.71	15.71	9.42	9.42	3	0.41	0.06	0.44	0.00	0.00	24.0
38	0	-14990	-2137	990	0	-131	-4697	15.71	15.71	9.42	9.42	3	0.09	0.03	0.17	0.00	0.00	24.0
39	0	-4355	-2913	-300	0	87	-10560	15.71	15.71	9.42	9.42	3	0.20	0.04	0.26	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-6446	-2007	723	0	-186	-7577	15.71	15.71	9.42	9.42	3	0.14	0.03	0.17	0.00	0.00	24.0
2	12	-3473	-1854	711	0	-189	-7013	15.71	15.71	9.42	9.42	2	0.19	0.02	0.17	0.00	0.00	24.0
3	12	-3477	-1856	416	0	-102	-7013	15.71	15.71	9.42	9.42	2	0.19	0.02	0.17	0.00	0.00	24.0
4	12	-6439	-1232	696	0	-184	-4644	15.71	15.71	9.42	9.42	2	0.13	0.02	0.11	0.00	0.00	24.0
5	12	-6444	-1234	401	0	-98	-4643	15.71	15.71	9.42	9.42	2	0.12	0.02	0.11	0.00	0.00	24.0
6	12	-4506	-1634	1050	0	-288	-6184	15.71	15.71	9.42	9.42	2	0.17	0.02	0.14	0.00	0.00	24.0
7	12	-4520	-1640	67	0	1	-6183	15.71	15.71	9.42	9.42	2	0.16	0.02	0.15	0.00	0.00	24.0
8	12	-5396	-1447	1045	0	-287	-5473	15.71	15.71	9.42	9.42	2	0.15	0.02	0.13	0.00	0.00	24.0
9	12	-5410	-1454	62	0	2	-5472	15.71	15.71	9.42	9.42	2	0.14	0.02	0.13	0.00	0.00	24.0
10	12	-3473	-1854	711	0	-189	-7013	15.71	15.71	9.42	9.42	2	0.19	0.02	0.17	0.00	0.00	24.0
11	12	-3477	-1856	416	0	-102	-7013	15.71	15.71	9.42	9.42	2	0.19	0.02	0.17	0.00	0.00	24.0
12	12	-6439	-1232	696	0	-184	-4644	15.71	15.71	9.42	9.42	2	0.13	0.02	0.11	0.00	0.00	24.0
13	12	-6444	-1234	401	0	-98	-4643	15.71	15.71	9.42	9.42	2	0.12	0.02	0.11	0.00	0.00	24.0
14	12	-4506	-1634	1050	0	-288	-6184	15.71	15.71	9.42	9.42	2	0.17	0.02	0.14	0.00	0.00	24.0
15	12	-4520	-1640	67	0	1	-6183	15.71	15.71	9.42	9.42	2	0.16	0.02	0.15	0.00	0.00	24.0
16	12	-5396	-1447	1045	0	-287	-5473	15.71	15.71	9.42	9.42	2	0.15	0.02	0.13	0.00	0.00	24.0
17	12	-5410	-1454	62	0	2	-5472	15.71	15.71	9.42	9.42	2	0.14	0.02	0.13	0.00	0.00	24.0
18	12	5857	-4880	1572	0	-419	-20150	15.71	15.71	9.42	9.42	3	0.40	0.06	0.46	0.00	0.00	24.0
19	12	-8396	-3338	1314	0	-344	-10685	15.71	15.71	9.42	9.42	3	0.20	0.04	0.28	0.00	0.00	24.0
20	12	-2013	-3803	540	0	-117	-14265	15.71	15.71	9.42	9.42	3	0.27	0.05	0.35	0.00	0.00	24.0
37	12	8893	-4708	1420	0	-379	-20750	15.71	15.71	9.42	9.42	3	0.42	0.06	0.44	0.00	0.00	24.0
38	12	-14860	-2137	990	0	-254	-4964	15.71	15.71	9.42	9.42	3	0.09	0.03	0.17	0.00	0.00	24.0
39	12	-4225	-2913	-300	0	124	-10925	15.71	15.71	9.42	9.42	3	0.21	0.04	0.26	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-6316	-2007	723	0	-276	-7828	15.71	15.71	9.42	9.42	3	0.15	0.03	0.17	0.00	0.00	24.0
2	25	-3373	-1854	711	0	-278	-7244	15.71	15.71	9.42	9.42	2	0.20	0.02	0.17	0.00	0.00	24.0
3	25	-3377	-1856	416	0	-154	-7244	15.71	15.71	9.42	9.42	2	0.20	0.02	0.17	0.00	0.00	24.0
4	25	-6339	-1232	696	0	-271	-4798	15.71	15.71	9.42	9.42	2	0.13	0.02	0.11	0.00	0.00	24.0
5	25	-6344	-1234	401	0	-148	-4798	15.71	15.71	9.42	9.42	2	0.13	0.02	0.11	0.00	0.00	24.0
6	25	-4406	-1634	1050	0	-420	-6388	15.71	15.71	9.42	9.42	2	0.18	0.02	0.14	0.00	0.00	24.0
7	25	-4420	-1640	67	0	-7	-6388	15.71	15.71	9.42	9.42	2	0.17	0.02	0.15	0.00	0.00	24.0
8	25	-5296	-1447	1045	0	-418	-5654	15.71	15.71	9.42	9.42	2	0.16	0.02	0.13	0.00	0.00	24.0
9	25	-5310	-1454	62	0	-5	-5654	15.71	15.71	9.42	9.42	2	0.15	0.02	0.13	0.00	0.00	24.0
10	25	-3373	-1854	711	0	-278	-7244	15.71	15.71	9.42	9.42	2	0.20	0.02	0.17	0.00	0.00	24.0
11	25	-3377	-1856	416	0	-154	-7244	15.71	15.71	9.42	9.42	2	0.20	0.02	0.17	0.00	0.00	24.0
12	25	-6339	-1232	696	0	-271	-4798	15.71	15.71	9.42	9.42	2	0.13	0.02	0.11	0.00	0.00	24.0

13	25	-6344	-1234	401	0	-148	-4798	15.71	15.71	9.42	9.42	2	0.13	0.02	0.11	0.00	0.00	24.0
14	25	-4406	-1634	1050	0	-420	-6388	15.71	15.71	9.42	9.42	2	0.18	0.02	0.14	0.00	0.00	24.0
15	25	-4420	-1640	67	0	-7	-6388	15.71	15.71	9.42	9.42	2	0.17	0.02	0.15	0.00	0.00	24.0
16	25	-5296	-1447	1045	0	-418	-5654	15.71	15.71	9.42	9.42	2	0.16	0.02	0.13	0.00	0.00	24.0
17	25	-5310	-1454	62	0	-5	-5654	15.71	15.71	9.42	9.42	2	0.15	0.02	0.13	0.00	0.00	24.0
18	25	5987	-4880	1572	0	-615	-20760	15.71	15.71	9.42	9.42	3	0.42	0.06	0.46	0.00	0.00	24.0
19	25	-8266	-3338	1314	0	-508	-11100	15.71	15.71	9.42	9.42	3	0.21	0.04	0.28	0.00	0.00	24.0
20	25	-1883	-3803	540	0	-184	-14740	15.71	15.71	9.42	9.42	3	0.28	0.05	0.35	0.00	0.00	24.0
37	25	9023	-4708	1420	0	-556	-21340	15.71	15.71	9.42	9.42	3	0.44	0.06	0.44	0.00	0.00	24.0
38	25	-14730	-2137	990	0	-378	-5231	15.71	15.71	9.42	9.42	3	0.10	0.03	0.17	0.00	0.00	24.0
39	25	-4095	-2913	-300	0	162	-11290	15.71	15.71	9.42	9.42	3	0.21	0.04	0.26	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-6186	-2007	723	0	-367	-8078	15.71	15.71	9.42	9.42	3	0.15	0.03	0.17	0.00	0.00	24.0
2	38	-3273	-1854	711	0	-366	-7476	15.71	15.71	9.42	9.42	2	0.21	0.02	0.17	0.00	0.00	24.0
3	38	-3277	-1856	416	0	-206	-7476	15.71	15.71	9.42	9.42	2	0.20	0.02	0.17	0.00	0.00	24.0
4	38	-6239	-1232	696	0	-358	-4951	15.71	15.71	9.42	9.42	2	0.14	0.02	0.11	0.00	0.00	24.0
5	38	-6244	-1234	401	0	-198	-4952	15.71	15.71	9.42	9.42	2	0.13	0.02	0.11	0.00	0.00	24.0
6	38	-4306	-1634	1050	0	-551	-6593	15.71	15.71	9.42	9.42	2	0.19	0.02	0.14	0.00	0.00	24.0
7	38	-4320	-1640	67	0	-16	-6593	15.71	15.71	9.42	9.42	2	0.17	0.02	0.15	0.00	0.00	24.0
8	38	-5196	-1447	1045	0	-549	-5835	15.71	15.71	9.42	9.42	2	0.17	0.02	0.13	0.00	0.00	24.0
9	38	-5210	-1454	62	0	-13	-5835	15.71	15.71	9.42	9.42	2	0.15	0.02	0.13	0.00	0.00	24.0
10	38	-3273	-1854	711	0	-366	-7476	15.71	15.71	9.42	9.42	2	0.21	0.02	0.17	0.00	0.00	24.0
11	38	-3277	-1856	416	0	-206	-7476	15.71	15.71	9.42	9.42	2	0.20	0.02	0.17	0.00	0.00	24.0
12	38	-6239	-1232	696	0	-358	-4951	15.71	15.71	9.42	9.42	2	0.14	0.02	0.11	0.00	0.00	24.0
13	38	-6244	-1234	401	0	-198	-4952	15.71	15.71	9.42	9.42	2	0.13	0.02	0.11	0.00	0.00	24.0
14	38	-4306	-1634	1050	0	-551	-6593	15.71	15.71	9.42	9.42	2	0.19	0.02	0.14	0.00	0.00	24.0
15	38	-4320	-1640	67	0	-16	-6593	15.71	15.71	9.42	9.42	2	0.17	0.02	0.15	0.00	0.00	24.0
16	38	-5196	-1447	1045	0	-549	-5835	15.71	15.71	9.42	9.42	2	0.17	0.02	0.13	0.00	0.00	24.0
17	38	-5210	-1454	62	0	-13	-5835	15.71	15.71	9.42	9.42	2	0.15	0.02	0.13	0.00	0.00	24.0
18	38	6117	-4880	1572	0	-812	-21370	15.71	15.71	9.42	9.42	3	0.43	0.06	0.46	0.00	0.00	24.0
19	38	-8136	-3338	1314	0	-672	-11515	15.71	15.71	9.42	9.42	3	0.22	0.04	0.28	0.00	0.00	24.0
20	38	-1753	-3803	540	0	-252	-15215	15.71	15.71	9.42	9.42	3	0.29	0.05	0.35	0.00	0.00	24.0
37	38	9153	-4708	1420	0	-734	-21930	15.71	15.71	9.42	9.42	3	0.45	0.06	0.44	0.00	0.00	24.0
38	38	-14600	-2137	990	0	-502	-5499	15.71	15.71	9.42	9.42	3	0.10	0.03	0.17	0.00	0.00	24.0
39	38	-3965	-2913	-300	0	199	-11655	15.71	15.71	9.42	9.42	3	0.22	0.04	0.26	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-6056	-2007	723	0	-457	-8329	15.71	15.71	9.42	9.42	3	0.16	0.03	0.17	0.00	0.00	24.0
2	50	-3173	-1854	711	0	-455	-7708	15.71	15.71	9.42	9.42	2	0.22	0.02	0.17	0.00	0.00	24.0
3	50	-3177	-1856	416	0	-258	-7708	15.71	15.71	9.42	9.42	2	0.21	0.02	0.17	0.00	0.00	24.0
4	50	-6139	-1232	696	0	-445	-5105	15.71	15.71	9.42	9.42	2	0.14	0.02	0.11	0.00	0.00	24.0
5	50	-6144	-1234	401	0	-248	-5106	15.71	15.71	9.42	9.42	2	0.14	0.02	0.11	0.00	0.00	24.0
6	50	-4206	-1634	1050	0	-682	-6797	15.71	15.71	9.42	9.42	2	0.20	0.02	0.15	0.00	0.00	24.0
7	50	-4220	-1640	67	0	-24	-6798	15.71	15.71	9.42	9.42	2	0.18	0.02	0.15	0.00	0.00	24.0
8	50	-5096	-1447	1045	0	-679	-6016	15.71	15.71	9.42	9.42	2	0.18	0.02	0.13	0.00	0.00	24.0
9	50	-5110	-1454	62	0	-21	-6017	15.71	15.71	9.42	9.42	2	0.16	0.02	0.13	0.00	0.00	24.0
10	50	-3173	-1854	711	0	-455	-7708	15.71	15.71	9.42	9.42	2	0.22	0.02	0.17	0.00	0.00	24.0
11	50	-3177	-1856	416	0	-258	-7708	15.71	15.71	9.42	9.42	2	0.21	0.02	0.17	0.00	0.00	24.0
12	50	-6139	-1232	696	0	-445	-5105	15.71	15.71	9.42	9.42	2	0.14	0.02	0.11	0.00	0.00	24.0
13	50	-6144	-1234	401	0	-248	-5106	15.71	15.71	9.42	9.42	2	0.14	0.02	0.11	0.00	0.00	24.0
14	50	-4206	-1634	1050	0	-682	-6797	15.71	15.71	9.42	9.42	2	0.20	0.02	0.15	0.00	0.00	24.0
15	50	-4220	-1640	67	0	-24	-6798	15.71	15.71	9.42	9.42	2	0.18	0.02	0.15	0.00	0.00	24.0
16	50	-5096	-1447	1045	0	-679	-6016	15.71	15.71	9.42	9.42	2	0.18	0.02	0.13	0.00	0.00	24.0
17	50	-5110	-1454	62	0	-21	-6017	15.71	15.71	9.42	9.42	2	0.16	0.02	0.13	0.00	0.00	24.0
18	50	6247	-4880	1572	0	-1008	-21980	15.71	15.71	9.42	9.42	3	0.45	0.06	0.46	0.00	0.00	24.0
19	50	-8006	-3338	1314	0	-837	-11930	15.71	15.71	9.42	9.42	3	0.23	0.04	0.28	0.00	0.00	24.0
20	50	-1623	-3803	540	0	-319	-15690	15.71	15.71	9.42	9.42	3	0.30	0.05	0.35	0.00	0.00	24.0
37	50	9283	-4708	1420	0	-911	-22520	15.71	15.71	9.42	9.42	3	0.46	0.06	0.44	0.00	0.00	24.0
38	50	-14470	-2137	990	0	-626	-5766	15.71	15.71	9.42	9.42	3	0.11	0.03	0.17	0.00	0.00	24.0
39	50	-3835	-2913	-300	0	237	-12020	15.71	15.71	9.42	9.42	3	0.23	0.04	0.26	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 81 NI 1699 NF 220 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 27A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-10750	-1268	1076	0	-64	-2758	15.71	15.71	9.42	9.42	3	0.05	0.02	0.10	0.00	0.00	24.0
2	0	-7145	-1288	953	0	-65	-2945	15.71	15.71	9.42	9.42	2	0.08	0.02	0.11	0.00	0.00	24.0
3	0	-7149	-1320	674	0	-15	-3009	15.71	15.71	9.42	9.42	2	0.08	0.02	0.11	0.00	0.00	24.0
4	0	-9387	-631	982	0	-84	-1235	15.71	15.71	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
5	0	-9392	-664	703	0	-33	-1298	15.71	15.71	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
6	0	-7924	-1020	1289	0	-130	-2273	15.71	15.71	9.42	9.42	2	0.06	0.02	0.09	0.00	0.00	24.0
7	0	-7940	-1129	358	0	38	-2484	15.71	15.71	9.42	9.42	2	0.06	0.01	0.10	0.00	0.00	24.0
8	0	-8597	-822	1298	0	-136	-1759	15.71	15.71	9.42	9.42	2	0.05	0.02	0.09	0.00	0.00	24.0
9	0	-8612	-932	367	0	32	-1971	15.71	15.71	9.42	9.42	2	0.05	0.01	0.08	0.00	0.00	24.0
10	0	-7145	-1288	953	0	-65	-2945	15.71	15.71	9.42	9.42	2	0.08	0.02	0.11	0.00	0.00	24.0
11	0	-7149	-1320	674	0	-15	-3009	15.71	15.71	9.42	9.42	2	0.08	0.02	0.11	0.00	0.00	24.0
12	0	-9387	-631	982	0	-84	-1235	15.71	15.71	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
13	0	-9392	-664	703	0	-33	-1298	15.71	15.71	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
14	0	-7924	-1020	1289	0	-130	-2273	15.71	15.71	9.42	9.42	2	0.06	0.02	0.09	0.00	0.00	24.0
15	0	-7940	-1129	358	0	38	-2484	15.71	15.71	9.42	9.42	2	0.06	0.01	0.10	0.00	0.00	24.0
16	0	-8597	-822	1298	0	-136	-1759	15.71	15.71	9.42	9.42	2	0.05	0.02	0.09	0.00	0.00	24.0
17	0	-8612	-932	367	0	32	-1971	15.71	15.71	9.42	9.42	2	0.05	0.01	0.08	0.00	0.00	24.0
18	0	-4030	-3679	1945	0	-68	-9865	15.71	15.71	9.42	9.42	3	0.19	0.05	0.33	0.00	0.00	24.0
19	0	-15240	-1909	1887	0	-116	-3023	15.71	15.71	9.42	9.42	3	0.06	0.03	0.15	0.00	0.00	24.0
20	0	-9810	-2657	1054	0	47	-6064	15.71	15.71	9.42	9.42	3	0.11	0.03	0.22	0.00	0.00	24.0
37	0	-683	-3769	1694	0	-44	-10940	15.71	15.71	9.42	9.42	3	0.21	0.05	0.35	0.00	0.00	24.0
38	0	-19370	-819	1596	0	-122	463	15.71	15.71	9.42	9.42	3	0.01	0.02	0.10	0.00	0.00	24.0
39	0	-10320	-2066	207	0	148	-4606	15.71	15.71	9.42	9.42	3	0.09	0.03	0.17	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-10620	-1268	1076	0	-198	-2916	15.71	15.71	9.42	9.42	3	0.05	0.02	0.10	0.00	0.00	24.0
2	12	-7045	-1288	953	0	-184	-3106	15.71	15.71	9.42	9.42	2	0.09	0.02	0.11	0.00	0.00	24.0
3	12	-7049	-1320	674	0	-99	-3174	15.71	15.71	9.42	9.42	2	0.08	0.02	0.11	0.00	0.00	24.0
4	12	-9287	-631	982	0	-206	-1314	15.71	15.71	9.42	9.42	2	0.04	0.01	0.06	0.00	0.00	24.0
5	12	-9292	-664	703	0	-121	-1381	15.71	15.71	9.42	9.42	2	0.04	0.01	0.06	0.00	0.00	24.0
6	12	-7824	-1020	1289	0	-291	-2400	15.71	15.71	9.42	9.42	2	0.07	0.02	0.09	0.00	0.00	24.0
7	12	-7840	-1129	358	0	-7	-2625	15.71	15.71	9.42	9.42	2	0.07	0.01	0.10	0.00	0.00	24.0
8	12	-8497	-822	1298	0	-298	-1862	15.71	15.71	9.42	9.42	2	0.06	0.02	0.09	0.00	0.00	24.0

9	12	-8512	-932	367	0	-14	-2088	15.71	15.71	9.42	9.42	2	0.05	0.01	0.08	0.00	0.00	24.0
10	12	-7045	-1288	953	0	-184	-3106	15.71	15.71	9.42	9.42	2	0.09	0.02	0.11	0.00	0.00	24.0
11	12	-7049	-1320	674	0	-99	-3174	15.71	15.71	9.42	9.42	2	0.08	0.02	0.11	0.00	0.00	24.0
12	12	-9287	-631	982	0	-206	-1314	15.71	15.71	9.42	9.42	2	0.04	0.01	0.06	0.00	0.00	24.0
13	12	-9292	-664	703	0	-121	-1381	15.71	15.71	9.42	9.42	2	0.04	0.01	0.06	0.00	0.00	24.0
14	12	-7824	-1020	1289	0	-291	-2400	15.71	15.71	9.42	9.42	2	0.07	0.02	0.09	0.00	0.00	24.0
15	12	-7840	-1129	358	0	-7	-2625	15.71	15.71	9.42	9.42	2	0.07	0.01	0.10	0.00	0.00	24.0
16	12	-8497	-822	1298	0	-298	-1862	15.71	15.71	9.42	9.42	2	0.06	0.02	0.09	0.00	0.00	24.0
17	12	-8512	-932	367	0	-14	-2088	15.71	15.71	9.42	9.42	2	0.05	0.01	0.08	0.00	0.00	24.0
18	12	-3900	-3679	1945	0	-311	-10324	15.71	15.71	9.42	9.42	3	0.20	0.05	0.33	0.00	0.00	24.0
19	12	-15110	-1909	1887	0	-351	-3262	15.71	15.71	9.42	9.42	3	0.06	0.03	0.15	0.00	0.00	24.0
20	12	-9680	-2657	1054	0	-85	-6396	15.71	15.71	9.42	9.42	3	0.12	0.03	0.22	0.00	0.00	24.0
37	12	-553	-3769	1694	0	-255	-11410	15.71	15.71	9.42	9.42	3	0.22	0.05	0.35	0.00	0.00	24.0
38	12	-19240	-819	1596	0	-322	361	15.71	15.71	9.42	9.42	3	0.01	0.02	0.10	0.00	0.00	24.0
39	12	-10189	-2066	207	0	122	-4864	15.71	15.71	9.42	9.42	3	0.09	0.03	0.17	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-10490	-1268	1076	0	-333	-3075	15.71	15.71	9.42	9.42	3	0.06	0.02	0.10	0.00	0.00	24.0
2	25	-6945	-1288	953	0	-303	-3267	15.71	15.71	9.42	9.42	2	0.09	0.02	0.11	0.00	0.00	24.0
3	25	-6949	-1320	674	0	-183	-3339	15.71	15.71	9.42	9.42	2	0.09	0.02	0.11	0.00	0.00	24.0
4	25	-9187	-631	982	0	-329	-1393	15.71	15.71	9.42	9.42	2	0.04	0.01	0.06	0.00	0.00	24.0
5	25	-9192	-664	703	0	-209	-1464	15.71	15.71	9.42	9.42	2	0.04	0.01	0.06	0.00	0.00	24.0
6	25	-7724	-1020	1289	0	-452	-2528	15.71	15.71	9.42	9.42	2	0.08	0.02	0.09	0.00	0.00	24.0
7	25	-7740	-1129	358	0	-52	-2766	15.71	15.71	9.42	9.42	2	0.07	0.01	0.10	0.00	0.00	24.0
8	25	-8397	-822	1298	0	-460	-1965	15.71	15.71	9.42	9.42	2	0.06	0.02	0.09	0.00	0.00	24.0
9	25	-8412	-932	367	0	-60	-2204	15.71	15.71	9.42	9.42	2	0.06	0.01	0.08	0.00	0.00	24.0
10	25	-6945	-1288	953	0	-303	-3267	15.71	15.71	9.42	9.42	2	0.09	0.02	0.11	0.00	0.00	24.0
11	25	-6949	-1320	674	0	-183	-3339	15.71	15.71	9.42	9.42	2	0.09	0.02	0.11	0.00	0.00	24.0
12	25	-9187	-631	982	0	-329	-1393	15.71	15.71	9.42	9.42	2	0.04	0.01	0.06	0.00	0.00	24.0
13	25	-9192	-664	703	0	-209	-1464	15.71	15.71	9.42	9.42	2	0.04	0.01	0.06	0.00	0.00	24.0
14	25	-7724	-1020	1289	0	-452	-2528	15.71	15.71	9.42	9.42	2	0.08	0.02	0.09	0.00	0.00	24.0
15	25	-7740	-1129	358	0	-52	-2766	15.71	15.71	9.42	9.42	2	0.07	0.01	0.10	0.00	0.00	24.0
16	25	-8397	-822	1298	0	-460	-1965	15.71	15.71	9.42	9.42	2	0.06	0.02	0.09	0.00	0.00	24.0
17	25	-8412	-932	367	0	-60	-2204	15.71	15.71	9.42	9.42	2	0.06	0.01	0.08	0.00	0.00	24.0
18	25	-3770	-3679	1945	0	-555	-10782	15.71	15.71	9.42	9.42	3	0.21	0.05	0.33	0.00	0.00	24.0
19	25	-14980	-1909	1887	0	-587	-3501	15.71	15.71	9.42	9.42	3	0.07	0.03	0.15	0.00	0.00	24.0
20	25	-9550	-2657	1054	0	-217	-6728	15.71	15.71	9.42	9.42	3	0.13	0.03	0.22	0.00	0.00	24.0
37	25	-423	-3769	1694	0	-467	-11880	15.71	15.71	9.42	9.42	3	0.23	0.05	0.35	0.00	0.00	24.0
38	25	-19110	-819	1596	0	-521	258	15.71	15.71	9.42	9.42	3	0.02	0.02	0.11	0.00	0.00	24.0
39	25	-10058	-2066	207	0	96	-5122	15.71	15.71	9.42	9.42	3	0.09	0.03	0.17	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-10360	-1268	1076	0	-468	-3234	15.71	15.71	9.42	9.42	3	0.06	0.02	0.10	0.00	0.00	24.0
2	38	-6845	-1288	953	0	-422	-3428	15.71	15.71	9.42	9.42	2	0.10	0.02	0.11	0.00	0.00	24.0
3	38	-6849	-1320	674	0	-267	-3504	15.71	15.71	9.42	9.42	2	0.10	0.02	0.11	0.00	0.00	24.0
4	38	-9087	-631	982	0	-452	-1471	15.71	15.71	9.42	9.42	2	0.05	0.01	0.06	0.00	0.00	24.0
5	38	-9092	-664	703	0	-297	-1547	15.71	15.71	9.42	9.42	2	0.05	0.01	0.06	0.00	0.00	24.0
6	38	-7624	-1020	1289	0	-613	-2655	15.71	15.71	9.42	9.42	2	0.08	0.02	0.09	0.00	0.00	24.0
7	38	-7640	-1129	358	0	-97	-2908	15.71	15.71	9.42	9.42	2	0.08	0.01	0.10	0.00	0.00	24.0
8	38	-8297	-822	1298	0	-622	-2068	15.71	15.71	9.42	9.42	2	0.07	0.02	0.09	0.00	0.00	24.0
9	38	-8312	-932	367	0	-106	-2320	15.71	15.71	9.42	9.42	2	0.06	0.01	0.08	0.00	0.00	24.0
10	38	-6845	-1288	953	0	-422	-3428	15.71	15.71	9.42	9.42	2	0.10	0.02	0.11	0.00	0.00	24.0
11	38	-6849	-1320	674	0	-267	-3504	15.71	15.71	9.42	9.42	2	0.10	0.02	0.11	0.00	0.00	24.0
12	38	-9087	-631	982	0	-452	-1471	15.71	15.71	9.42	9.42	2	0.05	0.01	0.06	0.00	0.00	24.0
13	38	-9092	-664	703	0	-297	-1547	15.71	15.71	9.42	9.42	2	0.05	0.01	0.06	0.00	0.00	24.0
14	38	-7624	-1020	1289	0	-613	-2655	15.71	15.71	9.42	9.42	2	0.08	0.02	0.09	0.00	0.00	24.0
15	38	-7640	-1129	358	0	-97	-2908	15.71	15.71	9.42	9.42	2	0.08	0.01	0.10	0.00	0.00	24.0
16	38	-8297	-822	1298	0	-622	-2068	15.71	15.71	9.42	9.42	2	0.07	0.02	0.09	0.00	0.00	24.0
17	38	-8312	-932	367	0	-106	-2320	15.71	15.71	9.42	9.42	2	0.06	0.01	0.08	0.00	0.00	24.0
18	38	-3640	-3679	1945	0	-798	-11241	15.71	15.71	9.42	9.42	3	0.22	0.05	0.33	0.00	0.00	24.0
19	38	-14850	-1909	1887	0	-823	-3739	15.71	15.71	9.42	9.42	3	0.08	0.03	0.15	0.00	0.00	24.0
20	38	-9420	-2657	1054	0	-348	-7061	15.71	15.71	9.42	9.42	3	0.13	0.03	0.22	0.00	0.00	24.0
37	38	-293	-3769	1694	0	-679	-12350	15.71	15.71	9.42	9.42	3	0.24	0.05	0.35	0.00	0.00	24.0
38	38	-18980	-819	1596	0	-721	156	15.71	15.71	9.42	9.42	3	0.03	0.02	0.11	0.00	0.00	24.0
39	38	-9928	-2066	207	0	70	-5380	15.71	15.71	9.42	9.42	3	0.10	0.03	0.17	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-10230	-1268	1076	0	-602	-3392	15.71	15.71	9.42	9.42	3	0.07	0.02	0.10	0.00	0.00	24.0
2	50	-6745	-1288	953	0	-541	-3589	15.71	15.71	9.42	9.42	2	0.11	0.02	0.11	0.00	0.00	24.0
3	50	-6749	-1320	674	0	-352	-3669	15.71	15.71	9.42	9.42	2	0.10	0.02	0.11	0.00	0.00	24.0
4	50	-8987	-631	982	0	-575	-1550	15.71	15.71	9.42	9.42	2	0.06	0.01	0.06	0.00	0.00	24.0
5	50	-8992	-664	703	0	-385	-1630	15.71	15.71	9.42	9.42	2	0.05	0.01	0.06	0.00	0.00	24.0
6	50	-7524	-1020	1289	0	-775	-2782	15.71	15.71	9.42	9.42	2	0.09	0.02	0.09	0.00	0.00	24.0
7	50	-7540	-1129	358	0	-142	-3049	15.71	15.71	9.42	9.42	2	0.08	0.01	0.10	0.00	0.00	24.0
8	50	-8197	-822	1298	0	-785	-2171	15.71	15.71	9.42	9.42	2	0.08	0.02	0.09	0.00	0.00	24.0
9	50	-8212	-932	367	0	-152	-2437	15.71	15.71	9.42	9.42	2	0.07	0.01	0.08	0.00	0.00	24.0
10	50	-6745	-1288	953	0	-541	-3589	15.71	15.71	9.42	9.42	2	0.11	0.02	0.11	0.00	0.00	24.0
11	50	-6749	-1320	674	0	-352	-3669	15.71	15.71	9.42	9.42	2	0.10	0.02	0.11	0.00	0.00	24.0
12	50	-8987	-631	982	0	-575	-1550	15.71	15.71	9.42	9.42	2	0.06	0.01	0.06	0.00	0.00	24.0
13	50	-8992	-664	703	0	-385	-1630	15.71	15.71	9.42	9.42	2	0.05	0.01	0.06	0.00	0.00	24.0
14	50	-7524	-1020	1289	0	-775	-2782	15.71	15.71	9.42	9.42	2	0.09	0.02	0.09	0.00	0.00	24.0
15	50	-7540	-1129	358	0	-142	-3049	15.71	15.71	9.42	9.42	2	0.08	0.01	0.10	0.00	0.00	24.0
16	50	-8197	-822	1298	0	-785	-2171	15.71	15.71	9.42	9.42	2	0.08	0.02	0.09	0.00	0.00	24.0
17	50	-8212	-932	367	0	-152	-2437	15.71	15.71	9.42	9.42	2	0.07	0.01	0.08	0.00	0.00	24.0
18	50	-3510	-3679	1945	0	-1041	-11700	15.71	15.71	9.42	9.42	3	0.23	0.05	0.33	0.00	0.00	24.0
19	50	-14720	-1909	1887	0	-1059	-3978	15.71	15.71	9.42	9.42	3	0.08	0.03	0.15	0.00	0.00	24.0
20	50	-9290	-2657	1054	0	-480	-7393	15.71	15.71	9.42	9.42	3	0.14	0.03	0.22	0.00	0.00	24.0
37	50	-163	-3769	1694	0	-890	-12820	15.71	15.71	9.42	9.42	3	0.25	0.05	0.35	0.00	0.00	24.0
38	50	-18850	-819	1596	0	-920	54	15.71	15.71	9.42	9.42	3	0.03	0.02	0.11	0.00	0.00	24.0
39	50	-9797	-2066	207	0	44	-5638	15.71	15.71	9.42	9.42	3	0.10	0.03	0.17	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 82 NI 1351 NF 1360 SEZ. Rp B= 0.400 H= 0.600 (pilastro)
PIL. NUM. 16
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-12700	820	695	0	1375	-2217	12.57	12.57	6.28	6.28	3	0.11	0.01	0.08	0.00	0.00	24.0
2	0	-9706	1020	512	0	1008	-2830	12.57	12.57	6.28	6.28	2	0.18	0.02	0.10	0.00	0.00	24.0
3	0	-9829	1021	547	0	1085	-2834	12.57	12.57	6.28	6.28	2	0.18	0.02	0.10	0.00	0.00	24.0
4	0	-9705	240	522	0	1029	-577	12.57	12.57	6.28	6.28	2	0.08	0.01	0.05	0.00	0.00	24.0

5	0	-9829	242	556	0	1106	-581	12.57	12.57	6.28	6.28	2	0.08	0.01	0.05	0.00	0.00	24.0
6	0	-9561	745	476	0	926	-2038	12.57	12.57	6.28	6.28	2	0.14	0.01	0.07	0.00	0.00	24.0
7	0	-9973	750	590	0	1182	-2049	12.57	12.57	6.28	6.28	2	0.15	0.01	0.07	0.00	0.00	24.0
8	0	-9561	512	478	0	933	-1362	12.57	12.57	6.28	6.28	2	0.10	0.01	0.05	0.00	0.00	24.0
9	0	-9973	516	593	0	1189	-1373	12.57	12.57	6.28	6.28	2	0.12	0.01	0.05	0.00	0.00	24.0
10	0	-9706	1020	512	0	1008	-2830	12.57	12.57	6.28	6.28	2	0.18	0.02	0.10	0.00	0.00	24.0
11	0	-9829	1021	547	0	1085	-2834	12.57	12.57	6.28	6.28	2	0.18	0.02	0.10	0.00	0.00	24.0
12	0	-9705	240	522	0	1029	-577	12.57	12.57	6.28	6.28	2	0.08	0.01	0.05	0.00	0.00	24.0
13	0	-9829	242	556	0	1106	-581	12.57	12.57	6.28	6.28	2	0.08	0.01	0.05	0.00	0.00	24.0
14	0	-9561	745	476	0	926	-2038	12.57	12.57	6.28	6.28	2	0.14	0.01	0.07	0.00	0.00	24.0
15	0	-9973	750	590	0	1182	-2049	12.57	12.57	6.28	6.28	2	0.15	0.01	0.07	0.00	0.00	24.0
16	0	-9561	512	478	0	933	-1362	12.57	12.57	6.28	6.28	2	0.10	0.01	0.05	0.00	0.00	24.0
17	0	-9973	516	593	0	1189	-1373	12.57	12.57	6.28	6.28	2	0.12	0.01	0.05	0.00	0.00	24.0
18	0	-13120	2690	704	0	1379	-7553	12.57	12.57	6.28	6.28	3	0.28	0.05	0.26	0.00	0.00	24.0
19	0	-13130	104	729	0	1433	-116	12.57	12.57	6.28	6.28	3	0.08	0.01	0.07	0.00	0.00	24.0
20	0	-13050	1319	625	0	1157	-3617	12.57	12.57	6.28	6.28	3	0.14	0.02	0.13	0.00	0.00	24.0
37	0	-12870	3363	679	0	1332	-9503	12.57	12.57	6.28	6.28	3	0.35	0.06	0.32	0.00	0.00	24.0
38	0	-12900	-946	720	0	1422	2891	12.57	12.57	6.28	6.28	3	0.13	0.02	0.09	0.00	0.00	24.0
39	0	-12760	1078	547	0	961	-2944	12.57	12.57	6.28	6.28	3	0.12	0.02	0.10	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-12602	820	695	0	1288	-2115	12.57	12.57	6.28	6.28	3	0.10	0.01	0.08	0.00	0.00	24.0
2	12	-9631	1020	512	0	944	-2703	12.57	12.57	6.28	6.28	2	0.17	0.02	0.10	0.00	0.00	24.0
3	12	-9754	1021	547	0	1017	-2706	12.57	12.57	6.28	6.28	2	0.17	0.02	0.10	0.00	0.00	24.0
4	12	-9630	240	522	0	964	-547	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
5	12	-9754	242	556	0	1037	-550	12.57	12.57	6.28	6.28	2	0.08	0.01	0.05	0.00	0.00	24.0
6	12	-9486	745	476	0	867	-1945	12.57	12.57	6.28	6.28	2	0.13	0.01	0.07	0.00	0.00	24.0
7	12	-9898	750	590	0	1108	-1955	12.57	12.57	6.28	6.28	2	0.14	0.01	0.07	0.00	0.00	24.0
8	12	-9486	512	478	0	873	-1298	12.57	12.57	6.28	6.28	2	0.10	0.01	0.05	0.00	0.00	24.0
9	12	-9898	516	593	0	1115	-1309	12.57	12.57	6.28	6.28	2	0.11	0.01	0.05	0.00	0.00	24.0
10	12	-9631	1020	512	0	944	-2703	12.57	12.57	6.28	6.28	2	0.17	0.02	0.10	0.00	0.00	24.0
11	12	-9754	1021	547	0	1017	-2706	12.57	12.57	6.28	6.28	2	0.17	0.02	0.10	0.00	0.00	24.0
12	12	-9630	240	522	0	964	-547	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
13	12	-9754	242	556	0	1037	-550	12.57	12.57	6.28	6.28	2	0.08	0.01	0.05	0.00	0.00	24.0
14	12	-9486	745	476	0	867	-1945	12.57	12.57	6.28	6.28	2	0.13	0.01	0.07	0.00	0.00	24.0
15	12	-9898	750	590	0	1108	-1955	12.57	12.57	6.28	6.28	2	0.14	0.01	0.07	0.00	0.00	24.0
16	12	-9486	512	478	0	873	-1298	12.57	12.57	6.28	6.28	2	0.10	0.01	0.05	0.00	0.00	24.0
17	12	-9898	516	593	0	1115	-1309	12.57	12.57	6.28	6.28	2	0.11	0.01	0.05	0.00	0.00	24.0
18	12	-13022	2690	704	0	1291	-7217	12.57	12.57	6.28	6.28	3	0.27	0.05	0.26	0.00	0.00	24.0
19	12	-13032	104	729	0	1342	-103	12.57	12.57	6.28	6.28	3	0.07	0.01	0.07	0.00	0.00	24.0
20	12	-12952	1319	625	0	1079	-3452	12.57	12.57	6.28	6.28	3	0.14	0.02	0.13	0.00	0.00	24.0
37	12	-12772	3363	679	0	1247	-9082	12.57	12.57	6.28	6.28	3	0.34	0.06	0.32	0.00	0.00	24.0
38	12	-12802	-946	720	0	1332	2773	12.57	12.57	6.28	6.28	3	0.12	0.02	0.09	0.00	0.00	24.0
39	12	-12662	1078	547	0	893	-2809	12.57	12.57	6.28	6.28	3	0.11	0.02	0.10	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-12505	820	695	0	1201	-2012	12.57	12.57	6.28	6.28	3	0.10	0.01	0.08	0.00	0.00	24.0
2	25	-9556	1020	512	0	880	-2575	12.57	12.57	6.28	6.28	2	0.16	0.02	0.10	0.00	0.00	24.0
3	25	-9679	1021	547	0	948	-2578	12.57	12.57	6.28	6.28	2	0.16	0.02	0.10	0.00	0.00	24.0
4	25	-9555	240	522	0	899	-517	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
5	25	-9679	242	556	0	967	-520	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
6	25	-9411	745	476	0	807	-1852	12.57	12.57	6.28	6.28	2	0.12	0.01	0.07	0.00	0.00	24.0
7	25	-9823	750	590	0	1035	-1862	12.57	12.57	6.28	6.28	2	0.13	0.01	0.07	0.00	0.00	24.0
8	25	-9411	512	478	0	813	-1234	12.57	12.57	6.28	6.28	2	0.09	0.01	0.05	0.00	0.00	24.0
9	25	-9823	516	593	0	1040	-1244	12.57	12.57	6.28	6.28	2	0.10	0.01	0.05	0.00	0.00	24.0
10	25	-9556	1020	512	0	880	-2575	12.57	12.57	6.28	6.28	2	0.16	0.02	0.10	0.00	0.00	24.0
11	25	-9679	1021	547	0	948	-2578	12.57	12.57	6.28	6.28	2	0.16	0.02	0.10	0.00	0.00	24.0
12	25	-9555	240	522	0	899	-517	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
13	25	-9679	242	556	0	967	-520	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
14	25	-9411	745	476	0	807	-1852	12.57	12.57	6.28	6.28	2	0.12	0.01	0.07	0.00	0.00	24.0
15	25	-9823	750	590	0	1035	-1862	12.57	12.57	6.28	6.28	2	0.13	0.01	0.07	0.00	0.00	24.0
16	25	-9411	512	478	0	813	-1234	12.57	12.57	6.28	6.28	2	0.09	0.01	0.05	0.00	0.00	24.0
17	25	-9823	516	593	0	1040	-1244	12.57	12.57	6.28	6.28	2	0.10	0.01	0.05	0.00	0.00	24.0
18	25	-12925	2690	704	0	1203	-6880	12.57	12.57	6.28	6.28	3	0.26	0.05	0.26	0.00	0.00	24.0
19	25	-12935	104	729	0	1251	-90	12.57	12.57	6.28	6.28	3	0.07	0.01	0.07	0.00	0.00	24.0
20	25	-12855	1319	625	0	1001	-3288	12.57	12.57	6.28	6.28	3	0.13	0.02	0.13	0.00	0.00	24.0
37	25	-12675	3363	679	0	1162	-8662	12.57	12.57	6.28	6.28	3	0.32	0.06	0.32	0.00	0.00	24.0
38	25	-12705	-946	720	0	1242	2655	12.57	12.57	6.28	6.28	3	0.12	0.02	0.09	0.00	0.00	24.0
39	25	-12565	1078	547	0	825	-2674	12.57	12.57	6.28	6.28	3	0.11	0.02	0.10	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	37	-12408	820	695	0	1114	-1910	12.57	12.57	6.28	6.28	3	0.09	0.01	0.08	0.00	0.00	24.0
2	37	-9481	1020	512	0	816	-2448	12.57	12.57	6.28	6.28	2	0.15	0.02	0.10	0.00	0.00	24.0
3	37	-9604	1021	547	0	880	-2451	12.57	12.57	6.28	6.28	2	0.15	0.02	0.10	0.00	0.00	24.0
4	37	-9480	240	522	0	834	-487	12.57	12.57	6.28	6.28	2	0.06	0.01	0.05	0.00	0.00	24.0
5	37	-9604	242	556	0	898	-490	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
6	37	-9336	745	476	0	748	-1758	12.57	12.57	6.28	6.28	2	0.12	0.01	0.07	0.00	0.00	24.0
7	37	-9748	750	590	0	961	-1768	12.57	12.57	6.28	6.28	2	0.12	0.01	0.07	0.00	0.00	24.0
8	37	-9336	512	478	0	753	-1170	12.57	12.57	6.28	6.28	2	0.09	0.01	0.05	0.00	0.00	24.0
9	37	-9748	516	593	0	966	-1180	12.57	12.57	6.28	6.28	2	0.10	0.01	0.05	0.00	0.00	24.0
10	37	-9481	1020	512	0	816	-2448	12.57	12.57	6.28	6.28	2	0.15	0.02	0.10	0.00	0.00	24.0
11	37	-9604	1021	547	0	880	-2451	12.57	12.57	6.28	6.28	2	0.15	0.02	0.10	0.00	0.00	24.0
12	37	-9480	240	522	0	834	-487	12.57	12.57	6.28	6.28	2	0.06	0.01	0.05	0.00	0.00	24.0
13	37	-9604	242	556	0	898	-490	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
14	37	-9336	745	476	0	748	-1758	12.57	12.57	6.28	6.28	2	0.12	0.01	0.07	0.00	0.00	24.0
15	37	-9748	750	590	0	961	-1768	12.57	12.57	6.28	6.28	2	0.12	0.01	0.07	0.00	0.00	24.0
16	37	-9336	512	478	0	753	-1170	12.57	12.57	6.28	6.28	2	0.09	0.01	0.05	0.00	0.00	24.0
17	37	-9748	516	593	0	966	-1180	12.57	12.57	6.28	6.28	2	0.10	0.01	0.05	0.00	0.00	24.0
18	37	-12828	2690	704	0	1115	-6544	12.57	12.57	6.28	6.28	3	0.25	0.05	0.26	0.00	0.00	24.0
19	37	-12838	104	729	0	1160	-77	12.57	12.57	6.28	6.28	3	0.06	0.01	0.07	0.00	0.00	24.0
20	37	-12758	1319	625	0	922	-3123	12.57	12.57	6.28	6.28	3	0.12	0.02	0.13	0.00	0.00	24.0
37	37	-12578	3363	679	0	1078	-8241	12.57	12.57	6.28	6.28	3	0.30	0.06	0.32	0.00	0.00	24.0
38	37	-12608	-946	720	0	1152	2536	12.57	12.57	6.28	6.28	3	0.11	0.02	0.09	0.00	0.00	24.0
39	37	-12468	1078	547	0	756	-2540	12.57	12.57	6.28	6.28	3	0.10	0.02	0.10	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-12310	820	695	0	1027	-1807	12.57	12.57	6.28	6.28	3	0.08	0.01	0.08	0.00	0.00	24.0
2	50	-9406	1020	512	0	752	-2320	12.57	12.57	6.28	6.28	2	0.14	0.02	0.10	0.00	0.00	24.0
3	50	-9529	1021	547	0	812	-2323	12.57	12.57	6.28	6.28	2	0.15	0.02	0.10	0.00	0.00	24.0
4	50	-9405	240	522	0	769	-457	12.57	12.57	6.28	6.28	2	0.06	0.01	0.05	0.00	0.00	24.0
5	50	-9529	242	556	0	828	-460	12.57	12.57	6.28	6.28	2	0.06	0.01	0.05	0.00	0.00	24.0
6	50	-9261	745	476	0	688	-1665	12.57	12.57	6.28	6.28	2	0.11	0.01	0.07	0.00	0.00	24.0
7	50	-9673	750	590	0	887	-1674	12.57	12.57	6.28	6.28	2	0.12	0.01	0.07	0.00	0.00	24.0
8	50	-9261	512	478	0	693	-1106	12.57	12.57	6.28	6.28	2	0.08	0.01	0.05	0.00	0.00	24.0
9	50	-9673	516	593	0	892	-1115	12.57	12.57	6.28	6.28	2	0.09	0.01	0.05	0.00	0.00	24.0
10	50	-9406	1020	512	0	752	-2320	12.57	12.57	6.28	6.28	2	0.14	0.02	0.10	0.00	0.00	24.0

11	50	-9529	1021	547	0	812	-2323	12.57	12.57	6.28	6.28	2	0.15	0.02	0.10	0.00	0.00	24.0
12	50	-9405	240	522	0	769	-457	12.57	12.57	6.28	6.28	2	0.06	0.01	0.05	0.00	0.00	24.0
13	50	-9529	242	556	0	828	-460	12.57	12.57	6.28	6.28	2	0.06	0.01	0.05	0.00	0.00	24.0
14	50	-9261	745	476	0	688	-1665	12.57	12.57	6.28	6.28	2	0.11	0.01	0.07	0.00	0.00	24.0
15	50	-9673	750	590	0	887	-1674	12.57	12.57	6.28	6.28	2	0.12	0.01	0.07	0.00	0.00	24.0
16	50	-9261	512	478	0	693	-1106	12.57	12.57	6.28	6.28	2	0.08	0.01	0.05	0.00	0.00	24.0
17	50	-9673	516	593	0	892	-1115	12.57	12.57	6.28	6.28	2	0.09	0.01	0.05	0.00	0.00	24.0
18	50	-12730	2690	704	0	1027	-6208	12.57	12.57	6.28	6.28	3	0.23	0.05	0.26	0.00	0.00	24.0
19	50	-12740	104	729	0	1069	-64	12.57	12.57	6.28	6.28	3	0.06	0.01	0.07	0.00	0.00	24.0
20	50	-12660	1319	625	0	844	-2958	12.57	12.57	6.28	6.28	3	0.12	0.02	0.13	0.00	0.00	24.0
37	50	-12480	3363	679	0	993	-7821	12.57	12.57	6.28	6.28	3	0.29	0.06	0.32	0.00	0.00	24.0
38	50	-12510	-946	720	0	1062	2418	12.57	12.57	6.28	6.28	3	0.10	0.02	0.09	0.00	0.00	24.0
39	50	-12370	1078	547	0	688	-2405	12.57	12.57	6.28	6.28	3	0.10	0.02	0.10	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 83 NI 1360 NF 170 SEZ. Rp B= 0.400 H= 0.600 (pilastro)
PIL. NUM. 16A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-12310	820	695	0	1027	-1807	12.57	12.57	6.28	6.28	3	0.08	0.01	0.08	0.00	0.00	24.0
2	0	-9406	1020	512	0	752	-2320	12.57	12.57	6.28	6.28	2	0.14	0.02	0.10	0.00	0.00	24.0
3	0	-9529	1021	547	0	812	-2323	12.57	12.57	6.28	6.28	2	0.15	0.02	0.10	0.00	0.00	24.0
4	0	-9405	240	522	0	769	-457	12.57	12.57	6.28	6.28	2	0.06	0.01	0.05	0.00	0.00	24.0
5	0	-9529	242	556	0	828	-460	12.57	12.57	6.28	6.28	2	0.06	0.01	0.05	0.00	0.00	24.0
6	0	-9261	745	476	0	688	-1665	12.57	12.57	6.28	6.28	2	0.11	0.01	0.07	0.00	0.00	24.0
7	0	-9673	750	590	0	887	-1674	12.57	12.57	6.28	6.28	2	0.12	0.01	0.07	0.00	0.00	24.0
8	0	-9261	512	478	0	693	-1106	12.57	12.57	6.28	6.28	2	0.08	0.01	0.05	0.00	0.00	24.0
9	0	-9673	516	593	0	892	-1115	12.57	12.57	6.28	6.28	2	0.09	0.01	0.05	0.00	0.00	24.0
10	0	-9406	1020	512	0	752	-2320	12.57	12.57	6.28	6.28	2	0.14	0.02	0.10	0.00	0.00	24.0
11	0	-9529	1021	547	0	812	-2323	12.57	12.57	6.28	6.28	2	0.15	0.02	0.10	0.00	0.00	24.0
12	0	-9405	240	522	0	769	-457	12.57	12.57	6.28	6.28	2	0.06	0.01	0.05	0.00	0.00	24.0
13	0	-9529	242	556	0	828	-460	12.57	12.57	6.28	6.28	2	0.06	0.01	0.05	0.00	0.00	24.0
14	0	-9261	745	476	0	688	-1665	12.57	12.57	6.28	6.28	2	0.11	0.01	0.07	0.00	0.00	24.0
15	0	-9673	750	590	0	887	-1674	12.57	12.57	6.28	6.28	2	0.12	0.01	0.07	0.00	0.00	24.0
16	0	-9261	512	478	0	693	-1106	12.57	12.57	6.28	6.28	2	0.08	0.01	0.05	0.00	0.00	24.0
17	0	-9673	516	593	0	892	-1115	12.57	12.57	6.28	6.28	2	0.09	0.01	0.05	0.00	0.00	24.0
18	0	-12730	2690	704	0	1027	-6208	12.57	12.57	6.28	6.28	3	0.23	0.05	0.26	0.00	0.00	24.0
19	0	-12740	104	729	0	1069	-64	12.57	12.57	6.28	6.28	3	0.06	0.01	0.07	0.00	0.00	24.0
20	0	-12660	1319	625	0	844	-2958	12.57	12.57	6.28	6.28	3	0.12	0.02	0.13	0.00	0.00	24.0
37	0	-12480	3363	679	0	993	-7821	12.57	12.57	6.28	6.28	3	0.29	0.06	0.32	0.00	0.00	24.0
38	0	-12510	-946	720	0	1062	2418	12.57	12.57	6.28	6.28	3	0.10	0.02	0.09	0.00	0.00	24.0
39	0	-12370	1078	547	0	688	-2405	12.57	12.57	6.28	6.28	3	0.10	0.02	0.10	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-12212	820	695	0	940	-1705	12.57	12.57	6.28	6.28	3	0.08	0.01	0.08	0.00	0.00	24.0
2	12	-9331	1020	512	0	688	-2193	12.57	12.57	6.28	6.28	2	0.13	0.02	0.10	0.00	0.00	24.0
3	12	-9454	1021	547	0	744	-2195	12.57	12.57	6.28	6.28	2	0.14	0.02	0.10	0.00	0.00	24.0
4	12	-9330	240	522	0	703	-427	12.57	12.57	6.28	6.28	2	0.05	0.01	0.05	0.00	0.00	24.0
5	12	-9454	242	556	0	759	-429	12.57	12.57	6.28	6.28	2	0.06	0.01	0.05	0.00	0.00	24.0
6	12	-9186	745	476	0	629	-1572	12.57	12.57	6.28	6.28	2	0.10	0.01	0.07	0.00	0.00	24.0
7	12	-9598	750	590	0	813	-1580	12.57	12.57	6.28	6.28	2	0.11	0.01	0.08	0.00	0.00	24.0
8	12	-9186	512	478	0	634	-1042	12.57	12.57	6.28	6.28	2	0.08	0.01	0.05	0.00	0.00	24.0
9	12	-9598	516	593	0	818	-1050	12.57	12.57	6.28	6.28	2	0.09	0.01	0.05	0.00	0.00	24.0
10	12	-9331	1020	512	0	688	-2193	12.57	12.57	6.28	6.28	2	0.13	0.02	0.10	0.00	0.00	24.0
11	12	-9454	1021	547	0	744	-2195	12.57	12.57	6.28	6.28	2	0.14	0.02	0.10	0.00	0.00	24.0
12	12	-9330	240	522	0	703	-427	12.57	12.57	6.28	6.28	2	0.05	0.01	0.05	0.00	0.00	24.0
13	12	-9454	242	556	0	759	-429	12.57	12.57	6.28	6.28	2	0.06	0.01	0.05	0.00	0.00	24.0
14	12	-9186	745	476	0	629	-1572	12.57	12.57	6.28	6.28	2	0.10	0.01	0.07	0.00	0.00	24.0
15	12	-9598	750	590	0	813	-1580	12.57	12.57	6.28	6.28	2	0.11	0.01	0.08	0.00	0.00	24.0
16	12	-9186	512	478	0	634	-1042	12.57	12.57	6.28	6.28	2	0.08	0.01	0.05	0.00	0.00	24.0
17	12	-9598	516	593	0	818	-1050	12.57	12.57	6.28	6.28	2	0.09	0.01	0.05	0.00	0.00	24.0
18	12	-12632	2690	704	0	939	-5872	12.57	12.57	6.28	6.28	3	0.22	0.05	0.26	0.00	0.00	24.0
19	12	-12642	104	729	0	978	-51	12.57	12.57	6.28	6.28	3	0.05	0.01	0.07	0.00	0.00	24.0
20	12	-12562	1319	625	0	766	-2793	12.57	12.57	6.28	6.28	3	0.11	0.02	0.13	0.00	0.00	24.0
37	12	-12382	3363	679	0	908	-7401	12.57	12.57	6.28	6.28	3	0.27	0.06	0.32	0.00	0.00	24.0
38	12	-12412	-946	720	0	972	2300	12.57	12.57	6.28	6.28	3	0.10	0.02	0.09	0.00	0.00	24.0
39	12	-12272	1078	547	0	620	-2270	12.57	12.57	6.28	6.28	3	0.09	0.02	0.10	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-12115	820	695	0	854	-1602	12.57	12.57	6.28	6.28	3	0.07	0.01	0.08	0.00	0.00	24.0
2	25	-9256	1020	512	0	624	-2065	12.57	12.57	6.28	6.28	2	0.13	0.02	0.10	0.00	0.00	24.0
3	25	-9379	1021	547	0	675	-2067	12.57	12.57	6.28	6.28	2	0.13	0.02	0.10	0.00	0.00	24.0
4	25	-9255	240	522	0	638	-397	12.57	12.57	6.28	6.28	2	0.05	0.01	0.05	0.00	0.00	24.0
5	25	-9379	242	556	0	689	-399	12.57	12.57	6.28	6.28	2	0.05	0.01	0.05	0.00	0.00	24.0
6	25	-9111	745	476	0	570	-1478	12.57	12.57	6.28	6.28	2	0.10	0.01	0.08	0.00	0.00	24.0
7	25	-9523	750	590	0	740	-1486	12.57	12.57	6.28	6.28	2	0.10	0.01	0.08	0.00	0.00	24.0
8	25	-9111	512	478	0	574	-978	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
9	25	-9523	516	593	0	744	-986	12.57	12.57	6.28	6.28	2	0.08	0.01	0.05	0.00	0.00	24.0
10	25	-9256	1020	512	0	624	-2065	12.57	12.57	6.28	6.28	2	0.13	0.02	0.10	0.00	0.00	24.0
11	25	-9379	1021	547	0	675	-2067	12.57	12.57	6.28	6.28	2	0.13	0.02	0.10	0.00	0.00	24.0
12	25	-9255	240	522	0	638	-397	12.57	12.57	6.28	6.28	2	0.05	0.01	0.05	0.00	0.00	24.0
13	25	-9379	242	556	0	689	-399	12.57	12.57	6.28	6.28	2	0.05	0.01	0.05	0.00	0.00	24.0
14	25	-9111	745	476	0	570	-1478	12.57	12.57	6.28	6.28	2	0.10	0.01	0.08	0.00	0.00	24.0
15	25	-9523	750	590	0	740	-1486	12.57	12.57	6.28	6.28	2	0.10	0.01	0.08	0.00	0.00	24.0
16	25	-9111	512	478	0	574	-978	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
17	25	-9523	516	593	0	744	-986	12.57	12.57	6.28	6.28	2	0.08	0.01	0.05	0.00	0.00	24.0
18	25	-12535	2690	704	0	851	-5536	12.57	12.57	6.28	6.28	3	0.21	0.05	0.26	0.00	0.00	24.0
19	25	-12545	104	729	0	886	-38	12.57	12.57	6.28	6.28	3	0.05	0.01	0.07	0.00	0.00	24.0
20	25	-12465	1319	625	0	688	-2628	12.57	12.57	6.28	6.28	3	0.10	0.02	0.13	0.00	0.00	24.0
37	25	-12285	3363	679	0	823	-6980	12.57	12.57	6.28	6.28	3	0.26	0.06	0.32	0.00	0.00	24.0
38	25	-12315	-946	720	0	882	2181	12.57	12.57	6.28	6.28	3	0.09	0.02	0.09	0.00	0.00	24.0
39	25	-12175	1078	547	0	551	-2135	12.57	12.57	6.28	6.28	3	0.08	0.02	0.10	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-12018	820	695	0	767	-1499	12.57	12.57	6.28	6.28	3	0.07	0.01	0.08	0.00	0.00	24.0
2	38	-9181	1020	512	0	560	-1937	12.57	12.57	6.28	6.28	2	0.12	0.02	0.10	0.00	0.00	24.0
3	38	-9304	1021	547	0	607	-1940	12.57	12.57	6.28	6.28	2	0.12	0.02	0.10	0.00	0.00	24.0
4	38	-9180	240	522	0	573	-367	12.57	12.57	6.28	6.28	2	0.05	0.01	0.05	0.00	0.00	24.0
5	38	-9304	242	556	0	620	-369	12.57	12.57	6.28	6.28	2	0.05	0.01	0.05	0.00	0.00	24.0
6	38	-9036	745	476	0	510	-1385	12.57	12.57	6.28	6.28	2	0.09	0.01	0.08	0.00	0.00	24.0

7	38	-9448	750	590	0	666	-1393	12.57	12.57	6.28	6.28	2	0.09	0.01	0.08	0.00	0.00	24.0
8	38	-9036	512	478	0	514	-914	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
9	38	-9448	516	593	0	670	-921	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
10	38	-9181	1020	512	0	560	-1937	12.57	12.57	6.28	6.28	2	0.12	0.02	0.10	0.00	0.00	24.0
11	38	-9304	1021	547	0	607	-1940	12.57	12.57	6.28	6.28	2	0.12	0.02	0.10	0.00	0.00	24.0
12	38	-9180	240	522	0	573	-367	12.57	12.57	6.28	6.28	2	0.05	0.01	0.05	0.00	0.00	24.0
13	38	-9304	242	556	0	620	-369	12.57	12.57	6.28	6.28	2	0.05	0.01	0.05	0.00	0.00	24.0
14	38	-9036	745	476	0	510	-1385	12.57	12.57	6.28	6.28	2	0.09	0.01	0.08	0.00	0.00	24.0
15	38	-9448	750	590	0	666	-1393	12.57	12.57	6.28	6.28	2	0.09	0.01	0.08	0.00	0.00	24.0
16	38	-9036	512	478	0	514	-914	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
17	38	-9448	516	593	0	670	-921	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
18	38	-12438	2690	704	0	763	-5199	12.57	12.57	6.28	6.28	3	0.19	0.05	0.26	0.00	0.00	24.0
19	38	-12448	104	729	0	795	-25	12.57	12.57	6.28	6.28	3	0.04	0.01	0.07	0.00	0.00	24.0
20	38	-12368	1319	625	0	610	-2463	12.57	12.57	6.28	6.28	3	0.10	0.02	0.13	0.00	0.00	24.0
37	38	-12188	3363	679	0	738	-6560	12.57	12.57	6.28	6.28	3	0.24	0.06	0.32	0.00	0.00	24.0
38	38	-12218	-946	720	0	792	2062	12.57	12.57	6.28	6.28	3	0.09	0.02	0.09	0.00	0.00	24.0
39	38	-12078	1078	547	0	483	-2000	12.57	12.57	6.28	6.28	3	0.08	0.02	0.10	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-11920	820	695	0	680	-1397	12.57	12.57	6.28	6.28	3	0.06	0.01	0.08	0.00	0.00	24.0
2	50	-9106	1020	512	0	496	-1810	12.57	12.57	6.28	6.28	2	0.11	0.02	0.10	0.00	0.00	24.0
3	50	-9229	1021	547	0	538	-1812	12.57	12.57	6.28	6.28	2	0.11	0.02	0.10	0.00	0.00	24.0
4	50	-9105	240	522	0	508	-337	12.57	12.57	6.28	6.28	2	0.04	0.01	0.05	0.00	0.00	24.0
5	50	-9229	242	556	0	550	-339	12.57	12.57	6.28	6.28	2	0.04	0.01	0.05	0.00	0.00	24.0
6	50	-8961	745	476	0	451	-1292	12.57	12.57	6.28	6.28	2	0.08	0.01	0.08	0.00	0.00	24.0
7	50	-9373	750	590	0	592	-1299	12.57	12.57	6.28	6.28	2	0.09	0.01	0.08	0.00	0.00	24.0
8	50	-8961	512	478	0	454	-850	12.57	12.57	6.28	6.28	2	0.06	0.01	0.05	0.00	0.00	24.0
9	50	-9373	516	593	0	596	-857	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
10	50	-9106	1020	512	0	496	-1810	12.57	12.57	6.28	6.28	2	0.11	0.02	0.10	0.00	0.00	24.0
11	50	-9229	1021	547	0	538	-1812	12.57	12.57	6.28	6.28	2	0.11	0.02	0.10	0.00	0.00	24.0
12	50	-9105	240	522	0	508	-337	12.57	12.57	6.28	6.28	2	0.04	0.01	0.05	0.00	0.00	24.0
13	50	-9229	242	556	0	550	-339	12.57	12.57	6.28	6.28	2	0.04	0.01	0.05	0.00	0.00	24.0
14	50	-8961	745	476	0	451	-1292	12.57	12.57	6.28	6.28	2	0.08	0.01	0.08	0.00	0.00	24.0
15	50	-9373	750	590	0	592	-1299	12.57	12.57	6.28	6.28	2	0.09	0.01	0.08	0.00	0.00	24.0
16	50	-8961	512	478	0	454	-850	12.57	12.57	6.28	6.28	2	0.06	0.01	0.05	0.00	0.00	24.0
17	50	-9373	516	593	0	596	-857	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
18	50	-12340	2690	704	0	675	-4863	12.57	12.57	6.28	6.28	3	0.18	0.05	0.26	0.00	0.00	24.0
19	50	-12350	104	729	0	704	-12	12.57	12.57	6.28	6.28	3	0.04	0.01	0.07	0.00	0.00	24.0
20	50	-12270	1319	625	0	532	-2298	12.57	12.57	6.28	6.28	3	0.09	0.02	0.13	0.00	0.00	24.0
37	50	-12090	3363	679	0	654	-6140	12.57	12.57	6.28	6.28	3	0.23	0.06	0.33	0.00	0.00	24.0
38	50	-12120	-946	720	0	702	1944	12.57	12.57	6.28	6.28	3	0.08	0.02	0.09	0.00	0.00	24.0
39	50	-11980	1078	547	0	415	-1865	12.57	12.57	6.28	6.28	3	0.07	0.02	0.10	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 84 NI 1037 NF 300 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 15A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-37440	142	578	0	987	-269	6.28	6.28	12.57	12.57	3	0.03	0.01	0.04	0.00	0.00	24.0
2	0	-28550	360	462	0	744	-842	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
3	0	-28450	359	423	0	764	-839	6.28	6.28	12.57	12.57	2	0.06	0.01	0.03	0.00	0.00	24.0
4	0	-29150	-141	467	0	755	425	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
5	0	-29060	-142	428	0	774	428	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
6	0	-28870	186	509	0	726	-402	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
7	0	-28550	182	380	0	790	-392	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
8	0	-29050	36	510	0	729	-22	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
9	0	-28730	32	381	0	793	-12	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
10	0	-28550	360	462	0	744	-842	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
11	0	-28450	359	423	0	764	-839	6.28	6.28	12.57	12.57	2	0.06	0.01	0.03	0.00	0.00	24.0
12	0	-29150	-141	467	0	755	425	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
13	0	-29060	-142	428	0	774	428	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
14	0	-28870	186	509	0	726	-402	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
15	0	-28550	182	380	0	790	-392	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
16	0	-29050	36	510	0	729	-22	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
17	0	-28730	32	381	0	793	-12	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
18	0	-43190	1007	708	0	982	-2336	6.28	6.28	12.57	12.57	3	0.11	0.02	0.07	0.00	0.00	24.0
19	0	-43180	-638	694	0	1018	1674	6.28	6.28	12.57	12.57	3	0.08	0.01	0.05	0.00	0.00	24.0
20	0	-42350	182	413	0	477	-331	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
37	0	-41060	1541	664	0	947	-3653	6.28	6.28	12.57	12.57	3	0.17	0.03	0.10	0.00	0.00	24.0
38	0	-41050	-1200	640	0	1007	3030	6.28	6.28	12.57	12.57	3	0.14	0.02	0.08	0.00	0.00	24.0
39	0	-39670	167	172	0	105	-311	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-37342	142	578	0	915	-251	6.28	6.28	12.57	12.57	3	0.03	0.01	0.04	0.00	0.00	24.0
2	12	-28475	360	462	0	687	-797	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
3	12	-28375	359	423	0	711	-794	6.28	6.28	12.57	12.57	2	0.06	0.01	0.03	0.00	0.00	24.0
4	12	-29075	-141	467	0	697	408	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
5	12	-28985	-142	428	0	721	411	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
6	12	-28795	186	509	0	662	-379	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
7	12	-28475	182	380	0	743	-369	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
8	12	-28975	36	510	0	665	-17	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
9	12	-28655	32	381	0	746	-8	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
10	12	-28475	360	462	0	687	-797	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
11	12	-28375	359	423	0	711	-794	6.28	6.28	12.57	12.57	2	0.06	0.01	0.03	0.00	0.00	24.0
12	12	-29075	-141	467	0	697	408	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
13	12	-28985	-142	428	0	721	411	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
14	12	-28795	186	509	0	662	-379	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
15	12	-28475	182	380	0	743	-369	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
16	12	-28975	36	510	0	665	-17	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
17	12	-28655	32	381	0	746	-8	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
18	12	-43092	1007	708	0	894	-2210	6.28	6.28	12.57	12.57	3	0.10	0.02	0.07	0.00	0.00	24.0
19	12	-43082	-638	694	0	931	1594	6.28	6.28	12.57	12.57	3	0.08	0.01	0.05	0.00	0.00	24.0
20	12	-42252	182	413	0	425	-308	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
37	12	-40962	1541	664	0	864	-3460	6.28	6.28	12.57	12.57	3	0.16	0.03	0.10	0.00	0.00	24.0
38	12	-40952	-1200	640	0	927	2880	6.28	6.28	12.57	12.57	3	0.13	0.02	0.08	0.00	0.00	24.0
39	12	-39572	167	172	0	83	-290	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-37245	142	578	0	843	-233	6.28	6.28	12.57	12.57	3	0.03	0.01	0.04	0.00	0.00	24.0
2	25	-28400	360	462	0	629	-752	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0

3	25	-28300	359	423	0	658	-749	6.28	6.28	12.57	12.57	2	0.06	0.01	0.03	0.00	0.00	24.0
4	25	-29000	-141	467	0	638	390	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
5	25	-28910	-142	428	0	667	393	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
6	25	-28720	186	509	0	598	-355	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
7	25	-28400	182	380	0	695	-346	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
8	25	-28900	36	510	0	601	-13	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
9	25	-28580	32	381	0	698	-4	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
10	25	-28400	360	462	0	629	-752	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
11	25	-28300	359	423	0	658	-749	6.28	6.28	12.57	12.57	2	0.06	0.01	0.03	0.00	0.00	24.0
12	25	-29000	-141	467	0	638	390	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
13	25	-28910	-142	428	0	667	393	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
14	25	-28720	186	509	0	598	-355	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
15	25	-28400	182	380	0	695	-346	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
16	25	-28900	36	510	0	601	-13	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
17	25	-28580	32	381	0	698	-4	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
18	25	-42995	1007	708	0	805	-2085	6.28	6.28	12.57	12.57	3	0.09	0.02	0.07	0.00	0.00	24.0
19	25	-42985	-638	694	0	845	1514	6.28	6.28	12.57	12.57	3	0.07	0.01	0.05	0.00	0.00	24.0
20	25	-42155	182	413	0	373	-285	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
37	25	-40865	1541	664	0	781	-3268	6.28	6.28	12.57	12.57	3	0.15	0.03	0.11	0.00	0.00	24.0
38	25	-40855	-1200	640	0	847	2730	6.28	6.28	12.57	12.57	3	0.12	0.02	0.08	0.00	0.00	24.0
39	25	-39475	167	172	0	62	-269	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-37148	142	578	0	770	-216	6.28	6.28	12.57	12.57	3	0.03	0.01	0.04	0.00	0.00	24.0
2	38	-28325	360	462	0	571	-707	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
3	38	-28225	359	423	0	605	-704	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
4	38	-28925	-141	467	0	580	373	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
5	38	-28835	-142	428	0	614	375	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
6	38	-28645	186	509	0	535	-332	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
7	38	-28325	182	380	0	648	-324	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
8	38	-28825	36	510	0	537	-8	6.28	6.28	12.57	12.57	2	0.02	0.01	0.04	0.00	0.00	24.0
9	38	-28505	32	381	0	650	0	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
10	38	-28325	360	462	0	571	-707	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
11	38	-28225	359	423	0	605	-704	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
12	38	-28925	-141	467	0	580	373	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
13	38	-28835	-142	428	0	614	375	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
14	38	-28645	186	509	0	535	-332	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
15	38	-28325	182	380	0	648	-324	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
16	38	-28825	36	510	0	537	-8	6.28	6.28	12.57	12.57	2	0.02	0.01	0.04	0.00	0.00	24.0
17	38	-28505	32	381	0	650	0	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
18	38	-42898	1007	708	0	717	-1959	6.28	6.28	12.57	12.57	3	0.09	0.02	0.07	0.00	0.00	24.0
19	38	-42888	-638	694	0	758	1435	6.28	6.28	12.57	12.57	3	0.07	0.01	0.05	0.00	0.00	24.0
20	38	-42058	182	413	0	322	-262	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
37	38	-40768	1541	664	0	698	-3075	6.28	6.28	12.57	12.57	3	0.14	0.03	0.11	0.00	0.00	24.0
38	38	-40758	-1200	640	0	767	2580	6.28	6.28	12.57	12.57	3	0.12	0.02	0.08	0.00	0.00	24.0
39	38	-39378	167	172	0	40	-248	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-37050	142	578	0	698	-198	6.28	6.28	12.57	12.57	3	0.02	0.01	0.04	0.00	0.00	24.0
2	50	-28250	360	462	0	514	-662	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
3	50	-28150	359	423	0	552	-660	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
4	50	-28850	-141	467	0	522	355	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
5	50	-28760	-142	428	0	560	357	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
6	50	-28570	186	509	0	471	-309	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
7	50	-28250	182	380	0	600	-301	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
8	50	-28750	36	510	0	474	-4	6.28	6.28	12.57	12.57	2	0.02	0.01	0.04	0.00	0.00	24.0
9	50	-28430	32	381	0	603	4	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
10	50	-28250	360	462	0	514	-662	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
11	50	-28150	359	423	0	552	-660	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
12	50	-28850	-141	467	0	522	355	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
13	50	-28760	-142	428	0	560	357	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
14	50	-28570	186	509	0	471	-309	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
15	50	-28250	182	380	0	600	-301	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
16	50	-28750	36	510	0	474	-4	6.28	6.28	12.57	12.57	2	0.02	0.01	0.04	0.00	0.00	24.0
17	50	-28430	32	381	0	603	4	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
18	50	-42800	1007	708	0	628	-1833	6.28	6.28	12.57	12.57	3	0.08	0.02	0.07	0.00	0.00	24.0
19	50	-42790	-638	694	0	671	1355	6.28	6.28	12.57	12.57	3	0.06	0.01	0.05	0.00	0.00	24.0
20	50	-41960	182	413	0	270	-240	6.28	6.28	12.57	12.57	3	0.01	0.01	0.03	0.00	0.00	24.0
37	50	-40670	1541	664	0	615	-2883	6.28	6.28	12.57	12.57	3	0.13	0.03	0.11	0.00	0.00	24.0
38	50	-40660	-1200	640	0	687	2430	6.28	6.28	12.57	12.57	3	0.11	0.02	0.08	0.00	0.00	24.0
39	50	-39280	167	172	0	19	-227	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 85 NI 1033 NF 1037 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 15
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-37830	142	578	0	1276	-340	6.28	6.28	12.57	12.57	3	0.04	0.01	0.04	0.00	0.00	24.0
2	0	-28850	360	462	0	975	-1022	6.28	6.28	12.57	12.57	2	0.08	0.01	0.04	0.00	0.00	24.0
3	0	-28750	359	423	0	975	-1019	6.28	6.28	12.57	12.57	2	0.08	0.01	0.03	0.00	0.00	24.0
4	0	-29450	-141	467	0	988	496	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
5	0	-29360	-142	428	0	988	500	6.28	6.28	12.57	12.57	2	0.06	0.01	0.03	0.00	0.00	24.0
6	0	-29170	186	509	0	980	-495	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
7	0	-28850	182	380	0	980	-483	6.28	6.28	12.57	12.57	2	0.06	0.01	0.03	0.00	0.00	24.0
8	0	-29350	36	510	0	984	-39	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
9	0	-29030	32	381	0	984	-28	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
10	0	-28850	360	462	0	975	-1022	6.28	6.28	12.57	12.57	2	0.08	0.01	0.04	0.00	0.00	24.0
11	0	-28750	359	423	0	975	-1019	6.28	6.28	12.57	12.57	2	0.08	0.01	0.03	0.00	0.00	24.0
12	0	-29450	-141	467	0	988	496	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
13	0	-29360	-142	428	0	988	500	6.28	6.28	12.57	12.57	2	0.06	0.01	0.03	0.00	0.00	24.0
14	0	-29170	186	509	0	980	-495	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
15	0	-28850	182	380	0	980	-483	6.28	6.28	12.57	12.57	2	0.06	0.01	0.03	0.00	0.00	24.0
16	0	-29350	36	510	0	984	-39	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
17	0	-29030	32	381	0	984	-28	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
18	0	-43580	1007	708	0	1336	-2839	6.28	6.28	12.57	12.57	3	0.13	0.02	0.07	0.00	0.00	24.0
19	0	-43570	-638	694	0	1365	1993	6.28	6.28	12.57	12.57	3	0.10	0.01	0.05	0.00	0.00	24.0
20	0	-42740	182	413	0	683	-421	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
37	0	-41450	1541	664	0	1279	-4424	6.28	6.28	12.57	12.57	3	0.20	0.03	0.10	0.00	0.00	24.0
38	0	-41440	-1200	640	0	1327	3630	6.28	6.28	12.57	12.57	3	0.17	0.02	0.08	0.00	0.00	24.0
39	0	-40060	167	172	0	191	-394	6.28	6.28	12.57	12.57	3	0.02	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-37732	142	578	0	1204	-322	6.28	6.28	12.57	12.57	3	0.04	0.01	0.04	0.00	0.00	24.0
2	12	-28775	360	462	0	918	-977	6.28	6.28	12.57	12.57	2	0.07	0.01	0.04	0.00	0.00	24.0
3	12	-28675	359	423	0	922	-974	6.28	6.28	12.57	12.57	2	0.07	0.01	0.03	0.00	0.00	24.0
4	12	-29375	-141	467	0	930	478	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
5	12	-29285	-142	428	0	935	482	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
6	12	-29095	186	509	0	916	-472	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
7	12	-28775	182	380	0	933	-460	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
8	12	-29275	36	510	0	920	-35	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
9	12	-28955	32	381	0	936	-24	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
10	12	-28775	360	462	0	918	-977	6.28	6.28	12.57	12.57	2	0.07	0.01	0.04	0.00	0.00	24.0
11	12	-28675	359	423	0	922	-974	6.28	6.28	12.57	12.57	2	0.07	0.01	0.03	0.00	0.00	24.0
12	12	-29375	-141	467	0	930	478	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
13	12	-29285	-142	428	0	935	482	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
14	12	-29095	186	509	0	916	-472	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
15	12	-28775	182	380	0	933	-460	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
16	12	-29275	36	510	0	920	-35	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
17	12	-28955	32	381	0	936	-24	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
18	12	-43482	1007	708	0	1248	-2713	6.28	6.28	12.57	12.57	3	0.12	0.02	0.07	0.00	0.00	24.0
19	12	-43472	-638	694	0	1278	1913	6.28	6.28	12.57	12.57	3	0.09	0.01	0.05	0.00	0.00	24.0
20	12	-42642	182	413	0	632	-399	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
37	12	-41352	1541	664	0	1196	-4231	6.28	6.28	12.57	12.57	3	0.19	0.03	0.10	0.00	0.00	24.0
38	12	-41342	-1200	640	0	1247	3480	6.28	6.28	12.57	12.57	3	0.16	0.02	0.08	0.00	0.00	24.0
39	12	-39962	167	172	0	169	-373	6.28	6.28	12.57	12.57	3	0.02	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-37635	142	578	0	1132	-304	6.28	6.28	12.57	12.57	3	0.04	0.01	0.04	0.00	0.00	24.0
2	25	-28700	360	462	0	860	-932	6.28	6.28	12.57	12.57	2	0.07	0.01	0.04	0.00	0.00	24.0
3	25	-28600	359	423	0	870	-929	6.28	6.28	12.57	12.57	2	0.07	0.01	0.03	0.00	0.00	24.0
4	25	-29300	-141	467	0	872	461	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
5	25	-29210	-142	428	0	881	464	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
6	25	-29020	186	509	0	853	-448	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
7	25	-28700	182	380	0	885	-438	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
8	25	-29200	36	510	0	856	-31	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
9	25	-28880	32	381	0	889	-20	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
10	25	-28700	360	462	0	860	-932	6.28	6.28	12.57	12.57	2	0.07	0.01	0.04	0.00	0.00	24.0
11	25	-28600	359	423	0	870	-929	6.28	6.28	12.57	12.57	2	0.07	0.01	0.03	0.00	0.00	24.0
12	25	-29300	-141	467	0	872	461	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
13	25	-29210	-142	428	0	881	464	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
14	25	-29020	186	509	0	853	-448	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
15	25	-28700	182	380	0	885	-438	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
16	25	-29200	36	510	0	856	-31	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
17	25	-28880	32	381	0	889	-20	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
18	25	-43385	1007	708	0	1159	-2588	6.28	6.28	12.57	12.57	3	0.12	0.02	0.07	0.00	0.00	24.0
19	25	-43375	-638	694	0	1192	1834	6.28	6.28	12.57	12.57	3	0.09	0.01	0.05	0.00	0.00	24.0
20	25	-42545	182	413	0	580	-376	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
37	25	-41255	1541	664	0	1113	-4039	6.28	6.28	12.57	12.57	3	0.18	0.03	0.10	0.00	0.00	24.0
38	25	-41245	-1200	640	0	1167	3330	6.28	6.28	12.57	12.57	3	0.15	0.02	0.08	0.00	0.00	24.0
39	25	-39865	167	172	0	148	-353	6.28	6.28	12.57	12.57	3	0.02	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-37538	142	578	0	1059	-287	6.28	6.28	12.57	12.57	3	0.04	0.01	0.04	0.00	0.00	24.0
2	38	-28625	360	462	0	802	-887	6.28	6.28	12.57	12.57	2	0.07	0.01	0.04	0.00	0.00	24.0
3	38	-28525	359	423	0	817	-884	6.28	6.28	12.57	12.57	2	0.07	0.01	0.03	0.00	0.00	24.0
4	38	-29225	-141	467	0	813	443	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
5	38	-29135	-142	428	0	828	446	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
6	38	-28945	186	509	0	789	-425	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
7	38	-28625	182	380	0	838	-415	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
8	38	-29125	36	510	0	793	-26	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
9	38	-28805	32	381	0	841	-16	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
10	38	-28625	360	462	0	802	-887	6.28	6.28	12.57	12.57	2	0.07	0.01	0.04	0.00	0.00	24.0
11	38	-28525	359	423	0	817	-884	6.28	6.28	12.57	12.57	2	0.07	0.01	0.03	0.00	0.00	24.0
12	38	-29225	-141	467	0	813	443	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
13	38	-29135	-142	428	0	828	446	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
14	38	-28945	186	509	0	789	-425	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
15	38	-28625	182	380	0	838	-415	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
16	38	-29125	36	510	0	793	-26	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
17	38	-28805	32	381	0	841	-16	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
18	38	-43288	1007	708	0	1071	-2462	6.28	6.28	12.57	12.57	3	0.11	0.02	0.07	0.00	0.00	24.0
19	38	-43278	-638	694	0	1105	1754	6.28	6.28	12.57	12.57	3	0.08	0.01	0.05	0.00	0.00	24.0
20	38	-42448	182	413	0	528	-353	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
37	38	-41158	1541	664	0	1030	-3846	6.28	6.28	12.57	12.57	3	0.17	0.03	0.10	0.00	0.00	24.0
38	38	-41148	-1200	640	0	1087	3180	6.28	6.28	12.57	12.57	3	0.15	0.02	0.08	0.00	0.00	24.0
39	38	-39768	167	172	0	126	-332	6.28	6.28	12.57	12.57	3	0.02	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-37440	142	578	0	987	-269	6.28	6.28	12.57	12.57	3	0.03	0.01	0.04	0.00	0.00	24.0
2	50	-28550	360	462	0	744	-842	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
3	50	-28450	359	423	0	764	-839	6.28	6.28	12.57	12.57	2	0.06	0.01	0.03	0.00	0.00	24.0
4	50	-29150	-141	467	0	755	425	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
5	50	-29060	-142	428	0	774	428	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
6	50	-28870	186	509	0	726	-402	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
7	50	-28550	182	380	0	790	-392	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
8	50	-29050	36	510	0	729	-22	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
9	50	-28730	32	381	0	793	-12	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
10	50	-28550	360	462	0	744	-842	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
11	50	-28450	359	423	0	764	-839	6.28	6.28	12.57	12.57	2	0.06	0.01	0.03	0.00	0.00	24.0
12	50	-29150	-141	467	0	755	425	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
13	50	-29060	-142	428	0	774	428	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
14	50	-28870	186	509	0	726	-402	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
15	50	-28550	182	380	0	790	-392	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
16	50	-29050	36	510	0	729	-22	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
17	50	-28730	32	381	0	793	-12	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
18	50	-43190	1007	708	0	982	-2336	6.28	6.28	12.57	12.57	3	0.11	0.02	0.07	0.00	0.00	24.0
19	50	-43180	-638	694	0	1018	1674	6.28	6.28	12.57	12.57	3	0.08	0.01	0.05	0.00	0.00	24.0
20	50	-42350	182	413	0	477	-331	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
37	50	-41060	1541	664	0	947	-3653	6.28	6.28	12.57	12.57	3	0.17	0.03	0.10	0.00	0.00	24.0
38	50	-41050	-1200	640	0	1007	3030	6.28	6.28	12.57	12.57	3	0.14	0.02	0.08	0.00	0.00	24.0
39	50	-39670	167	172	0	105	-311	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 86 NI 1255 NF 1262 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 14
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-20000	18	-360	0	-997	-39	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
2	0	-15420	92	-308	0	-843	-323	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
3	0	-15340	91	-237	0	-668	-321	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
4	0	-15440	-63	-318	0	-865	260	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
5	0	-15350	-63	-246	0	-690	262	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
6	0	-15520	38	-395	0	-1055	-122	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
7	0	-15250	36	-156	0	-472	-114	6.28	6.28	12.57	12.57	2	0.03	0.00	0.01	0.00	0.00	24.0
8	0	-15520	-8	-398	0	-1062	53	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
9	0	-15260	-10	-159	0	-479	61	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
10	0	-15420	92	-308	0	-843	-323	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
11	0	-15340	91	-237	0	-668	-321	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
12	0	-15440	-63	-318	0	-865	260	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
13	0	-15350	-63	-246	0	-690	262	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
14	0	-15520	38	-395	0	-1055	-122	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
15	0	-15250	36	-156	0	-472	-114	6.28	6.28	12.57	12.57	2	0.03	0.00	0.01	0.00	0.00	24.0
16	0	-15520	-8	-398	0	-1062	53	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
17	0	-15260	-10	-159	0	-479	61	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
18	0	-21920	242	-666	0	-1763	-870	6.28	6.28	12.57	12.57	3	0.07	0.01	0.06	0.00	0.00	24.0
19	0	-21870	-241	-612	0	-1631	918	6.28	6.28	12.57	12.57	3	0.07	0.01	0.05	0.00	0.00	24.0
20	0	-21780	5	-799	0	-2144	8	6.28	6.28	12.57	12.57	3	0.07	0.01	0.07	0.00	0.00	24.0
37	0	-21040	409	-595	0	-1582	-1488	6.28	6.28	12.57	12.57	3	0.09	0.01	0.05	0.00	0.00	24.0
38	0	-20960	-396	-506	0	-1363	1493	6.28	6.28	12.57	12.57	3	0.09	0.01	0.04	0.00	0.00	24.0
39	0	-20810	14	-817	0	-2216	-23	6.28	6.28	12.57	12.57	3	0.07	0.01	0.07	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-19902	18	-360	0	-952	-37	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
2	12	-15345	92	-308	0	-804	-311	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
3	12	-15265	91	-237	0	-638	-309	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
4	12	-15365	-63	-318	0	-826	252	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
5	12	-15275	-63	-246	0	-660	254	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
6	12	-15445	38	-395	0	-1006	-117	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
7	12	-15175	36	-156	0	-452	-109	6.28	6.28	12.57	12.57	2	0.03	0.00	0.01	0.00	0.00	24.0
8	12	-15445	-8	-398	0	-1012	52	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
9	12	-15185	-10	-159	0	-459	60	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
10	12	-15345	92	-308	0	-804	-311	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
11	12	-15265	91	-237	0	-638	-309	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
12	12	-15365	-63	-318	0	-826	252	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
13	12	-15275	-63	-246	0	-660	254	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
14	12	-15445	38	-395	0	-1006	-117	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
15	12	-15175	36	-156	0	-452	-109	6.28	6.28	12.57	12.57	2	0.03	0.00	0.01	0.00	0.00	24.0
16	12	-15445	-8	-398	0	-1012	52	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
17	12	-15185	-10	-159	0	-459	60	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
18	12	-21822	242	-666	0	-1680	-840	6.28	6.28	12.57	12.57	3	0.07	0.01	0.06	0.00	0.00	24.0
19	12	-21772	-241	-612	0	-1555	888	6.28	6.28	12.57	12.57	3	0.07	0.01	0.05	0.00	0.00	24.0
20	12	-21682	5	-799	0	-2044	9	6.28	6.28	12.57	12.57	3	0.07	0.01	0.07	0.00	0.00	24.0
37	12	-20942	409	-595	0	-1508	-1437	6.28	6.28	12.57	12.57	3	0.09	0.01	0.05	0.00	0.00	24.0
38	12	-20862	-396	-506	0	-1300	1444	6.28	6.28	12.57	12.57	3	0.08	0.01	0.04	0.00	0.00	24.0
39	12	-20712	14	-817	0	-2114	-22	6.28	6.28	12.57	12.57	3	0.07	0.01	0.07	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-19805	18	-360	0	-907	-35	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
2	25	-15270	92	-308	0	-766	-300	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
3	25	-15190	91	-237	0	-609	-298	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
4	25	-15290	-63	-318	0	-786	244	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
5	25	-15200	-63	-246	0	-629	247	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
6	25	-15370	38	-395	0	-956	-112	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
7	25	-15100	36	-156	0	-433	-105	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
8	25	-15370	-8	-398	0	-962	51	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
9	25	-15110	-10	-159	0	-439	59	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
10	25	-15270	92	-308	0	-766	-300	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
11	25	-15190	91	-237	0	-609	-298	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
12	25	-15290	-63	-318	0	-786	244	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
13	25	-15200	-63	-246	0	-629	247	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
14	25	-15370	38	-395	0	-956	-112	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
15	25	-15100	36	-156	0	-433	-105	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
16	25	-15370	-8	-398	0	-962	51	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
17	25	-15110	-10	-159	0	-439	59	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
18	25	-21725	242	-666	0	-1597	-810	6.28	6.28	12.57	12.57	3	0.07	0.01	0.06	0.00	0.00	24.0
19	25	-21675	-241	-612	0	-1478	858	6.28	6.28	12.57	12.57	3	0.07	0.01	0.05	0.00	0.00	24.0
20	25	-21585	5	-799	0	-1944	9	6.28	6.28	12.57	12.57	3	0.06	0.01	0.07	0.00	0.00	24.0
37	25	-20845	409	-595	0	-1433	-1385	6.28	6.28	12.57	12.57	3	0.08	0.01	0.05	0.00	0.00	24.0
38	25	-20765	-396	-506	0	-1237	1394	6.28	6.28	12.57	12.57	3	0.08	0.01	0.04	0.00	0.00	24.0
39	25	-20615	14	-817	0	-2012	-20	6.28	6.28	12.57	12.57	3	0.07	0.01	0.07	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-19708	18	-360	0	-862	-32	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
2	38	-15195	92	-308	0	-727	-289	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
3	38	-15115	91	-237	0	-579	-286	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
4	38	-15215	-63	-318	0	-746	237	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
5	38	-15125	-63	-246	0	-598	239	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
6	38	-15295	38	-395	0	-907	-107	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
7	38	-15025	36	-156	0	-413	-100	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
8	38	-15295	-8	-398	0	-912	50	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
9	38	-15035	-10	-159	0	-419	57	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
10	38	-15195	92	-308	0	-727	-289	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
11	38	-15115	91	-237	0	-579	-286	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
12	38	-15215	-63	-318	0	-746	237	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
13	38	-15125	-63	-246	0	-598	239	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
14	38	-15295	38	-395	0	-907	-107	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
15	38	-15025	36	-156	0	-413	-100	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
16	38	-15295	-8	-398	0	-912	50	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
17	38	-15035	-10	-159	0	-419	57	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
18	38	-21628	242	-666	0	-1513	-780	6.28	6.28	12.57	12.57	3	0.07	0.01	0.06	0.00	0.00	24.0
19	38	-21578	-241	-612	0	-1402	828	6.28	6.28	12.57	12.57	3	0.06	0.01	0.05	0.00	0.00	24.0
20	38	-21488	5	-799	0	-1844	10	6.28	6.28	12.57	12.57	3	0.06	0.01	0.07	0.00	0.00	24.0
37	38	-20748	409	-595	0	-1358	-1334	6.28	6.28	12.57	12.57	3	0.08	0.01	0.05	0.00	0.00	24.0
38	38	-20668	-396	-506	0	-1173	1345	6.28	6.28	12.57	12.57	3	0.08	0.01	0.04	0.00	0.00	24.0
39	38	-20518	14	-817	0	-1910	-18	6.28	6.28	12.57	12.57	3	0.06	0.01	0.07	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-19610	18	-360	0	-816	-30	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
2	50	-15120	92	-308	0	-689	-277	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
3	50	-15040	91	-237	0	-550	-275	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
4	50	-15140	-63	-318	0	-707	229	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
5	50	-15050	-63	-246	0	-567	231	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
6	50	-15220	38	-395	0	-857	-102	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
7	50	-14950	36	-156	0	-394	-96	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
8	50	-15220	-8	-398	0	-862	49	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
9	50	-14960	-10	-159	0	-399	56	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
10	50	-15120	92	-308	0	-689	-277	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
11	50	-15040	91	-237	0	-550	-275	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
12	50	-15140	-63	-318	0	-707	229	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
13	50	-15050	-63	-246	0	-567	231	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
14	50	-15220	38	-395	0	-857	-102	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
15	50	-14950	36	-156	0	-394	-96	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
16	50	-15220	-8	-398	0	-862	49	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
17	50	-14960	-10	-159	0	-399	56	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
18	50	-21530	242	-666	0	-1430	-749	6.28	6.28	12.57	12.57	3	0.06	0.01	0.06	0.00	0.00	24.0
19	50	-21480	-241	-612	0	-1325	798	6.28	6.28	12.57	12.57	3	0.06	0.01	0.05	0.00	0.00	24.0
20	50	-21390	5	-799	0	-1744	11	6.28	6.28	12.57	12.57	3	0.06	0.01	0.07	0.00	0.00	24.0
37	50	-20650	409	-595	0	-1284	-1283	6.28	6.28	12.57	12.57	3	0.08	0.01	0.05	0.00	0.00	24.0
38	50	-20570	-396	-506	0	-1110	1295	6.28	6.28	12.57	12.57	3	0.07	0.01	0.04	0.00	0.00	24.0
39	50	-20420	14	-817	0	-1808	-16	6.28	6.28	12.57	12.57	3	0.06	0.01	0.07	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 87 NI 1262 NF 128 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 14A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
													Fx,M	Bielle	V,Mx			
	cm		daN			daN*m				cmq						cmq/m		cm
1	0	-19610	18	-360	0	-816	-30	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
2	0	-15120	92	-308	0	-689	-277	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
3	0	-15040	91	-237	0	-550	-275	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
4	0	-15140	-63	-318	0	-707	229	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
5	0	-15050	-63	-246	0	-567	231	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
6	0	-15220	38	-395	0	-857	-102	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
7	0	-14950	36	-156	0	-394	-96	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
8	0	-15220	-8	-398	0	-862	49	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
9	0	-14960	-10	-159	0	-399	56	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
10	0	-15120	92	-308	0	-689	-277	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
11	0	-15040	91	-237	0	-550	-275	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
12	0	-15140	-63	-318	0	-707	229	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
13	0	-15050	-63	-246	0	-567	231	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
14	0	-15220	38	-395	0	-857	-102	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
15	0	-14950	36	-156	0	-394	-96	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
16	0	-15220	-8	-398	0	-862	49	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
17	0	-14960	-10	-159	0	-399	56	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
18	0	-21530	242	-666	0	-1430	-749	6.28	6.28	12.57	12.57	3	0.06	0.01	0.06	0.00	0.00	24.0
19	0	-21480	-241	-612	0	-1325	798	6.28	6.28	12.57	12.57	3	0.06	0.01	0.05	0.00	0.00	24.0
20	0	-21390	5	-799	0	-1744	11	6.28	6.28	12.57	12.57	3	0.06	0.01	0.07	0.00	0.00	24.0
37	0	-20650	409	-595	0	-1284	-1283	6.28	6.28	12.57	12.57	3	0.08	0.01	0.05	0.00	0.00	24.0
38	0	-20570	-396	-506	0	-1110	1295	6.28	6.28	12.57	12.57	3	0.07	0.01	0.04	0.00	0.00	24.0
39	0	-20420	14	-817	0	-1808	-16	6.28	6.28	12.57	12.57	3	0.06	0.01	0.07	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-19512	18	-360	0	-771	-28	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
2	12	-15045	92	-308	0	-650	-266	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
3	12	-14965	91	-237	0	-520	-264	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
4	12	-15065	-63	-318	0	-667	221	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
5	12	-14975	-63	-246	0	-537	223	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
6	12	-15145	38	-395	0	-808	-98	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
7	12	-14875	36	-156	0	-374	-91	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
8	12	-15145	-8	-398	0	-813	48	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
9	12	-14885	-10	-159	0	-379	55	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
10	12	-15045	92	-308	0	-650	-266	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
11	12	-14965	91	-237	0	-520	-264	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
12	12	-15065	-63	-318	0	-667	221	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
13	12	-14975	-63	-246	0	-537	223	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
14	12	-15145	38	-395	0	-808	-98	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
15	12	-14875	36	-156	0	-374	-91	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
16	12	-15145	-8	-398	0	-813	48	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
17	12	-14885	-10	-159	0	-379	55	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
18	12	-21432	242	-666	0	-1347	-719	6.28	6.28	12.57	12.57	3	0.06	0.01	0.06	0.00	0.00	24.0
19	12	-21382	-241	-612	0	-1249	768	6.28	6.28	12.57	12.57	3	0.06	0.01	0.05	0.00	0.00	24.0
20	12	-21292	5	-799	0	-1644	11	6.28	6.28	12.57	12.57	3	0.05	0.01	0.07	0.00	0.00	24.0
37	12	-20552	409	-595	0	-1210	-1232	6.28	6.28	12.57	12.57	3	0.07	0.01	0.05	0.00	0.00	24.0
38	12	-20472	-396	-506	0	-1047	1246	6.28	6.28	12.57	12.57	3	0.07	0.01	0.04	0.00	0.00	24.0
39	12	-20322	14	-817	0	-1706	-15	6.28	6.28	12.57	12.57	3	0.06	0.01	0.07	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-19415	18	-360	0	-726	-25	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
2	25	-14970	92	-308	0	-612	-254	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
3	25	-14890	91	-237	0	-490	-252	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
4	25	-14990	-63	-318	0	-627	213	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
5	25	-14900	-63	-246	0	-506	215	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
6	25	-15070	38	-395	0	-758	-93	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
7	25	-14800	36	-156	0	-355	-87	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
8	25	-15070	-8	-398	0	-763	47	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
9	25	-14810	-10	-159	0	-359	54	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
10	25	-14970	92	-308	0	-612	-254	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
11	25	-14890	91	-237	0	-490	-252	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
12	25	-14990	-63	-318	0	-627	213	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
13	25	-14900	-63	-246	0	-506	215	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
14	25	-15070	38	-395	0	-758	-93	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
15	25	-14800	36	-156	0	-355	-87	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
16	25	-15070	-8	-398	0	-763	47	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
17	25	-14810	-10	-159	0	-359	54	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
18	25	-21335	242	-666	0	-1264	-689	6.28	6.28	12.57	12.57	3	0.06	0.01	0.06	0.00	0.00	24.0
19	25	-21285	-241	-612	0	-1172	738	6.28	6.28	12.57	12.57	3	0.05	0.01	0.05	0.00	0.00	24.0
20	25	-21195	5	-799	0	-1544	12	6.28	6.28	12.57	12.57	3	0.05	0.01	0.07	0.00	0.00	24.0
37	25	-20455	409	-595	0	-1135	-1181	6.28	6.28	12.57	12.57	3	0.07	0.01	0.05	0.00	0.00	24.0
38	25	-20375	-396	-506	0	-983	1196	6.28	6.28	12.57	12.57	3	0.07	0.01	0.04	0.00	0.00	24.0

39	25	-20225	14	-817	0	-1604	-13	6.28	6.28	12.57	12.57	3	0.05	0.01	0.07	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-19318	18	-360	0	-681	-23	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
2	38	-14895	92	-308	0	-573	-243	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
3	38	-14815	91	-237	0	-461	-241	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
4	38	-14915	-63	-318	0	-587	205	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
5	38	-14825	-63	-246	0	-475	207	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
6	38	-14995	38	-395	0	-709	-88	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
7	38	-14725	36	-156	0	-335	-82	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
8	38	-14995	-8	-398	0	-713	46	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
9	38	-14735	-10	-159	0	-339	52	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
10	38	-14895	92	-308	0	-573	-243	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
11	38	-14815	91	-237	0	-461	-241	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
12	38	-14915	-63	-318	0	-587	205	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
13	38	-14825	-63	-246	0	-475	207	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
14	38	-14995	38	-395	0	-709	-88	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
15	38	-14725	36	-156	0	-335	-82	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
16	38	-14995	-8	-398	0	-713	46	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
17	38	-14735	-10	-159	0	-339	52	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
18	38	-21238	242	-666	0	-1180	-659	6.28	6.28	12.57	12.57	3	0.05	0.01	0.06	0.00	0.00	24.0
19	38	-21188	-241	-612	0	-1096	707	6.28	6.28	12.57	12.57	3	0.05	0.01	0.05	0.00	0.00	24.0
20	38	-21098	5	-799	0	-1445	13	6.28	6.28	12.57	12.57	3	0.05	0.01	0.07	0.00	0.00	24.0
37	38	-20358	409	-595	0	-1061	-1130	6.28	6.28	12.57	12.57	3	0.07	0.01	0.05	0.00	0.00	24.0
38	38	-20278	-396	-506	0	-920	1147	6.28	6.28	12.57	12.57	3	0.06	0.01	0.04	0.00	0.00	24.0
39	38	-20128	14	-817	0	-1501	-11	6.28	6.28	12.57	12.57	3	0.05	0.01	0.07	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-19220	18	-360	0	-636	-21	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
2	50	-14820	92	-308	0	-534	-231	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
3	50	-14740	91	-237	0	-431	-230	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
4	50	-14840	-63	-318	0	-548	197	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
5	50	-14750	-63	-246	0	-445	199	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
6	50	-14920	38	-395	0	-660	-83	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
7	50	-14650	36	-156	0	-316	-78	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
8	50	-14920	-8	-398	0	-663	45	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
9	50	-14660	-10	-159	0	-320	51	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
10	50	-14820	92	-308	0	-534	-231	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
11	50	-14740	91	-237	0	-431	-230	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
12	50	-14840	-63	-318	0	-548	197	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
13	50	-14750	-63	-246	0	-445	199	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
14	50	-14920	38	-395	0	-660	-83	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
15	50	-14650	36	-156	0	-316	-78	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
16	50	-14920	-8	-398	0	-663	45	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
17	50	-14660	-10	-159	0	-320	51	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
18	50	-21140	242	-666	0	-1097	-628	6.28	6.28	12.57	12.57	3	0.05	0.01	0.06	0.00	0.00	24.0
19	50	-21090	-241	-612	0	-1019	677	6.28	6.28	12.57	12.57	3	0.05	0.01	0.05	0.00	0.00	24.0
20	50	-21000	5	-799	0	-1345	13	6.28	6.28	12.57	12.57	3	0.05	0.01	0.07	0.00	0.00	24.0
37	50	-20260	409	-595	0	-987	-1079	6.28	6.28	12.57	12.57	3	0.06	0.01	0.05	0.00	0.00	24.0
38	50	-20180	-396	-506	0	-857	1098	6.28	6.28	12.57	12.57	3	0.06	0.01	0.04	0.00	0.00	24.0
39	50	-20030	14	-817	0	-1399	-9	6.28	6.28	12.57	12.57	3	0.05	0.01	0.07	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 88 NI 1168 NF 211 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 13A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-6916	-144	225	0	-1036	-7	6.28	6.28	9.42	9.42	3	0.05	0.01	0.03	0.00	0.00	24.0
2	0	-5327	-262	186	0	-824	-9	6.28	6.28	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
3	0	-5310	-258	162	0	-768	-9	6.28	6.28	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
4	0	-5330	37	185	0	-826	-2	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
5	0	-5313	40	160	0	-770	-2	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
6	0	-5348	-160	215	0	-891	-7	6.28	6.28	9.42	9.42	2	0.06	0.01	0.03	0.00	0.00	24.0
7	0	-5291	-150	132	0	-703	-6	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
8	0	-5349	-71	214	0	-891	-5	6.28	6.28	9.42	9.42	2	0.06	0.00	0.03	0.00	0.00	24.0
9	0	-5292	-61	132	0	-704	-5	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
10	0	-5327	-262	186	0	-824	-9	6.28	6.28	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
11	0	-5310	-258	162	0	-768	-9	6.28	6.28	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
12	0	-5330	37	185	0	-826	-2	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
13	0	-5313	40	160	0	-770	-2	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
14	0	-5348	-160	215	0	-891	-7	6.28	6.28	9.42	9.42	2	0.06	0.01	0.03	0.00	0.00	24.0
15	0	-5291	-150	132	0	-703	-6	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
16	0	-5349	-71	214	0	-891	-5	6.28	6.28	9.42	9.42	2	0.06	0.00	0.03	0.00	0.00	24.0
17	0	-5292	-61	132	0	-704	-5	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
18	0	-7365	-539	353	0	-1373	-17	6.28	6.28	9.42	9.42	3	0.07	0.01	0.05	0.00	0.00	24.0
19	0	-7354	348	323	0	-1323	3	6.28	6.28	9.42	9.42	3	0.06	0.01	0.04	0.00	0.00	24.0
20	0	-7418	-110	418	0	-1521	-8	6.28	6.28	9.42	9.42	3	0.07	0.01	0.05	0.00	0.00	24.0
37	0	-7156	-850	323	0	-1272	-23	6.28	6.28	9.42	9.42	3	0.06	0.02	0.09	0.00	0.00	24.0
38	0	-7139	628	274	0	-1189	9	6.28	6.28	9.42	9.42	3	0.06	0.02	0.06	0.00	0.00	24.0
39	0	-7246	-136	433	0	-1519	-8	6.28	6.28	9.42	9.42	3	0.07	0.01	0.05	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-6843	-144	225	0	-1064	-25	6.28	6.28	9.42	9.42	3	0.05	0.01	0.03	0.00	0.00	24.0
2	12	-5271	-262	186	0	-847	-42	6.28	6.28	9.42	9.42	2	0.06	0.01	0.03	0.00	0.00	24.0
3	12	-5254	-258	162	0	-788	-41	6.28	6.28	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
4	12	-5274	37	185	0	-849	2	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
5	12	-5257	40	160	0	-790	3	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
6	12	-5292	-160	215	0	-917	-27	6.28	6.28	9.42	9.42	2	0.06	0.01	0.03	0.00	0.00	24.0
7	12	-5235	-150	132	0	-720	-25	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
8	12	-5293	-71	214	0	-918	-14	6.28	6.28	9.42	9.42	2	0.06	0.00	0.03	0.00	0.00	24.0
9	12	-5236	-61	132	0	-720	-12	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
10	12	-5271	-262	186	0	-847	-42	6.28	6.28	9.42	9.42	2	0.06	0.01	0.03	0.00	0.00	24.0
11	12	-5254	-258	162	0	-788	-41	6.28	6.28	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
12	12	-5274	37	185	0	-849	2	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
13	12	-5257	40	160	0	-790	3	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
14	12	-5292	-160	215	0	-917	-27	6.28	6.28	9.42	9.42	2	0.06	0.01	0.03	0.00	0.00	24.0
15	12	-5235	-150	132	0	-720	-25	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
16	12	-5293	-71	214	0	-918	-14	6.28	6.28	9.42	9.42	2	0.06	0.00	0.03	0.00	0.00	24.0
17	12	-5236	-61	132	0	-720	-12	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
18	12	-7292	-539	353	0	-1417	-84	6.28	6.28	9.42	9.42	3	0.07	0.01	0.05	0.00	0.00	24.0

19	12	-7281	348	323	0	-1364	46	6.28	6.28	9.42	9.42	3	0.07	0.01	0.04	0.00	0.00	24.0
20	12	-7345	-110	418	0	-1574	-22	6.28	6.28	9.42	9.42	3	0.07	0.01	0.05	0.00	0.00	24.0
37	12	-7083	-850	323	0	-1312	-130	6.28	6.28	9.42	9.42	3	0.06	0.02	0.09	0.00	0.00	24.0
38	12	-7066	628	274	0	-1223	88	6.28	6.28	9.42	9.42	3	0.06	0.02	0.06	0.00	0.00	24.0
39	12	-7173	-136	433	0	-1573	-25	6.28	6.28	9.42	9.42	3	0.07	0.01	0.05	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-6770	-144	225	0	-1093	-43	6.28	6.28	9.42	9.42	3	0.05	0.01	0.03	0.00	0.00	24.0
2	25	-5214	-262	186	0	-871	-74	6.28	6.28	9.42	9.42	2	0.06	0.01	0.03	0.00	0.00	24.0
3	25	-5198	-258	162	0	-808	-73	6.28	6.28	9.42	9.42	2	0.06	0.01	0.03	0.00	0.00	24.0
4	25	-5218	37	185	0	-872	7	6.28	6.28	9.42	9.42	2	0.06	0.00	0.02	0.00	0.00	24.0
5	25	-5200	40	160	0	-810	8	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
6	25	-5236	-160	215	0	-944	-47	6.28	6.28	9.42	9.42	2	0.06	0.01	0.03	0.00	0.00	24.0
7	25	-5178	-150	132	0	-736	-44	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
8	25	-5236	-71	214	0	-945	-22	6.28	6.28	9.42	9.42	2	0.06	0.00	0.03	0.00	0.00	24.0
9	25	-5180	-61	132	0	-736	-20	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
10	25	-5214	-262	186	0	-871	-74	6.28	6.28	9.42	9.42	2	0.06	0.01	0.03	0.00	0.00	24.0
11	25	-5198	-258	162	0	-808	-73	6.28	6.28	9.42	9.42	2	0.06	0.01	0.03	0.00	0.00	24.0
12	25	-5218	37	185	0	-872	7	6.28	6.28	9.42	9.42	2	0.06	0.00	0.02	0.00	0.00	24.0
13	25	-5200	40	160	0	-810	8	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
14	25	-5236	-160	215	0	-944	-47	6.28	6.28	9.42	9.42	2	0.06	0.01	0.03	0.00	0.00	24.0
15	25	-5178	-150	132	0	-736	-44	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
16	25	-5236	-71	214	0	-945	-22	6.28	6.28	9.42	9.42	2	0.06	0.00	0.03	0.00	0.00	24.0
17	25	-5180	-61	132	0	-736	-20	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
18	25	-7218	-539	353	0	-1462	-151	6.28	6.28	9.42	9.42	3	0.07	0.01	0.05	0.00	0.00	24.0
19	25	-7208	348	323	0	-1404	90	6.28	6.28	9.42	9.42	3	0.07	0.01	0.04	0.00	0.00	24.0
20	25	-7272	-110	418	0	-1626	-35	6.28	6.28	9.42	9.42	3	0.08	0.01	0.05	0.00	0.00	24.0
37	25	-7010	-850	323	0	-1353	-236	6.28	6.28	9.42	9.42	3	0.07	0.02	0.09	0.00	0.00	24.0
38	25	-6993	628	274	0	-1258	166	6.28	6.28	9.42	9.42	3	0.06	0.02	0.06	0.00	0.00	24.0
39	25	-7100	-136	433	0	-1628	-42	6.28	6.28	9.42	9.42	3	0.08	0.01	0.05	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-6697	-144	225	0	-1121	-61	6.28	6.28	9.42	9.42	3	0.05	0.01	0.03	0.00	0.00	24.0
2	38	-5158	-262	186	0	-894	-107	6.28	6.28	9.42	9.42	2	0.06	0.01	0.03	0.00	0.00	24.0
3	38	-5141	-258	162	0	-828	-106	6.28	6.28	9.42	9.42	2	0.06	0.01	0.03	0.00	0.00	24.0
4	38	-5161	37	185	0	-896	12	6.28	6.28	9.42	9.42	2	0.06	0.00	0.02	0.00	0.00	24.0
5	38	-5144	40	160	0	-830	13	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
6	38	-5179	-160	215	0	-971	-67	6.28	6.28	9.42	9.42	2	0.07	0.01	0.03	0.00	0.00	24.0
7	38	-5122	-150	132	0	-753	-63	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
8	38	-5180	-71	214	0	-971	-31	6.28	6.28	9.42	9.42	2	0.06	0.00	0.03	0.00	0.00	24.0
9	38	-5123	-61	132	0	-753	-27	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
10	38	-5158	-262	186	0	-894	-107	6.28	6.28	9.42	9.42	2	0.06	0.01	0.03	0.00	0.00	24.0
11	38	-5141	-258	162	0	-828	-106	6.28	6.28	9.42	9.42	2	0.06	0.01	0.03	0.00	0.00	24.0
12	38	-5161	37	185	0	-896	12	6.28	6.28	9.42	9.42	2	0.06	0.00	0.02	0.00	0.00	24.0
13	38	-5144	40	160	0	-830	13	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
14	38	-5179	-160	215	0	-971	-67	6.28	6.28	9.42	9.42	2	0.07	0.01	0.03	0.00	0.00	24.0
15	38	-5122	-150	132	0	-753	-63	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
16	38	-5180	-71	214	0	-971	-31	6.28	6.28	9.42	9.42	2	0.06	0.00	0.03	0.00	0.00	24.0
17	38	-5123	-61	132	0	-753	-27	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
18	38	-7145	-539	353	0	-1506	-219	6.28	6.28	9.42	9.42	3	0.07	0.01	0.05	0.00	0.00	24.0
19	38	-7135	348	323	0	-1444	133	6.28	6.28	9.42	9.42	3	0.07	0.01	0.04	0.00	0.00	24.0
20	38	-7199	-110	418	0	-1678	-49	6.28	6.28	9.42	9.42	3	0.08	0.01	0.05	0.00	0.00	24.0
37	38	-6937	-850	323	0	-1394	-342	6.28	6.28	9.42	9.42	3	0.08	0.02	0.09	0.00	0.00	24.0
38	38	-6920	628	274	0	-1292	245	6.28	6.28	9.42	9.42	3	0.07	0.02	0.06	0.00	0.00	24.0
39	38	-7026	-136	433	0	-1682	-59	6.28	6.28	9.42	9.42	3	0.08	0.01	0.05	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-6624	-144	225	0	-1149	-79	6.28	6.28	9.42	9.42	3	0.06	0.01	0.03	0.00	0.00	24.0
2	50	-5102	-262	186	0	-917	-140	6.28	6.28	9.42	9.42	2	0.07	0.01	0.03	0.00	0.00	24.0
3	50	-5085	-258	162	0	-849	-138	6.28	6.28	9.42	9.42	2	0.06	0.01	0.03	0.00	0.00	24.0
4	50	-5105	37	185	0	-919	16	6.28	6.28	9.42	9.42	2	0.06	0.00	0.02	0.00	0.00	24.0
5	50	-5088	40	160	0	-850	18	6.28	6.28	9.42	9.42	2	0.06	0.00	0.02	0.00	0.00	24.0
6	50	-5123	-160	215	0	-998	-87	6.28	6.28	9.42	9.42	2	0.07	0.01	0.03	0.00	0.00	24.0
7	50	-5066	-150	132	0	-769	-82	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
8	50	-5124	-71	214	0	-998	-40	6.28	6.28	9.42	9.42	2	0.07	0.01	0.03	0.00	0.00	24.0
9	50	-5067	-61	132	0	-769	-35	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
10	50	-5102	-262	186	0	-917	-140	6.28	6.28	9.42	9.42	2	0.07	0.01	0.03	0.00	0.00	24.0
11	50	-5085	-258	162	0	-849	-138	6.28	6.28	9.42	9.42	2	0.06	0.01	0.03	0.00	0.00	24.0
12	50	-5105	37	185	0	-919	16	6.28	6.28	9.42	9.42	2	0.06	0.00	0.02	0.00	0.00	24.0
13	50	-5088	40	160	0	-850	18	6.28	6.28	9.42	9.42	2	0.06	0.00	0.02	0.00	0.00	24.0
14	50	-5123	-160	215	0	-998	-87	6.28	6.28	9.42	9.42	2	0.07	0.01	0.03	0.00	0.00	24.0
15	50	-5066	-150	132	0	-769	-82	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
16	50	-5124	-71	214	0	-998	-40	6.28	6.28	9.42	9.42	2	0.07	0.01	0.03	0.00	0.00	24.0
17	50	-5067	-61	132	0	-769	-35	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
18	50	-7072	-539	353	0	-1550	-286	6.28	6.28	9.42	9.42	3	0.08	0.01	0.05	0.00	0.00	24.0
19	50	-7062	348	323	0	-1485	177	6.28	6.28	9.42	9.42	3	0.07	0.01	0.04	0.00	0.00	24.0
20	50	-7126	-110	418	0	-1731	-63	6.28	6.28	9.42	9.42	3	0.08	0.01	0.05	0.00	0.00	24.0
37	50	-6864	-850	323	0	-1434	-448	6.28	6.28	9.42	9.42	3	0.08	0.02	0.09	0.00	0.00	24.0
38	50	-6847	628	274	0	-1326	323	6.28	6.28	9.42	9.42	3	0.07	0.02	0.06	0.00	0.00	24.0
39	50	-6953	-136	433	0	-1736	-76	6.28	6.28	9.42	9.42	3	0.08	0.01	0.05	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 89 NI 1160 NF 1168 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 13
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-4796	-43	-409	0	-1313	14	6.28	6.28	9.42	9.42	3	0.06	0.01	0.05	0.00	0.00	24.0
2	0	-3690	-60	-316	0	-1038	21	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
3	0	-3685	-60	-307	0	-976	21	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
4	0	-3694	-7	-322	0	-1043	1	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
5	0	-3689	-7	-313	0	-981	1	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
6	0	-3698	-42	-330	0	-1113	14	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
7	0	-3680	-41	-298	0	-905	14	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
8	0	-3699	-26	-331	0	-1115	8	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
9	0	-3681	-25	-299	0	-906	8	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
10	0	-3690	-60	-316	0	-1038	21	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
11	0	-3685	-60	-307	0	-976	21	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
12	0	-3694	-7	-322	0	-1043	1	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
13	0	-3689	-7	-313	0	-981	1	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
14	0	-3698	-42	-330	0	-1113	14	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0

15	0	-3680	-41	-298	0	-905	14	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
16	0	-3699	-26	-331	0	-1115	8	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
17	0	-3681	-25	-299	0	-906	8	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
18	0	-5046	-121	-483	0	-1700	44	6.28	6.28	9.42	9.42	3	0.08	0.01	0.06	0.00	0.00	24.0
19	0	-5047	39	-491	0	-1653	-17	6.28	6.28	9.42	9.42	3	0.08	0.01	0.06	0.00	0.00	24.0
20	0	-5071	-46	-502	0	-1863	15	6.28	6.28	9.42	9.42	3	0.09	0.01	0.06	0.00	0.00	24.0
37	0	-4924	-175	-446	0	-1576	64	6.28	6.28	9.42	9.42	3	0.08	0.01	0.06	0.00	0.00	24.0
38	0	-4926	92	-460	0	-1497	-37	6.28	6.28	9.42	9.42	3	0.07	0.01	0.06	0.00	0.00	24.0
39	0	-4965	-49	-479	0	-1847	16	6.28	6.28	9.42	9.42	3	0.09	0.01	0.06	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-4723	-43	-409	0	-1262	9	6.28	6.28	9.42	9.42	3	0.06	0.01	0.05	0.00	0.00	24.0
2	12	-3634	-60	-316	0	-999	14	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
3	12	-3629	-60	-307	0	-937	14	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
4	12	-3638	-7	-322	0	-1003	0	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
5	12	-3633	-7	-313	0	-942	0	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
6	12	-3642	-42	-330	0	-1072	9	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
7	12	-3624	-41	-298	0	-867	9	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
8	12	-3643	-26	-331	0	-1073	5	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
9	12	-3625	-25	-299	0	-869	5	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
10	12	-3634	-60	-316	0	-999	14	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
11	12	-3629	-60	-307	0	-937	14	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
12	12	-3638	-7	-322	0	-1003	0	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
13	12	-3633	-7	-313	0	-942	0	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
14	12	-3642	-42	-330	0	-1072	9	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
15	12	-3624	-41	-298	0	-867	9	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
16	12	-3643	-26	-331	0	-1073	5	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
17	12	-3625	-25	-299	0	-869	5	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
18	12	-4973	-121	-483	0	-1640	29	6.28	6.28	9.42	9.42	3	0.08	0.01	0.06	0.00	0.00	24.0
19	12	-4974	39	-491	0	-1592	-12	6.28	6.28	9.42	9.42	3	0.08	0.01	0.06	0.00	0.00	24.0
20	12	-4998	-46	-502	0	-1800	10	6.28	6.28	9.42	9.42	3	0.09	0.01	0.06	0.00	0.00	24.0
37	12	-4851	-175	-446	0	-1520	42	6.28	6.28	9.42	9.42	3	0.07	0.01	0.06	0.00	0.00	24.0
38	12	-4853	92	-460	0	-1439	-25	6.28	6.28	9.42	9.42	3	0.07	0.01	0.06	0.00	0.00	24.0
39	12	-4892	-49	-479	0	-1787	10	6.28	6.28	9.42	9.42	3	0.09	0.01	0.06	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-4650	-43	-409	0	-1210	4	6.28	6.28	9.42	9.42	3	0.06	0.01	0.05	0.00	0.00	24.0
2	25	-3578	-60	-316	0	-959	6	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
3	25	-3572	-60	-307	0	-899	6	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
4	25	-3582	-7	-322	0	-963	-1	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
5	25	-3576	-7	-313	0	-903	-1	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
6	25	-3586	-42	-330	0	-1031	4	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
7	25	-3568	-41	-298	0	-830	4	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
8	25	-3586	-26	-331	0	-1032	2	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
9	25	-3568	-25	-299	0	-831	2	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
10	25	-3578	-60	-316	0	-959	6	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
11	25	-3572	-60	-307	0	-899	6	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
12	25	-3582	-7	-322	0	-963	-1	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
13	25	-3576	-7	-313	0	-903	-1	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
14	25	-3586	-42	-330	0	-1031	4	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
15	25	-3568	-41	-298	0	-830	4	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
16	25	-3586	-26	-331	0	-1032	2	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
17	25	-3568	-25	-299	0	-831	2	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
18	25	-4900	-121	-483	0	-1580	14	6.28	6.28	9.42	9.42	3	0.08	0.01	0.06	0.00	0.00	24.0
19	25	-4901	39	-491	0	-1531	-7	6.28	6.28	9.42	9.42	3	0.07	0.01	0.06	0.00	0.00	24.0
20	25	-4924	-46	-502	0	-1737	4	6.28	6.28	9.42	9.42	3	0.08	0.01	0.06	0.00	0.00	24.0
37	25	-4778	-175	-446	0	-1465	21	6.28	6.28	9.42	9.42	3	0.07	0.01	0.06	0.00	0.00	24.0
38	25	-4780	92	-460	0	-1382	-14	6.28	6.28	9.42	9.42	3	0.07	0.01	0.06	0.00	0.00	24.0
39	25	-4819	-49	-479	0	-1727	4	6.28	6.28	9.42	9.42	3	0.08	0.01	0.06	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-4577	-43	-409	0	-1159	-2	6.28	6.28	9.42	9.42	3	0.06	0.01	0.05	0.00	0.00	24.0
2	38	-3521	-60	-316	0	-920	-1	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
3	38	-3516	-60	-307	0	-861	-1	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
4	38	-3525	-7	-322	0	-922	-2	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
5	38	-3520	-7	-313	0	-864	-2	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
6	38	-3529	-42	-330	0	-989	-1	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
7	38	-3511	-41	-298	0	-793	-1	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
8	38	-3530	-26	-331	0	-990	-1	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
9	38	-3512	-25	-299	0	-794	-1	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
10	38	-3521	-60	-316	0	-920	-1	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
11	38	-3516	-60	-307	0	-861	-1	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
12	38	-3525	-7	-322	0	-922	-2	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
13	38	-3520	-7	-313	0	-864	-2	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
14	38	-3529	-42	-330	0	-989	-1	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
15	38	-3511	-41	-298	0	-793	-1	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
16	38	-3530	-26	-331	0	-990	-1	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
17	38	-3512	-25	-299	0	-794	-1	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
18	38	-4827	-121	-483	0	-1519	-2	6.28	6.28	9.42	9.42	3	0.07	0.01	0.06	0.00	0.00	24.0
19	38	-4828	39	-491	0	-1469	-2	6.28	6.28	9.42	9.42	3	0.07	0.01	0.06	0.00	0.00	24.0
20	38	-4851	-46	-502	0	-1674	-2	6.28	6.28	9.42	9.42	3	0.08	0.01	0.06	0.00	0.00	24.0
37	38	-4705	-175	-446	0	-1409	-1	6.28	6.28	9.42	9.42	3	0.07	0.01	0.06	0.00	0.00	24.0
38	38	-4707	92	-460	0	-1324	-2	6.28	6.28	9.42	9.42	3	0.06	0.01	0.06	0.00	0.00	24.0
39	38	-4746	-49	-479	0	-1667	-2	6.28	6.28	9.42	9.42	3	0.08	0.01	0.06	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-4504	-43	-409	0	-1108	-7	6.28	6.28	9.42	9.42	3	0.05	0.01	0.05	0.00	0.00	24.0
2	50	-3465	-60	-316	0	-880	-9	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
3	50	-3460	-60	-307	0	-822	-9	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
4	50	-3469	-7	-322	0	-882	-2	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
5	50	-3464	-7	-313	0	-825	-2	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
6	50	-3473	-42	-330	0	-948	-7	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
7	50	-3455	-41	-298	0	-756	-6	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
8	50	-3474	-26	-331	0	-949	-5	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
9	50	-3456	-25	-299	0	-756	-5	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
10	50	-3465	-60	-316	0	-880	-9	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
11	50	-3460	-60	-307	0	-822	-9	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
12	50	-3469	-7	-322	0	-882	-2	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
13	50	-3464	-7	-313	0	-825	-2	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
14	50	-3473	-42	-330	0	-948	-7	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
15	50	-3455	-41	-298	0	-756	-6	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
16	50	-3474	-26	-331	0	-949	-5	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
17	50	-3456	-25	-299	0	-756	-5	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
18	50	-4754	-121	-483	0	-1459	-17	6.28	6.28	9.42	9.42	3	0.07	0.01	0.06	0.00	0.00	24.0
19	50	-4755	39	-491	0	-1408	3	6.28	6.28	9.42	9.42	3	0.07	0.01	0.06	0.00	0.00	24.0
20	50	-4778	-46	-502	0	-1611	-8	6.28	6.28	9.42	9.42	3	0.08	0.01	0.06	0.00	0.00	24.0

37	50	-4632	-175	-446	0	-1353	-23	6.28	6.28	9.42	9.42	3	0.07	0.01	0.06	0.00	0.00	24.0
38	50	-4634	92	-460	0	-1267	9	6.28	6.28	9.42	9.42	3	0.06	0.01	0.06	0.00	0.00	24.0
39	50	-4673	-49	-479	0	-1607	-8	6.28	6.28	9.42	9.42	3	0.08	0.01	0.06	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 90 NI 1159 NF 1161 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 18
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-5982	110	-466	0	-1379	-24	6.28	6.28	12.57	12.57	3	0.05	0.01	0.05	0.00	0.00	24.0
2	0	-4609	-5	-356	0	-1091	-0	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
3	0	-4599	-8	-343	0	-996	0	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
4	0	-4605	176	-374	0	-1126	-37	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
5	0	-4594	174	-361	0	-1030	-36	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
6	0	-4620	62	-378	0	-1215	-14	6.28	6.28	12.57	12.57	2	0.07	0.01	0.04	0.00	0.00	24.0
7	0	-4585	53	-333	0	-896	-12	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
8	0	-4619	116	-383	0	-1225	-25	6.28	6.28	12.57	12.57	2	0.07	0.01	0.04	0.00	0.00	24.0
9	0	-4584	107	-339	0	-906	-23	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
10	0	-4609	-5	-356	0	-1091	-0	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
11	0	-4599	-8	-343	0	-996	0	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
12	0	-4605	176	-374	0	-1126	-37	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
13	0	-4594	174	-361	0	-1030	-36	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
14	0	-4620	62	-378	0	-1215	-14	6.28	6.28	12.57	12.57	2	0.07	0.01	0.04	0.00	0.00	24.0
15	0	-4585	53	-333	0	-896	-12	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
16	0	-4619	116	-383	0	-1225	-25	6.28	6.28	12.57	12.57	2	0.07	0.01	0.04	0.00	0.00	24.0
17	0	-4584	107	-339	0	-906	-23	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
18	0	-6276	-130	-509	0	-1596	25	6.28	6.28	12.57	12.57	3	0.06	0.01	0.05	0.00	0.00	24.0
19	0	-6264	406	-565	0	-1739	-82	6.28	6.28	12.57	12.57	3	0.07	0.01	0.06	0.00	0.00	24.0
20	0	-6271	116	-552	0	-1792	-25	6.28	6.28	12.57	12.57	3	0.07	0.01	0.06	0.00	0.00	24.0
37	0	-6139	-318	-457	0	-1429	63	6.28	6.28	12.57	12.57	3	0.05	0.01	0.05	0.00	0.00	24.0
38	0	-6118	574	-551	0	-1667	-116	6.28	6.28	12.57	12.57	3	0.06	0.01	0.06	0.00	0.00	24.0
39	0	-6129	92	-530	0	-1756	-20	6.28	6.28	12.57	12.57	3	0.07	0.01	0.06	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-5884	110	-466	0	-1321	-10	6.28	6.28	12.57	12.57	3	0.05	0.01	0.05	0.00	0.00	24.0
2	12	-4534	-5	-356	0	-1047	-1	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
3	12	-4524	-8	-343	0	-953	-1	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
4	12	-4530	176	-374	0	-1079	-15	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
5	12	-4519	174	-361	0	-985	-15	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
6	12	-4545	62	-378	0	-1168	-6	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
7	12	-4510	53	-333	0	-854	-6	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
8	12	-4544	116	-383	0	-1177	-10	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
9	12	-4509	107	-339	0	-864	-10	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
10	12	-4534	-5	-356	0	-1047	-1	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
11	12	-4524	-8	-343	0	-953	-1	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
12	12	-4530	176	-374	0	-1079	-15	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
13	12	-4519	174	-361	0	-985	-15	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
14	12	-4545	62	-378	0	-1168	-6	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
15	12	-4510	53	-333	0	-854	-6	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
16	12	-4544	116	-383	0	-1177	-10	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
17	12	-4509	107	-339	0	-864	-10	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
18	12	-6178	-130	-509	0	-1532	9	6.28	6.28	12.57	12.57	3	0.06	0.01	0.05	0.00	0.00	24.0
19	12	-6166	406	-565	0	-1668	-32	6.28	6.28	12.57	12.57	3	0.06	0.01	0.06	0.00	0.00	24.0
20	12	-6174	116	-552	0	-1723	-10	6.28	6.28	12.57	12.57	3	0.06	0.01	0.06	0.00	0.00	24.0
37	12	-6042	-318	-457	0	-1372	23	6.28	6.28	12.57	12.57	3	0.05	0.01	0.05	0.00	0.00	24.0
38	12	-6020	574	-551	0	-1598	-45	6.28	6.28	12.57	12.57	3	0.06	0.01	0.06	0.00	0.00	24.0
39	12	-6032	92	-530	0	-1690	-9	6.28	6.28	12.57	12.57	3	0.06	0.01	0.06	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-5787	110	-466	0	-1262	4	6.28	6.28	12.57	12.57	3	0.05	0.01	0.05	0.00	0.00	24.0
2	25	-4459	-5	-356	0	-1002	-2	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
3	25	-4449	-8	-343	0	-910	-2	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
4	25	-4455	176	-374	0	-1032	7	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
5	25	-4444	174	-361	0	-940	7	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
6	25	-4470	62	-378	0	-1120	2	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
7	25	-4435	53	-333	0	-813	1	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
8	25	-4469	116	-383	0	-1130	4	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
9	25	-4434	107	-339	0	-822	4	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
10	25	-4459	-5	-356	0	-1002	-2	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
11	25	-4449	-8	-343	0	-910	-2	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
12	25	-4455	176	-374	0	-1032	7	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
13	25	-4444	174	-361	0	-940	7	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
14	25	-4470	62	-378	0	-1120	2	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
15	25	-4435	53	-333	0	-813	1	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
16	25	-4469	116	-383	0	-1130	4	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
17	25	-4434	107	-339	0	-822	4	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
18	25	-6081	-130	-509	0	-1469	-7	6.28	6.28	12.57	12.57	3	0.05	0.01	0.05	0.00	0.00	24.0
19	25	-6069	406	-565	0	-1598	19	6.28	6.28	12.57	12.57	3	0.06	0.01	0.06	0.00	0.00	24.0
20	25	-6076	116	-552	0	-1654	4	6.28	6.28	12.57	12.57	3	0.06	0.01	0.06	0.00	0.00	24.0
37	25	-5944	-318	-457	0	-1315	-17	6.28	6.28	12.57	12.57	3	0.05	0.01	0.05	0.00	0.00	24.0
38	25	-5923	574	-551	0	-1529	27	6.28	6.28	12.57	12.57	3	0.06	0.01	0.06	0.00	0.00	24.0
39	25	-5934	92	-530	0	-1624	3	6.28	6.28	12.57	12.57	3	0.06	0.01	0.06	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-5690	110	-466	0	-1204	17	6.28	6.28	12.57	12.57	3	0.05	0.01	0.05	0.00	0.00	24.0
2	38	-4384	-5	-356	0	-958	-2	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
3	38	-4374	-8	-343	0	-867	-3	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
4	38	-4380	176	-374	0	-985	29	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
5	38	-4369	174	-361	0	-895	29	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
6	38	-4395	62	-378	0	-1073	9	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
7	38	-4360	53	-333	0	-771	8	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
8	38	-4394	116	-383	0	-1082	19	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
9	38	-4359	107	-339	0	-779	17	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
10	38	-4384	-5	-356	0	-958	-2	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
11	38	-4374	-8	-343	0	-867	-3	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
12	38	-4380	176	-374	0	-985	29	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
13	38	-4369	174	-361	0	-895	29	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
14	38	-4395	62	-378	0	-1073	9	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
15	38	-4360	53	-333	0	-771	8	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
16	38	-4394	116	-383	0	-1082	19	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0

17	38	-4359	107	-339	0	-779	17	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
18	38	-5984	-130	-509	0	-1406	-23	6.28	6.28	12.57	12.57	3	0.05	0.01	0.05	0.00	0.00	24.0
19	38	-5972	406	-565	0	-1527	70	6.28	6.28	12.57	12.57	3	0.06	0.01	0.06	0.00	0.00	24.0
20	38	-5978	116	-552	0	-1585	19	6.28	6.28	12.57	12.57	3	0.06	0.01	0.06	0.00	0.00	24.0
37	38	-5846	-318	-457	0	-1258	-56	6.28	6.28	12.57	12.57	3	0.05	0.01	0.05	0.00	0.00	24.0
38	38	-5826	574	-551	0	-1460	99	6.28	6.28	12.57	12.57	3	0.06	0.01	0.06	0.00	0.00	24.0
39	38	-5836	92	-530	0	-1557	14	6.28	6.28	12.57	12.57	3	0.06	0.01	0.06	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-5592	110	-466	0	-1146	31	6.28	6.28	12.57	12.57	3	0.04	0.01	0.05	0.00	0.00	24.0
2	50	-4309	-5	-356	0	-913	-3	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
3	50	-4299	-8	-343	0	-824	-4	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
4	50	-4305	176	-374	0	-939	51	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
5	50	-4294	174	-361	0	-849	50	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
6	50	-4320	62	-378	0	-1026	17	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
7	50	-4285	53	-333	0	-729	14	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
8	50	-4319	116	-383	0	-1034	33	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
9	50	-4284	107	-339	0	-737	30	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
10	50	-4309	-5	-356	0	-913	-3	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
11	50	-4299	-8	-343	0	-824	-4	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
12	50	-4305	176	-374	0	-939	51	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
13	50	-4294	174	-361	0	-849	50	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
14	50	-4320	62	-378	0	-1026	17	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
15	50	-4285	53	-333	0	-729	14	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
16	50	-4319	116	-383	0	-1034	33	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
17	50	-4284	107	-339	0	-737	30	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
18	50	-5886	-130	-509	0	-1342	-40	6.28	6.28	12.57	12.57	3	0.05	0.01	0.05	0.00	0.00	24.0
19	50	-5874	406	-565	0	-1456	120	6.28	6.28	12.57	12.57	3	0.06	0.01	0.06	0.00	0.00	24.0
20	50	-5881	116	-552	0	-1516	34	6.28	6.28	12.57	12.57	3	0.06	0.01	0.06	0.00	0.00	24.0
37	50	-5749	-318	-457	0	-1201	-96	6.28	6.28	12.57	12.57	3	0.05	0.01	0.05	0.00	0.00	24.0
38	50	-5728	574	-551	0	-1391	171	6.28	6.28	12.57	12.57	3	0.05	0.01	0.06	0.00	0.00	24.0
39	50	-5739	92	-530	0	-1491	26	6.28	6.28	12.57	12.57	3	0.06	0.01	0.06	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 91 NI 1161 NF 142 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 18A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-8241	195	55	0	-1063	31	6.28	6.28	12.57	12.57	3	0.04	0.00	0.02	0.00	0.00	24.0
2	0	-6352	-94	56	0	-849	-3	6.28	6.28	12.57	12.57	2	0.04	0.00	0.01	0.00	0.00	24.0
3	0	-6326	-100	26	0	-763	-4	6.28	6.28	12.57	12.57	2	0.04	0.00	0.01	0.00	0.00	24.0
4	0	-6353	401	58	0	-873	51	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
5	0	-6327	394	28	0	-787	50	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
6	0	-6382	87	92	0	-958	17	6.28	6.28	12.57	12.57	2	0.05	0.00	0.01	0.00	0.00	24.0
7	0	-6296	65	-8	0	-670	14	6.28	6.28	12.57	12.57	2	0.04	0.00	0.01	0.00	0.00	24.0
8	0	-6382	235	92	0	-965	33	6.28	6.28	12.57	12.57	2	0.05	0.00	0.02	0.00	0.00	24.0
9	0	-6296	214	-7	0	-678	30	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
10	0	-6352	-94	56	0	-849	-3	6.28	6.28	12.57	12.57	2	0.04	0.00	0.01	0.00	0.00	24.0
11	0	-6326	-100	26	0	-763	-4	6.28	6.28	12.57	12.57	2	0.04	0.00	0.01	0.00	0.00	24.0
12	0	-6353	401	58	0	-873	51	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
13	0	-6327	394	28	0	-787	50	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
14	0	-6382	87	92	0	-958	17	6.28	6.28	12.57	12.57	2	0.05	0.00	0.01	0.00	0.00	24.0
15	0	-6296	65	-8	0	-670	14	6.28	6.28	12.57	12.57	2	0.04	0.00	0.01	0.00	0.00	24.0
16	0	-6382	235	92	0	-965	33	6.28	6.28	12.57	12.57	2	0.05	0.00	0.02	0.00	0.00	24.0
17	0	-6296	214	-7	0	-678	30	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
18	0	-8711	-455	95	0	-1249	-40	6.28	6.28	12.57	12.57	3	0.05	0.01	0.04	0.00	0.00	24.0
19	0	-8716	1005	116	0	-1359	120	6.28	6.28	12.57	12.57	3	0.05	0.02	0.09	0.00	0.00	24.0
20	0	-8735	220	143	0	-1417	34	6.28	6.28	12.57	12.57	3	0.05	0.00	0.02	0.00	0.00	24.0
37	0	-8478	-966	72	0	-1114	-96	6.28	6.28	12.57	12.57	3	0.04	0.02	0.08	0.00	0.00	24.0
38	0	-8487	1466	106	0	-1299	171	6.28	6.28	12.57	12.57	3	0.05	0.03	0.13	0.00	0.00	24.0
39	0	-8519	157	151	0	-1394	26	6.28	6.28	12.57	12.57	3	0.05	0.00	0.02	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-8144	195	55	0	-1070	55	6.28	6.28	12.57	12.57	3	0.04	0.00	0.02	0.00	0.00	24.0
2	12	-6277	-94	56	0	-856	-15	6.28	6.28	12.57	12.57	2	0.05	0.00	0.01	0.00	0.00	24.0
3	12	-6251	-100	26	0	-766	-16	6.28	6.28	12.57	12.57	2	0.04	0.00	0.01	0.00	0.00	24.0
4	12	-6278	401	58	0	-881	101	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
5	12	-6252	394	28	0	-791	100	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
6	12	-6307	87	92	0	-970	28	6.28	6.28	12.57	12.57	2	0.05	0.00	0.01	0.00	0.00	24.0
7	12	-6221	65	-8	0	-670	22	6.28	6.28	12.57	12.57	2	0.04	0.00	0.01	0.00	0.00	24.0
8	12	-6307	235	92	0	-977	63	6.28	6.28	12.57	12.57	2	0.05	0.00	0.02	0.00	0.00	24.0
9	12	-6221	214	-7	0	-677	57	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
10	12	-6277	-94	56	0	-856	-15	6.28	6.28	12.57	12.57	2	0.05	0.00	0.01	0.00	0.00	24.0
11	12	-6251	-100	26	0	-766	-16	6.28	6.28	12.57	12.57	2	0.04	0.00	0.01	0.00	0.00	24.0
12	12	-6278	401	58	0	-881	101	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
13	12	-6252	394	28	0	-791	100	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
14	12	-6307	87	92	0	-970	28	6.28	6.28	12.57	12.57	2	0.05	0.00	0.01	0.00	0.00	24.0
15	12	-6221	65	-8	0	-670	22	6.28	6.28	12.57	12.57	2	0.04	0.00	0.01	0.00	0.00	24.0
16	12	-6307	235	92	0	-977	63	6.28	6.28	12.57	12.57	2	0.05	0.00	0.02	0.00	0.00	24.0
17	12	-6221	214	-7	0	-677	57	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
18	12	-8614	-455	95	0	-1261	-96	6.28	6.28	12.57	12.57	3	0.05	0.01	0.04	0.00	0.00	24.0
19	12	-8618	1005	116	0	-1373	246	6.28	6.28	12.57	12.57	3	0.05	0.02	0.09	0.00	0.00	24.0
20	12	-8638	220	143	0	-1435	61	6.28	6.28	12.57	12.57	3	0.05	0.00	0.02	0.00	0.00	24.0
37	12	-8380	-966	72	0	-1123	-217	6.28	6.28	12.57	12.57	3	0.04	0.02	0.08	0.00	0.00	24.0
38	12	-8390	1466	106	0	-1312	354	6.28	6.28	12.57	12.57	3	0.05	0.03	0.13	0.00	0.00	24.0
39	12	-8422	157	151	0	-1413	46	6.28	6.28	12.57	12.57	3	0.05	0.00	0.02	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-8046	195	55	0	-1077	80	6.28	6.28	12.57	12.57	3	0.04	0.00	0.02	0.00	0.00	24.0
2	25	-6202	-94	56	0	-863	-26	6.28	6.28	12.57	12.57	2	0.05	0.00	0.01	0.00	0.00	24.0
3	25	-6176	-100	26	0	-769	-29	6.28	6.28	12.57	12.57	2	0.04	0.00	0.01	0.00	0.00	24.0
4	25	-6203	401	58	0	-888	152	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
5	25	-6177	394	28	0	-794	149	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
6	25	-6232	87	92	0	-981	39	6.28	6.28	12.57	12.57	2	0.05	0.00	0.01	0.00	0.00	24.0
7	25	-6146	65	-8	0	-669	30	6.28	6.28	12.57	12.57	2	0.04	0.00	0.01	0.00	0.00	24.0
8	25	-6232	235	92	0	-989	92	6.28	6.28	12.57	12.57	2	0.06	0.00	0.02	0.00	0.00	24.0
9	25	-6146	214	-7	0	-676	84	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
10	25	-6202	-94	56	0	-863	-26	6.28	6.28	12.57	12.57	2	0.05	0.00	0.01	0.00	0.00	24.0
11	25	-6176	-100	26	0	-769	-29	6.28	6.28	12.57	12.57	2	0.04	0.00	0.01	0.00	0.00	24.0
12	25	-6203	401	58	0	-888	152	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0

13	25	-6177	394	28	0	-794	149	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
14	25	-6232	87	92	0	-981	39	6.28	6.28	12.57	12.57	2	0.05	0.00	0.01	0.00	0.00	24.0
15	25	-6146	65	-8	0	-669	30	6.28	6.28	12.57	12.57	2	0.04	0.00	0.01	0.00	0.00	24.0
16	25	-6232	235	92	0	-989	92	6.28	6.28	12.57	12.57	2	0.06	0.00	0.02	0.00	0.00	24.0
17	25	-6146	214	-7	0	-676	84	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
18	25	-8516	-455	95	0	-1273	-153	6.28	6.28	12.57	12.57	3	0.05	0.01	0.04	0.00	0.00	24.0
19	25	-8521	1005	116	0	-1388	372	6.28	6.28	12.57	12.57	3	0.06	0.02	0.09	0.00	0.00	24.0
20	25	-8540	220	143	0	-1453	89	6.28	6.28	12.57	12.57	3	0.05	0.00	0.02	0.00	0.00	24.0
37	25	-8283	-966	72	0	-1132	-338	6.28	6.28	12.57	12.57	3	0.05	0.02	0.08	0.00	0.00	24.0
38	25	-8292	1466	106	0	-1325	537	6.28	6.28	12.57	12.57	3	0.06	0.03	0.13	0.00	0.00	24.0
39	25	-8324	157	151	0	-1432	65	6.28	6.28	12.57	12.57	3	0.05	0.00	0.02	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-7948	195	55	0	-1084	104	6.28	6.28	12.57	12.57	3	0.04	0.00	0.02	0.00	0.00	24.0
2	38	-6127	-94	56	0	-870	-38	6.28	6.28	12.57	12.57	2	0.05	0.00	0.01	0.00	0.00	24.0
3	38	-6101	-100	26	0	-772	-41	6.28	6.28	12.57	12.57	2	0.04	0.00	0.01	0.00	0.00	24.0
4	38	-6128	401	58	0	-895	202	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
5	38	-6102	394	28	0	-798	198	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
6	38	-6157	87	92	0	-993	50	6.28	6.28	12.57	12.57	2	0.05	0.00	0.01	0.00	0.00	24.0
7	38	-6071	65	-8	0	-668	39	6.28	6.28	12.57	12.57	2	0.04	0.00	0.01	0.00	0.00	24.0
8	38	-6157	235	92	0	-1000	122	6.28	6.28	12.57	12.57	2	0.06	0.00	0.02	0.00	0.00	24.0
9	38	-6071	214	-7	0	-675	111	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
10	38	-6127	-94	56	0	-870	-38	6.28	6.28	12.57	12.57	2	0.05	0.00	0.01	0.00	0.00	24.0
11	38	-6101	-100	26	0	-772	-41	6.28	6.28	12.57	12.57	2	0.04	0.00	0.01	0.00	0.00	24.0
12	38	-6128	401	58	0	-895	202	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
13	38	-6102	394	28	0	-798	198	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
14	38	-6157	87	92	0	-993	50	6.28	6.28	12.57	12.57	2	0.05	0.00	0.01	0.00	0.00	24.0
15	38	-6071	65	-8	0	-668	39	6.28	6.28	12.57	12.57	2	0.04	0.00	0.01	0.00	0.00	24.0
16	38	-6157	235	92	0	-1000	122	6.28	6.28	12.57	12.57	2	0.06	0.00	0.02	0.00	0.00	24.0
17	38	-6071	214	-7	0	-675	111	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
18	38	-8418	-455	95	0	-1284	-210	6.28	6.28	12.57	12.57	3	0.05	0.01	0.04	0.00	0.00	24.0
19	38	-8424	1005	116	0	-1402	497	6.28	6.28	12.57	12.57	3	0.06	0.02	0.09	0.00	0.00	24.0
20	38	-8442	220	143	0	-1470	116	6.28	6.28	12.57	12.57	3	0.05	0.00	0.02	0.00	0.00	24.0
37	38	-8186	-966	72	0	-1141	-459	6.28	6.28	12.57	12.57	3	0.05	0.02	0.08	0.00	0.00	24.0
38	38	-8194	1466	106	0	-1339	721	6.28	6.28	12.57	12.57	3	0.06	0.03	0.13	0.00	0.00	24.0
39	38	-8226	157	151	0	-1451	85	6.28	6.28	12.57	12.57	3	0.05	0.00	0.02	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-7851	195	55	0	-1091	129	6.28	6.28	12.57	12.57	3	0.04	0.00	0.02	0.00	0.00	24.0
2	50	-6052	-94	56	0	-877	-50	6.28	6.28	12.57	12.57	2	0.05	0.00	0.01	0.00	0.00	24.0
3	50	-6026	-100	26	0	-776	-54	6.28	6.28	12.57	12.57	2	0.04	0.00	0.01	0.00	0.00	24.0
4	50	-6053	401	58	0	-903	252	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
5	50	-6027	394	28	0	-801	248	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
6	50	-6082	87	92	0	-1004	61	6.28	6.28	12.57	12.57	2	0.06	0.00	0.01	0.00	0.00	24.0
7	50	-5996	65	-8	0	-667	47	6.28	6.28	12.57	12.57	2	0.04	0.00	0.01	0.00	0.00	24.0
8	50	-6082	235	92	0	-1012	151	6.28	6.28	12.57	12.57	2	0.06	0.00	0.02	0.00	0.00	24.0
9	50	-5996	214	-7	0	-674	137	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
10	50	-6052	-94	56	0	-877	-50	6.28	6.28	12.57	12.57	2	0.05	0.00	0.01	0.00	0.00	24.0
11	50	-6026	-100	26	0	-776	-54	6.28	6.28	12.57	12.57	2	0.04	0.00	0.01	0.00	0.00	24.0
12	50	-6053	401	58	0	-903	252	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
13	50	-6027	394	28	0	-801	248	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
14	50	-6082	87	92	0	-1004	61	6.28	6.28	12.57	12.57	2	0.06	0.00	0.01	0.00	0.00	24.0
15	50	-5996	65	-8	0	-667	47	6.28	6.28	12.57	12.57	2	0.04	0.00	0.01	0.00	0.00	24.0
16	50	-6082	235	92	0	-1012	151	6.28	6.28	12.57	12.57	2	0.06	0.00	0.02	0.00	0.00	24.0
17	50	-5996	214	-7	0	-674	137	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
18	50	-8321	-455	95	0	-1296	-267	6.28	6.28	12.57	12.57	3	0.05	0.01	0.04	0.00	0.00	24.0
19	50	-8326	1005	116	0	-1417	623	6.28	6.28	12.57	12.57	3	0.06	0.02	0.09	0.00	0.00	24.0
20	50	-8345	220	143	0	-1488	143	6.28	6.28	12.57	12.57	3	0.06	0.00	0.02	0.00	0.00	24.0
37	50	-8088	-966	72	0	-1150	-579	6.28	6.28	12.57	12.57	3	0.05	0.02	0.08	0.00	0.00	24.0
38	50	-8097	1466	106	0	-1352	904	6.28	6.28	12.57	12.57	3	0.07	0.03	0.13	0.00	0.00	24.0
39	50	-8129	157	151	0	-1470	104	6.28	6.28	12.57	12.57	3	0.05	0.00	0.02	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 92 NI 1256 NF 1259 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 19
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-19790	11	-184	0	-501	-71	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
2	0	-15260	78	-168	0	-447	-332	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
3	0	-15180	77	-86	0	-245	-328	6.28	6.28	12.57	12.57	2	0.03	0.00	0.01	0.00	0.00	24.0
4	0	-15270	-61	-198	0	-525	218	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
5	0	-15190	-62	-116	0	-323	222	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
6	0	-15350	31	-274	0	-711	-143	6.28	6.28	12.57	12.57	2	0.04	0.00	0.03	0.00	0.00	24.0
7	0	-15090	27	0	0	-36	-132	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
8	0	-15360	-11	-284	0	-734	22	6.28	6.28	12.57	12.57	2	0.04	0.00	0.03	0.00	0.00	24.0
9	0	-15090	-14	-9	0	-60	33	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
10	0	-15260	78	-168	0	-447	-332	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
11	0	-15180	77	-86	0	-245	-328	6.28	6.28	12.57	12.57	2	0.03	0.00	0.01	0.00	0.00	24.0
12	0	-15270	-61	-198	0	-525	218	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
13	0	-15190	-62	-116	0	-323	222	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
14	0	-15350	31	-274	0	-711	-143	6.28	6.28	12.57	12.57	2	0.04	0.00	0.03	0.00	0.00	24.0
15	0	-15090	27	0	0	-36	-132	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
16	0	-15360	-11	-284	0	-734	22	6.28	6.28	12.57	12.57	2	0.04	0.00	0.03	0.00	0.00	24.0
17	0	-15090	-14	-9	0	-60	33	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
18	0	-21570	228	-254	0	-657	-908	6.28	6.28	12.57	12.57	3	0.05	0.00	0.02	0.00	0.00	24.0
19	0	-21650	-205	-384	0	-988	764	6.28	6.28	12.57	12.57	3	0.05	0.01	0.03	0.00	0.00	24.0
20	0	-21460	13	-383	0	-1020	-79	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
37	0	-20670	372	-170	0	-446	-1464	6.28	6.28	12.57	12.57	3	0.08	0.01	0.03	0.00	0.00	24.0
38	0	-20810	-350	-385	0	-999	1322	6.28	6.28	12.57	12.57	3	0.07	0.01	0.03	0.00	0.00	24.0
39	0	-20490	14	-384	0	-1052	-83	6.28	6.28	12.57	12.57	3	0.04	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-19692	11	-184	0	-478	-70	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
2	12	-15185	78	-168	0	-426	-322	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
3	12	-15105	77	-86	0	-234	-318	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
4	12	-15195	-61	-198	0	-501	210	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
5	12	-15115	-62	-116	0	-309	214	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
6	12	-15275	31	-274	0	-676	-140	6.28	6.28	12.57	12.57	2	0.04	0.00	0.03	0.00	0.00	24.0
7	12	-15015	27	0	0	-36	-128	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
8	12	-15285	-11	-284	0	-699	20	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0

9	12	-15015	-14	-9	0	-58	32	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
10	12	-15185	78	-168	0	-426	-322	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
11	12	-15105	77	-86	0	-234	-318	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
12	12	-15195	-61	-198	0	-501	210	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
13	12	-15115	-62	-116	0	-309	214	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
14	12	-15275	31	-274	0	-676	-140	6.28	6.28	12.57	12.57	2	0.04	0.00	0.03	0.00	0.00	24.0
15	12	-15015	27	0	0	-36	-128	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
16	12	-15285	-11	-284	0	-699	20	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
17	12	-15015	-14	-9	0	-58	32	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
18	12	-21472	228	-254	0	-625	-880	6.28	6.28	12.57	12.57	3	0.05	0.00	0.02	0.00	0.00	24.0
19	12	-21552	-205	-384	0	-941	738	6.28	6.28	12.57	12.57	3	0.05	0.01	0.03	0.00	0.00	24.0
20	12	-21362	13	-383	0	-972	-77	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
37	12	-20572	372	-170	0	-424	-1418	6.28	6.28	12.57	12.57	3	0.07	0.01	0.03	0.00	0.00	24.0
38	12	-20712	-350	-385	0	-951	1279	6.28	6.28	12.57	12.57	3	0.07	0.01	0.03	0.00	0.00	24.0
39	12	-20392	14	-384	0	-1004	-81	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-19595	11	-184	0	-455	-69	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
2	25	-15110	78	-168	0	-405	-312	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
3	25	-15030	77	-86	0	-223	-309	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
4	25	-15120	-61	-198	0	-476	203	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
5	25	-15040	-62	-116	0	-294	206	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
6	25	-15200	31	-274	0	-642	-136	6.28	6.28	12.57	12.57	2	0.04	0.00	0.03	0.00	0.00	24.0
7	25	-14940	27	0	0	-36	-125	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
8	25	-15210	-11	-284	0	-663	19	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
9	25	-14940	-14	-9	0	-57	30	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
10	25	-15110	78	-168	0	-405	-312	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
11	25	-15030	77	-86	0	-223	-309	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
12	25	-15120	-61	-198	0	-476	203	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
13	25	-15040	-62	-116	0	-294	206	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
14	25	-15200	31	-274	0	-642	-136	6.28	6.28	12.57	12.57	2	0.04	0.00	0.03	0.00	0.00	24.0
15	25	-14940	27	0	0	-36	-125	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
16	25	-15210	-11	-284	0	-663	19	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
17	25	-14940	-14	-9	0	-57	30	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
18	25	-21375	228	-254	0	-593	-851	6.28	6.28	12.57	12.57	3	0.05	0.00	0.02	0.00	0.00	24.0
19	25	-21455	-205	-384	0	-893	713	6.28	6.28	12.57	12.57	3	0.05	0.01	0.03	0.00	0.00	24.0
20	25	-21265	13	-383	0	-924	-76	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
37	25	-20475	372	-170	0	-403	-1372	6.28	6.28	12.57	12.57	3	0.07	0.01	0.03	0.00	0.00	24.0
38	25	-20615	-350	-385	0	-903	1235	6.28	6.28	12.57	12.57	3	0.07	0.01	0.03	0.00	0.00	24.0
39	25	-20295	14	-384	0	-956	-79	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-19498	11	-184	0	-432	-67	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
2	38	-15035	78	-168	0	-384	-302	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
3	38	-14955	77	-86	0	-213	-299	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
4	38	-15045	-61	-198	0	-451	195	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
5	38	-14965	-62	-116	0	-280	198	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
6	38	-15125	31	-274	0	-608	-132	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
7	38	-14865	27	0	0	-36	-121	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
8	38	-15135	-11	-284	0	-628	17	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
9	38	-14865	-14	-9	0	-56	28	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
10	38	-15035	78	-168	0	-384	-302	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
11	38	-14955	77	-86	0	-213	-299	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
12	38	-15045	-61	-198	0	-451	195	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
13	38	-14965	-62	-116	0	-280	198	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
14	38	-15125	31	-274	0	-608	-132	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
15	38	-14865	27	0	0	-36	-121	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
16	38	-15135	-11	-284	0	-628	17	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
17	38	-14865	-14	-9	0	-56	28	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
18	38	-21278	228	-254	0	-561	-823	6.28	6.28	12.57	12.57	3	0.04	0.00	0.02	0.00	0.00	24.0
19	38	-21358	-205	-384	0	-845	687	6.28	6.28	12.57	12.57	3	0.04	0.01	0.03	0.00	0.00	24.0
20	38	-21168	13	-383	0	-877	-74	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
37	38	-20378	372	-170	0	-382	-1325	6.28	6.28	12.57	12.57	3	0.07	0.01	0.03	0.00	0.00	24.0
38	38	-20518	-350	-385	0	-854	1192	6.28	6.28	12.57	12.57	3	0.07	0.01	0.03	0.00	0.00	24.0
39	38	-20198	14	-384	0	-908	-77	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-19400	11	-184	0	-409	-66	6.28	6.28	12.57	12.57	3	0.01	0.00	0.02	0.00	0.00	24.0
2	50	-14960	78	-168	0	-363	-292	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
3	50	-14880	77	-86	0	-202	-289	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
4	50	-14970	-61	-198	0	-426	188	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
5	50	-14890	-62	-116	0	-265	191	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
6	50	-15050	31	-274	0	-573	-128	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
7	50	-14790	27	0	0	-36	-118	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
8	50	-15060	-11	-284	0	-592	16	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
9	50	-14790	-14	-9	0	-55	26	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
10	50	-14960	78	-168	0	-363	-292	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
11	50	-14880	77	-86	0	-202	-289	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
12	50	-14970	-61	-198	0	-426	188	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
13	50	-14890	-62	-116	0	-265	191	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
14	50	-15050	31	-274	0	-573	-128	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
15	50	-14790	27	0	0	-36	-118	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
16	50	-15060	-11	-284	0	-592	16	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
17	50	-14790	-14	-9	0	-55	26	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
18	50	-21180	228	-254	0	-529	-794	6.28	6.28	12.57	12.57	3	0.04	0.00	0.02	0.00	0.00	24.0
19	50	-21260	-205	-384	0	-797	662	6.28	6.28	12.57	12.57	3	0.04	0.01	0.03	0.00	0.00	24.0
20	50	-21070	13	-383	0	-829	-72	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
37	50	-20280	372	-170	0	-361	-1279	6.28	6.28	12.57	12.57	3	0.07	0.01	0.03	0.00	0.00	24.0
38	50	-20420	-350	-385	0	-806	1148	6.28	6.28	12.57	12.57	3	0.06	0.01	0.03	0.00	0.00	24.0
39	50	-20100	14	-384	0	-860	-76	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 93 NI 1259 NF 127 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 19A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-19400	11	-184	0	-409	-66	6.28	6.28	12.57	12.57	3	0.01	0.00	0.02	0.00	0.00	24.0
2	0	-14960	78	-168	0	-363	-292	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
3	0	-14880	77	-86	0	-202	-289	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
4	0	-14970	-61	-198	0	-426	188	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0

5	0	-14890	-62	-116	0	-265	191	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
6	0	-15050	31	-274	0	-573	-128	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
7	0	-14790	27	0	0	-36	-118	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
8	0	-15060	-11	-284	0	-592	16	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
9	0	-14790	-14	-9	0	-55	26	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
10	0	-14960	78	-168	0	-363	-292	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
11	0	-14880	77	-86	0	-202	-289	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
12	0	-14970	-61	-198	0	-426	188	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
13	0	-14890	-62	-116	0	-265	191	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
14	0	-15050	31	-274	0	-573	-128	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
15	0	-14790	27	0	0	-36	-118	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
16	0	-15060	-11	-284	0	-592	16	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
17	0	-14790	-14	-9	0	-55	26	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
18	0	-21180	228	-254	0	-529	-794	6.28	6.28	12.57	12.57	3	0.04	0.00	0.02	0.00	0.00	24.0
19	0	-21260	-205	-384	0	-797	662	6.28	6.28	12.57	12.57	3	0.04	0.01	0.03	0.00	0.00	24.0
20	0	-21070	13	-383	0	-829	-72	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
37	0	-20280	372	-170	0	-361	-1279	6.28	6.28	12.57	12.57	3	0.07	0.01	0.03	0.00	0.00	24.0
38	0	-20420	-350	-385	0	-806	1148	6.28	6.28	12.57	12.57	3	0.06	0.01	0.03	0.00	0.00	24.0
39	0	-20100	14	-384	0	-860	-76	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-19302	11	-184	0	-385	-65	6.28	6.28	12.57	12.57	3	0.01	0.00	0.02	0.00	0.00	24.0
2	12	-14885	78	-168	0	-342	-283	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
3	12	-14805	77	-86	0	-191	-280	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
4	12	-14895	-61	-198	0	-402	180	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
5	12	-14815	-62	-116	0	-251	183	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
6	12	-14975	31	-274	0	-539	-124	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
7	12	-14715	27	0	0	-36	-114	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
8	12	-14985	-11	-284	0	-557	15	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
9	12	-14715	-14	-9	0	-54	24	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
10	12	-14885	78	-168	0	-342	-283	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
11	12	-14805	77	-86	0	-191	-280	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
12	12	-14895	-61	-198	0	-402	180	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
13	12	-14815	-62	-116	0	-251	183	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
14	12	-14975	31	-274	0	-539	-124	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
15	12	-14715	27	0	0	-36	-114	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
16	12	-14985	-11	-284	0	-557	15	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
17	12	-14715	-14	-9	0	-54	24	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
18	12	-21082	228	-254	0	-498	-766	6.28	6.28	12.57	12.57	3	0.04	0.00	0.02	0.00	0.00	24.0
19	12	-21162	-205	-384	0	-749	636	6.28	6.28	12.57	12.57	3	0.04	0.01	0.03	0.00	0.00	24.0
20	12	-20972	13	-383	0	-781	-71	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
37	12	-20182	372	-170	0	-339	-1232	6.28	6.28	12.57	12.57	3	0.06	0.01	0.03	0.00	0.00	24.0
38	12	-20322	-350	-385	0	-758	1104	6.28	6.28	12.57	12.57	3	0.06	0.01	0.03	0.00	0.00	24.0
39	12	-20002	14	-384	0	-812	-74	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-19205	11	-184	0	-362	-63	6.28	6.28	12.57	12.57	3	0.01	0.00	0.02	0.00	0.00	24.0
2	25	-14810	78	-168	0	-321	-273	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
3	25	-14730	77	-86	0	-181	-270	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
4	25	-14820	-61	-198	0	-377	172	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
5	25	-14740	-62	-116	0	-236	175	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
6	25	-14900	31	-274	0	-505	-120	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
7	25	-14640	27	0	0	-36	-111	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
8	25	-14910	-11	-284	0	-522	13	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
9	25	-14640	-14	-9	0	-53	23	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
10	25	-14810	78	-168	0	-321	-273	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
11	25	-14730	77	-86	0	-181	-270	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
12	25	-14820	-61	-198	0	-377	172	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
13	25	-14740	-62	-116	0	-236	175	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
14	25	-14900	31	-274	0	-505	-120	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
15	25	-14640	27	0	0	-36	-111	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
16	25	-14910	-11	-284	0	-522	13	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
17	25	-14640	-14	-9	0	-53	23	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
18	25	-20985	228	-254	0	-466	-737	6.28	6.28	12.57	12.57	3	0.04	0.00	0.02	0.00	0.00	24.0
19	25	-21065	-205	-384	0	-701	610	6.28	6.28	12.57	12.57	3	0.04	0.01	0.03	0.00	0.00	24.0
20	25	-20875	13	-383	0	-733	-69	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
37	25	-20085	372	-170	0	-318	-1186	6.28	6.28	12.57	12.57	3	0.06	0.01	0.03	0.00	0.00	24.0
38	25	-20225	-350	-385	0	-710	1060	6.28	6.28	12.57	12.57	3	0.06	0.01	0.03	0.00	0.00	24.0
39	25	-19905	14	-384	0	-764	-72	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-19108	11	-184	0	-339	-62	6.28	6.28	12.57	12.57	3	0.01	0.00	0.02	0.00	0.00	24.0
2	38	-14735	78	-168	0	-300	-263	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
3	38	-14655	77	-86	0	-170	-260	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
4	38	-14745	-61	-198	0	-352	165	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
5	38	-14665	-62	-116	0	-222	167	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
6	38	-14825	31	-274	0	-471	-116	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
7	38	-14565	27	0	0	-36	-107	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
8	38	-14835	-11	-284	0	-486	12	6.28	6.28	12.57	12.57	2	0.02	0.00	0.03	0.00	0.00	24.0
9	38	-14565	-14	-9	0	-52	21	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
10	38	-14735	78	-168	0	-300	-263	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
11	38	-14655	77	-86	0	-170	-260	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
12	38	-14745	-61	-198	0	-352	165	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
13	38	-14665	-62	-116	0	-222	167	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
14	38	-14825	31	-274	0	-471	-116	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
15	38	-14565	27	0	0	-36	-107	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
16	38	-14835	-11	-284	0	-486	12	6.28	6.28	12.57	12.57	2	0.02	0.00	0.03	0.00	0.00	24.0
17	38	-14565	-14	-9	0	-52	21	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
18	38	-20888	228	-254	0	-434	-709	6.28	6.28	12.57	12.57	3	0.04	0.00	0.02	0.00	0.00	24.0
19	38	-20968	-205	-384	0	-653	585	6.28	6.28	12.57	12.57	3	0.04	0.01	0.03	0.00	0.00	24.0
20	38	-20778	13	-383	0	-685	-67	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
37	38	-19988	372	-170	0	-297	-1139	6.28	6.28	12.57	12.57	3	0.06	0.01	0.03	0.00	0.00	24.0
38	38	-20128	-350	-385	0	-662	1017	6.28	6.28	12.57	12.57	3	0.06	0.01	0.03	0.00	0.00	24.0
39	38	-19808	14	-384	0	-716	-70	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-19010	11	-184	0	-316	-61	6.28	6.28	12.57	12.57	3	0.01	0.00	0.02	0.00	0.00	24.0
2	50	-14660	78	-168	0	-279	-253	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
3	50	-14580	77	-86	0	-159	-251	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
4	50	-14670	-61	-198	0	-327	157	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
5	50	-14590	-62	-116	0	-207	160	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
6	50	-14750	31	-274	0	-436	-113	6.28	6.28	12.57	12.57	2	0.02	0.00	0.03	0.00	0.00	24.0
7	50	-14490	27	0	0	-36	-104	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
8	50	-14760	-11	-284	0	-451	10	6.28	6.28	12.57	12.57	2	0.02	0.00	0.03	0.00	0.00	24.0
9	50	-14490	-14	-9	0	-51	19	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
10	50	-14660	78	-168	0	-279	-253	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0

11	50	-14580	77	-86	0	-159	-251	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
12	50	-14670	-61	-198	0	-327	157	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
13	50	-14590	-62	-116	0	-207	160	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
14	50	-14750	31	-274	0	-436	-113	6.28	6.28	12.57	12.57	2	0.02	0.00	0.03	0.00	0.00	24.0
15	50	-14490	27	0	0	-36	-104	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
16	50	-14760	-11	-284	0	-451	10	6.28	6.28	12.57	12.57	2	0.02	0.00	0.03	0.00	0.00	24.0
17	50	-14490	-14	-9	0	-51	19	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
18	50	-20790	228	-254	0	-402	-680	6.28	6.28	12.57	12.57	3	0.04	0.00	0.02	0.00	0.00	24.0
19	50	-20870	-205	-384	0	-605	559	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
20	50	-20680	13	-383	0	-637	-66	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
37	50	-19890	372	-170	0	-276	-1093	6.28	6.28	12.57	12.57	3	0.06	0.01	0.03	0.00	0.00	24.0
38	50	-20030	-350	-385	0	-614	973	6.28	6.28	12.57	12.57	3	0.05	0.01	0.03	0.00	0.00	24.0
39	50	-19710	14	-384	0	-668	-69	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 94 NI 1034 NF 1040 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 20
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-35650	124	713	0	1634	-385	6.28	6.28	12.57	12.57	3	0.06	0.01	0.05	0.00	0.00	24.0
2	0	-27250	323	578	0	1282	-1011	6.28	6.28	12.57	12.57	2	0.09	0.01	0.05	0.00	0.00	24.0
3	0	-27210	322	547	0	1308	-1008	6.28	6.28	12.57	12.57	2	0.09	0.01	0.04	0.00	0.00	24.0
4	0	-27640	-131	550	0	1206	416	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
5	0	-27600	-132	520	0	1231	419	6.28	6.28	12.57	12.57	2	0.07	0.01	0.04	0.00	0.00	24.0
6	0	-27440	165	604	0	1225	-516	6.28	6.28	12.57	12.57	2	0.07	0.01	0.05	0.00	0.00	24.0
7	0	-27290	162	502	0	1311	-504	6.28	6.28	12.57	12.57	2	0.07	0.01	0.04	0.00	0.00	24.0
8	0	-27560	29	595	0	1202	-88	6.28	6.28	12.57	12.57	2	0.05	0.01	0.05	0.00	0.00	24.0
9	0	-27410	26	494	0	1288	-76	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
10	0	-27250	323	578	0	1282	-1011	6.28	6.28	12.57	12.57	2	0.09	0.01	0.05	0.00	0.00	24.0
11	0	-27210	322	547	0	1308	-1008	6.28	6.28	12.57	12.57	2	0.09	0.01	0.04	0.00	0.00	24.0
12	0	-27640	-131	550	0	1206	416	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
13	0	-27600	-132	520	0	1231	419	6.28	6.28	12.57	12.57	2	0.07	0.01	0.04	0.00	0.00	24.0
14	0	-27440	165	604	0	1225	-516	6.28	6.28	12.57	12.57	2	0.07	0.01	0.05	0.00	0.00	24.0
15	0	-27290	162	502	0	1311	-504	6.28	6.28	12.57	12.57	2	0.07	0.01	0.04	0.00	0.00	24.0
16	0	-27560	29	595	0	1202	-88	6.28	6.28	12.57	12.57	2	0.05	0.01	0.05	0.00	0.00	24.0
17	0	-27410	26	494	0	1288	-76	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
18	0	-38760	932	1006	0	2190	-2800	6.28	6.28	12.57	12.57	3	0.14	0.02	0.07	0.00	0.00	24.0
19	0	-40600	-585	902	0	1883	1792	6.28	6.28	12.57	12.57	3	0.10	0.01	0.06	0.00	0.00	24.0
20	0	-39160	173	704	0	1533	-504	6.28	6.28	12.57	12.57	3	0.05	0.01	0.05	0.00	0.00	24.0
37	0	-36610	1420	952	0	2136	-4289	6.28	6.28	12.57	12.57	3	0.21	0.02	0.10	0.00	0.00	24.0
38	0	-39680	-1108	779	0	1625	3364	6.28	6.28	12.57	12.57	3	0.16	0.02	0.08	0.00	0.00	24.0
39	0	-37280	155	450	0	1042	-461	6.28	6.28	12.57	12.57	3	0.04	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-35552	124	713	0	1545	-369	6.28	6.28	12.57	12.57	3	0.05	0.01	0.05	0.00	0.00	24.0
2	12	-27175	323	578	0	1210	-971	6.28	6.28	12.57	12.57	2	0.08	0.01	0.05	0.00	0.00	24.0
3	12	-27135	322	547	0	1240	-968	6.28	6.28	12.57	12.57	2	0.09	0.01	0.04	0.00	0.00	24.0
4	12	-27565	-131	550	0	1137	399	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
5	12	-27525	-132	520	0	1166	403	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
6	12	-27365	165	604	0	1150	-495	6.28	6.28	12.57	12.57	2	0.06	0.01	0.05	0.00	0.00	24.0
7	12	-27215	162	502	0	1248	-484	6.28	6.28	12.57	12.57	2	0.07	0.01	0.04	0.00	0.00	24.0
8	12	-27485	29	595	0	1128	-84	6.28	6.28	12.57	12.57	2	0.05	0.01	0.05	0.00	0.00	24.0
9	12	-27335	26	494	0	1226	-73	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
10	12	-27175	323	578	0	1210	-971	6.28	6.28	12.57	12.57	2	0.08	0.01	0.05	0.00	0.00	24.0
11	12	-27135	322	547	0	1240	-968	6.28	6.28	12.57	12.57	2	0.09	0.01	0.04	0.00	0.00	24.0
12	12	-27565	-131	550	0	1137	399	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
13	12	-27525	-132	520	0	1166	403	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
14	12	-27365	165	604	0	1150	-495	6.28	6.28	12.57	12.57	2	0.06	0.01	0.05	0.00	0.00	24.0
15	12	-27215	162	502	0	1248	-484	6.28	6.28	12.57	12.57	2	0.07	0.01	0.04	0.00	0.00	24.0
16	12	-27485	29	595	0	1128	-84	6.28	6.28	12.57	12.57	2	0.05	0.01	0.05	0.00	0.00	24.0
17	12	-27335	26	494	0	1226	-73	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
18	12	-38662	932	1006	0	2064	-2684	6.28	6.28	12.57	12.57	3	0.14	0.02	0.07	0.00	0.00	24.0
19	12	-40502	-585	902	0	1770	1719	6.28	6.28	12.57	12.57	3	0.10	0.01	0.06	0.00	0.00	24.0
20	12	-39062	173	704	0	1445	-482	6.28	6.28	12.57	12.57	3	0.05	0.01	0.05	0.00	0.00	24.0
37	12	-36512	1420	952	0	2017	-4112	6.28	6.28	12.57	12.57	3	0.20	0.02	0.10	0.00	0.00	24.0
38	12	-39582	-1108	779	0	1528	3226	6.28	6.28	12.57	12.57	3	0.15	0.02	0.08	0.00	0.00	24.0
39	12	-37182	155	450	0	986	-442	6.28	6.28	12.57	12.57	3	0.04	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-35455	124	713	0	1456	-354	6.28	6.28	12.57	12.57	3	0.05	0.01	0.05	0.00	0.00	24.0
2	25	-27100	323	578	0	1138	-930	6.28	6.28	12.57	12.57	2	0.08	0.01	0.05	0.00	0.00	24.0
3	25	-27060	322	547	0	1171	-927	6.28	6.28	12.57	12.57	2	0.08	0.01	0.04	0.00	0.00	24.0
4	25	-27490	-131	550	0	1068	383	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
5	25	-27450	-132	520	0	1101	386	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
6	25	-27290	165	604	0	1074	-475	6.28	6.28	12.57	12.57	2	0.06	0.01	0.05	0.00	0.00	24.0
7	25	-27140	162	502	0	1186	-464	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
8	25	-27410	29	595	0	1053	-81	6.28	6.28	12.57	12.57	2	0.05	0.01	0.05	0.00	0.00	24.0
9	25	-27260	26	494	0	1165	-70	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
10	25	-27100	323	578	0	1138	-930	6.28	6.28	12.57	12.57	2	0.08	0.01	0.05	0.00	0.00	24.0
11	25	-27060	322	547	0	1171	-927	6.28	6.28	12.57	12.57	2	0.08	0.01	0.04	0.00	0.00	24.0
12	25	-27490	-131	550	0	1068	383	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
13	25	-27450	-132	520	0	1101	386	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
14	25	-27290	165	604	0	1074	-475	6.28	6.28	12.57	12.57	2	0.06	0.01	0.05	0.00	0.00	24.0
15	25	-27140	162	502	0	1186	-464	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
16	25	-27410	29	595	0	1053	-81	6.28	6.28	12.57	12.57	2	0.05	0.01	0.05	0.00	0.00	24.0
17	25	-27260	26	494	0	1165	-70	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
18	25	-38565	932	1006	0	1939	-2568	6.28	6.28	12.57	12.57	3	0.13	0.02	0.07	0.00	0.00	24.0
19	25	-40405	-585	902	0	1658	1646	6.28	6.28	12.57	12.57	3	0.09	0.01	0.06	0.00	0.00	24.0
20	25	-38965	173	704	0	1357	-460	6.28	6.28	12.57	12.57	3	0.05	0.01	0.05	0.00	0.00	24.0
37	25	-36415	1420	952	0	1898	-3934	6.28	6.28	12.57	12.57	3	0.19	0.02	0.10	0.00	0.00	24.0
38	25	-39485	-1108	779	0	1430	3087	6.28	6.28	12.57	12.57	3	0.15	0.02	0.08	0.00	0.00	24.0
39	25	-37085	155	450	0	930	-422	6.28	6.28	12.57	12.57	3	0.04	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-35358	124	713	0	1366	-338	6.28	6.28	12.57	12.57	3	0.05	0.01	0.05	0.00	0.00	24.0
2	38	-27025	323	578	0	1066	-890	6.28	6.28	12.57	12.57	2	0.08	0.01	0.05	0.00	0.00	24.0
3	38	-26985	322	547	0	1102	-887	6.28	6.28	12.57	12.57	2	0.08	0.01	0.04	0.00	0.00	24.0
4	38	-27415	-131	550	0	999	366	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
5	38	-27375	-132	520	0	1036	370	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
6	38	-27215	165	604	0	999	-454	6.28	6.28	12.57	12.57	2	0.06	0.01	0.05	0.00	0.00	24.0

7	38	-27065	162	502	0	1123	-443	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
8	38	-27335	29	595	0	979	-77	6.28	6.28	12.57	12.57	2	0.04	0.01	0.05	0.00	0.00	24.0
9	38	-27185	26	494	0	1103	-66	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
10	38	-27025	323	578	0	1066	-890	6.28	6.28	12.57	12.57	2	0.08	0.01	0.05	0.00	0.00	24.0
11	38	-26985	322	547	0	1102	-887	6.28	6.28	12.57	12.57	2	0.08	0.01	0.04	0.00	0.00	24.0
12	38	-27415	-131	550	0	999	366	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
13	38	-27375	-132	520	0	1036	370	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
14	38	-27215	165	604	0	999	-454	6.28	6.28	12.57	12.57	2	0.06	0.01	0.05	0.00	0.00	24.0
15	38	-27065	162	502	0	1123	-443	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
16	38	-27335	29	595	0	979	-77	6.28	6.28	12.57	12.57	2	0.04	0.01	0.05	0.00	0.00	24.0
17	38	-27185	26	494	0	1103	-66	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
18	38	-38468	932	1006	0	1813	-2451	6.28	6.28	12.57	12.57	3	0.12	0.02	0.07	0.00	0.00	24.0
19	38	-40308	-585	902	0	1545	1572	6.28	6.28	12.57	12.57	3	0.09	0.01	0.06	0.00	0.00	24.0
20	38	-38868	173	704	0	1269	-439	6.28	6.28	12.57	12.57	3	0.05	0.01	0.05	0.00	0.00	24.0
37	38	-36318	1420	952	0	1779	-3756	6.28	6.28	12.57	12.57	3	0.18	0.02	0.10	0.00	0.00	24.0
38	38	-39388	-1108	779	0	1333	2949	6.28	6.28	12.57	12.57	3	0.14	0.02	0.08	0.00	0.00	24.0
39	38	-36988	155	450	0	873	-403	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-35260	124	713	0	1277	-323	6.28	6.28	12.57	12.57	3	0.04	0.01	0.05	0.00	0.00	24.0
2	50	-26950	323	578	0	993	-850	6.28	6.28	12.57	12.57	2	0.07	0.01	0.05	0.00	0.00	24.0
3	50	-26910	322	547	0	1034	-847	6.28	6.28	12.57	12.57	2	0.07	0.01	0.04	0.00	0.00	24.0
4	50	-27340	-131	550	0	930	350	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
5	50	-27300	-132	520	0	972	353	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
6	50	-27140	165	604	0	924	-434	6.28	6.28	12.57	12.57	2	0.05	0.01	0.05	0.00	0.00	24.0
7	50	-26990	162	502	0	1060	-423	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
8	50	-27260	29	595	0	905	-74	6.28	6.28	12.57	12.57	2	0.04	0.01	0.05	0.00	0.00	24.0
9	50	-27110	26	494	0	1041	-63	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
10	50	-26950	323	578	0	993	-850	6.28	6.28	12.57	12.57	2	0.07	0.01	0.05	0.00	0.00	24.0
11	50	-26910	322	547	0	1034	-847	6.28	6.28	12.57	12.57	2	0.07	0.01	0.04	0.00	0.00	24.0
12	50	-27340	-131	550	0	930	350	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
13	50	-27300	-132	520	0	972	353	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
14	50	-27140	165	604	0	924	-434	6.28	6.28	12.57	12.57	2	0.05	0.01	0.05	0.00	0.00	24.0
15	50	-26990	162	502	0	1060	-423	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
16	50	-27260	29	595	0	905	-74	6.28	6.28	12.57	12.57	2	0.04	0.01	0.05	0.00	0.00	24.0
17	50	-27110	26	494	0	1041	-63	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
18	50	-38370	932	1006	0	1687	-2335	6.28	6.28	12.57	12.57	3	0.12	0.02	0.07	0.00	0.00	24.0
19	50	-40210	-585	902	0	1432	1499	6.28	6.28	12.57	12.57	3	0.08	0.01	0.06	0.00	0.00	24.0
20	50	-38770	173	704	0	1181	-417	6.28	6.28	12.57	12.57	3	0.04	0.01	0.05	0.00	0.00	24.0
37	50	-36220	1420	952	0	1660	-3579	6.28	6.28	12.57	12.57	3	0.17	0.02	0.10	0.00	0.00	24.0
38	50	-39290	-1108	779	0	1235	2811	6.28	6.28	12.57	12.57	3	0.13	0.02	0.08	0.00	0.00	24.0
39	50	-36890	155	450	0	817	-383	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 95 NI 1040 NF 301 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 20A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-35260	124	713	0	1277	-323	6.28	6.28	12.57	12.57	3	0.04	0.01	0.05	0.00	0.00	24.0
2	0	-26950	323	578	0	993	-850	6.28	6.28	12.57	12.57	2	0.07	0.01	0.05	0.00	0.00	24.0
3	0	-26910	322	547	0	1034	-847	6.28	6.28	12.57	12.57	2	0.07	0.01	0.04	0.00	0.00	24.0
4	0	-27340	-131	550	0	930	350	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
5	0	-27300	-132	520	0	972	353	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
6	0	-27140	165	604	0	924	-434	6.28	6.28	12.57	12.57	2	0.05	0.01	0.05	0.00	0.00	24.0
7	0	-26990	162	502	0	1060	-423	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
8	0	-27260	29	595	0	905	-74	6.28	6.28	12.57	12.57	2	0.04	0.01	0.05	0.00	0.00	24.0
9	0	-27110	26	494	0	1041	-63	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
10	0	-26950	323	578	0	993	-850	6.28	6.28	12.57	12.57	2	0.07	0.01	0.05	0.00	0.00	24.0
11	0	-26910	322	547	0	1034	-847	6.28	6.28	12.57	12.57	2	0.07	0.01	0.04	0.00	0.00	24.0
12	0	-27340	-131	550	0	930	350	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
13	0	-27300	-132	520	0	972	353	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
14	0	-27140	165	604	0	924	-434	6.28	6.28	12.57	12.57	2	0.05	0.01	0.05	0.00	0.00	24.0
15	0	-26990	162	502	0	1060	-423	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
16	0	-27260	29	595	0	905	-74	6.28	6.28	12.57	12.57	2	0.04	0.01	0.05	0.00	0.00	24.0
17	0	-27110	26	494	0	1041	-63	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
18	0	-38370	932	1006	0	1687	-2335	6.28	6.28	12.57	12.57	3	0.12	0.02	0.07	0.00	0.00	24.0
19	0	-40210	-585	902	0	1432	1499	6.28	6.28	12.57	12.57	3	0.08	0.01	0.06	0.00	0.00	24.0
20	0	-38770	173	704	0	1181	-417	6.28	6.28	12.57	12.57	3	0.04	0.01	0.05	0.00	0.00	24.0
37	0	-36220	1420	952	0	1660	-3579	6.28	6.28	12.57	12.57	3	0.17	0.02	0.10	0.00	0.00	24.0
38	0	-39290	-1108	779	0	1235	2811	6.28	6.28	12.57	12.57	3	0.13	0.02	0.08	0.00	0.00	24.0
39	0	-36890	155	450	0	817	-383	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-35162	124	713	0	1188	-307	6.28	6.28	12.57	12.57	3	0.04	0.01	0.05	0.00	0.00	24.0
2	12	-26875	323	578	0	921	-809	6.28	6.28	12.57	12.57	2	0.07	0.01	0.05	0.00	0.00	24.0
3	12	-26835	322	547	0	966	-806	6.28	6.28	12.57	12.57	2	0.07	0.01	0.04	0.00	0.00	24.0
4	12	-27265	-131	550	0	862	334	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
5	12	-27225	-132	520	0	906	337	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
6	12	-27065	165	604	0	848	-413	6.28	6.28	12.57	12.57	2	0.05	0.01	0.05	0.00	0.00	24.0
7	12	-26915	162	502	0	997	-403	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
8	12	-27185	29	595	0	830	-70	6.28	6.28	12.57	12.57	2	0.04	0.01	0.05	0.00	0.00	24.0
9	12	-27035	26	494	0	979	-60	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
10	12	-26875	323	578	0	921	-809	6.28	6.28	12.57	12.57	2	0.07	0.01	0.05	0.00	0.00	24.0
11	12	-26835	322	547	0	966	-806	6.28	6.28	12.57	12.57	2	0.07	0.01	0.04	0.00	0.00	24.0
12	12	-27265	-131	550	0	862	334	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
13	12	-27225	-132	520	0	906	337	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
14	12	-27065	165	604	0	848	-413	6.28	6.28	12.57	12.57	2	0.05	0.01	0.05	0.00	0.00	24.0
15	12	-26915	162	502	0	997	-403	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
16	12	-27185	29	595	0	830	-70	6.28	6.28	12.57	12.57	2	0.04	0.01	0.05	0.00	0.00	24.0
17	12	-27035	26	494	0	979	-60	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
18	12	-38272	932	1006	0	1561	-2218	6.28	6.28	12.57	12.57	3	0.11	0.02	0.07	0.00	0.00	24.0
19	12	-40112	-585	902	0	1319	1426	6.28	6.28	12.57	12.57	3	0.08	0.01	0.06	0.00	0.00	24.0
20	12	-38672	173	704	0	1093	-396	6.28	6.28	12.57	12.57	3	0.04	0.01	0.05	0.00	0.00	24.0
37	12	-36122	1420	952	0	1541	-3402	6.28	6.28	12.57	12.57	3	0.16	0.02	0.10	0.00	0.00	24.0
38	12	-39192	-1108	779	0	1138	2673	6.28	6.28	12.57	12.57	3	0.13	0.02	0.08	0.00	0.00	24.0
39	12	-36792	155	450	0	761	-364	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-35065	124	713	0	1099	-292	6.28	6.28	12.57	12.57	3	0.04	0.01	0.05	0.00	0.00	24.0
2	25	-26800	323	578	0	849	-769	6.28	6.28	12.57	12.57	2	0.06	0.01	0.05	0.00	0.00	24.0

3	25	-26760	322	547	0	897	-766	6.28	6.28	12.57	12.57	2	0.07	0.01	0.04	0.00	0.00	24.0
4	25	-27190	-131	550	0	793	317	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
5	25	-27150	-132	520	0	842	320	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
6	25	-26990	165	604	0	773	-392	6.28	6.28	12.57	12.57	2	0.05	0.01	0.05	0.00	0.00	24.0
7	25	-26840	162	502	0	934	-382	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
8	25	-27110	29	595	0	756	-66	6.28	6.28	12.57	12.57	2	0.03	0.01	0.05	0.00	0.00	24.0
9	25	-26960	26	494	0	918	-57	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
10	25	-26800	323	578	0	849	-769	6.28	6.28	12.57	12.57	2	0.06	0.01	0.05	0.00	0.00	24.0
11	25	-26760	322	547	0	897	-766	6.28	6.28	12.57	12.57	2	0.07	0.01	0.04	0.00	0.00	24.0
12	25	-27190	-131	550	0	793	317	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
13	25	-27150	-132	520	0	842	320	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
14	25	-26990	165	604	0	773	-392	6.28	6.28	12.57	12.57	2	0.05	0.01	0.05	0.00	0.00	24.0
15	25	-26840	162	502	0	934	-382	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
16	25	-27110	29	595	0	756	-66	6.28	6.28	12.57	12.57	2	0.03	0.01	0.05	0.00	0.00	24.0
17	25	-26960	26	494	0	918	-57	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
18	25	-38175	932	1006	0	1436	-2102	6.28	6.28	12.57	12.57	3	0.10	0.02	0.07	0.00	0.00	24.0
19	25	-40015	-585	902	0	1207	1353	6.28	6.28	12.57	12.57	3	0.07	0.01	0.06	0.00	0.00	24.0
20	25	-38575	173	704	0	1005	-374	6.28	6.28	12.57	12.57	3	0.04	0.01	0.05	0.00	0.00	24.0
37	25	-36025	1420	952	0	1422	-3224	6.28	6.28	12.57	12.57	3	0.15	0.02	0.10	0.00	0.00	24.0
38	25	-39095	-1108	779	0	1040	2534	6.28	6.28	12.57	12.57	3	0.12	0.02	0.08	0.00	0.00	24.0
39	25	-36695	155	450	0	705	-345	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-34968	124	713	0	1010	-276	6.28	6.28	12.57	12.57	3	0.04	0.01	0.05	0.00	0.00	24.0
2	38	-26725	323	578	0	777	-729	6.28	6.28	12.57	12.57	2	0.06	0.01	0.05	0.00	0.00	24.0
3	38	-26685	322	547	0	829	-726	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
4	38	-27115	-131	550	0	724	301	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
5	38	-27075	-132	520	0	777	304	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
6	38	-26915	165	604	0	697	-372	6.28	6.28	12.57	12.57	2	0.04	0.01	0.05	0.00	0.00	24.0
7	38	-26765	162	502	0	872	-362	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
8	38	-27035	29	595	0	681	-63	6.28	6.28	12.57	12.57	2	0.03	0.01	0.05	0.00	0.00	24.0
9	38	-26885	26	494	0	856	-53	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
10	38	-26725	323	578	0	777	-729	6.28	6.28	12.57	12.57	2	0.06	0.01	0.05	0.00	0.00	24.0
11	38	-26685	322	547	0	829	-726	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
12	38	-27115	-131	550	0	724	301	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
13	38	-27075	-132	520	0	777	304	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
14	38	-26915	165	604	0	697	-372	6.28	6.28	12.57	12.57	2	0.04	0.01	0.05	0.00	0.00	24.0
15	38	-26765	162	502	0	872	-362	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
16	38	-27035	29	595	0	681	-63	6.28	6.28	12.57	12.57	2	0.03	0.01	0.05	0.00	0.00	24.0
17	38	-26885	26	494	0	856	-53	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
18	38	-38078	932	1006	0	1310	-1986	6.28	6.28	12.57	12.57	3	0.10	0.02	0.07	0.00	0.00	24.0
19	38	-39918	-585	902	0	1094	1280	6.28	6.28	12.57	12.57	3	0.07	0.01	0.06	0.00	0.00	24.0
20	38	-38478	173	704	0	917	-352	6.28	6.28	12.57	12.57	3	0.03	0.01	0.05	0.00	0.00	24.0
37	38	-35928	1420	952	0	1303	-3046	6.28	6.28	12.57	12.57	3	0.15	0.02	0.10	0.00	0.00	24.0
38	38	-38998	-1108	779	0	943	2396	6.28	6.28	12.57	12.57	3	0.11	0.02	0.08	0.00	0.00	24.0
39	38	-36598	155	450	0	648	-325	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-34870	124	713	0	921	-261	6.28	6.28	12.57	12.57	3	0.03	0.01	0.05	0.00	0.00	24.0
2	50	-26650	323	578	0	705	-688	6.28	6.28	12.57	12.57	2	0.06	0.01	0.05	0.00	0.00	24.0
3	50	-26610	322	547	0	761	-685	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
4	50	-27040	-131	550	0	655	284	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
5	50	-27000	-132	520	0	711	287	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
6	50	-26840	165	604	0	622	-351	6.28	6.28	12.57	12.57	2	0.04	0.01	0.05	0.00	0.00	24.0
7	50	-26690	162	502	0	809	-342	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
8	50	-26960	29	595	0	607	-59	6.28	6.28	12.57	12.57	2	0.03	0.01	0.05	0.00	0.00	24.0
9	50	-26810	26	494	0	794	-50	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
10	50	-26650	323	578	0	705	-688	6.28	6.28	12.57	12.57	2	0.06	0.01	0.05	0.00	0.00	24.0
11	50	-26610	322	547	0	761	-685	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
12	50	-27040	-131	550	0	655	284	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
13	50	-27000	-132	520	0	711	287	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
14	50	-26840	165	604	0	622	-351	6.28	6.28	12.57	12.57	2	0.04	0.01	0.05	0.00	0.00	24.0
15	50	-26690	162	502	0	809	-342	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
16	50	-26960	29	595	0	607	-59	6.28	6.28	12.57	12.57	2	0.03	0.01	0.05	0.00	0.00	24.0
17	50	-26810	26	494	0	794	-50	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
18	50	-37980	932	1006	0	1184	-1869	6.28	6.28	12.57	12.57	3	0.09	0.02	0.07	0.00	0.00	24.0
19	50	-39820	-585	902	0	981	1207	6.28	6.28	12.57	12.57	3	0.06	0.01	0.06	0.00	0.00	24.0
20	50	-38380	173	704	0	829	-331	6.28	6.28	12.57	12.57	3	0.03	0.01	0.05	0.00	0.00	24.0
37	50	-35830	1420	952	0	1184	-2869	6.28	6.28	12.57	12.57	3	0.14	0.02	0.10	0.00	0.00	24.0
38	50	-38900	-1108	779	0	846	2257	6.28	6.28	12.57	12.57	3	0.11	0.02	0.08	0.00	0.00	24.0
39	50	-36500	155	450	0	592	-306	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 96 NI 1352 NF 1355 SEZ. Rp B= 0.400 H= 0.600 (pilastro)
PIL. NUM. 21
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-12730	668	718	0	1449	-2024	12.57	12.57	6.28	6.28	3	0.10	0.01	0.06	0.00	0.00	24.0
2	0	-9713	905	539	0	1088	-2696	12.57	12.57	6.28	6.28	2	0.17	0.02	0.09	0.00	0.00	24.0
3	0	-9846	909	580	0	1180	-2704	12.57	12.57	6.28	6.28	2	0.18	0.02	0.09	0.00	0.00	24.0
4	0	-9733	120	526	0	1050	-409	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
5	0	-9866	123	566	0	1142	-417	12.57	12.57	6.28	6.28	2	0.08	0.01	0.05	0.00	0.00	24.0
6	0	-9564	626	487	0	966	-1886	12.57	12.57	6.28	6.28	2	0.13	0.01	0.06	0.00	0.00	24.0
7	0	-10010	638	622	0	1275	-1913	12.57	12.57	6.28	6.28	2	0.14	0.01	0.06	0.00	0.00	24.0
8	0	-9571	391	483	0	955	-1200	12.57	12.57	6.28	6.28	2	0.10	0.01	0.04	0.00	0.00	24.0
9	0	-10010	402	618	0	1264	-1227	12.57	12.57	6.28	6.28	2	0.11	0.01	0.06	0.00	0.00	24.0
10	0	-9713	905	539	0	1088	-2696	12.57	12.57	6.28	6.28	2	0.17	0.02	0.09	0.00	0.00	24.0
11	0	-9846	909	580	0	1180	-2704	12.57	12.57	6.28	6.28	2	0.18	0.02	0.09	0.00	0.00	24.0
12	0	-9733	120	526	0	1050	-409	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
13	0	-9866	123	566	0	1142	-417	12.57	12.57	6.28	6.28	2	0.08	0.01	0.05	0.00	0.00	24.0
14	0	-9564	626	487	0	966	-1886	12.57	12.57	6.28	6.28	2	0.13	0.01	0.06	0.00	0.00	24.0
15	0	-10010	638	622	0	1275	-1913	12.57	12.57	6.28	6.28	2	0.14	0.01	0.06	0.00	0.00	24.0
16	0	-9571	391	483	0	955	-1200	12.57	12.57	6.28	6.28	2	0.10	0.01	0.04	0.00	0.00	24.0
17	0	-10010	402	618	0	1264	-1227	12.57	12.57	6.28	6.28	2	0.11	0.01	0.06	0.00	0.00	24.0
18	0	-13140	2609	820	0	1695	-7621	12.57	12.57	6.28	6.28	3	0.29	0.04	0.25	0.00	0.00	24.0
19	0	-13190	-38	759	0	1530	62	12.57	12.57	6.28	6.28	3	0.08	0.01	0.07	0.00	0.00	24.0
20	0	-13230	1202	749	0	1491	-3540	12.57	12.57	6.28	6.28	3	0.15	0.02	0.11	0.00	0.00	24.0
37	0	-12880	3288	807	0	1679	-9604	12.57	12.57	6.28	6.28	3	0.36	0.06	0.31	0.00	0.00	24.0
38	0	-12970	-1124	706	0	1404	3202	12.57	12.57	6.28	6.28	3	0.14	0.02	0.11	0.00	0.00	24.0
39	0	-13020	942	690	0	1338	-2801	12.57	12.57	6.28	6.28	3	0.12	0.02	0.09	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-12632	668	718	0	1359	-1940	12.57	12.57	6.28	6.28	3	0.10	0.01	0.06	0.00	0.00	24.0
2	12	-9638	905	539	0	1020	-2583	12.57	12.57	6.28	6.28	2	0.17	0.02	0.09	0.00	0.00	24.0
3	12	-9771	909	580	0	1108	-2590	12.57	12.57	6.28	6.28	2	0.17	0.02	0.09	0.00	0.00	24.0
4	12	-9658	120	526	0	984	-394	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
5	12	-9791	123	566	0	1071	-402	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
6	12	-9489	626	487	0	905	-1808	12.57	12.57	6.28	6.28	2	0.12	0.01	0.06	0.00	0.00	24.0
7	12	-9934	638	622	0	1197	-1834	12.57	12.57	6.28	6.28	2	0.14	0.01	0.06	0.00	0.00	24.0
8	12	-9496	391	483	0	894	-1151	12.57	12.57	6.28	6.28	2	0.09	0.01	0.04	0.00	0.00	24.0
9	12	-9936	402	618	0	1187	-1177	12.57	12.57	6.28	6.28	2	0.11	0.01	0.06	0.00	0.00	24.0
10	12	-9638	905	539	0	1020	-2583	12.57	12.57	6.28	6.28	2	0.17	0.02	0.09	0.00	0.00	24.0
11	12	-9771	909	580	0	1108	-2590	12.57	12.57	6.28	6.28	2	0.17	0.02	0.09	0.00	0.00	24.0
12	12	-9658	120	526	0	984	-394	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
13	12	-9791	123	566	0	1071	-402	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
14	12	-9489	626	487	0	905	-1808	12.57	12.57	6.28	6.28	2	0.12	0.01	0.06	0.00	0.00	24.0
15	12	-9934	638	622	0	1197	-1834	12.57	12.57	6.28	6.28	2	0.14	0.01	0.06	0.00	0.00	24.0
16	12	-9496	391	483	0	894	-1151	12.57	12.57	6.28	6.28	2	0.09	0.01	0.04	0.00	0.00	24.0
17	12	-9936	402	618	0	1187	-1177	12.57	12.57	6.28	6.28	2	0.11	0.01	0.06	0.00	0.00	24.0
18	12	-13042	2609	820	0	1592	-7295	12.57	12.57	6.28	6.28	3	0.28	0.04	0.25	0.00	0.00	24.0
19	12	-13092	-38	759	0	1435	57	12.57	12.57	6.28	6.28	3	0.08	0.01	0.07	0.00	0.00	24.0
20	12	-13132	1202	749	0	1397	-3390	12.57	12.57	6.28	6.28	3	0.14	0.02	0.11	0.00	0.00	24.0
37	12	-12782	3288	807	0	1578	-9193	12.57	12.57	6.28	6.28	3	0.35	0.06	0.32	0.00	0.00	24.0
38	12	-12872	-1124	706	0	1316	3062	12.57	12.57	6.28	6.28	3	0.13	0.02	0.11	0.00	0.00	24.0
39	12	-12922	942	690	0	1252	-2683	12.57	12.57	6.28	6.28	3	0.12	0.02	0.09	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-12535	668	718	0	1270	-1856	12.57	12.57	6.28	6.28	3	0.09	0.01	0.06	0.00	0.00	24.0
2	25	-9563	905	539	0	953	-2469	12.57	12.57	6.28	6.28	2	0.16	0.02	0.09	0.00	0.00	24.0
3	25	-9696	909	580	0	1035	-2477	12.57	12.57	6.28	6.28	2	0.16	0.02	0.09	0.00	0.00	24.0
4	25	-9583	120	526	0	918	-379	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
5	25	-9716	123	566	0	1001	-386	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
6	25	-9414	626	487	0	844	-1730	12.57	12.57	6.28	6.28	2	0.12	0.01	0.06	0.00	0.00	24.0
7	25	-9859	638	622	0	1120	-1754	12.57	12.57	6.28	6.28	2	0.13	0.01	0.06	0.00	0.00	24.0
8	25	-9421	391	483	0	834	-1102	12.57	12.57	6.28	6.28	2	0.09	0.01	0.04	0.00	0.00	24.0
9	25	-9862	402	618	0	1109	-1126	12.57	12.57	6.28	6.28	2	0.10	0.01	0.05	0.00	0.00	24.0
10	25	-9563	905	539	0	953	-2469	12.57	12.57	6.28	6.28	2	0.16	0.02	0.09	0.00	0.00	24.0
11	25	-9696	909	580	0	1035	-2477	12.57	12.57	6.28	6.28	2	0.16	0.02	0.09	0.00	0.00	24.0
12	25	-9583	120	526	0	918	-379	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
13	25	-9716	123	566	0	1001	-386	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
14	25	-9414	626	487	0	844	-1730	12.57	12.57	6.28	6.28	2	0.12	0.01	0.06	0.00	0.00	24.0
15	25	-9859	638	622	0	1120	-1754	12.57	12.57	6.28	6.28	2	0.13	0.01	0.06	0.00	0.00	24.0
16	25	-9421	391	483	0	834	-1102	12.57	12.57	6.28	6.28	2	0.09	0.01	0.04	0.00	0.00	24.0
17	25	-9862	402	618	0	1109	-1126	12.57	12.57	6.28	6.28	2	0.10	0.01	0.05	0.00	0.00	24.0
18	25	-12945	2609	820	0	1490	-6969	12.57	12.57	6.28	6.28	3	0.27	0.04	0.25	0.00	0.00	24.0
19	25	-12995	-38	759	0	1340	53	12.57	12.57	6.28	6.28	3	0.07	0.01	0.07	0.00	0.00	24.0
20	25	-13035	1202	749	0	1304	-3240	12.57	12.57	6.28	6.28	3	0.14	0.02	0.11	0.00	0.00	24.0
37	25	-12685	3288	807	0	1477	-8782	12.57	12.57	6.28	6.28	3	0.33	0.06	0.32	0.00	0.00	24.0
38	25	-12775	-1124	706	0	1227	2921	12.57	12.57	6.28	6.28	3	0.12	0.02	0.11	0.00	0.00	24.0
39	25	-12825	942	690	0	1166	-2565	12.57	12.57	6.28	6.28	3	0.11	0.02	0.09	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	37	-12438	668	718	0	1180	-1773	12.57	12.57	6.28	6.28	3	0.09	0.01	0.06	0.00	0.00	24.0
2	37	-9488	905	539	0	885	-2356	12.57	12.57	6.28	6.28	2	0.15	0.02	0.09	0.00	0.00	24.0
3	37	-9621	909	580	0	963	-2363	12.57	12.57	6.28	6.28	2	0.15	0.02	0.09	0.00	0.00	24.0
4	37	-9508	120	526	0	853	-364	12.57	12.57	6.28	6.28	2	0.06	0.01	0.05	0.00	0.00	24.0
5	37	-9641	123	566	0	930	-371	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
6	37	-9339	626	487	0	784	-1651	12.57	12.57	6.28	6.28	2	0.11	0.01	0.06	0.00	0.00	24.0
7	37	-9783	638	622	0	1042	-1675	12.57	12.57	6.28	6.28	2	0.12	0.01	0.06	0.00	0.00	24.0
8	37	-9346	391	483	0	774	-1053	12.57	12.57	6.28	6.28	2	0.08	0.01	0.04	0.00	0.00	24.0
9	37	-9789	402	618	0	1032	-1076	12.57	12.57	6.28	6.28	2	0.10	0.01	0.05	0.00	0.00	24.0
10	37	-9488	905	539	0	885	-2356	12.57	12.57	6.28	6.28	2	0.15	0.02	0.09	0.00	0.00	24.0
11	37	-9621	909	580	0	963	-2363	12.57	12.57	6.28	6.28	2	0.15	0.02	0.09	0.00	0.00	24.0
12	37	-9508	120	526	0	853	-364	12.57	12.57	6.28	6.28	2	0.06	0.01	0.05	0.00	0.00	24.0
13	37	-9641	123	566	0	930	-371	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
14	37	-9339	626	487	0	784	-1651	12.57	12.57	6.28	6.28	2	0.11	0.01	0.06	0.00	0.00	24.0
15	37	-9783	638	622	0	1042	-1675	12.57	12.57	6.28	6.28	2	0.12	0.01	0.06	0.00	0.00	24.0
16	37	-9346	391	483	0	774	-1053	12.57	12.57	6.28	6.28	2	0.08	0.01	0.04	0.00	0.00	24.0
17	37	-9789	402	618	0	1032	-1076	12.57	12.57	6.28	6.28	2	0.10	0.01	0.05	0.00	0.00	24.0
18	37	-12848	2609	820	0	1388	-6643	12.57	12.57	6.28	6.28	3	0.25	0.04	0.25	0.00	0.00	24.0
19	37	-12898	-38	759	0	1245	48	12.57	12.57	6.28	6.28	3	0.07	0.01	0.07	0.00	0.00	24.0
20	37	-12938	1202	749	0	1210	-3089	12.57	12.57	6.28	6.28	3	0.13	0.02	0.11	0.00	0.00	24.0
37	37	-12588	3288	807	0	1376	-8371	12.57	12.57	6.28	6.28	3	0.31	0.06	0.32	0.00	0.00	24.0
38	37	-12678	-1124	706	0	1138	2781	12.57	12.57	6.28	6.28	3	0.12	0.02	0.11	0.00	0.00	24.0
39	37	-12728	942	690	0	1080	-2448	12.57	12.57	6.28	6.28	3	0.11	0.02	0.09	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-12340	668	718	0	1090	-1689	12.57	12.57	6.28	6.28	3	0.08	0.01	0.06	0.00	0.00	24.0
2	50	-9413	905	539	0	818	-2243	12.57	12.57	6.28	6.28	2	0.14	0.02	0.09	0.00	0.00	24.0
3	50	-9546	909	580	0	890	-2250	12.57	12.57	6.28	6.28	2	0.14	0.02	0.09	0.00	0.00	24.0
4	50	-9433	120	526	0	787	-349	12.57	12.57	6.28	6.28	2	0.06	0.01	0.05	0.00	0.00	24.0
5	50	-9566	123	566	0	859	-356	12.57	12.57	6.28	6.28	2	0.06	0.01	0.05	0.00	0.00	24.0
6	50	-9264	626	487	0	723	-1573	12.57	12.57	6.28	6.28	2	0.11	0.01	0.06	0.00	0.00	24.0
7	50	-9708	638	622	0	964	-1595	12.57	12.57	6.28	6.28	2	0.12	0.01	0.06	0.00	0.00	24.0
8	50	-9271	391	483	0	713	-1004	12.57	12.57	6.28	6.28	2	0.08	0.01	0.04	0.00	0.00	24.0
9	50	-9715	402	618	0	955	-1026	12.57	12.57	6.28	6.28	2	0.09	0.01	0.05	0.00	0.00	24.0
10	50	-9413	905	539	0	818	-2243	12.57	12.57	6.28	6.28	2	0.14	0.02	0.09	0.00	0.00	24.0
11	50	-9546	909	580	0	890	-2250	12.57	12.57	6.28	6.28	2	0.14	0.02	0.09	0.00	0.00	24.0
12	50	-9433	120	526	0	787	-349	12.57	12.57	6.28	6.28	2	0.06	0.01	0.05	0.00	0.00	24.0
13	50	-9566	123	566	0	859	-356	12.57	12.57	6.28	6.28	2	0.06	0.01	0.05	0.00	0.00	24.0
14	50	-9264	626	487	0	723	-1573	12.57	12.57	6.28	6.28	2	0.11	0.01	0.06	0.00	0.00	24.0
15	50	-9708	638	622	0	964	-1595	12.57	12.57	6.28	6.28	2	0.12	0.01	0.06	0.00	0.00	24.0
16	50	-9271	391	483	0	713	-1004	12.57	12.57	6.28	6.28	2	0.08	0.01	0.04	0.00	0.00	24.0
17	50	-9715	402	618	0	955	-1026	12.57	12.57	6.28	6.28	2	0.09	0.01	0.05	0.00	0.00	24.0
18	50	-12750	2609	820	0	1285	-6317	12.57	12.57	6.28	6.28	3	0.24	0.04	0.25	0.00	0.00	24.0
19	50	-12800	-38	759	0	1150	43	12.57	12.57	6.28	6.28	3	0.06	0.01	0.07	0.00	0.00	24.0
20	50	-12840	1202	749	0	1116	-2939	12.57	12.57	6.28	6.28	3	0.12	0.02	0.12	0.00	0.00	24.0
37	50	-12490	3288	807	0	1275	-7960	12.57	12.57	6.28	6.28	3	0.30	0.06	0.32	0.00	0.00	24.0
38	50	-12580	-1124	706	0	1050	2640	12.57	12.57	6.28	6.28	3	0.11	0.02	0.11	0.00	0.00	24.0
39	50	-12630	942	690	0	994	-2330	12.57	12.57	6.28	6.28	3	0.10	0.02	0.09	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 97 NI 1355 NF 172 SEZ. Rp B= 0.400 H= 0.600 (pilastro)
PIL. NUM. 21A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-12340	668	718	0	1090	-1689	12.57	12.57	6.28	6.28	3	0.08	0.01	0.06	0.00	0.00	24.0
2	0	-9413	905	539	0	818	-2243	12.57	12.57	6.28	6.28	2	0.14	0.02	0.09	0.00	0.00	24.0
3	0	-9546	909	580	0	890	-2250	12.57	12.57	6.28	6.28	2	0.14	0.02	0.09	0.00	0.00	24.0
4	0	-9433	120	526	0	787	-349	12.57	12.57	6.28	6.28	2	0.06	0.01	0.05	0.00	0.00	24.0
5	0	-9566	123	566	0	859	-356	12.57	12.57	6.28	6.28	2	0.06	0.01	0.05	0.00	0.00	24.0
6	0	-9264	626	487	0	723	-1573	12.57	12.57	6.28	6.28	2	0.11	0.01	0.06	0.00	0.00	24.0
7	0	-9708	638	622	0	964	-1595	12.57	12.57	6.28	6.28	2	0.12	0.01	0.06	0.00	0.00	24.0
8	0	-9271	391	483	0	713	-1004	12.57	12.57	6.28	6.28	2	0.08	0.01	0.04	0.00	0.00	24.0
9	0	-9715	402	618	0	955	-1026	12.57	12.57	6.28	6.28	2	0.09	0.01	0.05	0.00	0.00	24.0
10	0	-9413	905	539	0	818	-2243	12.57	12.57	6.28	6.28	2	0.14	0.02	0.09	0.00	0.00	24.0
11	0	-9546	909	580	0	890	-2250	12.57	12.57	6.28	6.28	2	0.14	0.02	0.09	0.00	0.00	24.0
12	0	-9433	120	526	0	787	-349	12.57	12.57	6.28	6.28	2	0.06	0.01	0.05	0.00	0.00	24.0
13	0	-9566	123	566	0	859	-356	12.57	12.57	6.28	6.28	2	0.06	0.01	0.05	0.00	0.00	24.0
14	0	-9264	626	487	0	723	-1573	12.57	12.57	6.28	6.28	2	0.11	0.01	0.06	0.00	0.00	24.0
15	0	-9708	638	622	0	964	-1595	12.57	12.57	6.28	6.28	2	0.12	0.01	0.06	0.00	0.00	24.0
16	0	-9271	391	483	0	713	-1004	12.57	12.57	6.28	6.28	2	0.08	0.01	0.04	0.00	0.00	24.0
17	0	-9715	402	618	0	955	-1026	12.57	12.57	6.28	6.28	2	0.09	0.01	0.05	0.00	0.00	24.0
18	0	-12750	2609	820	0	1285	-6317	12.57	12.57	6.28	6.28	3	0.24	0.04	0.25	0.00	0.00	24.0
19	0	-12800	-38	759	0	1150	43	12.57	12.57	6.28	6.28	3	0.06	0.01	0.07	0.00	0.00	24.0
20	0	-12840	1202	749	0	1116	-2939	12.57	12.57	6.28	6.28	3	0.12	0.02	0.12	0.00	0.00	24.0
37	0	-12490	3288	807	0	1275	-7960	12.57	12.57	6.28	6.28	3	0.30	0.06	0.32	0.00	0.00	24.0
38	0	-12580	-1124	706	0	1050	2640	12.57	12.57	6.28	6.28	3	0.11	0.02	0.11	0.00	0.00	24.0
39	0	-12630	942	690	0	994	-2330	12.57	12.57	6.28	6.28	3	0.10	0.02	0.09	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	12	-12242	668	718	0	1000	-1606	12.57	12.57	6.28	6.28	3	0.08	0.01	0.06	0.00	0.00	24.0
2	12	-9338	905	539	0	750	-2130	12.57	12.57	6.28	6.28	2	0.13	0.02	0.09	0.00	0.00	24.0
3	12	-9471	909	580	0	818	-2136	12.57	12.57	6.28	6.28	2	0.14	0.02	0.09	0.00	0.00	24.0
4	12	-9358	120	526	0	721	-334	12.57	12.57	6.28	6.28	2	0.05	0.01	0.05	0.00	0.00	24.0
5	12	-9491	123	566	0	789	-340	12.57	12.57	6.28	6.28	2	0.06	0.01	0.05	0.00	0.00	24.0
6	12	-9189	626	487	0	662	-1495	12.57	12.57	6.28	6.28	2	0.10	0.01	0.06	0.00	0.00	24.0
7	12	-9633	638	622	0	886	-1515	12.57	12.57	6.28	6.28	2	0.11	0.01	0.06	0.00	0.00	24.0
8	12	-9196	391	483	0	653	-955	12.57	12.57	6.28	6.28	2	0.07	0.01	0.04	0.00	0.00	24.0
9	12	-9640	402	618	0	877	-976	12.57	12.57	6.28	6.28	2	0.08	0.01	0.05	0.00	0.00	24.0
10	12	-9338	905	539	0	750	-2130	12.57	12.57	6.28	6.28	2	0.13	0.02	0.09	0.00	0.00	24.0
11	12	-9471	909	580	0	818	-2136	12.57	12.57	6.28	6.28	2	0.14	0.02	0.09	0.00	0.00	24.0
12	12	-9358	120	526	0	721	-334	12.57	12.57	6.28	6.28	2	0.05	0.01	0.05	0.00	0.00	24.0
13	12	-9491	123	566	0	789	-340	12.57	12.57	6.28	6.28	2	0.06	0.01	0.05	0.00	0.00	24.0
14	12	-9189	626	487	0	662	-1495	12.57	12.57	6.28	6.28	2	0.10	0.01	0.06	0.00	0.00	24.0
15	12	-9633	638	622	0	886	-1515	12.57	12.57	6.28	6.28	2	0.11	0.01	0.06	0.00	0.00	24.0
16	12	-9196	391	483	0	653	-955	12.57	12.57	6.28	6.28	2	0.07	0.01	0.04	0.00	0.00	24.0
17	12	-9640	402	618	0	877	-976	12.57	12.57	6.28	6.28	2	0.08	0.01	0.05	0.00	0.00	24.0
18	12	-12652	2609	820	0	1183	-5991	12.57	12.57	6.28	6.28	3	0.23	0.04	0.25	0.00	0.00	24.0
19	12	-12702	-38	759	0	1055	38	12.57	12.57	6.28	6.28	3	0.06	0.01	0.07	0.00	0.00	24.0
20	12	-12742	1202	749	0	1022	-2789	12.57	12.57	6.28	6.28	3	0.11	0.02	0.12	0.00	0.00	24.0
37	12	-12392	3288	807	0	1174	-7549	12.57	12.57	6.28	6.28	3	0.28	0.06	0.32	0.00	0.00	24.0
38	12	-12482	-1124	706	0	962	2499	12.57	12.57	6.28	6.28	3	0.10	0.02	0.11	0.00	0.00	24.0
39	12	-12532	942	690	0	907	-2212	12.57	12.57	6.28	6.28	3	0.09	0.02	0.09	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	25	-12145	668	718	0	910	-1522	12.57	12.57	6.28	6.28	3	0.07	0.01	0.06	0.00	0.00	24.0
2	25	-9263	905	539	0	683	-2017	12.57	12.57	6.28	6.28	2	0.13	0.02	0.09	0.00	0.00	24.0
3	25	-9396	909	580	0	745	-2023	12.57	12.57	6.28	6.28	2	0.13	0.02	0.09	0.00	0.00	24.0
4	25	-9283	120	526	0	656	-319	12.57	12.57	6.28	6.28	2	0.05	0.01	0.05	0.00	0.00	24.0
5	25	-9416	123	566	0	718	-325	12.57	12.57	6.28	6.28	2	0.05	0.01	0.05	0.00	0.00	24.0
6	25	-9114	626	487	0	601	-1417	12.57	12.57	6.28	6.28	2	0.09	0.01	0.06	0.00	0.00	24.0
7	25	-9558	638	622	0	808	-1436	12.57	12.57	6.28	6.28	2	0.10	0.01	0.06	0.00	0.00	24.0
8	25	-9121	391	483	0	592	-906	12.57	12.57	6.28	6.28	2	0.07	0.01	0.04	0.00	0.00	24.0
9	25	-9565	402	618	0	800	-926	12.57	12.57	6.28	6.28	2	0.08	0.01	0.05	0.00	0.00	24.0
10	25	-9263	905	539	0	683	-2017	12.57	12.57	6.28	6.28	2	0.13	0.02	0.09	0.00	0.00	24.0
11	25	-9396	909	580	0	745	-2023	12.57	12.57	6.28	6.28	2	0.13	0.02	0.09	0.00	0.00	24.0
12	25	-9283	120	526	0	656	-319	12.57	12.57	6.28	6.28	2	0.05	0.01	0.05	0.00	0.00	24.0
13	25	-9416	123	566	0	718	-325	12.57	12.57	6.28	6.28	2	0.05	0.01	0.05	0.00	0.00	24.0
14	25	-9114	626	487	0	601	-1417	12.57	12.57	6.28	6.28	2	0.09	0.01	0.06	0.00	0.00	24.0
15	25	-9558	638	622	0	808	-1436	12.57	12.57	6.28	6.28	2	0.10	0.01	0.06	0.00	0.00	24.0
16	25	-9121	391	483	0	592	-906	12.57	12.57	6.28	6.28	2	0.07	0.01	0.04	0.00	0.00	24.0
17	25	-9565	402	618	0	800	-926	12.57	12.57	6.28	6.28	2	0.08	0.01	0.05	0.00	0.00	24.0
18	25	-12555	2609	820	0	1080	-5665	12.57	12.57	6.28	6.28	3	0.21	0.04	0.25	0.00	0.00	24.0
19	25	-12605	-38	759	0	960	33	12.57	12.57	6.28	6.28	3	0.05	0.01	0.07	0.00	0.00	24.0
20	25	-12645	1202	749	0	929	-2638	12.57	12.57	6.28	6.28	3	0.11	0.02	0.12	0.00	0.00	24.0
37	25	-12295	3288	807	0	1073	-7138	12.57	12.57	6.28	6.28	3	0.27	0.06	0.32	0.00	0.00	24.0
38	25	-12385	-1124	706	0	874	2359	12.57	12.57	6.28	6.28	3	0.10	0.02	0.11	0.00	0.00	24.0
39	25	-12435	942	690	0	821	-2094	12.57	12.57	6.28	6.28	3	0.09	0.02	0.09	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	38	-12048	668	718	0	821	-1438	12.57	12.57	6.28	6.28	3	0.07	0.01	0.06	0.00	0.00	24.0
2	38	-9188	905	539	0	616	-1904	12.57	12.57	6.28	6.28	2	0.12	0.02	0.09	0.00	0.00	24.0
3	38	-9321	909	580	0	673	-1910	12.57	12.57	6.28	6.28	2	0.12	0.02	0.09	0.00	0.00	24.0
4	38	-9208	120	526	0	590	-304	12.57	12.57	6.28	6.28	2	0.04	0.01	0.05	0.00	0.00	24.0
5	38	-9341	123	566	0	647	-309	12.57	12.57	6.28	6.28	2	0.05	0.01	0.05	0.00	0.00	24.0
6	38	-9039	626	487	0	540	-1338	12.57	12.57	6.28	6.28	2	0.09	0.01	0.06	0.00	0.00	24.0
7	38	-9483	638	622	0	731	-1356	12.57	12.57	6.28	6.28	2	0.10	0.01	0.06	0.00	0.00	24.0
8	38	-9046	391	483	0	532	-858	12.57	12.57	6.28	6.28	2	0.06	0.01	0.04	0.00	0.00	24.0
9	38	-9490	402	618	0	723	-875	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
10	38	-9188	905	539	0	616	-1904	12.57	12.57	6.28	6.28	2	0.12	0.02	0.09	0.00	0.00	24.0
11	38	-9321	909	580	0	673	-1910	12.57	12.57	6.28	6.28	2	0.12	0.02	0.09	0.00	0.00	24.0
12	38	-9208	120	526	0	590	-304	12.57	12.57	6.28	6.28	2	0.04	0.01	0.05	0.00	0.00	24.0
13	38	-9341	123	566	0	647	-309	12.57	12.57	6.28	6.28	2	0.05	0.01	0.05	0.00	0.00	24.0
14	38	-9039	626	487	0	540	-1338	12.57	12.57	6.28	6.28	2	0.09	0.01	0.06	0.00	0.00	24.0
15	38	-9483	638	622	0	731	-1356	12.57	12.57	6.28	6.28	2	0.10	0.01	0.06	0.00	0.00	24.0
16	38	-9046	391	483	0	532	-858	12.57	12.57	6.28	6.28	2	0.06	0.01	0.04	0.00	0.00	24.0
17	38	-9490	402	618	0	723	-875	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
18	38	-12458	2609	820	0	978	-5338	12.57	12.57	6.28	6.28	3	0.20	0.05	0.25	0.00	0.00	24.0
19	38	-12508	-38	759	0	866	29	12.57	12.57	6.28	6.28	3	0.05	0.01	0.07	0.00	0.00	24.0
20	38	-12548	1202	749	0	835	-2488	12.57	12.57	6.28	6.28	3	0.10	0.02	0.12	0.00	0.00	24.0
37	38	-12198	3288	807	0	972	-6727	12.57	12.57	6.28	6.28	3	0.25	0.06	0.32	0.00	0.00	24.0
38	38	-12288	-1124	706	0	786	2218	12.57	12.57	6.28	6.28	3	0.09	0.02	0.11	0.00	0.00	24.0
39	38	-12338	942	690	0	735	-1977	12.57	12.57	6.28	6.28	3	0.08	0.02	0.09	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-11950	668	718	0	731	-1355	12.57	12.57	6.28	6.28	3	0.06	0.01	0.06	0.00	0.00	24.0
2	50	-9113	905	539	0	548	-1791	12.57	12.57	6.28	6.28	2	0.11	0.02	0.09	0.00	0.00	24.0
3	50	-9246	909	580	0	600	-1796	12.57	12.57	6.28	6.28	2	0.11	0.02	0.09	0.00	0.00	24.0
4	50	-9133	120	526	0	524	-289	12.57	12.57	6.28	6.28	2	0.04	0.01	0.05	0.00	0.00	24.0
5	50	-9266	123	566	0	576	-294	12.57	12.57	6.28	6.28	2	0.04	0.01	0.05	0.00	0.00	24.0
6	50	-8964	626	487	0	479	-1260	12.57	12.57	6.28	6.28	2	0.08	0.01	0.06	0.00	0.00	24.0
7	50	-9408	638	622	0	653	-1276	12.57	12.57	6.28	6.28	2	0.09	0.01	0.06	0.00	0.00	24.0
8	50	-8971	391	483	0	472	-809	12.57	12.57	6.28	6.28	2	0.06	0.01	0.04	0.00	0.00	24.0
9	50	-9415	402	618	0	646	-825	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
10	50	-9113	905	539	0	548	-1791	12.57	12.57	6.28	6.28	2	0.11	0.02	0.09	0.00	0.00	24.0
11	50	-9246	909	580	0	600	-1796	12.57	12.57	6.28	6.28	2	0.11	0.02	0.09	0.00	0.00	24.0
12	50	-9133	120	526	0	524	-289	12.57	12.57	6.28	6.28	2	0.04	0.01	0.05	0.00	0.00	24.0
13	50	-9266	123	566	0	576	-294	12.57	12.57	6.28	6.28	2	0.04	0.01	0.05	0.00	0.00	24.0
14	50	-8964	626	487	0	479	-1260	12.57	12.57	6.28	6.28	2	0.08	0.01	0.06	0.00	0.00	24.0
15	50	-9408	638	622	0	653	-1276	12.57	12.57	6.28	6.28	2	0.09	0.01	0.06	0.00	0.00	24.0
16	50	-8971	391	483	0	472	-809	12.57	12.57	6.28	6.28	2	0.06	0.01	0.04	0.00	0.00	24.0
17	50	-9415	402	618	0	646	-825	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
18	50	-12360	2609	820	0	876	-5012	12.57	12.57	6.28	6.28	3	0.19	0.05	0.25	0.00	0.00	24.0
19	50	-12410	-38	759	0	771	24	12.57	12.57	6.28	6.28	3	0.04	0.01	0.07	0.00	0.00	24.0
20	50	-12450	1202	749	0	742	-2338	12.57	12.57	6.28	6.28	3	0.09	0.02	0.12	0.00	0.00	24.0
37	50	-12100	3288	807	0	872	-6316	12.57	12.57	6.28	6.28	3	0.23	0.06	0.32	0.00	0.00	24.0
38	50	-12190	-1124	706	0	697	2078	12.57	12.57	6.28	6.28	3	0.08	0.02	0.11	0.00	0.00	24.0
39	50	-12240	942	690	0	649	-1859	12.57	12.57	6.28	6.28	3	0.08	0.02	0.09	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 98 NI 479 NF 595 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 7
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-1602	199	-263	0	57	-55	6.28	6.28	9.42	9.42	3	0.01	0.01	0.04	0.00	0.00	24.0
2	0	-1215	142	-166	0	40	-33	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
3	0	-1276	121	-305	0	31	-26	6.28	6.28	9.42	9.42	2	0.00	0.01	0.04	0.00	0.00	24.0
4	0	-1188	185	-99	0	57	-58	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
5	0	-1250	164	-239	0	48	-52	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
6	0	-1134	181	20	0	56	-50	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
7	0	-1339	111	-444	0	27	-27	6.28	6.28	9.42	9.42	2	0.00	0.01	0.06	0.00	0.00	24.0
8	0	-1126	194	40	0	61	-58	6.28	6.28	9.42	9.42	2	0.01	0.01	0.02	0.00	0.00	24.0
9	0	-1331	124	-425	0	32	-35	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
10	0	-1215	142	-166	0	40	-33	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
11	0	-1276	121	-305	0	31	-26	6.28	6.28	9.42	9.42	2	0.00	0.01	0.04	0.00	0.00	24.0
12	0	-1188	185	-99	0	57	-58	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
13	0	-1250	164	-239	0	48	-52	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
14	0	-1134	181	20	0	56	-50	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
15	0	-1339	111	-444	0	27	-27	6.28	6.28	9.42	9.42	2	0.00	0.01	0.06	0.00	0.00	24.0
16	0	-1126	194	40	0	61	-58	6.28	6.28	9.42	9.42	2	0.01	0.01	0.02	0.00	0.00	24.0
17	0	-1331	124	-425	0	32	-35	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
18	0	-1222	37	-450	0	-19	-34	6.28	6.28	9.42	9.42	3	0.00	0.01	0.06	0.00	0.00	24.0
19	0	-1431	507	61	0	92	-197	6.28	6.28	9.42	9.42	3	0.02	0.01	0.06	0.00	0.00	24.0
20	0	-908	-177	-1568	0	-622	13	6.28	6.28	9.42	9.42	3	0.03	0.04	0.22	0.00	0.00	24.0
37	0	-1254	-143	-643	0	-50	41	6.28	6.28	9.42	9.42	3	0.00	0.02	0.09	0.00	0.00	24.0
38	0	-1603	640	208	0	136	-231	6.28	6.28	9.42	9.42	3	0.03	0.02	0.08	0.00	0.00	24.0
39	0	-731	-500	-2507	0	-1055	118	6.28	6.28	9.42	9.42	3	0.06	0.06	0.35	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-1529	199	-263	0	90	-30	6.28	6.28	9.42	9.42	3	0.01	0.01	0.04	0.00	0.00	24.0
2	12	-1159	142	-166	0	61	-15	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
3	12	-1220	121	-305	0	69	-11	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
4	12	-1132	185	-99	0	69	-35	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
5	12	-1194	164	-239	0	78	-31	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
6	12	-1078	181	20	0	54	-27	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
7	12	-1283	111	-444	0	82	-13	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
8	12	-1070	194	40	0	56	-33	6.28	6.28	9.42	9.42	2	0.01	0.01	0.02	0.00	0.00	24.0
9	12	-1275	124	-425	0	85	-19	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
10	12	-1159	142	-166	0	61	-15	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
11	12	-1220	121	-305	0	69	-11	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
12	12	-1132	185	-99	0	69	-35	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
13	12	-1194	164	-239	0	78	-31	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
14	12	-1078	181	20	0	54	-27	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
15	12	-1283	111	-444	0	82	-13	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
16	12	-1070	194	40	0	56	-33	6.28	6.28	9.42	9.42	2	0.01	0.01	0.02	0.00	0.00	24.0
17	12	-1275	124	-425	0	85	-19	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
18	12	-1149	37	-450	0	37	-29	6.28	6.28	9.42	9.42	3	0.00	0.01	0.06	0.00	0.00	24.0
19	12	-1358	507	61	0	85	-133	6.28	6.28	9.42	9.42	3	0.02	0.01	0.06	0.00	0.00	24.0
20	12	-835	-177	-1568	0	-426	-10	6.28	6.28	9.42	9.42	3	0.02	0.04	0.22	0.00	0.00	24.0
37	12	-1181	-143	-643	0	30	23	6.28	6.28	9.42	9.42	3	0.00	0.02	0.09	0.00	0.00	24.0
38	12	-1530	640	208	0	110	-152	6.28	6.28	9.42	9.42	3	0.02	0.02	0.08	0.00	0.00	24.0
39	12	-657	-500	-2507	0	-742	55	6.28	6.28	9.42	9.42	3	0.04	0.06	0.35	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-1456	199	-263	0	123	-5	6.28	6.28	9.42	9.42	3	0.01	0.01	0.04	0.00	0.00	24.0
2	25	-1102	142	-166	0	81	2	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
3	25	-1164	121	-305	0	107	4	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
4	25	-1076	185	-99	0	82	-12	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
5	25	-1138	164	-239	0	108	-11	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
6	25	-1021	181	20	0	51	-5	6.28	6.28	9.42	9.42	2	0.00	0.00	0.02	0.00	0.00	24.0
7	25	-1226	111	-444	0	138	1	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
8	25	-1013	194	40	0	51	-9	6.28	6.28	9.42	9.42	2	0.00	0.01	0.02	0.00	0.00	24.0
9	25	-1218	124	-425	0	138	-4	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
10	25	-1102	142	-166	0	81	2	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
11	25	-1164	121	-305	0	107	4	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
12	25	-1076	185	-99	0	82	-12	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
13	25	-1138	164	-239	0	108	-11	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
14	25	-1021	181	20	0	51	-5	6.28	6.28	9.42	9.42	2	0.00	0.00	0.02	0.00	0.00	24.0
15	25	-1226	111	-444	0	138	1	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
16	25	-1013	194	40	0	51	-9	6.28	6.28	9.42	9.42	2	0.00	0.01	0.02	0.00	0.00	24.0
17	25	-1218	124	-425	0	138	-4	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
18	25	-1076	37	-450	0	93	-24	6.28	6.28	9.42	9.42	3	0.01	0.01	0.06	0.00	0.00	24.0
19	25	-1285	507	61	0	77	-70	6.28	6.28	9.42	9.42	3	0.01	0.01	0.05	0.00	0.00	24.0
20	25	-762	-177	-1568	0	-230	-32	6.28	6.28	9.42	9.42	3	0.01	0.04	0.22	0.00	0.00	24.0
37	25	-1108	-143	-643	0	111	5	6.28	6.28	9.42	9.42	3	0.01	0.02	0.09	0.00	0.00	24.0
38	25	-1457	640	208	0	84	-72	6.28	6.28	9.42	9.42	3	0.01	0.02	0.07	0.00	0.00	24.0

39	25	-584	-500	-2507	0	-428	-8	6.28	6.28	9.42	9.42	3	0.02	0.06	0.35	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-1382	199	-263	0	156	20	6.28	6.28	9.42	9.42	3	0.01	0.01	0.04	0.00	0.00	24.0
2	38	-1046	142	-166	0	102	20	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
3	38	-1107	121	-305	0	145	19	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
4	38	-1019	185	-99	0	94	11	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
5	38	-1081	164	-239	0	138	10	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
6	38	-965	181	20	0	49	18	6.28	6.28	9.42	9.42	2	0.00	0.00	0.02	0.00	0.00	24.0
7	38	-1170	111	-444	0	193	15	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
8	38	-957	194	40	0	46	15	6.28	6.28	9.42	9.42	2	0.00	0.01	0.02	0.00	0.00	24.0
9	38	-1162	124	-425	0	191	12	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
10	38	-1046	142	-166	0	102	20	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
11	38	-1107	121	-305	0	145	19	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
12	38	-1019	185	-99	0	94	11	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
13	38	-1081	164	-239	0	138	10	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
14	38	-965	181	20	0	49	18	6.28	6.28	9.42	9.42	2	0.00	0.00	0.02	0.00	0.00	24.0
15	38	-1170	111	-444	0	193	15	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
16	38	-957	194	40	0	46	15	6.28	6.28	9.42	9.42	2	0.00	0.01	0.02	0.00	0.00	24.0
17	38	-1162	124	-425	0	191	12	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
18	38	-1002	37	-450	0	149	-20	6.28	6.28	9.42	9.42	3	0.01	0.01	0.06	0.00	0.00	24.0
19	38	-1212	507	61	0	69	-7	6.28	6.28	9.42	9.42	3	0.00	0.01	0.05	0.00	0.00	24.0
20	38	-688	-177	-1568	0	-34	-54	6.28	6.28	9.42	9.42	3	0.01	0.04	0.22	0.00	0.00	24.0
37	38	-1035	-143	-643	0	191	-13	6.28	6.28	9.42	9.42	3	0.01	0.02	0.09	0.00	0.00	24.0
38	38	-1384	640	208	0	58	8	6.28	6.28	9.42	9.42	3	0.00	0.02	0.07	0.00	0.00	24.0
39	38	-511	-500	-2507	0	-115	-70	6.28	6.28	9.42	9.42	3	0.01	0.06	0.35	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-1309	199	-263	0	189	44	6.28	6.28	9.42	9.42	3	0.01	0.01	0.04	0.00	0.00	24.0
2	50	-990	142	-166	0	123	38	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
3	50	-1051	121	-305	0	184	34	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
4	50	-963	185	-99	0	107	34	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
5	50	-1025	164	-239	0	168	30	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
6	50	-908	181	20	0	46	41	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
7	50	-1114	111	-444	0	249	29	6.28	6.28	9.42	9.42	2	0.02	0.01	0.06	0.00	0.00	24.0
8	50	-900	194	40	0	41	40	6.28	6.28	9.42	9.42	2	0.01	0.01	0.02	0.00	0.00	24.0
9	50	-1106	124	-425	0	244	27	6.28	6.28	9.42	9.42	2	0.02	0.01	0.06	0.00	0.00	24.0
10	50	-990	142	-166	0	123	38	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
11	50	-1051	121	-305	0	184	34	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
12	50	-963	185	-99	0	107	34	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
13	50	-1025	164	-239	0	168	30	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
14	50	-908	181	20	0	46	41	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
15	50	-1114	111	-444	0	249	29	6.28	6.28	9.42	9.42	2	0.02	0.01	0.06	0.00	0.00	24.0
16	50	-900	194	40	0	41	40	6.28	6.28	9.42	9.42	2	0.01	0.01	0.02	0.00	0.00	24.0
17	50	-1106	124	-425	0	244	27	6.28	6.28	9.42	9.42	2	0.02	0.01	0.06	0.00	0.00	24.0
18	50	-929	37	-450	0	206	-15	6.28	6.28	9.42	9.42	3	0.01	0.01	0.06	0.00	0.00	24.0
19	50	-1139	507	61	0	62	56	6.28	6.28	9.42	9.42	3	0.01	0.01	0.05	0.00	0.00	24.0
20	50	-615	-177	-1568	0	162	-76	6.28	6.28	9.42	9.42	3	0.01	0.04	0.22	0.00	0.00	24.0
37	50	-961	-143	-643	0	272	-31	6.28	6.28	9.42	9.42	3	0.01	0.02	0.09	0.00	0.00	24.0
38	50	-1311	640	208	0	32	88	6.28	6.28	9.42	9.42	3	0.01	0.02	0.08	0.00	0.00	24.0
39	50	-438	-500	-2507	0	198	-133	6.28	6.28	9.42	9.42	3	0.02	0.06	0.35	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 99 NI 595 NF 23 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 7A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-1707	381	-324	0	260	68	6.28	6.28	9.42	9.42	3	0.01	0.01	0.04	0.00	0.00	24.0
2	0	-1271	318	-180	0	165	49	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
3	0	-1321	306	-359	0	248	49	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
4	0	-1304	280	-140	0	151	56	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
5	0	-1355	269	-320	0	235	56	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
6	0	-1223	318	43	0	62	52	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
7	0	-1392	279	-554	0	342	52	6.28	6.28	9.42	9.42	2	0.03	0.01	0.08	0.00	0.00	24.0
8	0	-1234	307	55	0	58	54	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
9	0	-1402	268	-542	0	338	54	6.28	6.28	9.42	9.42	2	0.03	0.01	0.07	0.00	0.00	24.0
10	0	-1271	318	-180	0	165	49	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
11	0	-1321	306	-359	0	248	49	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
12	0	-1304	280	-140	0	151	56	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
13	0	-1355	269	-320	0	235	56	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
14	0	-1223	318	43	0	62	52	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
15	0	-1392	279	-554	0	342	52	6.28	6.28	9.42	9.42	2	0.03	0.01	0.08	0.00	0.00	24.0
16	0	-1234	307	55	0	58	54	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
17	0	-1402	268	-542	0	338	54	6.28	6.28	9.42	9.42	2	0.03	0.01	0.07	0.00	0.00	24.0
18	0	-1341	23	-447	0	329	9	6.28	6.28	9.42	9.42	3	0.02	0.01	0.06	0.00	0.00	24.0
19	0	-1733	520	-61	0	167	150	6.28	6.28	9.42	9.42	3	0.02	0.01	0.06	0.00	0.00	24.0
20	0	-1208	147	-675	0	599	57	6.28	6.28	9.42	9.42	3	0.03	0.02	0.09	0.00	0.00	24.0
37	0	-1284	-106	-597	0	386	-41	6.28	6.28	9.42	9.42	3	0.02	0.01	0.08	0.00	0.00	24.0
38	0	-1937	722	46	0	117	193	6.28	6.28	9.42	9.42	3	0.02	0.02	0.09	0.00	0.00	24.0
39	0	-1062	100	-978	0	837	38	6.28	6.28	9.42	9.42	3	0.04	0.02	0.13	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-1634	381	-324	0	300	116	6.28	6.28	9.42	9.42	3	0.02	0.01	0.04	0.00	0.00	24.0
2	12	-1215	318	-180	0	187	89	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
3	12	-1265	306	-359	0	293	87	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
4	12	-1248	280	-140	0	168	91	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
5	12	-1299	269	-320	0	275	90	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
6	12	-1167	318	43	0	56	91	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
7	12	-1336	279	-554	0	411	86	6.28	6.28	9.42	9.42	2	0.03	0.01	0.08	0.00	0.00	24.0
8	12	-1178	307	55	0	51	92	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
9	12	-1346	268	-542	0	405	87	6.28	6.28	9.42	9.42	2	0.03	0.01	0.07	0.00	0.00	24.0
10	12	-1215	318	-180	0	187	89	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
11	12	-1265	306	-359	0	293	87	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
12	12	-1248	280	-140	0	168	91	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
13	12	-1299	269	-320	0	275	90	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
14	12	-1167	318	43	0	56	91	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
15	12	-1336	279	-554	0	411	86	6.28	6.28	9.42	9.42	2	0.03	0.01	0.08	0.00	0.00	24.0
16	12	-1178	307	55	0	51	92	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
17	12	-1346	268	-542	0	405	87	6.28	6.28	9.42	9.42	2	0.03	0.01	0.07	0.00	0.00	24.0
18	12	-1268	23	-447	0	384	12	6.28	6.28	9.42	9.42	3	0.02	0.01	0.06	0.00	0.00	24.0

19	12	-1660	520	-61	0	175	215	6.28	6.28	9.42	9.42	3	0.03	0.01	0.06	0.00	0.00	24.0
20	12	-1135	147	-675	0	684	75	6.28	6.28	9.42	9.42	3	0.04	0.02	0.09	0.00	0.00	24.0
37	12	-1211	-106	-597	0	461	-54	6.28	6.28	9.42	9.42	3	0.02	0.01	0.08	0.00	0.00	24.0
38	12	-1864	722	46	0	111	283	6.28	6.28	9.42	9.42	3	0.03	0.02	0.09	0.00	0.00	24.0
39	12	-989	100	-978	0	960	51	6.28	6.28	9.42	9.42	3	0.05	0.02	0.13	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-1560	381	-324	0	341	164	6.28	6.28	9.42	9.42	3	0.02	0.01	0.04	0.00	0.00	24.0
2	25	-1158	318	-180	0	209	129	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
3	25	-1208	306	-359	0	338	126	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
4	25	-1192	280	-140	0	186	126	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
5	25	-1242	269	-320	0	315	123	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
6	25	-1111	318	43	0	51	131	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
7	25	-1280	279	-554	0	480	121	6.28	6.28	9.42	9.42	2	0.04	0.01	0.08	0.00	0.00	24.0
8	25	-1122	307	55	0	44	130	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
9	25	-1290	268	-542	0	473	121	6.28	6.28	9.42	9.42	2	0.04	0.01	0.07	0.00	0.00	24.0
10	25	-1158	318	-180	0	209	129	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
11	25	-1208	306	-359	0	338	126	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
12	25	-1192	280	-140	0	186	126	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
13	25	-1242	269	-320	0	315	123	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
14	25	-1111	318	43	0	51	131	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
15	25	-1280	279	-554	0	480	121	6.28	6.28	9.42	9.42	2	0.04	0.01	0.08	0.00	0.00	24.0
16	25	-1122	307	55	0	44	130	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
17	25	-1290	268	-542	0	473	121	6.28	6.28	9.42	9.42	2	0.04	0.01	0.07	0.00	0.00	24.0
18	25	-1195	23	-447	0	440	15	6.28	6.28	9.42	9.42	3	0.02	0.01	0.06	0.00	0.00	24.0
19	25	-1586	520	-61	0	182	280	6.28	6.28	9.42	9.42	3	0.03	0.01	0.06	0.00	0.00	24.0
20	25	-1062	147	-675	0	768	94	6.28	6.28	9.42	9.42	3	0.04	0.02	0.09	0.00	0.00	24.0
37	25	-1138	-106	-597	0	536	-67	6.28	6.28	9.42	9.42	3	0.03	0.01	0.08	0.00	0.00	24.0
38	25	-1791	722	46	0	106	374	6.28	6.28	9.42	9.42	3	0.04	0.02	0.09	0.00	0.00	24.0
39	25	-916	100	-978	0	1082	63	6.28	6.28	9.42	9.42	3	0.06	0.02	0.13	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-1487	381	-324	0	381	211	6.28	6.28	9.42	9.42	3	0.03	0.01	0.04	0.00	0.00	24.0
2	38	-1102	318	-180	0	232	168	6.28	6.28	9.42	9.42	2	0.03	0.01	0.03	0.00	0.00	24.0
3	38	-1152	306	-359	0	383	164	6.28	6.28	9.42	9.42	2	0.04	0.01	0.05	0.00	0.00	24.0
4	38	-1135	280	-140	0	203	161	6.28	6.28	9.42	9.42	2	0.03	0.01	0.03	0.00	0.00	24.0
5	38	-1186	269	-320	0	355	157	6.28	6.28	9.42	9.42	2	0.04	0.01	0.04	0.00	0.00	24.0
6	38	-1055	318	43	0	46	171	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
7	38	-1223	279	-554	0	549	156	6.28	6.28	9.42	9.42	2	0.05	0.01	0.08	0.00	0.00	24.0
8	38	-1065	307	55	0	37	169	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
9	38	-1233	268	-542	0	541	154	6.28	6.28	9.42	9.42	2	0.05	0.01	0.07	0.00	0.00	24.0
10	38	-1102	318	-180	0	232	168	6.28	6.28	9.42	9.42	2	0.03	0.01	0.03	0.00	0.00	24.0
11	38	-1152	306	-359	0	383	164	6.28	6.28	9.42	9.42	2	0.04	0.01	0.05	0.00	0.00	24.0
12	38	-1135	280	-140	0	203	161	6.28	6.28	9.42	9.42	2	0.03	0.01	0.03	0.00	0.00	24.0
13	38	-1186	269	-320	0	355	157	6.28	6.28	9.42	9.42	2	0.04	0.01	0.04	0.00	0.00	24.0
14	38	-1055	318	43	0	46	171	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
15	38	-1223	279	-554	0	549	156	6.28	6.28	9.42	9.42	2	0.05	0.01	0.08	0.00	0.00	24.0
16	38	-1065	307	55	0	37	169	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
17	38	-1233	268	-542	0	541	154	6.28	6.28	9.42	9.42	2	0.05	0.01	0.07	0.00	0.00	24.0
18	38	-1122	23	-447	0	496	18	6.28	6.28	9.42	9.42	3	0.03	0.01	0.06	0.00	0.00	24.0
19	38	-1513	520	-61	0	190	345	6.28	6.28	9.42	9.42	3	0.04	0.01	0.06	0.00	0.00	24.0
20	38	-988	147	-675	0	852	112	6.28	6.28	9.42	9.42	3	0.04	0.02	0.09	0.00	0.00	24.0
37	38	-1065	-106	-597	0	610	-80	6.28	6.28	9.42	9.42	3	0.03	0.01	0.08	0.00	0.00	24.0
38	38	-1718	722	46	0	100	464	6.28	6.28	9.42	9.42	3	0.05	0.02	0.09	0.00	0.00	24.0
39	38	-842	100	-978	0	1204	76	6.28	6.28	9.42	9.42	3	0.06	0.02	0.13	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-1414	381	-324	0	422	259	6.28	6.28	9.42	9.42	3	0.03	0.01	0.04	0.00	0.00	24.0
2	50	-1046	318	-180	0	254	208	6.28	6.28	9.42	9.42	2	0.04	0.01	0.03	0.00	0.00	24.0
3	50	-1096	306	-359	0	428	202	6.28	6.28	9.42	9.42	2	0.04	0.01	0.05	0.00	0.00	24.0
4	50	-1079	280	-140	0	221	196	6.28	6.28	9.42	9.42	2	0.03	0.01	0.03	0.00	0.00	24.0
5	50	-1130	269	-320	0	394	190	6.28	6.28	9.42	9.42	2	0.04	0.01	0.04	0.00	0.00	24.0
6	50	-998	318	43	0	40	210	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
7	50	-1167	279	-554	0	619	191	6.28	6.28	9.42	9.42	2	0.06	0.01	0.08	0.00	0.00	24.0
8	50	-1009	307	55	0	30	207	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
9	50	-1177	268	-542	0	609	188	6.28	6.28	9.42	9.42	2	0.05	0.01	0.07	0.00	0.00	24.0
10	50	-1046	318	-180	0	254	208	6.28	6.28	9.42	9.42	2	0.04	0.01	0.03	0.00	0.00	24.0
11	50	-1096	306	-359	0	428	202	6.28	6.28	9.42	9.42	2	0.04	0.01	0.05	0.00	0.00	24.0
12	50	-1079	280	-140	0	221	196	6.28	6.28	9.42	9.42	2	0.03	0.01	0.03	0.00	0.00	24.0
13	50	-1130	269	-320	0	394	190	6.28	6.28	9.42	9.42	2	0.04	0.01	0.04	0.00	0.00	24.0
14	50	-998	318	43	0	40	210	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
15	50	-1167	279	-554	0	619	191	6.28	6.28	9.42	9.42	2	0.06	0.01	0.08	0.00	0.00	24.0
16	50	-1009	307	55	0	30	207	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
17	50	-1177	268	-542	0	609	188	6.28	6.28	9.42	9.42	2	0.05	0.01	0.07	0.00	0.00	24.0
18	50	-1049	23	-447	0	552	21	6.28	6.28	9.42	9.42	3	0.03	0.01	0.06	0.00	0.00	24.0
19	50	-1440	520	-61	0	198	410	6.28	6.28	9.42	9.42	3	0.05	0.01	0.06	0.00	0.00	24.0
20	50	-915	147	-675	0	937	130	6.28	6.28	9.42	9.42	3	0.05	0.02	0.09	0.00	0.00	24.0
37	50	-992	-106	-597	0	685	-94	6.28	6.28	9.42	9.42	3	0.04	0.01	0.08	0.00	0.00	24.0
38	50	-1645	722	46	0	94	554	6.28	6.28	9.42	9.42	3	0.06	0.02	0.09	0.00	0.00	24.0
39	50	-769	100	-978	0	1326	88	6.28	6.28	9.42	9.42	3	0.07	0.02	0.13	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 100 NI 606 NF 624 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 1
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-9151	-644	301	0	-237	421	6.28	6.28	9.42	9.42	3	0.04	0.02	0.07	0.00	0.00	24.0
2	0	-6525	-585	348	0	-168	328	6.28	6.28	9.42	9.42	2	0.04	0.01	0.07	0.00	0.00	24.0
3	0	-6357	-572	247	0	-146	320	6.28	6.28	9.42	9.42	2	0.04	0.01	0.07	0.00	0.00	24.0
4	0	-7722	-418	217	0	-219	327	6.28	6.28	9.42	9.42	2	0.04	0.01	0.05	0.00	0.00	24.0
5	0	-7554	-405	116	0	-196	319	6.28	6.28	9.42	9.42	2	0.04	0.01	0.05	0.00	0.00	24.0
6	0	-7141	-542	419	0	-212	336	6.28	6.28	9.42	9.42	2	0.05	0.01	0.06	0.00	0.00	24.0
7	0	-6579	-498	83	0	-137	311	6.28	6.28	9.42	9.42	2	0.04	0.01	0.06	0.00	0.00	24.0
8	0	-7500	-492	380	0	-227	336	6.28	6.28	9.42	9.42	2	0.05	0.01	0.06	0.00	0.00	24.0
9	0	-6938	-448	44	0	-152	311	6.28	6.28	9.42	9.42	2	0.04	0.01	0.05	0.00	0.00	24.0
10	0	-6525	-585	348	0	-168	328	6.28	6.28	9.42	9.42	2	0.04	0.01	0.07	0.00	0.00	24.0
11	0	-6357	-572	247	0	-146	320	6.28	6.28	9.42	9.42	2	0.04	0.01	0.07	0.00	0.00	24.0
12	0	-7722	-418	217	0	-219	327	6.28	6.28	9.42	9.42	2	0.04	0.01	0.05	0.00	0.00	24.0
13	0	-7554	-405	116	0	-196	319	6.28	6.28	9.42	9.42	2	0.04	0.01	0.05	0.00	0.00	24.0
14	0	-7141	-542	419	0	-212	336	6.28	6.28	9.42	9.42	2	0.05	0.01	0.06	0.00	0.00	24.0

15	0	-6579	-498	83	0	-137	311	6.28	6.28	9.42	9.42	2	0.04	0.01	0.06	0.00	0.00	24.0
16	0	-7500	-492	380	0	-227	336	6.28	6.28	9.42	9.42	2	0.05	0.01	0.06	0.00	0.00	24.0
17	0	-6938	-448	44	0	-152	311	6.28	6.28	9.42	9.42	2	0.04	0.01	0.05	0.00	0.00	24.0
18	0	-9347	-1128	684	0	-262	507	6.28	6.28	9.42	9.42	3	0.05	0.03	0.12	0.00	0.00	24.0
19	0	-11830	-269	21	0	-420	379	6.28	6.28	9.42	9.42	3	0.04	0.01	0.03	0.00	0.00	24.0
20	0	-10060	-673	151	0	-286	428	6.28	6.28	9.42	9.42	3	0.05	0.02	0.07	0.00	0.00	24.0
37	0	-8050	-1397	889	0	-175	543	6.28	6.28	9.42	9.42	3	0.06	0.04	0.16	0.00	0.00	24.0
38	0	-12190	34	-217	0	-439	330	6.28	6.28	9.42	9.42	3	0.04	0.00	0.02	0.00	0.00	24.0
39	0	-9237	-640	-0	0	-215	410	6.28	6.28	9.42	9.42	3	0.04	0.02	0.07	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-9078	-644	301	0	-275	340	6.28	6.28	9.42	9.42	3	0.04	0.02	0.07	0.00	0.00	24.0
2	12	-6469	-585	348	0	-212	255	6.28	6.28	9.42	9.42	2	0.04	0.01	0.07	0.00	0.00	24.0
3	12	-6301	-572	247	0	-177	249	6.28	6.28	9.42	9.42	2	0.03	0.01	0.07	0.00	0.00	24.0
4	12	-7666	-418	217	0	-246	274	6.28	6.28	9.42	9.42	2	0.04	0.01	0.05	0.00	0.00	24.0
5	12	-7498	-405	116	0	-211	269	6.28	6.28	9.42	9.42	2	0.04	0.01	0.05	0.00	0.00	24.0
6	12	-7085	-542	419	0	-265	269	6.28	6.28	9.42	9.42	2	0.04	0.01	0.06	0.00	0.00	24.0
7	12	-6523	-498	83	0	-148	249	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
8	12	-7444	-492	380	0	-275	274	6.28	6.28	9.42	9.42	2	0.04	0.01	0.05	0.00	0.00	24.0
9	12	-6882	-448	44	0	-158	255	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
10	12	-6469	-585	348	0	-212	255	6.28	6.28	9.42	9.42	2	0.04	0.01	0.07	0.00	0.00	24.0
11	12	-6301	-572	247	0	-177	249	6.28	6.28	9.42	9.42	2	0.03	0.01	0.07	0.00	0.00	24.0
12	12	-7666	-418	217	0	-246	274	6.28	6.28	9.42	9.42	2	0.04	0.01	0.05	0.00	0.00	24.0
13	12	-7498	-405	116	0	-211	269	6.28	6.28	9.42	9.42	2	0.04	0.01	0.05	0.00	0.00	24.0
14	12	-7085	-542	419	0	-265	269	6.28	6.28	9.42	9.42	2	0.04	0.01	0.06	0.00	0.00	24.0
15	12	-6523	-498	83	0	-148	249	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
16	12	-7444	-492	380	0	-275	274	6.28	6.28	9.42	9.42	2	0.04	0.01	0.05	0.00	0.00	24.0
17	12	-6882	-448	44	0	-158	255	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
18	12	-9274	-1128	684	0	-347	366	6.28	6.28	9.42	9.42	3	0.04	0.03	0.12	0.00	0.00	24.0
19	12	-11758	-269	21	0	-423	346	6.28	6.28	9.42	9.42	3	0.04	0.01	0.03	0.00	0.00	24.0
20	12	-9987	-673	151	0	-305	343	6.28	6.28	9.42	9.42	3	0.04	0.02	0.07	0.00	0.00	24.0
37	12	-7977	-1397	889	0	-286	368	6.28	6.28	9.42	9.42	3	0.04	0.04	0.16	0.00	0.00	24.0
38	12	-12118	34	-217	0	-412	334	6.28	6.28	9.42	9.42	3	0.04	0.00	0.02	0.00	0.00	24.0
39	12	-9164	-640	-0	0	-215	330	6.28	6.28	9.42	9.42	3	0.04	0.02	0.07	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-9005	-644	301	0	-312	260	6.28	6.28	9.42	9.42	3	0.03	0.02	0.06	0.00	0.00	24.0
2	25	-6412	-585	348	0	-255	182	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
3	25	-6244	-572	247	0	-207	177	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
4	25	-7610	-418	217	0	-273	222	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
5	25	-7442	-405	116	0	-225	218	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
6	25	-7028	-542	419	0	-317	201	6.28	6.28	9.42	9.42	2	0.04	0.01	0.05	0.00	0.00	24.0
7	25	-6466	-498	83	0	-158	187	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
8	25	-7388	-492	380	0	-322	213	6.28	6.28	9.42	9.42	2	0.04	0.01	0.05	0.00	0.00	24.0
9	25	-6826	-448	44	0	-163	199	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
10	25	-6412	-585	348	0	-255	182	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
11	25	-6244	-572	247	0	-207	177	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
12	25	-7610	-418	217	0	-273	222	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
13	25	-7442	-405	116	0	-225	218	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
14	25	-7028	-542	419	0	-317	201	6.28	6.28	9.42	9.42	2	0.04	0.01	0.05	0.00	0.00	24.0
15	25	-6466	-498	83	0	-158	187	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
16	25	-7388	-492	380	0	-322	213	6.28	6.28	9.42	9.42	2	0.04	0.01	0.05	0.00	0.00	24.0
17	25	-6826	-448	44	0	-163	199	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
18	25	-9201	-1128	684	0	-433	225	6.28	6.28	9.42	9.42	3	0.03	0.03	0.11	0.00	0.00	24.0
19	25	-11685	-269	21	0	-425	312	6.28	6.28	9.42	9.42	3	0.03	0.01	0.03	0.00	0.00	24.0
20	25	-9914	-673	151	0	-323	259	6.28	6.28	9.42	9.42	3	0.03	0.02	0.07	0.00	0.00	24.0
37	25	-7904	-1397	889	0	-397	194	6.28	6.28	9.42	9.42	3	0.03	0.04	0.14	0.00	0.00	24.0
38	25	-12045	34	-217	0	-385	338	6.28	6.28	9.42	9.42	3	0.04	0.00	0.02	0.00	0.00	24.0
39	25	-9091	-640	-0	0	-215	250	6.28	6.28	9.42	9.42	3	0.03	0.02	0.07	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-8932	-644	301	0	-350	179	6.28	6.28	9.42	9.42	3	0.02	0.02	0.06	0.00	0.00	24.0
2	38	-6356	-585	348	0	-299	109	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
3	38	-6188	-572	247	0	-238	106	6.28	6.28	9.42	9.42	2	0.02	0.01	0.06	0.00	0.00	24.0
4	38	-7553	-418	217	0	-300	170	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
5	38	-7385	-405	116	0	-240	167	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
6	38	-6972	-542	419	0	-370	133	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
7	38	-6410	-498	83	0	-168	124	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
8	38	-7331	-492	380	0	-370	151	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
9	38	-6769	-448	44	0	-169	143	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
10	38	-6356	-585	348	0	-299	109	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
11	38	-6188	-572	247	0	-238	106	6.28	6.28	9.42	9.42	2	0.02	0.01	0.06	0.00	0.00	24.0
12	38	-7553	-418	217	0	-300	170	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
13	38	-7385	-405	116	0	-240	167	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
14	38	-6972	-542	419	0	-370	133	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
15	38	-6410	-498	83	0	-168	124	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
16	38	-7331	-492	380	0	-370	151	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
17	38	-6769	-448	44	0	-169	143	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
18	38	-9128	-1128	684	0	-518	84	6.28	6.28	9.42	9.42	3	0.03	0.03	0.11	0.00	0.00	24.0
19	38	-11612	-269	21	0	-428	278	6.28	6.28	9.42	9.42	3	0.03	0.01	0.03	0.00	0.00	24.0
20	38	-9840	-673	151	0	-342	175	6.28	6.28	9.42	9.42	3	0.02	0.02	0.07	0.00	0.00	24.0
37	38	-7831	-1397	889	0	-508	19	6.28	6.28	9.42	9.42	3	0.02	0.04	0.14	0.00	0.00	24.0
38	38	-11972	34	-217	0	-358	342	6.28	6.28	9.42	9.42	3	0.04	0.00	0.02	0.00	0.00	24.0
39	38	-9018	-640	-0	0	-215	170	6.28	6.28	9.42	9.42	3	0.02	0.02	0.06	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-8859	-644	301	0	-388	99	6.28	6.28	9.42	9.42	3	0.02	0.02	0.06	0.00	0.00	24.0
2	50	-6300	-585	348	0	-342	35	6.28	6.28	9.42	9.42	2	0.02	0.01	0.06	0.00	0.00	24.0
3	50	-6132	-572	247	0	-269	34	6.28	6.28	9.42	9.42	2	0.02	0.01	0.06	0.00	0.00	24.0
4	50	-7497	-418	217	0	-327	118	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
5	50	-7329	-405	116	0	-254	117	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
6	50	-6916	-542	419	0	-422	65	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
7	50	-6354	-498	83	0	-179	62	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
8	50	-7275	-492	380	0	-417	90	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
9	50	-6713	-448	44	0	-174	87	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
10	50	-6300	-585	348	0	-342	35	6.28	6.28	9.42	9.42	2	0.02	0.01	0.06	0.00	0.00	24.0
11	50	-6132	-572	247	0	-269	34	6.28	6.28	9.42	9.42	2	0.02	0.01	0.06	0.00	0.00	24.0
12	50	-7497	-418	217	0	-327	118	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
13	50	-7329	-405	116	0	-254	117	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
14	50	-6916	-542	419	0	-422	65	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
15	50	-6354	-498	83	0	-179	62	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
16	50	-7275	-492	380	0	-417	90	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
17	50	-6713	-448	44	0	-174	87	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
18	50	-9055	-1128	684	0	-604	-56	6.28	6.28	9.42	9.42	3	0.03	0.03	0.11	0.00	0.00	24.0
19	50	-11540	-269	21	0	-430	245	6.28	6.28	9.42	9.42	3	0.03	0.01	0.03	0.00	0.00	24.0
20	50	-9767	-673	151	0	-361	91	6.28	6.28	9.42	9.42	3	0.02	0.02	0.07	0.00	0.00	24.0

37	50	-7758	-1397	889	0	-619	-155	6.28	6.28	9.42	9.42	3	0.03	0.04	0.14	0.00	0.00	24.0
38	50	-11900	34	-217	0	-331	346	6.28	6.28	9.42	9.42	3	0.04	0.00	0.02	0.00	0.00	24.0
39	50	-8945	-640	-0	0	-215	91	6.28	6.28	9.42	9.42	3	0.01	0.02	0.06	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 101 NI 624 NF 293 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 1A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-11050	-4	-163	0	-395	76	6.28	6.28	9.42	9.42	3	0.02	0.00	0.02	0.00	0.00	24.0
2	0	-7942	-406	48	0	-360	6	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
3	0	-7777	-399	-131	0	-277	6	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
4	0	-9228	392	-120	0	-332	111	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
5	0	-9063	400	-298	0	-248	110	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
6	0	-8585	-136	198	0	-447	43	6.28	6.28	9.42	9.42	2	0.03	0.00	0.02	0.00	0.00	24.0
7	0	-8034	-110	-398	0	-170	42	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
8	0	-8971	104	148	0	-438	74	6.28	6.28	9.42	9.42	2	0.03	0.00	0.02	0.00	0.00	24.0
9	0	-8420	129	-448	0	-161	74	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
10	0	-7942	-406	48	0	-360	6	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
11	0	-7777	-399	-131	0	-277	6	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
12	0	-9228	392	-120	0	-332	111	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
13	0	-9063	400	-298	0	-248	110	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
14	0	-8585	-136	198	0	-447	43	6.28	6.28	9.42	9.42	2	0.03	0.00	0.02	0.00	0.00	24.0
15	0	-8034	-110	-398	0	-170	42	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
16	0	-8971	104	148	0	-438	74	6.28	6.28	9.42	9.42	2	0.03	0.00	0.02	0.00	0.00	24.0
17	0	-8420	129	-448	0	-161	74	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
18	0	-11850	-1665	310	0	-653	-113	6.28	6.28	9.42	9.42	3	0.03	0.04	0.16	0.00	0.00	24.0
19	0	-14090	1299	-313	0	-429	299	6.28	6.28	9.42	9.42	3	0.03	0.03	0.12	0.00	0.00	24.0
20	0	-12370	-161	-424	0	-362	89	6.28	6.28	9.42	9.42	3	0.02	0.01	0.05	0.00	0.00	24.0
37	0	-10470	-2596	466	0	-681	-256	6.28	6.28	9.42	9.42	3	0.04	0.07	0.25	0.00	0.00	24.0
38	0	-14210	2345	-572	0	-306	430	6.28	6.28	9.42	9.42	3	0.04	0.06	0.24	0.00	0.00	24.0
39	0	-11340	-88	-757	0	-195	80	6.28	6.28	9.42	9.42	3	0.01	0.02	0.09	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-10978	-4	-163	0	-375	75	6.28	6.28	9.42	9.42	3	0.02	0.00	0.02	0.00	0.00	24.0
2	12	-7886	-406	48	0	-366	-45	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
3	12	-7721	-399	-131	0	-260	-44	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
4	12	-9172	392	-120	0	-317	160	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
5	12	-9007	400	-298	0	-211	160	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
6	12	-8529	-136	198	0	-471	26	6.28	6.28	9.42	9.42	2	0.03	0.00	0.02	0.00	0.00	24.0
7	12	-7978	-110	-398	0	-120	29	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
8	12	-8915	104	148	0	-457	87	6.28	6.28	9.42	9.42	2	0.03	0.00	0.02	0.00	0.00	24.0
9	12	-8364	129	-448	0	-105	90	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
10	12	-7886	-406	48	0	-366	-45	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
11	12	-7721	-399	-131	0	-260	-44	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
12	12	-9172	392	-120	0	-317	160	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
13	12	-9007	400	-298	0	-211	160	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
14	12	-8529	-136	198	0	-471	26	6.28	6.28	9.42	9.42	2	0.03	0.00	0.02	0.00	0.00	24.0
15	12	-7978	-110	-398	0	-120	29	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
16	12	-8915	104	148	0	-457	87	6.28	6.28	9.42	9.42	2	0.03	0.00	0.02	0.00	0.00	24.0
17	12	-8364	129	-448	0	-105	90	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
18	12	-11775	-1665	310	0	-692	-321	6.28	6.28	9.42	9.42	3	0.04	0.04	0.16	0.00	0.00	24.0
19	12	-14018	1299	-313	0	-389	461	6.28	6.28	9.42	9.42	3	0.05	0.03	0.13	0.00	0.00	24.0
20	12	-12295	-161	-424	0	-309	69	6.28	6.28	9.42	9.42	3	0.02	0.01	0.05	0.00	0.00	24.0
37	12	-10398	-2596	466	0	-739	-581	6.28	6.28	9.42	9.42	3	0.06	0.07	0.25	0.00	0.00	24.0
38	12	-14138	2345	-572	0	-235	723	6.28	6.28	9.42	9.42	3	0.07	0.06	0.24	0.00	0.00	24.0
39	12	-11268	-88	-757	0	-100	70	6.28	6.28	9.42	9.42	3	0.01	0.02	0.09	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-10905	-4	-163	0	-355	75	6.28	6.28	9.42	9.42	3	0.02	0.00	0.02	0.00	0.00	24.0
2	25	-7830	-406	48	0	-372	-96	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
3	25	-7664	-399	-131	0	-244	-94	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
4	25	-9116	392	-120	0	-302	209	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
5	25	-8950	400	-298	0	-174	210	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
6	25	-8472	-136	198	0	-496	9	6.28	6.28	9.42	9.42	2	0.03	0.00	0.02	0.00	0.00	24.0
7	25	-7922	-110	-398	0	-70	15	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
8	25	-8858	104	148	0	-475	100	6.28	6.28	9.42	9.42	2	0.03	0.00	0.02	0.00	0.00	24.0
9	25	-8308	129	-448	0	-49	106	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
10	25	-7830	-406	48	0	-372	-96	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
11	25	-7664	-399	-131	0	-244	-94	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
12	25	-9116	392	-120	0	-302	209	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
13	25	-8950	400	-298	0	-174	210	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
14	25	-8472	-136	198	0	-496	9	6.28	6.28	9.42	9.42	2	0.03	0.00	0.02	0.00	0.00	24.0
15	25	-7922	-110	-398	0	-70	15	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
16	25	-8858	104	148	0	-475	100	6.28	6.28	9.42	9.42	2	0.03	0.00	0.02	0.00	0.00	24.0
17	25	-8308	129	-448	0	-49	106	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
18	25	-11700	-1665	310	0	-731	-530	6.28	6.28	9.42	9.42	3	0.06	0.04	0.16	0.00	0.00	24.0
19	25	-13945	1299	-313	0	-350	623	6.28	6.28	9.42	9.42	3	0.06	0.03	0.13	0.00	0.00	24.0
20	25	-12220	-161	-424	0	-256	49	6.28	6.28	9.42	9.42	3	0.01	0.01	0.05	0.00	0.00	24.0
37	25	-10325	-2596	466	0	-798	-905	6.28	6.28	9.42	9.42	3	0.10	0.07	0.28	0.00	0.00	24.0
38	25	-14065	2345	-572	0	-163	1017	6.28	6.28	9.42	9.42	3	0.10	0.06	0.24	0.00	0.00	24.0
39	25	-11195	-88	-757	0	-6	59	6.28	6.28	9.42	9.42	3	0.01	0.02	0.09	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-10832	-4	-163	0	-334	74	6.28	6.28	9.42	9.42	3	0.02	0.00	0.02	0.00	0.00	24.0
2	38	-7773	-406	48	0	-378	-147	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
3	38	-7608	-399	-131	0	-228	-144	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
4	38	-9059	392	-120	0	-287	258	6.28	6.28	9.42	9.42	2	0.04	0.01	0.04	0.00	0.00	24.0
5	38	-8894	400	-298	0	-136	260	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
6	38	-8416	-136	198	0	-521	-8	6.28	6.28	9.42	9.42	2	0.03	0.00	0.02	0.00	0.00	24.0
7	38	-7865	-110	-398	0	-21	1	6.28	6.28	9.42	9.42	2	0.00	0.01	0.05	0.00	0.00	24.0
8	38	-8802	104	148	0	-494	113	6.28	6.28	9.42	9.42	2	0.04	0.00	0.02	0.00	0.00	24.0
9	38	-8251	129	-448	0	7	122	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
10	38	-7773	-406	48	0	-378	-147	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
11	38	-7608	-399	-131	0	-228	-144	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
12	38	-9059	392	-120	0	-287	258	6.28	6.28	9.42	9.42	2	0.04	0.01	0.04	0.00	0.00	24.0
13	38	-8894	400	-298	0	-136	260	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
14	38	-8416	-136	198	0	-521	-8	6.28	6.28	9.42	9.42	2	0.03	0.00	0.02	0.00	0.00	24.0
15	38	-7865	-110	-398	0	-21	1	6.28	6.28	9.42	9.42	2	0.00	0.01	0.05	0.00	0.00	24.0
16	38	-8802	104	148	0	-494	113	6.28	6.28	9.42	9.42	2	0.04	0.00	0.02	0.00	0.00	24.0

17	38	-8251	129	-448	0	7	122	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
18	38	-11625	-1665	310	0	-770	-738	6.28	6.28	9.42	9.42	3	0.08	0.04	0.16	0.00	0.00	24.0
19	38	-13872	1299	-313	0	-311	786	6.28	6.28	9.42	9.42	3	0.08	0.03	0.13	0.00	0.00	24.0
20	38	-12145	-161	-424	0	-203	29	6.28	6.28	9.42	9.42	3	0.01	0.01	0.05	0.00	0.00	24.0
37	38	-10252	-2596	466	0	-856	-1230	6.28	6.28	9.42	9.42	3	0.13	0.07	0.28	0.00	0.00	24.0
38	38	-13992	2345	-572	0	-92	1310	6.28	6.28	9.42	9.42	3	0.13	0.06	0.24	0.00	0.00	24.0
39	38	-11122	-88	-757	0	89	48	6.28	6.28	9.42	9.42	3	0.01	0.02	0.09	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-10760	-4	-163	0	-314	74	6.28	6.28	9.42	9.42	3	0.02	0.00	0.02	0.00	0.00	24.0
2	50	-7717	-406	48	0	-384	-197	6.28	6.28	9.42	9.42	2	0.04	0.01	0.04	0.00	0.00	24.0
3	50	-7552	-399	-131	0	-211	-194	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
4	50	-9003	392	-120	0	-272	307	6.28	6.28	9.42	9.42	2	0.04	0.01	0.04	0.00	0.00	24.0
5	50	-8838	400	-298	0	-99	310	6.28	6.28	9.42	9.42	2	0.04	0.01	0.04	0.00	0.00	24.0
6	50	-8360	-136	198	0	-546	-25	6.28	6.28	9.42	9.42	2	0.03	0.00	0.02	0.00	0.00	24.0
7	50	-7809	-110	-398	0	29	-13	6.28	6.28	9.42	9.42	2	0.00	0.01	0.05	0.00	0.00	24.0
8	50	-8746	104	148	0	-512	126	6.28	6.28	9.42	9.42	2	0.04	0.00	0.02	0.00	0.00	24.0
9	50	-8195	129	-448	0	63	138	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
10	50	-7717	-406	48	0	-384	-197	6.28	6.28	9.42	9.42	2	0.04	0.01	0.04	0.00	0.00	24.0
11	50	-7552	-399	-131	0	-211	-194	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
12	50	-9003	392	-120	0	-272	307	6.28	6.28	9.42	9.42	2	0.04	0.01	0.04	0.00	0.00	24.0
13	50	-8838	400	-298	0	-99	310	6.28	6.28	9.42	9.42	2	0.04	0.01	0.04	0.00	0.00	24.0
14	50	-8360	-136	198	0	-546	-25	6.28	6.28	9.42	9.42	2	0.03	0.00	0.02	0.00	0.00	24.0
15	50	-7809	-110	-398	0	29	-13	6.28	6.28	9.42	9.42	2	0.00	0.01	0.05	0.00	0.00	24.0
16	50	-8746	104	148	0	-512	126	6.28	6.28	9.42	9.42	2	0.04	0.00	0.02	0.00	0.00	24.0
17	50	-8195	129	-448	0	63	138	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
18	50	-11550	-1665	310	0	-808	-946	6.28	6.28	9.42	9.42	3	0.10	0.04	0.18	0.00	0.00	24.0
19	50	-13800	1299	-313	0	-272	948	6.28	6.28	9.42	9.42	3	0.09	0.03	0.13	0.00	0.00	24.0
20	50	-12070	-161	-424	0	-150	9	6.28	6.28	9.42	9.42	3	0.01	0.01	0.05	0.00	0.00	24.0
37	50	-10180	-2596	466	0	-914	-1554	6.28	6.28	9.42	9.42	3	0.16	0.07	0.28	0.00	0.00	24.0
38	50	-13920	2345	-572	0	-20	1603	6.28	6.28	9.42	9.42	3	0.16	0.06	0.24	0.00	0.00	24.0
39	50	-11050	-88	-757	0	183	37	6.28	6.28	9.42	9.42	3	0.01	0.02	0.09	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 102 NI 218 NF 132 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 12
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-7502	169	-27	0	117	-17	6.28	6.28	12.57	12.57	3	0.00	0.00	0.01	0.00	0.00	24.0
2	0	-5774	126	-2	0	58	-13	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
3	0	-5782	125	-57	0	168	-13	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
4	0	-5759	135	16	0	11	-13	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
5	0	-5767	134	-40	0	122	-13	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
6	0	-5759	131	70	0	-88	-13	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
7	0	-5786	126	-116	0	281	-13	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
8	0	-5755	134	75	0	-102	-13	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
9	0	-5782	129	-110	0	267	-13	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
10	0	-5774	126	-2	0	58	-13	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
11	0	-5782	125	-57	0	168	-13	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
12	0	-5759	135	16	0	11	-13	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
13	0	-5767	134	-40	0	122	-13	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
14	0	-5759	131	70	0	-88	-13	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
15	0	-5786	126	-116	0	281	-13	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
16	0	-5755	134	75	0	-102	-13	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
17	0	-5782	129	-110	0	267	-13	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
18	0	-8524	53	-144	0	482	-6	6.28	6.28	12.57	12.57	3	0.02	0.00	0.01	0.00	0.00	24.0
19	0	-7995	274	17	0	46	-20	6.28	6.28	12.57	12.57	3	0.00	0.01	0.02	0.00	0.00	24.0
20	0	-8160	142	-305	0	2370	-10	6.28	6.28	12.57	12.57	3	0.09	0.01	0.03	0.00	0.00	24.0
37	0	-8490	-18	-187	0	580	-2	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
38	0	-7608	350	82	0	-145	-27	6.28	6.28	12.57	12.57	3	0.01	0.01	0.03	0.00	0.00	24.0
39	0	-7884	130	-454	0	3728	-9	6.28	6.28	12.57	12.57	3	0.14	0.01	0.05	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-7404	169	-27	0	120	4	6.28	6.28	12.57	12.57	3	0.00	0.00	0.01	0.00	0.00	24.0
2	12	-5699	126	-2	0	58	3	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
3	12	-5707	125	-57	0	176	3	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
4	12	-5684	135	16	0	9	4	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
5	12	-5692	134	-40	0	127	4	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
6	12	-5684	131	70	0	-97	3	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
7	12	-5711	126	-116	0	296	3	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
8	12	-5680	134	75	0	-111	3	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
9	12	-5707	129	-110	0	281	4	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
10	12	-5699	126	-2	0	58	3	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
11	12	-5707	125	-57	0	176	3	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
12	12	-5684	135	16	0	9	4	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
13	12	-5692	134	-40	0	127	4	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
14	12	-5684	131	70	0	-97	3	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
15	12	-5711	126	-116	0	296	3	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
16	12	-5680	134	75	0	-111	3	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
17	12	-5707	129	-110	0	281	4	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
18	12	-8426	53	-144	0	500	1	6.28	6.28	12.57	12.57	3	0.02	0.00	0.01	0.00	0.00	24.0
19	12	-7898	274	17	0	44	14	6.28	6.28	12.57	12.57	3	0.00	0.01	0.02	0.00	0.00	24.0
20	12	-8062	142	-305	0	2408	8	6.28	6.28	12.57	12.57	3	0.09	0.01	0.03	0.00	0.00	24.0
37	12	-8392	-18	-187	0	604	-4	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
38	12	-7510	350	82	0	-155	17	6.28	6.28	12.57	12.57	3	0.01	0.01	0.03	0.00	0.00	24.0
39	12	-7786	130	-454	0	3785	8	6.28	6.28	12.57	12.57	3	0.14	0.01	0.05	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-7307	169	-27	0	123	25	6.28	6.28	12.57	12.57	3	0.00	0.00	0.01	0.00	0.00	24.0
2	25	-5624	126	-2	0	58	18	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
3	25	-5632	125	-57	0	183	18	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
4	25	-5609	135	16	0	7	21	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
5	25	-5617	134	-40	0	132	21	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
6	25	-5609	131	70	0	-105	19	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
7	25	-5636	126	-116	0	310	19	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
8	25	-5605	134	75	0	-121	20	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
9	25	-5632	129	-110	0	295	20	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
10	25	-5624	126	-2	0	58	18	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
11	25	-5632	125	-57	0	183	18	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
12	25	-5609	135	16	0	7	21	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0

13	25	-5617	134	-40	0	132	21	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
14	25	-5609	131	70	0	-105	19	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
15	25	-5636	126	-116	0	310	19	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
16	25	-5605	134	75	0	-121	20	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
17	25	-5632	129	-110	0	295	20	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
18	25	-8329	53	-144	0	518	8	6.28	6.28	12.57	12.57	3	0.02	0.00	0.01	0.00	0.00	24.0
19	25	-7800	274	17	0	42	48	6.28	6.28	12.57	12.57	3	0.00	0.01	0.03	0.00	0.00	24.0
20	25	-7965	142	-305	0	2446	26	6.28	6.28	12.57	12.57	3	0.09	0.01	0.03	0.00	0.00	24.0
37	25	-8295	-18	-187	0	627	-6	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
38	25	-7413	350	82	0	-166	61	6.28	6.28	12.57	12.57	3	0.01	0.01	0.03	0.00	0.00	24.0
39	25	-7689	130	-454	0	3842	24	6.28	6.28	12.57	12.57	3	0.14	0.01	0.05	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-7210	169	-27	0	127	46	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
2	38	-5549	126	-2	0	58	34	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
3	38	-5557	125	-57	0	190	34	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
4	38	-5534	135	16	0	5	38	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
5	38	-5542	134	-40	0	137	37	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
6	38	-5534	131	70	0	-114	36	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
7	38	-5561	126	-116	0	325	35	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
8	38	-5530	134	75	0	-130	37	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
9	38	-5557	129	-110	0	309	36	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
10	38	-5549	126	-2	0	58	34	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
11	38	-5557	125	-57	0	190	34	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
12	38	-5534	135	16	0	5	38	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
13	38	-5542	134	-40	0	137	37	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
14	38	-5534	131	70	0	-114	36	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
15	38	-5561	126	-116	0	325	35	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
16	38	-5530	134	75	0	-130	37	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
17	38	-5557	129	-110	0	309	36	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
18	38	-8232	53	-144	0	536	14	6.28	6.28	12.57	12.57	3	0.02	0.00	0.01	0.00	0.00	24.0
19	38	-7702	274	17	0	40	82	6.28	6.28	12.57	12.57	3	0.00	0.01	0.03	0.00	0.00	24.0
20	38	-7868	142	-305	0	2485	44	6.28	6.28	12.57	12.57	3	0.09	0.01	0.03	0.00	0.00	24.0
37	38	-8198	-18	-187	0	651	-9	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
38	38	-7316	350	82	0	-176	104	6.28	6.28	12.57	12.57	3	0.01	0.01	0.03	0.00	0.00	24.0
39	38	-7592	130	-454	0	3898	40	6.28	6.28	12.57	12.57	3	0.14	0.01	0.05	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-7112	169	-27	0	130	68	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
2	50	-5474	126	-2	0	58	50	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
3	50	-5482	125	-57	0	197	49	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
4	50	-5459	135	16	0	3	55	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
5	50	-5467	134	-40	0	141	54	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
6	50	-5459	131	70	0	-123	52	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
7	50	-5486	126	-116	0	339	50	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
8	50	-5455	134	75	0	-139	54	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
9	50	-5482	129	-110	0	323	52	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
10	50	-5474	126	-2	0	58	50	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
11	50	-5482	125	-57	0	197	49	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
12	50	-5459	135	16	0	3	55	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
13	50	-5467	134	-40	0	141	54	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
14	50	-5459	131	70	0	-123	52	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
15	50	-5486	126	-116	0	339	50	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
16	50	-5455	134	75	0	-139	54	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
17	50	-5482	129	-110	0	323	52	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
18	50	-8134	53	-144	0	554	21	6.28	6.28	12.57	12.57	3	0.02	0.00	0.01	0.00	0.00	24.0
19	50	-7605	274	17	0	38	116	6.28	6.28	12.57	12.57	3	0.01	0.01	0.03	0.00	0.00	24.0
20	50	-7770	142	-305	0	2523	61	6.28	6.28	12.57	12.57	3	0.09	0.01	0.03	0.00	0.00	24.0
37	50	-8100	-18	-187	0	674	-11	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
38	50	-7218	350	82	0	-186	148	6.28	6.28	12.57	12.57	3	0.01	0.01	0.03	0.00	0.00	24.0
39	50	-7494	130	-454	0	3955	56	6.28	6.28	12.57	12.57	3	0.15	0.01	0.05	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 103 NI 132 NF 40 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 12A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-11210	671	-47	0	122	68	6.28	6.28	12.57	12.57	3	0.01	0.01	0.06	0.00	0.00	24.0
2	0	-8631	491	-2	0	51	50	6.28	6.28	12.57	12.57	2	0.00	0.01	0.04	0.00	0.00	24.0
3	0	-8642	487	-101	0	190	49	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
4	0	-8604	545	30	0	-3	55	6.28	6.28	12.57	12.57	2	0.00	0.01	0.05	0.00	0.00	24.0
5	0	-8615	541	-70	0	136	54	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
6	0	-8609	514	126	0	-129	52	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
7	0	-8645	502	-207	0	333	50	6.28	6.28	12.57	12.57	2	0.02	0.01	0.04	0.00	0.00	24.0
8	0	-8601	531	135	0	-146	54	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
9	0	-8637	518	-197	0	316	52	6.28	6.28	12.57	12.57	2	0.02	0.01	0.04	0.00	0.00	24.0
10	0	-8631	491	-2	0	51	50	6.28	6.28	12.57	12.57	2	0.00	0.01	0.04	0.00	0.00	24.0
11	0	-8642	487	-101	0	190	49	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
12	0	-8604	545	30	0	-3	55	6.28	6.28	12.57	12.57	2	0.00	0.01	0.05	0.00	0.00	24.0
13	0	-8615	541	-70	0	136	54	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
14	0	-8609	514	126	0	-129	52	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
15	0	-8645	502	-207	0	333	50	6.28	6.28	12.57	12.57	2	0.02	0.01	0.04	0.00	0.00	24.0
16	0	-8601	531	135	0	-146	54	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
17	0	-8637	518	-197	0	316	52	6.28	6.28	12.57	12.57	2	0.02	0.01	0.04	0.00	0.00	24.0
18	0	-12840	235	-255	0	528	21	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
19	0	-11970	1187	32	0	27	116	6.28	6.28	12.57	12.57	3	0.01	0.02	0.11	0.00	0.00	24.0
20	0	-12230	649	-514	0	2287	61	6.28	6.28	12.57	12.57	3	0.08	0.01	0.05	0.00	0.00	24.0
37	0	-12800	-94	-331	0	646	-11	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
38	0	-11350	1494	148	0	-189	148	6.28	6.28	12.57	12.57	3	0.01	0.03	0.12	0.00	0.00	24.0
39	0	-11780	596	-761	0	3578	56	6.28	6.28	12.57	12.57	3	0.13	0.01	0.07	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-11112	671	-47	0	127	151	6.28	6.28	12.57	12.57	3	0.01	0.01	0.06	0.00	0.00	24.0
2	12	-8556	491	-2	0	51	111	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
3	12	-8567	487	-101	0	202	110	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
4	12	-8529	545	30	0	-7	123	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
5	12	-8540	541	-70	0	145	122	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
6	12	-8534	514	126	0	-145	116	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
7	12	-8570	502	-207	0	359	113	6.28	6.28	12.57	12.57	2	0.02	0.01	0.04	0.00	0.00	24.0
8	12	-8526	531	135	0	-163	120	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0

9	12	-8562	518	-197	0	341	117	6.28	6.28	12.57	12.57	2	0.02	0.01	0.04	0.00	0.00	24.0
10	12	-8556	491	-2	0	51	111	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
11	12	-8567	487	-101	0	202	110	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
12	12	-8529	545	30	0	-7	123	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
13	12	-8540	541	-70	0	145	122	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
14	12	-8534	514	126	0	-145	116	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
15	12	-8570	502	-207	0	359	113	6.28	6.28	12.57	12.57	2	0.02	0.01	0.04	0.00	0.00	24.0
16	12	-8526	531	135	0	-163	120	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
17	12	-8562	518	-197	0	341	117	6.28	6.28	12.57	12.57	2	0.02	0.01	0.04	0.00	0.00	24.0
18	12	-12742	235	-255	0	560	51	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
19	12	-11872	1187	32	0	23	265	6.28	6.28	12.57	12.57	3	0.01	0.02	0.11	0.00	0.00	24.0
20	12	-12132	649	-514	0	2351	142	6.28	6.28	12.57	12.57	3	0.08	0.01	0.05	0.00	0.00	24.0
37	12	-12702	-94	-331	0	688	-22	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
38	12	-11252	1494	148	0	-208	335	6.28	6.28	12.57	12.57	3	0.02	0.03	0.14	0.00	0.00	24.0
39	12	-11682	596	-761	0	3673	131	6.28	6.28	12.57	12.57	3	0.13	0.01	0.07	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-11015	671	-47	0	133	235	6.28	6.28	12.57	12.57	3	0.01	0.01	0.06	0.00	0.00	24.0
2	25	-8481	491	-2	0	52	173	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
3	25	-8492	487	-101	0	215	171	6.28	6.28	12.57	12.57	2	0.02	0.01	0.04	0.00	0.00	24.0
4	25	-8454	545	30	0	-10	191	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
5	25	-8465	541	-70	0	153	189	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
6	25	-8459	514	126	0	-161	181	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
7	25	-8495	502	-207	0	384	176	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
8	25	-8451	531	135	0	-179	186	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
9	25	-8487	518	-197	0	366	181	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
10	25	-8481	491	-2	0	52	173	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
11	25	-8492	487	-101	0	215	171	6.28	6.28	12.57	12.57	2	0.02	0.01	0.04	0.00	0.00	24.0
12	25	-8454	545	30	0	-10	191	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
13	25	-8465	541	-70	0	153	189	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
14	25	-8459	514	126	0	-161	181	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
15	25	-8495	502	-207	0	384	176	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
16	25	-8451	531	135	0	-179	186	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
17	25	-8487	518	-197	0	366	181	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
18	25	-12645	235	-255	0	592	80	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
19	25	-11775	1187	32	0	19	413	6.28	6.28	12.57	12.57	3	0.02	0.02	0.11	0.00	0.00	24.0
20	25	-12035	649	-514	0	2415	224	6.28	6.28	12.57	12.57	3	0.09	0.01	0.05	0.00	0.00	24.0
37	25	-12605	-94	-331	0	729	-34	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
38	25	-11155	1494	148	0	-226	522	6.28	6.28	12.57	12.57	3	0.03	0.03	0.14	0.00	0.00	24.0
39	25	-11585	596	-761	0	3768	205	6.28	6.28	12.57	12.57	3	0.14	0.01	0.07	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-10918	671	-47	0	139	319	6.28	6.28	12.57	12.57	3	0.02	0.01	0.06	0.00	0.00	24.0
2	38	-8406	491	-2	0	52	234	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
3	38	-8417	487	-101	0	228	232	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
4	38	-8379	545	30	0	-14	259	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
5	38	-8390	541	-70	0	162	257	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
6	38	-8384	514	126	0	-177	245	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
7	38	-8420	502	-207	0	410	239	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
8	38	-8376	531	135	0	-196	252	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
9	38	-8412	518	-197	0	391	246	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
10	38	-8406	491	-2	0	52	234	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
11	38	-8417	487	-101	0	228	232	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
12	38	-8379	545	30	0	-14	259	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
13	38	-8390	541	-70	0	162	257	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
14	38	-8384	514	126	0	-177	245	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
15	38	-8420	502	-207	0	410	239	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
16	38	-8376	531	135	0	-196	252	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
17	38	-8412	518	-197	0	391	246	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
18	38	-12548	235	-255	0	624	109	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
19	38	-11678	1187	32	0	15	562	6.28	6.28	12.57	12.57	3	0.03	0.02	0.11	0.00	0.00	24.0
20	38	-11938	649	-514	0	2480	305	6.28	6.28	12.57	12.57	3	0.09	0.01	0.05	0.00	0.00	24.0
37	38	-12508	-94	-331	0	771	-46	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
38	38	-11058	1494	148	0	-245	708	6.28	6.28	12.57	12.57	3	0.04	0.03	0.14	0.00	0.00	24.0
39	38	-11488	596	-761	0	3863	280	6.28	6.28	12.57	12.57	3	0.14	0.01	0.07	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-10820	671	-47	0	145	403	6.28	6.28	12.57	12.57	3	0.02	0.01	0.06	0.00	0.00	24.0
2	50	-8331	491	-2	0	52	295	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
3	50	-8342	487	-101	0	240	293	6.28	6.28	12.57	12.57	2	0.03	0.01	0.05	0.00	0.00	24.0
4	50	-8304	545	30	0	-18	327	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
5	50	-8315	541	-70	0	171	325	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
6	50	-8309	514	126	0	-192	309	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
7	50	-8345	502	-207	0	436	301	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
8	50	-8301	531	135	0	-213	319	6.28	6.28	12.57	12.57	2	0.03	0.01	0.05	0.00	0.00	24.0
9	50	-8337	518	-197	0	415	311	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
10	50	-8331	491	-2	0	52	295	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
11	50	-8342	487	-101	0	240	293	6.28	6.28	12.57	12.57	2	0.03	0.01	0.05	0.00	0.00	24.0
12	50	-8304	545	30	0	-18	327	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
13	50	-8315	541	-70	0	171	325	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
14	50	-8309	514	126	0	-192	309	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
15	50	-8345	502	-207	0	436	301	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
16	50	-8301	531	135	0	-213	319	6.28	6.28	12.57	12.57	2	0.03	0.01	0.05	0.00	0.00	24.0
17	50	-8337	518	-197	0	415	311	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
18	50	-12450	235	-255	0	656	138	6.28	6.28	12.57	12.57	3	0.03	0.00	0.02	0.00	0.00	24.0
19	50	-11580	1187	32	0	11	710	6.28	6.28	12.57	12.57	3	0.04	0.02	0.11	0.00	0.00	24.0
20	50	-11840	649	-514	0	2544	386	6.28	6.28	12.57	12.57	3	0.10	0.01	0.05	0.00	0.00	24.0
37	50	-12410	-94	-331	0	812	-58	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
38	50	-10960	1494	148	0	-263	895	6.28	6.28	12.57	12.57	3	0.05	0.03	0.14	0.00	0.00	24.0
39	50	-11390	596	-761	0	3958	354	6.28	6.28	12.57	12.57	3	0.14	0.01	0.07	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 104 NI 1350 NF 1445 SEZ. Rp B= 0.400 H= 0.600 (pilastro)
PIL. NUM. 11
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-8432	488	440	0	833	-2148	12.57	12.57	6.28	6.28	3	0.09	0.01	0.05	0.00	0.00	24.0
2	0	-6294	642	337	0	644	-2517	12.57	12.57	6.28	6.28	2	0.15	0.01	0.07	0.00	0.00	24.0
3	0	-6398	645	370	0	718	-2530	12.57	12.57	6.28	6.28	2	0.16	0.01	0.07	0.00	0.00	24.0
4	0	-6573	106	307	0	564	-774	12.57	12.57	6.28	6.28	2	0.06	0.01	0.03	0.00	0.00	24.0

5	0	-6678	110	340	0	638	-787	12.57	12.57	6.28	6.28	2	0.07	0.01	0.03	0.00	0.00	24.0
6	0	-6269	450	288	0	529	-1892	12.57	12.57	6.28	6.28	2	0.12	0.01	0.05	0.00	0.00	24.0
7	0	-6618	462	398	0	776	-1935	12.57	12.57	6.28	6.28	2	0.13	0.01	0.05	0.00	0.00	24.0
8	0	-6353	289	279	0	505	-1369	12.57	12.57	6.28	6.28	2	0.09	0.01	0.03	0.00	0.00	24.0
9	0	-6702	302	389	0	752	-1412	12.57	12.57	6.28	6.28	2	0.10	0.01	0.03	0.00	0.00	24.0
10	0	-6294	642	337	0	644	-2517	12.57	12.57	6.28	6.28	2	0.15	0.01	0.07	0.00	0.00	24.0
11	0	-6398	645	370	0	718	-2530	12.57	12.57	6.28	6.28	2	0.16	0.01	0.07	0.00	0.00	24.0
12	0	-6573	106	307	0	564	-774	12.57	12.57	6.28	6.28	2	0.06	0.01	0.03	0.00	0.00	24.0
13	0	-6678	110	340	0	638	-787	12.57	12.57	6.28	6.28	2	0.07	0.01	0.03	0.00	0.00	24.0
14	0	-6269	450	288	0	529	-1892	12.57	12.57	6.28	6.28	2	0.12	0.01	0.05	0.00	0.00	24.0
15	0	-6618	462	398	0	776	-1935	12.57	12.57	6.28	6.28	2	0.13	0.01	0.05	0.00	0.00	24.0
16	0	-6353	289	279	0	505	-1369	12.57	12.57	6.28	6.28	2	0.09	0.01	0.03	0.00	0.00	24.0
17	0	-6702	302	389	0	752	-1412	12.57	12.57	6.28	6.28	2	0.10	0.01	0.03	0.00	0.00	24.0
18	0	-7889	1768	502	0	1011	-6261	12.57	12.57	6.28	6.28	3	0.24	0.03	0.18	0.00	0.00	24.0
19	0	-8902	-2	427	0	790	-513	12.57	12.57	6.28	6.28	3	0.05	0.01	0.04	0.00	0.00	24.0
20	0	-8424	830	419	0	763	-3217	12.57	12.57	6.28	6.28	3	0.13	0.01	0.08	0.00	0.00	24.0
37	0	-7515	2229	516	0	1058	-7771	12.57	12.57	6.28	6.28	3	0.30	0.04	0.23	0.00	0.00	24.0
38	0	-9203	-721	390	0	690	1809	12.57	12.57	6.28	6.28	3	0.08	0.01	0.07	0.00	0.00	24.0
39	0	-8406	665	378	0	645	-2699	12.57	12.57	6.28	6.28	3	0.11	0.01	0.07	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-8334	488	440	0	778	-2087	12.57	12.57	6.28	6.28	3	0.09	0.01	0.05	0.00	0.00	24.0
2	12	-6219	642	337	0	601	-2437	12.57	12.57	6.28	6.28	2	0.15	0.01	0.07	0.00	0.00	24.0
3	12	-6323	645	370	0	671	-2450	12.57	12.57	6.28	6.28	2	0.15	0.01	0.07	0.00	0.00	24.0
4	12	-6498	106	307	0	525	-760	12.57	12.57	6.28	6.28	2	0.06	0.01	0.03	0.00	0.00	24.0
5	12	-6603	110	340	0	595	-773	12.57	12.57	6.28	6.28	2	0.06	0.01	0.03	0.00	0.00	24.0
6	12	-6194	450	288	0	493	-1836	12.57	12.57	6.28	6.28	2	0.11	0.01	0.05	0.00	0.00	24.0
7	12	-6543	462	398	0	726	-1877	12.57	12.57	6.28	6.28	2	0.12	0.01	0.05	0.00	0.00	24.0
8	12	-6278	289	279	0	470	-1333	12.57	12.57	6.28	6.28	2	0.09	0.01	0.03	0.00	0.00	24.0
9	12	-6627	302	389	0	704	-1374	12.57	12.57	6.28	6.28	2	0.10	0.01	0.03	0.00	0.00	24.0
10	12	-6219	642	337	0	601	-2437	12.57	12.57	6.28	6.28	2	0.15	0.01	0.07	0.00	0.00	24.0
11	12	-6323	645	370	0	671	-2450	12.57	12.57	6.28	6.28	2	0.15	0.01	0.07	0.00	0.00	24.0
12	12	-6498	106	307	0	525	-760	12.57	12.57	6.28	6.28	2	0.06	0.01	0.03	0.00	0.00	24.0
13	12	-6603	110	340	0	595	-773	12.57	12.57	6.28	6.28	2	0.06	0.01	0.03	0.00	0.00	24.0
14	12	-6194	450	288	0	493	-1836	12.57	12.57	6.28	6.28	2	0.11	0.01	0.05	0.00	0.00	24.0
15	12	-6543	462	398	0	726	-1877	12.57	12.57	6.28	6.28	2	0.12	0.01	0.05	0.00	0.00	24.0
16	12	-6278	289	279	0	470	-1333	12.57	12.57	6.28	6.28	2	0.09	0.01	0.03	0.00	0.00	24.0
17	12	-6627	302	389	0	704	-1374	12.57	12.57	6.28	6.28	2	0.10	0.01	0.03	0.00	0.00	24.0
18	12	-7792	1768	502	0	948	-6040	12.57	12.57	6.28	6.28	3	0.23	0.03	0.18	0.00	0.00	24.0
19	12	-8804	-2	427	0	737	-513	12.57	12.57	6.28	6.28	3	0.04	0.01	0.04	0.00	0.00	24.0
20	12	-8326	830	419	0	711	-3113	12.57	12.57	6.28	6.28	3	0.12	0.01	0.08	0.00	0.00	24.0
37	12	-7418	2229	516	0	993	-7492	12.57	12.57	6.28	6.28	3	0.29	0.04	0.23	0.00	0.00	24.0
38	12	-9106	-721	390	0	641	1719	12.57	12.57	6.28	6.28	3	0.07	0.01	0.07	0.00	0.00	24.0
39	12	-8308	665	378	0	598	-2616	12.57	12.57	6.28	6.28	3	0.10	0.01	0.07	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-8237	488	440	0	723	-2025	12.57	12.57	6.28	6.28	3	0.09	0.01	0.05	0.00	0.00	24.0
2	25	-6144	642	337	0	559	-2357	12.57	12.57	6.28	6.28	2	0.14	0.01	0.07	0.00	0.00	24.0
3	25	-6248	645	370	0	625	-2369	12.57	12.57	6.28	6.28	2	0.15	0.01	0.07	0.00	0.00	24.0
4	25	-6423	106	307	0	487	-747	12.57	12.57	6.28	6.28	2	0.06	0.01	0.03	0.00	0.00	24.0
5	25	-6528	110	340	0	553	-759	12.57	12.57	6.28	6.28	2	0.06	0.01	0.03	0.00	0.00	24.0
6	25	-6119	450	288	0	457	-1780	12.57	12.57	6.28	6.28	2	0.11	0.01	0.05	0.00	0.00	24.0
7	25	-6468	462	398	0	677	-1820	12.57	12.57	6.28	6.28	2	0.12	0.01	0.05	0.00	0.00	24.0
8	25	-6203	289	279	0	435	-1297	12.57	12.57	6.28	6.28	2	0.08	0.01	0.03	0.00	0.00	24.0
9	25	-6552	302	389	0	655	-1336	12.57	12.57	6.28	6.28	2	0.09	0.01	0.03	0.00	0.00	24.0
10	25	-6144	642	337	0	559	-2357	12.57	12.57	6.28	6.28	2	0.14	0.01	0.07	0.00	0.00	24.0
11	25	-6248	645	370	0	625	-2369	12.57	12.57	6.28	6.28	2	0.15	0.01	0.07	0.00	0.00	24.0
12	25	-6423	106	307	0	487	-747	12.57	12.57	6.28	6.28	2	0.06	0.01	0.03	0.00	0.00	24.0
13	25	-6528	110	340	0	553	-759	12.57	12.57	6.28	6.28	2	0.06	0.01	0.03	0.00	0.00	24.0
14	25	-6119	450	288	0	457	-1780	12.57	12.57	6.28	6.28	2	0.11	0.01	0.05	0.00	0.00	24.0
15	25	-6468	462	398	0	677	-1820	12.57	12.57	6.28	6.28	2	0.12	0.01	0.05	0.00	0.00	24.0
16	25	-6203	289	279	0	435	-1297	12.57	12.57	6.28	6.28	2	0.08	0.01	0.03	0.00	0.00	24.0
17	25	-6552	302	389	0	655	-1336	12.57	12.57	6.28	6.28	2	0.09	0.01	0.03	0.00	0.00	24.0
18	25	-7694	1768	502	0	885	-5819	12.57	12.57	6.28	6.28	3	0.22	0.03	0.18	0.00	0.00	24.0
19	25	-8707	-2	427	0	683	-513	12.57	12.57	6.28	6.28	3	0.04	0.01	0.04	0.00	0.00	24.0
20	25	-8229	830	419	0	658	-3009	12.57	12.57	6.28	6.28	3	0.12	0.01	0.08	0.00	0.00	24.0
37	25	-7320	2229	516	0	929	-7214	12.57	12.57	6.28	6.28	3	0.28	0.04	0.23	0.00	0.00	24.0
38	25	-9008	-721	390	0	593	1628	12.57	12.57	6.28	6.28	3	0.07	0.01	0.07	0.00	0.00	24.0
39	25	-8211	665	378	0	551	-2532	12.57	12.57	6.28	6.28	3	0.10	0.01	0.07	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	37	-8140	488	440	0	668	-1964	12.57	12.57	6.28	6.28	3	0.08	0.01	0.05	0.00	0.00	24.0
2	37	-6069	642	337	0	517	-2277	12.57	12.57	6.28	6.28	2	0.14	0.01	0.07	0.00	0.00	24.0
3	37	-6173	645	370	0	579	-2289	12.57	12.57	6.28	6.28	2	0.14	0.01	0.07	0.00	0.00	24.0
4	37	-6348	106	307	0	448	-734	12.57	12.57	6.28	6.28	2	0.06	0.01	0.03	0.00	0.00	24.0
5	37	-6453	110	340	0	510	-745	12.57	12.57	6.28	6.28	2	0.06	0.01	0.03	0.00	0.00	24.0
6	37	-6044	450	288	0	421	-1723	12.57	12.57	6.28	6.28	2	0.11	0.01	0.05	0.00	0.00	24.0
7	37	-6393	462	398	0	627	-1762	12.57	12.57	6.28	6.28	2	0.11	0.01	0.05	0.00	0.00	24.0
8	37	-6128	289	279	0	401	-1260	12.57	12.57	6.28	6.28	2	0.08	0.01	0.03	0.00	0.00	24.0
9	37	-6477	302	389	0	606	-1299	12.57	12.57	6.28	6.28	2	0.09	0.01	0.03	0.00	0.00	24.0
10	37	-6069	642	337	0	517	-2277	12.57	12.57	6.28	6.28	2	0.14	0.01	0.07	0.00	0.00	24.0
11	37	-6173	645	370	0	579	-2289	12.57	12.57	6.28	6.28	2	0.14	0.01	0.07	0.00	0.00	24.0
12	37	-6348	106	307	0	448	-734	12.57	12.57	6.28	6.28	2	0.06	0.01	0.03	0.00	0.00	24.0
13	37	-6453	110	340	0	510	-745	12.57	12.57	6.28	6.28	2	0.06	0.01	0.03	0.00	0.00	24.0
14	37	-6044	450	288	0	421	-1723	12.57	12.57	6.28	6.28	2	0.11	0.01	0.05	0.00	0.00	24.0
15	37	-6393	462	398	0	627	-1762	12.57	12.57	6.28	6.28	2	0.11	0.01	0.05	0.00	0.00	24.0
16	37	-6128	289	279	0	401	-1260	12.57	12.57	6.28	6.28	2	0.08	0.01	0.03	0.00	0.00	24.0
17	37	-6477	302	389	0	606	-1299	12.57	12.57	6.28	6.28	2	0.09	0.01	0.03	0.00	0.00	24.0
18	37	-7596	1768	502	0	823	-5598	12.57	12.57	6.28	6.28	3	0.22	0.03	0.18	0.00	0.00	24.0
19	37	-8610	-2	427	0	630	-513	12.57	12.57	6.28	6.28	3	0.04	0.01	0.04	0.00	0.00	24.0
20	37	-8132	830	419	0	606	-2906	12.57	12.57	6.28	6.28	3	0.11	0.01	0.08	0.00	0.00	24.0
37	37	-7222	2229	516	0	864	-6936	12.57	12.57	6.28	6.28	3	0.27	0.04	0.23	0.00	0.00	24.0
38	37	-8910	-721	390	0	544	1538	12.57	12.57	6.28	6.28	3	0.06	0.01	0.07	0.00	0.00	24.0
39	37	-8114	665	378	0	503	-2449	12.57	12.57	6.28	6.28	3	0.10	0.01	0.07	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-8042	488	440	0	613	-1903	12.57	12.57	6.28	6.28	3	0.08	0.01	0.05	0.00	0.00	24.0
2	50	-5994	642	337	0	475	-2197	12.57	12.57	6.28	6.28	2	0.13	0.01	0.07	0.00	0.00	24.0
3	50	-6098	645	370	0	533	-2208	12.57	12.57	6.28	6.28	2	0.13	0.01	0.07	0.00	0.00	24.0
4	50	-6273	106	307	0	410	-721	12.57	12.57	6.28	6.28	2	0.05	0.01	0.03	0.00	0.00	24.0
5	50	-6378	110	340	0	468	-732	12.57	12.57	6.28	6.28	2	0.06	0.01	0.03	0.00	0.00	24.0
6	50	-5969	450	288	0	385	-1667	12.57	12.57	6.28	6.28	2	0.10	0.01	0.05	0.00	0.00	24.0
7	50	-6318	462	398	0	577	-1704	12.57	12.57	6.28	6.28	2	0.11	0.01	0.05	0.00	0.00	24.0
8	50	-6053	289	279	0	366	-1224	12.57	12.57	6.28	6.28	2	0.08	0.01	0.03	0.00	0.00	24.0
9	50	-6402	302	389	0	558	-1261	12.57	12.57	6.28	6.28	2	0.09	0.01	0.03	0.00	0.00	24.0
10	50	-5994	642	337	0	475	-2197	12.57	12.57	6.28	6.28	2	0.13	0.01	0.07	0.00	0.00	24.0

11	50	-6098	645	370	0	533	-2208	12.57	12.57	6.28	6.28	2	0.13	0.01	0.07	0.00	0.00	24.0
12	50	-6273	106	307	0	410	-721	12.57	12.57	6.28	6.28	2	0.05	0.01	0.03	0.00	0.00	24.0
13	50	-6378	110	340	0	468	-732	12.57	12.57	6.28	6.28	2	0.06	0.01	0.03	0.00	0.00	24.0
14	50	-5969	450	288	0	385	-1667	12.57	12.57	6.28	6.28	2	0.10	0.01	0.05	0.00	0.00	24.0
15	50	-6318	462	398	0	577	-1704	12.57	12.57	6.28	6.28	2	0.11	0.01	0.05	0.00	0.00	24.0
16	50	-6053	289	279	0	366	-1224	12.57	12.57	6.28	6.28	2	0.08	0.01	0.03	0.00	0.00	24.0
17	50	-6402	302	389	0	558	-1261	12.57	12.57	6.28	6.28	2	0.09	0.01	0.03	0.00	0.00	24.0
18	50	-7499	1768	502	0	760	-5377	12.57	12.57	6.28	6.28	3	0.21	0.03	0.18	0.00	0.00	24.0
19	50	-8512	-2	427	0	577	-514	12.57	12.57	6.28	6.28	3	0.04	0.01	0.04	0.00	0.00	24.0
20	50	-8034	830	419	0	554	-2802	12.57	12.57	6.28	6.28	3	0.11	0.01	0.08	0.00	0.00	24.0
37	50	-7125	2229	516	0	800	-6657	12.57	12.57	6.28	6.28	3	0.25	0.04	0.23	0.00	0.00	24.0
38	50	-8813	-721	390	0	495	1448	12.57	12.57	6.28	6.28	3	0.06	0.01	0.07	0.00	0.00	24.0
39	50	-8016	665	378	0	456	-2366	12.57	12.57	6.28	6.28	3	0.09	0.01	0.07	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 105 NI 1445 NF 168 SEZ. Rp B= 0.400 H= 0.600 (pilastro)
PIL. NUM. 11A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-8042	488	440	0	613	-1903	12.57	12.57	6.28	6.28	3	0.08	0.01	0.05	0.00	0.00	24.0
2	0	-5994	642	337	0	475	-2197	12.57	12.57	6.28	6.28	2	0.13	0.01	0.07	0.00	0.00	24.0
3	0	-6098	645	370	0	533	-2208	12.57	12.57	6.28	6.28	2	0.13	0.01	0.07	0.00	0.00	24.0
4	0	-6273	106	307	0	410	-721	12.57	12.57	6.28	6.28	2	0.05	0.01	0.03	0.00	0.00	24.0
5	0	-6378	110	340	0	468	-732	12.57	12.57	6.28	6.28	2	0.06	0.01	0.03	0.00	0.00	24.0
6	0	-5969	450	288	0	385	-1667	12.57	12.57	6.28	6.28	2	0.10	0.01	0.05	0.00	0.00	24.0
7	0	-6318	462	398	0	577	-1704	12.57	12.57	6.28	6.28	2	0.11	0.01	0.05	0.00	0.00	24.0
8	0	-6053	289	279	0	366	-1224	12.57	12.57	6.28	6.28	2	0.08	0.01	0.03	0.00	0.00	24.0
9	0	-6402	302	389	0	558	-1261	12.57	12.57	6.28	6.28	2	0.09	0.01	0.03	0.00	0.00	24.0
10	0	-5994	642	337	0	475	-2197	12.57	12.57	6.28	6.28	2	0.13	0.01	0.07	0.00	0.00	24.0
11	0	-6098	645	370	0	533	-2208	12.57	12.57	6.28	6.28	2	0.13	0.01	0.07	0.00	0.00	24.0
12	0	-6273	106	307	0	410	-721	12.57	12.57	6.28	6.28	2	0.05	0.01	0.03	0.00	0.00	24.0
13	0	-6378	110	340	0	468	-732	12.57	12.57	6.28	6.28	2	0.06	0.01	0.03	0.00	0.00	24.0
14	0	-5969	450	288	0	385	-1667	12.57	12.57	6.28	6.28	2	0.10	0.01	0.05	0.00	0.00	24.0
15	0	-6318	462	398	0	577	-1704	12.57	12.57	6.28	6.28	2	0.11	0.01	0.05	0.00	0.00	24.0
16	0	-6053	289	279	0	366	-1224	12.57	12.57	6.28	6.28	2	0.08	0.01	0.03	0.00	0.00	24.0
17	0	-6402	302	389	0	558	-1261	12.57	12.57	6.28	6.28	2	0.09	0.01	0.03	0.00	0.00	24.0
18	0	-7499	1768	502	0	760	-5377	12.57	12.57	6.28	6.28	3	0.21	0.03	0.18	0.00	0.00	24.0
19	0	-8512	-2	427	0	577	-514	12.57	12.57	6.28	6.28	3	0.04	0.01	0.04	0.00	0.00	24.0
20	0	-8034	830	419	0	554	-2802	12.57	12.57	6.28	6.28	3	0.11	0.01	0.08	0.00	0.00	24.0
37	0	-7125	2229	516	0	800	-6657	12.57	12.57	6.28	6.28	3	0.25	0.04	0.23	0.00	0.00	24.0
38	0	-8813	-721	390	0	495	1448	12.57	12.57	6.28	6.28	3	0.06	0.01	0.07	0.00	0.00	24.0
39	0	-8016	665	378	0	456	-2366	12.57	12.57	6.28	6.28	3	0.09	0.01	0.07	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-7944	488	440	0	558	-1842	12.57	12.57	6.28	6.28	3	0.08	0.01	0.05	0.00	0.00	24.0
2	12	-5919	642	337	0	433	-2117	12.57	12.57	6.28	6.28	2	0.13	0.01	0.07	0.00	0.00	24.0
3	12	-6023	645	370	0	487	-2127	12.57	12.57	6.28	6.28	2	0.13	0.01	0.07	0.00	0.00	24.0
4	12	-6198	106	307	0	372	-707	12.57	12.57	6.28	6.28	2	0.05	0.01	0.03	0.00	0.00	24.0
5	12	-6303	110	340	0	425	-718	12.57	12.57	6.28	6.28	2	0.05	0.01	0.03	0.00	0.00	24.0
6	12	-5894	450	288	0	349	-1611	12.57	12.57	6.28	6.28	2	0.10	0.01	0.05	0.00	0.00	24.0
7	12	-6243	462	398	0	527	-1646	12.57	12.57	6.28	6.28	2	0.10	0.01	0.05	0.00	0.00	24.0
8	12	-5978	289	279	0	331	-1188	12.57	12.57	6.28	6.28	2	0.07	0.01	0.03	0.00	0.00	24.0
9	12	-6327	302	389	0	509	-1223	12.57	12.57	6.28	6.28	2	0.08	0.01	0.03	0.00	0.00	24.0
10	12	-5919	642	337	0	433	-2117	12.57	12.57	6.28	6.28	2	0.13	0.01	0.07	0.00	0.00	24.0
11	12	-6023	645	370	0	487	-2127	12.57	12.57	6.28	6.28	2	0.13	0.01	0.07	0.00	0.00	24.0
12	12	-6198	106	307	0	372	-707	12.57	12.57	6.28	6.28	2	0.05	0.01	0.03	0.00	0.00	24.0
13	12	-6303	110	340	0	425	-718	12.57	12.57	6.28	6.28	2	0.05	0.01	0.03	0.00	0.00	24.0
14	12	-5894	450	288	0	349	-1611	12.57	12.57	6.28	6.28	2	0.10	0.01	0.05	0.00	0.00	24.0
15	12	-6243	462	398	0	527	-1646	12.57	12.57	6.28	6.28	2	0.10	0.01	0.05	0.00	0.00	24.0
16	12	-5978	289	279	0	331	-1188	12.57	12.57	6.28	6.28	2	0.07	0.01	0.03	0.00	0.00	24.0
17	12	-6327	302	389	0	509	-1223	12.57	12.57	6.28	6.28	2	0.08	0.01	0.03	0.00	0.00	24.0
18	12	-7402	1768	502	0	697	-5156	12.57	12.57	6.28	6.28	3	0.20	0.03	0.18	0.00	0.00	24.0
19	12	-8414	-2	427	0	523	-514	12.57	12.57	6.28	6.28	3	0.03	0.01	0.04	0.00	0.00	24.0
20	12	-7936	830	419	0	501	-2698	12.57	12.57	6.28	6.28	3	0.11	0.01	0.08	0.00	0.00	24.0
37	12	-7028	2229	516	0	735	-6378	12.57	12.57	6.28	6.28	3	0.24	0.04	0.23	0.00	0.00	24.0
38	12	-8716	-721	390	0	446	1358	12.57	12.57	6.28	6.28	3	0.06	0.01	0.07	0.00	0.00	24.0
39	12	-7918	665	378	0	409	-2283	12.57	12.57	6.28	6.28	3	0.09	0.01	0.07	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-7847	488	440	0	503	-1781	12.57	12.57	6.28	6.28	3	0.07	0.01	0.05	0.00	0.00	24.0
2	25	-5844	642	337	0	391	-2037	12.57	12.57	6.28	6.28	2	0.12	0.01	0.07	0.00	0.00	24.0
3	25	-5948	645	370	0	440	-2046	12.57	12.57	6.28	6.28	2	0.12	0.01	0.07	0.00	0.00	24.0
4	25	-6123	106	307	0	333	-694	12.57	12.57	6.28	6.28	2	0.05	0.01	0.03	0.00	0.00	24.0
5	25	-6228	110	340	0	383	-704	12.57	12.57	6.28	6.28	2	0.05	0.01	0.03	0.00	0.00	24.0
6	25	-5819	450	288	0	313	-1555	12.57	12.57	6.28	6.28	2	0.09	0.01	0.05	0.00	0.00	24.0
7	25	-6168	462	398	0	478	-1588	12.57	12.57	6.28	6.28	2	0.10	0.01	0.05	0.00	0.00	24.0
8	25	-5903	289	279	0	296	-1152	12.57	12.57	6.28	6.28	2	0.07	0.01	0.03	0.00	0.00	24.0
9	25	-6252	302	389	0	460	-1186	12.57	12.57	6.28	6.28	2	0.08	0.01	0.03	0.00	0.00	24.0
10	25	-5844	642	337	0	391	-2037	12.57	12.57	6.28	6.28	2	0.12	0.01	0.07	0.00	0.00	24.0
11	25	-5948	645	370	0	440	-2046	12.57	12.57	6.28	6.28	2	0.12	0.01	0.07	0.00	0.00	24.0
12	25	-6123	106	307	0	333	-694	12.57	12.57	6.28	6.28	2	0.05	0.01	0.03	0.00	0.00	24.0
13	25	-6228	110	340	0	383	-704	12.57	12.57	6.28	6.28	2	0.05	0.01	0.03	0.00	0.00	24.0
14	25	-5819	450	288	0	313	-1555	12.57	12.57	6.28	6.28	2	0.09	0.01	0.05	0.00	0.00	24.0
15	25	-6168	462	398	0	478	-1588	12.57	12.57	6.28	6.28	2	0.10	0.01	0.05	0.00	0.00	24.0
16	25	-5903	289	279	0	296	-1152	12.57	12.57	6.28	6.28	2	0.07	0.01	0.03	0.00	0.00	24.0
17	25	-6252	302	389	0	460	-1186	12.57	12.57	6.28	6.28	2	0.08	0.01	0.03	0.00	0.00	24.0
18	25	-7304	1768	502	0	634	-4935	12.57	12.57	6.28	6.28	3	0.19	0.03	0.18	0.00	0.00	24.0
19	25	-8317	-2	427	0	470	-514	12.57	12.57	6.28	6.28	3	0.03	0.01	0.04	0.00	0.00	24.0
20	25	-7839	830	419	0	449	-2595	12.57	12.57	6.28	6.28	3	0.10	0.01	0.09	0.00	0.00	24.0
37	25	-6930	2229	516	0	671	-6100	12.57	12.57	6.28	6.28	3	0.23	0.04	0.23	0.00	0.00	24.0
38	25	-8618	-721	390	0	397	1268	12.57	12.57	6.28	6.28	3	0.05	0.01	0.07	0.00	0.00	24.0
39	25	-7821	665	378	0	362	-2200	12.57	12.57	6.28	6.28	3	0.09	0.01	0.07	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-7750	488	440	0	448	-1720	12.57	12.57	6.28	6.28	3	0.07	0.01	0.05	0.00	0.00	24.0
2	38	-5769	642	337	0	349	-1956	12.57	12.57	6.28	6.28	2	0.12	0.01	0.07	0.00	0.00	24.0
3	38	-5873	645	370	0	394	-1966	12.57	12.57	6.28	6.28	2	0.12	0.01	0.07	0.00	0.00	24.0
4	38	-6048	106	307	0	295	-681	12.57	12.57	6.28	6.28	2	0.05	0.01	0.03	0.00	0.00	24.0
5	38	-6153	110	340	0	340	-690	12.57	12.57	6.28	6.28	2	0.05	0.01	0.03	0.00	0.00	24.0
6	38	-5744	450	288	0	277	-1498	12.57	12.57	6.28	6.28	2	0.09	0.01	0.05	0.00	0.00	24.0

7	38	-6093	462	398	0	428	-1531	12.57	12.57	6.28	6.28	2	0.10	0.01	0.05	0.00	0.00	24.0
8	38	-5828	289	279	0	261	-1116	12.57	12.57	6.28	6.28	2	0.07	0.01	0.03	0.00	0.00	24.0
9	38	-6177	302	389	0	412	-1148	12.57	12.57	6.28	6.28	2	0.07	0.01	0.03	0.00	0.00	24.0
10	38	-5769	642	337	0	349	-1956	12.57	12.57	6.28	6.28	2	0.12	0.01	0.07	0.00	0.00	24.0
11	38	-5873	645	370	0	394	-1966	12.57	12.57	6.28	6.28	2	0.12	0.01	0.07	0.00	0.00	24.0
12	38	-6048	106	307	0	295	-681	12.57	12.57	6.28	6.28	2	0.05	0.01	0.03	0.00	0.00	24.0
13	38	-6153	110	340	0	340	-690	12.57	12.57	6.28	6.28	2	0.05	0.01	0.03	0.00	0.00	24.0
14	38	-5744	450	288	0	277	-1498	12.57	12.57	6.28	6.28	2	0.09	0.01	0.05	0.00	0.00	24.0
15	38	-6093	462	398	0	428	-1531	12.57	12.57	6.28	6.28	2	0.10	0.01	0.05	0.00	0.00	24.0
16	38	-5828	289	279	0	261	-1116	12.57	12.57	6.28	6.28	2	0.07	0.01	0.03	0.00	0.00	24.0
17	38	-6177	302	389	0	412	-1148	12.57	12.57	6.28	6.28	2	0.07	0.01	0.03	0.00	0.00	24.0
18	38	-7206	1768	502	0	571	-4714	12.57	12.57	6.28	6.28	3	0.18	0.03	0.18	0.00	0.00	24.0
19	38	-8220	-2	427	0	417	-514	12.57	12.57	6.28	6.28	3	0.03	0.01	0.04	0.00	0.00	24.0
20	38	-7742	830	419	0	396	-2491	12.57	12.57	6.28	6.28	3	0.10	0.01	0.09	0.00	0.00	24.0
37	38	-6832	2229	516	0	606	-5821	12.57	12.57	6.28	6.28	3	0.22	0.04	0.23	0.00	0.00	24.0
38	38	-8520	-721	390	0	349	1178	12.57	12.57	6.28	6.28	3	0.05	0.01	0.07	0.00	0.00	24.0
39	38	-7724	665	378	0	315	-2117	12.57	12.57	6.28	6.28	3	0.08	0.01	0.07	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-7652	488	440	0	393	-1659	12.57	12.57	6.28	6.28	3	0.07	0.01	0.05	0.00	0.00	24.0
2	50	-5694	642	337	0	307	-1876	12.57	12.57	6.28	6.28	2	0.11	0.01	0.07	0.00	0.00	24.0
3	50	-5798	645	370	0	348	-1885	12.57	12.57	6.28	6.28	2	0.11	0.01	0.07	0.00	0.00	24.0
4	50	-5973	106	307	0	256	-668	12.57	12.57	6.28	6.28	2	0.04	0.01	0.03	0.00	0.00	24.0
5	50	-6078	110	340	0	298	-677	12.57	12.57	6.28	6.28	2	0.05	0.01	0.03	0.00	0.00	24.0
6	50	-5669	450	288	0	241	-1442	12.57	12.57	6.28	6.28	2	0.08	0.01	0.05	0.00	0.00	24.0
7	50	-6018	462	398	0	378	-1473	12.57	12.57	6.28	6.28	2	0.09	0.01	0.05	0.00	0.00	24.0
8	50	-5753	289	279	0	226	-1080	12.57	12.57	6.28	6.28	2	0.06	0.01	0.03	0.00	0.00	24.0
9	50	-6102	302	389	0	363	-1110	12.57	12.57	6.28	6.28	2	0.07	0.01	0.03	0.00	0.00	24.0
10	50	-5694	642	337	0	307	-1876	12.57	12.57	6.28	6.28	2	0.11	0.01	0.07	0.00	0.00	24.0
11	50	-5798	645	370	0	348	-1885	12.57	12.57	6.28	6.28	2	0.11	0.01	0.07	0.00	0.00	24.0
12	50	-5973	106	307	0	256	-668	12.57	12.57	6.28	6.28	2	0.04	0.01	0.03	0.00	0.00	24.0
13	50	-6078	110	340	0	298	-677	12.57	12.57	6.28	6.28	2	0.05	0.01	0.03	0.00	0.00	24.0
14	50	-5669	450	288	0	241	-1442	12.57	12.57	6.28	6.28	2	0.08	0.01	0.05	0.00	0.00	24.0
15	50	-6018	462	398	0	378	-1473	12.57	12.57	6.28	6.28	2	0.09	0.01	0.05	0.00	0.00	24.0
16	50	-5753	289	279	0	226	-1080	12.57	12.57	6.28	6.28	2	0.06	0.01	0.03	0.00	0.00	24.0
17	50	-6102	302	389	0	363	-1110	12.57	12.57	6.28	6.28	2	0.07	0.01	0.03	0.00	0.00	24.0
18	50	-7109	1768	502	0	509	-4493	12.57	12.57	6.28	6.28	3	0.17	0.03	0.18	0.00	0.00	24.0
19	50	-8122	-2	427	0	363	-514	12.57	12.57	6.28	6.28	3	0.03	0.01	0.04	0.00	0.00	24.0
20	50	-7644	830	419	0	344	-2387	12.57	12.57	6.28	6.28	3	0.09	0.01	0.09	0.00	0.00	24.0
37	50	-6735	2229	516	0	542	-5542	12.57	12.57	6.28	6.28	3	0.21	0.04	0.23	0.00	0.00	24.0
38	50	-8423	-721	390	0	300	1088	12.57	12.57	6.28	6.28	3	0.04	0.01	0.07	0.00	0.00	24.0
39	50	-7626	665	378	0	267	-2034	12.57	12.57	6.28	6.28	3	0.08	0.01	0.07	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 106 NI 1032 NF 1045 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 10
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-16650	1140	1324	0	1383	-876	6.28	6.28	12.57	12.57	3	0.07	0.02	0.12	0.00	0.00	24.0
2	0	-13510	571	1191	0	1162	-720	6.28	6.28	12.57	12.57	2	0.08	0.02	0.11	0.00	0.00	24.0
3	0	-13500	596	1152	0	1147	-730	6.28	6.28	12.57	12.57	2	0.08	0.02	0.11	0.00	0.00	24.0
4	0	-12110	1157	885	0	981	-617	6.28	6.28	12.57	12.57	2	0.07	0.02	0.10	0.00	0.00	24.0
5	0	-12110	1182	846	0	966	-627	6.28	6.28	12.57	12.57	2	0.07	0.02	0.10	0.00	0.00	24.0
6	0	-13020	748	1129	0	1116	-672	6.28	6.28	12.57	12.57	2	0.08	0.02	0.11	0.00	0.00	24.0
7	0	-13010	830	1000	0	1066	-706	6.28	6.28	12.57	12.57	2	0.08	0.02	0.10	0.00	0.00	24.0
8	0	-12610	923	1037	0	1062	-642	6.28	6.28	12.57	12.57	2	0.08	0.02	0.10	0.00	0.00	24.0
9	0	-12590	1006	908	0	1012	-675	6.28	6.28	12.57	12.57	2	0.07	0.02	0.09	0.00	0.00	24.0
10	0	-13510	571	1191	0	1162	-720	6.28	6.28	12.57	12.57	2	0.08	0.02	0.11	0.00	0.00	24.0
11	0	-13500	596	1152	0	1147	-730	6.28	6.28	12.57	12.57	2	0.08	0.02	0.11	0.00	0.00	24.0
12	0	-12110	1157	885	0	981	-617	6.28	6.28	12.57	12.57	2	0.07	0.02	0.10	0.00	0.00	24.0
13	0	-12110	1182	846	0	966	-627	6.28	6.28	12.57	12.57	2	0.07	0.02	0.10	0.00	0.00	24.0
14	0	-13020	748	1129	0	1116	-672	6.28	6.28	12.57	12.57	2	0.08	0.02	0.11	0.00	0.00	24.0
15	0	-13010	830	1000	0	1066	-706	6.28	6.28	12.57	12.57	2	0.08	0.02	0.10	0.00	0.00	24.0
16	0	-12610	923	1037	0	1062	-642	6.28	6.28	12.57	12.57	2	0.08	0.02	0.10	0.00	0.00	24.0
17	0	-12590	1006	908	0	1012	-675	6.28	6.28	12.57	12.57	2	0.07	0.02	0.09	0.00	0.00	24.0
18	0	-20330	-56	2144	0	2002	-949	6.28	6.28	12.57	12.57	3	0.08	0.04	0.19	0.00	0.00	24.0
19	0	-15400	1891	942	0	1279	-666	6.28	6.28	12.57	12.57	3	0.06	0.03	0.15	0.00	0.00	24.0
20	0	-17420	954	1678	0	1488	-818	6.28	6.28	12.57	12.57	3	0.07	0.03	0.15	0.00	0.00	24.0
37	0	-21570	-632	2485	0	2163	-1067	6.28	6.28	12.57	12.57	3	0.09	0.04	0.21	0.00	0.00	24.0
38	0	-13360	2613	482	0	959	-594	6.28	6.28	12.57	12.57	3	0.05	0.05	0.21	0.00	0.00	24.0
39	0	-16720	1053	1708	0	1306	-847	6.28	6.28	12.57	12.57	3	0.06	0.03	0.16	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-16552	1140	1324	0	1218	-733	6.28	6.28	12.57	12.57	3	0.06	0.02	0.12	0.00	0.00	24.0
2	12	-13435	571	1191	0	1013	-649	6.28	6.28	12.57	12.57	2	0.07	0.02	0.11	0.00	0.00	24.0
3	12	-13425	596	1152	0	1003	-656	6.28	6.28	12.57	12.57	2	0.07	0.02	0.11	0.00	0.00	24.0
4	12	-12035	1157	885	0	870	-473	6.28	6.28	12.57	12.57	2	0.06	0.02	0.10	0.00	0.00	24.0
5	12	-12035	1182	846	0	860	-479	6.28	6.28	12.57	12.57	2	0.06	0.02	0.10	0.00	0.00	24.0
6	12	-12945	748	1129	0	975	-579	6.28	6.28	12.57	12.57	2	0.07	0.02	0.11	0.00	0.00	24.0
7	12	-12935	830	1000	0	941	-602	6.28	6.28	12.57	12.57	2	0.07	0.02	0.10	0.00	0.00	24.0
8	12	-12535	923	1037	0	932	-526	6.28	6.28	12.57	12.57	2	0.06	0.02	0.10	0.00	0.00	24.0
9	12	-12515	1006	908	0	898	-549	6.28	6.28	12.57	12.57	2	0.06	0.02	0.09	0.00	0.00	24.0
10	12	-13435	571	1191	0	1013	-649	6.28	6.28	12.57	12.57	2	0.07	0.02	0.11	0.00	0.00	24.0
11	12	-13425	596	1152	0	1003	-656	6.28	6.28	12.57	12.57	2	0.07	0.02	0.11	0.00	0.00	24.0
12	12	-12035	1157	885	0	870	-473	6.28	6.28	12.57	12.57	2	0.06	0.02	0.10	0.00	0.00	24.0
13	12	-12035	1182	846	0	860	-479	6.28	6.28	12.57	12.57	2	0.06	0.02	0.10	0.00	0.00	24.0
14	12	-12945	748	1129	0	975	-579	6.28	6.28	12.57	12.57	2	0.07	0.02	0.11	0.00	0.00	24.0
15	12	-12935	830	1000	0	941	-602	6.28	6.28	12.57	12.57	2	0.07	0.02	0.10	0.00	0.00	24.0
16	12	-12535	923	1037	0	932	-526	6.28	6.28	12.57	12.57	2	0.06	0.02	0.10	0.00	0.00	24.0
17	12	-12515	1006	908	0	898	-549	6.28	6.28	12.57	12.57	2	0.06	0.02	0.09	0.00	0.00	24.0
18	12	-20232	-56	2144	0	1734	-956	6.28	6.28	12.57	12.57	3	0.08	0.04	0.19	0.00	0.00	24.0
19	12	-15302	1891	942	0	1161	-429	6.28	6.28	12.57	12.57	3	0.05	0.03	0.15	0.00	0.00	24.0
20	12	-17322	954	1678	0	1278	-698	6.28	6.28	12.57	12.57	3	0.06	0.03	0.15	0.00	0.00	24.0
37	12	-21472	-632	2485	0	1852	-1146	6.28	6.28	12.57	12.57	3	0.09	0.04	0.21	0.00	0.00	24.0
38	12	-13262	2613	482	0	898	-267	6.28	6.28	12.57	12.57	3	0.04	0.05	0.21	0.00	0.00	24.0
39	12	-16622	1053	1708	0	1093	-716	6.28	6.28	12.57	12.57	3	0.05	0.03	0.16	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-16455	1140	1324	0	1052	-591	6.28	6.28	12.57	12.57	3	0.05	0.02	0.12	0.00	0.00	24.0
2	25	-13360	571	1191	0	864	-577	6.28	6.28	12.57	12.57	2	0.06	0.02	0.11	0.00	0.00	24.0

3	25	-13350	596	1152	0	859	-581	6.28	6.28	12.57	12.57	2	0.06	0.02	0.11	0.00	0.00	24.0
4	25	-11960	1157	885	0	760	-328	6.28	6.28	12.57	12.57	2	0.05	0.02	0.10	0.00	0.00	24.0
5	25	-11960	1182	846	0	754	-332	6.28	6.28	12.57	12.57	2	0.05	0.02	0.10	0.00	0.00	24.0
6	25	-12870	748	1129	0	834	-486	6.28	6.28	12.57	12.57	2	0.06	0.02	0.11	0.00	0.00	24.0
7	25	-12860	830	1000	0	816	-498	6.28	6.28	12.57	12.57	2	0.06	0.02	0.10	0.00	0.00	24.0
8	25	-12460	923	1037	0	803	-411	6.28	6.28	12.57	12.57	2	0.05	0.02	0.10	0.00	0.00	24.0
9	25	-12440	1006	908	0	785	-423	6.28	6.28	12.57	12.57	2	0.05	0.02	0.09	0.00	0.00	24.0
10	25	-13360	571	1191	0	864	-577	6.28	6.28	12.57	12.57	2	0.06	0.02	0.11	0.00	0.00	24.0
11	25	-13350	596	1152	0	859	-581	6.28	6.28	12.57	12.57	2	0.06	0.02	0.11	0.00	0.00	24.0
12	25	-11960	1157	885	0	760	-328	6.28	6.28	12.57	12.57	2	0.05	0.02	0.10	0.00	0.00	24.0
13	25	-11960	1182	846	0	754	-332	6.28	6.28	12.57	12.57	2	0.05	0.02	0.10	0.00	0.00	24.0
14	25	-12870	748	1129	0	834	-486	6.28	6.28	12.57	12.57	2	0.06	0.02	0.11	0.00	0.00	24.0
15	25	-12860	830	1000	0	816	-498	6.28	6.28	12.57	12.57	2	0.06	0.02	0.10	0.00	0.00	24.0
16	25	-12460	923	1037	0	803	-411	6.28	6.28	12.57	12.57	2	0.05	0.02	0.10	0.00	0.00	24.0
17	25	-12440	1006	908	0	785	-423	6.28	6.28	12.57	12.57	2	0.05	0.02	0.09	0.00	0.00	24.0
18	25	-20135	-56	2144	0	1466	-963	6.28	6.28	12.57	12.57	3	0.07	0.04	0.19	0.00	0.00	24.0
19	25	-15205	1891	942	0	1044	-193	6.28	6.28	12.57	12.57	3	0.04	0.03	0.15	0.00	0.00	24.0
20	25	-17225	954	1678	0	1069	-579	6.28	6.28	12.57	12.57	3	0.05	0.03	0.15	0.00	0.00	24.0
37	25	-21375	-632	2485	0	1542	-1225	6.28	6.28	12.57	12.57	3	0.08	0.04	0.21	0.00	0.00	24.0
38	25	-13165	2613	482	0	838	59	6.28	6.28	12.57	12.57	3	0.03	0.05	0.21	0.00	0.00	24.0
39	25	-16525	1053	1708	0	879	-584	6.28	6.28	12.57	12.57	3	0.04	0.03	0.16	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-16358	1140	1324	0	887	-448	6.28	6.28	12.57	12.57	3	0.04	0.02	0.12	0.00	0.00	24.0
2	38	-13285	571	1191	0	716	-506	6.28	6.28	12.57	12.57	2	0.05	0.02	0.11	0.00	0.00	24.0
3	38	-13275	596	1152	0	715	-507	6.28	6.28	12.57	12.57	2	0.05	0.02	0.11	0.00	0.00	24.0
4	38	-11885	1157	885	0	649	-183	6.28	6.28	12.57	12.57	2	0.04	0.02	0.10	0.00	0.00	24.0
5	38	-11885	1182	846	0	649	-184	6.28	6.28	12.57	12.57	2	0.04	0.02	0.10	0.00	0.00	24.0
6	38	-12795	748	1129	0	693	-392	6.28	6.28	12.57	12.57	2	0.05	0.02	0.11	0.00	0.00	24.0
7	38	-12785	830	1000	0	691	-394	6.28	6.28	12.57	12.57	2	0.05	0.02	0.10	0.00	0.00	24.0
8	38	-12385	923	1037	0	673	-295	6.28	6.28	12.57	12.57	2	0.04	0.02	0.10	0.00	0.00	24.0
9	38	-12365	1006	908	0	671	-298	6.28	6.28	12.57	12.57	2	0.04	0.02	0.09	0.00	0.00	24.0
10	38	-13285	571	1191	0	716	-506	6.28	6.28	12.57	12.57	2	0.05	0.02	0.11	0.00	0.00	24.0
11	38	-13275	596	1152	0	715	-507	6.28	6.28	12.57	12.57	2	0.05	0.02	0.11	0.00	0.00	24.0
12	38	-11885	1157	885	0	649	-183	6.28	6.28	12.57	12.57	2	0.04	0.02	0.10	0.00	0.00	24.0
13	38	-11885	1182	846	0	649	-184	6.28	6.28	12.57	12.57	2	0.04	0.02	0.10	0.00	0.00	24.0
14	38	-12795	748	1129	0	693	-392	6.28	6.28	12.57	12.57	2	0.05	0.02	0.11	0.00	0.00	24.0
15	38	-12785	830	1000	0	691	-394	6.28	6.28	12.57	12.57	2	0.05	0.02	0.10	0.00	0.00	24.0
16	38	-12385	923	1037	0	673	-295	6.28	6.28	12.57	12.57	2	0.04	0.02	0.10	0.00	0.00	24.0
17	38	-12365	1006	908	0	671	-298	6.28	6.28	12.57	12.57	2	0.04	0.02	0.09	0.00	0.00	24.0
18	38	-20038	-56	2144	0	1198	-970	6.28	6.28	12.57	12.57	3	0.06	0.04	0.19	0.00	0.00	24.0
19	38	-15108	1891	942	0	926	43	6.28	6.28	12.57	12.57	3	0.03	0.03	0.15	0.00	0.00	24.0
20	38	-17128	954	1678	0	859	-460	6.28	6.28	12.57	12.57	3	0.04	0.03	0.15	0.00	0.00	24.0
37	38	-21278	-632	2485	0	1231	-1304	6.28	6.28	12.57	12.57	3	0.08	0.04	0.21	0.00	0.00	24.0
38	38	-13068	2613	482	0	778	386	6.28	6.28	12.57	12.57	3	0.03	0.05	0.21	0.00	0.00	24.0
39	38	-16428	1053	1708	0	666	-452	6.28	6.28	12.57	12.57	3	0.03	0.03	0.16	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-16260	1140	1324	0	721	-306	6.28	6.28	12.57	12.57	3	0.03	0.02	0.12	0.00	0.00	24.0
2	50	-13210	571	1191	0	567	-435	6.28	6.28	12.57	12.57	2	0.04	0.02	0.11	0.00	0.00	24.0
3	50	-13200	596	1152	0	571	-432	6.28	6.28	12.57	12.57	2	0.04	0.02	0.11	0.00	0.00	24.0
4	50	-11810	1157	885	0	538	-38	6.28	6.28	12.57	12.57	2	0.03	0.02	0.10	0.00	0.00	24.0
5	50	-11810	1182	846	0	543	-36	6.28	6.28	12.57	12.57	2	0.03	0.02	0.10	0.00	0.00	24.0
6	50	-12720	748	1129	0	552	-299	6.28	6.28	12.57	12.57	2	0.04	0.02	0.11	0.00	0.00	24.0
7	50	-12710	830	1000	0	566	-291	6.28	6.28	12.57	12.57	2	0.04	0.02	0.10	0.00	0.00	24.0
8	50	-12310	923	1037	0	543	-180	6.28	6.28	12.57	12.57	2	0.03	0.02	0.10	0.00	0.00	24.0
9	50	-12290	1006	908	0	558	-172	6.28	6.28	12.57	12.57	2	0.03	0.02	0.09	0.00	0.00	24.0
10	50	-13210	571	1191	0	567	-435	6.28	6.28	12.57	12.57	2	0.04	0.02	0.11	0.00	0.00	24.0
11	50	-13200	596	1152	0	571	-432	6.28	6.28	12.57	12.57	2	0.04	0.02	0.11	0.00	0.00	24.0
12	50	-11810	1157	885	0	538	-38	6.28	6.28	12.57	12.57	2	0.03	0.02	0.10	0.00	0.00	24.0
13	50	-11810	1182	846	0	543	-36	6.28	6.28	12.57	12.57	2	0.03	0.02	0.10	0.00	0.00	24.0
14	50	-12720	748	1129	0	552	-299	6.28	6.28	12.57	12.57	2	0.04	0.02	0.11	0.00	0.00	24.0
15	50	-12710	830	1000	0	566	-291	6.28	6.28	12.57	12.57	2	0.04	0.02	0.10	0.00	0.00	24.0
16	50	-12310	923	1037	0	543	-180	6.28	6.28	12.57	12.57	2	0.03	0.02	0.10	0.00	0.00	24.0
17	50	-12290	1006	908	0	558	-172	6.28	6.28	12.57	12.57	2	0.03	0.02	0.09	0.00	0.00	24.0
18	50	-19940	-56	2144	0	930	-977	6.28	6.28	12.57	12.57	3	0.06	0.04	0.19	0.00	0.00	24.0
19	50	-15010	1891	942	0	808	280	6.28	6.28	12.57	12.57	3	0.03	0.03	0.15	0.00	0.00	24.0
20	50	-17030	954	1678	0	649	-340	6.28	6.28	12.57	12.57	3	0.03	0.03	0.15	0.00	0.00	24.0
37	50	-21180	-632	2485	0	921	-1383	6.28	6.28	12.57	12.57	3	0.08	0.04	0.21	0.00	0.00	24.0
38	50	-12970	2613	482	0	718	712	6.28	6.28	12.57	12.57	3	0.04	0.05	0.21	0.00	0.00	24.0
39	50	-16330	1053	1708	0	452	-321	6.28	6.28	12.57	12.57	3	0.02	0.03	0.16	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 107 NI 1045 NF 299 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 10A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-18330	443	680	0	594	-236	6.28	6.28	12.57	12.57	3	0.02	0.01	0.06	0.00	0.00	24.0
2	0	-14550	-559	608	0	461	-411	6.28	6.28	12.57	12.57	2	0.04	0.01	0.06	0.00	0.00	24.0
3	0	-14540	-546	564	0	469	-407	6.28	6.28	12.57	12.57	2	0.04	0.01	0.05	0.00	0.00	24.0
4	0	-13660	1227	482	0	445	44	6.28	6.28	12.57	12.57	2	0.02	0.02	0.10	0.00	0.00	24.0
5	0	-13650	1240	438	0	454	48	6.28	6.28	12.57	12.57	2	0.02	0.02	0.10	0.00	0.00	24.0
6	0	-14250	51	616	0	446	-256	6.28	6.28	12.57	12.57	2	0.03	0.01	0.06	0.00	0.00	24.0
7	0	-14220	94	468	0	473	-244	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
8	0	-13980	587	578	0	441	-119	6.28	6.28	12.57	12.57	2	0.03	0.01	0.05	0.00	0.00	24.0
9	0	-13950	630	430	0	468	-107	6.28	6.28	12.57	12.57	2	0.03	0.01	0.05	0.00	0.00	24.0
10	0	-14550	-559	608	0	461	-411	6.28	6.28	12.57	12.57	2	0.04	0.01	0.06	0.00	0.00	24.0
11	0	-14540	-546	564	0	469	-407	6.28	6.28	12.57	12.57	2	0.04	0.01	0.05	0.00	0.00	24.0
12	0	-13660	1227	482	0	445	44	6.28	6.28	12.57	12.57	2	0.02	0.02	0.10	0.00	0.00	24.0
13	0	-13650	1240	438	0	454	48	6.28	6.28	12.57	12.57	2	0.02	0.02	0.10	0.00	0.00	24.0
14	0	-14250	51	616	0	446	-256	6.28	6.28	12.57	12.57	2	0.03	0.01	0.06	0.00	0.00	24.0
15	0	-14220	94	468	0	473	-244	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
16	0	-13980	587	578	0	441	-119	6.28	6.28	12.57	12.57	2	0.03	0.01	0.05	0.00	0.00	24.0
17	0	-13950	630	430	0	468	-107	6.28	6.28	12.57	12.57	2	0.03	0.01	0.05	0.00	0.00	24.0
18	0	-21460	-2436	907	0	751	-1023	6.28	6.28	12.57	12.57	3	0.06	0.04	0.20	0.00	0.00	24.0
19	0	-18040	3188	402	0	689	427	6.28	6.28	12.57	12.57	3	0.03	0.06	0.25	0.00	0.00	24.0
20	0	-19380	380	1004	0	484	-288	6.28	6.28	12.57	12.57	3	0.02	0.02	0.09	0.00	0.00	24.0
37	0	-22130	-4290	1090	0	728	-1486	6.28	6.28	12.57	12.57	3	0.08	0.08	0.35	0.00	0.00	24.0
38	0	-16430	5082	249	0	625	930	6.28	6.28	12.57	12.57	3	0.05	0.09	0.44	0.00	0.00	24.0
39	0	-18660	402	1252	0	283	-262	6.28	6.28	12.57	12.57	3	0.02	0.02	0.11	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-18232	443	680	0	509	-181	6.28	6.28 12.57 12.57		3	0.02	0.01	0.06	0.00	0.00	24.0
2	12	-14475	-559	608	0	385	-481	6.28	6.28 12.57 12.57		2	0.04	0.01	0.06	0.00	0.00	24.0
3	12	-14465	-546	564	0	398	-476	6.28	6.28 12.57 12.57		2	0.04	0.01	0.05	0.00	0.00	24.0
4	12	-13585	1227	482	0	385	197	6.28	6.28 12.57 12.57		2	0.03	0.02	0.10	0.00	0.00	24.0
5	12	-13575	1240	438	0	399	203	6.28	6.28 12.57 12.57		2	0.03	0.02	0.10	0.00	0.00	24.0
6	12	-14175	51	616	0	369	-249	6.28	6.28 12.57 12.57		2	0.03	0.01	0.06	0.00	0.00	24.0
7	12	-14145	94	468	0	415	-232	6.28	6.28 12.57 12.57		2	0.03	0.01	0.04	0.00	0.00	24.0
8	12	-13905	587	578	0	369	-46	6.28	6.28 12.57 12.57		2	0.02	0.01	0.05	0.00	0.00	24.0
9	12	-13875	630	430	0	415	-29	6.28	6.28 12.57 12.57		2	0.02	0.01	0.05	0.00	0.00	24.0
10	12	-14475	-559	608	0	385	-481	6.28	6.28 12.57 12.57		2	0.04	0.01	0.06	0.00	0.00	24.0
11	12	-14465	-546	564	0	398	-476	6.28	6.28 12.57 12.57		2	0.04	0.01	0.05	0.00	0.00	24.0
12	12	-13585	1227	482	0	385	197	6.28	6.28 12.57 12.57		2	0.03	0.02	0.10	0.00	0.00	24.0
13	12	-13575	1240	438	0	399	203	6.28	6.28 12.57 12.57		2	0.03	0.02	0.10	0.00	0.00	24.0
14	12	-14175	51	616	0	369	-249	6.28	6.28 12.57 12.57		2	0.03	0.01	0.06	0.00	0.00	24.0
15	12	-14145	94	468	0	415	-232	6.28	6.28 12.57 12.57		2	0.03	0.01	0.04	0.00	0.00	24.0
16	12	-13905	587	578	0	369	-46	6.28	6.28 12.57 12.57		2	0.02	0.01	0.05	0.00	0.00	24.0
17	12	-13875	630	430	0	415	-29	6.28	6.28 12.57 12.57		2	0.02	0.01	0.05	0.00	0.00	24.0
18	12	-21362	-2436	907	0	638	-1327	6.28	6.28 12.57 12.57		3	0.07	0.04	0.20	0.00	0.00	24.0
19	12	-17942	3188	402	0	639	825	6.28	6.28 12.57 12.57		3	0.05	0.06	0.27	0.00	0.00	24.0
20	12	-19282	380	1004	0	358	-240	6.28	6.28 12.57 12.57		3	0.02	0.02	0.09	0.00	0.00	24.0
37	12	-22032	-4290	1090	0	592	-2022	6.28	6.28 12.57 12.57		3	0.10	0.08	0.35	0.00	0.00	24.0
38	12	-16332	5082	249	0	594	1565	6.28	6.28 12.57 12.57		3	0.09	0.09	0.44	0.00	0.00	24.0
39	12	-18562	402	1252	0	126	-211	6.28	6.28 12.57 12.57		3	0.01	0.02	0.11	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-18135	443	680	0	424	-125	6.28	6.28 12.57 12.57		3	0.02	0.01	0.06	0.00	0.00	24.0
2	25	-14400	-559	608	0	308	-551	6.28	6.28 12.57 12.57		2	0.04	0.01	0.06	0.00	0.00	24.0
3	25	-14390	-546	564	0	328	-544	6.28	6.28 12.57 12.57		2	0.04	0.01	0.05	0.00	0.00	24.0
4	25	-13510	1227	482	0	325	351	6.28	6.28 12.57 12.57		2	0.03	0.02	0.11	0.00	0.00	24.0
5	25	-13500	1240	438	0	344	358	6.28	6.28 12.57 12.57		2	0.03	0.02	0.11	0.00	0.00	24.0
6	25	-14100	51	616	0	292	-243	6.28	6.28 12.57 12.57		2	0.02	0.01	0.06	0.00	0.00	24.0
7	25	-14070	94	468	0	356	-220	6.28	6.28 12.57 12.57		2	0.03	0.01	0.04	0.00	0.00	24.0
8	25	-13830	587	578	0	297	27	6.28	6.28 12.57 12.57		2	0.02	0.01	0.05	0.00	0.00	24.0
9	25	-13800	630	430	0	361	50	6.28	6.28 12.57 12.57		2	0.02	0.01	0.05	0.00	0.00	24.0
10	25	-14400	-559	608	0	308	-551	6.28	6.28 12.57 12.57		2	0.04	0.01	0.06	0.00	0.00	24.0
11	25	-14390	-546	564	0	328	-544	6.28	6.28 12.57 12.57		2	0.04	0.01	0.05	0.00	0.00	24.0
12	25	-13510	1227	482	0	325	351	6.28	6.28 12.57 12.57		2	0.03	0.02	0.11	0.00	0.00	24.0
13	25	-13500	1240	438	0	344	358	6.28	6.28 12.57 12.57		2	0.03	0.02	0.11	0.00	0.00	24.0
14	25	-14100	51	616	0	292	-243	6.28	6.28 12.57 12.57		2	0.02	0.01	0.06	0.00	0.00	24.0
15	25	-14070	94	468	0	356	-220	6.28	6.28 12.57 12.57		2	0.03	0.01	0.04	0.00	0.00	24.0
16	25	-13830	587	578	0	297	27	6.28	6.28 12.57 12.57		2	0.02	0.01	0.05	0.00	0.00	24.0
17	25	-13800	630	430	0	361	50	6.28	6.28 12.57 12.57		2	0.02	0.01	0.05	0.00	0.00	24.0
18	25	-21265	-2436	907	0	524	-1631	6.28	6.28 12.57 12.57		3	0.09	0.04	0.20	0.00	0.00	24.0
19	25	-17845	3188	402	0	588	1224	6.28	6.28 12.57 12.57		3	0.07	0.06	0.27	0.00	0.00	24.0
20	25	-19185	380	1004	0	233	-193	6.28	6.28 12.57 12.57		3	0.01	0.02	0.09	0.00	0.00	24.0
37	25	-21935	-4290	1090	0	456	-2559	6.28	6.28 12.57 12.57		3	0.13	0.08	0.35	0.00	0.00	24.0
38	25	-16235	5082	249	0	562	2200	6.28	6.28 12.57 12.57		3	0.12	0.09	0.44	0.00	0.00	24.0
39	25	-18465	402	1252	0	-30	-161	6.28	6.28 12.57 12.57		3	0.01	0.02	0.11	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-18038	443	680	0	339	-70	6.28	6.28 12.57 12.57		3	0.01	0.01	0.06	0.00	0.00	24.0
2	38	-14325	-559	608	0	232	-621	6.28	6.28 12.57 12.57		2	0.04	0.01	0.06	0.00	0.00	24.0
3	38	-14315	-546	564	0	257	-612	6.28	6.28 12.57 12.57		2	0.04	0.01	0.05	0.00	0.00	24.0
4	38	-13435	1227	482	0	265	504	6.28	6.28 12.57 12.57		2	0.04	0.02	0.11	0.00	0.00	24.0
5	38	-13425	1240	438	0	289	513	6.28	6.28 12.57 12.57		2	0.04	0.02	0.11	0.00	0.00	24.0
6	38	-14025	51	616	0	215	-237	6.28	6.28 12.57 12.57		2	0.02	0.01	0.06	0.00	0.00	24.0
7	38	-13995	94	468	0	298	-209	6.28	6.28 12.57 12.57		2	0.02	0.01	0.04	0.00	0.00	24.0
8	38	-13755	587	578	0	224	101	6.28	6.28 12.57 12.57		2	0.01	0.01	0.05	0.00	0.00	24.0
9	38	-13725	630	430	0	307	129	6.28	6.28 12.57 12.57		2	0.02	0.01	0.05	0.00	0.00	24.0
10	38	-14325	-559	608	0	232	-621	6.28	6.28 12.57 12.57		2	0.04	0.01	0.06	0.00	0.00	24.0
11	38	-14315	-546	564	0	257	-612	6.28	6.28 12.57 12.57		2	0.04	0.01	0.05	0.00	0.00	24.0
12	38	-13435	1227	482	0	265	504	6.28	6.28 12.57 12.57		2	0.04	0.02	0.11	0.00	0.00	24.0
13	38	-13425	1240	438	0	289	513	6.28	6.28 12.57 12.57		2	0.04	0.02	0.11	0.00	0.00	24.0
14	38	-14025	51	616	0	215	-237	6.28	6.28 12.57 12.57		2	0.02	0.01	0.06	0.00	0.00	24.0
15	38	-13995	94	468	0	298	-209	6.28	6.28 12.57 12.57		2	0.02	0.01	0.04	0.00	0.00	24.0
16	38	-13755	587	578	0	224	101	6.28	6.28 12.57 12.57		2	0.01	0.01	0.05	0.00	0.00	24.0
17	38	-13725	630	430	0	307	129	6.28	6.28 12.57 12.57		2	0.02	0.01	0.05	0.00	0.00	24.0
18	38	-21168	-2436	907	0	411	-1936	6.28	6.28 12.57 12.57		3	0.10	0.04	0.20	0.00	0.00	24.0
19	38	-17748	3188	402	0	538	1622	6.28	6.28 12.57 12.57		3	0.09	0.06	0.27	0.00	0.00	24.0
20	38	-19088	380	1004	0	107	-146	6.28	6.28 12.57 12.57		3	0.01	0.02	0.09	0.00	0.00	24.0
37	38	-21838	-4290	1090	0	319	-3095	6.28	6.28 12.57 12.57		3	0.16	0.08	0.35	0.00	0.00	24.0
38	38	-16138	5082	249	0	531	2836	6.28	6.28 12.57 12.57		3	0.15	0.09	0.44	0.00	0.00	24.0
39	38	-18368	402	1252	0	-187	-111	6.28	6.28 12.57 12.57		3	0.01	0.02	0.11	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-17940	443	680	0	254	-15	6.28	6.28 12.57 12.57		3	0.01	0.01	0.06	0.00	0.00	24.0
2	50	-14250	-559	608	0	156	-690	6.28	6.28 12.57 12.57		2	0.04	0.01	0.06	0.00	0.00	24.0
3	50	-14240	-546	564	0	187	-680	6.28	6.28 12.57 12.57		2	0.04	0.01	0.05	0.00	0.00	24.0
4	50	-13360	1227	482	0	204	658	6.28	6.28 12.57 12.57		2	0.04	0.02	0.11	0.00	0.00	24.0
5	50	-13350	1240	438	0	235	668	6.28	6.28 12.57 12.57		2	0.04	0.02	0.11	0.00	0.00	24.0
6	50	-13950	51	616	0	138	-230	6.28	6.28 12.57 12.57		2	0.02	0.01	0.06	0.00	0.00	24.0
7	50	-13920	94	468	0	239	-197	6.28	6.28 12.57 12.57		2	0.02	0.01	0.04	0.00	0.00	24.0
8	50	-13680	587	578	0	152	174	6.28	6.28 12.57 12.57		2	0.01	0.01	0.05	0.00	0.00	24.0
9	50	-13650	630	430	0	253	208	6.28	6.28 12.57 12.57		2	0.02	0.01	0.05	0.00	0.00	24.0
10	50	-14250	-559	608	0	156	-690	6.28	6.28 12.57 12.57		2	0.04	0.01	0.06	0.00	0.00	24.0
11	50	-14240	-546	564	0	187	-680	6.28	6.28 12.57 12.57		2	0.04	0.01	0.05	0.00	0.00	24.0
12	50	-13360	1227	482	0	204	658	6.28	6.28 12.57 12.57		2	0.04	0.02	0.11	0.00	0.00	24.0
13	50	-13350	1240	438	0	235	668	6.28	6.28 12.57 12.57		2	0.04	0.02	0.11	0.00	0.00	24.0
14	50	-13950	51	616	0	138	-230	6.28	6.28 12.57 12.57		2	0.02	0.01	0.06	0.00	0.00	24.0
15	50	-13920	94	468	0	239	-197	6.28	6.28 12.57 12.57		2	0.02	0.01	0.04	0.00	0.00	24.0
16	50	-13680	587	578	0	152	174	6.28	6.28 12.57 12.57		2	0.01	0.01	0.05	0.00	0.00	24.0
17	50	-13650	630	430	0	253	208	6.28	6.28 12.57 12.57		2	0.02	0.01	0.05	0.00	0.00	24.0
18	50	-21070	-2436	907	0	298	-2240	6.28	6.28 12.57 12.57		3	0.12	0.04	0.20	0.00	0.00	24.0
19	50	-17650	3188	402	0	488	2021	6.28	6.28 12.57 12.57		3	0.11	0.06	0.27	0.00	0.00	24.0
20	50	-18990	380	1004	0	-18	-98	6.28	6.28 12.57 12.57		3	0.01	0.02	0.09	0.00	0.00	24.0
37	50	-21740	-4290	1090	0	183	-3631	6.28	6.28 12.57 12.57		3	0.19	0.08	0.35	0.00	0.00	24.0
38	50	-16040	5082	249	0	500	3471	6.28	6.28 12.57 12.57		3	0.19	0.09	0.45	0.00	0.00	24.0
39	50	-18270	402	1252	0	-343	-61	6.28	6.28 12.57 12.57		3	0.01	0.02	0.11	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 108 NI 1254 NF 1349 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 9
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-5105	-13	3	0	-37	-12	6.28	6.28	12.57	12.57	3	0.00	0.00	0.00	0.00	0.00	24.0
2	0	-3936	-69	74	0	-40	-100	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
3	0	-3911	-68	-24	0	-28	-98	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
4	0	-3943	47	29	0	-30	79	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
5	0	-3918	48	-69	0	-17	80	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
6	0	-3969	-29	173	0	-52	-39	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
7	0	-3883	-26	-154	0	-9	-34	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
8	0	-3971	6	159	0	-49	15	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
9	0	-3886	9	-168	0	-6	19	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
10	0	-3936	-69	74	0	-40	-100	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
11	0	-3911	-68	-24	0	-28	-98	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
12	0	-3943	47	29	0	-30	79	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
13	0	-3918	48	-69	0	-17	80	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
14	0	-3969	-29	173	0	-52	-39	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
15	0	-3883	-26	-154	0	-9	-34	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
16	0	-3971	6	159	0	-49	15	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
17	0	-3886	9	-168	0	-6	19	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
18	0	-5489	-169	264	0	-85	-250	6.28	6.28	12.57	12.57	3	0.01	0.00	0.03	0.00	0.00	24.0
19	0	-5460	180	-22	0	-30	289	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
20	0	-5440	4	265	0	-79	17	6.28	6.28	12.57	12.57	3	0.00	0.00	0.03	0.00	0.00	24.0
37	0	-5327	-291	326	0	-97	-441	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
38	0	-5279	290	-152	0	-6	459	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
39	0	-5244	-3	328	0	-86	5	6.28	6.28	12.57	12.57	3	0.00	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-5008	-13	3	0	-38	-14	6.28	6.28	12.57	12.57	3	0.00	0.00	0.00	0.00	0.00	24.0
2	12	-3861	-69	74	0	-50	-108	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
3	12	-3836	-68	-24	0	-25	-107	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
4	12	-3868	47	29	0	-34	85	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
5	12	-3843	48	-69	0	-9	86	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
6	12	-3894	-29	173	0	-73	-42	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
7	12	-3808	-26	-154	0	10	-37	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
8	12	-3896	6	159	0	-69	16	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
9	12	-3811	9	-168	0	15	21	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
10	12	-3861	-69	74	0	-50	-108	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
11	12	-3836	-68	-24	0	-25	-107	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
12	12	-3868	47	29	0	-34	85	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
13	12	-3843	48	-69	0	-9	86	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
14	12	-3894	-29	173	0	-73	-42	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
15	12	-3808	-26	-154	0	10	-37	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
16	12	-3896	6	159	0	-69	16	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
17	12	-3811	9	-168	0	15	21	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
18	12	-5392	-169	264	0	-118	-271	6.28	6.28	12.57	12.57	3	0.02	0.00	0.03	0.00	0.00	24.0
19	12	-5362	180	-22	0	-28	312	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
20	12	-5342	4	265	0	-112	18	6.28	6.28	12.57	12.57	3	0.00	0.00	0.03	0.00	0.00	24.0
37	12	-5230	-291	326	0	-138	-477	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
38	12	-5182	290	-152	0	13	495	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
39	12	-5146	-3	328	0	-127	5	6.28	6.28	12.57	12.57	3	0.00	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-4910	-13	3	0	-38	-16	6.28	6.28	12.57	12.57	3	0.00	0.00	0.00	0.00	0.00	24.0
2	25	-3786	-69	74	0	-59	-117	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
3	25	-3761	-68	-24	0	-22	-115	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
4	25	-3793	47	29	0	-37	91	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
5	25	-3768	48	-69	0	0	92	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
6	25	-3819	-29	173	0	-95	-46	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
7	25	-3733	-26	-154	0	30	-41	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
8	25	-3821	6	159	0	-89	16	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
9	25	-3736	9	-168	0	36	22	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
10	25	-3786	-69	74	0	-59	-117	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
11	25	-3761	-68	-24	0	-22	-115	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
12	25	-3793	47	29	0	-37	91	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
13	25	-3768	48	-69	0	0	92	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
14	25	-3819	-29	173	0	-95	-46	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
15	25	-3733	-26	-154	0	30	-41	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
16	25	-3821	6	159	0	-89	16	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
17	25	-3736	9	-168	0	36	22	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
18	25	-5294	-169	264	0	-151	-293	6.28	6.28	12.57	12.57	3	0.02	0.00	0.03	0.00	0.00	24.0
19	25	-5265	180	-22	0	-25	334	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
20	25	-5245	4	265	0	-145	18	6.28	6.28	12.57	12.57	3	0.01	0.00	0.03	0.00	0.00	24.0
37	25	-5132	-291	326	0	-178	-513	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
38	25	-5084	290	-152	0	32	531	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
39	25	-5049	-3	328	0	-168	4	6.28	6.28	12.57	12.57	3	0.01	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-4812	-13	3	0	-39	-17	6.28	6.28	12.57	12.57	3	0.00	0.00	0.00	0.00	0.00	24.0
2	38	-3711	-69	74	0	-68	-125	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
3	38	-3686	-68	-24	0	-19	-124	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
4	38	-3718	47	29	0	-41	97	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
5	38	-3693	48	-69	0	9	98	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
6	38	-3744	-29	173	0	-117	-50	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
7	38	-3658	-26	-154	0	49	-44	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
8	38	-3746	6	159	0	-108	17	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
9	38	-3661	9	-168	0	57	23	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
10	38	-3711	-69	74	0	-68	-125	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
11	38	-3686	-68	-24	0	-19	-124	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
12	38	-3718	47	29	0	-41	97	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
13	38	-3693	48	-69	0	9	98	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
14	38	-3744	-29	173	0	-117	-50	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
15	38	-3658	-26	-154	0	49	-44	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
16	38	-3746	6	159	0	-108	17	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
17	38	-3661	9	-168	0	57	23	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
18	38	-5196	-169	264	0	-184	-314	6.28	6.28	12.57	12.57	3	0.02	0.00	0.03	0.00	0.00	24.0
19	38	-5168	180	-22	0	-22	357	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
20	38	-5148	4	265	0	-178	19	6.28	6.28	12.57	12.57	3	0.01	0.00	0.03	0.00	0.00	24.0
37	38	-5034	-291	326	0	-219	-550	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
38	38	-4986	290	-152	0	51	568	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
39	38	-4952	-3	328	0	-209	4	6.28	6.28	12.57	12.57	3	0.01	0.01	0.04	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-4715	-13	3	0	-39	-19	6.28	6.28	12.57	12.57	3	0.00	0.00	0.00	0.00	0.00	24.0
2	50	-3636	-69	74	0	-78	-134	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
3	50	-3611	-68	-24	0	-16	-132	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
4	50	-3643	47	29	0	-45	103	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
5	50	-3618	48	-69	0	17	104	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
6	50	-3669	-29	173	0	-138	-53	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
7	50	-3583	-26	-154	0	68	-47	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
8	50	-3671	6	159	0	-128	18	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
9	50	-3586	9	-168	0	78	24	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
10	50	-3636	-69	74	0	-78	-134	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
11	50	-3611	-68	-24	0	-16	-132	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
12	50	-3643	47	29	0	-45	103	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
13	50	-3618	48	-69	0	17	104	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
14	50	-3669	-29	173	0	-138	-53	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
15	50	-3583	-26	-154	0	68	-47	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
16	50	-3671	6	159	0	-128	18	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
17	50	-3586	9	-168	0	78	24	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
18	50	-5099	-169	264	0	-217	-335	6.28	6.28	12.57	12.57	3	0.02	0.00	0.03	0.00	0.00	24.0
19	50	-5070	180	-22	0	-19	380	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
20	50	-5050	4	265	0	-211	19	6.28	6.28	12.57	12.57	3	0.01	0.00	0.03	0.00	0.00	24.0
37	50	-4937	-291	326	0	-260	-586	6.28	6.28	12.57	12.57	3	0.04	0.01	0.03	0.00	0.00	24.0
38	50	-4889	290	-152	0	70	604	6.28	6.28	12.57	12.57	3	0.04	0.01	0.03	0.00	0.00	24.0
39	50	-4854	-3	328	0	-250	4	6.28	6.28	12.57	12.57	3	0.01	0.01	0.04	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 109 NI 1349 NF 129 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 9A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-7224	-31	197	0	-39	-20	6.28	6.28	12.57	12.57	3	0.00	0.00	0.02	0.00	0.00	24.0
2	0	-5572	-177	321	0	-78	-128	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
3	0	-5533	-175	105	0	-16	-126	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
4	0	-5581	128	198	0	-45	96	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
5	0	-5542	130	-18	0	17	97	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
6	0	-5621	-73	529	0	-138	-52	6.28	6.28	12.57	12.57	2	0.01	0.01	0.06	0.00	0.00	24.0
7	0	-5490	-65	-189	0	68	-46	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
8	0	-5623	18	492	0	-128	16	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
9	0	-5493	26	-226	0	78	21	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
10	0	-5572	-177	321	0	-78	-128	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
11	0	-5533	-175	105	0	-16	-126	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
12	0	-5581	128	198	0	-45	96	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
13	0	-5542	130	-18	0	17	97	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
14	0	-5621	-73	529	0	-138	-52	6.28	6.28	12.57	12.57	2	0.01	0.01	0.06	0.00	0.00	24.0
15	0	-5490	-65	-189	0	68	-46	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
16	0	-5623	18	492	0	-128	16	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
17	0	-5493	26	-226	0	78	21	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
18	0	-7817	-440	836	0	-217	-318	6.28	6.28	12.57	12.57	3	0.02	0.01	0.09	0.00	0.00	24.0
19	0	-7776	480	116	0	-19	356	6.28	6.28	12.57	12.57	3	0.02	0.01	0.05	0.00	0.00	24.0
20	0	-7738	16	814	0	-211	16	6.28	6.28	12.57	12.57	3	0.01	0.01	0.08	0.00	0.00	24.0
37	0	-7564	-763	994	0	-260	-555	6.28	6.28	12.57	12.57	3	0.03	0.02	0.10	0.00	0.00	24.0
38	0	-7494	771	-205	0	70	568	6.28	6.28	12.57	12.57	3	0.03	0.01	0.07	0.00	0.00	24.0
39	0	-7432	-3	958	0	-250	2	6.28	6.28	12.57	12.57	3	0.01	0.02	0.10	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-7126	-31	197	0	-64	-24	6.28	6.28	12.57	12.57	3	0.00	0.00	0.02	0.00	0.00	24.0
2	12	-5497	-177	321	0	-118	-150	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
3	12	-5458	-175	105	0	-29	-148	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
4	12	-5506	128	198	0	-69	112	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
5	12	-5467	130	-18	0	20	114	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
6	12	-5546	-73	529	0	-204	-61	6.28	6.28	12.57	12.57	2	0.01	0.01	0.06	0.00	0.00	24.0
7	12	-5415	-65	-189	0	92	-54	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
8	12	-5548	18	492	0	-190	18	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
9	12	-5418	26	-226	0	106	24	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
10	12	-5497	-177	321	0	-118	-150	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
11	12	-5458	-175	105	0	-29	-148	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
12	12	-5506	128	198	0	-69	112	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
13	12	-5467	130	-18	0	20	114	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
14	12	-5546	-73	529	0	-204	-61	6.28	6.28	12.57	12.57	2	0.01	0.01	0.06	0.00	0.00	24.0
15	12	-5415	-65	-189	0	92	-54	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
16	12	-5548	18	492	0	-190	18	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
17	12	-5418	26	-226	0	106	24	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
18	12	-7720	-440	836	0	-321	-373	6.28	6.28	12.57	12.57	3	0.02	0.01	0.09	0.00	0.00	24.0
19	12	-7678	480	116	0	-34	416	6.28	6.28	12.57	12.57	3	0.02	0.01	0.05	0.00	0.00	24.0
20	12	-7640	16	814	0	-313	18	6.28	6.28	12.57	12.57	3	0.01	0.01	0.08	0.00	0.00	24.0
37	12	-7466	-763	994	0	-384	-651	6.28	6.28	12.57	12.57	3	0.04	0.02	0.10	0.00	0.00	24.0
38	12	-7396	771	-205	0	95	665	6.28	6.28	12.57	12.57	3	0.04	0.01	0.07	0.00	0.00	24.0
39	12	-7334	-3	958	0	-370	1	6.28	6.28	12.57	12.57	3	0.01	0.02	0.10	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-7029	-31	197	0	-88	-27	6.28	6.28	12.57	12.57	3	0.00	0.00	0.02	0.00	0.00	24.0
2	25	-5422	-177	321	0	-158	-172	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
3	25	-5383	-175	105	0	-42	-170	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
4	25	-5431	128	198	0	-94	128	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
5	25	-5392	130	-18	0	22	130	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
6	25	-5471	-73	529	0	-271	-70	6.28	6.28	12.57	12.57	2	0.02	0.01	0.06	0.00	0.00	24.0
7	25	-5340	-65	-189	0	116	-62	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
8	25	-5473	18	492	0	-251	20	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
9	25	-5343	26	-226	0	135	28	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
10	25	-5422	-177	321	0	-158	-172	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
11	25	-5383	-175	105	0	-42	-170	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
12	25	-5431	128	198	0	-94	128	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
13	25	-5392	130	-18	0	22	130	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
14	25	-5471	-73	529	0	-271	-70	6.28	6.28	12.57	12.57	2	0.02	0.01	0.06	0.00	0.00	24.0
15	25	-5340	-65	-189	0	116	-62	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
16	25	-5473	18	492	0	-251	20	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
17	25	-5343	26	-226	0	135	28	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
18	25	-7622	-440	836	0	-426	-428	6.28	6.28	12.57	12.57	3	0.03	0.01	0.09	0.00	0.00	24.0
19	25	-7581	480	116	0	-48	476	6.28	6.28	12.57	12.57	3	0.03	0.01	0.05	0.00	0.00	24.0
20	25	-7543	16	814	0	-415	20	6.28	6.28	12.57	12.57	3	0.02	0.01	0.08	0.00	0.00	24.0
37	25	-7369	-763	994	0	-508	-746	6.28	6.28	12.57	12.57	3	0.04	0.02	0.10	0.00	0.00	24.0
38	25	-7299	771	-205	0	121	761	6.28	6.28	12.57	12.57	3	0.04	0.01	0.08	0.00	0.00	24.0

39	25	-7237	-3	958	0	-490	1	6.28	6.28	12.57	12.57	3	0.02	0.02	0.10	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-6932	-31	197	0	-113	-31	6.28	6.28	12.57	12.57	3	0.00	0.00	0.02	0.00	0.00	24.0
2	38	-5347	-177	321	0	-198	-194	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
3	38	-5308	-175	105	0	-55	-192	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
4	38	-5356	128	198	0	-119	144	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
5	38	-5317	130	-18	0	24	146	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
6	38	-5396	-73	529	0	-337	-79	6.28	6.28	12.57	12.57	2	0.02	0.01	0.06	0.00	0.00	24.0
7	38	-5265	-65	-189	0	139	-70	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
8	38	-5398	18	492	0	-313	22	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
9	38	-5268	26	-226	0	163	31	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
10	38	-5347	-177	321	0	-198	-194	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
11	38	-5308	-175	105	0	-55	-192	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
12	38	-5356	128	198	0	-119	144	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
13	38	-5317	130	-18	0	24	146	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
14	38	-5396	-73	529	0	-337	-79	6.28	6.28	12.57	12.57	2	0.02	0.01	0.06	0.00	0.00	24.0
15	38	-5265	-65	-189	0	139	-70	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
16	38	-5398	18	492	0	-313	22	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
17	38	-5268	26	-226	0	163	31	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
18	38	-7524	-440	836	0	-530	-483	6.28	6.28	12.57	12.57	3	0.03	0.01	0.09	0.00	0.00	24.0
19	38	-7484	480	116	0	-63	536	6.28	6.28	12.57	12.57	3	0.03	0.01	0.05	0.00	0.00	24.0
20	38	-7446	16	814	0	-516	22	6.28	6.28	12.57	12.57	3	0.02	0.01	0.08	0.00	0.00	24.0
37	38	-7272	-763	994	0	-633	-842	6.28	6.28	12.57	12.57	3	0.05	0.02	0.10	0.00	0.00	24.0
38	38	-7202	771	-205	0	147	857	6.28	6.28	12.57	12.57	3	0.05	0.01	0.08	0.00	0.00	24.0
39	38	-7140	-3	958	0	-609	1	6.28	6.28	12.57	12.57	3	0.02	0.02	0.10	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-6834	-31	197	0	-138	-35	6.28	6.28	12.57	12.57	3	0.01	0.00	0.02	0.00	0.00	24.0
2	50	-5272	-177	321	0	-238	-216	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
3	50	-5233	-175	105	0	-68	-213	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
4	50	-5281	128	198	0	-143	160	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
5	50	-5242	130	-18	0	26	163	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
6	50	-5321	-73	529	0	-403	-88	6.28	6.28	12.57	12.57	2	0.02	0.01	0.06	0.00	0.00	24.0
7	50	-5190	-65	-189	0	163	-78	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
8	50	-5323	18	492	0	-374	25	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
9	50	-5193	26	-226	0	191	34	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
10	50	-5272	-177	321	0	-238	-216	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
11	50	-5233	-175	105	0	-68	-213	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
12	50	-5281	128	198	0	-143	160	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
13	50	-5242	130	-18	0	26	163	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
14	50	-5321	-73	529	0	-403	-88	6.28	6.28	12.57	12.57	2	0.02	0.01	0.06	0.00	0.00	24.0
15	50	-5190	-65	-189	0	163	-78	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
16	50	-5323	18	492	0	-374	25	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
17	50	-5193	26	-226	0	191	34	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
18	50	-7427	-440	836	0	-635	-538	6.28	6.28	12.57	12.57	3	0.04	0.01	0.09	0.00	0.00	24.0
19	50	-7386	480	116	0	-77	597	6.28	6.28	12.57	12.57	3	0.03	0.01	0.05	0.00	0.00	24.0
20	50	-7348	16	814	0	-618	24	6.28	6.28	12.57	12.57	3	0.02	0.01	0.08	0.00	0.00	24.0
37	50	-7174	-763	994	0	-757	-937	6.28	6.28	12.57	12.57	3	0.06	0.02	0.10	0.00	0.00	24.0
38	50	-7104	771	-205	0	172	954	6.28	6.28	12.57	12.57	3	0.06	0.01	0.08	0.00	0.00	24.0
39	50	-7042	-3	958	0	-729	0	6.28	6.28	12.57	12.57	3	0.03	0.02	0.10	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 110 NI 1158 NF 1253 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 8
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-3610	148	378	0	-159	-12	6.28	6.28	9.42	9.42	3	0.01	0.01	0.05	0.00	0.00	24.0
2	0	-2783	84	344	0	-127	-1	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
3	0	-2731	84	295	0	-116	-1	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
4	0	-2824	144	286	0	-129	-18	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
5	0	-2772	144	238	0	-117	-18	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
6	0	-2858	104	380	0	-141	-6	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
7	0	-2684	106	218	0	-103	-7	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
8	0	-2871	122	363	0	-142	-11	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
9	0	-2696	124	201	0	-103	-12	6.28	6.28	9.42	9.42	2	0.01	0.00	0.03	0.00	0.00	24.0
10	0	-2783	84	344	0	-127	-1	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
11	0	-2731	84	295	0	-116	-1	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
12	0	-2824	144	286	0	-129	-18	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
13	0	-2772	144	238	0	-117	-18	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
14	0	-2858	104	380	0	-141	-6	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
15	0	-2684	106	218	0	-103	-7	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
16	0	-2871	122	363	0	-142	-11	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
17	0	-2696	124	201	0	-103	-12	6.28	6.28	9.42	9.42	2	0.01	0.00	0.03	0.00	0.00	24.0
18	0	-3834	78	581	0	-197	9	6.28	6.28	9.42	9.42	3	0.01	0.01	0.08	0.00	0.00	24.0
19	0	-3873	255	333	0	-183	-41	6.28	6.28	9.42	9.42	3	0.01	0.01	0.04	0.00	0.00	24.0
20	0	-3958	162	555	0	-208	-14	6.28	6.28	9.42	9.42	3	0.01	0.01	0.07	0.00	0.00	24.0
37	0	-3713	11	634	0	-189	27	6.28	6.28	9.42	9.42	3	0.01	0.01	0.08	0.00	0.00	24.0
38	0	-3779	307	222	0	-166	-56	6.28	6.28	9.42	9.42	3	0.01	0.01	0.03	0.00	0.00	24.0
39	0	-3920	152	592	0	-208	-11	6.28	6.28	9.42	9.42	3	0.01	0.01	0.08	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-3537	148	378	0	-206	7	6.28	6.28	9.42	9.42	3	0.01	0.01	0.05	0.00	0.00	24.0
2	12	-2727	84	344	0	-170	10	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
3	12	-2675	84	295	0	-152	10	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
4	12	-2768	144	286	0	-164	0	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
5	12	-2716	144	238	0	-147	0	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
6	12	-2802	104	380	0	-189	7	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
7	12	-2628	106	218	0	-130	6	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
8	12	-2815	122	363	0	-187	4	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
9	12	-2640	124	201	0	-128	3	6.28	6.28	9.42	9.42	2	0.01	0.00	0.03	0.00	0.00	24.0
10	12	-2727	84	344	0	-170	10	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
11	12	-2675	84	295	0	-152	10	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
12	12	-2768	144	286	0	-164	0	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
13	12	-2716	144	238	0	-147	0	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
14	12	-2802	104	380	0	-189	7	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
15	12	-2628	106	218	0	-130	6	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
16	12	-2815	122	363	0	-187	4	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
17	12	-2640	124	201	0	-128	3	6.28	6.28	9.42	9.42	2	0.01	0.00	0.03	0.00	0.00	24.0
18	12	-3761	78	581	0	-270	19	6.28	6.28	9.42	9.42	3	0.01	0.01	0.08	0.00	0.00	24.0

19	12	-3800	255	333	0	-225	-9	6.28	6.28	9.42	9.42	3	0.01	0.01	0.04	0.00	0.00	24.0
20	12	-3885	162	555	0	-278	6	6.28	6.28	9.42	9.42	3	0.01	0.01	0.07	0.00	0.00	24.0
37	12	-3640	11	634	0	-269	29	6.28	6.28	9.42	9.42	3	0.01	0.01	0.08	0.00	0.00	24.0
38	12	-3706	307	222	0	-193	-18	6.28	6.28	9.42	9.42	3	0.01	0.01	0.03	0.00	0.00	24.0
39	12	-3847	152	592	0	-282	8	6.28	6.28	9.42	9.42	3	0.01	0.01	0.08	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-3464	148	378	0	-253	25	6.28	6.28	9.42	9.42	3	0.01	0.01	0.05	0.00	0.00	24.0
2	25	-2670	84	344	0	-213	20	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
3	25	-2618	84	295	0	-189	20	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
4	25	-2712	144	286	0	-200	18	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
5	25	-2660	144	238	0	-176	18	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
6	25	-2746	104	380	0	-236	20	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
7	25	-2572	106	218	0	-157	19	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
8	25	-2758	122	363	0	-232	19	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
9	25	-2584	124	201	0	-153	19	6.28	6.28	9.42	9.42	2	0.01	0.00	0.03	0.00	0.00	24.0
10	25	-2670	84	344	0	-213	20	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
11	25	-2618	84	295	0	-189	20	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
12	25	-2712	144	286	0	-200	18	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
13	25	-2660	144	238	0	-176	18	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
14	25	-2746	104	380	0	-236	20	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
15	25	-2572	106	218	0	-157	19	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
16	25	-2758	122	363	0	-232	19	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
17	25	-2584	124	201	0	-153	19	6.28	6.28	9.42	9.42	2	0.01	0.00	0.03	0.00	0.00	24.0
18	25	-3688	78	581	0	-343	29	6.28	6.28	9.42	9.42	3	0.02	0.01	0.08	0.00	0.00	24.0
19	25	-3727	255	333	0	-266	23	6.28	6.28	9.42	9.42	3	0.01	0.01	0.04	0.00	0.00	24.0
20	25	-3812	162	555	0	-347	26	6.28	6.28	9.42	9.42	3	0.02	0.01	0.07	0.00	0.00	24.0
37	25	-3566	11	634	0	-348	30	6.28	6.28	9.42	9.42	3	0.02	0.01	0.08	0.00	0.00	24.0
38	25	-3633	307	222	0	-221	20	6.28	6.28	9.42	9.42	3	0.01	0.01	0.03	0.00	0.00	24.0
39	25	-3774	152	592	0	-356	27	6.28	6.28	9.42	9.42	3	0.02	0.01	0.08	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-3391	148	378	0	-300	44	6.28	6.28	9.42	9.42	3	0.02	0.01	0.05	0.00	0.00	24.0
2	38	-2614	84	344	0	-256	31	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
3	38	-2562	84	295	0	-226	31	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
4	38	-2655	144	286	0	-236	36	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
5	38	-2603	144	238	0	-206	36	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
6	38	-2689	104	380	0	-284	33	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
7	38	-2515	106	218	0	-184	32	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
8	38	-2702	122	363	0	-278	35	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
9	38	-2527	124	201	0	-178	34	6.28	6.28	9.42	9.42	2	0.01	0.00	0.03	0.00	0.00	24.0
10	38	-2614	84	344	0	-256	31	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
11	38	-2562	84	295	0	-226	31	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
12	38	-2655	144	286	0	-236	36	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
13	38	-2603	144	238	0	-206	36	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
14	38	-2689	104	380	0	-284	33	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
15	38	-2515	106	218	0	-184	32	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
16	38	-2702	122	363	0	-278	35	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
17	38	-2527	124	201	0	-178	34	6.28	6.28	9.42	9.42	2	0.01	0.00	0.03	0.00	0.00	24.0
18	38	-3614	78	581	0	-415	38	6.28	6.28	9.42	9.42	3	0.02	0.01	0.08	0.00	0.00	24.0
19	38	-3654	255	333	0	-308	55	6.28	6.28	9.42	9.42	3	0.02	0.01	0.04	0.00	0.00	24.0
20	38	-3738	162	555	0	-417	47	6.28	6.28	9.42	9.42	3	0.02	0.01	0.07	0.00	0.00	24.0
37	38	-3493	11	634	0	-427	31	6.28	6.28	9.42	9.42	3	0.02	0.01	0.08	0.00	0.00	24.0
38	38	-3560	307	222	0	-249	59	6.28	6.28	9.42	9.42	3	0.01	0.01	0.03	0.00	0.00	24.0
39	38	-3701	152	592	0	-430	46	6.28	6.28	9.42	9.42	3	0.02	0.01	0.08	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-3318	148	378	0	-348	62	6.28	6.28	9.42	9.42	3	0.02	0.01	0.05	0.00	0.00	24.0
2	50	-2558	84	344	0	-299	41	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
3	50	-2506	84	295	0	-263	41	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
4	50	-2599	144	286	0	-272	54	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
5	50	-2547	144	238	0	-236	54	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
6	50	-2633	104	380	0	-332	46	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
7	50	-2459	106	218	0	-211	46	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
8	50	-2646	122	363	0	-323	50	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
9	50	-2471	124	201	0	-203	50	6.28	6.28	9.42	9.42	2	0.02	0.00	0.03	0.00	0.00	24.0
10	50	-2558	84	344	0	-299	41	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
11	50	-2506	84	295	0	-263	41	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
12	50	-2599	144	286	0	-272	54	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
13	50	-2547	144	238	0	-236	54	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
14	50	-2633	104	380	0	-332	46	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
15	50	-2459	106	218	0	-211	46	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
16	50	-2646	122	363	0	-323	50	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
17	50	-2471	124	201	0	-203	50	6.28	6.28	9.42	9.42	2	0.02	0.00	0.03	0.00	0.00	24.0
18	50	-3541	78	581	0	-488	48	6.28	6.28	9.42	9.42	3	0.02	0.01	0.08	0.00	0.00	24.0
19	50	-3581	255	333	0	-350	87	6.28	6.28	9.42	9.42	3	0.02	0.01	0.04	0.00	0.00	24.0
20	50	-3665	162	555	0	-486	67	6.28	6.28	9.42	9.42	3	0.02	0.01	0.07	0.00	0.00	24.0
37	50	-3420	11	634	0	-507	33	6.28	6.28	9.42	9.42	3	0.03	0.01	0.08	0.00	0.00	24.0
38	50	-3487	307	222	0	-277	97	6.28	6.28	9.42	9.42	3	0.02	0.01	0.03	0.00	0.00	24.0
39	50	-3628	152	592	0	-504	65	6.28	6.28	9.42	9.42	3	0.03	0.01	0.08	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 111 NI 1253 NF 213 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 8A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-4585	-35	386	0	-376	56	6.28	6.28	9.42	9.42	3	0.02	0.01	0.05	0.00	0.00	24.0
2	0	-3521	-99	378	0	-325	33	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
3	0	-3475	-94	289	0	-282	33	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
4	0	-3579	40	305	0	-296	53	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
5	0	-3533	45	216	0	-253	53	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
6	0	-3595	-56	456	0	-365	40	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
7	0	-3442	-40	160	0	-222	40	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
8	0	-3612	-15	434	0	-356	46	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
9	0	-3459	2	138	0	-213	46	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
10	0	-3521	-99	378	0	-325	33	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
11	0	-3475	-94	289	0	-282	33	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
12	0	-3579	40	305	0	-296	53	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
13	0	-3533	45	216	0	-253	53	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
14	0	-3595	-56	456	0	-365	40	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0

15	0	-3442	-40	160	0	-222	40	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
16	0	-3612	-15	434	0	-356	46	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
17	0	-3459	2	138	0	-213	46	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
18	0	-4828	-236	712	0	-535	33	6.28	6.28	9.42	9.42	3	0.03	0.02	0.09	0.00	0.00	24.0
19	0	-4926	181	354	0	-380	91	6.28	6.28	9.42	9.42	3	0.02	0.01	0.05	0.00	0.00	24.0
20	0	-4974	-38	697	0	-539	62	6.28	6.28	9.42	9.42	3	0.03	0.02	0.09	0.00	0.00	24.0
37	0	-4662	-376	778	0	-556	11	6.28	6.28	9.42	9.42	3	0.03	0.02	0.10	0.00	0.00	24.0
38	0	-4826	319	183	0	-298	108	6.28	6.28	9.42	9.42	3	0.02	0.01	0.03	0.00	0.00	24.0
39	0	-4905	-47	754	0	-562	60	6.28	6.28	9.42	9.42	3	0.03	0.02	0.10	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-4512	-35	386	0	-424	51	6.28	6.28	9.42	9.42	3	0.02	0.01	0.05	0.00	0.00	24.0
2	12	-3465	-99	378	0	-372	21	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
3	12	-3419	-94	289	0	-318	21	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
4	12	-3523	40	305	0	-334	58	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
5	12	-3477	45	216	0	-280	58	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
6	12	-3539	-56	456	0	-422	33	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
7	12	-3386	-40	160	0	-242	35	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
8	12	-3556	-15	434	0	-411	44	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
9	12	-3403	2	138	0	-230	46	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
10	12	-3465	-99	378	0	-372	21	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
11	12	-3419	-94	289	0	-318	21	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
12	12	-3523	40	305	0	-334	58	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
13	12	-3477	45	216	0	-280	58	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
14	12	-3539	-56	456	0	-422	33	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
15	12	-3386	-40	160	0	-242	35	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
16	12	-3556	-15	434	0	-411	44	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
17	12	-3403	2	138	0	-230	46	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
18	12	-4755	-236	712	0	-624	4	6.28	6.28	9.42	9.42	3	0.03	0.02	0.09	0.00	0.00	24.0
19	12	-4853	181	354	0	-425	114	6.28	6.28	9.42	9.42	3	0.02	0.01	0.05	0.00	0.00	24.0
20	12	-4901	-38	697	0	-626	57	6.28	6.28	9.42	9.42	3	0.03	0.02	0.09	0.00	0.00	24.0
37	12	-4589	-376	778	0	-653	-36	6.28	6.28	9.42	9.42	3	0.03	0.02	0.10	0.00	0.00	24.0
38	12	-4753	319	183	0	-321	148	6.28	6.28	9.42	9.42	3	0.02	0.01	0.03	0.00	0.00	24.0
39	12	-4832	-47	754	0	-657	54	6.28	6.28	9.42	9.42	3	0.03	0.02	0.10	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-4439	-35	386	0	-472	47	6.28	6.28	9.42	9.42	3	0.02	0.01	0.05	0.00	0.00	24.0
2	25	-3408	-99	378	0	-419	8	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
3	25	-3362	-94	289	0	-354	9	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
4	25	-3466	40	305	0	-372	63	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
5	25	-3420	45	216	0	-307	64	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
6	25	-3482	-56	456	0	-479	26	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
7	25	-3330	-40	160	0	-262	30	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
8	25	-3500	-15	434	0	-465	42	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
9	25	-3346	2	138	0	-247	46	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
10	25	-3408	-99	378	0	-419	8	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
11	25	-3362	-94	289	0	-354	9	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
12	25	-3466	40	305	0	-372	63	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
13	25	-3420	45	216	0	-307	64	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
14	25	-3482	-56	456	0	-479	26	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
15	25	-3330	-40	160	0	-262	30	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
16	25	-3500	-15	434	0	-465	42	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
17	25	-3346	2	138	0	-247	46	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
18	25	-4682	-236	712	0	-713	-26	6.28	6.28	9.42	9.42	3	0.04	0.02	0.09	0.00	0.00	24.0
19	25	-4780	181	354	0	-469	136	6.28	6.28	9.42	9.42	3	0.03	0.01	0.05	0.00	0.00	24.0
20	25	-4828	-38	697	0	-713	53	6.28	6.28	9.42	9.42	3	0.04	0.02	0.09	0.00	0.00	24.0
37	25	-4516	-376	778	0	-751	-83	6.28	6.28	9.42	9.42	3	0.04	0.02	0.10	0.00	0.00	24.0
38	25	-4680	319	183	0	-344	188	6.28	6.28	9.42	9.42	3	0.02	0.01	0.03	0.00	0.00	24.0
39	25	-4759	-47	754	0	-751	48	6.28	6.28	9.42	9.42	3	0.04	0.02	0.10	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-4366	-35	386	0	-521	43	6.28	6.28	9.42	9.42	3	0.03	0.01	0.05	0.00	0.00	24.0
2	38	-3352	-99	378	0	-467	-4	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
3	38	-3306	-94	289	0	-390	-2	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
4	38	-3410	40	305	0	-410	68	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
5	38	-3364	45	216	0	-334	69	6.28	6.28	9.42	9.42	2	0.03	0.01	0.03	0.00	0.00	24.0
6	38	-3426	-56	456	0	-536	19	6.28	6.28	9.42	9.42	2	0.04	0.01	0.06	0.00	0.00	24.0
7	38	-3273	-40	160	0	-282	25	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
8	38	-3443	-15	434	0	-519	41	6.28	6.28	9.42	9.42	2	0.04	0.01	0.06	0.00	0.00	24.0
9	38	-3290	2	138	0	-265	46	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
10	38	-3352	-99	378	0	-467	-4	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
11	38	-3306	-94	289	0	-390	-2	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
12	38	-3410	40	305	0	-410	68	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
13	38	-3364	45	216	0	-334	69	6.28	6.28	9.42	9.42	2	0.03	0.01	0.03	0.00	0.00	24.0
14	38	-3426	-56	456	0	-536	19	6.28	6.28	9.42	9.42	2	0.04	0.01	0.06	0.00	0.00	24.0
15	38	-3273	-40	160	0	-282	25	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
16	38	-3443	-15	434	0	-519	41	6.28	6.28	9.42	9.42	2	0.04	0.01	0.06	0.00	0.00	24.0
17	38	-3290	2	138	0	-265	46	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
18	38	-4608	-236	712	0	-802	-55	6.28	6.28	9.42	9.42	3	0.04	0.02	0.09	0.00	0.00	24.0
19	38	-4707	181	354	0	-513	159	6.28	6.28	9.42	9.42	3	0.03	0.01	0.05	0.00	0.00	24.0
20	38	-4754	-38	697	0	-801	48	6.28	6.28	9.42	9.42	3	0.04	0.02	0.09	0.00	0.00	24.0
37	38	-4442	-376	778	0	-848	-130	6.28	6.28	9.42	9.42	3	0.04	0.02	0.10	0.00	0.00	24.0
38	38	-4606	319	183	0	-366	228	6.28	6.28	9.42	9.42	3	0.03	0.01	0.03	0.00	0.00	24.0
39	38	-4686	-47	754	0	-845	42	6.28	6.28	9.42	9.42	3	0.04	0.02	0.10	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-4293	-35	386	0	-569	38	6.28	6.28	9.42	9.42	3	0.03	0.01	0.05	0.00	0.00	24.0
2	50	-3296	-99	378	0	-514	-16	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
3	50	-3250	-94	289	0	-426	-14	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
4	50	-3354	40	305	0	-449	73	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
5	50	-3308	45	216	0	-361	75	6.28	6.28	9.42	9.42	2	0.03	0.01	0.03	0.00	0.00	24.0
6	50	-3370	-56	456	0	-593	12	6.28	6.28	9.42	9.42	2	0.04	0.01	0.06	0.00	0.00	24.0
7	50	-3217	-40	160	0	-302	20	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
8	50	-3387	-15	434	0	-573	39	6.28	6.28	9.42	9.42	2	0.04	0.01	0.06	0.00	0.00	24.0
9	50	-3234	2	138	0	-282	47	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
10	50	-3296	-99	378	0	-514	-16	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
11	50	-3250	-94	289	0	-426	-14	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
12	50	-3354	40	305	0	-449	73	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
13	50	-3308	45	216	0	-361	75	6.28	6.28	9.42	9.42	2	0.03	0.01	0.03	0.00	0.00	24.0
14	50	-3370	-56	456	0	-593	12	6.28	6.28	9.42	9.42	2	0.04	0.01	0.06	0.00	0.00	24.0
15	50	-3217	-40	160	0	-302	20	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
16	50	-3387	-15	434	0	-573	39	6.28	6.28	9.42	9.42	2	0.04	0.01	0.06	0.00	0.00	24.0
17	50	-3234	2	138	0	-282	47	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
18	50	-4535	-236	712	0	-891	-85	6.28	6.28	9.42	9.42	3	0.04	0.02	0.09	0.00	0.00	24.0
19	50	-4634	181	354	0	-558	182	6.28	6.28	9.42	9.42	3	0.03	0.01	0.05	0.00	0.00	24.0
20	50	-4681	-38	697	0	-888	43	6.28	6.28	9.42	9.42	3	0.04	0.02	0.09	0.00	0.00	24.0

37	50	-4369	-376	778	0	-945	-177	6.28	6.28	9.42	9.42	3	0.05	0.02	0.10	0.00	0.00	24.0
38	50	-4533	319	183	0	-389	267	6.28	6.28	9.42	9.42	3	0.03	0.01	0.03	0.00	0.00	24.0
39	50	-4613	-47	754	0	-939	36	6.28	6.28	9.42	9.42	3	0.05	0.02	0.10	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 112 NI 175 NF 89 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 17
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-7676	29	-100	0	343	-9	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
2	0	-5905	16	-53	0	216	-7	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
3	0	-5923	16	-105	0	317	-7	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
4	0	-5887	28	-50	0	211	-7	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
5	0	-5905	29	-102	0	312	-7	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
6	0	-5877	19	9	0	96	-7	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
7	0	-5937	22	-165	0	434	-7	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
8	0	-5872	23	10	0	94	-7	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
9	0	-5932	25	-164	0	432	-7	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
10	0	-5905	16	-53	0	216	-7	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
11	0	-5923	16	-105	0	317	-7	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
12	0	-5887	28	-50	0	211	-7	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
13	0	-5905	29	-102	0	312	-7	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
14	0	-5877	19	9	0	96	-7	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
15	0	-5937	22	-165	0	434	-7	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
16	0	-5872	23	10	0	94	-7	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
17	0	-5932	25	-164	0	432	-7	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
18	0	-8876	-118	-256	0	836	0	6.28	6.28	12.57	12.57	3	0.03	0.00	0.03	0.00	0.00	24.0
19	0	-8473	149	-203	0	694	-19	6.28	6.28	12.57	12.57	3	0.03	0.00	0.02	0.00	0.00	24.0
20	0	-8574	22	-585	0	3306	-10	6.28	6.28	12.57	12.57	3	0.12	0.01	0.06	0.00	0.00	24.0
37	0	-8699	-202	-232	0	747	7	6.28	6.28	12.57	12.57	3	0.03	0.00	0.02	0.00	0.00	24.0
38	0	-8027	242	-144	0	511	-26	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
39	0	-8197	31	-781	0	4864	-10	6.28	6.28	12.57	12.57	3	0.18	0.01	0.08	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-7578	29	-100	0	356	-5	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
2	12	-5830	16	-53	0	223	-5	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
3	12	-5848	16	-105	0	331	-5	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
4	12	-5812	28	-50	0	217	-3	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
5	12	-5830	29	-102	0	325	-3	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
6	12	-5802	19	9	0	95	-4	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
7	12	-5862	22	-165	0	454	-4	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
8	12	-5797	23	10	0	93	-4	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
9	12	-5857	25	-164	0	453	-4	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
10	12	-5830	16	-53	0	223	-5	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
11	12	-5848	16	-105	0	331	-5	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
12	12	-5812	28	-50	0	217	-3	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
13	12	-5830	29	-102	0	325	-3	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
14	12	-5802	19	9	0	95	-4	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
15	12	-5862	22	-165	0	454	-4	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
16	12	-5797	23	10	0	93	-4	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
17	12	-5857	25	-164	0	453	-4	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
18	12	-8778	-118	-256	0	868	-14	6.28	6.28	12.57	12.57	3	0.03	0.00	0.03	0.00	0.00	24.0
19	12	-8376	149	-203	0	720	-1	6.28	6.28	12.57	12.57	3	0.03	0.00	0.02	0.00	0.00	24.0
20	12	-8476	22	-585	0	3379	-7	6.28	6.28	12.57	12.57	3	0.12	0.01	0.06	0.00	0.00	24.0
37	12	-8602	-202	-232	0	776	-18	6.28	6.28	12.57	12.57	3	0.03	0.00	0.02	0.00	0.00	24.0
38	12	-7930	242	-144	0	529	5	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
39	12	-8100	31	-781	0	4961	-6	6.28	6.28	12.57	12.57	3	0.18	0.01	0.08	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-7481	29	-100	0	368	-2	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
2	25	-5755	16	-53	0	229	-3	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
3	25	-5773	16	-105	0	344	-3	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
4	25	-5737	28	-50	0	223	0	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
5	25	-5755	29	-102	0	338	0	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
6	25	-5727	19	9	0	94	-2	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
7	25	-5787	22	-165	0	475	-1	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
8	25	-5722	23	10	0	92	-1	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
9	25	-5782	25	-164	0	473	-1	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
10	25	-5755	16	-53	0	229	-3	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
11	25	-5773	16	-105	0	344	-3	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
12	25	-5737	28	-50	0	223	0	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
13	25	-5755	29	-102	0	338	0	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
14	25	-5727	19	9	0	94	-2	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
15	25	-5787	22	-165	0	475	-1	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
16	25	-5722	23	10	0	92	-1	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
17	25	-5782	25	-164	0	473	-1	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
18	25	-8681	-118	-256	0	900	-29	6.28	6.28	12.57	12.57	3	0.03	0.00	0.03	0.00	0.00	24.0
19	25	-8278	149	-203	0	745	18	6.28	6.28	12.57	12.57	3	0.03	0.00	0.02	0.00	0.00	24.0
20	25	-8379	22	-585	0	3452	-4	6.28	6.28	12.57	12.57	3	0.13	0.01	0.06	0.00	0.00	24.0
37	25	-8504	-202	-232	0	805	-43	6.28	6.28	12.57	12.57	3	0.03	0.00	0.02	0.00	0.00	24.0
38	25	-7832	242	-144	0	547	35	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
39	25	-8002	31	-781	0	5059	-2	6.28	6.28	12.57	12.57	3	0.19	0.01	0.08	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-7384	29	-100	0	381	2	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
2	38	-5680	16	-53	0	236	-1	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
3	38	-5698	16	-105	0	357	-1	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
4	38	-5662	28	-50	0	229	4	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
5	38	-5680	29	-102	0	350	4	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
6	38	-5652	19	9	0	92	1	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
7	38	-5712	22	-165	0	496	1	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
8	38	-5647	23	10	0	91	2	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
9	38	-5707	25	-164	0	494	3	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
10	38	-5680	16	-53	0	236	-1	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
11	38	-5698	16	-105	0	357	-1	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
12	38	-5662	28	-50	0	229	4	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
13	38	-5680	29	-102	0	350	4	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
14	38	-5652	19	9	0	92	1	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
15	38	-5712	22	-165	0	496	1	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
16	38	-5647	23	10	0	91	2	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0

17	38	-5707	25	-164	0	494	3	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
18	38	-8584	-118	-256	0	932	-44	6.28	6.28	12.57	12.57	3	0.03	0.00	0.03	0.00	0.00	24.0
19	38	-8180	149	-203	0	770	37	6.28	6.28	12.57	12.57	3	0.03	0.00	0.02	0.00	0.00	24.0
20	38	-8282	22	-585	0	3525	-1	6.28	6.28	12.57	12.57	3	0.13	0.01	0.06	0.00	0.00	24.0
37	38	-8406	-202	-232	0	834	-69	6.28	6.28	12.57	12.57	3	0.03	0.00	0.02	0.00	0.00	24.0
38	38	-7734	242	-144	0	565	65	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
39	38	-7904	31	-781	0	5156	2	6.28	6.28	12.57	12.57	3	0.19	0.01	0.08	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-7286	29	-100	0	394	6	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
2	50	-5605	16	-53	0	242	1	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
3	50	-5623	16	-105	0	370	1	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
4	50	-5587	28	-50	0	236	7	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
5	50	-5605	29	-102	0	363	8	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
6	50	-5577	19	9	0	91	3	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
7	50	-5637	22	-165	0	516	4	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
8	50	-5572	23	10	0	89	5	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
9	50	-5632	25	-164	0	514	6	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
10	50	-5605	16	-53	0	242	1	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
11	50	-5623	16	-105	0	370	1	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
12	50	-5587	28	-50	0	236	7	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
13	50	-5605	29	-102	0	363	8	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
14	50	-5577	19	9	0	91	3	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
15	50	-5637	22	-165	0	516	4	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
16	50	-5572	23	10	0	89	5	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
17	50	-5632	25	-164	0	514	6	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
18	50	-8486	-118	-256	0	964	-58	6.28	6.28	12.57	12.57	3	0.04	0.00	0.03	0.00	0.00	24.0
19	50	-8083	149	-203	0	796	55	6.28	6.28	12.57	12.57	3	0.03	0.00	0.02	0.00	0.00	24.0
20	50	-8184	22	-585	0	3598	1	6.28	6.28	12.57	12.57	3	0.13	0.01	0.06	0.00	0.00	24.0
37	50	-8309	-202	-232	0	863	-94	6.28	6.28	12.57	12.57	3	0.03	0.00	0.02	0.00	0.00	24.0
38	50	-7637	242	-144	0	583	95	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
39	50	-7807	31	-781	0	5254	6	6.28	6.28	12.57	12.57	3	0.19	0.01	0.08	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 113 NI 89 NF 41 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 17A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-11360	15	-178	0	375	6	6.28	6.28	12.57	12.57	3	0.01	0.00	0.02	0.00	0.00	24.0
2	0	-8740	-24	-93	0	228	1	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
3	0	-8768	-21	-187	0	356	1	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
4	0	-8711	43	-87	0	221	7	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
5	0	-8739	46	-181	0	349	8	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
6	0	-8697	-3	19	0	76	3	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
7	0	-8790	5	-295	0	503	4	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
8	0	-8688	17	21	0	74	5	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
9	0	-8782	25	-293	0	501	6	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
10	0	-8740	-24	-93	0	228	1	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
11	0	-8768	-21	-187	0	356	1	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
12	0	-8711	43	-87	0	221	7	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
13	0	-8739	46	-181	0	349	8	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
14	0	-8697	-3	19	0	76	3	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
15	0	-8790	5	-295	0	503	4	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
16	0	-8688	17	21	0	74	5	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
17	0	-8782	25	-293	0	501	6	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
18	0	-13270	-634	-454	0	921	-58	6.28	6.28	12.57	12.57	3	0.03	0.01	0.05	0.00	0.00	24.0
19	0	-12620	494	-360	0	758	55	6.28	6.28	12.57	12.57	3	0.03	0.01	0.04	0.00	0.00	24.0
20	0	-12780	-40	-1017	0	3315	1	6.28	6.28	12.57	12.57	3	0.12	0.02	0.10	0.00	0.00	24.0
37	0	-12990	-982	-412	0	826	-94	6.28	6.28	12.57	12.57	3	0.03	0.02	0.08	0.00	0.00	24.0
38	0	-11910	897	-255	0	554	95	6.28	6.28	12.57	12.57	3	0.02	0.02	0.07	0.00	0.00	24.0
39	0	-12180	7	-1350	0	4816	6	6.28	6.28	12.57	12.57	3	0.17	0.02	0.13	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-11262	15	-178	0	397	7	6.28	6.28	12.57	12.57	3	0.01	0.00	0.02	0.00	0.00	24.0
2	12	-8665	-24	-93	0	239	-2	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
3	12	-8693	-21	-187	0	379	-1	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
4	12	-8636	43	-87	0	232	13	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
5	12	-8664	46	-181	0	372	13	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
6	12	-8622	-3	19	0	74	3	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
7	12	-8715	5	-295	0	540	5	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
8	12	-8613	17	21	0	71	7	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
9	12	-8707	25	-293	0	537	9	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
10	12	-8665	-24	-93	0	239	-2	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
11	12	-8693	-21	-187	0	379	-1	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
12	12	-8636	43	-87	0	232	13	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
13	12	-8664	46	-181	0	372	13	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
14	12	-8622	-3	19	0	74	3	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
15	12	-8715	5	-295	0	540	5	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
16	12	-8613	17	21	0	71	7	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
17	12	-8707	25	-293	0	537	9	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
18	12	-13172	-634	-454	0	978	-138	6.28	6.28	12.57	12.57	3	0.04	0.01	0.05	0.00	0.00	24.0
19	12	-12522	494	-360	0	802	117	6.28	6.28	12.57	12.57	3	0.03	0.01	0.04	0.00	0.00	24.0
20	12	-12682	-40	-1017	0	3442	-4	6.28	6.28	12.57	12.57	3	0.12	0.02	0.10	0.00	0.00	24.0
37	12	-12892	-982	-412	0	877	-217	6.28	6.28	12.57	12.57	3	0.03	0.02	0.08	0.00	0.00	24.0
38	12	-11812	897	-255	0	585	208	6.28	6.28	12.57	12.57	3	0.02	0.02	0.07	0.00	0.00	24.0
39	12	-12082	7	-1350	0	4985	7	6.28	6.28	12.57	12.57	3	0.18	0.02	0.13	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-11165	15	-178	0	419	9	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
2	25	-8590	-24	-93	0	251	-5	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
3	25	-8618	-21	-187	0	402	-4	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
4	25	-8561	43	-87	0	243	18	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
5	25	-8589	46	-181	0	394	19	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
6	25	-8547	-3	19	0	71	2	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
7	25	-8640	5	-295	0	576	5	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
8	25	-8538	17	21	0	69	9	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
9	25	-8632	25	-293	0	574	12	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
10	25	-8590	-24	-93	0	251	-5	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
11	25	-8618	-21	-187	0	402	-4	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
12	25	-8561	43	-87	0	243	18	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0

13	25	-8589	46	-181	0	394	19	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
14	25	-8547	-3	19	0	71	2	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
15	25	-8640	5	-295	0	576	5	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
16	25	-8538	17	21	0	69	9	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
17	25	-8632	25	-293	0	574	12	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
18	25	-13075	-634	-454	0	1034	-217	6.28	6.28	12.57	12.57	3	0.04	0.01	0.05	0.00	0.00	24.0
19	25	-12425	494	-360	0	847	179	6.28	6.28	12.57	12.57	3	0.03	0.01	0.04	0.00	0.00	24.0
20	25	-12585	-40	-1017	0	3570	-9	6.28	6.28	12.57	12.57	3	0.13	0.02	0.10	0.00	0.00	24.0
37	25	-12795	-982	-412	0	929	-339	6.28	6.28	12.57	12.57	3	0.04	0.02	0.08	0.00	0.00	24.0
38	25	-11715	897	-255	0	617	320	6.28	6.28	12.57	12.57	3	0.03	0.02	0.07	0.00	0.00	24.0
39	25	-11985	7	-1350	0	5154	8	6.28	6.28	12.57	12.57	3	0.18	0.02	0.13	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-11068	15	-178	0	442	11	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
2	38	-8515	-24	-93	0	262	-8	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
3	38	-8543	-21	-187	0	426	-6	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
4	38	-8486	43	-87	0	254	24	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
5	38	-8514	46	-181	0	417	25	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
6	38	-8472	-3	19	0	69	2	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
7	38	-8565	5	-295	0	613	6	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
8	38	-8463	17	21	0	66	11	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
9	38	-8557	25	-293	0	610	15	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
10	38	-8515	-24	-93	0	262	-8	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
11	38	-8543	-21	-187	0	426	-6	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
12	38	-8486	43	-87	0	254	24	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
13	38	-8514	46	-181	0	417	25	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
14	38	-8472	-3	19	0	69	2	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
15	38	-8565	5	-295	0	613	6	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
16	38	-8463	17	21	0	66	11	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
17	38	-8557	25	-293	0	610	15	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
18	38	-12978	-634	-454	0	1091	-296	6.28	6.28	12.57	12.57	3	0.04	0.01	0.05	0.00	0.00	24.0
19	38	-12328	494	-360	0	892	240	6.28	6.28	12.57	12.57	3	0.04	0.01	0.04	0.00	0.00	24.0
20	38	-12488	-40	-1017	0	3697	-14	6.28	6.28	12.57	12.57	3	0.13	0.02	0.10	0.00	0.00	24.0
37	38	-12698	-982	-412	0	980	-462	6.28	6.28	12.57	12.57	3	0.04	0.02	0.08	0.00	0.00	24.0
38	38	-11618	897	-255	0	649	432	6.28	6.28	12.57	12.57	3	0.03	0.02	0.07	0.00	0.00	24.0
39	38	-11888	7	-1350	0	5323	9	6.28	6.28	12.57	12.57	3	0.19	0.02	0.13	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-10970	15	-178	0	464	13	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
2	50	-8440	-24	-93	0	274	-11	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
3	50	-8468	-21	-187	0	449	-9	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
4	50	-8411	43	-87	0	264	29	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
5	50	-8439	46	-181	0	440	30	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
6	50	-8397	-3	19	0	66	2	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
7	50	-8490	5	-295	0	650	6	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
8	50	-8388	17	21	0	64	13	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
9	50	-8482	25	-293	0	647	18	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
10	50	-8440	-24	-93	0	274	-11	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
11	50	-8468	-21	-187	0	449	-9	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
12	50	-8411	43	-87	0	264	29	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
13	50	-8439	46	-181	0	440	30	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
14	50	-8397	-3	19	0	66	2	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
15	50	-8490	5	-295	0	650	6	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
16	50	-8388	17	21	0	64	13	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
17	50	-8482	25	-293	0	647	18	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
18	50	-12880	-634	-454	0	1148	-375	6.28	6.28	12.57	12.57	3	0.05	0.01	0.05	0.00	0.00	24.0
19	50	-12230	494	-360	0	937	302	6.28	6.28	12.57	12.57	3	0.04	0.01	0.04	0.00	0.00	24.0
20	50	-12390	-40	-1017	0	3824	-19	6.28	6.28	12.57	12.57	3	0.14	0.02	0.10	0.00	0.00	24.0
37	50	-12600	-982	-412	0	1032	-585	6.28	6.28	12.57	12.57	3	0.05	0.02	0.08	0.00	0.00	24.0
38	50	-11520	897	-255	0	681	544	6.28	6.28	12.57	12.57	3	0.04	0.02	0.07	0.00	0.00	24.0
39	50	-11790	7	-1350	0	5492	9	6.28	6.28	12.57	12.57	3	0.20	0.02	0.13	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 114 NI 477 NF 46 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 22
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-8485	-23	19	0	-16	-17	6.28	6.28	12.57	12.57	3	0.00	0.00	0.00	0.00	0.00	24.0
2	0	-6530	-18	50	0	-89	-14	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
3	0	-6548	-15	-5	0	16	-15	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
4	0	-6505	-19	35	0	-40	-11	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
5	0	-6523	-17	-20	0	65	-12	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
6	0	-6500	-22	109	0	-195	-13	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
7	0	-6561	-13	-75	0	157	-14	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
8	0	-6493	-22	104	0	-181	-12	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
9	0	-6553	-13	-79	0	171	-13	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
10	0	-6530	-18	50	0	-89	-14	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
11	0	-6548	-15	-5	0	16	-15	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
12	0	-6505	-19	35	0	-40	-11	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
13	0	-6523	-17	-20	0	65	-12	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
14	0	-6500	-22	109	0	-195	-13	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
15	0	-6561	-13	-75	0	157	-14	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
16	0	-6493	-22	104	0	-181	-12	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
17	0	-6553	-13	-79	0	171	-13	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
18	0	-9488	-104	75	0	-137	-30	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
19	0	-9660	94	-65	0	252	-34	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
20	0	-9480	23	-198	0	2079	-35	6.28	6.28	12.57	12.57	3	0.08	0.00	0.02	0.00	0.00	24.0
37	0	-9092	-175	125	0	-289	-24	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
38	0	-9378	154	-107	0	359	-30	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
39	0	-9078	36	-329	0	3404	-31	6.28	6.28	12.57	12.57	3	0.12	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-8388	-23	19	0	-18	-20	6.28	6.28	12.57	12.57	3	0.00	0.00	0.00	0.00	0.00	24.0
2	12	-6455	-18	50	0	-95	-17	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
3	12	-6473	-15	-5	0	17	-17	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
4	12	-6430	-19	35	0	-45	-14	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
5	12	-6448	-17	-20	0	68	-14	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
6	12	-6425	-22	109	0	-209	-16	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
7	12	-6486	-13	-75	0	166	-16	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
8	12	-6418	-22	104	0	-194	-15	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0

9	12	-6478	-13	-79	0	181	-15	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
10	12	-6455	-18	50	0	-95	-17	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
11	12	-6473	-15	-5	0	17	-17	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
12	12	-6430	-19	35	0	-45	-14	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
13	12	-6448	-17	-20	0	68	-14	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
14	12	-6425	-22	109	0	-209	-16	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
15	12	-6486	-13	-75	0	166	-16	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
16	12	-6418	-22	104	0	-194	-15	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
17	12	-6478	-13	-79	0	181	-15	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
18	12	-9390	-104	75	0	-146	-43	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
19	12	-9562	94	-65	0	260	-22	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
20	12	-9382	23	-198	0	2104	-32	6.28	6.28	12.57	12.57	3	0.08	0.00	0.02	0.00	0.00	24.0
37	12	-8994	-175	125	0	-305	-46	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
38	12	-9280	154	-107	0	372	-11	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
39	12	-8980	36	-329	0	3445	-27	6.28	6.28	12.57	12.57	3	0.13	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-8290	-23	19	0	-20	-23	6.28	6.28	12.57	12.57	3	0.00	0.00	0.00	0.00	0.00	24.0
2	25	-6380	-18	50	0	-102	-19	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
3	25	-6398	-15	-5	0	18	-19	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
4	25	-6355	-19	35	0	-49	-16	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
5	25	-6373	-17	-20	0	70	-16	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
6	25	-6350	-22	109	0	-223	-18	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
7	25	-6411	-13	-75	0	175	-17	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
8	25	-6343	-22	104	0	-207	-17	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
9	25	-6403	-13	-79	0	191	-16	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
10	25	-6380	-18	50	0	-102	-19	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
11	25	-6398	-15	-5	0	18	-19	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
12	25	-6355	-19	35	0	-49	-16	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
13	25	-6373	-17	-20	0	70	-16	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
14	25	-6350	-22	109	0	-223	-18	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
15	25	-6411	-13	-75	0	175	-17	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
16	25	-6343	-22	104	0	-207	-17	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
17	25	-6403	-13	-79	0	191	-16	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
18	25	-9293	-104	75	0	-155	-56	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
19	25	-9465	94	-65	0	268	-10	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
20	25	-9285	23	-198	0	2128	-29	6.28	6.28	12.57	12.57	3	0.08	0.00	0.02	0.00	0.00	24.0
37	25	-8897	-175	125	0	-320	-67	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
38	25	-9183	154	-107	0	386	8	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
39	25	-8883	36	-329	0	3486	-22	6.28	6.28	12.57	12.57	3	0.13	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-8192	-23	19	0	-23	-25	6.28	6.28	12.57	12.57	3	0.00	0.00	0.00	0.00	0.00	24.0
2	38	-6305	-18	50	0	-108	-21	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
3	38	-6323	-15	-5	0	18	-21	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
4	38	-6280	-19	35	0	-53	-18	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
5	38	-6298	-17	-20	0	73	-18	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
6	38	-6275	-22	109	0	-236	-21	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
7	38	-6336	-13	-75	0	185	-19	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
8	38	-6268	-22	104	0	-220	-20	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
9	38	-6328	-13	-79	0	201	-18	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
10	38	-6305	-18	50	0	-108	-21	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
11	38	-6323	-15	-5	0	18	-21	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
12	38	-6280	-19	35	0	-53	-18	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
13	38	-6298	-17	-20	0	73	-18	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
14	38	-6275	-22	109	0	-236	-21	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
15	38	-6336	-13	-75	0	185	-19	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
16	38	-6268	-22	104	0	-220	-20	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
17	38	-6328	-13	-79	0	201	-18	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
18	38	-9196	-104	75	0	-165	-69	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
19	38	-9368	94	-65	0	276	1	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
20	38	-9188	23	-198	0	2153	-26	6.28	6.28	12.57	12.57	3	0.08	0.00	0.02	0.00	0.00	24.0
37	38	-8800	-175	125	0	-336	-89	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
38	38	-9086	154	-107	0	399	27	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
39	38	-8786	36	-329	0	3528	-18	6.28	6.28	12.57	12.57	3	0.13	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-8095	-23	19	0	-25	-28	6.28	6.28	12.57	12.57	3	0.00	0.00	0.00	0.00	0.00	24.0
2	50	-6230	-18	50	0	-114	-23	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
3	50	-6248	-15	-5	0	19	-22	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
4	50	-6205	-19	35	0	-58	-21	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
5	50	-6223	-17	-20	0	75	-20	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
6	50	-6200	-22	109	0	-250	-24	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
7	50	-6261	-13	-75	0	194	-20	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
8	50	-6193	-22	104	0	-233	-23	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
9	50	-6253	-13	-79	0	211	-20	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
10	50	-6230	-18	50	0	-114	-23	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
11	50	-6248	-15	-5	0	19	-22	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
12	50	-6205	-19	35	0	-58	-21	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
13	50	-6223	-17	-20	0	75	-20	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
14	50	-6200	-22	109	0	-250	-24	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
15	50	-6261	-13	-75	0	194	-20	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
16	50	-6193	-22	104	0	-233	-23	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
17	50	-6253	-13	-79	0	211	-20	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
18	50	-9098	-104	75	0	-174	-82	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
19	50	-9270	94	-65	0	284	13	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
20	50	-9090	23	-198	0	2178	-23	6.28	6.28	12.57	12.57	3	0.08	0.00	0.02	0.00	0.00	24.0
37	50	-8702	-175	125	0	-352	-111	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
38	50	-8988	154	-107	0	413	47	6.28	6.28	12.57	12.57	3	0.02	0.00	0.01	0.00	0.00	24.0
39	50	-8688	36	-329	0	3569	-14	6.28	6.28	12.57	12.57	3	0.13	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 115 NI 46 NF 42 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 22A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-12710	-442	35	0	-28	-28	6.28	6.28	12.57	12.57	3	0.00	0.01	0.04	0.00	0.00	24.0
2	0	-9781	-368	89	0	-116	-23	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
3	0	-9807	-360	-10	0	18	-22	6.28	6.28	12.57	12.57	2	0.00	0.01	0.03	0.00	0.00	24.0
4	0	-9748	-320	63	0	-62	-21	6.28	6.28	12.57	12.57	2	0.00	0.01	0.03	0.00	0.00	24.0

5	0	-9775	-311	-36	0	72	-20	6.28	6.28	12.57	12.57	2	0.00	0.01	0.03	0.00	0.00	24.0
6	0	-9738	-361	196	0	-253	-24	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
7	0	-9827	-333	-134	0	193	-20	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
8	0	-9729	-346	188	0	-237	-23	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
9	0	-9817	-319	-142	0	209	-20	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
10	0	-9781	-368	89	0	-116	-23	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
11	0	-9807	-360	-10	0	18	-22	6.28	6.28	12.57	12.57	2	0.00	0.01	0.03	0.00	0.00	24.0
12	0	-9748	-320	63	0	-62	-21	6.28	6.28	12.57	12.57	2	0.00	0.01	0.03	0.00	0.00	24.0
13	0	-9775	-311	-36	0	72	-20	6.28	6.28	12.57	12.57	2	0.00	0.01	0.03	0.00	0.00	24.0
14	0	-9738	-361	196	0	-253	-24	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
15	0	-9827	-333	-134	0	193	-20	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
16	0	-9729	-346	188	0	-237	-23	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
17	0	-9817	-319	-142	0	209	-20	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
18	0	-14260	-1116	134	0	-176	-82	6.28	6.28	12.57	12.57	3	0.01	0.02	0.09	0.00	0.00	24.0
19	0	-14580	-99	-115	0	268	13	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
20	0	-14250	-497	-330	0	1954	-23	6.28	6.28	12.57	12.57	3	0.07	0.01	0.04	0.00	0.00	24.0
37	0	-13630	-1399	224	0	-347	-111	6.28	6.28	12.57	12.57	3	0.01	0.03	0.11	0.00	0.00	24.0
38	0	-14150	295	-190	0	394	47	6.28	6.28	12.57	12.57	3	0.01	0.01	0.02	0.00	0.00	24.0
39	0	-13610	-369	-548	0	3204	-14	6.28	6.28	12.57	12.57	3	0.11	0.01	0.05	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-12612	-442	35	0	-33	-83	6.28	6.28	12.57	12.57	3	0.00	0.01	0.04	0.00	0.00	24.0
2	12	-9706	-368	89	0	-127	-69	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
3	12	-9732	-360	-10	0	19	-67	6.28	6.28	12.57	12.57	2	0.00	0.01	0.03	0.00	0.00	24.0
4	12	-9673	-320	63	0	-70	-61	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
5	12	-9700	-311	-36	0	77	-59	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
6	12	-9663	-361	196	0	-277	-69	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
7	12	-9752	-333	-134	0	210	-62	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
8	12	-9654	-346	188	0	-260	-66	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
9	12	-9742	-319	-142	0	227	-59	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
10	12	-9706	-368	89	0	-127	-69	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
11	12	-9732	-360	-10	0	19	-67	6.28	6.28	12.57	12.57	2	0.00	0.01	0.03	0.00	0.00	24.0
12	12	-9673	-320	63	0	-70	-61	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
13	12	-9700	-311	-36	0	77	-59	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
14	12	-9663	-361	196	0	-277	-69	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
15	12	-9752	-333	-134	0	210	-62	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
16	12	-9654	-346	188	0	-260	-66	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
17	12	-9742	-319	-142	0	227	-59	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
18	12	-14162	-1116	134	0	-192	-221	6.28	6.28	12.57	12.57	3	0.01	0.02	0.10	0.00	0.00	24.0
19	12	-14482	-99	-115	0	283	1	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
20	12	-14152	-497	-330	0	1995	-85	6.28	6.28	12.57	12.57	3	0.07	0.01	0.04	0.00	0.00	24.0
37	12	-13532	-1399	224	0	-375	-286	6.28	6.28	12.57	12.57	3	0.02	0.03	0.11	0.00	0.00	24.0
38	12	-14052	295	-190	0	417	84	6.28	6.28	12.57	12.57	3	0.02	0.01	0.02	0.00	0.00	24.0
39	12	-13512	-369	-548	0	3273	-60	6.28	6.28	12.57	12.57	3	0.12	0.01	0.05	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-12515	-442	35	0	-37	-139	6.28	6.28	12.57	12.57	3	0.01	0.01	0.04	0.00	0.00	24.0
2	25	-9631	-368	89	0	-138	-115	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
3	25	-9657	-360	-10	0	21	-112	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
4	25	-9598	-320	63	0	-77	-101	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
5	25	-9625	-311	-36	0	81	-98	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
6	25	-9588	-361	196	0	-302	-114	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
7	25	-9677	-333	-134	0	227	-104	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
8	25	-9579	-346	188	0	-284	-109	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
9	25	-9667	-319	-142	0	245	-99	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
10	25	-9631	-368	89	0	-138	-115	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
11	25	-9657	-360	-10	0	21	-112	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
12	25	-9598	-320	63	0	-77	-101	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
13	25	-9625	-311	-36	0	81	-98	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
14	25	-9588	-361	196	0	-302	-114	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
15	25	-9677	-333	-134	0	227	-104	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
16	25	-9579	-346	188	0	-284	-109	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
17	25	-9667	-319	-142	0	245	-99	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
18	25	-14065	-1116	134	0	-209	-361	6.28	6.28	12.57	12.57	3	0.02	0.02	0.10	0.00	0.00	24.0
19	25	-14385	-99	-115	0	297	-12	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
20	25	-14055	-497	-330	0	2037	-147	6.28	6.28	12.57	12.57	3	0.07	0.01	0.04	0.00	0.00	24.0
37	25	-13435	-1399	224	0	-403	-461	6.28	6.28	12.57	12.57	3	0.03	0.03	0.13	0.00	0.00	24.0
38	25	-13955	295	-190	0	441	120	6.28	6.28	12.57	12.57	3	0.02	0.01	0.02	0.00	0.00	24.0
39	25	-13415	-369	-548	0	3341	-106	6.28	6.28	12.57	12.57	3	0.12	0.01	0.05	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-12418	-442	35	0	-41	-194	6.28	6.28	12.57	12.57	3	0.01	0.01	0.04	0.00	0.00	24.0
2	38	-9556	-368	89	0	-149	-161	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
3	38	-9582	-360	-10	0	22	-157	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
4	38	-9523	-320	63	0	-85	-141	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
5	38	-9550	-311	-36	0	86	-137	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
6	38	-9513	-361	196	0	-326	-159	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
7	38	-9602	-333	-134	0	244	-145	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
8	38	-9504	-346	188	0	-307	-153	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
9	38	-9592	-319	-142	0	263	-139	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
10	38	-9556	-368	89	0	-149	-161	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
11	38	-9582	-360	-10	0	22	-157	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
12	38	-9523	-320	63	0	-85	-141	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
13	38	-9550	-311	-36	0	86	-137	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
14	38	-9513	-361	196	0	-326	-159	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
15	38	-9602	-333	-134	0	244	-145	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
16	38	-9504	-346	188	0	-307	-153	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
17	38	-9592	-319	-142	0	263	-139	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
18	38	-13968	-1116	134	0	-226	-500	6.28	6.28	12.57	12.57	3	0.03	0.02	0.10	0.00	0.00	24.0
19	38	-14288	-99	-115	0	311	-24	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
20	38	-13958	-497	-330	0	2078	-210	6.28	6.28	12.57	12.57	3	0.08	0.01	0.04	0.00	0.00	24.0
37	38	-13338	-1399	224	0	-431	-636	6.28	6.28	12.57	12.57	3	0.04	0.03	0.13	0.00	0.00	24.0
38	38	-13858	295	-190	0	465	157	6.28	6.28	12.57	12.57	3	0.02	0.01	0.02	0.00	0.00	24.0
39	38	-13318	-369	-548	0	3410	-152	6.28	6.28	12.57	12.57	3	0.12	0.01	0.05	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-12320	-442	35	0	-46	-249	6.28	6.28	12.57	12.57	3	0.01	0.01	0.04	0.00	0.00	24.0
2	50	-9481	-368	89	0	-160	-207	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
3	50	-9507	-360	-10	0	23	-202	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
4	50	-9448	-320	63	0	-93	-181	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
5	50	-9475	-311	-36	0	90	-176	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
6	50	-9438	-361	196	0	-351	-204	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
7	50	-9527	-333	-134	0	260	-187	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
8	50	-9429	-346	188	0	-331	-196	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
9	50	-9517	-319	-142	0	280	-179	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
10	50	-9481	-368	89	0	-160	-207	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0

11	50	-9507	-360	-10	0	23	-202	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
12	50	-9448	-320	63	0	-93	-181	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
13	50	-9475	-311	-36	0	90	-176	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
14	50	-9438	-361	196	0	-351	-204	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
15	50	-9527	-333	-134	0	260	-187	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
16	50	-9429	-346	188	0	-331	-196	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
17	50	-9517	-319	-142	0	280	-179	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
18	50	-13870	-1116	134	0	-243	-640	6.28	6.28	12.57	12.57	3	0.04	0.02	0.10	0.00	0.00	24.0
19	50	-14190	-99	-115	0	326	-37	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
20	50	-13860	-497	-330	0	2119	-272	6.28	6.28	12.57	12.57	3	0.08	0.01	0.04	0.00	0.00	24.0
37	50	-13240	-1399	224	0	-459	-811	6.28	6.28	12.57	12.57	3	0.05	0.03	0.13	0.00	0.00	24.0
38	50	-13760	295	-190	0	489	194	6.28	6.28	12.57	12.57	3	0.02	0.01	0.02	0.00	0.00	24.0
39	50	-13220	-369	-548	0	3478	-198	6.28	6.28	12.57	12.57	3	0.12	0.01	0.05	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 116 NI 216 NF 482 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 32
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-3621	-839	141	0	148	455	6.28	6.28	12.57	12.57	3	0.03	0.02	0.09	0.00	0.00	24.0
2	0	-2748	-726	234	0	135	405	6.28	6.28	12.57	12.57	2	0.03	0.01	0.08	0.00	0.00	24.0
3	0	-2846	-699	76	0	130	395	6.28	6.28	12.57	12.57	2	0.03	0.01	0.07	0.00	0.00	24.0
4	0	-2725	-591	141	0	98	305	6.28	6.28	12.57	12.57	2	0.02	0.01	0.06	0.00	0.00	24.0
5	0	-2822	-565	-16	0	92	295	6.28	6.28	12.57	12.57	2	0.02	0.01	0.06	0.00	0.00	24.0
6	0	-2626	-709	385	0	128	383	6.28	6.28	12.57	12.57	2	0.03	0.01	0.07	0.00	0.00	24.0
7	0	-2951	-621	-139	0	110	347	6.28	6.28	12.57	12.57	2	0.03	0.01	0.06	0.00	0.00	24.0
8	0	-2619	-669	357	0	117	353	6.28	6.28	12.57	12.57	2	0.03	0.01	0.07	0.00	0.00	24.0
9	0	-2944	-581	-167	0	99	317	6.28	6.28	12.57	12.57	2	0.02	0.01	0.06	0.00	0.00	24.0
10	0	-2748	-726	234	0	135	405	6.28	6.28	12.57	12.57	2	0.03	0.01	0.08	0.00	0.00	24.0
11	0	-2846	-699	76	0	130	395	6.28	6.28	12.57	12.57	2	0.03	0.01	0.07	0.00	0.00	24.0
12	0	-2725	-591	141	0	98	305	6.28	6.28	12.57	12.57	2	0.02	0.01	0.06	0.00	0.00	24.0
13	0	-2822	-565	-16	0	92	295	6.28	6.28	12.57	12.57	2	0.02	0.01	0.06	0.00	0.00	24.0
14	0	-2626	-709	385	0	128	383	6.28	6.28	12.57	12.57	2	0.03	0.01	0.07	0.00	0.00	24.0
15	0	-2951	-621	-139	0	110	347	6.28	6.28	12.57	12.57	2	0.03	0.01	0.06	0.00	0.00	24.0
16	0	-2619	-669	357	0	117	353	6.28	6.28	12.57	12.57	2	0.03	0.01	0.07	0.00	0.00	24.0
17	0	-2944	-581	-167	0	99	317	6.28	6.28	12.57	12.57	2	0.02	0.01	0.06	0.00	0.00	24.0
18	0	-3425	-1826	817	0	273	1115	6.28	6.28	12.57	12.57	3	0.07	0.03	0.19	0.00	0.00	24.0
19	0	-3612	-881	214	0	96	604	6.28	6.28	12.57	12.57	3	0.04	0.02	0.09	0.00	0.00	24.0
20	0	-3172	-764	-1027	0	-557	652	6.28	6.28	12.57	12.57	3	0.04	0.02	0.11	0.00	0.00	24.0
37	0	-3404	-1973	893	0	320	1153	6.28	6.28	12.57	12.57	3	0.07	0.04	0.20	0.00	0.00	24.0
38	0	-3716	-398	-111	0	24	301	6.28	6.28	12.57	12.57	3	0.02	0.01	0.04	0.00	0.00	24.0
39	0	-2983	-202	-2180	0	-1063	382	6.28	6.28	12.57	12.57	3	0.05	0.04	0.24	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-3524	-839	141	0	130	350	6.28	6.28	12.57	12.57	3	0.02	0.02	0.09	0.00	0.00	24.0
2	12	-2673	-726	234	0	106	315	6.28	6.28	12.57	12.57	2	0.02	0.01	0.08	0.00	0.00	24.0
3	12	-2771	-699	76	0	120	307	6.28	6.28	12.57	12.57	2	0.02	0.01	0.07	0.00	0.00	24.0
4	12	-2650	-591	141	0	80	231	6.28	6.28	12.57	12.57	2	0.02	0.01	0.06	0.00	0.00	24.0
5	12	-2747	-565	-16	0	94	224	6.28	6.28	12.57	12.57	2	0.02	0.01	0.06	0.00	0.00	24.0
6	12	-2551	-709	385	0	80	294	6.28	6.28	12.57	12.57	2	0.02	0.01	0.07	0.00	0.00	24.0
7	12	-2876	-621	-139	0	128	270	6.28	6.28	12.57	12.57	2	0.02	0.01	0.06	0.00	0.00	24.0
8	12	-2544	-669	357	0	72	269	6.28	6.28	12.57	12.57	2	0.02	0.01	0.07	0.00	0.00	24.0
9	12	-2869	-581	-167	0	120	245	6.28	6.28	12.57	12.57	2	0.02	0.01	0.06	0.00	0.00	24.0
10	12	-2673	-726	234	0	106	315	6.28	6.28	12.57	12.57	2	0.02	0.01	0.08	0.00	0.00	24.0
11	12	-2771	-699	76	0	120	307	6.28	6.28	12.57	12.57	2	0.02	0.01	0.07	0.00	0.00	24.0
12	12	-2650	-591	141	0	80	231	6.28	6.28	12.57	12.57	2	0.02	0.01	0.06	0.00	0.00	24.0
13	12	-2747	-565	-16	0	94	224	6.28	6.28	12.57	12.57	2	0.02	0.01	0.06	0.00	0.00	24.0
14	12	-2551	-709	385	0	80	294	6.28	6.28	12.57	12.57	2	0.02	0.01	0.07	0.00	0.00	24.0
15	12	-2876	-621	-139	0	128	270	6.28	6.28	12.57	12.57	2	0.02	0.01	0.06	0.00	0.00	24.0
16	12	-2544	-669	357	0	72	269	6.28	6.28	12.57	12.57	2	0.02	0.01	0.07	0.00	0.00	24.0
17	12	-2869	-581	-167	0	120	245	6.28	6.28	12.57	12.57	2	0.02	0.01	0.06	0.00	0.00	24.0
18	12	-3328	-1826	817	0	171	887	6.28	6.28	12.57	12.57	3	0.05	0.03	0.19	0.00	0.00	24.0
19	12	-3514	-881	214	0	69	494	6.28	6.28	12.57	12.57	3	0.03	0.02	0.09	0.00	0.00	24.0
20	12	-3074	-764	-1027	0	-429	557	6.28	6.28	12.57	12.57	3	0.04	0.02	0.11	0.00	0.00	24.0
37	12	-3306	-1973	893	0	208	906	6.28	6.28	12.57	12.57	3	0.05	0.04	0.20	0.00	0.00	24.0
38	12	-3618	-398	-111	0	38	252	6.28	6.28	12.57	12.57	3	0.02	0.01	0.04	0.00	0.00	24.0
39	12	-2886	-202	-2180	0	-791	357	6.28	6.28	12.57	12.57	3	0.04	0.04	0.24	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-3426	-839	141	0	112	245	6.28	6.28	12.57	12.57	3	0.01	0.02	0.09	0.00	0.00	24.0
2	25	-2598	-726	234	0	76	224	6.28	6.28	12.57	12.57	2	0.02	0.01	0.08	0.00	0.00	24.0
3	25	-2696	-699	76	0	111	220	6.28	6.28	12.57	12.57	2	0.02	0.01	0.07	0.00	0.00	24.0
4	25	-2575	-591	141	0	62	158	6.28	6.28	12.57	12.57	2	0.01	0.01	0.06	0.00	0.00	24.0
5	25	-2672	-565	-16	0	96	154	6.28	6.28	12.57	12.57	2	0.01	0.01	0.06	0.00	0.00	24.0
6	25	-2476	-709	385	0	32	205	6.28	6.28	12.57	12.57	2	0.01	0.01	0.07	0.00	0.00	24.0
7	25	-2801	-621	-139	0	145	192	6.28	6.28	12.57	12.57	2	0.02	0.01	0.06	0.00	0.00	24.0
8	25	-2469	-669	357	0	27	185	6.28	6.28	12.57	12.57	2	0.01	0.01	0.07	0.00	0.00	24.0
9	25	-2794	-581	-167	0	141	172	6.28	6.28	12.57	12.57	2	0.02	0.01	0.06	0.00	0.00	24.0
10	25	-2598	-726	234	0	76	224	6.28	6.28	12.57	12.57	2	0.02	0.01	0.08	0.00	0.00	24.0
11	25	-2696	-699	76	0	111	220	6.28	6.28	12.57	12.57	2	0.02	0.01	0.07	0.00	0.00	24.0
12	25	-2575	-591	141	0	62	158	6.28	6.28	12.57	12.57	2	0.01	0.01	0.06	0.00	0.00	24.0
13	25	-2672	-565	-16	0	96	154	6.28	6.28	12.57	12.57	2	0.01	0.01	0.06	0.00	0.00	24.0
14	25	-2476	-709	385	0	32	205	6.28	6.28	12.57	12.57	2	0.01	0.01	0.07	0.00	0.00	24.0
15	25	-2801	-621	-139	0	145	192	6.28	6.28	12.57	12.57	2	0.02	0.01	0.06	0.00	0.00	24.0
16	25	-2469	-669	357	0	27	185	6.28	6.28	12.57	12.57	2	0.01	0.01	0.07	0.00	0.00	24.0
17	25	-2794	-581	-167	0	141	172	6.28	6.28	12.57	12.57	2	0.02	0.01	0.06	0.00	0.00	24.0
18	25	-3230	-1826	817	0	69	658	6.28	6.28	12.57	12.57	3	0.04	0.03	0.19	0.00	0.00	24.0
19	25	-3417	-881	214	0	42	384	6.28	6.28	12.57	12.57	3	0.02	0.02	0.09	0.00	0.00	24.0
20	25	-2977	-764	-1027	0	-300	461	6.28	6.28	12.57	12.57	3	0.03	0.02	0.11	0.00	0.00	24.0
37	25	-3209	-1973	893	0	97	660	6.28	6.28	12.57	12.57	3	0.04	0.04	0.20	0.00	0.00	24.0
38	25	-3521	-398	-111	0	52	202	6.28	6.28	12.57	12.57	3	0.01	0.01	0.04	0.00	0.00	24.0
39	25	-2788	-202	-2180	0	-518	332	6.28	6.28	12.57	12.57	3	0.03	0.04	0.24	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-3328	-839	141	0	95	140	6.28	6.28	12.57	12.57	3	0.01	0.02	0.09	0.00	0.00	24.0
2	38	-2523	-726	234	0	47	133	6.28	6.28	12.57	12.57	2	0.01	0.01	0.08	0.00	0.00	24.0
3	38	-2621	-699	76	0	101	133	6.28	6.28	12.57	12.57	2	0.01	0.01	0.07	0.00	0.00	24.0
4	38	-2500	-591	141	0	45	84	6.28	6.28	12.57	12.57	2	0.01	0.01	0.06	0.00	0.00	24.0
5	38	-2597	-565	-16	0	98	83	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
6	38	-2401	-709	385	0	-16	117	6.28	6.28	12.57	12.57	2	0.01	0.01	0.07	0.00	0.00	24.0

7	38	-2726	-621	-139	0	163	114	6.28	6.28	12.57	12.57	2	0.01	0.01	0.06	0.00	0.00	24.0
8	38	-2394	-669	357	0	-17	102	6.28	6.28	12.57	12.57	2	0.01	0.01	0.07	0.00	0.00	24.0
9	38	-2719	-581	-167	0	162	99	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
10	38	-2523	-726	234	0	47	133	6.28	6.28	12.57	12.57	2	0.01	0.01	0.08	0.00	0.00	24.0
11	38	-2621	-699	76	0	101	133	6.28	6.28	12.57	12.57	2	0.01	0.01	0.07	0.00	0.00	24.0
12	38	-2500	-591	141	0	45	84	6.28	6.28	12.57	12.57	2	0.01	0.01	0.06	0.00	0.00	24.0
13	38	-2597	-565	-16	0	98	83	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
14	38	-2401	-709	385	0	-16	117	6.28	6.28	12.57	12.57	2	0.01	0.01	0.07	0.00	0.00	24.0
15	38	-2726	-621	-139	0	163	114	6.28	6.28	12.57	12.57	2	0.01	0.01	0.06	0.00	0.00	24.0
16	38	-2394	-669	357	0	-17	102	6.28	6.28	12.57	12.57	2	0.01	0.01	0.07	0.00	0.00	24.0
17	38	-2719	-581	-167	0	162	99	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
18	38	-3132	-1826	817	0	-33	430	6.28	6.28	12.57	12.57	3	0.03	0.03	0.19	0.00	0.00	24.0
19	38	-3320	-881	214	0	15	274	6.28	6.28	12.57	12.57	3	0.02	0.02	0.09	0.00	0.00	24.0
20	38	-2880	-764	-1027	0	-172	366	6.28	6.28	12.57	12.57	3	0.02	0.02	0.11	0.00	0.00	24.0
37	38	-3112	-1973	893	0	-15	413	6.28	6.28	12.57	12.57	3	0.02	0.04	0.20	0.00	0.00	24.0
38	38	-3424	-398	-111	0	66	152	6.28	6.28	12.57	12.57	3	0.01	0.01	0.04	0.00	0.00	24.0
39	38	-2690	-202	-2180	0	-246	306	6.28	6.28	12.57	12.57	3	0.02	0.04	0.24	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-3231	-839	141	0	77	36	6.28	6.28	12.57	12.57	3	0.00	0.02	0.08	0.00	0.00	24.0
2	50	-2448	-726	234	0	18	43	6.28	6.28	12.57	12.57	2	0.00	0.01	0.08	0.00	0.00	24.0
3	50	-2546	-699	76	0	91	45	6.28	6.28	12.57	12.57	2	0.01	0.01	0.06	0.00	0.00	24.0
4	50	-2425	-591	141	0	27	10	6.28	6.28	12.57	12.57	2	0.00	0.01	0.05	0.00	0.00	24.0
5	50	-2522	-565	-16	0	100	12	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
6	50	-2326	-709	385	0	-64	28	6.28	6.28	12.57	12.57	2	0.00	0.01	0.07	0.00	0.00	24.0
7	50	-2651	-621	-139	0	180	37	6.28	6.28	12.57	12.57	2	0.01	0.01	0.06	0.00	0.00	24.0
8	50	-2319	-669	357	0	-62	18	6.28	6.28	12.57	12.57	2	0.00	0.01	0.06	0.00	0.00	24.0
9	50	-2644	-581	-167	0	183	27	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
10	50	-2448	-726	234	0	18	43	6.28	6.28	12.57	12.57	2	0.00	0.01	0.08	0.00	0.00	24.0
11	50	-2546	-699	76	0	91	45	6.28	6.28	12.57	12.57	2	0.01	0.01	0.06	0.00	0.00	24.0
12	50	-2425	-591	141	0	27	10	6.28	6.28	12.57	12.57	2	0.00	0.01	0.05	0.00	0.00	24.0
13	50	-2522	-565	-16	0	100	12	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
14	50	-2326	-709	385	0	-64	28	6.28	6.28	12.57	12.57	2	0.00	0.01	0.07	0.00	0.00	24.0
15	50	-2651	-621	-139	0	180	37	6.28	6.28	12.57	12.57	2	0.01	0.01	0.06	0.00	0.00	24.0
16	50	-2319	-669	357	0	-62	18	6.28	6.28	12.57	12.57	2	0.00	0.01	0.06	0.00	0.00	24.0
17	50	-2644	-581	-167	0	183	27	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
18	50	-3035	-1826	817	0	-135	202	6.28	6.28	12.57	12.57	3	0.01	0.03	0.19	0.00	0.00	24.0
19	50	-3222	-881	214	0	-12	163	6.28	6.28	12.57	12.57	3	0.01	0.02	0.09	0.00	0.00	24.0
20	50	-2782	-764	-1027	0	-44	270	6.28	6.28	12.57	12.57	3	0.02	0.02	0.11	0.00	0.00	24.0
37	50	-3014	-1973	893	0	-127	166	6.28	6.28	12.57	12.57	3	0.01	0.04	0.20	0.00	0.00	24.0
38	50	-3326	-398	-111	0	80	103	6.28	6.28	12.57	12.57	3	0.01	0.01	0.04	0.00	0.00	24.0
39	50	-2593	-202	-2180	0	27	281	6.28	6.28	12.57	12.57	3	0.02	0.04	0.24	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 117 NI 482 NF 33 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 32A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-5267	292	159	0	155	-176	6.28	6.28	12.57	12.57	3	0.01	0.01	0.03	0.00	0.00	24.0
2	0	-4096	272	216	0	73	-141	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
3	0	-4193	283	41	0	167	-140	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
4	0	-3909	165	204	0	72	-131	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
5	0	-4006	176	28	0	166	-130	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
6	0	-3917	222	417	0	-38	-139	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
7	0	-4241	258	-168	0	277	-135	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
8	0	-3861	190	413	0	-38	-136	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
9	0	-4185	226	-172	0	277	-132	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
10	0	-4096	272	216	0	73	-141	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
11	0	-4193	283	41	0	167	-140	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
12	0	-3909	165	204	0	72	-131	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
13	0	-4006	176	28	0	166	-130	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
14	0	-3917	222	417	0	-38	-139	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
15	0	-4241	258	-168	0	277	-135	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
16	0	-3861	190	413	0	-38	-136	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
17	0	-4185	226	-172	0	277	-132	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
18	0	-6015	719	474	0	31	-314	6.28	6.28	12.57	12.57	3	0.02	0.01	0.07	0.00	0.00	24.0
19	0	-5718	720	297	0	113	-110	6.28	6.28	12.57	12.57	3	0.01	0.01	0.06	0.00	0.00	24.0
20	0	-5582	773	-31	0	427	-160	6.28	6.28	12.57	12.57	3	0.02	0.01	0.07	0.00	0.00	24.0
37	0	-5930	580	458	0	33	-370	6.28	6.28	12.57	12.57	3	0.02	0.01	0.06	0.00	0.00	24.0
38	0	-5435	581	162	0	168	-31	6.28	6.28	12.57	12.57	3	0.01	0.01	0.05	0.00	0.00	24.0
39	0	-5209	669	-384	0	693	-114	6.28	6.28	12.57	12.57	3	0.03	0.01	0.06	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-5170	292	159	0	135	-140	6.28	6.28	12.57	12.57	3	0.01	0.01	0.03	0.00	0.00	24.0
2	12	-4021	272	216	0	46	-107	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
3	12	-4118	283	41	0	162	-104	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
4	12	-3834	165	204	0	46	-110	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
5	12	-3931	176	28	0	162	-108	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
6	12	-3842	222	417	0	-90	-111	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
7	12	-4166	258	-168	0	298	-103	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
8	12	-3786	190	413	0	-90	-112	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
9	12	-4110	226	-172	0	298	-104	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
10	12	-4021	272	216	0	46	-107	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
11	12	-4118	283	41	0	162	-104	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
12	12	-3834	165	204	0	46	-110	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
13	12	-3931	176	28	0	162	-108	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
14	12	-3842	222	417	0	-90	-111	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
15	12	-4166	258	-168	0	298	-103	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
16	12	-3786	190	413	0	-90	-112	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
17	12	-4110	226	-172	0	298	-104	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
18	12	-5918	719	474	0	-28	-224	6.28	6.28	12.57	12.57	3	0.01	0.01	0.07	0.00	0.00	24.0
19	12	-5620	720	297	0	76	-20	6.28	6.28	12.57	12.57	3	0.00	0.01	0.06	0.00	0.00	24.0
20	12	-5484	773	-31	0	431	-64	6.28	6.28	12.57	12.57	3	0.02	0.01	0.07	0.00	0.00	24.0
37	12	-5832	580	458	0	-24	-298	6.28	6.28	12.57	12.57	3	0.02	0.01	0.06	0.00	0.00	24.0
38	12	-5338	581	162	0	148	42	6.28	6.28	12.57	12.57	3	0.01	0.01	0.05	0.00	0.00	24.0
39	12	-5112	669	-384	0	741	-30	6.28	6.28	12.57	12.57	3	0.03	0.01	0.06	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-5072	292	159	0	115	-103	6.28	6.28	12.57	12.57	3	0.01	0.01	0.03	0.00	0.00	24.0
2	25	-3946	272	216	0	19	-73	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0

3	25	-4043	283	41	0	157	-69	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
4	25	-3759	165	204	0	21	-90	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
5	25	-3856	176	28	0	159	-86	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
6	25	-3767	222	417	0	-142	-83	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
7	25	-4091	258	-168	0	319	-70	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
8	25	-3711	190	413	0	-141	-88	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
9	25	-4035	226	-172	0	320	-75	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
10	25	-3946	272	216	0	19	-73	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
11	25	-4043	283	41	0	157	-69	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
12	25	-3759	165	204	0	21	-90	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
13	25	-3856	176	28	0	159	-86	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
14	25	-3767	222	417	0	-142	-83	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
15	25	-4091	258	-168	0	319	-70	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
16	25	-3711	190	413	0	-141	-88	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
17	25	-4035	226	-172	0	320	-75	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
18	25	-5820	719	474	0	-87	-134	6.28	6.28	12.57	12.57	3	0.01	0.01	0.07	0.00	0.00	24.0
19	25	-5523	720	297	0	39	70	6.28	6.28	12.57	12.57	3	0.00	0.01	0.07	0.00	0.00	24.0
20	25	-5387	773	-31	0	435	33	6.28	6.28	12.57	12.57	3	0.02	0.01	0.07	0.00	0.00	24.0
37	25	-5735	580	458	0	-82	-225	6.28	6.28	12.57	12.57	3	0.01	0.01	0.06	0.00	0.00	24.0
38	25	-5240	581	162	0	128	115	6.28	6.28	12.57	12.57	3	0.01	0.01	0.05	0.00	0.00	24.0
39	25	-5014	669	-384	0	789	54	6.28	6.28	12.57	12.57	3	0.03	0.01	0.06	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-4974	292	159	0	96	-67	6.28	6.28	12.57	12.57	3	0.01	0.01	0.03	0.00	0.00	24.0
2	38	-3871	272	216	0	-8	-39	6.28	6.28	12.57	12.57	2	0.00	0.01	0.03	0.00	0.00	24.0
3	38	-3968	283	41	0	152	-34	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
4	38	-3684	165	204	0	-5	-69	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
5	38	-3781	176	28	0	156	-64	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
6	38	-3692	222	417	0	-194	-56	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
7	38	-4016	258	-168	0	340	-38	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
8	38	-3636	190	413	0	-193	-65	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
9	38	-3960	226	-172	0	341	-47	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
10	38	-3871	272	216	0	-8	-39	6.28	6.28	12.57	12.57	2	0.00	0.01	0.03	0.00	0.00	24.0
11	38	-3968	283	41	0	152	-34	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
12	38	-3684	165	204	0	-5	-69	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
13	38	-3781	176	28	0	156	-64	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
14	38	-3692	222	417	0	-194	-56	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
15	38	-4016	258	-168	0	340	-38	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
16	38	-3636	190	413	0	-193	-65	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
17	38	-3960	226	-172	0	341	-47	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
18	38	-5722	719	474	0	-146	-44	6.28	6.28	12.57	12.57	3	0.01	0.01	0.06	0.00	0.00	24.0
19	38	-5426	720	297	0	1	160	6.28	6.28	12.57	12.57	3	0.01	0.01	0.07	0.00	0.00	24.0
20	38	-5290	773	-31	0	439	130	6.28	6.28	12.57	12.57	3	0.02	0.01	0.07	0.00	0.00	24.0
37	38	-5638	580	458	0	-139	-153	6.28	6.28	12.57	12.57	3	0.01	0.01	0.06	0.00	0.00	24.0
38	38	-5142	581	162	0	108	187	6.28	6.28	12.57	12.57	3	0.01	0.01	0.06	0.00	0.00	24.0
39	38	-4916	669	-384	0	837	137	6.28	6.28	12.57	12.57	3	0.03	0.01	0.06	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-4877	292	159	0	76	-30	6.28	6.28	12.57	12.57	3	0.00	0.01	0.03	0.00	0.00	24.0
2	50	-3796	272	216	0	-35	-5	6.28	6.28	12.57	12.57	2	0.00	0.01	0.02	0.00	0.00	24.0
3	50	-3893	283	41	0	147	2	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
4	50	-3609	165	204	0	-30	-48	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
5	50	-3706	176	28	0	152	-42	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
6	50	-3617	222	417	0	-246	-28	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
7	50	-3941	258	-168	0	361	-6	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
8	50	-3561	190	413	0	-244	-41	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
9	50	-3885	226	-172	0	363	-19	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
10	50	-3796	272	216	0	-35	-5	6.28	6.28	12.57	12.57	2	0.00	0.01	0.02	0.00	0.00	24.0
11	50	-3893	283	41	0	147	2	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
12	50	-3609	165	204	0	-30	-48	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
13	50	-3706	176	28	0	152	-42	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
14	50	-3617	222	417	0	-246	-28	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
15	50	-3941	258	-168	0	361	-6	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
16	50	-3561	190	413	0	-244	-41	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
17	50	-3885	226	-172	0	363	-19	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
18	50	-5625	719	474	0	-206	46	6.28	6.28	12.57	12.57	3	0.01	0.01	0.06	0.00	0.00	24.0
19	50	-5328	720	297	0	-36	250	6.28	6.28	12.57	12.57	3	0.01	0.01	0.07	0.00	0.00	24.0
20	50	-5192	773	-31	0	443	226	6.28	6.28	12.57	12.57	3	0.02	0.01	0.07	0.00	0.00	24.0
37	50	-5540	580	458	0	-196	-80	6.28	6.28	12.57	12.57	3	0.01	0.01	0.05	0.00	0.00	24.0
38	50	-5045	581	162	0	87	260	6.28	6.28	12.57	12.57	3	0.02	0.01	0.06	0.00	0.00	24.0
39	50	-4819	669	-384	0	885	221	6.28	6.28	12.57	12.57	3	0.04	0.01	0.06	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 118 NI 803 NF 821 SEZ. Rp B= 0.400 H= 0.600 (pilastro)
PIL. NUM. 26
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-5781	1466	180	0	55	43	12.57	12.57	6.28	6.28	3	0.00	0.03	0.15	0.00	0.00	24.0
2	0	-4472	1471	192	0	51	-529	12.57	12.57	6.28	6.28	2	0.03	0.03	0.16	0.00	0.00	24.0
3	0	-4472	1477	106	0	42	-531	12.57	12.57	6.28	6.28	2	0.03	0.03	0.16	0.00	0.00	24.0
4	0	-4423	778	171	0	43	598	12.57	12.57	6.28	6.28	2	0.03	0.01	0.08	0.00	0.00	24.0
5	0	-4422	784	84	0	33	595	12.57	12.57	6.28	6.28	2	0.03	0.01	0.08	0.00	0.00	24.0
6	0	-4456	1222	286	0	60	-132	12.57	12.57	6.28	6.28	2	0.01	0.02	0.13	0.00	0.00	24.0
7	0	-4453	1241	-3	0	28	-139	12.57	12.57	6.28	6.28	2	0.01	0.02	0.13	0.00	0.00	24.0
8	0	-4441	1014	280	0	57	206	12.57	12.57	6.28	6.28	2	0.01	0.02	0.11	0.00	0.00	24.0
9	0	-4438	1033	-10	0	25	199	12.57	12.57	6.28	6.28	2	0.01	0.02	0.11	0.00	0.00	24.0
10	0	-4472	1471	192	0	51	-529	12.57	12.57	6.28	6.28	2	0.03	0.03	0.16	0.00	0.00	24.0
11	0	-4472	1477	106	0	42	-531	12.57	12.57	6.28	6.28	2	0.03	0.03	0.16	0.00	0.00	24.0
12	0	-4423	778	171	0	43	598	12.57	12.57	6.28	6.28	2	0.03	0.01	0.08	0.00	0.00	24.0
13	0	-4422	784	84	0	33	595	12.57	12.57	6.28	6.28	2	0.03	0.01	0.08	0.00	0.00	24.0
14	0	-4456	1222	286	0	60	-132	12.57	12.57	6.28	6.28	2	0.01	0.02	0.13	0.00	0.00	24.0
15	0	-4453	1241	-3	0	28	-139	12.57	12.57	6.28	6.28	2	0.01	0.02	0.13	0.00	0.00	24.0
16	0	-4441	1014	280	0	57	206	12.57	12.57	6.28	6.28	2	0.01	0.02	0.11	0.00	0.00	24.0
17	0	-4438	1033	-10	0	25	199	12.57	12.57	6.28	6.28	2	0.01	0.02	0.11	0.00	0.00	24.0
18	0	-6087	4589	512	0	107	-2417	12.57	12.57	6.28	6.28	3	0.09	0.08	0.48	0.00	0.00	24.0
19	0	-6270	1482	393	0	75	1492	12.57	12.57	6.28	6.28	3	0.06	0.03	0.16	0.00	0.00	24.0
20	0	-6141	2809	228	0	67	-381	12.57	12.57	6.28	6.28	3	0.01	0.05	0.30	0.00	0.00	24.0
37	0	-5873	5111	465	0	106	-3553	12.57	12.57	6.28	6.28	3	0.13	0.09	0.54	0.00	0.00	24.0
38	0	-6177	-68	266	0	52	2962	12.57	12.57	6.28	6.28	3	0.11	0.00	0.02	0.00	0.00	24.0
39	0	-5962	2144	-9	0	40	-161	12.57	12.57	6.28	6.28	3	0.01	0.04	0.23	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-5684	1466	180	0	33	226	12.57	12.57	6.28	6.28	3	0.01	0.03	0.15	0.00	0.00	24.0
2	12	-4397	1471	192	0	27	-345	12.57	12.57	6.28	6.28	2	0.02	0.03	0.16	0.00	0.00	24.0
3	12	-4397	1477	106	0	29	-346	12.57	12.57	6.28	6.28	2	0.02	0.03	0.16	0.00	0.00	24.0
4	12	-4348	778	171	0	22	695	12.57	12.57	6.28	6.28	2	0.04	0.01	0.08	0.00	0.00	24.0
5	12	-4347	784	84	0	23	693	12.57	12.57	6.28	6.28	2	0.04	0.01	0.08	0.00	0.00	24.0
6	12	-4381	1222	286	0	24	21	12.57	12.57	6.28	6.28	2	0.00	0.02	0.13	0.00	0.00	24.0
7	12	-4378	1241	-3	0	28	16	12.57	12.57	6.28	6.28	2	0.00	0.02	0.13	0.00	0.00	24.0
8	12	-4366	1014	280	0	22	333	12.57	12.57	6.28	6.28	2	0.02	0.02	0.11	0.00	0.00	24.0
9	12	-4363	1033	-10	0	26	328	12.57	12.57	6.28	6.28	2	0.02	0.02	0.11	0.00	0.00	24.0
10	12	-4397	1471	192	0	27	-345	12.57	12.57	6.28	6.28	2	0.02	0.03	0.16	0.00	0.00	24.0
11	12	-4397	1477	106	0	29	-346	12.57	12.57	6.28	6.28	2	0.02	0.03	0.16	0.00	0.00	24.0
12	12	-4348	778	171	0	22	695	12.57	12.57	6.28	6.28	2	0.04	0.01	0.08	0.00	0.00	24.0
13	12	-4347	784	84	0	23	693	12.57	12.57	6.28	6.28	2	0.04	0.01	0.08	0.00	0.00	24.0
14	12	-4381	1222	286	0	24	21	12.57	12.57	6.28	6.28	2	0.00	0.02	0.13	0.00	0.00	24.0
15	12	-4378	1241	-3	0	28	16	12.57	12.57	6.28	6.28	2	0.00	0.02	0.13	0.00	0.00	24.0
16	12	-4366	1014	280	0	22	333	12.57	12.57	6.28	6.28	2	0.02	0.02	0.11	0.00	0.00	24.0
17	12	-4363	1033	-10	0	26	328	12.57	12.57	6.28	6.28	2	0.02	0.02	0.11	0.00	0.00	24.0
18	12	-5990	4589	512	0	44	-1843	12.57	12.57	6.28	6.28	3	0.07	0.08	0.48	0.00	0.00	24.0
19	12	-6172	1482	393	0	26	1677	12.57	12.57	6.28	6.28	3	0.06	0.03	0.16	0.00	0.00	24.0
20	12	-6044	2809	228	0	39	-30	12.57	12.57	6.28	6.28	3	0.00	0.05	0.30	0.00	0.00	24.0
37	12	-5776	5111	465	0	48	-2914	12.57	12.57	6.28	6.28	3	0.11	0.09	0.54	0.00	0.00	24.0
38	12	-6080	-68	266	0	19	2954	12.57	12.57	6.28	6.28	3	0.11	0.00	0.02	0.00	0.00	24.0
39	12	-5864	2144	-9	0	41	107	12.57	12.57	6.28	6.28	3	0.00	0.04	0.23	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-5586	1466	180	0	10	410	12.57	12.57	6.28	6.28	3	0.02	0.03	0.16	0.00	0.00	24.0
2	25	-4322	1471	192	0	3	-161	12.57	12.57	6.28	6.28	2	0.01	0.03	0.16	0.00	0.00	24.0
3	25	-4322	1477	106	0	15	-162	12.57	12.57	6.28	6.28	2	0.01	0.03	0.16	0.00	0.00	24.0
4	25	-4273	778	171	0	0	792	12.57	12.57	6.28	6.28	2	0.04	0.01	0.08	0.00	0.00	24.0
5	25	-4272	784	84	0	13	791	12.57	12.57	6.28	6.28	2	0.04	0.01	0.08	0.00	0.00	24.0
6	25	-4306	1222	286	0	-12	173	12.57	12.57	6.28	6.28	2	0.01	0.02	0.13	0.00	0.00	24.0
7	25	-4303	1241	-3	0	29	171	12.57	12.57	6.28	6.28	2	0.01	0.02	0.13	0.00	0.00	24.0
8	25	-4291	1014	280	0	-13	459	12.57	12.57	6.28	6.28	2	0.03	0.02	0.11	0.00	0.00	24.0
9	25	-4288	1033	-10	0	28	457	12.57	12.57	6.28	6.28	2	0.03	0.02	0.11	0.00	0.00	24.0
10	25	-4322	1471	192	0	3	-161	12.57	12.57	6.28	6.28	2	0.01	0.03	0.16	0.00	0.00	24.0
11	25	-4322	1477	106	0	15	-162	12.57	12.57	6.28	6.28	2	0.01	0.03	0.16	0.00	0.00	24.0
12	25	-4273	778	171	0	0	792	12.57	12.57	6.28	6.28	2	0.04	0.01	0.08	0.00	0.00	24.0
13	25	-4272	784	84	0	13	791	12.57	12.57	6.28	6.28	2	0.04	0.01	0.08	0.00	0.00	24.0
14	25	-4306	1222	286	0	-12	173	12.57	12.57	6.28	6.28	2	0.01	0.02	0.13	0.00	0.00	24.0
15	25	-4303	1241	-3	0	29	171	12.57	12.57	6.28	6.28	2	0.01	0.02	0.13	0.00	0.00	24.0
16	25	-4291	1014	280	0	-13	459	12.57	12.57	6.28	6.28	2	0.03	0.02	0.11	0.00	0.00	24.0
17	25	-4288	1033	-10	0	28	457	12.57	12.57	6.28	6.28	2	0.03	0.02	0.11	0.00	0.00	24.0
18	25	-5892	4589	512	0	-20	-1270	12.57	12.57	6.28	6.28	3	0.05	0.08	0.48	0.00	0.00	24.0
19	25	-6075	1482	393	0	-23	1862	12.57	12.57	6.28	6.28	3	0.07	0.03	0.16	0.00	0.00	24.0
20	25	-5946	2809	228	0	11	321	12.57	12.57	6.28	6.28	3	0.01	0.05	0.30	0.00	0.00	24.0
37	25	-5678	5111	465	0	-10	-2275	12.57	12.57	6.28	6.28	3	0.08	0.09	0.54	0.00	0.00	24.0
38	25	-5982	-68	266	0	-14	2945	12.57	12.57	6.28	6.28	3	0.11	0.00	0.02	0.00	0.00	24.0
39	25	-5767	2144	-9	0	42	375	12.57	12.57	6.28	6.28	3	0.01	0.04	0.23	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-5488	1466	180	0	-12	593	12.57	12.57	6.28	6.28	3	0.02	0.03	0.16	0.00	0.00	24.0
2	38	-4247	1471	192	0	-21	23	12.57	12.57	6.28	6.28	2	0.00	0.03	0.16	0.00	0.00	24.0
3	38	-4247	1477	106	0	2	23	12.57	12.57	6.28	6.28	2	0.00	0.03	0.16	0.00	0.00	24.0
4	38	-4198	778	171	0	-21	889	12.57	12.57	6.28	6.28	2	0.05	0.01	0.08	0.00	0.00	24.0
5	38	-4197	784	84	0	2	889	12.57	12.57	6.28	6.28	2	0.05	0.01	0.08	0.00	0.00	24.0
6	38	-4231	1222	286	0	-48	326	12.57	12.57	6.28	6.28	2	0.02	0.02	0.13	0.00	0.00	24.0
7	38	-4228	1241	-3	0	29	326	12.57	12.57	6.28	6.28	2	0.02	0.02	0.13	0.00	0.00	24.0
8	38	-4216	1014	280	0	-48	586	12.57	12.57	6.28	6.28	2	0.03	0.02	0.11	0.00	0.00	24.0
9	38	-4213	1033	-10	0	29	586	12.57	12.57	6.28	6.28	2	0.03	0.02	0.11	0.00	0.00	24.0
10	38	-4247	1471	192	0	-21	23	12.57	12.57	6.28	6.28	2	0.00	0.03	0.16	0.00	0.00	24.0
11	38	-4247	1477	106	0	2	23	12.57	12.57	6.28	6.28	2	0.00	0.03	0.16	0.00	0.00	24.0
12	38	-4198	778	171	0	-21	889	12.57	12.57	6.28	6.28	2	0.05	0.01	0.08	0.00	0.00	24.0
13	38	-4197	784	84	0	2	889	12.57	12.57	6.28	6.28	2	0.05	0.01	0.08	0.00	0.00	24.0
14	38	-4231	1222	286	0	-48	326	12.57	12.57	6.28	6.28	2	0.02	0.02	0.13	0.00	0.00	24.0
15	38	-4228	1241	-3	0	29	326	12.57	12.57	6.28	6.28	2	0.02	0.02	0.13	0.00	0.00	24.0
16	38	-4216	1014	280	0	-48	586	12.57	12.57	6.28	6.28	2	0.03	0.02	0.11	0.00	0.00	24.0
17	38	-4213	1033	-10	0	29	586	12.57	12.57	6.28	6.28	2	0.03	0.02	0.11	0.00	0.00	24.0
18	38	-5794	4589	512	0	-85	-696	12.57	12.57	6.28	6.28	3	0.03	0.08	0.48	0.00	0.00	24.0
19	38	-5978	1482	393	0	-72	2048	12.57	12.57	6.28	6.28	3	0.08	0.03	0.16	0.00	0.00	24.0
20	38	-5848	2809	228	0	-18	673	12.57	12.57	6.28	6.28	3	0.03	0.05	0.30	0.00	0.00	24.0
37	38	-5580	5111	465	0	-68	-1637	12.57	12.57	6.28	6.28	3	0.06	0.09	0.54	0.00	0.00	24.0
38	38	-5884	-68	266	0	-48	2937	12.57	12.57	6.28	6.28	3	0.11	0.00	0.02	0.00	0.00	24.0
39	38	-5670	2144	-9	0	43	643	12.57	12.57	6.28	6.28	3	0.02	0.04	0.23	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-5391	1466	180	0	-35	776	12.57	12.57	6.28	6.28	3	0.03	0.03	0.16	0.00	0.00	24.0
2	50	-4172	1471	192	0	-45	207	12.57	12.57	6.28	6.28	2	0.01	0.03	0.16	0.00	0.00	24.0
3	50	-4172	1477	106	0	-11	207	12.57	12.57	6.28	6.28	2	0.01	0.03	0.16	0.00	0.00	24.0
4	50	-4123	778	171	0	-42	986	12.57	12.57	6.28	6.28	2	0.05	0.01	0.08	0.00	0.00	24.0
5	50	-4122	784	84	0	-8	987	12.57	12.57	6.28	6.28	2	0.05	0.01	0.08	0.00	0.00	24.0
6	50	-4156	1222	286	0	-83	479	12.57	12.57	6.28	6.28	2	0.03	0.02	0.13	0.00	0.00	24.0
7	50	-4153	1241	-3	0	29	481	12.57	12.57	6.28	6.28	2	0.03	0.02	0.13	0.00	0.00	24.0
8	50	-4141	1014	280	0	-83	713	12.57	12.57	6.28	6.28	2	0.04	0.02	0.11	0.00	0.00	24.0
9	50	-4138	1033	-10	0	30	715	12.57	12.57	6.28	6.28	2	0.04	0.02	0.11	0.00	0.00	24.0
10	50	-4172	1471	192	0	-45	207	12.57	12.57	6.28	6.28	2	0.01	0.03	0.16	0.00	0.00	24.0
11	50	-4172	1477	106	0	-11	207	12.57	12.57	6.28	6.28	2	0.01	0.03	0.16	0.00	0.00	24.0
12	50	-4123	778	171	0	-42	986	12.57	12.57	6.28	6.28	2	0.05	0.01	0.08	0.00	0.00	24.0
13	50	-4122	784	84	0	-8	987	12.57	12.57	6.28	6.28	2	0.05	0.01	0.08	0.00	0.00	24.0
14	50	-4156	1222	286	0	-83	479	12.57	12.57	6.28	6.28	2	0.03	0.02	0.13	0.00	0.00	24.0
15	50	-4153	1241	-3	0	29	481	12.57	12.57	6.28	6.28	2	0.03	0.02	0.13	0.00	0.00	24.0
16	50	-4141	1014	280	0	-83	713	12.57	12.57	6.28	6.28	2	0.04	0.02	0.11	0.00	0.00	24.0
17	50	-4138	1033	-10	0	30	715	12.57	12.57	6.28	6.28	2	0.04	0.02	0.11	0.00	0.00	24.0
18	50	-5697	4589	512	0	-148	-122	12.57	12.57	6.28	6.28	3	0.01	0.08	0.49	0.00	0.00	24.0
19	50	-5880	1482	393	0	-121	2233	12.57	12.57	6.28	6.28	3	0.08	0.03	0.16	0.00	0.00	24.0
20	50	-5751	2809	228	0	-46	1024	12.57	12.57	6.28	6.28	3	0.04	0.05	0.30	0.00	0.00	24.0
37	50	-5483	5111	465	0	-126	-998	12.57	12.57	6.28	6.28	3	0.04	0.09	0.54	0.00	0.00	24.0
38	50	-5787	-68	266	0	-81	2928	12.57	12.57	6.28	6.28	3	0.11	0.00	0.02	0.00	0.00	24.0
39	50	-5572	2144	-9	0	44	912	12.57	12.57	6.28	6.28	3	0.03	0.04	0.23	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 119 NI 821 NF 166 SEZ. Rp B= 0.400 H= 0.600 (pilastro)
PIL. NUM. 26A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-6889	958	361	0	-35	729	12.57	12.57	6.28	6.28	3	0.03	0.02	0.10	0.00	0.00	24.0
2	0	-5411	724	422	0	-45	175	12.57	12.57	6.28	6.28	2	0.01	0.01	0.08	0.00	0.00	24.0
3	0	-5409	725	108	0	-11	175	12.57	12.57	6.28	6.28	2	0.01	0.01	0.08	0.00	0.00	24.0
4	0	-5190	748	448	0	-42	947	12.57	12.57	6.28	6.28	2	0.05	0.01	0.08	0.00	0.00	24.0
5	0	-5188	750	134	0	-8	947	12.57	12.57	6.28	6.28	2	0.05	0.01	0.08	0.00	0.00	24.0
6	0	-5337	731	798	0	-83	445	12.57	12.57	6.28	6.28	2	0.03	0.01	0.08	0.00	0.00	24.0
7	0	-5329	735	-250	0	29	446	12.57	12.57	6.28	6.28	2	0.02	0.01	0.08	0.00	0.00	24.0
8	0	-5270	738	806	0	-83	677	12.57	12.57	6.28	6.28	2	0.04	0.01	0.08	0.00	0.00	24.0
9	0	-5262	742	-242	0	30	677	12.57	12.57	6.28	6.28	2	0.04	0.01	0.08	0.00	0.00	24.0
10	0	-5411	724	422	0	-45	175	12.57	12.57	6.28	6.28	2	0.01	0.01	0.08	0.00	0.00	24.0
11	0	-5409	725	108	0	-11	175	12.57	12.57	6.28	6.28	2	0.01	0.01	0.08	0.00	0.00	24.0
12	0	-5190	748	448	0	-42	947	12.57	12.57	6.28	6.28	2	0.05	0.01	0.08	0.00	0.00	24.0
13	0	-5188	750	134	0	-8	947	12.57	12.57	6.28	6.28	2	0.05	0.01	0.08	0.00	0.00	24.0
14	0	-5337	731	798	0	-83	445	12.57	12.57	6.28	6.28	2	0.03	0.01	0.08	0.00	0.00	24.0
15	0	-5329	735	-250	0	29	446	12.57	12.57	6.28	6.28	2	0.02	0.01	0.08	0.00	0.00	24.0
16	0	-5270	738	806	0	-83	677	12.57	12.57	6.28	6.28	2	0.04	0.01	0.08	0.00	0.00	24.0
17	0	-5262	742	-242	0	30	677	12.57	12.57	6.28	6.28	2	0.04	0.01	0.08	0.00	0.00	24.0
18	0	-7784	1862	1398	0	-148	-219	12.57	12.57	6.28	6.28	3	0.01	0.03	0.19	0.00	0.00	24.0
19	0	-7281	1493	1308	0	-121	2130	12.57	12.57	6.28	6.28	3	0.08	0.03	0.15	0.00	0.00	24.0
20	0	-7465	1573	512	0	-46	930	12.57	12.57	6.28	6.28	3	0.03	0.03	0.16	0.00	0.00	24.0
37	0	-7707	1750	1119	0	-126	-1075	12.57	12.57	6.28	6.28	3	0.04	0.03	0.18	0.00	0.00	24.0
38	0	-6870	1134	969	0	-81	2840	12.57	12.57	6.28	6.28	3	0.11	0.02	0.12	0.00	0.00	24.0
39	0	-7176	1268	-357	0	44	840	12.57	12.57	6.28	6.28	3	0.03	0.02	0.13	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-6792	958	361	0	-80	849	12.57	12.57	6.28	6.28	3	0.03	0.02	0.10	0.00	0.00	24.0
2	12	-5336	724	422	0	-98	265	12.57	12.57	6.28	6.28	2	0.02	0.01	0.08	0.00	0.00	24.0
3	12	-5334	725	108	0	-24	266	12.57	12.57	6.28	6.28	2	0.01	0.01	0.08	0.00	0.00	24.0
4	12	-5115	748	448	0	-98	1041	12.57	12.57	6.28	6.28	2	0.06	0.01	0.08	0.00	0.00	24.0
5	12	-5113	750	134	0	-25	1041	12.57	12.57	6.28	6.28	2	0.06	0.01	0.08	0.00	0.00	24.0
6	12	-5262	731	798	0	-183	536	12.57	12.57	6.28	6.28	2	0.04	0.01	0.08	0.00	0.00	24.0
7	12	-5254	735	-250	0	61	538	12.57	12.57	6.28	6.28	2	0.03	0.01	0.08	0.00	0.00	24.0
8	12	-5195	738	806	0	-183	769	12.57	12.57	6.28	6.28	2	0.05	0.01	0.08	0.00	0.00	24.0
9	12	-5187	742	-242	0	60	770	12.57	12.57	6.28	6.28	2	0.04	0.01	0.08	0.00	0.00	24.0
10	12	-5336	724	422	0	-98	265	12.57	12.57	6.28	6.28	2	0.02	0.01	0.08	0.00	0.00	24.0
11	12	-5334	725	108	0	-24	266	12.57	12.57	6.28	6.28	2	0.01	0.01	0.08	0.00	0.00	24.0
12	12	-5115	748	448	0	-98	1041	12.57	12.57	6.28	6.28	2	0.06	0.01	0.08	0.00	0.00	24.0
13	12	-5113	750	134	0	-25	1041	12.57	12.57	6.28	6.28	2	0.06	0.01	0.08	0.00	0.00	24.0
14	12	-5262	731	798	0	-183	536	12.57	12.57	6.28	6.28	2	0.04	0.01	0.08	0.00	0.00	24.0
15	12	-5254	735	-250	0	61	538	12.57	12.57	6.28	6.28	2	0.03	0.01	0.08	0.00	0.00	24.0
16	12	-5195	738	806	0	-183	769	12.57	12.57	6.28	6.28	2	0.05	0.01	0.08	0.00	0.00	24.0
17	12	-5187	742	-242	0	60	770	12.57	12.57	6.28	6.28	2	0.04	0.01	0.08	0.00	0.00	24.0
18	12	-7686	1862	1398	0	-323	14	12.57	12.57	6.28	6.28	3	0.02	0.03	0.19	0.00	0.00	24.0
19	12	-7184	1493	1308	0	-285	2316	12.57	12.57	6.28	6.28	3	0.09	0.03	0.15	0.00	0.00	24.0
20	12	-7368	1573	512	0	-110	1127	12.57	12.57	6.28	6.28	3	0.04	0.03	0.16	0.00	0.00	24.0
37	12	-7610	1750	1119	0	-266	-856	12.57	12.57	6.28	6.28	3	0.04	0.03	0.18	0.00	0.00	24.0
38	12	-6772	1134	969	0	-202	2982	12.57	12.57	6.28	6.28	3	0.11	0.02	0.12	0.00	0.00	24.0
39	12	-7078	1268	-357	0	89	998	12.57	12.57	6.28	6.28	3	0.04	0.02	0.13	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-6694	958	361	0	-125	969	12.57	12.57	6.28	6.28	3	0.04	0.02	0.10	0.00	0.00	24.0
2	25	-5261	724	422	0	-150	356	12.57	12.57	6.28	6.28	2	0.02	0.01	0.08	0.00	0.00	24.0
3	25	-5259	725	108	0	-38	356	12.57	12.57	6.28	6.28	2	0.02	0.01	0.08	0.00	0.00	24.0
4	25	-5040	748	448	0	-154	1134	12.57	12.57	6.28	6.28	2	0.07	0.01	0.08	0.00	0.00	24.0
5	25	-5038	750	134	0	-42	1135	12.57	12.57	6.28	6.28	2	0.06	0.01	0.08	0.00	0.00	24.0
6	25	-5187	731	798	0	-283	628	12.57	12.57	6.28	6.28	2	0.04	0.01	0.08	0.00	0.00	24.0
7	25	-5179	735	-250	0	92	630	12.57	12.57	6.28	6.28	2	0.04	0.01	0.08	0.00	0.00	24.0
8	25	-5120	738	806	0	-284	861	12.57	12.57	6.28	6.28	2	0.06	0.01	0.08	0.00	0.00	24.0
9	25	-5112	742	-242	0	91	863	12.57	12.57	6.28	6.28	2	0.05	0.01	0.08	0.00	0.00	24.0
10	25	-5261	724	422	0	-150	356	12.57	12.57	6.28	6.28	2	0.02	0.01	0.08	0.00	0.00	24.0
11	25	-5259	725	108	0	-38	356	12.57	12.57	6.28	6.28	2	0.02	0.01	0.08	0.00	0.00	24.0
12	25	-5040	748	448	0	-154	1134	12.57	12.57	6.28	6.28	2	0.07	0.01	0.08	0.00	0.00	24.0
13	25	-5038	750	134	0	-42	1135	12.57	12.57	6.28	6.28	2	0.06	0.01	0.08	0.00	0.00	24.0
14	25	-5187	731	798	0	-283	628	12.57	12.57	6.28	6.28	2	0.04	0.01	0.08	0.00	0.00	24.0
15	25	-5179	735	-250	0	92	630	12.57	12.57	6.28	6.28	2	0.04	0.01	0.08	0.00	0.00	24.0
16	25	-5120	738	806	0	-284	861	12.57	12.57	6.28	6.28	2	0.06	0.01	0.08	0.00	0.00	24.0
17	25	-5112	742	-242	0	91	863	12.57	12.57	6.28	6.28	2	0.05	0.01	0.08	0.00	0.00	24.0
18	25	-7589	1862	1398	0	-498	247	12.57	12.57	6.28	6.28	3	0.03	0.03	0.19	0.00	0.00	24.0
19	25	-7086	1493	1308	0	-448	2503	12.57	12.57	6.28	6.28	3	0.10	0.03	0.15	0.00	0.00	24.0
20	25	-7270	1573	512	0	-174	1324	12.57	12.57	6.28	6.28	3	0.05	0.03	0.16	0.00	0.00	24.0
37	25	-7512	1750	1119	0	-406	-638	12.57	12.57	6.28	6.28	3	0.03	0.03	0.18	0.00	0.00	24.0
38	25	-6675	1134	969	0	-323	3123	12.57	12.57	6.28	6.28	3	0.12	0.02	0.12	0.00	0.00	24.0
39	25	-6981	1268	-357	0	133	1157	12.57	12.57	6.28	6.28	3	0.04	0.02	0.13	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-6596	958	361	0	-170	1088	12.57	12.57	6.28	6.28	3	0.04	0.02	0.10	0.00	0.00	24.0
2	38	-5186	724	422	0	-203	446	12.57	12.57	6.28	6.28	2	0.03	0.01	0.08	0.00	0.00	24.0
3	38	-5184	725	108	0	-51	447	12.57	12.57	6.28	6.28	2	0.03	0.01	0.08	0.00	0.00	24.0
4	38	-4965	748	448	0	-210	1228	12.57	12.57	6.28	6.28	2	0.07	0.01	0.08	0.00	0.00	24.0
5	38	-4963	750	134	0	-59	1228	12.57	12.57	6.28	6.28	2	0.07	0.01	0.08	0.00	0.00	24.0
6	38	-5112	731	798	0	-383	719	12.57	12.57	6.28	6.28	2	0.05	0.01	0.08	0.00	0.00	24.0
7	38	-5104	735	-250	0	123	721	12.57	12.57	6.28	6.28	2	0.04	0.01	0.08	0.00	0.00	24.0
8	38	-5045	738	806	0	-385	954	12.57	12.57	6.28	6.28	2	0.06	0.01	0.08	0.00	0.00	24.0
9	38	-5037	742	-242	0	121	956	12.57	12.57	6.28	6.28	2	0.06	0.01	0.08	0.00	0.00	24.0
10	38	-5186	724	422	0	-203	446	12.57	12.57	6.28	6.28	2	0.03	0.01	0.08	0.00	0.00	24.0
11	38	-5184	725	108	0	-51	447	12.57	12.57	6.28	6.28	2	0.03	0.01	0.08	0.00	0.00	24.0
12	38	-4965	748	448	0	-210	1228	12.57	12.57	6.28	6.28	2	0.07	0.01	0.08	0.00	0.00	24.0
13	38	-4963	750	134	0	-59	1228	12.57	12.57	6.28	6.28	2	0.07	0.01	0.08	0.00	0.00	24.0
14	38	-5112	731	798	0	-383	719	12.57	12.57	6.28	6.28	2	0.05	0.01	0.08	0.00	0.00	24.0
15	38	-5104	735	-250	0	123	721	12.57	12.57	6.28	6.28	2	0.04	0.01	0.08	0.00	0.00	24.0
16	38	-5045	738	806	0	-385	954	12.57	12.57	6.28	6.28	2	0.06	0.01	0.08	0.00	0.00	24.0
17	38	-5037	742	-242	0	121	956	12.57	12.57	6.28	6.28	2	0.06	0.01	0.08	0.00	0.00	24.0
18	38	-7492	1862	1398	0	-673	479	12.57	12.57	6.28	6.28	3	0.04	0.03	0.19	0.00	0.00	24.0
19	38	-6988	1493	1308	0	-612	2690	12.57	12.57	6.28	6.28	3	0.11	0.03	0.15	0.00	0.00	24.0
20	38	-7172	1573	512	0	-238	1520	12.57	12.57	6.28	6.28	3	0.06	0.03	0.16	0.00	0.00	24.0
37	38	-7414	1750	1119	0	-546	-419	12.57	12.57	6.28	6.28	3	0.03	0.03	0.18	0.00	0.00	24.0
38	38	-6578	1134	969	0	-444	3265	12.57	12.57	6.28	6.28	3	0.13	0.02	0.12	0.00	0.00	24.0
39	38	-6884	1268	-357	0	178	1315	12.57	12.57	6.28	6.28	3	0.05	0.02	0.13	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-6499	958	361	0	-215	1208	12.57	12.57	6.28	6.28	3	0.05	0.02	0.10	0.00	0.00	24.0
2	50	-5111	724	422	0	-256	537	12.57	12.57	6.28	6.28	2	0.04	0.01	0.08	0.00	0.00	24.0
3	50	-5109	725	108	0	-65	538	12.57	12.57	6.28	6.28	2	0.03	0.01	0.08	0.00	0.00	24.0
4	50	-4890	748	448	0	-266	1321	12.57	12.57	6.28	6.28	2	0.08	0.01	0.08	0.00	0.00	24.0
5	50	-4888	750	134	0	-75	1322	12.57	12.57	6.28	6.28	2	0.07	0.01	0.08	0.00	0.00	24.0
6	50	-5037	731	798	0	-482	810	12.57	12.57	6.28	6.28	2	0.06	0.01	0.08	0.00	0.00	24.0
7	50	-5029	735	-250	0	154	813	12.57	12.57	6.28	6.28	2	0.05	0.01	0.08	0.00	0.00	24.0
8	50	-4970	738	806	0	-485	1046	12.57	12.57	6.28	6.28	2	0.07	0.01	0.08	0.00	0.00	24.0
9	50	-4962	742	-242	0	151	1049	12.57	12.57	6.28	6.28	2	0.06	0.01	0.08	0.00	0.00	24.0
10	50	-5111	724	422	0	-256	537	12.57	12.57	6.28	6.28	2	0.04	0.01	0.08	0.00	0.00	24.0
11	50	-5109	725	108	0	-65	538	12.57	12.57	6.28	6.28	2	0.03	0.01	0.08	0.00	0.00	24.0
12	50	-4890	748	448	0	-266	1321	12.57	12.57	6.28	6.28	2	0.08	0.01	0.08	0.00	0.00	24.0
13	50	-4888	750	134	0	-75	1322	12.57	12.57	6.28	6.28	2	0.07	0.01	0.08	0.00	0.00	24.0
14	50	-5037	731	798	0	-482	810	12.57	12.57	6.28	6.28	2	0.06	0.01	0.08	0.00	0.00	24.0
15	50	-5029	735	-250	0	154	813	12.57	12.57	6.28	6.28	2	0.05	0.01	0.08	0.00	0.00	24.0
16	50	-4970	738	806	0	-485	1046	12.57	12.57	6.28	6.28	2	0.07	0.01	0.08	0.00	0.00	24.0
17	50	-4962	742	-242	0	151	1049	12.57	12.57	6.28	6.28	2	0.06	0.01	0.08	0.00	0.00	24.0
18	50	-7394	1862	1398	0	-847	712	12.57	12.57	6.28	6.28	3	0.05	0.03	0.19	0.00	0.00	24.0
19	50	-6891	1493	1308	0	-775	2876	12.57	12.57	6.28	6.28	3	0.12	0.03	0.16	0.00	0.00	24.0
20	50	-7075	1573	512	0	-302	1717	12.57	12.57	6.28	6.28	3	0.07	0.03	0.16	0.00	0.00	24.0
37	50	-7317	1750	1119	0	-686	-200	12.57	12.57	6.28	6.28	3	0.04	0.03	0.18	0.00	0.00	24.0
38	50	-6480	1134	969	0	-566	3407	12.57	12.57	6.28	6.28	3	0.13	0.02	0.12	0.00	0.00	24.0
39	50	-6786	1268	-357	0	222	1474	12.57	12.57	6.28	6.28	3	0.06	0.02	0.13	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 120 NI 804 NF 827 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 25
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-8414	139	390	0	37	-55	6.28	6.28	9.42	9.42	3	0.01	0.01	0.05	0.00	0.00	24.0
2	0	-6825	149	377	0	20	-160	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
3	0	-6770	148	247	0	34	-159	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
4	0	-6174	65	353	0	23	75	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
5	0	-6119	65	223	0	37	75	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
6	0	-6662	120	521	0	4	-78	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
7	0	-6478	119	87	0	52	-77	6.28	6.28	9.42	9.42	2	0.01	0.00	0.01	0.00	0.00	24.0
8	0	-6467	95	514	0	5	-8	6.28	6.28	9.42	9.42	2	0.00	0.01	0.06	0.00	0.00	24.0
9	0	-6283	94	79	0	53	-6	6.28	6.28	9.42	9.42	2	0.00	0.00	0.01	0.00	0.00	24.0
10	0	-6825	149	377	0	20	-160	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
11	0	-6770	148	247	0	34	-159	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
12	0	-6174	65	353	0	23	75	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
13	0	-6119	65	223	0	37	75	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
14	0	-6662	120	521	0	4	-78	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
15	0	-6478	119	87	0	52	-77	6.28	6.28	9.42	9.42	2	0.01	0.00	0.01	0.00	0.00	24.0
16	0	-6467	95	514	0	5	-8	6.28	6.28	9.42	9.42	2	0.00	0.01	0.06	0.00	0.00	24.0
17	0	-6283	94	79	0	53	-6	6.28	6.28	9.42	9.42	2	0.00	0.00	0.01	0.00	0.00	24.0
18	0	-10140	474	859	0	4	-528	6.28	6.28	9.42	9.42	3	0.05	0.02	0.10	0.00	0.00	24.0
19	0	-8876	94	737	0	26	328	6.28	6.28	9.42	9.42	3	0.03	0.02	0.09	0.00	0.00	24.0
20	0	-9259	262	484	0	45	-96	6.28	6.28	9.42	9.42	3	0.01	0.01	0.06	0.00	0.00	24.0
37	0	-10160	554	769	0	3	-798	6.28	6.28	9.42	9.42	3	0.08	0.02	0.09	0.00	0.00	24.0
38	0	-8056	-81	565	0	40	628	6.28	6.28	9.42	9.42	3	0.07	0.01	0.07	0.00	0.00	24.0
39	0	-8695	200	143	0	71	-78	6.28	6.28	9.42	9.42	3	0.01	0.01	0.02	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-8341	139	390	0	-12	-38	6.28	6.28	9.42	9.42	3	0.00	0.01	0.05	0.00	0.00	24.0
2	12	-6769	149	377	0	-28	-141	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
3	12	-6714	148	247	0	3	-141	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
4	12	-6118	65	353	0	-21	83	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
5	12	-6063	65	223	0	9	83	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
6	12	-6606	120	521	0	-61	-63	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
7	12	-6422	119	87	0	41	-62	6.28	6.28	9.42	9.42	2	0.01	0.00	0.01	0.00	0.00	24.0
8	12	-6411	95	514	0	-59	4	6.28	6.28	9.42	9.42	2	0.00	0.01	0.06	0.00	0.00	24.0
9	12	-6227	94	79	0	43	5	6.28	6.28	9.42	9.42	2	0.00	0.00	0.01	0.00	0.00	24.0
10	12	-6769	149	377	0	-28	-141	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
11	12	-6714	148	247	0	3	-141	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
12	12	-6118	65	353	0	-21	83	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
13	12	-6063	65	223	0	9	83	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
14	12	-6606	120	521	0	-61	-63	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
15	12	-6422	119	87	0	41	-62	6.28	6.28	9.42	9.42	2	0.01	0.00	0.01	0.00	0.00	24.0
16	12	-6411	95	514	0	-59	4	6.28	6.28	9.42	9.42	2	0.00	0.01	0.06	0.00	0.00	24.0
17	12	-6227	94	79	0	43	5	6.28	6.28	9.42	9.42	2	0.00	0.00	0.01	0.00	0.00	24.0
18	12	-10066	474	859	0	-103	-469	6.28	6.28	9.42	9.42	3	0.05	0.02	0.10	0.00	0.00	24.0
19	12	-8803	94	737	0	-66	340	6.28	6.28	9.42	9.42	3	0.04	0.02	0.09	0.00	0.00	24.0
20	12	-9186	262	484	0	-15	-63	6.28	6.28	9.42	9.42	3	0.01	0.01	0.06	0.00	0.00	24.0
37	12	-10086	554	769	0	-93	-729	6.28	6.28	9.42	9.42	3	0.08	0.02	0.09	0.00	0.00	24.0
38	12	-7983	-81	565	0	-31	618	6.28	6.28	9.42	9.42	3	0.07	0.01	0.07	0.00	0.00	24.0
39	12	-8622	200	143	0	54	-53	6.28	6.28	9.42	9.42	3	0.01	0.01	0.02	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-8268	139	390	0	-61	-20	6.28	6.28	9.42	9.42	3	0.00	0.01	0.05	0.00	0.00	24.0
2	25	-6712	149	377	0	-75	-122	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
3	25	-6658	148	247	0	-28	-122	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
4	25	-6062	65	353	0	-65	91	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
5	25	-6006	65	223	0	-18	91	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
6	25	-6550	120	521	0	-126	-48	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
7	25	-6366	119	87	0	30	-47	6.28	6.28	9.42	9.42	2	0.01	0.00	0.01	0.00	0.00	24.0
8	25	-6354	95	514	0	-123	16	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
9	25	-6170	94	79	0	33	17	6.28	6.28	9.42	9.42	2	0.00	0.00	0.01	0.00	0.00	24.0
10	25	-6712	149	377	0	-75	-122	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
11	25	-6658	148	247	0	-28	-122	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
12	25	-6062	65	353	0	-65	91	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
13	25	-6006	65	223	0	-18	91	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
14	25	-6550	120	521	0	-126	-48	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
15	25	-6366	119	87	0	30	-47	6.28	6.28	9.42	9.42	2	0.01	0.00	0.01	0.00	0.00	24.0
16	25	-6354	95	514	0	-123	16	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
17	25	-6170	94	79	0	33	17	6.28	6.28	9.42	9.42	2	0.00	0.00	0.01	0.00	0.00	24.0
18	25	-9992	474	859	0	-211	-409	6.28	6.28	9.42	9.42	3	0.04	0.02	0.10	0.00	0.00	24.0
19	25	-8730	94	737	0	-158	351	6.28	6.28	9.42	9.42	3	0.04	0.02	0.09	0.00	0.00	24.0
20	25	-9113	262	484	0	-76	-30	6.28	6.28	9.42	9.42	3	0.00	0.01	0.06	0.00	0.00	24.0
37	25	-10013	554	769	0	-189	-660	6.28	6.28	9.42	9.42	3	0.07	0.02	0.09	0.00	0.00	24.0

38	25	-7910	-81	565	0	-101	608	6.28	6.28	9.42	9.42	3	0.06	0.01	0.07	0.00	0.00	24.0
39	25	-8548	200	143	0	36	-28	6.28	6.28	9.42	9.42	3	0.00	0.01	0.02	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-8195	139	390	0	-109	-3	6.28	6.28	9.42	9.42	3	0.01	0.01	0.05	0.00	0.00	24.0
2	38	-6656	149	377	0	-122	-104	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
3	38	-6601	148	247	0	-59	-104	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
4	38	-6005	65	353	0	-109	99	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
5	38	-5950	65	223	0	-46	100	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
6	38	-6493	120	521	0	-191	-33	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
7	38	-6309	119	87	0	19	-32	6.28	6.28	9.42	9.42	2	0.00	0.00	0.01	0.00	0.00	24.0
8	38	-6298	95	514	0	-187	28	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
9	38	-6114	94	79	0	23	29	6.28	6.28	9.42	9.42	2	0.00	0.00	0.01	0.00	0.00	24.0
10	38	-6656	149	377	0	-122	-104	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
11	38	-6601	148	247	0	-59	-104	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
12	38	-6005	65	353	0	-109	99	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
13	38	-5950	65	223	0	-46	100	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
14	38	-6493	120	521	0	-191	-33	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
15	38	-6309	119	87	0	19	-32	6.28	6.28	9.42	9.42	2	0.00	0.00	0.01	0.00	0.00	24.0
16	38	-6298	95	514	0	-187	28	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
17	38	-6114	94	79	0	23	29	6.28	6.28	9.42	9.42	2	0.00	0.00	0.01	0.00	0.00	24.0
18	38	-9919	474	859	0	-318	-350	6.28	6.28	9.42	9.42	3	0.04	0.02	0.10	0.00	0.00	24.0
19	38	-8656	94	737	0	-250	363	6.28	6.28	9.42	9.42	3	0.04	0.02	0.09	0.00	0.00	24.0
20	38	-9040	262	484	0	-136	3	6.28	6.28	9.42	9.42	3	0.01	0.01	0.06	0.00	0.00	24.0
37	38	-9940	554	769	0	-286	-591	6.28	6.28	9.42	9.42	3	0.06	0.02	0.09	0.00	0.00	24.0
38	38	-7836	-81	565	0	-172	598	6.28	6.28	9.42	9.42	3	0.06	0.01	0.07	0.00	0.00	24.0
39	38	-8475	200	143	0	18	-3	6.28	6.28	9.42	9.42	3	0.00	0.01	0.02	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-8122	139	390	0	-158	15	6.28	6.28	9.42	9.42	3	0.01	0.01	0.05	0.00	0.00	24.0
2	50	-6600	149	377	0	-169	-85	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
3	50	-6545	148	247	0	-90	-85	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
4	50	-5949	65	353	0	-154	107	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
5	50	-5894	65	223	0	-74	108	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
6	50	-6437	120	521	0	-256	-18	6.28	6.28	9.42	9.42	2	0.02	0.01	0.06	0.00	0.00	24.0
7	50	-6253	119	87	0	8	-17	6.28	6.28	9.42	9.42	2	0.00	0.00	0.01	0.00	0.00	24.0
8	50	-6242	95	514	0	-252	40	6.28	6.28	9.42	9.42	2	0.02	0.01	0.06	0.00	0.00	24.0
9	50	-6058	94	79	0	13	41	6.28	6.28	9.42	9.42	2	0.01	0.00	0.01	0.00	0.00	24.0
10	50	-6600	149	377	0	-169	-85	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
11	50	-6545	148	247	0	-90	-85	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
12	50	-5949	65	353	0	-154	107	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
13	50	-5894	65	223	0	-74	108	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
14	50	-6437	120	521	0	-256	-18	6.28	6.28	9.42	9.42	2	0.02	0.01	0.06	0.00	0.00	24.0
15	50	-6253	119	87	0	8	-17	6.28	6.28	9.42	9.42	2	0.00	0.00	0.01	0.00	0.00	24.0
16	50	-6242	95	514	0	-252	40	6.28	6.28	9.42	9.42	2	0.02	0.01	0.06	0.00	0.00	24.0
17	50	-6058	94	79	0	13	41	6.28	6.28	9.42	9.42	2	0.01	0.00	0.01	0.00	0.00	24.0
18	50	-9845	474	859	0	-425	-291	6.28	6.28	9.42	9.42	3	0.03	0.02	0.10	0.00	0.00	24.0
19	50	-8583	94	737	0	-342	375	6.28	6.28	9.42	9.42	3	0.04	0.02	0.09	0.00	0.00	24.0
20	50	-8967	262	484	0	-196	35	6.28	6.28	9.42	9.42	3	0.01	0.01	0.06	0.00	0.00	24.0
37	50	-9866	554	769	0	-382	-522	6.28	6.28	9.42	9.42	3	0.06	0.02	0.09	0.00	0.00	24.0
38	50	-7763	-81	565	0	-242	588	6.28	6.28	9.42	9.42	3	0.06	0.01	0.07	0.00	0.00	24.0
39	50	-8402	200	143	0	-0	22	6.28	6.28	9.42	9.42	3	0.00	0.01	0.02	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 121 NI 827 NF 263 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 25A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-11750	77	682	0	-158	5	6.28	6.28	9.42	9.42	3	0.01	0.02	0.08	0.00	0.00	24.0
2	0	-9619	-122	738	0	-169	-84	6.28	6.28	9.42	9.42	2	0.02	0.02	0.09	0.00	0.00	24.0
3	0	-9529	-121	392	0	-90	-84	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
4	0	-8541	239	658	0	-154	92	6.28	6.28	9.42	9.42	2	0.02	0.02	0.08	0.00	0.00	24.0
5	0	-8451	240	312	0	-74	93	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
6	0	-9347	4	1114	0	-256	-23	6.28	6.28	9.42	9.42	2	0.02	0.03	0.13	0.00	0.00	24.0
7	0	-9046	6	-40	0	8	-22	6.28	6.28	9.42	9.42	2	0.00	0.00	0.00	0.00	0.00	24.0
8	0	-9024	112	1090	0	-252	30	6.28	6.28	9.42	9.42	2	0.02	0.03	0.13	0.00	0.00	24.0
9	0	-8723	114	-64	0	13	31	6.28	6.28	9.42	9.42	2	0.00	0.00	0.01	0.00	0.00	24.0
10	0	-9619	-122	738	0	-169	-84	6.28	6.28	9.42	9.42	2	0.02	0.02	0.09	0.00	0.00	24.0
11	0	-9529	-121	392	0	-90	-84	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
12	0	-8541	239	658	0	-154	92	6.28	6.28	9.42	9.42	2	0.02	0.02	0.08	0.00	0.00	24.0
13	0	-8451	240	312	0	-74	93	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
14	0	-9347	4	1114	0	-256	-23	6.28	6.28	9.42	9.42	2	0.02	0.03	0.13	0.00	0.00	24.0
15	0	-9046	6	-40	0	8	-22	6.28	6.28	9.42	9.42	2	0.00	0.00	0.00	0.00	0.00	24.0
16	0	-9024	112	1090	0	-252	30	6.28	6.28	9.42	9.42	2	0.02	0.03	0.13	0.00	0.00	24.0
17	0	-8723	114	-64	0	13	31	6.28	6.28	9.42	9.42	2	0.00	0.00	0.01	0.00	0.00	24.0
18	0	-14430	-422	1873	0	-425	-287	6.28	6.28	9.42	9.42	3	0.03	0.04	0.20	0.00	0.00	24.0
19	0	-12250	737	1455	0	-342	323	6.28	6.28	9.42	9.42	3	0.03	0.03	0.16	0.00	0.00	24.0
20	0	-12960	141	788	0	-196	14	6.28	6.28	9.42	9.42	3	0.01	0.02	0.09	0.00	0.00	24.0
37	0	-14570	-834	1700	0	-382	-494	6.28	6.28	9.42	9.42	3	0.05	0.04	0.19	0.00	0.00	24.0
38	0	-10950	1097	1005	0	-242	523	6.28	6.28	9.42	9.42	3	0.05	0.03	0.12	0.00	0.00	24.0
39	0	-12120	103	-108	0	-0	8	6.28	6.28	9.42	9.42	3	0.00	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-11675	77	682	0	-243	15	6.28	6.28	9.42	9.42	3	0.01	0.02	0.08	0.00	0.00	24.0
2	12	-9563	-122	738	0	-261	-100	6.28	6.28	9.42	9.42	2	0.02	0.02	0.09	0.00	0.00	24.0
3	12	-9473	-121	392	0	-139	-99	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
4	12	-8485	239	658	0	-236	122	6.28	6.28	9.42	9.42	2	0.02	0.02	0.08	0.00	0.00	24.0
5	12	-8395	240	312	0	-113	123	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
6	12	-9291	4	1114	0	-395	-22	6.28	6.28	9.42	9.42	2	0.03	0.03	0.13	0.00	0.00	24.0
7	12	-8990	6	-40	0	13	-21	6.28	6.28	9.42	9.42	2	0.00	0.00	0.00	0.00	0.00	24.0
8	12	-8968	112	1090	0	-388	44	6.28	6.28	9.42	9.42	2	0.03	0.03	0.13	0.00	0.00	24.0
9	12	-8667	114	-64	0	21	45	6.28	6.28	9.42	9.42	2	0.01	0.00	0.01	0.00	0.00	24.0
10	12	-9563	-122	738	0	-261	-100	6.28	6.28	9.42	9.42	2	0.02	0.02	0.09	0.00	0.00	24.0
11	12	-9473	-121	392	0	-139	-99	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
12	12	-8485	239	658	0	-236	122	6.28	6.28	9.42	9.42	2	0.02	0.02	0.08	0.00	0.00	24.0
13	12	-8395	240	312	0	-113	123	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
14	12	-9291	4	1114	0	-395	-22	6.28	6.28	9.42	9.42	2	0.03	0.03	0.13	0.00	0.00	24.0
15	12	-8990	6	-40	0	13	-21	6.28	6.28	9.42	9.42	2	0.00	0.00	0.00	0.00	0.00	24.0
16	12	-8968	112	1090	0	-388	44	6.28	6.28	9.42	9.42	2	0.03	0.03	0.13	0.00	0.00	24.0
17	12	-8667	114	-64	0	21	45	6.28	6.28	9.42	9.42	2	0.01	0.00	0.01	0.00	0.00	24.0

18	12	-14358	-422	1873	0	-660	-339	6.28	6.28	9.42	9.42	3	0.04	0.04	0.20	0.00	0.00	24.0
19	12	-12178	737	1455	0	-524	416	6.28	6.28	9.42	9.42	3	0.05	0.03	0.16	0.00	0.00	24.0
20	12	-12888	141	788	0	-295	32	6.28	6.28	9.42	9.42	3	0.01	0.02	0.09	0.00	0.00	24.0
37	12	-14498	-834	1700	0	-594	-598	6.28	6.28	9.42	9.42	3	0.06	0.04	0.19	0.00	0.00	24.0
38	12	-10875	1097	1005	0	-368	660	6.28	6.28	9.42	9.42	3	0.07	0.03	0.12	0.00	0.00	24.0
39	12	-12048	103	-108	0	14	20	6.28	6.28	9.42	9.42	3	0.00	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-11600	77	682	0	-329	25	6.28	6.28	9.42	9.42	3	0.02	0.02	0.08	0.00	0.00	24.0
2	25	-9506	-122	738	0	-353	-115	6.28	6.28	9.42	9.42	2	0.03	0.02	0.09	0.00	0.00	24.0
3	25	-9416	-121	392	0	-188	-114	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
4	25	-8428	239	658	0	-318	152	6.28	6.28	9.42	9.42	2	0.03	0.02	0.08	0.00	0.00	24.0
5	25	-8338	240	312	0	-152	153	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
6	25	-9234	4	1114	0	-535	-22	6.28	6.28	9.42	9.42	2	0.03	0.03	0.13	0.00	0.00	24.0
7	25	-8934	6	-40	0	18	-20	6.28	6.28	9.42	9.42	2	0.00	0.00	0.00	0.00	0.00	24.0
8	25	-8912	112	1090	0	-524	58	6.28	6.28	9.42	9.42	2	0.04	0.03	0.13	0.00	0.00	24.0
9	25	-8610	114	-64	0	29	60	6.28	6.28	9.42	9.42	2	0.01	0.00	0.01	0.00	0.00	24.0
10	25	-9506	-122	738	0	-353	-115	6.28	6.28	9.42	9.42	2	0.03	0.02	0.09	0.00	0.00	24.0
11	25	-9416	-121	392	0	-188	-114	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
12	25	-8428	239	658	0	-318	152	6.28	6.28	9.42	9.42	2	0.03	0.02	0.08	0.00	0.00	24.0
13	25	-8338	240	312	0	-152	153	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
14	25	-9234	4	1114	0	-535	-22	6.28	6.28	9.42	9.42	2	0.03	0.03	0.13	0.00	0.00	24.0
15	25	-8934	6	-40	0	18	-20	6.28	6.28	9.42	9.42	2	0.00	0.00	0.00	0.00	0.00	24.0
16	25	-8912	112	1090	0	-524	58	6.28	6.28	9.42	9.42	2	0.04	0.03	0.13	0.00	0.00	24.0
17	25	-8610	114	-64	0	29	60	6.28	6.28	9.42	9.42	2	0.01	0.00	0.01	0.00	0.00	24.0
18	25	-14285	-422	1873	0	-894	-392	6.28	6.28	9.42	9.42	3	0.05	0.04	0.21	0.00	0.00	24.0
19	25	-12105	737	1455	0	-706	508	6.28	6.28	9.42	9.42	3	0.06	0.03	0.16	0.00	0.00	24.0
20	25	-12815	141	788	0	-393	49	6.28	6.28	9.42	9.42	3	0.02	0.02	0.09	0.00	0.00	24.0
37	25	-14425	-834	1700	0	-807	-702	6.28	6.28	9.42	9.42	3	0.07	0.04	0.19	0.00	0.00	24.0
38	25	-10800	1097	1005	0	-494	797	6.28	6.28	9.42	9.42	3	0.08	0.03	0.12	0.00	0.00	24.0
39	25	-11975	103	-108	0	27	33	6.28	6.28	9.42	9.42	3	0.00	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-11525	77	682	0	-414	34	6.28	6.28	9.42	9.42	3	0.02	0.02	0.08	0.00	0.00	24.0
2	38	-9450	-122	738	0	-446	-130	6.28	6.28	9.42	9.42	2	0.03	0.02	0.09	0.00	0.00	24.0
3	38	-9360	-121	392	0	-237	-130	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
4	38	-8372	239	658	0	-400	182	6.28	6.28	9.42	9.42	2	0.04	0.02	0.08	0.00	0.00	24.0
5	38	-8282	240	312	0	-191	183	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
6	38	-9178	4	1114	0	-674	-21	6.28	6.28	9.42	9.42	2	0.04	0.03	0.13	0.00	0.00	24.0
7	38	-8877	6	-40	0	23	-20	6.28	6.28	9.42	9.42	2	0.00	0.00	0.00	0.00	0.00	24.0
8	38	-8855	112	1090	0	-660	72	6.28	6.28	9.42	9.42	2	0.04	0.03	0.13	0.00	0.00	24.0
9	38	-8554	114	-64	0	37	74	6.28	6.28	9.42	9.42	2	0.01	0.00	0.01	0.00	0.00	24.0
10	38	-9450	-122	738	0	-446	-130	6.28	6.28	9.42	9.42	2	0.03	0.02	0.09	0.00	0.00	24.0
11	38	-9360	-121	392	0	-237	-130	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
12	38	-8372	239	658	0	-400	182	6.28	6.28	9.42	9.42	2	0.04	0.02	0.08	0.00	0.00	24.0
13	38	-8282	240	312	0	-191	183	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
14	38	-9178	4	1114	0	-674	-21	6.28	6.28	9.42	9.42	2	0.04	0.03	0.13	0.00	0.00	24.0
15	38	-8877	6	-40	0	23	-20	6.28	6.28	9.42	9.42	2	0.00	0.00	0.00	0.00	0.00	24.0
16	38	-8855	112	1090	0	-660	72	6.28	6.28	9.42	9.42	2	0.04	0.03	0.13	0.00	0.00	24.0
17	38	-8554	114	-64	0	37	74	6.28	6.28	9.42	9.42	2	0.01	0.00	0.01	0.00	0.00	24.0
18	38	-14212	-422	1873	0	-1128	-445	6.28	6.28	9.42	9.42	3	0.07	0.04	0.21	0.00	0.00	24.0
19	38	-12032	737	1455	0	-888	600	6.28	6.28	9.42	9.42	3	0.07	0.03	0.17	0.00	0.00	24.0
20	38	-12742	141	788	0	-492	67	6.28	6.28	9.42	9.42	3	0.02	0.02	0.09	0.00	0.00	24.0
37	38	-14352	-834	1700	0	-1019	-807	6.28	6.28	9.42	9.42	3	0.09	0.04	0.19	0.00	0.00	24.0
38	38	-10725	1097	1005	0	-619	934	6.28	6.28	9.42	9.42	3	0.10	0.03	0.12	0.00	0.00	24.0
39	38	-11902	103	-108	0	41	46	6.28	6.28	9.42	9.42	3	0.00	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-11450	77	682	0	-499	44	6.28	6.28	9.42	9.42	3	0.02	0.02	0.08	0.00	0.00	24.0
2	50	-9394	-122	738	0	-538	-145	6.28	6.28	9.42	9.42	2	0.04	0.02	0.09	0.00	0.00	24.0
3	50	-9304	-121	392	0	-286	-145	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
4	50	-8316	239	658	0	-483	212	6.28	6.28	9.42	9.42	2	0.04	0.02	0.08	0.00	0.00	24.0
5	50	-8226	240	312	0	-230	213	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
6	50	-9122	4	1114	0	-813	-21	6.28	6.28	9.42	9.42	2	0.05	0.03	0.13	0.00	0.00	24.0
7	50	-8821	6	-40	0	28	-19	6.28	6.28	9.42	9.42	2	0.00	0.00	0.00	0.00	0.00	24.0
8	50	-8799	112	1090	0	-796	86	6.28	6.28	9.42	9.42	2	0.05	0.03	0.13	0.00	0.00	24.0
9	50	-8498	114	-64	0	45	88	6.28	6.28	9.42	9.42	2	0.01	0.00	0.01	0.00	0.00	24.0
10	50	-9394	-122	738	0	-538	-145	6.28	6.28	9.42	9.42	2	0.04	0.02	0.09	0.00	0.00	24.0
11	50	-9304	-121	392	0	-286	-145	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
12	50	-8316	239	658	0	-483	212	6.28	6.28	9.42	9.42	2	0.04	0.02	0.08	0.00	0.00	24.0
13	50	-8226	240	312	0	-230	213	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
14	50	-9122	4	1114	0	-813	-21	6.28	6.28	9.42	9.42	2	0.05	0.03	0.13	0.00	0.00	24.0
15	50	-8821	6	-40	0	28	-19	6.28	6.28	9.42	9.42	2	0.00	0.00	0.00	0.00	0.00	24.0
16	50	-8799	112	1090	0	-796	86	6.28	6.28	9.42	9.42	2	0.05	0.03	0.13	0.00	0.00	24.0
17	50	-8498	114	-64	0	45	88	6.28	6.28	9.42	9.42	2	0.01	0.00	0.01	0.00	0.00	24.0
18	50	-14140	-422	1873	0	-1362	-497	6.28	6.28	9.42	9.42	3	0.08	0.04	0.21	0.00	0.00	24.0
19	50	-11960	737	1455	0	-1070	692	6.28	6.28	9.42	9.42	3	0.08	0.03	0.17	0.00	0.00	24.0
20	50	-12670	141	788	0	-590	85	6.28	6.28	9.42	9.42	3	0.03	0.02	0.09	0.00	0.00	24.0
37	50	-14280	-834	1700	0	-1232	-911	6.28	6.28	9.42	9.42	3	0.10	0.04	0.19	0.00	0.00	24.0
38	50	-10650	1097	1005	0	-745	1071	6.28	6.28	9.42	9.42	3	0.11	0.03	0.12	0.00	0.00	24.0
39	50	-11830	103	-108	0	54	59	6.28	6.28	9.42	9.42	3	0.01	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 122 NI 805 NF 830 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 24
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-4213	24	363	0	-67	18	6.28	6.28	9.42	9.42	3	0.00	0.01	0.05	0.00	0.00	24.0
2	0	-3263	-4	376	0	-66	-13	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
3	0	-3252	-4	229	0	-49	-13	6.28	6.28	9.42	9.42	2	0.00	0.01	0.03	0.00	0.00	24.0
4	0	-3229	41	329	0	-54	41	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
5	0	-3218	42	182	0	-37	41	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
6	0	-3264	11	532	0	-82	5	6.28	6.28	9.42	9.42	2	0.01	0.01	0.07	0.00	0.00	24.0
7	0	-3227	12	41	0	-25	7	6.28	6.28	9.42	9.42	2	0.00	0.00	0.01	0.00	0.00	24.0
8	0	-3253	25	517	0	-78	22	6.28	6.28	9.42	9.42	2	0.01	0.01	0.07	0.00	0.00	24.0
9	0	-3217	26	27	0	-22	23	6.28	6.28	9.42	9.42	2	0.00	0.00	0.00	0.00	0.00	24.0
10	0	-3263	-4	376	0	-66	-13	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
11	0	-3252	-4	229	0	-49	-13	6.28	6.28	9.42	9.42	2	0.00	0.01	0.03	0.00	0.00	24.0
12	0	-3229	41	329	0	-54	41	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
13	0	-3218	42	182	0	-37	41	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0

14	0	-3264	11	532	0	-82	5	6.28	6.28	9.42	9.42	2	0.01	0.01	0.07	0.00	0.00	24.0
15	0	-3227	12	41	0	-25	7	6.28	6.28	9.42	9.42	2	0.00	0.00	0.01	0.00	0.00	24.0
16	0	-3253	25	517	0	-78	22	6.28	6.28	9.42	9.42	2	0.01	0.01	0.07	0.00	0.00	24.0
17	0	-3217	26	27	0	-22	23	6.28	6.28	9.42	9.42	2	0.00	0.00	0.00	0.00	0.00	24.0
18	0	-4600	-34	840	0	-123	-53	6.28	6.28	9.42	9.42	3	0.01	0.02	0.11	0.00	0.00	24.0
19	0	-4502	102	642	0	-84	112	6.28	6.28	9.42	9.42	3	0.01	0.02	0.08	0.00	0.00	24.0
20	0	-4519	33	346	0	-61	28	6.28	6.28	9.42	9.42	3	0.00	0.01	0.04	0.00	0.00	24.0
37	0	-4478	-83	784	0	-124	-112	6.28	6.28	9.42	9.42	3	0.01	0.02	0.10	0.00	0.00	24.0
38	0	-4315	145	454	0	-59	163	6.28	6.28	9.42	9.42	3	0.02	0.01	0.06	0.00	0.00	24.0
39	0	-4343	29	-39	0	-20	24	6.28	6.28	9.42	9.42	3	0.00	0.00	0.00	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-4140	24	363	0	-113	21	6.28	6.28	9.42	9.42	3	0.01	0.01	0.05	0.00	0.00	24.0
2	12	-3207	-4	376	0	-113	-14	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
3	12	-3196	-4	229	0	-78	-13	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
4	12	-3173	41	329	0	-95	46	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
5	12	-3162	42	182	0	-60	47	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
6	12	-3208	11	532	0	-148	7	6.28	6.28	9.42	9.42	2	0.01	0.01	0.07	0.00	0.00	24.0
7	12	-3171	12	41	0	-30	8	6.28	6.28	9.42	9.42	2	0.00	0.00	0.01	0.00	0.00	24.0
8	12	-3197	25	517	0	-143	25	6.28	6.28	9.42	9.42	2	0.01	0.01	0.07	0.00	0.00	24.0
9	12	-3161	26	27	0	-25	26	6.28	6.28	9.42	9.42	2	0.00	0.00	0.00	0.00	0.00	24.0
10	12	-3207	-4	376	0	-113	-14	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
11	12	-3196	-4	229	0	-78	-13	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
12	12	-3173	41	329	0	-95	46	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
13	12	-3162	42	182	0	-60	47	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
14	12	-3208	11	532	0	-148	7	6.28	6.28	9.42	9.42	2	0.01	0.01	0.07	0.00	0.00	24.0
15	12	-3171	12	41	0	-30	8	6.28	6.28	9.42	9.42	2	0.00	0.00	0.01	0.00	0.00	24.0
16	12	-3197	25	517	0	-143	25	6.28	6.28	9.42	9.42	2	0.01	0.01	0.07	0.00	0.00	24.0
17	12	-3161	26	27	0	-25	26	6.28	6.28	9.42	9.42	2	0.00	0.00	0.00	0.00	0.00	24.0
18	12	-4527	-34	840	0	-228	-57	6.28	6.28	9.42	9.42	3	0.01	0.02	0.11	0.00	0.00	24.0
19	12	-4429	102	642	0	-164	125	6.28	6.28	9.42	9.42	3	0.01	0.02	0.08	0.00	0.00	24.0
20	12	-4446	33	346	0	-104	32	6.28	6.28	9.42	9.42	3	0.01	0.01	0.04	0.00	0.00	24.0
37	12	-4405	-83	784	0	-222	-122	6.28	6.28	9.42	9.42	3	0.02	0.02	0.10	0.00	0.00	24.0
38	12	-4242	145	454	0	-116	181	6.28	6.28	9.42	9.42	3	0.02	0.01	0.06	0.00	0.00	24.0
39	12	-4270	29	-39	0	-15	27	6.28	6.28	9.42	9.42	3	0.00	0.00	0.00	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-4066	24	363	0	-158	24	6.28	6.28	9.42	9.42	3	0.01	0.01	0.05	0.00	0.00	24.0
2	25	-3150	-4	376	0	-160	-14	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
3	25	-3140	-4	229	0	-107	-14	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
4	25	-3116	41	329	0	-136	51	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
5	25	-3106	42	182	0	-83	52	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
6	25	-3152	11	532	0	-215	8	6.28	6.28	9.42	9.42	2	0.01	0.01	0.07	0.00	0.00	24.0
7	25	-3114	12	41	0	-36	10	6.28	6.28	9.42	9.42	2	0.00	0.00	0.01	0.00	0.00	24.0
8	25	-3140	25	517	0	-208	28	6.28	6.28	9.42	9.42	2	0.02	0.01	0.07	0.00	0.00	24.0
9	25	-3104	26	27	0	-28	29	6.28	6.28	9.42	9.42	2	0.00	0.00	0.00	0.00	0.00	24.0
10	25	-3150	-4	376	0	-160	-14	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
11	25	-3140	-4	229	0	-107	-14	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
12	25	-3116	41	329	0	-136	51	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
13	25	-3106	42	182	0	-83	52	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
14	25	-3152	11	532	0	-215	8	6.28	6.28	9.42	9.42	2	0.01	0.01	0.07	0.00	0.00	24.0
15	25	-3114	12	41	0	-36	10	6.28	6.28	9.42	9.42	2	0.00	0.00	0.01	0.00	0.00	24.0
16	25	-3140	25	517	0	-208	28	6.28	6.28	9.42	9.42	2	0.02	0.01	0.07	0.00	0.00	24.0
17	25	-3104	26	27	0	-28	29	6.28	6.28	9.42	9.42	2	0.00	0.00	0.00	0.00	0.00	24.0
18	25	-4454	-34	840	0	-333	-62	6.28	6.28	9.42	9.42	3	0.02	0.02	0.11	0.00	0.00	24.0
19	25	-4356	102	642	0	-245	137	6.28	6.28	9.42	9.42	3	0.02	0.02	0.08	0.00	0.00	24.0
20	25	-4373	33	346	0	-147	36	6.28	6.28	9.42	9.42	3	0.01	0.01	0.04	0.00	0.00	24.0
37	25	-4332	-83	784	0	-320	-132	6.28	6.28	9.42	9.42	3	0.02	0.02	0.10	0.00	0.00	24.0
38	25	-4169	145	454	0	-173	199	6.28	6.28	9.42	9.42	3	0.02	0.01	0.06	0.00	0.00	24.0
39	25	-4197	29	-39	0	-10	31	6.28	6.28	9.42	9.42	3	0.00	0.00	0.00	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-3993	24	363	0	-203	27	6.28	6.28	9.42	9.42	3	0.01	0.01	0.05	0.00	0.00	24.0
2	38	-3094	-4	376	0	-207	-15	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
3	38	-3083	-4	229	0	-135	-14	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
4	38	-3060	41	329	0	-178	57	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
5	38	-3049	42	182	0	-105	57	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
6	38	-3095	11	532	0	-281	10	6.28	6.28	9.42	9.42	2	0.02	0.01	0.07	0.00	0.00	24.0
7	38	-3058	12	41	0	-41	11	6.28	6.28	9.42	9.42	2	0.00	0.00	0.01	0.00	0.00	24.0
8	38	-3084	25	517	0	-272	31	6.28	6.28	9.42	9.42	2	0.02	0.01	0.07	0.00	0.00	24.0
9	38	-3048	26	27	0	-32	33	6.28	6.28	9.42	9.42	2	0.01	0.00	0.00	0.00	0.00	24.0
10	38	-3094	-4	376	0	-207	-15	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
11	38	-3083	-4	229	0	-135	-14	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
12	38	-3060	41	329	0	-178	57	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
13	38	-3049	42	182	0	-105	57	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
14	38	-3095	11	532	0	-281	10	6.28	6.28	9.42	9.42	2	0.02	0.01	0.07	0.00	0.00	24.0
15	38	-3058	12	41	0	-41	11	6.28	6.28	9.42	9.42	2	0.00	0.00	0.01	0.00	0.00	24.0
16	38	-3084	25	517	0	-272	31	6.28	6.28	9.42	9.42	2	0.02	0.01	0.07	0.00	0.00	24.0
17	38	-3048	26	27	0	-32	33	6.28	6.28	9.42	9.42	2	0.01	0.00	0.00	0.00	0.00	24.0
18	38	-4381	-34	840	0	-438	-66	6.28	6.28	9.42	9.42	3	0.02	0.02	0.11	0.00	0.00	24.0
19	38	-4283	102	642	0	-325	150	6.28	6.28	9.42	9.42	3	0.02	0.02	0.08	0.00	0.00	24.0
20	38	-4300	33	346	0	-190	40	6.28	6.28	9.42	9.42	3	0.01	0.01	0.04	0.00	0.00	24.0
37	38	-4258	-83	784	0	-418	-143	6.28	6.28	9.42	9.42	3	0.03	0.02	0.10	0.00	0.00	24.0
38	38	-4096	145	454	0	-230	217	6.28	6.28	9.42	9.42	3	0.03	0.01	0.06	0.00	0.00	24.0
39	38	-4124	29	-39	0	-5	34	6.28	6.28	9.42	9.42	3	0.00	0.00	0.00	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-3920	24	363	0	-249	30	6.28	6.28	9.42	9.42	3	0.01	0.01	0.05	0.00	0.00	24.0
2	50	-3038	-4	376	0	-254	-15	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
3	50	-3027	-4	229	0	-164	-15	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
4	50	-3004	41	329	0	-219	62	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
5	50	-2993	42	182	0	-128	62	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
6	50	-3039	11	532	0	-348	11	6.28	6.28	9.42	9.42	2	0.02	0.01	0.07	0.00	0.00	24.0
7	50	-3002	12	41	0	-46	13	6.28	6.28	9.42	9.42	2	0.00	0.00	0.01	0.00	0.00	24.0
8	50	-3028	25	517	0	-337	34	6.28	6.28	9.42	9.42	2	0.02	0.01	0.07	0.00	0.00	24.0
9	50	-2992	26	27	0	-35	36	6.28	6.28	9.42	9.42	2	0.01	0.00	0.00	0.00	0.00	24.0
10	50	-3038	-4	376	0	-254	-15	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
11	50	-3027	-4	229	0	-164	-15	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
12	50	-3004	41	329	0	-219	62	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
13	50	-2993	42	182	0	-128	62	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
14	50	-3039	11	532	0	-348	11	6.28	6.28	9.42	9.42	2	0.02	0.01	0.07	0.00	0.00	24.0
15	50	-3002	12	41	0	-46	13	6.28	6.28	9.42	9.42	2	0.00	0.00	0.01	0.00	0.00	24.0
16	50	-3028	25	517	0	-337	34	6.28	6.28	9.42	9.42	2	0.02	0.01	0.07	0.00	0.00	24.0
17	50	-2992	26	27	0	-35	36	6.28	6.28	9.42	9.42	2	0.01	0.00	0.00	0.00	0.00	24.0
18	50	-4308	-34	840	0	-543	-70	6.28	6.28	9.42	9.42	3	0.03	0.02	0.11	0.00	0.00	24.0
19	50	-4210	102	642	0	-405	163	6.28	6.28	9.42	9.42	3	0.03	0.02	0.08	0.00	0.00	24.0

20	50	-4227	33	346	0	-234	44	6.28	6.28	9.42	9.42	3	0.01	0.01	0.04	0.00	0.00	24.0
37	50	-4185	-83	784	0	-516	-153	6.28	6.28	9.42	9.42	3	0.03	0.02	0.10	0.00	0.00	24.0
38	50	-4023	145	454	0	-286	235	6.28	6.28	9.42	9.42	3	0.03	0.01	0.06	0.00	0.00	24.0
39	50	-4051	29	-39	0	-1	38	6.28	6.28	9.42	9.42	3	0.00	0.00	0.00	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 123 NI 830 NF 122 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 24A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-6195	85	1121	0	-249	27	6.28	6.28	9.42	9.42	3	0.01	0.03	0.14	0.00	0.00	24.0
2	0	-4788	-21	1139	0	-254	-12	6.28	6.28	9.42	9.42	2	0.02	0.03	0.15	0.00	0.00	24.0
3	0	-4774	-20	752	0	-164	-12	6.28	6.28	9.42	9.42	2	0.01	0.02	0.10	0.00	0.00	24.0
4	0	-4756	150	973	0	-219	53	6.28	6.28	9.42	9.42	2	0.02	0.02	0.12	0.00	0.00	24.0
5	0	-4743	151	586	0	-128	54	6.28	6.28	9.42	9.42	2	0.01	0.01	0.07	0.00	0.00	24.0
6	0	-4792	38	1533	0	-348	10	6.28	6.28	9.42	9.42	2	0.02	0.04	0.20	0.00	0.00	24.0
7	0	-4747	41	242	0	-46	12	6.28	6.28	9.42	9.42	2	0.00	0.01	0.03	0.00	0.00	24.0
8	0	-4783	89	1483	0	-337	30	6.28	6.28	9.42	9.42	2	0.02	0.03	0.19	0.00	0.00	24.0
9	0	-4738	93	192	0	-35	31	6.28	6.28	9.42	9.42	2	0.00	0.00	0.02	0.00	0.00	24.0
10	0	-4788	-21	1139	0	-254	-12	6.28	6.28	9.42	9.42	2	0.02	0.03	0.15	0.00	0.00	24.0
11	0	-4774	-20	752	0	-164	-12	6.28	6.28	9.42	9.42	2	0.01	0.02	0.10	0.00	0.00	24.0
12	0	-4756	150	973	0	-219	53	6.28	6.28	9.42	9.42	2	0.02	0.02	0.12	0.00	0.00	24.0
13	0	-4743	151	586	0	-128	54	6.28	6.28	9.42	9.42	2	0.01	0.01	0.07	0.00	0.00	24.0
14	0	-4792	38	1533	0	-348	10	6.28	6.28	9.42	9.42	2	0.02	0.04	0.20	0.00	0.00	24.0
15	0	-4747	41	242	0	-46	12	6.28	6.28	9.42	9.42	2	0.00	0.01	0.03	0.00	0.00	24.0
16	0	-4783	89	1483	0	-337	30	6.28	6.28	9.42	9.42	2	0.02	0.03	0.19	0.00	0.00	24.0
17	0	-4738	93	192	0	-35	31	6.28	6.28	9.42	9.42	2	0.00	0.00	0.02	0.00	0.00	24.0
18	0	-6755	-134	2381	0	-543	-59	6.28	6.28	9.42	9.42	3	0.03	0.06	0.29	0.00	0.00	24.0
19	0	-6665	376	1760	0	-405	140	6.28	6.28	9.42	9.42	3	0.02	0.04	0.22	0.00	0.00	24.0
20	0	-6673	117	1047	0	-234	39	6.28	6.28	9.42	9.42	3	0.01	0.02	0.13	0.00	0.00	24.0
37	0	-6545	-316	2279	0	-516	-129	6.28	6.28	9.42	9.42	3	0.03	0.05	0.28	0.00	0.00	24.0
38	0	-6394	535	1245	0	-286	201	6.28	6.28	9.42	9.42	3	0.02	0.03	0.15	0.00	0.00	24.0
39	0	-6407	102	57	0	-1	33	6.28	6.28	9.42	9.42	3	0.00	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-6122	85	1121	0	-389	38	6.28	6.28	9.42	9.42	3	0.02	0.03	0.14	0.00	0.00	24.0
2	12	-4732	-21	1139	0	-397	-15	6.28	6.28	9.42	9.42	2	0.03	0.03	0.15	0.00	0.00	24.0
3	12	-4718	-20	752	0	-258	-14	6.28	6.28	9.42	9.42	2	0.02	0.02	0.10	0.00	0.00	24.0
4	12	-4700	150	973	0	-340	72	6.28	6.28	9.42	9.42	2	0.03	0.02	0.12	0.00	0.00	24.0
5	12	-4687	151	586	0	-201	73	6.28	6.28	9.42	9.42	2	0.02	0.01	0.08	0.00	0.00	24.0
6	12	-4736	38	1533	0	-539	15	6.28	6.28	9.42	9.42	2	0.04	0.04	0.20	0.00	0.00	24.0
7	12	-4691	41	242	0	-76	17	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
8	12	-4727	89	1483	0	-522	41	6.28	6.28	9.42	9.42	2	0.04	0.03	0.19	0.00	0.00	24.0
9	12	-4682	93	192	0	-59	43	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
10	12	-4732	-21	1139	0	-397	-15	6.28	6.28	9.42	9.42	2	0.03	0.03	0.15	0.00	0.00	24.0
11	12	-4718	-20	752	0	-258	-14	6.28	6.28	9.42	9.42	2	0.02	0.02	0.10	0.00	0.00	24.0
12	12	-4700	150	973	0	-340	72	6.28	6.28	9.42	9.42	2	0.03	0.02	0.12	0.00	0.00	24.0
13	12	-4687	151	586	0	-201	73	6.28	6.28	9.42	9.42	2	0.02	0.01	0.08	0.00	0.00	24.0
14	12	-4736	38	1533	0	-539	15	6.28	6.28	9.42	9.42	2	0.04	0.04	0.20	0.00	0.00	24.0
15	12	-4691	41	242	0	-76	17	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
16	12	-4727	89	1483	0	-522	41	6.28	6.28	9.42	9.42	2	0.04	0.03	0.19	0.00	0.00	24.0
17	12	-4682	93	192	0	-59	43	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
18	12	-6682	-134	2381	0	-840	-76	6.28	6.28	9.42	9.42	3	0.04	0.06	0.29	0.00	0.00	24.0
19	12	-6592	376	1760	0	-625	187	6.28	6.28	9.42	9.42	3	0.04	0.04	0.22	0.00	0.00	24.0
20	12	-6600	117	1047	0	-365	54	6.28	6.28	9.42	9.42	3	0.02	0.02	0.13	0.00	0.00	24.0
37	12	-6472	-316	2279	0	-801	-169	6.28	6.28	9.42	9.42	3	0.04	0.05	0.28	0.00	0.00	24.0
38	12	-6321	535	1245	0	-442	268	6.28	6.28	9.42	9.42	3	0.03	0.03	0.15	0.00	0.00	24.0
39	12	-6334	102	57	0	-8	46	6.28	6.28	9.42	9.42	3	0.00	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-6048	85	1121	0	-529	48	6.28	6.28	9.42	9.42	3	0.03	0.03	0.14	0.00	0.00	24.0
2	25	-4676	-21	1139	0	-539	-18	6.28	6.28	9.42	9.42	2	0.04	0.03	0.15	0.00	0.00	24.0
3	25	-4662	-20	752	0	-352	-17	6.28	6.28	9.42	9.42	2	0.02	0.02	0.10	0.00	0.00	24.0
4	25	-4644	150	973	0	-462	91	6.28	6.28	9.42	9.42	2	0.04	0.02	0.12	0.00	0.00	24.0
5	25	-4630	151	586	0	-275	92	6.28	6.28	9.42	9.42	2	0.02	0.01	0.08	0.00	0.00	24.0
6	25	-4680	38	1533	0	-731	20	6.28	6.28	9.42	9.42	2	0.05	0.04	0.20	0.00	0.00	24.0
7	25	-4634	41	242	0	-106	22	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
8	25	-4670	89	1483	0	-708	52	6.28	6.28	9.42	9.42	2	0.05	0.03	0.19	0.00	0.00	24.0
9	25	-4626	93	192	0	-83	54	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
10	25	-4676	-21	1139	0	-539	-18	6.28	6.28	9.42	9.42	2	0.04	0.03	0.15	0.00	0.00	24.0
11	25	-4662	-20	752	0	-352	-17	6.28	6.28	9.42	9.42	2	0.02	0.02	0.10	0.00	0.00	24.0
12	25	-4644	150	973	0	-462	91	6.28	6.28	9.42	9.42	2	0.04	0.02	0.12	0.00	0.00	24.0
13	25	-4630	151	586	0	-275	92	6.28	6.28	9.42	9.42	2	0.02	0.01	0.08	0.00	0.00	24.0
14	25	-4680	38	1533	0	-731	20	6.28	6.28	9.42	9.42	2	0.05	0.04	0.20	0.00	0.00	24.0
15	25	-4634	41	242	0	-106	22	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
16	25	-4670	89	1483	0	-708	52	6.28	6.28	9.42	9.42	2	0.05	0.03	0.19	0.00	0.00	24.0
17	25	-4626	93	192	0	-83	54	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
18	25	-6609	-134	2381	0	-1138	-92	6.28	6.28	9.42	9.42	3	0.06	0.06	0.29	0.00	0.00	24.0
19	25	-6519	376	1760	0	-845	234	6.28	6.28	9.42	9.42	3	0.05	0.04	0.22	0.00	0.00	24.0
20	25	-6527	117	1047	0	-495	68	6.28	6.28	9.42	9.42	3	0.02	0.02	0.13	0.00	0.00	24.0
37	25	-6398	-316	2279	0	-1085	-208	6.28	6.28	9.42	9.42	3	0.06	0.05	0.28	0.00	0.00	24.0
38	25	-6248	535	1245	0	-598	335	6.28	6.28	9.42	9.42	3	0.04	0.03	0.16	0.00	0.00	24.0
39	25	-6261	102	57	0	-15	59	6.28	6.28	9.42	9.42	3	0.01	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-5975	85	1121	0	-669	59	6.28	6.28	9.42	9.42	3	0.03	0.03	0.14	0.00	0.00	24.0
2	38	-4619	-21	1139	0	-682	-20	6.28	6.28	9.42	9.42	2	0.04	0.03	0.15	0.00	0.00	24.0
3	38	-4605	-20	752	0	-446	-19	6.28	6.28	9.42	9.42	2	0.03	0.02	0.10	0.00	0.00	24.0
4	38	-4587	150	973	0	-584	110	6.28	6.28	9.42	9.42	2	0.04	0.02	0.12	0.00	0.00	24.0
5	38	-4574	151	586	0	-348	111	6.28	6.28	9.42	9.42	2	0.03	0.01	0.08	0.00	0.00	24.0
6	38	-4623	38	1533	0	-922	24	6.28	6.28	9.42	9.42	2	0.06	0.04	0.20	0.00	0.00	24.0
7	38	-4578	41	242	0	-136	27	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
8	38	-4614	89	1483	0	-893	63	6.28	6.28	9.42	9.42	2	0.06	0.03	0.19	0.00	0.00	24.0
9	38	-4569	93	192	0	-107	66	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
10	38	-4619	-21	1139	0	-682	-20	6.28	6.28	9.42	9.42	2	0.04	0.03	0.15	0.00	0.00	24.0
11	38	-4605	-20	752	0	-446	-19	6.28	6.28	9.42	9.42	2	0.03	0.02	0.10	0.00	0.00	24.0
12	38	-4587	150	973	0	-584	110	6.28	6.28	9.42	9.42	2	0.04	0.02	0.12	0.00	0.00	24.0
13	38	-4574	151	586	0	-348	111	6.28	6.28	9.42	9.42	2	0.03	0.01	0.08	0.00	0.00	24.0
14	38	-4623	38	1533	0	-922	24	6.28	6.28	9.42	9.42	2	0.06	0.04	0.20	0.00	0.00	24.0
15	38	-4578	41	242	0	-136	27	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0

16	38	-4614	89	1483	0	-893	63	6.28	6.28	9.42	9.42	2	0.06	0.03	0.19	0.00	0.00	24.0
17	38	-4569	93	192	0	-107	66	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
18	38	-6536	-134	2381	0	-1435	-109	6.28	6.28	9.42	9.42	3	0.07	0.06	0.30	0.00	0.00	24.0
19	38	-6446	376	1760	0	-1065	281	6.28	6.28	9.42	9.42	3	0.06	0.04	0.22	0.00	0.00	24.0
20	38	-6454	117	1047	0	-626	83	6.28	6.28	9.42	9.42	3	0.03	0.02	0.13	0.00	0.00	24.0
37	38	-6325	-316	2279	0	-1370	-248	6.28	6.28	9.42	9.42	3	0.07	0.05	0.28	0.00	0.00	24.0
38	38	-6175	535	1245	0	-753	402	6.28	6.28	9.42	9.42	3	0.05	0.03	0.16	0.00	0.00	24.0
39	38	-6188	102	57	0	-22	72	6.28	6.28	9.42	9.42	3	0.01	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-5902	85	1121	0	-809	69	6.28	6.28	9.42	9.42	3	0.04	0.03	0.14	0.00	0.00	24.0
2	50	-4563	-21	1139	0	-824	-23	6.28	6.28	9.42	9.42	2	0.05	0.03	0.15	0.00	0.00	24.0
3	50	-4549	-20	752	0	-540	-22	6.28	6.28	9.42	9.42	2	0.04	0.02	0.10	0.00	0.00	24.0
4	50	-4531	150	973	0	-705	128	6.28	6.28	9.42	9.42	2	0.05	0.02	0.12	0.00	0.00	24.0
5	50	-4518	151	586	0	-421	129	6.28	6.28	9.42	9.42	2	0.04	0.01	0.08	0.00	0.00	24.0
6	50	-4567	38	1533	0	-1114	29	6.28	6.28	9.42	9.42	2	0.07	0.04	0.20	0.00	0.00	24.0
7	50	-4522	41	242	0	-167	32	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
8	50	-4558	89	1483	0	-1079	74	6.28	6.28	9.42	9.42	2	0.07	0.03	0.19	0.00	0.00	24.0
9	50	-4513	93	192	0	-131	78	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
10	50	-4563	-21	1139	0	-824	-23	6.28	6.28	9.42	9.42	2	0.05	0.03	0.15	0.00	0.00	24.0
11	50	-4549	-20	752	0	-540	-22	6.28	6.28	9.42	9.42	2	0.04	0.02	0.10	0.00	0.00	24.0
12	50	-4531	150	973	0	-705	128	6.28	6.28	9.42	9.42	2	0.05	0.02	0.12	0.00	0.00	24.0
13	50	-4518	151	586	0	-421	129	6.28	6.28	9.42	9.42	2	0.04	0.01	0.08	0.00	0.00	24.0
14	50	-4567	38	1533	0	-1114	29	6.28	6.28	9.42	9.42	2	0.07	0.04	0.20	0.00	0.00	24.0
15	50	-4522	41	242	0	-167	32	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
16	50	-4558	89	1483	0	-1079	74	6.28	6.28	9.42	9.42	2	0.07	0.03	0.19	0.00	0.00	24.0
17	50	-4513	93	192	0	-131	78	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
18	50	-6463	-134	2381	0	-1733	-126	6.28	6.28	9.42	9.42	3	0.08	0.06	0.30	0.00	0.00	24.0
19	50	-6373	376	1760	0	-1285	328	6.28	6.28	9.42	9.42	3	0.07	0.04	0.22	0.00	0.00	24.0
20	50	-6381	117	1047	0	-757	97	6.28	6.28	9.42	9.42	3	0.04	0.02	0.13	0.00	0.00	24.0
37	50	-6252	-316	2279	0	-1655	-288	6.28	6.28	9.42	9.42	3	0.08	0.05	0.28	0.00	0.00	24.0
38	50	-6102	535	1245	0	-909	469	6.28	6.28	9.42	9.42	3	0.06	0.03	0.16	0.00	0.00	24.0
39	50	-6115	102	57	0	-29	84	6.28	6.28	9.42	9.42	3	0.01	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 124 NI 806 NF 833 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 23
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-3855	-192	616	0	-217	39	6.28	6.28	9.42	9.42	3	0.01	0.01	0.08	0.00	0.00	24.0
2	0	-3080	-179	536	0	-187	39	6.28	6.28	9.42	9.42	2	0.01	0.01	0.07	0.00	0.00	24.0
3	0	-2960	-179	427	0	-161	40	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
4	0	-2971	-116	521	0	-173	20	6.28	6.28	9.42	9.42	2	0.01	0.01	0.07	0.00	0.00	24.0
5	0	-2851	-116	411	0	-147	21	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
6	0	-3182	-157	659	0	-213	32	6.28	6.28	9.42	9.42	2	0.02	0.02	0.09	0.00	0.00	24.0
7	0	-2782	-157	293	0	-125	34	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
8	0	-3149	-138	654	0	-209	26	6.28	6.28	9.42	9.42	2	0.02	0.02	0.09	0.00	0.00	24.0
9	0	-2749	-138	288	0	-121	28	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
10	0	-3080	-179	536	0	-187	39	6.28	6.28	9.42	9.42	2	0.01	0.01	0.07	0.00	0.00	24.0
11	0	-2960	-179	427	0	-161	40	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
12	0	-2971	-116	521	0	-173	20	6.28	6.28	9.42	9.42	2	0.01	0.01	0.07	0.00	0.00	24.0
13	0	-2851	-116	411	0	-147	21	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
14	0	-3182	-157	659	0	-213	32	6.28	6.28	9.42	9.42	2	0.02	0.02	0.09	0.00	0.00	24.0
15	0	-2782	-157	293	0	-125	34	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
16	0	-3149	-138	654	0	-209	26	6.28	6.28	9.42	9.42	2	0.02	0.02	0.09	0.00	0.00	24.0
17	0	-2749	-138	288	0	-121	28	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
18	0	-4444	-296	939	0	-317	73	6.28	6.28	9.42	9.42	3	0.02	0.02	0.12	0.00	0.00	24.0
19	0	-4085	-104	862	0	-262	13	6.28	6.28	9.42	9.42	3	0.01	0.02	0.11	0.00	0.00	24.0
20	0	-3954	-199	618	0	-212	43	6.28	6.28	9.42	9.42	3	0.01	0.01	0.08	0.00	0.00	24.0
37	0	-4400	-355	867	0	-309	91	6.28	6.28	9.42	9.42	3	0.02	0.02	0.11	0.00	0.00	24.0
38	0	-3801	-37	738	0	-217	-9	6.28	6.28	9.42	9.42	3	0.01	0.02	0.10	0.00	0.00	24.0
39	0	-3584	-194	332	0	-134	42	6.28	6.28	9.42	9.42	3	0.01	0.01	0.04	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-3782	-192	616	0	-294	15	6.28	6.28	9.42	9.42	3	0.01	0.01	0.08	0.00	0.00	24.0
2	12	-3024	-179	536	0	-254	17	6.28	6.28	9.42	9.42	2	0.02	0.01	0.07	0.00	0.00	24.0
3	12	-2904	-179	427	0	-214	17	6.28	6.28	9.42	9.42	2	0.02	0.01	0.06	0.00	0.00	24.0
4	12	-2915	-116	521	0	-238	5	6.28	6.28	9.42	9.42	2	0.02	0.01	0.07	0.00	0.00	24.0
5	12	-2795	-116	411	0	-198	6	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
6	12	-3126	-157	659	0	-296	12	6.28	6.28	9.42	9.42	2	0.02	0.02	0.09	0.00	0.00	24.0
7	12	-2726	-157	293	0	-162	14	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
8	12	-3093	-138	654	0	-291	9	6.28	6.28	9.42	9.42	2	0.02	0.02	0.09	0.00	0.00	24.0
9	12	-2693	-138	288	0	-157	11	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
10	12	-3024	-179	536	0	-254	17	6.28	6.28	9.42	9.42	2	0.02	0.01	0.07	0.00	0.00	24.0
11	12	-2904	-179	427	0	-214	17	6.28	6.28	9.42	9.42	2	0.02	0.01	0.06	0.00	0.00	24.0
12	12	-2915	-116	521	0	-238	5	6.28	6.28	9.42	9.42	2	0.02	0.01	0.07	0.00	0.00	24.0
13	12	-2795	-116	411	0	-198	6	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
14	12	-3126	-157	659	0	-296	12	6.28	6.28	9.42	9.42	2	0.02	0.02	0.09	0.00	0.00	24.0
15	12	-2726	-157	293	0	-162	14	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
16	12	-3093	-138	654	0	-291	9	6.28	6.28	9.42	9.42	2	0.02	0.02	0.09	0.00	0.00	24.0
17	12	-2693	-138	288	0	-157	11	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
18	12	-4371	-296	939	0	-434	36	6.28	6.28	9.42	9.42	3	0.02	0.02	0.12	0.00	0.00	24.0
19	12	-4012	-104	862	0	-369	-0	6.28	6.28	9.42	9.42	3	0.02	0.02	0.11	0.00	0.00	24.0
20	12	-3881	-199	618	0	-289	19	6.28	6.28	9.42	9.42	3	0.01	0.01	0.08	0.00	0.00	24.0
37	12	-4327	-355	867	0	-417	47	6.28	6.28	9.42	9.42	3	0.02	0.02	0.11	0.00	0.00	24.0
38	12	-3728	-37	738	0	-309	-13	6.28	6.28	9.42	9.42	3	0.02	0.02	0.10	0.00	0.00	24.0
39	12	-3511	-194	332	0	-176	18	6.28	6.28	9.42	9.42	3	0.01	0.01	0.04	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-3709	-192	616	0	-371	-9	6.28	6.28	9.42	9.42	3	0.02	0.01	0.08	0.00	0.00	24.0
2	25	-2968	-179	536	0	-321	-6	6.28	6.28	9.42	9.42	2	0.02	0.01	0.07	0.00	0.00	24.0
3	25	-2848	-179	427	0	-267	-5	6.28	6.28	9.42	9.42	2	0.02	0.01	0.06	0.00	0.00	24.0
4	25	-2858	-116	521	0	-304	-9	6.28	6.28	9.42	9.42	2	0.02	0.01	0.07	0.00	0.00	24.0
5	25	-2738	-116	411	0	-250	-8	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
6	25	-3070	-157	659	0	-378	-8	6.28	6.28	9.42	9.42	2	0.03	0.02	0.09	0.00	0.00	24.0
7	25	-2670	-157	293	0	-198	-6	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
8	25	-3036	-138	654	0	-373	-9	6.28	6.28	9.42	9.42	2	0.02	0.02	0.09	0.00	0.00	24.0
9	25	-2636	-138	288	0	-193	-7	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
10	25	-2968	-179	536	0	-321	-6	6.28	6.28	9.42	9.42	2	0.02	0.01	0.07	0.00	0.00	24.0
11	25	-2848	-179	427	0	-267	-5	6.28	6.28	9.42	9.42	2	0.02	0.01	0.06	0.00	0.00	24.0

12	25	-2858	-116	521	0	-304	-9	6.28	6.28	9.42	9.42	2	0.02	0.01	0.07	0.00	0.00	24.0
13	25	-2738	-116	411	0	-250	-8	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
14	25	-3070	-157	659	0	-378	-8	6.28	6.28	9.42	9.42	2	0.03	0.02	0.09	0.00	0.00	24.0
15	25	-2670	-157	293	0	-198	-6	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
16	25	-3036	-138	654	0	-373	-9	6.28	6.28	9.42	9.42	2	0.02	0.02	0.09	0.00	0.00	24.0
17	25	-2636	-138	288	0	-193	-7	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
18	25	-4298	-296	939	0	-552	-1	6.28	6.28	9.42	9.42	3	0.03	0.02	0.12	0.00	0.00	24.0
19	25	-3938	-104	862	0	-477	-13	6.28	6.28	9.42	9.42	3	0.02	0.02	0.11	0.00	0.00	24.0
20	25	-3808	-199	618	0	-367	-6	6.28	6.28	9.42	9.42	3	0.02	0.01	0.08	0.00	0.00	24.0
37	25	-4254	-355	867	0	-526	3	6.28	6.28	9.42	9.42	3	0.03	0.02	0.11	0.00	0.00	24.0
38	25	-3655	-37	738	0	-401	-18	6.28	6.28	9.42	9.42	3	0.02	0.02	0.10	0.00	0.00	24.0
39	25	-3438	-194	332	0	-217	-6	6.28	6.28	9.42	9.42	3	0.01	0.01	0.04	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-3636	-192	616	0	-448	-33	6.28	6.28	9.42	9.42	3	0.02	0.01	0.08	0.00	0.00	24.0
2	38	-2911	-179	536	0	-388	-28	6.28	6.28	9.42	9.42	2	0.03	0.01	0.07	0.00	0.00	24.0
3	38	-2791	-179	427	0	-321	-27	6.28	6.28	9.42	9.42	2	0.02	0.01	0.06	0.00	0.00	24.0
4	38	-2802	-116	521	0	-369	-24	6.28	6.28	9.42	9.42	2	0.03	0.01	0.07	0.00	0.00	24.0
5	38	-2682	-116	411	0	-301	-23	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
6	38	-3013	-157	659	0	-460	-27	6.28	6.28	9.42	9.42	2	0.03	0.02	0.09	0.00	0.00	24.0
7	38	-2613	-157	293	0	-235	-25	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
8	38	-2980	-138	654	0	-455	-26	6.28	6.28	9.42	9.42	2	0.03	0.02	0.09	0.00	0.00	24.0
9	38	-2580	-138	288	0	-229	-24	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
10	38	-2911	-179	536	0	-388	-28	6.28	6.28	9.42	9.42	2	0.03	0.01	0.07	0.00	0.00	24.0
11	38	-2791	-179	427	0	-321	-27	6.28	6.28	9.42	9.42	2	0.02	0.01	0.06	0.00	0.00	24.0
12	38	-2802	-116	521	0	-369	-24	6.28	6.28	9.42	9.42	2	0.03	0.01	0.07	0.00	0.00	24.0
13	38	-2682	-116	411	0	-301	-23	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
14	38	-3013	-157	659	0	-460	-27	6.28	6.28	9.42	9.42	2	0.03	0.02	0.09	0.00	0.00	24.0
15	38	-2613	-157	293	0	-235	-25	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
16	38	-2980	-138	654	0	-455	-26	6.28	6.28	9.42	9.42	2	0.03	0.02	0.09	0.00	0.00	24.0
17	38	-2580	-138	288	0	-229	-24	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
18	38	-4225	-296	939	0	-669	-38	6.28	6.28	9.42	9.42	3	0.03	0.02	0.12	0.00	0.00	24.0
19	38	-3865	-104	862	0	-585	-26	6.28	6.28	9.42	9.42	3	0.03	0.02	0.11	0.00	0.00	24.0
20	38	-3734	-199	618	0	-444	-31	6.28	6.28	9.42	9.42	3	0.02	0.01	0.08	0.00	0.00	24.0
37	38	-4181	-355	867	0	-634	-42	6.28	6.28	9.42	9.42	3	0.03	0.02	0.11	0.00	0.00	24.0
38	38	-3582	-37	738	0	-494	-22	6.28	6.28	9.42	9.42	3	0.02	0.02	0.10	0.00	0.00	24.0
39	38	-3364	-194	332	0	-259	-31	6.28	6.28	9.42	9.42	3	0.01	0.01	0.04	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-3563	-192	616	0	-525	-57	6.28	6.28	9.42	9.42	3	0.03	0.01	0.08	0.00	0.00	24.0
2	50	-2855	-179	536	0	-455	-50	6.28	6.28	9.42	9.42	2	0.03	0.01	0.07	0.00	0.00	24.0
3	50	-2735	-179	427	0	-374	-50	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
4	50	-2746	-116	521	0	-434	-38	6.28	6.28	9.42	9.42	2	0.03	0.01	0.07	0.00	0.00	24.0
5	50	-2626	-116	411	0	-352	-38	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
6	50	-2957	-157	659	0	-543	-47	6.28	6.28	9.42	9.42	2	0.04	0.02	0.09	0.00	0.00	24.0
7	50	-2557	-157	293	0	-271	-45	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
8	50	-2924	-138	654	0	-536	-43	6.28	6.28	9.42	9.42	2	0.04	0.02	0.09	0.00	0.00	24.0
9	50	-2524	-138	288	0	-265	-41	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
10	50	-2855	-179	536	0	-455	-50	6.28	6.28	9.42	9.42	2	0.03	0.01	0.07	0.00	0.00	24.0
11	50	-2735	-179	427	0	-374	-50	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
12	50	-2746	-116	521	0	-434	-38	6.28	6.28	9.42	9.42	2	0.03	0.01	0.07	0.00	0.00	24.0
13	50	-2626	-116	411	0	-352	-38	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
14	50	-2957	-157	659	0	-543	-47	6.28	6.28	9.42	9.42	2	0.04	0.02	0.09	0.00	0.00	24.0
15	50	-2557	-157	293	0	-271	-45	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
16	50	-2924	-138	654	0	-536	-43	6.28	6.28	9.42	9.42	2	0.04	0.02	0.09	0.00	0.00	24.0
17	50	-2524	-138	288	0	-265	-41	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
18	50	-4152	-296	939	0	-786	-75	6.28	6.28	9.42	9.42	3	0.04	0.02	0.12	0.00	0.00	24.0
19	50	-3792	-104	862	0	-693	-39	6.28	6.28	9.42	9.42	3	0.03	0.02	0.11	0.00	0.00	24.0
20	50	-3661	-199	618	0	-521	-56	6.28	6.28	9.42	9.42	3	0.03	0.01	0.08	0.00	0.00	24.0
37	50	-4108	-355	867	0	-742	-86	6.28	6.28	9.42	9.42	3	0.04	0.02	0.11	0.00	0.00	24.0
38	50	-3509	-37	738	0	-586	-27	6.28	6.28	9.42	9.42	3	0.03	0.02	0.10	0.00	0.00	24.0
39	50	-3291	-194	332	0	-301	-55	6.28	6.28	9.42	9.42	3	0.02	0.01	0.04	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 125 NI 833 NF 209 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 23A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-4887	67	827	0	-602	-71	6.28	6.28	9.42	9.42	3	0.03	0.02	0.11	0.00	0.00	24.0
2	0	-3876	-9	760	0	-528	-65	6.28	6.28	9.42	9.42	2	0.04	0.02	0.10	0.00	0.00	24.0
3	0	-3769	-17	563	0	-431	-65	6.28	6.28	9.42	9.42	2	0.03	0.01	0.07	0.00	0.00	24.0
4	0	-3749	120	709	0	-495	-44	6.28	6.28	9.42	9.42	2	0.03	0.02	0.09	0.00	0.00	24.0
5	0	-3642	113	512	0	-397	-44	6.28	6.28	9.42	9.42	2	0.03	0.01	0.07	0.00	0.00	24.0
6	0	-3956	44	973	0	-630	-58	6.28	6.28	9.42	9.42	2	0.04	0.02	0.13	0.00	0.00	24.0
7	0	-3600	20	314	0	-306	-57	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
8	0	-3918	83	958	0	-620	-52	6.28	6.28	9.42	9.42	2	0.04	0.02	0.12	0.00	0.00	24.0
9	0	-3562	59	299	0	-296	-51	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
10	0	-3876	-9	760	0	-528	-65	6.28	6.28	9.42	9.42	2	0.04	0.02	0.10	0.00	0.00	24.0
11	0	-3769	-17	563	0	-431	-65	6.28	6.28	9.42	9.42	2	0.03	0.01	0.07	0.00	0.00	24.0
12	0	-3749	120	709	0	-495	-44	6.28	6.28	9.42	9.42	2	0.03	0.02	0.09	0.00	0.00	24.0
13	0	-3642	113	512	0	-397	-44	6.28	6.28	9.42	9.42	2	0.03	0.01	0.07	0.00	0.00	24.0
14	0	-3956	44	973	0	-630	-58	6.28	6.28	9.42	9.42	2	0.04	0.02	0.13	0.00	0.00	24.0
15	0	-3600	20	314	0	-306	-57	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
16	0	-3918	83	958	0	-620	-52	6.28	6.28	9.42	9.42	2	0.04	0.02	0.12	0.00	0.00	24.0
17	0	-3562	59	299	0	-296	-51	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
18	0	-5550	-73	1434	0	-926	-106	6.28	6.28	9.42	9.42	3	0.05	0.03	0.18	0.00	0.00	24.0
19	0	-5136	302	1211	0	-791	-43	6.28	6.28	9.42	9.42	3	0.04	0.03	0.15	0.00	0.00	24.0
20	0	-5068	85	799	0	-600	-75	6.28	6.28	9.42	9.42	3	0.03	0.02	0.10	0.00	0.00	24.0
37	0	-5499	-214	1338	0	-881	-125	6.28	6.28	9.42	9.42	3	0.04	0.03	0.17	0.00	0.00	24.0
38	0	-4809	410	968	0	-657	-21	6.28	6.28	9.42	9.42	3	0.03	0.02	0.12	0.00	0.00	24.0
39	0	-4697	49	280	0	-338	-74	6.28	6.28	9.42	9.42	3	0.02	0.01	0.04	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-4814	67	827	0	-705	-62	6.28	6.28	9.42	9.42	3	0.03	0.02	0.11	0.00	0.00	24.0
2	12	-3820	-9	760	0	-623	-66	6.28	6.28	9.42	9.42	2	0.04	0.02	0.10	0.00	0.00	24.0
3	12	-3713	-17	563	0	-501	-67	6.28	6.28	9.42	9.42	2	0.04	0.01	0.07	0.00	0.00	24.0
4	12	-3693	120	709	0	-583	-29	6.28	6.28	9.42	9.42	2	0.04	0.02	0.09	0.00	0.00	24.0
5	12	-3586	113	512	0	-461	-30	6.28	6.28	9.42	9.42	2	0.03	0.01	0.07	0.00	0.00	24.0
6	12	-3900	44	973	0	-752	-53	6.28	6.28	9.42	9.42	2	0.05	0.02	0.13	0.00	0.00	24.0
7	12	-3544	20	314	0	-345	-54	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0

8	12	-3862	83	958	0	-740	-42	6.28	6.28	9.42	9.42	2	0.05	0.02	0.12	0.00	0.00	24.0
9	12	-3506	59	299	0	-333	-43	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
10	12	-3820	-9	760	0	-623	-66	6.28	6.28	9.42	9.42	2	0.04	0.02	0.10	0.00	0.00	24.0
11	12	-3713	-17	563	0	-501	-67	6.28	6.28	9.42	9.42	2	0.04	0.01	0.07	0.00	0.00	24.0
12	12	-3693	120	709	0	-583	-29	6.28	6.28	9.42	9.42	2	0.04	0.02	0.09	0.00	0.00	24.0
13	12	-3586	113	512	0	-461	-30	6.28	6.28	9.42	9.42	2	0.03	0.01	0.07	0.00	0.00	24.0
14	12	-3900	44	973	0	-752	-53	6.28	6.28	9.42	9.42	2	0.05	0.02	0.13	0.00	0.00	24.0
15	12	-3544	20	314	0	-345	-54	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
16	12	-3862	83	958	0	-740	-42	6.28	6.28	9.42	9.42	2	0.05	0.02	0.12	0.00	0.00	24.0
17	12	-3506	59	299	0	-333	-43	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
18	12	-5477	-73	1434	0	-1105	-115	6.28	6.28	9.42	9.42	3	0.05	0.03	0.18	0.00	0.00	24.0
19	12	-5063	302	1211	0	-942	-5	6.28	6.28	9.42	9.42	3	0.05	0.03	0.15	0.00	0.00	24.0
20	12	-4995	85	799	0	-699	-64	6.28	6.28	9.42	9.42	3	0.03	0.02	0.10	0.00	0.00	24.0
37	12	-5426	-214	1338	0	-1049	-152	6.28	6.28	9.42	9.42	3	0.05	0.03	0.17	0.00	0.00	24.0
38	12	-4736	410	968	0	-778	31	6.28	6.28	9.42	9.42	3	0.04	0.02	0.12	0.00	0.00	24.0
39	12	-4624	49	280	0	-373	-68	6.28	6.28	9.42	9.42	3	0.02	0.01	0.04	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-4740	67	827	0	-808	-54	6.28	6.28	9.42	9.42	3	0.04	0.02	0.11	0.00	0.00	24.0
2	25	-3764	-9	760	0	-718	-67	6.28	6.28	9.42	9.42	2	0.05	0.02	0.10	0.00	0.00	24.0
3	25	-3656	-17	563	0	-572	-69	6.28	6.28	9.42	9.42	2	0.04	0.01	0.07	0.00	0.00	24.0
4	25	-3636	120	709	0	-672	-14	6.28	6.28	9.42	9.42	2	0.04	0.02	0.09	0.00	0.00	24.0
5	25	-3530	113	512	0	-525	-16	6.28	6.28	9.42	9.42	2	0.04	0.01	0.07	0.00	0.00	24.0
6	25	-3844	44	973	0	-874	-47	6.28	6.28	9.42	9.42	2	0.06	0.02	0.13	0.00	0.00	24.0
7	25	-3488	20	314	0	-384	-52	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
8	25	-3806	83	958	0	-860	-31	6.28	6.28	9.42	9.42	2	0.06	0.02	0.12	0.00	0.00	24.0
9	25	-3450	59	299	0	-370	-36	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
10	25	-3764	-9	760	0	-718	-67	6.28	6.28	9.42	9.42	2	0.05	0.02	0.10	0.00	0.00	24.0
11	25	-3656	-17	563	0	-572	-69	6.28	6.28	9.42	9.42	2	0.04	0.01	0.07	0.00	0.00	24.0
12	25	-3636	120	709	0	-672	-14	6.28	6.28	9.42	9.42	2	0.04	0.02	0.09	0.00	0.00	24.0
13	25	-3530	113	512	0	-525	-16	6.28	6.28	9.42	9.42	2	0.04	0.01	0.07	0.00	0.00	24.0
14	25	-3844	44	973	0	-874	-47	6.28	6.28	9.42	9.42	2	0.06	0.02	0.13	0.00	0.00	24.0
15	25	-3488	20	314	0	-384	-52	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
16	25	-3806	83	958	0	-860	-31	6.28	6.28	9.42	9.42	2	0.06	0.02	0.12	0.00	0.00	24.0
17	25	-3450	59	299	0	-370	-36	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
18	25	-5404	-73	1434	0	-1284	-124	6.28	6.28	9.42	9.42	3	0.06	0.03	0.18	0.00	0.00	24.0
19	25	-4990	302	1211	0	-1094	32	6.28	6.28	9.42	9.42	3	0.05	0.03	0.15	0.00	0.00	24.0
20	25	-4922	85	799	0	-799	-54	6.28	6.28	9.42	9.42	3	0.04	0.02	0.10	0.00	0.00	24.0
37	25	-5353	-214	1338	0	-1216	-179	6.28	6.28	9.42	9.42	3	0.06	0.03	0.17	0.00	0.00	24.0
38	25	-4663	410	968	0	-899	82	6.28	6.28	9.42	9.42	3	0.04	0.02	0.12	0.00	0.00	24.0
39	25	-4550	49	280	0	-408	-62	6.28	6.28	9.42	9.42	3	0.02	0.01	0.04	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-4667	67	827	0	-912	-46	6.28	6.28	9.42	9.42	3	0.04	0.02	0.11	0.00	0.00	24.0
2	38	-3707	-9	760	0	-814	-69	6.28	6.28	9.42	9.42	2	0.06	0.02	0.10	0.00	0.00	24.0
3	38	-3600	-17	563	0	-642	-71	6.28	6.28	9.42	9.42	2	0.05	0.01	0.07	0.00	0.00	24.0
4	38	-3580	120	709	0	-761	1	6.28	6.28	9.42	9.42	2	0.05	0.02	0.09	0.00	0.00	24.0
5	38	-3473	113	512	0	-589	-1	6.28	6.28	9.42	9.42	2	0.04	0.01	0.07	0.00	0.00	24.0
6	38	-3787	44	973	0	-995	-42	6.28	6.28	9.42	9.42	2	0.07	0.02	0.13	0.00	0.00	24.0
7	38	-3431	20	314	0	-423	-49	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
8	38	-3749	83	958	0	-979	-21	6.28	6.28	9.42	9.42	2	0.06	0.02	0.12	0.00	0.00	24.0
9	38	-3393	59	299	0	-407	-29	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
10	38	-3707	-9	760	0	-814	-69	6.28	6.28	9.42	9.42	2	0.06	0.02	0.10	0.00	0.00	24.0
11	38	-3600	-17	563	0	-642	-71	6.28	6.28	9.42	9.42	2	0.05	0.01	0.07	0.00	0.00	24.0
12	38	-3580	120	709	0	-761	1	6.28	6.28	9.42	9.42	2	0.05	0.02	0.09	0.00	0.00	24.0
13	38	-3473	113	512	0	-589	-1	6.28	6.28	9.42	9.42	2	0.04	0.01	0.07	0.00	0.00	24.0
14	38	-3787	44	973	0	-995	-42	6.28	6.28	9.42	9.42	2	0.07	0.02	0.13	0.00	0.00	24.0
15	38	-3431	20	314	0	-423	-49	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
16	38	-3749	83	958	0	-979	-21	6.28	6.28	9.42	9.42	2	0.06	0.02	0.12	0.00	0.00	24.0
17	38	-3393	59	299	0	-407	-29	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
18	38	-5330	-73	1434	0	-1464	-133	6.28	6.28	9.42	9.42	3	0.07	0.03	0.18	0.00	0.00	24.0
19	38	-4916	302	1211	0	-1246	70	6.28	6.28	9.42	9.42	3	0.06	0.03	0.15	0.00	0.00	24.0
20	38	-4849	85	799	0	-899	-43	6.28	6.28	9.42	9.42	3	0.04	0.02	0.10	0.00	0.00	24.0
37	38	-5280	-214	1338	0	-1384	-206	6.28	6.28	9.42	9.42	3	0.07	0.03	0.17	0.00	0.00	24.0
38	38	-4590	410	968	0	-1020	133	6.28	6.28	9.42	9.42	3	0.05	0.02	0.12	0.00	0.00	24.0
39	38	-4477	49	280	0	-443	-55	6.28	6.28	9.42	9.42	3	0.02	0.01	0.04	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-4594	67	827	0	-1015	-37	6.28	6.28	9.42	9.42	3	0.05	0.02	0.11	0.00	0.00	24.0
2	50	-3651	-9	760	0	-909	-70	6.28	6.28	9.42	9.42	2	0.06	0.02	0.10	0.00	0.00	24.0
3	50	-3544	-17	563	0	-712	-73	6.28	6.28	9.42	9.42	2	0.05	0.01	0.07	0.00	0.00	24.0
4	50	-3524	120	709	0	-849	16	6.28	6.28	9.42	9.42	2	0.06	0.02	0.09	0.00	0.00	24.0
5	50	-3417	113	512	0	-653	13	6.28	6.28	9.42	9.42	2	0.04	0.01	0.07	0.00	0.00	24.0
6	50	-3731	44	973	0	-1117	-36	6.28	6.28	9.42	9.42	2	0.07	0.02	0.13	0.00	0.00	24.0
7	50	-3375	20	314	0	-463	-47	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
8	50	-3693	83	958	0	-1099	-10	6.28	6.28	9.42	9.42	2	0.07	0.02	0.12	0.00	0.00	24.0
9	50	-3337	59	299	0	-445	-21	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
10	50	-3651	-9	760	0	-909	-70	6.28	6.28	9.42	9.42	2	0.06	0.02	0.10	0.00	0.00	24.0
11	50	-3544	-17	563	0	-712	-73	6.28	6.28	9.42	9.42	2	0.05	0.01	0.07	0.00	0.00	24.0
12	50	-3524	120	709	0	-849	16	6.28	6.28	9.42	9.42	2	0.06	0.02	0.09	0.00	0.00	24.0
13	50	-3417	113	512	0	-653	13	6.28	6.28	9.42	9.42	2	0.04	0.01	0.07	0.00	0.00	24.0
14	50	-3731	44	973	0	-1117	-36	6.28	6.28	9.42	9.42	2	0.07	0.02	0.13	0.00	0.00	24.0
15	50	-3375	20	314	0	-463	-47	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
16	50	-3693	83	958	0	-1099	-10	6.28	6.28	9.42	9.42	2	0.07	0.02	0.12	0.00	0.00	24.0
17	50	-3337	59	299	0	-445	-21	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
18	50	-5257	-73	1434	0	-1643	-142	6.28	6.28	9.42	9.42	3	0.08	0.03	0.18	0.00	0.00	24.0
19	50	-4843	302	1211	0	-1397	108	6.28	6.28	9.42	9.42	3	0.07	0.03	0.15	0.00	0.00	24.0
20	50	-4776	85	799	0	-999	-32	6.28	6.28	9.42	9.42	3	0.05	0.02	0.10	0.00	0.00	24.0
37	50	-5207	-214	1338	0	-1551	-232	6.28	6.28	9.42	9.42	3	0.08	0.03	0.17	0.00	0.00	24.0
38	50	-4517	410	968	0	-1141	184	6.28	6.28	9.42	9.42	3	0.06	0.02	0.12	0.00	0.00	24.0
39	50	-4404	49	280	0	-478	-49	6.28	6.28	9.42	9.42	3	0.02	0.01	0.04	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

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Lavoro: **D2403a** Intestazione lavoro: **Palestra Campobello**
Elemento: **PILASTRO** Gruppo: **2** Tabella: **Tabella pilastri**
Descrizione: **Pilastri**
Rck: **350.00** daN/cm^2 fyk: **4580.0** daN/cm^2 Condizioni ambientali: **Ordinaria**
Copriferro di calcolo: **5.0** cm Copriferro di disegno: **4.0** cm
Diametro staffe: **8** mm Numero braccia: **2**
ρ min.: **1.000** %

ASTA NUM. 1 NI 32 NF 26 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 32C
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-1225	1008	185	0	868	-985	4.02	4.02	10.05	10.05	-14.97	389.0
41	0	-910	942	402	0	977	-1078	4.02	4.02	10.05	10.05	-16.32	446.7
42	0	-496	963	773	0	1173	-1094	4.02	4.02	10.05	10.05	-16.47	515.4
43	0	-1084	1050	72	0	810	-956	4.02	4.02	10.05	10.05	-14.53	382.9
44	0	-482	834	760	0	1156	-1233	4.02	4.02	10.05	10.05	-18.55	538.4
45	0	130	974	1052	0	1318	-1138	4.02	4.02	10.05	10.05	-16.98	660.3
46	0	-349	936	455	0	999	-1133	4.02	4.02	10.05	10.05	-17.02	499.3
47	0	-209	934	468	0	1005	-1147	4.02	4.02	10.05	10.05	-17.20	512.6
49	0	-314	957	395	0	969	-1115	4.02	4.02	10.05	10.05	-16.74	492.8
50	0	-193	914	533	0	1038	-1171	4.02	4.02	10.05	10.05	-17.55	524.3
51	0	-71	942	591	0	1070	-1152	4.02	4.02	10.05	10.05	-17.24	521.7
apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)													
40	83	-854	939	185	0	716	-181	4.02	4.02	10.05	10.05	-6.73	251.9
41	83	-539	942	402	0	645	-301	4.02	4.02	10.05	10.05	-6.05	252.9
42	83	-125	963	620	0	598	-300	4.02	4.02	10.05	10.05	-5.51	278.0
43	83	-713	935	72	0	750	-138	4.02	4.02	10.05	10.05	-7.04	284.2
44	83	-111	949	760	0	529	-497	4.02	4.02	10.05	10.05	-7.46	245.8
45	83	501	974	798	0	554	-335	4.02	4.02	10.05	10.05	-4.86	332.0
46	83	22	936	455	0	624	-361	4.02	4.02	10.05	10.05	-5.69	308.0
47	83	162	934	468	0	619	-376	4.02	4.02	10.05	10.05	-5.58	322.2
49	83	57	934	395	0	642	-335	4.02	4.02	10.05	10.05	-5.84	321.2
50	83	178	937	533	0	598	-408	4.02	4.02	10.05	10.05	-6.05	314.1
51	83	300	942	541	0	603	-375	4.02	4.02	10.05	10.05	-5.53	331.2
apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)													
40	165	-482	871	185	0	564	566	4.02	4.02	10.05	10.05	-8.56	234.2
41	165	-167	942	402	0	313	476	4.02	4.02	10.05	10.05	-7.15	208.5
42	165	246	963	468	0	150	494	4.02	4.02	10.05	10.05	-7.33	237.7
43	165	-342	820	72	0	690	586	4.02	4.02	10.05	10.05	-8.84	297.6
44	165	261	1064	760	0	-98	333	4.02	4.02	10.05	10.05	-4.90	164.8
45	165	872	974	544	0	0	468	4.02	4.02	10.05	10.05	-6.73	257.4
46	165	393	936	455	0	249	411	4.02	4.02	10.05	10.05	-6.04	207.1
47	165	534	934	468	0	233	395	4.02	4.02	10.05	10.05	-5.75	206.9
49	165	429	911	395	0	316	425	4.02	4.02	10.05	10.05	-6.24	215.4
50	165	549	959	533	0	159	375	4.02	4.02	10.05	10.05	-5.44	198.5
51	165	671	942	490	0	178	402	4.02	4.02	10.05	10.05	-5.80	216.9
apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)													
40	248	-111	802	185	0	412	1256	4.02	4.02	10.05	10.05	-18.80	567.0
41	248	204	942	402	0	-18	1252	4.02	4.02	10.05	10.05	-18.67	581.1
42	248	617	963	316	0	-173	1289	4.02	4.02	10.05	10.05	-19.11	618.4
43	248	30	706	72	0	631	1215	4.02	4.02	10.05	10.05	-18.16	555.6
44	248	632	1178	760	0	-724	1258	4.02	4.02	10.05	10.05	-18.64	604.9
45	248	1244	974	291	0	-344	1271	4.02	4.02	10.05	10.05	-18.66	641.8
46	248	765	936	455	0	-126	1183	4.02	4.02	10.05	10.05	-17.48	577.6
47	248	905	934	468	0	-153	1166	4.02	4.02	10.05	10.05	-17.19	576.9
49	248	800	888	395	0	-10	1167	4.02	4.02	10.05	10.05	-17.23	572.1
50	248	921	982	533	0	-281	1176	4.02	4.02	10.05	10.05	-17.33	582.2
51	248	1043	942	439	0	-205	1178	4.02	4.02	10.05	10.05	-17.33	589.4
apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)													
40	330	260	733	185	0	259	1889	4.02	4.02	10.05	10.05	-28.18	874.2
41	330	575	942	402	0	-350	2029	4.02	4.02	10.05	10.05	-30.19	953.7
42	330	989	963	163	0	-371	2083	4.02	4.02	10.05	10.05	-30.88	999.0
43	330	401	591	72	0	571	1750	4.02	4.02	10.05	10.05	-26.06	817.9
44	330	1003	1293	760	0	-1351	2277	4.02	4.02	10.05	10.05	-33.78	1088.2
45	330	1615	974	37	0	-479	2074	4.02	4.02	10.05	10.05	-30.57	1026.4
46	330	1136	936	455	0	-502	1955	4.02	4.02	10.05	10.05	-28.93	948.1
47	330	1276	934	468	0	-539	1937	4.02	4.02	10.05	10.05	-28.62	946.9
49	330	1171	865	395	0	-336	1890	4.02	4.02	10.05	10.05	-27.94	920.2
50	330	1292	1005	533	0	-721	1996	4.02	4.02	10.05	10.05	-29.50	974.6
51	330	1414	942	388	0	-546	1955	4.02	4.02	10.05	10.05	-28.85	962.1
apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)													

ASTA NUM. 2 NI 33 NF 32 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 32B
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	

40	0	-7177	150	167	0	-10	-123	4.02	4.02	10.05	10.05	-4.53	-62.4
41	0	-6882	10	171	0	40	-17	4.02	4.02	10.05	10.05	-3.78	-56.2
42	0	-6526	-4	656	0	515	15	4.02	4.02	10.05	10.05	-5.91	-82.4
43	0	-7007	265	175	0	-2	-232	4.02	4.02	10.05	10.05	-5.44	-71.1
44	0	-6491	-226	177	0	122	166	4.02	4.02	10.05	10.05	-4.60	-61.4
45	0	-5921	9	989	0	872	-2	4.02	4.02	10.05	10.05	-7.54	-101.6
46	0	-6294	47	186	0	105	-79	4.02	4.02	10.05	10.05	-3.79	-55.5
47	0	-6147	56	190	0	121	-94	4.02	4.02	10.05	10.05	-3.79	-55.4
49	0	-6246	102	189	0	104	-130	4.02	4.02	10.05	10.05	-4.15	-56.3
50	0	-6143	4	190	0	129	-50	4.02	4.02	10.05	10.05	-3.83	-55.8
51	0	-6029	51	352	0	279	-83	4.02	4.02	10.05	10.05	-4.50	-64.1

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	110	-6682	80	167	0	-194	3	4.02	4.02	10.05	10.05	-4.42	-64.0
41	110	-6387	10	171	0	-148	-6	4.02	4.02	10.05	10.05	-4.05	-58.9
42	110	-6031	-4	453	0	-95	11	4.02	4.02	10.05	10.05	-3.60	-52.9
43	110	-6512	150	175	0	-195	-4	4.02	4.02	10.05	10.05	-4.34	-62.7
44	110	-5996	-110	177	0	-73	-19	4.02	4.02	10.05	10.05	-3.48	-51.3
45	110	-5426	9	651	0	-30	8	4.02	4.02	10.05	10.05	-2.97	-44.2
46	110	-5799	47	186	0	-100	-27	4.02	4.02	10.05	10.05	-3.51	-51.4
47	110	-5652	56	190	0	-88	-33	4.02	4.02	10.05	10.05	-3.37	-49.5
49	110	-5751	79	189	0	-104	-29	4.02	4.02	10.05	10.05	-3.50	-51.2
50	110	-5648	27	190	0	-79	-32	4.02	4.02	10.05	10.05	-3.33	-49.0
51	110	-5534	51	284	0	-71	-27	4.02	4.02	10.05	10.05	-3.23	-47.5

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	220	-6187	11	167	0	-378	54	4.02	4.02	10.05	10.05	-5.06	-71.3
41	220	-5892	10	171	0	-336	6	4.02	4.02	10.05	10.05	-4.70	-66.5
42	220	-5536	-4	250	0	-481	6	4.02	4.02	10.05	10.05	-5.23	-72.6
43	220	-6017	34	175	0	-387	97	4.02	4.02	10.05	10.05	-5.02	-70.6
44	220	-5501	5	177	0	-268	-76	4.02	4.02	10.05	10.05	-4.17	-59.3
45	220	-4931	9	312	0	-559	18	4.02	4.02	10.05	10.05	-5.30	-72.6
46	220	-5304	47	186	0	-306	24	4.02	4.02	10.05	10.05	-4.25	-60.0
47	220	-5157	56	190	0	-298	29	4.02	4.02	10.05	10.05	-4.14	-58.4
49	220	-5256	56	189	0	-312	45	4.02	4.02	10.05	10.05	-4.26	-60.1
50	220	-5153	50	190	0	-288	10	4.02	4.02	10.05	10.05	-4.09	-57.8
51	220	-5039	51	217	0	-346	29	4.02	4.02	10.05	10.05	-4.31	-60.5

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	330	-5692	-58	167	0	-562	28	4.02	4.02	10.05	10.05	-5.70	-78.7
41	330	-5397	10	171	0	-524	17	4.02	4.02	10.05	10.05	-5.36	-74.1
42	330	-5041	-4	47	0	-644	2	4.02	4.02	10.05	10.05	-5.81	-79.1
43	330	-5522	-81	175	0	-579	71	4.02	4.02	10.05	10.05	-5.70	-78.4
44	330	-5006	121	177	0	-463	-7	4.02	4.02	10.05	10.05	-4.86	-67.3
45	330	-4436	9	-26	0	-716	28	4.02	4.02	10.05	10.05	-6.09	-81.3
46	330	-4809	47	186	0	-511	76	4.02	4.02	10.05	10.05	-4.99	-68.7
47	330	-4662	56	190	0	-507	91	4.02	4.02	10.05	10.05	-4.90	-67.3
49	330	-4761	33	189	0	-520	94	4.02	4.02	10.05	10.05	-5.01	-68.9
50	330	-4658	74	190	0	-497	79	4.02	4.02	10.05	10.05	-4.85	-66.6
51	330	-4544	51	149	0	-547	86	4.02	4.02	10.05	10.05	-5.05	-69.0

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	440	-5197	-128	167	0	-746	-75	4.02	4.02	10.05	10.05	-6.49	-87.6
41	440	-4902	10	171	0	-712	28	4.02	4.02	10.05	10.05	-6.17	-83.3
42	440	-4546	-4	-157	0	-584	-3	4.02	4.02	10.05	10.05	-5.25	-71.5
43	440	-5027	-197	175	0	-771	-81	4.02	4.02	10.05	10.05	-6.61	-88.8
44	440	-4511	236	177	0	-657	189	4.02	4.02	10.05	10.05	-5.70	-76.8
45	440	-3941	9	-365	0	-501	38	4.02	4.02	10.05	10.05	-4.53	-61.7
46	440	-4314	47	186	0	-716	128	4.02	4.02	10.05	10.05	-6.06	-80.8
47	440	-4167	56	190	0	-717	153	4.02	4.02	10.05	10.05	-6.05	-80.3
49	440	-4266	10	189	0	-728	118	4.02	4.02	10.05	10.05	-6.15	-81.7
50	440	-4163	97	190	0	-705	172	4.02	4.02	10.05	10.05	-5.96	-79.3
51	440	-4049	51	81	0	-674	142	4.02	4.02	10.05	10.05	-5.71	-76.0

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

ASTA NUM. 3 NI 27 NF 25 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 7C
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	--												
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	4909	-563	794	0	1160	1030	4.02	4.02	10.05	10.05	-13.38	1185.0
41	0	4713	-758	691	0	1076	1053	4.02	4.02	10.05	10.05	-13.86	1119.8
42	0	5333	-775	1094	0	1198	1064	4.02	4.02	10.05	10.05	-13.67	1257.7
43	0	4945	-443	838	0	1221	1043	4.02	4.02	10.05	10.05	-13.57	1218.7
44	0	4331	-1089	520	0	934	1092	4.02	4.02	10.05	10.05	-14.67	1002.9
45	0	5653	-796	1337	0	1284	1099	4.02	4.02	10.05	10.05	-14.03	1339.9
46	0	4562	-774	651	0	1083	1096	4.02	4.02	10.05	10.05	-14.61	1103.6
47	0	4524	-777	641	0	1085	1107	4.02	4.02	10.05	10.05	-14.80	1099.7
49	0	4589	-712	676	0	1113	1100	4.02	4.02	10.05	10.05	-14.66	1121.4
50	0	4466	-842	612	0	1056	1110	4.02	4.02	10.05	10.05	-14.88	1078.4
51	0	4731	-783	775	0	1126	1111	4.02	4.02	10.05	10.05	-14.75	1145.9

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	83	5280	-689	794	0	505	513	4.02	4.02	10.05	10.05	-4.30	907.6
41	83	5084	-758	691	0	506	427	4.02	4.02	10.05	10.05	-2.69	883.8
42	83	5704	-775	942	0	359	424	4.02	4.02	10.05	10.05	-1.60	887.7
43	83	5316	-652	838	0	529	591	4.02	4.02	10.05	10.05	-5.76	924.2
44	83	4702	-879	520	0	505	280	4.02	4.02	10.05	10.05	0.00	835.8
45	83	6024	-796	1083	0	286	442	4.02	4.02	10.05	10.05	-1.52	891.2
46	83	4933	-774	651	0	546	458	4.02	4.02	10.05	10.05	-3.57	885.0
47	83	4895	-777	641	0	556	466	4.02	4.02	10.05	10.05	-3.78	885.2
49	83	4960	-754	676	0	556	495	4.02	4.02	10.05	10.05	-4.29	893.0
50	83	4837	-800	612	0	551	433	4.02	4.02	10.05	10.05	-3.16	875.5
51	83	5102	-783	725	0	507	465	4.02	4.02	10.05	10.05	-3.51	886.6

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	165	5652	-815	794	0	-150	-107	4.02	4.02	10.05	10.05	0.00	777.6
41	165	5456	-758	691	0	-64	-198	4.02	4.02	10.05	10.05	0.00	710.2
42	165	6076	-775	789	0	-355	-216	4.02	4.02	10.05	10.05	0.00	931.9
43	165	5688	-862	838	0	-162	-34	4.02	4.02	10.05	10.05	0.00	788.0
44	165	5074	-670	520	0	76	-359	4.02	4.02	10.05	10.05	-0.83	668.5
45	165	6396	-796	829	0	-503	-214	4.02	4.02	10.05	10.05	0.00	1045.4
46	165	5304	-774	651	0	9	-180	4.02	4.02	10.05	10.05	0.00	664.0
47	165	5266	-777	641	0	27	-176	4.02	4.02	10.05	10.05	0.00	668.3
49	165	5332	-796	676	0	-2	-145	4.02	4.02	10.05	10.05	0.00	663.9
50	165	5208	-758	612	0	46	-210	4.02	4.02	10.05	10.05	0.00	670.5
51	165	5474	-783	674	0	-70	-181	4.02	4.02	10.05	10.05	0.00	715.3

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	248	6023	-940	794	0	-806	-831	4.02	4.02	10.05	10.05	-9.38	1149.6
41	248	5827	-758	691	0	-634	-824	4.02	4.02	10.05	10.05	-9.42	1039.8
42	248	6447	-775	637	0	-943	-855	4.02	4.02	10.05	10.05	-9.45	1270.5
43	248	6059	-1072	838	0	-854	-831	4.02	4.02	10.05	10.05	-9.36	1178.2
44	248	5445	-460	520	0	-354	-825	4.02	4.02	10.05	10.05	-9.72	852.9
45	248	6767	-796	575	0	-1082	-871	4.02	4.02	10.05	10.05	-9.46	1379.6
46	248	5676	-774	651	0	-528	-819	4.02	4.02	10.05	10.05	-9.44	968.3
47	248	5638	-777	641	0	-502	-817	4.02	4.02	10.05	10.05	-9.44	950.7
49	248	5703	-838	676	0	-560	-819	4.02	4.02	10.05	10.05	-9.43	987.4
50	248	5580	-716	612	0	-459	-818	4.02	4.02	10.05	10.05	-9.50	922.0
51	248	5845	-783	623	0	-605	-827	4.02	4.02	10.05	10.05	-9.45	1027.6

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	330	6394	-1066	794	0	-1461	-1659	4.02	4.02	10.05	10.05	-22.39	1519.7
41	330	6198	-758	691	0	-1204	-1450	4.02	4.02	10.05	10.05	-19.24	1369.5
42	330	6818	-775	484	0	-1405	-1495	4.02	4.02	10.05	10.05	-19.60	1546.5
43	330	6430	-1281	838	0	-1546	-1802	4.02	4.02	10.05	10.05	-24.58	1564.8
44	330	5816	-251	520	0	-783	-1118	4.02	4.02	10.05	10.05	-14.23	1112.5
45	330	7138	-796	321	0	-1452	-1528	4.02	4.02	10.05	10.05	-19.94	1609.7
46	330	6047	-774	651	0	-1065	-1457	4.02	4.02	10.05	10.05	-19.44	1281.6
47	330	6009	-777	641	0	-1031	-1458	4.02	4.02	10.05	10.05	-19.47	1259.9
49	330	6074	-880	676	0	-1117	-1528	4.02	4.02	10.05	10.05	-20.52	1310.8
50	330	5951	-674	612	0	-964	-1391	4.02	4.02	10.05	10.05	-18.46	1219.4
51	330	6216	-783	572	0	-1098	-1473	4.02	4.02	10.05	10.05	-19.59	1319.0

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

ASTA NUM. 4 NI 23 NF 27 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 7B
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-1289	140	345	0	527	62	4.02	4.02	10.05	10.05	-4.86	117.5
41	0	-1420	-133	307	0	404	274	4.02	4.02	10.05	10.05	-4.24	60.0
42	0	-851	-124	805	0	895	257	4.02	4.02	10.05	10.05	-8.40	338.8
43	0	-1265	310	366	0	612	-65	4.02	4.02	10.05	10.05	-5.70	158.7
44	0	-1702	-586	244	0	196	628	4.02	4.02	10.05	10.05	-9.67	204.8
45	0	-536	-131	1132	0	1224	261	4.02	4.02	10.05	10.05	-11.36	535.6
46	0	-1523	-152	299	0	407	300	4.02	4.02	10.05	10.05	-4.63	66.7
47	0	-1549	-157	297	0	408	306	4.02	4.02	10.05	10.05	-4.73	68.4
49	0	-1505	-66	310	0	449	235	4.02	4.02	10.05	10.05	-4.00	65.6
50	0	-1592	-245	285	0	366	374	4.02	4.02	10.05	10.05	-5.77	96.0
51	0	-1359	-154	463	0	572	300	4.02	4.02	10.05	10.05	-5.28	130.9

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	110	-794	13	345	0	148	146	4.02	4.02	10.05	10.05	-2.25	30.3
41	110	-925	-133	307	0	66	128	4.02	4.02	10.05	10.05	-1.97	-19.9
42	110	-356	-124	602	0	121	120	4.02	4.02	10.05	10.05	-1.85	37.8
43	110	-770	99	366	0	210	160	4.02	4.02	10.05	10.05	-2.48	37.6
44	110	-1207	-375	244	0	-72	99	4.02	4.02	10.05	10.05	-1.55	-18.1
45	110	-41	-131	793	0	165	118	4.02	4.02	10.05	10.05	-1.77	75.8
46	110	-1028	-152	299	0	78	133	4.02	4.02	10.05	10.05	-2.03	-21.0
47	110	-1054	-157	297	0	81	134	4.02	4.02	10.05	10.05	-2.05	-21.3
49	110	-1010	-108	310	0	109	140	4.02	4.02	10.05	10.05	-2.14	-21.7
50	110	-1097	-203	285	0	52	127	4.02	4.02	10.05	10.05	-1.95	-20.8
51	110	-864	-154	395	0	100	131	4.02	4.02	10.05	10.05	-2.02	21.6

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	220	-299	-113	345	0	-232	91	4.02	4.02	10.05	10.05	-2.18	79.2
41	220	-430	-133	307	0	-272	-18	4.02	4.02	10.05	10.05	-2.55	84.0
42	220	139	-124	399	0	-430	-17	4.02	4.02	10.05	10.05	-3.85	226.8
43	220	-275	-112	366	0	-192	153	4.02	4.02	10.05	10.05	-2.34	62.6
44	220	-712	-164	244	0	-340	-197	4.02	4.02	10.05	10.05	-3.17	87.5
45	220	454	-131	455	0	-522	-26	4.02	4.02	10.05	10.05	-4.49	310.2
46	220	-533	-152	299	0	-250	-35	4.02	4.02	10.05	10.05	-2.33	63.3
47	220	-559	-157	297	0	-245	-39	4.02	4.02	10.05	10.05	-2.27	58.4
49	220	-515	-150	310	0	-232	-2	4.02	4.02	10.05	10.05	-2.15	56.6
50	220	-602	-161	285	0	-261	-72	4.02	4.02	10.05	10.05	-2.42	61.8
51	220	-369	-154	327	0	-298	-38	4.02	4.02	10.05	10.05	-2.80	103.2

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	330	196	-240	345	0	-612	-104	4.02	4.02	10.05	10.05	-5.48	322.7
41	330	65	-133	307	0	-609	-164	4.02	4.02	10.05	10.05	-5.53	305.7
42	330	634	-124	196	0	-757	-153	4.02	4.02	10.05	10.05	-6.53	446.9
43	330	220	-323	366	0	-594	-87	4.02	4.02	10.05	10.05	-5.31	317.1
44	330	-217	47	244	0	-609	-262	4.02	4.02	10.05	10.05	-5.63	272.1
45	330	949	-131	116	0	-836	-169	4.02	4.02	10.05	10.05	-7.01	524.4
46	330	-38	-152	299	0	-579	-202	4.02	4.02	10.05	10.05	-5.30	278.7
47	330	-64	-157	297	0	-571	-211	4.02	4.02	10.05	10.05	-5.24	272.0
49	330	-20	-192	310	0	-572	-191	4.02	4.02	10.05	10.05	-5.23	277.6
50	330	-107	-118	285	0	-575	-226	4.02	4.02	10.05	10.05	-5.29	268.6
51	330	126	-154	260	0	-621	-207	4.02	4.02	10.05	10.05	-5.60	318.7

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	440	691	-367	345	0	-991	-438	4.02	4.02	10.05	10.05	-8.66	568.4

41	440	560	-133	307	0	-947	-311	4.02	4.02	10.05	10.05	-8.33	530.6
42	440	1129	-124	-8	0	-860	-290	4.02	4.02	10.05	10.05	-7.08	558.5
43	440	715	-535	366	0	-996	-559	4.02	4.02	10.05	10.05	-8.69	573.8
44	440	278	258	244	0	-877	-94	4.02	4.02	10.05	10.05	-7.86	462.3
45	440	1444	-131	-222	0	-778	-313	4.02	4.02	10.05	10.05	-5.95	558.0
46	440	457	-152	299	0	-908	-369	4.02	4.02	10.05	10.05	-8.04	499.0
47	440	431	-157	297	0	-898	-383	4.02	4.02	10.05	10.05	-7.97	491.1
49	440	475	-235	310	0	-913	-426	4.02	4.02	10.05	10.05	-8.08	503.7
50	440	388	-76	285	0	-889	-333	4.02	4.02	10.05	10.05	-7.91	481.4
51	440	621	-154	192	0	-869	-377	4.02	4.02	10.05	10.05	-7.58	500.1

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

ASTA NUM. 5 NI 34 NF 35 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 12C
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	--												
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-10320	-446	457	0	-694	716	6.03	6.03	10.05	10.05	-7.51	-98.8
41	0	-9466	-287	346	0	-502	445	6.03	6.03	10.05	10.05	-5.80	-78.4
42	0	-9469	-280	879	0	-3923	433	6.03	6.03	10.05	10.05	-25.99	599.1
43	0	-10310	-537	451	0	-701	862	6.03	6.03	10.05	10.05	-8.30	-107.6
44	0	-8375	-28	176	0	-206	1	6.03	6.03	10.05	10.05	-3.99	-58.0
45	0	-8884	-260	1153	0	-6083	389	6.03	6.03	10.05	10.05	-40.77	1318.6
46	0	-8528	-263	216	0	-308	389	6.03	6.03	10.05	10.05	-5.16	-69.9
47	0	-8294	-256	184	0	-259	375	6.03	6.03	10.05	10.05	-5.00	-67.8
49	0	-8579	-309	221	0	-323	465	6.03	6.03	10.05	10.05	-5.57	-74.6
50	0	-8193	-208	166	0	-224	293	6.03	6.03	10.05	10.05	-4.54	-62.5
51	0	-8294	-254	362	0	-1399	371	6.03	6.03	10.05	10.05	-8.72	-116.2

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	83	-9826	-446	457	0	-1071	348	6.03	6.03	10.05	10.05	-7.67	-105.3
41	83	-8971	-287	346	0	-787	208	6.03	6.03	10.05	10.05	-6.31	-87.6
42	83	-8974	-280	577	0	-4523	202	6.03	6.03	10.05	10.05	-30.21	816.6
43	83	-9814	-537	451	0	-1073	419	6.03	6.03	10.05	10.05	-7.67	-105.3
44	83	-7880	-28	176	0	-352	-22	6.03	6.03	10.05	10.05	-4.32	-61.6
45	83	-8389	-260	650	0	-6827	175	6.03	6.03	10.05	10.05	-45.70	1593.9
46	83	-8033	-263	216	0	-486	172	6.03	6.03	10.05	10.05	-4.86	-68.6
47	83	-7799	-256	184	0	-411	163	6.03	6.03	10.05	10.05	-4.50	-63.8
49	83	-8084	-309	221	0	-506	210	6.03	6.03	10.05	10.05	-4.95	-69.7
50	83	-7698	-208	166	0	-361	122	6.03	6.03	10.05	10.05	-4.28	-61.0
51	83	-7799	-254	261	0	-1656	161	6.03	6.03	10.05	10.05	-10.28	-133.0

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	165	-9331	-446	457	0	-1449	-20	6.03	6.03	10.05	10.05	-9.15	-122.9
41	165	-8476	-287	346	0	-1072	-29	6.03	6.03	10.05	10.05	-7.19	-98.0
42	165	-8479	-280	275	0	-4874	-29	6.03	6.03	10.05	10.05	-32.64	961.1
43	165	-9318	-537	451	0	-1445	-24	6.03	6.03	10.05	10.05	-9.13	-122.6
44	165	-7385	-28	176	0	-497	-45	6.03	6.03	10.05	10.05	-4.65	-65.3
45	165	-7894	-260	146	0	-7155	-39	6.03	6.03	10.05	10.05	-47.84	1736.5
46	165	-7538	-263	216	0	-664	-45	6.03	6.03	10.05	10.05	-5.31	-73.7
47	165	-7304	-256	184	0	-562	-48	6.03	6.03	10.05	10.05	-4.86	-67.8
49	165	-7589	-309	221	0	-688	-45	6.03	6.03	10.05	10.05	-5.42	-75.1
50	165	-7203	-208	166	0	-498	-50	6.03	6.03	10.05	10.05	-4.59	-64.3
51	165	-7304	-254	160	0	-1830	-48	6.03	6.03	10.05	10.05	-11.54	-145.4

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	248	-8836	-446	457	0	-1826	-388	6.03	6.03	10.05	10.05	-11.31	-147.0
41	248	-7981	-287	346	0	-1358	-266	6.03	6.03	10.05	10.05	-8.46	-112.5
42	248	-7984	-280	-27	0	-4976	-260	6.03	6.03	10.05	10.05	-33.35	1028.0
43	248	-8822	-537	451	0	-1817	-467	6.03	6.03	10.05	10.05	-11.26	-146.3
44	248	-6890	-28	176	0	-642	-68	6.03	6.03	10.05	10.05	-4.98	-69.0
45	248	-7399	-260	-357	0	-7068	-253	6.03	6.03	10.05	10.05	-47.22	1744.9
46	248	-7043	-263	216	0	-843	-261	6.03	6.03	10.05	10.05	-5.78	-79.0
47	248	-6809	-256	184	0	-714	-260	6.03	6.03	10.05	10.05	-5.21	-71.7
49	248	-7094	-309	221	0	-870	-301	6.03	6.03	10.05	10.05	-5.91	-80.7
50	248	-6708	-208	166	0	-636	-221	6.03	6.03	10.05	10.05	-4.89	-67.6
51	248	-6809	-254	60	0	-1920	-258	6.03	6.03	10.05	10.05	-12.28	174.2

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	330	-8342	-446	457	0	-2203	-756	6.03	6.03	10.05	10.05	-13.98	176.3
41	330	-7486	-287	346	0	-1643	-503	6.03	6.03	10.05	10.05	-10.22	-131.6
42	330	-7489	-280	-330	0	-4829	-491	6.03	6.03	10.05	10.05	-32.36	1015.8
43	330	-8326	-537	451	0	-2189	-910	6.03	6.03	10.05	10.05	-13.88	173.6
44	330	-6395	-28	176	0	-788	-90	6.03	6.03	10.05	10.05	-5.34	-72.9
45	330	-6904	-260	-860	0	-6566	-467	6.03	6.03	10.05	10.05	-43.87	1618.6
46	330	-6548	-263	216	0	-1021	-478	6.03	6.03	10.05	10.05	-6.44	-86.5
47	330	-6314	-256	184	0	-866	-471	6.03	6.03	10.05	10.05	-5.65	-76.6
49	330	-6599	-309	221	0	-1053	-556	6.03	6.03	10.05	10.05	-6.62	-88.6
50	330	-6213	-208	166	0	-773	-392	6.03	6.03	10.05	10.05	-5.21	-71.2
51	330	-6314	-254	-41	0	-1928	-467	6.03	6.03	10.05	10.05	-12.45	200.2

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

ASTA NUM. 6 NI 36 NF 37 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 17C
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	--												
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-10670	-402	505	0	-1167	521	6.03	6.03	10.05	10.05	-8.34	-114.5
41	0	-9976	-244	432	0	-1039	272	6.03	6.03	10.05	10.05	-7.61	-104.7
42	0	-10050	-245	1139	0	-5029	272	6.03	6.03	10.05	10.05	-33.59	903.1
43	0	-10350	-496	454	0	-1017	670	6.03	6.03	10.05	10.05	-7.67	-105.9
44	0	-9034	16	329	0	-870	-143	6.03	6.03	10.05	10.05	-6.63	-91.7

45	0	-9317	-235	1512	0	-7454	254	6.03	6.03	10.05	10.05	-49.91	1728.9
46	0	-8721	-227	273	0	-664	243	6.03	6.03	10.05	10.05	-5.77	-80.6
47	0	-8408	-222	233	0	-570	236	6.03	6.03	10.05	10.05	-5.31	-74.5
49	0	-8639	-275	257	0	-612	319	6.03	6.03	10.05	10.05	-5.55	-77.8
50	0	-8376	-172	232	0	-583	156	6.03	6.03	10.05	10.05	-5.34	-74.9
51	0	-8433	-222	469	0	-1900	236	6.03	6.03	10.05	10.05	-11.85	-151.9

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	83	-10175	-402	505	0	-1583	189	6.03	6.03	10.05	10.05	-10.00	-134.2
41	83	-9481	-244	432	0	-1395	70	6.03	6.03	10.05	10.05	-8.92	-120.3
42	83	-9555	-245	837	0	-5844	70	6.03	6.03	10.05	10.05	-39.16	1194.8
43	83	-9854	-496	454	0	-1392	260	6.03	6.03	10.05	10.05	-9.00	-121.7
44	83	-8539	16	329	0	-1142	-129	6.03	6.03	10.05	10.05	-7.50	-101.9
45	83	-8822	-235	1008	0	-8493	60	6.03	6.03	10.05	10.05	-56.73	2101.8
46	83	-8226	-227	273	0	-889	56	6.03	6.03	10.05	10.05	-6.39	-87.8
47	83	-7913	-222	233	0	-762	52	6.03	6.03	10.05	10.05	-5.81	-80.3
49	83	-8144	-275	257	0	-825	92	6.03	6.03	10.05	10.05	-6.13	-84.5
50	83	-7881	-172	232	0	-775	14	6.03	6.03	10.05	10.05	-5.84	-80.7
51	83	-7938	-222	368	0	-2245	52	6.03	6.03	10.05	10.05	-14.37	204.7

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	165	-9680	-402	505	0	-2000	-143	6.03	6.03	10.05	10.05	-12.39	-160.9
41	165	-8986	-244	432	0	-1752	-132	6.03	6.03	10.05	10.05	-10.84	-141.9
42	165	-9060	-245	535	0	-6410	-133	6.03	6.03	10.05	10.05	-42.96	1411.1
43	165	-9358	-496	454	0	-1766	-149	6.03	6.03	10.05	10.05	-10.93	-143.7
44	165	-8044	16	329	0	-1413	-116	6.03	6.03	10.05	10.05	-8.77	-116.3
45	165	-8327	-235	505	0	-9118	-133	6.03	6.03	10.05	10.05	-60.78	2341.5
46	165	-7731	-227	273	0	-1114	-131	6.03	6.03	10.05	10.05	-7.16	-96.7
47	165	-7418	-222	233	0	-954	-131	6.03	6.03	10.05	10.05	-6.36	-86.6
49	165	-7649	-275	257	0	-1037	-134	6.03	6.03	10.05	10.05	-6.79	-92.1
50	165	-7386	-172	232	0	-966	-128	6.03	6.03	10.05	10.05	-6.40	-87.1
51	165	-7443	-222	268	0	-2508	-131	6.03	6.03	10.05	10.05	-16.36	301.1

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	248	-9184	-402	505	0	-2416	-474	6.03	6.03	10.05	10.05	-15.32	191.8
41	248	-8491	-244	432	0	-2108	-334	6.03	6.03	10.05	10.05	-13.27	-167.6
42	248	-8566	-245	233	0	-6727	-335	6.03	6.03	10.05	10.05	-45.05	1548.9
43	248	-8863	-496	454	0	-2141	-559	6.03	6.03	10.05	10.05	-13.44	-170.5
44	248	-7549	16	329	0	-1684	-103	6.03	6.03	10.05	10.05	-10.49	-134.7
45	248	-7832	-235	2	0	-9326	-327	6.03	6.03	10.05	10.05	-62.08	2446.6
46	248	-7236	-227	273	0	-1339	-318	6.03	6.03	10.05	10.05	-8.29	-109.3
47	248	-6923	-222	233	0	-1147	-314	6.03	6.03	10.05	10.05	-7.17	-95.6
49	248	-7154	-275	257	0	-1250	-361	6.03	6.03	10.05	10.05	-7.76	-103.0
50	248	-6891	-172	232	0	-1158	-270	6.03	6.03	10.05	10.05	-7.23	-96.3
51	248	-6948	-222	167	0	-2687	-315	6.03	6.03	10.05	10.05	-17.73	381.9

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	330	-8689	-402	505	0	-2832	-806	6.03	6.03	10.05	10.05	-18.41	324.6
41	330	-7996	-244	432	0	-2464	-535	6.03	6.03	10.05	10.05	-15.92	259.6
42	330	-8071	-245	-69	0	-6795	-538	6.03	6.03	10.05	10.05	-45.47	1606.9
43	330	-8367	-496	454	0	-2516	-968	6.03	6.03	10.05	10.05	-16.21	254.8
44	330	-7054	16	329	0	-1955	-89	6.03	6.03	10.05	10.05	-12.48	171.7
45	330	-7337	-235	-502	0	-9120	-520	6.03	6.03	10.05	10.05	-60.66	2416.6
46	330	-6741	-227	273	0	-1564	-505	6.03	6.03	10.05	10.05	-9.78	-124.8
47	330	-6428	-222	233	0	-1339	-497	6.03	6.03	10.05	10.05	-8.30	-107.7
49	330	-6659	-275	257	0	-1462	-588	6.03	6.03	10.05	10.05	-9.09	-117.1
50	330	-6396	-172	232	0	-1350	-412	6.03	6.03	10.05	10.05	-8.38	-108.4
51	330	-6453	-222	66	0	-2783	-498	6.03	6.03	10.05	10.05	-18.48	441.7

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

ASTA NUM. 7 NI 38 NF 39 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 22C
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-11820	-153	339	0	-148	205	6.03	6.03	10.05	10.05	-5.43	-77.5
41	0	-11780	14	362	0	-267	-57	6.03	6.03	10.05	10.05	-5.52	-80.5
42	0	-11840	-4	837	0	-3632	-38	6.03	6.03	10.05	10.05	-23.46	379.9
43	0	-11030	-247	237	0	8	369	6.03	6.03	10.05	10.05	-5.98	-82.6
44	0	-11930	292	417	0	-481	-496	6.03	6.03	10.05	10.05	-6.98	-95.0
45	0	-11060	2	1067	0	-5799	-36	6.03	6.03	10.05	10.05	-38.77	1076.9
46	0	-10460	41	225	0	-144	-74	6.03	6.03	10.05	10.05	-4.57	-67.3
47	0	-10130	48	190	0	-113	-78	6.03	6.03	10.05	10.05	-4.33	-64.0
49	0	-10140	-7	183	0	-73	9	6.03	6.03	10.05	10.05	-4.19	-62.2
50	0	-10320	100	219	0	-171	-164	6.03	6.03	10.05	10.05	-4.67	-67.7
51	0	-10150	43	349	0	-1235	-72	6.03	6.03	10.05	10.05	-8.41	-114.9

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	83	-11326	-153	339	0	-427	79	6.03	6.03	10.05	10.05	-5.93	-85.1
41	83	-11284	14	362	0	-566	-46	6.03	6.03	10.05	10.05	-6.41	-91.0
42	83	-11346	-4	535	0	-4198	-41	6.03	6.03	10.05	10.05	-27.60	567.4
43	83	-10535	-247	237	0	-188	165	6.03	6.03	10.05	10.05	-4.76	-69.7
44	83	-11436	292	417	0	-826	-255	6.03	6.03	10.05	10.05	-7.40	-103.6
45	83	-10566	2	564	0	-6472	-34	6.03	6.03	10.05	10.05	-43.36	1324.1
46	83	-9964	41	225	0	-329	-40	6.03	6.03	10.05	10.05	-5.05	-72.7
47	83	-9634	48	190	0	-270	-39	6.03	6.03	10.05	10.05	-4.71	-68.2
49	83	-9646	-7	183	0	-224	3	6.03	6.03	10.05	10.05	-4.54	-66.2
50	83	-9826	100	219	0	-352	-81	6.03	6.03	10.05	10.05	-5.07	-72.9
51	83	-9655	43	248	0	-1481	-37	6.03	6.03	10.05	10.05	-9.38	-126.1

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	165	-10832	-153	339	0	-707	-48	6.03	6.03	10.05	10.05	-6.74	-94.8
41	165	-10788	14	362	0	-864	-35	6.03	6.03	10.05	10.05	-7.29	-101.6
42	165	-10852	-4	233	0	-4514	-44	6.03	6.03	10.05	10.05	-29.92	692.1
43	165	-10040	-247	237	0	-384	-38	6.03	6.03	10.05	10.05	-5.27	-75.6
44	165	-10942	292	417	0	-1170	-14	6.03	6.03	10.05	10.05	-8.45	-116.2
45	165	-10072	2	60	0	-6729	-32	6.03	6.03	10.05	10.05	-45.10	1441.3

46	165	-9468	41	225	0	-515	-6	6.03	6.03	10.05	10.05	-5.52	-78.2
47	165	-9138	48	190	0	-427	1	6.03	6.03	10.05	10.05	-5.08	-72.4
49	165	-9152	-7	183	0	-375	-3	6.03	6.03	10.05	10.05	-4.90	-70.1
50	165	-9332	100	219	0	-532	2	6.03	6.03	10.05	10.05	-5.53	-78.2
51	165	-9160	43	147	0	-1644	-2	6.03	6.03	10.05	10.05	-10.20	-134.9

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	248	-10337	-153	339	0	-986	-174	6.03	6.03	10.05	10.05	-7.56	-104.5
41	248	-10291	14	362	0	-1163	-23	6.03	6.03	10.05	10.05	-8.18	-112.2
42	248	-10357	-4	-69	0	-4581	-46	6.03	6.03	10.05	10.05	-30.46	743.9
43	248	-9546	-247	237	0	-579	-242	6.03	6.03	10.05	10.05	-5.79	-81.6
44	248	-10449	292	417	0	-1514	227	6.03	6.03	10.05	10.05	-9.72	-131.2
45	248	-9579	2	-443	0	-6571	-30	6.03	6.03	10.05	10.05	-44.04	1425.8
46	248	-8973	41	225	0	-700	28	6.03	6.03	10.05	10.05	-6.00	-83.7
47	248	-8643	48	190	0	-585	41	6.03	6.03	10.05	10.05	-5.45	-76.5
49	248	-8657	-7	183	0	-526	-9	6.03	6.03	10.05	10.05	-5.25	-74.0
50	248	-8838	100	219	0	-713	85	6.03	6.03	10.05	10.05	-5.99	-83.4
51	248	-8665	43	47	0	-1724	33	6.03	6.03	10.05	10.05	-10.67	-139.3

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	330	-9843	-153	339	0	-1266	-300	6.03	6.03	10.05	10.05	-8.44	-114.9
41	330	-9795	14	362	0	-1462	-12	6.03	6.03	10.05	10.05	-9.31	-125.5
42	330	-9863	-4	-372	0	-4399	-49	6.03	6.03	10.05	10.05	-29.26	719.6
43	330	-9051	-247	237	0	-775	-445	6.03	6.03	10.05	10.05	-6.30	-87.5
44	330	-9955	292	417	0	-1858	468	6.03	6.03	10.05	10.05	-11.50	-151.4
45	330	-9085	2	-946	0	-5998	-28	6.03	6.03	10.05	10.05	-40.20	1277.1
46	330	-8477	41	225	0	-886	62	6.03	6.03	10.05	10.05	-6.47	-89.1
47	330	-8147	48	190	0	-742	81	6.03	6.03	10.05	10.05	-5.83	-80.7
49	330	-8163	-7	183	0	-676	-15	6.03	6.03	10.05	10.05	-5.60	-77.9
50	330	-8344	100	219	0	-893	168	6.03	6.03	10.05	10.05	-6.45	-88.7
51	330	-8170	43	-54	0	-1721	69	6.03	6.03	10.05	10.05	-10.68	-138.3

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

ASTA NUM. 8 NI 40 NF 34 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 12B
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-16740	-30	288	0	508	134	6.03	6.03	10.05	10.05	-8.32	-120.2
41	0	-15900	-123	178	0	241	321	6.03	6.03	10.05	10.05	-7.54	-106.9
42	0	-15910	-114	2134	0	1842	298	6.03	6.03	10.05	10.05	-12.81	-175.5
43	0	-16730	35	320	0	628	3	6.03	6.03	10.05	10.05	-8.74	-125.5
44	0	-14840	-280	3	0	-189	638	6.03	6.03	10.05	10.05	-8.78	-119.4
45	0	-15350	-105	3396	0	2850	278	6.03	6.03	10.05	10.05	-17.65	-232.5
46	0	-15000	-119	112	0	147	312	6.03	6.03	10.05	10.05	-7.16	-101.4
47	0	-14770	-117	95	0	123	310	6.03	6.03	10.05	10.05	-7.07	-100.0
49	0	-15050	-86	132	0	212	248	6.03	6.03	10.05	10.05	-6.85	-97.9
50	0	-14670	-149	68	0	49	374	6.03	6.03	10.05	10.05	-7.36	-103.2
51	0	-14770	-114	747	0	657	302	6.03	6.03	10.05	10.05	-8.09	-115.4

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	110	-16080	-30	288	0	191	101	6.03	6.03	10.05	10.05	-6.92	-102.1
41	110	-15240	-123	178	0	45	186	6.03	6.03	10.05	10.05	-6.60	-95.4
42	110	-15250	-114	1731	0	-284	173	6.03	6.03	10.05	10.05	-6.93	-101.4
43	110	-16070	35	320	0	275	41	6.03	6.03	10.05	10.05	-7.22	-105.8
44	110	-14180	-280	3	0	-192	330	6.03	6.03	10.05	10.05	-6.95	-97.9
45	110	-14690	-105	2725	0	-517	162	6.03	6.03	10.05	10.05	-7.55	-108.6
46	110	-14340	-119	112	0	24	182	6.03	6.03	10.05	10.05	-6.25	-90.2
47	110	-14110	-117	95	0	19	181	6.03	6.03	10.05	10.05	-6.16	-88.8
49	110	-14390	-86	132	0	68	152	6.03	6.03	10.05	10.05	-6.11	-88.7
50	110	-14010	-149	68	0	-26	210	6.03	6.03	10.05	10.05	-6.27	-90.0
51	110	-14110	-114	613	0	-91	177	6.03	6.03	10.05	10.05	-6.13	-88.6

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	220	-15420	-30	288	0	-126	67	6.03	6.03	10.05	10.05	-6.43	-95.3
41	220	-14580	-123	178	0	-150	50	6.03	6.03	10.05	10.05	-6.19	-91.5
42	220	-14590	-114	1328	0	-1967	48	6.03	6.03	10.05	10.05	-12.89	-175.0
43	220	-15410	35	320	0	-77	80	6.03	6.03	10.05	10.05	-6.25	-93.0
44	220	-13520	-280	3	0	-196	22	6.03	6.03	10.05	10.05	-5.95	-87.4
45	220	-14030	-105	2054	0	-3145	46	6.03	6.03	10.05	10.05	-19.60	-251.5
46	220	-13680	-119	112	0	-98	51	6.03	6.03	10.05	10.05	-5.65	-83.9
47	220	-13450	-117	95	0	-86	52	6.03	6.03	10.05	10.05	-5.52	-82.0
49	220	-13730	-86	132	0	-77	57	6.03	6.03	10.05	10.05	-5.60	-83.3
50	220	-13350	-149	68	0	-101	46	6.03	6.03	10.05	10.05	-5.54	-82.1
51	220	-13450	-114	478	0	-691	51	6.03	6.03	10.05	10.05	-7.70	-109.3

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	330	-14760	-30	288	0	-443	34	6.03	6.03	10.05	10.05	-7.31	-105.7
41	330	-13920	-123	178	0	-346	-85	6.03	6.03	10.05	10.05	-6.64	-96.5
42	330	-13930	-114	926	0	-3206	-78	6.03	6.03	10.05	10.05	-20.03	-255.9
43	330	-14750	35	320	0	-429	118	6.03	6.03	10.05	10.05	-7.26	-105.0
44	330	-12860	-280	3	0	-200	-286	6.03	6.03	10.05	10.05	-6.24	-88.0
45	330	-13370	-105	1383	0	-5035	-69	6.03	6.03	10.05	10.05	-33.16	694.9
46	330	-13020	-119	112	0	-221	-79	6.03	6.03	10.05	10.05	-5.84	-85.6
47	330	-12790	-117	95	0	-190	-78	6.03	6.03	10.05	10.05	-5.64	-82.9
49	330	-13070	-86	132	0	-222	-38	6.03	6.03	10.05	10.05	-5.86	-86.0
50	330	-12690	-149	68	0	-176	-119	6.03	6.03	10.05	10.05	-5.55	-81.7
51	330	-12790	-114	344	0	-1143	-75	6.03	6.03	10.05	10.05	-9.07	-125.8

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	440	-14100	-30	288	0	-760	1	6.03	6.03	10.05	10.05	-8.20	-116.1
41	440	-13260	-123	178	0	-542	-220	6.03	6.03	10.05	10.05	-7.09	-101.4
42	440	-13270	-114	523	0	-4003	-203	6.03	6.03	10.05	10.05	-25.81	407.5
43	440	-14090	35	320	0	-781	156	6.03	6.03	10.05	10.05	-8.27	-117.1
44	440	-12200	-280	3	0	-204	-594	6.03	6.03	10.05	10.05	-7.58	-102.2
45	440	-12710	-105	711	0	-6187	-185	6.03	6.03	10.05	10.05	-41.29	1088.0
46	440	-12360	-119	112	0	-344	-210	6.03	6.03	10.05	10.05	-6.03	-87.3

47	440	-12130	-117	95	0	-294	-207	6.03	6.03	10.05	10.05	-5.76	-83.7
49	440	-12410	-86	132	0	-367	-133	6.03	6.03	10.05	10.05	-6.13	-88.6
50	440	-12030	-149	68	0	-252	-283	6.03	6.03	10.05	10.05	-5.91	-83.2
51	440	-12130	-114	210	0	-1448	-201	6.03	6.03	10.05	10.05	-9.94	-135.9

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

ASTA NUM. 9 NI 41 NF 36 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 17B
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-17080	130	496	0	915	-249	6.03	6.03	10.05	10.05	-9.91	-140.5
41	0	-16390	19	430	0	769	-18	6.03	6.03	10.05	10.05	-9.12	-129.9
42	0	-16480	15	2665	0	2840	-11	6.03	6.03	10.05	10.05	-17.67	-234.8
43	0	-16760	198	440	0	829	-389	6.03	6.03	10.05	10.05	-9.48	-134.7
44	0	-15460	-167	339	0	562	364	6.03	6.03	10.05	10.05	-8.01	-115.2
45	0	-15750	7	4056	0	4037	8	6.03	6.03	10.05	10.05	-25.52	-320.4
46	0	-15140	8	270	0	474	4	6.03	6.03	10.05	10.05	-7.57	-109.3
47	0	-14830	5	230	0	401	10	6.03	6.03	10.05	10.05	-7.19	-104.2
49	0	-15060	43	253	0	450	-67	6.03	6.03	10.05	10.05	-7.45	-107.8
50	0	-14800	-31	232	0	396	84	6.03	6.03	10.05	10.05	-7.16	-103.8
51	0	-14850	4	976	0	1091	12	6.03	6.03	10.05	10.05	-9.68	-135.4

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	110	-16420	130	496	0	370	-105	6.03	6.03	10.05	10.05	-7.69	-112.1
41	110	-15730	19	430	0	296	2	6.03	6.03	10.05	10.05	-7.16	-104.8
42	110	-15820	15	2262	0	130	6	6.03	6.03	10.05	10.05	-6.60	-97.8
43	110	-16100	198	440	0	345	-170	6.03	6.03	10.05	10.05	-7.48	-109.1
44	110	-14800	-167	339	0	189	180	6.03	6.03	10.05	10.05	-6.42	-94.5
45	110	-15090	7	3385	0	-55	15	6.03	6.03	10.05	10.05	-6.04	-90.2
46	110	-14480	8	270	0	177	13	6.03	6.03	10.05	10.05	-6.25	-92.1
47	110	-14170	5	230	0	147	16	6.03	6.03	10.05	10.05	-6.02	-89.0
49	110	-14400	43	253	0	172	-20	6.03	6.03	10.05	10.05	-6.20	-91.4
50	110	-14140	-31	232	0	141	50	6.03	6.03	10.05	10.05	-5.99	-88.5
51	110	-14190	4	841	0	92	17	6.03	6.03	10.05	10.05	-5.83	-86.6

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	220	-15760	130	496	0	-175	38	6.03	6.03	10.05	10.05	-6.74	-99.5
41	220	-15070	19	430	0	-176	23	6.03	6.03	10.05	10.05	-6.47	-95.5
42	220	-15160	15	1859	0	-2137	23	6.03	6.03	10.05	10.05	-13.82	-187.0
43	220	-15440	198	440	0	-140	48	6.03	6.03	10.05	10.05	-6.48	-96.0
44	220	-14140	-167	339	0	-183	-3	6.03	6.03	10.05	10.05	-6.14	-90.4
45	220	-14430	7	2714	0	-3408	22	6.03	6.03	10.05	10.05	-21.35	-271.7
46	220	-13820	8	270	0	-120	22	6.03	6.03	10.05	10.05	-5.79	-85.7
47	220	-13510	5	230	0	-106	21	6.03	6.03	10.05	10.05	-5.62	-83.3
49	220	-13740	43	253	0	-106	27	6.03	6.03	10.05	10.05	-5.71	-84.6
50	220	-13480	-31	232	0	-115	16	6.03	6.03	10.05	10.05	-5.64	-83.5
51	220	-13530	4	707	0	-760	21	6.03	6.03	10.05	10.05	-7.98	-112.8

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	330	-15100	130	496	0	-721	182	6.03	6.03	10.05	10.05	-8.45	-120.2
41	330	-14410	19	430	0	-648	43	6.03	6.03	10.05	10.05	-7.92	-112.9
42	330	-14500	15	1457	0	-3960	40	6.03	6.03	10.05	10.05	-25.23	338.4
43	330	-14780	198	440	0	-624	266	6.03	6.03	10.05	10.05	-7.97	-114.0
44	330	-13480	-167	339	0	-556	-187	6.03	6.03	10.05	10.05	-7.23	-103.4
45	330	-13770	7	2042	0	-6023	29	6.03	6.03	10.05	10.05	-40.03	968.4
46	330	-13160	8	270	0	-418	30	6.03	6.03	10.05	10.05	-6.60	-95.3
47	330	-12850	5	230	0	-360	27	6.03	6.03	10.05	10.05	-6.28	-90.9
49	330	-13080	43	253	0	-384	73	6.03	6.03	10.05	10.05	-6.45	-93.3
50	330	-12820	-31	232	0	-370	-17	6.03	6.03	10.05	10.05	-6.30	-91.2
51	330	-12870	4	573	0	-1464	26	6.03	6.03	10.05	10.05	-10.26	-140.8

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	440	-14440	130	496	0	-1266	325	6.03	6.03	10.05	10.05	-10.15	-140.9
41	440	-13750	19	430	0	-1121	63	6.03	6.03	10.05	10.05	-9.36	-130.4
42	440	-13840	15	1054	0	-5341	56	6.03	6.03	10.05	10.05	-35.23	757.5
43	440	-14120	198	440	0	-1108	485	6.03	6.03	10.05	10.05	-9.46	-131.9
44	440	-12820	-167	339	0	-929	-371	6.03	6.03	10.05	10.05	-8.31	-116.3
45	440	-13110	7	1371	0	-7900	36	6.03	6.03	10.05	10.05	-52.93	1601.5
46	440	-12500	8	270	0	-715	39	6.03	6.03	10.05	10.05	-7.42	-104.8
47	440	-12190	5	230	0	-614	33	6.03	6.03	10.05	10.05	-6.93	-98.5
49	440	-12420	43	253	0	-662	120	6.03	6.03	10.05	10.05	-7.20	-102.0
50	440	-12160	-31	232	0	-626	-51	6.03	6.03	10.05	10.05	-6.97	-98.8
51	440	-12210	4	439	0	-2020	31	6.03	6.03	10.05	10.05	-12.63	-168.5

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

ASTA NUM. 10 NI 42 NF 38 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 22B
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-18240	207	-11	0	-194	-452	6.03	6.03	10.05	10.05	-9.08	-127.5
41	0	-18200	102	69	0	10	-242	6.03	6.03	10.05	10.05	-7.99	-115.1
42	0	-18270	88	1982	0	1498	-207	6.03	6.03	10.05	10.05	-12.47	-173.6
43	0	-17470	263	-88	0	-357	-566	6.03	6.03	10.05	10.05	-9.39	-129.8
44	0	-18350	-71	208	0	361	104	6.03	6.03	10.05	10.05	-8.41	-122.9
45	0	-17510	65	3233	0	2464	-158	6.03	6.03	10.05	10.05	-15.94	-215.8
46	0	-16910	81	31	0	-32	-202	6.03	6.03	10.05	10.05	-7.30	-105.6
47	0	-16590	75	22	0	-43	-192	6.03	6.03	10.05	10.05	-7.13	-103.2
49	0	-16600	110	-5	0	-111	-261	6.03	6.03	10.05	10.05	-7.49	-107.3
50	0	-16780	43	54	0	33	-127	6.03	6.03	10.05	10.05	-6.87	-100.6
51	0	-16610	70	659	0	453	-180	6.03	6.03	10.05	10.05	-8.07	-116.9

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	110	-17580	207	-11	0	-182	-224	6.03	6.03	10.05	10.05	-7.66	-110.6
41	110	-17540	102	69	0	-66	-130	6.03	6.03	10.05	10.05	-7.16	-104.9
42	110	-17610	88	1579	0	-460	-110	6.03	6.03	10.05	10.05	-8.48	-123.1
43	110	-16810	263	-88	0	-261	-276	6.03	6.03	10.05	10.05	-7.65	-109.4
44	110	-17690	-71	208	0	132	26	6.03	6.03	10.05	10.05	-7.33	-108.7
45	110	-16850	65	2562	0	-723	-86	6.03	6.03	10.05	10.05	-9.13	-130.5
46	110	-16250	81	31	0	-67	-113	6.03	6.03	10.05	10.05	-6.60	-97.4
47	110	-15930	75	22	0	-67	-109	6.03	6.03	10.05	10.05	-6.46	-95.6
49	110	-15940	110	-5	0	-106	-140	6.03	6.03	10.05	10.05	-6.62	-97.4
50	110	-16120	43	54	0	-27	-80	6.03	6.03	10.05	10.05	-6.38	-94.9
51	110	-15950	70	525	0	-198	-102	6.03	6.03	10.05	10.05	-6.89	-101.6

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	220	-16920	207	-11	0	-170	4	6.03	6.03	10.05	10.05	-7.17	-106.0
41	220	-16880	102	69	0	-141	-17	6.03	6.03	10.05	10.05	-7.05	-104.5
42	220	-16950	88	1176	0	-1975	-13	6.03	6.03	10.05	10.05	-13.70	-187.6
43	220	-16150	263	-88	0	-164	13	6.03	6.03	10.05	10.05	-6.85	-101.2
44	220	-17030	-71	208	0	-97	-52	6.03	6.03	10.05	10.05	-6.95	-103.3
45	220	-16190	65	1891	0	-3172	-15	6.03	6.03	10.05	10.05	-19.63	-256.8
46	220	-15590	81	31	0	-101	-24	6.03	6.03	10.05	10.05	-6.40	-95.1
47	220	-15270	75	22	0	-91	-26	6.03	6.03	10.05	10.05	-6.24	-92.8
49	220	-15280	110	-5	0	-100	-19	6.03	6.03	10.05	10.05	-6.28	-93.3
50	220	-15460	43	54	0	-87	-32	6.03	6.03	10.05	10.05	-6.30	-93.8
51	220	-15290	70	391	0	-702	-25	6.03	6.03	10.05	10.05	-8.45	-120.4

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	330	-16260	207	-11	0	-158	232	6.03	6.03	10.05	10.05	-7.21	-103.7
41	330	-16220	102	69	0	-217	95	6.03	6.03	10.05	10.05	-7.07	-104.0
42	330	-16290	88	773	0	-3047	83	6.03	6.03	10.05	10.05	-18.86	-248.2
43	330	-15490	263	-88	0	-67	303	6.03	6.03	10.05	10.05	-7.30	-103.6
44	330	-16370	-71	208	0	-326	-130	6.03	6.03	10.05	10.05	-7.52	-109.8
45	330	-15530	65	1219	0	-4883	56	6.03	6.03	10.05	10.05	-31.62	530.6
46	330	-14930	81	31	0	-135	65	6.03	6.03	10.05	10.05	-6.27	-92.8
47	330	-14610	75	22	0	-115	57	6.03	6.03	10.05	10.05	-6.07	-90.1
49	330	-14620	110	-5	0	-95	102	6.03	6.03	10.05	10.05	-6.01	-89.2
50	330	-14800	43	54	0	-147	16	6.03	6.03	10.05	10.05	-6.26	-92.6
51	330	-14630	70	257	0	-1058	53	6.03	6.03	10.05	10.05	-9.48	-132.6

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	440	-15600	207	-11	0	-146	459	6.03	6.03	10.05	10.05	-8.14	-113.3
41	440	-15560	102	69	0	-293	208	6.03	6.03	10.05	10.05	-7.08	-103.6
42	440	-15630	88	371	0	-3676	180	6.03	6.03	10.05	10.05	-23.01	-293.1
43	440	-14830	263	-88	0	30	593	6.03	6.03	10.05	10.05	-8.55	-116.7
44	440	-15710	-71	208	0	-555	-207	6.03	6.03	10.05	10.05	-8.08	-116.3
45	440	-14870	65	548	0	-5855	127	6.03	6.03	10.05	10.05	-38.68	848.7
46	440	-14270	81	31	0	-169	153	6.03	6.03	10.05	10.05	-6.14	-90.6
47	440	-13950	75	22	0	-138	140	6.03	6.03	10.05	10.05	-5.90	-87.3
49	440	-13960	110	-5	0	-89	224	6.03	6.03	10.05	10.05	-6.32	-90.5
50	440	-14140	43	54	0	-206	63	6.03	6.03	10.05	10.05	-6.22	-91.5
51	440	-13970	70	122	0	-1266	130	6.03	6.03	10.05	10.05	-9.97	-138.2

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

ASTA NUM. 11 NI 48 NF 49 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 31B
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-19620	1456	-87	0	-149	-10540	14.07	14.07	6.03	6.03	-42.15	1096.7
41	0	-20620	646	-56	0	-104	-8422	14.07	14.07	6.03	6.03	-32.47	603.3
42	0	-20720	582	117	0	326	-8333	14.07	14.07	6.03	6.03	-32.04	581.4
43	0	-17360	1845	-90	0	-141	-10280	14.07	14.07	6.03	6.03	-41.44	1179.9
44	0	-22630	-682	-5	0	-29	-5160	14.07	14.07	6.03	6.03	-18.57	-254.6
45	0	-19180	388	250	0	651	-6601	14.07	14.07	6.03	6.03	-24.67	340.1
46	0	-18060	404	-28	0	-44	-5745	14.07	14.07	6.03	6.03	-21.17	-279.9
47	0	-17420	343	-20	0	-29	-5075	14.07	14.07	6.03	6.03	-18.44	-246.6
49	0	-17090	613	-31	0	-44	-5781	14.07	14.07	6.03	6.03	-21.54	286.7
50	0	-18150	108	-14	0	-21	-4758	14.07	14.07	6.03	6.03	-17.11	-231.5
51	0	-17460	322	37	0	115	-5046	14.07	14.07	6.03	6.03	-18.32	-245.2

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	110	-18740	1317	-87	0	-53	-9014	14.07	14.07	6.03	6.03	-35.61	822.6
41	110	-19740	646	-56	0	-42	-7711	14.07	14.07	6.03	6.03	-29.50	511.1
42	110	-19840	582	117	0	198	-7692	14.07	14.07	6.03	6.03	-29.39	503.0
43	110	-16480	1614	-90	0	-43	-8377	14.07	14.07	6.03	6.03	-33.31	818.6
44	110	-21750	-451	-5	0	-23	-5783	14.07	14.07	6.03	6.03	-20.82	-281.2
45	110	-18300	388	250	0	375	-6174	14.07	14.07	6.03	6.03	-22.99	304.4
46	110	-17180	404	-28	0	-13	-5301	14.07	14.07	6.03	6.03	-19.43	-258.0
47	110	-16540	343	-20	0	-6	-4698	14.07	14.07	6.03	6.03	-17.02	-228.2
49	110	-16210	567	-31	0	-10	-5132	14.07	14.07	6.03	6.03	-18.89	-250.0
50	110	-17270	154	-14	0	-6	-4614	14.07	14.07	6.03	6.03	-16.61	-224.3
51	110	-16580	322	37	0	74	-4692	14.07	14.07	6.03	6.03	-16.99	-227.9

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	220	-17860	1179	-87	0	42	-7641	14.07	14.07	6.03	6.03	-29.68	590.1
41	220	-18860	646	-56	0	20	-7000	14.07	14.07	6.03	6.03	-26.54	421.6
42	220	-18960	582	117	0	69	-7052	14.07	14.07	6.03	6.03	-26.74	426.4
43	220	-15600	1383	-90	0	56	-6728	14.07	14.07	6.03	6.03	-26.17	526.2
44	220	-20870	-220	-5	0	-18	-6152	14.07	14.07	6.03	6.03	-22.40	-299.0
45	220	-17420	388	250	0	100	-5746	14.07	14.07	6.03	6.03	-21.31	-280.4
46	220	-16300	404	-28	0	17	-4856	14.07	14.07	6.03	6.03	-17.71	-236.1
47	220	-15660	343	-20	0	16	-4320	14.07	14.07	6.03	6.03	-15.60	-209.9
49	220	-15330	521	-31	0	24	-4534	14.07	14.07	6.03	6.03	-16.51	-220.4
50	220	-16390	200	-14	0	9	-4419	14.07	14.07	6.03	6.03	-15.92	-214.8
51	220	-15700	322	37	0	33	-4338	14.07	14.07	6.03	6.03	-15.66	-210.8

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	330	-16980	1040	-87	0	138	-6420	14.07	14.07	6.03	6.03	-24.42	400.6
41	330	-17980	646	-56	0	81	-6290	14.07	14.07	6.03	6.03	-23.58	335.7
42	330	-18080	582	117	0	-60	-6412	14.07	14.07	6.03	6.03	-24.10	352.1
43	330	-14720	1152	-90	0	155	-5334	14.07	14.07	6.03	6.03	-20.13	306.2
44	330	-19990	11	-5	0	-12	-6267	14.07	14.07	6.03	6.03	-23.04	-305.2
45	330	-16540	388	250	0	-175	-5319	14.07	14.07	6.03	6.03	-19.64	-259.3
46	330	-15420	404	-28	0	47	-4412	14.07	14.07	6.03	6.03	-16.00	-214.4
47	330	-14780	343	-20	0	39	-3943	14.07	14.07	6.03	6.03	-14.20	-191.7
49	330	-14450	475	-31	0	58	-3987	14.07	14.07	6.03	6.03	-14.39	-193.7
50	330	-15510	246	-14	0	24	-4173	14.07	14.07	6.03	6.03	-15.04	-202.9
51	330	-14820	322	37	0	-8	-3983	14.07	14.07	6.03	6.03	-14.35	-193.6

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	440	-16100	902	-87	0	234	-5352	14.07	14.07	6.03	6.03	-19.88	-261.2
41	440	-17100	646	-56	0	143	-5579	14.07	14.07	6.03	6.03	-20.65	-272.1
42	440	-17200	582	117	0	-188	-5771	14.07	14.07	6.03	6.03	-21.47	-281.8
43	440	-13840	921	-90	0	254	-4193	14.07	14.07	6.03	6.03	-15.33	-203.9
44	440	-19110	242	-5	0	-7	-6128	14.07	14.07	6.03	6.03	-22.61	-298.7
45	440	-15660	388	250	0	-450	-4892	14.07	14.07	6.03	6.03	-17.97	-238.2
46	440	-14540	404	-28	0	78	-3968	14.07	14.07	6.03	6.03	-14.31	-192.8
47	440	-13900	343	-20	0	61	-3566	14.07	14.07	6.03	6.03	-12.81	-173.7
49	440	-13570	428	-31	0	92	-3490	14.07	14.07	6.03	6.03	-12.54	-170.0
50	440	-14630	293	-14	0	40	-3877	14.07	14.07	6.03	6.03	-13.95	-188.6
51	440	-13940	322	37	0	-49	-3629	14.07	14.07	6.03	6.03	-13.04	-176.6

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

ASTA NUM. 12 NI 91 NF 92 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 30B
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-22520	2739	-106	0	-269	-21390	14.07	14.07	6.03	6.03	-87.61	3374.3
41	0	-22980	1581	-94	0	-250	-16410	14.07	14.07	6.03	6.03	-66.83	2193.3
42	0	-23020	1589	85	0	190	-16510	14.07	14.07	6.03	6.03	-67.25	2213.4
43	0	-20130	3161	-91	0	-223	-21410	14.07	14.07	6.03	6.03	-87.70	3550.2
44	0	-24170	-294	-75	0	-221	-8651	14.07	14.07	6.03	6.03	-32.57	484.3
45	0	-20950	1244	227	0	542	-13260	14.07	14.07	6.03	6.03	-53.69	1614.6
46	0	-19630	1021	-57	0	-155	-11120	14.07	14.07	6.03	6.03	-44.68	1222.8
47	0	-18800	880	-48	0	-132	-9793	14.07	14.07	6.03	6.03	-39.04	984.6
49	0	-18640	1267	-52	0	-138	-11450	14.07	14.07	6.03	6.03	-46.28	1358.7
50	0	-19450	576	-48	0	-138	-8903	14.07	14.07	6.03	6.03	-34.94	759.9
51	0	-18810	883	12	0	15	-9826	14.07	14.07	6.03	6.03	-39.18	991.1

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	110	-21640	2600	-106	0	-153	-18454	14.07	14.07	6.03	6.03	-75.50	2755.1
41	110	-22100	1581	-94	0	-147	-14671	14.07	14.07	6.03	6.03	-59.56	1857.1
42	110	-22140	1589	85	0	96	-14762	14.07	14.07	6.03	6.03	-59.94	1875.0
43	110	-19250	2930	-91	0	-124	-18059	14.07	14.07	6.03	6.03	-73.96	2832.0
44	110	-23290	-63	-75	0	-139	-8848	14.07	14.07	6.03	6.03	-33.68	557.0
45	110	-20070	1244	227	0	292	-11893	14.07	14.07	6.03	6.03	-47.95	1365.9
46	110	-18750	1021	-57	0	-93	-9996	14.07	14.07	6.03	6.03	-39.94	1031.5
47	110	-17920	880	-48	0	-79	-8824	14.07	14.07	6.03	6.03	-34.96	829.7
49	110	-17760	1221	-52	0	-81	-10083	14.07	14.07	6.03	6.03	-40.52	1111.3
50	110	-18570	622	-48	0	-84	-8245	14.07	14.07	6.03	6.03	-32.21	673.5
51	110	-17930	883	12	0	2	-8854	14.07	14.07	6.03	6.03	-35.09	835.4

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	220	-20760	2462	-106	0	-37	-15670	14.07	14.07	6.03	6.03	-63.94	2174.7
41	220	-21220	1581	-94	0	-44	-12932	14.07	14.07	6.03	6.03	-52.24	1523.7
42	220	-21260	1589	85	0	3	-13013	14.07	14.07	6.03	6.03	-52.58	1539.3
43	220	-18370	2699	-91	0	-24	-14962	14.07	14.07	6.03	6.03	-61.17	2176.4
44	220	-22410	168	-75	0	-56	-8790	14.07	14.07	6.03	6.03	-33.66	586.9
45	220	-19190	1244	227	0	42	-10526	14.07	14.07	6.03	6.03	-42.17	1119.8
46	220	-17870	1021	-57	0	-30	-8873	14.07	14.07	6.03	6.03	-35.18	842.8
47	220	-17040	880	-48	0	-27	-7856	14.07	14.07	6.03	6.03	-30.86	677.3
49	220	-16880	1174	-52	0	-25	-8767	14.07	14.07	6.03	6.03	-34.94	878.5
50	220	-17690	668	-48	0	-31	-7536	14.07	14.07	6.03	6.03	-29.26	578.0
51	220	-17050	883	12	0	-11	-7883	14.07	14.07	6.03	6.03	-30.98	682.3

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	330	-19880	2324	-106	0	79	-13039	14.07	14.07	6.03	6.03	-52.90	1634.8
41	330	-20340	1581	-94	0	59	-11192	14.07	14.07	6.03	6.03	-44.85	1194.7
42	330	-20380	1589	85	0	-91	-11264	14.07	14.07	6.03	6.03	-45.16	1208.0
43	330	-17490	2468	-91	0	76	-12120	14.07	14.07	6.03	6.03	-49.30	1585.1
44	330	-21530	399	-75	0	26	-8479	14.07	14.07	6.03	6.03	-32.49	570.1
45	330	-18310	1244	227	0	-207	-9158	14.07	14.07	6.03	6.03	-36.35	877.7
46	330	-16990	1021	-57	0	32	-7750	14.07	14.07	6.03	6.03	-30.39	658.2
47	330	-16160	880	-48	0	25	-6888	14.07	14.07	6.03	6.03	-26.74	528.7
49	330	-16000	1128	-52	0	32	-7502	14.07	14.07	6.03	6.03	-29.54	661.9
50	330	-16810	714	-48	0	22	-6776	14.07	14.07	6.03	6.03	-26.07	474.6
51	330	-16170	883	12	0	-24	-6912	14.07	14.07	6.03	6.03	-26.85	533.0

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	440	-19000	2185	-106	0	195	-10560	14.07	14.07	6.03	6.03	-42.36	1139.0
41	440	-19460	1581	-94	0	162	-9453	14.07	14.07	6.03	6.03	-37.38	873.6
42	440	-19500	1589	85	0	-184	-9516	14.07	14.07	6.03	6.03	-37.66	884.6
43	440	-16610	2237	-91	0	176	-9531	14.07	14.07	6.03	6.03	-38.33	1061.5
44	440	-20650	630	-75	0	108	-7913	14.07	14.07	6.03	6.03	-30.17	506.3
45	440	-17430	1244	227	0	-457	-7791	14.07	14.07	6.03	6.03	-30.47	642.8
46	440	-16110	1021	-57	0	95	-6626	14.07	14.07	6.03	6.03	-25.58	480.2
47	440	-15280	880	-48	0	78	-5919	14.07	14.07	6.03	6.03	-22.61	386.4
49	440	-15120	1082	-52	0	89	-6288	14.07	14.07	6.03	6.03	-24.32	464.1
50	440	-15930	760	-48	0	75	-5965	14.07	14.07	6.03	6.03	-22.65	365.4
51	440	-15290	883	12	0	-38	-5940	14.07	14.07	6.03	6.03	-22.70	389.8

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

ASTA NUM. 13 NI 134 NF 135 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 29B
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-22400	3005	-194	0	-539	-22740	14.07	14.07	8.04	8.04	-81.98	2818.7
41	0	-22980	1770	-167	0	-471	-17420	14.07	14.07	6.03	6.03	-71.09	2424.3
42	0	-22920	1754	-11	0	-80	-17260	14.07	14.07	6.03	6.03	-70.42	2391.7
43	0	-19930	3439	-177	0	-486	-22770	14.07	14.07	8.04	8.04	-81.89	2955.4
44	0	-24370	-225	-127	0	-368	-9130	14.07	14.07	6.03	6.03	-34.67	559.8
45	0	-20790	1354	127	0	279	-13640	14.07	14.07	6.03	6.03	-55.34	1710.6
46	0	-19630	1148	-112	0	-315	-11790	14.07	14.07	6.03	6.03	-47.58	1371.1
47	0	-18800	992	-98	0	-276	-10380	14.07	14.07	6.03	6.03	-41.61	1111.9
49	0	-18600	1404	-107	0	-299	-12160	14.07	14.07	6.03	6.03	-49.33	1520.7
50	0	-19490	671	-97	0	-275	-9428	14.07	14.07	6.03	6.03	-37.27	866.6
51	0	-18780	987	-46	0	-146	-10330	14.07	14.07	6.03	6.03	-41.40	1102.2
apost= 10.05 aant= 10.05 ainf= 4.02 asup= 4.02 (e arm. base= 4 X 2.01)													
40	110	-21520	2866	-194	0	-326	-19511	14.07	14.07	6.03	6.03	-79.88	3008.6
41	110	-22100	1770	-167	0	-287	-15472	14.07	14.07	6.03	6.03	-62.96	2038.8
42	110	-22040	1754	-11	0	-67	-15330	14.07	14.07	6.03	6.03	-62.37	2010.7
43	110	-19050	3208	-177	0	-292	-19114	14.07	14.07	6.03	6.03	-78.30	3091.9
44	110	-23490	6	-127	0	-229	-9251	14.07	14.07	6.03	6.03	-35.44	622.1
45	110	-19910	1354	127	0	139	-12150	14.07	14.07	6.03	6.03	-49.09	1433.4
46	110	-18750	1148	-112	0	-192	-10527	14.07	14.07	6.03	6.03	-42.26	1147.3
47	110	-17920	992	-98	0	-168	-9289	14.07	14.07	6.03	6.03	-37.01	928.7
49	110	-17720	1358	-107	0	-181	-10640	14.07	14.07	6.03	6.03	-42.94	1237.1
50	110	-18610	717	-97	0	-168	-8665	14.07	14.07	6.03	6.03	-34.08	757.2
51	110	-17900	987	-46	0	-95	-9245	14.07	14.07	6.03	6.03	-36.82	920.4
apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)													
40	220	-20640	2728	-194	0	-113	-16435	14.07	14.07	6.03	6.03	-67.15	2358.7
41	220	-21220	1770	-167	0	-103	-13524	14.07	14.07	6.03	6.03	-54.78	1656.2
42	220	-21160	1754	-11	0	-55	-13401	14.07	14.07	6.03	6.03	-54.27	1632.6
43	220	-18170	2977	-177	0	-98	-15712	14.07	14.07	6.03	6.03	-64.29	2363.6
44	220	-22610	237	-127	0	-89	-9118	14.07	14.07	6.03	6.03	-35.08	639.1
45	220	-19030	1354	127	0	-2	-10660	14.07	14.07	6.03	6.03	-42.79	1159.2
46	220	-17870	1148	-112	0	-69	-9264	14.07	14.07	6.03	6.03	-36.91	926.4
47	220	-17040	992	-98	0	-60	-8198	14.07	14.07	6.03	6.03	-32.39	748.4
49	220	-16840	1311	-107	0	-63	-9171	14.07	14.07	6.03	6.03	-36.72	968.4
50	220	-17730	763	-97	0	-62	-7851	14.07	14.07	6.03	6.03	-30.66	638.8
51	220	-17020	987	-46	0	-44	-8160	14.07	14.07	6.03	6.03	-32.22	741.4
apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)													
40	330	-19760	2590	-194	0	100	-13511	14.07	14.07	6.03	6.03	-54.93	1749.7
41	330	-20340	1770	-167	0	81	-11575	14.07	14.07	6.03	6.03	-46.52	1278.7
42	330	-20280	1754	-11	0	-43	-11472	14.07	14.07	6.03	6.03	-46.08	1259.6
43	330	-17290	2746	-177	0	96	-12564	14.07	14.07	6.03	6.03	-51.20	1699.8
44	330	-21730	468	-127	0	50	-8730	14.07	14.07	6.03	6.03	-33.57	608.0
45	330	-18150	1354	127	0	-142	-9171	14.07	14.07	6.03	6.03	-36.44	889.8
46	330	-16990	1148	-112	0	55	-8002	14.07	14.07	6.03	6.03	-31.52	710.2
47	330	-16160	992	-98	0	48	-7108	14.07	14.07	6.03	6.03	-27.73	572.6
49	330	-15960	1265	-107	0	54	-7753	14.07	14.07	6.03	6.03	-30.66	716.6
50	330	-16850	809	-97	0	45	-6986	14.07	14.07	6.03	6.03	-27.00	513.0
51	330	-16140	987	-46	0	7	-7074	14.07	14.07	6.03	6.03	-27.59	566.9
apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)													
40	440	-18880	2451	-194	0	313	-10740	14.07	14.07	6.03	6.03	-43.16	1186.0
41	440	-19460	1770	-167	0	265	-9627	14.07	14.07	6.03	6.03	-38.16	910.3
42	440	-19400	1754	-11	0	-30	-9542	14.07	14.07	6.03	6.03	-37.79	895.8
43	440	-16410	2515	-177	0	291	-9670	14.07	14.07	6.03	6.03	-38.97	1104.8
44	440	-20850	699	-127	0	190	-8089	14.07	14.07	6.03	6.03	-30.91	529.5
45	440	-17270	1354	127	0	-282	-7681	14.07	14.07	6.03	6.03	-30.02	629.1
46	440	-16110	1148	-112	0	178	-6739	14.07	14.07	6.03	6.03	-26.09	502.1
47	440	-15280	992	-98	0	156	-6017	14.07	14.07	6.03	6.03	-23.05	404.6
49	440	-15080	1219	-107	0	172	-6386	14.07	14.07	6.03	6.03	-24.77	485.3
50	440	-15970	856	-97	0	152	-6070	14.07	14.07	6.03	6.03	-23.11	382.5
51	440	-15260	987	-46	0	57	-5989	14.07	14.07	6.03	6.03	-22.93	400.3
apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)													

ASTA NUM. 14 NI 177 NF 178 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 28B
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-22320	2818	-233	0	-719	-21590	14.07	14.07	6.03	6.03	-88.43	3435.1
41	0	-22840	1596	-199	0	-617	-16220	14.07	14.07	6.03	6.03	-66.05	2159.4
42	0	-22840	1597	-61	0	-260	-16230	14.07	14.07	6.03	6.03	-66.09	2161.7
43	0	-19910	3276	-211	0	-654	-21860	14.07	14.07	8.04	8.04	-78.68	2795.8
44	0	-24140	-384	-149	0	-464	-7831	14.07	14.07	6.03	6.03	-28.95	-381.8
45	0	-20790	1241	76	0	111	-12930	14.07	14.07	6.03	6.03	-52.30	1551.0
46	0	-19550	1025	-128	0	-405	-10940	14.07	14.07	6.03	6.03	-43.91	1188.2
47	0	-18720	882	-110	0	-352	-9615	14.07	14.07	6.03	6.03	-38.27	951.1
49	0	-18550	1290	-122	0	-386	-11400	14.07	14.07	6.03	6.03	-46.08	1353.3
50	0	-19390	558	-109	0	-348	-8597	14.07	14.07	6.03	6.03	-33.58	700.9
51	0	-18720	883	-64	0	-233	-9617	14.07	14.07	6.03	6.03	-38.28	951.5
apost= 10.05 aant= 10.05 ainf= 4.02 asup= 4.02 (e arm. base= 4 X 2.01)													
40	110	-21440	2680	-233	0	-463	-18566	14.07	14.07	6.03	6.03	-75.98	2795.2
41	110	-21960	1596	-199	0	-398	-14466	14.07	14.07	6.03	6.03	-58.70	1820.0
42	110	-21960	1597	-61	0	-193	-14474	14.07	14.07	6.03	6.03	-58.74	1821.8

43	110	-19030	3045	-211	0	-422	-18384	14.07	14.07	6.03	6.03	-75.30	2923.2
44	110	-23260	-153	-149	0	-300	-8126	14.07	14.07	6.03	6.03	-30.46	432.5
45	110	-19910	1241	76	0	27	-11566	14.07	14.07	6.03	6.03	-46.56	1303.5
46	110	-18670	1025	-128	0	-264	-9812	14.07	14.07	6.03	6.03	-39.15	996.4
47	110	-17840	882	-110	0	-230	-8644	14.07	14.07	6.03	6.03	-34.18	796.3
49	110	-17670	1244	-122	0	-252	-10008	14.07	14.07	6.03	6.03	-40.21	1100.3
50	110	-18510	604	-109	0	-228	-7958	14.07	14.07	6.03	6.03	-30.94	619.3
51	110	-17840	883	-64	0	-162	-8646	14.07	14.07	6.03	6.03	-34.18	796.7

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	220	-20560	2541	-233	0	-206	-15695	14.07	14.07	6.03	6.03	-64.06	2194.1
41	220	-21080	1596	-199	0	-178	-12711	14.07	14.07	6.03	6.03	-51.31	1483.5
42	220	-21080	1597	-61	0	-126	-12717	14.07	14.07	6.03	6.03	-51.34	1484.8
43	220	-18150	2814	-211	0	-190	-15162	14.07	14.07	6.03	6.03	-62.01	2237.8
44	220	-22380	78	-149	0	-137	-8168	14.07	14.07	6.03	6.03	-30.86	475.7
45	220	-19030	1241	76	0	-56	-10201	14.07	14.07	6.03	6.03	-40.78	1058.9
46	220	-17790	1025	-128	0	-123	-8684	14.07	14.07	6.03	6.03	-34.36	807.4
47	220	-16960	882	-110	0	-109	-7674	14.07	14.07	6.03	6.03	-30.06	644.4
49	220	-16790	1197	-122	0	-118	-8666	14.07	14.07	6.03	6.03	-34.51	862.2
50	220	-17630	650	-109	0	-108	-7269	14.07	14.07	6.03	6.03	-28.07	528.9
51	220	-16960	883	-64	0	-91	-7676	14.07	14.07	6.03	6.03	-30.07	644.7

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	330	-19680	2402	-233	0	50	-12976	14.07	14.07	6.03	6.03	-52.66	1633.9
41	330	-20200	1596	-199	0	41	-10956	14.07	14.07	6.03	6.03	-43.85	1151.9
42	330	-20200	1597	-61	0	-59	-10960	14.07	14.07	6.03	6.03	-43.87	1152.8
43	330	-17270	2583	-211	0	42	-12194	14.07	14.07	6.03	6.03	-49.64	1616.7
44	330	-21500	309	-149	0	27	-7955	14.07	14.07	6.03	6.03	-30.14	476.1
45	330	-18150	1241	76	0	-140	-8836	14.07	14.07	6.03	6.03	-34.96	819.0
46	330	-16910	1025	-128	0	18	-7555	14.07	14.07	6.03	6.03	-29.55	622.9
47	330	-16080	882	-110	0	12	-6704	14.07	14.07	6.03	6.03	-25.93	496.7
49	330	-15910	1151	-122	0	16	-7376	14.07	14.07	6.03	6.03	-28.99	640.8
50	330	-16750	696	-109	0	13	-6528	14.07	14.07	6.03	6.03	-24.97	430.9
51	330	-16080	883	-64	0	-21	-6705	14.07	14.07	6.03	6.03	-25.94	497.0

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	440	-18800	2264	-233	0	306	-10410	14.07	14.07	6.03	6.03	-41.74	1118.5
41	440	-19320	1596	-199	0	260	-9202	14.07	14.07	6.03	6.03	-36.30	829.0
42	440	-19320	1597	-61	0	8	-9204	14.07	14.07	6.03	6.03	-36.31	829.4
43	440	-16390	2352	-211	0	274	-9480	14.07	14.07	6.03	6.03	-38.15	1064.0
44	440	-20620	540	-149	0	190	-7488	14.07	14.07	6.03	6.03	-28.27	431.8
45	440	-17270	1241	76	0	-223	-7472	14.07	14.07	6.03	6.03	-29.08	587.1
46	440	-16030	1025	-128	0	159	-6427	14.07	14.07	6.03	6.03	-24.70	446.0
47	440	-15200	882	-110	0	134	-5733	14.07	14.07	6.03	6.03	-21.80	356.1
49	440	-15030	1105	-122	0	149	-6136	14.07	14.07	6.03	6.03	-23.66	439.2
50	440	-15870	742	-109	0	133	-5737	14.07	14.07	6.03	6.03	-21.64	327.8
51	440	-15200	883	-64	0	50	-5734	14.07	14.07	6.03	6.03	-21.80	356.2

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

ASTA NUM. 15 NI 220 NF 221 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 27B
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-18580	95	-319	0	-756	-11760	14.07	14.07	6.03	6.03	-47.62	1432.0
41	0	-19470	-489	-316	0	-716	-7983	14.07	14.07	6.03	6.03	-30.80	575.5
42	0	-19740	-498	-182	0	-382	-8183	14.07	14.07	6.03	6.03	-31.63	600.8
43	0	-16430	544	-282	0	-655	-12540	14.07	14.07	6.03	6.03	-51.18	1752.8
44	0	-21290	-1473	-318	0	-675	-1981	14.07	14.07	6.03	6.03	-10.41	-148.4
45	0	-18360	-445	-53	0	-32	-6582	14.07	14.07	6.03	6.03	-24.79	369.7
46	0	-16970	-395	-253	0	-514	-5209	14.07	14.07	6.03	6.03	-19.08	-253.4
47	0	-16340	-372	-238	0	-463	-4515	14.07	14.07	6.03	6.03	-16.31	-219.4
49	0	-16040	-177	-239	0	-476	-5773	14.07	14.07	6.03	6.03	-21.76	326.9
50	0	-17020	-580	-246	0	-480	-3662	14.07	14.07	6.03	6.03	-13.26	-182.6
51	0	-16430	-374	-193	0	-352	-4582	14.07	14.07	6.03	6.03	-16.56	-222.6

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	110	-17700	-43	-319	0	-404	-11729	14.07	14.07	6.03	6.03	-47.61	1482.6
41	110	-18590	-489	-316	0	-369	-8520	14.07	14.07	6.03	6.03	-33.44	728.4
42	110	-18860	-498	-182	0	-182	-8730	14.07	14.07	6.03	6.03	-34.31	756.8
43	110	-15550	313	-282	0	-345	-12069	14.07	14.07	6.03	6.03	-49.28	1705.0
44	110	-20410	-1242	-318	0	-325	-3474	14.07	14.07	6.03	6.03	-13.35	-186.4
45	110	-17480	-445	-53	0	26	-7072	14.07	14.07	6.03	6.03	-27.22	498.4
46	110	-16090	-395	-253	0	-235	-5644	14.07	14.07	6.03	6.03	-21.17	302.9
47	110	-15460	-372	-238	0	-202	-4924	14.07	14.07	6.03	6.03	-18.15	-239.9
49	110	-15160	-223	-239	0	-214	-5993	14.07	14.07	6.03	6.03	-22.98	405.7
50	110	-16140	-534	-246	0	-210	-4274	14.07	14.07	6.03	6.03	-15.38	-207.9
51	110	-15550	-374	-193	0	-140	-4994	14.07	14.07	6.03	6.03	-18.43	-243.4

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	220	-16820	-182	-319	0	-53	-11850	14.07	14.07	6.03	6.03	-48.24	1568.7
41	220	-17710	-489	-316	0	-21	-9056	14.07	14.07	6.03	6.03	-36.03	891.3
42	220	-17980	-498	-182	0	18	-9276	14.07	14.07	6.03	6.03	-36.94	922.4
43	220	-14670	82	-282	0	-35	-11852	14.07	14.07	6.03	6.03	-48.44	1715.7
44	220	-19530	-1011	-318	0	25	-4713	14.07	14.07	6.03	6.03	-16.92	-230.8
45	220	-16600	-445	-53	0	85	-7561	14.07	14.07	6.03	6.03	-29.65	640.9
46	220	-15210	-395	-253	0	43	-6078	14.07	14.07	6.03	6.03	-23.35	419.4
47	220	-14580	-372	-238	0	59	-5332	14.07	14.07	6.03	6.03	-20.16	311.9
49	220	-14280	-269	-239	0	49	-6263	14.07	14.07	6.03	6.03	-24.43	502.5
50	220	-15260	-488	-246	0	61	-4836	14.07	14.07	6.03	6.03	-17.81	-235.6
51	220	-14670	-374	-193	0	72	-5406	14.07	14.07	6.03	6.03	-20.46	320.9

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	330	-15940	-320	-319	0	298	-12124	14.07	14.07	6.03	6.03	-49.48	1690.9
41	330	-16830	-489	-316	0	326	-9593	14.07	14.07	6.03	6.03	-38.56	1061.5
42	330	-17100	-498	-182	0	218	-9823	14.07	14.07	6.03	6.03	-39.51	1095.3
43	330	-13790	-149	-282	0	276	-11889	14.07	14.07	6.03	6.03	-48.65	1785.6

44	330	-18650	-780	-318	0	376	-5698	14.07	14.07	6.03	6.03	-20.86	-277.2
45	330	-15720	-445	-53	0	143	-8050	14.07	14.07	6.03	6.03	-32.03	793.6
46	330	-14330	-395	-253	0	322	-6512	14.07	14.07	6.03	6.03	-25.53	550.3
47	330	-13700	-372	-238	0	321	-5741	14.07	14.07	6.03	6.03	-22.23	429.0
49	330	-13400	-315	-239	0	311	-6585	14.07	14.07	6.03	6.03	-26.08	617.5
50	330	-14380	-442	-246	0	331	-5347	14.07	14.07	6.03	6.03	-20.28	323.1
51	330	-13790	-374	-193	0	284	-5817	14.07	14.07	6.03	6.03	-22.55	439.3

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	440	-15060	-459	-319	0	649	-12550	14.07	14.07	6.03	6.03	-51.33	1849.7
41	440	-15950	-489	-316	0	674	-10130	14.07	14.07	6.03	6.03	-41.03	1237.1
42	440	-16220	-498	-182	0	418	-10370	14.07	14.07	6.03	6.03	-42.02	1273.4
43	440	-12910	-380	-282	0	586	-12180	14.07	14.07	6.03	6.03	-49.88	1915.3
44	440	-17770	-549	-318	0	726	-6429	14.07	14.07	6.03	6.03	-24.25	367.9
45	440	-14840	-445	-53	0	201	-8540	14.07	14.07	6.03	6.03	-34.35	953.8
46	440	-13450	-395	-253	0	600	-6947	14.07	14.07	6.03	6.03	-27.67	691.7
47	440	-12820	-372	-238	0	582	-6150	14.07	14.07	6.03	6.03	-24.28	559.3
49	440	-12520	-362	-239	0	574	-6957	14.07	14.07	6.03	6.03	-27.90	750.2
50	440	-13500	-395	-246	0	601	-5807	14.07	14.07	6.03	6.03	-22.58	452.2
51	440	-12910	-374	-193	0	496	-6229	14.07	14.07	6.03	6.03	-24.61	570.7

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

ASTA NUM. 16 NI 263 NF 264 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 25B
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-20070	486	-380	0	-959	-598	4.02	4.02	10.05	10.05	-15.13	-215.2
41	0	-18370	57	-303	0	-787	119	4.02	4.02	10.05	10.05	-13.40	-191.4
42	0	-18110	60	-262	0	-445	114	4.02	4.02	10.05	10.05	-11.60	-168.5
43	0	-20340	780	-341	0	-872	-1103	4.02	4.02	10.05	10.05	-19.70	-245.4
44	0	-15410	-660	-198	0	-548	1321	4.02	4.02	10.05	10.05	-20.52	-237.4
45	0	-17070	70	-145	0	-15	84	4.02	4.02	10.05	10.05	-8.96	-134.2
46	0	-16990	70	-158	0	-465	77	4.02	4.02	10.05	10.05	-11.11	-161.0
47	0	-16640	73	-122	0	-384	66	4.02	4.02	10.05	10.05	-10.54	-153.4
49	0	-17210	216	-148	0	-442	-173	4.02	4.02	10.05	10.05	-11.11	-161.3
50	0	-16220	-72	-119	0	-377	312	4.02	4.02	10.05	10.05	-10.55	-149.6
51	0	-16550	74	-108	0	-270	64	4.02	4.02	10.05	10.05	-9.93	-145.7

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	97	-19632	425	-380	0	-588	-154	4.02	4.02	10.05	10.05	-13.09	-189.2
41	97	-17932	57	-303	0	-491	175	4.02	4.02	10.05	10.05	-11.73	-170.0
42	97	-17672	60	-175	0	-232	172	4.02	4.02	10.05	10.05	-10.33	-152.2
43	97	-19902	678	-341	0	-540	-392	4.02	4.02	10.05	10.05	-13.03	-188.3
44	97	-14970	-558	-198	0	-354	727	4.02	4.02	10.05	10.05	-13.73	-172.9
45	97	-16632	70	1	0	53	152	4.02	4.02	10.05	10.05	-9.29	-133.2
46	97	-16550	70	-158	0	-310	145	4.02	4.02	10.05	10.05	-10.13	-148.2
47	97	-16200	73	-122	0	-265	137	4.02	4.02	10.05	10.05	-9.73	-142.7
49	97	-16770	195	-148	0	-298	28	4.02	4.02	10.05	10.05	-10.18	-149.1
50	97	-15780	-52	-119	0	-260	252	4.02	4.02	10.05	10.05	-9.79	-139.1
51	97	-16112	74	-79	0	-179	136	4.02	4.02	10.05	10.05	-9.26	-136.7

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	195	-19195	364	-380	0	-217	230	4.02	4.02	10.05	10.05	-11.23	-163.2
41	195	-17495	57	-303	0	-196	231	4.02	4.02	10.05	10.05	-10.42	-148.6
42	195	-17235	60	-101	0	-99	231	4.02	4.02	10.05	10.05	-10.30	-144.0
43	195	-19465	575	-341	0	-207	219	4.02	4.02	10.05	10.05	-11.25	-164.6
44	195	-14530	-456	-198	0	-161	233	4.02	4.02	10.05	10.05	-9.03	-124.9
45	195	-16195	70	125	0	-9	219	4.02	4.02	10.05	10.05	-9.70	-135.5
46	195	-16110	70	-158	0	-156	213	4.02	4.02	10.05	10.05	-9.60	-135.3
47	195	-15760	73	-122	0	-146	208	4.02	4.02	10.05	10.05	-9.39	-132.0
49	195	-16330	175	-148	0	-154	208	4.02	4.02	10.05	10.05	-9.66	-136.9
50	195	-15340	-31	-119	0	-144	211	4.02	4.02	10.05	10.05	-9.22	-128.7
51	195	-15675	74	-54	0	-114	208	4.02	4.02	10.05	10.05	-9.35	-130.8

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	292	-18758	302	-380	0	154	555	4.02	4.02	10.05	10.05	-13.97	-184.3
41	292	-17058	57	-303	0	100	287	4.02	4.02	10.05	10.05	-10.72	-147.8
42	292	-16798	60	-39	0	-32	289	4.02	4.02	10.05	10.05	-10.62	-146.2
43	292	-19028	473	-341	0	126	730	4.02	4.02	10.05	10.05	-15.68	-202.1
44	292	-14090	-353	-198	0	32	-161	4.02	4.02	10.05	10.05	-8.17	-115.2
45	292	-15758	70	228	0	-183	287	4.02	4.02	10.05	10.05	-10.10	-138.5
46	292	-15670	70	-158	0	-2	281	4.02	4.02	10.05	10.05	-10.01	-137.4
47	292	-15320	73	-122	0	-27	280	4.02	4.02	10.05	10.05	-9.83	-134.7
49	292	-15890	154	-148	0	-10	369	4.02	4.02	10.05	10.05	-10.91	-146.9
50	292	-14900	-11	-119	0	-28	191	4.02	4.02	10.05	10.05	-8.82	-123.7
51	292	-15238	74	-34	0	-71	280	4.02	4.02	10.05	10.05	-9.80	-134.2

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	390	-18320	241	-380	0	525	820	4.02	4.02	10.05	10.05	-16.16	-205.2
41	390	-16620	57	-303	0	396	343	4.02	4.02	10.05	10.05	-11.02	-153.9
42	390	-16360	60	11	0	-19	348	4.02	4.02	10.05	10.05	-10.94	-148.4
43	390	-18590	371	-341	0	458	1141	4.02	4.02	10.05	10.05	-19.31	-237.1
44	390	-13650	-251	-198	0	226	-456	4.02	4.02	10.05	10.05	-10.63	-138.8
45	390	-15320	70	311	0	-448	355	4.02	4.02	10.05	10.05	-10.51	-147.0
46	390	-15230	70	-158	0	152	349	4.02	4.02	10.05	10.05	-10.42	-140.4
47	390	-14880	73	-122	0	92	351	4.02	4.02	10.05	10.05	-10.26	-138.0
49	390	-15450	134	-148	0	134	509	4.02	4.02	10.05	10.05	-11.98	-156.5
50	390	-14460	10	-119	0	88	190	4.02	4.02	10.05	10.05	-8.61	-120.5
51	390	-14800	74	-17	0	-47	352	4.02	4.02	10.05	10.05	-10.24	-137.6

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

ASTA NUM. 17 NI 49 NF 51 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 31C
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-11930	1098	-18	0	-45	-4639	14.07	14.07	6.03	6.03	-17.73	304.9
41	0	-12960	821	-60	0	-105	-4913	14.07	14.07	6.03	6.03	-18.70	308.1
42	0	-13030	854	73	0	49	-5086	14.07	14.07	6.03	6.03	-19.46	336.6
43	0	-9640	1092	11	0	-6	-3426	14.07	14.07	6.03	6.03	-12.88	189.0
44	0	-15030	386	-126	0	-202	-5542	14.07	14.07	6.03	6.03	-20.98	329.4
45	0	-11480	686	163	0	151	-4171	14.07	14.07	6.03	6.03	-15.75	240.8
46	0	-10400	517	-57	0	-106	-3266	14.07	14.07	6.03	6.03	-12.01	-159.0
47	0	-9755	441	-57	0	-106	-2854	14.07	14.07	6.03	6.03	-10.38	-138.7
49	0	-9412	533	-43	0	-86	-2763	14.07	14.07	6.03	6.03	-10.05	-134.3
50	0	-10490	392	-70	0	-126	-3186	14.07	14.07	6.03	6.03	-11.65	-155.0
51	0	-9779	452	-12	0	-55	-2912	14.07	14.07	6.03	6.03	-10.62	-141.6

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	83	-11270	960	-18	0	-30	-3790	14.07	14.07	6.03	6.03	-14.10	185.5
41	83	-12300	821	-60	0	-56	-4236	14.07	14.07	6.03	6.03	-15.83	218.6
42	83	-12370	854	73	0	-12	-4382	14.07	14.07	6.03	6.03	-16.46	240.0
43	83	-8980	863	11	0	-15	-2619	14.07	14.07	6.03	6.03	-9.52	-127.3
44	83	-14370	616	-126	0	-97	-5129	14.07	14.07	6.03	6.03	-19.30	285.4
45	83	-10820	686	163	0	16	-3605	14.07	14.07	6.03	6.03	-13.39	-176.0
46	83	-9739	517	-57	0	-59	-2840	14.07	14.07	6.03	6.03	-10.32	-138.0
47	83	-9095	441	-57	0	-60	-2490	14.07	14.07	6.03	6.03	-8.99	-121.0
49	83	-8752	488	-43	0	-51	-2342	14.07	14.07	6.03	6.03	-8.43	-113.9
50	83	-9830	438	-70	0	-68	-2844	14.07	14.07	6.03	6.03	-10.32	-138.2
51	83	-9119	452	-12	0	-45	-2539	14.07	14.07	6.03	6.03	-9.18	-123.4

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	165	-10610	823	-18	0	-15	-3054	14.07	14.07	6.03	6.03	-11.08	-148.4
41	165	-11640	821	-60	0	-7	-3559	14.07	14.07	6.03	6.03	-13.03	-173.1
42	165	-11710	854	73	0	-72	-3677	14.07	14.07	6.03	6.03	-13.52	-179.1
43	165	-8320	634	11	0	-23	-2002	14.07	14.07	6.03	6.03	-7.18	-98.0
44	165	-13710	845	-126	0	7	-4526	14.07	14.07	6.03	6.03	-16.79	-220.9
45	165	-10160	686	163	0	-118	-3040	14.07	14.07	6.03	6.03	-11.09	-147.8
46	165	-9078	517	-57	0	-12	-2413	14.07	14.07	6.03	6.03	-8.68	-117.3
47	165	-8435	441	-57	0	-13	-2126	14.07	14.07	6.03	6.03	-7.63	-103.7
49	165	-8092	442	-43	0	-16	-1958	14.07	14.07	6.03	6.03	-7.03	-95.9
50	165	-9170	484	-70	0	-10	-2463	14.07	14.07	6.03	6.03	-8.87	-119.7
51	165	-8459	452	-12	0	-35	-2166	14.07	14.07	6.03	6.03	-7.78	-105.5

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	248	-9951	685	-18	0	0	-2432	14.07	14.07	6.03	6.03	-8.73	-118.9
41	248	-10980	821	-60	0	43	-2882	14.07	14.07	6.03	6.03	-10.36	-140.2
42	248	-11050	854	73	0	-132	-2972	14.07	14.07	6.03	6.03	-10.71	-144.5
43	248	-7660	404	11	0	-32	-1573	14.07	14.07	6.03	6.03	-5.74	-79.3
44	248	-13050	1075	-126	0	111	-3734	14.07	14.07	6.03	6.03	-13.54	-181.4
45	248	-9499	686	163	0	-253	-2474	14.07	14.07	6.03	6.03	-8.89	-120.4
46	248	-8418	517	-57	0	36	-1986	14.07	14.07	6.03	6.03	-7.13	-97.5
47	248	-7775	441	-57	0	34	-1763	14.07	14.07	6.03	6.03	-6.35	-87.0
49	248	-7432	396	-43	0	20	-1613	14.07	14.07	6.03	6.03	-5.83	-80.3
50	248	-8510	530	-70	0	49	-2045	14.07	14.07	6.03	6.03	-7.34	-100.2
51	248	-7799	452	-12	0	-24	-1793	14.07	14.07	6.03	6.03	-6.45	-88.3

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	330	-9291	547	-18	0	16	-1924	14.07	14.07	6.03	6.03	-7.01	-96.8
41	330	-10320	821	-60	0	92	-2205	14.07	14.07	6.03	6.03	-7.99	-110.1
42	330	-10390	854	73	0	-192	-2268	14.07	14.07	6.03	6.03	-8.20	-112.7
43	330	-7000	175	11	0	-41	-1334	14.07	14.07	6.03	6.03	-4.95	-68.7
44	330	-12390	1304	-126	0	216	-2753	14.07	14.07	6.03	6.03	-9.93	-136.4
45	330	-8839	686	163	0	-388	-1908	14.07	14.07	6.03	6.03	-6.90	-95.1
46	330	-7757	517	-57	0	83	-1560	14.07	14.07	6.03	6.03	-5.71	-79.0
47	330	-7115	441	-57	0	81	-1399	14.07	14.07	6.03	6.03	-5.15	-71.3
49	330	-6772	350	-43	0	55	-1305	14.07	14.07	6.03	6.03	-4.83	-66.9
50	330	-7850	576	-70	0	107	-1589	14.07	14.07	6.03	6.03	-5.81	-80.4
51	330	-7139	452	-12	0	-14	-1420	14.07	14.07	6.03	6.03	-5.21	-72.2

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

ASTA NUM. 18 NI 92 NF 94 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 30C
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-15030	2563	-216	0	-319	-10620	14.07	14.07	6.03	6.03	-43.23	1408.8
41	0	-15460	1850	-221	0	-339	-9285	14.07	14.07	6.03	6.03	-37.47	1079.7
42	0	-15500	1870	-84	0	-150	-9370	14.07	14.07	6.03	6.03	-37.83	1096.1
43	0	-12630	2633	-168	0	-241	-9613	14.07	14.07	6.03	6.03	-39.23	1341.3
44	0	-16610	728	-234	0	-377	-7386	14.07	14.07	6.03	6.03	-28.86	604.8
45	0	-13430	1479	51	0	42	-7529	14.07	14.07	6.03	6.03	-30.22	819.3
46	0	-12080	1203	-151	0	-234	-6249	14.07	14.07	6.03	6.03	-24.89	623.3
47	0	-11240	1041	-133	0	-208	-5490	14.07	14.07	6.03	6.03	-21.73	510.9
49	0	-11090	1279	-132	0	-202	-5935	14.07	14.07	6.03	6.03	-23.72	615.0
50	0	-11890	898	-145	0	-229	-5490	14.07	14.07	6.03	6.03	-21.57	474.3
51	0	-11250	1048	-88	0	-145	-5518	14.07	14.07	6.03	6.03	-21.85	516.2

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	83	-14370	2425	-216	0	-141	-8562	14.07	14.07	6.03	6.03	-34.54	988.5
41	83	-14800	1850	-221	0	-156	-7758	14.07	14.07	6.03	6.03	-30.95	785.7
42	83	-14840	1870	-84	0	-80	-7827	14.07	14.07	6.03	6.03	-31.24	798.1
43	83	-11970	2404	-168	0	-102	-7535	14.07	14.07	6.03	6.03	-30.50	913.2
44	83	-15950	958	-234	0	-184	-6691	14.07	14.07	6.03	6.03	-25.91	500.7
45	83	-12770	1479	51	0	-0	-6309	14.07	14.07	6.03	6.03	-25.00	595.6
46	83	-11420	1203	-151	0	-110	-5256	14.07	14.07	6.03	6.03	-20.64	452.1
47	83	-10580	1041	-133	0	-98	-4631	14.07	14.07	6.03	6.03	-18.05	370.4
49	83	-10431	1233	-132	0	-93	-4899	14.07	14.07	6.03	6.03	-19.29	433.1

50	83	-11230	944	-145	0	-109	-4730	14.07	14.07	6.03	6.03	-18.33	356.4
51	83	-10591	1048	-88	0	-73	-4654	14.07	14.07	6.03	6.03	-18.15	374.3

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	165	-13710	2288	-216	0	37	-6618	14.07	14.07	6.03	6.03	-26.15	606.8
41	165	-14140	1850	-221	0	26	-6232	14.07	14.07	6.03	6.03	-24.32	503.6
42	165	-14180	1870	-84	0	-10	-6284	14.07	14.07	6.03	6.03	-24.55	512.0
43	165	-11310	2175	-168	0	37	-5646	14.07	14.07	6.03	6.03	-22.40	539.8
44	165	-15290	1187	-234	0	9	-5806	14.07	14.07	6.03	6.03	-22.10	365.2
45	165	-12110	1479	51	0	-42	-5089	14.07	14.07	6.03	6.03	-19.71	382.0
46	165	-10760	1203	-151	0	15	-4264	14.07	14.07	6.03	6.03	-16.35	289.8
47	165	-9919	1041	-133	0	12	-3772	14.07	14.07	6.03	6.03	-14.36	237.8
49	165	-9772	1187	-132	0	15	-3900	14.07	14.07	6.03	6.03	-14.98	268.5
50	165	-10570	989	-145	0	10	-3933	14.07	14.07	6.03	6.03	-14.91	237.9
51	165	-9932	1048	-88	0	-0	-3789	14.07	14.07	6.03	6.03	-14.44	240.4

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	248	-13050	2150	-216	0	215	-4788	14.07	14.07	6.03	6.03	-18.11	281.8
41	248	-13480	1850	-221	0	209	-4705	14.07	14.07	6.03	6.03	-17.63	250.0
42	248	-13520	1870	-84	0	59	-4742	14.07	14.07	6.03	6.03	-17.79	254.4
43	248	-10651	1945	-168	0	175	-3946	14.07	14.07	6.03	6.03	-14.95	236.8
44	248	-14630	1417	-234	0	203	-4732	14.07	14.07	6.03	6.03	-17.49	-230.7
45	248	-11450	1479	51	0	-84	-3869	14.07	14.07	6.03	6.03	-14.41	191.4
46	248	-10101	1203	-151	0	139	-3271	14.07	14.07	6.03	6.03	-12.09	-159.5
47	248	-9258	1041	-133	0	122	-2912	14.07	14.07	6.03	6.03	-10.71	-141.8
49	248	-9114	1141	-132	0	124	-2940	14.07	14.07	6.03	6.03	-10.86	-143.3
50	248	-9911	1035	-145	0	129	-3097	14.07	14.07	6.03	6.03	-11.38	-150.8
51	248	-9273	1048	-88	0	72	-2924	14.07	14.07	6.03	6.03	-10.76	-142.4

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	330	-12390	2012	-216	0	393	-3071	14.07	14.07	6.03	6.03	-11.02	-150.0
41	330	-12820	1850	-221	0	391	-3179	14.07	14.07	6.03	6.03	-11.41	-155.2
42	330	-12860	1870	-84	0	129	-3199	14.07	14.07	6.03	6.03	-11.48	-156.2
43	330	-9991	1716	-168	0	314	-2436	14.07	14.07	6.03	6.03	-8.74	-119.1
44	330	-13970	1646	-234	0	396	-3469	14.07	14.07	6.03	6.03	-12.45	-169.4
45	330	-10790	1479	51	0	-126	-2649	14.07	14.07	6.03	6.03	-9.51	-129.5
46	330	-9441	1203	-151	0	264	-2278	14.07	14.07	6.03	6.03	-8.18	-111.5
47	330	-8598	1041	-133	0	232	-2053	14.07	14.07	6.03	6.03	-7.37	-100.6
49	330	-8455	1095	-132	0	232	-2017	14.07	14.07	6.03	6.03	-7.24	-98.9
50	330	-9251	1081	-145	0	249	-2224	14.07	14.07	6.03	6.03	-7.98	-108.9
51	330	-8614	1048	-88	0	144	-2060	14.07	14.07	6.03	6.03	-7.40	-101.0

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

ASTA NUM. 19 NI 135 NF 137 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 29C
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-14830	2491	-439	0	-684	-10410	14.07	14.07	6.03	6.03	-42.37	1374.4
41	0	-15400	1812	-404	0	-636	-9197	14.07	14.07	6.03	6.03	-37.10	1064.0
42	0	-15340	1782	-249	0	-411	-9087	14.07	14.07	6.03	6.03	-36.64	1043.3
43	0	-12350	2546	-379	0	-587	-9335	14.07	14.07	6.03	6.03	-38.09	1296.7
44	0	-16790	744	-358	0	-574	-7498	14.07	14.07	6.03	6.03	-29.32	617.8
45	0	-13210	1364	-62	0	-131	-7130	14.07	14.07	6.03	6.03	-28.52	745.6
46	0	-12050	1176	-271	0	-429	-6185	14.07	14.07	6.03	6.03	-24.62	611.3
47	0	-11210	1017	-237	0	-377	-5431	14.07	14.07	6.03	6.03	-21.47	500.2
49	0	-11020	1243	-249	0	-393	-5836	14.07	14.07	6.03	6.03	-23.30	597.8
50	0	-11910	882	-244	0	-391	-5468	14.07	14.07	6.03	6.03	-21.47	468.7
51	0	-11190	1007	-185	0	-302	-5395	14.07	14.07	6.03	6.03	-21.32	493.8

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	83	-14170	2353	-439	0	-322	-8412	14.07	14.07	6.03	6.03	-33.92	967.7
41	83	-14740	1812	-404	0	-302	-7702	14.07	14.07	6.03	6.03	-30.71	777.1
42	83	-14680	1782	-249	0	-205	-7617	14.07	14.07	6.03	6.03	-30.35	762.3
43	83	-11691	2317	-379	0	-274	-7329	14.07	14.07	6.03	6.03	-29.66	885.2
44	83	-16130	973	-358	0	-279	-6790	14.07	14.07	6.03	6.03	-26.31	511.0
45	83	-12550	1364	-62	0	-79	-6004	14.07	14.07	6.03	6.03	-23.70	544.1
46	83	-11389	1176	-271	0	-206	-5215	14.07	14.07	6.03	6.03	-20.47	445.3
47	83	-10550	1017	-237	0	-182	-4592	14.07	14.07	6.03	6.03	-17.89	364.3
49	83	-10360	1197	-249	0	-188	-4829	14.07	14.07	6.03	6.03	-19.00	422.8
50	83	-11249	928	-244	0	-189	-4721	14.07	14.07	6.03	6.03	-18.28	353.6
51	83	-10530	1007	-185	0	-149	-4564	14.07	14.07	6.03	6.03	-17.77	359.7

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	165	-13510	2216	-439	0	41	-6527	14.07	14.07	6.03	6.03	-25.80	599.0
41	165	-14080	1812	-404	0	31	-6208	14.07	14.07	6.03	6.03	-24.23	501.8
42	165	-14020	1782	-249	0	1	-6146	14.07	14.07	6.03	6.03	-23.97	492.8
43	165	-11032	2088	-379	0	39	-5513	14.07	14.07	6.03	6.03	-21.87	527.7
44	165	-15470	1202	-358	0	16	-5892	14.07	14.07	6.03	6.03	-22.44	372.8
45	165	-11890	1364	-62	0	-28	-4878	14.07	14.07	6.03	6.03	-18.82	352.1
46	165	-10728	1176	-271	0	18	-4245	14.07	14.07	6.03	6.03	-16.28	287.9
47	165	-9889	1017	-237	0	14	-3754	14.07	14.07	6.03	6.03	-14.29	236.0
49	165	-9699	1151	-249	0	17	-3861	14.07	14.07	6.03	6.03	-14.82	264.6
50	165	-10588	974	-244	0	13	-3936	14.07	14.07	6.03	6.03	-14.93	237.8
51	165	-9869	1007	-185	0	4	-3734	14.07	14.07	6.03	6.03	-14.20	233.3

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	248	-12850	2078	-439	0	403	-4756	14.07	14.07	6.03	6.03	-18.02	284.8
41	248	-13420	1812	-404	0	365	-4713	14.07	14.07	6.03	6.03	-17.68	253.6
42	248	-13360	1782	-249	0	207	-4676	14.07	14.07	6.03	6.03	-17.53	249.9
43	248	-10374	1858	-379	0	351	-3885	14.07	14.07	6.03	6.03	-14.75	238.1
44	248	-14810	1432	-358	0	311	-4806	14.07	14.07	6.03	6.03	-17.77	-234.3
45	248	-11230	1364	-62	0	23	-3753	14.07	14.07	6.03	6.03	-13.95	-183.2
46	248	-10068	1176	-271	0	241	-3275	14.07	14.07	6.03	6.03	-12.11	-159.7
47	248	-9228	1017	-237	0	210	-2916	14.07	14.07	6.03	6.03	-10.73	-142.0
49	248	-9038	1105	-249	0	222	-2930	14.07	14.07	6.03	6.03	-10.83	-142.9
50	248	-9926	1020	-244	0	215	-3114	14.07	14.07	6.03	6.03	-11.44	-151.6

51	248	-9208	1007	-185	0	157	-2904	14.07	14.07	6.03	6.03	-10.68	-141.4

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	330	-12190	1940	-439	0	766	-3098	14.07	14.07	6.03	6.03	-11.12	-151.0
41	330	-12760	1812	-404	0	699	-3218	14.07	14.07	6.03	6.03	-11.55	-156.9
42	330	-12700	1782	-249	0	412	-3206	14.07	14.07	6.03	6.03	-11.51	-156.3
43	330	-9715	1629	-379	0	664	-2447	14.07	14.07	6.03	6.03	-8.78	-119.3
44	330	-14150	1661	-358	0	606	-3530	14.07	14.07	6.03	6.03	-12.67	-172.3
45	330	-10570	1364	-62	0	75	-2627	14.07	14.07	6.03	6.03	-9.43	-128.3
46	330	-9407	1176	-271	0	464	-2305	14.07	14.07	6.03	6.03	-8.27	-112.7
47	330	-8568	1017	-237	0	405	-2077	14.07	14.07	6.03	6.03	-7.45	-101.6
49	330	-8378	1059	-249	0	428	-2037	14.07	14.07	6.03	6.03	-7.31	-99.7
50	330	-9265	1066	-244	0	416	-2253	14.07	14.07	6.03	6.03	-8.09	-110.2
51	330	-8548	1007	-185	0	310	-2073	14.07	14.07	6.03	6.03	-7.44	-101.4

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

ASTA NUM. 20 NI 178 NF 180 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 28C
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-14650	2424	-507	0	-823	-10250	14.07	14.07	6.03	6.03	-41.71	1350.1
41	0	-15180	1722	-476	0	-765	-8897	14.07	14.07	6.03	6.03	-35.84	1011.3
42	0	-15190	1720	-296	0	-497	-8897	14.07	14.07	6.03	6.03	-35.84	1010.7
43	0	-12230	2509	-425	0	-688	-9318	14.07	14.07	6.03	6.03	-38.03	1301.0
44	0	-16490	613	-438	0	-695	-6952	14.07	14.07	6.03	6.03	-26.94	524.5
45	0	-13120	1335	-73	0	-145	-7057	14.07	14.07	6.03	6.03	-28.22	735.3
46	0	-11870	1108	-310	0	-489	-5953	14.07	14.07	6.03	6.03	-23.63	572.4
47	0	-11050	955	-269	0	-420	-5216	14.07	14.07	6.03	6.03	-20.55	464.3
49	0	-10870	1189	-279	0	-439	-5669	14.07	14.07	6.03	6.03	-22.60	570.7
50	0	-11720	810	-282	0	-440	-5196	14.07	14.07	6.03	6.03	-20.30	423.6
51	0	-11050	954	-209	0	-330	-5217	14.07	14.07	6.03	6.03	-20.56	464.5

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	83	-13990	2286	-507	0	-404	-8308	14.07	14.07	6.03	6.03	-33.50	956.0
41	83	-14520	1722	-476	0	-373	-7477	14.07	14.07	6.03	6.03	-29.77	741.8
42	83	-14530	1720	-296	0	-252	-7478	14.07	14.07	6.03	6.03	-29.77	741.5
43	83	-11571	2280	-425	0	-338	-7342	14.07	14.07	6.03	6.03	-29.74	896.0
44	83	-15830	842	-438	0	-333	-6352	14.07	14.07	6.03	6.03	-24.42	441.5
45	83	-12460	1335	-73	0	-85	-5955	14.07	14.07	6.03	6.03	-23.50	538.9
46	83	-11210	1108	-310	0	-233	-5038	14.07	14.07	6.03	6.03	-19.72	419.0
47	83	-10389	955	-269	0	-198	-4428	14.07	14.07	6.03	6.03	-17.19	340.0
49	83	-10210	1143	-279	0	-209	-4707	14.07	14.07	6.03	6.03	-18.49	405.7
50	83	-11060	856	-282	0	-208	-4509	14.07	14.07	6.03	6.03	-17.38	322.0
51	83	-10390	954	-209	0	-158	-4430	14.07	14.07	6.03	6.03	-17.20	340.2

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	165	-13330	2149	-507	0	14	-6479	14.07	14.07	6.03	6.03	-25.62	599.2
41	165	-13860	1722	-476	0	20	-6056	14.07	14.07	6.03	6.03	-23.61	483.2
42	165	-13870	1720	-296	0	-8	-6060	14.07	14.07	6.03	6.03	-23.62	483.2
43	165	-10912	2051	-425	0	13	-5556	14.07	14.07	6.03	6.03	-22.09	544.0
44	165	-15170	1071	-438	0	28	-5563	14.07	14.07	6.03	6.03	-21.04	327.1
45	165	-11800	1335	-73	0	-25	-4854	14.07	14.07	6.03	6.03	-18.74	351.8
46	165	-10551	1108	-310	0	23	-4124	14.07	14.07	6.03	6.03	-15.78	273.6
47	165	-9728	955	-269	0	24	-3640	14.07	14.07	6.03	6.03	-13.82	222.8
49	165	-9550	1098	-279	0	22	-3782	14.07	14.07	6.03	6.03	-14.51	256.9
50	165	-10400	902	-282	0	25	-3784	14.07	14.07	6.03	6.03	-14.29	219.1
51	165	-9729	954	-209	0	14	-3642	14.07	14.07	6.03	6.03	-13.83	223.0

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	248	-12670	2012	-507	0	433	-4764	14.07	14.07	6.03	6.03	-18.10	294.1
41	248	-13200	1722	-476	0	412	-4636	14.07	14.07	6.03	6.03	-17.39	249.5
42	248	-13210	1720	-296	0	236	-4641	14.07	14.07	6.03	6.03	-17.41	249.9
43	248	-10254	1821	-425	0	363	-3959	14.07	14.07	6.03	6.03	-15.12	256.9
44	248	-14510	1301	-438	0	390	-4585	14.07	14.07	6.03	6.03	-16.87	-223.3
45	248	-11140	1335	-73	0	35	-3752	14.07	14.07	6.03	6.03	-13.97	184.3
46	248	-9892	1108	-310	0	279	-3210	14.07	14.07	6.03	6.03	-11.87	-156.5
47	248	-9066	955	-269	0	246	-2853	14.07	14.07	6.03	6.03	-10.49	-138.9
49	248	-8890	1052	-279	0	252	-2896	14.07	14.07	6.03	6.03	-10.71	-141.2
50	248	-9740	947	-282	0	258	-3022	14.07	14.07	6.03	6.03	-11.09	-147.1
51	248	-9068	954	-209	0	187	-2854	14.07	14.07	6.03	6.03	-10.50	-139.0

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	330	-12010	1874	-507	0	851	-3162	14.07	14.07	6.03	6.03	-11.37	-153.8
41	330	-12540	1722	-476	0	804	-3216	14.07	14.07	6.03	6.03	-11.55	-156.7
42	330	-12550	1720	-296	0	480	-3222	14.07	14.07	6.03	6.03	-11.57	-156.9
43	330	-9595	1592	-425	0	714	-2551	14.07	14.07	6.03	6.03	-9.18	-124.1
44	330	-13850	1530	-438	0	751	-3417	14.07	14.07	6.03	6.03	-12.26	-166.9
45	330	-10480	1335	-73	0	95	-2650	14.07	14.07	6.03	6.03	-9.51	-129.2
46	330	-9232	1108	-310	0	535	-2295	14.07	14.07	6.03	6.03	-8.24	-112.1
47	330	-8405	955	-269	0	467	-2065	14.07	14.07	6.03	6.03	-7.41	-100.9
49	330	-8230	1006	-279	0	483	-2047	14.07	14.07	6.03	6.03	-7.35	-99.9
50	330	-9080	993	-282	0	490	-2221	14.07	14.07	6.03	6.03	-7.97	-108.6
51	330	-8408	954	-209	0	359	-2067	14.07	14.07	6.03	6.03	-7.42	-101.0

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

ASTA NUM. 21 NI 221 NF 223 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 27C
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	

40	0	-12890	3385	-1431	0	-2661	-13360	14.07	14.07	6.03	6.03	-54.73	2191.7
41	0	-13660	2280	-1311	0	-2402	-10600	14.07	14.07	6.03	6.03	-43.28	1497.3
42	0	-13780	2344	-1111	0	-2064	-10850	14.07	14.07	6.03	6.03	-44.32	1546.5
43	0	-10640	3622	-1245	0	-2411	-13000	14.07	14.07	6.03	6.03	-53.21	2270.7
44	0	-15310	515	-1154	0	-2039	-6354	14.07	14.07	6.03	6.03	-24.56	467.4
45	0	-12130	1887	-711	0	-1417	-8815	14.07	14.07	6.03	6.03	-35.92	1192.7
46	0	-10880	1479	-885	0	-1728	-7075	14.07	14.07	6.03	6.03	-28.69	881.0
47	0	-10190	1279	-779	0	-1560	-6194	14.07	14.07	6.03	6.03	-25.02	728.2
49	0	-9931	1648	-819	0	-1646	-7116	14.07	14.07	6.03	6.03	-28.99	953.4
50	0	-10870	1026	-800	0	-1571	-5786	14.07	14.07	6.03	6.03	-23.12	596.0
51	0	-10230	1301	-712	0	-1447	-6278	14.07	14.07	6.03	6.03	-25.37	744.3

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	83	-12230	3247	-1431	0	-1480	-10625	14.07	14.07	6.03	6.03	-43.48	1602.4
41	83	-13000	2280	-1311	0	-1320	-8719	14.07	14.07	6.03	6.03	-35.42	1112.6
42	83	-13120	2344	-1111	0	-1148	-8916	14.07	14.07	6.03	6.03	-36.24	1149.2
43	83	-9980	3393	-1245	0	-1384	-10108	14.07	14.07	6.03	6.03	-41.41	1641.7
44	83	-14650	745	-1154	0	-1088	-5834	14.07	14.07	6.03	6.03	-22.40	400.1
45	83	-11471	1887	-711	0	-830	-7258	14.07	14.07	6.03	6.03	-29.39	883.5
46	83	-10220	1479	-885	0	-998	-5855	14.07	14.07	6.03	6.03	-23.54	651.0
47	83	-9530	1279	-779	0	-918	-5139	14.07	14.07	6.03	6.03	-20.56	536.9
49	83	-9271	1602	-819	0	-970	-5775	14.07	14.07	6.03	6.03	-23.36	693.8
50	83	-10209	1072	-800	0	-911	-4920	14.07	14.07	6.03	6.03	-19.44	450.1
51	83	-9570	1301	-712	0	-860	-5205	14.07	14.07	6.03	6.03	-20.84	548.8

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	165	-11570	3110	-1431	0	-299	-8004	14.07	14.07	6.03	6.03	-32.56	1045.5
41	165	-12340	2280	-1311	0	-239	-6838	14.07	14.07	6.03	6.03	-27.42	735.4
42	165	-12460	2344	-1111	0	-231	-6982	14.07	14.07	6.03	6.03	-28.03	759.4
43	165	-9320	3164	-1245	0	-356	-7405	14.07	14.07	6.03	6.03	-30.25	1061.2
44	165	-13990	974	-1154	0	-136	-5125	14.07	14.07	6.03	6.03	-19.38	300.7
45	165	-10812	1887	-711	0	-244	-5701	14.07	14.07	6.03	6.03	-22.75	581.1
46	165	-9561	1479	-885	0	-268	-4634	14.07	14.07	6.03	6.03	-18.32	427.1
47	165	-8869	1279	-779	0	-275	-4084	14.07	14.07	6.03	6.03	-16.04	351.4
49	165	-8611	1556	-819	0	-295	-4473	14.07	14.07	6.03	6.03	-17.82	448.2
50	165	-9548	1118	-800	0	-250	-4017	14.07	14.07	6.03	6.03	-15.56	302.0
51	165	-8910	1301	-712	0	-272	-4132	14.07	14.07	6.03	6.03	-16.24	359.0

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	248	-10910	2972	-1431	0	882	-5496	14.07	14.07	6.03	6.03	-21.83	531.4
41	248	-11680	2280	-1311	0	843	-4958	14.07	14.07	6.03	6.03	-19.24	378.1
42	248	-11800	2344	-1111	0	686	-5048	14.07	14.07	6.03	6.03	-19.61	389.8
43	248	-8661	2934	-1245	0	671	-4891	14.07	14.07	6.03	6.03	-19.64	536.1
44	248	-13330	1204	-1154	0	816	-4227	14.07	14.07	6.03	6.03	-15.56	-205.9
45	248	-10153	1887	-711	0	343	-4144	14.07	14.07	6.03	6.03	-15.98	296.5
46	248	-8902	1479	-885	0	463	-3414	14.07	14.07	6.03	6.03	-13.02	218.8
47	248	-8208	1279	-779	0	368	-3028	14.07	14.07	6.03	6.03	-11.47	180.2
49	248	-7951	1510	-819	0	381	-3208	14.07	14.07	6.03	6.03	-12.34	225.1
50	248	-8886	1164	-800	0	410	-3075	14.07	14.07	6.03	6.03	-11.51	160.4
51	248	-8250	1301	-712	0	315	-3058	14.07	14.07	6.03	6.03	-11.59	183.7

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	330	-10250	2835	-1431	0	2063	-3102	14.07	14.07	6.03	6.03	-13.40	160.9
41	330	-11020	2280	-1311	0	1924	-3077	14.07	14.07	6.03	6.03	-12.45	-149.5
42	330	-11140	2344	-1111	0	1602	-3114	14.07	14.07	6.03	6.03	-11.26	-151.3
43	330	-8001	2705	-1245	0	1698	-2566	14.07	14.07	6.03	6.03	-11.04	142.8
44	330	-12670	1433	-1154	0	1767	-3139	14.07	14.07	6.03	6.03	-11.43	-153.3
45	330	-9494	1887	-711	0	930	-2587	14.07	14.07	6.03	6.03	-9.33	-125.7
46	330	-8242	1479	-885	0	1193	-2194	14.07	14.07	6.03	6.03	-7.90	-106.7
47	330	-7548	1279	-779	0	1010	-1973	14.07	14.07	6.03	6.03	-7.09	-96.0
49	330	-7291	1464	-819	0	1056	-1981	14.07	14.07	6.03	6.03	-7.14	-96.3
50	330	-8225	1210	-800	0	1070	-2096	14.07	14.07	6.03	6.03	-7.53	-102.1
51	330	-7590	1301	-712	0	902	-1985	14.07	14.07	6.03	6.03	-7.14	-96.6

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

ASTA NUM. 22 NI 264 NF 266 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 25C
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-9408	425	-326	0	-934	-984	4.02	4.02	10.05	10.05	-15.07	-165.9
41	0	-8091	-14	-276	0	-833	-220	4.02	4.02	10.05	10.05	-8.27	-113.9
42	0	-7922	-12	-306	0	-622	-221	4.02	4.02	10.05	10.05	-7.16	-99.8
43	0	-9655	787	-386	0	-898	-1589	4.02	4.02	10.05	10.05	-24.47	291.9
44	0	-6024	-752	-192	0	-683	1067	4.02	4.02	10.05	10.05	-16.45	213.6
45	0	-7179	60	-353	0	-378	-316	4.02	4.02	10.05	10.05	-6.29	-80.0
46	0	-7084	98	-321	0	-666	-371	4.02	4.02	10.05	10.05	-6.94	-95.9
47	0	-6832	126	-332	0	-625	-409	4.02	4.02	10.05	10.05	-7.00	-91.4
49	0	-7270	272	-348	0	-659	-664	4.02	4.02	10.05	10.05	-10.24	-116.8
50	0	-6544	-36	-310	0	-616	-133	4.02	4.02	10.05	10.05	-6.41	-88.6
51	0	-6775	127	-342	0	-555	-410	4.02	4.02	10.05	10.05	-6.98	-86.7

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	95	-8980	345	-326	0	-625	-618	4.02	4.02	10.05	10.05	-10.06	-121.4
41	95	-7664	-14	-276	0	-570	-233	4.02	4.02	10.05	10.05	-6.77	-94.6
42	95	-7494	-12	-221	0	-373	-232	4.02	4.02	10.05	10.05	-5.72	-81.2
43	95	-9228	655	-386	0	-531	-904	4.02	4.02	10.05	10.05	-13.87	-155.4
44	95	-5596	-620	-192	0	-500	415	4.02	4.02	10.05	10.05	-6.62	-78.9
45	95	-6752	60	-212	0	-111	-259	4.02	4.02	10.05	10.05	-5.56	-71.7
46	95	-6656	98	-321	0	-362	-279	4.02	4.02	10.05	10.05	-5.70	-74.0
47	95	-6404	126	-332	0	-310	-290	4.02	4.02	10.05	10.05	-5.68	-72.0
49	95	-6842	246	-348	0	-328	-418	4.02	4.02	10.05	10.05	-7.09	-87.1
50	95	-6116	-9	-310	0	-322	-155	4.02	4.02	10.05	10.05	-4.75	-67.4
51	95	-6348	127	-314	0	-244	-289	4.02	4.02	10.05	10.05	-5.65	-71.6

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	190	-8553	266	-326	0	-315	-328	4.02	4.02	10.05	10.05	-7.05	-90.8

41	190	-7236	-14	-276	0	-308	-247	4.02	4.02	10.05	10.05	-5.69	-75.3
42	190	-7067	-12	-148	0	-199	-243	4.02	4.02	10.05	10.05	-5.57	-72.5
43	190	-8800	523	-386	0	-164	-344	4.02	4.02	10.05	10.05	-7.31	-94.0
44	190	-5169	-488	-192	0	-318	-112	4.02	4.02	10.05	10.05	-4.24	-59.8
45	190	-6324	60	-90	0	31	-202	4.02	4.02	10.05	10.05	-4.84	-63.5
46	190	-6229	98	-321	0	-57	-186	4.02	4.02	10.05	10.05	-4.65	-61.3
47	190	-5977	126	-332	0	6	-170	4.02	4.02	10.05	10.05	-4.39	-58.1
49	190	-6415	219	-348	0	3	-197	4.02	4.02	10.05	10.05	-4.84	-63.7
50	190	-5689	17	-310	0	-28	-151	4.02	4.02	10.05	10.05	-4.08	-54.3
51	190	-5920	127	-289	0	42	-169	4.02	4.02	10.05	10.05	-4.35	-57.6

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	285	-8126	187	-326	0	-6	-113	4.02	4.02	10.05	10.05	-4.89	-68.2
41	285	-6808	-14	-276	0	-45	-261	4.02	4.02	10.05	10.05	-5.61	-72.3
42	285	-6640	-12	-88	0	-88	-254	4.02	4.02	10.05	10.05	-5.47	-70.5
43	285	-8372	391	-386	0	203	91	4.02	4.02	10.05	10.05	-5.35	-77.8
44	285	-4742	-356	-192	0	-136	-513	4.02	4.02	10.05	10.05	-7.86	-85.7
45	285	-5896	60	10	0	67	-145	4.02	4.02	10.05	10.05	-4.12	-55.2
46	285	-5802	98	-321	0	248	-93	4.02	4.02	10.05	10.05	-4.23	-60.4
47	285	-5550	126	-332	0	321	-51	4.02	4.02	10.05	10.05	-4.46	-62.9
49	285	-5988	193	-348	0	334	-1	4.02	4.02	10.05	10.05	-4.75	-67.1
50	285	-5262	43	-310	0	266	-122	4.02	4.02	10.05	10.05	-4.04	-57.3
51	285	-5492	127	-269	0	307	-49	4.02	4.02	10.05	10.05	-4.36	-61.6

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	380	-7698	108	-326	0	304	27	4.02	4.02	10.05	10.05	-5.49	-78.6
41	380	-6381	-14	-276	0	218	-275	4.02	4.02	10.05	10.05	-5.53	-70.5
42	380	-6212	-12	-39	0	-28	-265	4.02	4.02	10.05	10.05	-5.37	-68.4
43	380	-7945	259	-386	0	571	400	4.02	4.02	10.05	10.05	-7.41	-96.8
44	380	-4314	-224	-192	0	46	-789	4.02	4.02	10.05	10.05	-12.17	163.5
45	380	-5469	60	91	0	17	-87	4.02	4.02	10.05	10.05	-3.40	-47.0
46	380	-5374	98	-321	0	553	0	4.02	4.02	10.05	10.05	-5.49	-75.7
47	380	-5122	126	-332	0	637	69	4.02	4.02	10.05	10.05	-5.80	-79.1
49	380	-5560	166	-348	0	665	169	4.02	4.02	10.05	10.05	-6.16	-84.2
50	380	-4834	70	-310	0	560	-69	4.02	4.02	10.05	10.05	-5.26	-72.0
51	380	-5065	127	-253	0	555	72	4.02	4.02	10.05	10.05	-5.34	-73.4

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

ASTA NUM. 23 NI 298 NF 271 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 20C
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-10770	915	-133	0	-2025	-1483	6.03	6.03	10.05	10.05	-12.94	-164.9
41	0	-11170	-229	-160	0	-1943	549	6.03	6.03	10.05	10.05	-12.08	-160.3
42	0	-11100	-231	-520	0	-1303	553	6.03	6.03	10.05	10.05	-9.01	-123.3
43	0	-9783	1730	-71	0	-1609	-2945	6.03	6.03	10.05	10.05	-26.12	495.9
44	0	-12060	-2150	-214	0	-1892	3959	6.03	6.03	10.05	10.05	-35.12	711.0
45	0	-10340	-181	-716	0	-406	448	6.03	6.03	10.05	10.05	-6.14	-83.4
46	0	-10010	-148	-90	0	-1190	377	6.03	6.03	10.05	10.05	-8.18	-111.9
47	0	-9718	-127	-73	0	-1002	334	6.03	6.03	10.05	10.05	-7.37	-101.6
49	0	-9586	254	-64	0	-1029	-344	6.03	6.03	10.05	10.05	-7.42	-102.0
50	0	-10040	-521	-92	0	-1086	1037	6.03	6.03	10.05	10.05	-9.36	-118.4
51	0	-9697	-128	-193	0	-789	335	6.03	6.03	10.05	10.05	-6.60	-91.9

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	95	-10200	915	-133	0	-1898	-614	6.03	6.03	10.05	10.05	-11.75	-154.8
41	95	-10599	-229	-160	0	-1790	331	6.03	6.03	10.05	10.05	-11.16	-148.6
42	95	-10531	-231	-352	0	-891	334	6.03	6.03	10.05	10.05	-7.29	-101.3
43	95	-9213	1730	-71	0	-1542	-1302	6.03	6.03	10.05	10.05	-11.36	-136.3
44	95	-11490	-2150	-214	0	-1688	1917	6.03	6.03	10.05	10.05	-16.75	-194.1
45	95	-9769	-181	-435	0	138	276	6.03	6.03	10.05	10.05	-5.04	-70.3
46	95	-9440	-148	-90	0	-1104	236	6.03	6.03	10.05	10.05	-7.65	-104.7
47	95	-9148	-127	-73	0	-933	213	6.03	6.03	10.05	10.05	-6.90	-95.2
49	95	-9016	254	-64	0	-969	-102	6.03	6.03	10.05	10.05	-6.98	-96.0
50	95	-9470	-521	-92	0	-998	542	6.03	6.03	10.05	10.05	-7.26	-100.0
51	95	-9127	-128	-137	0	-633	214	6.03	6.03	10.05	10.05	-5.82	-81.5

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	190	-9631	915	-133	0	-1772	256	6.03	6.03	10.05	10.05	-10.98	-144.7
41	190	-10028	-229	-160	0	-1638	113	6.03	6.03	10.05	10.05	-10.26	-137.1
42	190	-9962	-231	-208	0	-627	114	6.03	6.03	10.05	10.05	-6.12	-86.1
43	190	-8643	1730	-71	0	-1474	341	6.03	6.03	10.05	10.05	-9.18	-122.1
44	190	-10920	-2150	-214	0	-1484	-126	6.03	6.03	10.05	10.05	-9.71	-131.7
45	190	-9198	-181	-195	0	434	104	6.03	6.03	10.05	10.05	-5.13	-73.0
46	190	-8869	-148	-90	0	-1018	96	6.03	6.03	10.05	10.05	-7.11	-97.5
47	190	-8578	-127	-73	0	-864	92	6.03	6.03	10.05	10.05	-6.43	-88.7
49	190	-8446	254	-64	0	-908	140	6.03	6.03	10.05	10.05	-6.54	-90.0
50	190	-8900	-521	-92	0	-910	46	6.03	6.03	10.05	10.05	-6.73	-92.7
51	190	-8557	-128	-88	0	-527	92	6.03	6.03	10.05	10.05	-5.21	-73.4

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	285	-9062	915	-133	0	-1646	1126	6.03	6.03	10.05	10.05	-10.20	-134.7
41	285	-9458	-229	-160	0	-1486	-105	6.03	6.03	10.05	10.05	-9.36	-125.6
42	285	-9392	-231	-88	0	-489	-105	6.03	6.03	10.05	10.05	-5.40	-76.6
43	285	-8073	1730	-71	0	-1406	1984	6.03	6.03	10.05	10.05	-17.55	276.8
44	285	-10350	-2150	-214	0	-1281	-2168	6.03	6.03	10.05	10.05	-19.09	248.4
45	285	-8626	-181	5	0	521	-68	6.03	6.03	10.05	10.05	-5.22	-73.6
46	285	-8298	-148	-90	0	-933	-44	6.03	6.03	10.05	10.05	-6.58	-90.2
47	285	-8008	-127	-73	0	-794	-29	6.03	6.03	10.05	10.05	-5.96	-82.3
49	285	-7876	254	-64	0	-848	381	6.03	6.03	10.05	10.05	-6.10	-83.9
50	285	-8331	-521	-92	0	-823	-449	6.03	6.03	10.05	10.05	-6.19	-85.4
51	285	-7987	-128	-49	0	-462	-29	6.03	6.03	10.05	10.05	-4.76	-67.2

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	380	-8492	915	-133	0	-1519	1995	6.03	6.03	10.05	10.05	-17.63	264.6
41	380	-8887	-229	-160	0	-1333	-322	6.03	6.03	10.05	10.05	-8.48	-114.2

42	380	-8823	-231	8	0	-453	-325	6.03	6.03	10.05	10.05	-5.05	-71.7
43	380	-7503	1730	-71	0	-1339	3627	6.03	6.03	10.05	10.05	-32.03	803.0
44	380	-9780	-2150	-214	0	-1077	-4210	6.03	6.03	10.05	10.05	-37.25	885.1
45	380	-8055	-181	164	0	437	-240	6.03	6.03	10.05	10.05	-4.70	-66.5
46	380	-7728	-148	-90	0	-847	-184	6.03	6.03	10.05	10.05	-6.04	-83.0
47	380	-7438	-127	-73	0	-725	-150	6.03	6.03	10.05	10.05	-5.49	-75.9
49	380	-7306	254	-64	0	-787	623	6.03	6.03	10.05	10.05	-5.96	-77.9
50	380	-7761	-521	-92	0	-735	-944	6.03	6.03	10.05	10.05	-8.30	-102.5
51	380	-7417	-128	-17	0	-432	-150	6.03	6.03	10.05	10.05	-4.43	-62.5

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

ASTA NUM. 24 NI 78 NF 77 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 6B
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-25680	301	50	0	81	10890	14.07	14.07	6.03	6.03	-42.25	829.4
41	0	-22420	-1031	9	0	-6	12590	14.07	14.07	6.03	6.03	-50.55	1372.3
42	0	-22540	-931	200	0	447	12360	14.07	14.07	6.03	6.03	-49.52	1314.6
43	0	-25860	1392	87	0	168	7441	14.07	14.07	6.03	6.03	-27.00	-361.5
44	0	-17440	-3285	-62	0	-155	15820	14.07	14.07	6.03	6.03	-64.77	2440.0
45	0	-20620	-662	336	0	778	9885	14.07	14.07	6.03	6.03	-39.03	898.1
46	0	-19230	-707	24	0	39	8874	14.07	14.07	6.03	6.03	-34.86	766.0
47	0	-18440	-626	27	0	51	7945	14.07	14.07	6.03	6.03	-30.90	620.3
49	0	-19520	-182	41	0	80	7379	14.07	14.07	6.03	6.03	-28.07	460.3
50	0	-17840	-1118	11	0	16	9055	14.07	14.07	6.03	6.03	-36.00	883.3
51	0	-18470	-593	91	0	202	7868	14.07	14.07	6.03	6.03	-30.55	603.5

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	110	-24800	48	50	0	25	11083	14.07	14.07	6.03	6.03	-43.34	914.1
41	110	-21540	-1031	9	0	-16	11456	14.07	14.07	6.03	6.03	-45.76	1179.0
42	110	-21660	-931	200	0	227	11336	14.07	14.07	6.03	6.03	-45.21	1145.8
43	110	-24980	970	87	0	71	8740	14.07	14.07	6.03	6.03	-32.77	466.5
44	110	-16560	-2862	-62	0	-87	12439	14.07	14.07	6.03	6.03	-50.75	1720.9
45	110	-19740	-662	336	0	408	9156	14.07	14.07	6.03	6.03	-36.00	796.1
46	110	-18350	-707	24	0	13	8096	14.07	14.07	6.03	6.03	-31.60	655.2
47	110	-17560	-626	27	0	21	7256	14.07	14.07	6.03	6.03	-28.03	529.9
49	110	-18640	-267	41	0	35	7132	14.07	14.07	6.03	6.03	-27.19	455.0
50	110	-16960	-1033	11	0	3	7872	14.07	14.07	6.03	6.03	-30.95	685.0
51	110	-17590	-593	91	0	102	7216	14.07	14.07	6.03	6.03	-27.84	520.6

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	220	-23920	-206	50	0	-30	10998	14.07	14.07	6.03	6.03	-43.18	944.5
41	220	-20660	-1031	9	0	-26	10322	14.07	14.07	6.03	6.03	-40.96	987.9
42	220	-20780	-931	200	0	8	10312	14.07	14.07	6.03	6.03	-40.89	978.8
43	220	-24100	547	87	0	-25	9574	14.07	14.07	6.03	6.03	-36.74	653.8
44	220	-15680	-2440	-62	0	-19	9523	14.07	14.07	6.03	6.03	-38.46	1118.7
45	220	-18860	-662	336	0	38	8428	14.07	14.07	6.03	6.03	-32.96	695.1
46	220	-17470	-707	24	0	-13	7318	14.07	14.07	6.03	6.03	-28.33	546.4
47	220	-16680	-626	27	0	-9	6566	14.07	14.07	6.03	6.03	-25.16	441.3
49	220	-17760	-351	41	0	-11	6792	14.07	14.07	6.03	6.03	-25.89	433.0
50	220	-16080	-949	11	0	-10	6782	14.07	14.07	6.03	6.03	-26.29	512.1
51	220	-16710	-593	91	0	2	6563	14.07	14.07	6.03	6.03	-25.13	439.2

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	330	-23040	-459	50	0	-85	10633	14.07	14.07	6.03	6.03	-41.77	918.0
41	330	-19780	-1031	9	0	-35	9188	14.07	14.07	6.03	6.03	-36.13	800.4
42	330	-19900	-931	200	0	-212	9288	14.07	14.07	6.03	6.03	-36.54	814.4
43	330	-23220	125	87	0	-121	9943	14.07	14.07	6.03	6.03	-38.63	768.9
44	330	-14800	-2018	-62	0	48	7072	14.07	14.07	6.03	6.03	-27.91	639.8
45	330	-17980	-662	336	0	-332	7700	14.07	14.07	6.03	6.03	-29.92	595.5
46	330	-16590	-707	24	0	-39	6539	14.07	14.07	6.03	6.03	-25.06	440.5
47	330	-15800	-626	27	0	-39	5877	14.07	14.07	6.03	6.03	-22.29	355.4
49	330	-16880	-436	41	0	-56	6359	14.07	14.07	6.03	6.03	-24.17	394.0
50	330	-15200	-864	11	0	-22	5785	14.07	14.07	6.03	6.03	-22.03	365.5
51	330	-15830	-593	91	0	-98	5910	14.07	14.07	6.03	6.03	-22.43	360.0

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	440	-22160	-712	50	0	-141	9990	14.07	14.07	6.03	6.03	-39.12	834.4
41	440	-18900	-1031	9	0	-45	8054	14.07	14.07	6.03	6.03	-31.27	618.1
42	440	-19020	-931	200	0	-431	8264	14.07	14.07	6.03	6.03	-32.18	653.6
43	440	-22340	-298	87	0	-217	9848	14.07	14.07	6.03	6.03	-38.43	796.0
44	440	-13920	-1595	-62	0	116	5085	14.07	14.07	6.03	6.03	-19.22	296.7
45	440	-17100	-662	336	0	-701	6971	14.07	14.07	6.03	6.03	-26.87	497.7
46	440	-15710	-707	24	0	-65	5761	14.07	14.07	6.03	6.03	-21.79	338.8
47	440	-14920	-626	27	0	-70	5188	14.07	14.07	6.03	6.03	-19.43	273.3
49	440	-16000	-520	41	0	-102	5833	14.07	14.07	6.03	6.03	-22.04	339.0
50	440	-14320	-780	11	0	-35	4881	14.07	14.07	6.03	6.03	-18.21	246.2
51	440	-14950	-593	91	0	-198	5258	14.07	14.07	6.03	6.03	-19.73	283.8

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

ASTA NUM. 25 NI 121 NF 120 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 5B
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-27960	-410	-71	0	-201	17880	14.07	14.07	8.04	8.04	-64.56	1693.8
41	0	-24660	-1924	-77	0	-209	21150	14.07	14.07	8.04	8.04	-76.43	2422.1
42	0	-24690	-1926	115	0	245	21180	14.07	14.07	8.04	8.04	-76.54	2425.8
43	0	-27740	998	-47	0	-146	11600	14.07	14.07	8.04	8.04	-40.97	686.7
44	0	-19680	-4514	-91	0	-228	27320	14.07	14.07	10.05	10.05	-88.12	3048.9
45	0	-22280	-1529	262	0	597	17110	14.07	14.07	8.04	8.04	-61.87	1840.8

46	0	-20770	-1286	-48	0	-130	14590	14.07	14.07	8.04	8.04	-52.74	1481.5
47	0	-19800	-1127	-40	0	-110	12950	14.07	14.07	8.04	8.04	-46.77	1248.4
49	0	-20900	-622	-38	0	-107	11860	14.07	14.07	8.04	8.04	-42.68	1013.3
50	0	-19290	-1725	-47	0	-123	15000	14.07	14.07	8.04	8.04	-54.24	1626.0
51	0	-19810	-1128	24	0	42	12960	14.07	14.07	8.04	8.04	-46.81	1249.7

apost= 10.05 aant= 10.05 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	110	-27080	-663	-71	0	-123	17288	14.07	14.07	6.03	6.03	-70.04	2120.4
41	110	-23780	-1924	-77	0	-124	19032	14.07	14.07	6.03	6.03	-77.78	2739.9
42	110	-23810	-1926	115	0	118	19062	14.07	14.07	6.03	6.03	-77.90	2744.7
43	110	-26860	576	-47	0	-93	12464	14.07	14.07	6.03	6.03	-49.00	1084.3
44	110	-18800	-4092	-91	0	-128	22586	14.07	14.07	8.04	8.04	-81.13	2983.5
45	110	-21400	-1529	262	0	308	15428	14.07	14.07	6.03	6.03	-62.85	2075.8
46	110	-19890	-1286	-48	0	-77	13174	14.07	14.07	6.03	6.03	-53.48	1664.8
47	110	-18920	-1127	-40	0	-65	11710	14.07	14.07	6.03	6.03	-47.35	1398.8
49	110	-20020	-707	-38	0	-65	11129	14.07	14.07	6.03	6.03	-44.64	1200.5
50	110	-18410	-1640	-47	0	-72	13150	14.07	14.07	6.03	6.03	-53.56	1757.9
51	110	-18930	-1128	24	0	15	11720	14.07	14.07	6.03	6.03	-47.39	1400.2

apost= 10.05 aant= 10.05 ainf= 4.02 asup= 4.02 (e arm. base= 4 X 2.01)

40	220	-26200	-916	-71	0	-46	16418	14.07	14.07	6.03	6.03	-66.44	1982.2
41	220	-22900	-1924	-77	0	-39	16915	14.07	14.07	6.03	6.03	-68.97	2314.1
42	220	-22930	-1926	115	0	-9	16945	14.07	14.07	6.03	6.03	-69.10	2318.9
43	220	-25980	153	-47	0	-41	12864	14.07	14.07	6.03	6.03	-50.99	1217.8
44	220	-17920	-3670	-91	0	-28	18316	14.07	14.07	6.03	6.03	-75.03	2986.8
45	220	-20520	-1529	262	0	20	13745	14.07	14.07	6.03	6.03	-55.83	1752.2
46	220	-19010	-1286	-48	0	-24	11759	14.07	14.07	6.03	6.03	-47.55	1403.9
47	220	-18040	-1127	-40	0	-21	10470	14.07	14.07	6.03	6.03	-42.15	1179.0
49	220	-19140	-791	-38	0	-23	10304	14.07	14.07	6.03	6.03	-41.21	1074.7
50	220	-17530	-1556	-47	0	-20	11393	14.07	14.07	6.03	6.03	-46.20	1417.9
51	220	-18050	-1128	24	0	-11	10479	14.07	14.07	6.03	6.03	-42.18	1180.4

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	330	-25320	-1170	-71	0	32	15268	14.07	14.07	6.03	6.03	-61.63	1782.0
41	330	-22020	-1924	-77	0	46	14798	14.07	14.07	6.03	6.03	-60.11	1891.1
42	330	-22050	-1926	115	0	-136	14828	14.07	14.07	6.03	6.03	-60.23	1895.9
43	330	-25100	-269	-47	0	11	12799	14.07	14.07	6.03	6.03	-50.91	1255.5
44	330	-17040	-3247	-91	0	72	14511	14.07	14.07	6.03	6.03	-59.37	2164.7
45	330	-19640	-1529	262	0	-269	12062	14.07	14.07	6.03	6.03	-48.75	1431.2
46	330	-18130	-1286	-48	0	28	10343	14.07	14.07	6.03	6.03	-41.58	1145.5
47	330	-17160	-1127	-40	0	24	9230	14.07	14.07	6.03	6.03	-36.91	961.7
49	330	-18260	-876	-38	0	19	9387	14.07	14.07	6.03	6.03	-37.37	929.5
50	330	-16650	-1472	-47	0	31	9728	14.07	14.07	6.03	6.03	-39.18	1102.6
51	330	-17170	-1128	24	0	-37	9238	14.07	14.07	6.03	6.03	-36.95	962.9

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	440	-24440	-1423	-71	0	110	13840	14.07	14.07	6.03	6.03	-55.60	1521.4
41	440	-21140	-1924	-77	0	132	12680	14.07	14.07	6.03	6.03	-51.17	1472.8
42	440	-21170	-1926	115	0	-263	12710	14.07	14.07	6.03	6.03	-51.29	1477.5
43	440	-24220	-691	-47	0	63	12270	14.07	14.07	6.03	6.03	-48.77	1194.2
44	440	-16160	-2825	-91	0	172	11170	14.07	14.07	6.03	6.03	-45.43	1458.2
45	440	-18760	-1529	262	0	-558	10380	14.07	14.07	6.03	6.03	-41.62	1114.4
46	440	-17250	-1286	-48	0	81	8928	14.07	14.07	6.03	6.03	-35.57	891.0
47	440	-16280	-1127	-40	0	68	7990	14.07	14.07	6.03	6.03	-31.64	748.1
49	440	-17380	-960	-38	0	61	8377	14.07	14.07	6.03	6.03	-33.10	766.5
50	440	-15770	-1387	-47	0	83	8157	14.07	14.07	6.03	6.03	-32.49	813.5
51	440	-16290	-1128	24	0	-63	7998	14.07	14.07	6.03	6.03	-31.67	749.2

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

ASTA NUM. 26 NI 164 NF 163 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 4B
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-28260	-614	-80	0	-237	19480	14.07	14.07	8.04	8.04	-70.41	1952.0
41	0	-24850	-2198	-83	0	-233	23130	14.07	14.07	8.04	8.04	-83.50	2758.6
42	0	-24790	-2186	90	0	178	22980	14.07	14.07	8.04	8.04	-82.97	2735.5
43	0	-28060	898	-62	0	-192	12530	14.07	14.07	8.04	8.04	-44.49	815.0
44	0	-19700	-4917	-89	0	-231	30010	14.07	14.07	10.05	10.05	-96.48	3432.0
45	0	-22290	-1723	221	0	500	18360	14.07	14.07	8.04	8.04	-66.37	2057.3
46	0	-20900	-1470	-57	0	-156	15920	14.07	14.07	8.04	8.04	-57.57	1704.2
47	0	-19920	-1288	-50	0	-137	14120	14.07	14.07	8.04	8.04	-51.05	1442.7
49	0	-21050	-760	-50	0	-138	12900	14.07	14.07	8.04	8.04	-46.53	1180.4
50	0	-19380	-1923	-55	0	-146	16390	14.07	14.07	8.04	8.04	-59.24	1863.1
51	0	-19900	-1284	7	0	-0	14060	14.07	14.07	8.04	8.04	-50.83	1433.3

apost= 10.05 aant= 10.05 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	110	-27380	-867	-80	0	-148	18666	14.07	14.07	6.03	6.03	-75.87	2411.7
41	110	-23970	-2198	-83	0	-142	20712	14.07	14.07	6.03	6.03	-84.76	3114.6
42	110	-23910	-2186	90	0	80	20575	14.07	14.07	6.03	6.03	-84.19	3087.0
43	110	-27180	475	-62	0	-123	13287	14.07	14.07	6.03	6.03	-52.59	1237.8
44	110	-18820	-4494	-89	0	-134	24836	14.07	14.07	8.04	8.04	-89.01	3381.0
45	110	-21410	-1723	221	0	258	16465	14.07	14.07	6.03	6.03	-67.22	2312.6
46	110	-20020	-1470	-57	0	-94	14303	14.07	14.07	6.03	6.03	-58.25	1912.3
47	110	-19040	-1288	-50	0	-82	12702	14.07	14.07	6.03	6.03	-51.58	1614.2
49	110	-20170	-844	-50	0	-84	12017	14.07	14.07	6.03	6.03	-48.47	1387.2
50	110	-18500	-1838	-55	0	-86	14323	14.07	14.07	6.03	6.03	-58.48	2020.2
51	110	-19020	-1284	7	0	-8	12649	14.07	14.07	6.03	6.03	-51.36	1603.4

apost= 10.05 aant= 10.05 ainf= 4.02 asup= 4.02 (e arm. base= 4 X 2.01)

40	220	-26500	-1121	-80	0	-60	17573	14.07	14.07	6.03	6.03	-71.34	2222.5
41	220	-23090	-2198	-83	0	-51	18295	14.07	14.07	6.03	6.03	-74.75	2617.7
42	220	-23030	-2186	90	0	-19	18170	14.07	14.07	6.03	6.03	-74.23	2593.1
43	220	-26300	53	-62	0	-54	13579	14.07	14.07	6.03	6.03	-54.08	1351.5
44	220	-17940	-4072	-89	0	-36	20126	14.07	14.07	6.03	6.03	-82.42	3408.4
45	220	-20530	-1723	221	0	15	14570	14.07	14.07	6.03	6.03	-59.33	1938.9
46	220	-19140	-1470	-57	0	-31	12686	14.07	14.07	6.03	6.03	-51.50	1603.9

47	220	-18160	-1288	-50	0	-26	11285	14.07	14.07	6.03	6.03	-45.65	1352.7
49	220	-19290	-929	-50	0	-29	11042	14.07	14.07	6.03	6.03	-44.40	1226.8
50	220	-17620	-1754	-55	0	-26	12348	14.07	14.07	6.03	6.03	-50.25	1628.4
51	220	-18140	-1284	7	0	-16	11238	14.07	14.07	6.03	6.03	-45.44	1343.4

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	330	-25620	-1374	-80	0	28	16201	14.07	14.07	6.03	6.03	-65.60	1971.2
41	330	-22210	-2198	-83	0	40	15878	14.07	14.07	6.03	6.03	-64.67	2123.8
42	330	-22150	-2186	90	0	-117	15765	14.07	14.07	6.03	6.03	-64.20	2102.2
43	330	-25420	-369	-62	0	14	13407	14.07	14.07	6.03	6.03	-53.51	1367.0
44	330	-17060	-3650	-89	0	61	15881	14.07	14.07	6.03	6.03	-65.03	2481.0
45	330	-19650	-1723	221	0	-228	12675	14.07	14.07	6.03	6.03	-51.38	1567.9
46	330	-18260	-1470	-57	0	31	11069	14.07	14.07	6.03	6.03	-44.70	1298.0
47	330	-17280	-1288	-50	0	29	9867	14.07	14.07	6.03	6.03	-39.67	1093.7
49	330	-18410	-1013	-50	0	25	9973	14.07	14.07	6.03	6.03	-39.91	1047.2
50	330	-16740	-1670	-55	0	34	10467	14.07	14.07	6.03	6.03	-42.35	1261.3
51	330	-17260	-1284	7	0	-23	9826	14.07	14.07	6.03	6.03	-39.49	1085.9

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	440	-24740	-1628	-80	0	116	14550	14.07	14.07	6.03	6.03	-58.63	1659.3
41	440	-21330	-2198	-83	0	131	13460	14.07	14.07	6.03	6.03	-54.49	1634.8
42	440	-21270	-2186	90	0	-216	13360	14.07	14.07	6.03	6.03	-54.07	1616.3
43	440	-24540	-792	-62	0	83	12770	14.07	14.07	6.03	6.03	-50.90	1282.4
44	440	-16180	-3227	-89	0	158	12100	14.07	14.07	6.03	6.03	-49.36	1669.0
45	440	-18770	-1723	221	0	-471	10780	14.07	14.07	6.03	6.03	-43.36	1201.6
46	440	-17380	-1470	-57	0	94	9452	14.07	14.07	6.03	6.03	-37.84	996.5
47	440	-16400	-1288	-50	0	85	8450	14.07	14.07	6.03	6.03	-33.65	838.9
49	440	-17530	-1098	-50	0	80	8812	14.07	14.07	6.03	6.03	-34.99	849.7
50	440	-15860	-1585	-55	0	95	8678	14.07	14.07	6.03	6.03	-34.76	920.9
51	440	-16380	-1284	7	0	-31	8415	14.07	14.07	6.03	6.03	-33.50	832.6

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

ASTA NUM. 27 NI 207 NF 206 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 3B
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-27760	-377	-98	0	-267	17370	14.07	14.07	8.04	8.04	-62.69	1617.0
41	0	-24440	-1947	-93	0	-248	21090	14.07	14.07	8.04	8.04	-76.21	2422.9
42	0	-24440	-1949	64	0	135	21100	14.07	14.07	8.04	8.04	-76.25	2424.7
43	0	-27590	1075	-84	0	-232	10780	14.07	14.07	8.04	8.04	-37.84	572.9
44	0	-19430	-4631	-88	0	-223	28010	14.07	14.07	10.05	10.05	-90.22	3158.1
45	0	-22050	-1545	186	0	438	17000	14.07	14.07	8.04	8.04	-61.47	1833.3
46	0	-20610	-1298	-67	0	-173	14520	14.07	14.07	8.04	8.04	-52.49	1477.3
47	0	-19650	-1135	-60	0	-154	12870	14.07	14.07	8.04	8.04	-46.49	1242.1
49	0	-20760	-612	-62	0	-160	11630	14.07	14.07	8.04	8.04	-41.83	981.6
50	0	-19130	-1753	-63	0	-158	15080	14.07	14.07	8.04	8.04	-54.53	1648.0
51	0	-19650	-1136	-8	0	-26	12880	14.07	14.07	8.04	8.04	-46.52	1243.8

apost= 10.05 aant= 10.05 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	110	-26880	-631	-98	0	-159	16816	14.07	14.07	6.03	6.03	-68.04	2027.3
41	110	-23560	-1947	-93	0	-146	18950	14.07	14.07	6.03	6.03	-77.45	2736.1
42	110	-23560	-1949	64	0	64	18958	14.07	14.07	6.03	6.03	-77.48	2737.8
43	110	-26710	653	-84	0	-139	11732	14.07	14.07	6.03	6.03	-45.76	943.2
44	110	-18550	-4208	-88	0	-126	23148	14.07	14.07	8.04	8.04	-83.08	3096.6
45	110	-21170	-1545	186	0	234	15300	14.07	14.07	6.03	6.03	-62.34	2062.2
46	110	-19730	-1298	-67	0	-99	13092	14.07	14.07	6.03	6.03	-53.15	1656.7
47	110	-18770	-1135	-60	0	-87	11622	14.07	14.07	6.03	6.03	-47.00	1388.7
49	110	-19880	-697	-62	0	-92	10911	14.07	14.07	6.03	6.03	-43.72	1161.5
50	110	-18250	-1668	-63	0	-89	13197	14.07	14.07	6.03	6.03	-53.77	1779.5
51	110	-18770	-1136	-8	0	-17	11629	14.07	14.07	6.03	6.03	-47.03	1390.4

apost= 10.05 aant= 10.05 ainf= 4.02 asup= 4.02 (e arm. base= 4 X 2.01)

40	220	-26000	-884	-98	0	-52	15983	14.07	14.07	6.03	6.03	-64.60	1897.7
41	220	-22680	-1947	-93	0	-43	16810	14.07	14.07	6.03	6.03	-68.55	2305.0
42	220	-22680	-1949	64	0	-6	16815	14.07	14.07	6.03	6.03	-68.57	2306.1
43	220	-25830	230	-84	0	-47	12219	14.07	14.07	6.03	6.03	-48.16	1091.0
44	220	-17670	-3786	-88	0	-29	18751	14.07	14.07	6.03	6.03	-76.81	3106.4
45	220	-20290	-1545	186	0	29	13600	14.07	14.07	6.03	6.03	-55.24	1734.6
46	220	-18850	-1298	-67	0	-25	11664	14.07	14.07	6.03	6.03	-47.16	1392.9
47	220	-17890	-1135	-60	0	-21	10374	14.07	14.07	6.03	6.03	-41.76	1167.1
49	220	-19000	-781	-62	0	-24	10099	14.07	14.07	6.03	6.03	-40.34	1038.6
50	220	-17370	-1584	-63	0	-20	11408	14.07	14.07	6.03	6.03	-46.29	1431.8
51	220	-17890	-1136	-8	0	-9	10378	14.07	14.07	6.03	6.03	-41.78	1168.2

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	330	-25120	-1138	-98	0	56	14871	14.07	14.07	6.03	6.03	-59.95	1706.3
41	330	-21800	-1947	-93	0	60	14670	14.07	14.07	6.03	6.03	-59.60	1876.8
42	330	-21800	-1949	64	0	-77	14672	14.07	14.07	6.03	6.03	-59.61	1877.3
43	330	-24950	-192	-84	0	45	12242	14.07	14.07	6.03	6.03	-48.47	1145.8
44	330	-16790	-3364	-88	0	68	14818	14.07	14.07	6.03	6.03	-60.65	2253.4
45	330	-19410	-1545	186	0	-176	11900	14.07	14.07	6.03	6.03	-48.09	1409.7
46	330	-17970	-1298	-67	0	48	10235	14.07	14.07	6.03	6.03	-41.14	1131.6
47	330	-17010	-1135	-60	0	46	9125	14.07	14.07	6.03	6.03	-36.48	948.0
49	330	-18120	-866	-62	0	44	9194	14.07	14.07	6.03	6.03	-36.55	896.5
50	330	-16490	-1500	-63	0	49	9711	14.07	14.07	6.03	6.03	-39.13	1108.8
51	330	-17010	-1136	-8	0	-0	9128	14.07	14.07	6.03	6.03	-36.49	948.6

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	440	-24240	-1391	-98	0	163	13480	14.07	14.07	6.03	6.03	-54.07	1454.8
41	440	-20920	-1947	-93	0	163	12530	14.07	14.07	6.03	6.03	-50.56	1453.4
42	440	-20920	-1949	64	0	-148	12530	14.07	14.07	6.03	6.03	-50.56	1453.4
43	440	-24070	-615	-84	0	138	11800	14.07	14.07	6.03	6.03	-46.72	1103.2
44	440	-15910	-2941	-88	0	165	11350	14.07	14.07	6.03	6.03	-46.22	1515.9
45	440	-18530	-1545	186	0	-380	10200	14.07	14.07	6.03	6.03	-40.88	1089.2
46	440	-17090	-1298	-67	0	122	8807	14.07	14.07	6.03	6.03	-35.07	874.6
47	440	-16130	-1135	-60	0	112	7877	14.07	14.07	6.03	6.03	-31.17	732.9

49	440	-17240	-950	-62	0	112	8196	14.07	14.07	6.03	6.03	-32.33	736.5
50	440	-15610	-1415	-63	0	118	8107	14.07	14.07	6.03	6.03	-32.31	812.3
51	440	-16130	-1136	-8	0	8	7877	14.07	14.07	6.03	6.03	-31.17	732.9

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

ASTA NUM. 28 NI 250 NF 249 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 2B
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-26260	543	-33	0	-234	9709	14.07	14.07	6.03	6.03	-36.78	580.2
41	0	-23010	-1016	-24	0	-168	13180	14.07	14.07	6.03	6.03	-53.00	1465.3
42	0	-23120	-1023	131	0	202	13380	14.07	14.07	6.03	6.03	-53.85	1502.6
43	0	-26350	1791	-41	0	-251	4889	14.07	14.07	6.03	6.03	-18.26	-253.9
44	0	-18050	-3649	-8	0	-63	19400	14.07	14.07	6.03	6.03	-79.46	3230.7
45	0	-21120	-819	233	0	475	11010	14.07	14.07	6.03	6.03	-43.89	1107.9
46	0	-19680	-681	-26	0	-125	9177	14.07	14.07	6.03	6.03	-36.10	803.6
47	0	-18850	-597	-26	0	-115	8175	14.07	14.07	6.03	6.03	-31.83	644.7
49	0	-19940	-78	-29	0	-137	7017	14.07	14.07	6.03	6.03	-26.34	379.2
50	0	-18280	-1166	-23	0	-99	9919	14.07	14.07	6.03	6.03	-39.70	1043.2
51	0	-18890	-600	25	0	8	8241	14.07	14.07	6.03	6.03	-32.11	655.8

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	110	-25380	289	-33	0	-197	10166	14.07	14.07	6.03	6.03	-39.07	704.4
41	110	-22130	-1016	-24	0	-142	12063	14.07	14.07	6.03	6.03	-48.30	1274.9
42	110	-22240	-1023	131	0	58	12254	14.07	14.07	6.03	6.03	-49.11	1309.9
43	110	-25470	1369	-41	0	-206	6627	14.07	14.07	6.03	6.03	-23.82	-322.6
44	110	-17170	-3226	-8	0	-54	15619	14.07	14.07	6.03	6.03	-63.95	2412.4
45	110	-20240	-819	233	0	218	10108	14.07	14.07	6.03	6.03	-40.11	967.0
46	110	-18800	-681	-26	0	-97	8428	14.07	14.07	6.03	6.03	-32.97	698.2
47	110	-17970	-597	-26	0	-86	7518	14.07	14.07	6.03	6.03	-29.10	560.3
49	110	-19060	-162	-29	0	-104	6885	14.07	14.07	6.03	6.03	-25.97	392.8
50	110	-17400	-1081	-23	0	-74	8683	14.07	14.07	6.03	6.03	-34.45	829.9
51	110	-18010	-600	25	0	-20	7581	14.07	14.07	6.03	6.03	-29.38	570.6

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	220	-24500	36	-33	0	-161	10345	14.07	14.07	6.03	6.03	-40.11	782.5
41	220	-21250	-1016	-24	0	-116	10946	14.07	14.07	6.03	6.03	-43.58	1086.3
42	220	-21360	-1023	131	0	-87	11128	14.07	14.07	6.03	6.03	-44.36	1119.0
43	220	-24590	946	-41	0	-161	7900	14.07	14.07	6.03	6.03	-29.16	-385.1
44	220	-16290	-2804	-8	0	-45	12303	14.07	14.07	6.03	6.03	-50.20	1708.0
45	220	-19360	-819	233	0	-38	9206	14.07	14.07	6.03	6.03	-36.31	827.7
46	220	-17920	-681	-26	0	-69	7678	14.07	14.07	6.03	6.03	-29.84	594.4
47	220	-17090	-597	-26	0	-57	6861	14.07	14.07	6.03	6.03	-26.38	477.2
49	220	-18180	-247	-29	0	-72	6660	14.07	14.07	6.03	6.03	-25.19	390.9
50	220	-16520	-997	-23	0	-49	7541	14.07	14.07	6.03	6.03	-29.58	641.1
51	220	-17130	-600	25	0	-48	6922	14.07	14.07	6.03	6.03	-26.64	486.8

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	330	-23620	-218	-33	0	-124	10245	14.07	14.07	6.03	6.03	-39.89	808.1
41	330	-20370	-1016	-24	0	-90	9828	14.07	14.07	6.03	6.03	-38.84	900.4
42	330	-20480	-1023	131	0	-231	10002	14.07	14.07	6.03	6.03	-39.58	930.7
43	330	-23710	524	-41	0	-116	8709	14.07	14.07	6.03	6.03	-32.95	513.8
44	330	-15410	-2382	-8	0	-37	9451	14.07	14.07	6.03	6.03	-38.20	1119.9
45	330	-18480	-819	233	0	-294	8305	14.07	14.07	6.03	6.03	-32.50	690.5
46	330	-17040	-681	-26	0	-41	6929	14.07	14.07	6.03	6.03	-26.70	492.7
47	330	-16210	-597	-26	0	-28	6204	14.07	14.07	6.03	6.03	-23.65	396.1
49	330	-17300	-331	-29	0	-40	6343	14.07	14.07	6.03	6.03	-23.99	372.8
50	330	-15640	-912	-23	0	-24	6491	14.07	14.07	6.03	6.03	-25.09	477.4
51	330	-16250	-600	25	0	-76	6262	14.07	14.07	6.03	6.03	-23.90	404.8

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	440	-22740	-471	-33	0	-87	9866	14.07	14.07	6.03	6.03	-38.41	778.6
41	440	-19490	-1016	-24	0	-64	8711	14.07	14.07	6.03	6.03	-34.07	718.6
42	440	-19600	-1023	131	0	-375	8876	14.07	14.07	6.03	6.03	-34.78	746.2
43	440	-22830	102	-41	0	-71	9053	14.07	14.07	6.03	6.03	-34.73	616.3
44	440	-14530	-1959	-8	0	-28	7064	14.07	14.07	6.03	6.03	-27.94	653.5
45	440	-17600	-819	233	0	-551	7403	14.07	14.07	6.03	6.03	-28.68	556.5
46	440	-16160	-681	-26	0	-13	6180	14.07	14.07	6.03	6.03	-23.55	394.0
47	440	-15330	-597	-26	0	0	5547	14.07	14.07	6.03	6.03	-20.93	317.5
49	440	-16420	-416	-29	0	-8	5932	14.07	14.07	6.03	6.03	-22.37	338.5
50	440	-14760	-828	-23	0	1	5534	14.07	14.07	6.03	6.03	-21.02	339.8
51	440	-15370	-600	25	0	-104	5602	14.07	14.07	6.03	6.03	-21.16	325.4

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

ASTA NUM. 29 NI 293 NF 292 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 1B
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-14820	554	-433	0	-658	-1029	4.02	4.02	10.05	10.05	-16.70	-201.3
41	0	-15040	-40	-342	0	-430	-25	4.02	4.02	10.05	10.05	-9.93	-143.7
42	0	-14800	-38	-375	0	-150	-26	4.02	4.02	10.05	10.05	-8.44	-124.7
43	0	-13780	932	-449	0	-728	-1665	4.02	4.02	10.05	10.05	-25.48	-269.1
44	0	-15550	-1025	-199	0	-65	1641	4.02	4.02	10.05	10.05	-25.13	-275.9
45	0	-13760	-55	-352	0	118	6	4.02	4.02	10.05	10.05	-7.74	-114.7
46	0	-13630	-68	-270	0	-300	28	4.02	4.02	10.05	10.05	-8.56	-124.7
47	0	-13280	-75	-253	0	-267	42	4.02	4.02	10.05	10.05	-8.22	-120.0
49	0	-13200	123	-283	0	-343	-293	4.02	4.02	10.05	10.05	-8.94	-124.0
50	0	-13550	-268	-233	0	-210	368	4.02	4.02	10.05	10.05	-9.79	-130.2
51	0	-13200	-74	-264	0	-174	41	4.02	4.02	10.05	10.05	-7.72	-113.7

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	97	-14380	441	-433	0	-236	-544	4.02	4.02	10.05	10.05	-11.78	-152.0
41	97	-14602	-40	-342	0	-96	-64	4.02	4.02	10.05	10.05	-8.07	-119.9
42	97	-14362	-38	-288	0	172	-64	4.02	4.02	10.05	10.05	-8.32	-122.7
43	97	-13342	745	-449	0	-291	-848	4.02	4.02	10.05	10.05	-14.17	-173.1
44	97	-15112	-838	-199	0	128	733	4.02	4.02	10.05	10.05	-13.85	-174.5
45	97	-13322	-55	-207	0	389	-47	4.02	4.02	10.05	10.05	-8.83	-127.8
46	97	-13190	-68	-270	0	-36	-38	4.02	4.02	10.05	10.05	-7.04	-105.2
47	97	-12840	-75	-253	0	-21	-31	4.02	4.02	10.05	10.05	-6.79	-101.6
49	97	-12762	86	-283	0	-67	-191	4.02	4.02	10.05	10.05	-7.81	-108.5
50	97	-13112	-231	-233	0	16	125	4.02	4.02	10.05	10.05	-7.38	-105.0
51	97	-12760	-74	-234	0	69	-31	4.02	4.02	10.05	10.05	-6.98	-103.8

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	195	-13940	329	-433	0	187	-169	4.02	4.02	10.05	10.05	-8.17	-120.3
41	195	-14165	-40	-342	0	237	-103	4.02	4.02	10.05	10.05	-8.53	-125.1
42	195	-13925	-38	-213	0	416	-101	4.02	4.02	10.05	10.05	-9.28	-134.1
43	195	-12905	557	-449	0	147	-213	4.02	4.02	10.05	10.05	-8.08	-111.5
44	195	-14675	-650	-199	0	322	8	4.02	4.02	10.05	10.05	-9.21	-134.2
45	195	-12885	-55	-83	0	529	-101	4.02	4.02	10.05	10.05	-9.29	-132.8
46	195	-12750	-68	-270	0	228	-104	4.02	4.02	10.05	10.05	-7.75	-113.5
47	195	-12400	-75	-253	0	225	-104	4.02	4.02	10.05	10.05	-7.55	-110.6
49	195	-12325	48	-283	0	208	-126	4.02	4.02	10.05	10.05	-7.43	-109.0
50	195	-12675	-193	-233	0	244	-82	4.02	4.02	10.05	10.05	-7.79	-113.8
51	195	-12320	-74	-210	0	285	-103	4.02	4.02	10.05	10.05	-7.80	-113.6

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	292	-13500	217	-433	0	609	97	4.02	4.02	10.05	10.05	-10.00	-142.6
41	292	-13728	-40	-342	0	571	-142	4.02	4.02	10.05	10.05	-9.93	-142.0
42	292	-13488	-38	-151	0	593	-139	4.02	4.02	10.05	10.05	-9.91	-141.4
43	292	-12468	370	-449	0	585	239	4.02	4.02	10.05	10.05	-9.34	-133.0
44	292	-14238	-463	-199	0	516	-534	4.02	4.02	10.05	10.05	-11.63	-150.2
45	292	-12448	-55	21	0	557	-154	4.02	4.02	10.05	10.05	-9.20	-131.2
46	292	-12310	-68	-270	0	492	-170	4.02	4.02	10.05	10.05	-8.81	-126.1
47	292	-11960	-75	-253	0	472	-177	4.02	4.02	10.05	10.05	-8.53	-122.1
49	292	-11888	11	-283	0	484	-97	4.02	4.02	10.05	10.05	-8.55	-122.4
50	292	-12238	-156	-233	0	470	-252	4.02	4.02	10.05	10.05	-8.67	-124.2
51	292	-11880	-74	-189	0	479	-176	4.02	4.02	10.05	10.05	-8.52	-122.0

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	390	-13060	104	-433	0	1032	254	4.02	4.02	10.05	10.05	-11.83	-164.9
41	390	-13290	-40	-342	0	905	-180	4.02	4.02	10.05	10.05	-11.33	-158.9
42	390	-13050	-38	-102	0	715	-176	4.02	4.02	10.05	10.05	-10.28	-145.5
43	390	-12030	183	-449	0	1023	508	4.02	4.02	10.05	10.05	-11.25	-156.3
44	390	-13800	-276	-199	0	710	-894	4.02	4.02	10.05	10.05	-14.84	-180.8
45	390	-12010	-55	104	0	495	-208	4.02	4.02	10.05	10.05	-8.66	-123.9
46	390	-11870	-68	-270	0	755	-236	4.02	4.02	10.05	10.05	-9.86	-138.7
47	390	-11520	-75	-253	0	718	-250	4.02	4.02	10.05	10.05	-9.50	-133.7
49	390	-11450	-27	-283	0	760	-105	4.02	4.02	10.05	10.05	-9.67	-135.7
50	390	-11800	-118	-233	0	698	-386	4.02	4.02	10.05	10.05	-9.54	-134.7
51	390	-11440	-74	-172	0	655	-248	4.02	4.02	10.05	10.05	-9.15	-129.2

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

ASTA NUM. 30 NI 77 NF 76 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 6C
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-18160	-809	174	0	97	9467	14.07	14.07	6.03	6.03	-37.74	952.6
41	0	-14850	-1133	181	0	82	7468	14.07	14.07	6.03	6.03	-29.66	720.5
42	0	-14950	-1145	235	0	100	7660	14.07	14.07	6.03	6.03	-30.48	755.6
43	0	-18370	-362	136	0	92	9334	14.07	14.07	6.03	6.03	-37.11	911.7
44	0	-9788	-1711	199	0	63	4398	14.07	14.07	6.03	6.03	-17.21	365.6
45	0	-13010	-922	238	0	98	6321	14.07	14.07	6.03	6.03	-25.00	584.3
46	0	-11640	-764	128	0	60	5122	14.07	14.07	6.03	6.03	-19.98	412.9
47	0	-10840	-672	114	0	55	4536	14.07	14.07	6.03	6.03	-17.56	338.2
49	0	-11940	-564	112	0	60	5202	14.07	14.07	6.03	6.03	-20.27	413.1
50	0	-10230	-834	125	0	54	4215	14.07	14.07	6.03	6.03	-16.28	306.4
51	0	-10870	-676	132	0	61	4600	14.07	14.07	6.03	6.03	-17.84	349.2

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	83	-17500	-1060	174	0	-47	8696	14.07	14.07	6.03	6.03	-34.49	826.8
41	83	-14190	-1133	181	0	-67	6533	14.07	14.07	6.03	6.03	-25.66	562.2
42	83	-14290	-1145	235	0	-94	6716	14.07	14.07	6.03	6.03	-26.45	594.3
43	83	-17710	-781	136	0	-20	8863	14.07	14.07	6.03	6.03	-35.17	849.9
44	83	-9128	-1292	199	0	-102	3159	14.07	14.07	6.03	6.03	-11.82	164.8
45	83	-12350	-922	238	0	-99	5560	14.07	14.07	6.03	6.03	-21.77	463.5
46	83	-10980	-764	128	0	-45	4492	14.07	14.07	6.03	6.03	-17.32	322.5
47	83	-10179	-672	114	0	-40	3982	14.07	14.07	6.03	6.03	-15.24	264.5
49	83	-11280	-648	112	0	-33	4702	14.07	14.07	6.03	6.03	-18.19	348.4
50	83	-9569	-750	125	0	-49	3562	14.07	14.07	6.03	6.03	-13.51	215.6
51	83	-10210	-676	132	0	-49	4042	14.07	14.07	6.03	6.03	-15.50	274.3

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	165	-16840	-1311	174	0	-190	7718	14.07	14.07	6.03	6.03	-30.29	659.9
41	165	-13530	-1133	181	0	-216	5598	14.07	14.07	6.03	6.03	-21.63	409.8
42	165	-13630	-1145	235	0	-289	5771	14.07	14.07	6.03	6.03	-22.38	438.4
43	165	-17050	-1200	136	0	-132	8046	14.07	14.07	6.03	6.03	-31.70	715.9
44	165	-8468	-873	199	0	-266	2266	14.07	14.07	6.03	6.03	-8.16	-110.2
45	165	-11690	-922	238	0	-296	4799	14.07	14.07	6.03	6.03	-18.52	346.7
46	165	-10320	-764	128	0	-150	3861	14.07	14.07	6.03	6.03	-14.66	236.1
47	165	-9518	-672	114	0	-134	3427	14.07	14.07	6.03	6.03	-12.92	194.2
49	165	-10620	-732	112	0	-125	4133	14.07	14.07	6.03	6.03	-15.80	272.1
50	165	-8908	-666	125	0	-152	2977	14.07	14.07	6.03	6.03	-11.07	-145.4
51	165	-9550	-676	132	0	-158	3484	14.07	14.07	6.03	6.03	-13.16	202.7

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	248	-16180	-1563	174	0	-334	6532	14.07	14.07	6.03	6.03	-25.14	458.8
41	248	-12870	-1133	181	0	-366	4664	14.07	14.07	6.03	6.03	-17.60	267.8
42	248	-12970	-1145	235	0	-483	4826	14.07	14.07	6.03	6.03	-18.30	292.1
43	248	-16390	-1619	136	0	-244	6883	14.07	14.07	6.03	6.03	-26.66	516.0
44	248	-7808	-454	199	0	-431	1719	14.07	14.07	6.03	6.03	-6.21	-85.3
45	248	-11030	-922	238	0	-492	4038	14.07	14.07	6.03	6.03	-15.27	236.6
46	248	-9660	-764	128	0	-256	3230	14.07	14.07	6.03	6.03	-12.01	-157.7
47	248	-8858	-672	114	0	-228	2872	14.07	14.07	6.03	6.03	-10.62	-140.1
49	248	-9961	-815	112	0	-218	3495	14.07	14.07	6.03	6.03	-13.11	187.8
50	248	-8247	-582	125	0	-255	2462	14.07	14.07	6.03	6.03	-8.98	-119.7
51	248	-8891	-676	132	0	-267	2926	14.07	14.07	6.03	6.03	-10.85	-142.8

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	330	-15520	-1814	174	0	-478	5139	14.07	14.07	6.03	6.03	-19.07	-250.8
41	330	-12210	-1133	181	0	-515	3729	14.07	14.07	6.03	6.03	-13.65	-181.4
42	330	-12310	-1145	235	0	-677	3882	14.07	14.07	6.03	6.03	-14.28	-189.1
43	330	-15730	-2038	136	0	-356	5374	14.07	14.07	6.03	6.03	-20.06	272.5
44	330	-7148	-35	199	0	-595	1518	14.07	14.07	6.03	6.03	-5.51	-75.9
45	330	-10370	-922	238	0	-689	3277	14.07	14.07	6.03	6.03	-12.06	-159.6
46	330	-9000	-764	128	0	-361	2600	14.07	14.07	6.03	6.03	-9.44	-126.3
47	330	-8197	-672	114	0	-323	2318	14.07	14.07	6.03	6.03	-8.39	-112.6
49	330	-9301	-899	112	0	-310	2788	14.07	14.07	6.03	6.03	-10.17	-135.6
50	330	-7586	-499	125	0	-358	2016	14.07	14.07	6.03	6.03	-7.26	-98.0
51	330	-8231	-676	132	0	-377	2368	14.07	14.07	6.03	6.03	-8.59	-115.1

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

ASTA NUM. 31 NI 120 NF 119 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 5C
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-20400	-1525	-12	0	-159	13360	14.07	14.07	6.03	6.03	-54.20	1673.1
41	0	-17090	-2061	33	0	-101	12280	14.07	14.07	6.03	6.03	-50.02	1648.5
42	0	-17130	-2067	75	0	-56	12330	14.07	14.07	6.03	6.03	-50.23	1657.2
43	0	-20170	-740	-39	0	-166	11650	14.07	14.07	6.03	6.03	-46.88	1305.8
44	0	-12120	-3028	108	0	-6	10920	14.07	14.07	6.03	6.03	-44.71	1678.5
45	0	-14720	-1643	106	0	5	9924	14.07	14.07	6.03	6.03	-40.32	1271.4
46	0	-13190	-1378	37	0	-49	8388	14.07	14.07	6.03	6.03	-33.97	1025.4
47	0	-12220	-1207	38	0	-36	7414	14.07	14.07	6.03	6.03	-29.94	870.1
49	0	-13320	-1028	23	0	-56	7774	14.07	14.07	6.03	6.03	-31.31	880.1
50	0	-11710	-1486	52	0	-24	7629	14.07	14.07	6.03	6.03	-30.94	951.4
51	0	-12230	-1209	52	0	-22	7430	14.07	14.07	6.03	6.03	-30.01	873.0

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	83	-19740	-1776	-12	0	-149	11999	14.07	14.07	6.03	6.03	-48.46	1410.6
41	83	-16430	-2061	33	0	-127	10580	14.07	14.07	6.03	6.03	-42.88	1306.9
42	83	-16470	-2067	75	0	-119	10624	14.07	14.07	6.03	6.03	-43.07	1314.3
43	83	-19510	-1159	-39	0	-134	10866	14.07	14.07	6.03	6.03	-43.59	1174.5
44	83	-11459	-2609	108	0	-95	8595	14.07	14.07	6.03	6.03	-35.06	1187.9
45	83	-14060	-1643	106	0	-83	8568	14.07	14.07	6.03	6.03	-34.61	1009.6
46	83	-12530	-1378	37	0	-79	7251	14.07	14.07	6.03	6.03	-29.18	814.3
47	83	-11559	-1207	38	0	-67	6418	14.07	14.07	6.03	6.03	-25.74	691.5
49	83	-12660	-1112	23	0	-75	6891	14.07	14.07	6.03	6.03	-27.59	727.2
50	83	-11050	-1402	52	0	-67	6438	14.07	14.07	6.03	6.03	-25.92	727.6
51	83	-11570	-1209	52	0	-65	6432	14.07	14.07	6.03	6.03	-25.80	694.0

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	165	-19080	-2028	-12	0	-139	10430	14.07	14.07	6.03	6.03	-41.78	1105.8
41	165	-15770	-2061	33	0	-154	8880	14.07	14.07	6.03	6.03	-35.66	970.6
42	165	-15810	-2067	75	0	-181	8919	14.07	14.07	6.03	6.03	-35.82	976.7
43	165	-18850	-1578	-39	0	-101	9737	14.07	14.07	6.03	6.03	-38.78	969.5
44	165	-10798	-2190	108	0	-184	6616	14.07	14.07	6.03	6.03	-26.74	783.3
45	165	-13400	-1643	106	0	-171	7212	14.07	14.07	6.03	6.03	-28.85	752.0
46	165	-11870	-1378	37	0	-110	6114	14.07	14.07	6.03	6.03	-24.34	606.8
47	165	-10898	-1207	38	0	-98	5422	14.07	14.07	6.03	6.03	-21.50	516.3
49	165	-12000	-1196	23	0	-93	5939	14.07	14.07	6.03	6.03	-23.54	561.8
50	165	-10390	-1318	52	0	-110	5315	14.07	14.07	6.03	6.03	-21.15	523.3
51	165	-10910	-1209	52	0	-107	5434	14.07	14.07	6.03	6.03	-21.56	518.3

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	248	-18420	-2279	-12	0	-129	8654	14.07	14.07	6.03	6.03	-34.08	765.6
41	248	-15110	-2061	33	0	-181	7180	14.07	14.07	6.03	6.03	-28.32	644.8
42	248	-15150	-2067	75	0	-243	7214	14.07	14.07	6.03	6.03	-28.46	649.6
43	248	-18190	-1997	-39	0	-69	8261	14.07	14.07	6.03	6.03	-32.38	697.3
44	248	-10138	-1770	108	0	-273	4983	14.07	14.07	6.03	6.03	-19.73	467.3
45	248	-12740	-1643	106	0	-259	5857	14.07	14.07	6.03	6.03	-23.00	502.9
46	248	-11210	-1378	37	0	-140	4977	14.07	14.07	6.03	6.03	-19.44	406.6
47	248	-10238	-1207	38	0	-129	4426	14.07	14.07	6.03	6.03	-17.22	347.4
49	248	-11340	-1280	23	0	-112	4917	14.07	14.07	6.03	6.03	-19.14	387.8
50	248	-9729	-1235	52	0	-153	4262	14.07	14.07	6.03	6.03	-16.62	341.3
51	248	-10249	-1209	52	0	-150	4437	14.07	14.07	6.03	6.03	-17.27	348.9

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	330	-17760	-2530	-12	0	-119	6671	14.07	14.07	6.03	6.03	-25.34	411.1
41	330	-14450	-2061	33	0	-208	5480	14.07	14.07	6.03	6.03	-20.86	343.9
42	330	-14490	-2067	75	0	-305	5508	14.07	14.07	6.03	6.03	-20.97	347.2
43	330	-17530	-2416	-39	0	-37	6440	14.07	14.07	6.03	6.03	-24.37	380.0
44	330	-9477	-1351	108	0	-363	3695	14.07	14.07	6.03	6.03	-14.13	244.1
45	330	-12080	-1643	106	0	-347	4501	14.07	14.07	6.03	6.03	-17.07	273.1
46	330	-10550	-1378	37	0	-170	3840	14.07	14.07	6.03	6.03	-14.50	222.5
47	330	-9577	-1207	38	0	-160	3430	14.07	14.07	6.03	6.03	-12.92	192.3
49	330	-10680	-1364	23	0	-131	3827	14.07	14.07	6.03	6.03	-14.41	214.8
50	330	-9069	-1151	52	0	-196	3278	14.07	14.07	6.03	6.03	-12.36	187.2
51	330	-9589	-1209	52	0	-193	3439	14.07	14.07	6.03	6.03	-12.95	193.3

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

ASTA NUM. 32 NI 163 NF 162 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 4C
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-20650	-1665	-254	0	-379	13970	14.07	14.07	6.03	6.03	-56.77	1794.5
41	0	-17240	-2223	-216	0	-305	12900	14.07	14.07	6.03	6.03	-52.62	1780.1
42	0	-17180	-2200	-151	0	-220	12770	14.07	14.07	6.03	6.03	-52.08	1754.4
43	0	-20460	-832	-225	0	-352	12120	14.07	14.07	6.03	6.03	-48.86	1391.6
44	0	-12080	-3233	-160	0	-192	11580	14.07	14.07	6.03	6.03	-47.43	1834.7
45	0	-14670	-1725	-52	0	-87	10130	14.07	14.07	6.03	6.03	-41.20	1321.5
46	0	-13290	-1487	-128	0	-182	8807	14.07	14.07	6.03	6.03	-35.75	1113.3
47	0	-12300	-1303	-106	0	-151	7784	14.07	14.07	6.03	6.03	-31.52	947.7
49	0	-13440	-1117	-119	0	-176	8140	14.07	14.07	6.03	6.03	-32.87	953.8
50	0	-11770	-1597	-106	0	-144	8032	14.07	14.07	6.03	6.03	-32.65	1038.6
51	0	-12290	-1296	-84	0	-123	7742	14.07	14.07	6.03	6.03	-31.34	938.9

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	83	-19990	-1917	-254	0	-169	12492	14.07	14.07	6.03	6.03	-50.54	1504.6
41	83	-16580	-2223	-216	0	-126	11066	14.07	14.07	6.03	6.03	-44.94	1406.6
42	83	-16520	-2200	-151	0	-96	10956	14.07	14.07	6.03	6.03	-44.48	1385.8
43	83	-19800	-1252	-225	0	-166	11260	14.07	14.07	6.03	6.03	-45.25	1243.0
44	83	-11421	-2814	-160	0	-60	9086	14.07	14.07	6.03	6.03	-37.13	1303.4
45	83	-14010	-1725	-52	0	-44	8708	14.07	14.07	6.03	6.03	-35.22	1044.0
46	83	-12630	-1487	-128	0	-76	7580	14.07	14.07	6.03	6.03	-30.59	880.9
47	83	-11641	-1303	-106	0	-63	6709	14.07	14.07	6.03	6.03	-26.99	750.3
49	83	-12780	-1201	-119	0	-78	7183	14.07	14.07	6.03	6.03	-28.84	783.8
50	83	-11109	-1513	-106	0	-56	6749	14.07	14.07	6.03	6.03	-27.26	792.9
51	83	-11629	-1296	-84	0	-53	6673	14.07	14.07	6.03	6.03	-26.84	743.3

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	165	-19330	-2168	-254	0	41	10806	14.07	14.07	6.03	6.03	-43.37	1172.5
41	165	-15920	-2223	-216	0	52	9231	14.07	14.07	6.03	6.03	-37.16	1038.6
42	165	-15860	-2200	-151	0	28	9142	14.07	14.07	6.03	6.03	-36.78	1022.7
43	165	-19140	-1671	-225	0	19	10054	14.07	14.07	6.03	6.03	-40.11	1020.5
44	165	-10762	-2394	-160	0	72	6938	14.07	14.07	6.03	6.03	-28.13	857.9
45	165	-13350	-1725	-52	0	-1	7286	14.07	14.07	6.03	6.03	-29.18	771.1
46	165	-11970	-1487	-128	0	30	6353	14.07	14.07	6.03	6.03	-25.37	652.3
47	165	-10982	-1303	-106	0	24	5634	14.07	14.07	6.03	6.03	-22.42	556.4
49	165	-12120	-1285	-119	0	21	6158	14.07	14.07	6.03	6.03	-24.48	601.4
50	165	-10448	-1430	-106	0	31	5535	14.07	14.07	6.03	6.03	-22.10	567.1
51	165	-10968	-1296	-84	0	17	5604	14.07	14.07	6.03	6.03	-22.30	551.1

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	248	-18670	-2420	-254	0	250	8913	14.07	14.07	6.03	6.03	-35.17	805.3
41	248	-15260	-2223	-216	0	230	7396	14.07	14.07	6.03	6.03	-29.24	681.6
42	248	-15200	-2200	-151	0	153	7328	14.07	14.07	6.03	6.03	-28.95	670.7
43	248	-18480	-2090	-225	0	205	8502	14.07	14.07	6.03	6.03	-33.39	730.9
44	248	-10103	-1975	-160	0	204	5136	14.07	14.07	6.03	6.03	-20.42	502.0
45	248	-12690	-1725	-52	0	42	5864	14.07	14.07	6.03	6.03	-23.04	507.2
46	248	-11310	-1487	-128	0	136	5126	14.07	14.07	6.03	6.03	-20.09	431.4
47	248	-10323	-1303	-106	0	112	4558	14.07	14.07	6.03	6.03	-17.79	369.4
49	248	-11460	-1369	-119	0	119	5063	14.07	14.07	6.03	6.03	-19.77	410.6
50	248	-9788	-1346	-106	0	119	4390	14.07	14.07	6.03	6.03	-17.18	363.9
51	248	-10306	-1296	-84	0	86	4536	14.07	14.07	6.03	6.03	-17.70	365.7

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	330	-18010	-2671	-254	0	460	6812	14.07	14.07	6.03	6.03	-25.91	425.3
41	330	-14600	-2223	-216	0	408	5562	14.07	14.07	6.03	6.03	-21.18	352.0
42	330	-14540	-2200	-151	0	277	5514	14.07	14.07	6.03	6.03	-20.98	346.0
43	330	-17820	-2509	-225	0	391	6605	14.07	14.07	6.03	6.03	-25.03	396.6
44	330	-9444	-1556	-160	0	336	3680	14.07	14.07	6.03	6.03	-14.07	242.8
45	330	-12030	-1725	-52	0	85	4442	14.07	14.07	6.03	6.03	-16.82	264.8
46	330	-10650	-1487	-128	0	242	3899	14.07	14.07	6.03	6.03	-14.74	228.5
47	330	-9664	-1303	-106	0	200	3483	14.07	14.07	6.03	6.03	-13.13	197.8
49	330	-10800	-1453	-119	0	217	3899	14.07	14.07	6.03	6.03	-14.70	222.2
50	330	-9127	-1262	-106	0	206	3314	14.07	14.07	6.03	6.03	-12.51	191.0
51	330	-9645	-1296	-84	0	156	3467	14.07	14.07	6.03	6.03	-13.06	195.8

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

ASTA NUM. 33 NI 206 NF 205 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 3C
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-20220	-1465	-384	0	-540	13000	14.07	14.07	6.03	6.03	-52.69	1603.8
41	0	-16880	-2040	-336	0	-422	12070	14.07	14.07	6.03	6.03	-49.16	1614.8
42	0	-16880	-2039	-239	0	-293	12070	14.07	14.07	6.03	6.03	-49.16	1614.8
43	0	-20050	-656	-335	0	-512	11210	14.07	14.07	6.03	6.03	-44.99	1216.5
44	0	-11830	-3070	-270	0	-242	10970	14.07	14.07	6.03	6.03	-44.92	1710.6
45	0	-14480	-1614	-93	0	-100	9669	14.07	14.07	6.03	6.03	-39.27	1229.6
46	0	-13030	-1360	-207	0	-251	8232	14.07	14.07	6.03	6.03	-33.33	1000.8
47	0	-12070	-1190	-175	0	-209	7271	14.07	14.07	6.03	6.03	-29.35	847.8
49	0	-13180	-998	-191	0	-248	7578	14.07	14.07	6.03	6.03	-30.48	845.6
50	0	-11540	-1481	-178	0	-194	7531	14.07	14.07	6.03	6.03	-30.55	940.5
51	0	-12070	-1190	-142	0	-166	7270	14.07	14.07	6.03	6.03	-29.35	847.6

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	83	-19560	-1716	-384	0	-223	11687	14.07	14.07	6.03	6.03	-47.15	1352.6
41	83	-16220	-2040	-336	0	-145	10388	14.07	14.07	6.03	6.03	-42.09	1277.5
42	83	-16220	-2039	-239	0	-96	10388	14.07	14.07	6.03	6.03	-42.09	1277.4
43	83	-19390	-1075	-335	0	-236	10495	14.07	14.07	6.03	6.03	-42.00	1100.9

44	83	-11171	-2651	-270	0	-19	8610	14.07	14.07	6.03	6.03	-35.15	1211.1
45	83	-13820	-1614	-93	0	-23	8337	14.07	14.07	6.03	6.03	-33.66	973.4
46	83	-12370	-1360	-207	0	-81	7110	14.07	14.07	6.03	6.03	-28.60	793.1
47	83	-11409	-1190	-175	0	-64	6289	14.07	14.07	6.03	6.03	-25.21	672.6
49	83	-12520	-1082	-191	0	-91	6720	14.07	14.07	6.03	6.03	-26.87	698.5
50	83	-10879	-1397	-178	0	-47	6344	14.07	14.07	6.03	6.03	-25.54	717.5
51	83	-11409	-1190	-142	0	-48	6288	14.07	14.07	6.03	6.03	-25.20	672.4

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	165	-18900	-1968	-384	0	93	10166	14.07	14.07	6.03	6.03	-40.66	1059.3
41	165	-15560	-2040	-336	0	133	8706	14.07	14.07	6.03	6.03	-34.94	945.6
42	165	-15560	-2039	-239	0	101	8706	14.07	14.07	6.03	6.03	-34.94	945.5
43	165	-18730	-1495	-335	0	40	9435	14.07	14.07	6.03	6.03	-37.47	912.0
44	165	-10512	-2232	-270	0	203	6596	14.07	14.07	6.03	6.03	-26.70	797.3
45	165	-13160	-1614	-93	0	53	7005	14.07	14.07	6.03	6.03	-27.99	721.6
46	165	-11710	-1360	-207	0	90	5988	14.07	14.07	6.03	6.03	-23.82	589.2
47	165	-10748	-1190	-175	0	80	5307	14.07	14.07	6.03	6.03	-21.03	500.7
49	165	-11860	-1166	-191	0	67	5792	14.07	14.07	6.03	6.03	-22.92	539.0
50	165	-10218	-1314	-178	0	99	5225	14.07	14.07	6.03	6.03	-20.79	514.2
51	165	-10748	-1190	-142	0	69	5306	14.07	14.07	6.03	6.03	-21.03	500.5

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	248	-18240	-2219	-384	0	410	8438	14.07	14.07	6.03	6.03	-33.16	731.0
41	248	-14900	-2040	-336	0	411	7025	14.07	14.07	6.03	6.03	-27.68	624.3
42	248	-14900	-2039	-239	0	298	7024	14.07	14.07	6.03	6.03	-27.67	624.2
43	248	-18070	-1914	-335	0	316	8028	14.07	14.07	6.03	6.03	-31.37	656.5
44	248	-9852	-1813	-270	0	426	4928	14.07	14.07	6.03	6.03	-19.56	472.2
45	248	-12500	-1614	-93	0	130	5673	14.07	14.07	6.03	6.03	-22.23	478.4
46	248	-11050	-1360	-207	0	261	4865	14.07	14.07	6.03	6.03	-18.98	392.6
47	248	-10086	-1190	-175	0	224	4325	14.07	14.07	6.03	6.03	-16.81	335.2
49	248	-11200	-1250	-191	0	224	4796	14.07	14.07	6.03	6.03	-18.63	370.8
50	248	-9558	-1230	-178	0	246	4176	14.07	14.07	6.03	6.03	-16.28	333.1
51	248	-10088	-1190	-142	0	186	4325	14.07	14.07	6.03	6.03	-16.81	335.1

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	330	-17580	-2470	-384	0	727	6503	14.07	14.07	6.03	6.03	-24.64	389.0
41	330	-14240	-2040	-336	0	688	5343	14.07	14.07	6.03	6.03	-20.29	328.5
42	330	-14240	-2039	-239	0	495	5342	14.07	14.07	6.03	6.03	-20.29	328.4
43	330	-17410	-2333	-335	0	592	6276	14.07	14.07	6.03	6.03	-23.66	356.5
44	330	-9193	-1394	-270	0	649	3605	14.07	14.07	6.03	6.03	-13.80	240.6
45	330	-11840	-1614	-93	0	206	4341	14.07	14.07	6.03	6.03	-16.42	255.2
46	330	-10390	-1360	-207	0	432	3743	14.07	14.07	6.03	6.03	-14.11	212.4
47	330	-9425	-1190	-175	0	368	3343	14.07	14.07	6.03	6.03	-12.57	183.7
49	330	-10540	-1334	-191	0	381	3730	14.07	14.07	6.03	6.03	-14.01	204.0
50	330	-8897	-1146	-178	0	392	3196	14.07	14.07	6.03	6.03	-12.04	180.3
51	330	-9427	-1190	-142	0	304	3343	14.07	14.07	6.03	6.03	-12.57	183.6

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

ASTA NUM. 34 NI 249 NF 248 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 2C
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-18580	-634	-1065	0	-1079	9348	14.07	14.07	6.03	6.03	-37.12	902.3
41	0	-15310	-1178	-794	0	-758	8230	14.07	14.07	6.03	6.03	-32.91	856.9
42	0	-15420	-1211	-738	0	-643	8417	14.07	14.07	6.03	6.03	-33.71	890.9
43	0	-18690	-22	-1018	0	-1060	8457	14.07	14.07	6.03	6.03	-33.13	710.1
44	0	-10310	-2126	-379	0	-260	6649	14.07	14.07	6.03	6.03	-26.95	822.3
45	0	-13410	-984	-474	0	-334	6905	14.07	14.07	6.03	6.03	-27.49	685.0
46	0	-11980	-779	-431	0	-386	5610	14.07	14.07	6.03	6.03	-22.08	494.1
47	0	-11150	-680	-340	0	-293	4955	14.07	14.07	6.03	6.03	-19.36	405.3
49	0	-12240	-498	-430	0	-400	5328	14.07	14.07	6.03	6.03	-20.75	422.6
50	0	-10570	-919	-302	0	-240	4966	14.07	14.07	6.03	6.03	-19.56	439.3
51	0	-11190	-691	-321	0	-255	5017	14.07	14.07	6.03	6.03	-19.63	415.7

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	83	-17920	-886	-1065	0	-200	8721	14.07	14.07	6.03	6.03	-34.50	807.9
41	83	-14650	-1178	-794	0	-103	7258	14.07	14.07	6.03	6.03	-28.77	687.5
42	83	-14760	-1211	-738	0	-34	7418	14.07	14.07	6.03	6.03	-29.45	715.0
43	83	-18030	-441	-1018	0	-220	8266	14.07	14.07	6.03	6.03	-32.44	707.1
44	83	-9650	-1707	-379	0	53	5068	14.07	14.07	6.03	6.03	-20.22	514.3
45	83	-12750	-984	-474	0	57	6094	14.07	14.07	6.03	6.03	-24.05	551.4
46	83	-11320	-779	-431	0	-31	4967	14.07	14.07	6.03	6.03	-19.37	398.7
47	83	-10490	-680	-340	0	-13	4394	14.07	14.07	6.03	6.03	-17.01	328.2
49	83	-11580	-582	-430	0	-45	4882	14.07	14.07	6.03	6.03	-18.92	368.4
50	83	-9909	-835	-302	0	9	4242	14.07	14.07	6.03	6.03	-16.48	328.0
51	83	-10529	-691	-321	0	10	4447	14.07	14.07	6.03	6.03	-17.24	336.6

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	165	-17260	-1137	-1065	0	678	7887	14.07	14.07	6.03	6.03	-30.94	671.5
41	165	-13990	-1178	-794	0	553	6286	14.07	14.07	6.03	6.03	-24.60	522.4
42	165	-14100	-1211	-738	0	575	6418	14.07	14.07	6.03	6.03	-25.17	543.6
43	165	-17370	-860	-1018	0	620	7730	14.07	14.07	6.03	6.03	-30.21	633.5
44	165	-8990	-1288	-379	0	365	3833	14.07	14.07	6.03	6.03	-14.88	294.4
45	165	-12090	-984	-474	0	447	5282	14.07	14.07	6.03	6.03	-20.59	421.3
46	165	-10660	-779	-431	0	325	4324	14.07	14.07	6.03	6.03	-16.65	306.1
47	165	-9830	-680	-340	0	268	3834	14.07	14.07	6.03	6.03	-14.66	253.3
49	165	-10921	-666	-430	0	310	4367	14.07	14.07	6.03	6.03	-16.78	301.7
50	165	-9248	-751	-302	0	259	3588	14.07	14.07	6.03	6.03	-13.71	234.8
51	165	-9868	-691	-321	0	275	3878	14.07	14.07	6.03	6.03	-14.85	259.7

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	248	-16600	-1388	-1065	0	1557	6845	14.07	14.07	6.03	6.03	-26.43	498.2
41	248	-13330	-1178	-794	0	1208	5313	14.07	14.07	6.03	6.03	-20.40	365.0
42	248	-13440	-1211	-738	0	1184	5419	14.07	14.07	6.03	6.03	-20.85	379.8
43	248	-16710	-1279	-1018	0	1459	6847	14.07	14.07	6.03	6.03	-26.41	493.1
44	248	-8331	-869	-379	0	678	2944	14.07	14.07	6.03	6.03	-11.06	160.5

45	248	-11430	-984	-474	0	838	4470	14.07	14.07	6.03	6.03	-17.11	297.0
46	248	-10000	-779	-431	0	680	3681	14.07	14.07	6.03	6.03	-13.93	218.1
47	248	-9169	-680	-340	0	549	3273	14.07	14.07	6.03	6.03	-12.32	182.2
49	248	-10262	-750	-430	0	665	3783	14.07	14.07	6.03	6.03	-14.32	224.8
50	248	-8587	-668	-302	0	509	3002	14.07	14.07	6.03	6.03	-11.25	160.0
51	248	-9206	-691	-321	0	540	3308	14.07	14.07	6.03	6.03	-12.46	186.6

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	330	-15940	-1640	-1065	0	2436	5596	14.07	14.07	6.03	6.03	-20.99	300.9
41	330	-12670	-1178	-794	0	1864	4341	14.07	14.07	6.03	6.03	-16.21	221.5
42	330	-12780	-1211	-738	0	1793	4420	14.07	14.07	6.03	6.03	-16.54	230.2
43	330	-16050	-1698	-1018	0	2299	5619	14.07	14.07	6.03	6.03	-21.07	300.4
44	330	-7671	-449	-379	0	991	2400	14.07	14.07	6.03	6.03	-8.82	-116.9
45	330	-10770	-984	-474	0	1229	3659	14.07	14.07	6.03	6.03	-13.64	183.2
46	330	-9340	-779	-431	0	1036	3038	14.07	14.07	6.03	6.03	-11.24	-148.2
47	330	-8509	-680	-340	0	829	2712	14.07	14.07	6.03	6.03	-10.00	-132.1
49	330	-9602	-834	-430	0	1020	3130	14.07	14.07	6.03	6.03	-11.58	-152.7
50	330	-7926	-584	-302	0	758	2486	14.07	14.07	6.03	6.03	-9.14	-121.1
51	330	-8545	-691	-321	0	806	2738	14.07	14.07	6.03	6.03	-10.10	-133.4

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

ASTA NUM. 35 NI 302 NF 291 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 1D
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-9366	747	304	0	-830	-562	4.02	4.02	10.05	10.05	-9.60	-123.7
41	0	-9072	69	38	0	-874	373	4.02	4.02	10.05	10.05	-8.98	-124.1
42	0	-8909	59	-49	0	-937	379	4.02	4.02	10.05	10.05	-9.21	-126.7
43	0	-8727	1116	298	0	-857	-1122	4.02	4.02	10.05	10.05	-17.19	-178.2
44	0	-8708	-1062	-378	0	-939	1931	4.02	4.02	10.05	10.05	-29.83	475.5
45	0	-7966	-30	-290	0	-1036	446	4.02	4.02	10.05	10.05	-9.29	-126.3
46	0	-7737	-63	-256	0	-964	475	4.02	4.02	10.05	10.05	-8.78	-119.7
47	0	-7403	-96	-330	0	-987	500	4.02	4.02	10.05	10.05	-8.77	-119.1
49	0	-7501	130	-241	0	-972	188	4.02	4.02	10.05	10.05	-8.73	-118.7
50	0	-7497	-306	-376	0	-989	799	4.02	4.02	10.05	10.05	-12.23	-133.9
51	0	-7348	-100	-359	0	-1008	502	4.02	4.02	10.05	10.05	-8.88	-120.3

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	83	-8995	621	304	0	-1081	3	4.02	4.02	10.05	10.05	-9.99	-136.5
41	83	-8701	69	38	0	-906	430	4.02	4.02	10.05	10.05	-8.95	-123.1
42	83	-8538	59	25	0	-929	428	4.02	4.02	10.05	10.05	-8.97	-123.3
43	83	-8356	907	298	0	-1103	-287	4.02	4.02	10.05	10.05	-9.83	-133.6
44	83	-8337	-852	-378	0	-627	1141	4.02	4.02	10.05	10.05	-17.51	-178.1
45	83	-7595	-30	-168	0	-848	421	4.02	4.02	10.05	10.05	-8.09	-111.0
46	83	-7366	-63	-256	0	-753	423	4.02	4.02	10.05	10.05	-7.51	-103.4
47	83	-7032	-96	-330	0	-715	421	4.02	4.02	10.05	10.05	-7.19	-98.5
49	83	-7130	88	-241	0	-774	278	4.02	4.02	10.05	10.05	-7.48	-102.8
50	83	-7126	-264	-376	0	-678	564	4.02	4.02	10.05	10.05	-8.87	-104.4
51	83	-6977	-100	-334	0	-723	420	4.02	4.02	10.05	10.05	-7.16	-98.5

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	165	-8624	496	304	0	-1332	464	4.02	4.02	10.05	10.05	-11.40	-153.0
41	165	-8330	69	38	0	-938	488	4.02	4.02	10.05	10.05	-8.91	-122.2
42	165	-8166	59	88	0	-976	477	4.02	4.02	10.05	10.05	-9.04	-123.6
43	165	-7984	697	298	0	-1348	374	4.02	4.02	10.05	10.05	-11.40	-151.6
44	165	-7966	-643	-378	0	-315	525	4.02	4.02	10.05	10.05	-8.66	-105.2
45	165	-7224	-30	-62	0	-755	397	4.02	4.02	10.05	10.05	-7.44	-102.4
46	165	-6994	-63	-256	0	-542	371	4.02	4.02	10.05	10.05	-6.69	-87.7
47	165	-6660	-96	-330	0	-443	341	4.02	4.02	10.05	10.05	-6.27	-79.0
49	165	-6758	46	-241	0	-575	333	4.02	4.02	10.05	10.05	-6.32	-87.8
50	165	-6754	-222	-376	0	-368	363	4.02	4.02	10.05	10.05	-6.51	-81.2
51	165	-6606	-100	-313	0	-456	338	4.02	4.02	10.05	10.05	-6.21	-79.4

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	248	-8252	370	304	0	-1583	821	4.02	4.02	10.05	10.05	-13.32	-174.5
41	248	-7958	69	38	0	-969	545	4.02	4.02	10.05	10.05	-8.90	-121.6
42	248	-7795	59	141	0	-1072	526	4.02	4.02	10.05	10.05	-9.43	-127.8
43	248	-7613	488	298	0	-1594	863	4.02	4.02	10.05	10.05	-13.48	-174.3
44	248	-7594	-433	-378	0	-2	81	4.02	4.02	10.05	10.05	-4.35	-61.5
45	248	-6852	-30	25	0	-740	372	4.02	4.02	10.05	10.05	-7.18	-98.6
46	248	-6623	-63	-256	0	-331	318	4.02	4.02	10.05	10.05	-6.04	-76.2
47	248	-6289	-96	-330	0	-171	262	4.02	4.02	10.05	10.05	-5.37	-68.7
49	248	-6387	4	-241	0	-376	354	4.02	4.02	10.05	10.05	-6.26	-77.7
50	248	-6383	-180	-376	0	-58	197	4.02	4.02	10.05	10.05	-4.83	-63.5
51	248	-6234	-100	-296	0	-205	255	4.02	4.02	10.05	10.05	-5.29	-67.7

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	330	-7881	244	304	0	-1834	1074	4.02	4.02	10.05	10.05	-16.47	-199.6
41	330	-7587	69	38	0	-1001	602	4.02	4.02	10.05	10.05	-9.46	-121.3
42	330	-7424	59	183	0	-1206	575	4.02	4.02	10.05	10.05	-10.24	-136.8
43	330	-7242	278	298	0	-1839	1179	4.02	4.02	10.05	10.05	-18.15	213.7
44	330	-7223	-224	-378	0	310	-190	4.02	4.02	10.05	10.05	-5.27	-75.3
45	330	-6481	-30	95	0	-791	347	4.02	4.02	10.05	10.05	-7.26	-99.2
46	330	-6252	-63	-256	0	-119	266	4.02	4.02	10.05	10.05	-5.39	-68.8
47	330	-5918	-96	-330	0	101	182	4.02	4.02	10.05	10.05	-4.47	-58.8
49	330	-6016	-38	-241	0	-177	340	4.02	4.02	10.05	10.05	-5.95	-73.8
50	330	-6012	-138	-376	0	253	66	4.02	4.02	10.05	10.05	-4.36	-62.4
51	330	-5863	-100	-282	0	33	173	4.02	4.02	10.05	10.05	-4.36	-57.6

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

ASTA NUM. 36 NI 325 NF 295 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 10D
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm²				daN/cm²	
40	0	-9915	922	-297	0	-2418	-1382	6.03	6.03	10.05	10.05	-15.20	-192.4
41	0	-8993	-242	-216	0	-1972	215	6.03	6.03	10.05	10.05	-12.27	-157.9
42	0	-8971	-242	-539	0	-1305	214	6.03	6.03	10.05	10.05	-8.37	-113.0
43	0	-10180	1781	-299	0	-2265	-2583	6.03	6.03	10.05	10.05	-22.87	372.7
44	0	-7799	-2187	-93	0	-1315	2885	6.03	6.03	10.05	10.05	-25.57	559.5
45	0	-8605	-158	-703	0	-410	76	6.03	6.03	10.05	10.05	-4.81	-68.5
46	0	-8431	-109	-135	0	-1252	-3	6.03	6.03	10.05	10.05	-7.99	-107.6
47	0	-8291	-75	-114	0	-1072	-58	6.03	6.03	10.05	10.05	-7.13	-97.1
49	0	-8598	312	-141	0	-1220	-590	6.03	6.03	10.05	10.05	-7.87	-106.5
50	0	-8122	-481	-100	0	-1030	503	6.03	6.03	10.05	10.05	-6.90	-94.0
51	0	-8283	-75	-222	0	-850	-58	6.03	6.03	10.05	10.05	-6.27	-86.4

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	83	-9420	922	-297	0	-2173	-622	6.03	6.03	10.05	10.05	-13.58	-173.4
41	83	-8498	-242	-216	0	-1793	15	6.03	6.03	10.05	10.05	-11.13	-144.1
42	83	-8476	-242	-393	0	-922	14	6.03	6.03	10.05	10.05	-6.60	-90.8
43	83	-9684	1781	-299	0	-2018	-1114	6.03	6.03	10.05	10.05	-12.51	-162.3
44	83	-7304	-2187	-93	0	-1238	1081	6.03	6.03	10.05	10.05	-9.43	-112.1
45	83	-8110	-158	-459	0	66	-54	6.03	6.03	10.05	10.05	-3.38	-50.1
46	83	-7936	-109	-135	0	-1141	-93	6.03	6.03	10.05	10.05	-7.34	-99.1
47	83	-7796	-75	-114	0	-978	-120	6.03	6.03	10.05	10.05	-6.58	-89.7
49	83	-8103	312	-141	0	-1104	-332	6.03	6.03	10.05	10.05	-7.21	-97.8
50	83	-7627	-481	-100	0	-948	106	6.03	6.03	10.05	10.05	-6.40	-87.3
51	83	-7788	-75	-173	0	-687	-121	6.03	6.03	10.05	10.05	-5.49	-76.2

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	165	-8925	922	-297	0	-1928	139	6.03	6.03	10.05	10.05	-11.98	-154.6
41	165	-8003	-242	-216	0	-1614	-184	6.03	6.03	10.05	10.05	-10.00	-130.3
42	165	-7981	-242	-268	0	-651	-185	6.03	6.03	10.05	10.05	-5.44	-75.7
43	165	-9189	1781	-299	0	-1771	356	6.03	6.03	10.05	10.05	-10.96	-143.7
44	165	-6809	-2187	-93	0	-1161	-723	6.03	6.03	10.05	10.05	-7.23	-96.2
45	165	-7615	-158	-250	0	357	-185	6.03	6.03	10.05	10.05	-4.24	-60.3
46	165	-7441	-109	-135	0	-1030	-183	6.03	6.03	10.05	10.05	-6.69	-90.7
47	165	-7301	-75	-114	0	-883	-182	6.03	6.03	10.05	10.05	-6.03	-82.4
49	165	-7608	312	-141	0	-988	-75	6.03	6.03	10.05	10.05	-6.56	-89.3
50	165	-7132	-481	-100	0	-865	-290	6.03	6.03	10.05	10.05	-5.90	-80.6
51	165	-7293	-75	-131	0	-562	-183	6.03	6.03	10.05	10.05	-4.85	-67.7

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	248	-8430	922	-297	0	-1683	900	6.03	6.03	10.05	10.05	-10.42	-136.0
41	248	-7508	-242	-216	0	-1436	-383	6.03	6.03	10.05	10.05	-8.88	-116.6
42	248	-7486	-242	-163	0	-475	-384	6.03	6.03	10.05	10.05	-4.75	-64.9
43	248	-8694	1781	-299	0	-1524	1825	6.03	6.03	10.05	10.05	-16.07	209.7
44	248	-6314	-2187	-93	0	-1084	-2527	6.03	6.03	10.05	10.05	-22.38	512.1
45	248	-7120	-158	-77	0	489	-315	6.03	6.03	10.05	10.05	-4.52	-63.4
46	248	-6946	-109	-135	0	-918	-272	6.03	6.03	10.05	10.05	-6.06	-82.4
47	248	-6806	-75	-114	0	-789	-245	6.03	6.03	10.05	10.05	-5.49	-75.1
49	248	-7113	312	-141	0	-871	183	6.03	6.03	10.05	10.05	-5.92	-80.8
50	248	-6637	-481	-100	0	-783	-687	6.03	6.03	10.05	10.05	-6.20	-78.4
51	248	-6798	-75	-97	0	-469	-245	6.03	6.03	10.05	10.05	-4.32	-60.6

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	330	-7935	922	-297	0	-1438	1660	6.03	6.03	10.05	10.05	-14.62	189.9
41	330	-7013	-242	-216	0	-1257	-583	6.03	6.03	10.05	10.05	-7.80	-103.1
42	330	-6991	-242	-80	0	-376	-584	6.03	6.03	10.05	10.05	-5.62	-72.9
43	330	-8198	1781	-299	0	-1277	3294	6.03	6.03	10.05	10.05	-29.17	668.9
44	330	-5819	-2187	-93	0	-1007	-4331	6.03	6.03	10.05	10.05	-37.91	1100.5
45	330	-6625	-158	62	0	493	-446	6.03	6.03	10.05	10.05	-4.75	-62.7
46	330	-6451	-109	-135	0	-807	-362	6.03	6.03	10.05	10.05	-5.43	-74.1
47	330	-6311	-75	-114	0	-695	-307	6.03	6.03	10.05	10.05	-4.95	-68.0
49	330	-6618	312	-141	0	-755	441	6.03	6.03	10.05	10.05	-5.29	-72.5
50	330	-6142	-481	-100	0	-701	-1084	6.03	6.03	10.05	10.05	-9.49	-108.6
51	330	-6303	-75	-69	0	-401	-307	6.03	6.03	10.05	10.05	-3.92	-54.7

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

ASTA NUM. 37 NI 296 NF 297 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 15C
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm²				daN/cm²	
40	0	-14770	878	-612	0	-2364	-1531	6.03	6.03	10.05	10.05	-14.85	-198.8
41	0	-14400	-250	-534	0	-2022	519	6.03	6.03	10.05	10.05	-13.09	-177.2
42	0	-14250	-251	-1058	0	-1717	522	6.03	6.03	10.05	10.05	-11.74	-160.5
43	0	-13750	1693	-535	0	-2095	-3026	6.03	6.03	10.05	10.05	-26.70	370.6
44	0	-14010	-2137	-429	0	-1548	3951	6.03	6.03	10.05	10.05	-35.03	630.1
45	0	-12870	-189	-1280	0	-1016	396	6.03	6.03	10.05	10.05	-8.65	-120.5
46	0	-12360	-150	-328	0	-1225	315	6.03	6.03	10.05	10.05	-9.20	-127.0
47	0	-11850	-125	-276	0	-1026	264	6.03	6.03	10.05	10.05	-8.29	-115.1
49	0	-11970	251	-302	0	-1140	-420	6.03	6.03	10.05	10.05	-8.74	-120.9
50	0	-12020	-515	-281	0	-1031	976	6.03	6.03	10.05	10.05	-9.51	-123.6
51	0	-11800	-125	-451	0	-924	265	6.03	6.03	10.05	10.05	-7.90	-110.2

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	95	-14200	878	-612	0	-1783	-697	6.03	6.03	10.05	10.05	-11.99	-163.5
41	95	-13830	-250	-534	0	-1515	282	6.03	6.03	10.05	10.05	-10.81	-148.6
42	95	-13680	-251	-890	0	-793	283	6.03	6.03	10.05	10.05	-8.16	-115.2
43	95	-13180	1693	-535	0	-1586	-1418	6.03	6.03	10.05	10.05	-12.69	-159.7
44	95	-13440	-2137	-429	0	-1141	1920	6.03	6.03	10.05	10.05	-16.75	-200.6
45	95	-12300	-189	-999	0	63	216	6.03	6.03	10.05	10.05	-5.67	-80.8
46	95	-11790	-150	-328	0	-914	172	6.03	6.03	10.05	10.05	-7.86	-109.6
47	95	-11280	-125	-276	0	-763	145	6.03	6.03	10.05	10.05	-7.12	-99.9
49	95	-11400	251	-302	0	-853	-181	6.03	6.03	10.05	10.05	-7.49	-104.6
50	95	-11451	-515	-281	0	-764	487	6.03	6.03	10.05	10.05	-7.19	-100.9

51	95	-11229	-125	-395	0	-523	146	6.03	6.03	10.05	10.05	-6.23	-88.8

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	190	-13630	878	-612	0	-1202	138	6.03	6.03	10.05	10.05	-9.61	-133.3
41	190	-13260	-250	-534	0	-1008	44	6.03	6.03	10.05	10.05	-8.77	-122.4
42	190	-13110	-251	-746	0	-18	45	6.03	6.03	10.05	10.05	-5.14	-77.0
43	190	-12610	1693	-535	0	-1078	190	6.03	6.03	10.05	10.05	-8.77	-121.8
44	190	-12870	-2137	-429	0	-733	-110	6.03	6.03	10.05	10.05	-7.63	-107.8
45	190	-11730	-189	-759	0	895	36	6.03	6.03	10.05	10.05	-7.77	-108.5
46	190	-11220	-150	-328	0	-602	30	6.03	6.03	10.05	10.05	-6.52	-92.3
47	190	-10709	-125	-276	0	-501	27	6.03	6.03	10.05	10.05	-5.95	-84.8
49	190	-10831	251	-302	0	-565	58	6.03	6.03	10.05	10.05	-6.23	-88.4
50	190	-10882	-515	-281	0	-497	-2	6.03	6.03	10.05	10.05	-6.01	-85.6
51	190	-10658	-125	-347	0	-171	27	6.03	6.03	10.05	10.05	-4.75	-69.6

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	285	-13060	878	-612	0	-621	972	6.03	6.03	10.05	10.05	-9.85	-128.9
41	285	-12690	-250	-534	0	-501	-193	6.03	6.03	10.05	10.05	-6.72	-96.3
42	285	-12540	-251	-626	0	632	-194	6.03	6.03	10.05	10.05	-7.13	-101.3
43	285	-12040	1693	-535	0	-569	1799	6.03	6.03	10.05	10.05	-15.69	-186.1
44	285	-12300	-2137	-429	0	-326	-2141	6.03	6.03	10.05	10.05	-18.73	-214.9
45	285	-11160	-189	-559	0	1518	-144	6.03	6.03	10.05	10.05	-9.92	-134.6
46	285	-10650	-150	-328	0	-291	-112	6.03	6.03	10.05	10.05	-5.17	-75.0
47	285	-10138	-125	-276	0	-238	-92	6.03	6.03	10.05	10.05	-4.79	-69.6
49	285	-10262	251	-302	0	-278	296	6.03	6.03	10.05	10.05	-5.33	-74.2
50	285	-10314	-515	-281	0	-230	-492	6.03	6.03	10.05	10.05	-6.35	-85.8
51	285	-10088	-125	-307	0	139	-92	6.03	6.03	10.05	10.05	-4.41	-64.9

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	380	-12490	878	-612	0	-40	1806	6.03	6.03	10.05	10.05	-15.75	-188.2
41	380	-12120	-250	-534	0	6	-431	6.03	6.03	10.05	10.05	-6.71	-92.3
42	380	-11970	-251	-530	0	1179	-433	6.03	6.03	10.05	10.05	-8.88	-122.6
43	380	-11470	1693	-535	0	-61	3407	6.03	6.03	10.05	10.05	-30.22	567.6
44	380	-11730	-2137	-429	0	81	-4171	6.03	6.03	10.05	10.05	-36.98	789.7
45	380	-10590	-189	-399	0	1970	-324	6.03	6.03	10.05	10.05	-12.20	-160.6
46	380	-10080	-150	-328	0	21	-255	6.03	6.03	10.05	10.05	-5.04	-70.7
47	380	-9568	-125	-276	0	24	-211	6.03	6.03	10.05	10.05	-4.63	-65.3
49	380	-9692	251	-302	0	9	535	6.03	6.03	10.05	10.05	-6.35	-84.8
50	380	-9745	-515	-281	0	38	-981	6.03	6.03	10.05	10.05	-8.90	-113.1
51	380	-9517	-125	-275	0	415	-211	6.03	6.03	10.05	10.05	-5.18	-74.0

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

ASTA NUM. 38 NI 299 NF 294 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 10B
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-23030	778	379	0	147	-1849	6.03	6.03	10.05	10.05	-18.11	-235.6
41	0	-22240	21	350	0	217	-52	6.03	6.03	10.05	10.05	-9.40	-139.0
42	0	-22210	24	158	0	-81	-58	6.03	6.03	10.05	10.05	-8.90	-132.7
43	0	-22970	1261	333	0	63	-3009	6.03	6.03	10.05	10.05	-26.31	-320.5
44	0	-20970	-1235	307	0	324	2932	6.03	6.03	10.05	10.05	-25.58	-307.7
45	0	-21610	4	-35	0	-317	-24	6.03	6.03	10.05	10.05	-9.52	-139.9
46	0	-21290	-15	246	0	156	9	6.03	6.03	10.05	10.05	-8.81	-130.8
47	0	-21060	-24	220	0	141	24	6.03	6.03	10.05	10.05	-8.67	-128.7
49	0	-21320	228	230	0	118	-575	6.03	6.03	10.05	10.05	-10.86	-151.7
50	0	-20920	-271	224	0	170	613	6.03	6.03	10.05	10.05	-10.91	-151.7
51	0	-21050	-23	156	0	42	22	6.03	6.03	10.05	10.05	-8.31	-124.2

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	97	-22445	778	379	0	-222	-1090	6.03	6.03	10.05	10.05	-13.93	-187.9
41	97	-21655	21	350	0	-124	-32	6.03	6.03	10.05	10.05	-8.84	-131.5
42	97	-21625	24	158	0	-235	-34	6.03	6.03	10.05	10.05	-9.22	-136.2
43	97	-22385	1261	333	0	-261	-1780	6.03	6.03	10.05	10.05	-17.50	-227.9
44	97	-20385	-1235	307	0	25	1728	6.03	6.03	10.05	10.05	-16.56	-214.3
45	97	-21025	4	-35	0	-283	-20	6.03	6.03	10.05	10.05	-9.16	-134.9
46	97	-20705	-15	246	0	-84	-6	6.03	6.03	10.05	10.05	-8.32	-124.1
47	97	-20475	-24	220	0	-74	0	6.03	6.03	10.05	10.05	-8.20	-122.3
49	97	-20735	228	230	0	-106	-352	6.03	6.03	10.05	10.05	-9.49	-135.6
50	97	-20335	-271	224	0	-49	349	6.03	6.03	10.05	10.05	-9.33	-133.2
51	97	-20465	-23	156	0	-110	-0	6.03	6.03	10.05	10.05	-8.33	-123.9

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	195	-21860	778	379	0	-591	-331	6.03	6.03	10.05	10.05	-10.60	-153.7
41	195	-21070	21	350	0	-466	-11	6.03	6.03	10.05	10.05	-9.84	-143.4
42	195	-21040	24	158	0	-389	-11	6.03	6.03	10.05	10.05	-9.55	-139.8
43	195	-21800	1261	333	0	-586	-550	6.03	6.03	10.05	10.05	-10.91	-153.1
44	195	-19800	-1235	307	0	-275	524	6.03	6.03	10.05	10.05	-10.03	-140.3
45	195	-20440	4	-35	0	-248	-17	6.03	6.03	10.05	10.05	-8.81	-130.0
46	195	-20120	-15	246	0	-324	-21	6.03	6.03	10.05	10.05	-8.96	-131.5
47	195	-19890	-24	220	0	-288	-23	6.03	6.03	10.05	10.05	-8.74	-128.6
49	195	-20150	228	230	0	-330	-130	6.03	6.03	10.05	10.05	-9.00	-132.0
50	195	-19750	-271	224	0	-268	85	6.03	6.03	10.05	10.05	-8.62	-126.8
51	195	-19880	-23	156	0	-263	-23	6.03	6.03	10.05	10.05	-8.65	-127.4

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	292	-21275	778	379	0	-961	428	6.03	6.03	10.05	10.05	-11.70	-166.9
41	292	-20485	21	350	0	-807	10	6.03	6.03	10.05	10.05	-10.84	-155.4
42	292	-20455	24	158	0	-543	13	6.03	6.03	10.05	10.05	-9.88	-143.3
43	292	-21215	1261	333	0	-910	679	6.03	6.03	10.05	10.05	-11.50	-164.2
44	292	-19215	-1235	307	0	-574	-680	6.03	6.03	10.05	10.05	-10.62	-146.1
45	292	-19855	4	-35	0	-214	-13	6.03	6.03	10.05	10.05	-8.46	-125.0
46	292	-19535	-15	246	0	-564	-35	6.03	6.03	10.05	10.05	-9.60	-138.9
47	292	-19305	-24	220	0	-503	-47	6.03	6.03	10.05	10.05	-9.29	-134.8
49	292	-19565	228	230	0	-554	93	6.03	6.03	10.05	10.05	-9.58	-138.6
50	292	-19165	-271	224	0	-487	-179	6.03	6.03	10.05	10.05	-9.18	-133.3
51	292	-19295	-23	156	0	-415	-45	6.03	6.03	10.05	10.05	-8.97	-130.8

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	390	-20690	778	379	0	-1330	1187	6.03	6.03	10.05	10.05	-13.78	-183.7
41	390	-19900	21	350	0	-1149	30	6.03	6.03	10.05	10.05	-11.85	-167.4
42	390	-19870	24	158	0	-697	36	6.03	6.03	10.05	10.05	-10.21	-146.8
43	390	-20630	1261	333	0	-1234	1908	6.03	6.03	10.05	10.05	-17.74	-227.5
44	390	-18630	-1235	307	0	-874	-1884	6.03	6.03	10.05	10.05	-17.08	-216.8
45	390	-19270	4	-35	0	-180	-10	6.03	6.03	10.05	10.05	-8.11	-120.1
46	390	-18950	-15	246	0	-804	-50	6.03	6.03	10.05	10.05	-10.24	-146.3
47	390	-18720	-24	220	0	-718	-70	6.03	6.03	10.05	10.05	-9.84	-141.1
49	390	-18980	228	230	0	-778	316	6.03	6.03	10.05	10.05	-10.15	-145.3
50	390	-18580	-271	224	0	-706	-443	6.03	6.03	10.05	10.05	-9.74	-139.7
51	390	-18710	-23	156	0	-567	-68	6.03	6.03	10.05	10.05	-9.29	-134.3

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

ASTA NUM. 39 NI 300 NF 296 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 15B
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-32330	686	532	0	490	-1242	6.03	6.03	10.05	10.05	-18.37	-251.6
41	0	-31910	133	520	0	518	-175	6.03	6.03	10.05	10.05	-14.23	-208.8
42	0	-31770	136	335	0	252	-180	6.03	6.03	10.05	10.05	-13.22	-196.0
43	0	-30920	1042	502	0	482	-1942	6.03	6.03	10.05	10.05	-21.46	-284.3
44	0	-30910	-786	486	0	530	1600	6.03	6.03	10.05	10.05	-19.69	-264.4
45	0	-29980	126	174	0	84	-172	6.03	6.03	10.05	10.05	-11.98	-178.0
46	0	-29180	114	460	0	533	-157	6.03	6.03	10.05	10.05	-13.23	-193.6
47	0	-28500	109	445	0	537	-152	6.03	6.03	10.05	10.05	-12.98	-189.8
49	0	-28650	293	449	0	528	-508	6.03	6.03	10.05	10.05	-13.22	-190.3
50	0	-28640	-72	446	0	537	200	6.03	6.03	10.05	10.05	-13.03	-190.6
51	0	-28460	110	383	0	448	-154	6.03	6.03	10.05	10.05	-12.64	-185.6

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	97	-31745	686	532	0	-28	-574	6.03	6.03	10.05	10.05	-14.71	-209.5
41	97	-31325	133	520	0	11	-46	6.03	6.03	10.05	10.05	-12.18	-182.6
42	97	-31185	136	335	0	-75	-48	6.03	6.03	10.05	10.05	-12.35	-184.6
43	97	-30335	1042	502	0	-8	-926	6.03	6.03	10.05	10.05	-16.00	-222.1
44	97	-30325	-786	486	0	56	834	6.03	6.03	10.05	10.05	-15.53	-216.8
45	97	-29395	126	174	0	-86	-49	6.03	6.03	10.05	10.05	-11.70	-174.7
46	97	-28595	114	460	0	85	-46	6.03	6.03	10.05	10.05	-11.38	-170.0
47	97	-27915	109	445	0	103	-46	6.03	6.03	10.05	10.05	-11.19	-166.9
49	97	-28065	293	449	0	90	-222	6.03	6.03	10.05	10.05	-11.53	-168.7
50	97	-28055	-72	446	0	103	130	6.03	6.03	10.05	10.05	-11.24	-167.7
51	97	-27875	110	383	0	74	-47	6.03	6.03	10.05	10.05	-11.07	-165.4

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	195	-31160	686	532	0	-546	95	6.03	6.03	10.05	10.05	-14.04	-205.7
41	195	-30740	133	520	0	-495	84	6.03	6.03	10.05	10.05	-13.69	-200.9
42	195	-30600	136	335	0	-401	85	6.03	6.03	10.05	10.05	-13.30	-195.9
43	195	-29750	1042	502	0	-498	90	6.03	6.03	10.05	10.05	-13.32	-195.3
44	195	-29740	-786	486	0	-418	68	6.03	6.03	10.05	10.05	-13.03	-191.6
45	195	-28810	126	174	0	-256	73	6.03	6.03	10.05	10.05	-12.08	-178.9
46	195	-28010	114	460	0	-363	65	6.03	6.03	10.05	10.05	-12.16	-179.1
47	195	-27330	109	445	0	-330	60	6.03	6.03	10.05	10.05	-11.78	-173.7
49	195	-27480	293	449	0	-348	64	6.03	6.03	10.05	10.05	-11.90	-175.4
50	195	-27470	-72	446	0	-332	59	6.03	6.03	10.05	10.05	-11.84	-174.6
51	195	-27290	110	383	0	-299	60	6.03	6.03	10.05	10.05	-11.65	-172.1

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	292	-30575	686	532	0	-1064	763	6.03	6.03	10.05	10.05	-15.68	-225.6
41	292	-30155	133	520	0	-1002	213	6.03	6.03	10.05	10.05	-15.29	-220.3
42	292	-30015	136	335	0	-728	217	6.03	6.03	10.05	10.05	-14.25	-207.2
43	292	-29165	1042	502	0	-987	1106	6.03	6.03	10.05	10.05	-16.50	-226.1
44	292	-29155	-786	486	0	-891	-698	6.03	6.03	10.05	10.05	-14.51	-209.6
45	292	-28225	126	174	0	-425	196	6.03	6.03	10.05	10.05	-12.47	-183.2
46	292	-27425	114	460	0	-812	176	6.03	6.03	10.05	10.05	-13.55	-195.9
47	292	-26745	109	445	0	-764	166	6.03	6.03	10.05	10.05	-13.11	-189.8
49	292	-26895	293	449	0	-785	350	6.03	6.03	10.05	10.05	-13.25	-191.7
50	292	-26885	-72	446	0	-766	-11	6.03	6.03	10.05	10.05	-13.18	-190.7
51	292	-26705	110	383	0	-673	168	6.03	6.03	10.05	10.05	-12.77	-185.5

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	390	-29990	686	532	0	-1582	1432	6.03	6.03	10.05	10.05	-18.48	-249.6
41	390	-29570	133	520	0	-1508	343	6.03	6.03	10.05	10.05	-16.89	-239.7
42	390	-29430	136	335	0	-1054	349	6.03	6.03	10.05	10.05	-15.20	-218.5
43	390	-28580	1042	502	0	-1477	2122	6.03	6.03	10.05	10.05	-21.53	-281.8
44	390	-28570	-786	486	0	-1365	-1464	6.03	6.03	10.05	10.05	-18.12	-243.6
45	390	-27640	126	174	0	-595	318	6.03	6.03	10.05	10.05	-12.85	-187.4
46	390	-26840	114	460	0	-1260	287	6.03	6.03	10.05	10.05	-14.94	-212.7
47	390	-26160	109	445	0	-1198	273	6.03	6.03	10.05	10.05	-14.45	-206.0
49	390	-26310	293	449	0	-1223	636	6.03	6.03	10.05	10.05	-14.60	-208.0
50	390	-26300	-72	446	0	-1201	-82	6.03	6.03	10.05	10.05	-14.51	-206.9
51	390	-26120	110	383	0	-1047	275	6.03	6.03	10.05	10.05	-13.89	-198.9

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

ASTA NUM. 40 NI 301 NF 298 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 20B
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-28900	634	744	0	884	-1272	6.03	6.03	10.05	10.05	-17.26	-234.3

41	0	-29230	124	690	0	808	-242	6.03	6.03	10.05	10.05	-14.24	-206.3
42	0	-29160	128	542	0	647	-247	6.03	6.03	10.05	10.05	-13.63	-198.6
43	0	-27460	960	708	0	884	-1939	6.03	6.03	10.05	10.05	-20.16	-264.9
44	0	-29510	-726	592	0	658	1478	6.03	6.03	10.05	10.05	-18.54	-249.6
45	0	-27910	116	373	0	489	-230	6.03	6.03	10.05	10.05	-12.58	-184.2
46	0	-27310	101	577	0	728	-209	6.03	6.03	10.05	10.05	-13.20	-191.5
47	0	-26820	96	549	0	708	-200	6.03	6.03	10.05	10.05	-12.94	-187.7
49	0	-26710	266	566	0	733	-544	6.03	6.03	10.05	10.05	-12.99	-188.2
50	0	-27120	-71	543	0	688	139	6.03	6.03	10.05	10.05	-12.99	-188.6
51	0	-26800	97	499	0	654	-202	6.03	6.03	10.05	10.05	-12.74	-185.2

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	97	-28315	634	744	0	159	-654	6.03	6.03	10.05	10.05	-13.85	-195.2
41	97	-28645	124	690	0	135	-121	6.03	6.03	10.05	10.05	-11.59	-172.6
42	97	-28575	128	542	0	118	-123	6.03	6.03	10.05	10.05	-11.50	-171.4
43	97	-26875	960	708	0	193	-1004	6.03	6.03	10.05	10.05	-15.12	-207.4
44	97	-28925	-726	592	0	80	770	6.03	6.03	10.05	10.05	-14.68	-205.3
45	97	-27325	116	373	0	126	-117	6.03	6.03	10.05	10.05	-11.04	-164.5
46	97	-26725	101	577	0	165	-110	6.03	6.03	10.05	10.05	-10.95	-162.8
47	97	-26235	96	549	0	173	-107	6.03	6.03	10.05	10.05	-10.79	-160.3
49	97	-26125	266	566	0	181	-285	6.03	6.03	10.05	10.05	-11.14	-161.6
50	97	-26535	-71	543	0	158	70	6.03	6.03	10.05	10.05	-10.85	-161.3
51	97	-26215	97	499	0	167	-108	6.03	6.03	10.05	10.05	-10.76	-159.9

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	195	-27730	634	744	0	-566	-36	6.03	6.03	10.05	10.05	-12.78	-186.6
41	195	-28060	124	690	0	-538	0	6.03	6.03	10.05	10.05	-12.81	-187.3
42	195	-27990	128	542	0	-410	2	6.03	6.03	10.05	10.05	-12.32	-181.1
43	195	-26290	960	708	0	-497	-68	6.03	6.03	10.05	10.05	-11.98	-175.2
44	195	-28340	-726	592	0	-497	63	6.03	6.03	10.05	10.05	-12.77	-187.1
45	195	-26740	116	373	0	-238	-4	6.03	6.03	10.05	10.05	-11.22	-166.1
46	195	-26140	101	577	0	-397	-11	6.03	6.03	10.05	10.05	-11.56	-169.8
47	195	-25650	96	549	0	-362	-14	6.03	6.03	10.05	10.05	-11.24	-165.4
49	195	-25540	266	566	0	-371	-26	6.03	6.03	10.05	10.05	-11.23	-165.2
50	195	-25950	-71	543	0	-371	-0	6.03	6.03	10.05	10.05	-11.39	-167.5
51	195	-25630	97	499	0	-319	-13	6.03	6.03	10.05	10.05	-11.08	-163.3

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	292	-27145	634	744	0	-1291	582	6.03	6.03	10.05	10.05	-15.17	-215.9
41	292	-27475	124	690	0	-1211	121	6.03	6.03	10.05	10.05	-15.01	-214.2
42	292	-27405	128	542	0	-939	127	6.03	6.03	10.05	10.05	-14.00	-201.5
43	292	-25705	960	708	0	-1188	867	6.03	6.03	10.05	10.05	-14.24	-202.8
44	292	-27755	-726	592	0	-1075	-644	6.03	6.03	10.05	10.05	-14.63	-209.7
45	292	-26155	116	373	0	-601	110	6.03	6.03	10.05	10.05	-12.30	-179.1
46	292	-25555	101	577	0	-960	88	6.03	6.03	10.05	10.05	-13.36	-191.7
47	292	-25065	96	549	0	-897	79	6.03	6.03	10.05	10.05	-12.94	-186.0
49	292	-24955	266	566	0	-924	233	6.03	6.03	10.05	10.05	-13.00	-186.6
50	292	-25365	-71	543	0	-901	-70	6.03	6.03	10.05	10.05	-13.07	-188.0
51	292	-25045	97	499	0	-806	81	6.03	6.03	10.05	10.05	-12.61	-181.8

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	390	-26560	634	744	0	-2016	1200	6.03	6.03	10.05	10.05	-17.55	-245.1
41	390	-26890	124	690	0	-1884	242	6.03	6.03	10.05	10.05	-17.20	-241.1
42	390	-26820	128	542	0	-1468	252	6.03	6.03	10.05	10.05	-15.68	-222.0
43	390	-25120	960	708	0	-1878	1803	6.03	6.03	10.05	10.05	-18.60	-244.1
44	390	-27170	-726	592	0	-1653	-1352	6.03	6.03	10.05	10.05	-17.03	-232.3
45	390	-25570	116	373	0	-965	223	6.03	6.03	10.05	10.05	-13.38	-192.0
46	390	-24970	101	577	0	-1523	186	6.03	6.03	10.05	10.05	-15.16	-213.7
47	390	-24480	96	549	0	-1432	172	6.03	6.03	10.05	10.05	-14.64	-206.7
49	390	-24370	266	566	0	-1476	492	6.03	6.03	10.05	10.05	-14.76	-208.1
50	390	-24780	-71	543	0	-1431	-140	6.03	6.03	10.05	10.05	-14.75	-208.4
51	390	-24460	97	499	0	-1293	176	6.03	6.03	10.05	10.05	-14.13	-200.4

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

ASTA NUM. 41 NI 35 NF 31 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 12D
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-5665	719	714	0	-2209	-1075	6.03	6.03	10.05	10.05	-14.58	316.9
41	0	-4747	705	584	0	-1634	-967	6.03	6.03	10.05	10.05	-10.68	201.9
42	0	-4723	759	-24	0	-5037	-1022	6.03	6.03	10.05	10.05	-33.59	1284.3
43	0	-5685	778	668	0	-2201	-1192	6.03	6.03	10.05	10.05	-14.52	313.3
44	0	-3552	696	393	0	-758	-807	6.03	6.03	10.05	10.05	-7.12	102.8
45	0	-4116	845	-562	0	-6914	-1104	6.03	6.03	10.05	10.05	-45.74	1942.0
46	0	-3800	785	373	0	-1008	-1039	6.03	6.03	10.05	10.05	-9.21	161.2
47	0	-3563	805	320	0	-852	-1057	6.03	6.03	10.05	10.05	-9.37	175.9
49	0	-3869	809	363	0	-1043	-1093	6.03	6.03	10.05	10.05	-9.69	174.6
50	0	-3443	793	308	0	-755	-1016	6.03	6.03	10.05	10.05	-9.01	168.4
51	0	-3555	822	117	0	-1986	-1076	6.03	6.03	10.05	10.05	-13.29	384.7

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	58	-5318	719	714	0	-2622	-659	6.03	6.03	10.05	10.05	-17.50	465.5
41	58	-4400	705	584	0	-1972	-559	6.03	6.03	10.05	10.05	-13.12	323.9
42	58	-4376	759	-236	0	-4962	-583	6.03	6.03	10.05	10.05	-33.05	1285.8
43	58	-5338	778	668	0	-2587	-742	6.03	6.03	10.05	10.05	-17.26	453.5
44	58	-3205	696	393	0	-985	-404	6.03	6.03	10.05	10.05	-6.36	103.3
45	58	-3769	845	-914	0	-6487	-616	6.03	6.03	10.05	10.05	-42.89	1829.2
46	58	-3453	785	373	0	-1224	-585	6.03	6.03	10.05	10.05	-8.02	156.9
47	58	-3216	805	320	0	-1037	-592	6.03	6.03	10.05	10.05	-6.73	117.0
49	58	-3522	809	363	0	-1253	-625	6.03	6.03	10.05	10.05	-8.21	161.5
50	58	-3096	793	308	0	-933	-558	6.03	6.03	10.05	10.05	-6.01	94.8
51	58	-3208	822	47	0	-2033	-600	6.03	6.03	10.05	10.05	-13.63	423.9

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	116	-4971	719	714	0	-3034	-243	6.03	6.03	10.05	10.05	-20.33	619.7
41	116	-4053	705	584	0	-2310	-152	6.03	6.03	10.05	10.05	-15.46	452.9

42	116	-4029	759	-448	0	-4764	-144	6.03	6.03	10.05	10.05	-31.71	1247.5
43	116	-4991	778	668	0	-2974	-292	6.03	6.03	10.05	10.05	-19.92	598.9
44	116	-2858	696	393	0	-1212	-2	6.03	6.03	10.05	10.05	-8.04	189.4
45	116	-3422	845	-1267	0	-5856	-127	6.03	6.03	10.05	10.05	-38.72	1649.8
46	116	-3106	785	373	0	-1439	-132	6.03	6.03	10.05	10.05	-9.59	243.2
47	116	-2869	805	320	0	-1222	-127	6.03	6.03	10.05	10.05	-8.11	191.6
49	116	-3175	809	363	0	-1463	-157	6.03	6.03	10.05	10.05	-9.74	246.1
50	116	-2749	793	308	0	-1111	-99	6.03	6.03	10.05	10.05	-7.35	165.4
51	116	-2862	822	-24	0	-2040	-124	6.03	6.03	10.05	10.05	-13.67	450.7

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	173	-4624	719	714	0	-3447	173	6.03	6.03	10.05	10.05	-23.09	776.7
41	173	-3706	705	584	0	-2647	256	6.03	6.03	10.05	10.05	-17.74	585.3
42	173	-3682	759	-659	0	-4444	295	6.03	6.03	10.05	10.05	-29.57	1169.4
43	173	-4644	778	668	0	-3360	159	6.03	6.03	10.05	10.05	-22.51	747.1
44	173	-2511	696	393	0	-1440	401	6.03	6.03	10.05	10.05	-9.64	283.4
45	173	-3075	845	-1620	0	-5021	361	6.03	6.03	10.05	10.05	-33.23	1403.7
46	173	-2759	785	373	0	-1654	322	6.03	6.03	10.05	10.05	-11.08	334.5
47	173	-2522	805	320	0	-1407	339	6.03	6.03	10.05	10.05	-9.42	272.3
49	173	-2828	809	363	0	-1673	311	6.03	6.03	10.05	10.05	-11.21	335.6
50	173	-2402	793	308	0	-1289	359	6.03	6.03	10.05	10.05	-8.62	243.2
51	173	-2515	822	-94	0	-2006	351	6.03	6.03	10.05	10.05	-13.43	464.7

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	231	-4277	719	714	0	-3860	589	6.03	6.03	10.05	10.05	-25.81	935.4
41	231	-3359	705	584	0	-2985	664	6.03	6.03	10.05	10.05	-19.96	719.6
42	231	-3335	759	-871	0	-4001	734	6.03	6.03	10.05	10.05	-26.63	1051.4
43	231	-4297	778	668	0	-3746	609	6.03	6.03	10.05	10.05	-25.06	897.0
44	231	-2164	696	393	0	-1667	804	6.03	6.03	10.05	10.05	-11.17	380.8
45	231	-2728	845	-1973	0	-3982	850	6.03	6.03	10.05	10.05	-26.41	1091.2
46	231	-2412	785	373	0	-1870	776	6.03	6.03	10.05	10.05	-12.52	428.3
47	231	-2175	805	320	0	-1592	804	6.03	6.03	10.05	10.05	-10.67	355.9
49	231	-2481	809	363	0	-1883	779	6.03	6.03	10.05	10.05	-12.61	427.5
50	231	-2055	793	308	0	-1467	818	6.03	6.03	10.05	10.05	-9.83	324.3
51	231	-2168	822	-165	0	-1931	827	6.03	6.03	10.05	10.05	-12.91	465.9

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

ASTA NUM. 42 NI 37 NF 43 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 17D
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-5844	403	484	0	-2921	-565	6.03	6.03	10.05	10.05	-19.51	524.1
41	0	-5134	187	402	0	-2541	-222	6.03	6.03	10.05	10.05	-16.96	452.6
42	0	-5208	191	78	0	-6833	-232	6.03	6.03	10.05	10.05	-45.40	1832.5
43	0	-5516	534	445	0	-2599	-768	6.03	6.03	10.05	10.05	-17.32	445.4
44	0	-4163	-160	282	0	-2015	329	6.03	6.03	10.05	10.05	-13.44	352.8
45	0	-4456	180	-230	0	-9119	-213	6.03	6.03	10.05	10.05	-60.12	2636.0
46	0	-3852	164	254	0	-1619	-182	6.03	6.03	10.05	10.05	-10.74	250.7
47	0	-3531	159	217	0	-1389	-171	6.03	6.03	10.05	10.05	-9.17	201.1
49	0	-3768	231	244	0	-1516	-285	6.03	6.03	10.05	10.05	-10.03	224.8
50	0	-3497	92	211	0	-1399	-66	6.03	6.03	10.05	10.05	-9.25	206.2
51	0	-3556	160	109	0	-2820	-174	6.03	6.03	10.05	10.05	-18.88	651.8

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	88	-5313	403	484	0	-3349	-208	6.03	6.03	10.05	10.05	-22.44	696.1
41	88	-4603	187	402	0	-2897	-57	6.03	6.03	10.05	10.05	-19.41	601.6
42	88	-4677	191	-246	0	-6759	-63	6.03	6.03	10.05	10.05	-44.83	1848.6
43	88	-4985	534	445	0	-2993	-295	6.03	6.03	10.05	10.05	-20.05	605.5
44	88	-3632	-160	282	0	-2264	187	6.03	6.03	10.05	10.05	-15.17	467.7
45	88	-3925	180	-771	0	-8676	-54	6.03	6.03	10.05	10.05	-57.13	2532.1
46	88	-3321	164	254	0	-1844	-36	6.03	6.03	10.05	10.05	-12.34	355.6
47	88	-3000	159	217	0	-1581	-31	6.03	6.03	10.05	10.05	-10.57	294.5
49	88	-3237	231	244	0	-1732	-81	6.03	6.03	10.05	10.05	-11.58	326.0
50	88	-2966	92	211	0	-1586	15	6.03	6.03	10.05	10.05	-10.61	298.4
51	88	-3025	160	1	0	-2868	-33	6.03	6.03	10.05	10.05	-19.16	706.4

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	177	-4782	403	484	0	-3777	149	6.03	6.03	10.05	10.05	-25.29	871.6
41	177	-4072	187	402	0	-3252	108	6.03	6.03	10.05	10.05	-21.78	753.9
42	177	-4146	191	-570	0	-6398	106	6.03	6.03	10.05	10.05	-42.39	1771.3
43	177	-4454	534	445	0	-3387	177	6.03	6.03	10.05	10.05	-22.69	769.6
44	177	-3101	-160	282	0	-2513	46	6.03	6.03	10.05	10.05	-16.82	585.8
45	177	-3394	180	-1311	0	-7755	105	6.03	6.03	10.05	10.05	-51.03	2272.1
46	177	-2790	164	254	0	-2068	109	6.03	6.03	10.05	10.05	-13.85	464.8
47	177	-2469	159	217	0	-1772	110	6.03	6.03	10.05	10.05	-11.88	392.8
49	177	-2706	231	244	0	-1948	123	6.03	6.03	10.05	10.05	-13.05	432.1
50	177	-2435	92	211	0	-1772	97	6.03	6.03	10.05	10.05	-11.88	395.2
51	177	-2494	160	-107	0	-2821	109	6.03	6.03	10.05	10.05	-18.79	730.7

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	266	-4251	403	484	0	-4205	506	6.03	6.03	10.05	10.05	-28.08	1049.2
41	266	-3541	187	402	0	-3608	274	6.03	6.03	10.05	10.05	-24.08	908.3
42	266	-3615	191	-894	0	-5750	275	6.03	6.03	10.05	10.05	-38.07	1600.5
43	266	-3923	534	445	0	-3781	650	6.03	6.03	10.05	10.05	-25.26	936.0
44	266	-2570	-160	282	0	-2762	-96	6.03	6.03	10.05	10.05	-18.42	705.7
45	266	-2863	180	-1851	0	-6356	264	6.03	6.03	10.05	10.05	-41.85	1856.0
46	266	-2259	164	254	0	-2292	255	6.03	6.03	10.05	10.05	-15.30	576.4
47	266	-1938	159	217	0	-1964	250	6.03	6.03	10.05	10.05	-13.11	493.7
49	266	-2175	231	244	0	-2163	328	6.03	6.03	10.05	10.05	-14.44	540.7
50	266	-1904	92	211	0	-1959	179	6.03	6.03	10.05	10.05	-13.07	494.6
51	266	-1963	160	-215	0	-2678	251	6.03	6.03	10.05	10.05	-17.78	724.2

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	354	-3720	403	484	0	-4633	863	6.03	6.03	10.05	10.05	-30.81	1228.2
41	354	-3010	187	402	0	-3964	439	6.03	6.03	10.05	10.05	-26.34	1063.9
42	354	-3084	191	-1218	0	-4816	444	6.03	6.03	10.05	10.05	-31.90	1336.1

43	354	-3392	534	445	0	-4175	1122	6.03	6.03	10.05	10.05	-27.77	1103.8
44	354	-2039	-160	282	0	-3011	-237	6.03	6.03	10.05	10.05	-19.96	826.9
45	354	-2332	180	-2391	0	-4479	423	6.03	6.03	10.05	10.05	-29.56	1283.7
46	354	-1728	164	254	0	-2517	400	6.03	6.03	10.05	10.05	-16.69	689.5
47	354	-1407	159	217	0	-2156	391	6.03	6.03	10.05	10.05	-14.29	596.1
49	354	-1644	231	244	0	-2379	532	6.03	6.03	10.05	10.05	-15.78	650.8
50	354	-1373	92	211	0	-2146	260	6.03	6.03	10.05	10.05	-14.21	595.5
51	354	-1432	160	-323	0	-2440	392	6.03	6.03	10.05	10.05	-16.14	686.9

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

ASTA NUM. 43 NI 39 NF 44 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 22D
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-5770	-556	771	0	-1285	148	6.03	6.03	10.05	10.05	-8.00	-102.8
41	0	-5805	-644	734	0	-1476	359	6.03	6.03	10.05	10.05	-9.32	-117.2
42	0	-5841	-661	53	0	-4637	374	6.03	6.03	10.05	10.05	-31.05	1072.2
43	0	-4957	-525	634	0	-789	55	6.03	6.03	10.05	10.05	-4.96	-66.5
44	0	-6094	-803	701	0	-1866	718	6.03	6.03	10.05	10.05	-12.05	194.6
45	0	-5076	-700	-563	0	-6375	433	6.03	6.03	10.05	10.05	-42.39	1693.2
46	0	-4543	-690	475	0	-886	437	6.03	6.03	10.05	10.05	-5.48	-71.7
47	0	-4228	-701	410	0	-738	456	6.03	6.03	10.05	10.05	-4.59	-60.9
49	0	-4216	-672	423	0	-674	386	6.03	6.03	10.05	10.05	-4.24	-56.7
50	0	-4443	-727	436	0	-890	518	6.03	6.03	10.05	10.05	-5.51	-71.9
51	0	-4240	-707	183	0	-1792	461	6.03	6.03	10.05	10.05	-11.89	279.0

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	53	-5453	-556	771	0	-1693	-146	6.03	6.03	10.05	10.05	-10.95	180.4
41	53	-5488	-644	734	0	-1864	19	6.03	6.03	10.05	10.05	-12.17	226.3
42	53	-5524	-661	-141	0	-4614	25	6.03	6.03	10.05	10.05	-30.88	1087.9
43	53	-4640	-525	634	0	-1124	-222	6.03	6.03	10.05	10.05	-7.06	-89.5
44	53	-5777	-803	701	0	-2236	293	6.03	6.03	10.05	10.05	-14.76	318.3
45	53	-4759	-700	-885	0	-5992	62	6.03	6.03	10.05	10.05	-39.84	1592.5
46	53	-4226	-690	475	0	-1137	72	6.03	6.03	10.05	10.05	-7.23	94.4
47	53	-3911	-701	410	0	-955	85	6.03	6.03	10.05	10.05	-6.00	-76.0
49	53	-3899	-672	423	0	-898	31	6.03	6.03	10.05	10.05	-5.61	-71.7
50	53	-4126	-727	436	0	-1120	134	6.03	6.03	10.05	10.05	-7.13	94.7
51	53	-3923	-707	119	0	-1872	88	6.03	6.03	10.05	10.05	-12.48	324.0

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	106	-5136	-556	771	0	-2100	-440	6.03	6.03	10.05	10.05	-13.91	316.7
41	106	-5170	-644	734	0	-2252	-322	6.03	6.03	10.05	10.05	-14.97	360.8
42	106	-5206	-661	-334	0	-4488	-325	6.03	6.03	10.05	10.05	-30.03	1070.5
43	106	-4322	-525	634	0	-1459	-500	6.03	6.03	10.05	10.05	-9.52	175.6
44	106	-5460	-803	701	0	-2607	-132	6.03	6.03	10.05	10.05	-17.39	451.6
45	106	-4442	-700	-1208	0	-5439	-308	6.03	6.03	10.05	10.05	-36.18	1436.2
46	106	-3908	-690	475	0	-1388	-293	6.03	6.03	10.05	10.05	-9.10	178.5
47	106	-3594	-701	410	0	-1172	-285	6.03	6.03	10.05	10.05	-7.62	134.5
49	106	-3582	-672	423	0	-1121	-325	6.03	6.03	10.05	10.05	-7.26	121.0
50	106	-3808	-727	436	0	-1351	-251	6.03	6.03	10.05	10.05	-8.85	173.5
51	106	-3606	-707	54	0	-1917	-286	6.03	6.03	10.05	10.05	-12.82	359.5

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	159	-4818	-556	771	0	-2508	-733	6.03	6.03	10.05	10.05	-16.77	463.5
41	159	-4853	-644	734	0	-2641	-662	6.03	6.03	10.05	10.05	-17.67	502.8
42	159	-4889	-661	-528	0	-4260	-674	6.03	6.03	10.05	10.05	-28.50	1020.0
43	159	-4005	-525	634	0	-1794	-777	6.03	6.03	10.05	10.05	-11.93	294.6
44	159	-5142	-803	701	0	-2977	-556	6.03	6.03	10.05	10.05	-19.94	589.6
45	159	-4124	-700	-1530	0	-4715	-679	6.03	6.03	10.05	10.05	-31.40	1224.4
46	159	-3591	-690	475	0	-1639	-657	6.03	6.03	10.05	10.05	-10.91	273.5
47	159	-3276	-701	410	0	-1389	-656	6.03	6.03	10.05	10.05	-9.22	216.9
49	159	-3264	-672	423	0	-1345	-680	6.03	6.03	10.05	10.05	-8.91	204.2
50	159	-3491	-727	436	0	-1581	-635	6.03	6.03	10.05	10.05	-10.53	262.2
51	159	-3288	-707	-10	0	-1929	-659	6.03	6.03	10.05	10.05	-12.92	384.9

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	211	-4501	-556	771	0	-2916	-1027	6.03	6.03	10.05	10.05	-19.54	614.9
41	211	-4536	-644	734	0	-3029	-1003	6.03	6.03	10.05	10.05	-20.30	648.6
42	211	-4572	-661	-721	0	-3930	-1024	6.03	6.03	10.05	10.05	-26.29	936.4
43	211	-3688	-525	634	0	-2129	-1055	6.03	6.03	10.05	10.05	-14.26	420.8
44	211	-4825	-803	701	0	-3348	-981	6.03	6.03	10.05	10.05	-22.44	730.4
45	211	-3807	-700	-1853	0	-3820	-1049	6.03	6.03	10.05	10.05	-25.50	957.3
46	211	-3274	-690	475	0	-1890	-1022	6.03	6.03	10.05	10.05	-12.66	373.6
47	211	-2959	-701	410	0	-1606	-1027	6.03	6.03	10.05	10.05	-10.75	305.3
49	211	-2947	-672	423	0	-1568	-1035	6.03	6.03	10.05	10.05	-10.49	294.1
50	211	-3174	-727	436	0	-1812	-1020	6.03	6.03	10.05	10.05	-12.13	355.8
51	211	-2971	-707	-75	0	-1906	-1033	6.03	6.03	10.05	10.05	-12.77	399.9

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

ASTA NUM. 44 NI 295 NF 261 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 10E
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-4802	-373	-593	0	-1671	1050	6.03	6.03	10.05	10.05	-10.93	209.4
41	0	-4033	-386	-520	0	-1466	1088	6.03	6.03	10.05	10.05	-9.64	194.1
42	0	-4001	-376	-380	0	-492	1058	6.03	6.03	10.05	10.05	-9.37	159.1
43	0	-4883	-292	-530	0	-1492	821	6.03	6.03	10.05	10.05	-9.63	155.1
44	0	-3093	-405	-420	0	-1183	1139	6.03	6.03	10.05	10.05	-10.10	220.3
45	0	-3550	-297	-174	0	473	835	6.03	6.03	10.05	10.05	-7.38	110.9
46	0	-3343	-270	-341	0	-960	761	6.03	6.03	10.05	10.05	-6.72	97.3

47	0	-3171	-242	-296	0	-834	680	6.03	6.03	10.05	10.05	-5.99	80.4
49	0	-3427	-237	-320	0	-902	667	6.03	6.03	10.05	10.05	-5.86	71.7
50	0	-3069	-260	-298	0	-840	731	6.03	6.03	10.05	10.05	-6.46	98.5
51	0	-3160	-238	-249	0	-509	670	6.03	6.03	10.05	10.05	-5.90	78.1

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	58	-4455	-373	-593	0	-1328	834	6.03	6.03	10.05	10.05	-8.55	132.5
41	58	-3686	-386	-520	0	-1165	864	6.03	6.03	10.05	10.05	-7.64	127.6
42	58	-3654	-376	-278	0	-302	841	6.03	6.03	10.05	10.05	-7.43	108.8
43	58	-4536	-292	-530	0	-1186	652	6.03	6.03	10.05	10.05	-7.51	-94.0
44	58	-2746	-405	-420	0	-940	905	6.03	6.03	10.05	10.05	-8.03	163.0
45	58	-3203	-297	-4	0	523	663	6.03	6.03	10.05	10.05	-5.84	74.8
46	58	-2996	-270	-341	0	-763	605	6.03	6.03	10.05	10.05	-5.32	65.7
47	58	-2824	-242	-296	0	-662	540	6.03	6.03	10.05	10.05	-4.74	53.9
49	58	-3080	-237	-320	0	-717	530	6.03	6.03	10.05	10.05	-4.64	-57.2
50	58	-2722	-260	-298	0	-668	581	6.03	6.03	10.05	10.05	-5.12	68.2
51	58	-2813	-238	-215	0	-375	532	6.03	6.03	10.05	10.05	-4.67	-52.6

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	116	-4108	-373	-593	0	-985	618	6.03	6.03	10.05	10.05	-6.18	-78.4
41	116	-3339	-386	-520	0	-864	641	6.03	6.03	10.05	10.05	-5.63	-68.5
42	116	-3307	-376	-190	0	-168	623	6.03	6.03	10.05	10.05	-5.47	-61.6
43	116	-4189	-292	-530	0	-879	483	6.03	6.03	10.05	10.05	-5.45	-70.7
44	116	-2399	-405	-420	0	-697	671	6.03	6.03	10.05	10.05	-5.95	106.3
45	116	-2856	-297	143	0	482	492	6.03	6.03	10.05	10.05	-4.30	-49.5
46	116	-2649	-270	-341	0	-566	448	6.03	6.03	10.05	10.05	-3.92	-45.4
47	116	-2477	-242	-296	0	-491	400	6.03	6.03	10.05	10.05	-3.49	-40.8
49	116	-2733	-237	-320	0	-532	393	6.03	6.03	10.05	10.05	-3.43	-43.1
50	116	-2375	-260	-298	0	-495	430	6.03	6.03	10.05	10.05	-3.77	-42.9
51	116	-2466	-238	-186	0	-259	395	6.03	6.03	10.05	10.05	-3.44	-40.3

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	173	-3761	-373	-593	0	-642	403	6.03	6.03	10.05	10.05	-4.00	-53.1
41	173	-2992	-386	-520	0	-563	417	6.03	6.03	10.05	10.05	-3.64	-45.8
42	173	-2960	-376	-117	0	-80	406	6.03	6.03	10.05	10.05	-3.54	-42.8
43	173	-3842	-292	-530	0	-573	315	6.03	6.03	10.05	10.05	-3.65	-49.2
44	173	-2052	-405	-420	0	-454	437	6.03	6.03	10.05	10.05	-3.85	51.3
45	173	-2509	-297	264	0	363	320	6.03	6.03	10.05	10.05	-2.81	-34.3
46	173	-2302	-270	-341	0	-369	292	6.03	6.03	10.05	10.05	-2.56	-31.3
47	173	-2130	-242	-296	0	-320	261	6.03	6.03	10.05	10.05	-2.29	-28.2
49	173	-2386	-237	-320	0	-346	256	6.03	6.03	10.05	10.05	-2.29	-30.0
50	173	-2028	-260	-298	0	-323	280	6.03	6.03	10.05	10.05	-2.45	-29.5
51	173	-2119	-238	-161	0	-159	257	6.03	6.03	10.05	10.05	-2.26	-27.9

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	231	-3414	-373	-593	0	-298	187	6.03	6.03	10.05	10.05	-2.40	-33.3
41	231	-2645	-386	-520	0	-262	194	6.03	6.03	10.05	10.05	-1.98	-27.2
42	231	-2613	-376	-59	0	-30	188	6.03	6.03	10.05	10.05	-1.94	-25.4
43	231	-3495	-292	-530	0	-266	146	6.03	6.03	10.05	10.05	-2.31	-32.3
44	231	-1705	-405	-420	0	-211	203	6.03	6.03	10.05	10.05	-1.79	-22.2
45	231	-2162	-297	362	0	181	149	6.03	6.03	10.05	10.05	-1.57	-20.7
46	231	-1955	-270	-341	0	-171	136	6.03	6.03	10.05	10.05	-1.42	-19.1
47	231	-1783	-242	-296	0	-149	121	6.03	6.03	10.05	10.05	-1.28	-17.1
49	231	-2039	-237	-320	0	-161	119	6.03	6.03	10.05	10.05	-1.37	-19.1
50	231	-1681	-260	-298	0	-150	130	6.03	6.03	10.05	10.05	-1.30	-16.9
51	231	-1772	-238	-142	0	-72	119	6.03	6.03	10.05	10.05	-1.27	-16.8

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

ASTA NUM. 45 NI 297 NF 260 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 15D
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-8854	-70	24	0	96	282	6.03	6.03	10.05	10.05	-4.73	-65.5
41	0	-8480	-23	32	0	130	93	6.03	6.03	10.05	10.05	-3.75	-55.1
42	0	-8325	-22	17	0	1293	87	6.03	6.03	10.05	10.05	-8.17	-109.7
43	0	-7800	-95	14	0	55	382	6.03	6.03	10.05	10.05	-4.86	-65.5
44	0	-8089	57	47	0	191	-229	6.03	6.03	10.05	10.05	-4.17	-58.2
45	0	-6918	-14	3	0	2050	58	6.03	6.03	10.05	10.05	-13.19	202.7
46	0	-6396	-13	25	0	101	53	6.03	6.03	10.05	10.05	-2.84	-41.7
47	0	-5875	-11	23	0	94	43	6.03	6.03	10.05	10.05	-2.62	-38.4
49	0	-6000	-26	21	0	83	106	6.03	6.03	10.05	10.05	-2.77	-39.5
50	0	-6058	4	27	0	110	-16	6.03	6.03	10.05	10.05	-2.74	-40.2
51	0	-5823	-10	18	0	482	41	6.03	6.03	10.05	10.05	-3.99	-55.5

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	88	-8323	-70	24	0	75	220	6.03	6.03	10.05	10.05	-4.22	-59.0
41	88	-7949	-23	32	0	102	73	6.03	6.03	10.05	10.05	-3.45	-50.8
42	88	-7794	-22	174	0	1207	68	6.03	6.03	10.05	10.05	-7.63	-102.4
43	88	-7269	-95	14	0	43	298	6.03	6.03	10.05	10.05	-4.23	-57.7
44	88	-7558	57	47	0	149	-179	6.03	6.03	10.05	10.05	-3.72	-52.3
45	88	-6387	-14	264	0	1929	45	6.03	6.03	10.05	10.05	-12.44	196.9
46	88	-5865	-13	25	0	79	42	6.03	6.03	10.05	10.05	-2.56	-37.6
47	88	-5344	-11	23	0	73	34	6.03	6.03	10.05	10.05	-2.33	-34.4
49	88	-5469	-26	21	0	64	83	6.03	6.03	10.05	10.05	-2.45	-35.2
50	88	-5527	4	27	0	86	-13	6.03	6.03	10.05	10.05	-2.45	-36.0
51	88	-5292	-10	71	0	442	32	6.03	6.03	10.05	10.05	-3.64	-50.6

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	177	-7792	-70	24	0	54	158	6.03	6.03	10.05	10.05	-3.70	-52.4
41	177	-7418	-23	32	0	73	53	6.03	6.03	10.05	10.05	-3.14	-46.4
42	177	-7263	-22	308	0	992	49	6.03	6.03	10.05	10.05	-6.47	-87.8
43	177	-6738	-95	14	0	31	215	6.03	6.03	10.05	10.05	-3.60	-49.9
44	177	-7027	57	47	0	107	-128	6.03	6.03	10.05	10.05	-3.26	-46.5
45	177	-5856	-14	488	0	1594	33	6.03	6.03	10.05	10.05	-10.15	135.3
46	177	-5334	-13	25	0	57	30	6.03	6.03	10.05	10.05	-2.27	-33.6
47	177	-4813	-11	23	0	53	24	6.03	6.03	10.05	10.05	-2.05	-30.3

49	177	-4938	-26	21	0	46	59	6.03	6.03	10.05	10.05	-2.13	-30.9
50	177	-4996	4	27	0	62	-9	6.03	6.03	10.05	10.05	-2.16	-31.8
51	177	-4761	-10	115	0	359	23	6.03	6.03	10.05	10.05	-3.14	-43.8

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	266	-7261	-70	24	0	32	97	6.03	6.03	10.05	10.05	-3.19	-45.9
41	266	-6887	-23	32	0	44	32	6.03	6.03	10.05	10.05	-2.83	-42.0
42	266	-6732	-22	420	0	668	30	6.03	6.03	10.05	10.05	-5.01	-69.2
43	266	-6207	-95	14	0	18	131	6.03	6.03	10.05	10.05	-2.97	-42.1
44	266	-6496	57	47	0	65	-78	6.03	6.03	10.05	10.05	-2.81	-40.7
45	266	-5325	-14	674	0	1077	20	6.03	6.03	10.05	10.05	-6.67	-86.9
46	266	-4803	-13	25	0	34	18	6.03	6.03	10.05	10.05	-1.98	-29.5
47	266	-4282	-11	23	0	32	15	6.03	6.03	10.05	10.05	-1.77	-26.3
49	266	-4407	-26	21	0	28	36	6.03	6.03	10.05	10.05	-1.82	-26.9
50	266	-4465	4	27	0	37	-6	6.03	6.03	10.05	10.05	-1.86	-27.6
51	266	-4230	-10	153	0	240	14	6.03	6.03	10.05	10.05	-2.50	-35.4

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	354	-6730	-70	24	0	11	35	6.03	6.03	10.05	10.05	-2.67	-39.6
41	354	-6356	-23	32	0	15	12	6.03	6.03	10.05	10.05	-2.52	-37.6
42	354	-6201	-22	509	0	255	11	6.03	6.03	10.05	10.05	-3.32	-47.5
43	354	-5676	-95	14	0	6	47	6.03	6.03	10.05	10.05	-2.34	-34.2
44	354	-5965	57	47	0	23	-28	6.03	6.03	10.05	10.05	-2.39	-35.7
45	354	-4794	-14	823	0	412	7	6.03	6.03	10.05	10.05	-3.34	-46.4
46	354	-4272	-13	25	0	12	7	6.03	6.03	10.05	10.05	-1.70	-25.4
47	354	-3751	-11	23	0	11	5	6.03	6.03	10.05	10.05	-1.49	-22.3
49	354	-3876	-26	21	0	10	13	6.03	6.03	10.05	10.05	-1.54	-23.0
50	354	-3934	4	27	0	13	-2	6.03	6.03	10.05	10.05	-1.57	-23.5
51	354	-3699	-10	182	0	91	5	6.03	6.03	10.05	10.05	-1.76	-25.6

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

ASTA NUM. 46 NI 271 NF 259 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 20D
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-5474	226	-670	0	-1755	-592	6.03	6.03	10.05	10.05	-11.39	196.4
41	0	-5665	220	-599	0	-1569	-576	6.03	6.03	10.05	10.05	-10.01	137.7
42	0	-5597	217	-414	0	-587	-568	6.03	6.03	10.05	10.05	-5.15	-65.3
43	0	-4571	189	-587	0	-1536	-494	6.03	6.03	10.05	10.05	-10.02	183.8
44	0	-6216	214	-504	0	-1319	-560	6.03	6.03	10.05	10.05	-8.19	-105.9
45	0	-4777	174	-159	0	412	-455	6.03	6.03	10.05	10.05	-4.19	-53.6
46	0	-4425	154	-389	0	-1019	-404	6.03	6.03	10.05	10.05	-6.37	-81.3
47	0	-4115	138	-337	0	-881	-360	6.03	6.03	10.05	10.05	-5.47	-70.7
49	0	-4051	140	-360	0	-943	-366	6.03	6.03	10.05	10.05	-5.90	-75.3
50	0	-4380	145	-344	0	-900	-379	6.03	6.03	10.05	10.05	-5.58	-72.5
51	0	-4092	137	-275	0	-554	-358	6.03	6.03	10.05	10.05	-3.63	-49.2

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	53	-5157	226	-670	0	-1400	-472	6.03	6.03	10.05	10.05	-8.92	118.4
41	53	-5348	220	-599	0	-1252	-460	6.03	6.03	10.05	10.05	-7.83	-99.8
42	53	-5280	217	-320	0	-393	-453	6.03	6.03	10.05	10.05	-4.32	-55.9
43	53	-4254	189	-587	0	-1226	-395	6.03	6.03	10.05	10.05	-7.86	115.5
44	53	-5899	214	-504	0	-1053	-447	6.03	6.03	10.05	10.05	-6.53	-86.4
45	53	-4460	174	-3	0	453	-363	6.03	6.03	10.05	10.05	-3.53	-46.3
46	53	-4108	154	-389	0	-813	-322	6.03	6.03	10.05	10.05	-5.03	-65.7
47	53	-3798	138	-337	0	-703	-287	6.03	6.03	10.05	10.05	-4.35	-57.4
49	53	-3734	140	-360	0	-753	-292	6.03	6.03	10.05	10.05	-4.66	-60.7
50	53	-4063	145	-344	0	-718	-302	6.03	6.03	10.05	10.05	-4.46	-59.1
51	53	-3775	137	-244	0	-417	-285	6.03	6.03	10.05	10.05	-2.96	-40.7

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	106	-4840	226	-670	0	-1046	-353	6.03	6.03	10.05	10.05	-6.50	-83.9
41	106	-5030	220	-599	0	-935	-343	6.03	6.03	10.05	10.05	-5.79	-76.3
42	106	-4962	217	-240	0	-246	-338	6.03	6.03	10.05	10.05	-3.58	-47.2
43	106	-3936	189	-587	0	-915	-295	6.03	6.03	10.05	10.05	-5.72	-73.0
44	106	-5582	214	-504	0	-786	-333	6.03	6.03	10.05	10.05	-5.09	-68.8
45	106	-4142	174	131	0	418	-271	6.03	6.03	10.05	10.05	-3.11	-42.9
46	106	-3790	154	-389	0	-607	-240	6.03	6.03	10.05	10.05	-3.81	-51.1
47	106	-3480	138	-337	0	-525	-215	6.03	6.03	10.05	10.05	-3.34	-44.9
49	106	-3416	140	-360	0	-562	-218	6.03	6.03	10.05	10.05	-3.52	-47.0
50	106	-3746	145	-344	0	-536	-226	6.03	6.03	10.05	10.05	-3.45	-46.7
51	106	-3458	137	-217	0	-296	-213	6.03	6.03	10.05	10.05	-2.40	-33.4

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	159	-4522	226	-670	0	-691	-233	6.03	6.03	10.05	10.05	-4.38	-58.9
41	159	-4713	220	-599	0	-618	-227	6.03	6.03	10.05	10.05	-4.09	-55.6
42	159	-4645	217	-173	0	-137	-224	6.03	6.03	10.05	10.05	-2.87	-38.8
43	159	-3619	189	-587	0	-605	-195	6.03	6.03	10.05	10.05	-3.78	-50.3
44	159	-5264	214	-504	0	-520	-220	6.03	6.03	10.05	10.05	-3.91	-54.0
45	159	-3825	174	242	0	318	-179	6.03	6.03	10.05	10.05	-2.63	-36.6
46	159	-3473	154	-389	0	-401	-159	6.03	6.03	10.05	10.05	-2.79	-38.3
47	159	-3163	138	-337	0	-347	-142	6.03	6.03	10.05	10.05	-2.48	-34.0
49	159	-3099	140	-360	0	-372	-144	6.03	6.03	10.05	10.05	-2.55	-34.8
50	159	-3428	145	-344	0	-355	-149	6.03	6.03	10.05	10.05	-2.61	-35.9
51	159	-3140	137	-195	0	-187	-141	6.03	6.03	10.05	10.05	-1.89	-26.7

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	211	-4205	226	-670	0	-337	-114	6.03	6.03	10.05	10.05	-2.84	-39.6
41	211	-4396	220	-599	0	-301	-110	6.03	6.03	10.05	10.05	-2.79	-39.1
42	211	-4328	217	-120	0	-61	-109	6.03	6.03	10.05	10.05	-2.16	-30.3
43	211	-3302	189	-587	0	-295	-95	6.03	6.03	10.05	10.05	-2.34	-32.5
44	211	-4947	214	-504	0	-253	-107	6.03	6.03	10.05	10.05	-2.83	-40.2
45	211	-3508	174	331	0	166	-87	6.03	6.03	10.05	10.05	-1.96	-27.9
46	211	-3156	154	-389	0	-196	-77	6.03	6.03	10.05	10.05	-1.93	-27.1
47	211	-2846	138	-337	0	-169	-69	6.03	6.03	10.05	10.05	-1.71	-24.2
49	211	-2782	140	-360	0	-181	-70	6.03	6.03	10.05	10.05	-1.73	-24.3

50	211	-3111	145	-344	0	-173	-72	6.03	6.03	10.05	10.05	-1.83	-25.9
51	211	-2823	137	-177	0	-89	-68	6.03	6.03	10.05	10.05	-1.41	-20.4

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

ASTA NUM. 47 NI 129 NF 124 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 9B
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-9974	110	-239	0	-437	-492	6.03	6.03	10.05	10.05	-6.23	-83.9
41	0	-9913	-32	-126	0	-226	11	6.03	6.03	10.05	10.05	-4.65	-67.8
42	0	-9858	-33	-218	0	-426	15	6.03	6.03	10.05	10.05	-5.35	-76.5
43	0	-9687	212	-280	0	-519	-852	6.03	6.03	10.05	10.05	-8.05	-103.9
44	0	-9545	-268	45	0	101	853	6.03	6.03	10.05	10.05	-8.02	-103.3
45	0	-9494	-26	-245	0	-500	-7	6.03	6.03	10.05	10.05	-5.48	-77.7
46	0	-9388	-18	-72	0	-130	-29	6.03	6.03	10.05	10.05	-4.10	-60.4
47	0	-9257	-15	-58	0	-106	-38	6.03	6.03	10.05	10.05	-3.97	-58.6
49	0	-9278	32	-96	0	-176	-206	6.03	6.03	10.05	10.05	-4.50	-63.5
50	0	-9249	-64	-31	0	-53	135	6.03	6.03	10.05	10.05	-4.12	-59.2
51	0	-9239	-15	-89	0	-173	-37	6.03	6.03	10.05	10.05	-4.20	-61.5

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	97	-9389	110	-239	0	-205	-386	6.03	6.03	10.05	10.05	-5.46	-74.5
41	97	-9328	-32	-126	0	-102	-20	6.03	6.03	10.05	10.05	-3.98	-58.8
42	97	-9273	-33	-218	0	-214	-18	6.03	6.03	10.05	10.05	-4.36	-63.5
43	97	-9102	212	-280	0	-246	-645	6.03	6.03	10.05	10.05	-6.70	-88.0
44	97	-8960	-268	45	0	57	591	6.03	6.03	10.05	10.05	-6.37	-84.1
45	97	-8909	-26	-245	0	-261	-32	6.03	6.03	10.05	10.05	-4.39	-63.5
46	97	-8803	-18	-72	0	-60	-46	6.03	6.03	10.05	10.05	-3.63	-53.8
47	97	-8672	-15	-58	0	-49	-53	6.03	6.03	10.05	10.05	-3.54	-52.6
49	97	-8693	32	-96	0	-83	-174	6.03	6.03	10.05	10.05	-4.12	-58.4
50	97	-8664	-64	-31	0	-22	73	6.03	6.03	10.05	10.05	-3.58	-52.3
51	97	-8654	-15	-89	0	-86	-52	6.03	6.03	10.05	10.05	-3.66	-54.2

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	195	-8804	110	-239	0	28	-279	6.03	6.03	10.05	10.05	-4.70	-65.1
41	195	-8743	-32	-126	0	21	-51	6.03	6.03	10.05	10.05	-3.50	-51.8
42	195	-8688	-33	-218	0	-1	-50	6.03	6.03	10.05	10.05	-3.48	-51.2
43	195	-8517	212	-280	0	26	-439	6.03	6.03	10.05	10.05	-5.41	-72.7
44	195	-8375	-268	45	0	14	330	6.03	6.03	10.05	10.05	-4.80	-65.6
45	195	-8324	-26	-245	0	-22	-57	6.03	6.03	10.05	10.05	-3.38	-49.5
46	195	-8218	-18	-72	0	11	-64	6.03	6.03	10.05	10.05	-3.37	-49.3
47	195	-8087	-15	-58	0	8	-67	6.03	6.03	10.05	10.05	-3.34	-48.8
49	195	-8108	32	-96	0	10	-143	6.03	6.03	10.05	10.05	-3.74	-53.3
50	195	-8079	-64	-31	0	8	11	6.03	6.03	10.05	10.05	-3.16	-47.3
51	195	-8069	-15	-89	0	1	-67	6.03	6.03	10.05	10.05	-3.33	-48.7

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	292	-8219	110	-239	0	261	-172	6.03	6.03	10.05	10.05	-4.12	-59.5
41	292	-8158	-32	-126	0	144	-82	6.03	6.03	10.05	10.05	-3.68	-53.9
42	292	-8103	-33	-218	0	212	-83	6.03	6.03	10.05	10.05	-3.90	-56.6
43	292	-7932	212	-280	0	299	-232	6.03	6.03	10.05	10.05	-4.15	-59.6
44	292	-7790	-268	45	0	-30	68	6.03	6.03	10.05	10.05	-3.23	-47.2
45	292	-7739	-26	-245	0	217	-83	6.03	6.03	10.05	10.05	-3.78	-54.7
46	292	-7633	-18	-72	0	81	-81	6.03	6.03	10.05	10.05	-3.25	-48.0
47	292	-7502	-15	-58	0	65	-81	6.03	6.03	10.05	10.05	-3.20	-46.5
49	292	-7523	32	-96	0	104	-111	6.03	6.03	10.05	10.05	-3.36	-48.4
50	292	-7494	-64	-31	0	38	-51	6.03	6.03	10.05	10.05	-3.04	-45.3
51	292	-7484	-15	-89	0	87	-81	6.03	6.03	10.05	10.05	-3.21	-47.4

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	390	-7634	110	-239	0	494	-66	6.03	6.03	10.05	10.05	-4.74	-66.6
41	390	-7573	-32	-126	0	268	-113	6.03	6.03	10.05	10.05	-3.90	-56.1
42	390	-7518	-33	-218	0	424	-115	6.03	6.03	10.05	10.05	-4.44	-62.8
43	390	-7347	212	-280	0	572	-25	6.03	6.03	10.05	10.05	-4.91	-68.4
44	390	-7205	-268	45	0	-73	-194	6.03	6.03	10.05	10.05	-3.67	-51.3
45	390	-7154	-26	-245	0	456	-108	6.03	6.03	10.05	10.05	-4.41	-62.1
46	390	-7048	-18	-72	0	151	-99	6.03	6.03	10.05	10.05	-3.27	-47.8
47	390	-6917	-15	-58	0	122	-96	6.03	6.03	10.05	10.05	-3.12	-45.7
49	390	-6938	32	-96	0	197	-80	6.03	6.03	10.05	10.05	-3.40	-49.2
50	390	-6909	-64	-31	0	68	-113	6.03	6.03	10.05	10.05	-3.14	-44.9
51	390	-6899	-15	-89	0	174	-96	6.03	6.03	10.05	10.05	-3.30	-47.9

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

ASTA NUM. 48 NI 128 NF 125 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 14B
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-16060	163	-481	0	-797	-421	6.03	6.03	10.05	10.05	-9.09	-129.2
41	0	-16020	4	-434	0	-728	10	6.03	6.03	10.05	10.05	-8.83	-125.9
42	0	-15970	5	-570	0	-962	7	6.03	6.03	10.05	10.05	-9.65	-136.1
43	0	-15480	274	-434	0	-723	-721	6.03	6.03	10.05	10.05	-9.45	-127.8
44	0	-15420	-262	-374	0	-636	730	6.03	6.03	10.05	10.05	-9.47	-127.9
45	0	-15320	11	-582	0	-998	-8	6.03	6.03	10.05	10.05	-9.53	-134.0
46	0	-15030	12	-309	0	-537	-11	6.03	6.03	10.05	10.05	-7.76	-111.5
47	0	-14790	14	-277	0	-490	-16	6.03	6.03	10.05	10.05	-7.49	-108.0
49	0	-14800	67	-293	0	-512	-160	6.03	6.03	10.05	10.05	-7.58	-109.1
50	0	-14790	-40	-281	0	-495	130	6.03	6.03	10.05	10.05	-7.51	-108.2
51	0	-14770	15	-322	0	-567	-17	6.03	6.03	10.05	10.05	-7.77	-111.4

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	97	-15475	163	-481	0	-328	-262	6.03	6.03	10.05	10.05	-7.18	-104.7
41	97	-15435	4	-434	0	-305	14	6.03	6.03	10.05	10.05	-7.08	-103.4
42	97	-15385	5	-570	0	-406	12	6.03	6.03	10.05	10.05	-7.42	-107.7
43	97	-14895	274	-434	0	-300	-454	6.03	6.03	10.05	10.05	-7.85	-109.0
44	97	-14835	-262	-374	0	-272	474	6.03	6.03	10.05	10.05	-7.94	-109.9
45	97	-14735	11	-582	0	-431	3	6.03	6.03	10.05	10.05	-7.26	-105.0
46	97	-14445	12	-309	0	-236	1	6.03	6.03	10.05	10.05	-6.45	-94.6
47	97	-14205	14	-277	0	-219	-2	6.03	6.03	10.05	10.05	-6.29	-92.4
49	97	-14215	67	-293	0	-227	-94	6.03	6.03	10.05	10.05	-6.32	-92.8
50	97	-14205	-40	-281	0	-221	91	6.03	6.03	10.05	10.05	-6.30	-92.5
51	97	-14185	15	-322	0	-253	-3	6.03	6.03	10.05	10.05	-6.41	-93.8

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	195	-14890	163	-481	0	141	-103	6.03	6.03	10.05	10.05	-6.28	-92.9
41	195	-14850	4	-434	0	118	18	6.03	6.03	10.05	10.05	-6.18	-91.6
42	195	-14800	5	-570	0	149	17	6.03	6.03	10.05	10.05	-6.27	-92.7
43	195	-14310	274	-434	0	123	-186	6.03	6.03	10.05	10.05	-6.26	-90.2
44	195	-14250	-262	-374	0	93	219	6.03	6.03	10.05	10.05	-6.40	-91.8
45	195	-14150	11	-582	0	136	14	6.03	6.03	10.05	10.05	-5.97	-88.4
46	195	-13860	12	-309	0	65	13	6.03	6.03	10.05	10.05	-5.60	-83.5
47	195	-13620	14	-277	0	51	12	6.03	6.03	10.05	10.05	-5.46	-81.5
49	195	-13630	67	-293	0	59	-28	6.03	6.03	10.05	10.05	-5.49	-81.9
50	195	-13620	-40	-281	0	53	52	6.03	6.03	10.05	10.05	-5.47	-81.5
51	195	-13600	15	-322	0	62	11	6.03	6.03	10.05	10.05	-5.49	-81.8

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	292	-14305	163	-481	0	610	57	6.03	6.03	10.05	10.05	-7.74	-110.6
41	292	-14265	4	-434	0	542	22	6.03	6.03	10.05	10.05	-7.48	-107.3
42	292	-14215	5	-570	0	705	23	6.03	6.03	10.05	10.05	-8.04	-114.3
43	292	-13725	274	-434	0	545	82	6.03	6.03	10.05	10.05	-7.28	-104.3
44	292	-13665	-262	-374	0	458	-37	6.03	6.03	10.05	10.05	-6.94	-100.0
45	292	-13565	11	-582	0	704	25	6.03	6.03	10.05	10.05	-7.79	-110.5
46	292	-13275	12	-309	0	365	25	6.03	6.03	10.05	10.05	-6.46	-93.6
47	292	-13035	14	-277	0	321	25	6.03	6.03	10.05	10.05	-6.21	-90.2
49	292	-13045	67	-293	0	344	37	6.03	6.03	10.05	10.05	-6.29	-91.3
50	292	-13035	-40	-281	0	327	13	6.03	6.03	10.05	10.05	-6.23	-90.5
51	292	-13015	15	-322	0	376	26	6.03	6.03	10.05	10.05	-6.40	-92.6

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	390	-13720	163	-481	0	1079	216	6.03	6.03	10.05	10.05	-9.20	-128.3
41	390	-13680	4	-434	0	965	26	6.03	6.03	10.05	10.05	-8.77	-122.9
42	390	-13630	5	-570	0	1260	28	6.03	6.03	10.05	10.05	-9.82	-135.9
43	390	-13140	274	-434	0	968	349	6.03	6.03	10.05	10.05	-8.58	-119.9
44	390	-13080	-262	-374	0	822	-292	6.03	6.03	10.05	10.05	-8.03	-113.0
45	390	-12980	11	-582	0	1271	36	6.03	6.03	10.05	10.05	-9.61	-132.6
46	390	-12690	12	-309	0	666	37	6.03	6.03	10.05	10.05	-7.32	-103.7
47	390	-12450	14	-277	0	592	39	6.03	6.03	10.05	10.05	-6.95	-99.0
49	390	-12460	67	-293	0	630	103	6.03	6.03	10.05	10.05	-7.10	-100.8
50	390	-12450	-40	-281	0	601	-26	6.03	6.03	10.05	10.05	-6.99	-99.4
51	390	-12430	15	-322	0	690	40	6.03	6.03	10.05	10.05	-7.30	-103.3

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

ASTA NUM. 49 NI 127 NF 126 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 19B
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-15810	153	-188	0	-300	-460	6.03	6.03	10.05	10.05	-8.22	-114.5
41	0	-15810	9	-217	0	-348	-47	6.03	6.03	10.05	10.05	-7.38	-107.6
42	0	-15740	10	-274	0	-457	-50	6.03	6.03	10.05	10.05	-7.75	-112.1
43	0	-15210	249	-132	0	-216	-735	6.03	6.03	10.05	10.05	-9.42	-127.1
44	0	-15300	-232	-276	0	-442	642	6.03	6.03	10.05	10.05	-8.97	-122.2
45	0	-15090	10	-275	0	-478	-52	6.03	6.03	10.05	10.05	-7.57	-109.2
46	0	-14860	8	-157	0	-264	-47	6.03	6.03	10.05	10.05	-6.71	-98.3
47	0	-14620	8	-142	0	-243	-47	6.03	6.03	10.05	10.05	-6.54	-95.9
49	0	-14620	56	-132	0	-228	-184	6.03	6.03	10.05	10.05	-6.48	-95.2
50	0	-14640	-40	-161	0	-272	91	6.03	6.03	10.05	10.05	-6.65	-97.4
51	0	-14600	9	-161	0	-280	-48	6.03	6.03	10.05	10.05	-6.66	-97.4

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	97	-15225	153	-188	0	-117	-311	6.03	6.03	10.05	10.05	-7.24	-102.6
41	97	-15225	9	-217	0	-137	-39	6.03	6.03	10.05	10.05	-6.39	-94.6
42	97	-15155	10	-274	0	-190	-40	6.03	6.03	10.05	10.05	-6.56	-96.6
43	97	-14625	249	-132	0	-87	-492	6.03	6.03	10.05	10.05	-7.95	-109.8
44	97	-14715	-232	-276	0	-173	416	6.03	6.03	10.05	10.05	-7.59	-105.8
45	97	-14505	10	-275	0	-209	-42	6.03	6.03	10.05	10.05	-6.37	-93.7
46	97	-14275	8	-157	0	-112	-39	6.03	6.03	10.05	10.05	-5.93	-88.0
47	97	-14035	8	-142	0	-105	-39	6.03	6.03	10.05	10.05	-5.82	-86.3
49	97	-14035	56	-132	0	-98	-130	6.03	6.03	10.05	10.05	-5.86	-86.0
50	97	-14055	-40	-161	0	-116	52	6.03	6.03	10.05	10.05	-5.86	-86.9
51	97	-14015	9	-161	0	-123	-39	6.03	6.03	10.05	10.05	-5.87	-87.0

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	195	-14640	153	-188	0	67	-162	6.03	6.03	10.05	10.05	-6.25	-90.7
41	195	-14640	9	-217	0	74	-30	6.03	6.03	10.05	10.05	-5.94	-88.4
42	195	-14570	10	-274	0	77	-31	6.03	6.03	10.05	10.05	-5.92	-88.2
43	195	-14040	249	-132	0	42	-250	6.03	6.03	10.05	10.05	-6.48	-92.4
44	195	-14130	-232	-276	0	96	190	6.03	6.03	10.05	10.05	-6.21	-89.5
45	195	-13920	10	-275	0	59	-32	6.03	6.03	10.05	10.05	-5.60	-83.5
46	195	-13690	8	-157	0	41	-31	6.03	6.03	10.05	10.05	-5.45	-81.4
47	195	-13450	8	-142	0	33	-31	6.03	6.03	10.05	10.05	-5.33	-79.7
49	195	-13450	56	-132	0	31	-75	6.03	6.03	10.05	10.05	-5.36	-79.5
50	195	-13470	-40	-161	0	42	13	6.03	6.03	10.05	10.05	-5.37	-80.2
51	195	-13430	9	-161	0	34	-31	6.03	6.03	10.05	10.05	-5.33	-79.6

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	292	-14055	153	-188	0	251	-13	6.03	6.03	10.05	10.05	-6.35	-93.0
41	292	-14055	9	-217	0	286	-22	6.03	6.03	10.05	10.05	-6.47	-94.6
42	292	-13985	10	-274	0	345	-21	6.03	6.03	10.05	10.05	-6.66	-96.8
43	292	-13455	249	-132	0	170	-7	6.03	6.03	10.05	10.05	-5.83	-85.9
44	292	-13545	-232	-276	0	365	-36	6.03	6.03	10.05	10.05	-6.56	-95.1
45	292	-13335	10	-275	0	327	-21	6.03	6.03	10.05	10.05	-6.34	-92.2
46	292	-13105	8	-157	0	194	-23	6.03	6.03	10.05	10.05	-5.78	-84.9
47	292	-12865	8	-142	0	171	-23	6.03	6.03	10.05	10.05	-5.60	-82.5
49	292	-12865	56	-132	0	160	-20	6.03	6.03	10.05	10.05	-5.56	-82.0
50	292	-12885	-40	-161	0	198	-26	6.03	6.03	10.05	10.05	-5.71	-83.8
51	292	-12845	9	-161	0	191	-23	6.03	6.03	10.05	10.05	-5.66	-83.2

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	390	-13470	153	-188	0	435	136	6.03	6.03	10.05	10.05	-6.78	-97.9
41	390	-13470	9	-217	0	497	-13	6.03	6.03	10.05	10.05	-7.01	-100.7
42	390	-13400	10	-274	0	612	-11	6.03	6.03	10.05	10.05	-7.40	-105.4
43	390	-12870	249	-132	0	299	235	6.03	6.03	10.05	10.05	-6.06	-88.3
44	390	-12960	-232	-276	0	634	-263	6.03	6.03	10.05	10.05	-7.30	-103.8
45	390	-12750	10	-275	0	595	-11	6.03	6.03	10.05	10.05	-7.08	-100.9
46	390	-12520	8	-157	0	347	-14	6.03	6.03	10.05	10.05	-6.10	-88.4
47	390	-12280	8	-142	0	309	-15	6.03	6.03	10.05	10.05	-5.87	-85.3
49	390	-12280	56	-132	0	289	35	6.03	6.03	10.05	10.05	-5.80	-84.4
50	390	-12300	-40	-161	0	356	-65	6.03	6.03	10.05	10.05	-6.05	-87.5
51	390	-12260	9	-161	0	348	-14	6.03	6.03	10.05	10.05	-6.00	-86.9

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

ASTA NUM. 50 NI 166 NF 167 SEZ. Rp B= 0.400 H= 0.600 (pilastro)
PIL. NUM. 26B
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-9179	-395	-221	0	-587	603	10.05	10.05	6.03	6.03	-6.42	-85.0
41	0	-8666	-648	-173	0	-499	1391	10.05	10.05	6.03	6.03	-8.74	-116.9
42	0	-8667	-658	-47	0	-224	1398	10.05	10.05	6.03	6.03	-8.77	-117.4
43	0	-9208	-96	-170	0	-479	-98	10.05	10.05	6.03	6.03	-5.88	-78.9
44	0	-7737	-1091	-120	0	-399	2735	10.05	10.05	6.03	6.03	-17.92	349.7
45	0	-8356	-535	121	0	126	1227	10.05	10.05	6.03	6.03	-7.85	-105.9
46	0	-8166	-439	-38	0	-232	1111	10.05	10.05	6.03	6.03	-7.26	-98.5
47	0	-8041	-386	-5	0	-166	1040	10.05	10.05	6.03	6.03	-6.92	-94.2
49	0	-8212	-302	-21	0	-195	778	10.05	10.05	6.03	6.03	-5.98	-82.7
50	0	-7918	-501	-11	0	-179	1344	10.05	10.05	6.03	6.03	-8.38	-111.5
51	0	-8042	-390	37	0	-74	1043	10.05	10.05	6.03	6.03	-6.93	-94.3

apost= 6.03 aant= 6.03 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	97	-8594	-395	-221	0	-371	218	10.05	10.05	6.03	6.03	-5.09	-69.2
41	97	-8081	-648	-173	0	-330	760	10.05	10.05	6.03	6.03	-5.87	-81.2
42	97	-8082	-658	-47	0	-178	756	10.05	10.05	6.03	6.03	-5.85	-81.0
43	97	-8623	-96	-170	0	-314	-192	10.05	10.05	6.03	6.03	-4.81	-66.1
44	97	-7152	-1091	-120	0	-282	1671	10.05	10.05	6.03	6.03	-10.46	-133.3
45	97	-7771	-535	121	0	9	706	10.05	10.05	6.03	6.03	-5.55	-76.9
46	97	-7581	-439	-38	0	-195	683	10.05	10.05	6.03	6.03	-5.40	-74.8
47	97	-7456	-386	-5	0	-161	663	10.05	10.05	6.03	6.03	-5.28	-73.2
49	97	-7627	-302	-21	0	-175	483	10.05	10.05	6.03	6.03	-4.69	-66.1
50	97	-7333	-501	-11	0	-168	855	10.05	10.05	6.03	6.03	-5.93	-81.2
51	97	-7457	-390	37	0	-110	663	10.05	10.05	6.03	6.03	-5.28	-73.2

apost= 6.03 aant= 6.03 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	195	-8009	-395	-221	0	-155	-167	10.05	10.05	6.03	6.03	-3.76	-54.1
41	195	-7496	-648	-173	0	-161	128	10.05	10.05	6.03	6.03	-3.61	-51.0
42	195	-7497	-658	-47	0	-131	114	10.05	10.05	6.03	6.03	-3.45	-49.2
43	195	-8038	-96	-170	0	-149	-286	10.05	10.05	6.03	6.03	-4.14	-59.6
44	195	-6567	-1091	-120	0	-164	608	10.05	10.05	6.03	6.03	-4.73	-65.5
45	195	-7186	-535	121	0	-109	184	10.05	10.05	6.03	6.03	-3.45	-50.1
46	195	-6996	-439	-38	0	-158	255	10.05	10.05	6.03	6.03	-3.63	-52.2
47	195	-6871	-386	-5	0	-157	286	10.05	10.05	6.03	6.03	-3.69	-52.8
49	195	-7042	-302	-21	0	-154	188	10.05	10.05	6.03	6.03	-3.41	-49.4
50	195	-6748	-501	-11	0	-158	366	10.05	10.05	6.03	6.03	-3.93	-55.7
51	195	-6872	-390	37	0	-147	282	10.05	10.05	6.03	6.03	-3.68	-52.6

apost= 6.03 aant= 6.03 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	292	-7424	-395	-221	0	61	-552	10.05	10.05	6.03	6.03	-4.87	-68.0
41	292	-6911	-648	-173	0	7	-503	10.05	10.05	6.03	6.03	-4.49	-62.8
42	292	-6912	-658	-47	0	-85	-527	10.05	10.05	6.03	6.03	-4.58	-63.9
43	292	-7453	-96	-170	0	17	-379	10.05	10.05	6.03	6.03	-4.25	-60.4
44	292	-5982	-1091	-120	0	-47	-456	10.05	10.05	6.03	6.03	-3.96	-55.3
45	292	-6601	-535	121	0	-227	-337	10.05	10.05	6.03	6.03	-3.77	-53.5
46	292	-6411	-439	-38	0	-120	-173	10.05	10.05	6.03	6.03	-3.11	-45.0
47	292	-6286	-386	-5	0	-152	-90	10.05	10.05	6.03	6.03	-3.11	-43.7
49	292	-6457	-302	-21	0	-134	-107	10.05	10.05	6.03	6.03	-3.08	-43.6
50	292	-6163	-501	-11	0	-147	-122	10.05	10.05	6.03	6.03	-3.04	-42.7
51	292	-6287	-390	37	0	-183	-98	10.05	10.05	6.03	6.03	-3.27	-45.5

apost= 6.03 aant= 6.03 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	390	-6839	-395	-221	0	277	-937	10.05	10.05	6.03	6.03	-6.11	-82.9
41	390	-6326	-648	-173	0	176	-1134	10.05	10.05	6.03	6.03	-7.03	-93.0
42	390	-6327	-658	-47	0	-39	-1169	10.05	10.05	6.03	6.03	-7.24	-95.4
43	390	-6868	-96	-170	0	182	-473	10.05	10.05	6.03	6.03	-4.36	-61.2
44	390	-5397	-1091	-120	0	71	-1520	10.05	10.05	6.03	6.03	-9.72	137.5
45	390	-6016	-535	121	0	-344	-859	10.05	10.05	6.03	6.03	-5.53	-74.8
46	390	-5826	-439	-38	0	-83	-600	10.05	10.05	6.03	6.03	-4.42	-60.9
47	390	-5701	-386	-5	0	-148	-467	10.05	10.05	6.03	6.03	-3.89	-54.2
49	390	-5872	-302	-21	0	-114	-402	10.05	10.05	6.03	6.03	-3.72	-52.2
50	390	-5578	-501	-11	0	-136	-611	10.05	10.05	6.03	6.03	-4.36	-59.9
51	390	-5702	-390	37	0	-219	-479	10.05	10.05	6.03	6.03	-3.93	-54.7

apost= 6.03 aant= 6.03 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

ASTA NUM. 51 NI 168 NF 169 SEZ. Rp B= 0.400 H= 0.600 (pilastro)

PIL. NUM. 11B
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-5524	1229	380	0	379	-3165	10.05	10.05	6.03	6.03	-21.19	622.8
41	0	-5893	600	354	0	327	-1756	10.05	10.05	6.03	6.03	-11.30	175.2
42	0	-5881	603	324	0	270	-1762	10.05	10.05	6.03	6.03	-11.35	177.4
43	0	-5275	1536	389	0	402	-3865	10.05	10.05	6.03	6.03	-25.90	864.3
44	0	-6400	-430	306	0	240	555	10.05	10.05	6.03	6.03	-4.48	-62.2
45	0	-5869	494	297	0	218	-1526	10.05	10.05	6.03	6.03	-9.66	-121.0
46	0	-5887	421	342	0	307	-1372	10.05	10.05	6.03	6.03	-8.58	-109.4
47	0	-5886	376	338	0	302	-1276	10.05	10.05	6.03	6.03	-7.93	-102.3
49	0	-5763	585	347	0	320	-1746	10.05	10.05	6.03	6.03	-11.26	179.0
50	0	-5988	192	330	0	287	-862	10.05	10.05	6.03	6.03	-5.54	-74.9
51	0	-5882	377	329	0	283	-1278	10.05	10.05	6.03	6.03	-7.94	-102.4

apost= 6.03 aant= 6.03 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	97	-4939	1229	380	0	9	-1967	10.05	10.05	6.03	6.03	-13.00	288.6
41	97	-5308	600	354	0	-18	-1171	10.05	10.05	6.03	6.03	-7.29	-93.8
42	97	-5296	603	324	0	-47	-1174	10.05	10.05	6.03	6.03	-7.31	-93.9
43	97	-4690	1536	389	0	22	-2367	10.05	10.05	6.03	6.03	-15.81	427.8
44	97	-5815	-430	306	0	-58	136	10.05	10.05	6.03	6.03	-2.74	-39.9
45	97	-5284	494	297	0	-71	-1045	10.05	10.05	6.03	6.03	-6.46	-84.5
46	97	-5302	421	342	0	-26	-962	10.05	10.05	6.03	6.03	-5.96	-78.8
47	97	-5301	376	338	0	-28	-910	10.05	10.05	6.03	6.03	-5.66	-75.3
49	97	-5178	585	347	0	-19	-1175	10.05	10.05	6.03	6.03	-7.33	-93.9
50	97	-5403	192	330	0	-35	-675	10.05	10.05	6.03	6.03	-4.55	-62.0
51	97	-5297	377	329	0	-38	-911	10.05	10.05	6.03	6.03	-5.67	-75.3

apost= 6.03 aant= 6.03 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	195	-4354	1229	380	0	-361	-769	10.05	10.05	6.03	6.03	-4.77	-63.3
41	195	-4723	600	354	0	-363	-586	10.05	10.05	6.03	6.03	-3.96	-54.0
42	195	-4711	603	324	0	-363	-585	10.05	10.05	6.03	6.03	-3.95	-53.9
43	195	-4105	1536	389	0	-357	-870	10.05	10.05	6.03	6.03	-5.40	-69.8
44	195	-5230	-430	306	0	-356	-284	10.05	10.05	6.03	6.03	-3.77	-49.7
45	195	-4699	494	297	0	-360	-563	10.05	10.05	6.03	6.03	-3.86	-52.8
46	195	-4717	421	342	0	-359	-552	10.05	10.05	6.03	6.03	-3.82	-52.3
47	195	-4716	376	338	0	-358	-543	10.05	10.05	6.03	6.03	-3.79	-51.9
49	195	-4593	585	347	0	-357	-604	10.05	10.05	6.03	6.03	-3.99	-54.3
50	195	-4818	192	330	0	-357	-487	10.05	10.05	6.03	6.03	-3.62	-49.9
51	195	-4712	377	329	0	-358	-543	10.05	10.05	6.03	6.03	-3.79	-51.9

apost= 6.03 aant= 6.03 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	292	-3769	1229	380	0	-732	429	10.05	10.05	6.03	6.03	-6.43	74.9
41	292	-4138	600	354	0	-709	-2	10.05	10.05	6.03	6.03	-6.20	-71.4
42	292	-4126	603	324	0	-679	3	10.05	10.05	6.03	6.03	-5.93	-69.0
43	292	-3520	1536	389	0	-737	628	10.05	10.05	6.03	6.03	-6.49	84.3
44	292	-4645	-430	306	0	-653	-703	10.05	10.05	6.03	6.03	-5.70	-68.5
45	292	-4114	494	297	0	-650	-82	10.05	10.05	6.03	6.03	-5.67	-66.5
46	292	-4132	421	342	0	-692	-142	10.05	10.05	6.03	6.03	-6.05	-70.0
47	292	-4131	376	338	0	-688	-177	10.05	10.05	6.03	6.03	-6.01	-69.7
49	292	-4008	585	347	0	-696	-34	10.05	10.05	6.03	6.03	-6.09	-69.9
50	292	-4233	192	330	0	-679	-300	10.05	10.05	6.03	6.03	-5.93	-69.3
51	292	-4127	377	329	0	-678	-176	10.05	10.05	6.03	6.03	-5.92	-68.9

apost= 6.03 aant= 6.03 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	390	-3184	1229	380	0	-1102	1627	10.05	10.05	6.03	6.03	-10.87	296.7
41	390	-3553	600	354	0	-1054	583	10.05	10.05	6.03	6.03	-9.35	175.4
42	390	-3541	603	324	0	-996	591	10.05	10.05	6.03	6.03	-8.83	158.4
43	390	-2935	1536	389	0	-1116	2126	10.05	10.05	6.03	6.03	-14.25	473.0
44	390	-4060	-430	306	0	-951	-1123	10.05	10.05	6.03	6.03	-8.41	125.8
45	390	-3529	494	297	0	-939	399	10.05	10.05	6.03	6.03	-8.32	142.1
46	390	-3547	421	342	0	-1025	268	10.05	10.05	6.03	6.03	-9.09	166.9
47	390	-3546	376	338	0	-1018	189	10.05	10.05	6.03	6.03	-9.03	164.9
49	390	-3423	585	347	0	-1034	537	10.05	10.05	6.03	6.03	-9.17	174.6
50	390	-3648	192	330	0	-1001	-113	10.05	10.05	6.03	6.03	-8.87	155.8
51	390	-3542	377	329	0	-999	192	10.05	10.05	6.03	6.03	-8.85	159.3

apost= 6.03 aant= 6.03 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

ASTA NUM. 52 NI 170 NF 171 SEZ. Rp B= 0.400 H= 0.600 (pilastro)
PIL. NUM. 16B
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-9446	1877	541	0	520	-3385	10.05	10.05	6.03	6.03	-22.20	440.3
41	0	-9467	958	552	0	534	-1665	10.05	10.05	6.03	6.03	-10.34	-137.1
42	0	-9401	963	488	0	424	-1676	10.05	10.05	6.03	6.03	-10.40	-137.6
43	0	-9281	2326	524	0	505	-4237	10.05	10.05	6.03	6.03	-28.21	707.3
44	0	-9300	-547	552	0	538	1153	10.05	10.05	6.03	6.03	-7.79	-106.3
45	0	-9206	803	436	0	346	-1387	10.05	10.05	6.03	6.03	-8.82	-118.7
46	0	-9227	696	538	0	525	-1193	10.05	10.05	6.03	6.03	-7.93	-108.0
47	0	-9167	631	534	0	523	-1075	10.05	10.05	6.03	6.03	-7.43	-101.8
49	0	-9160	937	530	0	518	-1648	10.05	10.05	6.03	6.03	-10.22	-135.1
50	0	-9164	362	536	0	525	-570	10.05	10.05	6.03	6.03	-6.10	-81.3
51	0	-9145	632	513	0	487	-1078	10.05	10.05	6.03	6.03	-7.44	-101.8

apost= 6.03 aant= 6.03 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	97	-8861	1877	541	0	-7	-1555	10.05	10.05	6.03	6.03	-9.66	-128.1
41	97	-8882	958	552	0	-5	-731	10.05	10.05	6.03	6.03	-6.07	-84.5
42	97	-8816	963	488	0	-52	-736	10.05	10.05	6.03	6.03	-6.07	-84.4
43	97	-8696	2326	524	0	-5	-1969	10.05	10.05	6.03	6.03	-12.28	-157.3
44	97	-8715	-547	552	0	-0	620	10.05	10.05	6.03	6.03	-5.61	-78.6

45	97	-8621	803	436	0	-79	-604	10.05	10.05	6.03	6.03	-5.52	-77.3
46	97	-8642	696	538	0	1	-514	10.05	10.05	6.03	6.03	-5.20	-73.4
47	97	-8582	631	534	0	2	-460	10.05	10.05	6.03	6.03	-4.98	-70.6
49	97	-8575	937	530	0	1	-734	10.05	10.05	6.03	6.03	-5.97	-82.9
50	97	-8579	362	536	0	2	-217	10.05	10.05	6.03	6.03	-4.10	-59.6
51	97	-8560	632	513	0	-13	-461	10.05	10.05	6.03	6.03	-4.98	-70.5

apost= 6.03 aant= 6.03 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	195	-8276	1877	541	0	-535	276	10.05	10.05	6.03	6.03	-5.82	-77.0
41	195	-8297	958	552	0	-544	204	10.05	10.05	6.03	6.03	-5.87	-77.6
42	195	-8231	963	488	0	-527	203	10.05	10.05	6.03	6.03	-5.77	-76.3
43	195	-8111	2326	524	0	-516	299	10.05	10.05	6.03	6.03	-5.66	-75.0
44	195	-8130	-547	552	0	-538	87	10.05	10.05	6.03	6.03	-5.78	-76.4
45	195	-8036	803	436	0	-504	179	10.05	10.05	6.03	6.03	-5.57	-73.9
46	195	-8057	696	538	0	-524	165	10.05	10.05	6.03	6.03	-5.68	-75.1
47	195	-7997	631	534	0	-519	155	10.05	10.05	6.03	6.03	-5.64	-74.5
49	195	-7990	937	530	0	-516	180	10.05	10.05	6.03	6.03	-5.62	-74.3
50	195	-7994	362	536	0	-520	137	10.05	10.05	6.03	6.03	-5.64	-74.6
51	195	-7975	632	513	0	-513	156	10.05	10.05	6.03	6.03	-5.60	-74.1

apost= 6.03 aant= 6.03 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	292	-7691	1877	541	0	-1062	2106	10.05	10.05	6.03	6.03	-13.42	180.8
41	292	-7712	958	552	0	-1082	1138	10.05	10.05	6.03	6.03	-9.44	-113.5
42	292	-7646	963	488	0	-1003	1142	10.05	10.05	6.03	6.03	-8.77	-106.8
43	292	-7526	2326	524	0	-1026	2567	10.05	10.05	6.03	6.03	-16.76	313.4
44	292	-7545	-547	552	0	-1076	-446	10.05	10.05	6.03	6.03	-9.39	-112.4
45	292	-7451	803	436	0	-929	962	10.05	10.05	6.03	6.03	-8.15	-100.2
46	292	-7472	696	538	0	-1048	844	10.05	10.05	6.03	6.03	-9.15	-109.9
47	292	-7412	631	534	0	-1040	770	10.05	10.05	6.03	6.03	-9.07	-109.1
49	292	-7405	937	530	0	-1033	1093	10.05	10.05	6.03	6.03	-9.01	-108.4
50	292	-7409	362	536	0	-1043	490	10.05	10.05	6.03	6.03	-9.09	-109.3
51	292	-7390	632	513	0	-1013	772	10.05	10.05	6.03	6.03	-8.84	-106.8

apost= 6.03 aant= 6.03 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	390	-7106	1877	541	0	-1589	3936	10.05	10.05	6.03	6.03	-26.34	758.2
41	390	-7127	958	552	0	-1621	2072	10.05	10.05	6.03	6.03	-14.31	206.9
42	390	-7061	963	488	0	-1479	2082	10.05	10.05	6.03	6.03	-13.39	204.1
43	390	-6941	2326	524	0	-1537	4835	10.05	10.05	6.03	6.03	-32.40	1056.7
44	390	-6960	-547	552	0	-1614	-979	10.05	10.05	6.03	6.03	-14.26	210.9
45	390	-6866	803	436	0	-1354	1745	10.05	10.05	6.03	6.03	-11.90	142.0
46	390	-6887	696	538	0	-1573	1523	10.05	10.05	6.03	6.03	-13.89	201.8
47	390	-6827	631	534	0	-1561	1385	10.05	10.05	6.03	6.03	-13.79	200.5
49	390	-6820	937	530	0	-1550	2007	10.05	10.05	6.03	6.03	-13.69	197.7
50	390	-6824	362	536	0	-1565	844	10.05	10.05	6.03	6.03	-13.82	201.8
51	390	-6805	632	513	0	-1513	1389	10.05	10.05	6.03	6.03	-13.35	187.7

apost= 6.03 aant= 6.03 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

ASTA NUM. 53 NI 172 NF 185 SEZ. Rp B= 0.400 H= 0.600 (pilastro)
PIL. NUM. 21B
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN				daN*m		cm^2				daN/cm^2	
40	0	-9467	1808	620	0	659	-3480	10.05	10.05	6.03	6.03	-22.87	466.9
41	0	-9498	865	598	0	620	-1691	10.05	10.05	6.03	6.03	-10.49	-138.9
42	0	-9523	870	573	0	570	-1698	10.05	10.05	6.03	6.03	-10.53	-139.4
43	0	-9292	2261	612	0	656	-4349	10.05	10.05	6.03	6.03	-28.98	741.2
44	0	-9350	-681	544	0	540	1246	10.05	10.05	6.03	6.03	-8.20	-111.4
45	0	-9384	697	533	0	508	-1378	10.05	10.05	6.03	6.03	-8.81	-118.9
46	0	-9251	584	562	0	574	-1172	10.05	10.05	6.03	6.03	-7.85	-107.1
47	0	-9190	514	553	0	562	-1042	10.05	10.05	6.03	6.03	-7.32	-100.4
49	0	-9179	828	560	0	575	-1639	10.05	10.05	6.03	6.03	-10.17	-134.6
50	0	-9191	240	546	0	552	-520	10.05	10.05	6.03	6.03	-6.25	-83.1
51	0	-9198	516	544	0	546	-1045	10.05	10.05	6.03	6.03	-7.33	-100.5

apost= 6.03 aant= 6.03 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	97	-8882	1808	620	0	54	-1718	10.05	10.05	6.03	6.03	-10.63	-139.3
41	97	-8913	865	598	0	36	-847	10.05	10.05	6.03	6.03	-6.50	-89.9
42	97	-8938	870	573	0	11	-850	10.05	10.05	6.03	6.03	-6.52	-90.2
43	97	-8707	2261	612	0	60	-2145	10.05	10.05	6.03	6.03	-13.50	-170.6
44	97	-8765	-681	544	0	9	582	10.05	10.05	6.03	6.03	-5.49	-77.1
45	97	-8799	697	533	0	-13	-698	10.05	10.05	6.03	6.03	-5.92	-82.6
46	97	-8666	584	562	0	26	-602	10.05	10.05	6.03	6.03	-5.53	-77.5
47	97	-8605	514	553	0	23	-541	10.05	10.05	6.03	6.03	-5.28	-74.4
49	97	-8594	828	560	0	29	-831	10.05	10.05	6.03	6.03	-6.32	-87.4
50	97	-8606	240	546	0	19	-286	10.05	10.05	6.03	6.03	-4.36	-62.9
51	97	-8613	516	544	0	15	-542	10.05	10.05	6.03	6.03	-5.29	-74.5

apost= 6.03 aant= 6.03 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	195	-8297	1808	620	0	-551	45	10.05	10.05	6.03	6.03	-5.91	-78.0
41	195	-8328	865	598	0	-547	-4	10.05	10.05	6.03	6.03	-5.90	-78.0
42	195	-8353	870	573	0	-548	-2	10.05	10.05	6.03	6.03	-5.92	-78.2
43	195	-8122	2261	612	0	-537	59	10.05	10.05	6.03	6.03	-5.78	-76.2
44	195	-8180	-681	544	0	-522	-82	10.05	10.05	6.03	6.03	-5.72	-75.7
45	195	-8214	697	533	0	-533	-19	10.05	10.05	6.03	6.03	-5.79	-76.5
46	195	-8081	584	562	0	-522	-32	10.05	10.05	6.03	6.03	-5.68	-75.1
47	195	-8020	514	553	0	-515	-39	10.05	10.05	6.03	6.03	-5.63	-74.4
49	195	-8009	828	560	0	-516	-24	10.05	10.05	6.03	6.03	-5.63	-74.4
50	195	-8021	240	546	0	-513	-52	10.05	10.05	6.03	6.03	-5.62	-74.3
51	195	-8028	516	544	0	-516	-39	10.05	10.05	6.03	6.03	-5.63	-74.5

apost= 6.03 aant= 6.03 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	292	-7712	1808	620	0	-1155	1807	10.05	10.05	6.03	6.03	-11.31	-144.1
41	292	-7743	865	598	0	-1131	840	10.05	10.05	6.03	6.03	-9.86	-117.6
42	292	-7768	870	573	0	-1106	846	10.05	10.05	6.03	6.03	-9.65	-115.6
43	292	-7537	2261	612	0	-1134	2263	10.05	10.05	6.03	6.03	-14.58	228.6
44	292	-7595	-681	544	0	-1052	-745	10.05	10.05	6.03	6.03	-9.18	-110.7
45	292	-7629	697	533	0	-1053	660	10.05	10.05	6.03	6.03	-9.19	-110.8

46	292	-7496	584	562	0	-1069	537	10.05	10.05	6.03	6.03	-9.33	-111.7
47	292	-7435	514	553	0	-1054	462	10.05	10.05	6.03	6.03	-9.19	-110.3
49	292	-7424	828	560	0	-1062	784	10.05	10.05	6.03	6.03	-9.26	-110.9
50	292	-7436	240	546	0	-1046	183	10.05	10.05	6.03	6.03	-9.13	-109.6
51	292	-7443	516	544	0	-1046	464	10.05	10.05	6.03	6.03	-9.13	-109.7

apost= 6.03 aant= 6.03 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	390	-7127	1808	620	0	-1760	3570	10.05	10.05	6.03	6.03	-23.84	641.6
41	390	-7158	865	598	0	-1714	1684	10.05	10.05	6.03	6.03	-15.16	232.4
42	390	-7183	870	573	0	-1665	1694	10.05	10.05	6.03	6.03	-14.71	217.4
43	390	-6952	2261	612	0	-1730	4467	10.05	10.05	6.03	6.03	-29.94	937.9
44	390	-7010	-681	544	0	-1583	-1409	10.05	10.05	6.03	6.03	-13.98	200.3
45	390	-7044	697	533	0	-1573	1340	10.05	10.05	6.03	6.03	-13.88	196.3
46	390	-6911	584	562	0	-1617	1107	10.05	10.05	6.03	6.03	-14.29	213.5
47	390	-6850	514	553	0	-1593	963	10.05	10.05	6.03	6.03	-14.08	208.8
49	390	-6839	828	560	0	-1608	1592	10.05	10.05	6.03	6.03	-14.21	213.5
50	390	-6851	240	546	0	-1579	417	10.05	10.05	6.03	6.03	-13.95	204.8
51	390	-6858	516	544	0	-1577	966	10.05	10.05	6.03	6.03	-13.93	204.0

apost= 6.03 aant= 6.03 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

ASTA NUM. 54 NI 167 NF 208 SEZ. Rp B= 0.400 H= 0.600 (pilastro)
PIL. NUM. 26C
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-2299	4043	-1298	0	1326	-4206	10.05	10.05	6.03	6.03	-27.78	1197.1
41	0	-2168	2929	-1120	0	1239	-3135	10.05	10.05	6.03	6.03	-20.79	857.5
42	0	-1939	2986	-182	0	1394	-3189	10.05	10.05	6.03	6.03	-21.10	892.6
43	0	-2174	4193	-1115	0	1268	-4298	10.05	10.05	6.03	6.03	-28.35	1236.7
44	0	-1981	1168	-871	0	1101	-1450	10.05	10.05	6.03	6.03	-9.72	324.1
45	0	-1575	2432	744	0	1382	-2604	10.05	10.05	6.03	6.03	-17.23	729.5
46	0	-1829	1982	-637	0	1053	-2140	10.05	10.05	6.03	6.03	-14.25	559.0
47	0	-1745	1745	-516	0	1007	-1892	10.05	10.05	6.03	6.03	-12.61	484.6
49	0	-1788	2116	-576	0	1036	-2249	10.05	10.05	6.03	6.03	-14.95	597.6
50	0	-1750	1511	-527	0	1002	-1679	10.05	10.05	6.03	6.03	-11.22	415.0
51	0	-1668	1764	-204	0	1059	-1910	10.05	10.05	6.03	6.03	-12.72	496.2

apost= 6.03 aant= 6.03 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	12	-2224	4043	-1298	0	1488	-3700	10.05	10.05	6.03	6.03	-24.48	1037.8
41	12	-2093	2929	-1120	0	1379	-2769	10.05	10.05	6.03	6.03	-18.39	743.8
42	12	-1864	2986	-182	0	1417	-2816	10.05	10.05	6.03	6.03	-18.66	776.5
43	12	-2099	4193	-1115	0	1408	-3774	10.05	10.05	6.03	6.03	-24.93	1071.3
44	12	-1906	1168	-871	0	1210	-1304	10.05	10.05	6.03	6.03	-10.63	294.6
45	12	-1500	2432	744	0	1289	-2300	10.05	10.05	6.03	6.03	-15.24	636.0
46	12	-1754	1982	-637	0	1133	-1892	10.05	10.05	6.03	6.03	-12.62	484.0
47	12	-1670	1745	-516	0	1072	-1674	10.05	10.05	6.03	6.03	-11.17	419.3
49	12	-1713	2116	-576	0	1108	-1984	10.05	10.05	6.03	6.03	-13.22	517.1
50	12	-1675	1511	-527	0	1068	-1490	10.05	10.05	6.03	6.03	-9.97	359.4
51	12	-1593	1764	-204	0	1084	-1690	10.05	10.05	6.03	6.03	-11.27	430.1

apost= 6.03 aant= 6.03 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	25	-2149	4043	-1298	0	1650	-3195	10.05	10.05	6.03	6.03	-21.18	878.6
41	25	-2018	2929	-1120	0	1519	-2402	10.05	10.05	6.03	6.03	-15.99	630.2
42	25	-1789	2986	-182	0	1440	-2442	10.05	10.05	6.03	6.03	-16.22	660.5
43	25	-2024	4193	-1115	0	1547	-3250	10.05	10.05	6.03	6.03	-21.51	905.9
44	25	-1831	1168	-871	0	1318	-1158	10.05	10.05	6.03	6.03	-11.55	332.3
45	25	-1425	2432	744	0	1196	-1996	10.05	10.05	6.03	6.03	-13.25	542.6
46	25	-1679	1982	-637	0	1212	-1644	10.05	10.05	6.03	6.03	-10.98	409.1
47	25	-1595	1745	-516	0	1136	-1456	10.05	10.05	6.03	6.03	-9.95	354.0
49	25	-1638	2116	-576	0	1180	-1720	10.05	10.05	6.03	6.03	-11.47	436.7
50	25	-1600	1511	-527	0	1134	-1301	10.05	10.05	6.03	6.03	-9.94	303.8
51	25	-1518	1764	-204	0	1110	-1469	10.05	10.05	6.03	6.03	-9.81	364.1

apost= 6.03 aant= 6.03 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	38	-2074	4043	-1298	0	1813	-2690	10.05	10.05	6.03	6.03	-17.87	719.4
41	38	-1943	2929	-1120	0	1659	-2036	10.05	10.05	6.03	6.03	-14.48	516.7
42	38	-1714	2986	-182	0	1463	-2069	10.05	10.05	6.03	6.03	-13.77	544.6
43	38	-1949	4193	-1115	0	1686	-2725	10.05	10.05	6.03	6.03	-18.09	740.6
44	38	-1756	1168	-871	0	1427	-1012	10.05	10.05	6.03	6.03	-12.47	370.1
45	38	-1350	2432	744	0	1103	-1692	10.05	10.05	6.03	6.03	-11.25	449.2
46	38	-1604	1982	-637	0	1292	-1397	10.05	10.05	6.03	6.03	-11.29	334.5
47	38	-1520	1745	-516	0	1200	-1237	10.05	10.05	6.03	6.03	-10.50	309.3
49	38	-1563	2116	-576	0	1252	-1456	10.05	10.05	6.03	6.03	-10.94	356.4
50	38	-1525	1511	-527	0	1200	-1112	10.05	10.05	6.03	6.03	-10.49	308.9
51	38	-1443	1764	-204	0	1136	-1248	10.05	10.05	6.03	6.03	-9.93	298.2

apost= 6.03 aant= 6.03 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	50	-1999	4043	-1298	0	1975	-2184	10.05	10.05	6.03	6.03	-17.19	560.5
41	50	-1868	2929	-1120	0	1799	-1670	10.05	10.05	6.03	6.03	-15.67	482.5
42	50	-1639	2986	-182	0	1486	-1696	10.05	10.05	6.03	6.03	-12.96	428.8
43	50	-1874	4193	-1115	0	1826	-2201	10.05	10.05	6.03	6.03	-15.90	575.4
44	50	-1681	1168	-871	0	1536	-866	10.05	10.05	6.03	6.03	-13.39	408.0
45	50	-1275	2432	744	0	1010	-1388	10.05	10.05	6.03	6.03	-9.25	355.9
46	50	-1529	1982	-637	0	1372	-1149	10.05	10.05	6.03	6.03	-11.96	363.1
47	50	-1445	1745	-516	0	1265	-1019	10.05	10.05	6.03	6.03	-11.04	333.2
49	50	-1488	2116	-576	0	1324	-1191	10.05	10.05	6.03	6.03	-11.55	349.9
50	50	-1450	1511	-527	0	1266	-924	10.05	10.05	6.03	6.03	-11.05	333.3
51	50	-1368	1764	-204	0	1161	-1028	10.05	10.05	6.03	6.03	-10.14	303.9

apost= 6.03 aant= 6.03 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

ASTA NUM. 55 NI 122 NF 165 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 24B
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf

	--												
	cm	daN		daN*m			cm²				daN/cm²	
40	0	-9435	87	-634	0	-1238	-139	4.02	4.02	10.05	10.05	-11.06	-150.4
41	0	-9394	-9	-518	0	-1019	135	4.02	4.02	10.05	10.05	-9.86	-135.5
42	0	-9382	-10	-298	0	-588	136	4.02	4.02	10.05	10.05	-7.75	-109.1
43	0	-9163	156	-609	0	-1187	-339	4.02	4.02	10.05	10.05	-10.65	-145.0
44	0	-9053	-171	-346	0	-689	594	4.02	4.02	10.05	10.05	-9.81	-119.3
45	0	-9075	-5	-50	0	-102	120	4.02	4.02	10.05	10.05	-5.40	-77.1
46	0	-8916	-1	-356	0	-702	108	4.02	4.02	10.05	10.05	-8.06	-112.4
47	0	-8797	1	-315	0	-623	101	4.02	4.02	10.05	10.05	-7.62	-106.6
49	0	-8810	33	-354	0	-696	10	4.02	4.02	10.05	10.05	-7.98	-111.2
50	0	-8788	-32	-301	0	-596	196	4.02	4.02	10.05	10.05	-7.48	-105.0
51	0	-8793	1	-242	0	-479	102	4.02	4.02	10.05	10.05	-6.91	-97.9

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	97	-8996	87	-634	0	-620	-55	4.02	4.02	10.05	10.05	-7.71	-108.1
41	97	-8955	-9	-518	0	-514	125	4.02	4.02	10.05	10.05	-7.17	-101.2
42	97	-8943	-10	-298	0	-297	126	4.02	4.02	10.05	10.05	-6.10	-87.9
43	97	-8724	156	-609	0	-593	-186	4.02	4.02	10.05	10.05	-7.43	-104.3
44	97	-8614	-171	-346	0	-352	427	4.02	4.02	10.05	10.05	-7.98	-100.3
45	97	-8636	-5	-50	0	-53	114	4.02	4.02	10.05	10.05	-5.15	-72.0
46	97	-8477	-1	-356	0	-355	107	4.02	4.02	10.05	10.05	-6.14	-87.8
47	97	-8358	1	-315	0	-315	102	4.02	4.02	10.05	10.05	-5.89	-84.5
49	97	-8371	33	-354	0	-351	42	4.02	4.02	10.05	10.05	-6.07	-86.8
50	97	-8349	-32	-301	0	-303	165	4.02	4.02	10.05	10.05	-5.82	-83.7
51	97	-8354	1	-242	0	-243	102	4.02	4.02	10.05	10.05	-5.53	-80.1

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	195	-8558	87	-634	0	-2	30	4.02	4.02	10.05	10.05	-4.47	-67.0
41	195	-8516	-9	-518	0	-8	116	4.02	4.02	10.05	10.05	-5.11	-71.3
42	195	-8504	-10	-298	0	-6	116	4.02	4.02	10.05	10.05	-5.10	-71.2
43	195	-8286	156	-609	0	0	-34	4.02	4.02	10.05	10.05	-4.32	-64.7
44	195	-8176	-171	-346	0	-15	260	4.02	4.02	10.05	10.05	-6.25	-82.0
45	195	-8198	-5	-50	0	-4	109	4.02	4.02	10.05	10.05	-4.89	-68.4
46	195	-8038	-1	-356	0	-8	106	4.02	4.02	10.05	10.05	-4.78	-67.0
47	195	-7920	1	-315	0	-8	103	4.02	4.02	10.05	10.05	-4.70	-65.9
49	195	-7932	33	-354	0	-6	74	4.02	4.02	10.05	10.05	-4.45	-63.4
50	195	-7910	-32	-301	0	-9	133	4.02	4.02	10.05	10.05	-4.97	-68.5
51	195	-7916	1	-242	0	-7	103	4.02	4.02	10.05	10.05	-4.70	-65.8

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	292	-8119	87	-634	0	615	115	4.02	4.02	10.05	10.05	-7.23	-100.9
41	292	-8078	-9	-518	0	497	107	4.02	4.02	10.05	10.05	-6.63	-93.4
42	292	-8066	-10	-298	0	285	106	4.02	4.02	10.05	10.05	-5.59	-80.4
43	292	-7847	156	-609	0	594	118	4.02	4.02	10.05	10.05	-6.98	-97.5
44	292	-7737	-171	-346	0	322	94	4.02	4.02	10.05	10.05	-5.60	-80.0
45	292	-7759	-5	-50	0	44	104	4.02	4.02	10.05	10.05	-4.63	-64.8
46	292	-7600	-1	-356	0	339	104	4.02	4.02	10.05	10.05	-5.61	-80.0
47	292	-7481	1	-315	0	299	104	4.02	4.02	10.05	10.05	-5.35	-76.7
49	292	-7494	33	-354	0	339	106	4.02	4.02	10.05	10.05	-5.55	-79.2
50	292	-7472	-32	-301	0	284	101	4.02	4.02	10.05	10.05	-5.27	-75.7
51	292	-7477	1	-242	0	229	103	4.02	4.02	10.05	10.05	-5.01	-72.3

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	390	-7680	87	-634	0	1233	200	4.02	4.02	10.05	10.05	-10.49	-140.2
41	390	-7639	-9	-518	0	1003	98	4.02	4.02	10.05	10.05	-8.96	-121.8
42	390	-7627	-10	-298	0	576	96	4.02	4.02	10.05	10.05	-6.78	-94.7
43	390	-7408	156	-609	0	1188	271	4.02	4.02	10.05	10.05	-10.11	-135.1
44	390	-7298	-171	-346	0	659	-73	4.02	4.02	10.05	10.05	-7.01	-97.1
45	390	-7320	-5	-50	0	93	98	4.02	4.02	10.05	10.05	-4.38	-62.9
46	390	-7161	-1	-356	0	686	103	4.02	4.02	10.05	10.05	-7.07	-97.7
47	390	-7042	1	-315	0	607	105	4.02	4.02	10.05	10.05	-6.62	-92.0
49	390	-7055	33	-354	0	683	138	4.02	4.02	10.05	10.05	-7.00	-96.7
50	390	-7033	-32	-301	0	578	70	4.02	4.02	10.05	10.05	-6.48	-90.1
51	390	-7038	1	-242	0	464	104	4.02	4.02	10.05	10.05	-5.93	-83.3

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

ASTA NUM. 56 NI 209 NF 210 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 23B
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	--												
	cm	daN			daN*m			cm²				daN/cm²	
40	0	-6278	138	-907	0	-1412	-151	4.02	4.02	10.05	10.05	-12.04	-153.9
41	0	-6153	80	-837	0	-1254	-23	4.02	4.02	10.05	10.05	-10.58	-137.4
42	0	-6038	87	-677	0	-896	-39	4.02	4.02	10.05	10.05	-7.73	-104.2
43	0	-6190	181	-866	0	-1345	-246	4.02	4.02	10.05	10.05	-11.42	-146.8
44	0	-5829	-18	-712	0	-994	191	4.02	4.02	10.05	10.05	-8.39	-111.5
45	0	-5791	97	-483	0	-486	-59	4.02	4.02	10.05	10.05	-5.38	-74.8
46	0	-5879	86	-698	0	-978	-37	4.02	4.02	10.05	10.05	-8.28	-110.3
47	0	-5811	87	-663	0	-909	-40	4.02	4.02	10.05	10.05	-7.77	-104.1
49	0	-5852	107	-686	0	-962	-83	4.02	4.02	10.05	10.05	-8.16	-108.8
50	0	-5780	67	-655	0	-892	4	4.02	4.02	10.05	10.05	-7.63	-102.5
51	0	-5773	90	-609	0	-790	-46	4.02	4.02	10.05	10.05	-6.97	-94.4

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	97	-5839	138	-907	0	-528	-16	4.02	4.02	10.05	10.05	-5.61	-77.8
41	97	-5714	80	-837	0	-438	55	4.02	4.02	10.05	10.05	-5.11	-71.3
42	97	-5599	87	-677	0	-236	46	4.02	4.02	10.05	10.05	-4.07	-58.1
43	97	-5751	181	-866	0	-501	-69	4.02	4.02	10.05	10.05	-5.44	-75.4
44	97	-5390	-18	-712	0	-300	174	4.02	4.02	10.05	10.05	-4.27	-60.4
45	97	-5352	97	-483	0	-15	36	4.02	4.02	10.05	10.05	-2.87	-42.7
46	97	-5440	86	-698	0	-298	47	4.02	4.02	10.05	10.05	-4.29	-60.7
47	97	-5372	87	-663	0	-263	45	4.02	4.02	10.05	10.05	-4.08	-58.0
49	97	-5413	107	-686	0	-293	21	4.02	4.02	10.05	10.05	-4.25	-60.2
50	97	-5341	67	-655	0	-253	70	4.02	4.02	10.05	10.05	-4.01	-57.1
51	97	-5334	90	-609	0	-196	42	4.02	4.02	10.05	10.05	-3.73	-53.6

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	195	-5400	138	-907	0	356	118	4.02	4.02	10.05	10.05	-4.55	-63.9
41	195	-5276	80	-837	0	378	133	4.02	4.02	10.05	10.05	-4.59	-64.2
42	195	-5160	87	-677	0	423	132	4.02	4.02	10.05	10.05	-4.75	-66.1
43	195	-5312	181	-866	0	344	108	4.02	4.02	10.05	10.05	-4.44	-62.4
44	195	-4952	-18	-712	0	394	156	4.02	4.02	10.05	10.05	-4.50	-62.7
45	195	-4914	97	-483	0	456	130	4.02	4.02	10.05	10.05	-4.78	-66.1
46	195	-5002	86	-698	0	382	131	4.02	4.02	10.05	10.05	-4.47	-62.3
47	195	-4934	87	-663	0	383	130	4.02	4.02	10.05	10.05	-4.44	-61.9
49	195	-4974	107	-686	0	375	125	4.02	4.02	10.05	10.05	-4.42	-61.7
50	195	-4902	67	-655	0	386	135	4.02	4.02	10.05	10.05	-4.43	-61.8
51	195	-4896	90	-609	0	398	130	4.02	4.02	10.05	10.05	-4.49	-62.5

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	292	-4962	138	-907	0	1240	253	4.02	4.02	10.05	10.05	-10.73	-134.7
41	292	-4837	80	-837	0	1194	210	4.02	4.02	10.05	10.05	-10.31	-129.7
42	292	-4722	87	-677	0	1083	217	4.02	4.02	10.05	10.05	-9.26	-118.0
43	292	-4874	181	-866	0	1188	285	4.02	4.02	10.05	10.05	-10.24	-129.1
44	292	-4513	-18	-712	0	1087	138	4.02	4.02	10.05	10.05	-9.36	-118.2
45	292	-4475	97	-483	0	926	224	4.02	4.02	10.05	10.05	-7.83	-101.4
46	292	-4563	86	-698	0	1062	214	4.02	4.02	10.05	10.05	-9.09	-115.6
47	292	-4495	87	-663	0	1029	215	4.02	4.02	10.05	10.05	-8.79	-112.1
49	292	-4536	107	-686	0	1044	230	4.02	4.02	10.05	10.05	-8.93	-113.7
50	292	-4464	67	-655	0	1024	201	4.02	4.02	10.05	10.05	-8.75	-111.5
51	292	-4457	90	-609	0	992	218	4.02	4.02	10.05	10.05	-8.45	-108.2

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	390	-4523	138	-907	0	2124	388	4.02	4.02	10.05	10.05	-19.77	537.7
41	390	-4398	80	-837	0	2010	288	4.02	4.02	10.05	10.05	-18.68	497.3
42	390	-4283	87	-677	0	1743	302	4.02	4.02	10.05	10.05	-16.07	386.2
43	390	-4435	181	-866	0	2032	461	4.02	4.02	10.05	10.05	-18.89	503.8
44	390	-4074	-18	-712	0	1781	120	4.02	4.02	10.05	10.05	-16.51	423.4
45	390	-4036	97	-483	0	1397	318	4.02	4.02	10.05	10.05	-12.68	255.6
46	390	-4124	86	-698	0	1742	298	4.02	4.02	10.05	10.05	-16.11	400.8
47	390	-4056	87	-663	0	1675	301	4.02	4.02	10.05	10.05	-15.46	376.8
49	390	-4097	107	-686	0	1713	334	4.02	4.02	10.05	10.05	-15.83	390.1
50	390	-4025	67	-655	0	1663	266	4.02	4.02	10.05	10.05	-15.35	374.2
51	390	-4018	90	-609	0	1586	306	4.02	4.02	10.05	10.05	-14.59	340.2

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

ASTA NUM. 57 NI 142 NF 123 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 18B
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	

40	0	-10760	44	-1046	0	-1077	-165	6.03	6.03	10.05	10.05	-8.05	-111.0
41	0	-10780	-88	-1062	0	-1106	127	6.03	6.03	10.05	10.05	-8.16	-112.4
42	0	-10830	-79	-1122	0	-1223	109	6.03	6.03	10.05	10.05	-8.60	-118.0
43	0	-10470	138	-972	0	-967	-373	6.03	6.03	10.05	10.05	-7.54	-104.4
44	0	-10560	-310	-1051	0	-1121	616	6.03	6.03	10.05	10.05	-8.13	-111.8
45	0	-10590	-66	-1098	0	-1210	83	6.03	6.03	10.05	10.05	-8.47	-116.1
46	0	-10340	-77	-960	0	-960	104	6.03	6.03	10.05	10.05	-7.46	-103.3
47	0	-10230	-74	-934	0	-924	99	6.03	6.03	10.05	10.05	-7.29	-101.0
49	0	-10230	-30	-929	0	-914	2	6.03	6.03	10.05	10.05	-7.26	-100.6
50	0	-10240	-120	-945	0	-945	200	6.03	6.03	10.05	10.05	-7.37	-102.1
51	0	-10250	-71	-954	0	-963	93	6.03	6.03	10.05	10.05	-7.44	-102.9

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	97	-10174	44	-1046	0	-57	-122	6.03	6.03	10.05	10.05	-4.40	-63.6
41	97	-10194	-88	-1062	0	-70	41	6.03	6.03	10.05	10.05	-4.20	-62.4
42	97	-10244	-79	-1122	0	-129	32	6.03	6.03	10.05	10.05	-4.43	-65.3
43	97	-9886	138	-972	0	-20	-238	6.03	6.03	10.05	10.05	-4.89	-68.7
44	97	-9974	-310	-1051	0	-96	314	6.03	6.03	10.05	10.05	-5.31	-73.6
45	97	-10005	-66	-1098	0	-140	18	6.03	6.03	10.05	10.05	-4.38	-64.4
46	97	-9756	-77	-960	0	-24	29	6.03	6.03	10.05	10.05	-3.87	-57.8
47	97	-9646	-74	-934	0	-13	26	6.03	6.03	10.05	10.05	-3.78	-56.7
49	97	-9644	-30	-929	0	-9	-28	6.03	6.03	10.05	10.05	-3.77	-56.4
50	97	-9656	-120	-945	0	-24	82	6.03	6.03	10.05	10.05	-4.00	-58.4
51	97	-9665	-71	-954	0	-33	23	6.03	6.03	10.05	10.05	-3.86	-57.6

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	195	-9588	44	-1046	0	964	-80	6.03	6.03	10.05	10.05	-7.18	-99.1
41	195	-9608	-88	-1062	0	966	-46	6.03	6.03	10.05	10.05	-7.20	-99.3
42	195	-9658	-79	-1122	0	965	-46	6.03	6.03	10.05	10.05	-7.22	-99.6
43	195	-9302	138	-972	0	927	-103	6.03	6.03	10.05	10.05	-6.94	-95.8
44	195	-9388	-310	-1051	0	928	12	6.03	6.03	10.05	10.05	-6.98	-96.4
45	195	-9420	-66	-1098	0	931	-46	6.03	6.03	10.05	10.05	-7.00	-96.7
46	195	-9172	-77	-960	0	911	-46	6.03	6.03	10.05	10.05	-6.84	-94.3
47	195	-9062	-74	-934	0	898	-46	6.03	6.03	10.05	10.05	-6.74	-93.1
49	195	-9059	-30	-929	0	897	-58	6.03	6.03	10.05	10.05	-6.74	-93.0
50	195	-9072	-120	-945	0	897	-35	6.03	6.03	10.05	10.05	-6.74	-93.1
51	195	-9080	-71	-954	0	898	-46	6.03	6.03	10.05	10.05	-6.75	-93.2

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	292	-9003	44	-1046	0	1984	-38	6.03	6.03	10.05	10.05	-12.34	-158.8
41	292	-9022	-88	-1062	0	2001	-132	6.03	6.03	10.05	10.05	-12.46	-160.1
42	292	-9072	-79	-1122	0	2059	-123	6.03	6.03	10.05	10.05	-12.85	-164.5
43	292	-8718	138	-972	0	1875	32	6.03	6.03	10.05	10.05	-11.64	-150.4
44	292	-8801	-310	-1051	0	1953	-290	6.03	6.03	10.05	10.05	-12.16	-156.3
45	292	-8834	-66	-1098	0	2002	-111	6.03	6.03	10.05	10.05	-12.48	-159.9
46	292	-8587	-77	-960	0	1847	-121	6.03	6.03	10.05	10.05	-11.47	-148.2
47	292	-8478	-74	-934	0	1808	-119	6.03	6.03	10.05	10.05	-11.23	-145.1
49	292	-8474	-30	-929	0	1802	-87	6.03	6.03	10.05	10.05	-11.19	-144.7
50	292	-8488	-120	-945	0	1818	-152	6.03	6.03	10.05	10.05	-11.29	-145.9
51	292	-8496	-71	-954	0	1828	-116	6.03	6.03	10.05	10.05	-11.35	-146.6

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	390	-8417	44	-1046	0	3004	5	6.03	6.03	10.05	10.05	-19.70	388.8
41	390	-8436	-88	-1062	0	3037	-218	6.03	6.03	10.05	10.05	-19.93	397.3
42	390	-8486	-79	-1122	0	3153	-200	6.03	6.03	10.05	10.05	-20.74	428.4
43	390	-8134	138	-972	0	2822	166	6.03	6.03	10.05	10.05	-18.46	352.3
44	390	-8215	-310	-1051	0	2978	-592	6.03	6.03	10.05	10.05	-19.55	392.9
45	390	-8249	-66	-1098	0	3072	-176	6.03	6.03	10.05	10.05	-20.21	418.5
46	390	-8003	-77	-960	0	2783	-197	6.03	6.03	10.05	10.05	-18.21	348.5
47	390	-7894	-74	-934	0	2719	-191	6.03	6.03	10.05	10.05	-17.77	336.3
49	390	-7888	-30	-929	0	2708	-117	6.03	6.03	10.05	10.05	-17.69	333.4
50	390	-7904	-120	-945	0	2739	-269	6.03	6.03	10.05	10.05	-17.91	341.4
51	390	-7911	-71	-954	0	2758	-186	6.03	6.03	10.05	10.05	-18.05	346.5

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

ASTA NUM. 58 NI 211 NF 212 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 13B
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-10200	111	-1121	0	-1353	-199	4.02	4.02	10.05	10.05	-12.05	-163.6
41	0	-10180	37	-1093	0	-1295	-47	4.02	4.02	10.05	10.05	-11.70	-159.4
42	0	-10270	38	-1196	0	-1498	-50	4.02	4.02	10.05	10.05	-12.98	-175.1
43	0	-9928	165	-1057	0	-1262	-307	4.02	4.02	10.05	10.05	-11.40	-155.3
44	0	-9895	-89	-1016	0	-1175	207	4.02	4.02	10.05	10.05	-10.91	-149.2
45	0	-10050	43	-1182	0	-1504	-59	4.02	4.02	10.05	10.05	-12.96	-174.4
46	0	-9722	42	-960	0	-1086	-58	4.02	4.02	10.05	10.05	-10.36	-142.2
47	0	-9609	44	-927	0	-1034	-61	4.02	4.02	10.05	10.05	-10.04	-138.1
49	0	-9616	68	-936	0	-1053	-112	4.02	4.02	10.05	10.05	-10.14	-139.3
50	0	-9609	18	-928	0	-1036	-9	4.02	4.02	10.05	10.05	-10.05	-138.2
51	0	-9641	44	-961	0	-1102	-62	4.02	4.02	10.05	10.05	-10.40	-142.6

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	97	-9760	111	-1121	0	-260	-90	4.02	4.02	10.05	10.05	-6.35	-92.1
41	97	-9740	37	-1093	0	-229	-11	4.02	4.02	10.05	10.05	-6.19	-90.0
42	97	-9832	38	-1196	0	-332	-13	4.02	4.02	10.05	10.05	-6.74	-97.0
43	97	-9489	165	-1057	0	-231	-147	4.02	4.02	10.05	10.05	-6.07	-88.2
44	97	-9456	-89	-1016	0	-184	121	4.02	4.02	10.05	10.05	-5.82	-85.1
45	97	-9612	43	-1182	0	-351	-17	4.02	4.02	10.05	10.05	-6.72	-96.5
46	97	-9283	42	-960	0	-150	-17	4.02	4.02	10.05	10.05	-5.56	-81.6
47	97	-9170	44	-927	0	-130	-18	4.02	4.02	10.05	10.05	-5.41	-79.6
49	97	-9177	68	-936	0	-140	-45	4.02	4.02	10.05	10.05	-5.46	-80.2
50	97	-9170	18	-928	0	-131	9	4.02	4.02	10.05	10.05	-5.41	-79.6
51	97	-9202	44	-961	0	-164	-19	4.02	4.02	10.05	10.05	-5.59	-81.9

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	195	-9321	111	-1121	0	834	18	4.02	4.02	10.05	10.05	-8.92	-123.6
41	195	-9300	37	-1093	0	836	24	4.02	4.02	10.05	10.05	-8.92	-123.6
42	195	-9394	38	-1196	0	835	24	4.02	4.02	10.05	10.05	-8.96	-124.2
43	195	-9050	165	-1057	0	800	14	4.02	4.02	10.05	10.05	-8.61	-119.4
44	195	-9018	-89	-1016	0	806	34	4.02	4.02	10.05	10.05	-8.63	-119.6
45	195	-9174	43	-1182	0	802	24	4.02	4.02	10.05	10.05	-8.68	-120.5
46	195	-8844	42	-960	0	786	24	4.02	4.02	10.05	10.05	-8.44	-117.0
47	195	-8732	44	-927	0	774	24	4.02	4.02	10.05	10.05	-8.32	-115.3
49	195	-8738	68	-936	0	772	22	4.02	4.02	10.05	10.05	-8.32	-115.3
50	195	-8732	18	-928	0	774	26	4.02	4.02	10.05	10.05	-8.32	-115.4
51	195	-8764	44	-961	0	773	24	4.02	4.02	10.05	10.05	-8.33	-115.5

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	292	-8882	111	-1121	0	1927	127	4.02	4.02	10.05	10.05	-16.35	-210.3
41	292	-8861	37	-1093	0	1902	60	4.02	4.02	10.05	10.05	-16.13	-207.8
42	292	-8955	38	-1196	0	2002	62	4.02	4.02	10.05	10.05	-17.05	-218.2
43	292	-8612	165	-1057	0	1830	175	4.02	4.02	10.05	10.05	-15.50	-200.0
44	292	-8579	-89	-1016	0	1797	-52	4.02	4.02	10.05	10.05	-15.20	-196.6
45	292	-8736	43	-1182	0	1954	66	4.02	4.02	10.05	10.05	-16.65	-213.0
46	292	-8406	42	-960	0	1722	65	4.02	4.02	10.05	10.05	-14.54	-188.6
47	292	-8293	44	-927	0	1677	67	4.02	4.02	10.05	10.05	-14.15	-183.9
49	292	-8300	68	-936	0	1685	89	4.02	4.02	10.05	10.05	-14.22	-184.7
50	292	-8293	18	-928	0	1679	44	4.02	4.02	10.05	10.05	-14.17	-184.1
51	292	-8325	44	-961	0	1710	67	4.02	4.02	10.05	10.05	-14.45	-187.3

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	390	-8442	111	-1121	0	3020	235	4.02	4.02	10.05	10.05	-27.51	576.9
41	390	-8421	37	-1093	0	2968	96	4.02	4.02	10.05	10.05	-26.99	556.2
42	390	-8517	38	-1196	0	3168	99	4.02	4.02	10.05	10.05	-28.98	635.0
43	390	-8173	165	-1057	0	2861	335	4.02	4.02	10.05	10.05	-26.00	531.3
44	390	-8140	-89	-1016	0	2788	-138	4.02	4.02	10.05	10.05	-25.27	502.8
45	390	-8298	43	-1182	0	3107	108	4.02	4.02	10.05	10.05	-28.44	627.7
46	390	-7967	42	-960	0	2658	106	4.02	4.02	10.05	10.05	-24.01	462.1
47	390	-7854	44	-927	0	2581	109	4.02	4.02	10.05	10.05	-23.27	439.1
49	390	-7861	68	-936	0	2598	156	4.02	4.02	10.05	10.05	-23.44	445.6
50	390	-7854	18	-928	0	2584	61	4.02	4.02	10.05	10.05	-23.30	440.3
51	390	-7886	44	-961	0	2648	110	4.02	4.02	10.05	10.05	-23.94	464.6

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

ASTA NUM. 59 NI 213 NF 214 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 8B
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-5833	-27	-596	0	-743	-96	4.02	4.02	10.05	10.05	-6.71	-91.4
41	0	-5855	-88	-534	0	-604	41	4.02	4.02	10.05	10.05	-5.99	-82.5

42	0	-5914	-86	-598	0	-746	37	4.02	4.02	10.05	10.05	-6.76	-92.1
43	0	-5684	16	-603	0	-782	-192	4.02	4.02	10.05	10.05	-6.89	-93.3
44	0	-5774	-190	-417	0	-364	272	4.02	4.02	10.05	10.05	-5.22	-67.3
45	0	-5818	-83	-607	0	-787	31	4.02	4.02	10.05	10.05	-6.96	-94.4
46	0	-5640	-84	-480	0	-518	34	4.02	4.02	10.05	10.05	-5.46	-75.6
47	0	-5586	-83	-467	0	-496	32	4.02	4.02	10.05	10.05	-5.33	-73.9
49	0	-5579	-63	-487	0	-543	-13	4.02	4.02	10.05	10.05	-5.55	-76.6
50	0	-5597	-104	-450	0	-459	79	4.02	4.02	10.05	10.05	-5.15	-71.7
51	0	-5606	-83	-488	0	-544	31	4.02	4.02	10.05	10.05	-5.57	-76.9

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	97	-5394	-27	-596	0	-162	-122	4.02	4.02	10.05	10.05	-3.68	-52.0
41	97	-5416	-88	-534	0	-83	-45	4.02	4.02	10.05	10.05	-3.23	-47.4
42	97	-5475	-86	-598	0	-163	-47	4.02	4.02	10.05	10.05	-3.64	-52.7
43	97	-5245	16	-603	0	-194	-176	4.02	4.02	10.05	10.05	-4.10	-53.5
44	97	-5335	-190	-417	0	42	86	4.02	4.02	10.05	10.05	-3.32	-45.9
45	97	-5379	-83	-607	0	-195	-50	4.02	4.02	10.05	10.05	-3.75	-53.9
46	97	-5201	-84	-480	0	-49	-48	4.02	4.02	10.05	10.05	-2.95	-43.6
47	97	-5147	-83	-467	0	-41	-49	4.02	4.02	10.05	10.05	-2.89	-42.7
49	97	-5140	-63	-487	0	-67	-75	4.02	4.02	10.05	10.05	-3.13	-44.3
50	97	-5158	-104	-450	0	-20	-22	4.02	4.02	10.05	10.05	-2.78	-41.5
51	97	-5167	-83	-488	0	-68	-50	4.02	4.02	10.05	10.05	-3.02	-44.5

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	195	-4956	-27	-596	0	418	-148	4.02	4.02	10.05	10.05	-4.62	-64.2
41	195	-4978	-88	-534	0	437	-130	4.02	4.02	10.05	10.05	-4.72	-65.5
42	195	-5036	-86	-598	0	421	-130	4.02	4.02	10.05	10.05	-4.67	-65.0
43	195	-4806	16	-603	0	394	-161	4.02	4.02	10.05	10.05	-4.42	-61.5
44	195	-4896	-190	-417	0	449	-99	4.02	4.02	10.05	10.05	-4.74	-65.6
45	195	-4940	-83	-607	0	398	-131	4.02	4.02	10.05	10.05	-4.51	-62.8
46	195	-4762	-84	-480	0	419	-130	4.02	4.02	10.05	10.05	-4.52	-62.7
47	195	-4708	-83	-467	0	414	-130	4.02	4.02	10.05	10.05	-4.47	-62.0
49	195	-4702	-63	-487	0	408	-136	4.02	4.02	10.05	10.05	-4.44	-61.6
50	195	-4720	-104	-450	0	419	-124	4.02	4.02	10.05	10.05	-4.50	-62.4
51	195	-4728	-83	-488	0	408	-131	4.02	4.02	10.05	10.05	-4.45	-61.8

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	292	-4517	-27	-596	0	999	-174	4.02	4.02	10.05	10.05	-8.50	-109.0
41	292	-4539	-88	-534	0	958	-215	4.02	4.02	10.05	10.05	-8.11	-104.7
42	292	-4598	-86	-598	0	1004	-214	4.02	4.02	10.05	10.05	-8.53	-109.5
43	292	-4368	16	-603	0	982	-145	4.02	4.02	10.05	10.05	-8.37	-107.0
44	292	-4458	-190	-417	0	856	-284	4.02	4.02	10.05	10.05	-7.20	-94.3
45	292	-4502	-83	-607	0	990	-212	4.02	4.02	10.05	10.05	-8.41	-108.0
46	292	-4324	-84	-480	0	887	-213	4.02	4.02	10.05	10.05	-7.49	-97.1
47	292	-4270	-83	-467	0	869	-212	4.02	4.02	10.05	10.05	-7.33	-95.2
49	292	-4263	-63	-487	0	883	-198	4.02	4.02	10.05	10.05	-7.46	-96.6
50	292	-4281	-104	-450	0	857	-226	4.02	4.02	10.05	10.05	-7.23	-94.1
51	292	-4290	-83	-488	0	884	-211	4.02	4.02	10.05	10.05	-7.47	-96.8

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	390	-4078	-27	-596	0	1580	-200	4.02	4.02	10.05	10.05	-14.51	332.0
41	390	-4100	-88	-534	0	1478	-301	4.02	4.02	10.05	10.05	-13.47	285.1
42	390	-4159	-86	-598	0	1587	-298	4.02	4.02	10.05	10.05	-14.55	327.8
43	390	-3929	16	-603	0	1570	-130	4.02	4.02	10.05	10.05	-14.46	341.2
44	390	-4019	-190	-417	0	1262	-469	4.02	4.02	10.05	10.05	-11.31	200.4
45	390	-4063	-83	-607	0	1582	-292	4.02	4.02	10.05	10.05	-14.53	334.3
46	390	-3885	-84	-480	0	1355	-295	4.02	4.02	10.05	10.05	-12.31	250.4
47	390	-3831	-83	-467	0	1324	-293	4.02	4.02	10.05	10.05	-12.01	241.7
49	390	-3824	-63	-487	0	1358	-260	4.02	4.02	10.05	10.05	-12.36	257.0
50	390	-3842	-104	-450	0	1296	-328	4.02	4.02	10.05	10.05	-11.72	228.9
51	390	-3851	-83	-488	0	1360	-292	4.02	4.02	10.05	10.05	-12.37	255.5

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

ASTA NUM. 60 NI 292 NF 302 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 1C
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-13060	104	-433	0	1032	254	4.02	4.02	10.05	10.05	-11.83	-164.9
41	0	-13290	-40	-342	0	905	-180	4.02	4.02	10.05	10.05	-11.33	-158.9
42	0	-13050	-38	-102	0	715	-176	4.02	4.02	10.05	10.05	-10.28	-145.5
43	0	-12030	183	-449	0	1023	508	4.02	4.02	10.05	10.05	-11.25	-156.3
44	0	-13800	-276	-199	0	710	-894	4.02	4.02	10.05	10.05	-14.84	-180.8
45	0	-12010	-55	104	0	495	-208	4.02	4.02	10.05	10.05	-8.66	-123.9
46	0	-11870	-68	-270	0	755	-236	4.02	4.02	10.05	10.05	-9.86	-138.7
47	0	-11520	-75	-253	0	718	-250	4.02	4.02	10.05	10.05	-9.50	-133.7
49	0	-11450	-27	-283	0	760	-105	4.02	4.02	10.05	10.05	-9.67	-135.7
50	0	-11800	-118	-233	0	698	-386	4.02	4.02	10.05	10.05	-9.54	-134.7
51	0	-11440	-74	-172	0	654	-248	4.02	4.02	10.05	10.05	-9.15	-129.2

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	12	-13005	85	-433	0	1086	266	4.02	4.02	10.05	10.05	-12.07	-167.7
41	12	-13232	-40	-342	0	948	-185	4.02	4.02	10.05	10.05	-11.51	-161.1
42	12	-12992	-38	-91	0	727	-181	4.02	4.02	10.05	10.05	-10.31	-145.8
43	12	-11972	151	-449	0	1079	529	4.02	4.02	10.05	10.05	-11.49	-159.3
44	12	-13742	-244	-199	0	734	-927	4.02	4.02	10.05	10.05	-15.18	-183.8
45	12	-11952	-55	122	0	480	-215	4.02	4.02	10.05	10.05	-8.57	-122.6
46	12	-11815	-68	-270	0	789	-244	4.02	4.02	10.05	10.05	-10.00	-140.4
47	12	-11465	-75	-253	0	749	-259	4.02	4.02	10.05	10.05	-9.62	-135.2
49	12	-11392	-33	-283	0	795	-109	4.02	4.02	10.05	10.05	-9.81	-137.4
50	12	-11742	-112	-233	0	727	-400	4.02	4.02	10.05	10.05	-9.66	-136.0
51	12	-11385	-74	-169	0	676	-257	4.02	4.02	10.05	10.05	-9.22	-130.1

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	25	-12950	66	-433	0	1140	275	4.02	4.02	10.05	10.05	-12.30	-170.6
41	25	-13175	-40	-342	0	990	-190	4.02	4.02	10.05	10.05	-11.69	-163.2
42	25	-12935	-38	-81	0	737	-186	4.02	4.02	10.05	10.05	-10.33	-146.0

43	25	-11915	119	-449	0	1135	546	4.02	4.02	10.05	10.05	-11.74	-162.2
44	25	-13685	-212	-199	0	759	-956	4.02	4.02	10.05	10.05	-15.49	-186.5
45	25	-11895	-55	138	0	464	-222	4.02	4.02	10.05	10.05	-8.46	-121.2
46	25	-11760	-68	-270	0	823	-253	4.02	4.02	10.05	10.05	-10.13	-142.0
47	25	-11410	-75	-253	0	781	-268	4.02	4.02	10.05	10.05	-9.75	-136.7
49	25	-11335	-39	-283	0	831	-113	4.02	4.02	10.05	10.05	-9.95	-139.2
50	25	-11685	-106	-233	0	756	-414	4.02	4.02	10.05	10.05	-9.77	-137.3
51	25	-11330	-74	-165	0	697	-267	4.02	4.02	10.05	10.05	-9.30	-130.9

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	38	-12895	47	-433	0	1194	282	4.02	4.02	10.05	10.05	-12.53	-173.5
41	38	-13118	-40	-342	0	1033	-195	4.02	4.02	10.05	10.05	-11.87	-165.4
42	38	-12878	-38	-73	0	747	-190	4.02	4.02	10.05	10.05	-10.35	-146.1
43	38	-11858	88	-449	0	1191	559	4.02	4.02	10.05	10.05	-11.98	-165.2
44	38	-13628	-180	-199	0	784	-980	4.02	4.02	10.05	10.05	-15.76	-188.8
45	38	-11838	-55	151	0	446	-228	4.02	4.02	10.05	10.05	-8.34	-119.6
46	38	-11705	-68	-270	0	857	-261	4.02	4.02	10.05	10.05	-10.27	-143.6
47	38	-11355	-75	-253	0	813	-278	4.02	4.02	10.05	10.05	-9.87	-138.2
49	38	-11278	-46	-283	0	866	-119	4.02	4.02	10.05	10.05	-10.09	-140.9
50	38	-11628	-99	-233	0	785	-426	4.02	4.02	10.05	10.05	-9.88	-138.6
51	38	-11275	-74	-163	0	717	-276	4.02	4.02	10.05	10.05	-9.37	-131.8

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	50	-12840	28	-433	0	1248	287	4.02	4.02	10.05	10.05	-12.77	-176.3
41	50	-13060	-40	-342	0	1076	-200	4.02	4.02	10.05	10.05	-12.05	-167.6
42	50	-12820	-38	-67	0	756	-195	4.02	4.02	10.05	10.05	-10.36	-146.2
43	50	-11800	56	-449	0	1247	568	4.02	4.02	10.05	10.05	-12.22	-168.1
44	50	-13570	-149	-199	0	809	-1001	4.02	4.02	10.05	10.05	-15.99	-190.7
45	50	-11780	-55	162	0	426	-235	4.02	4.02	10.05	10.05	-8.21	-118.0
46	50	-11650	-68	-270	0	890	-270	4.02	4.02	10.05	10.05	-10.41	-145.2
47	50	-11300	-75	-253	0	844	-287	4.02	4.02	10.05	10.05	-10.00	-139.7
49	50	-11220	-52	-283	0	902	-125	4.02	4.02	10.05	10.05	-10.24	-142.6
50	50	-11570	-93	-233	0	814	-438	4.02	4.02	10.05	10.05	-9.99	-140.0
51	50	-11220	-74	-161	0	737	-285	4.02	4.02	10.05	10.05	-9.44	-132.6

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

ASTA NUM. 61 NI 294 NF 325 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 10C
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-12760	1376	-250	0	-2406	1314	6.03	6.03	10.05	10.05	-14.89	-195.8
41	0	-11260	-412	-143	0	-1928	2053	6.03	6.03	10.05	10.05	-17.99	-204.3
42	0	-11240	-434	-503	0	-1414	2054	6.03	6.03	10.05	10.05	-18.00	-204.3
43	0	-13420	2649	-287	0	-2275	692	6.03	6.03	10.05	10.05	-14.18	-188.7
44	0	-9105	-3414	28	0	-1220	3297	6.03	6.03	10.05	10.05	-29.23	631.3
45	0	-10880	-367	-709	0	-621	1927	6.03	6.03	10.05	10.05	-16.87	-192.9
46	0	-10730	-282	-87	0	-1210	1847	6.03	6.03	10.05	10.05	-16.16	-185.9
47	0	-10590	-249	-73	0	-1030	1796	6.03	6.03	10.05	10.05	-15.70	-181.2
49	0	-11090	347	-109	0	-1189	1549	6.03	6.03	10.05	10.05	-13.51	-162.6
50	0	-10230	-866	-46	0	-978	2070	6.03	6.03	10.05	10.05	-18.21	225.7
51	0	-10580	-256	-193	0	-858	1796	6.03	6.03	10.05	10.05	-15.70	-181.2

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	12	-12685	1376	-250	0	-2375	1486	6.03	6.03	10.05	10.05	-14.70	-193.4
41	12	-11185	-412	-143	0	-1910	2002	6.03	6.03	10.05	10.05	-17.53	-199.9
42	12	-11165	-434	-481	0	-1353	2000	6.03	6.03	10.05	10.05	-17.52	-199.7
43	12	-13345	2649	-287	0	-2239	1024	6.03	6.03	10.05	10.05	-13.97	-186.2
44	12	-9030	-3414	28	0	-1224	2870	6.03	6.03	10.05	10.05	-25.46	503.8
45	12	-10805	-367	-672	0	-535	1881	6.03	6.03	10.05	10.05	-16.46	-188.9
46	12	-10655	-282	-87	0	-1199	1812	6.03	6.03	10.05	10.05	-15.84	-182.7
47	12	-10515	-249	-73	0	-1021	1765	6.03	6.03	10.05	10.05	-15.42	-178.5
49	12	-11015	347	-109	0	-1176	1592	6.03	6.03	10.05	10.05	-13.89	-165.9
50	12	-10155	-866	-46	0	-972	1962	6.03	6.03	10.05	10.05	-17.23	199.3
51	12	-10505	-256	-186	0	-835	1764	6.03	6.03	10.05	10.05	-15.42	-178.4

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	25	-12610	1376	-250	0	-2344	1658	6.03	6.03	10.05	10.05	-14.51	-191.1
41	25	-11110	-412	-143	0	-1892	1950	6.03	6.03	10.05	10.05	-17.07	-195.5
42	25	-11090	-434	-462	0	-1294	1946	6.03	6.03	10.05	10.05	-17.03	-195.1
43	25	-13270	2649	-287	0	-2203	1355	6.03	6.03	10.05	10.05	-13.77	-183.6
44	25	-8955	-3414	28	0	-1227	2444	6.03	6.03	10.05	10.05	-21.65	378.4
45	25	-10730	-367	-640	0	-453	1836	6.03	6.03	10.05	10.05	-16.05	-184.9
46	25	-10580	-282	-87	0	-1188	1776	6.03	6.03	10.05	10.05	-15.53	-179.6
47	25	-10440	-249	-73	0	-1012	1734	6.03	6.03	10.05	10.05	-15.15	-175.7
49	25	-10940	347	-109	0	-1162	1636	6.03	6.03	10.05	10.05	-14.27	-169.3
50	25	-10080	-866	-46	0	-967	1854	6.03	6.03	10.05	10.05	-16.25	-184.2
51	25	-10430	-256	-179	0	-812	1732	6.03	6.03	10.05	10.05	-15.13	-175.5

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	38	-12535	1376	-250	0	-2312	1830	6.03	6.03	10.05	10.05	-15.96	-190.3
41	38	-11035	-412	-143	0	-1875	1898	6.03	6.03	10.05	10.05	-16.61	-191.1
42	38	-11015	-434	-446	0	-1237	1892	6.03	6.03	10.05	10.05	-16.55	-190.5
43	38	-13195	2649	-287	0	-2167	1686	6.03	6.03	10.05	10.05	-14.76	-181.1
44	38	-8880	-3414	28	0	-1230	2017	6.03	6.03	10.05	10.05	-17.81	257.0
45	38	-10655	-367	-614	0	-375	1790	6.03	6.03	10.05	10.05	-15.64	-181.0
46	38	-10505	-282	-87	0	-1177	1741	6.03	6.03	10.05	10.05	-15.21	-176.5
47	38	-10365	-249	-73	0	-1003	1702	6.03	6.03	10.05	10.05	-14.87	-172.9
49	38	-10865	347	-109	0	-1148	1680	6.03	6.03	10.05	10.05	-14.65	-172.6
50	38	-10004	-866	-46	0	-961	1746	6.03	6.03	10.05	10.05	-15.28	-175.2
51	38	-10355	-256	-174	0	-790	1700	6.03	6.03	10.05	10.05	-14.85	-172.6

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	50	-12460	1376	-250	0	-2281	2002	6.03	6.03	10.05	10.05	-17.48	-204.2
41	50	-10960	-412	-143	0	-1857	1847	6.03	6.03	10.05	10.05	-16.14	-186.6
42	50	-10940	-434	-434	0	-1182	1838	6.03	6.03	10.05	10.05	-16.06	-185.8
43	50	-13120	2649	-287	0	-2131	2017	6.03	6.03	10.05	10.05	-17.59	-207.5

44	50	-8805	-3414	28	0	-1234	1590	6.03	6.03	10.05	10.05	-13.93	-158.5
45	50	-10580	-367	-593	0	-300	1744	6.03	6.03	10.05	10.05	-15.23	-177.0
46	50	-10430	-282	-87	0	-1166	1706	6.03	6.03	10.05	10.05	-14.90	-173.4
47	50	-10290	-249	-73	0	-994	1671	6.03	6.03	10.05	10.05	-14.59	-170.1
49	50	-10790	347	-109	0	-1135	1723	6.03	6.03	10.05	10.05	-15.04	-175.9
50	50	-9929	-866	-46	0	-955	1638	6.03	6.03	10.05	10.05	-14.31	-166.2
51	50	-10280	-256	-170	0	-768	1668	6.03	6.03	10.05	10.05	-14.56	-169.8

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

ASTA NUM. 62 NI 1543 NF 1542 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 6
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-4508	645	-526	0	-310	4700	14.07	14.07	6.03	6.03	-19.25	772.9
41	0	-395	202	-714	0	-439	6671	14.07	14.07	6.03	6.03	-26.51	1549.3
42	0	-700	215	-950	0	-452	6472	14.07	14.07	6.03	6.03	-25.81	1478.4
43	0	-8509	885	-247	0	-124	2007	14.07	14.07	6.03	6.03	-7.21	-98.5
44	0	6616	-526	-1055	0	-671	10190	14.07	14.07	6.03	6.03	-37.70	2940.9
45	0	-2162	170	-954	0	-360	4960	14.07	14.07	6.03	6.03	-20.11	1008.0
46	0	-2409	116	-470	0	-279	4464	14.07	14.07	6.03	6.03	-18.17	872.2
47	0	-2912	94	-408	0	-239	3912	14.07	14.07	6.03	6.03	-16.00	704.6
49	0	-4283	242	-346	0	-196	3255	14.07	14.07	6.03	6.03	-13.28	453.7
50	0	-1259	-41	-507	0	-305	4891	14.07	14.07	6.03	6.03	-19.67	1060.7
51	0	-3014	98	-487	0	-243	3846	14.07	14.07	6.03	6.03	-15.73	681.6

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	12	-4408	645	-526	0	-245	4780	14.07	14.07	6.03	6.03	-19.58	799.0
41	12	-295	202	-714	0	-350	6696	14.07	14.07	6.03	6.03	-26.59	1563.1
42	12	-600	215	-950	0	-333	6499	14.07	14.07	6.03	6.03	-25.89	1492.5
43	12	-8409	885	-247	0	-93	2118	14.07	14.07	6.03	6.03	-7.60	-103.3
44	12	6716	-526	-1055	0	-539	10123	14.07	14.07	6.03	6.03	-37.38	2933.2
45	12	-2062	170	-954	0	-241	4981	14.07	14.07	6.03	6.03	-20.18	1020.6
46	12	-2309	116	-470	0	-220	4478	14.07	14.07	6.03	6.03	-18.21	883.1
47	12	-2812	94	-408	0	-188	3924	14.07	14.07	6.03	6.03	-16.04	714.8
49	12	-4183	242	-346	0	-153	3285	14.07	14.07	6.03	6.03	-13.42	467.5
50	12	-1159	-41	-507	0	-242	4886	14.07	14.07	6.03	6.03	-19.63	1067.2
51	12	-2914	98	-487	0	-182	3858	14.07	14.07	6.03	6.03	-15.78	691.8

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	25	-4308	645	-526	0	-179	4861	14.07	14.07	6.03	6.03	-19.91	825.1
41	25	-195	202	-714	0	-261	6722	14.07	14.07	6.03	6.03	-26.66	1576.9
42	25	-500	215	-950	0	-215	6526	14.07	14.07	6.03	6.03	-25.97	1506.7
43	25	-8309	885	-247	0	-62	2228	14.07	14.07	6.03	6.03	-8.03	-108.3
44	25	6816	-526	-1055	0	-408	10056	14.07	14.07	6.03	6.03	-37.06	2925.6
45	25	-1962	170	-954	0	-122	5002	14.07	14.07	6.03	6.03	-20.25	1033.2
46	25	-2209	116	-470	0	-162	4493	14.07	14.07	6.03	6.03	-18.26	894.1
47	25	-2712	94	-408	0	-137	3936	14.07	14.07	6.03	6.03	-16.08	724.9
49	25	-4083	242	-346	0	-109	3316	14.07	14.07	6.03	6.03	-13.55	481.4
50	25	-1059	-41	-507	0	-178	4881	14.07	14.07	6.03	6.03	-19.59	1073.8
51	25	-2814	98	-487	0	-121	3870	14.07	14.07	6.03	6.03	-15.82	702.1

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	38	-4208	645	-526	0	-113	4942	14.07	14.07	6.03	6.03	-20.23	851.2
41	38	-95	202	-714	0	-172	6747	14.07	14.07	6.03	6.03	-26.73	1590.7
42	38	-400	215	-950	0	-96	6553	14.07	14.07	6.03	6.03	-26.05	1520.9
43	38	-8209	885	-247	0	-32	2339	14.07	14.07	6.03	6.03	-8.48	-113.6
44	38	6916	-526	-1055	0	-276	9990	14.07	14.07	6.03	6.03	-36.74	2917.9
45	38	-1862	170	-954	0	-2	5024	14.07	14.07	6.03	6.03	-20.32	1045.9
46	38	-2109	116	-470	0	-103	4508	14.07	14.07	6.03	6.03	-18.30	905.1
47	38	-2612	94	-408	0	-86	3947	14.07	14.07	6.03	6.03	-16.11	735.1
49	38	-3983	242	-346	0	-66	3346	14.07	14.07	6.03	6.03	-13.69	495.4
50	38	-959	-41	-507	0	-115	4876	14.07	14.07	6.03	6.03	-19.55	1080.3
51	38	-2714	98	-487	0	-60	3883	14.07	14.07	6.03	6.03	-15.86	712.4

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	50	-4108	645	-526	0	-48	5022	14.07	14.07	6.03	6.03	-20.55	877.4
41	50	5	202	-714	0	-82	6772	14.07	14.07	6.03	6.03	-26.80	1604.5
42	50	-300	215	-950	0	23	6580	14.07	14.07	6.03	6.03	-26.13	1535.1
43	50	-8109	885	-247	0	-1	2450	14.07	14.07	6.03	6.03	-8.95	-119.1
44	50	7016	-526	-1055	0	-144	9923	14.07	14.07	6.03	6.03	-36.42	2910.3
45	50	-1762	170	-954	0	117	5045	14.07	14.07	6.03	6.03	-20.38	1058.6
46	50	-2009	116	-470	0	-44	4522	14.07	14.07	6.03	6.03	-18.34	916.1
47	50	-2512	94	-408	0	-35	3959	14.07	14.07	6.03	6.03	-16.15	745.4
49	50	-3883	242	-346	0	-23	3376	14.07	14.07	6.03	6.03	-13.82	509.3
50	50	-859	-41	-507	0	-52	4871	14.07	14.07	6.03	6.03	-19.50	1086.9
51	50	-2614	98	-487	0	0	3895	14.07	14.07	6.03	6.03	-15.90	722.7

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

ASTA NUM. 63 NI 1542 NF 78 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 6A
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-9261	1917	-257	0	-48	6030	14.07	14.07	6.03	6.03	-24.46	751.6
41	0	-5313	1674	-152	0	-82	7688	14.07	14.07	6.03	6.03	-31.41	1415.1
42	0	-5631	1670	-848	0	23	7507	14.07	14.07	6.03	6.03	-30.70	1349.0
43	0	-12490	1725	-336	0	-1	3408	14.07	14.07	6.03	6.03	-12.29	-165.6
44	0	1291	1329	22	0	-144	10710	14.07	14.07	6.03	6.03	-41.99	2638.3
45	0	-6441	1313	-1322	0	117	5870	14.07	14.07	6.03	6.03	-24.03	907.5
46	0	-6269	1109	-167	0	-44	5261	14.07	14.07	6.03	6.03	-21.52	778.5
47	0	-6509	967	-171	0	-35	4654	14.07	14.07	6.03	6.03	-18.96	622.6

49	0	-7825	1048	-206	0	-23	4101	14.07	14.07	6.03	6.03	-16.36	415.2
50	0	-5068	969	-134	0	-52	5561	14.07	14.07	6.03	6.03	-22.78	933.7
51	0	-6615	966	-403	0	0	4594	14.07	14.07	6.03	6.03	-18.69	601.8

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	12	-9161	1917	-257	0	-15	6270	14.07	14.07	6.03	6.03	-25.49	812.5
41	12	-5213	1674	-152	0	-63	7897	14.07	14.07	6.03	6.03	-32.24	1471.7
42	12	-5531	1670	-848	0	129	7716	14.07	14.07	6.03	6.03	-31.53	1405.4
43	12	-12390	1725	-336	0	41	3624	14.07	14.07	6.03	6.03	-13.18	-176.1
44	12	1391	1329	22	0	-146	10875	14.07	14.07	6.03	6.03	-42.61	2685.3
45	12	-6341	1313	-1322	0	282	6034	14.07	14.07	6.03	6.03	-24.71	952.7
46	12	-6169	1109	-167	0	-23	5400	14.07	14.07	6.03	6.03	-22.10	817.5
47	12	-6409	967	-171	0	-13	4775	14.07	14.07	6.03	6.03	-19.47	657.0
49	12	-7725	1048	-206	0	3	4232	14.07	14.07	6.03	6.03	-16.95	449.7
50	12	-4968	969	-134	0	-35	5682	14.07	14.07	6.03	6.03	-23.27	969.4
51	12	-6515	966	-403	0	51	4714	14.07	14.07	6.03	6.03	-19.21	636.0

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	25	-9061	1917	-257	0	17	6510	14.07	14.07	6.03	6.03	-26.52	873.7
41	25	-5113	1674	-152	0	-44	8106	14.07	14.07	6.03	6.03	-33.07	1528.5
42	25	-5431	1670	-848	0	235	7924	14.07	14.07	6.03	6.03	-32.37	1462.0
43	25	-12290	1725	-336	0	83	3840	14.07	14.07	6.03	6.03	-14.10	-186.9
44	25	1491	1329	22	0	-149	11040	14.07	14.07	6.03	6.03	-43.23	2732.2
45	25	-6241	1313	-1322	0	447	6198	14.07	14.07	6.03	6.03	-25.39	998.0
46	25	-6069	1109	-167	0	-2	5538	14.07	14.07	6.03	6.03	-22.68	856.7
47	25	-6309	967	-171	0	8	4896	14.07	14.07	6.03	6.03	-19.99	691.5
49	25	-7625	1048	-206	0	28	4363	14.07	14.07	6.03	6.03	-17.54	484.6
50	25	-4868	969	-134	0	-18	5804	14.07	14.07	6.03	6.03	-23.76	1005.1
51	25	-6415	966	-403	0	101	4835	14.07	14.07	6.03	6.03	-19.73	670.4

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	38	-8961	1917	-257	0	49	6749	14.07	14.07	6.03	6.03	-27.54	935.3
41	38	-5013	1674	-152	0	-25	8316	14.07	14.07	6.03	6.03	-33.90	1585.3
42	38	-5331	1670	-848	0	341	8133	14.07	14.07	6.03	6.03	-33.20	1518.5
43	38	-12190	1725	-336	0	126	4055	14.07	14.07	6.03	6.03	-15.06	-198.0
44	38	1591	1329	22	0	-152	11205	14.07	14.07	6.03	6.03	-43.85	2779.2
45	38	-6141	1313	-1322	0	612	6362	14.07	14.07	6.03	6.03	-26.06	1043.5
46	38	-5969	1109	-167	0	19	5676	14.07	14.07	6.03	6.03	-23.25	896.0
47	38	-6209	967	-171	0	30	5016	14.07	14.07	6.03	6.03	-20.50	726.2
49	38	-7525	1048	-206	0	54	4494	14.07	14.07	6.03	6.03	-18.13	519.9
50	38	-4768	969	-134	0	-1	5925	14.07	14.07	6.03	6.03	-24.25	1040.8
51	38	-6315	966	-403	0	152	4956	14.07	14.07	6.03	6.03	-20.24	704.9

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	50	-8861	1917	-257	0	81	6989	14.07	14.07	6.03	6.03	-28.55	997.2
41	50	-4913	1674	-152	0	-6	8525	14.07	14.07	6.03	6.03	-34.73	1642.1
42	50	-5231	1670	-848	0	447	8342	14.07	14.07	6.03	6.03	-34.03	1575.2
43	50	-12090	1725	-336	0	168	4271	14.07	14.07	6.03	6.03	-16.04	232.7
44	50	1691	1329	22	0	-155	11370	14.07	14.07	6.03	6.03	-44.47	2826.2
45	50	-6041	1313	-1322	0	778	6526	14.07	14.07	6.03	6.03	-26.73	1089.0
46	50	-5869	1109	-167	0	39	5815	14.07	14.07	6.03	6.03	-23.82	935.4
47	50	-6109	967	-171	0	51	5137	14.07	14.07	6.03	6.03	-21.01	761.0
49	50	-7425	1048	-206	0	80	4625	14.07	14.07	6.03	6.03	-18.71	555.5
50	50	-4668	969	-134	0	16	6046	14.07	14.07	6.03	6.03	-24.73	1076.6
51	50	-6215	966	-403	0	202	5076	14.07	14.07	6.03	6.03	-20.75	739.5

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

ASTA NUM. 64 NI 1581 NF 121 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 5A
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-5096	3168	250	0	-76	10760	14.07	14.07	8.04	8.04	-38.11	1633.4
41	0	292	3145	243	0	-88	13530	14.07	14.07	8.04	8.04	-46.29	2436.4
42	0	310	3158	-424	0	33	13540	14.07	14.07	8.04	8.04	-46.31	2439.2
43	0	-10480	2538	196	0	-47	6185	14.07	14.07	8.04	8.04	-22.29	547.8
44	0	9510	3218	236	0	-111	18610	14.07	14.07	10.05	10.05	-53.50	3120.2
45	0	-1475	2521	-928	0	133	10820	14.07	14.07	8.04	8.04	-37.50	1849.6
46	0	-2583	2112	148	0	-56	9152	14.07	14.07	8.04	8.04	-32.05	1488.1
47	0	-3302	1853	124	0	-48	8058	14.07	14.07	8.04	8.04	-28.44	1252.1
49	0	-5098	1861	126	0	-44	7137	14.07	14.07	8.04	8.04	-25.54	988.5
50	0	-1099	1997	134	0	-56	9621	14.07	14.07	8.04	8.04	-33.29	1656.9
51	0	-3296	1858	-98	0	-8	8064	14.07	14.07	8.04	8.04	-28.46	1253.5

apost= 10.05 aant= 10.05 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	12	-4996	3168	250	0	-107	11158	14.07	14.07	8.04	8.04	-39.46	1709.9
41	12	392	3145	243	0	-118	13922	14.07	14.07	8.04	8.04	-47.60	2512.4
42	12	410	3158	-424	0	86	13935	14.07	14.07	8.04	8.04	-47.64	2515.6
43	12	-10380	2538	196	0	-72	6502	14.07	14.07	8.04	8.04	-23.47	605.9
44	12	9610	3218	236	0	-140	19012	14.07	14.07	10.05	10.05	-54.70	3182.7
45	12	-1375	2521	-928	0	249	11135	14.07	14.07	8.04	8.04	-38.56	1911.7
46	12	-2483	2112	148	0	-74	9416	14.07	14.07	8.04	8.04	-32.94	1541.1
47	12	-3202	1853	124	0	-63	8290	14.07	14.07	8.04	8.04	-29.22	1299.1
49	12	-4998	1861	126	0	-59	7370	14.07	14.07	8.04	8.04	-26.34	1035.2
50	12	-999	1997	134	0	-73	9871	14.07	14.07	8.04	8.04	-34.12	1707.3
51	12	-3196	1858	-98	0	5	8296	14.07	14.07	8.04	8.04	-29.24	1300.6

apost= 10.05 aant= 10.05 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	25	-4896	3168	250	0	-138	11555	14.07	14.07	8.04	8.04	-40.81	1786.4
41	25	492	3145	243	0	-148	14315	14.07	14.07	8.04	8.04	-48.91	2588.4
42	25	510	3158	-424	0	139	14330	14.07	14.07	8.04	8.04	-48.96	2592.1
43	25	-10280	2538	196	0	-96	6820	14.07	14.07	8.04	8.04	-24.64	664.5
44	25	9710	3218	236	0	-170	19415	14.07	14.07	10.05	10.05	-55.91	3245.1
45	25	-1275	2521	-928	0	365	11450	14.07	14.07	8.04	8.04	-39.61	1973.7
46	25	-2383	2112	148	0	-93	9681	14.07	14.07	8.04	8.04	-33.82	1594.0
47	25	-3102	1853	124	0	-79	8522	14.07	14.07	8.04	8.04	-30.00	1346.1
49	25	-4898	1861	126	0	-75	7602	14.07	14.07	8.04	8.04	-27.13	1082.1

50	25	-899	1997	134	0	-90	10120	14.07	14.07	8.04	8.04	-34.95	1757.7
51	25	-3096	1858	-98	0	17	8528	14.07	14.07	8.04	8.04	-30.02	1347.7

apost= 10.05 aant= 10.05 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	38	-4796	3168	250	0	-169	11952	14.07	14.07	8.04	8.04	-42.17	1863.0
41	38	592	3145	243	0	-179	14708	14.07	14.07	8.04	8.04	-50.23	2664.4
42	38	610	3158	-424	0	192	14725	14.07	14.07	8.04	8.04	-50.28	2668.5
43	38	-10180	2538	196	0	-121	7137	14.07	14.07	8.04	8.04	-25.80	723.7
44	38	9810	3218	236	0	-199	19818	14.07	14.07	10.05	10.05	-57.11	3307.6
45	38	-1175	2521	-928	0	481	11765	14.07	14.07	8.04	8.04	-40.66	2035.8
46	38	-2283	2112	148	0	-111	9946	14.07	14.07	8.04	8.04	-34.71	1647.0
47	38	-3002	1853	124	0	-94	8753	14.07	14.07	8.04	8.04	-30.77	1393.1
49	38	-4798	1861	126	0	-91	7834	14.07	14.07	8.04	8.04	-27.93	1128.9
50	38	-799	1997	134	0	-107	10370	14.07	14.07	8.04	8.04	-35.78	1808.1
51	38	-2996	1858	-98	0	29	8761	14.07	14.07	8.04	8.04	-30.80	1394.8

apost= 10.05 aant= 10.05 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	50	-4696	3168	250	0	-201	12350	14.07	14.07	8.04	8.04	-43.51	1939.6
41	50	692	3145	243	0	-209	15100	14.07	14.07	8.04	8.04	-51.54	2740.4
42	50	710	3158	-424	0	245	15120	14.07	14.07	8.04	8.04	-51.61	2745.0
43	50	-10080	2538	196	0	-146	7454	14.07	14.07	8.04	8.04	-26.95	783.2
44	50	9910	3218	236	0	-228	20220	14.07	14.07	10.05	10.05	-58.31	3370.1
45	50	-1075	2521	-928	0	597	12080	14.07	14.07	8.04	8.04	-41.71	2097.9
46	50	-2183	2112	148	0	-130	10210	14.07	14.07	8.04	8.04	-35.59	1700.0
47	50	-2902	1853	124	0	-110	8985	14.07	14.07	8.04	8.04	-31.55	1440.2
49	50	-4698	1861	126	0	-107	8067	14.07	14.07	8.04	8.04	-28.72	1175.8
50	50	-699	1997	134	0	-123	10620	14.07	14.07	8.04	8.04	-36.60	1858.6
51	50	-2896	1858	-98	0	42	8993	14.07	14.07	8.04	8.04	-31.58	1441.9

apost= 10.05 aant= 10.05 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

ASTA NUM. 65 NI 1601 NF 164 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 4A
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-3981	3407	356	0	-58	11890	14.07	14.07	10.05	10.05	-37.45	1528.5
41	0	1833	3407	347	0	-59	14940	14.07	14.07	10.05	10.05	-45.14	2232.5
42	0	1741	3375	-258	0	50	14830	14.07	14.07	10.05	10.05	-44.83	2212.4
43	0	-9977	2710	292	0	-46	6824	14.07	14.07	10.05	10.05	-22.48	554.3
44	0	11820	3529	338	0	-62	20550	14.07	14.07	10.05	10.05	-58.51	3508.2
45	0	-441	2657	-732	0	134	11740	14.07	14.07	10.05	10.05	-36.06	1667.5
46	0	-1560	2292	233	0	-40	10100	14.07	14.07	10.05	10.05	-31.36	1380.6
47	0	-2408	2014	204	0	-35	8887	14.07	14.07	10.05	10.05	-27.86	1167.9
49	0	-4346	2014	208	0	-35	7869	14.07	14.07	10.05	10.05	-25.15	935.7
50	0	13	2177	217	0	-38	10610	14.07	14.07	10.05	10.05	-32.46	1525.9
51	0	-2439	2003	3	0	1	8852	14.07	14.07	10.05	10.05	-27.76	1161.5

apost= 10.05 aant= 10.05 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	12	-3881	3407	356	0	-103	12315	14.07	14.07	10.05	10.05	-38.74	1594.0
41	12	1933	3407	347	0	-103	15365	14.07	14.07	10.05	10.05	-46.40	2298.2
42	12	1841	3375	-258	0	82	15252	14.07	14.07	10.05	10.05	-46.09	2277.8
43	12	-9877	2710	292	0	-82	7163	14.07	14.07	10.05	10.05	-23.57	604.9
44	12	11920	3529	338	0	-104	20992	14.07	14.07	10.05	10.05	-59.84	3576.3
45	12	-341	2657	-732	0	226	12072	14.07	14.07	10.05	10.05	-37.05	1719.9
46	12	-1460	2292	233	0	-69	10385	14.07	14.07	10.05	10.05	-32.20	1426.1
47	12	-2308	2014	204	0	-60	9139	14.07	14.07	10.05	10.05	-28.61	1208.6
49	12	-4246	2014	208	0	-61	8121	14.07	14.07	10.05	10.05	-25.91	976.1
50	12	113	2177	217	0	-65	10882	14.07	14.07	10.05	10.05	-33.27	1569.7
51	12	-2339	2003	3	0	1	9102	14.07	14.07	10.05	10.05	-28.50	1202.0

apost= 10.05 aant= 10.05 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	25	-3781	3407	356	0	-147	12740	14.07	14.07	10.05	10.05	-40.02	1659.5
41	25	2033	3407	347	0	-146	15790	14.07	14.07	10.05	10.05	-47.67	2363.9
42	25	1941	3375	-258	0	114	15675	14.07	14.07	10.05	10.05	-47.35	2343.1
43	25	-9777	2710	292	0	-119	7502	14.07	14.07	10.05	10.05	-24.66	655.8
44	25	12020	3529	338	0	-147	21435	14.07	14.07	10.05	10.05	-61.17	3644.5
45	25	-241	2657	-732	0	317	12405	14.07	14.07	10.05	10.05	-38.03	1772.3
46	25	-1360	2292	233	0	-98	10670	14.07	14.07	10.05	10.05	-33.05	1471.7
47	25	-2208	2014	204	0	-86	9390	14.07	14.07	10.05	10.05	-29.35	1249.3
49	25	-4146	2014	208	0	-86	8372	14.07	14.07	10.05	10.05	-26.67	1016.6
50	25	213	2177	217	0	-92	11155	14.07	14.07	10.05	10.05	-34.07	1613.4
51	25	-2239	2003	3	0	1	9353	14.07	14.07	10.05	10.05	-29.25	1242.5

apost= 10.05 aant= 10.05 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	38	-3681	3407	356	0	-192	13165	14.07	14.07	10.05	10.05	-41.30	1725.0
41	38	2133	3407	347	0	-189	16215	14.07	14.07	10.05	10.05	-48.94	2429.7
42	38	2041	3375	-258	0	146	16098	14.07	14.07	10.05	10.05	-48.61	2408.5
43	38	-9677	2710	292	0	-155	7840	14.07	14.07	10.05	10.05	-25.74	707.0
44	38	12120	3529	338	0	-189	21878	14.07	14.07	12.06	12.06	-56.57	3101.1
45	38	-141	2657	-732	0	409	12738	14.07	14.07	10.05	10.05	-39.02	1824.7
46	38	-1260	2292	233	0	-127	10955	14.07	14.07	10.05	10.05	-33.89	1517.2
47	38	-2108	2014	204	0	-112	9642	14.07	14.07	10.05	10.05	-30.10	1290.0
49	38	-4046	2014	208	0	-112	8624	14.07	14.07	10.05	10.05	-27.42	1057.1
50	38	313	2177	217	0	-119	11428	14.07	14.07	10.05	10.05	-34.87	1657.2
51	38	-2139	2003	3	0	0	9604	14.07	14.07	10.05	10.05	-29.99	1283.0

apost= 10.05 aant= 10.05 ainf= 8.04 asup= 8.04 (e arm. base= 4 X 2.01)

40	50	-3581	3407	356	0	-237	13590	14.07	14.07	10.05	10.05	-42.58	1790.6
41	50	2233	3407	347	0	-233	16640	14.07	14.07	10.05	10.05	-50.21	2495.4
42	50	2141	3375	-258	0	178	16520	14.07	14.07	10.05	10.05	-49.87	2473.9
43	50	-9577	2710	292	0	-192	8179	14.07	14.07	10.05	10.05	-26.81	758.5
44	50	12220	3529	338	0	-231	22320	14.07	14.07	12.06	12.06	-57.77	3158.1
45	50	-41	2657	-732	0	500	13070	14.07	14.07	10.05	10.05	-40.01	1877.1
46	50	-1160	2292	233	0	-156	11240	14.07	14.07	10.05	10.05	-34.74	1562.7
47	50	-2008	2014	204	0	-137	9894	14.07	14.07	10.05	10.05	-30.84	1330.7
49	50	-3946	2014	208	0	-138	8876	14.07	14.07	10.05	10.05	-28.18	1097.6
50	50	413	2177	217	0	-146	11700	14.07	14.07	10.05	10.05	-35.68	1701.0

51	50	-2039	2003	3	0	-0	9854	14.07	14.07	10.05	10.05	-30.73	1323.5

apost= 10.05 aant= 10.05 ainf= 8.04 asup= 8.04 (e arm. base= 4 X 2.01)

ASTA NUM. 66 NI 1621 NF 207 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 3A
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-5409	3084	450	0	-42	10430	14.07	14.07	8.04	8.04	-37.02	1557.2
41	0	380	3121	428	0	-34	13510	14.07	14.07	8.04	8.04	-46.19	2437.9
42	0	385	3122	-141	0	65	13520	14.07	14.07	8.04	8.04	-46.22	2440.0
43	0	-11100	2416	382	0	-41	5626	14.07	14.07	8.04	8.04	-20.14	428.0
44	0	10270	3293	403	0	-22	19130	14.07	14.07	10.05	10.05	-54.79	3230.9
45	0	-1441	2479	-603	0	137	10780	14.07	14.07	8.04	8.04	-37.36	1844.4
46	0	-2547	2091	297	0	-24	9120	14.07	14.07	8.04	8.04	-31.93	1484.4
47	0	-3279	1833	265	0	-22	8021	14.07	14.07	8.04	8.04	-28.31	1246.8
49	0	-5208	1821	272	0	-24	6993	14.07	14.07	8.04	8.04	-25.05	956.9
50	0	-935	1997	276	0	-20	9693	14.07	14.07	8.04	8.04	-33.49	1679.2
51	0	-3277	1834	75	0	11	8023	14.07	14.07	8.04	8.04	-28.31	1247.3

apost= 10.05 aant= 10.05 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	12	-5309	3084	450	0	-98	10815	14.07	14.07	8.04	8.04	-38.34	1631.3
41	12	480	3121	428	0	-88	13900	14.07	14.07	8.04	8.04	-47.50	2513.4
42	12	485	3122	-141	0	82	13910	14.07	14.07	8.04	8.04	-47.53	2515.5
43	12	-11000	2416	382	0	-89	5928	14.07	14.07	8.04	8.04	-21.29	481.5
44	12	10370	3293	403	0	-72	19542	14.07	14.07	10.05	10.05	-56.02	3294.8
45	12	-1341	2479	-603	0	212	11090	14.07	14.07	8.04	8.04	-38.39	1905.6
46	12	-2447	2091	297	0	-61	9382	14.07	14.07	8.04	8.04	-32.81	1537.0
47	12	-3179	1833	265	0	-55	8250	14.07	14.07	8.04	8.04	-29.08	1293.3
49	12	-5108	1821	272	0	-58	7220	14.07	14.07	8.04	8.04	-25.83	1002.8
50	12	-835	1997	276	0	-55	9942	14.07	14.07	8.04	8.04	-34.32	1729.5
51	12	-3177	1834	75	0	2	8252	14.07	14.07	8.04	8.04	-29.08	1293.8

apost= 10.05 aant= 10.05 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	25	-5209	3084	450	0	-154	11200	14.07	14.07	8.04	8.04	-39.65	1705.6
41	25	580	3121	428	0	-141	14290	14.07	14.07	8.04	8.04	-48.80	2589.0
42	25	585	3122	-141	0	100	14300	14.07	14.07	8.04	8.04	-48.83	2591.1
43	25	-10900	2416	382	0	-136	6230	14.07	14.07	8.04	8.04	-22.43	535.9
44	25	10470	3293	403	0	-122	19955	14.07	14.07	10.05	10.05	-57.25	3358.6
45	25	-1241	2479	-603	0	288	11400	14.07	14.07	8.04	8.04	-39.43	1966.8
46	25	-2347	2091	297	0	-98	9645	14.07	14.07	8.04	8.04	-33.69	1589.6
47	25	-3079	1833	265	0	-88	8480	14.07	14.07	8.04	8.04	-29.85	1339.9
49	25	-5008	1821	272	0	-92	7448	14.07	14.07	8.04	8.04	-26.61	1048.6
50	25	-735	1997	276	0	-89	10192	14.07	14.07	8.04	8.04	-35.15	1779.8
51	25	-3077	1834	75	0	-7	8482	14.07	14.07	8.04	8.04	-29.85	1340.4

apost= 10.05 aant= 10.05 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	38	-5109	3084	450	0	-211	11585	14.07	14.07	10.05	10.05	-36.77	1434.4
41	38	680	3121	428	0	-195	14680	14.07	14.07	10.05	10.05	-44.71	2141.7
42	38	685	3122	-141	0	118	14690	14.07	14.07	10.05	10.05	-44.74	2143.4
43	38	-10800	2416	382	0	-184	6532	14.07	14.07	10.05	10.05	-21.55	483.4
44	38	10570	3293	403	0	-173	20368	14.07	14.07	10.05	10.05	-58.49	3422.5
45	38	-1141	2479	-603	0	363	11710	14.07	14.07	10.05	10.05	-36.17	1631.1
46	38	-2247	2091	297	0	-136	9908	14.07	14.07	10.05	10.05	-30.95	1321.8
47	38	-2979	1833	265	0	-121	8709	14.07	14.07	10.05	10.05	-27.45	1116.7
49	38	-4908	1821	272	0	-126	7676	14.07	14.07	10.05	10.05	-24.65	883.5
50	38	-635	1997	276	0	-124	10441	14.07	14.07	10.05	10.05	-32.14	1471.8
51	38	-2977	1834	75	0	-17	8711	14.07	14.07	10.05	10.05	-27.45	1117.1

apost= 10.05 aant= 10.05 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	50	-5009	3084	450	0	-267	11970	14.07	14.07	10.05	10.05	-37.93	1494.1
41	50	780	3121	428	0	-248	15070	14.07	14.07	10.05	10.05	-45.87	2202.4
42	50	785	3122	-141	0	135	15080	14.07	14.07	10.05	10.05	-45.90	2204.1
43	50	-10700	2416	382	0	-232	6834	14.07	14.07	10.05	10.05	-22.53	528.1
44	50	10670	3293	403	0	-223	20780	14.07	14.07	10.05	10.05	-59.72	3486.4
45	50	-1041	2479	-603	0	438	12020	14.07	14.07	10.05	10.05	-37.09	1680.3
46	50	-2147	2091	297	0	-173	10170	14.07	14.07	10.05	10.05	-31.73	1364.0
47	50	-2879	1833	265	0	-154	8938	14.07	14.07	10.05	10.05	-28.13	1154.1
49	50	-4808	1821	272	0	-160	7903	14.07	14.07	10.05	10.05	-25.34	920.3
50	50	-535	1997	276	0	-158	10690	14.07	14.07	10.05	10.05	-32.87	1512.2
51	50	-2877	1834	75	0	-26	8940	14.07	14.07	10.05	10.05	-28.13	1154.5

apost= 10.05 aant= 10.05 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

ASTA NUM. 67 NI 1641 NF 250 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 2A
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-10810	1692	542	0	37	5197	14.07	14.07	6.03	6.03	-20.53	473.9
41	0	-5366	1785	432	0	48	8082	14.07	14.07	6.03	6.03	-33.00	1503.9
42	0	-5276	1829	-111	0	146	8206	14.07	14.07	6.03	6.03	-33.49	1539.8
43	0	-15110	1240	540	0	19	1636	14.07	14.07	6.03	6.03	-7.86	-111.6
44	0	3737	2004	262	0	68	13170	14.07	14.07	6.03	6.03	-50.87	3414.6
45	0	-5895	1468	-548	0	201	6652	14.07	14.07	6.03	6.03	-27.24	1129.1
46	0	-6451	1161	312	0	31	5464	14.07	14.07	6.03	6.03	-22.35	812.7
47	0	-6722	1005	282	0	26	4809	14.07	14.07	6.03	6.03	-19.59	643.6
49	0	-8536	974	318	0	23	3847	14.07	14.07	6.03	6.03	-15.06	321.2
50	0	-4766	1127	263	0	32	6153	14.07	14.07	6.03	6.03	-25.17	1094.6
51	0	-6693	1019	101	0	59	4850	14.07	14.07	6.03	6.03	-19.76	654.9

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	12	-10710	1692	542	0	-30	5408	14.07	14.07	6.03	6.03	-21.49	524.4
41	12	-5266	1785	432	0	-6	8305	14.07	14.07	6.03	6.03	-33.88	1563.9
42	12	-5176	1829	-111	0	160	8434	14.07	14.07	6.03	6.03	-34.39	1601.1
43	12	-15010	1240	540	0	-48	1791	14.07	14.07	6.03	6.03	-8.15	-115.4
44	12	3837	2004	262	0	35	13420	14.07	14.07	6.03	6.03	-51.82	3481.7
45	12	-5795	1468	-548	0	269	6835	14.07	14.07	6.03	6.03	-27.98	1179.3
46	12	-6351	1161	312	0	-8	5609	14.07	14.07	6.03	6.03	-22.96	853.3
47	12	-6622	1005	282	0	-9	4934	14.07	14.07	6.03	6.03	-20.13	679.0
49	12	-8436	974	318	0	-17	3969	14.07	14.07	6.03	6.03	-15.63	351.7
50	12	-4666	1127	263	0	-0	6294	14.07	14.07	6.03	6.03	-25.73	1135.0
51	12	-6593	1019	101	0	46	4978	14.07	14.07	6.03	6.03	-20.31	690.9

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	25	-10610	1692	542	0	-98	5620	14.07	14.07	6.03	6.03	-22.44	575.8
41	25	-5166	1785	432	0	-60	8528	14.07	14.07	6.03	6.03	-34.77	1624.0
42	25	-5076	1829	-111	0	174	8663	14.07	14.07	6.03	6.03	-35.30	1662.4
43	25	-14910	1240	540	0	-116	1946	14.07	14.07	6.03	6.03	-8.45	-119.1
44	25	3937	2004	262	0	3	13670	14.07	14.07	6.03	6.03	-52.78	3548.9
45	25	-5695	1468	-548	0	338	7018	14.07	14.07	6.03	6.03	-28.72	1229.5
46	25	-6251	1161	312	0	-47	5754	14.07	14.07	6.03	6.03	-23.56	894.0
47	25	-6522	1005	282	0	-44	5060	14.07	14.07	6.03	6.03	-20.66	714.7
49	25	-8336	974	318	0	-57	4090	14.07	14.07	6.03	6.03	-16.20	382.9
50	25	-4566	1127	263	0	-33	6434	14.07	14.07	6.03	6.03	-26.29	1175.5
51	25	-6493	1019	101	0	34	5105	14.07	14.07	6.03	6.03	-20.85	727.0

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	38	-10510	1692	542	0	-166	5832	14.07	14.07	6.03	6.03	-23.39	627.9
41	38	-5066	1785	432	0	-114	8752	14.07	14.07	6.03	6.03	-35.65	1684.1
42	38	-4976	1829	-111	0	188	8892	14.07	14.07	6.03	6.03	-36.20	1723.8
43	38	-14810	1240	540	0	-184	2101	14.07	14.07	6.03	6.03	-8.74	-122.9
44	38	4037	2004	262	0	-30	13920	14.07	14.07	6.03	6.03	-53.73	3616.0
45	38	-5595	1468	-548	0	406	7202	14.07	14.07	6.03	6.03	-29.46	1279.9
46	38	-6151	1161	312	0	-86	5899	14.07	14.07	6.03	6.03	-24.16	934.8
47	38	-6422	1005	282	0	-79	5186	14.07	14.07	6.03	6.03	-21.19	750.4
49	38	-8236	974	318	0	-97	4212	14.07	14.07	6.03	6.03	-16.76	414.6
50	38	-4466	1127	263	0	-66	6575	14.07	14.07	6.03	6.03	-26.85	1216.0
51	38	-6393	1019	101	0	21	5232	14.07	14.07	6.03	6.03	-21.39	763.3

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	50	-10410	1692	542	0	-234	6043	14.07	14.07	6.03	6.03	-24.33	680.6
41	50	-4966	1785	432	0	-168	8975	14.07	14.07	6.03	6.03	-36.54	1744.3
42	50	-4876	1829	-111	0	202	9120	14.07	14.07	6.03	6.03	-37.11	1785.3
43	50	-14710	1240	540	0	-251	2256	14.07	14.07	6.03	6.03	-9.04	-126.8
44	50	4137	2004	262	0	-63	14170	14.07	14.07	8.04	8.04	-47.17	2776.2
45	50	-5495	1468	-548	0	475	7385	14.07	14.07	6.03	6.03	-30.20	1330.3
46	50	-6051	1161	312	0	-125	6044	14.07	14.07	6.03	6.03	-24.76	975.7
47	50	-6322	1005	282	0	-115	5311	14.07	14.07	6.03	6.03	-21.72	786.4
49	50	-8136	974	318	0	-137	4334	14.07	14.07	6.03	6.03	-17.32	446.8
50	50	-4366	1127	263	0	-99	6716	14.07	14.07	6.03	6.03	-27.41	1256.6
51	50	-6293	1019	101	0	8	5360	14.07	14.07	6.03	6.03	-21.93	799.7

apost= 10.05 aant= 10.05 ainf= 4.02 asup= 4.02 (e arm. base= 4 X 2.01)

ASTA NUM. 68 NI 1580 NF 1581 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 5
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	852	1155	-223	0	-187	9000	14.07	14.07	8.04	8.04	-30.58	1659.0
41	0	6700	678	-334	0	-255	12050	14.07	14.07	8.04	8.04	-38.79	2550.1
42	0	6731	698	-550	0	-242	12050	14.07	14.07	8.04	8.04	-38.78	2552.0
43	0	-5829	1343	-79	0	-87	4455	14.07	14.07	8.04	8.04	-16.11	477.9
44	0	16870	-93	-534	0	-378	17570	14.07	14.07	10.05	10.05	-46.73	3324.6
45	0	3968	582	-624	0	-179	9547	14.07	14.07	8.04	8.04	-31.31	1940.4
46	0	2247	470	-222	0	-167	8033	14.07	14.07	8.04	8.04	-26.78	1568.0
47	0	1134	418	-194	0	-145	7029	14.07	14.07	8.04	8.04	-23.73	1323.1
49	0	-815	577	-157	0	-122	6012	14.07	14.07	8.04	8.04	-20.84	1027.9
50	0	3725	290	-248	0	-180	8634	14.07	14.07	8.04	8.04	-28.26	1763.0
51	0	1144	425	-266	0	-141	7030	14.07	14.07	8.04	8.04	-23.73	1323.8

apost= 10.05 aant= 10.05 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	12	952	1155	-223	0	-159	9144	14.07	14.07	8.04	8.04	-31.04	1690.6
41	12	6800	678	-334	0	-213	12135	14.07	14.07	8.04	8.04	-39.04	2571.3
42	12	6831	698	-550	0	-173	12138	14.07	14.07	8.04	8.04	-39.03	2573.6
43	12	-5729	1343	-79	0	-77	4623	14.07	14.07	8.04	8.04	-16.71	512.0
44	12	16970	-93	-534	0	-311	17558	14.07	14.07	10.05	10.05	-46.63	3327.6
45	12	4068	582	-624	0	-101	9620	14.07	14.07	8.04	8.04	-31.52	1959.4
46	12	2347	470	-222	0	-139	8092	14.07	14.07	8.04	8.04	-26.94	1584.4
47	12	1234	418	-194	0	-121	7081	14.07	14.07	8.04	8.04	-23.87	1338.3
49	12	-715	577	-157	0	-103	6084	14.07	14.07	8.04	8.04	-21.06	1046.6
50	12	3825	290	-248	0	-149	8670	14.07	14.07	8.04	8.04	-28.34	1775.4
51	12	1244	425	-266	0	-107	7083	14.07	14.07	8.04	8.04	-23.88	1339.2

apost= 10.05 aant= 10.05 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	25	1052	1155	-223	0	-131	9288	14.07	14.07	8.04	8.04	-31.50	1722.2
41	25	6900	678	-334	0	-171	12220	14.07	14.07	8.04	8.04	-39.29	2592.4
42	25	6931	698	-550	0	-105	12225	14.07	14.07	8.04	8.04	-39.29	2595.2
43	25	-5629	1343	-79	0	-67	4790	14.07	14.07	8.04	8.04	-17.31	546.4
44	25	17070	-93	-534	0	-244	17545	14.07	14.07	10.05	10.05	-46.54	3330.7
45	25	4168	582	-624	0	-23	9692	14.07	14.07	8.04	8.04	-31.73	1978.3
46	25	2447	470	-222	0	-111	8150	14.07	14.07	8.04	8.04	-27.10	1600.8
47	25	1334	418	-194	0	-96	7134	14.07	14.07	8.04	8.04	-24.02	1353.5
49	25	-615	577	-157	0	-83	6156	14.07	14.07	8.04	8.04	-21.28	1065.2
50	25	3925	290	-248	0	-118	8706	14.07	14.07	8.04	8.04	-28.43	1787.8
51	25	1344	425	-266	0	-74	7136	14.07	14.07	8.04	8.04	-24.02	1354.6

apost= 10.05 aant= 10.05 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	38	1152	1155	-223	0	-103	9433	14.07	14.07	8.04	8.04	-31.97	1753.9

41	38	7000	678	-334	0	-129	12305	14.07	14.07	8.04	8.04	-39.54	2613.6
42	38	7031	698	-550	0	-36	12312	14.07	14.07	8.04	8.04	-39.55	2616.8
43	38	-5529	1343	-79	0	-57	4958	14.07	14.07	8.04	8.04	-17.91	580.8
44	38	17170	-93	-534	0	-177	17532	14.07	14.07	10.05	10.05	-46.44	3333.8
45	38	4268	582	-624	0	55	9765	14.07	14.07	8.04	8.04	-31.94	1997.2
46	38	2547	470	-222	0	-83	8209	14.07	14.07	8.04	8.04	-27.27	1617.2
47	38	1434	418	-194	0	-72	7186	14.07	14.07	8.04	8.04	-24.16	1368.7
49	38	-515	577	-157	0	-63	6228	14.07	14.07	8.04	8.04	-21.50	1083.8
50	38	4025	290	-248	0	-87	8743	14.07	14.07	8.04	8.04	-28.51	1800.3
51	38	1444	425	-266	0	-41	7190	14.07	14.07	8.04	8.04	-24.17	1370.0

apost= 10.05 aant= 10.05 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	50	1252	1155	-223	0	-76	9577	14.07	14.07	8.04	8.04	-32.43	1785.5
41	50	7100	678	-334	0	-88	12390	14.07	14.07	8.04	8.04	-39.79	2634.7
42	50	7131	698	-550	0	33	12400	14.07	14.07	8.04	8.04	-39.81	2638.4
43	50	-5429	1343	-79	0	-47	5126	14.07	14.07	8.04	8.04	-18.50	615.4
44	50	17270	-93	-534	0	-111	17520	14.07	14.07	10.05	10.05	-46.35	3336.8
45	50	4368	582	-624	0	133	9838	14.07	14.07	8.04	8.04	-32.15	2016.2
46	50	2647	470	-222	0	-56	8268	14.07	14.07	8.04	8.04	-27.43	1633.6
47	50	1534	418	-194	0	-48	7238	14.07	14.07	8.04	8.04	-24.30	1383.9
49	50	-415	577	-157	0	-44	6300	14.07	14.07	8.04	8.04	-21.71	1102.5
50	50	4125	290	-248	0	-56	8779	14.07	14.07	8.04	8.04	-28.59	1812.7
51	50	1544	425	-266	0	-8	7243	14.07	14.07	8.04	8.04	-24.32	1385.4

apost= 10.05 aant= 10.05 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

ASTA NUM. 69 NI 1600 NF 1601 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 4
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	2285	1178	134	0	9	10060	14.07	14.07	10.05	10.05	-30.03	1552.2
41	0	8629	638	107	0	-6	13430	14.07	14.07	10.05	10.05	-37.84	2335.8
42	0	8509	620	-90	0	5	13340	14.07	14.07	10.05	10.05	-37.61	2317.2
43	0	-5132	1422	130	0	19	5025	14.07	14.07	10.05	10.05	-16.40	496.8
44	0	19700	-239	66	0	-29	19510	14.07	14.07	12.06	12.06	-46.28	3120.1
45	0	5241	492	-243	0	13	10480	14.07	14.07	10.05	10.05	-30.18	1751.7
46	0	3530	454	73	0	-3	8950	14.07	14.07	10.05	10.05	-26.16	1451.2
47	0	2255	408	64	0	-3	7831	14.07	14.07	10.05	10.05	-23.20	1230.5
49	0	140	588	73	0	2	6710	14.07	14.07	10.05	10.05	-20.49	971.1
50	0	5107	256	60	0	-8	9607	14.07	14.07	10.05	10.05	-27.54	1620.1
51	0	2215	402	-1	0	1	7801	14.07	14.07	10.05	10.05	-23.13	1224.4

apost= 10.05 aant= 10.05 ainf= 8.04 asup= 8.04 (e arm. base= 4 X 2.01)

40	12	2385	1178	134	0	-8	10208	14.07	14.07	10.05	10.05	-30.45	1578.0
41	12	8729	638	107	0	-19	13510	14.07	14.07	10.05	10.05	-38.04	2352.1
42	12	8609	620	-90	0	16	13418	14.07	14.07	10.05	10.05	-37.81	2333.1
43	12	-5032	1422	130	0	3	5203	14.07	14.07	10.05	10.05	-16.95	526.1
44	12	19800	-239	66	0	-37	19480	14.07	14.07	12.06	12.06	-46.14	3120.6
45	12	5341	492	-243	0	43	10542	14.07	14.07	10.05	10.05	-30.33	1765.4
46	12	3630	454	73	0	-12	9007	14.07	14.07	10.05	10.05	-26.29	1464.1
47	12	2355	408	64	0	-11	7882	14.07	14.07	10.05	10.05	-23.32	1242.6
49	12	240	588	73	0	-7	6784	14.07	14.07	10.05	10.05	-20.68	986.3
50	12	5207	256	60	0	-15	9639	14.07	14.07	10.05	10.05	-27.59	1629.5
51	12	2315	402	-1	0	1	7851	14.07	14.07	10.05	10.05	-23.24	1236.3

apost= 10.05 aant= 10.05 ainf= 8.04 asup= 8.04 (e arm. base= 4 X 2.01)

40	25	2485	1178	134	0	-25	10355	14.07	14.07	10.05	10.05	-30.86	1603.9
41	25	8829	638	107	0	-32	13590	14.07	14.07	10.05	10.05	-38.24	2368.3
42	25	8709	620	-90	0	27	13495	14.07	14.07	10.05	10.05	-38.00	2349.0
43	25	-4932	1422	130	0	-13	5380	14.07	14.07	10.05	10.05	-17.50	555.5
44	25	19900	-239	66	0	-46	19450	14.07	14.07	12.06	12.06	-46.00	3121.0
45	25	5441	492	-243	0	74	10605	14.07	14.07	10.05	10.05	-30.48	1779.1
46	25	3730	454	73	0	-21	9064	14.07	14.07	10.05	10.05	-26.43	1476.9
47	25	2455	408	64	0	-19	7933	14.07	14.07	10.05	10.05	-23.44	1254.6
49	25	340	588	73	0	-16	6857	14.07	14.07	10.05	10.05	-20.88	1001.4
50	25	5307	256	60	0	-23	9671	14.07	14.07	10.05	10.05	-27.65	1638.8
51	25	2415	402	-1	0	1	7902	14.07	14.07	10.05	10.05	-23.36	1248.2

apost= 10.05 aant= 10.05 ainf= 8.04 asup= 8.04 (e arm. base= 4 X 2.01)

40	38	2585	1178	134	0	-42	10502	14.07	14.07	10.05	10.05	-31.28	1629.8
41	38	8929	638	107	0	-46	13670	14.07	14.07	10.05	10.05	-38.44	2384.5
42	38	8809	620	-90	0	38	13572	14.07	14.07	10.05	10.05	-38.20	2364.8
43	38	-4832	1422	130	0	-29	5558	14.07	14.07	10.05	10.05	-18.05	584.9
44	38	20000	-239	66	0	-54	19420	14.07	14.07	12.06	12.06	-45.86	3121.5
45	38	5541	492	-243	0	104	10668	14.07	14.07	10.05	10.05	-30.63	1792.8
46	38	3830	454	73	0	-31	9120	14.07	14.07	10.05	10.05	-26.56	1489.8
47	38	2555	408	64	0	-27	7984	14.07	14.07	10.05	10.05	-23.56	1266.6
49	38	440	588	73	0	-25	6930	14.07	14.07	10.05	10.05	-21.07	1016.6
50	38	5407	256	60	0	-30	9703	14.07	14.07	10.05	10.05	-27.70	1648.1
51	38	2515	402	-1	0	1	7952	14.07	14.07	10.05	10.05	-23.48	1260.1

apost= 10.05 aant= 10.05 ainf= 8.04 asup= 8.04 (e arm. base= 4 X 2.01)

40	50	2685	1178	134	0	-58	10650	14.07	14.07	10.05	10.05	-31.70	1655.6
41	50	9029	638	107	0	-59	13750	14.07	14.07	10.05	10.05	-38.65	2400.8
42	50	8909	620	-90	0	50	13650	14.07	14.07	10.05	10.05	-38.39	2380.7
43	50	-4732	1422	130	0	-46	5736	14.07	14.07	10.05	10.05	-18.59	614.4
44	50	20100	-239	66	0	-62	19390	14.07	14.07	12.06	12.06	-45.72	3121.9
45	50	5641	492	-243	0	134	10730	14.07	14.07	10.05	10.05	-30.78	1806.5
46	50	3930	454	73	0	-40	9177	14.07	14.07	10.05	10.05	-26.70	1502.7
47	50	2655	408	64	0	-35	8035	14.07	14.07	10.05	10.05	-23.68	1278.6
49	50	540	588	73	0	-35	7004	14.07	14.07	10.05	10.05	-21.26	1031.8
50	50	5507	256	60	0	-38	9735	14.07	14.07	10.05	10.05	-27.76	1657.5
51	50	2615	402	-1	0	1	8002	14.07	14.07	10.05	10.05	-23.60	1272.0

apost= 10.05 aant= 10.05 ainf= 8.04 asup= 8.04 (e arm. base= 4 X 2.01)

ASTA NUM. 70 NI 1620 NF 1621 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 3

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	453	1142	477	0	196	8687	14.07	14.07	10.05	10.05	-26.44	1269.7
41	0	6783	650	517	0	224	12050	14.07	14.07	10.05	10.05	-34.37	2050.1
42	0	6788	650	320	0	225	12060	14.07	14.07	10.05	10.05	-34.40	2051.7
43	0	-6584	1346	343	0	130	3916	14.07	14.07	10.05	10.05	-12.92	285.8
44	0	17760	-147	601	0	279	18100	14.07	14.07	10.05	10.05	-47.93	3443.3
45	0	3975	527	82	0	178	9538	14.07	14.07	10.05	10.05	-27.79	1556.6
46	0	2277	452	345	0	148	8012	14.07	14.07	10.05	10.05	-23.75	1257.6
47	0	1150	403	302	0	129	7002	14.07	14.07	10.05	10.05	-21.06	1059.8
49	0	-960	567	289	0	120	5879	14.07	14.07	10.05	10.05	-18.27	801.3
50	0	3909	268	340	0	150	8715	14.07	14.07	10.05	10.05	-25.28	1435.4
51	0	1152	403	236	0	130	7004	14.07	14.07	10.05	10.05	-21.06	1060.2
apost= 10.05 aant= 10.05 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)													
40	12	553	1142	477	0	137	8830	14.07	14.07	10.05	10.05	-26.85	1294.9
41	12	6883	650	517	0	160	12132	14.07	14.07	10.05	10.05	-34.59	2066.6
42	12	6888	650	320	0	185	12142	14.07	14.07	10.05	10.05	-34.62	2068.3
43	12	-6484	1346	343	0	88	4084	14.07	14.07	10.05	10.05	-13.47	312.3
44	12	17860	-147	601	0	204	18080	14.07	14.07	10.05	10.05	-47.81	3445.3
45	12	4075	527	82	0	168	9604	14.07	14.07	10.05	10.05	-27.95	1570.8
46	12	2377	452	345	0	105	8068	14.07	14.07	10.05	10.05	-23.89	1270.4
47	12	1250	403	302	0	92	7052	14.07	14.07	10.05	10.05	-21.18	1071.7
49	12	-860	567	289	0	84	5950	14.07	14.07	10.05	10.05	-18.46	816.0
50	12	4009	268	340	0	107	8748	14.07	14.07	10.05	10.05	-25.34	1444.9
51	12	1252	403	236	0	100	7054	14.07	14.07	10.05	10.05	-21.18	1072.1
apost= 10.05 aant= 10.05 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)													
40	25	653	1142	477	0	77	8972	14.07	14.07	10.05	10.05	-27.25	1320.0
41	25	6983	650	517	0	95	12215	14.07	14.07	10.05	10.05	-34.80	2083.2
42	25	6988	650	320	0	145	12225	14.07	14.07	10.05	10.05	-34.83	2084.9
43	25	-6384	1346	343	0	45	4252	14.07	14.07	10.05	10.05	-14.02	339.0
44	25	17960	-147	601	0	129	18060	14.07	14.07	10.05	10.05	-47.69	3447.3
45	25	4175	527	82	0	157	9670	14.07	14.07	10.05	10.05	-28.12	1585.0
46	25	2477	452	345	0	62	8125	14.07	14.07	10.05	10.05	-24.02	1283.2
47	25	1350	403	302	0	54	7102	14.07	14.07	10.05	10.05	-21.29	1083.6
49	25	-760	567	289	0	48	6020	14.07	14.07	10.05	10.05	-18.64	830.7
50	25	4109	268	340	0	65	8782	14.07	14.07	10.05	10.05	-25.41	1454.5
51	25	1352	403	236	0	71	7104	14.07	14.07	10.05	10.05	-21.30	1084.0
apost= 10.05 aant= 10.05 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)													
40	38	753	1142	477	0	18	9115	14.07	14.07	10.05	10.05	-27.66	1345.2
41	38	7083	650	517	0	30	12298	14.07	14.07	10.05	10.05	-35.01	2099.8
42	38	7088	650	320	0	105	12308	14.07	14.07	10.05	10.05	-35.04	2101.5
43	38	-6284	1346	343	0	2	4421	14.07	14.07	10.05	10.05	-14.56	366.0
44	38	18060	-147	601	0	54	18040	14.07	14.07	10.05	10.05	-47.57	3449.3
45	38	4275	527	82	0	147	9736	14.07	14.07	10.05	10.05	-28.28	1599.2
46	38	2577	452	345	0	19	8182	14.07	14.07	10.05	10.05	-24.16	1296.0
47	38	1450	403	302	0	16	7153	14.07	14.07	10.05	10.05	-21.41	1095.5
49	38	-660	567	289	0	12	6091	14.07	14.07	10.05	10.05	-18.83	845.4
50	38	4209	268	340	0	22	8816	14.07	14.07	10.05	10.05	-25.47	1464.0
51	38	1452	403	236	0	41	7155	14.07	14.07	10.05	10.05	-21.42	1095.8
apost= 10.05 aant= 10.05 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)													
40	50	853	1142	477	0	-42	9258	14.07	14.07	10.05	10.05	-28.06	1370.3
41	50	7183	650	517	0	-34	12380	14.07	14.07	10.05	10.05	-35.22	2116.4
42	50	7188	650	320	0	65	12390	14.07	14.07	10.05	10.05	-35.25	2118.1
43	50	-6184	1346	343	0	-41	4589	14.07	14.07	10.05	10.05	-15.10	393.2
44	50	18160	-147	601	0	-22	18020	14.07	14.07	10.05	10.05	-47.45	3451.3
45	50	4375	527	82	0	137	9802	14.07	14.07	10.05	10.05	-28.44	1613.4
46	50	2677	452	345	0	-24	8238	14.07	14.07	10.05	10.05	-24.30	1308.8
47	50	1550	403	302	0	-22	7203	14.07	14.07	10.05	10.05	-21.53	1107.3
49	50	-560	567	289	0	-24	6162	14.07	14.07	10.05	10.05	-19.02	860.2
50	50	4309	268	340	0	-20	8849	14.07	14.07	10.05	10.05	-25.53	1473.5
51	50	1552	403	236	0	11	7205	14.07	14.07	10.05	10.05	-21.54	1107.7
apost= 10.05 aant= 10.05 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)													

ASTA NUM. 71 NI 1640 NF 1641 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 2
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-6137	466	597	0	336	3952	14.07	14.07	6.03	6.03	-16.02	488.2
41	0	-296	206	769	0	433	7031	14.07	14.07	6.03	6.03	-27.91	1642.2
42	0	-168	233	596	0	444	7134	14.07	14.07	6.03	6.03	-28.28	1676.7
43	0	-11400	570	305	0	171	414	14.07	14.07	6.03	6.03	-4.23	-61.9
44	0	9612	-219	1086	0	611	12410	14.07	14.07	8.04	8.04	-38.63	2789.6
45	0	-1455	183	304	0	352	5717	14.07	14.07	6.03	6.03	-22.99	1241.1
46	0	-2493	95	486	0	273	4655	14.07	14.07	6.03	6.03	-18.94	910.9
47	0	-3042	68	414	0	233	4061	14.07	14.07	6.03	6.03	-16.61	730.0
49	0	-4989	154	357	0	201	3034	14.07	14.07	6.03	6.03	-12.25	356.8
50	0	-786	-3	513	0	289	5434	14.07	14.07	6.03	6.03	-21.72	1225.9
51	0	-2999	77	357	0	237	4095	14.07	14.07	6.03	6.03	-16.74	741.2
apost= 10.05 aant= 10.05 ainf= 4.02 asup= 4.02 (e arm. base= 4 X 2.01)													
40	12	-6037	466	597	0	261	4010	14.07	14.07	6.03	6.03	-16.28	507.9
41	12	-196	206	769	0	337	7057	14.07	14.07	6.03	6.03	-27.99	1656.1
42	12	-68	233	596	0	370	7163	14.07	14.07	6.03	6.03	-28.37	1691.4
43	12	-11300	570	305	0	133	485	14.07	14.07	6.03	6.03	-4.35	-63.3
44	12	9712	-219	1086	0	475	12382	14.07	14.07	8.04	8.04	-38.49	2790.7
45	12	-1355	183	304	0	315	5740	14.07	14.07	6.03	6.03	-23.06	1254.2

46	12	-2393	95	486	0	213	4667	14.07	14.07	6.03	6.03	-18.98	921.3
47	12	-2942	68	414	0	182	4070	14.07	14.07	6.03	6.03	-16.63	739.4
49	12	-4889	154	357	0	156	3054	14.07	14.07	6.03	6.03	-12.35	367.6
50	12	-686	-3	513	0	225	5434	14.07	14.07	6.03	6.03	-21.69	1233.5
51	12	-2899	77	357	0	193	4105	14.07	14.07	6.03	6.03	-16.77	750.9

apost= 10.05 aant= 10.05 ainf= 4.02 asup= 4.02 (e arm. base= 4 X 2.01)

40	25	-5937	466	597	0	187	4068	14.07	14.07	6.03	6.03	-16.54	527.7
41	25	-96	206	769	0	241	7082	14.07	14.07	6.03	6.03	-28.06	1670.1
42	25	32	233	596	0	295	7192	14.07	14.07	6.03	6.03	-28.46	1706.2
43	25	-11200	570	305	0	95	557	14.07	14.07	6.03	6.03	-4.47	-64.8
44	25	9811	-219	1086	0	340	12355	14.07	14.07	8.04	8.04	-38.34	2791.8
45	25	-1255	183	304	0	277	5762	14.07	14.07	6.03	6.03	-23.13	1267.3
46	25	-2293	95	486	0	152	4679	14.07	14.07	6.03	6.03	-19.01	931.7
47	25	-2842	68	414	0	130	4078	14.07	14.07	6.03	6.03	-16.66	748.8
49	25	-4789	154	357	0	112	3073	14.07	14.07	6.03	6.03	-12.45	378.5
50	25	-586	-3	513	0	161	5433	14.07	14.07	6.03	6.03	-21.66	1241.2
51	25	-2799	77	357	0	148	4114	14.07	14.07	6.03	6.03	-16.80	760.6

apost= 10.05 aant= 10.05 ainf= 4.02 asup= 4.02 (e arm. base= 4 X 2.01)

40	38	-5837	466	597	0	112	4127	14.07	14.07	6.03	6.03	-16.80	547.7
41	38	3	206	769	0	144	7108	14.07	14.07	6.03	6.03	-28.13	1684.0
42	38	132	233	596	0	221	7222	14.07	14.07	6.03	6.03	-28.54	1720.9
43	38	-11100	570	305	0	57	628	14.07	14.07	6.03	6.03	-4.59	-66.3
44	38	9910	-219	1086	0	204	12328	14.07	14.07	8.04	8.04	-38.19	2792.9
45	38	-1155	183	304	0	239	5785	14.07	14.07	6.03	6.03	-23.20	1280.4
46	38	-2193	95	486	0	91	4691	14.07	14.07	6.03	6.03	-19.04	942.1
47	38	-2742	68	414	0	78	4086	14.07	14.07	6.03	6.03	-16.69	758.3
49	38	-4689	154	357	0	67	3092	14.07	14.07	6.03	6.03	-12.55	389.5
50	38	-486	-3	513	0	97	5432	14.07	14.07	6.03	6.03	-21.64	1248.8
51	38	-2699	77	357	0	104	4124	14.07	14.07	6.03	6.03	-16.83	770.3

apost= 10.05 aant= 10.05 ainf= 4.02 asup= 4.02 (e arm. base= 4 X 2.01)

40	50	-5737	466	597	0	37	4185	14.07	14.07	6.03	6.03	-17.06	567.7
41	50	104	206	769	0	48	7134	14.07	14.07	6.03	6.03	-28.20	1697.9
42	50	232	233	596	0	146	7251	14.07	14.07	6.03	6.03	-28.63	1735.7
43	50	-11000	570	305	0	19	699	14.07	14.07	6.03	6.03	-4.70	-67.8
44	50	10010	-219	1086	0	68	12300	14.07	14.07	8.04	8.04	-38.04	2794.1
45	50	-1055	183	304	0	201	5808	14.07	14.07	6.03	6.03	-23.26	1293.6
46	50	-2093	95	486	0	31	4703	14.07	14.07	6.03	6.03	-19.08	952.5
47	50	-2642	68	414	0	26	4095	14.07	14.07	6.03	6.03	-16.71	767.7
49	50	-4589	154	357	0	23	3112	14.07	14.07	6.03	6.03	-12.65	400.5
50	50	-386	-3	513	0	32	5432	14.07	14.07	6.03	6.03	-21.61	1256.5
51	50	-2599	77	357	0	59	4134	14.07	14.07	6.03	6.03	-16.86	780.1

apost= 10.05 aant= 10.05 ainf= 4.02 asup= 4.02 (e arm. base= 4 X 2.01)

ASTA NUM. 72 NI 1663 NF 1664 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 31
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	621	-327	-3004	0	-1636	-5301	14.07	14.07	6.03	6.03	-20.79	1304.4
41	0	-2668	-481	-2216	0	-1209	-3604	14.07	14.07	6.03	6.03	-14.74	650.2
42	0	-2829	-448	-2422	0	-1211	-3543	14.07	14.07	6.03	6.03	-14.50	624.1
43	0	1826	-138	-3092	0	-1679	-5515	14.07	14.07	6.03	6.03	-21.20	1450.7
44	0	-8043	-749	-978	0	-536	-916	14.07	14.07	6.03	6.03	-4.28	-60.6
45	0	-3924	-340	-2123	0	-970	-2586	14.07	14.07	6.03	6.03	-10.49	325.5
46	0	-4247	-343	-1518	0	-821	-2138	14.07	14.07	6.03	6.03	-8.49	206.5
47	0	-4642	-309	-1344	0	-724	-1772	14.07	14.07	6.03	6.03	-6.75	112.6
49	0	-3546	-257	-1606	0	-866	-2337	14.07	14.07	6.03	6.03	-9.48	294.1
50	0	-5520	-380	-1183	0	-638	-1417	14.07	14.07	6.03	6.03	-5.09	-69.0
51	0	-4696	-298	-1412	0	-724	-1751	14.07	14.07	6.03	6.03	-6.64	106.4

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	12	721	-327	-3004	0	-1261	-5342	14.07	14.07	6.03	6.03	-20.92	1322.0
41	12	-2568	-481	-2216	0	-932	-3664	14.07	14.07	6.03	6.03	-14.97	671.8
42	12	-2729	-448	-2422	0	-908	-3599	14.07	14.07	6.03	6.03	-14.72	644.6
43	12	1926	-138	-3092	0	-1292	-5532	14.07	14.07	6.03	6.03	-21.23	1462.7
44	12	-7943	-749	-978	0	-414	-1009	14.07	14.07	6.03	6.03	-4.44	-62.7
45	12	-3824	-340	-2123	0	-704	-2628	14.07	14.07	6.03	6.03	-10.69	341.7
46	12	-4147	-343	-1518	0	-631	-2181	14.07	14.07	6.03	6.03	-8.70	221.7
47	12	-4542	-309	-1344	0	-556	-1810	14.07	14.07	6.03	6.03	-6.95	124.4
49	12	-3446	-257	-1606	0	-666	-2369	14.07	14.07	6.03	6.03	-9.63	308.1
50	12	-5420	-380	-1183	0	-490	-1464	14.07	14.07	6.03	6.03	-5.28	-71.2
51	12	-4596	-298	-1412	0	-548	-1788	14.07	14.07	6.03	6.03	-6.84	117.7

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	25	821	-327	-3004	0	-885	-5382	14.07	14.07	6.03	6.03	-21.04	1339.5
41	25	-2468	-481	-2216	0	-655	-3724	14.07	14.07	6.03	6.03	-15.21	693.4
42	25	-2629	-448	-2422	0	-605	-3655	14.07	14.07	6.03	6.03	-14.94	665.1
43	25	2026	-138	-3092	0	-906	-5550	14.07	14.07	6.03	6.03	-21.26	1474.8
44	25	-7843	-749	-978	0	-291	-1103	14.07	14.07	6.03	6.03	-4.61	-64.8
45	25	-3724	-340	-2123	0	-439	-2670	14.07	14.07	6.03	6.03	-10.88	358.0
46	25	-4047	-343	-1518	0	-441	-2224	14.07	14.07	6.03	6.03	-8.91	237.1
47	25	-4442	-309	-1344	0	-388	-1849	14.07	14.07	6.03	6.03	-7.15	136.7
49	25	-3346	-257	-1606	0	-465	-2402	14.07	14.07	6.03	6.03	-9.78	322.1
50	25	-5320	-380	-1183	0	-342	-1512	14.07	14.07	6.03	6.03	-5.48	-73.5
51	25	-4496	-298	-1412	0	-371	-1826	14.07	14.07	6.03	6.03	-7.03	129.5

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	38	921	-327	-3004	0	-510	-5423	14.07	14.07	6.03	6.03	-21.17	1357.1
41	38	-2368	-481	-2216	0	-378	-3785	14.07	14.07	6.03	6.03	-15.44	715.0
42	38	-2529	-448	-2422	0	-303	-3711	14.07	14.07	6.03	6.03	-15.16	685.7
43	38	2126	-138	-3092	0	-519	-5567	14.07	14.07	6.03	6.03	-21.28	1486.9
44	38	-7743	-749	-978	0	-169	-1196	14.07	14.07	6.03	6.03	-4.78	-67.0
45	38	-3624	-340	-2123	0	-174	-2713	14.07	14.07	6.03	6.03	-11.07	374.4
46	38	-3947	-343	-1518	0	-251	-2267	14.07	14.07	6.03	6.03	-9.12	252.7

47	38	-4342	-309	-1344	0	-220	-1888	14.07	14.07	6.03	6.03	-7.35	149.4
49	38	-3246	-257	-1606	0	-264	-2434	14.07	14.07	6.03	6.03	-9.93	336.3
50	38	-5220	-380	-1183	0	-194	-1560	14.07	14.07	6.03	6.03	-5.69	-75.8
51	38	-4396	-298	-1412	0	-195	-1863	14.07	14.07	6.03	6.03	-7.23	141.7

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	50	1021	-327	-3004	0	-134	-5464	14.07	14.07	6.03	6.03	-21.30	1374.6
41	50	-2268	-481	-2216	0	-101	-3845	14.07	14.07	6.03	6.03	-15.67	736.7
42	50	-2429	-448	-2422	0	0	-3767	14.07	14.07	6.03	6.03	-15.37	706.3
43	50	2226	-138	-3092	0	-132	-5584	14.07	14.07	6.03	6.03	-21.31	1499.0
44	50	-7643	-749	-978	0	-47	-1290	14.07	14.07	6.03	6.03	-4.97	-69.4
45	50	-3524	-340	-2123	0	92	-2755	14.07	14.07	6.03	6.03	-11.25	391.0
46	50	-3847	-343	-1518	0	-62	-2310	14.07	14.07	6.03	6.03	-9.32	268.6
47	50	-4242	-309	-1344	0	-52	-1926	14.07	14.07	6.03	6.03	-7.55	162.5
49	50	-3146	-257	-1606	0	-63	-2466	14.07	14.07	6.03	6.03	-10.07	350.5
50	50	-5120	-380	-1183	0	-46	-1607	14.07	14.07	6.03	6.03	-5.91	-78.3
51	50	-4296	-298	-1412	0	-18	-1900	14.07	14.07	6.03	6.03	-7.42	154.3

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

ASTA NUM. 73 NI 1664 NF 48 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 31A
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-4676	-1304	29	0	-134	-6404	14.07	14.07	6.03	6.03	-26.18	1160.2
41	0	-7379	-1208	7	0	-101	-4746	14.07	14.07	6.03	6.03	-19.24	585.7
42	0	-7573	-1198	-652	0	0	-4680	14.07	14.07	6.03	6.03	-18.92	558.3
43	0	-3238	-1093	18	0	-132	-6444	14.07	14.07	6.03	6.03	-26.19	1277.1
44	0	-11900	-1089	-36	0	-47	-2146	14.07	14.07	6.03	6.03	-8.08	-112.6
45	0	-8068	-916	-1118	0	92	-3570	14.07	14.07	6.03	6.03	-13.94	290.2
46	0	-7963	-766	-36	0	-62	-3040	14.07	14.07	6.03	6.03	-11.58	193.2
47	0	-8109	-656	-47	0	-52	-2614	14.07	14.07	6.03	6.03	-9.65	-127.4
49	0	-7208	-688	-39	0	-63	-3167	14.07	14.07	6.03	6.03	-12.35	254.7
50	0	-8939	-687	-50	0	-46	-2307	14.07	14.07	6.03	6.03	-8.29	-112.3
51	0	-8174	-652	-266	0	-18	-2592	14.07	14.07	6.03	6.03	-9.55	-126.3

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	12	-4576	-1304	29	0	-138	-6567	14.07	14.07	6.03	6.03	-26.83	1205.9
41	12	-7279	-1208	7	0	-101	-4897	14.07	14.07	6.03	6.03	-19.89	626.4
42	12	-7473	-1198	-652	0	82	-4830	14.07	14.07	6.03	6.03	-19.58	598.4
43	12	-3138	-1093	18	0	-135	-6580	14.07	14.07	6.03	6.03	-26.72	1316.9
44	12	-11800	-1089	-36	0	-42	-2282	14.07	14.07	6.03	6.03	-8.43	-116.9
45	12	-7968	-916	-1118	0	231	-3684	14.07	14.07	6.03	6.03	-14.48	319.0
46	12	-7863	-766	-36	0	-57	-3136	14.07	14.07	6.03	6.03	-12.04	215.6
47	12	-8009	-656	-47	0	-46	-2696	14.07	14.07	6.03	6.03	-10.04	132.3
49	12	-7108	-688	-39	0	-58	-3253	14.07	14.07	6.03	6.03	-12.76	277.6
50	12	-8839	-687	-50	0	-40	-2393	14.07	14.07	6.03	6.03	-8.63	-116.3
51	12	-8074	-652	-266	0	15	-2674	14.07	14.07	6.03	6.03	-9.92	-130.5

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	25	-4476	-1304	29	0	-142	-6730	14.07	14.07	6.03	6.03	-27.48	1251.7
41	25	-7179	-1208	7	0	-102	-5048	14.07	14.07	6.03	6.03	-20.55	667.3
42	25	-7373	-1198	-652	0	163	-4980	14.07	14.07	6.03	6.03	-20.23	638.8
43	25	-3038	-1093	18	0	-137	-6717	14.07	14.07	6.03	6.03	-27.25	1356.7
44	25	-11700	-1089	-36	0	-38	-2418	14.07	14.07	6.03	6.03	-8.81	-121.7
45	25	-7868	-916	-1118	0	371	-3799	14.07	14.07	6.03	6.03	-15.01	348.4
46	25	-7763	-766	-36	0	-53	-3232	14.07	14.07	6.03	6.03	-12.50	238.9
47	25	-7909	-656	-47	0	-40	-2778	14.07	14.07	6.03	6.03	-10.42	149.5
49	25	-7008	-688	-39	0	-53	-3339	14.07	14.07	6.03	6.03	-13.17	300.9
50	25	-8739	-687	-50	0	-34	-2479	14.07	14.07	6.03	6.03	-8.98	-120.4
51	25	-7974	-652	-266	0	48	-2755	14.07	14.07	6.03	6.03	-10.30	143.2

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	38	-4376	-1304	29	0	-145	-6893	14.07	14.07	6.03	6.03	-28.12	1297.6
41	38	-7079	-1208	7	0	-103	-5199	14.07	14.07	6.03	6.03	-21.20	708.5
42	38	-7273	-1198	-652	0	245	-5129	14.07	14.07	6.03	6.03	-20.88	679.5
43	38	-2938	-1093	18	0	-139	-6854	14.07	14.07	6.03	6.03	-27.78	1396.5
44	38	-11600	-1089	-36	0	-33	-2554	14.07	14.07	6.03	6.03	-9.22	-126.8
45	38	-7768	-916	-1118	0	511	-3914	14.07	14.07	6.03	6.03	-15.54	378.4
46	38	-7663	-766	-36	0	-48	-3327	14.07	14.07	6.03	6.03	-12.96	262.9
47	38	-7809	-656	-47	0	-34	-2860	14.07	14.07	6.03	6.03	-10.81	167.7
49	38	-6908	-688	-39	0	-48	-3425	14.07	14.07	6.03	6.03	-13.58	324.7
50	38	-8639	-687	-50	0	-27	-2565	14.07	14.07	6.03	6.03	-9.35	-124.7
51	38	-7874	-652	-266	0	82	-2836	14.07	14.07	6.03	6.03	-10.69	160.9

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	50	-4276	-1304	29	0	-149	-7056	14.07	14.07	6.03	6.03	-28.77	1343.5
41	50	-6979	-1208	7	0	-104	-5350	14.07	14.07	6.03	6.03	-21.84	749.9
42	50	-7173	-1198	-652	0	326	-5279	14.07	14.07	6.03	6.03	-21.52	720.4
43	50	-2838	-1093	18	0	-141	-6990	14.07	14.07	6.03	6.03	-28.31	1436.4
44	50	-11500	-1089	-36	0	-29	-2690	14.07	14.07	6.03	6.03	-9.66	-132.2
45	50	-7668	-916	-1118	0	651	-4028	14.07	14.07	6.03	6.03	-16.07	408.8
46	50	-7563	-766	-36	0	-44	-3423	14.07	14.07	6.03	6.03	-13.41	287.5
47	50	-7709	-656	-47	0	-29	-2942	14.07	14.07	6.03	6.03	-11.21	186.8
49	50	-6808	-688	-39	0	-44	-3511	14.07	14.07	6.03	6.03	-13.98	349.0
50	50	-8539	-687	-50	0	-21	-2651	14.07	14.07	6.03	6.03	-9.73	-129.0
51	50	-7774	-652	-266	0	115	-2918	14.07	14.07	6.03	6.03	-11.08	179.6

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

ASTA NUM. 74 NI 1667 NF 1665 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 30
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf

	cm		daN			daN*m			cm²			daN/cm²	
40	0	10780	-1420	-1606	0	-915	-11600	14.07	14.07	6.03	6.03	-41.10	3612.1
41	0	4626	-1316	-1145	0	-666	-8213	14.07	14.07	6.03	6.03	-30.74	2313.3
42	0	4707	-1343	-1355	0	-655	-8256	14.07	14.07	6.03	6.03	-30.87	2330.0
43	0	12400	-1235	-1689	0	-948	-12000	14.07	14.07	8.04	8.04	-35.63	2886.2
44	0	-5271	-1186	-417	0	-274	-2861	14.07	14.07	6.03	6.03	-11.45	301.0
45	0	2278	-1107	-1271	0	-514	-6423	14.07	14.07	6.03	6.03	-24.63	1701.6
46	0	654	-909	-786	0	-452	-5235	14.07	14.07	6.03	6.03	-20.52	1291.4
47	0	-339	-808	-696	0	-399	-4490	14.07	14.07	6.03	6.03	-17.87	1037.0
49	0	1713	-842	-850	0	-482	-5621	14.07	14.07	6.03	6.03	-21.67	1466.8
50	0	-1822	-832	-595	0	-347	-3792	14.07	14.07	6.03	6.03	-15.40	757.8
51	0	-312	-816	-766	0	-395	-4504	14.07	14.07	6.03	6.03	-17.91	1042.4

apost= 10.05 aant= 10.05 ainf= 4.02 asup= 4.02 (e arm. base= 4 X 2.01)

40	12	10880	-1420	-1606	0	-714	-11778	14.07	14.07	6.03	6.03	-41.77	3662.0
41	12	4726	-1316	-1145	0	-523	-8378	14.07	14.07	6.03	6.03	-31.35	2360.2
42	12	4807	-1343	-1355	0	-486	-8424	14.07	14.07	6.03	6.03	-31.50	2377.7
43	12	12500	-1235	-1689	0	-736	-12155	14.07	14.07	8.04	8.04	-36.12	2919.8
44	12	-5171	-1186	-417	0	-222	-3009	14.07	14.07	6.03	6.03	-12.12	339.8
45	12	2378	-1107	-1271	0	-355	-6562	14.07	14.07	6.03	6.03	-25.14	1742.4
46	12	754	-909	-786	0	-354	-5348	14.07	14.07	6.03	6.03	-20.93	1326.2
47	12	-239	-808	-696	0	-312	-4591	14.07	14.07	6.03	6.03	-18.24	1068.7
49	12	1813	-842	-850	0	-376	-5726	14.07	14.07	6.03	6.03	-22.04	1499.6
50	12	-1722	-832	-595	0	-273	-3896	14.07	14.07	6.03	6.03	-15.80	790.0
51	12	-212	-816	-766	0	-300	-4606	14.07	14.07	6.03	6.03	-18.29	1074.5

apost= 10.05 aant= 10.05 ainf= 4.02 asup= 4.02 (e arm. base= 4 X 2.01)

40	25	10980	-1420	-1606	0	-514	-11955	14.07	14.07	8.04	8.04	-36.29	2791.6
41	25	4826	-1316	-1145	0	-380	-8542	14.07	14.07	6.03	6.03	-31.96	2407.1
42	25	4907	-1343	-1355	0	-316	-8592	14.07	14.07	6.03	6.03	-32.12	2425.5
43	25	12600	-1235	-1689	0	-525	-12310	14.07	14.07	8.04	8.04	-36.62	2953.4
44	25	-5071	-1186	-417	0	-170	-3158	14.07	14.07	6.03	6.03	-12.77	379.1
45	25	2478	-1107	-1271	0	-196	-6700	14.07	14.07	6.03	6.03	-25.65	1783.1
46	25	854	-909	-786	0	-256	-5462	14.07	14.07	6.03	6.03	-21.35	1360.9
47	25	-139	-808	-696	0	-225	-4692	14.07	14.07	6.03	6.03	-18.61	1100.5
49	25	1913	-842	-850	0	-270	-5832	14.07	14.07	6.03	6.03	-22.42	1532.5
50	25	-1622	-832	-595	0	-199	-4000	14.07	14.07	6.03	6.03	-16.20	822.1
51	25	-112	-816	-766	0	-204	-4708	14.07	14.07	6.03	6.03	-18.67	1106.5

apost= 10.05 aant= 10.05 ainf= 4.02 asup= 4.02 (e arm. base= 4 X 2.01)

40	38	11080	-1420	-1606	0	-313	-12132	14.07	14.07	8.04	8.04	-36.86	2829.3
41	38	4926	-1316	-1145	0	-237	-8706	14.07	14.07	6.03	6.03	-32.57	2454.0
42	38	5007	-1343	-1355	0	-147	-8760	14.07	14.07	6.03	6.03	-32.75	2473.2
43	38	12700	-1235	-1689	0	-314	-12465	14.07	14.07	8.04	8.04	-37.11	2987.0
44	38	-4971	-1186	-417	0	-117	-3306	14.07	14.07	6.03	6.03	-13.42	419.0
45	38	2578	-1107	-1271	0	-37	-6838	14.07	14.07	6.03	6.03	-26.16	1823.9
46	38	954	-909	-786	0	-158	-5576	14.07	14.07	6.03	6.03	-21.76	1395.7
47	38	-39	-808	-696	0	-138	-4793	14.07	14.07	6.03	6.03	-18.98	1132.2
49	38	2013	-842	-850	0	-164	-5937	14.07	14.07	6.03	6.03	-22.80	1565.4
50	38	-1522	-832	-595	0	-124	-4104	14.07	14.07	6.03	6.03	-16.60	854.3
51	38	-12	-816	-766	0	-108	-4811	14.07	14.07	6.03	6.03	-19.04	1138.5

apost= 10.05 aant= 10.05 ainf= 4.02 asup= 4.02 (e arm. base= 4 X 2.01)

40	50	11180	-1420	-1606	0	-112	-12310	14.07	14.07	8.04	8.04	-37.44	2866.9
41	50	5026	-1316	-1145	0	-94	-8871	14.07	14.07	6.03	6.03	-33.19	2501.0
42	50	5107	-1343	-1355	0	23	-8928	14.07	14.07	6.03	6.03	-33.38	2521.0
43	50	12800	-1235	-1689	0	-103	-12620	14.07	14.07	8.04	8.04	-37.61	3020.6
44	50	-4871	-1186	-417	0	-65	-3454	14.07	14.07	6.03	6.03	-14.06	459.4
45	50	2678	-1107	-1271	0	122	-6977	14.07	14.07	6.03	6.03	-26.67	1864.6
46	50	1054	-909	-786	0	-60	-5689	14.07	14.07	6.03	6.03	-22.18	1430.5
47	50	61	-808	-696	0	-51	-4894	14.07	14.07	6.03	6.03	-19.35	1164.0
49	50	2113	-842	-850	0	-57	-6042	14.07	14.07	6.03	6.03	-23.18	1598.3
50	50	-1422	-832	-595	0	-50	-4208	14.07	14.07	6.03	6.03	-16.99	886.6
51	50	88	-816	-766	0	-12	-4913	14.07	14.07	6.03	6.03	-19.42	1170.6

apost= 10.05 aant= 10.05 ainf= 4.02 asup= 4.02 (e arm. base= 4 X 2.01)

ASTA NUM. 75 NI 1684 NF 1683 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 29
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm		daN			daN*m			cm²			daN/cm²	
40	0	12590	-1230	375	0	54	-12620	14.07	14.07	8.04	8.04	-37.73	3007.8
41	0	5899	-1197	347	0	58	-8955	14.07	14.07	6.03	6.03	-33.09	2591.3
42	0	5775	-1171	154	0	65	-8872	14.07	14.07	6.03	6.03	-32.82	2561.7
43	0	14300	-1019	319	0	39	-13060	14.07	14.07	8.04	8.04	-38.28	3190.4
44	0	-4843	-1183	311	0	66	-3169	14.07	14.07	6.03	6.03	-12.86	396.6
45	0	2946	-920	-48	0	57	-6803	14.07	14.07	6.03	6.03	-25.86	1844.9
46	0	1505	-824	230	0	38	-5734	14.07	14.07	6.03	6.03	-22.19	1477.0
47	0	406	-730	200	0	33	-4928	14.07	14.07	6.03	6.03	-19.38	1199.2
49	0	2636	-741	209	0	31	-6151	14.07	14.07	6.03	6.03	-23.40	1665.9
50	0	-1193	-774	208	0	37	-4174	14.07	14.07	6.03	6.03	-16.81	896.1
51	0	365	-721	136	0	35	-4901	14.07	14.07	6.03	6.03	-19.29	1189.5

apost= 10.05 aant= 10.05 ainf= 4.02 asup= 4.02 (e arm. base= 4 X 2.01)

40	12	12690	-1230	375	0	7	-12775	14.07	14.07	8.04	8.04	-38.23	3041.4
41	12	5999	-1197	347	0	14	-9105	14.07	14.07	6.03	6.03	-33.64	2634.8
42	12	5875	-1171	154	0	46	-9018	14.07	14.07	6.03	6.03	-33.36	2604.4
43	12	14400	-1019	319	0	-1	-13185	14.07	14.07	8.04	8.04	-38.67	3218.7
44	12	-4743	-1183	311	0	27	-3317	14.07	14.07	6.03	6.03	-13.50	436.7
45	12	3046	-920	-48	0	63	-6918	14.07	14.07	6.03	6.03	-26.28	1880.1
46	12	1605	-824	230	0	9	-5837	14.07	14.07	6.03	6.03	-22.57	1509.3
47	12	506	-730	200	0	8	-5019	14.07	14.07	6.03	6.03	-19.71	1228.7
49	12	2736	-741	209	0	5	-6244	14.07	14.07	6.03	6.03	-23.72	1695.8
50	12	-1093	-774	208	0	11	-4271	14.07	14.07	6.03	6.03	-17.18	926.7
51	12	465	-721	136	0	18	-4991	14.07	14.07	6.03	6.03	-19.61	1218.7

apost= 10.05 aant= 10.05 ainf= 4.02 asup= 4.02 (e arm. base= 4 X 2.01)

40	25	12790	-1230	375	0	-40	-12930	14.07	14.07	8.04	8.04	-38.73	3075.0
41	25	6099	-1197	347	0	-29	-9254	14.07	14.07	6.03	6.03	-34.20	2678.2
42	25	5975	-1171	154	0	26	-9165	14.07	14.07	6.03	6.03	-33.90	2647.1
43	25	14500	-1019	319	0	-41	-13310	14.07	14.07	8.04	8.04	-39.06	3246.9
44	25	-4643	-1183	311	0	-12	-3464	14.07	14.07	6.03	6.03	-14.13	477.2
45	25	3146	-920	-48	0	69	-7033	14.07	14.07	6.03	6.03	-26.69	1915.4
46	25	1705	-824	230	0	-20	-5940	14.07	14.07	6.03	6.03	-22.94	1541.6
47	25	606	-730	200	0	-17	-5110	14.07	14.07	6.03	6.03	-20.04	1258.2
49	25	2836	-741	209	0	-21	-6336	14.07	14.07	6.03	6.03	-24.05	1725.8
50	25	-993	-774	208	0	-15	-4368	14.07	14.07	6.03	6.03	-17.54	957.3
51	25	565	-721	136	0	1	-5081	14.07	14.07	6.03	6.03	-19.94	1247.9

apost= 10.05 aant= 10.05 ainf= 4.02 asup= 4.02 (e arm. base= 4 X 2.01)

40	38	12890	-1230	375	0	-86	-13085	14.07	14.07	8.04	8.04	-39.22	3108.6
41	38	6199	-1197	347	0	-73	-9404	14.07	14.07	6.03	6.03	-34.75	2721.7
42	38	6075	-1171	154	0	7	-9312	14.07	14.07	6.03	6.03	-34.44	2689.7
43	38	14600	-1019	319	0	-81	-13435	14.07	14.07	8.04	8.04	-39.45	3275.2
44	38	-4543	-1183	311	0	-51	-3612	14.07	14.07	6.03	6.03	-14.76	518.0
45	38	3246	-920	-48	0	75	-7148	14.07	14.07	6.03	6.03	-27.11	1950.6
46	38	1805	-824	230	0	-48	-6043	14.07	14.07	6.03	6.03	-23.31	1574.0
47	38	706	-730	200	0	-42	-5202	14.07	14.07	6.03	6.03	-20.37	1287.7
49	38	2936	-741	209	0	-47	-6429	14.07	14.07	6.03	6.03	-24.38	1755.7
50	38	-893	-774	208	0	-41	-4464	14.07	14.07	6.03	6.03	-17.90	988.0
51	38	665	-721	136	0	-16	-5171	14.07	14.07	6.03	6.03	-20.26	1277.1

apost= 10.05 aant= 10.05 ainf= 4.02 asup= 4.02 (e arm. base= 4 X 2.01)

40	50	12990	-1230	375	0	-133	-13240	14.07	14.07	8.04	8.04	-39.72	3142.3
41	50	6299	-1197	347	0	-116	-9554	14.07	14.07	6.03	6.03	-35.30	2765.1
42	50	6175	-1171	154	0	-12	-9458	14.07	14.07	6.03	6.03	-34.98	2732.4
43	50	14700	-1019	319	0	-120	-13560	14.07	14.07	8.04	8.04	-39.84	3303.5
44	50	-4443	-1183	311	0	-90	-3760	14.07	14.07	6.03	6.03	-15.38	559.0
45	50	3346	-920	-48	0	81	-7263	14.07	14.07	6.03	6.03	-27.52	1985.8
46	50	1905	-824	230	0	-77	-6146	14.07	14.07	6.03	6.03	-23.68	1606.3
47	50	806	-730	200	0	-67	-5293	14.07	14.07	6.03	6.03	-20.70	1317.2
49	50	3036	-741	209	0	-73	-6522	14.07	14.07	6.03	6.03	-24.70	1785.7
50	50	-793	-774	208	0	-67	-4561	14.07	14.07	6.03	6.03	-18.26	1018.6
51	50	765	-721	136	0	-33	-5261	14.07	14.07	6.03	6.03	-20.58	1306.3

apost= 10.05 aant= 10.05 ainf= 4.02 asup= 4.02 (e arm. base= 4 X 2.01)

ASTA NUM. 76 NI 1692 NF 1691 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 28
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	10870	-1653	2334	0	1009	-11660	14.07	14.07	6.03	6.03	-41.29	3633.5
41	0	4345	-1437	1806	0	770	-8059	14.07	14.07	6.03	6.03	-30.25	2254.2
42	0	4344	-1446	1613	0	764	-8061	14.07	14.07	6.03	6.03	-30.26	2254.6
43	0	12750	-1503	2309	0	1011	-12210	14.07	14.07	8.04	8.04	-36.17	2944.9
44	0	-6162	-1128	988	0	397	-2361	14.07	14.07	6.03	6.03	-9.00	151.0
45	0	1883	-1157	1109	0	602	-6217	14.07	14.07	6.03	6.03	-23.97	1621.4
46	0	410	-967	1204	0	517	-5108	14.07	14.07	6.03	6.03	-20.09	1242.1
47	0	-573	-849	1054	0	453	-4370	14.07	14.07	6.03	6.03	-17.45	990.4
49	0	1600	-921	1230	0	533	-5569	14.07	14.07	6.03	6.03	-21.50	1445.5
50	0	-2183	-846	965	0	410	-3599	14.07	14.07	6.03	6.03	-14.67	685.1
51	0	-574	-852	990	0	452	-4370	14.07	14.07	6.03	6.03	-17.45	990.3

apost= 10.05 aant= 10.05 ainf= 4.02 asup= 4.02 (e arm. base= 4 X 2.01)

40	12	10970	-1653	2334	0	717	-11865	14.07	14.07	8.04	8.04	-35.98	2775.1
41	12	4445	-1437	1806	0	544	-8239	14.07	14.07	6.03	6.03	-30.93	2304.8
42	12	4444	-1446	1613	0	562	-8242	14.07	14.07	6.03	6.03	-30.94	2305.4
43	12	12850	-1503	2309	0	722	-12398	14.07	14.07	8.04	8.04	-36.78	2984.2
44	12	-6062	-1128	988	0	273	-2502	14.07	14.07	6.03	6.03	-9.66	182.4
45	12	1983	-1157	1109	0	464	-6362	14.07	14.07	6.03	6.03	-24.50	1663.6
46	12	510	-967	1204	0	366	-5229	14.07	14.07	6.03	6.03	-20.54	1278.6
47	12	-473	-849	1054	0	322	-4476	14.07	14.07	6.03	6.03	-17.85	1023.3
49	12	1700	-921	1230	0	379	-5684	14.07	14.07	6.03	6.03	-21.92	1480.7
50	12	-2083	-846	965	0	290	-3705	14.07	14.07	6.03	6.03	-15.09	717.5
51	12	-474	-852	990	0	328	-4476	14.07	14.07	6.03	6.03	-17.85	1023.3

apost= 10.05 aant= 10.05 ainf= 4.02 asup= 4.02 (e arm. base= 4 X 2.01)

40	25	11070	-1653	2334	0	426	-12070	14.07	14.07	8.04	8.04	-36.65	2817.5
41	25	4545	-1437	1806	0	318	-8418	14.07	14.07	6.03	6.03	-31.60	2355.3
42	25	4544	-1446	1613	0	361	-8422	14.07	14.07	6.03	6.03	-31.62	2356.2
43	25	12950	-1503	2309	0	433	-12585	14.07	14.07	8.04	8.04	-37.40	3023.6
44	25	-5962	-1128	988	0	150	-2643	14.07	14.07	6.03	6.03	-10.32	215.4
45	25	2083	-1157	1109	0	325	-6506	14.07	14.07	6.03	6.03	-25.04	1705.8
46	25	610	-967	1204	0	216	-5350	14.07	14.07	6.03	6.03	-20.98	1315.1
47	25	-373	-849	1054	0	190	-4582	14.07	14.07	6.03	6.03	-18.24	1056.3
49	25	1800	-921	1230	0	226	-5800	14.07	14.07	6.03	6.03	-22.34	1515.9
50	25	-1983	-846	965	0	169	-3810	14.07	14.07	6.03	6.03	-15.50	750.0
51	25	-374	-852	990	0	204	-4583	14.07	14.07	6.03	6.03	-18.24	1056.3

apost= 10.05 aant= 10.05 ainf= 4.02 asup= 4.02 (e arm. base= 4 X 2.01)

40	38	11170	-1653	2334	0	134	-12275	14.07	14.07	8.04	8.04	-37.32	2860.0
41	38	4645	-1437	1806	0	92	-8598	14.07	14.07	6.03	6.03	-32.27	2405.8
42	38	4644	-1446	1613	0	159	-8603	14.07	14.07	6.03	6.03	-32.29	2406.9
43	38	13050	-1503	2309	0	145	-12772	14.07	14.07	8.04	8.04	-38.01	3063.0
44	38	-5862	-1128	988	0	27	-2784	14.07	14.07	6.03	6.03	-10.98	249.9
45	38	2183	-1157	1109	0	187	-6651	14.07	14.07	6.03	6.03	-25.58	1748.0
46	38	710	-967	1204	0	65	-5470	14.07	14.07	6.03	6.03	-21.43	1351.6
47	38	-273	-849	1054	0	58	-4689	14.07	14.07	6.03	6.03	-18.63	1089.2
49	38	1900	-921	1230	0	72	-5915	14.07	14.07	6.03	6.03	-22.76	1551.2
50	38	-1883	-846	965	0	48	-3916	14.07	14.07	6.03	6.03	-15.91	782.5
51	38	-274	-852	990	0	80	-4690	14.07	14.07	6.03	6.03	-18.64	1089.4

apost= 10.05 aant= 10.05 ainf= 4.02 asup= 4.02 (e arm. base= 4 X 2.01)

40	50	11270	-1653	2334	0	-158	-12480	14.07	14.07	8.04	8.04	-37.99	2902.6
41	50	4745	-1437	1806	0	-134	-8778	14.07	14.07	6.03	6.03	-32.95	2456.4
42	50	4744	-1446	1613	0	-43	-8784	14.07	14.07	6.03	6.03	-32.97	2457.7
43	50	13150	-1503	2309	0	-144	-12960	14.07	14.07	8.04	8.04	-38.62	3102.3
44	50	-5762	-1128	988	0	-97	-2925	14.07	14.07	6.03	6.03	-11.63	285.4
45	50	2283	-1157	1109	0	48	-6796	14.07	14.07	6.03	6.03	-26.11	1790.3
46	50	810	-967	1204	0	-86	-5591	14.07	14.07	6.03	6.03	-21.87	1388.1
47	50	-173	-849	1054	0	-74	-4795	14.07	14.07	6.03	6.03	-19.03	1122.2
49	50	2000	-921	1230	0	-82	-6030	14.07	14.07	6.03	6.03	-23.18	1586.4
50	50	-1783	-846	965	0	-72	-4022	14.07	14.07	6.03	6.03	-16.31	815.1
51	50	-174	-852	990	0	-43	-4796	14.07	14.07	6.03	6.03	-19.03	1122.4

apost= 10.05 aant= 10.05 ainf= 4.02 asup= 4.02 (e arm. base= 4 X 2.01)

ASTA NUM. 77 NI 1700 NF 1699 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 27
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	717	-1588	4214	0	2055	-5187	14.07	14.07	6.03	6.03	-20.31	1285.0
41	0	-3674	-1110	3105	0	1488	-2829	14.07	14.07	6.03	6.03	-11.55	397.7
42	0	-3634	-1159	2951	0	1500	-2904	14.07	14.07	6.03	6.03	-11.87	417.7
43	0	2804	-1662	4315	0	2122	-5934	14.07	14.07	6.03	6.03	-22.46	1628.1
44	0	-10890	-349	1363	0	593	972	14.07	14.07	6.03	6.03	-5.28	-74.8
45	0	-4448	-947	2209	0	1197	-2129	14.07	14.07	6.03	6.03	-8.40	193.0
46	0	-5017	-719	2083	0	989	-1510	14.07	14.07	6.03	6.03	-6.42	74.8
47	0	-5353	-621	1827	0	864	-1180	14.07	14.07	6.03	6.03	-5.59	-65.3
49	0	-3889	-780	2197	0	1054	-1966	14.07	14.07	6.03	6.03	-7.81	190.9
50	0	-6629	-517	1606	0	748	-585	14.07	14.07	6.03	6.03	-4.93	-61.7
51	0	-5340	-637	1776	0	869	-1205	14.07	14.07	6.03	6.03	-5.61	-65.6

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	12	817	-1588	4214	0	1528	-5386	14.07	14.07	6.03	6.03	-21.06	1339.9
41	12	-3574	-1110	3105	0	1100	-2968	14.07	14.07	6.03	6.03	-12.14	436.5
42	12	-3534	-1159	2951	0	1131	-3049	14.07	14.07	6.03	6.03	-12.48	458.1
43	12	2904	-1662	4315	0	1583	-6142	14.07	14.07	6.03	6.03	-23.24	1685.2
44	12	-10790	-349	1363	0	423	928	14.07	14.07	6.03	6.03	-5.12	-73.1
45	12	-4348	-947	2209	0	921	-2248	14.07	14.07	6.03	6.03	-8.95	224.0
46	12	-4917	-719	2083	0	729	-1600	14.07	14.07	6.03	6.03	-5.92	-78.0
47	12	-5253	-621	1827	0	636	-1258	14.07	14.07	6.03	6.03	-4.51	-61.6
49	12	-3789	-780	2197	0	779	-2064	14.07	14.07	6.03	6.03	-8.26	217.9
50	12	-6529	-517	1606	0	547	-649	14.07	14.07	6.03	6.03	-3.92	-50.8
51	12	-5240	-637	1776	0	647	-1284	14.07	14.07	6.03	6.03	-4.61	-62.8

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	25	917	-1588	4214	0	1002	-5584	14.07	14.07	6.03	6.03	-21.81	1394.8
41	25	-3474	-1110	3105	0	712	-3106	14.07	14.07	6.03	6.03	-12.72	475.6
42	25	-3434	-1159	2951	0	762	-3194	14.07	14.07	6.03	6.03	-13.08	498.7
43	25	3004	-1662	4315	0	1043	-6350	14.07	14.07	6.03	6.03	-24.03	1742.4
44	25	-10690	-349	1363	0	252	884	14.07	14.07	6.03	6.03	-5.00	-71.5
45	25	-4248	-947	2209	0	644	-2366	14.07	14.07	6.03	6.03	-9.49	255.7
46	25	-4817	-719	2083	0	468	-1690	14.07	14.07	6.03	6.03	-6.34	90.7
47	25	-5153	-621	1827	0	408	-1335	14.07	14.07	6.03	6.03	-4.80	-65.0
49	25	-3689	-780	2197	0	505	-2161	14.07	14.07	6.03	6.03	-8.71	245.5
50	25	-6429	-517	1606	0	346	-714	14.07	14.07	6.03	6.03	-3.38	-48.0
51	25	-5140	-637	1776	0	425	-1364	14.07	14.07	6.03	6.03	-4.91	-66.3

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	38	1017	-1588	4214	0	475	-5782	14.07	14.07	6.03	6.03	-22.56	1449.7
41	38	-3374	-1110	3105	0	323	-3245	14.07	14.07	6.03	6.03	-13.29	515.0
42	38	-3334	-1159	2951	0	393	-3338	14.07	14.07	6.03	6.03	-13.67	539.5
43	38	3104	-1662	4315	0	504	-6557	14.07	14.07	6.03	6.03	-24.81	1799.5
44	38	-10590	-349	1363	0	82	841	14.07	14.07	6.03	6.03	-4.88	-69.9
45	38	-4148	-947	2209	0	368	-2484	14.07	14.07	6.03	6.03	-10.02	288.2
46	38	-4717	-719	2083	0	208	-1779	14.07	14.07	6.03	6.03	-6.76	110.5
47	38	-5053	-621	1827	0	179	-1412	14.07	14.07	6.03	6.03	-5.11	-68.6
49	38	-3589	-780	2197	0	230	-2258	14.07	14.07	6.03	6.03	-9.14	273.7
50	38	-6329	-517	1606	0	145	-779	14.07	14.07	6.03	6.03	-3.49	-49.3
51	38	-5040	-637	1776	0	203	-1444	14.07	14.07	6.03	6.03	-5.23	-70.1

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	50	1117	-1588	4214	0	-52	-5981	14.07	14.07	6.03	6.03	-23.31	1504.7
41	50	-3274	-1110	3105	0	-65	-3384	14.07	14.07	6.03	6.03	-13.86	554.5
42	50	-3234	-1159	2951	0	25	-3483	14.07	14.07	6.03	6.03	-14.27	580.5
43	50	3204	-1662	4315	0	-36	-6765	14.07	14.07	6.03	6.03	-25.60	1856.6
44	50	-10490	-349	1363	0	-88	797	14.07	14.07	6.03	6.03	-4.76	-68.2
45	50	-4048	-947	2209	0	92	-2603	14.07	14.07	6.03	6.03	-10.55	321.2
46	50	-4617	-719	2083	0	-52	-1869	14.07	14.07	6.03	6.03	-7.20	131.9
47	50	-4953	-621	1827	0	-49	-1490	14.07	14.07	6.03	6.03	-5.44	-72.5
49	50	-3489	-780	2197	0	-45	-2356	14.07	14.07	6.03	6.03	-9.57	302.2
50	50	-6229	-517	1606	0	-55	-843	14.07	14.07	6.03	6.03	-3.59	-50.6
51	50	-4940	-637	1776	0	-19	-1523	14.07	14.07	6.03	6.03	-5.58	-74.1

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

ASTA NUM. 78 NI 1665 NF 91 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 30A
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	2947	-3346	314	0	-112	-13640	14.07	14.07	6.03	6.03	-53.03	3463.1
41	0	-1956	-2723	312	0	-94	-10060	14.07	14.07	6.03	6.03	-40.32	2230.6
42	0	-1893	-2748	-334	0	23	-10120	14.07	14.07	6.03	6.03	-40.55	2249.7

43	0	4746	-3179	240	0	-103	-13880	14.07	14.07	6.03	6.03	-53.30	3663.0
44	0	-9947	-1780	311	0	-65	-4437	14.07	14.07	6.03	6.03	-17.35	365.0
45	0	-3321	-2183	-840	0	122	-8002	14.07	14.07	6.03	6.03	-32.42	1638.9
46	0	-4307	-1791	191	0	-60	-6611	14.07	14.07	6.03	6.03	-26.98	1236.3
47	0	-4895	-1558	161	0	-51	-5749	14.07	14.07	6.03	6.03	-23.54	990.3
49	0	-3260	-1766	161	0	-57	-6943	14.07	14.07	6.03	6.03	-28.19	1393.3
50	0	-6199	-1486	176	0	-50	-5056	14.07	14.07	6.03	6.03	-20.67	736.0
51	0	-4874	-1567	-55	0	-12	-5769	14.07	14.07	6.03	6.03	-23.62	996.5

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	12	3047	-3346	314	0	-152	-14058	14.07	14.07	6.03	6.03	-54.65	3569.9
41	12	-1856	-2723	312	0	-133	-10400	14.07	14.07	6.03	6.03	-41.65	2318.9
42	12	-1793	-2748	-334	0	64	-10462	14.07	14.07	6.03	6.03	-41.88	2338.5
43	12	4846	-3179	240	0	-133	-14278	14.07	14.07	8.04	8.04	-47.26	2837.3
44	12	-9847	-1780	311	0	-104	-4660	14.07	14.07	6.03	6.03	-18.37	416.2
45	12	-3221	-2183	-840	0	227	-8275	14.07	14.07	6.03	6.03	-33.49	1711.0
46	12	-4207	-1791	191	0	-84	-6835	14.07	14.07	6.03	6.03	-27.87	1296.5
47	12	-4795	-1558	161	0	-71	-5944	14.07	14.07	6.03	6.03	-24.32	1043.3
49	12	-3160	-1766	161	0	-77	-7164	14.07	14.07	6.03	6.03	-29.05	1453.0
50	12	-6099	-1486	176	0	-72	-5242	14.07	14.07	6.03	6.03	-21.45	785.9
51	12	-4774	-1567	-55	0	-6	-5965	14.07	14.07	6.03	6.03	-24.41	1049.8

apost= 10.05 aant= 10.05 ainf= 4.02 asup= 4.02 (e arm. base= 4 X 2.01)

40	25	3147	-3346	314	0	-191	-14475	14.07	14.07	8.04	8.04	-48.58	2772.3
41	25	-1756	-2723	312	0	-172	-10740	14.07	14.07	6.03	6.03	-42.97	2407.1
42	25	-1693	-2748	-334	0	106	-10805	14.07	14.07	6.03	6.03	-43.21	2427.4
43	25	4946	-3179	240	0	-163	-14675	14.07	14.07	8.04	8.04	-48.59	2914.2
44	25	-9747	-1780	311	0	-143	-4882	14.07	14.07	6.03	6.03	-19.38	468.7
45	25	-3121	-2183	-840	0	332	-8548	14.07	14.07	6.03	6.03	-34.56	1783.2
46	25	-4107	-1791	191	0	-107	-7058	14.07	14.07	6.03	6.03	-28.76	1356.7
47	25	-4695	-1558	161	0	-91	-6138	14.07	14.07	6.03	6.03	-25.11	1096.4
49	25	-3060	-1766	161	0	-98	-7384	14.07	14.07	6.03	6.03	-29.92	1512.8
50	25	-5999	-1486	176	0	-94	-5428	14.07	14.07	6.03	6.03	-22.22	836.0
51	25	-4674	-1567	-55	0	1	-6160	14.07	14.07	6.03	6.03	-25.19	1103.1

apost= 10.05 aant= 10.05 ainf= 4.02 asup= 4.02 (e arm. base= 4 X 2.01)

40	38	3247	-3346	314	0	-230	-14892	14.07	14.07	8.04	8.04	-49.98	2852.8
41	38	-1656	-2723	312	0	-211	-11080	14.07	14.07	6.03	6.03	-44.29	2495.4
42	38	-1593	-2748	-334	0	148	-11148	14.07	14.07	6.03	6.03	-44.55	2516.3
43	38	5046	-3179	240	0	-193	-15072	14.07	14.07	8.04	8.04	-49.92	2991.2
44	38	-9647	-1780	311	0	-182	-5104	14.07	14.07	6.03	6.03	-20.38	522.3
45	38	-3021	-2183	-840	0	437	-8821	14.07	14.07	6.03	6.03	-35.63	1855.4
46	38	-4007	-1791	191	0	-131	-7282	14.07	14.07	6.03	6.03	-29.64	1417.0
47	38	-4595	-1558	161	0	-111	-6333	14.07	14.07	6.03	6.03	-25.89	1149.5
49	38	-2960	-1766	161	0	-118	-7605	14.07	14.07	6.03	6.03	-30.78	1572.6
50	38	-5899	-1486	176	0	-116	-5613	14.07	14.07	6.03	6.03	-22.99	886.3
51	38	-4574	-1567	-55	0	8	-6356	14.07	14.07	6.03	6.03	-25.98	1156.5

apost= 10.05 aant= 10.05 ainf= 4.02 asup= 4.02 (e arm. base= 4 X 2.01)

40	50	3347	-3346	314	0	-269	-15310	14.07	14.07	8.04	8.04	-51.37	2933.3
41	50	-1556	-2723	312	0	-250	-11420	14.07	14.07	6.03	6.03	-45.62	2583.7
42	50	-1493	-2748	-334	0	190	-11490	14.07	14.07	6.03	6.03	-45.88	2605.1
43	50	5146	-3179	240	0	-223	-15470	14.07	14.07	8.04	8.04	-51.25	3068.1
44	50	-9547	-1780	311	0	-221	-5327	14.07	14.07	6.03	6.03	-21.37	576.9
45	50	-2921	-2183	-840	0	542	-9094	14.07	14.07	6.03	6.03	-36.69	1927.7
46	50	-3907	-1791	191	0	-155	-7506	14.07	14.07	6.03	6.03	-30.53	1477.3
47	50	-4495	-1558	161	0	-132	-6528	14.07	14.07	6.03	6.03	-26.67	1202.8
49	50	-2860	-1766	161	0	-138	-7826	14.07	14.07	6.03	6.03	-31.64	1632.4
50	50	-5799	-1486	176	0	-138	-5799	14.07	14.07	6.03	6.03	-23.75	936.7
51	50	-4474	-1567	-55	0	15	-6552	14.07	14.07	6.03	6.03	-26.76	1210.0

apost= 10.05 aant= 10.05 ainf= 4.02 asup= 4.02 (e arm. base= 4 X 2.01)

ASTA NUM. 79 NI 1683 NF 134 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 29A
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	4289	-3440	811	0	-133	-14630	14.07	14.07	8.04	8.04	-48.69	2867.3
41	0	-1030	-2804	710	0	-116	-10790	14.07	14.07	6.03	6.03	-42.99	2475.4
42	0	-1121	-2770	135	0	-12	-10690	14.07	14.07	6.03	6.03	-42.62	2444.6
43	0	6170	-3263	731	0	-120	-14890	14.07	14.07	8.04	8.04	-48.84	3025.3
44	0	-9678	-1845	557	0	-90	-4769	14.07	14.07	6.03	6.03	-18.89	448.7
45	0	-2847	-2147	-395	0	81	-8317	14.07	14.07	6.03	6.03	-33.59	1749.5
46	0	-3693	-1843	476	0	-77	-7102	14.07	14.07	6.03	6.03	-28.88	1398.1
47	0	-4359	-1603	417	0	-67	-6180	14.07	14.07	6.03	6.03	-25.25	1131.0
49	0	-2586	-1814	451	0	-73	-7460	14.07	14.07	6.03	6.03	-30.14	1566.8
50	0	-5756	-1531	416	0	-67	-5436	14.07	14.07	6.03	6.03	-22.26	855.2
51	0	-4389	-1591	225	0	-33	-6146	14.07	14.07	6.03	6.03	-25.12	1120.7

apost= 10.05 aant= 10.05 ainf= 4.02 asup= 4.02 (e arm. base= 4 X 2.01)

40	12	4389	-3440	811	0	-235	-15060	14.07	14.07	8.04	8.04	-50.13	2950.1
41	12	-930	-2804	710	0	-205	-11140	14.07	14.07	6.03	6.03	-44.35	2566.0
42	12	-1021	-2770	135	0	-29	-11038	14.07	14.07	6.03	6.03	-43.97	2534.7
43	12	6270	-3263	731	0	-212	-15298	14.07	14.07	8.04	8.04	-50.21	3104.0
44	12	-9578	-1845	557	0	-159	-5000	14.07	14.07	6.03	6.03	-19.93	503.8
45	12	-2747	-2147	-395	0	131	-8585	14.07	14.07	6.03	6.03	-34.64	1820.6
46	12	-3593	-1843	476	0	-137	-7332	14.07	14.07	6.03	6.03	-29.79	1460.0
47	12	-4259	-1603	417	0	-120	-6380	14.07	14.07	6.03	6.03	-26.05	1185.5
49	12	-2486	-1814	451	0	-130	-7687	14.07	14.07	6.03	6.03	-31.02	1628.1
50	12	-5656	-1531	416	0	-119	-5628	14.07	14.07	6.03	6.03	-23.05	906.9
51	12	-4289	-1591	225	0	-61	-6345	14.07	14.07	6.03	6.03	-25.91	1175.0

apost= 10.05 aant= 10.05 ainf= 4.02 asup= 4.02 (e arm. base= 4 X 2.01)

40	25	4489	-3440	811	0	-336	-15490	14.07	14.07	8.04	8.04	-51.57	3032.8
41	25	-830	-2804	710	0	-294	-11490	14.07	14.07	6.03	6.03	-45.71	2656.7
42	25	-921	-2770	135	0	-46	-11385	14.07	14.07	6.03	6.03	-45.32	2624.8
43	25	6370	-3263	731	0	-303	-15705	14.07	14.07	8.04	8.04	-51.57	3182.7

44	25	-9478	-1845	557	0	-229	-5230	14.07	14.07	6.03	6.03	-20.96	559.9
45	25	-2647	-2147	-395	0	180	-8854	14.07	14.07	6.03	6.03	-35.69	1891.8
46	25	-3493	-1843	476	0	-196	-7562	14.07	14.07	6.03	6.03	-30.69	1522.0
47	25	-4159	-1603	417	0	-172	-6580	14.07	14.07	6.03	6.03	-26.85	1240.1
49	25	-2386	-1814	451	0	-186	-7914	14.07	14.07	6.03	6.03	-31.90	1689.4
50	25	-5556	-1531	416	0	-171	-5819	14.07	14.07	6.03	6.03	-23.84	958.8
51	25	-4189	-1591	225	0	-89	-6544	14.07	14.07	6.03	6.03	-26.70	1229.3

apost= 10.05 aant= 10.05 ainf= 4.02 asup= 4.02 (e arm. base= 4 X 2.01)

40	38	4589	-3440	811	0	-437	-15920	14.07	14.07	8.04	8.04	-53.01	3115.5
41	38	-730	-2804	710	0	-382	-11840	14.07	14.07	6.03	6.03	-47.07	2747.5
42	38	-821	-2770	135	0	-63	-11732	14.07	14.07	6.03	6.03	-46.66	2714.9
43	38	6470	-3263	731	0	-395	-16112	14.07	14.07	8.04	8.04	-52.94	3261.4
44	38	-9378	-1845	557	0	-299	-5460	14.07	14.07	6.03	6.03	-21.99	616.8
45	38	-2547	-2147	-395	0	229	-9122	14.07	14.07	6.03	6.03	-36.73	1962.9
46	38	-3393	-1843	476	0	-256	-7793	14.07	14.07	6.03	6.03	-31.60	1584.0
47	38	-4059	-1603	417	0	-224	-6781	14.07	14.07	6.03	6.03	-27.64	1294.8
49	38	-2286	-1814	451	0	-242	-8140	14.07	14.07	6.03	6.03	-32.78	1750.7
50	38	-5456	-1531	416	0	-223	-6010	14.07	14.07	6.03	6.03	-24.62	1010.8
51	38	-4089	-1591	225	0	-117	-6743	14.07	14.07	6.03	6.03	-27.49	1283.7

apost= 10.05 aant= 10.05 ainf= 4.02 asup= 4.02 (e arm. base= 4 X 2.01)

40	50	4689	-3440	811	0	-539	-16350	14.07	14.07	8.04	8.04	-54.45	3198.3
41	50	-630	-2804	710	0	-471	-12190	14.07	14.07	6.03	6.03	-48.42	2838.2
42	50	-721	-2770	135	0	-80	-12080	14.07	14.07	6.03	6.03	-48.01	2805.0
43	50	6570	-3263	731	0	-486	-16520	14.07	14.07	8.04	8.04	-54.30	3340.1
44	50	-9278	-1845	557	0	-368	-5691	14.07	14.07	6.03	6.03	-23.00	674.4
45	50	-2447	-2147	-395	0	279	-9390	14.07	14.07	6.03	6.03	-37.77	2034.1
46	50	-3293	-1843	476	0	-315	-8023	14.07	14.07	6.03	6.03	-32.50	1646.0
47	50	-3959	-1603	417	0	-276	-6981	14.07	14.07	6.03	6.03	-28.43	1349.5
49	50	-2186	-1814	451	0	-299	-8367	14.07	14.07	6.03	6.03	-33.66	1812.1
50	50	-5356	-1531	416	0	-275	-6202	14.07	14.07	6.03	6.03	-25.39	1062.9
51	50	-3989	-1591	225	0	-146	-6942	14.07	14.07	6.03	6.03	-28.28	1338.1

apost= 10.05 aant= 10.05 ainf= 4.02 asup= 4.02 (e arm. base= 4 X 2.01)

ASTA NUM. 80 NI 1691 NF 177 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 28A
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	3144	-3459	1122	0	-158	-13780	14.07	14.07	6.03	6.03	-53.51	3511.9
41	0	-2106	-2737	966	0	-134	-9937	14.07	14.07	6.03	6.03	-39.87	2189.9
42	0	-2103	-2741	434	0	-43	-9942	14.07	14.07	6.03	6.03	-39.89	2191.3
43	0	5168	-3345	1021	0	-144	-14190	14.07	14.07	8.04	8.04	-46.83	2840.8
44	0	-10670	-1631	734	0	-97	-3883	14.07	14.07	6.03	6.03	-14.67	224.9
45	0	-3578	-2148	-126	0	48	-7794	14.07	14.07	6.03	6.03	-31.63	1570.2
46	0	-4468	-1782	638	0	-86	-6495	14.07	14.07	6.03	6.03	-26.53	1197.0
47	0	-5058	-1544	556	0	-74	-5635	14.07	14.07	6.03	6.03	-23.08	951.8
49	0	-3308	-1785	608	0	-82	-6916	14.07	14.07	6.03	6.03	-28.09	1383.2
50	0	-6476	-1442	551	0	-72	-4854	14.07	14.07	6.03	6.03	-19.80	670.6
51	0	-5057	-1545	379	0	-43	-5637	14.07	14.07	6.03	6.03	-23.09	952.3

apost= 10.05 aant= 10.05 ainf= 4.02 asup= 4.02 (e arm. base= 4 X 2.01)

40	12	3244	-3459	1122	0	-298	-14212	14.07	14.07	6.03	6.03	-55.19	3622.2
41	12	-2006	-2737	966	0	-254	-10280	14.07	14.07	6.03	6.03	-41.21	2278.9
42	12	-2003	-2741	434	0	-97	-10284	14.07	14.07	6.03	6.03	-41.22	2280.0
43	12	5268	-3345	1021	0	-272	-14608	14.07	14.07	8.04	8.04	-48.23	2921.3
44	12	-10570	-1631	734	0	-189	-4087	14.07	14.07	6.03	6.03	-15.61	265.8
45	12	-3478	-2148	-126	0	64	-8062	14.07	14.07	6.03	6.03	-32.69	1641.2
46	12	-4368	-1782	638	0	-165	-6718	14.07	14.07	6.03	6.03	-27.42	1256.9
47	12	-4958	-1544	556	0	-143	-5828	14.07	14.07	6.03	6.03	-23.86	1004.2
49	12	-3208	-1785	608	0	-158	-7139	14.07	14.07	6.03	6.03	-28.96	1443.6
50	12	-6376	-1442	551	0	-141	-5034	14.07	14.07	6.03	6.03	-20.57	718.8
51	12	-4957	-1545	379	0	-91	-5830	14.07	14.07	6.03	6.03	-23.87	1004.8

apost= 10.05 aant= 10.05 ainf= 4.02 asup= 4.02 (e arm. base= 4 X 2.01)

40	25	3344	-3459	1122	0	-438	-14645	14.07	14.07	8.04	8.04	-49.09	2814.3
41	25	-1906	-2737	966	0	-375	-10624	14.07	14.07	6.03	6.03	-42.55	2367.9
42	25	-1903	-2741	434	0	-151	-10626	14.07	14.07	6.03	6.03	-42.55	2368.7
43	25	5368	-3345	1021	0	-399	-15025	14.07	14.07	8.04	8.04	-49.63	3001.8
44	25	-10470	-1631	734	0	-280	-4290	14.07	14.07	6.03	6.03	-16.55	309.0
45	25	-3378	-2148	-126	0	80	-8331	14.07	14.07	6.03	6.03	-33.74	1712.3
46	25	-4268	-1782	638	0	-245	-6941	14.07	14.07	6.03	6.03	-28.30	1316.9
47	25	-4858	-1544	556	0	-213	-6021	14.07	14.07	6.03	6.03	-24.64	1056.8
49	25	-3108	-1785	608	0	-234	-7362	14.07	14.07	6.03	6.03	-29.84	1503.9
50	25	-6276	-1442	551	0	-210	-5214	14.07	14.07	6.03	6.03	-21.32	767.3
51	25	-4857	-1545	379	0	-138	-6023	14.07	14.07	6.03	6.03	-24.65	1057.4

apost= 10.05 aant= 10.05 ainf= 4.02 asup= 4.02 (e arm. base= 4 X 2.01)

40	38	3444	-3459	1122	0	-579	-15078	14.07	14.07	8.04	8.04	-50.54	2897.5
41	38	-1806	-2737	966	0	-496	-10967	14.07	14.07	6.03	6.03	-43.88	2456.9
42	38	-1803	-2741	434	0	-205	-10968	14.07	14.07	6.03	6.03	-43.89	2457.5
43	38	5468	-3345	1021	0	-527	-15442	14.07	14.07	8.04	8.04	-51.03	3082.3
44	38	-10370	-1631	734	0	-372	-4494	14.07	14.07	6.03	6.03	-17.49	354.1
45	38	-3278	-2148	-126	0	95	-8600	14.07	14.07	6.03	6.03	-34.79	1783.4
46	38	-4168	-1782	638	0	-325	-7164	14.07	14.07	6.03	6.03	-29.19	1377.0
47	38	-4758	-1544	556	0	-282	-6214	14.07	14.07	6.03	6.03	-25.42	1109.5
49	38	-3008	-1785	608	0	-310	-7586	14.07	14.07	6.03	6.03	-30.71	1564.3
50	38	-6176	-1442	551	0	-279	-5395	14.07	14.07	6.03	6.03	-22.08	815.9
51	38	-4757	-1545	379	0	-185	-6216	14.07	14.07	6.03	6.03	-25.42	1110.0

apost= 10.05 aant= 10.05 ainf= 4.02 asup= 4.02 (e arm. base= 4 X 2.01)

40	50	3544	-3459	1122	0	-719	-15510	14.07	14.07	8.04	8.04	-51.99	2980.6
41	50	-1706	-2737	966	0	-617	-11310	14.07	14.07	6.03	6.03	-45.22	2546.0
42	50	-1703	-2741	434	0	-260	-11310	14.07	14.07	6.03	6.03	-45.22	2546.2
43	50	5568	-3345	1021	0	-654	-15860	14.07	14.07	8.04	8.04	-52.43	3162.7
44	50	-10270	-1631	734	0	-464	-4698	14.07	14.07	6.03	6.03	-18.43	400.6

45	50	-3178	-2148	-126	0	111	-8868	14.07	14.07	6.03	6.03	-35.84	1854.5
46	50	-4068	-1782	638	0	-405	-7387	14.07	14.07	6.03	6.03	-30.07	1437.1
47	50	-4658	-1544	556	0	-352	-6407	14.07	14.07	6.03	6.03	-26.19	1162.2
49	50	-2908	-1785	608	0	-386	-7809	14.07	14.07	6.03	6.03	-31.58	1624.7
50	50	-6076	-1442	551	0	-348	-5575	14.07	14.07	6.03	6.03	-22.83	864.8
51	50	-4657	-1545	379	0	-233	-6409	14.07	14.07	6.03	6.03	-26.20	1162.8

apost= 10.05 aant= 10.05 ainf= 4.02 asup= 4.02 (e arm. base= 4 X 2.01)

ASTA NUM. 81 NI 1699 NF 220 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 27A
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-3789	-2583	1407	0	-52	-6859	14.07	14.07	6.03	6.03	-27.92	1333.5
41	0	-7621	-1843	1303	0	-65	-4215	14.07	14.07	6.03	6.03	-16.90	452.3
42	0	-7643	-1902	813	0	25	-4326	14.07	14.07	6.03	6.03	-17.38	475.3
43	0	-1558	-2643	1239	0	-36	-7576	14.07	14.07	6.03	6.03	-30.39	1673.3
44	0	-14010	-676	1174	0	-88	26	14.07	14.07	6.03	6.03	-4.21	-62.9
45	0	-7980	-1507	248	0	92	-3353	14.07	14.07	6.03	6.03	-12.99	251.6
46	0	-8139	-1149	923	0	-52	-2540	14.07	14.07	6.03	6.03	-9.33	-123.7
47	0	-8268	-976	828	0	-49	-2122	14.07	14.07	6.03	6.03	-7.62	-103.4
49	0	-6991	-1222	863	0	-45	-3003	14.07	14.07	6.03	6.03	-11.67	233.4
50	0	-9482	-829	850	0	-55	-1483	14.07	14.07	6.03	6.03	-5.89	-82.6
51	0	-8275	-995	665	0	-19	-2159	14.07	14.07	6.03	6.03	-7.76	-105.1

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	12	-3689	-2583	1407	0	-228	-7182	14.07	14.07	6.03	6.03	-29.20	1417.3
41	12	-7521	-1843	1303	0	-228	-4445	14.07	14.07	6.03	6.03	-17.92	509.3
42	12	-7543	-1902	813	0	-77	-4564	14.07	14.07	6.03	6.03	-18.43	534.3
43	12	-1458	-2643	1239	0	-191	-7906	14.07	14.07	6.03	6.03	-31.67	1759.2
44	12	-13910	-676	1174	0	-235	-59	14.07	14.07	6.03	6.03	-4.74	-67.7
45	12	-7880	-1507	248	0	61	-3542	14.07	14.07	6.03	6.03	-13.86	294.5
46	12	-8039	-1149	923	0	-168	-2684	14.07	14.07	6.03	6.03	-9.97	-131.0
47	12	-8168	-976	828	0	-153	-2244	14.07	14.07	6.03	6.03	-8.10	-109.0
49	12	-6891	-1222	863	0	-153	-3156	14.07	14.07	6.03	6.03	-12.38	269.5
50	12	-9382	-829	850	0	-162	-1586	14.07	14.07	6.03	6.03	-6.11	-85.3
51	12	-8175	-995	665	0	-102	-2283	14.07	14.07	6.03	6.03	-8.26	-110.9

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	25	-3589	-2583	1407	0	-404	-7505	14.07	14.07	6.03	6.03	-30.48	1501.1
41	25	-7421	-1843	1303	0	-390	-4676	14.07	14.07	6.03	6.03	-18.93	567.1
42	25	-7443	-1902	813	0	-179	-4802	14.07	14.07	6.03	6.03	-19.46	594.0
43	25	-1358	-2643	1239	0	-346	-8236	14.07	14.07	6.03	6.03	-32.96	1845.1
44	25	-13810	-676	1174	0	-382	-143	14.07	14.07	6.03	6.03	-5.28	-73.7
45	25	-7780	-1507	248	0	30	-3730	14.07	14.07	6.03	6.03	-14.73	338.9
46	25	-7939	-1149	923	0	-283	-2828	14.07	14.07	6.03	6.03	-10.64	156.7
47	25	-8068	-976	828	0	-256	-2366	14.07	14.07	6.03	6.03	-8.61	-115.0
49	25	-6791	-1222	863	0	-261	-3308	14.07	14.07	6.03	6.03	-13.09	306.9
50	25	-9282	-829	850	0	-268	-1690	14.07	14.07	6.03	6.03	-6.35	-88.3
51	25	-8075	-995	665	0	-186	-2408	14.07	14.07	6.03	6.03	-8.78	-117.0

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	38	-3489	-2583	1407	0	-580	-7828	14.07	14.07	6.03	6.03	-31.75	1585.0
41	38	-7321	-1843	1303	0	-553	-4906	14.07	14.07	6.03	6.03	-19.93	625.6
42	38	-7343	-1902	813	0	-280	-5039	14.07	14.07	6.03	6.03	-20.49	654.4
43	38	-1258	-2643	1239	0	-500	-8567	14.07	14.07	6.03	6.03	-34.24	1931.1
44	38	-13710	-676	1174	0	-529	-228	14.07	14.07	6.03	6.03	-5.81	-79.6
45	38	-7680	-1507	248	0	-1	-3918	14.07	14.07	6.03	6.03	-15.59	384.6
46	38	-7839	-1149	923	0	-398	-2971	14.07	14.07	6.03	6.03	-11.31	186.3
47	38	-7968	-976	828	0	-360	-2488	14.07	14.07	6.03	6.03	-9.14	-121.1
49	38	-6691	-1222	863	0	-368	-3461	14.07	14.07	6.03	6.03	-13.79	345.2
50	38	-9182	-829	850	0	-374	-1794	14.07	14.07	6.03	6.03	-6.61	-91.6
51	38	-7975	-995	665	0	-269	-2532	14.07	14.07	6.03	6.03	-9.33	-123.3

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	50	-3389	-2583	1407	0	-756	-8151	14.07	14.07	6.03	6.03	-33.02	1668.9
41	50	-7221	-1843	1303	0	-716	-5136	14.07	14.07	6.03	6.03	-20.91	684.5
42	50	-7243	-1902	813	0	-382	-5277	14.07	14.07	6.03	6.03	-21.51	715.2
43	50	-1158	-2643	1239	0	-655	-8897	14.07	14.07	6.03	6.03	-35.53	2017.1
44	50	-13610	-676	1174	0	-675	-312	14.07	14.07	6.03	6.03	-6.35	-85.5
45	50	-7580	-1507	248	0	-32	-4107	14.07	14.07	6.03	6.03	-16.44	431.3
46	50	-7739	-1149	923	0	-514	-3115	14.07	14.07	6.03	6.03	-11.98	217.6
47	50	-7868	-976	828	0	-463	-2610	14.07	14.07	6.03	6.03	-9.69	-127.4
49	50	-6591	-1222	863	0	-476	-3614	14.07	14.07	6.03	6.03	-14.48	384.4
50	50	-9082	-829	850	0	-480	-1897	14.07	14.07	6.03	6.03	-6.90	-95.2
51	50	-7875	-995	665	0	-352	-2656	14.07	14.07	6.03	6.03	-9.89	130.9

apost= 10.05 aant= 10.05 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

ASTA NUM. 82 NI 1351 NF 1360 SEZ. Rp B= 0.400 H= 0.600 (pilastro)
PIL. NUM. 16
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-10050	1877	541	0	1061	-5262	10.05	10.05	6.03	6.03	-35.18	976.2
41	0	-10070	958	552	0	1086	-2624	10.05	10.05	6.03	6.03	-16.62	-208.1
42	0	-10000	963	488	0	912	-2639	10.05	10.05	6.03	6.03	-16.74	210.9
43	0	-9881	2326	524	0	1029	-6563	10.05	10.05	6.03	6.03	-43.99	1401.6
44	0	-9900	-547	552	0	1089	1700	10.05	10.05	6.03	6.03	-10.58	-140.6
45	0	-9806	803	436	0	782	-2190	10.05	10.05	6.03	6.03	-13.64	-175.2
46	0	-9827	696	538	0	1063	-1889	10.05	10.05	6.03	6.03	-11.69	-153.3
47	0	-9767	631	534	0	1057	-1705	10.05	10.05	6.03	6.03	-10.60	-140.6
49	0	-9760	937	530	0	1049	-2585	10.05	10.05	6.03	6.03	-16.41	208.1

50	0	-9764	362	536	0	1061	-933	10.05	10.05	6.03	6.03	-9.48	-119.1
51	0	-9745	632	513	0	999	-1711	10.05	10.05	6.03	6.03	-10.63	-140.9

apost= 6.03 aant= 6.03 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	12	-9974	1877	541	0	993	-5028	10.05	10.05	6.03	6.03	-33.58	907.7
41	12	-9994	958	552	0	1017	-2504	10.05	10.05	6.03	6.03	-15.79	-199.0
42	12	-9925	963	488	0	851	-2518	10.05	10.05	6.03	6.03	-15.90	-200.0
43	12	-9806	2326	524	0	964	-6272	10.05	10.05	6.03	6.03	-42.03	1313.8
44	12	-9825	-547	552	0	1020	1632	10.05	10.05	6.03	6.03	-10.19	-136.0
45	12	-9731	803	436	0	727	-2090	10.05	10.05	6.03	6.03	-12.98	-167.6
46	12	-9752	696	538	0	996	-1802	10.05	10.05	6.03	6.03	-11.16	-147.1
47	12	-9692	631	534	0	990	-1626	10.05	10.05	6.03	6.03	-10.15	-135.2
49	12	-9685	937	530	0	983	-2468	10.05	10.05	6.03	6.03	-15.59	-195.9
50	12	-9689	362	536	0	994	-887	10.05	10.05	6.03	6.03	-8.98	-113.8
51	12	-9670	632	513	0	935	-1632	10.05	10.05	6.03	6.03	-10.18	-135.5

apost= 6.03 aant= 6.03 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	25	-9898	1877	541	0	926	-4793	10.05	10.05	6.03	6.03	-31.98	839.4
41	25	-9918	958	552	0	948	-2384	10.05	10.05	6.03	6.03	-14.96	-189.8
42	25	-9850	963	488	0	790	-2398	10.05	10.05	6.03	6.03	-15.07	-190.8
43	25	-9731	2326	524	0	898	-5982	10.05	10.05	6.03	6.03	-40.08	1226.3
44	25	-9750	-547	552	0	951	1563	10.05	10.05	6.03	6.03	-9.82	-131.4
45	25	-9656	803	436	0	673	-1989	10.05	10.05	6.03	6.03	-12.32	-160.1
46	25	-9677	696	538	0	929	-1715	10.05	10.05	6.03	6.03	-10.64	-141.0
47	25	-9617	631	534	0	924	-1548	10.05	10.05	6.03	6.03	-9.71	-130.0
49	25	-9610	937	530	0	916	-2351	10.05	10.05	6.03	6.03	-14.78	-187.0
50	25	-9614	362	536	0	927	-842	10.05	10.05	6.03	6.03	-8.51	-108.7
51	25	-9595	632	513	0	871	-1552	10.05	10.05	6.03	6.03	-9.74	-130.2

apost= 6.03 aant= 6.03 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	37	-9822	1877	541	0	858	-4558	10.05	10.05	6.03	6.03	-30.37	771.6
41	37	-9843	958	552	0	879	-2264	10.05	10.05	6.03	6.03	-14.14	-180.7
42	37	-9776	963	488	0	729	-2278	10.05	10.05	6.03	6.03	-14.24	-181.7
43	37	-9656	2326	524	0	833	-5691	10.05	10.05	6.03	6.03	-38.12	1138.9
44	37	-9675	-547	552	0	882	1494	10.05	10.05	6.03	6.03	-9.45	-126.9
45	37	-9581	803	436	0	618	-1888	10.05	10.05	6.03	6.03	-11.69	-152.8
46	37	-9602	696	538	0	861	-1628	10.05	10.05	6.03	6.03	-10.15	-135.0
47	37	-9542	631	534	0	857	-1469	10.05	10.05	6.03	6.03	-9.30	-124.9
49	37	-9535	937	530	0	850	-2234	10.05	10.05	6.03	6.03	-13.98	-178.1
50	37	-9539	362	536	0	860	-797	10.05	10.05	6.03	6.03	-8.06	-103.7
51	37	-9520	632	513	0	807	-1473	10.05	10.05	6.03	6.03	-9.31	-125.1

apost= 6.03 aant= 6.03 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	50	-9746	1877	541	0	790	-4324	10.05	10.05	6.03	6.03	-28.75	704.1
41	50	-9767	958	552	0	810	-2144	10.05	10.05	6.03	6.03	-13.34	-171.7
42	50	-9701	963	488	0	668	-2157	10.05	10.05	6.03	6.03	-13.43	-172.6
43	50	-9581	2326	524	0	767	-5400	10.05	10.05	6.03	6.03	-36.15	1051.8
44	50	-9600	-547	552	0	813	1426	10.05	10.05	6.03	6.03	-9.10	-122.6
45	50	-9506	803	436	0	564	-1788	10.05	10.05	6.03	6.03	-11.07	-145.6
46	50	-9527	696	538	0	794	-1541	10.05	10.05	6.03	6.03	-9.67	-129.3
47	50	-9467	631	534	0	790	-1390	10.05	10.05	6.03	6.03	-8.89	-119.9
49	50	-9460	937	530	0	784	-2117	10.05	10.05	6.03	6.03	-13.19	-169.3
50	50	-9464	362	536	0	793	-751	10.05	10.05	6.03	6.03	-7.63	-98.9
51	50	-9445	632	513	0	743	-1394	10.05	10.05	6.03	6.03	-8.91	-120.1

apost= 6.03 aant= 6.03 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

ASTA NUM. 83 NI 1360 NF 170 SEZ. Rp B= 0.400 H= 0.600 (pilastro)
PIL. NUM. 16A
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-9746	1877	541	0	790	-4324	10.05	10.05	6.03	6.03	-28.75	704.1
41	0	-9767	958	552	0	810	-2144	10.05	10.05	6.03	6.03	-13.34	-171.7
42	0	-9701	963	488	0	668	-2157	10.05	10.05	6.03	6.03	-13.43	-172.6
43	0	-9581	2326	524	0	767	-5400	10.05	10.05	6.03	6.03	-36.15	1051.8
44	0	-9600	-547	552	0	813	1426	10.05	10.05	6.03	6.03	-9.10	-122.6
45	0	-9506	803	436	0	564	-1788	10.05	10.05	6.03	6.03	-11.07	-145.6
46	0	-9527	696	538	0	794	-1541	10.05	10.05	6.03	6.03	-9.67	-129.3
47	0	-9467	631	534	0	790	-1390	10.05	10.05	6.03	6.03	-8.89	-119.9
49	0	-9460	937	530	0	784	-2117	10.05	10.05	6.03	6.03	-13.19	-169.3
50	0	-9464	362	536	0	793	-751	10.05	10.05	6.03	6.03	-7.63	-98.9
51	0	-9445	632	513	0	743	-1394	10.05	10.05	6.03	6.03	-8.91	-120.1

apost= 6.03 aant= 6.03 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	12	-9671	1877	541	0	723	-4089	10.05	10.05	6.03	6.03	-27.13	637.0
41	12	-9692	958	552	0	741	-2024	10.05	10.05	6.03	6.03	-12.55	-162.8
42	12	-9626	963	488	0	607	-2037	10.05	10.05	6.03	6.03	-12.64	-163.6
43	12	-9506	2326	524	0	702	-5109	10.05	10.05	6.03	6.03	-34.18	965.0
44	12	-9525	-547	552	0	744	1358	10.05	10.05	6.03	6.03	-8.75	-118.3
45	12	-9431	803	436	0	510	-1688	10.05	10.05	6.03	6.03	-10.47	-138.5
46	12	-9452	696	538	0	727	-1454	10.05	10.05	6.03	6.03	-9.20	-123.7
47	12	-9392	631	534	0	723	-1311	10.05	10.05	6.03	6.03	-8.50	-115.2
49	12	-9385	937	530	0	717	-2000	10.05	10.05	6.03	6.03	-12.41	-160.5
50	12	-9389	362	536	0	726	-706	10.05	10.05	6.03	6.03	-7.23	-94.3
51	12	-9370	632	513	0	679	-1315	10.05	10.05	6.03	6.03	-8.51	-115.3

apost= 6.03 aant= 6.03 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	25	-9596	1877	541	0	655	-3854	10.05	10.05	6.03	6.03	-25.49	570.5
41	25	-9617	958	552	0	672	-1904	10.05	10.05	6.03	6.03	-11.79	-154.0
42	25	-9551	963	488	0	546	-1916	10.05	10.05	6.03	6.03	-11.86	-154.7
43	25	-9431	2326	524	0	636	-4818	10.05	10.05	6.03	6.03	-32.20	878.5
44	25	-9450	-547	552	0	675	1290	10.05	10.05	6.03	6.03	-8.42	-114.2
45	25	-9356	803	436	0	455	-1588	10.05	10.05	6.03	6.03	-9.89	-131.7
46	25	-9377	696	538	0	660	-1367	10.05	10.05	6.03	6.03	-8.76	-118.2
47	25	-9317	631	534	0	657	-1232	10.05	10.05	6.03	6.03	-8.13	-110.5
49	25	-9310	937	530	0	651	-1882	10.05	10.05	6.03	6.03	-11.66	-151.9
50	25	-9314	362	536	0	659	-661	10.05	10.05	6.03	6.03	-6.85	-89.9

51	25	-9295	632	513	0	615	-1236	10.05	10.05	6.03	6.03	-8.14	-110.6

apost= 6.03 aant= 6.03 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	38	-9521	1877	541	0	587	-3620	10.05	10.05	6.03	6.03	-23.85	504.9
41	38	-9542	958	552	0	603	-1785	10.05	10.05	6.03	6.03	-11.05	-145.4
42	38	-9476	963	488	0	485	-1796	10.05	10.05	6.03	6.03	-11.12	-146.1
43	38	-9356	2326	524	0	571	-4528	10.05	10.05	6.03	6.03	-30.21	792.6
44	38	-9375	-547	552	0	606	1221	10.05	10.05	6.03	6.03	-8.10	-110.2
45	38	-9281	803	436	0	400	-1487	10.05	10.05	6.03	6.03	-9.34	-125.1
46	38	-9302	696	538	0	592	-1280	10.05	10.05	6.03	6.03	-8.34	-113.0
47	38	-9242	631	534	0	590	-1154	10.05	10.05	6.03	6.03	-7.78	-106.1
49	38	-9235	937	530	0	585	-1765	10.05	10.05	6.03	6.03	-10.92	-143.4
50	38	-9239	362	536	0	592	-615	10.05	10.05	6.03	6.03	-6.47	-85.6
51	38	-9220	632	513	0	551	-1157	10.05	10.05	6.03	6.03	-7.78	-106.1

apost= 6.03 aant= 6.03 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	50	-9446	1877	541	0	520	-3385	10.05	10.05	6.03	6.03	-22.20	440.3
41	50	-9467	958	552	0	534	-1665	10.05	10.05	6.03	6.03	-10.34	-137.1
42	50	-9401	963	488	0	424	-1676	10.05	10.05	6.03	6.03	-10.40	-137.6
43	50	-9281	2326	524	0	505	-4237	10.05	10.05	6.03	6.03	-28.21	707.3
44	50	-9300	-547	552	0	538	1153	10.05	10.05	6.03	6.03	-7.79	-106.3
45	50	-9206	803	436	0	346	-1387	10.05	10.05	6.03	6.03	-8.82	-118.7
46	50	-9227	696	538	0	525	-1193	10.05	10.05	6.03	6.03	-7.93	-108.0
47	50	-9167	631	534	0	523	-1075	10.05	10.05	6.03	6.03	-7.43	-101.8
49	50	-9160	937	530	0	518	-1648	10.05	10.05	6.03	6.03	-10.22	-135.1
50	50	-9164	362	536	0	525	-570	10.05	10.05	6.03	6.03	-6.10	-81.3
51	50	-9145	632	513	0	487	-1078	10.05	10.05	6.03	6.03	-7.44	-101.8

apost= 6.03 aant= 6.03 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

ASTA NUM. 84 NI 1037 NF 300 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 15A
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-32630	686	532	0	756	-1585	6.03	6.03	10.05	10.05	-20.25	-273.1
41	0	-32210	133	520	0	778	-242	6.03	6.03	10.05	10.05	-15.28	-222.2
42	0	-32070	136	335	0	419	-248	6.03	6.03	10.05	10.05	-13.93	-205.2
43	0	-31220	1042	502	0	733	-2463	6.03	6.03	10.05	10.05	-24.30	-316.6
44	0	-31210	-786	486	0	773	1993	6.03	6.03	10.05	10.05	-21.83	-288.9
45	0	-30280	126	174	0	171	-235	6.03	6.03	10.05	10.05	-12.42	-183.7
46	0	-29480	114	460	0	763	-214	6.03	6.03	10.05	10.05	-14.17	-205.7
47	0	-28800	109	445	0	759	-207	6.03	6.03	10.05	10.05	-13.89	-201.6
49	0	-28950	293	449	0	752	-655	6.03	6.03	10.05	10.05	-14.09	-202.1
50	0	-28940	-72	446	0	760	237	6.03	6.03	10.05	10.05	-13.95	-202.4
51	0	-28760	110	383	0	640	-209	6.03	6.03	10.05	10.05	-13.45	-196.0

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	12	-32555	686	532	0	690	-1499	6.03	6.03	10.05	10.05	-19.78	-267.7
41	12	-32135	133	520	0	713	-225	6.03	6.03	10.05	10.05	-15.02	-218.8
42	12	-31995	136	335	0	377	-231	6.03	6.03	10.05	10.05	-13.76	-202.9
43	12	-31145	1042	502	0	670	-2333	6.03	6.03	10.05	10.05	-23.57	-308.3
44	12	-31135	-786	486	0	712	1895	6.03	6.03	10.05	10.05	-21.30	-282.8
45	12	-30205	126	174	0	149	-219	6.03	6.03	10.05	10.05	-12.31	-182.3
46	12	-29405	114	460	0	706	-200	6.03	6.03	10.05	10.05	-13.93	-202.7
47	12	-28725	109	445	0	704	-193	6.03	6.03	10.05	10.05	-13.66	-198.6
49	12	-28875	293	449	0	696	-618	6.03	6.03	10.05	10.05	-13.87	-199.2
50	12	-28865	-72	446	0	705	228	6.03	6.03	10.05	10.05	-13.72	-199.5
51	12	-28685	110	383	0	592	-195	6.03	6.03	10.05	10.05	-13.25	-193.4

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	25	-32480	686	532	0	623	-1414	6.03	6.03	10.05	10.05	-19.31	-262.3
41	25	-32060	133	520	0	648	-208	6.03	6.03	10.05	10.05	-14.75	-215.5
42	25	-31920	136	335	0	335	-214	6.03	6.03	10.05	10.05	-13.58	-200.6
43	25	-31070	1042	502	0	607	-2202	6.03	6.03	10.05	10.05	-22.86	-300.3
44	25	-31060	-786	486	0	651	1796	6.03	6.03	10.05	10.05	-20.76	-276.7
45	25	-30130	126	174	0	128	-203	6.03	6.03	10.05	10.05	-12.20	-180.9
46	25	-29330	114	460	0	648	-185	6.03	6.03	10.05	10.05	-13.70	-199.6
47	25	-28650	109	445	0	648	-180	6.03	6.03	10.05	10.05	-13.43	-195.7
49	25	-28800	293	449	0	640	-581	6.03	6.03	10.05	10.05	-13.66	-196.2
50	25	-28790	-72	446	0	649	218	6.03	6.03	10.05	10.05	-13.49	-196.5
51	25	-28610	110	383	0	544	-181	6.03	6.03	10.05	10.05	-13.04	-190.8

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	38	-32405	686	532	0	557	-1328	6.03	6.03	10.05	10.05	-18.84	-256.9
41	38	-31985	133	520	0	583	-192	6.03	6.03	10.05	10.05	-14.49	-212.1
42	38	-31845	136	335	0	294	-197	6.03	6.03	10.05	10.05	-13.40	-198.3
43	38	-30995	1042	502	0	544	-2072	6.03	6.03	10.05	10.05	-22.16	-292.3
44	38	-30985	-786	486	0	590	1698	6.03	6.03	10.05	10.05	-20.23	-270.6
45	38	-30055	126	174	0	106	-188	6.03	6.03	10.05	10.05	-12.09	-179.4
46	38	-29255	114	460	0	591	-171	6.03	6.03	10.05	10.05	-13.46	-196.6
47	38	-28575	109	445	0	593	-166	6.03	6.03	10.05	10.05	-13.21	-192.7
49	38	-28725	293	449	0	584	-545	6.03	6.03	10.05	10.05	-13.44	-193.2
50	38	-28715	-72	446	0	593	209	6.03	6.03	10.05	10.05	-13.26	-193.6
51	38	-28535	110	383	0	496	-168	6.03	6.03	10.05	10.05	-12.84	-188.2

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	50	-32330	686	532	0	490	-1242	6.03	6.03	10.05	10.05	-18.37	-251.6
41	50	-31910	133	520	0	518	-175	6.03	6.03	10.05	10.05	-14.23	-208.8
42	50	-31770	136	335	0	252	-180	6.03	6.03	10.05	10.05	-13.22	-196.0
43	50	-30920	1042	502	0	482	-1942	6.03	6.03	10.05	10.05	-21.46	-284.3
44	50	-30910	-786	486	0	530	1600	6.03	6.03	10.05	10.05	-19.69	-264.4
45	50	-29980	126	174	0	84	-172	6.03	6.03	10.05	10.05	-11.98	-178.0
46	50	-29180	114	460	0	533	-157	6.03	6.03	10.05	10.05	-13.23	-193.6
47	50	-28500	109	445	0	537	-152	6.03	6.03	10.05	10.05	-12.98	-189.8
49	50	-28650	293	449	0	528	-508	6.03	6.03	10.05	10.05	-13.22	-190.3
50	50	-28640	-72	446	0	537	200	6.03	6.03	10.05	10.05	-13.03	-190.6
51	50	-28460	110	383	0	448	-154	6.03	6.03	10.05	10.05	-12.64	-185.6

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

ASTA NUM. 85 NI 1033 NF 1037 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 15
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-32930	686	532	0	1022	-1928	6.03	6.03	10.05	10.05	-22.13	-294.7
41	0	-32510	133	520	0	1037	-308	6.03	6.03	10.05	10.05	-16.33	-235.6
42	0	-32370	136	335	0	586	-316	6.03	6.03	10.05	10.05	-14.65	-214.5
43	0	-31520	1042	502	0	984	-2984	6.03	6.03	10.05	10.05	-27.54	-352.4
44	0	-31510	-786	486	0	1015	2385	6.03	6.03	10.05	10.05	-23.98	-313.4
45	0	-30580	126	174	0	258	-298	6.03	6.03	10.05	10.05	-12.85	-189.3
46	0	-29780	114	460	0	993	-271	6.03	6.03	10.05	10.05	-15.11	-217.8
47	0	-29100	109	445	0	982	-261	6.03	6.03	10.05	10.05	-14.81	-213.3
49	0	-29250	293	449	0	977	-801	6.03	6.03	10.05	10.05	-14.96	-214.0
50	0	-29240	-72	446	0	983	273	6.03	6.03	10.05	10.05	-14.87	-214.2
51	0	-29060	110	383	0	832	-264	6.03	6.03	10.05	10.05	-14.25	-206.3

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	12	-32855	686	532	0	956	-1842	6.03	6.03	10.05	10.05	-21.66	-289.3
41	12	-32435	133	520	0	972	-291	6.03	6.03	10.05	10.05	-16.07	-232.3
42	12	-32295	136	335	0	545	-299	6.03	6.03	10.05	10.05	-14.47	-212.2
43	12	-31445	1042	502	0	921	-2854	6.03	6.03	10.05	10.05	-26.69	-343.1
44	12	-31435	-786	486	0	954	2287	6.03	6.03	10.05	10.05	-23.43	-307.2
45	12	-30505	126	174	0	236	-282	6.03	6.03	10.05	10.05	-12.75	-187.9
46	12	-29705	114	460	0	936	-256	6.03	6.03	10.05	10.05	-14.88	-214.8
47	12	-29025	109	445	0	926	-248	6.03	6.03	10.05	10.05	-14.58	-210.4
49	12	-29175	293	449	0	921	-765	6.03	6.03	10.05	10.05	-14.74	-211.0
50	12	-29165	-72	446	0	927	264	6.03	6.03	10.05	10.05	-14.64	-211.2
51	12	-28985	110	383	0	784	-250	6.03	6.03	10.05	10.05	-14.05	-203.7

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	25	-32780	686	532	0	889	-1756	6.03	6.03	10.05	10.05	-21.19	-283.9
41	25	-32360	133	520	0	907	-275	6.03	6.03	10.05	10.05	-15.81	-228.9
42	25	-32220	136	335	0	503	-282	6.03	6.03	10.05	10.05	-14.29	-209.9
43	25	-31370	1042	502	0	858	-2724	6.03	6.03	10.05	10.05	-25.86	-334.0
44	25	-31360	-786	486	0	894	2189	6.03	6.03	10.05	10.05	-22.90	-301.1
45	25	-30430	126	174	0	215	-266	6.03	6.03	10.05	10.05	-12.64	-186.5
46	25	-29630	114	460	0	878	-242	6.03	6.03	10.05	10.05	-14.64	-211.7
47	25	-28950	109	445	0	871	-234	6.03	6.03	10.05	10.05	-14.35	-207.4
49	25	-29100	293	449	0	864	-728	6.03	6.03	10.05	10.05	-14.52	-208.0
50	25	-29090	-72	446	0	872	255	6.03	6.03	10.05	10.05	-14.41	-208.3
51	25	-28910	110	383	0	736	-236	6.03	6.03	10.05	10.05	-13.85	-201.1

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	38	-32705	686	532	0	822	-1671	6.03	6.03	10.05	10.05	-20.72	-278.5
41	38	-32285	133	520	0	842	-258	6.03	6.03	10.05	10.05	-15.54	-225.6
42	38	-32145	136	335	0	461	-265	6.03	6.03	10.05	10.05	-14.11	-207.6
43	38	-31295	1042	502	0	795	-2593	6.03	6.03	10.05	10.05	-25.07	-325.2
44	38	-31285	-786	486	0	833	2091	6.03	6.03	10.05	10.05	-22.36	-295.0
45	38	-30355	126	174	0	193	-251	6.03	6.03	10.05	10.05	-12.53	-185.1
46	38	-29555	114	460	0	821	-228	6.03	6.03	10.05	10.05	-14.41	-208.7
47	38	-28875	109	445	0	815	-220	6.03	6.03	10.05	10.05	-14.12	-204.5
49	38	-29025	293	449	0	808	-691	6.03	6.03	10.05	10.05	-14.31	-205.1
50	38	-29015	-72	446	0	816	246	6.03	6.03	10.05	10.05	-14.18	-205.4
51	38	-28835	110	383	0	688	-223	6.03	6.03	10.05	10.05	-13.65	-198.5

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	50	-32630	686	532	0	756	-1585	6.03	6.03	10.05	10.05	-20.25	-273.1
41	50	-32210	133	520	0	778	-242	6.03	6.03	10.05	10.05	-15.28	-222.2
42	50	-32070	136	335	0	419	-248	6.03	6.03	10.05	10.05	-13.93	-205.2
43	50	-31220	1042	502	0	733	-2463	6.03	6.03	10.05	10.05	-24.30	-316.6
44	50	-31210	-786	486	0	773	1993	6.03	6.03	10.05	10.05	-21.83	-288.9
45	50	-30280	126	174	0	171	-235	6.03	6.03	10.05	10.05	-12.42	-183.7
46	50	-29480	114	460	0	763	-214	6.03	6.03	10.05	10.05	-14.17	-205.7
47	50	-28800	109	445	0	759	-207	6.03	6.03	10.05	10.05	-13.89	-201.6
49	50	-28950	293	449	0	752	-655	6.03	6.03	10.05	10.05	-14.09	-202.1
50	50	-28940	-72	446	0	760	237	6.03	6.03	10.05	10.05	-13.95	-202.4
51	50	-28760	110	383	0	640	-209	6.03	6.03	10.05	10.05	-13.45	-196.0

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

ASTA NUM. 86 NI 1255 NF 1262 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 14
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-16660	163	-481	0	-1277	-584	6.03	6.03	10.05	10.05	-11.05	-154.3
41	0	-16620	4	-434	0	-1162	6	6.03	6.03	10.05	10.05	-10.62	-148.9
42	0	-16570	5	-570	0	-1531	1	6.03	6.03	10.05	10.05	-11.93	-165.2
43	0	-16080	274	-434	0	-1157	-996	6.03	6.03	10.05	10.05	-11.09	-147.0
44	0	-16020	-262	-374	0	-1011	992	6.03	6.03	10.05	10.05	-11.04	-146.5
45	0	-15920	11	-582	0	-1580	-20	6.03	6.03	10.05	10.05	-11.86	-163.6
46	0	-15630	12	-309	0	-846	-23	6.03	6.03	10.05	10.05	-9.10	-128.9
47	0	-15390	14	-277	0	-767	-30	6.03	6.03	10.05	10.05	-8.72	-124.0
49	0	-15400	67	-293	0	-805	-227	6.03	6.03	10.05	10.05	-8.87	-125.7
50	0	-15390	-40	-281	0	-776	170	6.03	6.03	10.05	10.05	-8.76	-124.4
51	0	-15370	15	-322	0	-890	-32	6.03	6.03	10.05	10.05	-9.16	-129.4

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	12	-16585	163	-481	0	-1217	-564	6.03	6.03	10.05	10.05	-10.81	-151.2

41	12	-16545	4	-434	0	-1108	6	6.03	6.03	10.05	10.05	-10.40	-146.0
42	12	-16495	5	-570	0	-1460	2	6.03	6.03	10.05	10.05	-11.65	-161.6
43	12	-16005	274	-434	0	-1103	-961	6.03	6.03	10.05	10.05	-10.88	-144.6
44	12	-15945	-262	-374	0	-964	959	6.03	6.03	10.05	10.05	-10.85	-144.1
45	12	-15845	11	-582	0	-1507	-18	6.03	6.03	10.05	10.05	-11.57	-159.9
46	12	-15555	12	-309	0	-807	-22	6.03	6.03	10.05	10.05	-8.93	-126.7
47	12	-15315	14	-277	0	-732	-28	6.03	6.03	10.05	10.05	-8.57	-122.0
49	12	-15325	67	-293	0	-769	-218	6.03	6.03	10.05	10.05	-8.71	-123.7
50	12	-15315	-40	-281	0	-741	166	6.03	6.03	10.05	10.05	-8.60	-122.4
51	12	-15295	15	-322	0	-850	-30	6.03	6.03	10.05	10.05	-8.99	-127.1

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	25	-16510	163	-481	0	-1157	-544	6.03	6.03	10.05	10.05	-10.56	-148.0
41	25	-16470	4	-434	0	-1054	7	6.03	6.03	10.05	10.05	-10.18	-143.1
42	25	-16420	5	-570	0	-1389	3	6.03	6.03	10.05	10.05	-11.36	-158.0
43	25	-15930	274	-434	0	-1048	-927	6.03	6.03	10.05	10.05	-10.68	-142.2
44	25	-15870	-262	-374	0	-917	926	6.03	6.03	10.05	10.05	-10.65	-141.8
45	25	-15770	11	-582	0	-1434	-17	6.03	6.03	10.05	10.05	-11.28	-156.2
46	25	-15480	12	-309	0	-769	-20	6.03	6.03	10.05	10.05	-8.77	-124.6
47	25	-15240	14	-277	0	-697	-27	6.03	6.03	10.05	10.05	-8.42	-120.0
49	25	-15250	67	-293	0	-732	-210	6.03	6.03	10.05	10.05	-8.54	-121.6
50	25	-15240	-40	-281	0	-706	160	6.03	6.03	10.05	10.05	-8.45	-120.3
51	25	-15220	15	-322	0	-809	-28	6.03	6.03	10.05	10.05	-8.81	-124.9

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	38	-16435	163	-481	0	-1097	-523	6.03	6.03	10.05	10.05	-10.32	-144.9
41	38	-16395	4	-434	0	-999	7	6.03	6.03	10.05	10.05	-9.95	-140.3
42	38	-16345	5	-570	0	-1318	3	6.03	6.03	10.05	10.05	-11.08	-154.3
43	38	-15855	274	-434	0	-994	-893	6.03	6.03	10.05	10.05	-10.47	-139.8
44	38	-15795	-262	-374	0	-870	893	6.03	6.03	10.05	10.05	-10.45	-139.5
45	38	-15695	11	-582	0	-1362	-15	6.03	6.03	10.05	10.05	-10.98	-152.5
46	38	-15405	12	-309	0	-730	-18	6.03	6.03	10.05	10.05	-8.60	-122.4
47	38	-15165	14	-277	0	-663	-25	6.03	6.03	10.05	10.05	-8.26	-118.0
49	38	-15175	67	-293	0	-695	-202	6.03	6.03	10.05	10.05	-8.38	-119.5
50	38	-15165	-40	-281	0	-671	156	6.03	6.03	10.05	10.05	-8.29	-118.3
51	38	-15145	15	-322	0	-769	-26	6.03	6.03	10.05	10.05	-8.64	-122.6

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	50	-16360	163	-481	0	-1037	-503	6.03	6.03	10.05	10.05	-10.07	-141.8
41	50	-16320	4	-434	0	-945	8	6.03	6.03	10.05	10.05	-9.73	-137.4
42	50	-16270	5	-570	0	-1247	4	6.03	6.03	10.05	10.05	-10.79	-150.7
43	50	-15780	274	-434	0	-940	-858	6.03	6.03	10.05	10.05	-10.27	-137.4
44	50	-15720	-262	-374	0	-824	860	6.03	6.03	10.05	10.05	-10.26	-137.2
45	50	-15620	11	-582	0	-1289	-14	6.03	6.03	10.05	10.05	-10.69	-148.8
46	50	-15330	12	-309	0	-692	-17	6.03	6.03	10.05	10.05	-8.43	-120.2
47	50	-15090	14	-277	0	-628	-23	6.03	6.03	10.05	10.05	-8.11	-116.0
49	50	-15100	67	-293	0	-659	-193	6.03	6.03	10.05	10.05	-8.22	-117.4
50	50	-15090	-40	-281	0	-636	150	6.03	6.03	10.05	10.05	-8.14	-116.3
51	50	-15070	15	-322	0	-729	-24	6.03	6.03	10.05	10.05	-8.46	-120.4

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

ASTA NUM. 87 NI 1262 NF 128 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 14A
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-16360	163	-481	0	-1037	-503	6.03	6.03	10.05	10.05	-10.07	-141.8
41	0	-16320	4	-434	0	-945	8	6.03	6.03	10.05	10.05	-9.73	-137.4
42	0	-16270	5	-570	0	-1247	4	6.03	6.03	10.05	10.05	-10.79	-150.7
43	0	-15780	274	-434	0	-940	-858	6.03	6.03	10.05	10.05	-10.27	-137.4
44	0	-15720	-262	-374	0	-824	860	6.03	6.03	10.05	10.05	-10.26	-137.2
45	0	-15620	11	-582	0	-1289	-14	6.03	6.03	10.05	10.05	-10.69	-148.8
46	0	-15330	12	-309	0	-692	-17	6.03	6.03	10.05	10.05	-8.43	-120.2
47	0	-15090	14	-277	0	-628	-23	6.03	6.03	10.05	10.05	-8.11	-116.0
49	0	-15100	67	-293	0	-659	-193	6.03	6.03	10.05	10.05	-8.22	-117.4
50	0	-15090	-40	-281	0	-636	150	6.03	6.03	10.05	10.05	-8.14	-116.3
51	0	-15070	15	-322	0	-729	-24	6.03	6.03	10.05	10.05	-8.46	-120.4

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	12	-16285	163	-481	0	-977	-482	6.03	6.03	10.05	10.05	-9.83	-138.6
41	12	-16245	4	-434	0	-891	8	6.03	6.03	10.05	10.05	-9.50	-134.5
42	12	-16195	5	-570	0	-1176	5	6.03	6.03	10.05	10.05	-10.51	-147.0
43	12	-15705	274	-434	0	-886	-824	6.03	6.03	10.05	10.05	-10.06	-135.0
44	12	-15645	-262	-374	0	-777	828	6.03	6.03	10.05	10.05	-10.06	-134.9
45	12	-15545	11	-582	0	-1216	-13	6.03	6.03	10.05	10.05	-10.40	-145.1
46	12	-15255	12	-309	0	-653	-15	6.03	6.03	10.05	10.05	-8.26	-118.0
47	12	-15015	14	-277	0	-593	-21	6.03	6.03	10.05	10.05	-7.95	-114.0
49	12	-15025	67	-293	0	-622	-185	6.03	6.03	10.05	10.05	-8.06	-115.3
50	12	-15015	-40	-281	0	-600	146	6.03	6.03	10.05	10.05	-7.98	-114.3
51	12	-14995	15	-322	0	-688	-23	6.03	6.03	10.05	10.05	-8.29	-118.1

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	25	-16210	163	-481	0	-917	-462	6.03	6.03	10.05	10.05	-9.58	-135.5
41	25	-16170	4	-434	0	-837	9	6.03	6.03	10.05	10.05	-9.28	-131.6
42	25	-16120	5	-570	0	-1104	5	6.03	6.03	10.05	10.05	-10.22	-143.4
43	25	-15630	274	-434	0	-831	-790	6.03	6.03	10.05	10.05	-9.86	-132.6
44	25	-15570	-262	-374	0	-730	795	6.03	6.03	10.05	10.05	-9.86	-132.6
45	25	-15470	11	-582	0	-1144	-11	6.03	6.03	10.05	10.05	-10.11	-141.4
46	25	-15180	12	-309	0	-614	-14	6.03	6.03	10.05	10.05	-8.09	-115.9
47	25	-14940	14	-277	0	-559	-20	6.03	6.03	10.05	10.05	-7.80	-112.0
49	25	-14950	67	-293	0	-586	-176	6.03	6.03	10.05	10.05	-7.90	-113.2
50	25	-14940	-40	-281	0	-565	140	6.03	6.03	10.05	10.05	-7.82	-112.3
51	25	-14920	15	-322	0	-648	-21	6.03	6.03	10.05	10.05	-8.11	-115.9

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	38	-16135	163	-481	0	-857	-441	6.03	6.03	10.05	10.05	-9.34	-132.3
41	38	-16095	4	-434	0	-782	9	6.03	6.03	10.05	10.05	-9.05	-128.8

42	38	-16045	5	-570	0	-1033	6	6.03	6.03	10.05	10.05	-9.94	-139.7
43	38	-15555	274	-434	0	-777	-756	6.03	6.03	10.05	10.05	-9.65	-130.2
44	38	-15495	-262	-374	0	-683	762	6.03	6.03	10.05	10.05	-9.67	-130.3
45	38	-15395	11	-582	0	-1071	-10	6.03	6.03	10.05	10.05	-9.82	-137.7
46	38	-15105	12	-309	0	-576	-12	6.03	6.03	10.05	10.05	-7.93	-113.7
47	38	-14865	14	-277	0	-524	-18	6.03	6.03	10.05	10.05	-7.65	-110.0
49	38	-14875	67	-293	0	-549	-168	6.03	6.03	10.05	10.05	-7.74	-111.2
50	38	-14865	-40	-281	0	-530	136	6.03	6.03	10.05	10.05	-7.67	-110.3
51	38	-14845	15	-322	0	-608	-19	6.03	6.03	10.05	10.05	-7.94	-113.6

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	50	-16060	163	-481	0	-797	-421	6.03	6.03	10.05	10.05	-9.09	-129.2
41	50	-16020	4	-434	0	-728	10	6.03	6.03	10.05	10.05	-8.83	-125.9
42	50	-15970	5	-570	0	-962	7	6.03	6.03	10.05	10.05	-9.65	-136.1
43	50	-15480	274	-434	0	-723	-721	6.03	6.03	10.05	10.05	-9.45	-127.8
44	50	-15420	-262	-374	0	-636	730	6.03	6.03	10.05	10.05	-9.47	-127.9
45	50	-15320	11	-582	0	-998	-8	6.03	6.03	10.05	10.05	-9.53	-134.0
46	50	-15030	12	-309	0	-537	-11	6.03	6.03	10.05	10.05	-7.76	-111.5
47	50	-14790	14	-277	0	-490	-16	6.03	6.03	10.05	10.05	-7.49	-108.0
49	50	-14800	67	-293	0	-512	-160	6.03	6.03	10.05	10.05	-7.58	-109.1
50	50	-14790	-40	-281	0	-495	130	6.03	6.03	10.05	10.05	-7.51	-108.2
51	50	-14770	15	-322	0	-567	-17	6.03	6.03	10.05	10.05	-7.77	-111.4

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

ASTA NUM. 88 NI 1168 NF 211 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 13A
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	--												
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-5619	-374	258	0	-1022	-12	4.02	4.02	10.05	10.05	-8.60	-113.4
41	0	-5610	-83	238	0	-983	-5	4.02	4.02	10.05	10.05	-8.29	-109.7
42	0	-5655	-88	302	0	-1120	-6	4.02	4.02	10.05	10.05	-9.44	-123.0
43	0	-5480	-582	239	0	-954	-16	4.02	4.02	10.05	10.05	-8.05	-106.7
44	0	-5469	404	206	0	-899	5	4.02	4.02	10.05	10.05	-7.62	-101.6
45	0	-5540	-106	312	0	-1119	-6	4.02	4.02	10.05	10.05	-9.44	-122.7
46	0	-5378	-105	186	0	-834	-6	4.02	4.02	10.05	10.05	-7.13	-95.7
47	0	-5320	-110	173	0	-797	-6	4.02	4.02	10.05	10.05	-6.86	-92.4
49	0	-5323	-208	180	0	-810	-8	4.02	4.02	10.05	10.05	-6.95	-93.4
50	0	-5321	-10	173	0	-799	-3	4.02	4.02	10.05	10.05	-6.88	-92.5
51	0	-5335	-112	194	0	-843	-6	4.02	4.02	10.05	10.05	-7.19	-96.2

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	12	-5563	-374	258	0	-1054	-59	4.02	4.02	10.05	10.05	-8.87	-116.4
41	12	-5554	-83	238	0	-1013	-16	4.02	4.02	10.05	10.05	-8.52	-112.3
42	12	-5599	-88	302	0	-1158	-17	4.02	4.02	10.05	10.05	-9.78	-126.8
43	12	-5424	-582	239	0	-984	-89	4.02	4.02	10.05	10.05	-8.29	-109.3
44	12	-5413	404	206	0	-925	56	4.02	4.02	10.05	10.05	-7.81	-103.7
45	12	-5484	-106	312	0	-1158	-19	4.02	4.02	10.05	10.05	-9.80	-126.6
46	12	-5322	-105	186	0	-857	-19	4.02	4.02	10.05	10.05	-7.29	-97.4
47	12	-5264	-110	173	0	-819	-19	4.02	4.02	10.05	10.05	-7.00	-93.9
49	12	-5267	-208	180	0	-832	-34	4.02	4.02	10.05	10.05	-7.10	-95.0
50	12	-5265	-10	173	0	-820	-5	4.02	4.02	10.05	10.05	-7.01	-94.0
51	12	-5279	-112	194	0	-867	-20	4.02	4.02	10.05	10.05	-7.35	-98.1

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	25	-5506	-374	258	0	-1086	-105	4.02	4.02	10.05	10.05	-9.15	-119.4
41	25	-5498	-83	238	0	-1042	-26	4.02	4.02	10.05	10.05	-8.77	-115.1
42	25	-5542	-88	302	0	-1196	-28	4.02	4.02	10.05	10.05	-10.15	-130.6
43	25	-5368	-582	239	0	-1014	-162	4.02	4.02	10.05	10.05	-8.53	-112.0
44	25	-5356	404	206	0	-950	106	4.02	4.02	10.05	10.05	-8.01	-105.9
45	25	-5428	-106	312	0	-1197	-33	4.02	4.02	10.05	10.05	-10.18	-130.6
46	25	-5266	-105	186	0	-881	-32	4.02	4.02	10.05	10.05	-7.45	-99.2
47	25	-5208	-110	173	0	-840	-33	4.02	4.02	10.05	10.05	-7.14	-95.4
49	25	-5210	-208	180	0	-855	-60	4.02	4.02	10.05	10.05	-7.25	-96.7
50	25	-5208	-10	173	0	-842	-6	4.02	4.02	10.05	10.05	-7.15	-95.6
51	25	-5222	-112	194	0	-891	-34	4.02	4.02	10.05	10.05	-7.53	-100.0

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	38	-5450	-374	258	0	-1119	-152	4.02	4.02	10.05	10.05	-9.45	-122.5
41	38	-5441	-83	238	0	-1072	-37	4.02	4.02	10.05	10.05	-9.03	-117.8
42	38	-5486	-88	302	0	-1234	-39	4.02	4.02	10.05	10.05	-10.52	-134.5
43	38	-5311	-582	239	0	-1044	-234	4.02	4.02	10.05	10.05	-8.79	-114.8
44	38	-5300	404	206	0	-976	157	4.02	4.02	10.05	10.05	-8.21	-108.1
45	38	-5371	-106	312	0	-1236	-46	4.02	4.02	10.05	10.05	-10.57	-134.6
46	38	-5209	-105	186	0	-904	-45	4.02	4.02	10.05	10.05	-7.62	-101.1
47	38	-5151	-110	173	0	-862	-47	4.02	4.02	10.05	10.05	-7.29	-97.1
49	38	-5154	-208	180	0	-877	-86	4.02	4.02	10.05	10.05	-7.41	-98.5
50	38	-5152	-10	173	0	-864	-7	4.02	4.02	10.05	10.05	-7.31	-97.3
51	38	-5166	-112	194	0	-916	-48	4.02	4.02	10.05	10.05	-7.71	-102.0

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	50	-5394	-374	258	0	-1151	-199	4.02	4.02	10.05	10.05	-9.75	-125.8
41	50	-5385	-83	238	0	-1102	-47	4.02	4.02	10.05	10.05	-9.30	-120.7
42	50	-5430	-88	302	0	-1272	-50	4.02	4.02	10.05	10.05	-10.90	-138.4
43	50	-5255	-582	239	0	-1074	-307	4.02	4.02	10.05	10.05	-9.07	-117.7
44	50	-5244	404	206	0	-1002	207	4.02	4.02	10.05	10.05	-8.43	-110.5
45	50	-5315	-106	312	0	-1275	-59	4.02	4.02	10.05	10.05	-10.97	-138.7
46	50	-5153	-105	186	0	-927	-58	4.02	4.02	10.05	10.05	-7.81	-103.1
47	50	-5095	-110	173	0	-884	-61	4.02	4.02	10.05	10.05	-7.45	-98.8
49	50	-5098	-208	180	0	-900	-112	4.02	4.02	10.05	10.05	-7.58	-100.3
50	50	-5096	-10	173	0	-885	-9	4.02	4.02	10.05	10.05	-7.47	-99.0
51	50	-5110	-112	194	0	-940	-62	4.02	4.02	10.05	10.05	-7.91	-104.1

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

ASTA NUM. 89 NI 1160 NF 1168 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 13
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm²				daN/cm²	
40	0	-3856	-85	-364	0	-1268	31	4.02	4.02	10.05	10.05	-11.43	215.9
41	0	-3854	-32	-363	0	-1228	11	4.02	4.02	10.05	10.05	-11.03	199.5
42	0	-3872	-35	-377	0	-1376	12	4.02	4.02	10.05	10.05	-12.52	260.6
43	0	-3775	-121	-340	0	-1185	44	4.02	4.02	10.05	10.05	-10.62	188.1
44	0	-3776	57	-349	0	-1133	-23	4.02	4.02	10.05	10.05	-10.09	167.1
45	0	-3802	-37	-361	0	-1366	12	4.02	4.02	10.05	10.05	-12.45	262.4
46	0	-3722	-33	-324	0	-1053	11	4.02	4.02	10.05	10.05	-9.29	139.9
47	0	-3689	-33	-314	0	-1010	11	4.02	4.02	10.05	10.05	-8.87	126.1
49	0	-3690	-51	-315	0	-1023	18	4.02	4.02	10.05	10.05	-9.00	130.8
50	0	-3690	-16	-316	0	-1012	4	4.02	4.02	10.05	10.05	-8.89	126.7
51	0	-3695	-34	-319	0	-1059	11	4.02	4.02	10.05	10.05	-9.36	144.1

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	12	-3800	-85	-364	0	-1222	20	4.02	4.02	10.05	10.05	-10.99	201.5
41	12	-3798	-32	-363	0	-1183	7	4.02	4.02	10.05	10.05	-10.59	185.4
42	12	-3816	-35	-377	0	-1329	7	4.02	4.02	10.05	10.05	-12.07	245.2
43	12	-3719	-121	-340	0	-1143	29	4.02	4.02	10.05	10.05	-10.21	175.3
44	12	-3720	57	-349	0	-1089	-16	4.02	4.02	10.05	10.05	-9.66	154.1
45	12	-3746	-37	-361	0	-1321	8	4.02	4.02	10.05	10.05	-12.01	247.6
46	12	-3666	-33	-324	0	-1013	7	4.02	4.02	10.05	10.05	-8.90	128.6
47	12	-3633	-33	-314	0	-971	7	4.02	4.02	10.05	10.05	-8.49	115.4
49	12	-3634	-51	-315	0	-984	11	4.02	4.02	10.05	10.05	-8.62	120.1
50	12	-3634	-16	-316	0	-973	2	4.02	4.02	10.05	10.05	-8.51	116.0
51	12	-3639	-34	-319	0	-1019	7	4.02	4.02	10.05	10.05	-8.98	132.9

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	25	-3744	-85	-364	0	-1177	9	4.02	4.02	10.05	10.05	-10.55	187.3
41	25	-3742	-32	-363	0	-1138	3	4.02	4.02	10.05	10.05	-10.15	171.5
42	25	-3760	-35	-377	0	-1282	3	4.02	4.02	10.05	10.05	-11.61	229.8
43	25	-3662	-121	-340	0	-1100	14	4.02	4.02	10.05	10.05	-9.80	162.7
44	25	-3664	57	-349	0	-1046	-9	4.02	4.02	10.05	10.05	-9.24	141.3
45	25	-3690	-37	-361	0	-1276	3	4.02	4.02	10.05	10.05	-11.57	233.0
46	25	-3610	-33	-324	0	-972	3	4.02	4.02	10.05	10.05	-8.51	117.4
47	25	-3576	-33	-314	0	-931	3	4.02	4.02	10.05	10.05	-8.11	105.0
49	25	-3578	-51	-315	0	-944	5	4.02	4.02	10.05	10.05	-8.24	109.5
50	25	-3578	-16	-316	0	-933	0	4.02	4.02	10.05	10.05	-8.13	105.6
51	25	-3582	-34	-319	0	-979	3	4.02	4.02	10.05	10.05	-8.60	121.8

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	38	-3687	-85	-364	0	-1132	-1	4.02	4.02	10.05	10.05	-10.11	173.2
41	38	-3685	-32	-363	0	-1092	-1	4.02	4.02	10.05	10.05	-9.71	157.7
42	38	-3703	-35	-377	0	-1235	-2	4.02	4.02	10.05	10.05	-11.16	214.6
43	38	-3606	-121	-340	0	-1058	-1	4.02	4.02	10.05	10.05	-9.39	150.2
44	38	-3607	57	-349	0	-1002	-2	4.02	4.02	10.05	10.05	-8.82	128.7
45	38	-3633	-37	-361	0	-1230	-2	4.02	4.02	10.05	10.05	-11.14	218.4
46	38	-3553	-33	-324	0	-932	-1	4.02	4.02	10.05	10.05	-8.12	106.6
47	38	-3520	-33	-314	0	-892	-1	4.02	4.02	10.05	10.05	-7.73	-96.8
49	38	-3521	-51	-315	0	-905	-1	4.02	4.02	10.05	10.05	-7.87	99.2
50	38	-3521	-16	-316	0	-894	-1	4.02	4.02	10.05	10.05	-7.75	-97.0
51	38	-3526	-34	-319	0	-939	-1	4.02	4.02	10.05	10.05	-8.21	111.0

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	50	-3631	-85	-364	0	-1086	-12	4.02	4.02	10.05	10.05	-9.67	159.3
41	50	-3629	-32	-363	0	-1047	-5	4.02	4.02	10.05	10.05	-9.27	144.2
42	50	-3647	-35	-377	0	-1188	-6	4.02	4.02	10.05	10.05	-10.70	199.5
43	50	-3550	-121	-340	0	-1016	-16	4.02	4.02	10.05	10.05	-8.98	137.9
44	50	-3551	57	-349	0	-959	5	4.02	4.02	10.05	10.05	-8.40	116.4
45	50	-3577	-37	-361	0	-1185	-6	4.02	4.02	10.05	10.05	-10.70	204.0
46	50	-3497	-33	-324	0	-891	-6	4.02	4.02	10.05	10.05	-7.74	-96.8
47	50	-3464	-33	-314	0	-852	-6	4.02	4.02	10.05	10.05	-7.36	-92.6
49	50	-3465	-51	-315	0	-866	-8	4.02	4.02	10.05	10.05	-7.49	-94.0
50	50	-3465	-16	-316	0	-854	-3	4.02	4.02	10.05	10.05	-7.38	-92.8
51	50	-3470	-34	-319	0	-900	-6	4.02	4.02	10.05	10.05	-7.83	100.4

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

ASTA NUM. 90 NI 1159 NF 1161 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 18
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm²				daN/cm²	
40	0	-4798	-75	-387	0	-1206	14	6.03	6.03	10.05	10.05	-7.61	-95.8
41	0	-4792	101	-404	0	-1239	-21	6.03	6.03	10.05	10.05	-7.84	-98.3
42	0	-4794	89	-416	0	-1336	-19	6.03	6.03	10.05	10.05	-8.53	118.6
43	0	-4706	-201	-352	0	-1094	39	6.03	6.03	10.05	10.05	-6.84	-87.3
44	0	-4692	394	-415	0	-1253	-80	6.03	6.03	10.05	10.05	-7.96	102.5
45	0	-4700	73	-401	0	-1312	-16	6.03	6.03	10.05	10.05	-8.38	116.8
46	0	-4640	88	-368	0	-1096	-19	6.03	6.03	10.05	10.05	-6.86	-87.4
47	0	-4602	84	-358	0	-1061	-18	6.03	6.03	10.05	10.05	-6.63	-84.7
49	0	-4604	26	-352	0	-1050	-7	6.03	6.03	10.05	10.05	-6.55	-83.9
50	0	-4601	145	-365	0	-1081	-30	6.03	6.03	10.05	10.05	-6.77	-86.2
51	0	-4602	80	-362	0	-1093	-18	6.03	6.03	10.05	10.05	-6.85	-87.1

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	12	-4723	-75	-387	0	-1158	5	6.03	6.03	10.05	10.05	-7.28	-92.1
41	12	-4717	101	-404	0	-1188	-9	6.03	6.03	10.05	10.05	-7.50	-94.4
42	12	-4719	89	-416	0	-1284	-8	6.03	6.03	10.05	10.05	-8.18	108.9
43	12	-4631	-201	-352	0	-1050	14	6.03	6.03	10.05	10.05	-6.55	-83.9
44	12	-4617	394	-415	0	-1201	-31	6.03	6.03	10.05	10.05	-7.61	-95.2
45	12	-4625	73	-401	0	-1262	-7	6.03	6.03	10.05	10.05	-8.04	107.6
46	12	-4565	88	-368	0	-1050	-8	6.03	6.03	10.05	10.05	-6.56	-83.8

47	12	-4527	84	-358	0	-1016	-8	6.03	6.03	10.05	10.05	-6.33	-81.2
49	12	-4529	26	-352	0	-1006	-3	6.03	6.03	10.05	10.05	-6.26	-80.5
50	12	-4526	145	-365	0	-1035	-12	6.03	6.03	10.05	10.05	-6.46	-82.7
51	12	-4527	80	-362	0	-1048	-8	6.03	6.03	10.05	10.05	-6.55	-83.6

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	25	-4648	-75	-387	0	-1109	-4	6.03	6.03	10.05	10.05	-6.95	-88.3
41	25	-4642	101	-404	0	-1138	4	6.03	6.03	10.05	10.05	-7.16	-90.5
42	25	-4644	89	-416	0	-1232	3	6.03	6.03	10.05	10.05	-7.82	99.5
43	25	-4556	-201	-352	0	-1006	-11	6.03	6.03	10.05	10.05	-6.26	-80.5
44	25	-4542	394	-415	0	-1149	18	6.03	6.03	10.05	10.05	-7.25	-91.3
45	25	-4550	73	-401	0	-1212	2	6.03	6.03	10.05	10.05	-7.69	98.6
46	25	-4490	88	-368	0	-1004	3	6.03	6.03	10.05	10.05	-6.26	-80.3
47	25	-4452	84	-358	0	-971	3	6.03	6.03	10.05	10.05	-6.04	-77.8
49	25	-4454	26	-352	0	-962	-0	6.03	6.03	10.05	10.05	-5.97	-77.1
50	25	-4451	145	-365	0	-990	6	6.03	6.03	10.05	10.05	-6.16	-79.2
51	25	-4452	80	-362	0	-1002	2	6.03	6.03	10.05	10.05	-6.25	-80.1

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	38	-4573	-75	-387	0	-1060	-14	6.03	6.03	10.05	10.05	-6.63	-84.6
41	38	-4567	101	-404	0	-1088	17	6.03	6.03	10.05	10.05	-6.82	-86.6
42	38	-4569	89	-416	0	-1180	14	6.03	6.03	10.05	10.05	-7.47	-93.6
43	38	-4481	-201	-352	0	-962	-36	6.03	6.03	10.05	10.05	-5.98	-77.2
44	38	-4467	394	-415	0	-1097	68	6.03	6.03	10.05	10.05	-6.90	-87.3
45	38	-4475	73	-401	0	-1161	11	6.03	6.03	10.05	10.05	-7.35	-92.1
46	38	-4415	88	-368	0	-958	14	6.03	6.03	10.05	10.05	-5.96	-76.8
47	38	-4377	84	-358	0	-926	13	6.03	6.03	10.05	10.05	-5.75	-74.4
49	38	-4379	26	-352	0	-917	3	6.03	6.03	10.05	10.05	-5.69	-73.8
50	38	-4376	145	-365	0	-944	24	6.03	6.03	10.05	10.05	-5.87	-75.7
51	38	-4377	80	-362	0	-957	13	6.03	6.03	10.05	10.05	-5.95	-76.7

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	50	-4498	-75	-387	0	-1012	-23	6.03	6.03	10.05	10.05	-6.31	-80.9
41	50	-4492	101	-404	0	-1037	29	6.03	6.03	10.05	10.05	-6.48	-82.8
42	50	-4494	89	-416	0	-1128	26	6.03	6.03	10.05	10.05	-7.11	-89.6
43	50	-4406	-201	-352	0	-918	-61	6.03	6.03	10.05	10.05	-5.69	-73.8
44	50	-4392	394	-415	0	-1045	117	6.03	6.03	10.05	10.05	-6.55	-83.3
45	50	-4400	73	-401	0	-1111	21	6.03	6.03	10.05	10.05	-7.01	-88.2
46	50	-4340	88	-368	0	-912	25	6.03	6.03	10.05	10.05	-5.66	-73.3
47	50	-4302	84	-358	0	-881	24	6.03	6.03	10.05	10.05	-5.46	-71.0
49	50	-4304	26	-352	0	-873	6	6.03	6.03	10.05	10.05	-5.41	-70.4
50	50	-4301	145	-365	0	-899	42	6.03	6.03	10.05	10.05	-5.57	-72.3
51	50	-4302	80	-362	0	-912	23	6.03	6.03	10.05	10.05	-5.66	-73.2

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

ASTA NUM. 91 NI 1161 NF 142 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 18A
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-6652	-283	69	0	-942	-23	6.03	6.03	10.05	10.05	-6.08	-82.3
41	0	-6651	195	71	0	-965	29	6.03	6.03	10.05	10.05	-6.19	-83.6
42	0	-6669	166	101	0	-1053	26	6.03	6.03	10.05	10.05	-6.63	-88.9
43	0	-6497	-624	53	0	-852	-61	6.03	6.03	10.05	10.05	-5.64	-76.7
44	0	-6503	997	76	0	-975	117	6.03	6.03	10.05	10.05	-6.21	-83.6
45	0	-6524	125	106	0	-1039	21	6.03	6.03	10.05	10.05	-6.53	-87.5
46	0	-6402	159	48	0	-847	25	6.03	6.03	10.05	10.05	-5.59	-76.0
47	0	-6339	150	42	0	-818	24	6.03	6.03	10.05	10.05	-5.44	-74.1
49	0	-6340	-9	42	0	-810	6	6.03	6.03	10.05	10.05	-5.41	-73.7
50	0	-6341	315	46	0	-835	42	6.03	6.03	10.05	10.05	-5.52	-75.0
51	0	-6345	141	52	0	-847	23	6.03	6.03	10.05	10.05	-5.57	-75.7

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	12	-6577	-283	69	0	-950	-59	6.03	6.03	10.05	10.05	-6.10	-82.4
41	12	-6576	195	71	0	-974	54	6.03	6.03	10.05	10.05	-6.22	-83.8
42	12	-6594	166	101	0	-1066	46	6.03	6.03	10.05	10.05	-6.69	-89.4
43	12	-6422	-624	53	0	-859	-139	6.03	6.03	10.05	10.05	-5.64	-76.7
44	12	-6428	997	76	0	-985	242	6.03	6.03	10.05	10.05	-6.24	-83.8
45	12	-6449	125	106	0	-1052	36	6.03	6.03	10.05	10.05	-6.59	-88.1
46	12	-6327	159	48	0	-853	45	6.03	6.03	10.05	10.05	-5.59	-75.9
47	12	-6264	150	42	0	-823	43	6.03	6.03	10.05	10.05	-5.44	-74.0
49	12	-6265	-9	42	0	-815	5	6.03	6.03	10.05	10.05	-5.41	-73.6
50	12	-6266	315	46	0	-840	81	6.03	6.03	10.05	10.05	-5.52	-75.0
51	12	-6270	141	52	0	-854	40	6.03	6.03	10.05	10.05	-5.58	-75.7

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	25	-6502	-283	69	0	-959	-94	6.03	6.03	10.05	10.05	-6.13	-82.6
41	25	-6501	195	71	0	-983	78	6.03	6.03	10.05	10.05	-6.25	-84.0
42	25	-6519	166	101	0	-1078	67	6.03	6.03	10.05	10.05	-6.74	-90.0
43	25	-6347	-624	53	0	-865	-217	6.03	6.03	10.05	10.05	-5.65	-76.7
44	25	-6353	997	76	0	-994	366	6.03	6.03	10.05	10.05	-6.27	-84.1
45	25	-6374	125	106	0	-1066	52	6.03	6.03	10.05	10.05	-6.65	-88.7
46	25	-6252	159	48	0	-859	65	6.03	6.03	10.05	10.05	-5.60	-75.9
47	25	-6189	150	42	0	-829	61	6.03	6.03	10.05	10.05	-5.44	-73.9
49	25	-6190	-9	42	0	-820	4	6.03	6.03	10.05	10.05	-5.41	-73.5
50	25	-6191	315	46	0	-846	121	6.03	6.03	10.05	10.05	-5.52	-74.9
51	25	-6195	141	52	0	-860	58	6.03	6.03	10.05	10.05	-5.59	-75.7

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	38	-6427	-283	69	0	-967	-129	6.03	6.03	10.05	10.05	-6.15	-82.8
41	38	-6426	195	71	0	-992	102	6.03	6.03	10.05	10.05	-6.27	-84.3
42	38	-6444	166	101	0	-1091	88	6.03	6.03	10.05	10.05	-6.80	-90.5
43	38	-6272	-624	53	0	-872	-295	6.03	6.03	10.05	10.05	-5.66	-76.7
44	38	-6278	997	76	0	-1004	491	6.03	6.03	10.05	10.05	-6.31	-84.4
45	38	-6299	125	106	0	-1079	67	6.03	6.03	10.05	10.05	-6.72	-89.3
46	38	-6177	159	48	0	-865	85	6.03	6.03	10.05	10.05	-5.61	-75.9
47	38	-6114	150	42	0	-834	80	6.03	6.03	10.05	10.05	-5.45	-73.9

49	38	-6115	-9	42	0	-826	3	6.03	6.03	10.05	10.05	-5.41	-73.4
50	38	-6116	315	46	0	-852	160	6.03	6.03	10.05	10.05	-5.53	-74.9
51	38	-6120	141	52	0	-867	75	6.03	6.03	10.05	10.05	-5.60	-75.7

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	50	-6352	-283	69	0	-976	-165	6.03	6.03	10.05	10.05	-6.18	-83.0
41	50	-6351	195	71	0	-1001	127	6.03	6.03	10.05	10.05	-6.31	-84.5
42	50	-6369	166	101	0	-1104	109	6.03	6.03	10.05	10.05	-6.86	-91.2
43	50	-6197	-624	53	0	-879	-373	6.03	6.03	10.05	10.05	-5.67	-76.7
44	50	-6203	997	76	0	-1013	616	6.03	6.03	10.05	10.05	-6.34	-84.8
45	50	-6224	125	106	0	-1092	83	6.03	6.03	10.05	10.05	-6.78	-89.9
46	50	-6102	159	48	0	-872	104	6.03	6.03	10.05	10.05	-5.62	-75.9
47	50	-6039	150	42	0	-839	99	6.03	6.03	10.05	10.05	-5.45	-73.8
49	50	-6040	-9	42	0	-831	2	6.03	6.03	10.05	10.05	-5.41	-73.4
50	50	-6041	315	46	0	-858	200	6.03	6.03	10.05	10.05	-5.54	-74.9
51	50	-6045	141	52	0	-874	93	6.03	6.03	10.05	10.05	-5.61	-75.8

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

ASTA NUM. 92 NI 1256 NF 1259 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 19
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-16410	153	-188	0	-489	-613	6.03	6.03	10.05	10.05	-9.23	-126.7
41	0	-16410	9	-217	0	-565	-56	6.03	6.03	10.05	10.05	-8.39	-120.8
42	0	-16340	10	-274	0	-731	-60	6.03	6.03	10.05	10.05	-8.96	-127.9
43	0	-15810	249	-132	0	-348	-984	6.03	6.03	10.05	10.05	-10.92	-144.8
44	0	-15900	-232	-276	0	-717	874	6.03	6.03	10.05	10.05	-10.39	-139.0
45	0	-15690	10	-275	0	-752	-62	6.03	6.03	10.05	10.05	-8.79	-125.1
46	0	-15460	8	-157	0	-421	-55	6.03	6.03	10.05	10.05	-7.51	-108.8
47	0	-15220	8	-142	0	-385	-55	6.03	6.03	10.05	10.05	-7.28	-105.8
49	0	-15220	56	-132	0	-360	-241	6.03	6.03	10.05	10.05	-7.19	-104.7
50	0	-15240	-40	-161	0	-434	131	6.03	6.03	10.05	10.05	-7.47	-108.1
51	0	-15200	9	-161	0	-441	-56	6.03	6.03	10.05	10.05	-7.48	-108.2

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	12	-16335	153	-188	0	-466	-594	6.03	6.03	10.05	10.05	-9.11	-125.1
41	12	-16335	9	-217	0	-538	-55	6.03	6.03	10.05	10.05	-8.27	-119.2
42	12	-16265	10	-274	0	-697	-59	6.03	6.03	10.05	10.05	-8.81	-125.9
43	12	-15735	249	-132	0	-332	-952	6.03	6.03	10.05	10.05	-10.74	-142.6
44	12	-15825	-232	-276	0	-683	845	6.03	6.03	10.05	10.05	-10.22	-136.9
45	12	-15615	10	-275	0	-718	-61	6.03	6.03	10.05	10.05	-8.64	-123.1
46	12	-15385	8	-157	0	-402	-54	6.03	6.03	10.05	10.05	-7.41	-107.5
47	12	-15145	8	-142	0	-367	-54	6.03	6.03	10.05	10.05	-7.19	-104.6
49	12	-15145	56	-132	0	-343	-234	6.03	6.03	10.05	10.05	-7.10	-103.5
50	12	-15165	-40	-161	0	-413	126	6.03	6.03	10.05	10.05	-7.36	-106.7
51	12	-15125	9	-161	0	-420	-55	6.03	6.03	10.05	10.05	-7.37	-106.8

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	25	-16260	153	-188	0	-442	-574	6.03	6.03	10.05	10.05	-8.98	-123.6
41	25	-16260	9	-217	0	-511	-54	6.03	6.03	10.05	10.05	-8.14	-117.5
42	25	-16190	10	-274	0	-663	-57	6.03	6.03	10.05	10.05	-8.66	-123.9
43	25	-15660	249	-132	0	-315	-921	6.03	6.03	10.05	10.05	-10.55	-140.4
44	25	-15750	-232	-276	0	-648	816	6.03	6.03	10.05	10.05	-10.04	-134.8
45	25	-15540	10	-275	0	-684	-60	6.03	6.03	10.05	10.05	-8.48	-121.1
46	25	-15310	8	-157	0	-382	-53	6.03	6.03	10.05	10.05	-7.31	-106.2
47	25	-15070	8	-142	0	-350	-53	6.03	6.03	10.05	10.05	-7.10	-103.3
49	25	-15070	56	-132	0	-327	-227	6.03	6.03	10.05	10.05	-7.02	-102.3
50	25	-15090	-40	-161	0	-393	121	6.03	6.03	10.05	10.05	-7.26	-105.4
51	25	-15050	9	-161	0	-400	-54	6.03	6.03	10.05	10.05	-7.27	-105.5

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	38	-16185	153	-188	0	-418	-555	6.03	6.03	10.05	10.05	-8.85	-122.1
41	38	-16185	9	-217	0	-484	-52	6.03	6.03	10.05	10.05	-8.01	-115.8
42	38	-16115	10	-274	0	-629	-56	6.03	6.03	10.05	10.05	-8.51	-122.0
43	38	-15585	249	-132	0	-299	-890	6.03	6.03	10.05	10.05	-10.36	-138.2
44	38	-15675	-232	-276	0	-614	787	6.03	6.03	10.05	10.05	-9.86	-132.7
45	38	-15465	10	-275	0	-649	-58	6.03	6.03	10.05	10.05	-8.33	-119.1
46	38	-15235	8	-157	0	-362	-52	6.03	6.03	10.05	10.05	-7.21	-104.9
47	38	-14995	8	-142	0	-332	-52	6.03	6.03	10.05	10.05	-7.01	-102.1
49	38	-14995	56	-132	0	-310	-220	6.03	6.03	10.05	10.05	-6.93	-101.1
50	38	-15015	-40	-161	0	-373	116	6.03	6.03	10.05	10.05	-7.16	-104.1
51	38	-14975	9	-161	0	-380	-53	6.03	6.03	10.05	10.05	-7.17	-104.1

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	50	-16110	153	-188	0	-395	-536	6.03	6.03	10.05	10.05	-8.73	-120.6
41	50	-16110	9	-217	0	-457	-51	6.03	6.03	10.05	10.05	-7.89	-114.2
42	50	-16040	10	-274	0	-594	-55	6.03	6.03	10.05	10.05	-8.36	-120.0
43	50	-15510	249	-132	0	-282	-859	6.03	6.03	10.05	10.05	-10.17	-136.0
44	50	-15600	-232	-276	0	-579	758	6.03	6.03	10.05	10.05	-9.68	-130.6
45	50	-15390	10	-275	0	-615	-57	6.03	6.03	10.05	10.05	-8.18	-117.1
46	50	-15160	8	-157	0	-343	-51	6.03	6.03	10.05	10.05	-7.11	-103.5
47	50	-14920	8	-142	0	-314	-51	6.03	6.03	10.05	10.05	-6.91	-100.9
49	50	-14920	56	-132	0	-294	-212	6.03	6.03	10.05	10.05	-6.84	-99.9
50	50	-14940	-40	-161	0	-353	111	6.03	6.03	10.05	10.05	-7.06	-102.7
51	50	-14900	9	-161	0	-360	-52	6.03	6.03	10.05	10.05	-7.07	-102.8

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

ASTA NUM. 93 NI 1259 NF 127 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 19A
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	

40	0	-16110	153	-188	0	-395	-536	6.03	6.03	10.05	10.05	-8.73	-120.6
41	0	-16110	9	-217	0	-457	-51	6.03	6.03	10.05	10.05	-7.89	-114.2
42	0	-16040	10	-274	0	-594	-55	6.03	6.03	10.05	10.05	-8.36	-120.0
43	0	-15510	249	-132	0	-282	-859	6.03	6.03	10.05	10.05	-10.17	-136.0
44	0	-15600	-232	-276	0	-579	758	6.03	6.03	10.05	10.05	-9.68	-130.6
45	0	-15390	10	-275	0	-615	-57	6.03	6.03	10.05	10.05	-8.18	-117.1
46	0	-15160	8	-157	0	-343	-51	6.03	6.03	10.05	10.05	-7.11	-103.5
47	0	-14920	8	-142	0	-314	-51	6.03	6.03	10.05	10.05	-6.91	-100.9
49	0	-14920	56	-132	0	-294	-212	6.03	6.03	10.05	10.05	-6.84	-99.9
50	0	-14940	-40	-161	0	-353	111	6.03	6.03	10.05	10.05	-7.06	-102.7
51	0	-14900	9	-161	0	-360	-52	6.03	6.03	10.05	10.05	-7.07	-102.8

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	12	-16035	153	-188	0	-371	-517	6.03	6.03	10.05	10.05	-8.60	-119.0
41	12	-16035	9	-217	0	-430	-50	6.03	6.03	10.05	10.05	-7.76	-112.5
42	12	-15965	10	-274	0	-560	-54	6.03	6.03	10.05	10.05	-8.20	-118.0
43	12	-15435	249	-132	0	-266	-828	6.03	6.03	10.05	10.05	-9.98	-133.7
44	12	-15525	-232	-276	0	-545	729	6.03	6.03	10.05	10.05	-9.51	-128.5
45	12	-15315	10	-275	0	-581	-56	6.03	6.03	10.05	10.05	-8.02	-115.1
46	12	-15085	8	-157	0	-323	-50	6.03	6.03	10.05	10.05	-7.01	-102.2
47	12	-14845	8	-142	0	-297	-50	6.03	6.03	10.05	10.05	-6.82	-99.6
49	12	-14845	56	-132	0	-277	-205	6.03	6.03	10.05	10.05	-6.75	-98.7
50	12	-14865	-40	-161	0	-333	106	6.03	6.03	10.05	10.05	-6.96	-101.4
51	12	-14825	9	-161	0	-340	-51	6.03	6.03	10.05	10.05	-6.97	-101.5

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	25	-15960	153	-188	0	-348	-498	6.03	6.03	10.05	10.05	-8.48	-117.5
41	25	-15960	9	-217	0	-402	-49	6.03	6.03	10.05	10.05	-7.63	-110.9
42	25	-15890	10	-274	0	-526	-52	6.03	6.03	10.05	10.05	-8.05	-116.0
43	25	-15360	249	-132	0	-249	-797	6.03	6.03	10.05	10.05	-9.80	-131.5
44	25	-15450	-232	-276	0	-510	700	6.03	6.03	10.05	10.05	-9.33	-126.4
45	25	-15240	10	-275	0	-546	-55	6.03	6.03	10.05	10.05	-7.87	-113.2
46	25	-15010	8	-157	0	-304	-49	6.03	6.03	10.05	10.05	-6.91	-100.9
47	25	-14770	8	-142	0	-279	-49	6.03	6.03	10.05	10.05	-6.73	-98.4
49	25	-14770	56	-132	0	-261	-198	6.03	6.03	10.05	10.05	-6.66	-97.6
50	25	-14790	-40	-161	0	-313	101	6.03	6.03	10.05	10.05	-6.86	-100.0
51	25	-14750	9	-161	0	-320	-50	6.03	6.03	10.05	10.05	-6.87	-100.1

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	38	-15885	153	-188	0	-324	-479	6.03	6.03	10.05	10.05	-8.35	-116.0
41	38	-15885	9	-217	0	-375	-48	6.03	6.03	10.05	10.05	-7.51	-109.2
42	38	-15815	10	-274	0	-492	-51	6.03	6.03	10.05	10.05	-7.90	-114.0
43	38	-15285	249	-132	0	-233	-766	6.03	6.03	10.05	10.05	-9.61	-129.3
44	38	-15375	-232	-276	0	-476	671	6.03	6.03	10.05	10.05	-9.15	-124.3
45	38	-15165	10	-275	0	-512	-53	6.03	6.03	10.05	10.05	-7.72	-111.2
46	38	-14935	8	-157	0	-284	-48	6.03	6.03	10.05	10.05	-6.81	-99.6
47	38	-14695	8	-142	0	-261	-48	6.03	6.03	10.05	10.05	-6.63	-97.2
49	38	-14695	56	-132	0	-244	-191	6.03	6.03	10.05	10.05	-6.57	-96.4
50	38	-14715	-40	-161	0	-293	96	6.03	6.03	10.05	10.05	-6.76	-98.7
51	38	-14675	9	-161	0	-300	-49	6.03	6.03	10.05	10.05	-6.77	-98.8

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	50	-15810	153	-188	0	-300	-460	6.03	6.03	10.05	10.05	-8.22	-114.5
41	50	-15810	9	-217	0	-348	-47	6.03	6.03	10.05	10.05	-7.38	-107.6
42	50	-15740	10	-274	0	-457	-50	6.03	6.03	10.05	10.05	-7.75	-112.1
43	50	-15210	249	-132	0	-216	-735	6.03	6.03	10.05	10.05	-9.42	-127.1
44	50	-15300	-232	-276	0	-442	642	6.03	6.03	10.05	10.05	-8.97	-122.2
45	50	-15090	10	-275	0	-478	-52	6.03	6.03	10.05	10.05	-7.57	-109.2
46	50	-14860	8	-157	0	-264	-47	6.03	6.03	10.05	10.05	-6.71	-98.3
47	50	-14620	8	-142	0	-243	-47	6.03	6.03	10.05	10.05	-6.54	-95.9
49	50	-14620	56	-132	0	-228	-184	6.03	6.03	10.05	10.05	-6.48	-95.2
50	50	-14640	-40	-161	0	-272	91	6.03	6.03	10.05	10.05	-6.65	-97.4
51	50	-14600	9	-161	0	-280	-48	6.03	6.03	10.05	10.05	-6.66	-97.4

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

ASTA NUM. 94 NI 1034 NF 1040 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 20
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-29500	634	744	0	1627	-1906	6.03	6.03	10.05	10.05	-20.75	-274.4
41	0	-29830	124	690	0	1499	-366	6.03	6.03	10.05	10.05	-16.96	-240.8
42	0	-29760	128	542	0	1189	-375	6.03	6.03	10.05	10.05	-15.81	-226.5
43	0	-28060	960	708	0	1592	-2899	6.03	6.03	10.05	10.05	-26.16	-331.1
44	0	-30110	-726	592	0	1251	2203	6.03	6.03	10.05	10.05	-22.51	-295.0
45	0	-28510	116	373	0	862	-347	6.03	6.03	10.05	10.05	-14.15	-204.5
46	0	-27910	101	577	0	1305	-310	6.03	6.03	10.05	10.05	-15.51	-220.9
47	0	-27420	96	549	0	1257	-296	6.03	6.03	10.05	10.05	-15.15	-215.9
49	0	-27310	266	566	0	1300	-810	6.03	6.03	10.05	10.05	-15.26	-217.2
50	0	-27720	-71	543	0	1231	211	6.03	6.03	10.05	10.05	-15.17	-216.5
51	0	-27400	97	499	0	1154	-299	6.03	6.03	10.05	10.05	-14.77	-211.2

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	12	-29425	634	744	0	1534	-1827	6.03	6.03	10.05	10.05	-20.31	-269.3
41	12	-29755	124	690	0	1413	-350	6.03	6.03	10.05	10.05	-16.62	-236.5
42	12	-29685	128	542	0	1121	-359	6.03	6.03	10.05	10.05	-15.54	-223.0
43	12	-27985	960	708	0	1504	-2779	6.03	6.03	10.05	10.05	-25.31	-322.0
44	12	-30035	-726	592	0	1177	2112	6.03	6.03	10.05	10.05	-22.01	-289.3
45	12	-28435	116	373	0	816	-332	6.03	6.03	10.05	10.05	-13.95	-202.0
46	12	-27835	101	577	0	1233	-297	6.03	6.03	10.05	10.05	-15.22	-217.3
47	12	-27345	96	549	0	1188	-284	6.03	6.03	10.05	10.05	-14.87	-212.4
49	12	-27235	266	566	0	1229	-776	6.03	6.03	10.05	10.05	-14.98	-213.6
50	12	-27645	-71	543	0	1163	202	6.03	6.03	10.05	10.05	-14.90	-213.0
51	12	-27325	97	499	0	1092	-287	6.03	6.03	10.05	10.05	-14.52	-207.9

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	25	-29350	634	744	0	1442	-1748	6.03	6.03	10.05	10.05	-19.87	-264.3
41	25	-29680	124	690	0	1326	-335	6.03	6.03	10.05	10.05	-16.28	-232.2
42	25	-29610	128	542	0	1054	-343	6.03	6.03	10.05	10.05	-15.27	-219.5
43	25	-27910	960	708	0	1415	-2659	6.03	6.03	10.05	10.05	-24.50	-313.2
44	25	-29960	-726	592	0	1103	2022	6.03	6.03	10.05	10.05	-21.52	-283.6
45	25	-28360	116	373	0	769	-318	6.03	6.03	10.05	10.05	-13.76	-199.4
46	25	-27760	101	577	0	1161	-285	6.03	6.03	10.05	10.05	-14.94	-213.6
47	25	-27270	96	549	0	1120	-272	6.03	6.03	10.05	10.05	-14.60	-208.9
49	25	-27160	266	566	0	1158	-743	6.03	6.03	10.05	10.05	-14.69	-210.0
50	25	-27570	-71	543	0	1095	193	6.03	6.03	10.05	10.05	-14.63	-209.5
51	25	-27250	97	499	0	1029	-275	6.03	6.03	10.05	10.05	-14.26	-204.7

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	38	-29275	634	744	0	1349	-1668	6.03	6.03	10.05	10.05	-19.44	-259.3
41	38	-29605	124	690	0	1240	-319	6.03	6.03	10.05	10.05	-15.94	-227.9
42	38	-29535	128	542	0	986	-327	6.03	6.03	10.05	10.05	-14.99	-216.0
43	38	-27835	960	708	0	1326	-2539	6.03	6.03	10.05	10.05	-23.70	-304.6
44	38	-29885	-726	592	0	1029	1932	6.03	6.03	10.05	10.05	-21.02	-278.0
45	38	-28285	116	373	0	722	-303	6.03	6.03	10.05	10.05	-13.56	-196.9
46	38	-27685	101	577	0	1089	-272	6.03	6.03	10.05	10.05	-14.65	-209.9
47	38	-27195	96	549	0	1051	-260	6.03	6.03	10.05	10.05	-14.32	-205.4
49	38	-27085	266	566	0	1087	-710	6.03	6.03	10.05	10.05	-14.41	-206.3
50	38	-27495	-71	543	0	1028	184	6.03	6.03	10.05	10.05	-14.35	-206.0
51	38	-27175	97	499	0	966	-263	6.03	6.03	10.05	10.05	-14.01	-201.4

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	50	-29200	634	744	0	1256	-1589	6.03	6.03	10.05	10.05	-19.00	-254.3
41	50	-29530	124	690	0	1154	-304	6.03	6.03	10.05	10.05	-15.60	-223.6
42	50	-29460	128	542	0	918	-311	6.03	6.03	10.05	10.05	-14.72	-212.6
43	50	-27760	960	708	0	1238	-2419	6.03	6.03	10.05	10.05	-22.94	-296.2
44	50	-29810	-726	592	0	955	1841	6.03	6.03	10.05	10.05	-20.53	-272.3
45	50	-28210	116	373	0	676	-289	6.03	6.03	10.05	10.05	-13.36	-194.4
46	50	-27610	101	577	0	1017	-259	6.03	6.03	10.05	10.05	-14.36	-206.2
47	50	-27120	96	549	0	982	-248	6.03	6.03	10.05	10.05	-14.05	-201.8
49	50	-27010	266	566	0	1016	-677	6.03	6.03	10.05	10.05	-14.12	-202.7
50	50	-27420	-71	543	0	960	175	6.03	6.03	10.05	10.05	-14.08	-202.6
51	50	-27100	97	499	0	904	-251	6.03	6.03	10.05	10.05	-13.76	-198.2

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

ASTA NUM. 95 NI 1040 NF 301 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 20A
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-29200	634	744	0	1256	-1589	6.03	6.03	10.05	10.05	-19.00	-254.3
41	0	-29530	124	690	0	1154	-304	6.03	6.03	10.05	10.05	-15.60	-223.6
42	0	-29460	128	542	0	918	-311	6.03	6.03	10.05	10.05	-14.72	-212.6
43	0	-27760	960	708	0	1238	-2419	6.03	6.03	10.05	10.05	-22.94	-296.2
44	0	-29810	-726	592	0	955	1841	6.03	6.03	10.05	10.05	-20.53	-272.3
45	0	-28210	116	373	0	676	-289	6.03	6.03	10.05	10.05	-13.36	-194.4
46	0	-27610	101	577	0	1017	-259	6.03	6.03	10.05	10.05	-14.36	-206.2
47	0	-27120	96	549	0	982	-248	6.03	6.03	10.05	10.05	-14.05	-201.8
49	0	-27010	266	566	0	1016	-677	6.03	6.03	10.05	10.05	-14.12	-202.7
50	0	-27420	-71	543	0	960	175	6.03	6.03	10.05	10.05	-14.08	-202.6
51	0	-27100	97	499	0	904	-251	6.03	6.03	10.05	10.05	-13.76	-198.2

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	12	-29125	634	744	0	1163	-1510	6.03	6.03	10.05	10.05	-18.57	-249.3
41	12	-29455	124	690	0	1068	-288	6.03	6.03	10.05	10.05	-15.26	-219.2
42	12	-29385	128	542	0	850	-295	6.03	6.03	10.05	10.05	-14.45	-209.1
43	12	-27685	960	708	0	1149	-2299	6.03	6.03	10.05	10.05	-22.20	-288.0
44	12	-29735	-726	592	0	881	1750	6.03	6.03	10.05	10.05	-20.03	-266.6
45	12	-28135	116	373	0	629	-274	6.03	6.03	10.05	10.05	-13.17	-191.8
46	12	-27535	101	577	0	945	-247	6.03	6.03	10.05	10.05	-14.07	-202.6
47	12	-27045	96	549	0	914	-236	6.03	6.03	10.05	10.05	-13.77	-198.3
49	12	-26935	266	566	0	945	-644	6.03	6.03	10.05	10.05	-13.84	-199.1
50	12	-27345	-71	543	0	892	166	6.03	6.03	10.05	10.05	-13.81	-199.1
51	12	-27025	97	499	0	842	-239	6.03	6.03	10.05	10.05	-13.50	-194.9

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	25	-29050	634	744	0	1070	-1430	6.03	6.03	10.05	10.05	-18.13	-244.3
41	25	-29380	124	690	0	981	-273	6.03	6.03	10.05	10.05	-14.92	-214.9
42	25	-29310	128	542	0	783	-279	6.03	6.03	10.05	10.05	-14.17	-205.6
43	25	-27610	960	708	0	1061	-2179	6.03	6.03	10.05	10.05	-21.50	-280.1
44	25	-29660	-726	592	0	806	1660	6.03	6.03	10.05	10.05	-19.54	-260.9
45	25	-28060	116	373	0	582	-260	6.03	6.03	10.05	10.05	-12.97	-189.3
46	25	-27460	101	577	0	873	-234	6.03	6.03	10.05	10.05	-13.78	-198.9
47	25	-26970	96	549	0	845	-224	6.03	6.03	10.05	10.05	-13.49	-194.8
49	25	-26860	266	566	0	875	-610	6.03	6.03	10.05	10.05	-13.56	-195.5
50	25	-27270	-71	543	0	824	157	6.03	6.03	10.05	10.05	-13.53	-195.6
51	25	-26950	97	499	0	779	-227	6.03	6.03	10.05	10.05	-13.25	-191.7

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	38	-28975	634	744	0	977	-1351	6.03	6.03	10.05	10.05	-17.69	-239.3
41	38	-29305	124	690	0	895	-257	6.03	6.03	10.05	10.05	-14.58	-210.6
42	38	-29235	128	542	0	715	-263	6.03	6.03	10.05	10.05	-13.90	-202.1
43	38	-27535	960	708	0	972	-2059	6.03	6.03	10.05	10.05	-20.82	-272.4
44	38	-29585	-726	592	0	732	1569	6.03	6.03	10.05	10.05	-19.04	-255.3
45	38	-27985	116	373	0	536	-245	6.03	6.03	10.05	10.05	-12.77	-186.8
46	38	-27385	101	577	0	800	-221	6.03	6.03	10.05	10.05	-13.49	-195.2
47	38	-26895	96	549	0	777	-212	6.03	6.03	10.05	10.05	-13.22	-191.3
49	38	-26785	266	566	0	804	-577	6.03	6.03	10.05	10.05	-13.27	-191.9
50	38	-27195	-71	543	0	756	148	6.03	6.03	10.05	10.05	-13.26	-192.1
51	38	-26875	97	499	0	717	-214	6.03	6.03	10.05	10.05	-12.99	-188.5

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	50	-28900	634	744	0	884	-1272	6.03	6.03	10.05	10.05	-17.26	-234.3
41	50	-29230	124	690	0	808	-242	6.03	6.03	10.05	10.05	-14.24	-206.3
42	50	-29160	128	542	0	647	-247	6.03	6.03	10.05	10.05	-13.63	-198.6
43	50	-27460	960	708	0	884	-1939	6.03	6.03	10.05	10.05	-20.16	-264.9
44	50	-29510	-726	592	0	658	1478	6.03	6.03	10.05	10.05	-18.54	-249.6
45	50	-27910	116	373	0	489	-230	6.03	6.03	10.05	10.05	-12.58	-184.2
46	50	-27310	101	577	0	728	-209	6.03	6.03	10.05	10.05	-13.20	-191.5
47	50	-26820	96	549	0	708	-200	6.03	6.03	10.05	10.05	-12.94	-187.7
49	50	-26710	266	566	0	733	-544	6.03	6.03	10.05	10.05	-12.99	-188.2
50	50	-27120	-71	543	0	688	139	6.03	6.03	10.05	10.05	-12.99	-188.6
51	50	-26800	97	499	0	654	-202	6.03	6.03	10.05	10.05	-12.74	-185.2

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

ASTA NUM. 96 NI 1352 NF 1355 SEZ. Rp B= 0.400 H= 0.600 (pilastro)
PIL. NUM. 21
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-10070	1808	620	0	1279	-5288	10.05	10.05	6.03	6.03	-35.36	983.0
41	0	-10100	865	598	0	1218	-2556	10.05	10.05	6.03	6.03	-16.13	-203.0
42	0	-10120	870	573	0	1143	-2567	10.05	10.05	6.03	6.03	-16.21	-203.8
43	0	-9892	2261	612	0	1268	-6610	10.05	10.05	6.03	6.03	-44.30	1415.9
44	0	-9950	-681	544	0	1084	1927	10.05	10.05	6.03	6.03	-11.92	-156.2
45	0	-9984	697	533	0	1041	-2075	10.05	10.05	6.03	6.03	-12.86	-166.9
46	0	-9851	584	562	0	1136	-1756	10.05	10.05	6.03	6.03	-10.89	-144.2
47	0	-9790	514	553	0	1115	-1557	10.05	10.05	6.03	6.03	-9.88	-131.2
49	0	-9779	828	560	0	1135	-2467	10.05	10.05	6.03	6.03	-15.57	-196.0
50	0	-9791	240	546	0	1099	-760	10.05	10.05	6.03	6.03	-9.76	-122.1
51	0	-9798	516	544	0	1090	-1560	10.05	10.05	6.03	6.03	-9.81	-131.4

apost= 6.03 aant= 6.03 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	12	-9994	1808	620	0	1201	-5062	10.05	10.05	6.03	6.03	-33.82	917.1
41	12	-10024	865	598	0	1143	-2448	10.05	10.05	6.03	6.03	-15.39	-194.7
42	12	-10046	870	573	0	1071	-2458	10.05	10.05	6.03	6.03	-15.46	-195.6
43	12	-9817	2261	612	0	1191	-6328	10.05	10.05	6.03	6.03	-42.41	1330.7
44	12	-9875	-681	544	0	1016	1842	10.05	10.05	6.03	6.03	-11.40	-150.1
45	12	-9909	697	533	0	974	-1988	10.05	10.05	6.03	6.03	-12.31	-160.5
46	12	-9776	584	562	0	1066	-1683	10.05	10.05	6.03	6.03	-10.47	-139.2
47	12	-9715	514	553	0	1046	-1492	10.05	10.05	6.03	6.03	-9.45	-127.0
49	12	-9704	828	560	0	1065	-2364	10.05	10.05	6.03	6.03	-14.85	-188.1
50	12	-9716	240	546	0	1031	-730	10.05	10.05	6.03	6.03	-9.25	-116.6
51	12	-9723	516	544	0	1022	-1496	10.05	10.05	6.03	6.03	-9.47	-127.2

apost= 6.03 aant= 6.03 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	25	-9918	1808	620	0	1124	-4836	10.05	10.05	6.03	6.03	-32.27	851.5
41	25	-9949	865	598	0	1068	-2340	10.05	10.05	6.03	6.03	-14.65	-186.5
42	25	-9972	870	573	0	1000	-2350	10.05	10.05	6.03	6.03	-14.71	-187.3
43	25	-9742	2261	612	0	1115	-6045	10.05	10.05	6.03	6.03	-40.51	1245.7
44	25	-9800	-681	544	0	948	1757	10.05	10.05	6.03	6.03	-10.90	-144.1
45	25	-9834	697	533	0	908	-1900	10.05	10.05	6.03	6.03	-11.76	-154.1
46	25	-9701	584	562	0	995	-1610	10.05	10.05	6.03	6.03	-10.06	-134.2
47	25	-9640	514	553	0	977	-1428	10.05	10.05	6.03	6.03	-9.11	-122.9
49	25	-9629	828	560	0	995	-2260	10.05	10.05	6.03	6.03	-14.15	-180.2
50	25	-9641	240	546	0	962	-700	10.05	10.05	6.03	6.03	-8.75	-111.3
51	25	-9648	516	544	0	954	-1431	10.05	10.05	6.03	6.03	-9.13	-123.1

apost= 6.03 aant= 6.03 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	37	-9843	1808	620	0	1046	-4610	10.05	10.05	6.03	6.03	-30.72	786.2
41	37	-9873	865	598	0	994	-2231	10.05	10.05	6.03	6.03	-13.91	-178.3
42	37	-9897	870	573	0	928	-2241	10.05	10.05	6.03	6.03	-13.98	-179.1
43	37	-9667	2261	612	0	1038	-5762	10.05	10.05	6.03	6.03	-38.60	1160.9
44	37	-9725	-681	544	0	880	1672	10.05	10.05	6.03	6.03	-10.40	-138.3
45	37	-9759	697	533	0	841	-1813	10.05	10.05	6.03	6.03	-11.23	-147.9
46	37	-9626	584	562	0	925	-1537	10.05	10.05	6.03	6.03	-9.66	-129.4
47	37	-9565	514	553	0	908	-1364	10.05	10.05	6.03	6.03	-8.79	-118.8
49	37	-9554	828	560	0	925	-2156	10.05	10.05	6.03	6.03	-13.45	-172.4
50	37	-9566	240	546	0	894	-670	10.05	10.05	6.03	6.03	-8.28	-106.1
51	37	-9573	516	544	0	886	-1366	10.05	10.05	6.03	6.03	-8.81	-119.1

apost= 6.03 aant= 6.03 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	50	-9767	1808	620	0	969	-4384	10.05	10.05	6.03	6.03	-29.17	721.2
41	50	-9798	865	598	0	919	-2123	10.05	10.05	6.03	6.03	-13.19	-170.2
42	50	-9823	870	573	0	856	-2132	10.05	10.05	6.03	6.03	-13.25	-170.9
43	50	-9592	2261	612	0	962	-5480	10.05	10.05	6.03	6.03	-36.69	1076.4
44	50	-9650	-681	544	0	812	1587	10.05	10.05	6.03	6.03	-9.93	-132.6
45	50	-9684	697	533	0	774	-1726	10.05	10.05	6.03	6.03	-10.71	-141.8
46	50	-9551	584	562	0	855	-1464	10.05	10.05	6.03	6.03	-9.27	-124.6
47	50	-9490	514	553	0	839	-1299	10.05	10.05	6.03	6.03	-8.47	-114.9
49	50	-9479	828	560	0	855	-2053	10.05	10.05	6.03	6.03	-12.76	-164.6
50	50	-9491	240	546	0	825	-640	10.05	10.05	6.03	6.03	-7.83	-101.1
51	50	-9498	516	544	0	818	-1302	10.05	10.05	6.03	6.03	-8.49	-115.1

apost= 6.03 aant= 6.03 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

ASTA NUM. 97 NI 1355 NF 172 SEZ. Rp B= 0.400 H= 0.600 (pilastro)
PIL. NUM. 21A
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-9767	1808	620	0	969	-4384	10.05	10.05	6.03	6.03	-29.17	721.2
41	0	-9798	865	598	0	919	-2123	10.05	10.05	6.03	6.03	-13.19	-170.2
42	0	-9823	870	573	0	856	-2132	10.05	10.05	6.03	6.03	-13.25	-170.9
43	0	-9592	2261	612	0	962	-5480	10.05	10.05	6.03	6.03	-36.69	1076.4

44	0	-9650	-681	544	0	812	1587	10.05	10.05	6.03	6.03	-9.93	-132.6
45	0	-9684	697	533	0	774	-1726	10.05	10.05	6.03	6.03	-10.71	-141.8
46	0	-9551	584	562	0	855	-1464	10.05	10.05	6.03	6.03	-9.27	-124.6
47	0	-9490	514	553	0	839	-1299	10.05	10.05	6.03	6.03	-8.47	-114.9
49	0	-9479	828	560	0	855	-2053	10.05	10.05	6.03	6.03	-12.76	-164.6
50	0	-9491	240	546	0	825	-640	10.05	10.05	6.03	6.03	-7.83	-101.1
51	0	-9498	516	544	0	818	-1302	10.05	10.05	6.03	6.03	-8.49	-115.1

apost= 6.03 aant= 6.03 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	12	-9692	1808	620	0	891	-4158	10.05	10.05	6.03	6.03	-27.60	656.6
41	12	-9723	865	598	0	844	-2015	10.05	10.05	6.03	6.03	-12.49	-162.1
42	12	-9748	870	573	0	784	-2024	10.05	10.05	6.03	6.03	-12.54	-162.8
43	12	-9517	2261	612	0	885	-5197	10.05	10.05	6.03	6.03	-34.78	992.0
44	12	-9575	-681	544	0	744	1502	10.05	10.05	6.03	6.03	-9.47	-127.0
45	12	-9609	697	533	0	708	-1639	10.05	10.05	6.03	6.03	-10.21	-135.8
46	12	-9476	584	562	0	784	-1391	10.05	10.05	6.03	6.03	-8.90	-120.0
47	12	-9415	514	553	0	770	-1235	10.05	10.05	6.03	6.03	-8.17	-111.1
49	12	-9404	828	560	0	785	-1950	10.05	10.05	6.03	6.03	-12.08	-156.9
50	12	-9416	240	546	0	757	-610	10.05	10.05	6.03	6.03	-7.41	-96.4
51	12	-9423	516	544	0	750	-1238	10.05	10.05	6.03	6.03	-8.19	-111.3

apost= 6.03 aant= 6.03 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	25	-9617	1808	620	0	814	-3932	10.05	10.05	6.03	6.03	-26.03	592.6
41	25	-9648	865	598	0	769	-1907	10.05	10.05	6.03	6.03	-11.80	-154.2
42	25	-9673	870	573	0	713	-1915	10.05	10.05	6.03	6.03	-11.85	-154.8
43	25	-9442	2261	612	0	809	-4914	10.05	10.05	6.03	6.03	-32.85	908.0
44	25	-9500	-681	544	0	676	1416	10.05	10.05	6.03	6.03	-9.03	-121.6
45	25	-9534	697	533	0	641	-1552	10.05	10.05	6.03	6.03	-9.72	-130.0
46	25	-9401	584	562	0	714	-1318	10.05	10.05	6.03	6.03	-8.54	-115.6
47	25	-9340	514	553	0	700	-1170	10.05	10.05	6.03	6.03	-7.88	-107.4
49	25	-9329	828	560	0	715	-1846	10.05	10.05	6.03	6.03	-11.42	-149.3
50	25	-9341	240	546	0	689	-580	10.05	10.05	6.03	6.03	-7.01	-91.8
51	25	-9348	516	544	0	682	-1174	10.05	10.05	6.03	6.03	-7.89	-107.6

apost= 6.03 aant= 6.03 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	38	-9542	1808	620	0	736	-3706	10.05	10.05	6.03	6.03	-24.46	529.3
41	38	-9573	865	598	0	694	-1799	10.05	10.05	6.03	6.03	-11.13	-146.5
42	38	-9598	870	573	0	641	-1806	10.05	10.05	6.03	6.03	-11.18	-147.0
43	38	-9367	2261	612	0	732	-4632	10.05	10.05	6.03	6.03	-30.92	824.3
44	38	-9425	-681	544	0	608	1331	10.05	10.05	6.03	6.03	-8.60	-116.4
45	38	-9459	697	533	0	574	-1465	10.05	10.05	6.03	6.03	-9.26	-124.3
46	38	-9326	584	562	0	644	-1245	10.05	10.05	6.03	6.03	-8.19	-111.2
47	38	-9265	514	553	0	631	-1106	10.05	10.05	6.03	6.03	-7.59	-103.8
49	38	-9254	828	560	0	645	-1742	10.05	10.05	6.03	6.03	-10.78	-141.8
50	38	-9266	240	546	0	620	-550	10.05	10.05	6.03	6.03	-6.63	-87.4
51	38	-9273	516	544	0	614	-1109	10.05	10.05	6.03	6.03	-7.61	-104.0

apost= 6.03 aant= 6.03 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	50	-9467	1808	620	0	659	-3480	10.05	10.05	6.03	6.03	-22.87	466.9
41	50	-9498	865	598	0	620	-1691	10.05	10.05	6.03	6.03	-10.49	-138.9
42	50	-9523	870	573	0	570	-1698	10.05	10.05	6.03	6.03	-10.53	-139.4
43	50	-9292	2261	612	0	656	-4349	10.05	10.05	6.03	6.03	-28.98	741.2
44	50	-9350	-681	544	0	540	1246	10.05	10.05	6.03	6.03	-8.20	-111.4
45	50	-9384	697	533	0	508	-1378	10.05	10.05	6.03	6.03	-8.81	-118.9
46	50	-9251	584	562	0	574	-1172	10.05	10.05	6.03	6.03	-7.85	-107.1
47	50	-9190	514	553	0	562	-1042	10.05	10.05	6.03	6.03	-7.32	-100.4
49	50	-9179	828	560	0	575	-1639	10.05	10.05	6.03	6.03	-10.17	-134.6
50	50	-9191	240	546	0	552	-520	10.05	10.05	6.03	6.03	-6.25	-83.1
51	50	-9198	516	544	0	546	-1045	10.05	10.05	6.03	6.03	-7.33	-100.5

apost= 6.03 aant= 6.03 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

ASTA NUM. 98 NI 479 NF 595 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 7
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-979	45	-327	0	-7	-28	4.02	4.02	10.05	10.05	-0.72	-9.5
41	0	-1069	194	-163	0	33	-76	4.02	4.02	10.05	10.05	-1.23	-14.8
42	0	-770	-98	-1072	0	-409	3	4.02	4.02	10.05	10.05	-3.83	113.7
43	0	-1000	-75	-456	0	-28	21	4.02	4.02	10.05	10.05	-0.67	-9.5
44	0	-1233	447	111	0	96	-160	4.02	4.02	10.05	10.05	-2.45	-25.3
45	0	-651	-313	-1698	0	-698	73	4.02	4.02	10.05	10.05	-6.55	265.6
46	0	-1200	161	-194	0	42	-49	4.02	4.02	10.05	10.05	-1.02	-13.0
47	0	-1232	153	-202	0	44	-42	4.02	4.02	10.05	10.05	-0.97	-12.6
49	0	-1202	103	-257	0	31	-26	4.02	4.02	10.05	10.05	-0.81	-11.3
50	0	-1249	207	-144	0	56	-62	4.02	4.02	10.05	10.05	-1.16	-14.6
51	0	-1132	55	-505	0	-103	-16	4.02	4.02	10.05	10.05	-1.09	-15.1

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	12	-923	45	-327	0	34	-22	4.02	4.02	10.05	10.05	-0.65	-9.3
41	12	-1013	194	-163	0	53	-52	4.02	4.02	10.05	10.05	-0.96	-12.0
42	12	-713	-98	-1072	0	-275	-9	4.02	4.02	10.05	10.05	-2.52	57.4
43	12	-944	-75	-456	0	29	12	4.02	4.02	10.05	10.05	-0.64	-9.2
44	12	-1177	447	111	0	82	-104	4.02	4.02	10.05	10.05	-1.61	-18.5
45	12	-595	-313	-1698	0	-485	34	4.02	4.02	10.05	10.05	-4.56	168.9
46	12	-1144	161	-194	0	66	-29	4.02	4.02	10.05	10.05	-0.92	-13.0
47	12	-1176	153	-202	0	69	-23	4.02	4.02	10.05	10.05	-0.95	-13.4
49	12	-1146	103	-257	0	63	-13	4.02	4.02	10.05	10.05	-0.90	-12.8
50	12	-1193	207	-144	0	74	-36	4.02	4.02	10.05	10.05	-0.98	-13.8
51	12	-1076	55	-505	0	-40	-9	4.02	4.02	10.05	10.05	-0.76	-10.8

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	25	-866	45	-327	0	75	-17	4.02	4.02	10.05	10.05	-0.82	-11.3
41	25	-957	194	-163	0	73	-28	4.02	4.02	10.05	10.05	-0.86	-11.9
42	25	-657	-98	-1072	0	-141	-22	4.02	4.02	10.05	10.05	-1.19	-15.4
43	25	-888	-75	-456	0	86	3	4.02	4.02	10.05	10.05	-0.88	-12.2
44	25	-1120	447	111	0	69	-48	4.02	4.02	10.05	10.05	-0.97	-12.9

45	25	-539	-313	-1698	0	-273	-6	4.02	4.02	10.05	10.05	-2.55	73.4
46	25	-1087	161	-194	0	90	-9	4.02	4.02	10.05	10.05	-1.01	-14.0
47	25	-1120	153	-202	0	95	-4	4.02	4.02	10.05	10.05	-1.04	-14.5
49	25	-1090	103	-257	0	95	-0	4.02	4.02	10.05	10.05	-1.03	-14.3
50	25	-1136	207	-144	0	92	-11	4.02	4.02	10.05	10.05	-1.04	-14.5
51	25	-1020	55	-505	0	23	-2	4.02	4.02	10.05	10.05	-0.64	-9.4

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	38	-810	45	-327	0	116	-11	4.02	4.02	10.05	10.05	-1.01	-13.6
41	38	-900	194	-163	0	94	-4	4.02	4.02	10.05	10.05	-0.92	-12.7
42	38	-601	-98	-1072	0	-7	-34	4.02	4.02	10.05	10.05	-0.59	-7.4
43	38	-831	-75	-456	0	143	-7	4.02	4.02	10.05	10.05	-1.21	-16.1
44	38	-1064	447	111	0	55	8	4.02	4.02	10.05	10.05	-0.82	-11.6
45	38	-483	-313	-1698	0	-61	-45	4.02	4.02	10.05	10.05	-0.69	-7.8
46	38	-1031	161	-194	0	115	11	4.02	4.02	10.05	10.05	-1.10	-15.0
47	38	-1063	153	-202	0	120	15	4.02	4.02	10.05	10.05	-1.14	-15.6
49	38	-1033	103	-257	0	127	13	4.02	4.02	10.05	10.05	-1.16	-15.9
50	38	-1080	207	-144	0	109	15	4.02	4.02	10.05	10.05	-1.10	-15.1
51	38	-963	55	-505	0	86	5	4.02	4.02	10.05	10.05	-0.92	-12.8

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	50	-754	45	-327	0	156	-5	4.02	4.02	10.05	10.05	-1.32	-17.1
41	50	-844	194	-163	0	114	21	4.02	4.02	10.05	10.05	-1.01	-13.7
42	50	-544	-98	-1072	0	127	-46	4.02	4.02	10.05	10.05	-1.09	-13.8
43	50	-775	-75	-456	0	200	-16	4.02	4.02	10.05	10.05	-1.74	22.2
44	50	-1008	447	111	0	41	63	4.02	4.02	10.05	10.05	-1.06	-13.0
45	50	-426	-313	-1698	0	152	-84	4.02	4.02	10.05	10.05	-1.38	28.7
46	50	-975	161	-194	0	139	31	4.02	4.02	10.05	10.05	-1.21	-16.4
47	50	-1007	153	-202	0	145	34	4.02	4.02	10.05	10.05	-1.26	-17.0
49	50	-977	103	-257	0	159	25	4.02	4.02	10.05	10.05	-1.35	-18.0
50	50	-1024	207	-144	0	127	41	4.02	4.02	10.05	10.05	-1.16	-15.8
51	50	-907	55	-505	0	150	12	4.02	4.02	10.05	10.05	-1.27	-16.9

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

ASTA NUM. 99 NI 595 NF 23 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 7A
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	--												
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-1069	55	-331	0	246	13	4.02	4.02	10.05	10.05	-2.10	-26.8
41	0	-1206	231	-210	0	193	59	4.02	4.02	10.05	10.05	-1.64	-21.9
42	0	-980	137	-483	0	426	45	4.02	4.02	10.05	10.05	-3.95	100.7
43	0	-1031	-32	-431	0	284	-20	4.02	4.02	10.05	10.05	-2.50	35.9
44	0	-1466	520	-3	0	105	136	4.02	4.02	10.05	10.05	-2.09	-23.8
45	0	-883	106	-685	0	585	33	4.02	4.02	10.05	10.05	-5.50	185.6
46	0	-1292	281	-242	0	198	54	4.02	4.02	10.05	10.05	-1.70	-22.8
47	0	-1313	293	-250	0	200	53	4.02	4.02	10.05	10.05	-1.71	-23.0
49	0	-1267	234	-290	0	217	37	4.02	4.02	10.05	10.05	-1.83	-24.3
50	0	-1354	345	-204	0	181	69	4.02	4.02	10.05	10.05	-1.61	-21.8
51	0	-1238	262	-340	0	277	48	4.02	4.02	10.05	10.05	-2.36	-30.2

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	12	-1013	55	-331	0	287	20	4.02	4.02	10.05	10.05	-2.53	38.3
41	12	-1150	231	-210	0	219	88	4.02	4.02	10.05	10.05	-1.84	-24.2
42	12	-924	137	-483	0	486	62	4.02	4.02	10.05	10.05	-4.55	134.4
43	12	-975	-32	-431	0	338	-24	4.02	4.02	10.05	10.05	-3.07	62.0
44	12	-1410	520	-3	0	105	201	4.02	4.02	10.05	10.05	-3.08	-31.0
45	12	-827	106	-685	0	671	46	4.02	4.02	10.05	10.05	-6.31	232.9
46	12	-1236	281	-242	0	228	89	4.02	4.02	10.05	10.05	-1.92	-25.3
47	12	-1257	293	-250	0	231	89	4.02	4.02	10.05	10.05	-1.94	-25.6
49	12	-1211	234	-290	0	253	67	4.02	4.02	10.05	10.05	-2.14	-27.7
50	12	-1298	345	-204	0	207	112	4.02	4.02	10.05	10.05	-1.76	-23.6
51	12	-1182	262	-340	0	320	81	4.02	4.02	10.05	10.05	-2.80	39.0

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	25	-957	55	-331	0	328	27	4.02	4.02	10.05	10.05	-2.98	59.4
41	25	-1094	231	-210	0	245	116	4.02	4.02	10.05	10.05	-2.09	-26.8
42	25	-868	137	-483	0	547	79	4.02	4.02	10.05	10.05	-5.14	169.0
43	25	-919	-32	-431	0	392	-28	4.02	4.02	10.05	10.05	-3.63	91.1
44	25	-1354	520	-3	0	105	266	4.02	4.02	10.05	10.05	-4.10	59.0
45	25	-770	106	-685	0	756	59	4.02	4.02	10.05	10.05	-7.10	280.7
46	25	-1180	281	-242	0	259	124	4.02	4.02	10.05	10.05	-2.20	-28.2
47	25	-1200	293	-250	0	262	126	4.02	4.02	10.05	10.05	-2.23	-28.6
49	25	-1154	234	-290	0	290	96	4.02	4.02	10.05	10.05	-2.51	-31.5
50	25	-1242	345	-204	0	232	155	4.02	4.02	10.05	10.05	-2.37	-25.7
51	25	-1126	262	-340	0	362	113	4.02	4.02	10.05	10.05	-3.26	59.8

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	38	-900	55	-331	0	370	34	4.02	4.02	10.05	10.05	-3.41	82.7
41	38	-1037	231	-210	0	272	145	4.02	4.02	10.05	10.05	-2.37	31.0
42	38	-811	137	-483	0	607	96	4.02	4.02	10.05	10.05	-5.71	204.1
43	38	-863	-32	-431	0	446	-32	4.02	4.02	10.05	10.05	-4.17	121.6
44	38	-1297	520	-3	0	106	331	4.02	4.02	10.05	10.05	-5.11	89.8
45	38	-714	106	-685	0	842	72	4.02	4.02	10.05	10.05	-7.89	328.6
46	38	-1123	281	-242	0	289	159	4.02	4.02	10.05	10.05	-2.51	31.7
47	38	-1144	293	-250	0	293	162	4.02	4.02	10.05	10.05	-2.55	31.9
49	38	-1098	234	-290	0	326	125	4.02	4.02	10.05	10.05	-2.90	47.1
50	38	-1185	345	-204	0	258	198	4.02	4.02	10.05	10.05	-3.05	37.0
51	38	-1069	262	-340	0	405	146	4.02	4.02	10.05	10.05	-3.71	82.9

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	50	-844	55	-331	0	411	41	4.02	4.02	10.05	10.05	-3.83	107.2
41	50	-981	231	-210	0	298	174	4.02	4.02	10.05	10.05	-2.68	44.9
42	50	-755	137	-483	0	668	113	4.02	4.02	10.05	10.05	-6.28	239.5
43	50	-806	-32	-431	0	500	-36	4.02	4.02	10.05	10.05	-4.69	153.0
44	50	-1241	520	-3	0	106	396	4.02	4.02	10.05	10.05	-6.10	121.3
45	50	-658	106	-685	0	927	85	4.02	4.02	10.05	10.05	-8.67	376.8

46	50	-1067	281	-242	0	319	194	4.02	4.02	10.05	10.05	-2.99	46.8
47	50	-1088	293	-250	0	324	199	4.02	4.02	10.05	10.05	-3.07	47.3
49	50	-1042	234	-290	0	362	155	4.02	4.02	10.05	10.05	-3.29	66.6
50	50	-1129	345	-204	0	283	241	4.02	4.02	10.05	10.05	-3.72	57.6
51	50	-1013	262	-340	0	448	179	4.02	4.02	10.05	10.05	-4.15	107.5

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

ASTA NUM. 100 NI 606 NF 624 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 1
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-7170	-818	487	0	-199	381	4.02	4.02	10.05	10.05	-6.88	-85.8
41	0	-7855	-525	260	0	-241	336	4.02	4.02	10.05	10.05	-6.79	-86.6
42	0	-7645	-515	131	0	-215	328	4.02	4.02	10.05	10.05	-6.62	-84.4
43	0	-6305	-997	623	0	-141	405	4.02	4.02	10.05	10.05	-6.74	-82.2
44	0	-9065	-43	-114	0	-317	263	4.02	4.02	10.05	10.05	-6.70	-90.1
45	0	-7097	-492	31	0	-168	317	4.02	4.02	10.05	10.05	-6.25	-79.4
46	0	-7203	-501	238	0	-194	326	4.02	4.02	10.05	10.05	-6.39	-81.0
47	0	-7040	-495	232	0	-182	324	4.02	4.02	10.05	10.05	-6.29	-79.6
49	0	-6811	-592	307	0	-168	339	4.02	4.02	10.05	10.05	-6.32	-79.4
50	0	-7363	-402	160	0	-203	310	4.02	4.02	10.05	10.05	-6.32	-80.7
51	0	-6969	-492	189	0	-173	321	4.02	4.02	10.05	10.05	-6.23	-78.9

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	12	-7114	-818	487	0	-260	279	4.02	4.02	10.05	10.05	-5.92	-76.1
41	12	-7799	-525	260	0	-274	270	4.02	4.02	10.05	10.05	-6.17	-80.2
42	12	-7589	-515	131	0	-231	264	4.02	4.02	10.05	10.05	-6.01	-78.1
43	12	-6249	-997	623	0	-219	281	4.02	4.02	10.05	10.05	-5.52	-70.1
44	12	-9009	-43	-114	0	-303	257	4.02	4.02	10.05	10.05	-6.62	-88.8
45	12	-7041	-492	31	0	-172	255	4.02	4.02	10.05	10.05	-5.67	-73.4
46	12	-7147	-501	238	0	-224	263	4.02	4.02	10.05	10.05	-5.79	-74.9
47	12	-6984	-495	232	0	-211	262	4.02	4.02	10.05	10.05	-5.70	-73.6
49	12	-6755	-592	307	0	-206	265	4.02	4.02	10.05	10.05	-5.62	-72.2
50	12	-7307	-402	160	0	-223	260	4.02	4.02	10.05	10.05	-5.84	-75.8
51	12	-6913	-492	189	0	-197	259	4.02	4.02	10.05	10.05	-5.65	-72.9

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	25	-7058	-818	487	0	-320	177	4.02	4.02	10.05	10.05	-5.24	-74.6
41	25	-7742	-525	260	0	-306	205	4.02	4.02	10.05	10.05	-5.54	-79.1
42	25	-7532	-515	131	0	-248	200	4.02	4.02	10.05	10.05	-5.40	-73.9
43	25	-6192	-997	623	0	-297	156	4.02	4.02	10.05	10.05	-4.67	-66.5
44	25	-8952	-43	-114	0	-289	252	4.02	4.02	10.05	10.05	-6.55	-87.5
45	25	-6984	-492	31	0	-175	194	4.02	4.02	10.05	10.05	-5.08	-67.4
46	25	-7090	-501	238	0	-253	201	4.02	4.02	10.05	10.05	-5.20	-70.8
47	25	-6928	-495	232	0	-240	200	4.02	4.02	10.05	10.05	-5.11	-68.7
49	25	-6698	-592	307	0	-245	191	4.02	4.02	10.05	10.05	-4.92	-67.2
50	25	-7250	-402	160	0	-243	210	4.02	4.02	10.05	10.05	-5.35	-71.4
51	25	-6856	-492	189	0	-221	198	4.02	4.02	10.05	10.05	-5.06	-67.0

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	38	-7001	-818	487	0	-381	75	4.02	4.02	10.05	10.05	-5.50	-77.9
41	38	-7686	-525	260	0	-339	139	4.02	4.02	10.05	10.05	-5.65	-80.7
42	38	-7476	-515	131	0	-264	135	4.02	4.02	10.05	10.05	-5.18	-74.5
43	38	-6136	-997	623	0	-375	31	4.02	4.02	10.05	10.05	-5.02	-70.8
44	38	-8896	-43	-114	0	-274	247	4.02	4.02	10.05	10.05	-6.47	-86.2
45	38	-6928	-492	31	0	-179	132	4.02	4.02	10.05	10.05	-4.50	-65.0
46	38	-7034	-501	238	0	-283	138	4.02	4.02	10.05	10.05	-5.04	-72.2
47	38	-6871	-495	232	0	-269	138	4.02	4.02	10.05	10.05	-4.89	-70.1
49	38	-6642	-592	307	0	-283	116	4.02	4.02	10.05	10.05	-4.84	-69.1
50	38	-7194	-402	160	0	-263	160	4.02	4.02	10.05	10.05	-5.03	-72.2
51	38	-6800	-492	189	0	-244	137	4.02	4.02	10.05	10.05	-4.73	-68.0

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	50	-6945	-818	487	0	-442	-28	4.02	4.02	10.05	10.05	-5.77	-81.2
41	50	-7630	-525	260	0	-371	73	4.02	4.02	10.05	10.05	-5.78	-82.2
42	50	-7420	-515	131	0	-280	71	4.02	4.02	10.05	10.05	-5.23	-75.0
43	50	-6080	-997	623	0	-453	-93	4.02	4.02	10.05	10.05	-5.37	-75.1
44	50	-8840	-43	-114	0	-260	241	4.02	4.02	10.05	10.05	-6.40	-85.0
45	50	-6872	-492	31	0	-183	70	4.02	4.02	10.05	10.05	-4.47	-64.8
46	50	-6978	-501	238	0	-313	76	4.02	4.02	10.05	10.05	-5.16	-73.6
47	50	-6815	-495	232	0	-298	76	4.02	4.02	10.05	10.05	-5.00	-71.4
49	50	-6586	-592	307	0	-322	42	4.02	4.02	10.05	10.05	-5.00	-71.0
50	50	-7138	-402	160	0	-283	109	4.02	4.02	10.05	10.05	-5.10	-73.0
51	50	-6744	-492	189	0	-268	75	4.02	4.02	10.05	10.05	-4.82	-69.0

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

ASTA NUM. 101 NI 624 NF 293 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 1A
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-9032	-1111	190	0	-476	-68	4.02	4.02	10.05	10.05	-7.02	-99.6
41	0	-9591	-105	-34	0	-386	68	4.02	4.02	10.05	10.05	-6.88	-98.5
42	0	-9378	-108	-299	0	-282	67	4.02	4.02	10.05	10.05	-6.26	-90.4
43	0	-8114	-1731	294	0	-494	-163	4.02	4.02	10.05	10.05	-6.64	-93.5
44	0	-10610	1563	-398	0	-245	295	4.02	4.02	10.05	10.05	-7.72	-102.5
45	0	-8692	-59	-521	0	-171	61	4.02	4.02	10.05	10.05	-5.36	-78.3
46	0	-8720	-24	-107	0	-321	60	4.02	4.02	10.05	10.05	-6.10	-87.6
47	0	-8502	-3	-125	0	-304	58	4.02	4.02	10.05	10.05	-5.91	-84.9
49	0	-8316	-339	-51	0	-334	13	4.02	4.02	10.05	10.05	-5.96	-85.3
50	0	-8815	320	-189	0	-284	104	4.02	4.02	10.05	10.05	-5.97	-86.2

51	0	-8432	-4	-214	0	-269	58	4.02	4.02	10.05	10.05	-5.70	-82.3

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	12	-8976	-1111	190	0	-500	-207	4.02	4.02	10.05	10.05	-7.11	-100.6
41	12	-9535	-105	-34	0	-382	55	4.02	4.02	10.05	10.05	-6.83	-97.8
42	12	-9322	-108	-299	0	-244	54	4.02	4.02	10.05	10.05	-6.04	-87.7
43	12	-8058	-1731	294	0	-531	-380	4.02	4.02	10.05	10.05	-7.28	-95.3
44	12	-10552	1563	-398	0	-195	490	4.02	4.02	10.05	10.05	-9.47	-119.8
45	12	-8636	-59	-521	0	-105	54	4.02	4.02	10.05	10.05	-5.01	-73.9
46	12	-8664	-24	-107	0	-307	57	4.02	4.02	10.05	10.05	-6.01	-86.4
47	12	-8446	-3	-125	0	-288	58	4.02	4.02	10.05	10.05	-5.80	-83.5
49	12	-8260	-339	-51	0	-328	-29	4.02	4.02	10.05	10.05	-5.90	-84.5
50	12	-8759	320	-189	0	-260	144	4.02	4.02	10.05	10.05	-5.83	-84.3
51	12	-8376	-4	-214	0	-242	57	4.02	4.02	10.05	10.05	-5.54	-80.2

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	25	-8920	-1111	190	0	-524	-345	4.02	4.02	10.05	10.05	-7.38	-101.6
41	25	-9478	-105	-34	0	-378	42	4.02	4.02	10.05	10.05	-6.78	-97.1
42	25	-9266	-108	-299	0	-207	40	4.02	4.02	10.05	10.05	-5.83	-85.0
43	25	-8002	-1731	294	0	-568	-596	4.02	4.02	10.05	10.05	-9.50	-113.1
44	25	-10495	1563	-398	0	-145	685	4.02	4.02	10.05	10.05	-11.34	-138.0
45	25	-8580	-59	-521	0	-40	47	4.02	4.02	10.05	10.05	-4.66	-69.5
46	25	-8608	-24	-107	0	-294	54	4.02	4.02	10.05	10.05	-5.91	-85.1
47	25	-8390	-3	-125	0	-273	57	4.02	4.02	10.05	10.05	-5.70	-82.1
49	25	-8204	-339	-51	0	-321	-72	4.02	4.02	10.05	10.05	-5.84	-83.6
50	25	-8702	320	-189	0	-237	184	4.02	4.02	10.05	10.05	-5.82	-82.4
51	25	-8320	-4	-214	0	-216	57	4.02	4.02	10.05	10.05	-5.38	-78.1

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	38	-8863	-1111	190	0	-547	-484	4.02	4.02	10.05	10.05	-8.62	-107.3
41	38	-9422	-105	-34	0	-374	29	4.02	4.02	10.05	10.05	-6.73	-96.4
42	38	-9209	-108	-299	0	-170	27	4.02	4.02	10.05	10.05	-5.62	-82.3
43	38	-7945	-1731	294	0	-605	-813	4.02	4.02	10.05	10.05	-12.45	-137.9
44	38	-10438	1563	-398	0	-95	881	4.02	4.02	10.05	10.05	-13.71	-159.2
45	38	-8523	-59	-521	0	25	39	4.02	4.02	10.05	10.05	-4.56	-68.1
46	38	-8551	-24	-107	0	-280	51	4.02	4.02	10.05	10.05	-5.82	-83.9
47	38	-8333	-3	-125	0	-257	57	4.02	4.02	10.05	10.05	-5.59	-80.7
49	38	-8147	-339	-51	0	-315	-114	4.02	4.02	10.05	10.05	-5.78	-82.8
50	38	-8646	320	-189	0	-213	224	4.02	4.02	10.05	10.05	-6.15	-82.1
51	38	-8263	-4	-214	0	-189	56	4.02	4.02	10.05	10.05	-5.22	-76.1

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	50	-8807	-1111	190	0	-571	-623	4.02	4.02	10.05	10.05	-10.06	-120.9
41	50	-9366	-105	-34	0	-370	16	4.02	4.02	10.05	10.05	-6.68	-95.7
42	50	-9153	-108	-299	0	-132	13	4.02	4.02	10.05	10.05	-5.41	-79.5
43	50	-7889	-1731	294	0	-642	-1029	4.02	4.02	10.05	10.05	-15.77	-162.8
44	50	-10380	1563	-398	0	-46	1076	4.02	4.02	10.05	10.05	-16.48	-181.9
45	50	-8467	-59	-521	0	90	32	4.02	4.02	10.05	10.05	-4.85	-71.6
46	50	-8495	-24	-107	0	-267	48	4.02	4.02	10.05	10.05	-5.73	-82.6
47	50	-8277	-3	-125	0	-241	57	4.02	4.02	10.05	10.05	-5.49	-79.4
49	50	-8091	-339	-51	0	-309	-156	4.02	4.02	10.05	10.05	-5.72	-82.0
50	50	-8590	320	-189	0	-190	264	4.02	4.02	10.05	10.05	-6.49	-85.3
51	50	-8207	-4	-214	0	-162	56	4.02	4.02	10.05	10.05	-5.06	-74.0

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

ASTA NUM. 102 NI 218 NF 132 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 12
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	--												
	cm		daN			daN*m				cm^2		daN/cm^2	
40	0	-6452	53	-99	0	333	-5	6.03	6.03	10.05	10.05	-3.70	-52.5
41	0	-6179	127	-41	0	172	-11	6.03	6.03	10.05	10.05	-3.02	-43.7
42	0	-6210	112	-206	0	1592	-8	6.03	6.03	10.05	10.05	-10.06	-126.3
43	0	-6430	6	-127	0	399	-3	6.03	6.03	10.05	10.05	-3.93	-55.3
44	0	-5841	250	52	0	-85	-20	6.03	6.03	10.05	10.05	-2.57	-37.8
45	0	-6025	104	-306	0	2497	-7	6.03	6.03	10.05	10.05	-16.55	381.5
46	0	-5852	129	-25	0	106	-13	6.03	6.03	10.05	10.05	-2.65	-38.8
47	0	-5770	130	-21	0	90	-13	6.03	6.03	10.05	10.05	-2.56	-37.6
49	0	-5861	106	-40	0	143	-11	6.03	6.03	10.05	10.05	-2.79	-40.5
50	0	-5744	154	-4	0	47	-15	6.03	6.03	10.05	10.05	-2.39	-35.5
51	0	-5781	125	-75	0	563	-12	6.03	6.03	10.05	10.05	-4.27	-58.9

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	12	-6377	53	-99	0	346	1	6.03	6.03	10.05	10.05	-3.72	-52.6
41	12	-6104	127	-41	0	178	5	6.03	6.03	10.05	10.05	-3.00	-43.5
42	12	-6135	112	-206	0	1618	6	6.03	6.03	10.05	10.05	-10.26	129.1
43	12	-6355	6	-127	0	415	-2	6.03	6.03	10.05	10.05	-3.96	-55.6
44	12	-5766	250	52	0	-91	12	6.03	6.03	10.05	10.05	-2.56	-37.6
45	12	-5950	104	-306	0	2535	6	6.03	6.03	10.05	10.05	-16.82	397.8
46	12	-5777	129	-25	0	109	4	6.03	6.03	10.05	10.05	-2.63	-38.5
47	12	-5695	130	-21	0	92	3	6.03	6.03	10.05	10.05	-2.54	-37.3
49	12	-5786	106	-40	0	148	2	6.03	6.03	10.05	10.05	-2.78	-40.3
50	12	-5669	154	-4	0	47	5	6.03	6.03	10.05	10.05	-2.37	-35.1
51	12	-5706	125	-75	0	572	4	6.03	6.03	10.05	10.05	-4.27	-58.9

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	25	-6302	53	-99	0	358	8	6.03	6.03	10.05	10.05	-3.73	-52.7
41	25	-6029	127	-41	0	183	21	6.03	6.03	10.05	10.05	-2.99	-43.3
42	25	-6060	112	-206	0	1644	20	6.03	6.03	10.05	10.05	-10.46	138.6
43	25	-6280	6	-127	0	431	-2	6.03	6.03	10.05	10.05	-3.98	-55.9
44	25	-5691	250	52	0	-98	43	6.03	6.03	10.05	10.05	-2.56	-37.5
45	25	-5875	104	-306	0	2574	18	6.03	6.03	10.05	10.05	-17.10	414.3
46	25	-5702	129	-25	0	112	20	6.03	6.03	10.05	10.05	-2.61	-38.2
47	25	-5620	130	-21	0	95	19	6.03	6.03	10.05	10.05	-2.52	-36.9
49	25	-5711	106	-40	0	153	15	6.03	6.03	10.05	10.05	-2.76	-40.1
50	25	-5594	154	-4	0	48	24	6.03	6.03	10.05	10.05	-2.34	-34.7
51	25	-5631	125	-75	0	582	19	6.03	6.03	10.05	10.05	-4.28	-58.9

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	38	-6227	53	-99	0	370	14	6.03	6.03	10.05	10.05	-3.75	-52.9
41	38	-5954	127	-41	0	188	37	6.03	6.03	10.05	10.05	-2.98	-43.1
42	38	-5985	112	-206	0	1669	34	6.03	6.03	10.05	10.05	-10.66	148.4
43	38	-6205	6	-127	0	447	-1	6.03	6.03	10.05	10.05	-4.01	-56.2
44	38	-5616	250	52	0	-104	74	6.03	6.03	10.05	10.05	-2.55	-37.3
45	38	-5800	104	-306	0	2612	31	6.03	6.03	10.05	10.05	-17.38	430.9
46	38	-5627	129	-25	0	116	36	6.03	6.03	10.05	10.05	-2.60	-37.9
47	38	-5545	130	-21	0	97	36	6.03	6.03	10.05	10.05	-2.50	-36.6
49	38	-5636	106	-40	0	158	28	6.03	6.03	10.05	10.05	-2.75	-39.9
50	38	-5519	154	-4	0	48	43	6.03	6.03	10.05	10.05	-2.31	-34.2
51	38	-5556	125	-75	0	591	35	6.03	6.03	10.05	10.05	-4.28	-58.9

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	50	-6152	53	-99	0	383	21	6.03	6.03	10.05	10.05	-3.76	-53.0
41	50	-5879	127	-41	0	193	53	6.03	6.03	10.05	10.05	-2.97	-42.9
42	50	-5910	112	-206	0	1695	48	6.03	6.03	10.05	10.05	-10.86	158.4
43	50	-6130	6	-127	0	463	-0	6.03	6.03	10.05	10.05	-4.04	-56.4
44	50	-5541	250	52	0	-111	106	6.03	6.03	10.05	10.05	-2.60	-37.2
45	50	-5725	104	-306	0	2650	44	6.03	6.03	10.05	10.05	-17.65	447.5
46	50	-5552	129	-25	0	119	52	6.03	6.03	10.05	10.05	-2.58	-37.6
47	50	-5470	130	-21	0	100	52	6.03	6.03	10.05	10.05	-2.48	-36.3
49	50	-5561	106	-40	0	163	42	6.03	6.03	10.05	10.05	-2.74	-39.7
50	50	-5444	154	-4	0	49	63	6.03	6.03	10.05	10.05	-2.34	-33.9
51	50	-5481	125	-75	0	601	50	6.03	6.03	10.05	10.05	-4.29	-58.9

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

ASTA NUM. 103 NI 132 NF 40 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 12A
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-9713	225	-175	0	365	21	6.03	6.03	10.05	10.05	-5.08	-72.9
41	0	-9270	537	-72	0	181	53	6.03	6.03	10.05	10.05	-4.24	-62.0
42	0	-9304	501	-347	0	1537	48	6.03	6.03	10.05	10.05	-9.61	-128.3
43	0	-9684	6	-226	0	443	-0	6.03	6.03	10.05	10.05	-5.35	-76.2
44	0	-8718	1065	94	0	-114	106	6.03	6.03	10.05	10.05	-3.79	-55.8
45	0	-9003	466	-512	0	2398	44	6.03	6.03	10.05	10.05	-15.23	195.2
46	0	-8753	520	-43	0	111	52	6.03	6.03	10.05	10.05	-3.79	-55.9
47	0	-8623	516	-36	0	94	52	6.03	6.03	10.05	10.05	-3.68	-54.3
49	0	-8771	412	-70	0	155	42	6.03	6.03	10.05	10.05	-3.96	-57.9
50	0	-8577	624	-6	0	43	63	6.03	6.03	10.05	10.05	-3.50	-51.8
51	0	-8634	504	-128	0	546	50	6.03	6.03	10.05	10.05	-5.31	-74.7

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	12	-9638	225	-175	0	387	49	6.03	6.03	10.05	10.05	-5.13	-73.4
41	12	-9195	537	-72	0	190	120	6.03	6.03	10.05	10.05	-4.25	-62.0
42	12	-9229	501	-347	0	1580	110	6.03	6.03	10.05	10.05	-9.84	-130.8
43	12	-9609	6	-226	0	472	1	6.03	6.03	10.05	10.05	-5.42	-77.1
44	12	-8643	1065	94	0	-125	239	6.03	6.03	10.05	10.05	-4.43	-61.8
45	12	-8928	466	-512	0	2462	103	6.03	6.03	10.05	10.05	-15.70	214.3
46	12	-8678	520	-43	0	116	117	6.03	6.03	10.05	10.05	-3.82	-55.7
47	12	-8548	516	-36	0	98	116	6.03	6.03	10.05	10.05	-3.76	-54.2
49	12	-8696	412	-70	0	163	93	6.03	6.03	10.05	10.05	-3.96	-57.9
50	12	-8502	624	-6	0	44	141	6.03	6.03	10.05	10.05	-3.87	-55.4
51	12	-8559	504	-128	0	562	113	6.03	6.03	10.05	10.05	-5.34	-75.0

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	25	-9563	225	-175	0	408	77	6.03	6.03	10.05	10.05	-5.18	-74.0
41	25	-9120	537	-72	0	199	187	6.03	6.03	10.05	10.05	-4.34	-62.0
42	25	-9154	501	-347	0	1624	173	6.03	6.03	10.05	10.05	-10.08	-133.5
43	25	-9534	6	-226	0	500	1	6.03	6.03	10.05	10.05	-5.49	-77.9
44	25	-8568	1065	94	0	-137	372	6.03	6.03	10.05	10.05	-5.09	-69.1
45	25	-8853	466	-512	0	2526	161	6.03	6.03	10.05	10.05	-16.18	233.9
46	25	-8603	520	-43	0	122	182	6.03	6.03	10.05	10.05	-4.12	-58.3
47	25	-8473	516	-36	0	102	181	6.03	6.03	10.05	10.05	-4.07	-57.5
49	25	-8621	412	-70	0	172	144	6.03	6.03	10.05	10.05	-3.96	-57.9
50	25	-8427	624	-6	0	45	219	6.03	6.03	10.05	10.05	-4.25	-59.5
51	25	-8484	504	-128	0	577	176	6.03	6.03	10.05	10.05	-5.37	-75.3

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	38	-9488	225	-175	0	430	105	6.03	6.03	10.05	10.05	-5.23	-74.5
41	38	-9045	537	-72	0	208	254	6.03	6.03	10.05	10.05	-4.66	-65.0
42	38	-9079	501	-347	0	1668	236	6.03	6.03	10.05	10.05	-10.33	-136.2
43	38	-9459	6	-226	0	528	2	6.03	6.03	10.05	10.05	-5.57	-78.7
44	38	-8493	1065	94	0	-149	505	6.03	6.03	10.05	10.05	-5.75	-76.5
45	38	-8778	466	-512	0	2590	219	6.03	6.03	10.05	10.05	-16.65	254.2
46	38	-8528	520	-43	0	127	247	6.03	6.03	10.05	10.05	-4.43	-61.7
47	38	-8398	516	-36	0	107	246	6.03	6.03	10.05	10.05	-4.37	-60.9
49	38	-8546	412	-70	0	181	196	6.03	6.03	10.05	10.05	-4.17	-58.8
50	38	-8352	624	-6	0	46	297	6.03	6.03	10.05	10.05	-4.62	-63.6
51	38	-8409	504	-128	0	593	239	6.03	6.03	10.05	10.05	-5.39	-75.6

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	50	-9413	225	-175	0	452	134	6.03	6.03	10.05	10.05	-5.28	-75.1
41	50	-8970	537	-72	0	217	321	6.03	6.03	10.05	10.05	-4.98	-68.4
42	50	-9004	501	-347	0	1711	298	6.03	6.03	10.05	10.05	-10.59	-139.1
43	50	-9384	6	-226	0	556	3	6.03	6.03	10.05	10.05	-5.64	-79.6
44	50	-8418	1065	94	0	-160	638	6.03	6.03	10.05	10.05	-6.41	-83.8
45	50	-8703	466	-512	0	2654	278	6.03	6.03	10.05	10.05	-17.13	275.0
46	50	-8453	520	-43	0	133	312	6.03	6.03	10.05	10.05	-4.74	-65.1
47	50	-8323	516	-36	0	111	310	6.03	6.03	10.05	10.05	-4.68	-64.2
49	50	-8471	412	-70	0	190	248	6.03	6.03	10.05	10.05	-4.41	-61.4
50	50	-8277	624	-6	0	46	374	6.03	6.03	10.05	10.05	-4.99	-67.7
51	50	-8334	504	-128	0	609	302	6.03	6.03	10.05	10.05	-5.42	-75.9

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

ASTA NUM. 104 NI 1350 NF 1445 SEZ. Rp B= 0.400 H= 0.600 (pilastro)
PIL. NUM. 11
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-6124	1229	380	0	759	-4394	10.05	10.05	6.03	6.03	-29.44	973.5
41	0	-6493	600	354	0	682	-2356	10.05	10.05	6.03	6.03	-15.47	311.2
42	0	-6481	603	324	0	594	-2365	10.05	10.05	6.03	6.03	-15.54	314.5
43	0	-5875	1536	389	0	791	-5401	10.05	10.05	6.03	6.03	-36.10	1316.9
44	0	-7000	-430	306	0	546	986	10.05	10.05	6.03	6.03	-6.38	-86.3
45	0	-6469	494	297	0	515	-2020	10.05	10.05	6.03	6.03	-13.07	217.2
46	0	-6487	421	342	0	649	-1793	10.05	10.05	6.03	6.03	-11.44	156.7
47	0	-6486	376	338	0	641	-1652	10.05	10.05	6.03	6.03	-10.44	-131.2
49	0	-6363	585	347	0	667	-2331	10.05	10.05	6.03	6.03	-15.32	311.4
50	0	-6588	192	330	0	618	-1054	10.05	10.05	6.03	6.03	-6.62	-88.7
51	0	-6482	377	329	0	612	-1655	10.05	10.05	6.03	6.03	-10.46	-131.4

apost= 6.03 aant= 6.03 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	12	-6049	1229	380	0	712	-4240	10.05	10.05	6.03	6.03	-28.42	929.5
41	12	-6418	600	354	0	637	-2281	10.05	10.05	6.03	6.03	-14.95	293.7
42	12	-6406	603	324	0	554	-2290	10.05	10.05	6.03	6.03	-15.01	296.8
43	12	-5800	1536	389	0	742	-5209	10.05	10.05	6.03	6.03	-34.83	1260.3
44	12	-6925	-430	306	0	507	932	10.05	10.05	6.03	6.03	-6.11	-83.0
45	12	-6394	494	297	0	478	-1958	10.05	10.05	6.03	6.03	-12.65	204.3
46	12	-6412	421	342	0	606	-1740	10.05	10.05	6.03	6.03	-11.08	146.9
47	12	-6411	376	338	0	598	-1605	10.05	10.05	6.03	6.03	-10.12	-127.5
49	12	-6288	585	347	0	623	-2258	10.05	10.05	6.03	6.03	-14.81	294.5
50	12	-6513	192	330	0	576	-1030	10.05	10.05	6.03	6.03	-6.48	-86.9
51	12	-6407	377	329	0	570	-1608	10.05	10.05	6.03	6.03	-10.14	-127.8

apost= 6.03 aant= 6.03 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	25	-5974	1229	380	0	664	-4087	10.05	10.05	6.03	6.03	-27.39	885.6
41	25	-6343	600	354	0	593	-2206	10.05	10.05	6.03	6.03	-14.43	276.3
42	25	-6331	603	324	0	513	-2214	10.05	10.05	6.03	6.03	-14.49	279.3
43	25	-5725	1536	389	0	693	-5017	10.05	10.05	6.03	6.03	-33.56	1203.6
44	25	-6850	-430	306	0	469	878	10.05	10.05	6.03	6.03	-5.86	-79.8
45	25	-6319	494	297	0	441	-1897	10.05	10.05	6.03	6.03	-12.22	191.5
46	25	-6337	421	342	0	563	-1688	10.05	10.05	6.03	6.03	-10.72	137.3
47	25	-6336	376	338	0	556	-1558	10.05	10.05	6.03	6.03	-9.80	-123.9
49	25	-6213	585	347	0	580	-2185	10.05	10.05	6.03	6.03	-14.31	277.6
50	25	-6438	192	330	0	535	-1006	10.05	10.05	6.03	6.03	-6.35	-85.2
51	25	-6332	377	329	0	529	-1561	10.05	10.05	6.03	6.03	-9.82	-124.1

apost= 6.03 aant= 6.03 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	37	-5899	1229	380	0	617	-3934	10.05	10.05	6.03	6.03	-26.36	841.7
41	37	-6268	600	354	0	549	-2131	10.05	10.05	6.03	6.03	-13.91	259.0
42	37	-6256	603	324	0	472	-2138	10.05	10.05	6.03	6.03	-13.97	261.8
43	37	-5650	1536	389	0	645	-4825	10.05	10.05	6.03	6.03	-32.28	1147.0
44	37	-6775	-430	306	0	431	824	10.05	10.05	6.03	6.03	-5.61	-76.7
45	37	-6244	494	297	0	404	-1835	10.05	10.05	6.03	6.03	-11.79	178.8
46	37	-6262	421	342	0	521	-1635	10.05	10.05	6.03	6.03	-10.36	-129.6
47	37	-6261	376	338	0	514	-1511	10.05	10.05	6.03	6.03	-9.49	-120.3
49	37	-6138	585	347	0	536	-2112	10.05	10.05	6.03	6.03	-13.80	260.8
50	37	-6363	192	330	0	494	-982	10.05	10.05	6.03	6.03	-6.21	-83.4
51	37	-6257	377	329	0	488	-1514	10.05	10.05	6.03	6.03	-9.51	-120.5

apost= 6.03 aant= 6.03 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	50	-5824	1229	380	0	569	-3780	10.05	10.05	6.03	6.03	-25.33	797.8
41	50	-6193	600	354	0	504	-2056	10.05	10.05	6.03	6.03	-13.39	241.9
42	50	-6181	603	324	0	432	-2063	10.05	10.05	6.03	6.03	-13.44	244.5
43	50	-5575	1536	389	0	596	-4633	10.05	10.05	6.03	6.03	-31.01	1090.3
44	50	-6700	-430	306	0	393	770	10.05	10.05	6.03	6.03	-5.38	-73.7
45	50	-6169	494	297	0	367	-1773	10.05	10.05	6.03	6.03	-11.37	166.3
46	50	-6187	421	342	0	478	-1582	10.05	10.05	6.03	6.03	-10.00	-125.6
47	50	-6186	376	338	0	471	-1464	10.05	10.05	6.03	6.03	-9.17	-116.7
49	50	-6063	585	347	0	493	-2039	10.05	10.05	6.03	6.03	-13.30	244.2
50	50	-6288	192	330	0	452	-958	10.05	10.05	6.03	6.03	-6.08	-81.7
51	50	-6182	377	329	0	447	-1467	10.05	10.05	6.03	6.03	-9.19	-116.9

apost= 6.03 aant= 6.03 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

ASTA NUM. 105 NI 1445 NF 168 SEZ. Rp B= 0.400 H= 0.600 (pilastro)
PIL. NUM. 11A
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-5824	1229	380	0	569	-3780	10.05	10.05	6.03	6.03	-25.33	797.8
41	0	-6193	600	354	0	504	-2056	10.05	10.05	6.03	6.03	-13.39	241.9
42	0	-6181	603	324	0	432	-2063	10.05	10.05	6.03	6.03	-13.44	244.5
43	0	-5575	1536	389	0	596	-4633	10.05	10.05	6.03	6.03	-31.01	1090.3
44	0	-6700	-430	306	0	393	770	10.05	10.05	6.03	6.03	-5.38	-73.7
45	0	-6169	494	297	0	367	-1773	10.05	10.05	6.03	6.03	-11.37	166.3
46	0	-6187	421	342	0	478	-1582	10.05	10.05	6.03	6.03	-10.00	-125.6
47	0	-6186	376	338	0	471	-1464	10.05	10.05	6.03	6.03	-9.17	-116.7
49	0	-6063	585	347	0	493	-2039	10.05	10.05	6.03	6.03	-13.30	244.2
50	0	-6288	192	330	0	452	-958	10.05	10.05	6.03	6.03	-6.08	-81.7
51	0	-6182	377	329	0	447	-1467	10.05	10.05	6.03	6.03	-9.19	-116.9

apost= 6.03 aant= 6.03 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	12	-5749	1229	380	0	522	-3626	10.05	10.05	6.03	6.03	-24.30	754.0
41	12	-6118	600	354	0	460	-1981	10.05	10.05	6.03	6.03	-12.87	224.9

42	12	-6106	603	324	0	391	-1988	10.05	10.05	6.03	6.03	-12.92	227.4
43	12	-5500	1536	389	0	547	-4441	10.05	10.05	6.03	6.03	-29.73	1033.8
44	12	-6625	-430	306	0	355	717	10.05	10.05	6.03	6.03	-5.15	-70.8
45	12	-6094	494	297	0	330	-1711	10.05	10.05	6.03	6.03	-10.94	154.0
46	12	-6112	421	342	0	435	-1530	10.05	10.05	6.03	6.03	-9.64	-121.5
47	12	-6111	376	338	0	429	-1417	10.05	10.05	6.03	6.03	-8.86	-113.1
49	12	-5988	585	347	0	450	-1966	10.05	10.05	6.03	6.03	-12.79	227.6
50	12	-6213	192	330	0	411	-934	10.05	10.05	6.03	6.03	-5.94	-80.0
51	12	-6107	377	329	0	406	-1420	10.05	10.05	6.03	6.03	-8.88	-113.3

apost= 6.03 aant= 6.03 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	25	-5674	1229	380	0	474	-3472	10.05	10.05	6.03	6.03	-23.27	710.2
41	25	-6043	600	354	0	416	-1906	10.05	10.05	6.03	6.03	-12.35	208.1
42	25	-6031	603	324	0	351	-1912	10.05	10.05	6.03	6.03	-12.40	210.5
43	25	-5425	1536	389	0	499	-4249	10.05	10.05	6.03	6.03	-28.45	977.2
44	25	-6550	-430	306	0	316	663	10.05	10.05	6.03	6.03	-4.92	-67.9
45	25	-6019	494	297	0	293	-1650	10.05	10.05	6.03	6.03	-10.51	141.9
46	25	-6037	421	342	0	393	-1477	10.05	10.05	6.03	6.03	-9.29	-117.5
47	25	-6036	376	338	0	387	-1370	10.05	10.05	6.03	6.03	-8.55	-109.5
49	25	-5913	585	347	0	406	-1892	10.05	10.05	6.03	6.03	-12.28	211.2
50	25	-6138	192	330	0	370	-910	10.05	10.05	6.03	6.03	-5.81	-78.3
51	25	-6032	377	329	0	365	-1372	10.05	10.05	6.03	6.03	-8.56	-109.6

apost= 6.03 aant= 6.03 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	38	-5599	1229	380	0	427	-3319	10.05	10.05	6.03	6.03	-22.23	666.4
41	38	-5968	600	354	0	372	-1831	10.05	10.05	6.03	6.03	-11.83	191.5
42	38	-5956	603	324	0	310	-1837	10.05	10.05	6.03	6.03	-11.87	193.8
43	38	-5350	1536	389	0	450	-4057	10.05	10.05	6.03	6.03	-27.18	920.8
44	38	-6475	-430	306	0	278	609	10.05	10.05	6.03	6.03	-4.70	-65.0
45	38	-5944	494	297	0	256	-1588	10.05	10.05	6.03	6.03	-10.09	130.0
46	38	-5962	421	342	0	350	-1424	10.05	10.05	6.03	6.03	-8.93	-113.5
47	38	-5961	376	338	0	344	-1323	10.05	10.05	6.03	6.03	-8.24	-105.9
49	38	-5838	585	347	0	363	-1819	10.05	10.05	6.03	6.03	-11.77	195.0
50	38	-6063	192	330	0	328	-886	10.05	10.05	6.03	6.03	-5.67	-76.6
51	38	-5957	377	329	0	324	-1325	10.05	10.05	6.03	6.03	-8.25	-106.0

apost= 6.03 aant= 6.03 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	50	-5524	1229	380	0	379	-3165	10.05	10.05	6.03	6.03	-21.19	622.8
41	50	-5893	600	354	0	327	-1756	10.05	10.05	6.03	6.03	-11.30	175.2
42	50	-5881	603	324	0	270	-1762	10.05	10.05	6.03	6.03	-11.35	177.4
43	50	-5275	1536	389	0	402	-3865	10.05	10.05	6.03	6.03	-25.90	864.3
44	50	-6400	-430	306	0	240	555	10.05	10.05	6.03	6.03	-4.48	-62.2
45	50	-5869	494	297	0	218	-1526	10.05	10.05	6.03	6.03	-9.66	-121.0
46	50	-5887	421	342	0	307	-1372	10.05	10.05	6.03	6.03	-8.58	-109.4
47	50	-5886	376	338	0	302	-1276	10.05	10.05	6.03	6.03	-7.93	-102.3
49	50	-5763	585	347	0	320	-1746	10.05	10.05	6.03	6.03	-11.26	179.0
50	50	-5988	192	330	0	287	-862	10.05	10.05	6.03	6.03	-5.54	-74.9
51	50	-5882	377	329	0	283	-1278	10.05	10.05	6.03	6.03	-7.94	-102.4

apost= 6.03 aant= 6.03 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

ASTA NUM. 106 NI 1032 NF 1045 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 10
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-15260	79	1565	0	1477	-723	6.03	6.03	10.05	10.05	-11.23	-155.2
41	0	-13500	750	1136	0	1208	-634	6.03	6.03	10.05	10.05	-9.58	-132.8
42	0	-13320	753	1254	0	1134	-635	6.03	6.03	10.05	10.05	-9.24	-128.5
43	0	-16090	-304	1792	0	1584	-801	6.03	6.03	10.05	10.05	-11.94	-164.8
44	0	-10610	1859	457	0	781	-486	6.03	6.03	10.05	10.05	-6.92	-96.8
45	0	-12850	819	1274	0	1013	-655	6.03	6.03	10.05	10.05	-8.63	-120.3
46	0	-12950	851	1042	0	1093	-666	6.03	6.03	10.05	10.05	-8.95	-124.5
47	0	-12810	877	1019	0	1064	-674	6.03	6.03	10.05	10.05	-8.79	-122.3
49	0	-13400	653	1162	0	1154	-703	6.03	6.03	10.05	10.05	-9.35	-129.8
50	0	-12300	1086	895	0	993	-640	6.03	6.03	10.05	10.05	-8.34	-116.2
51	0	-12750	878	1058	0	1039	-674	6.03	6.03	10.05	10.05	-8.68	-120.9

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	12	-15185	79	1565	0	1281	-713	6.03	6.03	10.05	10.05	-10.50	-145.9
41	12	-13425	750	1136	0	1066	-541	6.03	6.03	10.05	10.05	-9.04	-126.0
42	12	-13245	753	1254	0	977	-541	6.03	6.03	10.05	10.05	-8.65	-121.0
43	12	-16015	-304	1792	0	1360	-839	6.03	6.03	10.05	10.05	-11.10	-154.3
44	12	-10535	1859	457	0	724	-253	6.03	6.03	10.05	10.05	-6.69	-93.8
45	12	-12775	819	1274	0	854	-552	6.03	6.03	10.05	10.05	-8.02	-112.7
46	12	-12875	851	1042	0	963	-559	6.03	6.03	10.05	10.05	-8.46	-118.2
47	12	-12735	877	1019	0	937	-564	6.03	6.03	10.05	10.05	-8.31	-116.2
49	12	-13325	653	1162	0	1009	-621	6.03	6.03	10.05	10.05	-8.80	-122.8
50	12	-12225	1086	895	0	881	-504	6.03	6.03	10.05	10.05	-7.91	-110.7
51	12	-12675	878	1058	0	907	-564	6.03	6.03	10.05	10.05	-8.18	-114.5

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	25	-15110	79	1565	0	1086	-703	6.03	6.03	10.05	10.05	-9.76	-136.7
41	25	-13350	750	1136	0	924	-447	6.03	6.03	10.05	10.05	-8.50	-119.2
42	25	-13170	753	1254	0	820	-446	6.03	6.03	10.05	10.05	-8.06	-113.5
43	25	-15940	-304	1792	0	1136	-877	6.03	6.03	10.05	10.05	-10.42	-143.8
44	25	-10460	1859	457	0	667	-21	6.03	6.03	10.05	10.05	-6.45	-90.8
45	25	-12700	819	1274	0	694	-450	6.03	6.03	10.05	10.05	-7.42	-105.1
46	25	-12800	851	1042	0	832	-453	6.03	6.03	10.05	10.05	-7.96	-111.9
47	25	-12660	877	1019	0	809	-454	6.03	6.03	10.05	10.05	-7.82	-110.0
49	25	-13250	653	1162	0	863	-540	6.03	6.03	10.05	10.05	-8.24	-115.9
50	25	-12150	1086	895	0	769	-369	6.03	6.03	10.05	10.05	-7.48	-105.2
51	25	-12600	878	1058	0	775	-454	6.03	6.03	10.05	10.05	-7.67	-108.1

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	38	-15035	79	1565	0	890	-693	6.03	6.03	10.05	10.05	-9.14	-127.4
41	38	-13275	750	1136	0	782	-353	6.03	6.03	10.05	10.05	-7.96	-112.3
42	38	-13095	753	1254	0	664	-352	6.03	6.03	10.05	10.05	-7.46	-106.0

43	38	-15865	-304	1792	0	912	-915	6.03	6.03	10.05	10.05	-10.59	-141.2
44	38	-10385	1859	457	0	610	211	6.03	6.03	10.05	10.05	-6.22	-87.8
45	38	-12625	819	1274	0	535	-348	6.03	6.03	10.05	10.05	-6.82	-97.5
46	38	-12725	851	1042	0	702	-347	6.03	6.03	10.05	10.05	-7.46	-105.6
47	38	-12585	877	1019	0	682	-345	6.03	6.03	10.05	10.05	-7.33	-103.8
49	38	-13175	653	1162	0	718	-458	6.03	6.03	10.05	10.05	-7.69	-108.9
50	38	-12075	1086	895	0	658	-233	6.03	6.03	10.05	10.05	-7.05	-99.8
51	38	-12525	878	1058	0	643	-345	6.03	6.03	10.05	10.05	-7.17	-101.7

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	50	-14960	79	1565	0	694	-683	6.03	6.03	10.05	10.05	-9.06	-122.7
41	50	-13200	750	1136	0	640	-260	6.03	6.03	10.05	10.05	-7.42	-105.5
42	50	-13020	753	1254	0	507	-258	6.03	6.03	10.05	10.05	-6.87	-98.5
43	50	-15790	-304	1792	0	688	-953	6.03	6.03	10.05	10.05	-10.76	-143.0
44	50	-10310	1859	457	0	552	444	6.03	6.03	10.05	10.05	-6.10	-84.8
45	50	-12550	819	1274	0	376	-245	6.03	6.03	10.05	10.05	-6.21	-89.8
46	50	-12650	851	1042	0	572	-240	6.03	6.03	10.05	10.05	-6.96	-99.3
47	50	-12510	877	1019	0	555	-235	6.03	6.03	10.05	10.05	-6.84	-97.7
49	50	-13100	653	1162	0	573	-376	6.03	6.03	10.05	10.05	-7.14	-101.9
50	50	-12000	1086	895	0	546	-97	6.03	6.03	10.05	10.05	-6.61	-94.3
51	50	-12450	878	1058	0	510	-235	6.03	6.03	10.05	10.05	-6.66	-95.3

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

ASTA NUM. 107 NI 1045 NF 299 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 10A
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-16190	-1578	674	0	562	-706	6.03	6.03	10.05	10.05	-9.63	-130.8
41	0	-14910	304	505	0	530	-216	6.03	6.03	10.05	10.05	-7.68	-110.5
42	0	-14800	298	739	0	383	-216	6.03	6.03	10.05	10.05	-7.11	-103.3
43	0	-16630	-2815	796	0	546	-1015	6.03	6.03	10.05	10.05	-11.39	-151.2
44	0	-12830	3434	236	0	477	596	6.03	6.03	10.05	10.05	-7.82	-105.8
45	0	-14320	313	904	0	249	-199	6.03	6.03	10.05	10.05	-6.45	-94.4
46	0	-14260	333	519	0	472	-189	6.03	6.03	10.05	10.05	-7.22	-104.1
47	0	-14100	341	523	0	457	-182	6.03	6.03	10.05	10.05	-7.11	-102.5
49	0	-14530	-287	579	0	468	-345	6.03	6.03	10.05	10.05	-7.31	-105.5
50	0	-13770	963	467	0	454	-23	6.03	6.03	10.05	10.05	-6.97	-100.5
51	0	-14060	339	601	0	408	-182	6.03	6.03	10.05	10.05	-6.92	-100.1

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	12	-16115	-1578	674	0	477	-903	6.03	6.03	10.05	10.05	-10.62	-141.9
41	12	-14835	304	505	0	467	-178	6.03	6.03	10.05	10.05	-7.43	-107.2
42	12	-14725	298	739	0	291	-179	6.03	6.03	10.05	10.05	-6.75	-98.7
43	12	-16555	-2815	796	0	447	-1367	6.03	6.03	10.05	10.05	-13.23	-171.7
44	12	-12755	3434	236	0	448	1025	6.03	6.03	10.05	10.05	-10.03	-130.5
45	12	-14245	313	904	0	136	-159	6.03	6.03	10.05	10.05	-6.10	-88.9
46	12	-14185	333	519	0	407	-147	6.03	6.03	10.05	10.05	-6.96	-100.7
47	12	-14025	341	523	0	392	-139	6.03	6.03	10.05	10.05	-6.84	-99.1
49	12	-14455	-287	579	0	395	-381	6.03	6.03	10.05	10.05	-7.31	-102.3
50	12	-13695	963	467	0	395	98	6.03	6.03	10.05	10.05	-6.73	-97.4
51	12	-13985	339	601	0	333	-139	6.03	6.03	10.05	10.05	-6.62	-96.3

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	25	-16040	-1578	674	0	393	-1100	6.03	6.03	10.05	10.05	-11.61	-152.9
41	25	-14760	304	505	0	404	-140	6.03	6.03	10.05	10.05	-7.17	-103.9
42	25	-14650	298	739	0	199	-142	6.03	6.03	10.05	10.05	-6.39	-94.1
43	25	-16480	-2815	796	0	347	-1718	6.03	6.03	10.05	10.05	-15.48	-195.6
44	25	-12680	3434	236	0	418	1454	6.03	6.03	10.05	10.05	-12.88	-160.5
45	25	-14170	313	904	0	23	-120	6.03	6.03	10.05	10.05	-5.87	-85.7
46	25	-14110	333	519	0	342	-105	6.03	6.03	10.05	10.05	-6.70	-97.4
47	25	-13950	341	523	0	326	-96	6.03	6.03	10.05	10.05	-6.58	-95.8
49	25	-14380	-287	579	0	323	-416	6.03	6.03	10.05	10.05	-7.47	-104.0
50	25	-13620	963	467	0	337	218	6.03	6.03	10.05	10.05	-6.49	-94.3
51	25	-13910	339	601	0	258	-97	6.03	6.03	10.05	10.05	-6.32	-92.5

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	38	-15965	-1578	674	0	309	-1298	6.03	6.03	10.05	10.05	-12.64	-164.3
41	38	-14685	304	505	0	340	-102	6.03	6.03	10.05	10.05	-6.92	-100.7
42	38	-14575	298	739	0	106	-104	6.03	6.03	10.05	10.05	-6.03	-89.5
43	38	-16405	-2815	796	0	248	-2070	6.03	6.03	10.05	10.05	-18.15	-222.6
44	38	-12605	3434	236	0	389	1884	6.03	6.03	10.05	10.05	-16.43	-194.9
45	38	-14095	313	904	0	-90	-81	6.03	6.03	10.05	10.05	-5.78	-86.0
46	38	-14035	333	519	0	277	-64	6.03	6.03	10.05	10.05	-6.43	-94.0
47	38	-13875	341	523	0	261	-54	6.03	6.03	10.05	10.05	-6.32	-92.4
49	38	-14305	-287	579	0	250	-452	6.03	6.03	10.05	10.05	-7.63	-105.7
50	38	-13545	963	467	0	279	338	6.03	6.03	10.05	10.05	-6.76	-94.8
51	38	-13835	339	601	0	183	-54	6.03	6.03	10.05	10.05	-6.02	-88.6

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	50	-15890	-1578	674	0	224	-1495	6.03	6.03	10.05	10.05	-13.82	-177.0
41	50	-14610	304	505	0	277	-64	6.03	6.03	10.05	10.05	-6.66	-97.4
42	50	-14500	298	739	0	14	-67	6.03	6.03	10.05	10.05	-5.71	-84.9
43	50	-16330	-2815	796	0	148	-2422	6.03	6.03	10.05	10.05	-21.12	-251.0
44	50	-12530	3434	236	0	360	2313	6.03	6.03	10.05	10.05	-20.28	-229.6
45	50	-14020	313	904	0	-203	-42	6.03	6.03	10.05	10.05	-6.16	-90.6
46	50	-13960	333	519	0	212	-22	6.03	6.03	10.05	10.05	-6.17	-90.7
47	50	-13800	341	523	0	196	-11	6.03	6.03	10.05	10.05	-6.05	-89.0
49	50	-14230	-287	579	0	178	-488	6.03	6.03	10.05	10.05	-7.78	-107.3
50	50	-13470	963	467	0	220	459	6.03	6.03	10.05	10.05	-7.35	-101.4
51	50	-13760	339	601	0	108	-12	6.03	6.03	10.05	10.05	-5.72	-84.8

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

ASTA NUM. 108 NI 1254 NF 1349 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 9
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-4183	-114	176	0	-60	-168	6.03	6.03	10.05	10.05	-2.42	-33.0
41	0	-4166	1	67	0	-40	9	6.03	6.03	10.05	10.05	-1.76	-26.0
42	0	-4150	1	177	0	-56	10	6.03	6.03	10.05	10.05	-1.81	-26.6
43	0	-4075	-196	218	0	-69	-295	6.03	6.03	10.05	10.05	-3.03	-39.7
44	0	-4043	192	-101	0	-8	305	6.03	6.03	10.05	10.05	-3.07	-40.1
45	0	-4020	-3	219	0	-61	2	6.03	6.03	10.05	10.05	-1.78	-26.1
46	0	-3975	-8	15	0	-31	-6	6.03	6.03	10.05	10.05	-1.65	-24.5
47	0	-3927	-10	3	0	-29	-10	6.03	6.03	10.05	10.05	-1.63	-24.1
49	0	-3933	-48	39	0	-36	-69	6.03	6.03	10.05	10.05	-1.81	-25.8
50	0	-3926	29	-25	0	-24	51	6.03	6.03	10.05	10.05	-1.72	-24.8
51	0	-3922	-10	39	0	-34	-9	6.03	6.03	10.05	10.05	-1.64	-24.3

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	12	-4108	-114	176	0	-83	-182	6.03	6.03	10.05	10.05	-2.46	-33.4
41	12	-4091	1	67	0	-48	9	6.03	6.03	10.05	10.05	-1.76	-25.9
42	12	-4075	1	177	0	-78	10	6.03	6.03	10.05	10.05	-1.86	-27.2
43	12	-4000	-196	218	0	-96	-320	6.03	6.03	10.05	10.05	-3.14	-40.8
44	12	-3968	192	-101	0	5	329	6.03	6.03	10.05	10.05	-3.18	-41.2
45	12	-3945	-3	219	0	-89	2	6.03	6.03	10.05	10.05	-1.85	-26.9
46	12	-3900	-8	15	0	-33	-7	6.03	6.03	10.05	10.05	-1.63	-24.1
47	12	-3852	-10	3	0	-29	-11	6.03	6.03	10.05	10.05	-1.60	-23.7
49	12	-3858	-48	39	0	-41	-75	6.03	6.03	10.05	10.05	-1.81	-25.7
50	12	-3851	29	-25	0	-20	55	6.03	6.03	10.05	10.05	-1.71	-24.6
51	12	-3847	-10	39	0	-39	-10	6.03	6.03	10.05	10.05	-1.63	-24.1

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	25	-4033	-114	176	0	-105	-197	6.03	6.03	10.05	10.05	-2.51	-33.8
41	25	-4016	1	67	0	-57	9	6.03	6.03	10.05	10.05	-1.76	-25.9
42	25	-4000	1	177	0	-100	11	6.03	6.03	10.05	10.05	-1.91	-27.8
43	25	-3925	-196	218	0	-123	-344	6.03	6.03	10.05	10.05	-3.26	-42.0
44	25	-3893	192	-101	0	17	353	6.03	6.03	10.05	10.05	-3.30	-42.4
45	25	-3870	-3	219	0	-116	1	6.03	6.03	10.05	10.05	-1.92	-27.7
46	25	-3825	-8	15	0	-35	-8	6.03	6.03	10.05	10.05	-1.61	-23.8
47	25	-3777	-10	3	0	-29	-12	6.03	6.03	10.05	10.05	-1.57	-23.3
49	25	-3783	-48	39	0	-45	-81	6.03	6.03	10.05	10.05	-1.82	-25.7
50	25	-3776	29	-25	0	-17	59	6.03	6.03	10.05	10.05	-1.70	-24.4
51	25	-3772	-10	39	0	-44	-12	6.03	6.03	10.05	10.05	-1.62	-23.9

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	38	-3958	-114	176	0	-127	-211	6.03	6.03	10.05	10.05	-2.55	-34.2
41	38	-3941	1	67	0	-65	9	6.03	6.03	10.05	10.05	-1.76	-25.8
42	38	-3925	1	177	0	-123	11	6.03	6.03	10.05	10.05	-1.96	-28.3
43	38	-3850	-196	218	0	-150	-368	6.03	6.03	10.05	10.05	-3.39	-43.3
44	38	-3818	192	-101	0	30	377	6.03	6.03	10.05	10.05	-3.44	-43.8
45	38	-3795	-3	219	0	-143	1	6.03	6.03	10.05	10.05	-1.99	-28.5
46	38	-3750	-8	15	0	-37	-9	6.03	6.03	10.05	10.05	-1.59	-23.5
47	38	-3702	-10	3	0	-30	-13	6.03	6.03	10.05	10.05	-1.54	-22.9
49	38	-3708	-48	39	0	-50	-87	6.03	6.03	10.05	10.05	-1.82	-25.6
50	38	-3701	29	-25	0	-14	62	6.03	6.03	10.05	10.05	-1.69	-24.2
51	38	-3697	-10	39	0	-49	-13	6.03	6.03	10.05	10.05	-1.61	-23.7

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	50	-3883	-114	176	0	-149	-225	6.03	6.03	10.05	10.05	-2.60	-34.6
41	50	-3866	1	67	0	-73	9	6.03	6.03	10.05	10.05	-1.76	-25.8
42	50	-3850	1	177	0	-145	11	6.03	6.03	10.05	10.05	-2.01	-28.9
43	50	-3775	-196	218	0	-177	-393	6.03	6.03	10.05	10.05	-3.54	-44.7
44	50	-3743	192	-101	0	42	401	6.03	6.03	10.05	10.05	-3.59	-45.2
45	50	-3720	-3	219	0	-171	1	6.03	6.03	10.05	10.05	-2.06	-29.3
46	50	-3675	-8	15	0	-39	-10	6.03	6.03	10.05	10.05	-1.56	-23.1
47	50	-3627	-10	3	0	-30	-15	6.03	6.03	10.05	10.05	-1.51	-22.4
49	50	-3633	-48	39	0	-55	-93	6.03	6.03	10.05	10.05	-1.82	-25.5
50	50	-3626	29	-25	0	-11	66	6.03	6.03	10.05	10.05	-1.68	-24.0
51	50	-3622	-10	39	0	-54	-14	6.03	6.03	10.05	10.05	-1.60	-23.5

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

ASTA NUM. 109 NI 1349 NF 129 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 9A
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-5952	-297	577	0	-149	-214	6.03	6.03	10.05	10.05	-3.31	-45.5
41	0	-5928	5	304	0	-73	7	6.03	6.03	10.05	10.05	-2.56	-37.8
42	0	-5900	8	563	0	-145	9	6.03	6.03	10.05	10.05	-2.81	-40.8
43	0	-5783	-512	683	0	-177	-372	6.03	6.03	10.05	10.05	-4.06	-53.7
44	0	-5737	511	-116	0	42	377	6.03	6.03	10.05	10.05	-4.07	-53.7
45	0	-5695	-5	659	0	-171	-1	6.03	6.03	10.05	10.05	-2.82	-40.8
46	0	-5631	-18	182	0	-39	-11	6.03	6.03	10.05	10.05	-2.32	-34.5
47	0	-5557	-24	152	0	-30	-15	6.03	6.03	10.05	10.05	-2.26	-33.6
49	0	-5565	-124	242	0	-55	-89	6.03	6.03	10.05	10.05	-2.52	-36.0
50	0	-5556	80	83	0	-11	61	6.03	6.03	10.05	10.05	-2.37	-34.4
51	0	-5547	-23	238	0	-54	-15	6.03	6.03	10.05	10.05	-2.34	-34.7

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	12	-5877	-297	577	0	-221	-251	6.03	6.03	10.05	10.05	-3.47	-47.2
41	12	-5853	5	304	0	-111	8	6.03	6.03	10.05	10.05	-2.67	-39.0
42	12	-5825	8	563	0	-215	10	6.03	6.03	10.05	10.05	-3.03	-43.5
43	12	-5708	-512	683	0	-263	-436	6.03	6.03	10.05	10.05	-4.37	-57.0
44	12	-5662	511	-116	0	57	441	6.03	6.03	10.05	10.05	-4.37	-57.1
45	12	-5620	-5	659	0	-253	-2	6.03	6.03	10.05	10.05	-3.09	-44.1
46	12	-5556	-18	182	0	-61	-13	6.03	6.03	10.05	10.05	-2.37	-35.1
47	12	-5482	-24	152	0	-49	-18	6.03	6.03	10.05	10.05	-2.30	-34.1

49	12	-5490	-124	242	0	-85	-104	6.03	6.03	10.05	10.05	-2.57	-36.5
50	12	-5481	80	83	0	-22	71	6.03	6.03	10.05	10.05	-2.40	-34.6
51	12	-5472	-23	238	0	-84	-17	6.03	6.03	10.05	10.05	-2.42	-35.6

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	25	-5802	-297	577	0	-293	-288	6.03	6.03	10.05	10.05	-3.63	-48.9
41	25	-5778	5	304	0	-149	8	6.03	6.03	10.05	10.05	-2.78	-40.3
42	25	-5750	8	563	0	-286	11	6.03	6.03	10.05	10.05	-3.26	-46.3
43	25	-5633	-512	683	0	-348	-500	6.03	6.03	10.05	10.05	-4.71	-60.7
44	25	-5587	511	-116	0	72	505	6.03	6.03	10.05	10.05	-4.73	-60.8
45	25	-5545	-5	659	0	-336	-2	6.03	6.03	10.05	10.05	-3.36	-47.3
46	25	-5481	-18	182	0	-84	-15	6.03	6.03	10.05	10.05	-2.43	-35.6
47	25	-5407	-24	152	0	-68	-21	6.03	6.03	10.05	10.05	-2.34	-34.5
49	25	-5415	-124	242	0	-116	-120	6.03	6.03	10.05	10.05	-2.62	-37.0
50	25	-5406	80	83	0	-32	81	6.03	6.03	10.05	10.05	-2.42	-34.7
51	25	-5397	-23	238	0	-113	-20	6.03	6.03	10.05	10.05	-2.50	-36.5

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	38	-5727	-297	577	0	-365	-325	6.03	6.03	10.05	10.05	-3.80	-50.7
41	38	-5703	5	304	0	-188	9	6.03	6.03	10.05	10.05	-2.88	-41.6
42	38	-5675	8	563	0	-356	12	6.03	6.03	10.05	10.05	-3.48	-49.0
43	38	-5558	-512	683	0	-433	-564	6.03	6.03	10.05	10.05	-5.11	-64.8
44	38	-5512	511	-116	0	86	568	6.03	6.03	10.05	10.05	-5.13	-65.0
45	38	-5470	-5	659	0	-418	-3	6.03	6.03	10.05	10.05	-3.62	-50.6
46	38	-5406	-18	182	0	-107	-17	6.03	6.03	10.05	10.05	-2.48	-36.2
47	38	-5332	-24	152	0	-87	-24	6.03	6.03	10.05	10.05	-2.38	-34.9
49	38	-5340	-124	242	0	-146	-135	6.03	6.03	10.05	10.05	-2.67	-37.6
50	38	-5331	80	83	0	-42	91	6.03	6.03	10.05	10.05	-2.44	-34.9
51	38	-5322	-23	238	0	-143	-23	6.03	6.03	10.05	10.05	-2.58	-37.4

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	50	-5652	-297	577	0	-437	-362	6.03	6.03	10.05	10.05	-3.96	-52.5
41	50	-5628	5	304	0	-226	9	6.03	6.03	10.05	10.05	-2.99	-42.9
42	50	-5600	8	563	0	-426	13	6.03	6.03	10.05	10.05	-3.70	-51.7
43	50	-5483	-512	683	0	-519	-628	6.03	6.03	10.05	10.05	-5.56	-69.4
44	50	-5437	511	-116	0	101	632	6.03	6.03	10.05	10.05	-5.59	-69.5
45	50	-5395	-5	659	0	-500	-3	6.03	6.03	10.05	10.05	-3.89	-53.9
46	50	-5331	-18	182	0	-130	-20	6.03	6.03	10.05	10.05	-2.53	-36.8
47	50	-5257	-24	152	0	-106	-27	6.03	6.03	10.05	10.05	-2.42	-35.3
49	50	-5265	-124	242	0	-176	-151	6.03	6.03	10.05	10.05	-2.73	-38.5
50	50	-5256	80	83	0	-53	101	6.03	6.03	10.05	10.05	-2.47	-35.1
51	50	-5247	-23	238	0	-173	-26	6.03	6.03	10.05	10.05	-2.65	-38.3

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

ASTA NUM. 110 NI 1158 NF 1253 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 8
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	--												
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-2926	67	426	0	-148	5	4.02	4.02	10.05	10.05	-2.24	-31.9
41	0	-2931	125	337	0	-141	-12	4.02	4.02	10.05	10.05	-2.22	-31.5
42	0	-3009	123	409	0	-155	-11	4.02	4.02	10.05	10.05	-2.32	-33.0
43	0	-2845	23	462	0	-142	17	4.02	4.02	10.05	10.05	-2.18	-30.9
44	0	-2890	220	187	0	-127	-39	4.02	4.02	10.05	10.05	-2.12	-30.3
45	0	-2984	116	433	0	-155	-9	4.02	4.02	10.05	10.05	-2.31	-32.7
46	0	-2808	116	300	0	-126	-10	4.02	4.02	10.05	10.05	-2.08	-29.6
47	0	-2777	114	290	0	-122	-9	4.02	4.02	10.05	10.05	-2.04	-29.1
49	0	-2775	95	320	0	-124	-4	4.02	4.02	10.05	10.05	-2.05	-29.2
50	0	-2784	134	265	0	-121	-15	4.02	4.02	10.05	10.05	-2.04	-29.1
51	0	-2803	113	314	0	-127	-9	4.02	4.02	10.05	10.05	-2.08	-29.6

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	12	-2870	67	426	0	-201	13	4.02	4.02	10.05	10.05	-2.47	-34.7
41	12	-2875	125	337	0	-184	4	4.02	4.02	10.05	10.05	-2.39	-33.6
42	12	-2953	123	409	0	-206	5	4.02	4.02	10.05	10.05	-2.54	-35.6
43	12	-2789	23	462	0	-200	20	4.02	4.02	10.05	10.05	-2.43	-34.0
44	12	-2834	220	187	0	-150	-11	4.02	4.02	10.05	10.05	-2.21	-31.3
45	12	-2928	116	433	0	-209	6	4.02	4.02	10.05	10.05	-2.54	-35.6
46	12	-2752	116	300	0	-163	5	4.02	4.02	10.05	10.05	-2.23	-31.5
47	12	-2721	114	290	0	-158	5	4.02	4.02	10.05	10.05	-2.19	-30.9
49	12	-2719	95	320	0	-164	8	4.02	4.02	10.05	10.05	-2.22	-31.2
50	12	-2728	134	265	0	-154	2	4.02	4.02	10.05	10.05	-2.17	-30.7
51	12	-2747	113	314	0	-166	5	4.02	4.02	10.05	10.05	-2.24	-31.6

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	25	-2814	67	426	0	-254	22	4.02	4.02	10.05	10.05	-2.71	-37.5
41	25	-2818	125	337	0	-226	20	4.02	4.02	10.05	10.05	-2.57	-35.8
42	25	-2896	123	409	0	-257	20	4.02	4.02	10.05	10.05	-2.76	-38.3
43	25	-2732	23	462	0	-258	23	4.02	4.02	10.05	10.05	-2.68	-37.1
44	25	-2778	220	187	0	-173	16	4.02	4.02	10.05	10.05	-2.29	-32.3
45	25	-2872	116	433	0	-263	20	4.02	4.02	10.05	10.05	-2.78	-38.5
46	25	-2696	116	300	0	-201	19	4.02	4.02	10.05	10.05	-2.38	-33.3
47	25	-2664	114	290	0	-195	19	4.02	4.02	10.05	10.05	-2.34	-32.7
49	25	-2662	95	320	0	-204	20	4.02	4.02	10.05	10.05	-2.38	-33.2
50	25	-2672	134	265	0	-187	19	4.02	4.02	10.05	10.05	-2.30	-32.3
51	25	-2690	113	314	0	-205	19	4.02	4.02	10.05	10.05	-2.40	-33.5

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	38	-2757	67	426	0	-308	30	4.02	4.02	10.05	10.05	-2.94	-40.3
41	38	-2762	125	337	0	-268	35	4.02	4.02	10.05	10.05	-2.74	-37.9
42	38	-2840	123	409	0	-308	36	4.02	4.02	10.05	10.05	-2.98	-41.0
43	38	-2676	23	462	0	-316	25	4.02	4.02	10.05	10.05	-2.94	-40.2
44	38	-2721	220	187	0	-197	44	4.02	4.02	10.05	10.05	-2.38	-33.2
45	38	-2815	116	433	0	-317	35	4.02	4.02	10.05	10.05	-3.01	-41.3
46	38	-2639	116	300	0	-238	34	4.02	4.02	10.05	10.05	-2.54	-35.1
47	38	-2608	114	290	0	-231	34	4.02	4.02	10.05	10.05	-2.48	-34.5
49	38	-2606	95	320	0	-244	32	4.02	4.02	10.05	10.05	-2.55	-35.2

50	38	-2615	134	265	0	-220	35	4.02	4.02	10.05	10.05	-2.44	-33.9
51	38	-2634	113	314	0	-245	34	4.02	4.02	10.05	10.05	-2.56	-35.5

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	50	-2701	67	426	0	-361	38	4.02	4.02	10.05	10.05	-3.21	-43.5
41	50	-2706	125	337	0	-310	51	4.02	4.02	10.05	10.05	-2.92	-40.1
42	50	-2784	123	409	0	-360	51	4.02	4.02	10.05	10.05	-3.23	-44.0
43	50	-2620	23	462	0	-373	28	4.02	4.02	10.05	10.05	-3.25	-44.0
44	50	-2665	220	187	0	-220	71	4.02	4.02	10.05	10.05	-2.46	-34.2
45	50	-2759	116	433	0	-371	49	4.02	4.02	10.05	10.05	-3.29	-44.7
46	50	-2583	116	300	0	-276	48	4.02	4.02	10.05	10.05	-2.69	-37.0
47	50	-2552	114	290	0	-267	48	4.02	4.02	10.05	10.05	-2.63	-36.2
49	50	-2550	95	320	0	-284	44	4.02	4.02	10.05	10.05	-2.71	-37.3
50	50	-2559	134	265	0	-254	52	4.02	4.02	10.05	10.05	-2.57	-35.4
51	50	-2578	113	314	0	-284	48	4.02	4.02	10.05	10.05	-2.73	-37.4

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

ASTA NUM. 111 NI 1253 NF 213 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 8A
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	--												
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-3689	-161	514	0	-395	28	4.02	4.02	10.05	10.05	-3.85	-52.9
41	0	-3714	-23	383	0	-338	47	4.02	4.02	10.05	10.05	-3.58	-49.6
42	0	-3786	-29	504	0	-398	47	4.02	4.02	10.05	10.05	-3.91	-53.8
43	0	-3578	-254	558	0	-409	13	4.02	4.02	10.05	10.05	-3.86	-52.9
44	0	-3687	209	162	0	-237	78	4.02	4.02	10.05	10.05	-3.08	-43.2
45	0	-3740	-35	542	0	-413	45	4.02	4.02	10.05	10.05	-3.96	-54.4
46	0	-3564	-26	314	0	-299	44	4.02	4.02	10.05	10.05	-3.31	-46.0
47	0	-3527	-27	297	0	-289	43	4.02	4.02	10.05	10.05	-3.25	-45.2
49	0	-3518	-73	341	0	-308	37	4.02	4.02	10.05	10.05	-3.33	-46.3
50	0	-3540	20	261	0	-274	50	4.02	4.02	10.05	10.05	-3.18	-44.3
51	0	-3551	-29	338	0	-309	43	4.02	4.02	10.05	10.05	-3.36	-46.6

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	12	-3633	-161	514	0	-460	8	4.02	4.02	10.05	10.05	-4.16	-56.7
41	12	-3658	-23	383	0	-386	44	4.02	4.02	10.05	10.05	-3.79	-52.1
42	12	-3730	-29	504	0	-461	43	4.02	4.02	10.05	10.05	-4.21	-57.5
43	12	-3522	-254	558	0	-479	-19	4.02	4.02	10.05	10.05	-4.23	-57.4
44	12	-3631	209	162	0	-257	104	4.02	4.02	10.05	10.05	-3.14	-44.0
45	12	-3684	-35	542	0	-481	41	4.02	4.02	10.05	10.05	-4.31	-58.6
46	12	-3508	-26	314	0	-338	40	4.02	4.02	10.05	10.05	-3.47	-48.0
47	12	-3471	-27	297	0	-326	40	4.02	4.02	10.05	10.05	-3.40	-47.0
49	12	-3462	-73	341	0	-351	27	4.02	4.02	10.05	10.05	-3.51	-48.4
50	12	-3484	20	261	0	-306	52	4.02	4.02	10.05	10.05	-3.31	-45.9
51	12	-3495	-29	338	0	-351	39	4.02	4.02	10.05	10.05	-3.53	-48.7

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	25	-3576	-161	514	0	-524	-12	4.02	4.02	10.05	10.05	-4.53	-61.1
41	25	-3602	-23	383	0	-434	41	4.02	4.02	10.05	10.05	-4.00	-54.7
42	25	-3674	-29	504	0	-524	40	4.02	4.02	10.05	10.05	-4.57	-61.7
43	25	-3466	-254	558	0	-549	-50	4.02	4.02	10.05	10.05	-4.68	-62.6
44	25	-3574	209	162	0	-278	130	4.02	4.02	10.05	10.05	-3.21	-44.8
45	25	-3628	-35	542	0	-549	37	4.02	4.02	10.05	10.05	-4.72	-63.4
46	25	-3452	-26	314	0	-377	37	4.02	4.02	10.05	10.05	-3.64	-50.0
47	25	-3414	-27	297	0	-363	36	4.02	4.02	10.05	10.05	-3.55	-48.8
49	25	-3406	-73	341	0	-393	18	4.02	4.02	10.05	10.05	-3.70	-50.6
50	25	-3428	20	261	0	-339	54	4.02	4.02	10.05	10.05	-3.44	-47.4
51	25	-3438	-29	338	0	-393	36	4.02	4.02	10.05	10.05	-3.71	-50.9

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	38	-3520	-161	514	0	-588	-32	4.02	4.02	10.05	10.05	-4.98	-66.3
41	38	-3545	-23	383	0	-482	38	4.02	4.02	10.05	10.05	-4.25	-57.7
42	38	-3617	-29	504	0	-587	36	4.02	4.02	10.05	10.05	-4.99	-66.6
43	38	-3409	-254	558	0	-619	-82	4.02	4.02	10.05	10.05	-5.21	-68.7
44	38	-3518	209	162	0	-298	156	4.02	4.02	10.05	10.05	-3.28	-45.6
45	38	-3571	-35	542	0	-617	32	4.02	4.02	10.05	10.05	-5.20	-69.0
46	38	-3395	-26	314	0	-417	34	4.02	4.02	10.05	10.05	-3.82	-52.1
47	38	-3358	-27	297	0	-400	33	4.02	4.02	10.05	10.05	-3.71	-50.7
49	38	-3349	-73	341	0	-436	9	4.02	4.02	10.05	10.05	-3.91	-53.1
50	38	-3371	20	261	0	-372	57	4.02	4.02	10.05	10.05	-3.57	-49.0
51	38	-3382	-29	338	0	-436	32	4.02	4.02	10.05	10.05	-3.92	-53.3

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	50	-3464	-161	514	0	-652	-53	4.02	4.02	10.05	10.05	-5.49	-72.1
41	50	-3489	-23	383	0	-529	35	4.02	4.02	10.05	10.05	-4.55	-61.1
42	50	-3561	-29	504	0	-650	33	4.02	4.02	10.05	10.05	-5.47	-72.1
43	50	-3353	-254	558	0	-688	-114	4.02	4.02	10.05	10.05	-5.81	-75.4
44	50	-3462	209	162	0	-318	182	4.02	4.02	10.05	10.05	-3.35	-46.4
45	50	-3515	-35	542	0	-685	28	4.02	4.02	10.05	10.05	-5.76	-75.3
46	50	-3339	-26	314	0	-456	30	4.02	4.02	10.05	10.05	-4.02	-54.5
47	50	-3302	-27	297	0	-438	29	4.02	4.02	10.05	10.05	-3.90	-52.9
49	50	-3293	-73	341	0	-478	0	4.02	4.02	10.05	10.05	-4.15	-56.0
50	50	-3315	20	261	0	-404	59	4.02	4.02	10.05	10.05	-3.71	-50.7
51	50	-3326	-29	338	0	-478	29	4.02	4.02	10.05	10.05	-4.16	-56.1

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

ASTA NUM. 112 NI 175 NF 89 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 17
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	--												
	cm		daN			daN*m				cm^2			daN/cm^2

40	0	-6704	-76	-181	0	592	-1	6.03	6.03	10.05	10.05	-4.73	-65.6
41	0	-6463	14	-150	0	502	-7	6.03	6.03	10.05	10.05	-4.31	-60.2
42	0	-6504	18	-401	0	2239	-7	6.03	6.03	10.05	10.05	-14.63	276.7
43	0	-6587	-132	-165	0	533	4	6.03	6.03	10.05	10.05	-4.47	-62.3
44	0	-6139	164	-106	0	376	-18	6.03	6.03	10.05	10.05	-3.73	-52.6
45	0	-6252	24	-531	0	3278	-8	6.03	6.03	10.05	10.05	-21.92	608.7
46	0	-6016	21	-92	0	312	-7	6.03	6.03	10.05	10.05	-3.45	-49.0
47	0	-5905	22	-77	0	264	-7	6.03	6.03	10.05	10.05	-3.24	-46.2
49	0	-5985	-8	-88	0	294	-5	6.03	6.03	10.05	10.05	-3.38	-48.0
50	0	-5896	51	-76	0	263	-9	6.03	6.03	10.05	10.05	-3.23	-46.1
51	0	-5918	23	-161	0	843	-7	6.03	6.03	10.05	10.05	-5.44	-73.5

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	12	-6629	-76	-181	0	615	-10	6.03	6.03	10.05	10.05	-4.78	-66.2
41	12	-6388	14	-150	0	521	-5	6.03	6.03	10.05	10.05	-4.35	-60.6
42	12	-6429	18	-401	0	2289	-5	6.03	6.03	10.05	10.05	-15.01	295.4
43	12	-6512	-132	-165	0	554	-13	6.03	6.03	10.05	10.05	-4.52	-62.8
44	12	-6064	164	-106	0	389	3	6.03	6.03	10.05	10.05	-3.75	-52.8
45	12	-6177	24	-531	0	3344	-5	6.03	6.03	10.05	10.05	-22.37	634.7
46	12	-5941	21	-92	0	323	-4	6.03	6.03	10.05	10.05	-3.47	-49.1
47	12	-5830	22	-77	0	274	-4	6.03	6.03	10.05	10.05	-3.24	-46.2
49	12	-5910	-8	-88	0	305	-6	6.03	6.03	10.05	10.05	-3.39	-48.1
50	12	-5821	51	-76	0	272	-3	6.03	6.03	10.05	10.05	-3.24	-46.1
51	12	-5843	23	-161	0	863	-4	6.03	6.03	10.05	10.05	-5.51	-74.3

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	25	-6554	-76	-181	0	638	-19	6.03	6.03	10.05	10.05	-4.84	-66.8
41	25	-6313	14	-150	0	540	-3	6.03	6.03	10.05	10.05	-4.39	-61.0
42	25	-6354	18	-401	0	2339	-3	6.03	6.03	10.05	10.05	-15.38	314.3
43	25	-6437	-132	-165	0	574	-29	6.03	6.03	10.05	10.05	-4.56	-63.3
44	25	-5989	164	-106	0	403	23	6.03	6.03	10.05	10.05	-3.77	-52.9
45	25	-6102	24	-531	0	3410	-2	6.03	6.03	10.05	10.05	-22.83	660.8
46	25	-5866	21	-92	0	335	-2	6.03	6.03	10.05	10.05	-3.48	-49.2
47	25	-5755	22	-77	0	283	-1	6.03	6.03	10.05	10.05	-3.25	-46.2
49	25	-5835	-8	-88	0	316	-7	6.03	6.03	10.05	10.05	-3.40	-48.1
50	25	-5746	51	-76	0	282	4	6.03	6.03	10.05	10.05	-3.24	-46.1
51	25	-5768	23	-161	0	883	-1	6.03	6.03	10.05	10.05	-5.60	-75.2

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	38	-6479	-76	-181	0	660	-29	6.03	6.03	10.05	10.05	-4.89	-67.4
41	38	-6238	14	-150	0	559	-2	6.03	6.03	10.05	10.05	-4.43	-61.4
42	38	-6279	18	-401	0	2389	-1	6.03	6.03	10.05	10.05	-15.74	333.5
43	38	-6362	-132	-165	0	595	-45	6.03	6.03	10.05	10.05	-4.61	-63.8
44	38	-5914	164	-106	0	416	44	6.03	6.03	10.05	10.05	-3.79	-53.1
45	38	-6027	24	-531	0	3477	1	6.03	6.03	10.05	10.05	-23.28	686.9
46	38	-5791	21	-92	0	346	1	6.03	6.03	10.05	10.05	-3.49	-49.2
47	38	-5680	22	-77	0	293	2	6.03	6.03	10.05	10.05	-3.26	-46.2
49	38	-5760	-8	-88	0	327	-8	6.03	6.03	10.05	10.05	-3.41	-48.2
50	38	-5671	51	-76	0	291	10	6.03	6.03	10.05	10.05	-3.25	-46.1
51	38	-5693	23	-161	0	903	2	6.03	6.03	10.05	10.05	-5.68	-76.2

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	50	-6404	-76	-181	0	683	-38	6.03	6.03	10.05	10.05	-4.94	-68.0
41	50	-6163	14	-150	0	577	0	6.03	6.03	10.05	10.05	-4.47	-61.8
42	50	-6204	18	-401	0	2439	1	6.03	6.03	10.05	10.05	-16.11	353.0
43	50	-6287	-132	-165	0	616	-62	6.03	6.03	10.05	10.05	-4.65	-64.3
44	50	-5839	164	-106	0	429	64	6.03	6.03	10.05	10.05	-3.81	-53.3
45	50	-5952	24	-531	0	3543	4	6.03	6.03	10.05	10.05	-23.73	713.2
46	50	-5716	21	-92	0	358	4	6.03	6.03	10.05	10.05	-3.50	-49.3
47	50	-5605	22	-77	0	303	4	6.03	6.03	10.05	10.05	-3.26	-46.2
49	50	-5685	-8	-88	0	338	-8	6.03	6.03	10.05	10.05	-3.42	-48.2
50	50	-5596	51	-76	0	301	17	6.03	6.03	10.05	10.05	-3.25	-46.1
51	50	-5618	23	-161	0	923	5	6.03	6.03	10.05	10.05	-5.78	-77.1

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

ASTA NUM. 113 NI 89 NF 41 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 17A
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-10010	-421	-321	0	652	-38	6.03	6.03	10.05	10.05	-6.23	-87.5
41	0	-9625	-37	-266	0	551	0	6.03	6.03	10.05	10.05	-5.71	-80.7
42	0	-9687	-25	-696	0	2249	1	6.03	6.03	10.05	10.05	-14.06	-179.4
43	0	-9827	-653	-293	0	589	-62	6.03	6.03	10.05	10.05	-5.93	-83.6
44	0	-9104	600	-188	0	407	64	6.03	6.03	10.05	10.05	-4.99	-71.2
45	0	-9286	6	-919	0	3249	4	6.03	6.03	10.05	10.05	-21.27	410.1
46	0	-8916	2	-163	0	341	4	6.03	6.03	10.05	10.05	-4.68	-67.2
47	0	-8739	11	-137	0	288	4	6.03	6.03	10.05	10.05	-4.42	-63.8
49	0	-8868	-117	-155	0	322	-8	6.03	6.03	10.05	10.05	-4.60	-66.0
50	0	-8723	134	-134	0	286	17	6.03	6.03	10.05	10.05	-4.41	-63.6
51	0	-8760	15	-280	0	854	5	6.03	6.03	10.05	10.05	-6.47	-89.4

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	12	-9936	-421	-321	0	692	-91	6.03	6.03	10.05	10.05	-6.34	-88.9
41	12	-9550	-37	-266	0	584	-4	6.03	6.03	10.05	10.05	-5.80	-81.8
42	12	-9612	-25	-696	0	2336	-2	6.03	6.03	10.05	10.05	-14.68	-185.9
43	12	-9752	-653	-293	0	626	-144	6.03	6.03	10.05	10.05	-6.03	-84.8
44	12	-9029	600	-188	0	431	139	6.03	6.03	10.05	10.05	-5.05	-71.9
45	12	-9211	6	-919	0	3364	5	6.03	6.03	10.05	10.05	-22.10	447.8
46	12	-8841	2	-163	0	361	4	6.03	6.03	10.05	10.05	-4.73	-67.6
47	12	-8664	11	-137	0	305	6	6.03	6.03	10.05	10.05	-4.46	-64.1
49	12	-8793	-117	-155	0	342	-23	6.03	6.03	10.05	10.05	-4.64	-66.5
50	12	-8648	134	-134	0	303	33	6.03	6.03	10.05	10.05	-4.44	-63.9
51	12	-8685	15	-280	0	889	7	6.03	6.03	10.05	10.05	-6.57	-90.5

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	25	-9861	-421	-321	0	733	-144	6.03	6.03	10.05	10.05	-6.46	-90.3
41	25	-9475	-37	-266	0	617	-9	6.03	6.03	10.05	10.05	-5.89	-82.8
42	25	-9537	-25	-696	0	2423	-5	6.03	6.03	10.05	10.05	-15.30	-192.4
43	25	-9677	-653	-293	0	662	-225	6.03	6.03	10.05	10.05	-6.13	-86.0
44	25	-8954	600	-188	0	454	214	6.03	6.03	10.05	10.05	-5.11	-72.5
45	25	-9136	6	-919	0	3479	6	6.03	6.03	10.05	10.05	-22.93	486.2
46	25	-8766	2	-163	0	381	4	6.03	6.03	10.05	10.05	-4.77	-68.1
47	25	-8589	11	-137	0	323	7	6.03	6.03	10.05	10.05	-4.49	-64.4
49	25	-8718	-117	-155	0	361	-38	6.03	6.03	10.05	10.05	-4.68	-66.9
50	25	-8573	134	-134	0	319	50	6.03	6.03	10.05	10.05	-4.47	-64.2
51	25	-8610	15	-280	0	924	9	6.03	6.03	10.05	10.05	-6.66	-91.6

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	38	-9786	-421	-321	0	773	-196	6.03	6.03	10.05	10.05	-6.57	-91.7
41	38	-9400	-37	-266	0	650	-14	6.03	6.03	10.05	10.05	-5.98	-83.9
42	38	-9462	-25	-696	0	2510	-8	6.03	6.03	10.05	10.05	-15.93	202.7
43	38	-9602	-653	-293	0	699	-307	6.03	6.03	10.05	10.05	-6.24	-87.3
44	38	-8879	600	-188	0	478	289	6.03	6.03	10.05	10.05	-5.16	-73.1
45	38	-9061	6	-919	0	3594	7	6.03	6.03	10.05	10.05	-23.75	525.0
46	38	-8691	2	-163	0	402	4	6.03	6.03	10.05	10.05	-4.81	-68.6
47	38	-8514	11	-137	0	340	9	6.03	6.03	10.05	10.05	-4.52	-64.8
49	38	-8643	-117	-155	0	380	-52	6.03	6.03	10.05	10.05	-4.72	-67.4
50	38	-8498	134	-134	0	336	67	6.03	6.03	10.05	10.05	-4.50	-64.5
51	38	-8535	15	-280	0	959	10	6.03	6.03	10.05	10.05	-6.76	-92.8

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	50	-9712	-421	-321	0	813	-249	6.03	6.03	10.05	10.05	-6.69	-93.0
41	50	-9325	-37	-266	0	684	-18	6.03	6.03	10.05	10.05	-6.08	-85.0
42	50	-9387	-25	-696	0	2597	-11	6.03	6.03	10.05	10.05	-16.57	227.4
43	50	-9527	-653	-293	0	735	-389	6.03	6.03	10.05	10.05	-6.34	-88.5
44	50	-8804	600	-188	0	501	364	6.03	6.03	10.05	10.05	-5.22	-73.7
45	50	-8986	6	-919	0	3709	8	6.03	6.03	10.05	10.05	-24.57	564.3
46	50	-8616	2	-163	0	422	4	6.03	6.03	10.05	10.05	-4.86	-69.1
47	50	-8439	11	-137	0	357	10	6.03	6.03	10.05	10.05	-4.55	-65.1
49	50	-8568	-117	-155	0	400	-67	6.03	6.03	10.05	10.05	-4.76	-67.8
50	50	-8423	134	-134	0	353	84	6.03	6.03	10.05	10.05	-4.53	-64.8
51	50	-8460	15	-280	0	994	12	6.03	6.03	10.05	10.05	-6.87	-94.1

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

ASTA NUM. 114 NI 477 NF 46 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 22
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-7196	-72	52	0	-93	-22	6.03	6.03	10.05	10.05	-3.12	-46.0
41	0	-7135	-7	7	0	29	-22	6.03	6.03	10.05	10.05	-2.87	-42.8
42	0	-7190	13	-130	0	1384	-25	6.03	6.03	10.05	10.05	-8.56	-112.3
43	0	-6932	-119	86	0	-194	-17	6.03	6.03	10.05	10.05	-3.39	-49.0
44	0	-7122	100	-70	0	238	-22	6.03	6.03	10.05	10.05	-3.62	-52.1
45	0	-6922	21	-218	0	2268	-23	6.03	6.03	10.05	10.05	-14.75	261.9
46	0	-6648	-15	13	0	-4	-15	6.03	6.03	10.05	10.05	-2.59	-38.8
47	0	-6527	-17	15	0	-12	-13	6.03	6.03	10.05	10.05	-2.57	-38.5
49	0	-6547	-39	30	0	-52	-13	6.03	6.03	10.05	10.05	-2.73	-40.4
50	0	-6585	5	-1	0	34	-14	6.03	6.03	10.05	10.05	-2.67	-39.8
51	0	-6545	-11	-31	0	440	-14	6.03	6.03	10.05	10.05	-4.12	-57.8

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	12	-7121	-72	52	0	-99	-31	6.03	6.03	10.05	10.05	-3.12	-45.9
41	12	-7060	-7	7	0	28	-22	6.03	6.03	10.05	10.05	-2.84	-42.3
42	12	-7115	13	-130	0	1400	-23	6.03	6.03	10.05	10.05	-8.67	-113.3
43	12	-6857	-119	86	0	-205	-32	6.03	6.03	10.05	10.05	-3.39	-49.1
44	12	-7047	100	-70	0	246	-9	6.03	6.03	10.05	10.05	-3.62	-52.1
45	12	-6847	21	-218	0	2295	-20	6.03	6.03	10.05	10.05	-14.96	273.6
46	12	-6573	-15	13	0	-5	-17	6.03	6.03	10.05	10.05	-2.57	-38.4
47	12	-6452	-17	15	0	-14	-15	6.03	6.03	10.05	10.05	-2.55	-38.1
49	12	-6472	-39	30	0	-56	-18	6.03	6.03	10.05	10.05	-2.71	-40.1
50	12	-6510	5	-1	0	34	-13	6.03	6.03	10.05	10.05	-2.65	-39.4
51	12	-6470	-11	-31	0	444	-15	6.03	6.03	10.05	10.05	-4.10	-57.6

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	25	-7046	-72	52	0	-106	-40	6.03	6.03	10.05	10.05	-3.11	-45.7
41	25	-6985	-7	7	0	27	-23	6.03	6.03	10.05	10.05	-2.80	-41.8
42	25	-7040	13	-130	0	1416	-22	6.03	6.03	10.05	10.05	-8.77	-114.3
43	25	-6782	-119	86	0	-216	-47	6.03	6.03	10.05	10.05	-3.40	-49.1
44	25	-6972	100	-70	0	255	3	6.03	6.03	10.05	10.05	-3.62	-52.0
45	25	-6772	21	-218	0	2322	-17	6.03	6.03	10.05	10.05	-15.17	285.4
46	25	-6498	-15	13	0	-7	-19	6.03	6.03	10.05	10.05	-2.54	-38.1
47	25	-6377	-17	15	0	-16	-17	6.03	6.03	10.05	10.05	-2.53	-37.8
49	25	-6397	-39	30	0	-60	-23	6.03	6.03	10.05	10.05	-2.69	-39.9
50	25	-6435	5	-1	0	34	-13	6.03	6.03	10.05	10.05	-2.62	-38.9
51	25	-6395	-11	-31	0	448	-17	6.03	6.03	10.05	10.05	-4.09	-57.3

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	38	-6971	-72	52	0	-112	-48	6.03	6.03	10.05	10.05	-3.10	-45.6
41	38	-6910	-7	7	0	26	-24	6.03	6.03	10.05	10.05	-2.77	-41.3
42	38	-6965	13	-130	0	1433	-20	6.03	6.03	10.05	10.05	-8.88	-115.4
43	38	-6707	-119	86	0	-226	-62	6.03	6.03	10.05	10.05	-3.41	-49.2
44	38	-6897	100	-70	0	264	16	6.03	6.03	10.05	10.05	-3.62	-52.0
45	38	-6697	21	-218	0	2349	-15	6.03	6.03	10.05	10.05	-15.38	297.4
46	38	-6423	-15	13	0	-9	-20	6.03	6.03	10.05	10.05	-2.52	-37.7
47	38	-6302	-17	15	0	-18	-19	6.03	6.03	10.05	10.05	-2.50	-37.4
49	38	-6322	-39	30	0	-64	-28	6.03	6.03	10.05	10.05	-2.68	-39.6
50	38	-6360	5	-1	0	34	-12	6.03	6.03	10.05	10.05	-2.59	-38.5
51	38	-6320	-11	-31	0	451	-18	6.03	6.03	10.05	10.05	-4.07	-57.1

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	50	-6896	-72	52	0	-119	-57	6.03	6.03	10.05	10.05	-3.10	-45.4

41	50	-6835	-7	7	0	25	-25	6.03	6.03	10.05	10.05	-2.74	-40.9
42	50	-6890	13	-130	0	1449	-18	6.03	6.03	10.05	10.05	-8.99	-116.4
43	50	-6632	-119	86	0	-237	-77	6.03	6.03	10.05	10.05	-3.42	-49.2
44	50	-6822	100	-70	0	272	28	6.03	6.03	10.05	10.05	-3.62	-51.9
45	50	-6622	21	-218	0	2376	-12	6.03	6.03	10.05	10.05	-15.59	309.6
46	50	-6348	-15	13	0	-10	-22	6.03	6.03	10.05	10.05	-2.50	-37.4
47	50	-6227	-17	15	0	-19	-22	6.03	6.03	10.05	10.05	-2.48	-37.1
49	50	-6247	-39	30	0	-67	-32	6.03	6.03	10.05	10.05	-2.66	-39.3
50	50	-6285	5	-1	0	35	-11	6.03	6.03	10.05	10.05	-2.56	-38.1
51	50	-6245	-11	-31	0	455	-19	6.03	6.03	10.05	10.05	-4.06	-56.8

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

ASTA NUM. 115 NI 46 NF 42 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 22A
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-10810	-789	93	0	-120	-57	6.03	6.03	10.05	10.05	-4.62	-68.2
41	0	-10730	-434	13	0	20	-25	6.03	6.03	10.05	10.05	-4.23	-63.2
42	0	-10800	-377	-216	0	1300	-18	6.03	6.03	10.05	10.05	-8.89	-121.6
43	0	-10390	-978	153	0	-234	-77	6.03	6.03	10.05	10.05	-4.87	-70.9
44	0	-10740	151	-123	0	259	28	6.03	6.03	10.05	10.05	-5.10	-74.1
45	0	-10370	-291	-362	0	2133	-12	6.03	6.03	10.05	10.05	-13.22	-171.8
46	0	-9969	-359	24	0	-13	-22	6.03	6.03	10.05	10.05	-3.91	-58.5
47	0	-9778	-340	27	0	-22	-22	6.03	6.03	10.05	10.05	-3.87	-57.8
49	0	-9804	-458	53	0	-68	-32	6.03	6.03	10.05	10.05	-4.04	-60.1
50	0	-9874	-232	-2	0	30	-11	6.03	6.03	10.05	10.05	-3.94	-58.8
51	0	-9801	-321	-50	0	405	-19	6.03	6.03	10.05	10.05	-5.26	-75.2

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	12	-10735	-789	93	0	-132	-156	6.03	6.03	10.05	10.05	-4.78	-68.7
41	12	-10655	-434	13	0	18	-80	6.03	6.03	10.05	10.05	-4.35	-63.8
42	12	-10725	-377	-216	0	1327	-65	6.03	6.03	10.05	10.05	-8.97	-122.5
43	12	-10315	-978	153	0	-253	-199	6.03	6.03	10.05	10.05	-4.91	-71.3
44	12	-10665	151	-123	0	275	47	6.03	6.03	10.05	10.05	-5.12	-74.4
45	12	-10295	-291	-362	0	2178	-48	6.03	6.03	10.05	10.05	-13.52	-174.9
46	12	-9894	-359	24	0	-16	-67	6.03	6.03	10.05	10.05	-4.01	-58.8
47	12	-9703	-340	27	0	-25	-64	6.03	6.03	10.05	10.05	-3.92	-57.6
49	12	-9729	-458	53	0	-75	-90	6.03	6.03	10.05	10.05	-4.06	-59.9
50	12	-9799	-232	-2	0	31	-40	6.03	6.03	10.05	10.05	-3.91	-58.3
51	12	-9726	-321	-50	0	411	-59	6.03	6.03	10.05	10.05	-5.25	-75.0

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	25	-10660	-789	93	0	-143	-255	6.03	6.03	10.05	10.05	-5.26	-74.0
41	25	-10580	-434	13	0	16	-134	6.03	6.03	10.05	10.05	-4.61	-66.5
42	25	-10650	-377	-216	0	1354	-113	6.03	6.03	10.05	10.05	-9.06	-123.5
43	25	-10240	-978	153	0	-272	-322	6.03	6.03	10.05	10.05	-5.45	-75.5
44	25	-10590	151	-123	0	290	66	6.03	6.03	10.05	10.05	-5.15	-74.6
45	25	-10220	-291	-362	0	2224	-85	6.03	6.03	10.05	10.05	-13.82	-178.2
46	25	-9819	-359	24	0	-19	-112	6.03	6.03	10.05	10.05	-4.21	-61.0
47	25	-9628	-340	27	0	-28	-107	6.03	6.03	10.05	10.05	-4.11	-59.6
49	25	-9654	-458	53	0	-82	-147	6.03	6.03	10.05	10.05	-4.33	-62.1
50	25	-9724	-232	-2	0	31	-69	6.03	6.03	10.05	10.05	-3.96	-58.0
51	25	-9651	-321	-50	0	417	-99	6.03	6.03	10.05	10.05	-5.24	-74.9

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	38	-10585	-789	93	0	-155	-353	6.03	6.03	10.05	10.05	-5.74	-79.3
41	38	-10505	-434	13	0	15	-188	6.03	6.03	10.05	10.05	-4.86	-69.2
42	38	-10575	-377	-216	0	1381	-160	6.03	6.03	10.05	10.05	-9.15	-124.5
43	38	-10165	-978	153	0	-291	-444	6.03	6.03	10.05	10.05	-6.05	-82.2
44	38	-10515	151	-123	0	306	85	6.03	6.03	10.05	10.05	-5.17	-74.9
45	38	-10145	-291	-362	0	2269	-121	6.03	6.03	10.05	10.05	-14.13	-181.4
46	38	-9744	-359	24	0	-22	-157	6.03	6.03	10.05	10.05	-4.42	-63.2
47	38	-9553	-340	27	0	-32	-149	6.03	6.03	10.05	10.05	-4.30	-61.7
49	38	-9579	-458	53	0	-88	-204	6.03	6.03	10.05	10.05	-4.60	-65.0
50	38	-9649	-232	-2	0	31	-98	6.03	6.03	10.05	10.05	-4.08	-59.3
51	38	-9576	-321	-50	0	424	-140	6.03	6.03	10.05	10.05	-5.24	-74.7

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	50	-10510	-789	93	0	-166	-452	6.03	6.03	10.05	10.05	-6.22	-84.6
41	50	-10430	-434	13	0	13	-242	6.03	6.03	10.05	10.05	-5.11	-72.0
42	50	-10500	-377	-216	0	1408	-207	6.03	6.03	10.05	10.05	-9.25	-125.6
43	50	-10090	-978	153	0	-310	-566	6.03	6.03	10.05	10.05	-6.65	-88.9
44	50	-10440	151	-123	0	321	104	6.03	6.03	10.05	10.05	-5.20	-75.1
45	50	-10070	-291	-362	0	2314	-158	6.03	6.03	10.05	10.05	-14.45	-184.7
46	50	-9669	-359	24	0	-25	-202	6.03	6.03	10.05	10.05	-4.62	-65.4
47	50	-9478	-340	27	0	-35	-192	6.03	6.03	10.05	10.05	-4.50	-63.7
49	50	-9504	-458	53	0	-95	-261	6.03	6.03	10.05	10.05	-4.87	-67.9
50	50	-9574	-232	-2	0	31	-127	6.03	6.03	10.05	10.05	-4.20	-60.5
51	50	-9501	-321	-50	0	430	-180	6.03	6.03	10.05	10.05	-5.23	-74.6

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

ASTA NUM. 116 NI 216 NF 482 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 32
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-2654	-1303	559	0	197	790	6.03	6.03	10.05	10.05	-7.00	131.8
41	0	-2722	-938	323	0	134	580	6.03	6.03	10.05	10.05	-5.11	67.9
42	0	-2486	-595	-670	0	-356	482	6.03	6.03	10.05	10.05	-4.23	49.1
43	0	-2641	-1401	610	0	228	815	6.03	6.03	10.05	10.05	-7.23	139.9
44	0	-2849	-351	-60	0	31	248	6.03	6.03	10.05	10.05	-2.35	-30.4

45	0	-2360	-221	-1439	0	-694	301	6.03	6.03	10.05	10.05	-4.46	67.6
46	0	-2773	-704	152	0	118	396	6.03	6.03	10.05	10.05	-3.45	-41.4
47	0	-2785	-645	109	0	114	350	6.03	6.03	10.05	10.05	-3.07	-37.7
49	0	-2763	-767	188	0	134	420	6.03	6.03	10.05	10.05	-3.66	-43.3
50	0	-2804	-557	54	0	95	307	6.03	6.03	10.05	10.05	-2.74	-34.3
51	0	-2706	-531	-222	0	-50	317	6.03	6.03	10.05	10.05	-2.80	-34.8

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	12	-2579	-1303	559	0	127	627	6.03	6.03	10.05	10.05	-5.54	86.4
41	12	-2647	-938	323	0	94	462	6.03	6.03	10.05	10.05	-4.05	-46.4
42	12	-2411	-595	-670	0	-272	407	6.03	6.03	10.05	10.05	-3.56	-41.1
43	12	-2566	-1401	610	0	152	640	6.03	6.03	10.05	10.05	-5.66	90.7
44	12	-2774	-351	-60	0	39	204	6.03	6.03	10.05	10.05	-2.08	-27.2
45	12	-2285	-221	-1439	0	-514	274	6.03	6.03	10.05	10.05	-3.20	-41.1
46	12	-2698	-704	152	0	99	308	6.03	6.03	10.05	10.05	-2.73	-34.0
47	12	-2710	-645	109	0	100	269	6.03	6.03	10.05	10.05	-2.45	-31.2
49	12	-2688	-767	188	0	111	324	6.03	6.03	10.05	10.05	-2.85	-35.3
50	12	-2729	-557	54	0	88	237	6.03	6.03	10.05	10.05	-2.25	-29.1
51	12	-2631	-531	-222	0	-22	251	6.03	6.03	10.05	10.05	-2.31	-29.5

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	25	-2504	-1303	559	0	57	464	6.03	6.03	10.05	10.05	-4.07	-46.0
41	25	-2572	-938	323	0	54	345	6.03	6.03	10.05	10.05	-3.02	-36.6
42	25	-2336	-595	-670	0	-189	333	6.03	6.03	10.05	10.05	-2.90	-34.8
43	25	-2491	-1401	610	0	76	465	6.03	6.03	10.05	10.05	-4.08	-46.1
44	25	-2699	-351	-60	0	46	160	6.03	6.03	10.05	10.05	-1.82	-24.3
45	25	-2210	-221	-1439	0	-334	246	6.03	6.03	10.05	10.05	-2.19	-28.6
46	25	-2623	-704	152	0	80	220	6.03	6.03	10.05	10.05	-2.12	-27.4
47	25	-2635	-645	109	0	86	189	6.03	6.03	10.05	10.05	-1.95	-25.6
49	25	-2613	-767	188	0	88	228	6.03	6.03	10.05	10.05	-2.16	-27.9
50	25	-2654	-557	54	0	82	167	6.03	6.03	10.05	10.05	-1.85	-24.4
51	25	-2556	-531	-222	0	6	185	6.03	6.03	10.05	10.05	-1.90	-24.9

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	38	-2429	-1303	559	0	-13	301	6.03	6.03	10.05	10.05	-2.64	-32.5
41	38	-2497	-938	323	0	13	228	6.03	6.03	10.05	10.05	-2.13	-27.3
42	38	-2261	-595	-670	0	-105	258	6.03	6.03	10.05	10.05	-2.29	-28.5
43	38	-2416	-1401	610	0	-0	290	6.03	6.03	10.05	10.05	-2.55	-31.6
44	38	-2624	-351	-60	0	54	116	6.03	6.03	10.05	10.05	-1.57	-21.3
45	38	-2135	-221	-1439	0	-154	219	6.03	6.03	10.05	10.05	-1.98	-25.0
46	38	-2548	-704	152	0	61	132	6.03	6.03	10.05	10.05	-1.62	-21.8
47	38	-2560	-645	109	0	73	108	6.03	6.03	10.05	10.05	-1.50	-20.5
49	38	-2538	-767	188	0	64	132	6.03	6.03	10.05	10.05	-1.62	-21.8
50	38	-2579	-557	54	0	75	98	6.03	6.03	10.05	10.05	-1.46	-20.0
51	38	-2481	-531	-222	0	33	118	6.03	6.03	10.05	10.05	-1.53	-20.6

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	50	-2354	-1303	559	0	-82	138	6.03	6.03	10.05	10.05	-1.58	-21.1
41	50	-2422	-938	323	0	-27	111	6.03	6.03	10.05	10.05	-1.47	-19.9
42	50	-2186	-595	-670	0	-21	184	6.03	6.03	10.05	10.05	-1.77	-22.9
43	50	-2341	-1401	610	0	-76	115	6.03	6.03	10.05	10.05	-1.46	-19.6
44	50	-2549	-351	-60	0	61	72	6.03	6.03	10.05	10.05	-1.32	-18.3
45	50	-2060	-221	-1439	0	26	191	6.03	6.03	10.05	10.05	-1.77	-22.8
46	50	-2473	-704	152	0	42	44	6.03	6.03	10.05	10.05	-1.14	-16.3
47	50	-2485	-645	109	0	59	27	6.03	6.03	10.05	10.05	-1.18	-17.1
49	50	-2463	-767	188	0	41	37	6.03	6.03	10.05	10.05	-1.10	-16.1
50	50	-2504	-557	54	0	68	28	6.03	6.03	10.05	10.05	-1.22	-17.6
51	50	-2406	-531	-222	0	61	52	6.03	6.03	10.05	10.05	-1.16	-16.7

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

ASTA NUM. 117 NI 482 NF 33 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 32A
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-4550	509	332	0	37	-227	6.03	6.03	10.05	10.05	-2.86	-38.5
41	0	-4385	467	252	0	71	-156	6.03	6.03	10.05	10.05	-2.43	-33.4
42	0	-4262	545	-4	0	301	-125	6.03	6.03	10.05	10.05	-2.73	-38.3
43	0	-4493	417	321	0	38	-265	6.03	6.03	10.05	10.05	-3.03	-40.3
44	0	-4164	417	124	0	128	-38	6.03	6.03	10.05	10.05	-2.08	-30.0
45	0	-4013	476	-240	0	478	-94	6.03	6.03	10.05	10.05	-3.28	-44.9
46	0	-4118	273	148	0	110	-140	6.03	6.03	10.05	10.05	-2.24	-31.0
47	0	-4051	224	122	0	119	-135	6.03	6.03	10.05	10.05	-2.20	-30.3
49	0	-4106	238	149	0	108	-159	6.03	6.03	10.05	10.05	-2.34	-32.0
50	0	-4040	239	110	0	126	-114	6.03	6.03	10.05	10.05	-2.08	-29.2
51	0	-4010	250	37	0	196	-125	6.03	6.03	10.05	10.05	-2.26	-32.1

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	12	-4475	509	332	0	-5	-164	6.03	6.03	10.05	10.05	-2.50	-34.3
41	12	-4310	467	252	0	40	-98	6.03	6.03	10.05	10.05	-2.10	-29.6
42	12	-4187	545	-4	0	301	-57	6.03	6.03	10.05	10.05	-2.71	-37.9
43	12	-4418	417	321	0	-2	-213	6.03	6.03	10.05	10.05	-2.73	-36.9
44	12	-4089	417	124	0	113	14	6.03	6.03	10.05	10.05	-1.99	-28.8
45	12	-3938	476	-240	0	508	-34	6.03	6.03	10.05	10.05	-3.38	-46.0
46	12	-4043	273	148	0	91	-105	6.03	6.03	10.05	10.05	-2.04	-28.6
47	12	-3976	224	122	0	104	-107	6.03	6.03	10.05	10.05	-2.03	-28.3
49	12	-4031	238	149	0	89	-129	6.03	6.03	10.05	10.05	-2.16	-29.9
50	12	-3965	239	110	0	112	-84	6.03	6.03	10.05	10.05	-1.94	-28.1
51	12	-3935	250	37	0	191	-94	6.03	6.03	10.05	10.05	-2.21	-31.5

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	25	-4400	509	332	0	-46	-100	6.03	6.03	10.05	10.05	-2.14	-30.2
41	25	-4235	467	252	0	8	-39	6.03	6.03	10.05	10.05	-1.77	-25.8
42	25	-4112	545	-4	0	302	11	6.03	6.03	10.05	10.05	-2.68	-37.5
43	25	-4343	417	321	0	-43	-161	6.03	6.03	10.05	10.05	-2.44	-33.4
44	25	-4014	417	124	0	97	66	6.03	6.03	10.05	10.05	-1.90	-27.7
45	25	-3863	476	-240	0	538	25	6.03	6.03	10.05	10.05	-3.49	-47.3

46	25	-3968	273	148	0	73	-71	6.03	6.03	10.05	10.05	-1.84	-26.3
47	25	-3901	224	122	0	89	-79	6.03	6.03	10.05	10.05	-1.85	-26.7
49	25	-3956	238	149	0	71	-100	6.03	6.03	10.05	10.05	-1.98	-27.7
50	25	-3890	239	110	0	99	-54	6.03	6.03	10.05	10.05	-1.86	-27.0
51	25	-3860	250	37	0	187	-62	6.03	6.03	10.05	10.05	-2.17	-30.8

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	38	-4325	509	332	0	-88	-36	6.03	6.03	10.05	10.05	-1.99	-29.1
41	38	-4160	467	252	0	-23	19	6.03	6.03	10.05	10.05	-1.69	-25.2
42	38	-4037	545	-4	0	302	80	6.03	6.03	10.05	10.05	-2.65	-37.1
43	38	-4268	417	321	0	-83	-109	6.03	6.03	10.05	10.05	-2.14	-30.0
44	38	-3939	417	124	0	82	118	6.03	6.03	10.05	10.05	-2.07	-28.7
45	38	-3788	476	-240	0	567	85	6.03	6.03	10.05	10.05	-3.61	-48.6
46	38	-3893	273	148	0	54	-37	6.03	6.03	10.05	10.05	-1.70	-25.1
47	38	-3826	224	122	0	74	-51	6.03	6.03	10.05	10.05	-1.75	-25.5
49	38	-3881	238	149	0	52	-70	6.03	6.03	10.05	10.05	-1.80	-25.6
50	38	-3815	239	110	0	85	-25	6.03	6.03	10.05	10.05	-1.78	-26.0
51	38	-3785	250	37	0	182	-31	6.03	6.03	10.05	10.05	-2.12	-30.2

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	50	-4250	509	332	0	-129	27	6.03	6.03	10.05	10.05	-2.11	-30.5
41	50	-4085	467	252	0	-54	77	6.03	6.03	10.05	10.05	-1.91	-27.2
42	50	-3962	545	-4	0	303	148	6.03	6.03	10.05	10.05	-2.63	-36.7
43	50	-4193	417	321	0	-123	-57	6.03	6.03	10.05	10.05	-2.07	-29.9
44	50	-3864	417	124	0	66	170	6.03	6.03	10.05	10.05	-2.31	-31.3
45	50	-3713	476	-240	0	597	144	6.03	6.03	10.05	10.05	-3.75	-50.2
46	50	-3818	273	148	0	36	-3	6.03	6.03	10.05	10.05	-1.61	-23.8
47	50	-3751	224	122	0	58	-23	6.03	6.03	10.05	10.05	-1.66	-24.4
49	50	-3806	238	149	0	33	-40	6.03	6.03	10.05	10.05	-1.62	-23.6
50	50	-3740	239	110	0	71	5	6.03	6.03	10.05	10.05	-1.71	-24.9
51	50	-3710	250	37	0	177	0	6.03	6.03	10.05	10.05	-2.08	-29.5

apost= 2.01 aant= 2.01 ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

ASTA NUM. 118 NI 803 NF 821 SEZ. Rp B= 0.400 H= 0.600 (pilastro)
PIL. NUM. 26
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-4651	3210	360	0	77	-1607	10.05	10.05	6.03	6.03	-10.51	199.6
41	0	-4686	2019	292	0	63	-254	10.05	10.05	6.03	6.03	-2.73	-38.7
42	0	-4687	2023	170	0	51	-250	10.05	10.05	6.03	6.03	-2.72	-38.5
43	0	-4508	3557	328	0	77	-2364	10.05	10.05	6.03	6.03	-15.81	439.0
44	0	-4711	105	196	0	40	1979	10.05	10.05	6.03	6.03	-13.12	306.3
45	0	-4568	1580	13	0	32	-103	10.05	10.05	6.03	6.03	-2.14	-31.2
46	0	-4495	1306	169	0	47	-24	10.05	10.05	6.03	6.03	-1.90	-27.7
47	0	-4447	1127	138	0	42	33	10.05	10.05	6.03	6.03	-1.86	-27.3
49	0	-4436	1524	161	0	47	-418	10.05	10.05	6.03	6.03	-3.22	-44.6
50	0	-4476	834	134	0	40	451	10.05	10.05	6.03	6.03	-3.36	-46.3
51	0	-4447	1129	98	0	38	35	10.05	10.05	6.03	6.03	-1.85	-27.4

apost= 6.03 aant= 6.03 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	12	-4576	3210	360	0	32	-1206	10.05	10.05	6.03	6.03	-7.65	96.0
41	12	-4611	2019	292	0	27	-2	10.05	10.05	6.03	6.03	-1.84	-27.1
42	12	-4612	2023	170	0	29	3	10.05	10.05	6.03	6.03	-1.86	-27.3
43	12	-4433	3557	328	0	36	-1919	10.05	10.05	6.03	6.03	-12.75	305.7
44	12	-4636	105	196	0	16	1992	10.05	10.05	6.03	6.03	-13.23	315.0
45	12	-4493	1580	13	0	31	95	10.05	10.05	6.03	6.03	-2.08	-30.4
46	12	-4420	1306	169	0	25	139	10.05	10.05	6.03	6.03	-2.21	-31.9
47	12	-4372	1127	138	0	25	174	10.05	10.05	6.03	6.03	-2.32	-33.2
49	12	-4361	1524	161	0	27	-227	10.05	10.05	6.03	6.03	-2.51	-35.6
50	12	-4401	834	134	0	23	555	10.05	10.05	6.03	6.03	-3.73	-50.8
51	12	-4372	1129	98	0	26	176	10.05	10.05	6.03	6.03	-2.33	-33.3

apost= 6.03 aant= 6.03 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	25	-4501	3210	360	0	-13	-804	10.05	10.05	6.03	6.03	-4.99	-66.0
41	25	-4536	2019	292	0	-10	250	10.05	10.05	6.03	6.03	-2.66	-37.6
42	25	-4537	2023	170	0	8	256	10.05	10.05	6.03	6.03	-2.68	-37.9
43	25	-4358	3557	328	0	-6	-1475	10.05	10.05	6.03	6.03	-9.62	178.1
44	25	-4561	105	196	0	-9	2005	10.05	10.05	6.03	6.03	-13.33	323.8
45	25	-4418	1580	13	0	29	292	10.05	10.05	6.03	6.03	-2.76	-38.8
46	25	-4345	1306	169	0	4	302	10.05	10.05	6.03	6.03	-2.77	-38.9
47	25	-4297	1127	138	0	8	315	10.05	10.05	6.03	6.03	-2.80	-39.2
49	25	-4286	1524	161	0	7	-36	10.05	10.05	6.03	6.03	-1.79	-26.6
50	25	-4326	834	134	0	6	660	10.05	10.05	6.03	6.03	-4.18	-56.2
51	25	-4297	1129	98	0	14	317	10.05	10.05	6.03	6.03	-2.81	-39.2

apost= 6.03 aant= 6.03 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	38	-4426	3210	360	0	-58	-403	10.05	10.05	6.03	6.03	-3.17	-43.9
41	38	-4461	2019	292	0	-46	503	10.05	10.05	6.03	6.03	-3.54	-48.6
42	38	-4462	2023	170	0	-13	509	10.05	10.05	6.03	6.03	-3.56	-48.9
43	38	-4283	3557	328	0	-47	-1030	10.05	10.05	6.03	6.03	-6.47	-82.0
44	38	-4486	105	196	0	-33	2018	10.05	10.05	6.03	6.03	-13.43	332.6
45	38	-4343	1580	13	0	27	490	10.05	10.05	6.03	6.03	-3.45	-47.3
46	38	-4270	1306	169	0	-17	465	10.05	10.05	6.03	6.03	-3.33	-45.8
47	38	-4222	1127	138	0	-9	456	10.05	10.05	6.03	6.03	-3.28	-45.1
49	38	-4211	1524	161	0	-13	154	10.05	10.05	6.03	6.03	-2.19	-31.4
50	38	-4251	834	134	0	-10	764	10.05	10.05	6.03	6.03	-4.74	-62.6
51	38	-4222	1129	98	0	2	458	10.05	10.05	6.03	6.03	-3.29	-45.2

apost= 6.03 aant= 6.03 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	50	-4351	3210	360	0	-102	-2	10.05	10.05	6.03	6.03	-2.14	-30.1
41	50	-4386	2019	292	0	-83	755	10.05	10.05	6.03	6.03	-4.70	-62.4
42	50	-4387	2023	170	0	-34	762	10.05	10.05	6.03	6.03	-4.74	-62.9
43	50	-4208	3557	328	0	-88	-586	10.05	10.05	6.03	6.03	-3.80	-51.5
44	50	-4411	105	196	0	-58	2031	10.05	10.05	6.03	6.03	-13.53	341.5
45	50	-4268	1580	13	0	26	687	10.05	10.05	6.03	6.03	-4.31	-57.7
46	50	-4195	1306	169	0	-38	629	10.05	10.05	6.03	6.03	-4.00	-53.9

47	50	-4147	1127	138	0	-27	597	10.05	10.05	6.03	6.03	-3.84	-51.9
49	50	-4136	1524	161	0	-33	345	10.05	10.05	6.03	6.03	-2.84	-39.5
50	50	-4176	834	134	0	-27	868	10.05	10.05	6.03	6.03	-5.38	-69.8
51	50	-4147	1129	98	0	-11	599	10.05	10.05	6.03	6.03	-3.85	-52.0

apost= 6.03 aant= 6.03 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

ASTA NUM. 119 NI 821 NF 166 SEZ. Rp B= 0.400 H= 0.600 (pilastro)
PIL. NUM. 26A
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-5896	1340	969	0	-102	-71	10.05	10.05	6.03	6.03	-2.71	-38.7
41	0	-5684	1145	832	0	-83	689	10.05	10.05	6.03	6.03	-4.70	-64.2
42	0	-5683	1147	378	0	-34	695	10.05	10.05	6.03	6.03	-4.72	-64.5
43	0	-5845	1265	783	0	-88	-642	10.05	10.05	6.03	6.03	-4.58	-62.9
44	0	-5286	854	683	0	-58	1968	10.05	10.05	6.03	6.03	-12.95	268.0
45	0	-5490	944	-201	0	26	635	10.05	10.05	6.03	6.03	-4.42	-60.5
46	0	-5376	818	389	0	-38	587	10.05	10.05	6.03	6.03	-4.20	-57.7
47	0	-5300	737	278	0	-27	561	10.05	10.05	6.03	6.03	-4.07	-56.1
49	0	-5370	801	324	0	-33	308	10.05	10.05	6.03	6.03	-3.19	-45.1
50	0	-5258	719	304	0	-27	830	10.05	10.05	6.03	6.03	-5.23	-70.1
51	0	-5299	737	127	0	-11	563	10.05	10.05	6.03	6.03	-4.08	-56.1

apost= 6.03 aant= 6.03 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	12	-5821	1340	969	0	-224	96	10.05	10.05	6.03	6.03	-3.31	-45.3
41	12	-5609	1145	832	0	-187	832	10.05	10.05	6.03	6.03	-5.31	-71.6
42	12	-5608	1147	378	0	-82	838	10.05	10.05	6.03	6.03	-5.34	-71.9
43	12	-5770	1265	783	0	-186	-484	10.05	10.05	6.03	6.03	-3.98	-55.3
44	12	-5211	854	683	0	-143	2075	10.05	10.05	6.03	6.03	-13.71	304.3
45	12	-5415	944	-201	0	51	753	10.05	10.05	6.03	6.03	-4.89	-66.2
46	12	-5301	818	389	0	-86	689	10.05	10.05	6.03	6.03	-4.57	-62.3
47	12	-5225	737	278	0	-61	653	10.05	10.05	6.03	6.03	-4.40	-60.0
49	12	-5295	801	324	0	-74	408	10.05	10.05	6.03	6.03	-3.52	-49.1
50	12	-5183	719	304	0	-65	920	10.05	10.05	6.03	6.03	-5.71	-75.6
51	12	-5224	737	127	0	-26	655	10.05	10.05	6.03	6.03	-4.41	-60.1

apost= 6.03 aant= 6.03 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	25	-5746	1340	969	0	-345	264	10.05	10.05	6.03	6.03	-3.90	-51.9
41	25	-5534	1145	832	0	-291	976	10.05	10.05	6.03	6.03	-6.06	-80.3
42	25	-5533	1147	378	0	-129	981	10.05	10.05	6.03	6.03	-6.09	-80.7
43	25	-5695	1265	783	0	-283	-326	10.05	10.05	6.03	6.03	-3.57	-48.1
44	25	-5136	854	683	0	-228	2182	10.05	10.05	6.03	6.03	-14.47	341.3
45	25	-5340	944	-201	0	76	870	10.05	10.05	6.03	6.03	-5.45	-72.9
46	25	-5226	818	389	0	-135	791	10.05	10.05	6.03	6.03	-5.03	-67.6
47	25	-5150	737	278	0	-96	745	10.05	10.05	6.03	6.03	-4.79	-64.6
49	25	-5220	801	324	0	-114	508	10.05	10.05	6.03	6.03	-3.85	-53.2
50	25	-5108	719	304	0	-103	1009	10.05	10.05	6.03	6.03	-6.25	-81.6
51	25	-5149	737	127	0	-42	747	10.05	10.05	6.03	6.03	-4.79	-64.7

apost= 6.03 aant= 6.03 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	38	-5671	1340	969	0	-466	431	10.05	10.05	6.03	6.03	-4.52	-58.7
41	38	-5459	1145	832	0	-395	1119	10.05	10.05	6.03	6.03	-6.93	-90.1
42	38	-5458	1147	378	0	-176	1125	10.05	10.05	6.03	6.03	-6.97	-90.6
43	38	-5620	1265	783	0	-381	-168	10.05	10.05	6.03	6.03	-4.05	-53.3
44	38	-5061	854	683	0	-314	2288	10.05	10.05	6.03	6.03	-15.23	378.8
45	38	-5265	944	-201	0	101	988	10.05	10.05	6.03	6.03	-6.12	-80.5
46	38	-5151	818	389	0	-184	894	10.05	10.05	6.03	6.03	-5.56	-73.8
47	38	-5075	737	278	0	-131	837	10.05	10.05	6.03	6.03	-5.24	-69.9
49	38	-5145	801	324	0	-155	608	10.05	10.05	6.03	6.03	-4.19	-57.4
50	38	-5033	719	304	0	-141	1099	10.05	10.05	6.03	6.03	-6.84	-88.1
51	38	-5074	737	127	0	-58	840	10.05	10.05	6.03	6.03	-5.25	-70.0

apost= 6.03 aant= 6.03 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

40	50	-5596	1340	969	0	-587	599	10.05	10.05	6.03	6.03	-5.28	-66.7
41	50	-5384	1145	832	0	-499	1262	10.05	10.05	6.03	6.03	-7.90	-100.6
42	50	-5383	1147	378	0	-224	1268	10.05	10.05	6.03	6.03	-7.94	-101.1
43	50	-5545	1265	783	0	-479	-10	10.05	10.05	6.03	6.03	-4.56	-58.9
44	50	-4986	854	683	0	-399	2395	10.05	10.05	6.03	6.03	-15.98	416.8
45	50	-5190	944	-201	0	126	1106	10.05	10.05	6.03	6.03	-6.87	-88.8
46	50	-5076	818	389	0	-232	996	10.05	10.05	6.03	6.03	-6.16	-80.6
47	50	-5000	737	278	0	-166	930	10.05	10.05	6.03	6.03	-5.75	-75.8
49	50	-5070	801	324	0	-195	708	10.05	10.05	6.03	6.03	-4.59	-62.2
50	50	-4958	719	304	0	-179	1189	10.05	10.05	6.03	6.03	-7.46	-94.7
51	50	-4999	737	127	0	-74	932	10.05	10.05	6.03	6.03	-5.77	-75.9

apost= 6.03 aant= 6.03 ainf= 2.01 asup= 2.01 (e arm. base= 4 X 2.01)

ASTA NUM. 120 NI 804 NF 827 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 25
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-7621	330	613	0	7	-358	4.02	4.02	10.05	10.05	-6.87	-86.9
41	0	-7117	189	530	0	17	-68	4.02	4.02	10.05	10.05	-4.00	-57.0
42	0	-7036	189	362	0	34	-69	4.02	4.02	10.05	10.05	-3.98	-57.0
43	0	-7635	383	552	0	6	-538	4.02	4.02	10.05	10.05	-8.69	-104.5
44	0	-6233	-40	417	0	31	413	4.02	4.02	10.05	10.05	-6.80	-82.6
45	0	-6659	148	135	0	51	-58	4.02	4.02	10.05	10.05	-3.72	-55.1
46	0	-6601	123	346	0	26	-47	4.02	4.02	10.05	10.05	-3.57	-53.1
47	0	-6472	107	300	0	28	-42	4.02	4.02	10.05	10.05	-3.51	-52.3
49	0	-6641	154	328	0	25	-139	4.02	4.02	10.05	10.05	-4.42	-60.0
50	0	-6360	69	300	0	30	51	4.02	4.02	10.05	10.05	-3.49	-51.5
51	0	-6445	107	244	0	34	-43	4.02	4.02	10.05	10.05	-3.52	-52.4

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	12	-7565	330	613	0	-70	-316	4.02	4.02	10.05	10.05	-6.47	-82.7
41	12	-7061	189	530	0	-50	-44	4.02	4.02	10.05	10.05	-3.92	-58.2
42	12	-6980	189	362	0	-11	-46	4.02	4.02	10.05	10.05	-3.74	-55.2
43	12	-7579	383	552	0	-63	-490	4.02	4.02	10.05	10.05	-8.14	-99.2
44	12	-6177	-40	417	0	-22	408	4.02	4.02	10.05	10.05	-6.73	-81.7
45	12	-6603	148	135	0	35	-39	4.02	4.02	10.05	10.05	-3.61	-53.7
46	12	-6545	123	346	0	-17	-32	4.02	4.02	10.05	10.05	-3.49	-52.2
47	12	-6416	107	300	0	-9	-29	4.02	4.02	10.05	10.05	-3.38	-50.7
49	12	-6585	154	328	0	-16	-120	4.02	4.02	10.05	10.05	-4.22	-57.9
50	12	-6304	69	300	0	-8	60	4.02	4.02	10.05	10.05	-3.55	-50.5
51	12	-6389	107	244	0	4	-29	4.02	4.02	10.05	10.05	-3.34	-50.1

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	25	-7508	330	613	0	-147	-275	4.02	4.02	10.05	10.05	-6.07	-78.6
41	25	-7004	189	530	0	-116	-21	4.02	4.02	10.05	10.05	-4.21	-61.8
42	25	-6924	189	362	0	-57	-22	4.02	4.02	10.05	10.05	-3.88	-57.5
43	25	-7522	383	552	0	-132	-442	4.02	4.02	10.05	10.05	-7.62	-94.0
44	25	-6120	-40	417	0	-74	403	4.02	4.02	10.05	10.05	-6.65	-80.9
45	25	-6546	148	135	0	18	-21	4.02	4.02	10.05	10.05	-3.49	-52.2
46	25	-6488	123	346	0	-60	-17	4.02	4.02	10.05	10.05	-3.67	-54.4
47	25	-6360	107	300	0	-47	-16	4.02	4.02	10.05	10.05	-3.54	-52.5
49	25	-6528	154	328	0	-57	-100	4.02	4.02	10.05	10.05	-4.02	-55.7
50	25	-6248	69	300	0	-45	69	4.02	4.02	10.05	10.05	-3.60	-51.5
51	25	-6332	107	244	0	-27	-16	4.02	4.02	10.05	10.05	-3.43	-51.1

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	38	-7452	330	613	0	-223	-234	4.02	4.02	10.05	10.05	-5.67	-74.4
41	38	-6948	189	530	0	-182	3	4.02	4.02	10.05	10.05	-4.51	-65.4
42	38	-6867	189	362	0	-102	1	4.02	4.02	10.05	10.05	-4.07	-59.8
43	38	-7466	383	552	0	-202	-394	4.02	4.02	10.05	10.05	-7.13	-89.1
44	38	-6064	-40	417	0	-126	398	4.02	4.02	10.05	10.05	-6.58	-80.0
45	38	-6490	148	135	0	1	-2	4.02	4.02	10.05	10.05	-3.38	-50.7
46	38	-6432	123	346	0	-104	-1	4.02	4.02	10.05	10.05	-3.85	-56.6
47	38	-6303	107	300	0	-84	-2	4.02	4.02	10.05	10.05	-3.69	-54.4
49	38	-6472	154	328	0	-98	-81	4.02	4.02	10.05	10.05	-3.85	-56.5
50	38	-6191	69	300	0	-83	77	4.02	4.02	10.05	10.05	-3.65	-53.4
51	38	-6276	107	244	0	-57	-3	4.02	4.02	10.05	10.05	-3.55	-52.5

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	50	-7396	330	613	0	-300	-192	4.02	4.02	10.05	10.05	-5.31	-76.0
41	50	-6892	189	530	0	-248	27	4.02	4.02	10.05	10.05	-4.80	-69.0
42	50	-6811	189	362	0	-147	25	4.02	4.02	10.05	10.05	-4.26	-62.2
43	50	-7410	383	552	0	-271	-346	4.02	4.02	10.05	10.05	-6.67	-84.3
44	50	-6008	-40	417	0	-178	394	4.02	4.02	10.05	10.05	-6.51	-79.1
45	50	-6434	148	135	0	-16	16	4.02	4.02	10.05	10.05	-3.43	-51.2
46	50	-6376	123	346	0	-147	14	4.02	4.02	10.05	10.05	-4.04	-58.8
47	50	-6247	107	300	0	-122	11	4.02	4.02	10.05	10.05	-3.85	-56.2
49	50	-6416	154	328	0	-139	-62	4.02	4.02	10.05	10.05	-4.02	-58.6
50	50	-6135	69	300	0	-120	86	4.02	4.02	10.05	10.05	-3.78	-55.2
51	50	-6220	107	244	0	-88	11	4.02	4.02	10.05	10.05	-3.67	-53.9

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

ASTA NUM. 121 NI 827 NF 263 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 25A
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-10830	-273	1319	0	-300	-190	4.02	4.02	10.05	10.05	-7.10	-102.9
41	0	-9977	105	1077	0	-248	11	4.02	4.02	10.05	10.05	-6.41	-93.1
42	0	-9844	102	595	0	-147	10	4.02	4.02	10.05	10.05	-5.84	-85.9
43	0	-10920	-548	1204	0	-271	-329	4.02	4.02	10.05	10.05	-8.18	-107.8
44	0	-8502	739	740	0	-178	349	4.02	4.02	10.05	10.05	-7.22	-92.4
45	0	-9285	77	-2	0	-16	6	4.02	4.02	10.05	10.05	-4.91	-73.5
46	0	-9224	68	635	0	-147	6	4.02	4.02	10.05	10.05	-5.52	-81.0
47	0	-9035	59	525	0	-122	4	4.02	4.02	10.05	10.05	-5.30	-78.0
49	0	-9318	-67	606	0	-139	-63	4.02	4.02	10.05	10.05	-5.53	-81.2
50	0	-8834	190	513	0	-120	72	4.02	4.02	10.05	10.05	-5.19	-76.3
51	0	-8991	58	364	0	-88	4	4.02	4.02	10.05	10.05	-5.11	-75.6

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	12	-10772	-273	1319	0	-465	-225	4.02	4.02	10.05	10.05	-7.87	-112.5
41	12	-9921	105	1077	0	-383	25	4.02	4.02	10.05	10.05	-7.03	-100.8
42	12	-9788	102	595	0	-222	23	4.02	4.02	10.05	10.05	-6.18	-89.9
43	12	-10862	-548	1204	0	-421	-397	4.02	4.02	10.05	10.05	-8.78	-113.6
44	12	-8446	739	740	0	-270	441	4.02	4.02	10.05	10.05	-8.03	-100.4
45	12	-9229	77	-2	0	-16	15	4.02	4.02	10.05	10.05	-4.88	-73.0
46	12	-9168	68	635	0	-226	14	4.02	4.02	10.05	10.05	-5.88	-85.4
47	12	-8979	59	525	0	-187	12	4.02	4.02	10.05	10.05	-5.59	-81.5
49	12	-9262	-67	606	0	-214	-71	4.02	4.02	10.05	10.05	-5.87	-85.4
50	12	-8778	190	513	0	-184	96	4.02	4.02	10.05	10.05	-5.47	-79.8
51	12	-8935	58	364	0	-133	11	4.02	4.02	10.05	10.05	-5.30	-77.9

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	25	-10715	-273	1319	0	-630	-259	4.02	4.02	10.05	10.05	-8.65	-122.0
41	25	-9864	105	1077	0	-518	38	4.02	4.02	10.05	10.05	-7.66	-108.6
42	25	-9732	102	595	0	-296	36	4.02	4.02	10.05	10.05	-6.51	-94.0
43	25	-10805	-548	1204	0	-572	-466	4.02	4.02	10.05	10.05	-9.37	-119.4
44	25	-8390	739	740	0	-363	534	4.02	4.02	10.05	10.05	-8.92	-108.9
45	25	-9172	77	-2	0	-16	25	4.02	4.02	10.05	10.05	-4.85	-72.6
46	25	-9112	68	635	0	-306	23	4.02	4.02	10.05	10.05	-6.23	-89.8
47	25	-8922	59	525	0	-253	19	4.02	4.02	10.05	10.05	-5.88	-85.1
49	25	-9206	-67	606	0	-290	-80	4.02	4.02	10.05	10.05	-6.21	-89.6
50	25	-8722	190	513	0	-248	120	4.02	4.02	10.05	10.05	-5.75	-83.3
51	25	-8878	58	364	0	-179	18	4.02	4.02	10.05	10.05	-5.49	-80.2

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	38	-10658	-273	1319	0	-794	-293	4.02	4.02	10.05	10.05	-9.42	-131.6
41	38	-9808	105	1077	0	-652	51	4.02	4.02	10.05	10.05	-8.29	-116.4
42	38	-9675	102	595	0	-370	48	4.02	4.02	10.05	10.05	-6.84	-98.1
43	38	-10748	-548	1204	0	-722	-534	4.02	4.02	10.05	10.05	-9.97	-127.9
44	38	-8333	739	740	0	-455	626	4.02	4.02	10.05	10.05	-9.96	-118.4
45	38	-9116	77	-2	0	-15	34	4.02	4.02	10.05	10.05	-4.82	-72.1
46	38	-9055	68	635	0	-385	31	4.02	4.02	10.05	10.05	-6.59	-94.2
47	38	-8866	59	525	0	-318	26	4.02	4.02	10.05	10.05	-6.17	-88.7
49	38	-9149	-67	606	0	-366	-88	4.02	4.02	10.05	10.05	-6.55	-93.7
50	38	-8665	190	513	0	-312	144	4.02	4.02	10.05	10.05	-6.04	-86.7
51	38	-8822	58	364	0	-224	26	4.02	4.02	10.05	10.05	-5.69	-82.6

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	50	-10600	-273	1319	0	-959	-327	4.02	4.02	10.05	10.05	-10.19	-141.2
41	50	-9752	105	1077	0	-787	64	4.02	4.02	10.05	10.05	-8.91	-124.1
42	50	-9619	102	595	0	-445	61	4.02	4.02	10.05	10.05	-7.18	-102.2
43	50	-10690	-548	1204	0	-872	-603	4.02	4.02	10.05	10.05	-10.57	-136.7
44	50	-8277	739	740	0	-548	719	4.02	4.02	10.05	10.05	-11.15	-128.6
45	50	-9060	77	-2	0	-15	44	4.02	4.02	10.05	10.05	-4.79	-71.7
46	50	-8999	68	635	0	-465	40	4.02	4.02	10.05	10.05	-6.95	-98.6
47	50	-8810	59	525	0	-384	34	4.02	4.02	10.05	10.05	-6.46	-92.2
49	50	-9093	-67	606	0	-442	-97	4.02	4.02	10.05	10.05	-6.89	-97.9
50	50	-8609	190	513	0	-377	168	4.02	4.02	10.05	10.05	-6.32	-90.2
51	50	-8766	58	364	0	-270	33	4.02	4.02	10.05	10.05	-5.88	-84.9

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

ASTA NUM. 122 NI 805 NF 830 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 24
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	0	-3499	-21	597	0	-89	-33	4.02	4.02	10.05	10.05	-2.25	-32.7
41	0	-3458	24	493	0	-72	20	4.02	4.02	10.05	10.05	-2.15	-31.4
42	0	-3445	24	268	0	-47	21	4.02	4.02	10.05	10.05	-2.02	-29.8
43	0	-3417	-53	560	0	-89	-72	4.02	4.02	10.05	10.05	-2.28	-32.1
44	0	-3309	99	340	0	-46	111	4.02	4.02	10.05	10.05	-2.58	-33.7
45	0	-3327	22	12	0	-20	18	4.02	4.02	10.05	10.05	-1.83	-27.2
46	0	-3284	20	322	0	-56	15	4.02	4.02	10.05	10.05	-1.98	-29.1
47	0	-3240	19	279	0	-52	14	4.02	4.02	10.05	10.05	-1.94	-28.5
49	0	-3254	4	314	0	-57	-4	4.02	4.02	10.05	10.05	-1.97	-28.9
50	0	-3232	34	270	0	-49	33	4.02	4.02	10.05	10.05	-1.92	-28.2
51	0	-3236	19	204	0	-43	14	4.02	4.02	10.05	10.05	-1.90	-27.9

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	12	-3443	-21	597	0	-163	-36	4.02	4.02	10.05	10.05	-2.59	-36.8
41	12	-3402	24	493	0	-134	23	4.02	4.02	10.05	10.05	-2.42	-34.7
42	12	-3389	24	268	0	-81	24	4.02	4.02	10.05	10.05	-2.16	-31.4
43	12	-3361	-53	560	0	-159	-79	4.02	4.02	10.05	10.05	-2.53	-36.0
44	12	-3253	99	340	0	-89	123	4.02	4.02	10.05	10.05	-2.66	-34.4
45	12	-3271	22	12	0	-22	20	4.02	4.02	10.05	10.05	-1.81	-26.9
46	12	-3228	20	322	0	-96	18	4.02	4.02	10.05	10.05	-2.15	-31.1
47	12	-3184	19	279	0	-87	16	4.02	4.02	10.05	10.05	-2.08	-30.1
49	12	-3198	4	314	0	-96	-3	4.02	4.02	10.05	10.05	-2.14	-30.9
50	12	-3176	34	270	0	-82	37	4.02	4.02	10.05	10.05	-2.05	-29.8
51	12	-3180	19	204	0	-69	17	4.02	4.02	10.05	10.05	-1.99	-29.0

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	25	-3386	-21	597	0	-238	-39	4.02	4.02	10.05	10.05	-2.92	-41.0
41	25	-3346	24	493	0	-196	26	4.02	4.02	10.05	10.05	-2.70	-38.0
42	25	-3332	24	268	0	-114	27	4.02	4.02	10.05	10.05	-2.29	-33.0
43	25	-3304	-53	560	0	-229	-86	4.02	4.02	10.05	10.05	-2.84	-39.8
44	25	-3196	99	340	0	-131	135	4.02	4.02	10.05	10.05	-2.75	-35.1
45	25	-3214	22	12	0	-23	23	4.02	4.02	10.05	10.05	-1.79	-26.5
46	25	-3172	20	322	0	-136	20	4.02	4.02	10.05	10.05	-2.32	-33.1
47	25	-3128	19	279	0	-122	19	4.02	4.02	10.05	10.05	-2.22	-31.8
49	25	-3142	4	314	0	-136	-3	4.02	4.02	10.05	10.05	-2.30	-32.8
50	25	-3120	34	270	0	-116	41	4.02	4.02	10.05	10.05	-2.19	-31.4
51	25	-3124	19	204	0	-94	19	4.02	4.02	10.05	10.05	-2.09	-30.2

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	38	-3330	-21	597	0	-313	-41	4.02	4.02	10.05	10.05	-3.26	-45.1
41	38	-3289	24	493	0	-257	29	4.02	4.02	10.05	10.05	-2.97	-41.4
42	38	-3276	24	268	0	-148	30	4.02	4.02	10.05	10.05	-2.43	-34.6
43	38	-3248	-53	560	0	-299	-92	4.02	4.02	10.05	10.05	-3.15	-43.6
44	38	-3140	99	340	0	-174	148	4.02	4.02	10.05	10.05	-2.84	-35.8
45	38	-3158	22	12	0	-25	26	4.02	4.02	10.05	10.05	-1.76	-26.2
46	38	-3115	20	322	0	-177	23	4.02	4.02	10.05	10.05	-2.48	-35.1
47	38	-3071	19	279	0	-156	21	4.02	4.02	10.05	10.05	-2.36	-33.5
49	38	-3085	4	314	0	-175	-2	4.02	4.02	10.05	10.05	-2.46	-34.8
50	38	-3063	34	270	0	-150	46	4.02	4.02	10.05	10.05	-2.33	-33.1
51	38	-3067	19	204	0	-120	21	4.02	4.02	10.05	10.05	-2.18	-31.3

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	50	-3274	-21	597	0	-387	-44	4.02	4.02	10.05	10.05	-3.60	-49.3
41	50	-3233	24	493	0	-319	32	4.02	4.02	10.05	10.05	-3.24	-44.7
42	50	-3220	24	268	0	-181	33	4.02	4.02	10.05	10.05	-2.56	-36.2
43	50	-3192	-53	560	0	-369	-99	4.02	4.02	10.05	10.05	-3.47	-47.5
44	50	-3084	99	340	0	-216	160	4.02	4.02	10.05	10.05	-2.92	-37.3
45	50	-3102	22	12	0	-26	28	4.02	4.02	10.05	10.05	-1.74	-25.8
46	50	-3059	20	322	0	-217	25	4.02	4.02	10.05	10.05	-2.65	-37.1
47	50	-3015	19	279	0	-191	23	4.02	4.02	10.05	10.05	-2.50	-35.2
49	50	-3029	4	314	0	-214	-2	4.02	4.02	10.05	10.05	-2.62	-36.7
50	50	-3007	34	270	0	-184	50	4.02	4.02	10.05	10.05	-2.46	-34.7
51	50	-3011	19	204	0	-146	24	4.02	4.02	10.05	10.05	-2.28	-32.4

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

ASTA NUM. 123 NI 830 NF 122 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 24A
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-5139	-81	1702	0	-387	-36	4.02	4.02	10.05	10.05	-4.56	-63.7
41	0	-5099	86	1400	0	-319	28	4.02	4.02	10.05	10.05	-4.21	-59.2
42	0	-5084	86	813	0	-181	29	4.02	4.02	10.05	10.05	-3.53	-50.8
43	0	-4998	-202	1634	0	-369	-83	4.02	4.02	10.05	10.05	-4.40	-61.5
44	0	-4898	365	945	0	-216	137	4.02	4.02	10.05	10.05	-3.61	-51.4
45	0	-4907	76	153	0	-26	25	4.02	4.02	10.05	10.05	-2.68	-39.9
46	0	-4832	69	970	0	-217	22	4.02	4.02	10.05	10.05	-3.57	-51.0
47	0	-4765	65	862	0	-191	21	4.02	4.02	10.05	10.05	-3.41	-48.9
49	0	-4778	10	963	0	-214	-1	4.02	4.02	10.05	10.05	-3.53	-50.4
50	0	-4758	123	825	0	-184	43	4.02	4.02	10.05	10.05	-3.37	-48.3
51	0	-4760	65	667	0	-146	21	4.02	4.02	10.05	10.05	-3.19	-46.0
apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)													
40	12	-5083	-81	1702	0	-600	-47	4.02	4.02	10.05	10.05	-5.58	-76.4
41	12	-5043	86	1400	0	-494	39	4.02	4.02	10.05	10.05	-5.03	-69.5
42	12	-5028	86	813	0	-283	40	4.02	4.02	10.05	10.05	-4.00	-56.5
43	12	-4942	-202	1634	0	-574	-109	4.02	4.02	10.05	10.05	-5.38	-73.7
44	12	-4842	365	945	0	-335	183	4.02	4.02	10.05	10.05	-4.15	-58.2
45	12	-4851	76	153	0	-45	35	4.02	4.02	10.05	10.05	-2.75	-40.6
46	12	-4776	69	970	0	-338	31	4.02	4.02	10.05	10.05	-4.13	-57.9
47	12	-4709	65	862	0	-299	29	4.02	4.02	10.05	10.05	-3.91	-55.0
49	12	-4722	10	963	0	-335	0	4.02	4.02	10.05	10.05	-4.09	-57.3
50	12	-4702	123	825	0	-287	59	4.02	4.02	10.05	10.05	-3.85	-54.2
51	12	-4704	65	667	0	-229	29	4.02	4.02	10.05	10.05	-3.57	-50.7
apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)													
40	25	-5026	-81	1702	0	-813	-57	4.02	4.02	10.05	10.05	-6.90	-92.3
41	25	-4986	86	1400	0	-669	50	4.02	4.02	10.05	10.05	-5.93	-80.5
42	25	-4972	86	813	0	-385	50	4.02	4.02	10.05	10.05	-4.46	-62.3
43	25	-4886	-202	1634	0	-778	-134	4.02	4.02	10.05	10.05	-6.63	-88.7
44	25	-4786	365	945	0	-453	228	4.02	4.02	10.05	10.05	-4.70	-65.0
45	25	-4794	76	153	0	-64	44	4.02	4.02	10.05	10.05	-2.81	-41.4
46	25	-4720	69	970	0	-459	40	4.02	4.02	10.05	10.05	-4.70	-64.9
47	25	-4652	65	862	0	-407	37	4.02	4.02	10.05	10.05	-4.41	-61.1
49	25	-4666	10	963	0	-455	2	4.02	4.02	10.05	10.05	-4.65	-64.2
50	25	-4646	123	825	0	-390	74	4.02	4.02	10.05	10.05	-4.32	-60.0
51	25	-4648	65	667	0	-312	37	4.02	4.02	10.05	10.05	-3.94	-55.3
apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)													
40	38	-4970	-81	1702	0	-1025	-67	4.02	4.02	10.05	10.05	-8.66	-112.3
41	38	-4930	86	1400	0	-844	61	4.02	4.02	10.05	10.05	-7.13	-94.6
42	38	-4915	86	813	0	-486	61	4.02	4.02	10.05	10.05	-4.93	-68.0
43	38	-4829	-202	1634	0	-983	-159	4.02	4.02	10.05	10.05	-8.29	-107.7
44	38	-4729	365	945	0	-571	274	4.02	4.02	10.05	10.05	-5.26	-71.9
45	38	-4738	76	153	0	-83	54	4.02	4.02	10.05	10.05	-2.87	-42.1
46	38	-4663	69	970	0	-581	48	4.02	4.02	10.05	10.05	-5.29	-72.1
47	38	-4596	65	862	0	-515	45	4.02	4.02	10.05	10.05	-4.91	-67.3
49	38	-4609	10	963	0	-575	3	4.02	4.02	10.05	10.05	-5.24	-71.4
50	38	-4589	123	825	0	-493	89	4.02	4.02	10.05	10.05	-4.79	-65.9
51	38	-4591	65	667	0	-396	45	4.02	4.02	10.05	10.05	-4.32	-60.0
apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)													
40	50	-4914	-81	1702	0	-1238	-77	4.02	4.02	10.05	10.05	-10.73	-134.5
41	50	-4874	86	1400	0	-1019	71	4.02	4.02	10.05	10.05	-8.62	-111.5
42	50	-4859	86	813	0	-588	72	4.02	4.02	10.05	10.05	-5.41	-74.0
43	50	-4773	-202	1634	0	-1187	-185	4.02	4.02	10.05	10.05	-10.26	-129.0
44	50	-4673	365	945	0	-689	320	4.02	4.02	10.05	10.05	-5.95	-80.2
45	50	-4682	76	153	0	-102	63	4.02	4.02	10.05	10.05	-2.94	-42.8
46	50	-4607	69	970	0	-702	57	4.02	4.02	10.05	10.05	-6.02	-80.9
47	50	-4540	65	862	0	-623	53	4.02	4.02	10.05	10.05	-5.49	-74.3
49	50	-4553	10	963	0	-696	4	4.02	4.02	10.05	10.05	-5.97	-80.2
50	50	-4533	123	825	0	-596	105	4.02	4.02	10.05	10.05	-5.32	-72.4
51	50	-4535	65	667	0	-479	53	4.02	4.02	10.05	10.05	-4.70	-64.6
apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)													

ASTA NUM. 124 NI 806 NF 833 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 23
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-3358	-217	689	0	-233	53	4.02	4.02	10.05	10.05	-2.89	-40.4
41	0	-3215	-153	638	0	-209	32	4.02	4.02	10.05	10.05	-2.69	-37.9
42	0	-3031	-152	475	0	-164	33	4.02	4.02	10.05	10.05	-2.38	-33.6
43	0	-3329	-256	641	0	-228	65	4.02	4.02	10.05	10.05	-2.85	-39.9
44	0	-2930	-44	555	0	-167	-2	4.02	4.02	10.05	10.05	-2.34	-33.1
45	0	-2784	-149	285	0	-112	32	4.02	4.02	10.05	10.05	-2.00	-28.6
46	0	-3015	-148	506	0	-176	30	4.02	4.02	10.05	10.05	-2.43	-34.2
47	0	-2965	-147	474	0	-167	30	4.02	4.02	10.05	10.05	-2.36	-33.3
49	0	-3013	-169	491	0	-175	37	4.02	4.02	10.05	10.05	-2.42	-34.2
50	0	-2933	-126	474	0	-163	23	4.02	4.02	10.05	10.05	-2.32	-32.8
51	0	-2904	-147	419	0	-152	30	4.02	4.02	10.05	10.05	-2.25	-31.9
apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)													
40	12	-3302	-217	689	0	-320	26	4.02	4.02	10.05	10.05	-3.28	-45.3
41	12	-3159	-153	638	0	-289	13	4.02	4.02	10.05	10.05	-3.05	-42.3
42	12	-2975	-152	475	0	-223	14	4.02	4.02	10.05	10.05	-2.64	-36.8

43	12	-3273	-256	641	0	-308	33	4.02	4.02	10.05	10.05	-3.21	-44.3
44	12	-2874	-44	555	0	-236	-7	4.02	4.02	10.05	10.05	-2.65	-36.8
45	12	-2728	-149	285	0	-147	13	4.02	4.02	10.05	10.05	-2.14	-30.3
46	12	-2959	-148	506	0	-239	12	4.02	4.02	10.05	10.05	-2.70	-37.7
47	12	-2909	-147	474	0	-226	11	4.02	4.02	10.05	10.05	-2.62	-36.5
49	12	-2957	-169	491	0	-236	15	4.02	4.02	10.05	10.05	-2.69	-37.5
50	12	-2877	-126	474	0	-222	7	4.02	4.02	10.05	10.05	-2.58	-36.0
51	12	-2848	-147	419	0	-204	12	4.02	4.02	10.05	10.05	-2.48	-34.7

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	25	-3246	-217	689	0	-406	-2	4.02	4.02	10.05	10.05	-3.69	-50.3
41	25	-3102	-153	638	0	-369	-6	4.02	4.02	10.05	10.05	-3.42	-46.8
42	25	-2918	-152	475	0	-282	-5	4.02	4.02	10.05	10.05	-2.90	-40.0
43	25	-3216	-256	641	0	-388	1	4.02	4.02	10.05	10.05	-3.58	-48.9
44	25	-2818	-44	555	0	-306	-13	4.02	4.02	10.05	10.05	-2.96	-40.6
45	25	-2672	-149	285	0	-183	-5	4.02	4.02	10.05	10.05	-2.28	-32.0
46	25	-2902	-148	506	0	-302	-7	4.02	4.02	10.05	10.05	-2.98	-41.1
47	25	-2852	-147	474	0	-286	-7	4.02	4.02	10.05	10.05	-2.88	-39.7
49	25	-2900	-169	491	0	-298	-6	4.02	4.02	10.05	10.05	-2.96	-40.8
50	25	-2820	-126	474	0	-281	-8	4.02	4.02	10.05	10.05	-2.84	-39.2
51	25	-2792	-147	419	0	-257	-7	4.02	4.02	10.05	10.05	-2.70	-37.4

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	38	-3189	-217	689	0	-492	-29	4.02	4.02	10.05	10.05	-4.21	-56.5
41	38	-3046	-153	638	0	-449	-25	4.02	4.02	10.05	10.05	-3.88	-52.3
42	38	-2862	-152	475	0	-342	-24	4.02	4.02	10.05	10.05	-3.17	-43.3
43	38	-3160	-256	641	0	-469	-31	4.02	4.02	10.05	10.05	-4.04	-54.5
44	38	-2761	-44	555	0	-375	-18	4.02	4.02	10.05	10.05	-3.31	-45.0
45	38	-2615	-149	285	0	-219	-24	4.02	4.02	10.05	10.05	-2.43	-33.7
46	38	-2846	-148	506	0	-365	-25	4.02	4.02	10.05	10.05	-3.29	-44.8
47	38	-2796	-147	474	0	-345	-25	4.02	4.02	10.05	10.05	-3.15	-43.0
49	38	-2844	-169	491	0	-359	-27	4.02	4.02	10.05	10.05	-3.25	-44.3
50	38	-2764	-126	474	0	-340	-24	4.02	4.02	10.05	10.05	-3.11	-42.5
51	38	-2735	-147	419	0	-309	-25	4.02	4.02	10.05	10.05	-2.93	-40.2

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	50	-3133	-217	689	0	-578	-56	4.02	4.02	10.05	10.05	-4.86	-64.0
41	50	-2990	-153	638	0	-528	-44	4.02	4.02	10.05	10.05	-4.45	-58.9
42	50	-2806	-152	475	0	-401	-43	4.02	4.02	10.05	10.05	-3.49	-47.2
43	50	-3104	-256	641	0	-549	-63	4.02	4.02	10.05	10.05	-4.62	-61.2
44	50	-2705	-44	555	0	-445	-24	4.02	4.02	10.05	10.05	-3.77	-50.3
45	50	-2559	-149	285	0	-254	-42	4.02	4.02	10.05	10.05	-2.57	-35.5
46	50	-2790	-148	506	0	-429	-44	4.02	4.02	10.05	10.05	-3.67	-49.3
47	50	-2740	-147	474	0	-404	-44	4.02	4.02	10.05	10.05	-3.49	-47.0
49	50	-2788	-169	491	0	-420	-48	4.02	4.02	10.05	10.05	-3.62	-48.6
50	50	-2708	-126	474	0	-400	-40	4.02	4.02	10.05	10.05	-3.45	-46.5
51	50	-2679	-147	419	0	-362	-44	4.02	4.02	10.05	10.05	-3.20	-43.4

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

ASTA NUM. 125 NI 833 NF 209 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 23A
armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-4201	-42	1041	0	-679	-78	4.02	4.02	10.05	10.05	-5.77	-77.1
41	0	-4041	79	922	0	-612	-57	4.02	4.02	10.05	10.05	-5.26	-70.7
42	0	-3880	64	617	0	-461	-57	4.02	4.02	10.05	10.05	-4.28	-58.5
43	0	-4167	-136	977	0	-649	-91	4.02	4.02	10.05	10.05	-5.55	-74.4
44	0	-3707	280	730	0	-500	-21	4.02	4.02	10.05	10.05	-4.42	-60.0
45	0	-3632	40	272	0	-287	-56	4.02	4.02	10.05	10.05	-3.29	-45.8
46	0	-3815	57	693	0	-493	-55	4.02	4.02	10.05	10.05	-4.43	-60.2
47	0	-3759	52	636	0	-463	-54	4.02	4.02	10.05	10.05	-4.23	-57.8
49	0	-3812	11	676	0	-485	-61	4.02	4.02	10.05	10.05	-4.38	-59.7
50	0	-3721	95	626	0	-455	-48	4.02	4.02	10.05	10.05	-4.18	-57.0
51	0	-3706	46	534	0	-413	-55	4.02	4.02	10.05	10.05	-3.94	-54.1

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	12	-4145	-42	1041	0	-809	-83	4.02	4.02	10.05	10.05	-6.81	-89.0
41	12	-3985	79	922	0	-727	-47	4.02	4.02	10.05	10.05	-6.12	-80.6
42	12	-3824	64	617	0	-539	-49	4.02	4.02	10.05	10.05	-4.71	-63.7
43	12	-4111	-136	977	0	-771	-108	4.02	4.02	10.05	10.05	-6.49	-85.2
44	12	-3651	280	730	0	-591	14	4.02	4.02	10.05	10.05	-5.02	-67.0
45	12	-3576	40	272	0	-321	-52	4.02	4.02	10.05	10.05	-3.43	-47.5
46	12	-3759	57	693	0	-579	-48	4.02	4.02	10.05	10.05	-4.96	-66.6
47	12	-3703	52	636	0	-542	-48	4.02	4.02	10.05	10.05	-4.69	-63.3
49	12	-3756	11	676	0	-570	-60	4.02	4.02	10.05	10.05	-4.89	-65.8
50	12	-3665	95	626	0	-534	-36	4.02	4.02	10.05	10.05	-4.63	-62.4
51	12	-3650	46	534	0	-480	-49	4.02	4.02	10.05	10.05	-4.28	-58.2

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	25	-4088	-42	1041	0	-939	-88	4.02	4.02	10.05	10.05	-8.03	-102.2
41	25	-3928	79	922	0	-842	-37	4.02	4.02	10.05	10.05	-7.14	-92.0
42	25	-3768	64	617	0	-616	-41	4.02	4.02	10.05	10.05	-5.22	-69.7
43	25	-4054	-136	977	0	-894	-125	4.02	4.02	10.05	10.05	-7.60	-97.5
44	25	-3594	280	730	0	-682	49	4.02	4.02	10.05	10.05	-5.74	-75.3
45	25	-3520	40	272	0	-355	-47	4.02	4.02	10.05	10.05	-3.56	-49.1
46	25	-3702	57	693	0	-666	-41	4.02	4.02	10.05	10.05	-5.61	-74.0
47	25	-3646	52	636	0	-622	-42	4.02	4.02	10.05	10.05	-5.25	-69.8
49	25	-3700	11	676	0	-654	-59	4.02	4.02	10.05	10.05	-5.51	-72.9
50	25	-3608	95	626	0	-612	-24	4.02	4.02	10.05	10.05	-5.17	-68.7
51	25	-3594	46	534	0	-546	-43	4.02	4.02	10.05	10.05	-4.69	-63.0

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	38	-4032	-42	1041	0	-1069	-93	4.02	4.02	10.05	10.05	-9.34	125.1
41	38	-3872	79	922	0	-958	-27	4.02	4.02	10.05	10.05	-8.27	-104.1
42	38	-3711	64	617	0	-693	-33	4.02	4.02	10.05	10.05	-5.83	-76.6
43	38	-3998	-136	977	0	-1016	-142	4.02	4.02	10.05	10.05	-8.81	-110.3

44	38	-3538	280	730	0	-773	84	4.02	4.02	10.05	10.05	-6.57	-84.4
45	38	-3463	40	272	0	-389	-42	4.02	4.02	10.05	10.05	-3.70	-50.8
46	38	-3646	57	693	0	-753	-33	4.02	4.02	10.05	10.05	-6.36	-82.4
47	38	-3590	52	636	0	-701	-35	4.02	4.02	10.05	10.05	-5.91	-77.2
49	38	-3643	11	676	0	-739	-57	4.02	4.02	10.05	10.05	-6.23	-81.0
50	38	-3552	95	626	0	-690	-12	4.02	4.02	10.05	10.05	-5.81	-76.0
51	38	-3537	46	534	0	-613	-37	4.02	4.02	10.05	10.05	-5.17	-68.6

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

40	50	-3976	-42	1041	0	-1199	-99	4.02	4.02	10.05	10.05	-10.68	178.3
41	50	-3816	79	922	0	-1073	-17	4.02	4.02	10.05	10.05	-9.46	140.9
42	50	-3655	64	617	0	-770	-25	4.02	4.02	10.05	10.05	-6.52	-84.2
43	50	-3942	-136	977	0	-1138	-159	4.02	4.02	10.05	10.05	-10.07	156.9
44	50	-3482	280	730	0	-864	119	4.02	4.02	10.05	10.05	-7.47	-93.9
45	50	-3407	40	272	0	-423	-37	4.02	4.02	10.05	10.05	-3.85	-52.6
46	50	-3590	57	693	0	-839	-26	4.02	4.02	10.05	10.05	-7.19	-91.3
47	50	-3534	52	636	0	-781	-29	4.02	4.02	10.05	10.05	-6.64	-85.2
49	50	-3587	11	676	0	-823	-56	4.02	4.02	10.05	10.05	-7.03	-89.6
50	50	-3496	95	626	0	-768	-0	4.02	4.02	10.05	10.05	-6.53	-83.8
51	50	-3481	46	534	0	-680	-31	4.02	4.02	10.05	10.05	-5.73	-74.8

apost= -- aant= -- ainf= 6.03 asup= 6.03 (e arm. base= 4 X 2.01)

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Lavoro: **D2403a** Intestazione lavoro: **Palestra Campobello**
Elemento: **PILASTRO** Gruppo: **2** Tabella: **Tabella pilastri**
Descrizione: **Pilastri**
Rck: **350.00** daN/cm^2 fyk: **4580.0** daN/cm^2 Copriferro di calcolo: **5.0** cm Copriferro di disegno: **4.0** cm
Verifica in ottemperanza alle NTC2018
Per le combinazioni sismiche la capacità è valutata in campo elastico o sostanzialmente elastico(§7.4.1 NTC2018)
Diametro staffe: **8** mm Numero braccia: **2**
ρ min.: **1.000** % Passo max. armatura longitudinale: **50.0** cm
Progettazione in capacità (NTC 2018): **Limitazione della domanda di resistenza al caso NON dissipativo**

ASTA NUM. 1 NI 32 NF 26 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 32C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-272	1215	608	0	1306	-1491	6.28	6.28	9.42	9.42	3	0.18	0.03	0.15	0.00	0.00	24.0
2	0	-380	933	409	0	950	-1129	6.28	6.28	9.42	9.42	2	0.18	0.02	0.12	0.00	0.00	24.0
3	0	-395	940	424	0	1010	-1136	6.28	6.28	9.42	9.42	2	0.18	0.02	0.12	0.00	0.00	24.0
4	0	-23	928	512	0	1000	-1157	6.28	6.28	9.42	9.42	2	0.18	0.02	0.12	0.00	0.00	24.0
5	0	-38	935	527	0	1060	-1165	6.28	6.28	9.42	9.42	2	0.19	0.02	0.12	0.00	0.00	24.0
6	0	-238	923	428	0	896	-1130	6.28	6.28	9.42	9.42	2	0.17	0.02	0.12	0.00	0.00	24.0
7	0	-287	947	477	0	1099	-1155	6.28	6.28	9.42	9.42	2	0.19	0.02	0.12	0.00	0.00	24.0
8	0	-131	922	459	0	911	-1138	6.28	6.28	9.42	9.42	2	0.18	0.02	0.12	0.00	0.00	24.0
9	0	-180	945	508	0	1114	-1164	6.28	6.28	9.42	9.42	2	0.19	0.02	0.12	0.00	0.00	24.0
10	0	-380	933	409	0	950	-1129	6.28	6.28	9.42	9.42	2	0.18	0.02	0.12	0.00	0.00	24.0
11	0	-395	940	424	0	1010	-1136	6.28	6.28	9.42	9.42	2	0.18	0.02	0.12	0.00	0.00	24.0
12	0	-23	928	512	0	1000	-1157	6.28	6.28	9.42	9.42	2	0.18	0.02	0.12	0.00	0.00	24.0
13	0	-38	935	527	0	1060	-1165	6.28	6.28	9.42	9.42	2	0.19	0.02	0.12	0.00	0.00	24.0
14	0	-238	923	428	0	896	-1130	6.28	6.28	9.42	9.42	2	0.17	0.02	0.12	0.00	0.00	24.0
15	0	-287	947	477	0	1099	-1155	6.28	6.28	9.42	9.42	2	0.19	0.02	0.12	0.00	0.00	24.0
16	0	-131	922	459	0	911	-1138	6.28	6.28	9.42	9.42	2	0.18	0.02	0.12	0.00	0.00	24.0
17	0	-180	945	508	0	1114	-1164	6.28	6.28	9.42	9.42	2	0.19	0.02	0.12	0.00	0.00	24.0
18	0	-1795	1326	183	0	1102	-1248	6.28	6.28	9.42	9.42	3	0.15	0.03	0.16	0.00	0.00	24.0
19	0	-1253	1132	802	0	1413	-1497	6.28	6.28	9.42	9.42	3	0.18	0.03	0.14	0.00	0.00	24.0
20	0	-703	1257	1065	0	1559	-1411	6.28	6.28	9.42	9.42	3	0.17	0.03	0.15	0.00	0.00	24.0
37	0	-1584	1388	15	0	1014	-1205	6.28	6.28	9.42	9.42	3	0.14	0.04	0.17	0.00	0.00	24.0
38	0	-681	1065	1046	0	1533	-1621	6.28	6.28	9.42	9.42	3	0.19	0.03	0.14	0.00	0.00	24.0
39	0	237	1273	1485	0	1776	-1478	6.28	6.28	9.42	9.42	3	0.18	0.04	0.21	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	83	211	1215	608	0	804	-489	6.28	6.28	9.42	9.42	3	0.06	0.03	0.13	0.00	0.00	24.0
2	83	-9	933	409	0	612	-359	6.28	6.28	9.42	9.42	2	0.07	0.02	0.10	0.00	0.00	24.0
3	83	-23	940	424	0	661	-360	6.28	6.28	9.42	9.42	2	0.07	0.02	0.10	0.00	0.00	24.0
4	83	348	928	512	0	577	-391	6.28	6.28	9.42	9.42	2	0.07	0.02	0.10	0.00	0.00	24.0
5	83	333	935	527	0	625	-393	6.28	6.28	9.42	9.42	2	0.08	0.02	0.10	0.00	0.00	24.0
6	83	133	923	428	0	543	-368	6.28	6.28	9.42	9.42	2	0.07	0.02	0.10	0.00	0.00	24.0
7	83	85	947	477	0	706	-374	6.28	6.28	9.42	9.42	2	0.08	0.02	0.10	0.00	0.00	24.0
8	83	240	922	459	0	532	-378	6.28	6.28	9.42	9.42	2	0.07	0.02	0.10	0.00	0.00	24.0
9	83	192	945	508	0	695	-384	6.28	6.28	9.42	9.42	2	0.08	0.02	0.10	0.00	0.00	24.0
10	83	-9	933	409	0	612	-359	6.28	6.28	9.42	9.42	2	0.07	0.02	0.10	0.00	0.00	24.0
11	83	-23	940	424	0	661	-360	6.28	6.28	9.42	9.42	2	0.07	0.02	0.10	0.00	0.00	24.0
12	83	348	928	512	0	577	-391	6.28	6.28	9.42	9.42	2	0.07	0.02	0.10	0.00	0.00	24.0
13	83	333	935	527	0	625	-393	6.28	6.28	9.42	9.42	2	0.08	0.02	0.10	0.00	0.00	24.0
14	83	133	923	428	0	543	-368	6.28	6.28	9.42	9.42	2	0.07	0.02	0.10	0.00	0.00	24.0
15	83	85	947	477	0	706	-374	6.28	6.28	9.42	9.42	2	0.08	0.02	0.10	0.00	0.00	24.0
16	83	240	922	459	0	532	-378	6.28	6.28	9.42	9.42	2	0.07	0.02	0.10	0.00	0.00	24.0
17	83	192	945	508	0	695	-384	6.28	6.28	9.42	9.42	2	0.08	0.02	0.10	0.00	0.00	24.0
18	83	-1312	1223	183	0	951	-197	6.28	6.28	9.42	9.42	3	0.05	0.03	0.13	0.00	0.00	24.0
19	83	-770	1235	802	0	752	-520	6.28	6.28	9.42	9.42	3	0.06	0.03	0.13	0.00	0.00	24.0
20	83	-220	1257	837	0	774	-374	6.28	6.28	9.42	9.42	3	0.05	0.03	0.14	0.00	0.00	24.0
37	83	-1101	1216	15	0	1002	-131	6.28	6.28	9.42	9.42	3	0.05	0.03	0.13	0.00	0.00	24.0
38	83	-198	1237	1046	0	670	-672	6.28	6.28	9.42	9.42	3	0.08	0.03	0.16	0.00	0.00	24.0
39	83	719	1273	1104	0	708	-428	6.28	6.28	9.42	9.42	3	0.06	0.03	0.15	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	165	694	1215	608	0	302	513	6.28	6.28	9.42	9.42	3	0.06	0.03	0.15	0.00	0.00	24.0
2	165	362	933	409	0	275	411	6.28	6.28	9.42	9.42	2	0.06	0.02	0.12	0.00	0.00	24.0
3	165	348	940	424	0	311	416	6.28	6.28	9.42	9.42	2	0.06	0.02	0.12	0.00	0.00	24.0
4	165	719	928	512	0	154	374	6.28	6.28	9.42	9.42	2	0.05	0.02	0.12	0.00	0.00	24.0
5	165	705	935	527	0	190	379	6.28	6.28	9.42	9.42	2	0.05	0.02	0.12	0.00	0.00	24.0
6	165	504	923	428	0	190	394	6.28	6.28	9.42	9.42	2	0.06	0.02	0.12	0.00	0.00	24.0
7	165	456	947	477	0	312	407	6.28	6.28	9.42	9.42	2	0.06	0.02	0.12	0.00	0.00	24.0
8	165	611	922	459	0	154	382	6.28	6.28	9.42	9.42	2	0.05	0.02	0.12	0.00	0.00	24.0
9	165	563	945	508	0	276	396	6.28	6.28	9.42	9.42	2	0.06	0.02	0.12	0.00	0.00	24.0
10	165	362	933	409	0	275	411	6.28	6.28	9.42	9.42	2	0.06	0.02	0.12	0.00	0.00	24.0
11	165	348	940	424	0	311	416	6.28	6.28	9.42	9.42	2	0.06	0.02	0.12	0.00	0.00	24.0
12	165	719	928	512	0	154	374	6.28	6.28	9.42	9.42	2	0.05	0.02	0.12	0.00	0.00	24.0
13	165	705	935	527	0	190	379	6.28	6.28	9.42	9.42	2	0.05	0.02	0.12	0.00	0.00	24.0
14	165	504	923	428	0	190	394	6.28	6.28	9.42	9.42	2	0.06	0.02	0.12	0.00	0.00	24.0
15	165	456	947	477	0	312	407	6.28	6.28	9.42	9.42	2	0.06	0.02	0.12	0.00	0.00	24.0
16	165	611	922	459	0	154	382	6.28	6.28	9.42	9.42	2	0.05	0.02	0.12	0.00	0.00	24.0
17	165	563	945	508	0	276	396	6.28	6.28	9.42	9.42	2	0.06	0.02	0.12	0.00	0.00	24.0
18	165	-830	1120	183	0	799	769	6.28	6.28	9.42	9.42	3	0.09	0.03	0.12	0.00	0.00	24.0
19	165	-288	1338	802	0	90	542	6.28	6.28	9.42	9.42	3	0.06	0.03	0.17	0.00	0.00	24.0
20	165	263	1257	608	0	178	663	6.28	6.28	9.42	9.42	3	0.08	0.03	0.16	0.00	0.00	24.0
37	165	-619	1044	15	0	989	800	6.28	6.28	9.42	9.42	3	0.10	0.03	0.11	0.00	0.00	24.0
38	165	285	1409	1046	0	-193	420	6.28	6.28	9.42	9.42	3	0.05	0.04	0.18	0.00	0.00	24.0
39	165	1202	1273	723	0	-46	623	6.28	6.28	9.42	9.42	3	0.07	0.03	0.16	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	248	1176	1215	608	0	-199	1516	6.28	6.28	9.42	9.42	3	0.18	0.03	0.15	0.00	0.00	24.0
2	248	734	933	409	0	-62	1181	6.28	6.28	9.42	9.42	2	0.15	0.02	0.12	0.00	0.00	24.0
3	248	719	940	424	0	-38	1191	6.28	6.28	9.42	9.42	2	0.15	0.02	0.12	0.00	0.00	24.0
4	248	1091	928	512	0	-269	1140	6.28	6.28	9.42	9.42	2	0.15	0.02	0.12	0.00	0.00	24.0
5	248	1076	935	527	0	-244	1150	6.28	6.28	9.42	9.42	2	0.15	0.02	0.12	0.00	0.00	24.0
6	248	876	923	428	0	-163	1155	6.28	6.28	9.42	9.42	2	0.15	0.02	0.12	0.00	0.00	24.0
7	248	827	947	477	0	-81	1189	6.28	6.28	9.42	9.42	2	0.15	0.02	0.12	0.00	0.00	24.0
8	248	983	922	459	0	-225	1143	6.28	6.28	9.42	9.42	2	0.15	0.02	0.12	0.00	0.00	24.0
9	248	934	945	508	0	-143	1176	6.28	6.28	9.42	9.42	2	0.15	0.02	0.12	0.00	0.00	24.0
10	248	734	933	409	0	-62	1181	6.28	6.28	9.42	9.42	2	0.15	0.02	0.12	0.00	0.00	24.0
11	248	719	940	424	0	-38	1191	6.28	6.28	9.42	9.42	2	0.15	0.02	0.12	0.00	0.00	24.0
12	248	1091	928	512	0	-269	1140	6.28	6.28	9.42	9.42	2	0.15	0.02	0.12	0.00	0.00	24.0
13	248	1076	935	527	0	-244	1150	6.28	6.28	9.42	9.42	2	0.15	0.02	0.12	0.00	0.00	24.0
14	248	876	923	428	0	-163	1155	6.28	6.28	9.42	9.42	2	0.15	0.02	0.12	0.00	0.00	24.0
15	248	827	947	477	0	-81	1189	6.28	6.28	9.42	9.42	2	0.15	0.02	0.12	0.00	0.00	24.0
16	248	983	922	459	0	-225	1143	6.28	6.28	9.42	9.42	2	0.15	0.02	0.12	0.00	0.00	24.0
17	248	934	945	508	0	-143	1176	6.28	6.28	9.42	9.42	2	0.15	0.02	0.12	0.00	0.00	24.0
18	248	-347	1016	183	0	648	1650	6.28	6.28	9.42	9.42	3	0.19	0.03	0.13	0.00	0.00	24.0
19	248	195	1442	802	0	-572	1689	6.28	6.28	9.42	9.42	3	0.20	0.04	0.18	0.00	0.00	24.0
20	248	745	1257	380	0	-229	1701	6.28	6.28	9.42	9.42	3	0.20	0.03	0.16	0.00	0.00	24.0
37	248	-136	872	15	0	977	1590	6.28	6.28	9.42	9.42	3	0.19	0.02	0.11	0.00	0.00	24.0
38	248	767	1581	1046	0	-1056	1653	6.28	6.28	9.42	9.42	3	0.20	0.04	0.20	0.00	0.00	24.0
39	248	1684	1273	342	0	-485	1674	6.28	6.28	9.42	9.42	3	0.20	0.03	0.16	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	330	1659	1215	608	0	-701	2518	6.28	6.28	9.42	9.42	3	0.30	0.03	0.15	0.00	0.00	24.0
2	330	1105	933	409	0	-399	1951	6.28	6.28	9.42	9.42	2	0.26	0.02	0.12	0.00	0.00	24.0
3	330	1090	940	424	0	-387	1967	6.28	6.28	9.42	9.42	2	0.26	0.02	0.12	0.00	0.00	24.0
4	330	1462	928	512	0	-692	1906	6.28	6.28	9.42	9.42	2	0.26	0.02	0.12	0.00	0.00	24.0
5	330	1447	935	527	0	-679	1922	6.28	6.28	9.42	9.42	2	0.27	0.02	0.12	0.00	0.00	24.0
6	330	1247	923	428	0	-516	1917	6.28	6.28	9.42	9.42	2	0.26	0.02	0.12	0.00	0.00	24.0
7	330	1198	947	477	0	-475	1970	6.28	6.28	9.42	9.42	2	0.26	0.02	0.12	0.00	0.00	24.0
8	330	1354	922	459	0	-604	1903	6.28	6.28	9.42	9.42	2	0.26	0.02	0.12	0.00	0.00	24.0
9	330	1305	945	508	0	-562	1956	6.28	6.28	9.42	9.42	2	0.27	0.02	0.12	0.00	0.00	24.0
10	330	1105	933	409	0	-399	1951	6.28	6.28	9.42	9.42	2	0.26	0.02	0.12	0.00	0.00	24.0
11	330	1090	940	424	0	-387	1967	6.28	6.28	9.42	9.42	2	0.26	0.02	0.12	0.00	0.00	24.0
12	330	1462	928	512	0	-692	1906	6.28	6.28	9.42	9.42	2	0.26	0.02	0.12	0.00	0.00	24.0
13	330	1447	935	527	0	-679	1922	6.28	6.28	9.42	9.42	2	0.27	0.02	0.12	0.00	0.00	24.0
14	330	1247	923	428	0	-516	1917	6.28	6.28	9.42	9.42	2	0.26	0.02	0.12	0.00	0.00	24.0
15	330	1198	947	477	0	-475	1970	6.28	6.28	9.42	9.42	2	0.26	0.02	0.12	0.00	0.00	24.0
16	330	1354	922	459	0	-604	1903	6.28	6.28	9.42	9.42	2	0.26	0.02	0.12	0.00	0.00	24.0
17	330	1305	945	508	0	-562	1956	6.28	6.28	9.42	9.42	2	0.27	0.02	0.12	0.00	0.00	24.0
18	330	135	913	183	0	497	2446	6.28	6.28	9.42	9.42	3	0.28	0.02	0.11	0.00	0.00	24.0
19	330	677	1545	802	0	-1233	2921	6.28	6.28	9.42	9.42	3	0.34	0.04	0.19	0.00	0.00	24.0
20	330	1228	1257	151	0	-448	2738	6.28	6.28	9.42	9.42	3	0.32	0.03	0.16	0.00	0.00	24.0
37	330	346	700	15	0	965	2238	6.28	6.28	9.42	9.42	3	0.26	0.02	0.09	0.00	0.00	24.0
38	330	1250	1753	1046	0	-1919	3028	6.28	6.28	9.42	9.42	3	0.36	0.05	0.22	0.00	0.00	24.0
39	330	2167	1273	-38	0	-611	2724	6.28	6.28	9.42	9.42	3	0.32	0.03	0.16	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

VERIFICA NODO IN TESTA AL PILASTRO, NODO NUM. 26 NON CONFINATO

(par.7.2.2 NTC2018 "La domanda di resistenza valutata con i criteri della progettazione in capacità può essere assunta non superiore alla domanda di resistenza valutata per il caso di comportamento strutturale non dissipativo.")

PROGETTAZIONE IN CAPACITA'

Asse loc. pilastro y nodo ESTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 45.0 cm, hjc= 20.0 cm
Asse loc. pilastro z nodo ESTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 30.0 cm, hjc= 50.0 cm

FxMin,inf	FxMin,sup	FxMax,sup	FySup	FzSup	Vjbdy	Vjbdz	Vres,y	Vres,z	I.R.compr.	Ashy	Ashz	PASSO	Nota
daN					daN		daN			cmq		cm	
-10000000150474662198766888550 40		1	-0	0	0	17616	17616	63005	105009	0.28	7.07	--	6.63

VERIFICA DI RESISTENZA CON SOLLECITAZIONI COMPORTAMENTO NON DISSIPATIVO

Asse loc. pilastro y nodo ESTERNO: Hjw= 40.0 cm, bj= 45.0 cm, hjc= 20.0 cm, db1= 45.0 cm

NC	Fx,sup	Fx,inf	Mb	Vb	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-0	-0	1091	945	0	2693	63005	0.04	0.00	40.00	
3	-0	-0	1112	939	0	2746	63005	0.04	0.00	40.00	
4	-0	-0	985	973	0	2431	63005	0.04	0.00	40.00	
5	-0	-0	1006	967	0	2484	63005	0.04	0.00	40.00	
6	-0	-0	1029	962	0	2540	63005	0.04	0.00	40.00	
7	-0	-0	1100	941	0	2715	63005	0.04	0.00	40.00	
8	-0	-0	997	971	0	2462	63005	0.04	0.00	40.00	
9	-0	-0	1068	950	0	2636	63005	0.04	0.00	40.00	
10	-0	-0	1091	945	0	2693	63005	0.04	0.00	40.00	
11	-0	-0	1112	939	0	2746	63005	0.04	0.00	40.00	
12	-0	-0	985	973	0	2431	63005	0.04	0.00	40.00	
13	-0	-0	1006	967	0	2484	63005	0.04	0.00	40.00	
14	-0	-0	1029	962	0	2540	63005	0.04	0.00	40.00	
15	-0	-0	1100	941	0	2715	63005	0.04	0.00	40.00	
16	-0	-0	997	971	0	2462	63005	0.04	0.00	40.00	
17	-0	-0	1068	950	0	2636	63005	0.04	0.00	40.00	

Asse loc. pilastro z nodo ESTERNO: Hjw= 40.0 cm, bj= 30.0 cm, hjc= 50.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb	Vb	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-0	-0	-1575	1535	0	3889	105009	0.04	0.00	40.00	
3	-0	-0	-1791	1599	0	4422	105009	0.04	0.00	40.00	
4	-0	-0	-1449	1507	0	3578	105009	0.03	0.00	40.00	
5	-0	-0	-1664	1572	0	4109	105009	0.04	0.00	40.00	
6	-0	-0	-1279	1450	0	3158	105009	0.03	0.00	40.00	
7	-0	-0	-1998	1665	0	4933	105009	0.05	0.00	40.00	
8	-0	-0	-1241	1442	0	3064	105009	0.03	0.00	40.00	
9	-0	-0	-1960	1657	0	4840	105009	0.05	0.00	40.00	
10	-0	-0	-1575	1535	0	3889	105009	0.04	0.00	40.00	
11	-0	-0	-1791	1599	0	4422	105009	0.04	0.00	40.00	

12	-0	-0	-1449	1507	0	3578	105009	0.03	0.00	40.00
13	-0	-0	-1664	1572	0	4109	105009	0.04	0.00	40.00
14	-0	-0	-1279	1450	0	3158	105009	0.03	0.00	40.00
15	-0	-0	-1998	1665	0	4933	105009	0.05	0.00	40.00
16	-0	-0	-1241	1442	0	3064	105009	0.03	0.00	40.00
17	-0	-0	-1960	1657	0	4840	105009	0.05	0.00	40.00

CONFRONTO E SINTESI CONCLUSIVE (si assume in ogni caso passo <= 15 cm)

I.R.compr.	Ashy	Ashz	PASSO	Nota
	cmq		cm	
0.05	--	--	15.00	**VERIFICATO**

ASTA NUM. 2 NI 33 NF 32 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 32B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-7991	73	248	0	157	-122	6.28	6.28	9.42	9.42	3	0.01	0.01	0.03	0.00	0.00	24.0
2	0	-6293	47	162	0	22	-79	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
3	0	-6365	45	230	0	230	-74	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
4	0	-5930	67	151	0	12	-114	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
5	0	-6001	65	219	0	220	-110	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
6	0	-6082	56	79	0	-224	-97	6.28	6.28	9.42	9.42	2	0.02	0.00	0.01	0.00	0.00	24.0
7	0	-6321	50	306	0	469	-81	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
8	0	-5973	62	75	0	-227	-107	6.28	6.28	9.42	9.42	2	0.02	0.00	0.01	0.00	0.00	24.0
9	0	-6212	56	302	0	466	-92	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
10	0	-6293	47	162	0	22	-79	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
11	0	-6365	45	230	0	230	-74	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
12	0	-5930	67	151	0	12	-114	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
13	0	-6001	65	219	0	220	-110	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
14	0	-6082	56	79	0	-224	-97	6.28	6.28	9.42	9.42	2	0.02	0.00	0.01	0.00	0.00	24.0
15	0	-6321	50	306	0	469	-81	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
16	0	-5973	62	75	0	-227	-107	6.28	6.28	9.42	9.42	2	0.02	0.00	0.01	0.00	0.00	24.0
17	0	-6212	56	302	0	466	-92	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
18	0	-9536	213	213	0	-39	-166	6.28	6.28	9.42	9.42	3	0.02	0.01	0.03	0.00	0.00	24.0
19	0	-9072	-229	215	0	73	193	6.28	6.28	9.42	9.42	3	0.02	0.01	0.03	0.00	0.00	24.0
20	0	-8559	-17	946	0	748	41	6.28	6.28	9.42	9.42	3	0.04	0.02	0.11	0.00	0.00	24.0
37	0	-9281	387	224	0	-28	-329	6.28	6.28	9.42	9.42	3	0.03	0.01	0.04	0.00	0.00	24.0
38	0	-8507	-350	228	0	159	268	6.28	6.28	9.42	9.42	3	0.03	0.01	0.04	0.00	0.00	24.0
39	0	-7652	2	1446	0	1285	16	6.28	6.28	9.42	9.42	3	0.06	0.03	0.18	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	110	-7348	73	248	0	-115	-42	6.28	6.28	9.42	9.42	3	0.01	0.01	0.03	0.00	0.00	24.0
2	110	-5798	47	162	0	-156	-27	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
3	110	-5870	45	230	0	-24	-25	6.28	6.28	9.42	9.42	2	0.00	0.01	0.03	0.00	0.00	24.0
4	110	-5435	67	151	0	-153	-41	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
5	110	-5506	65	219	0	-21	-38	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
6	110	-5587	56	79	0	-310	-35	6.28	6.28	9.42	9.42	2	0.02	0.00	0.01	0.00	0.00	24.0
7	110	-5826	50	306	0	132	-26	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
8	110	-5478	62	75	0	-309	-39	6.28	6.28	9.42	9.42	2	0.02	0.00	0.01	0.00	0.00	24.0
9	110	-5717	56	302	0	133	-30	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
10	110	-5798	47	162	0	-156	-27	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
11	110	-5870	45	230	0	-24	-25	6.28	6.28	9.42	9.42	2	0.00	0.01	0.03	0.00	0.00	24.0
12	110	-5435	67	151	0	-153	-41	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
13	110	-5506	65	219	0	-21	-38	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
14	110	-5587	56	79	0	-310	-35	6.28	6.28	9.42	9.42	2	0.02	0.00	0.01	0.00	0.00	24.0
15	110	-5826	50	306	0	132	-26	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
16	110	-5478	62	75	0	-309	-39	6.28	6.28	9.42	9.42	2	0.02	0.00	0.01	0.00	0.00	24.0
17	110	-5717	56	302	0	133	-30	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
18	110	-8892	109	213	0	-273	12	6.28	6.28	9.42	9.42	3	0.01	0.00	0.03	0.00	0.00	24.0
19	110	-8428	-125	215	0	-164	-2	6.28	6.28	9.42	9.42	3	0.01	0.00	0.03	0.00	0.00	24.0
20	110	-7916	-17	641	0	-124	22	6.28	6.28	9.42	9.42	3	0.01	0.01	0.08	0.00	0.00	24.0
37	110	-8638	213	224	0	-274	1	6.28	6.28	9.42	9.42	3	0.01	0.01	0.03	0.00	0.00	24.0
38	110	-7864	-177	228	0	-92	-21	6.28	6.28	9.42	9.42	3	0.00	0.01	0.03	0.00	0.00	24.0
39	110	-7008	2	938	0	-26	19	6.28	6.28	9.42	9.42	3	0.00	0.02	0.12	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	220	-6704	73	248	0	-387	38	6.28	6.28	9.42	9.42	3	0.02	0.01	0.03	0.00	0.00	24.0
2	220	-5303	47	162	0	-334	25	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
3	220	-5375	45	230	0	-277	25	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
4	220	-4940	67	151	0	-319	33	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
5	220	-5011	65	219	0	-261	34	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
6	220	-5092	56	79	0	-397	27	6.28	6.28	9.42	9.42	2	0.03	0.00	0.01	0.00	0.00	24.0
7	220	-5331	50	306	0	-204	28	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
8	220	-4983	62	75	0	-392	30	6.28	6.28	9.42	9.42	2	0.03	0.00	0.01	0.00	0.00	24.0
9	220	-5222	56	302	0	-199	31	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
10	220	-5303	47	162	0	-334	25	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
11	220	-5375	45	230	0	-277	25	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
12	220	-4940	67	151	0	-319	33	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
13	220	-5011	65	219	0	-261	34	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
14	220	-5092	56	79	0	-397	27	6.28	6.28	9.42	9.42	2	0.03	0.00	0.01	0.00	0.00	24.0
15	220	-5331	50	306	0	-204	28	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
16	220	-4983	62	75	0	-392	30	6.28	6.28	9.42	9.42	2	0.03	0.00	0.01	0.00	0.00	24.0
17	220	-5222	56	302	0	-199	31	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
18	220	-8249	5	213	0	-507	75	6.28	6.28	9.42	9.42	3	0.02	0.00	0.03	0.00	0.00	24.0
19	220	-7785	-21	215	0	-400	-82	6.28	6.28	9.42	9.42	3	0.02	0.00	0.03	0.00	0.00	24.0
20	220	-7272	-17	336	0	-662	3	6.28	6.28	9.42	9.42	3	0.03	0.01	0.04	0.00	0.00	24.0
37	220	-7994	40	224	0	-521	140	6.28	6.28	9.42	9.42	3	0.03	0.01	0.03	0.00	0.00	24.0
38	220	-7220	-4	228	0	-342	-120	6.28	6.28	9.42	9.42	3	0.02	0.01	0.03	0.00	0.00	24.0
39	220	-6365	2	430	0	-779	21	6.28	6.28	9.42	9.42	3	0.04	0.01	0.05	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	330	-6060	73	248	0	-659	118	6.28	6.28	9.42	9.42	3	0.03	0.01	0.03	0.00	0.00	24.0
2	330	-4808	47	162	0	-513	77	6.28	6.28	9.42	9.42	2	0.04	0.00	0.02	0.00	0.00	24.0
3	330	-4880	45	230	0	-530	75	6.28	6.28	9.42	9.42	2	0.04	0.01	0.03	0.00	0.00	24.0
4	330	-4445	67	151	0	-485	107	6.28	6.28	9.42	9.42	2	0.04	0.00	0.02	0.00	0.00	24.0
5	330	-4516	65	219	0	-502	105	6.28	6.28	9.42	9.42	2	0.04	0.01	0.03	0.00	0.00	24.0

6	330	-4597	56	79	0	-483	89	6.28	6.28	9.42	9.42	2	0.04	0.00	0.01	0.00	0.00	24.0
7	330	-4836	50	306	0	-540	83	6.28	6.28	9.42	9.42	2	0.04	0.01	0.04	0.00	0.00	24.0
8	330	-4488	62	75	0	-475	99	6.28	6.28	9.42	9.42	2	0.04	0.00	0.01	0.00	0.00	24.0
9	330	-4727	56	302	0	-531	92	6.28	6.28	9.42	9.42	2	0.04	0.01	0.04	0.00	0.00	24.0
10	330	-4808	47	162	0	-513	77	6.28	6.28	9.42	9.42	2	0.04	0.00	0.02	0.00	0.00	24.0
11	330	-4880	45	230	0	-530	75	6.28	6.28	9.42	9.42	2	0.04	0.01	0.03	0.00	0.00	24.0
12	330	-4445	67	151	0	-485	107	6.28	6.28	9.42	9.42	2	0.04	0.00	0.02	0.00	0.00	24.0
13	330	-4516	65	219	0	-502	105	6.28	6.28	9.42	9.42	2	0.04	0.01	0.03	0.00	0.00	24.0
14	330	-4597	56	79	0	-483	89	6.28	6.28	9.42	9.42	2	0.04	0.00	0.01	0.00	0.00	24.0
15	330	-4836	50	306	0	-540	83	6.28	6.28	9.42	9.42	2	0.04	0.01	0.04	0.00	0.00	24.0
16	330	-4488	62	75	0	-475	99	6.28	6.28	9.42	9.42	2	0.04	0.00	0.01	0.00	0.00	24.0
17	330	-4727	56	302	0	-531	92	6.28	6.28	9.42	9.42	2	0.04	0.01	0.04	0.00	0.00	24.0
18	330	-7606	-99	213	0	-741	23	6.28	6.28	9.42	9.42	3	0.04	0.00	0.03	0.00	0.00	24.0
19	330	-7142	83	215	0	-636	-48	6.28	6.28	9.42	9.42	3	0.03	0.00	0.03	0.00	0.00	24.0
20	330	-6628	-17	32	0	-865	-16	6.28	6.28	9.42	9.42	3	0.04	0.00	0.00	0.00	0.00	24.0
37	330	-7350	-133	224	0	-767	89	6.28	6.28	9.42	9.42	3	0.04	0.01	0.03	0.00	0.00	24.0
38	330	-6576	170	228	0	-592	-29	6.28	6.28	9.42	9.42	3	0.03	0.01	0.03	0.00	0.00	24.0
39	330	-5722	2	-78	0	-973	24	6.28	6.28	9.42	9.42	3	0.05	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	440	-5417	73	248	0	-932	198	6.28	6.28	9.42	9.42	3	0.05	0.01	0.03	0.00	0.00	24.0
2	440	-4313	47	162	0	-691	129	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
3	440	-4385	45	230	0	-783	124	6.28	6.28	9.42	9.42	2	0.06	0.01	0.03	0.00	0.00	24.0
4	440	-3950	67	151	0	-651	181	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
5	440	-4021	65	219	0	-743	177	6.28	6.28	9.42	9.42	2	0.06	0.01	0.03	0.00	0.00	24.0
6	440	-4102	56	79	0	-570	152	6.28	6.28	9.42	9.42	2	0.05	0.00	0.01	0.00	0.00	24.0
7	440	-4341	50	306	0	-876	138	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
8	440	-3993	62	75	0	-557	167	6.28	6.28	9.42	9.42	2	0.05	0.00	0.01	0.00	0.00	24.0
9	440	-4232	56	302	0	-864	154	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
10	440	-4313	47	162	0	-691	129	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
11	440	-4385	45	230	0	-783	124	6.28	6.28	9.42	9.42	2	0.06	0.01	0.03	0.00	0.00	24.0
12	440	-3950	67	151	0	-651	181	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
13	440	-4021	65	219	0	-743	177	6.28	6.28	9.42	9.42	2	0.06	0.01	0.03	0.00	0.00	24.0
14	440	-4102	56	79	0	-570	152	6.28	6.28	9.42	9.42	2	0.05	0.00	0.01	0.00	0.00	24.0
15	440	-4341	50	306	0	-876	138	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
16	440	-3993	62	75	0	-557	167	6.28	6.28	9.42	9.42	2	0.05	0.00	0.01	0.00	0.00	24.0
17	440	-4232	56	302	0	-864	154	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
18	440	-6962	-203	213	0	-975	-143	6.28	6.28	9.42	9.42	3	0.05	0.01	0.03	0.00	0.00	24.0
19	440	-6498	187	215	0	-873	101	6.28	6.28	9.42	9.42	3	0.04	0.00	0.03	0.00	0.00	24.0
20	440	-5985	-17	-273	0	-732	-35	6.28	6.28	9.42	9.42	3	0.04	0.01	0.03	0.00	0.00	24.0
37	440	-6707	-306	224	0	-1014	-153	6.28	6.28	9.42	9.42	3	0.05	0.01	0.03	0.00	0.00	24.0
38	440	-5933	343	228	0	-843	253	6.28	6.28	9.42	9.42	3	0.05	0.01	0.03	0.00	0.00	24.0
39	440	-5078	2	-586	0	-608	27	6.28	6.28	9.42	9.42	3	0.03	0.01	0.07	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

VERIFICA NODO IN TESTA AL PILASTRO, NODO NUM. 32 NON CONFINATO

(par.7.2.2 NTC2018 "La domanda di resistenza valutata con i criteri della progettazione in capacità può essere assunta non superiore alla domanda di resistenza valutata per il caso di comportamento strutturale non dissipativo.")

PROGETTAZIONE IN CAPACITA'

Asse loc. pilastro y nodo ESTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 45.0 cm, hjc= 20.0 cm
Asse loc. pilastro z nodo ESTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 30.0 cm, hjc= 50.0 cm

FxMin,inf	FxMin,sup	FxMax,sup	FySup	FzSup	Vjbdy	Vjbdz	Vres,y	Vres,z	I.R.compr.	Ashy	Ashz	PASSO	Nota
daN					daN		daN			cmq		cm	
-3950	-23	-395	922	409	16695	17208	62907	104844	0.27	4.38	--	11.93	

VERIFICA DI RESISTENZA CON SOLLECITAZIONI COMPORTAMENTO NON DISSIPATIVO

Asse loc. pilastro y nodo ESTERNO: Hjw= 40.0 cm, bj= 45.0 cm, hjc= 20.0 cm, db1= 45.0 cm

NC	Fx,sup	Fx,inf	Mb	Vb	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-380	-4313	-1918	1981	933	3802	62910	0.06	0.00	40.00	
3	-395	-4385	-1912	1979	940	3780	62907	0.06	0.00	40.00	
4	-23	-3950	-1868	1971	928	3684	63000	0.06	0.00	40.00	
5	-38	-4021	-1862	1969	935	3662	62996	0.06	0.00	40.00	
6	-238	-4102	-1906	1980	923	3783	62946	0.06	0.00	40.00	
7	-287	-4341	-1889	1973	947	3717	62934	0.06	0.00	40.00	
8	-131	-3993	-1891	1977	922	3747	62973	0.06	0.00	40.00	
9	-180	-4232	-1874	1970	945	3682	62960	0.06	0.00	40.00	
10	-380	-4313	-1918	1981	933	3802	62910	0.06	0.00	40.00	
11	-395	-4385	-1912	1979	940	3780	62907	0.06	0.00	40.00	
12	-23	-3950	-1868	1971	928	3684	63000	0.06	0.00	40.00	
13	-38	-4021	-1862	1969	935	3662	62996	0.06	0.00	40.00	
14	-238	-4102	-1906	1980	923	3783	62946	0.06	0.00	40.00	
15	-287	-4341	-1889	1973	947	3717	62934	0.06	0.00	40.00	
16	-131	-3993	-1891	1977	922	3747	62973	0.06	0.00	40.00	
17	-180	-4232	-1874	1970	945	3682	62960	0.06	0.00	40.00	

Asse loc. pilastro z nodo ESTERNO: Hjw= 40.0 cm, bj= 30.0 cm, hjc= 50.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb	Vb	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-380	-4313	-1677	1952	409	3732	104850	0.04	0.00	40.00	
3	-395	-4385	-1860	2011	424	4169	104844	0.04	0.00	40.00	
4	-23	-3950	-1688	1955	512	3655	104999	0.03	0.00	40.00	
5	-38	-4021	-1870	2014	527	4090	104993	0.04	0.00	40.00	
6	-238	-4102	-1469	1884	428	3199	104910	0.03	0.00	40.00	
7	-287	-4341	-2076	2081	477	4649	104889	0.04	0.00	40.00	
8	-131	-3993	-1472	1885	459	3175	104954	0.03	0.00	40.00	
9	-180	-4232	-2079	2082	508	4625	104934	0.04	0.00	40.00	
10	-380	-4313	-1677	1952	409	3732	104850	0.04	0.00	40.00	
11	-395	-4385	-1860	2011	424	4169	104844	0.04	0.00	40.00	
12	-23	-3950	-1688	1955	512	3655	104999	0.03	0.00	40.00	
13	-38	-4021	-1870	2014	527	4090	104993	0.04	0.00	40.00	
14	-238	-4102	-1469	1884	428	3199	104910	0.03	0.00	40.00	
15	-287	-4341	-2076	2081	477	4649	104889	0.04	0.00	40.00	
16	-131	-3993	-1472	1885	459	3175	104954	0.03	0.00	40.00	
17	-180	-4232	-2079	2082	508	4625	104934	0.04	0.00	40.00	

CONFRONTO E SINTESI CONCLUSIVE (si assume in ogni caso passo <= 15 cm)

I.R.compr.	Ashy	Ashz	PASSO	Nota
	cmq		cm	
0.06	--	--	15.00	**VERIFICATO**

ASTA NUM. 3 NI 27 NF 25 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 7C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	5881	-1011	834	0	1410	1440	6.28	6.28	9.42	9.42	3	0.19	0.03	0.13	0.00	0.00	24.0
2	0	4546	-778	607	0	1083	1122	6.28	6.28	9.42	9.42	2	0.19	0.02	0.10	0.00	0.00	24.0
3	0	4598	-783	689	0	1127	1128	6.28	6.28	9.42	9.42	2	0.20	0.02	0.10	0.00	0.00	24.0
4	0	4450	-772	593	0	1043	1087	6.28	6.28	9.42	9.42	2	0.19	0.02	0.10	0.00	0.00	24.0
5	0	4502	-777	675	0	1087	1093	6.28	6.28	9.42	9.42	2	0.19	0.02	0.10	0.00	0.00	24.0
6	0	4451	-770	507	0	1018	1103	6.28	6.28	9.42	9.42	2	0.19	0.02	0.10	0.00	0.00	24.0
7	0	4626	-787	780	0	1164	1122	6.28	6.28	9.42	9.42	2	0.20	0.02	0.11	0.00	0.00	24.0
8	0	4422	-768	502	0	1006	1093	6.28	6.28	9.42	9.42	2	0.19	0.02	0.10	0.00	0.00	24.0
9	0	4597	-785	776	0	1152	1112	6.28	6.28	9.42	9.42	2	0.20	0.02	0.11	0.00	0.00	24.0
10	0	4546	-778	607	0	1083	1122	6.28	6.28	9.42	9.42	2	0.19	0.02	0.10	0.00	0.00	24.0
11	0	4598	-783	689	0	1127	1128	6.28	6.28	9.42	9.42	2	0.20	0.02	0.10	0.00	0.00	24.0
12	0	4450	-772	593	0	1043	1087	6.28	6.28	9.42	9.42	2	0.19	0.02	0.10	0.00	0.00	24.0
13	0	4502	-777	675	0	1087	1093	6.28	6.28	9.42	9.42	2	0.19	0.02	0.10	0.00	0.00	24.0
14	0	4451	-770	507	0	1018	1103	6.28	6.28	9.42	9.42	2	0.19	0.02	0.10	0.00	0.00	24.0
15	0	4626	-787	780	0	1164	1122	6.28	6.28	9.42	9.42	2	0.20	0.02	0.11	0.00	0.00	24.0
16	0	4422	-768	502	0	1006	1093	6.28	6.28	9.42	9.42	2	0.19	0.02	0.10	0.00	0.00	24.0
17	0	4597	-785	776	0	1152	1112	6.28	6.28	9.42	9.42	2	0.20	0.02	0.11	0.00	0.00	24.0
18	0	6459	-690	1063	0	1523	1324	6.28	6.28	9.42	9.42	3	0.17	0.03	0.15	0.00	0.00	24.0
19	0	5906	-1271	777	0	1266	1368	6.28	6.28	9.42	9.42	3	0.18	0.03	0.16	0.00	0.00	24.0
20	0	7095	-1007	1512	0	1580	1374	6.28	6.28	9.42	9.42	3	0.18	0.04	0.21	0.00	0.00	24.0
37	0	6513	-509	1129	0	1614	1343	6.28	6.28	9.42	9.42	3	0.18	0.03	0.16	0.00	0.00	24.0
38	0	5592	-1478	652	0	1184	1416	6.28	6.28	9.42	9.42	3	0.18	0.04	0.19	0.00	0.00	24.0
39	0	7574	-1039	1877	0	1709	1427	6.28	6.28	9.42	9.42	3	0.19	0.04	0.26	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	83	6364	-1011	834	0	723	606	6.28	6.28	9.42	9.42	3	0.08	0.03	0.12	0.00	0.00	24.0
2	83	4917	-778	607	0	582	480	6.28	6.28	9.42	9.42	2	0.09	0.02	0.09	0.00	0.00	24.0
3	83	4969	-783	689	0	558	482	6.28	6.28	9.42	9.42	2	0.09	0.02	0.10	0.00	0.00	24.0
4	83	4821	-772	593	0	554	450	6.28	6.28	9.42	9.42	2	0.08	0.02	0.08	0.00	0.00	24.0
5	83	4873	-777	675	0	530	452	6.28	6.28	9.42	9.42	2	0.08	0.02	0.09	0.00	0.00	24.0
6	83	4822	-770	507	0	600	467	6.28	6.28	9.42	9.42	2	0.09	0.02	0.08	0.00	0.00	24.0
7	83	4997	-787	780	0	520	473	6.28	6.28	9.42	9.42	2	0.09	0.02	0.11	0.00	0.00	24.0
8	83	4793	-768	502	0	591	459	6.28	6.28	9.42	9.42	2	0.09	0.02	0.08	0.00	0.00	24.0
9	83	4968	-785	776	0	512	464	6.28	6.28	9.42	9.42	2	0.08	0.02	0.11	0.00	0.00	24.0
10	83	4917	-778	607	0	582	480	6.28	6.28	9.42	9.42	2	0.09	0.02	0.09	0.00	0.00	24.0
11	83	4969	-783	689	0	558	482	6.28	6.28	9.42	9.42	2	0.09	0.02	0.10	0.00	0.00	24.0
12	83	4821	-772	593	0	554	450	6.28	6.28	9.42	9.42	2	0.08	0.02	0.08	0.00	0.00	24.0
13	83	4873	-777	675	0	530	452	6.28	6.28	9.42	9.42	2	0.08	0.02	0.09	0.00	0.00	24.0
14	83	4822	-770	507	0	600	467	6.28	6.28	9.42	9.42	2	0.09	0.02	0.08	0.00	0.00	24.0
15	83	4997	-787	780	0	520	473	6.28	6.28	9.42	9.42	2	0.09	0.02	0.11	0.00	0.00	24.0
16	83	4793	-768	502	0	591	459	6.28	6.28	9.42	9.42	2	0.09	0.02	0.08	0.00	0.00	24.0
17	83	4968	-785	776	0	512	464	6.28	6.28	9.42	9.42	2	0.08	0.02	0.11	0.00	0.00	24.0
18	83	6942	-878	1063	0	646	677	6.28	6.28	9.42	9.42	3	0.09	0.03	0.15	0.00	0.00	24.0
19	83	6388	-1082	777	0	625	397	6.28	6.28	9.42	9.42	3	0.05	0.03	0.12	0.00	0.00	24.0
20	83	7578	-1007	1284	0	427	543	6.28	6.28	9.42	9.42	3	0.07	0.03	0.18	0.00	0.00	24.0
37	83	6996	-823	1129	0	682	793	6.28	6.28	9.42	9.42	3	0.10	0.03	0.16	0.00	0.00	24.0
38	83	6074	-1164	652	0	646	327	6.28	6.28	9.42	9.42	3	0.05	0.03	0.13	0.00	0.00	24.0
39	83	8057	-1039	1496	0	317	570	6.28	6.28	9.42	9.42	3	0.07	0.04	0.21	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	165	6846	-1011	834	0	35	-228	6.28	6.28	9.42	9.42	3	0.03	0.03	0.13	0.00	0.00	24.0
2	165	5288	-778	607	0	81	-162	6.28	6.28	9.42	9.42	2	0.02	0.02	0.10	0.00	0.00	24.0
3	165	5340	-783	689	0	-10	-165	6.28	6.28	9.42	9.42	2	0.02	0.02	0.10	0.00	0.00	24.0
4	165	5192	-772	593	0	64	-186	6.28	6.28	9.42	9.42	2	0.03	0.02	0.10	0.00	0.00	24.0
5	165	5244	-777	675	0	-27	-189	6.28	6.28	9.42	9.42	2	0.03	0.02	0.10	0.00	0.00	24.0
6	165	5194	-770	507	0	182	-168	6.28	6.28	9.42	9.42	2	0.03	0.02	0.08	0.00	0.00	24.0
7	165	5368	-787	780	0	-123	-176	6.28	6.28	9.42	9.42	2	0.03	0.02	0.11	0.00	0.00	24.0
8	165	5164	-768	502	0	177	-175	6.28	6.28	9.42	9.42	2	0.03	0.02	0.08	0.00	0.00	24.0
9	165	5340	-785	776	0	-128	-183	6.28	6.28	9.42	9.42	2	0.03	0.02	0.11	0.00	0.00	24.0
10	165	5288	-778	607	0	81	-162	6.28	6.28	9.42	9.42	2	0.02	0.02	0.10	0.00	0.00	24.0
11	165	5340	-783	689	0	-10	-165	6.28	6.28	9.42	9.42	2	0.02	0.02	0.10	0.00	0.00	24.0
12	165	5192	-772	593	0	64	-186	6.28	6.28	9.42	9.42	2	0.03	0.02	0.10	0.00	0.00	24.0
13	165	5244	-777	675	0	-27	-189	6.28	6.28	9.42	9.42	2	0.03	0.02	0.10	0.00	0.00	24.0
14	165	5194	-770	507	0	182	-168	6.28	6.28	9.42	9.42	2	0.03	0.02	0.08	0.00	0.00	24.0
15	165	5368	-787	780	0	-123	-176	6.28	6.28	9.42	9.42	2	0.03	0.02	0.11	0.00	0.00	24.0
16	165	5164	-768	502	0	177	-175	6.28	6.28	9.42	9.42	2	0.03	0.02	0.08	0.00	0.00	24.0
17	165	5340	-785	776	0	-128	-183	6.28	6.28	9.42	9.42	2	0.03	0.02	0.11	0.00	0.00	24.0
18	165	7424	-1067	1063	0	-231	-125	6.28	6.28	9.42	9.42	3	0.02	0.03	0.15	0.00	0.00	24.0
19	165	6871	-894	777	0	-16	-418	6.28	6.28	9.42	9.42	3	0.05	0.02	0.11	0.00	0.00	24.0
20	165	8060	-1007	1055	0	-538	-288	6.28	6.28	9.42	9.42	3	0.04	0.03	0.15	0.00	0.00	24.0
37	165	7478	-1137	1129	0	-250	-15	6.28	6.28	9.42	9.42	3	0.01	0.03	0.16	0.00	0.00	24.0
38	165	6557	-849	652	0	108	-504	6.28	6.28	9.42	9.42	3	0.06	0.02	0.11	0.00	0.00	24.0
39	165	8540	-1039	1115	0	-760	-287	6.28	6.28	9.42	9.42	3	0.05	0.03	0.16	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	248	7329	-1011	834	0	-653	-1062	6.28	6.28	9.42	9.42	3	0.14	0.03	0.13	0.00	0.00	24.0
2	248	5660	-778	607	0	-420	-804	6.28	6.28	9.42	9.42	2	0.12	0.02	0.10	0.00	0.00	24.0
3	248	5712	-783	689	0	-579	-811	6.28	6.28	9.42	9.42	2	0.13	0.02	0.10	0.00	0.00	24.0
4	248	5564	-772	593	0	-425	-823	6.28	6.28	9.42	9.42	2	0.13	0.02	0.10	0.00	0.00	24.0
5	248	5616	-777	675	0	-584	-829	6.28	6.28	9.42	9.42	2	0.14	0.02	0.10	0.00	0.00	24.0
6	248	5565	-770	507	0	-236	-804	6.28	6.28	9.42	9.42	2	0.12	0.02	0.10	0.00	0.00	24.0
7	248	5740	-787	780	0	-766	-825	6.28	6.28	9.42	9.42	2	0.14	0.02	0.11	0.00	0.00	24.0
8	248	5536	-768	502	0	-238	-809	6.28	6.28	9.42	9.42	2	0.12	0.02	0.10	0.00	0.00	24.0
9	248	5711	-785	776	0	-767	-831	6.28	6.28	9.42	9.42	2	0.14	0.02	0.11	0.00	0.00	24.0
10	248	5660	-778	607	0	-420	-804	6.28	6.28	9.42	9.42	2	0.12	0.02	0.10	0.00	0.00	24.0
11	248	5712	-783	689	0	-579	-811	6.28	6.28	9.42	9.42	2	0.13	0.02	0.10	0.00	0.00	24.0

12	248	5564	-772	593	0	-425	-823	6.28	6.28	9.42	9.42	2	0.13	0.02	0.10	0.00	0.00	24.0
13	248	5616	-777	675	0	-584	-829	6.28	6.28	9.42	9.42	2	0.14	0.02	0.10	0.00	0.00	24.0
14	248	5565	-770	507	0	-236	-804	6.28	6.28	9.42	9.42	2	0.12	0.02	0.10	0.00	0.00	24.0
15	248	5740	-787	780	0	-766	-825	6.28	6.28	9.42	9.42	2	0.14	0.02	0.11	0.00	0.00	24.0
16	248	5536	-768	502	0	-238	-809	6.28	6.28	9.42	9.42	2	0.12	0.02	0.10	0.00	0.00	24.0
17	248	5711	-785	776	0	-767	-831	6.28	6.28	9.42	9.42	2	0.14	0.02	0.11	0.00	0.00	24.0
18	248	7906	-1255	1063	0	-1109	-1083	6.28	6.28	9.42	9.42	3	0.14	0.03	0.15	0.00	0.00	24.0
19	248	7354	-705	777	0	-658	-1077	6.28	6.28	9.42	9.42	3	0.14	0.02	0.11	0.00	0.00	24.0
20	248	8543	-1007	826	0	-1314	-1119	6.28	6.28	9.42	9.42	3	0.15	0.03	0.12	0.00	0.00	24.0
37	248	7961	-1452	1129	0	-1181	-1084	6.28	6.28	9.42	9.42	3	0.14	0.04	0.16	0.00	0.00	24.0
38	248	7040	-535	652	0	-430	-1074	6.28	6.28	9.42	9.42	3	0.14	0.02	0.09	0.00	0.00	24.0
39	248	9022	-1039	735	0	-1524	-1144	6.28	6.28	9.42	9.42	3	0.16	0.03	0.11	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	330	7812	-1011	834	0	-1340	-1896	6.28	6.28	9.42	9.42	3	0.25	0.03	0.13	0.00	0.00	24.0
2	330	6031	-778	607	0	-921	-1446	6.28	6.28	9.42	9.42	2	0.23	0.02	0.10	0.00	0.00	24.0
3	330	6083	-783	689	0	-1148	-1457	6.28	6.28	9.42	9.42	2	0.25	0.02	0.10	0.00	0.00	24.0
4	330	5935	-772	593	0	-914	-1460	6.28	6.28	9.42	9.42	2	0.23	0.02	0.10	0.00	0.00	24.0
5	330	5987	-777	675	0	-1141	-1470	6.28	6.28	9.42	9.42	2	0.25	0.02	0.10	0.00	0.00	24.0
6	330	5936	-770	507	0	-654	-1439	6.28	6.28	9.42	9.42	2	0.22	0.02	0.10	0.00	0.00	24.0
7	330	6111	-787	780	0	-1410	-1474	6.28	6.28	9.42	9.42	2	0.26	0.02	0.11	0.00	0.00	24.0
8	330	5907	-768	502	0	-652	-1443	6.28	6.28	9.42	9.42	2	0.22	0.02	0.10	0.00	0.00	24.0
9	330	6082	-785	776	0	-1407	-1478	6.28	6.28	9.42	9.42	2	0.26	0.02	0.11	0.00	0.00	24.0
10	330	6031	-778	607	0	-921	-1446	6.28	6.28	9.42	9.42	2	0.23	0.02	0.10	0.00	0.00	24.0
11	330	6083	-783	689	0	-1148	-1457	6.28	6.28	9.42	9.42	2	0.25	0.02	0.10	0.00	0.00	24.0
12	330	5935	-772	593	0	-914	-1460	6.28	6.28	9.42	9.42	2	0.23	0.02	0.10	0.00	0.00	24.0
13	330	5987	-777	675	0	-1141	-1470	6.28	6.28	9.42	9.42	2	0.25	0.02	0.10	0.00	0.00	24.0
14	330	5936	-770	507	0	-654	-1439	6.28	6.28	9.42	9.42	2	0.22	0.02	0.10	0.00	0.00	24.0
15	330	6111	-787	780	0	-1410	-1474	6.28	6.28	9.42	9.42	2	0.26	0.02	0.11	0.00	0.00	24.0
16	330	5907	-768	502	0	-652	-1443	6.28	6.28	9.42	9.42	2	0.22	0.02	0.10	0.00	0.00	24.0
17	330	6082	-785	776	0	-1407	-1478	6.28	6.28	9.42	9.42	2	0.26	0.02	0.11	0.00	0.00	24.0
18	330	8389	-1444	1063	0	-1986	-2197	6.28	6.28	9.42	9.42	3	0.29	0.04	0.18	0.00	0.00	24.0
19	330	7836	-517	777	0	-1299	-1581	6.28	6.28	9.42	9.42	3	0.21	0.02	0.11	0.00	0.00	24.0
20	330	9026	-1007	598	0	-1901	-1950	6.28	6.28	9.42	9.42	3	0.26	0.03	0.13	0.00	0.00	24.0
37	330	8444	-1766	1129	0	-2113	-2411	6.28	6.28	9.42	9.42	3	0.32	0.05	0.22	0.00	0.00	24.0
38	330	7522	-220	652	0	-968	-1386	6.28	6.28	9.42	9.42	3	0.18	0.02	0.09	0.00	0.00	24.0
39	330	9505	-1039	354	0	-1973	-2001	6.28	6.28	9.42	9.42	3	0.27	0.03	0.13	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

VERIFICA NODO IN TESTA AL PILASTRO, NODO NUM. 25 NON CONFINATO

(par.7.2.2 NTC2018 "La domanda di resistenza valutata con i criteri della progettazione in capacità può essere assunta non superiore alla domanda di resistenza valutata per il caso di comportamento strutturale non dissipativo.")

PROGETTAZIONE IN CAPACITA'

Asse loc. pilastro y nodo ESTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 45.0 cm, hjc= 20.0 cm
Asse loc. pilastro z nodo ESTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 30.0 cm, hjc= 50.0 cm

FxMin,inf	FxMin,sup	FxMax,sup	FySup	FzSup	Vjbdy	Vjbdz	Vres,y	Vres,z	I.R.compr.	Ashy	Ashz	PASSO	Nota
daN					daN		daN			cmq		cm	
-10000000150474662198766888550 40	1	-0	0	0	17616	17616	63005	105009		0.28	7.07	--	6.63

VERIFICA DI RESISTENZA CON SOLLECITAZIONI COMPORTAMENTO NON DISSIPATIVO

Asse loc. pilastro y nodo ESTERNO: Hjw= 40.0 cm, bj= 45.0 cm, hjc= 20.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb	Vb	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-0	-0	-692	1303	0	1708	63005	0.03	0.00	40.00	
3	-0	-0	-677	1299	0	1671	63005	0.03	0.00	40.00	
4	-0	-0	-650	1297	0	1606	63005	0.03	0.00	40.00	
5	-0	-0	-635	1293	0	1569	63005	0.02	0.00	40.00	
6	-0	-0	-695	1306	0	1716	63005	0.03	0.00	40.00	
7	-0	-0	-644	1292	0	1591	63005	0.03	0.00	40.00	
8	-0	-0	-683	1304	0	1686	63005	0.03	0.00	40.00	
9	-0	-0	-632	1290	0	1560	63005	0.02	0.00	40.00	
10	-0	-0	-692	1303	0	1708	63005	0.03	0.00	40.00	
11	-0	-0	-677	1299	0	1671	63005	0.03	0.00	40.00	
12	-0	-0	-650	1297	0	1606	63005	0.03	0.00	40.00	
13	-0	-0	-635	1293	0	1569	63005	0.02	0.00	40.00	
14	-0	-0	-695	1306	0	1716	63005	0.03	0.00	40.00	
15	-0	-0	-644	1292	0	1591	63005	0.03	0.00	40.00	
16	-0	-0	-683	1304	0	1686	63005	0.03	0.00	40.00	
17	-0	-0	-632	1290	0	1560	63005	0.02	0.00	40.00	

Asse loc. pilastro z nodo ESTERNO: Hjw= 40.0 cm, bj= 30.0 cm, hjc= 50.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb	Vb	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-0	-0	-1616	1557	0	3990	105009	0.04	0.00	40.00	
3	-0	-0	-1674	1583	0	4133	105009	0.04	0.00	40.00	
4	-0	-0	-1532	1522	0	3783	105009	0.04	0.00	40.00	
5	-0	-0	-1591	1548	0	3928	105009	0.04	0.00	40.00	
6	-0	-0	-1519	1514	0	3751	105009	0.04	0.00	40.00	
7	-0	-0	-1713	1601	0	4230	105009	0.04	0.00	40.00	
8	-0	-0	-1494	1503	0	3689	105009	0.04	0.00	40.00	
9	-0	-0	-1688	1591	0	4168	105009	0.04	0.00	40.00	
10	-0	-0	-1616	1557	0	3990	105009	0.04	0.00	40.00	
11	-0	-0	-1674	1583	0	4133	105009	0.04	0.00	40.00	
12	-0	-0	-1532	1522	0	3783	105009	0.04	0.00	40.00	
13	-0	-0	-1591	1548	0	3928	105009	0.04	0.00	40.00	
14	-0	-0	-1519	1514	0	3751	105009	0.04	0.00	40.00	
15	-0	-0	-1713	1601	0	4230	105009	0.04	0.00	40.00	
16	-0	-0	-1494	1503	0	3689	105009	0.04	0.00	40.00	
17	-0	-0	-1688	1591	0	4168	105009	0.04	0.00	40.00	

CONFRONTO E SINTESI CONCLUSIVE (si assume in ogni caso passo <= 15 cm)

I.R.compr.	Ashy	Ashz	PASSO	Nota

cmq	cm			
0.04	--	--	15.00	**VERIFICATO**

ASTA NUM. 4 NI 23 NF 27 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 7B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-2013	-204	386	0	530	398	6.28	6.28	9.42	9.42	3	0.05	0.01	0.05	0.00	0.00	24.0
2	0	-1498	-163	264	0	320	315	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
3	0	-1496	-162	332	0	525	312	6.28	6.28	9.42	9.42	2	0.06	0.01	0.05	0.00	0.00	24.0
4	0	-1601	-152	261	0	291	300	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
5	0	-1600	-151	330	0	496	298	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
6	0	-1535	-160	183	0	71	312	6.28	6.28	9.42	9.42	2	0.04	0.00	0.02	0.00	0.00	24.0
7	0	-1531	-157	411	0	754	304	6.28	6.28	9.42	9.42	2	0.07	0.01	0.06	0.00	0.00	24.0
8	0	-1566	-157	182	0	62	308	6.28	6.28	9.42	9.42	2	0.04	0.00	0.02	0.00	0.00	24.0
9	0	-1562	-154	410	0	745	300	6.28	6.28	9.42	9.42	2	0.07	0.01	0.06	0.00	0.00	24.0
10	0	-1498	-163	264	0	320	315	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
11	0	-1496	-162	332	0	525	312	6.28	6.28	9.42	9.42	2	0.06	0.01	0.05	0.00	0.00	24.0
12	0	-1601	-152	261	0	291	300	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
13	0	-1600	-151	330	0	496	298	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
14	0	-1535	-160	183	0	71	312	6.28	6.28	9.42	9.42	2	0.04	0.00	0.02	0.00	0.00	24.0
15	0	-1531	-157	411	0	754	304	6.28	6.28	9.42	9.42	2	0.07	0.01	0.06	0.00	0.00	24.0
16	0	-1566	-157	182	0	62	308	6.28	6.28	9.42	9.42	2	0.04	0.00	0.02	0.00	0.00	24.0
17	0	-1562	-154	410	0	745	300	6.28	6.28	9.42	9.42	2	0.07	0.01	0.06	0.00	0.00	24.0
18	0	-1623	241	458	0	709	31	6.28	6.28	9.42	9.42	3	0.04	0.01	0.06	0.00	0.00	24.0
19	0	-2016	-566	349	0	335	655	6.28	6.28	9.42	9.42	3	0.07	0.01	0.07	0.00	0.00	24.0
20	0	-967	-155	1148	0	1260	324	6.28	6.28	9.42	9.42	3	0.07	0.03	0.16	0.00	0.00	24.0
37	0	-1588	496	489	0	836	-158	6.28	6.28	9.42	9.42	3	0.04	0.01	0.07	0.00	0.00	24.0
38	0	-2243	-848	306	0	212	882	6.28	6.28	9.42	9.42	3	0.10	0.02	0.10	0.00	0.00	24.0
39	0	-495	-164	1639	0	1754	331	6.28	6.28	9.42	9.42	3	0.09	0.04	0.23	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	110	-1370	-204	386	0	106	174	6.28	6.28	9.42	9.42	3	0.02	0.01	0.05	0.00	0.00	24.0
2	110	-1003	-163	264	0	30	136	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
3	110	-1001	-162	332	0	159	134	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
4	110	-1106	-152	261	0	4	133	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
5	110	-1105	-151	330	0	133	132	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
6	110	-1040	-160	183	0	-131	136	6.28	6.28	9.42	9.42	2	0.02	0.00	0.03	0.00	0.00	24.0
7	110	-1036	-157	411	0	302	132	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
8	110	-1071	-157	182	0	-139	135	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
9	110	-1067	-154	410	0	294	131	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
10	110	-1003	-163	264	0	30	136	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
11	110	-1001	-162	332	0	159	134	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
12	110	-1106	-152	261	0	4	133	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
13	110	-1105	-151	330	0	133	132	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
14	110	-1040	-160	183	0	-131	136	6.28	6.28	9.42	9.42	2	0.02	0.00	0.03	0.00	0.00	24.0
15	110	-1036	-157	411	0	302	132	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
16	110	-1071	-157	182	0	-139	135	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
17	110	-1067	-154	410	0	294	131	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
18	110	-980	51	458	0	205	192	6.28	6.28	9.42	9.42	3	0.02	0.01	0.06	0.00	0.00	24.0
19	110	-1373	-376	349	0	-49	137	6.28	6.28	9.42	9.42	3	0.02	0.01	0.05	0.00	0.00	24.0
20	110	-324	-155	843	0	165	154	6.28	6.28	9.42	9.42	3	0.02	0.02	0.12	0.00	0.00	24.0
37	110	-945	180	489	0	298	214	6.28	6.28	9.42	9.42	3	0.03	0.01	0.07	0.00	0.00	24.0
38	110	-1599	-532	306	0	-125	122	6.28	6.28	9.42	9.42	3	0.01	0.01	0.06	0.00	0.00	24.0
39	110	149	-164	1131	0	231	150	6.28	6.28	9.42	9.42	3	0.02	0.03	0.16	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	220	-726	-204	386	0	-318	-50	6.28	6.28	9.42	9.42	3	0.02	0.01	0.05	0.00	0.00	24.0
2	220	-508	-163	264	0	-260	-43	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
3	220	-506	-162	332	0	-206	-44	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
4	220	-611	-152	261	0	-284	-34	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
5	220	-610	-151	330	0	-230	-34	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
6	220	-545	-160	183	0	-332	-40	6.28	6.28	9.42	9.42	2	0.03	0.00	0.03	0.00	0.00	24.0
7	220	-541	-157	411	0	-151	-41	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
8	220	-576	-157	182	0	-339	-37	6.28	6.28	9.42	9.42	2	0.03	0.00	0.03	0.00	0.00	24.0
9	220	-572	-154	410	0	-158	-38	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
10	220	-508	-163	264	0	-260	-43	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
11	220	-506	-162	332	0	-206	-44	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
12	220	-611	-152	261	0	-284	-34	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
13	220	-610	-151	330	0	-230	-34	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
14	220	-545	-160	183	0	-332	-40	6.28	6.28	9.42	9.42	2	0.03	0.00	0.03	0.00	0.00	24.0
15	220	-541	-157	411	0	-151	-41	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
16	220	-576	-157	182	0	-339	-37	6.28	6.28	9.42	9.42	2	0.03	0.00	0.03	0.00	0.00	24.0
17	220	-572	-154	410	0	-158	-38	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
18	220	-336	-139	458	0	-299	144	6.28	6.28	9.42	9.42	3	0.02	0.01	0.06	0.00	0.00	24.0
19	220	-729	-185	349	0	-433	-171	6.28	6.28	9.42	9.42	3	0.03	0.01	0.05	0.00	0.00	24.0
20	220	320	-155	539	0	-595	-17	6.28	6.28	9.42	9.42	3	0.03	0.01	0.08	0.00	0.00	24.0
37	220	-301	-137	489	0	-239	237	6.28	6.28	9.42	9.42	3	0.03	0.01	0.07	0.00	0.00	24.0
38	220	-956	-215	306	0	-461	-288	6.28	6.28	9.42	9.42	3	0.04	0.01	0.04	0.00	0.00	24.0
39	220	792	-164	623	0	-734	-31	6.28	6.28	9.42	9.42	3	0.04	0.01	0.09	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	330	-83	-204	386	0	-743	-274	6.28	6.28	9.42	9.42	3	0.05	0.01	0.05	0.00	0.00	24.0
2	330	-13	-163	264	0	-550	-223	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
3	330	-11	-162	332	0	-571	-222	6.28	6.28	9.42	9.42	2	0.06	0.01	0.05	0.00	0.00	24.0
4	330	-116	-152	261	0	-572	-200	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
5	330	-115	-151	330	0	-592	-200	6.28	6.28	9.42	9.42	2	0.06	0.01	0.05	0.00	0.00	24.0
6	330	-50	-160	183	0	-533	-216	6.28	6.28	9.42	9.42	2	0.05	0.00	0.03	0.00	0.00	24.0
7	330	-46	-157	411	0	-603	-213	6.28	6.28	9.42	9.42	2	0.06	0.01	0.06	0.00	0.00	24.0
8	330	-81	-157	182	0	-540	-209	6.28	6.28	9.42	9.42	2	0.05	0.00	0.03	0.00	0.00	24.0
9	330	-77	-154	410	0	-609	-206	6.28	6.28	9.42	9.42	2	0.06	0.01	0.06	0.00	0.00	24.0
10	330	-13	-163	264	0	-550	-223	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
11	330	-11	-162	332	0	-571	-222	6.28	6.28	9.42	9.42	2	0.06	0.01	0.05	0.00	0.00	24.0
12	330	-116	-152	261	0	-572	-200	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
13	330	-115	-151	330	0	-592	-200	6.28	6.28	9.42	9.42	2	0.06	0.01	0.05	0.00	0.00	24.0
14	330	-50	-160	183	0	-533	-216	6.28	6.28	9.42	9.42	2	0.05	0.00	0.03	0.00	0.00	24.0
15	330	-46	-157	411	0	-603	-213	6.28	6.28	9.42	9.42	2	0.06	0.01	0.06	0.00	0.00	24.0
16	330	-81	-157	182	0	-540	-209	6.28	6.28	9.42	9.42	2	0.05	0.00	0.03	0.00	0.00	24.0
17	330	-77	-154	410	0	-609	-206	6.28	6.28	9.42	9.42	2	0.06	0.01	0.06	0.00	0.00	24.0

18	330	307	-329	458	0	-803	-113	6.28	6.28	9.42	9.42	3	0.04	0.01	0.06	0.00	0.00	24.0
19	330	-86	5	349	0	-816	-271	6.28	6.28	9.42	9.42	3	0.05	0.01	0.05	0.00	0.00	24.0
20	330	963	-155	234	0	-1020	-188	6.28	6.28	9.42	9.42	3	0.06	0.01	0.03	0.00	0.00	24.0
37	330	342	-454	489	0	-777	-88	6.28	6.28	9.42	9.42	3	0.04	0.01	0.07	0.00	0.00	24.0
38	330	-312	102	306	0	-798	-350	6.28	6.28	9.42	9.42	3	0.05	0.01	0.04	0.00	0.00	24.0
39	330	1436	-164	115	0	-1140	-212	6.28	6.28	9.42	9.42	3	0.06	0.00	0.02	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	440	561	-204	386	0	-1167	-498	6.28	6.28	9.42	9.42	3	0.08	0.01	0.05	0.00	0.00	24.0
2	440	482	-163	264	0	-840	-402	6.28	6.28	9.42	9.42	2	0.09	0.01	0.04	0.00	0.00	24.0
3	440	484	-162	332	0	-936	-400	6.28	6.28	9.42	9.42	2	0.10	0.01	0.05	0.00	0.00	24.0
4	440	379	-152	261	0	-859	-367	6.28	6.28	9.42	9.42	2	0.09	0.01	0.04	0.00	0.00	24.0
5	440	380	-151	330	0	-955	-365	6.28	6.28	9.42	9.42	2	0.09	0.01	0.05	0.00	0.00	24.0
6	440	445	-160	183	0	-735	-392	6.28	6.28	9.42	9.42	2	0.08	0.00	0.03	0.00	0.00	24.0
7	440	449	-157	411	0	-1055	-386	6.28	6.28	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
8	440	414	-157	182	0	-740	-381	6.28	6.28	9.42	9.42	2	0.08	0.00	0.03	0.00	0.00	24.0
9	440	418	-154	410	0	-1061	-375	6.28	6.28	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
10	440	482	-163	264	0	-840	-402	6.28	6.28	9.42	9.42	2	0.09	0.01	0.04	0.00	0.00	24.0
11	440	484	-162	332	0	-936	-400	6.28	6.28	9.42	9.42	2	0.10	0.01	0.05	0.00	0.00	24.0
12	440	379	-152	261	0	-859	-367	6.28	6.28	9.42	9.42	2	0.09	0.01	0.04	0.00	0.00	24.0
13	440	380	-151	330	0	-955	-365	6.28	6.28	9.42	9.42	2	0.09	0.01	0.05	0.00	0.00	24.0
14	440	445	-160	183	0	-735	-392	6.28	6.28	9.42	9.42	2	0.08	0.00	0.03	0.00	0.00	24.0
15	440	449	-157	411	0	-1055	-386	6.28	6.28	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
16	440	414	-157	182	0	-740	-381	6.28	6.28	9.42	9.42	2	0.08	0.00	0.03	0.00	0.00	24.0
17	440	418	-154	410	0	-1061	-375	6.28	6.28	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
18	440	951	-519	458	0	-1307	-580	6.28	6.28	9.42	9.42	3	0.09	0.01	0.06	0.00	0.00	24.0
19	440	558	195	349	0	-1200	-161	6.28	6.28	9.42	9.42	3	0.06	0.01	0.05	0.00	0.00	24.0
20	440	1607	-155	-71	0	-1110	-359	6.28	6.28	9.42	9.42	3	0.07	0.00	0.02	0.00	0.00	24.0
37	440	986	-771	489	0	-1315	-761	6.28	6.28	9.42	9.42	3	0.10	0.02	0.08	0.00	0.00	24.0
38	440	331	419	306	0	-1135	-64	6.28	6.28	9.42	9.42	3	0.06	0.01	0.05	0.00	0.00	24.0
39	440	2079	-164	-393	0	-987	-393	6.28	6.28	9.42	9.42	3	0.07	0.01	0.05	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

VERIFICA NODO IN TESTA AL PILASTRO, NODO NUM. 27 NON CONFINATO

(par.7.2.2 NTC2018 "La domanda di resistenza valutata con i criteri della progettazione in capacità può essere assunta non superiore alla domanda di resistenza valutata per il caso di comportamento strutturale non dissipativo.")

PROGETTAZIONE IN CAPACITA'

Asse loc. pilastro y nodo ESTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 45.0 cm, hjc= 20.0 cm
Asse loc. pilastro z nodo ESTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 30.0 cm, hjc= 50.0 cm

FxMin,inf	FxMin,sup	FxMax,sup	FySup	FzSup	Vjbdy	Vjbdz	Vres,y	Vres,z	I.R.compr.	Ashy	Ashz	PASSO	Nota
daN					daN		daN			cmq		cm	
-10000000150474662198766888550 40	1	-0	768	502	16848	17114	63005	105009	0.27	5.96	--	8.12	

VERIFICA DI RESISTENZA CON SOLLECITAZIONI COMPORTAMENTO NON DISSIPATIVO

Asse loc. pilastro y nodo ESTERNO: Hjw= 40.0 cm, bj= 45.0 cm, hjc= 20.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb	Vb	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-0	-0	-1935	2017	778	3999	63005	0.06	0.00	40.00	
3	-0	-0	-1931	2015	783	3985	63005	0.06	0.00	40.00	
4	-0	-0	-2000	2032	772	4167	63005	0.07	0.00	40.00	
5	-0	-0	-1996	2031	777	4152	63005	0.07	0.00	40.00	
6	-0	-0	-1962	2024	770	4074	63005	0.06	0.00	40.00	
7	-0	-0	-1949	2019	787	4026	63005	0.06	0.00	40.00	
8	-0	-0	-1982	2028	768	4126	63005	0.07	0.00	40.00	
9	-0	-0	-1968	2023	785	4075	63005	0.06	0.00	40.00	
10	-0	-0	-1935	2017	778	3999	63005	0.06	0.00	40.00	
11	-0	-0	-1931	2015	783	3985	63005	0.06	0.00	40.00	
12	-0	-0	-2000	2032	772	4167	63005	0.07	0.00	40.00	
13	-0	-0	-1996	2031	777	4152	63005	0.07	0.00	40.00	
14	-0	-0	-1962	2024	770	4074	63005	0.06	0.00	40.00	
15	-0	-0	-1949	2019	787	4026	63005	0.06	0.00	40.00	
16	-0	-0	-1982	2028	768	4126	63005	0.07	0.00	40.00	
17	-0	-0	-1968	2023	785	4075	63005	0.06	0.00	40.00	

Asse loc. pilastro z nodo ESTERNO: Hjw= 40.0 cm, bj= 30.0 cm, hjc= 50.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb	Vb	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-0	-0	-1963	2047	607	4240	105009	0.04	0.00	40.00	
3	-0	-0	-2131	2099	689	4573	105009	0.04	0.00	40.00	
4	-0	-0	-1939	2039	593	4195	105009	0.04	0.00	40.00	
5	-0	-0	-2107	2091	675	4527	105009	0.04	0.00	40.00	
6	-0	-0	-1758	1983	507	3834	105009	0.04	0.00	40.00	
7	-0	-0	-2319	2158	780	4946	105009	0.05	0.00	40.00	
8	-0	-0	-1751	1980	502	3821	105009	0.04	0.00	40.00	
9	-0	-0	-2312	2155	776	4933	105009	0.05	0.00	40.00	
10	-0	-0	-1963	2047	607	4240	105009	0.04	0.00	40.00	
11	-0	-0	-2131	2099	689	4573	105009	0.04	0.00	40.00	
12	-0	-0	-1939	2039	593	4195	105009	0.04	0.00	40.00	
13	-0	-0	-2107	2091	675	4527	105009	0.04	0.00	40.00	
14	-0	-0	-1758	1983	507	3834	105009	0.04	0.00	40.00	
15	-0	-0	-2319	2158	780	4946	105009	0.05	0.00	40.00	
16	-0	-0	-1751	1980	502	3821	105009	0.04	0.00	40.00	
17	-0	-0	-2312	2155	776	4933	105009	0.05	0.00	40.00	

CONFRONTO E SINTESI CONCLUSIVE (si assume in ogni caso passo <= 15 cm)

I.R.compr.	Ashy	Ashz	PASSO	Nota
	cmq		cm	
0.07	--	--	15.00	**VERIFICATO**

ASTA NUM. 5 NI 34 NF 35 SEZ. Rp B= 0.600 H= 0.400 (pilastro)

PIL. NUM. 12C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-10780	-333	239	0	-337	487	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
2	0	-8317	-266	170	0	-332	379	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
3	0	-8328	-265	206	0	-230	378	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
4	0	-8260	-248	162	0	-288	371	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
5	0	-8271	-247	198	0	-186	370	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
6	0	-8284	-261	127	0	-436	378	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
7	0	-8321	-257	244	0	-96	374	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
8	0	-8267	-256	124	0	-422	376	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
9	0	-8303	-252	241	0	-82	371	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
10	0	-8317	-266	170	0	-332	379	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
11	0	-8328	-265	206	0	-230	378	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
12	0	-8260	-248	162	0	-288	371	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
13	0	-8271	-247	198	0	-186	370	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
14	0	-8284	-261	127	0	-436	378	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
15	0	-8321	-257	244	0	-96	374	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
16	0	-8267	-256	124	0	-422	376	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
17	0	-8303	-252	241	0	-82	371	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
18	0	-13820	-618	649	0	-990	999	6.28	6.28	12.57	12.57	3	0.06	0.01	0.06	0.00	0.00	24.0
19	0	-12090	-160	402	0	-544	224	6.28	6.28	12.57	12.57	3	0.02	0.01	0.04	0.00	0.00	24.0
20	0	-12540	-369	1281	0	-5833	574	6.28	6.28	12.57	12.57	3	0.21	0.02	0.12	0.00	0.00	24.0
37	0	-13800	-754	640	0	-1000	1218	6.28	6.28	12.57	12.57	3	0.07	0.01	0.07	0.00	0.00	24.0
38	0	-10900	10	227	0	-258	-74	6.28	6.28	12.57	12.57	3	0.01	0.00	0.02	0.00	0.00	24.0
39	0	-11670	-338	1693	0	-9072	509	6.28	6.28	12.57	12.57	3	0.33	0.03	0.16	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	83	-10137	-333	239	0	-534	212	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
2	83	-7822	-266	170	0	-473	160	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
3	83	-7833	-265	206	0	-400	160	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
4	83	-7765	-248	162	0	-422	167	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
5	83	-7776	-247	198	0	-349	166	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
6	83	-7789	-261	127	0	-540	163	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
7	83	-7826	-257	244	0	-297	162	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
8	83	-7772	-256	124	0	-525	165	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
9	83	-7808	-252	241	0	-281	164	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
10	83	-7822	-266	170	0	-473	160	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
11	83	-7833	-265	206	0	-400	160	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
12	83	-7765	-248	162	0	-422	167	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
13	83	-7776	-247	198	0	-349	166	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
14	83	-7789	-261	127	0	-540	163	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
15	83	-7826	-257	244	0	-297	162	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
16	83	-7772	-256	124	0	-525	165	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
17	83	-7808	-252	241	0	-281	164	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
18	83	-13178	-618	649	0	-1525	489	6.28	6.28	12.57	12.57	3	0.06	0.01	0.06	0.00	0.00	24.0
19	83	-11446	-160	402	0	-876	92	6.28	6.28	12.57	12.57	3	0.03	0.01	0.04	0.00	0.00	24.0
20	83	-11898	-369	828	0	-6703	270	6.28	6.28	12.57	12.57	3	0.24	0.01	0.08	0.00	0.00	24.0
37	83	-13158	-754	640	0	-1527	596	6.28	6.28	12.57	12.57	3	0.06	0.01	0.06	0.00	0.00	24.0
38	83	-10258	10	227	0	-445	-66	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
39	83	-11026	-338	938	0	-10157	230	6.28	6.28	12.57	12.57	3	0.36	0.02	0.09	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	165	-9494	-333	239	0	-731	-63	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
2	165	-7327	-266	170	0	-613	-60	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
3	165	-7338	-265	206	0	-569	-59	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
4	165	-7270	-248	162	0	-556	-38	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
5	165	-7281	-247	198	0	-512	-37	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
6	165	-7294	-261	127	0	-644	-53	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
7	165	-7331	-257	244	0	-498	-51	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
8	165	-7277	-256	124	0	-627	-46	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
9	165	-7313	-252	241	0	-481	-44	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
10	165	-7327	-266	170	0	-613	-60	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
11	165	-7338	-265	206	0	-569	-59	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
12	165	-7270	-248	162	0	-556	-38	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
13	165	-7281	-247	198	0	-512	-37	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
14	165	-7294	-261	127	0	-644	-53	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
15	165	-7331	-257	244	0	-498	-51	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
16	165	-7277	-256	124	0	-627	-46	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
17	165	-7313	-252	241	0	-481	-44	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
18	165	-12535	-618	649	0	-2061	-21	6.28	6.28	12.57	12.57	3	0.07	0.01	0.06	0.00	0.00	24.0
19	165	-10802	-160	402	0	-1208	-40	6.28	6.28	12.57	12.57	3	0.04	0.01	0.04	0.00	0.00	24.0
20	165	-11256	-369	375	0	-7200	-34	6.28	6.28	12.57	12.57	3	0.26	0.01	0.04	0.00	0.00	24.0
37	165	-12515	-754	640	0	-2055	-26	6.28	6.28	12.57	12.57	3	0.07	0.01	0.06	0.00	0.00	24.0
38	165	-9615	10	227	0	-633	-58	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
39	165	-10382	-338	183	0	-10620	-49	6.28	6.28	12.57	12.57	3	0.38	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	248	-8851	-333	239	0	-929	-338	6.28	6.28	12.57	12.57	3	0.04	0.01	0.03	0.00	0.00	24.0
2	248	-6832	-266	170	0	-754	-279	6.28	6.28	12.57	12.57	2	0.05	0.00	0.02	0.00	0.00	24.0
3	248	-6843	-265	206	0	-739	-277	6.28	6.28	12.57	12.57	2	0.05	0.00	0.02	0.00	0.00	24.0
4	248	-6775	-248	162	0	-690	-242	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
5	248	-6786	-247	198	0	-675	-241	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
6	248	-6799	-261	127	0	-749	-268	6.28	6.28	12.57	12.57	2	0.05	0.00	0.02	0.00	0.00	24.0
7	248	-6836	-257	244	0	-699	-263	6.28	6.28	12.57	12.57	2	0.05	0.00	0.03	0.00	0.00	24.0
8	248	-6782	-256	124	0	-730	-257	6.28	6.28	12.57	12.57	2	0.05	0.00	0.02	0.00	0.00	24.0
9	248	-6818	-252	241	0	-680	-252	6.28	6.28	12.57	12.57	2	0.04	0.00	0.03	0.00	0.00	24.0
10	248	-6832	-266	170	0	-754	-279	6.28	6.28	12.57	12.57	2	0.05	0.00	0.02	0.00	0.00	24.0
11	248	-6843	-265	206	0	-739	-277	6.28	6.28	12.57	12.57	2	0.05	0.00	0.02	0.00	0.00	24.0
12	248	-6775	-248	162	0	-690	-242	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
13	248	-6786	-247	198	0	-675	-241	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
14	248	-6799	-261	127	0	-749	-268	6.28	6.28	12.57	12.57	2	0.05	0.00	0.02	0.00	0.00	24.0
15	248	-6836	-257	244	0	-699	-263	6.28	6.28	12.57	12.57	2	0.05	0.00	0.03	0.00	0.00	24.0
16	248	-6782	-256	124	0	-730	-257	6.28	6.28	12.57	12.57	2	0.05	0.00	0.02	0.00	0.00	24.0
17	248	-6818	-252	241	0	-680	-252	6.28	6.28	12.57	12.57	2	0.04	0.00	0.03	0.00	0.00	24.0
18	248	-11892	-618	649	0	-2596	-531	6.28	6.28	12.57	12.57	3	0.10	0.01	0.06	0.00	0.00	24.0
19	248	-10157	-160	402	0	-1539	-171	6.28	6.28	12.57	12.57	3	0.06	0.01	0.04	0.00	0.00	24.0
20	248	-10613	-369	-78	0	-7322	-338	6.28	6.28	12.57	12.57	3	0.27	0.01	0.03	0.00	0.00	24.0
37	248	-11872	-754	640	0	-2582	-648	6.28	6.28	12.57	12.57	3	0.10	0.01	0.06	0.00	0.00	24.0
38	248	-8972	10	227	0	-820	-50	6.28	6.28	12.57	12.57	3	0.03	0.00	0.02	0.00	0.00	24.0
39	248	-9737	-338	-572	0	-10459	-328	6.28	6.28	12.57	12.57	3	0.38	0.01	0.06	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	330	-8208	-333	239	0	-1126	-613	6.28	6.28	12.57	12.57	3	0.05	0.01	0.03	0.00	0.00	24.0
2	330	-6337	-266	170	0	-894	-498	6.28	6.28	12.57	12.57	2	0.07	0.00	0.02	0.00	0.00	24.0
3	330	-6348	-265	206	0	-908	-496	6.28	6.28	12.57	12.57	2	0.07	0.00	0.02	0.00	0.00	24.0
4	330	-6280	-248	162	0	-824	-447	6.28	6.28	12.57	12.57	2	0.06	0.00	0.02	0.00	0.00	24.0
5	330	-6291	-247	198	0	-838	-444	6.28	6.28	12.57	12.57	2	0.06	0.00	0.02	0.00	0.00	24.0
6	330	-6304	-261	127	0	-853	-484	6.28	6.28	12.57	12.57	2	0.06	0.00	0.02	0.00	0.00	24.0
7	330	-6341	-257	244	0	-900	-475	6.28	6.28	12.57	12.57	2	0.06	0.00	0.03	0.00	0.00	24.0
8	330	-6287	-256	124	0	-832	-468	6.28	6.28	12.57	12.57	2	0.06	0.00	0.02	0.00	0.00	24.0
9	330	-6323	-252	241	0	-879	-459	6.28	6.28	12.57	12.57	2	0.06	0.00	0.03	0.00	0.00	24.0
10	330	-6337	-266	170	0	-894	-498	6.28	6.28	12.57	12.57	2	0.07	0.00	0.02	0.00	0.00	24.0
11	330	-6348	-265	206	0	-908	-496	6.28	6.28	12.57	12.57	2	0.07	0.00	0.02	0.00	0.00	24.0
12	330	-6280	-248	162	0	-824	-447	6.28	6.28	12.57	12.57	2	0.06	0.00	0.02	0.00	0.00	24.0
13	330	-6291	-247	198	0	-838	-444	6.28	6.28	12.57	12.57	2	0.06	0.00	0.02	0.00	0.00	24.0
14	330	-6304	-261	127	0	-853	-484	6.28	6.28	12.57	12.57	2	0.06	0.00	0.02	0.00	0.00	24.0
15	330	-6341	-257	244	0	-900	-475	6.28	6.28	12.57	12.57	2	0.06	0.00	0.03	0.00	0.00	24.0
16	330	-6287	-256	124	0	-832	-468	6.28	6.28	12.57	12.57	2	0.06	0.00	0.02	0.00	0.00	24.0
17	330	-6323	-252	241	0	-879	-459	6.28	6.28	12.57	12.57	2	0.06	0.00	0.03	0.00	0.00	24.0
18	330	-11250	-618	649	0	-3132	-1041	6.28	6.28	12.57	12.57	3	0.13	0.01	0.06	0.00	0.00	24.0
19	330	-9513	-160	402	0	-1871	-303	6.28	6.28	12.57	12.57	3	0.07	0.01	0.04	0.00	0.00	24.0
20	330	-9971	-369	-531	0	-7071	-642	6.28	6.28	12.57	12.57	3	0.26	0.01	0.05	0.00	0.00	24.0
37	330	-11230	-754	640	0	-3110	-1270	6.28	6.28	12.57	12.57	3	0.13	0.01	0.06	0.00	0.00	24.0
38	330	-8330	10	227	0	-1008	-41	6.28	6.28	12.57	12.57	3	0.04	0.00	0.02	0.00	0.00	24.0
39	330	-9093	-338	-1327	0	-9676	-607	6.28	6.28	12.57	12.57	3	0.36	0.02	0.13	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

VERIFICA NODO IN TESTA AL PILASTRO, NODO NUM. 35 NON CONFINATO

(par.7.2.2 NTC2018 "La domanda di resistenza valutata con i criteri della progettazione in capacità può essere assunta non superiore alla domanda di resistenza valutata per il caso di comportamento strutturale non dissipativo.")

PROGETTAZIONE IN CAPACITA'

Asse loc. pilastro y nodo INTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 50.0 cm, hjc= 30.0 cm
Asse loc. pilastro z nodo: --

FxMin,inf	FxMin,sup	FxMax,sup	FySup	FzSup	Vjbdy	Vjbdz	Vres,y	Vres,z	I.R.compr.	Ashy	Ashz	PASSO	Nota
daN					daN		daN			cmq		cm	
-6280	-3514	-3613	759	282	34474	--	130127	--	0.26	8.78	--	5.17	

VERIFICA DI RESISTENZA CON SOLLECITAZIONI COMPORTAMENTO NON DISSIPATIVO

Asse loc. pilastro y nodo INTERNO: Hjw= 40.0 cm, bj= 50.0 cm, hjc= 30.0 cm, db1= 45.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb,1	Mb,2	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-3607	-6337	-1529	-902	847	702	130129	0.01	0.00	40.00	
3	-3613	-6348	-1537	-904	850	713	130127	0.01	0.00	40.00	
4	-3514	-6280	-1522	-983	759	571	130158	0.00	0.00	40.00	
5	-3520	-6291	-1530	-986	762	582	130157	0.00	0.00	40.00	
6	-3567	-6304	-1517	-928	812	643	130142	0.00	0.00	40.00	
7	-3588	-6341	-1544	-935	823	680	130135	0.01	0.00	40.00	
8	-3539	-6287	-1515	-952	786	604	130151	0.00	0.00	40.00	
9	-3560	-6323	-1542	-960	797	641	130144	0.00	0.00	40.00	
10	-3607	-6337	-1529	-902	847	702	130129	0.01	0.00	40.00	
11	-3613	-6348	-1537	-904	850	713	130127	0.01	0.00	40.00	
12	-3514	-6280	-1522	-983	759	571	130158	0.00	0.00	40.00	
13	-3520	-6291	-1530	-986	762	582	130157	0.00	0.00	40.00	
14	-3567	-6304	-1517	-928	812	643	130142	0.00	0.00	40.00	
15	-3588	-6341	-1544	-935	823	680	130135	0.01	0.00	40.00	
16	-3539	-6287	-1515	-952	786	604	130151	0.00	0.00	40.00	
17	-3560	-6323	-1542	-960	797	641	130144	0.00	0.00	40.00	

CONFRONTO E SINTESI CONCLUSIVE (si assume in ogni caso passo <= 15 cm)

I.R.compr.	Ashy	Ashz	PASSO	Nota
	cmq		cm	
0.01	--	--	15.00	**VERIFICATO**

ASTA NUM. 6 NI 36 NF 37 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 17C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-10930	-289	303	0	-741	306	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
2	0	-8410	-235	223	0	-618	246	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
3	0	-8456	-236	244	0	-512	246	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
4	0	-8360	-209	222	0	-628	225	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
5	0	-8405	-209	243	0	-521	226	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
6	0	-8340	-226	198	0	-746	238	6.28	6.28	12.57	12.57	2	0.05	0.00	0.02	0.00	0.00	24.0
7	0	-8490	-227	268	0	-391	239	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
8	0	-8325	-218	198	0	-749	232	6.28	6.28	12.57	12.57	2	0.05	0.00	0.02	0.00	0.00	24.0
9	0	-8475	-219	268	0	-394	233	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
10	0	-8410	-235	223	0	-618	246	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
11	0	-8456	-236	244	0	-512	246	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
12	0	-8360	-209	222	0	-628	225	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
13	0	-8405	-209	243	0	-521	226	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
14	0	-8340	-226	198	0	-746	238	6.28	6.28	12.57	12.57	2	0.05	0.00	0.02	0.00	0.00	24.0
15	0	-8490	-227	268	0	-391	239	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
16	0	-8325	-218	198	0	-749	232	6.28	6.28	12.57	12.57	2	0.05	0.00	0.02	0.00	0.00	24.0
17	0	-8475	-219	268	0	-394	233	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
18	0	-14320	-559	710	0	-1636	735	6.28	6.28	12.57	12.57	3	0.07	0.01	0.07	0.00	0.00	24.0
19	0	-13140	-98	598	0	-1504	4	6.28	6.28	12.57	12.57	3	0.05	0.01	0.06	0.00	0.00	24.0
20	0	-13390	-324	1662	0	-7429	361	6.28	6.28	12.57	12.57	3	0.26	0.03	0.16	0.00	0.00	24.0
37	0	-13840	-700	635	0	-1412	957	6.28	6.28	12.57	12.57	3	0.07	0.01	0.06	0.00	0.00	24.0

38	0	-11870	69	446	0	-1192	-261	6.28	6.28	12.57	12.57	3	0.05	0.01	0.04	0.00	0.00	24.0
39	0	-12290	-308	2221	0	-11070	334	6.28	6.28	12.57	12.57	3	0.39	0.04	0.21	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	83	-10286	-289	303	0	-991	68	6.28	6.28	12.57	12.57	3	0.04	0.01	0.03	0.00	0.00	24.0
2	83	-7915	-235	223	0	-802	52	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
3	83	-7961	-236	244	0	-713	52	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
4	83	-7865	-209	222	0	-811	53	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
5	83	-7910	-209	243	0	-722	53	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
6	83	-7845	-226	198	0	-909	52	6.28	6.28	12.57	12.57	2	0.05	0.00	0.02	0.00	0.00	24.0
7	83	-7995	-227	268	0	-612	52	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
8	83	-7830	-218	198	0	-912	52	6.28	6.28	12.57	12.57	2	0.05	0.00	0.02	0.00	0.00	24.0
9	83	-7980	-219	268	0	-615	53	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
10	83	-7915	-235	223	0	-802	52	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
11	83	-7961	-236	244	0	-713	52	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
12	83	-7865	-209	222	0	-811	53	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
13	83	-7910	-209	243	0	-722	53	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
14	83	-7845	-226	198	0	-909	52	6.28	6.28	12.57	12.57	2	0.05	0.00	0.02	0.00	0.00	24.0
15	83	-7995	-227	268	0	-612	52	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
16	83	-7830	-218	198	0	-912	52	6.28	6.28	12.57	12.57	2	0.05	0.00	0.02	0.00	0.00	24.0
17	83	-7980	-219	268	0	-615	53	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
18	83	-13678	-559	710	0	-2222	274	6.28	6.28	12.57	12.57	3	0.08	0.01	0.07	0.00	0.00	24.0
19	83	-12498	-98	598	0	-1997	-77	6.28	6.28	12.57	12.57	3	0.07	0.01	0.06	0.00	0.00	24.0
20	83	-12748	-324	1209	0	-8614	94	6.28	6.28	12.57	12.57	3	0.31	0.02	0.12	0.00	0.00	24.0
37	83	-13195	-700	635	0	-1936	380	6.28	6.28	12.57	12.57	3	0.07	0.01	0.06	0.00	0.00	24.0
38	83	-11226	69	446	0	-1560	-205	6.28	6.28	12.57	12.57	3	0.06	0.01	0.04	0.00	0.00	24.0
39	83	-11648	-308	1466	0	-12589	80	6.28	6.28	12.57	12.57	3	0.45	0.03	0.14	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	165	-9643	-289	303	0	-1241	-170	6.28	6.28	12.57	12.57	3	0.05	0.01	0.03	0.00	0.00	24.0
2	165	-7420	-235	223	0	-986	-143	6.28	6.28	12.57	12.57	2	0.06	0.00	0.02	0.00	0.00	24.0
3	165	-7466	-236	244	0	-914	-143	6.28	6.28	12.57	12.57	2	0.05	0.00	0.03	0.00	0.00	24.0
4	165	-7370	-209	222	0	-995	-119	6.28	6.28	12.57	12.57	2	0.06	0.00	0.02	0.00	0.00	24.0
5	165	-7415	-209	243	0	-923	-119	6.28	6.28	12.57	12.57	2	0.05	0.00	0.03	0.00	0.00	24.0
6	165	-7350	-226	198	0	-1073	-134	6.28	6.28	12.57	12.57	2	0.06	0.00	0.02	0.00	0.00	24.0
7	165	-7500	-227	268	0	-833	-135	6.28	6.28	12.57	12.57	2	0.05	0.00	0.03	0.00	0.00	24.0
8	165	-7335	-218	198	0	-1075	-127	6.28	6.28	12.57	12.57	2	0.06	0.00	0.02	0.00	0.00	24.0
9	165	-7485	-219	268	0	-836	-128	6.28	6.28	12.57	12.57	2	0.05	0.00	0.03	0.00	0.00	24.0
10	165	-7420	-235	223	0	-986	-143	6.28	6.28	12.57	12.57	2	0.06	0.00	0.02	0.00	0.00	24.0
11	165	-7466	-236	244	0	-914	-143	6.28	6.28	12.57	12.57	2	0.05	0.00	0.03	0.00	0.00	24.0
12	165	-7370	-209	222	0	-995	-119	6.28	6.28	12.57	12.57	2	0.06	0.00	0.02	0.00	0.00	24.0
13	165	-7415	-209	243	0	-923	-119	6.28	6.28	12.57	12.57	2	0.05	0.00	0.03	0.00	0.00	24.0
14	165	-7350	-226	198	0	-1073	-134	6.28	6.28	12.57	12.57	2	0.06	0.00	0.02	0.00	0.00	24.0
15	165	-7500	-227	268	0	-833	-135	6.28	6.28	12.57	12.57	2	0.05	0.00	0.03	0.00	0.00	24.0
16	165	-7335	-218	198	0	-1075	-127	6.28	6.28	12.57	12.57	2	0.06	0.00	0.02	0.00	0.00	24.0
17	165	-7485	-219	268	0	-836	-128	6.28	6.28	12.57	12.57	2	0.05	0.00	0.03	0.00	0.00	24.0
18	165	-13035	-559	710	0	-2808	-188	6.28	6.28	12.57	12.57	3	0.10	0.01	0.07	0.00	0.00	24.0
19	165	-11855	-98	598	0	-2490	-158	6.28	6.28	12.57	12.57	3	0.09	0.01	0.06	0.00	0.00	24.0
20	165	-12105	-324	756	0	-9425	-173	6.28	6.28	12.57	12.57	3	0.34	0.01	0.07	0.00	0.00	24.0
37	165	-12550	-700	635	0	-2459	-198	6.28	6.28	12.57	12.57	3	0.09	0.01	0.06	0.00	0.00	24.0
38	165	-10582	69	446	0	-1928	-148	6.28	6.28	12.57	12.57	3	0.07	0.01	0.04	0.00	0.00	24.0
39	165	-11005	-308	711	0	-13486	-174	6.28	6.28	12.57	12.57	3	0.48	0.01	0.07	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	248	-9000	-289	303	0	-1491	-408	6.28	6.28	12.57	12.57	3	0.06	0.01	0.03	0.00	0.00	24.0
2	248	-6925	-235	223	0	-1170	-337	6.28	6.28	12.57	12.57	2	0.07	0.00	0.02	0.00	0.00	24.0
3	248	-6971	-236	244	0	-1115	-337	6.28	6.28	12.57	12.57	2	0.07	0.00	0.03	0.00	0.00	24.0
4	248	-6875	-209	222	0	-1178	-291	6.28	6.28	12.57	12.57	2	0.07	0.00	0.02	0.00	0.00	24.0
5	248	-6920	-209	243	0	-1123	-292	6.28	6.28	12.57	12.57	2	0.07	0.00	0.03	0.00	0.00	24.0
6	248	-6855	-226	198	0	-1236	-320	6.28	6.28	12.57	12.57	2	0.08	0.00	0.02	0.00	0.00	24.0
7	248	-7005	-227	268	0	-1055	-322	6.28	6.28	12.57	12.57	2	0.07	0.00	0.03	0.00	0.00	24.0
8	248	-6840	-218	198	0	-1239	-307	6.28	6.28	12.57	12.57	2	0.08	0.00	0.02	0.00	0.00	24.0
9	248	-6990	-219	268	0	-1057	-308	6.28	6.28	12.57	12.57	2	0.07	0.00	0.03	0.00	0.00	24.0
10	248	-6925	-235	223	0	-1170	-337	6.28	6.28	12.57	12.57	2	0.07	0.00	0.02	0.00	0.00	24.0
11	248	-6971	-236	244	0	-1115	-337	6.28	6.28	12.57	12.57	2	0.07	0.00	0.03	0.00	0.00	24.0
12	248	-6875	-209	222	0	-1178	-291	6.28	6.28	12.57	12.57	2	0.07	0.00	0.02	0.00	0.00	24.0
13	248	-6920	-209	243	0	-1123	-292	6.28	6.28	12.57	12.57	2	0.07	0.00	0.03	0.00	0.00	24.0
14	248	-6855	-226	198	0	-1236	-320	6.28	6.28	12.57	12.57	2	0.08	0.00	0.02	0.00	0.00	24.0
15	248	-7005	-227	268	0	-1055	-322	6.28	6.28	12.57	12.57	2	0.07	0.00	0.03	0.00	0.00	24.0
16	248	-6840	-218	198	0	-1239	-307	6.28	6.28	12.57	12.57	2	0.08	0.00	0.02	0.00	0.00	24.0
17	248	-6990	-219	268	0	-1057	-308	6.28	6.28	12.57	12.57	2	0.07	0.00	0.03	0.00	0.00	24.0
18	248	-12392	-559	710	0	-3395	-649	6.28	6.28	12.57	12.57	3	0.13	0.01	0.07	0.00	0.00	24.0
19	248	-11212	-98	598	0	-2983	-239	6.28	6.28	12.57	12.57	3	0.11	0.01	0.06	0.00	0.00	24.0
20	248	-11462	-324	303	0	-9862	-440	6.28	6.28	12.57	12.57	3	0.35	0.01	0.03	0.00	0.00	24.0
37	248	-11905	-700	635	0	-2982	-775	6.28	6.28	12.57	12.57	3	0.12	0.01	0.06	0.00	0.00	24.0
38	248	-9939	69	446	0	-2297	-91	6.28	6.28	12.57	12.57	3	0.08	0.01	0.04	0.00	0.00	24.0
39	248	-10362	-308	-44	0	-13759	-427	6.28	6.28	12.57	12.57	3	0.50	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	330	-8356	-289	303	0	-1741	-647	6.28	6.28	12.57	12.57	3	0.07	0.01	0.03	0.00	0.00	24.0
2	330	-6430	-235	223	0	-1354	-531	6.28	6.28	12.57	12.57	2	0.09	0.00	0.02	0.00	0.00	24.0
3	330	-6476	-236	244	0	-1316	-531	6.28	6.28	12.57	12.57	2	0.09	0.00	0.03	0.00	0.00	24.0
4	330	-6380	-209	222	0	-1362	-463	6.28	6.28	12.57	12.57	2	0.09	0.00	0.02	0.00	0.00	24.0
5	330	-6425	-209	243	0	-1324	-464	6.28	6.28	12.57	12.57	2	0.09	0.00	0.03	0.00	0.00	24.0
6	330	-6360	-226	198	0	-1400	-506	6.28	6.28	12.57	12.57	2	0.09	0.00	0.02	0.00	0.00	24.0
7	330	-6510	-227	268	0	-1276	-509	6.28	6.28	12.57	12.57	2	0.09	0.00	0.03	0.00	0.00	24.0
8	330	-6345	-218	198	0	-1402	-486	6.28	6.28	12.57	12.57	2	0.09	0.00	0.02	0.00	0.00	24.0
9	330	-6495	-219	268	0	-1278	-488	6.28	6.28	12.57	12.57	2	0.08	0.00	0.03	0.00	0.00	24.0
10	330	-6430	-235	223	0	-1354	-531	6.28	6.28	12.57	12.57	2	0.09	0.00	0.02	0.00	0.00	24.0
11	330	-6476	-236	244	0	-1316	-531	6.28	6.28	12.57	12.57	2	0.09	0.00	0.03	0.00	0.00	24.0
12	330	-6380	-209	222	0	-1362	-463	6.28	6.28	12.57	12.57	2	0.09	0.00	0.02	0.00	0.00	24.0
13	330	-6425	-209	243	0	-1324	-464	6.28	6.28	12.57	12.57	2	0.09	0.00	0.03	0.00	0.00	24.0
14	330	-6360	-226	198	0	-1400	-506	6.28	6.28	12.57	12.57	2	0.09	0.00	0.02	0.00	0.00	24.0
15	330	-6510	-227	268	0	-1276	-509	6.28	6.28	12.57	12.57	2	0.09	0.00	0.03	0.00	0.00	24.0
16	330	-6345	-218	198	0	-1402	-486	6.28	6.28	12.57	12.57	2	0.09	0.00	0.02	0.00	0.00	24.0
17	330	-6495	-219	268	0	-1278	-488	6.28	6.28	12.57	12.57	2	0.08	0.00	0.03	0.00	0.00	24.0
18	330	-11750	-559	710	0	-3981	-1110	6.28	6.28	12.57	12.57	3	0.16	0.01	0.07	0.00	0.00	24.0
19	330	-10570	-98	598	0	-3476	-319	6.28	6.28	12.57	12.57	3	0.13	0.01	0.06	0.00	0.00	24.0
20	330	-10820	-324	-150	0	-9925	-707	6.28	6.28	12.57	12.57	3	0.36	0.01	0.03	0.00	0.00	24.0
37	330	-11260	-700	635	0	-3506	-1353	6.28	6.28	12.57	12.57	3	0.15	0.01	0.06	0.00	0.00	24.0
38	330	-9295	69	446	0	-2665	-35	6.28	6.28	12.57	12.57	3	0.10	0.01	0.04	0.00	0.00	24.0
39	330	-9720	-308	-800	0	-13410	-681	6.28	6.28	12.57	12.57	3	0.49	0.01	0.08	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

VERIFICA NODO IN TESTA AL PILASTRO, NODO NUM. 37 NON CONFINATO

(par.7.2.2 NTC2018 "La domanda di resistenza valutata con i criteri della progettazione in capacità può essere assunta non superiore alla domanda di resistenza valutata per il caso di comportamento strutturale non dissipativo.")

PROGETTAZIONE IN CAPACITA'

Asse loc. pilastro y nodo INTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 50.0 cm, hjc= 30.0 cm
Asse loc. pilastro z nodo: --

FxMin,inf	FxMin,sup	FxMax,sup	FySup	FzSup	Vjbdy	Vjbdz	Vres,y	Vres,z	I.R.compr.	Ashy	Ashz	PASSO	Nota
daN					daN		daN			cmq		cm	
-6345	-3446	-3617	81	187	35152	--	130126	--	0.27	8.78	--	5.17	

VERIFICA DI RESISTENZA CON SOLLECITAZIONI COMPORTAMENTO NON DISSIPATIVO

Asse loc. pilastro y nodo INTERNO: Hjw= 40.0 cm, bj= 50.0 cm, hjc= 30.0 cm, db1= 45.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb,1	Mb,2	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-3534	-6430	-1179	-1417	236	351	130152	0.00	0.00	40.00	
3	-3581	-6476	-1179	-1416	237	348	130137	0.00	0.00	40.00	
4	-3482	-6380	-1093	-1508	81	944	130169	0.01	0.00	40.00	
5	-3528	-6425	-1092	-1506	81	941	130154	0.01	0.00	40.00	
6	-3462	-6360	-1150	-1451	182	562	130175	0.00	0.00	40.00	
7	-3617	-6510	-1147	-1446	183	555	130126	0.00	0.00	40.00	
8	-3446	-6345	-1124	-1478	135	739	130180	0.01	0.00	40.00	
9	-3601	-6495	-1122	-1473	136	731	130131	0.01	0.00	40.00	
10	-3534	-6430	-1179	-1417	236	351	130152	0.00	0.00	40.00	
11	-3581	-6476	-1179	-1416	237	348	130137	0.00	0.00	40.00	
12	-3482	-6380	-1093	-1508	81	944	130169	0.01	0.00	40.00	
13	-3528	-6425	-1092	-1506	81	941	130154	0.01	0.00	40.00	
14	-3462	-6360	-1150	-1451	182	562	130175	0.00	0.00	40.00	
15	-3617	-6510	-1147	-1446	183	555	130126	0.00	0.00	40.00	
16	-3446	-6345	-1124	-1478	135	739	130180	0.01	0.00	40.00	
17	-3601	-6495	-1122	-1473	136	731	130131	0.01	0.00	40.00	

CONFRONTO E SINTESI CONCLUSIVE (si assume in ogni caso passo <= 15 cm)

I.R.compr.	Ashy	Ashz	PASSO	Nota
	cmq		cm	
0.01	--	--	15.00	**VERIFICATO**

ASTA NUM. 7 NI 38 NF 39 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 22C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice resistenza Fx,M	Bielle	V,Mx	aswta cmq/m	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-13170	63	248	0	-147	-102	6.28	6.28	12.57	12.57	3	0.01	0.00	0.02	0.00	0.00	24.0
2	0	-10120	35	170	0	-128	-68	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
3	0	-10160	31	201	0	3	-64	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
4	0	-10100	65	180	0	-229	-92	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
5	0	-10140	62	211	0	-98	-89	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
6	0	-10070	50	138	0	-317	-81	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
7	0	-10190	37	240	0	121	-69	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
8	0	-10060	59	141	0	-347	-88	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
9	0	-10190	47	243	0	91	-76	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
10	0	-10120	35	170	0	-128	-68	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
11	0	-10160	31	201	0	3	-64	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
12	0	-10100	65	180	0	-229	-92	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
13	0	-10140	62	211	0	-98	-89	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
14	0	-10070	50	138	0	-317	-81	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
15	0	-10190	37	240	0	121	-69	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
16	0	-10060	59	141	0	-347	-88	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
17	0	-10190	47	243	0	91	-76	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
18	0	-15710	-239	470	0	-199	323	6.28	6.28	12.57	12.57	3	0.02	0.01	0.04	0.00	0.00	24.0
19	0	-16520	246	632	0	-640	-455	6.28	6.28	12.57	12.57	3	0.03	0.01	0.06	0.00	0.00	24.0
20	0	-15740	-15	1217	0	-5425	-41	6.28	6.28	12.57	12.57	3	0.19	0.02	0.11	0.00	0.00	24.0
37	0	-14520	-380	318	0	35	569	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
38	0	-15880	428	588	0	-699	-729	6.28	6.28	12.57	12.57	3	0.04	0.01	0.05	0.00	0.00	24.0
39	0	-14570	-6	1563	0	-8675	-38	6.28	6.28	12.57	12.57	3	0.30	0.03	0.15	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice resistenza Fx,M	Bielle	V,Mx	aswta cmq/m	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	83	-12525	63	248	0	-351	-50	6.28	6.28	12.57	12.57	3	0.01	0.00	0.02	0.00	0.00	24.0
2	83	-9624	35	170	0	-269	-39	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
3	83	-9664	31	201	0	-163	-39	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
4	83	-9604	65	180	0	-378	-38	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
5	83	-9644	62	211	0	-272	-38	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
6	83	-9574	50	138	0	-431	-39	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
7	83	-9696	37	240	0	-77	-38	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
8	83	-9565	59	141	0	-463	-39	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
9	83	-9694	47	243	0	-110	-38	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
10	83	-9624	35	170	0	-269	-39	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
11	83	-9664	31	201	0	-163	-39	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
12	83	-9604	65	180	0	-378	-38	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
13	83	-9644	62	211	0	-272	-38	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
14	83	-9574	50	138	0	-431	-39	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
15	83	-9696	37	240	0	-77	-38	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
16	83	-9565	59	141	0	-463	-39	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
17	83	-9694	47	243	0	-110	-38	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
18	83	-15065	-239	470	0	-587	126	6.28	6.28	12.57	12.57	3	0.02	0.01	0.04	0.00	0.00	24.0
19	83	-15878	246	632	0	-1161	-253	6.28	6.28	12.57	12.57	3	0.04	0.01	0.06	0.00	0.00	24.0
20	83	-15098	-15	764	0	-6242	-53	6.28	6.28	12.57	12.57	3	0.22	0.01	0.07	0.00	0.00	24.0
37	83	-13878	-380	318	0	-228	255	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
38	83	-15235	428	588	0	-1184	-375	6.28	6.28	12.57	12.57	3	0.05	0.01	0.05	0.00	0.00	24.0
39	83	-13928	-6	808	0	-9653	-43	6.28	6.28	12.57	12.57	3	0.34	0.01	0.08	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	165	-11880	63	248	0	-556	2	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
2	165	-9129	35	170	0	-409	-10	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
3	165	-9168	31	201	0	-328	-13	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
4	165	-9109	65	180	0	-527	15	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
5	165	-9148	62	211	0	-446	13	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
6	165	-9078	50	138	0	-544	2	6.28	6.28	12.57	12.57	2	0.03	0.00	0.01	0.00	0.00	24.0
7	165	-9202	37	240	0	-275	-7	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
8	165	-9070	59	141	0	-579	9	6.28	6.28	12.57	12.57	2	0.03	0.00	0.01	0.00	0.00	24.0
9	165	-9198	47	243	0	-311	1	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
10	165	-9129	35	170	0	-409	-10	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
11	165	-9168	31	201	0	-328	-13	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
12	165	-9109	65	180	0	-527	15	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
13	165	-9148	62	211	0	-446	13	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
14	165	-9078	50	138	0	-544	2	6.28	6.28	12.57	12.57	2	0.03	0.00	0.01	0.00	0.00	24.0
15	165	-9202	37	240	0	-275	-7	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
16	165	-9070	59	141	0	-579	9	6.28	6.28	12.57	12.57	2	0.03	0.00	0.01	0.00	0.00	24.0
17	165	-9198	47	243	0	-311	1	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
18	165	-14420	-239	470	0	-975	-72	6.28	6.28	12.57	12.57	3	0.03	0.01	0.04	0.00	0.00	24.0
19	165	-15235	246	632	0	-1682	-50	6.28	6.28	12.57	12.57	3	0.06	0.01	0.06	0.00	0.00	24.0
20	165	-14455	-15	311	0	-6686	-66	6.28	6.28	12.57	12.57	3	0.23	0.01	0.03	0.00	0.00	24.0
37	165	-13235	-380	318	0	-490	-58	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
38	165	-14590	428	588	0	-1669	-22	6.28	6.28	12.57	12.57	3	0.06	0.01	0.06	0.00	0.00	24.0
39	165	-13285	-6	52	0	-10007	-48	6.28	6.28	12.57	12.57	3	0.35	0.00	0.00	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	248	-11235	63	248	0	-760	53	6.28	6.28	12.57	12.57	3	0.03	0.00	0.02	0.00	0.00	24.0
2	248	-8634	35	170	0	-549	19	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
3	248	-8672	31	201	0	-494	13	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
4	248	-8614	65	180	0	-675	69	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
5	248	-8652	62	211	0	-620	64	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
6	248	-8583	50	138	0	-658	43	6.28	6.28	12.57	12.57	2	0.04	0.00	0.01	0.00	0.00	24.0
7	248	-8707	37	240	0	-474	24	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
8	248	-8576	59	141	0	-696	58	6.28	6.28	12.57	12.57	2	0.04	0.00	0.01	0.00	0.00	24.0
9	248	-8703	47	243	0	-512	39	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
10	248	-8634	35	170	0	-549	19	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
11	248	-8672	31	201	0	-494	13	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
12	248	-8614	65	180	0	-675	69	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
13	248	-8652	62	211	0	-620	64	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
14	248	-8583	50	138	0	-658	43	6.28	6.28	12.57	12.57	2	0.04	0.00	0.01	0.00	0.00	24.0
15	248	-8707	37	240	0	-474	24	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
16	248	-8576	59	141	0	-696	58	6.28	6.28	12.57	12.57	2	0.04	0.00	0.01	0.00	0.00	24.0
17	248	-8703	47	243	0	-512	39	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
18	248	-13775	-239	470	0	-1363	-269	6.28	6.28	12.57	12.57	3	0.05	0.01	0.04	0.00	0.00	24.0
19	248	-14592	246	632	0	-2204	153	6.28	6.28	12.57	12.57	3	0.08	0.01	0.06	0.00	0.00	24.0
20	248	-13812	-15	-142	0	-6755	-78	6.28	6.28	12.57	12.57	3	0.24	0.00	0.01	0.00	0.00	24.0
37	248	-12592	-380	318	0	-753	-371	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
38	248	-13945	428	588	0	-2154	332	6.28	6.28	12.57	12.57	3	0.08	0.01	0.06	0.00	0.00	24.0
39	248	-12642	-6	-703	0	-9739	-53	6.28	6.28	12.57	12.57	3	0.34	0.01	0.07	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	330	-10590	63	248	0	-964	105	6.28	6.28	12.57	12.57	3	0.04	0.00	0.02	0.00	0.00	24.0
2	330	-8138	35	170	0	-689	47	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
3	330	-8176	31	201	0	-660	39	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
4	330	-8118	65	180	0	-824	123	6.28	6.28	12.57	12.57	2	0.05	0.00	0.02	0.00	0.00	24.0
5	330	-8156	62	211	0	-794	115	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
6	330	-8087	50	138	0	-771	84	6.28	6.28	12.57	12.57	2	0.04	0.00	0.01	0.00	0.00	24.0
7	330	-8213	37	240	0	-672	55	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
8	330	-8081	59	141	0	-812	107	6.28	6.28	12.57	12.57	2	0.05	0.00	0.01	0.00	0.00	24.0
9	330	-8207	47	243	0	-712	78	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
10	330	-8138	35	170	0	-689	47	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
11	330	-8176	31	201	0	-660	39	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
12	330	-8118	65	180	0	-824	123	6.28	6.28	12.57	12.57	2	0.05	0.00	0.02	0.00	0.00	24.0
13	330	-8156	62	211	0	-794	115	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
14	330	-8087	50	138	0	-771	84	6.28	6.28	12.57	12.57	2	0.04	0.00	0.01	0.00	0.00	24.0
15	330	-8213	37	240	0	-672	55	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
16	330	-8081	59	141	0	-812	107	6.28	6.28	12.57	12.57	2	0.05	0.00	0.01	0.00	0.00	24.0
17	330	-8207	47	243	0	-712	78	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
18	330	-13130	-239	470	0	-1751	-466	6.28	6.28	12.57	12.57	3	0.07	0.01	0.04	0.00	0.00	24.0
19	330	-13950	246	632	0	-2725	355	6.28	6.28	12.57	12.57	3	0.10	0.01	0.06	0.00	0.00	24.0
20	330	-13170	-15	-595	0	-6451	-90	6.28	6.28	12.57	12.57	3	0.23	0.01	0.06	0.00	0.00	24.0
37	330	-11950	-380	318	0	-1015	-684	6.28	6.28	12.57	12.57	3	0.05	0.01	0.03	0.00	0.00	24.0
38	330	-13300	428	588	0	-2639	685	6.28	6.28	12.57	12.57	3	0.10	0.01	0.06	0.00	0.00	24.0
39	330	-12000	-6	-1458	0	-8848	-58	6.28	6.28	12.57	12.57	3	0.31	0.03	0.14	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

VERIFICA NODO IN TESTA AL PILASTRO, NODO NUM. 39 NON CONFINATO

(par.7.2.2 NTC2018 "La domanda di resistenza valutata con i criteri della progettazione in capacità può essere assunta non superiore alla domanda di resistenza valutata per il caso di comportamento strutturale non dissipativo.")

PROGETTAZIONE IN CAPACITA'

Asse loc. pilastro y nodo INTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 50.0 cm, hjc= 30.0 cm

Asse loc. pilastro z nodo: --

FxMin,inf	FxMin,sup	FxMax,sup	FySup	FzSup	Vjbdy	Vjbdz	Vres,y	Vres,z	I.R.compr.	Ashy	Ashz	PASSO	Nota
daN					daN		daN			cmq		cm	
-8081	-4171	-4284	675	351	34558	--	129916	--	0.27	8.77	--	5.18	

VERIFICA DI RESISTENZA CON SOLLECITAZIONI COMPORTAMENTO NON DISSIPATIVO

Asse loc. pilastro y nodo INTERNO: Hjw= 40.0 cm, bj= 50.0 cm, hjc= 30.0 cm, db1= 45.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb,1	Mb,2	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-4192	-8138	-1901	-2246	677	175	129945	0.00	0.00	40.00	
3	-4223	-8176	-1905	-2257	675	194	129935	0.00	0.00	40.00	
4	-4233	-8118	-1810	-2208	727	256	129932	0.00	0.00	40.00	
5	-4263	-8156	-1814	-2219	726	275	129922	0.00	0.00	40.00	
6	-4171	-8087	-1863	-2220	696	185	129951	0.00	0.00	40.00	
7	-4272	-8213	-1879	-2257	691	243	129919	0.00	0.00	40.00	
8	-4183	-8081	-1836	-2208	712	207	129947	0.00	0.00	40.00	
9	-4284	-8207	-1851	-2245	706	267	129916	0.00	0.00	40.00	

10	-4192	-8138	-1901	-2246	677	175	129945	0.00	0.00	40.00
11	-4223	-8176	-1905	-2257	675	194	129935	0.00	0.00	40.00
12	-4233	-8118	-1810	-2208	727	256	129932	0.00	0.00	40.00
13	-4263	-8156	-1814	-2219	726	275	129922	0.00	0.00	40.00
14	-4171	-8087	-1863	-2220	696	185	129951	0.00	0.00	40.00
15	-4272	-8213	-1879	-2257	691	243	129919	0.00	0.00	40.00
16	-4183	-8081	-1836	-2208	712	207	129947	0.00	0.00	40.00
17	-4284	-8207	-1851	-2245	706	267	129916	0.00	0.00	40.00

CONFRONTO E SINTESI CONCLUSIVE (si assume in ogni caso passo <= 15 cm)

I.R.compr.	Ashy	Ashz	PASSO	Nota
	cmq		cm	
0.00	--	--	15.00	**VERIFICATO**

ASTA NUM. 8 NI 40 NF 34 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 12B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-19200	-153	123	0	160	403	6.28	6.28	12.57	12.57	3	0.02	0.00	0.01	0.00	0.00	24.0
2	0	-14800	-110	94	0	54	295	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
3	0	-14810	-109	126	0	272	293	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
4	0	-14730	-126	64	0	-26	327	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
5	0	-14740	-125	96	0	193	325	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
6	0	-14760	-117	46	0	-229	309	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
7	0	-14800	-113	152	0	500	301	6.28	6.28	12.57	12.57	2	0.03	0.00	0.01	0.00	0.00	24.0
8	0	-14740	-122	37	0	-253	319	6.28	6.28	12.57	12.57	2	0.03	0.00	0.01	0.00	0.00	24.0
9	0	-14780	-118	144	0	476	311	6.28	6.28	12.57	12.57	2	0.03	0.00	0.01	0.00	0.00	24.0
10	0	-14800	-110	94	0	54	295	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
11	0	-14810	-109	126	0	272	293	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
12	0	-14730	-126	64	0	-26	327	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
13	0	-14740	-125	96	0	193	325	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
14	0	-14760	-117	46	0	-229	309	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
15	0	-14800	-113	152	0	500	301	6.28	6.28	12.57	12.57	2	0.03	0.00	0.01	0.00	0.00	24.0
16	0	-14740	-122	37	0	-253	319	6.28	6.28	12.57	12.57	2	0.03	0.00	0.01	0.00	0.00	24.0
17	0	-14780	-118	144	0	476	311	6.28	6.28	12.57	12.57	2	0.03	0.00	0.01	0.00	0.00	24.0
18	0	-22150	-22	413	0	738	138	6.28	6.28	12.57	12.57	3	0.03	0.01	0.04	0.00	0.00	24.0
19	0	-20450	-305	128	0	3	710	6.28	6.28	12.57	12.57	3	0.04	0.01	0.03	0.00	0.00	24.0
20	0	-20910	-148	3182	0	2738	386	6.28	6.28	12.57	12.57	3	0.10	0.05	0.28	0.00	0.00	24.0
37	0	-22140	76	461	0	917	-58	6.28	6.28	12.57	12.57	3	0.03	0.01	0.04	0.00	0.00	24.0
38	0	-19300	-397	-14	0	-308	895	6.28	6.28	12.57	12.57	3	0.05	0.01	0.03	0.00	0.00	24.0
39	0	-20070	-134	5075	0	4251	354	6.28	6.28	12.57	12.57	3	0.15	0.09	0.44	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	110	-18342	-153	123	0	25	235	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
2	110	-14140	-110	94	0	-49	174	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
3	110	-14150	-109	126	0	134	173	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
4	110	-14070	-126	64	0	-96	189	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
5	110	-14080	-125	96	0	87	187	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
6	110	-14100	-117	46	0	-280	181	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
7	110	-14140	-113	152	0	332	177	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
8	110	-14080	-122	37	0	-294	185	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
9	110	-14120	-118	144	0	318	181	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
10	110	-14140	-110	94	0	-49	174	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
11	110	-14150	-109	126	0	134	173	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
12	110	-14070	-126	64	0	-96	189	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
13	110	-14080	-125	96	0	87	187	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
14	110	-14100	-117	46	0	-280	181	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
15	110	-14140	-113	152	0	332	177	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
16	110	-14080	-122	37	0	-294	185	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
17	110	-14120	-118	144	0	318	181	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
18	110	-21292	-22	413	0	283	115	6.28	6.28	12.57	12.57	3	0.01	0.01	0.04	0.00	0.00	24.0
19	110	-19592	-305	128	0	-138	375	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
20	110	-20052	-148	2578	0	-430	223	6.28	6.28	12.57	12.57	3	0.02	0.04	0.23	0.00	0.00	24.0
37	110	-21282	76	461	0	409	26	6.28	6.28	12.57	12.57	3	0.01	0.01	0.04	0.00	0.00	24.0
38	110	-18442	-397	-14	0	-293	459	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
39	110	-19212	-134	4068	0	-778	207	6.28	6.28	12.57	12.57	3	0.03	0.07	0.36	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	220	-17485	-153	123	0	-111	67	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
2	220	-13480	-110	94	0	-153	53	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
3	220	-13490	-109	126	0	-4	53	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
4	220	-13410	-126	64	0	-167	50	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
5	220	-13420	-125	96	0	-18	50	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
6	220	-13440	-117	46	0	-331	52	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
7	220	-13480	-113	152	0	164	52	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
8	220	-13420	-122	37	0	-335	51	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
9	220	-13460	-118	144	0	160	51	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
10	220	-13480	-110	94	0	-153	53	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
11	220	-13490	-109	126	0	-4	53	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
12	220	-13410	-126	64	0	-167	50	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
13	220	-13420	-125	96	0	-18	50	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
14	220	-13440	-117	46	0	-331	52	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
15	220	-13480	-113	152	0	164	52	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
16	220	-13420	-122	37	0	-335	51	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
17	220	-13460	-118	144	0	160	51	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
18	220	-20435	-22	413	0	-171	91	6.28	6.28	12.57	12.57	3	0.01	0.01	0.04	0.00	0.00	24.0
19	220	-18735	-305	128	0	-279	39	6.28	6.28	12.57	12.57	3	0.01	0.01	0.02	0.00	0.00	24.0
20	220	-19195	-148	1974	0	-2933	61	6.28	6.28	12.57	12.57	3	0.10	0.03	0.17	0.00	0.00	24.0
37	220	-20425	76	461	0	-98	109	6.28	6.28	12.57	12.57	3	0.01	0.01	0.04	0.00	0.00	24.0
38	220	-17585	-397	-14	0	-277	22	6.28	6.28	12.57	12.57	3	0.01	0.01	0.03	0.00	0.00	24.0
39	220	-18355	-134	3062	0	-4700	59	6.28	6.28	12.57	12.57	3	0.16	0.05	0.27	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	330	-16628	-153	123	0	-247	-101	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
2	330	-12820	-110	94	0	-256	-68	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
3	330	-12830	-109	126	0	-142	-67	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0

4	330	-12750	-126	64	0	-238	-88	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
5	330	-12760	-125	96	0	-124	-87	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
6	330	-12780	-117	46	0	-382	-76	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
7	330	-12820	-113	152	0	-3	-73	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
8	330	-12760	-122	37	0	-377	-82	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
9	330	-12800	-118	144	0	2	-79	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
10	330	-12820	-110	94	0	-256	-68	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
11	330	-12830	-109	126	0	-142	-67	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
12	330	-12750	-126	64	0	-238	-88	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
13	330	-12760	-125	96	0	-124	-87	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
14	330	-12780	-117	46	0	-382	-76	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
15	330	-12820	-113	152	0	-3	-73	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
16	330	-12760	-122	37	0	-377	-82	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
17	330	-12800	-118	144	0	2	-79	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
18	330	-19578	-22	413	0	-626	67	6.28	6.28	12.57	12.57	3	0.02	0.01	0.04	0.00	0.00	24.0
19	330	-17878	-305	128	0	-420	-297	6.28	6.28	12.57	12.57	3	0.02	0.01	0.02	0.00	0.00	24.0
20	330	-18338	-148	1369	0	-4771	-101	6.28	6.28	12.57	12.57	3	0.16	0.02	0.12	0.00	0.00	24.0
37	330	-19568	76	461	0	-606	192	6.28	6.28	12.57	12.57	3	0.02	0.01	0.04	0.00	0.00	24.0
38	330	-16728	-397	-14	0	-262	-414	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
39	330	-17498	-134	2055	0	-7514	-88	6.28	6.28	12.57	12.57	3	0.26	0.04	0.19	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	440	-15770	-153	123	0	-383	-269	6.28	6.28	12.57	12.57	3	0.02	0.00	0.01	0.00	0.00	24.0
2	440	-12160	-110	94	0	-359	-189	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
3	440	-12170	-109	126	0	-281	-187	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
4	440	-12090	-126	64	0	-308	-227	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
5	440	-12100	-125	96	0	-230	-225	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
6	440	-12120	-117	46	0	-433	-204	6.28	6.28	12.57	12.57	2	0.03	0.00	0.01	0.00	0.00	24.0
7	440	-12160	-113	152	0	-171	-198	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
8	440	-12100	-122	37	0	-418	-216	6.28	6.28	12.57	12.57	2	0.03	0.00	0.01	0.00	0.00	24.0
9	440	-12140	-118	144	0	-156	-209	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
10	440	-12160	-110	94	0	-359	-189	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
11	440	-12170	-109	126	0	-281	-187	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
12	440	-12090	-126	64	0	-308	-227	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
13	440	-12100	-125	96	0	-230	-225	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
14	440	-12120	-117	46	0	-433	-204	6.28	6.28	12.57	12.57	2	0.03	0.00	0.01	0.00	0.00	24.0
15	440	-12160	-113	152	0	-171	-198	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
16	440	-12100	-122	37	0	-418	-216	6.28	6.28	12.57	12.57	2	0.03	0.00	0.01	0.00	0.00	24.0
17	440	-12140	-118	144	0	-156	-209	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
18	440	-18720	-22	413	0	-1080	43	6.28	6.28	12.57	12.57	3	0.04	0.01	0.04	0.00	0.00	24.0
19	440	-17020	-305	128	0	-561	-632	6.28	6.28	12.57	12.57	3	0.04	0.01	0.03	0.00	0.00	24.0
20	440	-17480	-148	765	0	-5945	-264	6.28	6.28	12.57	12.57	3	0.21	0.01	0.07	0.00	0.00	24.0
37	440	-18710	76	461	0	-1113	276	6.28	6.28	12.57	12.57	3	0.04	0.01	0.04	0.00	0.00	24.0
38	440	-15870	-397	-14	0	-247	-850	6.28	6.28	12.57	12.57	3	0.05	0.01	0.03	0.00	0.00	24.0
39	440	-16640	-134	1048	0	-9221	-236	6.28	6.28	12.57	12.57	3	0.32	0.02	0.10	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

VERIFICA NODO IN TESTA AL PILASTRO, NODO NUM. 34 NON CONFINATO

(par.7.2.2 NTC2018 "La domanda di resistenza valutata con i criteri della progettazione in capacità può essere assunta non superiore alla domanda di resistenza valutata per il caso di comportamento strutturale non dissipativo.")

PROGETTAZIONE IN CAPACITA'

Asse loc. pilastro y nodo INTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 50.0 cm, hjc= 30.0 cm
Asse loc. pilastro z nodo: --

FxMin,inf	FxMin,sup	FxMax,sup	FySup	FzSup	Vjbdy	Vjbdz	Vres,y	Vres,z	I.R.compr.	Ashy	Ashz	PASSO	Nota
daN					daN		daN			cmq		cm	
-12090	-8260	-8328	247	124	34986	--	128632	--	0.27	8.70	--	5.23	

VERIFICA DI RESISTENZA CON SOLLECITAZIONI COMPORTAMENTO NON DISSIPATIVO

Asse loc. pilastro y nodo INTERNO: Hjw= 40.0 cm, bj= 50.0 cm, hjc= 30.0 cm, db1= 45.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb,1	Mb,2	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-8317	-12160	-1443	-2012	266	1139	128636	0.01	0.00	40.00	
3	-8328	-12170	-1447	-2012	265	1130	128632	0.01	0.00	40.00	
4	-8260	-12090	-1421	-2019	248	1229	128654	0.01	0.00	40.00	
5	-8271	-12100	-1425	-2019	247	1220	128651	0.01	0.00	40.00	
6	-8284	-12120	-1431	-2013	261	1176	128646	0.01	0.00	40.00	
7	-8321	-12160	-1444	-2015	257	1153	128635	0.01	0.00	40.00	
8	-8267	-12100	-1424	-2015	256	1204	128652	0.01	0.00	40.00	
9	-8303	-12140	-1437	-2018	252	1183	128640	0.01	0.00	40.00	
10	-8317	-12160	-1443	-2012	266	1139	128636	0.01	0.00	40.00	
11	-8328	-12170	-1447	-2012	265	1130	128632	0.01	0.00	40.00	
12	-8260	-12090	-1421	-2019	248	1229	128654	0.01	0.00	40.00	
13	-8271	-12100	-1425	-2019	247	1220	128651	0.01	0.00	40.00	
14	-8284	-12120	-1431	-2013	261	1176	128646	0.01	0.00	40.00	
15	-8321	-12160	-1444	-2015	257	1153	128635	0.01	0.00	40.00	
16	-8267	-12100	-1424	-2015	256	1204	128652	0.01	0.00	40.00	
17	-8303	-12140	-1437	-2018	252	1183	128640	0.01	0.00	40.00	

CONFRONTO E SINTESI CONCLUSIVE (si assume in ogni caso passo <= 15 cm)

I.R.compr.	Ashy	Ashz	PASSO	Nota
	cmq		cm	
0.01	--	--	15.00	**VERIFICATO**

ASTA NUM. 9 NI 41 NF 36 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 17B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza	aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m	cm
1	0	-19280	7	300	0	521	13	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0

2	0	-14830	14	219	0	305	-11	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
3	0	-14880	14	243	0	508	-9	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
4	0	-14780	-3	218	0	293	29	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
5	0	-14830	-4	242	0	497	30	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
6	0	-14760	9	190	0	63	2	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
7	0	-14910	7	271	0	742	6	6.28	6.28	12.57	12.57	2	0.04	0.00	0.03	0.00	0.00	24.0
8	0	-14740	4	190	0	60	13	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
9	0	-14900	1	271	0	738	18	6.28	6.28	12.57	12.57	2	0.04	0.00	0.03	0.00	0.00	24.0
10	0	-14830	14	219	0	305	-11	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
11	0	-14880	14	243	0	508	-9	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
12	0	-14780	-3	218	0	293	29	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
13	0	-14830	-4	242	0	497	30	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
14	0	-14760	9	190	0	63	2	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
15	0	-14910	7	271	0	742	6	6.28	6.28	12.57	12.57	2	0.04	0.00	0.03	0.00	0.00	24.0
16	0	-14740	4	190	0	60	13	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
17	0	-14900	1	271	0	738	18	6.28	6.28	12.57	12.57	2	0.04	0.00	0.03	0.00	0.00	24.0
18	0	-22660	195	698	0	1293	-375	6.28	6.28	12.57	12.57	3	0.05	0.01	0.06	0.00	0.00	24.0
19	0	-21490	-134	606	0	1053	302	6.28	6.28	12.57	12.57	3	0.04	0.01	0.05	0.00	0.00	24.0
20	0	-21750	22	3951	0	4181	-19	6.28	6.28	12.57	12.57	3	0.14	0.07	0.34	0.00	0.00	24.0
37	0	-22180	297	614	0	1163	-585	6.28	6.28	12.57	12.57	3	0.05	0.01	0.05	0.00	0.00	24.0
38	0	-20220	-252	462	0	763	544	6.28	6.28	12.57	12.57	3	0.04	0.01	0.04	0.00	0.00	24.0
39	0	-20660	9	6037	0	5976	9	6.28	6.28	12.57	12.57	3	0.20	0.10	0.52	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	110	-18420	7	300	0	191	20	6.28	6.28	12.57	12.57	3	0.01	0.01	0.03	0.00	0.00	24.0
2	110	-14170	14	219	0	64	5	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
3	110	-14220	14	243	0	241	6	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
4	110	-14120	-3	218	0	53	25	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
5	110	-14170	-4	242	0	230	26	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
6	110	-14100	9	190	0	-146	11	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
7	110	-14250	7	271	0	444	14	6.28	6.28	12.57	12.57	2	0.02	0.00	0.03	0.00	0.00	24.0
8	110	-14080	4	190	0	-149	17	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
9	110	-14240	1	271	0	440	20	6.28	6.28	12.57	12.57	2	0.02	0.00	0.03	0.00	0.00	24.0
10	110	-14170	14	219	0	64	5	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
11	110	-14220	14	243	0	241	6	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
12	110	-14120	-3	218	0	53	25	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
13	110	-14170	-4	242	0	230	26	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
14	110	-14100	9	190	0	-146	11	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
15	110	-14250	7	271	0	444	14	6.28	6.28	12.57	12.57	2	0.02	0.00	0.03	0.00	0.00	24.0
16	110	-14080	4	190	0	-149	17	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
17	110	-14240	1	271	0	440	20	6.28	6.28	12.57	12.57	2	0.02	0.00	0.03	0.00	0.00	24.0
18	110	-21802	195	698	0	526	-161	6.28	6.28	12.57	12.57	3	0.02	0.01	0.06	0.00	0.00	24.0
19	110	-20632	-134	606	0	386	154	6.28	6.28	12.57	12.57	3	0.02	0.01	0.05	0.00	0.00	24.0
20	110	-20892	22	3347	0	167	5	6.28	6.28	12.57	12.57	3	0.01	0.06	0.29	0.00	0.00	24.0
37	110	-21320	297	614	0	487	-259	6.28	6.28	12.57	12.57	3	0.02	0.01	0.05	0.00	0.00	24.0
38	110	-19362	-252	462	0	254	267	6.28	6.28	12.57	12.57	3	0.02	0.01	0.04	0.00	0.00	24.0
39	110	-19800	9	5030	0	-112	19	6.28	6.28	12.57	12.57	3	0.00	0.09	0.44	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	220	-17560	7	300	0	-138	28	6.28	6.28	12.57	12.57	3	0.01	0.01	0.03	0.00	0.00	24.0
2	220	-13510	14	219	0	-176	21	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
3	220	-13560	14	243	0	-26	21	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
4	220	-13460	-3	218	0	-187	22	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
5	220	-13510	-4	242	0	-37	22	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
6	220	-13440	9	190	0	-355	21	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
7	220	-13590	7	271	0	146	21	6.28	6.28	12.57	12.57	2	0.01	0.00	0.03	0.00	0.00	24.0
8	220	-13420	4	190	0	-359	21	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
9	220	-13580	1	271	0	142	21	6.28	6.28	12.57	12.57	2	0.01	0.00	0.03	0.00	0.00	24.0
10	220	-13510	14	219	0	-176	21	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
11	220	-13560	14	243	0	-26	21	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
12	220	-13460	-3	218	0	-187	22	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
13	220	-13510	-4	242	0	-37	22	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
14	220	-13440	9	190	0	-355	21	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
15	220	-13590	7	271	0	146	21	6.28	6.28	12.57	12.57	2	0.01	0.00	0.03	0.00	0.00	24.0
16	220	-13420	4	190	0	-359	21	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
17	220	-13580	1	271	0	142	21	6.28	6.28	12.57	12.57	2	0.01	0.00	0.03	0.00	0.00	24.0
18	220	-20945	195	698	0	-242	53	6.28	6.28	12.57	12.57	3	0.01	0.01	0.06	0.00	0.00	24.0
19	220	-19775	-134	606	0	-281	7	6.28	6.28	12.57	12.57	3	0.01	0.01	0.05	0.00	0.00	24.0
20	220	-20035	22	2743	0	-3183	30	6.28	6.28	12.57	12.57	3	0.11	0.05	0.24	0.00	0.00	24.0
37	220	-20460	297	614	0	-189	68	6.28	6.28	12.57	12.57	3	0.01	0.01	0.05	0.00	0.00	24.0
38	220	-18505	-252	462	0	-254	-9	6.28	6.28	12.57	12.57	3	0.01	0.01	0.04	0.00	0.00	24.0
39	220	-18940	9	4024	0	-5092	29	6.28	6.28	12.57	12.57	3	0.17	0.07	0.36	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	330	-16700	7	300	0	-468	35	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
2	330	-12850	14	219	0	-417	37	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
3	330	-12900	14	243	0	-293	36	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
4	330	-12800	-3	218	0	-427	18	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
5	330	-12850	-4	242	0	-303	17	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
6	330	-12780	9	190	0	-565	31	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
7	330	-12930	7	271	0	-152	29	6.28	6.28	12.57	12.57	2	0.01	0.00	0.03	0.00	0.00	24.0
8	330	-12760	4	190	0	-568	25	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
9	330	-12920	1	271	0	-155	23	6.28	6.28	12.57	12.57	2	0.01	0.00	0.03	0.00	0.00	24.0
10	330	-12850	14	219	0	-417	37	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
11	330	-12900	14	243	0	-293	36	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
12	330	-12800	-3	218	0	-427	18	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
13	330	-12850	-4	242	0	-303	17	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
14	330	-12780	9	190	0	-565	31	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
15	330	-12930	7	271	0	-152	29	6.28	6.28	12.57	12.57	2	0.01	0.00	0.03	0.00	0.00	24.0
16	330	-12760	4	190	0	-568	25	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
17	330	-12920	1	271	0	-155	23	6.28	6.28	12.57	12.57	2	0.01	0.00	0.03	0.00	0.00	24.0
18	330	-20088	195	698	0	-1009	267	6.28	6.28	12.57	12.57	3	0.04	0.01	0.06	0.00	0.00	24.0
19	330	-18918	-134	606	0	-948	-141	6.28	6.28	12.57	12.57	3	0.03	0.01	0.05	0.00	0.00	24.0
20	330	-19178	22	2139	0	-5868	54	6.28	6.28	12.57	12.57	3	0.20	0.04	0.19	0.00	0.00	24.0
37	330	-19600	297	614	0	-864	394	6.28	6.28	12.57	12.57	3	0.04	0.01	0.05	0.00	0.00	24.0
38	330	-17648	-252	462	0	-762	-286	6.28	6.28	12.57	12.57	3	0.03	0.01	0.04	0.00	0.00	24.0
39	330	-18080	9	3017	0	-8965	38	6.28	6.28	12.57	12.57	3	0.31	0.05	0.27	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	440	-15840	7	300	0	-798	43	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
2	440	-12190	14	219	0	-657	53	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
3	440	-12240	14	243	0	-560	52	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
4	440	-12140	-3	218	0	-667	14	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
5	440	-12190	-4	242	0	-570	13	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
6	440	-12120	9	190	0	-774	41	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
7	440	-12270	7	271	0	-450	36	6.28	6.28	12.57	12.57	2	0.02	0.00	0.03	0.00	0.00	24.0

8	440	-12100	4	190	0	-777	29	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
9	440	-12260	1	271	0	-453	25	6.28	6.28	12.57	12.57	2	0.02	0.00	0.03	0.00	0.00	24.0
10	440	-12190	14	219	0	-657	53	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
11	440	-12240	14	243	0	-560	52	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
12	440	-12140	-3	218	0	-667	14	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
13	440	-12190	-4	242	0	-570	13	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
14	440	-12120	9	190	0	-774	41	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
15	440	-12270	7	271	0	-450	36	6.28	6.28	12.57	12.57	2	0.02	0.00	0.03	0.00	0.00	24.0
16	440	-12100	4	190	0	-777	29	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
17	440	-12260	1	271	0	-453	25	6.28	6.28	12.57	12.57	2	0.02	0.00	0.03	0.00	0.00	24.0
18	440	-19230	195	698	0	-1776	482	6.28	6.28	12.57	12.57	3	0.07	0.01	0.06	0.00	0.00	24.0
19	440	-18060	-134	606	0	-1615	-289	6.28	6.28	12.57	12.57	3	0.06	0.01	0.05	0.00	0.00	24.0
20	440	-18320	22	1535	0	-7889	78	6.28	6.28	12.57	12.57	3	0.27	0.03	0.14	0.00	0.00	24.0
37	440	-18740	297	614	0	-1540	721	6.28	6.28	12.57	12.57	3	0.07	0.01	0.05	0.00	0.00	24.0
38	440	-16790	-252	462	0	-1271	-563	6.28	6.28	12.57	12.57	3	0.05	0.01	0.04	0.00	0.00	24.0
39	440	-17220	9	2010	0	-11730	48	6.28	6.28	12.57	12.57	3	0.40	0.03	0.18	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

VERIFICA NODO IN TESTA AL PILASTRO, NODO NUM. 36 NON CONFINATO

(par.7.2.2 NTC2018 "La domanda di resistenza valutata con i criteri della progettazione in capacità può essere assunta non superiore alla domanda di resistenza valutata per il caso di comportamento strutturale non dissipativo.")

PROGETTAZIONE IN CAPACITA'

Asse loc. pilastro y nodo INTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 50.0 cm, hjc= 30.0 cm

Asse loc. pilastro z nodo: --

FxMin,inf	FxMin,sup	FxMax,sup	FySup	FzSup	Vjbdy	Vjbdz	Vres,y	Vres,z	I.R.compr.	Ashy	Ashz	PASSO	Nota
daN					daN		daN			cmq		cm	
-12100	-8325	-8490	209	198	35024	--	128581	--	0.27	8.70	--	5.23	

VERIFICA DI RESISTENZA CON SOLLECITAZIONI COMPORTAMENTO NON DISSIPATIVO

Asse loc. pilastro y nodo INTERNO: Hjw= 40.0 cm, bj= 50.0 cm, hjc= 30.0 cm, db1= 45.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb,1	Mb,2	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-8410	-12190	-1613	-1806	235	241	128606	0.00	0.00	40.00	
3	-8456	-12240	-1613	-1808	236	246	128592	0.00	0.00	40.00	
4	-8360	-12140	-1604	-1815	209	312	128622	0.00	0.00	40.00	
5	-8405	-12190	-1604	-1817	209	317	128608	0.00	0.00	40.00	
6	-8340	-12120	-1610	-1807	226	261	128629	0.00	0.00	40.00	
7	-8490	-12270	-1610	-1813	227	275	128581	0.00	0.00	40.00	
8	-8325	-12100	-1607	-1809	218	281	128633	0.00	0.00	40.00	
9	-8475	-12260	-1607	-1816	219	297	128585	0.00	0.00	40.00	
10	-8410	-12190	-1613	-1806	235	241	128606	0.00	0.00	40.00	
11	-8456	-12240	-1613	-1808	236	246	128592	0.00	0.00	40.00	
12	-8360	-12140	-1604	-1815	209	312	128622	0.00	0.00	40.00	
13	-8405	-12190	-1604	-1817	209	317	128608	0.00	0.00	40.00	
14	-8340	-12120	-1610	-1807	226	261	128629	0.00	0.00	40.00	
15	-8490	-12270	-1610	-1813	227	275	128581	0.00	0.00	40.00	
16	-8325	-12100	-1607	-1809	218	281	128633	0.00	0.00	40.00	
17	-8475	-12260	-1607	-1816	219	297	128585	0.00	0.00	40.00	

CONFRONTO E SINTESI CONCLUSIVE (si assume in ogni caso passo <= 15 cm)

I.R.compr.	Ashy	Ashz	PASSO	Nota
	cmq		cm	
0.00	--	--	15.00	**VERIFICATO**

ASTA NUM. 10 NI 42 NF 38 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 22B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-21560	98	28	0	-56	-249	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
2	0	-16570	83	-11	0	-187	-207	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
3	0	-16610	81	13	0	26	-202	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
4	0	-16560	69	30	0	-112	-181	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
5	0	-16600	67	55	0	101	-176	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
6	0	-16520	81	-25	0	-410	-204	6.28	6.28	12.57	12.57	2	0.03	0.00	0.01	0.00	0.00	24.0
7	0	-16650	74	56	0	301	-187	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
8	0	-16520	77	-13	0	-387	-196	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
9	0	-16650	70	68	0	324	-179	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
10	0	-16570	83	-11	0	-187	-207	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
11	0	-16610	81	13	0	26	-202	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
12	0	-16560	69	30	0	-112	-181	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
13	0	-16600	67	55	0	101	-176	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
14	0	-16520	81	-25	0	-410	-204	6.28	6.28	12.57	12.57	2	0.03	0.00	0.01	0.00	0.00	24.0
15	0	-16650	74	56	0	301	-187	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
16	0	-16520	77	-13	0	-387	-196	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
17	0	-16650	70	68	0	324	-179	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
18	0	-24050	296	-21	0	-283	-640	6.28	6.28	12.57	12.57	3	0.03	0.01	0.02	0.00	0.00	24.0
19	0	-24840	-5	245	0	363	-37	6.28	6.28	12.57	12.57	3	0.01	0.00	0.02	0.00	0.00	24.0
20	0	-24090	117	2968	0	2256	-272	6.28	6.28	12.57	12.57	3	0.08	0.05	0.25	0.00	0.00	24.0
37	0	-22890	380	-136	0	-528	-811	6.28	6.28	12.57	12.57	3	0.04	0.01	0.03	0.00	0.00	24.0
38	0	-24210	-121	308	0	550	194	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
39	0	-22950	82	4845	0	3705	-198	6.28	6.28	12.57	12.57	3	0.12	0.08	0.41	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	110	-20702	98	28	0	-87	-141	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
2	110	-15910	83	-11	0	-175	-116	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
3	110	-15950	81	13	0	12	-113	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
4	110	-15900	69	30	0	-145	-104	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
5	110	-15940	67	55	0	41	-102	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0

6	110	-15860	81	-25	0	-382	-115	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
7	110	-15990	74	56	0	240	-106	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
8	110	-15860	77	-13	0	-373	-112	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
9	110	-15990	70	68	0	249	-102	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
10	110	-15910	83	-11	0	-175	-116	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
11	110	-15950	81	13	0	12	-113	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
12	110	-15900	69	30	0	-145	-104	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
13	110	-15940	67	55	0	41	-102	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
14	110	-15860	81	-25	0	-382	-115	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
15	110	-15990	74	56	0	240	-106	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
16	110	-15860	77	-13	0	-373	-112	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
17	110	-15990	70	68	0	249	-102	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
18	110	-23190	296	-21	0	-260	-314	6.28	6.28	12.57	12.57	3	0.02	0.01	0.02	0.00	0.00	24.0
19	110	-23982	-5	245	0	93	-42	6.28	6.28	12.57	12.57	3	0.00	0.00	0.02	0.00	0.00	24.0
20	110	-23230	117	2364	0	-677	-143	6.28	6.28	12.57	12.57	3	0.02	0.04	0.20	0.00	0.00	24.0
37	110	-22032	380	-136	0	-378	-393	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
38	110	-23352	-121	308	0	211	61	6.28	6.28	12.57	12.57	3	0.01	0.01	0.03	0.00	0.00	24.0
39	110	-22092	82	3838	0	-1071	-108	6.28	6.28	12.57	12.57	3	0.04	0.06	0.33	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	220	-19845	98	28	0	-118	-34	6.28	6.28	12.57	12.57	3	0.00	0.00	0.01	0.00	0.00	24.0
2	220	-15250	83	-11	0	-163	-24	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
3	220	-15290	81	13	0	-3	-24	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
4	220	-15240	69	30	0	-178	-28	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
5	220	-15280	67	55	0	-19	-28	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
6	220	-15200	81	-25	0	-355	-26	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
7	220	-15330	74	56	0	178	-25	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
8	220	-15200	77	-13	0	-359	-27	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
9	220	-15330	70	68	0	173	-26	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
10	220	-15250	83	-11	0	-163	-24	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
11	220	-15290	81	13	0	-3	-24	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
12	220	-15240	69	30	0	-178	-28	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
13	220	-15280	67	55	0	-19	-28	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
14	220	-15200	81	-25	0	-355	-26	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
15	220	-15330	74	56	0	178	-25	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
16	220	-15200	77	-13	0	-359	-27	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
17	220	-15330	70	68	0	173	-26	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
18	220	-22330	296	-21	0	-237	11	6.28	6.28	12.57	12.57	3	0.01	0.01	0.02	0.00	0.00	24.0
19	220	-23125	-5	245	0	-177	-48	6.28	6.28	12.57	12.57	3	0.01	0.00	0.02	0.00	0.00	24.0
20	220	-22370	117	1760	0	-2945	-15	6.28	6.28	12.57	12.57	3	0.10	0.03	0.15	0.00	0.00	24.0
37	220	-21175	380	-136	0	-228	25	6.28	6.28	12.57	12.57	3	0.01	0.01	0.03	0.00	0.00	24.0
38	220	-22495	-121	308	0	-128	-72	6.28	6.28	12.57	12.57	3	0.01	0.01	0.03	0.00	0.00	24.0
39	220	-21235	82	2831	0	-4740	-18	6.28	6.28	12.57	12.57	3	0.16	0.05	0.24	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	330	-18988	98	28	0	-149	74	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
2	330	-14590	83	-11	0	-151	67	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
3	330	-14630	81	13	0	-17	66	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
4	330	-14580	69	30	0	-212	48	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
5	330	-14620	67	55	0	-79	46	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
6	330	-14540	81	-25	0	-327	63	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
7	330	-14670	74	56	0	116	57	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
8	330	-14540	77	-13	0	-346	57	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
9	330	-14670	70	68	0	98	51	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
10	330	-14590	83	-11	0	-151	67	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
11	330	-14630	81	13	0	-17	66	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
12	330	-14580	69	30	0	-212	48	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
13	330	-14620	67	55	0	-79	46	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
14	330	-14540	81	-25	0	-327	63	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
15	330	-14670	74	56	0	116	57	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
16	330	-14540	77	-13	0	-346	57	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
17	330	-14670	70	68	0	98	51	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
18	330	-21470	296	-21	0	-214	336	6.28	6.28	12.57	12.57	3	0.02	0.01	0.02	0.00	0.00	24.0
19	330	-22268	-5	245	0	-447	-53	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
20	330	-21510	117	1156	0	-4548	114	6.28	6.28	12.57	12.57	3	0.15	0.02	0.10	0.00	0.00	24.0
37	330	-20318	380	-136	0	-78	443	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
38	330	-21638	-121	308	0	-466	-206	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
39	330	-20378	82	1825	0	-7301	73	6.28	6.28	12.57	12.57	3	0.25	0.03	0.16	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	440	-18130	98	28	0	-180	182	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
2	440	-13930	83	-11	0	-138	159	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
3	440	-13970	81	13	0	-32	155	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
4	440	-13920	69	30	0	-245	125	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
5	440	-13960	67	55	0	-138	120	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
6	440	-13880	81	-25	0	-300	152	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
7	440	-14010	74	56	0	55	138	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
8	440	-13880	77	-13	0	-332	142	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
9	440	-14010	70	68	0	23	127	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
10	440	-13930	83	-11	0	-138	159	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
11	440	-13970	81	13	0	-32	155	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
12	440	-13920	69	30	0	-245	125	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
13	440	-13960	67	55	0	-138	120	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
14	440	-13880	81	-25	0	-300	152	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
15	440	-14010	74	56	0	55	138	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
16	440	-13880	77	-13	0	-332	142	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
17	440	-14010	70	68	0	23	127	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
18	440	-20610	296	-21	0	-190	661	6.28	6.28	12.57	12.57	3	0.03	0.01	0.02	0.00	0.00	24.0
19	440	-21410	-5	245	0	-717	-59	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
20	440	-20650	117	552	0	-5487	242	6.28	6.28	12.57	12.57	3	0.19	0.01	0.05	0.00	0.00	24.0
37	440	-19460	380	-136	0	72	861	6.28	6.28	12.57	12.57	3	0.05	0.01	0.03	0.00	0.00	24.0
38	440	-20780	-121	308	0	-805	-339	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
39	440	-19520	82	818	0	-8754	163	6.28	6.28	12.57	12.57	3	0.30	0.01	0.07	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

VERIFICA NODO IN TESTA AL PILASTRO, NODO NUM. 38 NON CONFINATO

(par.7.2.2 NTC2018 "La domanda di resistenza valutata con i criteri della progettazione in capacità può essere assunta non superiore alla domanda di resistenza valutata per il caso di comportamento strutturale non dissipativo.")

PROGETTAZIONE IN CAPACITA'

Asse loc. pilastro y nodo INTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 50.0 cm, hjc= 30.0 cm
Asse loc. pilastro z nodo: --

FxMin,inf	FxMin,sup	FxMax,sup	FySup	FzSup	Vjbdy	Vjbdz	Vres,y	Vres,z	I.R.compr.	Ashy	Ashz	PASSO	Nota
daN					daN		daN			cmq		cm	

-13880	-10060	-10190	31	138	35202	--	128037	--	0.27	8.67	--	5.25

VERIFICA DI RESISTENZA CON SOLLECITAZIONI COMPORTAMENTO NON DISSIPATIVO

Asse loc. pilastro y nodo INTERNO: Hjw= 40.0 cm, bj= 50.0 cm, hjc= 30.0 cm, db1= 45.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb,1	Mb,2	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-10120	-13930	-1855	-1627	35	528	128060	0.00	0.00	40.00	
3	-10160	-13970	-1853	-1634	31	510	128047	0.00	0.00	40.00	
4	-10100	-13920	-1848	-1631	65	470	128066	0.00	0.00	40.00	
5	-10140	-13960	-1846	-1637	62	454	128053	0.00	0.00	40.00	
6	-10070	-13880	-1854	-1621	50	525	128076	0.00	0.00	40.00	
7	-10190	-14010	-1849	-1642	37	474	128037	0.00	0.00	40.00	
8	-10060	-13880	-1852	-1622	59	509	128079	0.00	0.00	40.00	
9	-10190	-14010	-1847	-1643	47	457	128037	0.00	0.00	40.00	
10	-10120	-13930	-1855	-1627	35	528	128060	0.00	0.00	40.00	
11	-10160	-13970	-1853	-1634	31	510	128047	0.00	0.00	40.00	
12	-10100	-13920	-1848	-1631	65	470	128066	0.00	0.00	40.00	
13	-10140	-13960	-1846	-1637	62	454	128053	0.00	0.00	40.00	
14	-10070	-13880	-1854	-1621	50	525	128076	0.00	0.00	40.00	
15	-10190	-14010	-1849	-1642	37	474	128037	0.00	0.00	40.00	
16	-10060	-13880	-1852	-1622	59	509	128079	0.00	0.00	40.00	
17	-10190	-14010	-1847	-1643	47	457	128037	0.00	0.00	40.00	

CONFRONTO E SINTESI CONCLUSIVE (si assume in ogni caso passo <= 15 cm)

I.R.compr.	Ashy	Ashz	PASSO	Nota
	cmq		cm	
0.00	--	--	15.00	**VERIFICATO**

ASTA NUM. 11 NI 48 NF 49 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 31B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice resistenza Fx,M	Bielle	V,Mx	aswta aswto cmq/m	PASSO cm
	cm	daN			daN*m			cmq									
1	0	-22650	446	-27	0	-37	-6598	15.71	15.71	9.42	9.42	3	0.12	0.01	0.03	0.00 0.00	24.0
2	0	-17320	414	-59	0	-126	-5637	15.71	15.71	9.42	9.42	2	0.14	0.01	0.03	0.00 0.00	24.0
3	0	-17270	398	16	0	78	-5517	15.71	15.71	9.42	9.42	2	0.14	0.01	0.03	0.00 0.00	24.0
4	0	-17580	289	-57	0	-135	-4634	15.71	15.71	9.42	9.42	2	0.12	0.00	0.02	0.00 0.00	24.0
5	0	-17530	272	19	0	69	-4514	15.71	15.71	9.42	9.42	2	0.11	0.00	0.02	0.00 0.00	24.0
6	0	-17470	390	-146	0	-367	-5425	15.71	15.71	9.42	9.42	2	0.14	0.00	0.03	0.00 0.00	24.0
7	0	-17300	334	105	0	313	-5027	15.71	15.71	9.42	9.42	2	0.13	0.00	0.03	0.00 0.00	24.0
8	0	-17550	352	-146	0	-370	-5124	15.71	15.71	9.42	9.42	2	0.13	0.00	0.03	0.00 0.00	24.0
9	0	-17380	296	106	0	310	-4726	15.71	15.71	9.42	9.42	2	0.12	0.00	0.02	0.00 0.00	24.0
10	0	-17320	414	-59	0	-126	-5637	15.71	15.71	9.42	9.42	2	0.14	0.01	0.03	0.00 0.00	24.0
11	0	-17270	398	16	0	78	-5517	15.71	15.71	9.42	9.42	2	0.14	0.01	0.03	0.00 0.00	24.0
12	0	-17580	289	-57	0	-135	-4634	15.71	15.71	9.42	9.42	2	0.12	0.00	0.02	0.00 0.00	24.0
13	0	-17530	272	19	0	69	-4514	15.71	15.71	9.42	9.42	2	0.11	0.00	0.02	0.00 0.00	24.0
14	0	-17470	390	-146	0	-367	-5425	15.71	15.71	9.42	9.42	2	0.14	0.00	0.03	0.00 0.00	24.0
15	0	-17300	334	105	0	313	-5027	15.71	15.71	9.42	9.42	2	0.13	0.00	0.03	0.00 0.00	24.0
16	0	-17550	352	-146	0	-370	-5124	15.71	15.71	9.42	9.42	2	0.13	0.00	0.03	0.00 0.00	24.0
17	0	-17380	296	106	0	310	-4726	15.71	15.71	9.42	9.42	2	0.12	0.00	0.02	0.00 0.00	24.0
18	0	-25950	2116	-126	0	-218	-14790	15.71	15.71	9.42	9.42	3	0.26	0.03	0.15	0.00 0.00	24.0
19	0	-30690	-158	-50	0	-116	-10190	15.71	15.71	9.42	9.42	3	0.17	0.00	0.01	0.00 0.00	24.0
20	0	-27590	805	180	0	495	-11480	15.71	15.71	9.42	9.42	3	0.20	0.01	0.06	0.00 0.00	24.0
37	0	-22560	2698	-131	0	-206	-14400	15.71	15.71	9.42	9.42	3	0.25	0.03	0.19	0.00 0.00	24.0
38	0	-30460	-1092	-3	0	-37	-6724	15.71	15.71	9.42	9.42	3	0.11	0.01	0.07	0.00 0.00	24.0
39	0	-25290	514	379	0	982	-8886	15.71	15.71	9.42	9.42	3	0.16	0.01	0.04	0.00 0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	110	-21505	446	-27	0	-8	-6107	15.71	15.71	9.42	9.42	3	0.11	0.01	0.03	0.00	0.00	24.0
2	110	-16440	414	-59	0	-60	-5181	15.71	15.71	9.42	9.42	2	0.13	0.01	0.03	0.00	0.00	24.0
3	110	-16390	398	16	0	61	-5080	15.71	15.71	9.42	9.42	2	0.13	0.01	0.03	0.00	0.00	24.0
4	110	-16700	289	-57	0	-73	-4316	15.71	15.71	9.42	9.42	2	0.11	0.00	0.02	0.00	0.00	24.0
5	110	-16650	272	19	0	48	-4215	15.71	15.71	9.42	9.42	2	0.10	0.00	0.02	0.00	0.00	24.0
6	110	-16590	390	-146	0	-206	-4996	15.71	15.71	9.42	9.42	2	0.13	0.00	0.03	0.00	0.00	24.0
7	110	-16420	334	105	0	198	-4660	15.71	15.71	9.42	9.42	2	0.12	0.00	0.03	0.00	0.00	24.0
8	110	-16670	352	-146	0	-210	-4736	15.71	15.71	9.42	9.42	2	0.12	0.00	0.03	0.00	0.00	24.0
9	110	-16500	296	106	0	194	-4400	15.71	15.71	9.42	9.42	2	0.11	0.00	0.02	0.00	0.00	24.0
10	110	-16440	414	-59	0	-60	-5181	15.71	15.71	9.42	9.42	2	0.13	0.01	0.03	0.00	0.00	24.0
11	110	-16390	398	16	0	61	-5080	15.71	15.71	9.42	9.42	2	0.13	0.01	0.03	0.00	0.00	24.0
12	110	-16700	289	-57	0	-73	-4316	15.71	15.71	9.42	9.42	2	0.11	0.00	0.02	0.00	0.00	24.0
13	110	-16650	272	19	0	48	-4215	15.71	15.71	9.42	9.42	2	0.10	0.00	0.02	0.00	0.00	24.0
14	110	-16590	390	-146	0	-206	-4996	15.71	15.71	9.42	9.42	2	0.13	0.00	0.03	0.00	0.00	24.0
15	110	-16420	334	105	0	198	-4660	15.71	15.71	9.42	9.42	2	0.12	0.00	0.03	0.00	0.00	24.0
16	110	-16670	352	-146	0	-210	-4736	15.71	15.71	9.42	9.42	2	0.12	0.00	0.03	0.00	0.00	24.0
17	110	-16500	296	106	0	194	-4400	15.71	15.71	9.42	9.42	2	0.11	0.00	0.02	0.00	0.00	24.0
18	110	-24805	1908	-126	0	-79	-12578	15.71	15.71	9.42	9.42	3	0.22	0.02	0.13	0.00	0.00	24.0
19	110	-29545	49	-50	0	-61	-10250	15.71	15.71	9.42	9.42	3	0.17	0.00	0.00	0.00	0.00	24.0
20	110	-26445	805	180	0	298	-10596	15.71	15.71	9.42	9.42	3	0.18	0.01	0.06	0.00	0.00	24.0
37	110	-21415	2352	-131	0	-63	-11622	15.71	15.71	9.42	9.42	3	0.20	0.03	0.17	0.00	0.00	24.0
38	110	-29315	-745	-3	0	-34	-7734	15.71	15.71	9.42	9.42	3	0.13	0.01	0.05	0.00	0.00	24.0
39	110	-24148	514	379	0	564	-8321	15.71	15.71	9.42	9.42	3	0.15	0.01	0.04	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	220	-20360	446	-27	0	21	-5617	15.71	15.71	9.42	9.42	3	0.10	0.01	0.03	0.00	0.00	24.0
2	220	-15560	414	-59	0	5	-4725	15.71	15.71	9.42	9.42	2	0.12	0.01	0.03	0.00	0.00	24.0
3	220	-15510	398	16	0	43	-4642	15.71	15.71	9.42	9.42	2	0.12	0.01	0.03	0.00	0.00	24.0
4	220	-15820	289	-57	0	-10	-3999	15.71	15.71	9.42	9.42	2	0.10	0.00	0.02	0.00	0.00	24.0
5	220	-15770	272	19	0	28	-3916	15.71	15.71	9.42	9.42	2	0.10	0.00	0.02	0.00	0.00	24.0
6	220	-15710	390	-146	0	-45	-4567	15.71	15.71	9.42	9.42	2	0.11	0.00	0.03	0.00	0.00	24.0
7	220	-15540	334	105	0	82	-4292	15.71	15.71	9.42	9.42	2	0.11	0.00	0.03	0.00	0.00	24.0
8	220	-15790	352	-146	0	-50	-4349	15.71	15.71	9.42	9.42	2	0.11	0.00	0.03	0.00	0.00	24.0
9	220	-15620	296	106	0	78	-4074	15.71	15.71	9.42	9.42	2	0.10	0.00	0.02	0.00	0.00	24.0

10	220	-15560	414	-59	0	5	-4725	15.71	15.71	9.42	9.42	2	0.12	0.01	0.03	0.00	0.00	24.0
11	220	-15510	398	16	0	43	-4642	15.71	15.71	9.42	9.42	2	0.12	0.01	0.03	0.00	0.00	24.0
12	220	-15820	289	-57	0	-10	-3999	15.71	15.71	9.42	9.42	2	0.10	0.00	0.02	0.00	0.00	24.0
13	220	-15770	272	19	0	28	-3916	15.71	15.71	9.42	9.42	2	0.10	0.00	0.02	0.00	0.00	24.0
14	220	-15710	390	-146	0	-45	-4567	15.71	15.71	9.42	9.42	2	0.11	0.00	0.03	0.00	0.00	24.0
15	220	-15540	334	105	0	82	-4292	15.71	15.71	9.42	9.42	2	0.11	0.00	0.03	0.00	0.00	24.0
16	220	-15790	352	-146	0	-50	-4349	15.71	15.71	9.42	9.42	2	0.11	0.00	0.03	0.00	0.00	24.0
17	220	-15620	296	106	0	78	-4074	15.71	15.71	9.42	9.42	2	0.10	0.00	0.02	0.00	0.00	24.0
18	220	-23660	1700	-126	0	60	-10595	15.71	15.71	9.42	9.42	3	0.18	0.02	0.12	0.00	0.00	24.0
19	220	-28400	257	-50	0	-6	-10080	15.71	15.71	9.42	9.42	3	0.17	0.00	0.02	0.00	0.00	24.0
20	220	-25300	805	180	0	100	-9712	15.71	15.71	9.42	9.42	3	0.17	0.01	0.06	0.00	0.00	24.0
37	220	-20270	2005	-131	0	81	-9226	15.71	15.71	9.42	9.42	3	0.16	0.03	0.15	0.00	0.00	24.0
38	220	-28170	-399	-3	0	-30	-8363	15.71	15.71	9.42	9.42	3	0.14	0.00	0.03	0.00	0.00	24.0
39	220	-23005	514	379	0	147	-7756	15.71	15.71	9.42	9.42	3	0.14	0.01	0.04	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	330	-19215	446	-27	0	51	-5126	15.71	15.71	9.42	9.42	3	0.09	0.01	0.03	0.00	0.00	24.0
2	330	-14680	414	-59	0	70	-4269	15.71	15.71	9.42	9.42	2	0.11	0.01	0.03	0.00	0.00	24.0
3	330	-14630	398	16	0	26	-4204	15.71	15.71	9.42	9.42	2	0.10	0.01	0.03	0.00	0.00	24.0
4	330	-14940	289	-57	0	52	-3681	15.71	15.71	9.42	9.42	2	0.09	0.00	0.02	0.00	0.00	24.0
5	330	-14890	272	19	0	7	-3617	15.71	15.71	9.42	9.42	2	0.09	0.00	0.02	0.00	0.00	24.0
6	330	-14830	390	-146	0	116	-4138	15.71	15.71	9.42	9.42	2	0.10	0.00	0.03	0.00	0.00	24.0
7	330	-14660	334	105	0	-33	-3924	15.71	15.71	9.42	9.42	2	0.10	0.00	0.03	0.00	0.00	24.0
8	330	-14910	352	-146	0	111	-3962	15.71	15.71	9.42	9.42	2	0.10	0.00	0.03	0.00	0.00	24.0
9	330	-14740	296	106	0	-38	-3748	15.71	15.71	9.42	9.42	2	0.09	0.00	0.02	0.00	0.00	24.0
10	330	-14680	414	-59	0	70	-4269	15.71	15.71	9.42	9.42	2	0.11	0.01	0.03	0.00	0.00	24.0
11	330	-14630	398	16	0	26	-4204	15.71	15.71	9.42	9.42	2	0.10	0.01	0.03	0.00	0.00	24.0
12	330	-14940	289	-57	0	52	-3681	15.71	15.71	9.42	9.42	2	0.09	0.00	0.02	0.00	0.00	24.0
13	330	-14890	272	19	0	7	-3617	15.71	15.71	9.42	9.42	2	0.09	0.00	0.02	0.00	0.00	24.0
14	330	-14830	390	-146	0	116	-4138	15.71	15.71	9.42	9.42	2	0.10	0.00	0.03	0.00	0.00	24.0
15	330	-14660	334	105	0	-33	-3924	15.71	15.71	9.42	9.42	2	0.10	0.00	0.03	0.00	0.00	24.0
16	330	-14910	352	-146	0	111	-3962	15.71	15.71	9.42	9.42	2	0.10	0.00	0.03	0.00	0.00	24.0
17	330	-14740	296	106	0	-38	-3748	15.71	15.71	9.42	9.42	2	0.09	0.00	0.02	0.00	0.00	24.0
18	330	-22515	1492	-126	0	199	-8840	15.71	15.71	9.42	9.42	3	0.16	0.02	0.11	0.00	0.00	24.0
19	330	-27255	465	-50	0	49	-9683	15.71	15.71	9.42	9.42	3	0.17	0.01	0.03	0.00	0.00	24.0
20	330	-24155	805	180	0	-98	-8828	15.71	15.71	9.42	9.42	3	0.15	0.01	0.06	0.00	0.00	24.0
37	330	-19125	1658	-131	0	225	-7210	15.71	15.71	9.42	9.42	3	0.13	0.02	0.12	0.00	0.00	24.0
38	330	-27025	-52	-3	0	-26	-8611	15.71	15.71	9.42	9.42	3	0.15	0.00	0.00	0.00	0.00	24.0
39	330	-21862	514	379	0	-270	-7190	15.71	15.71	9.42	9.42	3	0.13	0.01	0.04	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	440	-18070	446	-27	0	80	-4635	15.71	15.71	9.42	9.42	3	0.08	0.01	0.03	0.00	0.00	24.0
2	440	-13800	414	-59	0	136	-3813	15.71	15.71	9.42	9.42	2	0.10	0.01	0.03	0.00	0.00	24.0
3	440	-13750	398	16	0	8	-3767	15.71	15.71	9.42	9.42	2	0.09	0.01	0.03	0.00	0.00	24.0
4	440	-14060	289	-57	0	115	-3364	15.71	15.71	9.42	9.42	2	0.09	0.00	0.02	0.00	0.00	24.0
5	440	-14010	272	19	0	-13	-3318	15.71	15.71	9.42	9.42	2	0.08	0.00	0.02	0.00	0.00	24.0
6	440	-13950	390	-146	0	277	-3709	15.71	15.71	9.42	9.42	2	0.10	0.00	0.03	0.00	0.00	24.0
7	440	-13780	334	105	0	-148	-3557	15.71	15.71	9.42	9.42	2	0.09	0.00	0.03	0.00	0.00	24.0
8	440	-14030	352	-146	0	271	-3574	15.71	15.71	9.42	9.42	2	0.09	0.00	0.03	0.00	0.00	24.0
9	440	-13860	296	106	0	-154	-3422	15.71	15.71	9.42	9.42	2	0.09	0.00	0.02	0.00	0.00	24.0
10	440	-13800	414	-59	0	136	-3813	15.71	15.71	9.42	9.42	2	0.10	0.01	0.03	0.00	0.00	24.0
11	440	-13750	398	16	0	8	-3767	15.71	15.71	9.42	9.42	2	0.09	0.01	0.03	0.00	0.00	24.0
12	440	-14060	289	-57	0	115	-3364	15.71	15.71	9.42	9.42	2	0.09	0.00	0.02	0.00	0.00	24.0
13	440	-14010	272	19	0	-13	-3318	15.71	15.71	9.42	9.42	2	0.08	0.00	0.02	0.00	0.00	24.0
14	440	-13950	390	-146	0	277	-3709	15.71	15.71	9.42	9.42	2	0.10	0.00	0.03	0.00	0.00	24.0
15	440	-13780	334	105	0	-148	-3557	15.71	15.71	9.42	9.42	2	0.09	0.00	0.03	0.00	0.00	24.0
16	440	-14030	352	-146	0	271	-3574	15.71	15.71	9.42	9.42	2	0.09	0.00	0.03	0.00	0.00	24.0
17	440	-13860	296	106	0	-154	-3422	15.71	15.71	9.42	9.42	2	0.09	0.00	0.02	0.00	0.00	24.0
18	440	-21370	1284	-126	0	338	-7314	15.71	15.71	9.42	9.42	3	0.13	0.02	0.09	0.00	0.00	24.0
19	440	-26110	673	-50	0	104	-9056	15.71	15.71	9.42	9.42	3	0.16	0.01	0.05	0.00	0.00	24.0
20	440	-23010	805	180	0	-295	-7944	15.71	15.71	9.42	9.42	3	0.14	0.01	0.06	0.00	0.00	24.0
37	440	-17980	1312	-131	0	368	-5576	15.71	15.71	9.42	9.42	3	0.10	0.02	0.10	0.00	0.00	24.0
38	440	-25880	294	-3	0	-22	-8478	15.71	15.71	9.42	9.42	3	0.15	0.00	0.02	0.00	0.00	24.0
39	440	-20720	514	379	0	-688	-6625	15.71	15.71	9.42	9.42	3	0.12	0.01	0.04	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 12 NI 91 NF 92 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 30B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-24430	1145	-62	0	-171	-12730	15.71	15.71	9.42	9.42	3	0.22	0.01	0.08	0.00	0.00	24.0
2	0	-18780	1059	-82	0	-223	-11270	15.71	15.71	9.42	9.42	2	0.28	0.01	0.08	0.00	0.00	24.0
3	0	-18820	1056	-5	0	-14	-11290	15.71	15.71	9.42	9.42	2	0.27	0.01	0.08	0.00	0.00	24.0
4	0	-18770	705	-90	0	-249	-8292	15.71	15.71	9.42	9.42	2	0.21	0.01	0.05	0.00	0.00	24.0
5	0	-18810	702	-13	0	-40	-8316	15.71	15.71	9.42	9.42	2	0.20	0.01	0.05	0.00	0.00	24.0
6	0	-18740	938	-175	0	-476	-10200	15.71	15.71	9.42	9.42	2	0.26	0.01	0.07	0.00	0.00	24.0
7	0	-18850	929	82	0	221	-10280	15.71	15.71	9.42	9.42	2	0.25	0.01	0.07	0.00	0.00	24.0
8	0	-18740	832	-177	0	-484	-9307	15.71	15.71	9.42	9.42	2	0.23	0.01	0.06	0.00	0.00	24.0
9	0	-18850	823	80	0	213	-9386	15.71	15.71	9.42	9.42	2	0.23	0.01	0.06	0.00	0.00	24.0
10	0	-18780	1059	-82	0	-223	-11270	15.71	15.71	9.42	9.42	2	0.28	0.01	0.08	0.00	0.00	24.0
11	0	-18820	1056	-5	0	-14	-11290	15.71	15.71	9.42	9.42	2	0.27	0.01	0.08	0.00	0.00	24.0
12	0	-18770	705	-90	0	-249	-8292	15.71	15.71	9.42	9.42	2	0.21	0.01	0.05	0.00	0.00	24.0
13	0	-18810	702	-13	0	-40	-8316	15.71	15.71	9.42	9.42	2	0.20	0.01	0.05	0.00	0.00	24.0
14	0	-18740	938	-175	0	-476	-10200	15.71	15.71	9.42	9.42	2	0.26	0.01	0.07	0.00	0.00	24.0
15	0	-18850	929	82	0	221	-10280	15.71	15.71	9.42	9.42	2	0.25	0.01	0.07	0.00	0.00	24.0
16	0	-18740	832	-177	0	-484	-9307	15.71	15.71	9.42	9.42	2	0.23	0.01	0.06	0.00	0.00	24.0
17	0	-18850	823	80	0	213	-9386	15.71	15.71	9.42	9.42	2	0.23	0.01	0.06	0.00	0.00	24.0
18	0	-30020	3933	-149	0	-378	-30130	15.71	15.71	9.42	9.42	3	0.51	0.05	0.26	0.00	0.00	24.0
19	0	-33660	823	-135	0	-376	-18650	15.71	15.71	9.42	9.42	3	0.31	0.01	0.05	0.00	0.00	24.0
20	0	-30770	2207	137	0	311	-22800	15.71	15.71	9.42	9.42	3	0.39	0.03	0.15	0.00	0.00	24.0
37	0	-26430	4566	-126	0	-308	-30150	15.71	15.71	9.42	9.42	3	0.52	0.06	0.32	0.00	0.00	24.0
38	0	-32500	-617	-103	0	-305	-11020	15.71	15.71	9.42	9.42	3	0.19	0.01	0.04	0.00	0.00	24.0
39	0	-27670	1690	350	0	839	-17940	15.71	15.71	9.42	9.42	3	0.31	0.02	0.12	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	110	-23288	1145	-62	0	-103	-11471	15.71	15.71	9.42	9.42	3	0.20	0.01	0.08	0.00	0.00	24.0
2	110	-17900	1059	-82	0	-133	-10106	15.71	15.71	9.42	9.42	2	0.25	0.01	0.08	0.00	0.00	24.0
3	110	-17940	1056	-5	0	-9	-10130	15.71	15.71	9.42	9.42	2	0.25	0.01	0.08	0.00	0.00	24.0
4	110	-17890	705	-90	0	-150	-7517	15.71	15.71	9.42	9.42	2	0.19	0.01	0.05	0.00	0.00	24.0
5	110	-17930	702	-13	0	-26	-7544	15.71	15.71	9.42	9.42	2	0.18	0.01	0.05	0.00	0.00	24.0

6	110	-17860	938	-175	0	-284	-9168	15.71	15.71	9.42	9.42	2	0.23	0.01	0.07	0.00	0.00	24.0
7	110	-17970	929	82	0	131	-9258	15.71	15.71	9.42	9.42	2	0.23	0.01	0.07	0.00	0.00	24.0
8	110	-17860	832	-177	0	-289	-8392	15.71	15.71	9.42	9.42	2	0.21	0.01	0.06	0.00	0.00	24.0
9	110	-17970	823	80	0	126	-8481	15.71	15.71	9.42	9.42	2	0.21	0.01	0.06	0.00	0.00	24.0
10	110	-17900	1059	-82	0	-133	-10106	15.71	15.71	9.42	9.42	2	0.25	0.01	0.08	0.00	0.00	24.0
11	110	-17940	1056	-5	0	-9	-10130	15.71	15.71	9.42	9.42	2	0.25	0.01	0.08	0.00	0.00	24.0
12	110	-17890	705	-90	0	-150	-7517	15.71	15.71	9.42	9.42	2	0.19	0.01	0.05	0.00	0.00	24.0
13	110	-17930	702	-13	0	-26	-7544	15.71	15.71	9.42	9.42	2	0.18	0.01	0.05	0.00	0.00	24.0
14	110	-17860	938	-175	0	-284	-9168	15.71	15.71	9.42	9.42	2	0.23	0.01	0.07	0.00	0.00	24.0
15	110	-17970	929	82	0	131	-9258	15.71	15.71	9.42	9.42	2	0.23	0.01	0.07	0.00	0.00	24.0
16	110	-17860	832	-177	0	-289	-8392	15.71	15.71	9.42	9.42	2	0.21	0.01	0.06	0.00	0.00	24.0
17	110	-17970	823	80	0	126	-8481	15.71	15.71	9.42	9.42	2	0.21	0.01	0.06	0.00	0.00	24.0
18	110	-28878	3725	-149	0	-214	-25919	15.71	15.71	9.42	9.42	3	0.44	0.05	0.25	0.00	0.00	24.0
19	110	-32518	1031	-135	0	-228	-17631	15.71	15.71	9.42	9.42	3	0.30	0.01	0.07	0.00	0.00	24.0
20	110	-29625	2207	137	0	160	-20372	15.71	15.71	9.42	9.42	3	0.35	0.03	0.15	0.00	0.00	24.0
37	110	-25288	4220	-126	0	-169	-25318	15.71	15.71	9.42	9.42	3	0.44	0.05	0.30	0.00	0.00	24.0
38	110	-31355	-271	-103	0	-192	-11509	15.71	15.71	9.42	9.42	3	0.20	0.00	0.02	0.00	0.00	24.0
39	110	-26528	1690	350	0	454	-16080	15.71	15.71	9.42	9.42	3	0.28	0.02	0.12	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	220	-22145	1145	-62	0	-35	-10212	15.71	15.71	9.42	9.42	3	0.18	0.01	0.08	0.00	0.00	24.0
2	220	-17020	1059	-82	0	-42	-8942	15.71	15.71	9.42	9.42	2	0.22	0.01	0.08	0.00	0.00	24.0
3	220	-17060	1056	-5	0	-3	-8969	15.71	15.71	9.42	9.42	2	0.22	0.01	0.08	0.00	0.00	24.0
4	220	-17010	705	-90	0	-51	-6742	15.71	15.71	9.42	9.42	2	0.17	0.01	0.05	0.00	0.00	24.0
5	220	-17050	702	-13	0	-11	-6771	15.71	15.71	9.42	9.42	2	0.17	0.01	0.05	0.00	0.00	24.0
6	220	-16980	938	-175	0	-91	-8137	15.71	15.71	9.42	9.42	2	0.20	0.01	0.07	0.00	0.00	24.0
7	220	-17090	929	82	0	40	-8235	15.71	15.71	9.42	9.42	2	0.20	0.01	0.07	0.00	0.00	24.0
8	220	-16980	832	-177	0	-94	-7478	15.71	15.71	9.42	9.42	2	0.18	0.01	0.06	0.00	0.00	24.0
9	220	-17090	823	80	0	38	-7576	15.71	15.71	9.42	9.42	2	0.19	0.01	0.06	0.00	0.00	24.0
10	220	-17020	1059	-82	0	-42	-8942	15.71	15.71	9.42	9.42	2	0.22	0.01	0.08	0.00	0.00	24.0
11	220	-17060	1056	-5	0	-3	-8969	15.71	15.71	9.42	9.42	2	0.22	0.01	0.08	0.00	0.00	24.0
12	220	-17010	705	-90	0	-51	-6742	15.71	15.71	9.42	9.42	2	0.17	0.01	0.05	0.00	0.00	24.0
13	220	-17050	702	-13	0	-11	-6771	15.71	15.71	9.42	9.42	2	0.17	0.01	0.05	0.00	0.00	24.0
14	220	-16980	938	-175	0	-91	-8137	15.71	15.71	9.42	9.42	2	0.20	0.01	0.07	0.00	0.00	24.0
15	220	-17090	929	82	0	40	-8235	15.71	15.71	9.42	9.42	2	0.20	0.01	0.07	0.00	0.00	24.0
16	220	-16980	832	-177	0	-94	-7478	15.71	15.71	9.42	9.42	2	0.18	0.01	0.06	0.00	0.00	24.0
17	220	-17090	823	80	0	38	-7576	15.71	15.71	9.42	9.42	2	0.19	0.01	0.06	0.00	0.00	24.0
18	220	-27735	3517	-149	0	-50	-21938	15.71	15.71	9.42	9.42	3	0.38	0.04	0.24	0.00	0.00	24.0
19	220	-31375	1239	-135	0	-80	-16382	15.71	15.71	9.42	9.42	3	0.28	0.02	0.08	0.00	0.00	24.0
20	220	-28480	2207	137	0	9	-17945	15.71	15.71	9.42	9.42	3	0.31	0.03	0.15	0.00	0.00	24.0
37	220	-24145	3873	-126	0	-30	-20868	15.71	15.71	9.42	9.42	3	0.36	0.05	0.28	0.00	0.00	24.0
38	220	-30210	76	-103	0	-79	-11617	15.71	15.71	9.42	9.42	3	0.20	0.00	0.01	0.00	0.00	24.0
39	220	-25385	1690	350	0	69	-14220	15.71	15.71	9.42	9.42	3	0.25	0.02	0.12	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	330	-21002	1145	-62	0	33	-8954	15.71	15.71	9.42	9.42	3	0.16	0.01	0.08	0.00	0.00	24.0
2	330	-16140	1059	-82	0	48	-7777	15.71	15.71	9.42	9.42	2	0.19	0.01	0.08	0.00	0.00	24.0
3	330	-16180	1056	-5	0	3	-7808	15.71	15.71	9.42	9.42	2	0.19	0.01	0.08	0.00	0.00	24.0
4	330	-16130	705	-90	0	48	-5966	15.71	15.71	9.42	9.42	2	0.15	0.01	0.05	0.00	0.00	24.0
5	330	-16170	702	-13	0	3	-5998	15.71	15.71	9.42	9.42	2	0.15	0.01	0.05	0.00	0.00	24.0
6	330	-16100	938	-175	0	101	-7106	15.71	15.71	9.42	9.42	2	0.18	0.01	0.07	0.00	0.00	24.0
7	330	-16210	929	82	0	-50	-7213	15.71	15.71	9.42	9.42	2	0.18	0.01	0.07	0.00	0.00	24.0
8	330	-16100	832	-177	0	101	-6563	15.71	15.71	9.42	9.42	2	0.16	0.01	0.06	0.00	0.00	24.0
9	330	-16210	823	80	0	-50	-6670	15.71	15.71	9.42	9.42	2	0.16	0.01	0.06	0.00	0.00	24.0
10	330	-16140	1059	-82	0	48	-7777	15.71	15.71	9.42	9.42	2	0.19	0.01	0.08	0.00	0.00	24.0
11	330	-16180	1056	-5	0	3	-7808	15.71	15.71	9.42	9.42	2	0.19	0.01	0.08	0.00	0.00	24.0
12	330	-16130	705	-90	0	48	-5966	15.71	15.71	9.42	9.42	2	0.15	0.01	0.05	0.00	0.00	24.0
13	330	-16170	702	-13	0	3	-5998	15.71	15.71	9.42	9.42	2	0.15	0.01	0.05	0.00	0.00	24.0
14	330	-16100	938	-175	0	101	-7106	15.71	15.71	9.42	9.42	2	0.18	0.01	0.07	0.00	0.00	24.0
15	330	-16210	929	82	0	-50	-7213	15.71	15.71	9.42	9.42	2	0.18	0.01	0.07	0.00	0.00	24.0
16	330	-16100	832	-177	0	101	-6563	15.71	15.71	9.42	9.42	2	0.16	0.01	0.06	0.00	0.00	24.0
17	330	-16210	823	80	0	-50	-6670	15.71	15.71	9.42	9.42	2	0.16	0.01	0.06	0.00	0.00	24.0
18	330	-26592	3309	-149	0	113	-18184	15.71	15.71	9.42	9.42	3	0.31	0.04	0.23	0.00	0.00	24.0
19	330	-30232	1447	-135	0	68	-14906	15.71	15.71	9.42	9.42	3	0.25	0.02	0.10	0.00	0.00	24.0
20	330	-27335	2207	137	0	-141	-15518	15.71	15.71	9.42	9.42	3	0.27	0.03	0.15	0.00	0.00	24.0
37	330	-23002	3527	-126	0	109	-16798	15.71	15.71	9.42	9.42	3	0.29	0.04	0.25	0.00	0.00	24.0
38	330	-29065	422	-103	0	34	-11344	15.71	15.71	9.42	9.42	3	0.19	0.01	0.03	0.00	0.00	24.0
39	330	-24242	1690	350	0	-316	-12360	15.71	15.71	9.42	9.42	3	0.22	0.02	0.12	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	440	-19860	1145	-62	0	101	-7695	15.71	15.71	9.42	9.42	3	0.14	0.01	0.09	0.00	0.00	24.0
2	440	-15260	1059	-82	0	139	-6613	15.71	15.71	9.42	9.42	2	0.17	0.01	0.08	0.00	0.00	24.0
3	440	-15300	1056	-5	0	8	-6648	15.71	15.71	9.42	9.42	2	0.16	0.01	0.08	0.00	0.00	24.0
4	440	-15250	705	-90	0	147	-5191	15.71	15.71	9.42	9.42	2	0.13	0.01	0.05	0.00	0.00	24.0
5	440	-15290	702	-13	0	17	-5226	15.71	15.71	9.42	9.42	2	0.13	0.01	0.05	0.00	0.00	24.0
6	440	-15220	938	-175	0	294	-6074	15.71	15.71	9.42	9.42	2	0.16	0.01	0.07	0.00	0.00	24.0
7	440	-15330	929	82	0	-141	-6191	15.71	15.71	9.42	9.42	2	0.16	0.01	0.07	0.00	0.00	24.0
8	440	-15220	832	-177	0	296	-5648	15.71	15.71	9.42	9.42	2	0.15	0.01	0.06	0.00	0.00	24.0
9	440	-15330	823	80	0	-138	-5765	15.71	15.71	9.42	9.42	2	0.14	0.01	0.06	0.00	0.00	24.0
10	440	-15260	1059	-82	0	139	-6613	15.71	15.71	9.42	9.42	2	0.17	0.01	0.08	0.00	0.00	24.0
11	440	-15300	1056	-5	0	8	-6648	15.71	15.71	9.42	9.42	2	0.16	0.01	0.08	0.00	0.00	24.0
12	440	-15250	705	-90	0	147	-5191	15.71	15.71	9.42	9.42	2	0.13	0.01	0.05	0.00	0.00	24.0
13	440	-15290	702	-13	0	17	-5226	15.71	15.71	9.42	9.42	2	0.13	0.01	0.05	0.00	0.00	24.0
14	440	-15220	938	-175	0	294	-6074	15.71	15.71	9.42	9.42	2	0.16	0.01	0.07	0.00	0.00	24.0
15	440	-15330	929	82	0	-141	-6191	15.71	15.71	9.42	9.42	2	0.16	0.01	0.07	0.00	0.00	24.0
16	440	-15220	832	-177	0	296	-5648	15.71	15.71	9.42	9.42	2	0.15	0.01	0.06	0.00	0.00	24.0
17	440	-15330	823	80	0	-138	-5765	15.71	15.71	9.42	9.42	2	0.14	0.01	0.06	0.00	0.00	24.0
18	440	-25450	3101	-149	0	277	-14660	15.71	15.71	9.42	9.42	3	0.25	0.04	0.22	0.00	0.00	24.0
19	440	-29090	1655	-135	0	216	-13200	15.71	15.71	9.42	9.42	3	0.23	0.02	0.11	0.00	0.00	24.0
20	440	-26190	2207	137	0	-292	-13090	15.71	15.71	9.42	9.42	3	0.23	0.03	0.15	0.00	0.00	24.0
37	440	-21860	3180	-126	0	248	-13110	15.71	15.71	9.42	9.42	3	0.23	0.04	0.23	0.00	0.00	24.0
38	440	-27920	769	-103	0	147	-10690	15.71	15.71	9.42	9.42	3	0.18	0.01	0.05	0.00	0.00	24.0
39	440	-23100	1690	350	0	-701	-10500	15.71	15.71	9.42	9.42	3	0.19	0.02	0.12	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 13 NI 134 NF 135 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 29B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-24440	1290	-128	0	-359	-13500	15.71	15.71	9.42	9.42	3	0.24	0.02	0.09	0.00	0.00	24.0

2	0	-18760	1202	-135	0	-377	-12040	15.71	15.71	9.42	9.42	2	0.30	0.02	0.09	0.00	0.00	24.0
3	0	-18730	1191	-61	0	-173	-11940	15.71	15.71	9.42	9.42	2	0.29	0.02	0.09	0.00	0.00	24.0
4	0	-18870	793	-136	0	-379	-8827	15.71	15.71	9.42	9.42	2	0.22	0.01	0.06	0.00	0.00	24.0
5	0	-18830	782	-61	0	-175	-8720	15.71	15.71	9.42	9.42	2	0.21	0.01	0.06	0.00	0.00	24.0
6	0	-18840	1071	-222	0	-616	-11040	15.71	15.71	9.42	9.42	2	0.28	0.01	0.08	0.00	0.00	24.0
7	0	-18720	1036	26	0	64	-10690	15.71	15.71	9.42	9.42	2	0.26	0.01	0.08	0.00	0.00	24.0
8	0	-18870	948	-222	0	-616	-10080	15.71	15.71	9.42	9.42	2	0.26	0.01	0.07	0.00	0.00	24.0
9	0	-18760	913	25	0	64	-9721	15.71	15.71	9.42	9.42	2	0.24	0.01	0.07	0.00	0.00	24.0
10	0	-18760	1202	-135	0	-377	-12040	15.71	15.71	9.42	9.42	2	0.30	0.02	0.09	0.00	0.00	24.0
11	0	-18730	1191	-61	0	-173	-11940	15.71	15.71	9.42	9.42	2	0.29	0.02	0.09	0.00	0.00	24.0
12	0	-18870	793	-136	0	-379	-8827	15.71	15.71	9.42	9.42	2	0.22	0.01	0.06	0.00	0.00	24.0
13	0	-18830	782	-61	0	-175	-8720	15.71	15.71	9.42	9.42	2	0.21	0.01	0.06	0.00	0.00	24.0
14	0	-18840	1071	-222	0	-616	-11040	15.71	15.71	9.42	9.42	2	0.28	0.01	0.08	0.00	0.00	24.0
15	0	-18720	1036	26	0	64	-10690	15.71	15.71	9.42	9.42	2	0.26	0.01	0.08	0.00	0.00	24.0
16	0	-18870	948	-222	0	-616	-10080	15.71	15.71	9.42	9.42	2	0.26	0.01	0.07	0.00	0.00	24.0
17	0	-18760	913	25	0	64	-9721	15.71	15.71	9.42	9.42	2	0.24	0.01	0.07	0.00	0.00	24.0
18	0	-29840	4309	-271	0	-753	-32030	15.71	15.71	9.42	9.42	3	0.55	0.05	0.29	0.00	0.00	24.0
19	0	-33840	1011	-226	0	-647	-19760	15.71	15.71	9.42	9.42	3	0.33	0.01	0.07	0.00	0.00	24.0
20	0	-30620	2433	3	0	-64	-23820	15.71	15.71	9.42	9.42	3	0.40	0.03	0.16	0.00	0.00	24.0
37	0	-26130	4961	-245	0	-674	-32080	15.71	15.71	9.42	9.42	3	0.56	0.06	0.35	0.00	0.00	24.0
38	0	-32800	-536	-170	0	-497	-11620	15.71	15.71	9.42	9.42	3	0.20	0.01	0.04	0.00	0.00	24.0
39	0	-27430	1833	211	0	473	-18380	15.71	15.71	9.42	9.42	3	0.32	0.02	0.13	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	110	-23295	1290	-128	0	-219	-12081	15.71	15.71	9.42	9.42	3	0.21	0.02	0.09	0.00	0.00	24.0
2	110	-17880	1202	-135	0	-229	-10719	15.71	15.71	9.42	9.42	2	0.26	0.02	0.09	0.00	0.00	24.0
3	110	-17850	1191	-61	0	-106	-10629	15.71	15.71	9.42	9.42	2	0.26	0.02	0.09	0.00	0.00	24.0
4	110	-17990	793	-136	0	-230	-7955	15.71	15.71	9.42	9.42	2	0.20	0.01	0.06	0.00	0.00	24.0
5	110	-17950	782	-61	0	-107	-7860	15.71	15.71	9.42	9.42	2	0.19	0.01	0.06	0.00	0.00	24.0
6	110	-17960	1071	-222	0	-372	-9862	15.71	15.71	9.42	9.42	2	0.25	0.01	0.08	0.00	0.00	24.0
7	110	-17840	1036	26	0	36	-9550	15.71	15.71	9.42	9.42	2	0.23	0.01	0.08	0.00	0.00	24.0
8	110	-17990	948	-222	0	-372	-9036	15.71	15.71	9.42	9.42	2	0.23	0.01	0.07	0.00	0.00	24.0
9	110	-17880	913	25	0	36	-8717	15.71	15.71	9.42	9.42	2	0.21	0.01	0.07	0.00	0.00	24.0
10	110	-17880	1202	-135	0	-229	-10719	15.71	15.71	9.42	9.42	2	0.26	0.02	0.09	0.00	0.00	24.0
11	110	-17850	1191	-61	0	-106	-10629	15.71	15.71	9.42	9.42	2	0.26	0.02	0.09	0.00	0.00	24.0
12	110	-17990	793	-136	0	-230	-7955	15.71	15.71	9.42	9.42	2	0.20	0.01	0.06	0.00	0.00	24.0
13	110	-17950	782	-61	0	-107	-7860	15.71	15.71	9.42	9.42	2	0.19	0.01	0.06	0.00	0.00	24.0
14	110	-17960	1071	-222	0	-372	-9862	15.71	15.71	9.42	9.42	2	0.25	0.01	0.08	0.00	0.00	24.0
15	110	-17840	1036	26	0	36	-9550	15.71	15.71	9.42	9.42	2	0.23	0.01	0.08	0.00	0.00	24.0
16	110	-17990	948	-222	0	-372	-9036	15.71	15.71	9.42	9.42	2	0.23	0.01	0.07	0.00	0.00	24.0
17	110	-17880	913	25	0	36	-8717	15.71	15.71	9.42	9.42	2	0.21	0.01	0.07	0.00	0.00	24.0
18	110	-28695	4101	-271	0	-455	-27404	15.71	15.71	9.42	9.42	3	0.47	0.05	0.28	0.00	0.00	24.0
19	110	-32695	1219	-226	0	-398	-18533	15.71	15.71	9.42	9.42	3	0.31	0.01	0.08	0.00	0.00	24.0
20	110	-29475	2433	3	0	-67	-21142	15.71	15.71	9.42	9.42	3	0.36	0.03	0.16	0.00	0.00	24.0
37	110	-24985	4614	-245	0	-404	-26813	15.71	15.71	9.42	9.42	3	0.47	0.06	0.33	0.00	0.00	24.0
38	110	-31655	-190	-170	0	-310	-12019	15.71	15.71	9.42	9.42	3	0.20	0.00	0.01	0.00	0.00	24.0
39	110	-26285	1833	211	0	241	-16365	15.71	15.71	9.42	9.42	3	0.28	0.02	0.13	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	220	-22150	1290	-128	0	-78	-10661	15.71	15.71	9.42	9.42	3	0.19	0.02	0.09	0.00	0.00	24.0
2	220	-17000	1202	-135	0	-80	-9398	15.71	15.71	9.42	9.42	2	0.23	0.02	0.09	0.00	0.00	24.0
3	220	-16970	1191	-61	0	-39	-9318	15.71	15.71	9.42	9.42	2	0.23	0.02	0.09	0.00	0.00	24.0
4	220	-17110	793	-136	0	-81	-7083	15.71	15.71	9.42	9.42	2	0.17	0.01	0.06	0.00	0.00	24.0
5	220	-17070	782	-61	0	-40	-7000	15.71	15.71	9.42	9.42	2	0.17	0.01	0.06	0.00	0.00	24.0
6	220	-17080	1071	-222	0	-128	-8685	15.71	15.71	9.42	9.42	2	0.21	0.01	0.08	0.00	0.00	24.0
7	220	-16960	1036	26	0	8	-8409	15.71	15.71	9.42	9.42	2	0.20	0.01	0.08	0.00	0.00	24.0
8	220	-17110	948	-222	0	-128	-7992	15.71	15.71	9.42	9.42	2	0.20	0.01	0.07	0.00	0.00	24.0
9	220	-17000	913	25	0	8	-7713	15.71	15.71	9.42	9.42	2	0.19	0.01	0.07	0.00	0.00	24.0
10	220	-17000	1202	-135	0	-80	-9398	15.71	15.71	9.42	9.42	2	0.23	0.02	0.09	0.00	0.00	24.0
11	220	-16970	1191	-61	0	-39	-9318	15.71	15.71	9.42	9.42	2	0.23	0.02	0.09	0.00	0.00	24.0
12	220	-17110	793	-136	0	-81	-7083	15.71	15.71	9.42	9.42	2	0.17	0.01	0.06	0.00	0.00	24.0
13	220	-17070	782	-61	0	-40	-7000	15.71	15.71	9.42	9.42	2	0.17	0.01	0.06	0.00	0.00	24.0
14	220	-17080	1071	-222	0	-128	-8685	15.71	15.71	9.42	9.42	2	0.21	0.01	0.08	0.00	0.00	24.0
15	220	-16960	1036	26	0	8	-8409	15.71	15.71	9.42	9.42	2	0.20	0.01	0.08	0.00	0.00	24.0
16	220	-17110	948	-222	0	-128	-7992	15.71	15.71	9.42	9.42	2	0.20	0.01	0.07	0.00	0.00	24.0
17	220	-17000	913	25	0	8	-7713	15.71	15.71	9.42	9.42	2	0.19	0.01	0.07	0.00	0.00	24.0
18	220	-27550	3893	-271	0	-157	-23008	15.71	15.71	9.42	9.42	3	0.39	0.05	0.27	0.00	0.00	24.0
19	220	-31550	1427	-226	0	-150	-17077	15.71	15.71	9.42	9.42	3	0.29	0.02	0.09	0.00	0.00	24.0
20	220	-28330	2433	3	0	-71	-18465	15.71	15.71	9.42	9.42	3	0.32	0.03	0.17	0.00	0.00	24.0
37	220	-23840	4268	-245	0	-135	-21928	15.71	15.71	9.42	9.42	3	0.38	0.05	0.30	0.00	0.00	24.0
38	220	-30510	157	-170	0	-122	-12037	15.71	15.71	9.42	9.42	3	0.20	0.00	0.01	0.00	0.00	24.0
39	220	-25140	1833	211	0	10	-14350	15.71	15.71	9.42	9.42	3	0.25	0.02	0.13	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	330	-21005	1290	-128	0	62	-9241	15.71	15.71	9.42	9.42	3	0.16	0.02	0.09	0.00	0.00	24.0
2	330	-16120	1202	-135	0	68	-8076	15.71	15.71	9.42	9.42	2	0.20	0.02	0.09	0.00	0.00	24.0
3	330	-16090	1191	-61	0	27	-8006	15.71	15.71	9.42	9.42	2	0.20	0.02	0.09	0.00	0.00	24.0
4	330	-16230	793	-136	0	69	-6211	15.71	15.71	9.42	9.42	2	0.15	0.01	0.06	0.00	0.00	24.0
5	330	-16190	782	-61	0	28	-6139	15.71	15.71	9.42	9.42	2	0.15	0.01	0.06	0.00	0.00	24.0
6	330	-16200	1071	-222	0	116	-7507	15.71	15.71	9.42	9.42	2	0.19	0.01	0.08	0.00	0.00	24.0
7	330	-16080	1036	26	0	-20	-7269	15.71	15.71	9.42	9.42	2	0.18	0.01	0.08	0.00	0.00	24.0
8	330	-16230	948	-222	0	116	-6948	15.71	15.71	9.42	9.42	2	0.17	0.01	0.07	0.00	0.00	24.0
9	330	-16120	913	25	0	-20	-6709	15.71	15.71	9.42	9.42	2	0.16	0.01	0.07	0.00	0.00	24.0
10	330	-16120	1202	-135	0	68	-8076	15.71	15.71	9.42	9.42	2	0.20	0.02	0.09	0.00	0.00	24.0
11	330	-16090	1191	-61	0	27	-8006	15.71	15.71	9.42	9.42	2	0.20	0.02	0.09	0.00	0.00	24.0
12	330	-16230	793	-136	0	69	-6211	15.71	15.71	9.42	9.42	2	0.15	0.01	0.06	0.00	0.00	24.0
13	330	-16190	782	-61	0	28	-6139	15.71	15.71	9.42	9.42	2	0.15	0.01	0.06	0.00	0.00	24.0
14	330	-16200	1071	-222	0	116	-7507	15.71	15.71	9.42	9.42	2	0.19	0.01	0.08	0.00	0.00	24.0
15	330	-16080	1036	26	0	-20	-7269	15.71	15.71	9.42	9.42	2	0.18	0.01	0.08	0.00	0.00	24.0
16	330	-16230	948	-222	0	116	-6948	15.71	15.71	9.42	9.42	2	0.17	0.01	0.07	0.00	0.00	24.0
17	330	-16120	913	25	0	-20	-6709	15.71	15.71	9.42	9.42	2	0.16	0.01	0.07	0.00	0.00	24.0
18	330	-26405	3686	-271	0	141	-18839	15.71	15.71	9.42	9.42	3	0.32	0.05	0.26	0.00	0.00	24.0
19	330	-30405	1635	-226	0	99	-15393	15.71	15.71	9.42	9.42	3	0.26	0.02	0.11	0.00	0.00	24.0
20	330	-27185	2433	3	0	-74	-15787	15.71	15.71	9.42	9.42	3	0.27	0.03	0.17	0.00	0.00	24.0
37	330	-22695	3922	-245	0	135	-17423	15.71	15.71	9.42	9.42	3	0.30	0.05	0.28	0.00	0.00	24.0
38	330	-29365	503	-170	0	66	-11674	15.71	15.71	9.42	9.42	3	0.20	0.01	0.03	0.00	0.00	24.0
39	330	-23995	1833	211	0	-222	-12335	15.71	15.71	9.42	9.42	3	0.22	0.02	0.13	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	440	-19860	1290	-128	0	203	-7822	15.71	15.71	9.42	9.42	3	0.14	0.02	0.10	0.00	0.00	24.0
2	440	-15240	1202	-135	0	216	-6755	15.71	15.71	9.42	9.42	2	0.17	0.02	0.09	0.00	0.00	24.0
3	440	-15210	1191	-61	0	94	-6695	15.71	15.71	9.42	9.42	2	0.17	0.02	0.09	0.00	0.00	24.0
4	440	-15350	793	-136	0	218	-5339	15.71	15.71	9.42	9.42	2	0.14	0.01	0.06	0.00	0.00	24.0
5	440	-15310	782	-61	0	95	-5279	15.71	15.71	9.42	9.42	2	0.13	0.01	0.06	0.00	0.00	24.0
6	440	-15320	1071	-222	0	360	-6329	15.71	15.71	9.42	9.42	2	0.16	0.01	0.08	0.00	0.00	24.0
7	440	-15200	1036	26	0	-48	-6129	15.71	15.71	9.42	9.42	2	0.15	0.01	0.08	0.00	0.00	24.0

8	440	-15350	948	-222	0	360	-5904	15.71	15.71	9.42	9.42	2	0.15	0.01	0.07	0.00	0.00	24.0
9	440	-15240	913	25	0	-48	-5705	15.71	15.71	9.42	9.42	2	0.14	0.01	0.07	0.00	0.00	24.0
10	440	-15240	1202	-135	0	216	-6755	15.71	15.71	9.42	9.42	2	0.17	0.02	0.09	0.00	0.00	24.0
11	440	-15210	1191	-61	0	94	-6695	15.71	15.71	9.42	9.42	2	0.17	0.02	0.09	0.00	0.00	24.0
12	440	-15350	793	-136	0	218	-5339	15.71	15.71	9.42	9.42	2	0.14	0.01	0.06	0.00	0.00	24.0
13	440	-15310	782	-61	0	95	-5279	15.71	15.71	9.42	9.42	2	0.13	0.01	0.06	0.00	0.00	24.0
14	440	-15320	1071	-222	0	360	-6329	15.71	15.71	9.42	9.42	2	0.16	0.01	0.08	0.00	0.00	24.0
15	440	-15200	1036	26	0	-48	-6129	15.71	15.71	9.42	9.42	2	0.15	0.01	0.08	0.00	0.00	24.0
16	440	-15350	948	-222	0	360	-5904	15.71	15.71	9.42	9.42	2	0.15	0.01	0.07	0.00	0.00	24.0
17	440	-15240	913	25	0	-48	-5705	15.71	15.71	9.42	9.42	2	0.14	0.01	0.07	0.00	0.00	24.0
18	440	-25260	3478	-271	0	439	-14900	15.71	15.71	9.42	9.42	3	0.26	0.04	0.24	0.00	0.00	24.0
19	440	-29260	1843	-226	0	348	-13480	15.71	15.71	9.42	9.42	3	0.23	0.02	0.12	0.00	0.00	24.0
20	440	-26040	2433	3	0	-77	-13110	15.71	15.71	9.42	9.42	3	0.23	0.03	0.17	0.00	0.00	24.0
37	440	-21550	3575	-245	0	405	-13300	15.71	15.71	9.42	9.42	3	0.24	0.04	0.26	0.00	0.00	24.0
38	440	-28220	850	-170	0	253	-10930	15.71	15.71	9.42	9.42	3	0.19	0.01	0.06	0.00	0.00	24.0
39	440	-22850	1833	211	0	-454	-10320	15.71	15.71	9.42	9.42	3	0.18	0.02	0.13	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 14 NI 177 NF 178 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 28B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-24340	1147	-144	0	-457	-12500	15.71	15.71	9.42	9.42	3	0.22	0.01	0.08	0.00	0.00	24.0
2	0	-18710	1088	-146	0	-455	-11290	15.71	15.71	9.42	9.42	2	0.28	0.01	0.08	0.00	0.00	24.0
3	0	-18710	1088	-76	0	-258	-11290	15.71	15.71	9.42	9.42	2	0.28	0.01	0.08	0.00	0.00	24.0
4	0	-18730	677	-145	0	-445	-7941	15.71	15.71	9.42	9.42	2	0.20	0.01	0.05	0.00	0.00	24.0
5	0	-18740	677	-75	0	-248	-7941	15.71	15.71	9.42	9.42	2	0.20	0.01	0.05	0.00	0.00	24.0
6	0	-18710	944	-227	0	-682	-10120	15.71	15.71	9.42	9.42	2	0.26	0.01	0.07	0.00	0.00	24.0
7	0	-18720	944	6	0	-24	-10120	15.71	15.71	9.42	9.42	2	0.24	0.01	0.07	0.00	0.00	24.0
8	0	-18720	821	-227	0	-679	-9112	15.71	15.71	9.42	9.42	2	0.23	0.01	0.06	0.00	0.00	24.0
9	0	-18730	820	6	0	-21	-9113	15.71	15.71	9.42	9.42	2	0.22	0.01	0.06	0.00	0.00	24.0
10	0	-18710	1088	-146	0	-455	-11290	15.71	15.71	9.42	9.42	2	0.28	0.01	0.08	0.00	0.00	24.0
11	0	-18710	1088	-76	0	-258	-11290	15.71	15.71	9.42	9.42	2	0.28	0.01	0.08	0.00	0.00	24.0
12	0	-18730	677	-145	0	-445	-7941	15.71	15.71	9.42	9.42	2	0.20	0.01	0.05	0.00	0.00	24.0
13	0	-18740	677	-75	0	-248	-7941	15.71	15.71	9.42	9.42	2	0.20	0.01	0.05	0.00	0.00	24.0
14	0	-18710	944	-227	0	-682	-10120	15.71	15.71	9.42	9.42	2	0.26	0.01	0.07	0.00	0.00	24.0
15	0	-18720	944	6	0	-24	-10120	15.71	15.71	9.42	9.42	2	0.24	0.01	0.07	0.00	0.00	24.0
16	0	-18720	821	-227	0	-679	-9112	15.71	15.71	9.42	9.42	2	0.23	0.01	0.06	0.00	0.00	24.0
17	0	-18730	820	6	0	-21	-9113	15.71	15.71	9.42	9.42	2	0.22	0.01	0.06	0.00	0.00	24.0
18	0	-29740	4051	-327	0	-1008	-30460	15.71	15.71	9.42	9.42	3	0.52	0.05	0.27	0.00	0.00	24.0
19	0	-33540	757	-271	0	-837	-17830	15.71	15.71	9.42	9.42	3	0.30	0.01	0.05	0.00	0.00	24.0
20	0	-30520	2220	-69	0	-319	-22430	15.71	15.71	9.42	9.42	3	0.38	0.03	0.15	0.00	0.00	24.0
37	0	-26130	4738	-295	0	-911	-30870	15.71	15.71	9.42	9.42	3	0.54	0.06	0.33	0.00	0.00	24.0
38	0	-32460	-752	-201	0	-626	-9824	15.71	15.71	9.42	9.42	3	0.17	0.01	0.05	0.00	0.00	24.0
39	0	-27440	1686	136	0	237	-17480	15.71	15.71	9.42	9.42	3	0.30	0.02	0.12	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	110	-23195	1147	-144	0	-299	-11238	15.71	15.71	9.42	9.42	3	0.20	0.01	0.08	0.00	0.00	24.0
2	110	-17830	1088	-146	0	-295	-10093	15.71	15.71	9.42	9.42	2	0.25	0.01	0.08	0.00	0.00	24.0
3	110	-17830	1088	-76	0	-175	-10093	15.71	15.71	9.42	9.42	2	0.25	0.01	0.08	0.00	0.00	24.0
4	110	-17850	677	-145	0	-286	-7197	15.71	15.71	9.42	9.42	2	0.18	0.01	0.05	0.00	0.00	24.0
5	110	-17860	677	-75	0	-165	-7197	15.71	15.71	9.42	9.42	2	0.18	0.01	0.05	0.00	0.00	24.0
6	110	-17830	944	-227	0	-433	-9081	15.71	15.71	9.42	9.42	2	0.23	0.01	0.07	0.00	0.00	24.0
7	110	-17840	944	6	0	-31	-9081	15.71	15.71	9.42	9.42	2	0.22	0.01	0.07	0.00	0.00	24.0
8	110	-17840	821	-227	0	-430	-8210	15.71	15.71	9.42	9.42	2	0.21	0.01	0.06	0.00	0.00	24.0
9	110	-17850	820	6	0	-28	-8211	15.71	15.71	9.42	9.42	2	0.20	0.01	0.06	0.00	0.00	24.0
10	110	-17830	1088	-146	0	-295	-10093	15.71	15.71	9.42	9.42	2	0.25	0.01	0.08	0.00	0.00	24.0
11	110	-17830	1088	-76	0	-175	-10093	15.71	15.71	9.42	9.42	2	0.25	0.01	0.08	0.00	0.00	24.0
12	110	-17850	677	-145	0	-286	-7197	15.71	15.71	9.42	9.42	2	0.18	0.01	0.05	0.00	0.00	24.0
13	110	-17860	677	-75	0	-165	-7197	15.71	15.71	9.42	9.42	2	0.18	0.01	0.05	0.00	0.00	24.0
14	110	-17830	944	-227	0	-433	-9081	15.71	15.71	9.42	9.42	2	0.23	0.01	0.07	0.00	0.00	24.0
15	110	-17840	944	6	0	-31	-9081	15.71	15.71	9.42	9.42	2	0.22	0.01	0.07	0.00	0.00	24.0
16	110	-17840	821	-227	0	-430	-8210	15.71	15.71	9.42	9.42	2	0.21	0.01	0.06	0.00	0.00	24.0
17	110	-17850	820	6	0	-28	-8211	15.71	15.71	9.42	9.42	2	0.20	0.01	0.06	0.00	0.00	24.0
18	110	-28595	3843	-327	0	-648	-26119	15.71	15.71	9.42	9.42	3	0.45	0.05	0.26	0.00	0.00	24.0
19	110	-32395	965	-271	0	-538	-16883	15.71	15.71	9.42	9.42	3	0.29	0.01	0.06	0.00	0.00	24.0
20	110	-29378	2220	-69	0	-243	-19988	15.71	15.71	9.42	9.42	3	0.34	0.03	0.15	0.00	0.00	24.0
37	110	-24985	4392	-295	0	-587	-25848	15.71	15.71	9.42	9.42	3	0.45	0.05	0.31	0.00	0.00	24.0
38	110	-31318	-406	-201	0	-405	-10460	15.71	15.71	9.42	9.42	3	0.18	0.00	0.03	0.00	0.00	24.0
39	110	-26295	1686	136	0	87	-15625	15.71	15.71	9.42	9.42	3	0.27	0.02	0.12	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	220	-22050	1147	-144	0	-141	-9976	15.71	15.71	9.42	9.42	3	0.18	0.01	0.08	0.00	0.00	24.0
2	220	-16950	1088	-146	0	-135	-8896	15.71	15.71	9.42	9.42	2	0.22	0.01	0.08	0.00	0.00	24.0
3	220	-16950	1088	-76	0	-91	-8896	15.71	15.71	9.42	9.42	2	0.22	0.01	0.08	0.00	0.00	24.0
4	220	-16970	677	-145	0	-126	-6452	15.71	15.71	9.42	9.42	2	0.16	0.01	0.05	0.00	0.00	24.0
5	220	-16980	677	-75	0	-83	-6452	15.71	15.71	9.42	9.42	2	0.16	0.01	0.05	0.00	0.00	24.0
6	220	-16950	944	-227	0	-183	-8042	15.71	15.71	9.42	9.42	2	0.20	0.01	0.07	0.00	0.00	24.0
7	220	-16960	944	6	0	-37	-8043	15.71	15.71	9.42	9.42	2	0.20	0.01	0.07	0.00	0.00	24.0
8	220	-16960	821	-227	0	-180	-7307	15.71	15.71	9.42	9.42	2	0.18	0.01	0.06	0.00	0.00	24.0
9	220	-16970	820	6	0	-35	-7308	15.71	15.71	9.42	9.42	2	0.18	0.01	0.06	0.00	0.00	24.0
10	220	-16950	1088	-146	0	-135	-8896	15.71	15.71	9.42	9.42	2	0.22	0.01	0.08	0.00	0.00	24.0
11	220	-16950	1088	-76	0	-91	-8896	15.71	15.71	9.42	9.42	2	0.22	0.01	0.08	0.00	0.00	24.0
12	220	-16970	677	-145	0	-126	-6452	15.71	15.71	9.42	9.42	2	0.16	0.01	0.05	0.00	0.00	24.0
13	220	-16980	677	-75	0	-83	-6452	15.71	15.71	9.42	9.42	2	0.16	0.01	0.05	0.00	0.00	24.0
14	220	-16950	944	-227	0	-183	-8042	15.71	15.71	9.42	9.42	2	0.20	0.01	0.07	0.00	0.00	24.0
15	220	-16960	944	6	0	-37	-8043	15.71	15.71	9.42	9.42	2	0.20	0.01	0.07	0.00	0.00	24.0
16	220	-16960	821	-227	0	-180	-7307	15.71	15.71	9.42	9.42	2	0.18	0.01	0.06	0.00	0.00	24.0
17	220	-16970	820	6	0	-35	-7308	15.71	15.71	9.42	9.42	2	0.18	0.01	0.06	0.00	0.00	24.0
18	220	-27450	3635	-327	0	-288	-22008	15.71	15.71	9.42	9.42	3	0.38	0.05	0.25	0.00	0.00	24.0
19	220	-31250	1173	-271	0	-240	-15707	15.71	15.71	9.42	9.42	3	0.27	0.01	0.08	0.00	0.00	24.0
20	220	-28235	2220	-69	0	-167	-17545	15.71	15.71	9.42	9.42	3	0.30	0.03	0.15	0.00	0.00	24.0
37	220	-23840	4045	-295	0	-263	-21208	15.71	15.71	9.42	9.42	3	0.37	0.05	0.29	0.00	0.00	24.0
38	220	-30175	-59	-201	0	-184	-10714	15.71	15.71	9.42	9.42	3	0.18	0.00	0.01	0.00	0.00	24.0
39	220	-25150	1686	136	0	-62	-13770	15.71	15.71	9.42	9.42	3	0.24	0.02	0.12	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	330	-20905	1147	-144	0	16	-8715	15.71	15.71	9.42	9.42	3	0.15	0.01	0.08	0.00	0.00	24.0
2	330	-16070	1088	-146	0	25	-7699	15.71	15.71	9.42	9.42	2	0.19	0.01	0.08	0.00	0.00	24.0
3	330	-16070	1088	-76	0	-8	-7700	15.71	15.71	9.42	9.42	2	0.19	0.01	0.08	0.00	0.00	24.0

4	330	-16090	677	-145	0	33	-5708	15.71	15.71	9.42	9.42	2	0.14	0.01	0.05	0.00	0.00	24.0
5	330	-16100	677	-75	0	-0	-5708	15.71	15.71	9.42	9.42	2	0.14	0.01	0.05	0.00	0.00	24.0
6	330	-16070	944	-227	0	67	-7002	15.71	15.71	9.42	9.42	2	0.17	0.01	0.07	0.00	0.00	24.0
7	330	-16080	944	6	0	-44	-7004	15.71	15.71	9.42	9.42	2	0.17	0.01	0.07	0.00	0.00	24.0
8	330	-16080	821	-227	0	69	-6404	15.71	15.71	9.42	9.42	2	0.16	0.01	0.06	0.00	0.00	24.0
9	330	-16090	820	6	0	-42	-6406	15.71	15.71	9.42	9.42	2	0.16	0.01	0.06	0.00	0.00	24.0
10	330	-16070	1088	-146	0	25	-7699	15.71	15.71	9.42	9.42	2	0.19	0.01	0.08	0.00	0.00	24.0
11	330	-16070	1088	-76	0	-8	-7700	15.71	15.71	9.42	9.42	2	0.19	0.01	0.08	0.00	0.00	24.0
12	330	-16090	677	-145	0	33	-5708	15.71	15.71	9.42	9.42	2	0.14	0.01	0.05	0.00	0.00	24.0
13	330	-16100	677	-75	0	-0	-5708	15.71	15.71	9.42	9.42	2	0.14	0.01	0.05	0.00	0.00	24.0
14	330	-16070	944	-227	0	67	-7002	15.71	15.71	9.42	9.42	2	0.17	0.01	0.07	0.00	0.00	24.0
15	330	-16080	944	6	0	-44	-7004	15.71	15.71	9.42	9.42	2	0.17	0.01	0.07	0.00	0.00	24.0
16	330	-16080	821	-227	0	69	-6404	15.71	15.71	9.42	9.42	2	0.16	0.01	0.06	0.00	0.00	24.0
17	330	-16090	820	6	0	-42	-6406	15.71	15.71	9.42	9.42	2	0.16	0.01	0.06	0.00	0.00	24.0
18	330	-26305	3428	-327	0	73	-18124	15.71	15.71	9.42	9.42	3	0.31	0.04	0.24	0.00	0.00	24.0
19	330	-30105	1381	-271	0	59	-14303	15.71	15.71	9.42	9.42	3	0.24	0.02	0.09	0.00	0.00	24.0
20	330	-27092	2220	-69	0	-91	-15102	15.71	15.71	9.42	9.42	3	0.26	0.03	0.15	0.00	0.00	24.0
37	330	-22695	3698	-295	0	61	-16948	15.71	15.71	9.42	9.42	3	0.30	0.05	0.27	0.00	0.00	24.0
38	330	-29032	287	-201	0	37	-10588	15.71	15.71	9.42	9.42	3	0.18	0.00	0.02	0.00	0.00	24.0
39	330	-24005	1686	136	0	-212	-11915	15.71	15.71	9.42	9.42	3	0.21	0.02	0.12	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	440	-19760	1147	-144	0	174	-7453	15.71	15.71	9.42	9.42	3	0.13	0.01	0.09	0.00	0.00	24.0
2	440	-15190	1088	-146	0	186	-6502	15.71	15.71	9.42	9.42	2	0.16	0.01	0.08	0.00	0.00	24.0
3	440	-15190	1088	-76	0	75	-6503	15.71	15.71	9.42	9.42	2	0.16	0.01	0.08	0.00	0.00	24.0
4	440	-15210	677	-145	0	192	-4964	15.71	15.71	9.42	9.42	2	0.13	0.01	0.05	0.00	0.00	24.0
5	440	-15220	677	-75	0	82	-4964	15.71	15.71	9.42	9.42	2	0.12	0.01	0.05	0.00	0.00	24.0
6	440	-15190	944	-227	0	317	-5963	15.71	15.71	9.42	9.42	2	0.15	0.01	0.07	0.00	0.00	24.0
7	440	-15200	944	6	0	-51	-5965	15.71	15.71	9.42	9.42	2	0.15	0.01	0.07	0.00	0.00	24.0
8	440	-15200	821	-227	0	319	-5502	15.71	15.71	9.42	9.42	2	0.14	0.01	0.06	0.00	0.00	24.0
9	440	-15210	820	6	0	-49	-5503	15.71	15.71	9.42	9.42	2	0.14	0.01	0.06	0.00	0.00	24.0
10	440	-15190	1088	-146	0	186	-6502	15.71	15.71	9.42	9.42	2	0.16	0.01	0.08	0.00	0.00	24.0
11	440	-15190	1088	-76	0	75	-6503	15.71	15.71	9.42	9.42	2	0.16	0.01	0.08	0.00	0.00	24.0
12	440	-15210	677	-145	0	192	-4964	15.71	15.71	9.42	9.42	2	0.13	0.01	0.05	0.00	0.00	24.0
13	440	-15220	677	-75	0	82	-4964	15.71	15.71	9.42	9.42	2	0.12	0.01	0.05	0.00	0.00	24.0
14	440	-15190	944	-227	0	317	-5963	15.71	15.71	9.42	9.42	2	0.15	0.01	0.07	0.00	0.00	24.0
15	440	-15200	944	6	0	-51	-5965	15.71	15.71	9.42	9.42	2	0.15	0.01	0.07	0.00	0.00	24.0
16	440	-15200	821	-227	0	319	-5502	15.71	15.71	9.42	9.42	2	0.14	0.01	0.06	0.00	0.00	24.0
17	440	-15210	820	6	0	-49	-5503	15.71	15.71	9.42	9.42	2	0.14	0.01	0.06	0.00	0.00	24.0
18	440	-25160	3220	-327	0	433	-14470	15.71	15.71	9.42	9.42	3	0.25	0.04	0.23	0.00	0.00	24.0
19	440	-28960	1589	-271	0	357	-12670	15.71	15.71	9.42	9.42	3	0.22	0.02	0.11	0.00	0.00	24.0
20	440	-25950	2220	-69	0	-15	-12660	15.71	15.71	9.42	9.42	3	0.22	0.03	0.16	0.00	0.00	24.0
37	440	-21550	3352	-295	0	385	-13070	15.71	15.71	9.42	9.42	3	0.23	0.04	0.24	0.00	0.00	24.0
38	440	-27890	634	-201	0	258	-10080	15.71	15.71	9.42	9.42	3	0.17	0.01	0.04	0.00	0.00	24.0
39	440	-22860	1686	136	0	-362	-10060	15.71	15.71	9.42	9.42	3	0.18	0.02	0.12	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 15 NI 220 NF 221 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 27B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-21240	-483	-309	0	-602	-5870	15.71	15.71	9.42	9.42	3	0.11	0.01	0.04	0.00	0.00	24.0
2	0	-16180	-340	-263	0	-541	-5753	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
3	0	-16330	-342	-194	0	-352	-5866	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
4	0	-16350	-401	-281	0	-575	-3164	15.71	15.71	9.42	9.42	2	0.09	0.01	0.03	0.00	0.00	24.0
5	0	-16500	-403	-212	0	-385	-3277	15.71	15.71	9.42	9.42	2	0.09	0.01	0.03	0.00	0.00	24.0
6	0	-16070	-359	-350	0	-775	-4716	15.71	15.71	9.42	9.42	2	0.13	0.00	0.03	0.00	0.00	24.0
7	0	-16550	-366	-119	0	-142	-5092	15.71	15.71	9.42	9.42	2	0.13	0.00	0.03	0.00	0.00	24.0
8	0	-16120	-377	-356	0	-785	-3939	15.71	15.71	9.42	9.42	2	0.12	0.00	0.03	0.00	0.00	24.0
9	0	-16610	-384	-125	0	-152	-4315	15.71	15.71	9.42	9.42	2	0.11	0.00	0.03	0.00	0.00	24.0
10	0	-16180	-340	-263	0	-541	-5753	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
11	0	-16330	-342	-194	0	-352	-5866	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
12	0	-16350	-401	-281	0	-575	-3164	15.71	15.71	9.42	9.42	2	0.09	0.01	0.03	0.00	0.00	24.0
13	0	-16500	-403	-212	0	-385	-3277	15.71	15.71	9.42	9.42	2	0.09	0.01	0.03	0.00	0.00	24.0
14	0	-16070	-359	-350	0	-775	-4716	15.71	15.71	9.42	9.42	2	0.13	0.00	0.03	0.00	0.00	24.0
15	0	-16550	-366	-119	0	-142	-5092	15.71	15.71	9.42	9.42	2	0.13	0.00	0.03	0.00	0.00	24.0
16	0	-16120	-377	-356	0	-785	-3939	15.71	15.71	9.42	9.42	2	0.12	0.00	0.03	0.00	0.00	24.0
17	0	-16610	-384	-125	0	-152	-4315	15.71	15.71	9.42	9.42	2	0.11	0.00	0.03	0.00	0.00	24.0
18	0	-24610	218	-431	0	-1041	-16730	15.71	15.71	9.42	9.42	3	0.30	0.01	0.02	0.00	0.00	24.0
19	0	-28990	-1598	-464	0	-1059	-7230	15.71	15.71	9.42	9.42	3	0.13	0.02	0.11	0.00	0.00	24.0
20	0	-26340	-672	-225	0	-480	-11370	15.71	15.71	9.42	9.42	3	0.20	0.01	0.05	0.00	0.00	24.0
37	0	-21370	890	-376	0	-890	-17900	15.71	15.71	9.42	9.42	3	0.32	0.01	0.07	0.00	0.00	24.0
38	0	-28670	-2135	-430	0	-920	-2068	15.71	15.71	9.42	9.42	3	0.05	0.03	0.15	0.00	0.00	24.0
39	0	-24270	-593	-32	0	44	-8970	15.71	15.71	9.42	9.42	3	0.16	0.01	0.04	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	110	-20095	-483	-309	0	-262	-6401	15.71	15.71	9.42	9.42	3	0.11	0.01	0.04	0.00	0.00	24.0
2	110	-15300	-340	-263	0	-252	-6127	15.71	15.71	9.42	9.42	2	0.16	0.00	0.03	0.00	0.00	24.0
3	110	-15450	-342	-194	0	-138	-6242	15.71	15.71	9.42	9.42	2	0.16	0.00	0.03	0.00	0.00	24.0
4	110	-15470	-401	-281	0	-266	-3605	15.71	15.71	9.42	9.42	2	0.09	0.01	0.03	0.00	0.00	24.0
5	110	-15620	-403	-212	0	-152	-3720	15.71	15.71	9.42	9.42	2	0.09	0.01	0.03	0.00	0.00	24.0
6	110	-15190	-359	-350	0	-389	-5111	15.71	15.71	9.42	9.42	2	0.13	0.00	0.03	0.00	0.00	24.0
7	110	-15670	-366	-119	0	-10	-5494	15.71	15.71	9.42	9.42	2	0.14	0.00	0.03	0.00	0.00	24.0
8	110	-15240	-377	-356	0	-393	-4354	15.71	15.71	9.42	9.42	2	0.12	0.00	0.03	0.00	0.00	24.0
9	110	-15730	-384	-125	0	-15	-4737	15.71	15.71	9.42	9.42	2	0.12	0.00	0.03	0.00	0.00	24.0
10	110	-15300	-340	-263	0	-252	-6127	15.71	15.71	9.42	9.42	2	0.16	0.00	0.03	0.00	0.00	24.0
11	110	-15450	-342	-194	0	-138	-6242	15.71	15.71	9.42	9.42	2	0.16	0.00	0.03	0.00	0.00	24.0
12	110	-15470	-401	-281	0	-266	-3605	15.71	15.71	9.42	9.42	2	0.09	0.01	0.03	0.00	0.00	24.0
13	110	-15620	-403	-212	0	-152	-3720	15.71	15.71	9.42	9.42	2	0.09	0.01	0.03	0.00	0.00	24.0
14	110	-15190	-359	-350	0	-389	-5111	15.71	15.71	9.42	9.42	2	0.13	0.00	0.03	0.00	0.00	24.0
15	110	-15670	-366	-119	0	-10	-5494	15.71	15.71	9.42	9.42	2	0.14	0.00	0.03	0.00	0.00	24.0
16	110	-15240	-377	-356	0	-393	-4354	15.71	15.71	9.42	9.42	2	0.12	0.00	0.03	0.00	0.00	24.0
17	110	-15730	-384	-125	0	-15	-4737	15.71	15.71	9.42	9.42	2	0.12	0.00	0.03	0.00	0.00	24.0
18	110	-23465	10	-431	0	-567	-16604	15.71	15.71	9.42	9.42	3	0.29	0.01	0.03	0.00	0.00	24.0
19	110	-27845	-1390	-464	0	-549	-8873	15.71	15.71	9.42	9.42	3	0.15	0.02	0.10	0.00	0.00	24.0
20	110	-25198	-672	-225	0	-232	-12110	15.71	15.71	9.42	9.42	3	0.21	0.01	0.05	0.00	0.00	24.0
37	110	-20228	543	-376	0	-477	-17111	15.71	15.71	9.42	9.42	3	0.30	0.01	0.04	0.00	0.00	24.0
38	110	-27528	-1789	-430	0	-447	-4226	15.71	15.71	9.42	9.42	3	0.08	0.02	0.12	0.00	0.00	24.0
39	110	-23125	-593	-32	0	79	-9622	15.71	15.71	9.42	9.42	3	0.17	0.01	0.04	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	220	-18950	-483	-309	0	77	-6932	15.71	15.71	9.42	9.42	3	0.12	0.01	0.04	0.00	0.00	24.0
2	220	-14420	-340	-263	0	38	-6501	15.71	15.71	9.42	9.42	2	0.16	0.00	0.03	0.00	0.00	24.0
3	220	-14570	-342	-194	0	75	-6618	15.71	15.71	9.42	9.42	2	0.17	0.00	0.03	0.00	0.00	24.0
4	220	-14590	-401	-281	0	44	-4046	15.71	15.71	9.42	9.42	2	0.10	0.01	0.03	0.00	0.00	24.0
5	220	-14740	-403	-212	0	81	-4164	15.71	15.71	9.42	9.42	2	0.10	0.01	0.03	0.00	0.00	24.0
6	220	-14310	-359	-350	0	-4	-5506	15.71	15.71	9.42	9.42	2	0.14	0.00	0.03	0.00	0.00	24.0
7	220	-14790	-366	-119	0	121	-5896	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
8	220	-14360	-377	-356	0	-2	-4769	15.71	15.71	9.42	9.42	2	0.12	0.00	0.03	0.00	0.00	24.0
9	220	-14850	-384	-125	0	123	-5159	15.71	15.71	9.42	9.42	2	0.13	0.00	0.03	0.00	0.00	24.0
10	220	-14420	-340	-263	0	38	-6501	15.71	15.71	9.42	9.42	2	0.16	0.00	0.03	0.00	0.00	24.0
11	220	-14570	-342	-194	0	75	-6618	15.71	15.71	9.42	9.42	2	0.17	0.00	0.03	0.00	0.00	24.0
12	220	-14590	-401	-281	0	44	-4046	15.71	15.71	9.42	9.42	2	0.10	0.01	0.03	0.00	0.00	24.0
13	220	-14740	-403	-212	0	81	-4164	15.71	15.71	9.42	9.42	2	0.10	0.01	0.03	0.00	0.00	24.0
14	220	-14310	-359	-350	0	-4	-5506	15.71	15.71	9.42	9.42	2	0.14	0.00	0.03	0.00	0.00	24.0
15	220	-14790	-366	-119	0	121	-5896	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
16	220	-14360	-377	-356	0	-2	-4769	15.71	15.71	9.42	9.42	2	0.12	0.00	0.03	0.00	0.00	24.0
17	220	-14850	-384	-125	0	123	-5159	15.71	15.71	9.42	9.42	2	0.13	0.00	0.03	0.00	0.00	24.0
18	220	-22320	-198	-431	0	-92	-16708	15.71	15.71	9.42	9.42	3	0.29	0.01	0.03	0.00	0.00	24.0
19	220	-26700	-1182	-464	0	-38	-10287	15.71	15.71	9.42	9.42	3	0.18	0.01	0.08	0.00	0.00	24.0
20	220	-24055	-672	-225	0	15	-12850	15.71	15.71	9.42	9.42	3	0.22	0.01	0.05	0.00	0.00	24.0
37	220	-19085	197	-376	0	-64	-16703	15.71	15.71	9.42	9.42	3	0.30	0.01	0.02	0.00	0.00	24.0
38	220	-26385	-1442	-430	0	26	-6003	15.71	15.71	9.42	9.42	3	0.10	0.02	0.10	0.00	0.00	24.0
39	220	-21980	-593	-32	0	115	-10275	15.71	15.71	9.42	9.42	3	0.18	0.01	0.04	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	330	-17805	-483	-309	0	417	-7464	15.71	15.71	9.42	9.42	3	0.14	0.01	0.04	0.00	0.00	24.0
2	330	-13540	-340	-263	0	327	-6875	15.71	15.71	9.42	9.42	2	0.18	0.00	0.03	0.00	0.00	24.0
3	330	-13690	-342	-194	0	288	-6994	15.71	15.71	9.42	9.42	2	0.18	0.00	0.03	0.00	0.00	24.0
4	330	-13710	-401	-281	0	353	-4488	15.71	15.71	9.42	9.42	2	0.12	0.01	0.03	0.00	0.00	24.0
5	330	-13860	-403	-212	0	314	-4607	15.71	15.71	9.42	9.42	2	0.12	0.01	0.03	0.00	0.00	24.0
6	330	-13430	-359	-350	0	381	-5900	15.71	15.71	9.42	9.42	2	0.16	0.00	0.03	0.00	0.00	24.0
7	330	-13910	-366	-119	0	252	-6298	15.71	15.71	9.42	9.42	2	0.16	0.00	0.03	0.00	0.00	24.0
8	330	-13480	-377	-356	0	389	-5184	15.71	15.71	9.42	9.42	2	0.14	0.00	0.03	0.00	0.00	24.0
9	330	-13970	-384	-125	0	260	-5582	15.71	15.71	9.42	9.42	2	0.14	0.00	0.03	0.00	0.00	24.0
10	330	-13540	-340	-263	0	327	-6875	15.71	15.71	9.42	9.42	2	0.18	0.00	0.03	0.00	0.00	24.0
11	330	-13690	-342	-194	0	288	-6994	15.71	15.71	9.42	9.42	2	0.18	0.00	0.03	0.00	0.00	24.0
12	330	-13710	-401	-281	0	353	-4488	15.71	15.71	9.42	9.42	2	0.12	0.01	0.03	0.00	0.00	24.0
13	330	-13860	-403	-212	0	314	-4607	15.71	15.71	9.42	9.42	2	0.12	0.01	0.03	0.00	0.00	24.0
14	330	-13430	-359	-350	0	381	-5900	15.71	15.71	9.42	9.42	2	0.16	0.00	0.03	0.00	0.00	24.0
15	330	-13910	-366	-119	0	252	-6298	15.71	15.71	9.42	9.42	2	0.16	0.00	0.03	0.00	0.00	24.0
16	330	-13480	-377	-356	0	389	-5184	15.71	15.71	9.42	9.42	2	0.14	0.00	0.03	0.00	0.00	24.0
17	330	-13970	-384	-125	0	260	-5582	15.71	15.71	9.42	9.42	2	0.14	0.00	0.03	0.00	0.00	24.0
18	330	-21175	-406	-431	0	382	-17039	15.71	15.71	9.42	9.42	3	0.30	0.01	0.03	0.00	0.00	24.0
19	330	-25555	-974	-464	0	472	-11473	15.71	15.71	9.42	9.42	3	0.20	0.01	0.07	0.00	0.00	24.0
20	330	-22912	-672	-225	0	263	-13590	15.71	15.71	9.42	9.42	3	0.24	0.01	0.05	0.00	0.00	24.0
37	330	-17942	-150	-376	0	350	-16676	15.71	15.71	9.42	9.42	3	0.30	0.01	0.02	0.00	0.00	24.0
38	330	-25242	-1096	-430	0	499	-7399	15.71	15.71	9.42	9.42	3	0.13	0.01	0.08	0.00	0.00	24.0
39	330	-20835	-593	-32	0	150	-10928	15.71	15.71	9.42	9.42	3	0.19	0.01	0.04	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	440	-16660	-483	-309	0	756	-7995	15.71	15.71	9.42	9.42	3	0.15	0.01	0.04	0.00	0.00	24.0
2	440	-12660	-340	-263	0	616	-7249	15.71	15.71	9.42	9.42	2	0.20	0.00	0.03	0.00	0.00	24.0
3	440	-12810	-342	-194	0	501	-7370	15.71	15.71	9.42	9.42	2	0.20	0.00	0.03	0.00	0.00	24.0
4	440	-12830	-401	-281	0	662	-4929	15.71	15.71	9.42	9.42	2	0.14	0.01	0.03	0.00	0.00	24.0
5	440	-12980	-403	-212	0	547	-5051	15.71	15.71	9.42	9.42	2	0.14	0.01	0.03	0.00	0.00	24.0
6	440	-12550	-359	-350	0	767	-6295	15.71	15.71	9.42	9.42	2	0.18	0.00	0.03	0.00	0.00	24.0
7	440	-13030	-366	-119	0	383	-6700	15.71	15.71	9.42	9.42	2	0.18	0.00	0.03	0.00	0.00	24.0
8	440	-12600	-377	-356	0	780	-5599	15.71	15.71	9.42	9.42	2	0.16	0.00	0.03	0.00	0.00	24.0
9	440	-13090	-384	-125	0	397	-6004	15.71	15.71	9.42	9.42	2	0.16	0.00	0.03	0.00	0.00	24.0
10	440	-12660	-340	-263	0	616	-7249	15.71	15.71	9.42	9.42	2	0.20	0.00	0.03	0.00	0.00	24.0
11	440	-12810	-342	-194	0	501	-7370	15.71	15.71	9.42	9.42	2	0.20	0.00	0.03	0.00	0.00	24.0
12	440	-12830	-401	-281	0	662	-4929	15.71	15.71	9.42	9.42	2	0.14	0.01	0.03	0.00	0.00	24.0
13	440	-12980	-403	-212	0	547	-5051	15.71	15.71	9.42	9.42	2	0.14	0.01	0.03	0.00	0.00	24.0
14	440	-12550	-359	-350	0	767	-6295	15.71	15.71	9.42	9.42	2	0.18	0.00	0.03	0.00	0.00	24.0
15	440	-13030	-366	-119	0	383	-6700	15.71	15.71	9.42	9.42	2	0.18	0.00	0.03	0.00	0.00	24.0
16	440	-12600	-377	-356	0	780	-5599	15.71	15.71	9.42	9.42	2	0.16	0.00	0.03	0.00	0.00	24.0
17	440	-13090	-384	-125	0	397	-6004	15.71	15.71	9.42	9.42	2	0.16	0.00	0.03	0.00	0.00	24.0
18	440	-20030	-614	-431	0	857	-17600	15.71	15.71	9.42	9.42	3	0.32	0.01	0.05	0.00	0.00	24.0
19	440	-24410	-766	-464	0	983	-12430	15.71	15.71	9.42	9.42	3	0.22	0.01	0.05	0.00	0.00	24.0
20	440	-21770	-672	-225	0	511	-14330	15.71	15.71	9.42	9.42	3	0.25	0.01	0.05	0.00	0.00	24.0
37	440	-16800	-496	-376	0	763	-17030	15.71	15.71	9.42	9.42	3	0.31	0.01	0.04	0.00	0.00	24.0
38	440	-24100	-749	-430	0	973	-8414	15.71	15.71	9.42	9.42	3	0.15	0.01	0.05	0.00	0.00	24.0
39	440	-19690	-593	-32	0	186	-11580	15.71	15.71	9.42	9.42	3	0.21	0.01	0.04	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 16 NI 263 NF 264 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 25B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-21630	95	-159	0	-499	86	6.28	6.28	9.42	9.42	3	0.02	0.00	0.02	0.00	0.00	24.0
2	0	-17810	227	-189	0	-538	-265	6.28	6.28	9.42	9.42	2	0.05	0.01	0.02	0.00	0.00	24.0
3	0	-17630	226	-80	0	-286	-264	6.28	6.28	9.42	9.42	2	0.04	0.01	0.02	0.00	0.00	24.0
4	0	-15650	-81	-164	0	-483	396	6.28	6.28	9.42	9.42	2	0.06	0.00	0.02	0.00	0.00	24.0
5	0	-15470	-81	-55	0	-230	397	6.28	6.28	9.42	9.42	2	0.05	0.00	0.01	0.00	0.00	24.0
6	0	-17260	120	-308	0	-813	-34	6.28	6.28	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
7	0	-16670	118	56	0	28	-31	6.28	6.28	9.42	9.42	2	0.00	0.00	0.01	0.00	0.00	24.0
8	0	-16610	28	-300	0	-796	164	6.28	6.28	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
9	0	-16020	26	64	0	45	167	6.28	6.28	9.42	9.42	2	0.02	0.00	0.01	0.00	0.00	24.0
10	0	-17810	227	-189	0	-538	-265	6.28	6.28	9.42	9.42	2	0.05	0.01	0.02	0.00	0.00	24.0
11	0	-17630	226	-80	0	-286	-264	6.28	6.28	9.42	9.42	2	0.04	0.01	0.02	0.00	0.00	24.0
12	0	-15650	-81	-164	0	-483	396	6.28	6.28	9.42	9.42	2	0.06	0.00	0.02	0.00	0.00	24.0
13	0	-15470	-81	-55	0	-230	397	6.28	6.28	9.42	9.42	2	0.05	0.00	0.01	0.00	0.00	24.0
14	0	-17260	120	-308	0	-813	-34	6.28	6.28	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
15	0	-16670	118	56	0	28	-31	6.28	6.28	9.42	9.42	2	0.00	0.00	0.01	0.00	0.00	24.0
16	0	-16610	28	-300	0	-796	164	6.28	6.28	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
17	0	-16020	26	64	0	45	167	6.28	6.28	9.42	9.42	2	0.02	0.00	0.01	0.00	0.00	24.0
18	0	-26780	715	-546	0	-1362	-911	6.28	6.28	9.42	9.42	3	0.10	0.02	0.06	0.00	0.00	24.0
19	0	-22340	-581	-418	0	-1070	1271	6.28	6.28	9.42	9.42	3	0.12	0.01	0.05	0.00	0.00	24.0
20	0	-23840	75	-369	0	-590	158	6.28	6.28	9.42	9.42	3	0.03	0.01	0.04	0.00	0.00	24.0
37	0	-27190	1156	-487	0	-1232	-1668	6.28	6.28	9.42	9.42	3	0.15	0.03	0.10	0.00	0.00	24.0

38	0	-19780	-1005	-273	0	-745	1968	6.28	6.28	9.42	9.42	3	0.19	0.02	0.10	0.00	0.00	24.0
39	0	-22280	90	-192	0	54	112	6.28	6.28	9.42	9.42	3	0.01	0.00	0.02	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	97	-21060	95	-159	0	-345	179	6.28	6.28	9.42	9.42	3	0.02	0.00	0.02	0.00	0.00	24.0
2	97	-17370	227	-189	0	-354	-43	6.28	6.28	9.42	9.42	2	0.02	0.01	0.02	0.00	0.00	24.0
3	97	-17192	226	-80	0	-208	-43	6.28	6.28	9.42	9.42	2	0.01	0.01	0.02	0.00	0.00	24.0
4	97	-15210	-81	-164	0	-323	318	6.28	6.28	9.42	9.42	2	0.04	0.00	0.02	0.00	0.00	24.0
5	97	-15030	-81	-55	0	-177	318	6.28	6.28	9.42	9.42	2	0.04	0.00	0.01	0.00	0.00	24.0
6	97	-16820	120	-308	0	-513	82	6.28	6.28	9.42	9.42	2	0.03	0.01	0.03	0.00	0.00	24.0
7	97	-16232	118	56	0	-26	84	6.28	6.28	9.42	9.42	2	0.01	0.00	0.01	0.00	0.00	24.0
8	97	-16170	28	-300	0	-504	191	6.28	6.28	9.42	9.42	2	0.04	0.01	0.03	0.00	0.00	24.0
9	97	-15582	26	64	0	-17	192	6.28	6.28	9.42	9.42	2	0.02	0.00	0.01	0.00	0.00	24.0
10	97	-17370	227	-189	0	-354	-43	6.28	6.28	9.42	9.42	2	0.02	0.01	0.02	0.00	0.00	24.0
11	97	-17192	226	-80	0	-208	-43	6.28	6.28	9.42	9.42	2	0.01	0.01	0.02	0.00	0.00	24.0
12	97	-15210	-81	-164	0	-323	318	6.28	6.28	9.42	9.42	2	0.04	0.00	0.02	0.00	0.00	24.0
13	97	-15030	-81	-55	0	-177	318	6.28	6.28	9.42	9.42	2	0.04	0.00	0.01	0.00	0.00	24.0
14	97	-16820	120	-308	0	-513	82	6.28	6.28	9.42	9.42	2	0.03	0.01	0.03	0.00	0.00	24.0
15	97	-16232	118	56	0	-26	84	6.28	6.28	9.42	9.42	2	0.01	0.00	0.01	0.00	0.00	24.0
16	97	-16170	28	-300	0	-504	191	6.28	6.28	9.42	9.42	2	0.04	0.01	0.03	0.00	0.00	24.0
17	97	-15582	26	64	0	-17	192	6.28	6.28	9.42	9.42	2	0.02	0.00	0.01	0.00	0.00	24.0
18	97	-26210	623	-546	0	-829	-259	6.28	6.28	9.42	9.42	3	0.04	0.01	0.05	0.00	0.00	24.0
19	97	-21770	-489	-418	0	-663	749	6.28	6.28	9.42	9.42	3	0.07	0.01	0.05	0.00	0.00	24.0
20	97	-23270	75	-239	0	-295	231	6.28	6.28	9.42	9.42	3	0.02	0.01	0.02	0.00	0.00	24.0
37	97	-26618	1002	-487	0	-757	-616	6.28	6.28	9.42	9.42	3	0.06	0.02	0.08	0.00	0.00	24.0
38	97	-19210	-851	-273	0	-479	1063	6.28	6.28	9.42	9.42	3	0.10	0.02	0.08	0.00	0.00	24.0
39	97	-21710	90	25	0	133	200	6.28	6.28	9.42	9.42	3	0.02	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	195	-20490	95	-159	0	-190	271	6.28	6.28	9.42	9.42	3	0.03	0.00	0.02	0.00	0.00	24.0
2	195	-16930	227	-189	0	-170	178	6.28	6.28	9.42	9.42	2	0.02	0.01	0.02	0.00	0.00	24.0
3	195	-16755	226	-80	0	-130	178	6.28	6.28	9.42	9.42	2	0.02	0.01	0.02	0.00	0.00	24.0
4	195	-14770	-81	-164	0	-163	239	6.28	6.28	9.42	9.42	2	0.03	0.00	0.02	0.00	0.00	24.0
5	195	-14590	-81	-55	0	-123	239	6.28	6.28	9.42	9.42	2	0.03	0.00	0.01	0.00	0.00	24.0
6	195	-16380	120	-308	0	-213	199	6.28	6.28	9.42	9.42	2	0.03	0.01	0.03	0.00	0.00	24.0
7	195	-15795	118	56	0	-81	199	6.28	6.28	9.42	9.42	2	0.02	0.00	0.01	0.00	0.00	24.0
8	195	-15730	28	-300	0	-211	218	6.28	6.28	9.42	9.42	2	0.03	0.01	0.03	0.00	0.00	24.0
9	195	-15145	26	64	0	-79	218	6.28	6.28	9.42	9.42	2	0.02	0.00	0.01	0.00	0.00	24.0
10	195	-16930	227	-189	0	-170	178	6.28	6.28	9.42	9.42	2	0.02	0.01	0.02	0.00	0.00	24.0
11	195	-16755	226	-80	0	-130	178	6.28	6.28	9.42	9.42	2	0.02	0.01	0.02	0.00	0.00	24.0
12	195	-14770	-81	-164	0	-163	239	6.28	6.28	9.42	9.42	2	0.03	0.00	0.02	0.00	0.00	24.0
13	195	-14590	-81	-55	0	-123	239	6.28	6.28	9.42	9.42	2	0.03	0.00	0.01	0.00	0.00	24.0
14	195	-16380	120	-308	0	-213	199	6.28	6.28	9.42	9.42	2	0.03	0.01	0.03	0.00	0.00	24.0
15	195	-15795	118	56	0	-81	199	6.28	6.28	9.42	9.42	2	0.02	0.00	0.01	0.00	0.00	24.0
16	195	-15730	28	-300	0	-211	218	6.28	6.28	9.42	9.42	2	0.03	0.01	0.03	0.00	0.00	24.0
17	195	-15145	26	64	0	-79	218	6.28	6.28	9.42	9.42	2	0.02	0.00	0.01	0.00	0.00	24.0
18	195	-25640	531	-546	0	-297	304	6.28	6.28	9.42	9.42	3	0.03	0.01	0.05	0.00	0.00	24.0
19	195	-21200	-397	-418	0	-255	317	6.28	6.28	9.42	9.42	3	0.03	0.01	0.04	0.00	0.00	24.0
20	195	-22700	75	-127	0	-119	305	6.28	6.28	9.42	9.42	3	0.03	0.00	0.01	0.00	0.00	24.0
37	195	-26045	849	-487	0	-281	286	6.28	6.28	9.42	9.42	3	0.03	0.02	0.08	0.00	0.00	24.0
38	195	-18640	-698	-273	0	-212	308	6.28	6.28	9.42	9.42	3	0.03	0.02	0.07	0.00	0.00	24.0
39	195	-21140	90	212	0	15	287	6.28	6.28	9.42	9.42	3	0.03	0.00	0.02	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	292	-19920	95	-159	0	-36	363	6.28	6.28	9.42	9.42	3	0.03	0.00	0.02	0.00	0.00	24.0
2	292	-16490	227	-189	0	14	399	6.28	6.28	9.42	9.42	2	0.04	0.01	0.02	0.00	0.00	24.0
3	292	-16318	226	-80	0	-52	399	6.28	6.28	9.42	9.42	2	0.04	0.01	0.02	0.00	0.00	24.0
4	292	-14330	-81	-164	0	-3	160	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
5	292	-14150	-81	-55	0	-69	160	6.28	6.28	9.42	9.42	2	0.02	0.00	0.01	0.00	0.00	24.0
6	292	-15940	120	-308	0	86	316	6.28	6.28	9.42	9.42	2	0.03	0.01	0.03	0.00	0.00	24.0
7	292	-15358	118	56	0	-136	314	6.28	6.28	9.42	9.42	2	0.04	0.00	0.01	0.00	0.00	24.0
8	292	-15290	28	-300	0	81	245	6.28	6.28	9.42	9.42	2	0.03	0.01	0.03	0.00	0.00	24.0
9	292	-14708	26	64	0	-141	243	6.28	6.28	9.42	9.42	2	0.03	0.00	0.01	0.00	0.00	24.0
10	292	-16490	227	-189	0	14	399	6.28	6.28	9.42	9.42	2	0.04	0.01	0.02	0.00	0.00	24.0
11	292	-16318	226	-80	0	-52	399	6.28	6.28	9.42	9.42	2	0.04	0.01	0.02	0.00	0.00	24.0
12	292	-14330	-81	-164	0	-3	160	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
13	292	-14150	-81	-55	0	-69	160	6.28	6.28	9.42	9.42	2	0.02	0.00	0.01	0.00	0.00	24.0
14	292	-15940	120	-308	0	86	316	6.28	6.28	9.42	9.42	2	0.03	0.01	0.03	0.00	0.00	24.0
15	292	-15358	118	56	0	-136	314	6.28	6.28	9.42	9.42	2	0.04	0.00	0.01	0.00	0.00	24.0
16	292	-15290	28	-300	0	81	245	6.28	6.28	9.42	9.42	2	0.03	0.01	0.03	0.00	0.00	24.0
17	292	-14708	26	64	0	-141	243	6.28	6.28	9.42	9.42	2	0.03	0.00	0.01	0.00	0.00	24.0
18	292	-25070	439	-546	0	236	776	6.28	6.28	9.42	9.42	3	0.07	0.01	0.05	0.00	0.00	24.0
19	292	-20630	-305	-418	0	152	-25	6.28	6.28	9.42	9.42	3	0.01	0.01	0.04	0.00	0.00	24.0
20	292	-22130	75	-34	0	-42	378	6.28	6.28	9.42	9.42	3	0.03	0.00	0.01	0.00	0.00	24.0
37	292	-25472	695	-487	0	194	1038	6.28	6.28	9.42	9.42	3	0.09	0.02	0.06	0.00	0.00	24.0
38	292	-18070	-544	-273	0	54	-298	6.28	6.28	9.42	9.42	3	0.03	0.01	0.05	0.00	0.00	24.0
39	292	-20570	90	367	0	-270	375	6.28	6.28	9.42	9.42	3	0.04	0.01	0.04	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	390	-19350	95	-159	0	119	456	6.28	6.28	9.42	9.42	3	0.04	0.00	0.02	0.00	0.00	24.0
2	390	-16050	227	-189	0	199	620	6.28	6.28	9.42	9.42	2	0.07	0.01	0.02	0.00	0.00	24.0
3	390	-15880	226	-80	0	26	619	6.28	6.28	9.42	9.42	2	0.06	0.01	0.02	0.00	0.00	24.0
4	390	-13890	-81	-164	0	158	82	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
5	390	-13710	-81	-55	0	-16	81	6.28	6.28	9.42	9.42	2	0.01	0.00	0.01	0.00	0.00	24.0
6	390	-15500	120	-308	0	386	433	6.28	6.28	9.42	9.42	2	0.06	0.01	0.03	0.00	0.00	24.0
7	390	-14920	118	56	0	-191	430	6.28	6.28	9.42	9.42	2	0.05	0.00	0.01	0.00	0.00	24.0
8	390	-14850	28	-300	0	374	272	6.28	6.28	9.42	9.42	2	0.04	0.01	0.03	0.00	0.00	24.0
9	390	-14270	26	64	0	-203	268	6.28	6.28	9.42	9.42	2	0.03	0.00	0.01	0.00	0.00	24.0
10	390	-16050	227	-189	0	199	620	6.28	6.28	9.42	9.42	2	0.07	0.01	0.02	0.00	0.00	24.0
11	390	-15880	226	-80	0	26	619	6.28	6.28	9.42	9.42	2	0.06	0.01	0.02	0.00	0.00	24.0
12	390	-13890	-81	-164	0	158	82	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
13	390	-13710	-81	-55	0	-16	81	6.28	6.28	9.42	9.42	2	0.01	0.00	0.01	0.00	0.00	24.0
14	390	-15500	120	-308	0	386	433	6.28	6.28	9.42	9.42	2	0.06	0.01	0.03	0.00	0.00	24.0
15	390	-14920	118	56	0	-191	430	6.28	6.28	9.42	9.42	2	0.05	0.00	0.01	0.00	0.00	24.0
16	390	-14850	28	-300	0	374	272	6.28	6.28	9.42	9.42	2	0.04	0.01	0.03	0.00	0.00	24.0
17	390	-14270	26	64	0	-203	268	6.28	6.28	9.42	9.42	2	0.03	0.00	0.01	0.00	0.00	24.0
18	390	-24500	346	-546	0	769	1159	6.28	6.28	9.42	9.42	3	0.11	0.01	0.05	0.00	0.00	24.0
19	390	-20060	-213	-418	0	559	-278	6.28	6.28	9.42	9.42	3	0.03	0.01	0.04	0.00	0.00	24.0
20	390	-21560	75	41	0	-47	452	6.28	6.28	9.42	9.42	3	0.04	0.00	0.01	0.00	0.00	24.0
37	390	-24900	542	-487	0	669	1641	6.28	6.28	9.42	9.42	3	0.15	0.01	0.05	0.00	0.00	24.0
38	390	-17500	-391	-273	0	320	-753	6.28	6.28	9.42	9.42	3	0.07	0.01	0.04	0.00	0.00	24.0
39	390	-20000	90	491	0	-690	462	6.28	6.28	9.42	9.42	3	0.05	0.01	0.05	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

VERIFICA NODO IN TESTA AL PILASTRO, NODO NUM. 264 NON CONFINATO

(par.7.2.2 NTC2018 "La domanda di resistenza valutata con i criteri della progettazione in capacità può essere assunta non superiore alla domanda di resistenza valutata per il caso di comportamento strutturale non dissipativo.")

PROGETTAZIONE IN CAPACITA'

Asse loc. pilastro y nodo ESTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 45.0 cm, hjc= 20.0 cm
Asse loc. pilastro z nodo INTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 30.0 cm, hjc= 50.0 cm

FxMin,inf	FxMin,sup	FxMax,sup	FySup	FzSup	Vjbdy	Vjbdz	Vres,y	Vres,z	I.R.compr.	Ashy	Ashz	PASSO	Nota
daN					daN		daN			cmq		cm	
-13710	-5873	-7790	45	169	17571	35064	61027	127974	0.29	4.26	5.97	8.10	

VERIFICA DI RESISTENZA CON SOLLECITAZIONI COMPORTAMENTO NON DISSIPATIVO

Asse loc. pilastro y nodo ESTERNO: Hjw= 40.0 cm, bj= 45.0 cm, hjc= 20.0 cm, db1= 45.0 cm

NC	Fx,sup	Fx,inf	Mb	Vb	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-7790	-16050	-1724	1988	297	3960	61027	0.06	0.00	40.00	
3	-7657	-15880	-1722	1987	298	3954	61061	0.06	0.00	40.00	
4	-6006	-13890	-382	1500	46	896	61486	0.01	0.00	40.00	
5	-5873	-13710	-380	1499	45	892	61520	0.01	0.00	40.00	
6	-7321	-15500	-1256	1818	176	2926	61148	0.05	0.00	40.00	
7	-6878	-14920	-1250	1815	179	2908	61262	0.05	0.00	40.00	
8	-6786	-14850	-853	1672	73	2034	61285	0.03	0.00	40.00	
9	-6342	-14270	-847	1669	76	2016	61399	0.03	0.00	40.00	
10	-7790	-16050	-1724	1988	297	3960	61027	0.06	0.00	40.00	
11	-7657	-15880	-1722	1987	298	3954	61061	0.06	0.00	40.00	
12	-6006	-13890	-382	1500	46	896	61486	0.01	0.00	40.00	
13	-5873	-13710	-380	1499	45	892	61520	0.01	0.00	40.00	
14	-7321	-15500	-1256	1818	176	2926	61148	0.05	0.00	40.00	
15	-6878	-14920	-1250	1815	179	2908	61262	0.05	0.00	40.00	
16	-6786	-14850	-853	1672	73	2034	61285	0.03	0.00	40.00	
17	-6342	-14270	-847	1669	76	2016	61399	0.03	0.00	40.00	

Asse loc. pilastro z nodo INTERNO: Hjw= 40.0 cm, bj= 30.0 cm, hjc= 50.0 cm, db1= 45.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb,1	Mb,2	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-7790	-16050	-2069	-1098	379	2018	127974	0.02	0.00	40.00	
3	-7657	-15880	-1839	-1295	282	1061	128031	0.01	0.00	40.00	
4	-6006	-13890	-2142	-1224	382	1884	128734	0.01	0.00	40.00	
5	-5873	-13710	-1912	-1421	285	927	128791	0.01	0.00	40.00	
6	-7321	-15500	-2362	-913	494	3085	128175	0.02	0.00	40.00	
7	-6878	-14920	-1597	-1568	169	98	128363	0.00	0.00	40.00	
8	-6786	-14850	-2384	-950	495	3045	128403	0.02	0.00	40.00	
9	-6342	-14270	-1619	-1606	170	138	128592	0.00	0.00	40.00	
10	-7790	-16050	-2069	-1098	379	2018	127974	0.02	0.00	40.00	
11	-7657	-15880	-1839	-1295	282	1061	128031	0.01	0.00	40.00	
12	-6006	-13890	-2142	-1224	382	1884	128734	0.01	0.00	40.00	
13	-5873	-13710	-1912	-1421	285	927	128791	0.01	0.00	40.00	
14	-7321	-15500	-2362	-913	494	3085	128175	0.02	0.00	40.00	
15	-6878	-14920	-1597	-1568	169	98	128363	0.00	0.00	40.00	
16	-6786	-14850	-2384	-950	495	3045	128403	0.02	0.00	40.00	
17	-6342	-14270	-1619	-1606	170	138	128592	0.00	0.00	40.00	

CONFRONTO E SINTESI CONCLUSIVE (si assume in ogni caso passo <= 15 cm)

I.R.compr.	Ashy	Ashz	PASSO	Nota
	cmq		cm	
0.06	--	--	15.00	**VERIFICATO**

ASTA NUM. 17 NI 49 NF 51 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 31C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-12680	573	-74	0	-138	-3711	15.71	15.71	9.42	9.42	3	0.07	0.01	0.05	0.00	0.00	24.0
2	0	-9644	507	-107	0	-192	-3084	15.71	15.71	9.42	9.42	2	0.08	0.01	0.04	0.00	0.00	24.0
3	0	-9591	488	42	0	40	-3021	15.71	15.71	9.42	9.42	2	0.08	0.01	0.04	0.00	0.00	24.0
4	0	-9920	394	-155	0	-253	-2688	15.71	15.71	9.42	9.42	2	0.07	0.01	0.03	0.00	0.00	24.0
5	0	-9867	375	-6	0	-21	-2625	15.71	15.71	9.42	9.42	2	0.07	0.00	0.03	0.00	0.00	24.0
6	0	-9802	490	-298	0	-484	-3019	15.71	15.71	9.42	9.42	2	0.09	0.01	0.04	0.00	0.00	24.0
7	0	-9626	426	199	0	289	-2809	15.71	15.71	9.42	9.42	2	0.08	0.01	0.04	0.00	0.00	24.0
8	0	-9885	456	-313	0	-502	-2900	15.71	15.71	9.42	9.42	2	0.09	0.01	0.04	0.00	0.00	24.0
9	0	-9709	392	185	0	271	-2690	15.71	15.71	9.42	9.42	2	0.08	0.01	0.03	0.00	0.00	24.0
10	0	-9644	507	-107	0	-192	-3084	15.71	15.71	9.42	9.42	2	0.08	0.01	0.04	0.00	0.00	24.0
11	0	-9591	488	42	0	40	-3021	15.71	15.71	9.42	9.42	2	0.08	0.01	0.04	0.00	0.00	24.0
12	0	-9920	394	-155	0	-253	-2688	15.71	15.71	9.42	9.42	2	0.07	0.01	0.03	0.00	0.00	24.0
13	0	-9867	375	-6	0	-21	-2625	15.71	15.71	9.42	9.42	2	0.07	0.00	0.03	0.00	0.00	24.0
14	0	-9802	490	-298	0	-484	-3019	15.71	15.71	9.42	9.42	2	0.09	0.01	0.04	0.00	0.00	24.0
15	0	-9626	426	199	0	289	-2809	15.71	15.71	9.42	9.42	2	0.08	0.01	0.04	0.00	0.00	24.0
16	0	-9885	456	-313	0	-502	-2900	15.71	15.71	9.42	9.42	2	0.09	0.01	0.04	0.00	0.00	24.0
17	0	-9709	392	185	0	271	-2690	15.71	15.71	9.42	9.42	2	0.08	0.01	0.03	0.00	0.00	24.0
18	0	-15950	1558	-16	0	-46	-6387	15.71	15.71	9.42	9.42	3	0.11	0.02	0.12	0.00	0.00	24.0
19	0	-20800	923	-140	0	-223	-8292	15.71	15.71	9.42	9.42	3	0.15	0.01	0.07	0.00	0.00	24.0
20	0	-17600	1192	121	0	94	-7058	15.71	15.71	9.42	9.42	3	0.13	0.02	0.09	0.00	0.00	24.0
37	0	-12510	1550	28	0	13	-4568	15.71	15.71	9.42	9.42	3	0.08	0.02	0.12	0.00	0.00	24.0
38	0	-20600	491	-178	0	-281	-7742	15.71	15.71	9.42	9.42	3	0.14	0.01	0.04	0.00	0.00	24.0
39	0	-15270	940	256	0	248	-5685	15.71	15.71	9.42	9.42	3	0.10	0.01	0.07	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	83	-11822	573	-74	0	-78	-3238	15.71	15.71	9.42	9.42	3	0.06	0.01	0.05	0.00	0.00	24.0

2	83	-8984	507	-107	0	-104	-2666	15.71	15.71	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
3	83	-8931	488	42	0	5	-2619	15.71	15.71	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
4	83	-9260	394	-155	0	-125	-2362	15.71	15.71	9.42	9.42	2	0.06	0.01	0.03	0.00	0.00	24.0
5	83	-9207	375	-6	0	-16	-2315	15.71	15.71	9.42	9.42	2	0.06	0.00	0.03	0.00	0.00	24.0
6	83	-9142	490	-298	0	-238	-2615	15.71	15.71	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
7	83	-8966	426	199	0	125	-2457	15.71	15.71	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
8	83	-9225	456	-313	0	-244	-2524	15.71	15.71	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
9	83	-9049	392	185	0	118	-2366	15.71	15.71	9.42	9.42	2	0.06	0.01	0.03	0.00	0.00	24.0
10	83	-8984	507	-107	0	-104	-2666	15.71	15.71	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
11	83	-8931	488	42	0	5	-2619	15.71	15.71	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
12	83	-9260	394	-155	0	-125	-2362	15.71	15.71	9.42	9.42	2	0.06	0.01	0.03	0.00	0.00	24.0
13	83	-9207	375	-6	0	-16	-2315	15.71	15.71	9.42	9.42	2	0.06	0.00	0.03	0.00	0.00	24.0
14	83	-9142	490	-298	0	-238	-2615	15.71	15.71	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
15	83	-8966	426	199	0	125	-2457	15.71	15.71	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
16	83	-9225	456	-313	0	-244	-2524	15.71	15.71	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
17	83	-9049	392	185	0	118	-2366	15.71	15.71	9.42	9.42	2	0.06	0.01	0.03	0.00	0.00	24.0
18	83	-15090	1352	-16	0	-33	-5187	15.71	15.71	9.42	9.42	3	0.09	0.02	0.11	0.00	0.00	24.0
19	83	-19942	1129	-140	0	-108	-7445	15.71	15.71	9.42	9.42	3	0.13	0.01	0.08	0.00	0.00	24.0
20	83	-16742	1192	121	0	-5	-6074	15.71	15.71	9.42	9.42	3	0.11	0.02	0.09	0.00	0.00	24.0
37	83	-11652	1206	28	0	-10	-3431	15.71	15.71	9.42	9.42	3	0.06	0.02	0.10	0.00	0.00	24.0
38	83	-19742	836	-178	0	-134	-7195	15.71	15.71	9.42	9.42	3	0.13	0.01	0.06	0.00	0.00	24.0
39	83	-14412	940	256	0	36	-4909	15.71	15.71	9.42	9.42	3	0.09	0.01	0.07	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	165	-10965	573	-74	0	-17	-2764	15.71	15.71	9.42	9.42	3	0.05	0.01	0.05	0.00	0.00	24.0
2	165	-8324	507	-107	0	-15	-2247	15.71	15.71	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
3	165	-8271	488	42	0	-29	-2216	15.71	15.71	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
4	165	-8600	394	-155	0	4	-2037	15.71	15.71	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
5	165	-8547	375	-6	0	-11	-2006	15.71	15.71	9.42	9.42	2	0.05	0.00	0.03	0.00	0.00	24.0
6	165	-8482	490	-298	0	8	-2211	15.71	15.71	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
7	165	-8306	426	199	0	-40	-2106	15.71	15.71	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
8	165	-8565	456	-313	0	14	-2148	15.71	15.71	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
9	165	-8389	392	185	0	-34	-2043	15.71	15.71	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
10	165	-8324	507	-107	0	-15	-2247	15.71	15.71	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
11	165	-8271	488	42	0	-29	-2216	15.71	15.71	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
12	165	-8600	394	-155	0	4	-2037	15.71	15.71	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
13	165	-8547	375	-6	0	-11	-2006	15.71	15.71	9.42	9.42	2	0.05	0.00	0.03	0.00	0.00	24.0
14	165	-8482	490	-298	0	8	-2211	15.71	15.71	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
15	165	-8306	426	199	0	-40	-2106	15.71	15.71	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
16	165	-8565	456	-313	0	14	-2148	15.71	15.71	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
17	165	-8389	392	185	0	-34	-2043	15.71	15.71	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
18	165	-14230	1145	-16	0	-20	-4156	15.71	15.71	9.42	9.42	3	0.08	0.01	0.09	0.00	0.00	24.0
19	165	-19085	1336	-140	0	8	-6429	15.71	15.71	9.42	9.42	3	0.11	0.02	0.10	0.00	0.00	24.0
20	165	-15885	1192	121	0	-105	-5090	15.71	15.71	9.42	9.42	3	0.09	0.02	0.09	0.00	0.00	24.0
37	165	-10794	862	28	0	-33	-2577	15.71	15.71	9.42	9.42	3	0.05	0.01	0.07	0.00	0.00	24.0
38	165	-18885	1180	-178	0	13	-6364	15.71	15.71	9.42	9.42	3	0.11	0.01	0.09	0.00	0.00	24.0
39	165	-13555	940	256	0	-175	-4133	15.71	15.71	9.42	9.42	3	0.08	0.01	0.07	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	248	-10108	573	-74	0	44	-2291	15.71	15.71	9.42	9.42	3	0.04	0.01	0.05	0.00	0.00	24.0
2	248	-7664	507	-107	0	74	-1829	15.71	15.71	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
3	248	-7611	488	42	0	-64	-1814	15.71	15.71	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
4	248	-7940	394	-155	0	132	-1712	15.71	15.71	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
5	248	-7887	375	-6	0	-6	-1696	15.71	15.71	9.42	9.42	2	0.04	0.00	0.03	0.00	0.00	24.0
6	248	-7822	490	-298	0	255	-1806	15.71	15.71	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
7	248	-7646	426	199	0	-204	-1754	15.71	15.71	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
8	248	-7905	456	-313	0	272	-1771	15.71	15.71	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
9	248	-7729	392	185	0	-187	-1719	15.71	15.71	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
10	248	-7664	507	-107	0	74	-1829	15.71	15.71	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
11	248	-7611	488	42	0	-64	-1814	15.71	15.71	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
12	248	-7940	394	-155	0	132	-1712	15.71	15.71	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
13	248	-7887	375	-6	0	-6	-1696	15.71	15.71	9.42	9.42	2	0.04	0.00	0.03	0.00	0.00	24.0
14	248	-7822	490	-298	0	255	-1806	15.71	15.71	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
15	248	-7646	426	199	0	-204	-1754	15.71	15.71	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
16	248	-7905	456	-313	0	272	-1771	15.71	15.71	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
17	248	-7729	392	185	0	-187	-1719	15.71	15.71	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
18	248	-13370	939	-16	0	-6	-3297	15.71	15.71	9.42	9.42	3	0.06	0.01	0.07	0.00	0.00	24.0
19	248	-18228	1542	-140	0	123	-5241	15.71	15.71	9.42	9.42	3	0.09	0.02	0.12	0.00	0.00	24.0
20	248	-15028	1192	121	0	-205	-4107	15.71	15.71	9.42	9.42	3	0.08	0.02	0.09	0.00	0.00	24.0
37	248	-9935	518	28	0	-55	-2008	15.71	15.71	9.42	9.42	3	0.04	0.01	0.04	0.00	0.00	24.0
38	248	-18028	1524	-178	0	160	-5249	15.71	15.71	9.42	9.42	3	0.09	0.02	0.12	0.00	0.00	24.0
39	248	-12698	940	256	0	-386	-3358	15.71	15.71	9.42	9.42	3	0.06	0.01	0.08	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	330	-9250	573	-74	0	105	-1818	15.71	15.71	9.42	9.42	3	0.03	0.01	0.05	0.00	0.00	24.0
2	330	-7004	507	-107	0	162	-1411	15.71	15.71	9.42	9.42	2	0.04	0.01	0.04	0.00	0.00	24.0
3	330	-6951	488	42	0	-98	-1411	15.71	15.71	9.42	9.42	2	0.04	0.01	0.04	0.00	0.00	24.0
4	330	-7280	394	-155	0	260	-1386	15.71	15.71	9.42	9.42	2	0.04	0.01	0.03	0.00	0.00	24.0
5	330	-7227	375	-6	0	-1	-1386	15.71	15.71	9.42	9.42	2	0.04	0.00	0.03	0.00	0.00	24.0
6	330	-7162	490	-298	0	501	-1402	15.71	15.71	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
7	330	-6986	426	199	0	-368	-1403	15.71	15.71	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
8	330	-7245	456	-313	0	530	-1395	15.71	15.71	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
9	330	-7069	392	185	0	-339	-1395	15.71	15.71	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
10	330	-7004	507	-107	0	162	-1411	15.71	15.71	9.42	9.42	2	0.04	0.01	0.04	0.00	0.00	24.0
11	330	-6951	488	42	0	-98	-1411	15.71	15.71	9.42	9.42	2	0.04	0.01	0.04	0.00	0.00	24.0
12	330	-7280	394	-155	0	260	-1386	15.71	15.71	9.42	9.42	2	0.04	0.01	0.03	0.00	0.00	24.0
13	330	-7227	375	-6	0	-1	-1386	15.71	15.71	9.42	9.42	2	0.04	0.00	0.03	0.00	0.00	24.0
14	330	-7162	490	-298	0	501	-1402	15.71	15.71	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
15	330	-6986	426	199	0	-368	-1403	15.71	15.71	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
16	330	-7245	456	-313	0	530	-1395	15.71	15.71	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
17	330	-7069	392	185	0	-339	-1395	15.71	15.71	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
18	330	-12510	733	-16	0	7	-2607	15.71	15.71	9.42	9.42	3	0.05	0.01	0.06	0.00	0.00	24.0
19	330	-17370	1749	-140	0	239	-3884	15.71	15.71	9.42	9.42	3	0.07	0.02	0.13	0.00	0.00	24.0
20	330	-14170	1192	121	0	-305	-3123	15.71	15.71	9.42	9.42	3	0.06	0.02	0.09	0.00	0.00	24.0
37	330	-9077	174	28	0	-78	-1722	15.71	15.71	9.42	9.42	3	0.03	0.00	0.01	0.00	0.00	24.0
38	330	-17170	1868	-178	0	308	-3850	15.71	15.71	9.42	9.42	3	0.07	0.02	0.14	0.00	0.00	24.0
39	330	-11840	940	256	0	-598	-2582	15.71	15.71	9.42	9.42	3	0.05	0.01	0.08	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 18 NI 92 NF 94 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 30C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza	aswta	aswto	PASSO
	--																

	cm		daN		daN*m		cmq				Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-14610	1354	-173	0	-271	-7137	15.71	15.71	9.42	9.42	3	0.13	0.02	0.11	0.00	0.00	24.0
2	0	-11230	1249	-197	0	-309	-6247	15.71	15.71	9.42	9.42	2	0.17	0.02	0.10	0.00	0.00	24.0
3	0	-11270	1261	-50	0	-73	-6298	15.71	15.71	9.42	9.42	2	0.16	0.02	0.10	0.00	0.00	24.0
4	0	-11210	822	-216	0	-343	-4682	15.71	15.71	9.42	9.42	2	0.13	0.01	0.07	0.00	0.00	24.0
5	0	-11240	834	-70	0	-107	-4733	15.71	15.71	9.42	9.42	2	0.12	0.01	0.07	0.00	0.00	24.0
6	0	-11180	1085	-374	0	-596	-5639	15.71	15.71	9.42	9.42	2	0.16	0.01	0.09	0.00	0.00	24.0
7	0	-11300	1126	113	0	190	-5810	15.71	15.71	9.42	9.42	2	0.15	0.01	0.09	0.00	0.00	24.0
8	0	-11170	957	-380	0	-606	-5170	15.71	15.71	9.42	9.42	2	0.15	0.01	0.08	0.00	0.00	24.0
9	0	-11290	998	107	0	180	-5340	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
10	0	-11230	1249	-197	0	-309	-6247	15.71	15.71	9.42	9.42	2	0.17	0.02	0.10	0.00	0.00	24.0
11	0	-11270	1261	-50	0	-73	-6298	15.71	15.71	9.42	9.42	2	0.16	0.02	0.10	0.00	0.00	24.0
12	0	-11210	822	-216	0	-343	-4682	15.71	15.71	9.42	9.42	2	0.13	0.01	0.07	0.00	0.00	24.0
13	0	-11240	834	-70	0	-107	-4733	15.71	15.71	9.42	9.42	2	0.12	0.01	0.07	0.00	0.00	24.0
14	0	-11180	1085	-374	0	-596	-5639	15.71	15.71	9.42	9.42	2	0.16	0.01	0.09	0.00	0.00	24.0
15	0	-11300	1126	113	0	190	-5810	15.71	15.71	9.42	9.42	2	0.15	0.01	0.09	0.00	0.00	24.0
16	0	-11170	957	-380	0	-606	-5170	15.71	15.71	9.42	9.42	2	0.15	0.01	0.08	0.00	0.00	24.0
17	0	-11290	998	107	0	180	-5340	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
18	0	-20290	3636	-297	0	-437	-14830	15.71	15.71	9.42	9.42	3	0.26	0.05	0.27	0.00	0.00	24.0
19	0	-23870	1922	-356	0	-560	-12830	15.71	15.71	9.42	9.42	3	0.23	0.02	0.14	0.00	0.00	24.0
20	0	-21010	2597	-100	0	-183	-12960	15.71	15.71	9.42	9.42	3	0.23	0.03	0.19	0.00	0.00	24.0
37	0	-16700	3742	-226	0	-320	-13320	15.71	15.71	9.42	9.42	3	0.24	0.05	0.29	0.00	0.00	24.0
38	0	-22670	884	-325	0	-525	-9982	15.71	15.71	9.42	9.42	3	0.18	0.01	0.06	0.00	0.00	24.0
39	0	-17900	2010	103	0	104	-10190	15.71	15.71	9.42	9.42	3	0.18	0.03	0.15	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	83	-13752	1354	-173	0	-127	-6020	15.71	15.71	9.42	9.42	3	0.11	0.02	0.11	0.00	0.00	24.0
2	83	-10571	1249	-197	0	-147	-5216	15.71	15.71	9.42	9.42	2	0.14	0.02	0.10	0.00	0.00	24.0
3	83	-10610	1261	-50	0	-32	-5258	15.71	15.71	9.42	9.42	2	0.13	0.02	0.10	0.00	0.00	24.0
4	83	-10549	822	-216	0	-164	-4004	15.71	15.71	9.42	9.42	2	0.11	0.01	0.07	0.00	0.00	24.0
5	83	-10580	834	-70	0	-49	-4045	15.71	15.71	9.42	9.42	2	0.10	0.01	0.07	0.00	0.00	24.0
6	83	-10520	1085	-374	0	-287	-4744	15.71	15.71	9.42	9.42	2	0.13	0.01	0.09	0.00	0.00	24.0
7	83	-10641	1126	113	0	96	-4881	15.71	15.71	9.42	9.42	2	0.13	0.01	0.09	0.00	0.00	24.0
8	83	-10511	957	-380	0	-292	-4381	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
9	83	-10631	998	107	0	91	-4517	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
10	83	-10571	1249	-197	0	-147	-5216	15.71	15.71	9.42	9.42	2	0.14	0.02	0.10	0.00	0.00	24.0
11	83	-10610	1261	-50	0	-32	-5258	15.71	15.71	9.42	9.42	2	0.13	0.02	0.10	0.00	0.00	24.0
12	83	-10549	822	-216	0	-164	-4004	15.71	15.71	9.42	9.42	2	0.11	0.01	0.07	0.00	0.00	24.0
13	83	-10580	834	-70	0	-49	-4045	15.71	15.71	9.42	9.42	2	0.10	0.01	0.07	0.00	0.00	24.0
14	83	-10520	1085	-374	0	-287	-4744	15.71	15.71	9.42	9.42	2	0.13	0.01	0.09	0.00	0.00	24.0
15	83	-10641	1126	113	0	96	-4881	15.71	15.71	9.42	9.42	2	0.13	0.01	0.09	0.00	0.00	24.0
16	83	-10511	957	-380	0	-292	-4381	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
17	83	-10631	998	107	0	91	-4517	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
18	83	-19432	3430	-297	0	-192	-11916	15.71	15.71	9.42	9.42	3	0.21	0.04	0.26	0.00	0.00	24.0
19	83	-23012	2128	-356	0	-266	-11159	15.71	15.71	9.42	9.42	3	0.20	0.03	0.15	0.00	0.00	24.0
20	83	-20152	2597	-100	0	-100	-10817	15.71	15.71	9.42	9.42	3	0.19	0.03	0.19	0.00	0.00	24.0
37	83	-15842	3398	-226	0	-134	-10375	15.71	15.71	9.42	9.42	3	0.19	0.04	0.26	0.00	0.00	24.0
38	83	-21812	1229	-325	0	-256	-9110	15.71	15.71	9.42	9.42	3	0.16	0.02	0.09	0.00	0.00	24.0
39	83	-17040	2010	103	0	19	-8533	15.71	15.71	9.42	9.42	3	0.15	0.03	0.15	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	165	-12895	1354	-173	0	16	-4903	15.71	15.71	9.42	9.42	3	0.09	0.02	0.11	0.00	0.00	24.0
2	165	-9912	1249	-197	0	15	-4186	15.71	15.71	9.42	9.42	2	0.11	0.02	0.10	0.00	0.00	24.0
3	165	-9950	1261	-50	0	10	-4217	15.71	15.71	9.42	9.42	2	0.11	0.02	0.10	0.00	0.00	24.0
4	165	-9888	822	-216	0	14	-3326	15.71	15.71	9.42	9.42	2	0.09	0.01	0.07	0.00	0.00	24.0
5	165	-9921	834	-70	0	9	-3357	15.71	15.71	9.42	9.42	2	0.09	0.01	0.07	0.00	0.00	24.0
6	165	-9860	1085	-374	0	22	-3849	15.71	15.71	9.42	9.42	2	0.10	0.01	0.09	0.00	0.00	24.0
7	165	-9982	1126	113	0	3	-3952	15.71	15.71	9.42	9.42	2	0.10	0.01	0.09	0.00	0.00	24.0
8	165	-9852	957	-380	0	21	-3591	15.71	15.71	9.42	9.42	2	0.09	0.01	0.08	0.00	0.00	24.0
9	165	-9972	998	107	0	2	-3694	15.71	15.71	9.42	9.42	2	0.09	0.01	0.08	0.00	0.00	24.0
10	165	-9912	1249	-197	0	15	-4186	15.71	15.71	9.42	9.42	2	0.11	0.02	0.10	0.00	0.00	24.0
11	165	-9950	1261	-50	0	10	-4217	15.71	15.71	9.42	9.42	2	0.11	0.02	0.10	0.00	0.00	24.0
12	165	-9888	822	-216	0	14	-3326	15.71	15.71	9.42	9.42	2	0.09	0.01	0.07	0.00	0.00	24.0
13	165	-9921	834	-70	0	9	-3357	15.71	15.71	9.42	9.42	2	0.09	0.01	0.07	0.00	0.00	24.0
14	165	-9860	1085	-374	0	22	-3849	15.71	15.71	9.42	9.42	2	0.10	0.01	0.09	0.00	0.00	24.0
15	165	-9982	1126	113	0	3	-3952	15.71	15.71	9.42	9.42	2	0.10	0.01	0.09	0.00	0.00	24.0
16	165	-9852	957	-380	0	21	-3591	15.71	15.71	9.42	9.42	2	0.09	0.01	0.08	0.00	0.00	24.0
17	165	-9972	998	107	0	2	-3694	15.71	15.71	9.42	9.42	2	0.09	0.01	0.08	0.00	0.00	24.0
18	165	-18575	3223	-297	0	53	-9172	15.71	15.71	9.42	9.42	3	0.16	0.04	0.24	0.00	0.00	24.0
19	165	-22155	2334	-356	0	28	-9318	15.71	15.71	9.42	9.42	3	0.16	0.03	0.17	0.00	0.00	24.0
20	165	-19295	2597	-100	0	-18	-8673	15.71	15.71	9.42	9.42	3	0.15	0.03	0.19	0.00	0.00	24.0
37	165	-14985	3054	-226	0	53	-7714	15.71	15.71	9.42	9.42	3	0.14	0.04	0.24	0.00	0.00	24.0
38	165	-20955	1573	-325	0	12	-7955	15.71	15.71	9.42	9.42	3	0.14	0.02	0.12	0.00	0.00	24.0
39	165	-16180	2010	103	0	-65	-6877	15.71	15.71	9.42	9.42	3	0.12	0.03	0.16	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	248	-12038	1354	-173	0	159	-3786	15.71	15.71	9.42	9.42	3	0.07	0.02	0.11	0.00	0.00	24.0
2	248	-9252	1249	-197	0	178	-3156	15.71	15.71	9.42	9.42	2	0.08	0.02	0.10	0.00	0.00	24.0
3	248	-9290	1261	-50	0	51	-3177	15.71	15.71	9.42	9.42	2	0.08	0.02	0.11	0.00	0.00	24.0
4	248	-9227	822	-216	0	192	-2648	15.71	15.71	9.42	9.42	2	0.07	0.01	0.07	0.00	0.00	24.0
5	248	-9262	834	-70	0	66	-2669	15.71	15.71	9.42	9.42	2	0.07	0.01	0.07	0.00	0.00	24.0
6	248	-9201	1085	-374	0	330	-2953	15.71	15.71	9.42	9.42	2	0.08	0.01	0.09	0.00	0.00	24.0
7	248	-9322	1126	113	0	-90	-3024	15.71	15.71	9.42	9.42	2	0.08	0.01	0.09	0.00	0.00	24.0
8	248	-9192	957	-380	0	334	-2802	15.71	15.71	9.42	9.42	2	0.08	0.01	0.08	0.00	0.00	24.0
9	248	-9314	998	107	0	-86	-2872	15.71	15.71	9.42	9.42	2	0.08	0.01	0.08	0.00	0.00	24.0
10	248	-9252	1249	-197	0	178	-3156	15.71	15.71	9.42	9.42	2	0.08	0.02	0.10	0.00	0.00	24.0
11	248	-9290	1261	-50	0	51	-3177	15.71	15.71	9.42	9.42	2	0.08	0.02	0.11	0.00	0.00	24.0
12	248	-9227	822	-216	0	192	-2648	15.71	15.71	9.42	9.42	2	0.07	0.01	0.07	0.00	0.00	24.0
13	248	-9262	834	-70	0	66	-2669	15.71	15.71	9.42	9.42	2	0.07	0.01	0.07	0.00	0.00	24.0
14	248	-9201	1085	-374	0	330	-2953	15.71	15.71	9.42	9.42	2	0.08	0.01	0.09	0.00	0.00	24.0
15	248	-9322	1126	113	0	-90	-3024	15.71	15.71	9.42	9.42	2	0.08	0.01	0.09	0.00	0.00	24.0
16	248	-9192	957	-380	0	334	-2802	15.71	15.71	9.42	9.42	2	0.08	0.01	0.08	0.00	0.00	24.0
17	248	-9314	998	107	0	-86	-2872	15.71	15.71	9.42	9.42	2	0.08	0.01	0.08	0.00	0.00	24.0
18	248	-17718	3016	-297	0	298	-6599	15.71	15.71	9.42	9.42	3	0.12	0.04	0.23	0.00	0.00	24.0
19	248	-21298	2541	-356	0	322	-7307	15.71	15.71	9.42	9.42	3	0.13	0.03	0.19	0.00	0.00	24.0
20	248	-18438	2597	-100	0	65	-6530	15.71	15.71	9.42	9.42	3	0.12	0.03	0.20	0.00	0.00	24.0
37	248	-14128	2710	-226	0	239	-5337	15.71	15.71	9.42	9.42	3	0.10	0.03	0.21	0.00	0.00	24.0
38	248	-20098	1917	-325	0	280	-6515	15.71	15.71	9.42	9.42	3	0.12	0.02	0.14	0.00	0.00	24.0
39	248	-15320	2010	103	0	-150	-5220	15.71	15.71	9.42	9.42	3	0.09	0.03	0.16	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	330	-11180	1354	-173	0	302	-2669	15.71	15.71	9.42	9.42	3	0.05	0.02	0.11	0.00	0.00	24.0
2	330	-8593	1249	-197	0	340	-2125	15.71	15.71	9.42	9.42	2	0.06	0.02	0.11	0.00	0.00	24.0
3	330	-8630	1261	-50	0	93	-2136	15.71	15.71	9.42	9.42	2	0.06	0.02	0.11	0.00	0.00	24.0

4	330	-8566	822	-216	0	371	-1970	15.71	15.71	9.42	9.42	2	0.06	0.01	0.07	0.00	0.00	24.0
5	330	-8602	834	-70	0	124	-1981	15.71	15.71	9.42	9.42	2	0.05	0.01	0.07	0.00	0.00	24.0
6	330	-8541	1085	-374	0	639	-2058	15.71	15.71	9.42	9.42	2	0.07	0.01	0.09	0.00	0.00	24.0
7	330	-8663	1126	113	0	-184	-2095	15.71	15.71	9.42	9.42	2	0.06	0.01	0.09	0.00	0.00	24.0
8	330	-8533	957	-380	0	648	-2012	15.71	15.71	9.42	9.42	2	0.07	0.01	0.08	0.00	0.00	24.0
9	330	-8655	998	107	0	-175	-2049	15.71	15.71	9.42	9.42	2	0.06	0.01	0.08	0.00	0.00	24.0
10	330	-8593	1249	-197	0	340	-2125	15.71	15.71	9.42	9.42	2	0.06	0.02	0.11	0.00	0.00	24.0
11	330	-8630	1261	-50	0	93	-2136	15.71	15.71	9.42	9.42	2	0.06	0.02	0.11	0.00	0.00	24.0
12	330	-8566	822	-216	0	371	-1970	15.71	15.71	9.42	9.42	2	0.06	0.01	0.07	0.00	0.00	24.0
13	330	-8602	834	-70	0	124	-1981	15.71	15.71	9.42	9.42	2	0.05	0.01	0.07	0.00	0.00	24.0
14	330	-8541	1085	-374	0	639	-2058	15.71	15.71	9.42	9.42	2	0.07	0.01	0.09	0.00	0.00	24.0
15	330	-8663	1126	113	0	-184	-2095	15.71	15.71	9.42	9.42	2	0.06	0.01	0.09	0.00	0.00	24.0
16	330	-8533	957	-380	0	648	-2012	15.71	15.71	9.42	9.42	2	0.07	0.01	0.08	0.00	0.00	24.0
17	330	-8655	998	107	0	-175	-2049	15.71	15.71	9.42	9.42	2	0.06	0.01	0.08	0.00	0.00	24.0
18	330	-16860	2810	-297	0	543	-4196	15.71	15.71	9.42	9.42	3	0.08	0.04	0.22	0.00	0.00	24.0
19	330	-20440	2747	-356	0	616	-5125	15.71	15.71	9.42	9.42	3	0.09	0.03	0.20	0.00	0.00	24.0
20	330	-17580	2597	-100	0	147	-4387	15.71	15.71	9.42	9.42	3	0.08	0.03	0.20	0.00	0.00	24.0
37	330	-13270	2366	-226	0	425	-3244	15.71	15.71	9.42	9.42	3	0.06	0.03	0.19	0.00	0.00	24.0
38	330	-19240	2261	-325	0	548	-4792	15.71	15.71	9.42	9.42	3	0.09	0.03	0.17	0.00	0.00	24.0
39	330	-14460	2010	103	0	-235	-3563	15.71	15.71	9.42	9.42	3	0.07	0.03	0.16	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 19 NI 135 NF 137 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 29C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-14570	1322	-308	0	-490	-7061	15.71	15.71	9.42	9.42	3	0.13	0.02	0.10	0.00	0.00	24.0
2	0	-11170	1228	-315	0	-502	-6203	15.71	15.71	9.42	9.42	2	0.17	0.02	0.10	0.00	0.00	24.0
3	0	-11140	1207	-163	0	-253	-6127	15.71	15.71	9.42	9.42	2	0.16	0.02	0.10	0.00	0.00	24.0
4	0	-11280	826	-311	0	-501	-4736	15.71	15.71	9.42	9.42	2	0.13	0.01	0.07	0.00	0.00	24.0
5	0	-11240	806	-159	0	-253	-4660	15.71	15.71	9.42	9.42	2	0.12	0.01	0.07	0.00	0.00	24.0
6	0	-11260	1111	-491	0	-791	-5779	15.71	15.71	9.42	9.42	2	0.17	0.01	0.09	0.00	0.00	24.0
7	0	-11130	1043	15	0	37	-5524	15.71	15.71	9.42	9.42	2	0.14	0.01	0.09	0.00	0.00	24.0
8	0	-11290	990	-490	0	-791	-5339	15.71	15.71	9.42	9.42	2	0.15	0.01	0.08	0.00	0.00	24.0
9	0	-11160	922	16	0	37	-5084	15.71	15.71	9.42	9.42	2	0.13	0.01	0.08	0.00	0.00	24.0
10	0	-11170	1228	-315	0	-502	-6203	15.71	15.71	9.42	9.42	2	0.17	0.02	0.10	0.00	0.00	24.0
11	0	-11140	1207	-163	0	-253	-6127	15.71	15.71	9.42	9.42	2	0.16	0.02	0.10	0.00	0.00	24.0
12	0	-11280	826	-311	0	-501	-4736	15.71	15.71	9.42	9.42	2	0.13	0.01	0.07	0.00	0.00	24.0
13	0	-11240	806	-159	0	-253	-4660	15.71	15.71	9.42	9.42	2	0.12	0.01	0.07	0.00	0.00	24.0
14	0	-11260	1111	-491	0	-791	-5779	15.71	15.71	9.42	9.42	2	0.17	0.01	0.09	0.00	0.00	24.0
15	0	-11130	1043	15	0	37	-5524	15.71	15.71	9.42	9.42	2	0.14	0.01	0.09	0.00	0.00	24.0
16	0	-11290	990	-490	0	-791	-5339	15.71	15.71	9.42	9.42	2	0.15	0.01	0.08	0.00	0.00	24.0
17	0	-11160	922	16	0	37	-5084	15.71	15.71	9.42	9.42	2	0.13	0.01	0.08	0.00	0.00	24.0
18	0	-20010	3533	-612	0	-951	-14530	15.71	15.71	9.42	9.42	3	0.26	0.04	0.26	0.00	0.00	24.0
19	0	-24000	1911	-592	0	-939	-12880	15.71	15.71	9.42	9.42	3	0.23	0.02	0.14	0.00	0.00	24.0
20	0	-20780	2470	-327	0	-540	-12540	15.71	15.71	9.42	9.42	3	0.22	0.03	0.18	0.00	0.00	24.0
37	0	-16290	3616	-521	0	-804	-12920	15.71	15.71	9.42	9.42	3	0.24	0.05	0.28	0.00	0.00	24.0
38	0	-22950	912	-489	0	-785	-10160	15.71	15.71	9.42	9.42	3	0.18	0.01	0.07	0.00	0.00	24.0
39	0	-17570	1843	-46	0	-121	-9609	15.71	15.71	9.42	9.42	3	0.17	0.02	0.14	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	83	-13712	1322	-308	0	-236	-5971	15.71	15.71	9.42	9.42	3	0.11	0.02	0.10	0.00	0.00	24.0
2	83	-10511	1228	-315	0	-242	-5190	15.71	15.71	9.42	9.42	2	0.14	0.02	0.10	0.00	0.00	24.0
3	83	-10479	1207	-163	0	-119	-5131	15.71	15.71	9.42	9.42	2	0.13	0.02	0.10	0.00	0.00	24.0
4	83	-10620	826	-311	0	-244	-4055	15.71	15.71	9.42	9.42	2	0.11	0.01	0.07	0.00	0.00	24.0
5	83	-10580	806	-159	0	-121	-3995	15.71	15.71	9.42	9.42	2	0.10	0.01	0.07	0.00	0.00	24.0
6	83	-10599	1111	-491	0	-386	-4862	15.71	15.71	9.42	9.42	2	0.13	0.01	0.09	0.00	0.00	24.0
7	83	-10470	1043	15	0	24	-4664	15.71	15.71	9.42	9.42	2	0.12	0.01	0.09	0.00	0.00	24.0
8	83	-10629	990	-490	0	-387	-4522	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
9	83	-10500	922	16	0	23	-4323	15.71	15.71	9.42	9.42	2	0.11	0.01	0.08	0.00	0.00	24.0
10	83	-10511	1228	-315	0	-242	-5190	15.71	15.71	9.42	9.42	2	0.14	0.02	0.10	0.00	0.00	24.0
11	83	-10479	1207	-163	0	-119	-5131	15.71	15.71	9.42	9.42	2	0.13	0.02	0.10	0.00	0.00	24.0
12	83	-10620	826	-311	0	-244	-4055	15.71	15.71	9.42	9.42	2	0.11	0.01	0.07	0.00	0.00	24.0
13	83	-10580	806	-159	0	-121	-3995	15.71	15.71	9.42	9.42	2	0.10	0.01	0.07	0.00	0.00	24.0
14	83	-10599	1111	-491	0	-386	-4862	15.71	15.71	9.42	9.42	2	0.13	0.01	0.09	0.00	0.00	24.0
15	83	-10470	1043	15	0	24	-4664	15.71	15.71	9.42	9.42	2	0.12	0.01	0.09	0.00	0.00	24.0
16	83	-10629	990	-490	0	-387	-4522	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
17	83	-10500	922	16	0	23	-4323	15.71	15.71	9.42	9.42	2	0.11	0.01	0.08	0.00	0.00	24.0
18	83	-19152	3326	-612	0	-446	-11700	15.71	15.71	9.42	9.42	3	0.21	0.04	0.25	0.00	0.00	24.0
19	83	-23142	2118	-592	0	-450	-11217	15.71	15.71	9.42	9.42	3	0.20	0.03	0.15	0.00	0.00	24.0
20	83	-19920	2470	-327	0	-271	-10503	15.71	15.71	9.42	9.42	3	0.19	0.03	0.18	0.00	0.00	24.0
37	83	-15432	3272	-521	0	-375	-10078	15.71	15.71	9.42	9.42	3	0.18	0.04	0.25	0.00	0.00	24.0
38	83	-22090	1257	-489	0	-382	-9266	15.71	15.71	9.42	9.42	3	0.16	0.02	0.09	0.00	0.00	24.0
39	83	-16712	1843	-46	0	-83	-8088	15.71	15.71	9.42	9.42	3	0.15	0.02	0.14	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	165	-12855	1322	-308	0	18	-4880	15.71	15.71	9.42	9.42	3	0.09	0.02	0.11	0.00	0.00	24.0
2	165	-9852	1228	-315	0	18	-4178	15.71	15.71	9.42	9.42	2	0.11	0.02	0.10	0.00	0.00	24.0
3	165	-9818	1207	-163	0	16	-4135	15.71	15.71	9.42	9.42	2	0.11	0.02	0.10	0.00	0.00	24.0
4	165	-9960	826	-311	0	12	-3374	15.71	15.71	9.42	9.42	2	0.09	0.01	0.07	0.00	0.00	24.0
5	165	-9921	806	-159	0	10	-3330	15.71	15.71	9.42	9.42	2	0.09	0.01	0.07	0.00	0.00	24.0
6	165	-9938	1111	-491	0	18	-3946	15.71	15.71	9.42	9.42	2	0.10	0.01	0.09	0.00	0.00	24.0
7	165	-9810	1043	15	0	11	-3803	15.71	15.71	9.42	9.42	2	0.10	0.01	0.09	0.00	0.00	24.0
8	165	-9968	990	-490	0	17	-3705	15.71	15.71	9.42	9.42	2	0.09	0.01	0.08	0.00	0.00	24.0
9	165	-9840	922	16	0	10	-3562	15.71	15.71	9.42	9.42	2	0.09	0.01	0.08	0.00	0.00	24.0
10	165	-9852	1228	-315	0	18	-4178	15.71	15.71	9.42	9.42	2	0.11	0.02	0.10	0.00	0.00	24.0
11	165	-9818	1207	-163	0	16	-4135	15.71	15.71	9.42	9.42	2	0.11	0.02	0.10	0.00	0.00	24.0
12	165	-9960	826	-311	0	12	-3374	15.71	15.71	9.42	9.42	2	0.09	0.01	0.07	0.00	0.00	24.0
13	165	-9921	806	-159	0	10	-3330	15.71	15.71	9.42	9.42	2	0.09	0.01	0.07	0.00	0.00	24.0
14	165	-9938	1111	-491	0	18	-3946	15.71	15.71	9.42	9.42	2	0.10	0.01	0.09	0.00	0.00	24.0
15	165	-9810	1043	15	0	11	-3803	15.71	15.71	9.42	9.42	2	0.10	0.01	0.09	0.00	0.00	24.0
16	165	-9968	990	-490	0	17	-3705	15.71	15.71	9.42	9.42	2	0.09	0.01	0.08	0.00	0.00	24.0
17	165	-9840	922	16	0	10	-3562	15.71	15.71	9.42	9.42	2	0.09	0.01	0.08	0.00	0.00	24.0
18	165	-18295	3120	-612	0	59	-9040	15.71	15.71	9.42	9.42	3	0.16	0.04	0.24	0.00	0.00	24.0
19	165	-22285	2324	-592	0	39	-9384	15.71	15.71	9.42	9.42	3	0.16	0.03	0.17	0.00	0.00	24.0
20	165	-19060	2470	-327	0	-2	-8467	15.71	15.71	9.42	9.42	3	0.15	0.03	0.19	0.00	0.00	24.0
37	165	-14575	2928	-521	0	55	-7520	15.71	15.71	9.42	9.42	3	0.14	0.04	0.23	0.00	0.00	24.0
38	165	-21230	1601	-489	0	22	-8088	15.71	15.71	9.42	9.42	3	0.14	0.02	0.12	0.00	0.00	24.0
39	165	-15855	1843	-46	0	-45	-6568	15.71	15.71	9.42	9.42	3	0.12	0.02	0.14	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	248	-11998	1322	-308	0	273	-3790	15.71	15.71	9.42	9.42	3	0.07	0.02	0.11	0.00	0.00	24.0
2	248	-9193	1228	-315	0	278	-3165	15.71	15.71	9.42	9.42	2	0.09	0.02	0.10	0.00	0.00	24.0
3	248	-9157	1207	-163	0	150	-3139	15.71	15.71	9.42	9.42	2	0.08	0.02	0.10	0.00	0.00	24.0
4	248	-9300	826	-311	0	269	-2692	15.71	15.71	9.42	9.42	2	0.08	0.01	0.07	0.00	0.00	24.0
5	248	-9262	806	-159	0	142	-2666	15.71	15.71	9.42	9.42	2	0.07	0.01	0.07	0.00	0.00	24.0
6	248	-9276	1111	-491	0	423	-3030	15.71	15.71	9.42	9.42	2	0.09	0.01	0.09	0.00	0.00	24.0
7	248	-9149	1043	15	0	-1	-2943	15.71	15.71	9.42	9.42	2	0.08	0.01	0.09	0.00	0.00	24.0
8	248	-9308	990	-490	0	421	-2888	15.71	15.71	9.42	9.42	2	0.08	0.01	0.08	0.00	0.00	24.0
9	248	-9181	922	16	0	-4	-2801	15.71	15.71	9.42	9.42	2	0.07	0.01	0.08	0.00	0.00	24.0
10	248	-9193	1228	-315	0	278	-3165	15.71	15.71	9.42	9.42	2	0.09	0.02	0.10	0.00	0.00	24.0
11	248	-9157	1207	-163	0	150	-3139	15.71	15.71	9.42	9.42	2	0.08	0.02	0.10	0.00	0.00	24.0
12	248	-9300	826	-311	0	269	-2692	15.71	15.71	9.42	9.42	2	0.08	0.01	0.07	0.00	0.00	24.0
13	248	-9262	806	-159	0	142	-2666	15.71	15.71	9.42	9.42	2	0.07	0.01	0.07	0.00	0.00	24.0
14	248	-9276	1111	-491	0	423	-3030	15.71	15.71	9.42	9.42	2	0.09	0.01	0.09	0.00	0.00	24.0
15	248	-9149	1043	15	0	-1	-2943	15.71	15.71	9.42	9.42	2	0.08	0.01	0.09	0.00	0.00	24.0
16	248	-9308	990	-490	0	421	-2888	15.71	15.71	9.42	9.42	2	0.08	0.01	0.08	0.00	0.00	24.0
17	248	-9181	922	16	0	-4	-2801	15.71	15.71	9.42	9.42	2	0.07	0.01	0.08	0.00	0.00	24.0
18	248	-17438	2914	-612	0	563	-6551	15.71	15.71	9.42	9.42	3	0.12	0.04	0.22	0.00	0.00	24.0
19	248	-21428	2530	-592	0	527	-7380	15.71	15.71	9.42	9.42	3	0.13	0.03	0.18	0.00	0.00	24.0
20	248	-18200	2470	-327	0	268	-6430	15.71	15.71	9.42	9.42	3	0.12	0.03	0.19	0.00	0.00	24.0
37	248	-13718	2584	-521	0	485	-5246	15.71	15.71	9.42	9.42	3	0.10	0.03	0.21	0.00	0.00	24.0
38	248	-20370	1945	-489	0	425	-6626	15.71	15.71	9.42	9.42	3	0.12	0.02	0.14	0.00	0.00	24.0
39	248	-14998	1843	-46	0	-7	-5047	15.71	15.71	9.42	9.42	3	0.09	0.02	0.14	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	330	-11140	1322	-308	0	527	-2700	15.71	15.71	9.42	9.42	3	0.05	0.02	0.11	0.00	0.00	24.0
2	330	-8534	1228	-315	0	537	-2152	15.71	15.71	9.42	9.42	2	0.07	0.02	0.10	0.00	0.00	24.0
3	330	-8496	1207	-163	0	285	-2143	15.71	15.71	9.42	9.42	2	0.06	0.02	0.10	0.00	0.00	24.0
4	330	-8640	826	-311	0	526	-2011	15.71	15.71	9.42	9.42	2	0.07	0.01	0.07	0.00	0.00	24.0
5	330	-8602	806	-159	0	273	-2001	15.71	15.71	9.42	9.42	2	0.06	0.01	0.07	0.00	0.00	24.0
6	330	-8615	1111	-491	0	828	-2113	15.71	15.71	9.42	9.42	2	0.08	0.01	0.09	0.00	0.00	24.0
7	330	-8489	1043	15	0	-14	-2082	15.71	15.71	9.42	9.42	2	0.05	0.01	0.09	0.00	0.00	24.0
8	330	-8647	990	-490	0	825	-2071	15.71	15.71	9.42	9.42	2	0.08	0.01	0.08	0.00	0.00	24.0
9	330	-8521	922	16	0	-17	-2040	15.71	15.71	9.42	9.42	2	0.05	0.01	0.08	0.00	0.00	24.0
10	330	-8534	1228	-315	0	537	-2152	15.71	15.71	9.42	9.42	2	0.07	0.02	0.10	0.00	0.00	24.0
11	330	-8496	1207	-163	0	285	-2143	15.71	15.71	9.42	9.42	2	0.06	0.02	0.10	0.00	0.00	24.0
12	330	-8640	826	-311	0	526	-2011	15.71	15.71	9.42	9.42	2	0.07	0.01	0.07	0.00	0.00	24.0
13	330	-8602	806	-159	0	273	-2001	15.71	15.71	9.42	9.42	2	0.06	0.01	0.07	0.00	0.00	24.0
14	330	-8615	1111	-491	0	828	-2113	15.71	15.71	9.42	9.42	2	0.08	0.01	0.09	0.00	0.00	24.0
15	330	-8489	1043	15	0	-14	-2082	15.71	15.71	9.42	9.42	2	0.05	0.01	0.09	0.00	0.00	24.0
16	330	-8647	990	-490	0	825	-2071	15.71	15.71	9.42	9.42	2	0.08	0.01	0.08	0.00	0.00	24.0
17	330	-8521	922	16	0	-17	-2040	15.71	15.71	9.42	9.42	2	0.05	0.01	0.08	0.00	0.00	24.0
18	330	-16580	2707	-612	0	1068	-4232	15.71	15.71	9.42	9.42	3	0.09	0.03	0.21	0.00	0.00	24.0
19	330	-20570	2737	-592	0	1016	-5206	15.71	15.71	9.42	9.42	3	0.10	0.03	0.20	0.00	0.00	24.0
20	330	-17340	2470	-327	0	537	-4394	15.71	15.71	9.42	9.42	3	0.08	0.03	0.19	0.00	0.00	24.0
37	330	-12860	2240	-521	0	915	-3256	15.71	15.71	9.42	9.42	3	0.07	0.03	0.18	0.00	0.00	24.0
38	330	-19510	2289	-489	0	828	-4880	15.71	15.71	9.42	9.42	3	0.09	0.03	0.17	0.00	0.00	24.0
39	330	-14140	1843	-46	0	31	-3526	15.71	15.71	9.42	9.42	3	0.06	0.02	0.15	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 20 NI 178 NF 180 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 28C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-14360	1241	-350	0	-546	-6781	15.71	15.71	9.42	9.42	3	0.13	0.02	0.10	0.00	0.00	24.0
2	0	-11030	1170	-348	0	-551	-6026	15.71	15.71	9.42	9.42	2	0.17	0.01	0.10	0.00	0.00	24.0
3	0	-11030	1169	-183	0	-281	-6026	15.71	15.71	9.42	9.42	2	0.16	0.01	0.10	0.00	0.00	24.0
4	0	-11060	740	-354	0	-559	-4407	15.71	15.71	9.42	9.42	2	0.13	0.01	0.06	0.00	0.00	24.0
5	0	-11060	740	-190	0	-289	-4407	15.71	15.71	9.42	9.42	2	0.12	0.01	0.06	0.00	0.00	24.0
6	0	-11030	1021	-543	0	-869	-5460	15.71	15.71	9.42	9.42	2	0.16	0.01	0.08	0.00	0.00	24.0
7	0	-11050	1018	7	0	32	-5459	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
8	0	-11040	892	-545	0	-872	-4974	15.71	15.71	9.42	9.42	2	0.15	0.01	0.07	0.00	0.00	24.0
9	0	-11060	889	5	0	30	-4973	15.71	15.71	9.42	9.42	2	0.13	0.01	0.07	0.00	0.00	24.0
10	0	-11030	1170	-348	0	-551	-6026	15.71	15.71	9.42	9.42	2	0.17	0.01	0.10	0.00	0.00	24.0
11	0	-11030	1169	-183	0	-281	-6026	15.71	15.71	9.42	9.42	2	0.16	0.01	0.10	0.00	0.00	24.0
12	0	-11060	740	-354	0	-559	-4407	15.71	15.71	9.42	9.42	2	0.13	0.01	0.06	0.00	0.00	24.0
13	0	-11060	740	-190	0	-289	-4407	15.71	15.71	9.42	9.42	2	0.12	0.01	0.06	0.00	0.00	24.0
14	0	-11030	1021	-543	0	-869	-5460	15.71	15.71	9.42	9.42	2	0.16	0.01	0.08	0.00	0.00	24.0
15	0	-11050	1018	7	0	32	-5459	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
16	0	-11040	892	-545	0	-872	-4974	15.71	15.71	9.42	9.42	2	0.15	0.01	0.07	0.00	0.00	24.0
17	0	-11060	889	5	0	30	-4973	15.71	15.71	9.42	9.42	2	0.13	0.01	0.07	0.00	0.00	24.0
18	0	-19770	3445	-707	0	-1150	-14340	15.71	15.71	9.42	9.42	3	0.26	0.04	0.26	0.00	0.00	24.0
19	0	-23600	1738	-719	0	-1156	-12210	15.71	15.71	9.42	9.42	3	0.22	0.02	0.12	0.00	0.00	24.0
20	0	-20570	2389	-390	0	-661	-12300	15.71	15.71	9.42	9.42	3	0.22	0.03	0.18	0.00	0.00	24.0
37	0	-16140	3573	-584	0	-949	-12930	15.71	15.71	9.42	9.42	3	0.24	0.05	0.28	0.00	0.00	24.0
38	0	-22520	728	-604	0	-958	-9385	15.71	15.71	9.42	9.42	3	0.17	0.01	0.05	0.00	0.00	24.0
39	0	-17480	1812	-56	0	-134	-9543	15.71	15.71	9.42	9.42	3	0.17	0.02	0.14	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	83	-13502	1241	-350	0	-257	-5757	15.71	15.71	9.42	9.42	3	0.11	0.02	0.10	0.00	0.00	24.0
2	83	-10369	1170	-348	0	-264	-5060	15.71	15.71	9.42	9.42	2	0.13	0.01	0.10	0.00	0.00	24.0
3	83	-10370	1169	-183	0	-130	-5061	15.71	15.71	9.42	9.42	2	0.13	0.01	0.10	0.00	0.00	24.0
4	83	-10400	740	-354	0	-266	-3796	15.71	15.71	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
5	83	-10401	740	-190	0	-132	-3797	15.71	15.71	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
6	83	-10371	1021	-543	0	-421	-4618	15.71	15.71	9.42	9.42	2	0.13	0.01	0.08	0.00	0.00	24.0
7	83	-10390	1018	7	0	26	-4619	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
8	83	-10381	892	-545	0	-422	-4238	15.71	15.71	9.42	9.42	2	0.12	0.01	0.07	0.00	0.00	24.0
9	83	-10399	889	5	0	25	-4240	15.71	15.71	9.42	9.42	2	0.11	0.01	0.07	0.00	0.00	24.0
10	83	-10369	1170	-348	0	-264	-5060	15.71	15.71	9.42	9.42	2	0.13	0.01	0.10	0.00	0.00	24.0
11	83	-10370	1169	-183	0	-130	-5061	15.71	15.71	9.42	9.42	2	0.13	0.01	0.10	0.00	0.00	24.0
12	83	-10400	740	-354	0	-266	-3796	15.71	15.71	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
13	83	-10401	740	-190	0	-132	-3797	15.71	15.71	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
14	83	-10371	1021	-543	0	-421	-4618	15.71	15.71	9.42	9.42	2	0.13	0.01	0.08	0.00	0.00	24.0
15	83	-10390	1018	7	0	26	-4619	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
16	83	-10381	892	-545	0	-422	-4238	15.71	15.71	9.42	9.42	2	0.12	0.01	0.07	0.00	0.00	24.0
17	83	-10399	889	5	0	25	-4240	15.71	15.71	9.42	9.42	2	0.11	0.01	0.07	0.00	0.00	24.0
18	83	-18912	3239	-707	0	-567	-11582	15.71	15.71	9.42	9.42	3	0.21	0.04	0.24	0.00	0.00	24.0
19	83	-22740	1944	-719	0	-563	-10690	15.71	15.71	9.42	9.42	3	0.19	0.02	0.14	0.00	0.00	24.0
20	83	-19712	2389	-390	0	-339	-10330	15.71	15.71	9.42	9.42	3	0.18	0.03	0.18	0.00	0.00	24.0
37	83	-15282	3229	-584	0	-467	-10125	15.71	15.71	9.42	9.42	3	0.18	0.04	0.25	0.00	0.00	24.0

38	83	-21662	1072	-604	0	-460	-8642	15.71	15.71	9.42	9.42	3	0.15	0.01	0.08	0.00	0.00	24.0
39	83	-16622	1812	-56	0	-88	-8048	15.71	15.71	9.42	9.42	3	0.14	0.02	0.14	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	165	-12645	1241	-350	0	31	-4733	15.71	15.71	9.42	9.42	3	0.09	0.02	0.10	0.00	0.00	24.0
2	165	-9708	1170	-348	0	23	-4095	15.71	15.71	9.42	9.42	2	0.10	0.01	0.10	0.00	0.00	24.0
3	165	-9711	1169	-183	0	21	-4096	15.71	15.71	9.42	9.42	2	0.10	0.01	0.10	0.00	0.00	24.0
4	165	-9740	740	-354	0	26	-3186	15.71	15.71	9.42	9.42	2	0.08	0.01	0.06	0.00	0.00	24.0
5	165	-9742	740	-190	0	24	-3187	15.71	15.71	9.42	9.42	2	0.08	0.01	0.06	0.00	0.00	24.0
6	165	-9712	1021	-543	0	26	-3776	15.71	15.71	9.42	9.42	2	0.10	0.01	0.08	0.00	0.00	24.0
7	165	-9729	1018	7	0	20	-3780	15.71	15.71	9.42	9.42	2	0.10	0.01	0.08	0.00	0.00	24.0
8	165	-9722	892	-545	0	27	-3502	15.71	15.71	9.42	9.42	2	0.09	0.01	0.07	0.00	0.00	24.0
9	165	-9738	889	5	0	21	-3507	15.71	15.71	9.42	9.42	2	0.09	0.01	0.07	0.00	0.00	24.0
10	165	-9708	1170	-348	0	23	-4095	15.71	15.71	9.42	9.42	2	0.10	0.01	0.10	0.00	0.00	24.0
11	165	-9711	1169	-183	0	21	-4096	15.71	15.71	9.42	9.42	2	0.10	0.01	0.10	0.00	0.00	24.0
12	165	-9740	740	-354	0	26	-3186	15.71	15.71	9.42	9.42	2	0.08	0.01	0.06	0.00	0.00	24.0
13	165	-9742	740	-190	0	24	-3187	15.71	15.71	9.42	9.42	2	0.08	0.01	0.06	0.00	0.00	24.0
14	165	-9712	1021	-543	0	26	-3776	15.71	15.71	9.42	9.42	2	0.10	0.01	0.08	0.00	0.00	24.0
15	165	-9729	1018	7	0	20	-3780	15.71	15.71	9.42	9.42	2	0.10	0.01	0.08	0.00	0.00	24.0
16	165	-9722	892	-545	0	27	-3502	15.71	15.71	9.42	9.42	2	0.09	0.01	0.07	0.00	0.00	24.0
17	165	-9738	889	5	0	21	-3507	15.71	15.71	9.42	9.42	2	0.09	0.01	0.07	0.00	0.00	24.0
18	165	-18055	3032	-707	0	16	-8994	15.71	15.71	9.42	9.42	3	0.16	0.04	0.23	0.00	0.00	24.0
19	165	-21880	2151	-719	0	31	-9000	15.71	15.71	9.42	9.42	3	0.16	0.03	0.16	0.00	0.00	24.0
20	165	-18855	2389	-390	0	-17	-8360	15.71	15.71	9.42	9.42	3	0.15	0.03	0.18	0.00	0.00	24.0
37	165	-14425	2885	-584	0	14	-7604	15.71	15.71	9.42	9.42	3	0.14	0.04	0.23	0.00	0.00	24.0
38	165	-20805	1416	-604	0	38	-7616	15.71	15.71	9.42	9.42	3	0.13	0.02	0.10	0.00	0.00	24.0
39	165	-15765	1812	-56	0	-42	-6553	15.71	15.71	9.42	9.42	3	0.12	0.02	0.14	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	248	-11788	1241	-350	0	319	-3709	15.71	15.71	9.42	9.42	3	0.07	0.02	0.10	0.00	0.00	24.0
2	248	-9048	1170	-348	0	311	-3129	15.71	15.71	9.42	9.42	2	0.09	0.02	0.10	0.00	0.00	24.0
3	248	-9052	1169	-183	0	173	-3132	15.71	15.71	9.42	9.42	2	0.08	0.01	0.10	0.00	0.00	24.0
4	248	-9079	740	-354	0	319	-2575	15.71	15.71	9.42	9.42	2	0.07	0.01	0.06	0.00	0.00	24.0
5	248	-9082	740	-190	0	181	-2577	15.71	15.71	9.42	9.42	2	0.07	0.01	0.06	0.00	0.00	24.0
6	248	-9052	1021	-543	0	474	-2933	15.71	15.71	9.42	9.42	2	0.09	0.01	0.09	0.00	0.00	24.0
7	248	-9068	1018	7	0	14	-2940	15.71	15.71	9.42	9.42	2	0.08	0.01	0.09	0.00	0.00	24.0
8	248	-9062	892	-545	0	477	-2767	15.71	15.71	9.42	9.42	2	0.08	0.01	0.07	0.00	0.00	24.0
9	248	-9078	889	5	0	17	-2773	15.71	15.71	9.42	9.42	2	0.07	0.01	0.07	0.00	0.00	24.0
10	248	-9048	1170	-348	0	311	-3129	15.71	15.71	9.42	9.42	2	0.09	0.02	0.10	0.00	0.00	24.0
11	248	-9052	1169	-183	0	173	-3132	15.71	15.71	9.42	9.42	2	0.08	0.01	0.10	0.00	0.00	24.0
12	248	-9079	740	-354	0	319	-2575	15.71	15.71	9.42	9.42	2	0.07	0.01	0.06	0.00	0.00	24.0
13	248	-9082	740	-190	0	181	-2577	15.71	15.71	9.42	9.42	2	0.07	0.01	0.06	0.00	0.00	24.0
14	248	-9052	1021	-543	0	474	-2933	15.71	15.71	9.42	9.42	2	0.09	0.01	0.09	0.00	0.00	24.0
15	248	-9068	1018	7	0	14	-2940	15.71	15.71	9.42	9.42	2	0.08	0.01	0.09	0.00	0.00	24.0
16	248	-9062	892	-545	0	477	-2767	15.71	15.71	9.42	9.42	2	0.08	0.01	0.07	0.00	0.00	24.0
17	248	-9078	889	5	0	17	-2773	15.71	15.71	9.42	9.42	2	0.07	0.01	0.07	0.00	0.00	24.0
18	248	-17198	2826	-707	0	600	-6577	15.71	15.71	9.42	9.42	3	0.12	0.04	0.22	0.00	0.00	24.0
19	248	-21020	2358	-719	0	624	-7140	15.71	15.71	9.42	9.42	3	0.13	0.03	0.17	0.00	0.00	24.0
20	248	-17998	2389	-390	0	305	-6390	15.71	15.71	9.42	9.42	3	0.12	0.03	0.18	0.00	0.00	24.0
37	248	-13568	2541	-584	0	496	-5367	15.71	15.71	9.42	9.42	3	0.10	0.03	0.20	0.00	0.00	24.0
38	248	-19948	1760	-604	0	536	-6306	15.71	15.71	9.42	9.42	3	0.11	0.02	0.13	0.00	0.00	24.0
39	248	-14908	1812	-56	0	4	-5058	15.71	15.71	9.42	9.42	3	0.09	0.02	0.14	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	330	-10930	1241	-350	0	608	-2685	15.71	15.71	9.42	9.42	3	0.06	0.02	0.10	0.00	0.00	24.0
2	330	-8387	1170	-348	0	598	-2164	15.71	15.71	9.42	9.42	2	0.07	0.02	0.10	0.00	0.00	24.0
3	330	-8392	1169	-183	0	324	-2167	15.71	15.71	9.42	9.42	2	0.06	0.02	0.10	0.00	0.00	24.0
4	330	-8419	740	-354	0	611	-1964	15.71	15.71	9.42	9.42	2	0.07	0.01	0.06	0.00	0.00	24.0
5	330	-8423	740	-190	0	337	-1967	15.71	15.71	9.42	9.42	2	0.06	0.01	0.06	0.00	0.00	24.0
6	330	-8393	1021	-543	0	922	-2091	15.71	15.71	9.42	9.42	2	0.08	0.01	0.09	0.00	0.00	24.0
7	330	-8408	1018	7	0	9	-2100	15.71	15.71	9.42	9.42	2	0.05	0.01	0.09	0.00	0.00	24.0
8	330	-8403	892	-545	0	926	-2031	15.71	15.71	9.42	9.42	2	0.08	0.01	0.08	0.00	0.00	24.0
9	330	-8417	889	5	0	13	-2040	15.71	15.71	9.42	9.42	2	0.05	0.01	0.07	0.00	0.00	24.0
10	330	-8387	1170	-348	0	598	-2164	15.71	15.71	9.42	9.42	2	0.07	0.02	0.10	0.00	0.00	24.0
11	330	-8392	1169	-183	0	324	-2167	15.71	15.71	9.42	9.42	2	0.06	0.02	0.10	0.00	0.00	24.0
12	330	-8419	740	-354	0	611	-1964	15.71	15.71	9.42	9.42	2	0.07	0.01	0.06	0.00	0.00	24.0
13	330	-8423	740	-190	0	337	-1967	15.71	15.71	9.42	9.42	2	0.06	0.01	0.06	0.00	0.00	24.0
14	330	-8393	1021	-543	0	922	-2091	15.71	15.71	9.42	9.42	2	0.08	0.01	0.09	0.00	0.00	24.0
15	330	-8408	1018	7	0	9	-2100	15.71	15.71	9.42	9.42	2	0.05	0.01	0.09	0.00	0.00	24.0
16	330	-8403	892	-545	0	926	-2031	15.71	15.71	9.42	9.42	2	0.08	0.01	0.08	0.00	0.00	24.0
17	330	-8417	889	5	0	13	-2040	15.71	15.71	9.42	9.42	2	0.05	0.01	0.07	0.00	0.00	24.0
18	330	-16340	2620	-707	0	1183	-4330	15.71	15.71	9.42	9.42	3	0.09	0.03	0.20	0.00	0.00	24.0
19	330	-20160	2564	-719	0	1217	-5109	15.71	15.71	9.42	9.42	3	0.10	0.03	0.19	0.00	0.00	24.0
20	330	-17140	2389	-390	0	627	-4420	15.71	15.71	9.42	9.42	3	0.08	0.03	0.18	0.00	0.00	24.0
37	330	-12710	2197	-584	0	977	-3414	15.71	15.71	9.42	9.42	3	0.07	0.03	0.18	0.00	0.00	24.0
38	330	-19090	2104	-604	0	1034	-4712	15.71	15.71	9.42	9.42	3	0.09	0.03	0.16	0.00	0.00	24.0
39	330	-14050	1812	-56	0	50	-3563	15.71	15.71	9.42	9.42	3	0.06	0.02	0.14	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 21 NI 221 NF 223 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 27C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-13240	1663	-1012	0	-2027	-8053	15.71	15.71	9.42	9.42	3	0.17	0.02	0.13	0.00	0.00	24.0
2	0	-10110	1614	-905	0	-1787	-7420	15.71	15.71	9.42	9.42	2	0.24	0.02	0.13	0.00	0.00	24.0
3	0	-10180	1648	-724	0	-1476	-7549	15.71	15.71	9.42	9.42	2	0.23	0.02	0.14	0.00	0.00	24.0
4	0	-10190	910	-833	0	-1643	-4839	15.71	15.71	9.42	9.42	2	0.17	0.01	0.08	0.00	0.00	24.0
5	0	-10260	945	-652	0	-1332	-4969	15.71	15.71	9.42	9.42	2	0.16	0.01	0.08	0.00	0.00	24.0
6	0	-10060	1328	-1091	0	-2099	-6366	15.71	15.71	9.42	9.42	2	0.22	0.02	0.11	0.00	0.00	24.0
7	0	-10290	1442	-488	0	-1063	-6797	15.71	15.71	9.42	9.42	2	0.20	0.02	0.12	0.00	0.00	24.0
8	0	-10090	1117	-1070	0	-2056	-5592	15.71	15.71	9.42	9.42	2	0.20	0.01	0.09	0.00	0.00	24.0
9	0	-10310	1231	-466	0	-1020	-6023	15.71	15.71	9.42	9.42	2	0.18	0.02	0.10	0.00	0.00	24.0
10	0	-10110	1614	-905	0	-1787	-7420	15.71	15.71	9.42	9.42	2	0.24	0.02	0.13	0.00	0.00	24.0
11	0	-10180	1648	-724	0	-1476	-7549	15.71	15.71	9.42	9.42	2	0.23	0.02	0.14	0.00	0.00	24.0
12	0	-10190	910	-833	0	-1643	-4839	15.71	15.71	9.42	9.42	2	0.17	0.01	0.08	0.00	0.00	24.0
13	0	-10260	945	-652	0	-1332	-4969	15.71	15.71	9.42	9.42	2	0.16	0.01	0.08	0.00	0.00	24.0
14	0	-10060	1328	-1091	0	-2099	-6366	15.71	15.71	9.42	9.42	2	0.22	0.02	0.11	0.00	0.00	24.0
15	0	-10290	1442	-488	0	-1063	-6797	15.71	15.71	9.42	9.42	2	0.20	0.02	0.12	0.00	0.00	24.0
16	0	-10090	1117	-1070	0	-2056	-5592	15.71	15.71	9.42	9.42	2	0.20	0.01	0.09	0.00	0.00	24.0
17	0	-10310	1231	-466	0	-1020	-6023	15.71	15.71	9.42	9.42	2	0.18	0.02	0.10	0.00	0.00	24.0

18	0	-17290	4822	-1991	0	-3679	-18810	15.71	15.71	9.42	9.42	3	0.37	0.06	0.37	0.00	0.00	24.0
19	0	-21500	2026	-1909	0	-3344	-12820	15.71	15.71	9.42	9.42	3	0.26	0.03	0.15	0.00	0.00	24.0
20	0	-18640	3261	-1510	0	-2784	-15040	15.71	15.71	9.42	9.42	3	0.29	0.04	0.25	0.00	0.00	24.0
37	0	-13920	5177	-1712	0	-3305	-18270	15.71	15.71	9.42	9.42	3	0.36	0.07	0.41	0.00	0.00	24.0
38	0	-20930	517	-1575	0	-2747	-8292	15.71	15.71	9.42	9.42	3	0.18	0.02	0.09	0.00	0.00	24.0
39	0	-16160	2575	-911	0	-1814	-11980	15.71	15.71	9.42	9.42	3	0.23	0.03	0.20	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	83	-12383	1663	-1012	0	-1192	-6681	15.71	15.71	9.42	9.42	3	0.13	0.02	0.13	0.00	0.00	24.0
2	83	-9451	1614	-905	0	-1040	-6088	15.71	15.71	9.42	9.42	2	0.18	0.02	0.13	0.00	0.00	24.0
3	83	-9520	1648	-724	0	-879	-6190	15.71	15.71	9.42	9.42	2	0.18	0.02	0.14	0.00	0.00	24.0
4	83	-9531	910	-833	0	-956	-4088	15.71	15.71	9.42	9.42	2	0.13	0.01	0.08	0.00	0.00	24.0
5	83	-9600	945	-652	0	-794	-4190	15.71	15.71	9.42	9.42	2	0.13	0.01	0.08	0.00	0.00	24.0
6	83	-9401	1328	-1091	0	-1199	-5270	15.71	15.71	9.42	9.42	2	0.17	0.02	0.11	0.00	0.00	24.0
7	83	-9629	1442	-488	0	-661	-5608	15.71	15.71	9.42	9.42	2	0.16	0.02	0.12	0.00	0.00	24.0
8	83	-9430	1117	-1070	0	-1174	-4670	15.71	15.71	9.42	9.42	2	0.15	0.01	0.09	0.00	0.00	24.0
9	83	-9650	1231	-466	0	-636	-5008	15.71	15.71	9.42	9.42	2	0.14	0.02	0.10	0.00	0.00	24.0
10	83	-9451	1614	-905	0	-1040	-6088	15.71	15.71	9.42	9.42	2	0.18	0.02	0.13	0.00	0.00	24.0
11	83	-9520	1648	-724	0	-879	-6190	15.71	15.71	9.42	9.42	2	0.18	0.02	0.14	0.00	0.00	24.0
12	83	-9531	910	-833	0	-956	-4088	15.71	15.71	9.42	9.42	2	0.13	0.01	0.08	0.00	0.00	24.0
13	83	-9600	945	-652	0	-794	-4190	15.71	15.71	9.42	9.42	2	0.13	0.01	0.08	0.00	0.00	24.0
14	83	-9401	1328	-1091	0	-1199	-5270	15.71	15.71	9.42	9.42	2	0.17	0.02	0.11	0.00	0.00	24.0
15	83	-9629	1442	-488	0	-661	-5608	15.71	15.71	9.42	9.42	2	0.16	0.02	0.12	0.00	0.00	24.0
16	83	-9430	1117	-1070	0	-1174	-4670	15.71	15.71	9.42	9.42	2	0.15	0.01	0.09	0.00	0.00	24.0
17	83	-9650	1231	-466	0	-636	-5008	15.71	15.71	9.42	9.42	2	0.14	0.02	0.10	0.00	0.00	24.0
18	83	-16432	4616	-1991	0	-2036	-14917	15.71	15.71	9.42	9.42	3	0.28	0.06	0.36	0.00	0.00	24.0
19	83	-20642	2232	-1909	0	-1769	-11064	15.71	15.71	9.42	9.42	3	0.21	0.03	0.16	0.00	0.00	24.0
20	83	-17782	3261	-1510	0	-1538	-12349	15.71	15.71	9.42	9.42	3	0.23	0.04	0.25	0.00	0.00	24.0
37	83	-13062	4833	-1712	0	-1892	-14140	15.71	15.71	9.42	9.42	3	0.27	0.06	0.39	0.00	0.00	24.0
38	83	-20072	861	-1575	0	-1448	-7723	15.71	15.71	9.42	9.42	3	0.15	0.02	0.09	0.00	0.00	24.0
39	83	-15302	2575	-911	0	-1062	-9856	15.71	15.71	9.42	9.42	3	0.19	0.03	0.20	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	165	-11526	1663	-1012	0	-357	-5309	15.71	15.71	9.42	9.42	3	0.10	0.02	0.14	0.00	0.00	24.0
2	165	-8792	1614	-905	0	-293	-4757	15.71	15.71	9.42	9.42	2	0.13	0.02	0.14	0.00	0.00	24.0
3	165	-8861	1648	-724	0	-281	-4830	15.71	15.71	9.42	9.42	2	0.13	0.02	0.14	0.00	0.00	24.0
4	165	-8872	910	-833	0	-268	-3337	15.71	15.71	9.42	9.42	2	0.09	0.01	0.08	0.00	0.00	24.0
5	165	-8940	945	-652	0	-256	-3410	15.71	15.71	9.42	9.42	2	0.09	0.01	0.08	0.00	0.00	24.0
6	165	-8742	1328	-1091	0	-298	-4175	15.71	15.71	9.42	9.42	2	0.11	0.02	0.11	0.00	0.00	24.0
7	165	-8968	1442	-488	0	-259	-4418	15.71	15.71	9.42	9.42	2	0.12	0.02	0.12	0.00	0.00	24.0
8	165	-8769	1117	-1070	0	-291	-3749	15.71	15.71	9.42	9.42	2	0.10	0.01	0.09	0.00	0.00	24.0
9	165	-8990	1231	-466	0	-251	-3992	15.71	15.71	9.42	9.42	2	0.11	0.02	0.10	0.00	0.00	24.0
10	165	-8792	1614	-905	0	-293	-4757	15.71	15.71	9.42	9.42	2	0.13	0.02	0.14	0.00	0.00	24.0
11	165	-8861	1648	-724	0	-281	-4830	15.71	15.71	9.42	9.42	2	0.13	0.02	0.14	0.00	0.00	24.0
12	165	-8872	910	-833	0	-268	-3337	15.71	15.71	9.42	9.42	2	0.09	0.01	0.08	0.00	0.00	24.0
13	165	-8940	945	-652	0	-256	-3410	15.71	15.71	9.42	9.42	2	0.09	0.01	0.08	0.00	0.00	24.0
14	165	-8742	1328	-1091	0	-298	-4175	15.71	15.71	9.42	9.42	2	0.11	0.02	0.11	0.00	0.00	24.0
15	165	-8968	1442	-488	0	-259	-4418	15.71	15.71	9.42	9.42	2	0.12	0.02	0.12	0.00	0.00	24.0
16	165	-8769	1117	-1070	0	-291	-3749	15.71	15.71	9.42	9.42	2	0.10	0.01	0.09	0.00	0.00	24.0
17	165	-8990	1231	-466	0	-251	-3992	15.71	15.71	9.42	9.42	2	0.11	0.02	0.10	0.00	0.00	24.0
18	165	-15575	4409	-1991	0	-394	-11193	15.71	15.71	9.42	9.42	3	0.20	0.06	0.34	0.00	0.00	24.0
19	165	-19785	2438	-1909	0	-195	-9138	15.71	15.71	9.42	9.42	3	0.16	0.03	0.18	0.00	0.00	24.0
20	165	-16925	3261	-1510	0	-292	-9658	15.71	15.71	9.42	9.42	3	0.17	0.04	0.25	0.00	0.00	24.0
37	165	-12205	4489	-1712	0	-479	-10294	15.71	15.71	9.42	9.42	3	0.19	0.06	0.36	0.00	0.00	24.0
38	165	-19215	1205	-1575	0	-149	-6871	15.71	15.71	9.42	9.42	3	0.12	0.02	0.09	0.00	0.00	24.0
39	165	-14445	2575	-911	0	-310	-7733	15.71	15.71	9.42	9.42	3	0.14	0.03	0.20	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	248	-10669	1663	-1012	0	478	-3937	15.71	15.71	9.42	9.42	3	0.08	0.02	0.14	0.00	0.00	24.0
2	248	-8134	1614	-905	0	453	-3426	15.71	15.71	9.42	9.42	2	0.10	0.02	0.14	0.00	0.00	24.0
3	248	-8202	1648	-724	0	316	-3471	15.71	15.71	9.42	9.42	2	0.10	0.02	0.14	0.00	0.00	24.0
4	248	-8213	910	-833	0	419	-2586	15.71	15.71	9.42	9.42	2	0.08	0.01	0.08	0.00	0.00	24.0
5	248	-8281	945	-652	0	281	-2631	15.71	15.71	9.42	9.42	2	0.07	0.01	0.08	0.00	0.00	24.0
6	248	-8083	1328	-1091	0	602	-3080	15.71	15.71	9.42	9.42	2	0.10	0.02	0.11	0.00	0.00	24.0
7	248	-8308	1442	-488	0	143	-3228	15.71	15.71	9.42	9.42	2	0.09	0.02	0.12	0.00	0.00	24.0
8	248	-8108	1117	-1070	0	592	-2828	15.71	15.71	9.42	9.42	2	0.09	0.01	0.09	0.00	0.00	24.0
9	248	-8331	1231	-466	0	133	-2976	15.71	15.71	9.42	9.42	2	0.08	0.02	0.10	0.00	0.00	24.0
10	248	-8134	1614	-905	0	453	-3426	15.71	15.71	9.42	9.42	2	0.10	0.02	0.14	0.00	0.00	24.0
11	248	-8202	1648	-724	0	316	-3471	15.71	15.71	9.42	9.42	2	0.10	0.02	0.14	0.00	0.00	24.0
12	248	-8213	910	-833	0	419	-2586	15.71	15.71	9.42	9.42	2	0.08	0.01	0.08	0.00	0.00	24.0
13	248	-8281	945	-652	0	281	-2631	15.71	15.71	9.42	9.42	2	0.07	0.01	0.08	0.00	0.00	24.0
14	248	-8083	1328	-1091	0	602	-3080	15.71	15.71	9.42	9.42	2	0.10	0.02	0.11	0.00	0.00	24.0
15	248	-8308	1442	-488	0	143	-3228	15.71	15.71	9.42	9.42	2	0.09	0.02	0.12	0.00	0.00	24.0
16	248	-8108	1117	-1070	0	592	-2828	15.71	15.71	9.42	9.42	2	0.09	0.01	0.09	0.00	0.00	24.0
17	248	-8331	1231	-466	0	133	-2976	15.71	15.71	9.42	9.42	2	0.08	0.02	0.10	0.00	0.00	24.0
18	248	-14718	4202	-1991	0	1249	-7641	15.71	15.71	9.42	9.42	3	0.15	0.05	0.33	0.00	0.00	24.0
19	248	-18928	2645	-1909	0	1380	-7041	15.71	15.71	9.42	9.42	3	0.14	0.03	0.20	0.00	0.00	24.0
20	248	-16068	3261	-1510	0	954	-6968	15.71	15.71	9.42	9.42	3	0.13	0.04	0.25	0.00	0.00	24.0
37	248	-11348	4145	-1712	0	933	-6732	15.71	15.71	9.42	9.42	3	0.13	0.05	0.34	0.00	0.00	24.0
38	248	-18358	1549	-1575	0	1150	-5735	15.71	15.71	9.42	9.42	3	0.11	0.02	0.12	0.00	0.00	24.0
39	248	-13588	2575	-911	0	441	-5609	15.71	15.71	9.42	9.42	3	0.10	0.03	0.20	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	330	-9812	1663	-1012	0	1313	-2565	15.71	15.71	9.42	9.42	3	0.07	0.02	0.14	0.00	0.00	24.0
2	330	-7475	1614	-905	0	1200	-2094	15.71	15.71	9.42	9.42	2	0.09	0.02	0.14	0.00	0.00	24.0
3	330	-7542	1648	-724	0	913	-2111	15.71	15.71	9.42	9.42	2	0.08	0.02	0.14	0.00	0.00	24.0
4	330	-7554	910	-833	0	1106	-1835	15.71	15.71	9.42	9.42	2	0.08	0.01	0.08	0.00	0.00	24.0
5	330	-7621	945	-652	0	819	-1851	15.71	15.71	9.42	9.42	2	0.07	0.01	0.08	0.00	0.00	24.0
6	330	-7424	1328	-1091	0	1502	-1984	15.71	15.71	9.42	9.42	2	0.10	0.02	0.11	0.00	0.00	24.0
7	330	-7647	1442	-488	0	546	-2039	15.71	15.71	9.42	9.42	2	0.07	0.02	0.12	0.00	0.00	24.0
8	330	-7448	1117	-1070	0	1474	-1906	15.71	15.71	9.42	9.42	2	0.10	0.01	0.10	0.00	0.00	24.0
9	330	-7671	1231	-466	0	517	-1961	15.71	15.71	9.42	9.42	2	0.06	0.02	0.10	0.00	0.00	24.0
10	330	-7475	1614	-905	0	1200	-2094	15.71	15.71	9.42	9.42	2	0.09	0.02	0.14	0.00	0.00	24.0
11	330	-7542	1648	-724	0	913	-2111	15.71	15.71	9.42	9.42	2	0.08	0.02	0.14	0.00	0.00	24.0
12	330	-7554	910	-833	0	1106	-1835	15.71	15.71	9.42	9.42	2	0.08	0.01	0.08	0.00	0.00	24.0
13	330	-7621	945	-652	0	819	-1851	15.71	15.71	9.42	9.42	2	0.07	0.01	0.08	0.00	0.00	24.0
14	330	-7424	1328	-1091	0	1502	-1984	15.71	15.71	9.42	9.42	2	0.10	0.02	0.11	0.00	0.00	24.0
15	330	-7647	1442	-488	0	546	-2039	15.71	15.71	9.42	9.42	2	0.07	0.02	0.12	0.00	0.00	24.0
16	330	-7448	1117	-1070	0	1474	-1906	15.71	15.71	9.42	9.42	2	0.10	0.01	0.10	0.00	0.00	24.0
17	330	-7671	1231	-466	0	517	-1961	15.71	15.71	9.42	9.42	2	0.06	0.02	0.10	0.00	0.00	24.0
18	330	-13860	3996	-1991	0	2892	-4258	15.71	15.71	9.42	9.42	3	0.13	0.05	0.32	0.00	0.00	24.0
19	330	-18070	2851	-1909	0	2954	-4774	15.71	15.71	9.42	9.42	3	0.14	0.04	0.22	0.00	0.00	24.0
20	330	-15210	3261	-1510	0	2200	-4277	15.71	15.71	9.42	9.42	3	0.11	0.04	0.25	0.00	0.00	24.0
37	330	-10490	3801	-1712	0	2346	-3454	15.71	15.71	9.42	9.42	3	0.11	0.05	0.31	0.00	0.00	24.0
38	330	-17500	1893	-1575	0	2449	-4315	15.71	15.71	9.42	9.42	3	0.12	0.02	0.14	0.00	0.00	24.0
39	330	-12730	2575	-911	0	1193	-3486	15.71	15.71	9.42	9.42	3	0.08	0.03	0.21	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 22 NI 264 NF 266 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 25C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-8881	164	-432	0	-812	-532	6.28	6.28	9.42	9.42	3	0.06	0.01	0.05	0.00	0.00	24.0
2	0	-7790	297	-379	0	-756	-823	6.28	6.28	9.42	9.42	2	0.12	0.01	0.05	0.00	0.00	24.0
3	0	-7657	298	-282	0	-507	-821	6.28	6.28	9.42	9.42	2	0.11	0.01	0.03	0.00	0.00	24.0
4	0	-6006	-46	-382	0	-743	2	6.28	6.28	9.42	9.42	2	0.05	0.01	0.05	0.00	0.00	24.0
5	0	-5873	-45	-285	0	-494	4	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
6	0	-7321	176	-494	0	-1042	-536	6.28	6.28	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
7	0	-6878	179	-169	0	-212	-530	6.28	6.28	9.42	9.42	2	0.07	0.00	0.02	0.00	0.00	24.0
8	0	-6786	73	-495	0	-1038	-289	6.28	6.28	9.42	9.42	2	0.08	0.01	0.06	0.00	0.00	24.0
9	0	-6342	76	-170	0	-208	-283	6.28	6.28	9.42	9.42	2	0.04	0.00	0.02	0.00	0.00	24.0
10	0	-7790	297	-379	0	-756	-823	6.28	6.28	9.42	9.42	2	0.12	0.01	0.05	0.00	0.00	24.0
11	0	-7657	298	-282	0	-507	-821	6.28	6.28	9.42	9.42	2	0.11	0.01	0.03	0.00	0.00	24.0
12	0	-6006	-46	-382	0	-743	2	6.28	6.28	9.42	9.42	2	0.05	0.01	0.05	0.00	0.00	24.0
13	0	-5873	-45	-285	0	-494	4	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
14	0	-7321	176	-494	0	-1042	-536	6.28	6.28	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
15	0	-6878	179	-169	0	-212	-530	6.28	6.28	9.42	9.42	2	0.07	0.00	0.02	0.00	0.00	24.0
16	0	-6786	73	-495	0	-1038	-289	6.28	6.28	9.42	9.42	2	0.08	0.01	0.06	0.00	0.00	24.0
17	0	-6342	76	-170	0	-208	-283	6.28	6.28	9.42	9.42	2	0.04	0.00	0.02	0.00	0.00	24.0
18	0	-12750	612	-422	0	-1276	-1394	6.28	6.28	9.42	9.42	3	0.15	0.02	0.06	0.00	0.00	24.0
19	0	-9477	-774	-247	0	-1082	995	6.28	6.28	9.42	9.42	3	0.11	0.02	0.08	0.00	0.00	24.0
20	0	-10520	-43	-392	0	-808	-249	6.28	6.28	9.42	9.42	3	0.04	0.01	0.05	0.00	0.00	24.0
37	0	-13120	1156	-513	0	-1222	-2301	6.28	6.28	9.42	9.42	3	0.23	0.03	0.12	0.00	0.00	24.0
38	0	-7669	-1154	-221	0	-899	1682	6.28	6.28	9.42	9.42	3	0.18	0.03	0.13	0.00	0.00	24.0
39	0	-9403	65	-463	0	-441	-392	6.28	6.28	9.42	9.42	3	0.04	0.01	0.05	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
1	95	-8325	164	-432	0	-402	-377	6.28	6.28	9.42	9.42	3	0.04	0.01	0.05	0.00	0.00	24.0
2	95	-7362	297	-379	0	-395	-540	6.28	6.28	9.42	9.42	2	0.07	0.01	0.05	0.00	0.00	24.0
3	95	-7230	298	-282	0	-239	-538	6.28	6.28	9.42	9.42	2	0.07	0.01	0.03	0.00	0.00	24.0
4	95	-5578	-46	-382	0	-380	-42	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
5	95	-5446	-45	-285	0	-224	-39	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
6	95	-6894	176	-494	0	-573	-369	6.28	6.28	9.42	9.42	2	0.06	0.01	0.06	0.00	0.00	24.0
7	95	-6450	179	-169	0	-51	-360	6.28	6.28	9.42	9.42	2	0.04	0.00	0.02	0.00	0.00	24.0
8	95	-6358	73	-495	0	-568	-220	6.28	6.28	9.42	9.42	2	0.05	0.01	0.06	0.00	0.00	24.0
9	95	-5914	76	-170	0	-46	-210	6.28	6.28	9.42	9.42	2	0.03	0.00	0.02	0.00	0.00	24.0
10	95	-7362	297	-379	0	-395	-540	6.28	6.28	9.42	9.42	2	0.07	0.01	0.05	0.00	0.00	24.0
11	95	-7230	298	-282	0	-239	-538	6.28	6.28	9.42	9.42	2	0.07	0.01	0.03	0.00	0.00	24.0
12	95	-5578	-46	-382	0	-380	-42	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
13	95	-5446	-45	-285	0	-224	-39	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
14	95	-6894	176	-494	0	-573	-369	6.28	6.28	9.42	9.42	2	0.06	0.01	0.06	0.00	0.00	24.0
15	95	-6450	179	-169	0	-51	-360	6.28	6.28	9.42	9.42	2	0.04	0.00	0.02	0.00	0.00	24.0
16	95	-6358	73	-495	0	-568	-220	6.28	6.28	9.42	9.42	2	0.05	0.01	0.06	0.00	0.00	24.0
17	95	-5914	76	-170	0	-46	-210	6.28	6.28	9.42	9.42	2	0.03	0.00	0.02	0.00	0.00	24.0
18	95	-12192	493	-422	0	-875	-869	6.28	6.28	9.42	9.42	3	0.09	0.01	0.05	0.00	0.00	24.0
19	95	-8921	-655	-247	0	-848	317	6.28	6.28	9.42	9.42	3	0.05	0.02	0.06	0.00	0.00	24.0
20	95	-9964	-43	-265	0	-497	-290	6.28	6.28	9.42	9.42	3	0.04	0.01	0.03	0.00	0.00	24.0
37	95	-12562	958	-513	0	-734	-1297	6.28	6.28	9.42	9.42	3	0.13	0.02	0.10	0.00	0.00	24.0
38	95	-7113	-956	-221	0	-689	680	6.28	6.28	9.42	9.42	3	0.08	0.02	0.10	0.00	0.00	24.0
39	95	-8847	65	-251	0	-105	-331	6.28	6.28	9.42	9.42	3	0.03	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
1	190	-7770	164	-432	0	8	-221	6.28	6.28	9.42	9.42	3	0.02	0.01	0.05	0.00	0.00	24.0
2	190	-6935	297	-379	0	-35	-258	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
3	190	-6802	298	-282	0	29	-255	6.28	6.28	9.42	9.42	2	0.03	0.01	0.03	0.00	0.00	24.0
4	190	-5151	-46	-382	0	-17	-86	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
5	190	-5018	-45	-285	0	47	-82	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
6	190	-6466	176	-494	0	-104	-202	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
7	190	-6023	179	-169	0	110	-190	6.28	6.28	9.42	9.42	2	0.03	0.00	0.02	0.00	0.00	24.0
8	190	-5931	73	-495	0	-98	-151	6.28	6.28	9.42	9.42	2	0.02	0.01	0.06	0.00	0.00	24.0
9	190	-5487	76	-170	0	116	-138	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
10	190	-6935	297	-379	0	-35	-258	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
11	190	-6802	298	-282	0	29	-255	6.28	6.28	9.42	9.42	2	0.03	0.01	0.03	0.00	0.00	24.0
12	190	-5151	-46	-382	0	-17	-86	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
13	190	-5018	-45	-285	0	47	-82	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
14	190	-6466	176	-494	0	-104	-202	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
15	190	-6023	179	-169	0	110	-190	6.28	6.28	9.42	9.42	2	0.03	0.00	0.02	0.00	0.00	24.0
16	190	-5931	73	-495	0	-98	-151	6.28	6.28	9.42	9.42	2	0.02	0.01	0.06	0.00	0.00	24.0
17	190	-5487	76	-170	0	116	-138	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
18	190	-11635	374	-422	0	-474	-458	6.28	6.28	9.42	9.42	3	0.05	0.01	0.05	0.00	0.00	24.0
19	190	-8366	-537	-247	0	-613	-250	6.28	6.28	9.42	9.42	3	0.04	0.01	0.05	0.00	0.00	24.0
20	190	-9407	-43	-156	0	-299	-330	6.28	6.28	9.42	9.42	3	0.04	0.00	0.02	0.00	0.00	24.0
37	190	-12005	760	-513	0	-247	-481	6.28	6.28	9.42	9.42	3	0.05	0.02	0.08	0.00	0.00	24.0
38	190	-6558	-758	-221	0	-479	-134	6.28	6.28	9.42	9.42	3	0.03	0.02	0.08	0.00	0.00	24.0
39	190	-8292	65	-69	0	45	-269	6.28	6.28	9.42	9.42	3	0.03	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
1	285	-7214	164	-432	0	418	-66	6.28	6.28	9.42	9.42	3	0.02	0.01	0.05	0.00	0.00	24.0
2	285	-6508	297	-379	0	325	24	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
3	285	-6374	298	-282	0	297	28	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
4	285	-4724	-46	-382	0	346	-130	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
5	285	-4590	-45	-285	0	318	-125	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
6	285	-6038	176	-494	0	365	-35	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
7	285	-5596	179	-169	0	271	-20	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
8	285	-5504	73	-495	0	372	-82	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
9	285	-5060	76	-170	0	277	-66	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
10	285	-6508	297	-379	0	325	24	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
11	285	-6374	298	-282	0	297	28	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
12	285	-4724	-46	-382	0	346	-130	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
13	285	-4590	-45	-285	0	318	-125	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
14	285	-6038	176	-494	0	365	-35	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
15	285	-5596	179	-169	0	271	-20	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
16	285	-5504	73	-495	0	372	-82	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
17	285	-5060	76	-170	0	277	-66	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
18	285	-11078	255	-422	0	-73	-159	6.28	6.28	9.42	9.42	3	0.02	0.01	0.05	0.00	0.00	24.0
19	285	-7810	-418	-247	0	-379	-703	6.28	6.28	9.42	9.42	3	0.08	0.01	0.05	0.00	0.00	24.0

20	285	-8850	-43	-65	0	-196	-371	6.28	6.28	9.42	9.42	3	0.04	0.00	0.01	0.00	0.00	24.0
37	285	-11448	562	-513	0	241	146	6.28	6.28	9.42	9.42	3	0.02	0.01	0.06	0.00	0.00	24.0
38	285	-6002	-560	-221	0	-269	-760	6.28	6.28	9.42	9.42	3	0.08	0.01	0.06	0.00	0.00	24.0
39	285	-7736	65	82	0	37	-207	6.28	6.28	9.42	9.42	3	0.02	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	380	-6658	164	-432	0	828	89	6.28	6.28	9.42	9.42	3	0.04	0.01	0.05	0.00	0.00	24.0
2	380	-6080	297	-379	0	685	306	6.28	6.28	9.42	9.42	2	0.06	0.01	0.05	0.00	0.00	24.0
3	380	-5947	298	-282	0	564	312	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
4	380	-4296	-46	-382	0	709	-174	6.28	6.28	9.42	9.42	2	0.06	0.01	0.05	0.00	0.00	24.0
5	380	-4163	-45	-285	0	588	-169	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
6	380	-5611	176	-494	0	834	132	6.28	6.28	9.42	9.42	2	0.06	0.01	0.06	0.00	0.00	24.0
7	380	-5168	179	-169	0	432	150	6.28	6.28	9.42	9.42	2	0.04	0.00	0.02	0.00	0.00	24.0
8	380	-5076	73	-495	0	842	-13	6.28	6.28	9.42	9.42	2	0.05	0.01	0.06	0.00	0.00	24.0
9	380	-4632	76	-170	0	439	6	6.28	6.28	9.42	9.42	2	0.03	0.00	0.02	0.00	0.00	24.0
10	380	-6080	297	-379	0	685	306	6.28	6.28	9.42	9.42	2	0.06	0.01	0.05	0.00	0.00	24.0
11	380	-5947	298	-282	0	564	312	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
12	380	-4296	-46	-382	0	709	-174	6.28	6.28	9.42	9.42	2	0.06	0.01	0.05	0.00	0.00	24.0
13	380	-4163	-45	-285	0	588	-169	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
14	380	-5611	176	-494	0	834	132	6.28	6.28	9.42	9.42	2	0.06	0.01	0.06	0.00	0.00	24.0
15	380	-5168	179	-169	0	432	150	6.28	6.28	9.42	9.42	2	0.04	0.00	0.02	0.00	0.00	24.0
16	380	-5076	73	-495	0	842	-13	6.28	6.28	9.42	9.42	2	0.05	0.01	0.06	0.00	0.00	24.0
17	380	-4632	76	-170	0	439	6	6.28	6.28	9.42	9.42	2	0.03	0.00	0.02	0.00	0.00	24.0
18	380	-10520	136	-422	0	328	27	6.28	6.28	9.42	9.42	3	0.02	0.01	0.05	0.00	0.00	24.0
19	380	-7254	-299	-247	0	-144	-1043	6.28	6.28	9.42	9.42	3	0.11	0.01	0.03	0.00	0.00	24.0
20	380	-8294	-43	8	0	-170	-412	6.28	6.28	9.42	9.42	3	0.04	0.00	0.00	0.00	0.00	24.0
37	380	-10890	364	-513	0	729	586	6.28	6.28	9.42	9.42	3	0.06	0.01	0.06	0.00	0.00	24.0
38	380	-5446	-362	-221	0	-59	-1198	6.28	6.28	9.42	9.42	3	0.13	0.01	0.04	0.00	0.00	24.0
39	380	-7180	65	203	0	-101	-145	6.28	6.28	9.42	9.42	3	0.02	0.00	0.02	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

VERIFICA NODO IN TESTA AL PILASTRO, NODO NUM. 266 NON CONFINATO

(par.7.2.2 NTC2018 "La domanda di resistenza valutata con i criteri della progettazione in capacità può essere assunta non superiore alla domanda di resistenza valutata per il caso di comportamento strutturale non dissipativo.")

PROGETTAZIONE IN CAPACITA'

Asse loc. pilastro y nodo ESTERNO: As2(inf)= 4.02, As1(sup)= 6.03, Hjw= 40.0 cm, bj= 45.0 cm, hjc= 20.0 cm
Asse loc. pilastro z nodo ESTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 30.0 cm, hjc= 50.0 cm

FxMin,inf	FxMin,sup	FxMax,sup	FySup	FzSup	Vjbdy	Vjbdz	Vres,y	Vres,z	I.R.compr.	Ashy	Ashz	PASSO	Nota
daN					daN		daN			cmq		cm	
-4163	1	-0	0	0	26425	17616	63005	105009	0.42	4.37	--	11.94	

VERIFICA DI RESISTENZA CON SOLLECITAZIONI COMPORTAMENTO NON DISSIPATIVO

Asse loc. pilastro y nodo ESTERNO: Hjw= 40.0 cm, bj= 45.0 cm, hjc= 20.0 cm, db1= 45.0 cm

NC	Fx,sup	Fx,inf	Mb	Vb	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-0	-6080	-2673	1806	0	6600	63005	0.10	0.00	40.00	
3	-0	-5947	-2651	1800	0	6546	63005	0.10	0.00	40.00	
4	-0	-4296	-462	1135	0	1142	63005	0.02	0.00	40.00	
5	-0	-4163	-440	1129	0	1086	63005	0.02	0.00	40.00	
6	-0	-5611	-1925	1579	0	4753	63005	0.08	0.00	40.00	
7	-0	-5168	-1851	1558	0	4570	63005	0.07	0.00	40.00	
8	-0	-5076	-1262	1377	0	3116	63005	0.05	0.00	40.00	
9	-0	-4632	-1188	1357	0	2933	63005	0.05	0.00	40.00	
10	-0	-6080	-2673	1806	0	6600	63005	0.10	0.00	40.00	
11	-0	-5947	-2651	1800	0	6546	63005	0.10	0.00	40.00	
12	-0	-4296	-462	1135	0	1142	63005	0.02	0.00	40.00	
13	-0	-4163	-440	1129	0	1086	63005	0.02	0.00	40.00	
14	-0	-5611	-1925	1579	0	4753	63005	0.08	0.00	40.00	
15	-0	-5168	-1851	1558	0	4570	63005	0.07	0.00	40.00	
16	-0	-5076	-1262	1377	0	3116	63005	0.05	0.00	40.00	
17	-0	-4632	-1188	1357	0	2933	63005	0.05	0.00	40.00	

Asse loc. pilastro z nodo ESTERNO: Hjw= 40.0 cm, bj= 30.0 cm, hjc= 50.0 cm, db1= 45.0 cm

NC	Fx,sup	Fx,inf	Mb	Vb	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-0	-6080	-2200	1743	0	5432	105009	0.05	0.00	40.00	
3	-0	-5947	-1953	1666	0	4822	105009	0.05	0.00	40.00	
4	-0	-4296	-2128	1720	0	5254	105009	0.05	0.00	40.00	
5	-0	-4163	-1881	1643	0	4644	105009	0.04	0.00	40.00	
6	-0	-5611	-2463	1825	0	6081	105009	0.06	0.00	40.00	
7	-0	-5168	-1640	1568	0	4049	105009	0.04	0.00	40.00	
8	-0	-5076	-2441	1818	0	6027	105009	0.06	0.00	40.00	
9	-0	-4632	-1618	1561	0	3995	105009	0.04	0.00	40.00	
10	-0	-6080	-2200	1743	0	5432	105009	0.05	0.00	40.00	
11	-0	-5947	-1953	1666	0	4822	105009	0.05	0.00	40.00	
12	-0	-4296	-2128	1720	0	5254	105009	0.05	0.00	40.00	
13	-0	-4163	-1881	1643	0	4644	105009	0.04	0.00	40.00	
14	-0	-5611	-2463	1825	0	6081	105009	0.06	0.00	40.00	
15	-0	-5168	-1640	1568	0	4049	105009	0.04	0.00	40.00	
16	-0	-5076	-2441	1818	0	6027	105009	0.06	0.00	40.00	
17	-0	-4632	-1618	1561	0	3995	105009	0.04	0.00	40.00	

CONFRONTO E SINTESI CONCLUSIVE (si assume in ogni caso passo <= 15 cm)

I.R.compr.	Ashy	Ashz	PASSO	Nota
	cmq		cm	
0.10	--	--	15.00	**VERIFICATO**

ASTA NUM. 23 NI 298 NF 271 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 20C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-12630	-165	-95	0	-1302	434	6.28	6.28	12.57	12.57	3	0.05	0.00	0.01	0.00	0.00	24.0
2	0	-9499	556	-125	0	-1380	-901	6.28	6.28	12.57	12.57	2	0.10	0.01	0.05	0.00	0.00	24.0
3	0	-9473	550	-0	0	-591	-889	6.28	6.28	12.57	12.57	2	0.07	0.01	0.05	0.00	0.00	24.0
4	0	-9963	-804	-146	0	-1413	1556	6.28	6.28	12.57	12.57	2	0.14	0.01	0.08	0.00	0.00	24.0
5	0	-9937	-811	-21	0	-624	1568	6.28	6.28	12.57	12.57	2	0.11	0.01	0.08	0.00	0.00	24.0
6	0	-9691	88	-278	0	-2313	-56	6.28	6.28	12.57	12.57	2	0.12	0.00	0.03	0.00	0.00	24.0
7	0	-9605	66	138	0	319	-15	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
8	0	-9830	-320	-284	0	-2323	682	6.28	6.28	12.57	12.57	2	0.14	0.01	0.03	0.00	0.00	24.0
9	0	-9745	-342	132	0	309	723	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
10	0	-9499	556	-125	0	-1380	-901	6.28	6.28	12.57	12.57	2	0.10	0.01	0.05	0.00	0.00	24.0
11	0	-9473	550	-0	0	-591	-889	6.28	6.28	12.57	12.57	2	0.07	0.01	0.05	0.00	0.00	24.0
12	0	-9963	-804	-146	0	-1413	1556	6.28	6.28	12.57	12.57	2	0.14	0.01	0.08	0.00	0.00	24.0
13	0	-9937	-811	-21	0	-624	1568	6.28	6.28	12.57	12.57	2	0.11	0.01	0.08	0.00	0.00	24.0
14	0	-9691	88	-278	0	-2313	-56	6.28	6.28	12.57	12.57	2	0.12	0.00	0.03	0.00	0.00	24.0
15	0	-9605	66	138	0	319	-15	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
16	0	-9830	-320	-284	0	-2323	682	6.28	6.28	12.57	12.57	2	0.14	0.01	0.03	0.00	0.00	24.0
17	0	-9745	-342	132	0	309	723	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
18	0	-14210	1398	-185	0	-2837	-2291	6.28	6.28	12.57	12.57	3	0.15	0.03	0.11	0.00	0.00	24.0
19	0	-16260	-2093	-314	0	-3092	3923	6.28	6.28	12.57	12.57	3	0.23	0.04	0.18	0.00	0.00	24.0
20	0	-14710	-321	-765	0	-1754	763	6.28	6.28	12.57	12.57	3	0.07	0.01	0.07	0.00	0.00	24.0
37	0	-12730	2620	-92	0	-2214	-4485	6.28	6.28	12.57	12.57	3	0.25	0.05	0.24	0.00	0.00	24.0
38	0	-16150	-3199	-307	0	-2638	5872	6.28	6.28	12.57	12.57	3	0.32	0.06	0.28	0.00	0.00	24.0
39	0	-13560	-246	-1059	0	-409	606	6.28	6.28	12.57	12.57	3	0.03	0.02	0.10	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	95	-11890	-165	-95	0	-1212	277	6.28	6.28	12.57	12.57	3	0.05	0.00	0.01	0.00	0.00	24.0
2	95	-8929	556	-125	0	-1261	-373	6.28	6.28	12.57	12.57	2	0.08	0.01	0.05	0.00	0.00	24.0
3	95	-8903	550	-0	0	-590	-367	6.28	6.28	12.57	12.57	2	0.04	0.01	0.05	0.00	0.00	24.0
4	95	-9393	-804	-146	0	-1275	792	6.28	6.28	12.57	12.57	2	0.09	0.01	0.07	0.00	0.00	24.0
5	95	-9367	-811	-21	0	-604	798	6.28	6.28	12.57	12.57	2	0.07	0.01	0.08	0.00	0.00	24.0
6	95	-9121	88	-278	0	-2049	28	6.28	6.28	12.57	12.57	2	0.11	0.00	0.03	0.00	0.00	24.0
7	95	-9035	66	138	0	187	48	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
8	95	-9260	-320	-284	0	-2053	378	6.28	6.28	12.57	12.57	2	0.12	0.01	0.03	0.00	0.00	24.0
9	95	-9175	-342	132	0	183	397	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
10	95	-8929	556	-125	0	-1261	-373	6.28	6.28	12.57	12.57	2	0.08	0.01	0.05	0.00	0.00	24.0
11	95	-8903	550	-0	0	-590	-367	6.28	6.28	12.57	12.57	2	0.04	0.01	0.05	0.00	0.00	24.0
12	95	-9393	-804	-146	0	-1275	792	6.28	6.28	12.57	12.57	2	0.09	0.01	0.07	0.00	0.00	24.0
13	95	-9367	-811	-21	0	-604	798	6.28	6.28	12.57	12.57	2	0.07	0.01	0.08	0.00	0.00	24.0
14	95	-9121	88	-278	0	-2049	28	6.28	6.28	12.57	12.57	2	0.11	0.00	0.03	0.00	0.00	24.0
15	95	-9035	66	138	0	187	48	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
16	95	-9260	-320	-284	0	-2053	378	6.28	6.28	12.57	12.57	2	0.12	0.01	0.03	0.00	0.00	24.0
17	95	-9175	-342	132	0	183	397	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
18	95	-13470	1398	-185	0	-2661	-963	6.28	6.28	12.57	12.57	3	0.11	0.03	0.11	0.00	0.00	24.0
19	95	-15520	-2093	-314	0	-2793	1935	6.28	6.28	12.57	12.57	3	0.14	0.04	0.17	0.00	0.00	24.0
20	95	-13970	-321	-513	0	-1150	458	6.28	6.28	12.57	12.57	3	0.05	0.01	0.05	0.00	0.00	24.0
37	95	-11989	2620	-92	0	-2126	-1996	6.28	6.28	12.57	12.57	3	0.13	0.05	0.22	0.00	0.00	24.0
38	95	-15408	-3199	-307	0	-2346	2833	6.28	6.28	12.57	12.57	3	0.17	0.06	0.28	0.00	0.00	24.0
39	95	-12820	-246	-638	0	393	372	6.28	6.28	12.57	12.57	3	0.02	0.01	0.06	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	190	-11150	-165	-95	0	-1122	120	6.28	6.28	12.57	12.57	3	0.04	0.00	0.01	0.00	0.00	24.0
2	190	-8359	556	-125	0	-1143	156	6.28	6.28	12.57	12.57	2	0.06	0.01	0.05	0.00	0.00	24.0
3	190	-8333	550	-0	0	-590	156	6.28	6.28	12.57	12.57	2	0.04	0.01	0.05	0.00	0.00	24.0
4	190	-8823	-804	-146	0	-1137	28	6.28	6.28	12.57	12.57	2	0.06	0.01	0.07	0.00	0.00	24.0
5	190	-8797	-811	-21	0	-585	28	6.28	6.28	12.57	12.57	2	0.03	0.01	0.07	0.00	0.00	24.0
6	190	-8551	88	-278	0	-1785	112	6.28	6.28	12.57	12.57	2	0.10	0.00	0.03	0.00	0.00	24.0
7	190	-8465	66	138	0	56	110	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
8	190	-8690	-320	-284	0	-1784	74	6.28	6.28	12.57	12.57	2	0.09	0.01	0.03	0.00	0.00	24.0
9	190	-8605	-342	132	0	58	72	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
10	190	-8359	556	-125	0	-1143	156	6.28	6.28	12.57	12.57	2	0.06	0.01	0.05	0.00	0.00	24.0
11	190	-8333	550	-0	0	-590	156	6.28	6.28	12.57	12.57	2	0.04	0.01	0.05	0.00	0.00	24.0
12	190	-8823	-804	-146	0	-1137	28	6.28	6.28	12.57	12.57	2	0.06	0.01	0.07	0.00	0.00	24.0
13	190	-8797	-811	-21	0	-585	28	6.28	6.28	12.57	12.57	2	0.03	0.01	0.07	0.00	0.00	24.0
14	190	-8551	88	-278	0	-1785	112	6.28	6.28	12.57	12.57	2	0.10	0.00	0.03	0.00	0.00	24.0
15	190	-8465	66	138	0	56	110	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
16	190	-8690	-320	-284	0	-1784	74	6.28	6.28	12.57	12.57	2	0.09	0.01	0.03	0.00	0.00	24.0
17	190	-8605	-342	132	0	58	72	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
18	190	-12730	1398	-185	0	-2485	366	6.28	6.28	12.57	12.57	3	0.09	0.03	0.11	0.00	0.00	24.0
19	190	-14780	-2093	-314	0	-2494	-54	6.28	6.28	12.57	12.57	3	0.09	0.04	0.17	0.00	0.00	24.0
20	190	-13230	-321	-297	0	-768	153	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
37	190	-11248	2620	-92	0	-2038	492	6.28	6.28	12.57	12.57	3	0.08	0.05	0.22	0.00	0.00	24.0
38	190	-14665	-3199	-307	0	-2054	-207	6.28	6.28	12.57	12.57	3	0.07	0.06	0.26	0.00	0.00	24.0
39	190	-12080	-246	-278	0	823	138	6.28	6.28	12.57	12.57	3	0.03	0.00	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	285	-10409	-165	-95	0	-1033	-37	6.28	6.28	12.57	12.57	3	0.04	0.00	0.01	0.00	0.00	24.0
2	285	-7789	556	-125	0	-1024	684	6.28	6.28	12.57	12.57	2	0.08	0.01	0.05	0.00	0.00	24.0
3	285	-7763	550	-0	0	-590	678	6.28	6.28	12.57	12.57	2	0.06	0.01	0.05	0.00	0.00	24.0
4	285	-8253	-804	-146	0	-998	-735	6.28	6.28	12.57	12.57	2	0.08	0.01	0.07	0.00	0.00	24.0
5	285	-8227	-811	-21	0	-565	-742	6.28	6.28	12.57	12.57	2	0.06	0.01	0.08	0.00	0.00	24.0
6	285	-7981	88	-278	0	-1521	196	6.28	6.28	12.57	12.57	2	0.09	0.00	0.03	0.00	0.00	24.0
7	285	-7895	66	138	0	-75	173	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
8	285	-8120	-320	-284	0	-1514	-230	6.28	6.28	12.57	12.57	2	0.09	0.01	0.03	0.00	0.00	24.0
9	285	-8035	-342	132	0	-68	-253	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
10	285	-7789	556	-125	0	-1024	684	6.28	6.28	12.57	12.57	2	0.08	0.01	0.05	0.00	0.00	24.0
11	285	-7763	550	-0	0	-590	678	6.28	6.28	12.57	12.57	2	0.06	0.01	0.05	0.00	0.00	24.0
12	285	-8253	-804	-146	0	-998	-735	6.28	6.28	12.57	12.57	2	0.08	0.01	0.07	0.00	0.00	24.0
13	285	-8227	-811	-21	0	-565	-742	6.28	6.28	12.57	12.57	2	0.06	0.01	0.08	0.00	0.00	24.0
14	285	-7981	88	-278	0	-1521	196	6.28	6.28	12.57	12.57	2	0.09	0.00	0.03	0.00	0.00	24.0
15	285	-7895	66	138	0	-75	173	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
16	285	-8120	-320	-284	0	-1514	-230	6.28	6.28	12.57	12.57	2	0.09	0.01	0.03	0.00	0.00	24.0
17	285	-8035	-342	132	0	-68	-253	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
18	285	-11990	1398	-185	0	-2309	1694	6.28	6.28	12.57	12.57	3	0.12	0.03	0.12	0.00	0.00	24.0
19	285	-14040	-2093	-314	0	-2196	-2042	6.28	6.28	12.57	12.57	3	0.13	0.04	0.17	0.00	0.00	24.0
20	285	-12490	-321	-117	0	-574	-152	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
37	285	-10508	2620	-92	0	-1951	2981	6.28	6.28	12.57	12.57	3	0.17	0.05	0.25	0.00	0.00	24.0
38	285	-13922	-3199	-307	0	-1762	-3246	6.28	6.28	12.57	12.57	3	0.18	0.06	0.29	0.00	0.00	24.0
39	285	-11340	-246	22	0	940	-96	6.28	6.28	12.57	12.57	3	0.03	0.00	0.02	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	380	-9669	-165	-95	0	-943	-194	6.28	6.28	12.57	12.57	3	0.04	0.00	0.01	0.00	0.00	24.0
2	380	-7219	556	-125	0	-905	1213	6.28	6.28	12.57	12.57	2	0.10	0.01	0.05	0.00	0.00	24.0
3	380	-7193	550	-0	0	-590	1200	6.28	6.28	12.57	12.57	2	0.09	0.01	0.05	0.00	0.00	24.0
4	380	-7683	-804	-146	0	-860	-1499	6.28	6.28	12.57	12.57	2	0.12	0.01	0.08	0.00	0.00	24.0
5	380	-7657	-811	-21	0	-545	-1512	6.28	6.28	12.57	12.57	2	0.11	0.01	0.08	0.00	0.00	24.0
6	380	-7411	88	-278	0	-1257	279	6.28	6.28	12.57	12.57	2	0.07	0.00	0.03	0.00	0.00	24.0
7	380	-7325	66	138	0	-207	235	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
8	380	-7550	-320	-284	0	-1244	-534	6.28	6.28	12.57	12.57	2	0.08	0.01	0.03	0.00	0.00	24.0
9	380	-7465	-342	132	0	-193	-578	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
10	380	-7219	556	-125	0	-905	1213	6.28	6.28	12.57	12.57	2	0.10	0.01	0.05	0.00	0.00	24.0
11	380	-7193	550	-0	0	-590	1200	6.28	6.28	12.57	12.57	2	0.09	0.01	0.05	0.00	0.00	24.0
12	380	-7683	-804	-146	0	-860	-1499	6.28	6.28	12.57	12.57	2	0.12	0.01	0.08	0.00	0.00	24.0
13	380	-7657	-811	-21	0	-545	-1512	6.28	6.28	12.57	12.57	2	0.11	0.01	0.08	0.00	0.00	24.0
14	380	-7411	88	-278	0	-1257	279	6.28	6.28	12.57	12.57	2	0.07	0.00	0.03	0.00	0.00	24.0
15	380	-7325	66	138	0	-207	235	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
16	380	-7550	-320	-284	0	-1244	-534	6.28	6.28	12.57	12.57	2	0.08	0.01	0.03	0.00	0.00	24.0
17	380	-7465	-342	132	0	-193	-578	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
18	380	-11250	1398	-185	0	-2133	3023	6.28	6.28	12.57	12.57	3	0.18	0.03	0.13	0.00	0.00	24.0
19	380	-13300	-2093	-314	0	-1897	-4030	6.28	6.28	12.57	12.57	3	0.23	0.04	0.19	0.00	0.00	24.0
20	380	-11750	-321	27	0	-534	-458	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
37	380	-9767	2620	-92	0	-1863	5470	6.28	6.28	12.57	12.57	3	0.31	0.05	0.25	0.00	0.00	24.0
38	380	-13180	-3199	-307	0	-1470	-6285	6.28	6.28	12.57	12.57	3	0.35	0.06	0.29	0.00	0.00	24.0
39	380	-10600	-246	261	0	801	-330	6.28	6.28	12.57	12.57	3	0.03	0.00	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

VERIFICA NODO IN TESTA AL PILASTRO, NODO NUM. 271 NON CONFINATO

(par.7.2.2 NTC2018 "La domanda di resistenza valutata con i criteri della progettazione in capacità può essere assunta non superiore alla domanda di resistenza valutata per il caso di comportamento strutturale non dissipativo.")

PROGETTAZIONE IN CAPACITA'

Asse loc. pilastro y nodo INTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 50.0 cm, hjc= 30.0 cm
Asse loc. pilastro z nodo: --

FxMin,inf	FxMin,sup	FxMax,sup	FySup	FzSup	Vjbdy	Vjbdz	Vres,y	Vres,z	I.R.compr.	Ashy	Ashz	PASSO	Nota
daN					daN		daN			cmq		cm	
-7193	-3996	-4233	131	96	35102	--	129932	--	0.27	8.78	--	5.18	

VERIFICA DI RESISTENZA CON SOLLECITAZIONI COMPORTAMENTO NON DISSIPATIVO

Asse loc. pilastro y nodo INTERNO: Hjw= 40.0 cm, bj= 50.0 cm, hjc= 30.0 cm, db1= 45.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb,1	Mb,2	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m			daN			cmq	cm	
2	-4026	-7219	-2256	-665	144	3783	129997	0.03	0.00	40.00	
3	-3996	-7193	-2248	-677	142	3737	130006	0.03	0.00	40.00	
4	-4233	-7683	-1097	-2247	134	2706	129932	0.02	0.00	40.00	
5	-4204	-7657	-1090	-2259	131	2755	129941	0.02	0.00	40.00	
6	-4133	-7411	-1858	-1206	143	1467	129963	0.01	0.00	40.00	
7	-4035	-7325	-1835	-1244	136	1323	129994	0.01	0.00	40.00	
8	-4195	-7550	-1511	-1680	140	278	129944	0.00	0.00	40.00	
9	-4097	-7465	-1487	-1719	133	440	129975	0.00	0.00	40.00	
10	-4026	-7219	-2256	-665	144	3783	129997	0.03	0.00	40.00	
11	-3996	-7193	-2248	-677	142	3737	130006	0.03	0.00	40.00	
12	-4233	-7683	-1097	-2247	134	2706	129932	0.02	0.00	40.00	
13	-4204	-7657	-1090	-2259	131	2755	129941	0.02	0.00	40.00	
14	-4133	-7411	-1858	-1206	143	1467	129963	0.01	0.00	40.00	
15	-4035	-7325	-1835	-1244	136	1323	129994	0.01	0.00	40.00	
16	-4195	-7550	-1511	-1680	140	278	129944	0.00	0.00	40.00	
17	-4097	-7465	-1487	-1719	133	440	129975	0.00	0.00	40.00	

CONFRONTO E SINTESI CONCLUSIVE (si assume in ogni caso passo <= 15 cm)

I.R.compr.	Ashy	Ashz	PASSO	Nota
	cmq		cm	
0.03	--	--	15.00	**VERIFICATO**

ASTA NUM. 24 NI 78 NF 77 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 6B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-23970	-814	36	0	66	10330	15.71	15.71	9.42	9.42	3	0.18	0.01	0.06	0.00	0.00	24.0
2	0	-18560	-519	-8	0	-37	6966	15.71	15.71	9.42	9.42	2	0.17	0.01	0.04	0.00	0.00	24.0
3	0	-18540	-494	80	0	180	6821	15.71	15.71	9.42	9.42	2	0.17	0.01	0.04	0.00	0.00	24.0
4	0	-18330	-759	-25	0	-78	9068	15.71	15.71	9.42	9.42	2	0.22	0.01	0.06	0.00	0.00	24.0
5	0	-18310	-734	62	0	139	8923	15.71	15.71	9.42	9.42	2	0.22	0.01	0.06	0.00	0.00	24.0
6	0	-18510	-631	-116	0	-304	7871	15.71	15.71	9.42	9.42	2	0.20	0.01	0.05	0.00	0.00	24.0
7	0	-18430	-550	176	0	418	7387	15.71	15.71	9.42	9.42	2	0.19	0.01	0.04	0.00	0.00	24.0
8	0	-18440	-703	-121	0	-317	8502	15.71	15.71	9.42	9.42	2	0.21	0.01	0.05	0.00	0.00	24.0
9	0	-18360	-622	171	0	406	8018	15.71	15.71	9.42	9.42	2	0.20	0.01	0.05	0.00	0.00	24.0
10	0	-18560	-519	-8	0	-37	6966	15.71	15.71	9.42	9.42	2	0.17	0.01	0.04	0.00	0.00	24.0
11	0	-18540	-494	80	0	180	6821	15.71	15.71	9.42	9.42	2	0.17	0.01	0.04	0.00	0.00	24.0
12	0	-18330	-759	-25	0	-78	9068	15.71	15.71	9.42	9.42	2	0.22	0.01	0.06	0.00	0.00	24.0
13	0	-18310	-734	62	0	139	8923	15.71	15.71	9.42	9.42	2	0.22	0.01	0.06	0.00	0.00	24.0
14	0	-18510	-631	-116	0	-304	7871	15.71	15.71	9.42	9.42	2	0.20	0.01	0.05	0.00	0.00	24.0
15	0	-18430	-550	176	0	418	7387	15.71	15.71	9.42	9.42	2	0.19	0.01	0.04	0.00	0.00	24.0
16	0	-18440	-703	-121	0	-317	8502	15.71	15.71	9.42	9.42	2	0.21	0.01	0.05	0.00	0.00	24.0
17	0	-18360	-622	171	0	406	8018	15.71	15.71	9.42	9.42	2	0.20	0.01	0.05	0.00	0.00	24.0
18	0	-34830	577	70	0	111	14750	15.71	15.71	9.42	9.42	3	0.25	0.01	0.04	0.00	0.00	24.0
19	0	-27250	-3632	-64	0	-179	22290	15.71	15.71	9.42	9.42	3	0.38	0.05	0.25	0.00	0.00	24.0
20	0	-30120	-1271	294	0	660	16950	15.71	15.71	9.42	9.42	3	0.29	0.02	0.09	0.00	0.00	24.0
37	0	-35100	2213	126	0	241	9572	15.71	15.71	9.42	9.42	3	0.16	0.03	0.14	0.00	0.00	24.0
38	0	-22470	-4802	-98	0	-242	22140	15.71	15.71	9.42	9.42	3	0.39	0.06	0.35	0.00	0.00	24.0
39	0	-27250	-868	499	0	1156	13240	15.71	15.71	9.42	9.42	3	0.23	0.01	0.06	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	110	-22825	-814	36	0	27	9434	15.71	15.71	9.42	9.42	3	0.16	0.01	0.06	0.00	0.00	24.0
2	110	-17680	-519	-8	0	-29	6395	15.71	15.71	9.42	9.42	2	0.16	0.01	0.04	0.00	0.00	24.0
3	110	-17660	-494	80	0	92	6277	15.71	15.71	9.42	9.42	2	0.15	0.01	0.04	0.00	0.00	24.0
4	110	-17450	-759	-25	0	-50	8234	15.71	15.71	9.42	9.42	2	0.20	0.01	0.06	0.00	0.00	24.0
5	110	-17430	-734	62	0	70	8115	15.71	15.71	9.42	9.42	2	0.20	0.01	0.06	0.00	0.00	24.0
6	110	-17630	-631	-116	0	-177	7177	15.71	15.71	9.42	9.42	2	0.18	0.01	0.05	0.00	0.00	24.0
7	110	-17550	-550	176	0	225	6782	15.71	15.71	9.42	9.42	2	0.17	0.01	0.04	0.00	0.00	24.0
8	110	-17560	-703	-121	0	-183	7729	15.71	15.71	9.42	9.42	2	0.19	0.01	0.05	0.00	0.00	24.0
9	110	-17480	-622	171	0	218	7334	15.71	15.71	9.42	9.42	2	0.18	0.01	0.05	0.00	0.00	24.0
10	110	-17680	-519	-8	0	-29	6395	15.71	15.71	9.42	9.42	2	0.16	0.01	0.04	0.00	0.00	24.0
11	110	-17660	-494	80	0	92	6277	15.71	15.71	9.42	9.42	2	0.15	0.01	0.04	0.00	0.00	24.0
12	110	-17450	-759	-25	0	-50	8234	15.71	15.71	9.42	9.42	2	0.20	0.01	0.06	0.00	0.00	24.0
13	110	-17430	-734	62	0	70	8115	15.71	15.71	9.42	9.42	2	0.20	0.01	0.06	0.00	0.00	24.0
14	110	-17630	-631	-116	0	-177	7177	15.71	15.71	9.42	9.42	2	0.18	0.01	0.05	0.00	0.00	24.0
15	110	-17550	-550	176	0	225	6782	15.71	15.71	9.42	9.42	2	0.17	0.01	0.04	0.00	0.00	24.0
16	110	-17560	-703	-121	0	-183	7729	15.71	15.71	9.42	9.42	2	0.19	0.01	0.05	0.00	0.00	24.0
17	110	-17480	-622	171	0	218	7334	15.71	15.71	9.42	9.42	2	0.18	0.01	0.05	0.00	0.00	24.0
18	110	-33688	197	70	0	34	15177	15.71	15.71	9.42	9.42	3	0.25	0.00	0.01	0.00	0.00	24.0
19	110	-26108	-3252	-64	0	-109	18506	15.71	15.71	9.42	9.42	3	0.32	0.04	0.23	0.00	0.00	24.0
20	110	-28975	-1271	294	0	337	15552	15.71	15.71	9.42	9.42	3	0.27	0.02	0.09	0.00	0.00	24.0
37	110	-33958	1579	126	0	103	11657	15.71	15.71	9.42	9.42	3	0.20	0.02	0.10	0.00	0.00	24.0
38	110	-21328	-4168	-98	0	-135	17207	15.71	15.71	9.42	9.42	3	0.30	0.05	0.30	0.00	0.00	24.0
39	110	-26105	-868	499	0	608	12285	15.71	15.71	9.42	9.42	3	0.21	0.01	0.06	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	220	-21680	-814	36	0	-12	8537	15.71	15.71	9.42	9.42	3	0.15	0.01	0.06	0.00	0.00	24.0
2	220	-16800	-519	-8	0	-20	5825	15.71	15.71	9.42	9.42	2	0.14	0.01	0.04	0.00	0.00	24.0
3	220	-16780	-494	80	0	4	5734	15.71	15.71	9.42	9.42	2	0.14	0.01	0.04	0.00	0.00	24.0
4	220	-16570	-759	-25	0	-23	7399	15.71	15.71	9.42	9.42	2	0.18	0.01	0.06	0.00	0.00	24.0
5	220	-16550	-734	62	0	1	7307	15.71	15.71	9.42	9.42	2	0.18	0.01	0.06	0.00	0.00	24.0
6	220	-16750	-631	-116	0	-49	6482	15.71	15.71	9.42	9.42	2	0.16	0.01	0.05	0.00	0.00	24.0
7	220	-16670	-550	176	0	31	6178	15.71	15.71	9.42	9.42	2	0.15	0.01	0.04	0.00	0.00	24.0
8	220	-16680	-703	-121	0	-50	6955	15.71	15.71	9.42	9.42	2	0.17	0.01	0.05	0.00	0.00	24.0
9	220	-16600	-622	171	0	31	6650	15.71	15.71	9.42	9.42	2	0.16	0.01	0.05	0.00	0.00	24.0
10	220	-16800	-519	-8	0	-20	5825	15.71	15.71	9.42	9.42	2	0.14	0.01	0.04	0.00	0.00	24.0
11	220	-16780	-494	80	0	4	5734	15.71	15.71	9.42	9.42	2	0.14	0.01	0.04	0.00	0.00	24.0
12	220	-16570	-759	-25	0	-23	7399	15.71	15.71	9.42	9.42	2	0.18	0.01	0.06	0.00	0.00	24.0
13	220	-16550	-734	62	0	1	7307	15.71	15.71	9.42	9.42	2	0.18	0.01	0.06	0.00	0.00	24.0
14	220	-16750	-631	-116	0	-49	6482	15.71	15.71	9.42	9.42	2	0.16	0.01	0.05	0.00	0.00	24.0
15	220	-16670	-550	176	0	31	6178	15.71	15.71	9.42	9.42	2	0.15	0.01	0.04	0.00	0.00	24.0
16	220	-16680	-703	-121	0	-50	6955	15.71	15.71	9.42	9.42	2	0.17	0.01	0.05	0.00	0.00	24.0
17	220	-16600	-622	171	0	31	6650	15.71	15.71	9.42	9.42	2	0.16	0.01	0.05	0.00	0.00	24.0
18	220	-32545	-183	70	0	-43	15186	15.71	15.71	9.42	9.42	3	0.26	0.00	0.01	0.00	0.00	24.0
19	220	-24965	-2872	-64	0	-38	15140	15.71	15.71	9.42	9.42	3	0.26	0.04	0.20	0.00	0.00	24.0
20	220	-27830	-1271	294	0	14	14155	15.71	15.71	9.42	9.42	3	0.24	0.02	0.09	0.00	0.00	24.0
37	220	-32815	946	126	0	-35	13045	15.71	15.71	9.42	9.42	3	0.22	0.01	0.06	0.00	0.00	24.0
38	220	-20185	-3535	-98	0	-27	12972	15.71	15.71	9.42	9.42	3	0.23	0.04	0.26	0.00	0.00	24.0
39	220	-24960	-868	499	0	59	11330	15.71	15.71	9.42	9.42	3	0.20	0.01	0.06	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	330	-20535	-814	36	0	-51	7640	15.71	15.71	9.42	9.42	3	0.13	0.01	0.06	0.00	0.00	24.0
2	330	-15920	-519	-8	0	-12	5254	15.71	15.71	9.42	9.42	2	0.13	0.01	0.04	0.00	0.00	24.0
3	330	-15900	-494	80	0	-84	5190	15.71	15.71	9.42	9.42	2	0.13	0.01	0.04	0.00	0.00	24.0
4	330	-15690	-759	-25	0	5	6565	15.71	15.71	9.42	9.42	2	0.16	0.01	0.06	0.00	0.00	24.0
5	330	-15670	-734	62	0	-67	6500	15.71	15.71	9.42	9.42	2	0.16	0.01	0.06	0.00	0.00	24.0
6	330	-15870	-631	-116	0	78	5788	15.71	15.71	9.42	9.42	2	0.14	0.01	0.05	0.00	0.00	24.0
7	330	-15790	-550	176	0	-162	5573	15.71	15.71	9.42	9.42	2	0.14	0.01	0.04	0.00	0.00	24.0
8	330	-15800	-703	-121	0	83	6182	15.71	15.71	9.42	9.42	2	0.15	0.01	0.05	0.00	0.00	24.0
9	330	-15720	-622	171	0	-157	5966	15.71	15.71	9.42	9.42	2	0.15	0.01	0.05	0.00	0.00	24.0
10	330	-15920	-519	-8	0	-12	5254	15.71	15.71	9.42	9.42	2	0.13	0.01	0.04	0.00	0.00	24.0
11	330	-15900	-494	80	0	-84	5190	15.71	15.71	9.42	9.42	2	0.13	0.01	0.04	0.00	0.00	24.0
12	330	-15690	-759	-25	0	5	6565	15.71	15.71	9.42	9.42	2	0.16	0.01	0.06	0.00	0.00	24.0
13	330	-15670	-734	62	0	-67	6500	15.71	15.71	9.42	9.42	2	0.16	0.01	0.06	0.00	0.00	24.0
14	330	-15870	-631	-116	0	78	5788	15.71	15.71	9.42	9.42	2	0.14	0.01	0.05	0.00	0.00	24.0
15	330	-15790	-550	176	0	-162	5573	15.71	15.71	9.42	9.42	2	0.14	0.01	0.04	0.00	0.00	24.0
16	330	-15800	-703	-121	0	83	6182	15.71	15.71	9.42	9.42	2	0.15	0.01	0.05	0.00	0.00	24.0
17	330	-15720	-622	171	0	-157	5966	15.71	15.71	9.42	9.42	2	0.15	0.01	0.05	0.00	0.00	24.0
18	330	-31402	-563	70	0	-120	14777	15.71	15.71	9.42	9.42	3	0.25	0.01	0.04	0.00	0.00	24.0
19	330	-23822	-2491	-64	0	32	12192	15.71	15.71	9.42	9.42	3	0.21	0.03	0.18	0.00	0.00	24.0
20	330	-26685	-1271	294	0	-310	12758	15.71	15.71	9.42	9.42	3	0.22	0.02	0.09	0.00	0.00	24.0
37	330	-31672	312	126	0	-174	13736	15.71	15.71	9.42	9.42	3	0.23	0.00	0.02	0.00	0.00	24.0
38	330	-19042	-2901	-98	0	80	9433	15.71	15.71	9.42	9.42	3	0.17	0.04	0.22	0.00	0.00	24.0
39	330	-23815	-868	499	0	-489	10374	15.71	15.71	9.42	9.42	3	0.18	0.01	0.06	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	440	-19390	-814	36	0	-90	6744	15.71	15.71	9.42	9.42	3	0.12	0.01	0.06	0.00	0.00	24.0
2	440	-15040	-519	-8	0	-3	4684	15.71	15.71	9.42	9.42	2	0.12	0.01	0.04	0.00	0.00	24.0
3	440	-15020	-494	80	0	-171	4646	15.71	15.71	9.42	9.42	2	0.12	0.01	0.04	0.00	0.00	24.0
4	440	-14810	-759	-25	0	32	5730	15.71	15.71	9.42	9.42	2	0.14	0.01	0.06	0.00	0.00	24.0
5	440	-14790	-734	62	0	-136	5692	15.71	15.71	9.42	9.42	2	0.14	0.01	0.06	0.00	0.00	24.0
6	440	-14990	-631	-116	0	206	5094	15.71	15.71	9.42	9.42	2	0.13	0.01	0.05	0.00	0.00	24.0
7	440	-14910	-550	176	0	-356	4968	15.71	15.71	9.42	9.42	2	0.13	0.01	0.04	0.00	0.00	24.0
8	440	-14920	-703	-121	0	216	5408	15.71	15.71	9.42	9.42	2	0.14	0.01	0.06	0.00	0.00	24.0
9	440	-14840	-622	171	0	-345	5282	15.71	15.71	9.42	9.42	2	0.14	0.01	0.05	0.00	0.00	24.0
10	440	-15040	-519	-8	0	-3	4684	15.71	15.71	9.42	9.42	2	0.12	0.01	0.04	0.00	0.00	24.0
11	440	-15020	-494	80	0	-171	4646	15.71	15.71	9.42	9.42	2	0.12	0.01	0.04	0.00	0.00	24.0
12	440	-14810	-759	-25	0	32	5730	15.71	15.71	9.42	9.42	2	0.14	0.01	0.06	0.00	0.00	24.0
13	440	-14790	-734	62	0	-136	5692	15.71	15.71	9.42	9.42	2	0.14	0.01	0.06	0.00	0.00	24.0
14	440	-14990	-631	-116	0	206	5094	15.71	15.71	9.42	9.42	2	0.13	0.01	0.05	0.00	0.00	24.0
15	440	-14910	-550	176	0	-356	4968	15.71	15.71	9.42	9.42	2	0.13	0.01	0.04	0.00	0.00	24.0
16	440	-14920	-703	-121	0	216	5408	15.71	15.71	9.42	9.42	2	0.14	0.01	0.06	0.00	0.00	24.0
17	440	-14840	-622	171	0	-345	5282	15.71	15.71	9.42	9.42	2	0.14	0.01	0.05	0.00	0.00	24.0
18	440	-30260	-943	70	0	-197	13950	15.71	15.71	9.42	9.42	3	0.24	0.01	0.06	0.00	0.00	24.0
19	440	-22680	-2111	-64	0	102	9662	15.71	15.71	9.42	9.42	3	0.17	0.03	0.15	0.00	0.00	24.0
20	440	-25540	-1271	294	0	-633	11360	15.71	15.71	9.42	9.42	3	0.20	0.02	0.09	0.00	0.00	24.0
37	440	-30530	-321	126	0	-312	13730	15.71	15.71	9.42	9.42	3	0.23	0.00	0.02	0.00	0.00	24.0
38	440	-17900	-2267	-98	0	188	6591	15.71	15.71	9.42	9.42	3	0.12	0.03	0.17	0.00	0.00	24.0
39	440	-22670	-868	499	0	-1038	9419	15.71	15.71	9.42	9.42	3	0.17	0.01	0.06	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 25 NI 121 NF 120 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 5B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-25740	-1465	-53	0	-142	16830	15.71	15.71	9.42	9.42	3	0.29	0.02	0.10	0.00	0.00	24.0
2	0	-19760	-872	-78	0	-206	10560	15.71	15.71	9.42	9.42	2	0.26	0.01	0.06	0.00	0.00	24.0
3	0	-19800	-867	7	0	9	10580	15.71	15.71	9.42	9.42	2	0.25	0.01	0.06	0.00	0.00	24.0
4	0	-19800	-1387	-88	0	-229	15320	15.71	15.71	9.42	9.42	2	0.37	0.02	0.10	0.00	0.00	24.0
5	0	-19830	-1382	-3	0	-14	15330	15.71	15.71	9.42	9.42	2	0.37	0.02	0.10	0.00	0.00	24.0
6	0	-19730	-1058	-180	0	-465	12210	15.71	15.71	9.42	9.42	2	0.30	0.01	0.08	0.00	0.00	24.0
7	0	-19860	-1042	102	0	252	12260	15.71	15.71	9.42	9.42	2	0.30	0.01	0.08	0.00	0.00	24.0
8	0	-19740	-1212	-183	0	-472	13640	15.71	15.71	9.42	9.42	2	0.34	0.02	0.09	0.00	0.00	24.0
9	0	-19870	-1196	99	0	245	13680	15.71	15.71	9.42	9.42	2	0.33	0.02	0.09	0.00	0.00	24.0
10	0	-19760	-872	-78	0	-206	10560	15.71	15.71	9.42	9.42	2	0.26	0.01	0.06	0.00	0.00	24.0
11	0	-19800	-867	7	0	9	10580	15.71	15.71	9.42	9.42	2	0.25	0.01	0.06	0.00	0.00	24.0
12	0	-19800	-1387	-88	0	-229	15320	15.71	15.71	9.42	9.42	2	0.37	0.02	0.10	0.00	0.00	24.0
13	0	-19830	-1382	-3	0	-14	15330	15.71	15.71	9.42	9.42	2	0.37	0.02	0.10	0.00	0.00	24.0
14	0	-19730	-1058	-180	0	-465	12210	15.71	15.71	9.42	9.42	2	0.30	0.01	0.08	0.00	0.00	24.0
15	0	-19860	-1042	102	0	252	12260	15.71	15.71	9.42	9.42	2	0.30	0.01	0.08	0.00	0.00	24.0
16	0	-19740	-1212	-183	0	-472	13640	15.71	15.71	9.42	9.42	2	0.34	0.02	0.09	0.00	0.00	24.0
17	0	-19870	-1196	99	0	245	13680	15.71	15.71	9.42	9.42	2	0.33	0.02	0.09	0.00	0.00	24.0
18	0	-37980	-389	-98	0	-279	24230	15.71	15.71	9.42	9.42	3	0.40	0.00	0.02	0.00	0.00	24.0
19	0	-30730	-5350	-137	0	-354	38370	15.71	15.71	9.42	9.42	3	0.65	0.07	0.36	0.00	0.00	24.0
20	0	-33070	-2663	181	0	389	29180	15.71	15.71	9.42	9.42	3	0.49	0.03	0.17	0.00	0.00	24.0
37	0	-37650	1723	-63	0	-196	14810	15.71	15.71	9.42	9.42	3	0.25	0.02	0.11	0.00	0.00	24.0
38	0	-25560	-6546	-128	0	-321	38390	15.71	15.71	9.42	9.42	3	0.66	0.08	0.46	0.00	0.00	24.0
39	0	-29460	-2067	402	0	918	23070	15.71	15.71	9.42	9.42	3	0.40	0.03	0.14	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	110	-24595	-1465	-53	0	-85	15220	15.71	15.71	9.42	9.42	3	0.26	0.02	0.10	0.00	0.00	24.0
2	110	-18880	-872	-78	0	-120	9602	15.71	15.71	9.42	9.42	2	0.23	0.01	0.07	0.00	0.00	24.0
3	110	-18920	-867	7	0	2	9625	15.71	15.71	9.42	9.42	2	0.23	0.01	0.07	0.00	0.00	24.0
4	110	-18920	-1387	-88	0	-132	13795	15.71	15.71	9.42	9.42	2	0.33	0.02	0.10	0.00	0.00	24.0
5	110	-18950	-1382	-3	0	-10	13811	15.71	15.71	9.42	9.42	2	0.33	0.02	0.10	0.00	0.00	24.0
6	110	-18850	-1058	-180	0	-267	11047	15.71	15.71	9.42	9.42	2	0.27	0.01	0.08	0.00	0.00	24.0
7	110	-18980	-1042	102	0	140	11113	15.71	15.71	9.42	9.42	2	0.27	0.01	0.08	0.00	0.00	24.0
8	110	-18860	-1212	-183	0	-270	12307	15.71	15.71	9.42	9.42	2	0.30	0.02	0.09	0.00	0.00	24.0
9	110	-18990	-1196	99	0	137	12365	15.71	15.71	9.42	9.42	2	0.30	0.02	0.09	0.00	0.00	24.0
10	110	-18880	-872	-78	0	-120	9602	15.71	15.71	9.42	9.42	2	0.23	0.01	0.07	0.00	0.00	24.0
11	110	-18920	-867	7	0	2	9625	15.71	15.71	9.42	9.42	2	0.23	0.01	0.07	0.00	0.00	24.0
12	110	-18920	-1387	-88	0	-132	13795	15.71	15.71	9.42	9.42	2	0.33	0.02	0.10	0.00	0.00	24.0
13	110	-18950	-1382	-3	0	-10	13811	15.71	15.71	9.42	9.42	2	0.33	0.02	0.10	0.00	0.00	24.0
14	110	-18850	-1058	-180	0	-267	11047	15.71	15.71	9.42	9.42	2	0.27	0.01	0.08	0.00	0.00	24.0
15	110	-18980	-1042	102	0	140	11113	15.71	15.71	9.42	9.42	2	0.27	0.01	0.08	0.00	0.00	24.0
16	110	-18860	-1212	-183	0	-270	12307	15.71	15.71	9.42	9.42	2	0.30	0.02	0.09	0.00	0.00	24.0
17	110	-18990	-1196	99	0	137	12365	15.71	15.71	9.42	9.42	2	0.30	0.02	0.09	0.00	0.00	24.0
18	110	-36838	-769	-98	0	-172	23592	15.71	15.71	9.42	9.42	3	0.39	0.01	0.05	0.00	0.00	24.0
19	110	-29588	-4970	-137	0	-203	32695	15.71	15.71	9.42	9.42	3	0.56	0.06	0.34	0.00	0.00	24.0
20	110	-31925	-2663	181	0	190	26252	15.71	15.71	9.42	9.42	3	0.44	0.03	0.18	0.00	0.00	24.0
37	110	-36505	1089	-63	0	-127	16355	15.71	15.71	9.42	9.42	3	0.27	0.01	0.07	0.00	0.00	24.0
38	110	-24415	-5912	-128	0	-180	31537	15.71	15.71	9.42	9.42	3	0.55	0.07	0.42	0.00	0.00	24.0
39	110	-28315	-2067	402	0	476	20795	15.71	15.71	9.42	9.42	3	0.36	0.03	0.14	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	220	-23450	-1465	-53	0	-27	13610	15.71	15.71	9.42	9.42	3	0.24	0.02	0.10	0.00	0.00	24.0
2	220	-18000	-872	-78	0	-35	8643	15.71	15.71	9.42	9.42	2	0.21	0.01	0.07	0.00	0.00	24.0
3	220	-18040	-867	7	0	-6	8670	15.71	15.71	9.42	9.42	2	0.21	0.01	0.07	0.00	0.00	24.0
4	220	-18040	-1387	-88	0	-35	12270	15.71	15.71	9.42	9.42	2	0.30	0.02	0.11	0.00	0.00	24.0
5	220	-18070	-1382	-3	0	-6	12291	15.71	15.71	9.42	9.42	2	0.30	0.02	0.10	0.00	0.00	24.0
6	220	-17970	-1058	-180	0	-69	9885	15.71	15.71	9.42	9.42	2	0.24	0.01	0.08	0.00	0.00	24.0
7	220	-18100	-1042	102	0	28	9966	15.71	15.71	9.42	9.42	2	0.24	0.01	0.08	0.00	0.00	24.0
8	220	-17980	-1212	-183	0	-69	10974	15.71	15.71	9.42	9.42	2	0.27	0.02	0.09	0.00	0.00	24.0
9	220	-18110	-1196	99	0	28	11050	15.71	15.71	9.42	9.42	2	0.27	0.02	0.09	0.00	0.00	24.0
10	220	-18000	-872	-78	0	-35	8643	15.71	15.71	9.42	9.42	2	0.21	0.01	0.07	0.00	0.00	24.0
11	220	-18040	-867	7	0	-6	8670	15.71	15.71	9.42	9.42	2	0.21	0.01	0.07	0.00	0.00	24.0
12	220	-18040	-1387	-88	0	-35	12270	15.71	15.71	9.42	9.42	2	0.30	0.02	0.11	0.00	0.00	24.0
13	220	-18070	-1382	-3	0	-6	12291	15.71	15.71	9.42	9.42	2	0.30	0.02	0.10	0.00	0.00	24.0
14	220	-17970	-1058	-180	0	-69	9885	15.71	15.71	9.42	9.42	2	0.24	0.01	0.08	0.00	0.00	24.0
15	220	-18100	-1042	102	0	28	9966	15.71	15.71	9.42	9.42	2	0.24	0.01	0.08	0.00	0.00	24.0
16	220	-17980	-1212	-183	0	-69	10974	15.71	15.71	9.42	9.42	2	0.27	0.02	0.09	0.00	0.00	24.0
17	220	-18110	-1196	99	0	28	11050	15.71	15.71	9.42	9.42	2	0.27	0.02	0.09	0.00	0.00	24.0
18	220	-35695	-1150	-98	0	-64	22536	15.71	15.71	9.42	9.42	3	0.37	0.01	0.07	0.00	0.00	24.0
19	220	-28445	-4590	-137	0	-53	27439	15.71	15.71	9.42	9.42	3	0.47	0.06	0.31	0.00	0.00	24.0
20	220	-30780	-2663	181	0	-9	23325	15.71	15.71	9.42	9.42	3	0.40	0.03	0.18	0.00	0.00	24.0
37	220	-35360	456	-63	0	-58	17204	15.71	15.71	9.42	9.42	3	0.29	0.01	0.03	0.00	0.00	24.0
38	220	-23270	-5279	-128	0	-38	25381	15.71	15.71	9.42	9.42	3	0.44	0.07	0.38	0.00	0.00	24.0
39	220	-27170	-2067	402	0	34	18520	15.71	15.71	9.42	9.42	3	0.32	0.03	0.14	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	330	-22305	-1465	-53	0	31	12000	15.71	15.71	9.42	9.42	3	0.21	0.02	0.11	0.00	0.00	24.0
2	330	-17120	-872	-78	0	51	7684	15.71	15.71	9.42	9.42	2	0.19	0.01	0.07	0.00	0.00	24.0
3	330	-17160	-867	7	0	-13	7716	15.71	15.71	9.42	9.42	2	0.19	0.01	0.07	0.00	0.00	24.0
4	330	-17160	-1387	-88	0	61	10744	15.71	15.71	9.42	9.42	2	0.26	0.02	0.11	0.00	0.00	24.0
5	330	-17190	-1382	-3	0	-3	10772	15.71	15.71	9.42	9.42	2	0.26	0.02	0.11	0.00	0.00	24.0
6	330	-17090	-1058	-180	0	129	8722	15.71	15.71	9.42	9.42	2	0.22	0.01	0.08	0.00	0.00	24.0
7	330	-17220	-1042	102	0	-84	8820	15.71	15.71	9.42	9.42	2	0.22	0.01	0.08	0.00	0.00	24.0
8	330	-17100	-1212	-183	0	132	9640	15.71	15.71	9.42	9.42	2	0.24	0.02	0.09	0.00	0.00	24.0
9	330	-17230	-1196	99	0	-81	9736	15.71	15.71	9.42	9.42	2	0.24	0.02	0.09	0.00	0.00	24.0
10	330	-17120	-872	-78	0	51	7684	15.71	15.71	9.42	9.42	2	0.19	0.01	0.07	0.00	0.00	24.0
11	330	-17160	-867	7	0	-13	7716	15.71	15.71	9.42	9.42	2	0.19	0.01	0.07	0.00	0.00	24.0
12	330	-17160	-1387	-88	0	61	10744	15.71	15.71	9.42	9.42	2	0.26	0.02	0.11	0.00	0.00	24.0
13	330	-17190	-1382	-3	0	-3	10772	15.71	15.71	9.42	9.42	2	0.26	0.02	0.11	0.00	0.00	24.0
14	330	-17090	-1058	-180	0	129	8722	15.71	15.71	9.42	9.42	2	0.22	0.01	0.08	0.00	0.00	24.0
15	330	-17220	-1042	102	0	-84	8820	15.71	15.71	9.42	9.42	2	0.22	0.01	0.08	0.00	0.00	24.0
16	330	-17100	-1212	-183	0	132	9640	15.71	15.71	9.42	9.42	2	0.24	0.02	0.09	0.00	0.00	24.0
17	330	-17230	-1196	99	0	-81	9736	15.71	15.71	9.42	9.42	2	0.24	0.02	0.09	0.00	0.00	24.0
18	330	-34552	-1530	-98	0	43	21062	15.71	15.71	9.42	9.42	3	0.35	0.02	0.10	0.00	0.00	24.0
19	330	-27302	-4210	-137	0	98	22600	15.71	15.71	9.42	9.42	3	0.39	0.05	0.29	0.00	0.00	24.0
20	330	-29635	-2663	181	0	-209	20397	15.71	15.71	9.42	9.42	3	0.35	0.03	0.18	0.00	0.00	24.0
37	330	-34215	-178	-63	0	12	17355	15.71	15.71	9.42	9.42	3	0.29	0.00	0.01	0.00	0.00	24.0
38	330	-22125	-4646	-128	0	103	19922	15.71	15.71	9.42	9.42	3	0.35	0.06	0.34	0.00	0.00	24.0
39	330	-26025	-2067	402	0	-408	16245	15.71	15.71	9.42	9.42	3	0.28	0.03	0.14	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	440	-21160	-1465	-53	0	89	10390	15.71	15.71	9.42	9.42	3	0.18	0.02	0.11	0.00	0.00	24.0
2	440	-16240	-872	-78	0	136	6726	15.71	15.71	9.42	9.42	2	0.17	0.01	0.07	0.00	0.00	24.0
3	440	-16280	-867	7	0	-21	6761	15.71	15.71	9.42	9.42	2	0.17	0.01	0.07	0.00	0.00	24.0
4	440	-16280	-1387	-88	0	158	9219	15.71	15.71	9.42	9.42	2	0.23	0.02	0.11	0.00	0.00	24.0
5	440	-16310	-1382	-3	0	1	9253	15.71	15.71	9.42	9.42	2	0.23	0.02	0.11	0.00	0.00	24.0
6	440	-16210	-1058	-180	0	327	7559	15.71	15.71	9.42	9.42	2	0.19	0.01	0.08	0.00	0.00	24.0
7	440	-16340	-1042	102	0	-197	7673	15.71	15.71	9.42	9.42	2	0.19	0.01	0.08	0.00	0.00	24.0
8	440	-16220	-1212	-183	0	333	8307	15.71	15.71	9.42	9.42	2	0.21	0.02	0.09	0.00	0.00	24.0
9	440	-16350	-1196	99	0	-190	8421	15.71	15.71	9.42	9.42	2	0.21	0.02	0.09	0.00	0.00	24.0
10	440	-16240	-872	-78	0	136	6726	15.71	15.71	9.42	9.42	2	0.17	0.01	0.07	0.00	0.00	24.0
11	440	-16280	-867	7	0	-21	6761	15.71	15.71	9.42	9.42	2	0.17	0.01	0.07	0.00	0.00	24.0
12	440	-16280	-1387	-88	0	158	9219	15.71	15.71	9.42	9.42	2	0.23	0.02	0.11	0.00	0.00	24.0
13	440	-16310	-1382	-3	0	1	9253	15.71	15.71	9.42	9.42	2	0.23	0.02	0.11	0.00	0.00	24.0
14	440	-16210	-1058	-180	0	327	7559	15.71	15.71	9.42	9.42	2	0.19	0.01	0.08	0.00	0.00	24.0
15	440	-16340	-1042	102	0	-197	7673	15.71	15.71	9.42	9.42	2	0.19	0.01	0.08	0.00	0.00	24.0
16	440	-16220	-1212	-183	0	333	8307	15.71	15.71	9.42	9.42	2	0.21	0.02	0.09	0.00	0.00	24.0
17	440	-16350	-1196	99	0	-190	8421	15.71	15.71	9.42	9.42	2	0.21	0.02	0.09	0.00	0.00	24.0
18	440	-33410	-1910	-98	0	151	19170	15.71	15.71	9.42	9.42	3	0.32	0.02	0.12	0.00	0.00	24.0
19	440	-26160	-3830	-137	0	248	18180	15.71	15.71	9.42	9.42	3	0.31	0.05	0.27	0.00	0.00	24.0
20	440	-28490	-2663	181	0	-408	17470	15.71	15.71	9.42	9.42	3	0.30	0.03	0.18	0.00	0.00	24.0
37	440	-33070	-812	-63	0	81	16810	15.71	15.71	9.42	9.42	3	0.28	0.01	0.05	0.00	0.00	24.0
38	440	-20980	-4012	-128	0	244	15160	15.71	15.71	9.42	9.42	3	0.27	0.05	0.29	0.00	0.00	24.0
39	440	-24880	-2067	402	0	-850	13970	15.71	15.71	9.42	9.42	3	0.25	0.03	0.15	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 26 NI 164 NF 163 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 4B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-25890	-1674	-65	0	-178	18350	15.71	15.71	9.42	9.42	3	0.32	0.02	0.12	0.00	0.00	24.0
2	0	-19950	-980	-89	0	-236	11460	15.71	15.71	9.42	9.42	2	0.28	0.01	0.07	0.00	0.00	24.0
3	0	-19920	-974	-6	0	-24	11370	15.71	15.71	9.42	9.42	2	0.27	0.01	0.07	0.00	0.00	24.0
4	0	-19910	-1602	-94	0	-250	16860	15.71	15.71	9.42	9.42	2	0.41	0.02	0.12	0.00	0.00	24.0
5	0	-19880	-1596	-12	0	-38	16770	15.71	15.71	9.42	9.42	2	0.40	0.02	0.12	0.00	0.00	24.0
6	0	-19980	-1205	-187	0	-488	13460	15.71	15.71	9.42	9.42	2	0.33	0.02	0.09	0.00	0.00	24.0
7	0	-19870	-1184	88	0	218	13150	15.71	15.71	9.42	9.42	2	0.32	0.01	0.09	0.00	0.00	24.0
8	0	-19960	-1392	-189	0	-493	15080	15.71	15.71	9.42	9.42	2	0.37	0.02	0.10	0.00	0.00	24.0
9	0	-19860	-1371	86	0	214	14770	15.71	15.71	9.42	9.42	2	0.36	0.02	0.10	0.00	0.00	24.0
10	0	-19950	-980	-89	0	-236	11460	15.71	15.71	9.42	9.42	2	0.28	0.01	0.07	0.00	0.00	24.0
11	0	-19920	-974	-6	0	-24	11370	15.71	15.71	9.42	9.42	2	0.27	0.01	0.07	0.00	0.00	24.0
12	0	-19910	-1602	-94	0	-250	16860	15.71	15.71	9.42	9.42	2	0.41	0.02	0.12	0.00	0.00	24.0
13	0	-19880	-1596	-12	0	-38	16770	15.71	15.71	9.42	9.42	2	0.40	0.02	0.12	0.00	0.00	24.0
14	0	-19980	-1205	-187	0	-488	13460	15.71	15.71	9.42	9.42	2	0.33	0.02	0.09	0.00	0.00	24.0
15	0	-19870	-1184	88	0	218	13150	15.71	15.71	9.42	9.42	2	0.32	0.01	0.09	0.00	0.00	24.0
16	0	-19960	-1392	-189	0	-493	15080	15.71	15.71	9.42	9.42	2	0.37	0.02	0.10	0.00	0.00	24.0
17	0	-19860	-1371	86	0	214	14770	15.71	15.71	9.42	9.42	2	0.36	0.02	0.10	0.00	0.00	24.0
18	0	-38400	-663	-110	0	-327	26390	15.71	15.71	9.42	9.42	3	0.44	0.01	0.04	0.00	0.00	24.0
19	0	-30870	-5896	-134	0	-363	42120	15.71	15.71	9.42	9.42	3	0.71	0.07	0.39	0.00	0.00	24.0
20	0	-33200	-3022	145	0	295	31640	15.71	15.71	9.42	9.42	3	0.53	0.04	0.20	0.00	0.00	24.0
37	0	-38110	1604	-83	0	-260	15980	15.71	15.71	9.42	9.42	3	0.26	0.02	0.10	0.00	0.00	24.0
38	0	-25570	-7117	-123	0	-319	42190	15.71	15.71	9.42	9.42	3	0.73	0.09	0.50	0.00	0.00	24.0
39	0	-29450	-2327	341	0	778	24720	15.71	15.71	9.42	9.42	3	0.42	0.03	0.16	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	110	-24748	-1674	-65	0	-106	16508	15.71	15.71	9.42	9.42	3	0.29	0.02	0.12	0.00	0.00	24.0
2	110	-19070	-980	-89	0	-139	10382	15.71	15.71	9.42	9.42	2	0.25	0.01	0.07	0.00	0.00	24.0
3	110	-19040	-974	-6	0	-17	10298	15.71	15.71	9.42	9.42	2	0.25	0.01	0.07	0.00	0.00	24.0
4	110	-19030	-1602	-94	0	-146	15099	15.71	15.71	9.42	9.42	2	0.37	0.02	0.12	0.00	0.00	24.0
5	110	-19000	-1596	-12	0	-25	15015	15.71	15.71	9.42	9.42	2	0.36	0.02	0.12	0.00	0.00	24.0
6	110	-19100	-1205	-187	0	-283	12135	15.71	15.71	9.42	9.42	2	0.30	0.02	0.09	0.00	0.00	24.0
7	110	-18990	-1184	88	0	122	11847	15.71	15.71	9.42	9.42	2	0.29	0.01	0.09	0.00	0.00	24.0
8	110	-19080	-1392	-189	0	-285	13550	15.71	15.71	9.42	9.42	2	0.33	0.02	0.10	0.00	0.00	24.0
9	110	-18980	-1371	86	0	119	13263	15.71	15.71	9.42	9.42	2	0.32	0.02	0.10	0.00	0.00	24.0
10	110	-19070	-980	-89	0	-139	10382	15.71	15.71	9.42	9.42	2	0.25	0.01	0.07	0.00	0.00	24.0
11	110	-19040	-974	-6	0	-17	10298	15.71	15.71	9.42	9.42	2	0.25	0.01	0.07	0.00	0.00	24.0
12	110	-19030	-1602	-94	0	-146	15099	15.71	15.71	9.42	9.42	2	0.37	0.02	0.12	0.00	0.00	24.0
13	110	-19000	-1596	-12	0	-25	15015	15.71	15.71	9.42	9.42	2	0.36	0.02	0.12	0.00	0.00	24.0
14	110	-19100	-1205	-187	0	-283	12135	15.71	15.71	9.42	9.42	2	0.30	0.02	0.09	0.00	0.00	24.0
15	110	-18990	-1184	88	0	122	11847	15.71	15.71	9.42	9.42	2	0.29	0.01	0.09	0.00	0.00	24.0
16	110	-19080	-1392	-189	0	-285	13550	15.71	15.71	9.42	9.42	2	0.33	0.02	0.10	0.00	0.00	24.0
17	110	-18980	-1371	86	0	119	13263	15.71	15.71	9.42	9.42	2	0.32	0.02	0.10	0.00	0.00	24.0
18	110	-37255	-1043	-110	0	-206	25452	15.71	15.71	9.42	9.42	3	0.42	0.01	0.07	0.00	0.00	24.0
19	110	-29728	-5516	-134	0	-216	35845	15.71	15.71	9.42	9.42	3	0.61	0.07	0.37	0.00	0.00	24.0
20	110	-32058	-3022	145	0	136	28315	15.71	15.71	9.42	9.42	3	0.48	0.04	0.20	0.00	0.00	24.0
37	110	-36968	970	-83	0	-168	17395	15.71	15.71	9.42	9.42	3	0.29	0.01	0.06	0.00	0.00	24.0
38	110	-24425	-6484	-123	0	-184	34710	15.71	15.71	9.42	9.42	3	0.60	0.08	0.46	0.00	0.00	24.0
39	110	-28308	-2327	341	0	403	22160	15.71	15.71	9.42	9.42	3	0.38	0.03	0.16	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	220	-23605	-1674	-65	0	-34	14665	15.71	15.71	9.42	9.42	3	0.26	0.02	0.12	0.00	0.00	24.0
2	220	-18190	-980	-89	0	-41	9304	15.71	15.71	9.42	9.42	2	0.23	0.01	0.07	0.00	0.00	24.0
3	220	-18160	-974	-6	0	-10	9226	15.71	15.71	9.42	9.42	2	0.22	0.01	0.07	0.00	0.00	24.0
4	220	-18150	-1602	-94	0	-42	13338	15.71	15.71	9.42	9.42	2	0.32	0.02	0.12	0.00	0.00	24.0
5	220	-18120	-1596	-12	0	-12	13260	15.71	15.71	9.42	9.42	2	0.32	0.02	0.12	0.00	0.00	24.0
6	220	-18220	-1205	-187	0	-77	10809	15.71	15.71	9.42	9.42	2	0.26	0.02	0.09	0.00	0.00	24.0
7	220	-18110	-1184	88	0	25	10545	15.71	15.71	9.42	9.42	2	0.26	0.01	0.09	0.00	0.00	24.0
8	220	-18200	-1392	-189	0	-78	12020	15.71	15.71	9.42	9.42	2	0.29	0.02	0.11	0.00	0.00	24.0
9	220	-18100	-1371	86	0	25	11755	15.71	15.71	9.42	9.42	2	0.28	0.02	0.10	0.00	0.00	24.0
10	220	-18190	-980	-89	0	-41	9304	15.71	15.71	9.42	9.42	2	0.23	0.01	0.07	0.00	0.00	24.0
11	220	-18160	-974	-6	0	-10	9226	15.71	15.71	9.42	9.42	2	0.22	0.01	0.07	0.00	0.00	24.0
12	220	-18150	-1602	-94	0	-42	13338	15.71	15.71	9.42	9.42	2	0.32	0.02	0.12	0.00	0.00	24.0
13	220	-18120	-1596	-12	0	-12	13260	15.71	15.71	9.42	9.42	2	0.32	0.02	0.12	0.00	0.00	24.0
14	220	-18220	-1205	-187	0	-77	10809	15.71	15.71	9.42	9.42	2	0.26	0.02	0.09	0.00	0.00	24.0
15	220	-18110	-1184	88	0	25	10545	15.71	15.71	9.42	9.42	2	0.26	0.01	0.09	0.00	0.00	24.0
16	220	-18200	-1392	-189	0	-78	12020	15.71	15.71	9.42	9.42	2	0.29	0.02	0.11	0.00	0.00	24.0
17	220	-18100	-1371	86	0	25	11755	15.71	15.71	9.42	9.42	2	0.28	0.02	0.10	0.00	0.00	24.0
18	220	-36110	-1424	-110	0	-85	24096	15.71	15.71	9.42	9.42	3	0.40	0.02	0.09	0.00	0.00	24.0
19	220	-28585	-5136	-134	0	-69	29989	15.71	15.71	9.42	9.42	3	0.51	0.06	0.35	0.00	0.00	24.0
20	220	-30915	-3022	145	0	-23	24990	15.71	15.71	9.42	9.42	3	0.42	0.04	0.20	0.00	0.00	24.0
37	220	-35825	337	-83	0	-76	18114	15.71	15.71	9.42	9.42	3	0.30	0.00	0.02	0.00	0.00	24.0

38	220	-23280	-5850	-123	0	-49	27926	15.71	15.71	9.42	9.42	3	0.49	0.07	0.42	0.00	0.00	24.0
39	220	-27165	-2327	341	0	27	19600	15.71	15.71	9.42	9.42	3	0.34	0.03	0.16	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	330	-22462	-1674	-65	0	38	12822	15.71	15.71	9.42	9.42	3	0.22	0.02	0.12	0.00	0.00	24.0
2	330	-17310	-980	-89	0	57	8227	15.71	15.71	9.42	9.42	2	0.20	0.01	0.07	0.00	0.00	24.0
3	330	-17280	-974	-6	0	-3	8155	15.71	15.71	9.42	9.42	2	0.20	0.01	0.07	0.00	0.00	24.0
4	330	-17270	-1602	-94	0	62	11577	15.71	15.71	9.42	9.42	2	0.28	0.02	0.12	0.00	0.00	24.0
5	330	-17240	-1596	-12	0	2	11505	15.71	15.71	9.42	9.42	2	0.28	0.02	0.12	0.00	0.00	24.0
6	330	-17340	-1205	-187	0	128	9484	15.71	15.71	9.42	9.42	2	0.23	0.02	0.09	0.00	0.00	24.0
7	330	-17230	-1184	88	0	-72	9242	15.71	15.71	9.42	9.42	2	0.23	0.01	0.09	0.00	0.00	24.0
8	330	-17320	-1392	-189	0	130	10490	15.71	15.71	9.42	9.42	2	0.26	0.02	0.11	0.00	0.00	24.0
9	330	-17220	-1371	86	0	-70	10247	15.71	15.71	9.42	9.42	2	0.25	0.02	0.10	0.00	0.00	24.0
10	330	-17310	-980	-89	0	57	8227	15.71	15.71	9.42	9.42	2	0.20	0.01	0.07	0.00	0.00	24.0
11	330	-17280	-974	-6	0	-3	8155	15.71	15.71	9.42	9.42	2	0.20	0.01	0.07	0.00	0.00	24.0
12	330	-17270	-1602	-94	0	62	11577	15.71	15.71	9.42	9.42	2	0.28	0.02	0.12	0.00	0.00	24.0
13	330	-17240	-1596	-12	0	2	11505	15.71	15.71	9.42	9.42	2	0.28	0.02	0.12	0.00	0.00	24.0
14	330	-17340	-1205	-187	0	128	9484	15.71	15.71	9.42	9.42	2	0.23	0.02	0.09	0.00	0.00	24.0
15	330	-17230	-1184	88	0	-72	9242	15.71	15.71	9.42	9.42	2	0.23	0.01	0.09	0.00	0.00	24.0
16	330	-17320	-1392	-189	0	130	10490	15.71	15.71	9.42	9.42	2	0.26	0.02	0.11	0.00	0.00	24.0
17	330	-17220	-1371	86	0	-70	10247	15.71	15.71	9.42	9.42	2	0.25	0.02	0.10	0.00	0.00	24.0
18	330	-34965	-1804	-110	0	36	22322	15.71	15.71	9.42	9.42	3	0.37	0.02	0.12	0.00	0.00	24.0
19	330	-27442	-4756	-134	0	78	24550	15.71	15.71	9.42	9.42	3	0.42	0.06	0.33	0.00	0.00	24.0
20	330	-29772	-3022	145	0	-182	21665	15.71	15.71	9.42	9.42	3	0.37	0.04	0.20	0.00	0.00	24.0
37	330	-34682	-297	-83	0	16	18135	15.71	15.71	9.42	9.42	3	0.30	0.00	0.02	0.00	0.00	24.0
38	330	-22135	-5216	-123	0	86	21840	15.71	15.71	9.42	9.42	3	0.38	0.07	0.38	0.00	0.00	24.0
39	330	-26022	-2327	341	0	-348	17040	15.71	15.71	9.42	9.42	3	0.30	0.03	0.16	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	440	-21320	-1674	-65	0	110	10980	15.71	15.71	9.42	9.42	3	0.19	0.02	0.12	0.00	0.00	24.0
2	440	-16430	-980	-89	0	154	7149	15.71	15.71	9.42	9.42	2	0.18	0.01	0.08	0.00	0.00	24.0
3	440	-16400	-974	-6	0	4	7083	15.71	15.71	9.42	9.42	2	0.17	0.01	0.08	0.00	0.00	24.0
4	440	-16390	-1602	-94	0	165	9816	15.71	15.71	9.42	9.42	2	0.24	0.02	0.12	0.00	0.00	24.0
5	440	-16360	-1596	-12	0	15	9750	15.71	15.71	9.42	9.42	2	0.24	0.02	0.12	0.00	0.00	24.0
6	440	-16460	-1205	-187	0	334	8159	15.71	15.71	9.42	9.42	2	0.21	0.02	0.09	0.00	0.00	24.0
7	440	-16350	-1184	88	0	-168	7939	15.71	15.71	9.42	9.42	2	0.20	0.01	0.09	0.00	0.00	24.0
8	440	-16440	-1392	-189	0	337	8960	15.71	15.71	9.42	9.42	2	0.23	0.02	0.11	0.00	0.00	24.0
9	440	-16340	-1371	86	0	-165	8740	15.71	15.71	9.42	9.42	2	0.22	0.02	0.11	0.00	0.00	24.0
10	440	-16430	-980	-89	0	154	7149	15.71	15.71	9.42	9.42	2	0.18	0.01	0.08	0.00	0.00	24.0
11	440	-16400	-974	-6	0	4	7083	15.71	15.71	9.42	9.42	2	0.17	0.01	0.08	0.00	0.00	24.0
12	440	-16390	-1602	-94	0	165	9816	15.71	15.71	9.42	9.42	2	0.24	0.02	0.12	0.00	0.00	24.0
13	440	-16360	-1596	-12	0	15	9750	15.71	15.71	9.42	9.42	2	0.24	0.02	0.12	0.00	0.00	24.0
14	440	-16460	-1205	-187	0	334	8159	15.71	15.71	9.42	9.42	2	0.21	0.02	0.09	0.00	0.00	24.0
15	440	-16350	-1184	88	0	-168	7939	15.71	15.71	9.42	9.42	2	0.20	0.01	0.09	0.00	0.00	24.0
16	440	-16440	-1392	-189	0	337	8960	15.71	15.71	9.42	9.42	2	0.23	0.02	0.11	0.00	0.00	24.0
17	440	-16340	-1371	86	0	-165	8740	15.71	15.71	9.42	9.42	2	0.22	0.02	0.11	0.00	0.00	24.0
18	440	-33820	-2184	-110	0	157	20130	15.71	15.71	9.42	9.42	3	0.34	0.03	0.14	0.00	0.00	24.0
19	440	-26300	-4376	-134	0	225	19530	15.71	15.71	9.42	9.42	3	0.34	0.05	0.30	0.00	0.00	24.0
20	440	-28630	-3022	145	0	-341	18340	15.71	15.71	9.42	9.42	3	0.31	0.04	0.21	0.00	0.00	24.0
37	440	-33540	-930	-83	0	107	17460	15.71	15.71	9.42	9.42	3	0.29	0.01	0.06	0.00	0.00	24.0
38	440	-20990	-4583	-123	0	221	16450	15.71	15.71	9.42	9.42	3	0.29	0.06	0.34	0.00	0.00	24.0
39	440	-24880	-2327	341	0	-724	14480	15.71	15.71	9.42	9.42	3	0.25	0.03	0.16	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 27 NI 207 NF 206 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 3B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-25550	-1476	-79	0	-200	16740	15.71	15.71	9.42	9.42	3	0.29	0.02	0.10	0.00	0.00	24.0
2	0	-19650	-844	-99	0	-256	10230	15.71	15.71	9.42	9.42	2	0.25	0.01	0.06	0.00	0.00	24.0
3	0	-19650	-845	-20	0	-48	10240	15.71	15.71	9.42	9.42	2	0.25	0.01	0.06	0.00	0.00	24.0
4	0	-19650	-1426	-101	0	-260	15500	15.71	15.71	9.42	9.42	2	0.38	0.02	0.11	0.00	0.00	24.0
5	0	-19660	-1427	-22	0	-52	15520	15.71	15.71	9.42	9.42	2	0.37	0.02	0.11	0.00	0.00	24.0
6	0	-19640	-1046	-192	0	-500	12060	15.71	15.71	9.42	9.42	2	0.30	0.01	0.08	0.00	0.00	24.0
7	0	-19660	-1050	72	0	194	12100	15.71	15.71	9.42	9.42	2	0.29	0.01	0.08	0.00	0.00	24.0
8	0	-19640	-1221	-193	0	-501	13640	15.71	15.71	9.42	9.42	2	0.34	0.02	0.09	0.00	0.00	24.0
9	0	-19660	-1225	71	0	193	13690	15.71	15.71	9.42	9.42	2	0.33	0.02	0.09	0.00	0.00	24.0
10	0	-19650	-844	-99	0	-256	10230	15.71	15.71	9.42	9.42	2	0.25	0.01	0.06	0.00	0.00	24.0
11	0	-19650	-845	-20	0	-48	10240	15.71	15.71	9.42	9.42	2	0.25	0.01	0.06	0.00	0.00	24.0
12	0	-19650	-1426	-101	0	-260	15500	15.71	15.71	9.42	9.42	2	0.38	0.02	0.11	0.00	0.00	24.0
13	0	-19660	-1427	-22	0	-52	15520	15.71	15.71	9.42	9.42	2	0.37	0.02	0.11	0.00	0.00	24.0
14	0	-19640	-1046	-192	0	-500	12060	15.71	15.71	9.42	9.42	2	0.30	0.01	0.08	0.00	0.00	24.0
15	0	-19660	-1050	72	0	194	12100	15.71	15.71	9.42	9.42	2	0.29	0.01	0.08	0.00	0.00	24.0
16	0	-19640	-1221	-193	0	-501	13640	15.71	15.71	9.42	9.42	2	0.34	0.02	0.09	0.00	0.00	24.0
17	0	-19660	-1225	71	0	193	13690	15.71	15.71	9.42	9.42	2	0.33	0.02	0.09	0.00	0.00	24.0
18	0	-37720	-339	-134	0	-369	23490	15.71	15.71	9.42	9.42	3	0.39	0.00	0.02	0.00	0.00	24.0
19	0	-30370	-5474	-138	0	-362	38990	15.71	15.71	9.42	9.42	3	0.66	0.07	0.37	0.00	0.00	24.0
20	0	-32740	-2697	109	0	234	29080	15.71	15.71	9.42	9.42	3	0.49	0.03	0.18	0.00	0.00	24.0
37	0	-37450	1839	-114	0	-317	13600	15.71	15.71	9.42	9.42	3	0.23	0.02	0.12	0.00	0.00	24.0
38	0	-25210	-6719	-120	0	-304	39440	15.71	15.71	9.42	9.42	3	0.68	0.08	0.47	0.00	0.00	24.0
39	0	-29150	-2090	291	0	688	22920	15.71	15.71	9.42	9.42	3	0.39	0.03	0.14	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	110	-24405	-1476	-79	0	-114	15115	15.71	15.71	9.42	9.42	3	0.26	0.02	0.10	0.00	0.00	24.0
2	110	-18770	-844	-99	0	-147	9302	15.71	15.71	9.42	9.42	2	0.23	0.01	0.06	0.00	0.00	24.0
3	110	-18770	-845	-20	0	-26	9311	15.71	15.71	9.42	9.42	2	0.22	0.01	0.06	0.00	0.00	24.0
4	110	-18770	-1426	-101	0	-149	13933	15.71	15.71	9.42	9.42	2	0.34	0.02	0.11	0.00	0.00	24.0
5	110	-18780	-1427	-22	0	-28	13950	15.71	15.71	9.42	9.42	2	0.34	0.02	0.11	0.00	0.00	24.0
6	110	-18760	-1046	-192	0	-289	10910	15.71	15.71	9.42	9.42	2	0.27	0.01	0.08	0.00	0.00	24.0
7	110	-18780	-1050	72	0	115	10946	15.71	15.71	9.42	9.42	2	0.27	0.01	0.08	0.00	0.00	24.0
8	110	-18760	-1221	-193	0	-290	12298	15.71	15.71	9.42	9.42	2	0.30	0.02	0.09	0.00	0.00	24.0
9	110	-18780	-1225	71	0	114	12342	15.71	15.71	9.42	9.42	2	0.30	0.02	0.09	0.00	0.00	24.0
10	110	-18770	-844	-99	0	-147	9302	15.71	15.71	9.42	9.42	2	0.23	0.01	0.06	0.00	0.00	24.0
11	110	-18770	-845	-20	0	-26	9311	15.71	15.71	9.42	9.42	2	0.22	0.01	0.06	0.00	0.00	24.0
12	110	-18770	-1426	-101	0	-149	13933	15.71	15.71	9.42	9.42	2	0.34	0.02	0.11	0.00	0.00	24.0
13	110	-18780	-1427	-22	0	-28	13950	15.71	15.71	9.42	9.42	2	0.34	0.02	0.11	0.00	0.00	24.0
14	110	-18760	-1046	-192	0	-289	10910	15.71	15.71	9.42	9.42	2	0.27	0.01	0.08	0.00	0.00	24.0
15	110	-18780	-1050	72	0	115	10946	15.71	15.71	9.42	9.42	2	0.27	0.01	0.08	0.00	0.00	24.0
16	110	-18760	-1221	-193	0	-290	12298	15.71	15.71	9.42	9.42	2	0.30	0.02	0.09	0.00	0.00	24.0
17	110	-18780	-1225	71	0	114	12342	15.71	15.71	9.42	9.42	2	0.30	0.02	0.09	0.00	0.00	24.0

18	110	-36575	-719	-134	0	-222	22907	15.71	15.71	9.42	9.42	3	0.38	0.01	0.05	0.00	0.00	24.0
19	110	-29228	-5094	-138	0	-210	33178	15.71	15.71	9.42	9.42	3	0.57	0.06	0.34	0.00	0.00	24.0
20	110	-31595	-2697	109	0	114	26113	15.71	15.71	9.42	9.42	3	0.44	0.03	0.18	0.00	0.00	24.0
37	110	-36305	1205	-114	0	-192	15275	15.71	15.71	9.42	9.42	3	0.25	0.01	0.08	0.00	0.00	24.0
38	110	-24065	-6086	-120	0	-172	32397	15.71	15.71	9.42	9.42	3	0.56	0.08	0.43	0.00	0.00	24.0
39	110	-28005	-2090	291	0	368	20623	15.71	15.71	9.42	9.42	3	0.35	0.03	0.14	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	220	-23260	-1476	-79	0	-27	13490	15.71	15.71	9.42	9.42	3	0.24	0.02	0.11	0.00	0.00	24.0
2	220	-17890	-844	-99	0	-38	8373	15.71	15.71	9.42	9.42	2	0.20	0.01	0.06	0.00	0.00	24.0
3	220	-17890	-845	-20	0	-4	8382	15.71	15.71	9.42	9.42	2	0.20	0.01	0.06	0.00	0.00	24.0
4	220	-17890	-1426	-101	0	-38	12366	15.71	15.71	9.42	9.42	2	0.30	0.02	0.11	0.00	0.00	24.0
5	220	-17900	-1427	-22	0	-4	12379	15.71	15.71	9.42	9.42	2	0.30	0.02	0.11	0.00	0.00	24.0
6	220	-17880	-1046	-192	0	-78	9759	15.71	15.71	9.42	9.42	2	0.24	0.01	0.08	0.00	0.00	24.0
7	220	-17900	-1050	72	0	36	9791	15.71	15.71	9.42	9.42	2	0.24	0.01	0.08	0.00	0.00	24.0
8	220	-17880	-1221	-193	0	-78	10956	15.71	15.71	9.42	9.42	2	0.27	0.02	0.09	0.00	0.00	24.0
9	220	-17900	-1225	71	0	36	10993	15.71	15.71	9.42	9.42	2	0.27	0.02	0.09	0.00	0.00	24.0
10	220	-17890	-844	-99	0	-38	8373	15.71	15.71	9.42	9.42	2	0.20	0.01	0.06	0.00	0.00	24.0
11	220	-17890	-845	-20	0	-4	8382	15.71	15.71	9.42	9.42	2	0.20	0.01	0.06	0.00	0.00	24.0
12	220	-17890	-1426	-101	0	-38	12366	15.71	15.71	9.42	9.42	2	0.30	0.02	0.11	0.00	0.00	24.0
13	220	-17900	-1427	-22	0	-4	12379	15.71	15.71	9.42	9.42	2	0.30	0.02	0.11	0.00	0.00	24.0
14	220	-17880	-1046	-192	0	-78	9759	15.71	15.71	9.42	9.42	2	0.24	0.01	0.08	0.00	0.00	24.0
15	220	-17900	-1050	72	0	36	9791	15.71	15.71	9.42	9.42	2	0.24	0.01	0.08	0.00	0.00	24.0
16	220	-17880	-1221	-193	0	-78	10956	15.71	15.71	9.42	9.42	2	0.27	0.02	0.09	0.00	0.00	24.0
17	220	-17900	-1225	71	0	36	10993	15.71	15.71	9.42	9.42	2	0.27	0.02	0.09	0.00	0.00	24.0
18	220	-35430	-1100	-134	0	-74	21906	15.71	15.71	9.42	9.42	3	0.36	0.01	0.07	0.00	0.00	24.0
19	220	-28085	-4714	-138	0	-58	27784	15.71	15.71	9.42	9.42	3	0.48	0.06	0.32	0.00	0.00	24.0
20	220	-30450	-2697	109	0	-5	23145	15.71	15.71	9.42	9.42	3	0.39	0.03	0.18	0.00	0.00	24.0
37	220	-35160	572	-114	0	-66	16254	15.71	15.71	9.42	9.42	3	0.27	0.01	0.04	0.00	0.00	24.0
38	220	-22920	-5452	-120	0	-40	26051	15.71	15.71	9.42	9.42	3	0.46	0.07	0.39	0.00	0.00	24.0
39	220	-26860	-2090	291	0	48	18325	15.71	15.71	9.42	9.42	3	0.32	0.03	0.14	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	330	-22115	-1476	-79	0	59	11865	15.71	15.71	9.42	9.42	3	0.21	0.02	0.11	0.00	0.00	24.0
2	330	-17010	-844	-99	0	71	7445	15.71	15.71	9.42	9.42	2	0.18	0.01	0.06	0.00	0.00	24.0
3	330	-17010	-845	-20	0	18	7453	15.71	15.71	9.42	9.42	2	0.18	0.01	0.06	0.00	0.00	24.0
4	330	-17010	-1426	-101	0	73	10798	15.71	15.71	9.42	9.42	2	0.26	0.02	0.11	0.00	0.00	24.0
5	330	-17020	-1427	-22	0	20	10809	15.71	15.71	9.42	9.42	2	0.26	0.02	0.11	0.00	0.00	24.0
6	330	-17000	-1046	-192	0	134	8609	15.71	15.71	9.42	9.42	2	0.21	0.01	0.08	0.00	0.00	24.0
7	330	-17020	-1050	72	0	-43	8637	15.71	15.71	9.42	9.42	2	0.21	0.01	0.08	0.00	0.00	24.0
8	330	-17000	-1221	-193	0	134	9615	15.71	15.71	9.42	9.42	2	0.24	0.02	0.09	0.00	0.00	24.0
9	330	-17020	-1225	71	0	-43	9644	15.71	15.71	9.42	9.42	2	0.24	0.02	0.09	0.00	0.00	24.0
10	330	-17010	-844	-99	0	71	7445	15.71	15.71	9.42	9.42	2	0.18	0.01	0.06	0.00	0.00	24.0
11	330	-17010	-845	-20	0	18	7453	15.71	15.71	9.42	9.42	2	0.18	0.01	0.06	0.00	0.00	24.0
12	330	-17010	-1426	-101	0	73	10798	15.71	15.71	9.42	9.42	2	0.26	0.02	0.11	0.00	0.00	24.0
13	330	-17020	-1427	-22	0	20	10809	15.71	15.71	9.42	9.42	2	0.26	0.02	0.11	0.00	0.00	24.0
14	330	-17000	-1046	-192	0	134	8609	15.71	15.71	9.42	9.42	2	0.21	0.01	0.08	0.00	0.00	24.0
15	330	-17020	-1050	72	0	-43	8637	15.71	15.71	9.42	9.42	2	0.21	0.01	0.08	0.00	0.00	24.0
16	330	-17000	-1221	-193	0	134	9615	15.71	15.71	9.42	9.42	2	0.24	0.02	0.09	0.00	0.00	24.0
17	330	-17020	-1225	71	0	-43	9644	15.71	15.71	9.42	9.42	2	0.24	0.02	0.09	0.00	0.00	24.0
18	330	-34285	-1480	-134	0	74	20487	15.71	15.71	9.42	9.42	3	0.34	0.02	0.10	0.00	0.00	24.0
19	330	-26942	-4333	-138	0	94	22808	15.71	15.71	9.42	9.42	3	0.39	0.05	0.30	0.00	0.00	24.0
20	330	-29305	-2697	109	0	-125	20177	15.71	15.71	9.42	9.42	3	0.34	0.03	0.18	0.00	0.00	24.0
37	330	-34015	-62	-114	0	59	16535	15.71	15.71	9.42	9.42	3	0.28	0.00	0.01	0.00	0.00	24.0
38	330	-21775	-4818	-120	0	93	20402	15.71	15.71	9.42	9.42	3	0.36	0.06	0.35	0.00	0.00	24.0
39	330	-25715	-2090	291	0	-273	16028	15.71	15.71	9.42	9.42	3	0.28	0.03	0.15	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	440	-20970	-1476	-79	0	146	10240	15.71	15.71	9.42	9.42	3	0.18	0.02	0.11	0.00	0.00	24.0
2	440	-16130	-844	-99	0	180	6517	15.71	15.71	9.42	9.42	2	0.16	0.01	0.07	0.00	0.00	24.0
3	440	-16130	-845	-20	0	40	6524	15.71	15.71	9.42	9.42	2	0.16	0.01	0.07	0.00	0.00	24.0
4	440	-16130	-1426	-101	0	184	9231	15.71	15.71	9.42	9.42	2	0.23	0.02	0.11	0.00	0.00	24.0
5	440	-16140	-1427	-22	0	44	9238	15.71	15.71	9.42	9.42	2	0.23	0.02	0.11	0.00	0.00	24.0
6	440	-16120	-1046	-192	0	345	7459	15.71	15.71	9.42	9.42	2	0.19	0.01	0.08	0.00	0.00	24.0
7	440	-16140	-1050	72	0	-122	7482	15.71	15.71	9.42	9.42	2	0.19	0.01	0.08	0.00	0.00	24.0
8	440	-16120	-1221	-193	0	346	8273	15.71	15.71	9.42	9.42	2	0.21	0.02	0.09	0.00	0.00	24.0
9	440	-16140	-1225	71	0	-121	8296	15.71	15.71	9.42	9.42	2	0.21	0.02	0.09	0.00	0.00	24.0
10	440	-16130	-844	-99	0	180	6517	15.71	15.71	9.42	9.42	2	0.16	0.01	0.07	0.00	0.00	24.0
11	440	-16130	-845	-20	0	40	6524	15.71	15.71	9.42	9.42	2	0.16	0.01	0.07	0.00	0.00	24.0
12	440	-16130	-1426	-101	0	184	9231	15.71	15.71	9.42	9.42	2	0.23	0.02	0.11	0.00	0.00	24.0
13	440	-16140	-1427	-22	0	44	9238	15.71	15.71	9.42	9.42	2	0.23	0.02	0.11	0.00	0.00	24.0
14	440	-16120	-1046	-192	0	345	7459	15.71	15.71	9.42	9.42	2	0.19	0.01	0.08	0.00	0.00	24.0
15	440	-16140	-1050	72	0	-122	7482	15.71	15.71	9.42	9.42	2	0.19	0.01	0.08	0.00	0.00	24.0
16	440	-16120	-1221	-193	0	346	8273	15.71	15.71	9.42	9.42	2	0.21	0.02	0.09	0.00	0.00	24.0
17	440	-16140	-1225	71	0	-121	8296	15.71	15.71	9.42	9.42	2	0.21	0.02	0.09	0.00	0.00	24.0
18	440	-33140	-1860	-134	0	222	18650	15.71	15.71	9.42	9.42	3	0.31	0.02	0.12	0.00	0.00	24.0
19	440	-25800	-3953	-138	0	247	18250	15.71	15.71	9.42	9.42	3	0.32	0.05	0.28	0.00	0.00	24.0
20	440	-28160	-2697	109	0	-244	17210	15.71	15.71	9.42	9.42	3	0.30	0.03	0.18	0.00	0.00	24.0
37	440	-32870	-695	-114	0	184	16120	15.71	15.71	9.42	9.42	3	0.27	0.01	0.05	0.00	0.00	24.0
38	440	-20630	-4185	-120	0	225	15450	15.71	15.71	9.42	9.42	3	0.27	0.05	0.31	0.00	0.00	24.0
39	440	-24570	-2090	291	0	-593	13730	15.71	15.71	9.42	9.42	3	0.24	0.03	0.15	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 28 NI 250 NF 249 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 2B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm

1	0	-24510	-776	-34	0	-149	10630	15.71	15.71	9.42	9.42	3	0.18	0.01	0.06	0.00	0.00	24.0
2	0	-18880	-352	-74	0	-241	6047	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
3	0	-18940	-362	4	0	-37	6178	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
4	0	-18760	-833	-56	0	-193	10170	15.71	15.71	9.42	9.42	2	0.25	0.01	0.06	0.00	0.00	24.0
5	0	-18830	-842	22	0	11	10300	15.71	15.71	9.42	9.42	2	0.25	0.01	0.06	0.00	0.00	24.0
6	0	-18760	-510	-159	0	-462	7337	15.71	15.71	9.42	9.42	2	0.19	0.01	0.04	0.00	0.00	24.0
7	0	-18970	-541	101	0	218	7776	15.71	15.71	9.42	9.42	2	0.19	0.01	0.04	0.00	0.00	24.0
8	0	-18730	-654	-154	0	-448	8574	15.71	15.71	9.42	9.42	2	0.22	0.01	0.05	0.00	0.00	24.0
9	0	-18940	-685	107	0	233	9014	15.71	15.71	9.42	9.42	2	0.22	0.01	0.05	0.00	0.00	24.0
10	0	-18880	-352	-74	0	-241	6047	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
11	0	-18940	-362	4	0	-37	6178	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
12	0	-18760	-833	-56	0	-193	10170	15.71	15.71	9.42	9.42	2	0.25	0.01	0.06	0.00	0.00	24.0
13	0	-18830	-842	22	0	11	10300	15.71	15.71	9.42	9.42	2	0.25	0.01	0.06	0.00	0.00	24.0

14	0	-18760	-510	-159	0	-462	7337	15.71	15.71	9.42	9.42	2	0.19	0.01	0.04	0.00	0.00	24.0
15	0	-18970	-541	101	0	218	7776	15.71	15.71	9.42	9.42	2	0.19	0.01	0.04	0.00	0.00	24.0
16	0	-18730	-654	-154	0	-448	8574	15.71	15.71	9.42	9.42	2	0.22	0.01	0.05	0.00	0.00	24.0
17	0	-18940	-685	107	0	233	9014	15.71	15.71	9.42	9.42	2	0.22	0.01	0.05	0.00	0.00	24.0
18	0	-35620	933	-45	0	-328	12930	15.71	15.71	9.42	9.42	3	0.22	0.01	0.06	0.00	0.00	24.0
19	0	-28150	-3962	-15	0	-158	25990	15.71	15.71	9.42	9.42	3	0.45	0.05	0.27	0.00	0.00	24.0
20	0	-30910	-1416	202	0	326	18430	15.71	15.71	9.42	9.42	3	0.31	0.02	0.09	0.00	0.00	24.0
37	0	-35760	2806	-56	0	-354	5698	15.71	15.71	9.42	9.42	3	0.10	0.03	0.18	0.00	0.00	24.0
38	0	-23310	-5353	-7	0	-71	27460	15.71	15.71	9.42	9.42	3	0.48	0.07	0.38	0.00	0.00	24.0
39	0	-27910	-1109	355	0	735	14870	15.71	15.71	9.42	9.42	3	0.26	0.01	0.08	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	110	-23365	-776	-34	0	-112	9775	15.71	15.71	9.42	9.42	3	0.17	0.01	0.06	0.00	0.00	24.0
2	110	-18000	-352	-74	0	-159	5660	15.71	15.71	9.42	9.42	2	0.14	0.00	0.03	0.00	0.00	24.0
3	110	-18060	-362	4	0	-41	5780	15.71	15.71	9.42	9.42	2	0.14	0.00	0.03	0.00	0.00	24.0
4	110	-17880	-833	-56	0	-131	9254	15.71	15.71	9.42	9.42	2	0.23	0.01	0.06	0.00	0.00	24.0
5	110	-17950	-842	22	0	-13	9374	15.71	15.71	9.42	9.42	2	0.23	0.01	0.06	0.00	0.00	24.0
6	110	-17880	-510	-159	0	-287	6776	15.71	15.71	9.42	9.42	2	0.17	0.01	0.04	0.00	0.00	24.0
7	110	-18090	-541	101	0	107	7181	15.71	15.71	9.42	9.42	2	0.18	0.01	0.04	0.00	0.00	24.0
8	110	-17850	-654	-154	0	-279	7855	15.71	15.71	9.42	9.42	2	0.20	0.01	0.05	0.00	0.00	24.0
9	110	-18060	-685	107	0	116	8260	15.71	15.71	9.42	9.42	2	0.20	0.01	0.05	0.00	0.00	24.0
10	110	-18000	-352	-74	0	-159	5660	15.71	15.71	9.42	9.42	2	0.14	0.00	0.03	0.00	0.00	24.0
11	110	-18060	-362	4	0	-41	5780	15.71	15.71	9.42	9.42	2	0.14	0.00	0.03	0.00	0.00	24.0
12	110	-17880	-833	-56	0	-131	9254	15.71	15.71	9.42	9.42	2	0.23	0.01	0.06	0.00	0.00	24.0
13	110	-17950	-842	22	0	-13	9374	15.71	15.71	9.42	9.42	2	0.23	0.01	0.06	0.00	0.00	24.0
14	110	-17880	-510	-159	0	-287	6776	15.71	15.71	9.42	9.42	2	0.17	0.01	0.04	0.00	0.00	24.0
15	110	-18090	-541	101	0	107	7181	15.71	15.71	9.42	9.42	2	0.18	0.01	0.04	0.00	0.00	24.0
16	110	-17850	-654	-154	0	-279	7855	15.71	15.71	9.42	9.42	2	0.20	0.01	0.05	0.00	0.00	24.0
17	110	-18060	-685	107	0	116	8260	15.71	15.71	9.42	9.42	2	0.20	0.01	0.05	0.00	0.00	24.0
18	110	-34475	553	-45	0	-278	13747	15.71	15.71	9.42	9.42	3	0.23	0.01	0.04	0.00	0.00	24.0
19	110	-27005	-3582	-15	0	-142	21840	15.71	15.71	9.42	9.42	3	0.38	0.04	0.25	0.00	0.00	24.0
20	110	-29768	-1416	202	0	104	16873	15.71	15.71	9.42	9.42	3	0.29	0.02	0.10	0.00	0.00	24.0
37	110	-34615	2172	-56	0	-292	8436	15.71	15.71	9.42	9.42	3	0.14	0.03	0.14	0.00	0.00	24.0
38	110	-22165	-4720	-7	0	-64	21921	15.71	15.71	9.42	9.42	3	0.38	0.06	0.34	0.00	0.00	24.0
39	110	-26765	-1109	355	0	345	13651	15.71	15.71	9.42	9.42	3	0.24	0.01	0.08	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	220	-22220	-776	-34	0	-74	8920	15.71	15.71	9.42	9.42	3	0.16	0.01	0.06	0.00	0.00	24.0
2	220	-17120	-352	-74	0	-78	5272	15.71	15.71	9.42	9.42	2	0.13	0.00	0.03	0.00	0.00	24.0
3	220	-17180	-362	4	0	-46	5383	15.71	15.71	9.42	9.42	2	0.13	0.00	0.03	0.00	0.00	24.0
4	220	-17000	-833	-56	0	-69	8338	15.71	15.71	9.42	9.42	2	0.20	0.01	0.06	0.00	0.00	24.0
5	220	-17070	-842	22	0	-36	8448	15.71	15.71	9.42	9.42	2	0.21	0.01	0.06	0.00	0.00	24.0
6	220	-17000	-510	-159	0	-113	6215	15.71	15.71	9.42	9.42	2	0.15	0.01	0.04	0.00	0.00	24.0
7	220	-17210	-541	101	0	-4	6586	15.71	15.71	9.42	9.42	2	0.16	0.01	0.04	0.00	0.00	24.0
8	220	-16970	-654	-154	0	-110	7136	15.71	15.71	9.42	9.42	2	0.18	0.01	0.05	0.00	0.00	24.0
9	220	-17180	-685	107	0	-2	7507	15.71	15.71	9.42	9.42	2	0.18	0.01	0.05	0.00	0.00	24.0
10	220	-17120	-352	-74	0	-78	5272	15.71	15.71	9.42	9.42	2	0.13	0.00	0.03	0.00	0.00	24.0
11	220	-17180	-362	4	0	-46	5383	15.71	15.71	9.42	9.42	2	0.13	0.00	0.03	0.00	0.00	24.0
12	220	-17000	-833	-56	0	-69	8338	15.71	15.71	9.42	9.42	2	0.20	0.01	0.06	0.00	0.00	24.0
13	220	-17070	-842	22	0	-36	8448	15.71	15.71	9.42	9.42	2	0.21	0.01	0.06	0.00	0.00	24.0
14	220	-17000	-510	-159	0	-113	6215	15.71	15.71	9.42	9.42	2	0.15	0.01	0.04	0.00	0.00	24.0
15	220	-17210	-541	101	0	-4	6586	15.71	15.71	9.42	9.42	2	0.16	0.01	0.04	0.00	0.00	24.0
16	220	-16970	-654	-154	0	-110	7136	15.71	15.71	9.42	9.42	2	0.18	0.01	0.05	0.00	0.00	24.0
17	220	-17180	-685	107	0	-2	7507	15.71	15.71	9.42	9.42	2	0.18	0.01	0.05	0.00	0.00	24.0
18	220	-33330	173	-45	0	-229	14146	15.71	15.71	9.42	9.42	3	0.24	0.00	0.01	0.00	0.00	24.0
19	220	-25860	-3202	-15	0	-125	18109	15.71	15.71	9.42	9.42	3	0.31	0.04	0.22	0.00	0.00	24.0
20	220	-28625	-1416	202	0	-119	15315	15.71	15.71	9.42	9.42	3	0.26	0.02	0.10	0.00	0.00	24.0
37	220	-33470	1539	-56	0	-230	10478	15.71	15.71	9.42	9.42	3	0.18	0.02	0.10	0.00	0.00	24.0
38	220	-21020	-4086	-7	0	-57	17079	15.71	15.71	9.42	9.42	3	0.30	0.05	0.30	0.00	0.00	24.0
39	220	-25620	-1109	355	0	-45	12432	15.71	15.71	9.42	9.42	3	0.21	0.01	0.08	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	330	-21075	-776	-34	0	-37	8066	15.71	15.71	9.42	9.42	3	0.14	0.01	0.06	0.00	0.00	24.0
2	330	-16240	-352	-74	0	3	4885	15.71	15.71	9.42	9.42	2	0.12	0.00	0.03	0.00	0.00	24.0
3	330	-16300	-362	4	0	-50	4985	15.71	15.71	9.42	9.42	2	0.12	0.00	0.03	0.00	0.00	24.0
4	330	-16120	-833	-56	0	-7	7422	15.71	15.71	9.42	9.42	2	0.18	0.01	0.06	0.00	0.00	24.0
5	330	-16190	-842	22	0	-60	7523	15.71	15.71	9.42	9.42	2	0.19	0.01	0.07	0.00	0.00	24.0
6	330	-16120	-510	-159	0	62	5655	15.71	15.71	9.42	9.42	2	0.14	0.01	0.04	0.00	0.00	24.0
7	330	-16330	-541	101	0	-116	5992	15.71	15.71	9.42	9.42	2	0.15	0.01	0.04	0.00	0.00	24.0
8	330	-16090	-654	-154	0	59	6416	15.71	15.71	9.42	9.42	2	0.16	0.01	0.05	0.00	0.00	24.0
9	330	-16300	-685	107	0	-119	6754	15.71	15.71	9.42	9.42	2	0.17	0.01	0.05	0.00	0.00	24.0
10	330	-16240	-352	-74	0	3	4885	15.71	15.71	9.42	9.42	2	0.12	0.00	0.03	0.00	0.00	24.0
11	330	-16300	-362	4	0	-50	4985	15.71	15.71	9.42	9.42	2	0.12	0.00	0.03	0.00	0.00	24.0
12	330	-16120	-833	-56	0	-7	7422	15.71	15.71	9.42	9.42	2	0.18	0.01	0.06	0.00	0.00	24.0
13	330	-16190	-842	22	0	-60	7523	15.71	15.71	9.42	9.42	2	0.19	0.01	0.07	0.00	0.00	24.0
14	330	-16120	-510	-159	0	62	5655	15.71	15.71	9.42	9.42	2	0.14	0.01	0.04	0.00	0.00	24.0
15	330	-16330	-541	101	0	-116	5992	15.71	15.71	9.42	9.42	2	0.15	0.01	0.04	0.00	0.00	24.0
16	330	-16090	-654	-154	0	59	6416	15.71	15.71	9.42	9.42	2	0.16	0.01	0.05	0.00	0.00	24.0
17	330	-16300	-685	107	0	-119	6754	15.71	15.71	9.42	9.42	2	0.17	0.01	0.05	0.00	0.00	24.0
18	330	-32185	-207	-45	0	-180	14127	15.71	15.71	9.42	9.42	3	0.24	0.00	0.01	0.00	0.00	24.0
19	330	-24715	-2822	-15	0	-109	14795	15.71	15.71	9.42	9.42	3	0.26	0.04	0.20	0.00	0.00	24.0
20	330	-27482	-1416	202	0	-341	13758	15.71	15.71	9.42	9.42	3	0.24	0.02	0.10	0.00	0.00	24.0
37	330	-32325	905	-56	0	-168	11822	15.71	15.71	9.42	9.42	3	0.20	0.01	0.06	0.00	0.00	24.0
38	330	-19875	-3452	-7	0	-50	12934	15.71	15.71	9.42	9.42	3	0.23	0.04	0.26	0.00	0.00	24.0
39	330	-24475	-1109	355	0	-436	11214	15.71	15.71	9.42	9.42	3	0.20	0.01	0.08	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	440	-19930	-776	-34	0	0	7211	15.71	15.71	9.42	9.42	3	0.13	0.01	0.06	0.00	0.00	24.0
2	440	-15360	-352	-74	0	85	4497	15.71	15.71	9.42	9.42	2	0.11	0.00	0.03	0.00	0.00	24.0
3	440	-15420	-362	4	0	-54	4588	15.71	15.71	9.42	9.42	2	0.11	0.00	0.03	0.00	0.00	24.0
4	440	-15240	-833	-56	0	55	6506	15.71	15.71	9.42	9.42	2	0.16	0.01	0.07	0.00	0.00	24.0
5	440	-15310	-842	22	0	-84	6597	15.71	15.71	9.42	9.42	2	0.16	0.01	0.07	0.00	0.00	24.0
6	440	-15240	-510	-159	0	237	5094	15.71	15.71	9.42	9.42	2	0.13	0.01	0.04	0.00	0.00	24.0
7	440	-15450	-541	101	0	-227	5397	15.71	15.71	9.42	9.42	2	0.14	0.01	0.04	0.00	0.00	24.0
8	440	-15210	-654	-154	0	228	5697	15.71	15.71	9.42	9.42	2	0.15	0.01	0.05	0.00	0.00	24.0
9	440	-15420	-685	107	0	-236	6000	15.71	15.71	9.42	9.42	2	0.15	0.01	0.05	0.00	0.00	24.0
10	440	-15360	-352	-74	0	85	4497	15.71	15.71	9.42	9.42	2	0.11	0.00	0.03	0.00	0.00	24.0
11	440	-15420	-362	4	0	-54	4588	15.71	15.71	9.42	9.42	2	0.11	0.00	0.03	0.00	0.00	24.0
12	440	-15240	-833	-56	0	55	6506	15.71	15.71	9.42	9.42	2	0.16	0.01	0.07	0.00	0.00	24.0
13	440	-15310	-842	22	0	-84	6597	15.71	15.71	9.42	9.42	2	0.16	0.01	0.07	0.00	0.00	24.0
14	440	-15240	-510	-159	0	237	5094	15.71	15.71	9.42	9.42	2	0.13	0.01	0.04	0.00	0.00	24.0
15	440	-15450	-541	101	0	-227	5397	15.71	15.71	9.42	9.42	2	0.14	0.01	0.04	0.00	0.00	24.0
16	440	-15210	-654	-154	0	228	5697	15.71	15.71	9.42	9.42	2	0.15	0.01	0.05	0.00	0.00	24.0
17	440	-15420	-685	107	0	-236	6000	15.71	15.71	9.42	9.42	2	0.15	0.01	0.05	0.00	0.00	24.0
18	440	-31040	-587	-45	0	-131	13690	15.71	15.71	9.42	9.42	3	0.23	0.01	0.04	0.00	0.00	24.0
19	440	-23570	-2442	-15	0	-93	11900	15.71	15.71	9.42	9.42	3	0.21	0.03	0.17	0.00	0.00	24.0

20	440	-26340	-1416	202	0	-563	12200	15.71	15.71	9.42	9.42	3	0.21	0.02	0.10	0.00	0.00	24.0
37	440	-31180	272	-56	0	-107	12470	15.71	15.71	9.42	9.42	3	0.21	0.00	0.02	0.00	0.00	24.0
38	440	-18730	-2819	-7	0	-42	9486	15.71	15.71	9.42	9.42	3	0.17	0.04	0.21	0.00	0.00	24.0
39	440	-23330	-1109	355	0	-826	9995	15.71	15.71	9.42	9.42	3	0.18	0.01	0.08	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 29 NI 293 NF 292 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 1B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-17260	-97	-328	0	-347	54	6.28	6.28	9.42	9.42	3	0.02	0.01	0.03	0.00	0.00	24.0
2	0	-12590	84	-302	0	-432	-355	6.28	6.28	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
3	0	-12410	82	-238	0	-230	-348	6.28	6.28	9.42	9.42	2	0.04	0.01	0.03	0.00	0.00	24.0
4	0	-14150	-231	-267	0	-304	432	6.28	6.28	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
5	0	-13970	-234	-203	0	-102	439	6.28	6.28	9.42	9.42	2	0.05	0.01	0.02	0.00	0.00	24.0
6	0	-13340	-24	-365	0	-623	-87	6.28	6.28	9.42	9.42	2	0.04	0.01	0.04	0.00	0.00	24.0
7	0	-12740	-31	-151	0	50	-65	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
8	0	-13810	-118	-354	0	-585	149	6.28	6.28	9.42	9.42	2	0.04	0.01	0.04	0.00	0.00	24.0
9	0	-13210	-126	-140	0	88	171	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
10	0	-12590	84	-302	0	-432	-355	6.28	6.28	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
11	0	-12410	82	-238	0	-230	-348	6.28	6.28	9.42	9.42	2	0.04	0.01	0.03	0.00	0.00	24.0
12	0	-14150	-231	-267	0	-304	432	6.28	6.28	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
13	0	-13970	-234	-203	0	-102	439	6.28	6.28	9.42	9.42	2	0.05	0.01	0.02	0.00	0.00	24.0
14	0	-13340	-24	-365	0	-623	-87	6.28	6.28	9.42	9.42	2	0.04	0.01	0.04	0.00	0.00	24.0
15	0	-12740	-31	-151	0	50	-65	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
16	0	-13810	-118	-354	0	-585	149	6.28	6.28	9.42	9.42	2	0.04	0.01	0.04	0.00	0.00	24.0
17	0	-13210	-126	-140	0	88	171	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
18	0	-19570	845	-599	0	-933	-1552	6.28	6.28	9.42	9.42	3	0.15	0.02	0.08	0.00	0.00	24.0
19	0	-21160	-915	-374	0	-337	1423	6.28	6.28	9.42	9.42	3	0.13	0.02	0.09	0.00	0.00	24.0
20	0	-19550	-43	-512	0	-171	-48	6.28	6.28	9.42	9.42	3	0.01	0.01	0.05	0.00	0.00	24.0
37	0	-18020	1413	-623	0	-1039	-2506	6.28	6.28	9.42	9.42	3	0.24	0.03	0.14	0.00	0.00	24.0
38	0	-20670	-1522	-248	0	-45	2453	6.28	6.28	9.42	9.42	3	0.23	0.04	0.14	0.00	0.00	24.0
39	0	-17990	-67	-478	0	231	1	6.28	6.28	9.42	9.42	3	0.01	0.01	0.05	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	97	-16690	-97	-328	0	-27	-40	6.28	6.28	9.42	9.42	3	0.00	0.01	0.03	0.00	0.00	24.0
2	97	-12150	84	-302	0	-137	-273	6.28	6.28	9.42	9.42	2	0.03	0.01	0.03	0.00	0.00	24.0
3	97	-11970	82	-238	0	2	-269	6.28	6.28	9.42	9.42	2	0.03	0.01	0.03	0.00	0.00	24.0
4	97	-13710	-231	-267	0	-44	206	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
5	97	-13530	-234	-203	0	95	211	6.28	6.28	9.42	9.42	2	0.03	0.01	0.02	0.00	0.00	24.0
6	97	-12902	-24	-365	0	-267	-111	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
7	97	-12302	-31	-151	0	197	-95	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
8	97	-13370	-118	-354	0	-239	33	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
9	97	-12772	-126	-140	0	225	48	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
10	97	-12150	84	-302	0	-137	-273	6.28	6.28	9.42	9.42	2	0.03	0.01	0.03	0.00	0.00	24.0
11	97	-11970	82	-238	0	2	-269	6.28	6.28	9.42	9.42	2	0.03	0.01	0.03	0.00	0.00	24.0
12	97	-13710	-231	-267	0	-44	206	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
13	97	-13530	-234	-203	0	95	211	6.28	6.28	9.42	9.42	2	0.03	0.01	0.02	0.00	0.00	24.0
14	97	-12902	-24	-365	0	-267	-111	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
15	97	-12302	-31	-151	0	197	-95	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
16	97	-13370	-118	-354	0	-239	33	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
17	97	-12772	-126	-140	0	225	48	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
18	97	-19000	677	-599	0	-349	-810	6.28	6.28	9.42	9.42	3	0.08	0.02	0.07	0.00	0.00	24.0
19	97	-20590	-747	-374	0	28	613	6.28	6.28	9.42	9.42	3	0.06	0.02	0.07	0.00	0.00	24.0
20	97	-18980	-43	-381	0	263	-90	6.28	6.28	9.42	9.42	3	0.01	0.01	0.04	0.00	0.00	24.0
37	97	-17450	1132	-623	0	-431	-1266	6.28	6.28	9.42	9.42	3	0.12	0.03	0.11	0.00	0.00	24.0
38	97	-20100	-1241	-248	0	197	1106	6.28	6.28	9.42	9.42	3	0.10	0.03	0.12	0.00	0.00	24.0
39	97	-17420	-67	-260	0	588	-65	6.28	6.28	9.42	9.42	3	0.03	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	195	-16120	-97	-328	0	293	-135	6.28	6.28	9.42	9.42	3	0.02	0.01	0.04	0.00	0.00	24.0
2	195	-11710	84	-302	0	158	-191	6.28	6.28	9.42	9.42	2	0.03	0.01	0.03	0.00	0.00	24.0
3	195	-11530	82	-238	0	234	-189	6.28	6.28	9.42	9.42	2	0.03	0.01	0.03	0.00	0.00	24.0
4	195	-13270	-231	-267	0	217	-19	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
5	195	-13090	-234	-203	0	293	-17	6.28	6.28	9.42	9.42	2	0.02	0.01	0.02	0.00	0.00	24.0
6	195	-12465	-24	-365	0	89	-134	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
7	195	-11865	-31	-151	0	344	-126	6.28	6.28	9.42	9.42	2	0.03	0.00	0.02	0.00	0.00	24.0
8	195	-12930	-118	-354	0	107	-82	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
9	195	-12335	-126	-140	0	362	-74	6.28	6.28	9.42	9.42	2	0.03	0.00	0.02	0.00	0.00	24.0
10	195	-11710	84	-302	0	158	-191	6.28	6.28	9.42	9.42	2	0.03	0.01	0.03	0.00	0.00	24.0
11	195	-11530	82	-238	0	234	-189	6.28	6.28	9.42	9.42	2	0.03	0.01	0.03	0.00	0.00	24.0
12	195	-13270	-231	-267	0	217	-19	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
13	195	-13090	-234	-203	0	293	-17	6.28	6.28	9.42	9.42	2	0.02	0.01	0.02	0.00	0.00	24.0
14	195	-12465	-24	-365	0	89	-134	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
15	195	-11865	-31	-151	0	344	-126	6.28	6.28	9.42	9.42	2	0.03	0.00	0.02	0.00	0.00	24.0
16	195	-12930	-118	-354	0	107	-82	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
17	195	-12335	-126	-140	0	362	-74	6.28	6.28	9.42	9.42	2	0.03	0.00	0.02	0.00	0.00	24.0
18	195	-18430	508	-599	0	235	-232	6.28	6.28	9.42	9.42	3	0.02	0.01	0.06	0.00	0.00	24.0
19	195	-20020	-578	-374	0	393	-33	6.28	6.28	9.42	9.42	3	0.02	0.01	0.05	0.00	0.00	24.0
20	195	-18410	-43	-270	0	579	-131	6.28	6.28	9.42	9.42	3	0.03	0.01	0.03	0.00	0.00	24.0
37	195	-16880	851	-623	0	176	-299	6.28	6.28	9.42	9.42	3	0.03	0.02	0.08	0.00	0.00	24.0
38	195	-19530	-960	-248	0	438	33	6.28	6.28	9.42	9.42	3	0.02	0.02	0.08	0.00	0.00	24.0
39	195	-16850	-67	-73	0	748	-130	6.28	6.28	9.42	9.42	3	0.04	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	292	-15550	-97	-328	0	613	-230	6.28	6.28	9.42	9.42	3	0.03	0.01	0.04	0.00	0.00	24.0
2	292	-11270	84	-302	0	452	-109	6.28	6.28	9.42	9.42	2	0.03	0.01	0.03	0.00	0.00	24.0
3	292	-11090	82	-238	0	466	-109	6.28	6.28	9.42	9.42	2	0.03	0.01	0.03	0.00	0.00	24.0
4	292	-12830	-231	-267	0	477	-245	6.28	6.28	9.42	9.42	2	0.04	0.01	0.03	0.00	0.00	24.0
5	292	-12650	-234	-203	0	491	-244	6.28	6.28	9.42	9.42	2	0.04	0.01	0.02	0.00	0.00	24.0
6	292	-12028	-24	-365	0	445	-157	6.28	6.28	9.42	9.42	2	0.04	0.01	0.04	0.00	0.00	24.0
7	292	-11428	-31	-151	0	491	-156	6.28	6.28	9.42	9.42	2	0.04	0.00	0.02	0.00	0.00	24.0
8	292	-12490	-118	-354	0	452	-197	6.28	6.28	9.42	9.42	2	0.04	0.01	0.04	0.00	0.00	24.0
9	292	-11898	-126	-140	0	498	-197	6.28	6.28	9.42	9.42	2	0.04	0.00	0.02	0.00	0.00	24.0
10	292	-11270	84	-302	0	452	-109	6.28	6.28	9.42	9.42	2	0.03	0.01	0.03	0.00	0.00	24.0
11	292	-11090	82	-238	0	466	-109	6.28	6.28	9.42	9.42	2	0.03	0.01	0.03	0.00	0.00	24.0
12	292	-12830	-231	-267	0	477	-245	6.28	6.28	9.42	9.42	2	0.04	0.01	0.03	0.00	0.00	24.0
13	292	-12650	-234	-203	0	491	-244	6.28	6.28	9.42	9.42	2	0.04	0.01	0.02	0.00	0.00	24.0
14	292	-12028	-24	-365	0	445	-157	6.28	6.28	9.42	9.42	2	0.04	0.01	0.04	0.00	0.00	24.0
15	292	-11428	-31	-151	0	491	-156	6.28	6.28	9.42	9.42	2	0.04	0.00	0.02	0.00	0.00	24.0

16	292	-12490	-118	-354	0	452	-197	6.28	6.28	9.42	9.42	2	0.04	0.01	0.04	0.00	0.00	24.0
17	292	-11898	-126	-140	0	498	-197	6.28	6.28	9.42	9.42	2	0.04	0.00	0.02	0.00	0.00	24.0
18	292	-17860	340	-599	0	820	181	6.28	6.28	9.42	9.42	3	0.04	0.01	0.06	0.00	0.00	24.0
19	292	-19450	-410	-374	0	757	-515	6.28	6.28	9.42	9.42	3	0.06	0.01	0.04	0.00	0.00	24.0
20	292	-17840	-43	-176	0	795	-173	6.28	6.28	9.42	9.42	3	0.04	0.00	0.02	0.00	0.00	24.0
37	292	-16310	570	-623	0	783	393	6.28	6.28	9.42	9.42	3	0.05	0.01	0.07	0.00	0.00	24.0
38	292	-18960	-680	-248	0	679	-766	6.28	6.28	9.42	9.42	3	0.08	0.02	0.07	0.00	0.00	24.0
39	292	-16280	-67	82	0	741	-196	6.28	6.28	9.42	9.42	3	0.04	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	390	-14980	-97	-328	0	933	-325	6.28	6.28	9.42	9.42	3	0.05	0.01	0.04	0.00	0.00	24.0
2	390	-10830	84	-302	0	747	-27	6.28	6.28	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
3	390	-10650	82	-238	0	698	-29	6.28	6.28	9.42	9.42	2	0.04	0.01	0.03	0.00	0.00	24.0
4	390	-12390	-231	-267	0	737	-470	6.28	6.28	9.42	9.42	2	0.08	0.01	0.03	0.00	0.00	24.0
5	390	-12210	-234	-203	0	689	-472	6.28	6.28	9.42	9.42	2	0.08	0.01	0.02	0.00	0.00	24.0
6	390	-11590	-24	-365	0	801	-180	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
7	390	-10990	-31	-151	0	638	-187	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
8	390	-12050	-118	-354	0	798	-313	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
9	390	-11460	-126	-140	0	635	-320	6.28	6.28	9.42	9.42	2	0.06	0.00	0.02	0.00	0.00	24.0
10	390	-10830	84	-302	0	747	-27	6.28	6.28	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
11	390	-10650	82	-238	0	698	-29	6.28	6.28	9.42	9.42	2	0.04	0.01	0.03	0.00	0.00	24.0
12	390	-12390	-231	-267	0	737	-470	6.28	6.28	9.42	9.42	2	0.08	0.01	0.03	0.00	0.00	24.0
13	390	-12210	-234	-203	0	689	-472	6.28	6.28	9.42	9.42	2	0.08	0.01	0.02	0.00	0.00	24.0
14	390	-11590	-24	-365	0	801	-180	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
15	390	-10990	-31	-151	0	638	-187	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
16	390	-12050	-118	-354	0	798	-313	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
17	390	-11460	-126	-140	0	635	-320	6.28	6.28	9.42	9.42	2	0.06	0.00	0.02	0.00	0.00	24.0
18	390	-17290	171	-599	0	1404	430	6.28	6.28	9.42	9.42	3	0.07	0.01	0.06	0.00	0.00	24.0
19	390	-18880	-241	-374	0	1122	-832	6.28	6.28	9.42	9.42	3	0.09	0.01	0.04	0.00	0.00	24.0
20	390	-17270	-43	-102	0	929	-214	6.28	6.28	9.42	9.42	3	0.05	0.00	0.01	0.00	0.00	24.0
37	390	-15740	289	-623	0	1391	812	6.28	6.28	9.42	9.42	3	0.10	0.01	0.07	0.00	0.00	24.0
38	390	-18390	-399	-248	0	921	-1292	6.28	6.28	9.42	9.42	3	0.13	0.01	0.04	0.00	0.00	24.0
39	390	-15710	-67	206	0	598	-262	6.28	6.28	9.42	9.42	3	0.04	0.00	0.02	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 30 NI 77 NF 76 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 6C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-14090	-874	149	0	71	5896	15.71	15.71	9.42	9.42	3	0.11	0.01	0.07	0.00	0.00	24.0
2	0	-10970	-567	52	0	-20	4059	15.71	15.71	9.42	9.42	2	0.10	0.01	0.05	0.00	0.00	24.0
3	0	-10950	-546	124	0	105	4006	15.71	15.71	9.42	9.42	2	0.10	0.01	0.04	0.00	0.00	24.0
4	0	-10730	-799	105	0	4	5066	15.71	15.71	9.42	9.42	2	0.13	0.01	0.07	0.00	0.00	24.0
5	0	-10710	-778	177	0	129	5012	15.71	15.71	9.42	9.42	2	0.13	0.01	0.06	0.00	0.00	24.0
6	0	-10910	-673	-14	0	-157	4474	15.71	15.71	9.42	9.42	2	0.12	0.01	0.06	0.00	0.00	24.0
7	0	-10840	-602	227	0	259	4295	15.71	15.71	9.42	9.42	2	0.11	0.01	0.05	0.00	0.00	24.0
8	0	-10830	-742	2	0	-150	4776	15.71	15.71	9.42	9.42	2	0.12	0.01	0.06	0.00	0.00	24.0
9	0	-10770	-672	242	0	267	4597	15.71	15.71	9.42	9.42	2	0.12	0.01	0.06	0.00	0.00	24.0
10	0	-10970	-567	52	0	-20	4059	15.71	15.71	9.42	9.42	2	0.10	0.01	0.05	0.00	0.00	24.0
11	0	-10950	-546	124	0	105	4006	15.71	15.71	9.42	9.42	2	0.10	0.01	0.04	0.00	0.00	24.0
12	0	-10730	-799	105	0	4	5066	15.71	15.71	9.42	9.42	2	0.13	0.01	0.07	0.00	0.00	24.0
13	0	-10710	-778	177	0	129	5012	15.71	15.71	9.42	9.42	2	0.13	0.01	0.06	0.00	0.00	24.0
14	0	-10910	-673	-14	0	-157	4474	15.71	15.71	9.42	9.42	2	0.12	0.01	0.06	0.00	0.00	24.0
15	0	-10840	-602	227	0	259	4295	15.71	15.71	9.42	9.42	2	0.11	0.01	0.05	0.00	0.00	24.0
16	0	-10830	-742	2	0	-150	4776	15.71	15.71	9.42	9.42	2	0.12	0.01	0.06	0.00	0.00	24.0
17	0	-10770	-672	242	0	267	4597	15.71	15.71	9.42	9.42	2	0.12	0.01	0.06	0.00	0.00	24.0
18	0	-25080	-1078	238	0	134	13290	15.71	15.71	9.42	9.42	3	0.23	0.01	0.08	0.00	0.00	24.0
19	0	-17360	-2293	295	0	107	8851	15.71	15.71	9.42	9.42	3	0.16	0.03	0.17	0.00	0.00	24.0
20	0	-20260	-1583	330	0	139	10580	15.71	15.71	9.42	9.42	3	0.19	0.02	0.12	0.00	0.00	24.0
37	0	-25380	-408	181	0	127	13090	15.71	15.71	9.42	9.42	3	0.23	0.01	0.03	0.00	0.00	24.0
38	0	-12510	-2432	276	0	83	5689	15.71	15.71	9.42	9.42	3	0.10	0.03	0.20	0.00	0.00	24.0
39	0	-17350	-1249	335	0	135	8574	15.71	15.71	9.42	9.42	3	0.15	0.02	0.10	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	83	-13232	-874	149	0	-51	5175	15.71	15.71	9.42	9.42	3	0.09	0.01	0.07	0.00	0.00	24.0
2	83	-10309	-567	52	0	-63	3591	15.71	15.71	9.42	9.42	2	0.09	0.01	0.05	0.00	0.00	24.0
3	83	-10289	-546	124	0	3	3556	15.71	15.71	9.42	9.42	2	0.09	0.01	0.05	0.00	0.00	24.0
4	83	-10070	-799	105	0	-82	4407	15.71	15.71	9.42	9.42	2	0.11	0.01	0.07	0.00	0.00	24.0
5	83	-10050	-778	177	0	-17	4370	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
6	83	-10249	-673	-14	0	-146	3919	15.71	15.71	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
7	83	-10180	-602	227	0	72	3798	15.71	15.71	9.42	9.42	2	0.10	0.01	0.05	0.00	0.00	24.0
8	83	-10171	-742	2	0	-152	4164	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
9	83	-10110	-672	242	0	67	4043	15.71	15.71	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
10	83	-10309	-567	52	0	-63	3591	15.71	15.71	9.42	9.42	2	0.09	0.01	0.05	0.00	0.00	24.0
11	83	-10289	-546	124	0	3	3556	15.71	15.71	9.42	9.42	2	0.09	0.01	0.05	0.00	0.00	24.0
12	83	-10070	-799	105	0	-82	4407	15.71	15.71	9.42	9.42	2	0.11	0.01	0.07	0.00	0.00	24.0
13	83	-10050	-778	177	0	-17	4370	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
14	83	-10249	-673	-14	0	-146	3919	15.71	15.71	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
15	83	-10180	-602	227	0	72	3798	15.71	15.71	9.42	9.42	2	0.10	0.01	0.05	0.00	0.00	24.0
16	83	-10171	-742	2	0	-152	4164	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
17	83	-10110	-672	242	0	67	4043	15.71	15.71	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
18	83	-24222	-1455	238	0	-63	12246	15.71	15.71	9.42	9.42	3	0.21	0.02	0.10	0.00	0.00	24.0
19	83	-16502	-1916	295	0	-136	7115	15.71	15.71	9.42	9.42	3	0.13	0.02	0.15	0.00	0.00	24.0
20	83	-19402	-1583	330	0	-134	9275	15.71	15.71	9.42	9.42	3	0.16	0.02	0.12	0.00	0.00	24.0
37	83	-24522	-1037	181	0	-22	12495	15.71	15.71	9.42	9.42	3	0.22	0.01	0.07	0.00	0.00	24.0
38	83	-11653	-1803	276	0	-145	3942	15.71	15.71	9.42	9.42	3	0.07	0.02	0.15	0.00	0.00	24.0
39	83	-16492	-1249	335	0	-141	7544	15.71	15.71	9.42	9.42	3	0.14	0.02	0.10	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	165	-12375	-874	149	0	-174	4454	15.71	15.71	9.42	9.42	3	0.08	0.01	0.07	0.00	0.00	24.0
2	165	-9648	-567	52	0	-105	3124	15.71	15.71	9.42	9.42	2	0.08	0.01	0.05	0.00	0.00	24.0
3	165	-9628	-546	124	0	-99	3105	15.71	15.71	9.42	9.42	2	0.08	0.01	0.05	0.00	0.00	24.0
4	165	-9409	-799	105	0	-168	3748	15.71	15.71	9.42	9.42	2	0.10	0.01	0.07	0.00	0.00	24.0
5	165	-9389	-778	177	0	-163	3729	15.71	15.71	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
6	165	-9588	-673	-14	0	-134	3364	15.71	15.71	9.42	9.42	2	0.09	0.01	0.06	0.00	0.00	24.0
7	165	-9520	-602	227	0	-115	3302	15.71	15.71	9.42	9.42	2	0.09	0.01	0.05	0.00	0.00	24.0
8	165	-9512	-742	2	0	-153	3552	15.71	15.71	9.42	9.42	2	0.09	0.01	0.06	0.00	0.00	24.0
9	165	-9450	-672	242	0	-133	3489	15.71	15.71	9.42	9.42	2	0.09	0.01	0.06	0.00	0.00	24.0
10	165	-9648	-567	52	0	-105	3124	15.71	15.71	9.42	9.42	2	0.08	0.01	0.05	0.00	0.00	24.0
11	165	-9628	-546	124	0	-99	3105	15.71	15.71	9.42	9.42	2	0.08	0.01	0.05	0.00	0.00	24.0

12	165	-9409	-799	105	0	-168	3748	15.71	15.71	9.42	9.42	2	0.10	0.01	0.07	0.00	0.00	24.0
13	165	-9389	-778	177	0	-163	3729	15.71	15.71	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
14	165	-9588	-673	-14	0	-134	3364	15.71	15.71	9.42	9.42	2	0.09	0.01	0.06	0.00	0.00	24.0
15	165	-9520	-602	227	0	-115	3302	15.71	15.71	9.42	9.42	2	0.09	0.01	0.05	0.00	0.00	24.0
16	165	-9512	-742	2	0	-153	3552	15.71	15.71	9.42	9.42	2	0.09	0.01	0.06	0.00	0.00	24.0
17	165	-9450	-672	242	0	-133	3489	15.71	15.71	9.42	9.42	2	0.09	0.01	0.06	0.00	0.00	24.0
18	165	-23365	-1832	238	0	-259	10890	15.71	15.71	9.42	9.42	3	0.19	0.02	0.13	0.00	0.00	24.0
19	165	-15645	-1538	295	0	-380	5691	15.71	15.71	9.42	9.42	3	0.10	0.02	0.12	0.00	0.00	24.0
20	165	-18545	-1583	330	0	-406	7970	15.71	15.71	9.42	9.42	3	0.14	0.02	0.12	0.00	0.00	24.0
37	165	-23665	-1666	181	0	-171	11381	15.71	15.71	9.42	9.42	3	0.20	0.02	0.12	0.00	0.00	24.0
38	165	-10796	-1175	276	0	-373	2714	15.71	15.71	9.42	9.42	3	0.05	0.02	0.10	0.00	0.00	24.0
39	165	-15635	-1249	335	0	-417	6514	15.71	15.71	9.42	9.42	3	0.12	0.02	0.10	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	248	-11518	-874	149	0	-297	3734	15.71	15.71	9.42	9.42	3	0.07	0.01	0.07	0.00	0.00	24.0
2	248	-8987	-567	52	0	-148	2656	15.71	15.71	9.42	9.42	2	0.07	0.01	0.05	0.00	0.00	24.0
3	248	-8968	-546	124	0	-202	2655	15.71	15.71	9.42	9.42	2	0.07	0.01	0.05	0.00	0.00	24.0
4	248	-8748	-799	105	0	-255	3089	15.71	15.71	9.42	9.42	2	0.09	0.01	0.07	0.00	0.00	24.0
5	248	-8728	-778	177	0	-308	3087	15.71	15.71	9.42	9.42	2	0.09	0.01	0.07	0.00	0.00	24.0
6	248	-8927	-673	-14	0	-123	2810	15.71	15.71	9.42	9.42	2	0.07	0.01	0.06	0.00	0.00	24.0
7	248	-8860	-602	227	0	-302	2805	15.71	15.71	9.42	9.42	2	0.08	0.01	0.05	0.00	0.00	24.0
8	248	-8853	-742	2	0	-155	2939	15.71	15.71	9.42	9.42	2	0.08	0.01	0.06	0.00	0.00	24.0
9	248	-8789	-672	242	0	-334	2934	15.71	15.71	9.42	9.42	2	0.08	0.01	0.06	0.00	0.00	24.0
10	248	-8987	-567	52	0	-148	2656	15.71	15.71	9.42	9.42	2	0.07	0.01	0.05	0.00	0.00	24.0
11	248	-8968	-546	124	0	-202	2655	15.71	15.71	9.42	9.42	2	0.07	0.01	0.05	0.00	0.00	24.0
12	248	-8748	-799	105	0	-255	3089	15.71	15.71	9.42	9.42	2	0.09	0.01	0.07	0.00	0.00	24.0
13	248	-8728	-778	177	0	-308	3087	15.71	15.71	9.42	9.42	2	0.09	0.01	0.07	0.00	0.00	24.0
14	248	-8927	-673	-14	0	-123	2810	15.71	15.71	9.42	9.42	2	0.07	0.01	0.06	0.00	0.00	24.0
15	248	-8860	-602	227	0	-302	2805	15.71	15.71	9.42	9.42	2	0.08	0.01	0.05	0.00	0.00	24.0
16	248	-8853	-742	2	0	-155	2939	15.71	15.71	9.42	9.42	2	0.08	0.01	0.06	0.00	0.00	24.0
17	248	-8789	-672	242	0	-334	2934	15.71	15.71	9.42	9.42	2	0.08	0.01	0.06	0.00	0.00	24.0
18	248	-22508	-2210	238	0	-455	9224	15.71	15.71	9.42	9.42	3	0.16	0.03	0.16	0.00	0.00	24.0
19	248	-14788	-1161	295	0	-623	4577	15.71	15.71	9.42	9.42	3	0.09	0.01	0.09	0.00	0.00	24.0
20	248	-17688	-1583	330	0	-679	6664	15.71	15.71	9.42	9.42	3	0.12	0.02	0.12	0.00	0.00	24.0
37	248	-22808	-2294	181	0	-321	9748	15.71	15.71	9.42	9.42	3	0.17	0.03	0.17	0.00	0.00	24.0
38	248	-9940	-546	276	0	-600	2004	15.71	15.71	9.42	9.42	3	0.04	0.01	0.05	0.00	0.00	24.0
39	248	-14778	-1249	335	0	-693	5483	15.71	15.71	9.42	9.42	3	0.10	0.02	0.10	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	330	-10660	-874	149	0	-419	3013	15.71	15.71	9.42	9.42	3	0.06	0.01	0.07	0.00	0.00	24.0
2	330	-8326	-567	52	0	-191	2189	15.71	15.71	9.42	9.42	2	0.06	0.01	0.05	0.00	0.00	24.0
3	330	-8307	-546	124	0	-304	2205	15.71	15.71	9.42	9.42	2	0.06	0.01	0.05	0.00	0.00	24.0
4	330	-8088	-799	105	0	-341	2430	15.71	15.71	9.42	9.42	2	0.07	0.01	0.07	0.00	0.00	24.0
5	330	-8068	-778	177	0	-454	2446	15.71	15.71	9.42	9.42	2	0.07	0.01	0.07	0.00	0.00	24.0
6	330	-8266	-673	-14	0	-112	2255	15.71	15.71	9.42	9.42	2	0.06	0.01	0.06	0.00	0.00	24.0
7	330	-8200	-602	227	0	-489	2308	15.71	15.71	9.42	9.42	2	0.07	0.01	0.05	0.00	0.00	24.0
8	330	-8194	-742	2	0	-157	2327	15.71	15.71	9.42	9.42	2	0.06	0.01	0.06	0.00	0.00	24.0
9	330	-8129	-672	242	0	-534	2380	15.71	15.71	9.42	9.42	2	0.08	0.01	0.06	0.00	0.00	24.0
10	330	-8326	-567	52	0	-191	2189	15.71	15.71	9.42	9.42	2	0.06	0.01	0.05	0.00	0.00	24.0
11	330	-8307	-546	124	0	-304	2205	15.71	15.71	9.42	9.42	2	0.06	0.01	0.05	0.00	0.00	24.0
12	330	-8088	-799	105	0	-341	2430	15.71	15.71	9.42	9.42	2	0.07	0.01	0.07	0.00	0.00	24.0
13	330	-8068	-778	177	0	-454	2446	15.71	15.71	9.42	9.42	2	0.07	0.01	0.07	0.00	0.00	24.0
14	330	-8266	-673	-14	0	-112	2255	15.71	15.71	9.42	9.42	2	0.06	0.01	0.06	0.00	0.00	24.0
15	330	-8200	-602	227	0	-489	2308	15.71	15.71	9.42	9.42	2	0.07	0.01	0.05	0.00	0.00	24.0
16	330	-8194	-742	2	0	-157	2327	15.71	15.71	9.42	9.42	2	0.06	0.01	0.06	0.00	0.00	24.0
17	330	-8129	-672	242	0	-534	2380	15.71	15.71	9.42	9.42	2	0.08	0.01	0.06	0.00	0.00	24.0
18	330	-21650	-2587	238	0	-652	7246	15.71	15.71	9.42	9.42	3	0.13	0.03	0.19	0.00	0.00	24.0
19	330	-13930	-784	295	0	-866	3775	15.71	15.71	9.42	9.42	3	0.08	0.01	0.06	0.00	0.00	24.0
20	330	-16830	-1583	330	0	-951	5359	15.71	15.71	9.42	9.42	3	0.10	0.02	0.12	0.00	0.00	24.0
37	330	-21950	-2923	181	0	-470	7597	15.71	15.71	9.42	9.42	3	0.14	0.04	0.21	0.00	0.00	24.0
38	330	-9083	83	276	0	-828	1813	15.71	15.71	9.42	9.42	3	0.05	0.00	0.02	0.00	0.00	24.0
39	330	-13920	-1249	335	0	-969	4453	15.71	15.71	9.42	9.42	3	0.09	0.02	0.10	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 31 NI 120 NF 119 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 5C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-15880	-1569	49	0	-47	9639	15.71	15.71	9.42	9.42	3	0.17	0.02	0.12	0.00	0.00	24.0
2	0	-12180	-919	-20	0	-120	6078	15.71	15.71	9.42	9.42	2	0.16	0.01	0.07	0.00	0.00	24.0
3	0	-12210	-926	60	0	23	6128	15.71	15.71	9.42	9.42	2	0.15	0.01	0.07	0.00	0.00	24.0
4	0	-12220	-1489	15	0	-96	8701	15.71	15.71	9.42	9.42	2	0.22	0.02	0.12	0.00	0.00	24.0
5	0	-12260	-1495	95	0	47	8750	15.71	15.71	9.42	9.42	2	0.22	0.02	0.12	0.00	0.00	24.0
6	0	-12150	-1112	-102	0	-279	6938	15.71	15.71	9.42	9.42	2	0.18	0.01	0.09	0.00	0.00	24.0
7	0	-12270	-1132	167	0	198	7104	15.71	15.71	9.42	9.42	2	0.18	0.01	0.09	0.00	0.00	24.0
8	0	-12160	-1283	-92	0	-271	7725	15.71	15.71	9.42	9.42	2	0.20	0.02	0.10	0.00	0.00	24.0
9	0	-12290	-1303	177	0	206	7890	15.71	15.71	9.42	9.42	2	0.20	0.02	0.11	0.00	0.00	24.0
10	0	-12180	-919	-20	0	-120	6078	15.71	15.71	9.42	9.42	2	0.16	0.01	0.07	0.00	0.00	24.0
11	0	-12210	-926	60	0	23	6128	15.71	15.71	9.42	9.42	2	0.15	0.01	0.07	0.00	0.00	24.0
12	0	-12220	-1489	15	0	-96	8701	15.71	15.71	9.42	9.42	2	0.22	0.02	0.12	0.00	0.00	24.0
13	0	-12260	-1495	95	0	47	8750	15.71	15.71	9.42	9.42	2	0.22	0.02	0.12	0.00	0.00	24.0
14	0	-12150	-1112	-102	0	-279	6938	15.71	15.71	9.42	9.42	2	0.18	0.01	0.09	0.00	0.00	24.0
15	0	-12270	-1132	167	0	198	7104	15.71	15.71	9.42	9.42	2	0.18	0.01	0.09	0.00	0.00	24.0
16	0	-12160	-1283	-92	0	-271	7725	15.71	15.71	9.42	9.42	2	0.20	0.02	0.10	0.00	0.00	24.0
17	0	-12290	-1303	177	0	206	7890	15.71	15.71	9.42	9.42	2	0.20	0.02	0.11	0.00	0.00	24.0
18	0	-28160	-2045	-26	0	-231	18560	15.71	15.71	9.42	9.42	3	0.32	0.03	0.14	0.00	0.00	24.0
19	0	-20910	-4104	107	0	-87	17910	15.71	15.71	9.42	9.42	3	0.32	0.05	0.30	0.00	0.00	24.0
20	0	-23250	-2858	106	0	-77	17010	15.71	15.71	9.42	9.42	3	0.30	0.04	0.21	0.00	0.00	24.0
37	0	-27810	-868	-66	0	-242	15990	15.71	15.71	9.42	9.42	3	0.27	0.01	0.06	0.00	0.00	24.0
38	0	-15730	-4300	155	0	-1	14900	15.71	15.71	9.42	9.42	3	0.27	0.05	0.33	0.00	0.00	24.0
39	0	-19630	-2224	152	0	15	13400	15.71	15.71	9.42	9.42	3	0.24	0.03	0.17	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	83	-15022	-1569	49	0	-88	8344	15.71	15.71	9.42	9.42	3	0.15	0.02	0.12	0.00	0.00	24.0
2	83	-11519	-919	-20	0	-103	5320	15.71	15.71	9.42	9.42	2	0.14	0.01	0.07	0.00	0.00	24.0
3	83	-11551	-926	60	0	-27	5365	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
4	83	-11560	-1489	15	0	-108	7472	15.71	15.71	9.42	9.42	2	0.19	0.02	0.12	0.00	0.00	24.0
5	83	-11599	-1495	95	0	-31	7516	15.71	15.71	9.42	9.42	2	0.19	0.02	0.12	0.00	0.00	24.0
6	83	-11490	-1112	-102	0	-194	6021	15.71	15.71	9.42	9.42	2	0.16	0.01	0.09	0.00	0.00	24.0
7	83	-11610	-1132	167	0	61	6170	15.71	15.71	9.42	9.42	2	0.16	0.01	0.09	0.00	0.00	24.0

8	83	-11500	-1283	-92	0	-196	6667	15.71	15.71	9.42	9.42	2	0.17	0.02	0.10	0.00	0.00	24.0
9	83	-11629	-1303	177	0	59	6815	15.71	15.71	9.42	9.42	2	0.17	0.02	0.11	0.00	0.00	24.0
10	83	-11519	-919	-20	0	-103	5320	15.71	15.71	9.42	9.42	2	0.14	0.01	0.07	0.00	0.00	24.0
11	83	-11551	-926	60	0	-27	5365	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
12	83	-11560	-1489	15	0	-108	7472	15.71	15.71	9.42	9.42	2	0.19	0.02	0.12	0.00	0.00	24.0
13	83	-11599	-1495	95	0	-31	7516	15.71	15.71	9.42	9.42	2	0.19	0.02	0.12	0.00	0.00	24.0
14	83	-11490	-1112	-102	0	-194	6021	15.71	15.71	9.42	9.42	2	0.16	0.01	0.09	0.00	0.00	24.0
15	83	-11610	-1132	167	0	61	6170	15.71	15.71	9.42	9.42	2	0.16	0.01	0.09	0.00	0.00	24.0
16	83	-11500	-1283	-92	0	-196	6667	15.71	15.71	9.42	9.42	2	0.17	0.02	0.10	0.00	0.00	24.0
17	83	-11629	-1303	177	0	59	6815	15.71	15.71	9.42	9.42	2	0.17	0.02	0.11	0.00	0.00	24.0
18	83	-27300	-2422	-26	0	-210	16717	15.71	15.71	9.42	9.42	3	0.29	0.03	0.17	0.00	0.00	24.0
19	83	-20052	-3727	107	0	-175	14678	15.71	15.71	9.42	9.42	3	0.26	0.05	0.28	0.00	0.00	24.0
20	83	-22392	-2858	106	0	-165	14652	15.71	15.71	9.42	9.42	3	0.26	0.04	0.21	0.00	0.00	24.0
37	83	-26950	-1497	-66	0	-187	15014	15.71	15.71	9.42	9.42	3	0.26	0.02	0.10	0.00	0.00	24.0
38	83	-14872	-3672	155	0	-129	11611	15.71	15.71	9.42	9.42	3	0.21	0.05	0.29	0.00	0.00	24.0
39	83	-18772	-2224	152	0	-111	11566	15.71	15.71	9.42	9.42	3	0.21	0.03	0.17	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	165	-14165	-1569	49	0	-128	7049	15.71	15.71	9.42	9.42	3	0.13	0.02	0.12	0.00	0.00	24.0
2	165	-10858	-919	-20	0	-87	4561	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
3	165	-10892	-926	60	0	-77	4601	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
4	165	-10900	-1489	15	0	-120	6244	15.71	15.71	9.42	9.42	2	0.16	0.02	0.12	0.00	0.00	24.0
5	165	-10938	-1495	95	0	-110	6283	15.71	15.71	9.42	9.42	2	0.16	0.02	0.12	0.00	0.00	24.0
6	165	-10829	-1112	-102	0	-110	5104	15.71	15.71	9.42	9.42	2	0.13	0.01	0.09	0.00	0.00	24.0
7	165	-10951	-1132	167	0	-77	5236	15.71	15.71	9.42	9.42	2	0.13	0.01	0.09	0.00	0.00	24.0
8	165	-10840	-1283	-92	0	-120	5609	15.71	15.71	9.42	9.42	2	0.14	0.02	0.11	0.00	0.00	24.0
9	165	-10968	-1303	177	0	-87	5740	15.71	15.71	9.42	9.42	2	0.15	0.02	0.11	0.00	0.00	24.0
10	165	-10858	-919	-20	0	-87	4561	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
11	165	-10892	-926	60	0	-77	4601	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
12	165	-10900	-1489	15	0	-120	6244	15.71	15.71	9.42	9.42	2	0.16	0.02	0.12	0.00	0.00	24.0
13	165	-10938	-1495	95	0	-110	6283	15.71	15.71	9.42	9.42	2	0.16	0.02	0.12	0.00	0.00	24.0
14	165	-10829	-1112	-102	0	-110	5104	15.71	15.71	9.42	9.42	2	0.13	0.01	0.09	0.00	0.00	24.0
15	165	-10951	-1132	167	0	-77	5236	15.71	15.71	9.42	9.42	2	0.13	0.01	0.09	0.00	0.00	24.0
16	165	-10840	-1283	-92	0	-120	5609	15.71	15.71	9.42	9.42	2	0.14	0.02	0.11	0.00	0.00	24.0
17	165	-10968	-1303	177	0	-87	5740	15.71	15.71	9.42	9.42	2	0.15	0.02	0.11	0.00	0.00	24.0
18	165	-26440	-2800	-26	0	-189	14562	15.71	15.71	9.42	9.42	3	0.25	0.03	0.19	0.00	0.00	24.0
19	165	-19195	-3350	107	0	-264	11758	15.71	15.71	9.42	9.42	3	0.21	0.04	0.25	0.00	0.00	24.0
20	165	-21535	-2858	106	0	-252	12293	15.71	15.71	9.42	9.42	3	0.22	0.04	0.21	0.00	0.00	24.0
37	165	-26090	-2126	-66	0	-133	13519	15.71	15.71	9.42	9.42	3	0.23	0.03	0.15	0.00	0.00	24.0
38	165	-14015	-3043	155	0	-257	8841	15.71	15.71	9.42	9.42	3	0.16	0.04	0.24	0.00	0.00	24.0
39	165	-17915	-2224	152	0	-236	9733	15.71	15.71	9.42	9.42	3	0.17	0.03	0.17	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	248	-13308	-1569	49	0	-168	5754	15.71	15.71	9.42	9.42	3	0.11	0.02	0.13	0.00	0.00	24.0
2	248	-10197	-919	-20	0	-70	3802	15.71	15.71	9.42	9.42	2	0.10	0.01	0.08	0.00	0.00	24.0
3	248	-10232	-926	60	0	-126	3837	15.71	15.71	9.42	9.42	2	0.10	0.01	0.08	0.00	0.00	24.0
4	248	-10240	-1489	15	0	-132	5015	15.71	15.71	9.42	9.42	2	0.13	0.02	0.12	0.00	0.00	24.0
5	248	-10278	-1495	95	0	-189	5050	15.71	15.71	9.42	9.42	2	0.13	0.02	0.12	0.00	0.00	24.0
6	248	-10168	-1112	-102	0	-26	4187	15.71	15.71	9.42	9.42	2	0.11	0.01	0.09	0.00	0.00	24.0
7	248	-10292	-1132	167	0	-214	4302	15.71	15.71	9.42	9.42	2	0.11	0.01	0.09	0.00	0.00	24.0
8	248	-10181	-1283	-92	0	-44	4551	15.71	15.71	9.42	9.42	2	0.12	0.02	0.11	0.00	0.00	24.0
9	248	-10306	-1303	177	0	-233	4666	15.71	15.71	9.42	9.42	2	0.12	0.02	0.11	0.00	0.00	24.0
10	248	-10197	-919	-20	0	-70	3802	15.71	15.71	9.42	9.42	2	0.10	0.01	0.08	0.00	0.00	24.0
11	248	-10232	-926	60	0	-126	3837	15.71	15.71	9.42	9.42	2	0.10	0.01	0.08	0.00	0.00	24.0
12	248	-10240	-1489	15	0	-132	5015	15.71	15.71	9.42	9.42	2	0.13	0.02	0.12	0.00	0.00	24.0
13	248	-10278	-1495	95	0	-189	5050	15.71	15.71	9.42	9.42	2	0.13	0.02	0.12	0.00	0.00	24.0
14	248	-10168	-1112	-102	0	-26	4187	15.71	15.71	9.42	9.42	2	0.11	0.01	0.09	0.00	0.00	24.0
15	248	-10292	-1132	167	0	-214	4302	15.71	15.71	9.42	9.42	2	0.11	0.01	0.09	0.00	0.00	24.0
16	248	-10181	-1283	-92	0	-44	4551	15.71	15.71	9.42	9.42	2	0.12	0.02	0.11	0.00	0.00	24.0
17	248	-10306	-1303	177	0	-233	4666	15.71	15.71	9.42	9.42	2	0.12	0.02	0.11	0.00	0.00	24.0
18	248	-25580	-3177	-26	0	-168	12097	15.71	15.71	9.42	9.42	3	0.21	0.04	0.22	0.00	0.00	24.0
19	248	-18338	-2973	107	0	-352	9148	15.71	15.71	9.42	9.42	3	0.16	0.04	0.22	0.00	0.00	24.0
20	248	-20678	-2858	106	0	-339	9934	15.71	15.71	9.42	9.42	3	0.18	0.04	0.21	0.00	0.00	24.0
37	248	-25230	-2754	-66	0	-78	11506	15.71	15.71	9.42	9.42	3	0.20	0.03	0.19	0.00	0.00	24.0
38	248	-13158	-2414	155	0	-384	6590	15.71	15.71	9.42	9.42	3	0.12	0.03	0.19	0.00	0.00	24.0
39	248	-17058	-2224	152	0	-362	7899	15.71	15.71	9.42	9.42	3	0.14	0.03	0.17	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	330	-12450	-1569	49	0	-208	4459	15.71	15.71	9.42	9.42	3	0.08	0.02	0.13	0.00	0.00	24.0
2	330	-9536	-919	-20	0	-53	3044	15.71	15.71	9.42	9.42	2	0.08	0.01	0.08	0.00	0.00	24.0
3	330	-9573	-926	60	0	-176	3074	15.71	15.71	9.42	9.42	2	0.08	0.01	0.08	0.00	0.00	24.0
4	330	-9580	-1489	15	0	-144	3787	15.71	15.71	9.42	9.42	2	0.10	0.02	0.12	0.00	0.00	24.0
5	330	-9617	-1495	95	0	-268	3816	15.71	15.71	9.42	9.42	2	0.10	0.02	0.12	0.00	0.00	24.0
6	330	-9508	-1112	-102	0	59	3270	15.71	15.71	9.42	9.42	2	0.08	0.01	0.09	0.00	0.00	24.0
7	330	-9632	-1132	167	0	-352	3368	15.71	15.71	9.42	9.42	2	0.09	0.01	0.09	0.00	0.00	24.0
8	330	-9521	-1283	-92	0	31	3493	15.71	15.71	9.42	9.42	2	0.09	0.02	0.11	0.00	0.00	24.0
9	330	-9645	-1303	177	0	-379	3591	15.71	15.71	9.42	9.42	2	0.10	0.02	0.11	0.00	0.00	24.0
10	330	-9536	-919	-20	0	-53	3044	15.71	15.71	9.42	9.42	2	0.08	0.01	0.08	0.00	0.00	24.0
11	330	-9573	-926	60	0	-176	3074	15.71	15.71	9.42	9.42	2	0.08	0.01	0.08	0.00	0.00	24.0
12	330	-9580	-1489	15	0	-144	3787	15.71	15.71	9.42	9.42	2	0.10	0.02	0.12	0.00	0.00	24.0
13	330	-9617	-1495	95	0	-268	3816	15.71	15.71	9.42	9.42	2	0.10	0.02	0.12	0.00	0.00	24.0
14	330	-9508	-1112	-102	0	59	3270	15.71	15.71	9.42	9.42	2	0.08	0.01	0.09	0.00	0.00	24.0
15	330	-9632	-1132	167	0	-352	3368	15.71	15.71	9.42	9.42	2	0.09	0.01	0.09	0.00	0.00	24.0
16	330	-9521	-1283	-92	0	31	3493	15.71	15.71	9.42	9.42	2	0.09	0.02	0.11	0.00	0.00	24.0
17	330	-9645	-1303	177	0	-379	3591	15.71	15.71	9.42	9.42	2	0.10	0.02	0.11	0.00	0.00	24.0
18	330	-24720	-3554	-26	0	-147	9320	15.71	15.71	9.42	9.42	3	0.16	0.04	0.25	0.00	0.00	24.0
19	330	-17480	-2596	107	0	-440	6850	15.71	15.71	9.42	9.42	3	0.12	0.03	0.20	0.00	0.00	24.0
20	330	-19820	-2858	106	0	-426	7576	15.71	15.71	9.42	9.42	3	0.14	0.04	0.21	0.00	0.00	24.0
37	330	-24370	-3383	-66	0	-23	8974	15.71	15.71	9.42	9.42	3	0.16	0.04	0.24	0.00	0.00	24.0
38	330	-12300	-1786	155	0	-512	4857	15.71	15.71	9.42	9.42	3	0.09	0.02	0.14	0.00	0.00	24.0
39	330	-16200	-2224	152	0	-488	6066	15.71	15.71	9.42	9.42	3	0.11	0.03	0.17	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 32 NI 163 NF 162 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 4C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-16000	-1695	-138	0	-196	10120	15.71	15.71	9.42	9.42	3	0.18	0.02	0.13	0.00	0.00	24.0
2	0	-12340	-1005	-141	0	-230	6466	15.71	15.71	9.42	9.42	2	0.17	0.01	0.08	0.00	0.00	24.0
3	0	-12310	-990	-54	0	-68	6386	15.71	15.71	9.42	9.42	2	0.16	0.01	0.08	0.00	0.00	24.0

4	0	-12300	-1617	-158	0	-234	9183	15.71	15.71	9.42	9.42	2	0.24	0.02	0.13	0.00	0.00	24.0
5	0	-12260	-1602	-71	0	-72	9102	15.71	15.71	9.42	9.42	2	0.23	0.02	0.13	0.00	0.00	24.0
6	0	-12370	-1236	-249	0	-420	7511	15.71	15.71	9.42	9.42	2	0.20	0.02	0.10	0.00	0.00	24.0
7	0	-12250	-1187	41	0	119	7243	15.71	15.71	9.42	9.42	2	0.18	0.02	0.10	0.00	0.00	24.0
8	0	-12360	-1420	-254	0	-421	8326	15.71	15.71	9.42	9.42	2	0.22	0.02	0.11	0.00	0.00	24.0
9	0	-12240	-1371	36	0	118	8058	15.71	15.71	9.42	9.42	2	0.20	0.02	0.11	0.00	0.00	24.0
10	0	-12340	-1005	-141	0	-230	6466	15.71	15.71	9.42	9.42	2	0.17	0.01	0.08	0.00	0.00	24.0
11	0	-12310	-990	-54	0	-68	6386	15.71	15.71	9.42	9.42	2	0.16	0.01	0.08	0.00	0.00	24.0
12	0	-12300	-1617	-158	0	-234	9183	15.71	15.71	9.42	9.42	2	0.24	0.02	0.13	0.00	0.00	24.0
13	0	-12260	-1602	-71	0	-72	9102	15.71	15.71	9.42	9.42	2	0.23	0.02	0.13	0.00	0.00	24.0
14	0	-12370	-1236	-249	0	-420	7511	15.71	15.71	9.42	9.42	2	0.20	0.02	0.10	0.00	0.00	24.0
15	0	-12250	-1187	41	0	119	7243	15.71	15.71	9.42	9.42	2	0.18	0.02	0.10	0.00	0.00	24.0
16	0	-12360	-1420	-254	0	-421	8326	15.71	15.71	9.42	9.42	2	0.22	0.02	0.11	0.00	0.00	24.0
17	0	-12240	-1371	36	0	118	8058	15.71	15.71	9.42	9.42	2	0.20	0.02	0.11	0.00	0.00	24.0
18	0	-28510	-2237	-360	0	-538	19390	15.71	15.71	9.42	9.42	3	0.33	0.03	0.15	0.00	0.00	24.0
19	0	-20970	-4397	-302	0	-394	18910	15.71	15.71	9.42	9.42	3	0.33	0.06	0.32	0.00	0.00	24.0
20	0	-23310	-3040	-205	0	-300	17610	15.71	15.71	9.42	9.42	3	0.31	0.04	0.22	0.00	0.00	24.0
37	0	-28230	-988	-316	0	-498	16620	15.71	15.71	9.42	9.42	3	0.29	0.01	0.07	0.00	0.00	24.0
38	0	-15670	-4588	-219	0	-257	15820	15.71	15.71	9.42	9.42	3	0.29	0.06	0.36	0.00	0.00	24.0
39	0	-19550	-2326	-57	0	-100	13640	15.71	15.71	9.42	9.42	3	0.24	0.03	0.17	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	83	-15140	-1695	-138	0	-82	8722	15.71	15.71	9.42	9.42	3	0.16	0.02	0.13	0.00	0.00	24.0
2	83	-11681	-1005	-141	0	-114	5637	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
3	83	-11650	-990	-54	0	-24	5569	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
4	83	-11640	-1617	-158	0	-103	7849	15.71	15.71	9.42	9.42	2	0.20	0.02	0.13	0.00	0.00	24.0
5	83	-11601	-1602	-71	0	-13	7780	15.71	15.71	9.42	9.42	2	0.20	0.02	0.13	0.00	0.00	24.0
6	83	-11710	-1236	-249	0	-215	6491	15.71	15.71	9.42	9.42	2	0.17	0.02	0.10	0.00	0.00	24.0
7	83	-11591	-1187	41	0	85	6263	15.71	15.71	9.42	9.42	2	0.16	0.02	0.10	0.00	0.00	24.0
8	83	-11699	-1420	-254	0	-212	7155	15.71	15.71	9.42	9.42	2	0.19	0.02	0.12	0.00	0.00	24.0
9	83	-11580	-1371	36	0	88	6927	15.71	15.71	9.42	9.42	2	0.18	0.02	0.11	0.00	0.00	24.0
10	83	-11681	-1005	-141	0	-114	5637	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
11	83	-11650	-990	-54	0	-24	5569	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
12	83	-11640	-1617	-158	0	-103	7849	15.71	15.71	9.42	9.42	2	0.20	0.02	0.13	0.00	0.00	24.0
13	83	-11601	-1602	-71	0	-13	7780	15.71	15.71	9.42	9.42	2	0.20	0.02	0.13	0.00	0.00	24.0
14	83	-11710	-1236	-249	0	-215	6491	15.71	15.71	9.42	9.42	2	0.17	0.02	0.10	0.00	0.00	24.0
15	83	-11591	-1187	41	0	85	6263	15.71	15.71	9.42	9.42	2	0.16	0.02	0.10	0.00	0.00	24.0
16	83	-11699	-1420	-254	0	-212	7155	15.71	15.71	9.42	9.42	2	0.19	0.02	0.12	0.00	0.00	24.0
17	83	-11580	-1371	36	0	88	6927	15.71	15.71	9.42	9.42	2	0.18	0.02	0.11	0.00	0.00	24.0
18	83	-27652	-2614	-360	0	-241	17390	15.71	15.71	9.42	9.42	3	0.30	0.03	0.18	0.00	0.00	24.0
19	83	-20112	-4020	-302	0	-145	15438	15.71	15.71	9.42	9.42	3	0.27	0.05	0.30	0.00	0.00	24.0
20	83	-22450	-3040	-205	0	-131	15101	15.71	15.71	9.42	9.42	3	0.26	0.04	0.22	0.00	0.00	24.0
37	83	-27372	-1617	-316	0	-237	15546	15.71	15.71	9.42	9.42	3	0.27	0.02	0.11	0.00	0.00	24.0
38	83	-14810	-3960	-219	0	-77	12293	15.71	15.71	9.42	9.42	3	0.22	0.05	0.31	0.00	0.00	24.0
39	83	-18692	-2326	-57	0	-53	11721	15.71	15.71	9.42	9.42	3	0.21	0.03	0.17	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	165	-14280	-1695	-138	0	32	7324	15.71	15.71	9.42	9.42	3	0.13	0.02	0.13	0.00	0.00	24.0
2	165	-11022	-1005	-141	0	3	4808	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
3	165	-10990	-990	-54	0	21	4752	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
4	165	-10980	-1617	-158	0	28	6515	15.71	15.71	9.42	9.42	2	0.17	0.02	0.13	0.00	0.00	24.0
5	165	-10942	-1602	-71	0	46	6458	15.71	15.71	9.42	9.42	2	0.16	0.02	0.13	0.00	0.00	24.0
6	165	-11050	-1236	-249	0	-10	5471	15.71	15.71	9.42	9.42	2	0.14	0.02	0.10	0.00	0.00	24.0
7	165	-10932	-1187	41	0	51	5284	15.71	15.71	9.42	9.42	2	0.13	0.02	0.10	0.00	0.00	24.0
8	165	-11038	-1420	-254	0	-3	5984	15.71	15.71	9.42	9.42	2	0.15	0.02	0.12	0.00	0.00	24.0
9	165	-10920	-1371	36	0	59	5796	15.71	15.71	9.42	9.42	2	0.15	0.02	0.11	0.00	0.00	24.0
10	165	-11022	-1005	-141	0	3	4808	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
11	165	-10990	-990	-54	0	21	4752	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
12	165	-10980	-1617	-158	0	28	6515	15.71	15.71	9.42	9.42	2	0.17	0.02	0.13	0.00	0.00	24.0
13	165	-10942	-1602	-71	0	46	6458	15.71	15.71	9.42	9.42	2	0.16	0.02	0.13	0.00	0.00	24.0
14	165	-11050	-1236	-249	0	-10	5471	15.71	15.71	9.42	9.42	2	0.14	0.02	0.10	0.00	0.00	24.0
15	165	-10932	-1187	41	0	51	5284	15.71	15.71	9.42	9.42	2	0.13	0.02	0.10	0.00	0.00	24.0
16	165	-11038	-1420	-254	0	-3	5984	15.71	15.71	9.42	9.42	2	0.15	0.02	0.12	0.00	0.00	24.0
17	165	-10920	-1371	36	0	59	5796	15.71	15.71	9.42	9.42	2	0.15	0.02	0.11	0.00	0.00	24.0
18	165	-26795	-2991	-360	0	56	15078	15.71	15.71	9.42	9.42	3	0.26	0.04	0.21	0.00	0.00	24.0
19	165	-19255	-3642	-302	0	104	12277	15.71	15.71	9.42	9.42	3	0.22	0.05	0.27	0.00	0.00	24.0
20	165	-21590	-3040	-205	0	38	12592	15.71	15.71	9.42	9.42	3	0.22	0.04	0.22	0.00	0.00	24.0
37	165	-26515	-2246	-316	0	24	13953	15.71	15.71	9.42	9.42	3	0.24	0.03	0.16	0.00	0.00	24.0
38	165	-13950	-3331	-219	0	104	9285	15.71	15.71	9.42	9.42	3	0.17	0.04	0.26	0.00	0.00	24.0
39	165	-17835	-2326	-57	0	-6	9803	15.71	15.71	9.42	9.42	3	0.17	0.03	0.18	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	248	-13420	-1695	-138	0	146	5926	15.71	15.71	9.42	9.42	3	0.11	0.02	0.13	0.00	0.00	24.0
2	248	-10363	-1005	-141	0	119	3979	15.71	15.71	9.42	9.42	2	0.10	0.01	0.08	0.00	0.00	24.0
3	248	-10329	-990	-54	0	66	3935	15.71	15.71	9.42	9.42	2	0.10	0.01	0.08	0.00	0.00	24.0
4	248	-10319	-1617	-158	0	158	5182	15.71	15.71	9.42	9.42	2	0.14	0.02	0.13	0.00	0.00	24.0
5	248	-10283	-1602	-71	0	105	5137	15.71	15.71	9.42	9.42	2	0.13	0.02	0.13	0.00	0.00	24.0
6	248	-10389	-1236	-249	0	195	4452	15.71	15.71	9.42	9.42	2	0.12	0.02	0.10	0.00	0.00	24.0
7	248	-10272	-1187	41	0	17	4304	15.71	15.71	9.42	9.42	2	0.11	0.02	0.10	0.00	0.00	24.0
8	248	-10377	-1420	-254	0	207	4812	15.71	15.71	9.42	9.42	2	0.13	0.02	0.12	0.00	0.00	24.0
9	248	-10259	-1371	36	0	29	4665	15.71	15.71	9.42	9.42	2	0.12	0.02	0.11	0.00	0.00	24.0
10	248	-10363	-1005	-141	0	119	3979	15.71	15.71	9.42	9.42	2	0.10	0.01	0.08	0.00	0.00	24.0
11	248	-10329	-990	-54	0	66	3935	15.71	15.71	9.42	9.42	2	0.10	0.01	0.08	0.00	0.00	24.0
12	248	-10319	-1617	-158	0	158	5182	15.71	15.71	9.42	9.42	2	0.14	0.02	0.13	0.00	0.00	24.0
13	248	-10283	-1602	-71	0	105	5137	15.71	15.71	9.42	9.42	2	0.13	0.02	0.13	0.00	0.00	24.0
14	248	-10389	-1236	-249	0	195	4452	15.71	15.71	9.42	9.42	2	0.12	0.02	0.10	0.00	0.00	24.0
15	248	-10272	-1187	41	0	17	4304	15.71	15.71	9.42	9.42	2	0.11	0.02	0.10	0.00	0.00	24.0
16	248	-10377	-1420	-254	0	207	4812	15.71	15.71	9.42	9.42	2	0.13	0.02	0.12	0.00	0.00	24.0
17	248	-10259	-1371	36	0	29	4665	15.71	15.71	9.42	9.42	2	0.12	0.02	0.11	0.00	0.00	24.0
18	248	-25938	-3368	-360	0	353	12455	15.71	15.71	9.42	9.42	3	0.22	0.04	0.24	0.00	0.00	24.0
19	248	-18398	-3265	-302	0	353	9427	15.71	15.71	9.42	9.42	3	0.17	0.04	0.25	0.00	0.00	24.0
20	248	-20730	-3040	-205	0	207	10083	15.71	15.71	9.42	9.42	3	0.18	0.04	0.22	0.00	0.00	24.0
37	248	-25658	-2874	-316	0	285	11841	15.71	15.71	9.42	9.42	3	0.21	0.04	0.20	0.00	0.00	24.0
38	248	-13090	-2702	-219	0	284	6795	15.71	15.71	9.42	9.42	3	0.12	0.03	0.22	0.00	0.00	24.0
39	248	-16978	-2326	-57	0	41	7884	15.71	15.71	9.42	9.42	3	0.14	0.03	0.18	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	330	-12560	-1695	-138	0	260	4528	15.71	15.71	9.42	9.42	3	0.08	0.02	0.14	0.00	0.00	24.0
2	330	-9704	-1005	-141	0	236	3150	15.71	15.71	9.42	9.42	2	0.09	0.01	0.08	0.00	0.00	24.0
3	330	-9669	-990	-54	0	110	3118	15.71	15.71	9.42	9.42	2	0.08	0.01	0.08	0.00	0.00	24.0
4	330	-9659	-1617	-158	0	289	3848	15.71	15.71	9.42	9.42	2	0.11	0.02	0.13	0.00	0.00	24.0
5	330	-9624	-1602	-71	0	164	3815	15.71	15.71	9.42	9.42	2	0.10	0.02	0.13	0.00	0.00	24.0
6	330	-9729	-1236	-249	0	400	3432	15.71	15.71	9.42	9.42	2	0.10	0.02	0.10	0.00	0.00	24.0
7	330	-9613	-1187	41	0	-17	3324	15.71	15.71	9.42	9.42	2	0.09	0.02	0.10	0.00	0.00	24.0
8	330	-9716	-1420	-254	0	416	3641	15.71	15.71	9.42	9.42	2	0.10	0.02	0.12	0.00	0.00	24.0
9	330	-9599	-1371	36	0	-1	3534	15.71	15.71	9.42	9.42	2	0.09	0.02	0.11	0.00	0.00	24.0

10	330	-9704	-1005	-141	0	236	3150	15.71	15.71	9.42	9.42	2	0.09	0.01	0.08	0.00	0.00	24.0
11	330	-9669	-990	-54	0	110	3118	15.71	15.71	9.42	9.42	2	0.08	0.01	0.08	0.00	0.00	24.0
12	330	-9659	-1617	-158	0	289	3848	15.71	15.71	9.42	9.42	2	0.11	0.02	0.13	0.00	0.00	24.0
13	330	-9624	-1602	-71	0	164	3815	15.71	15.71	9.42	9.42	2	0.10	0.02	0.13	0.00	0.00	24.0
14	330	-9729	-1236	-249	0	400	3432	15.71	15.71	9.42	9.42	2	0.10	0.02	0.10	0.00	0.00	24.0
15	330	-9613	-1187	41	0	-17	3324	15.71	15.71	9.42	9.42	2	0.09	0.02	0.10	0.00	0.00	24.0
16	330	-9716	-1420	-254	0	416	3641	15.71	15.71	9.42	9.42	2	0.10	0.02	0.12	0.00	0.00	24.0
17	330	-9599	-1371	36	0	-1	3534	15.71	15.71	9.42	9.42	2	0.09	0.02	0.11	0.00	0.00	24.0
18	330	-25080	-3745	-360	0	651	9521	15.71	15.71	9.42	9.42	3	0.17	0.05	0.26	0.00	0.00	24.0
19	330	-17540	-2888	-302	0	602	6889	15.71	15.71	9.42	9.42	3	0.13	0.04	0.22	0.00	0.00	24.0
20	330	-19870	-3040	-205	0	376	7574	15.71	15.71	9.42	9.42	3	0.14	0.04	0.23	0.00	0.00	24.0
37	330	-24800	-3503	-316	0	546	9211	15.71	15.71	9.42	9.42	3	0.16	0.04	0.25	0.00	0.00	24.0
38	330	-12230	-2074	-219	0	464	4824	15.71	15.71	9.42	9.42	3	0.09	0.03	0.17	0.00	0.00	24.0
39	330	-16120	-2326	-57	0	88	5966	15.71	15.71	9.42	9.42	3	0.11	0.03	0.18	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 33 NI 206 NF 205 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 3C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-15680	-1547	-227	0	-271	9453	15.71	15.71	9.42	9.42	3	0.17	0.02	0.12	0.00	0.00	24.0
2	0	-12060	-883	-214	0	-307	5873	15.71	15.71	9.42	9.42	2	0.15	0.01	0.07	0.00	0.00	24.0
3	0	-12070	-884	-106	0	-117	5879	15.71	15.71	9.42	9.42	2	0.15	0.01	0.07	0.00	0.00	24.0
4	0	-12060	-1497	-243	0	-301	8663	15.71	15.71	9.42	9.42	2	0.22	0.02	0.12	0.00	0.00	24.0
5	0	-12070	-1498	-136	0	-111	8669	15.71	15.71	9.42	9.42	2	0.22	0.02	0.12	0.00	0.00	24.0
6	0	-12060	-1097	-349	0	-526	6843	15.71	15.71	9.42	9.42	2	0.18	0.01	0.09	0.00	0.00	24.0
7	0	-12070	-1100	8	0	107	6863	15.71	15.71	9.42	9.42	2	0.17	0.01	0.09	0.00	0.00	24.0
8	0	-12060	-1281	-358	0	-524	7680	15.71	15.71	9.42	9.42	2	0.21	0.02	0.10	0.00	0.00	24.0
9	0	-12070	-1284	-1	0	109	7700	15.71	15.71	9.42	9.42	2	0.20	0.02	0.10	0.00	0.00	24.0
10	0	-12060	-883	-214	0	-307	5873	15.71	15.71	9.42	9.42	2	0.15	0.01	0.07	0.00	0.00	24.0
11	0	-12070	-884	-106	0	-117	5879	15.71	15.71	9.42	9.42	2	0.15	0.01	0.07	0.00	0.00	24.0
12	0	-12060	-1497	-243	0	-301	8663	15.71	15.71	9.42	9.42	2	0.22	0.02	0.12	0.00	0.00	24.0
13	0	-12070	-1498	-136	0	-111	8669	15.71	15.71	9.42	9.42	2	0.22	0.02	0.12	0.00	0.00	24.0
14	0	-12060	-1097	-349	0	-526	6843	15.71	15.71	9.42	9.42	2	0.18	0.01	0.09	0.00	0.00	24.0
15	0	-12070	-1100	8	0	107	6863	15.71	15.71	9.42	9.42	2	0.17	0.01	0.09	0.00	0.00	24.0
16	0	-12060	-1281	-358	0	-524	7680	15.71	15.71	9.42	9.42	2	0.21	0.02	0.10	0.00	0.00	24.0
17	0	-12070	-1284	-1	0	109	7700	15.71	15.71	9.42	9.42	2	0.20	0.02	0.10	0.00	0.00	24.0
18	0	-27920	-1959	-541	0	-768	18040	15.71	15.71	9.42	9.42	3	0.31	0.02	0.13	0.00	0.00	24.0
19	0	-20530	-4131	-483	0	-526	17830	15.71	15.71	9.42	9.42	3	0.32	0.05	0.30	0.00	0.00	24.0
20	0	-22910	-2821	-323	0	-398	16650	15.71	15.71	9.42	9.42	3	0.29	0.04	0.20	0.00	0.00	24.0
37	0	-27660	-746	-467	0	-726	15360	15.71	15.71	9.42	9.42	3	0.27	0.01	0.05	0.00	0.00	24.0
38	0	-15340	-4367	-370	0	-321	15000	15.71	15.71	9.42	9.42	3	0.27	0.06	0.34	0.00	0.00	24.0
39	0	-19310	-2183	-104	0	-108	13050	15.71	15.71	9.42	9.42	3	0.23	0.03	0.16	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	83	-14822	-1547	-227	0	-84	8176	15.71	15.71	9.42	9.42	3	0.15	0.02	0.12	0.00	0.00	24.0
2	83	-11400	-883	-214	0	-130	5144	15.71	15.71	9.42	9.42	2	0.13	0.01	0.07	0.00	0.00	24.0
3	83	-11409	-884	-106	0	-29	5150	15.71	15.71	9.42	9.42	2	0.13	0.01	0.07	0.00	0.00	24.0
4	83	-11401	-1497	-243	0	-100	7429	15.71	15.71	9.42	9.42	2	0.19	0.02	0.12	0.00	0.00	24.0
5	83	-11410	-1498	-136	0	1	7434	15.71	15.71	9.42	9.42	2	0.19	0.02	0.12	0.00	0.00	24.0
6	83	-11399	-1097	-349	0	-238	5938	15.71	15.71	9.42	9.42	2	0.16	0.01	0.09	0.00	0.00	24.0
7	83	-11411	-1100	8	0	100	5956	15.71	15.71	9.42	9.42	2	0.15	0.01	0.09	0.00	0.00	24.0
8	83	-11399	-1281	-358	0	-229	6623	15.71	15.71	9.42	9.42	2	0.17	0.02	0.10	0.00	0.00	24.0
9	83	-11411	-1284	-1	0	109	6641	15.71	15.71	9.42	9.42	2	0.17	0.02	0.10	0.00	0.00	24.0
10	83	-11400	-883	-214	0	-130	5144	15.71	15.71	9.42	9.42	2	0.13	0.01	0.07	0.00	0.00	24.0
11	83	-11409	-884	-106	0	-29	5150	15.71	15.71	9.42	9.42	2	0.13	0.01	0.07	0.00	0.00	24.0
12	83	-11401	-1497	-243	0	-100	7429	15.71	15.71	9.42	9.42	2	0.19	0.02	0.12	0.00	0.00	24.0
13	83	-11410	-1498	-136	0	1	7434	15.71	15.71	9.42	9.42	2	0.19	0.02	0.12	0.00	0.00	24.0
14	83	-11399	-1097	-349	0	-238	5938	15.71	15.71	9.42	9.42	2	0.16	0.01	0.09	0.00	0.00	24.0
15	83	-11411	-1100	8	0	100	5956	15.71	15.71	9.42	9.42	2	0.15	0.01	0.09	0.00	0.00	24.0
16	83	-11399	-1281	-358	0	-229	6623	15.71	15.71	9.42	9.42	2	0.17	0.02	0.10	0.00	0.00	24.0
17	83	-11411	-1284	-1	0	109	6641	15.71	15.71	9.42	9.42	2	0.17	0.02	0.10	0.00	0.00	24.0
18	83	-27062	-2336	-541	0	-322	16268	15.71	15.71	9.42	9.42	3	0.28	0.03	0.16	0.00	0.00	24.0
19	83	-19672	-3754	-483	0	-127	14576	15.71	15.71	9.42	9.42	3	0.26	0.05	0.28	0.00	0.00	24.0
20	83	-22052	-2821	-323	0	-131	14324	15.71	15.71	9.42	9.42	3	0.25	0.04	0.20	0.00	0.00	24.0
37	83	-26800	-1375	-467	0	-341	14484	15.71	15.71	9.42	9.42	3	0.25	0.02	0.10	0.00	0.00	24.0
38	83	-14482	-3738	-370	0	-16	11657	15.71	15.71	9.42	9.42	3	0.21	0.05	0.29	0.00	0.00	24.0
39	83	-18452	-2183	-104	0	-22	11248	15.71	15.71	9.42	9.42	3	0.20	0.03	0.16	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	165	-13965	-1547	-227	0	104	6900	15.71	15.71	9.42	9.42	3	0.13	0.02	0.12	0.00	0.00	24.0
2	165	-10740	-883	-214	0	46	4416	15.71	15.71	9.42	9.42	2	0.11	0.01	0.07	0.00	0.00	24.0
3	165	-10748	-884	-106	0	59	4420	15.71	15.71	9.42	9.42	2	0.11	0.01	0.07	0.00	0.00	24.0
4	165	-10742	-1497	-243	0	101	6194	15.71	15.71	9.42	9.42	2	0.16	0.02	0.12	0.00	0.00	24.0
5	165	-10750	-1498	-136	0	114	6199	15.71	15.71	9.42	9.42	2	0.16	0.02	0.12	0.00	0.00	24.0
6	165	-10738	-1097	-349	0	50	5033	15.71	15.71	9.42	9.42	2	0.13	0.01	0.09	0.00	0.00	24.0
7	165	-10752	-1100	8	0	93	5048	15.71	15.71	9.42	9.42	2	0.13	0.01	0.09	0.00	0.00	24.0
8	165	-10738	-1281	-358	0	66	5566	15.71	15.71	9.42	9.42	2	0.14	0.02	0.11	0.00	0.00	24.0
9	165	-10752	-1284	-1	0	110	5582	15.71	15.71	9.42	9.42	2	0.14	0.02	0.11	0.00	0.00	24.0
10	165	-10740	-883	-214	0	46	4416	15.71	15.71	9.42	9.42	2	0.11	0.01	0.07	0.00	0.00	24.0
11	165	-10748	-884	-106	0	59	4420	15.71	15.71	9.42	9.42	2	0.11	0.01	0.07	0.00	0.00	24.0
12	165	-10742	-1497	-243	0	101	6194	15.71	15.71	9.42	9.42	2	0.16	0.02	0.12	0.00	0.00	24.0
13	165	-10750	-1498	-136	0	114	6199	15.71	15.71	9.42	9.42	2	0.16	0.02	0.12	0.00	0.00	24.0
14	165	-10738	-1097	-349	0	50	5033	15.71	15.71	9.42	9.42	2	0.13	0.01	0.09	0.00	0.00	24.0
15	165	-10752	-1100	8	0	93	5048	15.71	15.71	9.42	9.42	2	0.13	0.01	0.09	0.00	0.00	24.0
16	165	-10738	-1281	-358	0	66	5566	15.71	15.71	9.42	9.42	2	0.14	0.02	0.11	0.00	0.00	24.0
17	165	-10752	-1284	-1	0	110	5582	15.71	15.71	9.42	9.42	2	0.14	0.02	0.11	0.00	0.00	24.0
18	165	-26205	-2714	-541	0	124	14185	15.71	15.71	9.42	9.42	3	0.24	0.03	0.19	0.00	0.00	24.0
19	165	-18815	-3376	-483	0	271	11634	15.71	15.71	9.42	9.42	3	0.21	0.04	0.25	0.00	0.00	24.0
20	165	-21195	-2821	-323	0	136	11997	15.71	15.71	9.42	9.42	3	0.21	0.04	0.21	0.00	0.00	24.0
37	165	-25940	-2004	-467	0	45	13090	15.71	15.71	9.42	9.42	3	0.23	0.02	0.14	0.00	0.00	24.0
38	165	-13625	-3110	-370	0	289	8832	15.71	15.71	9.42	9.42	3	0.16	0.04	0.25	0.00	0.00	24.0
39	165	-17595	-2183	-104	0	64	9447	15.71	15.71	9.42	9.42	3	0.17	0.03	0.17	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	248	-13108	-1547	-227	0	291	5624	15.71	15.71	9.42	9.42	3	0.10	0.02	0.12	0.00	0.00	24.0
2	248	-10081	-883	-214	0	222	3687	15.71	15.71	9.42	9.42	2	0.10	0.01	0.07	0.00	0.00	24.0
3	248	-10087	-884	-106	0	146	3691	15.71	15.71	9.42	9.42	2	0.10	0.01	0.07	0.00	0.00	24.0
4	248	-10083	-1497	-243	0	301	4960	15.71	15.71	9.42	9.42	2	0.13	0.02	0.12	0.00	0.00	24.0
5	248	-10090	-1498	-136	0	226	4963	15.71	15.71	9.42	9.42	2	0.13	0.02	0.12	0.00	0.00	24.0

6	248	-10077	-1097	-349	0	338	4129	15.71	15.71	9.42	9.42	2	0.11	0.01	0.09	0.00	0.00	24.0
7	248	-10092	-1100	8	0	86	4141	15.71	15.71	9.42	9.42	2	0.11	0.01	0.09	0.00	0.00	24.0
8	248	-10078	-1281	-358	0	362	4510	15.71	15.71	9.42	9.42	2	0.12	0.02	0.11	0.00	0.00	24.0
9	248	-10093	-1284	-1	0	110	4522	15.71	15.71	9.42	9.42	2	0.12	0.02	0.11	0.00	0.00	24.0
10	248	-10081	-883	-214	0	222	3687	15.71	15.71	9.42	9.42	2	0.10	0.01	0.07	0.00	0.00	24.0
11	248	-10087	-884	-106	0	146	3691	15.71	15.71	9.42	9.42	2	0.10	0.01	0.07	0.00	0.00	24.0
12	248	-10083	-1497	-243	0	301	4960	15.71	15.71	9.42	9.42	2	0.13	0.02	0.12	0.00	0.00	24.0
13	248	-10090	-1498	-136	0	226	4963	15.71	15.71	9.42	9.42	2	0.13	0.02	0.12	0.00	0.00	24.0
14	248	-10077	-1097	-349	0	338	4129	15.71	15.71	9.42	9.42	2	0.11	0.01	0.09	0.00	0.00	24.0
15	248	-10092	-1100	8	0	86	4141	15.71	15.71	9.42	9.42	2	0.11	0.01	0.09	0.00	0.00	24.0
16	248	-10078	-1281	-358	0	362	4510	15.71	15.71	9.42	9.42	2	0.12	0.02	0.11	0.00	0.00	24.0
17	248	-10093	-1284	-1	0	110	4522	15.71	15.71	9.42	9.42	2	0.12	0.02	0.11	0.00	0.00	24.0
18	248	-25348	-3091	-541	0	571	11791	15.71	15.71	9.42	9.42	3	0.21	0.04	0.22	0.00	0.00	24.0
19	248	-17958	-2999	-483	0	669	9002	15.71	15.71	9.42	9.42	3	0.16	0.04	0.23	0.00	0.00	24.0
20	248	-20338	-2821	-323	0	402	9670	15.71	15.71	9.42	9.42	3	0.17	0.04	0.21	0.00	0.00	24.0
37	248	-25080	-2632	-467	0	430	11177	15.71	15.71	9.42	9.42	3	0.20	0.03	0.19	0.00	0.00	24.0
38	248	-12768	-2482	-370	0	594	6526	15.71	15.71	9.42	9.42	3	0.12	0.03	0.20	0.00	0.00	24.0
39	248	-16738	-2183	-104	0	150	7645	15.71	15.71	9.42	9.42	3	0.14	0.03	0.17	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	330	-12250	-1547	-227	0	479	4347	15.71	15.71	9.42	9.42	3	0.08	0.02	0.12	0.00	0.00	24.0
2	330	-9421	-883	-214	0	398	2959	15.71	15.71	9.42	9.42	2	0.09	0.01	0.07	0.00	0.00	24.0
3	330	-9426	-884	-106	0	234	2962	15.71	15.71	9.42	9.42	2	0.08	0.01	0.07	0.00	0.00	24.0
4	330	-9424	-1497	-243	0	502	3725	15.71	15.71	9.42	9.42	2	0.11	0.02	0.12	0.00	0.00	24.0
5	330	-9430	-1498	-136	0	338	3728	15.71	15.71	9.42	9.42	2	0.10	0.02	0.12	0.00	0.00	24.0
6	330	-9416	-1097	-349	0	626	3224	15.71	15.71	9.42	9.42	2	0.10	0.01	0.09	0.00	0.00	24.0
7	330	-9433	-1100	8	0	79	3234	15.71	15.71	9.42	9.42	2	0.08	0.01	0.09	0.00	0.00	24.0
8	330	-9417	-1281	-358	0	657	3453	15.71	15.71	9.42	9.42	2	0.11	0.02	0.11	0.00	0.00	24.0
9	330	-9434	-1284	-1	0	110	3463	15.71	15.71	9.42	9.42	2	0.09	0.02	0.11	0.00	0.00	24.0
10	330	-9421	-883	-214	0	398	2959	15.71	15.71	9.42	9.42	2	0.09	0.01	0.07	0.00	0.00	24.0
11	330	-9426	-884	-106	0	234	2962	15.71	15.71	9.42	9.42	2	0.08	0.01	0.07	0.00	0.00	24.0
12	330	-9424	-1497	-243	0	502	3725	15.71	15.71	9.42	9.42	2	0.11	0.02	0.12	0.00	0.00	24.0
13	330	-9430	-1498	-136	0	338	3728	15.71	15.71	9.42	9.42	2	0.10	0.02	0.12	0.00	0.00	24.0
14	330	-9416	-1097	-349	0	626	3224	15.71	15.71	9.42	9.42	2	0.10	0.01	0.09	0.00	0.00	24.0
15	330	-9433	-1100	8	0	79	3234	15.71	15.71	9.42	9.42	2	0.08	0.01	0.09	0.00	0.00	24.0
16	330	-9417	-1281	-358	0	657	3453	15.71	15.71	9.42	9.42	2	0.11	0.02	0.11	0.00	0.00	24.0
17	330	-9434	-1284	-1	0	110	3463	15.71	15.71	9.42	9.42	2	0.09	0.02	0.11	0.00	0.00	24.0
18	330	-24490	-3468	-541	0	1017	9085	15.71	15.71	9.42	9.42	3	0.16	0.04	0.25	0.00	0.00	24.0
19	330	-17100	-2622	-483	0	1067	6682	15.71	15.71	9.42	9.42	3	0.13	0.03	0.20	0.00	0.00	24.0
20	330	-19480	-2821	-323	0	669	7344	15.71	15.71	9.42	9.42	3	0.13	0.04	0.21	0.00	0.00	24.0
37	330	-24220	-3261	-467	0	815	8745	15.71	15.71	9.42	9.42	3	0.16	0.04	0.23	0.00	0.00	24.0
38	330	-11910	-1853	-370	0	900	4739	15.71	15.71	9.42	9.42	3	0.10	0.02	0.15	0.00	0.00	24.0
39	330	-15880	-2183	-104	0	236	5843	15.71	15.71	9.42	9.42	3	0.11	0.03	0.17	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 34 NI 249 NF 248 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 2C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-14490	-884	-442	0	-381	6441	15.71	15.71	9.42	9.42	3	0.12	0.01	0.07	0.00	0.00	24.0
2	0	-11180	-432	-378	0	-401	3857	15.71	15.71	9.42	9.42	2	0.11	0.01	0.04	0.00	0.00	24.0
3	0	-11240	-452	-280	0	-209	3962	15.71	15.71	9.42	9.42	2	0.10	0.01	0.04	0.00	0.00	24.0
4	0	-11060	-907	-400	0	-377	5947	15.71	15.71	9.42	9.42	2	0.16	0.01	0.07	0.00	0.00	24.0
5	0	-11120	-927	-302	0	-186	6052	15.71	15.71	9.42	9.42	2	0.16	0.01	0.08	0.00	0.00	24.0
6	0	-11070	-574	-500	0	-616	4466	15.71	15.71	9.42	9.42	2	0.13	0.01	0.05	0.00	0.00	24.0
7	0	-11270	-642	-174	0	22	4817	15.71	15.71	9.42	9.42	2	0.12	0.01	0.05	0.00	0.00	24.0
8	0	-11030	-717	-507	0	-609	5093	15.71	15.71	9.42	9.42	2	0.14	0.01	0.06	0.00	0.00	24.0
9	0	-11230	-785	-180	0	29	5443	15.71	15.71	9.42	9.42	2	0.14	0.01	0.06	0.00	0.00	24.0
10	0	-11180	-432	-378	0	-401	3857	15.71	15.71	9.42	9.42	2	0.11	0.01	0.04	0.00	0.00	24.0
11	0	-11240	-452	-280	0	-209	3962	15.71	15.71	9.42	9.42	2	0.10	0.01	0.04	0.00	0.00	24.0
12	0	-11060	-907	-400	0	-377	5947	15.71	15.71	9.42	9.42	2	0.16	0.01	0.07	0.00	0.00	24.0
13	0	-11120	-927	-302	0	-186	6052	15.71	15.71	9.42	9.42	2	0.16	0.01	0.08	0.00	0.00	24.0
14	0	-11070	-574	-500	0	-616	4466	15.71	15.71	9.42	9.42	2	0.13	0.01	0.05	0.00	0.00	24.0
15	0	-11270	-642	-174	0	22	4817	15.71	15.71	9.42	9.42	2	0.12	0.01	0.05	0.00	0.00	24.0
16	0	-11030	-717	-507	0	-609	5093	15.71	15.71	9.42	9.42	2	0.14	0.01	0.06	0.00	0.00	24.0
17	0	-11230	-785	-180	0	29	5443	15.71	15.71	9.42	9.42	2	0.14	0.01	0.06	0.00	0.00	24.0
18	0	-25650	-815	-1529	0	-1559	13030	15.71	15.71	9.42	9.42	3	0.24	0.02	0.09	0.00	0.00	24.0
19	0	-18100	-2709	-954	0	-839	11400	15.71	15.71	9.42	9.42	3	0.21	0.03	0.20	0.00	0.00	24.0
20	0	-20890	-1681	-1039	0	-906	11640	15.71	15.71	9.42	9.42	3	0.21	0.02	0.12	0.00	0.00	24.0
37	0	-25810	103	-1459	0	-1531	11690	15.71	15.71	9.42	9.42	3	0.21	0.02	0.08	0.00	0.00	24.0
38	0	-13240	-3053	-500	0	-331	8983	15.71	15.71	9.42	9.42	3	0.16	0.04	0.24	0.00	0.00	24.0
39	0	-17890	-1340	-642	0	-443	9367	15.71	15.71	9.42	9.42	3	0.17	0.02	0.10	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	83	-13632	-884	-442	0	-16	5712	15.71	15.71	9.42	9.42	3	0.10	0.01	0.07	0.00	0.00	24.0
2	83	-10520	-432	-378	0	-89	3501	15.71	15.71	9.42	9.42	2	0.09	0.01	0.04	0.00	0.00	24.0
3	83	-10580	-452	-280	0	22	3589	15.71	15.71	9.42	9.42	2	0.09	0.01	0.04	0.00	0.00	24.0
4	83	-10399	-907	-400	0	-47	5199	15.71	15.71	9.42	9.42	2	0.13	0.01	0.07	0.00	0.00	24.0
5	83	-10459	-927	-302	0	64	5287	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
6	83	-10410	-574	-500	0	-203	3992	15.71	15.71	9.42	9.42	2	0.11	0.01	0.05	0.00	0.00	24.0
7	83	-10609	-642	-174	0	165	4287	15.71	15.71	9.42	9.42	2	0.11	0.01	0.05	0.00	0.00	24.0
8	83	-10370	-717	-507	0	-191	4502	15.71	15.71	9.42	9.42	2	0.12	0.01	0.06	0.00	0.00	24.0
9	83	-10570	-785	-180	0	178	4796	15.71	15.71	9.42	9.42	2	0.13	0.01	0.06	0.00	0.00	24.0
10	83	-10520	-432	-378	0	-89	3501	15.71	15.71	9.42	9.42	2	0.09	0.01	0.04	0.00	0.00	24.0
11	83	-10580	-452	-280	0	22	3589	15.71	15.71	9.42	9.42	2	0.09	0.01	0.04	0.00	0.00	24.0
12	83	-10399	-907	-400	0	-47	5199	15.71	15.71	9.42	9.42	2	0.13	0.01	0.07	0.00	0.00	24.0
13	83	-10459	-927	-302	0	64	5287	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
14	83	-10410	-574	-500	0	-203	3992	15.71	15.71	9.42	9.42	2	0.11	0.01	0.05	0.00	0.00	24.0
15	83	-10609	-642	-174	0	165	4287	15.71	15.71	9.42	9.42	2	0.11	0.01	0.05	0.00	0.00	24.0
16	83	-10370	-717	-507	0	-191	4502	15.71	15.71	9.42	9.42	2	0.12	0.01	0.06	0.00	0.00	24.0
17	83	-10570	-785	-180	0	178	4796	15.71	15.71	9.42	9.42	2	0.13	0.01	0.06	0.00	0.00	24.0
18	83	-24790	-1192	-1529	0	-298	12202	15.71	15.71	9.42	9.42	3	0.21	0.02	0.09	0.00	0.00	24.0
19	83	-17242	-2332	-954	0	-52	9322	15.71	15.71	9.42	9.42	3	0.17	0.03	0.18	0.00	0.00	24.0
20	83	-20032	-1681	-1039	0	-49	10252	15.71	15.71	9.42	9.42	3	0.18	0.02	0.12	0.00	0.00	24.0
37	83	-24952	-525	-1459	0	-328	11517	15.71	15.71	9.42	9.42	3	0.20	0.02	0.08	0.00	0.00	24.0
38	83	-12381	-2424	-500	0	82	6724	15.71	15.71	9.42	9.42	3	0.12	0.03	0.20	0.00	0.00	24.0
39	83	-17030	-1340	-642	0	87	8262	15.71	15.71	9.42	9.42	3	0.15	0.02	0.10	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	165	-12775	-884	-442	0	348	4983	15.71	15.71	9.42	9.42	3	0.09	0.01	0.07	0.00	0.00	24.0

2	165	-9861	-432	-378	0	223	3144	15.71	15.71	9.42	9.42	2	0.09	0.01	0.04	0.00	0.00	24.0
3	165	-9920	-452	-280	0	253	3216	15.71	15.71	9.42	9.42	2	0.09	0.01	0.04	0.00	0.00	24.0
4	165	-9738	-907	-400	0	283	4450	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
5	165	-9798	-927	-302	0	313	4522	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
6	165	-9750	-574	-500	0	209	3518	15.71	15.71	9.42	9.42	2	0.09	0.01	0.05	0.00	0.00	24.0
7	165	-9948	-642	-174	0	309	3757	15.71	15.71	9.42	9.42	2	0.10	0.01	0.05	0.00	0.00	24.0
8	165	-9710	-717	-507	0	227	3910	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
9	165	-9910	-785	-180	0	327	4148	15.71	15.71	9.42	9.42	2	0.11	0.01	0.07	0.00	0.00	24.0
10	165	-9861	-432	-378	0	223	3144	15.71	15.71	9.42	9.42	2	0.09	0.01	0.04	0.00	0.00	24.0
11	165	-9920	-452	-280	0	253	3216	15.71	15.71	9.42	9.42	2	0.09	0.01	0.04	0.00	0.00	24.0
12	165	-9738	-907	-400	0	283	4450	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
13	165	-9798	-927	-302	0	313	4522	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
14	165	-9750	-574	-500	0	209	3518	15.71	15.71	9.42	9.42	2	0.09	0.01	0.05	0.00	0.00	24.0
15	165	-9948	-642	-174	0	309	3757	15.71	15.71	9.42	9.42	2	0.10	0.01	0.05	0.00	0.00	24.0
16	165	-9710	-717	-507	0	227	3910	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
17	165	-9910	-785	-180	0	327	4148	15.71	15.71	9.42	9.42	2	0.11	0.01	0.07	0.00	0.00	24.0
18	165	-23930	-1570	-1529	0	964	11063	15.71	15.71	9.42	9.42	3	0.20	0.02	0.11	0.00	0.00	24.0
19	165	-16385	-1954	-954	0	735	7555	15.71	15.71	9.42	9.42	3	0.14	0.02	0.15	0.00	0.00	24.0
20	165	-19175	-1681	-1039	0	809	8864	15.71	15.71	9.42	9.42	3	0.16	0.02	0.13	0.00	0.00	24.0
37	165	-24095	-1154	-1459	0	876	10825	15.71	15.71	9.42	9.42	3	0.19	0.02	0.08	0.00	0.00	24.0
38	165	-11522	-1796	-500	0	494	4983	15.71	15.71	9.42	9.42	3	0.09	0.02	0.15	0.00	0.00	24.0
39	165	-16170	-1340	-642	0	617	7156	15.71	15.71	9.42	9.42	3	0.13	0.02	0.10	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	248	-11918	-884	-442	0	713	4254	15.71	15.71	9.42	9.42	3	0.08	0.01	0.07	0.00	0.00	24.0
2	248	-9202	-432	-378	0	535	2788	15.71	15.71	9.42	9.42	2	0.09	0.01	0.04	0.00	0.00	24.0
3	248	-9261	-452	-280	0	484	2843	15.71	15.71	9.42	9.42	2	0.09	0.01	0.04	0.00	0.00	24.0
4	248	-9077	-907	-400	0	613	3702	15.71	15.71	9.42	9.42	2	0.11	0.01	0.08	0.00	0.00	24.0
5	248	-9137	-927	-302	0	562	3757	15.71	15.71	9.42	9.42	2	0.11	0.01	0.08	0.00	0.00	24.0
6	248	-9089	-574	-500	0	622	3044	15.71	15.71	9.42	9.42	2	0.09	0.01	0.05	0.00	0.00	24.0
7	248	-9288	-642	-174	0	452	3227	15.71	15.71	9.42	9.42	2	0.09	0.01	0.05	0.00	0.00	24.0
8	248	-9051	-717	-507	0	645	3318	15.71	15.71	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
9	248	-9249	-785	-180	0	476	3501	15.71	15.71	9.42	9.42	2	0.10	0.01	0.07	0.00	0.00	24.0
10	248	-9202	-432	-378	0	535	2788	15.71	15.71	9.42	9.42	2	0.09	0.01	0.04	0.00	0.00	24.0
11	248	-9261	-452	-280	0	484	2843	15.71	15.71	9.42	9.42	2	0.09	0.01	0.04	0.00	0.00	24.0
12	248	-9077	-907	-400	0	613	3702	15.71	15.71	9.42	9.42	2	0.11	0.01	0.08	0.00	0.00	24.0
13	248	-9137	-927	-302	0	562	3757	15.71	15.71	9.42	9.42	2	0.11	0.01	0.08	0.00	0.00	24.0
14	248	-9089	-574	-500	0	622	3044	15.71	15.71	9.42	9.42	2	0.09	0.01	0.05	0.00	0.00	24.0
15	248	-9288	-642	-174	0	452	3227	15.71	15.71	9.42	9.42	2	0.09	0.01	0.05	0.00	0.00	24.0
16	248	-9051	-717	-507	0	645	3318	15.71	15.71	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
17	248	-9249	-785	-180	0	476	3501	15.71	15.71	9.42	9.42	2	0.10	0.01	0.07	0.00	0.00	24.0
18	248	-23070	-1947	-1529	0	2226	9613	15.71	15.71	9.42	9.42	3	0.19	0.02	0.14	0.00	0.00	24.0
19	248	-15528	-1577	-954	0	1523	6099	15.71	15.71	9.42	9.42	3	0.13	0.02	0.12	0.00	0.00	24.0
20	248	-18318	-1681	-1039	0	1666	7476	15.71	15.71	9.42	9.42	3	0.15	0.02	0.13	0.00	0.00	24.0
37	248	-23238	-1782	-1459	0	2079	9615	15.71	15.71	9.42	9.42	3	0.19	0.02	0.13	0.00	0.00	24.0
38	248	-10664	-1167	-500	0	907	3761	15.71	15.71	9.42	9.42	3	0.08	0.01	0.10	0.00	0.00	24.0
39	248	-15310	-1340	-642	0	1147	6051	15.71	15.71	9.42	9.42	3	0.12	0.02	0.10	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	330	-11060	-884	-442	0	1078	3525	15.71	15.71	9.42	9.42	3	0.08	0.01	0.07	0.00	0.00	24.0
2	330	-8542	-432	-378	0	846	2432	15.71	15.71	9.42	9.42	2	0.09	0.01	0.04	0.00	0.00	24.0
3	330	-8601	-452	-280	0	715	2470	15.71	15.71	9.42	9.42	2	0.08	0.01	0.04	0.00	0.00	24.0
4	330	-8416	-907	-400	0	944	2954	15.71	15.71	9.42	9.42	2	0.10	0.01	0.08	0.00	0.00	24.0
5	330	-8476	-927	-302	0	812	2992	15.71	15.71	9.42	9.42	2	0.10	0.01	0.08	0.00	0.00	24.0
6	330	-8429	-574	-500	0	1034	2570	15.71	15.71	9.42	9.42	2	0.10	0.01	0.05	0.00	0.00	24.0
7	330	-8627	-642	-174	0	595	2697	15.71	15.71	9.42	9.42	2	0.08	0.01	0.05	0.00	0.00	24.0
8	330	-8391	-717	-507	0	1063	2727	15.71	15.71	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
9	330	-8589	-785	-180	0	624	2853	15.71	15.71	9.42	9.42	2	0.09	0.01	0.07	0.00	0.00	24.0
10	330	-8542	-432	-378	0	846	2432	15.71	15.71	9.42	9.42	2	0.09	0.01	0.04	0.00	0.00	24.0
11	330	-8601	-452	-280	0	715	2470	15.71	15.71	9.42	9.42	2	0.08	0.01	0.04	0.00	0.00	24.0
12	330	-8416	-907	-400	0	944	2954	15.71	15.71	9.42	9.42	2	0.10	0.01	0.08	0.00	0.00	24.0
13	330	-8476	-927	-302	0	812	2992	15.71	15.71	9.42	9.42	2	0.10	0.01	0.08	0.00	0.00	24.0
14	330	-8429	-574	-500	0	1034	2570	15.71	15.71	9.42	9.42	2	0.10	0.01	0.05	0.00	0.00	24.0
15	330	-8627	-642	-174	0	595	2697	15.71	15.71	9.42	9.42	2	0.08	0.01	0.05	0.00	0.00	24.0
16	330	-8391	-717	-507	0	1063	2727	15.71	15.71	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
17	330	-8589	-785	-180	0	624	2853	15.71	15.71	9.42	9.42	2	0.09	0.01	0.07	0.00	0.00	24.0
18	330	-22210	-2324	-1529	0	3487	7852	15.71	15.71	9.42	9.42	3	0.19	0.03	0.17	0.00	0.00	24.0
19	330	-14670	-1200	-954	0	2310	4955	15.71	15.71	9.42	9.42	3	0.13	0.02	0.09	0.00	0.00	24.0
20	330	-17460	-1681	-1039	0	2524	6088	15.71	15.71	9.42	9.42	3	0.15	0.02	0.13	0.00	0.00	24.0
37	330	-22380	-2411	-1459	0	3283	7886	15.71	15.71	9.42	9.42	3	0.19	0.03	0.17	0.00	0.00	24.0
38	330	-9805	-538	-500	0	1320	3057	15.71	15.71	9.42	9.42	3	0.08	0.01	0.04	0.00	0.00	24.0
39	330	-14450	-1340	-642	0	1677	4946	15.71	15.71	9.42	9.42	3	0.11	0.02	0.11	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 35 NI 302 NF 291 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 1D
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-9624	-125	-429	0	-1283	650	6.28	6.28	9.42	9.42	3	0.09	0.01	0.05	0.00	0.00	24.0
2	0	-6990	108	-345	0	-1046	66	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
3	0	-6862	98	-317	0	-957	75	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
4	0	-7944	-291	-343	0	-1018	925	6.28	6.28	9.42	9.42	2	0.14	0.01	0.04	0.00	0.00	24.0
5	0	-7816	-300	-315	0	-928	935	6.28	6.28	9.42	9.42	2	0.14	0.01	0.04	0.00	0.00	24.0
6	0	-7473	-21	-377	0	-1140	355	6.28	6.28	9.42	9.42	2	0.09	0.01	0.05	0.00	0.00	24.0
7	0	-7046	-52	-283	0	-843	387	6.28	6.28	9.42	9.42	2	0.08	0.01	0.03	0.00	0.00	24.0
8	0	-7759	-140	-376	0	-1132	613	6.28	6.28	9.42	9.42	2	0.11	0.01	0.05	0.00	0.00	24.0
9	0	-7333	-172	-283	0	-834	645	6.28	6.28	9.42	9.42	2	0.10	0.01	0.03	0.00	0.00	24.0
10	0	-6990	108	-345	0	-1046	66	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
11	0	-6862	98	-317	0	-957	75	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
12	0	-7944	-291	-343	0	-1018	925	6.28	6.28	9.42	9.42	2	0.14	0.01	0.04	0.00	0.00	24.0
13	0	-7816	-300	-315	0	-928	935	6.28	6.28	9.42	9.42	2	0.14	0.01	0.04	0.00	0.00	24.0
14	0	-7473	-21	-377	0	-1140	355	6.28	6.28	9.42	9.42	2	0.09	0.01	0.05	0.00	0.00	24.0
15	0	-7046	-52	-283	0	-843	387	6.28	6.28	9.42	9.42	2	0.08	0.01	0.03	0.00	0.00	24.0
16	0	-7759	-140	-376	0	-1132	613	6.28	6.28	9.42	9.42	2	0.11	0.01	0.05	0.00	0.00	24.0
17	0	-7333	-172	-283	0	-834	645	6.28	6.28	9.42	9.42	2	0.10	0.01	0.03	0.00	0.00	24.0
18	0	-12570	1140	522	0	-1048	-943	6.28	6.28	9.42	9.42	3	0.10	0.03	0.11	0.00	0.00	24.0
19	0	-12550	-821	-86	0	-1122	1805	6.28	6.28	9.42	9.42	3	0.18	0.02	0.09	0.00	0.00	24.0
20	0	-11880	108	-7	0	-1209	469	6.28	6.28	9.42	9.42	3	0.07	0.00	0.01	0.00	0.00	24.0
37	0	-11610	1694	512	0	-1088	-1783	6.28	6.28	9.42	9.42	3	0.18	0.04	0.18	0.00	0.00	24.0
38	0	-11580	-1574	-502	0	-1212	2797	6.28	6.28	9.42	9.42	3	0.29	0.04	0.17	0.00	0.00	24.0
39	0	-10470	-26	-370	0	-1357	569	6.28	6.28	9.42	9.42	3	0.08	0.01	0.04	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	83	-9141	-125	-429	0	-929	547	6.28	6.28	9.42	9.42	3	0.07	0.01	0.05	0.00	0.00	24.0
2	83	-6619	108	-345	0	-761	155	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
3	83	-6491	98	-317	0	-695	156	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
4	83	-7573	-291	-343	0	-735	685	6.28	6.28	9.42	9.42	2	0.10	0.01	0.04	0.00	0.00	24.0
5	83	-7445	-300	-315	0	-669	687	6.28	6.28	9.42	9.42	2	0.10	0.01	0.04	0.00	0.00	24.0
6	83	-7102	-21	-377	0	-829	338	6.28	6.28	9.42	9.42	2	0.07	0.01	0.05	0.00	0.00	24.0
7	83	-6675	-52	-283	0	-609	344	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
8	83	-7388	-140	-376	0	-822	497	6.28	6.28	9.42	9.42	2	0.09	0.01	0.05	0.00	0.00	24.0
9	83	-6962	-172	-283	0	-601	503	6.28	6.28	9.42	9.42	2	0.08	0.01	0.03	0.00	0.00	24.0
10	83	-6619	108	-345	0	-761	155	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
11	83	-6491	98	-317	0	-695	156	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
12	83	-7573	-291	-343	0	-735	685	6.28	6.28	9.42	9.42	2	0.10	0.01	0.04	0.00	0.00	24.0
13	83	-7445	-300	-315	0	-669	687	6.28	6.28	9.42	9.42	2	0.10	0.01	0.04	0.00	0.00	24.0
14	83	-7102	-21	-377	0	-829	338	6.28	6.28	9.42	9.42	2	0.07	0.01	0.05	0.00	0.00	24.0
15	83	-6675	-52	-283	0	-609	344	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
16	83	-7388	-140	-376	0	-822	497	6.28	6.28	9.42	9.42	2	0.09	0.01	0.05	0.00	0.00	24.0
17	83	-6962	-172	-283	0	-601	503	6.28	6.28	9.42	9.42	2	0.08	0.01	0.03	0.00	0.00	24.0
18	83	-12088	951	522	0	-1479	-80	6.28	6.28	9.42	9.42	3	0.07	0.02	0.09	0.00	0.00	24.0
19	83	-12068	-632	-86	0	-1051	1206	6.28	6.28	9.42	9.42	3	0.13	0.02	0.07	0.00	0.00	24.0
20	83	-11398	108	104	0	-1250	558	6.28	6.28	9.42	9.42	3	0.08	0.00	0.01	0.00	0.00	24.0
37	83	-11128	1380	512	0	-1511	-515	6.28	6.28	9.42	9.42	3	0.09	0.03	0.13	0.00	0.00	24.0
38	83	-11098	-1260	-502	0	-798	1628	6.28	6.28	9.42	9.42	3	0.17	0.03	0.13	0.00	0.00	24.0
39	83	-9987	-26	-186	0	-1130	548	6.28	6.28	9.42	9.42	3	0.07	0.00	0.02	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	165	-8658	-125	-429	0	-576	444	6.28	6.28	9.42	9.42	3	0.05	0.01	0.05	0.00	0.00	24.0
2	165	-6248	108	-345	0	-477	244	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
3	165	-6120	98	-317	0	-434	237	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
4	165	-7202	-291	-343	0	-452	445	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
5	165	-7074	-300	-315	0	-409	439	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
6	165	-6730	-21	-377	0	-518	321	6.28	6.28	9.42	9.42	2	0.06	0.01	0.05	0.00	0.00	24.0
7	165	-6304	-52	-283	0	-375	301	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
8	165	-7016	-140	-376	0	-511	382	6.28	6.28	9.42	9.42	2	0.06	0.01	0.05	0.00	0.00	24.0
9	165	-6590	-172	-283	0	-368	361	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
10	165	-6248	108	-345	0	-477	244	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
11	165	-6120	98	-317	0	-434	237	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
12	165	-7202	-291	-343	0	-452	445	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
13	165	-7074	-300	-315	0	-409	439	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
14	165	-6730	-21	-377	0	-518	321	6.28	6.28	9.42	9.42	2	0.06	0.01	0.05	0.00	0.00	24.0
15	165	-6304	-52	-283	0	-375	301	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
16	165	-7016	-140	-376	0	-511	382	6.28	6.28	9.42	9.42	2	0.06	0.01	0.05	0.00	0.00	24.0
17	165	-6590	-172	-283	0	-368	361	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
18	165	-11605	763	522	0	-1910	627	6.28	6.28	9.42	9.42	3	0.11	0.02	0.07	0.00	0.00	24.0
19	165	-11585	-443	-86	0	-980	762	6.28	6.28	9.42	9.42	3	0.08	0.01	0.04	0.00	0.00	24.0
20	165	-10916	108	198	0	-1376	647	6.28	6.28	9.42	9.42	3	0.09	0.00	0.02	0.00	0.00	24.0
37	165	-10645	1065	512	0	-1934	493	6.28	6.28	9.42	9.42	3	0.10	0.03	0.10	0.00	0.00	24.0
38	165	-10616	-945	-502	0	-384	719	6.28	6.28	9.42	9.42	3	0.07	0.02	0.10	0.00	0.00	24.0
39	165	-9504	-26	-28	0	-1043	527	6.28	6.28	9.42	9.42	3	0.07	0.00	0.00	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	248	-8176	-125	-429	0	-222	340	6.28	6.28	9.42	9.42	3	0.04	0.01	0.05	0.00	0.00	24.0
2	248	-5876	108	-345	0	-192	333	6.28	6.28	9.42	9.42	2	0.04	0.01	0.04	0.00	0.00	24.0
3	248	-5748	98	-317	0	-172	319	6.28	6.28	9.42	9.42	2	0.04	0.01	0.04	0.00	0.00	24.0
4	248	-6830	-291	-343	0	-170	205	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
5	248	-6702	-300	-315	0	-150	191	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
6	248	-6359	-21	-377	0	-208	305	6.28	6.28	9.42	9.42	2	0.04	0.01	0.05	0.00	0.00	24.0
7	248	-5932	-52	-283	0	-141	257	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
8	248	-6645	-140	-376	0	-201	266	6.28	6.28	9.42	9.42	2	0.04	0.01	0.05	0.00	0.00	24.0
9	248	-6219	-172	-283	0	-135	219	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
10	248	-5876	108	-345	0	-192	333	6.28	6.28	9.42	9.42	2	0.04	0.01	0.04	0.00	0.00	24.0
11	248	-5748	98	-317	0	-172	319	6.28	6.28	9.42	9.42	2	0.04	0.01	0.04	0.00	0.00	24.0
12	248	-6830	-291	-343	0	-170	205	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
13	248	-6702	-300	-315	0	-150	191	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
14	248	-6359	-21	-377	0	-208	305	6.28	6.28	9.42	9.42	2	0.04	0.01	0.05	0.00	0.00	24.0
15	248	-5932	-52	-283	0	-141	257	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
16	248	-6645	-140	-376	0	-201	266	6.28	6.28	9.42	9.42	2	0.04	0.01	0.05	0.00	0.00	24.0
17	248	-6219	-172	-283	0	-135	219	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
18	248	-11122	574	522	0	-2341	1178	6.28	6.28	9.42	9.42	3	0.15	0.01	0.06	0.00	0.00	24.0
19	248	-11102	-255	-86	0	-909	474	6.28	6.28	9.42	9.42	3	0.06	0.01	0.02	0.00	0.00	24.0
20	248	-10434	108	277	0	-1573	736	6.28	6.28	9.42	9.42	3	0.10	0.01	0.03	0.00	0.00	24.0
37	248	-10162	751	512	0	-2356	1242	6.28	6.28	9.42	9.42	3	0.16	0.02	0.07	0.00	0.00	24.0
38	248	-10133	-631	-502	0	30	69	6.28	6.28	9.42	9.42	3	0.01	0.02	0.07	0.00	0.00	24.0
39	248	-9020	-26	104	0	-1076	505	6.28	6.28	9.42	9.42	3	0.07	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	330	-7693	-125	-429	0	131	237	6.28	6.28	9.42	9.42	3	0.03	0.01	0.05	0.00	0.00	24.0
2	330	-5505	108	-345	0	92	422	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
3	330	-5377	98	-317	0	89	400	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
4	330	-6459	-291	-343	0	113	-35	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
5	330	-6331	-300	-315	0	110	-57	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
6	330	-5988	-21	-377	0	103	288	6.28	6.28	9.42	9.42	2	0.04	0.01	0.05	0.00	0.00	24.0
7	330	-5561	-52	-283	0	92	214	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
8	330	-6274	-140	-376	0	110	151	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
9	330	-5848	-172	-283	0	99	77	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
10	330	-5505	108	-345	0	92	422	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
11	330	-5377	98	-317	0	89	400	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
12	330	-6459	-291	-343	0	113	-35	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
13	330	-6331	-300	-315	0	110	-57	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
14	330	-5988	-21	-377	0	103	288	6.28	6.28	9.42	9.42	2	0.04	0.01	0.05	0.00	0.00	24.0
15	330	-5561	-52	-283	0	92	214	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
16	330	-6274	-140	-376	0	110	151	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
17	330	-5848	-172	-283	0	99	77	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
18	330	-10640	386	522	0	-2772	1574	6.28	6.28	9.42	9.42	3	0.19	0.01	0.06	0.00	0.00	24.0
19	330	-10620	-66	-86	0	-838	342	6.28	6.28	9.42	9.42	3	0.05	0.00	0.01	0.00	0.00	24.0
20	330	-9952	108	340	0	-1829	826	6.28	6.28	9.42	9.42	3	0.12	0.01	0.04	0.00	0.00	24.0
37	330	-9680	436	512	0	-2779	1732	6.28	6.28	9.42	9.42	3	0.20	0.01	0.06	0.00	0.00	24.0
38	330	-9651	-316	-502	0	445	-322	6.28	6.28	9.42	9.42	3	0.04	0.01	0.06	0.00	0.00	24.0
39	330	-8537	-26	208	0	-1207	484	6.28	6.28	9.42	9.42	3	0.07	0.00	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

VERIFICA NODO IN TESTA AL PILASTRO, NODO NUM. 291 NON CONFINATO

(par.7.2.2 NTC2018 "La domanda di resistenza valutata con i criteri della progettazione in capacità può essere assunta non superiore alla domanda di resistenza valutata per il caso di comportamento strutturale non dissipativo.")

PROGETTAZIONE IN CAPACITA'

Asse loc. pilastro y nodo ESTERNO: As2(inf)= 4.02, As1(sup)= 6.03, Hjw= 40.0 cm, bj= 45.0 cm, hjc= 20.0 cm
Asse loc. pilastro z nodo ESTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 30.0 cm, hjc= 50.0 cm

FxMin,inf	FxMin,sup	FxMax,sup	FySup	FzSup	Vjbdy	Vjbdz	Vres,y	Vres,z	I.R.compr.	Ashy	Ashz	PASSO	Nota
daN					daN		daN			cmq		cm	
-5377	1	-0	0	0	26425	17616	63005	105009	0.42	4.36	--	11.99	

VERIFICA DI RESISTENZA CON SOLLECITAZIONI COMPORTAMENTO NON DISSIPATIVO

Asse loc. pilastro y nodo ESTERNO: Hjw= 40.0 cm, bj= 45.0 cm, hjc= 20.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb	Vb	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m			daN			cmq	cm	
2	-0	-5505	-1329	1376	0	3281	63005	0.05	0.00	40.00	
3	-0	-5377	-1314	1373	0	3244	63005	0.05	0.00	40.00	
4	-0	-6459	-3671	2093	0	9064	63005	0.14	0.00	40.00	
5	-0	-6331	-3656	2090	0	9027	63005	0.14	0.00	40.00	
6	-0	-5988	-2166	1631	0	5348	63005	0.08	0.00	40.00	
7	-0	-5561	-2116	1621	0	5225	63005	0.08	0.00	40.00	
8	-0	-6274	-2868	1846	0	7081	63005	0.11	0.00	40.00	
9	-0	-5848	-2819	1836	0	6960	63005	0.11	0.00	40.00	
10	-0	-5505	-1329	1376	0	3281	63005	0.05	0.00	40.00	
11	-0	-5377	-1314	1373	0	3244	63005	0.05	0.00	40.00	
12	-0	-6459	-3671	2093	0	9064	63005	0.14	0.00	40.00	
13	-0	-6331	-3656	2090	0	9027	63005	0.14	0.00	40.00	
14	-0	-5988	-2166	1631	0	5348	63005	0.08	0.00	40.00	
15	-0	-5561	-2116	1621	0	5225	63005	0.08	0.00	40.00	
16	-0	-6274	-2868	1846	0	7081	63005	0.11	0.00	40.00	
17	-0	-5848	-2819	1836	0	6960	63005	0.11	0.00	40.00	

Asse loc. pilastro z nodo ESTERNO: Hjw= 40.0 cm, bj= 30.0 cm, hjc= 50.0 cm, db1= 45.0 cm

NC	Fx,sup	Fx,inf	Mb	Vb	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m			daN			cmq	cm	
2	-0	-5505	-1979	1626	0	4886	105009	0.05	0.00	40.00	
3	-0	-5377	-1724	1544	0	4257	105009	0.04	0.00	40.00	
4	-0	-6459	-1862	1583	0	4598	105009	0.04	0.00	40.00	
5	-0	-6331	-1607	1501	0	3968	105009	0.04	0.00	40.00	
6	-0	-5988	-2237	1706	0	5523	105009	0.05	0.00	40.00	
7	-0	-5561	-1384	1433	0	3417	105009	0.03	0.00	40.00	
8	-0	-6274	-2202	1693	0	5437	105009	0.05	0.00	40.00	
9	-0	-5848	-1349	1420	0	3331	105009	0.03	0.00	40.00	
10	-0	-5505	-1979	1626	0	4886	105009	0.05	0.00	40.00	
11	-0	-5377	-1724	1544	0	4257	105009	0.04	0.00	40.00	
12	-0	-6459	-1862	1583	0	4598	105009	0.04	0.00	40.00	
13	-0	-6331	-1607	1501	0	3968	105009	0.04	0.00	40.00	
14	-0	-5988	-2237	1706	0	5523	105009	0.05	0.00	40.00	
15	-0	-5561	-1384	1433	0	3417	105009	0.03	0.00	40.00	
16	-0	-6274	-2202	1693	0	5437	105009	0.05	0.00	40.00	
17	-0	-5848	-1349	1420	0	3331	105009	0.03	0.00	40.00	

CONFRONTO E SINTESI CONCLUSIVE (si assume in ogni caso passo <= 15 cm)

I.R.compr.	Ashy	Ashz	PASSO	Nota
	cmq		cm	
0.14	--	--	15.00	**VERIFICATO**

ASTA NUM. 36 NI 325 NF 295 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 10D
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-10780	-98	-148	0	-1393	-75	6.28	6.28	12.57	12.57	3	0.05	0.00	0.01	0.00	0.00	24.0
2	0	-8475	655	-172	0	-1386	-1107	6.28	6.28	12.57	12.57	2	0.11	0.01	0.06	0.00	0.00	24.0
3	0	-8468	647	-63	0	-734	-1097	6.28	6.28	12.57	12.57	2	0.09	0.01	0.06	0.00	0.00	24.0
4	0	-8113	-798	-166	0	-1410	981	6.28	6.28	12.57	12.57	2	0.11	0.01	0.07	0.00	0.00	24.0
5	0	-8107	-806	-57	0	-757	991	6.28	6.28	12.57	12.57	2	0.08	0.01	0.08	0.00	0.00	24.0
6	0	-8356	156	-297	0	-2155	-389	6.28	6.28	12.57	12.57	2	0.12	0.01	0.03	0.00	0.00	24.0
7	0	-8334	129	67	0	19	-354	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
8	0	-8247	-280	-295	0	-2162	238	6.28	6.28	12.57	12.57	2	0.12	0.01	0.03	0.00	0.00	24.0
9	0	-8226	-307	69	0	12	273	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
10	0	-8475	655	-172	0	-1386	-1107	6.28	6.28	12.57	12.57	2	0.11	0.01	0.06	0.00	0.00	24.0
11	0	-8468	647	-63	0	-734	-1097	6.28	6.28	12.57	12.57	2	0.09	0.01	0.06	0.00	0.00	24.0
12	0	-8113	-798	-166	0	-1410	981	6.28	6.28	12.57	12.57	2	0.11	0.01	0.07	0.00	0.00	24.0
13	0	-8107	-806	-57	0	-757	991	6.28	6.28	12.57	12.57	2	0.08	0.01	0.08	0.00	0.00	24.0
14	0	-8356	156	-297	0	-2155	-389	6.28	6.28	12.57	12.57	2	0.12	0.01	0.03	0.00	0.00	24.0
15	0	-8334	129	67	0	19	-354	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
16	0	-8247	-280	-295	0	-2162	238	6.28	6.28	12.57	12.57	2	0.12	0.01	0.03	0.00	0.00	24.0
17	0	-8226	-307	69	0	12	273	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
18	0	-13210	1398	-422	0	-3412	-2061	6.28	6.28	12.57	12.57	3	0.16	0.03	0.11	0.00	0.00	24.0
19	0	-11070	-2173	-237	0	-2557	2860	6.28	6.28	12.57	12.57	3	0.17	0.04	0.20	0.00	0.00	24.0
20	0	-11800	-347	-785	0	-1743	332	6.28	6.28	12.57	12.57	3	0.07	0.01	0.08	0.00	0.00	24.0
37	0	-13610	2686	-426	0	-3183	-3862	6.28	6.28	12.57	12.57	3	0.23	0.05	0.24	0.00	0.00	24.0
38	0	-10040	-3265	-117	0	-1758	4340	6.28	6.28	12.57	12.57	3	0.25	0.06	0.31	0.00	0.00	24.0
39	0	-11250	-222	-1031	0	-401	126	6.28	6.28	12.57	12.57	3	0.02	0.02	0.10	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	83	-10136	-98	-148	0	-1271	-156	6.28	6.28	12.57	12.57	3	0.05	0.00	0.01	0.00	0.00	24.0
2	83	-7980	655	-172	0	-1244	-566	6.28	6.28	12.57	12.57	2	0.08	0.01	0.06	0.00	0.00	24.0
3	83	-7973	647	-63	0	-682	-563	6.28	6.28	12.57	12.57	2	0.06	0.01	0.06	0.00	0.00	24.0

4	83	-7618	-798	-166	0	-1273	322	6.28	6.28	12.57	12.57	2	0.08	0.01	0.07	0.00	0.00	24.0
5	83	-7612	-806	-57	0	-711	326	6.28	6.28	12.57	12.57	2	0.05	0.01	0.07	0.00	0.00	24.0
6	83	-7861	156	-297	0	-1910	-260	6.28	6.28	12.57	12.57	2	0.11	0.01	0.03	0.00	0.00	24.0
7	83	-7839	129	67	0	-36	-247	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
8	83	-7752	-280	-295	0	-1918	6	6.28	6.28	12.57	12.57	2	0.10	0.01	0.03	0.00	0.00	24.0
9	83	-7731	-307	69	0	-45	20	6.28	6.28	12.57	12.57	2	0.00	0.01	0.03	0.00	0.00	24.0
10	83	-7980	655	-172	0	-1244	-566	6.28	6.28	12.57	12.57	2	0.08	0.01	0.06	0.00	0.00	24.0
11	83	-7973	647	-63	0	-682	-563	6.28	6.28	12.57	12.57	2	0.06	0.01	0.06	0.00	0.00	24.0
12	83	-7618	-798	-166	0	-1273	322	6.28	6.28	12.57	12.57	2	0.08	0.01	0.07	0.00	0.00	24.0
13	83	-7612	-806	-57	0	-711	326	6.28	6.28	12.57	12.57	2	0.05	0.01	0.07	0.00	0.00	24.0
14	83	-7861	156	-297	0	-1910	-260	6.28	6.28	12.57	12.57	2	0.11	0.01	0.03	0.00	0.00	24.0
15	83	-7839	129	67	0	-36	-247	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
16	83	-7752	-280	-295	0	-1918	6	6.28	6.28	12.57	12.57	2	0.10	0.01	0.03	0.00	0.00	24.0
17	83	-7731	-307	69	0	-45	20	6.28	6.28	12.57	12.57	2	0.00	0.01	0.03	0.00	0.00	24.0
18	83	-12568	1398	-422	0	-3063	-908	6.28	6.28	12.57	12.57	3	0.12	0.03	0.11	0.00	0.00	24.0
19	83	-10427	-2173	-237	0	-2361	1067	6.28	6.28	12.57	12.57	3	0.10	0.04	0.18	0.00	0.00	24.0
20	83	-11156	-347	-566	0	-1188	45	6.28	6.28	12.57	12.57	3	0.04	0.01	0.06	0.00	0.00	24.0
37	83	-12965	2686	-426	0	-2832	-1646	6.28	6.28	12.57	12.57	3	0.13	0.05	0.22	0.00	0.00	24.0
38	83	-9396	-3265	-117	0	-1661	1646	6.28	6.28	12.57	12.57	3	0.10	0.06	0.28	0.00	0.00	24.0
39	83	-10606	-222	-666	0	295	-57	6.28	6.28	12.57	12.57	3	0.01	0.01	0.07	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	165	-9492	-98	-148	0	-1148	-237	6.28	6.28	12.57	12.57	3	0.04	0.00	0.01	0.00	0.00	24.0
2	165	-7485	655	-172	0	-1102	-26	6.28	6.28	12.57	12.57	2	0.06	0.01	0.06	0.00	0.00	24.0
3	165	-7478	647	-63	0	-630	-28	6.28	6.28	12.57	12.57	2	0.03	0.01	0.06	0.00	0.00	24.0
4	165	-7123	-798	-166	0	-1136	-337	6.28	6.28	12.57	12.57	2	0.07	0.01	0.07	0.00	0.00	24.0
5	165	-7117	-806	-57	0	-664	-339	6.28	6.28	12.57	12.57	2	0.05	0.01	0.07	0.00	0.00	24.0
6	165	-7366	156	-297	0	-1665	-132	6.28	6.28	12.57	12.57	2	0.09	0.01	0.03	0.00	0.00	24.0
7	165	-7344	129	67	0	-91	-140	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
8	165	-7257	-280	-295	0	-1675	-225	6.28	6.28	12.57	12.57	2	0.09	0.01	0.03	0.00	0.00	24.0
9	165	-7236	-307	69	0	-101	-233	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
10	165	-7485	655	-172	0	-1102	-26	6.28	6.28	12.57	12.57	2	0.06	0.01	0.06	0.00	0.00	24.0
11	165	-7478	647	-63	0	-630	-28	6.28	6.28	12.57	12.57	2	0.03	0.01	0.06	0.00	0.00	24.0
12	165	-7123	-798	-166	0	-1136	-337	6.28	6.28	12.57	12.57	2	0.07	0.01	0.07	0.00	0.00	24.0
13	165	-7117	-806	-57	0	-664	-339	6.28	6.28	12.57	12.57	2	0.05	0.01	0.07	0.00	0.00	24.0
14	165	-7366	156	-297	0	-1665	-132	6.28	6.28	12.57	12.57	2	0.09	0.01	0.03	0.00	0.00	24.0
15	165	-7344	129	67	0	-91	-140	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
16	165	-7257	-280	-295	0	-1675	-225	6.28	6.28	12.57	12.57	2	0.09	0.01	0.03	0.00	0.00	24.0
17	165	-7236	-307	69	0	-101	-233	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
18	165	-11925	1398	-422	0	-2715	246	6.28	6.28	12.57	12.57	3	0.10	0.03	0.12	0.00	0.00	24.0
19	165	-9784	-2173	-237	0	-2166	-726	6.28	6.28	12.57	12.57	3	0.09	0.04	0.18	0.00	0.00	24.0
20	165	-10512	-347	-378	0	-800	-241	6.28	6.28	12.57	12.57	3	0.03	0.01	0.04	0.00	0.00	24.0
37	165	-12320	2686	-426	0	-2480	570	6.28	6.28	12.57	12.57	3	0.10	0.05	0.22	0.00	0.00	24.0
38	165	-8753	-3265	-117	0	-1564	-1048	6.28	6.28	12.57	12.57	3	0.08	0.06	0.28	0.00	0.00	24.0
39	165	-9962	-222	-353	0	712	-241	6.28	6.28	12.57	12.57	3	0.03	0.01	0.04	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	248	-8848	-98	-148	0	-1026	-318	6.28	6.28	12.57	12.57	3	0.04	0.00	0.02	0.00	0.00	24.0
2	248	-6990	655	-172	0	-961	515	6.28	6.28	12.57	12.57	2	0.07	0.01	0.06	0.00	0.00	24.0
3	248	-6983	647	-63	0	-578	506	6.28	6.28	12.57	12.57	2	0.05	0.01	0.06	0.00	0.00	24.0
4	248	-6628	-798	-166	0	-1000	-995	6.28	6.28	12.57	12.57	2	0.09	0.01	0.07	0.00	0.00	24.0
5	248	-6622	-806	-57	0	-617	-1004	6.28	6.28	12.57	12.57	2	0.08	0.01	0.08	0.00	0.00	24.0
6	248	-6871	156	-297	0	-1420	-3	6.28	6.28	12.57	12.57	2	0.07	0.01	0.03	0.00	0.00	24.0
7	248	-6849	129	67	0	-146	-33	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
8	248	-6762	-280	-295	0	-1432	-456	6.28	6.28	12.57	12.57	2	0.09	0.01	0.03	0.00	0.00	24.0
9	248	-6741	-307	69	0	-158	-486	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
10	248	-6990	655	-172	0	-961	515	6.28	6.28	12.57	12.57	2	0.07	0.01	0.06	0.00	0.00	24.0
11	248	-6983	647	-63	0	-578	506	6.28	6.28	12.57	12.57	2	0.05	0.01	0.06	0.00	0.00	24.0
12	248	-6628	-798	-166	0	-1000	-995	6.28	6.28	12.57	12.57	2	0.09	0.01	0.07	0.00	0.00	24.0
13	248	-6622	-806	-57	0	-617	-1004	6.28	6.28	12.57	12.57	2	0.08	0.01	0.08	0.00	0.00	24.0
14	248	-6871	156	-297	0	-1420	-3	6.28	6.28	12.57	12.57	2	0.07	0.01	0.03	0.00	0.00	24.0
15	248	-6849	129	67	0	-146	-33	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
16	248	-6762	-280	-295	0	-1432	-456	6.28	6.28	12.57	12.57	2	0.09	0.01	0.03	0.00	0.00	24.0
17	248	-6741	-307	69	0	-158	-486	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
18	248	-11282	1398	-422	0	-2367	1399	6.28	6.28	12.57	12.57	3	0.11	0.03	0.12	0.00	0.00	24.0
19	248	-9142	-2173	-237	0	-1970	-2518	6.28	6.28	12.57	12.57	3	0.15	0.04	0.21	0.00	0.00	24.0
20	248	-9868	-347	-222	0	-554	-527	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
37	248	-11675	2686	-426	0	-2128	2786	6.28	6.28	12.57	12.57	3	0.16	0.05	0.25	0.00	0.00	24.0
38	248	-8110	-3265	-117	0	-1468	-3742	6.28	6.28	12.57	12.57	3	0.22	0.06	0.31	0.00	0.00	24.0
39	248	-9319	-222	-92	0	892	-424	6.28	6.28	12.57	12.57	3	0.04	0.00	0.02	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	330	-8204	-98	-148	0	-903	-399	6.28	6.28	12.57	12.57	3	0.04	0.00	0.02	0.00	0.00	24.0
2	330	-6495	655	-172	0	-819	1056	6.28	6.28	12.57	12.57	2	0.09	0.01	0.06	0.00	0.00	24.0
3	330	-6488	647	-63	0	-527	1040	6.28	6.28	12.57	12.57	2	0.08	0.01	0.06	0.00	0.00	24.0
4	330	-6133	-798	-166	0	-863	-1654	6.28	6.28	12.57	12.57	2	0.13	0.01	0.08	0.00	0.00	24.0
5	330	-6127	-806	-57	0	-571	-1669	6.28	6.28	12.57	12.57	2	0.12	0.01	0.08	0.00	0.00	24.0
6	330	-6376	156	-297	0	-1175	126	6.28	6.28	12.57	12.57	2	0.07	0.01	0.03	0.00	0.00	24.0
7	330	-6354	129	67	0	-201	73	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
8	330	-6267	-280	-295	0	-1188	-687	6.28	6.28	12.57	12.57	2	0.09	0.01	0.03	0.00	0.00	24.0
9	330	-6246	-307	69	0	-215	-739	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
10	330	-6495	655	-172	0	-819	1056	6.28	6.28	12.57	12.57	2	0.09	0.01	0.06	0.00	0.00	24.0
11	330	-6488	647	-63	0	-527	1040	6.28	6.28	12.57	12.57	2	0.08	0.01	0.06	0.00	0.00	24.0
12	330	-6133	-798	-166	0	-863	-1654	6.28	6.28	12.57	12.57	2	0.13	0.01	0.08	0.00	0.00	24.0
13	330	-6127	-806	-57	0	-571	-1669	6.28	6.28	12.57	12.57	2	0.12	0.01	0.08	0.00	0.00	24.0
14	330	-6376	156	-297	0	-1175	126	6.28	6.28	12.57	12.57	2	0.07	0.01	0.03	0.00	0.00	24.0
15	330	-6354	129	67	0	-201	73	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
16	330	-6267	-280	-295	0	-1188	-687	6.28	6.28	12.57	12.57	2	0.09	0.01	0.03	0.00	0.00	24.0
17	330	-6246	-307	69	0	-215	-739	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
18	330	-10640	1398	-422	0	-2018	2552	6.28	6.28	12.57	12.57	3	0.15	0.03	0.13	0.00	0.00	24.0
19	330	-8499	-2173	-237	0	-1774	-4311	6.28	6.28	12.57	12.57	3	0.25	0.04	0.21	0.00	0.00	24.0
20	330	-9224	-347	-97	0	-424	-814	6.28	6.28	12.57	12.57	3	0.05	0.01	0.03	0.00	0.00	24.0
37	330	-11030	2686	-426	0	-1777	5002	6.28	6.28	12.57	12.57	3	0.28	0.05	0.25	0.00	0.00	24.0
38	330	-7466	-3265	-117	0	-1371	-6436	6.28	6.28	12.57	12.57	3	0.37	0.06	0.32	0.00	0.00	24.0
39	330	-8675	-222	116	0	879	-608	6.28	6.28	12.57	12.57	3	0.05	0.00	0.02	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

VERIFICA NODO IN TESTA AL PILASTRO, NODO NUM. 295 NON CONFINATO

(par.7.2.2 NTC2018 "La domanda di resistenza valutata con i criteri della progettazione in capacità può essere assunta non superiore alla domanda di resistenza valutata per il caso di comportamento strutturale non dissipativo.")

PROGETTAZIONE IN CAPACITA'

Asse loc. pilastro y nodo INTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 50.0 cm, hjc= 30.0 cm

Asse loc. pilastro z nodo: --

FxMin,inf	FxMin,sup	FxMax,sup	FySup	FzSup	Vjbdy	Vjbdz	Vres,y	Vres,z	I.R.compr.	Ashy	Ashz	PASSO	Nota

8	190	-10959	-315	-451	0	-1426	17	6.28	6.28	12.57	12.57	2	0.07	0.01	0.04	0.00	0.00	24.0
9	190	-10670	-336	-102	0	426	15	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
10	190	-10392	546	-328	0	-781	62	6.28	6.28	12.57	12.57	2	0.04	0.01	0.05	0.00	0.00	24.0
11	190	-10309	540	-224	0	-225	61	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
12	190	-11108	-790	-329	0	-776	-9	6.28	6.28	12.57	12.57	2	0.04	0.01	0.07	0.00	0.00	24.0
13	190	-11020	-796	-225	0	-221	-9	6.28	6.28	12.57	12.57	2	0.01	0.01	0.07	0.00	0.00	24.0
14	190	-10742	86	-450	0	-1427	38	6.28	6.28	12.57	12.57	2	0.07	0.01	0.04	0.00	0.00	24.0
15	190	-10458	65	-102	0	424	37	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
16	190	-10959	-315	-451	0	-1426	17	6.28	6.28	12.57	12.57	2	0.07	0.01	0.04	0.00	0.00	24.0
17	190	-10670	-336	-102	0	426	15	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
18	190	-18305	1342	-862	0	-1703	201	6.28	6.28	12.57	12.57	3	0.06	0.02	0.10	0.00	0.00	24.0
19	190	-18545	-2105	-767	0	-1393	-70	6.28	6.28	12.57	12.57	3	0.05	0.04	0.16	0.00	0.00	24.0
20	190	-17520	-352	-1064	0	72	61	6.28	6.28	12.57	12.57	3	0.00	0.02	0.10	0.00	0.00	24.0
37	190	-16770	2564	-748	0	-1517	280	6.28	6.28	12.57	12.57	3	0.06	0.05	0.20	0.00	0.00	24.0
38	190	-17160	-3181	-588	0	-1000	-170	6.28	6.28	12.57	12.57	3	0.04	0.06	0.25	0.00	0.00	24.0
39	190	-15450	-259	-1083	0	1443	49	6.28	6.28	12.57	12.57	3	0.05	0.02	0.10	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	285	-13180	-162	-359	0	-310	-120	6.28	6.28	12.57	12.57	3	0.01	0.01	0.03	0.00	0.00	24.0
2	285	-9824	546	-328	0	-469	581	6.28	6.28	12.57	12.57	2	0.05	0.01	0.05	0.00	0.00	24.0
3	285	-9738	540	-224	0	-13	574	6.28	6.28	12.57	12.57	2	0.03	0.01	0.05	0.00	0.00	24.0
4	285	-10538	-790	-329	0	-464	-759	6.28	6.28	12.57	12.57	2	0.06	0.01	0.07	0.00	0.00	24.0
5	285	-10450	-796	-225	0	-7	-765	6.28	6.28	12.57	12.57	2	0.05	0.01	0.07	0.00	0.00	24.0
6	285	-10174	86	-450	0	-999	119	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
7	285	-9888	65	-102	0	521	98	6.28	6.28	12.57	12.57	2	0.03	0.00	0.01	0.00	0.00	24.0
8	285	-10388	-315	-451	0	-998	-282	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
9	285	-10100	-336	-102	0	523	-303	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
10	285	-9824	546	-328	0	-469	581	6.28	6.28	12.57	12.57	2	0.05	0.01	0.05	0.00	0.00	24.0
11	285	-9738	540	-224	0	-13	574	6.28	6.28	12.57	12.57	2	0.03	0.01	0.05	0.00	0.00	24.0
12	285	-10538	-790	-329	0	-464	-759	6.28	6.28	12.57	12.57	2	0.06	0.01	0.07	0.00	0.00	24.0
13	285	-10450	-796	-225	0	-7	-765	6.28	6.28	12.57	12.57	2	0.05	0.01	0.07	0.00	0.00	24.0
14	285	-10174	86	-450	0	-999	119	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
15	285	-9888	65	-102	0	521	98	6.28	6.28	12.57	12.57	2	0.03	0.00	0.01	0.00	0.00	24.0
16	285	-10388	-315	-451	0	-998	-282	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
17	285	-10100	-336	-102	0	523	-303	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
18	285	-17562	1342	-862	0	-883	1476	6.28	6.28	12.57	12.57	3	0.08	0.02	0.12	0.00	0.00	24.0
19	285	-17802	-2105	-767	0	-664	-2069	6.28	6.28	12.57	12.57	3	0.11	0.04	0.18	0.00	0.00	24.0
20	285	-16780	-352	-884	0	995	-273	6.28	6.28	12.57	12.57	3	0.04	0.02	0.08	0.00	0.00	24.0
37	285	-16030	2564	-748	0	-806	2716	6.28	6.28	12.57	12.57	3	0.15	0.05	0.22	0.00	0.00	24.0
38	285	-16420	-3181	-588	0	-441	-3192	6.28	6.28	12.57	12.57	3	0.17	0.06	0.28	0.00	0.00	24.0
39	285	-14710	-259	-783	0	2324	-197	6.28	6.28	12.57	12.57	3	0.08	0.01	0.07	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	380	-12440	-162	-359	0	32	-274	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
2	380	-9255	546	-328	0	-157	1100	6.28	6.28	12.57	12.57	2	0.07	0.01	0.05	0.00	0.00	24.0
3	380	-9168	540	-224	0	200	1087	6.28	6.28	12.57	12.57	2	0.07	0.01	0.05	0.00	0.00	24.0
4	380	-9967	-790	-329	0	-151	-1509	6.28	6.28	12.57	12.57	2	0.09	0.01	0.07	0.00	0.00	24.0
5	380	-9880	-796	-225	0	206	-1521	6.28	6.28	12.57	12.57	2	0.10	0.01	0.08	0.00	0.00	24.0
6	380	-9605	86	-450	0	-572	201	6.28	6.28	12.57	12.57	2	0.04	0.01	0.05	0.00	0.00	24.0
7	380	-9317	65	-102	0	618	160	6.28	6.28	12.57	12.57	2	0.04	0.00	0.01	0.00	0.00	24.0
8	380	-9818	-315	-451	0	-570	-582	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
9	380	-9530	-336	-102	0	620	-622	6.28	6.28	12.57	12.57	2	0.06	0.01	0.03	0.00	0.00	24.0
10	380	-9255	546	-328	0	-157	1100	6.28	6.28	12.57	12.57	2	0.07	0.01	0.05	0.00	0.00	24.0
11	380	-9168	540	-224	0	200	1087	6.28	6.28	12.57	12.57	2	0.07	0.01	0.05	0.00	0.00	24.0
12	380	-9967	-790	-329	0	-151	-1509	6.28	6.28	12.57	12.57	2	0.09	0.01	0.07	0.00	0.00	24.0
13	380	-9880	-796	-225	0	206	-1521	6.28	6.28	12.57	12.57	2	0.10	0.01	0.08	0.00	0.00	24.0
14	380	-9605	86	-450	0	-572	201	6.28	6.28	12.57	12.57	2	0.04	0.01	0.05	0.00	0.00	24.0
15	380	-9317	65	-102	0	618	160	6.28	6.28	12.57	12.57	2	0.04	0.00	0.01	0.00	0.00	24.0
16	380	-9818	-315	-451	0	-570	-582	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
17	380	-9530	-336	-102	0	620	-622	6.28	6.28	12.57	12.57	2	0.06	0.01	0.03	0.00	0.00	24.0
18	380	-16820	1342	-862	0	-64	2751	6.28	6.28	12.57	12.57	3	0.15	0.02	0.12	0.00	0.00	24.0
19	380	-17060	-2105	-767	0	64	-4069	6.28	6.28	12.57	12.57	3	0.22	0.04	0.18	0.00	0.00	24.0
20	380	-16040	-352	-740	0	1763	-607	6.28	6.28	12.57	12.57	3	0.07	0.01	0.07	0.00	0.00	24.0
37	380	-15290	2564	-748	0	-96	5152	6.28	6.28	12.57	12.57	3	0.28	0.05	0.23	0.00	0.00	24.0
38	380	-15680	-3181	-588	0	117	-6214	6.28	6.28	12.57	12.57	3	0.33	0.06	0.28	0.00	0.00	24.0
39	380	-13970	-259	-544	0	2950	-443	6.28	6.28	12.57	12.57	3	0.11	0.01	0.05	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

VERIFICA NODO IN TESTA AL PILASTRO, NODO NUM. 297 NON CONFINATO

(par.7.2.2 NTC2018 "La domanda di resistenza valutata con i criteri della progettazione in capacità può essere assunta non superiore alla domanda di resistenza valutata per il caso di comportamento strutturale non dissipativo.")

PROGETTAZIONE IN CAPACITA'

Asse loc. pilastro y nodo INTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 50.0 cm, hjc= 30.0 cm

Asse loc. pilastro z nodo: --

FxMin,inf	FxMin,sup	FxMax,sup	FySup	FzSup	Vjbdy	Vjbdz	Vres,y	Vres,z	I.R.compr.	Ashy	Ashz	PASSO	Nota
daN					daN		daN			cmq		cm	
-9168	-5460	-6290	1	20	35232	--	129281	--	0.27	8.75	--	5.19	

VERIFICA DI RESISTENZA CON SOLLECITAZIONI COMPORTAMENTO NON DISSIPATIVO

Asse loc. pilastro y nodo INTERNO: Hjw= 40.0 cm, bj= 50.0 cm, hjc= 30.0 cm, db1= 45.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb,1	Mb,2	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-5550	-9255	-2125	-1159	33	2352	129515	0.02	0.00	40.00	
3	-5460	-9168	-2126	-1165	31	2341	129544	0.02	0.00	40.00	
4	-6290	-9967	-874	-2343	10	3616	129281	0.03	0.00	40.00	
5	-6201	-9880	-875	-2349	12	3627	129309	0.03	0.00	40.00	
6	-5913	-9605	-1686	-1566	20	276	129400	0.00	0.00	40.00	
7	-5615	-9317	-1689	-1587	14	238	129495	0.00	0.00	40.00	
8	-6136	-9818	-1311	-1921	7	1499	129329	0.01	0.00	40.00	
9	-5837	-9530	-1314	-1942	1	1549	129424	0.01	0.00	40.00	
10	-5550	-9255	-2125	-1159	33	2352	129515	0.02	0.00	40.00	
11	-5460	-9168	-2126	-1165	31	2341	129544	0.02	0.00	40.00	
12	-6290	-9967	-874	-2343	10	3616	129281	0.03	0.00	40.00	
13	-6201	-9880	-875	-2349	12	3627	129309	0.03	0.00	40.00	
14	-5913	-9605	-1686	-1566	20	276	129400	0.00	0.00	40.00	
15	-5615	-9317	-1689	-1587	14	238	129495	0.00	0.00	40.00	
16	-6136	-9818	-1311	-1921	7	1499	129329	0.01	0.00	40.00	
17	-5837	-9530	-1314	-1942	1	1549	129424	0.01	0.00	40.00	

CONFRONTO E SINTESI CONCLUSIVE (si assume in ogni caso passo <= 15 cm)

I.R.compr.	Ashy	Ashz	PASSO	Nota
	cmq		cm	
0.03	--	--	15.00	**VERIFICATO**

ASTA NUM. 38 NI 299 NF 294 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 10B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-27370	-31	286	0	183	31	6.28	6.28	12.57	12.57	3	0.01	0.00	0.02	0.00	0.00	24.0
2	0	-21210	326	236	0	95	-827	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
3	0	-21190	321	188	0	130	-814	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
4	0	-20920	-369	252	0	152	862	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
5	0	-20900	-374	204	0	187	875	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
6	0	-21130	89	297	0	73	-251	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
7	0	-21070	72	139	0	192	-208	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
8	0	-21040	-120	302	0	90	256	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
9	0	-20980	-137	143	0	209	298	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
10	0	-21210	326	236	0	95	-827	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
11	0	-21190	321	188	0	130	-814	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
12	0	-20920	-369	252	0	152	862	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
13	0	-20900	-374	204	0	187	875	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
14	0	-21130	89	297	0	73	-251	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
15	0	-21070	72	139	0	192	-208	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
16	0	-21040	-120	302	0	90	256	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
17	0	-20980	-137	143	0	209	298	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
18	0	-30330	1173	524	0	193	-2779	6.28	6.28	12.57	12.57	3	0.13	0.02	0.09	0.00	0.00	24.0
19	0	-28540	-1074	501	0	428	2568	6.28	6.28	12.57	12.57	3	0.13	0.02	0.08	0.00	0.00	24.0
20	0	-29110	41	193	0	-149	-92	6.28	6.28	12.57	12.57	3	0.01	0.00	0.02	0.00	0.00	24.0
37	0	-30240	1896	455	0	66	-4518	6.28	6.28	12.57	12.57	3	0.22	0.03	0.14	0.00	0.00	24.0
38	0	-27250	-1848	417	0	458	4393	6.28	6.28	12.57	12.57	3	0.22	0.03	0.14	0.00	0.00	24.0
39	0	-28200	10	-97	0	-504	-40	6.28	6.28	12.57	12.57	3	0.02	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	97	-26610	-31	286	0	-96	1	6.28	6.28	12.57	12.57	3	0.00	0.00	0.02	0.00	0.00	24.0
2	97	-20625	326	236	0	-135	-509	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
3	97	-20605	321	188	0	-53	-501	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
4	97	-20335	-369	252	0	-94	502	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
5	97	-20315	-374	204	0	-12	510	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
6	97	-20545	89	297	0	-216	-164	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
7	97	-20485	72	139	0	57	-138	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
8	97	-20455	-120	302	0	-204	139	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
9	97	-20395	-137	143	0	69	165	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
10	97	-20625	326	236	0	-135	-509	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
11	97	-20605	321	188	0	-53	-501	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
12	97	-20335	-369	252	0	-94	502	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
13	97	-20315	-374	204	0	-12	510	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
14	97	-20545	89	297	0	-216	-164	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
15	97	-20485	72	139	0	57	-138	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
16	97	-20455	-120	302	0	-204	139	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
17	97	-20395	-137	143	0	69	165	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
18	97	-29570	1173	524	0	-318	-1636	6.28	6.28	12.57	12.57	3	0.08	0.02	0.09	0.00	0.00	24.0
19	97	-27778	-1074	501	0	-60	1521	6.28	6.28	12.57	12.57	3	0.07	0.02	0.08	0.00	0.00	24.0
20	97	-28350	41	193	0	-337	-52	6.28	6.28	12.57	12.57	3	0.01	0.00	0.02	0.00	0.00	24.0
37	97	-29480	1896	455	0	-377	-2670	6.28	6.28	12.57	12.57	3	0.13	0.03	0.14	0.00	0.00	24.0
38	97	-26490	-1848	417	0	52	2592	6.28	6.28	12.57	12.57	3	0.13	0.03	0.14	0.00	0.00	24.0
39	97	-27440	10	-97	0	-410	-30	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	195	-25850	-31	286	0	-375	-30	6.28	6.28	12.57	12.57	3	0.01	0.00	0.02	0.00	0.00	24.0
2	195	-20040	326	236	0	-366	-192	6.28	6.28	12.57	12.57	2	0.02	0.01	0.02	0.00	0.00	24.0
3	195	-20020	321	188	0	-237	-189	6.28	6.28	12.57	12.57	2	0.02	0.01	0.02	0.00	0.00	24.0
4	195	-19750	-369	252	0	-339	142	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
5	195	-19730	-374	204	0	-211	145	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
6	195	-19960	89	297	0	-506	-78	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
7	195	-19900	72	139	0	-78	-68	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
8	195	-19870	-120	302	0	-498	22	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
9	195	-19810	-137	143	0	-70	32	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
10	195	-20040	326	236	0	-366	-192	6.28	6.28	12.57	12.57	2	0.02	0.01	0.02	0.00	0.00	24.0
11	195	-20020	321	188	0	-237	-189	6.28	6.28	12.57	12.57	2	0.02	0.01	0.02	0.00	0.00	24.0
12	195	-19750	-369	252	0	-339	142	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
13	195	-19730	-374	204	0	-211	145	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
14	195	-19960	89	297	0	-506	-78	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
15	195	-19900	72	139	0	-78	-68	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
16	195	-19870	-120	302	0	-498	22	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
17	195	-19810	-137	143	0	-70	32	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
18	195	-28810	1173	524	0	-829	-492	6.28	6.28	12.57	12.57	3	0.04	0.02	0.08	0.00	0.00	24.0
19	195	-27015	-1074	501	0	-549	475	6.28	6.28	12.57	12.57	3	0.03	0.02	0.08	0.00	0.00	24.0
20	195	-27590	41	193	0	-525	-12	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
37	195	-28720	1896	455	0	-821	-821	6.28	6.28	12.57	12.57	3	0.05	0.03	0.14	0.00	0.00	24.0
38	195	-25730	-1848	417	0	-354	790	6.28	6.28	12.57	12.57	3	0.04	0.03	0.15	0.00	0.00	24.0
39	195	-26680	10	-97	0	-315	-20	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	292	-25090	-31	286	0	-654	-61	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
2	292	-19455	326	236	0	-596	126	6.28	6.28	12.57	12.57	2	0.03	0.01	0.02	0.00	0.00	24.0
3	292	-19435	321	188	0	-421	124	6.28	6.28	12.57	12.57	2	0.02	0.01	0.02	0.00	0.00	24.0
4	292	-19165	-369	252	0	-585	-218	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
5	292	-19145	-374	204	0	-410	-219	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
6	292	-19375	89	297	0	-795	8	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
7	292	-19315	72	139	0	-213	2	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
8	292	-19285	-120	302	0	-792	-95	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
9	292	-19225	-137	143	0	-210	-101	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
10	292	-19455	326	236	0	-596	126	6.28	6.28	12.57	12.57	2	0.03	0.01	0.02	0.00	0.00	24.0
11	292	-19435	321	188	0	-421	124	6.28	6.28	12.57	12.57	2	0.02	0.01	0.02	0.00	0.00	24.0

12	292	-19165	-369	252	0	-585	-218	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
13	292	-19145	-374	204	0	-410	-219	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
14	292	-19375	89	297	0	-795	8	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
15	292	-19315	72	139	0	-213	2	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
16	292	-19285	-120	302	0	-792	-95	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
17	292	-19225	-137	143	0	-210	-101	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
18	292	-28050	1173	524	0	-1340	651	6.28	6.28	12.57	12.57	3	0.05	0.02	0.08	0.00	0.00	24.0
19	292	-26252	-1074	501	0	-1037	-572	6.28	6.28	12.57	12.57	3	0.04	0.02	0.08	0.00	0.00	24.0
20	292	-26830	41	193	0	-714	29	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
37	292	-27960	1896	455	0	-1264	1027	6.28	6.28	12.57	12.57	3	0.06	0.03	0.13	0.00	0.00	24.0
38	292	-24970	-1848	417	0	-761	-1011	6.28	6.28	12.57	12.57	3	0.05	0.03	0.15	0.00	0.00	24.0
39	292	-25920	10	-97	0	-220	-10	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	390	-24330	-31	286	0	-933	-91	6.28	6.28	12.57	12.57	3	0.03	0.00	0.02	0.00	0.00	24.0
2	390	-18870	326	236	0	-826	444	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
3	390	-18850	321	188	0	-605	437	6.28	6.28	12.57	12.57	2	0.04	0.01	0.02	0.00	0.00	24.0
4	390	-18580	-369	252	0	-830	-578	6.28	6.28	12.57	12.57	2	0.06	0.01	0.03	0.00	0.00	24.0
5	390	-18560	-374	204	0	-609	-584	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
6	390	-18790	89	297	0	-1085	94	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
7	390	-18730	72	139	0	-349	72	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
8	390	-18700	-120	302	0	-1086	-212	6.28	6.28	12.57	12.57	2	0.06	0.01	0.03	0.00	0.00	24.0
9	390	-18640	-137	143	0	-350	-234	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
10	390	-18870	326	236	0	-826	444	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
11	390	-18850	321	188	0	-605	437	6.28	6.28	12.57	12.57	2	0.04	0.01	0.02	0.00	0.00	24.0
12	390	-18580	-369	252	0	-830	-578	6.28	6.28	12.57	12.57	2	0.06	0.01	0.03	0.00	0.00	24.0
13	390	-18560	-374	204	0	-609	-584	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
14	390	-18790	89	297	0	-1085	94	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
15	390	-18730	72	139	0	-349	72	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
16	390	-18700	-120	302	0	-1086	-212	6.28	6.28	12.57	12.57	2	0.06	0.01	0.03	0.00	0.00	24.0
17	390	-18640	-137	143	0	-350	-234	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
18	390	-27290	1173	524	0	-1851	1794	6.28	6.28	12.57	12.57	3	0.10	0.02	0.08	0.00	0.00	24.0
19	390	-25490	-1074	501	0	-1526	-1619	6.28	6.28	12.57	12.57	3	0.09	0.02	0.08	0.00	0.00	24.0
20	390	-26070	41	193	0	-902	69	6.28	6.28	12.57	12.57	3	0.03	0.00	0.02	0.00	0.00	24.0
37	390	-27200	1896	455	0	-1708	2876	6.28	6.28	12.57	12.57	3	0.15	0.03	0.15	0.00	0.00	24.0
38	390	-24210	-1848	417	0	-1167	-2813	6.28	6.28	12.57	12.57	3	0.14	0.03	0.15	0.00	0.00	24.0
39	390	-25160	10	-97	0	-126	-0	6.28	6.28	12.57	12.57	3	0.00	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

VERIFICA NODO IN TESTA AL PILASTRO, NODO NUM. 294 NON CONFINATO

(par.7.2.2 NTC2018 "La domanda di resistenza valutata con i criteri della progettazione in capacità può essere assunta non superiore alla domanda di resistenza valutata per il caso di comportamento strutturale non dissipativo.")

PROGETTAZIONE IN CAPACITA'

Asse loc. pilastro y nodo ESTERNO: As2(inf)= 4.02, As1(sup)= 6.03, Hjw= 40.0 cm, bj= 50.0 cm, hjc= 30.0 cm
Asse loc. pilastro z nodo INTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 40.0 cm, hjc= 50.0 cm

FxMin,inf	FxMin,sup	FxMax,sup	FySup	FzSup	Vjbdy	Vjbdz	Vres,y	Vres,z	I.R.compr.	Ashy	Ashz	PASSO	Nota
daN					daN		daN			cmq		cm	
-18560	-10090	-11090	14	2	26411	35231	101484	170331	0.26	2.26	1.81	32.06	

VERIFICA DI RESISTENZA CON SOLLECITAZIONI COMPORTAMENTO NON DISSIPATIVO

Asse loc. pilastro y nodo ESTERNO: Hjw= 40.0 cm, bj= 50.0 cm, hjc= 30.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb	Vb	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-11090	-18870	-847	1621	540	1550	101484	0.02	0.00	40.00	
3	-11080	-18850	-852	1622	523	1581	101487	0.02	0.00	40.00	
4	-10110	-18580	-2677	2240	1021	5589	101801	0.05	0.00	40.00	
5	-10090	-18560	-2683	2242	1038	5587	101807	0.05	0.00	40.00	
6	-10760	-18790	-1481	1835	14	3643	101591	0.04	0.00	40.00	
7	-10720	-18730	-1499	1841	43	3658	101604	0.04	0.00	40.00	
8	-10470	-18700	-2030	2021	455	4558	101684	0.04	0.00	40.00	
9	-10420	-18640	-2048	2027	512	4545	101701	0.04	0.00	40.00	
10	-11090	-18870	-847	1621	540	1550	101484	0.02	0.00	40.00	
11	-11080	-18850	-852	1622	523	1581	101487	0.02	0.00	40.00	
12	-10110	-18580	-2677	2240	1021	5589	101801	0.05	0.00	40.00	
13	-10090	-18560	-2683	2242	1038	5587	101807	0.05	0.00	40.00	
14	-10760	-18790	-1481	1835	14	3643	101591	0.04	0.00	40.00	
15	-10720	-18730	-1499	1841	43	3658	101604	0.04	0.00	40.00	
16	-10470	-18700	-2030	2021	455	4558	101684	0.04	0.00	40.00	
17	-10420	-18640	-2048	2027	512	4545	101701	0.04	0.00	40.00	

Asse loc. pilastro z nodo INTERNO: Hjw= 40.0 cm, bj= 40.0 cm, hjc= 50.0 cm, db1= 45.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb,1	Mb,2	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-11090	-18870	-1776	-1215	144	1241	170331	0.01	0.00	40.00	
3	-11080	-18850	-1535	-1453	23	180	170336	0.00	0.00	40.00	
4	-10110	-18580	-1858	-1283	123	1297	170750	0.01	0.00	40.00	
5	-10090	-18560	-1617	-1522	2	233	170759	0.00	0.00	40.00	
6	-10760	-18790	-2086	-961	278	2501	170473	0.01	0.00	40.00	
7	-10720	-18730	-1283	-1755	126	1040	170490	0.01	0.00	40.00	
8	-10470	-18700	-2111	-982	271	2517	170597	0.01	0.00	40.00	
9	-10420	-18640	-1307	-1775	132	1023	170618	0.01	0.00	40.00	
10	-11090	-18870	-1776	-1215	144	1241	170331	0.01	0.00	40.00	
11	-11080	-18850	-1535	-1453	23	180	170336	0.00	0.00	40.00	
12	-10110	-18580	-1858	-1283	123	1297	170750	0.01	0.00	40.00	
13	-10090	-18560	-1617	-1522	2	233	170759	0.00	0.00	40.00	
14	-10760	-18790	-2086	-961	278	2501	170473	0.01	0.00	40.00	
15	-10720	-18730	-1283	-1755	126	1040	170490	0.01	0.00	40.00	
16	-10470	-18700	-2111	-982	271	2517	170597	0.01	0.00	40.00	
17	-10420	-18640	-1307	-1775	132	1023	170618	0.01	0.00	40.00	

CONFRONTO E SINTESI CONCLUSIVE (si assume in ogni caso passo <= 15 cm)

I.R.compr.	Ashy	Ashz	PASSO	Nota

	cmq	cm		
0.05	--	--	15.00	**VERIFICATO**

ASTA NUM. 39 NI 300 NF 296 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 15B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-37050	142	578	0	698	-198	6.28	6.28	12.57	12.57	3	0.02	0.01	0.04	0.00	0.00	24.0
2	0	-28250	360	462	0	514	-662	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
3	0	-28150	359	423	0	552	-660	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
4	0	-28850	-141	467	0	522	355	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
5	0	-28760	-142	428	0	560	357	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
6	0	-28570	186	509	0	471	-309	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
7	0	-28250	182	380	0	600	-301	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
8	0	-28750	36	510	0	474	-4	6.28	6.28	12.57	12.57	2	0.02	0.01	0.04	0.00	0.00	24.0
9	0	-28430	32	381	0	603	4	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
10	0	-28250	360	462	0	514	-662	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
11	0	-28150	359	423	0	552	-660	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
12	0	-28850	-141	467	0	522	355	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
13	0	-28760	-142	428	0	560	357	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
14	0	-28570	186	509	0	471	-309	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
15	0	-28250	182	380	0	600	-301	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
16	0	-28750	36	510	0	474	-4	6.28	6.28	12.57	12.57	2	0.02	0.01	0.04	0.00	0.00	24.0
17	0	-28430	32	381	0	603	4	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
18	0	-42800	1007	708	0	628	-1833	6.28	6.28	12.57	12.57	3	0.08	0.02	0.07	0.00	0.00	24.0
19	0	-42790	-638	694	0	671	1355	6.28	6.28	12.57	12.57	3	0.06	0.01	0.05	0.00	0.00	24.0
20	0	-41960	182	413	0	270	-240	6.28	6.28	12.57	12.57	3	0.01	0.01	0.03	0.00	0.00	24.0
37	0	-40670	1541	664	0	615	-2883	6.28	6.28	12.57	12.57	3	0.13	0.03	0.11	0.00	0.00	24.0
38	0	-40660	-1200	640	0	687	2430	6.28	6.28	12.57	12.57	3	0.11	0.02	0.08	0.00	0.00	24.0
39	0	-39280	167	172	0	19	-227	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	97	-36290	142	578	0	134	-60	6.28	6.28	12.57	12.57	3	0.01	0.01	0.04	0.00	0.00	24.0
2	97	-27665	360	462	0	63	-311	6.28	6.28	12.57	12.57	2	0.02	0.01	0.04	0.00	0.00	24.0
3	97	-27565	359	423	0	140	-309	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
4	97	-28265	-141	467	0	67	217	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
5	97	-28175	-142	428	0	143	219	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
6	97	-27985	186	509	0	-25	-128	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
7	97	-27665	182	380	0	230	-123	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
8	97	-28165	36	510	0	-24	31	6.28	6.28	12.57	12.57	2	0.00	0.01	0.04	0.00	0.00	24.0
9	97	-27845	32	381	0	231	35	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
10	97	-27665	360	462	0	63	-311	6.28	6.28	12.57	12.57	2	0.02	0.01	0.04	0.00	0.00	24.0
11	97	-27565	359	423	0	140	-309	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
12	97	-28265	-141	467	0	67	217	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
13	97	-28175	-142	428	0	143	219	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
14	97	-27985	186	509	0	-25	-128	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
15	97	-27665	182	380	0	230	-123	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
16	97	-28165	36	510	0	-24	31	6.28	6.28	12.57	12.57	2	0.00	0.01	0.04	0.00	0.00	24.0
17	97	-27845	32	381	0	231	35	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
18	97	-42040	1007	708	0	-62	-852	6.28	6.28	12.57	12.57	3	0.04	0.02	0.07	0.00	0.00	24.0
19	97	-42030	-638	694	0	-5	732	6.28	6.28	12.57	12.57	3	0.03	0.01	0.05	0.00	0.00	24.0
20	97	-41200	182	413	0	-133	-62	6.28	6.28	12.57	12.57	3	0.01	0.01	0.03	0.00	0.00	24.0
37	97	-39910	1541	664	0	-33	-1380	6.28	6.28	12.57	12.57	3	0.06	0.03	0.11	0.00	0.00	24.0
38	97	-39900	-1200	640	0	64	1260	6.28	6.28	12.57	12.57	3	0.06	0.02	0.08	0.00	0.00	24.0
39	97	-38518	167	172	0	-149	-65	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	195	-35530	142	578	0	-430	78	6.28	6.28	12.57	12.57	3	0.01	0.01	0.04	0.00	0.00	24.0
2	195	-27080	360	462	0	-387	40	6.28	6.28	12.57	12.57	2	0.02	0.01	0.04	0.00	0.00	24.0
3	195	-26980	359	423	0	-273	41	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
4	195	-27680	-141	467	0	-389	80	6.28	6.28	12.57	12.57	2	0.02	0.01	0.04	0.00	0.00	24.0
5	195	-27590	-142	428	0	-274	80	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
6	195	-27400	186	509	0	-521	54	6.28	6.28	12.57	12.57	2	0.02	0.01	0.04	0.00	0.00	24.0
7	195	-27080	182	380	0	-140	55	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
8	195	-27580	36	510	0	-521	66	6.28	6.28	12.57	12.57	2	0.02	0.01	0.04	0.00	0.00	24.0
9	195	-27260	32	381	0	-141	67	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
10	195	-27080	360	462	0	-387	40	6.28	6.28	12.57	12.57	2	0.02	0.01	0.04	0.00	0.00	24.0
11	195	-26980	359	423	0	-273	41	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
12	195	-27680	-141	467	0	-389	80	6.28	6.28	12.57	12.57	2	0.02	0.01	0.04	0.00	0.00	24.0
13	195	-27590	-142	428	0	-274	80	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
14	195	-27400	186	509	0	-521	54	6.28	6.28	12.57	12.57	2	0.02	0.01	0.04	0.00	0.00	24.0
15	195	-27080	182	380	0	-140	55	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
16	195	-27580	36	510	0	-521	66	6.28	6.28	12.57	12.57	2	0.02	0.01	0.04	0.00	0.00	24.0
17	195	-27260	32	381	0	-141	67	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
18	195	-41280	1007	708	0	-753	130	6.28	6.28	12.57	12.57	3	0.02	0.02	0.06	0.00	0.00	24.0
19	195	-41270	-638	694	0	-681	110	6.28	6.28	12.57	12.57	3	0.02	0.01	0.05	0.00	0.00	24.0
20	195	-40440	182	413	0	-535	115	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
37	195	-39150	1541	664	0	-681	123	6.28	6.28	12.57	12.57	3	0.02	0.03	0.10	0.00	0.00	24.0
38	195	-39140	-1200	640	0	-560	90	6.28	6.28	12.57	12.57	3	0.02	0.02	0.08	0.00	0.00	24.0
39	195	-37755	167	172	0	-317	98	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	292	-34770	142	578	0	-994	216	6.28	6.28	12.57	12.57	3	0.03	0.01	0.04	0.00	0.00	24.0
2	292	-26495	360	462	0	-838	392	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
3	292	-26395	359	423	0	-685	391	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
4	292	-27095	-141	467	0	-844	-58	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
5	292	-27005	-142	428	0	-692	-59	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
6	292	-26815	186	509	0	-1017	235	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
7	292	-26495	182	380	0	-510	233	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
8	292	-26995	36	510	0	-1019	100	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
9	292	-26675	32	381	0	-512	98	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
10	292	-26495	360	462	0	-838	392	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
11	292	-26395	359	423	0	-685	391	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
12	292	-27095	-141	467	0	-844	-58	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
13	292	-27005	-142	428	0	-692	-59	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
14	292	-26815	186	509	0	-1017	235	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
15	292	-26495	182	380	0	-510	233	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
16	292	-26995	36	510	0	-1019	100	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
17	292	-26675	32	381	0	-512	98	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0

18	292	-40520	1007	708	0	-1444	1111	6.28	6.28	12.57	12.57	3	0.07	0.02	0.06	0.00	0.00	24.0
19	292	-40510	-638	694	0	-1357	-512	6.28	6.28	12.57	12.57	3	0.05	0.01	0.05	0.00	0.00	24.0
20	292	-39680	182	413	0	-938	292	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
37	292	-38390	1541	664	0	-1328	1626	6.28	6.28	12.57	12.57	3	0.08	0.03	0.11	0.00	0.00	24.0
38	292	-38380	-1200	640	0	-1183	-1080	6.28	6.28	12.57	12.57	3	0.06	0.02	0.08	0.00	0.00	24.0
39	292	-36992	167	172	0	-485	261	6.28	6.28	12.57	12.57	3	0.02	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	390	-34010	142	578	0	-1558	354	6.28	6.28	12.57	12.57	3	0.05	0.01	0.04	0.00	0.00	24.0
2	390	-25910	360	462	0	-1288	743	6.28	6.28	12.57	12.57	2	0.08	0.01	0.04	0.00	0.00	24.0
3	390	-25810	359	423	0	-1098	741	6.28	6.28	12.57	12.57	2	0.07	0.01	0.03	0.00	0.00	24.0
4	390	-26510	-141	467	0	-1299	-196	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
5	390	-26420	-142	428	0	-1109	-198	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
6	390	-26230	186	509	0	-1513	416	6.28	6.28	12.57	12.57	2	0.08	0.01	0.04	0.00	0.00	24.0
7	390	-25910	182	380	0	-880	410	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
8	390	-26410	36	510	0	-1516	135	6.28	6.28	12.57	12.57	2	0.07	0.01	0.04	0.00	0.00	24.0
9	390	-26090	32	381	0	-884	129	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
10	390	-25910	360	462	0	-1288	743	6.28	6.28	12.57	12.57	2	0.08	0.01	0.04	0.00	0.00	24.0
11	390	-25810	359	423	0	-1098	741	6.28	6.28	12.57	12.57	2	0.07	0.01	0.03	0.00	0.00	24.0
12	390	-26510	-141	467	0	-1299	-196	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
13	390	-26420	-142	428	0	-1109	-198	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
14	390	-26230	186	509	0	-1513	416	6.28	6.28	12.57	12.57	2	0.08	0.01	0.04	0.00	0.00	24.0
15	390	-25910	182	380	0	-880	410	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
16	390	-26410	36	510	0	-1516	135	6.28	6.28	12.57	12.57	2	0.07	0.01	0.04	0.00	0.00	24.0
17	390	-26090	32	381	0	-884	129	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
18	390	-39760	1007	708	0	-2134	2093	6.28	6.28	12.57	12.57	3	0.12	0.02	0.06	0.00	0.00	24.0
19	390	-39750	-638	694	0	-2033	-1135	6.28	6.28	12.57	12.57	3	0.08	0.01	0.05	0.00	0.00	24.0
20	390	-38920	182	413	0	-1341	470	6.28	6.28	12.57	12.57	3	0.05	0.01	0.03	0.00	0.00	24.0
37	390	-37630	1541	664	0	-1976	3129	6.28	6.28	12.57	12.57	3	0.15	0.03	0.11	0.00	0.00	24.0
38	390	-37620	-1200	640	0	-1807	-2250	6.28	6.28	12.57	12.57	3	0.12	0.02	0.08	0.00	0.00	24.0
39	390	-36230	167	172	0	-653	423	6.28	6.28	12.57	12.57	3	0.03	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

VERIFICA NODO IN TESTA AL PILASTRO, NODO NUM. 296 NON CONFINATO

(par.7.2.2 NTC2018 "La domanda di resistenza valutata con i criteri della progettazione in capacità può essere assunta non superiore alla domanda di resistenza valutata per il caso di comportamento strutturale non dissipativo.")

PROGETTAZIONE IN CAPACITA'

Asse loc. pilastro y nodo INTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 50.0 cm, hjc= 30.0 cm
Asse loc. pilastro z nodo INTERNO: As2(inf)= 6.03, As1(sup)= 6.03, Hjw= 40.0 cm, bj= 40.0 cm, hjc= 50.0 cm

FxMin,inf	FxMin,sup	FxMax,sup	FySup	FzSup	Vjbdy	Vjbdz	Vres,y	Vres,z	I.R.compr.	Ashy	Ashz	PASSO	Nota
daN					daN		daN			cmq		cm	
-25810	-11450	-12250	65	102	35168	52747	127376	169834	0.31	8.64	10.18	4.39	

VERIFICA DI RESISTENZA CON SOLLECITAZIONI COMPORTAMENTO NON DISSIPATIVO

Asse loc. pilastro y nodo INTERNO: Hjw= 40.0 cm, bj= 50.0 cm, hjc= 30.0 cm, db1= 45.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb,1	Mb,2	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-11530	-25910	-2591	-888	546	3658	127607	0.03	0.00	40.00	
3	-11450	-25810	-2587	-896	540	3636	127633	0.03	0.00	40.00	
4	-12250	-26510	-923	-2419	790	2903	127376	0.02	0.00	40.00	
5	-12160	-26420	-919	-2427	796	2928	127405	0.02	0.00	40.00	
6	-11880	-26230	-2012	-1415	86	1388	127495	0.01	0.00	40.00	
7	-11600	-25910	-1998	-1441	65	1310	127585	0.01	0.00	40.00	
8	-12100	-26410	-1512	-1875	315	581	127424	0.00	0.00	40.00	
9	-11810	-26090	-1498	-1900	336	657	127517	0.01	0.00	40.00	
10	-11530	-25910	-2591	-888	546	3658	127607	0.03	0.00	40.00	
11	-11450	-25810	-2587	-896	540	3636	127633	0.03	0.00	40.00	
12	-12250	-26510	-923	-2419	790	2903	127376	0.02	0.00	40.00	
13	-12160	-26420	-919	-2427	796	2928	127405	0.02	0.00	40.00	
14	-11880	-26230	-2012	-1415	86	1388	127495	0.01	0.00	40.00	
15	-11600	-25910	-1998	-1441	65	1310	127585	0.01	0.00	40.00	
16	-12100	-26410	-1512	-1875	315	581	127424	0.00	0.00	40.00	
17	-11810	-26090	-1498	-1900	336	657	127517	0.01	0.00	40.00	

Asse loc. pilastro z nodo INTERNO: Hjw= 40.0 cm, bj= 40.0 cm, hjc= 50.0 cm, db1= 45.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb,1	Mb,2	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-11530	-25910	-2584	-2484	328	81	170143	0.00	0.00	40.00	
3	-11450	-25810	-2298	-2766	224	932	170177	0.01	0.00	40.00	
4	-12250	-26510	-2535	-2452	329	124	169834	0.00	0.00	40.00	
5	-12160	-26420	-2250	-2733	225	968	169873	0.01	0.00	40.00	
6	-11880	-26230	-2900	-2145	450	1414	169993	0.01	0.00	40.00	
7	-11600	-25910	-1948	-3083	102	2700	170113	0.02	0.00	40.00	
8	-12100	-26410	-2885	-2135	451	1401	169898	0.01	0.00	40.00	
9	-11810	-26090	-1934	-3073	102	2710	170023	0.02	0.00	40.00	
10	-11530	-25910	-2584	-2484	328	81	170143	0.00	0.00	40.00	
11	-11450	-25810	-2298	-2766	224	932	170177	0.01	0.00	40.00	
12	-12250	-26510	-2535	-2452	329	124	169834	0.00	0.00	40.00	
13	-12160	-26420	-2250	-2733	225	968	169873	0.01	0.00	40.00	
14	-11880	-26230	-2900	-2145	450	1414	169993	0.01	0.00	40.00	
15	-11600	-25910	-1948	-3083	102	2700	170113	0.02	0.00	40.00	
16	-12100	-26410	-2885	-2135	451	1401	169898	0.01	0.00	40.00	
17	-11810	-26090	-1934	-3073	102	2710	170023	0.02	0.00	40.00	

CONFRONTO E SINTESI CONCLUSIVE (si assume in ogni caso passo <= 15 cm)

I.R.compr.	Ashy	Ashz	PASSO	Nota
	cmq		cm	
0.03	--	--	15.00	**VERIFICATO**

ASTA NUM. 40 NI 301 NF 298 SEZ. Rp B= 0.600 H= 0.400 (pilastro)

PIL. NUM. 20B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-34870	124	713	0	921	-261	6.28	6.28	12.57	12.57	3	0.03	0.01	0.05	0.00	0.00	24.0
2	0	-26650	323	578	0	705	-688	6.28	6.28	12.57	12.57	2	0.06	0.01	0.05	0.00	0.00	24.0
3	0	-26610	322	547	0	761	-685	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
4	0	-27040	-131	550	0	655	284	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
5	0	-27000	-132	520	0	711	287	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
6	0	-26840	165	604	0	622	-351	6.28	6.28	12.57	12.57	2	0.04	0.01	0.05	0.00	0.00	24.0
7	0	-26690	162	502	0	809	-342	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
8	0	-26960	29	595	0	607	-59	6.28	6.28	12.57	12.57	2	0.03	0.01	0.05	0.00	0.00	24.0
9	0	-26810	26	494	0	794	-50	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
10	0	-26650	323	578	0	705	-688	6.28	6.28	12.57	12.57	2	0.06	0.01	0.05	0.00	0.00	24.0
11	0	-26610	322	547	0	761	-685	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
12	0	-27040	-131	550	0	655	284	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
13	0	-27000	-132	520	0	711	287	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
14	0	-26840	165	604	0	622	-351	6.28	6.28	12.57	12.57	2	0.04	0.01	0.05	0.00	0.00	24.0
15	0	-26690	162	502	0	809	-342	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
16	0	-26960	29	595	0	607	-59	6.28	6.28	12.57	12.57	2	0.03	0.01	0.05	0.00	0.00	24.0
17	0	-26810	26	494	0	794	-50	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
18	0	-37980	932	1006	0	1184	-1869	6.28	6.28	12.57	12.57	3	0.09	0.02	0.07	0.00	0.00	24.0
19	0	-39820	-585	902	0	981	1207	6.28	6.28	12.57	12.57	3	0.06	0.01	0.06	0.00	0.00	24.0
20	0	-38380	173	704	0	829	-331	6.28	6.28	12.57	12.57	3	0.03	0.01	0.05	0.00	0.00	24.0
37	0	-35830	1420	952	0	1184	-2869	6.28	6.28	12.57	12.57	3	0.14	0.02	0.10	0.00	0.00	24.0
38	0	-38900	-1108	779	0	846	2257	6.28	6.28	12.57	12.57	3	0.11	0.02	0.08	0.00	0.00	24.0
39	0	-36500	155	450	0	592	-306	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
1	97	-34110	124	713	0	225	-139	6.28	6.28	12.57	12.57	3	0.01	0.01	0.05	0.00	0.00	24.0
2	97	-26065	323	578	0	141	-373	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
3	97	-26025	322	547	0	227	-371	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
4	97	-26455	-131	550	0	119	157	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
5	97	-26415	-132	520	0	205	159	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
6	97	-26255	165	604	0	33	-190	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
7	97	-26105	162	502	0	319	-183	6.28	6.28	12.57	12.57	2	0.02	0.01	0.04	0.00	0.00	24.0
8	97	-26375	29	595	0	27	-31	6.28	6.28	12.57	12.57	2	0.00	0.01	0.05	0.00	0.00	24.0
9	97	-26225	26	494	0	312	-25	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
10	97	-26065	323	578	0	141	-373	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
11	97	-26025	322	547	0	227	-371	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
12	97	-26455	-131	550	0	119	157	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
13	97	-26415	-132	520	0	205	159	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
14	97	-26255	165	604	0	33	-190	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
15	97	-26105	162	502	0	319	-183	6.28	6.28	12.57	12.57	2	0.02	0.01	0.04	0.00	0.00	24.0
16	97	-26375	29	595	0	27	-31	6.28	6.28	12.57	12.57	2	0.00	0.01	0.05	0.00	0.00	24.0
17	97	-26225	26	494	0	312	-25	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
18	97	-37220	932	1006	0	204	-960	6.28	6.28	12.57	12.57	3	0.04	0.02	0.07	0.00	0.00	24.0
19	97	-39060	-585	902	0	102	637	6.28	6.28	12.57	12.57	3	0.03	0.01	0.06	0.00	0.00	24.0
20	97	-37620	173	704	0	143	-162	6.28	6.28	12.57	12.57	3	0.01	0.01	0.05	0.00	0.00	24.0
37	97	-35070	1420	952	0	255	-1484	6.28	6.28	12.57	12.57	3	0.07	0.02	0.10	0.00	0.00	24.0
38	97	-38140	-1108	779	0	86	1177	6.28	6.28	12.57	12.57	3	0.05	0.02	0.08	0.00	0.00	24.0
39	97	-35740	155	450	0	154	-154	6.28	6.28	12.57	12.57	3	0.01	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
1	195	-33350	124	713	0	-471	-18	6.28	6.28	12.57	12.57	3	0.01	0.01	0.05	0.00	0.00	24.0
2	195	-25480	323	578	0	-422	-58	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
3	195	-25440	322	547	0	-306	-57	6.28	6.28	12.57	12.57	2	0.02	0.01	0.04	0.00	0.00	24.0
4	195	-25870	-131	550	0	-418	29	6.28	6.28	12.57	12.57	2	0.02	0.01	0.04	0.00	0.00	24.0
5	195	-25830	-132	520	0	-302	30	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
6	195	-25670	165	604	0	-555	-29	6.28	6.28	12.57	12.57	2	0.03	0.01	0.05	0.00	0.00	24.0
7	195	-25520	162	502	0	-171	-25	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
8	195	-25790	29	595	0	-553	-3	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
9	195	-25640	26	494	0	-169	1	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
10	195	-25480	323	578	0	-422	-58	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
11	195	-25440	322	547	0	-306	-57	6.28	6.28	12.57	12.57	2	0.02	0.01	0.04	0.00	0.00	24.0
12	195	-25870	-131	550	0	-418	29	6.28	6.28	12.57	12.57	2	0.02	0.01	0.04	0.00	0.00	24.0
13	195	-25830	-132	520	0	-302	30	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
14	195	-25670	165	604	0	-555	-29	6.28	6.28	12.57	12.57	2	0.03	0.01	0.05	0.00	0.00	24.0
15	195	-25520	162	502	0	-171	-25	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
16	195	-25790	29	595	0	-553	-3	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
17	195	-25640	26	494	0	-169	1	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
18	195	-36460	932	1006	0	-777	-52	6.28	6.28	12.57	12.57	3	0.02	0.02	0.07	0.00	0.00	24.0
19	195	-38300	-585	902	0	-777	67	6.28	6.28	12.57	12.57	3	0.02	0.01	0.06	0.00	0.00	24.0
20	195	-36860	173	704	0	-543	6	6.28	6.28	12.57	12.57	3	0.02	0.01	0.05	0.00	0.00	24.0
37	195	-34310	1420	952	0	-674	-100	6.28	6.28	12.57	12.57	3	0.02	0.02	0.09	0.00	0.00	24.0
38	195	-37380	-1108	779	0	-673	97	6.28	6.28	12.57	12.57	3	0.02	0.02	0.07	0.00	0.00	24.0
39	195	-34980	155	450	0	-284	-3	6.28	6.28	12.57	12.57	3	0.01	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
1	292	-32590	124	713	0	-1166	103	6.28	6.28	12.57	12.57	3	0.04	0.01	0.05	0.00	0.00	24.0
2	292	-24895	323	578	0	-985	257	6.28	6.28	12.57	12.57	2	0.05	0.01	0.05	0.00	0.00	24.0
3	292	-24855	322	547	0	-840	258	6.28	6.28	12.57	12.57	2	0.04	0.01	0.05	0.00	0.00	24.0
4	292	-25285	-131	550	0	-954	-99	6.28	6.28	12.57	12.57	2	0.04	0.01	0.05	0.00	0.00	24.0
5	292	-25245	-132	520	0	-809	-99	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
6	292	-25085	165	604	0	-1144	132	6.28	6.28	12.57	12.57	2	0.05	0.01	0.05	0.00	0.00	24.0
7	292	-24935	162	502	0	-660	133	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
8	292	-25205	29	595	0	-1134	25	6.28	6.28	12.57	12.57	2	0.05	0.01	0.05	0.00	0.00	24.0
9	292	-25055	26	494	0	-651	26	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
10	292	-24895	323	578	0	-985	257	6.28	6.28	12.57	12.57	2	0.05	0.01	0.05	0.00	0.00	24.0
11	292	-24855	322	547	0	-840	258	6.28	6.28	12.57	12.57	2	0.04	0.01	0.05	0.00	0.00	24.0
12	292	-25285	-131	550	0	-954	-99	6.28	6.28	12.57	12.57	2	0.04	0.01	0.05	0.00	0.00	24.0
13	292	-25245	-132	520	0	-809	-99	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
14	292	-25085	165	604	0	-1144	132	6.28	6.28	12.57	12.57	2	0.05	0.01	0.05	0.00	0.00	24.0
15	292	-24935	162	502	0	-660	133	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
16	292	-25205	29	595	0	-1134	25	6.28	6.28	12.57	12.57	2	0.05	0.01	0.05	0.00	0.00	24.0
17	292	-25055	26	494	0	-651	26	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
18	292	-35700	932	1006	0	-1757	856	6.28	6.28	12.57	12.57	3	0.07	0.02	0.07	0.00	0.00	24.0
19	292	-37540	-585	902	0	-1656	-504	6.28	6.28	12.57	12.57	3	0.06	0.01	0.07	0.00	0.00	24.0
20	292	-36100	173	704	0	-1230	175	6.28	6.28	12.57	12.57	3	0.04	0.01	0.05	0.00	0.00	24.0
37	292	-33550	1420	952	0	-1602	1285	6.28	6.28	12.57	12.57	3	0.08	0.02	0.09	0.00	0.00	24.0
38	292	-36620	-1108	779	0	-1433	-983	6.28	6.28	12.57	12.57	3	0.06	0.02	0.07	0.00	0.00	24.0
39	292	-34220	155	450	0	-723	149	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	390	-31830	124	713	0	-1862	224	6.28	6.28	12.57	12.57	3	0.06	0.01	0.05	0.00	0.00	24.0
2	390	-24310	323	578	0	-1548	573	6.28	6.28	12.57	12.57	2	0.09	0.01	0.05	0.00	0.00	24.0
3	390	-24270	322	547	0	-1373	572	6.28	6.28	12.57	12.57	2	0.08	0.01	0.05	0.00	0.00	24.0
4	390	-24700	-131	550	0	-1491	-227	6.28	6.28	12.57	12.57	2	0.07	0.01	0.05	0.00	0.00	24.0
5	390	-24660	-132	520	0	-1316	-228	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
6	390	-24500	165	604	0	-1732	293	6.28	6.28	12.57	12.57	2	0.09	0.01	0.05	0.00	0.00	24.0
7	390	-24350	162	502	0	-1150	292	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
8	390	-24620	29	595	0	-1714	53	6.28	6.28	12.57	12.57	2	0.08	0.01	0.05	0.00	0.00	24.0
9	390	-24470	26	494	0	-1133	52	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
10	390	-24310	323	578	0	-1548	573	6.28	6.28	12.57	12.57	2	0.09	0.01	0.05	0.00	0.00	24.0
11	390	-24270	322	547	0	-1373	572	6.28	6.28	12.57	12.57	2	0.08	0.01	0.05	0.00	0.00	24.0
12	390	-24700	-131	550	0	-1491	-227	6.28	6.28	12.57	12.57	2	0.07	0.01	0.05	0.00	0.00	24.0
13	390	-24660	-132	520	0	-1316	-228	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
14	390	-24500	165	604	0	-1732	293	6.28	6.28	12.57	12.57	2	0.09	0.01	0.05	0.00	0.00	24.0
15	390	-24350	162	502	0	-1150	292	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
16	390	-24620	29	595	0	-1714	53	6.28	6.28	12.57	12.57	2	0.08	0.01	0.05	0.00	0.00	24.0
17	390	-24470	26	494	0	-1133	52	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
18	390	-34940	932	1006	0	-2738	1765	6.28	6.28	12.57	12.57	3	0.12	0.02	0.07	0.00	0.00	24.0
19	390	-36780	-585	902	0	-2535	-1074	6.28	6.28	12.57	12.57	3	0.10	0.01	0.07	0.00	0.00	24.0
20	390	-35340	173	704	0	-1916	343	6.28	6.28	12.57	12.57	3	0.06	0.01	0.05	0.00	0.00	24.0
37	390	-32790	1420	952	0	-2531	2670	6.28	6.28	12.57	12.57	3	0.15	0.02	0.10	0.00	0.00	24.0
38	390	-35860	-1108	779	0	-2192	-2063	6.28	6.28	12.57	12.57	3	0.12	0.02	0.07	0.00	0.00	24.0
39	390	-33460	155	450	0	-1161	300	6.28	6.28	12.57	12.57	3	0.04	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

VERIFICA NODO IN TESTA AL PILASTRO, NODO NUM. 298 NON CONFINATO

(par.7.2.2 NTC2018 "La domanda di resistenza valutata con i criteri della progettazione in capacità può essere assunta non superiore alla domanda di resistenza valutata per il caso di comportamento strutturale non dissipativo.")

PROGETTAZIONE IN CAPACITA'

Asse loc. pilastro y nodo INTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 50.0 cm, hjc= 30.0 cm
Asse loc. pilastro z nodo INTERNO: As2(inf)= 6.03, As1(sup)= 6.03, Hjw= 40.0 cm, bj= 40.0 cm, hjc= 50.0 cm

FxMin,inf	FxMin,sup	FxMax,sup	FySup	FzSup	Vjbdy	Vjbdz	Vres,y	Vres,z	I.R.compr.	Ashy	Ashz	PASSO	Nota
daN					daN		daN			cmq		cm	
-24270	-9473	-9963	66	0	35167	52849	128110	170813	0.31	8.68	10.98	4.03	

VERIFICA DI RESISTENZA CON SOLLECITAZIONI COMPORTAMENTO NON DISSIPATIVO

Asse loc. pilastro y nodo INTERNO: Hjw= 40.0 cm, bj= 50.0 cm, hjc= 30.0 cm, db1= 45.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb,1	Mb,2	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-9499	-24310	-2841	-1393	556	3019	128258	0.02	0.00	40.00	
3	-9473	-24270	-2832	-1396	550	2996	128267	0.02	0.00	40.00	
4	-9963	-24700	-1261	-2810	804	3021	128110	0.02	0.00	40.00	
5	-9937	-24660	-1253	-2813	811	3041	128118	0.02	0.00	40.00	
6	-9691	-24500	-2297	-1886	88	927	128197	0.01	0.00	40.00	
7	-9605	-24350	-2270	-1896	66	858	128224	0.01	0.00	40.00	
8	-9830	-24620	-1823	-2311	320	885	128152	0.01	0.00	40.00	
9	-9745	-24470	-1796	-2321	342	954	128180	0.01	0.00	40.00	
10	-9499	-24310	-2841	-1393	556	3019	128258	0.02	0.00	40.00	
11	-9473	-24270	-2832	-1396	550	2996	128267	0.02	0.00	40.00	
12	-9963	-24700	-1261	-2810	804	3021	128110	0.02	0.00	40.00	
13	-9937	-24660	-1253	-2813	811	3041	128118	0.02	0.00	40.00	
14	-9691	-24500	-2297	-1886	88	927	128197	0.01	0.00	40.00	
15	-9605	-24350	-2270	-1896	66	858	128224	0.01	0.00	40.00	
16	-9830	-24620	-1823	-2311	320	885	128152	0.01	0.00	40.00	
17	-9745	-24470	-1796	-2321	342	954	128180	0.01	0.00	40.00	

Asse loc. pilastro z nodo INTERNO: Hjw= 40.0 cm, bj= 40.0 cm, hjc= 50.0 cm, db1= 45.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb,1	Mb,2	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-9499	-24310	-2564	-2745	125	322	171011	0.00	0.00	40.00	
3	-9473	-24270	-2252	-3043	0	1953	171022	0.01	0.00	40.00	
4	-9963	-24700	-2597	-2688	146	79	170813	0.00	0.00	40.00	
5	-9937	-24660	-2285	-2986	21	1710	170824	0.01	0.00	40.00	
6	-9691	-24500	-2940	-2378	278	1110	170929	0.01	0.00	40.00	
7	-9605	-24350	-1900	-3371	138	3494	170966	0.02	0.00	40.00	
8	-9830	-24620	-2949	-2361	284	1168	170870	0.01	0.00	40.00	
9	-9745	-24470	-1910	-3354	132	3433	170906	0.02	0.00	40.00	
10	-9499	-24310	-2564	-2745	125	322	171011	0.00	0.00	40.00	
11	-9473	-24270	-2252	-3043	0	1953	171022	0.01	0.00	40.00	
12	-9963	-24700	-2597	-2688	146	79	170813	0.00	0.00	40.00	
13	-9937	-24660	-2285	-2986	21	1710	170824	0.01	0.00	40.00	
14	-9691	-24500	-2940	-2378	278	1110	170929	0.01	0.00	40.00	
15	-9605	-24350	-1900	-3371	138	3494	170966	0.02	0.00	40.00	
16	-9830	-24620	-2949	-2361	284	1168	170870	0.01	0.00	40.00	
17	-9745	-24470	-1910	-3354	132	3433	170906	0.02	0.00	40.00	

CONFRONTO E SINTESI CONCLUSIVE (si assume in ogni caso passo <= 15 cm)

I.R.compr.	Ashy	Ashz	PASSO	Nota
	cmq		cm	
0.02	--	--	15.00	**VERIFICATO**

ASTA NUM. 41 NI 35 NF 31 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 12D
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice resistenza	aswta	aswto	PASSO
--																

	cm		daN		daN*m		cmq				Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-4632	1046	416	0	-1107	-1374	6.28	6.28	12.57	12.57	3	0.09	0.02	0.11	0.00	0.00	24.0
2	0	-3607	847	302	0	-903	-1126	6.28	6.28	12.57	12.57	2	0.10	0.02	0.09	0.00	0.00	24.0
3	0	-3613	850	324	0	-879	-1129	6.28	6.28	12.57	12.57	2	0.10	0.02	0.09	0.00	0.00	24.0
4	0	-3514	759	316	0	-824	-986	6.28	6.28	12.57	12.57	2	0.09	0.01	0.08	0.00	0.00	24.0
5	0	-3520	762	338	0	-801	-989	6.28	6.28	12.57	12.57	2	0.09	0.01	0.08	0.00	0.00	24.0
6	0	-3567	812	282	0	-903	-1073	6.28	6.28	12.57	12.57	2	0.10	0.02	0.08	0.00	0.00	24.0
7	0	-3588	823	354	0	-824	-1084	6.28	6.28	12.57	12.57	2	0.09	0.02	0.08	0.00	0.00	24.0
8	0	-3539	786	286	0	-879	-1031	6.28	6.28	12.57	12.57	2	0.09	0.01	0.08	0.00	0.00	24.0
9	0	-3560	797	358	0	-801	-1041	6.28	6.28	12.57	12.57	2	0.09	0.01	0.08	0.00	0.00	24.0
10	0	-3607	847	302	0	-903	-1126	6.28	6.28	12.57	12.57	2	0.10	0.02	0.09	0.00	0.00	24.0
11	0	-3613	850	324	0	-879	-1129	6.28	6.28	12.57	12.57	2	0.10	0.02	0.09	0.00	0.00	24.0
12	0	-3514	759	316	0	-824	-986	6.28	6.28	12.57	12.57	2	0.09	0.01	0.08	0.00	0.00	24.0
13	0	-3520	762	338	0	-801	-989	6.28	6.28	12.57	12.57	2	0.09	0.01	0.08	0.00	0.00	24.0
14	0	-3567	812	282	0	-903	-1073	6.28	6.28	12.57	12.57	2	0.10	0.02	0.08	0.00	0.00	24.0
15	0	-3588	823	354	0	-824	-1084	6.28	6.28	12.57	12.57	2	0.09	0.02	0.08	0.00	0.00	24.0
16	0	-3539	786	286	0	-879	-1031	6.28	6.28	12.57	12.57	2	0.09	0.01	0.08	0.00	0.00	24.0
17	0	-3560	797	358	0	-801	-1041	6.28	6.28	12.57	12.57	2	0.09	0.01	0.08	0.00	0.00	24.0
18	0	-7784	918	1006	0	-3143	-1401	6.28	6.28	12.57	12.57	3	0.14	0.02	0.10	0.00	0.00	24.0
19	0	-5865	844	759	0	-1844	-1054	6.28	6.28	12.57	12.57	3	0.09	0.02	0.08	0.00	0.00	24.0
20	0	-6372	978	-100	0	-7385	-1322	6.28	6.28	12.57	12.57	3	0.29	0.02	0.09	0.00	0.00	24.0
37	0	-7815	1007	938	0	-3131	-1576	6.28	6.28	12.57	12.57	3	0.14	0.02	0.10	0.00	0.00	24.0
38	0	-4615	883	526	0	-966	-999	6.28	6.28	12.57	12.57	3	0.06	0.02	0.09	0.00	0.00	24.0
39	0	-5461	1106	-906	0	-10200	-1445	6.28	6.28	12.57	12.57	3	0.40	0.02	0.10	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	58	-4181	1046	416	0	-1348	-769	6.28	6.28	12.57	12.57	3	0.07	0.02	0.09	0.00	0.00	24.0
2	58	-3260	847	302	0	-1078	-636	6.28	6.28	12.57	12.57	2	0.08	0.02	0.08	0.00	0.00	24.0
3	58	-3266	850	324	0	-1066	-637	6.28	6.28	12.57	12.57	2	0.08	0.02	0.08	0.00	0.00	24.0
4	58	-3167	759	316	0	-1007	-547	6.28	6.28	12.57	12.57	2	0.08	0.01	0.07	0.00	0.00	24.0
5	58	-3173	762	338	0	-996	-548	6.28	6.28	12.57	12.57	2	0.08	0.01	0.07	0.00	0.00	24.0
6	58	-3220	812	282	0	-1066	-603	6.28	6.28	12.57	12.57	2	0.08	0.02	0.07	0.00	0.00	24.0
7	58	-3241	823	354	0	-1029	-608	6.28	6.28	12.57	12.57	2	0.08	0.02	0.08	0.00	0.00	24.0
8	58	-3192	786	286	0	-1045	-577	6.28	6.28	12.57	12.57	2	0.08	0.01	0.07	0.00	0.00	24.0
9	58	-3213	797	358	0	-1008	-580	6.28	6.28	12.57	12.57	2	0.08	0.01	0.07	0.00	0.00	24.0
10	58	-3260	847	302	0	-1078	-636	6.28	6.28	12.57	12.57	2	0.08	0.02	0.08	0.00	0.00	24.0
11	58	-3266	850	324	0	-1066	-637	6.28	6.28	12.57	12.57	2	0.08	0.02	0.08	0.00	0.00	24.0
12	58	-3167	759	316	0	-1007	-547	6.28	6.28	12.57	12.57	2	0.08	0.01	0.07	0.00	0.00	24.0
13	58	-3173	762	338	0	-996	-548	6.28	6.28	12.57	12.57	2	0.08	0.01	0.07	0.00	0.00	24.0
14	58	-3220	812	282	0	-1066	-603	6.28	6.28	12.57	12.57	2	0.08	0.02	0.07	0.00	0.00	24.0
15	58	-3241	823	354	0	-1029	-608	6.28	6.28	12.57	12.57	2	0.08	0.02	0.08	0.00	0.00	24.0
16	58	-3192	786	286	0	-1045	-577	6.28	6.28	12.57	12.57	2	0.08	0.01	0.07	0.00	0.00	24.0
17	58	-3213	797	358	0	-1008	-580	6.28	6.28	12.57	12.57	2	0.08	0.01	0.07	0.00	0.00	24.0
18	58	-7333	918	1006	0	-3725	-870	6.28	6.28	12.57	12.57	3	0.15	0.02	0.10	0.00	0.00	24.0
19	58	-5414	844	759	0	-2283	-566	6.28	6.28	12.57	12.57	3	0.09	0.02	0.08	0.00	0.00	24.0
20	58	-5921	978	-418	0	-7235	-757	6.28	6.28	12.57	12.57	3	0.28	0.02	0.09	0.00	0.00	24.0
37	58	-7364	1007	938	0	-3674	-994	6.28	6.28	12.57	12.57	3	0.15	0.02	0.10	0.00	0.00	24.0
38	58	-4164	883	526	0	-1270	-488	6.28	6.28	12.57	12.57	3	0.06	0.02	0.08	0.00	0.00	24.0
39	58	-5010	1106	-1435	0	-9523	-805	6.28	6.28	12.57	12.57	3	0.36	0.03	0.15	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	116	-3730	1046	416	0	-1588	-165	6.28	6.28	12.57	12.57	3	0.06	0.02	0.09	0.00	0.00	24.0
2	116	-2913	847	302	0	-1252	-146	6.28	6.28	12.57	12.57	2	0.07	0.02	0.08	0.00	0.00	24.0
3	116	-2919	850	324	0	-1254	-146	6.28	6.28	12.57	12.57	2	0.07	0.02	0.08	0.00	0.00	24.0
4	116	-2820	759	316	0	-1190	-108	6.28	6.28	12.57	12.57	2	0.07	0.01	0.07	0.00	0.00	24.0
5	116	-2826	762	338	0	-1191	-107	6.28	6.28	12.57	12.57	2	0.07	0.01	0.07	0.00	0.00	24.0
6	116	-2873	812	282	0	-1229	-134	6.28	6.28	12.57	12.57	2	0.07	0.02	0.07	0.00	0.00	24.0
7	116	-2894	823	354	0	-1233	-132	6.28	6.28	12.57	12.57	2	0.07	0.02	0.08	0.00	0.00	24.0
8	116	-2845	786	286	0	-1210	-122	6.28	6.28	12.57	12.57	2	0.07	0.01	0.07	0.00	0.00	24.0
9	116	-2866	797	358	0	-1214	-120	6.28	6.28	12.57	12.57	2	0.07	0.01	0.07	0.00	0.00	24.0
10	116	-2913	847	302	0	-1252	-146	6.28	6.28	12.57	12.57	2	0.07	0.02	0.08	0.00	0.00	24.0
11	116	-2919	850	324	0	-1254	-146	6.28	6.28	12.57	12.57	2	0.07	0.02	0.08	0.00	0.00	24.0
12	116	-2820	759	316	0	-1190	-108	6.28	6.28	12.57	12.57	2	0.07	0.01	0.07	0.00	0.00	24.0
13	116	-2826	762	338	0	-1191	-107	6.28	6.28	12.57	12.57	2	0.07	0.01	0.07	0.00	0.00	24.0
14	116	-2873	812	282	0	-1229	-134	6.28	6.28	12.57	12.57	2	0.07	0.02	0.07	0.00	0.00	24.0
15	116	-2894	823	354	0	-1233	-132	6.28	6.28	12.57	12.57	2	0.07	0.02	0.08	0.00	0.00	24.0
16	116	-2845	786	286	0	-1210	-122	6.28	6.28	12.57	12.57	2	0.07	0.01	0.07	0.00	0.00	24.0
17	116	-2866	797	358	0	-1214	-120	6.28	6.28	12.57	12.57	2	0.07	0.01	0.07	0.00	0.00	24.0
18	116	-6882	918	1006	0	-4307	-339	6.28	6.28	12.57	12.57	3	0.16	0.02	0.10	0.00	0.00	24.0
19	116	-4963	844	759	0	-2722	-78	6.28	6.28	12.57	12.57	3	0.10	0.02	0.08	0.00	0.00	24.0
20	116	-5470	978	-736	0	-6902	-191	6.28	6.28	12.57	12.57	3	0.26	0.02	0.09	0.00	0.00	24.0
37	116	-6912	1007	938	0	-4216	-412	6.28	6.28	12.57	12.57	3	0.16	0.02	0.10	0.00	0.00	24.0
38	116	-3713	883	526	0	-1574	23	6.28	6.28	12.57	12.57	3	0.06	0.02	0.08	0.00	0.00	24.0
39	116	-4558	1106	-1965	0	-8540	-165	6.28	6.28	12.57	12.57	3	0.32	0.03	0.21	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	173	-3279	1046	416	0	-1829	440	6.28	6.28	12.57	12.57	3	0.08	0.02	0.10	0.00	0.00	24.0
2	173	-2566	847	302	0	-1427	343	6.28	6.28	12.57	12.57	2	0.09	0.02	0.08	0.00	0.00	24.0
3	173	-2572	850	324	0	-1441	346	6.28	6.28	12.57	12.57	2	0.09	0.02	0.08	0.00	0.00	24.0
4	173	-2473	759	316	0	-1372	331	6.28	6.28	12.57	12.57	2	0.09	0.01	0.07	0.00	0.00	24.0
5	173	-2479	762	338	0	-1386	334	6.28	6.28	12.57	12.57	2	0.09	0.01	0.07	0.00	0.00	24.0
6	173	-2526	812	282	0	-1393	336	6.28	6.28	12.57	12.57	2	0.09	0.02	0.07	0.00	0.00	24.0
7	173	-2547	823	354	0	-1438	345	6.28	6.28	12.57	12.57	2	0.09	0.02	0.08	0.00	0.00	24.0
8	173	-2498	786	286	0	-1376	332	6.28	6.28	12.57	12.57	2	0.09	0.01	0.07	0.00	0.00	24.0
9	173	-2519	797	358	0	-1421	341	6.28	6.28	12.57	12.57	2	0.09	0.01	0.07	0.00	0.00	24.0
10	173	-2566	847	302	0	-1427	343	6.28	6.28	12.57	12.57	2	0.09	0.02	0.08	0.00	0.00	24.0
11	173	-2572	850	324	0	-1441	346	6.28	6.28	12.57	12.57	2	0.09	0.02	0.08	0.00	0.00	24.0
12	173	-2473	759	316	0	-1372	331	6.28	6.28	12.57	12.57	2	0.09	0.01	0.07	0.00	0.00	24.0
13	173	-2479	762	338	0	-1386	334	6.28	6.28	12.57	12.57	2	0.09	0.01	0.07	0.00	0.00	24.0
14	173	-2526	812	282	0	-1393	336	6.28	6.28	12.57	12.57	2	0.09	0.02	0.07	0.00	0.00	24.0
15	173	-2547	823	354	0	-1438	345	6.28	6.28	12.57	12.57	2	0.09	0.02	0.08	0.00	0.00	24.0
16	173	-2498	786	286	0	-1376	332	6.28	6.28	12.57	12.57	2	0.09	0.01	0.07	0.00	0.00	24.0
17	173	-2519	797	358	0	-1421	341	6.28	6.28	12.57	12.57	2	0.09	0.01	0.07	0.00	0.00	24.0
18	173	-6431	918	1006	0	-4889	192	6.28	6.28	12.57	12.57	3	0.18	0.02	0.11	0.00	0.00	24.0
19	173	-4512	844	759	0	-3161	410	6.28	6.28	12.57	12.57	3	0.12	0.02	0.08	0.00	0.00	24.0
20	173	-5019	978	-1053	0	-6385	374	6.28	6.28	12.57	12.57	3	0.24	0.02	0.11	0.00	0.00	24.0
37	173	-6461	1007	938	0	-4758	170	6.28	6.28	12.57	12.57	3	0.18	0.02	0.10	0.00	0.00	24.0
38	173	-3262	883	526	0	-1878	534	6.28	6.28	12.57	12.57	3	0.08	0.02	0.08	0.00	0.00	24.0
39	173	-4107	1106	-2494	0	-7250	474	6.28	6.28	12.57	12.57	3	0.28	0.04	0.27	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	231	-2828	1046	416	0	-2069	1045	6.28	6.28	12.57	12.57	3	0.10	0.02	0.10	0.00	0.00	24.0
2	231	-2219	847	302	0	-1602	833	6.28	6.28	12.57	12.57	2	0.12	0.02	0.08	0.00	0.00	24.0
3	231	-2225	850	324	0	-1628	838	6.28	6.28	12.57	12.57	2	0.12	0.02	0.08	0.00	0.00	24.0

4	231	-2126	759	316	0	-1555	770	6.28	6.28	12.57	12.57	2	0.12	0.01	0.07	0.00	0.00	24.0
5	231	-2132	762	338	0	-1581	774	6.28	6.28	12.57	12.57	2	0.12	0.01	0.07	0.00	0.00	24.0
6	231	-2179	812	282	0	-1556	806	6.28	6.28	12.57	12.57	2	0.12	0.02	0.07	0.00	0.00	24.0
7	231	-2200	823	354	0	-1642	821	6.28	6.28	12.57	12.57	2	0.12	0.02	0.08	0.00	0.00	24.0
8	231	-2151	786	286	0	-1542	787	6.28	6.28	12.57	12.57	2	0.12	0.01	0.07	0.00	0.00	24.0
9	231	-2172	797	358	0	-1628	802	6.28	6.28	12.57	12.57	2	0.12	0.01	0.07	0.00	0.00	24.0
10	231	-2219	847	302	0	-1602	833	6.28	6.28	12.57	12.57	2	0.12	0.02	0.08	0.00	0.00	24.0
11	231	-2225	850	324	0	-1628	838	6.28	6.28	12.57	12.57	2	0.12	0.02	0.08	0.00	0.00	24.0
12	231	-2126	759	316	0	-1555	770	6.28	6.28	12.57	12.57	2	0.12	0.01	0.07	0.00	0.00	24.0
13	231	-2132	762	338	0	-1581	774	6.28	6.28	12.57	12.57	2	0.12	0.01	0.07	0.00	0.00	24.0
14	231	-2179	812	282	0	-1556	806	6.28	6.28	12.57	12.57	2	0.12	0.02	0.07	0.00	0.00	24.0
15	231	-2200	823	354	0	-1642	821	6.28	6.28	12.57	12.57	2	0.12	0.02	0.08	0.00	0.00	24.0
16	231	-2151	786	286	0	-1542	787	6.28	6.28	12.57	12.57	2	0.12	0.01	0.07	0.00	0.00	24.0
17	231	-2172	797	358	0	-1628	802	6.28	6.28	12.57	12.57	2	0.12	0.01	0.07	0.00	0.00	24.0
18	231	-5980	918	1006	0	-5471	723	6.28	6.28	12.57	12.57	3	0.21	0.02	0.11	0.00	0.00	24.0
19	231	-4061	844	759	0	-3600	898	6.28	6.28	12.57	12.57	3	0.15	0.02	0.08	0.00	0.00	24.0
20	231	-4568	978	-1371	0	-5684	939	6.28	6.28	12.57	12.57	3	0.23	0.02	0.15	0.00	0.00	24.0
37	231	-6010	1007	938	0	-5301	753	6.28	6.28	12.57	12.57	3	0.21	0.02	0.10	0.00	0.00	24.0
38	231	-2811	883	526	0	-2182	1045	6.28	6.28	12.57	12.57	3	0.10	0.02	0.08	0.00	0.00	24.0
39	231	-3656	1106	-3023	0	-5655	1114	6.28	6.28	12.57	12.57	3	0.23	0.05	0.33	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 42 NI 37 NF 43 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 17D
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-4591	206	282	0	-1806	-223	6.28	6.28	12.57	12.57	3	0.07	0.00	0.03	0.00	0.00	24.0
2	0	-3534	236	208	0	-1411	-293	6.28	6.28	12.57	12.57	2	0.09	0.00	0.02	0.00	0.00	24.0
3	0	-3581	237	225	0	-1363	-294	6.28	6.28	12.57	12.57	2	0.08	0.00	0.02	0.00	0.00	24.0
4	0	-3482	81	208	0	-1415	-49	6.28	6.28	12.57	12.57	2	0.08	0.00	0.02	0.00	0.00	24.0
5	0	-3528	81	226	0	-1366	-50	6.28	6.28	12.57	12.57	2	0.08	0.00	0.02	0.00	0.00	24.0
6	0	-3462	182	187	0	-1470	-206	6.28	6.28	12.57	12.57	2	0.09	0.00	0.02	0.00	0.00	24.0
7	0	-3617	183	246	0	-1307	-210	6.28	6.28	12.57	12.57	2	0.08	0.00	0.03	0.00	0.00	24.0
8	0	-3446	135	187	0	-1471	-132	6.28	6.28	12.57	12.57	2	0.08	0.00	0.02	0.00	0.00	24.0
9	0	-3601	136	246	0	-1308	-137	6.28	6.28	12.57	12.57	2	0.08	0.00	0.03	0.00	0.00	24.0
10	0	-3534	236	208	0	-1411	-293	6.28	6.28	12.57	12.57	2	0.09	0.00	0.02	0.00	0.00	24.0
11	0	-3581	237	225	0	-1363	-294	6.28	6.28	12.57	12.57	2	0.08	0.00	0.02	0.00	0.00	24.0
12	0	-3482	81	208	0	-1415	-49	6.28	6.28	12.57	12.57	2	0.08	0.00	0.02	0.00	0.00	24.0
13	0	-3528	81	226	0	-1366	-50	6.28	6.28	12.57	12.57	2	0.08	0.00	0.02	0.00	0.00	24.0
14	0	-3462	182	187	0	-1470	-206	6.28	6.28	12.57	12.57	2	0.09	0.00	0.02	0.00	0.00	24.0
15	0	-3617	183	246	0	-1307	-210	6.28	6.28	12.57	12.57	2	0.08	0.00	0.03	0.00	0.00	24.0
16	0	-3446	135	187	0	-1471	-132	6.28	6.28	12.57	12.57	2	0.08	0.00	0.02	0.00	0.00	24.0
17	0	-3601	136	246	0	-1308	-137	6.28	6.28	12.57	12.57	2	0.08	0.00	0.03	0.00	0.00	24.0
18	0	-8060	573	682	0	-4104	-813	6.28	6.28	12.57	12.57	3	0.16	0.01	0.07	0.00	0.00	24.0
19	0	-6842	-51	535	0	-3578	174	6.28	6.28	12.57	12.57	3	0.13	0.01	0.06	0.00	0.00	24.0
20	0	-7106	255	74	0	-9972	-314	6.28	6.28	12.57	12.57	3	0.37	0.00	0.02	0.00	0.00	24.0
37	0	-7568	769	624	0	-3621	-1117	6.28	6.28	12.57	12.57	3	0.15	0.01	0.07	0.00	0.00	24.0
38	0	-5538	-272	379	0	-2744	527	6.28	6.28	12.57	12.57	3	0.11	0.01	0.04	0.00	0.00	24.0
39	0	-5978	238	-389	0	-13400	-285	6.28	6.28	12.57	12.57	3	0.50	0.01	0.04	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	88	-3901	206	282	0	-2055	-40	6.28	6.28	12.57	12.57	3	0.08	0.00	0.03	0.00	0.00	24.0
2	88	-3003	236	208	0	-1595	-83	6.28	6.28	12.57	12.57	2	0.09	0.00	0.02	0.00	0.00	24.0
3	88	-3050	237	225	0	-1562	-84	6.28	6.28	12.57	12.57	2	0.09	0.00	0.02	0.00	0.00	24.0
4	88	-2951	81	208	0	-1599	23	6.28	6.28	12.57	12.57	2	0.09	0.00	0.02	0.00	0.00	24.0
5	88	-2997	81	226	0	-1566	22	6.28	6.28	12.57	12.57	2	0.09	0.00	0.02	0.00	0.00	24.0
6	88	-2931	182	187	0	-1636	-45	6.28	6.28	12.57	12.57	2	0.09	0.00	0.02	0.00	0.00	24.0
7	88	-3086	183	246	0	-1525	-48	6.28	6.28	12.57	12.57	2	0.08	0.00	0.03	0.00	0.00	24.0
8	88	-2915	135	187	0	-1637	-13	6.28	6.28	12.57	12.57	2	0.09	0.00	0.02	0.00	0.00	24.0
9	88	-3070	136	246	0	-1526	-17	6.28	6.28	12.57	12.57	2	0.08	0.00	0.03	0.00	0.00	24.0
10	88	-3003	236	208	0	-1595	-83	6.28	6.28	12.57	12.57	2	0.09	0.00	0.02	0.00	0.00	24.0
11	88	-3050	237	225	0	-1562	-84	6.28	6.28	12.57	12.57	2	0.09	0.00	0.02	0.00	0.00	24.0
12	88	-2951	81	208	0	-1599	23	6.28	6.28	12.57	12.57	2	0.09	0.00	0.02	0.00	0.00	24.0
13	88	-2997	81	226	0	-1566	22	6.28	6.28	12.57	12.57	2	0.09	0.00	0.02	0.00	0.00	24.0
14	88	-2931	182	187	0	-1636	-45	6.28	6.28	12.57	12.57	2	0.09	0.00	0.02	0.00	0.00	24.0
15	88	-3086	183	246	0	-1525	-48	6.28	6.28	12.57	12.57	2	0.08	0.00	0.03	0.00	0.00	24.0
16	88	-2915	135	187	0	-1637	-13	6.28	6.28	12.57	12.57	2	0.09	0.00	0.02	0.00	0.00	24.0
17	88	-3070	136	246	0	-1526	-17	6.28	6.28	12.57	12.57	2	0.08	0.00	0.03	0.00	0.00	24.0
18	88	-7370	573	682	0	-4708	-305	6.28	6.28	12.57	12.57	3	0.18	0.01	0.07	0.00	0.00	24.0
19	88	-6152	-51	535	0	-4051	129	6.28	6.28	12.57	12.57	3	0.15	0.01	0.06	0.00	0.00	24.0
20	88	-6416	255	-412	0	-9822	-88	6.28	6.28	12.57	12.57	3	0.36	0.01	0.04	0.00	0.00	24.0
37	88	-6878	769	624	0	-4174	-436	6.28	6.28	12.57	12.57	3	0.16	0.01	0.07	0.00	0.00	24.0
38	88	-4848	-272	379	0	-3080	287	6.28	6.28	12.57	12.57	3	0.12	0.01	0.04	0.00	0.00	24.0
39	88	-5288	238	-1199	0	-12697	-75	6.28	6.28	12.57	12.57	3	0.48	0.02	0.13	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	177	-3210	206	282	0	-2304	143	6.28	6.28	12.57	12.57	3	0.09	0.00	0.03	0.00	0.00	24.0
2	177	-2472	236	208	0	-1778	126	6.28	6.28	12.57	12.57	2	0.10	0.00	0.02	0.00	0.00	24.0
3	177	-2519	237	225	0	-1762	125	6.28	6.28	12.57	12.57	2	0.10	0.00	0.02	0.00	0.00	24.0
4	177	-2420	81	208	0	-1783	94	6.28	6.28	12.57	12.57	2	0.10	0.00	0.02	0.00	0.00	24.0
5	177	-2466	81	226	0	-1766	93	6.28	6.28	12.57	12.57	2	0.10	0.00	0.03	0.00	0.00	24.0
6	177	-2400	182	187	0	-1801	116	6.28	6.28	12.57	12.57	2	0.10	0.00	0.02	0.00	0.00	24.0
7	177	-2555	183	246	0	-1742	113	6.28	6.28	12.57	12.57	2	0.10	0.00	0.03	0.00	0.00	24.0
8	177	-2384	135	187	0	-1802	106	6.28	6.28	12.57	12.57	2	0.10	0.00	0.02	0.00	0.00	24.0
9	177	-2539	136	246	0	-1744	104	6.28	6.28	12.57	12.57	2	0.10	0.00	0.03	0.00	0.00	24.0
10	177	-2472	236	208	0	-1778	126	6.28	6.28	12.57	12.57	2	0.10	0.00	0.02	0.00	0.00	24.0
11	177	-2519	237	225	0	-1762	125	6.28	6.28	12.57	12.57	2	0.10	0.00	0.02	0.00	0.00	24.0
12	177	-2420	81	208	0	-1783	94	6.28	6.28	12.57	12.57	2	0.10	0.00	0.02	0.00	0.00	24.0
13	177	-2466	81	226	0	-1766	93	6.28	6.28	12.57	12.57	2	0.10	0.00	0.03	0.00	0.00	24.0
14	177	-2400	182	187	0	-1801	116	6.28	6.28	12.57	12.57	2	0.10	0.00	0.02	0.00	0.00	24.0
15	177	-2555	183	246	0	-1742	113	6.28	6.28	12.57	12.57	2	0.10	0.00	0.03	0.00	0.00	24.0
16	177	-2384	135	187	0	-1802	106	6.28	6.28	12.57	12.57	2	0.10	0.00	0.02	0.00	0.00	24.0
17	177	-2539	136	246	0	-1744	104	6.28	6.28	12.57	12.57	2	0.10	0.00	0.03	0.00	0.00	24.0
18	177	-6680	573	682	0	-5311	202	6.28	6.28	12.57	12.57	3	0.20	0.01	0.07	0.00	0.00	24.0
19	177	-5462	-51	535	0	-4525	84	6.28	6.28	12.57	12.57	3	0.17	0.01	0.06	0.00	0.00	24.0
20	177	-5726	255	-898	0	-9242	137	6.28	6.28	12.57	12.57	3	0.35	0.02	0.09	0.00	0.00	24.0
37	177	-6188	769	624	0	-4726	244	6.28	6.28	12.57	12.57	3	0.18	0.01	0.07	0.00	0.00	24.0
38	177	-4158	-272	379	0	-3415	47	6.28	6.28	12.57	12.57	3	0.13	0.01	0.04	0.00	0.00	24.0
39	177	-4598	238	-2009	0	-11278	136	6.28	6.28	12.57	12.57	3	0.43	0.04	0.22	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	266	-2520	206	282	0	-2553	325	6.28	6.28	12.57	12.57	3	0.10	0.00	0.03	0.00	0.00	24.0
2	266	-1941	236	208	0	-1962	335	6.28	6.28	12.57	12.57	2	0.12	0.00	0.02	0.00	0.00	24.0
3	266	-1988	237	225	0	-1961	335	6.28	6.28	12.57	12.57	2	0.12	0.00	0.03	0.00	0.00	24.0
4	266	-1889	81	208	0	-1967	165	6.28	6.28	12.57	12.57	2	0.11	0.00	0.02	0.00	0.00	24.0
5	266	-1935	81	226	0	-1965	165	6.28	6.28	12.57	12.57	2	0.11	0.00	0.03	0.00	0.00	24.0
6	266	-1869	182	187	0	-1966	276	6.28	6.28	12.57	12.57	2	0.12	0.00	0.02	0.00	0.00	24.0
7	266	-2024	183	246	0	-1960	275	6.28	6.28	12.57	12.57	2	0.12	0.00	0.03	0.00	0.00	24.0
8	266	-1853	135	187	0	-1968	225	6.28	6.28	12.57	12.57	2	0.12	0.00	0.02	0.00	0.00	24.0
9	266	-2008	136	246	0	-1961	224	6.28	6.28	12.57	12.57	2	0.12	0.00	0.03	0.00	0.00	24.0
10	266	-1941	236	208	0	-1962	335	6.28	6.28	12.57	12.57	2	0.12	0.00	0.02	0.00	0.00	24.0
11	266	-1988	237	225	0	-1961	335	6.28	6.28	12.57	12.57	2	0.12	0.00	0.03	0.00	0.00	24.0
12	266	-1889	81	208	0	-1967	165	6.28	6.28	12.57	12.57	2	0.11	0.00	0.02	0.00	0.00	24.0
13	266	-1935	81	226	0	-1965	165	6.28	6.28	12.57	12.57	2	0.11	0.00	0.03	0.00	0.00	24.0
14	266	-1869	182	187	0	-1966	276	6.28	6.28	12.57	12.57	2	0.12	0.00	0.02	0.00	0.00	24.0
15	266	-2024	183	246	0	-1960	275	6.28	6.28	12.57	12.57	2	0.12	0.00	0.03	0.00	0.00	24.0
16	266	-1853	135	187	0	-1968	225	6.28	6.28	12.57	12.57	2	0.12	0.00	0.02	0.00	0.00	24.0
17	266	-2008	136	246	0	-1961	224	6.28	6.28	12.57	12.57	2	0.12	0.00	0.03	0.00	0.00	24.0
18	266	-5989	573	682	0	-5914	710	6.28	6.28	12.57	12.57	3	0.23	0.01	0.07	0.00	0.00	24.0
19	266	-4771	-51	535	0	-4998	38	6.28	6.28	12.57	12.57	3	0.19	0.01	0.06	0.00	0.00	24.0
20	266	-5035	255	-1384	0	-8232	362	6.28	6.28	12.57	12.57	3	0.31	0.02	0.15	0.00	0.00	24.0
37	266	-5497	769	624	0	-5278	924	6.28	6.28	12.57	12.57	3	0.21	0.01	0.07	0.00	0.00	24.0
38	266	-3467	-272	379	0	-3750	-194	6.28	6.28	12.57	12.57	3	0.14	0.01	0.04	0.00	0.00	24.0
39	266	-3907	238	-2819	0	-9141	346	6.28	6.28	12.57	12.57	3	0.35	0.05	0.31	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	354	-1830	206	282	0	-2802	508	6.28	6.28	12.57	12.57	3	0.11	0.00	0.03	0.00	0.00	24.0
2	354	-1410	236	208	0	-2146	545	6.28	6.28	12.57	12.57	2	0.14	0.00	0.02	0.00	0.00	24.0
3	354	-1457	237	225	0	-2160	545	6.28	6.28	12.57	12.57	2	0.14	0.00	0.03	0.00	0.00	24.0
4	354	-1358	81	208	0	-2151	237	6.28	6.28	12.57	12.57	2	0.13	0.00	0.02	0.00	0.00	24.0
5	354	-1404	81	226	0	-2165	237	6.28	6.28	12.57	12.57	2	0.13	0.00	0.03	0.00	0.00	24.0
6	354	-1338	182	187	0	-2132	437	6.28	6.28	12.57	12.57	2	0.13	0.00	0.02	0.00	0.00	24.0
7	354	-1493	183	246	0	-2178	437	6.28	6.28	12.57	12.57	2	0.14	0.00	0.03	0.00	0.00	24.0
8	354	-1322	135	187	0	-2134	344	6.28	6.28	12.57	12.57	2	0.13	0.00	0.02	0.00	0.00	24.0
9	354	-1477	136	246	0	-2179	344	6.28	6.28	12.57	12.57	2	0.13	0.00	0.03	0.00	0.00	24.0
10	354	-1410	236	208	0	-2146	545	6.28	6.28	12.57	12.57	2	0.14	0.00	0.02	0.00	0.00	24.0
11	354	-1457	237	225	0	-2160	545	6.28	6.28	12.57	12.57	2	0.14	0.00	0.03	0.00	0.00	24.0
12	354	-1358	81	208	0	-2151	237	6.28	6.28	12.57	12.57	2	0.13	0.00	0.02	0.00	0.00	24.0
13	354	-1404	81	226	0	-2165	237	6.28	6.28	12.57	12.57	2	0.13	0.00	0.03	0.00	0.00	24.0
14	354	-1338	182	187	0	-2132	437	6.28	6.28	12.57	12.57	2	0.13	0.00	0.02	0.00	0.00	24.0
15	354	-1493	183	246	0	-2178	437	6.28	6.28	12.57	12.57	2	0.14	0.00	0.03	0.00	0.00	24.0
16	354	-1322	135	187	0	-2134	344	6.28	6.28	12.57	12.57	2	0.13	0.00	0.02	0.00	0.00	24.0
17	354	-1477	136	246	0	-2179	344	6.28	6.28	12.57	12.57	2	0.13	0.00	0.03	0.00	0.00	24.0
18	354	-5299	573	682	0	-6518	1217	6.28	6.28	12.57	12.57	3	0.26	0.01	0.07	0.00	0.00	24.0
19	354	-4081	-51	535	0	-5471	-7	6.28	6.28	12.57	12.57	3	0.21	0.01	0.06	0.00	0.00	24.0
20	354	-4345	255	-1870	0	-6792	588	6.28	6.28	12.57	12.57	3	0.26	0.03	0.20	0.00	0.00	24.0
37	354	-4807	769	624	0	-5831	1605	6.28	6.28	12.57	12.57	3	0.24	0.01	0.07	0.00	0.00	24.0
38	354	-2777	-272	379	0	-4086	-434	6.28	6.28	12.57	12.57	3	0.16	0.01	0.04	0.00	0.00	24.0
39	354	-3217	238	-3629	0	-6288	556	6.28	6.28	12.57	12.57	3	0.24	0.06	0.40	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 43 NI 39 NF 44 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 22D
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-5496	-911	533	0	-959	593	6.28	6.28	12.57	12.57	3	0.05	0.02	0.08	0.00	0.00	24.0
2	0	-4192	-677	407	0	-700	393	6.28	6.28	12.57	12.57	2	0.05	0.01	0.06	0.00	0.00	24.0
3	0	-4223	-675	440	0	-641	391	6.28	6.28	12.57	12.57	2	0.05	0.01	0.06	0.00	0.00	24.0
4	0	-4233	-727	380	0	-835	521	6.28	6.28	12.57	12.57	2	0.07	0.01	0.07	0.00	0.00	24.0
5	0	-4263	-726	414	0	-776	519	6.28	6.28	12.57	12.57	2	0.06	0.01	0.07	0.00	0.00	24.0
6	0	-4171	-696	359	0	-816	441	6.28	6.28	12.57	12.57	2	0.06	0.01	0.06	0.00	0.00	24.0
7	0	-4272	-691	470	0	-619	433	6.28	6.28	12.57	12.57	2	0.05	0.01	0.06	0.00	0.00	24.0
8	0	-4183	-712	351	0	-857	479	6.28	6.28	12.57	12.57	2	0.06	0.01	0.06	0.00	0.00	24.0
9	0	-4284	-706	462	0	-660	472	6.28	6.28	12.57	12.57	2	0.05	0.01	0.06	0.00	0.00	24.0
10	0	-4192	-677	407	0	-700	393	6.28	6.28	12.57	12.57	2	0.05	0.01	0.06	0.00	0.00	24.0
11	0	-4223	-675	440	0	-641	391	6.28	6.28	12.57	12.57	2	0.05	0.01	0.06	0.00	0.00	24.0
12	0	-4233	-727	380	0	-835	521	6.28	6.28	12.57	12.57	2	0.07	0.01	0.07	0.00	0.00	24.0
13	0	-4263	-726	414	0	-776	519	6.28	6.28	12.57	12.57	2	0.06	0.01	0.07	0.00	0.00	24.0
14	0	-4171	-696	359	0	-816	441	6.28	6.28	12.57	12.57	2	0.06	0.01	0.06	0.00	0.00	24.0
15	0	-4272	-691	470	0	-619	433	6.28	6.28	12.57	12.57	2	0.05	0.01	0.06	0.00	0.00	24.0
16	0	-4183	-712	351	0	-857	479	6.28	6.28	12.57	12.57	2	0.06	0.01	0.06	0.00	0.00	24.0
17	0	-4284	-706	462	0	-660	472	6.28	6.28	12.57	12.57	2	0.05	0.01	0.06	0.00	0.00	24.0
18	0	-7809	-693	1074	0	-1781	130	6.28	6.28	12.57	12.57	3	0.07	0.02	0.11	0.00	0.00	24.0
19	0	-8832	-944	1135	0	-2750	727	6.28	6.28	12.57	12.57	3	0.11	0.02	0.11	0.00	0.00	24.0
20	0	-7916	-851	-3	0	-6808	470	6.28	6.28	12.57	12.57	3	0.25	0.02	0.07	0.00	0.00	24.0
37	0	-6591	-647	869	0	-1036	-8	6.28	6.28	12.57	12.57	3	0.04	0.02	0.09	0.00	0.00	24.0
38	0	-8296	-1064	969	0	-2652	985	6.28	6.28	12.57	12.57	3	0.11	0.02	0.10	0.00	0.00	24.0
39	0	-6769	-911	-926	0	-9415	558	6.28	6.28	12.57	12.57	3	0.35	0.02	0.10	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	53	-5084	-911	533	0	-1242	111	6.28	6.28	12.57	12.57	3	0.05	0.02	0.08	0.00	0.00	24.0
2	53	-3875	-677	407	0	-915	35	6.28	6.28	12.57	12.57	2	0.05	0.01	0.06	0.00	0.00	24.0
3	53	-3906	-675	440	0	-873	34	6.28	6.28	12.57	12.57	2	0.05	0.01	0.06	0.00	0.00	24.0
4	53	-3916	-727	380	0	-1037	137	6.28	6.28	12.57	12.57	2	0.06	0.01	0.07	0.00	0.00	24.0
5	53	-3946	-726	414	0	-995	136	6.28	6.28	12.57	12.57	2	0.06	0.01	0.07	0.00	0.00	24.0
6	53	-3854	-696	359	0	-1006	73	6.28	6.28	12.57	12.57	2	0.06	0.01	0.06	0.00	0.00	24.0
7	53	-3955	-691	470	0	-868	68	6.28	6.28	12.57	12.57	2	0.05	0.01	0.06	0.00	0.00	24.0
8	53	-3866	-712	351	0	-1042	103	6.28	6.28	12.57	12.57	2	0.06	0.01	0.06	0.00	0.00	24.0
9	53	-3967	-706	462	0	-904	99	6.28	6.28	12.57	12.57	2	0.05	0.01	0.06	0.00	0.00	24.0
10	53	-3875	-677	407	0	-915	35	6.28	6.28	12.57	12.57	2	0.05	0.01	0.06	0.00	0.00	24.0
11	53	-3906	-675	440	0	-873	34	6.28	6.28	12.57	12.57	2	0.05	0.01	0.06	0.00	0.00	24.0
12	53	-3916	-727	380	0	-1037	137	6.28	6.28	12.57	12.57	2	0.06	0.01	0.07	0.00	0.00	24.0
13	53	-3946	-726	414	0	-995	136	6.28	6.28	12.57	12.57	2	0.06	0.01	0.07	0.00	0.00	24.0
14	53	-3854	-696	359	0	-1006	73	6.28	6.28	12.57	12.57	2	0.06	0.01	0.06	0.00	0.00	24.0
15	53	-3955	-691	470	0	-868	68	6.28	6.28	12.57	12.57	2	0.05	0.01	0.06	0.00	0.00	24.0
16	53	-3866	-712	351	0	-1042	103	6.28	6.28	12.57	12.57	2	0.06	0.01	0.06	0.00	0.00	24.0
17	53	-3967	-706	462	0	-904	99	6.28	6.28	12.57	12.57	2	0.05	0.01	0.06	0.00	0.00	24.0
18	53	-7396	-693	1074	0	-2349	-236	6.28	6.28	12.57	12.57	3	0.09	0.02	0.11	0.00	0.00	24.0
19	53	-8420	-944	1135	0	-3350	228	6.28	6.28	12.57	12.57	3	0.12	0.02	0.12	0.00	0.00	24.0
20	53	-7504	-851	-293	0	-6730	20	6.28	6.28	12.57	12.57	3	0.25	0.02	0.07	0.00	0.00	24.0
37	53	-6178	-647	869	0	-1495	-350	6.28	6.28	12.57	12.57	3	0.06	0.02	0.09	0.00	0.00	24.0

38	53	-7884	-1064	969	0	-3164	422	6.28	6.28	12.57	12.57	3	0.12	0.02	0.10	0.00	0.00	24.0
39	53	-6356	-911	-1410	0	-8797	76	6.28	6.28	12.57	12.57	3	0.33	0.02	0.15	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	106	-4671	-911	533	0	-1524	-371	6.28	6.28	12.57	12.57	3	0.06	0.02	0.08	0.00	0.00	24.0
2	106	-3558	-677	407	0	-1130	-322	6.28	6.28	12.57	12.57	2	0.07	0.01	0.06	0.00	0.00	24.0
3	106	-3588	-675	440	0	-1106	-323	6.28	6.28	12.57	12.57	2	0.07	0.01	0.06	0.00	0.00	24.0
4	106	-3598	-727	380	0	-1238	-248	6.28	6.28	12.57	12.57	2	0.08	0.01	0.07	0.00	0.00	24.0
5	106	-3628	-726	414	0	-1214	-248	6.28	6.28	12.57	12.57	2	0.07	0.01	0.07	0.00	0.00	24.0
6	106	-3536	-696	359	0	-1195	-296	6.28	6.28	12.57	12.57	2	0.08	0.01	0.06	0.00	0.00	24.0
7	106	-3638	-691	470	0	-1116	-297	6.28	6.28	12.57	12.57	2	0.07	0.01	0.06	0.00	0.00	24.0
8	106	-3548	-712	351	0	-1228	-273	6.28	6.28	12.57	12.57	2	0.08	0.01	0.06	0.00	0.00	24.0
9	106	-3650	-706	462	0	-1149	-275	6.28	6.28	12.57	12.57	2	0.07	0.01	0.06	0.00	0.00	24.0
10	106	-3558	-677	407	0	-1130	-322	6.28	6.28	12.57	12.57	2	0.07	0.01	0.06	0.00	0.00	24.0
11	106	-3588	-675	440	0	-1106	-323	6.28	6.28	12.57	12.57	2	0.07	0.01	0.06	0.00	0.00	24.0
12	106	-3598	-727	380	0	-1238	-248	6.28	6.28	12.57	12.57	2	0.08	0.01	0.07	0.00	0.00	24.0
13	106	-3628	-726	414	0	-1214	-248	6.28	6.28	12.57	12.57	2	0.07	0.01	0.07	0.00	0.00	24.0
14	106	-3536	-696	359	0	-1195	-296	6.28	6.28	12.57	12.57	2	0.08	0.01	0.06	0.00	0.00	24.0
15	106	-3638	-691	470	0	-1116	-297	6.28	6.28	12.57	12.57	2	0.07	0.01	0.06	0.00	0.00	24.0
16	106	-3548	-712	351	0	-1228	-273	6.28	6.28	12.57	12.57	2	0.08	0.01	0.06	0.00	0.00	24.0
17	106	-3650	-706	462	0	-1149	-275	6.28	6.28	12.57	12.57	2	0.07	0.01	0.06	0.00	0.00	24.0
18	106	-6984	-693	1074	0	-2917	-603	6.28	6.28	12.57	12.57	3	0.12	0.02	0.11	0.00	0.00	24.0
19	106	-8008	-944	1135	0	-3950	-271	6.28	6.28	12.57	12.57	3	0.15	0.02	0.12	0.00	0.00	24.0
20	106	-7091	-851	-583	0	-6499	-430	6.28	6.28	12.57	12.57	3	0.24	0.02	0.07	0.00	0.00	24.0
37	106	-5766	-647	869	0	-1954	-693	6.28	6.28	12.57	12.57	3	0.08	0.02	0.09	0.00	0.00	24.0
38	106	-7471	-1064	969	0	-3676	-140	6.28	6.28	12.57	12.57	3	0.14	0.02	0.10	0.00	0.00	24.0
39	106	-5944	-911	-1894	0	-7924	-405	6.28	6.28	12.57	12.57	3	0.30	0.03	0.20	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	159	-4259	-911	533	0	-1806	-853	6.28	6.28	12.57	12.57	3	0.08	0.02	0.08	0.00	0.00	24.0
2	159	-3240	-677	407	0	-1345	-680	6.28	6.28	12.57	12.57	2	0.10	0.01	0.06	0.00	0.00	24.0
3	159	-3271	-675	440	0	-1339	-680	6.28	6.28	12.57	12.57	2	0.10	0.01	0.06	0.00	0.00	24.0
4	159	-3281	-727	380	0	-1439	-632	6.28	6.28	12.57	12.57	2	0.10	0.01	0.07	0.00	0.00	24.0
5	159	-3311	-726	414	0	-1433	-631	6.28	6.28	12.57	12.57	2	0.10	0.01	0.07	0.00	0.00	24.0
6	159	-3219	-696	359	0	-1385	-664	6.28	6.28	12.57	12.57	2	0.10	0.01	0.06	0.00	0.00	24.0
7	159	-3320	-691	470	0	-1365	-663	6.28	6.28	12.57	12.57	2	0.10	0.01	0.06	0.00	0.00	24.0
8	159	-3231	-712	351	0	-1413	-650	6.28	6.28	12.57	12.57	2	0.10	0.01	0.06	0.00	0.00	24.0
9	159	-3332	-706	462	0	-1393	-648	6.28	6.28	12.57	12.57	2	0.10	0.01	0.06	0.00	0.00	24.0
10	159	-3240	-677	407	0	-1345	-680	6.28	6.28	12.57	12.57	2	0.10	0.01	0.06	0.00	0.00	24.0
11	159	-3271	-675	440	0	-1339	-680	6.28	6.28	12.57	12.57	2	0.10	0.01	0.06	0.00	0.00	24.0
12	159	-3281	-727	380	0	-1439	-632	6.28	6.28	12.57	12.57	2	0.10	0.01	0.07	0.00	0.00	24.0
13	159	-3311	-726	414	0	-1433	-631	6.28	6.28	12.57	12.57	2	0.10	0.01	0.07	0.00	0.00	24.0
14	159	-3219	-696	359	0	-1385	-664	6.28	6.28	12.57	12.57	2	0.10	0.01	0.06	0.00	0.00	24.0
15	159	-3320	-691	470	0	-1365	-663	6.28	6.28	12.57	12.57	2	0.10	0.01	0.06	0.00	0.00	24.0
16	159	-3231	-712	351	0	-1413	-650	6.28	6.28	12.57	12.57	2	0.10	0.01	0.06	0.00	0.00	24.0
17	159	-3332	-706	462	0	-1393	-648	6.28	6.28	12.57	12.57	2	0.10	0.01	0.06	0.00	0.00	24.0
18	159	-6572	-693	1074	0	-3485	-969	6.28	6.28	12.57	12.57	3	0.14	0.02	0.11	0.00	0.00	24.0
19	159	-7595	-944	1135	0	-4550	-770	6.28	6.28	12.57	12.57	3	0.18	0.02	0.12	0.00	0.00	24.0
20	159	-6678	-851	-874	0	-6114	-880	6.28	6.28	12.57	12.57	3	0.24	0.02	0.09	0.00	0.00	24.0
37	159	-5354	-647	869	0	-2414	-1035	6.28	6.28	12.57	12.57	3	0.11	0.02	0.09	0.00	0.00	24.0
38	159	-7059	-1064	969	0	-4189	-703	6.28	6.28	12.57	12.57	3	0.16	0.02	0.10	0.00	0.00	24.0
39	159	-5532	-911	-2378	0	-6794	-887	6.28	6.28	12.57	12.57	3	0.26	0.04	0.25	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	211	-3846	-911	533	0	-2088	-1335	6.28	6.28	12.57	12.57	3	0.11	0.02	0.08	0.00	0.00	24.0
2	211	-2923	-677	407	0	-1560	-1038	6.28	6.28	12.57	12.57	2	0.13	0.01	0.06	0.00	0.00	24.0
3	211	-2954	-675	440	0	-1572	-1037	6.28	6.28	12.57	12.57	2	0.13	0.01	0.06	0.00	0.00	24.0
4	211	-2964	-727	380	0	-1640	-1017	6.28	6.28	12.57	12.57	2	0.13	0.01	0.07	0.00	0.00	24.0
5	211	-2994	-726	414	0	-1652	-1015	6.28	6.28	12.57	12.57	2	0.13	0.01	0.07	0.00	0.00	24.0
6	211	-2902	-696	359	0	-1575	-1032	6.28	6.28	12.57	12.57	2	0.13	0.01	0.06	0.00	0.00	24.0
7	211	-3003	-691	470	0	-1613	-1028	6.28	6.28	12.57	12.57	2	0.13	0.01	0.06	0.00	0.00	24.0
8	211	-2914	-712	351	0	-1599	-1026	6.28	6.28	12.57	12.57	2	0.13	0.01	0.07	0.00	0.00	24.0
9	211	-3015	-706	462	0	-1637	-1021	6.28	6.28	12.57	12.57	2	0.13	0.01	0.06	0.00	0.00	24.0
10	211	-2923	-677	407	0	-1560	-1038	6.28	6.28	12.57	12.57	2	0.13	0.01	0.06	0.00	0.00	24.0
11	211	-2954	-675	440	0	-1572	-1037	6.28	6.28	12.57	12.57	2	0.13	0.01	0.06	0.00	0.00	24.0
12	211	-2964	-727	380	0	-1640	-1017	6.28	6.28	12.57	12.57	2	0.13	0.01	0.07	0.00	0.00	24.0
13	211	-2994	-726	414	0	-1652	-1015	6.28	6.28	12.57	12.57	2	0.13	0.01	0.07	0.00	0.00	24.0
14	211	-2902	-696	359	0	-1575	-1032	6.28	6.28	12.57	12.57	2	0.13	0.01	0.06	0.00	0.00	24.0
15	211	-3003	-691	470	0	-1613	-1028	6.28	6.28	12.57	12.57	2	0.13	0.01	0.06	0.00	0.00	24.0
16	211	-2914	-712	351	0	-1599	-1026	6.28	6.28	12.57	12.57	2	0.13	0.01	0.07	0.00	0.00	24.0
17	211	-3015	-706	462	0	-1637	-1021	6.28	6.28	12.57	12.57	2	0.13	0.01	0.06	0.00	0.00	24.0
18	211	-6159	-693	1074	0	-4053	-1336	6.28	6.28	12.57	12.57	3	0.17	0.02	0.11	0.00	0.00	24.0
19	211	-7183	-944	1135	0	-5150	-1269	6.28	6.28	12.57	12.57	3	0.21	0.02	0.12	0.00	0.00	24.0
20	211	-6266	-851	-1164	0	-5575	-1330	6.28	6.28	12.57	12.57	3	0.23	0.02	0.12	0.00	0.00	24.0
37	211	-4941	-647	869	0	-2873	-1377	6.28	6.28	12.57	12.57	3	0.13	0.02	0.09	0.00	0.00	24.0
38	211	-6646	-1064	969	0	-4701	-1266	6.28	6.28	12.57	12.57	3	0.19	0.02	0.10	0.00	0.00	24.0
39	211	-5119	-911	-2862	0	-5409	-1368	6.28	6.28	12.57	12.57	3	0.22	0.05	0.31	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 44 NI 295 NF 261 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 10E
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-4122	-314	-385	0	-1084	884	6.28	6.28	12.57	12.57	3	0.06	0.01	0.04	0.00	0.00	24.0
2	0	-3219	-200	-347	0	-978	564	6.28	6.28	12.57	12.57	2	0.08	0.01	0.04	0.00	0.00	24.0
3	0	-3210	-193	-226	0	-638	543	6.28	6.28	12.57	12.57	2	0.06	0.00	0.02	0.00	0.00	24.0
4	0	-3131	-290	-366	0	-1029	816	6.28	6.28	12.57	12.57	2	0.09	0.01	0.04	0.00	0.00	24.0
5	0	-3123	-282	-245	0	-689	795	6.28	6.28	12.57	12.57	2	0.07	0.01	0.03	0.00	0.00	24.0
6	0	-3198	-240	-495	0	-1393	677	6.28	6.28	12.57	12.57	2	0.10	0.01	0.05	0.00	0.00	24.0
7	0	-3169	-216	-92	0	-259	607	6.28	6.28	12.57	12.57	2	0.05	0.00	0.02	0.00	0.00	24.0
8	0	-3172	-267	-500	0	-1408	752	6.28	6.28	12.57	12.57	2	0.11	0.01	0.05	0.00	0.00	24.0
9	0	-3143	-242	-97	0	-274	682	6.28	6.28	12.57	12.57	2	0.05	0.00	0.02	0.00	0.00	24.0
10	0	-3219	-200	-347	0	-978	564	6.28	6.28	12.57	12.57	2	0.08	0.01	0.04	0.00	0.00	24.0
11	0	-3210	-193	-226	0	-638	543	6.28	6.28	12.57	12.57	2	0.06	0.00	0.02	0.00	0.00	24.0
12	0	-3131	-290	-366	0	-1029	816	6.28	6.28	12.57	12.57	2	0.09	0.01	0.04	0.00	0.00	24.0
13	0	-3123	-282	-245	0	-689	795	6.28	6.28	12.57	12.57	2	0.07	0.01	0.03	0.00	0.00	24.0
14	0	-3198	-240	-495	0	-1393	677	6.28	6.28	12.57	12.57	2	0.10	0.01	0.05	0.00	0.00	24.0
15	0	-3169	-216	-92	0	-259	607	6.28	6.28	12.57	12.57	2	0.05	0.00	0.02	0.00	0.00	24.0
16	0	-3172	-267	-500	0	-1408	752	6.28	6.28	12.57	12.57	2	0.11	0.01	0.05	0.00	0.00	24.0
17	0	-3143	-242	-97	0	-274	682	6.28	6.28	12.57	12.57	2	0.05	0.00	0.02	0.00	0.00	24.0

18	0	-6568	-511	-831	0	-2340	1439	6.28	6.28	12.57	12.57	3	0.12	0.01	0.09	0.00	0.00	24.0
19	0	-4957	-613	-732	0	-2061	1726	6.28	6.28	12.57	12.57	3	0.12	0.01	0.08	0.00	0.00	24.0
20	0	-5368	-516	-511	0	-571	1452	6.28	6.28	12.57	12.57	3	0.09	0.01	0.05	0.00	0.00	24.0
37	0	-6691	-390	-735	0	-2071	1095	6.28	6.28	12.57	12.57	3	0.10	0.01	0.08	0.00	0.00	24.0
38	0	-4005	-559	-571	0	-1607	1573	6.28	6.28	12.57	12.57	3	0.10	0.01	0.06	0.00	0.00	24.0
39	0	-4690	-397	-202	0	876	1117	6.28	6.28	12.57	12.57	3	0.07	0.01	0.04	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	58	-3671	-314	-385	0	-861	702	6.28	6.28	12.57	12.57	3	0.05	0.01	0.04	0.00	0.00	24.0
2	58	-2872	-200	-347	0	-777	448	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
3	58	-2863	-193	-226	0	-507	432	6.28	6.28	12.57	12.57	2	0.05	0.00	0.02	0.00	0.00	24.0
4	58	-2784	-290	-366	0	-818	648	6.28	6.28	12.57	12.57	2	0.07	0.01	0.04	0.00	0.00	24.0
5	58	-2776	-282	-245	0	-548	632	6.28	6.28	12.57	12.57	2	0.06	0.01	0.03	0.00	0.00	24.0
6	58	-2851	-240	-495	0	-1107	538	6.28	6.28	12.57	12.57	2	0.08	0.01	0.05	0.00	0.00	24.0
7	58	-2822	-216	-92	0	-206	482	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
8	58	-2825	-267	-500	0	-1119	598	6.28	6.28	12.57	12.57	2	0.08	0.01	0.06	0.00	0.00	24.0
9	58	-2796	-242	-97	0	-218	542	6.28	6.28	12.57	12.57	2	0.04	0.00	0.03	0.00	0.00	24.0
10	58	-2872	-200	-347	0	-777	448	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
11	58	-2863	-193	-226	0	-507	432	6.28	6.28	12.57	12.57	2	0.05	0.00	0.02	0.00	0.00	24.0
12	58	-2784	-290	-366	0	-818	648	6.28	6.28	12.57	12.57	2	0.07	0.01	0.04	0.00	0.00	24.0
13	58	-2776	-282	-245	0	-548	632	6.28	6.28	12.57	12.57	2	0.06	0.01	0.03	0.00	0.00	24.0
14	58	-2851	-240	-495	0	-1107	538	6.28	6.28	12.57	12.57	2	0.08	0.01	0.05	0.00	0.00	24.0
15	58	-2822	-216	-92	0	-206	482	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
16	58	-2825	-267	-500	0	-1119	598	6.28	6.28	12.57	12.57	2	0.08	0.01	0.06	0.00	0.00	24.0
17	58	-2796	-242	-97	0	-218	542	6.28	6.28	12.57	12.57	2	0.04	0.00	0.03	0.00	0.00	24.0
18	58	-6117	-511	-831	0	-1859	1143	6.28	6.28	12.57	12.57	3	0.09	0.01	0.09	0.00	0.00	24.0
19	58	-4506	-613	-732	0	-1638	1371	6.28	6.28	12.57	12.57	3	0.09	0.01	0.08	0.00	0.00	24.0
20	58	-4917	-516	-357	0	-321	1154	6.28	6.28	12.57	12.57	3	0.07	0.01	0.05	0.00	0.00	24.0
37	58	-6240	-390	-735	0	-1646	870	6.28	6.28	12.57	12.57	3	0.08	0.01	0.08	0.00	0.00	24.0
38	58	-3554	-559	-571	0	-1277	1250	6.28	6.28	12.57	12.57	3	0.08	0.01	0.06	0.00	0.00	24.0
39	58	-4239	-397	54	0	918	887	6.28	6.28	12.57	12.57	3	0.06	0.01	0.04	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	116	-3220	-314	-385	0	-639	520	6.28	6.28	12.57	12.57	3	0.04	0.01	0.04	0.00	0.00	24.0
2	116	-2525	-200	-347	0	-576	332	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
3	116	-2516	-193	-226	0	-376	320	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
4	116	-2437	-290	-366	0	-606	481	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
5	116	-2429	-282	-245	0	-406	468	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
6	116	-2504	-240	-495	0	-821	399	6.28	6.28	12.57	12.57	2	0.06	0.01	0.05	0.00	0.00	24.0
7	116	-2476	-216	-92	0	-152	357	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
8	116	-2478	-267	-500	0	-830	443	6.28	6.28	12.57	12.57	2	0.06	0.01	0.06	0.00	0.00	24.0
9	116	-2449	-242	-97	0	-162	402	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
10	116	-2525	-200	-347	0	-576	332	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
11	116	-2516	-193	-226	0	-376	320	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
12	116	-2437	-290	-366	0	-606	481	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
13	116	-2429	-282	-245	0	-406	468	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
14	116	-2504	-240	-495	0	-821	399	6.28	6.28	12.57	12.57	2	0.06	0.01	0.05	0.00	0.00	24.0
15	116	-2476	-216	-92	0	-152	357	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
16	116	-2478	-267	-500	0	-830	443	6.28	6.28	12.57	12.57	2	0.06	0.01	0.06	0.00	0.00	24.0
17	116	-2449	-242	-97	0	-162	402	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
18	116	-5666	-511	-831	0	-1379	847	6.28	6.28	12.57	12.57	3	0.07	0.01	0.09	0.00	0.00	24.0
19	116	-4054	-613	-732	0	-1214	1017	6.28	6.28	12.57	12.57	3	0.07	0.01	0.08	0.00	0.00	24.0
20	116	-4466	-516	-226	0	-154	855	6.28	6.28	12.57	12.57	3	0.05	0.01	0.05	0.00	0.00	24.0
37	116	-5789	-390	-735	0	-1220	645	6.28	6.28	12.57	12.57	3	0.06	0.01	0.08	0.00	0.00	24.0
38	116	-3103	-559	-571	0	-947	927	6.28	6.28	12.57	12.57	3	0.06	0.01	0.06	0.00	0.00	24.0
39	116	-3788	-397	273	0	821	658	6.28	6.28	12.57	12.57	3	0.05	0.01	0.04	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	173	-2769	-314	-385	0	-416	339	6.28	6.28	12.57	12.57	3	0.02	0.01	0.04	0.00	0.00	24.0
2	173	-2178	-200	-347	0	-375	216	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
3	173	-2169	-193	-226	0	-245	208	6.28	6.28	12.57	12.57	2	0.02	0.00	0.03	0.00	0.00	24.0
4	173	-2090	-290	-366	0	-395	313	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
5	173	-2082	-282	-245	0	-265	305	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
6	173	-2157	-240	-495	0	-535	260	6.28	6.28	12.57	12.57	2	0.04	0.01	0.06	0.00	0.00	24.0
7	173	-2129	-216	-92	0	-99	233	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
8	173	-2131	-267	-500	0	-541	289	6.28	6.28	12.57	12.57	2	0.04	0.01	0.06	0.00	0.00	24.0
9	173	-2102	-242	-97	0	-105	262	6.28	6.28	12.57	12.57	2	0.02	0.00	0.03	0.00	0.00	24.0
10	173	-2178	-200	-347	0	-375	216	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
11	173	-2169	-193	-226	0	-245	208	6.28	6.28	12.57	12.57	2	0.02	0.00	0.03	0.00	0.00	24.0
12	173	-2090	-290	-366	0	-395	313	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
13	173	-2082	-282	-245	0	-265	305	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
14	173	-2157	-240	-495	0	-535	260	6.28	6.28	12.57	12.57	2	0.04	0.01	0.06	0.00	0.00	24.0
15	173	-2129	-216	-92	0	-99	233	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
16	173	-2131	-267	-500	0	-541	289	6.28	6.28	12.57	12.57	2	0.04	0.01	0.06	0.00	0.00	24.0
17	173	-2102	-242	-97	0	-105	262	6.28	6.28	12.57	12.57	2	0.02	0.00	0.03	0.00	0.00	24.0
18	173	-5215	-511	-831	0	-898	552	6.28	6.28	12.57	12.57	3	0.05	0.01	0.09	0.00	0.00	24.0
19	173	-3603	-613	-732	0	-791	662	6.28	6.28	12.57	12.57	3	0.05	0.01	0.08	0.00	0.00	24.0
20	173	-4015	-516	-116	0	-56	557	6.28	6.28	12.57	12.57	3	0.03	0.01	0.05	0.00	0.00	24.0
37	173	-5338	-390	-735	0	-795	420	6.28	6.28	12.57	12.57	3	0.04	0.01	0.08	0.00	0.00	24.0
38	173	-2652	-559	-571	0	-617	604	6.28	6.28	12.57	12.57	3	0.04	0.01	0.06	0.00	0.00	24.0
39	173	-3337	-397	456	0	609	428	6.28	6.28	12.57	12.57	3	0.03	0.01	0.05	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	231	-2318	-314	-385	0	-193	157	6.28	6.28	12.57	12.57	3	0.01	0.01	0.04	0.00	0.00	24.0
2	231	-1831	-200	-347	0	-175	100	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
3	231	-1822	-193	-226	0	-114	97	6.28	6.28	12.57	12.57	2	0.01	0.00	0.03	0.00	0.00	24.0
4	231	-1743	-290	-366	0	-184	146	6.28	6.28	12.57	12.57	2	0.02	0.01	0.04	0.00	0.00	24.0
5	231	-1735	-282	-245	0	-123	142	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
6	231	-1810	-240	-495	0	-249	121	6.28	6.28	12.57	12.57	2	0.02	0.01	0.06	0.00	0.00	24.0
7	231	-1782	-216	-92	0	-46	108	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
8	231	-1784	-267	-500	0	-251	134	6.28	6.28	12.57	12.57	2	0.02	0.01	0.06	0.00	0.00	24.0
9	231	-1755	-242	-97	0	-49	122	6.28	6.28	12.57	12.57	2	0.01	0.00	0.03	0.00	0.00	24.0
10	231	-1831	-200	-347	0	-175	100	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
11	231	-1822	-193	-226	0	-114	97	6.28	6.28	12.57	12.57	2	0.01	0.00	0.03	0.00	0.00	24.0
12	231	-1743	-290	-366	0	-184	146	6.28	6.28	12.57	12.57	2	0.02	0.01	0.04	0.00	0.00	24.0
13	231	-1735	-282	-245	0	-123	142	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
14	231	-1810	-240	-495	0	-249	121	6.28	6.28	12.57	12.57	2	0.02	0.01	0.06	0.00	0.00	24.0
15	231	-1782	-216	-92	0	-46	108	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
16	231	-1784	-267	-500	0	-251	134	6.28	6.28	12.57	12.57	2	0.02	0.01	0.06	0.00	0.00	24.0
17	231	-1755	-242	-97	0	-49	122	6.28	6.28	12.57	12.57	2	0.01	0.00	0.03	0.00	0.00	24.0
18	231	-4764	-511	-831	0	-418	256	6.28	6.28	12.57	12.57	3	0.02	0.01	0.09	0.00	0.00	24.0
19	231	-3152	-613	-732	0	-368	308	6.28	6.28	12.57	12.57	3	0.02	0.01	0.08	0.00	0.00	24.0
20	231	-3564	-516	-29	0	-15	259	6.28	6.28	12.57	12.57	3	0.02	0.01	0.05	0.00	0.00	24.0
37	231	-4887	-390	-735	0	-370	194	6.28	6.28	12.57	12.57	3	0.02	0.01	0.08	0.00	0.00	24.0
38	231	-2201	-559	-571	0	-287	281	6.28	6.28	12.57	12.57	3	0.02	0.01	0.06	0.00	0.00	24.0
39	231	-2886	-397	602	0	301	199	6.28	6.28	12.57	12.57	3	0.02	0.01	0.07	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 45 NI 297 NF 260 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 15D
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-7638	-14	30	0	122	56	6.28	6.28	12.57	12.57	3	0.01	0.00	0.00	0.00	0.00	24.0
2	0	-5550	-33	-22	0	-91	134	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
3	0	-5460	-31	67	0	271	127	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
4	0	-6290	10	-20	0	-83	-40	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
5	0	-6201	12	69	0	279	-47	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
6	0	-5913	-20	-126	0	-510	80	6.28	6.28	12.57	12.57	2	0.03	0.00	0.01	0.00	0.00	24.0
7	0	-5615	-14	172	0	696	58	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
8	0	-6136	-7	-125	0	-508	28	6.28	6.28	12.57	12.57	2	0.03	0.00	0.01	0.00	0.00	24.0
9	0	-5837	-1	173	0	698	6	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
10	0	-5550	-33	-22	0	-91	134	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
11	0	-5460	-31	67	0	271	127	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
12	0	-6290	10	-20	0	-83	-40	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
13	0	-6201	12	69	0	279	-47	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
14	0	-5913	-20	-126	0	-510	80	6.28	6.28	12.57	12.57	2	0.03	0.00	0.01	0.00	0.00	24.0
15	0	-5615	-14	172	0	696	58	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
16	0	-6136	-7	-125	0	-508	28	6.28	6.28	12.57	12.57	2	0.03	0.00	0.01	0.00	0.00	24.0
17	0	-5837	-1	173	0	698	6	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
18	0	-12110	-102	31	0	126	414	6.28	6.28	12.57	12.57	3	0.02	0.00	0.01	0.00	0.00	24.0
19	0	-12370	34	62	0	248	-136	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
20	0	-11310	-30	21	0	1921	122	6.28	6.28	12.57	12.57	3	0.07	0.00	0.00	0.00	0.00	24.0
37	0	-10530	-140	16	0	64	564	6.28	6.28	12.57	12.57	3	0.03	0.00	0.01	0.00	0.00	24.0
38	0	-10960	87	66	0	268	-352	6.28	6.28	12.57	12.57	3	0.02	0.00	0.01	0.00	0.00	24.0
39	0	-9203	-19	-1	0	3056	78	6.28	6.28	12.57	12.57	3	0.11	0.00	0.00	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	88	-6948	-14	30	0	95	44	6.28	6.28	12.57	12.57	3	0.00	0.00	0.00	0.00	0.00	24.0
2	88	-5019	-33	-22	0	-71	104	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
3	88	-4929	-31	67	0	212	99	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
4	88	-5759	10	-20	0	-65	-32	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
5	88	-5670	12	69	0	218	-37	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
6	88	-5382	-20	-126	0	-399	63	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
7	88	-5084	-14	172	0	544	45	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
8	88	-5605	-7	-125	0	-397	22	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
9	88	-5306	-1	173	0	545	4	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
10	88	-5019	-33	-22	0	-71	104	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
11	88	-4929	-31	67	0	212	99	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
12	88	-5759	10	-20	0	-65	-32	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
13	88	-5670	12	69	0	218	-37	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
14	88	-5382	-20	-126	0	-399	63	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
15	88	-5084	-14	172	0	544	45	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
16	88	-5605	-7	-125	0	-397	22	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
17	88	-5306	-1	173	0	545	4	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
18	88	-11418	-102	31	0	98	323	6.28	6.28	12.57	12.57	3	0.02	0.00	0.01	0.00	0.00	24.0
19	88	-11678	34	62	0	193	-106	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
20	88	-10620	-30	256	0	1796	95	6.28	6.28	12.57	12.57	3	0.07	0.00	0.03	0.00	0.00	24.0
37	88	-9838	-140	16	0	50	441	6.28	6.28	12.57	12.57	3	0.02	0.00	0.01	0.00	0.00	24.0
38	88	-10269	87	66	0	209	-275	6.28	6.28	12.57	12.57	3	0.02	0.00	0.01	0.00	0.00	24.0
39	88	-8512	-19	391	0	2879	61	6.28	6.28	12.57	12.57	3	0.11	0.01	0.04	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	177	-6258	-14	30	0	68	32	6.28	6.28	12.57	12.57	3	0.00	0.00	0.00	0.00	0.00	24.0
2	177	-4488	-33	-22	0	-51	75	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
3	177	-4398	-31	67	0	152	71	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
4	177	-5228	10	-20	0	-47	-23	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
5	177	-5139	12	69	0	157	-26	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
6	177	-4851	-20	-126	0	-287	45	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
7	177	-4553	-14	172	0	391	33	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
8	177	-5074	-7	-125	0	-286	16	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
9	177	-4775	-1	173	0	392	3	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
10	177	-4488	-33	-22	0	-51	75	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
11	177	-4398	-31	67	0	152	71	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
12	177	-5228	10	-20	0	-47	-23	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
13	177	-5139	12	69	0	157	-26	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
14	177	-4851	-20	-126	0	-287	45	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
15	177	-4553	-14	172	0	391	33	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
16	177	-5074	-7	-125	0	-286	16	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
17	177	-4775	-1	173	0	392	3	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
18	177	-10727	-102	31	0	70	233	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
19	177	-10987	34	62	0	139	-76	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
20	177	-9930	-30	458	0	1477	69	6.28	6.28	12.57	12.57	3	0.05	0.01	0.05	0.00	0.00	24.0
37	177	-9147	-140	16	0	36	317	6.28	6.28	12.57	12.57	3	0.02	0.00	0.01	0.00	0.00	24.0
38	177	-9578	87	66	0	150	-197	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
39	177	-7822	-19	727	0	2380	44	6.28	6.28	12.57	12.57	3	0.09	0.01	0.07	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	266	-5567	-14	30	0	42	19	6.28	6.28	12.57	12.57	3	0.00	0.00	0.00	0.00	0.00	24.0
2	266	-3957	-33	-22	0	-32	46	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
3	266	-3867	-31	67	0	93	43	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
4	266	-4697	10	-20	0	-29	-14	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
5	266	-4608	12	69	0	95	-16	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
6	266	-4320	-20	-126	0	-176	28	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
7	266	-4022	-14	172	0	239	20	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
8	266	-4543	-7	-125	0	-175	10	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
9	266	-4244	-1	173	0	240	2	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
10	266	-3957	-33	-22	0	-32	46	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
11	266	-3867	-31	67	0	93	43	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
12	266	-4697	10	-20	0	-29	-14	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
13	266	-4608	12	69	0	95	-16	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
14	266	-4320	-20	-126	0	-176	28	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
15	266	-4022	-14	172	0	239	20	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
16	266	-4543	-7	-125	0	-175	10	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
17	266	-4244	-1	173	0	240	2	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
18	266	-10036	-102	31	0	42	142	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
19	266	-10296	34	62	0	84	-46	6.28	6.28	12.57	12.57	3	0.00	0.00	0.01	0.00	0.00	24.0

20	266	-9241	-30	625	0	995	42	6.28	6.28	12.57	12.57	3	0.04	0.01	0.06	0.00	0.00	24.0
37	266	-8456	-140	16	0	21	193	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
38	266	-8888	87	66	0	91	-120	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
39	266	-7132	-19	1006	0	1609	27	6.28	6.28	12.57	12.57	3	0.06	0.02	0.10	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	354	-4877	-14	30	0	15	7	6.28	6.28	12.57	12.57	3	0.00	0.00	0.00	0.00	0.00	24.0
2	354	-3426	-33	-22	0	-12	16	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
3	354	-3336	-31	67	0	33	16	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
4	354	-4166	10	-20	0	-11	-5	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
5	354	-4077	12	69	0	34	-6	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
6	354	-3789	-20	-126	0	-64	10	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
7	354	-3491	-14	172	0	86	7	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
8	354	-4012	-7	-125	0	-64	4	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
9	354	-3713	-1	173	0	87	1	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
10	354	-3426	-33	-22	0	-12	16	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
11	354	-3336	-31	67	0	33	16	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
12	354	-4166	10	-20	0	-11	-5	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
13	354	-4077	12	69	0	34	-6	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
14	354	-3789	-20	-126	0	-64	10	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
15	354	-3491	-14	172	0	86	7	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
16	354	-4012	-7	-125	0	-64	4	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
17	354	-3713	-1	173	0	87	1	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
18	354	-9344	-102	31	0	14	51	6.28	6.28	12.57	12.57	3	0.00	0.00	0.01	0.00	0.00	24.0
19	354	-9604	34	62	0	30	-16	6.28	6.28	12.57	12.57	3	0.00	0.00	0.01	0.00	0.00	24.0
20	354	-8551	-30	759	0	380	15	6.28	6.28	12.57	12.57	3	0.01	0.01	0.08	0.00	0.00	24.0
37	354	-7764	-140	16	0	7	70	6.28	6.28	12.57	12.57	3	0.00	0.00	0.01	0.00	0.00	24.0
38	354	-8197	87	66	0	32	-43	6.28	6.28	12.57	12.57	3	0.00	0.00	0.01	0.00	0.00	24.0
39	354	-6441	-19	1229	0	616	10	6.28	6.28	12.57	12.57	3	0.02	0.02	0.13	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 46 NI 271 NF 259 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 20D
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-5349	179	-438	0	-1146	-468	6.28	6.28	12.57	12.57	3	0.05	0.01	0.05	0.00	0.00	24.0
2	0	-4026	144	-416	0	-1090	-377	6.28	6.28	12.57	12.57	2	0.07	0.01	0.05	0.00	0.00	24.0
3	0	-3996	142	-273	0	-715	-372	6.28	6.28	12.57	12.57	2	0.05	0.00	0.03	0.00	0.00	24.0
4	0	-4233	134	-400	0	-1048	-349	6.28	6.28	12.57	12.57	2	0.07	0.01	0.04	0.00	0.00	24.0
5	0	-4204	131	-257	0	-673	-344	6.28	6.28	12.57	12.57	2	0.05	0.00	0.03	0.00	0.00	24.0
6	0	-4133	143	-578	0	-1512	-374	6.28	6.28	12.57	12.57	2	0.09	0.01	0.06	0.00	0.00	24.0
7	0	-4035	136	-100	0	-263	-356	6.28	6.28	12.57	12.57	2	0.03	0.00	0.01	0.00	0.00	24.0
8	0	-4195	140	-573	0	-1499	-365	6.28	6.28	12.57	12.57	2	0.09	0.01	0.06	0.00	0.00	24.0
9	0	-4097	133	-96	0	-250	-347	6.28	6.28	12.57	12.57	2	0.03	0.00	0.01	0.00	0.00	24.0
10	0	-4026	144	-416	0	-1090	-377	6.28	6.28	12.57	12.57	2	0.07	0.01	0.05	0.00	0.00	24.0
11	0	-3996	142	-273	0	-715	-372	6.28	6.28	12.57	12.57	2	0.05	0.00	0.03	0.00	0.00	24.0
12	0	-4233	134	-400	0	-1048	-349	6.28	6.28	12.57	12.57	2	0.07	0.01	0.04	0.00	0.00	24.0
13	0	-4204	131	-257	0	-673	-344	6.28	6.28	12.57	12.57	2	0.05	0.00	0.03	0.00	0.00	24.0
14	0	-4133	143	-578	0	-1512	-374	6.28	6.28	12.57	12.57	2	0.09	0.01	0.06	0.00	0.00	24.0
15	0	-4035	136	-100	0	-263	-356	6.28	6.28	12.57	12.57	2	0.03	0.00	0.01	0.00	0.00	24.0
16	0	-4195	140	-573	0	-1499	-365	6.28	6.28	12.57	12.57	2	0.09	0.01	0.06	0.00	0.00	24.0
17	0	-4097	133	-96	0	-250	-347	6.28	6.28	12.57	12.57	2	0.03	0.00	0.01	0.00	0.00	24.0
18	0	-7388	312	-938	0	-2456	-816	6.28	6.28	12.57	12.57	3	0.10	0.02	0.10	0.00	0.00	24.0
19	0	-8868	335	-864	0	-2261	-875	6.28	6.28	12.57	12.57	3	0.10	0.02	0.09	0.00	0.00	24.0
20	0	-7573	298	-553	0	-704	-780	6.28	6.28	12.57	12.57	3	0.05	0.01	0.06	0.00	0.00	24.0
37	0	-6034	256	-813	0	-2127	-670	6.28	6.28	12.57	12.57	3	0.09	0.01	0.09	0.00	0.00	24.0
38	0	-8501	294	-688	0	-1802	-768	6.28	6.28	12.57	12.57	3	0.08	0.01	0.07	0.00	0.00	24.0
39	0	-6342	233	-171	0	794	-610	6.28	6.28	12.57	12.57	3	0.04	0.00	0.02	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	53	-4937	179	-438	0	-914	-374	6.28	6.28	12.57	12.57	3	0.04	0.01	0.05	0.00	0.00	24.0
2	53	-3709	144	-416	0	-870	-301	6.28	6.28	12.57	12.57	2	0.06	0.01	0.05	0.00	0.00	24.0
3	53	-3679	142	-273	0	-570	-297	6.28	6.28	12.57	12.57	2	0.04	0.00	0.03	0.00	0.00	24.0
4	53	-3916	134	-400	0	-836	-278	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
5	53	-3887	131	-257	0	-537	-274	6.28	6.28	12.57	12.57	2	0.04	0.00	0.03	0.00	0.00	24.0
6	53	-3816	143	-578	0	-1207	-298	6.28	6.28	12.57	12.57	2	0.08	0.01	0.06	0.00	0.00	24.0
7	53	-3718	136	-100	0	-210	-284	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
8	53	-3878	140	-573	0	-1196	-291	6.28	6.28	12.57	12.57	2	0.07	0.01	0.06	0.00	0.00	24.0
9	53	-3780	133	-96	0	-200	-277	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
10	53	-3709	144	-416	0	-870	-301	6.28	6.28	12.57	12.57	2	0.06	0.01	0.05	0.00	0.00	24.0
11	53	-3679	142	-273	0	-570	-297	6.28	6.28	12.57	12.57	2	0.04	0.00	0.03	0.00	0.00	24.0
12	53	-3916	134	-400	0	-836	-278	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
13	53	-3887	131	-257	0	-537	-274	6.28	6.28	12.57	12.57	2	0.04	0.00	0.03	0.00	0.00	24.0
14	53	-3816	143	-578	0	-1207	-298	6.28	6.28	12.57	12.57	2	0.08	0.01	0.06	0.00	0.00	24.0
15	53	-3718	136	-100	0	-210	-284	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
16	53	-3878	140	-573	0	-1196	-291	6.28	6.28	12.57	12.57	2	0.07	0.01	0.06	0.00	0.00	24.0
17	53	-3780	133	-96	0	-200	-277	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
18	53	-6976	312	-938	0	-1960	-651	6.28	6.28	12.57	12.57	3	0.08	0.02	0.10	0.00	0.00	24.0
19	53	-8456	335	-864	0	-1804	-698	6.28	6.28	12.57	12.57	3	0.08	0.02	0.09	0.00	0.00	24.0
20	53	-7160	298	-413	0	-449	-622	6.28	6.28	12.57	12.57	3	0.04	0.01	0.04	0.00	0.00	24.0
37	53	-5622	256	-813	0	-1697	-534	6.28	6.28	12.57	12.57	3	0.07	0.01	0.09	0.00	0.00	24.0
38	53	-8088	294	-688	0	-1438	-613	6.28	6.28	12.57	12.57	3	0.06	0.01	0.07	0.00	0.00	24.0
39	53	-5930	233	64	0	820	-487	6.28	6.28	12.57	12.57	3	0.04	0.00	0.02	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	106	-4524	179	-438	0	-683	-279	6.28	6.28	12.57	12.57	3	0.03	0.01	0.05	0.00	0.00	24.0
2	106	-3392	144	-416	0	-650	-225	6.28	6.28	12.57	12.57	2	0.04	0.01	0.05	0.00	0.00	24.0
3	106	-3362	142	-273	0	-426	-221	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
4	106	-3598	134	-400	0	-625	-208	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
5	106	-3570	131	-257	0	-401	-205	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
6	106	-3498	143	-578	0	-901	-223	6.28	6.28	12.57	12.57	2	0.06	0.01	0.06	0.00	0.00	24.0
7	106	-3400	136	-100	0	-157	-212	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
8	106	-3560	140	-573	0	-894	-217	6.28	6.28	12.57	12.57	2	0.06	0.01	0.06	0.00	0.00	24.0
9	106	-3462	133	-96	0	-149	-207	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
10	106	-3392	144	-416	0	-650	-225	6.28	6.28	12.57	12.57	2	0.04	0.01	0.05	0.00	0.00	24.0
11	106	-3362	142	-273	0	-426	-221	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
12	106	-3598	134	-400	0	-625	-208	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
13	106	-3570	131	-257	0	-401	-205	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
14	106	-3498	143	-578	0	-901	-223	6.28	6.28	12.57	12.57	2	0.06	0.01	0.06	0.00	0.00	24.0
15	106	-3400	136	-100	0	-157	-212	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0

16	106	-3560	140	-573	0	-894	-217	6.28	6.28	12.57	12.57	2	0.06	0.01	0.06	0.00	0.00	24.0
17	106	-3462	133	-96	0	-149	-207	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
18	106	-6564	312	-938	0	-1464	-486	6.28	6.28	12.57	12.57	3	0.06	0.02	0.10	0.00	0.00	24.0
19	106	-8044	335	-864	0	-1348	-521	6.28	6.28	12.57	12.57	3	0.06	0.02	0.09	0.00	0.00	24.0
20	106	-6748	298	-292	0	-264	-465	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
37	106	-5209	256	-813	0	-1268	-399	6.28	6.28	12.57	12.57	3	0.05	0.01	0.09	0.00	0.00	24.0
38	106	-7676	294	-688	0	-1074	-457	6.28	6.28	12.57	12.57	3	0.05	0.01	0.07	0.00	0.00	24.0
39	106	-5517	233	264	0	732	-363	6.28	6.28	12.57	12.57	3	0.03	0.00	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	159	-4112	179	-438	0	-451	-184	6.28	6.28	12.57	12.57	3	0.02	0.01	0.05	0.00	0.00	24.0
2	159	-3074	144	-416	0	-429	-148	6.28	6.28	12.57	12.57	2	0.03	0.01	0.05	0.00	0.00	24.0
3	159	-3044	142	-273	0	-282	-146	6.28	6.28	12.57	12.57	2	0.02	0.00	0.03	0.00	0.00	24.0
4	159	-3281	134	-400	0	-413	-137	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
5	159	-3252	131	-257	0	-265	-135	6.28	6.28	12.57	12.57	2	0.02	0.00	0.03	0.00	0.00	24.0
6	159	-3181	143	-578	0	-596	-147	6.28	6.28	12.57	12.57	2	0.04	0.01	0.06	0.00	0.00	24.0
7	159	-3083	136	-100	0	-103	-140	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
8	159	-3243	140	-573	0	-591	-144	6.28	6.28	12.57	12.57	2	0.04	0.01	0.06	0.00	0.00	24.0
9	159	-3145	133	-96	0	-99	-137	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
10	159	-3074	144	-416	0	-429	-148	6.28	6.28	12.57	12.57	2	0.03	0.01	0.05	0.00	0.00	24.0
11	159	-3044	142	-273	0	-282	-146	6.28	6.28	12.57	12.57	2	0.02	0.00	0.03	0.00	0.00	24.0
12	159	-3281	134	-400	0	-413	-137	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
13	159	-3252	131	-257	0	-265	-135	6.28	6.28	12.57	12.57	2	0.02	0.00	0.03	0.00	0.00	24.0
14	159	-3181	143	-578	0	-596	-147	6.28	6.28	12.57	12.57	2	0.04	0.01	0.06	0.00	0.00	24.0
15	159	-3083	136	-100	0	-103	-140	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
16	159	-3243	140	-573	0	-591	-144	6.28	6.28	12.57	12.57	2	0.04	0.01	0.06	0.00	0.00	24.0
17	159	-3145	133	-96	0	-99	-137	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
18	159	-6151	312	-938	0	-968	-321	6.28	6.28	12.57	12.57	3	0.04	0.02	0.10	0.00	0.00	24.0
19	159	-7631	335	-864	0	-891	-344	6.28	6.28	12.57	12.57	3	0.04	0.02	0.09	0.00	0.00	24.0
20	159	-6336	298	-192	0	-137	-307	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
37	159	-4797	256	-813	0	-838	-264	6.28	6.28	12.57	12.57	3	0.04	0.01	0.09	0.00	0.00	24.0
38	159	-7264	294	-688	0	-710	-302	6.28	6.28	12.57	12.57	3	0.03	0.01	0.07	0.00	0.00	24.0
39	159	-5105	233	431	0	547	-240	6.28	6.28	12.57	12.57	3	0.02	0.01	0.05	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	211	-3700	179	-438	0	-220	-90	6.28	6.28	12.57	12.57	3	0.01	0.01	0.05	0.00	0.00	24.0
2	211	-2757	144	-416	0	-209	-72	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
3	211	-2727	142	-273	0	-137	-71	6.28	6.28	12.57	12.57	2	0.01	0.00	0.03	0.00	0.00	24.0
4	211	-2964	134	-400	0	-201	-67	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
5	211	-2935	131	-257	0	-129	-66	6.28	6.28	12.57	12.57	2	0.01	0.00	0.03	0.00	0.00	24.0
6	211	-2864	143	-578	0	-290	-72	6.28	6.28	12.57	12.57	2	0.02	0.01	0.06	0.00	0.00	24.0
7	211	-2766	136	-100	0	-50	-68	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
8	211	-2926	140	-573	0	-288	-70	6.28	6.28	12.57	12.57	2	0.02	0.01	0.06	0.00	0.00	24.0
9	211	-2828	133	-96	0	-48	-66	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
10	211	-2757	144	-416	0	-209	-72	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
11	211	-2727	142	-273	0	-137	-71	6.28	6.28	12.57	12.57	2	0.01	0.00	0.03	0.00	0.00	24.0
12	211	-2964	134	-400	0	-201	-67	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
13	211	-2935	131	-257	0	-129	-66	6.28	6.28	12.57	12.57	2	0.01	0.00	0.03	0.00	0.00	24.0
14	211	-2864	143	-578	0	-290	-72	6.28	6.28	12.57	12.57	2	0.02	0.01	0.06	0.00	0.00	24.0
15	211	-2766	136	-100	0	-50	-68	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
16	211	-2926	140	-573	0	-288	-70	6.28	6.28	12.57	12.57	2	0.02	0.01	0.06	0.00	0.00	24.0
17	211	-2828	133	-96	0	-48	-66	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
18	211	-5739	312	-938	0	-472	-157	6.28	6.28	12.57	12.57	3	0.02	0.02	0.10	0.00	0.00	24.0
19	211	-7219	335	-864	0	-434	-167	6.28	6.28	12.57	12.57	3	0.02	0.02	0.09	0.00	0.00	24.0
20	211	-5923	298	-112	0	-57	-149	6.28	6.28	12.57	12.57	3	0.01	0.01	0.03	0.00	0.00	24.0
37	211	-4384	256	-813	0	-408	-129	6.28	6.28	12.57	12.57	3	0.02	0.01	0.09	0.00	0.00	24.0
38	211	-6851	294	-688	0	-346	-146	6.28	6.28	12.57	12.57	3	0.02	0.01	0.07	0.00	0.00	24.0
39	211	-4692	233	564	0	283	-117	6.28	6.28	12.57	12.57	3	0.01	0.01	0.06	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 47 NI 129 NF 124 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 9B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
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	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm

1	0	-12030	-19	-76	0	-138	-50	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
2	0	-9293	57	-128	0	-238	-295	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
3	0	-9227	56	-37	0	-68	-291	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
4	0	-9287	-86	-80	0	-143	214	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
5	0	-9222	-87	11	0	26	218	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
6	0	-9367	9	-216	0	-403	-121	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
7	0	-9149	5	85	0	163	-108	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
8	0	-9366	-34	-202	0	-374	31	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
9	0	-9147	-38	100	0	191	44	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
10	0	-9293	57	-128	0	-238	-295	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
11	0	-9227	56	-37	0	-68	-291	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
12	0	-9287	-86	-80	0	-143	214	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
13	0	-9222	-87	11	0	26	218	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
14	0	-9367	9	-216	0	-403	-121	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
15	0	-9149	5	85	0	163	-108	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
16	0	-9366	-34	-202	0	-374	31	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
17	0	-9147	-38	100	0	191	44	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
18	0	-13110	167	-346	0	-635	-731	6.28	6.28	12.57	12.57	3	0.04	0.01	0.03	0.00	0.00	24.0
19	0	-12980	-266	-55	0	-77	804	6.28	6.28	12.57	12.57	3	0.04	0.00	0.02	0.00	0.00	24.0
20	0	-12940	-47	-316	0	-618	30	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
37	0	-12680	321	-408	0	-757	-1271	6.28	6.28	12.57	12.57	3	0.07	0.01	0.04	0.00	0.00	24.0
38	0	-12470	-400	79	0	172	1287	6.28	6.28	12.57	12.57	3	0.07	0.01	0.04	0.00	0.00	24.0
39	0	-12390	-36	-356	0	-729	-3	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	97	-11270	-19	-76	0	-64	-69	6.28	6.28	12.57	12.57	3	0.00	0.00	0.01	0.00	0.00	24.0
2	97	-8708	57	-128	0	-113	-239	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
3	97	-8642	56	-37	0	-32	-236	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
4	97	-8702	-86	-80	0	-66	131	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
5	97	-8637	-87	11	0	16	133	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
6	97	-8782	9	-216	0	-192	-113	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
7	97	-8564	5	85	0	80	-103	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
8	97	-8781	-34	-202	0	-177	-2	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
9	97	-8562	-38	100	0	94	8	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
10	97	-8708	57	-128	0	-113	-239	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
11	97	-8642	56	-37	0	-32	-236	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0

12	97	-8702	-86	-80	0	-66	131	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
13	97	-8637	-87	11	0	16	133	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
14	97	-8782	9	-216	0	-192	-113	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
15	97	-8564	5	85	0	80	-103	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
16	97	-8781	-34	-202	0	-177	-2	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
17	97	-8562	-38	100	0	94	8	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
18	97	-12350	167	-346	0	-297	-568	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
19	97	-12220	-266	-55	0	-24	545	6.28	6.28	12.57	12.57	3	0.03	0.00	0.02	0.00	0.00	24.0
20	97	-12178	-47	-316	0	-311	-16	6.28	6.28	12.57	12.57	3	0.01	0.01	0.03	0.00	0.00	24.0
37	97	-11920	321	-408	0	-359	-958	6.28	6.28	12.57	12.57	3	0.05	0.01	0.04	0.00	0.00	24.0
38	97	-11708	-400	79	0	96	897	6.28	6.28	12.57	12.57	3	0.05	0.01	0.04	0.00	0.00	24.0
39	97	-11630	-36	-356	0	-382	-38	6.28	6.28	12.57	12.57	3	0.01	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	195	-10511	-19	-76	0	10	-87	6.28	6.28	12.57	12.57	3	0.00	0.00	0.01	0.00	0.00	24.0
2	195	-8123	57	-128	0	11	-183	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
3	195	-8057	56	-37	0	4	-181	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
4	195	-8117	-86	-80	0	12	47	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
5	195	-8052	-87	11	0	5	49	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
6	195	-8197	9	-216	0	19	-105	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
7	195	-7979	5	85	0	-4	-98	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
8	195	-8196	-34	-202	0	20	-36	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
9	195	-7977	-38	100	0	-3	-29	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
10	195	-8123	57	-128	0	11	-183	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
11	195	-8057	56	-37	0	4	-181	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
12	195	-8117	-86	-80	0	12	47	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
13	195	-8052	-87	11	0	5	49	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
14	195	-8197	9	-216	0	19	-105	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
15	195	-7979	5	85	0	-4	-98	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
16	195	-8196	-34	-202	0	20	-36	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
17	195	-7977	-38	100	0	-3	-29	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
18	195	-11590	167	-346	0	41	-405	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
19	195	-11460	-266	-55	0	29	286	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
20	195	-11417	-47	-316	0	-3	-62	6.28	6.28	12.57	12.57	3	0.00	0.01	0.03	0.00	0.00	24.0
37	195	-11159	321	-408	0	38	-645	6.28	6.28	12.57	12.57	3	0.04	0.01	0.04	0.00	0.00	24.0
38	195	-10947	-400	79	0	19	508	6.28	6.28	12.57	12.57	3	0.03	0.01	0.04	0.00	0.00	24.0
39	195	-10869	-36	-356	0	-35	-73	6.28	6.28	12.57	12.57	3	0.00	0.01	0.04	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	292	-9752	-19	-76	0	84	-106	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
2	292	-7538	57	-128	0	136	-127	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
3	292	-7472	56	-37	0	40	-126	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
4	292	-7532	-86	-80	0	89	-36	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
5	292	-7467	-87	11	0	-6	-35	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
6	292	-7612	9	-216	0	230	-96	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
7	292	-7394	5	85	0	-87	-94	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
8	292	-7611	-34	-202	0	217	-69	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
9	292	-7392	-38	100	0	-101	-66	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
10	292	-7538	57	-128	0	136	-127	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
11	292	-7472	56	-37	0	40	-126	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
12	292	-7532	-86	-80	0	89	-36	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
13	292	-7467	-87	11	0	-6	-35	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
14	292	-7612	9	-216	0	230	-96	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
15	292	-7394	5	85	0	-87	-94	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
16	292	-7611	-34	-202	0	217	-69	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
17	292	-7392	-38	100	0	-101	-66	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
18	292	-10830	167	-346	0	379	-242	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
19	292	-10699	-266	-55	0	82	27	6.28	6.28	12.57	12.57	3	0.00	0.00	0.02	0.00	0.00	24.0
20	292	-10656	-47	-316	0	305	-108	6.28	6.28	12.57	12.57	3	0.01	0.01	0.03	0.00	0.00	24.0
37	292	-10398	321	-408	0	436	-331	6.28	6.28	12.57	12.57	3	0.02	0.01	0.04	0.00	0.00	24.0
38	292	-10186	-400	79	0	-58	118	6.28	6.28	12.57	12.57	3	0.01	0.01	0.04	0.00	0.00	24.0
39	292	-10108	-36	-356	0	313	-108	6.28	6.28	12.57	12.57	3	0.01	0.01	0.04	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	390	-8992	-19	-76	0	158	-124	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
2	390	-6953	57	-128	0	260	-71	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
3	390	-6887	56	-37	0	77	-71	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
4	390	-6947	-86	-80	0	167	-120	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
5	390	-6882	-87	11	0	-17	-120	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
6	390	-7027	9	-216	0	442	-88	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
7	390	-6809	5	85	0	-170	-89	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
8	390	-7026	-34	-202	0	414	-102	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
9	390	-6807	-38	100	0	-198	-103	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
10	390	-6953	57	-128	0	260	-71	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
11	390	-6887	56	-37	0	77	-71	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
12	390	-6947	-86	-80	0	167	-120	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
13	390	-6882	-87	11	0	-17	-120	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
14	390	-7027	9	-216	0	442	-88	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
15	390	-6809	5	85	0	-170	-89	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
16	390	-7026	-34	-202	0	414	-102	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
17	390	-6807	-38	100	0	-198	-103	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
18	390	-10070	167	-346	0	716	-79	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
19	390	-9939	-266	-55	0	136	-231	6.28	6.28	12.57	12.57	3	0.01	0.00	0.03	0.00	0.00	24.0
20	390	-9894	-47	-316	0	612	-154	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
37	390	-9638	321	-408	0	833	-18	6.28	6.28	12.57	12.57	3	0.03	0.01	0.04	0.00	0.00	24.0
38	390	-9424	-400	79	0	-135	-272	6.28	6.28	12.57	12.57	3	0.02	0.01	0.04	0.00	0.00	24.0
39	390	-9348	-36	-356	0	660	-143	6.28	6.28	12.57	12.57	3	0.03	0.01	0.04	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

VERIFICA NODO IN TESTA AL PILASTRO, NODO NUM. 124 NON CONFINATO

(par.7.2.2 NTC2018 "La domanda di resistenza valutata con i criteri della progettazione in capacità può essere assunta non superiore alla domanda di resistenza valutata per il caso di comportamento strutturale non dissipativo.")

PROGETTAZIONE IN CAPACITA'

Asse loc. pilastro y nodo: --

Asse loc. pilastro z nodo INTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 40.0 cm, hjc= 50.0 cm

FxMin,inf	FxMin,sup	FxMax,sup	FySup	FzSup	Vjbdy	Vjbdz	Vres,y	Vres,z	I.R.compr.	Ashy	Ashz	PASSO	Nota
daN					daN		daN			cmq		cm	
-6807	1	-0	0	0	--	35233	--	175015	0.20	--	4.08	13.08	

VERIFICA DI RESISTENZA CON SOLLECITAZIONI COMPORTAMENTO NON DISSIPATIVO

Asse loc. pilastro z nodo INTERNO: Hjw= 40.0 cm, bj= 40.0 cm, hjc= 50.0 cm, db1= 45.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb,1	Mb,2	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-0	-6953	-2489	-2229	0	642	175015	0.00	0.00	40.00	
3	-0	-6887	-2358	-2281	0	190	175015	0.00	0.00	40.00	
4	-0	-6947	-2441	-2274	0	412	175015	0.00	0.00	40.00	
5	-0	-6882	-2309	-2326	0	42	175015	0.00	0.00	40.00	
6	-0	-7027	-2626	-2185	0	1089	175015	0.01	0.00	40.00	
7	-0	-6809	-2187	-2357	0	420	175015	0.00	0.00	40.00	
8	-0	-7026	-2612	-2198	0	1022	175015	0.01	0.00	40.00	
9	-0	-6807	-2173	-2371	0	489	175015	0.00	0.00	40.00	
10	-0	-6953	-2489	-2229	0	642	175015	0.00	0.00	40.00	
11	-0	-6887	-2358	-2281	0	190	175015	0.00	0.00	40.00	
12	-0	-6947	-2441	-2274	0	412	175015	0.00	0.00	40.00	
13	-0	-6882	-2309	-2326	0	42	175015	0.00	0.00	40.00	
14	-0	-7027	-2626	-2185	0	1089	175015	0.01	0.00	40.00	
15	-0	-6809	-2187	-2357	0	420	175015	0.00	0.00	40.00	
16	-0	-7026	-2612	-2198	0	1022	175015	0.01	0.00	40.00	
17	-0	-6807	-2173	-2371	0	489	175015	0.00	0.00	40.00	

CONFRONTO E SINTESI CONCLUSIVE (si assume in ogni caso passo <= 15 cm)

I.R.compr.	Ashy	Ashz	PASSO	Nota
	cmq		cm	
0.01	--	--	15.00	**VERIFICATO**

ASTA NUM. 48 NI 128 NF 125 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 14B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-19220	18	-360	0	-636	-21	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
2	0	-14820	92	-308	0	-534	-231	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
3	0	-14740	91	-237	0	-431	-230	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
4	0	-14840	-63	-318	0	-548	197	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
5	0	-14750	-63	-246	0	-445	199	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
6	0	-14920	38	-395	0	-660	-83	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
7	0	-14650	36	-156	0	-316	-78	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
8	0	-14920	-8	-398	0	-663	45	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
9	0	-14660	-10	-159	0	-320	51	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
10	0	-14820	92	-308	0	-534	-231	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
11	0	-14740	91	-237	0	-431	-230	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
12	0	-14840	-63	-318	0	-548	197	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
13	0	-14750	-63	-246	0	-445	199	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
14	0	-14920	38	-395	0	-660	-83	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
15	0	-14650	36	-156	0	-316	-78	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
16	0	-14920	-8	-398	0	-663	45	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
17	0	-14660	-10	-159	0	-320	51	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
18	0	-21140	242	-666	0	-1097	-628	6.28	6.28	12.57	12.57	3	0.05	0.01	0.06	0.00	0.00	24.0
19	0	-21090	-241	-612	0	-1019	677	6.28	6.28	12.57	12.57	3	0.05	0.01	0.05	0.00	0.00	24.0
20	0	-21000	5	-799	0	-1345	13	6.28	6.28	12.57	12.57	3	0.05	0.01	0.07	0.00	0.00	24.0
37	0	-20260	409	-595	0	-987	-1079	6.28	6.28	12.57	12.57	3	0.06	0.01	0.05	0.00	0.00	24.0
38	0	-20180	-396	-506	0	-857	1098	6.28	6.28	12.57	12.57	3	0.06	0.01	0.04	0.00	0.00	24.0
39	0	-20030	14	-817	0	-1399	-9	6.28	6.28	12.57	12.57	3	0.05	0.01	0.07	0.00	0.00	24.0
apost= --		aant= --		ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0														
1	97	-18460	18	-360	0	-285	-3	6.28	6.28	12.57	12.57	3	0.01	0.01	0.03	0.00	0.00	24.0
2	97	-14235	92	-308	0	-234	-142	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
3	97	-14155	91	-237	0	-200	-141	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
4	97	-14255	-63	-318	0	-238	136	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
5	97	-14165	-63	-246	0	-205	137	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
6	97	-14335	38	-395	0	-274	-46	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
7	97	-14065	36	-156	0	-163	-42	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
8	97	-14335	-8	-398	0	-275	38	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
9	97	-14075	-10	-159	0	-164	41	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
10	97	-14235	92	-308	0	-234	-142	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
11	97	-14155	91	-237	0	-200	-141	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
12	97	-14255	-63	-318	0	-238	136	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
13	97	-14165	-63	-246	0	-205	137	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
14	97	-14335	38	-395	0	-274	-46	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
15	97	-14065	36	-156	0	-163	-42	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
16	97	-14335	-8	-398	0	-275	38	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
17	97	-14075	-10	-159	0	-164	41	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
18	97	-20378	242	-666	0	-448	-392	6.28	6.28	12.57	12.57	3	0.02	0.01	0.06	0.00	0.00	24.0
19	97	-20330	-241	-612	0	-422	443	6.28	6.28	12.57	12.57	3	0.03	0.01	0.05	0.00	0.00	24.0
20	97	-20240	5	-799	0	-566	18	6.28	6.28	12.57	12.57	3	0.02	0.01	0.07	0.00	0.00	24.0
37	97	-19498	409	-595	0	-406	-680	6.28	6.28	12.57	12.57	3	0.04	0.01	0.05	0.00	0.00	24.0
38	97	-19420	-396	-506	0	-364	712	6.28	6.28	12.57	12.57	3	0.04	0.01	0.04	0.00	0.00	24.0
39	97	-19270	14	-817	0	-602	5	6.28	6.28	12.57	12.57	3	0.02	0.01	0.07	0.00	0.00	24.0
apost= --		aant= --		ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0														
1	195	-17700	18	-360	0	67	15	6.28	6.28	12.57	12.57	3	0.00	0.01	0.03	0.00	0.00	24.0
2	195	-13650	92	-308	0	67	-52	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
3	195	-13570	91	-237	0	30	-52	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
4	195	-13670	-63	-318	0	72	75	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
5	195	-13580	-63	-246	0	35	76	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
6	195	-13750	38	-395	0	112	-8	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
7	195	-13480	36	-156	0	-11	-7	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
8	195	-13750	-8	-398	0	113	30	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
9	195	-13490	-10	-159	0	-9	31	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
10	195	-13650	92	-308	0	67	-52	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
11	195	-13570	91	-237	0	30	-52	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
12	195	-13670	-63	-318	0	72	75	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
13	195	-13580	-63	-246	0	35	76	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
14	195	-13750	38	-395	0	112	-8	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
15	195	-13480	36	-156	0	-11	-7	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0

16	195	-13750	-8	-398	0	113	30	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
17	195	-13490	-10	-159	0	-9	31	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
18	195	-19615	242	-666	0	201	-156	6.28	6.28	12.57	12.57	3	0.01	0.01	0.06	0.00	0.00	24.0
19	195	-19570	-241	-612	0	174	208	6.28	6.28	12.57	12.57	3	0.01	0.01	0.05	0.00	0.00	24.0
20	195	-19480	5	-799	0	213	24	6.28	6.28	12.57	12.57	3	0.01	0.01	0.07	0.00	0.00	24.0
37	195	-18735	409	-595	0	174	-281	6.28	6.28	12.57	12.57	3	0.02	0.01	0.05	0.00	0.00	24.0
38	195	-18660	-396	-506	0	129	326	6.28	6.28	12.57	12.57	3	0.02	0.01	0.04	0.00	0.00	24.0
39	195	-18510	14	-817	0	195	18	6.28	6.28	12.57	12.57	3	0.01	0.01	0.07	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	292	-16940	18	-360	0	418	33	6.28	6.28	12.57	12.57	3	0.01	0.01	0.03	0.00	0.00	24.0
2	292	-13065	92	-308	0	368	37	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
3	292	-12985	91	-237	0	261	37	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
4	292	-13085	-63	-318	0	382	14	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
5	292	-12995	-63	-246	0	275	14	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
6	292	-13165	38	-395	0	497	29	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
7	292	-12895	36	-156	0	142	29	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
8	292	-13165	-8	-398	0	501	22	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
9	292	-12905	-10	-159	0	146	22	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
10	292	-13065	92	-308	0	368	37	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
11	292	-12985	91	-237	0	261	37	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
12	292	-13085	-63	-318	0	382	14	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
13	292	-12995	-63	-246	0	275	14	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
14	292	-13165	38	-395	0	497	29	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
15	292	-12895	36	-156	0	142	29	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
16	292	-13165	-8	-398	0	501	22	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
17	292	-12905	-10	-159	0	146	22	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
18	292	-18852	242	-666	0	851	80	6.28	6.28	12.57	12.57	3	0.03	0.01	0.06	0.00	0.00	24.0
19	292	-18810	-241	-612	0	771	-27	6.28	6.28	12.57	12.57	3	0.03	0.01	0.05	0.00	0.00	24.0
20	292	-18720	5	-799	0	993	29	6.28	6.28	12.57	12.57	3	0.03	0.01	0.07	0.00	0.00	24.0
37	292	-17972	409	-595	0	754	117	6.28	6.28	12.57	12.57	3	0.03	0.01	0.05	0.00	0.00	24.0
38	292	-17900	-396	-506	0	622	-60	6.28	6.28	12.57	12.57	3	0.02	0.01	0.05	0.00	0.00	24.0
39	292	-17750	14	-817	0	991	32	6.28	6.28	12.57	12.57	3	0.03	0.01	0.07	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	390	-16180	18	-360	0	769	51	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
2	390	-12480	92	-308	0	669	126	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
3	390	-12400	91	-237	0	492	126	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
4	390	-12500	-63	-318	0	692	-47	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
5	390	-12410	-63	-246	0	515	-48	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
6	390	-12580	38	-395	0	883	67	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
7	390	-12310	36	-156	0	294	64	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
8	390	-12580	-8	-398	0	890	15	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
9	390	-12320	-10	-159	0	301	12	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
10	390	-12480	92	-308	0	669	126	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
11	390	-12400	91	-237	0	492	126	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
12	390	-12500	-63	-318	0	692	-47	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
13	390	-12410	-63	-246	0	515	-48	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
14	390	-12580	38	-395	0	883	67	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
15	390	-12310	36	-156	0	294	64	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
16	390	-12580	-8	-398	0	890	15	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
17	390	-12320	-10	-159	0	301	12	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
18	390	-18090	242	-666	0	1500	316	6.28	6.28	12.57	12.57	3	0.06	0.01	0.06	0.00	0.00	24.0
19	390	-18050	-241	-612	0	1368	-262	6.28	6.28	12.57	12.57	3	0.05	0.01	0.05	0.00	0.00	24.0
20	390	-17960	5	-799	0	1772	34	6.28	6.28	12.57	12.57	3	0.06	0.01	0.07	0.00	0.00	24.0
37	390	-17210	409	-595	0	1334	516	6.28	6.28	12.57	12.57	3	0.05	0.01	0.05	0.00	0.00	24.0
38	390	-17140	-396	-506	0	1115	-446	6.28	6.28	12.57	12.57	3	0.05	0.01	0.05	0.00	0.00	24.0
39	390	-16990	14	-817	0	1788	46	6.28	6.28	12.57	12.57	3	0.06	0.01	0.07	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

VERIFICA NODO IN TESTA AL PILASTRO, NODO NUM. 125 NON CONFINATO

(par.7.2.2 NTC2018 "La domanda di resistenza valutata con i criteri della progettazione in capacità può essere assunta non superiore alla domanda di resistenza valutata per il caso di comportamento strutturale non dissipativo.")

PROGETTAZIONE IN CAPACITA'

Asse loc. pilastro y nodo: --

Asse loc. pilastro z nodo INTERNO: As2(inf)= 6.03, As1(sup)= 6.03, Hjw= 40.0 cm, bj= 40.0 cm, hjc= 50.0 cm

FxMin,inf	FxMin,sup	FxMax,sup	FySup	FzSup	Vjbdy	Vjbdz	Vres,y	Vres,z	I.R.compr.	Ashy	Ashz	PASSO	Nota
daN					daN		daN			cmq		cm	
-12310	1	-0	0	0	--	52849	--	175015	0.30	--	13.27	3.28	

VERIFICA DI RESISTENZA CON SOLLECITAZIONI COMPORTAMENTO NON DISSIPATIVO

Asse loc. pilastro z nodo INTERNO: Hjw= 40.0 cm, bj= 40.0 cm, hjc= 50.0 cm, db1= 45.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb,1	Mb,2	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-0	-12480	-4325	-3657	0	1649	175015	0.01	0.00	40.00	
3	-0	-12400	-4188	-3696	0	1215	175015	0.01	0.00	40.00	
4	-0	-12500	-4350	-3658	0	1709	175015	0.01	0.00	40.00	
5	-0	-12410	-4213	-3698	0	1272	175015	0.01	0.00	40.00	
6	-0	-12580	-4494	-3611	0	2180	175015	0.01	0.00	40.00	
7	-0	-12310	-4037	-3743	0	726	175015	0.00	0.00	40.00	
8	-0	-12580	-4501	-3612	0	2195	175015	0.01	0.00	40.00	
9	-0	-12320	-4044	-3744	0	741	175015	0.00	0.00	40.00	
10	-0	-12480	-4325	-3657	0	1649	175015	0.01	0.00	40.00	
11	-0	-12400	-4188	-3696	0	1215	175015	0.01	0.00	40.00	
12	-0	-12500	-4350	-3658	0	1709	175015	0.01	0.00	40.00	
13	-0	-12410	-4213	-3698	0	1272	175015	0.01	0.00	40.00	
14	-0	-12580	-4494	-3611	0	2180	175015	0.01	0.00	40.00	
15	-0	-12310	-4037	-3743	0	726	175015	0.00	0.00	40.00	
16	-0	-12580	-4501	-3612	0	2195	175015	0.01	0.00	40.00	
17	-0	-12320	-4044	-3744	0	741	175015	0.00	0.00	40.00	

CONFRONTO E SINTESI CONCLUSIVE (si assume in ogni caso passo <= 15 cm)

I.R.compr.	Ashy	Ashz	PASSO	Nota
	cmq		cm	

0.01 -- -- 15.00 **VERIFICATO**

ASTA NUM. 49 NI 127 NF 126 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 19B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-19010	11	-184	0	-316	-61	6.28	6.28	12.57	12.57	3	0.01	0.00	0.02	0.00	0.00	24.0
2	0	-14660	78	-168	0	-279	-253	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
3	0	-14580	77	-86	0	-159	-251	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
4	0	-14670	-61	-198	0	-327	157	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
5	0	-14590	-62	-116	0	-207	160	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
6	0	-14750	31	-274	0	-436	-113	6.28	6.28	12.57	12.57	2	0.02	0.00	0.03	0.00	0.00	24.0
7	0	-14490	27	0	0	-36	-104	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
8	0	-14760	-11	-284	0	-451	10	6.28	6.28	12.57	12.57	2	0.02	0.00	0.03	0.00	0.00	24.0
9	0	-14490	-14	-9	0	-51	19	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
10	0	-14660	78	-168	0	-279	-253	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
11	0	-14580	77	-86	0	-159	-251	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
12	0	-14670	-61	-198	0	-327	157	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
13	0	-14590	-62	-116	0	-207	160	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
14	0	-14750	31	-274	0	-436	-113	6.28	6.28	12.57	12.57	2	0.02	0.00	0.03	0.00	0.00	24.0
15	0	-14490	27	0	0	-36	-104	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
16	0	-14760	-11	-284	0	-451	10	6.28	6.28	12.57	12.57	2	0.02	0.00	0.03	0.00	0.00	24.0
17	0	-14490	-14	-9	0	-51	19	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
18	0	-20790	228	-254	0	-402	-680	6.28	6.28	12.57	12.57	3	0.04	0.00	0.02	0.00	0.00	24.0
19	0	-20870	-205	-384	0	-605	559	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
20	0	-20680	13	-383	0	-637	-66	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
37	0	-19890	372	-170	0	-276	-1093	6.28	6.28	12.57	12.57	3	0.06	0.01	0.03	0.00	0.00	24.0
38	0	-20030	-350	-385	0	-614	973	6.28	6.28	12.57	12.57	3	0.05	0.01	0.03	0.00	0.00	24.0
39	0	-19710	14	-384	0	-668	-69	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	97	-18250	11	-184	0	-137	-50	6.28	6.28	12.57	12.57	3	0.01	0.00	0.02	0.00	0.00	24.0
2	97	-14075	78	-168	0	-116	-177	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
3	97	-13995	77	-86	0	-76	-175	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
4	97	-14085	-61	-198	0	-134	98	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
5	97	-14005	-62	-116	0	-95	99	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
6	97	-14165	31	-274	0	-169	-83	6.28	6.28	12.57	12.57	2	0.01	0.00	0.03	0.00	0.00	24.0
7	97	-13905	27	0	0	-36	-77	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
8	97	-14175	-11	-284	0	-174	-0	6.28	6.28	12.57	12.57	2	0.01	0.00	0.03	0.00	0.00	24.0
9	97	-13905	-14	-9	0	-42	5	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
10	97	-14075	78	-168	0	-116	-177	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
11	97	-13995	77	-86	0	-76	-175	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
12	97	-14085	-61	-198	0	-134	98	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
13	97	-14005	-62	-116	0	-95	99	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
14	97	-14165	31	-274	0	-169	-83	6.28	6.28	12.57	12.57	2	0.01	0.00	0.03	0.00	0.00	24.0
15	97	-13905	27	0	0	-36	-77	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
16	97	-14175	-11	-284	0	-174	-0	6.28	6.28	12.57	12.57	2	0.01	0.00	0.03	0.00	0.00	24.0
17	97	-13905	-14	-9	0	-42	5	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
18	97	-20030	228	-254	0	-154	-458	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
19	97	-20110	-205	-384	0	-231	359	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
20	97	-19920	13	-383	0	-264	-53	6.28	6.28	12.57	12.57	3	0.01	0.01	0.03	0.00	0.00	24.0
37	97	-19130	372	-170	0	-110	-731	6.28	6.28	12.57	12.57	3	0.04	0.01	0.03	0.00	0.00	24.0
38	97	-19268	-350	-385	0	-238	632	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
39	97	-18948	14	-384	0	-293	-55	6.28	6.28	12.57	12.57	3	0.01	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	195	-17490	11	-184	0	43	-40	6.28	6.28	12.57	12.57	3	0.00	0.00	0.02	0.00	0.00	24.0
2	195	-13490	78	-168	0	48	-100	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
3	195	-13410	77	-86	0	7	-100	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
4	195	-13500	-61	-198	0	59	38	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
5	195	-13420	-62	-116	0	18	39	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
6	195	-13580	31	-274	0	99	-53	6.28	6.28	12.57	12.57	2	0.01	0.00	0.03	0.00	0.00	24.0
7	195	-13320	27	0	0	-36	-50	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
8	195	-13590	-11	-284	0	102	-11	6.28	6.28	12.57	12.57	2	0.01	0.00	0.03	0.00	0.00	24.0
9	195	-13320	-14	-9	0	-33	-9	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
10	195	-13490	78	-168	0	48	-100	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
11	195	-13410	77	-86	0	7	-100	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
12	195	-13500	-61	-198	0	59	38	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
13	195	-13420	-62	-116	0	18	39	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
14	195	-13580	31	-274	0	99	-53	6.28	6.28	12.57	12.57	2	0.01	0.00	0.03	0.00	0.00	24.0
15	195	-13320	27	0	0	-36	-50	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
16	195	-13590	-11	-284	0	102	-11	6.28	6.28	12.57	12.57	2	0.01	0.00	0.03	0.00	0.00	24.0
17	195	-13320	-14	-9	0	-33	-9	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
18	195	-19270	228	-254	0	94	-236	6.28	6.28	12.57	12.57	3	0.01	0.00	0.02	0.00	0.00	24.0
19	195	-19350	-205	-384	0	143	159	6.28	6.28	12.57	12.57	3	0.01	0.01	0.03	0.00	0.00	24.0
20	195	-19160	13	-383	0	109	-40	6.28	6.28	12.57	12.57	3	0.00	0.01	0.03	0.00	0.00	24.0
37	195	-18370	372	-170	0	56	-368	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
38	195	-18505	-350	-385	0	137	291	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
39	195	-18185	14	-384	0	81	-41	6.28	6.28	12.57	12.57	3	0.00	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	292	-16730	11	-184	0	223	-30	6.28	6.28	12.57	12.57	3	0.01	0.00	0.02	0.00	0.00	24.0
2	292	-12905	78	-168	0	212	-24	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
3	292	-12825	77	-86	0	91	-24	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
4	292	-12915	-61	-198	0	252	-21	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
5	292	-12835	-62	-116	0	131	-22	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
6	292	-12995	31	-274	0	367	-23	6.28	6.28	12.57	12.57	2	0.02	0.00	0.03	0.00	0.00	24.0
7	292	-12735	27	0	0	-36	-24	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
8	292	-13005	-11	-284	0	379	-22	6.28	6.28	12.57	12.57	2	0.02	0.00	0.03	0.00	0.00	24.0
9	292	-12735	-14	-9	0	-24	-23	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
10	292	-12905	78	-168	0	212	-24	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
11	292	-12825	77	-86	0	91	-24	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
12	292	-12915	-61	-198	0	252	-21	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
13	292	-12835	-62	-116	0	131	-22	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
14	292	-12995	31	-274	0	367	-23	6.28	6.28	12.57	12.57	2	0.02	0.00	0.03	0.00	0.00	24.0
15	292	-12735	27	0	0	-36	-24	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
16	292	-13005	-11	-284	0	379	-22	6.28	6.28	12.57	12.57	2	0.02	0.00	0.03	0.00	0.00	24.0
17	292	-12735	-14	-9	0	-24	-23	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
18	292	-18510	228	-254	0	342	-14	6.28	6.28	12.57	12.57	3	0.01	0.00	0.02	0.00	0.00	24.0
19	292	-18590	-205	-384	0	517	-41	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0

20	292	-18400	13	-383	0	483	-27	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
37	292	-17610	372	-170	0	221	-6	6.28	6.28	12.57	12.57	3	0.01	0.01	0.03	0.00	0.00	24.0
38	292	-17742	-350	-385	0	513	-50	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
39	292	-17422	14	-384	0	456	-27	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	390	-15970	11	-184	0	402	-19	6.28	6.28	12.57	12.57	3	0.01	0.00	0.02	0.00	0.00	24.0
2	390	-12320	78	-168	0	375	53	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
3	390	-12240	77	-86	0	174	51	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
4	390	-12330	-61	-198	0	445	-81	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
5	390	-12250	-62	-116	0	243	-82	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
6	390	-12410	31	-274	0	634	7	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
7	390	-12150	27	0	0	-36	3	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
8	390	-12420	-11	-284	0	655	-33	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
9	390	-12150	-14	-9	0	-16	-37	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
10	390	-12320	78	-168	0	375	53	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
11	390	-12240	77	-86	0	174	51	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
12	390	-12330	-61	-198	0	445	-81	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
13	390	-12250	-62	-116	0	243	-82	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
14	390	-12410	31	-274	0	634	7	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
15	390	-12150	27	0	0	-36	3	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
16	390	-12420	-11	-284	0	655	-33	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
17	390	-12150	-14	-9	0	-16	-37	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
18	390	-17750	228	-254	0	590	208	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
19	390	-17830	-205	-384	0	891	-240	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
20	390	-17640	13	-383	0	856	-14	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
37	390	-16850	372	-170	0	387	356	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
38	390	-16980	-350	-385	0	888	-391	6.28	6.28	12.57	12.57	3	0.04	0.01	0.03	0.00	0.00	24.0
39	390	-16660	14	-384	0	830	-14	6.28	6.28	12.57	12.57	3	0.03	0.01	0.04	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

VERIFICA NODO IN TESTA AL PILASTRO, NODO NUM. 126 NON CONFINATO

(par.7.2.2 NTC2018 "La domanda di resistenza valutata con i criteri della progettazione in capacità può essere assunta non superiore alla domanda di resistenza valutata per il caso di comportamento strutturale non dissipativo.")

PROGETTAZIONE IN CAPACITA'

Asse loc. pilastro y nodo: --

Asse loc. pilastro z nodo INTERNO: As2(inf)= 6.03, As1(sup)= 6.03, Hjw= 40.0 cm, bj= 40.0 cm, hjc= 50.0 cm

FxMin,inf	FxMin,sup	FxMax,sup	FySup	FzSup	Vjbdy	Vjbdz	Vres,y	Vres,z	I.R.compr.	Ashy	Ashz	PASSO	Nota
daN					daN		daN			cmq		cm	
-12150	1	-0	0	0	--	52849	--	175015	0.30	--	13.27	3.28	

VERIFICA DI RESISTENZA CON SOLLECITAZIONI COMPORTAMENTO NON DISSIPATIVO

Asse loc. pilastro z nodo INTERNO: Hjw= 40.0 cm, bj= 40.0 cm, hjc= 50.0 cm, db1= 45.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb,1	Mb,2	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m			daN			cmq	cm	
2	-0	-12320	-4058	-3682	0	928	175015	0.01	0.00	40.00	
3	-0	-12240	-3909	-3735	0	430	175015	0.00	0.00	40.00	
4	-0	-12330	-4108	-3663	0	1099	175015	0.01	0.00	40.00	
5	-0	-12250	-3959	-3716	0	600	175015	0.00	0.00	40.00	
6	-0	-12410	-4249	-3614	0	1568	175015	0.01	0.00	40.00	
7	-0	-12150	-3753	-3789	0	89	175015	0.00	0.00	40.00	
8	-0	-12420	-4264	-3609	0	1617	175015	0.01	0.00	40.00	
9	-0	-12150	-3768	-3784	0	40	175015	0.00	0.00	40.00	
10	-0	-12320	-4058	-3682	0	928	175015	0.01	0.00	40.00	
11	-0	-12240	-3909	-3735	0	430	175015	0.00	0.00	40.00	
12	-0	-12330	-4108	-3663	0	1099	175015	0.01	0.00	40.00	
13	-0	-12250	-3959	-3716	0	600	175015	0.00	0.00	40.00	
14	-0	-12410	-4249	-3614	0	1568	175015	0.01	0.00	40.00	
15	-0	-12150	-3753	-3789	0	89	175015	0.00	0.00	40.00	
16	-0	-12420	-4264	-3609	0	1617	175015	0.01	0.00	40.00	
17	-0	-12150	-3768	-3784	0	40	175015	0.00	0.00	40.00	

CONFRONTO E SINTESI CONCLUSIVE (si assume in ogni caso passo <= 15 cm)

I.R.compr.	Ashy	Ashz	PASSO	Nota
	cmq		cm	
0.01	--	--	15.00	**VERIFICATO**

ASTA NUM. 50 NI 166 NF 167 SEZ. Rp B= 0.400 H= 0.600 (pilastro)
PIL. NUM. 26B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice resistenza			aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-10450	-502	-6	0	-215	1352	12.57	12.57	6.28	6.28	3	0.05	0.01	0.05	0.00	0.00	24.0
2	0	-8280	-219	-50	0	-256	583	12.57	12.57	6.28	6.28	2	0.04	0.00	0.02	0.00	0.00	24.0
3	0	-8279	-223	44	0	-65	584	12.57	12.57	6.28	6.28	2	0.03	0.00	0.02	0.00	0.00	24.0
4	0	-7803	-550	-53	0	-266	1497	12.57	12.57	6.28	6.28	2	0.09	0.01	0.06	0.00	0.00	24.0
5	0	-7802	-554	40	0	-75	1498	12.57	12.57	6.28	6.28	2	0.08	0.01	0.06	0.00	0.00	24.0
6	0	-8113	-331	-160	0	-482	902	12.57	12.57	6.28	6.28	2	0.06	0.01	0.03	0.00	0.00	24.0
7	0	-8112	-343	152	0	154	904	12.57	12.57	6.28	6.28	2	0.05	0.01	0.04	0.00	0.00	24.0
8	0	-7970	-430	-161	0	-485	1176	12.57	12.57	6.28	6.28	2	0.08	0.01	0.04	0.00	0.00	24.0
9	0	-7969	-442	151	0	151	1178	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
10	0	-8280	-219	-50	0	-256	583	12.57	12.57	6.28	6.28	2	0.04	0.00	0.02	0.00	0.00	24.0
11	0	-8279	-223	44	0	-65	584	12.57	12.57	6.28	6.28	2	0.03	0.00	0.02	0.00	0.00	24.0
12	0	-7803	-550	-53	0	-266	1497	12.57	12.57	6.28	6.28	2	0.09	0.01	0.06	0.00	0.00	24.0
13	0	-7802	-554	40	0	-75	1498	12.57	12.57	6.28	6.28	2	0.08	0.01	0.06	0.00	0.00	24.0
14	0	-8113	-331	-160	0	-482	902	12.57	12.57	6.28	6.28	2	0.06	0.01	0.03	0.00	0.00	24.0
15	0	-8112	-343	152	0	154	904	12.57	12.57	6.28	6.28	2	0.05	0.01	0.04	0.00	0.00	24.0
16	0	-7970	-430	-161	0	-485	1176	12.57	12.57	6.28	6.28	2	0.08	0.01	0.04	0.00	0.00	24.0
17	0	-7969	-442	151	0	151	1178	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0

18	0	-12160	-515	-331	0	-847	696	12.57	12.57	6.28	6.28	3	0.05	0.01	0.05	0.00	0.00	24.0
19	0	-10840	-1411	-287	0	-775	3246	12.57	12.57	6.28	6.28	3	0.13	0.02	0.14	0.00	0.00	24.0
20	0	-11390	-910	-70	0	-302	1889	12.57	12.57	6.28	6.28	3	0.07	0.02	0.09	0.00	0.00	24.0
37	0	-12200	-67	-253	0	-686	-355	12.57	12.57	6.28	6.28	3	0.04	0.00	0.02	0.00	0.00	24.0
38	0	-9997	-1559	-180	0	-566	3894	12.57	12.57	6.28	6.28	3	0.15	0.03	0.16	0.00	0.00	24.0
39	0	-10930	-725	182	0	222	1632	12.57	12.57	6.28	6.28	3	0.06	0.01	0.07	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	97	-9690	-502	-6	0	-209	862	12.57	12.57	6.28	6.28	3	0.03	0.01	0.05	0.00	0.00	24.0
2	97	-7695	-219	-50	0	-208	369	12.57	12.57	6.28	6.28	2	0.03	0.00	0.02	0.00	0.00	24.0
3	97	-7694	-223	44	0	-108	366	12.57	12.57	6.28	6.28	2	0.02	0.00	0.02	0.00	0.00	24.0
4	97	-7218	-550	-53	0	-214	961	12.57	12.57	6.28	6.28	2	0.06	0.01	0.06	0.00	0.00	24.0
5	97	-7217	-554	40	0	-115	958	12.57	12.57	6.28	6.28	2	0.05	0.01	0.06	0.00	0.00	24.0
6	97	-7528	-331	-160	0	-326	580	12.57	12.57	6.28	6.28	2	0.04	0.01	0.03	0.00	0.00	24.0
7	97	-7527	-343	152	0	6	570	12.57	12.57	6.28	6.28	2	0.03	0.01	0.04	0.00	0.00	24.0
8	97	-7385	-430	-161	0	-328	757	12.57	12.57	6.28	6.28	2	0.05	0.01	0.04	0.00	0.00	24.0
9	97	-7384	-442	151	0	4	747	12.57	12.57	6.28	6.28	2	0.04	0.01	0.05	0.00	0.00	24.0
10	97	-7695	-219	-50	0	-208	369	12.57	12.57	6.28	6.28	2	0.03	0.00	0.02	0.00	0.00	24.0
11	97	-7694	-223	44	0	-108	366	12.57	12.57	6.28	6.28	2	0.02	0.00	0.02	0.00	0.00	24.0
12	97	-7218	-550	-53	0	-214	961	12.57	12.57	6.28	6.28	2	0.06	0.01	0.06	0.00	0.00	24.0
13	97	-7217	-554	40	0	-115	958	12.57	12.57	6.28	6.28	2	0.05	0.01	0.06	0.00	0.00	24.0
14	97	-7528	-331	-160	0	-326	580	12.57	12.57	6.28	6.28	2	0.04	0.01	0.03	0.00	0.00	24.0
15	97	-7527	-343	152	0	6	570	12.57	12.57	6.28	6.28	2	0.03	0.01	0.04	0.00	0.00	24.0
16	97	-7385	-430	-161	0	-328	757	12.57	12.57	6.28	6.28	2	0.05	0.01	0.04	0.00	0.00	24.0
17	97	-7384	-442	151	0	4	747	12.57	12.57	6.28	6.28	2	0.04	0.01	0.05	0.00	0.00	24.0
18	97	-11400	-515	-331	0	-524	194	12.57	12.57	6.28	6.28	3	0.03	0.01	0.05	0.00	0.00	24.0
19	97	-10078	-1411	-287	0	-495	1871	12.57	12.57	6.28	6.28	3	0.07	0.02	0.14	0.00	0.00	24.0
20	97	-10630	-910	-70	0	-234	1002	12.57	12.57	6.28	6.28	3	0.04	0.02	0.09	0.00	0.00	24.0
37	97	-11440	-67	-253	0	-439	-420	12.57	12.57	6.28	6.28	3	0.03	0.00	0.02	0.00	0.00	24.0
38	97	-9236	-1559	-180	0	-390	2374	12.57	12.57	6.28	6.28	3	0.09	0.03	0.16	0.00	0.00	24.0
39	97	-10168	-725	182	0	45	925	12.57	12.57	6.28	6.28	3	0.03	0.01	0.07	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	195	-8930	-502	-6	0	-204	372	12.57	12.57	6.28	6.28	3	0.02	0.01	0.05	0.00	0.00	24.0
2	195	-7110	-219	-50	0	-159	156	12.57	12.57	6.28	6.28	2	0.01	0.00	0.02	0.00	0.00	24.0
3	195	-7109	-223	44	0	-151	149	12.57	12.57	6.28	6.28	2	0.01	0.00	0.02	0.00	0.00	24.0
4	195	-6633	-550	-53	0	-162	424	12.57	12.57	6.28	6.28	2	0.03	0.01	0.06	0.00	0.00	24.0
5	195	-6632	-554	40	0	-154	418	12.57	12.57	6.28	6.28	2	0.03	0.01	0.06	0.00	0.00	24.0
6	195	-6943	-331	-160	0	-170	257	12.57	12.57	6.28	6.28	2	0.02	0.01	0.03	0.00	0.00	24.0
7	195	-6942	-343	152	0	-142	236	12.57	12.57	6.28	6.28	2	0.02	0.01	0.04	0.00	0.00	24.0
8	195	-6800	-430	-161	0	-171	337	12.57	12.57	6.28	6.28	2	0.02	0.01	0.04	0.00	0.00	24.0
9	195	-6799	-442	151	0	-143	316	12.57	12.57	6.28	6.28	2	0.02	0.01	0.05	0.00	0.00	24.0
10	195	-7110	-219	-50	0	-159	156	12.57	12.57	6.28	6.28	2	0.01	0.00	0.02	0.00	0.00	24.0
11	195	-7109	-223	44	0	-151	149	12.57	12.57	6.28	6.28	2	0.01	0.00	0.02	0.00	0.00	24.0
12	195	-6633	-550	-53	0	-162	424	12.57	12.57	6.28	6.28	2	0.03	0.01	0.06	0.00	0.00	24.0
13	195	-6632	-554	40	0	-154	418	12.57	12.57	6.28	6.28	2	0.03	0.01	0.06	0.00	0.00	24.0
14	195	-6943	-331	-160	0	-170	257	12.57	12.57	6.28	6.28	2	0.02	0.01	0.03	0.00	0.00	24.0
15	195	-6942	-343	152	0	-142	236	12.57	12.57	6.28	6.28	2	0.02	0.01	0.04	0.00	0.00	24.0
16	195	-6800	-430	-161	0	-171	337	12.57	12.57	6.28	6.28	2	0.02	0.01	0.04	0.00	0.00	24.0
17	195	-6799	-442	151	0	-143	316	12.57	12.57	6.28	6.28	2	0.02	0.01	0.05	0.00	0.00	24.0
18	195	-10639	-515	-331	0	-201	-308	12.57	12.57	6.28	6.28	3	0.02	0.01	0.05	0.00	0.00	24.0
19	195	-9317	-1411	-287	0	-215	495	12.57	12.57	6.28	6.28	3	0.02	0.02	0.14	0.00	0.00	24.0
20	195	-9870	-910	-70	0	-166	115	12.57	12.57	6.28	6.28	3	0.01	0.02	0.09	0.00	0.00	24.0
37	195	-10681	-67	-253	0	-192	-486	12.57	12.57	6.28	6.28	3	0.02	0.00	0.02	0.00	0.00	24.0
38	195	-8476	-1559	-180	0	-215	854	12.57	12.57	6.28	6.28	3	0.03	0.03	0.16	0.00	0.00	24.0
39	195	-9407	-725	182	0	-132	219	12.57	12.57	6.28	6.28	3	0.01	0.01	0.07	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	292	-8171	-502	-6	0	-198	-117	12.57	12.57	6.28	6.28	3	0.01	0.01	0.05	0.00	0.00	24.0
2	292	-6525	-219	-50	0	-111	-58	12.57	12.57	6.28	6.28	2	0.01	0.00	0.02	0.00	0.00	24.0
3	292	-6524	-223	44	0	-194	-68	12.57	12.57	6.28	6.28	2	0.01	0.00	0.02	0.00	0.00	24.0
4	292	-6048	-550	-53	0	-110	-112	12.57	12.57	6.28	6.28	2	0.01	0.01	0.06	0.00	0.00	24.0
5	292	-6047	-554	40	0	-193	-122	12.57	12.57	6.28	6.28	2	0.02	0.01	0.06	0.00	0.00	24.0
6	292	-6358	-331	-160	0	-14	-66	12.57	12.57	6.28	6.28	2	0.00	0.01	0.03	0.00	0.00	24.0
7	292	-6357	-343	152	0	-291	-99	12.57	12.57	6.28	6.28	2	0.02	0.01	0.04	0.00	0.00	24.0
8	292	-6215	-430	-161	0	-13	-82	12.57	12.57	6.28	6.28	2	0.00	0.01	0.05	0.00	0.00	24.0
9	292	-6214	-442	151	0	-290	-115	12.57	12.57	6.28	6.28	2	0.02	0.01	0.05	0.00	0.00	24.0
10	292	-6525	-219	-50	0	-111	-58	12.57	12.57	6.28	6.28	2	0.01	0.00	0.02	0.00	0.00	24.0
11	292	-6524	-223	44	0	-194	-68	12.57	12.57	6.28	6.28	2	0.01	0.00	0.02	0.00	0.00	24.0
12	292	-6048	-550	-53	0	-110	-112	12.57	12.57	6.28	6.28	2	0.01	0.01	0.06	0.00	0.00	24.0
13	292	-6047	-554	40	0	-193	-122	12.57	12.57	6.28	6.28	2	0.02	0.01	0.06	0.00	0.00	24.0
14	292	-6358	-331	-160	0	-14	-66	12.57	12.57	6.28	6.28	2	0.00	0.01	0.03	0.00	0.00	24.0
15	292	-6357	-343	152	0	-291	-99	12.57	12.57	6.28	6.28	2	0.02	0.01	0.04	0.00	0.00	24.0
16	292	-6215	-430	-161	0	-13	-82	12.57	12.57	6.28	6.28	2	0.00	0.01	0.05	0.00	0.00	24.0
17	292	-6214	-442	151	0	-290	-115	12.57	12.57	6.28	6.28	2	0.02	0.01	0.05	0.00	0.00	24.0
18	292	-9878	-515	-331	0	121	-811	12.57	12.57	6.28	6.28	3	0.03	0.01	0.05	0.00	0.00	24.0
19	292	-8556	-1411	-287	0	64	-880	12.57	12.57	6.28	6.28	3	0.03	0.02	0.14	0.00	0.00	24.0
20	292	-9111	-910	-70	0	-97	-773	12.57	12.57	6.28	6.28	3	0.03	0.02	0.09	0.00	0.00	24.0
37	292	-9922	-67	-253	0	55	-551	12.57	12.57	6.28	6.28	3	0.02	0.00	0.02	0.00	0.00	24.0
38	292	-7716	-1559	-180	0	-40	-667	12.57	12.57	6.28	6.28	3	0.02	0.03	0.16	0.00	0.00	24.0
39	292	-8646	-725	182	0	-309	-488	12.57	12.57	6.28	6.28	3	0.02	0.01	0.07	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	390	-7411	-502	-6	0	-192	-607	12.57	12.57	6.28	6.28	3	0.03	0.01	0.05	0.00	0.00	24.0
2	390	-5940	-219	-50	0	-63	-272	12.57	12.57	6.28	6.28	2	0.02	0.00	0.02	0.00	0.00	24.0
3	390	-5939	-223	44	0	-237	-285	12.57	12.57	6.28	6.28	2	0.02	0.00	0.02	0.00	0.00	24.0
4	390	-5463	-550	-53	0	-58	-649	12.57	12.57	6.28	6.28	2	0.04	0.01	0.06	0.00	0.00	24.0
5	390	-5462	-554	40	0	-232	-662	12.57	12.57	6.28	6.28	2	0.04	0.01	0.06	0.00	0.00	24.0
6	390	-5773	-331	-160	0	143	-388	12.57	12.57	6.28	6.28	2	0.03	0.01	0.03	0.00	0.00	24.0
7	390	-5772	-343	152	0	-439	-433	12.57	12.57	6.28	6.28	2	0.04	0.01	0.04	0.00	0.00	24.0
8	390	-5630	-430	-161	0	144	-501	12.57	12.57	6.28	6.28	2	0.03	0.01	0.05	0.00	0.00	24.0
9	390	-5629	-442	151	0	-438	-546	12.57	12.57	6.28	6.28	2	0.05	0.01	0.05	0.00	0.00	24.0
10	390	-5940	-219	-50	0	-63	-272	12.57	12.57	6.28	6.28	2	0.02	0.00	0.02	0.00	0.00	24.0
11	390	-5939	-223	44	0	-237	-285	12.57	12.57	6.28	6.28	2	0.02	0.00	0.02	0.00	0.00	24.0
12	390	-5463	-550	-53	0	-58	-649	12.57	12.57	6.28	6.28	2	0.04	0.01	0.06	0.00	0.00	24.0
13	390	-5462	-554	40	0	-232	-662	12.57	12.57	6.28	6.28	2	0.04	0.01	0.06	0.00	0.00	24.0
14	390	-5773	-331	-160	0	143	-388	12.57	12.57	6.28	6.28	2	0.03	0.01	0.03	0.00	0.00	24.0
15	390	-5772	-343	152	0	-439	-433	12.57	12.57	6.28	6.28	2	0.04	0.01	0.04	0.00	0.00	24.0
16	390	-5630	-430	-161	0	144	-501	12.57	12.57	6.28	6.28	2	0.03	0.01	0.05	0.00	0.00	24.0
17	390	-5629	-442	151	0	-438	-546	12.57	12.57	6.28	6.28	2	0.05	0.01	0.05	0.00	0.00	24.0
18	390	-9118	-515	-331	0	444	-1313	12.57	12.57	6.28	6.28	3	0.05	0.01	0.05	0.00	0.00	24.0
19	390	-7794	-1411	-287	0	344	-2255	12.57	12.57	6.28	6.28	3	0.09	0.02	0.14	0.00	0.00	24.0
20	390	-8351	-910	-70	0	-29	-1660	12.57	12.57	6.28	6.28	3	0.06	0.02	0.09	0.00	0.00	24.0
37	390	-9162	-67	-253	0	302	-616	12.57	12.57	6.28	6.28	3	0.03	0.00	0.02	0.00	0.00	24.0
38	390	-6955	-1559	-180	0	136	-2187	12.57	12.57	6.28	6.28	3	0.08	0.03	0.16	0.00	0.00	24.0
39	390	-7884	-725	182	0	-487	-1195	12.57	12.57	6.28	6.28	3	0.05	0.01	0.07	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

VERIFICA NODO IN TESTA AL PILASTRO, NODO NUM. 167 NON CONFINATO
(par.7.2.2 NTC2018 "La domanda di resistenza valutata con i criteri della progettazione in capacità può essere assunta non superiore alla domanda di resistenza valutata per il caso di comportamento strutturale non dissipativo.")

PROGETTAZIONE IN CAPACITA'
Asse loc. pilastro y nodo ESTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 40.0 cm, hjc= 50.0 cm
Asse loc. pilastro z nodo ESTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 50.0 cm, hjc= 30.0 cm

FxMin,inf	FxMin,sup	FxMax,sup	FySup	FzSup	Vjbdy	Vjbdz	Vres,y	Vres,z	I.R.compr.	Ashy	Ashz	PASSO	Nota
daN					daN		daN			cmq		cm	
-5462	-1499	-1990	1402	99	16214	17517	139180	104385	0.17	--	--	40.00	

VERIFICA DI RESISTENZA CON SOLLECITAZIONI COMPORTAMENTO NON DISSIPATIVO

Asse loc. pilastro y nodo ESTERNO: Hjw= 40.0 cm, bj= 40.0 cm, hjc= 50.0 cm, db1= 45.0 cm

NC	Fx,sup	Fx,inf	Mb	Vb	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-1857	-5940	-1717	1304	2062	2178	139236	0.02	0.00	40.00	
3	-1718	-5939	-1729	1307	2087	2182	139294	0.02	0.00	40.00	
4	-1772	-5463	-665	960	1402	240	139272	0.00	0.00	40.00	
5	-1632	-5462	-677	964	1428	244	139330	0.00	0.00	40.00	
6	-1990	-5773	-1335	1179	1801	1495	139180	0.01	0.00	40.00	
7	-1524	-5772	-1375	1191	1886	1509	139375	0.01	0.00	40.00	
8	-1965	-5630	-1019	1076	1603	913	139191	0.01	0.00	40.00	
9	-1499	-5629	-1060	1088	1688	929	139386	0.01	0.00	40.00	
10	-1857	-5940	-1717	1304	2062	2178	139236	0.02	0.00	40.00	
11	-1718	-5939	-1729	1307	2087	2182	139294	0.02	0.00	40.00	
12	-1772	-5463	-665	960	1402	240	139272	0.00	0.00	40.00	
13	-1632	-5462	-677	964	1428	244	139330	0.00	0.00	40.00	
14	-1990	-5773	-1335	1179	1801	1495	139180	0.01	0.00	40.00	
15	-1524	-5772	-1375	1191	1886	1509	139375	0.01	0.00	40.00	
16	-1965	-5630	-1019	1076	1603	913	139191	0.01	0.00	40.00	
17	-1499	-5629	-1060	1088	1688	929	139386	0.01	0.00	40.00	

Asse loc. pilastro z nodo ESTERNO: Hjw= 40.0 cm, bj= 50.0 cm, hjc= 30.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb	Vb	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-1857	-5940	-1021	2779	759	1762	104427	0.02	0.00	40.00	
3	-1718	-5939	-1213	2915	380	2615	104471	0.03	0.00	40.00	
4	-1772	-5463	-947	2731	652	1685	104454	0.02	0.00	40.00	
5	-1632	-5462	-1138	2867	274	2536	104498	0.02	0.00	40.00	
6	-1990	-5773	-771	2603	1164	740	104385	0.01	0.00	40.00	
7	-1524	-5772	-1411	3057	99	3385	104532	0.03	0.00	40.00	
8	-1965	-5630	-749	2589	1132	717	104393	0.01	0.00	40.00	
9	-1499	-5629	-1388	3042	131	3296	104539	0.03	0.00	40.00	
10	-1857	-5940	-1021	2779	759	1762	104427	0.02	0.00	40.00	
11	-1718	-5939	-1213	2915	380	2615	104471	0.03	0.00	40.00	
12	-1772	-5463	-947	2731	652	1685	104454	0.02	0.00	40.00	
13	-1632	-5462	-1138	2867	274	2536	104498	0.02	0.00	40.00	
14	-1990	-5773	-771	2603	1164	740	104385	0.01	0.00	40.00	
15	-1524	-5772	-1411	3057	99	3385	104532	0.03	0.00	40.00	
16	-1965	-5630	-749	2589	1132	717	104393	0.01	0.00	40.00	
17	-1499	-5629	-1388	3042	131	3296	104539	0.03	0.00	40.00	

CONFRONTO E SINTESI CONCLUSIVE (si assume in ogni caso passo <= 15 cm)

I.R.compr.	Ashy	Ashz	PASSO	Nota
	cmq		cm	
0.03	--	--	15.00	**VERIFICATO**

ASTA NUM. 51 NI 168 NF 169 SEZ. Rp B= 0.400 H= 0.600 (pilastro)
PIL. NUM. 11B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-7652	488	440	0	393	-1659	12.57	12.57	6.28	6.28	3	0.07	0.01	0.05	0.00	0.00	24.0
2	0	-5694	642	337	0	307	-1876	12.57	12.57	6.28	6.28	2	0.11	0.01	0.07	0.00	0.00	24.0
3	0	-5798	645	370	0	348	-1885	12.57	12.57	6.28	6.28	2	0.11	0.01	0.07	0.00	0.00	24.0
4	0	-5973	106	307	0	256	-668	12.57	12.57	6.28	6.28	2	0.04	0.01	0.03	0.00	0.00	24.0
5	0	-6078	110	340	0	298	-677	12.57	12.57	6.28	6.28	2	0.05	0.01	0.03	0.00	0.00	24.0
6	0	-5669	450	288	0	241	-1442	12.57	12.57	6.28	6.28	2	0.08	0.01	0.05	0.00	0.00	24.0
7	0	-6018	462	398	0	378	-1473	12.57	12.57	6.28	6.28	2	0.09	0.01	0.05	0.00	0.00	24.0
8	0	-5753	289	279	0	226	-1080	12.57	12.57	6.28	6.28	2	0.06	0.01	0.03	0.00	0.00	24.0
9	0	-6102	302	389	0	363	-1110	12.57	12.57	6.28	6.28	2	0.07	0.01	0.03	0.00	0.00	24.0
10	0	-5694	642	337	0	307	-1876	12.57	12.57	6.28	6.28	2	0.11	0.01	0.07	0.00	0.00	24.0
11	0	-5798	645	370	0	348	-1885	12.57	12.57	6.28	6.28	2	0.11	0.01	0.07	0.00	0.00	24.0
12	0	-5973	106	307	0	256	-668	12.57	12.57	6.28	6.28	2	0.04	0.01	0.03	0.00	0.00	24.0
13	0	-6078	110	340	0	298	-677	12.57	12.57	6.28	6.28	2	0.05	0.01	0.03	0.00	0.00	24.0
14	0	-5669	450	288	0	241	-1442	12.57	12.57	6.28	6.28	2	0.08	0.01	0.05	0.00	0.00	24.0
15	0	-6018	462	398	0	378	-1473	12.57	12.57	6.28	6.28	2	0.09	0.01	0.05	0.00	0.00	24.0
16	0	-5753	289	279	0	226	-1080	12.57	12.57	6.28	6.28	2	0.06	0.01	0.03	0.00	0.00	24.0
17	0	-6102	302	389	0	363	-1110	12.57	12.57	6.28	6.28	2	0.07	0.01	0.03	0.00	0.00	24.0
18	0	-7109	1768	502	0	509	-4493	12.57	12.57	6.28	6.28	3	0.17	0.03	0.18	0.00	0.00	24.0
19	0	-8122	-2	427	0	363	-514	12.57	12.57	6.28	6.28	3	0.03	0.01	0.04	0.00	0.00	24.0
20	0	-7644	830	419	0	344	-2387	12.57	12.57	6.28	6.28	3	0.09	0.01	0.09	0.00	0.00	24.0
37	0	-6735	2229	516	0	542	-5542	12.57	12.57	6.28	6.28	3	0.21	0.04	0.23	0.00	0.00	24.0
38	0	-8423	-721	390	0	300	1088	12.57	12.57	6.28	6.28	3	0.04	0.01	0.07	0.00	0.00	24.0
39	0	-7626	665	378	0	267	-2034	12.57	12.57	6.28	6.28	3	0.08	0.01	0.07	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	97	-6892	488	440	0	-36	-1183	12.57	12.57	6.28	6.28	3	0.04	0.01	0.05	0.00	0.00	24.0
2	97	-5109	642	337	0	-22	-1251	12.57	12.57	6.28	6.28	2	0.07	0.01	0.07	0.00	0.00	24.0
3	97	-5213	645	370	0	-13	-1256	12.57	12.57	6.28	6.28	2	0.07	0.01	0.07	0.00	0.00	24.0
4	97	-5388	106	307	0	-43	-564	12.57	12.57	6.28	6.28	2	0.03	0.01	0.03	0.00	0.00	24.0
5	97	-5493	110	340	0	-34	-569	12.57	12.57	6.28	6.28	2	0.03	0.01	0.03	0.00	0.00	24.0
6	97	-5084	450	288	0	-39	-1003	12.57	12.57	6.28	6.28	2	0.05	0.01	0.05	0.00	0.00	24.0
7	97	-5433	462	398	0	-10	-1022	12.57	12.57	6.28	6.28	2	0.05	0.01	0.05	0.00	0.00	24.0
8	97	-5168	289	279	0	-46	-798	12.57	12.57	6.28	6.28	2	0.04	0.01	0.03	0.00	0.00	24.0
9	97	-5517	302	389	0	-16	-816	12.57	12.57	6.28	6.28	2	0.04	0.01	0.03	0.00	0.00	24.0
10	97	-5109	642	337	0	-22	-1251	12.57	12.57	6.28	6.28	2	0.07	0.01	0.07	0.00	0.00	24.0
11	97	-5213	645	370	0	-13	-1256	12.57	12.57	6.28	6.28	2	0.07	0.01	0.07	0.00	0.00	24.0
12	97	-5388	106	307	0	-43	-564	12.57	12.57	6.28	6.28	2	0.03	0.01	0.03	0.00	0.00	24.0
13	97	-5493	110	340	0	-34	-569	12.57	12.57	6.28	6.28	2	0.03	0.01	0.03	0.00	0.00	24.0
14	97	-5084	450	288	0	-39	-1003	12.57	12.57	6.28	6.28	2	0.05	0.01	0.05	0.00	0.00	24.0
15	97	-5433	462	398	0	-10	-1022	12.57	12.57	6.28	6.28	2	0.05	0.01	0.05	0.00	0.00	24.0
16	97	-5168	289	279	0	-46	-798	12.57	12.57	6.28	6.28	2	0.04	0.01	0.03	0.00	0.00	24.0
17	97	-5517	302	389	0	-16	-816	12.57	12.57	6.28	6.28	2	0.04	0.01	0.03	0.00	0.00	24.0
18	97	-6348	1768	502	0	19	-2769	12.57	12.57	6.28	6.28	3	0.10	0.03	0.19	0.00	0.00	24.0
19	97	-7362	-2	427	0	-53	-516	12.57	12.57	6.28	6.28	3	0.02	0.01	0.04	0.00	0.00	24.0
20	97	-6884	830	419	0	-64	-1578	12.57	12.57	6.28	6.28	3	0.06	0.01	0.09	0.00	0.00	24.0
37	97	-5974	2229	516	0	39	-3369	12.57	12.57	6.28	6.28	3	0.13	0.04	0.23	0.00	0.00	24.0
38	97	-7662	-721	390	0	-81	386	12.57	12.57	6.28	6.28	3	0.02	0.01	0.07	0.00	0.00	24.0
39	97	-6866	665	378	0	-101	-1385	12.57	12.57	6.28	6.28	3	0.05	0.01	0.07	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	195	-6131	488	440	0	-465	-706	12.57	12.57	6.28	6.28	3	0.04	0.01	0.05	0.00	0.00	24.0
2	195	-4524	642	337	0	-350	-625	12.57	12.57	6.28	6.28	2	0.05	0.01	0.07	0.00	0.00	24.0
3	195	-4628	645	370	0	-374	-627	12.57	12.57	6.28	6.28	2	0.05	0.01	0.07	0.00	0.00	24.0
4	195	-4803	106	307	0	-342	-460	12.57	12.57	6.28	6.28	2	0.04	0.01	0.03	0.00	0.00	24.0
5	195	-4908	110	340	0	-366	-462	12.57	12.57	6.28	6.28	2	0.04	0.01	0.03	0.00	0.00	24.0
6	195	-4499	450	288	0	-320	-565	12.57	12.57	6.28	6.28	2	0.04	0.01	0.05	0.00	0.00	24.0
7	195	-4848	462	398	0	-398	-572	12.57	12.57	6.28	6.28	2	0.05	0.01	0.05	0.00	0.00	24.0
8	195	-4583	289	279	0	-318	-516	12.57	12.57	6.28	6.28	2	0.04	0.01	0.03	0.00	0.00	24.0
9	195	-4932	302	389	0	-396	-522	12.57	12.57	6.28	6.28	2	0.04	0.01	0.03	0.00	0.00	24.0
10	195	-4524	642	337	0	-350	-625	12.57	12.57	6.28	6.28	2	0.05	0.01	0.07	0.00	0.00	24.0
11	195	-4628	645	370	0	-374	-627	12.57	12.57	6.28	6.28	2	0.05	0.01	0.07	0.00	0.00	24.0
12	195	-4803	106	307	0	-342	-460	12.57	12.57	6.28	6.28	2	0.04	0.01	0.03	0.00	0.00	24.0
13	195	-4908	110	340	0	-366	-462	12.57	12.57	6.28	6.28	2	0.04	0.01	0.03	0.00	0.00	24.0
14	195	-4499	450	288	0	-320	-565	12.57	12.57	6.28	6.28	2	0.04	0.01	0.05	0.00	0.00	24.0
15	195	-4848	462	398	0	-398	-572	12.57	12.57	6.28	6.28	2	0.05	0.01	0.05	0.00	0.00	24.0
16	195	-4583	289	279	0	-318	-516	12.57	12.57	6.28	6.28	2	0.04	0.01	0.03	0.00	0.00	24.0
17	195	-4932	302	389	0	-396	-522	12.57	12.57	6.28	6.28	2	0.04	0.01	0.03	0.00	0.00	24.0
18	195	-5588	1768	502	0	-470	-1045	12.57	12.57	6.28	6.28	3	0.05	0.03	0.19	0.00	0.00	24.0
19	195	-6601	-2	427	0	-469	-518	12.57	12.57	6.28	6.28	3	0.03	0.01	0.04	0.00	0.00	24.0
20	195	-6123	830	419	0	-473	-769	12.57	12.57	6.28	6.28	3	0.04	0.01	0.09	0.00	0.00	24.0
37	195	-5214	2229	516	0	-465	-1195	12.57	12.57	6.28	6.28	3	0.05	0.04	0.24	0.00	0.00	24.0
38	195	-6902	-721	390	0	-462	-317	12.57	12.57	6.28	6.28	3	0.03	0.01	0.07	0.00	0.00	24.0
39	195	-6105	665	378	0	-469	-736	12.57	12.57	6.28	6.28	3	0.04	0.01	0.07	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	292	-5370	488	440	0	-894	-230	12.57	12.57	6.28	6.28	3	0.05	0.01	0.05	0.00	0.00	24.0
2	292	-3939	642	337	0	-679	0	12.57	12.57	6.28	6.28	2	0.04	0.01	0.07	0.00	0.00	24.0
3	292	-4043	645	370	0	-734	2	12.57	12.57	6.28	6.28	2	0.05	0.01	0.07	0.00	0.00	24.0
4	292	-4218	106	307	0	-642	-357	12.57	12.57	6.28	6.28	2	0.05	0.01	0.03	0.00	0.00	24.0
5	292	-4323	110	340	0	-697	-355	12.57	12.57	6.28	6.28	2	0.05	0.01	0.03	0.00	0.00	24.0
6	292	-3914	450	288	0	-601	-126	12.57	12.57	6.28	6.28	2	0.04	0.01	0.05	0.00	0.00	24.0
7	292	-4263	462	398	0	-786	-121	12.57	12.57	6.28	6.28	2	0.05	0.01	0.05	0.00	0.00	24.0
8	292	-3998	289	279	0	-590	-234	12.57	12.57	6.28	6.28	2	0.04	0.01	0.03	0.00	0.00	24.0
9	292	-4347	302	389	0	-775	-228	12.57	12.57	6.28	6.28	2	0.05	0.01	0.04	0.00	0.00	24.0
10	292	-3939	642	337	0	-679	0	12.57	12.57	6.28	6.28	2	0.04	0.01	0.07	0.00	0.00	24.0
11	292	-4043	645	370	0	-734	2	12.57	12.57	6.28	6.28	2	0.05	0.01	0.07	0.00	0.00	24.0
12	292	-4218	106	307	0	-642	-357	12.57	12.57	6.28	6.28	2	0.05	0.01	0.03	0.00	0.00	24.0
13	292	-4323	110	340	0	-697	-355	12.57	12.57	6.28	6.28	2	0.05	0.01	0.03	0.00	0.00	24.0
14	292	-3914	450	288	0	-601	-126	12.57	12.57	6.28	6.28	2	0.04	0.01	0.05	0.00	0.00	24.0
15	292	-4263	462	398	0	-786	-121	12.57	12.57	6.28	6.28	2	0.05	0.01	0.05	0.00	0.00	24.0
16	292	-3998	289	279	0	-590	-234	12.57	12.57	6.28	6.28	2	0.04	0.01	0.03	0.00	0.00	24.0
17	292	-4347	302	389	0	-775	-228	12.57	12.57	6.28	6.28	2	0.05	0.01	0.04	0.00	0.00	24.0
18	292	-4828	1768	502	0	-960	679	12.57	12.57	6.28	6.28	3	0.06	0.03	0.19	0.00	0.00	24.0
19	292	-5840	-2	427	0	-885	-520	12.57	12.57	6.28	6.28	3	0.05	0.01	0.04	0.00	0.00	24.0
20	292	-5362	830	419	0	-882	40	12.57	12.57	6.28	6.28	3	0.05	0.01	0.09	0.00	0.00	24.0
37	292	-4454	2229	516	0	-968	978	12.57	12.57	6.28	6.28	3	0.06	0.04	0.24	0.00	0.00	24.0
38	292	-6142	-721	390	0	-842	-1019	12.57	12.57	6.28	6.28	3	0.06	0.01	0.08	0.00	0.00	24.0
39	292	-5344	665	378	0	-838	-88	12.57	12.57	6.28	6.28	3	0.05	0.01	0.07	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	390	-4610	488	440	0	-1323	246	12.57	12.57	6.28	6.28	3	0.08	0.01	0.05	0.00	0.00	24.0
2	390	-3354	642	337	0	-1007	626	12.57	12.57	6.28	6.28	2	0.08	0.01	0.07	0.00	0.00	24.0
3	390	-3458	645	370	0	-1095	631	12.57	12.57	6.28	6.28	2	0.09	0.01	0.07	0.00	0.00	24.0
4	390	-3633	106	307	0	-941	-253	12.57	12.57	6.28	6.28	2	0.07	0.01	0.03	0.00	0.00	24.0
5	390	-3738	110	340	0	-1029	-248	12.57	12.57	6.28	6.28	2	0.07	0.01	0.03	0.00	0.00	24.0
6	390	-3329	450	288	0	-881	312	12.57	12.57	6.28	6.28	2	0.06	0.01	0.05	0.00	0.00	24.0
7	390	-3678	462	398	0	-1174	330	12.57	12.57	6.28	6.28	2	0.08	0.01	0.05	0.00	0.00	24.0
8	390	-3413	289	279	0	-862	48	12.57	12.57	6.28	6.28	2	0.06	0.01	0.03	0.00	0.00	24.0
9	390	-3762	302	389	0	-1155	66	12.57	12.57	6.28	6.28	2	0.07	0.01	0.04	0.00	0.00	24.0
10	390	-3354	642	337	0	-1007	626	12.57	12.57	6.28	6.28	2	0.08	0.01	0.07	0.00	0.00	24.0
11	390	-3458	645	370	0	-1095	631	12.57	12.57	6.28	6.28	2	0.09	0.01	0.07	0.00	0.00	24.0
12	390	-3633	106	307	0	-941	-253	12.57	12.57	6.28	6.28	2	0.07	0.01	0.03	0.00	0.00	24.0
13	390	-3738	110	340	0	-1029	-248	12.57	12.57	6.28	6.28	2	0.07	0.01	0.03	0.00	0.00	24.0
14	390	-3329	450	288	0	-881	312	12.57	12.57	6.28	6.28	2	0.06	0.01	0.05	0.00	0.00	24.0
15	390	-3678	462	398	0	-1174	330	12.57	12.57	6.28	6.28	2	0.08	0.01	0.05	0.00	0.00	24.0
16	390	-3413	289	279	0	-862	48	12.57	12.57	6.28	6.28	2	0.06	0.01	0.03	0.00	0.00	24.0
17	390	-3762	302	389	0	-1155	66	12.57	12.57	6.28	6.28	2	0.07	0.01	0.04	0.00	0.00	24.0
18	390	-4067	1768	502	0	-1449	2403	12.57	12.57	6.28	6.28	3	0.12	0.03	0.19	0.00	0.00	24.0
19	390	-5080	-2	427	0	-1301	-521	12.57	12.57	6.28	6.28	3	0.08	0.01	0.04	0.00	0.00	24.0
20	390	-4602	830	419	0	-1290	849	12.57	12.57	6.28	6.28	3	0.08	0.01	0.09	0.00	0.00	24.0
37	390	-3693	2229	516	0	-1471	3152	12.57	12.57	6.28	6.28	3	0.14	0.04	0.24	0.00	0.00	24.0
38	390	-5381	-721	390	0	-1223	-1722	12.57	12.57	6.28	6.28	3	0.09	0.01	0.08	0.00	0.00	24.0
39	390	-4584	665	378	0	-1206	561	12.57	12.57	6.28	6.28	3	0.07	0.01	0.07	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

VERIFICA NODO IN TESTA AL PILASTRO, NODO NUM. 169 NON CONFINATO

(par.7.2.2 NTC2018 "La domanda di resistenza valutata con i criteri della progettazione in capacità può essere assunta non superiore alla domanda di resistenza valutata per il caso di comportamento strutturale non dissipativo.")

PROGETTAZIONE IN CAPACITA'

Asse loc. pilastro y nodo ESTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 40.0 cm, hjc= 50.0 cm
Asse loc. pilastro z nodo ESTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 50.0 cm, hjc= 30.0 cm

FxMin,inf	FxMin,sup	FxMax,sup	FySup	FzSup	Vjbdy	Vjbdz	Vres,y	Vres,z	I.R.compr.	Ashy	Ashz	PASSO	Nota
daN					daN		daN			cmq		cm	
-3329	1	-0	0	0	17616	17616	140012	105009	0.17	--	--	40.00	

VERIFICA DI RESISTENZA CON SOLLECITAZIONI COMPORTAMENTO NON DISSIPATIVO

Asse loc. pilastro y nodo ESTERNO: Hjw= 40.0 cm, bj= 40.0 cm, hjc= 50.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb	Vb	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-0	-3354	850	571	0	2099	140012	0.01	0.00	40.00	
3	-0	-3458	854	569	0	2108	140012	0.02	0.00	40.00	
4	-0	-3633	-421	900	0	1040	140012	0.01	0.00	40.00	
5	-0	-3738	-417	898	0	1030	140012	0.01	0.00	40.00	
6	-0	-3329	561	687	0	1384	140012	0.01	0.00	40.00	
7	-0	-3678	572	683	0	1412	140012	0.01	0.00	40.00	
8	-0	-3413	-82	786	0	202	140012	0.00	0.00	40.00	
9	-0	-3762	-69	782	0	170	140012	0.00	0.00	40.00	
10	-0	-3354	850	571	0	2099	140012	0.01	0.00	40.00	
11	-0	-3458	854	569	0	2108	140012	0.02	0.00	40.00	
12	-0	-3633	-421	900	0	1040	140012	0.01	0.00	40.00	
13	-0	-3738	-417	898	0	1030	140012	0.01	0.00	40.00	
14	-0	-3329	561	687	0	1384	140012	0.01	0.00	40.00	
15	-0	-3678	572	683	0	1412	140012	0.01	0.00	40.00	
16	-0	-3413	-82	786	0	202	140012	0.00	0.00	40.00	
17	-0	-3762	-69	782	0	170	140012	0.00	0.00	40.00	

Asse loc. pilastro z nodo ESTERNO: Hjw= 40.0 cm, bj= 50.0 cm, hjc= 30.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb	Vb	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-0	-3354	-965	2783	0	2383	105009	0.02	0.00	40.00	
3	-0	-3458	-1053	2889	0	2600	105009	0.02	0.00	40.00	
4	-0	-3633	-894	2734	0	2207	105009	0.02	0.00	40.00	
5	-0	-3738	-981	2840	0	2423	105009	0.02	0.00	40.00	
6	-0	-3329	-838	2642	0	2070	105009	0.02	0.00	40.00	
7	-0	-3678	-1130	2995	0	2790	105009	0.03	0.00	40.00	
8	-0	-3413	-817	2627	0	2017	105009	0.02	0.00	40.00	
9	-0	-3762	-1108	2980	0	2736	105009	0.03	0.00	40.00	
10	-0	-3354	-965	2783	0	2383	105009	0.02	0.00	40.00	
11	-0	-3458	-1053	2889	0	2600	105009	0.02	0.00	40.00	
12	-0	-3633	-894	2734	0	2207	105009	0.02	0.00	40.00	
13	-0	-3738	-981	2840	0	2423	105009	0.02	0.00	40.00	
14	-0	-3329	-838	2642	0	2070	105009	0.02	0.00	40.00	
15	-0	-3678	-1130	2995	0	2790	105009	0.03	0.00	40.00	
16	-0	-3413	-817	2627	0	2017	105009	0.02	0.00	40.00	
17	-0	-3762	-1108	2980	0	2736	105009	0.03	0.00	40.00	

CONFRONTO E SINTESI CONCLUSIVE (si assume in ogni caso passo <= 15 cm)

I.R.compr.	Ashy	Ashz	PASSO	Nota
	cmq		cm	
0.03	--	--	15.00	**VERIFICATO**

ASTA NUM. 52 NI 170 NF 171 SEZ. Rp B= 0.400 H= 0.600 (pilastro)
PIL. NUM. 16B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-11920	820	695	0	680	-1397	12.57	12.57	6.28	6.28	3	0.06	0.01	0.08	0.00	0.00	24.0
2	0	-9106	1020	512	0	496	-1810	12.57	12.57	6.28	6.28	2	0.11	0.02	0.10	0.00	0.00	24.0
3	0	-9229	1021	547	0	538	-1812	12.57	12.57	6.28	6.28	2	0.11	0.02	0.10	0.00	0.00	24.0
4	0	-9105	240	522	0	508	-337	12.57	12.57	6.28	6.28	2	0.04	0.01	0.05	0.00	0.00	24.0
5	0	-9229	242	556	0	550	-339	12.57	12.57	6.28	6.28	2	0.04	0.01	0.05	0.00	0.00	24.0
6	0	-8961	745	476	0	451	-1292	12.57	12.57	6.28	6.28	2	0.08	0.01	0.08	0.00	0.00	24.0
7	0	-9373	750	590	0	592	-1299	12.57	12.57	6.28	6.28	2	0.09	0.01	0.08	0.00	0.00	24.0
8	0	-8961	512	478	0	454	-850	12.57	12.57	6.28	6.28	2	0.06	0.01	0.05	0.00	0.00	24.0
9	0	-9373	516	593	0	596	-857	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
10	0	-9106	1020	512	0	496	-1810	12.57	12.57	6.28	6.28	2	0.11	0.02	0.10	0.00	0.00	24.0
11	0	-9229	1021	547	0	538	-1812	12.57	12.57	6.28	6.28	2	0.11	0.02	0.10	0.00	0.00	24.0
12	0	-9105	240	522	0	508	-337	12.57	12.57	6.28	6.28	2	0.04	0.01	0.05	0.00	0.00	24.0
13	0	-9229	242	556	0	550	-339	12.57	12.57	6.28	6.28	2	0.04	0.01	0.05	0.00	0.00	24.0
14	0	-8961	745	476	0	451	-1292	12.57	12.57	6.28	6.28	2	0.08	0.01	0.08	0.00	0.00	24.0
15	0	-9373	750	590	0	592	-1299	12.57	12.57	6.28	6.28	2	0.09	0.01	0.08	0.00	0.00	24.0
16	0	-8961	512	478	0	454	-850	12.57	12.57	6.28	6.28	2	0.06	0.01	0.05	0.00	0.00	24.0
17	0	-9373	516	593	0	596	-857	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
18	0	-12340	2690	704	0	675	-4863	12.57	12.57	6.28	6.28	3	0.18	0.05	0.26	0.00	0.00	24.0
19	0	-12350	104	729	0	704	-12	12.57	12.57	6.28	6.28	3	0.04	0.01	0.07	0.00	0.00	24.0
20	0	-12270	1319	625	0	532	-2298	12.57	12.57	6.28	6.28	3	0.09	0.02	0.13	0.00	0.00	24.0
37	0	-12090	3363	679	0	654	-6140	12.57	12.57	6.28	6.28	3	0.23	0.06	0.33	0.00	0.00	24.0
38	0	-12120	-946	720	0	702	1944	12.57	12.57	6.28	6.28	3	0.08	0.02	0.09	0.00	0.00	24.0
39	0	-11980	1078	547	0	415	-1865	12.57	12.57	6.28	6.28	3	0.07	0.02	0.10	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	97	-11159	820	695	0	3	-597	12.57	12.57	6.28	6.28	3	0.02	0.01	0.08	0.00	0.00	24.0
2	97	-8521	1020	512	0	-3	-816	12.57	12.57	6.28	6.28	2	0.04	0.02	0.10	0.00	0.00	24.0
3	97	-8644	1021	547	0	5	-816	12.57	12.57	6.28	6.28	2	0.04	0.02	0.10	0.00	0.00	24.0

4	97	-8520	240	522	0	-1	-102	12.57	12.57	6.28	6.28	2	0.01	0.01	0.04	0.00	0.00	24.0
5	97	-8644	242	556	0	8	-103	12.57	12.57	6.28	6.28	2	0.01	0.01	0.05	0.00	0.00	24.0
6	97	-8376	745	476	0	-13	-566	12.57	12.57	6.28	6.28	2	0.03	0.01	0.08	0.00	0.00	24.0
7	97	-8788	750	590	0	16	-568	12.57	12.57	6.28	6.28	2	0.03	0.01	0.08	0.00	0.00	24.0
8	97	-8376	512	478	0	-12	-351	12.57	12.57	6.28	6.28	2	0.02	0.01	0.05	0.00	0.00	24.0
9	97	-8788	516	593	0	17	-354	12.57	12.57	6.28	6.28	2	0.02	0.01	0.05	0.00	0.00	24.0
10	97	-8521	1020	512	0	-3	-816	12.57	12.57	6.28	6.28	2	0.04	0.02	0.10	0.00	0.00	24.0
11	97	-8644	1021	547	0	5	-816	12.57	12.57	6.28	6.28	2	0.04	0.02	0.10	0.00	0.00	24.0
12	97	-8520	240	522	0	-1	-102	12.57	12.57	6.28	6.28	2	0.01	0.01	0.04	0.00	0.00	24.0
13	97	-8644	242	556	0	8	-103	12.57	12.57	6.28	6.28	2	0.01	0.01	0.05	0.00	0.00	24.0
14	97	-8376	745	476	0	-13	-566	12.57	12.57	6.28	6.28	2	0.03	0.01	0.08	0.00	0.00	24.0
15	97	-8788	750	590	0	16	-568	12.57	12.57	6.28	6.28	2	0.03	0.01	0.08	0.00	0.00	24.0
16	97	-8376	512	478	0	-12	-351	12.57	12.57	6.28	6.28	2	0.02	0.01	0.05	0.00	0.00	24.0
17	97	-8788	516	593	0	17	-354	12.57	12.57	6.28	6.28	2	0.02	0.01	0.05	0.00	0.00	24.0
18	97	-11578	2690	704	0	-11	-2241	12.57	12.57	6.28	6.28	3	0.08	0.05	0.26	0.00	0.00	24.0
19	97	-11590	104	729	0	-7	89	12.57	12.57	6.28	6.28	3	0.00	0.01	0.06	0.00	0.00	24.0
20	97	-11509	1319	625	0	-78	-1012	12.57	12.57	6.28	6.28	3	0.04	0.02	0.13	0.00	0.00	24.0
37	97	-11329	3363	679	0	-8	-2861	12.57	12.57	6.28	6.28	3	0.10	0.06	0.33	0.00	0.00	24.0
38	97	-11358	-946	720	0	-1	1022	12.57	12.57	6.28	6.28	3	0.04	0.02	0.09	0.00	0.00	24.0
39	97	-11218	1078	547	0	-119	-814	12.57	12.57	6.28	6.28	3	0.03	0.02	0.11	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	195	-10398	820	695	0	-675	202	12.57	12.57	6.28	6.28	3	0.04	0.01	0.08	0.00	0.00	24.0
2	195	-7936	1020	512	0	-503	178	12.57	12.57	6.28	6.28	2	0.04	0.02	0.10	0.00	0.00	24.0
3	195	-8059	1021	547	0	-528	179	12.57	12.57	6.28	6.28	2	0.04	0.02	0.10	0.00	0.00	24.0
4	195	-7935	240	522	0	-510	132	12.57	12.57	6.28	6.28	2	0.03	0.01	0.05	0.00	0.00	24.0
5	195	-8059	242	556	0	-534	133	12.57	12.57	6.28	6.28	2	0.04	0.01	0.05	0.00	0.00	24.0
6	195	-7791	745	476	0	-477	161	12.57	12.57	6.28	6.28	2	0.03	0.01	0.08	0.00	0.00	24.0
7	195	-8203	750	590	0	-559	164	12.57	12.57	6.28	6.28	2	0.04	0.01	0.08	0.00	0.00	24.0
8	195	-7791	512	478	0	-478	147	12.57	12.57	6.28	6.28	2	0.03	0.01	0.05	0.00	0.00	24.0
9	195	-8203	516	593	0	-561	150	12.57	12.57	6.28	6.28	2	0.04	0.01	0.06	0.00	0.00	24.0
10	195	-7936	1020	512	0	-503	178	12.57	12.57	6.28	6.28	2	0.04	0.02	0.10	0.00	0.00	24.0
11	195	-8059	1021	547	0	-528	179	12.57	12.57	6.28	6.28	2	0.04	0.02	0.10	0.00	0.00	24.0
12	195	-7935	240	522	0	-510	132	12.57	12.57	6.28	6.28	2	0.03	0.01	0.05	0.00	0.00	24.0
13	195	-8059	242	556	0	-534	133	12.57	12.57	6.28	6.28	2	0.04	0.01	0.05	0.00	0.00	24.0
14	195	-7791	745	476	0	-477	161	12.57	12.57	6.28	6.28	2	0.03	0.01	0.08	0.00	0.00	24.0
15	195	-8203	750	590	0	-559	164	12.57	12.57	6.28	6.28	2	0.04	0.01	0.08	0.00	0.00	24.0
16	195	-7791	512	478	0	-478	147	12.57	12.57	6.28	6.28	2	0.03	0.01	0.05	0.00	0.00	24.0
17	195	-8203	516	593	0	-561	150	12.57	12.57	6.28	6.28	2	0.04	0.01	0.06	0.00	0.00	24.0
18	195	-10816	2690	704	0	-698	382	12.57	12.57	6.28	6.28	3	0.04	0.05	0.26	0.00	0.00	24.0
19	195	-10830	104	729	0	-718	191	12.57	12.57	6.28	6.28	3	0.04	0.01	0.07	0.00	0.00	24.0
20	195	-10748	1319	625	0	-687	274	12.57	12.57	6.28	6.28	3	0.04	0.02	0.13	0.00	0.00	24.0
37	195	-10568	3363	679	0	-670	418	12.57	12.57	6.28	6.28	3	0.04	0.06	0.33	0.00	0.00	24.0
38	195	-10597	-946	720	0	-704	99	12.57	12.57	6.28	6.28	3	0.04	0.02	0.09	0.00	0.00	24.0
39	195	-10457	1078	547	0	-652	237	12.57	12.57	6.28	6.28	3	0.04	0.02	0.11	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	292	-9636	820	695	0	-1352	1001	12.57	12.57	6.28	6.28	3	0.08	0.01	0.08	0.00	0.00	24.0
2	292	-7351	1020	512	0	-1002	1173	12.57	12.57	6.28	6.28	2	0.10	0.02	0.11	0.00	0.00	24.0
3	292	-7474	1021	547	0	-1061	1174	12.57	12.57	6.28	6.28	2	0.10	0.02	0.11	0.00	0.00	24.0
4	292	-7350	240	522	0	-1018	366	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
5	292	-7474	242	556	0	-1077	368	12.57	12.57	6.28	6.28	2	0.08	0.01	0.05	0.00	0.00	24.0
6	292	-7206	745	476	0	-940	887	12.57	12.57	6.28	6.28	2	0.09	0.01	0.08	0.00	0.00	24.0
7	292	-7618	750	590	0	-1135	895	12.57	12.57	6.28	6.28	2	0.10	0.01	0.08	0.00	0.00	24.0
8	292	-7206	512	478	0	-945	646	12.57	12.57	6.28	6.28	2	0.08	0.01	0.05	0.00	0.00	24.0
9	292	-7618	516	593	0	-1140	653	12.57	12.57	6.28	6.28	2	0.09	0.01	0.06	0.00	0.00	24.0
10	292	-7351	1020	512	0	-1002	1173	12.57	12.57	6.28	6.28	2	0.10	0.02	0.11	0.00	0.00	24.0
11	292	-7474	1021	547	0	-1061	1174	12.57	12.57	6.28	6.28	2	0.10	0.02	0.11	0.00	0.00	24.0
12	292	-7350	240	522	0	-1018	366	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
13	292	-7474	242	556	0	-1077	368	12.57	12.57	6.28	6.28	2	0.08	0.01	0.05	0.00	0.00	24.0
14	292	-7206	745	476	0	-940	887	12.57	12.57	6.28	6.28	2	0.09	0.01	0.08	0.00	0.00	24.0
15	292	-7618	750	590	0	-1135	895	12.57	12.57	6.28	6.28	2	0.10	0.01	0.08	0.00	0.00	24.0
16	292	-7206	512	478	0	-945	646	12.57	12.57	6.28	6.28	2	0.08	0.01	0.05	0.00	0.00	24.0
17	292	-7618	516	593	0	-1140	653	12.57	12.57	6.28	6.28	2	0.09	0.01	0.06	0.00	0.00	24.0
18	292	-10055	2690	704	0	-1384	3005	12.57	12.57	6.28	6.28	3	0.13	0.05	0.27	0.00	0.00	24.0
19	292	-10070	104	729	0	-1429	292	12.57	12.57	6.28	6.28	3	0.08	0.01	0.07	0.00	0.00	24.0
20	292	-9987	1319	625	0	-1297	1559	12.57	12.57	6.28	6.28	3	0.09	0.02	0.13	0.00	0.00	24.0
37	292	-9808	3363	679	0	-1332	3697	12.57	12.57	6.28	6.28	3	0.15	0.06	0.34	0.00	0.00	24.0
38	292	-9836	-946	720	0	-1406	-823	12.57	12.57	6.28	6.28	3	0.08	0.02	0.09	0.00	0.00	24.0
39	292	-9696	1078	547	0	-1185	1289	12.57	12.57	6.28	6.28	3	0.08	0.02	0.11	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	390	-8875	820	695	0	-2029	1801	12.57	12.57	6.28	6.28	3	0.13	0.01	0.08	0.00	0.00	24.0
2	390	-6766	1020	512	0	-1502	2167	12.57	12.57	6.28	6.28	2	0.17	0.02	0.11	0.00	0.00	24.0
3	390	-6889	1021	547	0	-1594	2170	12.57	12.57	6.28	6.28	2	0.18	0.02	0.11	0.00	0.00	24.0
4	390	-6765	240	522	0	-1527	601	12.57	12.57	6.28	6.28	2	0.11	0.01	0.05	0.00	0.00	24.0
5	390	-6889	242	556	0	-1619	604	12.57	12.57	6.28	6.28	2	0.12	0.01	0.05	0.00	0.00	24.0
6	390	-6621	745	476	0	-1404	1614	12.57	12.57	6.28	6.28	2	0.14	0.01	0.08	0.00	0.00	24.0
7	390	-7033	750	590	0	-1710	1626	12.57	12.57	6.28	6.28	2	0.16	0.01	0.08	0.00	0.00	24.0
8	390	-6621	512	478	0	-1411	1145	12.57	12.57	6.28	6.28	2	0.12	0.01	0.05	0.00	0.00	24.0
9	390	-7033	516	593	0	-1718	1156	12.57	12.57	6.28	6.28	2	0.14	0.01	0.06	0.00	0.00	24.0
10	390	-6766	1020	512	0	-1502	2167	12.57	12.57	6.28	6.28	2	0.17	0.02	0.11	0.00	0.00	24.0
11	390	-6889	1021	547	0	-1594	2170	12.57	12.57	6.28	6.28	2	0.18	0.02	0.11	0.00	0.00	24.0
12	390	-6765	240	522	0	-1527	601	12.57	12.57	6.28	6.28	2	0.11	0.01	0.05	0.00	0.00	24.0
13	390	-6889	242	556	0	-1619	604	12.57	12.57	6.28	6.28	2	0.12	0.01	0.05	0.00	0.00	24.0
14	390	-6621	745	476	0	-1404	1614	12.57	12.57	6.28	6.28	2	0.14	0.01	0.08	0.00	0.00	24.0
15	390	-7033	750	590	0	-1710	1626	12.57	12.57	6.28	6.28	2	0.16	0.01	0.08	0.00	0.00	24.0
16	390	-6621	512	478	0	-1411	1145	12.57	12.57	6.28	6.28	2	0.12	0.01	0.05	0.00	0.00	24.0
17	390	-7033	516	593	0	-1718	1156	12.57	12.57	6.28	6.28	2	0.14	0.01	0.06	0.00	0.00	24.0
18	390	-9293	2690	704	0	-2071	5627	12.57	12.57	6.28	6.28	3	0.24	0.05	0.27	0.00	0.00	24.0
19	390	-9310	104	729	0	-2140	394	12.57	12.57	6.28	6.28	3	0.12	0.01	0.07	0.00	0.00	24.0
20	390	-9226	1319	625	0	-1906	2845	12.57	12.57	6.28	6.28	3	0.14	0.02	0.13	0.00	0.00	24.0
37	390	-9047	3363	679	0	-1994	6976	12.57	12.57	6.28	6.28	3	0.28	0.06	0.34	0.00	0.00	24.0
38	390	-9074	-946	720	0	-2109	-1746	12.57	12.57	6.28	6.28	3	0.13	0.02	0.10	0.00	0.00	24.0
39	390	-8934	1078	547	0	-1718	2340	12.57	12.57	6.28	6.28	3	0.12	0.02	0.11	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

VERIFICA NODO IN TESTA AL PILASTRO, NODO NUM. 171 NON CONFINATO

(par.7.2.2 NTC2018 "La domanda di resistenza valutata con i criteri della progettazione in capacità può essere assunta non superiore alla domanda di resistenza valutata per il caso di comportamento strutturale non dissipativo.")

PROGETTAZIONE IN CAPACITA'

Asse loc. pilastro y nodo INTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 40.0 cm, hjc= 50.0 cm
Asse loc. pilastro z nodo ESTERNO: As2(inf)= 6.03, As1(sup)= 6.03, Hjw= 40.0 cm, bj= 60.0 cm, hjc= 30.0 cm

FxMin,inf	FxMin,sup	FxMax,sup	FySup	FzSup	Vjbdy	Vjbdz	Vres,y	Vres,z	I.R.compr.	Ashy	Ashz	PASSO	Nota

daN					daN		daN			cmq		cm
-6621	1	-0	0	0	35233	26425	175015	126011	0.21	4.08	1.81	13.08

VERIFICA DI RESISTENZA CON SOLLECITAZIONI COMPORTAMENTO NON DISSIPATIVO

Asse loc. pilastro y nodo INTERNO: Hjw= 40.0 cm, bj= 40.0 cm, hjc= 50.0 cm, db1= 45.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb,1	Mb,2	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-0	-6766	-2200	-45	0	5321	175015	0.03	0.00	40.00	
3	-0	-6889	-2203	-46	0	5327	175015	0.03	0.00	40.00	
4	-0	-6765	-1323	-895	0	1058	175015	0.01	0.00	40.00	
5	-0	-6889	-1326	-896	0	1063	175015	0.01	0.00	40.00	
6	-0	-6621	-1889	-341	0	3821	175015	0.02	0.00	40.00	
7	-0	-7033	-1900	-344	0	3841	175015	0.02	0.00	40.00	
8	-0	-6621	-1626	-596	0	2543	175015	0.01	0.00	40.00	
9	-0	-7033	-1637	-599	0	2563	175015	0.01	0.00	40.00	
10	-0	-6766	-2200	-45	0	5321	175015	0.03	0.00	40.00	
11	-0	-6889	-2203	-46	0	5327	175015	0.03	0.00	40.00	
12	-0	-6765	-1323	-895	0	1058	175015	0.01	0.00	40.00	
13	-0	-6889	-1326	-896	0	1063	175015	0.01	0.00	40.00	
14	-0	-6621	-1889	-341	0	3821	175015	0.02	0.00	40.00	
15	-0	-7033	-1900	-344	0	3841	175015	0.02	0.00	40.00	
16	-0	-6621	-1626	-596	0	2543	175015	0.01	0.00	40.00	
17	-0	-7033	-1637	-599	0	2563	175015	0.01	0.00	40.00	

Asse loc. pilastro z nodo ESTERNO: Hjw= 40.0 cm, bj= 60.0 cm, hjc= 30.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb	Vb	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-0	-6766	-1551	4514	0	3830	126011	0.03	0.00	40.00	
3	-0	-6889	-1644	4636	0	4059	126011	0.03	0.00	40.00	
4	-0	-6765	-1583	4540	0	3909	126011	0.03	0.00	40.00	
5	-0	-6889	-1676	4662	0	4138	126011	0.03	0.00	40.00	
6	-0	-6621	-1454	4381	0	3590	126011	0.03	0.00	40.00	
7	-0	-7033	-1763	4788	0	4353	126011	0.03	0.00	40.00	
8	-0	-6621	-1464	4389	0	3615	126011	0.03	0.00	40.00	
9	-0	-7033	-1773	4795	0	4378	126011	0.03	0.00	40.00	
10	-0	-6766	-1551	4514	0	3830	126011	0.03	0.00	40.00	
11	-0	-6889	-1644	4636	0	4059	126011	0.03	0.00	40.00	
12	-0	-6765	-1583	4540	0	3909	126011	0.03	0.00	40.00	
13	-0	-6889	-1676	4662	0	4138	126011	0.03	0.00	40.00	
14	-0	-6621	-1454	4381	0	3590	126011	0.03	0.00	40.00	
15	-0	-7033	-1763	4788	0	4353	126011	0.03	0.00	40.00	
16	-0	-6621	-1464	4389	0	3615	126011	0.03	0.00	40.00	
17	-0	-7033	-1773	4795	0	4378	126011	0.03	0.00	40.00	

CONFRONTO E SINTESI CONCLUSIVE (si assume in ogni caso passo <= 15 cm)

I.R.compr.	Ashy	Ashz	PASSO	Nota
	cmq		cm	
0.03	--	--	15.00	**VERIFICATO**

ASTA NUM. 53 NI 172 NF 185 SEZ. Rp B= 0.400 H= 0.600 (pilastro)
PIL. NUM. 21B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-11950	668	718	0	731	-1355	12.57	12.57	6.28	6.28	3	0.06	0.01	0.06	0.00	0.00	24.0
2	0	-9113	905	539	0	548	-1791	12.57	12.57	6.28	6.28	2	0.11	0.02	0.09	0.00	0.00	24.0
3	0	-9246	909	580	0	600	-1796	12.57	12.57	6.28	6.28	2	0.11	0.02	0.09	0.00	0.00	24.0
4	0	-9133	120	526	0	524	-289	12.57	12.57	6.28	6.28	2	0.04	0.01	0.05	0.00	0.00	24.0
5	0	-9266	123	566	0	576	-294	12.57	12.57	6.28	6.28	2	0.04	0.01	0.05	0.00	0.00	24.0
6	0	-8964	626	487	0	479	-1260	12.57	12.57	6.28	6.28	2	0.08	0.01	0.06	0.00	0.00	24.0
7	0	-9408	638	622	0	653	-1276	12.57	12.57	6.28	6.28	2	0.09	0.01	0.06	0.00	0.00	24.0
8	0	-8971	391	483	0	472	-809	12.57	12.57	6.28	6.28	2	0.06	0.01	0.04	0.00	0.00	24.0
9	0	-9415	402	618	0	646	-825	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
10	0	-9113	905	539	0	548	-1791	12.57	12.57	6.28	6.28	2	0.11	0.02	0.09	0.00	0.00	24.0
11	0	-9246	909	580	0	600	-1796	12.57	12.57	6.28	6.28	2	0.11	0.02	0.09	0.00	0.00	24.0
12	0	-9133	120	526	0	524	-289	12.57	12.57	6.28	6.28	2	0.04	0.01	0.05	0.00	0.00	24.0
13	0	-9266	123	566	0	576	-294	12.57	12.57	6.28	6.28	2	0.04	0.01	0.05	0.00	0.00	24.0
14	0	-8964	626	487	0	479	-1260	12.57	12.57	6.28	6.28	2	0.08	0.01	0.06	0.00	0.00	24.0
15	0	-9408	638	622	0	653	-1276	12.57	12.57	6.28	6.28	2	0.09	0.01	0.06	0.00	0.00	24.0
16	0	-8971	391	483	0	472	-809	12.57	12.57	6.28	6.28	2	0.06	0.01	0.04	0.00	0.00	24.0
17	0	-9415	402	618	0	646	-825	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
18	0	-12360	2609	820	0	876	-5012	12.57	12.57	6.28	6.28	3	0.19	0.05	0.25	0.00	0.00	24.0
19	0	-12410	-38	759	0	771	24	12.57	12.57	6.28	6.28	3	0.04	0.01	0.07	0.00	0.00	24.0
20	0	-12450	1202	749	0	742	-2338	12.57	12.57	6.28	6.28	3	0.09	0.02	0.12	0.00	0.00	24.0
37	0	-12100	3288	807	0	872	-6316	12.57	12.57	6.28	6.28	3	0.23	0.06	0.32	0.00	0.00	24.0
38	0	-12190	-1124	706	0	697	2078	12.57	12.57	6.28	6.28	3	0.08	0.02	0.11	0.00	0.00	24.0
39	0	-12240	942	690	0	649	-1859	12.57	12.57	6.28	6.28	3	0.08	0.02	0.09	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	97	-11188	668	718	0	31	-703	12.57	12.57	6.28	6.28	3	0.03	0.01	0.07	0.00	0.00	24.0
2	97	-8528	905	539	0	22	-908	12.57	12.57	6.28	6.28	2	0.05	0.02	0.09	0.00	0.00	24.0
3	97	-8661	909	580	0	35	-910	12.57	12.57	6.28	6.28	2	0.05	0.02	0.09	0.00	0.00	24.0
4	97	-8548	120	526	0	12	-172	12.57	12.57	6.28	6.28	2	0.01	0.01	0.05	0.00	0.00	24.0
5	97	-8681	123	566	0	25	-174	12.57	12.57	6.28	6.28	2	0.01	0.01	0.05	0.00	0.00	24.0
6	97	-8379	626	487	0	4	-649	12.57	12.57	6.28	6.28	2	0.03	0.01	0.06	0.00	0.00	24.0
7	97	-8823	638	622	0	46	-654	12.57	12.57	6.28	6.28	2	0.04	0.01	0.06	0.00	0.00	24.0
8	97	-8386	391	483	0	1	-428	12.57	12.57	6.28	6.28	2	0.02	0.01	0.04	0.00	0.00	24.0
9	97	-8830	402	618	0	43	-433	12.57	12.57	6.28	6.28	2	0.02	0.01	0.05	0.00	0.00	24.0

10	97	-8528	905	539	0	22	-908	12.57	12.57	6.28	6.28	2	0.05	0.02	0.09	0.00	0.00	24.0
11	97	-8661	909	580	0	35	-910	12.57	12.57	6.28	6.28	2	0.05	0.02	0.09	0.00	0.00	24.0
12	97	-8548	120	526	0	12	-172	12.57	12.57	6.28	6.28	2	0.01	0.01	0.05	0.00	0.00	24.0
13	97	-8681	123	566	0	25	-174	12.57	12.57	6.28	6.28	2	0.01	0.01	0.05	0.00	0.00	24.0
14	97	-8379	626	487	0	4	-649	12.57	12.57	6.28	6.28	2	0.03	0.01	0.06	0.00	0.00	24.0
15	97	-8823	638	622	0	46	-654	12.57	12.57	6.28	6.28	2	0.04	0.01	0.06	0.00	0.00	24.0
16	97	-8386	391	483	0	1	-428	12.57	12.57	6.28	6.28	2	0.02	0.01	0.04	0.00	0.00	24.0
17	97	-8830	402	618	0	43	-433	12.57	12.57	6.28	6.28	2	0.02	0.01	0.05	0.00	0.00	24.0
18	97	-11600	2609	820	0	76	-2468	12.57	12.57	6.28	6.28	3	0.09	0.05	0.25	0.00	0.00	24.0
19	97	-11651	-38	759	0	31	-14	12.57	12.57	6.28	6.28	3	0.00	0.01	0.07	0.00	0.00	24.0
20	97	-11688	1202	749	0	12	-1166	12.57	12.57	6.28	6.28	3	0.04	0.02	0.12	0.00	0.00	24.0
37	97	-11340	3288	807	0	85	-3110	12.57	12.57	6.28	6.28	3	0.11	0.06	0.32	0.00	0.00	24.0
38	97	-11428	-1124	706	0	9	982	12.57	12.57	6.28	6.28	3	0.04	0.02	0.11	0.00	0.00	24.0
39	97	-11479	942	690	0	-23	-940	12.57	12.57	6.28	6.28	3	0.03	0.02	0.09	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	195	-10427	668	718	0	-670	-51	12.57	12.57	6.28	6.28	3	0.04	0.01	0.07	0.00	0.00	24.0
2	195	-7943	905	539	0	-503	-26	12.57	12.57	6.28	6.28	2	0.03	0.02	0.09	0.00	0.00	24.0
3	195	-8076	909	580	0	-530	-24	12.57	12.57	6.28	6.28	2	0.03	0.02	0.09	0.00	0.00	24.0
4	195	-7963	120	526	0	-500	-55	12.57	12.57	6.28	6.28	2	0.03	0.01	0.05	0.00	0.00	24.0
5	195	-8096	123	566	0	-527	-54	12.57	12.57	6.28	6.28	2	0.03	0.01	0.05	0.00	0.00	24.0
6	195	-7794	626	487	0	-472	-38	12.57	12.57	6.28	6.28	2	0.03	0.01	0.06	0.00	0.00	24.0
7	195	-8238	638	622	0	-560	-33	12.57	12.57	6.28	6.28	2	0.03	0.01	0.06	0.00	0.00	24.0
8	195	-7801	391	483	0	-471	-47	12.57	12.57	6.28	6.28	2	0.03	0.01	0.05	0.00	0.00	24.0
9	195	-8245	402	618	0	-559	-41	12.57	12.57	6.28	6.28	2	0.03	0.01	0.06	0.00	0.00	24.0
10	195	-7943	905	539	0	-503	-26	12.57	12.57	6.28	6.28	2	0.03	0.02	0.09	0.00	0.00	24.0
11	195	-8076	909	580	0	-530	-24	12.57	12.57	6.28	6.28	2	0.03	0.02	0.09	0.00	0.00	24.0
12	195	-7963	120	526	0	-500	-55	12.57	12.57	6.28	6.28	2	0.03	0.01	0.05	0.00	0.00	24.0
13	195	-8096	123	566	0	-527	-54	12.57	12.57	6.28	6.28	2	0.03	0.01	0.05	0.00	0.00	24.0
14	195	-7794	626	487	0	-472	-38	12.57	12.57	6.28	6.28	2	0.03	0.01	0.06	0.00	0.00	24.0
15	195	-8238	638	622	0	-560	-33	12.57	12.57	6.28	6.28	2	0.03	0.01	0.06	0.00	0.00	24.0
16	195	-7801	391	483	0	-471	-47	12.57	12.57	6.28	6.28	2	0.03	0.01	0.05	0.00	0.00	24.0
17	195	-8245	402	618	0	-559	-41	12.57	12.57	6.28	6.28	2	0.03	0.01	0.06	0.00	0.00	24.0
18	195	-10840	2609	820	0	-723	76	12.57	12.57	6.28	6.28	3	0.04	0.05	0.26	0.00	0.00	24.0
19	195	-10892	-38	759	0	-709	-51	12.57	12.57	6.28	6.28	3	0.04	0.01	0.07	0.00	0.00	24.0
20	195	-10927	1202	749	0	-719	5	12.57	12.57	6.28	6.28	3	0.04	0.02	0.12	0.00	0.00	24.0
37	195	-10579	3288	807	0	-702	97	12.57	12.57	6.28	6.28	3	0.04	0.06	0.32	0.00	0.00	24.0
38	195	-10667	-1124	706	0	-679	-114	12.57	12.57	6.28	6.28	3	0.04	0.02	0.11	0.00	0.00	24.0
39	195	-10718	942	690	0	-696	-21	12.57	12.57	6.28	6.28	3	0.04	0.02	0.09	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	292	-9666	668	718	0	-1370	600	12.57	12.57	6.28	6.28	3	0.08	0.01	0.07	0.00	0.00	24.0
2	292	-7358	905	539	0	-1029	857	12.57	12.57	6.28	6.28	2	0.09	0.02	0.09	0.00	0.00	24.0
3	292	-7491	909	580	0	-1096	862	12.57	12.57	6.28	6.28	2	0.09	0.02	0.09	0.00	0.00	24.0
4	292	-7378	120	526	0	-1013	62	12.57	12.57	6.28	6.28	2	0.06	0.01	0.05	0.00	0.00	24.0
5	292	-7511	123	566	0	-1079	66	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
6	292	-7209	626	487	0	-947	573	12.57	12.57	6.28	6.28	2	0.07	0.01	0.06	0.00	0.00	24.0
7	292	-7653	638	622	0	-1167	589	12.57	12.57	6.28	6.28	2	0.09	0.01	0.07	0.00	0.00	24.0
8	292	-7216	391	483	0	-942	334	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
9	292	-7660	402	618	0	-1162	351	12.57	12.57	6.28	6.28	2	0.08	0.01	0.06	0.00	0.00	24.0
10	292	-7358	905	539	0	-1029	857	12.57	12.57	6.28	6.28	2	0.09	0.02	0.09	0.00	0.00	24.0
11	292	-7491	909	580	0	-1096	862	12.57	12.57	6.28	6.28	2	0.09	0.02	0.09	0.00	0.00	24.0
12	292	-7378	120	526	0	-1013	62	12.57	12.57	6.28	6.28	2	0.06	0.01	0.05	0.00	0.00	24.0
13	292	-7511	123	566	0	-1079	66	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
14	292	-7209	626	487	0	-947	573	12.57	12.57	6.28	6.28	2	0.07	0.01	0.06	0.00	0.00	24.0
15	292	-7653	638	622	0	-1167	589	12.57	12.57	6.28	6.28	2	0.09	0.01	0.07	0.00	0.00	24.0
16	292	-7216	391	483	0	-942	334	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
17	292	-7660	402	618	0	-1162	351	12.57	12.57	6.28	6.28	2	0.08	0.01	0.06	0.00	0.00	24.0
18	292	-10081	2609	820	0	-1522	2619	12.57	12.57	6.28	6.28	3	0.13	0.05	0.26	0.00	0.00	24.0
19	292	-10132	-38	759	0	-1449	-88	12.57	12.57	6.28	6.28	3	0.08	0.01	0.07	0.00	0.00	24.0
20	292	-10166	1202	749	0	-1449	1176	12.57	12.57	6.28	6.28	3	0.09	0.02	0.12	0.00	0.00	24.0
37	292	-9818	3288	807	0	-1489	3303	12.57	12.57	6.28	6.28	3	0.15	0.06	0.33	0.00	0.00	24.0
38	292	-9906	-1124	706	0	-1368	-1210	12.57	12.57	6.28	6.28	3	0.08	0.02	0.11	0.00	0.00	24.0
39	292	-9958	942	690	0	-1368	898	12.57	12.57	6.28	6.28	3	0.08	0.02	0.09	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	390	-8904	668	718	0	-2071	1252	12.57	12.57	6.28	6.28	3	0.12	0.01	0.07	0.00	0.00	24.0
2	390	-6773	905	539	0	-1555	1740	12.57	12.57	6.28	6.28	2	0.16	0.02	0.09	0.00	0.00	24.0
3	390	-6906	909	580	0	-1661	1748	12.57	12.57	6.28	6.28	2	0.16	0.02	0.09	0.00	0.00	24.0
4	390	-6793	120	526	0	-1525	178	12.57	12.57	6.28	6.28	2	0.10	0.01	0.05	0.00	0.00	24.0
5	390	-6926	123	566	0	-1631	186	12.57	12.57	6.28	6.28	2	0.10	0.01	0.06	0.00	0.00	24.0
6	390	-6624	626	487	0	-1422	1184	12.57	12.57	6.28	6.28	2	0.12	0.01	0.07	0.00	0.00	24.0
7	390	-7068	638	622	0	-1773	1211	12.57	12.57	6.28	6.28	2	0.14	0.01	0.07	0.00	0.00	24.0
8	390	-6631	391	483	0	-1413	715	12.57	12.57	6.28	6.28	2	0.11	0.01	0.05	0.00	0.00	24.0
9	390	-7075	402	618	0	-1764	742	12.57	12.57	6.28	6.28	2	0.13	0.01	0.06	0.00	0.00	24.0
10	390	-6773	905	539	0	-1555	1740	12.57	12.57	6.28	6.28	2	0.16	0.02	0.09	0.00	0.00	24.0
11	390	-6906	909	580	0	-1661	1748	12.57	12.57	6.28	6.28	2	0.16	0.02	0.09	0.00	0.00	24.0
12	390	-6793	120	526	0	-1525	178	12.57	12.57	6.28	6.28	2	0.10	0.01	0.05	0.00	0.00	24.0
13	390	-6926	123	566	0	-1631	186	12.57	12.57	6.28	6.28	2	0.10	0.01	0.06	0.00	0.00	24.0
14	390	-6624	626	487	0	-1422	1184	12.57	12.57	6.28	6.28	2	0.12	0.01	0.07	0.00	0.00	24.0
15	390	-7068	638	622	0	-1773	1211	12.57	12.57	6.28	6.28	2	0.14	0.01	0.07	0.00	0.00	24.0
16	390	-6631	391	483	0	-1413	715	12.57	12.57	6.28	6.28	2	0.11	0.01	0.05	0.00	0.00	24.0
17	390	-7075	402	618	0	-1764	742	12.57	12.57	6.28	6.28	2	0.13	0.01	0.06	0.00	0.00	24.0
18	390	-9321	2609	820	0	-2321	5163	12.57	12.57	6.28	6.28	3	0.23	0.05	0.26	0.00	0.00	24.0
19	390	-9373	-38	759	0	-2189	-126	12.57	12.57	6.28	6.28	3	0.12	0.01	0.07	0.00	0.00	24.0
20	390	-9404	1202	749	0	-2179	2348	12.57	12.57	6.28	6.28	3	0.14	0.02	0.12	0.00	0.00	24.0
37	390	-9058	3288	807	0	-2276	6509	12.57	12.57	6.28	6.28	3	0.27	0.06	0.33	0.00	0.00	24.0
38	390	-9144	-1124	706	0	-2056	-2306	12.57	12.57	6.28	6.28	3	0.13	0.02	0.11	0.00	0.00	24.0
39	390	-9197	942	690	0	-2040	1817	12.57	12.57	6.28	6.28	3	0.13	0.02	0.09	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

VERIFICA NODO IN TESTA AL PILASTRO, NODO NUM. 185 NON CONFINATO

(par.7.2.2 NTC2018 "La domanda di resistenza valutata con i criteri della progettazione in capacità può essere assunta non superiore alla domanda di resistenza valutata per il caso di comportamento strutturale non dissipativo.")

PROGETTAZIONE IN CAPACITA'

Asse loc. pilastro y nodo INTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 40.0 cm, hjc= 50.0 cm
Asse loc. pilastro z nodo ESTERNO: As2(inf)= 6.03, As1(sup)= 6.03, Hjw= 40.0 cm, bj= 60.0 cm, hjc= 30.0 cm

FxMin,inf	FxMin,sup	FxMax,sup	FySup	FzSup	Vjbdy	Vjbdz	Vres,y	Vres,z	I.R.compr.	Ashy	Ashz	PASSO	Nota
daN					daN		daN			cmq		cm	
-6624	1	-0	0	0	35233	26425	175015	126011	0.21	4.08	1.81	13.08	

VERIFICA DI RESISTENZA CON SOLLECITAZIONI COMPORTAMENTO NON DISSIPATIVO

Asse loc. pilastro y nodo INTERNO: Hjw= 40.0 cm, bj= 40.0 cm, hjc= 50.0 cm, db1= 45.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb,1	Mb,2	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m			daN			cmq	cm	
2	-0	-6773	-2057	-337	0	4247	175015	0.02	0.00	40.00	
3	-0	-6906	-2056	-329	0	4264	175015	0.02	0.00	40.00	
4	-0	-6793	-1197	-1227	0	74	175015	0.00	0.00	40.00	
5	-0	-6926	-1196	-1219	0	57	175015	0.00	0.00	40.00	
6	-0	-6624	-1757	-658	0	2715	175015	0.02	0.00	40.00	
7	-0	-7068	-1753	-631	0	2770	175015	0.02	0.00	40.00	
8	-0	-6631	-1499	-924	0	1419	175015	0.01	0.00	40.00	
9	-0	-7075	-1495	-898	0	1474	175015	0.01	0.00	40.00	
10	-0	-6773	-2057	-337	0	4247	175015	0.02	0.00	40.00	
11	-0	-6906	-2056	-329	0	4264	175015	0.02	0.00	40.00	
12	-0	-6793	-1197	-1227	0	74	175015	0.00	0.00	40.00	
13	-0	-6926	-1196	-1219	0	57	175015	0.00	0.00	40.00	
14	-0	-6624	-1757	-658	0	2715	175015	0.02	0.00	40.00	
15	-0	-7068	-1753	-631	0	2770	175015	0.02	0.00	40.00	
16	-0	-6631	-1499	-924	0	1419	175015	0.01	0.00	40.00	
17	-0	-7075	-1495	-898	0	1474	175015	0.01	0.00	40.00	

Asse loc. pilastro z nodo ESTERNO: Hjw= 40.0 cm, bj= 60.0 cm, hjc= 30.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb	Vb	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-0	-6773	-1618	4542	0	3995	126011	0.03	0.00	40.00	
3	-0	-6906	-1731	4679	0	4274	126011	0.03	0.00	40.00	
4	-0	-6793	-1588	4522	0	3921	126011	0.03	0.00	40.00	
5	-0	-6926	-1701	4659	0	4200	126011	0.03	0.00	40.00	
6	-0	-6624	-1476	4375	0	3644	126011	0.03	0.00	40.00	
7	-0	-7068	-1853	4832	0	4575	126011	0.04	0.00	40.00	
8	-0	-6631	-1466	4369	0	3620	126011	0.03	0.00	40.00	
9	-0	-7075	-1843	4826	0	4551	126011	0.04	0.00	40.00	
10	-0	-6773	-1618	4542	0	3995	126011	0.03	0.00	40.00	
11	-0	-6906	-1731	4679	0	4274	126011	0.03	0.00	40.00	
12	-0	-6793	-1588	4522	0	3921	126011	0.03	0.00	40.00	
13	-0	-6926	-1701	4659	0	4200	126011	0.03	0.00	40.00	
14	-0	-6624	-1476	4375	0	3644	126011	0.03	0.00	40.00	
15	-0	-7068	-1853	4832	0	4575	126011	0.04	0.00	40.00	
16	-0	-6631	-1466	4369	0	3620	126011	0.03	0.00	40.00	
17	-0	-7075	-1843	4826	0	4551	126011	0.04	0.00	40.00	

CONFRONTO E SINTESI CONCLUSIVE (si assume in ogni caso passo <= 15 cm)

I.R.compr.	Ashy	Ashz	PASSO	Nota
	cmq		cm	
0.04	--	--	15.00	**VERIFICATO**

ASTA NUM. 54 NI 167 NF 208 SEZ. Rp B= 0.400 H= 0.600 (pilastro)
PIL. NUM. 26C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-2268	2268	-671	0	1309	-2459	12.57	12.57	6.28	6.28	3	0.12	0.04	0.25	0.00	0.00	24.0
2	0	-1857	2062	-759	0	1029	-2211	12.57	12.57	6.28	6.28	2	0.16	0.04	0.23	0.00	0.00	24.0
3	0	-1718	2087	-380	0	1054	-2238	12.57	12.57	6.28	6.28	2	0.16	0.04	0.23	0.00	0.00	24.0
4	0	-1772	1402	-652	0	959	-1545	12.57	12.57	6.28	6.28	2	0.12	0.02	0.16	0.00	0.00	24.0
5	0	-1632	1428	-274	0	985	-1573	12.57	12.57	6.28	6.28	2	0.13	0.03	0.16	0.00	0.00	24.0
6	0	-1990	1801	-1164	0	975	-1946	12.57	12.57	6.28	6.28	2	0.15	0.03	0.20	0.00	0.00	24.0
7	0	-1524	1886	99	0	1059	-2037	12.57	12.57	6.28	6.28	2	0.15	0.03	0.21	0.00	0.00	24.0
8	0	-1965	1603	-1132	0	954	-1746	12.57	12.57	6.28	6.28	2	0.13	0.03	0.18	0.00	0.00	24.0
9	0	-1499	1688	131	0	1039	-1837	12.57	12.57	6.28	6.28	2	0.14	0.03	0.19	0.00	0.00	24.0
10	0	-1857	2062	-759	0	1029	-2211	12.57	12.57	6.28	6.28	2	0.16	0.04	0.23	0.00	0.00	24.0
11	0	-1718	2087	-380	0	1054	-2238	12.57	12.57	6.28	6.28	2	0.16	0.04	0.23	0.00	0.00	24.0
12	0	-1772	1402	-652	0	959	-1545	12.57	12.57	6.28	6.28	2	0.12	0.02	0.16	0.00	0.00	24.0
13	0	-1632	1428	-274	0	985	-1573	12.57	12.57	6.28	6.28	2	0.13	0.03	0.16	0.00	0.00	24.0
14	0	-1990	1801	-1164	0	975	-1946	12.57	12.57	6.28	6.28	2	0.15	0.03	0.20	0.00	0.00	24.0
15	0	-1524	1886	99	0	1059	-2037	12.57	12.57	6.28	6.28	2	0.15	0.03	0.21	0.00	0.00	24.0
16	0	-1965	1603	-1132	0	954	-1746	12.57	12.57	6.28	6.28	2	0.13	0.03	0.18	0.00	0.00	24.0
17	0	-1499	1688	131	0	1039	-1837	12.57	12.57	6.28	6.28	2	0.14	0.03	0.19	0.00	0.00	24.0
18	0	-3099	5715	-1844	0	1787	-5930	12.57	12.57	6.28	6.28	3	0.25	0.10	0.63	0.00	0.00	24.0
19	0	-2925	2992	-1624	0	1637	-3367	12.57	12.57	6.28	6.28	3	0.16	0.05	0.33	0.00	0.00	24.0
20	0	-2560	4130	-170	0	1890	-4406	12.57	12.57	6.28	6.28	3	0.20	0.07	0.46	0.00	0.00	24.0
37	0	-2912	5941	-1569	0	1701	-6069	12.57	12.57	6.28	6.28	3	0.26	0.10	0.65	0.00	0.00	24.0
38	0	-2623	1403	-1204	0	1449	-1797	12.57	12.57	6.28	6.28	3	0.10	0.02	0.16	0.00	0.00	24.0
39	0	-2014	3299	1219	0	1872	-3528	12.57	12.57	6.28	6.28	3	0.17	0.06	0.37	0.00	0.00	24.0
apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0																		
1	12	-2170	2268	-671	0	1393	-2175	12.57	12.57	6.28	6.28	3	0.11	0.04	0.25	0.00	0.00	24.0
2	12	-1782	2062	-759	0	1124	-1953	12.57	12.57	6.28	6.28	2	0.15	0.04	0.23	0.00	0.00	24.0
3	12	-1643	2087	-380	0	1102	-1977	12.57	12.57	6.28	6.28	2	0.15	0.04	0.23	0.00	0.00	24.0
4	12	-1697	1402	-652	0	1041	-1370	12.57	12.57	6.28	6.28	2	0.12	0.02	0.16	0.00	0.00	24.0
5	12	-1557	1428	-274	0	1019	-1394	12.57	12.57	6.28	6.28	2	0.12	0.03	0.16	0.00	0.00	24.0
6	12	-1915	1801	-1164	0	1120	-1721	12.57	12.57	6.28	6.28	2	0.14	0.03	0.20	0.00	0.00	24.0
7	12	-1449	1886	99	0	1047	-1801	12.57	12.57	6.28	6.28	2	0.14	0.03	0.21	0.00	0.00	24.0
8	12	-1890	1603	-1132	0	1096	-1546	12.57	12.57	6.28	6.28	2	0.13	0.03	0.18	0.00	0.00	24.0
9	12	-1424	1688	131	0	1023	-1626	12.57	12.57	6.28	6.28	2	0.13	0.03	0.19	0.00	0.00	24.0
10	12	-1782	2062	-759	0	1124	-1953	12.57	12.57	6.28	6.28	2	0.15	0.04	0.23	0.00	0.00	24.0
11	12	-1643	2087	-380	0	1102	-1977	12.57	12.57	6.28	6.28	2	0.15	0.04	0.23	0.00	0.00	24.0
12	12	-1697	1402	-652	0	1041	-1370	12.57	12.57	6.28	6.28	2	0.12	0.02	0.16	0.00	0.00	24.0
13	12	-1557	1428	-274	0	1019	-1394	12.57	12.57	6.28	6.28	2	0.12	0.03	0.16	0.00	0.00	24.0
14	12	-1915	1801	-1164	0	1120	-1721	12.57	12.57	6.28	6.28	2	0.14	0.03	0.20	0.00	0.00	24.0
15	12	-1449	1886	99	0	1047	-1801	12.57	12.57	6.28	6.28	2	0.14	0.03	0.21	0.00	0.00	24.0

16	12	-1890	1603	-1132	0	1096	-1546	12.57	12.57	6.28	6.28	2	0.13	0.03	0.18	0.00	0.00	24.0
17	12	-1424	1688	131	0	1023	-1626	12.57	12.57	6.28	6.28	2	0.13	0.03	0.19	0.00	0.00	24.0
18	12	-3002	5715	-1844	0	2018	-5216	12.57	12.57	6.28	6.28	3	0.23	0.10	0.63	0.00	0.00	24.0
19	12	-2828	2992	-1624	0	1840	-2993	12.57	12.57	6.28	6.28	3	0.15	0.05	0.33	0.00	0.00	24.0
20	12	-2462	4130	-170	0	1911	-3890	12.57	12.57	6.28	6.28	3	0.18	0.07	0.46	0.00	0.00	24.0
37	12	-2814	5941	-1569	0	1897	-5326	12.57	12.57	6.28	6.28	3	0.23	0.10	0.66	0.00	0.00	24.0
38	12	-2526	1403	-1204	0	1600	-1622	12.57	12.57	6.28	6.28	3	0.11	0.02	0.16	0.00	0.00	24.0
39	12	-1916	3299	1219	0	1720	-3116	12.57	12.57	6.28	6.28	3	0.15	0.06	0.37	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-2073	2268	-671	0	1477	-1892	12.57	12.57	6.28	6.28	3	0.11	0.04	0.25	0.00	0.00	24.0
2	25	-1707	2062	-759	0	1219	-1696	12.57	12.57	6.28	6.28	2	0.14	0.04	0.23	0.00	0.00	24.0
3	25	-1568	2087	-380	0	1149	-1716	12.57	12.57	6.28	6.28	2	0.14	0.04	0.23	0.00	0.00	24.0
4	25	-1622	1402	-652	0	1123	-1195	12.57	12.57	6.28	6.28	2	0.12	0.02	0.16	0.00	0.00	24.0
5	25	-1482	1428	-274	0	1053	-1216	12.57	12.57	6.28	6.28	2	0.11	0.03	0.16	0.00	0.00	24.0
6	25	-1840	1801	-1164	0	1266	-1496	12.57	12.57	6.28	6.28	2	0.14	0.03	0.20	0.00	0.00	24.0
7	25	-1374	1886	99	0	1034	-1565	12.57	12.57	6.28	6.28	2	0.13	0.03	0.21	0.00	0.00	24.0
8	25	-1815	1603	-1132	0	1237	-1345	12.57	12.57	6.28	6.28	2	0.13	0.03	0.18	0.00	0.00	24.0
9	25	-1349	1688	131	0	1006	-1415	12.57	12.57	6.28	6.28	2	0.12	0.03	0.19	0.00	0.00	24.0
10	25	-1707	2062	-759	0	1219	-1696	12.57	12.57	6.28	6.28	2	0.14	0.04	0.23	0.00	0.00	24.0
11	25	-1568	2087	-380	0	1149	-1716	12.57	12.57	6.28	6.28	2	0.14	0.04	0.23	0.00	0.00	24.0
12	25	-1622	1402	-652	0	1123	-1195	12.57	12.57	6.28	6.28	2	0.12	0.02	0.16	0.00	0.00	24.0
13	25	-1482	1428	-274	0	1053	-1216	12.57	12.57	6.28	6.28	2	0.11	0.03	0.16	0.00	0.00	24.0
14	25	-1840	1801	-1164	0	1266	-1496	12.57	12.57	6.28	6.28	2	0.14	0.03	0.20	0.00	0.00	24.0
15	25	-1374	1886	99	0	1034	-1565	12.57	12.57	6.28	6.28	2	0.13	0.03	0.21	0.00	0.00	24.0
16	25	-1815	1603	-1132	0	1237	-1345	12.57	12.57	6.28	6.28	2	0.13	0.03	0.18	0.00	0.00	24.0
17	25	-1349	1688	131	0	1006	-1415	12.57	12.57	6.28	6.28	2	0.12	0.03	0.19	0.00	0.00	24.0
18	25	-2904	5715	-1844	0	2248	-4501	12.57	12.57	6.28	6.28	3	0.21	0.10	0.63	0.00	0.00	24.0
19	25	-2730	2992	-1624	0	2043	-2619	12.57	12.57	6.28	6.28	3	0.15	0.05	0.33	0.00	0.00	24.0
20	25	-2365	4130	-170	0	1933	-3374	12.57	12.57	6.28	6.28	3	0.17	0.07	0.46	0.00	0.00	24.0
37	25	-2717	5941	-1569	0	2093	-4583	12.57	12.57	6.28	6.28	3	0.21	0.11	0.66	0.00	0.00	24.0
38	25	-2428	1403	-1204	0	1750	-1446	12.57	12.57	6.28	6.28	3	0.11	0.02	0.16	0.00	0.00	24.0
39	25	-1819	3299	1219	0	1567	-2703	12.57	12.57	6.28	6.28	3	0.14	0.06	0.37	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-1976	2268	-671	0	1560	-1609	12.57	12.57	6.28	6.28	3	0.10	0.04	0.25	0.00	0.00	24.0
2	38	-1632	2062	-759	0	1313	-1438	12.57	12.57	6.28	6.28	2	0.14	0.04	0.23	0.00	0.00	24.0
3	38	-1493	2087	-380	0	1196	-1455	12.57	12.57	6.28	6.28	2	0.13	0.04	0.23	0.00	0.00	24.0
4	38	-1547	1402	-652	0	1204	-1019	12.57	12.57	6.28	6.28	2	0.11	0.02	0.16	0.00	0.00	24.0
5	38	-1407	1428	-274	0	1088	-1037	12.57	12.57	6.28	6.28	2	0.11	0.03	0.16	0.00	0.00	24.0
6	38	-1765	1801	-1164	0	1412	-1270	12.57	12.57	6.28	6.28	2	0.13	0.03	0.20	0.00	0.00	24.0
7	38	-1299	1886	99	0	1022	-1330	12.57	12.57	6.28	6.28	2	0.12	0.03	0.21	0.00	0.00	24.0
8	38	-1740	1603	-1132	0	1379	-1145	12.57	12.57	6.28	6.28	2	0.13	0.03	0.18	0.00	0.00	24.0
9	38	-1274	1688	131	0	990	-1204	12.57	12.57	6.28	6.28	2	0.11	0.03	0.19	0.00	0.00	24.0
10	38	-1632	2062	-759	0	1313	-1438	12.57	12.57	6.28	6.28	2	0.14	0.04	0.23	0.00	0.00	24.0
11	38	-1493	2087	-380	0	1196	-1455	12.57	12.57	6.28	6.28	2	0.13	0.04	0.23	0.00	0.00	24.0
12	38	-1547	1402	-652	0	1204	-1019	12.57	12.57	6.28	6.28	2	0.11	0.02	0.16	0.00	0.00	24.0
13	38	-1407	1428	-274	0	1088	-1037	12.57	12.57	6.28	6.28	2	0.11	0.03	0.16	0.00	0.00	24.0
14	38	-1765	1801	-1164	0	1412	-1270	12.57	12.57	6.28	6.28	2	0.13	0.03	0.20	0.00	0.00	24.0
15	38	-1299	1886	99	0	1022	-1330	12.57	12.57	6.28	6.28	2	0.12	0.03	0.21	0.00	0.00	24.0
16	38	-1740	1603	-1132	0	1379	-1145	12.57	12.57	6.28	6.28	2	0.13	0.03	0.18	0.00	0.00	24.0
17	38	-1274	1688	131	0	990	-1204	12.57	12.57	6.28	6.28	2	0.11	0.03	0.19	0.00	0.00	24.0
18	38	-2806	5715	-1844	0	2478	-3786	12.57	12.57	6.28	6.28	3	0.20	0.10	0.63	0.00	0.00	24.0
19	38	-2632	2992	-1624	0	2246	-2245	12.57	12.57	6.28	6.28	3	0.15	0.05	0.33	0.00	0.00	24.0
20	38	-2268	4130	-170	0	1954	-2857	12.57	12.57	6.28	6.28	3	0.15	0.07	0.46	0.00	0.00	24.0
37	38	-2620	5941	-1569	0	2289	-3841	12.57	12.57	6.28	6.28	3	0.19	0.11	0.66	0.00	0.00	24.0
38	38	-2330	1403	-1204	0	1900	-1270	12.57	12.57	6.28	6.28	3	0.12	0.02	0.16	0.00	0.00	24.0
39	38	-1722	3299	1219	0	1414	-2291	12.57	12.57	6.28	6.28	3	0.12	0.06	0.37	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-1878	2268	-671	0	1644	-1325	12.57	12.57	6.28	6.28	3	0.11	0.04	0.25	0.00	0.00	24.0
2	50	-1557	2062	-759	0	1408	-1180	12.57	12.57	6.28	6.28	2	0.13	0.04	0.23	0.00	0.00	24.0
3	50	-1418	2087	-380	0	1244	-1194	12.57	12.57	6.28	6.28	2	0.12	0.04	0.24	0.00	0.00	24.0
4	50	-1472	1402	-652	0	1286	-844	12.57	12.57	6.28	6.28	2	0.11	0.02	0.16	0.00	0.00	24.0
5	50	-1332	1428	-274	0	1122	-859	12.57	12.57	6.28	6.28	2	0.10	0.03	0.16	0.00	0.00	24.0
6	50	-1690	1801	-1164	0	1557	-1045	12.57	12.57	6.28	6.28	2	0.13	0.03	0.20	0.00	0.00	24.0
7	50	-1224	1886	99	0	1010	-1094	12.57	12.57	6.28	6.28	2	0.11	0.03	0.21	0.00	0.00	24.0
8	50	-1665	1603	-1132	0	1520	-945	12.57	12.57	6.28	6.28	2	0.13	0.03	0.18	0.00	0.00	24.0
9	50	-1199	1688	131	0	973	-993	12.57	12.57	6.28	6.28	2	0.10	0.03	0.19	0.00	0.00	24.0
10	50	-1557	2062	-759	0	1408	-1180	12.57	12.57	6.28	6.28	2	0.13	0.04	0.23	0.00	0.00	24.0
11	50	-1418	2087	-380	0	1244	-1194	12.57	12.57	6.28	6.28	2	0.12	0.04	0.24	0.00	0.00	24.0
12	50	-1472	1402	-652	0	1286	-844	12.57	12.57	6.28	6.28	2	0.11	0.02	0.16	0.00	0.00	24.0
13	50	-1332	1428	-274	0	1122	-859	12.57	12.57	6.28	6.28	2	0.10	0.03	0.16	0.00	0.00	24.0
14	50	-1690	1801	-1164	0	1557	-1045	12.57	12.57	6.28	6.28	2	0.13	0.03	0.20	0.00	0.00	24.0
15	50	-1224	1886	99	0	1010	-1094	12.57	12.57	6.28	6.28	2	0.11	0.03	0.21	0.00	0.00	24.0
16	50	-1665	1603	-1132	0	1520	-945	12.57	12.57	6.28	6.28	2	0.13	0.03	0.18	0.00	0.00	24.0
17	50	-1199	1688	131	0	973	-993	12.57	12.57	6.28	6.28	2	0.10	0.03	0.19	0.00	0.00	24.0
18	50	-2709	5715	-1844	0	2709	-3072	12.57	12.57	6.28	6.28	3	0.19	0.10	0.63	0.00	0.00	24.0
19	50	-2535	2992	-1624	0	2449	-1871	12.57	12.57	6.28	6.28	3	0.16	0.05	0.33	0.00	0.00	24.0
20	50	-2170	4130	-170	0	1975	-2341	12.57	12.57	6.28	6.28	3	0.14	0.07	0.46	0.00	0.00	24.0
37	50	-2522	5941	-1569	0	2485	-3098	12.57	12.57	6.28	6.28	3	0.18	0.11	0.66	0.00	0.00	24.0
38	50	-2233	1403	-1204	0	2051	-1095	12.57	12.57	6.28	6.28	3	0.13	0.02	0.16	0.00	0.00	24.0
39	50	-1624	3299	1219	0	1262	-1879	12.57	12.57	6.28	6.28	3	0.10	0.06	0.37	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

VERIFICA NODO IN TESTA AL PILASTRO, NODO NUM. 208 NON CONFINATO

(par.7.2.2 NTC2018 "La domanda di resistenza valutata con i criteri della progettazione in capacità può essere assunta non superiore alla domanda di resistenza valutata per il caso di comportamento strutturale non dissipativo.")

PROGETTAZIONE IN CAPACITA'

Asse loc. pilastro y nodo: --

Asse loc. pilastro z nodo ESTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 50.0 cm, hjc= 30.0 cm

FxMin,inf	FxMin,sup	FxMax,sup	FySup	FzSup	Vjbdy	Vjbdz	Vres,y	Vres,z	I.R.compr.	Ashy	Ashz	PASSO	Nota
daN					daN		daN			cmq		cm	
-1199	1	-0	0	0	--	17616	--	105009	0.17	--	--	40.00	

VERIFICA DI RESISTENZA CON SOLLECITAZIONI COMPORTAMENTO NON DISSIPATIVO

Asse loc. pilastro z nodo ESTERNO: Hjw= 40.0 cm, bj= 50.0 cm, hjc= 30.0 cm, db1= 45.0 cm

NC	Fx,sup	Fx,inf	Mb	Vb	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota

	daN	daN*m		daN			cmq		cm
2	-0	-1557	-1408	1557	0	3477	105009	0.03	0.00	40.00
3	-0	-1418	-1244	1418	0	3072	105009	0.03	0.00	40.00
4	-0	-1472	-1286	1472	0	3175	105009	0.03	0.00	40.00
5	-0	-1332	-1122	1332	0	2770	105009	0.03	0.00	40.00
6	-0	-1690	-1557	1690	0	3844	105009	0.04	0.00	40.00
7	-0	-1224	-1010	1224	0	2494	105009	0.02	0.00	40.00
8	-0	-1665	-1520	1665	0	3753	105009	0.04	0.00	40.00
9	-0	-1199	-973	1199	0	2403	105009	0.02	0.00	40.00
10	-0	-1557	-1408	1557	0	3477	105009	0.03	0.00	40.00
11	-0	-1418	-1244	1418	0	3072	105009	0.03	0.00	40.00
12	-0	-1472	-1286	1472	0	3175	105009	0.03	0.00	40.00
13	-0	-1332	-1122	1332	0	2770	105009	0.03	0.00	40.00
14	-0	-1690	-1557	1690	0	3844	105009	0.04	0.00	40.00
15	-0	-1224	-1010	1224	0	2494	105009	0.02	0.00	40.00
16	-0	-1665	-1520	1665	0	3753	105009	0.04	0.00	40.00
17	-0	-1199	-973	1199	0	2403	105009	0.02	0.00	40.00

CONFRONTO E SINTESI CONCLUSIVE (si assume in ogni caso passo <= 15 cm)

I.R.compr.	Ashy	Ashz	PASSO	Nota
	cmq		cm	
0.04	--	--	15.00	**VERIFICATO**

ASTA NUM. 55 NI 122 NF 165 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 24B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-11440	1	-410	0	-809	132	6.28	6.28	9.42	9.42	3	0.04	0.01	0.05	0.00	0.00	24.0
2	0	-8824	50	-420	0	-824	-39	6.28	6.28	9.42	9.42	2	0.05	0.01	0.05	0.00	0.00	24.0
3	0	-8809	49	-275	0	-540	-38	6.28	6.28	9.42	9.42	2	0.03	0.01	0.03	0.00	0.00	24.0
4	0	-8784	-47	-356	0	-705	240	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
5	0	-8770	-48	-210	0	-421	242	6.28	6.28	9.42	9.42	2	0.04	0.00	0.03	0.00	0.00	24.0
6	0	-8828	17	-568	0	-1114	56	6.28	6.28	9.42	9.42	2	0.07	0.01	0.07	0.00	0.00	24.0
7	0	-8778	14	-82	0	-167	62	6.28	6.28	9.42	9.42	2	0.01	0.00	0.01	0.00	0.00	24.0
8	0	-8816	-12	-549	0	-1079	140	6.28	6.28	9.42	9.42	2	0.07	0.01	0.07	0.00	0.00	24.0
9	0	-8766	-15	-62	0	-131	146	6.28	6.28	9.42	9.42	2	0.02	0.00	0.01	0.00	0.00	24.0
10	0	-8824	50	-420	0	-824	-39	6.28	6.28	9.42	9.42	2	0.05	0.01	0.05	0.00	0.00	24.0
11	0	-8809	49	-275	0	-540	-38	6.28	6.28	9.42	9.42	2	0.03	0.01	0.03	0.00	0.00	24.0
12	0	-8784	-47	-356	0	-705	240	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
13	0	-8770	-48	-210	0	-421	242	6.28	6.28	9.42	9.42	2	0.04	0.00	0.03	0.00	0.00	24.0
14	0	-8828	17	-568	0	-1114	56	6.28	6.28	9.42	9.42	2	0.07	0.01	0.07	0.00	0.00	24.0
15	0	-8778	14	-82	0	-167	62	6.28	6.28	9.42	9.42	2	0.01	0.00	0.01	0.00	0.00	24.0
16	0	-8816	-12	-549	0	-1079	140	6.28	6.28	9.42	9.42	2	0.07	0.01	0.07	0.00	0.00	24.0
17	0	-8766	-15	-62	0	-131	146	6.28	6.28	9.42	9.42	2	0.02	0.00	0.01	0.00	0.00	24.0
18	0	-12390	130	-887	0	-1733	-229	6.28	6.28	9.42	9.42	3	0.08	0.02	0.10	0.00	0.00	24.0
19	0	-12290	-164	-650	0	-1285	610	6.28	6.28	9.42	9.42	3	0.08	0.01	0.07	0.00	0.00	24.0
20	0	-12310	-15	-384	0	-757	183	6.28	6.28	9.42	9.42	3	0.04	0.01	0.04	0.00	0.00	24.0
37	0	-11980	234	-850	0	-1655	-528	6.28	6.28	9.42	9.42	3	0.09	0.02	0.10	0.00	0.00	24.0
38	0	-11820	-257	-455	0	-909	870	6.28	6.28	9.42	9.42	3	0.09	0.01	0.05	0.00	0.00	24.0
39	0	-11850	-8	-12	0	-29	159	6.28	6.28	9.42	9.42	3	0.02	0.00	0.00	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	97	-10868	1	-410	0	-410	133	6.28	6.28	9.42	9.42	3	0.02	0.01	0.05	0.00	0.00	24.0
2	97	-8385	50	-420	0	-414	9	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
3	97	-8370	49	-275	0	-272	10	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
4	97	-8345	-47	-356	0	-358	194	6.28	6.28	9.42	9.42	2	0.04	0.01	0.04	0.00	0.00	24.0
5	97	-8331	-48	-210	0	-216	195	6.28	6.28	9.42	9.42	2	0.03	0.00	0.03	0.00	0.00	24.0
6	97	-8389	17	-568	0	-560	73	6.28	6.28	9.42	9.42	2	0.04	0.01	0.07	0.00	0.00	24.0
7	97	-8339	14	-82	0	-87	76	6.28	6.28	9.42	9.42	2	0.01	0.00	0.01	0.00	0.00	24.0
8	97	-8377	-12	-549	0	-544	128	6.28	6.28	9.42	9.42	2	0.04	0.01	0.07	0.00	0.00	24.0
9	97	-8327	-15	-62	0	-70	131	6.28	6.28	9.42	9.42	2	0.02	0.00	0.01	0.00	0.00	24.0
10	97	-8385	50	-420	0	-414	9	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
11	97	-8370	49	-275	0	-272	10	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
12	97	-8345	-47	-356	0	-358	194	6.28	6.28	9.42	9.42	2	0.04	0.01	0.04	0.00	0.00	24.0
13	97	-8331	-48	-210	0	-216	195	6.28	6.28	9.42	9.42	2	0.03	0.00	0.03	0.00	0.00	24.0
14	97	-8389	17	-568	0	-560	73	6.28	6.28	9.42	9.42	2	0.04	0.01	0.07	0.00	0.00	24.0
15	97	-8339	14	-82	0	-87	76	6.28	6.28	9.42	9.42	2	0.01	0.00	0.01	0.00	0.00	24.0
16	97	-8377	-12	-549	0	-544	128	6.28	6.28	9.42	9.42	2	0.04	0.01	0.07	0.00	0.00	24.0
17	97	-8327	-15	-62	0	-70	131	6.28	6.28	9.42	9.42	2	0.02	0.00	0.01	0.00	0.00	24.0
18	97	-11820	130	-887	0	-868	-102	6.28	6.28	9.42	9.42	3	0.04	0.02	0.10	0.00	0.00	24.0
19	97	-11720	-164	-650	0	-651	450	6.28	6.28	9.42	9.42	3	0.05	0.01	0.07	0.00	0.00	24.0
20	97	-11740	-15	-384	0	-382	168	6.28	6.28	9.42	9.42	3	0.02	0.01	0.04	0.00	0.00	24.0
37	97	-11411	234	-850	0	-826	-300	6.28	6.28	9.42	9.42	3	0.05	0.02	0.10	0.00	0.00	24.0
38	97	-11250	-257	-455	0	-465	620	6.28	6.28	9.42	9.42	3	0.06	0.01	0.05	0.00	0.00	24.0
39	97	-11280	-8	-12	0	-17	151	6.28	6.28	9.42	9.42	3	0.02	0.00	0.00	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	195	-10297	1	-410	0	-10	134	6.28	6.28	9.42	9.42	3	0.01	0.01	0.05	0.00	0.00	24.0
2	195	-7946	50	-420	0	-4	58	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
3	195	-7932	49	-275	0	-4	58	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
4	195	-7906	-47	-356	0	-12	148	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
5	195	-7892	-48	-210	0	-12	148	6.28	6.28	9.42	9.42	2	0.02	0.00	0.03	0.00	0.00	24.0
6	195	-7950	17	-568	0	-7	89	6.28	6.28	9.42	9.42	2	0.01	0.01	0.07	0.00	0.00	24.0
7	195	-7900	14	-82	0	-7	90	6.28	6.28	9.42	9.42	2	0.01	0.00	0.01	0.00	0.00	24.0
8	195	-7938	-12	-549	0	-9	116	6.28	6.28	9.42	9.42	2	0.01	0.01	0.07	0.00	0.00	24.0
9	195	-7888	-15	-62	0	-10	117	6.28	6.28	9.42	9.42	2	0.01	0.00	0.01	0.00	0.00	24.0
10	195	-7946	50	-420	0	-4	58	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
11	195	-7932	49	-275	0	-4	58	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
12	195	-7906	-47	-356	0	-12	148	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
13	195	-7892	-48	-210	0	-12	148	6.28	6.28	9.42	9.42	2	0.02	0.00	0.03	0.00	0.00	24.0
14	195	-7950	17	-568	0	-7	89	6.28	6.28	9.42	9.42	2	0.01	0.01	0.07	0.00	0.00	24.0
15	195	-7900	14	-82	0	-7	90	6.28	6.28	9.42	9.42	2	0.01	0.00	0.01	0.00	0.00	24.0
16	195	-7938	-12	-549	0	-9	116	6.28	6.28	9.42	9.42	2	0.01	0.01	0.07	0.00	0.00	24.0
17	195	-7888	-15	-62	0	-10	117	6.28	6.28	9.42	9.42	2	0.01	0.00	0.01	0.00	0.00	24.0
18	195	-11250	130	-887	0	-3	25	6.28	6.28	9.42	9.42	3	0.00	0.02	0.10	0.00	0.00	24.0
19	195	-11150	-164	-650	0	-17	289	6.28	6.28	9.42	9.42	3	0.03	0.01	0.07	0.00	0.00	24.0

20	195	-11170	-15	-384	0	-7	153	6.28	6.28	9.42	9.42	3	0.02	0.01	0.04	0.00	0.00	24.0
37	195	-10842	234	-850	0	3	-71	6.28	6.28	9.42	9.42	3	0.01	0.02	0.10	0.00	0.00	24.0
38	195	-10680	-257	-455	0	-21	370	6.28	6.28	9.42	9.42	3	0.04	0.01	0.05	0.00	0.00	24.0
39	195	-10711	-8	-12	0	-5	143	6.28	6.28	9.42	9.42	3	0.01	0.00	0.00	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	292	-9726	1	-410	0	389	135	6.28	6.28	9.42	9.42	3	0.02	0.01	0.05	0.00	0.00	24.0
2	292	-7508	50	-420	0	406	106	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
3	292	-7493	49	-275	0	263	106	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
4	292	-7468	-47	-356	0	335	102	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
5	292	-7454	-48	-210	0	193	101	6.28	6.28	9.42	9.42	2	0.02	0.00	0.03	0.00	0.00	24.0
6	292	-7512	17	-568	0	547	105	6.28	6.28	9.42	9.42	2	0.04	0.01	0.07	0.00	0.00	24.0
7	292	-7462	14	-82	0	73	103	6.28	6.28	9.42	9.42	2	0.01	0.00	0.01	0.00	0.00	24.0
8	292	-7500	-12	-549	0	526	104	6.28	6.28	9.42	9.42	2	0.04	0.01	0.07	0.00	0.00	24.0
9	292	-7450	-15	-62	0	51	102	6.28	6.28	9.42	9.42	2	0.01	0.00	0.01	0.00	0.00	24.0
10	292	-7508	50	-420	0	406	106	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
11	292	-7493	49	-275	0	263	106	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
12	292	-7468	-47	-356	0	335	102	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
13	292	-7454	-48	-210	0	193	101	6.28	6.28	9.42	9.42	2	0.02	0.00	0.03	0.00	0.00	24.0
14	292	-7512	17	-568	0	547	105	6.28	6.28	9.42	9.42	2	0.04	0.01	0.07	0.00	0.00	24.0
15	292	-7462	14	-82	0	73	103	6.28	6.28	9.42	9.42	2	0.01	0.00	0.01	0.00	0.00	24.0
16	292	-7500	-12	-549	0	526	104	6.28	6.28	9.42	9.42	2	0.04	0.01	0.07	0.00	0.00	24.0
17	292	-7450	-15	-62	0	51	102	6.28	6.28	9.42	9.42	2	0.01	0.00	0.01	0.00	0.00	24.0
18	292	-10680	130	-887	0	863	151	6.28	6.28	9.42	9.42	3	0.04	0.02	0.10	0.00	0.00	24.0
19	292	-10580	-164	-650	0	617	129	6.28	6.28	9.42	9.42	3	0.03	0.01	0.08	0.00	0.00	24.0
20	292	-10600	-15	-384	0	368	138	6.28	6.28	9.42	9.42	3	0.02	0.01	0.04	0.00	0.00	24.0
37	292	-10272	234	-850	0	832	157	6.28	6.28	9.42	9.42	3	0.04	0.02	0.10	0.00	0.00	24.0
38	292	-10109	-257	-455	0	423	120	6.28	6.28	9.42	9.42	3	0.02	0.01	0.05	0.00	0.00	24.0
39	292	-10142	-8	-12	0	7	135	6.28	6.28	9.42	9.42	3	0.01	0.00	0.00	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	390	-9154	1	-410	0	789	136	6.28	6.28	9.42	9.42	3	0.04	0.01	0.05	0.00	0.00	24.0
2	390	-7069	50	-420	0	816	155	6.28	6.28	9.42	9.42	2	0.06	0.01	0.05	0.00	0.00	24.0
3	390	-7054	49	-275	0	531	153	6.28	6.28	9.42	9.42	2	0.04	0.01	0.03	0.00	0.00	24.0
4	390	-7029	-47	-356	0	682	56	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
5	390	-7015	-48	-210	0	397	55	6.28	6.28	9.42	9.42	2	0.03	0.00	0.03	0.00	0.00	24.0
6	390	-7073	17	-568	0	1101	122	6.28	6.28	9.42	9.42	2	0.08	0.01	0.07	0.00	0.00	24.0
7	390	-7023	14	-82	0	152	117	6.28	6.28	9.42	9.42	2	0.02	0.00	0.01	0.00	0.00	24.0
8	390	-7061	-12	-549	0	1061	92	6.28	6.28	9.42	9.42	2	0.07	0.01	0.07	0.00	0.00	24.0
9	390	-7011	-15	-62	0	112	88	6.28	6.28	9.42	9.42	2	0.01	0.00	0.01	0.00	0.00	24.0
10	390	-7069	50	-420	0	816	155	6.28	6.28	9.42	9.42	2	0.06	0.01	0.05	0.00	0.00	24.0
11	390	-7054	49	-275	0	531	153	6.28	6.28	9.42	9.42	2	0.04	0.01	0.03	0.00	0.00	24.0
12	390	-7029	-47	-356	0	682	56	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
13	390	-7015	-48	-210	0	397	55	6.28	6.28	9.42	9.42	2	0.03	0.00	0.03	0.00	0.00	24.0
14	390	-7073	17	-568	0	1101	122	6.28	6.28	9.42	9.42	2	0.08	0.01	0.07	0.00	0.00	24.0
15	390	-7023	14	-82	0	152	117	6.28	6.28	9.42	9.42	2	0.02	0.00	0.01	0.00	0.00	24.0
16	390	-7061	-12	-549	0	1061	92	6.28	6.28	9.42	9.42	2	0.07	0.01	0.07	0.00	0.00	24.0
17	390	-7011	-15	-62	0	112	88	6.28	6.28	9.42	9.42	2	0.01	0.00	0.01	0.00	0.00	24.0
18	390	-10110	130	-887	0	1728	278	6.28	6.28	9.42	9.42	3	0.08	0.02	0.10	0.00	0.00	24.0
19	390	-10010	-164	-650	0	1251	-31	6.28	6.28	9.42	9.42	3	0.06	0.01	0.08	0.00	0.00	24.0
20	390	-10030	-15	-384	0	742	123	6.28	6.28	9.42	9.42	3	0.04	0.01	0.05	0.00	0.00	24.0
37	390	-9703	234	-850	0	1661	385	6.28	6.28	9.42	9.42	3	0.09	0.02	0.10	0.00	0.00	24.0
38	390	-9539	-257	-455	0	867	-130	6.28	6.28	9.42	9.42	3	0.04	0.01	0.05	0.00	0.00	24.0
39	390	-9572	-8	-12	0	19	126	6.28	6.28	9.42	9.42	3	0.01	0.00	0.00	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

VERIFICA NODO IN TESTA AL PILASTRO, NODO NUM. 165 NON CONFINATO

(par.7.2.2 NTC2018 "La domanda di resistenza valutata con i criteri della progettazione in capacità può essere assunta non superiore alla domanda di resistenza valutata per il caso di comportamento strutturale non dissipativo.")

PROGETTAZIONE IN CAPACITA'

Asse loc. pilastro y nodo: --

Asse loc. pilastro z nodo INTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 30.0 cm, hjc= 50.0 cm

FxMin,inf	FxMin,sup	FxMax,sup	FySup	FzSup	Vjbdy	Vjbdz	Vres,y	Vres,z	I.R.compr.	Ashy	Ashz	PASSO	Nota
daN					daN		daN			cmq		cm	
-7011	1	-0	0	0	--	35233	--	131261	0.27	--	8.55	5.33	

VERIFICA DI RESISTENZA CON SOLLECITAZIONI COMPORTAMENTO NON DISSIPATIVO

Asse loc. pilastro z nodo INTERNO: Hjw= 40.0 cm, bj= 30.0 cm, hjc= 50.0 cm, db1= 45.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb,1	Mb,2	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-0	-7069	-2799	-1984	0	2012	131261	0.02	0.00	40.00	
3	-0	-7054	-2645	-2114	0	1311	131261	0.01	0.00	40.00	
4	-0	-7029	-2695	-2013	0	1684	131261	0.01	0.00	40.00	
5	-0	-7015	-2541	-2144	0	980	131261	0.01	0.00	40.00	
6	-0	-7073	-2943	-1842	0	2719	131261	0.02	0.00	40.00	
7	-0	-7023	-2429	-2277	0	375	131261	0.00	0.00	40.00	
8	-0	-7061	-2912	-1851	0	2620	131261	0.02	0.00	40.00	
9	-0	-7011	-2398	-2285	0	279	131261	0.00	0.00	40.00	
10	-0	-7069	-2799	-1984	0	2012	131261	0.02	0.00	40.00	
11	-0	-7054	-2645	-2114	0	1311	131261	0.01	0.00	40.00	
12	-0	-7029	-2695	-2013	0	1684	131261	0.01	0.00	40.00	
13	-0	-7015	-2541	-2144	0	980	131261	0.01	0.00	40.00	
14	-0	-7073	-2943	-1842	0	2719	131261	0.02	0.00	40.00	
15	-0	-7023	-2429	-2277	0	375	131261	0.00	0.00	40.00	
16	-0	-7061	-2912	-1851	0	2620	131261	0.02	0.00	40.00	
17	-0	-7011	-2398	-2285	0	279	131261	0.00	0.00	40.00	

CONFRONTO E SINTESI CONCLUSIVE (si assume in ogni caso passo <= 15 cm)

I.R.compr.	Ashy	Ashz	PASSO	Nota
	cmq		cm	
0.02	--	--	15.00	**VERIFICATO**

ASTA NUM. 56 NI 209 NF 210 SEZ. Rp B= 0.600 H= 0.300 (pilastro)

PIL. NUM. 23B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-7554	114	-861	0	-1182	-53	6.28	6.28	9.42	9.42	3	0.06	0.02	0.11	0.00	0.00	24.0
2	0	-5899	117	-731	0	-1064	-105	6.28	6.28	9.42	9.42	2	0.07	0.02	0.09	0.00	0.00	24.0
3	0	-5822	120	-628	0	-832	-111	6.28	6.28	9.42	9.42	2	0.06	0.01	0.08	0.00	0.00	24.0
4	0	-5800	55	-697	0	-986	30	6.28	6.28	9.42	9.42	2	0.06	0.02	0.09	0.00	0.00	24.0
5	0	-5723	58	-594	0	-754	24	6.28	6.28	9.42	9.42	2	0.05	0.01	0.07	0.00	0.00	24.0
6	0	-5954	92	-839	0	-1307	-51	6.28	6.28	9.42	9.42	2	0.09	0.02	0.11	0.00	0.00	24.0
7	0	-5697	102	-496	0	-535	-71	6.28	6.28	9.42	9.42	2	0.04	0.01	0.06	0.00	0.00	24.0
8	0	-5924	74	-829	0	-1284	-10	6.28	6.28	9.42	9.42	2	0.08	0.02	0.10	0.00	0.00	24.0
9	0	-5667	83	-486	0	-511	-30	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
10	0	-5899	117	-731	0	-1064	-105	6.28	6.28	9.42	9.42	2	0.07	0.02	0.09	0.00	0.00	24.0
11	0	-5822	120	-628	0	-832	-111	6.28	6.28	9.42	9.42	2	0.06	0.01	0.08	0.00	0.00	24.0
12	0	-5800	55	-697	0	-986	30	6.28	6.28	9.42	9.42	2	0.06	0.02	0.09	0.00	0.00	24.0
13	0	-5723	58	-594	0	-754	24	6.28	6.28	9.42	9.42	2	0.05	0.01	0.07	0.00	0.00	24.0
14	0	-5954	92	-839	0	-1307	-51	6.28	6.28	9.42	9.42	2	0.09	0.02	0.11	0.00	0.00	24.0
15	0	-5697	102	-496	0	-535	-71	6.28	6.28	9.42	9.42	2	0.04	0.01	0.06	0.00	0.00	24.0
16	0	-5924	74	-829	0	-1284	-10	6.28	6.28	9.42	9.42	2	0.08	0.02	0.10	0.00	0.00	24.0
17	0	-5667	83	-486	0	-511	-30	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
18	0	-8255	190	-1227	0	-1936	-219	6.28	6.28	9.42	9.42	3	0.09	0.03	0.15	0.00	0.00	24.0
19	0	-7930	10	-1088	0	-1620	175	6.28	6.28	9.42	9.42	3	0.08	0.03	0.13	0.00	0.00	24.0
20	0	-7895	114	-882	0	-1163	-50	6.28	6.28	9.42	9.42	3	0.06	0.02	0.11	0.00	0.00	24.0
37	0	-8123	254	-1167	0	-1836	-360	6.28	6.28	9.42	9.42	3	0.09	0.03	0.14	0.00	0.00	24.0
38	0	-7581	-45	-935	0	-1309	295	6.28	6.28	9.42	9.42	3	0.07	0.02	0.11	0.00	0.00	24.0
39	0	-7524	128	-592	0	-547	-80	6.28	6.28	9.42	9.42	3	0.03	0.01	0.07	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	97	-6984	114	-861	0	-342	58	6.28	6.28	9.42	9.42	3	0.02	0.02	0.11	0.00	0.00	24.0
2	97	-5460	117	-731	0	-351	9	6.28	6.28	9.42	9.42	2	0.02	0.02	0.09	0.00	0.00	24.0
3	97	-5383	120	-628	0	-220	6	6.28	6.28	9.42	9.42	2	0.01	0.01	0.08	0.00	0.00	24.0
4	97	-5361	55	-697	0	-306	84	6.28	6.28	9.42	9.42	2	0.02	0.02	0.09	0.00	0.00	24.0
5	97	-5284	58	-594	0	-175	81	6.28	6.28	9.42	9.42	2	0.02	0.01	0.08	0.00	0.00	24.0
6	97	-5515	92	-839	0	-489	39	6.28	6.28	9.42	9.42	2	0.03	0.02	0.11	0.00	0.00	24.0
7	97	-5258	102	-496	0	-51	28	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
8	97	-5485	74	-829	0	-476	62	6.28	6.28	9.42	9.42	2	0.03	0.02	0.10	0.00	0.00	24.0
9	97	-5228	83	-486	0	-37	51	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
10	97	-5460	117	-731	0	-351	9	6.28	6.28	9.42	9.42	2	0.02	0.02	0.09	0.00	0.00	24.0
11	97	-5383	120	-628	0	-220	6	6.28	6.28	9.42	9.42	2	0.01	0.01	0.08	0.00	0.00	24.0
12	97	-5361	55	-697	0	-306	84	6.28	6.28	9.42	9.42	2	0.02	0.02	0.09	0.00	0.00	24.0
13	97	-5284	58	-594	0	-175	81	6.28	6.28	9.42	9.42	2	0.02	0.01	0.08	0.00	0.00	24.0
14	97	-5515	92	-839	0	-489	39	6.28	6.28	9.42	9.42	2	0.03	0.02	0.11	0.00	0.00	24.0
15	97	-5258	102	-496	0	-51	28	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
16	97	-5485	74	-829	0	-476	62	6.28	6.28	9.42	9.42	2	0.03	0.02	0.10	0.00	0.00	24.0
17	97	-5228	83	-486	0	-37	51	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
18	97	-7684	190	-1227	0	-740	-33	6.28	6.28	9.42	9.42	3	0.04	0.03	0.15	0.00	0.00	24.0
19	97	-7360	10	-1088	0	-559	185	6.28	6.28	9.42	9.42	3	0.03	0.03	0.13	0.00	0.00	24.0
20	97	-7325	114	-882	0	-302	61	6.28	6.28	9.42	9.42	3	0.02	0.02	0.11	0.00	0.00	24.0
37	97	-7552	254	-1167	0	-699	-112	6.28	6.28	9.42	9.42	3	0.03	0.03	0.14	0.00	0.00	24.0
38	97	-7011	-45	-935	0	-398	251	6.28	6.28	9.42	9.42	3	0.03	0.02	0.12	0.00	0.00	24.0
39	97	-6954	128	-592	0	30	44	6.28	6.28	9.42	9.42	3	0.00	0.01	0.07	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	195	-6413	114	-861	0	498	169	6.28	6.28	9.42	9.42	3	0.03	0.02	0.11	0.00	0.00	24.0
2	195	-5022	117	-731	0	362	123	6.28	6.28	9.42	9.42	2	0.03	0.02	0.09	0.00	0.00	24.0
3	195	-4944	120	-628	0	392	123	6.28	6.28	9.42	9.42	2	0.03	0.01	0.08	0.00	0.00	24.0
4	195	-4922	55	-697	0	373	138	6.28	6.28	9.42	9.42	2	0.03	0.02	0.09	0.00	0.00	24.0
5	195	-4846	58	-594	0	404	137	6.28	6.28	9.42	9.42	2	0.04	0.01	0.08	0.00	0.00	24.0
6	195	-5076	92	-839	0	329	129	6.28	6.28	9.42	9.42	2	0.03	0.02	0.11	0.00	0.00	24.0
7	195	-4820	102	-496	0	433	127	6.28	6.28	9.42	9.42	2	0.04	0.01	0.06	0.00	0.00	24.0
8	195	-5046	74	-829	0	332	133	6.28	6.28	9.42	9.42	2	0.03	0.02	0.11	0.00	0.00	24.0
9	195	-4790	83	-486	0	436	132	6.28	6.28	9.42	9.42	2	0.04	0.01	0.06	0.00	0.00	24.0
10	195	-5022	117	-731	0	362	123	6.28	6.28	9.42	9.42	2	0.03	0.02	0.09	0.00	0.00	24.0
11	195	-4944	120	-628	0	392	123	6.28	6.28	9.42	9.42	2	0.03	0.01	0.08	0.00	0.00	24.0
12	195	-4922	55	-697	0	373	138	6.28	6.28	9.42	9.42	2	0.03	0.02	0.09	0.00	0.00	24.0
13	195	-4846	58	-594	0	404	137	6.28	6.28	9.42	9.42	2	0.04	0.01	0.08	0.00	0.00	24.0
14	195	-5076	92	-839	0	329	129	6.28	6.28	9.42	9.42	2	0.03	0.02	0.11	0.00	0.00	24.0
15	195	-4820	102	-496	0	433	127	6.28	6.28	9.42	9.42	2	0.04	0.01	0.06	0.00	0.00	24.0
16	195	-5046	74	-829	0	332	133	6.28	6.28	9.42	9.42	2	0.03	0.02	0.11	0.00	0.00	24.0
17	195	-4790	83	-486	0	436	132	6.28	6.28	9.42	9.42	2	0.04	0.01	0.06	0.00	0.00	24.0
18	195	-7114	190	-1227	0	457	152	6.28	6.28	9.42	9.42	3	0.03	0.03	0.15	0.00	0.00	24.0
19	195	-6789	10	-1088	0	502	195	6.28	6.28	9.42	9.42	3	0.03	0.03	0.13	0.00	0.00	24.0
20	195	-6754	114	-882	0	558	171	6.28	6.28	9.42	9.42	3	0.03	0.02	0.11	0.00	0.00	24.0
37	195	-6982	254	-1167	0	439	136	6.28	6.28	9.42	9.42	3	0.03	0.03	0.14	0.00	0.00	24.0
38	195	-6440	-45	-935	0	514	208	6.28	6.28	9.42	9.42	3	0.03	0.02	0.12	0.00	0.00	24.0
39	195	-6383	128	-592	0	607	169	6.28	6.28	9.42	9.42	3	0.03	0.01	0.07	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	292	-5842	114	-861	0	1337	280	6.28	6.28	9.42	9.42	3	0.07	0.02	0.11	0.00	0.00	24.0
2	292	-4583	117	-731	0	1074	237	6.28	6.28	9.42	9.42	2	0.08	0.02	0.09	0.00	0.00	24.0
3	292	-4506	120	-628	0	1005	239	6.28	6.28	9.42	9.42	2	0.08	0.01	0.08	0.00	0.00	24.0
4	292	-4484	55	-697	0	1053	192	6.28	6.28	9.42	9.42	2	0.08	0.02	0.09	0.00	0.00	24.0
5	292	-4407	58	-594	0	984	194	6.28	6.28	9.42	9.42	2	0.08	0.01	0.08	0.00	0.00	24.0
6	292	-4638	92	-839	0	1148	219	6.28	6.28	9.42	9.42	2	0.09	0.02	0.11	0.00	0.00	24.0
7	292	-4381	102	-496	0	916	226	6.28	6.28	9.42	9.42	2	0.07	0.01	0.06	0.00	0.00	24.0
8	292	-4608	74	-829	0	1141	205	6.28	6.28	9.42	9.42	2	0.09	0.02	0.11	0.00	0.00	24.0
9	292	-4351	83	-486	0	910	212	6.28	6.28	9.42	9.42	2	0.07	0.01	0.06	0.00	0.00	24.0
10	292	-4583	117	-731	0	1074	237	6.28	6.28	9.42	9.42	2	0.08	0.02	0.09	0.00	0.00	24.0
11	292	-4506	120	-628	0	1005	239	6.28	6.28	9.42	9.42	2	0.08	0.01	0.08	0.00	0.00	24.0
12	292	-4484	55	-697	0	1053	192	6.28	6.28	9.42	9.42	2	0.08	0.02	0.09	0.00	0.00	24.0
13	292	-4407	58	-594	0	984	194	6.28	6.28	9.42	9.42	2	0.08	0.01	0.08	0.00	0.00	24.0
14	292	-4638	92	-839	0	1148	219	6.28	6.28	9.42	9.42	2	0.09	0.02	0.11	0.00	0.00	24.0
15	292	-4381	102	-496	0	916	226	6.28	6.28	9.42	9.42	2	0.07	0.01	0.06	0.00	0.00	24.0
16	292	-4608	74	-829	0	1141	205	6.28	6.28	9.42	9.42	2	0.09	0.02	0.11	0.00	0.00	24.0
17	292	-4351	83	-486	0	910	212	6.28	6.28	9.42	9.42	2	0.07	0.01	0.06	0.00	0.00	24.0
18	292	-6544	190	-1227	0	1654	337	6.28	6.28	9.42	9.42	3	0.09	0.03	0.15	0.00	0.00	24.0
19	292	-6218	10	-1088	0	1564	205	6.28	6.28	9.42	9.42	3	0.08	0.03	0.14	0.00	0.00	24.0
20	292	-6184	114	-882	0	1418	282	6.28	6.28	9.42	9.42	3	0.07	0.02	0.11	0.00	0.00	24.0
37	292	-6412	254	-1167	0	1576	384	6.28	6.28	9.42	9.42	3	0.09	0.03	0.15	0.00	0.00	24.0
38	292	-5870	-45	-935	0	1426	164	6.28	6.28	9.42	9.42	3	0.07	0.02	0.12	0.00	0.00	24.0
39	292	-5812	128	-592	0	1183	293	6.28	6.28	9.42	9.42	3	0.06	0.01	0.07	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	390	-5272	114	-861	0	2177	391	6.28	6.28	9.42	9.42	3	0.11	0.02	0.11	0.00	0.00	24.0
2	390	-4144	117	-731	0	1787	351	6.28	6.28	9.42	9.42	2	0.14	0.02	0.09	0.00	0.00	24.0
3	390	-4067	120	-628	0	1617	356	6.28	6.28	9.42	9.42	2	0.13	0.01	0.08	0.00	0.00	24.0
4	390	-4045	55	-697	0	1733	245	6.28	6.28	9.42	9.42	2	0.13	0.02	0.09	0.00	0.00	24.0
5	390	-3968	58	-594	0	1563	250	6.28	6.28	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
6	390	-4199	92	-839	0	1966	308	6.28	6.28	9.42	9.42	2	0.15	0.02	0.11	0.00	0.00	24.0
7	390	-3942	102	-496	0	1400	325	6.28	6.28	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
8	390	-4169	74	-829	0	1949	277	6.28	6.28	9.42	9.42	2	0.14	0.02	0.11	0.00	0.00	24.0
9	390	-3912	83	-486	0	1384	293	6.28	6.28	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
10	390	-4144	117	-731	0	1787	351	6.28	6.28	9.42	9.42	2	0.14	0.02	0.09	0.00	0.00	24.0
11	390	-4067	120	-628	0	1617	356	6.28	6.28	9.42	9.42	2	0.13	0.01	0.08	0.00	0.00	24.0
12	390	-4045	55	-697	0	1733	245	6.28	6.28	9.42	9.42	2	0.13	0.02	0.09	0.00	0.00	24.0
13	390	-3968	58	-594	0	1563	250	6.28	6.28	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
14	390	-4199	92	-839	0	1966	308	6.28	6.28	9.42	9.42	2	0.15	0.02	0.11	0.00	0.00	24.0
15	390	-3942	102	-496	0	1400	325	6.28	6.28	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
16	390	-4169	74	-829	0	1949	277	6.28	6.28	9.42	9.42	2	0.14	0.02	0.11	0.00	0.00	24.0
17	390	-3912	83	-486	0	1384	293	6.28	6.28	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
18	390	-5973	190	-1227	0	2850	522	6.28	6.28	9.42	9.42	3	0.15	0.03	0.15	0.00	0.00	24.0
19	390	-5648	10	-1088	0	2625	215	6.28	6.28	9.42	9.42	3	0.13	0.03	0.14	0.00	0.00	24.0
20	390	-5614	114	-882	0	2279	393	6.28	6.28	9.42	9.42	3	0.12	0.02	0.11	0.00	0.00	24.0
37	390	-5841	254	-1167	0	2713	632	6.28	6.28	9.42	9.42	3	0.15	0.03	0.15	0.00	0.00	24.0
38	390	-5300	-45	-935	0	2337	121	6.28	6.28	9.42	9.42	3	0.11	0.02	0.12	0.00	0.00	24.0
39	390	-5242	128	-592	0	1760	417	6.28	6.28	9.42	9.42	3	0.10	0.01	0.08	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

VERIFICA NODO IN TESTA AL PILASTRO, NODO NUM. 210 NON CONFINATO

(par.7.2.2 NTC2018 "La domanda di resistenza valutata con i criteri della progettazione in capacità può essere assunta non superiore alla domanda di resistenza valutata per il caso di comportamento strutturale non dissipativo.")

PROGETTAZIONE IN CAPACITA'

Asse loc. pilastro y nodo ESTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 45.0 cm, hjc= 20.0 cm
Asse loc. pilastro z nodo ESTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 30.0 cm, hjc= 50.0 cm

FxMin,inf	FxMin,sup	FxMax,sup	FySup	FzSup	Vjbdy	Vjbdz	Vres,y	Vres,z	I.R.compr.	Ashy	Ashz	PASSO	Nota
daN					daN		daN			cmq		cm	
-3912	1	-0	0	0	17616	17616	63005	105009	0.28	4.38	--	11.93	

VERIFICA DI RESISTENZA CON SOLLECITAZIONI COMPORTAMENTO NON DISSIPATIVO

Asse loc. pilastro y nodo ESTERNO: Hjw= 40.0 cm, bj= 45.0 cm, hjc= 20.0 cm, db1= 45.0 cm

NC	Fx,sup	Fx,inf	Mb	Vb	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-0	-4144	-447	934	0	1103	63005	0.02	0.00	40.00	
3	-0	-4067	-451	935	0	1114	63005	0.02	0.00	40.00	
4	-0	-4045	-231	856	0	570	63005	0.01	0.00	40.00	
5	-0	-3968	-235	858	0	581	63005	0.01	0.00	40.00	
6	-0	-4199	-366	905	0	904	63005	0.01	0.00	40.00	
7	-0	-3942	-381	910	0	940	63005	0.01	0.00	40.00	
8	-0	-4169	-301	882	0	744	63005	0.01	0.00	40.00	
9	-0	-3912	-316	887	0	780	63005	0.01	0.00	40.00	
10	-0	-4144	-447	934	0	1103	63005	0.02	0.00	40.00	
11	-0	-4067	-451	935	0	1114	63005	0.02	0.00	40.00	
12	-0	-4045	-231	856	0	570	63005	0.01	0.00	40.00	
13	-0	-3968	-235	858	0	581	63005	0.01	0.00	40.00	
14	-0	-4199	-366	905	0	904	63005	0.01	0.00	40.00	
15	-0	-3942	-381	910	0	940	63005	0.01	0.00	40.00	
16	-0	-4169	-301	882	0	744	63005	0.01	0.00	40.00	
17	-0	-3912	-316	887	0	780	63005	0.01	0.00	40.00	

Asse loc. pilastro z nodo ESTERNO: Hjw= 40.0 cm, bj= 30.0 cm, hjc= 50.0 cm, db1= 45.0 cm

NC	Fx,sup	Fx,inf	Mb	Vb	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-0	-4144	-1740	3210	0	4296	105009	0.04	0.00	40.00	
3	-0	-4067	-1575	3132	0	3889	105009	0.04	0.00	40.00	
4	-0	-4045	-1687	3188	0	4165	105009	0.04	0.00	40.00	
5	-0	-3968	-1523	3110	0	3760	105009	0.04	0.00	40.00	
6	-0	-4199	-1914	3294	0	4726	105009	0.05	0.00	40.00	
7	-0	-3942	-1365	3032	0	3370	105009	0.03	0.00	40.00	
8	-0	-4169	-1898	3288	0	4686	105009	0.04	0.00	40.00	
9	-0	-3912	-1349	3025	0	3331	105009	0.03	0.00	40.00	
10	-0	-4144	-1740	3210	0	4296	105009	0.04	0.00	40.00	
11	-0	-4067	-1575	3132	0	3889	105009	0.04	0.00	40.00	
12	-0	-4045	-1687	3188	0	4165	105009	0.04	0.00	40.00	
13	-0	-3968	-1523	3110	0	3760	105009	0.04	0.00	40.00	
14	-0	-4199	-1914	3294	0	4726	105009	0.05	0.00	40.00	
15	-0	-3942	-1365	3032	0	3370	105009	0.03	0.00	40.00	
16	-0	-4169	-1898	3288	0	4686	105009	0.04	0.00	40.00	
17	-0	-3912	-1349	3025	0	3331	105009	0.03	0.00	40.00	

CONFRONTO E SINTESI CONCLUSIVE (si assume in ogni caso passo <= 15 cm)

I.R.compr.	Ashy	Ashz	PASSO	Nota
	cmq		cm	
0.05	--	--	15.00	**VERIFICATO**

ASTA NUM. 57 NI 142 NF 123 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 18B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice resistenza	aswta	aswto	PASSO
	--															

	cm		daN		daN*m		cmq				Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-13300	-97	-1214	0	-1201	129	6.28	6.28	12.57	12.57	3	0.04	0.02	0.12	0.00	0.00	24.0
2	0	-10250	-7	-953	0	-967	-50	6.28	6.28	12.57	12.57	2	0.05	0.02	0.09	0.00	0.00	24.0
3	0	-10200	-5	-900	0	-851	-54	6.28	6.28	12.57	12.57	2	0.04	0.02	0.09	0.00	0.00	24.0
4	0	-10260	-144	-969	0	-996	252	6.28	6.28	12.57	12.57	2	0.06	0.02	0.10	0.00	0.00	24.0
5	0	-10220	-142	-915	0	-881	248	6.28	6.28	12.57	12.57	2	0.05	0.02	0.09	0.00	0.00	24.0
6	0	-10300	-58	-1021	0	-1112	61	6.28	6.28	12.57	12.57	2	0.06	0.02	0.10	0.00	0.00	24.0
7	0	-10160	-50	-842	0	-727	47	6.28	6.28	12.57	12.57	2	0.04	0.01	0.08	0.00	0.00	24.0
8	0	-10310	-99	-1026	0	-1121	151	6.28	6.28	12.57	12.57	2	0.06	0.02	0.10	0.00	0.00	24.0
9	0	-10170	-91	-847	0	-736	137	6.28	6.28	12.57	12.57	2	0.04	0.01	0.08	0.00	0.00	24.0
10	0	-10250	-7	-953	0	-967	-50	6.28	6.28	12.57	12.57	2	0.05	0.02	0.09	0.00	0.00	24.0
11	0	-10200	-5	-900	0	-851	-54	6.28	6.28	12.57	12.57	2	0.04	0.02	0.09	0.00	0.00	24.0
12	0	-10260	-144	-969	0	-996	252	6.28	6.28	12.57	12.57	2	0.06	0.02	0.10	0.00	0.00	24.0
13	0	-10220	-142	-915	0	-881	248	6.28	6.28	12.57	12.57	2	0.05	0.02	0.09	0.00	0.00	24.0
14	0	-10300	-58	-1021	0	-1112	61	6.28	6.28	12.57	12.57	2	0.06	0.02	0.10	0.00	0.00	24.0
15	0	-10160	-50	-842	0	-727	47	6.28	6.28	12.57	12.57	2	0.04	0.01	0.08	0.00	0.00	24.0
16	0	-10310	-99	-1026	0	-1121	151	6.28	6.28	12.57	12.57	2	0.06	0.02	0.10	0.00	0.00	24.0
17	0	-10170	-91	-847	0	-736	137	6.28	6.28	12.57	12.57	2	0.04	0.01	0.08	0.00	0.00	24.0
18	0	-14090	80	-1383	0	-1431	-267	6.28	6.28	12.57	12.57	3	0.05	0.02	0.13	0.00	0.00	24.0
19	0	-14160	-323	-1454	0	-1570	623	6.28	6.28	12.57	12.57	3	0.07	0.02	0.14	0.00	0.00	24.0
20	0	-14190	-104	-1496	0	-1649	143	6.28	6.28	12.57	12.57	3	0.06	0.03	0.14	0.00	0.00	24.0
37	0	-13660	222	-1271	0	-1266	-579	6.28	6.28	12.57	12.57	3	0.05	0.02	0.12	0.00	0.00	24.0
38	0	-13790	-450	-1390	0	-1497	904	6.28	6.28	12.57	12.57	3	0.07	0.02	0.13	0.00	0.00	24.0
39	0	-13840	-85	-1460	0	-1630	104	6.28	6.28	12.57	12.57	3	0.06	0.03	0.14	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	97	-12540	-97	-1214	0	-17	34	6.28	6.28	12.57	12.57	3	0.00	0.02	0.12	0.00	0.00	24.0
2	97	-9664	-7	-953	0	-37	-57	6.28	6.28	12.57	12.57	2	0.00	0.02	0.10	0.00	0.00	24.0
3	97	-9616	-5	-900	0	26	-59	6.28	6.28	12.57	12.57	2	0.00	0.02	0.09	0.00	0.00	24.0
4	97	-9676	-144	-969	0	-52	111	6.28	6.28	12.57	12.57	2	0.01	0.02	0.10	0.00	0.00	24.0
5	97	-9636	-142	-915	0	11	110	6.28	6.28	12.57	12.57	2	0.01	0.02	0.09	0.00	0.00	24.0
6	97	-9715	-58	-1021	0	-116	4	6.28	6.28	12.57	12.57	2	0.01	0.02	0.10	0.00	0.00	24.0
7	97	-9576	-50	-842	0	95	-2	6.28	6.28	12.57	12.57	2	0.00	0.01	0.08	0.00	0.00	24.0
8	97	-9724	-99	-1026	0	-121	55	6.28	6.28	12.57	12.57	2	0.01	0.02	0.10	0.00	0.00	24.0
9	97	-9584	-91	-847	0	90	48	6.28	6.28	12.57	12.57	2	0.01	0.01	0.08	0.00	0.00	24.0
10	97	-9664	-7	-953	0	-37	-57	6.28	6.28	12.57	12.57	2	0.00	0.02	0.10	0.00	0.00	24.0
11	97	-9616	-5	-900	0	26	-59	6.28	6.28	12.57	12.57	2	0.00	0.02	0.09	0.00	0.00	24.0
12	97	-9676	-144	-969	0	-52	111	6.28	6.28	12.57	12.57	2	0.01	0.02	0.10	0.00	0.00	24.0
13	97	-9636	-142	-915	0	11	110	6.28	6.28	12.57	12.57	2	0.01	0.02	0.09	0.00	0.00	24.0
14	97	-9715	-58	-1021	0	-116	4	6.28	6.28	12.57	12.57	2	0.01	0.02	0.10	0.00	0.00	24.0
15	97	-9576	-50	-842	0	95	-2	6.28	6.28	12.57	12.57	2	0.00	0.01	0.08	0.00	0.00	24.0
16	97	-9724	-99	-1026	0	-121	55	6.28	6.28	12.57	12.57	2	0.01	0.02	0.10	0.00	0.00	24.0
17	97	-9584	-91	-847	0	90	48	6.28	6.28	12.57	12.57	2	0.01	0.01	0.08	0.00	0.00	24.0
18	97	-13330	80	-1383	0	-83	-189	6.28	6.28	12.57	12.57	3	0.01	0.02	0.13	0.00	0.00	24.0
19	97	-13400	-323	-1454	0	-152	308	6.28	6.28	12.57	12.57	3	0.02	0.03	0.14	0.00	0.00	24.0
20	97	-13430	-104	-1496	0	-190	42	6.28	6.28	12.57	12.57	3	0.01	0.03	0.14	0.00	0.00	24.0
37	97	-12900	222	-1271	0	-27	-362	6.28	6.28	12.57	12.57	3	0.02	0.02	0.12	0.00	0.00	24.0
38	97	-13028	-450	-1390	0	-142	465	6.28	6.28	12.57	12.57	3	0.03	0.02	0.13	0.00	0.00	24.0
39	97	-13078	-85	-1460	0	-207	22	6.28	6.28	12.57	12.57	3	0.01	0.03	0.14	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	195	-11780	-97	-1214	0	1167	-60	6.28	6.28	12.57	12.57	3	0.04	0.02	0.12	0.00	0.00	24.0
2	195	-9078	-7	-953	0	892	-64	6.28	6.28	12.57	12.57	2	0.05	0.02	0.10	0.00	0.00	24.0
3	195	-9032	-5	-900	0	903	-64	6.28	6.28	12.57	12.57	2	0.05	0.02	0.09	0.00	0.00	24.0
4	195	-9092	-144	-969	0	893	-29	6.28	6.28	12.57	12.57	2	0.05	0.02	0.10	0.00	0.00	24.0
5	195	-9052	-142	-915	0	904	-28	6.28	6.28	12.57	12.57	2	0.05	0.02	0.09	0.00	0.00	24.0
6	195	-9130	-58	-1021	0	879	-52	6.28	6.28	12.57	12.57	2	0.05	0.02	0.10	0.00	0.00	24.0
7	195	-8991	-50	-842	0	916	-51	6.28	6.28	12.57	12.57	2	0.05	0.01	0.08	0.00	0.00	24.0
8	195	-9138	-99	-1026	0	879	-41	6.28	6.28	12.57	12.57	2	0.05	0.02	0.10	0.00	0.00	24.0
9	195	-8999	-91	-847	0	916	-41	6.28	6.28	12.57	12.57	2	0.05	0.01	0.09	0.00	0.00	24.0
10	195	-9078	-7	-953	0	892	-64	6.28	6.28	12.57	12.57	2	0.05	0.02	0.10	0.00	0.00	24.0
11	195	-9032	-5	-900	0	903	-64	6.28	6.28	12.57	12.57	2	0.05	0.02	0.09	0.00	0.00	24.0
12	195	-9092	-144	-969	0	893	-29	6.28	6.28	12.57	12.57	2	0.05	0.02	0.10	0.00	0.00	24.0
13	195	-9052	-142	-915	0	904	-28	6.28	6.28	12.57	12.57	2	0.05	0.02	0.09	0.00	0.00	24.0
14	195	-9130	-58	-1021	0	879	-52	6.28	6.28	12.57	12.57	2	0.05	0.02	0.10	0.00	0.00	24.0
15	195	-8991	-50	-842	0	916	-51	6.28	6.28	12.57	12.57	2	0.05	0.01	0.08	0.00	0.00	24.0
16	195	-9138	-99	-1026	0	879	-41	6.28	6.28	12.57	12.57	2	0.05	0.02	0.10	0.00	0.00	24.0
17	195	-8999	-91	-847	0	916	-41	6.28	6.28	12.57	12.57	2	0.05	0.01	0.09	0.00	0.00	24.0
18	195	-12570	80	-1383	0	1265	-111	6.28	6.28	12.57	12.57	3	0.05	0.02	0.13	0.00	0.00	24.0
19	195	-12640	-323	-1454	0	1265	-7	6.28	6.28	12.57	12.57	3	0.04	0.03	0.14	0.00	0.00	24.0
20	195	-12670	-104	-1496	0	1268	-59	6.28	6.28	12.57	12.57	3	0.05	0.03	0.14	0.00	0.00	24.0
37	195	-12140	222	-1271	0	1212	-146	6.28	6.28	12.57	12.57	3	0.04	0.02	0.12	0.00	0.00	24.0
38	195	-12265	-450	-1390	0	1213	27	6.28	6.28	12.57	12.57	3	0.04	0.02	0.13	0.00	0.00	24.0
39	195	-12315	-85	-1460	0	1217	-60	6.28	6.28	12.57	12.57	3	0.04	0.03	0.14	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	292	-11020	-97	-1214	0	2351	-154	6.28	6.28	12.57	12.57	3	0.09	0.02	0.12	0.00	0.00	24.0
2	292	-8491	-7	-953	0	1822	-71	6.28	6.28	12.57	12.57	2	0.10	0.02	0.10	0.00	0.00	24.0
3	292	-8447	-5	-900	0	1780	-69	6.28	6.28	12.57	12.57	2	0.09	0.02	0.09	0.00	0.00	24.0
4	292	-8509	-144	-969	0	1837	-169	6.28	6.28	12.57	12.57	2	0.10	0.02	0.10	0.00	0.00	24.0
5	292	-8467	-142	-915	0	1796	-167	6.28	6.28	12.57	12.57	2	0.10	0.02	0.09	0.00	0.00	24.0
6	292	-8546	-58	-1021	0	1875	-108	6.28	6.28	12.57	12.57	2	0.10	0.02	0.10	0.00	0.00	24.0
7	292	-8406	-50	-842	0	1738	-100	6.28	6.28	12.57	12.57	2	0.09	0.01	0.09	0.00	0.00	24.0
8	292	-8553	-99	-1026	0	1880	-138	6.28	6.28	12.57	12.57	2	0.10	0.02	0.10	0.00	0.00	24.0
9	292	-8414	-91	-847	0	1742	-129	6.28	6.28	12.57	12.57	2	0.09	0.01	0.09	0.00	0.00	24.0
10	292	-8491	-7	-953	0	1822	-71	6.28	6.28	12.57	12.57	2	0.10	0.02	0.10	0.00	0.00	24.0
11	292	-8447	-5	-900	0	1780	-69	6.28	6.28	12.57	12.57	2	0.09	0.02	0.09	0.00	0.00	24.0
12	292	-8509	-144	-969	0	1837	-169	6.28	6.28	12.57	12.57	2	0.10	0.02	0.10	0.00	0.00	24.0
13	292	-8467	-142	-915	0	1796	-167	6.28	6.28	12.57	12.57	2	0.10	0.02	0.09	0.00	0.00	24.0
14	292	-8546	-58	-1021	0	1875	-108	6.28	6.28	12.57	12.57	2	0.10	0.02	0.10	0.00	0.00	24.0
15	292	-8406	-50	-842	0	1738	-100	6.28	6.28	12.57	12.57	2	0.09	0.01	0.09	0.00	0.00	24.0
16	292	-8553	-99	-1026	0	1880	-138	6.28	6.28	12.57	12.57	2	0.10	0.02	0.10	0.00	0.00	24.0
17	292	-8414	-91	-847	0	1742	-129	6.28	6.28	12.57	12.57	2	0.09	0.01	0.09	0.00	0.00	24.0
18	292	-11810	80	-1383	0	2614	-33	6.28	6.28	12.57	12.57	3	0.09	0.02	0.13	0.00	0.00	24.0
19	292	-11880	-323	-1454	0	2683	-322	6.28	6.28	12.57	12.57	3	0.10	0.03	0.14	0.00	0.00	24.0
20	292	-11910	-104	-1496	0	2727	-161	6.28	6.28	12.57	12.57	3	0.10	0.03	0.15	0.00	0.00	24.0
37	292	-11380	222	-1271	0	2451	71	6.28	6.28	12.57	12.57	3	0.09	0.02	0.12	0.00	0.00	24.0
38	292	-11502	-450	-1390	0	2567	-411	6.28	6.28	12.57	12.57	3	0.10	0.02	0.14	0.00	0.00	24.0
39	292	-11552	-85	-1460	0	2640	-143	6.28	6.28	12.57	12.57	3	0.10	0.03	0.14	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	390	-10260	-97	-1214	0	3535	-249	6.28	6.28	12.57	12.57	3	0.13	0.02	0.12	0.00	0.00	24.0
2	390	-7905	-7	-953	0	2751	-78	6.28	6.28	12.57	12.57	2	0.15	0.02	0.10	0.00	0.00	24.0
3	390	-7863	-5	-900	0	2657	-74	6.28	6.28	12.57	12.57	2	0.14	0.02	0.09	0.00	0.00	24.0

4	390	-7925	-144	-969	0	2782	-309	6.28	6.28	12.57	12.57	2	0.15	0.02	0.10	0.00	0.00	24.0
5	390	-7883	-142	-915	0	2688	-305	6.28	6.28	12.57	12.57	2	0.15	0.02	0.09	0.00	0.00	24.0
6	390	-7961	-58	-1021	0	2871	-165	6.28	6.28	12.57	12.57	2	0.15	0.02	0.10	0.00	0.00	24.0
7	390	-7822	-50	-842	0	2559	-149	6.28	6.28	12.57	12.57	2	0.14	0.01	0.09	0.00	0.00	24.0
8	390	-7967	-99	-1026	0	2880	-234	6.28	6.28	12.57	12.57	2	0.16	0.02	0.10	0.00	0.00	24.0
9	390	-7828	-91	-847	0	2568	-218	6.28	6.28	12.57	12.57	2	0.14	0.01	0.09	0.00	0.00	24.0
10	390	-7905	-7	-953	0	2751	-78	6.28	6.28	12.57	12.57	2	0.15	0.02	0.10	0.00	0.00	24.0
11	390	-7863	-5	-900	0	2657	-74	6.28	6.28	12.57	12.57	2	0.14	0.02	0.09	0.00	0.00	24.0
12	390	-7925	-144	-969	0	2782	-309	6.28	6.28	12.57	12.57	2	0.15	0.02	0.10	0.00	0.00	24.0
13	390	-7883	-142	-915	0	2688	-305	6.28	6.28	12.57	12.57	2	0.15	0.02	0.09	0.00	0.00	24.0
14	390	-7961	-58	-1021	0	2871	-165	6.28	6.28	12.57	12.57	2	0.15	0.02	0.10	0.00	0.00	24.0
15	390	-7822	-50	-842	0	2559	-149	6.28	6.28	12.57	12.57	2	0.14	0.01	0.09	0.00	0.00	24.0
16	390	-7967	-99	-1026	0	2880	-234	6.28	6.28	12.57	12.57	2	0.16	0.02	0.10	0.00	0.00	24.0
17	390	-7828	-91	-847	0	2568	-218	6.28	6.28	12.57	12.57	2	0.14	0.01	0.09	0.00	0.00	24.0
18	390	-11050	80	-1383	0	3962	46	6.28	6.28	12.57	12.57	3	0.14	0.02	0.14	0.00	0.00	24.0
19	390	-11120	-323	-1454	0	4101	-637	6.28	6.28	12.57	12.57	3	0.15	0.03	0.14	0.00	0.00	24.0
20	390	-11150	-104	-1496	0	4186	-262	6.28	6.28	12.57	12.57	3	0.15	0.03	0.15	0.00	0.00	24.0
37	390	-10620	222	-1271	0	3690	288	6.28	6.28	12.57	12.57	3	0.14	0.02	0.13	0.00	0.00	24.0
38	390	-10740	-450	-1390	0	3922	-849	6.28	6.28	12.57	12.57	3	0.15	0.02	0.14	0.00	0.00	24.0
39	390	-10790	-85	-1460	0	4064	-225	6.28	6.28	12.57	12.57	3	0.15	0.03	0.14	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

VERIFICA NODO IN TESTA AL PILASTRO, NODO NUM. 123 NON CONFINATO

(par.7.2.2 NTC2018 "La domanda di resistenza valutata con i criteri della progettazione in capacità può essere assunta non superiore alla domanda di resistenza valutata per il caso di comportamento strutturale non dissipativo.")

PROGETTAZIONE IN CAPACITA'

Asse loc. pilastro y nodo INTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 50.0 cm, hjc= 30.0 cm
Asse loc. pilastro z nodo ESTERNO: As2(inf)= 6.03, As1(sup)= 6.03, Hjw= 40.0 cm, bj= 40.0 cm, hjc= 50.0 cm

FxMin,inf	FxMin,sup	FxMax,sup	FySup	FzSup	Vjbdy	Vjbdz	Vres,y	Vres,z	I.R.compr.	Ashy	Ashz	PASSO	Nota
daN					daN		daN			cmq		cm	
-7822	1	-0	0	0	35233	26425	131261	140012	0.27	8.85	--	5.13	

VERIFICA DI RESISTENZA CON SOLLECITAZIONI COMPORTAMENTO NON DISSIPATIVO

Asse loc. pilastro y nodo INTERNO: Hjw= 40.0 cm, bj= 50.0 cm, hjc= 30.0 cm, db1= 45.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb,1	Mb,2	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-0	-7905	-1177	-1156	0	52	131261	0.00	0.00	40.00	
3	-0	-7863	-1176	-1152	0	59	131261	0.00	0.00	40.00	
4	-0	-7925	-962	-1378	0	1026	131261	0.01	0.00	40.00	
5	-0	-7883	-961	-1374	0	1019	131261	0.01	0.00	40.00	
6	-0	-7961	-1103	-1239	0	336	131261	0.00	0.00	40.00	
7	-0	-7822	-1100	-1224	0	306	131261	0.00	0.00	40.00	
8	-0	-7967	-1039	-1306	0	659	131261	0.01	0.00	40.00	
9	-0	-7828	-1035	-1291	0	632	131261	0.00	0.00	40.00	
10	-0	-7905	-1177	-1156	0	52	131261	0.00	0.00	40.00	
11	-0	-7863	-1176	-1152	0	59	131261	0.00	0.00	40.00	
12	-0	-7925	-962	-1378	0	1026	131261	0.01	0.00	40.00	
13	-0	-7883	-961	-1374	0	1019	131261	0.01	0.00	40.00	
14	-0	-7961	-1103	-1239	0	336	131261	0.00	0.00	40.00	
15	-0	-7822	-1100	-1224	0	306	131261	0.00	0.00	40.00	
16	-0	-7967	-1039	-1306	0	659	131261	0.01	0.00	40.00	
17	-0	-7828	-1035	-1291	0	632	131261	0.00	0.00	40.00	

Asse loc. pilastro z nodo ESTERNO: Hjw= 40.0 cm, bj= 40.0 cm, hjc= 50.0 cm, db1= 45.0 cm

NC	Fx,sup	Fx,inf	Mb	Vb	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-0	-7905	-2787	5625	0	6881	140012	0.05	0.00	40.00	
3	-0	-7863	-2690	5585	0	6642	140012	0.05	0.00	40.00	
4	-0	-7925	-2816	5638	0	6953	140012	0.05	0.00	40.00	
5	-0	-7883	-2719	5598	0	6714	140012	0.05	0.00	40.00	
6	-0	-7961	-2911	5676	0	7188	140012	0.05	0.00	40.00	
7	-0	-7822	-2586	5543	0	6385	140012	0.05	0.00	40.00	
8	-0	-7967	-2920	5680	0	7210	140012	0.05	0.00	40.00	
9	-0	-7828	-2595	5547	0	6407	140012	0.05	0.00	40.00	
10	-0	-7905	-2787	5625	0	6881	140012	0.05	0.00	40.00	
11	-0	-7863	-2690	5585	0	6642	140012	0.05	0.00	40.00	
12	-0	-7925	-2816	5638	0	6953	140012	0.05	0.00	40.00	
13	-0	-7883	-2719	5598	0	6714	140012	0.05	0.00	40.00	
14	-0	-7961	-2911	5676	0	7188	140012	0.05	0.00	40.00	
15	-0	-7822	-2586	5543	0	6385	140012	0.05	0.00	40.00	
16	-0	-7967	-2920	5680	0	7210	140012	0.05	0.00	40.00	
17	-0	-7828	-2595	5547	0	6407	140012	0.05	0.00	40.00	

CONFRONTO E SINTESI CONCLUSIVE (si assume in ogni caso passo <= 15 cm)

I.R.compr.	Ashy	Ashz	PASSO	Nota
	cmq		cm	
0.05	--	--	15.00	**VERIFICATO**

ASTA NUM. 58 NI 211 NF 212 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 13B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-12490	57	-1205	0	-1344	-79	6.28	6.28	9.42	9.42	3	0.06	0.03	0.14	0.00	0.00	24.0
2	0	-9624	82	-946	0	-1075	-140	6.28	6.28	9.42	9.42	2	0.07	0.02	0.11	0.00	0.00	24.0
3	0	-9593	82	-906	0	-992	-138	6.28	6.28	9.42	9.42	2	0.07	0.02	0.11	0.00	0.00	24.0

4	0	-9625	6	-948	0	-1076	16	6.28	6.28	9.42	9.42	2	0.07	0.02	0.11	0.00	0.00	24.0
5	0	-9593	5	-908	0	-993	18	6.28	6.28	9.42	9.42	2	0.06	0.02	0.11	0.00	0.00	24.0
6	0	-9662	56	-994	0	-1172	-87	6.28	6.28	9.42	9.42	2	0.08	0.02	0.12	0.00	0.00	24.0
7	0	-9556	54	-860	0	-896	-82	6.28	6.28	9.42	9.42	2	0.06	0.02	0.10	0.00	0.00	24.0
8	0	-9662	33	-994	0	-1172	-40	6.28	6.28	9.42	9.42	2	0.07	0.02	0.12	0.00	0.00	24.0
9	0	-9556	31	-860	0	-896	-35	6.28	6.28	9.42	9.42	2	0.06	0.02	0.10	0.00	0.00	24.0
10	0	-9624	82	-946	0	-1075	-140	6.28	6.28	9.42	9.42	2	0.07	0.02	0.11	0.00	0.00	24.0
11	0	-9593	82	-906	0	-992	-138	6.28	6.28	9.42	9.42	2	0.07	0.02	0.11	0.00	0.00	24.0
12	0	-9625	6	-948	0	-1076	16	6.28	6.28	9.42	9.42	2	0.07	0.02	0.11	0.00	0.00	24.0
13	0	-9593	5	-908	0	-993	18	6.28	6.28	9.42	9.42	2	0.06	0.02	0.11	0.00	0.00	24.0
14	0	-9662	56	-994	0	-1172	-87	6.28	6.28	9.42	9.42	2	0.08	0.02	0.12	0.00	0.00	24.0
15	0	-9556	54	-860	0	-896	-82	6.28	6.28	9.42	9.42	2	0.06	0.02	0.10	0.00	0.00	24.0
16	0	-9662	33	-994	0	-1172	-40	6.28	6.28	9.42	9.42	2	0.07	0.02	0.12	0.00	0.00	24.0
17	0	-9556	31	-860	0	-896	-35	6.28	6.28	9.42	9.42	2	0.06	0.02	0.10	0.00	0.00	24.0
18	0	-13370	158	-1497	0	-1823	-286	6.28	6.28	9.42	9.42	3	0.09	0.03	0.17	0.00	0.00	24.0
19	0	-13340	-70	-1460	0	-1745	177	6.28	6.28	9.42	9.42	3	0.08	0.03	0.16	0.00	0.00	24.0
20	0	-13490	49	-1609	0	-2041	-63	6.28	6.28	9.42	9.42	3	0.09	0.04	0.18	0.00	0.00	24.0
37	0	-12970	238	-1400	0	-1686	-448	6.28	6.28	9.42	9.42	3	0.09	0.03	0.16	0.00	0.00	24.0
38	0	-12920	-142	-1339	0	-1556	323	6.28	6.28	9.42	9.42	3	0.08	0.03	0.15	0.00	0.00	24.0
39	0	-13160	56	-1588	0	-2049	-76	6.28	6.28	9.42	9.42	3	0.09	0.04	0.18	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	97	-11920	57	-1205	0	-169	-24	6.28	6.28	9.42	9.42	3	0.01	0.03	0.14	0.00	0.00	24.0
2	97	-9185	82	-946	0	-152	-59	6.28	6.28	9.42	9.42	2	0.01	0.02	0.11	0.00	0.00	24.0
3	97	-9154	82	-906	0	-108	-58	6.28	6.28	9.42	9.42	2	0.01	0.02	0.11	0.00	0.00	24.0
4	97	-9186	6	-948	0	-152	22	6.28	6.28	9.42	9.42	2	0.01	0.02	0.11	0.00	0.00	24.0
5	97	-9154	5	-908	0	-109	22	6.28	6.28	9.42	9.42	2	0.01	0.02	0.11	0.00	0.00	24.0
6	97	-9223	56	-994	0	-203	-32	6.28	6.28	9.42	9.42	2	0.01	0.02	0.12	0.00	0.00	24.0
7	97	-9117	54	-860	0	-57	-29	6.28	6.28	9.42	9.42	2	0.01	0.02	0.10	0.00	0.00	24.0
8	97	-9223	33	-994	0	-203	-8	6.28	6.28	9.42	9.42	2	0.01	0.02	0.12	0.00	0.00	24.0
9	97	-9117	31	-860	0	-57	-5	6.28	6.28	9.42	9.42	2	0.00	0.02	0.10	0.00	0.00	24.0
10	97	-9185	82	-946	0	-152	-59	6.28	6.28	9.42	9.42	2	0.01	0.02	0.11	0.00	0.00	24.0
11	97	-9154	82	-906	0	-108	-58	6.28	6.28	9.42	9.42	2	0.01	0.02	0.11	0.00	0.00	24.0
12	97	-9186	6	-948	0	-152	22	6.28	6.28	9.42	9.42	2	0.01	0.02	0.11	0.00	0.00	24.0
13	97	-9154	5	-908	0	-109	22	6.28	6.28	9.42	9.42	2	0.01	0.02	0.11	0.00	0.00	24.0
14	97	-9223	56	-994	0	-203	-32	6.28	6.28	9.42	9.42	2	0.01	0.02	0.12	0.00	0.00	24.0
15	97	-9117	54	-860	0	-57	-29	6.28	6.28	9.42	9.42	2	0.01	0.02	0.10	0.00	0.00	24.0
16	97	-9223	33	-994	0	-203	-8	6.28	6.28	9.42	9.42	2	0.01	0.02	0.12	0.00	0.00	24.0
17	97	-9117	31	-860	0	-57	-5	6.28	6.28	9.42	9.42	2	0.00	0.02	0.10	0.00	0.00	24.0
18	97	-12800	158	-1497	0	-364	-132	6.28	6.28	9.42	9.42	3	0.02	0.03	0.17	0.00	0.00	24.0
19	97	-12770	-70	-1460	0	-322	109	6.28	6.28	9.42	9.42	3	0.02	0.03	0.16	0.00	0.00	24.0
20	97	-12920	49	-1609	0	-472	-16	6.28	6.28	9.42	9.42	3	0.02	0.04	0.18	0.00	0.00	24.0
37	97	-12400	238	-1400	0	-321	-216	6.28	6.28	9.42	9.42	3	0.02	0.03	0.16	0.00	0.00	24.0
38	97	-12350	-142	-1339	0	-250	185	6.28	6.28	9.42	9.42	3	0.02	0.03	0.15	0.00	0.00	24.0
39	97	-12590	56	-1588	0	-501	-22	6.28	6.28	9.42	9.42	3	0.02	0.04	0.18	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	195	-11350	57	-1205	0	1006	31	6.28	6.28	9.42	9.42	3	0.05	0.03	0.14	0.00	0.00	24.0
2	195	-8746	82	-946	0	771	21	6.28	6.28	9.42	9.42	2	0.05	0.02	0.11	0.00	0.00	24.0
3	195	-8716	82	-906	0	776	21	6.28	6.28	9.42	9.42	2	0.05	0.02	0.11	0.00	0.00	24.0
4	195	-8748	6	-948	0	771	27	6.28	6.28	9.42	9.42	2	0.05	0.02	0.11	0.00	0.00	24.0
5	195	-8716	5	-908	0	776	27	6.28	6.28	9.42	9.42	2	0.05	0.02	0.11	0.00	0.00	24.0
6	195	-8784	56	-994	0	765	23	6.28	6.28	9.42	9.42	2	0.05	0.02	0.12	0.00	0.00	24.0
7	195	-8678	54	-860	0	781	23	6.28	6.28	9.42	9.42	2	0.05	0.02	0.10	0.00	0.00	24.0
8	195	-8784	33	-994	0	766	25	6.28	6.28	9.42	9.42	2	0.05	0.02	0.12	0.00	0.00	24.0
9	195	-8678	31	-860	0	781	25	6.28	6.28	9.42	9.42	2	0.05	0.02	0.10	0.00	0.00	24.0
10	195	-8746	82	-946	0	771	21	6.28	6.28	9.42	9.42	2	0.05	0.02	0.11	0.00	0.00	24.0
11	195	-8716	82	-906	0	776	21	6.28	6.28	9.42	9.42	2	0.05	0.02	0.11	0.00	0.00	24.0
12	195	-8748	6	-948	0	771	27	6.28	6.28	9.42	9.42	2	0.05	0.02	0.11	0.00	0.00	24.0
13	195	-8716	5	-908	0	776	27	6.28	6.28	9.42	9.42	2	0.05	0.02	0.11	0.00	0.00	24.0
14	195	-8784	56	-994	0	765	23	6.28	6.28	9.42	9.42	2	0.05	0.02	0.12	0.00	0.00	24.0
15	195	-8678	54	-860	0	781	23	6.28	6.28	9.42	9.42	2	0.05	0.02	0.10	0.00	0.00	24.0
16	195	-8784	33	-994	0	766	25	6.28	6.28	9.42	9.42	2	0.05	0.02	0.12	0.00	0.00	24.0
17	195	-8678	31	-860	0	781	25	6.28	6.28	9.42	9.42	2	0.05	0.02	0.10	0.00	0.00	24.0
18	195	-12230	158	-1497	0	1096	22	6.28	6.28	9.42	9.42	3	0.05	0.03	0.17	0.00	0.00	24.0
19	195	-12200	-70	-1460	0	1102	41	6.28	6.28	9.42	9.42	3	0.05	0.03	0.17	0.00	0.00	24.0
20	195	-12350	49	-1609	0	1097	32	6.28	6.28	9.42	9.42	3	0.05	0.04	0.18	0.00	0.00	24.0
37	195	-11830	238	-1400	0	1045	16	6.28	6.28	9.42	9.42	3	0.05	0.03	0.16	0.00	0.00	24.0
38	195	-11780	-142	-1339	0	1055	47	6.28	6.28	9.42	9.42	3	0.05	0.03	0.15	0.00	0.00	24.0
39	195	-12020	56	-1588	0	1048	32	6.28	6.28	9.42	9.42	3	0.05	0.04	0.18	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	292	-10780	57	-1205	0	2180	87	6.28	6.28	9.42	9.42	3	0.10	0.03	0.14	0.00	0.00	24.0
2	292	-8308	82	-946	0	1693	101	6.28	6.28	9.42	9.42	2	0.11	0.02	0.11	0.00	0.00	24.0
3	292	-8277	82	-906	0	1659	100	6.28	6.28	9.42	9.42	2	0.11	0.02	0.11	0.00	0.00	24.0
4	292	-8309	6	-948	0	1695	33	6.28	6.28	9.42	9.42	2	0.11	0.02	0.11	0.00	0.00	24.0
5	292	-8277	5	-908	0	1661	32	6.28	6.28	9.42	9.42	2	0.10	0.02	0.11	0.00	0.00	24.0
6	292	-8346	56	-994	0	1734	78	6.28	6.28	9.42	9.42	2	0.11	0.02	0.12	0.00	0.00	24.0
7	292	-8240	54	-860	0	1620	75	6.28	6.28	9.42	9.42	2	0.10	0.02	0.10	0.00	0.00	24.0
8	292	-8346	33	-994	0	1735	58	6.28	6.28	9.42	9.42	2	0.11	0.02	0.12	0.00	0.00	24.0
9	292	-8240	31	-860	0	1620	55	6.28	6.28	9.42	9.42	2	0.10	0.02	0.10	0.00	0.00	24.0
10	292	-8308	82	-946	0	1693	101	6.28	6.28	9.42	9.42	2	0.11	0.02	0.11	0.00	0.00	24.0
11	292	-8277	82	-906	0	1659	100	6.28	6.28	9.42	9.42	2	0.11	0.02	0.11	0.00	0.00	24.0
12	292	-8309	6	-948	0	1695	33	6.28	6.28	9.42	9.42	2	0.11	0.02	0.11	0.00	0.00	24.0
13	292	-8277	5	-908	0	1661	32	6.28	6.28	9.42	9.42	2	0.10	0.02	0.11	0.00	0.00	24.0
14	292	-8346	56	-994	0	1734	78	6.28	6.28	9.42	9.42	2	0.11	0.02	0.12	0.00	0.00	24.0
15	292	-8240	54	-860	0	1620	75	6.28	6.28	9.42	9.42	2	0.10	0.02	0.10	0.00	0.00	24.0
16	292	-8346	33	-994	0	1735	58	6.28	6.28	9.42	9.42	2	0.11	0.02	0.12	0.00	0.00	24.0
17	292	-8240	31	-860	0	1620	55	6.28	6.28	9.42	9.42	2	0.10	0.02	0.10	0.00	0.00	24.0
18	292	-11660	158	-1497	0	2555	177	6.28	6.28	9.42	9.42	3	0.12	0.03	0.17	0.00	0.00	24.0
19	292	-11630	-70	-1460	0	2525	-27	6.28	6.28	9.42	9.42	3	0.11	0.03	0.17	0.00	0.00	24.0
20	292	-11780	49	-1609	0	2666	79	6.28	6.28	9.42	9.42	3	0.12	0.04	0.18	0.00	0.00	24.0
37	292	-11260	238	-1400	0	2410	248	6.28	6.28	9.42	9.42	3	0.11	0.03	0.16	0.00	0.00	24.0
38	292	-11210	-142	-1339	0	2361	-91	6.28	6.28	9.42	9.42	3	0.11	0.03	0.15	0.00	0.00	24.0
39	292	-11450	56	-1588	0	2596	86	6.28	6.28	9.42	9.42	3	0.12	0.04	0.18	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	390	-10210	57	-1205	0	3355	142	6.28	6.28	9.42	9.42	3	0.16	0.03	0.14	0.00	0.00	24.0
2	390	-7869	82	-946	0	2616	182	6.28	6.28	9.42	9.42	2	0.17	0.02	0.11	0.00	0.00	24.0
3	390	-7838	82	-906	0	2543	180	6.28	6.28	9.42	9.42	2	0.17	0.02	0.11	0.00	0.00	24.0
4	390	-7870	6	-948	0	2619	38	6.28	6.28	9.42	9.42	2	0.16	0.02	0.11	0.00	0.00	24.0
5	390	-7838	5	-908	0	2546	37	6.28	6.28	9.42	9.42	2	0.16	0.02	0.11	0.00	0.00	24.0
6	390	-7907	56	-994	0	2703	133	6.28	6.28	9.42	9.42	2	0.17	0.02	0.12	0.00	0.00	24.0
7	390	-7801	54	-860	0	2458	128	6.28	6.28	9.42	9.42	2	0.16	0.02	0.10	0.00	0.00	24.0
8	390	-7907	33	-994	0	2704	90	6.28	6.28	9.42	9.42	2	0.17	0.02	0.12	0.00	0.00	24.0
9	390	-7801	31	-860	0	2459	85	6.28	6.28	9.42	9.42	2	0.16	0.02	0.10	0.00	0.00	24.0

10	390	-7869	82	-946	0	2616	182	6.28	6.28	9.42	9.42	2	0.17	0.02	0.11	0.00	0.00	24.0
11	390	-7838	82	-906	0	2543	180	6.28	6.28	9.42	9.42	2	0.17	0.02	0.11	0.00	0.00	24.0
12	390	-7870	6	-948	0	2619	38	6.28	6.28	9.42	9.42	2	0.16	0.02	0.11	0.00	0.00	24.0
13	390	-7838	5	-908	0	2546	37	6.28	6.28	9.42	9.42	2	0.16	0.02	0.11	0.00	0.00	24.0
14	390	-7907	56	-994	0	2703	133	6.28	6.28	9.42	9.42	2	0.17	0.02	0.12	0.00	0.00	24.0
15	390	-7801	54	-860	0	2458	128	6.28	6.28	9.42	9.42	2	0.16	0.02	0.10	0.00	0.00	24.0
16	390	-7907	33	-994	0	2704	90	6.28	6.28	9.42	9.42	2	0.17	0.02	0.12	0.00	0.00	24.0
17	390	-7801	31	-860	0	2459	85	6.28	6.28	9.42	9.42	2	0.16	0.02	0.10	0.00	0.00	24.0
18	390	-11090	158	-1497	0	4014	331	6.28	6.28	9.42	9.42	3	0.19	0.03	0.17	0.00	0.00	24.0
19	390	-11060	-70	-1460	0	3948	-95	6.28	6.28	9.42	9.42	3	0.18	0.03	0.17	0.00	0.00	24.0
20	390	-11210	49	-1609	0	4235	126	6.28	6.28	9.42	9.42	3	0.19	0.04	0.18	0.00	0.00	24.0
37	390	-10690	238	-1400	0	3775	481	6.28	6.28	9.42	9.42	3	0.18	0.03	0.16	0.00	0.00	24.0
38	390	-10640	-142	-1339	0	3666	-230	6.28	6.28	9.42	9.42	3	0.17	0.03	0.16	0.00	0.00	24.0
39	390	-10880	56	-1588	0	4145	140	6.28	6.28	9.42	9.42	3	0.19	0.04	0.18	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

VERIFICA NODO IN TESTA AL PILASTRO, NODO NUM. 212 NON CONFINATO

(par.7.2.2 NTC2018 "La domanda di resistenza valutata con i criteri della progettazione in capacità può essere assunta non superiore alla domanda di resistenza valutata per il caso di comportamento strutturale non dissipativo.")

PROGETTAZIONE IN CAPACITA'

Asse loc. pilastro y nodo INTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 45.0 cm, hjc= 20.0 cm
Asse loc. pilastro z nodo ESTERNO: As2(inf)= 6.03, As1(sup)= 6.03, Hjw= 40.0 cm, bj= 40.0 cm, hjc= 50.0 cm

FxMin,inf	FxMin,sup	FxMax,sup	FySup	FzSup	Vjbdy	Vjbdz	Vres,y	Vres,z	I.R.compr.	Ashy	Ashz	PASSO	Nota
daN					daN		daN			cmq		cm	
-7801	1	-0	0	0	35233	26425	78757	140012	0.45	8.85	--	5.13	

VERIFICA DI RESISTENZA CON SOLLECITAZIONI COMPORTAMENTO NON DISSIPATIVO

Asse loc. pilastro y nodo INTERNO: Hjw= 40.0 cm, bj= 45.0 cm, hjc= 20.0 cm, db1= 45.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb,1	Mb,2	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-0	-7869	-1310	-975	0	827	78757	0.01	0.00	40.00	
3	-0	-7838	-1307	-975	0	820	78757	0.01	0.00	40.00	
4	-0	-7870	-1130	-1158	0	69	78757	0.00	0.00	40.00	
5	-0	-7838	-1126	-1157	0	77	78757	0.00	0.00	40.00	
6	-0	-7907	-1251	-1040	0	521	78757	0.01	0.00	40.00	
7	-0	-7801	-1240	-1038	0	499	78757	0.01	0.00	40.00	
8	-0	-7907	-1197	-1094	0	254	78757	0.00	0.00	40.00	
9	-0	-7801	-1186	-1093	0	230	78757	0.00	0.00	40.00	
10	-0	-7869	-1310	-975	0	827	78757	0.01	0.00	40.00	
11	-0	-7838	-1307	-975	0	820	78757	0.01	0.00	40.00	
12	-0	-7870	-1130	-1158	0	69	78757	0.00	0.00	40.00	
13	-0	-7838	-1126	-1157	0	77	78757	0.00	0.00	40.00	
14	-0	-7907	-1251	-1040	0	521	78757	0.01	0.00	40.00	
15	-0	-7801	-1240	-1038	0	499	78757	0.01	0.00	40.00	
16	-0	-7907	-1197	-1094	0	254	78757	0.00	0.00	40.00	
17	-0	-7801	-1186	-1093	0	230	78757	0.00	0.00	40.00	

Asse loc. pilastro z nodo ESTERNO: Hjw= 40.0 cm, bj= 40.0 cm, hjc= 50.0 cm, db1= 45.0 cm

NC	Fx,sup	Fx,inf	Mb	Vb	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-0	-7869	-2672	5601	0	6598	140012	0.05	0.00	40.00	
3	-0	-7838	-2596	5570	0	6410	140012	0.05	0.00	40.00	
4	-0	-7870	-2675	5601	0	6605	140012	0.05	0.00	40.00	
5	-0	-7838	-2599	5571	0	6417	140012	0.05	0.00	40.00	
6	-0	-7907	-2761	5637	0	6817	140012	0.05	0.00	40.00	
7	-0	-7801	-2509	5535	0	6195	140012	0.04	0.00	40.00	
8	-0	-7907	-2762	5637	0	6820	140012	0.05	0.00	40.00	
9	-0	-7801	-2510	5535	0	6198	140012	0.04	0.00	40.00	
10	-0	-7869	-2672	5601	0	6598	140012	0.05	0.00	40.00	
11	-0	-7838	-2596	5570	0	6410	140012	0.05	0.00	40.00	
12	-0	-7870	-2675	5601	0	6605	140012	0.05	0.00	40.00	
13	-0	-7838	-2599	5571	0	6417	140012	0.05	0.00	40.00	
14	-0	-7907	-2761	5637	0	6817	140012	0.05	0.00	40.00	
15	-0	-7801	-2509	5535	0	6195	140012	0.04	0.00	40.00	
16	-0	-7907	-2762	5637	0	6820	140012	0.05	0.00	40.00	
17	-0	-7801	-2510	5535	0	6198	140012	0.04	0.00	40.00	

CONFRONTO E SINTESI CONCLUSIVE (si assume in ogni caso passo <= 15 cm)

I.R.compr.	Ashy	Ashz	PASSO	Nota
	cmq		cm	
0.05	--	--	15.00	**VERIFICATO**

ASTA NUM. 59 NI 213 NF 214 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 8B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-7262	-108	-607	0	-645	42	6.28	6.28	9.42	9.42	3	0.03	0.01	0.07	0.00	0.00	24.0
2	0	-5580	-52	-505	0	-583	-39	6.28	6.28	9.42	9.42	2	0.04	0.01	0.06	0.00	0.00	24.0
3	0	-5548	-53	-460	0	-480	-35	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
4	0	-5624	-114	-473	0	-512	100	6.28	6.28	9.42	9.42	2	0.04	0.01	0.06	0.00	0.00	24.0
5	0	-5592	-115	-428	0	-409	104	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
6	0	-5633	-71	-547	0	-679	5	6.28	6.28	9.42	9.42	2	0.04	0.01	0.07	0.00	0.00	24.0
7	0	-5526	-77	-396	0	-335	18	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
8	0	-5646	-90	-537	0	-657	47	6.28	6.28	9.42	9.42	2	0.04	0.01	0.07	0.00	0.00	24.0
9	0	-5540	-96	-386	0	-314	60	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0

10	0	-5580	-52	-505	0	-583	-39	6.28	6.28	9.42	9.42	2	0.04	0.01	0.06	0.00	0.00	24.0
11	0	-5548	-53	-460	0	-480	-35	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
12	0	-5624	-114	-473	0	-512	100	6.28	6.28	9.42	9.42	2	0.04	0.01	0.06	0.00	0.00	24.0
13	0	-5592	-115	-428	0	-409	104	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
14	0	-5633	-71	-547	0	-679	5	6.28	6.28	9.42	9.42	2	0.04	0.01	0.07	0.00	0.00	24.0
15	0	-5526	-77	-396	0	-335	18	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
16	0	-5646	-90	-537	0	-657	47	6.28	6.28	9.42	9.42	2	0.04	0.01	0.07	0.00	0.00	24.0
17	0	-5540	-96	-386	0	-314	60	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
18	0	-7633	-23	-800	0	-1016	-151	6.28	6.28	9.42	9.42	3	0.05	0.02	0.10	0.00	0.00	24.0
19	0	-7713	-209	-632	0	-639	266	6.28	6.28	9.42	9.42	3	0.04	0.01	0.08	0.00	0.00	24.0
20	0	-7754	-112	-804	0	-1020	50	6.28	6.28	9.42	9.42	3	0.05	0.02	0.10	0.00	0.00	24.0
37	0	-7408	41	-812	0	-1074	-295	6.28	6.28	9.42	9.42	3	0.06	0.02	0.10	0.00	0.00	24.0
38	0	-7543	-268	-532	0	-447	401	6.28	6.28	9.42	9.42	3	0.05	0.01	0.06	0.00	0.00	24.0
39	0	-7610	-108	-818	0	-1081	40	6.28	6.28	9.42	9.42	3	0.05	0.02	0.10	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	97	-6692	-108	-607	0	-53	-64	6.28	6.28	9.42	9.42	3	0.01	0.01	0.08	0.00	0.00	24.0
2	97	-5141	-52	-505	0	-91	-90	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
3	97	-5109	-53	-460	0	-32	-87	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
4	97	-5185	-114	-473	0	-51	-11	6.28	6.28	9.42	9.42	2	0.00	0.01	0.06	0.00	0.00	24.0
5	97	-5153	-115	-428	0	8	-8	6.28	6.28	9.42	9.42	2	0.00	0.01	0.05	0.00	0.00	24.0
6	97	-5194	-71	-547	0	-146	-64	6.28	6.28	9.42	9.42	2	0.01	0.01	0.07	0.00	0.00	24.0
7	97	-5087	-77	-396	0	51	-57	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
8	97	-5207	-90	-537	0	-133	-41	6.28	6.28	9.42	9.42	2	0.01	0.01	0.07	0.00	0.00	24.0
9	97	-5101	-96	-386	0	63	-34	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
10	97	-5141	-52	-505	0	-91	-90	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
11	97	-5109	-53	-460	0	-32	-87	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
12	97	-5185	-114	-473	0	-51	-11	6.28	6.28	9.42	9.42	2	0.00	0.01	0.06	0.00	0.00	24.0
13	97	-5153	-115	-428	0	8	-8	6.28	6.28	9.42	9.42	2	0.00	0.01	0.05	0.00	0.00	24.0
14	97	-5194	-71	-547	0	-146	-64	6.28	6.28	9.42	9.42	2	0.01	0.01	0.07	0.00	0.00	24.0
15	97	-5087	-77	-396	0	51	-57	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
16	97	-5207	-90	-537	0	-133	-41	6.28	6.28	9.42	9.42	2	0.01	0.01	0.07	0.00	0.00	24.0
17	97	-5101	-96	-386	0	63	-34	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
18	97	-7062	-23	-800	0	-236	-174	6.28	6.28	9.42	9.42	3	0.02	0.02	0.10	0.00	0.00	24.0
19	97	-7143	-209	-632	0	-22	63	6.28	6.28	9.42	9.42	3	0.01	0.01	0.08	0.00	0.00	24.0
20	97	-7184	-112	-804	0	-236	-60	6.28	6.28	9.42	9.42	3	0.01	0.02	0.10	0.00	0.00	24.0
37	97	-6838	41	-812	0	-283	-255	6.28	6.28	9.42	9.42	3	0.03	0.02	0.10	0.00	0.00	24.0
38	97	-6973	-268	-532	0	72	140	6.28	6.28	9.42	9.42	3	0.02	0.01	0.07	0.00	0.00	24.0
39	97	-7040	-108	-818	0	-284	-65	6.28	6.28	9.42	9.42	3	0.02	0.02	0.10	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	195	-6122	-108	-607	0	538	-170	6.28	6.28	9.42	9.42	3	0.03	0.01	0.08	0.00	0.00	24.0
2	195	-4702	-52	-505	0	402	-140	6.28	6.28	9.42	9.42	2	0.04	0.01	0.06	0.00	0.00	24.0
3	195	-4670	-53	-460	0	417	-139	6.28	6.28	9.42	9.42	2	0.04	0.01	0.06	0.00	0.00	24.0
4	195	-4746	-114	-473	0	411	-121	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
5	195	-4714	-115	-428	0	426	-121	6.28	6.28	9.42	9.42	2	0.04	0.01	0.05	0.00	0.00	24.0
6	195	-4756	-71	-547	0	388	-134	6.28	6.28	9.42	9.42	2	0.03	0.01	0.07	0.00	0.00	24.0
7	195	-4648	-77	-396	0	437	-132	6.28	6.28	9.42	9.42	2	0.04	0.01	0.05	0.00	0.00	24.0
8	195	-4768	-90	-537	0	390	-128	6.28	6.28	9.42	9.42	2	0.03	0.01	0.07	0.00	0.00	24.0
9	195	-4662	-96	-386	0	440	-127	6.28	6.28	9.42	9.42	2	0.04	0.01	0.05	0.00	0.00	24.0
10	195	-4702	-52	-505	0	402	-140	6.28	6.28	9.42	9.42	2	0.04	0.01	0.06	0.00	0.00	24.0
11	195	-4670	-53	-460	0	417	-139	6.28	6.28	9.42	9.42	2	0.04	0.01	0.06	0.00	0.00	24.0
12	195	-4746	-114	-473	0	411	-121	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
13	195	-4714	-115	-428	0	426	-121	6.28	6.28	9.42	9.42	2	0.04	0.01	0.05	0.00	0.00	24.0
14	195	-4756	-71	-547	0	388	-134	6.28	6.28	9.42	9.42	2	0.03	0.01	0.07	0.00	0.00	24.0
15	195	-4648	-77	-396	0	437	-132	6.28	6.28	9.42	9.42	2	0.04	0.01	0.05	0.00	0.00	24.0
16	195	-4768	-90	-537	0	390	-128	6.28	6.28	9.42	9.42	2	0.03	0.01	0.07	0.00	0.00	24.0
17	195	-4662	-96	-386	0	440	-127	6.28	6.28	9.42	9.42	2	0.04	0.01	0.05	0.00	0.00	24.0
18	195	-6492	-23	-800	0	544	-196	6.28	6.28	9.42	9.42	3	0.03	0.02	0.10	0.00	0.00	24.0
19	195	-6572	-209	-632	0	595	-141	6.28	6.28	9.42	9.42	3	0.03	0.01	0.08	0.00	0.00	24.0
20	195	-6613	-112	-804	0	548	-170	6.28	6.28	9.42	9.42	3	0.03	0.02	0.10	0.00	0.00	24.0
37	195	-6268	41	-812	0	508	-215	6.28	6.28	9.42	9.42	3	0.03	0.02	0.10	0.00	0.00	24.0
38	195	-6402	-268	-532	0	591	-122	6.28	6.28	9.42	9.42	3	0.03	0.01	0.07	0.00	0.00	24.0
39	195	-6470	-108	-818	0	513	-170	6.28	6.28	9.42	9.42	3	0.03	0.02	0.10	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	292	-5551	-108	-607	0	1130	-275	6.28	6.28	9.42	9.42	3	0.06	0.01	0.08	0.00	0.00	24.0
2	292	-4264	-52	-505	0	894	-190	6.28	6.28	9.42	9.42	2	0.07	0.01	0.07	0.00	0.00	24.0
3	292	-4232	-53	-460	0	865	-191	6.28	6.28	9.42	9.42	2	0.07	0.01	0.06	0.00	0.00	24.0
4	292	-4308	-114	-473	0	872	-232	6.28	6.28	9.42	9.42	2	0.07	0.01	0.06	0.00	0.00	24.0
5	292	-4276	-115	-428	0	843	-233	6.28	6.28	9.42	9.42	2	0.07	0.01	0.06	0.00	0.00	24.0
6	292	-4317	-71	-547	0	921	-203	6.28	6.28	9.42	9.42	2	0.07	0.01	0.07	0.00	0.00	24.0
7	292	-4210	-77	-396	0	823	-208	6.28	6.28	9.42	9.42	2	0.07	0.01	0.05	0.00	0.00	24.0
8	292	-4330	-90	-537	0	914	-216	6.28	6.28	9.42	9.42	2	0.07	0.01	0.07	0.00	0.00	24.0
9	292	-4224	-96	-386	0	816	-220	6.28	6.28	9.42	9.42	2	0.07	0.01	0.05	0.00	0.00	24.0
10	292	-4264	-52	-505	0	894	-190	6.28	6.28	9.42	9.42	2	0.07	0.01	0.07	0.00	0.00	24.0
11	292	-4232	-53	-460	0	865	-191	6.28	6.28	9.42	9.42	2	0.07	0.01	0.06	0.00	0.00	24.0
12	292	-4308	-114	-473	0	872	-232	6.28	6.28	9.42	9.42	2	0.07	0.01	0.06	0.00	0.00	24.0
13	292	-4276	-115	-428	0	843	-233	6.28	6.28	9.42	9.42	2	0.07	0.01	0.06	0.00	0.00	24.0
14	292	-4317	-71	-547	0	921	-203	6.28	6.28	9.42	9.42	2	0.07	0.01	0.07	0.00	0.00	24.0
15	292	-4210	-77	-396	0	823	-208	6.28	6.28	9.42	9.42	2	0.07	0.01	0.05	0.00	0.00	24.0
16	292	-4330	-90	-537	0	914	-216	6.28	6.28	9.42	9.42	2	0.07	0.01	0.07	0.00	0.00	24.0
17	292	-4224	-96	-386	0	816	-220	6.28	6.28	9.42	9.42	2	0.07	0.01	0.05	0.00	0.00	24.0
18	292	-5922	-23	-800	0	1325	-219	6.28	6.28	9.42	9.42	3	0.07	0.02	0.10	0.00	0.00	24.0
19	292	-6002	-209	-632	0	1211	-344	6.28	6.28	9.42	9.42	3	0.07	0.01	0.08	0.00	0.00	24.0
20	292	-6042	-112	-804	0	1332	-279	6.28	6.28	9.42	9.42	3	0.07	0.02	0.10	0.00	0.00	24.0
37	292	-5697	41	-812	0	1299	-175	6.28	6.28	9.42	9.42	3	0.06	0.02	0.10	0.00	0.00	24.0
38	292	-5832	-268	-532	0	1110	-384	6.28	6.28	9.42	9.42	3	0.07	0.01	0.07	0.00	0.00	24.0
39	292	-5899	-108	-818	0	1311	-275	6.28	6.28	9.42	9.42	3	0.07	0.02	0.10	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	390	-4981	-108	-607	0	1721	-381	6.28	6.28	9.42	9.42	3	0.09	0.01	0.08	0.00	0.00	24.0
2	390	-3825	-52	-505	0	1387	-241	6.28	6.28	9.42	9.42	2	0.10	0.01	0.07	0.00	0.00	24.0
3	390	-3793	-53	-460	0	1314	-243	6.28	6.28	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
4	390	-3869	-114	-473	0	1334	-343	6.28	6.28	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
5	390	-3837	-115	-428	0	1260	-346	6.28	6.28	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
6	390	-3878	-71	-547	0	1454	-273	6.28	6.28	9.42	9.42	2	0.11	0.01	0.07	0.00	0.00	24.0
7	390	-3771	-77	-396	0	1209	-283	6.28	6.28	9.42	9.42	2	0.10	0.01	0.05	0.00	0.00	24.0
8	390	-3891	-90	-537	0	1438	-304	6.28	6.28	9.42	9.42	2	0.11	0.01	0.07	0.00	0.00	24.0
9	390	-3785	-96	-386	0	1193	-313	6.28	6.28	9.42	9.42	2	0.10	0.01	0.05	0.00	0.00	24.0
10	390	-3825	-52	-505	0	1387	-241	6.28	6.28	9.42	9.42	2	0.10	0.01	0.07	0.00	0.00	24.0
11	390	-3793	-53	-460	0	1314	-243	6.28	6.28	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
12	390	-3869	-114	-473	0	1334	-343	6.28	6.28	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
13	390	-3837	-115	-428	0	1260	-346	6.28	6.28	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
14	390	-3878	-71	-547	0	1454	-273	6.28	6.28	9.42	9.42	2	0.11	0.01	0.07	0.00	0.00	24.0
15	390	-3771	-77	-396	0	1209	-283	6.28	6.28	9.42	9.42	2	0.10	0.01	0.05	0.00	0.00	24.0

16	390	-3891	-90	-537	0	1438	-304	6.28	6.28	9.42	9.42	2	0.11	0.01	0.07	0.00	0.00	24.0
17	390	-3785	-96	-386	0	1193	-313	6.28	6.28	9.42	9.42	2	0.10	0.01	0.05	0.00	0.00	24.0
18	390	-5351	-23	-800	0	2105	-242	6.28	6.28	9.42	9.42	3	0.10	0.02	0.10	0.00	0.00	24.0
19	390	-5432	-209	-632	0	1828	-548	6.28	6.28	9.42	9.42	3	0.10	0.01	0.08	0.00	0.00	24.0
20	390	-5472	-112	-804	0	2116	-388	6.28	6.28	9.42	9.42	3	0.11	0.02	0.10	0.00	0.00	24.0
37	390	-5127	41	-812	0	2090	-136	6.28	6.28	9.42	9.42	3	0.10	0.02	0.10	0.00	0.00	24.0
38	390	-5262	-268	-532	0	1629	-645	6.28	6.28	9.42	9.42	3	0.10	0.01	0.07	0.00	0.00	24.0
39	390	-5329	-108	-818	0	2108	-380	6.28	6.28	9.42	9.42	3	0.11	0.02	0.10	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

VERIFICA NODO IN TESTA AL PILASTRO, NODO NUM. 214 NON CONFINATO

(par.7.2.2 NTC2018 "La domanda di resistenza valutata con i criteri della progettazione in capacità può essere assunta non superiore alla domanda di resistenza valutata per il caso di comportamento strutturale non dissipativo.")

PROGETTAZIONE IN CAPACITA'

Asse loc. pilastro y nodo ESTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 45.0 cm, hjc= 20.0 cm
Asse loc. pilastro z nodo ESTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 30.0 cm, hjc= 50.0 cm

FxMin,inf	FxMin,sup	FxMax,sup	FySup	FzSup	Vjbdy	Vjbdz	Vres,y	Vres,z	I.R.compr.	Ashy	Ashz	PASSO	Nota
daN					daN		daN			cmq		cm	
-3771	1	-0	0	0	17616	17616	63005	105009	0.28	4.38	--	11.92	

VERIFICA DI RESISTENZA CON SOLLECITAZIONI COMPORTAMENTO NON DISSIPATIVO

Asse loc. pilastro y nodo ESTERNO: Hjw= 40.0 cm, bj= 45.0 cm, hjc= 20.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb	Vb	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m			daN			cmq	cm	
2	-0	-3825	-264	874	0	651	63005	0.01	0.00	40.00	
3	-0	-3793	-267	875	0	660	63005	0.01	0.00	40.00	
4	-0	-3869	-478	944	0	1181	63005	0.02	0.00	40.00	
5	-0	-3837	-482	945	0	1190	63005	0.02	0.00	40.00	
6	-0	-3878	-335	897	0	827	63005	0.01	0.00	40.00	
7	-0	-3771	-346	901	0	855	63005	0.01	0.00	40.00	
8	-0	-3891	-399	918	0	986	63005	0.02	0.00	40.00	
9	-0	-3785	-411	922	0	1014	63005	0.02	0.00	40.00	
10	-0	-3825	-264	874	0	651	63005	0.01	0.00	40.00	
11	-0	-3793	-267	875	0	660	63005	0.01	0.00	40.00	
12	-0	-3869	-478	944	0	1181	63005	0.02	0.00	40.00	
13	-0	-3837	-482	945	0	1190	63005	0.02	0.00	40.00	
14	-0	-3878	-335	897	0	827	63005	0.01	0.00	40.00	
15	-0	-3771	-346	901	0	855	63005	0.01	0.00	40.00	
16	-0	-3891	-399	918	0	986	63005	0.02	0.00	40.00	
17	-0	-3785	-411	922	0	1014	63005	0.02	0.00	40.00	

Asse loc. pilastro z nodo ESTERNO: Hjw= 40.0 cm, bj= 30.0 cm, hjc= 50.0 cm, db1= 45.0 cm

NC	Fx,sup	Fx,inf	Mb	Vb	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m			daN			cmq	cm	
2	-0	-3825	-1341	2951	0	3311	105009	0.03	0.00	40.00	
3	-0	-3793	-1269	2918	0	3133	105009	0.03	0.00	40.00	
4	-0	-3869	-1289	2925	0	3183	105009	0.03	0.00	40.00	
5	-0	-3837	-1217	2892	0	3005	105009	0.03	0.00	40.00	
6	-0	-3878	-1408	2981	0	3477	105009	0.03	0.00	40.00	
7	-0	-3771	-1166	2870	0	2879	105009	0.03	0.00	40.00	
8	-0	-3891	-1392	2973	0	3437	105009	0.03	0.00	40.00	
9	-0	-3785	-1150	2863	0	2840	105009	0.03	0.00	40.00	
10	-0	-3825	-1341	2951	0	3311	105009	0.03	0.00	40.00	
11	-0	-3793	-1269	2918	0	3133	105009	0.03	0.00	40.00	
12	-0	-3869	-1289	2925	0	3183	105009	0.03	0.00	40.00	
13	-0	-3837	-1217	2892	0	3005	105009	0.03	0.00	40.00	
14	-0	-3878	-1408	2981	0	3477	105009	0.03	0.00	40.00	
15	-0	-3771	-1166	2870	0	2879	105009	0.03	0.00	40.00	
16	-0	-3891	-1392	2973	0	3437	105009	0.03	0.00	40.00	
17	-0	-3785	-1150	2863	0	2840	105009	0.03	0.00	40.00	

CONFRONTO E SINTESI CONCLUSIVE (si assume in ogni caso passo <= 15 cm)

I.R.compr.	Ashy	Ashz	PASSO	Nota
	cmq		cm	
0.03	--	--	15.00	**VERIFICATO**

ASTA NUM. 60 NI 292 NF 302 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 1C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-14980	-97	-328	0	933	-325	6.28	6.28	9.42	9.42	3	0.05	0.01	0.04	0.00	0.00	24.0
2	0	-10830	84	-302	0	747	-27	6.28	6.28	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
3	0	-10650	82	-238	0	698	-29	6.28	6.28	9.42	9.42	2	0.04	0.01	0.03	0.00	0.00	24.0
4	0	-12390	-231	-267	0	737	-470	6.28	6.28	9.42	9.42	2	0.08	0.01	0.03	0.00	0.00	24.0
5	0	-12210	-234	-203	0	689	-472	6.28	6.28	9.42	9.42	2	0.08	0.01	0.02	0.00	0.00	24.0
6	0	-11590	-24	-365	0	801	-180	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
7	0	-10990	-31	-151	0	638	-187	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
8	0	-12050	-118	-354	0	798	-313	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
9	0	-11460	-126	-140	0	635	-320	6.28	6.28	9.42	9.42	2	0.06	0.00	0.02	0.00	0.00	24.0
10	0	-10830	84	-302	0	747	-27	6.28	6.28	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
11	0	-10650	82	-238	0	698	-29	6.28	6.28	9.42	9.42	2	0.04	0.01	0.03	0.00	0.00	24.0
12	0	-12390	-231	-267	0	737	-470	6.28	6.28	9.42	9.42	2	0.08	0.01	0.03	0.00	0.00	24.0
13	0	-12210	-234	-203	0	689	-472	6.28	6.28	9.42	9.42	2	0.08	0.01	0.02	0.00	0.00	24.0
14	0	-11590	-24	-365	0	801	-180	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
15	0	-10990	-31	-151	0	638	-187	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0

16	0	-12050	-118	-354	0	798	-313	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
17	0	-11460	-126	-140	0	635	-320	6.28	6.28	9.42	9.42	2	0.06	0.00	0.02	0.00	0.00	24.0
18	0	-17290	171	-599	0	1404	430	6.28	6.28	9.42	9.42	3	0.07	0.01	0.06	0.00	0.00	24.0
19	0	-18880	-241	-374	0	1122	-832	6.28	6.28	9.42	9.42	3	0.09	0.01	0.04	0.00	0.00	24.0
20	0	-17270	-43	-102	0	929	-214	6.28	6.28	9.42	9.42	3	0.05	0.00	0.01	0.00	0.00	24.0
37	0	-15740	289	-623	0	1391	812	6.28	6.28	9.42	9.42	3	0.10	0.01	0.07	0.00	0.00	24.0
38	0	-18390	-399	-248	0	921	-1292	6.28	6.28	9.42	9.42	3	0.13	0.01	0.04	0.00	0.00	24.0
39	0	-15710	-67	206	0	598	-262	6.28	6.28	9.42	9.42	3	0.04	0.00	0.02	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-14908	-97	-328	0	974	-337	6.28	6.28	9.42	9.42	3	0.05	0.01	0.04	0.00	0.00	24.0
2	12	-10775	84	-302	0	785	-17	6.28	6.28	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
3	12	-10595	82	-238	0	728	-19	6.28	6.28	9.42	9.42	2	0.04	0.01	0.03	0.00	0.00	24.0
4	12	-12335	-231	-267	0	771	-499	6.28	6.28	9.42	9.42	2	0.08	0.01	0.03	0.00	0.00	24.0
5	12	-12155	-234	-203	0	714	-501	6.28	6.28	9.42	9.42	2	0.08	0.01	0.02	0.00	0.00	24.0
6	12	-11532	-24	-365	0	846	-183	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
7	12	-10932	-31	-151	0	657	-190	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
8	12	-11995	-118	-354	0	842	-328	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
9	12	-11402	-126	-140	0	653	-335	6.28	6.28	9.42	9.42	2	0.06	0.00	0.02	0.00	0.00	24.0
10	12	-10775	84	-302	0	785	-17	6.28	6.28	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
11	12	-10595	82	-238	0	728	-19	6.28	6.28	9.42	9.42	2	0.04	0.01	0.03	0.00	0.00	24.0
12	12	-12335	-231	-267	0	771	-499	6.28	6.28	9.42	9.42	2	0.08	0.01	0.03	0.00	0.00	24.0
13	12	-12155	-234	-203	0	714	-501	6.28	6.28	9.42	9.42	2	0.08	0.01	0.02	0.00	0.00	24.0
14	12	-11532	-24	-365	0	846	-183	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
15	12	-10932	-31	-151	0	657	-190	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
16	12	-11995	-118	-354	0	842	-328	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
17	12	-11402	-126	-140	0	653	-335	6.28	6.28	9.42	9.42	2	0.06	0.00	0.02	0.00	0.00	24.0
18	12	-17218	143	-599	0	1479	450	6.28	6.28	9.42	9.42	3	0.08	0.01	0.06	0.00	0.00	24.0
19	12	-18805	-213	-374	0	1169	-860	6.28	6.28	9.42	9.42	3	0.09	0.01	0.04	0.00	0.00	24.0
20	12	-17198	-43	-85	0	940	-220	6.28	6.28	9.42	9.42	3	0.05	0.00	0.01	0.00	0.00	24.0
37	12	-15668	242	-623	0	1469	846	6.28	6.28	9.42	9.42	3	0.10	0.01	0.07	0.00	0.00	24.0
38	12	-18318	-351	-248	0	951	-1339	6.28	6.28	9.42	9.42	3	0.13	0.01	0.03	0.00	0.00	24.0
39	12	-15638	-67	234	0	571	-270	6.28	6.28	9.42	9.42	3	0.04	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-14835	-97	-328	0	1015	-349	6.28	6.28	9.42	9.42	3	0.06	0.01	0.04	0.00	0.00	24.0
2	25	-10720	84	-302	0	823	-6	6.28	6.28	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
3	25	-10540	82	-238	0	758	-9	6.28	6.28	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
4	25	-12280	-231	-267	0	804	-528	6.28	6.28	9.42	9.42	2	0.09	0.01	0.03	0.00	0.00	24.0
5	25	-12100	-234	-203	0	739	-531	6.28	6.28	9.42	9.42	2	0.08	0.01	0.02	0.00	0.00	24.0
6	25	-11475	-24	-365	0	892	-186	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
7	25	-10875	-31	-151	0	676	-194	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
8	25	-11940	-118	-354	0	886	-342	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
9	25	-11345	-126	-140	0	670	-351	6.28	6.28	9.42	9.42	2	0.06	0.00	0.02	0.00	0.00	24.0
10	25	-10720	84	-302	0	823	-6	6.28	6.28	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
11	25	-10540	82	-238	0	758	-9	6.28	6.28	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
12	25	-12280	-231	-267	0	804	-528	6.28	6.28	9.42	9.42	2	0.09	0.01	0.03	0.00	0.00	24.0
13	25	-12100	-234	-203	0	739	-531	6.28	6.28	9.42	9.42	2	0.08	0.01	0.02	0.00	0.00	24.0
14	25	-11475	-24	-365	0	892	-186	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
15	25	-10875	-31	-151	0	676	-194	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
16	25	-11940	-118	-354	0	886	-342	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
17	25	-11345	-126	-140	0	670	-351	6.28	6.28	9.42	9.42	2	0.06	0.00	0.02	0.00	0.00	24.0
18	25	-17145	114	-599	0	1554	466	6.28	6.28	9.42	9.42	3	0.08	0.01	0.06	0.00	0.00	24.0
19	25	-18730	-184	-374	0	1216	-885	6.28	6.28	9.42	9.42	3	0.09	0.01	0.04	0.00	0.00	24.0
20	25	-17125	-43	-71	0	950	-225	6.28	6.28	9.42	9.42	3	0.05	0.00	0.01	0.00	0.00	24.0
37	25	-15595	194	-623	0	1546	873	6.28	6.28	9.42	9.42	3	0.10	0.01	0.07	0.00	0.00	24.0
38	25	-18245	-303	-248	0	982	-1379	6.28	6.28	9.42	9.42	3	0.13	0.01	0.03	0.00	0.00	24.0
39	25	-15565	-67	258	0	540	-279	6.28	6.28	9.42	9.42	3	0.03	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-14762	-97	-328	0	1056	-361	6.28	6.28	9.42	9.42	3	0.06	0.01	0.04	0.00	0.00	24.0
2	38	-10665	84	-302	0	861	4	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
3	38	-10485	82	-238	0	788	2	6.28	6.28	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
4	38	-12225	-231	-267	0	838	-557	6.28	6.28	9.42	9.42	2	0.09	0.01	0.03	0.00	0.00	24.0
5	38	-12045	-234	-203	0	765	-560	6.28	6.28	9.42	9.42	2	0.09	0.01	0.02	0.00	0.00	24.0
6	38	-11418	-24	-365	0	938	-189	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
7	38	-10818	-31	-151	0	694	-198	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
8	38	-11885	-118	-354	0	931	-357	6.28	6.28	9.42	9.42	2	0.08	0.01	0.04	0.00	0.00	24.0
9	38	-11288	-126	-140	0	688	-367	6.28	6.28	9.42	9.42	2	0.07	0.00	0.02	0.00	0.00	24.0
10	38	-10665	84	-302	0	861	4	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
11	38	-10485	82	-238	0	788	2	6.28	6.28	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
12	38	-12225	-231	-267	0	838	-557	6.28	6.28	9.42	9.42	2	0.09	0.01	0.03	0.00	0.00	24.0
13	38	-12045	-234	-203	0	765	-560	6.28	6.28	9.42	9.42	2	0.09	0.01	0.02	0.00	0.00	24.0
14	38	-11418	-24	-365	0	938	-189	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
15	38	-10818	-31	-151	0	694	-198	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
16	38	-11885	-118	-354	0	931	-357	6.28	6.28	9.42	9.42	2	0.08	0.01	0.04	0.00	0.00	24.0
17	38	-11288	-126	-140	0	688	-367	6.28	6.28	9.42	9.42	2	0.07	0.00	0.02	0.00	0.00	24.0
18	38	-17072	86	-599	0	1629	479	6.28	6.28	9.42	9.42	3	0.09	0.01	0.06	0.00	0.00	24.0
19	38	-18655	-156	-374	0	1262	-907	6.28	6.28	9.42	9.42	3	0.10	0.01	0.04	0.00	0.00	24.0
20	38	-17052	-43	-59	0	958	-230	6.28	6.28	9.42	9.42	3	0.05	0.00	0.01	0.00	0.00	24.0
37	38	-15522	147	-623	0	1624	894	6.28	6.28	9.42	9.42	3	0.11	0.01	0.07	0.00	0.00	24.0
38	38	-18172	-256	-248	0	1013	-1414	6.28	6.28	9.42	9.42	3	0.14	0.01	0.03	0.00	0.00	24.0
39	38	-15492	-67	278	0	506	-287	6.28	6.28	9.42	9.42	3	0.03	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-14690	-97	-328	0	1097	-373	6.28	6.28	9.42	9.42	3	0.06	0.01	0.04	0.00	0.00	24.0
2	50	-10610	84	-302	0	898	15	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
3	50	-10430	82	-238	0	817	12	6.28	6.28	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
4	50	-12170	-231	-267	0	871	-586	6.28	6.28	9.42	9.42	2	0.09	0.01	0.03	0.00	0.00	24.0
5	50	-11990	-234	-203	0	790	-589	6.28	6.28	9.42	9.42	2	0.09	0.01	0.02	0.00	0.00	24.0
6	50	-11360	-24	-365	0	983	-192	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
7	50	-10760	-31	-151	0	713	-202	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
8	50	-11830	-118	-354	0	975	-372	6.28	6.28	9.42	9.42	2	0.08	0.01	0.04	0.00	0.00	24.0
9	50	-11230	-126	-140	0	705	-382	6.28	6.28	9.42	9.42	2	0.07	0.00	0.02	0.00	0.00	24.0
10	50	-10610	84	-302	0	898	15	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
11	50	-10430	82	-238	0	817	12	6.28	6.28	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
12	50	-12170	-231	-267	0	871	-586	6.28	6.28	9.42	9.42	2	0.09	0.01	0.03	0.00	0.00	24.0
13	50	-11990	-234	-203	0	790	-589	6.28	6.28	9.42	9.42	2	0.09	0.01	0.02	0.00	0.00	24.0
14	50	-11360	-24	-365	0	983	-192	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
15	50	-10760	-31	-151	0	713	-202	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
16	50	-11830	-118	-354	0	975	-372	6.28	6.28	9.42	9.42	2	0.08	0.01	0.04	0.00	0.00	24.0
17	50	-11230	-126	-140	0	705	-382	6.28	6.28	9.42	9.42	2	0.07	0.00	0.02	0.00	0.00	24.0
18	50	-17000	57	-599	0	1704	488	6.28	6.28	9.42	9.42	3	0.09	0.01	0.06	0.00	0.00	24.0
19	50	-18580	-127	-374	0	1309	-924	6.28	6.28	9.42	9.42	3	0.10	0.01	0.04	0.00	0.00	24.0
20	50	-16980	-43	-49	0	965	-236	6.28	6.28	9.42	9.42	3	0.05	0.00	0.01	0.00	0.00	24.0
37	50	-15450	99	-623	0	1702	909	6.28	6.28	9.42	9.42	3	0.11	0.01	0.07	0.00	0.00	24.0

38	50	-18100	-208	-248	0	1044	-1443	6.28	6.28	9.42	9.42	3	0.14	0.01	0.03	0.00	0.00	24.0
39	50	-15420	-67	294	0	471	-296	6.28	6.28	9.42	9.42	3	0.03	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

VERIFICA NODO IN TESTA AL PILASTRO, NODO NUM. 302 NON CONFINATO
(par.7.2.2 NTC2018 "La domanda di resistenza valutata con i criteri della progettazione in capacità può essere assunta non superiore alla domanda di resistenza valutata per il caso di comportamento strutturale non dissipativo.")

PROGETTAZIONE IN CAPACITA'
Asse loc. pilastro y nodo ESTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 45.0 cm, hjc= 20.0 cm
Asse loc. pilastro z nodo ESTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 30.0 cm, hjc= 50.0 cm

FxMin,inf	FxMin,sup	FxMax,sup	FySup	FzSup	Vjbdy	Vjbdz	Vres,y	Vres,z	I.R.compr.	Ashy	Ashz	PASSO	Nota
daN					daN		daN			cmq		cm	
-10430	-6862	-7944	21	283	17596	17334	60987	101645	0.29	4.13	--	12.87	

VERIFICA DI RESISTENZA CON SOLLECITAZIONI COMPORTAMENTO NON DISSIPATIVO

Asse loc. pilastro y nodo ESTERNO: Hjw= 40.0 cm, bj= 45.0 cm, hjc= 20.0 cm, db2= 45.0 cm

NC	Fx,sup	Fx,inf	Mb	Vb	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m			daN			cmq	cm	
2	-6990	-10610	-494	1542	108	1112	61233	0.02	0.00	40.00	
3	-6862	-10430	-514	1549	98	1171	61266	0.02	0.00	40.00	
4	-7944	-12170	-2121	2165	291	4946	60987	0.08	0.00	40.00	
5	-7816	-11990	-2141	2171	300	4986	61020	0.08	0.00	40.00	
6	-7473	-11360	-1040	1752	21	2547	61109	0.04	0.00	40.00	
7	-7046	-10760	-1107	1775	52	2681	61219	0.04	0.00	40.00	
8	-7759	-11830	-1528	1939	140	3633	61035	0.06	0.00	40.00	
9	-7333	-11230	-1595	1961	172	3766	61145	0.06	0.00	40.00	
10	-6990	-10610	-494	1542	108	1112	61233	0.02	0.00	40.00	
11	-6862	-10430	-514	1549	98	1171	61266	0.02	0.00	40.00	
12	-7944	-12170	-2121	2165	291	4946	60987	0.08	0.00	40.00	
13	-7816	-11990	-2141	2171	300	4986	61020	0.08	0.00	40.00	
14	-7473	-11360	-1040	1752	21	2547	61109	0.04	0.00	40.00	
15	-7046	-10760	-1107	1775	52	2681	61219	0.04	0.00	40.00	
16	-7759	-11830	-1528	1939	140	3633	61035	0.06	0.00	40.00	
17	-7333	-11230	-1595	1961	172	3766	61145	0.06	0.00	40.00	

Asse loc. pilastro z nodo ESTERNO: Hjw= 40.0 cm, bj= 30.0 cm, hjc= 50.0 cm, db1= 45.0 cm

NC	Fx,sup	Fx,inf	Mb	Vb	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m			daN			cmq	cm	
2	-6990	-10610	-2028	2074	345	4663	102055	0.05	0.00	40.00	
3	-6862	-10430	-1846	2017	317	4241	102110	0.04	0.00	40.00	
4	-7944	-12170	-1973	2057	343	4529	101645	0.04	0.00	40.00	
5	-7816	-11990	-1791	2000	315	4108	101700	0.04	0.00	40.00	
6	-7473	-11360	-2220	2136	377	5105	101848	0.05	0.00	40.00	
7	-7046	-10760	-1615	1943	283	3704	102031	0.04	0.00	40.00	
8	-7759	-11830	-2203	2131	376	5063	101725	0.05	0.00	40.00	
9	-7333	-11230	-1599	1938	283	3665	101908	0.04	0.00	40.00	
10	-6990	-10610	-2028	2074	345	4663	102055	0.05	0.00	40.00	
11	-6862	-10430	-1846	2017	317	4241	102110	0.04	0.00	40.00	
12	-7944	-12170	-1973	2057	343	4529	101645	0.04	0.00	40.00	
13	-7816	-11990	-1791	2000	315	4108	101700	0.04	0.00	40.00	
14	-7473	-11360	-2220	2136	377	5105	101848	0.05	0.00	40.00	
15	-7046	-10760	-1615	1943	283	3704	102031	0.04	0.00	40.00	
16	-7759	-11830	-2203	2131	376	5063	101725	0.05	0.00	40.00	
17	-7333	-11230	-1599	1938	283	3665	101908	0.04	0.00	40.00	

CONFRONTO E SINTESI CONCLUSIVE (si assume in ogni caso passo <= 15 cm)

I.R.compr.	Ashy	Ashz	PASSO	Nota
	cmq		cm	
0.08	--	--	15.00	**VERIFICATO**

ASTA NUM. 61 NI 294 NF 325 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 10C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-13770	-324	-95	0	-1339	2335	6.28	6.28	12.57	12.57	3	0.13	0.01	0.03	0.00	0.00	24.0
2	0	-11090	540	-144	0	-1374	1307	6.28	6.28	12.57	12.57	2	0.12	0.01	0.04	0.00	0.00	24.0
3	0	-11080	523	-23	0	-673	1308	6.28	6.28	12.57	12.57	2	0.10	0.01	0.05	0.00	0.00	24.0
4	0	-10110	-1021	-123	0	-1387	2284	6.28	6.28	12.57	12.57	2	0.18	0.02	0.10	0.00	0.00	24.0
5	0	-10090	-1038	-2	0	-686	2284	6.28	6.28	12.57	12.57	2	0.15	0.02	0.10	0.00	0.00	24.0
6	0	-10760	14	-278	0	-2197	1649	6.28	6.28	12.57	12.57	2	0.17	0.00	0.03	0.00	0.00	24.0
7	0	-10720	-43	126	0	141	1650	6.28	6.28	12.57	12.57	2	0.10	0.00	0.01	0.00	0.00	24.0
8	0	-10470	-455	-271	0	-2201	1942	6.28	6.28	12.57	12.57	2	0.19	0.01	0.04	0.00	0.00	24.0
9	0	-10420	-512	132	0	138	1943	6.28	6.28	12.57	12.57	2	0.12	0.01	0.05	0.00	0.00	24.0
10	0	-11090	540	-144	0	-1374	1307	6.28	6.28	12.57	12.57	2	0.12	0.01	0.04	0.00	0.00	24.0
11	0	-11080	523	-23	0	-673	1308	6.28	6.28	12.57	12.57	2	0.10	0.01	0.05	0.00	0.00	24.0
12	0	-10110	-1021	-123	0	-1387	2284	6.28	6.28	12.57	12.57	2	0.18	0.02	0.10	0.00	0.00	24.0
13	0	-10090	-1038	-2	0	-686	2284	6.28	6.28	12.57	12.57	2	0.15	0.02	0.10	0.00	0.00	24.0
14	0	-10760	14	-278	0	-2197	1649	6.28	6.28	12.57	12.57	2	0.17	0.00	0.03	0.00	0.00	24.0
15	0	-10720	-43	126	0	141	1650	6.28	6.28	12.57	12.57	2	0.10	0.00	0.01	0.00	0.00	24.0
16	0	-10470	-455	-271	0	-2201	1942	6.28	6.28	12.57	12.57	2	0.19	0.01	0.04	0.00	0.00	24.0
17	0	-10420	-512	132	0	138	1943	6.28	6.28	12.57	12.57	2	0.12	0.01	0.05	0.00	0.00	24.0
18	0	-17020	2114	-361	0	-3403	1611	6.28	6.28	12.57	12.57	3	0.15	0.04	0.17	0.00	0.00	24.0
19	0	-13130	-3343	-77	0	-2454	3956	6.28	6.28	12.57	12.57	3	0.23	0.06	0.30	0.00	0.00	24.0
20	0	-14730	-601	-740	0	-1915	2723	6.28	6.28	12.57	12.57	3	0.16	0.01	0.07	0.00	0.00	24.0
37	0	-18010	4024	-416	0	-3206	680	6.28	6.28	12.57	12.57	3	0.12	0.07	0.31	0.00	0.00	24.0

38	0	-11540	-5071	57	0	-1624	4586	6.28	6.28	12.57	12.57	3	0.26	0.09	0.47	0.00	0.00	24.0
39	0	-14210	-500	-1048	0	-726	2532	6.28	6.28	12.57	12.57	3	0.14	0.02	0.10	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-13672	-324	-95	0	-1327	2295	6.28	6.28	12.57	12.57	3	0.13	0.01	0.03	0.00	0.00	24.0
2	12	-11015	540	-144	0	-1356	1375	6.28	6.28	12.57	12.57	2	0.12	0.01	0.05	0.00	0.00	24.0
3	12	-11005	523	-23	0	-670	1373	6.28	6.28	12.57	12.57	2	0.10	0.01	0.05	0.00	0.00	24.0
4	12	-10034	-1021	-123	0	-1372	2156	6.28	6.28	12.57	12.57	2	0.17	0.02	0.10	0.00	0.00	24.0
5	12	-10016	-1038	-2	0	-685	2154	6.28	6.28	12.57	12.57	2	0.15	0.02	0.10	0.00	0.00	24.0
6	12	-10685	14	-278	0	-2163	1651	6.28	6.28	12.57	12.57	2	0.17	0.00	0.03	0.00	0.00	24.0
7	12	-10645	-43	126	0	126	1645	6.28	6.28	12.57	12.57	2	0.10	0.00	0.01	0.00	0.00	24.0
8	12	-10395	-455	-271	0	-2167	1885	6.28	6.28	12.57	12.57	2	0.18	0.01	0.04	0.00	0.00	24.0
9	12	-10345	-512	132	0	121	1879	6.28	6.28	12.57	12.57	2	0.11	0.01	0.05	0.00	0.00	24.0
10	12	-11015	540	-144	0	-1356	1375	6.28	6.28	12.57	12.57	2	0.12	0.01	0.05	0.00	0.00	24.0
11	12	-11005	523	-23	0	-670	1373	6.28	6.28	12.57	12.57	2	0.10	0.01	0.05	0.00	0.00	24.0
12	12	-10034	-1021	-123	0	-1372	2156	6.28	6.28	12.57	12.57	2	0.17	0.02	0.10	0.00	0.00	24.0
13	12	-10016	-1038	-2	0	-685	2154	6.28	6.28	12.57	12.57	2	0.15	0.02	0.10	0.00	0.00	24.0
14	12	-10685	14	-278	0	-2163	1651	6.28	6.28	12.57	12.57	2	0.17	0.00	0.03	0.00	0.00	24.0
15	12	-10645	-43	126	0	126	1645	6.28	6.28	12.57	12.57	2	0.10	0.00	0.01	0.00	0.00	24.0
16	12	-10395	-455	-271	0	-2167	1885	6.28	6.28	12.57	12.57	2	0.18	0.01	0.04	0.00	0.00	24.0
17	12	-10345	-512	132	0	121	1879	6.28	6.28	12.57	12.57	2	0.11	0.01	0.05	0.00	0.00	24.0
18	12	-16922	2114	-361	0	-3358	1875	6.28	6.28	12.57	12.57	3	0.15	0.04	0.17	0.00	0.00	24.0
19	12	-13032	-3343	-77	0	-2444	3538	6.28	6.28	12.57	12.57	3	0.20	0.06	0.30	0.00	0.00	24.0
20	12	-14632	-601	-707	0	-1825	2648	6.28	6.28	12.57	12.57	3	0.15	0.01	0.07	0.00	0.00	24.0
37	12	-17912	4024	-416	0	-3154	1182	6.28	6.28	12.57	12.57	3	0.13	0.07	0.31	0.00	0.00	24.0
38	12	-11442	-5071	57	0	-1631	3952	6.28	6.28	12.57	12.57	3	0.22	0.09	0.47	0.00	0.00	24.0
39	12	-14112	-500	-993	0	-599	2469	6.28	6.28	12.57	12.57	3	0.14	0.02	0.09	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-13575	-324	-95	0	-1316	2254	6.28	6.28	12.57	12.57	3	0.13	0.01	0.03	0.00	0.00	24.0
2	25	-10940	540	-144	0	-1338	1442	6.28	6.28	12.57	12.57	2	0.13	0.01	0.05	0.00	0.00	24.0
3	25	-10930	523	-23	0	-667	1438	6.28	6.28	12.57	12.57	2	0.10	0.01	0.05	0.00	0.00	24.0
4	25	-9959	-1021	-123	0	-1357	2028	6.28	6.28	12.57	12.57	2	0.16	0.02	0.10	0.00	0.00	24.0
5	25	-9942	-1038	-2	0	-685	2025	6.28	6.28	12.57	12.57	2	0.14	0.02	0.10	0.00	0.00	24.0
6	25	-10610	14	-278	0	-2128	1652	6.28	6.28	12.57	12.57	2	0.17	0.00	0.03	0.00	0.00	24.0
7	25	-10570	-43	126	0	110	1639	6.28	6.28	12.57	12.57	2	0.10	0.00	0.01	0.00	0.00	24.0
8	25	-10320	-455	-271	0	-2133	1828	6.28	6.28	12.57	12.57	2	0.18	0.01	0.04	0.00	0.00	24.0
9	25	-10270	-512	132	0	104	1815	6.28	6.28	12.57	12.57	2	0.11	0.01	0.05	0.00	0.00	24.0
10	25	-10940	540	-144	0	-1338	1442	6.28	6.28	12.57	12.57	2	0.13	0.01	0.05	0.00	0.00	24.0
11	25	-10930	523	-23	0	-667	1438	6.28	6.28	12.57	12.57	2	0.10	0.01	0.05	0.00	0.00	24.0
12	25	-9959	-1021	-123	0	-1357	2028	6.28	6.28	12.57	12.57	2	0.16	0.02	0.10	0.00	0.00	24.0
13	25	-9942	-1038	-2	0	-685	2025	6.28	6.28	12.57	12.57	2	0.14	0.02	0.10	0.00	0.00	24.0
14	25	-10610	14	-278	0	-2128	1652	6.28	6.28	12.57	12.57	2	0.17	0.00	0.03	0.00	0.00	24.0
15	25	-10570	-43	126	0	110	1639	6.28	6.28	12.57	12.57	2	0.10	0.00	0.01	0.00	0.00	24.0
16	25	-10320	-455	-271	0	-2133	1828	6.28	6.28	12.57	12.57	2	0.18	0.01	0.04	0.00	0.00	24.0
17	25	-10270	-512	132	0	104	1815	6.28	6.28	12.57	12.57	2	0.11	0.01	0.05	0.00	0.00	24.0
18	25	-16825	2114	-361	0	-3312	2139	6.28	6.28	12.57	12.57	3	0.16	0.04	0.17	0.00	0.00	24.0
19	25	-12935	-3343	-77	0	-2434	3120	6.28	6.28	12.57	12.57	3	0.18	0.06	0.30	0.00	0.00	24.0
20	25	-14535	-601	-679	0	-1738	2572	6.28	6.28	12.57	12.57	3	0.15	0.01	0.06	0.00	0.00	24.0
37	25	-17815	4024	-416	0	-3102	1685	6.28	6.28	12.57	12.57	3	0.14	0.07	0.31	0.00	0.00	24.0
38	25	-11345	-5071	57	0	-1639	3318	6.28	6.28	12.57	12.57	3	0.19	0.09	0.47	0.00	0.00	24.0
39	25	-14015	-500	-945	0	-478	2406	6.28	6.28	12.57	12.57	3	0.13	0.02	0.09	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-13478	-324	-95	0	-1304	2214	6.28	6.28	12.57	12.57	3	0.13	0.01	0.03	0.00	0.00	24.0
2	38	-10865	540	-144	0	-1320	1510	6.28	6.28	12.57	12.57	2	0.13	0.01	0.05	0.00	0.00	24.0
3	38	-10855	523	-23	0	-664	1504	6.28	6.28	12.57	12.57	2	0.11	0.01	0.05	0.00	0.00	24.0
4	38	-9884	-1021	-123	0	-1341	1901	6.28	6.28	12.57	12.57	2	0.15	0.02	0.10	0.00	0.00	24.0
5	38	-9868	-1038	-2	0	-685	1895	6.28	6.28	12.57	12.57	2	0.13	0.02	0.10	0.00	0.00	24.0
6	38	-10535	14	-278	0	-2094	1654	6.28	6.28	12.57	12.57	2	0.17	0.00	0.03	0.00	0.00	24.0
7	38	-10495	-43	126	0	94	1634	6.28	6.28	12.57	12.57	2	0.10	0.00	0.01	0.00	0.00	24.0
8	38	-10245	-455	-271	0	-2100	1771	6.28	6.28	12.57	12.57	2	0.18	0.01	0.04	0.00	0.00	24.0
9	38	-10195	-512	132	0	88	1751	6.28	6.28	12.57	12.57	2	0.11	0.01	0.05	0.00	0.00	24.0
10	38	-10865	540	-144	0	-1320	1510	6.28	6.28	12.57	12.57	2	0.13	0.01	0.05	0.00	0.00	24.0
11	38	-10855	523	-23	0	-664	1504	6.28	6.28	12.57	12.57	2	0.11	0.01	0.05	0.00	0.00	24.0
12	38	-9884	-1021	-123	0	-1341	1901	6.28	6.28	12.57	12.57	2	0.15	0.02	0.10	0.00	0.00	24.0
13	38	-9868	-1038	-2	0	-685	1895	6.28	6.28	12.57	12.57	2	0.13	0.02	0.10	0.00	0.00	24.0
14	38	-10535	14	-278	0	-2094	1654	6.28	6.28	12.57	12.57	2	0.17	0.00	0.03	0.00	0.00	24.0
15	38	-10495	-43	126	0	94	1634	6.28	6.28	12.57	12.57	2	0.10	0.00	0.01	0.00	0.00	24.0
16	38	-10245	-455	-271	0	-2100	1771	6.28	6.28	12.57	12.57	2	0.18	0.01	0.04	0.00	0.00	24.0
17	38	-10195	-512	132	0	88	1751	6.28	6.28	12.57	12.57	2	0.11	0.01	0.05	0.00	0.00	24.0
18	38	-16728	2114	-361	0	-3267	2404	6.28	6.28	12.57	12.57	3	0.17	0.04	0.17	0.00	0.00	24.0
19	38	-12838	-3343	-77	0	-2425	2702	6.28	6.28	12.57	12.57	3	0.16	0.06	0.30	0.00	0.00	24.0
20	38	-14438	-601	-655	0	-1655	2497	6.28	6.28	12.57	12.57	3	0.14	0.01	0.06	0.00	0.00	24.0
37	38	-17718	4024	-416	0	-3050	2188	6.28	6.28	12.57	12.57	3	0.15	0.07	0.31	0.00	0.00	24.0
38	38	-11248	-5071	57	0	-1646	2685	6.28	6.28	12.57	12.57	3	0.16	0.09	0.47	0.00	0.00	24.0
39	38	-13918	-500	-906	0	-362	2344	6.28	6.28	12.57	12.57	3	0.13	0.02	0.09	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-13380	-324	-95	0	-1292	2173	6.28	6.28	12.57	12.57	3	0.12	0.01	0.03	0.00	0.00	24.0
2	50	-10790	540	-144	0	-1302	1577	6.28	6.28	12.57	12.57	2	0.13	0.01	0.05	0.00	0.00	24.0
3	50	-10780	523	-23	0	-661	1569	6.28	6.28	12.57	12.57	2	0.11	0.01	0.05	0.00	0.00	24.0
4	50	-9808	-1021	-123	0	-1326	1773	6.28	6.28	12.57	12.57	2	0.15	0.02	0.10	0.00	0.00	24.0
5	50	-9794	-1038	-2	0	-685	1765	6.28	6.28	12.57	12.57	2	0.12	0.02	0.10	0.00	0.00	24.0
6	50	-10460	14	-278	0	-2059	1655	6.28	6.28	12.57	12.57	2	0.17	0.00	0.03	0.00	0.00	24.0
7	50	-10420	-43	126	0	78	1628	6.28	6.28	12.57	12.57	2	0.10	0.00	0.01	0.00	0.00	24.0
8	50	-10170	-455	-271	0	-2066	1714	6.28	6.28	12.57	12.57	2	0.17	0.01	0.04	0.00	0.00	24.0
9	50	-10120	-512	132	0	71	1687	6.28	6.28	12.57	12.57	2	0.10	0.01	0.05	0.00	0.00	24.0
10	50	-10790	540	-144	0	-1302	1577	6.28	6.28	12.57	12.57	2	0.13	0.01	0.05	0.00	0.00	24.0
11	50	-10780	523	-23	0	-661	1569	6.28	6.28	12.57	12.57	2	0.11	0.01	0.05	0.00	0.00	24.0
12	50	-9808	-1021	-123	0	-1326	1773	6.28	6.28	12.57	12.57	2	0.15	0.02	0.10	0.00	0.00	24.0
13	50	-9794	-1038	-2	0	-685	1765	6.28	6.28	12.57	12.57	2	0.12	0.02	0.10	0.00	0.00	24.0
14	50	-10460	14	-278	0	-2059	1655	6.28	6.28	12.57	12.57	2	0.17	0.00	0.03	0.00	0.00	24.0
15	50	-10420	-43	126	0	78	1628	6.28	6.28	12.57	12.57	2	0.10	0.00	0.01	0.00	0.00	24.0
16	50	-10170	-455	-271	0	-2066	1714	6.28	6.28	12.57	12.57	2	0.17	0.01	0.04	0.00	0.00	24.0
17	50	-10120	-512	132	0	71	1687	6.28	6.28	12.57	12.57	2	0.10	0.01	0.05	0.00	0.00	24.0
18	50	-16630	2114	-361	0	-3222	2668	6.28	6.28	12.57	12.57	3	0.17	0.04	0.17	0.00	0.00	24.0
19	50	-12740	-3343	-77	0	-2415	2284	6.28	6.28	12.57	12.57	3	0.14	0.06	0.27	0.00	0.00	24.0
20	50	-14340	-601	-636	0	-1574	2422	6.28	6.28	12.57	12.57	3	0.14	0.01	0.06	0.00	0.00	24.0
37	50	-17620	4024	-416	0	-2998	2691	6.28	6.28	12.57	12.57	3	0.17	0.07	0.31	0.00	0.00	24.0
38	50	-11150	-5071	57	0	-1653	2051	6.28	6.28	12.57	12.57	3	0.12	0.09	0.47	0.00	0.00	24.0
39	50	-13820	-500	-875	0	-251	2281	6.28	6.28	12.57	12.57	3	0.12	0.02	0.08	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

VERIFICA NODO IN TESTA AL PILASTRO, NODO NUM. 325 NON CONFINATO

(par.7.2.2 NTC2018 "La domanda di resistenza valutata con i criteri della progettazione in capacità può essere assunta non superiore alla domanda di resistenza valutata per il caso di comportamento strutturale non dissipativo.")

PROGETTAZIONE IN CAPACITA'

Asse loc. pilastro y nodo ESTERNO: As2(inf)= 4.02, As1(sup)= 4.02, Hjw= 40.0 cm, bj= 50.0 cm, hjc= 30.0 cm
Asse loc. pilastro z nodo: --

FxMin,inf	FxMin,sup	FxMax,sup	FySup	FzSup	Vjbdy	Vjbdz	Vres,y	Vres,z	I.R.compr.	Ashy	Ashz	PASSO	Nota
daN					daN		daN			cmq		cm	
-9794	-8107	-8475	129	57	17487	--	102326	--	0.17	--	--	40.00	

VERIFICA DI RESISTENZA CON SOLLECITAZIONI COMPORTAMENTO NON DISSIPATIVO

Asse loc. pilastro y nodo ESTERNO: Hjw= 40.0 cm, bj= 50.0 cm, hjc= 30.0 cm, db1= 45.0 cm

NC	Fx,sup	Fx,inf	Mb	Vb	Vc	Vjbd	Vres	I.R.c.	Ash	PASSO	Nota
	daN		daN*m		daN				cmq	cm	
2	-8475	-10790	-2685	2317	655	5974	102326	0.06	0.00	40.00	
3	-8468	-10780	-2666	2310	647	5935	102328	0.06	0.00	40.00	
4	-8113	-9808	-793	1694	798	1159	102442	0.01	0.00	40.00	
5	-8107	-9794	-774	1688	806	1105	102444	0.01	0.00	40.00	
6	-8356	-10460	-2044	2107	156	4891	102364	0.05	0.00	40.00	
7	-8334	-10420	-1982	2084	129	4764	102371	0.05	0.00	40.00	
8	-8247	-10170	-1477	1920	280	3367	102399	0.03	0.00	40.00	
9	-8226	-10120	-1414	1898	307	3185	102406	0.03	0.00	40.00	
10	-8475	-10790	-2685	2317	655	5974	102326	0.06	0.00	40.00	
11	-8468	-10780	-2666	2310	647	5935	102328	0.06	0.00	40.00	
12	-8113	-9808	-793	1694	798	1159	102442	0.01	0.00	40.00	
13	-8107	-9794	-774	1688	806	1105	102444	0.01	0.00	40.00	
14	-8356	-10460	-2044	2107	156	4891	102364	0.05	0.00	40.00	
15	-8334	-10420	-1982	2084	129	4764	102371	0.05	0.00	40.00	
16	-8247	-10170	-1477	1920	280	3367	102399	0.03	0.00	40.00	
17	-8226	-10120	-1414	1898	307	3185	102406	0.03	0.00	40.00	

CONFRONTO E SINTESI CONCLUSIVE (si assume in ogni caso passo <= 15 cm)

I.R.compr.	Ashy	Ashz	PASSO	Nota
	cmq		cm	
0.06	--	--	15.00	**VERIFICATO**

ASTA NUM. 62 NI 1543 NF 1542 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 6
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice resistenza Fx,M	Bielle	V,Mx	aswta cmq/m	aswto	PASSO
	cm	daN			daN*m			cmq										cm	
1	0	-3786	122	-531	0	-310	5086	15.71	15.71	9.42	9.42	3	0.10	0.01	0.04	0.00	0.00	24.0
2	0	-3979	101	-251	0	-171	3235	15.71	15.71	9.42	9.42	2	0.09	0.00	0.02	0.00	0.00	24.0
3	0	-4114	88	-356	0	-168	3143	15.71	15.71	9.42	9.42	2	0.09	0.00	0.02	0.00	0.00	24.0
4	0	-1711	100	-461	0	-310	4681	15.71	15.71	9.42	9.42	2	0.13	0.01	0.03	0.00	0.00	24.0
5	0	-1846	88	-566	0	-307	4590	15.71	15.71	9.42	9.42	2	0.13	0.01	0.04	0.00	0.00	24.0
6	0	-3027	115	-202	0	-223	3848	15.71	15.71	9.42	9.42	2	0.11	0.00	0.01	0.00	0.00	24.0
7	0	-3478	74	-551	0	-213	3542	15.71	15.71	9.42	9.42	2	0.10	0.01	0.04	0.00	0.00	24.0
8	0	-2347	115	-266	0	-265	4282	15.71	15.71	9.42	9.42	2	0.12	0.00	0.02	0.00	0.00	24.0
9	0	-2797	73	-614	0	-254	3976	15.71	15.71	9.42	9.42	2	0.11	0.01	0.04	0.00	0.00	24.0
10	0	-3979	101	-251	0	-171	3235	15.71	15.71	9.42	9.42	2	0.09	0.00	0.02	0.00	0.00	24.0
11	0	-4114	88	-356	0	-168	3143	15.71	15.71	9.42	9.42	2	0.09	0.00	0.02	0.00	0.00	24.0
12	0	-1711	100	-461	0	-310	4681	15.71	15.71	9.42	9.42	2	0.13	0.01	0.03	0.00	0.00	24.0
13	0	-1846	88	-566	0	-307	4590	15.71	15.71	9.42	9.42	2	0.13	0.01	0.04	0.00	0.00	24.0
14	0	-3027	115	-202	0	-223	3848	15.71	15.71	9.42	9.42	2	0.11	0.00	0.01	0.00	0.00	24.0
15	0	-3478	74	-551	0	-213	3542	15.71	15.71	9.42	9.42	2	0.10	0.01	0.04	0.00	0.00	24.0
16	0	-2347	115	-266	0	-265	4282	15.71	15.71	9.42	9.42	2	0.12	0.00	0.02	0.00	0.00	24.0
17	0	-2797	73	-614	0	-254	3976	15.71	15.71	9.42	9.42	2	0.11	0.01	0.04	0.00	0.00	24.0
18	0	-6179	948	-707	0	-418	6268	15.71	15.71	9.42	9.42	3	0.12	0.01	0.08	0.00	0.00	24.0
19	0	7432	-322	-1434	0	-910	13630	15.71	15.71	9.42	9.42	3	0.28	0.02	0.10	0.00	0.00	24.0
20	0	-467	304	-1343	0	-630	8926	15.71	15.71	9.42	9.42	3	0.18	0.02	0.10	0.00	0.00	24.0
37	0	-12180	1309	-289	0	-138	2228	15.71	15.71	9.42	9.42	3	0.04	0.02	0.11	0.00	0.00	24.0
38	0	10510	-809	-1501	0	-959	14500	15.71	15.71	9.42	9.42	3	0.30	0.02	0.11	0.00	0.00	24.0
39	0	-2661	236	-1349	0	-492	6658	15.71	15.71	9.42	9.42	3	0.13	0.02	0.09	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice resistenza Fx,M	Bielle	V,Mx	aswta cmq/m	aswto	PASSO
1	12	-3656	122	-531	0	-244	5101	15.71	15.71	9.42	9.42	3	0.10	0.01	0.04	0.00	0.00	24.0
2	12	-3879	101	-251	0	-140	3248	15.71	15.71	9.42	9.42	2	0.09	0.00	0.02	0.00	0.00	24.0
3	12	-4014	88	-356	0	-123	3154	15.71	15.71	9.42	9.42	2	0.09	0.00	0.02	0.00	0.00	24.0
4	12	-1611	100	-461	0	-252	4694	15.71	15.71	9.42	9.42	2	0.13	0.01	0.03	0.00	0.00	24.0
5	12	-1746	88	-566	0	-236	4601	15.71	15.71	9.42	9.42	2	0.13	0.01	0.04	0.00	0.00	24.0
6	12	-2927	115	-202	0	-198	3862	15.71	15.71	9.42	9.42	2	0.11	0.00	0.01	0.00	0.00	24.0
7	12	-3378	74	-551	0	-144	3551	15.71	15.71	9.42	9.42	2	0.10	0.01	0.04	0.00	0.00	24.0
8	12	-2247	115	-266	0	-232	4296	15.71	15.71	9.42	9.42	2	0.12	0.00	0.02	0.00	0.00	24.0
9	12	-2697	73	-614	0	-177	3985	15.71	15.71	9.42	9.42	2	0.11	0.01	0.04	0.00	0.00	24.0
10	12	-3879	101	-251	0	-140	3248	15.71	15.71	9.42	9.42	2	0.09	0.00	0.02	0.00	0.00	24.0
11	12	-4014	88	-356	0	-123	3154	15.71	15.71	9.42	9.42	2	0.09	0.00	0.02	0.00	0.00	24.0
12	12	-1611	100	-461	0	-252	4694	15.71	15.71	9.42	9.42	2	0.13	0.01	0.03	0.00	0.00	24.0
13	12	-1746	88	-566	0	-236	4601	15.71	15.71	9.42	9.42	2	0.13	0.01	0.04	0.00	0.00	24.0
14	12	-2927	115	-202	0	-198	3862	15.71	15.71	9.42	9.42	2	0.11	0.00	0.01	0.00	0.00	24.0
15	12	-3378	74	-551	0	-144	3551	15.71	15.71	9.42	9.42	2	0.10	0.01	0.04	0.00	0.00	24.0
16	12	-2247	115	-266	0	-232	4296	15.71	15.71	9.42	9.42	2	0.12	0.00	0.02	0.00	0.00	24.0
17	12	-2697	73	-614	0	-177	3985	15.71	15.71	9.42	9.42	2	0.11	0.01	0.04	0.00	0.00	24.0
18	12	-6049	948	-707	0	-330	6386	15.71	15.71	9.42	9.42	3	0.12	0.01	0.08	0.00	0.00	24.0
19	12	7562	-322	-1434	0	-731	13590	15.71	15.71	9.42	9.42	3	0.28	0.02	0.10	0.00	0.00	24.0
20	12	-337	304	-1343	0	-462	8964	15.71	15.71	9.42	9.42	3	0.18	0.02	0.10	0.00	0.00	24.0
37	12	-12050	1309	-289	0	-102	2392	15.71	15.71	9.42	9.42	3	0.04	0.02	0.11	0.00	0.00	24.0
38	12	10640	-809	-1501	0	-771	14397	15.71	15.71	9.42	9.42	3	0.30	0.02	0.11	0.00	0.00	24.0
39	12	-2531	236	-1349	0	-324	6688	15.71	15.71	9.42	9.42	3	0.13	0.02	0.09	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-3526	122	-531	0	-178	5116	15.71	15.71	9.42	9.42	3	0.10	0.01	0.04	0.00	0.00	24.0
2	25	-3779	101	-251	0	-108	3260	15.71	15.71	9.42	9.42	2	0.09	0.00	0.02	0.00	0.00	24.0
3	25	-3914	88	-356	0	-79	3165	15.71	15.71	9.42	9.42	2	0.09	0.00	0.02	0.00	0.00	24.0
4	25	-1511	100	-461	0	-194	4706	15.71	15.71	9.42	9.42	2	0.13	0.01	0.03	0.00	0.00	24.0
5	25	-1646	88	-566	0	-165	4612	15.71	15.71	9.42	9.42	2	0.13	0.01	0.04	0.00	0.00	24.0
6	25	-2827	115	-202	0	-173	3876	15.71	15.71	9.42	9.42	2	0.11	0.00	0.01	0.00	0.00	24.0
7	25	-3278	74	-551	0	-75	3561	15.71	15.71	9.42	9.42	2	0.10	0.01	0.04	0.00	0.00	24.0
8	25	-2147	115	-266	0	-198	4310	15.71	15.71	9.42	9.42	2	0.12	0.00	0.02	0.00	0.00	24.0
9	25	-2597	73	-614	0	-101	3994	15.71	15.71	9.42	9.42	2	0.11	0.01	0.04	0.00	0.00	24.0
10	25	-3779	101	-251	0	-108	3260	15.71	15.71	9.42	9.42	2	0.09	0.00	0.02	0.00	0.00	24.0
11	25	-3914	88	-356	0	-79	3165	15.71	15.71	9.42	9.42	2	0.09	0.00	0.02	0.00	0.00	24.0
12	25	-1511	100	-461	0	-194	4706	15.71	15.71	9.42	9.42	2	0.13	0.01	0.03	0.00	0.00	24.0
13	25	-1646	88	-566	0	-165	4612	15.71	15.71	9.42	9.42	2	0.13	0.01	0.04	0.00	0.00	24.0
14	25	-2827	115	-202	0	-173	3876	15.71	15.71	9.42	9.42	2	0.11	0.00	0.01	0.00	0.00	24.0
15	25	-3278	74	-551	0	-75	3561	15.71	15.71	9.42	9.42	2	0.10	0.01	0.04	0.00	0.00	24.0
16	25	-2147	115	-266	0	-198	4310	15.71	15.71	9.42	9.42	2	0.12	0.00	0.02	0.00	0.00	24.0
17	25	-2597	73	-614	0	-101	3994	15.71	15.71	9.42	9.42	2	0.11	0.01	0.04	0.00	0.00	24.0
18	25	-5919	948	-707	0	-241	6505	15.71	15.71	9.42	9.42	3	0.12	0.01	0.08	0.00	0.00	24.0
19	25	7692	-322	-1434	0	-552	13550	15.71	15.71	9.42	9.42	3	0.28	0.02	0.10	0.00	0.00	24.0
20	25	-207	304	-1343	0	-295	9002	15.71	15.71	9.42	9.42	3	0.18	0.02	0.10	0.00	0.00	24.0
37	25	-11920	1309	-289	0	-66	2556	15.71	15.71	9.42	9.42	3	0.05	0.02	0.11	0.00	0.00	24.0
38	25	10770	-809	-1501	0	-584	14295	15.71	15.71	9.42	9.42	3	0.30	0.02	0.11	0.00	0.00	24.0
39	25	-2401	236	-1349	0	-155	6717	15.71	15.71	9.42	9.42	3	0.13	0.02	0.09	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-3396	122	-531	0	-111	5132	15.71	15.71	9.42	9.42	3	0.10	0.01	0.04	0.00	0.00	24.0
2	38	-3679	101	-251	0	-77	3273	15.71	15.71	9.42	9.42	2	0.09	0.00	0.02	0.00	0.00	24.0
3	38	-3814	88	-356	0	-35	3176	15.71	15.71	9.42	9.42	2	0.09	0.00	0.02	0.00	0.00	24.0
4	38	-1411	100	-461	0	-137	4718	15.71	15.71	9.42	9.42	2	0.13	0.01	0.03	0.00	0.00	24.0
5	38	-1546	88	-566	0	-94	4622	15.71	15.71	9.42	9.42	2	0.13	0.01	0.04	0.00	0.00	24.0
6	38	-2727	115	-202	0	-147	3891	15.71	15.71	9.42	9.42	2	0.11	0.00	0.01	0.00	0.00	24.0
7	38	-3178	74	-551	0	-6	3570	15.71	15.71	9.42	9.42	2	0.10	0.01	0.04	0.00	0.00	24.0
8	38	-2047	115	-266	0	-165	4325	15.71	15.71	9.42	9.42	2	0.12	0.00	0.02	0.00	0.00	24.0
9	38	-2497	73	-614	0	-24	4004	15.71	15.71	9.42	9.42	2	0.11	0.01	0.04	0.00	0.00	24.0
10	38	-3679	101	-251	0	-77	3273	15.71	15.71	9.42	9.42	2	0.09	0.00	0.02	0.00	0.00	24.0
11	38	-3814	88	-356	0	-35	3176	15.71	15.71	9.42	9.42	2	0.09	0.00	0.02	0.00	0.00	24.0
12	38	-1411	100	-461	0	-137	4718	15.71	15.71	9.42	9.42	2	0.13	0.01	0.03	0.00	0.00	24.0
13	38	-1546	88	-566	0	-94	4622	15.71	15.71	9.42	9.42	2	0.13	0.01	0.04	0.00	0.00	24.0
14	38	-2727	115	-202	0	-147	3891	15.71	15.71	9.42	9.42	2	0.11	0.00	0.01	0.00	0.00	24.0
15	38	-3178	74	-551	0	-6	3570	15.71	15.71	9.42	9.42	2	0.10	0.01	0.04	0.00	0.00	24.0
16	38	-2047	115	-266	0	-165	4325	15.71	15.71	9.42	9.42	2	0.12	0.00	0.02	0.00	0.00	24.0
17	38	-2497	73	-614	0	-24	4004	15.71	15.71	9.42	9.42	2	0.11	0.01	0.04	0.00	0.00	24.0
18	38	-5789	948	-707	0	-153	6623	15.71	15.71	9.42	9.42	3	0.12	0.01	0.08	0.00	0.00	24.0
19	38	7822	-322	-1434	0	-373	13510	15.71	15.71	9.42	9.42	3	0.27	0.02	0.10	0.00	0.00	24.0
20	38	-77	304	-1343	0	-127	9040	15.71	15.71	9.42	9.42	3	0.17	0.02	0.10	0.00	0.00	24.0
37	38	-11790	1309	-289	0	-30	2719	15.71	15.71	9.42	9.42	3	0.05	0.02	0.11	0.00	0.00	24.0
38	38	10900	-809	-1501	0	-396	14193	15.71	15.71	9.42	9.42	3	0.29	0.02	0.11	0.00	0.00	24.0
39	38	-2271	236	-1349	0	14	6746	15.71	15.71	9.42	9.42	3	0.13	0.02	0.09	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-3266	122	-531	0	-45	5147	15.71	15.71	9.42	9.42	3	0.10	0.01	0.04	0.00	0.00	24.0
2	50	-3579	101	-251	0	-46	3285	15.71	15.71	9.42	9.42	2	0.09	0.00	0.02	0.00	0.00	24.0
3	50	-3714	88	-356	0	10	3187	15.71	15.71	9.42	9.42	2	0.08	0.00	0.02	0.00	0.00	24.0
4	50	-1311	100	-461	0	-79	4731	15.71	15.71	9.42	9.42	2	0.13	0.01	0.03	0.00	0.00	24.0
5	50	-1446	88	-566	0	-23	4633	15.71	15.71	9.42	9.42	2	0.13	0.01	0.04	0.00	0.00	24.0
6	50	-2627	115	-202	0	-122	3905	15.71	15.71	9.42	9.42	2	0.11	0.00	0.01	0.00	0.00	24.0
7	50	-3078	74	-551	0	63	3579	15.71	15.71	9.42	9.42	2	0.10	0.01	0.04	0.00	0.00	24.0
8	50	-1947	115	-266	0	-132	4339	15.71	15.71	9.42	9.42	2	0.12	0.00	0.02	0.00	0.00	24.0
9	50	-2397	73	-614	0	53	4013	15.71	15.71	9.42	9.42	2	0.11	0.01	0.04	0.00	0.00	24.0
10	50	-3579	101	-251	0	-46	3285	15.71	15.71	9.42	9.42	2	0.09	0.00	0.02	0.00	0.00	24.0
11	50	-3714	88	-356	0	10	3187	15.71	15.71	9.42	9.42	2	0.08	0.00	0.02	0.00	0.00	24.0
12	50	-1311	100	-461	0	-79	4731	15.71	15.71	9.42	9.42	2	0.13	0.01	0.03	0.00	0.00	24.0
13	50	-1446	88	-566	0	-23	4633	15.71	15.71	9.42	9.42	2	0.13	0.01	0.04	0.00	0.00	24.0
14	50	-2627	115	-202	0	-122	3905	15.71	15.71	9.42	9.42	2	0.11	0.00	0.01	0.00	0.00	24.0
15	50	-3078	74	-551	0	63	3579	15.71	15.71	9.42	9.42	2	0.10	0.01	0.04	0.00	0.00	24.0
16	50	-1947	115	-266	0	-132	4339	15.71	15.71	9.42	9.42	2	0.12	0.00	0.02	0.00	0.00	24.0
17	50	-2397	73	-614	0	53	4013	15.71	15.71	9.42	9.42	2	0.11	0.01	0.04	0.00	0.00	24.0
18	50	-5659	948	-707	0	-65	6742	15.71	15.71	9.42	9.42	3	0.13	0.01	0.08	0.00	0.00	24.0
19	50	7952	-322	-1434	0	-193	13470	15.71	15.71	9.42	9.42	3	0.27	0.02	0.10	0.00	0.00	24.0
20	50	53	304	-1343	0	41	9078	15.71	15.71	9.42	9.42	3	0.18	0.02	0.10	0.00	0.00	24.0
37	50	-11660	1309	-289	0	6	2883	15.71	15.71	9.42	9.42	3	0.05	0.02	0.11	0.00	0.00	24.0
38	50	11030	-809	-1501	0	-209	14090	15.71	15.71	9.42	9.42	3	0.29	0.02	0.11	0.00	0.00	24.0
39	50	-2141	236	-1349	0	182	6776	15.71	15.71	9.42	9.42	3	0.13	0.02	0.09	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 63 NI 1542 NF 78 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 6A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-8461	1257	-222	0	-45	6050	15.71	15.71	9.42	9.42	3	0.11	0.02	0.11	0.00	0.00	24.0
2	0	-7430	820	-17	0	-46	3959	15.71	15.71	9.42	9.42	2	0.10	0.01	0.07	0.00	0.00	24.0
3	0	-7543	796	-340	0	10	3859	15.71	15.71	9.42	9.42	2	0.10	0.01	0.07	0.00	0.00	24.0
4	0	-5475	1138	-2	0	-79	5449	15.71	15.71	9.42	9.42	2	0.14	0.01	0.10	0.00	0.00	24.0
5	0	-5588	1115	-325	0	-23	5349	15.71	15.71	9.42	9.42	2	0.14	0.01	0.10	0.00	0.00	24.0
6	0	-6613	959	365	0	-122	4597	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
7	0	-6990	880	-711	0	63	4264	15.71	15.71	9.42	9.42	2	0.11	0.01	0.08	0.00	0.00	24.0
8	0	-6027	1055	369	0	-132	5044	15.71	15.71	9.42	9.42	2	0.14	0.01	0.09	0.00	0.00	24.0
9	0	-6404	975	-706	0	53	4711	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
10	0	-7430	820	-17	0	-46	3959	15.71	15.71	9.42	9.42	2	0.10	0.01	0.07	0.00	0.00	24.0
11	0	-7543	796	-340	0	10	3859	15.71	15.71	9.42	9.42	2	0.10	0.01	0.07	0.00	0.00	24.0
12	0	-5475	1138	-2	0	-79	5449	15.71	15.71	9.42	9.42	2	0.14	0.01	0.10	0.00	0.00	24.0
13	0	-5588	1115	-325	0	-23	5349	15.71	15.71	9.42	9.42	2	0.14	0.01	0.10	0.00	0.00	24.0
14	0	-6613	959	365	0	-122	4597	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
15	0	-6990	880	-711	0	63	4264	15.71	15.71	9.42	9.42	2	0.11	0.01	0.08	0.00	0.00	24.0
16	0	-6027	1055	369	0	-132	5044	15.71	15.71	9.42	9.42	2	0.14	0.01	0.09	0.00	0.00	24.0
17	0	-6404	975	-706	0	53	4711	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
18	0	-12590	2682	-352	0	-65	8115	15.71	15.71	9.42	9.42	3	0.15	0.03	0.22	0.00	0.00	24.0
19	0	-186	2326	-29	0	-193	14690	15.71	15.71	9.42	9.42	3	0.28	0.03	0.22	0.00	0.00	24.0
20	0	-7145	2311	-1238	0	41	10330	15.71	15.71	9.42	9.42	3	0.19	0.03	0.20	0.00	0.00	24.0
37	0	-17430	2395	-471	0	6	4181	15.71	15.71	9.42	9.42	3	0.07	0.03	0.18	0.00	0.00	24.0

38	0	3238	1801	67	0	-209	15130	15.71	15.71	9.42	9.42	3	0.30	0.02	0.17	0.00	0.00	24.0
39	0	-8360	1776	-1948	0	182	7874	15.71	15.71	9.42	9.42	3	0.15	0.03	0.15	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-8331	1257	-222	0	-17	6207	15.71	15.71	9.42	9.42	3	0.12	0.02	0.11	0.00	0.00	24.0
2	12	-7330	820	-17	0	-43	4061	15.71	15.71	9.42	9.42	2	0.11	0.01	0.07	0.00	0.00	24.0
3	12	-7443	796	-340	0	52	3958	15.71	15.71	9.42	9.42	2	0.10	0.01	0.07	0.00	0.00	24.0
4	12	-5375	1138	-2	0	-79	5591	15.71	15.71	9.42	9.42	2	0.15	0.01	0.10	0.00	0.00	24.0
5	12	-5488	1115	-325	0	17	5488	15.71	15.71	9.42	9.42	2	0.14	0.01	0.10	0.00	0.00	24.0
6	12	-6513	959	365	0	-168	4717	15.71	15.71	9.42	9.42	2	0.13	0.01	0.08	0.00	0.00	24.0
7	12	-6890	880	-711	0	152	4374	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
8	12	-5927	1055	369	0	-178	5176	15.71	15.71	9.42	9.42	2	0.14	0.01	0.09	0.00	0.00	24.0
9	12	-6304	975	-706	0	141	4833	15.71	15.71	9.42	9.42	2	0.13	0.01	0.08	0.00	0.00	24.0
10	12	-7330	820	-17	0	-43	4061	15.71	15.71	9.42	9.42	2	0.11	0.01	0.07	0.00	0.00	24.0
11	12	-7443	796	-340	0	52	3958	15.71	15.71	9.42	9.42	2	0.10	0.01	0.07	0.00	0.00	24.0
12	12	-5375	1138	-2	0	-79	5591	15.71	15.71	9.42	9.42	2	0.15	0.01	0.10	0.00	0.00	24.0
13	12	-5488	1115	-325	0	17	5488	15.71	15.71	9.42	9.42	2	0.14	0.01	0.10	0.00	0.00	24.0
14	12	-6513	959	365	0	-168	4717	15.71	15.71	9.42	9.42	2	0.13	0.01	0.08	0.00	0.00	24.0
15	12	-6890	880	-711	0	152	4374	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
16	12	-5927	1055	369	0	-178	5176	15.71	15.71	9.42	9.42	2	0.14	0.01	0.09	0.00	0.00	24.0
17	12	-6304	975	-706	0	141	4833	15.71	15.71	9.42	9.42	2	0.13	0.01	0.08	0.00	0.00	24.0
18	12	-12460	2682	-352	0	-21	8450	15.71	15.71	9.42	9.42	3	0.15	0.03	0.22	0.00	0.00	24.0
19	12	-56	2326	-29	0	-190	14980	15.71	15.71	9.42	9.42	3	0.29	0.03	0.22	0.00	0.00	24.0
20	12	-7015	2311	-1238	0	196	10620	15.71	15.71	9.42	9.42	3	0.20	0.03	0.20	0.00	0.00	24.0
37	12	-17300	2395	-471	0	65	4480	15.71	15.71	9.42	9.42	3	0.08	0.03	0.18	0.00	0.00	24.0
38	12	3368	1801	67	0	-217	15355	15.71	15.71	9.42	9.42	3	0.30	0.02	0.17	0.00	0.00	24.0
39	12	-8230	1776	-1948	0	426	8096	15.71	15.71	9.42	9.42	3	0.15	0.03	0.15	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-8201	1257	-222	0	11	6364	15.71	15.71	9.42	9.42	3	0.12	0.02	0.11	0.00	0.00	24.0
2	25	-7230	820	-17	0	-41	4164	15.71	15.71	9.42	9.42	2	0.11	0.01	0.07	0.00	0.00	24.0
3	25	-7343	796	-340	0	95	4058	15.71	15.71	9.42	9.42	2	0.11	0.01	0.07	0.00	0.00	24.0
4	25	-5275	1138	-2	0	-79	5734	15.71	15.71	9.42	9.42	2	0.15	0.01	0.10	0.00	0.00	24.0
5	25	-5388	1115	-325	0	58	5627	15.71	15.71	9.42	9.42	2	0.15	0.01	0.10	0.00	0.00	24.0
6	25	-6413	959	365	0	-213	4837	15.71	15.71	9.42	9.42	2	0.13	0.01	0.08	0.00	0.00	24.0
7	25	-6790	880	-711	0	241	4484	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
8	25	-5827	1055	369	0	-224	5308	15.71	15.71	9.42	9.42	2	0.14	0.01	0.09	0.00	0.00	24.0
9	25	-6204	975	-706	0	230	4954	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
10	25	-7230	820	-17	0	-41	4164	15.71	15.71	9.42	9.42	2	0.11	0.01	0.07	0.00	0.00	24.0
11	25	-7343	796	-340	0	95	4058	15.71	15.71	9.42	9.42	2	0.11	0.01	0.07	0.00	0.00	24.0
12	25	-5275	1138	-2	0	-79	5734	15.71	15.71	9.42	9.42	2	0.15	0.01	0.10	0.00	0.00	24.0
13	25	-5388	1115	-325	0	58	5627	15.71	15.71	9.42	9.42	2	0.15	0.01	0.10	0.00	0.00	24.0
14	25	-6413	959	365	0	-213	4837	15.71	15.71	9.42	9.42	2	0.13	0.01	0.08	0.00	0.00	24.0
15	25	-6790	880	-711	0	241	4484	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
16	25	-5827	1055	369	0	-224	5308	15.71	15.71	9.42	9.42	2	0.14	0.01	0.09	0.00	0.00	24.0
17	25	-6204	975	-706	0	230	4954	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
18	25	-12330	2682	-352	0	23	8786	15.71	15.71	9.42	9.42	3	0.16	0.03	0.22	0.00	0.00	24.0
19	25	74	2326	-29	0	-186	15270	15.71	15.71	9.42	9.42	3	0.30	0.03	0.22	0.00	0.00	24.0
20	25	-6885	2311	-1238	0	351	10910	15.71	15.71	9.42	9.42	3	0.21	0.03	0.20	0.00	0.00	24.0
37	25	-17170	2395	-471	0	124	4780	15.71	15.71	9.42	9.42	3	0.09	0.03	0.18	0.00	0.00	24.0
38	25	3498	1801	67	0	-225	15580	15.71	15.71	9.42	9.42	3	0.31	0.02	0.17	0.00	0.00	24.0
39	25	-8100	1776	-1948	0	669	8318	15.71	15.71	9.42	9.42	3	0.16	0.03	0.15	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-8071	1257	-222	0	38	6522	15.71	15.71	9.42	9.42	3	0.12	0.02	0.11	0.00	0.00	24.0
2	38	-7130	820	-17	0	-39	4267	15.71	15.71	9.42	9.42	2	0.11	0.01	0.07	0.00	0.00	24.0
3	38	-7243	796	-340	0	137	4157	15.71	15.71	9.42	9.42	2	0.11	0.01	0.07	0.00	0.00	24.0
4	38	-5175	1138	-2	0	-78	5876	15.71	15.71	9.42	9.42	2	0.16	0.01	0.10	0.00	0.00	24.0
5	38	-5288	1115	-325	0	98	5767	15.71	15.71	9.42	9.42	2	0.15	0.01	0.10	0.00	0.00	24.0
6	38	-6313	959	365	0	-259	4956	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
7	38	-6690	880	-711	0	330	4593	15.71	15.71	9.42	9.42	2	0.13	0.01	0.08	0.00	0.00	24.0
8	38	-5727	1055	369	0	-271	5439	15.71	15.71	9.42	9.42	2	0.15	0.01	0.09	0.00	0.00	24.0
9	38	-6104	975	-706	0	318	5076	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
10	38	-7130	820	-17	0	-39	4267	15.71	15.71	9.42	9.42	2	0.11	0.01	0.07	0.00	0.00	24.0
11	38	-7243	796	-340	0	137	4157	15.71	15.71	9.42	9.42	2	0.11	0.01	0.07	0.00	0.00	24.0
12	38	-5175	1138	-2	0	-78	5876	15.71	15.71	9.42	9.42	2	0.16	0.01	0.10	0.00	0.00	24.0
13	38	-5288	1115	-325	0	98	5767	15.71	15.71	9.42	9.42	2	0.15	0.01	0.10	0.00	0.00	24.0
14	38	-6313	959	365	0	-259	4956	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
15	38	-6690	880	-711	0	330	4593	15.71	15.71	9.42	9.42	2	0.13	0.01	0.08	0.00	0.00	24.0
16	38	-5727	1055	369	0	-271	5439	15.71	15.71	9.42	9.42	2	0.15	0.01	0.09	0.00	0.00	24.0
17	38	-6104	975	-706	0	318	5076	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
18	38	-12200	2682	-352	0	67	9121	15.71	15.71	9.42	9.42	3	0.17	0.03	0.22	0.00	0.00	24.0
19	38	204	2326	-29	0	-182	15560	15.71	15.71	9.42	9.42	3	0.30	0.03	0.22	0.00	0.00	24.0
20	38	-6755	2311	-1238	0	506	11200	15.71	15.71	9.42	9.42	3	0.21	0.03	0.20	0.00	0.00	24.0
37	38	-17040	2395	-471	0	182	5079	15.71	15.71	9.42	9.42	3	0.09	0.03	0.18	0.00	0.00	24.0
38	38	3628	1801	67	0	-234	15805	15.71	15.71	9.42	9.42	3	0.31	0.02	0.17	0.00	0.00	24.0
39	38	-7970	1776	-1948	0	913	8539	15.71	15.71	9.42	9.42	3	0.17	0.03	0.15	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-7941	1257	-222	0	66	6679	15.71	15.71	9.42	9.42	3	0.12	0.02	0.11	0.00	0.00	24.0
2	50	-7030	820	-17	0	-37	4369	15.71	15.71	9.42	9.42	2	0.11	0.01	0.07	0.00	0.00	24.0
3	50	-7143	796	-340	0	180	4257	15.71	15.71	9.42	9.42	2	0.11	0.01	0.07	0.00	0.00	24.0
4	50	-5075	1138	-2	0	-78	6018	15.71	15.71	9.42	9.42	2	0.16	0.01	0.10	0.00	0.00	24.0
5	50	-5188	1115	-325	0	139	5906	15.71	15.71	9.42	9.42	2	0.16	0.01	0.10	0.00	0.00	24.0
6	50	-6213	959	365	0	-304	5076	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
7	50	-6590	880	-711	0	418	4703	15.71	15.71	9.42	9.42	2	0.13	0.01	0.08	0.00	0.00	24.0
8	50	-5627	1055	369	0	-317	5571	15.71	15.71	9.42	9.42	2	0.15	0.01	0.09	0.00	0.00	24.0
9	50	-6004	975	-706	0	406	5198	15.71	15.71	9.42	9.42	2	0.15	0.01	0.08	0.00	0.00	24.0
10	50	-7030	820	-17	0	-37	4369	15.71	15.71	9.42	9.42	2	0.11	0.01	0.07	0.00	0.00	24.0
11	50	-7143	796	-340	0	180	4257	15.71	15.71	9.42	9.42	2	0.11	0.01	0.07	0.00	0.00	24.0
12	50	-5075	1138	-2	0	-78	6018	15.71	15.71	9.42	9.42	2	0.16	0.01	0.10	0.00	0.00	24.0
13	50	-5188	1115	-325	0	139	5906	15.71	15.71	9.42	9.42	2	0.16	0.01	0.10	0.00	0.00	24.0
14	50	-6213	959	365	0	-304	5076	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
15	50	-6590	880	-711	0	418	4703	15.71	15.71	9.42	9.42	2	0.13	0.01	0.08	0.00	0.00	24.0
16	50	-5627	1055	369	0	-317	5571	15.71	15.71	9.42	9.42	2	0.15	0.01	0.09	0.00	0.00	24.0
17	50	-6004	975	-706	0	406	5198	15.71	15.71	9.42	9.42	2	0.15	0.01	0.08	0.00	0.00	24.0
18	50	-12070	2682	-352	0	111	9456	15.71	15.71	9.42	9.42	3	0.17	0.03	0.22	0.00	0.00	24.0
19	50	334	2326	-29	0	-179	15850	15.71	15.71	9.42	9.42	3	0.31	0.03	0.22	0.00	0.00	24.0
20	50	-6625	2311	-1238	0	660	11490	15.71	15.71	9.42	9.42	3	0.22	0.03	0.20	0.00	0.00	24.0
37	50	-16910	2395	-471	0	241	5378	15.71	15.71	9.42	9.42	3	0.10	0.03	0.18	0.00	0.00	24.0
38	50	3758	1801	67	0	-242	16030	15.71	15.71	9.42	9.42	3	0.32	0.02	0.17	0.00	0.00	24.0
39	50	-7840	1776	-1948	0	1156	8761	15.71	15.71	9.42	9.42	3	0.17	0.03	0.15	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 64 NI 1581 NF 121 SEZ. Rp B= 0.400 H= 0.800 (pilastro)

PIL. NUM. 5A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-4292	2409	161	0	-62	10480	15.71	15.71	9.42	9.42	3	0.20	0.03	0.21	0.00	0.00	24.0
2	0	-5317	1457	279	0	-66	6400	15.71	15.71	9.42	9.42	2	0.17	0.02	0.13	0.00	0.00	24.0
3	0	-5333	1465	-38	0	-9	6404	15.71	15.71	9.42	9.42	2	0.17	0.02	0.13	0.00	0.00	24.0
4	0	-1271	2241	285	0	-86	9712	15.71	15.71	9.42	9.42	2	0.26	0.03	0.21	0.00	0.00	24.0
5	0	-1286	2250	-31	0	-29	9717	15.71	15.71	9.42	9.42	2	0.26	0.03	0.21	0.00	0.00	24.0
6	0	-3883	1722	651	0	-139	7554	15.71	15.71	9.42	9.42	2	0.20	0.02	0.15	0.00	0.00	24.0
7	0	-3934	1749	-405	0	50	7568	15.71	15.71	9.42	9.42	2	0.20	0.02	0.16	0.00	0.00	24.0
8	0	-2669	1957	653	0	-145	8548	15.71	15.71	9.42	9.42	2	0.23	0.03	0.18	0.00	0.00	24.0
9	0	-2720	1985	-403	0	44	8562	15.71	15.71	9.42	9.42	2	0.23	0.03	0.18	0.00	0.00	24.0
10	0	-5317	1457	279	0	-66	6400	15.71	15.71	9.42	9.42	2	0.17	0.02	0.13	0.00	0.00	24.0
11	0	-5333	1465	-38	0	-9	6404	15.71	15.71	9.42	9.42	2	0.17	0.02	0.13	0.00	0.00	24.0
12	0	-1271	2241	285	0	-86	9712	15.71	15.71	9.42	9.42	2	0.26	0.03	0.21	0.00	0.00	24.0
13	0	-1286	2250	-31	0	-29	9717	15.71	15.71	9.42	9.42	2	0.26	0.03	0.21	0.00	0.00	24.0
14	0	-3883	1722	651	0	-139	7554	15.71	15.71	9.42	9.42	2	0.20	0.02	0.15	0.00	0.00	24.0
15	0	-3934	1749	-405	0	50	7568	15.71	15.71	9.42	9.42	2	0.20	0.02	0.16	0.00	0.00	24.0
16	0	-2669	1957	653	0	-145	8548	15.71	15.71	9.42	9.42	2	0.23	0.03	0.18	0.00	0.00	24.0
17	0	-2720	1985	-403	0	44	8562	15.71	15.71	9.42	9.42	2	0.23	0.03	0.18	0.00	0.00	24.0
18	0	-6983	4381	351	0	-104	14530	15.71	15.71	9.42	9.42	3	0.27	0.06	0.38	0.00	0.00	24.0
19	0	11010	4994	386	0	-161	25710	15.71	15.71	9.42	9.42	3	0.53	0.07	0.47	0.00	0.00	24.0
20	0	1126	4367	-661	0	59	18700	15.71	15.71	9.42	9.42	3	0.36	0.06	0.41	0.00	0.00	24.0
37	0	-15070	3436	270	0	-62	7666	15.71	15.71	9.42	9.42	3	0.14	0.04	0.27	0.00	0.00	24.0
38	0	14930	4457	329	0	-156	26300	15.71	15.71	9.42	9.42	3	0.55	0.06	0.42	0.00	0.00	24.0
39	0	-1552	3411	-1417	0	209	14620	15.71	15.71	9.42	9.42	3	0.28	0.04	0.31	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-4162	2409	161	0	-82	10780	15.71	15.71	9.42	9.42	3	0.20	0.03	0.21	0.00	0.00	24.0
2	12	-5217	1457	279	0	-101	6582	15.71	15.71	9.42	9.42	2	0.18	0.02	0.13	0.00	0.00	24.0
3	12	-5233	1465	-38	0	-5	6587	15.71	15.71	9.42	9.42	2	0.17	0.02	0.13	0.00	0.00	24.0
4	12	-1171	2241	285	0	-122	9992	15.71	15.71	9.42	9.42	2	0.27	0.03	0.21	0.00	0.00	24.0
5	12	-1186	2250	-31	0	-25	9998	15.71	15.71	9.42	9.42	2	0.27	0.03	0.21	0.00	0.00	24.0
6	12	-3783	1722	651	0	-221	7769	15.71	15.71	9.42	9.42	2	0.21	0.02	0.15	0.00	0.00	24.0
7	12	-3834	1749	-405	0	100	7787	15.71	15.71	9.42	9.42	2	0.21	0.02	0.16	0.00	0.00	24.0
8	12	-2569	1957	653	0	-227	8793	15.71	15.71	9.42	9.42	2	0.24	0.03	0.18	0.00	0.00	24.0
9	12	-2620	1985	-403	0	94	8810	15.71	15.71	9.42	9.42	2	0.24	0.03	0.18	0.00	0.00	24.0
10	12	-5217	1457	279	0	-101	6582	15.71	15.71	9.42	9.42	2	0.18	0.02	0.13	0.00	0.00	24.0
11	12	-5233	1465	-38	0	-5	6587	15.71	15.71	9.42	9.42	2	0.17	0.02	0.13	0.00	0.00	24.0
12	12	-1171	2241	285	0	-122	9992	15.71	15.71	9.42	9.42	2	0.27	0.03	0.21	0.00	0.00	24.0
13	12	-1186	2250	-31	0	-25	9998	15.71	15.71	9.42	9.42	2	0.27	0.03	0.21	0.00	0.00	24.0
14	12	-3783	1722	651	0	-221	7769	15.71	15.71	9.42	9.42	2	0.21	0.02	0.15	0.00	0.00	24.0
15	12	-3834	1749	-405	0	100	7787	15.71	15.71	9.42	9.42	2	0.21	0.02	0.16	0.00	0.00	24.0
16	12	-2569	1957	653	0	-227	8793	15.71	15.71	9.42	9.42	2	0.24	0.03	0.18	0.00	0.00	24.0
17	12	-2620	1985	-403	0	94	8810	15.71	15.71	9.42	9.42	2	0.24	0.03	0.18	0.00	0.00	24.0
18	12	-6853	4381	351	0	-148	15078	15.71	15.71	9.42	9.42	3	0.28	0.06	0.38	0.00	0.00	24.0
19	12	11140	4994	386	0	-209	26335	15.71	15.71	9.42	9.42	3	0.54	0.07	0.47	0.00	0.00	24.0
20	12	1256	4367	-661	0	141	19247	15.71	15.71	9.42	9.42	3	0.37	0.06	0.41	0.00	0.00	24.0
37	12	-14940	3436	270	0	-95	8096	15.71	15.71	9.42	9.42	3	0.15	0.04	0.27	0.00	0.00	24.0
38	12	15060	4457	329	0	-197	26858	15.71	15.71	9.42	9.42	3	0.57	0.06	0.42	0.00	0.00	24.0
39	12	-1422	3411	-1417	0	386	15045	15.71	15.71	9.42	9.42	3	0.29	0.04	0.31	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-4032	2409	161	0	-102	11080	15.71	15.71	9.42	9.42	3	0.21	0.03	0.21	0.00	0.00	24.0
2	25	-5117	1457	279	0	-136	6764	15.71	15.71	9.42	9.42	2	0.18	0.02	0.13	0.00	0.00	24.0
3	25	-5133	1465	-38	0	0	6770	15.71	15.71	9.42	9.42	2	0.18	0.02	0.13	0.00	0.00	24.0
4	25	-1071	2241	285	0	-157	10271	15.71	15.71	9.42	9.42	2	0.28	0.03	0.21	0.00	0.00	24.0
5	25	-1086	2250	-31	0	-21	10278	15.71	15.71	9.42	9.42	2	0.28	0.03	0.21	0.00	0.00	24.0
6	25	-3683	1722	651	0	-302	7984	15.71	15.71	9.42	9.42	2	0.22	0.02	0.15	0.00	0.00	24.0
7	25	-3734	1749	-405	0	151	8006	15.71	15.71	9.42	9.42	2	0.22	0.02	0.16	0.00	0.00	24.0
8	25	-2469	1957	653	0	-308	9038	15.71	15.71	9.42	9.42	2	0.25	0.03	0.18	0.00	0.00	24.0
9	25	-2520	1985	-403	0	145	9058	15.71	15.71	9.42	9.42	2	0.25	0.03	0.18	0.00	0.00	24.0
10	25	-5117	1457	279	0	-136	6764	15.71	15.71	9.42	9.42	2	0.18	0.02	0.13	0.00	0.00	24.0
11	25	-5133	1465	-38	0	0	6770	15.71	15.71	9.42	9.42	2	0.18	0.02	0.13	0.00	0.00	24.0
12	25	-1071	2241	285	0	-157	10271	15.71	15.71	9.42	9.42	2	0.28	0.03	0.21	0.00	0.00	24.0
13	25	-1086	2250	-31	0	-21	10278	15.71	15.71	9.42	9.42	2	0.28	0.03	0.21	0.00	0.00	24.0
14	25	-3683	1722	651	0	-302	7984	15.71	15.71	9.42	9.42	2	0.22	0.02	0.15	0.00	0.00	24.0
15	25	-3734	1749	-405	0	151	8006	15.71	15.71	9.42	9.42	2	0.22	0.02	0.16	0.00	0.00	24.0
16	25	-2469	1957	653	0	-308	9038	15.71	15.71	9.42	9.42	2	0.25	0.03	0.18	0.00	0.00	24.0
17	25	-2520	1985	-403	0	145	9058	15.71	15.71	9.42	9.42	2	0.25	0.03	0.18	0.00	0.00	24.0
18	25	-6723	4381	351	0	-191	15625	15.71	15.71	9.42	9.42	3	0.29	0.06	0.38	0.00	0.00	24.0
19	25	11270	4994	386	0	-257	26960	15.71	15.71	9.42	9.42	3	0.56	0.07	0.47	0.00	0.00	24.0
20	25	1386	4367	-661	0	224	19795	15.71	15.71	9.42	9.42	3	0.39	0.06	0.41	0.00	0.00	24.0
37	25	-14810	3436	270	0	-129	8525	15.71	15.71	9.42	9.42	3	0.15	0.04	0.27	0.00	0.00	24.0
38	25	15190	4457	329	0	-239	27415	15.71	15.71	9.42	9.42	3	0.58	0.06	0.42	0.00	0.00	24.0
39	25	-1292	3411	-1417	0	564	15470	15.71	15.71	9.42	9.42	3	0.30	0.04	0.31	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-3902	2409	161	0	-122	11380	15.71	15.71	9.42	9.42	3	0.22	0.03	0.21	0.00	0.00	24.0
2	38	-5017	1457	279	0	-171	6946	15.71	15.71	9.42	9.42	2	0.19	0.02	0.13	0.00	0.00	24.0
3	38	-5033	1465	-38	0	5	6954	15.71	15.71	9.42	9.42	2	0.18	0.02	0.13	0.00	0.00	24.0
4	38	-971	2241	285	0	-193	10551	15.71	15.71	9.42	9.42	2	0.29	0.03	0.21	0.00	0.00	24.0
5	38	-986	2250	-31	0	-18	10559	15.71	15.71	9.42	9.42	2	0.29	0.03	0.21	0.00	0.00	24.0
6	38	-3583	1722	651	0	-383	8200	15.71	15.71	9.42	9.42	2	0.23	0.02	0.15	0.00	0.00	24.0
7	38	-3634	1749	-405	0	202	8224	15.71	15.71	9.42	9.42	2	0.22	0.02	0.16	0.00	0.00	24.0
8	38	-2369	1957	653	0	-390	9282	15.71	15.71	9.42	9.42	2	0.26	0.03	0.18	0.00	0.00	24.0
9	38	-2420	1985	-403	0	195	9306	15.71	15.71	9.42	9.42	2	0.25	0.03	0.18	0.00	0.00	24.0
10	38	-5017	1457	279	0	-171	6946	15.71	15.71	9.42	9.42	2	0.19	0.02	0.13	0.00	0.00	24.0
11	38	-5033	1465	-38	0	5	6954	15.71	15.71	9.42	9.42	2	0.18	0.02	0.13	0.00	0.00	24.0
12	38	-971	2241	285	0	-193	10551	15.71	15.71	9.42	9.42	2	0.29	0.03	0.21	0.00	0.00	24.0
13	38	-986	2250	-31	0	-18	10559	15.71	15.71	9.42	9.42	2	0.29	0.03	0.21	0.00	0.00	24.0
14	38	-3583	1722	651	0	-383	8200	15.71	15.71	9.42	9.42	2	0.23	0.02	0.15	0.00	0.00	24.0
15	38	-3634	1749	-405	0	202	8224	15.71	15.71	9.42	9.42	2	0.22	0.02	0.16	0.00	0.00	24.0
16	38	-2369	1957	653	0	-390	9282	15.71	15.71	9.42	9.42	2	0.26	0.03	0.18	0.00	0.00	24.0
17	38	-2420	1985	-403	0	195	9306	15.71	15.71	9.42	9.42	2	0.25	0.03	0.18	0.00	0.00	24.0
18	38	-6593	4381	351	0	-235	16172	15.71	15.71	9.42	9.42	3	0.30	0.06	0.38	0.00	0.00	24.0
19	38	11400	4994	386	0	-305	27585	15.71	15.71	9.42	9.42	3	0.57	0.07	0.47	0.00	0.00	24.0
20	38	1516	4367	-661	0	307	20342	15.71	15.71	9.42	9.42	3	0.40	0.06	0.41	0.00	0.00	24.0
37	38	-14680	3436	270	0	-163	8955	15.71	15.71	9.42	9.42	3	0.16	0.04	0.27	0.00	0.00	24.0
38	38	15320	4457	329	0	-280	27973	15.71	15.71	9.42	9.42	3	0.59	0.06	0.42	0.00	0.00	24.0
39	38	-1162	3411	-1417	0	741	15895	15.71	15.71	9.42	9.42	3	0.31	0.04	0.31	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-3772	2409	161	0	-142	11680	15.71	15.71	9.42	9.42	3	0.22	0.03	0.22	0.00	0.00	24.0
2	50	-4917	1457	279	0	-206	7128	15.71	15.71	9.42	9.42	2	0.19	0.02	0.13	0.00	0.00	24.0
3	50	-4933	1465	-38	0	9	7137	15.71	15.71	9.42	9.42	2	0.19	0.02	0.13	0.00	0.00	24.0
4	50	-870	2241	285	0	-229	10830	15.71	15.71	9.42	9.42	2	0.30	0.03	0.21	0.00	0.00	24.0
5	50	-886	2250	-31	0	-14	10840	15.71	15.71	9.42	9.42	2	0.29	0.03	0.21	0.00	0.00	24.0
6	50	-3483	1722	651	0	-465	8415	15.71	15.71	9.42	9.42	2	0.24	0.02	0.15	0.00	0.00	24.0
7	50	-3534	1749	-405	0	252	8443	15.71	15.71	9.42	9.42	2	0.23	0.02	0.16	0.00	0.00	24.0
8	50	-2269	1957	653	0	-472	9527	15.71	15.71	9.42	9.42	2	0.27	0.03	0.18	0.00	0.00	24.0
9	50	-2320	1985	-403	0	245	9554	15.71	15.71	9.42	9.42	2	0.26	0.03	0.18	0.00	0.00	24.0
10	50	-4917	1457	279	0	-206	7128	15.71	15.71	9.42	9.42	2	0.19	0.02	0.13	0.00	0.00	24.0
11	50	-4933	1465	-38	0	9	7137	15.71	15.71	9.42	9.42	2	0.19	0.02	0.13	0.00	0.00	24.0
12	50	-870	2241	285	0	-229	10830	15.71	15.71	9.42	9.42	2	0.30	0.03	0.21	0.00	0.00	24.0
13	50	-886	2250	-31	0	-14	10840	15.71	15.71	9.42	9.42	2	0.29	0.03	0.21	0.00	0.00	24.0
14	50	-3483	1722	651	0	-465	8415	15.71	15.71	9.42	9.42	2	0.24	0.02	0.15	0.00	0.00	24.0
15	50	-3534	1749	-405	0	252	8443	15.71	15.71	9.42	9.42	2	0.23	0.02	0.16	0.00	0.00	24.0
16	50	-2269	1957	653	0	-472	9527	15.71	15.71	9.42	9.42	2	0.27	0.03	0.18	0.00	0.00	24.0
17	50	-2320	1985	-403	0	245	9554	15.71	15.71	9.42	9.42	2	0.26	0.03	0.18	0.00	0.00	24.0
18	50	-6463	4381	351	0	-279	16720	15.71	15.71	9.42	9.42	3	0.31	0.06	0.38	0.00	0.00	24.0
19	50	11530	4994	386	0	-354	28210	15.71	15.71	9.42	9.42	3	0.58	0.07	0.47	0.00	0.00	24.0
20	50	1646	4367	-661	0	389	20890	15.71	15.71	9.42	9.42	3	0.41	0.06	0.41	0.00	0.00	24.0
37	50	-14550	3436	270	0	-196	9384	15.71	15.71	9.42	9.42	3	0.17	0.04	0.27	0.00	0.00	24.0
38	50	15450	4457	329	0	-321	28530	15.71	15.71	9.42	9.42	3	0.60	0.06	0.42	0.00	0.00	24.0
39	50	-1032	3411	-1417	0	918	16320	15.71	15.71	9.42	9.42	3	0.32	0.04	0.32	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 65 NI 1601 NF 164 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 4A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-3131	2618	266	0	-45	11550	15.71	15.71	9.42	9.42	3	0.22	0.03	0.24	0.00	0.00	24.0
2	0	-4713	1598	352	0	-60	7025	15.71	15.71	9.42	9.42	2	0.19	0.02	0.14	0.00	0.00	24.0
3	0	-4771	1578	40	0	-4	6964	15.71	15.71	9.42	9.42	2	0.18	0.02	0.14	0.00	0.00	24.0
4	0	-46	2449	369	0	-66	10810	15.71	15.71	9.42	9.42	2	0.30	0.03	0.23	0.00	0.00	24.0
5	0	-104	2430	57	0	-10	10750	15.71	15.71	9.42	9.42	2	0.29	0.03	0.23	0.00	0.00	24.0
6	0	-3012	1918	722	0	-127	8422	15.71	15.71	9.42	9.42	2	0.23	0.02	0.17	0.00	0.00	24.0
7	0	-3205	1854	-318	0	59	8217	15.71	15.71	9.42	9.42	2	0.22	0.02	0.17	0.00	0.00	24.0
8	0	-1612	2174	727	0	-129	9557	15.71	15.71	9.42	9.42	2	0.26	0.03	0.20	0.00	0.00	24.0
9	0	-1805	2109	-313	0	58	9352	15.71	15.71	9.42	9.42	2	0.25	0.03	0.19	0.00	0.00	24.0
10	0	-4713	1598	352	0	-60	7025	15.71	15.71	9.42	9.42	2	0.19	0.02	0.14	0.00	0.00	24.0
11	0	-4771	1578	40	0	-4	6964	15.71	15.71	9.42	9.42	2	0.18	0.02	0.14	0.00	0.00	24.0
12	0	-46	2449	369	0	-66	10810	15.71	15.71	9.42	9.42	2	0.30	0.03	0.23	0.00	0.00	24.0
13	0	-104	2430	57	0	-10	10750	15.71	15.71	9.42	9.42	2	0.29	0.03	0.23	0.00	0.00	24.0
14	0	-3012	1918	722	0	-127	8422	15.71	15.71	9.42	9.42	2	0.23	0.02	0.17	0.00	0.00	24.0
15	0	-3205	1854	-318	0	59	8217	15.71	15.71	9.42	9.42	2	0.22	0.02	0.17	0.00	0.00	24.0
16	0	-1612	2174	727	0	-129	9557	15.71	15.71	9.42	9.42	2	0.26	0.03	0.20	0.00	0.00	24.0
17	0	-1805	2109	-313	0	58	9352	15.71	15.71	9.42	9.42	2	0.25	0.03	0.19	0.00	0.00	24.0
18	0	-5489	4708	494	0	-81	16050	15.71	15.71	9.42	9.42	3	0.30	0.06	0.41	0.00	0.00	24.0
19	0	14130	5445	536	0	-95	28410	15.71	15.71	9.42	9.42	3	0.60	0.07	0.51	0.00	0.00	24.0
20	0	3093	4660	-428	0	81	20470	15.71	15.71	9.42	9.42	3	0.40	0.06	0.44	0.00	0.00	24.0
37	0	-14480	3662	397	0	-61	8458	15.71	15.71	9.42	9.42	3	0.15	0.05	0.29	0.00	0.00	24.0
38	0	18210	4891	467	0	-86	29050	15.71	15.71	9.42	9.42	3	0.63	0.06	0.46	0.00	0.00	24.0
39	0	-180	3582	-1139	0	208	15830	15.71	15.71	9.42	9.42	3	0.31	0.05	0.33	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-3001	2618	266	0	-79	11877	15.71	15.71	9.42	9.42	3	0.23	0.03	0.24	0.00	0.00	24.0
2	12	-4613	1598	352	0	-104	7225	15.71	15.71	9.42	9.42	2	0.19	0.02	0.14	0.00	0.00	24.0
3	12	-4671	1578	40	0	-9	7161	15.71	15.71	9.42	9.42	2	0.19	0.02	0.14	0.00	0.00	24.0
4	12	54	2449	369	0	-112	11115	15.71	15.71	9.42	9.42	2	0.31	0.03	0.23	0.00	0.00	24.0
5	12	-4	2430	57	0	-17	11052	15.71	15.71	9.42	9.42	2	0.30	0.03	0.23	0.00	0.00	24.0
6	12	-2912	1918	722	0	-218	8662	15.71	15.71	9.42	9.42	2	0.24	0.02	0.17	0.00	0.00	24.0
7	12	-3105	1854	-318	0	99	8448	15.71	15.71	9.42	9.42	2	0.23	0.02	0.17	0.00	0.00	24.0
8	12	-1512	2174	727	0	-220	9828	15.71	15.71	9.42	9.42	2	0.27	0.03	0.20	0.00	0.00	24.0
9	12	-1705	2109	-313	0	97	9616	15.71	15.71	9.42	9.42	2	0.26	0.03	0.19	0.00	0.00	24.0
10	12	-4613	1598	352	0	-104	7225	15.71	15.71	9.42	9.42	2	0.19	0.02	0.14	0.00	0.00	24.0
11	12	-4671	1578	40	0	-9	7161	15.71	15.71	9.42	9.42	2	0.19	0.02	0.14	0.00	0.00	24.0
12	12	54	2449	369	0	-112	11115	15.71	15.71	9.42	9.42	2	0.31	0.03	0.23	0.00	0.00	24.0
13	12	-4	2430	57	0	-17	11052	15.71	15.71	9.42	9.42	2	0.30	0.03	0.23	0.00	0.00	24.0
14	12	-2912	1918	722	0	-218	8662	15.71	15.71	9.42	9.42	2	0.24	0.02	0.17	0.00	0.00	24.0
15	12	-3105	1854	-318	0	99	8448	15.71	15.71	9.42	9.42	2	0.23	0.02	0.17	0.00	0.00	24.0
16	12	-1512	2174	727	0	-220	9828	15.71	15.71	9.42	9.42	2	0.27	0.03	0.20	0.00	0.00	24.0
17	12	-1705	2109	-313	0	97	9616	15.71	15.71	9.42	9.42	2	0.26	0.03	0.19	0.00	0.00	24.0
18	12	-5359	4708	494	0	-142	16637	15.71	15.71	9.42	9.42	3	0.31	0.06	0.41	0.00	0.00	24.0
19	12	14260	5445	536	0	-162	29090	15.71	15.71	9.42	9.42	3	0.61	0.07	0.51	0.00	0.00	24.0
20	12	3223	4660	-428	0	135	21052	15.71	15.71	9.42	9.42	3	0.41	0.06	0.44	0.00	0.00	24.0
37	12	-14350	3662	397	0	-111	8916	15.71	15.71	9.42	9.42	3	0.16	0.05	0.29	0.00	0.00	24.0
38	12	18340	4891	467	0	-144	29662	15.71	15.71	9.42	9.42	3	0.64	0.06	0.42	0.00	0.00	24.0
39	12	-50	3582	-1139	0	351	16277	15.71	15.71	9.42	9.42	3	0.32	0.05	0.34	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-2871	2618	266	0	-112	12205	15.71	15.71	9.42	9.42	3	0.23	0.03	0.24	0.00	0.00	24.0
2	25	-4513	1598	352	0	-148	7424	15.71	15.71	9.42	9.42	2	0.20	0.02	0.14	0.00	0.00	24.0
3	25	-4571	1578	40	0	-14	7358	15.71	15.71	9.42	9.42	2	0.19	0.02	0.14	0.00	0.00	24.0
4	25	154	2449	369	0	-158	11420	15.71	15.71	9.42	9.42	2	0.32	0.03	0.23	0.00	0.00	24.0
5	25	96	2430	57	0	-24	11355	15.71	15.71	9.42	9.42	2	0.31	0.03	0.23	0.00	0.00	24.0
6	25	-2812	1918	722	0	-308	8901	15.71	15.71	9.42	9.42	2	0.25	0.02	0.17	0.00	0.00	24.0
7	25	-3005	1854	-318	0	139	8680	15.71	15.71	9.42	9.42	2	0.24	0.02	0.17	0.00	0.00	24.0
8	25	-1412	2174	727	0	-311	10098	15.71	15.71	9.42	9.42	2	0.28	0.03	0.20	0.00	0.00	24.0
9	25	-1605	2109	-313	0	136	9881	15.71	15.71	9.42	9.42	2	0.27	0.03	0.19	0.00	0.00	24.0
10	25	-4513	1598	352	0	-148	7424	15.71	15.71	9.42	9.42	2	0.20	0.02	0.14	0.00	0.00	24.0
11	25	-4571	1578	40	0	-14	7358	15.71	15.71	9.42	9.42	2	0.19	0.02	0.14	0.00	0.00	24.0
12	25	154	2449	369	0	-158	11420	15.71	15.71	9.42	9.42	2	0.32	0.03	0.23	0.00	0.00	24.0
13	25	96	2430	57	0	-24	11355	15.71	15.71	9.42	9.42	2	0.31	0.03	0.23	0.00	0.00	24.0
14	25	-2812	1918	722	0	-308	8901	15.71	15.71	9.42	9.42	2	0.25	0.02	0.17	0.00	0.00	24.0
15	25	-3005	1854	-318	0	139	8680	15.71	15.71	9.42	9.42	2	0.24	0.02	0.17	0.00	0.00	24.0
16	25	-1412	2174	727	0	-311	10098	15.71	15.71	9.42	9.42	2	0.28	0.03	0.20	0.00	0.00	24.0
17	25	-1605	2109	-313	0	136	9881	15.71	15.71	9.42	9.42	2	0.27	0.03	0.19	0.00	0.00	24.0
18	25	-5229	4708	494	0	-204	17225	15.71	15.71	9.42	9.42	3	0.32	0.06	0.41	0.00	0.00	24.0
19	25	14390	5445	536	0	-229	29770	15.71	15.71	9.42	9.42	3	0.63	0.07	0.51	0.00	0.00	24.0

20	25	3353	4660	-428	0	188	21635	15.71	15.71	9.42	9.42	3	0.42	0.06	0.44	0.00	0.00	24.0
37	25	-14220	3662	397	0	-161	9374	15.71	15.71	9.42	9.42	3	0.17	0.05	0.29	0.00	0.00	24.0
38	25	18470	4891	467	0	-203	30275	15.71	15.71	9.42	9.42	3	0.65	0.06	0.42	0.00	0.00	24.0
39	25	80	3582	-1139	0	493	16725	15.71	15.71	9.42	9.42	3	0.33	0.05	0.34	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-2741	2618	266	0	-145	12532	15.71	15.71	9.42	9.42	3	0.24	0.03	0.24	0.00	0.00	24.0
2	38	-4413	1598	352	0	-192	7624	15.71	15.71	9.42	9.42	2	0.21	0.02	0.14	0.00	0.00	24.0
3	38	-4471	1578	40	0	-19	7556	15.71	15.71	9.42	9.42	2	0.20	0.02	0.14	0.00	0.00	24.0
4	38	254	2449	369	0	-204	11725	15.71	15.71	9.42	9.42	2	0.33	0.03	0.23	0.00	0.00	24.0
5	38	196	2430	57	0	-31	11658	15.71	15.71	9.42	9.42	2	0.32	0.03	0.23	0.00	0.00	24.0
6	38	-2712	1918	722	0	-398	9141	15.71	15.71	9.42	9.42	2	0.25	0.02	0.17	0.00	0.00	24.0
7	38	-2905	1854	-318	0	179	8912	15.71	15.71	9.42	9.42	2	0.24	0.02	0.17	0.00	0.00	24.0
8	38	-1312	2174	727	0	-402	10369	15.71	15.71	9.42	9.42	2	0.29	0.03	0.20	0.00	0.00	24.0
9	38	-1505	2109	-313	0	175	10146	15.71	15.71	9.42	9.42	2	0.28	0.03	0.19	0.00	0.00	24.0
10	38	-4413	1598	352	0	-192	7624	15.71	15.71	9.42	9.42	2	0.21	0.02	0.14	0.00	0.00	24.0
11	38	-4471	1578	40	0	-19	7556	15.71	15.71	9.42	9.42	2	0.20	0.02	0.14	0.00	0.00	24.0
12	38	254	2449	369	0	-204	11725	15.71	15.71	9.42	9.42	2	0.33	0.03	0.23	0.00	0.00	24.0
13	38	196	2430	57	0	-31	11658	15.71	15.71	9.42	9.42	2	0.32	0.03	0.23	0.00	0.00	24.0
14	38	-2712	1918	722	0	-398	9141	15.71	15.71	9.42	9.42	2	0.25	0.02	0.17	0.00	0.00	24.0
15	38	-2905	1854	-318	0	179	8912	15.71	15.71	9.42	9.42	2	0.24	0.02	0.17	0.00	0.00	24.0
16	38	-1312	2174	727	0	-402	10369	15.71	15.71	9.42	9.42	2	0.29	0.03	0.20	0.00	0.00	24.0
17	38	-1505	2109	-313	0	175	10146	15.71	15.71	9.42	9.42	2	0.28	0.03	0.19	0.00	0.00	24.0
18	38	-5099	4708	494	0	-266	17812	15.71	15.71	9.42	9.42	3	0.34	0.06	0.41	0.00	0.00	24.0
19	38	14520	5445	536	0	-296	30450	15.71	15.71	9.42	9.42	3	0.64	0.07	0.51	0.00	0.00	24.0
20	38	3483	4660	-428	0	242	22217	15.71	15.71	9.42	9.42	3	0.44	0.06	0.44	0.00	0.00	24.0
37	38	-14090	3662	397	0	-210	9832	15.71	15.71	9.42	9.42	3	0.18	0.05	0.29	0.00	0.00	24.0
38	38	18600	4891	467	0	-261	30887	15.71	15.71	9.42	9.42	3	0.67	0.06	0.42	0.00	0.00	24.0
39	38	210	3582	-1139	0	636	17173	15.71	15.71	9.42	9.42	3	0.34	0.05	0.34	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-2611	2618	266	0	-178	12860	15.71	15.71	9.42	9.42	3	0.25	0.03	0.24	0.00	0.00	24.0
2	50	-4313	1598	352	0	-236	7824	15.71	15.71	9.42	9.42	2	0.21	0.02	0.14	0.00	0.00	24.0
3	50	-4371	1578	40	0	-24	7753	15.71	15.71	9.42	9.42	2	0.21	0.02	0.14	0.00	0.00	24.0
4	50	354	2449	369	0	-250	12030	15.71	15.71	9.42	9.42	2	0.34	0.03	0.23	0.00	0.00	24.0
5	50	296	2430	57	0	-38	11960	15.71	15.71	9.42	9.42	2	0.33	0.03	0.23	0.00	0.00	24.0
6	50	-2612	1918	722	0	-488	9381	15.71	15.71	9.42	9.42	2	0.26	0.02	0.17	0.00	0.00	24.0
7	50	-2805	1854	-318	0	218	9143	15.71	15.71	9.42	9.42	2	0.25	0.02	0.17	0.00	0.00	24.0
8	50	-1212	2174	727	0	-493	10640	15.71	15.71	9.42	9.42	2	0.30	0.03	0.20	0.00	0.00	24.0
9	50	-1405	2109	-313	0	214	10410	15.71	15.71	9.42	9.42	2	0.29	0.03	0.19	0.00	0.00	24.0
10	50	-4313	1598	352	0	-236	7824	15.71	15.71	9.42	9.42	2	0.21	0.02	0.14	0.00	0.00	24.0
11	50	-4371	1578	40	0	-24	7753	15.71	15.71	9.42	9.42	2	0.21	0.02	0.14	0.00	0.00	24.0
12	50	354	2449	369	0	-250	12030	15.71	15.71	9.42	9.42	2	0.34	0.03	0.23	0.00	0.00	24.0
13	50	296	2430	57	0	-38	11960	15.71	15.71	9.42	9.42	2	0.33	0.03	0.23	0.00	0.00	24.0
14	50	-2612	1918	722	0	-488	9381	15.71	15.71	9.42	9.42	2	0.26	0.02	0.17	0.00	0.00	24.0
15	50	-2805	1854	-318	0	218	9143	15.71	15.71	9.42	9.42	2	0.25	0.02	0.17	0.00	0.00	24.0
16	50	-1212	2174	727	0	-493	10640	15.71	15.71	9.42	9.42	2	0.30	0.03	0.20	0.00	0.00	24.0
17	50	-1405	2109	-313	0	214	10410	15.71	15.71	9.42	9.42	2	0.29	0.03	0.19	0.00	0.00	24.0
18	50	-4969	4708	494	0	-327	18400	15.71	15.71	9.42	9.42	3	0.35	0.06	0.41	0.00	0.00	24.0
19	50	14650	5445	536	0	-363	31130	15.71	15.71	9.42	9.42	3	0.66	0.07	0.47	0.00	0.00	24.0
20	50	3613	4660	-428	0	295	22800	15.71	15.71	9.42	9.42	3	0.45	0.06	0.44	0.00	0.00	24.0
37	50	-13960	3662	397	0	-260	10290	15.71	15.71	9.42	9.42	3	0.19	0.05	0.29	0.00	0.00	24.0
38	50	18730	4891	467	0	-319	31500	15.71	15.71	9.42	9.42	3	0.68	0.06	0.42	0.00	0.00	24.0
39	50	340	3582	-1139	0	778	17620	15.71	15.71	9.42	9.42	3	0.35	0.05	0.34	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 66 NI 1621 NF 207 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 3A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta aswto		PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-4262	2383	344	0	-28	10430	15.71	15.71	9.42	9.42	3	0.20	0.03	0.21	0.00	0.00	24.0
2	0	-5537	1406	411	0	-51	6175	15.71	15.71	9.42	9.42	2	0.16	0.02	0.12	0.00	0.00	24.0
3	0	-5531	1408	101	0	3	6183	15.71	15.71	9.42	9.42	2	0.16	0.02	0.12	0.00	0.00	24.0
4	0	-1026	2259	428	0	-46	9859	15.71	15.71	9.42	9.42	2	0.27	0.03	0.21	0.00	0.00	24.0
5	0	-1020	2261	118	0	8	9867	15.71	15.71	9.42	9.42	2	0.27	0.03	0.21	0.00	0.00	24.0
6	0	-3966	1702	778	0	-111	7454	15.71	15.71	9.42	9.42	2	0.20	0.02	0.15	0.00	0.00	24.0
7	0	-3945	1709	-254	0	67	7483	15.71	15.71	9.42	9.42	2	0.20	0.02	0.15	0.00	0.00	24.0
8	0	-2612	1958	783	0	-110	8559	15.71	15.71	9.42	9.42	2	0.23	0.03	0.18	0.00	0.00	24.0
9	0	-2592	1965	-249	0	68	8588	15.71	15.71	9.42	9.42	2	0.23	0.03	0.18	0.00	0.00	24.0
10	0	-5537	1406	411	0	-51	6175	15.71	15.71	9.42	9.42	2	0.16	0.02	0.12	0.00	0.00	24.0
11	0	-5531	1408	101	0	3	6183	15.71	15.71	9.42	9.42	2	0.16	0.02	0.12	0.00	0.00	24.0
12	0	-1026	2259	428	0	-46	9859	15.71	15.71	9.42	9.42	2	0.27	0.03	0.21	0.00	0.00	24.0
13	0	-1020	2261	118	0	8	9867	15.71	15.71	9.42	9.42	2	0.27	0.03	0.21	0.00	0.00	24.0
14	0	-3966	1702	778	0	-111	7454	15.71	15.71	9.42	9.42	2	0.20	0.02	0.15	0.00	0.00	24.0
15	0	-3945	1709	-254	0	67	7483	15.71	15.71	9.42	9.42	2	0.20	0.02	0.15	0.00	0.00	24.0
16	0	-2612	1958	783	0	-110	8559	15.71	15.71	9.42	9.42	2	0.23	0.03	0.18	0.00	0.00	24.0
17	0	-2592	1965	-249	0	68	8588	15.71	15.71	9.42	9.42	2	0.23	0.03	0.18	0.00	0.00	24.0
18	0	-7458	4259	621	0	-59	14040	15.71	15.71	9.42	9.42	3	0.26	0.05	0.36	0.00	0.00	24.0
19	0	11770	5049	641	0	-41	26190	15.71	15.71	9.42	9.42	3	0.54	0.07	0.47	0.00	0.00	24.0
20	0	1233	4316	-265	0	101	18680	15.71	15.71	9.42	9.42	3	0.36	0.06	0.40	0.00	0.00	24.0
37	0	-15990	3257	520	0	-57	6834	15.71	15.71	9.42	9.42	3	0.12	0.04	0.25	0.00	0.00	24.0
38	0	16060	4573	552	0	-28	27090	15.71	15.71	9.42	9.42	3	0.57	0.06	0.43	0.00	0.00	24.0
39	0	-1506	3351	-957	0	210	14560	15.71	15.71	9.42	9.42	3	0.28	0.04	0.31	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-4132	2383	344	0	-71	10728	15.71	15.71	9.42	9.42	3	0.20	0.03	0.21	0.00	0.00	24.0
2	12	-5437	1406	411	0	-102	6351	15.71	15.71	9.42	9.42	2	0.17	0.02	0.12	0.00	0.00	24.0
3	12	-5431	1408	101	0	-10	6359	15.71	15.71	9.42	9.42	2	0.17	0.02	0.12	0.00	0.00	24.0
4	12	-926	2259	428	0	-99	10142	15.71	15.71	9.42	9.42	2	0.28	0.03	0.21	0.00	0.00	24.0
5	12	-920	2261	118	0	-7	10150	15.71	15.71	9.42	9.42	2	0.28	0.03	0.21	0.00	0.00	24.0
6	12	-3866	1702	778	0	-209	7667	15.71	15.71	9.42	9.42	2	0.21	0.02	0.15	0.00	0.00	24.0
7	12	-3845	1709	-254	0	98	7696	15.71	15.71	9.42	9.42	2	0.21	0.02	0.15	0.00	0.00	24.0
8	12	-2512	1958	783	0	-208	8804	15.71	15.71	9.42	9.42	2	0.24	0.03	0.18	0.00	0.00	24.0
9	12	-2492	1965	-249	0	99	8834	15.71	15.71	9.42	9.42	2	0.24	0.03	0.18	0.00	0.00	24.0
10	12	-5437	1406	411	0	-102	6351	15.71	15.71	9.42	9.42	2	0.17	0.02	0.12	0.00	0.00	24.0
11	12	-5431	1408	101	0	-10	6359	15.71	15.71	9.42	9.42	2	0.17	0.02	0.12	0.00	0.00	24.0
12	12	-926	2259	428	0	-99	10142	15.71	15.71	9.42	9.42	2	0.28	0.03	0.21	0.00	0.00	24.0
13	12	-920	2261	118	0	-7	10150	15.71	15.71	9.42	9.42	2	0.28	0.03	0.21	0.00	0.00	24.0
14	12	-3866	1702	778	0	-209	7667	15.71	15.71	9.42	9.42	2	0.21	0.02	0.15	0.00	0.00	24.0
15	12	-3845	1709	-254	0	98	7696	15.71	15.71	9.42	9.42	2	0.21	0.02	0.15	0.00	0.00	24.0

16	12	-2512	1958	783	0	-208	8804	15.71	15.71	9.42	9.42	2	0.24	0.03	0.18	0.00	0.00	24.0
17	12	-2492	1965	-249	0	99	8834	15.71	15.71	9.42	9.42	2	0.24	0.03	0.18	0.00	0.00	24.0
18	12	-7328	4259	621	0	-136	14572	15.71	15.71	9.42	9.42	3	0.27	0.05	0.36	0.00	0.00	24.0
19	12	11900	5049	641	0	-121	26822	15.71	15.71	9.42	9.42	3	0.55	0.07	0.47	0.00	0.00	24.0
20	12	1363	4316	-265	0	134	19217	15.71	15.71	9.42	9.42	3	0.37	0.06	0.40	0.00	0.00	24.0
37	12	-15860	3257	520	0	-122	7241	15.71	15.71	9.42	9.42	3	0.13	0.04	0.25	0.00	0.00	24.0
38	12	16190	4573	552	0	-97	27662	15.71	15.71	9.42	9.42	3	0.59	0.06	0.43	0.00	0.00	24.0
39	12	-1376	3351	-957	0	329	14980	15.71	15.71	9.42	9.42	3	0.29	0.04	0.31	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-4002	2383	344	0	-114	11025	15.71	15.71	9.42	9.42	3	0.21	0.03	0.21	0.00	0.00	24.0
2	25	-5337	1406	411	0	-153	6526	15.71	15.71	9.42	9.42	2	0.18	0.02	0.12	0.00	0.00	24.0
3	25	-5331	1408	101	0	-23	6536	15.71	15.71	9.42	9.42	2	0.17	0.02	0.12	0.00	0.00	24.0
4	25	-826	2259	428	0	-153	10425	15.71	15.71	9.42	9.42	2	0.29	0.03	0.21	0.00	0.00	24.0
5	25	-820	2261	118	0	-22	10434	15.71	15.71	9.42	9.42	2	0.28	0.03	0.21	0.00	0.00	24.0
6	25	-3766	1702	778	0	-306	7880	15.71	15.71	9.42	9.42	2	0.22	0.02	0.15	0.00	0.00	24.0
7	25	-3745	1709	-254	0	130	7910	15.71	15.71	9.42	9.42	2	0.21	0.02	0.15	0.00	0.00	24.0
8	25	-2412	1958	783	0	-306	9048	15.71	15.71	9.42	9.42	2	0.25	0.03	0.18	0.00	0.00	24.0
9	25	-2392	1965	-249	0	130	9079	15.71	15.71	9.42	9.42	2	0.25	0.03	0.18	0.00	0.00	24.0
10	25	-5337	1406	411	0	-153	6526	15.71	15.71	9.42	9.42	2	0.18	0.02	0.12	0.00	0.00	24.0
11	25	-5331	1408	101	0	-23	6536	15.71	15.71	9.42	9.42	2	0.17	0.02	0.12	0.00	0.00	24.0
12	25	-826	2259	428	0	-153	10425	15.71	15.71	9.42	9.42	2	0.29	0.03	0.21	0.00	0.00	24.0
13	25	-820	2261	118	0	-22	10434	15.71	15.71	9.42	9.42	2	0.28	0.03	0.21	0.00	0.00	24.0
14	25	-3766	1702	778	0	-306	7880	15.71	15.71	9.42	9.42	2	0.22	0.02	0.15	0.00	0.00	24.0
15	25	-3745	1709	-254	0	130	7910	15.71	15.71	9.42	9.42	2	0.21	0.02	0.15	0.00	0.00	24.0
16	25	-2412	1958	783	0	-306	9048	15.71	15.71	9.42	9.42	2	0.25	0.03	0.18	0.00	0.00	24.0
17	25	-2392	1965	-249	0	130	9079	15.71	15.71	9.42	9.42	2	0.25	0.03	0.18	0.00	0.00	24.0
18	25	-7198	4259	621	0	-214	15105	15.71	15.71	9.42	9.42	3	0.28	0.05	0.36	0.00	0.00	24.0
19	25	12030	5049	641	0	-201	27455	15.71	15.71	9.42	9.42	3	0.57	0.07	0.47	0.00	0.00	24.0
20	25	1493	4316	-265	0	167	19755	15.71	15.71	9.42	9.42	3	0.38	0.06	0.40	0.00	0.00	24.0
37	25	-15730	3257	520	0	-187	7648	15.71	15.71	9.42	9.42	3	0.14	0.04	0.25	0.00	0.00	24.0
38	25	16320	4573	552	0	-166	28235	15.71	15.71	9.42	9.42	3	0.60	0.06	0.43	0.00	0.00	24.0
39	25	-1246	3351	-957	0	449	15400	15.71	15.71	9.42	9.42	3	0.30	0.04	0.31	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-3872	2383	344	0	-157	11322	15.71	15.71	9.42	9.42	3	0.21	0.03	0.21	0.00	0.00	24.0
2	38	-5237	1406	411	0	-205	6702	15.71	15.71	9.42	9.42	2	0.18	0.02	0.12	0.00	0.00	24.0
3	38	-5231	1408	101	0	-35	6712	15.71	15.71	9.42	9.42	2	0.18	0.02	0.12	0.00	0.00	24.0
4	38	-726	2259	428	0	-206	10707	15.71	15.71	9.42	9.42	2	0.30	0.03	0.21	0.00	0.00	24.0
5	38	-720	2261	118	0	-37	10717	15.71	15.71	9.42	9.42	2	0.29	0.03	0.21	0.00	0.00	24.0
6	38	-3666	1702	778	0	-403	8092	15.71	15.71	9.42	9.42	2	0.23	0.02	0.15	0.00	0.00	24.0
7	38	-3645	1709	-254	0	162	8124	15.71	15.71	9.42	9.42	2	0.22	0.02	0.15	0.00	0.00	24.0
8	38	-2312	1958	783	0	-404	9293	15.71	15.71	9.42	9.42	2	0.26	0.03	0.18	0.00	0.00	24.0
9	38	-2292	1965	-249	0	161	9324	15.71	15.71	9.42	9.42	2	0.25	0.03	0.18	0.00	0.00	24.0
10	38	-5237	1406	411	0	-205	6702	15.71	15.71	9.42	9.42	2	0.18	0.02	0.12	0.00	0.00	24.0
11	38	-5231	1408	101	0	-35	6712	15.71	15.71	9.42	9.42	2	0.18	0.02	0.12	0.00	0.00	24.0
12	38	-726	2259	428	0	-206	10707	15.71	15.71	9.42	9.42	2	0.30	0.03	0.21	0.00	0.00	24.0
13	38	-720	2261	118	0	-37	10717	15.71	15.71	9.42	9.42	2	0.29	0.03	0.21	0.00	0.00	24.0
14	38	-3666	1702	778	0	-403	8092	15.71	15.71	9.42	9.42	2	0.23	0.02	0.15	0.00	0.00	24.0
15	38	-3645	1709	-254	0	162	8124	15.71	15.71	9.42	9.42	2	0.22	0.02	0.15	0.00	0.00	24.0
16	38	-2312	1958	783	0	-404	9293	15.71	15.71	9.42	9.42	2	0.26	0.03	0.18	0.00	0.00	24.0
17	38	-2292	1965	-249	0	161	9324	15.71	15.71	9.42	9.42	2	0.25	0.03	0.18	0.00	0.00	24.0
18	38	-7068	4259	621	0	-292	15638	15.71	15.71	9.42	9.42	3	0.29	0.05	0.37	0.00	0.00	24.0
19	38	12160	5049	641	0	-282	28088	15.71	15.71	9.42	9.42	3	0.58	0.07	0.47	0.00	0.00	24.0
20	38	1623	4316	-265	0	201	20293	15.71	15.71	9.42	9.42	3	0.40	0.06	0.40	0.00	0.00	24.0
37	38	-15600	3257	520	0	-252	8056	15.71	15.71	9.42	9.42	3	0.15	0.04	0.25	0.00	0.00	24.0
38	38	16450	4573	552	0	-235	28808	15.71	15.71	9.42	9.42	3	0.61	0.06	0.43	0.00	0.00	24.0
39	38	-1116	3351	-957	0	569	15820	15.71	15.71	9.42	9.42	3	0.31	0.04	0.31	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-3742	2383	344	0	-200	11620	15.71	15.71	9.42	9.42	3	0.22	0.03	0.21	0.00	0.00	24.0
2	50	-5137	1406	411	0	-256	6878	15.71	15.71	9.42	9.42	2	0.19	0.02	0.12	0.00	0.00	24.0
3	50	-5131	1408	101	0	-48	6888	15.71	15.71	9.42	9.42	2	0.18	0.02	0.12	0.00	0.00	24.0
4	50	-626	2259	428	0	-260	10990	15.71	15.71	9.42	9.42	2	0.30	0.03	0.21	0.00	0.00	24.0
5	50	-620	2261	118	0	-52	11000	15.71	15.71	9.42	9.42	2	0.30	0.03	0.21	0.00	0.00	24.0
6	50	-3566	1702	778	0	-500	8305	15.71	15.71	9.42	9.42	2	0.23	0.02	0.15	0.00	0.00	24.0
7	50	-3545	1709	-254	0	194	8337	15.71	15.71	9.42	9.42	2	0.23	0.02	0.15	0.00	0.00	24.0
8	50	-2212	1958	783	0	-501	9538	15.71	15.71	9.42	9.42	2	0.27	0.03	0.18	0.00	0.00	24.0
9	50	-2192	1965	-249	0	193	9570	15.71	15.71	9.42	9.42	2	0.26	0.03	0.18	0.00	0.00	24.0
10	50	-5137	1406	411	0	-256	6878	15.71	15.71	9.42	9.42	2	0.19	0.02	0.12	0.00	0.00	24.0
11	50	-5131	1408	101	0	-48	6888	15.71	15.71	9.42	9.42	2	0.18	0.02	0.12	0.00	0.00	24.0
12	50	-626	2259	428	0	-260	10990	15.71	15.71	9.42	9.42	2	0.30	0.03	0.21	0.00	0.00	24.0
13	50	-620	2261	118	0	-52	11000	15.71	15.71	9.42	9.42	2	0.30	0.03	0.21	0.00	0.00	24.0
14	50	-3566	1702	778	0	-500	8305	15.71	15.71	9.42	9.42	2	0.23	0.02	0.15	0.00	0.00	24.0
15	50	-3545	1709	-254	0	194	8337	15.71	15.71	9.42	9.42	2	0.23	0.02	0.15	0.00	0.00	24.0
16	50	-2212	1958	783	0	-501	9538	15.71	15.71	9.42	9.42	2	0.27	0.03	0.18	0.00	0.00	24.0
17	50	-2192	1965	-249	0	193	9570	15.71	15.71	9.42	9.42	2	0.26	0.03	0.18	0.00	0.00	24.0
18	50	-6938	4259	621	0	-369	16170	15.71	15.71	9.42	9.42	3	0.30	0.05	0.37	0.00	0.00	24.0
19	50	12290	5049	641	0	-362	28720	15.71	15.71	9.42	9.42	3	0.60	0.07	0.47	0.00	0.00	24.0
20	50	1753	4316	-265	0	234	20830	15.71	15.71	9.42	9.42	3	0.41	0.06	0.40	0.00	0.00	24.0
37	50	-15470	3257	520	0	-317	8463	15.71	15.71	9.42	9.42	3	0.15	0.04	0.25	0.00	0.00	24.0
38	50	16580	4573	552	0	-304	29380	15.71	15.71	9.42	9.42	3	0.63	0.06	0.43	0.00	0.00	24.0
39	50	-986	3351	-957	0	688	16240	15.71	15.71	9.42	9.42	3	0.32	0.04	0.31	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 67 NI 1641 NF 250 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 2A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-8739	1306	366	0	34	6251	15.71	15.71	9.42	9.42	3	0.12	0.02	0.11	0.00	0.00	24.0
2	0	-8538	641	462	0	-10	3324	15.71	15.71	9.42	9.42	2	0.09	0.01	0.05	0.00	0.00	24.0
3	0	-8466	669	161	0	44	3409	15.71	15.71	9.42	9.42	2	0.09	0.01	0.06	0.00	0.00	24.0
4	0	-4979	1341	403	0	9	6209	15.71	15.71	9.42	9.42	2	0.16	0.02	0.12	0.00	0.00	24.0
5	0	-4907	1368	102	0	62	6294	15.71	15.71	9.42	9.42	2	0.17	0.02	0.12	0.00	0.00	24.0
6	0	-7376	854	793	0	-66	4234	15.71	15.71	9.42	9.42	2	0.11	0.01	0.07	0.00	0.00	24.0
7	0	-7136	946	-212	0	112	4518	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
8	0	-6309	1064	776	0	-60	5100	15.71	15.71	9.42	9.42	2	0.13	0.01	0.09	0.00	0.00	24.0
9	0	-6068	1156	-230	0	118	5383	15.71	15.71	9.42	9.42	2	0.14	0.01	0.10	0.00	0.00	24.0
10	0	-8538	641	462	0	-10	3324	15.71	15.71	9.42	9.42	2	0.09	0.01	0.05	0.00	0.00	24.0
11	0	-8466	669	161	0	44	3409	15.71	15.71	9.42	9.42	2	0.09	0.01	0.06	0.00	0.00	24.0

12	0	-4979	1341	403	0	9	6209	15.71	15.71	9.42	9.42	2	0.16	0.02	0.12	0.00	0.00	24.0
13	0	-4907	1368	102	0	62	6294	15.71	15.71	9.42	9.42	2	0.17	0.02	0.12	0.00	0.00	24.0
14	0	-7376	854	793	0	-66	4234	15.71	15.71	9.42	9.42	2	0.11	0.01	0.07	0.00	0.00	24.0
15	0	-7136	946	-212	0	112	4518	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
16	0	-6309	1064	776	0	-60	5100	15.71	15.71	9.42	9.42	2	0.13	0.01	0.09	0.00	0.00	24.0
17	0	-6068	1156	-230	0	118	5383	15.71	15.71	9.42	9.42	2	0.14	0.01	0.10	0.00	0.00	24.0
18	0	-14860	2337	756	0	51	6833	15.71	15.71	9.42	9.42	3	0.12	0.03	0.18	0.00	0.00	24.0
19	0	2099	3025	506	0	95	17210	15.71	15.71	9.42	9.42	3	0.34	0.04	0.28	0.00	0.00	24.0
20	0	-6570	2542	-223	0	214	11350	15.71	15.71	9.42	9.42	3	0.21	0.03	0.22	0.00	0.00	24.0
37	0	-21320	1658	754	0	23	1492	15.71	15.71	9.42	9.42	3	0.03	0.02	0.12	0.00	0.00	24.0
38	0	6950	2805	336	0	97	18790	15.71	15.71	9.42	9.42	3	0.38	0.04	0.26	0.00	0.00	24.0
39	0	-7499	2000	-878	0	296	9016	15.71	15.71	9.42	9.42	3	0.17	0.03	0.17	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-8609	1306	366	0	-12	6415	15.71	15.71	9.42	9.42	3	0.12	0.02	0.11	0.00	0.00	24.0
2	12	-8438	641	462	0	-68	3404	15.71	15.71	9.42	9.42	2	0.09	0.01	0.05	0.00	0.00	24.0
3	12	-8366	669	161	0	24	3492	15.71	15.71	9.42	9.42	2	0.09	0.01	0.06	0.00	0.00	24.0
4	12	-4879	1341	403	0	-42	6376	15.71	15.71	9.42	9.42	2	0.17	0.02	0.12	0.00	0.00	24.0
5	12	-4807	1368	102	0	49	6465	15.71	15.71	9.42	9.42	2	0.17	0.02	0.12	0.00	0.00	24.0
6	12	-7276	854	793	0	-165	4341	15.71	15.71	9.42	9.42	2	0.12	0.01	0.07	0.00	0.00	24.0
7	12	-7036	946	-212	0	139	4636	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
8	12	-6209	1064	776	0	-157	5233	15.71	15.71	9.42	9.42	2	0.14	0.01	0.09	0.00	0.00	24.0
9	12	-5968	1156	-230	0	147	5528	15.71	15.71	9.42	9.42	2	0.15	0.01	0.10	0.00	0.00	24.0
10	12	-8438	641	462	0	-68	3404	15.71	15.71	9.42	9.42	2	0.09	0.01	0.05	0.00	0.00	24.0
11	12	-8366	669	161	0	24	3492	15.71	15.71	9.42	9.42	2	0.09	0.01	0.06	0.00	0.00	24.0
12	12	-4879	1341	403	0	-42	6376	15.71	15.71	9.42	9.42	2	0.17	0.02	0.12	0.00	0.00	24.0
13	12	-4807	1368	102	0	49	6465	15.71	15.71	9.42	9.42	2	0.17	0.02	0.12	0.00	0.00	24.0
14	12	-7276	854	793	0	-165	4341	15.71	15.71	9.42	9.42	2	0.12	0.01	0.07	0.00	0.00	24.0
15	12	-7036	946	-212	0	139	4636	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
16	12	-6209	1064	776	0	-157	5233	15.71	15.71	9.42	9.42	2	0.14	0.01	0.09	0.00	0.00	24.0
17	12	-5968	1156	-230	0	147	5528	15.71	15.71	9.42	9.42	2	0.15	0.01	0.10	0.00	0.00	24.0
18	12	-14730	2337	756	0	-44	7125	15.71	15.71	9.42	9.42	3	0.13	0.03	0.18	0.00	0.00	24.0
19	12	2229	3025	506	0	32	17588	15.71	15.71	9.42	9.42	3	0.34	0.04	0.28	0.00	0.00	24.0
20	12	-6440	2542	-223	0	242	11667	15.71	15.71	9.42	9.42	3	0.22	0.03	0.22	0.00	0.00	24.0
37	12	-21190	1658	754	0	-71	1699	15.71	15.71	9.42	9.42	3	0.03	0.02	0.12	0.00	0.00	24.0
38	12	7080	2805	336	0	55	19140	15.71	15.71	9.42	9.42	3	0.38	0.04	0.26	0.00	0.00	24.0
39	12	-7369	2000	-878	0	406	9267	15.71	15.71	9.42	9.42	3	0.17	0.03	0.17	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-8479	1306	366	0	-58	6578	15.71	15.71	9.42	9.42	3	0.12	0.02	0.11	0.00	0.00	24.0
2	25	-8338	641	462	0	-125	3484	15.71	15.71	9.42	9.42	2	0.09	0.01	0.05	0.00	0.00	24.0
3	25	-8266	669	161	0	4	3576	15.71	15.71	9.42	9.42	2	0.09	0.01	0.06	0.00	0.00	24.0
4	25	-4779	1341	403	0	-92	6544	15.71	15.71	9.42	9.42	2	0.17	0.02	0.12	0.00	0.00	24.0
5	25	-4707	1368	102	0	37	6636	15.71	15.71	9.42	9.42	2	0.18	0.02	0.12	0.00	0.00	24.0
6	25	-7176	854	793	0	-264	4448	15.71	15.71	9.42	9.42	2	0.12	0.01	0.07	0.00	0.00	24.0
7	25	-6936	946	-212	0	165	4754	15.71	15.71	9.42	9.42	2	0.13	0.01	0.08	0.00	0.00	24.0
8	25	-6109	1064	776	0	-254	5366	15.71	15.71	9.42	9.42	2	0.15	0.01	0.09	0.00	0.00	24.0
9	25	-5868	1156	-230	0	175	5672	15.71	15.71	9.42	9.42	2	0.15	0.01	0.10	0.00	0.00	24.0
10	25	-8338	641	462	0	-125	3484	15.71	15.71	9.42	9.42	2	0.09	0.01	0.05	0.00	0.00	24.0
11	25	-8266	669	161	0	4	3576	15.71	15.71	9.42	9.42	2	0.09	0.01	0.06	0.00	0.00	24.0
12	25	-4779	1341	403	0	-92	6544	15.71	15.71	9.42	9.42	2	0.17	0.02	0.12	0.00	0.00	24.0
13	25	-4707	1368	102	0	37	6636	15.71	15.71	9.42	9.42	2	0.18	0.02	0.12	0.00	0.00	24.0
14	25	-7176	854	793	0	-264	4448	15.71	15.71	9.42	9.42	2	0.12	0.01	0.07	0.00	0.00	24.0
15	25	-6936	946	-212	0	165	4754	15.71	15.71	9.42	9.42	2	0.13	0.01	0.08	0.00	0.00	24.0
16	25	-6109	1064	776	0	-254	5366	15.71	15.71	9.42	9.42	2	0.15	0.01	0.09	0.00	0.00	24.0
17	25	-5868	1156	-230	0	175	5672	15.71	15.71	9.42	9.42	2	0.15	0.01	0.10	0.00	0.00	24.0
18	25	-14600	2337	756	0	-138	7418	15.71	15.71	9.42	9.42	3	0.13	0.03	0.18	0.00	0.00	24.0
19	25	2359	3025	506	0	-32	17965	15.71	15.71	9.42	9.42	3	0.35	0.04	0.28	0.00	0.00	24.0
20	25	-6310	2542	-223	0	270	11985	15.71	15.71	9.42	9.42	3	0.23	0.03	0.22	0.00	0.00	24.0
37	25	-21060	1658	754	0	-165	1906	15.71	15.71	9.42	9.42	3	0.03	0.02	0.12	0.00	0.00	24.0
38	25	7210	2805	336	0	13	19490	15.71	15.71	9.42	9.42	3	0.39	0.04	0.26	0.00	0.00	24.0
39	25	-7239	2000	-878	0	515	9518	15.71	15.71	9.42	9.42	3	0.18	0.03	0.17	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-8349	1306	366	0	-103	6742	15.71	15.71	9.42	9.42	3	0.13	0.02	0.11	0.00	0.00	24.0
2	38	-8238	641	462	0	-183	3565	15.71	15.71	9.42	9.42	2	0.10	0.01	0.05	0.00	0.00	24.0
3	38	-8166	669	161	0	-17	3660	15.71	15.71	9.42	9.42	2	0.09	0.01	0.06	0.00	0.00	24.0
4	38	-4679	1341	403	0	-142	6712	15.71	15.71	9.42	9.42	2	0.18	0.02	0.12	0.00	0.00	24.0
5	38	-4607	1368	102	0	24	6807	15.71	15.71	9.42	9.42	2	0.18	0.02	0.12	0.00	0.00	24.0
6	38	-7076	854	793	0	-363	4554	15.71	15.71	9.42	9.42	2	0.13	0.01	0.07	0.00	0.00	24.0
7	38	-6836	946	-212	0	192	4873	15.71	15.71	9.42	9.42	2	0.13	0.01	0.08	0.00	0.00	24.0
8	38	-6009	1064	776	0	-351	5499	15.71	15.71	9.42	9.42	2	0.15	0.01	0.09	0.00	0.00	24.0
9	38	-5768	1156	-230	0	204	5816	15.71	15.71	9.42	9.42	2	0.16	0.01	0.10	0.00	0.00	24.0
10	38	-8238	641	462	0	-183	3565	15.71	15.71	9.42	9.42	2	0.10	0.01	0.05	0.00	0.00	24.0
11	38	-8166	669	161	0	-17	3660	15.71	15.71	9.42	9.42	2	0.09	0.01	0.06	0.00	0.00	24.0
12	38	-4679	1341	403	0	-142	6712	15.71	15.71	9.42	9.42	2	0.18	0.02	0.12	0.00	0.00	24.0
13	38	-4607	1368	102	0	24	6807	15.71	15.71	9.42	9.42	2	0.18	0.02	0.12	0.00	0.00	24.0
14	38	-7076	854	793	0	-363	4554	15.71	15.71	9.42	9.42	2	0.13	0.01	0.07	0.00	0.00	24.0
15	38	-6836	946	-212	0	192	4873	15.71	15.71	9.42	9.42	2	0.13	0.01	0.08	0.00	0.00	24.0
16	38	-6009	1064	776	0	-351	5499	15.71	15.71	9.42	9.42	2	0.15	0.01	0.09	0.00	0.00	24.0
17	38	-5768	1156	-230	0	204	5816	15.71	15.71	9.42	9.42	2	0.16	0.01	0.10	0.00	0.00	24.0
18	38	-14470	2337	756	0	-233	7710	15.71	15.71	9.42	9.42	3	0.14	0.03	0.18	0.00	0.00	24.0
19	38	2489	3025	506	0	-95	18343	15.71	15.71	9.42	9.42	3	0.36	0.04	0.28	0.00	0.00	24.0
20	38	-6180	2542	-223	0	298	12303	15.71	15.71	9.42	9.42	3	0.23	0.03	0.22	0.00	0.00	24.0
37	38	-20930	1658	754	0	-259	2114	15.71	15.71	9.42	9.42	3	0.04	0.02	0.12	0.00	0.00	24.0
38	38	7340	2805	336	0	-29	19840	15.71	15.71	9.42	9.42	3	0.40	0.04	0.26	0.00	0.00	24.0
39	38	-7109	2000	-878	0	625	9769	15.71	15.71	9.42	9.42	3	0.19	0.03	0.17	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-8219	1306	366	0	-149	6905	15.71	15.71	9.42	9.42	3	0.13	0.02	0.11	0.00	0.00	24.0
2	50	-8138	641	462	0	-241	3645	15.71	15.71	9.42	9.42	2	0.10	0.01	0.05	0.00	0.00	24.0
3	50	-8066	669	161	0	-37	3743	15.71	15.71	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
4	50	-4579	1341	403	0	-193	6879	15.71	15.71	9.42	9.42	2	0.19	0.02	0.12	0.00	0.00	24.0
5	50	-4507	1368	102	0	11	6978	15.71	15.71	9.42	9.42	2	0.18	0.02	0.12	0.00	0.00	24.0
6	50	-6976	854	793	0	-462	4661	15.71	15.71	9.42	9.42	2	0.13	0.01	0.07	0.00	0.00	24.0
7	50	-6736	946	-212	0	218	4991	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
8	50	-5909	1064	776	0	-448	5632	15.71	15.71	9.42	9.42	2	0.16	0.01	0.09	0.00	0.00	24.0
9	50	-5668	1156	-230	0	233	5961	15.71	15.71	9.42	9.42	2	0.16	0.01	0.10	0.00	0.00	24.0
10	50	-8138	641	462	0	-241	3645	15.71	15.71	9.42	9.42	2	0.10	0.01	0.05	0.00	0.00	24.0
11	50	-8066	669	161	0	-37	3743	15.71	15.71	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
12	50	-4579	1341	403	0	-193	6879	15.71	15.71	9.42	9.42	2	0.19	0.02	0.12	0.00	0.00	24.0
13	50	-4507	1368	102	0	11	6978	15.71	15.71	9.42	9.42	2	0.18	0.02	0.12	0.00	0.00	24.0
14	50	-6976	854	793	0	-462	4661	15.71	15.71	9.42	9.42	2	0.13	0.01	0.07	0.00	0.00	24.0
15	50	-6736	946	-212	0	218	4991	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
16	50	-5909	1064	776	0	-448	5632	15.71	15.71	9.42	9.42	2	0.16	0.01	0.09	0.00	0.00	24.0
17	50	-5668	1156	-230	0	233	5961	15.71	15.71	9.42	9.42	2	0.16	0.01	0.10	0.00	0.00	24.0

18	50	-14340	2337	756	0	-328	8002	15.71	15.71	9.42	9.42	3	0.15	0.03	0.18	0.00	0.00	24.0
19	50	2619	3025	506	0	-158	18720	15.71	15.71	9.42	9.42	3	0.37	0.04	0.28	0.00	0.00	24.0
20	50	-6050	2542	-223	0	326	12620	15.71	15.71	9.42	9.42	3	0.24	0.03	0.22	0.00	0.00	24.0
37	50	-20800	1658	754	0	-354	2321	15.71	15.71	9.42	9.42	3	0.04	0.02	0.12	0.00	0.00	24.0
38	50	7470	2805	336	0	-71	20190	15.71	15.71	9.42	9.42	3	0.41	0.04	0.26	0.00	0.00	24.0
39	50	-6979	2000	-878	0	735	10020	15.71	15.71	9.42	9.42	3	0.19	0.03	0.17	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 68 NI 1580 NF 1581 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 5
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	1474	544	-253	0	-188	9137	15.71	15.71	9.42	9.42	3	0.18	0.01	0.05	0.00	0.00	24.0
2	0	-1255	337	-72	0	-102	5465	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
3	0	-1266	348	-174	0	-97	5463	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
4	0	3533	488	-214	0	-193	8595	15.71	15.71	9.42	9.42	2	0.25	0.01	0.05	0.00	0.00	24.0
5	0	3522	500	-317	0	-188	8592	15.71	15.71	9.42	9.42	2	0.25	0.01	0.05	0.00	0.00	24.0
6	0	434	376	-1	0	-140	6564	15.71	15.71	9.42	9.42	2	0.18	0.00	0.04	0.00	0.00	24.0
7	0	397	415	-345	0	-122	6554	15.71	15.71	9.42	9.42	2	0.18	0.01	0.04	0.00	0.00	24.0
8	0	1870	422	-44	0	-167	7503	15.71	15.71	9.42	9.42	2	0.21	0.01	0.04	0.00	0.00	24.0
9	0	1834	460	-387	0	-150	7493	15.71	15.71	9.42	9.42	2	0.21	0.01	0.04	0.00	0.00	24.0
10	0	-1255	337	-72	0	-102	5465	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
11	0	-1266	348	-174	0	-97	5463	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
12	0	3533	488	-214	0	-193	8595	15.71	15.71	9.42	9.42	2	0.25	0.01	0.05	0.00	0.00	24.0
13	0	3522	500	-317	0	-188	8592	15.71	15.71	9.42	9.42	2	0.25	0.01	0.05	0.00	0.00	24.0
14	0	434	376	-1	0	-140	6564	15.71	15.71	9.42	9.42	2	0.18	0.00	0.04	0.00	0.00	24.0
15	0	397	415	-345	0	-122	6554	15.71	15.71	9.42	9.42	2	0.18	0.01	0.04	0.00	0.00	24.0
16	0	1870	422	-44	0	-167	7503	15.71	15.71	9.42	9.42	2	0.21	0.01	0.04	0.00	0.00	24.0
17	0	1834	460	-387	0	-150	7493	15.71	15.71	9.42	9.42	2	0.21	0.01	0.04	0.00	0.00	24.0
18	0	1051	1648	-295	0	-251	12090	15.71	15.71	9.42	9.42	3	0.24	0.02	0.15	0.00	0.00	24.0
19	0	21480	356	-705	0	-513	23890	15.71	15.71	9.42	9.42	3	0.53	0.01	0.05	0.00	0.00	24.0
20	0	9869	963	-786	0	-334	16680	15.71	15.71	9.42	9.42	3	0.34	0.01	0.09	0.00	0.00	24.0
37	0	-8970	1931	-79	0	-101	5277	15.71	15.71	9.42	9.42	3	0.10	0.02	0.16	0.00	0.00	24.0
38	0	25080	-224	-762	0	-537	24940	15.71	15.71	9.42	9.42	3	0.56	0.01	0.05	0.00	0.00	24.0
39	0	5726	789	-897	0	-239	12910	15.71	15.71	9.42	9.42	3	0.26	0.01	0.07	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	1604	544	-253	0	-157	9205	15.71	15.71	9.42	9.42	3	0.18	0.01	0.05	0.00	0.00	24.0
2	12	-1155	337	-72	0	-93	5507	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
3	12	-1166	348	-174	0	-75	5506	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
4	12	3633	488	-214	0	-166	8656	15.71	15.71	9.42	9.42	2	0.25	0.01	0.05	0.00	0.00	24.0
5	12	3622	500	-317	0	-148	8655	15.71	15.71	9.42	9.42	2	0.25	0.01	0.05	0.00	0.00	24.0
6	12	534	376	-1	0	-140	6611	15.71	15.71	9.42	9.42	2	0.18	0.00	0.04	0.00	0.00	24.0
7	12	497	415	-345	0	-79	6606	15.71	15.71	9.42	9.42	2	0.18	0.01	0.04	0.00	0.00	24.0
8	12	1970	422	-44	0	-162	7556	15.71	15.71	9.42	9.42	2	0.21	0.01	0.04	0.00	0.00	24.0
9	12	1934	460	-387	0	-101	7551	15.71	15.71	9.42	9.42	2	0.21	0.01	0.04	0.00	0.00	24.0
10	12	-1155	337	-72	0	-93	5507	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
11	12	-1166	348	-174	0	-75	5506	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
12	12	3633	488	-214	0	-166	8656	15.71	15.71	9.42	9.42	2	0.25	0.01	0.05	0.00	0.00	24.0
13	12	3622	500	-317	0	-148	8655	15.71	15.71	9.42	9.42	2	0.25	0.01	0.05	0.00	0.00	24.0
14	12	534	376	-1	0	-140	6611	15.71	15.71	9.42	9.42	2	0.18	0.00	0.04	0.00	0.00	24.0
15	12	497	415	-345	0	-79	6606	15.71	15.71	9.42	9.42	2	0.18	0.01	0.04	0.00	0.00	24.0
16	12	1970	422	-44	0	-162	7556	15.71	15.71	9.42	9.42	2	0.21	0.01	0.04	0.00	0.00	24.0
17	12	1934	460	-387	0	-101	7551	15.71	15.71	9.42	9.42	2	0.21	0.01	0.04	0.00	0.00	24.0
18	12	1181	1648	-295	0	-214	12297	15.71	15.71	9.42	9.42	3	0.24	0.02	0.15	0.00	0.00	24.0
19	12	21610	356	-705	0	-425	23935	15.71	15.71	9.42	9.42	3	0.53	0.01	0.05	0.00	0.00	24.0
20	12	9999	963	-786	0	-236	16800	15.71	15.71	9.42	9.42	3	0.34	0.01	0.09	0.00	0.00	24.0
37	12	-8840	1931	-79	0	-91	5518	15.71	15.71	9.42	9.42	3	0.10	0.02	0.16	0.00	0.00	24.0
38	12	25210	-224	-762	0	-442	24913	15.71	15.71	9.42	9.42	3	0.56	0.01	0.05	0.00	0.00	24.0
39	12	5856	789	-897	0	-127	13010	15.71	15.71	9.42	9.42	3	0.26	0.01	0.07	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	1734	544	-253	0	-125	9273	15.71	15.71	9.42	9.42	3	0.18	0.01	0.05	0.00	0.00	24.0
2	25	-1055	337	-72	0	-84	5549	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
3	25	-1066	348	-174	0	-53	5550	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
4	25	3733	488	-214	0	-140	8717	15.71	15.71	9.42	9.42	2	0.25	0.01	0.05	0.00	0.00	24.0
5	25	3722	500	-317	0	-109	8717	15.71	15.71	9.42	9.42	2	0.25	0.01	0.05	0.00	0.00	24.0
6	25	634	376	-1	0	-140	6658	15.71	15.71	9.42	9.42	2	0.19	0.00	0.04	0.00	0.00	24.0
7	25	597	415	-345	0	-36	6658	15.71	15.71	9.42	9.42	2	0.18	0.01	0.04	0.00	0.00	24.0
8	25	2070	422	-44	0	-156	7609	15.71	15.71	9.42	9.42	2	0.21	0.01	0.04	0.00	0.00	24.0
9	25	2034	460	-387	0	-53	7609	15.71	15.71	9.42	9.42	2	0.21	0.01	0.04	0.00	0.00	24.0
10	25	-1055	337	-72	0	-84	5549	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
11	25	-1066	348	-174	0	-53	5550	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
12	25	3733	488	-214	0	-140	8717	15.71	15.71	9.42	9.42	2	0.25	0.01	0.05	0.00	0.00	24.0
13	25	3722	500	-317	0	-109	8717	15.71	15.71	9.42	9.42	2	0.25	0.01	0.05	0.00	0.00	24.0
14	25	634	376	-1	0	-140	6658	15.71	15.71	9.42	9.42	2	0.19	0.00	0.04	0.00	0.00	24.0
15	25	597	415	-345	0	-36	6658	15.71	15.71	9.42	9.42	2	0.18	0.01	0.04	0.00	0.00	24.0
16	25	2070	422	-44	0	-156	7609	15.71	15.71	9.42	9.42	2	0.21	0.01	0.04	0.00	0.00	24.0
17	25	2034	460	-387	0	-53	7609	15.71	15.71	9.42	9.42	2	0.21	0.01	0.04	0.00	0.00	24.0
18	25	1311	1648	-295	0	-178	12505	15.71	15.71	9.42	9.42	3	0.24	0.02	0.15	0.00	0.00	24.0
19	25	21740	356	-705	0	-337	23980	15.71	15.71	9.42	9.42	3	0.53	0.01	0.05	0.00	0.00	24.0
20	25	10130	963	-786	0	-138	16920	15.71	15.71	9.42	9.42	3	0.35	0.01	0.09	0.00	0.00	24.0
37	25	-8710	1931	-79	0	-81	5759	15.71	15.71	9.42	9.42	3	0.11	0.02	0.16	0.00	0.00	24.0
38	25	25340	-224	-762	0	-347	24885	15.71	15.71	9.42	9.42	3	0.56	0.01	0.05	0.00	0.00	24.0
39	25	5986	789	-897	0	-15	13110	15.71	15.71	9.42	9.42	3	0.26	0.01	0.07	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	1864	544	-253	0	-94	9341	15.71	15.71	9.42	9.42	3	0.18	0.01	0.05	0.00	0.00	24.0
2	38	-955	337	-72	0	-75	5592	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
3	38	-966	348	-174	0	-31	5594	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
4	38	3833	488	-214	0	-113	8778	15.71	15.71	9.42	9.42	2	0.25	0.01	0.05	0.00	0.00	24.0
5	38	3822	500	-317	0	-69	8780	15.71	15.71	9.42	9.42	2	0.25	0.01	0.05	0.00	0.00	24.0
6	38	734	376	-1	0	-139	6705	15.71	15.71	9.42	9.42	2	0.19	0.00	0.04	0.00	0.00	24.0
7	38	697	415	-345	0	7	6710	15.71	15.71	9.42	9.42	2	0.18	0.01	0.04	0.00	0.00	24.0
8	38	2170	422	-44	0	-151	7661	15.71	15.71	9.42	9.42	2	0.22	0.01	0.04	0.00	0.00	24.0
9	38	2134	460	-387	0	-5	7666	15.71	15.71	9.42	9.42	2	0.21	0.01	0.04	0.00	0.00	24.0
10	38	-955	337	-72	0	-75	5592	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
11	38	-966	348	-174	0	-31	5594	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
12	38	3833	488	-214	0	-113	8778	15.71	15.71	9.42	9.42	2	0.25	0.01	0.05	0.00	0.00	24.0
13	38	3822	500	-317	0	-69	8780	15.71	15.71	9.42	9.42	2	0.25	0.01	0.05	0.00	0.00	24.0

14	38	734	376	-1	0	-139	6705	15.71	15.71	9.42	9.42	2	0.19	0.00	0.04	0.00	0.00	24.0
15	38	697	415	-345	0	7	6710	15.71	15.71	9.42	9.42	2	0.18	0.01	0.04	0.00	0.00	24.0
16	38	2170	422	-44	0	-151	7661	15.71	15.71	9.42	9.42	2	0.22	0.01	0.04	0.00	0.00	24.0
17	38	2134	460	-387	0	-5	7666	15.71	15.71	9.42	9.42	2	0.21	0.01	0.04	0.00	0.00	24.0
18	38	1441	1648	-295	0	-141	12712	15.71	15.71	9.42	9.42	3	0.25	0.02	0.15	0.00	0.00	24.0
19	38	21870	356	-705	0	-249	24025	15.71	15.71	9.42	9.42	3	0.53	0.01	0.05	0.00	0.00	24.0
20	38	10260	963	-786	0	-39	17040	15.71	15.71	9.42	9.42	3	0.35	0.01	0.09	0.00	0.00	24.0
37	38	-8580	1931	-79	0	-71	6001	15.71	15.71	9.42	9.42	3	0.11	0.02	0.16	0.00	0.00	24.0
38	38	25470	-224	-762	0	-252	24857	15.71	15.71	9.42	9.42	3	0.56	0.01	0.05	0.00	0.00	24.0
39	38	6116	789	-897	0	97	13210	15.71	15.71	9.42	9.42	3	0.26	0.01	0.07	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	1994	544	-253	0	-62	9409	15.71	15.71	9.42	9.42	3	0.18	0.01	0.05	0.00	0.00	24.0
2	50	-855	337	-72	0	-66	5634	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
3	50	-866	348	-174	0	-9	5637	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
4	50	3933	488	-214	0	-86	8839	15.71	15.71	9.42	9.42	2	0.25	0.01	0.05	0.00	0.00	24.0
5	50	3922	500	-317	0	-29	8842	15.71	15.71	9.42	9.42	2	0.25	0.01	0.05	0.00	0.00	24.0
6	50	834	376	-1	0	-139	6752	15.71	15.71	9.42	9.42	2	0.19	0.00	0.04	0.00	0.00	24.0
7	50	797	415	-345	0	50	6762	15.71	15.71	9.42	9.42	2	0.19	0.01	0.04	0.00	0.00	24.0
8	50	2270	422	-44	0	-145	7714	15.71	15.71	9.42	9.42	2	0.22	0.01	0.04	0.00	0.00	24.0
9	50	2234	460	-387	0	44	7724	15.71	15.71	9.42	9.42	2	0.22	0.01	0.04	0.00	0.00	24.0
10	50	-855	337	-72	0	-66	5634	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
11	50	-866	348	-174	0	-9	5637	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
12	50	3933	488	-214	0	-86	8839	15.71	15.71	9.42	9.42	2	0.25	0.01	0.05	0.00	0.00	24.0
13	50	3922	500	-317	0	-29	8842	15.71	15.71	9.42	9.42	2	0.25	0.01	0.05	0.00	0.00	24.0
14	50	834	376	-1	0	-139	6752	15.71	15.71	9.42	9.42	2	0.19	0.00	0.04	0.00	0.00	24.0
15	50	797	415	-345	0	50	6762	15.71	15.71	9.42	9.42	2	0.19	0.01	0.04	0.00	0.00	24.0
16	50	2270	422	-44	0	-145	7714	15.71	15.71	9.42	9.42	2	0.22	0.01	0.04	0.00	0.00	24.0
17	50	2234	460	-387	0	44	7724	15.71	15.71	9.42	9.42	2	0.22	0.01	0.04	0.00	0.00	24.0
18	50	1571	1648	-295	0	-104	12920	15.71	15.71	9.42	9.42	3	0.25	0.02	0.15	0.00	0.00	24.0
19	50	22000	356	-705	0	-161	24070	15.71	15.71	9.42	9.42	3	0.53	0.01	0.05	0.00	0.00	24.0
20	50	10390	963	-786	0	59	17160	15.71	15.71	9.42	9.42	3	0.35	0.01	0.09	0.00	0.00	24.0
37	50	-8450	1931	-79	0	-62	6242	15.71	15.71	9.42	9.42	3	0.12	0.02	0.16	0.00	0.00	24.0
38	50	25600	-224	-762	0	-156	24830	15.71	15.71	9.42	9.42	3	0.56	0.01	0.05	0.00	0.00	24.0
39	50	6246	789	-897	0	209	13310	15.71	15.71	9.42	9.42	3	0.27	0.01	0.07	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 69 NI 1600 NF 1601 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 4
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	2931	531	84	0	-3	10180	15.71	15.71	9.42	9.42	3	0.20	0.01	0.05	0.00	0.00	24.0
2	0	-471	362	126	0	3	6052	15.71	15.71	9.42	9.42	2	0.16	0.00	0.03	0.00	0.00	24.0
3	0	-545	351	25	0	8	5999	15.71	15.71	9.42	9.42	2	0.16	0.00	0.03	0.00	0.00	24.0
4	0	5055	466	104	0	-14	9663	15.71	15.71	9.42	9.42	2	0.27	0.01	0.04	0.00	0.00	24.0
5	0	4981	455	3	0	-8	9609	15.71	15.71	9.42	9.42	2	0.27	0.01	0.04	0.00	0.00	24.0
6	0	1549	411	237	0	-9	7378	15.71	15.71	9.42	9.42	2	0.20	0.01	0.04	0.00	0.00	24.0
7	0	1303	375	-101	0	9	7200	15.71	15.71	9.42	9.42	2	0.20	0.00	0.04	0.00	0.00	24.0
8	0	3207	442	230	0	-14	8461	15.71	15.71	9.42	9.42	2	0.24	0.01	0.04	0.00	0.00	24.0
9	0	2961	406	-108	0	4	8283	15.71	15.71	9.42	9.42	2	0.23	0.01	0.04	0.00	0.00	24.0
10	0	-471	362	126	0	3	6052	15.71	15.71	9.42	9.42	2	0.16	0.00	0.03	0.00	0.00	24.0
11	0	-545	351	25	0	8	5999	15.71	15.71	9.42	9.42	2	0.16	0.00	0.03	0.00	0.00	24.0
12	0	5055	466	104	0	-14	9663	15.71	15.71	9.42	9.42	2	0.27	0.01	0.04	0.00	0.00	24.0
13	0	4981	455	3	0	-8	9609	15.71	15.71	9.42	9.42	2	0.27	0.01	0.04	0.00	0.00	24.0
14	0	1549	411	237	0	-9	7378	15.71	15.71	9.42	9.42	2	0.20	0.01	0.04	0.00	0.00	24.0
15	0	1303	375	-101	0	9	7200	15.71	15.71	9.42	9.42	2	0.20	0.00	0.04	0.00	0.00	24.0
16	0	3207	442	230	0	-14	8461	15.71	15.71	9.42	9.42	2	0.24	0.01	0.04	0.00	0.00	24.0
17	0	2961	406	-108	0	4	8283	15.71	15.71	9.42	9.42	2	0.23	0.01	0.04	0.00	0.00	24.0
18	0	2976	1685	188	0	13	13530	15.71	15.71	9.42	9.42	3	0.27	0.02	0.16	0.00	0.00	24.0
19	0	25330	190	130	0	-30	26570	15.71	15.71	9.42	9.42	3	0.60	0.00	0.02	0.00	0.00	24.0
20	0	12310	848	-148	0	8	18440	15.71	15.71	9.42	9.42	3	0.38	0.01	0.08	0.00	0.00	24.0
37	0	-8149	2051	182	0	30	5972	15.71	15.71	9.42	9.42	3	0.11	0.03	0.17	0.00	0.00	24.0
38	0	29100	-440	86	0	-43	27700	15.71	15.71	9.42	9.42	3	0.65	0.01	0.04	0.00	0.00	24.0
39	0	7411	657	-377	0	20	14150	15.71	15.71	9.42	9.42	3	0.28	0.01	0.06	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	3061	531	84	0	-14	10248	15.71	15.71	9.42	9.42	3	0.20	0.01	0.05	0.00	0.00	24.0
2	12	-371	362	126	0	-13	6097	15.71	15.71	9.42	9.42	2	0.17	0.00	0.03	0.00	0.00	24.0
3	12	-445	351	25	0	5	6043	15.71	15.71	9.42	9.42	2	0.16	0.00	0.03	0.00	0.00	24.0
4	12	5155	466	104	0	-27	9721	15.71	15.71	9.42	9.42	2	0.28	0.01	0.04	0.00	0.00	24.0
5	12	5081	455	3	0	-9	9666	15.71	15.71	9.42	9.42	2	0.27	0.01	0.04	0.00	0.00	24.0
6	12	1649	411	237	0	-39	7430	15.71	15.71	9.42	9.42	2	0.21	0.01	0.04	0.00	0.00	24.0
7	12	1403	375	-101	0	21	7247	15.71	15.71	9.42	9.42	2	0.20	0.00	0.04	0.00	0.00	24.0
8	12	3307	442	230	0	-43	8516	15.71	15.71	9.42	9.42	2	0.24	0.01	0.04	0.00	0.00	24.0
9	12	3061	406	-108	0	17	8334	15.71	15.71	9.42	9.42	2	0.23	0.01	0.04	0.00	0.00	24.0
10	12	-371	362	126	0	-13	6097	15.71	15.71	9.42	9.42	2	0.17	0.00	0.03	0.00	0.00	24.0
11	12	-445	351	25	0	5	6043	15.71	15.71	9.42	9.42	2	0.16	0.00	0.03	0.00	0.00	24.0
12	12	5155	466	104	0	-27	9721	15.71	15.71	9.42	9.42	2	0.28	0.01	0.04	0.00	0.00	24.0
13	12	5081	455	3	0	-9	9666	15.71	15.71	9.42	9.42	2	0.27	0.01	0.04	0.00	0.00	24.0
14	12	1649	411	237	0	-39	7430	15.71	15.71	9.42	9.42	2	0.21	0.01	0.04	0.00	0.00	24.0
15	12	1403	375	-101	0	21	7247	15.71	15.71	9.42	9.42	2	0.20	0.00	0.04	0.00	0.00	24.0
16	12	3307	442	230	0	-43	8516	15.71	15.71	9.42	9.42	2	0.24	0.01	0.04	0.00	0.00	24.0
17	12	3061	406	-108	0	17	8334	15.71	15.71	9.42	9.42	2	0.23	0.01	0.04	0.00	0.00	24.0
18	12	3106	1685	188	0	-10	13740	15.71	15.71	9.42	9.42	3	0.27	0.02	0.16	0.00	0.00	24.0
19	12	25460	190	130	0	-47	26593	15.71	15.71	9.42	9.42	3	0.60	0.00	0.02	0.00	0.00	24.0
20	12	12440	848	-148	0	26	18545	15.71	15.71	9.42	9.42	3	0.38	0.01	0.08	0.00	0.00	24.0
37	12	-8019	2051	182	0	7	6228	15.71	15.71	9.42	9.42	3	0.12	0.03	0.17	0.00	0.00	24.0
38	12	29230	-440	86	0	-54	27645	15.71	15.71	9.42	9.42	3	0.65	0.01	0.04	0.00	0.00	24.0
39	12	7541	657	-377	0	67	14232	15.71	15.71	9.42	9.42	3	0.29	0.01	0.06	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	3191	531	84	0	-24	10315	15.71	15.71	9.42	9.42	3	0.20	0.01	0.05	0.00	0.00	24.0
2	25	-271	362	126	0	-29	6142	15.71	15.71	9.42	9.42	2	0.17	0.00	0.03	0.00	0.00	24.0
3	25	-345	351	25	0	2	6086	15.71	15.71	9.42	9.42	2	0.17	0.00	0.03	0.00	0.00	24.0
4	25	5255	466	104	0	-40	9780	15.71	15.71	9.42	9.42	2	0.28	0.01	0.04	0.00	0.00	24.0
5	25	5181	455	3	0	-9	9723	15.71	15.71	9.42	9.42	2	0.28	0.01	0.04	0.00	0.00	24.0
6	25	1749	411	237	0	-68	7481	15.71	15.71	9.42	9.42	2	0.21	0.01	0.04	0.00	0.00	24.0
7	25	1503	375	-101	0	34	7294	15.71	15.71	9.42	9.42	2	0.20	0.00	0.04	0.00	0.00	24.0
8	25	3407	442	230	0	-72	8571	15.71	15.71	9.42	9.42	2	0.24	0.01	0.04	0.00	0.00	24.0
9	25	3161	406	-108	0	31	8385	15.71	15.71	9.42	9.42	2	0.23	0.01	0.04	0.00	0.00	24.0

10	25	-271	362	126	0	-29	6142	15.71	15.71	9.42	9.42	2	0.17	0.00	0.03	0.00	0.00	24.0
11	25	-345	351	25	0	2	6086	15.71	15.71	9.42	9.42	2	0.17	0.00	0.03	0.00	0.00	24.0
12	25	5255	466	104	0	-40	9780	15.71	15.71	9.42	9.42	2	0.28	0.01	0.04	0.00	0.00	24.0
13	25	5181	455	3	0	-9	9723	15.71	15.71	9.42	9.42	2	0.28	0.01	0.04	0.00	0.00	24.0
14	25	1749	411	237	0	-68	7481	15.71	15.71	9.42	9.42	2	0.21	0.01	0.04	0.00	0.00	24.0
15	25	1503	375	-101	0	34	7294	15.71	15.71	9.42	9.42	2	0.20	0.00	0.04	0.00	0.00	24.0
16	25	3407	442	230	0	-72	8571	15.71	15.71	9.42	9.42	2	0.24	0.01	0.04	0.00	0.00	24.0
17	25	3161	406	-108	0	31	8385	15.71	15.71	9.42	9.42	2	0.23	0.01	0.04	0.00	0.00	24.0
18	25	3236	1685	188	0	-34	13950	15.71	15.71	9.42	9.42	3	0.27	0.02	0.16	0.00	0.00	24.0
19	25	25590	190	130	0	-63	26615	15.71	15.71	9.42	9.42	3	0.60	0.00	0.02	0.00	0.00	24.0
20	25	12570	848	-148	0	44	18650	15.71	15.71	9.42	9.42	3	0.39	0.01	0.08	0.00	0.00	24.0
37	25	-7889	2051	182	0	-16	6484	15.71	15.71	9.42	9.42	3	0.12	0.03	0.17	0.00	0.00	24.0
38	25	29360	-440	86	0	-65	27590	15.71	15.71	9.42	9.42	3	0.64	0.01	0.04	0.00	0.00	24.0
39	25	7671	657	-377	0	114	14315	15.71	15.71	9.42	9.42	3	0.29	0.01	0.06	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	3321	531	84	0	-35	10383	15.71	15.71	9.42	9.42	3	0.20	0.01	0.05	0.00	0.00	24.0
2	38	-171	362	126	0	-44	6188	15.71	15.71	9.42	9.42	2	0.17	0.00	0.03	0.00	0.00	24.0
3	38	-245	351	25	0	-1	6130	15.71	15.71	9.42	9.42	2	0.17	0.00	0.03	0.00	0.00	24.0
4	38	5355	466	104	0	-53	9838	15.71	15.71	9.42	9.42	2	0.28	0.01	0.04	0.00	0.00	24.0
5	38	5281	455	3	0	-9	9780	15.71	15.71	9.42	9.42	2	0.28	0.01	0.04	0.00	0.00	24.0
6	38	1849	411	237	0	-98	7532	15.71	15.71	9.42	9.42	2	0.21	0.01	0.04	0.00	0.00	24.0
7	38	1603	375	-101	0	47	7340	15.71	15.71	9.42	9.42	2	0.20	0.00	0.04	0.00	0.00	24.0
8	38	3507	442	230	0	-100	8627	15.71	15.71	9.42	9.42	2	0.24	0.01	0.04	0.00	0.00	24.0
9	38	3261	406	-108	0	44	8435	15.71	15.71	9.42	9.42	2	0.24	0.01	0.04	0.00	0.00	24.0
10	38	-171	362	126	0	-44	6188	15.71	15.71	9.42	9.42	2	0.17	0.00	0.03	0.00	0.00	24.0
11	38	-245	351	25	0	-1	6130	15.71	15.71	9.42	9.42	2	0.17	0.00	0.03	0.00	0.00	24.0
12	38	5355	466	104	0	-53	9838	15.71	15.71	9.42	9.42	2	0.28	0.01	0.04	0.00	0.00	24.0
13	38	5281	455	3	0	-9	9780	15.71	15.71	9.42	9.42	2	0.28	0.01	0.04	0.00	0.00	24.0
14	38	1849	411	237	0	-98	7532	15.71	15.71	9.42	9.42	2	0.21	0.01	0.04	0.00	0.00	24.0
15	38	1603	375	-101	0	47	7340	15.71	15.71	9.42	9.42	2	0.20	0.00	0.04	0.00	0.00	24.0
16	38	3507	442	230	0	-100	8627	15.71	15.71	9.42	9.42	2	0.24	0.01	0.04	0.00	0.00	24.0
17	38	3261	406	-108	0	44	8435	15.71	15.71	9.42	9.42	2	0.24	0.01	0.04	0.00	0.00	24.0
18	38	3366	1685	188	0	-57	14160	15.71	15.71	9.42	9.42	3	0.28	0.02	0.16	0.00	0.00	24.0
19	38	25720	190	130	0	-79	26638	15.71	15.71	9.42	9.42	3	0.61	0.00	0.02	0.00	0.00	24.0
20	38	12700	848	-148	0	63	18755	15.71	15.71	9.42	9.42	3	0.39	0.01	0.08	0.00	0.00	24.0
37	38	-7759	2051	182	0	-39	6741	15.71	15.71	9.42	9.42	3	0.13	0.03	0.17	0.00	0.00	24.0
38	38	29490	-440	86	0	-75	27535	15.71	15.71	9.42	9.42	3	0.64	0.01	0.04	0.00	0.00	24.0
39	38	7801	657	-377	0	161	14397	15.71	15.71	9.42	9.42	3	0.29	0.01	0.06	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	3451	531	84	0	-45	10450	15.71	15.71	9.42	9.42	3	0.21	0.01	0.05	0.00	0.00	24.0
2	50	-71	362	126	0	-60	6233	15.71	15.71	9.42	9.42	2	0.17	0.00	0.03	0.00	0.00	24.0
3	50	-145	351	25	0	-4	6174	15.71	15.71	9.42	9.42	2	0.17	0.00	0.03	0.00	0.00	24.0
4	50	5455	466	104	0	-66	9896	15.71	15.71	9.42	9.42	2	0.28	0.01	0.04	0.00	0.00	24.0
5	50	5381	455	3	0	-10	9837	15.71	15.71	9.42	9.42	2	0.28	0.01	0.04	0.00	0.00	24.0
6	50	1949	411	237	0	-127	7584	15.71	15.71	9.42	9.42	2	0.21	0.01	0.04	0.00	0.00	24.0
7	50	1703	375	-101	0	59	7387	15.71	15.71	9.42	9.42	2	0.21	0.00	0.04	0.00	0.00	24.0
8	50	3607	442	230	0	-129	8682	15.71	15.71	9.42	9.42	2	0.25	0.01	0.04	0.00	0.00	24.0
9	50	3361	406	-108	0	58	8486	15.71	15.71	9.42	9.42	2	0.24	0.01	0.04	0.00	0.00	24.0
10	50	-71	362	126	0	-60	6233	15.71	15.71	9.42	9.42	2	0.17	0.00	0.03	0.00	0.00	24.0
11	50	-145	351	25	0	-4	6174	15.71	15.71	9.42	9.42	2	0.17	0.00	0.03	0.00	0.00	24.0
12	50	5455	466	104	0	-66	9896	15.71	15.71	9.42	9.42	2	0.28	0.01	0.04	0.00	0.00	24.0
13	50	5381	455	3	0	-10	9837	15.71	15.71	9.42	9.42	2	0.28	0.01	0.04	0.00	0.00	24.0
14	50	1949	411	237	0	-127	7584	15.71	15.71	9.42	9.42	2	0.21	0.01	0.04	0.00	0.00	24.0
15	50	1703	375	-101	0	59	7387	15.71	15.71	9.42	9.42	2	0.21	0.00	0.04	0.00	0.00	24.0
16	50	3607	442	230	0	-129	8682	15.71	15.71	9.42	9.42	2	0.25	0.01	0.04	0.00	0.00	24.0
17	50	3361	406	-108	0	58	8486	15.71	15.71	9.42	9.42	2	0.24	0.01	0.04	0.00	0.00	24.0
18	50	3496	1685	188	0	-81	14370	15.71	15.71	9.42	9.42	3	0.28	0.02	0.16	0.00	0.00	24.0
19	50	25850	190	130	0	-95	26660	15.71	15.71	9.42	9.42	3	0.61	0.00	0.02	0.00	0.00	24.0
20	50	12830	848	-148	0	81	18860	15.71	15.71	9.42	9.42	3	0.39	0.01	0.08	0.00	0.00	24.0
37	50	-7629	2051	182	0	-61	6997	15.71	15.71	9.42	9.42	3	0.13	0.03	0.17	0.00	0.00	24.0
38	50	29620	-440	86	0	-86	27480	15.71	15.71	9.42	9.42	3	0.64	0.01	0.04	0.00	0.00	24.0
39	50	7931	657	-377	0	208	14480	15.71	15.71	9.42	9.42	3	0.29	0.01	0.06	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 70 NI 1620 NF 1621 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 3
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	1495	524	392	0	168	9102	15.71	15.71	9.42	9.42	3	0.18	0.01	0.05	0.00	0.00	24.0
2	0	-1528	336	317	0	108	5250	15.71	15.71	9.42	9.42	2	0.14	0.00	0.03	0.00	0.00	24.0
3	0	-1521	336	211	0	108	5257	15.71	15.71	9.42	9.42	2	0.14	0.00	0.03	0.00	0.00	24.0
4	0	3820	469	393	0	151	8746	15.71	15.71	9.42	9.42	2	0.25	0.01	0.04	0.00	0.00	24.0
5	0	3828	470	286	0	151	8754	15.71	15.71	9.42	9.42	2	0.25	0.01	0.04	0.00	0.00	24.0
6	0	334	382	468	0	123	6464	15.71	15.71	9.42	9.42	2	0.18	0.01	0.04	0.00	0.00	24.0
7	0	361	384	113	0	123	6490	15.71	15.71	9.42	9.42	2	0.18	0.01	0.04	0.00	0.00	24.0
8	0	1939	422	491	0	136	7513	15.71	15.71	9.42	9.42	2	0.21	0.01	0.04	0.00	0.00	24.0
9	0	1965	424	136	0	136	7539	15.71	15.71	9.42	9.42	2	0.21	0.01	0.04	0.00	0.00	24.0
10	0	-1528	336	317	0	108	5250	15.71	15.71	9.42	9.42	2	0.14	0.00	0.03	0.00	0.00	24.0
11	0	-1521	336	211	0	108	5257	15.71	15.71	9.42	9.42	2	0.14	0.00	0.03	0.00	0.00	24.0
12	0	3820	469	393	0	151	8746	15.71	15.71	9.42	9.42	2	0.25	0.01	0.04	0.00	0.00	24.0
13	0	3828	470	286	0	151	8754	15.71	15.71	9.42	9.42	2	0.25	0.01	0.04	0.00	0.00	24.0
14	0	334	382	468	0	123	6464	15.71	15.71	9.42	9.42	2	0.18	0.01	0.04	0.00	0.00	24.0
15	0	361	384	113	0	123	6490	15.71	15.71	9.42	9.42	2	0.18	0.01	0.04	0.00	0.00	24.0
16	0	1939	422	491	0	136	7513	15.71	15.71	9.42	9.42	2	0.21	0.01	0.04	0.00	0.00	24.0
17	0	1965	424	136	0	136	7539	15.71	15.71	9.42	9.42	2	0.21	0.01	0.04	0.00	0.00	24.0
18	0	449	1633	655	0	269	11630	15.71	15.71	9.42	9.42	3	0.23	0.02	0.15	0.00	0.00	24.0
19	0	22360	288	887	0	402	24390	15.71	15.71	9.42	9.42	3	0.54	0.01	0.06	0.00	0.00	24.0
20	0	9953	895	420	0	311	16690	15.71	15.71	9.42	9.42	3	0.34	0.01	0.08	0.00	0.00	24.0
37	0	-10110	1939	454	0	170	4474	15.71	15.71	9.42	9.42	3	0.08	0.02	0.16	0.00	0.00	24.0
38	0	26410	-302	841	0	392	25750	15.71	15.71	9.42	9.42	3	0.59	0.01	0.06	0.00	0.00	24.0
39	0	5733	710	63	0	241	12910	15.71	15.71	9.42	9.42	3	0.26	0.01	0.07	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	1625	524	392	0	119	9168	15.71	15.71	9.42	9.42	3	0.18	0.01	0.05	0.00	0.00	24.0
2	12	-1428	336	317	0	68	5292	15.71	15.71	9.42	9.42	2	0.14	0.00	0.03	0.00	0.00	24.0
3	12	-1421	336	211	0	82	5299	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
4	12	3920	469	393	0	101	8805	15.71	15.71	9.42	9.42	2	0.25	0.01	0.04	0.00	0.00	24.0
5	12	3928	470	286	0	115	8812	15.71	15.71	9.42	9.42	2	0.25	0.01	0.04	0.00	0.00	24.0

6	12	434	382	468	0	64	6512	15.71	15.71	9.42	9.42	2	0.18	0.01	0.04	0.00	0.00	24.0
7	12	461	384	113	0	109	6538	15.71	15.71	9.42	9.42	2	0.18	0.01	0.04	0.00	0.00	24.0
8	12	2039	422	491	0	74	7566	15.71	15.71	9.42	9.42	2	0.21	0.01	0.04	0.00	0.00	24.0
9	12	2065	424	136	0	119	7592	15.71	15.71	9.42	9.42	2	0.21	0.01	0.04	0.00	0.00	24.0
10	12	-1428	336	317	0	68	5292	15.71	15.71	9.42	9.42	2	0.14	0.00	0.03	0.00	0.00	24.0
11	12	-1421	336	211	0	82	5299	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
12	12	3920	469	393	0	101	8805	15.71	15.71	9.42	9.42	2	0.25	0.01	0.04	0.00	0.00	24.0
13	12	3928	470	286	0	115	8812	15.71	15.71	9.42	9.42	2	0.25	0.01	0.04	0.00	0.00	24.0
14	12	434	382	468	0	64	6512	15.71	15.71	9.42	9.42	2	0.18	0.01	0.04	0.00	0.00	24.0
15	12	461	384	113	0	109	6538	15.71	15.71	9.42	9.42	2	0.18	0.01	0.04	0.00	0.00	24.0
16	12	2039	422	491	0	74	7566	15.71	15.71	9.42	9.42	2	0.21	0.01	0.04	0.00	0.00	24.0
17	12	2065	424	136	0	119	7592	15.71	15.71	9.42	9.42	2	0.21	0.01	0.04	0.00	0.00	24.0
18	12	579	1633	655	0	187	11835	15.71	15.71	9.42	9.42	3	0.23	0.02	0.15	0.00	0.00	24.0
19	12	22490	288	887	0	291	24428	15.71	15.71	9.42	9.42	3	0.54	0.01	0.06	0.00	0.00	24.0
20	12	10082	895	420	0	259	16802	15.71	15.71	9.42	9.42	3	0.34	0.01	0.08	0.00	0.00	24.0
37	12	-9979	1939	454	0	113	4716	15.71	15.71	9.42	9.42	3	0.09	0.02	0.16	0.00	0.00	24.0
38	12	26540	-302	841	0	287	25710	15.71	15.71	9.42	9.42	3	0.59	0.01	0.06	0.00	0.00	24.0
39	12	5863	710	63	0	233	12998	15.71	15.71	9.42	9.42	3	0.26	0.01	0.07	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	1755	524	392	0	70	9233	15.71	15.71	9.42	9.42	3	0.18	0.01	0.05	0.00	0.00	24.0
2	25	-1328	336	317	0	29	5333	15.71	15.71	9.42	9.42	2	0.14	0.00	0.03	0.00	0.00	24.0
3	25	-1321	336	211	0	55	5342	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
4	25	4020	469	393	0	52	8863	15.71	15.71	9.42	9.42	2	0.25	0.01	0.04	0.00	0.00	24.0
5	25	4028	470	286	0	79	8871	15.71	15.71	9.42	9.42	2	0.25	0.01	0.04	0.00	0.00	24.0
6	25	534	382	468	0	6	6560	15.71	15.71	9.42	9.42	2	0.18	0.01	0.04	0.00	0.00	24.0
7	25	561	384	113	0	95	6586	15.71	15.71	9.42	9.42	2	0.18	0.01	0.04	0.00	0.00	24.0
8	25	2139	422	491	0	13	7618	15.71	15.71	9.42	9.42	2	0.21	0.01	0.04	0.00	0.00	24.0
9	25	2165	424	136	0	102	7645	15.71	15.71	9.42	9.42	2	0.21	0.01	0.04	0.00	0.00	24.0
10	25	-1328	336	317	0	29	5333	15.71	15.71	9.42	9.42	2	0.14	0.00	0.03	0.00	0.00	24.0
11	25	-1321	336	211	0	55	5342	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
12	25	4020	469	393	0	52	8863	15.71	15.71	9.42	9.42	2	0.25	0.01	0.04	0.00	0.00	24.0
13	25	4028	470	286	0	79	8871	15.71	15.71	9.42	9.42	2	0.25	0.01	0.04	0.00	0.00	24.0
14	25	534	382	468	0	6	6560	15.71	15.71	9.42	9.42	2	0.18	0.01	0.04	0.00	0.00	24.0
15	25	561	384	113	0	95	6586	15.71	15.71	9.42	9.42	2	0.18	0.01	0.04	0.00	0.00	24.0
16	25	2139	422	491	0	13	7618	15.71	15.71	9.42	9.42	2	0.21	0.01	0.04	0.00	0.00	24.0
17	25	2165	424	136	0	102	7645	15.71	15.71	9.42	9.42	2	0.21	0.01	0.04	0.00	0.00	24.0
18	25	709	1633	655	0	105	12040	15.71	15.71	9.42	9.42	3	0.23	0.02	0.15	0.00	0.00	24.0
19	25	22620	288	887	0	180	24465	15.71	15.71	9.42	9.42	3	0.54	0.01	0.06	0.00	0.00	24.0
20	25	10212	895	420	0	206	16915	15.71	15.71	9.42	9.42	3	0.35	0.01	0.08	0.00	0.00	24.0
37	25	-9848	1939	454	0	56	4958	15.71	15.71	9.42	9.42	3	0.09	0.02	0.16	0.00	0.00	24.0
38	25	26670	-302	841	0	182	25670	15.71	15.71	9.42	9.42	3	0.59	0.01	0.06	0.00	0.00	24.0
39	25	5993	710	63	0	225	13085	15.71	15.71	9.42	9.42	3	0.26	0.01	0.07	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	1885	524	392	0	21	9298	15.71	15.71	9.42	9.42	3	0.18	0.01	0.05	0.00	0.00	24.0
2	38	-1228	336	317	0	-11	5375	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
3	38	-1221	336	211	0	29	5384	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
4	38	4120	469	393	0	3	8922	15.71	15.71	9.42	9.42	2	0.25	0.01	0.04	0.00	0.00	24.0
5	38	4128	470	286	0	43	8930	15.71	15.71	9.42	9.42	2	0.25	0.01	0.04	0.00	0.00	24.0
6	38	634	382	468	0	-53	6607	15.71	15.71	9.42	9.42	2	0.18	0.01	0.04	0.00	0.00	24.0
7	38	661	384	113	0	81	6634	15.71	15.71	9.42	9.42	2	0.18	0.01	0.04	0.00	0.00	24.0
8	38	2239	422	491	0	-48	7671	15.71	15.71	9.42	9.42	2	0.21	0.01	0.04	0.00	0.00	24.0
9	38	2265	424	136	0	85	7698	15.71	15.71	9.42	9.42	2	0.22	0.01	0.04	0.00	0.00	24.0
10	38	-1228	336	317	0	-11	5375	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
11	38	-1221	336	211	0	29	5384	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
12	38	4120	469	393	0	3	8922	15.71	15.71	9.42	9.42	2	0.25	0.01	0.04	0.00	0.00	24.0
13	38	4128	470	286	0	43	8930	15.71	15.71	9.42	9.42	2	0.25	0.01	0.04	0.00	0.00	24.0
14	38	634	382	468	0	-53	6607	15.71	15.71	9.42	9.42	2	0.18	0.01	0.04	0.00	0.00	24.0
15	38	661	384	113	0	81	6634	15.71	15.71	9.42	9.42	2	0.18	0.01	0.04	0.00	0.00	24.0
16	38	2239	422	491	0	-48	7671	15.71	15.71	9.42	9.42	2	0.21	0.01	0.04	0.00	0.00	24.0
17	38	2265	424	136	0	85	7698	15.71	15.71	9.42	9.42	2	0.22	0.01	0.04	0.00	0.00	24.0
18	38	839	1633	655	0	23	12245	15.71	15.71	9.42	9.42	3	0.24	0.02	0.15	0.00	0.00	24.0
19	38	22750	288	887	0	70	24502	15.71	15.71	9.42	9.42	3	0.54	0.01	0.06	0.00	0.00	24.0
20	38	10341	895	420	0	154	17027	15.71	15.71	9.42	9.42	3	0.35	0.01	0.08	0.00	0.00	24.0
37	38	-9717	1939	454	0	-0	5201	15.71	15.71	9.42	9.42	3	0.10	0.02	0.16	0.00	0.00	24.0
38	38	26800	-302	841	0	77	25630	15.71	15.71	9.42	9.42	3	0.59	0.01	0.06	0.00	0.00	24.0
39	38	6123	710	63	0	218	13173	15.71	15.71	9.42	9.42	3	0.26	0.01	0.07	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	2015	524	392	0	-28	9364	15.71	15.71	9.42	9.42	3	0.18	0.01	0.05	0.00	0.00	24.0
2	50	-1128	336	317	0	-51	5417	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
3	50	-1121	336	211	0	3	5426	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
4	50	4220	469	393	0	-46	8980	15.71	15.71	9.42	9.42	2	0.25	0.01	0.04	0.00	0.00	24.0
5	50	4228	470	286	0	8	8988	15.71	15.71	9.42	9.42	2	0.25	0.01	0.04	0.00	0.00	24.0
6	50	734	382	468	0	-111	6655	15.71	15.71	9.42	9.42	2	0.19	0.01	0.04	0.00	0.00	24.0
7	50	761	384	113	0	67	6682	15.71	15.71	9.42	9.42	2	0.18	0.01	0.04	0.00	0.00	24.0
8	50	2339	422	491	0	-110	7724	15.71	15.71	9.42	9.42	2	0.22	0.01	0.04	0.00	0.00	24.0
9	50	2365	424	136	0	68	7751	15.71	15.71	9.42	9.42	2	0.22	0.01	0.04	0.00	0.00	24.0
10	50	-1128	336	317	0	-51	5417	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
11	50	-1121	336	211	0	3	5426	15.71	15.71	9.42	9.42	2	0.15	0.00	0.03	0.00	0.00	24.0
12	50	4220	469	393	0	-46	8980	15.71	15.71	9.42	9.42	2	0.25	0.01	0.04	0.00	0.00	24.0
13	50	4228	470	286	0	8	8988	15.71	15.71	9.42	9.42	2	0.25	0.01	0.04	0.00	0.00	24.0
14	50	734	382	468	0	-111	6655	15.71	15.71	9.42	9.42	2	0.19	0.01	0.04	0.00	0.00	24.0
15	50	761	384	113	0	67	6682	15.71	15.71	9.42	9.42	2	0.18	0.01	0.04	0.00	0.00	24.0
16	50	2339	422	491	0	-110	7724	15.71	15.71	9.42	9.42	2	0.22	0.01	0.04	0.00	0.00	24.0
17	50	2365	424	136	0	68	7751	15.71	15.71	9.42	9.42	2	0.22	0.01	0.04	0.00	0.00	24.0
18	50	969	1633	655	0	-59	12450	15.71	15.71	9.42	9.42	3	0.24	0.02	0.15	0.00	0.00	24.0
19	50	22880	288	887	0	-41	24540	15.71	15.71	9.42	9.42	3	0.55	0.01	0.06	0.00	0.00	24.0
20	50	10470	895	420	0	101	17140	15.71	15.71	9.42	9.42	3	0.35	0.01	0.08	0.00	0.00	24.0
37	50	-9586	1939	454	0	-57	5443	15.71	15.71	9.42	9.42	3	0.10	0.02	0.16	0.00	0.00	24.0
38	50	26930	-302	841	0	-28	25590	15.71	15.71	9.42	9.42	3	0.59	0.01	0.06	0.00	0.00	24.0
39	50	6253	710	63	0	210	13260	15.71	15.71	9.42	9.42	3	0.27	0.01	0.07	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 71 NI 1640 NF 1641 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 2
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-3955	88	539	0	304	5279	15.71	15.71	9.42	9.42	3	0.10	0.01	0.04	0.00	0.00	24.0

2	0	-5168	-37	375	0	178	2671	15.71	15.71	9.42	9.42	2	0.07	0.01	0.03	0.00	0.00	24.0
3	0	-5072	-20	280	0	184	2743	15.71	15.71	9.42	9.42	2	0.08	0.00	0.02	0.00	0.00	24.0
4	0	-1012	155	549	0	283	5378	15.71	15.71	9.42	9.42	2	0.15	0.01	0.04	0.00	0.00	24.0
5	0	-916	173	454	0	289	5451	15.71	15.71	9.42	9.42	2	0.16	0.01	0.03	0.00	0.00	24.0
6	0	-3826	10	547	0	208	3534	15.71	15.71	9.42	9.42	2	0.10	0.01	0.04	0.00	0.00	24.0
7	0	-3506	68	230	0	228	3775	15.71	15.71	9.42	9.42	2	0.11	0.00	0.02	0.00	0.00	24.0
8	0	-2579	68	599	0	239	4346	15.71	15.71	9.42	9.42	2	0.12	0.01	0.04	0.00	0.00	24.0
9	0	-2259	126	282	0	259	4587	15.71	15.71	9.42	9.42	2	0.13	0.00	0.02	0.00	0.00	24.0
10	0	-5168	-37	375	0	178	2671	15.71	15.71	9.42	9.42	2	0.07	0.01	0.03	0.00	0.00	24.0
11	0	-5072	-20	280	0	184	2743	15.71	15.71	9.42	9.42	2	0.08	0.00	0.02	0.00	0.00	24.0
12	0	-1012	155	549	0	283	5378	15.71	15.71	9.42	9.42	2	0.15	0.01	0.04	0.00	0.00	24.0
13	0	-916	173	454	0	289	5451	15.71	15.71	9.42	9.42	2	0.16	0.01	0.03	0.00	0.00	24.0
14	0	-3826	10	547	0	208	3534	15.71	15.71	9.42	9.42	2	0.10	0.01	0.04	0.00	0.00	24.0
15	0	-3506	68	230	0	228	3775	15.71	15.71	9.42	9.42	2	0.11	0.00	0.02	0.00	0.00	24.0
16	0	-2579	68	599	0	239	4346	15.71	15.71	9.42	9.42	2	0.12	0.01	0.04	0.00	0.00	24.0
17	0	-2259	126	282	0	259	4587	15.71	15.71	9.42	9.42	2	0.13	0.00	0.02	0.00	0.00	24.0
18	0	-8597	686	813	0	457	5116	15.71	15.71	9.42	9.42	3	0.10	0.01	0.06	0.00	0.00	24.0
19	0	10320	-25	1516	0	853	15910	15.71	15.71	9.42	9.42	3	0.33	0.02	0.11	0.00	0.00	24.0
20	0	356	336	812	0	620	9889	15.71	15.71	9.42	9.42	3	0.20	0.01	0.06	0.00	0.00	24.0
37	0	-16500	842	374	0	210	-191	15.71	15.71	9.42	9.42	3	0.01	0.01	0.06	0.00	0.00	24.0
38	0	15030	-342	1546	0	870	17800	15.71	15.71	9.42	9.42	3	0.38	0.02	0.11	0.00	0.00	24.0
39	0	-1574	260	372	0	482	7764	15.71	15.71	9.42	9.42	3	0.15	0.01	0.03	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-3825	88	539	0	236	5290	15.71	15.71	9.42	9.42	3	0.10	0.01	0.04	0.00	0.00	24.0
2	12	-5068	-37	375	0	131	2666	15.71	15.71	9.42	9.42	2	0.07	0.01	0.03	0.00	0.00	24.0
3	12	-4972	-20	280	0	149	2740	15.71	15.71	9.42	9.42	2	0.08	0.00	0.02	0.00	0.00	24.0
4	12	-912	155	549	0	215	5398	15.71	15.71	9.42	9.42	2	0.15	0.01	0.04	0.00	0.00	24.0
5	12	-816	173	454	0	232	5473	15.71	15.71	9.42	9.42	2	0.15	0.01	0.03	0.00	0.00	24.0
6	12	-3726	10	547	0	139	3535	15.71	15.71	9.42	9.42	2	0.10	0.01	0.04	0.00	0.00	24.0
7	12	-3406	68	230	0	199	3783	15.71	15.71	9.42	9.42	2	0.11	0.00	0.02	0.00	0.00	24.0
8	12	-2479	68	599	0	164	4354	15.71	15.71	9.42	9.42	2	0.12	0.01	0.04	0.00	0.00	24.0
9	12	-2159	126	282	0	224	4603	15.71	15.71	9.42	9.42	2	0.13	0.00	0.02	0.00	0.00	24.0
10	12	-5068	-37	375	0	131	2666	15.71	15.71	9.42	9.42	2	0.07	0.01	0.03	0.00	0.00	24.0
11	12	-4972	-20	280	0	149	2740	15.71	15.71	9.42	9.42	2	0.08	0.00	0.02	0.00	0.00	24.0
12	12	-912	155	549	0	215	5398	15.71	15.71	9.42	9.42	2	0.15	0.01	0.04	0.00	0.00	24.0
13	12	-816	173	454	0	232	5473	15.71	15.71	9.42	9.42	2	0.15	0.01	0.03	0.00	0.00	24.0
14	12	-3726	10	547	0	139	3535	15.71	15.71	9.42	9.42	2	0.10	0.01	0.04	0.00	0.00	24.0
15	12	-3406	68	230	0	199	3783	15.71	15.71	9.42	9.42	2	0.11	0.00	0.02	0.00	0.00	24.0
16	12	-2479	68	599	0	164	4354	15.71	15.71	9.42	9.42	2	0.12	0.01	0.04	0.00	0.00	24.0
17	12	-2159	126	282	0	224	4603	15.71	15.71	9.42	9.42	2	0.13	0.00	0.02	0.00	0.00	24.0
18	12	-8467	686	813	0	356	5202	15.71	15.71	9.42	9.42	3	0.10	0.01	0.06	0.00	0.00	24.0
19	12	10450	-25	1516	0	663	15908	15.71	15.71	9.42	9.42	3	0.33	0.02	0.11	0.00	0.00	24.0
20	12	486	336	812	0	519	9932	15.71	15.71	9.42	9.42	3	0.20	0.01	0.06	0.00	0.00	24.0
37	12	-16370	842	374	0	164	-86	15.71	15.71	9.42	9.42	3	0.01	0.01	0.06	0.00	0.00	24.0
38	12	15160	-342	1546	0	677	17758	15.71	15.71	9.42	9.42	3	0.38	0.02	0.11	0.00	0.00	24.0
39	12	-1444	260	372	0	436	7796	15.71	15.71	9.42	9.42	3	0.15	0.01	0.03	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-3695	88	539	0	169	5301	15.71	15.71	9.42	9.42	3	0.10	0.01	0.04	0.00	0.00	24.0
2	25	-4968	-37	375	0	84	2661	15.71	15.71	9.42	9.42	2	0.07	0.01	0.03	0.00	0.00	24.0
3	25	-4872	-20	280	0	114	2738	15.71	15.71	9.42	9.42	2	0.07	0.00	0.02	0.00	0.00	24.0
4	25	-812	155	549	0	146	5417	15.71	15.71	9.42	9.42	2	0.15	0.01	0.04	0.00	0.00	24.0
5	25	-716	173	454	0	176	5494	15.71	15.71	9.42	9.42	2	0.15	0.01	0.03	0.00	0.00	24.0
6	25	-3626	10	547	0	71	3537	15.71	15.71	9.42	9.42	2	0.10	0.01	0.04	0.00	0.00	24.0
7	25	-3306	68	230	0	170	3792	15.71	15.71	9.42	9.42	2	0.11	0.00	0.02	0.00	0.00	24.0
8	25	-2379	68	599	0	90	4363	15.71	15.71	9.42	9.42	2	0.12	0.01	0.04	0.00	0.00	24.0
9	25	-2059	126	282	0	189	4618	15.71	15.71	9.42	9.42	2	0.13	0.00	0.02	0.00	0.00	24.0
10	25	-4968	-37	375	0	84	2661	15.71	15.71	9.42	9.42	2	0.07	0.01	0.03	0.00	0.00	24.0
11	25	-4872	-20	280	0	114	2738	15.71	15.71	9.42	9.42	2	0.07	0.00	0.02	0.00	0.00	24.0
12	25	-812	155	549	0	146	5417	15.71	15.71	9.42	9.42	2	0.15	0.01	0.04	0.00	0.00	24.0
13	25	-716	173	454	0	176	5494	15.71	15.71	9.42	9.42	2	0.15	0.01	0.03	0.00	0.00	24.0
14	25	-3626	10	547	0	71	3537	15.71	15.71	9.42	9.42	2	0.10	0.01	0.04	0.00	0.00	24.0
15	25	-3306	68	230	0	170	3792	15.71	15.71	9.42	9.42	2	0.11	0.00	0.02	0.00	0.00	24.0
16	25	-2379	68	599	0	90	4363	15.71	15.71	9.42	9.42	2	0.12	0.01	0.04	0.00	0.00	24.0
17	25	-2059	126	282	0	189	4618	15.71	15.71	9.42	9.42	2	0.13	0.00	0.02	0.00	0.00	24.0
18	25	-8337	686	813	0	254	5288	15.71	15.71	9.42	9.42	3	0.10	0.01	0.06	0.00	0.00	24.0
19	25	10580	-25	1516	0	474	15905	15.71	15.71	9.42	9.42	3	0.33	0.02	0.11	0.00	0.00	24.0
20	25	616	336	812	0	417	9975	15.71	15.71	9.42	9.42	3	0.20	0.01	0.06	0.00	0.00	24.0
37	25	-16240	842	374	0	117	19	15.71	15.71	9.42	9.42	3	0.00	0.01	0.07	0.00	0.00	24.0
38	25	15290	-342	1546	0	483	17715	15.71	15.71	9.42	9.42	3	0.38	0.02	0.11	0.00	0.00	24.0
39	25	-1314	260	372	0	389	7829	15.71	15.71	9.42	9.42	3	0.15	0.01	0.03	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-3565	88	539	0	101	5312	15.71	15.71	9.42	9.42	3	0.10	0.01	0.04	0.00	0.00	24.0
2	38	-4868	-37	375	0	37	2657	15.71	15.71	9.42	9.42	2	0.07	0.01	0.03	0.00	0.00	24.0
3	38	-4772	-20	280	0	79	2736	15.71	15.71	9.42	9.42	2	0.07	0.00	0.02	0.00	0.00	24.0
4	38	-712	155	549	0	77	5437	15.71	15.71	9.42	9.42	2	0.15	0.01	0.04	0.00	0.00	24.0
5	38	-616	173	454	0	119	5516	15.71	15.71	9.42	9.42	2	0.15	0.01	0.03	0.00	0.00	24.0
6	38	-3526	10	547	0	3	3538	15.71	15.71	9.42	9.42	2	0.09	0.01	0.04	0.00	0.00	24.0
7	38	-3206	68	230	0	141	3801	15.71	15.71	9.42	9.42	2	0.10	0.00	0.02	0.00	0.00	24.0
8	38	-2279	68	599	0	15	4372	15.71	15.71	9.42	9.42	2	0.12	0.01	0.04	0.00	0.00	24.0
9	38	-1959	126	282	0	153	4634	15.71	15.71	9.42	9.42	2	0.13	0.00	0.02	0.00	0.00	24.0
10	38	-4868	-37	375	0	37	2657	15.71	15.71	9.42	9.42	2	0.07	0.01	0.03	0.00	0.00	24.0
11	38	-4772	-20	280	0	79	2736	15.71	15.71	9.42	9.42	2	0.07	0.00	0.02	0.00	0.00	24.0
12	38	-712	155	549	0	77	5437	15.71	15.71	9.42	9.42	2	0.15	0.01	0.04	0.00	0.00	24.0
13	38	-616	173	454	0	119	5516	15.71	15.71	9.42	9.42	2	0.15	0.01	0.03	0.00	0.00	24.0
14	38	-3526	10	547	0	3	3538	15.71	15.71	9.42	9.42	2	0.09	0.01	0.04	0.00	0.00	24.0
15	38	-3206	68	230	0	141	3801	15.71	15.71	9.42	9.42	2	0.10	0.00	0.02	0.00	0.00	24.0
16	38	-2279	68	599	0	15	4372	15.71	15.71	9.42	9.42	2	0.12	0.01	0.04	0.00	0.00	24.0
17	38	-1959	126	282	0	153	4634	15.71	15.71	9.42	9.42	2	0.13	0.00	0.02	0.00	0.00	24.0
18	38	-8207	686	813	0	152	5373	15.71	15.71	9.42	9.42	3	0.10	0.01	0.06	0.00	0.00	24.0
19	38	10710	-25	1516	0	284	15902	15.71	15.71	9.42	9.42	3	0.33	0.02	0.11	0.00	0.00	24.0
20	38	746	336	812	0	316	10017	15.71	15.71	9.42	9.42	3	0.20	0.01	0.06	0.00	0.00	24.0
37	38	-16110	842	374	0	70	125	15.71	15.71	9.42	9.42	3	0.00	0.01	0.07	0.00	0.00	24.0
38	38	15420	-342	1546	0	290	17672	15.71	15.71	9.42	9.42	3	0.37	0.02	0.11	0.00	0.00	24.0
39	38	-1184	260	372	0	342	7862	15.71	15.71	9.42	9.42	3	0.15	0.01	0.03	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-3435	88	539	0	34	5323	15.71	15.71	9.42	9.42	3	0.10	0.01	0.04	0.00	0.00	24.0
2	50	-4768	-37	375	0	-10	2652	15.71	15.71	9.42	9.42	2	0.07	0.01	0.03	0.00	0.00	24.0
3	50	-4672	-20	280	0	44	2733	15.71	15.71	9.42	9.42	2	0.07	0.00	0.02	0.00	0.00	24.0
4	50	-612	155	549	0	9	5456	15.71	15.71	9.42	9.42	2	0.15	0.01	0.04	0.00	0.00	24.0
5	50	-516	173	454	0	62	5537	15.71	15.71	9.42	9.42	2	0.15	0.01	0.03	0.00	0.00	24.0
6	50	-3426	10	547	0	-66	3539	15.71	15.71	9.42	9.42	2	0.10	0.01	0.04	0.00	0.00	24.0
7	50	-3106	68	230	0	112	3809	15.71	15.71	9.42	9.42	2	0.10	0.00	0.02	0.00	0.00	24.0

8	50	-2179	68	599	0	-60	4380	15.71	15.71	9.42	9.42	2	0.12	0.01	0.04	0.00	0.00	24.0
9	50	-1859	126	282	0	118	4650	15.71	15.71	9.42	9.42	2	0.13	0.00	0.02	0.00	0.00	24.0
10	50	-4768	-37	375	0	-10	2652	15.71	15.71	9.42	9.42	2	0.07	0.01	0.03	0.00	0.00	24.0
11	50	-4672	-20	280	0	44	2733	15.71	15.71	9.42	9.42	2	0.07	0.00	0.02	0.00	0.00	24.0
12	50	-612	155	549	0	9	5456	15.71	15.71	9.42	9.42	2	0.15	0.01	0.04	0.00	0.00	24.0
13	50	-516	173	454	0	62	5537	15.71	15.71	9.42	9.42	2	0.15	0.01	0.03	0.00	0.00	24.0
14	50	-3426	10	547	0	-66	3539	15.71	15.71	9.42	9.42	2	0.10	0.01	0.04	0.00	0.00	24.0
15	50	-3106	68	230	0	112	3809	15.71	15.71	9.42	9.42	2	0.10	0.00	0.02	0.00	0.00	24.0
16	50	-2179	68	599	0	-60	4380	15.71	15.71	9.42	9.42	2	0.12	0.01	0.04	0.00	0.00	24.0
17	50	-1859	126	282	0	118	4650	15.71	15.71	9.42	9.42	2	0.13	0.00	0.02	0.00	0.00	24.0
18	50	-8077	686	813	0	51	5459	15.71	15.71	9.42	9.42	3	0.10	0.01	0.06	0.00	0.00	24.0
19	50	10840	-25	1516	0	95	15900	15.71	15.71	9.42	9.42	3	0.33	0.02	0.11	0.00	0.00	24.0
20	50	876	336	812	0	214	10060	15.71	15.71	9.42	9.42	3	0.20	0.01	0.06	0.00	0.00	24.0
37	50	-15980	842	374	0	23	230	15.71	15.71	9.42	9.42	3	0.00	0.01	0.07	0.00	0.00	24.0
38	50	15550	-342	1546	0	97	17630	15.71	15.71	9.42	9.42	3	0.37	0.02	0.11	0.00	0.00	24.0
39	50	-1054	260	372	0	296	7894	15.71	15.71	9.42	9.42	3	0.15	0.01	0.03	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 72 NI 1663 NF 1664 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 31
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-6035	-401	-1747	0	-941	-2303	15.71	15.71	9.42	9.42	3	0.06	0.02	0.12	0.00	0.00	24.0
2	0	-3934	-305	-1515	0	-843	-2150	15.71	15.71	9.42	9.42	2	0.08	0.02	0.10	0.00	0.00	24.0
3	0	-4032	-283	-1605	0	-835	-2087	15.71	15.71	9.42	9.42	2	0.08	0.02	0.11	0.00	0.00	24.0
4	0	-5252	-334	-1082	0	-613	-1456	15.71	15.71	9.42	9.42	2	0.06	0.01	0.07	0.00	0.00	24.0
5	0	-5351	-312	-1172	0	-605	-1394	15.71	15.71	9.42	9.42	2	0.05	0.02	0.08	0.00	0.00	24.0
6	0	-4281	-342	-1259	0	-771	-1980	15.71	15.71	9.42	9.42	2	0.08	0.02	0.09	0.00	0.00	24.0
7	0	-4608	-267	-1558	0	-745	-1771	15.71	15.71	9.42	9.42	2	0.07	0.02	0.11	0.00	0.00	24.0
8	0	-4676	-350	-1129	0	-702	-1772	15.71	15.71	9.42	9.42	2	0.07	0.02	0.08	0.00	0.00	24.0
9	0	-5004	-276	-1428	0	-676	-1563	15.71	15.71	9.42	9.42	2	0.06	0.02	0.10	0.00	0.00	24.0
10	0	-3934	-305	-1515	0	-843	-2150	15.71	15.71	9.42	9.42	2	0.08	0.02	0.10	0.00	0.00	24.0
11	0	-4032	-283	-1605	0	-835	-2087	15.71	15.71	9.42	9.42	2	0.08	0.02	0.11	0.00	0.00	24.0
12	0	-5252	-334	-1082	0	-613	-1456	15.71	15.71	9.42	9.42	2	0.06	0.01	0.07	0.00	0.00	24.0
13	0	-5351	-312	-1172	0	-605	-1394	15.71	15.71	9.42	9.42	2	0.05	0.02	0.08	0.00	0.00	24.0
14	0	-4281	-342	-1259	0	-771	-1980	15.71	15.71	9.42	9.42	2	0.08	0.02	0.09	0.00	0.00	24.0
15	0	-4608	-267	-1558	0	-745	-1771	15.71	15.71	9.42	9.42	2	0.07	0.02	0.11	0.00	0.00	24.0
16	0	-4676	-350	-1129	0	-702	-1772	15.71	15.71	9.42	9.42	2	0.07	0.02	0.08	0.00	0.00	24.0
17	0	-5004	-276	-1428	0	-676	-1563	15.71	15.71	9.42	9.42	2	0.06	0.02	0.10	0.00	0.00	24.0
18	0	1859	-428	-4237	0	-2310	-7597	15.71	15.71	9.42	9.42	3	0.18	0.06	0.30	0.00	0.00	24.0
19	0	-7023	-978	-2334	0	-1281	-3457	15.71	15.71	9.42	9.42	3	0.08	0.03	0.16	0.00	0.00	24.0
20	0	-3315	-610	-3365	0	-1672	-4960	15.71	15.71	9.42	9.42	3	0.12	0.05	0.23	0.00	0.00	24.0
37	0	3667	-145	-4370	0	-2373	-7919	15.71	15.71	9.42	9.42	3	0.19	0.06	0.31	0.00	0.00	24.0
38	0	-11140	-1062	-1199	0	-659	-1019	15.71	15.71	9.42	9.42	3	0.03	0.02	0.09	0.00	0.00	24.0
39	0	-4957	-448	-2916	0	-1310	-3524	15.71	15.71	9.42	9.42	3	0.08	0.04	0.20	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-5905	-401	-1747	0	-723	-2353	15.71	15.71	9.42	9.42	3	0.05	0.02	0.12	0.00	0.00	24.0
2	12	-3834	-305	-1515	0	-653	-2188	15.71	15.71	9.42	9.42	2	0.08	0.02	0.10	0.00	0.00	24.0
3	12	-3932	-283	-1605	0	-634	-2122	15.71	15.71	9.42	9.42	2	0.07	0.02	0.11	0.00	0.00	24.0
4	12	-5152	-334	-1082	0	-478	-1498	15.71	15.71	9.42	9.42	2	0.05	0.01	0.07	0.00	0.00	24.0
5	12	-5251	-312	-1172	0	-458	-1433	15.71	15.71	9.42	9.42	2	0.05	0.02	0.08	0.00	0.00	24.0
6	12	-4181	-342	-1259	0	-614	-2023	15.71	15.71	9.42	9.42	2	0.07	0.02	0.09	0.00	0.00	24.0
7	12	-4508	-267	-1558	0	-550	-1804	15.71	15.71	9.42	9.42	2	0.06	0.02	0.11	0.00	0.00	24.0
8	12	-4576	-350	-1129	0	-561	-1816	15.71	15.71	9.42	9.42	2	0.06	0.02	0.08	0.00	0.00	24.0
9	12	-4904	-276	-1428	0	-498	-1598	15.71	15.71	9.42	9.42	2	0.06	0.02	0.10	0.00	0.00	24.0
10	12	-3834	-305	-1515	0	-653	-2188	15.71	15.71	9.42	9.42	2	0.08	0.02	0.10	0.00	0.00	24.0
11	12	-3932	-283	-1605	0	-634	-2122	15.71	15.71	9.42	9.42	2	0.07	0.02	0.11	0.00	0.00	24.0
12	12	-5152	-334	-1082	0	-478	-1498	15.71	15.71	9.42	9.42	2	0.05	0.01	0.07	0.00	0.00	24.0
13	12	-5251	-312	-1172	0	-458	-1433	15.71	15.71	9.42	9.42	2	0.05	0.02	0.08	0.00	0.00	24.0
14	12	-4181	-342	-1259	0	-614	-2023	15.71	15.71	9.42	9.42	2	0.07	0.02	0.09	0.00	0.00	24.0
15	12	-4508	-267	-1558	0	-550	-1804	15.71	15.71	9.42	9.42	2	0.06	0.02	0.11	0.00	0.00	24.0
16	12	-4576	-350	-1129	0	-561	-1816	15.71	15.71	9.42	9.42	2	0.06	0.02	0.08	0.00	0.00	24.0
17	12	-4904	-276	-1428	0	-498	-1598	15.71	15.71	9.42	9.42	2	0.06	0.02	0.10	0.00	0.00	24.0
18	12	1989	-428	-4237	0	-1780	-7651	15.71	15.71	9.42	9.42	3	0.17	0.06	0.30	0.00	0.00	24.0
19	12	-6893	-978	-2334	0	-989	-3579	15.71	15.71	9.42	9.42	3	0.08	0.03	0.16	0.00	0.00	24.0
20	12	-3185	-610	-3365	0	-1251	-5036	15.71	15.71	9.42	9.42	3	0.11	0.05	0.23	0.00	0.00	24.0
37	12	3797	-145	-4370	0	-1827	-7937	15.71	15.71	9.42	9.42	3	0.18	0.06	0.31	0.00	0.00	24.0
38	12	-11010	-1062	-1199	0	-509	-1152	15.71	15.71	9.42	9.42	3	0.03	0.02	0.09	0.00	0.00	24.0
39	12	-4827	-448	-2916	0	-945	-3580	15.71	15.71	9.42	9.42	3	0.08	0.04	0.20	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-5775	-401	-1747	0	-504	-2403	15.71	15.71	9.42	9.42	3	0.05	0.02	0.12	0.00	0.00	24.0
2	25	-3734	-305	-1515	0	-464	-2226	15.71	15.71	9.42	9.42	2	0.07	0.02	0.10	0.00	0.00	24.0
3	25	-3832	-283	-1605	0	-433	-2157	15.71	15.71	9.42	9.42	2	0.07	0.02	0.11	0.00	0.00	24.0
4	25	-5052	-334	-1082	0	-342	-1540	15.71	15.71	9.42	9.42	2	0.05	0.01	0.07	0.00	0.00	24.0
5	25	-5151	-312	-1172	0	-312	-1472	15.71	15.71	9.42	9.42	2	0.05	0.02	0.08	0.00	0.00	24.0
6	25	-4081	-342	-1259	0	-457	-2066	15.71	15.71	9.42	9.42	2	0.07	0.02	0.09	0.00	0.00	24.0
7	25	-4408	-267	-1558	0	-355	-1838	15.71	15.71	9.42	9.42	2	0.06	0.02	0.11	0.00	0.00	24.0
8	25	-4476	-350	-1129	0	-420	-1860	15.71	15.71	9.42	9.42	2	0.06	0.02	0.08	0.00	0.00	24.0
9	25	-4804	-276	-1428	0	-319	-1632	15.71	15.71	9.42	9.42	2	0.05	0.02	0.10	0.00	0.00	24.0
10	25	-3734	-305	-1515	0	-464	-2226	15.71	15.71	9.42	9.42	2	0.07	0.02	0.10	0.00	0.00	24.0
11	25	-3832	-283	-1605	0	-433	-2157	15.71	15.71	9.42	9.42	2	0.07	0.02	0.11	0.00	0.00	24.0
12	25	-5052	-334	-1082	0	-342	-1540	15.71	15.71	9.42	9.42	2	0.05	0.01	0.07	0.00	0.00	24.0
13	25	-5151	-312	-1172	0	-312	-1472	15.71	15.71	9.42	9.42	2	0.05	0.02	0.08	0.00	0.00	24.0
14	25	-4081	-342	-1259	0	-457	-2066	15.71	15.71	9.42	9.42	2	0.07	0.02	0.09	0.00	0.00	24.0
15	25	-4408	-267	-1558	0	-355	-1838	15.71	15.71	9.42	9.42	2	0.06	0.02	0.11	0.00	0.00	24.0
16	25	-4476	-350	-1129	0	-420	-1860	15.71	15.71	9.42	9.42	2	0.06	0.02	0.08	0.00	0.00	24.0
17	25	-4804	-276	-1428	0	-319	-1632	15.71	15.71	9.42	9.42	2	0.05	0.02	0.10	0.00	0.00	24.0
18	25	2119	-428	-4237	0	-1251	-7704	15.71	15.71	9.42	9.42	3	0.16	0.06	0.30	0.00	0.00	24.0
19	25	-6763	-978	-2334	0	-697	-3702	15.71	15.71	9.42	9.42	3	0.08	0.03	0.16	0.00	0.00	24.0
20	25	-3055	-610	-3365	0	-831	-5113	15.71	15.71	9.42	9.42	3	0.10	0.05	0.23	0.00	0.00	24.0
37	25	3927	-145	-4370	0	-1281	-7955	15.71	15.71	9.42	9.42	3	0.17	0.06	0.31	0.00	0.00	24.0
38	25	-10880	-1062	-1199	0	-359	-1285	15.71	15.71	9.42	9.42	3	0.03	0.02	0.09	0.00	0.00	24.0
39	25	-4697	-448	-2916	0	-581	-3636	15.71	15.71	9.42	9.42	3	0.07	0.04	0.20	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-5645	-401	-1747	0	-286	-2454	15.71	15.71	9.42	9.42	3	0.05	0.02	0.12	0.00	0.00	24.0
2	38	-3634	-305	-1515	0	-274	-2264	15.71	15.71	9.42	9.42	2	0.07	0.02	0.10	0.00	0.00	24.0
3	38	-3732	-283	-1605	0	-233	-2193	15.71	15.71	9.42	9.42	2	0.06	0.02	0.11	0.00	0.00	24.0

4	38	-4952	-334	-1082	0	-207	-1582	15.71	15.71	9.42	9.42	2	0.05	0.01	0.07	0.00	0.00	24.0
5	38	-5051	-312	-1172	0	-165	-1511	15.71	15.71	9.42	9.42	2	0.04	0.02	0.08	0.00	0.00	24.0
6	38	-3981	-342	-1259	0	-299	-2108	15.71	15.71	9.42	9.42	2	0.06	0.02	0.09	0.00	0.00	24.0
7	38	-4308	-267	-1558	0	-161	-1871	15.71	15.71	9.42	9.42	2	0.05	0.02	0.11	0.00	0.00	24.0
8	38	-4376	-350	-1129	0	-279	-1904	15.71	15.71	9.42	9.42	2	0.06	0.02	0.08	0.00	0.00	24.0
9	38	-4704	-276	-1428	0	-140	-1666	15.71	15.71	9.42	9.42	2	0.05	0.02	0.10	0.00	0.00	24.0
10	38	-3634	-305	-1515	0	-274	-2264	15.71	15.71	9.42	9.42	2	0.07	0.02	0.10	0.00	0.00	24.0
11	38	-3732	-283	-1605	0	-233	-2193	15.71	15.71	9.42	9.42	2	0.06	0.02	0.11	0.00	0.00	24.0
12	38	-4952	-334	-1082	0	-207	-1582	15.71	15.71	9.42	9.42	2	0.05	0.01	0.07	0.00	0.00	24.0
13	38	-5051	-312	-1172	0	-165	-1511	15.71	15.71	9.42	9.42	2	0.04	0.02	0.08	0.00	0.00	24.0
14	38	-3981	-342	-1259	0	-299	-2108	15.71	15.71	9.42	9.42	2	0.06	0.02	0.09	0.00	0.00	24.0
15	38	-4308	-267	-1558	0	-161	-1871	15.71	15.71	9.42	9.42	2	0.05	0.02	0.11	0.00	0.00	24.0
16	38	-4376	-350	-1129	0	-279	-1904	15.71	15.71	9.42	9.42	2	0.06	0.02	0.08	0.00	0.00	24.0
17	38	-4704	-276	-1428	0	-140	-1666	15.71	15.71	9.42	9.42	2	0.05	0.02	0.10	0.00	0.00	24.0
18	38	2249	-428	-4237	0	-721	-7757	15.71	15.71	9.42	9.42	3	0.16	0.06	0.30	0.00	0.00	24.0
19	38	-6633	-978	-2334	0	-406	-3824	15.71	15.71	9.42	9.42	3	0.07	0.03	0.16	0.00	0.00	24.0
20	38	-2925	-610	-3365	0	-410	-5189	15.71	15.71	9.42	9.42	3	0.10	0.05	0.23	0.00	0.00	24.0
37	38	4057	-145	-4370	0	-735	-7973	15.71	15.71	9.42	9.42	3	0.16	0.06	0.31	0.00	0.00	24.0
38	38	-10750	-1062	-1199	0	-209	-1417	15.71	15.71	9.42	9.42	3	0.03	0.02	0.09	0.00	0.00	24.0
39	38	-4567	-448	-2916	0	-216	-3692	15.71	15.71	9.42	9.42	3	0.07	0.04	0.20	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-5515	-401	-1747	0	-67	-2504	15.71	15.71	9.42	9.42	3	0.05	0.02	0.12	0.00	0.00	24.0
2	50	-3534	-305	-1515	0	-85	-2302	15.71	15.71	9.42	9.42	2	0.06	0.02	0.10	0.00	0.00	24.0
3	50	-3632	-283	-1605	0	-32	-2228	15.71	15.71	9.42	9.42	2	0.06	0.02	0.11	0.00	0.00	24.0
4	50	-4852	-334	-1082	0	-72	-1624	15.71	15.71	9.42	9.42	2	0.04	0.01	0.07	0.00	0.00	24.0
5	50	-4951	-312	-1172	0	-19	-1550	15.71	15.71	9.42	9.42	2	0.04	0.02	0.08	0.00	0.00	24.0
6	50	-3881	-342	-1259	0	-142	-2151	15.71	15.71	9.42	9.42	2	0.06	0.02	0.09	0.00	0.00	24.0
7	50	-4208	-267	-1558	0	34	-1905	15.71	15.71	9.42	9.42	2	0.05	0.02	0.11	0.00	0.00	24.0
8	50	-4276	-350	-1129	0	-138	-1948	15.71	15.71	9.42	9.42	2	0.06	0.02	0.08	0.00	0.00	24.0
9	50	-4604	-276	-1428	0	38	-1701	15.71	15.71	9.42	9.42	2	0.05	0.02	0.10	0.00	0.00	24.0
10	50	-3534	-305	-1515	0	-85	-2302	15.71	15.71	9.42	9.42	2	0.06	0.02	0.10	0.00	0.00	24.0
11	50	-3632	-283	-1605	0	-32	-2228	15.71	15.71	9.42	9.42	2	0.06	0.02	0.11	0.00	0.00	24.0
12	50	-4852	-334	-1082	0	-72	-1624	15.71	15.71	9.42	9.42	2	0.04	0.01	0.07	0.00	0.00	24.0
13	50	-4951	-312	-1172	0	-19	-1550	15.71	15.71	9.42	9.42	2	0.04	0.02	0.08	0.00	0.00	24.0
14	50	-3881	-342	-1259	0	-142	-2151	15.71	15.71	9.42	9.42	2	0.06	0.02	0.09	0.00	0.00	24.0
15	50	-4208	-267	-1558	0	34	-1905	15.71	15.71	9.42	9.42	2	0.05	0.02	0.11	0.00	0.00	24.0
16	50	-4276	-350	-1129	0	-138	-1948	15.71	15.71	9.42	9.42	2	0.06	0.02	0.08	0.00	0.00	24.0
17	50	-4604	-276	-1428	0	38	-1701	15.71	15.71	9.42	9.42	2	0.05	0.02	0.10	0.00	0.00	24.0
18	50	2379	-428	-4237	0	-191	-7811	15.71	15.71	9.42	9.42	3	0.15	0.06	0.30	0.00	0.00	24.0
19	50	-6503	-978	-2334	0	-114	-3946	15.71	15.71	9.42	9.42	3	0.07	0.03	0.16	0.00	0.00	24.0
20	50	-2795	-610	-3365	0	11	-5265	15.71	15.71	9.42	9.42	3	0.10	0.05	0.23	0.00	0.00	24.0
37	50	4187	-145	-4370	0	-188	-7991	15.71	15.71	9.42	9.42	3	0.16	0.06	0.31	0.00	0.00	24.0
38	50	-10620	-1062	-1199	0	-60	-1550	15.71	15.71	9.42	9.42	3	0.03	0.02	0.09	0.00	0.00	24.0
39	50	-4437	-448	-2916	0	148	-3748	15.71	15.71	9.42	9.42	3	0.07	0.04	0.20	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 73 NI 1664 NF 48 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 31A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-10540	-852	-61	0	-67	-3398	15.71	15.71	9.42	9.42	3	0.06	0.01	0.07	0.00	0.00	24.0
2	0	-7533	-741	82	0	-85	-3011	15.71	15.71	9.42	9.42	2	0.08	0.01	0.06	0.00	0.00	24.0
3	0	-7609	-715	-221	0	-32	-2934	15.71	15.71	9.42	9.42	2	0.08	0.01	0.06	0.00	0.00	24.0
4	0	-8610	-596	128	0	-72	-2294	15.71	15.71	9.42	9.42	2	0.06	0.01	0.05	0.00	0.00	24.0
5	0	-8685	-571	-175	0	-19	-2217	15.71	15.71	9.42	9.42	2	0.06	0.01	0.05	0.00	0.00	24.0
6	0	-7822	-720	451	0	-142	-2850	15.71	15.71	9.42	9.42	2	0.08	0.01	0.06	0.00	0.00	24.0
7	0	-8074	-635	-558	0	34	-2593	15.71	15.71	9.42	9.42	2	0.07	0.01	0.05	0.00	0.00	24.0
8	0	-8145	-676	464	0	-138	-2635	15.71	15.71	9.42	9.42	2	0.07	0.01	0.06	0.00	0.00	24.0
9	0	-8397	-592	-544	0	38	-2378	15.71	15.71	9.42	9.42	2	0.06	0.01	0.05	0.00	0.00	24.0
10	0	-7533	-741	82	0	-85	-3011	15.71	15.71	9.42	9.42	2	0.08	0.01	0.06	0.00	0.00	24.0
11	0	-7609	-715	-221	0	-32	-2934	15.71	15.71	9.42	9.42	2	0.08	0.01	0.06	0.00	0.00	24.0
12	0	-8610	-596	128	0	-72	-2294	15.71	15.71	9.42	9.42	2	0.06	0.01	0.05	0.00	0.00	24.0
13	0	-8685	-571	-175	0	-19	-2217	15.71	15.71	9.42	9.42	2	0.06	0.01	0.05	0.00	0.00	24.0
14	0	-7822	-720	451	0	-142	-2850	15.71	15.71	9.42	9.42	2	0.08	0.01	0.06	0.00	0.00	24.0
15	0	-8074	-635	-558	0	34	-2593	15.71	15.71	9.42	9.42	2	0.07	0.01	0.05	0.00	0.00	24.0
16	0	-8145	-676	464	0	-138	-2635	15.71	15.71	9.42	9.42	2	0.07	0.01	0.06	0.00	0.00	24.0
17	0	-8397	-592	-544	0	38	-2378	15.71	15.71	9.42	9.42	2	0.06	0.01	0.05	0.00	0.00	24.0
18	0	-5392	-1825	53	0	-191	-9083	15.71	15.71	9.42	9.42	3	0.17	0.02	0.16	0.00	0.00	24.0
19	0	-13180	-1822	5	0	-114	-5215	15.71	15.71	9.42	9.42	3	0.10	0.02	0.15	0.00	0.00	24.0
20	0	-9738	-1666	-969	0	11	-6497	15.71	15.71	9.42	9.42	3	0.12	0.02	0.14	0.00	0.00	24.0
37	0	-3236	-1508	36	0	-188	-9143	15.71	15.71	9.42	9.42	3	0.17	0.02	0.14	0.00	0.00	24.0
38	0	-16220	-1502	-44	0	-60	-2696	15.71	15.71	9.42	9.42	3	0.05	0.02	0.12	0.00	0.00	24.0
39	0	-10480	-1243	-1668	0	148	-4833	15.71	15.71	9.42	9.42	3	0.09	0.02	0.11	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-10410	-852	-61	0	-60	-3504	15.71	15.71	9.42	9.42	3	0.06	0.01	0.07	0.00	0.00	24.0
2	12	-7433	-741	82	0	-95	-3104	15.71	15.71	9.42	9.42	2	0.08	0.01	0.06	0.00	0.00	24.0
3	12	-7509	-715	-221	0	-4	-3023	15.71	15.71	9.42	9.42	2	0.08	0.01	0.06	0.00	0.00	24.0
4	12	-8510	-596	128	0	-88	-2368	15.71	15.71	9.42	9.42	2	0.06	0.01	0.05	0.00	0.00	24.0
5	12	-8585	-571	-175	0	3	-2288	15.71	15.71	9.42	9.42	2	0.06	0.01	0.05	0.00	0.00	24.0
6	12	-7722	-720	451	0	-198	-2940	15.71	15.71	9.42	9.42	2	0.08	0.01	0.06	0.00	0.00	24.0
7	12	-7974	-635	-558	0	104	-2673	15.71	15.71	9.42	9.42	2	0.07	0.01	0.05	0.00	0.00	24.0
8	12	-8045	-676	464	0	-196	-2720	15.71	15.71	9.42	9.42	2	0.07	0.01	0.06	0.00	0.00	24.0
9	12	-8297	-592	-544	0	106	-2452	15.71	15.71	9.42	9.42	2	0.07	0.01	0.05	0.00	0.00	24.0
10	12	-7433	-741	82	0	-95	-3104	15.71	15.71	9.42	9.42	2	0.08	0.01	0.06	0.00	0.00	24.0
11	12	-7509	-715	-221	0	-4	-3023	15.71	15.71	9.42	9.42	2	0.08	0.01	0.06	0.00	0.00	24.0
12	12	-8510	-596	128	0	-88	-2368	15.71	15.71	9.42	9.42	2	0.06	0.01	0.05	0.00	0.00	24.0
13	12	-8585	-571	-175	0	3	-2288	15.71	15.71	9.42	9.42	2	0.06	0.01	0.05	0.00	0.00	24.0
14	12	-7722	-720	451	0	-198	-2940	15.71	15.71	9.42	9.42	2	0.08	0.01	0.06	0.00	0.00	24.0
15	12	-7974	-635	-558	0	104	-2673	15.71	15.71	9.42	9.42	2	0.07	0.01	0.05	0.00	0.00	24.0
16	12	-8045	-676	464	0	-196	-2720	15.71	15.71	9.42	9.42	2	0.07	0.01	0.06	0.00	0.00	24.0
17	12	-8297	-592	-544	0	106	-2452	15.71	15.71	9.42	9.42	2	0.07	0.01	0.05	0.00	0.00	24.0
18	12	-5262	-1825	53	0	-198	-9311	15.71	15.71	9.42	9.42	3	0.18	0.02	0.16	0.00	0.00	24.0
19	12	-13050	-1822	5	0	-114	-5443	15.71	15.71	9.42	9.42	3	0.10	0.02	0.15	0.00	0.00	24.0
20	12	-9608	-1666	-969	0	132	-6705	15.71	15.71	9.42	9.42	3	0.12	0.02	0.14	0.00	0.00	24.0
37	12	-3106	-1508	36	0	-193	-9332	15.71	15.71	9.42	9.42	3	0.18	0.02	0.14	0.00	0.00	24.0
38	12	-16090	-1502	-44	0	-54	-2884	15.71	15.71	9.42	9.42	3	0.05	0.02	0.12	0.00	0.00	24.0
39	12	-10350	-1243	-1668	0	356	-4988	15.71	15.71	9.42	9.42	3	0.09	0.02	0.11	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-10280	-852	-61	0	-52	-3611	15.71	15.71	9.42	9.42	3	0.07	0.01	0.07	0.00	0.00	24.0
2	25	-7333	-741	82	0	-105	-3196	15.71	15.71	9.42	9.42	2	0.09	0.01	0.06	0.00	0.00	24.0
3	25	-7409	-715	-221	0	23	-3112	15.71	15.71	9.42	9.42	2	0.08	0.01	0.06	0.00	0.00	24.0
4	25	-8410	-596	128	0	-104	-2443	15.71	15.71	9.42	9.42	2	0.07	0.01	0.05	0.00	0.00	24.0
5	25	-8485	-571	-175	0	25	-2360	15.71	15.71	9.42	9.42	2	0.06	0.01	0.05	0.00	0.00	24.0
6	25	-7622	-720	451	0	-254	-3030	15.71	15.71	9.42	9.42	2	0.08	0.01	0.06	0.00	0.00	24.0
7	25	-7874	-635	-558	0	174	-2752	15.71	15.71	9.42	9.42	2	0.08	0.01	0.05	0.00	0.00	24.0
8	25	-7945	-676	464	0	-254	-2804	15.71	15.71	9.42	9.42	2	0.08	0.01	0.06	0.00	0.00	24.0
9	25	-8197	-592	-544	0	174	-2526	15.71	15.71	9.42	9.42	2	0.07	0.01	0.05	0.00	0.00	24.0
10	25	-7333	-741	82	0	-105	-3196	15.71	15.71	9.42	9.42	2	0.09	0.01	0.06	0.00	0.00	24.0
11	25	-7409	-715	-221	0	23	-3112	15.71	15.71	9.42	9.42	2	0.08	0.01	0.06	0.00	0.00	24.0
12	25	-8410	-596	128	0	-104	-2443	15.71	15.71	9.42	9.42	2	0.07	0.01	0.05	0.00	0.00	24.0
13	25	-8485	-571	-175	0	25	-2360	15.71	15.71	9.42	9.42	2	0.06	0.01	0.05	0.00	0.00	24.0
14	25	-7622	-720	451	0	-254	-3030	15.71	15.71	9.42	9.42	2	0.08	0.01	0.06	0.00	0.00	24.0
15	25	-7874	-635	-558	0	174	-2752	15.71	15.71	9.42	9.42	2	0.08	0.01	0.05	0.00	0.00	24.0
16	25	-7945	-676	464	0	-254	-2804	15.71	15.71	9.42	9.42	2	0.08	0.01	0.06	0.00	0.00	24.0
17	25	-8197	-592	-544	0	174	-2526	15.71	15.71	9.42	9.42	2	0.07	0.01	0.05	0.00	0.00	24.0
18	25	-5132	-1825	53	0	-204	-9540	15.71	15.71	9.42	9.42	3	0.18	0.02	0.16	0.00	0.00	24.0
19	25	-12920	-1822	5	0	-115	-5671	15.71	15.71	9.42	9.42	3	0.10	0.02	0.15	0.00	0.00	24.0
20	25	-9478	-1666	-969	0	253	-6914	15.71	15.71	9.42	9.42	3	0.13	0.02	0.14	0.00	0.00	24.0
37	25	-2976	-1508	36	0	-197	-9520	15.71	15.71	9.42	9.42	3	0.18	0.02	0.14	0.00	0.00	24.0
38	25	-15960	-1502	-44	0	-48	-3072	15.71	15.71	9.42	9.42	3	0.06	0.02	0.12	0.00	0.00	24.0
39	25	-10220	-1243	-1668	0	565	-5144	15.71	15.71	9.42	9.42	3	0.10	0.02	0.11	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-10150	-852	-61	0	-45	-3717	15.71	15.71	9.42	9.42	3	0.07	0.01	0.07	0.00	0.00	24.0
2	38	-7233	-741	82	0	-115	-3288	15.71	15.71	9.42	9.42	2	0.09	0.01	0.06	0.00	0.00	24.0
3	38	-7309	-715	-221	0	51	-3202	15.71	15.71	9.42	9.42	2	0.08	0.01	0.06	0.00	0.00	24.0
4	38	-8310	-596	128	0	-120	-2517	15.71	15.71	9.42	9.42	2	0.07	0.01	0.05	0.00	0.00	24.0
5	38	-8385	-571	-175	0	47	-2431	15.71	15.71	9.42	9.42	2	0.06	0.01	0.05	0.00	0.00	24.0
6	38	-7522	-720	451	0	-311	-3119	15.71	15.71	9.42	9.42	2	0.09	0.01	0.06	0.00	0.00	24.0
7	38	-7774	-635	-558	0	243	-2832	15.71	15.71	9.42	9.42	2	0.08	0.01	0.05	0.00	0.00	24.0
8	38	-7845	-676	464	0	-312	-2889	15.71	15.71	9.42	9.42	2	0.08	0.01	0.06	0.00	0.00	24.0
9	38	-8097	-592	-544	0	242	-2600	15.71	15.71	9.42	9.42	2	0.07	0.01	0.05	0.00	0.00	24.0
10	38	-7233	-741	82	0	-115	-3288	15.71	15.71	9.42	9.42	2	0.09	0.01	0.06	0.00	0.00	24.0
11	38	-7309	-715	-221	0	51	-3202	15.71	15.71	9.42	9.42	2	0.08	0.01	0.06	0.00	0.00	24.0
12	38	-8310	-596	128	0	-120	-2517	15.71	15.71	9.42	9.42	2	0.07	0.01	0.05	0.00	0.00	24.0
13	38	-8385	-571	-175	0	47	-2431	15.71	15.71	9.42	9.42	2	0.06	0.01	0.05	0.00	0.00	24.0
14	38	-7522	-720	451	0	-311	-3119	15.71	15.71	9.42	9.42	2	0.09	0.01	0.06	0.00	0.00	24.0
15	38	-7774	-635	-558	0	243	-2832	15.71	15.71	9.42	9.42	2	0.08	0.01	0.05	0.00	0.00	24.0
16	38	-7845	-676	464	0	-312	-2889	15.71	15.71	9.42	9.42	2	0.08	0.01	0.06	0.00	0.00	24.0
17	38	-8097	-592	-544	0	242	-2600	15.71	15.71	9.42	9.42	2	0.07	0.01	0.05	0.00	0.00	24.0
18	38	-5002	-1825	53	0	-211	-9768	15.71	15.71	9.42	9.42	3	0.18	0.02	0.16	0.00	0.00	24.0
19	38	-12790	-1822	5	0	-116	-5898	15.71	15.71	9.42	9.42	3	0.11	0.02	0.15	0.00	0.00	24.0
20	38	-9348	-1666	-969	0	374	-7122	15.71	15.71	9.42	9.42	3	0.13	0.02	0.14	0.00	0.00	24.0
37	38	-2846	-1508	36	0	-202	-9708	15.71	15.71	9.42	9.42	3	0.19	0.02	0.14	0.00	0.00	24.0
38	38	-15830	-1502	-44	0	-43	-3259	15.71	15.71	9.42	9.42	3	0.06	0.02	0.12	0.00	0.00	24.0
39	38	-10089	-1243	-1668	0	773	-5299	15.71	15.71	9.42	9.42	3	0.10	0.02	0.11	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-10020	-852	-61	0	-37	-3824	15.71	15.71	9.42	9.42	3	0.07	0.01	0.07	0.00	0.00	24.0
2	50	-7133	-741	82	0	-126	-3381	15.71	15.71	9.42	9.42	2	0.09	0.01	0.06	0.00	0.00	24.0
3	50	-7209	-715	-221	0	78	-3291	15.71	15.71	9.42	9.42	2	0.09	0.01	0.06	0.00	0.00	24.0
4	50	-8210	-596	128	0	-135	-2592	15.71	15.71	9.42	9.42	2	0.07	0.01	0.05	0.00	0.00	24.0
5	50	-8285	-571	-175	0	69	-2502	15.71	15.71	9.42	9.42	2	0.07	0.01	0.05	0.00	0.00	24.0
6	50	-7422	-720	451	0	-367	-3209	15.71	15.71	9.42	9.42	2	0.09	0.01	0.06	0.00	0.00	24.0
7	50	-7674	-635	-558	0	313	-2911	15.71	15.71	9.42	9.42	2	0.08	0.01	0.05	0.00	0.00	24.0
8	50	-7745	-676	464	0	-370	-2973	15.71	15.71	9.42	9.42	2	0.09	0.01	0.06	0.00	0.00	24.0
9	50	-7997	-592	-544	0	310	-2674	15.71	15.71	9.42	9.42	2	0.08	0.01	0.05	0.00	0.00	24.0
10	50	-7133	-741	82	0	-126	-3381	15.71	15.71	9.42	9.42	2	0.09	0.01	0.06	0.00	0.00	24.0
11	50	-7209	-715	-221	0	78	-3291	15.71	15.71	9.42	9.42	2	0.09	0.01	0.06	0.00	0.00	24.0
12	50	-8210	-596	128	0	-135	-2592	15.71	15.71	9.42	9.42	2	0.07	0.01	0.05	0.00	0.00	24.0
13	50	-8285	-571	-175	0	69	-2502	15.71	15.71	9.42	9.42	2	0.07	0.01	0.05	0.00	0.00	24.0
14	50	-7422	-720	451	0	-367	-3209	15.71	15.71	9.42	9.42	2	0.09	0.01	0.06	0.00	0.00	24.0
15	50	-7674	-635	-558	0	313	-2911	15.71	15.71	9.42	9.42	2	0.08	0.01	0.05	0.00	0.00	24.0
16	50	-7745	-676	464	0	-370	-2973	15.71	15.71	9.42	9.42	2	0.09	0.01	0.06	0.00	0.00	24.0
17	50	-7997	-592	-544	0	310	-2674	15.71	15.71	9.42	9.42	2	0.08	0.01	0.05	0.00	0.00	24.0
18	50	-4872	-1825	53	0	-218	-9996	15.71	15.71	9.42	9.42	3	0.19	0.02	0.16	0.00	0.00	24.0
19	50	-12660	-1822	5	0	-116	-6126	15.71	15.71	9.42	9.42	3	0.11	0.02	0.15	0.00	0.00	24.0
20	50	-9218	-1666	-969	0	495	-7330	15.71	15.71	9.42	9.42	3	0.14	0.02	0.14	0.00	0.00	24.0
37	50	-2716	-1508	36	0	-206	-9897	15.71	15.71	9.42	9.42	3	0.19	0.02	0.14	0.00	0.00	24.0
38	50	-15700	-1502	-44	0	-37	-3447	15.71	15.71	9.42	9.42	3	0.06	0.02	0.12	0.00	0.00	24.0
39	50	-9959	-1243	-1668	0	982	-5454	15.71	15.71	9.42	9.42	3	0.11	0.02	0.11	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 74 NI 1667 NF 1665 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 30
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-441	-1050	-904	0	-519	-5837	15.71	15.71	9.42	9.42	3	0.12	0.01	0.10	0.00	0.00	24.0
2	0	1300	-910	-796	0	-479	-5404	15.71	15.71	9.42	9.42	2	0.16	0.01	0.09	0.00	0.00	24.0
3	0	1298	-923	-894	0	-472	-5408	15.71	15.71	9.42	9.42	2	0.16	0.01	0.09	0.00	0.00	24.0
4	0	-1976	-692	-497	0	-326	-3572	15.71	15.71	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
5	0	-1978	-705	-595	0	-320	-3576	15.71	15.71	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
6	0	156	-818	-578	0	-433	-4758	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
7	0	148	-862	-903	0	-412	-4772	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
8	0	-827	-753	-488	0	-387	-4208	15.71	15.71	9.42	9.42	2	0.12	0.01	0.07	0.00	0.00	24.0
9	0	-834	-797	-814	0	-366	-4222	15.71	15.71	9.42	9.42	2	0.12	0.01	0.07	0.00	0.00	24.0
10	0	1300	-910	-796	0	-479	-5404	15.71	15.71	9.42	9.42	2	0.16	0.01	0.09	0.00	0.00	24.0
11	0	1298	-923	-894	0	-472	-5408	15.71	15.71	9.42	9.42	2	0.16	0.01	0.09	0.00	0.00	24.0
12	0	-1976	-692	-497	0	-326	-3572	15.71	15.71	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
13	0	-1978	-705	-595	0	-320	-3576	15.71	15.71	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
14	0	156	-818	-578	0	-433	-4758	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
15	0	148	-862	-903	0	-412	-4772	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
16	0	-827	-753	-488	0	-387	-4208	15.71	15.71	9.42	9.42	2	0.12	0.01	0.07	0.00	0.00	24.0
17	0	-834	-797	-814	0	-366	-4222	15.71	15.71	9.42	9.42	2	0.12	0.01	0.07	0.00	0.00	24.0
18	0	16240	-1968	-2270	0	-1293	-16510	15.71	15.71	9.42	9.42	3	0.36	0.03	0.18	0.00	0.00	24.0
19	0	333	-1924	-1125	0	-687	-8280	15.71	15.71	9.42	9.42	3	0.17	0.03	0.18	0.00	0.00	24.0
20	0	7128	-1853	-1894	0	-903	-11490	15.71	15.71	9.42	9.42	3	0.24	0.03	0.17	0.00	0.00	24.0
37	0	18670	-1691	-2394	0	-1342	-17110	15.71	15.71	9.42	9.42	3	0.38	0.03	0.17	0.00	0.00	24.0

38	0	-7839	-1618	-486	0	-331	-3394	15.71	15.71	9.42	9.42	3	0.07	0.02	0.14	0.00	0.00	24.0
39	0	3485	-1499	-1767	0	-691	-8737	15.71	15.71	9.42	9.42	3	0.18	0.02	0.14	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-311	-1050	-904	0	-406	-5968	15.71	15.71	9.42	9.42	3	0.12	0.01	0.10	0.00	0.00	24.0
2	12	1400	-910	-796	0	-379	-5518	15.71	15.71	9.42	9.42	2	0.16	0.01	0.09	0.00	0.00	24.0
3	12	1398	-923	-894	0	-361	-5524	15.71	15.71	9.42	9.42	2	0.16	0.01	0.09	0.00	0.00	24.0
4	12	-1876	-692	-497	0	-264	-3658	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
5	12	-1878	-705	-595	0	-245	-3664	15.71	15.71	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
6	12	256	-818	-578	0	-360	-4860	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
7	12	248	-862	-903	0	-299	-4880	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
8	12	-727	-753	-488	0	-326	-4302	15.71	15.71	9.42	9.42	2	0.13	0.01	0.07	0.00	0.00	24.0
9	12	-734	-797	-814	0	-264	-4322	15.71	15.71	9.42	9.42	2	0.12	0.01	0.07	0.00	0.00	24.0
10	12	1400	-910	-796	0	-379	-5518	15.71	15.71	9.42	9.42	2	0.16	0.01	0.09	0.00	0.00	24.0
11	12	1398	-923	-894	0	-361	-5524	15.71	15.71	9.42	9.42	2	0.16	0.01	0.09	0.00	0.00	24.0
12	12	-1876	-692	-497	0	-264	-3658	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
13	12	-1878	-705	-595	0	-245	-3664	15.71	15.71	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
14	12	256	-818	-578	0	-360	-4860	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
15	12	248	-862	-903	0	-299	-4880	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
16	12	-727	-753	-488	0	-326	-4302	15.71	15.71	9.42	9.42	2	0.13	0.01	0.07	0.00	0.00	24.0
17	12	-734	-797	-814	0	-264	-4322	15.71	15.71	9.42	9.42	2	0.12	0.01	0.07	0.00	0.00	24.0
18	12	16370	-1968	-2270	0	-1009	-16755	15.71	15.71	9.42	9.42	3	0.36	0.03	0.18	0.00	0.00	24.0
19	12	463	-1924	-1125	0	-546	-8520	15.71	15.71	9.42	9.42	3	0.17	0.03	0.18	0.00	0.00	24.0
20	12	7258	-1853	-1894	0	-666	-11720	15.71	15.71	9.42	9.42	3	0.24	0.03	0.17	0.00	0.00	24.0
37	12	18800	-1691	-2394	0	-1043	-17320	15.71	15.71	9.42	9.42	3	0.38	0.03	0.17	0.00	0.00	24.0
38	12	-7709	-1618	-486	0	-270	-3596	15.71	15.71	9.42	9.42	3	0.07	0.02	0.14	0.00	0.00	24.0
39	12	3615	-1499	-1767	0	-470	-8925	15.71	15.71	9.42	9.42	3	0.18	0.02	0.14	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-181	-1050	-904	0	-293	-6100	15.71	15.71	9.42	9.42	3	0.12	0.01	0.10	0.00	0.00	24.0
2	25	1500	-910	-796	0	-279	-5632	15.71	15.71	9.42	9.42	2	0.16	0.01	0.09	0.00	0.00	24.0
3	25	1498	-923	-894	0	-249	-5639	15.71	15.71	9.42	9.42	2	0.16	0.01	0.09	0.00	0.00	24.0
4	25	-1776	-692	-497	0	-202	-3745	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
5	25	-1778	-705	-595	0	-171	-3753	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
6	25	356	-818	-578	0	-288	-4963	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
7	25	348	-862	-903	0	-186	-4988	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
8	25	-627	-753	-488	0	-265	-4396	15.71	15.71	9.42	9.42	2	0.13	0.01	0.07	0.00	0.00	24.0
9	25	-634	-797	-814	0	-162	-4421	15.71	15.71	9.42	9.42	2	0.12	0.01	0.07	0.00	0.00	24.0
10	25	1500	-910	-796	0	-279	-5632	15.71	15.71	9.42	9.42	2	0.16	0.01	0.09	0.00	0.00	24.0
11	25	1498	-923	-894	0	-249	-5639	15.71	15.71	9.42	9.42	2	0.16	0.01	0.09	0.00	0.00	24.0
12	25	-1776	-692	-497	0	-202	-3745	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
13	25	-1778	-705	-595	0	-171	-3753	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
14	25	356	-818	-578	0	-288	-4963	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
15	25	348	-862	-903	0	-186	-4988	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
16	25	-627	-753	-488	0	-265	-4396	15.71	15.71	9.42	9.42	2	0.13	0.01	0.07	0.00	0.00	24.0
17	25	-634	-797	-814	0	-162	-4421	15.71	15.71	9.42	9.42	2	0.12	0.01	0.07	0.00	0.00	24.0
18	25	16500	-1968	-2270	0	-726	-17000	15.71	15.71	9.42	9.42	3	0.37	0.03	0.18	0.00	0.00	24.0
19	25	593	-1924	-1125	0	-405	-8761	15.71	15.71	9.42	9.42	3	0.17	0.03	0.18	0.00	0.00	24.0
20	25	7388	-1853	-1894	0	-429	-11950	15.71	15.71	9.42	9.42	3	0.24	0.03	0.17	0.00	0.00	24.0
37	25	18930	-1691	-2394	0	-743	-17530	15.71	15.71	9.42	9.42	3	0.38	0.03	0.17	0.00	0.00	24.0
38	25	-7579	-1618	-486	0	-209	-3798	15.71	15.71	9.42	9.42	3	0.07	0.02	0.14	0.00	0.00	24.0
39	25	3745	-1499	-1767	0	-249	-9112	15.71	15.71	9.42	9.42	3	0.18	0.02	0.14	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-51	-1050	-904	0	-180	-6231	15.71	15.71	9.42	9.42	3	0.12	0.01	0.10	0.00	0.00	24.0
2	38	1600	-910	-796	0	-180	-5745	15.71	15.71	9.42	9.42	2	0.16	0.01	0.09	0.00	0.00	24.0
3	38	1598	-923	-894	0	-137	-5755	15.71	15.71	9.42	9.42	2	0.16	0.01	0.09	0.00	0.00	24.0
4	38	-1676	-692	-497	0	-139	-3831	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
5	38	-1678	-705	-595	0	-97	-3841	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
6	38	456	-818	-578	0	-216	-5065	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
7	38	448	-862	-903	0	-73	-5095	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
8	38	-527	-753	-488	0	-204	-4490	15.71	15.71	9.42	9.42	2	0.13	0.01	0.07	0.00	0.00	24.0
9	38	-534	-797	-814	0	-61	-4521	15.71	15.71	9.42	9.42	2	0.12	0.01	0.07	0.00	0.00	24.0
10	38	1600	-910	-796	0	-180	-5745	15.71	15.71	9.42	9.42	2	0.16	0.01	0.09	0.00	0.00	24.0
11	38	1598	-923	-894	0	-137	-5755	15.71	15.71	9.42	9.42	2	0.16	0.01	0.09	0.00	0.00	24.0
12	38	-1676	-692	-497	0	-139	-3831	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
13	38	-1678	-705	-595	0	-97	-3841	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
14	38	456	-818	-578	0	-216	-5065	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
15	38	448	-862	-903	0	-73	-5095	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
16	38	-527	-753	-488	0	-204	-4490	15.71	15.71	9.42	9.42	2	0.13	0.01	0.07	0.00	0.00	24.0
17	38	-534	-797	-814	0	-61	-4521	15.71	15.71	9.42	9.42	2	0.12	0.01	0.07	0.00	0.00	24.0
18	38	16630	-1968	-2270	0	-442	-17245	15.71	15.71	9.42	9.42	3	0.37	0.03	0.18	0.00	0.00	24.0
19	38	723	-1924	-1125	0	-265	-9002	15.71	15.71	9.42	9.42	3	0.18	0.03	0.18	0.00	0.00	24.0
20	38	7518	-1853	-1894	0	-193	-12180	15.71	15.71	9.42	9.42	3	0.25	0.03	0.17	0.00	0.00	24.0
37	38	19060	-1691	-2394	0	-444	-17740	15.71	15.71	9.42	9.42	3	0.39	0.03	0.17	0.00	0.00	24.0
38	38	-7449	-1618	-486	0	-148	-4000	15.71	15.71	9.42	9.42	3	0.08	0.02	0.14	0.00	0.00	24.0
39	38	3875	-1499	-1767	0	-28	-9300	15.71	15.71	9.42	9.42	3	0.18	0.02	0.14	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	79	-1050	-904	0	-67	-6362	15.71	15.71	9.42	9.42	3	0.12	0.01	0.10	0.00	0.00	24.0
2	50	1700	-910	-796	0	-80	-5859	15.71	15.71	9.42	9.42	2	0.16	0.01	0.09	0.00	0.00	24.0
3	50	1698	-923	-894	0	-25	-5870	15.71	15.71	9.42	9.42	2	0.16	0.01	0.09	0.00	0.00	24.0
4	50	-1576	-692	-497	0	-77	-3918	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
5	50	-1578	-705	-595	0	-22	-3929	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
6	50	556	-818	-578	0	-144	-5167	15.71	15.71	9.42	9.42	2	0.15	0.01	0.08	0.00	0.00	24.0
7	50	548	-862	-903	0	40	-5203	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
8	50	-427	-753	-488	0	-143	-4584	15.71	15.71	9.42	9.42	2	0.13	0.01	0.07	0.00	0.00	24.0
9	50	-434	-797	-814	0	41	-4621	15.71	15.71	9.42	9.42	2	0.13	0.01	0.07	0.00	0.00	24.0
10	50	1700	-910	-796	0	-80	-5859	15.71	15.71	9.42	9.42	2	0.16	0.01	0.09	0.00	0.00	24.0
11	50	1698	-923	-894	0	-25	-5870	15.71	15.71	9.42	9.42	2	0.16	0.01	0.09	0.00	0.00	24.0
12	50	-1576	-692	-497	0	-77	-3918	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
13	50	-1578	-705	-595	0	-22	-3929	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
14	50	556	-818	-578	0	-144	-5167	15.71	15.71	9.42	9.42	2	0.15	0.01	0.08	0.00	0.00	24.0
15	50	548	-862	-903	0	40	-5203	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
16	50	-427	-753	-488	0	-143	-4584	15.71	15.71	9.42	9.42	2	0.13	0.01	0.07	0.00	0.00	24.0
17	50	-434	-797	-814	0	41	-4621	15.71	15.71	9.42	9.42	2	0.13	0.01	0.07	0.00	0.00	24.0
18	50	16760	-1968	-2270	0	-158	-17490	15.71	15.71	9.42	9.42	3	0.37	0.03	0.18	0.00	0.00	24.0
19	50	853	-1924	-1125	0	-124	-9242	15.71	15.71	9.42	9.42	3	0.18	0.03	0.18	0.00	0.00	24.0
20	50	7648	-1853	-1894	0	44	-12410	15.71	15.71	9.42	9.42	3	0.25	0.03	0.17	0.00	0.00	24.0
37	50	19190	-1691	-2394	0	-144	-17950	15.71	15.71	9.42	9.42	3	0.39	0.03	0.17	0.00	0.00	24.0
38	50	-7319	-1618	-486	0	-88	-4202	15.71	15.71	9.42	9.42	3	0.08	0.02	0.14	0.00	0.00	24.0
39	50	4005	-1499	-1767	0	193	-9487	15.71	15.71	9.42	9.42	3	0.19	0.02	0.14	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 75 NI 1684 NF 1683 SEZ. Rp B= 0.400 H= 0.800 (pilastro)

PIL. NUM. 29
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	528	-949	260	0	42	-6407	15.71	15.71	9.42	9.42	3	0.12	0.01	0.09	0.00	0.00	24.0
2	0	2282	-826	234	0	23	-5970	15.71	15.71	9.42	9.42	2	0.17	0.01	0.08	0.00	0.00	24.0
3	0	2192	-808	134	0	27	-5913	15.71	15.71	9.42	9.42	2	0.16	0.01	0.08	0.00	0.00	24.0
4	0	-1379	-652	266	0	39	-3944	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
5	0	-1469	-634	167	0	43	-3887	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
6	0	1106	-786	361	0	23	-5328	15.71	15.71	9.42	9.42	2	0.15	0.01	0.07	0.00	0.00	24.0
7	0	805	-726	30	0	37	-5137	15.71	15.71	9.42	9.42	2	0.14	0.01	0.07	0.00	0.00	24.0
8	0	8	-734	371	0	28	-4720	15.71	15.71	9.42	9.42	2	0.13	0.01	0.07	0.00	0.00	24.0
9	0	-293	-674	40	0	42	-4529	15.71	15.71	9.42	9.42	2	0.12	0.01	0.06	0.00	0.00	24.0
10	0	2282	-826	234	0	23	-5970	15.71	15.71	9.42	9.42	2	0.17	0.01	0.08	0.00	0.00	24.0
11	0	2192	-808	134	0	27	-5913	15.71	15.71	9.42	9.42	2	0.16	0.01	0.08	0.00	0.00	24.0
12	0	-1379	-652	266	0	39	-3944	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
13	0	-1469	-634	167	0	43	-3887	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
14	0	1106	-786	361	0	23	-5328	15.71	15.71	9.42	9.42	2	0.15	0.01	0.07	0.00	0.00	24.0
15	0	805	-726	30	0	37	-5137	15.71	15.71	9.42	9.42	2	0.14	0.01	0.07	0.00	0.00	24.0
16	0	8	-734	371	0	28	-4720	15.71	15.71	9.42	9.42	2	0.13	0.01	0.07	0.00	0.00	24.0
17	0	-293	-674	40	0	42	-4529	15.71	15.71	9.42	9.42	2	0.12	0.01	0.06	0.00	0.00	24.0
18	0	18800	-1699	522	0	75	-17950	15.71	15.71	9.42	9.42	3	0.39	0.02	0.16	0.00	0.00	24.0
19	0	1572	-1847	514	0	99	-9052	15.71	15.71	9.42	9.42	3	0.18	0.02	0.17	0.00	0.00	24.0
20	0	8582	-1610	192	0	91	-12320	15.71	15.71	9.42	9.42	3	0.25	0.02	0.15	0.00	0.00	24.0
37	0	21370	-1382	439	0	52	-18600	15.71	15.71	9.42	9.42	3	0.41	0.02	0.13	0.00	0.00	24.0
38	0	-7345	-1628	426	0	92	-3768	15.71	15.71	9.42	9.42	3	0.07	0.02	0.14	0.00	0.00	24.0
39	0	4338	-1234	-112	0	79	-9219	15.71	15.71	9.42	9.42	3	0.18	0.02	0.12	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	658	-949	260	0	10	-6526	15.71	15.71	9.42	9.42	3	0.13	0.01	0.09	0.00	0.00	24.0
2	12	2382	-826	234	0	-7	-6073	15.71	15.71	9.42	9.42	2	0.17	0.01	0.08	0.00	0.00	24.0
3	12	2292	-808	134	0	10	-6014	15.71	15.71	9.42	9.42	2	0.17	0.01	0.08	0.00	0.00	24.0
4	12	-1279	-652	266	0	5	-4025	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
5	12	-1369	-634	167	0	22	-3966	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
6	12	1206	-786	361	0	-22	-5426	15.71	15.71	9.42	9.42	2	0.15	0.01	0.07	0.00	0.00	24.0
7	12	905	-726	30	0	33	-5228	15.71	15.71	9.42	9.42	2	0.14	0.01	0.07	0.00	0.00	24.0
8	12	108	-734	371	0	-18	-4812	15.71	15.71	9.42	9.42	2	0.13	0.01	0.07	0.00	0.00	24.0
9	12	-193	-674	40	0	37	-4613	15.71	15.71	9.42	9.42	2	0.13	0.01	0.06	0.00	0.00	24.0
10	12	2382	-826	234	0	-7	-6073	15.71	15.71	9.42	9.42	2	0.17	0.01	0.08	0.00	0.00	24.0
11	12	2292	-808	134	0	10	-6014	15.71	15.71	9.42	9.42	2	0.17	0.01	0.08	0.00	0.00	24.0
12	12	-1279	-652	266	0	5	-4025	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
13	12	-1369	-634	167	0	22	-3966	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
14	12	1206	-786	361	0	-22	-5426	15.71	15.71	9.42	9.42	2	0.15	0.01	0.07	0.00	0.00	24.0
15	12	905	-726	30	0	33	-5228	15.71	15.71	9.42	9.42	2	0.14	0.01	0.07	0.00	0.00	24.0
16	12	108	-734	371	0	-18	-4812	15.71	15.71	9.42	9.42	2	0.13	0.01	0.07	0.00	0.00	24.0
17	12	-193	-674	40	0	37	-4613	15.71	15.71	9.42	9.42	2	0.13	0.01	0.06	0.00	0.00	24.0
18	12	18930	-1699	522	0	9	-18163	15.71	15.71	9.42	9.42	3	0.39	0.02	0.16	0.00	0.00	24.0
19	12	1702	-1847	514	0	34	-9283	15.71	15.71	9.42	9.42	3	0.18	0.02	0.17	0.00	0.00	24.0
20	12	8712	-1610	192	0	67	-12522	15.71	15.71	9.42	9.42	3	0.25	0.02	0.15	0.00	0.00	24.0
37	12	21500	-1382	439	0	-3	-18772	15.71	15.71	9.42	9.42	3	0.41	0.02	0.13	0.00	0.00	24.0
38	12	-7215	-1628	426	0	39	-3971	15.71	15.71	9.42	9.42	3	0.07	0.02	0.14	0.00	0.00	24.0
39	12	4468	-1234	-112	0	93	-9373	15.71	15.71	9.42	9.42	3	0.19	0.02	0.12	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	788	-949	260	0	-23	-6644	15.71	15.71	9.42	9.42	3	0.13	0.01	0.09	0.00	0.00	24.0
2	25	2482	-826	234	0	-36	-6176	15.71	15.71	9.42	9.42	2	0.17	0.01	0.08	0.00	0.00	24.0
3	25	2392	-808	134	0	-7	-6115	15.71	15.71	9.42	9.42	2	0.17	0.01	0.08	0.00	0.00	24.0
4	25	-1179	-652	266	0	-28	-4107	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
5	25	-1269	-634	167	0	1	-4046	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
6	25	1306	-786	361	0	-67	-5524	15.71	15.71	9.42	9.42	2	0.15	0.01	0.07	0.00	0.00	24.0
7	25	1005	-726	30	0	30	-5318	15.71	15.71	9.42	9.42	2	0.15	0.01	0.07	0.00	0.00	24.0
8	25	208	-734	371	0	-64	-4904	15.71	15.71	9.42	9.42	2	0.14	0.01	0.07	0.00	0.00	24.0
9	25	-93	-674	40	0	32	-4697	15.71	15.71	9.42	9.42	2	0.13	0.01	0.06	0.00	0.00	24.0
10	25	2482	-826	234	0	-36	-6176	15.71	15.71	9.42	9.42	2	0.17	0.01	0.08	0.00	0.00	24.0
11	25	2392	-808	134	0	-7	-6115	15.71	15.71	9.42	9.42	2	0.17	0.01	0.08	0.00	0.00	24.0
12	25	-1179	-652	266	0	-28	-4107	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
13	25	-1269	-634	167	0	1	-4046	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
14	25	1306	-786	361	0	-67	-5524	15.71	15.71	9.42	9.42	2	0.15	0.01	0.07	0.00	0.00	24.0
15	25	1005	-726	30	0	30	-5318	15.71	15.71	9.42	9.42	2	0.15	0.01	0.07	0.00	0.00	24.0
16	25	208	-734	371	0	-64	-4904	15.71	15.71	9.42	9.42	2	0.14	0.01	0.07	0.00	0.00	24.0
17	25	-93	-674	40	0	32	-4697	15.71	15.71	9.42	9.42	2	0.13	0.01	0.06	0.00	0.00	24.0
18	25	19060	-1699	522	0	-56	-18375	15.71	15.71	9.42	9.42	3	0.40	0.02	0.16	0.00	0.00	24.0
19	25	1832	-1847	514	0	-30	-9513	15.71	15.71	9.42	9.42	3	0.19	0.02	0.17	0.00	0.00	24.0
20	25	8842	-1610	192	0	43	-12725	15.71	15.71	9.42	9.42	3	0.26	0.02	0.15	0.00	0.00	24.0
37	25	21630	-1382	439	0	-58	-18945	15.71	15.71	9.42	9.42	3	0.42	0.02	0.13	0.00	0.00	24.0
38	25	-7085	-1628	426	0	-14	-4175	15.71	15.71	9.42	9.42	3	0.08	0.02	0.14	0.00	0.00	24.0
39	25	4598	-1234	-112	0	107	-9528	15.71	15.71	9.42	9.42	3	0.19	0.02	0.12	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	918	-949	260	0	-55	-6763	15.71	15.71	9.42	9.42	3	0.13	0.01	0.09	0.00	0.00	24.0
2	38	2582	-826	234	0	-65	-6280	15.71	15.71	9.42	9.42	2	0.18	0.01	0.08	0.00	0.00	24.0
3	38	2492	-808	134	0	-24	-6216	15.71	15.71	9.42	9.42	2	0.17	0.01	0.08	0.00	0.00	24.0
4	38	-1079	-652	266	0	-61	-4189	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
5	38	-1169	-634	167	0	-20	-4125	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
6	38	1406	-786	361	0	-112	-5623	15.71	15.71	9.42	9.42	2	0.16	0.01	0.07	0.00	0.00	24.0
7	38	1105	-726	30	0	26	-5409	15.71	15.71	9.42	9.42	2	0.15	0.01	0.07	0.00	0.00	24.0
8	38	308	-734	371	0	-111	-4995	15.71	15.71	9.42	9.42	2	0.14	0.01	0.07	0.00	0.00	24.0
9	38	7	-674	40	0	27	-4782	15.71	15.71	9.42	9.42	2	0.13	0.01	0.06	0.00	0.00	24.0
10	38	2582	-826	234	0	-65	-6280	15.71	15.71	9.42	9.42	2	0.18	0.01	0.08	0.00	0.00	24.0
11	38	2492	-808	134	0	-24	-6216	15.71	15.71	9.42	9.42	2	0.17	0.01	0.08	0.00	0.00	24.0
12	38	-1079	-652	266	0	-61	-4189	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
13	38	-1169	-634	167	0	-20	-4125	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
14	38	1406	-786	361	0	-112	-5623	15.71	15.71	9.42	9.42	2	0.16	0.01	0.07	0.00	0.00	24.0
15	38	1105	-726	30	0	26	-5409	15.71	15.71	9.42	9.42	2	0.15	0.01	0.07	0.00	0.00	24.0
16	38	308	-734	371	0	-111	-4995	15.71	15.71	9.42	9.42	2	0.14	0.01	0.07	0.00	0.00	24.0
17	38	7	-674	40	0	27	-4782	15.71	15.71	9.42	9.42	2	0.13	0.01	0.06	0.00	0.00	24.0
18	38	19190	-1699	522	0	-121	-18587	15.71	15.71	9.42	9.42	3	0.40	0.02	0.16	0.00	0.00	24.0
19	38	1962	-1847	514	0	-94	-9744	15.71	15.71	9.42	9.42	3	0.19	0.02	0.17	0.00	0.00	24.0
20	38	8972	-1610	192	0	19	-12927	15.71	15.71	9.42	9.42	3	0.26	0.02	0.15	0.00	0.00	24.0
37	38	21760	-1382	439	0	-112	-19118	15.71	15.71	9.42	9.42	3	0.42	0.02	0.13	0.00	0.00	24.0
38	38	-6955	-1628	426	0	-68	-4378	15.71	15.71	9.42	9.42	3	0.08	0.02	0.14	0.00	0.00	24.0
39	38	4728	-1234	-112	0	121	-9682	15.71	15.71	9.42	9.42	3	0.19	0.02	0.12	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	1048	-949	260	0	-88	-6881	15.71	15.71	9.42	9.42	3	0.13	0.01	0.09	0.00	0.00	24.0
2	50	2682	-826	234	0	-94	-6383	15.71	15.71	9.42	9.42	2	0.18	0.01	0.08	0.00	0.00	24.0
3	50	2592	-808	134	0	-40	-6317	15.71	15.71	9.42	9.42	2	0.18	0.01	0.08	0.00	0.00	24.0
4	50	-979	-652	266	0	-94	-4270	15.71	15.71	9.42	9.42	2	0.12	0.01	0.06	0.00	0.00	24.0
5	50	-1069	-634	167	0	-41	-4204	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
6	50	1506	-786	361	0	-157	-5721	15.71	15.71	9.42	9.42	2	0.16	0.01	0.07	0.00	0.00	24.0
7	50	1205	-726	30	0	22	-5500	15.71	15.71	9.42	9.42	2	0.15	0.01	0.07	0.00	0.00	24.0
8	50	408	-734	371	0	-157	-5087	15.71	15.71	9.42	9.42	2	0.14	0.01	0.07	0.00	0.00	24.0
9	50	107	-674	40	0	22	-4866	15.71	15.71	9.42	9.42	2	0.13	0.01	0.06	0.00	0.00	24.0
10	50	2682	-826	234	0	-94	-6383	15.71	15.71	9.42	9.42	2	0.18	0.01	0.08	0.00	0.00	24.0
11	50	2592	-808	134	0	-40	-6317	15.71	15.71	9.42	9.42	2	0.18	0.01	0.08	0.00	0.00	24.0
12	50	-979	-652	266	0	-94	-4270	15.71	15.71	9.42	9.42	2	0.12	0.01	0.06	0.00	0.00	24.0
13	50	-1069	-634	167	0	-41	-4204	15.71	15.71	9.42	9.42	2	0.11	0.01	0.06	0.00	0.00	24.0
14	50	1506	-786	361	0	-157	-5721	15.71	15.71	9.42	9.42	2	0.16	0.01	0.07	0.00	0.00	24.0
15	50	1205	-726	30	0	22	-5500	15.71	15.71	9.42	9.42	2	0.15	0.01	0.07	0.00	0.00	24.0
16	50	408	-734	371	0	-157	-5087	15.71	15.71	9.42	9.42	2	0.14	0.01	0.07	0.00	0.00	24.0
17	50	107	-674	40	0	22	-4866	15.71	15.71	9.42	9.42	2	0.13	0.01	0.06	0.00	0.00	24.0
18	50	19320	-1699	522	0	-186	-18800	15.71	15.71	9.42	9.42	3	0.41	0.02	0.16	0.00	0.00	24.0
19	50	2092	-1847	514	0	-159	-9975	15.71	15.71	9.42	9.42	3	0.20	0.02	0.17	0.00	0.00	24.0
20	50	9102	-1610	192	0	-5	-13130	15.71	15.71	9.42	9.42	3	0.27	0.02	0.15	0.00	0.00	24.0
37	50	21890	-1382	439	0	-167	-19290	15.71	15.71	9.42	9.42	3	0.43	0.02	0.13	0.00	0.00	24.0
38	50	-6825	-1628	426	0	-121	-4582	15.71	15.71	9.42	9.42	3	0.09	0.02	0.14	0.00	0.00	24.0
39	50	4858	-1234	-112	0	135	-9836	15.71	15.71	9.42	9.42	3	0.20	0.02	0.12	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 76 NI 1692 NF 1691 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 28
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-745	-1104	1370	0	589	-5681	15.71	15.71	9.42	9.42	3	0.11	0.02	0.10	0.00	0.00	24.0
2	0	1257	-988	1225	0	513	-5395	15.71	15.71	9.42	9.42	2	0.16	0.02	0.09	0.00	0.00	24.0
3	0	1250	-993	1118	0	509	-5393	15.71	15.71	9.42	9.42	2	0.16	0.02	0.09	0.00	0.00	24.0
4	0	-2397	-706	990	0	398	-3347	15.71	15.71	9.42	9.42	2	0.10	0.01	0.07	0.00	0.00	24.0
5	0	-2404	-710	882	0	394	-3344	15.71	15.71	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
6	0	-13	-884	1268	0	477	-4681	15.71	15.71	9.42	9.42	2	0.14	0.02	0.09	0.00	0.00	24.0
7	0	-38	-900	911	0	465	-4673	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
8	0	-1109	-799	1197	0	442	-4066	15.71	15.71	9.42	9.42	2	0.12	0.02	0.08	0.00	0.00	24.0
9	0	-1134	-815	840	0	430	-4059	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
10	0	1257	-988	1225	0	513	-5395	15.71	15.71	9.42	9.42	2	0.16	0.02	0.09	0.00	0.00	24.0
11	0	1250	-993	1118	0	509	-5393	15.71	15.71	9.42	9.42	2	0.16	0.02	0.09	0.00	0.00	24.0
12	0	-2397	-706	990	0	398	-3347	15.71	15.71	9.42	9.42	2	0.10	0.01	0.07	0.00	0.00	24.0
13	0	-2404	-710	882	0	394	-3344	15.71	15.71	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
14	0	-13	-884	1268	0	477	-4681	15.71	15.71	9.42	9.42	2	0.14	0.02	0.09	0.00	0.00	24.0
15	0	-38	-900	911	0	465	-4673	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
16	0	-1109	-799	1197	0	442	-4066	15.71	15.71	9.42	9.42	2	0.12	0.02	0.08	0.00	0.00	24.0
17	0	-1134	-815	840	0	430	-4059	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
18	0	16410	-2309	3290	0	1423	-16610	15.71	15.71	9.42	9.42	3	0.36	0.05	0.23	0.00	0.00	24.0
19	0	-610	-1973	2100	0	870	-7747	15.71	15.71	9.42	9.42	3	0.16	0.03	0.18	0.00	0.00	24.0
20	0	6630	-1999	2209	0	1055	-11220	15.71	15.71	9.42	9.42	3	0.23	0.03	0.19	0.00	0.00	24.0
37	0	19250	-2084	3253	0	1425	-17440	15.71	15.71	9.42	9.42	3	0.39	0.05	0.23	0.00	0.00	24.0
38	0	-9129	-1523	1271	0	505	-2668	15.71	15.71	9.42	9.42	3	0.05	0.02	0.13	0.00	0.00	24.0
39	0	2939	-1566	1452	0	813	-8452	15.71	15.71	9.42	9.42	3	0.17	0.02	0.15	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-615	-1104	1370	0	418	-5819	15.71	15.71	9.42	9.42	3	0.11	0.02	0.10	0.00	0.00	24.0
2	12	1357	-988	1225	0	360	-5519	15.71	15.71	9.42	9.42	2	0.16	0.02	0.09	0.00	0.00	24.0
3	12	1350	-993	1118	0	370	-5517	15.71	15.71	9.42	9.42	2	0.16	0.02	0.09	0.00	0.00	24.0
4	12	-2297	-706	990	0	274	-3435	15.71	15.71	9.42	9.42	2	0.10	0.01	0.07	0.00	0.00	24.0
5	12	-2304	-710	882	0	284	-3433	15.71	15.71	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
6	12	87	-884	1268	0	318	-4792	15.71	15.71	9.42	9.42	2	0.14	0.02	0.09	0.00	0.00	24.0
7	12	62	-900	911	0	351	-4786	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
8	12	-1009	-799	1197	0	292	-4166	15.71	15.71	9.42	9.42	2	0.12	0.02	0.08	0.00	0.00	24.0
9	12	-1034	-815	840	0	325	-4161	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
10	12	1357	-988	1225	0	360	-5519	15.71	15.71	9.42	9.42	2	0.16	0.02	0.09	0.00	0.00	24.0
11	12	1350	-993	1118	0	370	-5517	15.71	15.71	9.42	9.42	2	0.16	0.02	0.09	0.00	0.00	24.0
12	12	-2297	-706	990	0	274	-3435	15.71	15.71	9.42	9.42	2	0.10	0.01	0.07	0.00	0.00	24.0
13	12	-2304	-710	882	0	284	-3433	15.71	15.71	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
14	12	87	-884	1268	0	318	-4792	15.71	15.71	9.42	9.42	2	0.14	0.02	0.09	0.00	0.00	24.0
15	12	62	-900	911	0	351	-4786	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
16	12	-1009	-799	1197	0	292	-4166	15.71	15.71	9.42	9.42	2	0.12	0.02	0.08	0.00	0.00	24.0
17	12	-1034	-815	840	0	325	-4161	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
18	12	16540	-2309	3290	0	1012	-16900	15.71	15.71	9.42	9.42	3	0.37	0.05	0.23	0.00	0.00	24.0
19	12	-481	-1973	2100	0	608	-7994	15.71	15.71	9.42	9.42	3	0.16	0.03	0.18	0.00	0.00	24.0
20	12	6760	-1999	2209	0	779	-11470	15.71	15.71	9.42	9.42	3	0.24	0.03	0.19	0.00	0.00	24.0
37	12	19380	-2084	3253	0	1018	-17700	15.71	15.71	9.42	9.42	3	0.39	0.05	0.23	0.00	0.00	24.0
38	12	-8999	-1523	1271	0	346	-2858	15.71	15.71	9.42	9.42	3	0.06	0.02	0.13	0.00	0.00	24.0
39	12	3069	-1566	1452	0	631	-8648	15.71	15.71	9.42	9.42	3	0.17	0.02	0.15	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-485	-1104	1370	0	247	-5957	15.71	15.71	9.42	9.42	3	0.12	0.02	0.10	0.00	0.00	24.0
2	25	1457	-988	1225	0	207	-5642	15.71	15.71	9.42	9.42	2	0.16	0.02	0.09	0.00	0.00	24.0
3	25	1450	-993	1118	0	230	-5642	15.71	15.71	9.42	9.42	2	0.16	0.02	0.09	0.00	0.00	24.0
4	25	-2197	-706	990	0	150	-3523	15.71	15.71	9.42	9.42	2	0.10	0.01	0.07	0.00	0.00	24.0
5	25	-2204	-710	882	0	173	-3522	15.71	15.71	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
6	25	187	-884	1268	0	160	-4902	15.71	15.71	9.42	9.42	2	0.14	0.02	0.09	0.00	0.00	24.0
7	25	162	-900	911	0	237	-4898	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
8	25	-909	-799	1197	0	143	-4266	15.71	15.71	9.42	9.42	2	0.12	0.02	0.08	0.00	0.00	24.0
9	25	-934	-815	840	0	220	-4262	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
10	25	1457	-988	1225	0	207	-5642	15.71	15.71	9.42	9.42	2	0.16	0.02	0.09	0.00	0.00	24.0
11	25	1450	-993	1118	0	230	-5642	15.71	15.71	9.42	9.42	2	0.16	0.02	0.09	0.00	0.00	24.0
12	25	-2197	-706	990	0	150	-3523	15.71	15.71	9.42	9.42	2	0.10	0.01	0.07	0.00	0.00	24.0
13	25	-2204	-710	882	0	173	-3522	15.71	15.71	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
14	25	187	-884	1268	0	160	-4902	15.71	15.71	9.42	9.42	2	0.14	0.02	0.09	0.00	0.00	24.0
15	25	162	-900	911	0	237	-4898	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
16	25	-909	-799	1197	0	143	-4266	15.71	15.71	9.42	9.42	2	0.12	0.02	0.08	0.00	0.00	24.0
17	25	-934	-815	840	0	220	-4262	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
18	25	16670	-2309	3290	0	600	-17190	15.71	15.71	9.42	9.42	3	0.37	0.05	0.23	0.00	0.00	24.0
19	25	-351	-1973	2100	0	346	-8240	15.71	15.71	9.42	9.42	3	0.16	0.03	0.18	0.00	0.00	24.0

20	25	6890	-1999	2209	0	503	-11720	15.71	15.71	9.42	9.42	3	0.24	0.03	0.19	0.00	0.00	24.0
37	25	19510	-2084	3253	0	612	-17960	15.71	15.71	9.42	9.42	3	0.39	0.05	0.23	0.00	0.00	24.0
38	25	-8869	-1523	1271	0	187	-3048	15.71	15.71	9.42	9.42	3	0.06	0.02	0.13	0.00	0.00	24.0
39	25	3199	-1566	1452	0	450	-8844	15.71	15.71	9.42	9.42	3	0.18	0.02	0.15	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-355	-1104	1370	0	76	-6095	15.71	15.71	9.42	9.42	3	0.12	0.02	0.10	0.00	0.00	24.0
2	38	1557	-988	1225	0	53	-5766	15.71	15.71	9.42	9.42	2	0.16	0.02	0.09	0.00	0.00	24.0
3	38	1550	-993	1118	0	90	-5766	15.71	15.71	9.42	9.42	2	0.16	0.02	0.09	0.00	0.00	24.0
4	38	-2097	-706	990	0	26	-3611	15.71	15.71	9.42	9.42	2	0.10	0.01	0.07	0.00	0.00	24.0
5	38	-2104	-710	882	0	63	-3610	15.71	15.71	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
6	38	287	-884	1268	0	1	-5012	15.71	15.71	9.42	9.42	2	0.14	0.02	0.09	0.00	0.00	24.0
7	38	262	-900	911	0	123	-5011	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
8	38	-809	-799	1197	0	-7	-4366	15.71	15.71	9.42	9.42	2	0.12	0.02	0.08	0.00	0.00	24.0
9	38	-834	-815	840	0	115	-4364	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
10	38	1557	-988	1225	0	53	-5766	15.71	15.71	9.42	9.42	2	0.16	0.02	0.09	0.00	0.00	24.0
11	38	1550	-993	1118	0	90	-5766	15.71	15.71	9.42	9.42	2	0.16	0.02	0.09	0.00	0.00	24.0
12	38	-2097	-706	990	0	26	-3611	15.71	15.71	9.42	9.42	2	0.10	0.01	0.07	0.00	0.00	24.0
13	38	-2104	-710	882	0	63	-3610	15.71	15.71	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
14	38	287	-884	1268	0	1	-5012	15.71	15.71	9.42	9.42	2	0.14	0.02	0.09	0.00	0.00	24.0
15	38	262	-900	911	0	123	-5011	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
16	38	-809	-799	1197	0	-7	-4366	15.71	15.71	9.42	9.42	2	0.12	0.02	0.08	0.00	0.00	24.0
17	38	-834	-815	840	0	115	-4364	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
18	38	16800	-2309	3290	0	189	-17480	15.71	15.71	9.42	9.42	3	0.37	0.05	0.23	0.00	0.00	24.0
19	38	-221	-1973	2100	0	83	-8487	15.71	15.71	9.42	9.42	3	0.16	0.03	0.18	0.00	0.00	24.0
20	38	7020	-1999	2209	0	227	-11970	15.71	15.71	9.42	9.42	3	0.24	0.03	0.19	0.00	0.00	24.0
37	38	19640	-2084	3253	0	205	-18220	15.71	15.71	9.42	9.42	3	0.40	0.05	0.23	0.00	0.00	24.0
38	38	-8739	-1523	1271	0	28	-3239	15.71	15.71	9.42	9.42	3	0.06	0.02	0.13	0.00	0.00	24.0
39	38	3329	-1566	1452	0	268	-9039	15.71	15.71	9.42	9.42	3	0.18	0.02	0.15	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-225	-1104	1370	0	-96	-6233	15.71	15.71	9.42	9.42	3	0.12	0.02	0.10	0.00	0.00	24.0
2	50	1657	-988	1225	0	-100	-5890	15.71	15.71	9.42	9.42	2	0.17	0.02	0.09	0.00	0.00	24.0
3	50	1650	-993	1118	0	-50	-5890	15.71	15.71	9.42	9.42	2	0.16	0.02	0.09	0.00	0.00	24.0
4	50	-1997	-706	990	0	-97	-3699	15.71	15.71	9.42	9.42	2	0.10	0.01	0.07	0.00	0.00	24.0
5	50	-2004	-710	882	0	-47	-3699	15.71	15.71	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
6	50	387	-884	1268	0	-157	-5123	15.71	15.71	9.42	9.42	2	0.14	0.02	0.09	0.00	0.00	24.0
7	50	362	-900	911	0	9	-5123	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
8	50	-709	-799	1197	0	-156	-4466	15.71	15.71	9.42	9.42	2	0.13	0.02	0.08	0.00	0.00	24.0
9	50	-734	-815	840	0	10	-4466	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
10	50	1657	-988	1225	0	-100	-5890	15.71	15.71	9.42	9.42	2	0.17	0.02	0.09	0.00	0.00	24.0
11	50	1650	-993	1118	0	-50	-5890	15.71	15.71	9.42	9.42	2	0.16	0.02	0.09	0.00	0.00	24.0
12	50	-1997	-706	990	0	-97	-3699	15.71	15.71	9.42	9.42	2	0.10	0.01	0.07	0.00	0.00	24.0
13	50	-2004	-710	882	0	-47	-3699	15.71	15.71	9.42	9.42	2	0.10	0.01	0.06	0.00	0.00	24.0
14	50	387	-884	1268	0	-157	-5123	15.71	15.71	9.42	9.42	2	0.14	0.02	0.09	0.00	0.00	24.0
15	50	362	-900	911	0	9	-5123	15.71	15.71	9.42	9.42	2	0.14	0.01	0.08	0.00	0.00	24.0
16	50	-709	-799	1197	0	-156	-4466	15.71	15.71	9.42	9.42	2	0.13	0.02	0.08	0.00	0.00	24.0
17	50	-734	-815	840	0	10	-4466	15.71	15.71	9.42	9.42	2	0.12	0.01	0.08	0.00	0.00	24.0
18	50	16930	-2309	3290	0	-222	-17770	15.71	15.71	9.42	9.42	3	0.38	0.05	0.23	0.00	0.00	24.0
19	50	-91	-1973	2100	0	-180	-8733	15.71	15.71	9.42	9.42	3	0.17	0.03	0.18	0.00	0.00	24.0
20	50	7150	-1999	2209	0	-49	-12220	15.71	15.71	9.42	9.42	3	0.25	0.03	0.19	0.00	0.00	24.0
37	50	19770	-2084	3253	0	-201	-18480	15.71	15.71	9.42	9.42	3	0.40	0.05	0.23	0.00	0.00	24.0
38	50	-8609	-1523	1271	0	-131	-3429	15.71	15.71	9.42	9.42	3	0.06	0.02	0.13	0.00	0.00	24.0
39	50	3459	-1566	1452	0	87	-9235	15.71	15.71	9.42	9.42	3	0.18	0.02	0.15	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 77 NI 1700 NF 1699 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 27
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-6958	-807	2375	0	1124	-1534	15.71	15.71	9.42	9.42	3	0.05	0.03	0.16	0.00	0.00	24.0
2	0	-4085	-833	2152	0	1011	-1873	15.71	15.71	9.42	9.42	2	0.08	0.03	0.15	0.00	0.00	24.0
3	0	-4058	-862	2065	0	1018	-1916	15.71	15.71	9.42	9.42	2	0.08	0.03	0.14	0.00	0.00	24.0
4	0	-6647	-380	1589	0	711	-444	15.71	15.71	9.42	9.42	2	0.04	0.02	0.12	0.00	0.00	24.0
5	0	-6620	-408	1502	0	718	-487	15.71	15.71	9.42	9.42	2	0.04	0.02	0.11	0.00	0.00	24.0
6	0	-5014	-640	2056	0	898	-1322	15.71	15.71	9.42	9.42	2	0.06	0.03	0.14	0.00	0.00	24.0
7	0	-4923	-737	1767	0	921	-1466	15.71	15.71	9.42	9.42	2	0.07	0.02	0.12	0.00	0.00	24.0
8	0	-5783	-504	1888	0	808	-893	15.71	15.71	9.42	9.42	2	0.05	0.03	0.13	0.00	0.00	24.0
9	0	-5691	-601	1598	0	831	-1038	15.71	15.71	9.42	9.42	2	0.06	0.02	0.11	0.00	0.00	24.0
10	0	-4085	-833	2152	0	1011	-1873	15.71	15.71	9.42	9.42	2	0.08	0.03	0.15	0.00	0.00	24.0
11	0	-4058	-862	2065	0	1018	-1916	15.71	15.71	9.42	9.42	2	0.08	0.03	0.14	0.00	0.00	24.0
12	0	-6647	-380	1589	0	711	-444	15.71	15.71	9.42	9.42	2	0.04	0.02	0.12	0.00	0.00	24.0
13	0	-6620	-408	1502	0	718	-487	15.71	15.71	9.42	9.42	2	0.04	0.02	0.11	0.00	0.00	24.0
14	0	-5014	-640	2056	0	898	-1322	15.71	15.71	9.42	9.42	2	0.06	0.03	0.14	0.00	0.00	24.0
15	0	-4923	-737	1767	0	921	-1466	15.71	15.71	9.42	9.42	2	0.07	0.02	0.12	0.00	0.00	24.0
16	0	-5783	-504	1888	0	808	-893	15.71	15.71	9.42	9.42	2	0.05	0.03	0.13	0.00	0.00	24.0
17	0	-5691	-601	1598	0	831	-1038	15.71	15.71	9.42	9.42	2	0.06	0.02	0.11	0.00	0.00	24.0
18	0	2146	-2258	5956	0	2910	-7544	15.71	15.71	9.42	9.42	3	0.19	0.08	0.42	0.00	0.00	24.0
19	0	-10180	-1076	3299	0	1534	-1329	15.71	15.71	9.42	9.42	3	0.06	0.05	0.24	0.00	0.00	24.0
20	0	-4381	-1615	4061	0	2077	-4120	15.71	15.71	9.42	9.42	3	0.11	0.06	0.28	0.00	0.00	24.0
37	0	5277	-2369	6107	0	3010	-8665	15.71	15.71	9.42	9.42	3	0.21	0.09	0.43	0.00	0.00	24.0
38	0	-15270	-399	1679	0	717	1694	15.71	15.71	9.42	9.42	3	0.04	0.02	0.10	0.00	0.00	24.0
39	0	-5601	-1297	2948	0	1622	-2958	15.71	15.71	9.42	9.42	3	0.08	0.04	0.20	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-6828	-807	2375	0	827	-1635	15.71	15.71	9.42	9.42	3	0.04	0.03	0.16	0.00	0.00	24.0
2	12	-3985	-833	2152	0	742	-1977	15.71	15.71	9.42	9.42	2	0.07	0.03	0.15	0.00	0.00	24.0
3	12	-3958	-862	2065	0	760	-2024	15.71	15.71	9.42	9.42	2	0.08	0.03	0.14	0.00	0.00	24.0
4	12	-6547	-380	1589	0	512	-491	15.71	15.71	9.42	9.42	2	0.03	0.02	0.12	0.00	0.00	24.0
5	12	-6520	-408	1502	0	530	-538	15.71	15.71	9.42	9.42	2	0.03	0.02	0.10	0.00	0.00	24.0
6	12	-4914	-640	2056	0	641	-1402	15.71	15.71	9.42	9.42	2	0.06	0.03	0.14	0.00	0.00	24.0
7	12	-4823	-737	1767	0	700	-1558	15.71	15.71	9.42	9.42	2	0.06	0.02	0.12	0.00	0.00	24.0
8	12	-5683	-504	1888	0	572	-956	15.71	15.71	9.42	9.42	2	0.04	0.03	0.13	0.00	0.00	24.0
9	12	-5591	-601	1598	0	631	-1113	15.71	15.71	9.42	9.42	2	0.05	0.02	0.11	0.00	0.00	24.0
10	12	-3985	-833	2152	0	742	-1977	15.71	15.71	9.42	9.42	2	0.07	0.03	0.15	0.00	0.00	24.0
11	12	-3958	-862	2065	0	760	-2024	15.71	15.71	9.42	9.42	2	0.08	0.03	0.14	0.00	0.00	24.0
12	12	-6547	-380	1589	0	512	-491	15.71	15.71	9.42	9.42	2	0.03	0.02	0.12	0.00	0.00	24.0
13	12	-6520	-408	1502	0	530	-538	15.71	15.71	9.42	9.42	2	0.03	0.02	0.10	0.00	0.00	24.0
14	12	-4914	-640	2056	0	641	-1402	15.71	15.71	9.42	9.42	2	0.06	0.03	0.14	0.00	0.00	24.0
15	12	-4823	-737	1767	0	700	-1558	15.71	15.71	9.42	9.42	2	0.06	0.02	0.12	0.00	0.00	24.0

16	12	-5683	-504	1888	0	572	-956	15.71	15.71	9.42	9.42	2	0.04	0.03	0.13	0.00	0.00	24.0
17	12	-5591	-601	1598	0	631	-1113	15.71	15.71	9.42	9.42	2	0.05	0.02	0.11	0.00	0.00	24.0
18	12	2276	-2258	5956	0	2165	-7826	15.71	15.71	9.42	9.42	3	0.18	0.08	0.42	0.00	0.00	24.0
19	12	-10050	-1076	3299	0	1122	-1463	15.71	15.71	9.42	9.42	3	0.05	0.05	0.21	0.00	0.00	24.0
20	12	-4251	-1615	4061	0	1569	-4322	15.71	15.71	9.42	9.42	3	0.10	0.06	0.28	0.00	0.00	24.0
37	12	5407	-2369	6107	0	2247	-8961	15.71	15.71	9.42	9.42	3	0.20	0.09	0.43	0.00	0.00	24.0
38	12	-15140	-399	1679	0	507	1644	15.71	15.71	9.42	9.42	3	0.04	0.02	0.10	0.00	0.00	24.0
39	12	-5471	-1297	2948	0	1253	-3120	15.71	15.71	9.42	9.42	3	0.08	0.04	0.20	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-6698	-807	2375	0	530	-1736	15.71	15.71	9.42	9.42	3	0.04	0.03	0.16	0.00	0.00	24.0
2	25	-3885	-833	2152	0	473	-2081	15.71	15.71	9.42	9.42	2	0.07	0.03	0.15	0.00	0.00	24.0
3	25	-3858	-862	2065	0	502	-2132	15.71	15.71	9.42	9.42	2	0.07	0.03	0.14	0.00	0.00	24.0
4	25	-6447	-380	1589	0	314	-539	15.71	15.71	9.42	9.42	2	0.02	0.02	0.11	0.00	0.00	24.0
5	25	-6420	-408	1502	0	342	-589	15.71	15.71	9.42	9.42	2	0.03	0.02	0.10	0.00	0.00	24.0
6	25	-4814	-640	2056	0	384	-1482	15.71	15.71	9.42	9.42	2	0.05	0.03	0.14	0.00	0.00	24.0
7	25	-4723	-737	1767	0	479	-1651	15.71	15.71	9.42	9.42	2	0.06	0.02	0.12	0.00	0.00	24.0
8	25	-5583	-504	1888	0	336	-1019	15.71	15.71	9.42	9.42	2	0.04	0.03	0.13	0.00	0.00	24.0
9	25	-5491	-601	1598	0	431	-1188	15.71	15.71	9.42	9.42	2	0.04	0.02	0.11	0.00	0.00	24.0
10	25	-3885	-833	2152	0	473	-2081	15.71	15.71	9.42	9.42	2	0.07	0.03	0.15	0.00	0.00	24.0
11	25	-3858	-862	2065	0	502	-2132	15.71	15.71	9.42	9.42	2	0.07	0.03	0.14	0.00	0.00	24.0
12	25	-6447	-380	1589	0	314	-539	15.71	15.71	9.42	9.42	2	0.02	0.02	0.11	0.00	0.00	24.0
13	25	-6420	-408	1502	0	342	-589	15.71	15.71	9.42	9.42	2	0.03	0.02	0.10	0.00	0.00	24.0
14	25	-4814	-640	2056	0	384	-1482	15.71	15.71	9.42	9.42	2	0.05	0.03	0.14	0.00	0.00	24.0
15	25	-4723	-737	1767	0	479	-1651	15.71	15.71	9.42	9.42	2	0.06	0.02	0.12	0.00	0.00	24.0
16	25	-5583	-504	1888	0	336	-1019	15.71	15.71	9.42	9.42	2	0.04	0.03	0.13	0.00	0.00	24.0
17	25	-5491	-601	1598	0	431	-1188	15.71	15.71	9.42	9.42	2	0.04	0.02	0.11	0.00	0.00	24.0
18	25	2406	-2258	5956	0	1421	-8109	15.71	15.71	9.42	9.42	3	0.17	0.08	0.42	0.00	0.00	24.0
19	25	-9921	-1076	3299	0	709	-1598	15.71	15.71	9.42	9.42	3	0.04	0.05	0.21	0.00	0.00	24.0
20	25	-4121	-1615	4061	0	1062	-4523	15.71	15.71	9.42	9.42	3	0.10	0.06	0.28	0.00	0.00	24.0
37	25	5537	-2369	6107	0	1483	-9258	15.71	15.71	9.42	9.42	3	0.20	0.09	0.43	0.00	0.00	24.0
38	25	-15010	-399	1679	0	297	1594	15.71	15.71	9.42	9.42	3	0.03	0.02	0.10	0.00	0.00	24.0
39	25	-5341	-1297	2948	0	885	-3282	15.71	15.71	9.42	9.42	3	0.07	0.04	0.20	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-6568	-807	2375	0	233	-1836	15.71	15.71	9.42	9.42	3	0.04	0.03	0.16	0.00	0.00	24.0
2	38	-3785	-833	2152	0	204	-2185	15.71	15.71	9.42	9.42	2	0.06	0.03	0.15	0.00	0.00	24.0
3	38	-3758	-862	2065	0	244	-2239	15.71	15.71	9.42	9.42	2	0.07	0.03	0.14	0.00	0.00	24.0
4	38	-6347	-380	1589	0	115	-586	15.71	15.71	9.42	9.42	2	0.02	0.02	0.11	0.00	0.00	24.0
5	38	-6320	-408	1502	0	154	-640	15.71	15.71	9.42	9.42	2	0.02	0.02	0.10	0.00	0.00	24.0
6	38	-4714	-640	2056	0	127	-1562	15.71	15.71	9.42	9.42	2	0.04	0.03	0.14	0.00	0.00	24.0
7	38	-4623	-737	1767	0	258	-1743	15.71	15.71	9.42	9.42	2	0.05	0.02	0.12	0.00	0.00	24.0
8	38	-5483	-504	1888	0	100	-1082	15.71	15.71	9.42	9.42	2	0.03	0.03	0.13	0.00	0.00	24.0
9	38	-5391	-601	1598	0	232	-1263	15.71	15.71	9.42	9.42	2	0.04	0.02	0.11	0.00	0.00	24.0
10	38	-3785	-833	2152	0	204	-2185	15.71	15.71	9.42	9.42	2	0.06	0.03	0.15	0.00	0.00	24.0
11	38	-3758	-862	2065	0	244	-2239	15.71	15.71	9.42	9.42	2	0.07	0.03	0.14	0.00	0.00	24.0
12	38	-6347	-380	1589	0	115	-586	15.71	15.71	9.42	9.42	2	0.02	0.02	0.11	0.00	0.00	24.0
13	38	-6320	-408	1502	0	154	-640	15.71	15.71	9.42	9.42	2	0.02	0.02	0.10	0.00	0.00	24.0
14	38	-4714	-640	2056	0	127	-1562	15.71	15.71	9.42	9.42	2	0.04	0.03	0.14	0.00	0.00	24.0
15	38	-4623	-737	1767	0	258	-1743	15.71	15.71	9.42	9.42	2	0.05	0.02	0.12	0.00	0.00	24.0
16	38	-5483	-504	1888	0	100	-1082	15.71	15.71	9.42	9.42	2	0.03	0.03	0.13	0.00	0.00	24.0
17	38	-5391	-601	1598	0	232	-1263	15.71	15.71	9.42	9.42	2	0.04	0.02	0.11	0.00	0.00	24.0
18	38	2536	-2258	5956	0	676	-8391	15.71	15.71	9.42	9.42	3	0.17	0.08	0.42	0.00	0.00	24.0
19	38	-9792	-1076	3299	0	297	-1732	15.71	15.71	9.42	9.42	3	0.03	0.05	0.21	0.00	0.00	24.0
20	38	-3991	-1615	4061	0	554	-4725	15.71	15.71	9.42	9.42	3	0.09	0.06	0.28	0.00	0.00	24.0
37	38	5667	-2369	6107	0	720	-9554	15.71	15.71	9.42	9.42	3	0.20	0.09	0.43	0.00	0.00	24.0
38	38	-14880	-399	1679	0	87	1544	15.71	15.71	9.42	9.42	3	0.03	0.02	0.10	0.00	0.00	24.0
39	38	-5211	-1297	2948	0	516	-3444	15.71	15.71	9.42	9.42	3	0.07	0.04	0.20	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-6438	-807	2375	0	-64	-1937	15.71	15.71	9.42	9.42	3	0.04	0.03	0.16	0.00	0.00	24.0
2	50	-3685	-833	2152	0	-65	-2289	15.71	15.71	9.42	9.42	2	0.06	0.03	0.15	0.00	0.00	24.0
3	50	-3658	-862	2065	0	-15	-2347	15.71	15.71	9.42	9.42	2	0.06	0.03	0.14	0.00	0.00	24.0
4	50	-6247	-380	1589	0	-84	-633	15.71	15.71	9.42	9.42	2	0.02	0.02	0.11	0.00	0.00	24.0
5	50	-6220	-408	1502	0	-33	-691	15.71	15.71	9.42	9.42	2	0.02	0.02	0.10	0.00	0.00	24.0
6	50	-4614	-640	2056	0	-130	-1642	15.71	15.71	9.42	9.42	2	0.05	0.03	0.14	0.00	0.00	24.0
7	50	-4523	-737	1767	0	38	-1835	15.71	15.71	9.42	9.42	2	0.05	0.02	0.12	0.00	0.00	24.0
8	50	-5383	-504	1888	0	-136	-1145	15.71	15.71	9.42	9.42	2	0.03	0.03	0.13	0.00	0.00	24.0
9	50	-5291	-601	1598	0	32	-1338	15.71	15.71	9.42	9.42	2	0.04	0.02	0.11	0.00	0.00	24.0
10	50	-3685	-833	2152	0	-65	-2289	15.71	15.71	9.42	9.42	2	0.06	0.03	0.15	0.00	0.00	24.0
11	50	-3658	-862	2065	0	-15	-2347	15.71	15.71	9.42	9.42	2	0.06	0.03	0.14	0.00	0.00	24.0
12	50	-6247	-380	1589	0	-84	-633	15.71	15.71	9.42	9.42	2	0.02	0.02	0.11	0.00	0.00	24.0
13	50	-6220	-408	1502	0	-33	-691	15.71	15.71	9.42	9.42	2	0.02	0.02	0.10	0.00	0.00	24.0
14	50	-4614	-640	2056	0	-130	-1642	15.71	15.71	9.42	9.42	2	0.05	0.03	0.14	0.00	0.00	24.0
15	50	-4523	-737	1767	0	38	-1835	15.71	15.71	9.42	9.42	2	0.05	0.02	0.12	0.00	0.00	24.0
16	50	-5383	-504	1888	0	-136	-1145	15.71	15.71	9.42	9.42	2	0.03	0.03	0.13	0.00	0.00	24.0
17	50	-5291	-601	1598	0	32	-1338	15.71	15.71	9.42	9.42	2	0.04	0.02	0.11	0.00	0.00	24.0
18	50	2666	-2258	5956	0	-68	-8673	15.71	15.71	9.42	9.42	3	0.17	0.08	0.42	0.00	0.00	24.0
19	50	-9662	-1076	3299	0	-116	-1867	15.71	15.71	9.42	9.42	3	0.04	0.05	0.22	0.00	0.00	24.0
20	50	-3861	-1615	4061	0	47	-4927	15.71	15.71	9.42	9.42	3	0.09	0.06	0.28	0.00	0.00	24.0
37	50	5797	-2369	6107	0	-44	-9850	15.71	15.71	9.42	9.42	3	0.20	0.09	0.43	0.00	0.00	24.0
38	50	-14750	-399	1679	0	-122	1494	15.71	15.71	9.42	9.42	3	0.03	0.02	0.10	0.00	0.00	24.0
39	50	-5081	-1297	2948	0	148	-3606	15.71	15.71	9.42	9.42	3	0.07	0.04	0.20	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 78 NI 1665 NF 91 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 30A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm

1	0	-6363	-2026	209	0	-67	-7473	15.71	15.71	9.42	9.42	3	0.14	0.03	0.18	0.00	0.00	24.0
2	0	-3573	-1824	286	0	-80	-6762	15.71	15.71	9.42	9.42	2	0.18	0.02	0.16	0.00	0.00	24.0
3	0	-3578	-1835	-22	0	-25	-6774	15.71	15.71	9.42	9.42	2	0.18	0.02	0.16	0.00	0.00	24.0
4	0	-6212	-1282	344	0	-77	-4724	15.71	15.71	9.42	9.42	2	0.13	0.02	0.11	0.00	0.00	24.0
5	0	-6217	-1292	35	0	-22	-4736	15.71	15.71	9.42	9.42	2	0.12	0.02	0.11	0.00	0.00	24.0
6	0	-4490	-1623	666	0	-144	-6035	15.71	15.71	9.42	9.42	2	0.16	0.02	0.14	0.00	0.00	24.0
7	0	-4508	-1656	-362	0	40	-6074	15.71	15.71	9.42	9.42	2	0.16	0.02	0.15	0.00	0.00	24.0
8	0	-5282	-1460	683	0	-143	-5424	15.71	15.71	9.42	9.42	2	0.15	0.02	0.13	0.00	0.00	24.0
9	0	-5300	-1494	-344	0	41	-5463	15.71	15.71	9.42	9.42	2	0.14	0.02	0.13	0.00	0.00	24.0
10	0	-3573	-1824	286	0	-80	-6762	15.71	15.71	9.42	9.42	2	0.18	0.02	0.16	0.00	0.00	24.0
11	0	-3578	-1835	-22	0	-25	-6774	15.71	15.71	9.42	9.42	2	0.18	0.02	0.16	0.00	0.00	24.0

12	0	-6212	-1282	344	0	-77	-4724	15.71	15.71	9.42	9.42	2	0.13	0.02	0.11	0.00	0.00	24.0
13	0	-6217	-1292	35	0	-22	-4736	15.71	15.71	9.42	9.42	2	0.12	0.02	0.11	0.00	0.00	24.0
14	0	-4490	-1623	666	0	-144	-6035	15.71	15.71	9.42	9.42	2	0.16	0.02	0.14	0.00	0.00	24.0
15	0	-4508	-1656	-362	0	40	-6074	15.71	15.71	9.42	9.42	2	0.16	0.02	0.15	0.00	0.00	24.0
16	0	-5282	-1460	683	0	-143	-5424	15.71	15.71	9.42	9.42	2	0.15	0.02	0.13	0.00	0.00	24.0
17	0	-5300	-1494	-344	0	41	-5463	15.71	15.71	9.42	9.42	2	0.14	0.02	0.13	0.00	0.00	24.0
18	0	5399	-4707	439	0	-158	-19310	15.71	15.71	9.42	9.42	3	0.38	0.06	0.44	0.00	0.00	24.0
19	0	-7824	-3448	503	0	-124	-10820	15.71	15.71	9.42	9.42	3	0.20	0.04	0.29	0.00	0.00	24.0
20	0	-1861	-3811	-533	0	44	-14030	15.71	15.71	9.42	9.42	3	0.27	0.05	0.35	0.00	0.00	24.0
37	0	8098	-4457	328	0	-144	-19660	15.71	15.71	9.42	9.42	3	0.40	0.06	0.42	0.00	0.00	24.0
38	0	-13940	-2359	435	0	-88	-5506	15.71	15.71	9.42	9.42	3	0.10	0.03	0.19	0.00	0.00	24.0
39	0	-4002	-2964	-1293	0	193	-10850	15.71	15.71	9.42	9.42	3	0.21	0.04	0.26	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-6233	-2026	209	0	-93	-7726	15.71	15.71	9.42	9.42	3	0.14	0.03	0.18	0.00	0.00	24.0
2	12	-3473	-1824	286	0	-116	-6990	15.71	15.71	9.42	9.42	2	0.19	0.02	0.16	0.00	0.00	24.0
3	12	-3478	-1835	-22	0	-22	-7003	15.71	15.71	9.42	9.42	2	0.19	0.02	0.16	0.00	0.00	24.0
4	12	-6112	-1282	344	0	-120	-4884	15.71	15.71	9.42	9.42	2	0.13	0.02	0.11	0.00	0.00	24.0
5	12	-6117	-1292	35	0	-27	-4898	15.71	15.71	9.42	9.42	2	0.13	0.02	0.11	0.00	0.00	24.0
6	12	-4390	-1623	666	0	-227	-6238	15.71	15.71	9.42	9.42	2	0.17	0.02	0.14	0.00	0.00	24.0
7	12	-4408	-1656	-362	0	85	-6281	15.71	15.71	9.42	9.42	2	0.17	0.02	0.15	0.00	0.00	24.0
8	12	-5182	-1460	683	0	-228	-5606	15.71	15.71	9.42	9.42	2	0.15	0.02	0.13	0.00	0.00	24.0
9	12	-5200	-1494	-344	0	84	-5650	15.71	15.71	9.42	9.42	2	0.15	0.02	0.13	0.00	0.00	24.0
10	12	-3473	-1824	286	0	-116	-6990	15.71	15.71	9.42	9.42	2	0.19	0.02	0.16	0.00	0.00	24.0
11	12	-3478	-1835	-22	0	-22	-7003	15.71	15.71	9.42	9.42	2	0.19	0.02	0.16	0.00	0.00	24.0
12	12	-6112	-1282	344	0	-120	-4884	15.71	15.71	9.42	9.42	2	0.13	0.02	0.11	0.00	0.00	24.0
13	12	-6117	-1292	35	0	-27	-4898	15.71	15.71	9.42	9.42	2	0.13	0.02	0.11	0.00	0.00	24.0
14	12	-4390	-1623	666	0	-227	-6238	15.71	15.71	9.42	9.42	2	0.17	0.02	0.14	0.00	0.00	24.0
15	12	-4408	-1656	-362	0	85	-6281	15.71	15.71	9.42	9.42	2	0.17	0.02	0.15	0.00	0.00	24.0
16	12	-5182	-1460	683	0	-228	-5606	15.71	15.71	9.42	9.42	2	0.15	0.02	0.13	0.00	0.00	24.0
17	12	-5200	-1494	-344	0	84	-5650	15.71	15.71	9.42	9.42	2	0.15	0.02	0.13	0.00	0.00	24.0
18	12	5529	-4707	439	0	-213	-19900	15.71	15.71	9.42	9.42	3	0.40	0.06	0.44	0.00	0.00	24.0
19	12	-7694	-3448	503	0	-187	-11250	15.71	15.71	9.42	9.42	3	0.21	0.04	0.29	0.00	0.00	24.0
20	12	-1731	-3811	-533	0	111	-14505	15.71	15.71	9.42	9.42	3	0.28	0.05	0.35	0.00	0.00	24.0
37	12	8228	-4457	328	0	-186	-20218	15.71	15.71	9.42	9.42	3	0.41	0.06	0.42	0.00	0.00	24.0
38	12	-13810	-2359	435	0	-142	-5801	15.71	15.71	9.42	9.42	3	0.11	0.03	0.19	0.00	0.00	24.0
39	12	-3872	-2964	-1293	0	354	-11223	15.71	15.71	9.42	9.42	3	0.21	0.04	0.26	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-6103	-2026	209	0	-119	-7980	15.71	15.71	9.42	9.42	3	0.15	0.03	0.18	0.00	0.00	24.0
2	25	-3373	-1824	286	0	-152	-7218	15.71	15.71	9.42	9.42	2	0.20	0.02	0.16	0.00	0.00	24.0
3	25	-3378	-1835	-22	0	-20	-7232	15.71	15.71	9.42	9.42	2	0.19	0.02	0.16	0.00	0.00	24.0
4	25	-6012	-1282	344	0	-163	-5044	15.71	15.71	9.42	9.42	2	0.14	0.02	0.11	0.00	0.00	24.0
5	25	-6017	-1292	35	0	-31	-5059	15.71	15.71	9.42	9.42	2	0.13	0.02	0.11	0.00	0.00	24.0
6	25	-4290	-1623	666	0	-310	-6440	15.71	15.71	9.42	9.42	2	0.18	0.02	0.14	0.00	0.00	24.0
7	25	-4308	-1656	-362	0	131	-6488	15.71	15.71	9.42	9.42	2	0.17	0.02	0.15	0.00	0.00	24.0
8	25	-5082	-1460	683	0	-313	-5789	15.71	15.71	9.42	9.42	2	0.16	0.02	0.13	0.00	0.00	24.0
9	25	-5100	-1494	-344	0	127	-5836	15.71	15.71	9.42	9.42	2	0.16	0.02	0.13	0.00	0.00	24.0
10	25	-3373	-1824	286	0	-152	-7218	15.71	15.71	9.42	9.42	2	0.20	0.02	0.16	0.00	0.00	24.0
11	25	-3378	-1835	-22	0	-20	-7232	15.71	15.71	9.42	9.42	2	0.19	0.02	0.16	0.00	0.00	24.0
12	25	-6012	-1282	344	0	-163	-5044	15.71	15.71	9.42	9.42	2	0.14	0.02	0.11	0.00	0.00	24.0
13	25	-6017	-1292	35	0	-31	-5059	15.71	15.71	9.42	9.42	2	0.13	0.02	0.11	0.00	0.00	24.0
14	25	-4290	-1623	666	0	-310	-6440	15.71	15.71	9.42	9.42	2	0.18	0.02	0.14	0.00	0.00	24.0
15	25	-4308	-1656	-362	0	131	-6488	15.71	15.71	9.42	9.42	2	0.17	0.02	0.15	0.00	0.00	24.0
16	25	-5082	-1460	683	0	-313	-5789	15.71	15.71	9.42	9.42	2	0.16	0.02	0.13	0.00	0.00	24.0
17	25	-5100	-1494	-344	0	127	-5836	15.71	15.71	9.42	9.42	2	0.16	0.02	0.13	0.00	0.00	24.0
18	25	5659	-4707	439	0	-268	-20490	15.71	15.71	9.42	9.42	3	0.41	0.06	0.44	0.00	0.00	24.0
19	25	-7564	-3448	503	0	-250	-11680	15.71	15.71	9.42	9.42	3	0.22	0.04	0.29	0.00	0.00	24.0
20	25	-1601	-3811	-533	0	177	-14980	15.71	15.71	9.42	9.42	3	0.29	0.05	0.35	0.00	0.00	24.0
37	25	8358	-4457	328	0	-226	-20775	15.71	15.71	9.42	9.42	3	0.42	0.06	0.42	0.00	0.00	24.0
38	25	-13680	-2359	435	0	-196	-6096	15.71	15.71	9.42	9.42	3	0.11	0.03	0.19	0.00	0.00	24.0
39	25	-3742	-2964	-1293	0	516	-11595	15.71	15.71	9.42	9.42	3	0.22	0.04	0.26	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-5973	-2026	209	0	-145	-8233	15.71	15.71	9.42	9.42	3	0.15	0.03	0.18	0.00	0.00	24.0
2	38	-3273	-1824	286	0	-188	-7446	15.71	15.71	9.42	9.42	2	0.20	0.02	0.16	0.00	0.00	24.0
3	38	-3278	-1835	-22	0	-17	-7462	15.71	15.71	9.42	9.42	2	0.20	0.02	0.16	0.00	0.00	24.0
4	38	-5912	-1282	344	0	-206	-5205	15.71	15.71	9.42	9.42	2	0.14	0.02	0.11	0.00	0.00	24.0
5	38	-5917	-1292	35	0	-35	-5221	15.71	15.71	9.42	9.42	2	0.14	0.02	0.11	0.00	0.00	24.0
6	38	-4190	-1623	666	0	-393	-6643	15.71	15.71	9.42	9.42	2	0.19	0.02	0.14	0.00	0.00	24.0
7	38	-4208	-1656	-362	0	176	-6695	15.71	15.71	9.42	9.42	2	0.18	0.02	0.15	0.00	0.00	24.0
8	38	-4982	-1460	683	0	-399	-5972	15.71	15.71	9.42	9.42	2	0.17	0.02	0.13	0.00	0.00	24.0
9	38	-5000	-1494	-344	0	170	-6023	15.71	15.71	9.42	9.42	2	0.16	0.02	0.13	0.00	0.00	24.0
10	38	-3273	-1824	286	0	-188	-7446	15.71	15.71	9.42	9.42	2	0.20	0.02	0.16	0.00	0.00	24.0
11	38	-3278	-1835	-22	0	-17	-7462	15.71	15.71	9.42	9.42	2	0.20	0.02	0.16	0.00	0.00	24.0
12	38	-5912	-1282	344	0	-206	-5205	15.71	15.71	9.42	9.42	2	0.14	0.02	0.11	0.00	0.00	24.0
13	38	-5917	-1292	35	0	-35	-5221	15.71	15.71	9.42	9.42	2	0.14	0.02	0.11	0.00	0.00	24.0
14	38	-4190	-1623	666	0	-393	-6643	15.71	15.71	9.42	9.42	2	0.19	0.02	0.14	0.00	0.00	24.0
15	38	-4208	-1656	-362	0	176	-6695	15.71	15.71	9.42	9.42	2	0.18	0.02	0.15	0.00	0.00	24.0
16	38	-4982	-1460	683	0	-399	-5972	15.71	15.71	9.42	9.42	2	0.17	0.02	0.13	0.00	0.00	24.0
17	38	-5000	-1494	-344	0	170	-6023	15.71	15.71	9.42	9.42	2	0.16	0.02	0.13	0.00	0.00	24.0
18	38	5789	-4707	439	0	-323	-21080	15.71	15.71	9.42	9.42	3	0.42	0.06	0.44	0.00	0.00	24.0
19	38	-7434	-3448	503	0	-313	-12110	15.71	15.71	9.42	9.42	3	0.23	0.04	0.29	0.00	0.00	24.0
20	38	-1471	-3811	-533	0	244	-15455	15.71	15.71	9.42	9.42	3	0.30	0.05	0.35	0.00	0.00	24.0
37	38	8488	-4457	328	0	-268	-21332	15.71	15.71	9.42	9.42	3	0.43	0.06	0.42	0.00	0.00	24.0
38	38	-13550	-2359	435	0	-251	-6391	15.71	15.71	9.42	9.42	3	0.12	0.03	0.19	0.00	0.00	24.0
39	38	-3612	-2964	-1293	0	677	-11967	15.71	15.71	9.42	9.42	3	0.23	0.04	0.27	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-5843	-2026	209	0	-171	-8486	15.71	15.71	9.42	9.42	3	0.16	0.03	0.18	0.00	0.00	24.0
2	50	-3173	-1824	286	0	-223	-7674	15.71	15.71	9.42	9.42	2	0.21	0.02	0.16	0.00	0.00	24.0
3	50	-3178	-1835	-22	0	-14	-7691	15.71	15.71	9.42	9.42	2	0.21	0.02	0.17	0.00	0.00	24.0
4	50	-5812	-1282	344	0	-249	-5365	15.71	15.71	9.42	9.42	2	0.15	0.02	0.11	0.00	0.00	24.0
5	50	-5817	-1292	35	0	-40	-5382	15.71	15.71	9.42	9.42	2	0.14	0.02	0.11	0.00	0.00	24.0
6	50	-4090	-1623	666	0	-476	-6846	15.71	15.71	9.42	9.42	2	0.19	0.02	0.14	0.00	0.00	24.0
7	50	-4108	-1656	-362	0	221	-6902	15.71	15.71	9.42	9.42	2	0.19	0.02	0.15	0.00	0.00	24.0
8	50	-4882	-1460	683	0	-484	-6154	15.71	15.71	9.42	9.42	2	0.17	0.02	0.13	0.00	0.00	24.0
9	50	-4900	-1494	-344	0	213	-6210	15.71	15.71	9.42	9.42	2	0.17	0.02	0.13	0.00	0.00	24.0
10	50	-3173	-1824	286	0	-223	-7674	15.71	15.71	9.42	9.42	2	0.21	0.02	0.16	0.00	0.00	24.0
11	50	-3178	-1835	-22	0	-14	-7691	15.71	15.71	9.42	9.42	2	0.21	0.02	0.17	0.00	0.00	24.0
12	50	-5812	-1282	344	0	-249	-5365	15.71	15.71	9.42	9.42	2	0.15	0.02	0.11	0.00	0.00	24.0
13	50	-5817	-1292	35	0	-40	-5382	15.71	15.71	9.42	9.42	2	0.14	0.02	0.11	0.00	0.00	24.0
14	50	-4090	-1623	666	0	-476	-6846	15.71	15.71	9.42	9.42	2	0.19	0.02	0.14	0.00	0.00	24.0
15	50	-4108	-1656	-362	0	221	-6902	15.71	15.71	9.42	9.42	2	0.19	0.02	0.15	0.00	0.00	24.0
16	50	-4882	-1460	683	0	-484	-6154	15.71	15.71	9.42	9.42	2	0.17	0.02	0.13	0.00	0.00	24.0
17	50	-4900	-1494	-344	0	213	-6210	15.71	15.71	9.42	9.42	2	0.17	0.02	0.13	0.00	0.00	24.0

18	50	5919	-4707	439	0	-378	-21670	15.71	15.71	9.42	9.42	3	0.43	0.06	0.44	0.00	0.00	24.0
19	50	-7304	-3448	503	0	-376	-12540	15.71	15.71	9.42	9.42	3	0.24	0.04	0.29	0.00	0.00	24.0
20	50	-1341	-3811	-533	0	311	-15930	15.71	15.71	9.42	9.42	3	0.31	0.05	0.35	0.00	0.00	24.0
37	50	8618	-4457	328	0	-308	-21890	15.71	15.71	9.42	9.42	3	0.44	0.06	0.42	0.00	0.00	24.0
38	50	-13420	-2359	435	0	-305	-6686	15.71	15.71	9.42	9.42	3	0.12	0.03	0.19	0.00	0.00	24.0
39	50	-3482	-2964	-1293	0	839	-12340	15.71	15.71	9.42	9.42	3	0.24	0.04	0.27	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 79 NI 1683 NF 134 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 29A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-5666	-2083	542	0	-88	-8034	15.71	15.71	9.42	9.42	3	0.15	0.03	0.18	0.00	0.00	24.0
2	0	-2849	-1891	566	0	-94	-7324	15.71	15.71	9.42	9.42	2	0.20	0.02	0.17	0.00	0.00	24.0
3	0	-2919	-1867	265	0	-40	-7254	15.71	15.71	9.42	9.42	2	0.19	0.02	0.17	0.00	0.00	24.0
4	0	-5799	-1338	569	0	-94	-5105	15.71	15.71	9.42	9.42	2	0.14	0.02	0.12	0.00	0.00	24.0
5	0	-5868	-1314	269	0	-41	-5035	15.71	15.71	9.42	9.42	2	0.13	0.02	0.11	0.00	0.00	24.0
6	0	-3801	-1725	918	0	-157	-6628	15.71	15.71	9.42	9.42	2	0.18	0.02	0.15	0.00	0.00	24.0
7	0	-4032	-1646	-84	0	22	-6397	15.71	15.71	9.42	9.42	2	0.17	0.02	0.15	0.00	0.00	24.0
8	0	-4686	-1559	919	0	-157	-5963	15.71	15.71	9.42	9.42	2	0.16	0.02	0.14	0.00	0.00	24.0
9	0	-4916	-1480	-83	0	22	-5731	15.71	15.71	9.42	9.42	2	0.15	0.02	0.13	0.00	0.00	24.0
10	0	-2849	-1891	566	0	-94	-7324	15.71	15.71	9.42	9.42	2	0.20	0.02	0.17	0.00	0.00	24.0
11	0	-2919	-1867	265	0	-40	-7254	15.71	15.71	9.42	9.42	2	0.19	0.02	0.17	0.00	0.00	24.0
12	0	-5799	-1338	569	0	-94	-5105	15.71	15.71	9.42	9.42	2	0.14	0.02	0.12	0.00	0.00	24.0
13	0	-5868	-1314	269	0	-41	-5035	15.71	15.71	9.42	9.42	2	0.13	0.02	0.11	0.00	0.00	24.0
14	0	-3801	-1725	918	0	-157	-6628	15.71	15.71	9.42	9.42	2	0.18	0.02	0.15	0.00	0.00	24.0
15	0	-4032	-1646	-84	0	22	-6397	15.71	15.71	9.42	9.42	2	0.17	0.02	0.15	0.00	0.00	24.0
16	0	-4686	-1559	919	0	-157	-5963	15.71	15.71	9.42	9.42	2	0.16	0.02	0.14	0.00	0.00	24.0
17	0	-4916	-1480	-83	0	22	-5731	15.71	15.71	9.42	9.42	2	0.15	0.02	0.13	0.00	0.00	24.0
18	0	7305	-4839	1133	0	-186	-20710	15.71	15.71	9.42	9.42	3	0.42	0.06	0.45	0.00	0.00	24.0
19	0	-6958	-3563	976	0	-159	-11610	15.71	15.71	9.42	9.42	3	0.22	0.05	0.31	0.00	0.00	24.0
20	0	-810	-3835	119	0	-5	-14800	15.71	15.71	9.42	9.42	3	0.28	0.05	0.36	0.00	0.00	24.0
37	0	10130	-4573	1014	0	-167	-21100	15.71	15.71	9.42	9.42	3	0.43	0.06	0.43	0.00	0.00	24.0
38	0	-13650	-2447	753	0	-121	-5917	15.71	15.71	9.42	9.42	3	0.11	0.03	0.19	0.00	0.00	24.0
39	0	-3398	-2900	-676	0	135	-11240	15.71	15.71	9.42	9.42	3	0.21	0.04	0.26	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-5536	-2083	542	0	-155	-8294	15.71	15.71	9.42	9.42	3	0.16	0.03	0.18	0.00	0.00	24.0
2	12	-2749	-1891	566	0	-165	-7560	15.71	15.71	9.42	9.42	2	0.21	0.02	0.17	0.00	0.00	24.0
3	12	-2819	-1867	265	0	-74	-7487	15.71	15.71	9.42	9.42	2	0.20	0.02	0.17	0.00	0.00	24.0
4	12	-5699	-1338	569	0	-166	-5272	15.71	15.71	9.42	9.42	2	0.14	0.02	0.12	0.00	0.00	24.0
5	12	-5768	-1314	269	0	-74	-5199	15.71	15.71	9.42	9.42	2	0.14	0.02	0.11	0.00	0.00	24.0
6	12	-3701	-1725	918	0	-272	-6844	15.71	15.71	9.42	9.42	2	0.19	0.02	0.15	0.00	0.00	24.0
7	12	-3932	-1646	-84	0	33	-6603	15.71	15.71	9.42	9.42	2	0.18	0.02	0.15	0.00	0.00	24.0
8	12	-4586	-1559	919	0	-272	-6158	15.71	15.71	9.42	9.42	2	0.17	0.02	0.14	0.00	0.00	24.0
9	12	-4816	-1480	-83	0	33	-5916	15.71	15.71	9.42	9.42	2	0.16	0.02	0.13	0.00	0.00	24.0
10	12	-2749	-1891	566	0	-165	-7560	15.71	15.71	9.42	9.42	2	0.21	0.02	0.17	0.00	0.00	24.0
11	12	-2819	-1867	265	0	-74	-7487	15.71	15.71	9.42	9.42	2	0.20	0.02	0.17	0.00	0.00	24.0
12	12	-5699	-1338	569	0	-166	-5272	15.71	15.71	9.42	9.42	2	0.14	0.02	0.12	0.00	0.00	24.0
13	12	-5768	-1314	269	0	-74	-5199	15.71	15.71	9.42	9.42	2	0.14	0.02	0.11	0.00	0.00	24.0
14	12	-3701	-1725	918	0	-272	-6844	15.71	15.71	9.42	9.42	2	0.19	0.02	0.15	0.00	0.00	24.0
15	12	-3932	-1646	-84	0	33	-6603	15.71	15.71	9.42	9.42	2	0.18	0.02	0.15	0.00	0.00	24.0
16	12	-4586	-1559	919	0	-272	-6158	15.71	15.71	9.42	9.42	2	0.17	0.02	0.14	0.00	0.00	24.0
17	12	-4816	-1480	-83	0	33	-5916	15.71	15.71	9.42	9.42	2	0.16	0.02	0.13	0.00	0.00	24.0
18	12	7435	-4839	1133	0	-328	-21315	15.71	15.71	9.42	9.42	3	0.43	0.06	0.45	0.00	0.00	24.0
19	12	-6828	-3563	976	0	-281	-12055	15.71	15.71	9.42	9.42	3	0.23	0.05	0.31	0.00	0.00	24.0
20	12	-680	-3835	119	0	-20	-15280	15.71	15.71	9.42	9.42	3	0.29	0.05	0.36	0.00	0.00	24.0
37	12	10260	-4573	1014	0	-294	-21670	15.71	15.71	9.42	9.42	3	0.44	0.06	0.43	0.00	0.00	24.0
38	12	-13520	-2447	753	0	-215	-6223	15.71	15.71	9.42	9.42	3	0.11	0.03	0.19	0.00	0.00	24.0
39	12	-3268	-2900	-676	0	220	-11602	15.71	15.71	9.42	9.42	3	0.22	0.04	0.26	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-5406	-2083	542	0	-223	-8554	15.71	15.71	9.42	9.42	3	0.16	0.03	0.18	0.00	0.00	24.0
2	25	-2649	-1891	566	0	-236	-7796	15.71	15.71	9.42	9.42	2	0.21	0.02	0.17	0.00	0.00	24.0
3	25	-2719	-1867	265	0	-107	-7721	15.71	15.71	9.42	9.42	2	0.21	0.02	0.17	0.00	0.00	24.0
4	25	-5599	-1338	569	0	-237	-5440	15.71	15.71	9.42	9.42	2	0.15	0.02	0.12	0.00	0.00	24.0
5	25	-5668	-1314	269	0	-108	-5363	15.71	15.71	9.42	9.42	2	0.14	0.02	0.11	0.00	0.00	24.0
6	25	-3601	-1725	918	0	-386	-7060	15.71	15.71	9.42	9.42	2	0.20	0.02	0.15	0.00	0.00	24.0
7	25	-3832	-1646	-84	0	43	-6808	15.71	15.71	9.42	9.42	2	0.18	0.02	0.15	0.00	0.00	24.0
8	25	-4486	-1559	919	0	-387	-6352	15.71	15.71	9.42	9.42	2	0.18	0.02	0.14	0.00	0.00	24.0
9	25	-4716	-1480	-83	0	43	-6101	15.71	15.71	9.42	9.42	2	0.16	0.02	0.13	0.00	0.00	24.0
10	25	-2649	-1891	566	0	-236	-7796	15.71	15.71	9.42	9.42	2	0.21	0.02	0.17	0.00	0.00	24.0
11	25	-2719	-1867	265	0	-107	-7721	15.71	15.71	9.42	9.42	2	0.21	0.02	0.17	0.00	0.00	24.0
12	25	-5599	-1338	569	0	-237	-5440	15.71	15.71	9.42	9.42	2	0.15	0.02	0.12	0.00	0.00	24.0
13	25	-5668	-1314	269	0	-108	-5363	15.71	15.71	9.42	9.42	2	0.14	0.02	0.11	0.00	0.00	24.0
14	25	-3601	-1725	918	0	-386	-7060	15.71	15.71	9.42	9.42	2	0.20	0.02	0.15	0.00	0.00	24.0
15	25	-3832	-1646	-84	0	43	-6808	15.71	15.71	9.42	9.42	2	0.18	0.02	0.15	0.00	0.00	24.0
16	25	-4486	-1559	919	0	-387	-6352	15.71	15.71	9.42	9.42	2	0.18	0.02	0.14	0.00	0.00	24.0
17	25	-4716	-1480	-83	0	43	-6101	15.71	15.71	9.42	9.42	2	0.16	0.02	0.13	0.00	0.00	24.0
18	25	7565	-4839	1133	0	-470	-21920	15.71	15.71	9.42	9.42	3	0.44	0.06	0.45	0.00	0.00	24.0
19	25	-6698	-3563	976	0	-403	-12500	15.71	15.71	9.42	9.42	3	0.24	0.05	0.31	0.00	0.00	24.0
20	25	-550	-3835	119	0	-35	-15760	15.71	15.71	9.42	9.42	3	0.30	0.05	0.36	0.00	0.00	24.0
37	25	10390	-4573	1014	0	-421	-22240	15.71	15.71	9.42	9.42	3	0.46	0.06	0.43	0.00	0.00	24.0
38	25	-13390	-2447	753	0	-309	-6529	15.71	15.71	9.42	9.42	3	0.12	0.03	0.19	0.00	0.00	24.0
39	25	-3138	-2900	-676	0	304	-11965	15.71	15.71	9.42	9.42	3	0.23	0.04	0.26	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-5276	-2083	542	0	-291	-8815	15.71	15.71	9.42	9.42	3	0.17	0.03	0.18	0.00	0.00	24.0
2	38	-2549	-1891	566	0	-306	-8033	15.71	15.71	9.42	9.42	2	0.22	0.02	0.17	0.00	0.00	24.0
3	38	-2619	-1867	265	0	-140	-7954	15.71	15.71	9.42	9.42	2	0.22	0.02	0.17	0.00	0.00	24.0
4	38	-5499	-1338	569	0	-308	-5607	15.71	15.71	9.42	9.42	2	0.15	0.02	0.12	0.00	0.00	24.0
5	38	-5568	-1314	269	0	-141	-5528	15.71	15.71	9.42	9.42	2	0.15	0.02	0.11	0.00	0.00	24.0
6	38	-3501	-1725	918	0	-501	-7275	15.71	15.71	9.42	9.42	2	0.21	0.02	0.15	0.00	0.00	24.0
7	38	-3732	-1646	-84	0	54	-7014	15.71	15.71	9.42	9.42	2	0.19	0.02	0.15	0.00	0.00	24.0
8	38	-4386	-1559	919	0	-502	-6547	15.71	15.71	9.42	9.42	2	0.19	0.02	0.14	0.00	0.00	24.0
9	38	-4616	-1480	-83	0	53	-6286	15.71	15.71	9.42	9.42	2	0.17	0.02	0.13	0.00	0.00	24.0
10	38	-2549	-1891	566	0	-306	-8033	15.71	15.71	9.42	9.42	2	0.22	0.02	0.17	0.00	0.00	24.0
11	38	-2619	-1867	265	0	-140	-7954	15.71	15.71	9.42	9.42	2	0.22	0.02	0.17	0.00	0.00	24.0
12	38	-5499	-1338	569	0	-308	-5607	15.71	15.71	9.42	9.42	2	0.15	0.02	0.12	0.00	0.00	24.0
13	38	-5568	-1314	269	0	-141	-5528	15.71	15.71	9.42	9.42	2	0.15	0.02	0.11	0.00	0.00	24.0

14	38	-3501	-1725	918	0	-501	-7275	15.71	15.71	9.42	9.42	2	0.21	0.02	0.15	0.00	0.00	24.0
15	38	-3732	-1646	-84	0	54	-7014	15.71	15.71	9.42	9.42	2	0.19	0.02	0.15	0.00	0.00	24.0
16	38	-4386	-1559	919	0	-502	-6547	15.71	15.71	9.42	9.42	2	0.19	0.02	0.14	0.00	0.00	24.0
17	38	-4616	-1480	-83	0	53	-6286	15.71	15.71	9.42	9.42	2	0.17	0.02	0.13	0.00	0.00	24.0
18	38	7695	-4839	1133	0	-611	-22525	15.71	15.71	9.42	9.42	3	0.46	0.06	0.45	0.00	0.00	24.0
19	38	-6568	-3563	976	0	-525	-12945	15.71	15.71	9.42	9.42	3	0.24	0.05	0.31	0.00	0.00	24.0
20	38	-420	-3835	119	0	-50	-16240	15.71	15.71	9.42	9.42	3	0.31	0.05	0.36	0.00	0.00	24.0
37	38	10520	-4573	1014	0	-547	-22810	15.71	15.71	9.42	9.42	3	0.47	0.06	0.43	0.00	0.00	24.0
38	38	-13260	-2447	753	0	-403	-6834	15.71	15.71	9.42	9.42	3	0.13	0.03	0.20	0.00	0.00	24.0
39	38	-3008	-2900	-676	0	389	-12327	15.71	15.71	9.42	9.42	3	0.24	0.04	0.26	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-5146	-2083	542	0	-359	-9075	15.71	15.71	9.42	9.42	3	0.17	0.03	0.18	0.00	0.00	24.0
2	50	-2449	-1891	566	0	-377	-8269	15.71	15.71	9.42	9.42	2	0.23	0.02	0.17	0.00	0.00	24.0
3	50	-2519	-1867	265	0	-173	-8188	15.71	15.71	9.42	9.42	2	0.22	0.02	0.17	0.00	0.00	24.0
4	50	-5399	-1338	569	0	-379	-5774	15.71	15.71	9.42	9.42	2	0.16	0.02	0.12	0.00	0.00	24.0
5	50	-5468	-1314	269	0	-175	-5692	15.71	15.71	9.42	9.42	2	0.15	0.02	0.11	0.00	0.00	24.0
6	50	-3401	-1725	918	0	-616	-7491	15.71	15.71	9.42	9.42	2	0.22	0.02	0.15	0.00	0.00	24.0
7	50	-3632	-1646	-84	0	64	-7220	15.71	15.71	9.42	9.42	2	0.19	0.02	0.15	0.00	0.00	24.0
8	50	-4286	-1559	919	0	-616	-6742	15.71	15.71	9.42	9.42	2	0.19	0.02	0.14	0.00	0.00	24.0
9	50	-4516	-1480	-83	0	64	-6471	15.71	15.71	9.42	9.42	2	0.17	0.02	0.13	0.00	0.00	24.0
10	50	-2449	-1891	566	0	-377	-8269	15.71	15.71	9.42	9.42	2	0.23	0.02	0.17	0.00	0.00	24.0
11	50	-2519	-1867	265	0	-173	-8188	15.71	15.71	9.42	9.42	2	0.22	0.02	0.17	0.00	0.00	24.0
12	50	-5399	-1338	569	0	-379	-5774	15.71	15.71	9.42	9.42	2	0.16	0.02	0.12	0.00	0.00	24.0
13	50	-5468	-1314	269	0	-175	-5692	15.71	15.71	9.42	9.42	2	0.15	0.02	0.11	0.00	0.00	24.0
14	50	-3401	-1725	918	0	-616	-7491	15.71	15.71	9.42	9.42	2	0.22	0.02	0.15	0.00	0.00	24.0
15	50	-3632	-1646	-84	0	64	-7220	15.71	15.71	9.42	9.42	2	0.19	0.02	0.15	0.00	0.00	24.0
16	50	-4286	-1559	919	0	-616	-6742	15.71	15.71	9.42	9.42	2	0.19	0.02	0.14	0.00	0.00	24.0
17	50	-4516	-1480	-83	0	64	-6471	15.71	15.71	9.42	9.42	2	0.17	0.02	0.13	0.00	0.00	24.0
18	50	7825	-4839	1133	0	-753	-23130	15.71	15.71	9.42	9.42	3	0.47	0.06	0.45	0.00	0.00	24.0
19	50	-6438	-3563	976	0	-647	-13390	15.71	15.71	9.42	9.42	3	0.25	0.05	0.31	0.00	0.00	24.0
20	50	-290	-3835	119	0	-64	-16720	15.71	15.71	9.42	9.42	3	0.32	0.05	0.36	0.00	0.00	24.0
37	50	10650	-4573	1014	0	-674	-23380	15.71	15.71	9.42	9.42	3	0.48	0.06	0.43	0.00	0.00	24.0
38	50	-13130	-2447	753	0	-497	-7140	15.71	15.71	9.42	9.42	3	0.13	0.03	0.20	0.00	0.00	24.0
39	50	-2878	-2900	-676	0	473	-12690	15.71	15.71	9.42	9.42	3	0.24	0.04	0.26	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 80 NI 1691 NF 177 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 28A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-6576	-2007	723	0	-96	-7326	15.71	15.71	9.42	9.42	3	0.14	0.03	0.17	0.00	0.00	24.0
2	0	-3573	-1854	711	0	-100	-6781	15.71	15.71	9.42	9.42	2	0.18	0.02	0.17	0.00	0.00	24.0
3	0	-3577	-1856	416	0	-50	-6781	15.71	15.71	9.42	9.42	2	0.18	0.02	0.17	0.00	0.00	24.0
4	0	-6539	-1232	696	0	-97	-4490	15.71	15.71	9.42	9.42	2	0.12	0.02	0.11	0.00	0.00	24.0
5	0	-6544	-1234	401	0	-47	-4489	15.71	15.71	9.42	9.42	2	0.12	0.02	0.11	0.00	0.00	24.0
6	0	-4606	-1634	1050	0	-157	-5980	15.71	15.71	9.42	9.42	2	0.16	0.02	0.14	0.00	0.00	24.0
7	0	-4620	-1640	67	0	9	-5978	15.71	15.71	9.42	9.42	2	0.16	0.02	0.14	0.00	0.00	24.0
8	0	-5496	-1447	1045	0	-156	-5292	15.71	15.71	9.42	9.42	2	0.14	0.02	0.13	0.00	0.00	24.0
9	0	-5510	-1454	62	0	10	-5290	15.71	15.71	9.42	9.42	2	0.14	0.02	0.13	0.00	0.00	24.0
10	0	-3573	-1854	711	0	-100	-6781	15.71	15.71	9.42	9.42	2	0.18	0.02	0.17	0.00	0.00	24.0
11	0	-3577	-1856	416	0	-50	-6781	15.71	15.71	9.42	9.42	2	0.18	0.02	0.17	0.00	0.00	24.0
12	0	-6539	-1232	696	0	-97	-4490	15.71	15.71	9.42	9.42	2	0.12	0.02	0.11	0.00	0.00	24.0
13	0	-6544	-1234	401	0	-47	-4489	15.71	15.71	9.42	9.42	2	0.12	0.02	0.11	0.00	0.00	24.0
14	0	-4606	-1634	1050	0	-157	-5980	15.71	15.71	9.42	9.42	2	0.16	0.02	0.14	0.00	0.00	24.0
15	0	-4620	-1640	67	0	9	-5978	15.71	15.71	9.42	9.42	2	0.16	0.02	0.14	0.00	0.00	24.0
16	0	-5496	-1447	1045	0	-156	-5292	15.71	15.71	9.42	9.42	2	0.14	0.02	0.13	0.00	0.00	24.0
17	0	-5510	-1454	62	0	10	-5290	15.71	15.71	9.42	9.42	2	0.14	0.02	0.13	0.00	0.00	24.0
18	0	5727	-4880	1572	0	-222	-19540	15.71	15.71	9.42	9.42	3	0.39	0.06	0.46	0.00	0.00	24.0
19	0	-8526	-3338	1314	0	-180	-10270	15.71	15.71	9.42	9.42	3	0.19	0.04	0.28	0.00	0.00	24.0
20	0	-2143	-3803	540	0	-49	-13790	15.71	15.71	9.42	9.42	3	0.26	0.05	0.35	0.00	0.00	24.0
37	0	8763	-4708	1420	0	-201	-20160	15.71	15.71	9.42	9.42	3	0.41	0.06	0.44	0.00	0.00	24.0
38	0	-14990	-2137	990	0	-131	-4697	15.71	15.71	9.42	9.42	3	0.09	0.03	0.17	0.00	0.00	24.0
39	0	-4355	-2913	-300	0	87	-10560	15.71	15.71	9.42	9.42	3	0.20	0.04	0.26	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-6446	-2007	723	0	-186	-7577	15.71	15.71	9.42	9.42	3	0.14	0.03	0.17	0.00	0.00	24.0
2	12	-3473	-1854	711	0	-189	-7013	15.71	15.71	9.42	9.42	2	0.19	0.02	0.17	0.00	0.00	24.0
3	12	-3477	-1856	416	0	-102	-7013	15.71	15.71	9.42	9.42	2	0.19	0.02	0.17	0.00	0.00	24.0
4	12	-6439	-1232	696	0	-184	-4644	15.71	15.71	9.42	9.42	2	0.13	0.02	0.11	0.00	0.00	24.0
5	12	-6444	-1234	401	0	-98	-4643	15.71	15.71	9.42	9.42	2	0.12	0.02	0.11	0.00	0.00	24.0
6	12	-4506	-1634	1050	0	-288	-6184	15.71	15.71	9.42	9.42	2	0.17	0.02	0.14	0.00	0.00	24.0
7	12	-4520	-1640	67	0	1	-6183	15.71	15.71	9.42	9.42	2	0.16	0.02	0.15	0.00	0.00	24.0
8	12	-5396	-1447	1045	0	-287	-5473	15.71	15.71	9.42	9.42	2	0.15	0.02	0.13	0.00	0.00	24.0
9	12	-5410	-1454	62	0	2	-5472	15.71	15.71	9.42	9.42	2	0.14	0.02	0.13	0.00	0.00	24.0
10	12	-3473	-1854	711	0	-189	-7013	15.71	15.71	9.42	9.42	2	0.19	0.02	0.17	0.00	0.00	24.0
11	12	-3477	-1856	416	0	-102	-7013	15.71	15.71	9.42	9.42	2	0.19	0.02	0.17	0.00	0.00	24.0
12	12	-6439	-1232	696	0	-184	-4644	15.71	15.71	9.42	9.42	2	0.13	0.02	0.11	0.00	0.00	24.0
13	12	-6444	-1234	401	0	-98	-4643	15.71	15.71	9.42	9.42	2	0.12	0.02	0.11	0.00	0.00	24.0
14	12	-4506	-1634	1050	0	-288	-6184	15.71	15.71	9.42	9.42	2	0.17	0.02	0.14	0.00	0.00	24.0
15	12	-4520	-1640	67	0	1	-6183	15.71	15.71	9.42	9.42	2	0.16	0.02	0.15	0.00	0.00	24.0
16	12	-5396	-1447	1045	0	-287	-5473	15.71	15.71	9.42	9.42	2	0.15	0.02	0.13	0.00	0.00	24.0
17	12	-5410	-1454	62	0	2	-5472	15.71	15.71	9.42	9.42	2	0.14	0.02	0.13	0.00	0.00	24.0
18	12	5857	-4880	1572	0	-419	-20150	15.71	15.71	9.42	9.42	3	0.40	0.06	0.46	0.00	0.00	24.0
19	12	-8396	-3338	1314	0	-344	-10685	15.71	15.71	9.42	9.42	3	0.20	0.04	0.28	0.00	0.00	24.0
20	12	-2013	-3803	540	0	-117	-14265	15.71	15.71	9.42	9.42	3	0.27	0.05	0.35	0.00	0.00	24.0
37	12	8893	-4708	1420	0	-379	-20750	15.71	15.71	9.42	9.42	3	0.42	0.06	0.44	0.00	0.00	24.0
38	12	-14860	-2137	990	0	-254	-4964	15.71	15.71	9.42	9.42	3	0.09	0.03	0.17	0.00	0.00	24.0
39	12	-4225	-2913	-300	0	124	-10925	15.71	15.71	9.42	9.42	3	0.21	0.04	0.26	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-6316	-2007	723	0	-276	-7828	15.71	15.71	9.42	9.42	3	0.15	0.03	0.17	0.00	0.00	24.0
2	25	-3373	-1854	711	0	-278	-7244	15.71	15.71	9.42	9.42	2	0.20	0.02	0.17	0.00	0.00	24.0
3	25	-3377	-1856	416	0	-154	-7244	15.71	15.71	9.42	9.42	2	0.20	0.02	0.17	0.00	0.00	24.0
4	25	-6339	-1232	696	0	-271	-4798	15.71	15.71	9.42	9.42	2	0.13	0.02	0.11	0.00	0.00	24.0
5	25	-6344	-1234	401	0	-148	-4798	15.71	15.71	9.42	9.42	2	0.13	0.02	0.11	0.00	0.00	24.0
6	25	-4406	-1634	1050	0	-420	-6388	15.71	15.71	9.42	9.42	2	0.18	0.02	0.14	0.00	0.00	24.0
7	25	-4420	-1640	67	0	-7	-6388	15.71	15.71	9.42	9.42	2	0.17	0.02	0.15	0.00	0.00	24.0
8	25	-5296	-1447	1045	0	-418	-5654	15.71	15.71	9.42	9.42	2	0.16	0.02	0.13	0.00	0.00	24.0
9	25	-5310	-1454	62	0	-5	-5654	15.71	15.71	9.42	9.42	2	0.15	0.02	0.13	0.00	0.00	24.0

10	25	-3373	-1854	711	0	-278	-7244	15.71	15.71	9.42	9.42	2	0.20	0.02	0.17	0.00	0.00	24.0
11	25	-3377	-1856	416	0	-154	-7244	15.71	15.71	9.42	9.42	2	0.20	0.02	0.17	0.00	0.00	24.0
12	25	-6339	-1232	696	0	-271	-4798	15.71	15.71	9.42	9.42	2	0.13	0.02	0.11	0.00	0.00	24.0
13	25	-6344	-1234	401	0	-148	-4798	15.71	15.71	9.42	9.42	2	0.13	0.02	0.11	0.00	0.00	24.0
14	25	-4406	-1634	1050	0	-420	-6388	15.71	15.71	9.42	9.42	2	0.18	0.02	0.14	0.00	0.00	24.0
15	25	-4420	-1640	67	0	-7	-6388	15.71	15.71	9.42	9.42	2	0.17	0.02	0.15	0.00	0.00	24.0
16	25	-5296	-1447	1045	0	-418	-5654	15.71	15.71	9.42	9.42	2	0.16	0.02	0.13	0.00	0.00	24.0
17	25	-5310	-1454	62	0	-5	-5654	15.71	15.71	9.42	9.42	2	0.15	0.02	0.13	0.00	0.00	24.0
18	25	5987	-4880	1572	0	-615	-20760	15.71	15.71	9.42	9.42	3	0.42	0.06	0.46	0.00	0.00	24.0
19	25	-8266	-3338	1314	0	-508	-11100	15.71	15.71	9.42	9.42	3	0.21	0.04	0.28	0.00	0.00	24.0
20	25	-1883	-3803	540	0	-184	-14740	15.71	15.71	9.42	9.42	3	0.28	0.05	0.35	0.00	0.00	24.0
37	25	9023	-4708	1420	0	-556	-21340	15.71	15.71	9.42	9.42	3	0.44	0.06	0.44	0.00	0.00	24.0
38	25	-14730	-2137	990	0	-378	-5231	15.71	15.71	9.42	9.42	3	0.10	0.03	0.17	0.00	0.00	24.0
39	25	-4095	-2913	-300	0	162	-11290	15.71	15.71	9.42	9.42	3	0.21	0.04	0.26	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-6186	-2007	723	0	-367	-8078	15.71	15.71	9.42	9.42	3	0.15	0.03	0.17	0.00	0.00	24.0
2	38	-3273	-1854	711	0	-366	-7476	15.71	15.71	9.42	9.42	2	0.21	0.02	0.17	0.00	0.00	24.0
3	38	-3277	-1856	416	0	-206	-7476	15.71	15.71	9.42	9.42	2	0.20	0.02	0.17	0.00	0.00	24.0
4	38	-6239	-1232	696	0	-358	-4951	15.71	15.71	9.42	9.42	2	0.14	0.02	0.11	0.00	0.00	24.0
5	38	-6244	-1234	401	0	-198	-4952	15.71	15.71	9.42	9.42	2	0.13	0.02	0.11	0.00	0.00	24.0
6	38	-4306	-1634	1050	0	-551	-6593	15.71	15.71	9.42	9.42	2	0.19	0.02	0.14	0.00	0.00	24.0
7	38	-4320	-1640	67	0	-16	-6593	15.71	15.71	9.42	9.42	2	0.17	0.02	0.15	0.00	0.00	24.0
8	38	-5196	-1447	1045	0	-549	-5835	15.71	15.71	9.42	9.42	2	0.17	0.02	0.13	0.00	0.00	24.0
9	38	-5210	-1454	62	0	-13	-5835	15.71	15.71	9.42	9.42	2	0.15	0.02	0.13	0.00	0.00	24.0
10	38	-3273	-1854	711	0	-366	-7476	15.71	15.71	9.42	9.42	2	0.21	0.02	0.17	0.00	0.00	24.0
11	38	-3277	-1856	416	0	-206	-7476	15.71	15.71	9.42	9.42	2	0.20	0.02	0.17	0.00	0.00	24.0
12	38	-6239	-1232	696	0	-358	-4951	15.71	15.71	9.42	9.42	2	0.14	0.02	0.11	0.00	0.00	24.0
13	38	-6244	-1234	401	0	-198	-4952	15.71	15.71	9.42	9.42	2	0.13	0.02	0.11	0.00	0.00	24.0
14	38	-4306	-1634	1050	0	-551	-6593	15.71	15.71	9.42	9.42	2	0.19	0.02	0.14	0.00	0.00	24.0
15	38	-4320	-1640	67	0	-16	-6593	15.71	15.71	9.42	9.42	2	0.17	0.02	0.15	0.00	0.00	24.0
16	38	-5196	-1447	1045	0	-549	-5835	15.71	15.71	9.42	9.42	2	0.17	0.02	0.13	0.00	0.00	24.0
17	38	-5210	-1454	62	0	-13	-5835	15.71	15.71	9.42	9.42	2	0.15	0.02	0.13	0.00	0.00	24.0
18	38	6117	-4880	1572	0	-812	-21370	15.71	15.71	9.42	9.42	3	0.43	0.06	0.46	0.00	0.00	24.0
19	38	-8136	-3338	1314	0	-672	-11515	15.71	15.71	9.42	9.42	3	0.22	0.04	0.28	0.00	0.00	24.0
20	38	-1753	-3803	540	0	-252	-15215	15.71	15.71	9.42	9.42	3	0.29	0.05	0.35	0.00	0.00	24.0
37	38	9153	-4708	1420	0	-734	-21930	15.71	15.71	9.42	9.42	3	0.45	0.06	0.44	0.00	0.00	24.0
38	38	-14600	-2137	990	0	-502	-5499	15.71	15.71	9.42	9.42	3	0.10	0.03	0.17	0.00	0.00	24.0
39	38	-3965	-2913	-300	0	199	-11655	15.71	15.71	9.42	9.42	3	0.22	0.04	0.26	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-6056	-2007	723	0	-457	-8329	15.71	15.71	9.42	9.42	3	0.16	0.03	0.17	0.00	0.00	24.0
2	50	-3173	-1854	711	0	-455	-7708	15.71	15.71	9.42	9.42	2	0.22	0.02	0.17	0.00	0.00	24.0
3	50	-3177	-1856	416	0	-258	-7708	15.71	15.71	9.42	9.42	2	0.21	0.02	0.17	0.00	0.00	24.0
4	50	-6139	-1232	696	0	-445	-5105	15.71	15.71	9.42	9.42	2	0.14	0.02	0.11	0.00	0.00	24.0
5	50	-6144	-1234	401	0	-248	-5106	15.71	15.71	9.42	9.42	2	0.14	0.02	0.11	0.00	0.00	24.0
6	50	-4206	-1634	1050	0	-682	-6797	15.71	15.71	9.42	9.42	2	0.20	0.02	0.15	0.00	0.00	24.0
7	50	-4220	-1640	67	0	-24	-6798	15.71	15.71	9.42	9.42	2	0.18	0.02	0.15	0.00	0.00	24.0
8	50	-5096	-1447	1045	0	-679	-6016	15.71	15.71	9.42	9.42	2	0.18	0.02	0.13	0.00	0.00	24.0
9	50	-5110	-1454	62	0	-21	-6017	15.71	15.71	9.42	9.42	2	0.16	0.02	0.13	0.00	0.00	24.0
10	50	-3173	-1854	711	0	-455	-7708	15.71	15.71	9.42	9.42	2	0.22	0.02	0.17	0.00	0.00	24.0
11	50	-3177	-1856	416	0	-258	-7708	15.71	15.71	9.42	9.42	2	0.21	0.02	0.17	0.00	0.00	24.0
12	50	-6139	-1232	696	0	-445	-5105	15.71	15.71	9.42	9.42	2	0.14	0.02	0.11	0.00	0.00	24.0
13	50	-6144	-1234	401	0	-248	-5106	15.71	15.71	9.42	9.42	2	0.14	0.02	0.11	0.00	0.00	24.0
14	50	-4206	-1634	1050	0	-682	-6797	15.71	15.71	9.42	9.42	2	0.20	0.02	0.15	0.00	0.00	24.0
15	50	-4220	-1640	67	0	-24	-6798	15.71	15.71	9.42	9.42	2	0.18	0.02	0.15	0.00	0.00	24.0
16	50	-5096	-1447	1045	0	-679	-6016	15.71	15.71	9.42	9.42	2	0.18	0.02	0.13	0.00	0.00	24.0
17	50	-5110	-1454	62	0	-21	-6017	15.71	15.71	9.42	9.42	2	0.16	0.02	0.13	0.00	0.00	24.0
18	50	6247	-4880	1572	0	-1008	-21980	15.71	15.71	9.42	9.42	3	0.45	0.06	0.46	0.00	0.00	24.0
19	50	-8006	-3338	1314	0	-837	-11930	15.71	15.71	9.42	9.42	3	0.23	0.04	0.28	0.00	0.00	24.0
20	50	-1623	-3803	540	0	-319	-15690	15.71	15.71	9.42	9.42	3	0.30	0.05	0.35	0.00	0.00	24.0
37	50	9283	-4708	1420	0	-911	-22520	15.71	15.71	9.42	9.42	3	0.46	0.06	0.44	0.00	0.00	24.0
38	50	-14470	-2137	990	0	-626	-5766	15.71	15.71	9.42	9.42	3	0.11	0.03	0.17	0.00	0.00	24.0
39	50	-3835	-2913	-300	0	237	-12020	15.71	15.71	9.42	9.42	3	0.23	0.04	0.26	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 81 NI 1699 NF 220 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 27A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-10750	-1268	1076	0	-64	-2758	15.71	15.71	9.42	9.42	3	0.05	0.02	0.10	0.00	0.00	24.0
2	0	-7145	-1288	953	0	-65	-2945	15.71	15.71	9.42	9.42	2	0.08	0.02	0.11	0.00	0.00	24.0
3	0	-7149	-1320	674	0	-15	-3009	15.71	15.71	9.42	9.42	2	0.08	0.02	0.11	0.00	0.00	24.0
4	0	-9387	-631	982	0	-84	-1235	15.71	15.71	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
5	0	-9392	-664	703	0	-33	-1298	15.71	15.71	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
6	0	-7924	-1020	1289	0	-130	-2273	15.71	15.71	9.42	9.42	2	0.06	0.02	0.09	0.00	0.00	24.0
7	0	-7940	-1129	358	0	38	-2484	15.71	15.71	9.42	9.42	2	0.06	0.01	0.10	0.00	0.00	24.0
8	0	-8597	-822	1298	0	-136	-1759	15.71	15.71	9.42	9.42	2	0.05	0.02	0.09	0.00	0.00	24.0
9	0	-8612	-932	367	0	32	-1971	15.71	15.71	9.42	9.42	2	0.05	0.01	0.08	0.00	0.00	24.0
10	0	-7145	-1288	953	0	-65	-2945	15.71	15.71	9.42	9.42	2	0.08	0.02	0.11	0.00	0.00	24.0
11	0	-7149	-1320	674	0	-15	-3009	15.71	15.71	9.42	9.42	2	0.08	0.02	0.11	0.00	0.00	24.0
12	0	-9387	-631	982	0	-84	-1235	15.71	15.71	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
13	0	-9392	-664	703	0	-33	-1298	15.71	15.71	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
14	0	-7924	-1020	1289	0	-130	-2273	15.71	15.71	9.42	9.42	2	0.06	0.02	0.09	0.00	0.00	24.0
15	0	-7940	-1129	358	0	38	-2484	15.71	15.71	9.42	9.42	2	0.06	0.01	0.10	0.00	0.00	24.0
16	0	-8597	-822	1298	0	-136	-1759	15.71	15.71	9.42	9.42	2	0.05	0.02	0.09	0.00	0.00	24.0
17	0	-8612	-932	367	0	32	-1971	15.71	15.71	9.42	9.42	2	0.05	0.01	0.08	0.00	0.00	24.0
18	0	-4030	-3679	1945	0	-68	-9865	15.71	15.71	9.42	9.42	3	0.19	0.05	0.33	0.00	0.00	24.0
19	0	-15240	-1909	1887	0	-116	-3023	15.71	15.71	9.42	9.42	3	0.06	0.03	0.15	0.00	0.00	24.0
20	0	-9810	-2657	1054	0	47	-6064	15.71	15.71	9.42	9.42	3	0.11	0.03	0.22	0.00	0.00	24.0
37	0	-683	-3769	1694	0	-44	-10940	15.71	15.71	9.42	9.42	3	0.21	0.05	0.35	0.00	0.00	24.0
38	0	-19370	-819	1596	0	-122	463	15.71	15.71	9.42	9.42	3	0.01	0.02	0.10	0.00	0.00	24.0
39	0	-10320	-2066	207	0	148	-4606	15.71	15.71	9.42	9.42	3	0.09	0.03	0.17	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-10620	-1268	1076	0	-198	-2916	15.71	15.71	9.42	9.42	3	0.05	0.02	0.10	0.00	0.00	24.0
2	12	-7045	-1288	953	0	-184	-3106	15.71	15.71	9.42	9.42	2	0.09	0.02	0.11	0.00	0.00	24.0
3	12	-7049	-1320	674	0	-99	-3174	15.71	15.71	9.42	9.42	2	0.08	0.02	0.11	0.00	0.00	24.0
4	12	-9287	-631	982	0	-206	-1314	15.71	15.71	9.42	9.42	2	0.04	0.01	0.06	0.00	0.00	24.0
5	12	-9292	-664	703	0	-121	-1381	15.71	15.71	9.42	9.42	2	0.04	0.01	0.06	0.00	0.00	24.0

6	12	-7824	-1020	1289	0	-291	-2400	15.71	15.71	9.42	9.42	2	0.07	0.02	0.09	0.00	0.00	24.0
7	12	-7840	-1129	358	0	-7	-2625	15.71	15.71	9.42	9.42	2	0.07	0.01	0.10	0.00	0.00	24.0
8	12	-8497	-822	1298	0	-298	-1862	15.71	15.71	9.42	9.42	2	0.06	0.02	0.09	0.00	0.00	24.0
9	12	-8512	-932	367	0	-14	-2088	15.71	15.71	9.42	9.42	2	0.05	0.01	0.08	0.00	0.00	24.0
10	12	-7045	-1288	953	0	-184	-3106	15.71	15.71	9.42	9.42	2	0.09	0.02	0.11	0.00	0.00	24.0
11	12	-7049	-1320	674	0	-99	-3174	15.71	15.71	9.42	9.42	2	0.08	0.02	0.11	0.00	0.00	24.0
12	12	-9287	-631	982	0	-206	-1314	15.71	15.71	9.42	9.42	2	0.04	0.01	0.06	0.00	0.00	24.0
13	12	-9292	-664	703	0	-121	-1381	15.71	15.71	9.42	9.42	2	0.04	0.01	0.06	0.00	0.00	24.0
14	12	-7824	-1020	1289	0	-291	-2400	15.71	15.71	9.42	9.42	2	0.07	0.02	0.09	0.00	0.00	24.0
15	12	-7840	-1129	358	0	-7	-2625	15.71	15.71	9.42	9.42	2	0.07	0.01	0.10	0.00	0.00	24.0
16	12	-8497	-822	1298	0	-298	-1862	15.71	15.71	9.42	9.42	2	0.06	0.02	0.09	0.00	0.00	24.0
17	12	-8512	-932	367	0	-14	-2088	15.71	15.71	9.42	9.42	2	0.05	0.01	0.08	0.00	0.00	24.0
18	12	-3900	-3679	1945	0	-311	-10324	15.71	15.71	9.42	9.42	3	0.20	0.05	0.33	0.00	0.00	24.0
19	12	-15110	-1909	1887	0	-351	-3262	15.71	15.71	9.42	9.42	3	0.06	0.03	0.15	0.00	0.00	24.0
20	12	-9680	-2657	1054	0	-85	-6396	15.71	15.71	9.42	9.42	3	0.12	0.03	0.22	0.00	0.00	24.0
37	12	-553	-3769	1694	0	-255	-11410	15.71	15.71	9.42	9.42	3	0.22	0.05	0.35	0.00	0.00	24.0
38	12	-19240	-819	1596	0	-322	361	15.71	15.71	9.42	9.42	3	0.01	0.02	0.10	0.00	0.00	24.0
39	12	-10189	-2066	207	0	122	-4864	15.71	15.71	9.42	9.42	3	0.09	0.03	0.17	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-10490	-1268	1076	0	-333	-3075	15.71	15.71	9.42	9.42	3	0.06	0.02	0.10	0.00	0.00	24.0
2	25	-6945	-1288	953	0	-303	-3267	15.71	15.71	9.42	9.42	2	0.09	0.02	0.11	0.00	0.00	24.0
3	25	-6949	-1320	674	0	-183	-3339	15.71	15.71	9.42	9.42	2	0.09	0.02	0.11	0.00	0.00	24.0
4	25	-9187	-631	982	0	-329	-1393	15.71	15.71	9.42	9.42	2	0.04	0.01	0.06	0.00	0.00	24.0
5	25	-9192	-664	703	0	-209	-1464	15.71	15.71	9.42	9.42	2	0.04	0.01	0.06	0.00	0.00	24.0
6	25	-7724	-1020	1289	0	-452	-2528	15.71	15.71	9.42	9.42	2	0.08	0.02	0.09	0.00	0.00	24.0
7	25	-7740	-1129	358	0	-52	-2766	15.71	15.71	9.42	9.42	2	0.07	0.01	0.10	0.00	0.00	24.0
8	25	-8397	-822	1298	0	-460	-1965	15.71	15.71	9.42	9.42	2	0.06	0.02	0.09	0.00	0.00	24.0
9	25	-8412	-932	367	0	-60	-2204	15.71	15.71	9.42	9.42	2	0.06	0.01	0.08	0.00	0.00	24.0
10	25	-6945	-1288	953	0	-303	-3267	15.71	15.71	9.42	9.42	2	0.09	0.02	0.11	0.00	0.00	24.0
11	25	-6949	-1320	674	0	-183	-3339	15.71	15.71	9.42	9.42	2	0.09	0.02	0.11	0.00	0.00	24.0
12	25	-9187	-631	982	0	-329	-1393	15.71	15.71	9.42	9.42	2	0.04	0.01	0.06	0.00	0.00	24.0
13	25	-9192	-664	703	0	-209	-1464	15.71	15.71	9.42	9.42	2	0.04	0.01	0.06	0.00	0.00	24.0
14	25	-7724	-1020	1289	0	-452	-2528	15.71	15.71	9.42	9.42	2	0.08	0.02	0.09	0.00	0.00	24.0
15	25	-7740	-1129	358	0	-52	-2766	15.71	15.71	9.42	9.42	2	0.07	0.01	0.10	0.00	0.00	24.0
16	25	-8397	-822	1298	0	-460	-1965	15.71	15.71	9.42	9.42	2	0.06	0.02	0.09	0.00	0.00	24.0
17	25	-8412	-932	367	0	-60	-2204	15.71	15.71	9.42	9.42	2	0.06	0.01	0.08	0.00	0.00	24.0
18	25	-3770	-3679	1945	0	-555	-10782	15.71	15.71	9.42	9.42	3	0.21	0.05	0.33	0.00	0.00	24.0
19	25	-14980	-1909	1887	0	-587	-3501	15.71	15.71	9.42	9.42	3	0.07	0.03	0.15	0.00	0.00	24.0
20	25	-9550	-2657	1054	0	-217	-6728	15.71	15.71	9.42	9.42	3	0.13	0.03	0.22	0.00	0.00	24.0
37	25	-423	-3769	1694	0	-467	-11880	15.71	15.71	9.42	9.42	3	0.23	0.05	0.35	0.00	0.00	24.0
38	25	-19110	-819	1596	0	-521	258	15.71	15.71	9.42	9.42	3	0.02	0.02	0.11	0.00	0.00	24.0
39	25	-10058	-2066	207	0	96	-5122	15.71	15.71	9.42	9.42	3	0.09	0.03	0.17	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-10360	-1268	1076	0	-468	-3234	15.71	15.71	9.42	9.42	3	0.06	0.02	0.10	0.00	0.00	24.0
2	38	-6845	-1288	953	0	-422	-3428	15.71	15.71	9.42	9.42	2	0.10	0.02	0.11	0.00	0.00	24.0
3	38	-6849	-1320	674	0	-267	-3504	15.71	15.71	9.42	9.42	2	0.10	0.02	0.11	0.00	0.00	24.0
4	38	-9087	-631	982	0	-452	-1471	15.71	15.71	9.42	9.42	2	0.05	0.01	0.06	0.00	0.00	24.0
5	38	-9092	-664	703	0	-297	-1547	15.71	15.71	9.42	9.42	2	0.05	0.01	0.06	0.00	0.00	24.0
6	38	-7624	-1020	1289	0	-613	-2655	15.71	15.71	9.42	9.42	2	0.08	0.02	0.09	0.00	0.00	24.0
7	38	-7640	-1129	358	0	-97	-2908	15.71	15.71	9.42	9.42	2	0.08	0.01	0.10	0.00	0.00	24.0
8	38	-8297	-822	1298	0	-622	-2068	15.71	15.71	9.42	9.42	2	0.07	0.02	0.09	0.00	0.00	24.0
9	38	-8312	-932	367	0	-106	-2320	15.71	15.71	9.42	9.42	2	0.06	0.01	0.08	0.00	0.00	24.0
10	38	-6845	-1288	953	0	-422	-3428	15.71	15.71	9.42	9.42	2	0.10	0.02	0.11	0.00	0.00	24.0
11	38	-6849	-1320	674	0	-267	-3504	15.71	15.71	9.42	9.42	2	0.10	0.02	0.11	0.00	0.00	24.0
12	38	-9087	-631	982	0	-452	-1471	15.71	15.71	9.42	9.42	2	0.05	0.01	0.06	0.00	0.00	24.0
13	38	-9092	-664	703	0	-297	-1547	15.71	15.71	9.42	9.42	2	0.05	0.01	0.06	0.00	0.00	24.0
14	38	-7624	-1020	1289	0	-613	-2655	15.71	15.71	9.42	9.42	2	0.08	0.02	0.09	0.00	0.00	24.0
15	38	-7640	-1129	358	0	-97	-2908	15.71	15.71	9.42	9.42	2	0.08	0.01	0.10	0.00	0.00	24.0
16	38	-8297	-822	1298	0	-622	-2068	15.71	15.71	9.42	9.42	2	0.07	0.02	0.09	0.00	0.00	24.0
17	38	-8312	-932	367	0	-106	-2320	15.71	15.71	9.42	9.42	2	0.06	0.01	0.08	0.00	0.00	24.0
18	38	-3640	-3679	1945	0	-798	-11241	15.71	15.71	9.42	9.42	3	0.22	0.05	0.33	0.00	0.00	24.0
19	38	-14850	-1909	1887	0	-823	-3739	15.71	15.71	9.42	9.42	3	0.08	0.03	0.15	0.00	0.00	24.0
20	38	-9420	-2657	1054	0	-348	-7061	15.71	15.71	9.42	9.42	3	0.13	0.03	0.22	0.00	0.00	24.0
37	38	-293	-3769	1694	0	-679	-12350	15.71	15.71	9.42	9.42	3	0.24	0.05	0.35	0.00	0.00	24.0
38	38	-18980	-819	1596	0	-721	156	15.71	15.71	9.42	9.42	3	0.03	0.02	0.11	0.00	0.00	24.0
39	38	-9928	-2066	207	0	70	-5380	15.71	15.71	9.42	9.42	3	0.10	0.03	0.17	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-10230	-1268	1076	0	-602	-3392	15.71	15.71	9.42	9.42	3	0.07	0.02	0.10	0.00	0.00	24.0
2	50	-6745	-1288	953	0	-541	-3589	15.71	15.71	9.42	9.42	2	0.11	0.02	0.11	0.00	0.00	24.0
3	50	-6749	-1320	674	0	-352	-3669	15.71	15.71	9.42	9.42	2	0.10	0.02	0.11	0.00	0.00	24.0
4	50	-8987	-631	982	0	-575	-1550	15.71	15.71	9.42	9.42	2	0.06	0.01	0.06	0.00	0.00	24.0
5	50	-8992	-664	703	0	-385	-1630	15.71	15.71	9.42	9.42	2	0.05	0.01	0.06	0.00	0.00	24.0
6	50	-7524	-1020	1289	0	-775	-2782	15.71	15.71	9.42	9.42	2	0.09	0.02	0.09	0.00	0.00	24.0
7	50	-7540	-1129	358	0	-142	-3049	15.71	15.71	9.42	9.42	2	0.08	0.01	0.10	0.00	0.00	24.0
8	50	-8197	-822	1298	0	-785	-2171	15.71	15.71	9.42	9.42	2	0.08	0.02	0.09	0.00	0.00	24.0
9	50	-8212	-932	367	0	-152	-2437	15.71	15.71	9.42	9.42	2	0.07	0.01	0.08	0.00	0.00	24.0
10	50	-6745	-1288	953	0	-541	-3589	15.71	15.71	9.42	9.42	2	0.11	0.02	0.11	0.00	0.00	24.0
11	50	-6749	-1320	674	0	-352	-3669	15.71	15.71	9.42	9.42	2	0.10	0.02	0.11	0.00	0.00	24.0
12	50	-8987	-631	982	0	-575	-1550	15.71	15.71	9.42	9.42	2	0.06	0.01	0.06	0.00	0.00	24.0
13	50	-8992	-664	703	0	-385	-1630	15.71	15.71	9.42	9.42	2	0.05	0.01	0.06	0.00	0.00	24.0
14	50	-7524	-1020	1289	0	-775	-2782	15.71	15.71	9.42	9.42	2	0.09	0.02	0.09	0.00	0.00	24.0
15	50	-7540	-1129	358	0	-142	-3049	15.71	15.71	9.42	9.42	2	0.08	0.01	0.10	0.00	0.00	24.0
16	50	-8197	-822	1298	0	-785	-2171	15.71	15.71	9.42	9.42	2	0.08	0.02	0.09	0.00	0.00	24.0
17	50	-8212	-932	367	0	-152	-2437	15.71	15.71	9.42	9.42	2	0.07	0.01	0.08	0.00	0.00	24.0
18	50	-3510	-3679	1945	0	-1041	-11700	15.71	15.71	9.42	9.42	3	0.23	0.05	0.33	0.00	0.00	24.0
19	50	-14720	-1909	1887	0	-1059	-3978	15.71	15.71	9.42	9.42	3	0.08	0.03	0.15	0.00	0.00	24.0
20	50	-9290	-2657	1054	0	-480	-7393	15.71	15.71	9.42	9.42	3	0.14	0.03	0.22	0.00	0.00	24.0
37	50	-163	-3769	1694	0	-890	-12820	15.71	15.71	9.42	9.42	3	0.25	0.05	0.35	0.00	0.00	24.0
38	50	-18850	-819	1596	0	-920	54	15.71	15.71	9.42	9.42	3	0.03	0.02	0.11	0.00	0.00	24.0
39	50	-9797	-2066	207	0	44	-5638	15.71	15.71	9.42	9.42	3	0.10	0.03	0.17	0.00	0.00	24.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 82 NI 1351 NF 1360 SEZ. Rp B= 0.400 H= 0.600 (pilastro)
PIL. NUM. 16
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-12700	820	695	0	1375	-2217	12.57	12.57	6.28	6.28	3	0.11	0.01	0.08	0.00	0.00	24.0

2	0	-9706	1020	512	0	1008	-2830	12.57	12.57	6.28	6.28	2	0.18	0.02	0.10	0.00	0.00	24.0
3	0	-9829	1021	547	0	1085	-2834	12.57	12.57	6.28	6.28	2	0.18	0.02	0.10	0.00	0.00	24.0
4	0	-9705	240	522	0	1029	-577	12.57	12.57	6.28	6.28	2	0.08	0.01	0.05	0.00	0.00	24.0
5	0	-9829	242	556	0	1106	-581	12.57	12.57	6.28	6.28	2	0.08	0.01	0.05	0.00	0.00	24.0
6	0	-9561	745	476	0	926	-2038	12.57	12.57	6.28	6.28	2	0.14	0.01	0.07	0.00	0.00	24.0
7	0	-9973	750	590	0	1182	-2049	12.57	12.57	6.28	6.28	2	0.15	0.01	0.07	0.00	0.00	24.0
8	0	-9561	512	478	0	933	-1362	12.57	12.57	6.28	6.28	2	0.10	0.01	0.05	0.00	0.00	24.0
9	0	-9973	516	593	0	1189	-1373	12.57	12.57	6.28	6.28	2	0.12	0.01	0.05	0.00	0.00	24.0
10	0	-9706	1020	512	0	1008	-2830	12.57	12.57	6.28	6.28	2	0.18	0.02	0.10	0.00	0.00	24.0
11	0	-9829	1021	547	0	1085	-2834	12.57	12.57	6.28	6.28	2	0.18	0.02	0.10	0.00	0.00	24.0
12	0	-9705	240	522	0	1029	-577	12.57	12.57	6.28	6.28	2	0.08	0.01	0.05	0.00	0.00	24.0
13	0	-9829	242	556	0	1106	-581	12.57	12.57	6.28	6.28	2	0.08	0.01	0.05	0.00	0.00	24.0
14	0	-9561	745	476	0	926	-2038	12.57	12.57	6.28	6.28	2	0.14	0.01	0.07	0.00	0.00	24.0
15	0	-9973	750	590	0	1182	-2049	12.57	12.57	6.28	6.28	2	0.15	0.01	0.07	0.00	0.00	24.0
16	0	-9561	512	478	0	933	-1362	12.57	12.57	6.28	6.28	2	0.10	0.01	0.05	0.00	0.00	24.0
17	0	-9973	516	593	0	1189	-1373	12.57	12.57	6.28	6.28	2	0.12	0.01	0.05	0.00	0.00	24.0
18	0	-13120	2690	704	0	1379	-7553	12.57	12.57	6.28	6.28	3	0.28	0.05	0.26	0.00	0.00	24.0
19	0	-13130	104	729	0	1433	-116	12.57	12.57	6.28	6.28	3	0.08	0.01	0.07	0.00	0.00	24.0
20	0	-13050	1319	625	0	1157	-3617	12.57	12.57	6.28	6.28	3	0.14	0.02	0.13	0.00	0.00	24.0
37	0	-12870	3363	679	0	1332	-9503	12.57	12.57	6.28	6.28	3	0.35	0.06	0.32	0.00	0.00	24.0
38	0	-12900	-946	720	0	1422	2891	12.57	12.57	6.28	6.28	3	0.13	0.02	0.09	0.00	0.00	24.0
39	0	-12760	1078	547	0	961	-2944	12.57	12.57	6.28	6.28	3	0.12	0.02	0.10	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-12602	820	695	0	1288	-2115	12.57	12.57	6.28	6.28	3	0.10	0.01	0.08	0.00	0.00	24.0
2	12	-9631	1020	512	0	944	-2703	12.57	12.57	6.28	6.28	2	0.17	0.02	0.10	0.00	0.00	24.0
3	12	-9754	1021	547	0	1017	-2706	12.57	12.57	6.28	6.28	2	0.17	0.02	0.10	0.00	0.00	24.0
4	12	-9630	240	522	0	964	-547	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
5	12	-9754	242	556	0	1037	-550	12.57	12.57	6.28	6.28	2	0.08	0.01	0.05	0.00	0.00	24.0
6	12	-9486	745	476	0	867	-1945	12.57	12.57	6.28	6.28	2	0.13	0.01	0.07	0.00	0.00	24.0
7	12	-9898	750	590	0	1108	-1955	12.57	12.57	6.28	6.28	2	0.14	0.01	0.07	0.00	0.00	24.0
8	12	-9486	512	478	0	873	-1298	12.57	12.57	6.28	6.28	2	0.10	0.01	0.05	0.00	0.00	24.0
9	12	-9898	516	593	0	1115	-1309	12.57	12.57	6.28	6.28	2	0.11	0.01	0.05	0.00	0.00	24.0
10	12	-9631	1020	512	0	944	-2703	12.57	12.57	6.28	6.28	2	0.17	0.02	0.10	0.00	0.00	24.0
11	12	-9754	1021	547	0	1017	-2706	12.57	12.57	6.28	6.28	2	0.17	0.02	0.10	0.00	0.00	24.0
12	12	-9630	240	522	0	964	-547	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
13	12	-9754	242	556	0	1037	-550	12.57	12.57	6.28	6.28	2	0.08	0.01	0.05	0.00	0.00	24.0
14	12	-9486	745	476	0	867	-1945	12.57	12.57	6.28	6.28	2	0.13	0.01	0.07	0.00	0.00	24.0
15	12	-9898	750	590	0	1108	-1955	12.57	12.57	6.28	6.28	2	0.14	0.01	0.07	0.00	0.00	24.0
16	12	-9486	512	478	0	873	-1298	12.57	12.57	6.28	6.28	2	0.10	0.01	0.05	0.00	0.00	24.0
17	12	-9898	516	593	0	1115	-1309	12.57	12.57	6.28	6.28	2	0.11	0.01	0.05	0.00	0.00	24.0
18	12	-13022	2690	704	0	1291	-7217	12.57	12.57	6.28	6.28	3	0.27	0.05	0.26	0.00	0.00	24.0
19	12	-13032	104	729	0	1342	-103	12.57	12.57	6.28	6.28	3	0.07	0.01	0.07	0.00	0.00	24.0
20	12	-12952	1319	625	0	1079	-3452	12.57	12.57	6.28	6.28	3	0.14	0.02	0.13	0.00	0.00	24.0
37	12	-12772	3363	679	0	1247	-9082	12.57	12.57	6.28	6.28	3	0.34	0.06	0.32	0.00	0.00	24.0
38	12	-12802	-946	720	0	1332	2773	12.57	12.57	6.28	6.28	3	0.12	0.02	0.09	0.00	0.00	24.0
39	12	-12662	1078	547	0	893	-2809	12.57	12.57	6.28	6.28	3	0.11	0.02	0.10	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-12505	820	695	0	1201	-2012	12.57	12.57	6.28	6.28	3	0.10	0.01	0.08	0.00	0.00	24.0
2	25	-9556	1020	512	0	880	-2575	12.57	12.57	6.28	6.28	2	0.16	0.02	0.10	0.00	0.00	24.0
3	25	-9679	1021	547	0	948	-2578	12.57	12.57	6.28	6.28	2	0.16	0.02	0.10	0.00	0.00	24.0
4	25	-9555	240	522	0	899	-517	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
5	25	-9679	242	556	0	967	-520	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
6	25	-9411	745	476	0	807	-1852	12.57	12.57	6.28	6.28	2	0.12	0.01	0.07	0.00	0.00	24.0
7	25	-9823	750	590	0	1035	-1862	12.57	12.57	6.28	6.28	2	0.13	0.01	0.07	0.00	0.00	24.0
8	25	-9411	512	478	0	813	-1234	12.57	12.57	6.28	6.28	2	0.09	0.01	0.05	0.00	0.00	24.0
9	25	-9823	516	593	0	1040	-1244	12.57	12.57	6.28	6.28	2	0.10	0.01	0.05	0.00	0.00	24.0
10	25	-9556	1020	512	0	880	-2575	12.57	12.57	6.28	6.28	2	0.16	0.02	0.10	0.00	0.00	24.0
11	25	-9679	1021	547	0	948	-2578	12.57	12.57	6.28	6.28	2	0.16	0.02	0.10	0.00	0.00	24.0
12	25	-9555	240	522	0	899	-517	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
13	25	-9679	242	556	0	967	-520	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
14	25	-9411	745	476	0	807	-1852	12.57	12.57	6.28	6.28	2	0.12	0.01	0.07	0.00	0.00	24.0
15	25	-9823	750	590	0	1035	-1862	12.57	12.57	6.28	6.28	2	0.13	0.01	0.07	0.00	0.00	24.0
16	25	-9411	512	478	0	813	-1234	12.57	12.57	6.28	6.28	2	0.09	0.01	0.05	0.00	0.00	24.0
17	25	-9823	516	593	0	1040	-1244	12.57	12.57	6.28	6.28	2	0.10	0.01	0.05	0.00	0.00	24.0
18	25	-12925	2690	704	0	1203	-6880	12.57	12.57	6.28	6.28	3	0.26	0.05	0.26	0.00	0.00	24.0
19	25	-12935	104	729	0	1251	-90	12.57	12.57	6.28	6.28	3	0.07	0.01	0.07	0.00	0.00	24.0
20	25	-12855	1319	625	0	1001	-3288	12.57	12.57	6.28	6.28	3	0.13	0.02	0.13	0.00	0.00	24.0
37	25	-12675	3363	679	0	1162	-8662	12.57	12.57	6.28	6.28	3	0.32	0.06	0.32	0.00	0.00	24.0
38	25	-12705	-946	720	0	1242	2655	12.57	12.57	6.28	6.28	3	0.12	0.02	0.09	0.00	0.00	24.0
39	25	-12565	1078	547	0	825	-2674	12.57	12.57	6.28	6.28	3	0.11	0.02	0.10	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	37	-12408	820	695	0	1114	-1910	12.57	12.57	6.28	6.28	3	0.09	0.01	0.08	0.00	0.00	24.0
2	37	-9481	1020	512	0	816	-2448	12.57	12.57	6.28	6.28	2	0.15	0.02	0.10	0.00	0.00	24.0
3	37	-9604	1021	547	0	880	-2451	12.57	12.57	6.28	6.28	2	0.15	0.02	0.10	0.00	0.00	24.0
4	37	-9480	240	522	0	834	-487	12.57	12.57	6.28	6.28	2	0.06	0.01	0.05	0.00	0.00	24.0
5	37	-9604	242	556	0	898	-490	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
6	37	-9336	745	476	0	748	-1758	12.57	12.57	6.28	6.28	2	0.12	0.01	0.07	0.00	0.00	24.0
7	37	-9748	750	590	0	961	-1768	12.57	12.57	6.28	6.28	2	0.12	0.01	0.07	0.00	0.00	24.0
8	37	-9336	512	478	0	753	-1170	12.57	12.57	6.28	6.28	2	0.09	0.01	0.05	0.00	0.00	24.0
9	37	-9748	516	593	0	966	-1180	12.57	12.57	6.28	6.28	2	0.10	0.01	0.05	0.00	0.00	24.0
10	37	-9481	1020	512	0	816	-2448	12.57	12.57	6.28	6.28	2	0.15	0.02	0.10	0.00	0.00	24.0
11	37	-9604	1021	547	0	880	-2451	12.57	12.57	6.28	6.28	2	0.15	0.02	0.10	0.00	0.00	24.0
12	37	-9480	240	522	0	834	-487	12.57	12.57	6.28	6.28	2	0.06	0.01	0.05	0.00	0.00	24.0
13	37	-9604	242	556	0	898	-490	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
14	37	-9336	745	476	0	748	-1758	12.57	12.57	6.28	6.28	2	0.12	0.01	0.07	0.00	0.00	24.0
15	37	-9748	750	590	0	961	-1768	12.57	12.57	6.28	6.28	2	0.12	0.01	0.07	0.00	0.00	24.0
16	37	-9336	512	478	0	753	-1170	12.57	12.57	6.28	6.28	2	0.09	0.01	0.05	0.00	0.00	24.0
17	37	-9748	516	593	0	966	-1180	12.57	12.57	6.28	6.28	2	0.10	0.01	0.05	0.00	0.00	24.0
18	37	-12828	2690	704	0	1115	-6544	12.57	12.57	6.28	6.28	3	0.25	0.05	0.26	0.00	0.00	24.0
19	37	-12838	104	729	0	1160	-77	12.57	12.57	6.28	6.28	3	0.06	0.01	0.07	0.00	0.00	24.0
20	37	-12758	1319	625	0	922	-3123	12.57	12.57	6.28	6.28	3	0.12	0.02	0.13	0.00	0.00	24.0
37	37	-12578	3363	679	0	1078	-8241	12.57	12.57	6.28	6.28	3	0.30	0.06	0.32	0.00	0.00	24.0
38	37	-12608	-946	720	0	1152	2536	12.57	12.57	6.28	6.28	3	0.11	0.02	0.09	0.00	0.00	24.0
39	37	-12468	1078	547	0	756	-2540	12.57	12.57	6.28	6.28	3	0.10	0.02	0.10	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-12310	820	695	0	1027	-1807	12.57	12.57	6.28	6.28	3	0.08	0.01	0.08	0.00	0.00	24.0
2	50	-9406	1020	512	0	752	-2320	12.57	12.57	6.28	6.28	2	0.14	0.02	0.10	0.00	0.00	24.0
3	50	-9529	1021	547	0	812	-2323	12.57	12.57	6.28	6.28	2	0.15	0.02	0.10	0.00	0.00	24.0
4	50	-9405	240	522	0	769	-457	12.57	12.57	6.28	6.28	2	0.06	0.01	0.05	0.00	0.00	24.0
5	50	-9529	242	556	0	828	-460	12.57	12.57	6.28	6.28	2	0.06	0.01	0.05	0.00	0.00	24.0
6	50	-9261	745	476	0	688	-1665	12.57	12.57	6.28	6.28	2	0.11	0.01	0.07	0.00	0.00	24.0
7	50	-9673	750	590	0	887	-1674	12.57	12.57	6.28	6.28	2	0.12	0.01	0.07	0.00	0.00	24.0

8	50	-9261	512	478	0	693	-1106	12.57	12.57	6.28	6.28	2	0.08	0.01	0.05	0.00	0.00	24.0
9	50	-9673	516	593	0	892	-1115	12.57	12.57	6.28	6.28	2	0.09	0.01	0.05	0.00	0.00	24.0
10	50	-9406	1020	512	0	752	-2320	12.57	12.57	6.28	6.28	2	0.14	0.02	0.10	0.00	0.00	24.0
11	50	-9529	1021	547	0	812	-2323	12.57	12.57	6.28	6.28	2	0.15	0.02	0.10	0.00	0.00	24.0
12	50	-9405	240	522	0	769	-457	12.57	12.57	6.28	6.28	2	0.06	0.01	0.05	0.00	0.00	24.0
13	50	-9529	242	556	0	828	-460	12.57	12.57	6.28	6.28	2	0.06	0.01	0.05	0.00	0.00	24.0
14	50	-9261	745	476	0	688	-1665	12.57	12.57	6.28	6.28	2	0.11	0.01	0.07	0.00	0.00	24.0
15	50	-9673	750	590	0	887	-1674	12.57	12.57	6.28	6.28	2	0.12	0.01	0.07	0.00	0.00	24.0
16	50	-9261	512	478	0	693	-1106	12.57	12.57	6.28	6.28	2	0.08	0.01	0.05	0.00	0.00	24.0
17	50	-9673	516	593	0	892	-1115	12.57	12.57	6.28	6.28	2	0.09	0.01	0.05	0.00	0.00	24.0
18	50	-12730	2690	704	0	1027	-6208	12.57	12.57	6.28	6.28	3	0.23	0.05	0.26	0.00	0.00	24.0
19	50	-12740	104	729	0	1069	-64	12.57	12.57	6.28	6.28	3	0.06	0.01	0.07	0.00	0.00	24.0
20	50	-12660	1319	625	0	844	-2958	12.57	12.57	6.28	6.28	3	0.12	0.02	0.13	0.00	0.00	24.0
37	50	-12480	3363	679	0	993	-7821	12.57	12.57	6.28	6.28	3	0.29	0.06	0.32	0.00	0.00	24.0
38	50	-12510	-946	720	0	1062	2418	12.57	12.57	6.28	6.28	3	0.10	0.02	0.09	0.00	0.00	24.0
39	50	-12370	1078	547	0	688	-2405	12.57	12.57	6.28	6.28	3	0.10	0.02	0.10	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 83 NI 1360 NF 170 SEZ. Rp B= 0.400 H= 0.600 (pilastro)
PIL. NUM. 16A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-12310	820	695	0	1027	-1807	12.57	12.57	6.28	6.28	3	0.08	0.01	0.08	0.00	0.00	24.0
2	0	-9406	1020	512	0	752	-2320	12.57	12.57	6.28	6.28	2	0.14	0.02	0.10	0.00	0.00	24.0
3	0	-9529	1021	547	0	812	-2323	12.57	12.57	6.28	6.28	2	0.15	0.02	0.10	0.00	0.00	24.0
4	0	-9405	240	522	0	769	-457	12.57	12.57	6.28	6.28	2	0.06	0.01	0.05	0.00	0.00	24.0
5	0	-9529	242	556	0	828	-460	12.57	12.57	6.28	6.28	2	0.06	0.01	0.05	0.00	0.00	24.0
6	0	-9261	745	476	0	688	-1665	12.57	12.57	6.28	6.28	2	0.11	0.01	0.07	0.00	0.00	24.0
7	0	-9673	750	590	0	887	-1674	12.57	12.57	6.28	6.28	2	0.12	0.01	0.07	0.00	0.00	24.0
8	0	-9261	512	478	0	693	-1106	12.57	12.57	6.28	6.28	2	0.08	0.01	0.05	0.00	0.00	24.0
9	0	-9673	516	593	0	892	-1115	12.57	12.57	6.28	6.28	2	0.09	0.01	0.05	0.00	0.00	24.0
10	0	-9406	1020	512	0	752	-2320	12.57	12.57	6.28	6.28	2	0.14	0.02	0.10	0.00	0.00	24.0
11	0	-9529	1021	547	0	812	-2323	12.57	12.57	6.28	6.28	2	0.15	0.02	0.10	0.00	0.00	24.0
12	0	-9405	240	522	0	769	-457	12.57	12.57	6.28	6.28	2	0.06	0.01	0.05	0.00	0.00	24.0
13	0	-9529	242	556	0	828	-460	12.57	12.57	6.28	6.28	2	0.06	0.01	0.05	0.00	0.00	24.0
14	0	-9261	745	476	0	688	-1665	12.57	12.57	6.28	6.28	2	0.11	0.01	0.07	0.00	0.00	24.0
15	0	-9673	750	590	0	887	-1674	12.57	12.57	6.28	6.28	2	0.12	0.01	0.07	0.00	0.00	24.0
16	0	-9261	512	478	0	693	-1106	12.57	12.57	6.28	6.28	2	0.08	0.01	0.05	0.00	0.00	24.0
17	0	-9673	516	593	0	892	-1115	12.57	12.57	6.28	6.28	2	0.09	0.01	0.05	0.00	0.00	24.0
18	0	-12730	2690	704	0	1027	-6208	12.57	12.57	6.28	6.28	3	0.23	0.05	0.26	0.00	0.00	24.0
19	0	-12740	104	729	0	1069	-64	12.57	12.57	6.28	6.28	3	0.06	0.01	0.07	0.00	0.00	24.0
20	0	-12660	1319	625	0	844	-2958	12.57	12.57	6.28	6.28	3	0.12	0.02	0.13	0.00	0.00	24.0
37	0	-12480	3363	679	0	993	-7821	12.57	12.57	6.28	6.28	3	0.29	0.06	0.32	0.00	0.00	24.0
38	0	-12510	-946	720	0	1062	2418	12.57	12.57	6.28	6.28	3	0.10	0.02	0.09	0.00	0.00	24.0
39	0	-12370	1078	547	0	688	-2405	12.57	12.57	6.28	6.28	3	0.10	0.02	0.10	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-12212	820	695	0	940	-1705	12.57	12.57	6.28	6.28	3	0.08	0.01	0.08	0.00	0.00	24.0
2	12	-9331	1020	512	0	688	-2193	12.57	12.57	6.28	6.28	2	0.13	0.02	0.10	0.00	0.00	24.0
3	12	-9454	1021	547	0	744	-2195	12.57	12.57	6.28	6.28	2	0.14	0.02	0.10	0.00	0.00	24.0
4	12	-9330	240	522	0	703	-427	12.57	12.57	6.28	6.28	2	0.05	0.01	0.05	0.00	0.00	24.0
5	12	-9454	242	556	0	759	-429	12.57	12.57	6.28	6.28	2	0.06	0.01	0.05	0.00	0.00	24.0
6	12	-9186	745	476	0	629	-1572	12.57	12.57	6.28	6.28	2	0.10	0.01	0.07	0.00	0.00	24.0
7	12	-9598	750	590	0	813	-1580	12.57	12.57	6.28	6.28	2	0.11	0.01	0.08	0.00	0.00	24.0
8	12	-9186	512	478	0	634	-1042	12.57	12.57	6.28	6.28	2	0.08	0.01	0.05	0.00	0.00	24.0
9	12	-9598	516	593	0	818	-1050	12.57	12.57	6.28	6.28	2	0.09	0.01	0.05	0.00	0.00	24.0
10	12	-9331	1020	512	0	688	-2193	12.57	12.57	6.28	6.28	2	0.13	0.02	0.10	0.00	0.00	24.0
11	12	-9454	1021	547	0	744	-2195	12.57	12.57	6.28	6.28	2	0.14	0.02	0.10	0.00	0.00	24.0
12	12	-9330	240	522	0	703	-427	12.57	12.57	6.28	6.28	2	0.05	0.01	0.05	0.00	0.00	24.0
13	12	-9454	242	556	0	759	-429	12.57	12.57	6.28	6.28	2	0.06	0.01	0.05	0.00	0.00	24.0
14	12	-9186	745	476	0	629	-1572	12.57	12.57	6.28	6.28	2	0.10	0.01	0.07	0.00	0.00	24.0
15	12	-9598	750	590	0	813	-1580	12.57	12.57	6.28	6.28	2	0.11	0.01	0.08	0.00	0.00	24.0
16	12	-9186	512	478	0	634	-1042	12.57	12.57	6.28	6.28	2	0.08	0.01	0.05	0.00	0.00	24.0
17	12	-9598	516	593	0	818	-1050	12.57	12.57	6.28	6.28	2	0.09	0.01	0.05	0.00	0.00	24.0
18	12	-12632	2690	704	0	939	-5872	12.57	12.57	6.28	6.28	3	0.22	0.05	0.26	0.00	0.00	24.0
19	12	-12642	104	729	0	978	-51	12.57	12.57	6.28	6.28	3	0.05	0.01	0.07	0.00	0.00	24.0
20	12	-12562	1319	625	0	766	-2793	12.57	12.57	6.28	6.28	3	0.11	0.02	0.13	0.00	0.00	24.0
37	12	-12382	3363	679	0	908	-7401	12.57	12.57	6.28	6.28	3	0.27	0.06	0.32	0.00	0.00	24.0
38	12	-12412	-946	720	0	972	2300	12.57	12.57	6.28	6.28	3	0.10	0.02	0.09	0.00	0.00	24.0
39	12	-12272	1078	547	0	620	-2270	12.57	12.57	6.28	6.28	3	0.09	0.02	0.10	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-12115	820	695	0	854	-1602	12.57	12.57	6.28	6.28	3	0.07	0.01	0.08	0.00	0.00	24.0
2	25	-9256	1020	512	0	624	-2065	12.57	12.57	6.28	6.28	2	0.13	0.02	0.10	0.00	0.00	24.0
3	25	-9379	1021	547	0	675	-2067	12.57	12.57	6.28	6.28	2	0.13	0.02	0.10	0.00	0.00	24.0
4	25	-9255	240	522	0	638	-397	12.57	12.57	6.28	6.28	2	0.05	0.01	0.05	0.00	0.00	24.0
5	25	-9379	242	556	0	689	-399	12.57	12.57	6.28	6.28	2	0.05	0.01	0.05	0.00	0.00	24.0
6	25	-9111	745	476	0	570	-1478	12.57	12.57	6.28	6.28	2	0.10	0.01	0.08	0.00	0.00	24.0
7	25	-9523	750	590	0	740	-1486	12.57	12.57	6.28	6.28	2	0.10	0.01	0.08	0.00	0.00	24.0
8	25	-9111	512	478	0	574	-978	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
9	25	-9523	516	593	0	744	-986	12.57	12.57	6.28	6.28	2	0.08	0.01	0.05	0.00	0.00	24.0
10	25	-9256	1020	512	0	624	-2065	12.57	12.57	6.28	6.28	2	0.13	0.02	0.10	0.00	0.00	24.0
11	25	-9379	1021	547	0	675	-2067	12.57	12.57	6.28	6.28	2	0.13	0.02	0.10	0.00	0.00	24.0
12	25	-9255	240	522	0	638	-397	12.57	12.57	6.28	6.28	2	0.05	0.01	0.05	0.00	0.00	24.0
13	25	-9379	242	556	0	689	-399	12.57	12.57	6.28	6.28	2	0.05	0.01	0.05	0.00	0.00	24.0
14	25	-9111	745	476	0	570	-1478	12.57	12.57	6.28	6.28	2	0.10	0.01	0.08	0.00	0.00	24.0
15	25	-9523	750	590	0	740	-1486	12.57	12.57	6.28	6.28	2	0.10	0.01	0.08	0.00	0.00	24.0
16	25	-9111	512	478	0	574	-978	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
17	25	-9523	516	593	0	744	-986	12.57	12.57	6.28	6.28	2	0.08	0.01	0.05	0.00	0.00	24.0
18	25	-12535	2690	704	0	851	-5536	12.57	12.57	6.28	6.28	3	0.21	0.05	0.26	0.00	0.00	24.0
19	25	-12545	104	729	0	886	-38	12.57	12.57	6.28	6.28	3	0.05	0.01	0.07	0.00	0.00	24.0
20	25	-12465	1319	625	0	688	-2628	12.57	12.57	6.28	6.28	3	0.10	0.02	0.13	0.00	0.00	24.0
37	25	-12285	3363	679	0	823	-6980	12.57	12.57	6.28	6.28	3	0.26	0.06	0.32	0.00	0.00	24.0
38	25	-12315	-946	720	0	882	2181	12.57	12.57	6.28	6.28	3	0.09	0.02	0.09	0.00	0.00	24.0
39	25	-12175	1078	547	0	551	-2135	12.57	12.57	6.28	6.28	3	0.08	0.02	0.10	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-12018	820	695	0	767	-1499	12.57	12.57	6.28	6.28	3	0.07	0.01	0.08	0.00	0.00	24.0
2	38	-9181	1020	512	0	560	-1937	12.57	12.57	6.28	6.28	2	0.12	0.02	0.10	0.00	0.00	24.0
3	38	-9304	1021	547	0	607	-1940	12.57	12.57	6.28	6.28	2	0.12	0.02	0.10	0.00	0.00	24.0

4	38	-9180	240	522	0	573	-367	12.57	12.57	6.28	6.28	2	0.05	0.01	0.05	0.00	0.00	24.0
5	38	-9304	242	556	0	620	-369	12.57	12.57	6.28	6.28	2	0.05	0.01	0.05	0.00	0.00	24.0
6	38	-9036	745	476	0	510	-1385	12.57	12.57	6.28	6.28	2	0.09	0.01	0.08	0.00	0.00	24.0
7	38	-9448	750	590	0	666	-1393	12.57	12.57	6.28	6.28	2	0.09	0.01	0.08	0.00	0.00	24.0
8	38	-9036	512	478	0	514	-914	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
9	38	-9448	516	593	0	670	-921	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
10	38	-9181	1020	512	0	560	-1937	12.57	12.57	6.28	6.28	2	0.12	0.02	0.10	0.00	0.00	24.0
11	38	-9304	1021	547	0	607	-1940	12.57	12.57	6.28	6.28	2	0.12	0.02	0.10	0.00	0.00	24.0
12	38	-9180	240	522	0	573	-367	12.57	12.57	6.28	6.28	2	0.05	0.01	0.05	0.00	0.00	24.0
13	38	-9304	242	556	0	620	-369	12.57	12.57	6.28	6.28	2	0.05	0.01	0.05	0.00	0.00	24.0
14	38	-9036	745	476	0	510	-1385	12.57	12.57	6.28	6.28	2	0.09	0.01	0.08	0.00	0.00	24.0
15	38	-9448	750	590	0	666	-1393	12.57	12.57	6.28	6.28	2	0.09	0.01	0.08	0.00	0.00	24.0
16	38	-9036	512	478	0	514	-914	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
17	38	-9448	516	593	0	670	-921	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
18	38	-12438	2690	704	0	763	-5199	12.57	12.57	6.28	6.28	3	0.19	0.05	0.26	0.00	0.00	24.0
19	38	-12448	104	729	0	795	-25	12.57	12.57	6.28	6.28	3	0.04	0.01	0.07	0.00	0.00	24.0
20	38	-12368	1319	625	0	610	-2463	12.57	12.57	6.28	6.28	3	0.10	0.02	0.13	0.00	0.00	24.0
37	38	-12188	3363	679	0	738	-6560	12.57	12.57	6.28	6.28	3	0.24	0.06	0.32	0.00	0.00	24.0
38	38	-12218	-946	720	0	792	2062	12.57	12.57	6.28	6.28	3	0.09	0.02	0.09	0.00	0.00	24.0
39	38	-12078	1078	547	0	483	-2000	12.57	12.57	6.28	6.28	3	0.08	0.02	0.10	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-11920	820	695	0	680	-1397	12.57	12.57	6.28	6.28	3	0.06	0.01	0.08	0.00	0.00	24.0
2	50	-9106	1020	512	0	496	-1810	12.57	12.57	6.28	6.28	2	0.11	0.02	0.10	0.00	0.00	24.0
3	50	-9229	1021	547	0	538	-1812	12.57	12.57	6.28	6.28	2	0.11	0.02	0.10	0.00	0.00	24.0
4	50	-9105	240	522	0	508	-337	12.57	12.57	6.28	6.28	2	0.04	0.01	0.05	0.00	0.00	24.0
5	50	-9229	242	556	0	550	-339	12.57	12.57	6.28	6.28	2	0.04	0.01	0.05	0.00	0.00	24.0
6	50	-8961	745	476	0	451	-1292	12.57	12.57	6.28	6.28	2	0.08	0.01	0.08	0.00	0.00	24.0
7	50	-9373	750	590	0	592	-1299	12.57	12.57	6.28	6.28	2	0.09	0.01	0.08	0.00	0.00	24.0
8	50	-8961	512	478	0	454	-850	12.57	12.57	6.28	6.28	2	0.06	0.01	0.05	0.00	0.00	24.0
9	50	-9373	516	593	0	596	-857	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
10	50	-9106	1020	512	0	496	-1810	12.57	12.57	6.28	6.28	2	0.11	0.02	0.10	0.00	0.00	24.0
11	50	-9229	1021	547	0	538	-1812	12.57	12.57	6.28	6.28	2	0.11	0.02	0.10	0.00	0.00	24.0
12	50	-9105	240	522	0	508	-337	12.57	12.57	6.28	6.28	2	0.04	0.01	0.05	0.00	0.00	24.0
13	50	-9229	242	556	0	550	-339	12.57	12.57	6.28	6.28	2	0.04	0.01	0.05	0.00	0.00	24.0
14	50	-8961	745	476	0	451	-1292	12.57	12.57	6.28	6.28	2	0.08	0.01	0.08	0.00	0.00	24.0
15	50	-9373	750	590	0	592	-1299	12.57	12.57	6.28	6.28	2	0.09	0.01	0.08	0.00	0.00	24.0
16	50	-8961	512	478	0	454	-850	12.57	12.57	6.28	6.28	2	0.06	0.01	0.05	0.00	0.00	24.0
17	50	-9373	516	593	0	596	-857	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
18	50	-12340	2690	704	0	675	-4863	12.57	12.57	6.28	6.28	3	0.18	0.05	0.26	0.00	0.00	24.0
19	50	-12350	104	729	0	704	-12	12.57	12.57	6.28	6.28	3	0.04	0.01	0.07	0.00	0.00	24.0
20	50	-12270	1319	625	0	532	-2298	12.57	12.57	6.28	6.28	3	0.09	0.02	0.13	0.00	0.00	24.0
37	50	-12090	3363	679	0	654	-6140	12.57	12.57	6.28	6.28	3	0.23	0.06	0.33	0.00	0.00	24.0
38	50	-12120	-946	720	0	702	1944	12.57	12.57	6.28	6.28	3	0.08	0.02	0.09	0.00	0.00	24.0
39	50	-11980	1078	547	0	415	-1865	12.57	12.57	6.28	6.28	3	0.07	0.02	0.10	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 84 NI 1037 NF 300 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 15A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-37440	142	578	0	987	-269	6.28	6.28	12.57	12.57	3	0.03	0.01	0.04	0.00	0.00	24.0
2	0	-28550	360	462	0	744	-842	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
3	0	-28450	359	423	0	764	-839	6.28	6.28	12.57	12.57	2	0.06	0.01	0.03	0.00	0.00	24.0
4	0	-29150	-141	467	0	755	425	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
5	0	-29060	-142	428	0	774	428	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
6	0	-28870	186	509	0	726	-402	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
7	0	-28550	182	380	0	790	-392	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
8	0	-29050	36	510	0	729	-22	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
9	0	-28730	32	381	0	793	-12	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
10	0	-28550	360	462	0	744	-842	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
11	0	-28450	359	423	0	764	-839	6.28	6.28	12.57	12.57	2	0.06	0.01	0.03	0.00	0.00	24.0
12	0	-29150	-141	467	0	755	425	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
13	0	-29060	-142	428	0	774	428	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
14	0	-28870	186	509	0	726	-402	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
15	0	-28550	182	380	0	790	-392	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
16	0	-29050	36	510	0	729	-22	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
17	0	-28730	32	381	0	793	-12	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
18	0	-43190	1007	708	0	982	-2336	6.28	6.28	12.57	12.57	3	0.11	0.02	0.07	0.00	0.00	24.0
19	0	-43180	-638	694	0	1018	1674	6.28	6.28	12.57	12.57	3	0.08	0.01	0.05	0.00	0.00	24.0
20	0	-42350	182	413	0	477	-331	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
37	0	-41060	1541	664	0	947	-3653	6.28	6.28	12.57	12.57	3	0.17	0.03	0.10	0.00	0.00	24.0
38	0	-41050	-1200	640	0	1007	3030	6.28	6.28	12.57	12.57	3	0.14	0.02	0.08	0.00	0.00	24.0
39	0	-39670	167	172	0	105	-311	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-37342	142	578	0	915	-251	6.28	6.28	12.57	12.57	3	0.03	0.01	0.04	0.00	0.00	24.0
2	12	-28475	360	462	0	687	-797	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
3	12	-28375	359	423	0	711	-794	6.28	6.28	12.57	12.57	2	0.06	0.01	0.03	0.00	0.00	24.0
4	12	-29075	-141	467	0	697	408	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
5	12	-28985	-142	428	0	721	411	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
6	12	-28795	186	509	0	662	-379	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
7	12	-28475	182	380	0	743	-369	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
8	12	-28975	36	510	0	665	-17	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
9	12	-28655	32	381	0	746	-8	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
10	12	-28475	360	462	0	687	-797	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
11	12	-28375	359	423	0	711	-794	6.28	6.28	12.57	12.57	2	0.06	0.01	0.03	0.00	0.00	24.0
12	12	-29075	-141	467	0	697	408	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
13	12	-28985	-142	428	0	721	411	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
14	12	-28795	186	509	0	662	-379	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
15	12	-28475	182	380	0	743	-369	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
16	12	-28975	36	510	0	665	-17	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
17	12	-28655	32	381	0	746	-8	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
18	12	-43092	1007	708	0	894	-2210	6.28	6.28	12.57	12.57	3	0.10	0.02	0.07	0.00	0.00	24.0
19	12	-43082	-638	694	0	931	1594	6.28	6.28	12.57	12.57	3	0.08	0.01	0.05	0.00	0.00	24.0
20	12	-42252	182	413	0	425	-308	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
37	12	-40962	1541	664	0	864	-3460	6.28	6.28	12.57	12.57	3	0.16	0.03	0.10	0.00	0.00	24.0
38	12	-40952	-1200	640	0	927	2880	6.28	6.28	12.57	12.57	3	0.13	0.02	0.08	0.00	0.00	24.0
39	12	-39572	167	172	0	83	-290	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-37245	142	578	0	843	-233	6.28	6.28	12.57	12.57	3	0.03	0.01	0.04	0.00	0.00	24.0
2	25	-28400	360	462	0	629	-752	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
3	25	-28300	359	423	0	658	-749	6.28	6.28	12.57	12.57	2	0.06	0.01	0.03	0.00	0.00	24.0
4	25	-29000	-141	467	0	638	390	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
5	25	-28910	-142	428	0	667	393	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
6	25	-28720	186	509	0	598	-355	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
7	25	-28400	182	380	0	695	-346	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
8	25	-28900	36	510	0	601	-13	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
9	25	-28580	32	381	0	698	-4	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
10	25	-28400	360	462	0	629	-752	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
11	25	-28300	359	423	0	658	-749	6.28	6.28	12.57	12.57	2	0.06	0.01	0.03	0.00	0.00	24.0
12	25	-29000	-141	467	0	638	390	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
13	25	-28910	-142	428	0	667	393	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
14	25	-28720	186	509	0	598	-355	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
15	25	-28400	182	380	0	695	-346	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
16	25	-28900	36	510	0	601	-13	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
17	25	-28580	32	381	0	698	-4	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
18	25	-42995	1007	708	0	805	-2085	6.28	6.28	12.57	12.57	3	0.09	0.02	0.07	0.00	0.00	24.0
19	25	-42985	-638	694	0	845	1514	6.28	6.28	12.57	12.57	3	0.07	0.01	0.05	0.00	0.00	24.0
20	25	-42155	182	413	0	373	-285	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
37	25	-40865	1541	664	0	781	-3268	6.28	6.28	12.57	12.57	3	0.15	0.03	0.11	0.00	0.00	24.0
38	25	-40855	-1200	640	0	847	2730	6.28	6.28	12.57	12.57	3	0.12	0.02	0.08	0.00	0.00	24.0
39	25	-39475	167	172	0	62	-269	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-37148	142	578	0	770	-216	6.28	6.28	12.57	12.57	3	0.03	0.01	0.04	0.00	0.00	24.0
2	38	-28325	360	462	0	571	-707	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
3	38	-28225	359	423	0	605	-704	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
4	38	-28925	-141	467	0	580	373	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
5	38	-28835	-142	428	0	614	375	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
6	38	-28645	186	509	0	535	-332	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
7	38	-28325	182	380	0	648	-324	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
8	38	-28825	36	510	0	537	-8	6.28	6.28	12.57	12.57	2	0.02	0.01	0.04	0.00	0.00	24.0
9	38	-28505	32	381	0	650	0	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
10	38	-28325	360	462	0	571	-707	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
11	38	-28225	359	423	0	605	-704	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
12	38	-28925	-141	467	0	580	373	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
13	38	-28835	-142	428	0	614	375	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
14	38	-28645	186	509	0	535	-332	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
15	38	-28325	182	380	0	648	-324	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
16	38	-28825	36	510	0	537	-8	6.28	6.28	12.57	12.57	2	0.02	0.01	0.04	0.00	0.00	24.0
17	38	-28505	32	381	0	650	0	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
18	38	-42898	1007	708	0	717	-1959	6.28	6.28	12.57	12.57	3	0.09	0.02	0.07	0.00	0.00	24.0
19	38	-42888	-638	694	0	758	1435	6.28	6.28	12.57	12.57	3	0.07	0.01	0.05	0.00	0.00	24.0
20	38	-42058	182	413	0	322	-262	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
37	38	-40768	1541	664	0	698	-3075	6.28	6.28	12.57	12.57	3	0.14	0.03	0.11	0.00	0.00	24.0
38	38	-40758	-1200	640	0	767	2580	6.28	6.28	12.57	12.57	3	0.12	0.02	0.08	0.00	0.00	24.0
39	38	-39378	167	172	0	40	-248	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-37050	142	578	0	698	-198	6.28	6.28	12.57	12.57	3	0.02	0.01	0.04	0.00	0.00	24.0
2	50	-28250	360	462	0	514	-662	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
3	50	-28150	359	423	0	552	-660	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
4	50	-28850	-141	467	0	522	355	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
5	50	-28760	-142	428	0	560	357	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
6	50	-28570	186	509	0	471	-309	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
7	50	-28250	182	380	0	600	-301	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
8	50	-28750	36	510	0	474	-4	6.28	6.28	12.57	12.57	2	0.02	0.01	0.04	0.00	0.00	24.0
9	50	-28430	32	381	0	603	4	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
10	50	-28250	360	462	0	514	-662	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
11	50	-28150	359	423	0	552	-660	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
12	50	-28850	-141	467	0	522	355	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
13	50	-28760	-142	428	0	560	357	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
14	50	-28570	186	509	0	471	-309	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
15	50	-28250	182	380	0	600	-301	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
16	50	-28750	36	510	0	474	-4	6.28	6.28	12.57	12.57	2	0.02	0.01	0.04	0.00	0.00	24.0
17	50	-28430	32	381	0	603	4	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
18	50	-42800	1007	708	0	628	-1833	6.28	6.28	12.57	12.57	3	0.08	0.02	0.07	0.00	0.00	24.0
19	50	-42790	-638	694	0	671	1355	6.28	6.28	12.57	12.57	3	0.06	0.01	0.05	0.00	0.00	24.0
20	50	-41960	182	413	0	270	-240	6.28	6.28	12.57	12.57	3	0.01	0.01	0.03	0.00	0.00	24.0
37	50	-40670	1541	664	0	615	-2883	6.28	6.28	12.57	12.57	3	0.13	0.03	0.11	0.00	0.00	24.0
38	50	-40660	-1200	640	0	687	2430	6.28	6.28	12.57	12.57	3	0.11	0.02	0.08	0.00	0.00	24.0
39	50	-39280	167	172	0	19	-227	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 85 NI 1033 NF 1037 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 15
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-37830	142	578	0	1276	-340	6.28	6.28	12.57	12.57	3	0.04	0.01	0.04	0.00	0.00	24.0
2	0	-28850	360	462	0	975	-1022	6.28	6.28	12.57	12.57	2	0.08	0.01	0.04	0.00	0.00	24.0
3	0	-28750	359	423	0	975	-1019	6.28	6.28	12.57	12.57	2	0.08	0.01	0.03	0.00	0.00	24.0
4	0	-29450	-141	467	0	988	496	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
5	0	-29360	-142	428	0	988	500	6.28	6.28	12.57	12.57	2	0.06	0.01	0.03	0.00	0.00	24.0
6	0	-29170	186	509	0	980	-495	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
7	0	-28850	182	380	0	980	-483	6.28	6.28	12.57	12.57	2	0.06	0.01	0.03	0.00	0.00	24.0
8	0	-29350	36	510	0	984	-39	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
9	0	-29030	32	381	0	984	-28	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
10	0	-28850	360	462	0	975	-1022	6.28	6.28	12.57	12.57	2	0.08	0.01	0.04	0.00	0.00	24.0
11	0	-28750	359	423	0	975	-1019	6.28	6.28	12.57	12.57	2	0.08	0.01	0.03	0.00	0.00	24.0
12	0	-29450	-141	467	0	988	496	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
13	0	-29360	-142	428	0	988	500	6.28	6.28	12.57	12.57	2	0.06	0.01	0.03	0.00	0.00	24.0
14	0	-29170	186	509	0	980	-495	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
15	0	-28850	182	380	0	980	-483	6.28	6.28	12.57	12.57	2	0.06	0.01	0.03	0.00	0.00	24.0
16	0	-29350	36	510	0	984	-39	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
17	0	-29030	32	381	0	984	-28	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
18	0	-43580	1007	708	0	1336	-2839	6.28	6.28	12.57	12.57	3	0.13	0.02	0.07	0.00	0.00	24.0
19	0	-43570	-638	694	0	1365	1993	6.28	6.28	12.57	12.57	3	0.10	0.01	0.05	0.00	0.00	24.0
20	0	-42740	182	413	0	683	-421	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
37	0	-41450	1541	664	0	1279	-4424	6.28	6.28	12.57	12.57	3	0.20	0.03	0.10	0.00	0.00	24.0

38	0	-41440	-1200	640	0	1327	3630	6.28	6.28	12.57	12.57	3	0.17	0.02	0.08	0.00	0.00	24.0
39	0	-40060	167	172	0	191	-394	6.28	6.28	12.57	12.57	3	0.02	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-37732	142	578	0	1204	-322	6.28	6.28	12.57	12.57	3	0.04	0.01	0.04	0.00	0.00	24.0
2	12	-28775	360	462	0	918	-977	6.28	6.28	12.57	12.57	2	0.07	0.01	0.04	0.00	0.00	24.0
3	12	-28675	359	423	0	922	-974	6.28	6.28	12.57	12.57	2	0.07	0.01	0.03	0.00	0.00	24.0
4	12	-29375	-141	467	0	930	478	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
5	12	-29285	-142	428	0	935	482	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
6	12	-29095	186	509	0	916	-472	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
7	12	-28775	182	380	0	933	-460	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
8	12	-29275	36	510	0	920	-35	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
9	12	-28955	32	381	0	936	-24	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
10	12	-28775	360	462	0	918	-977	6.28	6.28	12.57	12.57	2	0.07	0.01	0.04	0.00	0.00	24.0
11	12	-28675	359	423	0	922	-974	6.28	6.28	12.57	12.57	2	0.07	0.01	0.03	0.00	0.00	24.0
12	12	-29375	-141	467	0	930	478	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
13	12	-29285	-142	428	0	935	482	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
14	12	-29095	186	509	0	916	-472	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
15	12	-28775	182	380	0	933	-460	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
16	12	-29275	36	510	0	920	-35	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
17	12	-28955	32	381	0	936	-24	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
18	12	-43482	1007	708	0	1248	-2713	6.28	6.28	12.57	12.57	3	0.12	0.02	0.07	0.00	0.00	24.0
19	12	-43472	-638	694	0	1278	1913	6.28	6.28	12.57	12.57	3	0.09	0.01	0.05	0.00	0.00	24.0
20	12	-42642	182	413	0	632	-399	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
37	12	-41352	1541	664	0	1196	-4231	6.28	6.28	12.57	12.57	3	0.19	0.03	0.10	0.00	0.00	24.0
38	12	-41342	-1200	640	0	1247	3480	6.28	6.28	12.57	12.57	3	0.16	0.02	0.08	0.00	0.00	24.0
39	12	-39962	167	172	0	169	-373	6.28	6.28	12.57	12.57	3	0.02	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-37635	142	578	0	1132	-304	6.28	6.28	12.57	12.57	3	0.04	0.01	0.04	0.00	0.00	24.0
2	25	-28700	360	462	0	860	-932	6.28	6.28	12.57	12.57	2	0.07	0.01	0.04	0.00	0.00	24.0
3	25	-28600	359	423	0	870	-929	6.28	6.28	12.57	12.57	2	0.07	0.01	0.03	0.00	0.00	24.0
4	25	-29300	-141	467	0	872	461	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
5	25	-29210	-142	428	0	881	464	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
6	25	-29020	186	509	0	853	-448	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
7	25	-28700	182	380	0	885	-438	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
8	25	-29200	36	510	0	856	-31	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
9	25	-28880	32	381	0	889	-20	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
10	25	-28700	360	462	0	860	-932	6.28	6.28	12.57	12.57	2	0.07	0.01	0.04	0.00	0.00	24.0
11	25	-28600	359	423	0	870	-929	6.28	6.28	12.57	12.57	2	0.07	0.01	0.03	0.00	0.00	24.0
12	25	-29300	-141	467	0	872	461	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
13	25	-29210	-142	428	0	881	464	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
14	25	-29020	186	509	0	853	-448	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
15	25	-28700	182	380	0	885	-438	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
16	25	-29200	36	510	0	856	-31	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
17	25	-28880	32	381	0	889	-20	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
18	25	-43385	1007	708	0	1159	-2588	6.28	6.28	12.57	12.57	3	0.12	0.02	0.07	0.00	0.00	24.0
19	25	-43375	-638	694	0	1192	1834	6.28	6.28	12.57	12.57	3	0.09	0.01	0.05	0.00	0.00	24.0
20	25	-42545	182	413	0	580	-376	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
37	25	-41255	1541	664	0	1113	-4039	6.28	6.28	12.57	12.57	3	0.18	0.03	0.10	0.00	0.00	24.0
38	25	-41245	-1200	640	0	1167	3330	6.28	6.28	12.57	12.57	3	0.15	0.02	0.08	0.00	0.00	24.0
39	25	-39865	167	172	0	148	-353	6.28	6.28	12.57	12.57	3	0.02	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-37538	142	578	0	1059	-287	6.28	6.28	12.57	12.57	3	0.04	0.01	0.04	0.00	0.00	24.0
2	38	-28625	360	462	0	802	-887	6.28	6.28	12.57	12.57	2	0.07	0.01	0.04	0.00	0.00	24.0
3	38	-28525	359	423	0	817	-884	6.28	6.28	12.57	12.57	2	0.07	0.01	0.03	0.00	0.00	24.0
4	38	-29225	-141	467	0	813	443	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
5	38	-29135	-142	428	0	828	446	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
6	38	-28945	186	509	0	789	-425	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
7	38	-28625	182	380	0	838	-415	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
8	38	-29125	36	510	0	793	-26	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
9	38	-28805	32	381	0	841	-16	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
10	38	-28625	360	462	0	802	-887	6.28	6.28	12.57	12.57	2	0.07	0.01	0.04	0.00	0.00	24.0
11	38	-28525	359	423	0	817	-884	6.28	6.28	12.57	12.57	2	0.07	0.01	0.03	0.00	0.00	24.0
12	38	-29225	-141	467	0	813	443	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
13	38	-29135	-142	428	0	828	446	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
14	38	-28945	186	509	0	789	-425	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
15	38	-28625	182	380	0	838	-415	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
16	38	-29125	36	510	0	793	-26	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
17	38	-28805	32	381	0	841	-16	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
18	38	-43288	1007	708	0	1071	-2462	6.28	6.28	12.57	12.57	3	0.11	0.02	0.07	0.00	0.00	24.0
19	38	-43278	-638	694	0	1105	1754	6.28	6.28	12.57	12.57	3	0.08	0.01	0.05	0.00	0.00	24.0
20	38	-42448	182	413	0	528	-353	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
37	38	-41158	1541	664	0	1030	-3846	6.28	6.28	12.57	12.57	3	0.17	0.03	0.10	0.00	0.00	24.0
38	38	-41148	-1200	640	0	1087	3180	6.28	6.28	12.57	12.57	3	0.15	0.02	0.08	0.00	0.00	24.0
39	38	-39768	167	172	0	126	-332	6.28	6.28	12.57	12.57	3	0.02	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-37440	142	578	0	987	-269	6.28	6.28	12.57	12.57	3	0.03	0.01	0.04	0.00	0.00	24.0
2	50	-28550	360	462	0	744	-842	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
3	50	-28450	359	423	0	764	-839	6.28	6.28	12.57	12.57	2	0.06	0.01	0.03	0.00	0.00	24.0
4	50	-29150	-141	467	0	755	425	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
5	50	-29060	-142	428	0	774	428	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
6	50	-28870	186	509	0	726	-402	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
7	50	-28550	182	380	0	790	-392	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
8	50	-29050	36	510	0	729	-22	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
9	50	-28730	32	381	0	793	-12	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
10	50	-28550	360	462	0	744	-842	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
11	50	-28450	359	423	0	764	-839	6.28	6.28	12.57	12.57	2	0.06	0.01	0.03	0.00	0.00	24.0
12	50	-29150	-141	467	0	755	425	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
13	50	-29060	-142	428	0	774	428	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
14	50	-28870	186	509	0	726	-402	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
15	50	-28550	182	380	0	790	-392	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
16	50	-29050	36	510	0	729	-22	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
17	50	-28730	32	381	0	793	-12	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
18	50	-43190	1007	708	0	982	-2336	6.28	6.28	12.57	12.57	3	0.11	0.02	0.07	0.00	0.00	24.0
19	50	-43180	-638	694	0	1018	1674	6.28	6.28	12.57	12.57	3	0.08	0.01	0.05	0.00	0.00	24.0
20	50	-42350	182	413	0	477	-331	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
37	50	-41060	1541	664	0	947	-3653	6.28	6.28	12.57	12.57	3	0.17	0.03	0.10	0.00	0.00	24.0
38	50	-41050	-1200	640	0	1007	3030	6.28	6.28	12.57	12.57	3	0.14	0.02	0.08	0.00	0.00	24.0
39	50	-39670	167	172	0	105	-311	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 86 NI 1255 NF 1262 SEZ. Rp B= 0.600 H= 0.400 (pilastro)

PIL. NUM. 14
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-20000	18	-360	0	-997	-39	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
2	0	-15420	92	-308	0	-843	-323	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
3	0	-15340	91	-237	0	-668	-321	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
4	0	-15440	-63	-318	0	-865	260	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
5	0	-15350	-63	-246	0	-690	262	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
6	0	-15520	38	-395	0	-1055	-122	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
7	0	-15250	36	-156	0	-472	-114	6.28	6.28	12.57	12.57	2	0.03	0.00	0.01	0.00	0.00	24.0
8	0	-15520	-8	-398	0	-1062	53	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
9	0	-15260	-10	-159	0	-479	61	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
10	0	-15420	92	-308	0	-843	-323	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
11	0	-15340	91	-237	0	-668	-321	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
12	0	-15440	-63	-318	0	-865	260	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
13	0	-15350	-63	-246	0	-690	262	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
14	0	-15520	38	-395	0	-1055	-122	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
15	0	-15250	36	-156	0	-472	-114	6.28	6.28	12.57	12.57	2	0.03	0.00	0.01	0.00	0.00	24.0
16	0	-15520	-8	-398	0	-1062	53	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
17	0	-15260	-10	-159	0	-479	61	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
18	0	-21920	242	-666	0	-1763	-870	6.28	6.28	12.57	12.57	3	0.07	0.01	0.06	0.00	0.00	24.0
19	0	-21870	-241	-612	0	-1631	918	6.28	6.28	12.57	12.57	3	0.07	0.01	0.05	0.00	0.00	24.0
20	0	-21780	5	-799	0	-2144	8	6.28	6.28	12.57	12.57	3	0.07	0.01	0.07	0.00	0.00	24.0
37	0	-21040	409	-595	0	-1582	-1488	6.28	6.28	12.57	12.57	3	0.09	0.01	0.05	0.00	0.00	24.0
38	0	-20960	-396	-506	0	-1363	1493	6.28	6.28	12.57	12.57	3	0.09	0.01	0.04	0.00	0.00	24.0
39	0	-20810	14	-817	0	-2216	-23	6.28	6.28	12.57	12.57	3	0.07	0.01	0.07	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	12	-19902	18	-360	0	-952	-37	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
2	12	-15345	92	-308	0	-804	-311	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
3	12	-15265	91	-237	0	-638	-309	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
4	12	-15365	-63	-318	0	-826	252	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
5	12	-15275	-63	-246	0	-660	254	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
6	12	-15445	38	-395	0	-1006	-117	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
7	12	-15175	36	-156	0	-452	-109	6.28	6.28	12.57	12.57	2	0.03	0.00	0.01	0.00	0.00	24.0
8	12	-15445	-8	-398	0	-1012	52	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
9	12	-15185	-10	-159	0	-459	60	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
10	12	-15345	92	-308	0	-804	-311	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
11	12	-15265	91	-237	0	-638	-309	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
12	12	-15365	-63	-318	0	-826	252	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
13	12	-15275	-63	-246	0	-660	254	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
14	12	-15445	38	-395	0	-1006	-117	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
15	12	-15175	36	-156	0	-452	-109	6.28	6.28	12.57	12.57	2	0.03	0.00	0.01	0.00	0.00	24.0
16	12	-15445	-8	-398	0	-1012	52	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
17	12	-15185	-10	-159	0	-459	60	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
18	12	-21822	242	-666	0	-1680	-840	6.28	6.28	12.57	12.57	3	0.07	0.01	0.06	0.00	0.00	24.0
19	12	-21772	-241	-612	0	-1555	888	6.28	6.28	12.57	12.57	3	0.07	0.01	0.05	0.00	0.00	24.0
20	12	-21682	5	-799	0	-2044	9	6.28	6.28	12.57	12.57	3	0.07	0.01	0.07	0.00	0.00	24.0
37	12	-20942	409	-595	0	-1508	-1437	6.28	6.28	12.57	12.57	3	0.09	0.01	0.05	0.00	0.00	24.0
38	12	-20862	-396	-506	0	-1300	1444	6.28	6.28	12.57	12.57	3	0.08	0.01	0.04	0.00	0.00	24.0
39	12	-20712	14	-817	0	-2114	-22	6.28	6.28	12.57	12.57	3	0.07	0.01	0.07	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	25	-19805	18	-360	0	-907	-35	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
2	25	-15270	92	-308	0	-766	-300	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
3	25	-15190	91	-237	0	-609	-298	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
4	25	-15290	-63	-318	0	-786	244	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
5	25	-15200	-63	-246	0	-629	247	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
6	25	-15370	38	-395	0	-956	-112	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
7	25	-15100	36	-156	0	-433	-105	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
8	25	-15370	-8	-398	0	-962	51	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
9	25	-15110	-10	-159	0	-439	59	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
10	25	-15270	92	-308	0	-766	-300	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
11	25	-15190	91	-237	0	-609	-298	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
12	25	-15290	-63	-318	0	-786	244	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
13	25	-15200	-63	-246	0	-629	247	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
14	25	-15370	38	-395	0	-956	-112	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
15	25	-15100	36	-156	0	-433	-105	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
16	25	-15370	-8	-398	0	-962	51	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
17	25	-15110	-10	-159	0	-439	59	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
18	25	-21725	242	-666	0	-1597	-810	6.28	6.28	12.57	12.57	3	0.07	0.01	0.06	0.00	0.00	24.0
19	25	-21675	-241	-612	0	-1478	858	6.28	6.28	12.57	12.57	3	0.07	0.01	0.05	0.00	0.00	24.0
20	25	-21585	5	-799	0	-1944	9	6.28	6.28	12.57	12.57	3	0.06	0.01	0.07	0.00	0.00	24.0
37	25	-20845	409	-595	0	-1433	-1385	6.28	6.28	12.57	12.57	3	0.08	0.01	0.05	0.00	0.00	24.0
38	25	-20765	-396	-506	0	-1237	1394	6.28	6.28	12.57	12.57	3	0.08	0.01	0.04	0.00	0.00	24.0
39	25	-20615	14	-817	0	-2012	-20	6.28	6.28	12.57	12.57	3	0.07	0.01	0.07	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	38	-19708	18	-360	0	-862	-32	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
2	38	-15195	92	-308	0	-727	-289	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
3	38	-15115	91	-237	0	-579	-286	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
4	38	-15215	-63	-318	0	-746	237	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
5	38	-15125	-63	-246	0	-598	239	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
6	38	-15295	38	-395	0	-907	-107	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
7	38	-15025	36	-156	0	-413	-100	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
8	38	-15295	-8	-398	0	-912	50	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
9	38	-15035	-10	-159	0	-419	57	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
10	38	-15195	92	-308	0	-727	-289	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
11	38	-15115	91	-237	0	-579	-286	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
12	38	-15215	-63	-318	0	-746	237	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
13	38	-15125	-63	-246	0	-598	239	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
14	38	-15295	38	-395	0	-907	-107	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
15	38	-15025	36	-156	0	-413	-100	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
16	38	-15295	-8	-398	0	-912	50	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
17	38	-15035	-10	-159	0	-419	57	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
18	38	-21628	242	-666	0	-1513	-780	6.28	6.28	12.57	12.57	3	0.07	0.01	0.06	0.00	0.00	24.0
19	38	-21578	-241	-612	0	-1402	828	6.28	6.28	12.57	12.57	3	0.06	0.01	0.05	0.00	0.00	24.0
20	38	-21488	5	-799	0	-1844	10	6.28	6.28	12.57	12.57	3	0.06	0.01	0.07	0.00	0.00	24.0
37	38	-20748	409	-595	0	-1358	-1334	6.28	6.28	12.57	12.57	3	0.08	0.01	0.05	0.00	0.00	24.0
38	38	-20668	-396	-506	0	-1173	1345	6.28	6.28	12.57	12.57	3	0.08	0.01	0.04	0.00	0.00	24.0
39	38	-20518	14	-817	0	-1910	-18	6.28	6.28	12.57	12.57	3	0.06	0.01	0.07	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-19610	18	-360	0	-816	-30	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
2	50	-15120	92	-308	0	-689	-277	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
3	50	-15040	91	-237	0	-550	-275	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
4	50	-15140	-63	-318	0	-707	229	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
5	50	-15050	-63	-246	0	-567	231	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
6	50	-15220	38	-395	0	-857	-102	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
7	50	-14950	36	-156	0	-394	-96	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
8	50	-15220	-8	-398	0	-862	49	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
9	50	-14960	-10	-159	0	-399	56	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
10	50	-15120	92	-308	0	-689	-277	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
11	50	-15040	91	-237	0	-550	-275	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
12	50	-15140	-63	-318	0	-707	229	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
13	50	-15050	-63	-246	0	-567	231	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
14	50	-15220	38	-395	0	-857	-102	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
15	50	-14950	36	-156	0	-394	-96	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
16	50	-15220	-8	-398	0	-862	49	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
17	50	-14960	-10	-159	0	-399	56	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
18	50	-21530	242	-666	0	-1430	-749	6.28	6.28	12.57	12.57	3	0.06	0.01	0.06	0.00	0.00	24.0
19	50	-21480	-241	-612	0	-1325	798	6.28	6.28	12.57	12.57	3	0.06	0.01	0.05	0.00	0.00	24.0
20	50	-21390	5	-799	0	-1744	11	6.28	6.28	12.57	12.57	3	0.06	0.01	0.07	0.00	0.00	24.0
37	50	-20650	409	-595	0	-1284	-1283	6.28	6.28	12.57	12.57	3	0.08	0.01	0.05	0.00	0.00	24.0
38	50	-20570	-396	-506	0	-1110	1295	6.28	6.28	12.57	12.57	3	0.07	0.01	0.04	0.00	0.00	24.0
39	50	-20420	14	-817	0	-1808	-16	6.28	6.28	12.57	12.57	3	0.06	0.01	0.07	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 87 NI 1262 NF 128 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 14A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
													Fx,M	Bielle	V,Mx			
	cm		daN			daN*m				cmq						cmq/m		cm
1	0	-19610	18	-360	0	-816	-30	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
2	0	-15120	92	-308	0	-689	-277	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
3	0	-15040	91	-237	0	-550	-275	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
4	0	-15140	-63	-318	0	-707	229	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
5	0	-15050	-63	-246	0	-567	231	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
6	0	-15220	38	-395	0	-857	-102	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
7	0	-14950	36	-156	0	-394	-96	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
8	0	-15220	-8	-398	0	-862	49	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
9	0	-14960	-10	-159	0	-399	56	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
10	0	-15120	92	-308	0	-689	-277	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
11	0	-15040	91	-237	0	-550	-275	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
12	0	-15140	-63	-318	0	-707	229	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
13	0	-15050	-63	-246	0	-567	231	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
14	0	-15220	38	-395	0	-857	-102	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
15	0	-14950	36	-156	0	-394	-96	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
16	0	-15220	-8	-398	0	-862	49	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
17	0	-14960	-10	-159	0	-399	56	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
18	0	-21530	242	-666	0	-1430	-749	6.28	6.28	12.57	12.57	3	0.06	0.01	0.06	0.00	0.00	24.0
19	0	-21480	-241	-612	0	-1325	798	6.28	6.28	12.57	12.57	3	0.06	0.01	0.05	0.00	0.00	24.0
20	0	-21390	5	-799	0	-1744	11	6.28	6.28	12.57	12.57	3	0.06	0.01	0.07	0.00	0.00	24.0
37	0	-20650	409	-595	0	-1284	-1283	6.28	6.28	12.57	12.57	3	0.08	0.01	0.05	0.00	0.00	24.0
38	0	-20570	-396	-506	0	-1110	1295	6.28	6.28	12.57	12.57	3	0.07	0.01	0.04	0.00	0.00	24.0
39	0	-20420	14	-817	0	-1808	-16	6.28	6.28	12.57	12.57	3	0.06	0.01	0.07	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-19512	18	-360	0	-771	-28	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
2	12	-15045	92	-308	0	-650	-266	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
3	12	-14965	91	-237	0	-520	-264	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
4	12	-15065	-63	-318	0	-667	221	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
5	12	-14975	-63	-246	0	-537	223	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
6	12	-15145	38	-395	0	-808	-98	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
7	12	-14875	36	-156	0	-374	-91	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
8	12	-15145	-8	-398	0	-813	48	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
9	12	-14885	-10	-159	0	-379	55	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
10	12	-15045	92	-308	0	-650	-266	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
11	12	-14965	91	-237	0	-520	-264	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
12	12	-15065	-63	-318	0	-667	221	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
13	12	-14975	-63	-246	0	-537	223	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
14	12	-15145	38	-395	0	-808	-98	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
15	12	-14875	36	-156	0	-374	-91	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
16	12	-15145	-8	-398	0	-813	48	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
17	12	-14885	-10	-159	0	-379	55	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
18	12	-21432	242	-666	0	-1347	-719	6.28	6.28	12.57	12.57	3	0.06	0.01	0.06	0.00	0.00	24.0
19	12	-21382	-241	-612	0	-1249	768	6.28	6.28	12.57	12.57	3	0.06	0.01	0.05	0.00	0.00	24.0
20	12	-21292	5	-799	0	-1644	11	6.28	6.28	12.57	12.57	3	0.05	0.01	0.07	0.00	0.00	24.0
37	12	-20552	409	-595	0	-1210	-1232	6.28	6.28	12.57	12.57	3	0.07	0.01	0.05	0.00	0.00	24.0
38	12	-20472	-396	-506	0	-1047	1246	6.28	6.28	12.57	12.57	3	0.07	0.01	0.04	0.00	0.00	24.0
39	12	-20322	14	-817	0	-1706	-15	6.28	6.28	12.57	12.57	3	0.06	0.01	0.07	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-19415	18	-360	0	-726	-25	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
2	25	-14970	92	-308	0	-612	-254	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
3	25	-14890	91	-237	0	-490	-252	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
4	25	-14990	-63	-318	0	-627	213	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
5	25	-14900	-63	-246	0	-506	215	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
6	25	-15070	38	-395	0	-758	-93	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
7	25	-14800	36	-156	0	-355	-87	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
8	25	-15070	-8	-398	0	-763	47	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
9	25	-14810	-10	-159	0	-359	54	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
10	25	-14970	92	-308	0	-612	-254	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
11	25	-14890	91	-237	0	-490	-252	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
12	25	-14990	-63	-318	0	-627	213	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
13	25	-14900	-63	-246	0	-506	215	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
14	25	-15070	38	-395	0	-758	-93	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
15	25	-14800	36	-156	0	-355	-87	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
16	25	-15070	-8	-398	0	-763	47	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
17	25	-14810	-10	-159	0	-359	54	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
18	25	-21335	242	-666	0	-1264	-689	6.28	6.28	12.57	12.57	3	0.06	0.01	0.06	0.00	0.00	24.0
19	25	-21285	-241	-612	0	-1172	738	6.28	6.28	12.57	12.57	3	0.05	0.01	0.05	0.00	0.00	24.0

20	25	-21195	5	-799	0	-1544	12	6.28	6.28	12.57	12.57	3	0.05	0.01	0.07	0.00	0.00	24.0
37	25	-20455	409	-595	0	-1135	-1181	6.28	6.28	12.57	12.57	3	0.07	0.01	0.05	0.00	0.00	24.0
38	25	-20375	-396	-506	0	-983	1196	6.28	6.28	12.57	12.57	3	0.07	0.01	0.04	0.00	0.00	24.0
39	25	-20225	14	-817	0	-1604	-13	6.28	6.28	12.57	12.57	3	0.05	0.01	0.07	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-19318	18	-360	0	-681	-23	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
2	38	-14895	92	-308	0	-573	-243	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
3	38	-14815	91	-237	0	-461	-241	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
4	38	-14915	-63	-318	0	-587	205	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
5	38	-14825	-63	-246	0	-475	207	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
6	38	-14995	38	-395	0	-709	-88	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
7	38	-14725	36	-156	0	-335	-82	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
8	38	-14995	-8	-398	0	-713	46	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
9	38	-14735	-10	-159	0	-339	52	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
10	38	-14895	92	-308	0	-573	-243	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
11	38	-14815	91	-237	0	-461	-241	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
12	38	-14915	-63	-318	0	-587	205	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
13	38	-14825	-63	-246	0	-475	207	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
14	38	-14995	38	-395	0	-709	-88	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
15	38	-14725	36	-156	0	-335	-82	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
16	38	-14995	-8	-398	0	-713	46	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
17	38	-14735	-10	-159	0	-339	52	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
18	38	-21238	242	-666	0	-1180	-659	6.28	6.28	12.57	12.57	3	0.05	0.01	0.06	0.00	0.00	24.0
19	38	-21188	-241	-612	0	-1096	707	6.28	6.28	12.57	12.57	3	0.05	0.01	0.05	0.00	0.00	24.0
20	38	-21098	5	-799	0	-1445	13	6.28	6.28	12.57	12.57	3	0.05	0.01	0.07	0.00	0.00	24.0
37	38	-20358	409	-595	0	-1061	-1130	6.28	6.28	12.57	12.57	3	0.07	0.01	0.05	0.00	0.00	24.0
38	38	-20278	-396	-506	0	-920	1147	6.28	6.28	12.57	12.57	3	0.06	0.01	0.04	0.00	0.00	24.0
39	38	-20128	14	-817	0	-1501	-11	6.28	6.28	12.57	12.57	3	0.05	0.01	0.07	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-19220	18	-360	0	-636	-21	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
2	50	-14820	92	-308	0	-534	-231	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
3	50	-14740	91	-237	0	-431	-230	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
4	50	-14840	-63	-318	0	-548	197	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
5	50	-14750	-63	-246	0	-445	199	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
6	50	-14920	38	-395	0	-660	-83	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
7	50	-14650	36	-156	0	-316	-78	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
8	50	-14920	-8	-398	0	-663	45	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
9	50	-14660	-10	-159	0	-320	51	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
10	50	-14820	92	-308	0	-534	-231	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
11	50	-14740	91	-237	0	-431	-230	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
12	50	-14840	-63	-318	0	-548	197	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
13	50	-14750	-63	-246	0	-445	199	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
14	50	-14920	38	-395	0	-660	-83	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
15	50	-14650	36	-156	0	-316	-78	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
16	50	-14920	-8	-398	0	-663	45	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
17	50	-14660	-10	-159	0	-320	51	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
18	50	-21140	242	-666	0	-1097	-628	6.28	6.28	12.57	12.57	3	0.05	0.01	0.06	0.00	0.00	24.0
19	50	-21090	-241	-612	0	-1019	677	6.28	6.28	12.57	12.57	3	0.05	0.01	0.05	0.00	0.00	24.0
20	50	-21000	5	-799	0	-1345	13	6.28	6.28	12.57	12.57	3	0.05	0.01	0.07	0.00	0.00	24.0
37	50	-20260	409	-595	0	-987	-1079	6.28	6.28	12.57	12.57	3	0.06	0.01	0.05	0.00	0.00	24.0
38	50	-20180	-396	-506	0	-857	1098	6.28	6.28	12.57	12.57	3	0.06	0.01	0.04	0.00	0.00	24.0
39	50	-20030	14	-817	0	-1399	-9	6.28	6.28	12.57	12.57	3	0.05	0.01	0.07	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 88 NI 1168 NF 211 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 13A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-6916	-144	225	0	-1036	-7	6.28	6.28	9.42	9.42	3	0.05	0.01	0.03	0.00	0.00	24.0
2	0	-5327	-262	186	0	-824	-9	6.28	6.28	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
3	0	-5310	-258	162	0	-768	-9	6.28	6.28	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
4	0	-5330	37	185	0	-826	-2	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
5	0	-5313	40	160	0	-770	-2	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
6	0	-5348	-160	215	0	-891	-7	6.28	6.28	9.42	9.42	2	0.06	0.01	0.03	0.00	0.00	24.0
7	0	-5291	-150	132	0	-703	-6	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
8	0	-5349	-71	214	0	-891	-5	6.28	6.28	9.42	9.42	2	0.06	0.00	0.03	0.00	0.00	24.0
9	0	-5292	-61	132	0	-704	-5	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
10	0	-5327	-262	186	0	-824	-9	6.28	6.28	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
11	0	-5310	-258	162	0	-768	-9	6.28	6.28	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
12	0	-5330	37	185	0	-826	-2	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
13	0	-5313	40	160	0	-770	-2	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
14	0	-5348	-160	215	0	-891	-7	6.28	6.28	9.42	9.42	2	0.06	0.01	0.03	0.00	0.00	24.0
15	0	-5291	-150	132	0	-703	-6	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
16	0	-5349	-71	214	0	-891	-5	6.28	6.28	9.42	9.42	2	0.06	0.00	0.03	0.00	0.00	24.0
17	0	-5292	-61	132	0	-704	-5	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
18	0	-7365	-539	353	0	-1373	-17	6.28	6.28	9.42	9.42	3	0.07	0.01	0.05	0.00	0.00	24.0
19	0	-7354	348	323	0	-1323	3	6.28	6.28	9.42	9.42	3	0.06	0.01	0.04	0.00	0.00	24.0
20	0	-7418	-110	418	0	-1521	-8	6.28	6.28	9.42	9.42	3	0.07	0.01	0.05	0.00	0.00	24.0
37	0	-7156	-850	323	0	-1272	-23	6.28	6.28	9.42	9.42	3	0.06	0.02	0.09	0.00	0.00	24.0
38	0	-7139	628	274	0	-1189	9	6.28	6.28	9.42	9.42	3	0.06	0.02	0.06	0.00	0.00	24.0
39	0	-7246	-136	433	0	-1519	-8	6.28	6.28	9.42	9.42	3	0.07	0.01	0.05	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-6843	-144	225	0	-1064	-25	6.28	6.28	9.42	9.42	3	0.05	0.01	0.03	0.00	0.00	24.0
2	12	-5271	-262	186	0	-847	-42	6.28	6.28	9.42	9.42	2	0.06	0.01	0.03	0.00	0.00	24.0
3	12	-5254	-258	162	0	-788	-41	6.28	6.28	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
4	12	-5274	37	185	0	-849	2	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
5	12	-5257	40	160	0	-790	3	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
6	12	-5292	-160	215	0	-917	-27	6.28	6.28	9.42	9.42	2	0.06	0.01	0.03	0.00	0.00	24.0
7	12	-5235	-150	132	0	-720	-25	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
8	12	-5293	-71	214	0	-918	-14	6.28	6.28	9.42	9.42	2	0.06	0.00	0.03	0.00	0.00	24.0
9	12	-5236	-61	132	0	-720	-12	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
10	12	-5271	-262	186	0	-847	-42	6.28	6.28	9.42	9.42	2	0.06	0.01	0.03	0.00	0.00	24.0
11	12	-5254	-258	162	0	-788	-41	6.28	6.28	9.42	9.42	2	0.05	0.01	0.03	0.00	0.00	24.0
12	12	-5274	37	185	0	-849	2	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
13	12	-5257	40	160	0	-790	3	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
14	12	-5292	-160	215	0	-917	-27	6.28	6.28	9.42	9.42	2	0.06	0.01	0.03	0.00	0.00	24.0
15	12	-5235	-150	132	0	-720	-25	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0

16	12	-5293	-71	214	0	-918	-14	6.28	6.28	9.42	9.42	2	0.06	0.00	0.03	0.00	0.00	24.0
17	12	-5236	-61	132	0	-720	-12	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
18	12	-7292	-539	353	0	-1417	-84	6.28	6.28	9.42	9.42	3	0.07	0.01	0.05	0.00	0.00	24.0
19	12	-7281	348	323	0	-1364	46	6.28	6.28	9.42	9.42	3	0.07	0.01	0.04	0.00	0.00	24.0
20	12	-7345	-110	418	0	-1574	-22	6.28	6.28	9.42	9.42	3	0.07	0.01	0.05	0.00	0.00	24.0
37	12	-7083	-850	323	0	-1312	-130	6.28	6.28	9.42	9.42	3	0.06	0.02	0.09	0.00	0.00	24.0
38	12	-7066	628	274	0	-1223	88	6.28	6.28	9.42	9.42	3	0.06	0.02	0.06	0.00	0.00	24.0
39	12	-7173	-136	433	0	-1573	-25	6.28	6.28	9.42	9.42	3	0.07	0.01	0.05	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-6770	-144	225	0	-1093	-43	6.28	6.28	9.42	9.42	3	0.05	0.01	0.03	0.00	0.00	24.0
2	25	-5214	-262	186	0	-871	-74	6.28	6.28	9.42	9.42	2	0.06	0.01	0.03	0.00	0.00	24.0
3	25	-5198	-258	162	0	-808	-73	6.28	6.28	9.42	9.42	2	0.06	0.01	0.03	0.00	0.00	24.0
4	25	-5218	37	185	0	-872	7	6.28	6.28	9.42	9.42	2	0.06	0.00	0.02	0.00	0.00	24.0
5	25	-5200	40	160	0	-810	8	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
6	25	-5236	-160	215	0	-944	-47	6.28	6.28	9.42	9.42	2	0.06	0.01	0.03	0.00	0.00	24.0
7	25	-5178	-150	132	0	-736	-44	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
8	25	-5236	-71	214	0	-945	-22	6.28	6.28	9.42	9.42	2	0.06	0.00	0.03	0.00	0.00	24.0
9	25	-5180	-61	132	0	-736	-20	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
10	25	-5214	-262	186	0	-871	-74	6.28	6.28	9.42	9.42	2	0.06	0.01	0.03	0.00	0.00	24.0
11	25	-5198	-258	162	0	-808	-73	6.28	6.28	9.42	9.42	2	0.06	0.01	0.03	0.00	0.00	24.0
12	25	-5218	37	185	0	-872	7	6.28	6.28	9.42	9.42	2	0.06	0.00	0.02	0.00	0.00	24.0
13	25	-5200	40	160	0	-810	8	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
14	25	-5236	-160	215	0	-944	-47	6.28	6.28	9.42	9.42	2	0.06	0.01	0.03	0.00	0.00	24.0
15	25	-5178	-150	132	0	-736	-44	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
16	25	-5236	-71	214	0	-945	-22	6.28	6.28	9.42	9.42	2	0.06	0.00	0.03	0.00	0.00	24.0
17	25	-5180	-61	132	0	-736	-20	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
18	25	-7218	-539	353	0	-1462	-151	6.28	6.28	9.42	9.42	3	0.07	0.01	0.05	0.00	0.00	24.0
19	25	-7208	348	323	0	-1404	90	6.28	6.28	9.42	9.42	3	0.07	0.01	0.04	0.00	0.00	24.0
20	25	-7272	-110	418	0	-1626	-35	6.28	6.28	9.42	9.42	3	0.08	0.01	0.05	0.00	0.00	24.0
37	25	-7010	-850	323	0	-1353	-236	6.28	6.28	9.42	9.42	3	0.07	0.02	0.09	0.00	0.00	24.0
38	25	-6993	628	274	0	-1258	166	6.28	6.28	9.42	9.42	3	0.06	0.02	0.06	0.00	0.00	24.0
39	25	-7100	-136	433	0	-1628	-42	6.28	6.28	9.42	9.42	3	0.08	0.01	0.05	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-6697	-144	225	0	-1121	-61	6.28	6.28	9.42	9.42	3	0.05	0.01	0.03	0.00	0.00	24.0
2	38	-5158	-262	186	0	-894	-107	6.28	6.28	9.42	9.42	2	0.06	0.01	0.03	0.00	0.00	24.0
3	38	-5141	-258	162	0	-828	-106	6.28	6.28	9.42	9.42	2	0.06	0.01	0.03	0.00	0.00	24.0
4	38	-5161	37	185	0	-896	12	6.28	6.28	9.42	9.42	2	0.06	0.00	0.02	0.00	0.00	24.0
5	38	-5144	40	160	0	-830	13	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
6	38	-5179	-160	215	0	-971	-67	6.28	6.28	9.42	9.42	2	0.07	0.01	0.03	0.00	0.00	24.0
7	38	-5122	-150	132	0	-753	-63	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
8	38	-5180	-71	214	0	-971	-31	6.28	6.28	9.42	9.42	2	0.06	0.00	0.03	0.00	0.00	24.0
9	38	-5123	-61	132	0	-753	-27	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
10	38	-5158	-262	186	0	-894	-107	6.28	6.28	9.42	9.42	2	0.06	0.01	0.03	0.00	0.00	24.0
11	38	-5141	-258	162	0	-828	-106	6.28	6.28	9.42	9.42	2	0.06	0.01	0.03	0.00	0.00	24.0
12	38	-5161	37	185	0	-896	12	6.28	6.28	9.42	9.42	2	0.06	0.00	0.02	0.00	0.00	24.0
13	38	-5144	40	160	0	-830	13	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
14	38	-5179	-160	215	0	-971	-67	6.28	6.28	9.42	9.42	2	0.07	0.01	0.03	0.00	0.00	24.0
15	38	-5122	-150	132	0	-753	-63	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
16	38	-5180	-71	214	0	-971	-31	6.28	6.28	9.42	9.42	2	0.06	0.00	0.03	0.00	0.00	24.0
17	38	-5123	-61	132	0	-753	-27	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
18	38	-7145	-539	353	0	-1506	-219	6.28	6.28	9.42	9.42	3	0.07	0.01	0.05	0.00	0.00	24.0
19	38	-7135	348	323	0	-1444	133	6.28	6.28	9.42	9.42	3	0.07	0.01	0.04	0.00	0.00	24.0
20	38	-7199	-110	418	0	-1678	-49	6.28	6.28	9.42	9.42	3	0.08	0.01	0.05	0.00	0.00	24.0
37	38	-6937	-850	323	0	-1394	-342	6.28	6.28	9.42	9.42	3	0.08	0.02	0.09	0.00	0.00	24.0
38	38	-6920	628	274	0	-1292	245	6.28	6.28	9.42	9.42	3	0.07	0.02	0.06	0.00	0.00	24.0
39	38	-7026	-136	433	0	-1682	-59	6.28	6.28	9.42	9.42	3	0.08	0.01	0.05	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-6624	-144	225	0	-1149	-79	6.28	6.28	9.42	9.42	3	0.06	0.01	0.03	0.00	0.00	24.0
2	50	-5102	-262	186	0	-917	-140	6.28	6.28	9.42	9.42	2	0.07	0.01	0.03	0.00	0.00	24.0
3	50	-5085	-258	162	0	-849	-138	6.28	6.28	9.42	9.42	2	0.06	0.01	0.03	0.00	0.00	24.0
4	50	-5105	37	185	0	-919	16	6.28	6.28	9.42	9.42	2	0.06	0.00	0.02	0.00	0.00	24.0
5	50	-5088	40	160	0	-850	18	6.28	6.28	9.42	9.42	2	0.06	0.00	0.02	0.00	0.00	24.0
6	50	-5123	-160	215	0	-998	-87	6.28	6.28	9.42	9.42	2	0.07	0.01	0.03	0.00	0.00	24.0
7	50	-5066	-150	132	0	-769	-82	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
8	50	-5124	-71	214	0	-998	-40	6.28	6.28	9.42	9.42	2	0.07	0.01	0.03	0.00	0.00	24.0
9	50	-5067	-61	132	0	-769	-35	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
10	50	-5102	-262	186	0	-917	-140	6.28	6.28	9.42	9.42	2	0.07	0.01	0.03	0.00	0.00	24.0
11	50	-5085	-258	162	0	-849	-138	6.28	6.28	9.42	9.42	2	0.06	0.01	0.03	0.00	0.00	24.0
12	50	-5105	37	185	0	-919	16	6.28	6.28	9.42	9.42	2	0.06	0.00	0.02	0.00	0.00	24.0
13	50	-5088	40	160	0	-850	18	6.28	6.28	9.42	9.42	2	0.06	0.00	0.02	0.00	0.00	24.0
14	50	-5123	-160	215	0	-998	-87	6.28	6.28	9.42	9.42	2	0.07	0.01	0.03	0.00	0.00	24.0
15	50	-5066	-150	132	0	-769	-82	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
16	50	-5124	-71	214	0	-998	-40	6.28	6.28	9.42	9.42	2	0.07	0.01	0.03	0.00	0.00	24.0
17	50	-5067	-61	132	0	-769	-35	6.28	6.28	9.42	9.42	2	0.05	0.00	0.02	0.00	0.00	24.0
18	50	-7072	-539	353	0	-1550	-286	6.28	6.28	9.42	9.42	3	0.08	0.01	0.05	0.00	0.00	24.0
19	50	-7062	348	323	0	-1485	177	6.28	6.28	9.42	9.42	3	0.07	0.01	0.04	0.00	0.00	24.0
20	50	-7126	-110	418	0	-1731	-63	6.28	6.28	9.42	9.42	3	0.08	0.01	0.05	0.00	0.00	24.0
37	50	-6864	-850	323	0	-1434	-448	6.28	6.28	9.42	9.42	3	0.08	0.02	0.09	0.00	0.00	24.0
38	50	-6847	628	274	0	-1326	323	6.28	6.28	9.42	9.42	3	0.07	0.02	0.06	0.00	0.00	24.0
39	50	-6953	-136	433	0	-1736	-76	6.28	6.28	9.42	9.42	3	0.08	0.01	0.05	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 89 NI 1160 NF 1168 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 13
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm

1	0	-4796	-43	-409	0	-1313	14	6.28	6.28	9.42	9.42	3	0.06	0.01	0.05	0.00	0.00	24.0
2	0	-3690	-60	-316	0	-1038	21	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
3	0	-3685	-60	-307	0	-976	21	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
4	0	-3694	-7	-322	0	-1043	1	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
5	0	-3689	-7	-313	0	-981	1	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
6	0	-3698	-42	-330	0	-1113	14	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
7	0	-3680	-41	-298	0	-905	14	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
8	0	-3699	-26	-331	0	-1115	8	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
9	0	-3681	-25	-299	0	-906	8	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
10	0	-3690	-60	-316	0	-1038	21	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
11	0	-3685	-60	-307	0	-976	21	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0

12	0	-3694	-7	-322	0	-1043	1	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
13	0	-3689	-7	-313	0	-981	1	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
14	0	-3698	-42	-330	0	-1113	14	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
15	0	-3680	-41	-298	0	-905	14	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
16	0	-3699	-26	-331	0	-1115	8	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
17	0	-3681	-25	-299	0	-906	8	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
18	0	-5046	-121	-483	0	-1700	44	6.28	6.28	9.42	9.42	3	0.08	0.01	0.06	0.00	0.00	24.0
19	0	-5047	39	-491	0	-1653	-17	6.28	6.28	9.42	9.42	3	0.08	0.01	0.06	0.00	0.00	24.0
20	0	-5071	-46	-502	0	-1863	15	6.28	6.28	9.42	9.42	3	0.09	0.01	0.06	0.00	0.00	24.0
37	0	-4924	-175	-446	0	-1576	64	6.28	6.28	9.42	9.42	3	0.08	0.01	0.06	0.00	0.00	24.0
38	0	-4926	92	-460	0	-1497	-37	6.28	6.28	9.42	9.42	3	0.07	0.01	0.06	0.00	0.00	24.0
39	0	-4965	-49	-479	0	-1847	16	6.28	6.28	9.42	9.42	3	0.09	0.01	0.06	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-4723	-43	-409	0	-1262	9	6.28	6.28	9.42	9.42	3	0.06	0.01	0.05	0.00	0.00	24.0
2	12	-3634	-60	-316	0	-999	14	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
3	12	-3629	-60	-307	0	-937	14	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
4	12	-3638	-7	-322	0	-1003	0	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
5	12	-3633	-7	-313	0	-942	0	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
6	12	-3642	-42	-330	0	-1072	9	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
7	12	-3624	-41	-298	0	-867	9	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
8	12	-3643	-26	-331	0	-1073	5	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
9	12	-3625	-25	-299	0	-869	5	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
10	12	-3634	-60	-316	0	-999	14	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
11	12	-3629	-60	-307	0	-937	14	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
12	12	-3638	-7	-322	0	-1003	0	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
13	12	-3633	-7	-313	0	-942	0	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
14	12	-3642	-42	-330	0	-1072	9	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
15	12	-3624	-41	-298	0	-867	9	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
16	12	-3643	-26	-331	0	-1073	5	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
17	12	-3625	-25	-299	0	-869	5	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
18	12	-4973	-121	-483	0	-1640	29	6.28	6.28	9.42	9.42	3	0.08	0.01	0.06	0.00	0.00	24.0
19	12	-4974	39	-491	0	-1592	-12	6.28	6.28	9.42	9.42	3	0.08	0.01	0.06	0.00	0.00	24.0
20	12	-4998	-46	-502	0	-1800	10	6.28	6.28	9.42	9.42	3	0.09	0.01	0.06	0.00	0.00	24.0
37	12	-4851	-175	-446	0	-1520	42	6.28	6.28	9.42	9.42	3	0.07	0.01	0.06	0.00	0.00	24.0
38	12	-4853	92	-460	0	-1439	-25	6.28	6.28	9.42	9.42	3	0.07	0.01	0.06	0.00	0.00	24.0
39	12	-4892	-49	-479	0	-1787	10	6.28	6.28	9.42	9.42	3	0.09	0.01	0.06	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-4650	-43	-409	0	-1210	4	6.28	6.28	9.42	9.42	3	0.06	0.01	0.05	0.00	0.00	24.0
2	25	-3578	-60	-316	0	-959	6	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
3	25	-3572	-60	-307	0	-899	6	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
4	25	-3582	-7	-322	0	-963	-1	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
5	25	-3576	-7	-313	0	-903	-1	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
6	25	-3586	-42	-330	0	-1031	4	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
7	25	-3568	-41	-298	0	-830	4	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
8	25	-3586	-26	-331	0	-1032	2	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
9	25	-3568	-25	-299	0	-831	2	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
10	25	-3578	-60	-316	0	-959	6	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
11	25	-3572	-60	-307	0	-899	6	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
12	25	-3582	-7	-322	0	-963	-1	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
13	25	-3576	-7	-313	0	-903	-1	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
14	25	-3586	-42	-330	0	-1031	4	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
15	25	-3568	-41	-298	0	-830	4	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
16	25	-3586	-26	-331	0	-1032	2	6.28	6.28	9.42	9.42	2	0.07	0.01	0.04	0.00	0.00	24.0
17	25	-3568	-25	-299	0	-831	2	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
18	25	-4900	-121	-483	0	-1580	14	6.28	6.28	9.42	9.42	3	0.08	0.01	0.06	0.00	0.00	24.0
19	25	-4901	39	-491	0	-1531	-7	6.28	6.28	9.42	9.42	3	0.07	0.01	0.06	0.00	0.00	24.0
20	25	-4924	-46	-502	0	-1737	4	6.28	6.28	9.42	9.42	3	0.08	0.01	0.06	0.00	0.00	24.0
37	25	-4778	-175	-446	0	-1465	21	6.28	6.28	9.42	9.42	3	0.07	0.01	0.06	0.00	0.00	24.0
38	25	-4780	92	-460	0	-1382	-14	6.28	6.28	9.42	9.42	3	0.07	0.01	0.06	0.00	0.00	24.0
39	25	-4819	-49	-479	0	-1727	4	6.28	6.28	9.42	9.42	3	0.08	0.01	0.06	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-4577	-43	-409	0	-1159	-2	6.28	6.28	9.42	9.42	3	0.06	0.01	0.05	0.00	0.00	24.0
2	38	-3521	-60	-316	0	-920	-1	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
3	38	-3516	-60	-307	0	-861	-1	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
4	38	-3525	-7	-322	0	-922	-2	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
5	38	-3520	-7	-313	0	-864	-2	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
6	38	-3529	-42	-330	0	-989	-1	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
7	38	-3511	-41	-298	0	-793	-1	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
8	38	-3530	-26	-331	0	-990	-1	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
9	38	-3512	-25	-299	0	-794	-1	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
10	38	-3521	-60	-316	0	-920	-1	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
11	38	-3516	-60	-307	0	-861	-1	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
12	38	-3525	-7	-322	0	-922	-2	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
13	38	-3520	-7	-313	0	-864	-2	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
14	38	-3529	-42	-330	0	-989	-1	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
15	38	-3511	-41	-298	0	-793	-1	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
16	38	-3530	-26	-331	0	-990	-1	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
17	38	-3512	-25	-299	0	-794	-1	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
18	38	-4827	-121	-483	0	-1519	-2	6.28	6.28	9.42	9.42	3	0.07	0.01	0.06	0.00	0.00	24.0
19	38	-4828	39	-491	0	-1469	-2	6.28	6.28	9.42	9.42	3	0.07	0.01	0.06	0.00	0.00	24.0
20	38	-4851	-46	-502	0	-1674	-2	6.28	6.28	9.42	9.42	3	0.08	0.01	0.06	0.00	0.00	24.0
37	38	-4705	-175	-446	0	-1409	-1	6.28	6.28	9.42	9.42	3	0.07	0.01	0.06	0.00	0.00	24.0
38	38	-4707	92	-460	0	-1324	-2	6.28	6.28	9.42	9.42	3	0.06	0.01	0.06	0.00	0.00	24.0
39	38	-4746	-49	-479	0	-1667	-2	6.28	6.28	9.42	9.42	3	0.08	0.01	0.06	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-4504	-43	-409	0	-1108	-7	6.28	6.28	9.42	9.42	3	0.05	0.01	0.05	0.00	0.00	24.0
2	50	-3465	-60	-316	0	-880	-9	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
3	50	-3460	-60	-307	0	-822	-9	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
4	50	-3469	-7	-322	0	-882	-2	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
5	50	-3464	-7	-313	0	-825	-2	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
6	50	-3473	-42	-330	0	-948	-7	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
7	50	-3455	-41	-298	0	-756	-6	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
8	50	-3474	-26	-331	0	-949	-5	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
9	50	-3456	-25	-299	0	-756	-5	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
10	50	-3465	-60	-316	0	-880	-9	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
11	50	-3460	-60	-307	0	-822	-9	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
12	50	-3469	-7	-322	0	-882	-2	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
13	50	-3464	-7	-313	0	-825	-2	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
14	50	-3473	-42	-330	0	-948	-7	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
15	50	-3455	-41	-298	0	-756	-6	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0
16	50	-3474	-26	-331	0	-949	-5	6.28	6.28	9.42	9.42	2	0.06	0.01	0.04	0.00	0.00	24.0
17	50	-3456	-25	-299	0	-756	-5	6.28	6.28	9.42	9.42	2	0.05	0.01	0.04	0.00	0.00	24.0

18	50	-4754	-121	-483	0	-1459	-17	6.28	6.28	9.42	9.42	3	0.07	0.01	0.06	0.00	0.00	24.0
19	50	-4755	39	-491	0	-1408	3	6.28	6.28	9.42	9.42	3	0.07	0.01	0.06	0.00	0.00	24.0
20	50	-4778	-46	-502	0	-1611	-8	6.28	6.28	9.42	9.42	3	0.08	0.01	0.06	0.00	0.00	24.0
37	50	-4632	-175	-446	0	-1353	-23	6.28	6.28	9.42	9.42	3	0.07	0.01	0.06	0.00	0.00	24.0
38	50	-4634	92	-460	0	-1267	9	6.28	6.28	9.42	9.42	3	0.06	0.01	0.06	0.00	0.00	24.0
39	50	-4673	-49	-479	0	-1607	-8	6.28	6.28	9.42	9.42	3	0.08	0.01	0.06	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 90 NI 1159 NF 1161 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 18
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-5982	110	-466	0	-1379	-24	6.28	6.28	12.57	12.57	3	0.05	0.01	0.05	0.00	0.00	24.0
2	0	-4609	-5	-356	0	-1091	-0	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
3	0	-4599	-8	-343	0	-996	0	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
4	0	-4605	176	-374	0	-1126	-37	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
5	0	-4594	174	-361	0	-1030	-36	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
6	0	-4620	62	-378	0	-1215	-14	6.28	6.28	12.57	12.57	2	0.07	0.01	0.04	0.00	0.00	24.0
7	0	-4585	53	-333	0	-896	-12	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
8	0	-4619	116	-383	0	-1225	-25	6.28	6.28	12.57	12.57	2	0.07	0.01	0.04	0.00	0.00	24.0
9	0	-4584	107	-339	0	-906	-23	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
10	0	-4609	-5	-356	0	-1091	-0	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
11	0	-4599	-8	-343	0	-996	0	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
12	0	-4605	176	-374	0	-1126	-37	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
13	0	-4594	174	-361	0	-1030	-36	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
14	0	-4620	62	-378	0	-1215	-14	6.28	6.28	12.57	12.57	2	0.07	0.01	0.04	0.00	0.00	24.0
15	0	-4585	53	-333	0	-896	-12	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
16	0	-4619	116	-383	0	-1225	-25	6.28	6.28	12.57	12.57	2	0.07	0.01	0.04	0.00	0.00	24.0
17	0	-4584	107	-339	0	-906	-23	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
18	0	-6276	-130	-509	0	-1596	25	6.28	6.28	12.57	12.57	3	0.06	0.01	0.05	0.00	0.00	24.0
19	0	-6264	406	-565	0	-1739	-82	6.28	6.28	12.57	12.57	3	0.07	0.01	0.06	0.00	0.00	24.0
20	0	-6271	116	-552	0	-1792	-25	6.28	6.28	12.57	12.57	3	0.07	0.01	0.06	0.00	0.00	24.0
37	0	-6139	-318	-457	0	-1429	63	6.28	6.28	12.57	12.57	3	0.05	0.01	0.05	0.00	0.00	24.0
38	0	-6118	574	-551	0	-1667	-116	6.28	6.28	12.57	12.57	3	0.06	0.01	0.06	0.00	0.00	24.0
39	0	-6129	92	-530	0	-1756	-20	6.28	6.28	12.57	12.57	3	0.07	0.01	0.06	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-5884	110	-466	0	-1321	-10	6.28	6.28	12.57	12.57	3	0.05	0.01	0.05	0.00	0.00	24.0
2	12	-4534	-5	-356	0	-1047	-1	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
3	12	-4524	-8	-343	0	-953	-1	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
4	12	-4530	176	-374	0	-1079	-15	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
5	12	-4519	174	-361	0	-985	-15	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
6	12	-4545	62	-378	0	-1168	-6	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
7	12	-4510	53	-333	0	-854	-6	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
8	12	-4544	116	-383	0	-1177	-10	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
9	12	-4509	107	-339	0	-864	-10	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
10	12	-4534	-5	-356	0	-1047	-1	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
11	12	-4524	-8	-343	0	-953	-1	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
12	12	-4530	176	-374	0	-1079	-15	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
13	12	-4519	174	-361	0	-985	-15	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
14	12	-4545	62	-378	0	-1168	-6	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
15	12	-4510	53	-333	0	-854	-6	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
16	12	-4544	116	-383	0	-1177	-10	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
17	12	-4509	107	-339	0	-864	-10	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
18	12	-6178	-130	-509	0	-1532	9	6.28	6.28	12.57	12.57	3	0.06	0.01	0.05	0.00	0.00	24.0
19	12	-6166	406	-565	0	-1668	-32	6.28	6.28	12.57	12.57	3	0.06	0.01	0.06	0.00	0.00	24.0
20	12	-6174	116	-552	0	-1723	-10	6.28	6.28	12.57	12.57	3	0.06	0.01	0.06	0.00	0.00	24.0
37	12	-6042	-318	-457	0	-1372	23	6.28	6.28	12.57	12.57	3	0.05	0.01	0.05	0.00	0.00	24.0
38	12	-6020	574	-551	0	-1598	-45	6.28	6.28	12.57	12.57	3	0.06	0.01	0.06	0.00	0.00	24.0
39	12	-6032	92	-530	0	-1690	-9	6.28	6.28	12.57	12.57	3	0.06	0.01	0.06	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-5787	110	-466	0	-1262	4	6.28	6.28	12.57	12.57	3	0.05	0.01	0.05	0.00	0.00	24.0
2	25	-4459	-5	-356	0	-1002	-2	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
3	25	-4449	-8	-343	0	-910	-2	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
4	25	-4455	176	-374	0	-1032	7	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
5	25	-4444	174	-361	0	-940	7	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
6	25	-4470	62	-378	0	-1120	2	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
7	25	-4435	53	-333	0	-813	1	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
8	25	-4469	116	-383	0	-1130	4	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
9	25	-4434	107	-339	0	-822	4	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
10	25	-4459	-5	-356	0	-1002	-2	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
11	25	-4449	-8	-343	0	-910	-2	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
12	25	-4455	176	-374	0	-1032	7	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
13	25	-4444	174	-361	0	-940	7	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
14	25	-4470	62	-378	0	-1120	2	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
15	25	-4435	53	-333	0	-813	1	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
16	25	-4469	116	-383	0	-1130	4	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
17	25	-4434	107	-339	0	-822	4	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
18	25	-6081	-130	-509	0	-1469	-7	6.28	6.28	12.57	12.57	3	0.05	0.01	0.05	0.00	0.00	24.0
19	25	-6069	406	-565	0	-1598	19	6.28	6.28	12.57	12.57	3	0.06	0.01	0.06	0.00	0.00	24.0
20	25	-6076	116	-552	0	-1654	4	6.28	6.28	12.57	12.57	3	0.06	0.01	0.06	0.00	0.00	24.0
37	25	-5944	-318	-457	0	-1315	-17	6.28	6.28	12.57	12.57	3	0.05	0.01	0.05	0.00	0.00	24.0
38	25	-5923	574	-551	0	-1529	27	6.28	6.28	12.57	12.57	3	0.06	0.01	0.06	0.00	0.00	24.0
39	25	-5934	92	-530	0	-1624	3	6.28	6.28	12.57	12.57	3	0.06	0.01	0.06	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-5690	110	-466	0	-1204	17	6.28	6.28	12.57	12.57	3	0.05	0.01	0.05	0.00	0.00	24.0
2	38	-4384	-5	-356	0	-958	-2	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
3	38	-4374	-8	-343	0	-867	-3	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
4	38	-4380	176	-374	0	-985	29	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
5	38	-4369	174	-361	0	-895	29	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
6	38	-4395	62	-378	0	-1073	9	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
7	38	-4360	53	-333	0	-771	8	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
8	38	-4394	116	-383	0	-1082	19	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
9	38	-4359	107	-339	0	-779	17	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
10	38	-4384	-5	-356	0	-958	-2	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
11	38	-4374	-8	-343	0	-867	-3	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
12	38	-4380	176	-374	0	-985	29	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
13	38	-4369	174	-361	0	-895	29	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0

14	38	-4395	62	-378	0	-1073	9	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
15	38	-4360	53	-333	0	-771	8	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
16	38	-4394	116	-383	0	-1082	19	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
17	38	-4359	107	-339	0	-779	17	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
18	38	-5984	-130	-509	0	-1406	-23	6.28	6.28	12.57	12.57	3	0.05	0.01	0.05	0.00	0.00	24.0
19	38	-5972	406	-565	0	-1527	70	6.28	6.28	12.57	12.57	3	0.06	0.01	0.06	0.00	0.00	24.0
20	38	-5978	116	-552	0	-1585	19	6.28	6.28	12.57	12.57	3	0.06	0.01	0.06	0.00	0.00	24.0
37	38	-5846	-318	-457	0	-1258	-56	6.28	6.28	12.57	12.57	3	0.05	0.01	0.05	0.00	0.00	24.0
38	38	-5826	574	-551	0	-1460	99	6.28	6.28	12.57	12.57	3	0.06	0.01	0.06	0.00	0.00	24.0
39	38	-5836	92	-530	0	-1557	14	6.28	6.28	12.57	12.57	3	0.06	0.01	0.06	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-5592	110	-466	0	-1146	31	6.28	6.28	12.57	12.57	3	0.04	0.01	0.05	0.00	0.00	24.0
2	50	-4309	-5	-356	0	-913	-3	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
3	50	-4299	-8	-343	0	-824	-4	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
4	50	-4305	176	-374	0	-939	51	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
5	50	-4294	174	-361	0	-849	50	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
6	50	-4320	62	-378	0	-1026	17	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
7	50	-4285	53	-333	0	-729	14	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
8	50	-4319	116	-383	0	-1034	33	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
9	50	-4284	107	-339	0	-737	30	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
10	50	-4309	-5	-356	0	-913	-3	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
11	50	-4299	-8	-343	0	-824	-4	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
12	50	-4305	176	-374	0	-939	51	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
13	50	-4294	174	-361	0	-849	50	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
14	50	-4320	62	-378	0	-1026	17	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
15	50	-4285	53	-333	0	-729	14	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
16	50	-4319	116	-383	0	-1034	33	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
17	50	-4284	107	-339	0	-737	30	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
18	50	-5886	-130	-509	0	-1342	-40	6.28	6.28	12.57	12.57	3	0.05	0.01	0.05	0.00	0.00	24.0
19	50	-5874	406	-565	0	-1456	120	6.28	6.28	12.57	12.57	3	0.06	0.01	0.06	0.00	0.00	24.0
20	50	-5881	116	-552	0	-1516	34	6.28	6.28	12.57	12.57	3	0.06	0.01	0.06	0.00	0.00	24.0
37	50	-5749	-318	-457	0	-1201	-96	6.28	6.28	12.57	12.57	3	0.05	0.01	0.05	0.00	0.00	24.0
38	50	-5728	574	-551	0	-1391	171	6.28	6.28	12.57	12.57	3	0.05	0.01	0.06	0.00	0.00	24.0
39	50	-5739	92	-530	0	-1491	26	6.28	6.28	12.57	12.57	3	0.06	0.01	0.06	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 91 NI 1161 NF 142 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 18A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-8241	195	55	0	-1063	31	6.28	6.28	12.57	12.57	3	0.04	0.00	0.02	0.00	0.00	24.0
2	0	-6352	-94	56	0	-849	-3	6.28	6.28	12.57	12.57	2	0.04	0.00	0.01	0.00	0.00	24.0
3	0	-6326	-100	26	0	-763	-4	6.28	6.28	12.57	12.57	2	0.04	0.00	0.01	0.00	0.00	24.0
4	0	-6353	401	58	0	-873	51	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
5	0	-6327	394	28	0	-787	50	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
6	0	-6382	87	92	0	-958	17	6.28	6.28	12.57	12.57	2	0.05	0.00	0.01	0.00	0.00	24.0
7	0	-6296	65	-8	0	-670	14	6.28	6.28	12.57	12.57	2	0.04	0.00	0.01	0.00	0.00	24.0
8	0	-6382	235	92	0	-965	33	6.28	6.28	12.57	12.57	2	0.05	0.00	0.02	0.00	0.00	24.0
9	0	-6296	214	-7	0	-678	30	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
10	0	-6352	-94	56	0	-849	-3	6.28	6.28	12.57	12.57	2	0.04	0.00	0.01	0.00	0.00	24.0
11	0	-6326	-100	26	0	-763	-4	6.28	6.28	12.57	12.57	2	0.04	0.00	0.01	0.00	0.00	24.0
12	0	-6353	401	58	0	-873	51	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
13	0	-6327	394	28	0	-787	50	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
14	0	-6382	87	92	0	-958	17	6.28	6.28	12.57	12.57	2	0.05	0.00	0.01	0.00	0.00	24.0
15	0	-6296	65	-8	0	-670	14	6.28	6.28	12.57	12.57	2	0.04	0.00	0.01	0.00	0.00	24.0
16	0	-6382	235	92	0	-965	33	6.28	6.28	12.57	12.57	2	0.05	0.00	0.02	0.00	0.00	24.0
17	0	-6296	214	-7	0	-678	30	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
18	0	-8711	-455	95	0	-1249	-40	6.28	6.28	12.57	12.57	3	0.05	0.01	0.04	0.00	0.00	24.0
19	0	-8716	1005	116	0	-1359	120	6.28	6.28	12.57	12.57	3	0.05	0.02	0.09	0.00	0.00	24.0
20	0	-8735	220	143	0	-1417	34	6.28	6.28	12.57	12.57	3	0.05	0.00	0.02	0.00	0.00	24.0
37	0	-8478	-966	72	0	-1114	-96	6.28	6.28	12.57	12.57	3	0.04	0.02	0.08	0.00	0.00	24.0
38	0	-8487	1466	106	0	-1299	171	6.28	6.28	12.57	12.57	3	0.05	0.03	0.13	0.00	0.00	24.0
39	0	-8519	157	151	0	-1394	26	6.28	6.28	12.57	12.57	3	0.05	0.00	0.02	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-8144	195	55	0	-1070	55	6.28	6.28	12.57	12.57	3	0.04	0.00	0.02	0.00	0.00	24.0
2	12	-6277	-94	56	0	-856	-15	6.28	6.28	12.57	12.57	2	0.05	0.00	0.01	0.00	0.00	24.0
3	12	-6251	-100	26	0	-766	-16	6.28	6.28	12.57	12.57	2	0.04	0.00	0.01	0.00	0.00	24.0
4	12	-6278	401	58	0	-881	101	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
5	12	-6252	394	28	0	-791	100	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
6	12	-6307	87	92	0	-970	28	6.28	6.28	12.57	12.57	2	0.05	0.00	0.01	0.00	0.00	24.0
7	12	-6221	65	-8	0	-670	22	6.28	6.28	12.57	12.57	2	0.04	0.00	0.01	0.00	0.00	24.0
8	12	-6307	235	92	0	-977	63	6.28	6.28	12.57	12.57	2	0.05	0.00	0.02	0.00	0.00	24.0
9	12	-6221	214	-7	0	-677	57	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
10	12	-6277	-94	56	0	-856	-15	6.28	6.28	12.57	12.57	2	0.05	0.00	0.01	0.00	0.00	24.0
11	12	-6251	-100	26	0	-766	-16	6.28	6.28	12.57	12.57	2	0.04	0.00	0.01	0.00	0.00	24.0
12	12	-6278	401	58	0	-881	101	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
13	12	-6252	394	28	0	-791	100	6.28	6.28	12.57	12.57	2	0.04	0.01	0.03	0.00	0.00	24.0
14	12	-6307	87	92	0	-970	28	6.28	6.28	12.57	12.57	2	0.05	0.00	0.01	0.00	0.00	24.0
15	12	-6221	65	-8	0	-670	22	6.28	6.28	12.57	12.57	2	0.04	0.00	0.01	0.00	0.00	24.0
16	12	-6307	235	92	0	-977	63	6.28	6.28	12.57	12.57	2	0.05	0.00	0.02	0.00	0.00	24.0
17	12	-6221	214	-7	0	-677	57	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
18	12	-8614	-455	95	0	-1261	-96	6.28	6.28	12.57	12.57	3	0.05	0.01	0.04	0.00	0.00	24.0
19	12	-8618	1005	116	0	-1373	246	6.28	6.28	12.57	12.57	3	0.05	0.02	0.09	0.00	0.00	24.0
20	12	-8638	220	143	0	-1435	61	6.28	6.28	12.57	12.57	3	0.05	0.00	0.02	0.00	0.00	24.0
37	12	-8380	-966	72	0	-1123	-217	6.28	6.28	12.57	12.57	3	0.04	0.02	0.08	0.00	0.00	24.0
38	12	-8390	1466	106	0	-1312	354	6.28	6.28	12.57	12.57	3	0.05	0.03	0.13	0.00	0.00	24.0
39	12	-8422	157	151	0	-1413	46	6.28	6.28	12.57	12.57	3	0.05	0.00	0.02	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-8046	195	55	0	-1077	80	6.28	6.28	12.57	12.57	3	0.04	0.00	0.02	0.00	0.00	24.0
2	25	-6202	-94	56	0	-863	-26	6.28	6.28	12.57	12.57	2	0.05	0.00	0.01	0.00	0.00	24.0
3	25	-6176	-100	26	0	-769	-29	6.28	6.28	12.57	12.57	2	0.04	0.00	0.01	0.00	0.00	24.0
4	25	-6203	401	58	0	-888	152	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
5	25	-6177	394	28	0	-794	149	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
6	25	-6232	87	92	0	-981	39	6.28	6.28	12.57	12.57	2	0.05	0.00	0.01	0.00	0.00	24.0
7	25	-6146	65	-8	0	-669	30	6.28	6.28	12.57	12.57	2	0.04	0.00	0.01	0.00	0.00	24.0
8	25	-6232	235	92	0	-989	92	6.28	6.28	12.57	12.57	2	0.06	0.00	0.02	0.00	0.00	24.0
9	25	-6146	214	-7	0	-676	84	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0

10	25	-6202	-94	56	0	-863	-26	6.28	6.28	12.57	12.57	2	0.05	0.00	0.01	0.00	0.00	24.0
11	25	-6176	-100	26	0	-769	-29	6.28	6.28	12.57	12.57	2	0.04	0.00	0.01	0.00	0.00	24.0
12	25	-6203	401	58	0	-888	152	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
13	25	-6177	394	28	0	-794	149	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
14	25	-6232	87	92	0	-981	39	6.28	6.28	12.57	12.57	2	0.05	0.00	0.01	0.00	0.00	24.0
15	25	-6146	65	-8	0	-669	30	6.28	6.28	12.57	12.57	2	0.04	0.00	0.01	0.00	0.00	24.0
16	25	-6232	235	92	0	-989	92	6.28	6.28	12.57	12.57	2	0.06	0.00	0.02	0.00	0.00	24.0
17	25	-6146	214	-7	0	-676	84	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
18	25	-8516	-455	95	0	-1273	-153	6.28	6.28	12.57	12.57	3	0.05	0.01	0.04	0.00	0.00	24.0
19	25	-8521	1005	116	0	-1388	372	6.28	6.28	12.57	12.57	3	0.06	0.02	0.09	0.00	0.00	24.0
20	25	-8540	220	143	0	-1453	89	6.28	6.28	12.57	12.57	3	0.05	0.00	0.02	0.00	0.00	24.0
37	25	-8283	-966	72	0	-1132	-338	6.28	6.28	12.57	12.57	3	0.05	0.02	0.08	0.00	0.00	24.0
38	25	-8292	1466	106	0	-1325	537	6.28	6.28	12.57	12.57	3	0.06	0.03	0.13	0.00	0.00	24.0
39	25	-8324	157	151	0	-1432	65	6.28	6.28	12.57	12.57	3	0.05	0.00	0.02	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-7948	195	55	0	-1084	104	6.28	6.28	12.57	12.57	3	0.04	0.00	0.02	0.00	0.00	24.0
2	38	-6127	-94	56	0	-870	-38	6.28	6.28	12.57	12.57	2	0.05	0.00	0.01	0.00	0.00	24.0
3	38	-6101	-100	26	0	-772	-41	6.28	6.28	12.57	12.57	2	0.04	0.00	0.01	0.00	0.00	24.0
4	38	-6128	401	58	0	-895	202	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
5	38	-6102	394	28	0	-798	198	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
6	38	-6157	87	92	0	-993	50	6.28	6.28	12.57	12.57	2	0.05	0.00	0.01	0.00	0.00	24.0
7	38	-6071	65	-8	0	-668	39	6.28	6.28	12.57	12.57	2	0.04	0.00	0.01	0.00	0.00	24.0
8	38	-6157	235	92	0	-1000	122	6.28	6.28	12.57	12.57	2	0.06	0.00	0.02	0.00	0.00	24.0
9	38	-6071	214	-7	0	-675	111	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
10	38	-6127	-94	56	0	-870	-38	6.28	6.28	12.57	12.57	2	0.05	0.00	0.01	0.00	0.00	24.0
11	38	-6101	-100	26	0	-772	-41	6.28	6.28	12.57	12.57	2	0.04	0.00	0.01	0.00	0.00	24.0
12	38	-6128	401	58	0	-895	202	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
13	38	-6102	394	28	0	-798	198	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
14	38	-6157	87	92	0	-993	50	6.28	6.28	12.57	12.57	2	0.05	0.00	0.01	0.00	0.00	24.0
15	38	-6071	65	-8	0	-668	39	6.28	6.28	12.57	12.57	2	0.04	0.00	0.01	0.00	0.00	24.0
16	38	-6157	235	92	0	-1000	122	6.28	6.28	12.57	12.57	2	0.06	0.00	0.02	0.00	0.00	24.0
17	38	-6071	214	-7	0	-675	111	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
18	38	-8418	-455	95	0	-1284	-210	6.28	6.28	12.57	12.57	3	0.05	0.01	0.04	0.00	0.00	24.0
19	38	-8424	1005	116	0	-1402	497	6.28	6.28	12.57	12.57	3	0.06	0.02	0.09	0.00	0.00	24.0
20	38	-8442	220	143	0	-1470	116	6.28	6.28	12.57	12.57	3	0.05	0.00	0.02	0.00	0.00	24.0
37	38	-8186	-966	72	0	-1141	-459	6.28	6.28	12.57	12.57	3	0.05	0.02	0.08	0.00	0.00	24.0
38	38	-8194	1466	106	0	-1339	721	6.28	6.28	12.57	12.57	3	0.06	0.03	0.13	0.00	0.00	24.0
39	38	-8226	157	151	0	-1451	85	6.28	6.28	12.57	12.57	3	0.05	0.00	0.02	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-7851	195	55	0	-1091	129	6.28	6.28	12.57	12.57	3	0.04	0.00	0.02	0.00	0.00	24.0
2	50	-6052	-94	56	0	-877	-50	6.28	6.28	12.57	12.57	2	0.05	0.00	0.01	0.00	0.00	24.0
3	50	-6026	-100	26	0	-776	-54	6.28	6.28	12.57	12.57	2	0.04	0.00	0.01	0.00	0.00	24.0
4	50	-6053	401	58	0	-903	252	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
5	50	-6027	394	28	0	-801	248	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
6	50	-6082	87	92	0	-1004	61	6.28	6.28	12.57	12.57	2	0.06	0.00	0.01	0.00	0.00	24.0
7	50	-5996	65	-8	0	-667	47	6.28	6.28	12.57	12.57	2	0.04	0.00	0.01	0.00	0.00	24.0
8	50	-6082	235	92	0	-1012	151	6.28	6.28	12.57	12.57	2	0.06	0.00	0.02	0.00	0.00	24.0
9	50	-5996	214	-7	0	-674	137	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
10	50	-6052	-94	56	0	-877	-50	6.28	6.28	12.57	12.57	2	0.05	0.00	0.01	0.00	0.00	24.0
11	50	-6026	-100	26	0	-776	-54	6.28	6.28	12.57	12.57	2	0.04	0.00	0.01	0.00	0.00	24.0
12	50	-6053	401	58	0	-903	252	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
13	50	-6027	394	28	0	-801	248	6.28	6.28	12.57	12.57	2	0.05	0.01	0.03	0.00	0.00	24.0
14	50	-6082	87	92	0	-1004	61	6.28	6.28	12.57	12.57	2	0.06	0.00	0.01	0.00	0.00	24.0
15	50	-5996	65	-8	0	-667	47	6.28	6.28	12.57	12.57	2	0.04	0.00	0.01	0.00	0.00	24.0
16	50	-6082	235	92	0	-1012	151	6.28	6.28	12.57	12.57	2	0.06	0.00	0.02	0.00	0.00	24.0
17	50	-5996	214	-7	0	-674	137	6.28	6.28	12.57	12.57	2	0.04	0.00	0.02	0.00	0.00	24.0
18	50	-8321	-455	95	0	-1296	-267	6.28	6.28	12.57	12.57	3	0.05	0.01	0.04	0.00	0.00	24.0
19	50	-8326	1005	116	0	-1417	623	6.28	6.28	12.57	12.57	3	0.06	0.02	0.09	0.00	0.00	24.0
20	50	-8345	220	143	0	-1488	143	6.28	6.28	12.57	12.57	3	0.06	0.00	0.02	0.00	0.00	24.0
37	50	-8088	-966	72	0	-1150	-579	6.28	6.28	12.57	12.57	3	0.05	0.02	0.08	0.00	0.00	24.0
38	50	-8097	1466	106	0	-1352	904	6.28	6.28	12.57	12.57	3	0.07	0.03	0.13	0.00	0.00	24.0
39	50	-8129	157	151	0	-1470	104	6.28	6.28	12.57	12.57	3	0.05	0.00	0.02	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 92 NI 1256 NF 1259 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 19
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-19790	11	-184	0	-501	-71	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
2	0	-15260	78	-168	0	-447	-332	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
3	0	-15180	77	-86	0	-245	-328	6.28	6.28	12.57	12.57	2	0.03	0.00	0.01	0.00	0.00	24.0
4	0	-15270	-61	-198	0	-525	218	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
5	0	-15190	-62	-116	0	-323	222	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
6	0	-15350	31	-274	0	-711	-143	6.28	6.28	12.57	12.57	2	0.04	0.00	0.03	0.00	0.00	24.0
7	0	-15090	27	0	0	-36	-132	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
8	0	-15360	-11	-284	0	-734	22	6.28	6.28	12.57	12.57	2	0.04	0.00	0.03	0.00	0.00	24.0
9	0	-15090	-14	-9	0	-60	33	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
10	0	-15260	78	-168	0	-447	-332	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
11	0	-15180	77	-86	0	-245	-328	6.28	6.28	12.57	12.57	2	0.03	0.00	0.01	0.00	0.00	24.0
12	0	-15270	-61	-198	0	-525	218	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
13	0	-15190	-62	-116	0	-323	222	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
14	0	-15350	31	-274	0	-711	-143	6.28	6.28	12.57	12.57	2	0.04	0.00	0.03	0.00	0.00	24.0
15	0	-15090	27	0	0	-36	-132	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
16	0	-15360	-11	-284	0	-734	22	6.28	6.28	12.57	12.57	2	0.04	0.00	0.03	0.00	0.00	24.0
17	0	-15090	-14	-9	0	-60	33	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
18	0	-21570	228	-254	0	-657	-908	6.28	6.28	12.57	12.57	3	0.05	0.00	0.02	0.00	0.00	24.0
19	0	-21650	-205	-384	0	-988	764	6.28	6.28	12.57	12.57	3	0.05	0.01	0.03	0.00	0.00	24.0
20	0	-21460	13	-383	0	-1020	-79	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
37	0	-20670	372	-170	0	-446	-1464	6.28	6.28	12.57	12.57	3	0.08	0.01	0.03	0.00	0.00	24.0
38	0	-20810	-350	-385	0	-999	1322	6.28	6.28	12.57	12.57	3	0.07	0.01	0.03	0.00	0.00	24.0
39	0	-20490	14	-384	0	-1052	-83	6.28	6.28	12.57	12.57	3	0.04	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-19692	11	-184	0	-478	-70	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
2	12	-15185	78	-168	0	-426	-322	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
3	12	-15105	77	-86	0	-234	-318	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
4	12	-15195	-61	-198	0	-501	210	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
5	12	-15115	-62	-116	0	-309	214	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0

6	12	-15275	31	-274	0	-676	-140	6.28	6.28	12.57	12.57	2	0.04	0.00	0.03	0.00	0.00	24.0
7	12	-15015	27	0	0	-36	-128	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
8	12	-15285	-11	-284	0	-699	20	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
9	12	-15015	-14	-9	0	-58	32	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
10	12	-15185	78	-168	0	-426	-322	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
11	12	-15105	77	-86	0	-234	-318	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
12	12	-15195	-61	-198	0	-501	210	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
13	12	-15115	-62	-116	0	-309	214	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
14	12	-15275	31	-274	0	-676	-140	6.28	6.28	12.57	12.57	2	0.04	0.00	0.03	0.00	0.00	24.0
15	12	-15015	27	0	0	-36	-128	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
16	12	-15285	-11	-284	0	-699	20	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
17	12	-15015	-14	-9	0	-58	32	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
18	12	-21472	228	-254	0	-625	-880	6.28	6.28	12.57	12.57	3	0.05	0.00	0.02	0.00	0.00	24.0
19	12	-21552	-205	-384	0	-941	738	6.28	6.28	12.57	12.57	3	0.05	0.01	0.03	0.00	0.00	24.0
20	12	-21362	13	-383	0	-972	-77	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
37	12	-20572	372	-170	0	-424	-1418	6.28	6.28	12.57	12.57	3	0.07	0.01	0.03	0.00	0.00	24.0
38	12	-20712	-350	-385	0	-951	1279	6.28	6.28	12.57	12.57	3	0.07	0.01	0.03	0.00	0.00	24.0
39	12	-20392	14	-384	0	-1004	-81	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-19595	11	-184	0	-455	-69	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
2	25	-15110	78	-168	0	-405	-312	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
3	25	-15030	77	-86	0	-223	-309	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
4	25	-15120	-61	-198	0	-476	203	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
5	25	-15040	-62	-116	0	-294	206	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
6	25	-15200	31	-274	0	-642	-136	6.28	6.28	12.57	12.57	2	0.04	0.00	0.03	0.00	0.00	24.0
7	25	-14940	27	0	0	-36	-125	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
8	25	-15210	-11	-284	0	-663	19	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
9	25	-14940	-14	-9	0	-57	30	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
10	25	-15110	78	-168	0	-405	-312	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
11	25	-15030	77	-86	0	-223	-309	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
12	25	-15120	-61	-198	0	-476	203	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
13	25	-15040	-62	-116	0	-294	206	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
14	25	-15200	31	-274	0	-642	-136	6.28	6.28	12.57	12.57	2	0.04	0.00	0.03	0.00	0.00	24.0
15	25	-14940	27	0	0	-36	-125	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
16	25	-15210	-11	-284	0	-663	19	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
17	25	-14940	-14	-9	0	-57	30	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
18	25	-21375	228	-254	0	-593	-851	6.28	6.28	12.57	12.57	3	0.05	0.00	0.02	0.00	0.00	24.0
19	25	-21455	-205	-384	0	-893	713	6.28	6.28	12.57	12.57	3	0.05	0.01	0.03	0.00	0.00	24.0
20	25	-21265	13	-383	0	-924	-76	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
37	25	-20475	372	-170	0	-403	-1372	6.28	6.28	12.57	12.57	3	0.07	0.01	0.03	0.00	0.00	24.0
38	25	-20615	-350	-385	0	-903	1235	6.28	6.28	12.57	12.57	3	0.07	0.01	0.03	0.00	0.00	24.0
39	25	-20295	14	-384	0	-956	-79	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-19498	11	-184	0	-432	-67	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
2	38	-15035	78	-168	0	-384	-302	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
3	38	-14955	77	-86	0	-213	-299	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
4	38	-15045	-61	-198	0	-451	195	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
5	38	-14965	-62	-116	0	-280	198	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
6	38	-15125	31	-274	0	-608	-132	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
7	38	-14865	27	0	0	-36	-121	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
8	38	-15135	-11	-284	0	-628	17	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
9	38	-14865	-14	-9	0	-56	28	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
10	38	-15035	78	-168	0	-384	-302	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
11	38	-14955	77	-86	0	-213	-299	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
12	38	-15045	-61	-198	0	-451	195	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
13	38	-14965	-62	-116	0	-280	198	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
14	38	-15125	31	-274	0	-608	-132	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
15	38	-14865	27	0	0	-36	-121	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
16	38	-15135	-11	-284	0	-628	17	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
17	38	-14865	-14	-9	0	-56	28	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
18	38	-21278	228	-254	0	-561	-823	6.28	6.28	12.57	12.57	3	0.04	0.00	0.02	0.00	0.00	24.0
19	38	-21358	-205	-384	0	-845	687	6.28	6.28	12.57	12.57	3	0.04	0.01	0.03	0.00	0.00	24.0
20	38	-21168	13	-383	0	-877	-74	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
37	38	-20378	372	-170	0	-382	-1325	6.28	6.28	12.57	12.57	3	0.07	0.01	0.03	0.00	0.00	24.0
38	38	-20518	-350	-385	0	-854	1192	6.28	6.28	12.57	12.57	3	0.07	0.01	0.03	0.00	0.00	24.0
39	38	-20198	14	-384	0	-908	-77	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-19400	11	-184	0	-409	-66	6.28	6.28	12.57	12.57	3	0.01	0.00	0.02	0.00	0.00	24.0
2	50	-14960	78	-168	0	-363	-292	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
3	50	-14880	77	-86	0	-202	-289	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
4	50	-14970	-61	-198	0	-426	188	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
5	50	-14890	-62	-116	0	-265	191	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
6	50	-15050	31	-274	0	-573	-128	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
7	50	-14790	27	0	0	-36	-118	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
8	50	-15060	-11	-284	0	-592	16	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
9	50	-14790	-14	-9	0	-55	26	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
10	50	-14960	78	-168	0	-363	-292	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
11	50	-14880	77	-86	0	-202	-289	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
12	50	-14970	-61	-198	0	-426	188	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
13	50	-14890	-62	-116	0	-265	191	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
14	50	-15050	31	-274	0	-573	-128	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
15	50	-14790	27	0	0	-36	-118	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
16	50	-15060	-11	-284	0	-592	16	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
17	50	-14790	-14	-9	0	-55	26	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
18	50	-21180	228	-254	0	-529	-794	6.28	6.28	12.57	12.57	3	0.04	0.00	0.02	0.00	0.00	24.0
19	50	-21260	-205	-384	0	-797	662	6.28	6.28	12.57	12.57	3	0.04	0.01	0.03	0.00	0.00	24.0
20	50	-21070	13	-383	0	-829	-72	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
37	50	-20280	372	-170	0	-361	-1279	6.28	6.28	12.57	12.57	3	0.07	0.01	0.03	0.00	0.00	24.0
38	50	-20420	-350	-385	0	-806	1148	6.28	6.28	12.57	12.57	3	0.06	0.01	0.03	0.00	0.00	24.0
39	50	-20100	14	-384	0	-860	-76	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 93 NI 1259 NF 127 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 19A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-19400	11	-184	0	-409	-66	6.28	6.28	12.57	12.57	3	0.01	0.00	0.02	0.00	0.00	24.0

2	0	-14960	78	-168	0	-363	-292	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
3	0	-14880	77	-86	0	-202	-289	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
4	0	-14970	-61	-198	0	-426	188	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
5	0	-14890	-62	-116	0	-265	191	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
6	0	-15050	31	-274	0	-573	-128	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
7	0	-14790	27	0	0	-36	-118	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
8	0	-15060	-11	-284	0	-592	16	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
9	0	-14790	-14	-9	0	-55	26	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
10	0	-14960	78	-168	0	-363	-292	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
11	0	-14880	77	-86	0	-202	-289	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
12	0	-14970	-61	-198	0	-426	188	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
13	0	-14890	-62	-116	0	-265	191	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
14	0	-15050	31	-274	0	-573	-128	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
15	0	-14790	27	0	0	-36	-118	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
16	0	-15060	-11	-284	0	-592	16	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
17	0	-14790	-14	-9	0	-55	26	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
18	0	-21180	228	-254	0	-529	-794	6.28	6.28	12.57	12.57	3	0.04	0.00	0.02	0.00	0.00	24.0
19	0	-21260	-205	-384	0	-797	662	6.28	6.28	12.57	12.57	3	0.04	0.01	0.03	0.00	0.00	24.0
20	0	-21070	13	-383	0	-829	-72	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
37	0	-20280	372	-170	0	-361	-1279	6.28	6.28	12.57	12.57	3	0.07	0.01	0.03	0.00	0.00	24.0
38	0	-20420	-350	-385	0	-806	1148	6.28	6.28	12.57	12.57	3	0.06	0.01	0.03	0.00	0.00	24.0
39	0	-20100	14	-384	0	-860	-76	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-19302	11	-184	0	-385	-65	6.28	6.28	12.57	12.57	3	0.01	0.00	0.02	0.00	0.00	24.0
2	12	-14885	78	-168	0	-342	-283	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
3	12	-14805	77	-86	0	-191	-280	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
4	12	-14895	-61	-198	0	-402	180	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
5	12	-14815	-62	-116	0	-251	183	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
6	12	-14975	31	-274	0	-539	-124	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
7	12	-14715	27	0	0	-36	-114	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
8	12	-14985	-11	-284	0	-557	15	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
9	12	-14715	-14	-9	0	-54	24	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
10	12	-14885	78	-168	0	-342	-283	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
11	12	-14805	77	-86	0	-191	-280	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
12	12	-14895	-61	-198	0	-402	180	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
13	12	-14815	-62	-116	0	-251	183	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
14	12	-14975	31	-274	0	-539	-124	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
15	12	-14715	27	0	0	-36	-114	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
16	12	-14985	-11	-284	0	-557	15	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
17	12	-14715	-14	-9	0	-54	24	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
18	12	-21082	228	-254	0	-498	-766	6.28	6.28	12.57	12.57	3	0.04	0.00	0.02	0.00	0.00	24.0
19	12	-21162	-205	-384	0	-749	636	6.28	6.28	12.57	12.57	3	0.04	0.01	0.03	0.00	0.00	24.0
20	12	-20972	13	-383	0	-781	-71	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
37	12	-20182	372	-170	0	-339	-1232	6.28	6.28	12.57	12.57	3	0.06	0.01	0.03	0.00	0.00	24.0
38	12	-20322	-350	-385	0	-758	1104	6.28	6.28	12.57	12.57	3	0.06	0.01	0.03	0.00	0.00	24.0
39	12	-20002	14	-384	0	-812	-74	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-19205	11	-184	0	-362	-63	6.28	6.28	12.57	12.57	3	0.01	0.00	0.02	0.00	0.00	24.0
2	25	-14810	78	-168	0	-321	-273	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
3	25	-14730	77	-86	0	-181	-270	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
4	25	-14820	-61	-198	0	-377	172	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
5	25	-14740	-62	-116	0	-236	175	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
6	25	-14900	31	-274	0	-505	-120	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
7	25	-14640	27	0	0	-36	-111	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
8	25	-14910	-11	-284	0	-522	13	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
9	25	-14640	-14	-9	0	-53	23	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
10	25	-14810	78	-168	0	-321	-273	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
11	25	-14730	77	-86	0	-181	-270	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
12	25	-14820	-61	-198	0	-377	172	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
13	25	-14740	-62	-116	0	-236	175	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
14	25	-14900	31	-274	0	-505	-120	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
15	25	-14640	27	0	0	-36	-111	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
16	25	-14910	-11	-284	0	-522	13	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
17	25	-14640	-14	-9	0	-53	23	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
18	25	-20985	228	-254	0	-466	-737	6.28	6.28	12.57	12.57	3	0.04	0.00	0.02	0.00	0.00	24.0
19	25	-21065	-205	-384	0	-701	610	6.28	6.28	12.57	12.57	3	0.04	0.01	0.03	0.00	0.00	24.0
20	25	-20875	13	-383	0	-733	-69	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
37	25	-20085	372	-170	0	-318	-1186	6.28	6.28	12.57	12.57	3	0.06	0.01	0.03	0.00	0.00	24.0
38	25	-20225	-350	-385	0	-710	1060	6.28	6.28	12.57	12.57	3	0.06	0.01	0.03	0.00	0.00	24.0
39	25	-19905	14	-384	0	-764	-72	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-19108	11	-184	0	-339	-62	6.28	6.28	12.57	12.57	3	0.01	0.00	0.02	0.00	0.00	24.0
2	38	-14735	78	-168	0	-300	-263	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
3	38	-14655	77	-86	0	-170	-260	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
4	38	-14745	-61	-198	0	-352	165	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
5	38	-14665	-62	-116	0	-222	167	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
6	38	-14825	31	-274	0	-471	-116	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
7	38	-14565	27	0	0	-36	-107	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
8	38	-14835	-11	-284	0	-486	12	6.28	6.28	12.57	12.57	2	0.02	0.00	0.03	0.00	0.00	24.0
9	38	-14565	-14	-9	0	-52	21	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
10	38	-14735	78	-168	0	-300	-263	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
11	38	-14655	77	-86	0	-170	-260	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
12	38	-14745	-61	-198	0	-352	165	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
13	38	-14665	-62	-116	0	-222	167	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
14	38	-14825	31	-274	0	-471	-116	6.28	6.28	12.57	12.57	2	0.03	0.00	0.03	0.00	0.00	24.0
15	38	-14565	27	0	0	-36	-107	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
16	38	-14835	-11	-284	0	-486	12	6.28	6.28	12.57	12.57	2	0.02	0.00	0.03	0.00	0.00	24.0
17	38	-14565	-14	-9	0	-52	21	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
18	38	-20888	228	-254	0	-434	-709	6.28	6.28	12.57	12.57	3	0.04	0.00	0.02	0.00	0.00	24.0
19	38	-20968	-205	-384	0	-653	585	6.28	6.28	12.57	12.57	3	0.04	0.01	0.03	0.00	0.00	24.0
20	38	-20778	13	-383	0	-685	-67	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
37	38	-19988	372	-170	0	-297	-1139	6.28	6.28	12.57	12.57	3	0.06	0.01	0.03	0.00	0.00	24.0
38	38	-20128	-350	-385	0	-662	1017	6.28	6.28	12.57	12.57	3	0.06	0.01	0.03	0.00	0.00	24.0
39	38	-19808	14	-384	0	-716	-70	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-19010	11	-184	0	-316	-61	6.28	6.28	12.57	12.57	3	0.01	0.00	0.02	0.00	0.00	24.0
2	50	-14660	78	-168	0	-279	-253	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
3	50	-14580	77	-86	0	-159	-251	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
4	50	-14670	-61	-198	0	-327	157	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
5	50	-14590	-62	-116	0	-207	160	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
6	50	-14750	31	-274	0	-436	-113	6.28	6.28	12.57	12.57	2	0.02	0.00	0.03	0.00	0.00	24.0
7	50	-14490	27	0	0	-36	-104	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0

8	50	-14760	-11	-284	0	-451	10	6.28	6.28	12.57	12.57	2	0.02	0.00	0.03	0.00	0.00	24.0
9	50	-14490	-14	-9	0	-51	19	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
10	50	-14660	78	-168	0	-279	-253	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
11	50	-14580	77	-86	0	-159	-251	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
12	50	-14670	-61	-198	0	-327	157	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
13	50	-14590	-62	-116	0	-207	160	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
14	50	-14750	31	-274	0	-436	-113	6.28	6.28	12.57	12.57	2	0.02	0.00	0.03	0.00	0.00	24.0
15	50	-14490	27	0	0	-36	-104	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
16	50	-14760	-11	-284	0	-451	10	6.28	6.28	12.57	12.57	2	0.02	0.00	0.03	0.00	0.00	24.0
17	50	-14490	-14	-9	0	-51	19	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
18	50	-20790	228	-254	0	-402	-680	6.28	6.28	12.57	12.57	3	0.04	0.00	0.02	0.00	0.00	24.0
19	50	-20870	-205	-384	0	-605	559	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
20	50	-20680	13	-383	0	-637	-66	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
37	50	-19890	372	-170	0	-276	-1093	6.28	6.28	12.57	12.57	3	0.06	0.01	0.03	0.00	0.00	24.0
38	50	-20030	-350	-385	0	-614	973	6.28	6.28	12.57	12.57	3	0.05	0.01	0.03	0.00	0.00	24.0
39	50	-19710	14	-384	0	-668	-69	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 94 NI 1034 NF 1040 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 20
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-35650	124	713	0	1634	-385	6.28	6.28	12.57	12.57	3	0.06	0.01	0.05	0.00	0.00	24.0
2	0	-27250	323	578	0	1282	-1011	6.28	6.28	12.57	12.57	2	0.09	0.01	0.05	0.00	0.00	24.0
3	0	-27210	322	547	0	1308	-1008	6.28	6.28	12.57	12.57	2	0.09	0.01	0.04	0.00	0.00	24.0
4	0	-27640	-131	550	0	1206	416	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
5	0	-27600	-132	520	0	1231	419	6.28	6.28	12.57	12.57	2	0.07	0.01	0.04	0.00	0.00	24.0
6	0	-27440	165	604	0	1225	-516	6.28	6.28	12.57	12.57	2	0.07	0.01	0.05	0.00	0.00	24.0
7	0	-27290	162	502	0	1311	-504	6.28	6.28	12.57	12.57	2	0.07	0.01	0.04	0.00	0.00	24.0
8	0	-27560	29	595	0	1202	-88	6.28	6.28	12.57	12.57	2	0.05	0.01	0.05	0.00	0.00	24.0
9	0	-27410	26	494	0	1288	-76	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
10	0	-27250	323	578	0	1282	-1011	6.28	6.28	12.57	12.57	2	0.09	0.01	0.05	0.00	0.00	24.0
11	0	-27210	322	547	0	1308	-1008	6.28	6.28	12.57	12.57	2	0.09	0.01	0.04	0.00	0.00	24.0
12	0	-27640	-131	550	0	1206	416	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
13	0	-27600	-132	520	0	1231	419	6.28	6.28	12.57	12.57	2	0.07	0.01	0.04	0.00	0.00	24.0
14	0	-27440	165	604	0	1225	-516	6.28	6.28	12.57	12.57	2	0.07	0.01	0.05	0.00	0.00	24.0
15	0	-27290	162	502	0	1311	-504	6.28	6.28	12.57	12.57	2	0.07	0.01	0.04	0.00	0.00	24.0
16	0	-27560	29	595	0	1202	-88	6.28	6.28	12.57	12.57	2	0.05	0.01	0.05	0.00	0.00	24.0
17	0	-27410	26	494	0	1288	-76	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
18	0	-38760	932	1006	0	2190	-2800	6.28	6.28	12.57	12.57	3	0.14	0.02	0.07	0.00	0.00	24.0
19	0	-40600	-585	902	0	1883	1792	6.28	6.28	12.57	12.57	3	0.10	0.01	0.06	0.00	0.00	24.0
20	0	-39160	173	704	0	1533	-504	6.28	6.28	12.57	12.57	3	0.05	0.01	0.05	0.00	0.00	24.0
37	0	-36610	1420	952	0	2136	-4289	6.28	6.28	12.57	12.57	3	0.21	0.02	0.10	0.00	0.00	24.0
38	0	-39680	-1108	779	0	1625	3364	6.28	6.28	12.57	12.57	3	0.16	0.02	0.08	0.00	0.00	24.0
39	0	-37280	155	450	0	1042	-461	6.28	6.28	12.57	12.57	3	0.04	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-35552	124	713	0	1545	-369	6.28	6.28	12.57	12.57	3	0.05	0.01	0.05	0.00	0.00	24.0
2	12	-27175	323	578	0	1210	-971	6.28	6.28	12.57	12.57	2	0.08	0.01	0.05	0.00	0.00	24.0
3	12	-27135	322	547	0	1240	-968	6.28	6.28	12.57	12.57	2	0.09	0.01	0.04	0.00	0.00	24.0
4	12	-27565	-131	550	0	1137	399	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
5	12	-27525	-132	520	0	1166	403	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
6	12	-27365	165	604	0	1150	-495	6.28	6.28	12.57	12.57	2	0.06	0.01	0.05	0.00	0.00	24.0
7	12	-27215	162	502	0	1248	-484	6.28	6.28	12.57	12.57	2	0.07	0.01	0.04	0.00	0.00	24.0
8	12	-27485	29	595	0	1128	-84	6.28	6.28	12.57	12.57	2	0.05	0.01	0.05	0.00	0.00	24.0
9	12	-27335	26	494	0	1226	-73	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
10	12	-27175	323	578	0	1210	-971	6.28	6.28	12.57	12.57	2	0.08	0.01	0.05	0.00	0.00	24.0
11	12	-27135	322	547	0	1240	-968	6.28	6.28	12.57	12.57	2	0.09	0.01	0.04	0.00	0.00	24.0
12	12	-27565	-131	550	0	1137	399	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
13	12	-27525	-132	520	0	1166	403	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
14	12	-27365	165	604	0	1150	-495	6.28	6.28	12.57	12.57	2	0.06	0.01	0.05	0.00	0.00	24.0
15	12	-27215	162	502	0	1248	-484	6.28	6.28	12.57	12.57	2	0.07	0.01	0.04	0.00	0.00	24.0
16	12	-27485	29	595	0	1128	-84	6.28	6.28	12.57	12.57	2	0.05	0.01	0.05	0.00	0.00	24.0
17	12	-27335	26	494	0	1226	-73	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
18	12	-38662	932	1006	0	2064	-2684	6.28	6.28	12.57	12.57	3	0.14	0.02	0.07	0.00	0.00	24.0
19	12	-40502	-585	902	0	1770	1719	6.28	6.28	12.57	12.57	3	0.10	0.01	0.06	0.00	0.00	24.0
20	12	-39062	173	704	0	1445	-482	6.28	6.28	12.57	12.57	3	0.05	0.01	0.05	0.00	0.00	24.0
37	12	-36512	1420	952	0	2017	-4112	6.28	6.28	12.57	12.57	3	0.20	0.02	0.10	0.00	0.00	24.0
38	12	-39582	-1108	779	0	1528	3226	6.28	6.28	12.57	12.57	3	0.15	0.02	0.08	0.00	0.00	24.0
39	12	-37182	155	450	0	986	-442	6.28	6.28	12.57	12.57	3	0.04	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-35455	124	713	0	1456	-354	6.28	6.28	12.57	12.57	3	0.05	0.01	0.05	0.00	0.00	24.0
2	25	-27100	323	578	0	1138	-930	6.28	6.28	12.57	12.57	2	0.08	0.01	0.05	0.00	0.00	24.0
3	25	-27060	322	547	0	1171	-927	6.28	6.28	12.57	12.57	2	0.08	0.01	0.04	0.00	0.00	24.0
4	25	-27490	-131	550	0	1068	383	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
5	25	-27450	-132	520	0	1101	386	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
6	25	-27290	165	604	0	1074	-475	6.28	6.28	12.57	12.57	2	0.06	0.01	0.05	0.00	0.00	24.0
7	25	-27140	162	502	0	1186	-464	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
8	25	-27410	29	595	0	1053	-81	6.28	6.28	12.57	12.57	2	0.05	0.01	0.05	0.00	0.00	24.0
9	25	-27260	26	494	0	1165	-70	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
10	25	-27100	323	578	0	1138	-930	6.28	6.28	12.57	12.57	2	0.08	0.01	0.05	0.00	0.00	24.0
11	25	-27060	322	547	0	1171	-927	6.28	6.28	12.57	12.57	2	0.08	0.01	0.04	0.00	0.00	24.0
12	25	-27490	-131	550	0	1068	383	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
13	25	-27450	-132	520	0	1101	386	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
14	25	-27290	165	604	0	1074	-475	6.28	6.28	12.57	12.57	2	0.06	0.01	0.05	0.00	0.00	24.0
15	25	-27140	162	502	0	1186	-464	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
16	25	-27410	29	595	0	1053	-81	6.28	6.28	12.57	12.57	2	0.05	0.01	0.05	0.00	0.00	24.0
17	25	-27260	26	494	0	1165	-70	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
18	25	-38565	932	1006	0	1939	-2568	6.28	6.28	12.57	12.57	3	0.13	0.02	0.07	0.00	0.00	24.0
19	25	-40405	-585	902	0	1658	1646	6.28	6.28	12.57	12.57	3	0.09	0.01	0.06	0.00	0.00	24.0
20	25	-38965	173	704	0	1357	-460	6.28	6.28	12.57	12.57	3	0.05	0.01	0.05	0.00	0.00	24.0
37	25	-36415	1420	952	0	1898	-3934	6.28	6.28	12.57	12.57	3	0.19	0.02	0.10	0.00	0.00	24.0
38	25	-39485	-1108	779	0	1430	3087	6.28	6.28	12.57	12.57	3	0.15	0.02	0.08	0.00	0.00	24.0
39	25	-37085	155	450	0	930	-422	6.28	6.28	12.57	12.57	3	0.04	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-35358	124	713	0	1366	-338	6.28	6.28	12.57	12.57	3	0.05	0.01	0.05	0.00	0.00	24.0
2	38	-27025	323	578	0	1066	-890	6.28	6.28	12.57	12.57	2	0.08	0.01	0.05	0.00	0.00	24.0
3	38	-26985	322	547	0	1102	-887	6.28	6.28	12.57	12.57	2	0.08	0.01	0.04	0.00	0.00	24.0

4	38	-27415	-131	550	0	999	366	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
5	38	-27375	-132	520	0	1036	370	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
6	38	-27215	165	604	0	999	-454	6.28	6.28	12.57	12.57	2	0.06	0.01	0.05	0.00	0.00	24.0
7	38	-27065	162	502	0	1123	-443	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
8	38	-27335	29	595	0	979	-77	6.28	6.28	12.57	12.57	2	0.04	0.01	0.05	0.00	0.00	24.0
9	38	-27185	26	494	0	1103	-66	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
10	38	-27025	323	578	0	1066	-890	6.28	6.28	12.57	12.57	2	0.08	0.01	0.05	0.00	0.00	24.0
11	38	-26985	322	547	0	1102	-887	6.28	6.28	12.57	12.57	2	0.08	0.01	0.04	0.00	0.00	24.0
12	38	-27415	-131	550	0	999	366	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
13	38	-27375	-132	520	0	1036	370	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
14	38	-27215	165	604	0	999	-454	6.28	6.28	12.57	12.57	2	0.06	0.01	0.05	0.00	0.00	24.0
15	38	-27065	162	502	0	1123	-443	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
16	38	-27335	29	595	0	979	-77	6.28	6.28	12.57	12.57	2	0.04	0.01	0.05	0.00	0.00	24.0
17	38	-27185	26	494	0	1103	-66	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
18	38	-38468	932	1006	0	1813	-2451	6.28	6.28	12.57	12.57	3	0.12	0.02	0.07	0.00	0.00	24.0
19	38	-40308	-585	902	0	1545	1572	6.28	6.28	12.57	12.57	3	0.09	0.01	0.06	0.00	0.00	24.0
20	38	-38868	173	704	0	1269	-439	6.28	6.28	12.57	12.57	3	0.05	0.01	0.05	0.00	0.00	24.0
37	38	-36318	1420	952	0	1779	-3756	6.28	6.28	12.57	12.57	3	0.18	0.02	0.10	0.00	0.00	24.0
38	38	-39388	-1108	779	0	1333	2949	6.28	6.28	12.57	12.57	3	0.14	0.02	0.08	0.00	0.00	24.0
39	38	-36988	155	450	0	873	-403	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-35260	124	713	0	1277	-323	6.28	6.28	12.57	12.57	3	0.04	0.01	0.05	0.00	0.00	24.0
2	50	-26950	323	578	0	993	-850	6.28	6.28	12.57	12.57	2	0.07	0.01	0.05	0.00	0.00	24.0
3	50	-26910	322	547	0	1034	-847	6.28	6.28	12.57	12.57	2	0.07	0.01	0.04	0.00	0.00	24.0
4	50	-27340	-131	550	0	930	350	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
5	50	-27300	-132	520	0	972	353	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
6	50	-27140	165	604	0	924	-434	6.28	6.28	12.57	12.57	2	0.05	0.01	0.05	0.00	0.00	24.0
7	50	-26990	162	502	0	1060	-423	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
8	50	-27260	29	595	0	905	-74	6.28	6.28	12.57	12.57	2	0.04	0.01	0.05	0.00	0.00	24.0
9	50	-27110	26	494	0	1041	-63	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
10	50	-26950	323	578	0	993	-850	6.28	6.28	12.57	12.57	2	0.07	0.01	0.05	0.00	0.00	24.0
11	50	-26910	322	547	0	1034	-847	6.28	6.28	12.57	12.57	2	0.07	0.01	0.04	0.00	0.00	24.0
12	50	-27340	-131	550	0	930	350	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
13	50	-27300	-132	520	0	972	353	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
14	50	-27140	165	604	0	924	-434	6.28	6.28	12.57	12.57	2	0.05	0.01	0.05	0.00	0.00	24.0
15	50	-26990	162	502	0	1060	-423	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
16	50	-27260	29	595	0	905	-74	6.28	6.28	12.57	12.57	2	0.04	0.01	0.05	0.00	0.00	24.0
17	50	-27110	26	494	0	1041	-63	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
18	50	-38370	932	1006	0	1687	-2335	6.28	6.28	12.57	12.57	3	0.12	0.02	0.07	0.00	0.00	24.0
19	50	-40210	-585	902	0	1432	1499	6.28	6.28	12.57	12.57	3	0.08	0.01	0.06	0.00	0.00	24.0
20	50	-38770	173	704	0	1181	-417	6.28	6.28	12.57	12.57	3	0.04	0.01	0.05	0.00	0.00	24.0
37	50	-36220	1420	952	0	1660	-3579	6.28	6.28	12.57	12.57	3	0.17	0.02	0.10	0.00	0.00	24.0
38	50	-39290	-1108	779	0	1235	2811	6.28	6.28	12.57	12.57	3	0.13	0.02	0.08	0.00	0.00	24.0
39	50	-36890	155	450	0	817	-383	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 95 NI 1040 NF 301 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 20A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-35260	124	713	0	1277	-323	6.28	6.28	12.57	12.57	3	0.04	0.01	0.05	0.00	0.00	24.0
2	0	-26950	323	578	0	993	-850	6.28	6.28	12.57	12.57	2	0.07	0.01	0.05	0.00	0.00	24.0
3	0	-26910	322	547	0	1034	-847	6.28	6.28	12.57	12.57	2	0.07	0.01	0.04	0.00	0.00	24.0
4	0	-27340	-131	550	0	930	350	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
5	0	-27300	-132	520	0	972	353	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
6	0	-27140	165	604	0	924	-434	6.28	6.28	12.57	12.57	2	0.05	0.01	0.05	0.00	0.00	24.0
7	0	-26990	162	502	0	1060	-423	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
8	0	-27260	29	595	0	905	-74	6.28	6.28	12.57	12.57	2	0.04	0.01	0.05	0.00	0.00	24.0
9	0	-27110	26	494	0	1041	-63	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
10	0	-26950	323	578	0	993	-850	6.28	6.28	12.57	12.57	2	0.07	0.01	0.05	0.00	0.00	24.0
11	0	-26910	322	547	0	1034	-847	6.28	6.28	12.57	12.57	2	0.07	0.01	0.04	0.00	0.00	24.0
12	0	-27340	-131	550	0	930	350	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
13	0	-27300	-132	520	0	972	353	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
14	0	-27140	165	604	0	924	-434	6.28	6.28	12.57	12.57	2	0.05	0.01	0.05	0.00	0.00	24.0
15	0	-26990	162	502	0	1060	-423	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
16	0	-27260	29	595	0	905	-74	6.28	6.28	12.57	12.57	2	0.04	0.01	0.05	0.00	0.00	24.0
17	0	-27110	26	494	0	1041	-63	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
18	0	-38370	932	1006	0	1687	-2335	6.28	6.28	12.57	12.57	3	0.12	0.02	0.07	0.00	0.00	24.0
19	0	-40210	-585	902	0	1432	1499	6.28	6.28	12.57	12.57	3	0.08	0.01	0.06	0.00	0.00	24.0
20	0	-38770	173	704	0	1181	-417	6.28	6.28	12.57	12.57	3	0.04	0.01	0.05	0.00	0.00	24.0
37	0	-36220	1420	952	0	1660	-3579	6.28	6.28	12.57	12.57	3	0.17	0.02	0.10	0.00	0.00	24.0
38	0	-39290	-1108	779	0	1235	2811	6.28	6.28	12.57	12.57	3	0.13	0.02	0.08	0.00	0.00	24.0
39	0	-36890	155	450	0	817	-383	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-35162	124	713	0	1188	-307	6.28	6.28	12.57	12.57	3	0.04	0.01	0.05	0.00	0.00	24.0
2	12	-26875	323	578	0	921	-809	6.28	6.28	12.57	12.57	2	0.07	0.01	0.05	0.00	0.00	24.0
3	12	-26835	322	547	0	966	-806	6.28	6.28	12.57	12.57	2	0.07	0.01	0.04	0.00	0.00	24.0
4	12	-27265	-131	550	0	862	334	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
5	12	-27225	-132	520	0	906	337	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
6	12	-27065	165	604	0	848	-413	6.28	6.28	12.57	12.57	2	0.05	0.01	0.05	0.00	0.00	24.0
7	12	-26915	162	502	0	997	-403	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
8	12	-27185	29	595	0	830	-70	6.28	6.28	12.57	12.57	2	0.04	0.01	0.05	0.00	0.00	24.0
9	12	-27035	26	494	0	979	-60	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
10	12	-26875	323	578	0	921	-809	6.28	6.28	12.57	12.57	2	0.07	0.01	0.05	0.00	0.00	24.0
11	12	-26835	322	547	0	966	-806	6.28	6.28	12.57	12.57	2	0.07	0.01	0.04	0.00	0.00	24.0
12	12	-27265	-131	550	0	862	334	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
13	12	-27225	-132	520	0	906	337	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
14	12	-27065	165	604	0	848	-413	6.28	6.28	12.57	12.57	2	0.05	0.01	0.05	0.00	0.00	24.0
15	12	-26915	162	502	0	997	-403	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
16	12	-27185	29	595	0	830	-70	6.28	6.28	12.57	12.57	2	0.04	0.01	0.05	0.00	0.00	24.0
17	12	-27035	26	494	0	979	-60	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
18	12	-38272	932	1006	0	1561	-2218	6.28	6.28	12.57	12.57	3	0.11	0.02	0.07	0.00	0.00	24.0
19	12	-40112	-585	902	0	1319	1426	6.28	6.28	12.57	12.57	3	0.08	0.01	0.06	0.00	0.00	24.0
20	12	-38672	173	704	0	1093	-396	6.28	6.28	12.57	12.57	3	0.04	0.01	0.05	0.00	0.00	24.0
37	12	-36122	1420	952	0	1541	-3402	6.28	6.28	12.57	12.57	3	0.16	0.02	0.10	0.00	0.00	24.0
38	12	-39192	-1108	779	0	1138	2673	6.28	6.28	12.57	12.57	3	0.13	0.02	0.08	0.00	0.00	24.0
39	12	-36792	155	450	0	761	-364	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-35065	124	713	0	1099	-292	6.28	6.28	12.57	12.57	3	0.04	0.01	0.05	0.00	0.00	24.0
2	25	-26800	323	578	0	849	-769	6.28	6.28	12.57	12.57	2	0.06	0.01	0.05	0.00	0.00	24.0
3	25	-26760	322	547	0	897	-766	6.28	6.28	12.57	12.57	2	0.07	0.01	0.04	0.00	0.00	24.0
4	25	-27190	-131	550	0	793	317	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
5	25	-27150	-132	520	0	842	320	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
6	25	-26990	165	604	0	773	-392	6.28	6.28	12.57	12.57	2	0.05	0.01	0.05	0.00	0.00	24.0
7	25	-26840	162	502	0	934	-382	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
8	25	-27110	29	595	0	756	-66	6.28	6.28	12.57	12.57	2	0.03	0.01	0.05	0.00	0.00	24.0
9	25	-26960	26	494	0	918	-57	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
10	25	-26800	323	578	0	849	-769	6.28	6.28	12.57	12.57	2	0.06	0.01	0.05	0.00	0.00	24.0
11	25	-26760	322	547	0	897	-766	6.28	6.28	12.57	12.57	2	0.07	0.01	0.04	0.00	0.00	24.0
12	25	-27190	-131	550	0	793	317	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
13	25	-27150	-132	520	0	842	320	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
14	25	-26990	165	604	0	773	-392	6.28	6.28	12.57	12.57	2	0.05	0.01	0.05	0.00	0.00	24.0
15	25	-26840	162	502	0	934	-382	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
16	25	-27110	29	595	0	756	-66	6.28	6.28	12.57	12.57	2	0.03	0.01	0.05	0.00	0.00	24.0
17	25	-26960	26	494	0	918	-57	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
18	25	-38175	932	1006	0	1436	-2102	6.28	6.28	12.57	12.57	3	0.10	0.02	0.07	0.00	0.00	24.0
19	25	-40015	-585	902	0	1207	1353	6.28	6.28	12.57	12.57	3	0.07	0.01	0.06	0.00	0.00	24.0
20	25	-38575	173	704	0	1005	-374	6.28	6.28	12.57	12.57	3	0.04	0.01	0.05	0.00	0.00	24.0
37	25	-36025	1420	952	0	1422	-3224	6.28	6.28	12.57	12.57	3	0.15	0.02	0.10	0.00	0.00	24.0
38	25	-39095	-1108	779	0	1040	2534	6.28	6.28	12.57	12.57	3	0.12	0.02	0.08	0.00	0.00	24.0
39	25	-36695	155	450	0	705	-345	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-34968	124	713	0	1010	-276	6.28	6.28	12.57	12.57	3	0.04	0.01	0.05	0.00	0.00	24.0
2	38	-26725	323	578	0	777	-729	6.28	6.28	12.57	12.57	2	0.06	0.01	0.05	0.00	0.00	24.0
3	38	-26685	322	547	0	829	-726	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
4	38	-27115	-131	550	0	724	301	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
5	38	-27075	-132	520	0	777	304	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
6	38	-26915	165	604	0	697	-372	6.28	6.28	12.57	12.57	2	0.04	0.01	0.05	0.00	0.00	24.0
7	38	-26765	162	502	0	872	-362	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
8	38	-27035	29	595	0	681	-63	6.28	6.28	12.57	12.57	2	0.03	0.01	0.05	0.00	0.00	24.0
9	38	-26885	26	494	0	856	-53	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
10	38	-26725	323	578	0	777	-729	6.28	6.28	12.57	12.57	2	0.06	0.01	0.05	0.00	0.00	24.0
11	38	-26685	322	547	0	829	-726	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
12	38	-27115	-131	550	0	724	301	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
13	38	-27075	-132	520	0	777	304	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
14	38	-26915	165	604	0	697	-372	6.28	6.28	12.57	12.57	2	0.04	0.01	0.05	0.00	0.00	24.0
15	38	-26765	162	502	0	872	-362	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
16	38	-27035	29	595	0	681	-63	6.28	6.28	12.57	12.57	2	0.03	0.01	0.05	0.00	0.00	24.0
17	38	-26885	26	494	0	856	-53	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
18	38	-38078	932	1006	0	1310	-1986	6.28	6.28	12.57	12.57	3	0.10	0.02	0.07	0.00	0.00	24.0
19	38	-39918	-585	902	0	1094	1280	6.28	6.28	12.57	12.57	3	0.07	0.01	0.06	0.00	0.00	24.0
20	38	-38478	173	704	0	917	-352	6.28	6.28	12.57	12.57	3	0.03	0.01	0.05	0.00	0.00	24.0
37	38	-35928	1420	952	0	1303	-3046	6.28	6.28	12.57	12.57	3	0.15	0.02	0.10	0.00	0.00	24.0
38	38	-38998	-1108	779	0	943	2396	6.28	6.28	12.57	12.57	3	0.11	0.02	0.08	0.00	0.00	24.0
39	38	-36598	155	450	0	648	-325	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-34870	124	713	0	921	-261	6.28	6.28	12.57	12.57	3	0.03	0.01	0.05	0.00	0.00	24.0
2	50	-26650	323	578	0	705	-688	6.28	6.28	12.57	12.57	2	0.06	0.01	0.05	0.00	0.00	24.0
3	50	-26610	322	547	0	761	-685	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
4	50	-27040	-131	550	0	655	284	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
5	50	-27000	-132	520	0	711	287	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
6	50	-26840	165	604	0	622	-351	6.28	6.28	12.57	12.57	2	0.04	0.01	0.05	0.00	0.00	24.0
7	50	-26690	162	502	0	809	-342	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
8	50	-26960	29	595	0	607	-59	6.28	6.28	12.57	12.57	2	0.03	0.01	0.05	0.00	0.00	24.0
9	50	-26810	26	494	0	794	-50	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
10	50	-26650	323	578	0	705	-688	6.28	6.28	12.57	12.57	2	0.06	0.01	0.05	0.00	0.00	24.0
11	50	-26610	322	547	0	761	-685	6.28	6.28	12.57	12.57	2	0.06	0.01	0.04	0.00	0.00	24.0
12	50	-27040	-131	550	0	655	284	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
13	50	-27000	-132	520	0	711	287	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
14	50	-26840	165	604	0	622	-351	6.28	6.28	12.57	12.57	2	0.04	0.01	0.05	0.00	0.00	24.0
15	50	-26690	162	502	0	809	-342	6.28	6.28	12.57	12.57	2	0.05	0.01	0.04	0.00	0.00	24.0
16	50	-26960	29	595	0	607	-59	6.28	6.28	12.57	12.57	2	0.03	0.01	0.05	0.00	0.00	24.0
17	50	-26810	26	494	0	794	-50	6.28	6.28	12.57	12.57	2	0.04	0.01	0.04	0.00	0.00	24.0
18	50	-37980	932	1006	0	1184	-1869	6.28	6.28	12.57	12.57	3	0.09	0.02	0.07	0.00	0.00	24.0
19	50	-39820	-585	902	0	981	1207	6.28	6.28	12.57	12.57	3	0.06	0.01	0.06	0.00	0.00	24.0
20	50	-38380	173	704	0	829	-331	6.28	6.28	12.57	12.57	3	0.03	0.01	0.05	0.00	0.00	24.0
37	50	-35830	1420	952	0	1184	-2869	6.28	6.28	12.57	12.57	3	0.14	0.02	0.10	0.00	0.00	24.0
38	50	-38900	-1108	779	0	846	2257	6.28	6.28	12.57	12.57	3	0.11	0.02	0.08	0.00	0.00	24.0
39	50	-36500	155	450	0	592	-306	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 96 NI 1352 NF 1355 SEZ. Rp B= 0.400 H= 0.600 (pilastro)
PIL. NUM. 21
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m			cmq				Fx,M	Bielle	V,Mx		cmq/m	cm

1	0	-12730	668	718	0	1449	-2024	12.57	12.57	6.28	6.28	3	0.10	0.01	0.06	0.00	0.00	24.0
2	0	-9713	905	539	0	1088	-2696	12.57	12.57	6.28	6.28	2	0.17	0.02	0.09	0.00	0.00	24.0
3	0	-9846	909	580	0	1180	-2704	12.57	12.57	6.28	6.28	2	0.18	0.02	0.09	0.00	0.00	24.0
4	0	-9733	120	526	0	1050	-409	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
5	0	-9866	123	566	0	1142	-417	12.57	12.57	6.28	6.28	2	0.08	0.01	0.05	0.00	0.00	24.0
6	0	-9564	626	487	0	966	-1886	12.57	12.57	6.28	6.28	2	0.13	0.01	0.06	0.00	0.00	24.0
7	0	-10010	638	622	0	1275	-1913	12.57	12.57	6.28	6.28	2	0.14	0.01	0.06	0.00	0.00	24.0
8	0	-9571	391	483	0	955	-1200	12.57	12.57	6.28	6.28	2	0.10	0.01	0.04	0.00	0.00	24.0
9	0	-10010	402	618	0	1264	-1227	12.57	12.57	6.28	6.28	2	0.11	0.01	0.06	0.00	0.00	24.0
10	0	-9713	905	539	0	1088	-2696	12.57	12.57	6.28	6.28	2	0.17	0.02	0.09	0.00	0.00	24.0
11	0	-9846	909	580	0	1180	-2704	12.57	12.57	6.28	6.28	2	0.18	0.02	0.09	0.00	0.00	24.0
12	0	-9733	120	526	0	1050	-409	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
13	0	-9866	123	566	0	1142	-417	12.57	12.57	6.28	6.28	2	0.08	0.01	0.05	0.00	0.00	24.0
14	0	-9564	626	487	0	966	-1886	12.57	12.57	6.28	6.28	2	0.13	0.01	0.06	0.00	0.00	24.0
15	0	-10010	638	622	0	1275	-1913	12.57	12.57	6.28	6.28	2	0.14	0.01	0.06	0.00	0.00	24.0
16	0	-9571	391	483	0	955	-1200	12.57	12.57	6.28	6.28	2	0.10	0.01	0.04	0.00	0.00	24.0
17	0	-10010	402	618	0	1264	-1227	12.57	12.57	6.28	6.28	2	0.11	0.01	0.06	0.00	0.00	24.0
18	0	-13140	2609	820	0	1695	-7621	12.57	12.57	6.28	6.28	3	0.29	0.04	0.25	0.00	0.00	24.0
19	0	-13190	-38	759	0	1530	62	12.57	12.57	6.28	6.28	3	0.08	0.01	0.07	0.00	0.00	24.0
20	0	-13230	1202	749	0	1491	-3540	12.57	12.57	6.28	6.28	3	0.15	0.02	0.11	0.00	0.00	24.0
37	0	-12880	3288	807	0	1679	-9604	12.57	12.57	6.28	6.28	3	0.36	0.06	0.31	0.00	0.00	24.0

38	0	-12970	-1124	706	0	1404	3202	12.57	12.57	6.28	6.28	3	0.14	0.02	0.11	0.00	0.00	24.0
39	0	-13020	942	690	0	1338	-2801	12.57	12.57	6.28	6.28	3	0.12	0.02	0.09	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-12632	668	718	0	1359	-1940	12.57	12.57	6.28	6.28	3	0.10	0.01	0.06	0.00	0.00	24.0
2	12	-9638	905	539	0	1020	-2583	12.57	12.57	6.28	6.28	2	0.17	0.02	0.09	0.00	0.00	24.0
3	12	-9771	909	580	0	1108	-2590	12.57	12.57	6.28	6.28	2	0.17	0.02	0.09	0.00	0.00	24.0
4	12	-9658	120	526	0	984	-394	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
5	12	-9791	123	566	0	1071	-402	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
6	12	-9489	626	487	0	905	-1808	12.57	12.57	6.28	6.28	2	0.12	0.01	0.06	0.00	0.00	24.0
7	12	-9934	638	622	0	1197	-1834	12.57	12.57	6.28	6.28	2	0.14	0.01	0.06	0.00	0.00	24.0
8	12	-9496	391	483	0	894	-1151	12.57	12.57	6.28	6.28	2	0.09	0.01	0.04	0.00	0.00	24.0
9	12	-9936	402	618	0	1187	-1177	12.57	12.57	6.28	6.28	2	0.11	0.01	0.06	0.00	0.00	24.0
10	12	-9638	905	539	0	1020	-2583	12.57	12.57	6.28	6.28	2	0.17	0.02	0.09	0.00	0.00	24.0
11	12	-9771	909	580	0	1108	-2590	12.57	12.57	6.28	6.28	2	0.17	0.02	0.09	0.00	0.00	24.0
12	12	-9658	120	526	0	984	-394	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
13	12	-9791	123	566	0	1071	-402	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
14	12	-9489	626	487	0	905	-1808	12.57	12.57	6.28	6.28	2	0.12	0.01	0.06	0.00	0.00	24.0
15	12	-9934	638	622	0	1197	-1834	12.57	12.57	6.28	6.28	2	0.14	0.01	0.06	0.00	0.00	24.0
16	12	-9496	391	483	0	894	-1151	12.57	12.57	6.28	6.28	2	0.09	0.01	0.04	0.00	0.00	24.0
17	12	-9936	402	618	0	1187	-1177	12.57	12.57	6.28	6.28	2	0.11	0.01	0.06	0.00	0.00	24.0
18	12	-13042	2609	820	0	1592	-7295	12.57	12.57	6.28	6.28	3	0.28	0.04	0.25	0.00	0.00	24.0
19	12	-13092	-38	759	0	1435	57	12.57	12.57	6.28	6.28	3	0.08	0.01	0.07	0.00	0.00	24.0
20	12	-13132	1202	749	0	1397	-3390	12.57	12.57	6.28	6.28	3	0.14	0.02	0.11	0.00	0.00	24.0
37	12	-12782	3288	807	0	1578	-9193	12.57	12.57	6.28	6.28	3	0.35	0.06	0.32	0.00	0.00	24.0
38	12	-12872	-1124	706	0	1316	3062	12.57	12.57	6.28	6.28	3	0.13	0.02	0.11	0.00	0.00	24.0
39	12	-12922	942	690	0	1252	-2683	12.57	12.57	6.28	6.28	3	0.12	0.02	0.09	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-12535	668	718	0	1270	-1856	12.57	12.57	6.28	6.28	3	0.09	0.01	0.06	0.00	0.00	24.0
2	25	-9563	905	539	0	953	-2469	12.57	12.57	6.28	6.28	2	0.16	0.02	0.09	0.00	0.00	24.0
3	25	-9696	909	580	0	1035	-2477	12.57	12.57	6.28	6.28	2	0.16	0.02	0.09	0.00	0.00	24.0
4	25	-9583	120	526	0	918	-379	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
5	25	-9716	123	566	0	1001	-386	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
6	25	-9414	626	487	0	844	-1730	12.57	12.57	6.28	6.28	2	0.12	0.01	0.06	0.00	0.00	24.0
7	25	-9859	638	622	0	1120	-1754	12.57	12.57	6.28	6.28	2	0.13	0.01	0.06	0.00	0.00	24.0
8	25	-9421	391	483	0	834	-1102	12.57	12.57	6.28	6.28	2	0.09	0.01	0.04	0.00	0.00	24.0
9	25	-9862	402	618	0	1109	-1126	12.57	12.57	6.28	6.28	2	0.10	0.01	0.05	0.00	0.00	24.0
10	25	-9563	905	539	0	953	-2469	12.57	12.57	6.28	6.28	2	0.16	0.02	0.09	0.00	0.00	24.0
11	25	-9696	909	580	0	1035	-2477	12.57	12.57	6.28	6.28	2	0.16	0.02	0.09	0.00	0.00	24.0
12	25	-9583	120	526	0	918	-379	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
13	25	-9716	123	566	0	1001	-386	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
14	25	-9414	626	487	0	844	-1730	12.57	12.57	6.28	6.28	2	0.12	0.01	0.06	0.00	0.00	24.0
15	25	-9859	638	622	0	1120	-1754	12.57	12.57	6.28	6.28	2	0.13	0.01	0.06	0.00	0.00	24.0
16	25	-9421	391	483	0	834	-1102	12.57	12.57	6.28	6.28	2	0.09	0.01	0.04	0.00	0.00	24.0
17	25	-9862	402	618	0	1109	-1126	12.57	12.57	6.28	6.28	2	0.10	0.01	0.05	0.00	0.00	24.0
18	25	-12945	2609	820	0	1490	-6969	12.57	12.57	6.28	6.28	3	0.27	0.04	0.25	0.00	0.00	24.0
19	25	-12995	-38	759	0	1340	53	12.57	12.57	6.28	6.28	3	0.07	0.01	0.07	0.00	0.00	24.0
20	25	-13035	1202	749	0	1304	-3240	12.57	12.57	6.28	6.28	3	0.14	0.02	0.11	0.00	0.00	24.0
37	25	-12685	3288	807	0	1477	-8782	12.57	12.57	6.28	6.28	3	0.33	0.06	0.32	0.00	0.00	24.0
38	25	-12775	-1124	706	0	1227	2921	12.57	12.57	6.28	6.28	3	0.12	0.02	0.11	0.00	0.00	24.0
39	25	-12825	942	690	0	1166	-2565	12.57	12.57	6.28	6.28	3	0.11	0.02	0.09	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	37	-12438	668	718	0	1180	-1773	12.57	12.57	6.28	6.28	3	0.09	0.01	0.06	0.00	0.00	24.0
2	37	-9488	905	539	0	885	-2356	12.57	12.57	6.28	6.28	2	0.15	0.02	0.09	0.00	0.00	24.0
3	37	-9621	909	580	0	963	-2363	12.57	12.57	6.28	6.28	2	0.15	0.02	0.09	0.00	0.00	24.0
4	37	-9508	120	526	0	853	-364	12.57	12.57	6.28	6.28	2	0.06	0.01	0.05	0.00	0.00	24.0
5	37	-9641	123	566	0	930	-371	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
6	37	-9339	626	487	0	784	-1651	12.57	12.57	6.28	6.28	2	0.11	0.01	0.06	0.00	0.00	24.0
7	37	-9783	638	622	0	1042	-1675	12.57	12.57	6.28	6.28	2	0.12	0.01	0.06	0.00	0.00	24.0
8	37	-9346	391	483	0	774	-1053	12.57	12.57	6.28	6.28	2	0.08	0.01	0.04	0.00	0.00	24.0
9	37	-9789	402	618	0	1032	-1076	12.57	12.57	6.28	6.28	2	0.10	0.01	0.05	0.00	0.00	24.0
10	37	-9488	905	539	0	885	-2356	12.57	12.57	6.28	6.28	2	0.15	0.02	0.09	0.00	0.00	24.0
11	37	-9621	909	580	0	963	-2363	12.57	12.57	6.28	6.28	2	0.15	0.02	0.09	0.00	0.00	24.0
12	37	-9508	120	526	0	853	-364	12.57	12.57	6.28	6.28	2	0.06	0.01	0.05	0.00	0.00	24.0
13	37	-9641	123	566	0	930	-371	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
14	37	-9339	626	487	0	784	-1651	12.57	12.57	6.28	6.28	2	0.11	0.01	0.06	0.00	0.00	24.0
15	37	-9783	638	622	0	1042	-1675	12.57	12.57	6.28	6.28	2	0.12	0.01	0.06	0.00	0.00	24.0
16	37	-9346	391	483	0	774	-1053	12.57	12.57	6.28	6.28	2	0.08	0.01	0.04	0.00	0.00	24.0
17	37	-9789	402	618	0	1032	-1076	12.57	12.57	6.28	6.28	2	0.10	0.01	0.05	0.00	0.00	24.0
18	37	-12848	2609	820	0	1388	-6643	12.57	12.57	6.28	6.28	3	0.25	0.04	0.25	0.00	0.00	24.0
19	37	-12898	-38	759	0	1245	48	12.57	12.57	6.28	6.28	3	0.07	0.01	0.07	0.00	0.00	24.0
20	37	-12938	1202	749	0	1210	-3089	12.57	12.57	6.28	6.28	3	0.13	0.02	0.11	0.00	0.00	24.0
37	37	-12588	3288	807	0	1376	-8371	12.57	12.57	6.28	6.28	3	0.31	0.06	0.32	0.00	0.00	24.0
38	37	-12678	-1124	706	0	1138	2781	12.57	12.57	6.28	6.28	3	0.12	0.02	0.11	0.00	0.00	24.0
39	37	-12728	942	690	0	1080	-2448	12.57	12.57	6.28	6.28	3	0.11	0.02	0.09	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-12340	668	718	0	1090	-1689	12.57	12.57	6.28	6.28	3	0.08	0.01	0.06	0.00	0.00	24.0
2	50	-9413	905	539	0	818	-2243	12.57	12.57	6.28	6.28	2	0.14	0.02	0.09	0.00	0.00	24.0
3	50	-9546	909	580	0	890	-2250	12.57	12.57	6.28	6.28	2	0.14	0.02	0.09	0.00	0.00	24.0
4	50	-9433	120	526	0	787	-349	12.57	12.57	6.28	6.28	2	0.06	0.01	0.05	0.00	0.00	24.0
5	50	-9566	123	566	0	859	-356	12.57	12.57	6.28	6.28	2	0.06	0.01	0.05	0.00	0.00	24.0
6	50	-9264	626	487	0	723	-1573	12.57	12.57	6.28	6.28	2	0.11	0.01	0.06	0.00	0.00	24.0
7	50	-9708	638	622	0	964	-1595	12.57	12.57	6.28	6.28	2	0.12	0.01	0.06	0.00	0.00	24.0
8	50	-9271	391	483	0	713	-1004	12.57	12.57	6.28	6.28	2	0.08	0.01	0.04	0.00	0.00	24.0
9	50	-9715	402	618	0	955	-1026	12.57	12.57	6.28	6.28	2	0.09	0.01	0.05	0.00	0.00	24.0
10	50	-9413	905	539	0	818	-2243	12.57	12.57	6.28	6.28	2	0.14	0.02	0.09	0.00	0.00	24.0
11	50	-9546	909	580	0	890	-2250	12.57	12.57	6.28	6.28	2	0.14	0.02	0.09	0.00	0.00	24.0
12	50	-9433	120	526	0	787	-349	12.57	12.57	6.28	6.28	2	0.06	0.01	0.05	0.00	0.00	24.0
13	50	-9566	123	566	0	859	-356	12.57	12.57	6.28	6.28	2	0.06	0.01	0.05	0.00	0.00	24.0
14	50	-9264	626	487	0	723	-1573	12.57	12.57	6.28	6.28	2	0.11	0.01	0.06	0.00	0.00	24.0
15	50	-9708	638	622	0	964	-1595	12.57	12.57	6.28	6.28	2	0.12	0.01	0.06	0.00	0.00	24.0
16	50	-9271	391	483	0	713	-1004	12.57	12.57	6.28	6.28	2	0.08	0.01	0.04	0.00	0.00	24.0
17	50	-9715	402	618	0	955	-1026	12.57	12.57	6.28	6.28	2	0.09	0.01	0.05	0.00	0.00	24.0
18	50	-12750	2609	820	0	1285	-6317	12.57	12.57	6.28	6.28	3	0.24	0.04	0.25	0.00	0.00	24.0
19	50	-12800	-38	759	0	1150	43	12.57	12.57	6.28	6.28	3	0.06	0.01	0.07	0.00	0.00	24.0
20	50	-12840	1202	749	0	1116	-2939	12.57	12.57	6.28	6.28	3	0.12	0.02	0.12	0.00	0.00	24.0
37	50	-12490	3288	807	0	1275	-7960	12.57	12.57	6.28	6.28	3	0.30	0.06	0.32	0.00	0.00	24.0
38	50	-12580	-1124	706	0	1050	2640	12.57	12.57	6.28	6.28	3	0.11	0.02	0.11	0.00	0.00	24.0
39	50	-12630	942	690	0	994	-2330	12.57	12.57	6.28	6.28	3	0.10	0.02	0.09	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 97 NI 1355 NF 172 SEZ. Rp B= 0.400 H= 0.600 (pilastro)

PIL. NUM. 21A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-12340	668	718	0	1090	-1689	12.57	12.57	6.28	6.28	3	0.08	0.01	0.06	0.00	0.00	24.0
2	0	-9413	905	539	0	818	-2243	12.57	12.57	6.28	6.28	2	0.14	0.02	0.09	0.00	0.00	24.0
3	0	-9546	909	580	0	890	-2250	12.57	12.57	6.28	6.28	2	0.14	0.02	0.09	0.00	0.00	24.0
4	0	-9433	120	526	0	787	-349	12.57	12.57	6.28	6.28	2	0.06	0.01	0.05	0.00	0.00	24.0
5	0	-9566	123	566	0	859	-356	12.57	12.57	6.28	6.28	2	0.06	0.01	0.05	0.00	0.00	24.0
6	0	-9264	626	487	0	723	-1573	12.57	12.57	6.28	6.28	2	0.11	0.01	0.06	0.00	0.00	24.0
7	0	-9708	638	622	0	964	-1595	12.57	12.57	6.28	6.28	2	0.12	0.01	0.06	0.00	0.00	24.0
8	0	-9271	391	483	0	713	-1004	12.57	12.57	6.28	6.28	2	0.08	0.01	0.04	0.00	0.00	24.0
9	0	-9715	402	618	0	955	-1026	12.57	12.57	6.28	6.28	2	0.09	0.01	0.05	0.00	0.00	24.0
10	0	-9413	905	539	0	818	-2243	12.57	12.57	6.28	6.28	2	0.14	0.02	0.09	0.00	0.00	24.0
11	0	-9546	909	580	0	890	-2250	12.57	12.57	6.28	6.28	2	0.14	0.02	0.09	0.00	0.00	24.0
12	0	-9433	120	526	0	787	-349	12.57	12.57	6.28	6.28	2	0.06	0.01	0.05	0.00	0.00	24.0
13	0	-9566	123	566	0	859	-356	12.57	12.57	6.28	6.28	2	0.06	0.01	0.05	0.00	0.00	24.0
14	0	-9264	626	487	0	723	-1573	12.57	12.57	6.28	6.28	2	0.11	0.01	0.06	0.00	0.00	24.0
15	0	-9708	638	622	0	964	-1595	12.57	12.57	6.28	6.28	2	0.12	0.01	0.06	0.00	0.00	24.0
16	0	-9271	391	483	0	713	-1004	12.57	12.57	6.28	6.28	2	0.08	0.01	0.04	0.00	0.00	24.0
17	0	-9715	402	618	0	955	-1026	12.57	12.57	6.28	6.28	2	0.09	0.01	0.05	0.00	0.00	24.0
18	0	-12750	2609	820	0	1285	-6317	12.57	12.57	6.28	6.28	3	0.24	0.04	0.25	0.00	0.00	24.0
19	0	-12800	-38	759	0	1150	43	12.57	12.57	6.28	6.28	3	0.06	0.01	0.07	0.00	0.00	24.0
20	0	-12840	1202	749	0	1116	-2939	12.57	12.57	6.28	6.28	3	0.12	0.02	0.12	0.00	0.00	24.0
37	0	-12490	3288	807	0	1275	-7960	12.57	12.57	6.28	6.28	3	0.30	0.06	0.32	0.00	0.00	24.0
38	0	-12580	-1124	706	0	1050	2640	12.57	12.57	6.28	6.28	3	0.11	0.02	0.11	0.00	0.00	24.0
39	0	-12630	942	690	0	994	-2330	12.57	12.57	6.28	6.28	3	0.10	0.02	0.09	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-12242	668	718	0	1000	-1606	12.57	12.57	6.28	6.28	3	0.08	0.01	0.06	0.00	0.00	24.0
2	12	-9338	905	539	0	750	-2130	12.57	12.57	6.28	6.28	2	0.13	0.02	0.09	0.00	0.00	24.0
3	12	-9471	909	580	0	818	-2136	12.57	12.57	6.28	6.28	2	0.14	0.02	0.09	0.00	0.00	24.0
4	12	-9358	120	526	0	721	-334	12.57	12.57	6.28	6.28	2	0.05	0.01	0.05	0.00	0.00	24.0
5	12	-9491	123	566	0	789	-340	12.57	12.57	6.28	6.28	2	0.06	0.01	0.05	0.00	0.00	24.0
6	12	-9189	626	487	0	662	-1495	12.57	12.57	6.28	6.28	2	0.10	0.01	0.06	0.00	0.00	24.0
7	12	-9633	638	622	0	886	-1515	12.57	12.57	6.28	6.28	2	0.11	0.01	0.06	0.00	0.00	24.0
8	12	-9196	391	483	0	653	-955	12.57	12.57	6.28	6.28	2	0.07	0.01	0.04	0.00	0.00	24.0
9	12	-9640	402	618	0	877	-976	12.57	12.57	6.28	6.28	2	0.08	0.01	0.05	0.00	0.00	24.0
10	12	-9338	905	539	0	750	-2130	12.57	12.57	6.28	6.28	2	0.13	0.02	0.09	0.00	0.00	24.0
11	12	-9471	909	580	0	818	-2136	12.57	12.57	6.28	6.28	2	0.14	0.02	0.09	0.00	0.00	24.0
12	12	-9358	120	526	0	721	-334	12.57	12.57	6.28	6.28	2	0.05	0.01	0.05	0.00	0.00	24.0
13	12	-9491	123	566	0	789	-340	12.57	12.57	6.28	6.28	2	0.06	0.01	0.05	0.00	0.00	24.0
14	12	-9189	626	487	0	662	-1495	12.57	12.57	6.28	6.28	2	0.10	0.01	0.06	0.00	0.00	24.0
15	12	-9633	638	622	0	886	-1515	12.57	12.57	6.28	6.28	2	0.11	0.01	0.06	0.00	0.00	24.0
16	12	-9196	391	483	0	653	-955	12.57	12.57	6.28	6.28	2	0.07	0.01	0.04	0.00	0.00	24.0
17	12	-9640	402	618	0	877	-976	12.57	12.57	6.28	6.28	2	0.08	0.01	0.05	0.00	0.00	24.0
18	12	-12652	2609	820	0	1183	-5991	12.57	12.57	6.28	6.28	3	0.23	0.04	0.25	0.00	0.00	24.0
19	12	-12702	-38	759	0	1055	38	12.57	12.57	6.28	6.28	3	0.06	0.01	0.07	0.00	0.00	24.0
20	12	-12742	1202	749	0	1022	-2789	12.57	12.57	6.28	6.28	3	0.11	0.02	0.12	0.00	0.00	24.0
37	12	-12392	3288	807	0	1174	-7549	12.57	12.57	6.28	6.28	3	0.28	0.06	0.32	0.00	0.00	24.0
38	12	-12482	-1124	706	0	962	2499	12.57	12.57	6.28	6.28	3	0.10	0.02	0.11	0.00	0.00	24.0
39	12	-12532	942	690	0	907	-2212	12.57	12.57	6.28	6.28	3	0.09	0.02	0.09	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-12145	668	718	0	910	-1522	12.57	12.57	6.28	6.28	3	0.07	0.01	0.06	0.00	0.00	24.0
2	25	-9263	905	539	0	683	-2017	12.57	12.57	6.28	6.28	2	0.13	0.02	0.09	0.00	0.00	24.0
3	25	-9396	909	580	0	745	-2023	12.57	12.57	6.28	6.28	2	0.13	0.02	0.09	0.00	0.00	24.0
4	25	-9283	120	526	0	656	-319	12.57	12.57	6.28	6.28	2	0.05	0.01	0.05	0.00	0.00	24.0
5	25	-9416	123	566	0	718	-325	12.57	12.57	6.28	6.28	2	0.05	0.01	0.05	0.00	0.00	24.0
6	25	-9114	626	487	0	601	-1417	12.57	12.57	6.28	6.28	2	0.09	0.01	0.06	0.00	0.00	24.0
7	25	-9558	638	622	0	808	-1436	12.57	12.57	6.28	6.28	2	0.10	0.01	0.06	0.00	0.00	24.0
8	25	-9121	391	483	0	592	-906	12.57	12.57	6.28	6.28	2	0.07	0.01	0.04	0.00	0.00	24.0
9	25	-9565	402	618	0	800	-926	12.57	12.57	6.28	6.28	2	0.08	0.01	0.05	0.00	0.00	24.0
10	25	-9263	905	539	0	683	-2017	12.57	12.57	6.28	6.28	2	0.13	0.02	0.09	0.00	0.00	24.0
11	25	-9396	909	580	0	745	-2023	12.57	12.57	6.28	6.28	2	0.13	0.02	0.09	0.00	0.00	24.0
12	25	-9283	120	526	0	656	-319	12.57	12.57	6.28	6.28	2	0.05	0.01	0.05	0.00	0.00	24.0
13	25	-9416	123	566	0	718	-325	12.57	12.57	6.28	6.28	2	0.05	0.01	0.05	0.00	0.00	24.0
14	25	-9114	626	487	0	601	-1417	12.57	12.57	6.28	6.28	2	0.09	0.01	0.06	0.00	0.00	24.0
15	25	-9558	638	622	0	808	-1436	12.57	12.57	6.28	6.28	2	0.10	0.01	0.06	0.00	0.00	24.0
16	25	-9121	391	483	0	592	-906	12.57	12.57	6.28	6.28	2	0.07	0.01	0.04	0.00	0.00	24.0
17	25	-9565	402	618	0	800	-926	12.57	12.57	6.28	6.28	2	0.08	0.01	0.05	0.00	0.00	24.0
18	25	-12555	2609	820	0	1080	-5665	12.57	12.57	6.28	6.28	3	0.21	0.04	0.25	0.00	0.00	24.0
19	25	-12605	-38	759	0	960	33	12.57	12.57	6.28	6.28	3	0.05	0.01	0.07	0.00	0.00	24.0
20	25	-12645	1202	749	0	929	-2638	12.57	12.57	6.28	6.28	3	0.11	0.02	0.12	0.00	0.00	24.0
37	25	-12295	3288	807	0	1073	-7138	12.57	12.57	6.28	6.28	3	0.27	0.06	0.32	0.00	0.00	24.0
38	25	-12385	-1124	706	0	874	2359	12.57	12.57	6.28	6.28	3	0.10	0.02	0.11	0.00	0.00	24.0
39	25	-12435	942	690	0	821	-2094	12.57	12.57	6.28	6.28	3	0.09	0.02	0.09	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-12048	668	718	0	821	-1438	12.57	12.57	6.28	6.28	3	0.07	0.01	0.06	0.00	0.00	24.0
2	38	-9188	905	539	0	616	-1904	12.57	12.57	6.28	6.28	2	0.12	0.02	0.09	0.00	0.00	24.0
3	38	-9321	909	580	0	673	-1910	12.57	12.57	6.28	6.28	2	0.12	0.02	0.09	0.00	0.00	24.0
4	38	-9208	120	526	0	590	-304	12.57	12.57	6.28	6.28	2	0.04	0.01	0.05	0.00	0.00	24.0
5	38	-9341	123	566	0	647	-309	12.57	12.57	6.28	6.28	2	0.05	0.01	0.05	0.00	0.00	24.0
6	38	-9039	626	487	0	540	-1338	12.57	12.57	6.28	6.28	2	0.09	0.01	0.06	0.00	0.00	24.0
7	38	-9483	638	622	0	731	-1356	12.57	12.57	6.28	6.28	2	0.10	0.01	0.06	0.00	0.00	24.0
8	38	-9046	391	483	0	532	-858	12.57	12.57	6.28	6.28	2	0.06	0.01	0.04	0.00	0.00	24.0
9	38	-9490	402	618	0	723	-875	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
10	38	-9188	905	539	0	616	-1904	12.57	12.57	6.28	6.28	2	0.12	0.02	0.09	0.00	0.00	24.0
11	38	-9321	909	580	0	673	-1910	12.57	12.57	6.28	6.28	2	0.12	0.02	0.09	0.00	0.00	24.0
12	38	-9208	120	526	0	590	-304	12.57	12.57	6.28	6.28	2	0.04	0.01	0.05	0.00	0.00	24.0
13	38	-9341	123	566	0	647	-309	12.57	12.57	6.28	6.28	2	0.05	0.01	0.05	0.00	0.00	24.0
14	38	-9039	626	487	0	540	-1338	12.57	12.57	6.28	6.28	2	0.09	0.01	0.06	0.00	0.00	24.0
15	38	-9483	638	622	0	731	-1356	12.57	12.57	6.28	6.28	2	0.10	0.01	0.06	0.00	0.00	24.0
16	38	-9046	391	483	0	532	-858	12.57	12.57	6.28	6.28	2	0.06	0.01	0.04	0.00	0.00	24.0
17	38	-9490	402	618	0	723	-875	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
18	38	-12458	2609	820	0	978	-5338	12.57	12.57	6.28	6.28	3	0.20	0.05	0.25	0.00	0.00	24.0
19	38	-12508	-38	759	0	866	29	12.57	12.57	6.28	6.28	3	0.05	0.01	0.07	0.00	0.00	24.0
20	38	-12548	1202	749	0	835	-2488	12.57	12.57	6.28	6.28	3	0.10	0.02	0.12	0.00	0.00	24.0
37	38	-12198	3288	807	0	972	-6727	12.57	12.57	6.28	6.28	3	0.25	0.06	0.32	0.00	0.00	24.0
38	38	-12288	-1124	706	0	786	2218	12.57	12.57	6.28	6.28	3	0.09	0.02	0.11	0.00	0.00	24.0
39	38	-12338	942	690	0	735	-1977	12.57	12.57	6.28	6.28	3	0.08	0.02	0.09	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-11950	668	718	0	731	-1355	12.57	12.57	6.28	6.28	3	0.06	0.01	0.06	0.00	0.00	24.0
2	50	-9113	905	539	0	548	-1791	12.57	12.57	6.28	6.28	2	0.11	0.02	0.09	0.00	0.00	24.0
3	50	-9246	909	580	0	600	-1796	12.57	12.57	6.28	6.28	2	0.11	0.02	0.09	0.00	0.00	24.0
4	50	-9133	120	526	0	524	-289	12.57	12.57	6.28	6.28	2	0.04	0.01	0.05	0.00	0.00	24.0
5	50	-9266	123	566	0	576	-294	12.57	12.57	6.28	6.28	2	0.04	0.01	0.05	0.00	0.00	24.0
6	50	-8964	626	487	0	479	-1260	12.57	12.57	6.28	6.28	2	0.08	0.01	0.06	0.00	0.00	24.0
7	50	-9408	638	622	0	653	-1276	12.57	12.57	6.28	6.28	2	0.09	0.01	0.06	0.00	0.00	24.0
8	50	-8971	391	483	0	472	-809	12.57	12.57	6.28	6.28	2	0.06	0.01	0.04	0.00	0.00	24.0
9	50	-9415	402	618	0	646	-825	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
10	50	-9113	905	539	0	548	-1791	12.57	12.57	6.28	6.28	2	0.11	0.02	0.09	0.00	0.00	24.0
11	50	-9246	909	580	0	600	-1796	12.57	12.57	6.28	6.28	2	0.11	0.02	0.09	0.00	0.00	24.0
12	50	-9133	120	526	0	524	-289	12.57	12.57	6.28	6.28	2	0.04	0.01	0.05	0.00	0.00	24.0
13	50	-9266	123	566	0	576	-294	12.57	12.57	6.28	6.28	2	0.04	0.01	0.05	0.00	0.00	24.0
14	50	-8964	626	487	0	479	-1260	12.57	12.57	6.28	6.28	2	0.08	0.01	0.06	0.00	0.00	24.0
15	50	-9408	638	622	0	653	-1276	12.57	12.57	6.28	6.28	2	0.09	0.01	0.06	0.00	0.00	24.0
16	50	-8971	391	483	0	472	-809	12.57	12.57	6.28	6.28	2	0.06	0.01	0.04	0.00	0.00	24.0
17	50	-9415	402	618	0	646	-825	12.57	12.57	6.28	6.28	2	0.07	0.01	0.05	0.00	0.00	24.0
18	50	-12360	2609	820	0	876	-5012	12.57	12.57	6.28	6.28	3	0.19	0.05	0.25	0.00	0.00	24.0
19	50	-12410	-38	759	0	771	24	12.57	12.57	6.28	6.28	3	0.04	0.01	0.07	0.00	0.00	24.0
20	50	-12450	1202	749	0	742	-2338	12.57	12.57	6.28	6.28	3	0.09	0.02	0.12	0.00	0.00	24.0
37	50	-12100	3288	807	0	872	-6316	12.57	12.57	6.28	6.28	3	0.23	0.06	0.32	0.00	0.00	24.0
38	50	-12190	-1124	706	0	697	2078	12.57	12.57	6.28	6.28	3	0.08	0.02	0.11	0.00	0.00	24.0
39	50	-12240	942	690	0	649	-1859	12.57	12.57	6.28	6.28	3	0.08	0.02	0.09	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 98 NI 479 NF 595 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 7
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
													Fx,M	Bielle	V,Mx			
	cm		daN			daN*m				cmq						cmq/m		cm
1	0	-1602	199	-263	0	57	-55	6.28	6.28	9.42	9.42	3	0.01	0.01	0.04	0.00	0.00	24.0
2	0	-1215	142	-166	0	40	-33	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
3	0	-1276	121	-305	0	31	-26	6.28	6.28	9.42	9.42	2	0.00	0.01	0.04	0.00	0.00	24.0
4	0	-1188	185	-99	0	57	-58	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
5	0	-1250	164	-239	0	48	-52	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
6	0	-1134	181	20	0	56	-50	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
7	0	-1339	111	-444	0	27	-27	6.28	6.28	9.42	9.42	2	0.00	0.01	0.06	0.00	0.00	24.0
8	0	-1126	194	40	0	61	-58	6.28	6.28	9.42	9.42	2	0.01	0.01	0.02	0.00	0.00	24.0
9	0	-1331	124	-425	0	32	-35	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
10	0	-1215	142	-166	0	40	-33	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
11	0	-1276	121	-305	0	31	-26	6.28	6.28	9.42	9.42	2	0.00	0.01	0.04	0.00	0.00	24.0
12	0	-1188	185	-99	0	57	-58	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
13	0	-1250	164	-239	0	48	-52	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
14	0	-1134	181	20	0	56	-50	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
15	0	-1339	111	-444	0	27	-27	6.28	6.28	9.42	9.42	2	0.00	0.01	0.06	0.00	0.00	24.0
16	0	-1126	194	40	0	61	-58	6.28	6.28	9.42	9.42	2	0.01	0.01	0.02	0.00	0.00	24.0
17	0	-1331	124	-425	0	32	-35	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
18	0	-1222	37	-450	0	-19	-34	6.28	6.28	9.42	9.42	3	0.00	0.01	0.06	0.00	0.00	24.0
19	0	-1431	507	61	0	92	-197	6.28	6.28	9.42	9.42	3	0.02	0.01	0.06	0.00	0.00	24.0
20	0	-908	-177	-1568	0	-622	13	6.28	6.28	9.42	9.42	3	0.03	0.04	0.22	0.00	0.00	24.0
37	0	-1254	-143	-643	0	-50	41	6.28	6.28	9.42	9.42	3	0.00	0.02	0.09	0.00	0.00	24.0
38	0	-1603	640	208	0	136	-231	6.28	6.28	9.42	9.42	3	0.03	0.02	0.08	0.00	0.00	24.0
39	0	-731	-500	-2507	0	-1055	118	6.28	6.28	9.42	9.42	3	0.06	0.06	0.35	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-1529	199	-263	0	90	-30	6.28	6.28	9.42	9.42	3	0.01	0.01	0.04	0.00	0.00	24.0
2	12	-1159	142	-166	0	61	-15	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
3	12	-1220	121	-305	0	69	-11	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
4	12	-1132	185	-99	0	69	-35	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
5	12	-1194	164	-239	0	78	-31	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
6	12	-1078	181	20	0	54	-27	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
7	12	-1283	111	-444	0	82	-13	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
8	12	-1070	194	40	0	56	-33	6.28	6.28	9.42	9.42	2	0.01	0.01	0.02	0.00	0.00	24.0
9	12	-1275	124	-425	0	85	-19	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
10	12	-1159	142	-166	0	61	-15	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
11	12	-1220	121	-305	0	69	-11	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
12	12	-1132	185	-99	0	69	-35	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
13	12	-1194	164	-239	0	78	-31	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
14	12	-1078	181	20	0	54	-27	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
15	12	-1283	111	-444	0	82	-13	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
16	12	-1070	194	40	0	56	-33	6.28	6.28	9.42	9.42	2	0.01	0.01	0.02	0.00	0.00	24.0
17	12	-1275	124	-425	0	85	-19	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
18	12	-1149	37	-450	0	37	-29	6.28	6.28	9.42	9.42	3	0.00	0.01	0.06	0.00	0.00	24.0
19	12	-1358	507	61	0	85	-133	6.28	6.28	9.42	9.42	3	0.02	0.01	0.06	0.00	0.00	24.0
20	12	-835	-177	-1568	0	-426	-10	6.28	6.28	9.42	9.42	3	0.02	0.04	0.22	0.00	0.00	24.0
37	12	-1181	-143	-643	0	30	23	6.28	6.28	9.42	9.42	3	0.00	0.02	0.09	0.00	0.00	24.0
38	12	-1530	640	208	0	110	-152	6.28	6.28	9.42	9.42	3	0.02	0.02	0.08	0.00	0.00	24.0
39	12	-657	-500	-2507	0	-742	55	6.28	6.28	9.42	9.42	3	0.04	0.06	0.35	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-1456	199	-263	0	123	-5	6.28	6.28	9.42	9.42	3	0.01	0.01	0.04	0.00	0.00	24.0
2	25	-1102	142	-166	0	81	2	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
3	25	-1164	121	-305	0	107	4	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
4	25	-1076	185	-99	0	82	-12	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
5	25	-1138	164	-239	0	108	-11	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
6	25	-1021	181	20	0	51	-5	6.28	6.28	9.42	9.42	2	0.00	0.00	0.02	0.00	0.00	24.0
7	25	-1226	111	-444	0	138	1	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
8	25	-1013	194	40	0	51	-9	6.28	6.28	9.42	9.42	2	0.00	0.01	0.02	0.00	0.00	24.0
9	25	-1218	124	-425	0	138	-4	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
10	25	-1102	142	-166	0	81	2	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
11	25	-1164	121	-305	0	107	4	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
12	25	-1076	185	-99	0	82	-12	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
13	25	-1138	164	-239	0	108	-11	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
14	25	-1021	181	20	0	51	-5	6.28	6.28	9.42	9.42	2	0.00	0.00	0.02	0.00	0.00	24.0
15	25	-1226	111	-444	0	138	1	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
16	25	-1013	194	40	0	51	-9	6.28	6.28	9.42	9.42	2	0.00	0.01	0.02	0.00	0.00	24.0
17	25	-1218	124	-425	0	138	-4	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
18	25	-1076	37	-450	0	93	-24	6.28	6.28	9.42	9.42	3	0.01	0.01	0.06	0.00	0.00	24.0
19	25	-1285	507	61	0	77	-70	6.28	6.28	9.42	9.42	3	0.01	0.01	0.05	0.00	0.00	24.0

20	25	-762	-177	-1568	0	-230	-32	6.28	6.28	9.42	9.42	3	0.01	0.04	0.22	0.00	0.00	24.0
37	25	-1108	-143	-643	0	111	5	6.28	6.28	9.42	9.42	3	0.01	0.02	0.09	0.00	0.00	24.0
38	25	-1457	640	208	0	84	-72	6.28	6.28	9.42	9.42	3	0.01	0.02	0.07	0.00	0.00	24.0
39	25	-584	-500	-2507	0	-428	-8	6.28	6.28	9.42	9.42	3	0.02	0.06	0.35	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-1382	199	-263	0	156	20	6.28	6.28	9.42	9.42	3	0.01	0.01	0.04	0.00	0.00	24.0
2	38	-1046	142	-166	0	102	20	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
3	38	-1107	121	-305	0	145	19	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
4	38	-1019	185	-99	0	94	11	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
5	38	-1081	164	-239	0	138	10	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
6	38	-965	181	20	0	49	18	6.28	6.28	9.42	9.42	2	0.00	0.00	0.02	0.00	0.00	24.0
7	38	-1170	111	-444	0	193	15	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
8	38	-957	194	40	0	46	15	6.28	6.28	9.42	9.42	2	0.00	0.01	0.02	0.00	0.00	24.0
9	38	-1162	124	-425	0	191	12	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
10	38	-1046	142	-166	0	102	20	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
11	38	-1107	121	-305	0	145	19	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
12	38	-1019	185	-99	0	94	11	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
13	38	-1081	164	-239	0	138	10	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
14	38	-965	181	20	0	49	18	6.28	6.28	9.42	9.42	2	0.00	0.00	0.02	0.00	0.00	24.0
15	38	-1170	111	-444	0	193	15	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
16	38	-957	194	40	0	46	15	6.28	6.28	9.42	9.42	2	0.00	0.01	0.02	0.00	0.00	24.0
17	38	-1162	124	-425	0	191	12	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
18	38	-1002	37	-450	0	149	-20	6.28	6.28	9.42	9.42	3	0.01	0.01	0.06	0.00	0.00	24.0
19	38	-1212	507	61	0	69	-7	6.28	6.28	9.42	9.42	3	0.00	0.01	0.05	0.00	0.00	24.0
20	38	-688	-177	-1568	0	-34	-54	6.28	6.28	9.42	9.42	3	0.01	0.04	0.22	0.00	0.00	24.0
37	38	-1035	-143	-643	0	191	-13	6.28	6.28	9.42	9.42	3	0.01	0.02	0.09	0.00	0.00	24.0
38	38	-1384	640	208	0	58	8	6.28	6.28	9.42	9.42	3	0.00	0.02	0.07	0.00	0.00	24.0
39	38	-511	-500	-2507	0	-115	-70	6.28	6.28	9.42	9.42	3	0.01	0.06	0.35	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-1309	199	-263	0	189	44	6.28	6.28	9.42	9.42	3	0.01	0.01	0.04	0.00	0.00	24.0
2	50	-990	142	-166	0	123	38	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
3	50	-1051	121	-305	0	184	34	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
4	50	-963	185	-99	0	107	34	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
5	50	-1025	164	-239	0	168	30	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
6	50	-908	181	20	0	46	41	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
7	50	-1114	111	-444	0	249	29	6.28	6.28	9.42	9.42	2	0.02	0.01	0.06	0.00	0.00	24.0
8	50	-900	194	40	0	41	40	6.28	6.28	9.42	9.42	2	0.01	0.01	0.02	0.00	0.00	24.0
9	50	-1106	124	-425	0	244	27	6.28	6.28	9.42	9.42	2	0.02	0.01	0.06	0.00	0.00	24.0
10	50	-990	142	-166	0	123	38	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
11	50	-1051	121	-305	0	184	34	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
12	50	-963	185	-99	0	107	34	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
13	50	-1025	164	-239	0	168	30	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
14	50	-908	181	20	0	46	41	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
15	50	-1114	111	-444	0	249	29	6.28	6.28	9.42	9.42	2	0.02	0.01	0.06	0.00	0.00	24.0
16	50	-900	194	40	0	41	40	6.28	6.28	9.42	9.42	2	0.01	0.01	0.02	0.00	0.00	24.0
17	50	-1106	124	-425	0	244	27	6.28	6.28	9.42	9.42	2	0.02	0.01	0.06	0.00	0.00	24.0
18	50	-929	37	-450	0	206	-15	6.28	6.28	9.42	9.42	3	0.01	0.01	0.06	0.00	0.00	24.0
19	50	-1139	507	61	0	62	56	6.28	6.28	9.42	9.42	3	0.01	0.01	0.05	0.00	0.00	24.0
20	50	-615	-177	-1568	0	162	-76	6.28	6.28	9.42	9.42	3	0.01	0.04	0.22	0.00	0.00	24.0
37	50	-961	-143	-643	0	272	-31	6.28	6.28	9.42	9.42	3	0.01	0.02	0.09	0.00	0.00	24.0
38	50	-1311	640	208	0	32	88	6.28	6.28	9.42	9.42	3	0.01	0.02	0.08	0.00	0.00	24.0
39	50	-438	-500	-2507	0	198	-133	6.28	6.28	9.42	9.42	3	0.02	0.06	0.35	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 99 NI 595 NF 23 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 7A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-1707	381	-324	0	260	68	6.28	6.28	9.42	9.42	3	0.01	0.01	0.04	0.00	0.00	24.0
2	0	-1271	318	-180	0	165	49	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
3	0	-1321	306	-359	0	248	49	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
4	0	-1304	280	-140	0	151	56	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
5	0	-1355	269	-320	0	235	56	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
6	0	-1223	318	43	0	62	52	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
7	0	-1392	279	-554	0	342	52	6.28	6.28	9.42	9.42	2	0.03	0.01	0.08	0.00	0.00	24.0
8	0	-1234	307	55	0	58	54	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
9	0	-1402	268	-542	0	338	54	6.28	6.28	9.42	9.42	2	0.03	0.01	0.07	0.00	0.00	24.0
10	0	-1271	318	-180	0	165	49	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
11	0	-1321	306	-359	0	248	49	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
12	0	-1304	280	-140	0	151	56	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
13	0	-1355	269	-320	0	235	56	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
14	0	-1223	318	43	0	62	52	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
15	0	-1392	279	-554	0	342	52	6.28	6.28	9.42	9.42	2	0.03	0.01	0.08	0.00	0.00	24.0
16	0	-1234	307	55	0	58	54	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
17	0	-1402	268	-542	0	338	54	6.28	6.28	9.42	9.42	2	0.03	0.01	0.07	0.00	0.00	24.0
18	0	-1341	23	-447	0	329	9	6.28	6.28	9.42	9.42	3	0.02	0.01	0.06	0.00	0.00	24.0
19	0	-1733	520	-61	0	167	150	6.28	6.28	9.42	9.42	3	0.02	0.01	0.06	0.00	0.00	24.0
20	0	-1208	147	-675	0	599	57	6.28	6.28	9.42	9.42	3	0.03	0.02	0.09	0.00	0.00	24.0
37	0	-1284	-106	-597	0	386	-41	6.28	6.28	9.42	9.42	3	0.02	0.01	0.08	0.00	0.00	24.0
38	0	-1937	722	46	0	117	193	6.28	6.28	9.42	9.42	3	0.02	0.02	0.09	0.00	0.00	24.0
39	0	-1062	100	-978	0	837	38	6.28	6.28	9.42	9.42	3	0.04	0.02	0.13	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-1634	381	-324	0	300	116	6.28	6.28	9.42	9.42	3	0.02	0.01	0.04	0.00	0.00	24.0
2	12	-1215	318	-180	0	187	89	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
3	12	-1265	306	-359	0	293	87	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
4	12	-1248	280	-140	0	168	91	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
5	12	-1299	269	-320	0	275	90	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
6	12	-1167	318	43	0	56	91	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
7	12	-1336	279	-554	0	411	86	6.28	6.28	9.42	9.42	2	0.03	0.01	0.08	0.00	0.00	24.0
8	12	-1178	307	55	0	51	92	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
9	12	-1346	268	-542	0	405	87	6.28	6.28	9.42	9.42	2	0.03	0.01	0.07	0.00	0.00	24.0
10	12	-1215	318	-180	0	187	89	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
11	12	-1265	306	-359	0	293	87	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
12	12	-1248	280	-140	0	168	91	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
13	12	-1299	269	-320	0	275	90	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
14	12	-1167	318	43	0	56	91	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
15	12	-1336	279	-554	0	411	86	6.28	6.28	9.42	9.42	2	0.03	0.01	0.08	0.00	0.00	24.0

16	12	-1178	307	55	0	51	92	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
17	12	-1346	268	-542	0	405	87	6.28	6.28	9.42	9.42	2	0.03	0.01	0.07	0.00	0.00	24.0
18	12	-1268	23	-447	0	384	12	6.28	6.28	9.42	9.42	3	0.02	0.01	0.06	0.00	0.00	24.0
19	12	-1660	520	-61	0	175	215	6.28	6.28	9.42	9.42	3	0.03	0.01	0.06	0.00	0.00	24.0
20	12	-1135	147	-675	0	684	75	6.28	6.28	9.42	9.42	3	0.04	0.02	0.09	0.00	0.00	24.0
37	12	-1211	-106	-597	0	461	-54	6.28	6.28	9.42	9.42	3	0.02	0.01	0.08	0.00	0.00	24.0
38	12	-1864	722	46	0	111	283	6.28	6.28	9.42	9.42	3	0.03	0.02	0.09	0.00	0.00	24.0
39	12	-989	100	-978	0	960	51	6.28	6.28	9.42	9.42	3	0.05	0.02	0.13	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-1560	381	-324	0	341	164	6.28	6.28	9.42	9.42	3	0.02	0.01	0.04	0.00	0.00	24.0
2	25	-1158	318	-180	0	209	129	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
3	25	-1208	306	-359	0	338	126	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
4	25	-1192	280	-140	0	186	126	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
5	25	-1242	269	-320	0	315	123	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
6	25	-1111	318	43	0	51	131	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
7	25	-1280	279	-554	0	480	121	6.28	6.28	9.42	9.42	2	0.04	0.01	0.08	0.00	0.00	24.0
8	25	-1122	307	55	0	44	130	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
9	25	-1290	268	-542	0	473	121	6.28	6.28	9.42	9.42	2	0.04	0.01	0.07	0.00	0.00	24.0
10	25	-1158	318	-180	0	209	129	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
11	25	-1208	306	-359	0	338	126	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
12	25	-1192	280	-140	0	186	126	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
13	25	-1242	269	-320	0	315	123	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
14	25	-1111	318	43	0	51	131	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
15	25	-1280	279	-554	0	480	121	6.28	6.28	9.42	9.42	2	0.04	0.01	0.08	0.00	0.00	24.0
16	25	-1122	307	55	0	44	130	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
17	25	-1290	268	-542	0	473	121	6.28	6.28	9.42	9.42	2	0.04	0.01	0.07	0.00	0.00	24.0
18	25	-1195	23	-447	0	440	15	6.28	6.28	9.42	9.42	3	0.02	0.01	0.06	0.00	0.00	24.0
19	25	-1586	520	-61	0	182	280	6.28	6.28	9.42	9.42	3	0.03	0.01	0.06	0.00	0.00	24.0
20	25	-1062	147	-675	0	768	94	6.28	6.28	9.42	9.42	3	0.04	0.02	0.09	0.00	0.00	24.0
37	25	-1138	-106	-597	0	536	-67	6.28	6.28	9.42	9.42	3	0.03	0.01	0.08	0.00	0.00	24.0
38	25	-1791	722	46	0	106	374	6.28	6.28	9.42	9.42	3	0.04	0.02	0.09	0.00	0.00	24.0
39	25	-916	100	-978	0	1082	63	6.28	6.28	9.42	9.42	3	0.06	0.02	0.13	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-1487	381	-324	0	381	211	6.28	6.28	9.42	9.42	3	0.03	0.01	0.04	0.00	0.00	24.0
2	38	-1102	318	-180	0	232	168	6.28	6.28	9.42	9.42	2	0.03	0.01	0.03	0.00	0.00	24.0
3	38	-1152	306	-359	0	383	164	6.28	6.28	9.42	9.42	2	0.04	0.01	0.05	0.00	0.00	24.0
4	38	-1135	280	-140	0	203	161	6.28	6.28	9.42	9.42	2	0.03	0.01	0.03	0.00	0.00	24.0
5	38	-1186	269	-320	0	355	157	6.28	6.28	9.42	9.42	2	0.04	0.01	0.04	0.00	0.00	24.0
6	38	-1055	318	43	0	46	171	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
7	38	-1223	279	-554	0	549	156	6.28	6.28	9.42	9.42	2	0.05	0.01	0.08	0.00	0.00	24.0
8	38	-1065	307	55	0	37	169	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
9	38	-1233	268	-542	0	541	154	6.28	6.28	9.42	9.42	2	0.05	0.01	0.07	0.00	0.00	24.0
10	38	-1102	318	-180	0	232	168	6.28	6.28	9.42	9.42	2	0.03	0.01	0.03	0.00	0.00	24.0
11	38	-1152	306	-359	0	383	164	6.28	6.28	9.42	9.42	2	0.04	0.01	0.05	0.00	0.00	24.0
12	38	-1135	280	-140	0	203	161	6.28	6.28	9.42	9.42	2	0.03	0.01	0.03	0.00	0.00	24.0
13	38	-1186	269	-320	0	355	157	6.28	6.28	9.42	9.42	2	0.04	0.01	0.04	0.00	0.00	24.0
14	38	-1055	318	43	0	46	171	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
15	38	-1223	279	-554	0	549	156	6.28	6.28	9.42	9.42	2	0.05	0.01	0.08	0.00	0.00	24.0
16	38	-1065	307	55	0	37	169	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
17	38	-1233	268	-542	0	541	154	6.28	6.28	9.42	9.42	2	0.05	0.01	0.07	0.00	0.00	24.0
18	38	-1122	23	-447	0	496	18	6.28	6.28	9.42	9.42	3	0.03	0.01	0.06	0.00	0.00	24.0
19	38	-1513	520	-61	0	190	345	6.28	6.28	9.42	9.42	3	0.04	0.01	0.06	0.00	0.00	24.0
20	38	-988	147	-675	0	852	112	6.28	6.28	9.42	9.42	3	0.04	0.02	0.09	0.00	0.00	24.0
37	38	-1065	-106	-597	0	610	-80	6.28	6.28	9.42	9.42	3	0.03	0.01	0.08	0.00	0.00	24.0
38	38	-1718	722	46	0	100	464	6.28	6.28	9.42	9.42	3	0.05	0.02	0.09	0.00	0.00	24.0
39	38	-842	100	-978	0	1204	76	6.28	6.28	9.42	9.42	3	0.06	0.02	0.13	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-1414	381	-324	0	422	259	6.28	6.28	9.42	9.42	3	0.03	0.01	0.04	0.00	0.00	24.0
2	50	-1046	318	-180	0	254	208	6.28	6.28	9.42	9.42	2	0.04	0.01	0.03	0.00	0.00	24.0
3	50	-1096	306	-359	0	428	202	6.28	6.28	9.42	9.42	2	0.04	0.01	0.05	0.00	0.00	24.0
4	50	-1079	280	-140	0	221	196	6.28	6.28	9.42	9.42	2	0.03	0.01	0.03	0.00	0.00	24.0
5	50	-1130	269	-320	0	394	190	6.28	6.28	9.42	9.42	2	0.04	0.01	0.04	0.00	0.00	24.0
6	50	-998	318	43	0	40	210	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
7	50	-1167	279	-554	0	619	191	6.28	6.28	9.42	9.42	2	0.06	0.01	0.08	0.00	0.00	24.0
8	50	-1009	307	55	0	30	207	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
9	50	-1177	268	-542	0	609	188	6.28	6.28	9.42	9.42	2	0.05	0.01	0.07	0.00	0.00	24.0
10	50	-1046	318	-180	0	254	208	6.28	6.28	9.42	9.42	2	0.04	0.01	0.03	0.00	0.00	24.0
11	50	-1096	306	-359	0	428	202	6.28	6.28	9.42	9.42	2	0.04	0.01	0.05	0.00	0.00	24.0
12	50	-1079	280	-140	0	221	196	6.28	6.28	9.42	9.42	2	0.03	0.01	0.03	0.00	0.00	24.0
13	50	-1130	269	-320	0	394	190	6.28	6.28	9.42	9.42	2	0.04	0.01	0.04	0.00	0.00	24.0
14	50	-998	318	43	0	40	210	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
15	50	-1167	279	-554	0	619	191	6.28	6.28	9.42	9.42	2	0.06	0.01	0.08	0.00	0.00	24.0
16	50	-1009	307	55	0	30	207	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
17	50	-1177	268	-542	0	609	188	6.28	6.28	9.42	9.42	2	0.05	0.01	0.07	0.00	0.00	24.0
18	50	-1049	23	-447	0	552	21	6.28	6.28	9.42	9.42	3	0.03	0.01	0.06	0.00	0.00	24.0
19	50	-1440	520	-61	0	198	410	6.28	6.28	9.42	9.42	3	0.05	0.01	0.06	0.00	0.00	24.0
20	50	-915	147	-675	0	937	130	6.28	6.28	9.42	9.42	3	0.05	0.02	0.09	0.00	0.00	24.0
37	50	-992	-106	-597	0	685	-94	6.28	6.28	9.42	9.42	3	0.04	0.01	0.08	0.00	0.00	24.0
38	50	-1645	722	46	0	94	554	6.28	6.28	9.42	9.42	3	0.06	0.02	0.09	0.00	0.00	24.0
39	50	-769	100	-978	0	1326	88	6.28	6.28	9.42	9.42	3	0.07	0.02	0.13	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 100 NI 606 NF 624 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 1
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-9151	-644	301	0	-237	421	6.28	6.28	9.42	9.42	3	0.04	0.02	0.07	0.00	0.00	24.0
2	0	-6525	-585	348	0	-168	328	6.28	6.28	9.42	9.42	2	0.04	0.01	0.07	0.00	0.00	24.0
3	0	-6357	-572	247	0	-146	320	6.28	6.28	9.42	9.42	2	0.04	0.01	0.07	0.00	0.00	24.0
4	0	-7722	-418	217	0	-219	327	6.28	6.28	9.42	9.42	2	0.04	0.01	0.05	0.00	0.00	24.0
5	0	-7554	-405	116	0	-196	319	6.28	6.28	9.42	9.42	2	0.04	0.01	0.05	0.00	0.00	24.0
6	0	-7141	-542	419	0	-212	336	6.28	6.28	9.42	9.42	2	0.05	0.01	0.06	0.00	0.00	24.0
7	0	-6579	-498	83	0	-137	311	6.28	6.28	9.42	9.42	2	0.04	0.01	0.06	0.00	0.00	24.0
8	0	-7500	-492	380	0	-227	336	6.28	6.28	9.42	9.42	2	0.05	0.01	0.06	0.00	0.00	24.0
9	0	-6938	-448	44	0	-152	311	6.28	6.28	9.42	9.42	2	0.04	0.01	0.05	0.00	0.00	24.0
10	0	-6525	-585	348	0	-168	328	6.28	6.28	9.42	9.42	2	0.04	0.01	0.07	0.00	0.00	24.0
11	0	-6357	-572	247	0	-146	320	6.28	6.28	9.42	9.42	2	0.04	0.01	0.07	0.00	0.00	24.0

12	0	-7722	-418	217	0	-219	327	6.28	6.28	9.42	9.42	2	0.04	0.01	0.05	0.00	0.00	24.0
13	0	-7554	-405	116	0	-196	319	6.28	6.28	9.42	9.42	2	0.04	0.01	0.05	0.00	0.00	24.0
14	0	-7141	-542	419	0	-212	336	6.28	6.28	9.42	9.42	2	0.05	0.01	0.06	0.00	0.00	24.0
15	0	-6579	-498	83	0	-137	311	6.28	6.28	9.42	9.42	2	0.04	0.01	0.06	0.00	0.00	24.0
16	0	-7500	-492	380	0	-227	336	6.28	6.28	9.42	9.42	2	0.05	0.01	0.06	0.00	0.00	24.0
17	0	-6938	-448	44	0	-152	311	6.28	6.28	9.42	9.42	2	0.04	0.01	0.05	0.00	0.00	24.0
18	0	-9347	-1128	684	0	-262	507	6.28	6.28	9.42	9.42	3	0.05	0.03	0.12	0.00	0.00	24.0
19	0	-11830	-269	21	0	-420	379	6.28	6.28	9.42	9.42	3	0.04	0.01	0.03	0.00	0.00	24.0
20	0	-10060	-673	151	0	-286	428	6.28	6.28	9.42	9.42	3	0.05	0.02	0.07	0.00	0.00	24.0
37	0	-8050	-1397	889	0	-175	543	6.28	6.28	9.42	9.42	3	0.06	0.04	0.16	0.00	0.00	24.0
38	0	-12190	34	-217	0	-439	330	6.28	6.28	9.42	9.42	3	0.04	0.00	0.02	0.00	0.00	24.0
39	0	-9237	-640	-0	0	-215	410	6.28	6.28	9.42	9.42	3	0.04	0.02	0.07	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-9078	-644	301	0	-275	340	6.28	6.28	9.42	9.42	3	0.04	0.02	0.07	0.00	0.00	24.0
2	12	-6469	-585	348	0	-212	255	6.28	6.28	9.42	9.42	2	0.04	0.01	0.07	0.00	0.00	24.0
3	12	-6301	-572	247	0	-177	249	6.28	6.28	9.42	9.42	2	0.03	0.01	0.07	0.00	0.00	24.0
4	12	-7666	-418	217	0	-246	274	6.28	6.28	9.42	9.42	2	0.04	0.01	0.05	0.00	0.00	24.0
5	12	-7498	-405	116	0	-211	269	6.28	6.28	9.42	9.42	2	0.04	0.01	0.05	0.00	0.00	24.0
6	12	-7085	-542	419	0	-265	269	6.28	6.28	9.42	9.42	2	0.04	0.01	0.06	0.00	0.00	24.0
7	12	-6523	-498	83	0	-148	249	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
8	12	-7444	-492	380	0	-275	274	6.28	6.28	9.42	9.42	2	0.04	0.01	0.05	0.00	0.00	24.0
9	12	-6882	-448	44	0	-158	255	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
10	12	-6469	-585	348	0	-212	255	6.28	6.28	9.42	9.42	2	0.04	0.01	0.07	0.00	0.00	24.0
11	12	-6301	-572	247	0	-177	249	6.28	6.28	9.42	9.42	2	0.03	0.01	0.07	0.00	0.00	24.0
12	12	-7666	-418	217	0	-246	274	6.28	6.28	9.42	9.42	2	0.04	0.01	0.05	0.00	0.00	24.0
13	12	-7498	-405	116	0	-211	269	6.28	6.28	9.42	9.42	2	0.04	0.01	0.05	0.00	0.00	24.0
14	12	-7085	-542	419	0	-265	269	6.28	6.28	9.42	9.42	2	0.04	0.01	0.06	0.00	0.00	24.0
15	12	-6523	-498	83	0	-148	249	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
16	12	-7444	-492	380	0	-275	274	6.28	6.28	9.42	9.42	2	0.04	0.01	0.05	0.00	0.00	24.0
17	12	-6882	-448	44	0	-158	255	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
18	12	-9274	-1128	684	0	-347	366	6.28	6.28	9.42	9.42	3	0.04	0.03	0.12	0.00	0.00	24.0
19	12	-11758	-269	21	0	-423	346	6.28	6.28	9.42	9.42	3	0.04	0.01	0.03	0.00	0.00	24.0
20	12	-9987	-673	151	0	-305	343	6.28	6.28	9.42	9.42	3	0.04	0.02	0.07	0.00	0.00	24.0
37	12	-7977	-1397	889	0	-286	368	6.28	6.28	9.42	9.42	3	0.04	0.04	0.16	0.00	0.00	24.0
38	12	-12118	34	-217	0	-412	334	6.28	6.28	9.42	9.42	3	0.04	0.00	0.02	0.00	0.00	24.0
39	12	-9164	-640	-0	0	-215	330	6.28	6.28	9.42	9.42	3	0.04	0.02	0.07	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-9005	-644	301	0	-312	260	6.28	6.28	9.42	9.42	3	0.03	0.02	0.06	0.00	0.00	24.0
2	25	-6412	-585	348	0	-255	182	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
3	25	-6244	-572	247	0	-207	177	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
4	25	-7610	-418	217	0	-273	222	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
5	25	-7442	-405	116	0	-225	218	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
6	25	-7028	-542	419	0	-317	201	6.28	6.28	9.42	9.42	2	0.04	0.01	0.05	0.00	0.00	24.0
7	25	-6466	-498	83	0	-158	187	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
8	25	-7388	-492	380	0	-322	213	6.28	6.28	9.42	9.42	2	0.04	0.01	0.05	0.00	0.00	24.0
9	25	-6826	-448	44	0	-163	199	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
10	25	-6412	-585	348	0	-255	182	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
11	25	-6244	-572	247	0	-207	177	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
12	25	-7610	-418	217	0	-273	222	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
13	25	-7442	-405	116	0	-225	218	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
14	25	-7028	-542	419	0	-317	201	6.28	6.28	9.42	9.42	2	0.04	0.01	0.05	0.00	0.00	24.0
15	25	-6466	-498	83	0	-158	187	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
16	25	-7388	-492	380	0	-322	213	6.28	6.28	9.42	9.42	2	0.04	0.01	0.05	0.00	0.00	24.0
17	25	-6826	-448	44	0	-163	199	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
18	25	-9201	-1128	684	0	-433	225	6.28	6.28	9.42	9.42	3	0.03	0.03	0.11	0.00	0.00	24.0
19	25	-11685	-269	21	0	-425	312	6.28	6.28	9.42	9.42	3	0.03	0.01	0.03	0.00	0.00	24.0
20	25	-9914	-673	151	0	-323	259	6.28	6.28	9.42	9.42	3	0.03	0.02	0.07	0.00	0.00	24.0
37	25	-7904	-1397	889	0	-397	194	6.28	6.28	9.42	9.42	3	0.03	0.04	0.14	0.00	0.00	24.0
38	25	-12045	34	-217	0	-385	338	6.28	6.28	9.42	9.42	3	0.04	0.00	0.02	0.00	0.00	24.0
39	25	-9091	-640	-0	0	-215	250	6.28	6.28	9.42	9.42	3	0.03	0.02	0.07	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-8932	-644	301	0	-350	179	6.28	6.28	9.42	9.42	3	0.02	0.02	0.06	0.00	0.00	24.0
2	38	-6356	-585	348	0	-299	109	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
3	38	-6188	-572	247	0	-238	106	6.28	6.28	9.42	9.42	2	0.02	0.01	0.06	0.00	0.00	24.0
4	38	-7553	-418	217	0	-300	170	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
5	38	-7385	-405	116	0	-240	167	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
6	38	-6972	-542	419	0	-370	133	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
7	38	-6410	-498	83	0	-168	124	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
8	38	-7331	-492	380	0	-370	151	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
9	38	-6769	-448	44	0	-169	143	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
10	38	-6356	-585	348	0	-299	109	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
11	38	-6188	-572	247	0	-238	106	6.28	6.28	9.42	9.42	2	0.02	0.01	0.06	0.00	0.00	24.0
12	38	-7553	-418	217	0	-300	170	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
13	38	-7385	-405	116	0	-240	167	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
14	38	-6972	-542	419	0	-370	133	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
15	38	-6410	-498	83	0	-168	124	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
16	38	-7331	-492	380	0	-370	151	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
17	38	-6769	-448	44	0	-169	143	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
18	38	-9128	-1128	684	0	-518	84	6.28	6.28	9.42	9.42	3	0.03	0.03	0.11	0.00	0.00	24.0
19	38	-11612	-269	21	0	-428	278	6.28	6.28	9.42	9.42	3	0.03	0.01	0.03	0.00	0.00	24.0
20	38	-9840	-673	151	0	-342	175	6.28	6.28	9.42	9.42	3	0.02	0.02	0.07	0.00	0.00	24.0
37	38	-7831	-1397	889	0	-508	19	6.28	6.28	9.42	9.42	3	0.02	0.04	0.14	0.00	0.00	24.0
38	38	-11972	34	-217	0	-358	342	6.28	6.28	9.42	9.42	3	0.04	0.00	0.02	0.00	0.00	24.0
39	38	-9018	-640	-0	0	-215	170	6.28	6.28	9.42	9.42	3	0.02	0.02	0.06	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-8859	-644	301	0	-388	99	6.28	6.28	9.42	9.42	3	0.02	0.02	0.06	0.00	0.00	24.0
2	50	-6300	-585	348	0	-342	35	6.28	6.28	9.42	9.42	2	0.02	0.01	0.06	0.00	0.00	24.0
3	50	-6132	-572	247	0	-269	34	6.28	6.28	9.42	9.42	2	0.02	0.01	0.06	0.00	0.00	24.0
4	50	-7497	-418	217	0	-327	118	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
5	50	-7329	-405	116	0	-254	117	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
6	50	-6916	-542	419	0	-422	65	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
7	50	-6354	-498	83	0	-179	62	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
8	50	-7275	-492	380	0	-417	90	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
9	50	-6713	-448	44	0	-174	87	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
10	50	-6300	-585	348	0	-342	35	6.28	6.28	9.42	9.42	2	0.02	0.01	0.06	0.00	0.00	24.0
11	50	-6132	-572	247	0	-269	34	6.28	6.28	9.42	9.42	2	0.02	0.01	0.06	0.00	0.00	24.0
12	50	-7497	-418	217	0	-327	118	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
13	50	-7329	-405	116	0	-254	117	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
14	50	-6916	-542	419	0	-422	65	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
15	50	-6354	-498	83	0	-179	62	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
16	50	-7275	-492	380	0	-417	90	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
17	50	-6713	-448	44	0	-174	87	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0

18	50	-9055	-1128	684	0	-604	-56	6.28	6.28	9.42	9.42	3	0.03	0.03	0.11	0.00	0.00	24.0
19	50	-11540	-269	21	0	-430	245	6.28	6.28	9.42	9.42	3	0.03	0.01	0.03	0.00	0.00	24.0
20	50	-9767	-673	151	0	-361	91	6.28	6.28	9.42	9.42	3	0.02	0.02	0.07	0.00	0.00	24.0
37	50	-7758	-1397	889	0	-619	-155	6.28	6.28	9.42	9.42	3	0.03	0.04	0.14	0.00	0.00	24.0
38	50	-11900	34	-217	0	-331	346	6.28	6.28	9.42	9.42	3	0.04	0.00	0.02	0.00	0.00	24.0
39	50	-8945	-640	-0	0	-215	91	6.28	6.28	9.42	9.42	3	0.01	0.02	0.06	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 101 NI 624 NF 293 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 1A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-11050	-4	-163	0	-395	76	6.28	6.28	9.42	9.42	3	0.02	0.00	0.02	0.00	0.00	24.0
2	0	-7942	-406	48	0	-360	6	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
3	0	-7777	-399	-131	0	-277	6	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
4	0	-9228	392	-120	0	-332	111	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
5	0	-9063	400	-298	0	-248	110	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
6	0	-8585	-136	198	0	-447	43	6.28	6.28	9.42	9.42	2	0.03	0.00	0.02	0.00	0.00	24.0
7	0	-8034	-110	-398	0	-170	42	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
8	0	-8971	104	148	0	-438	74	6.28	6.28	9.42	9.42	2	0.03	0.00	0.02	0.00	0.00	24.0
9	0	-8420	129	-448	0	-161	74	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
10	0	-7942	-406	48	0	-360	6	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
11	0	-7777	-399	-131	0	-277	6	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
12	0	-9228	392	-120	0	-332	111	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
13	0	-9063	400	-298	0	-248	110	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
14	0	-8585	-136	198	0	-447	43	6.28	6.28	9.42	9.42	2	0.03	0.00	0.02	0.00	0.00	24.0
15	0	-8034	-110	-398	0	-170	42	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
16	0	-8971	104	148	0	-438	74	6.28	6.28	9.42	9.42	2	0.03	0.00	0.02	0.00	0.00	24.0
17	0	-8420	129	-448	0	-161	74	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
18	0	-11850	-1665	310	0	-653	-113	6.28	6.28	9.42	9.42	3	0.03	0.04	0.16	0.00	0.00	24.0
19	0	-14090	1299	-313	0	-429	299	6.28	6.28	9.42	9.42	3	0.03	0.03	0.12	0.00	0.00	24.0
20	0	-12370	-161	-424	0	-362	89	6.28	6.28	9.42	9.42	3	0.02	0.01	0.05	0.00	0.00	24.0
37	0	-10470	-2596	466	0	-681	-256	6.28	6.28	9.42	9.42	3	0.04	0.07	0.25	0.00	0.00	24.0
38	0	-14210	2345	-572	0	-306	430	6.28	6.28	9.42	9.42	3	0.04	0.06	0.24	0.00	0.00	24.0
39	0	-11340	-88	-757	0	-195	80	6.28	6.28	9.42	9.42	3	0.01	0.02	0.09	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-10978	-4	-163	0	-375	75	6.28	6.28	9.42	9.42	3	0.02	0.00	0.02	0.00	0.00	24.0
2	12	-7886	-406	48	0	-366	-45	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
3	12	-7721	-399	-131	0	-260	-44	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
4	12	-9172	392	-120	0	-317	160	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
5	12	-9007	400	-298	0	-211	160	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
6	12	-8529	-136	198	0	-471	26	6.28	6.28	9.42	9.42	2	0.03	0.00	0.02	0.00	0.00	24.0
7	12	-7978	-110	-398	0	-120	29	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
8	12	-8915	104	148	0	-457	87	6.28	6.28	9.42	9.42	2	0.03	0.00	0.02	0.00	0.00	24.0
9	12	-8364	129	-448	0	-105	90	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
10	12	-7886	-406	48	0	-366	-45	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
11	12	-7721	-399	-131	0	-260	-44	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
12	12	-9172	392	-120	0	-317	160	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
13	12	-9007	400	-298	0	-211	160	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
14	12	-8529	-136	198	0	-471	26	6.28	6.28	9.42	9.42	2	0.03	0.00	0.02	0.00	0.00	24.0
15	12	-7978	-110	-398	0	-120	29	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
16	12	-8915	104	148	0	-457	87	6.28	6.28	9.42	9.42	2	0.03	0.00	0.02	0.00	0.00	24.0
17	12	-8364	129	-448	0	-105	90	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
18	12	-11775	-1665	310	0	-692	-321	6.28	6.28	9.42	9.42	3	0.04	0.04	0.16	0.00	0.00	24.0
19	12	-14018	1299	-313	0	-389	461	6.28	6.28	9.42	9.42	3	0.05	0.03	0.13	0.00	0.00	24.0
20	12	-12295	-161	-424	0	-309	69	6.28	6.28	9.42	9.42	3	0.02	0.01	0.05	0.00	0.00	24.0
37	12	-10398	-2596	466	0	-739	-581	6.28	6.28	9.42	9.42	3	0.06	0.07	0.25	0.00	0.00	24.0
38	12	-14138	2345	-572	0	-235	723	6.28	6.28	9.42	9.42	3	0.07	0.06	0.24	0.00	0.00	24.0
39	12	-11268	-88	-757	0	-100	70	6.28	6.28	9.42	9.42	3	0.01	0.02	0.09	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-10905	-4	-163	0	-355	75	6.28	6.28	9.42	9.42	3	0.02	0.00	0.02	0.00	0.00	24.0
2	25	-7830	-406	48	0	-372	-96	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
3	25	-7664	-399	-131	0	-244	-94	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
4	25	-9116	392	-120	0	-302	209	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
5	25	-8950	400	-298	0	-174	210	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
6	25	-8472	-136	198	0	-496	9	6.28	6.28	9.42	9.42	2	0.03	0.00	0.02	0.00	0.00	24.0
7	25	-7922	-110	-398	0	-70	15	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
8	25	-8858	104	148	0	-475	100	6.28	6.28	9.42	9.42	2	0.03	0.00	0.02	0.00	0.00	24.0
9	25	-8308	129	-448	0	-49	106	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
10	25	-7830	-406	48	0	-372	-96	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
11	25	-7664	-399	-131	0	-244	-94	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
12	25	-9116	392	-120	0	-302	209	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
13	25	-8950	400	-298	0	-174	210	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
14	25	-8472	-136	198	0	-496	9	6.28	6.28	9.42	9.42	2	0.03	0.00	0.02	0.00	0.00	24.0
15	25	-7922	-110	-398	0	-70	15	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
16	25	-8858	104	148	0	-475	100	6.28	6.28	9.42	9.42	2	0.03	0.00	0.02	0.00	0.00	24.0
17	25	-8308	129	-448	0	-49	106	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
18	25	-11700	-1665	310	0	-731	-530	6.28	6.28	9.42	9.42	3	0.06	0.04	0.16	0.00	0.00	24.0
19	25	-13945	1299	-313	0	-350	623	6.28	6.28	9.42	9.42	3	0.06	0.03	0.13	0.00	0.00	24.0
20	25	-12220	-161	-424	0	-256	49	6.28	6.28	9.42	9.42	3	0.01	0.01	0.05	0.00	0.00	24.0
37	25	-10325	-2596	466	0	-798	-905	6.28	6.28	9.42	9.42	3	0.10	0.07	0.28	0.00	0.00	24.0
38	25	-14065	2345	-572	0	-163	1017	6.28	6.28	9.42	9.42	3	0.10	0.06	0.24	0.00	0.00	24.0
39	25	-11195	-88	-757	0	-6	59	6.28	6.28	9.42	9.42	3	0.01	0.02	0.09	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-10832	-4	-163	0	-334	74	6.28	6.28	9.42	9.42	3	0.02	0.00	0.02	0.00	0.00	24.0
2	38	-7773	-406	48	0	-378	-147	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
3	38	-7608	-399	-131	0	-228	-144	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
4	38	-9059	392	-120	0	-287	258	6.28	6.28	9.42	9.42	2	0.04	0.01	0.04	0.00	0.00	24.0
5	38	-8894	400	-298	0	-136	260	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
6	38	-8416	-136	198	0	-521	-8	6.28	6.28	9.42	9.42	2	0.03	0.00	0.02	0.00	0.00	24.0
7	38	-7865	-110	-398	0	-21	1	6.28	6.28	9.42	9.42	2	0.00	0.01	0.05	0.00	0.00	24.0
8	38	-8802	104	148	0	-494	113	6.28	6.28	9.42	9.42	2	0.04	0.00	0.02	0.00	0.00	24.0
9	38	-8251	129	-448	0	7	122	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
10	38	-7773	-406	48	0	-378	-147	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
11	38	-7608	-399	-131	0	-228	-144	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
12	38	-9059	392	-120	0	-287	258	6.28	6.28	9.42	9.42	2	0.04	0.01	0.04	0.00	0.00	24.0
13	38	-8894	400	-298	0	-136	260	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0

14	38	-8416	-136	198	0	-521	-8	6.28	6.28	9.42	9.42	2	0.03	0.00	0.02	0.00	0.00	24.0
15	38	-7865	-110	-398	0	-21	1	6.28	6.28	9.42	9.42	2	0.00	0.01	0.05	0.00	0.00	24.0
16	38	-8802	104	148	0	-494	113	6.28	6.28	9.42	9.42	2	0.04	0.00	0.02	0.00	0.00	24.0
17	38	-8251	129	-448	0	7	122	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
18	38	-11625	-1665	310	0	-770	-738	6.28	6.28	9.42	9.42	3	0.08	0.04	0.16	0.00	0.00	24.0
19	38	-13872	1299	-313	0	-311	786	6.28	6.28	9.42	9.42	3	0.08	0.03	0.13	0.00	0.00	24.0
20	38	-12145	-161	-424	0	-203	29	6.28	6.28	9.42	9.42	3	0.01	0.01	0.05	0.00	0.00	24.0
37	38	-10252	-2596	466	0	-856	-1230	6.28	6.28	9.42	9.42	3	0.13	0.07	0.28	0.00	0.00	24.0
38	38	-13992	2345	-572	0	-92	1310	6.28	6.28	9.42	9.42	3	0.13	0.06	0.24	0.00	0.00	24.0
39	38	-11122	-88	-757	0	89	48	6.28	6.28	9.42	9.42	3	0.01	0.02	0.09	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-10760	-4	-163	0	-314	74	6.28	6.28	9.42	9.42	3	0.02	0.00	0.02	0.00	0.00	24.0
2	50	-7717	-406	48	0	-384	-197	6.28	6.28	9.42	9.42	2	0.04	0.01	0.04	0.00	0.00	24.0
3	50	-7552	-399	-131	0	-211	-194	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
4	50	-9003	392	-120	0	-272	307	6.28	6.28	9.42	9.42	2	0.04	0.01	0.04	0.00	0.00	24.0
5	50	-8838	400	-298	0	-99	310	6.28	6.28	9.42	9.42	2	0.04	0.01	0.04	0.00	0.00	24.0
6	50	-8360	-136	198	0	-546	-25	6.28	6.28	9.42	9.42	2	0.03	0.00	0.02	0.00	0.00	24.0
7	50	-7809	-110	-398	0	29	-13	6.28	6.28	9.42	9.42	2	0.00	0.01	0.05	0.00	0.00	24.0
8	50	-8746	104	148	0	-512	126	6.28	6.28	9.42	9.42	2	0.04	0.00	0.02	0.00	0.00	24.0
9	50	-8195	129	-448	0	63	138	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
10	50	-7717	-406	48	0	-384	-197	6.28	6.28	9.42	9.42	2	0.04	0.01	0.04	0.00	0.00	24.0
11	50	-7552	-399	-131	0	-211	-194	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
12	50	-9003	392	-120	0	-272	307	6.28	6.28	9.42	9.42	2	0.04	0.01	0.04	0.00	0.00	24.0
13	50	-8838	400	-298	0	-99	310	6.28	6.28	9.42	9.42	2	0.04	0.01	0.04	0.00	0.00	24.0
14	50	-8360	-136	198	0	-546	-25	6.28	6.28	9.42	9.42	2	0.03	0.00	0.02	0.00	0.00	24.0
15	50	-7809	-110	-398	0	29	-13	6.28	6.28	9.42	9.42	2	0.00	0.01	0.05	0.00	0.00	24.0
16	50	-8746	104	148	0	-512	126	6.28	6.28	9.42	9.42	2	0.04	0.00	0.02	0.00	0.00	24.0
17	50	-8195	129	-448	0	63	138	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
18	50	-11550	-1665	310	0	-808	-946	6.28	6.28	9.42	9.42	3	0.10	0.04	0.18	0.00	0.00	24.0
19	50	-13800	1299	-313	0	-272	948	6.28	6.28	9.42	9.42	3	0.09	0.03	0.13	0.00	0.00	24.0
20	50	-12070	-161	-424	0	-150	9	6.28	6.28	9.42	9.42	3	0.01	0.01	0.05	0.00	0.00	24.0
37	50	-10180	-2596	466	0	-914	-1554	6.28	6.28	9.42	9.42	3	0.16	0.07	0.28	0.00	0.00	24.0
38	50	-13920	2345	-572	0	-20	1603	6.28	6.28	9.42	9.42	3	0.16	0.06	0.24	0.00	0.00	24.0
39	50	-11050	-88	-757	0	183	37	6.28	6.28	9.42	9.42	3	0.01	0.02	0.09	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 102 NI 218 NF 132 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 12
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	--													Bielle	V,Mx			
	cm		daN			daN*m				cmq			Fx,M			cmq/m		cm
1	0	-7502	169	-27	0	117	-17	6.28	6.28	12.57	12.57	3	0.00	0.00	0.01	0.00	0.00	24.0
2	0	-5774	126	-2	0	58	-13	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
3	0	-5782	125	-57	0	168	-13	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
4	0	-5759	135	16	0	11	-13	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
5	0	-5767	134	-40	0	122	-13	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
6	0	-5759	131	70	0	-88	-13	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
7	0	-5786	126	-116	0	281	-13	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
8	0	-5755	134	75	0	-102	-13	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
9	0	-5782	129	-110	0	267	-13	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
10	0	-5774	126	-2	0	58	-13	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
11	0	-5782	125	-57	0	168	-13	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
12	0	-5759	135	16	0	11	-13	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
13	0	-5767	134	-40	0	122	-13	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
14	0	-5759	131	70	0	-88	-13	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
15	0	-5786	126	-116	0	281	-13	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
16	0	-5755	134	75	0	-102	-13	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
17	0	-5782	129	-110	0	267	-13	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
18	0	-8524	53	-144	0	482	-6	6.28	6.28	12.57	12.57	3	0.02	0.00	0.01	0.00	0.00	24.0
19	0	-7995	274	17	0	46	-20	6.28	6.28	12.57	12.57	3	0.00	0.01	0.02	0.00	0.00	24.0
20	0	-8160	142	-305	0	2370	-10	6.28	6.28	12.57	12.57	3	0.09	0.01	0.03	0.00	0.00	24.0
37	0	-8490	-18	-187	0	580	-2	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
38	0	-7608	350	82	0	-145	-27	6.28	6.28	12.57	12.57	3	0.01	0.01	0.03	0.00	0.00	24.0
39	0	-7884	130	-454	0	3728	-9	6.28	6.28	12.57	12.57	3	0.14	0.01	0.05	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-7404	169	-27	0	120	4	6.28	6.28	12.57	12.57	3	0.00	0.00	0.01	0.00	0.00	24.0
2	12	-5699	126	-2	0	58	3	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
3	12	-5707	125	-57	0	176	3	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
4	12	-5684	135	16	0	9	4	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
5	12	-5692	134	-40	0	127	4	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
6	12	-5684	131	70	0	-97	3	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
7	12	-5711	126	-116	0	296	3	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
8	12	-5680	134	75	0	-111	3	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
9	12	-5707	129	-110	0	281	4	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
10	12	-5699	126	-2	0	58	3	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
11	12	-5707	125	-57	0	176	3	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
12	12	-5684	135	16	0	9	4	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
13	12	-5692	134	-40	0	127	4	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
14	12	-5684	131	70	0	-97	3	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
15	12	-5711	126	-116	0	296	3	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
16	12	-5680	134	75	0	-111	3	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
17	12	-5707	129	-110	0	281	4	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
18	12	-8426	53	-144	0	500	1	6.28	6.28	12.57	12.57	3	0.02	0.00	0.01	0.00	0.00	24.0
19	12	-7898	274	17	0	44	14	6.28	6.28	12.57	12.57	3	0.00	0.01	0.02	0.00	0.00	24.0
20	12	-8062	142	-305	0	2408	8	6.28	6.28	12.57	12.57	3	0.09	0.01	0.03	0.00	0.00	24.0
37	12	-8392	-18	-187	0	604	-4	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
38	12	-7510	350	82	0	-155	17	6.28	6.28	12.57	12.57	3	0.01	0.01	0.03	0.00	0.00	24.0
39	12	-7786	130	-454	0	3785	8	6.28	6.28	12.57	12.57	3	0.14	0.01	0.05	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-7307	169	-27	0	123	25	6.28	6.28	12.57	12.57	3	0.00	0.00	0.01	0.00	0.00	24.0
2	25	-5624	126	-2	0	58	18	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
3	25	-5632	125	-57	0	183	18	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
4	25	-5609	135	16	0	7	21	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
5	25	-5617	134	-40	0	132	21	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
6	25	-5609	131	70	0	-105	19	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
7	25	-5636	126	-116	0	310	19	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
8	25	-5605	134	75	0	-121	20	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
9	25	-5632	129	-110	0	295	20	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0

10	25	-5624	126	-2	0	58	18	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
11	25	-5632	125	-57	0	183	18	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
12	25	-5609	135	16	0	7	21	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
13	25	-5617	134	-40	0	132	21	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
14	25	-5609	131	70	0	-105	19	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
15	25	-5636	126	-116	0	310	19	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
16	25	-5605	134	75	0	-121	20	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
17	25	-5632	129	-110	0	295	20	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
18	25	-8329	53	-144	0	518	8	6.28	6.28	12.57	12.57	3	0.02	0.00	0.01	0.00	0.00	24.0
19	25	-7800	274	17	0	42	48	6.28	6.28	12.57	12.57	3	0.00	0.01	0.03	0.00	0.00	24.0
20	25	-7965	142	-305	0	2446	26	6.28	6.28	12.57	12.57	3	0.09	0.01	0.03	0.00	0.00	24.0
37	25	-8295	-18	-187	0	627	-6	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
38	25	-7413	350	82	0	-166	61	6.28	6.28	12.57	12.57	3	0.01	0.01	0.03	0.00	0.00	24.0
39	25	-7689	130	-454	0	3842	24	6.28	6.28	12.57	12.57	3	0.14	0.01	0.05	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-7210	169	-27	0	127	46	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
2	38	-5549	126	-2	0	58	34	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
3	38	-5557	125	-57	0	190	34	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
4	38	-5534	135	16	0	5	38	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
5	38	-5542	134	-40	0	137	37	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
6	38	-5534	131	70	0	-114	36	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
7	38	-5561	126	-116	0	325	35	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
8	38	-5530	134	75	0	-130	37	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
9	38	-5557	129	-110	0	309	36	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
10	38	-5549	126	-2	0	58	34	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
11	38	-5557	125	-57	0	190	34	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
12	38	-5534	135	16	0	5	38	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
13	38	-5542	134	-40	0	137	37	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
14	38	-5534	131	70	0	-114	36	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
15	38	-5561	126	-116	0	325	35	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
16	38	-5530	134	75	0	-130	37	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
17	38	-5557	129	-110	0	309	36	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
18	38	-8232	53	-144	0	536	14	6.28	6.28	12.57	12.57	3	0.02	0.00	0.01	0.00	0.00	24.0
19	38	-7702	274	17	0	40	82	6.28	6.28	12.57	12.57	3	0.00	0.01	0.03	0.00	0.00	24.0
20	38	-7868	142	-305	0	2485	44	6.28	6.28	12.57	12.57	3	0.09	0.01	0.03	0.00	0.00	24.0
37	38	-8198	-18	-187	0	651	-9	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
38	38	-7316	350	82	0	-176	104	6.28	6.28	12.57	12.57	3	0.01	0.01	0.03	0.00	0.00	24.0
39	38	-7592	130	-454	0	3898	40	6.28	6.28	12.57	12.57	3	0.14	0.01	0.05	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-7112	169	-27	0	130	68	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
2	50	-5474	126	-2	0	58	50	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
3	50	-5482	125	-57	0	197	49	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
4	50	-5459	135	16	0	3	55	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
5	50	-5467	134	-40	0	141	54	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
6	50	-5459	131	70	0	-123	52	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
7	50	-5486	126	-116	0	339	50	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
8	50	-5455	134	75	0	-139	54	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
9	50	-5482	129	-110	0	323	52	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
10	50	-5474	126	-2	0	58	50	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
11	50	-5482	125	-57	0	197	49	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
12	50	-5459	135	16	0	3	55	6.28	6.28	12.57	12.57	2	0.00	0.00	0.01	0.00	0.00	24.0
13	50	-5467	134	-40	0	141	54	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
14	50	-5459	131	70	0	-123	52	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
15	50	-5486	126	-116	0	339	50	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
16	50	-5455	134	75	0	-139	54	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
17	50	-5482	129	-110	0	323	52	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
18	50	-8134	53	-144	0	554	21	6.28	6.28	12.57	12.57	3	0.02	0.00	0.01	0.00	0.00	24.0
19	50	-7605	274	17	0	38	116	6.28	6.28	12.57	12.57	3	0.01	0.01	0.03	0.00	0.00	24.0
20	50	-7770	142	-305	0	2523	61	6.28	6.28	12.57	12.57	3	0.09	0.01	0.03	0.00	0.00	24.0
37	50	-8100	-18	-187	0	674	-11	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
38	50	-7218	350	82	0	-186	148	6.28	6.28	12.57	12.57	3	0.01	0.01	0.03	0.00	0.00	24.0
39	50	-7494	130	-454	0	3955	56	6.28	6.28	12.57	12.57	3	0.15	0.01	0.05	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 103 NI 132 NF 40 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 12A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-11210	671	-47	0	122	68	6.28	6.28	12.57	12.57	3	0.01	0.01	0.06	0.00	0.00	24.0
2	0	-8631	491	-2	0	51	50	6.28	6.28	12.57	12.57	2	0.00	0.01	0.04	0.00	0.00	24.0
3	0	-8642	487	-101	0	190	49	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
4	0	-8604	545	30	0	-3	55	6.28	6.28	12.57	12.57	2	0.00	0.01	0.05	0.00	0.00	24.0
5	0	-8615	541	-70	0	136	54	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
6	0	-8609	514	126	0	-129	52	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
7	0	-8645	502	-207	0	333	50	6.28	6.28	12.57	12.57	2	0.02	0.01	0.04	0.00	0.00	24.0
8	0	-8601	531	135	0	-146	54	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
9	0	-8637	518	-197	0	316	52	6.28	6.28	12.57	12.57	2	0.02	0.01	0.04	0.00	0.00	24.0
10	0	-8631	491	-2	0	51	50	6.28	6.28	12.57	12.57	2	0.00	0.01	0.04	0.00	0.00	24.0
11	0	-8642	487	-101	0	190	49	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
12	0	-8604	545	30	0	-3	55	6.28	6.28	12.57	12.57	2	0.00	0.01	0.05	0.00	0.00	24.0
13	0	-8615	541	-70	0	136	54	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
14	0	-8609	514	126	0	-129	52	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
15	0	-8645	502	-207	0	333	50	6.28	6.28	12.57	12.57	2	0.02	0.01	0.04	0.00	0.00	24.0
16	0	-8601	531	135	0	-146	54	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
17	0	-8637	518	-197	0	316	52	6.28	6.28	12.57	12.57	2	0.02	0.01	0.04	0.00	0.00	24.0
18	0	-12840	235	-255	0	528	21	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
19	0	-11970	1187	32	0	27	116	6.28	6.28	12.57	12.57	3	0.01	0.02	0.11	0.00	0.00	24.0
20	0	-12230	649	-514	0	2287	61	6.28	6.28	12.57	12.57	3	0.08	0.01	0.05	0.00	0.00	24.0
37	0	-12800	-94	-331	0	646	-11	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
38	0	-11350	1494	148	0	-189	148	6.28	6.28	12.57	12.57	3	0.01	0.03	0.12	0.00	0.00	24.0
39	0	-11780	596	-761	0	3578	56	6.28	6.28	12.57	12.57	3	0.13	0.01	0.07	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-11112	671	-47	0	127	151	6.28	6.28	12.57	12.57	3	0.01	0.01	0.06	0.00	0.00	24.0
2	12	-8556	491	-2	0	51	111	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
3	12	-8567	487	-101	0	202	110	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
4	12	-8529	545	30	0	-7	123	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
5	12	-8540	541	-70	0	145	122	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0

6	12	-8534	514	126	0	-145	116	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
7	12	-8570	502	-207	0	359	113	6.28	6.28	12.57	12.57	2	0.02	0.01	0.04	0.00	0.00	24.0
8	12	-8526	531	135	0	-163	120	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
9	12	-8562	518	-197	0	341	117	6.28	6.28	12.57	12.57	2	0.02	0.01	0.04	0.00	0.00	24.0
10	12	-8556	491	-2	0	51	111	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
11	12	-8567	487	-101	0	202	110	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
12	12	-8529	545	30	0	-7	123	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
13	12	-8540	541	-70	0	145	122	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
14	12	-8534	514	126	0	-145	116	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
15	12	-8570	502	-207	0	359	113	6.28	6.28	12.57	12.57	2	0.02	0.01	0.04	0.00	0.00	24.0
16	12	-8526	531	135	0	-163	120	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
17	12	-8562	518	-197	0	341	117	6.28	6.28	12.57	12.57	2	0.02	0.01	0.04	0.00	0.00	24.0
18	12	-12742	235	-255	0	560	51	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
19	12	-11872	1187	32	0	23	265	6.28	6.28	12.57	12.57	3	0.01	0.02	0.11	0.00	0.00	24.0
20	12	-12132	649	-514	0	2351	142	6.28	6.28	12.57	12.57	3	0.08	0.01	0.05	0.00	0.00	24.0
37	12	-12702	-94	-331	0	688	-22	6.28	6.28	12.57	12.57	3	0.02	0.01	0.03	0.00	0.00	24.0
38	12	-11252	1494	148	0	-208	335	6.28	6.28	12.57	12.57	3	0.02	0.03	0.14	0.00	0.00	24.0
39	12	-11682	596	-761	0	3673	131	6.28	6.28	12.57	12.57	3	0.13	0.01	0.07	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-11015	671	-47	0	133	235	6.28	6.28	12.57	12.57	3	0.01	0.01	0.06	0.00	0.00	24.0
2	25	-8481	491	-2	0	52	173	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
3	25	-8492	487	-101	0	215	171	6.28	6.28	12.57	12.57	2	0.02	0.01	0.04	0.00	0.00	24.0
4	25	-8454	545	30	0	-10	191	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
5	25	-8465	541	-70	0	153	189	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
6	25	-8459	514	126	0	-161	181	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
7	25	-8495	502	-207	0	384	176	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
8	25	-8451	531	135	0	-179	186	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
9	25	-8487	518	-197	0	366	181	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
10	25	-8481	491	-2	0	52	173	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
11	25	-8492	487	-101	0	215	171	6.28	6.28	12.57	12.57	2	0.02	0.01	0.04	0.00	0.00	24.0
12	25	-8454	545	30	0	-10	191	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
13	25	-8465	541	-70	0	153	189	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
14	25	-8459	514	126	0	-161	181	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
15	25	-8495	502	-207	0	384	176	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
16	25	-8451	531	135	0	-179	186	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
17	25	-8487	518	-197	0	366	181	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
18	25	-12645	235	-255	0	592	80	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
19	25	-11775	1187	32	0	19	413	6.28	6.28	12.57	12.57	3	0.02	0.02	0.11	0.00	0.00	24.0
20	25	-12035	649	-514	0	2415	224	6.28	6.28	12.57	12.57	3	0.09	0.01	0.05	0.00	0.00	24.0
37	25	-12605	-94	-331	0	729	-34	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
38	25	-11155	1494	148	0	-226	522	6.28	6.28	12.57	12.57	3	0.03	0.03	0.14	0.00	0.00	24.0
39	25	-11585	596	-761	0	3768	205	6.28	6.28	12.57	12.57	3	0.14	0.01	0.07	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-10918	671	-47	0	139	319	6.28	6.28	12.57	12.57	3	0.02	0.01	0.06	0.00	0.00	24.0
2	38	-8406	491	-2	0	52	234	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
3	38	-8417	487	-101	0	228	232	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
4	38	-8379	545	30	0	-14	259	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
5	38	-8390	541	-70	0	162	257	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
6	38	-8384	514	126	0	-177	245	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
7	38	-8420	502	-207	0	410	239	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
8	38	-8376	531	135	0	-196	252	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
9	38	-8412	518	-197	0	391	246	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
10	38	-8406	491	-2	0	52	234	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
11	38	-8417	487	-101	0	228	232	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
12	38	-8379	545	30	0	-14	259	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
13	38	-8390	541	-70	0	162	257	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
14	38	-8384	514	126	0	-177	245	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
15	38	-8420	502	-207	0	410	239	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
16	38	-8376	531	135	0	-196	252	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
17	38	-8412	518	-197	0	391	246	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
18	38	-12548	235	-255	0	624	109	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
19	38	-11678	1187	32	0	15	562	6.28	6.28	12.57	12.57	3	0.03	0.02	0.11	0.00	0.00	24.0
20	38	-11938	649	-514	0	2480	305	6.28	6.28	12.57	12.57	3	0.09	0.01	0.05	0.00	0.00	24.0
37	38	-12508	-94	-331	0	771	-46	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
38	38	-11058	1494	148	0	-245	708	6.28	6.28	12.57	12.57	3	0.04	0.03	0.14	0.00	0.00	24.0
39	38	-11488	596	-761	0	3863	280	6.28	6.28	12.57	12.57	3	0.14	0.01	0.07	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-10820	671	-47	0	145	403	6.28	6.28	12.57	12.57	3	0.02	0.01	0.06	0.00	0.00	24.0
2	50	-8331	491	-2	0	52	295	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
3	50	-8342	487	-101	0	240	293	6.28	6.28	12.57	12.57	2	0.03	0.01	0.05	0.00	0.00	24.0
4	50	-8304	545	30	0	-18	327	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
5	50	-8315	541	-70	0	171	325	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
6	50	-8309	514	126	0	-192	309	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
7	50	-8345	502	-207	0	436	301	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
8	50	-8301	531	135	0	-213	319	6.28	6.28	12.57	12.57	2	0.03	0.01	0.05	0.00	0.00	24.0
9	50	-8337	518	-197	0	415	311	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
10	50	-8331	491	-2	0	52	295	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
11	50	-8342	487	-101	0	240	293	6.28	6.28	12.57	12.57	2	0.03	0.01	0.05	0.00	0.00	24.0
12	50	-8304	545	30	0	-18	327	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
13	50	-8315	541	-70	0	171	325	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
14	50	-8309	514	126	0	-192	309	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
15	50	-8345	502	-207	0	436	301	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
16	50	-8301	531	135	0	-213	319	6.28	6.28	12.57	12.57	2	0.03	0.01	0.05	0.00	0.00	24.0
17	50	-8337	518	-197	0	415	311	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
18	50	-12450	235	-255	0	656	138	6.28	6.28	12.57	12.57	3	0.03	0.00	0.02	0.00	0.00	24.0
19	50	-11580	1187	32	0	11	710	6.28	6.28	12.57	12.57	3	0.04	0.02	0.11	0.00	0.00	24.0
20	50	-11840	649	-514	0	2544	386	6.28	6.28	12.57	12.57	3	0.10	0.01	0.05	0.00	0.00	24.0
37	50	-12410	-94	-331	0	812	-58	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
38	50	-10960	1494	148	0	-263	895	6.28	6.28	12.57	12.57	3	0.05	0.03	0.14	0.00	0.00	24.0
39	50	-11390	596	-761	0	3958	354	6.28	6.28	12.57	12.57	3	0.14	0.01	0.07	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 104 NI 1350 NF 1445 SEZ. Rp B= 0.400 H= 0.600 (pilastro)
PIL. NUM. 11
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-8432	488	440	0	833	-2148	12.57	12.57	6.28	6.28	3	0.09	0.01	0.05	0.00	0.00	24.0

2	0	-6294	642	337	0	644	-2517	12.57	12.57	6.28	6.28	2	0.15	0.01	0.07	0.00	0.00	24.0
3	0	-6398	645	370	0	718	-2530	12.57	12.57	6.28	6.28	2	0.16	0.01	0.07	0.00	0.00	24.0
4	0	-6573	106	307	0	564	-774	12.57	12.57	6.28	6.28	2	0.06	0.01	0.03	0.00	0.00	24.0
5	0	-6678	110	340	0	638	-787	12.57	12.57	6.28	6.28	2	0.07	0.01	0.03	0.00	0.00	24.0
6	0	-6269	450	288	0	529	-1892	12.57	12.57	6.28	6.28	2	0.12	0.01	0.05	0.00	0.00	24.0
7	0	-6618	462	398	0	776	-1935	12.57	12.57	6.28	6.28	2	0.13	0.01	0.05	0.00	0.00	24.0
8	0	-6353	289	279	0	505	-1369	12.57	12.57	6.28	6.28	2	0.09	0.01	0.03	0.00	0.00	24.0
9	0	-6702	302	389	0	752	-1412	12.57	12.57	6.28	6.28	2	0.10	0.01	0.03	0.00	0.00	24.0
10	0	-6294	642	337	0	644	-2517	12.57	12.57	6.28	6.28	2	0.15	0.01	0.07	0.00	0.00	24.0
11	0	-6398	645	370	0	718	-2530	12.57	12.57	6.28	6.28	2	0.16	0.01	0.07	0.00	0.00	24.0
12	0	-6573	106	307	0	564	-774	12.57	12.57	6.28	6.28	2	0.06	0.01	0.03	0.00	0.00	24.0
13	0	-6678	110	340	0	638	-787	12.57	12.57	6.28	6.28	2	0.07	0.01	0.03	0.00	0.00	24.0
14	0	-6269	450	288	0	529	-1892	12.57	12.57	6.28	6.28	2	0.12	0.01	0.05	0.00	0.00	24.0
15	0	-6618	462	398	0	776	-1935	12.57	12.57	6.28	6.28	2	0.13	0.01	0.05	0.00	0.00	24.0
16	0	-6353	289	279	0	505	-1369	12.57	12.57	6.28	6.28	2	0.09	0.01	0.03	0.00	0.00	24.0
17	0	-6702	302	389	0	752	-1412	12.57	12.57	6.28	6.28	2	0.10	0.01	0.03	0.00	0.00	24.0
18	0	-7889	1768	502	0	1011	-6261	12.57	12.57	6.28	6.28	3	0.24	0.03	0.18	0.00	0.00	24.0
19	0	-8902	-2	427	0	790	-513	12.57	12.57	6.28	6.28	3	0.05	0.01	0.04	0.00	0.00	24.0
20	0	-8424	830	419	0	763	-3217	12.57	12.57	6.28	6.28	3	0.13	0.01	0.08	0.00	0.00	24.0
37	0	-7515	2229	516	0	1058	-7771	12.57	12.57	6.28	6.28	3	0.30	0.04	0.23	0.00	0.00	24.0
38	0	-9203	-721	390	0	690	1809	12.57	12.57	6.28	6.28	3	0.08	0.01	0.07	0.00	0.00	24.0
39	0	-8406	665	378	0	645	-2699	12.57	12.57	6.28	6.28	3	0.11	0.01	0.07	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-8334	488	440	0	778	-2087	12.57	12.57	6.28	6.28	3	0.09	0.01	0.05	0.00	0.00	24.0
2	12	-6219	642	337	0	601	-2437	12.57	12.57	6.28	6.28	2	0.15	0.01	0.07	0.00	0.00	24.0
3	12	-6323	645	370	0	671	-2450	12.57	12.57	6.28	6.28	2	0.15	0.01	0.07	0.00	0.00	24.0
4	12	-6498	106	307	0	525	-760	12.57	12.57	6.28	6.28	2	0.06	0.01	0.03	0.00	0.00	24.0
5	12	-6603	110	340	0	595	-773	12.57	12.57	6.28	6.28	2	0.06	0.01	0.03	0.00	0.00	24.0
6	12	-6194	450	288	0	493	-1836	12.57	12.57	6.28	6.28	2	0.11	0.01	0.05	0.00	0.00	24.0
7	12	-6543	462	398	0	726	-1877	12.57	12.57	6.28	6.28	2	0.12	0.01	0.05	0.00	0.00	24.0
8	12	-6278	289	279	0	470	-1333	12.57	12.57	6.28	6.28	2	0.09	0.01	0.03	0.00	0.00	24.0
9	12	-6627	302	389	0	704	-1374	12.57	12.57	6.28	6.28	2	0.10	0.01	0.03	0.00	0.00	24.0
10	12	-6219	642	337	0	601	-2437	12.57	12.57	6.28	6.28	2	0.15	0.01	0.07	0.00	0.00	24.0
11	12	-6323	645	370	0	671	-2450	12.57	12.57	6.28	6.28	2	0.15	0.01	0.07	0.00	0.00	24.0
12	12	-6498	106	307	0	525	-760	12.57	12.57	6.28	6.28	2	0.06	0.01	0.03	0.00	0.00	24.0
13	12	-6603	110	340	0	595	-773	12.57	12.57	6.28	6.28	2	0.06	0.01	0.03	0.00	0.00	24.0
14	12	-6194	450	288	0	493	-1836	12.57	12.57	6.28	6.28	2	0.11	0.01	0.05	0.00	0.00	24.0
15	12	-6543	462	398	0	726	-1877	12.57	12.57	6.28	6.28	2	0.12	0.01	0.05	0.00	0.00	24.0
16	12	-6278	289	279	0	470	-1333	12.57	12.57	6.28	6.28	2	0.09	0.01	0.03	0.00	0.00	24.0
17	12	-6627	302	389	0	704	-1374	12.57	12.57	6.28	6.28	2	0.10	0.01	0.03	0.00	0.00	24.0
18	12	-7792	1768	502	0	948	-6040	12.57	12.57	6.28	6.28	3	0.23	0.03	0.18	0.00	0.00	24.0
19	12	-8804	-2	427	0	737	-513	12.57	12.57	6.28	6.28	3	0.04	0.01	0.04	0.00	0.00	24.0
20	12	-8326	830	419	0	711	-3113	12.57	12.57	6.28	6.28	3	0.12	0.01	0.08	0.00	0.00	24.0
37	12	-7418	2229	516	0	993	-7492	12.57	12.57	6.28	6.28	3	0.29	0.04	0.23	0.00	0.00	24.0
38	12	-9106	-721	390	0	641	1719	12.57	12.57	6.28	6.28	3	0.07	0.01	0.07	0.00	0.00	24.0
39	12	-8308	665	378	0	598	-2616	12.57	12.57	6.28	6.28	3	0.10	0.01	0.07	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-8237	488	440	0	723	-2025	12.57	12.57	6.28	6.28	3	0.09	0.01	0.05	0.00	0.00	24.0
2	25	-6144	642	337	0	559	-2357	12.57	12.57	6.28	6.28	2	0.14	0.01	0.07	0.00	0.00	24.0
3	25	-6248	645	370	0	625	-2369	12.57	12.57	6.28	6.28	2	0.15	0.01	0.07	0.00	0.00	24.0
4	25	-6423	106	307	0	487	-747	12.57	12.57	6.28	6.28	2	0.06	0.01	0.03	0.00	0.00	24.0
5	25	-6528	110	340	0	553	-759	12.57	12.57	6.28	6.28	2	0.06	0.01	0.03	0.00	0.00	24.0
6	25	-6119	450	288	0	457	-1780	12.57	12.57	6.28	6.28	2	0.11	0.01	0.05	0.00	0.00	24.0
7	25	-6468	462	398	0	677	-1820	12.57	12.57	6.28	6.28	2	0.12	0.01	0.05	0.00	0.00	24.0
8	25	-6203	289	279	0	435	-1297	12.57	12.57	6.28	6.28	2	0.08	0.01	0.03	0.00	0.00	24.0
9	25	-6552	302	389	0	655	-1336	12.57	12.57	6.28	6.28	2	0.09	0.01	0.03	0.00	0.00	24.0
10	25	-6144	642	337	0	559	-2357	12.57	12.57	6.28	6.28	2	0.14	0.01	0.07	0.00	0.00	24.0
11	25	-6248	645	370	0	625	-2369	12.57	12.57	6.28	6.28	2	0.15	0.01	0.07	0.00	0.00	24.0
12	25	-6423	106	307	0	487	-747	12.57	12.57	6.28	6.28	2	0.06	0.01	0.03	0.00	0.00	24.0
13	25	-6528	110	340	0	553	-759	12.57	12.57	6.28	6.28	2	0.06	0.01	0.03	0.00	0.00	24.0
14	25	-6119	450	288	0	457	-1780	12.57	12.57	6.28	6.28	2	0.11	0.01	0.05	0.00	0.00	24.0
15	25	-6468	462	398	0	677	-1820	12.57	12.57	6.28	6.28	2	0.12	0.01	0.05	0.00	0.00	24.0
16	25	-6203	289	279	0	435	-1297	12.57	12.57	6.28	6.28	2	0.08	0.01	0.03	0.00	0.00	24.0
17	25	-6552	302	389	0	655	-1336	12.57	12.57	6.28	6.28	2	0.09	0.01	0.03	0.00	0.00	24.0
18	25	-7694	1768	502	0	885	-5819	12.57	12.57	6.28	6.28	3	0.22	0.03	0.18	0.00	0.00	24.0
19	25	-8707	-2	427	0	683	-513	12.57	12.57	6.28	6.28	3	0.04	0.01	0.04	0.00	0.00	24.0
20	25	-8229	830	419	0	658	-3009	12.57	12.57	6.28	6.28	3	0.12	0.01	0.08	0.00	0.00	24.0
37	25	-7320	2229	516	0	929	-7214	12.57	12.57	6.28	6.28	3	0.28	0.04	0.23	0.00	0.00	24.0
38	25	-9008	-721	390	0	593	1628	12.57	12.57	6.28	6.28	3	0.07	0.01	0.07	0.00	0.00	24.0
39	25	-8211	665	378	0	551	-2532	12.57	12.57	6.28	6.28	3	0.10	0.01	0.07	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	37	-8140	488	440	0	668	-1964	12.57	12.57	6.28	6.28	3	0.08	0.01	0.05	0.00	0.00	24.0
2	37	-6069	642	337	0	517	-2277	12.57	12.57	6.28	6.28	2	0.14	0.01	0.07	0.00	0.00	24.0
3	37	-6173	645	370	0	579	-2289	12.57	12.57	6.28	6.28	2	0.14	0.01	0.07	0.00	0.00	24.0
4	37	-6348	106	307	0	448	-734	12.57	12.57	6.28	6.28	2	0.06	0.01	0.03	0.00	0.00	24.0
5	37	-6453	110	340	0	510	-745	12.57	12.57	6.28	6.28	2	0.06	0.01	0.03	0.00	0.00	24.0
6	37	-6044	450	288	0	421	-1723	12.57	12.57	6.28	6.28	2	0.11	0.01	0.05	0.00	0.00	24.0
7	37	-6393	462	398	0	627	-1762	12.57	12.57	6.28	6.28	2	0.11	0.01	0.05	0.00	0.00	24.0
8	37	-6128	289	279	0	401	-1260	12.57	12.57	6.28	6.28	2	0.08	0.01	0.03	0.00	0.00	24.0
9	37	-6477	302	389	0	606	-1299	12.57	12.57	6.28	6.28	2	0.09	0.01	0.03	0.00	0.00	24.0
10	37	-6069	642	337	0	517	-2277	12.57	12.57	6.28	6.28	2	0.14	0.01	0.07	0.00	0.00	24.0
11	37	-6173	645	370	0	579	-2289	12.57	12.57	6.28	6.28	2	0.14	0.01	0.07	0.00	0.00	24.0
12	37	-6348	106	307	0	448	-734	12.57	12.57	6.28	6.28	2	0.06	0.01	0.03	0.00	0.00	24.0
13	37	-6453	110	340	0	510	-745	12.57	12.57	6.28	6.28	2	0.06	0.01	0.03	0.00	0.00	24.0
14	37	-6044	450	288	0	421	-1723	12.57	12.57	6.28	6.28	2	0.11	0.01	0.05	0.00	0.00	24.0
15	37	-6393	462	398	0	627	-1762	12.57	12.57	6.28	6.28	2	0.11	0.01	0.05	0.00	0.00	24.0
16	37	-6128	289	279	0	401	-1260	12.57	12.57	6.28	6.28	2	0.08	0.01	0.03	0.00	0.00	24.0
17	37	-6477	302	389	0	606	-1299	12.57	12.57	6.28	6.28	2	0.09	0.01	0.03	0.00	0.00	24.0
18	37	-7596	1768	502	0	823	-5598	12.57	12.57	6.28	6.28	3	0.22	0.03	0.18	0.00	0.00	24.0
19	37	-8610	-2	427	0	630	-513	12.57	12.57	6.28	6.28	3	0.04	0.01	0.04	0.00	0.00	24.0
20	37	-8132	830	419	0	606	-2906	12.57	12.57	6.28	6.28	3	0.11	0.01	0.08	0.00	0.00	24.0
37	37	-7222	2229	516	0	864	-6936	12.57	12.57	6.28	6.28	3	0.27	0.04	0.23	0.00	0.00	24.0
38	37	-8910	-721	390	0	544	1538	12.57	12.57	6.28	6.28	3	0.06	0.01	0.07	0.00	0.00	24.0
39	37	-8114	665	378	0	503	-2449	12.57	12.57	6.28	6.28	3	0.10	0.01	0.07	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-8042	488	440	0	613	-1903	12.57	12.57	6.28	6.28	3	0.08	0.01	0.05	0.00	0.00	24.0
2	50	-5994	642	337	0	475	-2197	12.57	12.57	6.28	6.28	2	0.13	0.01	0.07	0.00	0.00	24.0
3	50	-6098	645	370	0	533	-2208	12.57	12.57	6.28	6.28	2	0.13	0.01	0.07	0.00	0.00	24.0
4	50	-6273	106	307	0	410	-721	12.57	12.57	6.28	6.28	2	0.05	0.01	0.03	0.00	0.00	24.0
5	50	-6378	110	340	0	468	-732	12.57	12.57	6.28	6.28	2	0.06	0.01	0.03	0.00	0.00	24.0
6	50	-5969	450	288	0	385	-1667	12.57	12.57	6.28	6.28	2	0.10	0.01	0.05	0.00	0.00	24.0
7	50	-6318	462	398	0	577	-1704	12.57	12.57	6.28	6.28	2	0.11	0.01	0.05	0.00	0.00	24.0

8	50	-6053	289	279	0	366	-1224	12.57	12.57	6.28	6.28	2	0.08	0.01	0.03	0.00	0.00	24.0
9	50	-6402	302	389	0	558	-1261	12.57	12.57	6.28	6.28	2	0.09	0.01	0.03	0.00	0.00	24.0
10	50	-5994	642	337	0	475	-2197	12.57	12.57	6.28	6.28	2	0.13	0.01	0.07	0.00	0.00	24.0
11	50	-6098	645	370	0	533	-2208	12.57	12.57	6.28	6.28	2	0.13	0.01	0.07	0.00	0.00	24.0
12	50	-6273	106	307	0	410	-721	12.57	12.57	6.28	6.28	2	0.05	0.01	0.03	0.00	0.00	24.0
13	50	-6378	110	340	0	468	-732	12.57	12.57	6.28	6.28	2	0.06	0.01	0.03	0.00	0.00	24.0
14	50	-5969	450	288	0	385	-1667	12.57	12.57	6.28	6.28	2	0.10	0.01	0.05	0.00	0.00	24.0
15	50	-6318	462	398	0	577	-1704	12.57	12.57	6.28	6.28	2	0.11	0.01	0.05	0.00	0.00	24.0
16	50	-6053	289	279	0	366	-1224	12.57	12.57	6.28	6.28	2	0.08	0.01	0.03	0.00	0.00	24.0
17	50	-6402	302	389	0	558	-1261	12.57	12.57	6.28	6.28	2	0.09	0.01	0.03	0.00	0.00	24.0
18	50	-7499	1768	502	0	760	-5377	12.57	12.57	6.28	6.28	3	0.21	0.03	0.18	0.00	0.00	24.0
19	50	-8512	-2	427	0	577	-514	12.57	12.57	6.28	6.28	3	0.04	0.01	0.04	0.00	0.00	24.0
20	50	-8034	830	419	0	554	-2802	12.57	12.57	6.28	6.28	3	0.11	0.01	0.08	0.00	0.00	24.0
37	50	-7125	2229	516	0	800	-6657	12.57	12.57	6.28	6.28	3	0.25	0.04	0.23	0.00	0.00	24.0
38	50	-8813	-721	390	0	495	1448	12.57	12.57	6.28	6.28	3	0.06	0.01	0.07	0.00	0.00	24.0
39	50	-8016	665	378	0	456	-2366	12.57	12.57	6.28	6.28	3	0.09	0.01	0.07	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 105 NI 1445 NF 168 SEZ. Rp B= 0.400 H= 0.600 (pilastro)
PIL. NUM. 11A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-8042	488	440	0	613	-1903	12.57	12.57	6.28	6.28	3	0.08	0.01	0.05	0.00	0.00	24.0
2	0	-5994	642	337	0	475	-2197	12.57	12.57	6.28	6.28	2	0.13	0.01	0.07	0.00	0.00	24.0
3	0	-6098	645	370	0	533	-2208	12.57	12.57	6.28	6.28	2	0.13	0.01	0.07	0.00	0.00	24.0
4	0	-6273	106	307	0	410	-721	12.57	12.57	6.28	6.28	2	0.05	0.01	0.03	0.00	0.00	24.0
5	0	-6378	110	340	0	468	-732	12.57	12.57	6.28	6.28	2	0.06	0.01	0.03	0.00	0.00	24.0
6	0	-5969	450	288	0	385	-1667	12.57	12.57	6.28	6.28	2	0.10	0.01	0.05	0.00	0.00	24.0
7	0	-6318	462	398	0	577	-1704	12.57	12.57	6.28	6.28	2	0.11	0.01	0.05	0.00	0.00	24.0
8	0	-6053	289	279	0	366	-1224	12.57	12.57	6.28	6.28	2	0.08	0.01	0.03	0.00	0.00	24.0
9	0	-6402	302	389	0	558	-1261	12.57	12.57	6.28	6.28	2	0.09	0.01	0.03	0.00	0.00	24.0
10	0	-5994	642	337	0	475	-2197	12.57	12.57	6.28	6.28	2	0.13	0.01	0.07	0.00	0.00	24.0
11	0	-6098	645	370	0	533	-2208	12.57	12.57	6.28	6.28	2	0.13	0.01	0.07	0.00	0.00	24.0
12	0	-6273	106	307	0	410	-721	12.57	12.57	6.28	6.28	2	0.05	0.01	0.03	0.00	0.00	24.0
13	0	-6378	110	340	0	468	-732	12.57	12.57	6.28	6.28	2	0.06	0.01	0.03	0.00	0.00	24.0
14	0	-5969	450	288	0	385	-1667	12.57	12.57	6.28	6.28	2	0.10	0.01	0.05	0.00	0.00	24.0
15	0	-6318	462	398	0	577	-1704	12.57	12.57	6.28	6.28	2	0.11	0.01	0.05	0.00	0.00	24.0
16	0	-6053	289	279	0	366	-1224	12.57	12.57	6.28	6.28	2	0.08	0.01	0.03	0.00	0.00	24.0
17	0	-6402	302	389	0	558	-1261	12.57	12.57	6.28	6.28	2	0.09	0.01	0.03	0.00	0.00	24.0
18	0	-7499	1768	502	0	760	-5377	12.57	12.57	6.28	6.28	3	0.21	0.03	0.18	0.00	0.00	24.0
19	0	-8512	-2	427	0	577	-514	12.57	12.57	6.28	6.28	3	0.04	0.01	0.04	0.00	0.00	24.0
20	0	-8034	830	419	0	554	-2802	12.57	12.57	6.28	6.28	3	0.11	0.01	0.08	0.00	0.00	24.0
37	0	-7125	2229	516	0	800	-6657	12.57	12.57	6.28	6.28	3	0.25	0.04	0.23	0.00	0.00	24.0
38	0	-8813	-721	390	0	495	1448	12.57	12.57	6.28	6.28	3	0.06	0.01	0.07	0.00	0.00	24.0
39	0	-8016	665	378	0	456	-2366	12.57	12.57	6.28	6.28	3	0.09	0.01	0.07	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-7944	488	440	0	558	-1842	12.57	12.57	6.28	6.28	3	0.08	0.01	0.05	0.00	0.00	24.0
2	12	-5919	642	337	0	433	-2117	12.57	12.57	6.28	6.28	2	0.13	0.01	0.07	0.00	0.00	24.0
3	12	-6023	645	370	0	487	-2127	12.57	12.57	6.28	6.28	2	0.13	0.01	0.07	0.00	0.00	24.0
4	12	-6198	106	307	0	372	-707	12.57	12.57	6.28	6.28	2	0.05	0.01	0.03	0.00	0.00	24.0
5	12	-6303	110	340	0	425	-718	12.57	12.57	6.28	6.28	2	0.05	0.01	0.03	0.00	0.00	24.0
6	12	-5894	450	288	0	349	-1611	12.57	12.57	6.28	6.28	2	0.10	0.01	0.05	0.00	0.00	24.0
7	12	-6243	462	398	0	527	-1646	12.57	12.57	6.28	6.28	2	0.10	0.01	0.05	0.00	0.00	24.0
8	12	-5978	289	279	0	331	-1188	12.57	12.57	6.28	6.28	2	0.07	0.01	0.03	0.00	0.00	24.0
9	12	-6327	302	389	0	509	-1223	12.57	12.57	6.28	6.28	2	0.08	0.01	0.03	0.00	0.00	24.0
10	12	-5919	642	337	0	433	-2117	12.57	12.57	6.28	6.28	2	0.13	0.01	0.07	0.00	0.00	24.0
11	12	-6023	645	370	0	487	-2127	12.57	12.57	6.28	6.28	2	0.13	0.01	0.07	0.00	0.00	24.0
12	12	-6198	106	307	0	372	-707	12.57	12.57	6.28	6.28	2	0.05	0.01	0.03	0.00	0.00	24.0
13	12	-6303	110	340	0	425	-718	12.57	12.57	6.28	6.28	2	0.05	0.01	0.03	0.00	0.00	24.0
14	12	-5894	450	288	0	349	-1611	12.57	12.57	6.28	6.28	2	0.10	0.01	0.05	0.00	0.00	24.0
15	12	-6243	462	398	0	527	-1646	12.57	12.57	6.28	6.28	2	0.10	0.01	0.05	0.00	0.00	24.0
16	12	-5978	289	279	0	331	-1188	12.57	12.57	6.28	6.28	2	0.07	0.01	0.03	0.00	0.00	24.0
17	12	-6327	302	389	0	509	-1223	12.57	12.57	6.28	6.28	2	0.08	0.01	0.03	0.00	0.00	24.0
18	12	-7402	1768	502	0	697	-5156	12.57	12.57	6.28	6.28	3	0.20	0.03	0.18	0.00	0.00	24.0
19	12	-8414	-2	427	0	523	-514	12.57	12.57	6.28	6.28	3	0.03	0.01	0.04	0.00	0.00	24.0
20	12	-7936	830	419	0	501	-2698	12.57	12.57	6.28	6.28	3	0.11	0.01	0.08	0.00	0.00	24.0
37	12	-7028	2229	516	0	735	-6378	12.57	12.57	6.28	6.28	3	0.24	0.04	0.23	0.00	0.00	24.0
38	12	-8716	-721	390	0	446	1358	12.57	12.57	6.28	6.28	3	0.06	0.01	0.07	0.00	0.00	24.0
39	12	-7918	665	378	0	409	-2283	12.57	12.57	6.28	6.28	3	0.09	0.01	0.07	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-7847	488	440	0	503	-1781	12.57	12.57	6.28	6.28	3	0.07	0.01	0.05	0.00	0.00	24.0
2	25	-5844	642	337	0	391	-2037	12.57	12.57	6.28	6.28	2	0.12	0.01	0.07	0.00	0.00	24.0
3	25	-5948	645	370	0	440	-2046	12.57	12.57	6.28	6.28	2	0.12	0.01	0.07	0.00	0.00	24.0
4	25	-6123	106	307	0	333	-694	12.57	12.57	6.28	6.28	2	0.05	0.01	0.03	0.00	0.00	24.0
5	25	-6228	110	340	0	383	-704	12.57	12.57	6.28	6.28	2	0.05	0.01	0.03	0.00	0.00	24.0
6	25	-5819	450	288	0	313	-1555	12.57	12.57	6.28	6.28	2	0.09	0.01	0.05	0.00	0.00	24.0
7	25	-6168	462	398	0	478	-1588	12.57	12.57	6.28	6.28	2	0.10	0.01	0.05	0.00	0.00	24.0
8	25	-5903	289	279	0	296	-1152	12.57	12.57	6.28	6.28	2	0.07	0.01	0.03	0.00	0.00	24.0
9	25	-6252	302	389	0	460	-1186	12.57	12.57	6.28	6.28	2	0.08	0.01	0.03	0.00	0.00	24.0
10	25	-5844	642	337	0	391	-2037	12.57	12.57	6.28	6.28	2	0.12	0.01	0.07	0.00	0.00	24.0
11	25	-5948	645	370	0	440	-2046	12.57	12.57	6.28	6.28	2	0.12	0.01	0.07	0.00	0.00	24.0
12	25	-6123	106	307	0	333	-694	12.57	12.57	6.28	6.28	2	0.05	0.01	0.03	0.00	0.00	24.0
13	25	-6228	110	340	0	383	-704	12.57	12.57	6.28	6.28	2	0.05	0.01	0.03	0.00	0.00	24.0
14	25	-5819	450	288	0	313	-1555	12.57	12.57	6.28	6.28	2	0.09	0.01	0.05	0.00	0.00	24.0
15	25	-6168	462	398	0	478	-1588	12.57	12.57	6.28	6.28	2	0.10	0.01	0.05	0.00	0.00	24.0
16	25	-5903	289	279	0	296	-1152	12.57	12.57	6.28	6.28	2	0.07	0.01	0.03	0.00	0.00	24.0
17	25	-6252	302	389	0	460	-1186	12.57	12.57	6.28	6.28	2	0.08	0.01	0.03	0.00	0.00	24.0
18	25	-7304	1768	502	0	634	-4935	12.57	12.57	6.28	6.28	3	0.19	0.03	0.18	0.00	0.00	24.0
19	25	-8317	-2	427	0	470	-514	12.57	12.57	6.28	6.28	3	0.03	0.01	0.04	0.00	0.00	24.0
20	25	-7839	830	419	0	449	-2595	12.57	12.57	6.28	6.28	3	0.10	0.01	0.09	0.00	0.00	24.0
37	25	-6930	2229	516	0	671	-6100	12.57	12.57	6.28	6.28	3	0.23	0.04	0.23	0.00	0.00	24.0
38	25	-8618	-721	390	0	397	1268	12.57	12.57	6.28	6.28	3	0.05	0.01	0.07	0.00	0.00	24.0
39	25	-7821	665	378	0	362	-2200	12.57	12.57	6.28	6.28	3	0.09	0.01	0.07	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-7750	488	440	0	448	-1720	12.57	12.57	6.28	6.28	3	0.07	0.01	0.05	0.00	0.00	24.0
2	38	-5769	642	337	0	349	-1956	12.57	12.57	6.28	6.28	2	0.12	0.01	0.07	0.00	0.00	24.0
3	38	-5873	645	370	0	394	-1966	12.57	12.57	6.28	6.28	2	0.12	0.01	0.07	0.00	0.00	24.0

4	38	-6048	106	307	0	295	-681	12.57	12.57	6.28	6.28	2	0.05	0.01	0.03	0.00	0.00	24.0
5	38	-6153	110	340	0	340	-690	12.57	12.57	6.28	6.28	2	0.05	0.01	0.03	0.00	0.00	24.0
6	38	-5744	450	288	0	277	-1498	12.57	12.57	6.28	6.28	2	0.09	0.01	0.05	0.00	0.00	24.0
7	38	-6093	462	398	0	428	-1531	12.57	12.57	6.28	6.28	2	0.10	0.01	0.05	0.00	0.00	24.0
8	38	-5828	289	279	0	261	-1116	12.57	12.57	6.28	6.28	2	0.07	0.01	0.03	0.00	0.00	24.0
9	38	-6177	302	389	0	412	-1148	12.57	12.57	6.28	6.28	2	0.07	0.01	0.03	0.00	0.00	24.0
10	38	-5769	642	337	0	349	-1956	12.57	12.57	6.28	6.28	2	0.12	0.01	0.07	0.00	0.00	24.0
11	38	-5873	645	370	0	394	-1966	12.57	12.57	6.28	6.28	2	0.12	0.01	0.07	0.00	0.00	24.0
12	38	-6048	106	307	0	295	-681	12.57	12.57	6.28	6.28	2	0.05	0.01	0.03	0.00	0.00	24.0
13	38	-6153	110	340	0	340	-690	12.57	12.57	6.28	6.28	2	0.05	0.01	0.03	0.00	0.00	24.0
14	38	-5744	450	288	0	277	-1498	12.57	12.57	6.28	6.28	2	0.09	0.01	0.05	0.00	0.00	24.0
15	38	-6093	462	398	0	428	-1531	12.57	12.57	6.28	6.28	2	0.10	0.01	0.05	0.00	0.00	24.0
16	38	-5828	289	279	0	261	-1116	12.57	12.57	6.28	6.28	2	0.07	0.01	0.03	0.00	0.00	24.0
17	38	-6177	302	389	0	412	-1148	12.57	12.57	6.28	6.28	2	0.07	0.01	0.03	0.00	0.00	24.0
18	38	-7206	1768	502	0	571	-4714	12.57	12.57	6.28	6.28	3	0.18	0.03	0.18	0.00	0.00	24.0
19	38	-8220	-2	427	0	417	-514	12.57	12.57	6.28	6.28	3	0.03	0.01	0.04	0.00	0.00	24.0
20	38	-7742	830	419	0	396	-2491	12.57	12.57	6.28	6.28	3	0.10	0.01	0.09	0.00	0.00	24.0
37	38	-6832	2229	516	0	606	-5821	12.57	12.57	6.28	6.28	3	0.22	0.04	0.23	0.00	0.00	24.0
38	38	-8520	-721	390	0	349	1178	12.57	12.57	6.28	6.28	3	0.05	0.01	0.07	0.00	0.00	24.0
39	38	-7724	665	378	0	315	-2117	12.57	12.57	6.28	6.28	3	0.08	0.01	0.07	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-7652	488	440	0	393	-1659	12.57	12.57	6.28	6.28	3	0.07	0.01	0.05	0.00	0.00	24.0
2	50	-5694	642	337	0	307	-1876	12.57	12.57	6.28	6.28	2	0.11	0.01	0.07	0.00	0.00	24.0
3	50	-5798	645	370	0	348	-1885	12.57	12.57	6.28	6.28	2	0.11	0.01	0.07	0.00	0.00	24.0
4	50	-5973	106	307	0	256	-668	12.57	12.57	6.28	6.28	2	0.04	0.01	0.03	0.00	0.00	24.0
5	50	-6078	110	340	0	298	-677	12.57	12.57	6.28	6.28	2	0.05	0.01	0.03	0.00	0.00	24.0
6	50	-5669	450	288	0	241	-1442	12.57	12.57	6.28	6.28	2	0.08	0.01	0.05	0.00	0.00	24.0
7	50	-6018	462	398	0	378	-1473	12.57	12.57	6.28	6.28	2	0.09	0.01	0.05	0.00	0.00	24.0
8	50	-5753	289	279	0	226	-1080	12.57	12.57	6.28	6.28	2	0.06	0.01	0.03	0.00	0.00	24.0
9	50	-6102	302	389	0	363	-1110	12.57	12.57	6.28	6.28	2	0.07	0.01	0.03	0.00	0.00	24.0
10	50	-5694	642	337	0	307	-1876	12.57	12.57	6.28	6.28	2	0.11	0.01	0.07	0.00	0.00	24.0
11	50	-5798	645	370	0	348	-1885	12.57	12.57	6.28	6.28	2	0.11	0.01	0.07	0.00	0.00	24.0
12	50	-5973	106	307	0	256	-668	12.57	12.57	6.28	6.28	2	0.04	0.01	0.03	0.00	0.00	24.0
13	50	-6078	110	340	0	298	-677	12.57	12.57	6.28	6.28	2	0.05	0.01	0.03	0.00	0.00	24.0
14	50	-5669	450	288	0	241	-1442	12.57	12.57	6.28	6.28	2	0.08	0.01	0.05	0.00	0.00	24.0
15	50	-6018	462	398	0	378	-1473	12.57	12.57	6.28	6.28	2	0.09	0.01	0.05	0.00	0.00	24.0
16	50	-5753	289	279	0	226	-1080	12.57	12.57	6.28	6.28	2	0.06	0.01	0.03	0.00	0.00	24.0
17	50	-6102	302	389	0	363	-1110	12.57	12.57	6.28	6.28	2	0.07	0.01	0.03	0.00	0.00	24.0
18	50	-7109	1768	502	0	509	-4493	12.57	12.57	6.28	6.28	3	0.17	0.03	0.18	0.00	0.00	24.0
19	50	-8122	-2	427	0	363	-514	12.57	12.57	6.28	6.28	3	0.03	0.01	0.04	0.00	0.00	24.0
20	50	-7644	830	419	0	344	-2387	12.57	12.57	6.28	6.28	3	0.09	0.01	0.09	0.00	0.00	24.0
37	50	-6735	2229	516	0	542	-5542	12.57	12.57	6.28	6.28	3	0.21	0.04	0.23	0.00	0.00	24.0
38	50	-8423	-721	390	0	300	1088	12.57	12.57	6.28	6.28	3	0.04	0.01	0.07	0.00	0.00	24.0
39	50	-7626	665	378	0	267	-2034	12.57	12.57	6.28	6.28	3	0.08	0.01	0.07	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 106 NI 1032 NF 1045 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 10
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-16650	1140	1324	0	1383	-876	6.28	6.28	12.57	12.57	3	0.07	0.02	0.12	0.00	0.00	24.0
2	0	-13510	571	1191	0	1162	-720	6.28	6.28	12.57	12.57	2	0.08	0.02	0.11	0.00	0.00	24.0
3	0	-13500	596	1152	0	1147	-730	6.28	6.28	12.57	12.57	2	0.08	0.02	0.11	0.00	0.00	24.0
4	0	-12110	1157	885	0	981	-617	6.28	6.28	12.57	12.57	2	0.07	0.02	0.10	0.00	0.00	24.0
5	0	-12110	1182	846	0	966	-627	6.28	6.28	12.57	12.57	2	0.07	0.02	0.10	0.00	0.00	24.0
6	0	-13020	748	1129	0	1116	-672	6.28	6.28	12.57	12.57	2	0.08	0.02	0.11	0.00	0.00	24.0
7	0	-13010	830	1000	0	1066	-706	6.28	6.28	12.57	12.57	2	0.08	0.02	0.10	0.00	0.00	24.0
8	0	-12610	923	1037	0	1062	-642	6.28	6.28	12.57	12.57	2	0.08	0.02	0.10	0.00	0.00	24.0
9	0	-12590	1006	908	0	1012	-675	6.28	6.28	12.57	12.57	2	0.07	0.02	0.09	0.00	0.00	24.0
10	0	-13510	571	1191	0	1162	-720	6.28	6.28	12.57	12.57	2	0.08	0.02	0.11	0.00	0.00	24.0
11	0	-13500	596	1152	0	1147	-730	6.28	6.28	12.57	12.57	2	0.08	0.02	0.11	0.00	0.00	24.0
12	0	-12110	1157	885	0	981	-617	6.28	6.28	12.57	12.57	2	0.07	0.02	0.10	0.00	0.00	24.0
13	0	-12110	1182	846	0	966	-627	6.28	6.28	12.57	12.57	2	0.07	0.02	0.10	0.00	0.00	24.0
14	0	-13020	748	1129	0	1116	-672	6.28	6.28	12.57	12.57	2	0.08	0.02	0.11	0.00	0.00	24.0
15	0	-13010	830	1000	0	1066	-706	6.28	6.28	12.57	12.57	2	0.08	0.02	0.10	0.00	0.00	24.0
16	0	-12610	923	1037	0	1062	-642	6.28	6.28	12.57	12.57	2	0.08	0.02	0.10	0.00	0.00	24.0
17	0	-12590	1006	908	0	1012	-675	6.28	6.28	12.57	12.57	2	0.07	0.02	0.09	0.00	0.00	24.0
18	0	-20330	-56	2144	0	2002	-949	6.28	6.28	12.57	12.57	3	0.08	0.04	0.19	0.00	0.00	24.0
19	0	-15400	1891	942	0	1279	-666	6.28	6.28	12.57	12.57	3	0.06	0.03	0.15	0.00	0.00	24.0
20	0	-17420	954	1678	0	1488	-818	6.28	6.28	12.57	12.57	3	0.07	0.03	0.15	0.00	0.00	24.0
37	0	-21570	-632	2485	0	2163	-1067	6.28	6.28	12.57	12.57	3	0.09	0.04	0.21	0.00	0.00	24.0
38	0	-13360	2613	482	0	959	-594	6.28	6.28	12.57	12.57	3	0.05	0.05	0.21	0.00	0.00	24.0
39	0	-16720	1053	1708	0	1306	-847	6.28	6.28	12.57	12.57	3	0.06	0.03	0.16	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-16552	1140	1324	0	1218	-733	6.28	6.28	12.57	12.57	3	0.06	0.02	0.12	0.00	0.00	24.0
2	12	-13435	571	1191	0	1013	-649	6.28	6.28	12.57	12.57	2	0.07	0.02	0.11	0.00	0.00	24.0
3	12	-13425	596	1152	0	1003	-656	6.28	6.28	12.57	12.57	2	0.07	0.02	0.11	0.00	0.00	24.0
4	12	-12035	1157	885	0	870	-473	6.28	6.28	12.57	12.57	2	0.06	0.02	0.10	0.00	0.00	24.0
5	12	-12035	1182	846	0	860	-479	6.28	6.28	12.57	12.57	2	0.06	0.02	0.10	0.00	0.00	24.0
6	12	-12945	748	1129	0	975	-579	6.28	6.28	12.57	12.57	2	0.07	0.02	0.11	0.00	0.00	24.0
7	12	-12935	830	1000	0	941	-602	6.28	6.28	12.57	12.57	2	0.07	0.02	0.10	0.00	0.00	24.0
8	12	-12535	923	1037	0	932	-526	6.28	6.28	12.57	12.57	2	0.06	0.02	0.10	0.00	0.00	24.0
9	12	-12515	1006	908	0	898	-549	6.28	6.28	12.57	12.57	2	0.06	0.02	0.09	0.00	0.00	24.0
10	12	-13435	571	1191	0	1013	-649	6.28	6.28	12.57	12.57	2	0.07	0.02	0.11	0.00	0.00	24.0
11	12	-13425	596	1152	0	1003	-656	6.28	6.28	12.57	12.57	2	0.07	0.02	0.11	0.00	0.00	24.0
12	12	-12035	1157	885	0	870	-473	6.28	6.28	12.57	12.57	2	0.06	0.02	0.10	0.00	0.00	24.0
13	12	-12035	1182	846	0	860	-479	6.28	6.28	12.57	12.57	2	0.06	0.02	0.10	0.00	0.00	24.0
14	12	-12945	748	1129	0	975	-579	6.28	6.28	12.57	12.57	2	0.07	0.02	0.11	0.00	0.00	24.0
15	12	-12935	830	1000	0	941	-602	6.28	6.28	12.57	12.57	2	0.07	0.02	0.10	0.00	0.00	24.0
16	12	-12535	923	1037	0	932	-526	6.28	6.28	12.57	12.57	2	0.06	0.02	0.10	0.00	0.00	24.0
17	12	-12515	1006	908	0	898	-549	6.28	6.28	12.57	12.57	2	0.06	0.02	0.09	0.00	0.00	24.0
18	12	-20232	-56	2144	0	1734	-956	6.28	6.28	12.57	12.57	3	0.08	0.04	0.19	0.00	0.00	24.0
19	12	-15302	1891	942	0	1161	-429	6.28	6.28	12.57	12.57	3	0.05	0.03	0.15	0.00	0.00	24.0
20	12	-17322	954	1678	0	1278	-698	6.28	6.28	12.57	12.57	3	0.06	0.03	0.15	0.00	0.00	24.0
37	12	-21472	-632	2485	0	1852	-1146	6.28	6.28	12.57	12.57	3	0.09	0.04	0.21	0.00	0.00	24.0
38	12	-13262	2613	482	0	898	-267	6.28	6.28	12.57	12.57	3	0.04	0.05	0.21	0.00	0.00	24.0
39	12	-16622	1053	1708	0	1093	-716	6.28	6.28	12.57	12.57	3	0.05	0.03	0.16	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-16455	1140	1324	0	1052	-591	6.28	6.28	12.57	12.57	3	0.05	0.02	0.12	0.00	0.00	24.0
2	25	-13360	571	1191	0	864	-577	6.28	6.28	12.57	12.57	2	0.06	0.02	0.11	0.00	0.00	24.0
3	25	-13350	596	1152	0	859	-581	6.28	6.28	12.57	12.57	2	0.06	0.02	0.11	0.00	0.00	24.0
4	25	-11960	1157	885	0	760	-328	6.28	6.28	12.57	12.57	2	0.05	0.02	0.10	0.00	0.00	24.0
5	25	-11960	1182	846	0	754	-332	6.28	6.28	12.57	12.57	2	0.05	0.02	0.10	0.00	0.00	24.0
6	25	-12870	748	1129	0	834	-486	6.28	6.28	12.57	12.57	2	0.06	0.02	0.11	0.00	0.00	24.0
7	25	-12860	830	1000	0	816	-498	6.28	6.28	12.57	12.57	2	0.06	0.02	0.10	0.00	0.00	24.0
8	25	-12460	923	1037	0	803	-411	6.28	6.28	12.57	12.57	2	0.05	0.02	0.10	0.00	0.00	24.0
9	25	-12440	1006	908	0	785	-423	6.28	6.28	12.57	12.57	2	0.05	0.02	0.09	0.00	0.00	24.0
10	25	-13360	571	1191	0	864	-577	6.28	6.28	12.57	12.57	2	0.06	0.02	0.11	0.00	0.00	24.0
11	25	-13350	596	1152	0	859	-581	6.28	6.28	12.57	12.57	2	0.06	0.02	0.11	0.00	0.00	24.0
12	25	-11960	1157	885	0	760	-328	6.28	6.28	12.57	12.57	2	0.05	0.02	0.10	0.00	0.00	24.0
13	25	-11960	1182	846	0	754	-332	6.28	6.28	12.57	12.57	2	0.05	0.02	0.10	0.00	0.00	24.0
14	25	-12870	748	1129	0	834	-486	6.28	6.28	12.57	12.57	2	0.06	0.02	0.11	0.00	0.00	24.0
15	25	-12860	830	1000	0	816	-498	6.28	6.28	12.57	12.57	2	0.06	0.02	0.10	0.00	0.00	24.0
16	25	-12460	923	1037	0	803	-411	6.28	6.28	12.57	12.57	2	0.05	0.02	0.10	0.00	0.00	24.0
17	25	-12440	1006	908	0	785	-423	6.28	6.28	12.57	12.57	2	0.05	0.02	0.09	0.00	0.00	24.0
18	25	-20135	-56	2144	0	1466	-963	6.28	6.28	12.57	12.57	3	0.07	0.04	0.19	0.00	0.00	24.0
19	25	-15205	1891	942	0	1044	-193	6.28	6.28	12.57	12.57	3	0.04	0.03	0.15	0.00	0.00	24.0
20	25	-17225	954	1678	0	1069	-579	6.28	6.28	12.57	12.57	3	0.05	0.03	0.15	0.00	0.00	24.0
37	25	-21375	-632	2485	0	1542	-1225	6.28	6.28	12.57	12.57	3	0.08	0.04	0.21	0.00	0.00	24.0
38	25	-13165	2613	482	0	838	59	6.28	6.28	12.57	12.57	3	0.03	0.05	0.21	0.00	0.00	24.0
39	25	-16525	1053	1708	0	879	-584	6.28	6.28	12.57	12.57	3	0.04	0.03	0.16	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-16358	1140	1324	0	887	-448	6.28	6.28	12.57	12.57	3	0.04	0.02	0.12	0.00	0.00	24.0
2	38	-13285	571	1191	0	716	-506	6.28	6.28	12.57	12.57	2	0.05	0.02	0.11	0.00	0.00	24.0
3	38	-13275	596	1152	0	715	-507	6.28	6.28	12.57	12.57	2	0.05	0.02	0.11	0.00	0.00	24.0
4	38	-11885	1157	885	0	649	-183	6.28	6.28	12.57	12.57	2	0.04	0.02	0.10	0.00	0.00	24.0
5	38	-11885	1182	846	0	649	-184	6.28	6.28	12.57	12.57	2	0.04	0.02	0.10	0.00	0.00	24.0
6	38	-12795	748	1129	0	693	-392	6.28	6.28	12.57	12.57	2	0.05	0.02	0.11	0.00	0.00	24.0
7	38	-12785	830	1000	0	691	-394	6.28	6.28	12.57	12.57	2	0.05	0.02	0.10	0.00	0.00	24.0
8	38	-12385	923	1037	0	673	-295	6.28	6.28	12.57	12.57	2	0.04	0.02	0.10	0.00	0.00	24.0
9	38	-12365	1006	908	0	671	-298	6.28	6.28	12.57	12.57	2	0.04	0.02	0.09	0.00	0.00	24.0
10	38	-13285	571	1191	0	716	-506	6.28	6.28	12.57	12.57	2	0.05	0.02	0.11	0.00	0.00	24.0
11	38	-13275	596	1152	0	715	-507	6.28	6.28	12.57	12.57	2	0.05	0.02	0.11	0.00	0.00	24.0
12	38	-11885	1157	885	0	649	-183	6.28	6.28	12.57	12.57	2	0.04	0.02	0.10	0.00	0.00	24.0
13	38	-11885	1182	846	0	649	-184	6.28	6.28	12.57	12.57	2	0.04	0.02	0.10	0.00	0.00	24.0
14	38	-12795	748	1129	0	693	-392	6.28	6.28	12.57	12.57	2	0.05	0.02	0.11	0.00	0.00	24.0
15	38	-12785	830	1000	0	691	-394	6.28	6.28	12.57	12.57	2	0.05	0.02	0.10	0.00	0.00	24.0
16	38	-12385	923	1037	0	673	-295	6.28	6.28	12.57	12.57	2	0.04	0.02	0.10	0.00	0.00	24.0
17	38	-12365	1006	908	0	671	-298	6.28	6.28	12.57	12.57	2	0.04	0.02	0.09	0.00	0.00	24.0
18	38	-20038	-56	2144	0	1198	-970	6.28	6.28	12.57	12.57	3	0.06	0.04	0.19	0.00	0.00	24.0
19	38	-15108	1891	942	0	926	43	6.28	6.28	12.57	12.57	3	0.03	0.03	0.15	0.00	0.00	24.0
20	38	-17128	954	1678	0	859	-460	6.28	6.28	12.57	12.57	3	0.04	0.03	0.15	0.00	0.00	24.0
37	38	-21278	-632	2485	0	1231	-1304	6.28	6.28	12.57	12.57	3	0.08	0.04	0.21	0.00	0.00	24.0
38	38	-13068	2613	482	0	778	386	6.28	6.28	12.57	12.57	3	0.03	0.05	0.21	0.00	0.00	24.0
39	38	-16428	1053	1708	0	666	-452	6.28	6.28	12.57	12.57	3	0.03	0.03	0.16	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-16260	1140	1324	0	721	-306	6.28	6.28	12.57	12.57	3	0.03	0.02	0.12	0.00	0.00	24.0
2	50	-13210	571	1191	0	567	-435	6.28	6.28	12.57	12.57	2	0.04	0.02	0.11	0.00	0.00	24.0
3	50	-13200	596	1152	0	571	-432	6.28	6.28	12.57	12.57	2	0.04	0.02	0.11	0.00	0.00	24.0
4	50	-11810	1157	885	0	538	-38	6.28	6.28	12.57	12.57	2	0.03	0.02	0.10	0.00	0.00	24.0
5	50	-11810	1182	846	0	543	-36	6.28	6.28	12.57	12.57	2	0.03	0.02	0.10	0.00	0.00	24.0
6	50	-12720	748	1129	0	552	-299	6.28	6.28	12.57	12.57	2	0.04	0.02	0.11	0.00	0.00	24.0
7	50	-12710	830	1000	0	566	-291	6.28	6.28	12.57	12.57	2	0.04	0.02	0.10	0.00	0.00	24.0
8	50	-12310	923	1037	0	543	-180	6.28	6.28	12.57	12.57	2	0.03	0.02	0.10	0.00	0.00	24.0
9	50	-12290	1006	908	0	558	-172	6.28	6.28	12.57	12.57	2	0.03	0.02	0.09	0.00	0.00	24.0
10	50	-13210	571	1191	0	567	-435	6.28	6.28	12.57	12.57	2	0.04	0.02	0.11	0.00	0.00	24.0
11	50	-13200	596	1152	0	571	-432	6.28	6.28	12.57	12.57	2	0.04	0.02	0.11	0.00	0.00	24.0
12	50	-11810	1157	885	0	538	-38	6.28	6.28	12.57	12.57	2	0.03	0.02	0.10	0.00	0.00	24.0
13	50	-11810	1182	846	0	543	-36	6.28	6.28	12.57	12.57	2	0.03	0.02	0.10	0.00	0.00	24.0
14	50	-12720	748	1129	0	552	-299	6.28	6.28	12.57	12.57	2	0.04	0.02	0.11	0.00	0.00	24.0
15	50	-12710	830	1000	0	566	-291	6.28	6.28	12.57	12.57	2	0.04	0.02	0.10	0.00	0.00	24.0
16	50	-12310	923	1037	0	543	-180	6.28	6.28	12.57	12.57	2	0.03	0.02	0.10	0.00	0.00	24.0
17	50	-12290	1006	908	0	558	-172	6.28	6.28	12.57	12.57	2	0.03	0.02	0.09	0.00	0.00	24.0
18	50	-19940	-56	2144	0	930	-977	6.28	6.28	12.57	12.57	3	0.06	0.04	0.19	0.00	0.00	24.0
19	50	-15010	1891	942	0	808	280	6.28	6.28	12.57	12.57	3	0.03	0.03	0.15	0.00	0.00	24.0
20	50	-17030	954	1678	0	649	-340	6.28	6.28	12.57	12.57	3	0.03	0.03	0.15	0.00	0.00	24.0
37	50	-21180	-632	2485	0	921	-1383	6.28	6.28	12.57	12.57	3	0.08	0.04	0.21	0.00	0.00	24.0
38	50	-12970	2613	482	0	718	712	6.28	6.28	12.57	12.57	3	0.04	0.05	0.21	0.00	0.00	24.0
39	50	-16330	1053	1708	0	452	-321	6.28	6.28	12.57	12.57	3	0.02	0.03	0.16	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 107 NI 1045 NF 299 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 10A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-18330	443	680	0	594	-236	6.28	6.28	12.57	12.57	3	0.02	0.01	0.06	0.00	0.00	24.0
2	0	-14550	-559	608	0	461	-411	6.28	6.28	12.57	12.57	2	0.04	0.01	0.06	0.00	0.00	24.0
3	0	-14540	-546	564	0	469	-407	6.28	6.28	12.57	12.57	2	0.04	0.01	0.05	0.00	0.00	24.0
4	0	-13660	1227	482	0	445	44	6.28	6.28	12.57	12.57	2	0.02	0.02	0.10	0.00	0.00	24.0
5	0	-13650	1240	438	0	454	48	6.28	6.28	12.57	12.57	2	0.02	0.02	0.10	0.00	0.00	24.0
6	0	-14250	51	616	0	446	-256	6.28	6.28	12.57	12.57	2	0.03	0.01	0.06	0.00	0.00	24.0
7	0	-14220	94	468	0	473	-244	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
8	0	-13980	587	578	0	441	-119	6.28	6.28	12.57	12.57	2	0.03	0.01	0.05	0.00	0.00	24.0
9	0	-13950	630	430	0	468	-107	6.28	6.28	12.57	12.57	2	0.03	0.01	0.05	0.00	0.00	24.0
10	0	-14550	-559	608	0	461	-411	6.28	6.28	12.57	12.57	2	0.04	0.01	0.06	0.00	0.00	24.0
11	0	-14540	-546	564	0	469	-407	6.28	6.28	12.57	12.57	2	0.04	0.01	0.05	0.00	0.00	24.0
12	0	-13660	1227	482	0	445	44	6.28	6.28	12.57	12.57	2	0.02	0.02	0.10	0.00	0.00	24.0
13	0	-13650	1240	438	0	454	48	6.28	6.28	12.57	12.57	2	0.02	0.02	0.10	0.00	0.00	24.0
14	0	-14250	51	616	0	446	-256	6.28	6.28	12.57	12.57	2	0.03	0.01	0.06	0.00	0.00	24.0
15	0	-14220	94	468	0	473	-244	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
16	0	-13980	587	578	0	441	-119	6.28	6.28	12.57	12.57	2	0.03	0.01	0.05	0.00	0.00	24.0
17	0	-13950	630	430	0	468	-107	6.28	6.28	12.57	12.57	2	0.03	0.01	0.05	0.00	0.00	24.0
18	0	-21460	-2436	907	0	751	-1023	6.28	6.28	12.57	12.57	3	0.06	0.04	0.20	0.00	0.00	24.0
19	0	-18040	3188	402	0	689	427	6.28	6.28	12.57	12.57	3	0.03	0.06	0.25	0.00	0.00	24.0
20	0	-19380	380	1004	0	484	-288	6.28	6.28	12.57	12.57	3	0.02	0.02	0.09	0.00	0.00	24.0
37	0	-22130	-4290	1090	0	728	-1486	6.28	6.28	12.57	12.57	3	0.08	0.08	0.35	0.00	0.00	24.0

38	0	-16430	5082	249	0	625	930	6.28	6.28	12.57	12.57	3	0.05	0.09	0.44	0.00	0.00	24.0
39	0	-18660	402	1252	0	283	-262	6.28	6.28	12.57	12.57	3	0.02	0.02	0.11	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-18232	443	680	0	509	-181	6.28	6.28	12.57	12.57	3	0.02	0.01	0.06	0.00	0.00	24.0
2	12	-14475	-559	608	0	385	-481	6.28	6.28	12.57	12.57	2	0.04	0.01	0.06	0.00	0.00	24.0
3	12	-14465	-546	564	0	398	-476	6.28	6.28	12.57	12.57	2	0.04	0.01	0.05	0.00	0.00	24.0
4	12	-13585	1227	482	0	385	197	6.28	6.28	12.57	12.57	2	0.03	0.02	0.10	0.00	0.00	24.0
5	12	-13575	1240	438	0	399	203	6.28	6.28	12.57	12.57	2	0.03	0.02	0.10	0.00	0.00	24.0
6	12	-14175	51	616	0	369	-249	6.28	6.28	12.57	12.57	2	0.03	0.01	0.06	0.00	0.00	24.0
7	12	-14145	94	468	0	415	-232	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
8	12	-13905	587	578	0	369	-46	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
9	12	-13875	630	430	0	415	-29	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
10	12	-14475	-559	608	0	385	-481	6.28	6.28	12.57	12.57	2	0.04	0.01	0.06	0.00	0.00	24.0
11	12	-14465	-546	564	0	398	-476	6.28	6.28	12.57	12.57	2	0.04	0.01	0.05	0.00	0.00	24.0
12	12	-13585	1227	482	0	385	197	6.28	6.28	12.57	12.57	2	0.03	0.02	0.10	0.00	0.00	24.0
13	12	-13575	1240	438	0	399	203	6.28	6.28	12.57	12.57	2	0.03	0.02	0.10	0.00	0.00	24.0
14	12	-14175	51	616	0	369	-249	6.28	6.28	12.57	12.57	2	0.03	0.01	0.06	0.00	0.00	24.0
15	12	-14145	94	468	0	415	-232	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
16	12	-13905	587	578	0	369	-46	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
17	12	-13875	630	430	0	415	-29	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
18	12	-21362	-2436	907	0	638	-1327	6.28	6.28	12.57	12.57	3	0.07	0.04	0.20	0.00	0.00	24.0
19	12	-17942	3188	402	0	639	825	6.28	6.28	12.57	12.57	3	0.05	0.06	0.27	0.00	0.00	24.0
20	12	-19282	380	1004	0	358	-240	6.28	6.28	12.57	12.57	3	0.02	0.02	0.09	0.00	0.00	24.0
37	12	-22032	-4290	1090	0	592	-2022	6.28	6.28	12.57	12.57	3	0.10	0.08	0.35	0.00	0.00	24.0
38	12	-16332	5082	249	0	594	1565	6.28	6.28	12.57	12.57	3	0.09	0.09	0.44	0.00	0.00	24.0
39	12	-18562	402	1252	0	126	-211	6.28	6.28	12.57	12.57	3	0.01	0.02	0.11	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-18135	443	680	0	424	-125	6.28	6.28	12.57	12.57	3	0.02	0.01	0.06	0.00	0.00	24.0
2	25	-14400	-559	608	0	308	-551	6.28	6.28	12.57	12.57	2	0.04	0.01	0.06	0.00	0.00	24.0
3	25	-14390	-546	564	0	328	-544	6.28	6.28	12.57	12.57	2	0.04	0.01	0.05	0.00	0.00	24.0
4	25	-13510	1227	482	0	325	351	6.28	6.28	12.57	12.57	2	0.03	0.02	0.11	0.00	0.00	24.0
5	25	-13500	1240	438	0	344	358	6.28	6.28	12.57	12.57	2	0.03	0.02	0.11	0.00	0.00	24.0
6	25	-14100	51	616	0	292	-243	6.28	6.28	12.57	12.57	2	0.02	0.01	0.06	0.00	0.00	24.0
7	25	-14070	94	468	0	356	-220	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
8	25	-13830	587	578	0	297	27	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
9	25	-13800	630	430	0	361	50	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
10	25	-14400	-559	608	0	308	-551	6.28	6.28	12.57	12.57	2	0.04	0.01	0.06	0.00	0.00	24.0
11	25	-14390	-546	564	0	328	-544	6.28	6.28	12.57	12.57	2	0.04	0.01	0.05	0.00	0.00	24.0
12	25	-13510	1227	482	0	325	351	6.28	6.28	12.57	12.57	2	0.03	0.02	0.11	0.00	0.00	24.0
13	25	-13500	1240	438	0	344	358	6.28	6.28	12.57	12.57	2	0.03	0.02	0.11	0.00	0.00	24.0
14	25	-14100	51	616	0	292	-243	6.28	6.28	12.57	12.57	2	0.02	0.01	0.06	0.00	0.00	24.0
15	25	-14070	94	468	0	356	-220	6.28	6.28	12.57	12.57	2	0.03	0.01	0.04	0.00	0.00	24.0
16	25	-13830	587	578	0	297	27	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
17	25	-13800	630	430	0	361	50	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
18	25	-21265	-2436	907	0	524	-1631	6.28	6.28	12.57	12.57	3	0.09	0.04	0.20	0.00	0.00	24.0
19	25	-17845	3188	402	0	588	1224	6.28	6.28	12.57	12.57	3	0.07	0.06	0.27	0.00	0.00	24.0
20	25	-19185	380	1004	0	233	-193	6.28	6.28	12.57	12.57	3	0.01	0.02	0.09	0.00	0.00	24.0
37	25	-21935	-4290	1090	0	456	-2559	6.28	6.28	12.57	12.57	3	0.13	0.08	0.35	0.00	0.00	24.0
38	25	-16235	5082	249	0	562	2200	6.28	6.28	12.57	12.57	3	0.12	0.09	0.44	0.00	0.00	24.0
39	25	-18465	402	1252	0	-30	-161	6.28	6.28	12.57	12.57	3	0.01	0.02	0.11	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-18038	443	680	0	339	-70	6.28	6.28	12.57	12.57	3	0.01	0.01	0.06	0.00	0.00	24.0
2	38	-14325	-559	608	0	232	-621	6.28	6.28	12.57	12.57	2	0.04	0.01	0.06	0.00	0.00	24.0
3	38	-14315	-546	564	0	257	-612	6.28	6.28	12.57	12.57	2	0.04	0.01	0.05	0.00	0.00	24.0
4	38	-13435	1227	482	0	265	504	6.28	6.28	12.57	12.57	2	0.04	0.02	0.11	0.00	0.00	24.0
5	38	-13425	1240	438	0	289	513	6.28	6.28	12.57	12.57	2	0.04	0.02	0.11	0.00	0.00	24.0
6	38	-14025	51	616	0	215	-237	6.28	6.28	12.57	12.57	2	0.02	0.01	0.06	0.00	0.00	24.0
7	38	-13995	94	468	0	298	-209	6.28	6.28	12.57	12.57	2	0.02	0.01	0.04	0.00	0.00	24.0
8	38	-13755	587	578	0	224	101	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
9	38	-13725	630	430	0	307	129	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
10	38	-14325	-559	608	0	232	-621	6.28	6.28	12.57	12.57	2	0.04	0.01	0.06	0.00	0.00	24.0
11	38	-14315	-546	564	0	257	-612	6.28	6.28	12.57	12.57	2	0.04	0.01	0.05	0.00	0.00	24.0
12	38	-13435	1227	482	0	265	504	6.28	6.28	12.57	12.57	2	0.04	0.02	0.11	0.00	0.00	24.0
13	38	-13425	1240	438	0	289	513	6.28	6.28	12.57	12.57	2	0.04	0.02	0.11	0.00	0.00	24.0
14	38	-14025	51	616	0	215	-237	6.28	6.28	12.57	12.57	2	0.02	0.01	0.06	0.00	0.00	24.0
15	38	-13995	94	468	0	298	-209	6.28	6.28	12.57	12.57	2	0.02	0.01	0.04	0.00	0.00	24.0
16	38	-13755	587	578	0	224	101	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
17	38	-13725	630	430	0	307	129	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
18	38	-21168	-2436	907	0	411	-1936	6.28	6.28	12.57	12.57	3	0.10	0.04	0.20	0.00	0.00	24.0
19	38	-17748	3188	402	0	538	1622	6.28	6.28	12.57	12.57	3	0.09	0.06	0.27	0.00	0.00	24.0
20	38	-19088	380	1004	0	107	-146	6.28	6.28	12.57	12.57	3	0.01	0.02	0.09	0.00	0.00	24.0
37	38	-21838	-4290	1090	0	319	-3095	6.28	6.28	12.57	12.57	3	0.16	0.08	0.35	0.00	0.00	24.0
38	38	-16138	5082	249	0	531	2836	6.28	6.28	12.57	12.57	3	0.15	0.09	0.44	0.00	0.00	24.0
39	38	-18368	402	1252	0	-187	-111	6.28	6.28	12.57	12.57	3	0.01	0.02	0.11	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-17940	443	680	0	254	-15	6.28	6.28	12.57	12.57	3	0.01	0.01	0.06	0.00	0.00	24.0
2	50	-14250	-559	608	0	156	-690	6.28	6.28	12.57	12.57	2	0.04	0.01	0.06	0.00	0.00	24.0
3	50	-14240	-546	564	0	187	-680	6.28	6.28	12.57	12.57	2	0.04	0.01	0.05	0.00	0.00	24.0
4	50	-13360	1227	482	0	204	658	6.28	6.28	12.57	12.57	2	0.04	0.02	0.11	0.00	0.00	24.0
5	50	-13350	1240	438	0	235	668	6.28	6.28	12.57	12.57	2	0.04	0.02	0.11	0.00	0.00	24.0
6	50	-13950	51	616	0	138	-230	6.28	6.28	12.57	12.57	2	0.02	0.01	0.06	0.00	0.00	24.0
7	50	-13920	94	468	0	239	-197	6.28	6.28	12.57	12.57	2	0.02	0.01	0.04	0.00	0.00	24.0
8	50	-13680	587	578	0	152	174	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
9	50	-13650	630	430	0	253	208	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
10	50	-14250	-559	608	0	156	-690	6.28	6.28	12.57	12.57	2	0.04	0.01	0.06	0.00	0.00	24.0
11	50	-14240	-546	564	0	187	-680	6.28	6.28	12.57	12.57	2	0.04	0.01	0.05	0.00	0.00	24.0
12	50	-13360	1227	482	0	204	658	6.28	6.28	12.57	12.57	2	0.04	0.02	0.11	0.00	0.00	24.0
13	50	-13350	1240	438	0	235	668	6.28	6.28	12.57	12.57	2	0.04	0.02	0.11	0.00	0.00	24.0
14	50	-13950	51	616	0	138	-230	6.28	6.28	12.57	12.57	2	0.02	0.01	0.06	0.00	0.00	24.0
15	50	-13920	94	468	0	239	-197	6.28	6.28	12.57	12.57	2	0.02	0.01	0.04	0.00	0.00	24.0
16	50	-13680	587	578	0	152	174	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
17	50	-13650	630	430	0	253	208	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
18	50	-21070	-2436	907	0	298	-2240	6.28	6.28	12.57	12.57	3	0.12	0.04	0.20	0.00	0.00	24.0
19	50	-17650	3188	402	0	488	2021	6.28	6.28	12.57	12.57	3	0.11	0.06	0.27	0.00	0.00	24.0
20	50	-18990	380	1004	0	-18	-98	6.28	6.28	12.57	12.57	3	0.01	0.02	0.09	0.00	0.00	24.0
37	50	-21740	-4290	1090	0	183	-3631	6.28	6.28	12.57	12.57	3	0.19	0.08	0.35	0.00	0.00	24.0
38	50	-16040	5082	249	0	500	3471	6.28	6.28	12.57	12.57	3	0.19	0.09	0.45	0.00	0.00	24.0
39	50	-18270	402	1252	0	-343	-61	6.28	6.28	12.57	12.57	3	0.01	0.02	0.11	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 108 NI 1254 NF 1349 SEZ. Rp B= 0.600 H= 0.400 (pilastro)

PIL. NUM. 9
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-5105	-13	3	0	-37	-12	6.28	6.28	12.57	12.57	3	0.00	0.00	0.00	0.00	0.00	24.0
2	0	-3936	-69	74	0	-40	-100	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
3	0	-3911	-68	-24	0	-28	-98	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
4	0	-3943	47	29	0	-30	79	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
5	0	-3918	48	-69	0	-17	80	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
6	0	-3969	-29	173	0	-52	-39	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
7	0	-3883	-26	-154	0	-9	-34	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
8	0	-3971	6	159	0	-49	15	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
9	0	-3886	9	-168	0	-6	19	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
10	0	-3936	-69	74	0	-40	-100	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
11	0	-3911	-68	-24	0	-28	-98	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
12	0	-3943	47	29	0	-30	79	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
13	0	-3918	48	-69	0	-17	80	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
14	0	-3969	-29	173	0	-52	-39	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
15	0	-3883	-26	-154	0	-9	-34	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
16	0	-3971	6	159	0	-49	15	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
17	0	-3886	9	-168	0	-6	19	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
18	0	-5489	-169	264	0	-85	-250	6.28	6.28	12.57	12.57	3	0.01	0.00	0.03	0.00	0.00	24.0
19	0	-5460	180	-22	0	-30	289	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
20	0	-5440	4	265	0	-79	17	6.28	6.28	12.57	12.57	3	0.00	0.00	0.03	0.00	0.00	24.0
37	0	-5327	-291	326	0	-97	-441	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
38	0	-5279	290	-152	0	-6	459	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
39	0	-5244	-3	328	0	-86	5	6.28	6.28	12.57	12.57	3	0.00	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	12	-5008	-13	3	0	-38	-14	6.28	6.28	12.57	12.57	3	0.00	0.00	0.00	0.00	0.00	24.0
2	12	-3861	-69	74	0	-50	-108	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
3	12	-3836	-68	-24	0	-25	-107	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
4	12	-3868	47	29	0	-34	85	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
5	12	-3843	48	-69	0	-9	86	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
6	12	-3894	-29	173	0	-73	-42	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
7	12	-3808	-26	-154	0	10	-37	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
8	12	-3896	6	159	0	-69	16	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
9	12	-3811	9	-168	0	15	21	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
10	12	-3861	-69	74	0	-50	-108	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
11	12	-3836	-68	-24	0	-25	-107	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
12	12	-3868	47	29	0	-34	85	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
13	12	-3843	48	-69	0	-9	86	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
14	12	-3894	-29	173	0	-73	-42	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
15	12	-3808	-26	-154	0	10	-37	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
16	12	-3896	6	159	0	-69	16	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
17	12	-3811	9	-168	0	15	21	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
18	12	-5392	-169	264	0	-118	-271	6.28	6.28	12.57	12.57	3	0.02	0.00	0.03	0.00	0.00	24.0
19	12	-5362	180	-22	0	-28	312	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
20	12	-5342	4	265	0	-112	18	6.28	6.28	12.57	12.57	3	0.00	0.00	0.03	0.00	0.00	24.0
37	12	-5230	-291	326	0	-138	-477	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
38	12	-5182	290	-152	0	13	495	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
39	12	-5146	-3	328	0	-127	5	6.28	6.28	12.57	12.57	3	0.00	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	25	-4910	-13	3	0	-38	-16	6.28	6.28	12.57	12.57	3	0.00	0.00	0.00	0.00	0.00	24.0
2	25	-3786	-69	74	0	-59	-117	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
3	25	-3761	-68	-24	0	-22	-115	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
4	25	-3793	47	29	0	-37	91	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
5	25	-3768	48	-69	0	0	92	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
6	25	-3819	-29	173	0	-95	-46	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
7	25	-3733	-26	-154	0	30	-41	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
8	25	-3821	6	159	0	-89	16	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
9	25	-3736	9	-168	0	36	22	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
10	25	-3786	-69	74	0	-59	-117	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
11	25	-3761	-68	-24	0	-22	-115	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
12	25	-3793	47	29	0	-37	91	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
13	25	-3768	48	-69	0	0	92	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
14	25	-3819	-29	173	0	-95	-46	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
15	25	-3733	-26	-154	0	30	-41	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
16	25	-3821	6	159	0	-89	16	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
17	25	-3736	9	-168	0	36	22	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
18	25	-5294	-169	264	0	-151	-293	6.28	6.28	12.57	12.57	3	0.02	0.00	0.03	0.00	0.00	24.0
19	25	-5265	180	-22	0	-25	334	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
20	25	-5245	4	265	0	-145	18	6.28	6.28	12.57	12.57	3	0.01	0.00	0.03	0.00	0.00	24.0
37	25	-5132	-291	326	0	-178	-513	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
38	25	-5084	290	-152	0	32	531	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
39	25	-5049	-3	328	0	-168	4	6.28	6.28	12.57	12.57	3	0.01	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	38	-4812	-13	3	0	-39	-17	6.28	6.28	12.57	12.57	3	0.00	0.00	0.00	0.00	0.00	24.0
2	38	-3711	-69	74	0	-68	-125	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
3	38	-3686	-68	-24	0	-19	-124	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
4	38	-3718	47	29	0	-41	97	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
5	38	-3693	48	-69	0	9	98	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
6	38	-3744	-29	173	0	-117	-50	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
7	38	-3658	-26	-154	0	49	-44	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
8	38	-3746	6	159	0	-108	17	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
9	38	-3661	9	-168	0	57	23	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
10	38	-3711	-69	74	0	-68	-125	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
11	38	-3686	-68	-24	0	-19	-124	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
12	38	-3718	47	29	0	-41	97	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
13	38	-3693	48	-69	0	9	98	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
14	38	-3744	-29	173	0	-117	-50	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
15	38	-3658	-26	-154	0	49	-44	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
16	38	-3746	6	159	0	-108	17	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
17	38	-3661	9	-168	0	57	23	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
18	38	-5196	-169	264	0	-184	-314	6.28	6.28	12.57	12.57	3	0.02	0.00	0.03	0.00	0.00	24.0
19	38	-5168	180	-22	0	-22	357	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
20	38	-5148	4	265	0	-178	19	6.28	6.28	12.57	12.57	3	0.01	0.00	0.03	0.00	0.00	24.0
37	38	-5034	-291	326	0	-219	-550	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
38	38	-4986	290	-152	0	51	568	6.28	6.28	12.57	12.57	3	0.03	0.01	0.03	0.00	0.00	24.0
39	38	-4952	-3	328	0	-209	4	6.28	6.28	12.57	12.57	3	0.01	0.01	0.04	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-4715	-13	3	0	-39	-19	6.28	6.28	12.57	12.57	3	0.00	0.00	0.00	0.00	0.00	24.0
2	50	-3636	-69	74	0	-78	-134	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
3	50	-3611	-68	-24	0	-16	-132	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
4	50	-3643	47	29	0	-45	103	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
5	50	-3618	48	-69	0	17	104	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
6	50	-3669	-29	173	0	-138	-53	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
7	50	-3583	-26	-154	0	68	-47	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
8	50	-3671	6	159	0	-128	18	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
9	50	-3586	9	-168	0	78	24	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
10	50	-3636	-69	74	0	-78	-134	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
11	50	-3611	-68	-24	0	-16	-132	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
12	50	-3643	47	29	0	-45	103	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
13	50	-3618	48	-69	0	17	104	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
14	50	-3669	-29	173	0	-138	-53	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
15	50	-3583	-26	-154	0	68	-47	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
16	50	-3671	6	159	0	-128	18	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
17	50	-3586	9	-168	0	78	24	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
18	50	-5099	-169	264	0	-217	-335	6.28	6.28	12.57	12.57	3	0.02	0.00	0.03	0.00	0.00	24.0
19	50	-5070	180	-22	0	-19	380	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
20	50	-5050	4	265	0	-211	19	6.28	6.28	12.57	12.57	3	0.01	0.00	0.03	0.00	0.00	24.0
37	50	-4937	-291	326	0	-260	-586	6.28	6.28	12.57	12.57	3	0.04	0.01	0.03	0.00	0.00	24.0
38	50	-4889	290	-152	0	70	604	6.28	6.28	12.57	12.57	3	0.04	0.01	0.03	0.00	0.00	24.0
39	50	-4854	-3	328	0	-250	4	6.28	6.28	12.57	12.57	3	0.01	0.01	0.04	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 109 NI 1349 NF 129 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 9A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-7224	-31	197	0	-39	-20	6.28	6.28	12.57	12.57	3	0.00	0.00	0.02	0.00	0.00	24.0
2	0	-5572	-177	321	0	-78	-128	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
3	0	-5533	-175	105	0	-16	-126	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
4	0	-5581	128	198	0	-45	96	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
5	0	-5542	130	-18	0	17	97	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
6	0	-5621	-73	529	0	-138	-52	6.28	6.28	12.57	12.57	2	0.01	0.01	0.06	0.00	0.00	24.0
7	0	-5490	-65	-189	0	68	-46	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
8	0	-5623	18	492	0	-128	16	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
9	0	-5493	26	-226	0	78	21	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
10	0	-5572	-177	321	0	-78	-128	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
11	0	-5533	-175	105	0	-16	-126	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
12	0	-5581	128	198	0	-45	96	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
13	0	-5542	130	-18	0	17	97	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
14	0	-5621	-73	529	0	-138	-52	6.28	6.28	12.57	12.57	2	0.01	0.01	0.06	0.00	0.00	24.0
15	0	-5490	-65	-189	0	68	-46	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
16	0	-5623	18	492	0	-128	16	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
17	0	-5493	26	-226	0	78	21	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
18	0	-7817	-440	836	0	-217	-318	6.28	6.28	12.57	12.57	3	0.02	0.01	0.09	0.00	0.00	24.0
19	0	-7776	480	116	0	-19	356	6.28	6.28	12.57	12.57	3	0.02	0.01	0.05	0.00	0.00	24.0
20	0	-7738	16	814	0	-211	16	6.28	6.28	12.57	12.57	3	0.01	0.01	0.08	0.00	0.00	24.0
37	0	-7564	-763	994	0	-260	-555	6.28	6.28	12.57	12.57	3	0.03	0.02	0.10	0.00	0.00	24.0
38	0	-7494	771	-205	0	70	568	6.28	6.28	12.57	12.57	3	0.03	0.01	0.07	0.00	0.00	24.0
39	0	-7432	-3	958	0	-250	2	6.28	6.28	12.57	12.57	3	0.01	0.02	0.10	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-7126	-31	197	0	-64	-24	6.28	6.28	12.57	12.57	3	0.00	0.00	0.02	0.00	0.00	24.0
2	12	-5497	-177	321	0	-118	-150	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
3	12	-5458	-175	105	0	-29	-148	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
4	12	-5506	128	198	0	-69	112	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
5	12	-5467	130	-18	0	20	114	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
6	12	-5546	-73	529	0	-204	-61	6.28	6.28	12.57	12.57	2	0.01	0.01	0.06	0.00	0.00	24.0
7	12	-5415	-65	-189	0	92	-54	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
8	12	-5548	18	492	0	-190	18	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
9	12	-5418	26	-226	0	106	24	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
10	12	-5497	-177	321	0	-118	-150	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
11	12	-5458	-175	105	0	-29	-148	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
12	12	-5506	128	198	0	-69	112	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
13	12	-5467	130	-18	0	20	114	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
14	12	-5546	-73	529	0	-204	-61	6.28	6.28	12.57	12.57	2	0.01	0.01	0.06	0.00	0.00	24.0
15	12	-5415	-65	-189	0	92	-54	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
16	12	-5548	18	492	0	-190	18	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
17	12	-5418	26	-226	0	106	24	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
18	12	-7720	-440	836	0	-321	-373	6.28	6.28	12.57	12.57	3	0.02	0.01	0.09	0.00	0.00	24.0
19	12	-7678	480	116	0	-34	416	6.28	6.28	12.57	12.57	3	0.02	0.01	0.05	0.00	0.00	24.0
20	12	-7640	16	814	0	-313	18	6.28	6.28	12.57	12.57	3	0.01	0.01	0.08	0.00	0.00	24.0
37	12	-7466	-763	994	0	-384	-651	6.28	6.28	12.57	12.57	3	0.04	0.02	0.10	0.00	0.00	24.0
38	12	-7396	771	-205	0	95	665	6.28	6.28	12.57	12.57	3	0.04	0.01	0.07	0.00	0.00	24.0
39	12	-7334	-3	958	0	-370	1	6.28	6.28	12.57	12.57	3	0.01	0.02	0.10	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-7029	-31	197	0	-88	-27	6.28	6.28	12.57	12.57	3	0.00	0.00	0.02	0.00	0.00	24.0
2	25	-5422	-177	321	0	-158	-172	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
3	25	-5383	-175	105	0	-42	-170	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
4	25	-5431	128	198	0	-94	128	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
5	25	-5392	130	-18	0	22	130	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
6	25	-5471	-73	529	0	-271	-70	6.28	6.28	12.57	12.57	2	0.02	0.01	0.06	0.00	0.00	24.0
7	25	-5340	-65	-189	0	116	-62	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
8	25	-5473	18	492	0	-251	20	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
9	25	-5343	26	-226	0	135	28	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
10	25	-5422	-177	321	0	-158	-172	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
11	25	-5383	-175	105	0	-42	-170	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
12	25	-5431	128	198	0	-94	128	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
13	25	-5392	130	-18	0	22	130	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
14	25	-5471	-73	529	0	-271	-70	6.28	6.28	12.57	12.57	2	0.02	0.01	0.06	0.00	0.00	24.0
15	25	-5340	-65	-189	0	116	-62	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
16	25	-5473	18	492	0	-251	20	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
17	25	-5343	26	-226	0	135	28	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
18	25	-7622	-440	836	0	-426	-428	6.28	6.28	12.57	12.57	3	0.03	0.01	0.09	0.00	0.00	24.0
19	25	-7581	480	116	0	-48	476	6.28	6.28	12.57	12.57	3	0.03	0.01	0.05	0.00	0.00	24.0

20	25	-7543	16	814	0	-415	20	6.28	6.28	12.57	12.57	3	0.02	0.01	0.08	0.00	0.00	24.0
37	25	-7369	-763	994	0	-508	-746	6.28	6.28	12.57	12.57	3	0.04	0.02	0.10	0.00	0.00	24.0
38	25	-7299	771	-205	0	121	761	6.28	6.28	12.57	12.57	3	0.04	0.01	0.08	0.00	0.00	24.0
39	25	-7237	-3	958	0	-490	1	6.28	6.28	12.57	12.57	3	0.02	0.02	0.10	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-6932	-31	197	0	-113	-31	6.28	6.28	12.57	12.57	3	0.00	0.00	0.02	0.00	0.00	24.0
2	38	-5347	-177	321	0	-198	-194	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
3	38	-5308	-175	105	0	-55	-192	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
4	38	-5356	128	198	0	-119	144	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
5	38	-5317	130	-18	0	24	146	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
6	38	-5396	-73	529	0	-337	-79	6.28	6.28	12.57	12.57	2	0.02	0.01	0.06	0.00	0.00	24.0
7	38	-5265	-65	-189	0	139	-70	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
8	38	-5398	18	492	0	-313	22	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
9	38	-5268	26	-226	0	163	31	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
10	38	-5347	-177	321	0	-198	-194	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
11	38	-5308	-175	105	0	-55	-192	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
12	38	-5356	128	198	0	-119	144	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
13	38	-5317	130	-18	0	24	146	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
14	38	-5396	-73	529	0	-337	-79	6.28	6.28	12.57	12.57	2	0.02	0.01	0.06	0.00	0.00	24.0
15	38	-5265	-65	-189	0	139	-70	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
16	38	-5398	18	492	0	-313	22	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
17	38	-5268	26	-226	0	163	31	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
18	38	-7524	-440	836	0	-530	-483	6.28	6.28	12.57	12.57	3	0.03	0.01	0.09	0.00	0.00	24.0
19	38	-7484	480	116	0	-63	536	6.28	6.28	12.57	12.57	3	0.03	0.01	0.05	0.00	0.00	24.0
20	38	-7446	16	814	0	-516	22	6.28	6.28	12.57	12.57	3	0.02	0.01	0.08	0.00	0.00	24.0
37	38	-7272	-763	994	0	-633	-842	6.28	6.28	12.57	12.57	3	0.05	0.02	0.10	0.00	0.00	24.0
38	38	-7202	771	-205	0	147	857	6.28	6.28	12.57	12.57	3	0.05	0.01	0.08	0.00	0.00	24.0
39	38	-7140	-3	958	0	-609	1	6.28	6.28	12.57	12.57	3	0.02	0.02	0.10	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-6834	-31	197	0	-138	-35	6.28	6.28	12.57	12.57	3	0.01	0.00	0.02	0.00	0.00	24.0
2	50	-5272	-177	321	0	-238	-216	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
3	50	-5233	-175	105	0	-68	-213	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
4	50	-5281	128	198	0	-143	160	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
5	50	-5242	130	-18	0	26	163	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
6	50	-5321	-73	529	0	-403	-88	6.28	6.28	12.57	12.57	2	0.02	0.01	0.06	0.00	0.00	24.0
7	50	-5190	-65	-189	0	163	-78	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
8	50	-5323	18	492	0	-374	25	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
9	50	-5193	26	-226	0	191	34	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
10	50	-5272	-177	321	0	-238	-216	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
11	50	-5233	-175	105	0	-68	-213	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
12	50	-5281	128	198	0	-143	160	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
13	50	-5242	130	-18	0	26	163	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
14	50	-5321	-73	529	0	-403	-88	6.28	6.28	12.57	12.57	2	0.02	0.01	0.06	0.00	0.00	24.0
15	50	-5190	-65	-189	0	163	-78	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
16	50	-5323	18	492	0	-374	25	6.28	6.28	12.57	12.57	2	0.02	0.01	0.05	0.00	0.00	24.0
17	50	-5193	26	-226	0	191	34	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
18	50	-7427	-440	836	0	-635	-538	6.28	6.28	12.57	12.57	3	0.04	0.01	0.09	0.00	0.00	24.0
19	50	-7386	480	116	0	-77	597	6.28	6.28	12.57	12.57	3	0.03	0.01	0.05	0.00	0.00	24.0
20	50	-7348	16	814	0	-618	24	6.28	6.28	12.57	12.57	3	0.02	0.01	0.08	0.00	0.00	24.0
37	50	-7174	-763	994	0	-757	-937	6.28	6.28	12.57	12.57	3	0.06	0.02	0.10	0.00	0.00	24.0
38	50	-7104	771	-205	0	172	954	6.28	6.28	12.57	12.57	3	0.06	0.01	0.08	0.00	0.00	24.0
39	50	-7042	-3	958	0	-729	0	6.28	6.28	12.57	12.57	3	0.03	0.02	0.10	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 110 NI 1158 NF 1253 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 8
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-3610	148	378	0	-159	-12	6.28	6.28	9.42	9.42	3	0.01	0.01	0.05	0.00	0.00	24.0
2	0	-2783	84	344	0	-127	-1	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
3	0	-2731	84	295	0	-116	-1	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
4	0	-2824	144	286	0	-129	-18	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
5	0	-2772	144	238	0	-117	-18	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
6	0	-2858	104	380	0	-141	-6	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
7	0	-2684	106	218	0	-103	-7	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
8	0	-2871	122	363	0	-142	-11	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
9	0	-2696	124	201	0	-103	-12	6.28	6.28	9.42	9.42	2	0.01	0.00	0.03	0.00	0.00	24.0
10	0	-2783	84	344	0	-127	-1	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
11	0	-2731	84	295	0	-116	-1	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
12	0	-2824	144	286	0	-129	-18	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
13	0	-2772	144	238	0	-117	-18	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
14	0	-2858	104	380	0	-141	-6	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
15	0	-2684	106	218	0	-103	-7	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
16	0	-2871	122	363	0	-142	-11	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
17	0	-2696	124	201	0	-103	-12	6.28	6.28	9.42	9.42	2	0.01	0.00	0.03	0.00	0.00	24.0
18	0	-3834	78	581	0	-197	9	6.28	6.28	9.42	9.42	3	0.01	0.01	0.08	0.00	0.00	24.0
19	0	-3873	255	333	0	-183	-41	6.28	6.28	9.42	9.42	3	0.01	0.01	0.04	0.00	0.00	24.0
20	0	-3958	162	555	0	-208	-14	6.28	6.28	9.42	9.42	3	0.01	0.01	0.07	0.00	0.00	24.0
37	0	-3713	11	634	0	-189	27	6.28	6.28	9.42	9.42	3	0.01	0.01	0.08	0.00	0.00	24.0
38	0	-3779	307	222	0	-166	-56	6.28	6.28	9.42	9.42	3	0.01	0.01	0.03	0.00	0.00	24.0
39	0	-3920	152	592	0	-208	-11	6.28	6.28	9.42	9.42	3	0.01	0.01	0.08	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-3537	148	378	0	-206	7	6.28	6.28	9.42	9.42	3	0.01	0.01	0.05	0.00	0.00	24.0
2	12	-2727	84	344	0	-170	10	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
3	12	-2675	84	295	0	-152	10	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
4	12	-2768	144	286	0	-164	0	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
5	12	-2716	144	238	0	-147	0	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
6	12	-2802	104	380	0	-189	7	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
7	12	-2628	106	218	0	-130	6	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
8	12	-2815	122	363	0	-187	4	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
9	12	-2640	124	201	0	-128	3	6.28	6.28	9.42	9.42	2	0.01	0.00	0.03	0.00	0.00	24.0
10	12	-2727	84	344	0	-170	10	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
11	12	-2675	84	295	0	-152	10	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
12	12	-2768	144	286	0	-164	0	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
13	12	-2716	144	238	0	-147	0	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
14	12	-2802	104	380	0	-189	7	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
15	12	-2628	106	218	0	-130	6	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0

16	12	-2815	122	363	0	-187	4	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
17	12	-2640	124	201	0	-128	3	6.28	6.28	9.42	9.42	2	0.01	0.00	0.03	0.00	0.00	24.0
18	12	-3761	78	581	0	-270	19	6.28	6.28	9.42	9.42	3	0.01	0.01	0.08	0.00	0.00	24.0
19	12	-3800	255	333	0	-225	-9	6.28	6.28	9.42	9.42	3	0.01	0.01	0.04	0.00	0.00	24.0
20	12	-3885	162	555	0	-278	6	6.28	6.28	9.42	9.42	3	0.01	0.01	0.07	0.00	0.00	24.0
37	12	-3640	11	634	0	-269	29	6.28	6.28	9.42	9.42	3	0.01	0.01	0.08	0.00	0.00	24.0
38	12	-3706	307	222	0	-193	-18	6.28	6.28	9.42	9.42	3	0.01	0.01	0.03	0.00	0.00	24.0
39	12	-3847	152	592	0	-282	8	6.28	6.28	9.42	9.42	3	0.01	0.01	0.08	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-3464	148	378	0	-253	25	6.28	6.28	9.42	9.42	3	0.01	0.01	0.05	0.00	0.00	24.0
2	25	-2670	84	344	0	-213	20	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
3	25	-2618	84	295	0	-189	20	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
4	25	-2712	144	286	0	-200	18	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
5	25	-2660	144	238	0	-176	18	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
6	25	-2746	104	380	0	-236	20	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
7	25	-2572	106	218	0	-157	19	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
8	25	-2758	122	363	0	-232	19	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
9	25	-2584	124	201	0	-153	19	6.28	6.28	9.42	9.42	2	0.01	0.00	0.03	0.00	0.00	24.0
10	25	-2670	84	344	0	-213	20	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
11	25	-2618	84	295	0	-189	20	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
12	25	-2712	144	286	0	-200	18	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
13	25	-2660	144	238	0	-176	18	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
14	25	-2746	104	380	0	-236	20	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
15	25	-2572	106	218	0	-157	19	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
16	25	-2758	122	363	0	-232	19	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
17	25	-2584	124	201	0	-153	19	6.28	6.28	9.42	9.42	2	0.01	0.00	0.03	0.00	0.00	24.0
18	25	-3688	78	581	0	-343	29	6.28	6.28	9.42	9.42	3	0.02	0.01	0.08	0.00	0.00	24.0
19	25	-3727	255	333	0	-266	23	6.28	6.28	9.42	9.42	3	0.01	0.01	0.04	0.00	0.00	24.0
20	25	-3812	162	555	0	-347	26	6.28	6.28	9.42	9.42	3	0.02	0.01	0.07	0.00	0.00	24.0
37	25	-3566	11	634	0	-348	30	6.28	6.28	9.42	9.42	3	0.02	0.01	0.08	0.00	0.00	24.0
38	25	-3633	307	222	0	-221	20	6.28	6.28	9.42	9.42	3	0.01	0.01	0.03	0.00	0.00	24.0
39	25	-3774	152	592	0	-356	27	6.28	6.28	9.42	9.42	3	0.02	0.01	0.08	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-3391	148	378	0	-300	44	6.28	6.28	9.42	9.42	3	0.02	0.01	0.05	0.00	0.00	24.0
2	38	-2614	84	344	0	-256	31	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
3	38	-2562	84	295	0	-226	31	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
4	38	-2655	144	286	0	-236	36	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
5	38	-2603	144	238	0	-206	36	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
6	38	-2689	104	380	0	-284	33	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
7	38	-2515	106	218	0	-184	32	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
8	38	-2702	122	363	0	-278	35	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
9	38	-2527	124	201	0	-178	34	6.28	6.28	9.42	9.42	2	0.01	0.00	0.03	0.00	0.00	24.0
10	38	-2614	84	344	0	-256	31	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
11	38	-2562	84	295	0	-226	31	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
12	38	-2655	144	286	0	-236	36	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
13	38	-2603	144	238	0	-206	36	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
14	38	-2689	104	380	0	-284	33	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
15	38	-2515	106	218	0	-184	32	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
16	38	-2702	122	363	0	-278	35	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
17	38	-2527	124	201	0	-178	34	6.28	6.28	9.42	9.42	2	0.01	0.00	0.03	0.00	0.00	24.0
18	38	-3614	78	581	0	-415	38	6.28	6.28	9.42	9.42	3	0.02	0.01	0.08	0.00	0.00	24.0
19	38	-3654	255	333	0	-308	55	6.28	6.28	9.42	9.42	3	0.02	0.01	0.04	0.00	0.00	24.0
20	38	-3738	162	555	0	-417	47	6.28	6.28	9.42	9.42	3	0.02	0.01	0.07	0.00	0.00	24.0
37	38	-3493	11	634	0	-427	31	6.28	6.28	9.42	9.42	3	0.02	0.01	0.08	0.00	0.00	24.0
38	38	-3560	307	222	0	-249	59	6.28	6.28	9.42	9.42	3	0.01	0.01	0.03	0.00	0.00	24.0
39	38	-3701	152	592	0	-430	46	6.28	6.28	9.42	9.42	3	0.02	0.01	0.08	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-3318	148	378	0	-348	62	6.28	6.28	9.42	9.42	3	0.02	0.01	0.05	0.00	0.00	24.0
2	50	-2558	84	344	0	-299	41	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
3	50	-2506	84	295	0	-263	41	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
4	50	-2599	144	286	0	-272	54	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
5	50	-2547	144	238	0	-236	54	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
6	50	-2633	104	380	0	-332	46	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
7	50	-2459	106	218	0	-211	46	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
8	50	-2646	122	363	0	-323	50	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
9	50	-2471	124	201	0	-203	50	6.28	6.28	9.42	9.42	2	0.02	0.00	0.03	0.00	0.00	24.0
10	50	-2558	84	344	0	-299	41	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
11	50	-2506	84	295	0	-263	41	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
12	50	-2599	144	286	0	-272	54	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
13	50	-2547	144	238	0	-236	54	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
14	50	-2633	104	380	0	-332	46	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
15	50	-2459	106	218	0	-211	46	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
16	50	-2646	122	363	0	-323	50	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
17	50	-2471	124	201	0	-203	50	6.28	6.28	9.42	9.42	2	0.02	0.00	0.03	0.00	0.00	24.0
18	50	-3541	78	581	0	-488	48	6.28	6.28	9.42	9.42	3	0.02	0.01	0.08	0.00	0.00	24.0
19	50	-3581	255	333	0	-350	87	6.28	6.28	9.42	9.42	3	0.02	0.01	0.04	0.00	0.00	24.0
20	50	-3665	162	555	0	-486	67	6.28	6.28	9.42	9.42	3	0.02	0.01	0.07	0.00	0.00	24.0
37	50	-3420	11	634	0	-507	33	6.28	6.28	9.42	9.42	3	0.03	0.01	0.08	0.00	0.00	24.0
38	50	-3487	307	222	0	-277	97	6.28	6.28	9.42	9.42	3	0.02	0.01	0.03	0.00	0.00	24.0
39	50	-3628	152	592	0	-504	65	6.28	6.28	9.42	9.42	3	0.03	0.01	0.08	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 111 NI 1253 NF 213 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 8A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m			cmq				Fx,M	Bielle	V,Mx		cmq/m	cm

1	0	-4585	-35	386	0	-376	56	6.28	6.28	9.42	9.42	3	0.02	0.01	0.05	0.00	0.00	24.0
2	0	-3521	-99	378	0	-325	33	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
3	0	-3475	-94	289	0	-282	33	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
4	0	-3579	40	305	0	-296	53	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
5	0	-3533	45	216	0	-253	53	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
6	0	-3595	-56	456	0	-365	40	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
7	0	-3442	-40	160	0	-222	40	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
8	0	-3612	-15	434	0	-356	46	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
9	0	-3459	2	138	0	-213	46	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
10	0	-3521	-99	378	0	-325	33	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
11	0	-3475	-94	289	0	-282	33	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0

12	0	-3579	40	305	0	-296	53	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
13	0	-3533	45	216	0	-253	53	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
14	0	-3595	-56	456	0	-365	40	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
15	0	-3442	-40	160	0	-222	40	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
16	0	-3612	-15	434	0	-356	46	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
17	0	-3459	2	138	0	-213	46	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
18	0	-4828	-236	712	0	-535	33	6.28	6.28	9.42	9.42	3	0.03	0.02	0.09	0.00	0.00	24.0
19	0	-4926	181	354	0	-380	91	6.28	6.28	9.42	9.42	3	0.02	0.01	0.05	0.00	0.00	24.0
20	0	-4974	-38	697	0	-539	62	6.28	6.28	9.42	9.42	3	0.03	0.02	0.09	0.00	0.00	24.0
37	0	-4662	-376	778	0	-556	11	6.28	6.28	9.42	9.42	3	0.03	0.02	0.10	0.00	0.00	24.0
38	0	-4826	319	183	0	-298	108	6.28	6.28	9.42	9.42	3	0.02	0.01	0.03	0.00	0.00	24.0
39	0	-4905	-47	754	0	-562	60	6.28	6.28	9.42	9.42	3	0.03	0.02	0.10	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-4512	-35	386	0	-424	51	6.28	6.28	9.42	9.42	3	0.02	0.01	0.05	0.00	0.00	24.0
2	12	-3465	-99	378	0	-372	21	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
3	12	-3419	-94	289	0	-318	21	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
4	12	-3523	40	305	0	-334	58	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
5	12	-3477	45	216	0	-280	58	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
6	12	-3539	-56	456	0	-422	33	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
7	12	-3386	-40	160	0	-242	35	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
8	12	-3556	-15	434	0	-411	44	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
9	12	-3403	2	138	0	-230	46	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
10	12	-3465	-99	378	0	-372	21	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
11	12	-3419	-94	289	0	-318	21	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
12	12	-3523	40	305	0	-334	58	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
13	12	-3477	45	216	0	-280	58	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
14	12	-3539	-56	456	0	-422	33	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
15	12	-3386	-40	160	0	-242	35	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
16	12	-3556	-15	434	0	-411	44	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
17	12	-3403	2	138	0	-230	46	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
18	12	-4755	-236	712	0	-624	4	6.28	6.28	9.42	9.42	3	0.03	0.02	0.09	0.00	0.00	24.0
19	12	-4853	181	354	0	-425	114	6.28	6.28	9.42	9.42	3	0.02	0.01	0.05	0.00	0.00	24.0
20	12	-4901	-38	697	0	-626	57	6.28	6.28	9.42	9.42	3	0.03	0.02	0.09	0.00	0.00	24.0
37	12	-4589	-376	778	0	-653	-36	6.28	6.28	9.42	9.42	3	0.03	0.02	0.10	0.00	0.00	24.0
38	12	-4753	319	183	0	-321	148	6.28	6.28	9.42	9.42	3	0.02	0.01	0.03	0.00	0.00	24.0
39	12	-4832	-47	754	0	-657	54	6.28	6.28	9.42	9.42	3	0.03	0.02	0.10	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-4439	-35	386	0	-472	47	6.28	6.28	9.42	9.42	3	0.02	0.01	0.05	0.00	0.00	24.0
2	25	-3408	-99	378	0	-419	8	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
3	25	-3362	-94	289	0	-354	9	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
4	25	-3466	40	305	0	-372	63	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
5	25	-3420	45	216	0	-307	64	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
6	25	-3482	-56	456	0	-479	26	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
7	25	-3330	-40	160	0	-262	30	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
8	25	-3500	-15	434	0	-465	42	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
9	25	-3346	2	138	0	-247	46	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
10	25	-3408	-99	378	0	-419	8	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
11	25	-3362	-94	289	0	-354	9	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
12	25	-3466	40	305	0	-372	63	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
13	25	-3420	45	216	0	-307	64	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
14	25	-3482	-56	456	0	-479	26	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
15	25	-3330	-40	160	0	-262	30	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
16	25	-3500	-15	434	0	-465	42	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
17	25	-3346	2	138	0	-247	46	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
18	25	-4682	-236	712	0	-713	-26	6.28	6.28	9.42	9.42	3	0.04	0.02	0.09	0.00	0.00	24.0
19	25	-4780	181	354	0	-469	136	6.28	6.28	9.42	9.42	3	0.03	0.01	0.05	0.00	0.00	24.0
20	25	-4828	-38	697	0	-713	53	6.28	6.28	9.42	9.42	3	0.04	0.02	0.09	0.00	0.00	24.0
37	25	-4516	-376	778	0	-751	-83	6.28	6.28	9.42	9.42	3	0.04	0.02	0.10	0.00	0.00	24.0
38	25	-4680	319	183	0	-344	188	6.28	6.28	9.42	9.42	3	0.02	0.01	0.03	0.00	0.00	24.0
39	25	-4759	-47	754	0	-751	48	6.28	6.28	9.42	9.42	3	0.04	0.02	0.10	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-4366	-35	386	0	-521	43	6.28	6.28	9.42	9.42	3	0.03	0.01	0.05	0.00	0.00	24.0
2	38	-3352	-99	378	0	-467	-4	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
3	38	-3306	-94	289	0	-390	-2	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
4	38	-3410	40	305	0	-410	68	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
5	38	-3364	45	216	0	-334	69	6.28	6.28	9.42	9.42	2	0.03	0.01	0.03	0.00	0.00	24.0
6	38	-3426	-56	456	0	-536	19	6.28	6.28	9.42	9.42	2	0.04	0.01	0.06	0.00	0.00	24.0
7	38	-3273	-40	160	0	-282	25	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
8	38	-3443	-15	434	0	-519	41	6.28	6.28	9.42	9.42	2	0.04	0.01	0.06	0.00	0.00	24.0
9	38	-3290	2	138	0	-265	46	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
10	38	-3352	-99	378	0	-467	-4	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
11	38	-3306	-94	289	0	-390	-2	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
12	38	-3410	40	305	0	-410	68	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
13	38	-3364	45	216	0	-334	69	6.28	6.28	9.42	9.42	2	0.03	0.01	0.03	0.00	0.00	24.0
14	38	-3426	-56	456	0	-536	19	6.28	6.28	9.42	9.42	2	0.04	0.01	0.06	0.00	0.00	24.0
15	38	-3273	-40	160	0	-282	25	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
16	38	-3443	-15	434	0	-519	41	6.28	6.28	9.42	9.42	2	0.04	0.01	0.06	0.00	0.00	24.0
17	38	-3290	2	138	0	-265	46	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
18	38	-4608	-236	712	0	-802	-55	6.28	6.28	9.42	9.42	3	0.04	0.02	0.09	0.00	0.00	24.0
19	38	-4707	181	354	0	-513	159	6.28	6.28	9.42	9.42	3	0.03	0.01	0.05	0.00	0.00	24.0
20	38	-4754	-38	697	0	-801	48	6.28	6.28	9.42	9.42	3	0.04	0.02	0.09	0.00	0.00	24.0
37	38	-4442	-376	778	0	-848	-130	6.28	6.28	9.42	9.42	3	0.04	0.02	0.10	0.00	0.00	24.0
38	38	-4606	319	183	0	-366	228	6.28	6.28	9.42	9.42	3	0.03	0.01	0.03	0.00	0.00	24.0
39	38	-4686	-47	754	0	-845	42	6.28	6.28	9.42	9.42	3	0.04	0.02	0.10	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-4293	-35	386	0	-569	38	6.28	6.28	9.42	9.42	3	0.03	0.01	0.05	0.00	0.00	24.0
2	50	-3296	-99	378	0	-514	-16	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
3	50	-3250	-94	289	0	-426	-14	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
4	50	-3354	40	305	0	-449	73	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
5	50	-3308	45	216	0	-361	75	6.28	6.28	9.42	9.42	2	0.03	0.01	0.03	0.00	0.00	24.0
6	50	-3370	-56	456	0	-593	12	6.28	6.28	9.42	9.42	2	0.04	0.01	0.06	0.00	0.00	24.0
7	50	-3217	-40	160	0	-302	20	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
8	50	-3387	-15	434	0	-573	39	6.28	6.28	9.42	9.42	2	0.04	0.01	0.06	0.00	0.00	24.0
9	50	-3234	2	138	0	-282	47	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
10	50	-3296	-99	378	0	-514	-16	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
11	50	-3250	-94	289	0	-426	-14	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
12	50	-3354	40	305	0	-449	73	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
13	50	-3308	45	216	0	-361	75	6.28	6.28	9.42	9.42	2	0.03	0.01	0.03	0.00	0.00	24.0
14	50	-3370	-56	456	0	-593	12	6.28	6.28	9.42	9.42	2	0.04	0.01	0.06	0.00	0.00	24.0
15	50	-3217	-40	160	0	-302	20	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0
16	50	-3387	-15	434	0	-573	39	6.28	6.28	9.42	9.42	2	0.04	0.01	0.06	0.00	0.00	24.0
17	50	-3234	2	138	0	-282	47	6.28	6.28	9.42	9.42	2	0.02	0.00	0.02	0.00	0.00	24.0

18	50	-4535	-236	712	0	-891	-85	6.28	6.28	9.42	9.42	3	0.04	0.02	0.09	0.00	0.00	24.0
19	50	-4634	181	354	0	-558	182	6.28	6.28	9.42	9.42	3	0.03	0.01	0.05	0.00	0.00	24.0
20	50	-4681	-38	697	0	-888	43	6.28	6.28	9.42	9.42	3	0.04	0.02	0.09	0.00	0.00	24.0
37	50	-4369	-376	778	0	-945	-177	6.28	6.28	9.42	9.42	3	0.05	0.02	0.10	0.00	0.00	24.0
38	50	-4533	319	183	0	-389	267	6.28	6.28	9.42	9.42	3	0.03	0.01	0.03	0.00	0.00	24.0
39	50	-4613	-47	754	0	-939	36	6.28	6.28	9.42	9.42	3	0.05	0.02	0.10	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 112 NI 175 NF 89 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 17
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-7676	29	-100	0	343	-9	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
2	0	-5905	16	-53	0	216	-7	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
3	0	-5923	16	-105	0	317	-7	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
4	0	-5887	28	-50	0	211	-7	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
5	0	-5905	29	-102	0	312	-7	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
6	0	-5877	19	9	0	96	-7	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
7	0	-5937	22	-165	0	434	-7	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
8	0	-5872	23	10	0	94	-7	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
9	0	-5932	25	-164	0	432	-7	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
10	0	-5905	16	-53	0	216	-7	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
11	0	-5923	16	-105	0	317	-7	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
12	0	-5887	28	-50	0	211	-7	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
13	0	-5905	29	-102	0	312	-7	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
14	0	-5877	19	9	0	96	-7	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
15	0	-5937	22	-165	0	434	-7	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
16	0	-5872	23	10	0	94	-7	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
17	0	-5932	25	-164	0	432	-7	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
18	0	-8876	-118	-256	0	836	0	6.28	6.28	12.57	12.57	3	0.03	0.00	0.03	0.00	0.00	24.0
19	0	-8473	149	-203	0	694	-19	6.28	6.28	12.57	12.57	3	0.03	0.00	0.02	0.00	0.00	24.0
20	0	-8574	22	-585	0	3306	-10	6.28	6.28	12.57	12.57	3	0.12	0.01	0.06	0.00	0.00	24.0
37	0	-8699	-202	-232	0	747	7	6.28	6.28	12.57	12.57	3	0.03	0.00	0.02	0.00	0.00	24.0
38	0	-8027	242	-144	0	511	-26	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
39	0	-8197	31	-781	0	4864	-10	6.28	6.28	12.57	12.57	3	0.18	0.01	0.08	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-7578	29	-100	0	356	-5	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
2	12	-5830	16	-53	0	223	-5	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
3	12	-5848	16	-105	0	331	-5	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
4	12	-5812	28	-50	0	217	-3	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
5	12	-5830	29	-102	0	325	-3	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
6	12	-5802	19	9	0	95	-4	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
7	12	-5862	22	-165	0	454	-4	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
8	12	-5797	23	10	0	93	-4	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
9	12	-5857	25	-164	0	453	-4	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
10	12	-5830	16	-53	0	223	-5	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
11	12	-5848	16	-105	0	331	-5	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
12	12	-5812	28	-50	0	217	-3	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
13	12	-5830	29	-102	0	325	-3	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
14	12	-5802	19	9	0	95	-4	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
15	12	-5862	22	-165	0	454	-4	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
16	12	-5797	23	10	0	93	-4	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
17	12	-5857	25	-164	0	453	-4	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
18	12	-8778	-118	-256	0	868	-14	6.28	6.28	12.57	12.57	3	0.03	0.00	0.03	0.00	0.00	24.0
19	12	-8376	149	-203	0	720	-1	6.28	6.28	12.57	12.57	3	0.03	0.00	0.02	0.00	0.00	24.0
20	12	-8476	22	-585	0	3379	-7	6.28	6.28	12.57	12.57	3	0.12	0.01	0.06	0.00	0.00	24.0
37	12	-8602	-202	-232	0	776	-18	6.28	6.28	12.57	12.57	3	0.03	0.00	0.02	0.00	0.00	24.0
38	12	-7930	242	-144	0	529	5	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
39	12	-8100	31	-781	0	4961	-6	6.28	6.28	12.57	12.57	3	0.18	0.01	0.08	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-7481	29	-100	0	368	-2	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
2	25	-5755	16	-53	0	229	-3	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
3	25	-5773	16	-105	0	344	-3	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
4	25	-5737	28	-50	0	223	0	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
5	25	-5755	29	-102	0	338	0	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
6	25	-5727	19	9	0	94	-2	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
7	25	-5787	22	-165	0	475	-1	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
8	25	-5722	23	10	0	92	-1	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
9	25	-5782	25	-164	0	473	-1	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
10	25	-5755	16	-53	0	229	-3	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
11	25	-5773	16	-105	0	344	-3	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
12	25	-5737	28	-50	0	223	0	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
13	25	-5755	29	-102	0	338	0	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
14	25	-5727	19	9	0	94	-2	6.28	6.28	12.57	12.57	2	0.01	0.00	0.00	0.00	0.00	24.0
15	25	-5787	22	-165	0	475	-1	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
16	25	-5722	23	10	0	92	-1	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
17	25	-5782	25	-164	0	473	-1	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
18	25	-8681	-118	-256	0	900	-29	6.28	6.28	12.57	12.57	3	0.03	0.00	0.03	0.00	0.00	24.0
19	25	-8278	149	-203	0	745	18	6.28	6.28	12.57	12.57	3	0.03	0.00	0.02	0.00	0.00	24.0
20	25	-8379	22	-585	0	3452	-4	6.28	6.28	12.57	12.57	3	0.13	0.01	0.06	0.00	0.00	24.0
37	25	-8504	-202	-232	0	805	-43	6.28	6.28	12.57	12.57	3	0.03	0.00	0.02	0.00	0.00	24.0
38	25	-7832	242	-144	0	547	35	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
39	25	-8002	31	-781	0	5059	-2	6.28	6.28	12.57	12.57	3	0.19	0.01	0.08	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-7384	29	-100	0	381	2	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
2	38	-5680	16	-53	0	236	-1	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
3	38	-5698	16	-105	0	357	-1	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
4	38	-5662	28	-50	0	229	4	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
5	38	-5680	29	-102	0	350	4	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
6	38	-5652	19	9	0	92	1	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
7	38	-5712	22	-165	0	496	1	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
8	38	-5647	23	10	0	91	2	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
9	38	-5707	25	-164	0	494	3	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
10	38	-5680	16	-53	0	236	-1	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
11	38	-5698	16	-105	0	357	-1	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
12	38	-5662	28	-50	0	229	4	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
13	38	-5680	29	-102	0	350	4	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0

14	38	-5652	19	9	0	92	1	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
15	38	-5712	22	-165	0	496	1	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
16	38	-5647	23	10	0	91	2	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
17	38	-5707	25	-164	0	494	3	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
18	38	-8584	-118	-256	0	932	-44	6.28	6.28	12.57	12.57	3	0.03	0.00	0.03	0.00	0.00	24.0
19	38	-8180	149	-203	0	770	37	6.28	6.28	12.57	12.57	3	0.03	0.00	0.02	0.00	0.00	24.0
20	38	-8282	22	-585	0	3525	-1	6.28	6.28	12.57	12.57	3	0.13	0.01	0.06	0.00	0.00	24.0
37	38	-8406	-202	-232	0	834	-69	6.28	6.28	12.57	12.57	3	0.03	0.00	0.02	0.00	0.00	24.0
38	38	-7734	242	-144	0	565	65	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
39	38	-7904	31	-781	0	5156	2	6.28	6.28	12.57	12.57	3	0.19	0.01	0.08	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-7286	29	-100	0	394	6	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
2	50	-5605	16	-53	0	242	1	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
3	50	-5623	16	-105	0	370	1	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
4	50	-5587	28	-50	0	236	7	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
5	50	-5605	29	-102	0	363	8	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
6	50	-5577	19	9	0	91	3	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
7	50	-5637	22	-165	0	516	4	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
8	50	-5572	23	10	0	89	5	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
9	50	-5632	25	-164	0	514	6	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
10	50	-5605	16	-53	0	242	1	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
11	50	-5623	16	-105	0	370	1	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
12	50	-5587	28	-50	0	236	7	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
13	50	-5605	29	-102	0	363	8	6.28	6.28	12.57	12.57	2	0.02	0.00	0.01	0.00	0.00	24.0
14	50	-5577	19	9	0	91	3	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
15	50	-5637	22	-165	0	516	4	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
16	50	-5572	23	10	0	89	5	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
17	50	-5632	25	-164	0	514	6	6.28	6.28	12.57	12.57	2	0.03	0.00	0.02	0.00	0.00	24.0
18	50	-8486	-118	-256	0	964	-58	6.28	6.28	12.57	12.57	3	0.04	0.00	0.03	0.00	0.00	24.0
19	50	-8083	149	-203	0	796	55	6.28	6.28	12.57	12.57	3	0.03	0.00	0.02	0.00	0.00	24.0
20	50	-8184	22	-585	0	3598	1	6.28	6.28	12.57	12.57	3	0.13	0.01	0.06	0.00	0.00	24.0
37	50	-8309	-202	-232	0	863	-94	6.28	6.28	12.57	12.57	3	0.03	0.00	0.02	0.00	0.00	24.0
38	50	-7637	242	-144	0	583	95	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
39	50	-7807	31	-781	0	5254	6	6.28	6.28	12.57	12.57	3	0.19	0.01	0.08	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 113 NI 89 NF 41 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 17A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-11360	15	-178	0	375	6	6.28	6.28	12.57	12.57	3	0.01	0.00	0.02	0.00	0.00	24.0
2	0	-8740	-24	-93	0	228	1	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
3	0	-8768	-21	-187	0	356	1	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
4	0	-8711	43	-87	0	221	7	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
5	0	-8739	46	-181	0	349	8	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
6	0	-8697	-3	19	0	76	3	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
7	0	-8790	5	-295	0	503	4	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
8	0	-8688	17	21	0	74	5	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
9	0	-8782	25	-293	0	501	6	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
10	0	-8740	-24	-93	0	228	1	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
11	0	-8768	-21	-187	0	356	1	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
12	0	-8711	43	-87	0	221	7	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
13	0	-8739	46	-181	0	349	8	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
14	0	-8697	-3	19	0	76	3	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
15	0	-8790	5	-295	0	503	4	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
16	0	-8688	17	21	0	74	5	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
17	0	-8782	25	-293	0	501	6	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
18	0	-13270	-634	-454	0	921	-58	6.28	6.28	12.57	12.57	3	0.03	0.01	0.05	0.00	0.00	24.0
19	0	-12620	494	-360	0	758	55	6.28	6.28	12.57	12.57	3	0.03	0.01	0.04	0.00	0.00	24.0
20	0	-12780	-40	-1017	0	3315	1	6.28	6.28	12.57	12.57	3	0.12	0.02	0.10	0.00	0.00	24.0
37	0	-12990	-982	-412	0	826	-94	6.28	6.28	12.57	12.57	3	0.03	0.02	0.08	0.00	0.00	24.0
38	0	-11910	897	-255	0	554	95	6.28	6.28	12.57	12.57	3	0.02	0.02	0.07	0.00	0.00	24.0
39	0	-12180	7	-1350	0	4816	6	6.28	6.28	12.57	12.57	3	0.17	0.02	0.13	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-11262	15	-178	0	397	7	6.28	6.28	12.57	12.57	3	0.01	0.00	0.02	0.00	0.00	24.0
2	12	-8665	-24	-93	0	239	-2	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
3	12	-8693	-21	-187	0	379	-1	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
4	12	-8636	43	-87	0	232	13	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
5	12	-8664	46	-181	0	372	13	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
6	12	-8622	-3	19	0	74	3	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
7	12	-8715	5	-295	0	540	5	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
8	12	-8613	17	21	0	71	7	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
9	12	-8707	25	-293	0	537	9	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
10	12	-8665	-24	-93	0	239	-2	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
11	12	-8693	-21	-187	0	379	-1	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
12	12	-8636	43	-87	0	232	13	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
13	12	-8664	46	-181	0	372	13	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
14	12	-8622	-3	19	0	74	3	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
15	12	-8715	5	-295	0	540	5	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
16	12	-8613	17	21	0	71	7	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
17	12	-8707	25	-293	0	537	9	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
18	12	-13172	-634	-454	0	978	-138	6.28	6.28	12.57	12.57	3	0.04	0.01	0.05	0.00	0.00	24.0
19	12	-12522	494	-360	0	802	117	6.28	6.28	12.57	12.57	3	0.03	0.01	0.04	0.00	0.00	24.0
20	12	-12682	-40	-1017	0	3442	-4	6.28	6.28	12.57	12.57	3	0.12	0.02	0.10	0.00	0.00	24.0
37	12	-12892	-982	-412	0	877	-217	6.28	6.28	12.57	12.57	3	0.03	0.02	0.08	0.00	0.00	24.0
38	12	-11812	897	-255	0	585	208	6.28	6.28	12.57	12.57	3	0.02	0.02	0.07	0.00	0.00	24.0
39	12	-12082	7	-1350	0	4985	7	6.28	6.28	12.57	12.57	3	0.18	0.02	0.13	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-11165	15	-178	0	419	9	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
2	25	-8590	-24	-93	0	251	-5	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
3	25	-8618	-21	-187	0	402	-4	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
4	25	-8561	43	-87	0	243	18	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
5	25	-8589	46	-181	0	394	19	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
6	25	-8547	-3	19	0	71	2	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
7	25	-8640	5	-295	0	576	5	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
8	25	-8538	17	21	0	69	9	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
9	25	-8632	25	-293	0	574	12	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0

10	25	-8590	-24	-93	0	251	-5	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
11	25	-8618	-21	-187	0	402	-4	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
12	25	-8561	43	-87	0	243	18	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
13	25	-8589	46	-181	0	394	19	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
14	25	-8547	-3	19	0	71	2	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
15	25	-8640	5	-295	0	576	5	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
16	25	-8538	17	21	0	69	9	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
17	25	-8632	25	-293	0	574	12	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
18	25	-13075	-634	-454	0	1034	-217	6.28	6.28	12.57	12.57	3	0.04	0.01	0.05	0.00	0.00	24.0
19	25	-12425	494	-360	0	847	179	6.28	6.28	12.57	12.57	3	0.03	0.01	0.04	0.00	0.00	24.0
20	25	-12585	-40	-1017	0	3570	-9	6.28	6.28	12.57	12.57	3	0.13	0.02	0.10	0.00	0.00	24.0
37	25	-12795	-982	-412	0	929	-339	6.28	6.28	12.57	12.57	3	0.04	0.02	0.08	0.00	0.00	24.0
38	25	-11715	897	-255	0	617	320	6.28	6.28	12.57	12.57	3	0.03	0.02	0.07	0.00	0.00	24.0
39	25	-11985	7	-1350	0	5154	8	6.28	6.28	12.57	12.57	3	0.18	0.02	0.13	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-11068	15	-178	0	442	11	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
2	38	-8515	-24	-93	0	262	-8	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
3	38	-8543	-21	-187	0	426	-6	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
4	38	-8486	43	-87	0	254	24	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
5	38	-8514	46	-181	0	417	25	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
6	38	-8472	-3	19	0	69	2	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
7	38	-8565	5	-295	0	613	6	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
8	38	-8463	17	21	0	66	11	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
9	38	-8557	25	-293	0	610	15	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
10	38	-8515	-24	-93	0	262	-8	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
11	38	-8543	-21	-187	0	426	-6	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
12	38	-8486	43	-87	0	254	24	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
13	38	-8514	46	-181	0	417	25	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
14	38	-8472	-3	19	0	69	2	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
15	38	-8565	5	-295	0	613	6	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
16	38	-8463	17	21	0	66	11	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
17	38	-8557	25	-293	0	610	15	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
18	38	-12978	-634	-454	0	1091	-296	6.28	6.28	12.57	12.57	3	0.04	0.01	0.05	0.00	0.00	24.0
19	38	-12328	494	-360	0	892	240	6.28	6.28	12.57	12.57	3	0.04	0.01	0.04	0.00	0.00	24.0
20	38	-12488	-40	-1017	0	3697	-14	6.28	6.28	12.57	12.57	3	0.13	0.02	0.10	0.00	0.00	24.0
37	38	-12698	-982	-412	0	980	-462	6.28	6.28	12.57	12.57	3	0.04	0.02	0.08	0.00	0.00	24.0
38	38	-11618	897	-255	0	649	432	6.28	6.28	12.57	12.57	3	0.03	0.02	0.07	0.00	0.00	24.0
39	38	-11888	7	-1350	0	5323	9	6.28	6.28	12.57	12.57	3	0.19	0.02	0.13	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-10970	15	-178	0	464	13	6.28	6.28	12.57	12.57	3	0.02	0.00	0.02	0.00	0.00	24.0
2	50	-8440	-24	-93	0	274	-11	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
3	50	-8468	-21	-187	0	449	-9	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
4	50	-8411	43	-87	0	264	29	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
5	50	-8439	46	-181	0	440	30	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
6	50	-8397	-3	19	0	66	2	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
7	50	-8490	5	-295	0	650	6	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
8	50	-8388	17	21	0	64	13	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
9	50	-8482	25	-293	0	647	18	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
10	50	-8440	-24	-93	0	274	-11	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
11	50	-8468	-21	-187	0	449	-9	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
12	50	-8411	43	-87	0	264	29	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
13	50	-8439	46	-181	0	440	30	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
14	50	-8397	-3	19	0	66	2	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
15	50	-8490	5	-295	0	650	6	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
16	50	-8388	17	21	0	64	13	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
17	50	-8482	25	-293	0	647	18	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
18	50	-12880	-634	-454	0	1148	-375	6.28	6.28	12.57	12.57	3	0.05	0.01	0.05	0.00	0.00	24.0
19	50	-12230	494	-360	0	937	302	6.28	6.28	12.57	12.57	3	0.04	0.01	0.04	0.00	0.00	24.0
20	50	-12390	-40	-1017	0	3824	-19	6.28	6.28	12.57	12.57	3	0.14	0.02	0.10	0.00	0.00	24.0
37	50	-12600	-982	-412	0	1032	-585	6.28	6.28	12.57	12.57	3	0.05	0.02	0.08	0.00	0.00	24.0
38	50	-11520	897	-255	0	681	544	6.28	6.28	12.57	12.57	3	0.04	0.02	0.07	0.00	0.00	24.0
39	50	-11790	7	-1350	0	5492	9	6.28	6.28	12.57	12.57	3	0.20	0.02	0.13	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 114 NI 477 NF 46 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 22
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-8485	-23	19	0	-16	-17	6.28	6.28	12.57	12.57	3	0.00	0.00	0.00	0.00	0.00	24.0
2	0	-6530	-18	50	0	-89	-14	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
3	0	-6548	-15	-5	0	16	-15	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
4	0	-6505	-19	35	0	-40	-11	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
5	0	-6523	-17	-20	0	65	-12	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
6	0	-6500	-22	109	0	-195	-13	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
7	0	-6561	-13	-75	0	157	-14	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
8	0	-6493	-22	104	0	-181	-12	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
9	0	-6553	-13	-79	0	171	-13	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
10	0	-6530	-18	50	0	-89	-14	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
11	0	-6548	-15	-5	0	16	-15	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
12	0	-6505	-19	35	0	-40	-11	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
13	0	-6523	-17	-20	0	65	-12	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
14	0	-6500	-22	109	0	-195	-13	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
15	0	-6561	-13	-75	0	157	-14	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
16	0	-6493	-22	104	0	-181	-12	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
17	0	-6553	-13	-79	0	171	-13	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
18	0	-9488	-104	75	0	-137	-30	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
19	0	-9660	94	-65	0	252	-34	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
20	0	-9480	23	-198	0	2079	-35	6.28	6.28	12.57	12.57	3	0.08	0.00	0.02	0.00	0.00	24.0
37	0	-9092	-175	125	0	-289	-24	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
38	0	-9378	154	-107	0	359	-30	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
39	0	-9078	36	-329	0	3404	-31	6.28	6.28	12.57	12.57	3	0.12	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-8388	-23	19	0	-18	-20	6.28	6.28	12.57	12.57	3	0.00	0.00	0.00	0.00	0.00	24.0
2	12	-6455	-18	50	0	-95	-17	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
3	12	-6473	-15	-5	0	17	-17	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
4	12	-6430	-19	35	0	-45	-14	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
5	12	-6448	-17	-20	0	68	-14	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0

6	12	-6425	-22	109	0	-209	-16	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
7	12	-6486	-13	-75	0	166	-16	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
8	12	-6418	-22	104	0	-194	-15	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
9	12	-6478	-13	-79	0	181	-15	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
10	12	-6455	-18	50	0	-95	-17	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
11	12	-6473	-15	-5	0	17	-17	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
12	12	-6430	-19	35	0	-45	-14	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
13	12	-6448	-17	-20	0	68	-14	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
14	12	-6425	-22	109	0	-209	-16	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
15	12	-6486	-13	-75	0	166	-16	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
16	12	-6418	-22	104	0	-194	-15	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
17	12	-6478	-13	-79	0	181	-15	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
18	12	-9390	-104	75	0	-146	-43	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
19	12	-9562	94	-65	0	260	-22	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
20	12	-9382	23	-198	0	2104	-32	6.28	6.28	12.57	12.57	3	0.08	0.00	0.02	0.00	0.00	24.0
37	12	-8994	-175	125	0	-305	-46	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
38	12	-9280	154	-107	0	372	-11	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
39	12	-8980	36	-329	0	3445	-27	6.28	6.28	12.57	12.57	3	0.13	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-8290	-23	19	0	-20	-23	6.28	6.28	12.57	12.57	3	0.00	0.00	0.00	0.00	0.00	24.0
2	25	-6380	-18	50	0	-102	-19	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
3	25	-6398	-15	-5	0	18	-19	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
4	25	-6355	-19	35	0	-49	-16	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
5	25	-6373	-17	-20	0	70	-16	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
6	25	-6350	-22	109	0	-223	-18	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
7	25	-6411	-13	-75	0	175	-17	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
8	25	-6343	-22	104	0	-207	-17	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
9	25	-6403	-13	-79	0	191	-16	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
10	25	-6380	-18	50	0	-102	-19	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
11	25	-6398	-15	-5	0	18	-19	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
12	25	-6355	-19	35	0	-49	-16	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
13	25	-6373	-17	-20	0	70	-16	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
14	25	-6350	-22	109	0	-223	-18	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
15	25	-6411	-13	-75	0	175	-17	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
16	25	-6343	-22	104	0	-207	-17	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
17	25	-6403	-13	-79	0	191	-16	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
18	25	-9293	-104	75	0	-155	-56	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
19	25	-9465	94	-65	0	268	-10	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
20	25	-9285	23	-198	0	2128	-29	6.28	6.28	12.57	12.57	3	0.08	0.00	0.02	0.00	0.00	24.0
37	25	-8897	-175	125	0	-320	-67	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
38	25	-9183	154	-107	0	386	8	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
39	25	-8883	36	-329	0	3486	-22	6.28	6.28	12.57	12.57	3	0.13	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-8192	-23	19	0	-23	-25	6.28	6.28	12.57	12.57	3	0.00	0.00	0.00	0.00	0.00	24.0
2	38	-6305	-18	50	0	-108	-21	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
3	38	-6323	-15	-5	0	18	-21	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
4	38	-6280	-19	35	0	-53	-18	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
5	38	-6298	-17	-20	0	73	-18	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
6	38	-6275	-22	109	0	-236	-21	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
7	38	-6336	-13	-75	0	185	-19	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
8	38	-6268	-22	104	0	-220	-20	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
9	38	-6328	-13	-79	0	201	-18	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
10	38	-6305	-18	50	0	-108	-21	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
11	38	-6323	-15	-5	0	18	-21	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
12	38	-6280	-19	35	0	-53	-18	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
13	38	-6298	-17	-20	0	73	-18	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
14	38	-6275	-22	109	0	-236	-21	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
15	38	-6336	-13	-75	0	185	-19	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
16	38	-6268	-22	104	0	-220	-20	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
17	38	-6328	-13	-79	0	201	-18	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
18	38	-9196	-104	75	0	-165	-69	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
19	38	-9368	94	-65	0	276	1	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
20	38	-9188	23	-198	0	2153	-26	6.28	6.28	12.57	12.57	3	0.08	0.00	0.02	0.00	0.00	24.0
37	38	-8800	-175	125	0	-336	-89	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
38	38	-9086	154	-107	0	399	27	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
39	38	-8786	36	-329	0	3528	-18	6.28	6.28	12.57	12.57	3	0.13	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-8095	-23	19	0	-25	-28	6.28	6.28	12.57	12.57	3	0.00	0.00	0.00	0.00	0.00	24.0
2	50	-6230	-18	50	0	-114	-23	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
3	50	-6248	-15	-5	0	19	-22	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
4	50	-6205	-19	35	0	-58	-21	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
5	50	-6223	-17	-20	0	75	-20	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
6	50	-6200	-22	109	0	-250	-24	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
7	50	-6261	-13	-75	0	194	-20	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
8	50	-6193	-22	104	0	-233	-23	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
9	50	-6253	-13	-79	0	211	-20	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
10	50	-6230	-18	50	0	-114	-23	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
11	50	-6248	-15	-5	0	19	-22	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
12	50	-6205	-19	35	0	-58	-21	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
13	50	-6223	-17	-20	0	75	-20	6.28	6.28	12.57	12.57	2	0.00	0.00	0.00	0.00	0.00	24.0
14	50	-6200	-22	109	0	-250	-24	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
15	50	-6261	-13	-75	0	194	-20	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
16	50	-6193	-22	104	0	-233	-23	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
17	50	-6253	-13	-79	0	211	-20	6.28	6.28	12.57	12.57	2	0.01	0.00	0.01	0.00	0.00	24.0
18	50	-9098	-104	75	0	-174	-82	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
19	50	-9270	94	-65	0	284	13	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
20	50	-9090	23	-198	0	2178	-23	6.28	6.28	12.57	12.57	3	0.08	0.00	0.02	0.00	0.00	24.0
37	50	-8702	-175	125	0	-352	-111	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
38	50	-8988	154	-107	0	413	47	6.28	6.28	12.57	12.57	3	0.02	0.00	0.01	0.00	0.00	24.0
39	50	-8688	36	-329	0	3569	-14	6.28	6.28	12.57	12.57	3	0.13	0.01	0.03	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 115 NI 46 NF 42 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 22A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	--												Fx,M	Bielle	V,Mx			
	cm		daN			daN*m				cmq						cmq/m		cm
1	0	-12710	-442	35	0	-28	-28	6.28	6.28	12.57	12.57	3	0.00	0.01	0.04	0.00	0.00	24.0

2	0	-9781	-368	89	0	-116	-23	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
3	0	-9807	-360	-10	0	18	-22	6.28	6.28	12.57	12.57	2	0.00	0.01	0.03	0.00	0.00	24.0
4	0	-9748	-320	63	0	-62	-21	6.28	6.28	12.57	12.57	2	0.00	0.01	0.03	0.00	0.00	24.0
5	0	-9775	-311	-36	0	72	-20	6.28	6.28	12.57	12.57	2	0.00	0.01	0.03	0.00	0.00	24.0
6	0	-9738	-361	196	0	-253	-24	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
7	0	-9827	-333	-134	0	193	-20	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
8	0	-9729	-346	188	0	-237	-23	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
9	0	-9817	-319	-142	0	209	-20	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
10	0	-9781	-368	89	0	-116	-23	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
11	0	-9807	-360	-10	0	18	-22	6.28	6.28	12.57	12.57	2	0.00	0.01	0.03	0.00	0.00	24.0
12	0	-9748	-320	63	0	-62	-21	6.28	6.28	12.57	12.57	2	0.00	0.01	0.03	0.00	0.00	24.0
13	0	-9775	-311	-36	0	72	-20	6.28	6.28	12.57	12.57	2	0.00	0.01	0.03	0.00	0.00	24.0
14	0	-9738	-361	196	0	-253	-24	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
15	0	-9827	-333	-134	0	193	-20	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
16	0	-9729	-346	188	0	-237	-23	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
17	0	-9817	-319	-142	0	209	-20	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
18	0	-14260	-1116	134	0	-176	-82	6.28	6.28	12.57	12.57	3	0.01	0.02	0.09	0.00	0.00	24.0
19	0	-14580	-99	-115	0	268	13	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
20	0	-14250	-497	-330	0	1954	-23	6.28	6.28	12.57	12.57	3	0.07	0.01	0.04	0.00	0.00	24.0
37	0	-13630	-1399	224	0	-347	-111	6.28	6.28	12.57	12.57	3	0.01	0.03	0.11	0.00	0.00	24.0
38	0	-14150	295	-190	0	394	47	6.28	6.28	12.57	12.57	3	0.01	0.01	0.02	0.00	0.00	24.0
39	0	-13610	-369	-548	0	3204	-14	6.28	6.28	12.57	12.57	3	0.11	0.01	0.05	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-12612	-442	35	0	-33	-83	6.28	6.28	12.57	12.57	3	0.00	0.01	0.04	0.00	0.00	24.0
2	12	-9706	-368	89	0	-127	-69	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
3	12	-9732	-360	-10	0	19	-67	6.28	6.28	12.57	12.57	2	0.00	0.01	0.03	0.00	0.00	24.0
4	12	-9673	-320	63	0	-70	-61	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
5	12	-9700	-311	-36	0	77	-59	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
6	12	-9663	-361	196	0	-277	-69	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
7	12	-9752	-333	-134	0	210	-62	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
8	12	-9654	-346	188	0	-260	-66	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
9	12	-9742	-319	-142	0	227	-59	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
10	12	-9706	-368	89	0	-127	-69	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
11	12	-9732	-360	-10	0	19	-67	6.28	6.28	12.57	12.57	2	0.00	0.01	0.03	0.00	0.00	24.0
12	12	-9673	-320	63	0	-70	-61	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
13	12	-9700	-311	-36	0	77	-59	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
14	12	-9663	-361	196	0	-277	-69	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
15	12	-9752	-333	-134	0	210	-62	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
16	12	-9654	-346	188	0	-260	-66	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
17	12	-9742	-319	-142	0	227	-59	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
18	12	-14162	-1116	134	0	-192	-221	6.28	6.28	12.57	12.57	3	0.01	0.02	0.10	0.00	0.00	24.0
19	12	-14482	-99	-115	0	283	1	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
20	12	-14152	-497	-330	0	1995	-85	6.28	6.28	12.57	12.57	3	0.07	0.01	0.04	0.00	0.00	24.0
37	12	-13532	-1399	224	0	-375	-286	6.28	6.28	12.57	12.57	3	0.02	0.03	0.11	0.00	0.00	24.0
38	12	-14052	295	-190	0	417	84	6.28	6.28	12.57	12.57	3	0.02	0.01	0.02	0.00	0.00	24.0
39	12	-13512	-369	-548	0	3273	-60	6.28	6.28	12.57	12.57	3	0.12	0.01	0.05	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-12515	-442	35	0	-37	-139	6.28	6.28	12.57	12.57	3	0.01	0.01	0.04	0.00	0.00	24.0
2	25	-9631	-368	89	0	-138	-115	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
3	25	-9657	-360	-10	0	21	-112	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
4	25	-9598	-320	63	0	-77	-101	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
5	25	-9625	-311	-36	0	81	-98	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
6	25	-9588	-361	196	0	-302	-114	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
7	25	-9677	-333	-134	0	227	-104	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
8	25	-9579	-346	188	0	-284	-109	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
9	25	-9667	-319	-142	0	245	-99	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
10	25	-9631	-368	89	0	-138	-115	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
11	25	-9657	-360	-10	0	21	-112	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
12	25	-9598	-320	63	0	-77	-101	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
13	25	-9625	-311	-36	0	81	-98	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
14	25	-9588	-361	196	0	-302	-114	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
15	25	-9677	-333	-134	0	227	-104	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
16	25	-9579	-346	188	0	-284	-109	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
17	25	-9667	-319	-142	0	245	-99	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
18	25	-14065	-1116	134	0	-209	-361	6.28	6.28	12.57	12.57	3	0.02	0.02	0.10	0.00	0.00	24.0
19	25	-14385	-99	-115	0	297	-12	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
20	25	-14055	-497	-330	0	2037	-147	6.28	6.28	12.57	12.57	3	0.07	0.01	0.04	0.00	0.00	24.0
37	25	-13435	-1399	224	0	-403	-461	6.28	6.28	12.57	12.57	3	0.03	0.03	0.13	0.00	0.00	24.0
38	25	-13955	295	-190	0	441	120	6.28	6.28	12.57	12.57	3	0.02	0.01	0.02	0.00	0.00	24.0
39	25	-13415	-369	-548	0	3341	-106	6.28	6.28	12.57	12.57	3	0.12	0.01	0.05	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-12418	-442	35	0	-41	-194	6.28	6.28	12.57	12.57	3	0.01	0.01	0.04	0.00	0.00	24.0
2	38	-9556	-368	89	0	-149	-161	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
3	38	-9582	-360	-10	0	22	-157	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
4	38	-9523	-320	63	0	-85	-141	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
5	38	-9550	-311	-36	0	86	-137	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
6	38	-9513	-361	196	0	-326	-159	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
7	38	-9602	-333	-134	0	244	-145	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
8	38	-9504	-346	188	0	-307	-153	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
9	38	-9592	-319	-142	0	263	-139	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
10	38	-9556	-368	89	0	-149	-161	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
11	38	-9582	-360	-10	0	22	-157	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
12	38	-9523	-320	63	0	-85	-141	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
13	38	-9550	-311	-36	0	86	-137	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
14	38	-9513	-361	196	0	-326	-159	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
15	38	-9602	-333	-134	0	244	-145	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
16	38	-9504	-346	188	0	-307	-153	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
17	38	-9592	-319	-142	0	263	-139	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
18	38	-13968	-1116	134	0	-226	-500	6.28	6.28	12.57	12.57	3	0.03	0.02	0.10	0.00	0.00	24.0
19	38	-14288	-99	-115	0	311	-24	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
20	38	-13958	-497	-330	0	2078	-210	6.28	6.28	12.57	12.57	3	0.08	0.01	0.04	0.00	0.00	24.0
37	38	-13338	-1399	224	0	-431	-636	6.28	6.28	12.57	12.57	3	0.04	0.03	0.13	0.00	0.00	24.0
38	38	-13858	295	-190	0	465	157	6.28	6.28	12.57	12.57	3	0.02	0.01	0.02	0.00	0.00	24.0
39	38	-13318	-369	-548	0	3410	-152	6.28	6.28	12.57	12.57	3	0.12	0.01	0.05	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-12320	-442	35	0	-46	-249	6.28	6.28	12.57	12.57	3	0.01	0.01	0.04	0.00	0.00	24.0
2	50	-9481	-368	89	0	-160	-207	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
3	50	-9507	-360	-10	0	23	-202	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
4	50	-9448	-320	63	0	-93	-181	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
5	50	-9475	-311	-36	0	90	-176	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
6	50	-9438	-361	196	0	-351	-204	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
7	50	-9527	-333	-134	0	260	-187	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0

8	50	-9429	-346	188	0	-331	-196	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
9	50	-9517	-319	-142	0	280	-179	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
10	50	-9481	-368	89	0	-160	-207	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
11	50	-9507	-360	-10	0	23	-202	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
12	50	-9448	-320	63	0	-93	-181	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
13	50	-9475	-311	-36	0	90	-176	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
14	50	-9438	-361	196	0	-351	-204	6.28	6.28	12.57	12.57	2	0.03	0.01	0.03	0.00	0.00	24.0
15	50	-9527	-333	-134	0	260	-187	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
16	50	-9429	-346	188	0	-331	-196	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
17	50	-9517	-319	-142	0	280	-179	6.28	6.28	12.57	12.57	2	0.02	0.01	0.03	0.00	0.00	24.0
18	50	-13870	-1116	134	0	-243	-640	6.28	6.28	12.57	12.57	3	0.04	0.02	0.10	0.00	0.00	24.0
19	50	-14190	-99	-115	0	326	-37	6.28	6.28	12.57	12.57	3	0.01	0.00	0.01	0.00	0.00	24.0
20	50	-13860	-497	-330	0	2119	-272	6.28	6.28	12.57	12.57	3	0.08	0.01	0.04	0.00	0.00	24.0
37	50	-13240	-1399	224	0	-459	-811	6.28	6.28	12.57	12.57	3	0.05	0.03	0.13	0.00	0.00	24.0
38	50	-13760	295	-190	0	489	194	6.28	6.28	12.57	12.57	3	0.02	0.01	0.02	0.00	0.00	24.0
39	50	-13220	-369	-548	0	3478	-198	6.28	6.28	12.57	12.57	3	0.12	0.01	0.05	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 116 NI 216 NF 482 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 32
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-3621	-839	141	0	148	455	6.28	6.28	12.57	12.57	3	0.03	0.02	0.09	0.00	0.00	24.0
2	0	-2748	-726	234	0	135	405	6.28	6.28	12.57	12.57	2	0.03	0.01	0.08	0.00	0.00	24.0
3	0	-2846	-699	76	0	130	395	6.28	6.28	12.57	12.57	2	0.03	0.01	0.07	0.00	0.00	24.0
4	0	-2725	-591	141	0	98	305	6.28	6.28	12.57	12.57	2	0.02	0.01	0.06	0.00	0.00	24.0
5	0	-2822	-565	-16	0	92	295	6.28	6.28	12.57	12.57	2	0.02	0.01	0.06	0.00	0.00	24.0
6	0	-2626	-709	385	0	128	383	6.28	6.28	12.57	12.57	2	0.03	0.01	0.07	0.00	0.00	24.0
7	0	-2951	-621	-139	0	110	347	6.28	6.28	12.57	12.57	2	0.03	0.01	0.06	0.00	0.00	24.0
8	0	-2619	-669	357	0	117	353	6.28	6.28	12.57	12.57	2	0.03	0.01	0.07	0.00	0.00	24.0
9	0	-2944	-581	-167	0	99	317	6.28	6.28	12.57	12.57	2	0.02	0.01	0.06	0.00	0.00	24.0
10	0	-2748	-726	234	0	135	405	6.28	6.28	12.57	12.57	2	0.03	0.01	0.08	0.00	0.00	24.0
11	0	-2846	-699	76	0	130	395	6.28	6.28	12.57	12.57	2	0.03	0.01	0.07	0.00	0.00	24.0
12	0	-2725	-591	141	0	98	305	6.28	6.28	12.57	12.57	2	0.02	0.01	0.06	0.00	0.00	24.0
13	0	-2822	-565	-16	0	92	295	6.28	6.28	12.57	12.57	2	0.02	0.01	0.06	0.00	0.00	24.0
14	0	-2626	-709	385	0	128	383	6.28	6.28	12.57	12.57	2	0.03	0.01	0.07	0.00	0.00	24.0
15	0	-2951	-621	-139	0	110	347	6.28	6.28	12.57	12.57	2	0.03	0.01	0.06	0.00	0.00	24.0
16	0	-2619	-669	357	0	117	353	6.28	6.28	12.57	12.57	2	0.03	0.01	0.07	0.00	0.00	24.0
17	0	-2944	-581	-167	0	99	317	6.28	6.28	12.57	12.57	2	0.02	0.01	0.06	0.00	0.00	24.0
18	0	-3425	-1826	817	0	273	1115	6.28	6.28	12.57	12.57	3	0.07	0.03	0.19	0.00	0.00	24.0
19	0	-3612	-881	214	0	96	604	6.28	6.28	12.57	12.57	3	0.04	0.02	0.09	0.00	0.00	24.0
20	0	-3172	-764	-1027	0	-557	652	6.28	6.28	12.57	12.57	3	0.04	0.02	0.11	0.00	0.00	24.0
37	0	-3404	-1973	893	0	320	1153	6.28	6.28	12.57	12.57	3	0.07	0.04	0.20	0.00	0.00	24.0
38	0	-3716	-398	-111	0	24	301	6.28	6.28	12.57	12.57	3	0.02	0.01	0.04	0.00	0.00	24.0
39	0	-2983	-202	-2180	0	-1063	382	6.28	6.28	12.57	12.57	3	0.05	0.04	0.24	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-3524	-839	141	0	130	350	6.28	6.28	12.57	12.57	3	0.02	0.02	0.09	0.00	0.00	24.0
2	12	-2673	-726	234	0	106	315	6.28	6.28	12.57	12.57	2	0.02	0.01	0.08	0.00	0.00	24.0
3	12	-2771	-699	76	0	120	307	6.28	6.28	12.57	12.57	2	0.02	0.01	0.07	0.00	0.00	24.0
4	12	-2650	-591	141	0	80	231	6.28	6.28	12.57	12.57	2	0.02	0.01	0.06	0.00	0.00	24.0
5	12	-2747	-565	-16	0	94	224	6.28	6.28	12.57	12.57	2	0.02	0.01	0.06	0.00	0.00	24.0
6	12	-2551	-709	385	0	80	294	6.28	6.28	12.57	12.57	2	0.02	0.01	0.07	0.00	0.00	24.0
7	12	-2876	-621	-139	0	128	270	6.28	6.28	12.57	12.57	2	0.02	0.01	0.06	0.00	0.00	24.0
8	12	-2544	-669	357	0	72	269	6.28	6.28	12.57	12.57	2	0.02	0.01	0.07	0.00	0.00	24.0
9	12	-2869	-581	-167	0	120	245	6.28	6.28	12.57	12.57	2	0.02	0.01	0.06	0.00	0.00	24.0
10	12	-2673	-726	234	0	106	315	6.28	6.28	12.57	12.57	2	0.02	0.01	0.08	0.00	0.00	24.0
11	12	-2771	-699	76	0	120	307	6.28	6.28	12.57	12.57	2	0.02	0.01	0.07	0.00	0.00	24.0
12	12	-2650	-591	141	0	80	231	6.28	6.28	12.57	12.57	2	0.02	0.01	0.06	0.00	0.00	24.0
13	12	-2747	-565	-16	0	94	224	6.28	6.28	12.57	12.57	2	0.02	0.01	0.06	0.00	0.00	24.0
14	12	-2551	-709	385	0	80	294	6.28	6.28	12.57	12.57	2	0.02	0.01	0.07	0.00	0.00	24.0
15	12	-2876	-621	-139	0	128	270	6.28	6.28	12.57	12.57	2	0.02	0.01	0.06	0.00	0.00	24.0
16	12	-2544	-669	357	0	72	269	6.28	6.28	12.57	12.57	2	0.02	0.01	0.07	0.00	0.00	24.0
17	12	-2869	-581	-167	0	120	245	6.28	6.28	12.57	12.57	2	0.02	0.01	0.06	0.00	0.00	24.0
18	12	-3328	-1826	817	0	171	887	6.28	6.28	12.57	12.57	3	0.05	0.03	0.19	0.00	0.00	24.0
19	12	-3514	-881	214	0	69	494	6.28	6.28	12.57	12.57	3	0.03	0.02	0.09	0.00	0.00	24.0
20	12	-3074	-764	-1027	0	-429	557	6.28	6.28	12.57	12.57	3	0.04	0.02	0.11	0.00	0.00	24.0
37	12	-3306	-1973	893	0	208	906	6.28	6.28	12.57	12.57	3	0.05	0.04	0.20	0.00	0.00	24.0
38	12	-3618	-398	-111	0	38	252	6.28	6.28	12.57	12.57	3	0.02	0.01	0.04	0.00	0.00	24.0
39	12	-2886	-202	-2180	0	-791	357	6.28	6.28	12.57	12.57	3	0.04	0.04	0.24	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-3426	-839	141	0	112	245	6.28	6.28	12.57	12.57	3	0.01	0.02	0.09	0.00	0.00	24.0
2	25	-2598	-726	234	0	76	224	6.28	6.28	12.57	12.57	2	0.02	0.01	0.08	0.00	0.00	24.0
3	25	-2696	-699	76	0	111	220	6.28	6.28	12.57	12.57	2	0.02	0.01	0.07	0.00	0.00	24.0
4	25	-2575	-591	141	0	62	158	6.28	6.28	12.57	12.57	2	0.01	0.01	0.06	0.00	0.00	24.0
5	25	-2672	-565	-16	0	96	154	6.28	6.28	12.57	12.57	2	0.01	0.01	0.06	0.00	0.00	24.0
6	25	-2476	-709	385	0	32	205	6.28	6.28	12.57	12.57	2	0.01	0.01	0.07	0.00	0.00	24.0
7	25	-2801	-621	-139	0	145	192	6.28	6.28	12.57	12.57	2	0.02	0.01	0.06	0.00	0.00	24.0
8	25	-2469	-669	357	0	27	185	6.28	6.28	12.57	12.57	2	0.01	0.01	0.07	0.00	0.00	24.0
9	25	-2794	-581	-167	0	141	172	6.28	6.28	12.57	12.57	2	0.02	0.01	0.06	0.00	0.00	24.0
10	25	-2598	-726	234	0	76	224	6.28	6.28	12.57	12.57	2	0.02	0.01	0.08	0.00	0.00	24.0
11	25	-2696	-699	76	0	111	220	6.28	6.28	12.57	12.57	2	0.02	0.01	0.07	0.00	0.00	24.0
12	25	-2575	-591	141	0	62	158	6.28	6.28	12.57	12.57	2	0.01	0.01	0.06	0.00	0.00	24.0
13	25	-2672	-565	-16	0	96	154	6.28	6.28	12.57	12.57	2	0.01	0.01	0.06	0.00	0.00	24.0
14	25	-2476	-709	385	0	32	205	6.28	6.28	12.57	12.57	2	0.01	0.01	0.07	0.00	0.00	24.0
15	25	-2801	-621	-139	0	145	192	6.28	6.28	12.57	12.57	2	0.02	0.01	0.06	0.00	0.00	24.0
16	25	-2469	-669	357	0	27	185	6.28	6.28	12.57	12.57	2	0.01	0.01	0.07	0.00	0.00	24.0
17	25	-2794	-581	-167	0	141	172	6.28	6.28	12.57	12.57	2	0.02	0.01	0.06	0.00	0.00	24.0
18	25	-3230	-1826	817	0	69	658	6.28	6.28	12.57	12.57	3	0.04	0.03	0.19	0.00	0.00	24.0
19	25	-3417	-881	214	0	42	384	6.28	6.28	12.57	12.57	3	0.02	0.02	0.09	0.00	0.00	24.0
20	25	-2977	-764	-1027	0	-300	461	6.28	6.28	12.57	12.57	3	0.03	0.02	0.11	0.00	0.00	24.0
37	25	-3209	-1973	893	0	97	660	6.28	6.28	12.57	12.57	3	0.04	0.04	0.20	0.00	0.00	24.0
38	25	-3521	-398	-111	0	52	202	6.28	6.28	12.57	12.57	3	0.01	0.01	0.04	0.00	0.00	24.0
39	25	-2788	-202	-2180	0	-518	332	6.28	6.28	12.57	12.57	3	0.03	0.04	0.24	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-3328	-839	141	0	95	140	6.28	6.28	12.57	12.57	3	0.01	0.02	0.09	0.00	0.00	24.0
2	38	-2523	-726	234	0	47	133	6.28	6.28	12.57	12.57	2	0.01	0.01	0.08	0.00	0.00	24.0
3	38	-2621	-699	76	0	101	133	6.28	6.28	12.57	12.57	2	0.01	0.01	0.07	0.00	0.00	24.0

4	38	-2500	-591	141	0	45	84	6.28	6.28	12.57	12.57	2	0.01	0.01	0.06	0.00	0.00	24.0
5	38	-2597	-565	-16	0	98	83	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
6	38	-2401	-709	385	0	-16	117	6.28	6.28	12.57	12.57	2	0.01	0.01	0.07	0.00	0.00	24.0
7	38	-2726	-621	-139	0	163	114	6.28	6.28	12.57	12.57	2	0.01	0.01	0.06	0.00	0.00	24.0
8	38	-2394	-669	357	0	-17	102	6.28	6.28	12.57	12.57	2	0.01	0.01	0.07	0.00	0.00	24.0
9	38	-2719	-581	-167	0	162	99	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
10	38	-2523	-726	234	0	47	133	6.28	6.28	12.57	12.57	2	0.01	0.01	0.08	0.00	0.00	24.0
11	38	-2621	-699	76	0	101	133	6.28	6.28	12.57	12.57	2	0.01	0.01	0.07	0.00	0.00	24.0
12	38	-2500	-591	141	0	45	84	6.28	6.28	12.57	12.57	2	0.01	0.01	0.06	0.00	0.00	24.0
13	38	-2597	-565	-16	0	98	83	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
14	38	-2401	-709	385	0	-16	117	6.28	6.28	12.57	12.57	2	0.01	0.01	0.07	0.00	0.00	24.0
15	38	-2726	-621	-139	0	163	114	6.28	6.28	12.57	12.57	2	0.01	0.01	0.06	0.00	0.00	24.0
16	38	-2394	-669	357	0	-17	102	6.28	6.28	12.57	12.57	2	0.01	0.01	0.07	0.00	0.00	24.0
17	38	-2719	-581	-167	0	162	99	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
18	38	-3132	-1826	817	0	-33	430	6.28	6.28	12.57	12.57	3	0.03	0.03	0.19	0.00	0.00	24.0
19	38	-3320	-881	214	0	15	274	6.28	6.28	12.57	12.57	3	0.02	0.02	0.09	0.00	0.00	24.0
20	38	-2880	-764	-1027	0	-172	366	6.28	6.28	12.57	12.57	3	0.02	0.02	0.11	0.00	0.00	24.0
37	38	-3112	-1973	893	0	-15	413	6.28	6.28	12.57	12.57	3	0.02	0.04	0.20	0.00	0.00	24.0
38	38	-3424	-398	-111	0	66	152	6.28	6.28	12.57	12.57	3	0.01	0.01	0.04	0.00	0.00	24.0
39	38	-2690	-202	-2180	0	-246	306	6.28	6.28	12.57	12.57	3	0.02	0.04	0.24	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-3231	-839	141	0	77	36	6.28	6.28	12.57	12.57	3	0.00	0.02	0.08	0.00	0.00	24.0
2	50	-2448	-726	234	0	18	43	6.28	6.28	12.57	12.57	2	0.00	0.01	0.08	0.00	0.00	24.0
3	50	-2546	-699	76	0	91	45	6.28	6.28	12.57	12.57	2	0.01	0.01	0.06	0.00	0.00	24.0
4	50	-2425	-591	141	0	27	10	6.28	6.28	12.57	12.57	2	0.00	0.01	0.05	0.00	0.00	24.0
5	50	-2522	-565	-16	0	100	12	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
6	50	-2326	-709	385	0	-64	28	6.28	6.28	12.57	12.57	2	0.00	0.01	0.07	0.00	0.00	24.0
7	50	-2651	-621	-139	0	180	37	6.28	6.28	12.57	12.57	2	0.01	0.01	0.06	0.00	0.00	24.0
8	50	-2319	-669	357	0	-62	18	6.28	6.28	12.57	12.57	2	0.00	0.01	0.06	0.00	0.00	24.0
9	50	-2644	-581	-167	0	183	27	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
10	50	-2448	-726	234	0	18	43	6.28	6.28	12.57	12.57	2	0.00	0.01	0.08	0.00	0.00	24.0
11	50	-2546	-699	76	0	91	45	6.28	6.28	12.57	12.57	2	0.01	0.01	0.06	0.00	0.00	24.0
12	50	-2425	-591	141	0	27	10	6.28	6.28	12.57	12.57	2	0.00	0.01	0.05	0.00	0.00	24.0
13	50	-2522	-565	-16	0	100	12	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
14	50	-2326	-709	385	0	-64	28	6.28	6.28	12.57	12.57	2	0.00	0.01	0.07	0.00	0.00	24.0
15	50	-2651	-621	-139	0	180	37	6.28	6.28	12.57	12.57	2	0.01	0.01	0.06	0.00	0.00	24.0
16	50	-2319	-669	357	0	-62	18	6.28	6.28	12.57	12.57	2	0.00	0.01	0.06	0.00	0.00	24.0
17	50	-2644	-581	-167	0	183	27	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
18	50	-3035	-1826	817	0	-135	202	6.28	6.28	12.57	12.57	3	0.01	0.03	0.19	0.00	0.00	24.0
19	50	-3222	-881	214	0	-12	163	6.28	6.28	12.57	12.57	3	0.01	0.02	0.09	0.00	0.00	24.0
20	50	-2782	-764	-1027	0	-44	270	6.28	6.28	12.57	12.57	3	0.02	0.02	0.11	0.00	0.00	24.0
37	50	-3014	-1973	893	0	-127	166	6.28	6.28	12.57	12.57	3	0.01	0.04	0.20	0.00	0.00	24.0
38	50	-3326	-398	-111	0	80	103	6.28	6.28	12.57	12.57	3	0.01	0.01	0.04	0.00	0.00	24.0
39	50	-2593	-202	-2180	0	27	281	6.28	6.28	12.57	12.57	3	0.02	0.04	0.24	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 117 NI 482 NF 33 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 32A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-5267	292	159	0	155	-176	6.28	6.28	12.57	12.57	3	0.01	0.01	0.03	0.00	0.00	24.0
2	0	-4096	272	216	0	73	-141	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
3	0	-4193	283	41	0	167	-140	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
4	0	-3909	165	204	0	72	-131	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
5	0	-4006	176	28	0	166	-130	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
6	0	-3917	222	417	0	-38	-139	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
7	0	-4241	258	-168	0	277	-135	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
8	0	-3861	190	413	0	-38	-136	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
9	0	-4185	226	-172	0	277	-132	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
10	0	-4096	272	216	0	73	-141	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
11	0	-4193	283	41	0	167	-140	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
12	0	-3909	165	204	0	72	-131	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
13	0	-4006	176	28	0	166	-130	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
14	0	-3917	222	417	0	-38	-139	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
15	0	-4241	258	-168	0	277	-135	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
16	0	-3861	190	413	0	-38	-136	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
17	0	-4185	226	-172	0	277	-132	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
18	0	-6015	719	474	0	31	-314	6.28	6.28	12.57	12.57	3	0.02	0.01	0.07	0.00	0.00	24.0
19	0	-5718	720	297	0	113	-110	6.28	6.28	12.57	12.57	3	0.01	0.01	0.06	0.00	0.00	24.0
20	0	-5582	773	-31	0	427	-160	6.28	6.28	12.57	12.57	3	0.02	0.01	0.07	0.00	0.00	24.0
37	0	-5930	580	458	0	33	-370	6.28	6.28	12.57	12.57	3	0.02	0.01	0.06	0.00	0.00	24.0
38	0	-5435	581	162	0	168	-31	6.28	6.28	12.57	12.57	3	0.01	0.01	0.05	0.00	0.00	24.0
39	0	-5209	669	-384	0	693	-114	6.28	6.28	12.57	12.57	3	0.03	0.01	0.06	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-5170	292	159	0	135	-140	6.28	6.28	12.57	12.57	3	0.01	0.01	0.03	0.00	0.00	24.0
2	12	-4021	272	216	0	46	-107	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
3	12	-4118	283	41	0	162	-104	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
4	12	-3834	165	204	0	46	-110	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
5	12	-3931	176	28	0	162	-108	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
6	12	-3842	222	417	0	-90	-111	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
7	12	-4166	258	-168	0	298	-103	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
8	12	-3786	190	413	0	-90	-112	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
9	12	-4110	226	-172	0	298	-104	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
10	12	-4021	272	216	0	46	-107	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
11	12	-4118	283	41	0	162	-104	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
12	12	-3834	165	204	0	46	-110	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
13	12	-3931	176	28	0	162	-108	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
14	12	-3842	222	417	0	-90	-111	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
15	12	-4166	258	-168	0	298	-103	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
16	12	-3786	190	413	0	-90	-112	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
17	12	-4110	226	-172	0	298	-104	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
18	12	-5918	719	474	0	-28	-224	6.28	6.28	12.57	12.57	3	0.01	0.01	0.07	0.00	0.00	24.0
19	12	-5620	720	297	0	76	-20	6.28	6.28	12.57	12.57	3	0.00	0.01	0.06	0.00	0.00	24.0
20	12	-5484	773	-31	0	431	-64	6.28	6.28	12.57	12.57	3	0.02	0.01	0.07	0.00	0.00	24.0
37	12	-5832	580	458	0	-24	-298	6.28	6.28	12.57	12.57	3	0.02	0.01	0.06	0.00	0.00	24.0
38	12	-5338	581	162	0	148	42	6.28	6.28	12.57	12.57	3	0.01	0.01	0.05	0.00	0.00	24.0
39	12	-5112	669	-384	0	741	-30	6.28	6.28	12.57	12.57	3	0.03	0.01	0.06	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-5072	292	159	0	115	-103	6.28	6.28	12.57	12.57	3	0.01	0.01	0.03	0.00	0.00	24.0
2	25	-3946	272	216	0	19	-73	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
3	25	-4043	283	41	0	157	-69	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
4	25	-3759	165	204	0	21	-90	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
5	25	-3856	176	28	0	159	-86	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
6	25	-3767	222	417	0	-142	-83	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
7	25	-4091	258	-168	0	319	-70	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
8	25	-3711	190	413	0	-141	-88	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
9	25	-4035	226	-172	0	320	-75	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
10	25	-3946	272	216	0	19	-73	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
11	25	-4043	283	41	0	157	-69	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
12	25	-3759	165	204	0	21	-90	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
13	25	-3856	176	28	0	159	-86	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
14	25	-3767	222	417	0	-142	-83	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
15	25	-4091	258	-168	0	319	-70	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
16	25	-3711	190	413	0	-141	-88	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
17	25	-4035	226	-172	0	320	-75	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
18	25	-5820	719	474	0	-87	-134	6.28	6.28	12.57	12.57	3	0.01	0.01	0.07	0.00	0.00	24.0
19	25	-5523	720	297	0	39	70	6.28	6.28	12.57	12.57	3	0.00	0.01	0.07	0.00	0.00	24.0
20	25	-5387	773	-31	0	435	33	6.28	6.28	12.57	12.57	3	0.02	0.01	0.07	0.00	0.00	24.0
37	25	-5735	580	458	0	-82	-225	6.28	6.28	12.57	12.57	3	0.01	0.01	0.06	0.00	0.00	24.0
38	25	-5240	581	162	0	128	115	6.28	6.28	12.57	12.57	3	0.01	0.01	0.05	0.00	0.00	24.0
39	25	-5014	669	-384	0	789	54	6.28	6.28	12.57	12.57	3	0.03	0.01	0.06	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-4974	292	159	0	96	-67	6.28	6.28	12.57	12.57	3	0.01	0.01	0.03	0.00	0.00	24.0
2	38	-3871	272	216	0	-8	-39	6.28	6.28	12.57	12.57	2	0.00	0.01	0.03	0.00	0.00	24.0
3	38	-3968	283	41	0	152	-34	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
4	38	-3684	165	204	0	-5	-69	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
5	38	-3781	176	28	0	156	-64	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
6	38	-3692	222	417	0	-194	-56	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
7	38	-4016	258	-168	0	340	-38	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
8	38	-3636	190	413	0	-193	-65	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
9	38	-3960	226	-172	0	341	-47	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
10	38	-3871	272	216	0	-8	-39	6.28	6.28	12.57	12.57	2	0.00	0.01	0.03	0.00	0.00	24.0
11	38	-3968	283	41	0	152	-34	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
12	38	-3684	165	204	0	-5	-69	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
13	38	-3781	176	28	0	156	-64	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
14	38	-3692	222	417	0	-194	-56	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
15	38	-4016	258	-168	0	340	-38	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
16	38	-3636	190	413	0	-193	-65	6.28	6.28	12.57	12.57	2	0.01	0.01	0.04	0.00	0.00	24.0
17	38	-3960	226	-172	0	341	-47	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
18	38	-5722	719	474	0	-146	-44	6.28	6.28	12.57	12.57	3	0.01	0.01	0.06	0.00	0.00	24.0
19	38	-5426	720	297	0	1	160	6.28	6.28	12.57	12.57	3	0.01	0.01	0.07	0.00	0.00	24.0
20	38	-5290	773	-31	0	439	130	6.28	6.28	12.57	12.57	3	0.02	0.01	0.07	0.00	0.00	24.0
37	38	-5638	580	458	0	-139	-153	6.28	6.28	12.57	12.57	3	0.01	0.01	0.06	0.00	0.00	24.0
38	38	-5142	581	162	0	108	187	6.28	6.28	12.57	12.57	3	0.01	0.01	0.06	0.00	0.00	24.0
39	38	-4916	669	-384	0	837	137	6.28	6.28	12.57	12.57	3	0.03	0.01	0.06	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-4877	292	159	0	76	-30	6.28	6.28	12.57	12.57	3	0.00	0.01	0.03	0.00	0.00	24.0
2	50	-3796	272	216	0	-35	-5	6.28	6.28	12.57	12.57	2	0.00	0.01	0.02	0.00	0.00	24.0
3	50	-3893	283	41	0	147	2	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
4	50	-3609	165	204	0	-30	-48	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
5	50	-3706	176	28	0	152	-42	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
6	50	-3617	222	417	0	-246	-28	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
7	50	-3941	258	-168	0	361	-6	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
8	50	-3561	190	413	0	-244	-41	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
9	50	-3885	226	-172	0	363	-19	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
10	50	-3796	272	216	0	-35	-5	6.28	6.28	12.57	12.57	2	0.00	0.01	0.02	0.00	0.00	24.0
11	50	-3893	283	41	0	147	2	6.28	6.28	12.57	12.57	2	0.01	0.01	0.03	0.00	0.00	24.0
12	50	-3609	165	204	0	-30	-48	6.28	6.28	12.57	12.57	2	0.00	0.00	0.02	0.00	0.00	24.0
13	50	-3706	176	28	0	152	-42	6.28	6.28	12.57	12.57	2	0.01	0.00	0.02	0.00	0.00	24.0
14	50	-3617	222	417	0	-246	-28	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
15	50	-3941	258	-168	0	361	-6	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
16	50	-3561	190	413	0	-244	-41	6.28	6.28	12.57	12.57	2	0.01	0.01	0.05	0.00	0.00	24.0
17	50	-3885	226	-172	0	363	-19	6.28	6.28	12.57	12.57	2	0.02	0.00	0.02	0.00	0.00	24.0
18	50	-5625	719	474	0	-206	46	6.28	6.28	12.57	12.57	3	0.01	0.01	0.06	0.00	0.00	24.0
19	50	-5328	720	297	0	-36	250	6.28	6.28	12.57	12.57	3	0.01	0.01	0.07	0.00	0.00	24.0
20	50	-5192	773	-31	0	443	226	6.28	6.28	12.57	12.57	3	0.02	0.01	0.07	0.00	0.00	24.0
37	50	-5540	580	458	0	-196	-80	6.28	6.28	12.57	12.57	3	0.01	0.01	0.05	0.00	0.00	24.0
38	50	-5045	581	162	0	87	260	6.28	6.28	12.57	12.57	3	0.02	0.01	0.06	0.00	0.00	24.0
39	50	-4819	669	-384	0	885	221	6.28	6.28	12.57	12.57	3	0.04	0.01	0.06	0.00	0.00	24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 118 NI 803 NF 821 SEZ. Rp B= 0.400 H= 0.600 (pilastro)
PIL. NUM. 26
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-5781	1466	180	0	55	43	12.57	12.57	6.28	6.28	3	0.00	0.03	0.15	0.00	0.00	24.0
2	0	-4472	1471	192	0	51	-529	12.57	12.57	6.28	6.28	2	0.03	0.03	0.16	0.00	0.00	24.0
3	0	-4472	1477	106	0	42	-531	12.57	12.57	6.28	6.28	2	0.03	0.03	0.16	0.00	0.00	24.0
4	0	-4423	778	171	0	43	598	12.57	12.57	6.28	6.28	2	0.03	0.01	0.08	0.00	0.00	24.0
5	0	-4422	784	84	0	33	595	12.57	12.57	6.28	6.28	2	0.03	0.01	0.08	0.00	0.00	24.0
6	0	-4456	1222	286	0	60	-132	12.57	12.57	6.28	6.28	2	0.01	0.02	0.13	0.00	0.00	24.0
7	0	-4453	1241	-3	0	28	-139	12.57	12.57	6.28	6.28	2	0.01	0.02	0.13	0.00	0.00	24.0
8	0	-4441	1014	280	0	57	206	12.57	12.57	6.28	6.28	2	0.01	0.02	0.11	0.00	0.00	24.0
9	0	-4438	1033	-10	0	25	199	12.57	12.57	6.28	6.28	2	0.01	0.02	0.11	0.00	0.00	24.0
10	0	-4472	1471	192	0	51	-529	12.57	12.57	6.28	6.28	2	0.03	0.03	0.16	0.00	0.00	24.0
11	0	-4472	1477	106	0	42	-531	12.57	12.57	6.28	6.28	2	0.03	0.03	0.16	0.00	0.00	24.0
12	0	-4423	778	171	0	43	598	12.57	12.57	6.28	6.28	2	0.03	0.01	0.08	0.00	0.00	24.0
13	0	-4422	784	84	0	33	595	12.57	12.57	6.28	6.28	2	0.03	0.01	0.08	0.00	0.00	24.0
14	0	-4456	1222	286	0	60	-132	12.57	12.57	6.28	6.28	2	0.01	0.02	0.13	0.00	0.00	24.0
15	0	-4453	1241	-3	0	28	-139	12.57	12.57	6.28	6.28	2	0.01	0.02	0.13	0.00	0.00	24.0
16	0	-4441	1014	280	0	57	206	12.57	12.57	6.28	6.28	2	0.01	0.02	0.11	0.00	0.00	24.0
17	0	-4438	1033	-10	0	25	199	12.57	12.57	6.28	6.28	2	0.01	0.02	0.11	0.00	0.00	24.0
18	0	-6087	4589	512	0	107	-2417	12.57	12.57	6.28	6.28	3	0.09	0.08	0.48	0.00	0.00	24.0
19	0	-6270	1482	393	0	75	1492	12.57	12.57	6.28	6.28	3	0.06	0.03	0.16	0.00	0.00	24.0
20	0	-6141	2809	228	0	67	-381	12.57	12.57	6.28	6.28	3	0.01	0.05	0.30	0.00	0.00	24.0
37	0	-5873	5111	465	0	106	-3553	12.57	12.57	6.28	6.28	3	0.13	0.09	0.54	0.00	0.00	24.0

38	0	-6177	-68	266	0	52	2962	12.57	12.57	6.28	6.28	3	0.11	0.00	0.02	0.00	0.00	24.0
39	0	-5962	2144	-9	0	40	-161	12.57	12.57	6.28	6.28	3	0.01	0.04	0.23	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-5684	1466	180	0	33	226	12.57	12.57	6.28	6.28	3	0.01	0.03	0.15	0.00	0.00	24.0
2	12	-4397	1471	192	0	27	-345	12.57	12.57	6.28	6.28	2	0.02	0.03	0.16	0.00	0.00	24.0
3	12	-4397	1477	106	0	29	-346	12.57	12.57	6.28	6.28	2	0.02	0.03	0.16	0.00	0.00	24.0
4	12	-4348	778	171	0	22	695	12.57	12.57	6.28	6.28	2	0.04	0.01	0.08	0.00	0.00	24.0
5	12	-4347	784	84	0	23	693	12.57	12.57	6.28	6.28	2	0.04	0.01	0.08	0.00	0.00	24.0
6	12	-4381	1222	286	0	24	21	12.57	12.57	6.28	6.28	2	0.00	0.02	0.13	0.00	0.00	24.0
7	12	-4378	1241	-3	0	28	16	12.57	12.57	6.28	6.28	2	0.00	0.02	0.13	0.00	0.00	24.0
8	12	-4366	1014	280	0	22	333	12.57	12.57	6.28	6.28	2	0.02	0.02	0.11	0.00	0.00	24.0
9	12	-4363	1033	-10	0	26	328	12.57	12.57	6.28	6.28	2	0.02	0.02	0.11	0.00	0.00	24.0
10	12	-4397	1471	192	0	27	-345	12.57	12.57	6.28	6.28	2	0.02	0.03	0.16	0.00	0.00	24.0
11	12	-4397	1477	106	0	29	-346	12.57	12.57	6.28	6.28	2	0.02	0.03	0.16	0.00	0.00	24.0
12	12	-4348	778	171	0	22	695	12.57	12.57	6.28	6.28	2	0.04	0.01	0.08	0.00	0.00	24.0
13	12	-4347	784	84	0	23	693	12.57	12.57	6.28	6.28	2	0.04	0.01	0.08	0.00	0.00	24.0
14	12	-4381	1222	286	0	24	21	12.57	12.57	6.28	6.28	2	0.00	0.02	0.13	0.00	0.00	24.0
15	12	-4378	1241	-3	0	28	16	12.57	12.57	6.28	6.28	2	0.00	0.02	0.13	0.00	0.00	24.0
16	12	-4366	1014	280	0	22	333	12.57	12.57	6.28	6.28	2	0.02	0.02	0.11	0.00	0.00	24.0
17	12	-4363	1033	-10	0	26	328	12.57	12.57	6.28	6.28	2	0.02	0.02	0.11	0.00	0.00	24.0
18	12	-5990	4589	512	0	44	-1843	12.57	12.57	6.28	6.28	3	0.07	0.08	0.48	0.00	0.00	24.0
19	12	-6172	1482	393	0	26	1677	12.57	12.57	6.28	6.28	3	0.06	0.03	0.16	0.00	0.00	24.0
20	12	-6044	2809	228	0	39	-30	12.57	12.57	6.28	6.28	3	0.00	0.05	0.30	0.00	0.00	24.0
37	12	-5776	5111	465	0	48	-2914	12.57	12.57	6.28	6.28	3	0.11	0.09	0.54	0.00	0.00	24.0
38	12	-6080	-68	266	0	19	2954	12.57	12.57	6.28	6.28	3	0.11	0.00	0.02	0.00	0.00	24.0
39	12	-5864	2144	-9	0	41	107	12.57	12.57	6.28	6.28	3	0.00	0.04	0.23	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-5586	1466	180	0	10	410	12.57	12.57	6.28	6.28	3	0.02	0.03	0.16	0.00	0.00	24.0
2	25	-4322	1471	192	0	3	-161	12.57	12.57	6.28	6.28	2	0.01	0.03	0.16	0.00	0.00	24.0
3	25	-4322	1477	106	0	15	-162	12.57	12.57	6.28	6.28	2	0.01	0.03	0.16	0.00	0.00	24.0
4	25	-4273	778	171	0	0	792	12.57	12.57	6.28	6.28	2	0.04	0.01	0.08	0.00	0.00	24.0
5	25	-4272	784	84	0	13	791	12.57	12.57	6.28	6.28	2	0.04	0.01	0.08	0.00	0.00	24.0
6	25	-4306	1222	286	0	-12	173	12.57	12.57	6.28	6.28	2	0.01	0.02	0.13	0.00	0.00	24.0
7	25	-4303	1241	-3	0	29	171	12.57	12.57	6.28	6.28	2	0.01	0.02	0.13	0.00	0.00	24.0
8	25	-4291	1014	280	0	-13	459	12.57	12.57	6.28	6.28	2	0.03	0.02	0.11	0.00	0.00	24.0
9	25	-4288	1033	-10	0	28	457	12.57	12.57	6.28	6.28	2	0.03	0.02	0.11	0.00	0.00	24.0
10	25	-4322	1471	192	0	3	-161	12.57	12.57	6.28	6.28	2	0.01	0.03	0.16	0.00	0.00	24.0
11	25	-4322	1477	106	0	15	-162	12.57	12.57	6.28	6.28	2	0.01	0.03	0.16	0.00	0.00	24.0
12	25	-4273	778	171	0	0	792	12.57	12.57	6.28	6.28	2	0.04	0.01	0.08	0.00	0.00	24.0
13	25	-4272	784	84	0	13	791	12.57	12.57	6.28	6.28	2	0.04	0.01	0.08	0.00	0.00	24.0
14	25	-4306	1222	286	0	-12	173	12.57	12.57	6.28	6.28	2	0.01	0.02	0.13	0.00	0.00	24.0
15	25	-4303	1241	-3	0	29	171	12.57	12.57	6.28	6.28	2	0.01	0.02	0.13	0.00	0.00	24.0
16	25	-4291	1014	280	0	-13	459	12.57	12.57	6.28	6.28	2	0.03	0.02	0.11	0.00	0.00	24.0
17	25	-4288	1033	-10	0	28	457	12.57	12.57	6.28	6.28	2	0.03	0.02	0.11	0.00	0.00	24.0
18	25	-5892	4589	512	0	-20	-1270	12.57	12.57	6.28	6.28	3	0.05	0.08	0.48	0.00	0.00	24.0
19	25	-6075	1482	393	0	-23	1862	12.57	12.57	6.28	6.28	3	0.07	0.03	0.16	0.00	0.00	24.0
20	25	-5946	2809	228	0	11	321	12.57	12.57	6.28	6.28	3	0.01	0.05	0.30	0.00	0.00	24.0
37	25	-5678	5111	465	0	-10	-2275	12.57	12.57	6.28	6.28	3	0.08	0.09	0.54	0.00	0.00	24.0
38	25	-5982	-68	266	0	-14	2945	12.57	12.57	6.28	6.28	3	0.11	0.00	0.02	0.00	0.00	24.0
39	25	-5767	2144	-9	0	42	375	12.57	12.57	6.28	6.28	3	0.01	0.04	0.23	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-5488	1466	180	0	-12	593	12.57	12.57	6.28	6.28	3	0.02	0.03	0.16	0.00	0.00	24.0
2	38	-4247	1471	192	0	-21	23	12.57	12.57	6.28	6.28	2	0.00	0.03	0.16	0.00	0.00	24.0
3	38	-4247	1477	106	0	2	23	12.57	12.57	6.28	6.28	2	0.00	0.03	0.16	0.00	0.00	24.0
4	38	-4198	778	171	0	-21	889	12.57	12.57	6.28	6.28	2	0.05	0.01	0.08	0.00	0.00	24.0
5	38	-4197	784	84	0	2	889	12.57	12.57	6.28	6.28	2	0.05	0.01	0.08	0.00	0.00	24.0
6	38	-4231	1222	286	0	-48	326	12.57	12.57	6.28	6.28	2	0.02	0.02	0.13	0.00	0.00	24.0
7	38	-4228	1241	-3	0	29	326	12.57	12.57	6.28	6.28	2	0.02	0.02	0.13	0.00	0.00	24.0
8	38	-4216	1014	280	0	-48	586	12.57	12.57	6.28	6.28	2	0.03	0.02	0.11	0.00	0.00	24.0
9	38	-4213	1033	-10	0	29	586	12.57	12.57	6.28	6.28	2	0.03	0.02	0.11	0.00	0.00	24.0
10	38	-4247	1471	192	0	-21	23	12.57	12.57	6.28	6.28	2	0.00	0.03	0.16	0.00	0.00	24.0
11	38	-4247	1477	106	0	2	23	12.57	12.57	6.28	6.28	2	0.00	0.03	0.16	0.00	0.00	24.0
12	38	-4198	778	171	0	-21	889	12.57	12.57	6.28	6.28	2	0.05	0.01	0.08	0.00	0.00	24.0
13	38	-4197	784	84	0	2	889	12.57	12.57	6.28	6.28	2	0.05	0.01	0.08	0.00	0.00	24.0
14	38	-4231	1222	286	0	-48	326	12.57	12.57	6.28	6.28	2	0.02	0.02	0.13	0.00	0.00	24.0
15	38	-4228	1241	-3	0	29	326	12.57	12.57	6.28	6.28	2	0.02	0.02	0.13	0.00	0.00	24.0
16	38	-4216	1014	280	0	-48	586	12.57	12.57	6.28	6.28	2	0.03	0.02	0.11	0.00	0.00	24.0
17	38	-4213	1033	-10	0	29	586	12.57	12.57	6.28	6.28	2	0.03	0.02	0.11	0.00	0.00	24.0
18	38	-5794	4589	512	0	-85	-696	12.57	12.57	6.28	6.28	3	0.03	0.08	0.48	0.00	0.00	24.0
19	38	-5978	1482	393	0	-72	2048	12.57	12.57	6.28	6.28	3	0.08	0.03	0.16	0.00	0.00	24.0
20	38	-5848	2809	228	0	-18	673	12.57	12.57	6.28	6.28	3	0.03	0.05	0.30	0.00	0.00	24.0
37	38	-5580	5111	465	0	-68	-1637	12.57	12.57	6.28	6.28	3	0.06	0.09	0.54	0.00	0.00	24.0
38	38	-5884	-68	266	0	-48	2937	12.57	12.57	6.28	6.28	3	0.11	0.00	0.02	0.00	0.00	24.0
39	38	-5670	2144	-9	0	43	643	12.57	12.57	6.28	6.28	3	0.02	0.04	0.23	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-5391	1466	180	0	-35	776	12.57	12.57	6.28	6.28	3	0.03	0.03	0.16	0.00	0.00	24.0
2	50	-4172	1471	192	0	-45	207	12.57	12.57	6.28	6.28	2	0.01	0.03	0.16	0.00	0.00	24.0
3	50	-4172	1477	106	0	-11	207	12.57	12.57	6.28	6.28	2	0.01	0.03	0.16	0.00	0.00	24.0
4	50	-4123	778	171	0	-42	986	12.57	12.57	6.28	6.28	2	0.05	0.01	0.08	0.00	0.00	24.0
5	50	-4122	784	84	0	-8	987	12.57	12.57	6.28	6.28	2	0.05	0.01	0.08	0.00	0.00	24.0
6	50	-4156	1222	286	0	-83	479	12.57	12.57	6.28	6.28	2	0.03	0.02	0.13	0.00	0.00	24.0
7	50	-4153	1241	-3	0	29	481	12.57	12.57	6.28	6.28	2	0.03	0.02	0.13	0.00	0.00	24.0
8	50	-4141	1014	280	0	-83	713	12.57	12.57	6.28	6.28	2	0.04	0.02	0.11	0.00	0.00	24.0
9	50	-4138	1033	-10	0	30	715	12.57	12.57	6.28	6.28	2	0.04	0.02	0.11	0.00	0.00	24.0
10	50	-4172	1471	192	0	-45	207	12.57	12.57	6.28	6.28	2	0.01	0.03	0.16	0.00	0.00	24.0
11	50	-4172	1477	106	0	-11	207	12.57	12.57	6.28	6.28	2	0.01	0.03	0.16	0.00	0.00	24.0
12	50	-4123	778	171	0	-42	986	12.57	12.57	6.28	6.28	2	0.05	0.01	0.08	0.00	0.00	24.0
13	50	-4122	784	84	0	-8	987	12.57	12.57	6.28	6.28	2	0.05	0.01	0.08	0.00	0.00	24.0
14	50	-4156	1222	286	0	-83	479	12.57	12.57	6.28	6.28	2	0.03	0.02	0.13	0.00	0.00	24.0
15	50	-4153	1241	-3	0	29	481	12.57	12.57	6.28	6.28	2	0.03	0.02	0.13	0.00	0.00	24.0
16	50	-4141	1014	280	0	-83	713	12.57	12.57	6.28	6.28	2	0.04	0.02	0.11	0.00	0.00	24.0
17	50	-4138	1033	-10	0	30	715	12.57	12.57	6.28	6.28	2	0.04	0.02	0.11	0.00	0.00	24.0
18	50	-5697	4589	512	0	-148	-122	12.57	12.57	6.28	6.28	3	0.01	0.08	0.49	0.00	0.00	24.0
19	50	-5880	1482	393	0	-121	2233	12.57	12.57	6.28	6.28	3	0.08	0.03	0.16	0.00	0.00	24.0
20	50	-5751	2809	228	0	-46	1024	12.57	12.57	6.28	6.28	3	0.04	0.05	0.30	0.00	0.00	24.0
37	50	-5483	5111	465	0	-126	-998	12.57	12.57	6.28	6.28	3	0.04	0.09	0.54	0.00	0.00	24.0
38	50	-5787	-68	266	0	-81	2928	12.57	12.57	6.28	6.28	3	0.11	0.00	0.02	0.00	0.00	24.0
39	50	-5572	2144	-9	0	44	912	12.57	12.57	6.28	6.28	3	0.03	0.04	0.23	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 119 NI 821 NF 166 SEZ. Rp B= 0.400 H= 0.600 (pilastro)

PIL. NUM. 26A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-6889	958	361	0	-35	729	12.57	12.57	6.28	6.28	3	0.03	0.02	0.10	0.00	0.00	24.0
2	0	-5411	724	422	0	-45	175	12.57	12.57	6.28	6.28	2	0.01	0.01	0.08	0.00	0.00	24.0
3	0	-5409	725	108	0	-11	175	12.57	12.57	6.28	6.28	2	0.01	0.01	0.08	0.00	0.00	24.0
4	0	-5190	748	448	0	-42	947	12.57	12.57	6.28	6.28	2	0.05	0.01	0.08	0.00	0.00	24.0
5	0	-5188	750	134	0	-8	947	12.57	12.57	6.28	6.28	2	0.05	0.01	0.08	0.00	0.00	24.0
6	0	-5337	731	798	0	-83	445	12.57	12.57	6.28	6.28	2	0.03	0.01	0.08	0.00	0.00	24.0
7	0	-5329	735	-250	0	29	446	12.57	12.57	6.28	6.28	2	0.02	0.01	0.08	0.00	0.00	24.0
8	0	-5270	738	806	0	-83	677	12.57	12.57	6.28	6.28	2	0.04	0.01	0.08	0.00	0.00	24.0
9	0	-5262	742	-242	0	30	677	12.57	12.57	6.28	6.28	2	0.04	0.01	0.08	0.00	0.00	24.0
10	0	-5411	724	422	0	-45	175	12.57	12.57	6.28	6.28	2	0.01	0.01	0.08	0.00	0.00	24.0
11	0	-5409	725	108	0	-11	175	12.57	12.57	6.28	6.28	2	0.01	0.01	0.08	0.00	0.00	24.0
12	0	-5190	748	448	0	-42	947	12.57	12.57	6.28	6.28	2	0.05	0.01	0.08	0.00	0.00	24.0
13	0	-5188	750	134	0	-8	947	12.57	12.57	6.28	6.28	2	0.05	0.01	0.08	0.00	0.00	24.0
14	0	-5337	731	798	0	-83	445	12.57	12.57	6.28	6.28	2	0.03	0.01	0.08	0.00	0.00	24.0
15	0	-5329	735	-250	0	29	446	12.57	12.57	6.28	6.28	2	0.02	0.01	0.08	0.00	0.00	24.0
16	0	-5270	738	806	0	-83	677	12.57	12.57	6.28	6.28	2	0.04	0.01	0.08	0.00	0.00	24.0
17	0	-5262	742	-242	0	30	677	12.57	12.57	6.28	6.28	2	0.04	0.01	0.08	0.00	0.00	24.0
18	0	-7784	1862	1398	0	-148	-219	12.57	12.57	6.28	6.28	3	0.01	0.03	0.19	0.00	0.00	24.0
19	0	-7281	1493	1308	0	-121	2130	12.57	12.57	6.28	6.28	3	0.08	0.03	0.15	0.00	0.00	24.0
20	0	-7465	1573	512	0	-46	930	12.57	12.57	6.28	6.28	3	0.03	0.03	0.16	0.00	0.00	24.0
37	0	-7707	1750	1119	0	-126	-1075	12.57	12.57	6.28	6.28	3	0.04	0.03	0.18	0.00	0.00	24.0
38	0	-6870	1134	969	0	-81	2840	12.57	12.57	6.28	6.28	3	0.11	0.02	0.12	0.00	0.00	24.0
39	0	-7176	1268	-357	0	44	840	12.57	12.57	6.28	6.28	3	0.03	0.02	0.13	0.00	0.00	24.0
apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0																		
1	12	-6792	958	361	0	-80	849	12.57	12.57	6.28	6.28	3	0.03	0.02	0.10	0.00	0.00	24.0
2	12	-5336	724	422	0	-98	265	12.57	12.57	6.28	6.28	2	0.02	0.01	0.08	0.00	0.00	24.0
3	12	-5334	725	108	0	-24	266	12.57	12.57	6.28	6.28	2	0.01	0.01	0.08	0.00	0.00	24.0
4	12	-5115	748	448	0	-98	1041	12.57	12.57	6.28	6.28	2	0.06	0.01	0.08	0.00	0.00	24.0
5	12	-5113	750	134	0	-25	1041	12.57	12.57	6.28	6.28	2	0.06	0.01	0.08	0.00	0.00	24.0
6	12	-5262	731	798	0	-183	536	12.57	12.57	6.28	6.28	2	0.04	0.01	0.08	0.00	0.00	24.0
7	12	-5254	735	-250	0	61	538	12.57	12.57	6.28	6.28	2	0.03	0.01	0.08	0.00	0.00	24.0
8	12	-5195	738	806	0	-183	769	12.57	12.57	6.28	6.28	2	0.05	0.01	0.08	0.00	0.00	24.0
9	12	-5187	742	-242	0	60	770	12.57	12.57	6.28	6.28	2	0.04	0.01	0.08	0.00	0.00	24.0
10	12	-5336	724	422	0	-98	265	12.57	12.57	6.28	6.28	2	0.02	0.01	0.08	0.00	0.00	24.0
11	12	-5334	725	108	0	-24	266	12.57	12.57	6.28	6.28	2	0.01	0.01	0.08	0.00	0.00	24.0
12	12	-5115	748	448	0	-98	1041	12.57	12.57	6.28	6.28	2	0.06	0.01	0.08	0.00	0.00	24.0
13	12	-5113	750	134	0	-25	1041	12.57	12.57	6.28	6.28	2	0.06	0.01	0.08	0.00	0.00	24.0
14	12	-5262	731	798	0	-183	536	12.57	12.57	6.28	6.28	2	0.04	0.01	0.08	0.00	0.00	24.0
15	12	-5254	735	-250	0	61	538	12.57	12.57	6.28	6.28	2	0.03	0.01	0.08	0.00	0.00	24.0
16	12	-5195	738	806	0	-183	769	12.57	12.57	6.28	6.28	2	0.05	0.01	0.08	0.00	0.00	24.0
17	12	-5187	742	-242	0	60	770	12.57	12.57	6.28	6.28	2	0.04	0.01	0.08	0.00	0.00	24.0
18	12	-7686	1862	1398	0	-323	14	12.57	12.57	6.28	6.28	3	0.02	0.03	0.19	0.00	0.00	24.0
19	12	-7184	1493	1308	0	-285	2316	12.57	12.57	6.28	6.28	3	0.09	0.03	0.15	0.00	0.00	24.0
20	12	-7368	1573	512	0	-110	1127	12.57	12.57	6.28	6.28	3	0.04	0.03	0.16	0.00	0.00	24.0
37	12	-7610	1750	1119	0	-266	-856	12.57	12.57	6.28	6.28	3	0.04	0.03	0.18	0.00	0.00	24.0
38	12	-6772	1134	969	0	-202	2982	12.57	12.57	6.28	6.28	3	0.11	0.02	0.12	0.00	0.00	24.0
39	12	-7078	1268	-357	0	89	998	12.57	12.57	6.28	6.28	3	0.04	0.02	0.13	0.00	0.00	24.0
apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0																		
1	25	-6694	958	361	0	-125	969	12.57	12.57	6.28	6.28	3	0.04	0.02	0.10	0.00	0.00	24.0
2	25	-5261	724	422	0	-150	356	12.57	12.57	6.28	6.28	2	0.02	0.01	0.08	0.00	0.00	24.0
3	25	-5259	725	108	0	-38	356	12.57	12.57	6.28	6.28	2	0.02	0.01	0.08	0.00	0.00	24.0
4	25	-5040	748	448	0	-154	1134	12.57	12.57	6.28	6.28	2	0.07	0.01	0.08	0.00	0.00	24.0
5	25	-5038	750	134	0	-42	1135	12.57	12.57	6.28	6.28	2	0.06	0.01	0.08	0.00	0.00	24.0
6	25	-5187	731	798	0	-283	628	12.57	12.57	6.28	6.28	2	0.04	0.01	0.08	0.00	0.00	24.0
7	25	-5179	735	-250	0	92	630	12.57	12.57	6.28	6.28	2	0.04	0.01	0.08	0.00	0.00	24.0
8	25	-5120	738	806	0	-284	861	12.57	12.57	6.28	6.28	2	0.06	0.01	0.08	0.00	0.00	24.0
9	25	-5112	742	-242	0	91	863	12.57	12.57	6.28	6.28	2	0.05	0.01	0.08	0.00	0.00	24.0
10	25	-5261	724	422	0	-150	356	12.57	12.57	6.28	6.28	2	0.02	0.01	0.08	0.00	0.00	24.0
11	25	-5259	725	108	0	-38	356	12.57	12.57	6.28	6.28	2	0.02	0.01	0.08	0.00	0.00	24.0
12	25	-5040	748	448	0	-154	1134	12.57	12.57	6.28	6.28	2	0.07	0.01	0.08	0.00	0.00	24.0
13	25	-5038	750	134	0	-42	1135	12.57	12.57	6.28	6.28	2	0.06	0.01	0.08	0.00	0.00	24.0
14	25	-5187	731	798	0	-283	628	12.57	12.57	6.28	6.28	2	0.04	0.01	0.08	0.00	0.00	24.0
15	25	-5179	735	-250	0	92	630	12.57	12.57	6.28	6.28	2	0.04	0.01	0.08	0.00	0.00	24.0
16	25	-5120	738	806	0	-284	861	12.57	12.57	6.28	6.28	2	0.06	0.01	0.08	0.00	0.00	24.0
17	25	-5112	742	-242	0	91	863	12.57	12.57	6.28	6.28	2	0.05	0.01	0.08	0.00	0.00	24.0
18	25	-7589	1862	1398	0	-498	247	12.57	12.57	6.28	6.28	3	0.03	0.03	0.19	0.00	0.00	24.0
19	25	-7086	1493	1308	0	-448	2503	12.57	12.57	6.28	6.28	3	0.10	0.03	0.15	0.00	0.00	24.0
20	25	-7270	1573	512	0	-174	1324	12.57	12.57	6.28	6.28	3	0.05	0.03	0.16	0.00	0.00	24.0
37	25	-7512	1750	1119	0	-406	-638	12.57	12.57	6.28	6.28	3	0.03	0.03	0.18	0.00	0.00	24.0
38	25	-6675	1134	969	0	-323	3123	12.57	12.57	6.28	6.28	3	0.12	0.02	0.12	0.00	0.00	24.0
39	25	-6981	1268	-357	0	133	1157	12.57	12.57	6.28	6.28	3	0.04	0.02	0.13	0.00	0.00	24.0
apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0																		
1	38	-6596	958	361	0	-170	1088	12.57	12.57	6.28	6.28	3	0.04	0.02	0.10	0.00	0.00	24.0
2	38	-5186	724	422	0	-203	446	12.57	12.57	6.28	6.28	2	0.03	0.01	0.08	0.00	0.00	24.0
3	38	-5184	725	108	0	-51	447	12.57	12.57	6.28	6.28	2	0.03	0.01	0.08	0.00	0.00	24.0
4	38	-4965	748	448	0	-210	1228	12.57	12.57	6.28	6.28	2	0.07	0.01	0.08	0.00	0.00	24.0
5	38	-4963	750	134	0	-59	1228	12.57	12.57	6.28	6.28	2	0.07	0.01	0.08	0.00	0.00	24.0
6	38	-5112	731	798	0	-383	719	12.57	12.57	6.28	6.28	2	0.05	0.01	0.08	0.00	0.00	24.0
7	38	-5104	735	-250	0	123	721	12.57	12.57	6.28	6.28	2	0.04	0.01	0.08	0.00	0.00	24.0
8	38	-5045	738	806	0	-385	954	12.57	12.57	6.28	6.28	2	0.06	0.01	0.08	0.00	0.00	24.0
9	38	-5037	742	-242	0	121	956	12.57	12.57	6.28	6.28	2	0.06	0.01	0.08	0.00	0.00	24.0
10	38	-5186	724	422	0	-203	446	12.57	12.57	6.28	6.28	2	0.03	0.01	0.08	0.00	0.00	24.0
11	38	-5184	725	108	0	-51	447	12.57	12.57	6.28	6.28	2	0.03	0.01	0.08	0.00	0.00	24.0
12	38	-4965	748	448	0	-210	1228	12.57	12.57	6.28	6.28	2	0.07	0.01	0.08	0.00	0.00	24.0
13	38	-4963	750	134	0	-59	1228	12.57	12.57	6.28	6.28	2	0.07	0.01	0.08	0.00	0.00	24.0
14	38	-5112	731	798	0	-383	719	12.57	12.57	6.28	6.28	2	0.05	0.01	0.08	0.00	0.00	24.0
15	38	-5104	735	-250	0	123	721	12.57	12.57	6.28	6.28	2	0.04	0.01	0.08	0.00	0.00	24.0
16	38	-5045	738	806	0	-385	954	12.57	12.57	6.28	6.28	2	0.06	0.01	0.08	0.00	0.00	24.0
17	38	-5037	742	-242	0	121	956	12.57	12.57	6.28	6.28	2	0.06	0.01	0.08	0.00	0.00	24.0
18	38	-7492	1862	1398	0	-673	479	12.57	12.57	6.28	6.28	3	0.04	0.03	0.19	0.00	0.00	24.0
19	38	-6988	1493	1308	0	-612	2690	12.57	12.57	6.28	6.28	3	0.11	0.03	0.15	0.00	0.00	24.0
20	38	-7172	1573	512	0	-238	1520	12.57	12.57	6.28	6.28	3	0.06	0.03	0.16	0.00	0.00	24.0
37	38	-7414	1750	1119	0	-546	-419	12.57	12.57	6.28	6.28	3	0.03	0.03	0.18	0.00	0.00	24.0
38	38	-6578	1134	969	0	-444	3265	12.57	12.57	6.28	6.28	3	0.13	0.02	0.12	0.00	0.00	24.0
39	38	-6884	1268	-357	0	178	1315	12.57	12.57	6.28	6.28	3	0.05	0.02	0.13	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-6499	958	361	0	-215	1208	12.57	12.57	6.28	6.28	3	0.05	0.02	0.10	0.00	0.00	24.0
2	50	-5111	724	422	0	-256	537	12.57	12.57	6.28	6.28	2	0.04	0.01	0.08	0.00	0.00	24.0
3	50	-5109	725	108	0	-65	538	12.57	12.57	6.28	6.28	2	0.03	0.01	0.08	0.00	0.00	24.0
4	50	-4890	748	448	0	-266	1321	12.57	12.57	6.28	6.28	2	0.08	0.01	0.08	0.00	0.00	24.0
5	50	-4888	750	134	0	-75	1322	12.57	12.57	6.28	6.28	2	0.07	0.01	0.08	0.00	0.00	24.0
6	50	-5037	731	798	0	-482	810	12.57	12.57	6.28	6.28	2	0.06	0.01	0.08	0.00	0.00	24.0
7	50	-5029	735	-250	0	154	813	12.57	12.57	6.28	6.28	2	0.05	0.01	0.08	0.00	0.00	24.0
8	50	-4970	738	806	0	-485	1046	12.57	12.57	6.28	6.28	2	0.07	0.01	0.08	0.00	0.00	24.0
9	50	-4962	742	-242	0	151	1049	12.57	12.57	6.28	6.28	2	0.06	0.01	0.08	0.00	0.00	24.0
10	50	-5111	724	422	0	-256	537	12.57	12.57	6.28	6.28	2	0.04	0.01	0.08	0.00	0.00	24.0
11	50	-5109	725	108	0	-65	538	12.57	12.57	6.28	6.28	2	0.03	0.01	0.08	0.00	0.00	24.0
12	50	-4890	748	448	0	-266	1321	12.57	12.57	6.28	6.28	2	0.08	0.01	0.08	0.00	0.00	24.0
13	50	-4888	750	134	0	-75	1322	12.57	12.57	6.28	6.28	2	0.07	0.01	0.08	0.00	0.00	24.0
14	50	-5037	731	798	0	-482	810	12.57	12.57	6.28	6.28	2	0.06	0.01	0.08	0.00	0.00	24.0
15	50	-5029	735	-250	0	154	813	12.57	12.57	6.28	6.28	2	0.05	0.01	0.08	0.00	0.00	24.0
16	50	-4970	738	806	0	-485	1046	12.57	12.57	6.28	6.28	2	0.07	0.01	0.08	0.00	0.00	24.0
17	50	-4962	742	-242	0	151	1049	12.57	12.57	6.28	6.28	2	0.06	0.01	0.08	0.00	0.00	24.0
18	50	-7394	1862	1398	0	-847	712	12.57	12.57	6.28	6.28	3	0.05	0.03	0.19	0.00	0.00	24.0
19	50	-6891	1493	1308	0	-775	2876	12.57	12.57	6.28	6.28	3	0.12	0.03	0.16	0.00	0.00	24.0
20	50	-7075	1573	512	0	-302	1717	12.57	12.57	6.28	6.28	3	0.07	0.03	0.16	0.00	0.00	24.0
37	50	-7317	1750	1119	0	-686	-200	12.57	12.57	6.28	6.28	3	0.04	0.03	0.18	0.00	0.00	24.0
38	50	-6480	1134	969	0	-566	3407	12.57	12.57	6.28	6.28	3	0.13	0.02	0.12	0.00	0.00	24.0
39	50	-6786	1268	-357	0	222	1474	12.57	12.57	6.28	6.28	3	0.06	0.02	0.13	0.00	0.00	24.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 120 NI 804 NF 827 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 25
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-8414	139	390	0	37	-55	6.28	6.28	9.42	9.42	3	0.01	0.01	0.05	0.00	0.00	24.0
2	0	-6825	149	377	0	20	-160	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
3	0	-6770	148	247	0	34	-159	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
4	0	-6174	65	353	0	23	75	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
5	0	-6119	65	223	0	37	75	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
6	0	-6662	120	521	0	4	-78	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
7	0	-6478	119	87	0	52	-77	6.28	6.28	9.42	9.42	2	0.01	0.00	0.01	0.00	0.00	24.0
8	0	-6467	95	514	0	5	-8	6.28	6.28	9.42	9.42	2	0.00	0.01	0.06	0.00	0.00	24.0
9	0	-6283	94	79	0	53	-6	6.28	6.28	9.42	9.42	2	0.00	0.00	0.01	0.00	0.00	24.0
10	0	-6825	149	377	0	20	-160	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
11	0	-6770	148	247	0	34	-159	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
12	0	-6174	65	353	0	23	75	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
13	0	-6119	65	223	0	37	75	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
14	0	-6662	120	521	0	4	-78	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
15	0	-6478	119	87	0	52	-77	6.28	6.28	9.42	9.42	2	0.01	0.00	0.01	0.00	0.00	24.0
16	0	-6467	95	514	0	5	-8	6.28	6.28	9.42	9.42	2	0.00	0.01	0.06	0.00	0.00	24.0
17	0	-6283	94	79	0	53	-6	6.28	6.28	9.42	9.42	2	0.00	0.00	0.01	0.00	0.00	24.0
18	0	-10140	474	859	0	4	-528	6.28	6.28	9.42	9.42	3	0.05	0.02	0.10	0.00	0.00	24.0
19	0	-8876	94	737	0	26	328	6.28	6.28	9.42	9.42	3	0.03	0.02	0.09	0.00	0.00	24.0
20	0	-9259	262	484	0	45	-96	6.28	6.28	9.42	9.42	3	0.01	0.01	0.06	0.00	0.00	24.0
37	0	-10160	554	769	0	3	-798	6.28	6.28	9.42	9.42	3	0.08	0.02	0.09	0.00	0.00	24.0
38	0	-8056	-81	565	0	40	628	6.28	6.28	9.42	9.42	3	0.07	0.01	0.07	0.00	0.00	24.0
39	0	-8695	200	143	0	71	-78	6.28	6.28	9.42	9.42	3	0.01	0.01	0.02	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-8341	139	390	0	-12	-38	6.28	6.28	9.42	9.42	3	0.00	0.01	0.05	0.00	0.00	24.0
2	12	-6769	149	377	0	-28	-141	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
3	12	-6714	148	247	0	3	-141	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
4	12	-6118	65	353	0	-21	83	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
5	12	-6063	65	223	0	9	83	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
6	12	-6606	120	521	0	-61	-63	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
7	12	-6422	119	87	0	41	-62	6.28	6.28	9.42	9.42	2	0.01	0.00	0.01	0.00	0.00	24.0
8	12	-6411	95	514	0	-59	4	6.28	6.28	9.42	9.42	2	0.00	0.01	0.06	0.00	0.00	24.0
9	12	-6227	94	79	0	43	5	6.28	6.28	9.42	9.42	2	0.00	0.00	0.01	0.00	0.00	24.0
10	12	-6769	149	377	0	-28	-141	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
11	12	-6714	148	247	0	3	-141	6.28	6.28	9.42	9.42	2	0.02	0.01	0.03	0.00	0.00	24.0
12	12	-6118	65	353	0	-21	83	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
13	12	-6063	65	223	0	9	83	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
14	12	-6606	120	521	0	-61	-63	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
15	12	-6422	119	87	0	41	-62	6.28	6.28	9.42	9.42	2	0.01	0.00	0.01	0.00	0.00	24.0
16	12	-6411	95	514	0	-59	4	6.28	6.28	9.42	9.42	2	0.00	0.01	0.06	0.00	0.00	24.0
17	12	-6227	94	79	0	43	5	6.28	6.28	9.42	9.42	2	0.00	0.00	0.01	0.00	0.00	24.0
18	12	-10066	474	859	0	-103	-469	6.28	6.28	9.42	9.42	3	0.05	0.02	0.10	0.00	0.00	24.0
19	12	-8803	94	737	0	-66	340	6.28	6.28	9.42	9.42	3	0.04	0.02	0.09	0.00	0.00	24.0
20	12	-9186	262	484	0	-15	-63	6.28	6.28	9.42	9.42	3	0.01	0.01	0.06	0.00	0.00	24.0
37	12	-10086	554	769	0	-93	-729	6.28	6.28	9.42	9.42	3	0.08	0.02	0.09	0.00	0.00	24.0
38	12	-7983	-81	565	0	-31	618	6.28	6.28	9.42	9.42	3	0.07	0.01	0.07	0.00	0.00	24.0
39	12	-8622	200	143	0	54	-53	6.28	6.28	9.42	9.42	3	0.01	0.01	0.02	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-8268	139	390	0	-61	-20	6.28	6.28	9.42	9.42	3	0.00	0.01	0.05	0.00	0.00	24.0
2	25	-6712	149	377	0	-75	-122	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
3	25	-6658	148	247	0	-28	-122	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
4	25	-6062	65	353	0	-65	91	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
5	25	-6006	65	223	0	-18	91	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
6	25	-6550	120	521	0	-126	-48	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
7	25	-6366	119	87	0	30	-47	6.28	6.28	9.42	9.42	2	0.01	0.00	0.01	0.00	0.00	24.0
8	25	-6354	95	514	0	-123	16	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
9	25	-6170	94	79	0	33	17	6.28	6.28	9.42	9.42	2	0.00	0.00	0.01	0.00	0.00	24.0
10	25	-6712	149	377	0	-75	-122	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
11	25	-6658	148	247	0	-28	-122	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
12	25	-6062	65	353	0	-65	91	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
13	25	-6006	65	223	0	-18	91	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
14	25	-6550	120	521	0	-126	-48	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
15	25	-6366	119	87	0	30	-47	6.28	6.28	9.42	9.42	2	0.01	0.00	0.01	0.00	0.00	24.0
16	25	-6354	95	514	0	-123	16	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
17	25	-6170	94	79	0	33	17	6.28	6.28	9.42	9.42	2	0.00	0.00	0.01	0.00	0.00	24.0
18	25	-9992	474	859	0	-211	-409	6.28	6.28	9.42	9.42	3	0.04	0.02	0.10	0.00	0.00	24.0
19	25	-8730	94	737	0	-158	351	6.28	6.28	9.42	9.42	3	0.04	0.02	0.09	0.00	0.00	24.0

20	25	-9113	262	484	0	-76	-30	6.28	6.28	9.42	9.42	3	0.00	0.01	0.06	0.00	0.00	24.0
37	25	-10013	554	769	0	-189	-660	6.28	6.28	9.42	9.42	3	0.07	0.02	0.09	0.00	0.00	24.0
38	25	-7910	-81	565	0	-101	608	6.28	6.28	9.42	9.42	3	0.06	0.01	0.07	0.00	0.00	24.0
39	25	-8548	200	143	0	36	-28	6.28	6.28	9.42	9.42	3	0.00	0.01	0.02	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-8195	139	390	0	-109	-3	6.28	6.28	9.42	9.42	3	0.01	0.01	0.05	0.00	0.00	24.0
2	38	-6656	149	377	0	-122	-104	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
3	38	-6601	148	247	0	-59	-104	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
4	38	-6005	65	353	0	-109	99	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
5	38	-5950	65	223	0	-46	100	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
6	38	-6493	120	521	0	-191	-33	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
7	38	-6309	119	87	0	19	-32	6.28	6.28	9.42	9.42	2	0.00	0.00	0.01	0.00	0.00	24.0
8	38	-6298	95	514	0	-187	28	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
9	38	-6114	94	79	0	23	29	6.28	6.28	9.42	9.42	2	0.00	0.00	0.01	0.00	0.00	24.0
10	38	-6656	149	377	0	-122	-104	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
11	38	-6601	148	247	0	-59	-104	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
12	38	-6005	65	353	0	-109	99	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
13	38	-5950	65	223	0	-46	100	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
14	38	-6493	120	521	0	-191	-33	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
15	38	-6309	119	87	0	19	-32	6.28	6.28	9.42	9.42	2	0.00	0.00	0.01	0.00	0.00	24.0
16	38	-6298	95	514	0	-187	28	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
17	38	-6114	94	79	0	23	29	6.28	6.28	9.42	9.42	2	0.00	0.00	0.01	0.00	0.00	24.0
18	38	-9919	474	859	0	-318	-350	6.28	6.28	9.42	9.42	3	0.04	0.02	0.10	0.00	0.00	24.0
19	38	-8656	94	737	0	-250	363	6.28	6.28	9.42	9.42	3	0.04	0.02	0.09	0.00	0.00	24.0
20	38	-9040	262	484	0	-136	3	6.28	6.28	9.42	9.42	3	0.01	0.01	0.06	0.00	0.00	24.0
37	38	-9940	554	769	0	-286	-591	6.28	6.28	9.42	9.42	3	0.06	0.02	0.09	0.00	0.00	24.0
38	38	-7836	-81	565	0	-172	598	6.28	6.28	9.42	9.42	3	0.06	0.01	0.07	0.00	0.00	24.0
39	38	-8475	200	143	0	18	-3	6.28	6.28	9.42	9.42	3	0.00	0.01	0.02	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-8122	139	390	0	-158	15	6.28	6.28	9.42	9.42	3	0.01	0.01	0.05	0.00	0.00	24.0
2	50	-6600	149	377	0	-169	-85	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
3	50	-6545	148	247	0	-90	-85	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
4	50	-5949	65	353	0	-154	107	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
5	50	-5894	65	223	0	-74	108	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
6	50	-6437	120	521	0	-256	-18	6.28	6.28	9.42	9.42	2	0.02	0.01	0.06	0.00	0.00	24.0
7	50	-6253	119	87	0	8	-17	6.28	6.28	9.42	9.42	2	0.00	0.00	0.01	0.00	0.00	24.0
8	50	-6242	95	514	0	-252	40	6.28	6.28	9.42	9.42	2	0.02	0.01	0.06	0.00	0.00	24.0
9	50	-6058	94	79	0	13	41	6.28	6.28	9.42	9.42	2	0.01	0.00	0.01	0.00	0.00	24.0
10	50	-6600	149	377	0	-169	-85	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
11	50	-6545	148	247	0	-90	-85	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
12	50	-5949	65	353	0	-154	107	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
13	50	-5894	65	223	0	-74	108	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
14	50	-6437	120	521	0	-256	-18	6.28	6.28	9.42	9.42	2	0.02	0.01	0.06	0.00	0.00	24.0
15	50	-6253	119	87	0	8	-17	6.28	6.28	9.42	9.42	2	0.00	0.00	0.01	0.00	0.00	24.0
16	50	-6242	95	514	0	-252	40	6.28	6.28	9.42	9.42	2	0.02	0.01	0.06	0.00	0.00	24.0
17	50	-6058	94	79	0	13	41	6.28	6.28	9.42	9.42	2	0.01	0.00	0.01	0.00	0.00	24.0
18	50	-9845	474	859	0	-425	-291	6.28	6.28	9.42	9.42	3	0.03	0.02	0.10	0.00	0.00	24.0
19	50	-8583	94	737	0	-342	375	6.28	6.28	9.42	9.42	3	0.04	0.02	0.09	0.00	0.00	24.0
20	50	-8967	262	484	0	-196	35	6.28	6.28	9.42	9.42	3	0.01	0.01	0.06	0.00	0.00	24.0
37	50	-9866	554	769	0	-382	-522	6.28	6.28	9.42	9.42	3	0.06	0.02	0.09	0.00	0.00	24.0
38	50	-7763	-81	565	0	-242	588	6.28	6.28	9.42	9.42	3	0.06	0.01	0.07	0.00	0.00	24.0
39	50	-8402	200	143	0	-0	22	6.28	6.28	9.42	9.42	3	0.00	0.01	0.02	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 121 NI 827 NF 263 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 25A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-11750	77	682	0	-158	5	6.28	6.28	9.42	9.42	3	0.01	0.02	0.08	0.00	0.00	24.0
2	0	-9619	-122	738	0	-169	-84	6.28	6.28	9.42	9.42	2	0.02	0.02	0.09	0.00	0.00	24.0
3	0	-9529	-121	392	0	-90	-84	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
4	0	-8541	239	658	0	-154	92	6.28	6.28	9.42	9.42	2	0.02	0.02	0.08	0.00	0.00	24.0
5	0	-8451	240	312	0	-74	93	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
6	0	-9347	4	1114	0	-256	-23	6.28	6.28	9.42	9.42	2	0.02	0.03	0.13	0.00	0.00	24.0
7	0	-9046	6	-40	0	8	-22	6.28	6.28	9.42	9.42	2	0.00	0.00	0.00	0.00	0.00	24.0
8	0	-9024	112	1090	0	-252	30	6.28	6.28	9.42	9.42	2	0.02	0.03	0.13	0.00	0.00	24.0
9	0	-8723	114	-64	0	13	31	6.28	6.28	9.42	9.42	2	0.00	0.00	0.01	0.00	0.00	24.0
10	0	-9619	-122	738	0	-169	-84	6.28	6.28	9.42	9.42	2	0.02	0.02	0.09	0.00	0.00	24.0
11	0	-9529	-121	392	0	-90	-84	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
12	0	-8541	239	658	0	-154	92	6.28	6.28	9.42	9.42	2	0.02	0.02	0.08	0.00	0.00	24.0
13	0	-8451	240	312	0	-74	93	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
14	0	-9347	4	1114	0	-256	-23	6.28	6.28	9.42	9.42	2	0.02	0.03	0.13	0.00	0.00	24.0
15	0	-9046	6	-40	0	8	-22	6.28	6.28	9.42	9.42	2	0.00	0.00	0.00	0.00	0.00	24.0
16	0	-9024	112	1090	0	-252	30	6.28	6.28	9.42	9.42	2	0.02	0.03	0.13	0.00	0.00	24.0
17	0	-8723	114	-64	0	13	31	6.28	6.28	9.42	9.42	2	0.00	0.00	0.01	0.00	0.00	24.0
18	0	-14430	-422	1873	0	-425	-287	6.28	6.28	9.42	9.42	3	0.03	0.04	0.20	0.00	0.00	24.0
19	0	-12250	737	1455	0	-342	323	6.28	6.28	9.42	9.42	3	0.03	0.03	0.16	0.00	0.00	24.0
20	0	-12960	141	788	0	-196	14	6.28	6.28	9.42	9.42	3	0.01	0.02	0.09	0.00	0.00	24.0
37	0	-14570	-834	1700	0	-382	-494	6.28	6.28	9.42	9.42	3	0.05	0.04	0.19	0.00	0.00	24.0
38	0	-10950	1097	1005	0	-242	523	6.28	6.28	9.42	9.42	3	0.05	0.03	0.12	0.00	0.00	24.0
39	0	-12120	103	-108	0	-0	8	6.28	6.28	9.42	9.42	3	0.00	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-11675	77	682	0	-243	15	6.28	6.28	9.42	9.42	3	0.01	0.02	0.08	0.00	0.00	24.0
2	12	-9563	-122	738	0	-261	-100	6.28	6.28	9.42	9.42	2	0.02	0.02	0.09	0.00	0.00	24.0
3	12	-9473	-121	392	0	-139	-99	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
4	12	-8485	239	658	0	-236	122	6.28	6.28	9.42	9.42	2	0.02	0.02	0.08	0.00	0.00	24.0
5	12	-8395	240	312	0	-113	123	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
6	12	-9291	4	1114	0	-395	-22	6.28	6.28	9.42	9.42	2	0.03	0.03	0.13	0.00	0.00	24.0
7	12	-8990	6	-40	0	13	-21	6.28	6.28	9.42	9.42	2	0.00	0.00	0.00	0.00	0.00	24.0
8	12	-8968	112	1090	0	-388	44	6.28	6.28	9.42	9.42	2	0.03	0.03	0.13	0.00	0.00	24.0
9	12	-8667	114	-64	0	21	45	6.28	6.28	9.42	9.42	2	0.01	0.00	0.01	0.00	0.00	24.0
10	12	-9563	-122	738	0	-261	-100	6.28	6.28	9.42	9.42	2	0.02	0.02	0.09	0.00	0.00	24.0
11	12	-9473	-121	392	0	-139	-99	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
12	12	-8485	239	658	0	-236	122	6.28	6.28	9.42	9.42	2	0.02	0.02	0.08	0.00	0.00	24.0
13	12	-8395	240	312	0	-113	123	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
14	12	-9291	4	1114	0	-395	-22	6.28	6.28	9.42	9.42	2	0.03	0.03	0.13	0.00	0.00	24.0
15	12	-8990	6	-40	0	13	-21	6.28	6.28	9.42	9.42	2	0.00	0.00	0.00	0.00	0.00	24.0

16	12	-8968	112	1090	0	-388	44	6.28	6.28	9.42	9.42	2	0.03	0.03	0.13	0.00	0.00	24.0
17	12	-8667	114	-64	0	21	45	6.28	6.28	9.42	9.42	2	0.01	0.00	0.01	0.00	0.00	24.0
18	12	-14358	-422	1873	0	-660	-339	6.28	6.28	9.42	9.42	3	0.04	0.04	0.20	0.00	0.00	24.0
19	12	-12178	737	1455	0	-524	416	6.28	6.28	9.42	9.42	3	0.05	0.03	0.16	0.00	0.00	24.0
20	12	-12888	141	788	0	-295	32	6.28	6.28	9.42	9.42	3	0.01	0.02	0.09	0.00	0.00	24.0
37	12	-14498	-834	1700	0	-594	-598	6.28	6.28	9.42	9.42	3	0.06	0.04	0.19	0.00	0.00	24.0
38	12	-10875	1097	1005	0	-368	660	6.28	6.28	9.42	9.42	3	0.07	0.03	0.12	0.00	0.00	24.0
39	12	-12048	103	-108	0	14	20	6.28	6.28	9.42	9.42	3	0.00	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-11600	77	682	0	-329	25	6.28	6.28	9.42	9.42	3	0.02	0.02	0.08	0.00	0.00	24.0
2	25	-9506	-122	738	0	-353	-115	6.28	6.28	9.42	9.42	2	0.03	0.02	0.09	0.00	0.00	24.0
3	25	-9416	-121	392	0	-188	-114	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
4	25	-8428	239	658	0	-318	152	6.28	6.28	9.42	9.42	2	0.03	0.02	0.08	0.00	0.00	24.0
5	25	-8338	240	312	0	-152	153	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
6	25	-9234	4	1114	0	-535	-22	6.28	6.28	9.42	9.42	2	0.03	0.03	0.13	0.00	0.00	24.0
7	25	-8934	6	-40	0	18	-20	6.28	6.28	9.42	9.42	2	0.00	0.00	0.00	0.00	0.00	24.0
8	25	-8912	112	1090	0	-524	58	6.28	6.28	9.42	9.42	2	0.04	0.03	0.13	0.00	0.00	24.0
9	25	-8610	114	-64	0	29	60	6.28	6.28	9.42	9.42	2	0.01	0.00	0.01	0.00	0.00	24.0
10	25	-9506	-122	738	0	-353	-115	6.28	6.28	9.42	9.42	2	0.03	0.02	0.09	0.00	0.00	24.0
11	25	-9416	-121	392	0	-188	-114	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
12	25	-8428	239	658	0	-318	152	6.28	6.28	9.42	9.42	2	0.03	0.02	0.08	0.00	0.00	24.0
13	25	-8338	240	312	0	-152	153	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
14	25	-9234	4	1114	0	-535	-22	6.28	6.28	9.42	9.42	2	0.03	0.03	0.13	0.00	0.00	24.0
15	25	-8934	6	-40	0	18	-20	6.28	6.28	9.42	9.42	2	0.00	0.00	0.00	0.00	0.00	24.0
16	25	-8912	112	1090	0	-524	58	6.28	6.28	9.42	9.42	2	0.04	0.03	0.13	0.00	0.00	24.0
17	25	-8610	114	-64	0	29	60	6.28	6.28	9.42	9.42	2	0.01	0.00	0.01	0.00	0.00	24.0
18	25	-14285	-422	1873	0	-894	-392	6.28	6.28	9.42	9.42	3	0.05	0.04	0.21	0.00	0.00	24.0
19	25	-12105	737	1455	0	-706	508	6.28	6.28	9.42	9.42	3	0.06	0.03	0.16	0.00	0.00	24.0
20	25	-12815	141	788	0	-393	49	6.28	6.28	9.42	9.42	3	0.02	0.02	0.09	0.00	0.00	24.0
37	25	-14425	-834	1700	0	-807	-702	6.28	6.28	9.42	9.42	3	0.07	0.04	0.19	0.00	0.00	24.0
38	25	-10800	1097	1005	0	-494	797	6.28	6.28	9.42	9.42	3	0.08	0.03	0.12	0.00	0.00	24.0
39	25	-11975	103	-108	0	27	33	6.28	6.28	9.42	9.42	3	0.00	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-11525	77	682	0	-414	34	6.28	6.28	9.42	9.42	3	0.02	0.02	0.08	0.00	0.00	24.0
2	38	-9450	-122	738	0	-446	-130	6.28	6.28	9.42	9.42	2	0.03	0.02	0.09	0.00	0.00	24.0
3	38	-9360	-121	392	0	-237	-130	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
4	38	-8372	239	658	0	-400	182	6.28	6.28	9.42	9.42	2	0.04	0.02	0.08	0.00	0.00	24.0
5	38	-8282	240	312	0	-191	183	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
6	38	-9178	4	1114	0	-674	-21	6.28	6.28	9.42	9.42	2	0.04	0.03	0.13	0.00	0.00	24.0
7	38	-8877	6	-40	0	23	-20	6.28	6.28	9.42	9.42	2	0.00	0.00	0.00	0.00	0.00	24.0
8	38	-8855	112	1090	0	-660	72	6.28	6.28	9.42	9.42	2	0.04	0.03	0.13	0.00	0.00	24.0
9	38	-8554	114	-64	0	37	74	6.28	6.28	9.42	9.42	2	0.01	0.00	0.01	0.00	0.00	24.0
10	38	-9450	-122	738	0	-446	-130	6.28	6.28	9.42	9.42	2	0.03	0.02	0.09	0.00	0.00	24.0
11	38	-9360	-121	392	0	-237	-130	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
12	38	-8372	239	658	0	-400	182	6.28	6.28	9.42	9.42	2	0.04	0.02	0.08	0.00	0.00	24.0
13	38	-8282	240	312	0	-191	183	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
14	38	-9178	4	1114	0	-674	-21	6.28	6.28	9.42	9.42	2	0.04	0.03	0.13	0.00	0.00	24.0
15	38	-8877	6	-40	0	23	-20	6.28	6.28	9.42	9.42	2	0.00	0.00	0.00	0.00	0.00	24.0
16	38	-8855	112	1090	0	-660	72	6.28	6.28	9.42	9.42	2	0.04	0.03	0.13	0.00	0.00	24.0
17	38	-8554	114	-64	0	37	74	6.28	6.28	9.42	9.42	2	0.01	0.00	0.01	0.00	0.00	24.0
18	38	-14212	-422	1873	0	-1128	-445	6.28	6.28	9.42	9.42	3	0.07	0.04	0.21	0.00	0.00	24.0
19	38	-12032	737	1455	0	-888	600	6.28	6.28	9.42	9.42	3	0.07	0.03	0.17	0.00	0.00	24.0
20	38	-12742	141	788	0	-492	67	6.28	6.28	9.42	9.42	3	0.02	0.02	0.09	0.00	0.00	24.0
37	38	-14352	-834	1700	0	-1019	-807	6.28	6.28	9.42	9.42	3	0.09	0.04	0.19	0.00	0.00	24.0
38	38	-10725	1097	1005	0	-619	934	6.28	6.28	9.42	9.42	3	0.10	0.03	0.12	0.00	0.00	24.0
39	38	-11902	103	-108	0	41	46	6.28	6.28	9.42	9.42	3	0.00	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-11450	77	682	0	-499	44	6.28	6.28	9.42	9.42	3	0.02	0.02	0.08	0.00	0.00	24.0
2	50	-9394	-122	738	0	-538	-145	6.28	6.28	9.42	9.42	2	0.04	0.02	0.09	0.00	0.00	24.0
3	50	-9304	-121	392	0	-286	-145	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
4	50	-8316	239	658	0	-483	212	6.28	6.28	9.42	9.42	2	0.04	0.02	0.08	0.00	0.00	24.0
5	50	-8226	240	312	0	-230	213	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
6	50	-9122	4	1114	0	-813	-21	6.28	6.28	9.42	9.42	2	0.05	0.03	0.13	0.00	0.00	24.0
7	50	-8821	6	-40	0	28	-19	6.28	6.28	9.42	9.42	2	0.00	0.00	0.00	0.00	0.00	24.0
8	50	-8799	112	1090	0	-796	86	6.28	6.28	9.42	9.42	2	0.05	0.03	0.13	0.00	0.00	24.0
9	50	-8498	114	-64	0	45	88	6.28	6.28	9.42	9.42	2	0.01	0.00	0.01	0.00	0.00	24.0
10	50	-9394	-122	738	0	-538	-145	6.28	6.28	9.42	9.42	2	0.04	0.02	0.09	0.00	0.00	24.0
11	50	-9304	-121	392	0	-286	-145	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
12	50	-8316	239	658	0	-483	212	6.28	6.28	9.42	9.42	2	0.04	0.02	0.08	0.00	0.00	24.0
13	50	-8226	240	312	0	-230	213	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
14	50	-9122	4	1114	0	-813	-21	6.28	6.28	9.42	9.42	2	0.05	0.03	0.13	0.00	0.00	24.0
15	50	-8821	6	-40	0	28	-19	6.28	6.28	9.42	9.42	2	0.00	0.00	0.00	0.00	0.00	24.0
16	50	-8799	112	1090	0	-796	86	6.28	6.28	9.42	9.42	2	0.05	0.03	0.13	0.00	0.00	24.0
17	50	-8498	114	-64	0	45	88	6.28	6.28	9.42	9.42	2	0.01	0.00	0.01	0.00	0.00	24.0
18	50	-14140	-422	1873	0	-1362	-497	6.28	6.28	9.42	9.42	3	0.08	0.04	0.21	0.00	0.00	24.0
19	50	-11960	737	1455	0	-1070	692	6.28	6.28	9.42	9.42	3	0.08	0.03	0.17	0.00	0.00	24.0
20	50	-12670	141	788	0	-590	85	6.28	6.28	9.42	9.42	3	0.03	0.02	0.09	0.00	0.00	24.0
37	50	-14280	-834	1700	0	-1232	-911	6.28	6.28	9.42	9.42	3	0.10	0.04	0.19	0.00	0.00	24.0
38	50	-10650	1097	1005	0	-745	1071	6.28	6.28	9.42	9.42	3	0.11	0.03	0.12	0.00	0.00	24.0
39	50	-11830	103	-108	0	54	59	6.28	6.28	9.42	9.42	3	0.01	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 122 NI 805 NF 830 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 24
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-4213	24	363	0	-67	18	6.28	6.28	9.42	9.42	3	0.00	0.01	0.05	0.00	0.00	24.0
2	0	-3263	-4	376	0	-66	-13	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
3	0	-3252	-4	229	0	-49	-13	6.28	6.28	9.42	9.42	2	0.00	0.01	0.03	0.00	0.00	24.0
4	0	-3229	41	329	0	-54	41	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
5	0	-3218	42	182	0	-37	41	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
6	0	-3264	11	532	0	-82	5	6.28	6.28	9.42	9.42	2	0.01	0.01	0.07	0.00	0.00	24.0
7	0	-3227	12	41	0	-25	7	6.28	6.28	9.42	9.42	2	0.00	0.00	0.01	0.00	0.00	24.0
8	0	-3253	25	517	0	-78	22	6.28	6.28	9.42	9.42	2	0.01	0.01	0.07	0.00	0.00	24.0
9	0	-3217	26	27	0	-22	23	6.28	6.28	9.42	9.42	2	0.00	0.00	0.00	0.00	0.00	24.0
10	0	-3263	-4	376	0	-66	-13	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
11	0	-3252	-4	229	0	-49	-13	6.28	6.28	9.42	9.42	2	0.00	0.01	0.03	0.00	0.00	24.0

12	0	-3229	41	329	0	-54	41	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
13	0	-3218	42	182	0	-37	41	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
14	0	-3264	11	532	0	-82	5	6.28	6.28	9.42	9.42	2	0.01	0.01	0.07	0.00	0.00	24.0
15	0	-3227	12	41	0	-25	7	6.28	6.28	9.42	9.42	2	0.00	0.00	0.01	0.00	0.00	24.0
16	0	-3253	25	517	0	-78	22	6.28	6.28	9.42	9.42	2	0.01	0.01	0.07	0.00	0.00	24.0
17	0	-3217	26	27	0	-22	23	6.28	6.28	9.42	9.42	2	0.00	0.00	0.00	0.00	0.00	24.0
18	0	-4600	-34	840	0	-123	-53	6.28	6.28	9.42	9.42	3	0.01	0.02	0.11	0.00	0.00	24.0
19	0	-4502	102	642	0	-84	112	6.28	6.28	9.42	9.42	3	0.01	0.02	0.08	0.00	0.00	24.0
20	0	-4519	33	346	0	-61	28	6.28	6.28	9.42	9.42	3	0.00	0.01	0.04	0.00	0.00	24.0
37	0	-4478	-83	784	0	-124	-112	6.28	6.28	9.42	9.42	3	0.01	0.02	0.10	0.00	0.00	24.0
38	0	-4315	145	454	0	-59	163	6.28	6.28	9.42	9.42	3	0.02	0.01	0.06	0.00	0.00	24.0
39	0	-4343	29	-39	0	-20	24	6.28	6.28	9.42	9.42	3	0.00	0.00	0.00	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-4140	24	363	0	-113	21	6.28	6.28	9.42	9.42	3	0.01	0.01	0.05	0.00	0.00	24.0
2	12	-3207	-4	376	0	-113	-14	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
3	12	-3196	-4	229	0	-78	-13	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
4	12	-3173	41	329	0	-95	46	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
5	12	-3162	42	182	0	-60	47	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
6	12	-3208	11	532	0	-148	7	6.28	6.28	9.42	9.42	2	0.01	0.01	0.07	0.00	0.00	24.0
7	12	-3171	12	41	0	-30	8	6.28	6.28	9.42	9.42	2	0.00	0.00	0.01	0.00	0.00	24.0
8	12	-3197	25	517	0	-143	25	6.28	6.28	9.42	9.42	2	0.01	0.01	0.07	0.00	0.00	24.0
9	12	-3161	26	27	0	-25	26	6.28	6.28	9.42	9.42	2	0.00	0.00	0.00	0.00	0.00	24.0
10	12	-3207	-4	376	0	-113	-14	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
11	12	-3196	-4	229	0	-78	-13	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
12	12	-3173	41	329	0	-95	46	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
13	12	-3162	42	182	0	-60	47	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
14	12	-3208	11	532	0	-148	7	6.28	6.28	9.42	9.42	2	0.01	0.01	0.07	0.00	0.00	24.0
15	12	-3171	12	41	0	-30	8	6.28	6.28	9.42	9.42	2	0.00	0.00	0.01	0.00	0.00	24.0
16	12	-3197	25	517	0	-143	25	6.28	6.28	9.42	9.42	2	0.01	0.01	0.07	0.00	0.00	24.0
17	12	-3161	26	27	0	-25	26	6.28	6.28	9.42	9.42	2	0.00	0.00	0.00	0.00	0.00	24.0
18	12	-4527	-34	840	0	-228	-57	6.28	6.28	9.42	9.42	3	0.01	0.02	0.11	0.00	0.00	24.0
19	12	-4429	102	642	0	-164	125	6.28	6.28	9.42	9.42	3	0.01	0.02	0.08	0.00	0.00	24.0
20	12	-4446	33	346	0	-104	32	6.28	6.28	9.42	9.42	3	0.01	0.01	0.04	0.00	0.00	24.0
37	12	-4405	-83	784	0	-222	-122	6.28	6.28	9.42	9.42	3	0.02	0.02	0.10	0.00	0.00	24.0
38	12	-4242	145	454	0	-116	181	6.28	6.28	9.42	9.42	3	0.02	0.01	0.06	0.00	0.00	24.0
39	12	-4270	29	-39	0	-15	27	6.28	6.28	9.42	9.42	3	0.00	0.00	0.00	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-4066	24	363	0	-158	24	6.28	6.28	9.42	9.42	3	0.01	0.01	0.05	0.00	0.00	24.0
2	25	-3150	-4	376	0	-160	-14	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
3	25	-3140	-4	229	0	-107	-14	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
4	25	-3116	41	329	0	-136	51	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
5	25	-3106	42	182	0	-83	52	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
6	25	-3152	11	532	0	-215	8	6.28	6.28	9.42	9.42	2	0.01	0.01	0.07	0.00	0.00	24.0
7	25	-3114	12	41	0	-36	10	6.28	6.28	9.42	9.42	2	0.00	0.00	0.01	0.00	0.00	24.0
8	25	-3140	25	517	0	-208	28	6.28	6.28	9.42	9.42	2	0.02	0.01	0.07	0.00	0.00	24.0
9	25	-3104	26	27	0	-28	29	6.28	6.28	9.42	9.42	2	0.00	0.00	0.00	0.00	0.00	24.0
10	25	-3150	-4	376	0	-160	-14	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
11	25	-3140	-4	229	0	-107	-14	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
12	25	-3116	41	329	0	-136	51	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
13	25	-3106	42	182	0	-83	52	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
14	25	-3152	11	532	0	-215	8	6.28	6.28	9.42	9.42	2	0.01	0.01	0.07	0.00	0.00	24.0
15	25	-3114	12	41	0	-36	10	6.28	6.28	9.42	9.42	2	0.00	0.00	0.01	0.00	0.00	24.0
16	25	-3140	25	517	0	-208	28	6.28	6.28	9.42	9.42	2	0.02	0.01	0.07	0.00	0.00	24.0
17	25	-3104	26	27	0	-28	29	6.28	6.28	9.42	9.42	2	0.00	0.00	0.00	0.00	0.00	24.0
18	25	-4454	-34	840	0	-333	-62	6.28	6.28	9.42	9.42	3	0.02	0.02	0.11	0.00	0.00	24.0
19	25	-4356	102	642	0	-245	137	6.28	6.28	9.42	9.42	3	0.02	0.02	0.08	0.00	0.00	24.0
20	25	-4373	33	346	0	-147	36	6.28	6.28	9.42	9.42	3	0.01	0.01	0.04	0.00	0.00	24.0
37	25	-4332	-83	784	0	-320	-132	6.28	6.28	9.42	9.42	3	0.02	0.02	0.10	0.00	0.00	24.0
38	25	-4169	145	454	0	-173	199	6.28	6.28	9.42	9.42	3	0.02	0.01	0.06	0.00	0.00	24.0
39	25	-4197	29	-39	0	-10	31	6.28	6.28	9.42	9.42	3	0.00	0.00	0.00	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-3993	24	363	0	-203	27	6.28	6.28	9.42	9.42	3	0.01	0.01	0.05	0.00	0.00	24.0
2	38	-3094	-4	376	0	-207	-15	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
3	38	-3083	-4	229	0	-135	-14	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
4	38	-3060	41	329	0	-178	57	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
5	38	-3049	42	182	0	-105	57	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
6	38	-3095	11	532	0	-281	10	6.28	6.28	9.42	9.42	2	0.02	0.01	0.07	0.00	0.00	24.0
7	38	-3058	12	41	0	-41	11	6.28	6.28	9.42	9.42	2	0.00	0.00	0.01	0.00	0.00	24.0
8	38	-3084	25	517	0	-272	31	6.28	6.28	9.42	9.42	2	0.02	0.01	0.07	0.00	0.00	24.0
9	38	-3048	26	27	0	-32	33	6.28	6.28	9.42	9.42	2	0.01	0.00	0.00	0.00	0.00	24.0
10	38	-3094	-4	376	0	-207	-15	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
11	38	-3083	-4	229	0	-135	-14	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
12	38	-3060	41	329	0	-178	57	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
13	38	-3049	42	182	0	-105	57	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
14	38	-3095	11	532	0	-281	10	6.28	6.28	9.42	9.42	2	0.02	0.01	0.07	0.00	0.00	24.0
15	38	-3058	12	41	0	-41	11	6.28	6.28	9.42	9.42	2	0.00	0.00	0.01	0.00	0.00	24.0
16	38	-3084	25	517	0	-272	31	6.28	6.28	9.42	9.42	2	0.02	0.01	0.07	0.00	0.00	24.0
17	38	-3048	26	27	0	-32	33	6.28	6.28	9.42	9.42	2	0.01	0.00	0.00	0.00	0.00	24.0
18	38	-4381	-34	840	0	-438	-66	6.28	6.28	9.42	9.42	3	0.02	0.02	0.11	0.00	0.00	24.0
19	38	-4283	102	642	0	-325	150	6.28	6.28	9.42	9.42	3	0.02	0.02	0.08	0.00	0.00	24.0
20	38	-4300	33	346	0	-190	40	6.28	6.28	9.42	9.42	3	0.01	0.01	0.04	0.00	0.00	24.0
37	38	-4258	-83	784	0	-418	-143	6.28	6.28	9.42	9.42	3	0.03	0.02	0.10	0.00	0.00	24.0
38	38	-4096	145	454	0	-230	217	6.28	6.28	9.42	9.42	3	0.03	0.01	0.06	0.00	0.00	24.0
39	38	-4124	29	-39	0	-5	34	6.28	6.28	9.42	9.42	3	0.00	0.00	0.00	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-3920	24	363	0	-249	30	6.28	6.28	9.42	9.42	3	0.01	0.01	0.05	0.00	0.00	24.0
2	50	-3038	-4	376	0	-254	-15	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
3	50	-3027	-4	229	0	-164	-15	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
4	50	-3004	41	329	0	-219	62	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
5	50	-2993	42	182	0	-128	62	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
6	50	-3039	11	532	0	-348	11	6.28	6.28	9.42	9.42	2	0.02	0.01	0.07	0.00	0.00	24.0
7	50	-3002	12	41	0	-46	13	6.28	6.28	9.42	9.42	2	0.00	0.00	0.01	0.00	0.00	24.0
8	50	-3028	25	517	0	-337	34	6.28	6.28	9.42	9.42	2	0.02	0.01	0.07	0.00	0.00	24.0
9	50	-2992	26	27	0	-35	36	6.28	6.28	9.42	9.42	2	0.01	0.00	0.00	0.00	0.00	24.0
10	50	-3038	-4	376	0	-254	-15	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
11	50	-3027	-4	229	0	-164	-15	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
12	50	-3004	41	329	0	-219	62	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
13	50	-2993	42	182	0	-128	62	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
14	50	-3039	11	532	0	-348	11	6.28	6.28	9.42	9.42	2	0.02	0.01	0.07	0.00	0.00	24.0
15	50	-3002	12	41	0	-46	13	6.28	6.28	9.42	9.42	2	0.00	0.00	0.01	0.00	0.00	24.0
16	50	-3028	25	517	0	-337	34	6.28	6.28	9.42	9.42	2	0.02	0.01	0.07	0.00	0.00	24.0
17	50	-2992	26	27	0	-35	36	6.28	6.28	9.42	9.42	2	0.01	0.00	0.00	0.00	0.00	24.0

18	50	-4308	-34	840	0	-543	-70	6.28	6.28	9.42	9.42	3	0.03	0.02	0.11	0.00	0.00	24.0
19	50	-4210	102	642	0	-405	163	6.28	6.28	9.42	9.42	3	0.03	0.02	0.08	0.00	0.00	24.0
20	50	-4227	33	346	0	-234	44	6.28	6.28	9.42	9.42	3	0.01	0.01	0.04	0.00	0.00	24.0
37	50	-4185	-83	784	0	-516	-153	6.28	6.28	9.42	9.42	3	0.03	0.02	0.10	0.00	0.00	24.0
38	50	-4023	145	454	0	-286	235	6.28	6.28	9.42	9.42	3	0.03	0.01	0.06	0.00	0.00	24.0
39	50	-4051	29	-39	0	-1	38	6.28	6.28	9.42	9.42	3	0.00	0.00	0.00	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 123 NI 830 NF 122 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 24A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-6195	85	1121	0	-249	27	6.28	6.28	9.42	9.42	3	0.01	0.03	0.14	0.00	0.00	24.0
2	0	-4788	-21	1139	0	-254	-12	6.28	6.28	9.42	9.42	2	0.02	0.03	0.15	0.00	0.00	24.0
3	0	-4774	-20	752	0	-164	-12	6.28	6.28	9.42	9.42	2	0.01	0.02	0.10	0.00	0.00	24.0
4	0	-4756	150	973	0	-219	53	6.28	6.28	9.42	9.42	2	0.02	0.02	0.12	0.00	0.00	24.0
5	0	-4743	151	586	0	-128	54	6.28	6.28	9.42	9.42	2	0.01	0.01	0.07	0.00	0.00	24.0
6	0	-4792	38	1533	0	-348	10	6.28	6.28	9.42	9.42	2	0.02	0.04	0.20	0.00	0.00	24.0
7	0	-4747	41	242	0	-46	12	6.28	6.28	9.42	9.42	2	0.00	0.01	0.03	0.00	0.00	24.0
8	0	-4783	89	1483	0	-337	30	6.28	6.28	9.42	9.42	2	0.02	0.03	0.19	0.00	0.00	24.0
9	0	-4738	93	192	0	-35	31	6.28	6.28	9.42	9.42	2	0.00	0.00	0.02	0.00	0.00	24.0
10	0	-4788	-21	1139	0	-254	-12	6.28	6.28	9.42	9.42	2	0.02	0.03	0.15	0.00	0.00	24.0
11	0	-4774	-20	752	0	-164	-12	6.28	6.28	9.42	9.42	2	0.01	0.02	0.10	0.00	0.00	24.0
12	0	-4756	150	973	0	-219	53	6.28	6.28	9.42	9.42	2	0.02	0.02	0.12	0.00	0.00	24.0
13	0	-4743	151	586	0	-128	54	6.28	6.28	9.42	9.42	2	0.01	0.01	0.07	0.00	0.00	24.0
14	0	-4792	38	1533	0	-348	10	6.28	6.28	9.42	9.42	2	0.02	0.04	0.20	0.00	0.00	24.0
15	0	-4747	41	242	0	-46	12	6.28	6.28	9.42	9.42	2	0.00	0.01	0.03	0.00	0.00	24.0
16	0	-4783	89	1483	0	-337	30	6.28	6.28	9.42	9.42	2	0.02	0.03	0.19	0.00	0.00	24.0
17	0	-4738	93	192	0	-35	31	6.28	6.28	9.42	9.42	2	0.00	0.00	0.02	0.00	0.00	24.0
18	0	-6755	-134	2381	0	-543	-59	6.28	6.28	9.42	9.42	3	0.03	0.06	0.29	0.00	0.00	24.0
19	0	-6665	376	1760	0	-405	140	6.28	6.28	9.42	9.42	3	0.02	0.04	0.22	0.00	0.00	24.0
20	0	-6673	117	1047	0	-234	39	6.28	6.28	9.42	9.42	3	0.01	0.02	0.13	0.00	0.00	24.0
37	0	-6545	-316	2279	0	-516	-129	6.28	6.28	9.42	9.42	3	0.03	0.05	0.28	0.00	0.00	24.0
38	0	-6394	535	1245	0	-286	201	6.28	6.28	9.42	9.42	3	0.02	0.03	0.15	0.00	0.00	24.0
39	0	-6407	102	57	0	-1	33	6.28	6.28	9.42	9.42	3	0.00	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-6122	85	1121	0	-389	38	6.28	6.28	9.42	9.42	3	0.02	0.03	0.14	0.00	0.00	24.0
2	12	-4732	-21	1139	0	-397	-15	6.28	6.28	9.42	9.42	2	0.03	0.03	0.15	0.00	0.00	24.0
3	12	-4718	-20	752	0	-258	-14	6.28	6.28	9.42	9.42	2	0.02	0.02	0.10	0.00	0.00	24.0
4	12	-4700	150	973	0	-340	72	6.28	6.28	9.42	9.42	2	0.03	0.02	0.12	0.00	0.00	24.0
5	12	-4687	151	586	0	-201	73	6.28	6.28	9.42	9.42	2	0.02	0.01	0.08	0.00	0.00	24.0
6	12	-4736	38	1533	0	-539	15	6.28	6.28	9.42	9.42	2	0.04	0.04	0.20	0.00	0.00	24.0
7	12	-4691	41	242	0	-76	17	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
8	12	-4727	89	1483	0	-522	41	6.28	6.28	9.42	9.42	2	0.04	0.03	0.19	0.00	0.00	24.0
9	12	-4682	93	192	0	-59	43	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
10	12	-4732	-21	1139	0	-397	-15	6.28	6.28	9.42	9.42	2	0.03	0.03	0.15	0.00	0.00	24.0
11	12	-4718	-20	752	0	-258	-14	6.28	6.28	9.42	9.42	2	0.02	0.02	0.10	0.00	0.00	24.0
12	12	-4700	150	973	0	-340	72	6.28	6.28	9.42	9.42	2	0.03	0.02	0.12	0.00	0.00	24.0
13	12	-4687	151	586	0	-201	73	6.28	6.28	9.42	9.42	2	0.02	0.01	0.08	0.00	0.00	24.0
14	12	-4736	38	1533	0	-539	15	6.28	6.28	9.42	9.42	2	0.04	0.04	0.20	0.00	0.00	24.0
15	12	-4691	41	242	0	-76	17	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
16	12	-4727	89	1483	0	-522	41	6.28	6.28	9.42	9.42	2	0.04	0.03	0.19	0.00	0.00	24.0
17	12	-4682	93	192	0	-59	43	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
18	12	-6682	-134	2381	0	-840	-76	6.28	6.28	9.42	9.42	3	0.04	0.06	0.29	0.00	0.00	24.0
19	12	-6592	376	1760	0	-625	187	6.28	6.28	9.42	9.42	3	0.04	0.04	0.22	0.00	0.00	24.0
20	12	-6600	117	1047	0	-365	54	6.28	6.28	9.42	9.42	3	0.02	0.02	0.13	0.00	0.00	24.0
37	12	-6472	-316	2279	0	-801	-169	6.28	6.28	9.42	9.42	3	0.04	0.05	0.28	0.00	0.00	24.0
38	12	-6321	535	1245	0	-442	268	6.28	6.28	9.42	9.42	3	0.03	0.03	0.15	0.00	0.00	24.0
39	12	-6334	102	57	0	-8	46	6.28	6.28	9.42	9.42	3	0.00	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-6048	85	1121	0	-529	48	6.28	6.28	9.42	9.42	3	0.03	0.03	0.14	0.00	0.00	24.0
2	25	-4676	-21	1139	0	-539	-18	6.28	6.28	9.42	9.42	2	0.04	0.03	0.15	0.00	0.00	24.0
3	25	-4662	-20	752	0	-352	-17	6.28	6.28	9.42	9.42	2	0.02	0.02	0.10	0.00	0.00	24.0
4	25	-4644	150	973	0	-462	91	6.28	6.28	9.42	9.42	2	0.04	0.02	0.12	0.00	0.00	24.0
5	25	-4630	151	586	0	-275	92	6.28	6.28	9.42	9.42	2	0.02	0.01	0.08	0.00	0.00	24.0
6	25	-4680	38	1533	0	-731	20	6.28	6.28	9.42	9.42	2	0.05	0.04	0.20	0.00	0.00	24.0
7	25	-4634	41	242	0	-106	22	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
8	25	-4670	89	1483	0	-708	52	6.28	6.28	9.42	9.42	2	0.05	0.03	0.19	0.00	0.00	24.0
9	25	-4626	93	192	0	-83	54	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
10	25	-4676	-21	1139	0	-539	-18	6.28	6.28	9.42	9.42	2	0.04	0.03	0.15	0.00	0.00	24.0
11	25	-4662	-20	752	0	-352	-17	6.28	6.28	9.42	9.42	2	0.02	0.02	0.10	0.00	0.00	24.0
12	25	-4644	150	973	0	-462	91	6.28	6.28	9.42	9.42	2	0.04	0.02	0.12	0.00	0.00	24.0
13	25	-4630	151	586	0	-275	92	6.28	6.28	9.42	9.42	2	0.02	0.01	0.08	0.00	0.00	24.0
14	25	-4680	38	1533	0	-731	20	6.28	6.28	9.42	9.42	2	0.05	0.04	0.20	0.00	0.00	24.0
15	25	-4634	41	242	0	-106	22	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
16	25	-4670	89	1483	0	-708	52	6.28	6.28	9.42	9.42	2	0.05	0.03	0.19	0.00	0.00	24.0
17	25	-4626	93	192	0	-83	54	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
18	25	-6609	-134	2381	0	-1138	-92	6.28	6.28	9.42	9.42	3	0.06	0.06	0.29	0.00	0.00	24.0
19	25	-6519	376	1760	0	-845	234	6.28	6.28	9.42	9.42	3	0.05	0.04	0.22	0.00	0.00	24.0
20	25	-6527	117	1047	0	-495	68	6.28	6.28	9.42	9.42	3	0.02	0.02	0.13	0.00	0.00	24.0
37	25	-6398	-316	2279	0	-1085	-208	6.28	6.28	9.42	9.42	3	0.06	0.05	0.28	0.00	0.00	24.0
38	25	-6248	535	1245	0	-598	335	6.28	6.28	9.42	9.42	3	0.04	0.03	0.16	0.00	0.00	24.0
39	25	-6261	102	57	0	-15	59	6.28	6.28	9.42	9.42	3	0.01	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-5975	85	1121	0	-669	59	6.28	6.28	9.42	9.42	3	0.03	0.03	0.14	0.00	0.00	24.0
2	38	-4619	-21	1139	0	-682	-20	6.28	6.28	9.42	9.42	2	0.04	0.03	0.15	0.00	0.00	24.0
3	38	-4605	-20	752	0	-446	-19	6.28	6.28	9.42	9.42	2	0.03	0.02	0.10	0.00	0.00	24.0
4	38	-4587	150	973	0	-584	110	6.28	6.28	9.42	9.42	2	0.04	0.02	0.12	0.00	0.00	24.0
5	38	-4574	151	586	0	-348	111	6.28	6.28	9.42	9.42	2	0.03	0.01	0.08	0.00	0.00	24.0
6	38	-4623	38	1533	0	-922	24	6.28	6.28	9.42	9.42	2	0.06	0.04	0.20	0.00	0.00	24.0
7	38	-4578	41	242	0	-136	27	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
8	38	-4614	89	1483	0	-893	63	6.28	6.28	9.42	9.42	2	0.06	0.03	0.19	0.00	0.00	24.0
9	38	-4569	93	192	0	-107	66	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
10	38	-4619	-21	1139	0	-682	-20	6.28	6.28	9.42	9.42	2	0.04	0.03	0.15	0.00	0.00	24.0
11	38	-4605	-20	752	0	-446	-19	6.28	6.28	9.42	9.42	2	0.03	0.02	0.10	0.00	0.00	24.0
12	38	-4587	150	973	0	-584	110	6.28	6.28	9.42	9.42	2	0.04	0.02	0.12	0.00	0.00	24.0
13	38	-4574	151	586	0	-348	111	6.28	6.28	9.42	9.42	2	0.03	0.01	0.08	0.00	0.00	24.0

14	38	-4623	38	1533	0	-922	24	6.28	6.28	9.42	9.42	2	0.06	0.04	0.20	0.00	0.00	24.0
15	38	-4578	41	242	0	-136	27	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
16	38	-4614	89	1483	0	-893	63	6.28	6.28	9.42	9.42	2	0.06	0.03	0.19	0.00	0.00	24.0
17	38	-4569	93	192	0	-107	66	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
18	38	-6536	-134	2381	0	-1435	-109	6.28	6.28	9.42	9.42	3	0.07	0.06	0.30	0.00	0.00	24.0
19	38	-6446	376	1760	0	-1065	281	6.28	6.28	9.42	9.42	3	0.06	0.04	0.22	0.00	0.00	24.0
20	38	-6454	117	1047	0	-626	83	6.28	6.28	9.42	9.42	3	0.03	0.02	0.13	0.00	0.00	24.0
37	38	-6325	-316	2279	0	-1370	-248	6.28	6.28	9.42	9.42	3	0.07	0.05	0.28	0.00	0.00	24.0
38	38	-6175	535	1245	0	-753	402	6.28	6.28	9.42	9.42	3	0.05	0.03	0.16	0.00	0.00	24.0
39	38	-6188	102	57	0	-22	72	6.28	6.28	9.42	9.42	3	0.01	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-5902	85	1121	0	-809	69	6.28	6.28	9.42	9.42	3	0.04	0.03	0.14	0.00	0.00	24.0
2	50	-4563	-21	1139	0	-824	-23	6.28	6.28	9.42	9.42	2	0.05	0.03	0.15	0.00	0.00	24.0
3	50	-4549	-20	752	0	-540	-22	6.28	6.28	9.42	9.42	2	0.04	0.02	0.10	0.00	0.00	24.0
4	50	-4531	150	973	0	-705	128	6.28	6.28	9.42	9.42	2	0.05	0.02	0.12	0.00	0.00	24.0
5	50	-4518	151	586	0	-421	129	6.28	6.28	9.42	9.42	2	0.04	0.01	0.08	0.00	0.00	24.0
6	50	-4567	38	1533	0	-1114	29	6.28	6.28	9.42	9.42	2	0.07	0.04	0.20	0.00	0.00	24.0
7	50	-4522	41	242	0	-167	32	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
8	50	-4558	89	1483	0	-1079	74	6.28	6.28	9.42	9.42	2	0.07	0.03	0.19	0.00	0.00	24.0
9	50	-4513	93	192	0	-131	78	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
10	50	-4563	-21	1139	0	-824	-23	6.28	6.28	9.42	9.42	2	0.05	0.03	0.15	0.00	0.00	24.0
11	50	-4549	-20	752	0	-540	-22	6.28	6.28	9.42	9.42	2	0.04	0.02	0.10	0.00	0.00	24.0
12	50	-4531	150	973	0	-705	128	6.28	6.28	9.42	9.42	2	0.05	0.02	0.12	0.00	0.00	24.0
13	50	-4518	151	586	0	-421	129	6.28	6.28	9.42	9.42	2	0.04	0.01	0.08	0.00	0.00	24.0
14	50	-4567	38	1533	0	-1114	29	6.28	6.28	9.42	9.42	2	0.07	0.04	0.20	0.00	0.00	24.0
15	50	-4522	41	242	0	-167	32	6.28	6.28	9.42	9.42	2	0.01	0.01	0.03	0.00	0.00	24.0
16	50	-4558	89	1483	0	-1079	74	6.28	6.28	9.42	9.42	2	0.07	0.03	0.19	0.00	0.00	24.0
17	50	-4513	93	192	0	-131	78	6.28	6.28	9.42	9.42	2	0.01	0.00	0.02	0.00	0.00	24.0
18	50	-6463	-134	2381	0	-1733	-126	6.28	6.28	9.42	9.42	3	0.08	0.06	0.30	0.00	0.00	24.0
19	50	-6373	376	1760	0	-1285	328	6.28	6.28	9.42	9.42	3	0.07	0.04	0.22	0.00	0.00	24.0
20	50	-6381	117	1047	0	-757	97	6.28	6.28	9.42	9.42	3	0.04	0.02	0.13	0.00	0.00	24.0
37	50	-6252	-316	2279	0	-1655	-288	6.28	6.28	9.42	9.42	3	0.08	0.05	0.28	0.00	0.00	24.0
38	50	-6102	535	1245	0	-909	469	6.28	6.28	9.42	9.42	3	0.06	0.03	0.16	0.00	0.00	24.0
39	50	-6115	102	57	0	-29	84	6.28	6.28	9.42	9.42	3	0.01	0.00	0.01	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 124 NI 806 NF 833 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 23
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-3855	-192	616	0	-217	39	6.28	6.28	9.42	9.42	3	0.01	0.01	0.08	0.00	0.00	24.0
2	0	-3080	-179	536	0	-187	39	6.28	6.28	9.42	9.42	2	0.01	0.01	0.07	0.00	0.00	24.0
3	0	-2960	-179	427	0	-161	40	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
4	0	-2971	-116	521	0	-173	20	6.28	6.28	9.42	9.42	2	0.01	0.01	0.07	0.00	0.00	24.0
5	0	-2851	-116	411	0	-147	21	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
6	0	-3182	-157	659	0	-213	32	6.28	6.28	9.42	9.42	2	0.02	0.02	0.09	0.00	0.00	24.0
7	0	-2782	-157	293	0	-125	34	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
8	0	-3149	-138	654	0	-209	26	6.28	6.28	9.42	9.42	2	0.02	0.02	0.09	0.00	0.00	24.0
9	0	-2749	-138	288	0	-121	28	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
10	0	-3080	-179	536	0	-187	39	6.28	6.28	9.42	9.42	2	0.01	0.01	0.07	0.00	0.00	24.0
11	0	-2960	-179	427	0	-161	40	6.28	6.28	9.42	9.42	2	0.01	0.01	0.06	0.00	0.00	24.0
12	0	-2971	-116	521	0	-173	20	6.28	6.28	9.42	9.42	2	0.01	0.01	0.07	0.00	0.00	24.0
13	0	-2851	-116	411	0	-147	21	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
14	0	-3182	-157	659	0	-213	32	6.28	6.28	9.42	9.42	2	0.02	0.02	0.09	0.00	0.00	24.0
15	0	-2782	-157	293	0	-125	34	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
16	0	-3149	-138	654	0	-209	26	6.28	6.28	9.42	9.42	2	0.02	0.02	0.09	0.00	0.00	24.0
17	0	-2749	-138	288	0	-121	28	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
18	0	-4444	-296	939	0	-317	73	6.28	6.28	9.42	9.42	3	0.02	0.02	0.12	0.00	0.00	24.0
19	0	-4085	-104	862	0	-262	13	6.28	6.28	9.42	9.42	3	0.01	0.02	0.11	0.00	0.00	24.0
20	0	-3954	-199	618	0	-212	43	6.28	6.28	9.42	9.42	3	0.01	0.01	0.08	0.00	0.00	24.0
37	0	-4400	-355	867	0	-309	91	6.28	6.28	9.42	9.42	3	0.02	0.02	0.11	0.00	0.00	24.0
38	0	-3801	-37	738	0	-217	-9	6.28	6.28	9.42	9.42	3	0.01	0.02	0.10	0.00	0.00	24.0
39	0	-3584	-194	332	0	-134	42	6.28	6.28	9.42	9.42	3	0.01	0.01	0.04	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-3782	-192	616	0	-294	15	6.28	6.28	9.42	9.42	3	0.01	0.01	0.08	0.00	0.00	24.0
2	12	-3024	-179	536	0	-254	17	6.28	6.28	9.42	9.42	2	0.02	0.01	0.07	0.00	0.00	24.0
3	12	-2904	-179	427	0	-214	17	6.28	6.28	9.42	9.42	2	0.02	0.01	0.06	0.00	0.00	24.0
4	12	-2915	-116	521	0	-238	5	6.28	6.28	9.42	9.42	2	0.02	0.01	0.07	0.00	0.00	24.0
5	12	-2795	-116	411	0	-198	6	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
6	12	-3126	-157	659	0	-296	12	6.28	6.28	9.42	9.42	2	0.02	0.02	0.09	0.00	0.00	24.0
7	12	-2726	-157	293	0	-162	14	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
8	12	-3093	-138	654	0	-291	9	6.28	6.28	9.42	9.42	2	0.02	0.02	0.09	0.00	0.00	24.0
9	12	-2693	-138	288	0	-157	11	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
10	12	-3024	-179	536	0	-254	17	6.28	6.28	9.42	9.42	2	0.02	0.01	0.07	0.00	0.00	24.0
11	12	-2904	-179	427	0	-214	17	6.28	6.28	9.42	9.42	2	0.02	0.01	0.06	0.00	0.00	24.0
12	12	-2915	-116	521	0	-238	5	6.28	6.28	9.42	9.42	2	0.02	0.01	0.07	0.00	0.00	24.0
13	12	-2795	-116	411	0	-198	6	6.28	6.28	9.42	9.42	2	0.01	0.01	0.05	0.00	0.00	24.0
14	12	-3126	-157	659	0	-296	12	6.28	6.28	9.42	9.42	2	0.02	0.02	0.09	0.00	0.00	24.0
15	12	-2726	-157	293	0	-162	14	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
16	12	-3093	-138	654	0	-291	9	6.28	6.28	9.42	9.42	2	0.02	0.02	0.09	0.00	0.00	24.0
17	12	-2693	-138	288	0	-157	11	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
18	12	-4371	-296	939	0	-434	36	6.28	6.28	9.42	9.42	3	0.02	0.02	0.12	0.00	0.00	24.0
19	12	-4012	-104	862	0	-369	-0	6.28	6.28	9.42	9.42	3	0.02	0.02	0.11	0.00	0.00	24.0
20	12	-3881	-199	618	0	-289	19	6.28	6.28	9.42	9.42	3	0.01	0.01	0.08	0.00	0.00	24.0
37	12	-4327	-355	867	0	-417	47	6.28	6.28	9.42	9.42	3	0.02	0.02	0.11	0.00	0.00	24.0
38	12	-3728	-37	738	0	-309	-13	6.28	6.28	9.42	9.42	3	0.02	0.02	0.10	0.00	0.00	24.0
39	12	-3511	-194	332	0	-176	18	6.28	6.28	9.42	9.42	3	0.01	0.01	0.04	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-3709	-192	616	0	-371	-9	6.28	6.28	9.42	9.42	3	0.02	0.01	0.08	0.00	0.00	24.0
2	25	-2968	-179	536	0	-321	-6	6.28	6.28	9.42	9.42	2	0.02	0.01	0.07	0.00	0.00	24.0
3	25	-2848	-179	427	0	-267	-5	6.28	6.28	9.42	9.42	2	0.02	0.01	0.06	0.00	0.00	24.0
4	25	-2858	-116	521	0	-304	-9	6.28	6.28	9.42	9.42	2	0.02	0.01	0.07	0.00	0.00	24.0
5	25	-2738	-116	411	0	-250	-8	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
6	25	-3070	-157	659	0	-378	-8	6.28	6.28	9.42	9.42	2	0.03	0.02	0.09	0.00	0.00	24.0
7	25	-2670	-157	293	0	-198	-6	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
8	25	-3036	-138	654	0	-373	-9	6.28	6.28	9.42	9.42	2	0.02	0.02	0.09	0.00	0.00	24.0
9	25	-2636	-138	288	0	-193	-7	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0

10	25	-2968	-179	536	0	-321	-6	6.28	6.28	9.42	9.42	2	0.02	0.01	0.07	0.00	0.00	24.0
11	25	-2848	-179	427	0	-267	-5	6.28	6.28	9.42	9.42	2	0.02	0.01	0.06	0.00	0.00	24.0
12	25	-2858	-116	521	0	-304	-9	6.28	6.28	9.42	9.42	2	0.02	0.01	0.07	0.00	0.00	24.0
13	25	-2738	-116	411	0	-250	-8	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
14	25	-3070	-157	659	0	-378	-8	6.28	6.28	9.42	9.42	2	0.03	0.02	0.09	0.00	0.00	24.0
15	25	-2670	-157	293	0	-198	-6	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
16	25	-3036	-138	654	0	-373	-9	6.28	6.28	9.42	9.42	2	0.02	0.02	0.09	0.00	0.00	24.0
17	25	-2636	-138	288	0	-193	-7	6.28	6.28	9.42	9.42	2	0.01	0.01	0.04	0.00	0.00	24.0
18	25	-4298	-296	939	0	-552	-1	6.28	6.28	9.42	9.42	3	0.03	0.02	0.12	0.00	0.00	24.0
19	25	-3938	-104	862	0	-477	-13	6.28	6.28	9.42	9.42	3	0.02	0.02	0.11	0.00	0.00	24.0
20	25	-3808	-199	618	0	-367	-6	6.28	6.28	9.42	9.42	3	0.02	0.01	0.08	0.00	0.00	24.0
37	25	-4254	-355	867	0	-526	3	6.28	6.28	9.42	9.42	3	0.03	0.02	0.11	0.00	0.00	24.0
38	25	-3655	-37	738	0	-401	-18	6.28	6.28	9.42	9.42	3	0.02	0.02	0.10	0.00	0.00	24.0
39	25	-3438	-194	332	0	-217	-6	6.28	6.28	9.42	9.42	3	0.01	0.01	0.04	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-3636	-192	616	0	-448	-33	6.28	6.28	9.42	9.42	3	0.02	0.01	0.08	0.00	0.00	24.0
2	38	-2911	-179	536	0	-388	-28	6.28	6.28	9.42	9.42	2	0.03	0.01	0.07	0.00	0.00	24.0
3	38	-2791	-179	427	0	-321	-27	6.28	6.28	9.42	9.42	2	0.02	0.01	0.06	0.00	0.00	24.0
4	38	-2802	-116	521	0	-369	-24	6.28	6.28	9.42	9.42	2	0.03	0.01	0.07	0.00	0.00	24.0
5	38	-2682	-116	411	0	-301	-23	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
6	38	-3013	-157	659	0	-460	-27	6.28	6.28	9.42	9.42	2	0.03	0.02	0.09	0.00	0.00	24.0
7	38	-2613	-157	293	0	-235	-25	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
8	38	-2980	-138	654	0	-455	-26	6.28	6.28	9.42	9.42	2	0.03	0.02	0.09	0.00	0.00	24.0
9	38	-2580	-138	288	0	-229	-24	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
10	38	-2911	-179	536	0	-388	-28	6.28	6.28	9.42	9.42	2	0.03	0.01	0.07	0.00	0.00	24.0
11	38	-2791	-179	427	0	-321	-27	6.28	6.28	9.42	9.42	2	0.02	0.01	0.06	0.00	0.00	24.0
12	38	-2802	-116	521	0	-369	-24	6.28	6.28	9.42	9.42	2	0.03	0.01	0.07	0.00	0.00	24.0
13	38	-2682	-116	411	0	-301	-23	6.28	6.28	9.42	9.42	2	0.02	0.01	0.05	0.00	0.00	24.0
14	38	-3013	-157	659	0	-460	-27	6.28	6.28	9.42	9.42	2	0.03	0.02	0.09	0.00	0.00	24.0
15	38	-2613	-157	293	0	-235	-25	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
16	38	-2980	-138	654	0	-455	-26	6.28	6.28	9.42	9.42	2	0.03	0.02	0.09	0.00	0.00	24.0
17	38	-2580	-138	288	0	-229	-24	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
18	38	-4225	-296	939	0	-669	-38	6.28	6.28	9.42	9.42	3	0.03	0.02	0.12	0.00	0.00	24.0
19	38	-3865	-104	862	0	-585	-26	6.28	6.28	9.42	9.42	3	0.03	0.02	0.11	0.00	0.00	24.0
20	38	-3734	-199	618	0	-444	-31	6.28	6.28	9.42	9.42	3	0.02	0.01	0.08	0.00	0.00	24.0
37	38	-4181	-355	867	0	-634	-42	6.28	6.28	9.42	9.42	3	0.03	0.02	0.11	0.00	0.00	24.0
38	38	-3582	-37	738	0	-494	-22	6.28	6.28	9.42	9.42	3	0.02	0.02	0.10	0.00	0.00	24.0
39	38	-3364	-194	332	0	-259	-31	6.28	6.28	9.42	9.42	3	0.01	0.01	0.04	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-3563	-192	616	0	-525	-57	6.28	6.28	9.42	9.42	3	0.03	0.01	0.08	0.00	0.00	24.0
2	50	-2855	-179	536	0	-455	-50	6.28	6.28	9.42	9.42	2	0.03	0.01	0.07	0.00	0.00	24.0
3	50	-2735	-179	427	0	-374	-50	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
4	50	-2746	-116	521	0	-434	-38	6.28	6.28	9.42	9.42	2	0.03	0.01	0.07	0.00	0.00	24.0
5	50	-2626	-116	411	0	-352	-38	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
6	50	-2957	-157	659	0	-543	-47	6.28	6.28	9.42	9.42	2	0.04	0.02	0.09	0.00	0.00	24.0
7	50	-2557	-157	293	0	-271	-45	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
8	50	-2924	-138	654	0	-536	-43	6.28	6.28	9.42	9.42	2	0.04	0.02	0.09	0.00	0.00	24.0
9	50	-2524	-138	288	0	-265	-41	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
10	50	-2855	-179	536	0	-455	-50	6.28	6.28	9.42	9.42	2	0.03	0.01	0.07	0.00	0.00	24.0
11	50	-2735	-179	427	0	-374	-50	6.28	6.28	9.42	9.42	2	0.03	0.01	0.06	0.00	0.00	24.0
12	50	-2746	-116	521	0	-434	-38	6.28	6.28	9.42	9.42	2	0.03	0.01	0.07	0.00	0.00	24.0
13	50	-2626	-116	411	0	-352	-38	6.28	6.28	9.42	9.42	2	0.03	0.01	0.05	0.00	0.00	24.0
14	50	-2957	-157	659	0	-543	-47	6.28	6.28	9.42	9.42	2	0.04	0.02	0.09	0.00	0.00	24.0
15	50	-2557	-157	293	0	-271	-45	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
16	50	-2924	-138	654	0	-536	-43	6.28	6.28	9.42	9.42	2	0.04	0.02	0.09	0.00	0.00	24.0
17	50	-2524	-138	288	0	-265	-41	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
18	50	-4152	-296	939	0	-786	-75	6.28	6.28	9.42	9.42	3	0.04	0.02	0.12	0.00	0.00	24.0
19	50	-3792	-104	862	0	-693	-39	6.28	6.28	9.42	9.42	3	0.03	0.02	0.11	0.00	0.00	24.0
20	50	-3661	-199	618	0	-521	-56	6.28	6.28	9.42	9.42	3	0.03	0.01	0.08	0.00	0.00	24.0
37	50	-4108	-355	867	0	-742	-86	6.28	6.28	9.42	9.42	3	0.04	0.02	0.11	0.00	0.00	24.0
38	50	-3509	-37	738	0	-586	-27	6.28	6.28	9.42	9.42	3	0.03	0.02	0.10	0.00	0.00	24.0
39	50	-3291	-194	332	0	-301	-55	6.28	6.28	9.42	9.42	3	0.02	0.01	0.04	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

ASTA NUM. 125 NI 833 NF 209 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 23A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-4887	67	827	0	-602	-71	6.28	6.28	9.42	9.42	3	0.03	0.02	0.11	0.00	0.00	24.0
2	0	-3876	-9	760	0	-528	-65	6.28	6.28	9.42	9.42	2	0.04	0.02	0.10	0.00	0.00	24.0
3	0	-3769	-17	563	0	-431	-65	6.28	6.28	9.42	9.42	2	0.03	0.01	0.07	0.00	0.00	24.0
4	0	-3749	120	709	0	-495	-44	6.28	6.28	9.42	9.42	2	0.03	0.02	0.09	0.00	0.00	24.0
5	0	-3642	113	512	0	-397	-44	6.28	6.28	9.42	9.42	2	0.03	0.01	0.07	0.00	0.00	24.0
6	0	-3956	44	973	0	-630	-58	6.28	6.28	9.42	9.42	2	0.04	0.02	0.13	0.00	0.00	24.0
7	0	-3600	20	314	0	-306	-57	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
8	0	-3918	83	958	0	-620	-52	6.28	6.28	9.42	9.42	2	0.04	0.02	0.12	0.00	0.00	24.0
9	0	-3562	59	299	0	-296	-51	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
10	0	-3876	-9	760	0	-528	-65	6.28	6.28	9.42	9.42	2	0.04	0.02	0.10	0.00	0.00	24.0
11	0	-3769	-17	563	0	-431	-65	6.28	6.28	9.42	9.42	2	0.03	0.01	0.07	0.00	0.00	24.0
12	0	-3749	120	709	0	-495	-44	6.28	6.28	9.42	9.42	2	0.03	0.02	0.09	0.00	0.00	24.0
13	0	-3642	113	512	0	-397	-44	6.28	6.28	9.42	9.42	2	0.03	0.01	0.07	0.00	0.00	24.0
14	0	-3956	44	973	0	-630	-58	6.28	6.28	9.42	9.42	2	0.04	0.02	0.13	0.00	0.00	24.0
15	0	-3600	20	314	0	-306	-57	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
16	0	-3918	83	958	0	-620	-52	6.28	6.28	9.42	9.42	2	0.04	0.02	0.12	0.00	0.00	24.0
17	0	-3562	59	299	0	-296	-51	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
18	0	-5550	-73	1434	0	-926	-106	6.28	6.28	9.42	9.42	3	0.05	0.03	0.18	0.00	0.00	24.0
19	0	-5136	302	1211	0	-791	-43	6.28	6.28	9.42	9.42	3	0.04	0.03	0.15	0.00	0.00	24.0
20	0	-5068	85	799	0	-600	-75	6.28	6.28	9.42	9.42	3	0.03	0.02	0.10	0.00	0.00	24.0
37	0	-5499	-214	1338	0	-881	-125	6.28	6.28	9.42	9.42	3	0.04	0.03	0.17	0.00	0.00	24.0
38	0	-4809	410	968	0	-657	-21	6.28	6.28	9.42	9.42	3	0.03	0.02	0.12	0.00	0.00	24.0
39	0	-4697	49	280	0	-338	-74	6.28	6.28	9.42	9.42	3	0.02	0.01	0.04	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	12	-4814	67	827	0	-705	-62	6.28	6.28	9.42	9.42	3	0.03	0.02	0.11	0.00	0.00	24.0
2	12	-3820	-9	760	0	-623	-66	6.28	6.28	9.42	9.42	2	0.04	0.02	0.10	0.00	0.00	24.0
3	12	-3713	-17	563	0	-501	-67	6.28	6.28	9.42	9.42	2	0.04	0.01	0.07	0.00	0.00	24.0
4	12	-3693	120	709	0	-583	-29	6.28	6.28	9.42	9.42	2	0.04	0.02	0.09	0.00	0.00	24.0
5	12	-3586	113	512	0	-461	-30	6.28	6.28	9.42	9.42	2	0.03	0.01	0.07	0.00	0.00	24.0

6	12	-3900	44	973	0	-752	-53	6.28	6.28	9.42	9.42	2	0.05	0.02	0.13	0.00	0.00	24.0
7	12	-3544	20	314	0	-345	-54	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
8	12	-3862	83	958	0	-740	-42	6.28	6.28	9.42	9.42	2	0.05	0.02	0.12	0.00	0.00	24.0
9	12	-3506	59	299	0	-333	-43	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
10	12	-3820	-9	760	0	-623	-66	6.28	6.28	9.42	9.42	2	0.04	0.02	0.10	0.00	0.00	24.0
11	12	-3713	-17	563	0	-501	-67	6.28	6.28	9.42	9.42	2	0.04	0.01	0.07	0.00	0.00	24.0
12	12	-3693	120	709	0	-583	-29	6.28	6.28	9.42	9.42	2	0.04	0.02	0.09	0.00	0.00	24.0
13	12	-3586	113	512	0	-461	-30	6.28	6.28	9.42	9.42	2	0.03	0.01	0.07	0.00	0.00	24.0
14	12	-3900	44	973	0	-752	-53	6.28	6.28	9.42	9.42	2	0.05	0.02	0.13	0.00	0.00	24.0
15	12	-3544	20	314	0	-345	-54	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
16	12	-3862	83	958	0	-740	-42	6.28	6.28	9.42	9.42	2	0.05	0.02	0.12	0.00	0.00	24.0
17	12	-3506	59	299	0	-333	-43	6.28	6.28	9.42	9.42	2	0.02	0.01	0.04	0.00	0.00	24.0
18	12	-5477	-73	1434	0	-1105	-115	6.28	6.28	9.42	9.42	3	0.05	0.03	0.18	0.00	0.00	24.0
19	12	-5063	302	1211	0	-942	-5	6.28	6.28	9.42	9.42	3	0.05	0.03	0.15	0.00	0.00	24.0
20	12	-4995	85	799	0	-699	-64	6.28	6.28	9.42	9.42	3	0.03	0.02	0.10	0.00	0.00	24.0
37	12	-5426	-214	1338	0	-1049	-152	6.28	6.28	9.42	9.42	3	0.05	0.03	0.17	0.00	0.00	24.0
38	12	-4736	410	968	0	-778	31	6.28	6.28	9.42	9.42	3	0.04	0.02	0.12	0.00	0.00	24.0
39	12	-4624	49	280	0	-373	-68	6.28	6.28	9.42	9.42	3	0.02	0.01	0.04	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	25	-4740	67	827	0	-808	-54	6.28	6.28	9.42	9.42	3	0.04	0.02	0.11	0.00	0.00	24.0
2	25	-3764	-9	760	0	-718	-67	6.28	6.28	9.42	9.42	2	0.05	0.02	0.10	0.00	0.00	24.0
3	25	-3656	-17	563	0	-572	-69	6.28	6.28	9.42	9.42	2	0.04	0.01	0.07	0.00	0.00	24.0
4	25	-3636	120	709	0	-672	-14	6.28	6.28	9.42	9.42	2	0.04	0.02	0.09	0.00	0.00	24.0
5	25	-3530	113	512	0	-525	-16	6.28	6.28	9.42	9.42	2	0.04	0.01	0.07	0.00	0.00	24.0
6	25	-3844	44	973	0	-874	-47	6.28	6.28	9.42	9.42	2	0.06	0.02	0.13	0.00	0.00	24.0
7	25	-3488	20	314	0	-384	-52	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
8	25	-3806	83	958	0	-860	-31	6.28	6.28	9.42	9.42	2	0.06	0.02	0.12	0.00	0.00	24.0
9	25	-3450	59	299	0	-370	-36	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
10	25	-3764	-9	760	0	-718	-67	6.28	6.28	9.42	9.42	2	0.05	0.02	0.10	0.00	0.00	24.0
11	25	-3656	-17	563	0	-572	-69	6.28	6.28	9.42	9.42	2	0.04	0.01	0.07	0.00	0.00	24.0
12	25	-3636	120	709	0	-672	-14	6.28	6.28	9.42	9.42	2	0.04	0.02	0.09	0.00	0.00	24.0
13	25	-3530	113	512	0	-525	-16	6.28	6.28	9.42	9.42	2	0.04	0.01	0.07	0.00	0.00	24.0
14	25	-3844	44	973	0	-874	-47	6.28	6.28	9.42	9.42	2	0.06	0.02	0.13	0.00	0.00	24.0
15	25	-3488	20	314	0	-384	-52	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
16	25	-3806	83	958	0	-860	-31	6.28	6.28	9.42	9.42	2	0.06	0.02	0.12	0.00	0.00	24.0
17	25	-3450	59	299	0	-370	-36	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
18	25	-5404	-73	1434	0	-1284	-124	6.28	6.28	9.42	9.42	3	0.06	0.03	0.18	0.00	0.00	24.0
19	25	-4990	302	1211	0	-1094	32	6.28	6.28	9.42	9.42	3	0.05	0.03	0.15	0.00	0.00	24.0
20	25	-4922	85	799	0	-799	-54	6.28	6.28	9.42	9.42	3	0.04	0.02	0.10	0.00	0.00	24.0
37	25	-5353	-214	1338	0	-1216	-179	6.28	6.28	9.42	9.42	3	0.06	0.03	0.17	0.00	0.00	24.0
38	25	-4663	410	968	0	-899	82	6.28	6.28	9.42	9.42	3	0.04	0.02	0.12	0.00	0.00	24.0
39	25	-4550	49	280	0	-408	-62	6.28	6.28	9.42	9.42	3	0.02	0.01	0.04	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	38	-4667	67	827	0	-912	-46	6.28	6.28	9.42	9.42	3	0.04	0.02	0.11	0.00	0.00	24.0
2	38	-3707	-9	760	0	-814	-69	6.28	6.28	9.42	9.42	2	0.06	0.02	0.10	0.00	0.00	24.0
3	38	-3600	-17	563	0	-642	-71	6.28	6.28	9.42	9.42	2	0.05	0.01	0.07	0.00	0.00	24.0
4	38	-3580	120	709	0	-761	1	6.28	6.28	9.42	9.42	2	0.05	0.02	0.09	0.00	0.00	24.0
5	38	-3473	113	512	0	-589	-1	6.28	6.28	9.42	9.42	2	0.04	0.01	0.07	0.00	0.00	24.0
6	38	-3787	44	973	0	-995	-42	6.28	6.28	9.42	9.42	2	0.07	0.02	0.13	0.00	0.00	24.0
7	38	-3431	20	314	0	-423	-49	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
8	38	-3749	83	958	0	-979	-21	6.28	6.28	9.42	9.42	2	0.06	0.02	0.12	0.00	0.00	24.0
9	38	-3393	59	299	0	-407	-29	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
10	38	-3707	-9	760	0	-814	-69	6.28	6.28	9.42	9.42	2	0.06	0.02	0.10	0.00	0.00	24.0
11	38	-3600	-17	563	0	-642	-71	6.28	6.28	9.42	9.42	2	0.05	0.01	0.07	0.00	0.00	24.0
12	38	-3580	120	709	0	-761	1	6.28	6.28	9.42	9.42	2	0.05	0.02	0.09	0.00	0.00	24.0
13	38	-3473	113	512	0	-589	-1	6.28	6.28	9.42	9.42	2	0.04	0.01	0.07	0.00	0.00	24.0
14	38	-3787	44	973	0	-995	-42	6.28	6.28	9.42	9.42	2	0.07	0.02	0.13	0.00	0.00	24.0
15	38	-3431	20	314	0	-423	-49	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
16	38	-3749	83	958	0	-979	-21	6.28	6.28	9.42	9.42	2	0.06	0.02	0.12	0.00	0.00	24.0
17	38	-3393	59	299	0	-407	-29	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
18	38	-5330	-73	1434	0	-1464	-133	6.28	6.28	9.42	9.42	3	0.07	0.03	0.18	0.00	0.00	24.0
19	38	-4916	302	1211	0	-1246	70	6.28	6.28	9.42	9.42	3	0.06	0.03	0.15	0.00	0.00	24.0
20	38	-4849	85	799	0	-899	-43	6.28	6.28	9.42	9.42	3	0.04	0.02	0.10	0.00	0.00	24.0
37	38	-5280	-214	1338	0	-1384	-206	6.28	6.28	9.42	9.42	3	0.07	0.03	0.17	0.00	0.00	24.0
38	38	-4590	410	968	0	-1020	133	6.28	6.28	9.42	9.42	3	0.05	0.02	0.12	0.00	0.00	24.0
39	38	-4477	49	280	0	-443	-55	6.28	6.28	9.42	9.42	3	0.02	0.01	0.04	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

1	50	-4594	67	827	0	-1015	-37	6.28	6.28	9.42	9.42	3	0.05	0.02	0.11	0.00	0.00	24.0
2	50	-3651	-9	760	0	-909	-70	6.28	6.28	9.42	9.42	2	0.06	0.02	0.10	0.00	0.00	24.0
3	50	-3544	-17	563	0	-712	-73	6.28	6.28	9.42	9.42	2	0.05	0.01	0.07	0.00	0.00	24.0
4	50	-3524	120	709	0	-849	16	6.28	6.28	9.42	9.42	2	0.06	0.02	0.09	0.00	0.00	24.0
5	50	-3417	113	512	0	-653	13	6.28	6.28	9.42	9.42	2	0.04	0.01	0.07	0.00	0.00	24.0
6	50	-3731	44	973	0	-1117	-36	6.28	6.28	9.42	9.42	2	0.07	0.02	0.13	0.00	0.00	24.0
7	50	-3375	20	314	0	-463	-47	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
8	50	-3693	83	958	0	-1099	-10	6.28	6.28	9.42	9.42	2	0.07	0.02	0.12	0.00	0.00	24.0
9	50	-3337	59	299	0	-445	-21	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
10	50	-3651	-9	760	0	-909	-70	6.28	6.28	9.42	9.42	2	0.06	0.02	0.10	0.00	0.00	24.0
11	50	-3544	-17	563	0	-712	-73	6.28	6.28	9.42	9.42	2	0.05	0.01	0.07	0.00	0.00	24.0
12	50	-3524	120	709	0	-849	16	6.28	6.28	9.42	9.42	2	0.06	0.02	0.09	0.00	0.00	24.0
13	50	-3417	113	512	0	-653	13	6.28	6.28	9.42	9.42	2	0.04	0.01	0.07	0.00	0.00	24.0
14	50	-3731	44	973	0	-1117	-36	6.28	6.28	9.42	9.42	2	0.07	0.02	0.13	0.00	0.00	24.0
15	50	-3375	20	314	0	-463	-47	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
16	50	-3693	83	958	0	-1099	-10	6.28	6.28	9.42	9.42	2	0.07	0.02	0.12	0.00	0.00	24.0
17	50	-3337	59	299	0	-445	-21	6.28	6.28	9.42	9.42	2	0.03	0.01	0.04	0.00	0.00	24.0
18	50	-5257	-73	1434	0	-1643	-142	6.28	6.28	9.42	9.42	3	0.08	0.03	0.18	0.00	0.00	24.0
19	50	-4843	302	1211	0	-1397	108	6.28	6.28	9.42	9.42	3	0.07	0.03	0.15	0.00	0.00	24.0
20	50	-4776	85	799	0	-999	-32	6.28	6.28	9.42	9.42	3	0.05	0.02	0.10	0.00	0.00	24.0
37	50	-5207	-214	1338	0	-1551	-232	6.28	6.28	9.42	9.42	3	0.08	0.03	0.17	0.00	0.00	24.0
38	50	-4517	410	968	0	-1141	184	6.28	6.28	9.42	9.42	3	0.06	0.02	0.12	0.00	0.00	24.0
39	50	-4404	49	280	0	-478	-49	6.28	6.28	9.42	9.42	3	0.02	0.01	0.04	0.00	0.00	24.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14) staffe= 2 d 8 / 24.0

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Lavoro: **D2403a** Intestazione lavoro: **Palestra Campobello**
Elemento: **PILASTRO** Gruppo: **2** Tabella: **Tabella pilastri**
Descrizione: **Pilastri**
Rck: **350.00** daN/cm^2 fyk: **4580.0** daN/cm^2 Condizioni ambientali: **Ordinaria**
Copriferro di calcolo: **5.0** cm Copriferro di disegno: **4.0** cm
Diametro staffe: **8** mm Numero braccia: **2**
ρ min.: **1.000** %

ASTA NUM. 1 NI 32 NF 26 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 32C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-1225	1008	185	0	868	-985	6.28	6.28	9.42	9.42	-15.43	413.2
41	0	-910	942	402	0	977	-1078	6.28	6.28	9.42	9.42	-16.82	474.7
42	0	-496	963	773	0	1173	-1094	6.28	6.28	9.42	9.42	-16.98	504.1
43	0	-1084	1050	72	0	810	-956	6.28	6.28	9.42	9.42	-14.97	406.8
44	0	-482	834	760	0	1156	-1233	6.28	6.28	9.42	9.42	-19.13	572.2
45	0	130	974	1052	0	1318	-1138	6.28	6.28	9.42	9.42	-17.52	558.6
46	0	-349	936	455	0	999	-1133	6.28	6.28	9.42	9.42	-17.56	530.7
47	0	-209	934	468	0	1005	-1147	6.28	6.28	9.42	9.42	-17.74	544.9
49	0	-314	957	395	0	969	-1115	6.28	6.28	9.42	9.42	-17.27	523.9
50	0	-193	914	533	0	1038	-1171	6.28	6.28	9.42	9.42	-18.11	557.4
51	0	-71	942	591	0	1070	-1152	6.28	6.28	9.42	9.42	-17.79	554.7
apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)													
40	83	-854	939	185	0	716	-181	6.28	6.28	9.42	9.42	-5.51	165.3
41	83	-539	942	402	0	645	-301	6.28	6.28	9.42	9.42	-4.91	165.1
42	83	-125	963	620	0	598	-300	6.28	6.28	9.42	9.42	-4.65	180.3
43	83	-713	935	72	0	750	-138	6.28	6.28	9.42	9.42	-5.73	185.9
44	83	-111	949	760	0	529	-497	6.28	6.28	9.42	9.42	-7.70	235.3
45	83	501	974	798	0	554	-335	6.28	6.28	9.42	9.42	-5.02	214.0
46	83	22	936	455	0	624	-361	6.28	6.28	9.42	9.42	-5.56	199.4
47	83	162	934	468	0	619	-376	6.28	6.28	9.42	9.42	-5.76	208.3
49	83	57	934	395	0	642	-335	6.28	6.28	9.42	9.42	-5.16	207.9
50	83	178	937	533	0	598	-408	6.28	6.28	9.42	9.42	-6.24	207.1
51	83	300	942	541	0	603	-375	6.28	6.28	9.42	9.42	-5.71	213.8
apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)													
40	165	-482	871	185	0	564	566	6.28	6.28	9.42	9.42	-8.83	248.8
41	165	-167	942	402	0	313	476	6.28	6.28	9.42	9.42	-7.37	221.6
42	165	246	963	468	0	150	494	6.28	6.28	9.42	9.42	-7.57	252.8
43	165	-342	820	72	0	690	586	6.28	6.28	9.42	9.42	-9.11	266.0
44	165	261	1064	760	0	-98	333	6.28	6.28	9.42	9.42	-5.06	175.3
45	165	872	974	544	0	0	468	6.28	6.28	9.42	9.42	-6.96	273.9
46	165	393	936	455	0	249	411	6.28	6.28	9.42	9.42	-6.23	220.3
47	165	534	934	468	0	233	395	6.28	6.28	9.42	9.42	-5.94	220.2
49	165	429	911	395	0	316	425	6.28	6.28	9.42	9.42	-6.45	229.2
50	165	549	959	533	0	159	375	6.28	6.28	9.42	9.42	-5.62	211.2
51	165	671	942	490	0	178	402	6.28	6.28	9.42	9.42	-6.00	230.8
apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)													
40	248	-111	802	185	0	412	1256	6.28	6.28	9.42	9.42	-19.40	602.8
41	248	204	942	402	0	-18	1252	6.28	6.28	9.42	9.42	-19.27	617.9
42	248	617	963	316	0	-173	1289	6.28	6.28	9.42	9.42	-19.72	657.7
43	248	30	706	72	0	631	1215	6.28	6.28	9.42	9.42	-18.74	590.7
44	248	632	1178	760	0	-724	1258	6.28	6.28	9.42	9.42	-19.24	643.3
45	248	1244	974	291	0	-344	1271	6.28	6.28	9.42	9.42	-19.27	682.8
46	248	765	936	455	0	-126	1183	6.28	6.28	9.42	9.42	-18.05	614.3
47	248	905	934	468	0	-153	1166	6.28	6.28	9.42	9.42	-17.75	613.6
49	248	800	888	395	0	-10	1167	6.28	6.28	9.42	9.42	-17.80	608.5
50	248	921	982	533	0	-281	1176	6.28	6.28	9.42	9.42	-17.90	619.3
51	248	1043	942	439	0	-205	1178	6.28	6.28	9.42	9.42	-17.90	627.0
apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)													
40	330	260	733	185	0	259	1889	6.28	6.28	9.42	9.42	-29.08	929.6
41	330	575	942	402	0	-350	2029	6.28	6.28	9.42	9.42	-31.16	1014.2
42	330	989	963	163	0	-371	2083	6.28	6.28	9.42	9.42	-31.88	1062.5
43	330	401	591	72	0	571	1750	6.28	6.28	9.42	9.42	-26.90	869.7
44	330	1003	1293	760	0	-1351	2277	6.28	6.28	9.42	9.42	-34.87	1157.3
45	330	1615	974	37	0	-479	2074	6.28	6.28	9.42	9.42	-31.57	1091.8
46	330	1136	936	455	0	-502	1955	6.28	6.28	9.42	9.42	-29.87	1008.4
47	330	1276	934	468	0	-539	1937	6.28	6.28	9.42	9.42	-29.55	1007.2
49	330	1171	865	395	0	-336	1890	6.28	6.28	9.42	9.42	-28.85	978.7
50	330	1292	1005	533	0	-721	1996	6.28	6.28	9.42	9.42	-30.46	1036.6
51	330	1414	942	388	0	-546	1955	6.28	6.28	9.42	9.42	-29.79	1023.3
apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)													

ASTA NUM. 2 NI 33 NF 32 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 32B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	

40	0	-7177	150	167	0	-10	-123	6.28	6.28	9.42	9.42	-4.58	-63.0
41	0	-6882	10	171	0	40	-17	6.28	6.28	9.42	9.42	-3.64	-54.2
42	0	-6526	-4	656	0	515	15	6.28	6.28	9.42	9.42	-5.63	-78.6
43	0	-7007	265	175	0	-2	-232	6.28	6.28	9.42	9.42	-5.50	-71.8
44	0	-6491	-226	177	0	122	166	6.28	6.28	9.42	9.42	-4.65	-62.0
45	0	-5921	9	989	0	872	-2	6.28	6.28	9.42	9.42	-7.09	-95.9
46	0	-6294	47	186	0	105	-79	6.28	6.28	9.42	9.42	-3.75	-53.4
47	0	-6147	56	190	0	121	-94	6.28	6.28	9.42	9.42	-3.82	-53.3
49	0	-6246	102	189	0	104	-130	6.28	6.28	9.42	9.42	-4.19	-56.9
50	0	-6143	4	190	0	129	-50	6.28	6.28	9.42	9.42	-3.68	-53.7
51	0	-6029	51	352	0	279	-83	6.28	6.28	9.42	9.42	-4.31	-61.4

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	110	-6682	80	167	0	-194	3	6.28	6.28	9.42	9.42	-4.24	-61.5
41	110	-6387	10	171	0	-148	-6	6.28	6.28	9.42	9.42	-3.89	-56.6
42	110	-6031	-4	453	0	-95	11	6.28	6.28	9.42	9.42	-3.47	-50.9
43	110	-6512	150	175	0	-195	-4	6.28	6.28	9.42	9.42	-4.16	-60.2
44	110	-5996	-110	177	0	-73	-19	6.28	6.28	9.42	9.42	-3.35	-49.4
45	110	-5426	9	651	0	-30	8	6.28	6.28	9.42	9.42	-2.86	-42.6
46	110	-5799	47	186	0	-100	-27	6.28	6.28	9.42	9.42	-3.37	-49.5
47	110	-5652	56	190	0	-88	-33	6.28	6.28	9.42	9.42	-3.25	-47.7
49	110	-5751	79	189	0	-104	-29	6.28	6.28	9.42	9.42	-3.37	-49.3
50	110	-5648	27	190	0	-79	-32	6.28	6.28	9.42	9.42	-3.20	-47.1
51	110	-5534	51	284	0	-71	-27	6.28	6.28	9.42	9.42	-3.11	-45.8

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	220	-6187	11	167	0	-378	54	6.28	6.28	9.42	9.42	-4.83	-68.2
41	220	-5892	10	171	0	-336	6	6.28	6.28	9.42	9.42	-4.49	-63.6
42	220	-5536	-4	250	0	-481	6	6.28	6.28	9.42	9.42	-4.98	-69.2
43	220	-6017	34	175	0	-387	97	6.28	6.28	9.42	9.42	-4.79	-67.4
44	220	-5501	5	177	0	-268	-76	6.28	6.28	9.42	9.42	-3.99	-56.8
45	220	-4931	9	312	0	-559	18	6.28	6.28	9.42	9.42	-5.03	-69.1
46	220	-5304	47	186	0	-306	24	6.28	6.28	9.42	9.42	-4.06	-57.4
47	220	-5157	56	190	0	-298	29	6.28	6.28	9.42	9.42	-3.95	-55.9
49	220	-5256	56	189	0	-312	45	6.28	6.28	9.42	9.42	-4.07	-57.4
50	220	-5153	50	190	0	-288	10	6.28	6.28	9.42	9.42	-3.91	-55.3
51	220	-5039	51	217	0	-346	29	6.28	6.28	9.42	9.42	-4.11	-57.8

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	330	-5692	-58	167	0	-562	28	6.28	6.28	9.42	9.42	-5.42	-75.0
41	330	-5397	10	171	0	-524	17	6.28	6.28	9.42	9.42	-5.10	-70.6
42	330	-5041	-4	47	0	-644	2	6.28	6.28	9.42	9.42	-5.50	-75.0
43	330	-5522	-81	175	0	-579	71	6.28	6.28	9.42	9.42	-5.42	-74.7
44	330	-5006	121	177	0	-463	-7	6.28	6.28	9.42	9.42	-4.63	-64.1
45	330	-4436	9	-26	0	-716	28	6.28	6.28	9.42	9.42	-5.69	-76.4
46	330	-4809	47	186	0	-511	76	6.28	6.28	9.42	9.42	-4.75	-65.4
47	330	-4662	56	190	0	-507	91	6.28	6.28	9.42	9.42	-4.66	-64.1
49	330	-4761	33	189	0	-520	94	6.28	6.28	9.42	9.42	-4.77	-65.6
50	330	-4658	74	190	0	-497	79	6.28	6.28	9.42	9.42	-4.61	-63.5
51	330	-4544	51	149	0	-547	86	6.28	6.28	9.42	9.42	-4.79	-65.6

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	440	-5197	-128	167	0	-746	-75	6.28	6.28	9.42	9.42	-6.11	-82.7
41	440	-4902	10	171	0	-712	28	6.28	6.28	9.42	9.42	-5.81	-78.6
42	440	-4546	-4	-157	0	-584	-3	6.28	6.28	9.42	9.42	-4.97	-67.8
43	440	-5027	-197	175	0	-771	-81	6.28	6.28	9.42	9.42	-6.20	-83.6
44	440	-4511	236	177	0	-657	189	6.28	6.28	9.42	9.42	-5.36	-72.5
45	440	-3941	9	-365	0	-501	38	6.28	6.28	9.42	9.42	-4.28	-58.5
46	440	-4314	47	186	0	-716	128	6.28	6.28	9.42	9.42	-5.66	-75.7
47	440	-4167	56	190	0	-717	153	6.28	6.28	9.42	9.42	-5.63	-75.1
49	440	-4266	10	189	0	-728	118	6.28	6.28	9.42	9.42	-5.72	-76.4
50	440	-4163	97	190	0	-705	172	6.28	6.28	9.42	9.42	-5.55	-74.2
51	440	-4049	51	81	0	-674	142	6.28	6.28	9.42	9.42	-5.32	-71.2

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 3 NI 27 NF 25 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 7C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	--												
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	4909	-563	794	0	1160	1030	6.28	6.28	9.42	9.42	-13.88	768.9
41	0	4713	-758	691	0	1076	1053	6.28	6.28	9.42	9.42	-14.37	768.9
42	0	5333	-775	1094	0	1198	1064	6.28	6.28	9.42	9.42	-14.18	809.0
43	0	4945	-443	838	0	1221	1043	6.28	6.28	9.42	9.42	-14.07	780.4
44	0	4331	-1089	520	0	934	1092	6.28	6.28	9.42	9.42	-15.20	766.2
45	0	5653	-796	1337	0	1284	1099	6.28	6.28	9.42	9.42	-14.56	857.8
46	0	4562	-774	651	0	1083	1096	6.28	6.28	9.42	9.42	-15.14	781.1
47	0	4524	-777	641	0	1085	1107	6.28	6.28	9.42	9.42	-15.34	784.2
49	0	4589	-712	676	0	1113	1100	6.28	6.28	9.42	9.42	-15.19	784.5
50	0	4466	-842	612	0	1056	1110	6.28	6.28	9.42	9.42	-15.42	782.4
51	0	4731	-783	775	0	1126	1111	6.28	6.28	9.42	9.42	-15.29	797.7

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	83	5280	-689	794	0	505	513	6.28	6.28	9.42	9.42	-4.49	580.9
41	83	5084	-758	691	0	506	427	6.28	6.28	9.42	9.42	-2.82	565.7
42	83	5704	-775	942	0	359	424	6.28	6.28	9.42	9.42	-1.68	568.1
43	83	5316	-652	838	0	529	591	6.28	6.28	9.42	9.42	-6.00	591.5
44	83	4702	-879	520	0	505	280	6.28	6.28	9.42	9.42	0.00	534.9
45	83	6024	-796	1083	0	286	442	6.28	6.28	9.42	9.42	-1.59	570.4
46	83	4933	-774	651	0	546	458	6.28	6.28	9.42	9.42	-3.72	566.4
47	83	4895	-777	641	0	556	466	6.28	6.28	9.42	9.42	-3.94	566.5
49	83	4960	-754	676	0	556	495	6.28	6.28	9.42	9.42	-4.48	571.5
50	83	4837	-800	612	0	551	433	6.28	6.28	9.42	9.42	-3.30	560.3
51	83	5102	-783	725	0	507	465	6.28	6.28	9.42	9.42	-3.67	567.5

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	165	5652	-815	794	0	-150	-107	6.28	6.28	9.42	9.42	0.00	497.6
41	165	5456	-758	691	0	-64	-198	6.28	6.28	9.42	9.42	0.00	454.5
42	165	6076	-775	789	0	-355	-216	6.28	6.28	9.42	9.42	0.00	596.4
43	165	5688	-862	838	0	-162	-34	6.28	6.28	9.42	9.42	0.00	504.3
44	165	5074	-670	520	0	76	-359	6.28	6.28	9.42	9.42	-0.88	459.0
45	165	6396	-796	829	0	-503	-214	6.28	6.28	9.42	9.42	0.00	669.0
46	165	5304	-774	651	0	9	-180	6.28	6.28	9.42	9.42	0.00	425.0
47	165	5266	-777	641	0	27	-176	6.28	6.28	9.42	9.42	0.00	427.7
49	165	5332	-796	676	0	-2	-145	6.28	6.28	9.42	9.42	0.00	424.9
50	165	5208	-758	612	0	46	-210	6.28	6.28	9.42	9.42	0.00	429.1
51	165	5474	-783	674	0	-70	-181	6.28	6.28	9.42	9.42	0.00	457.8

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	248	6023	-940	794	0	-806	-831	6.28	6.28	9.42	9.42	-9.75	737.2
41	248	5827	-758	691	0	-634	-824	6.28	6.28	9.42	9.42	-9.79	722.8
42	248	6447	-775	637	0	-943	-855	6.28	6.28	9.42	9.42	-9.83	813.1
43	248	6059	-1072	838	0	-854	-831	6.28	6.28	9.42	9.42	-9.73	754.1
44	248	5445	-460	520	0	-354	-825	6.28	6.28	9.42	9.42	-10.10	701.3
45	248	6767	-796	575	0	-1082	-871	6.28	6.28	9.42	9.42	-9.84	883.0
46	248	5676	-774	651	0	-528	-819	6.28	6.28	9.42	9.42	-9.81	711.6
47	248	5638	-777	641	0	-502	-817	6.28	6.28	9.42	9.42	-9.81	708.4
49	248	5703	-838	676	0	-560	-819	6.28	6.28	9.42	9.42	-9.80	713.3
50	248	5580	-716	612	0	-459	-818	6.28	6.28	9.42	9.42	-9.87	705.6
51	248	5845	-783	623	0	-605	-827	6.28	6.28	9.42	9.42	-9.82	725.1

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	330	6394	-1066	794	0	-1461	-1659	6.28	6.28	9.42	9.42	-23.20	1153.7
41	330	6198	-758	691	0	-1204	-1450	6.28	6.28	9.42	9.42	-19.95	1042.5
42	330	6818	-775	484	0	-1405	-1495	6.28	6.28	9.42	9.42	-20.32	1098.8
43	330	6430	-1281	838	0	-1546	-1802	6.28	6.28	9.42	9.42	-25.46	1224.4
44	330	5816	-251	520	0	-783	-1118	6.28	6.28	9.42	9.42	-14.77	862.1
45	330	7138	-796	321	0	-1452	-1528	6.28	6.28	9.42	9.42	-20.67	1132.6
46	330	6047	-774	651	0	-1065	-1457	6.28	6.28	9.42	9.42	-20.14	1037.4
47	330	6009	-777	641	0	-1031	-1458	6.28	6.28	9.42	9.42	-20.18	1035.7
49	330	6074	-880	676	0	-1117	-1528	6.28	6.28	9.42	9.42	-21.27	1072.9
50	330	5951	-674	612	0	-964	-1391	6.28	6.28	9.42	9.42	-19.13	1000.3
51	330	6216	-783	572	0	-1098	-1473	6.28	6.28	9.42	9.42	-20.31	1054.5

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 4 NI 23 NF 27 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 7B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-1289	140	345	0	527	62	6.28	6.28	9.42	9.42	-4.11	79.5
41	0	-1420	-133	307	0	404	274	6.28	6.28	9.42	9.42	-4.34	63.4
42	0	-851	-124	805	0	895	257	6.28	6.28	9.42	9.42	-6.84	221.6
43	0	-1265	310	366	0	612	-65	6.28	6.28	9.42	9.42	-4.77	106.1
44	0	-1702	-586	244	0	196	628	6.28	6.28	9.42	9.42	-9.94	217.2
45	0	-536	-131	1132	0	1224	261	6.28	6.28	9.42	9.42	-9.16	348.2
46	0	-1523	-152	299	0	407	300	6.28	6.28	9.42	9.42	-4.74	70.5
47	0	-1549	-157	297	0	408	306	6.28	6.28	9.42	9.42	-4.84	72.3
49	0	-1505	-66	310	0	449	235	6.28	6.28	9.42	9.42	-3.69	46.1
50	0	-1592	-245	285	0	366	374	6.28	6.28	9.42	9.42	-5.92	101.6
51	0	-1359	-154	463	0	572	300	6.28	6.28	9.42	9.42	-4.76	88.4

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	110	-794	13	345	0	148	146	6.28	6.28	9.42	9.42	-2.30	32.0
41	110	-925	-133	307	0	66	128	6.28	6.28	9.42	9.42	-2.01	-20.2
42	110	-356	-124	602	0	121	120	6.28	6.28	9.42	9.42	-1.90	40.1
43	110	-770	99	366	0	210	160	6.28	6.28	9.42	9.42	-2.54	39.7
44	110	-1207	-375	244	0	-72	99	6.28	6.28	9.42	9.42	-1.57	-18.3
45	110	-41	-131	793	0	165	118	6.28	6.28	9.42	9.42	-1.83	54.9
46	110	-1028	-152	299	0	78	133	6.28	6.28	9.42	9.42	-2.07	-21.3
47	110	-1054	-157	297	0	81	134	6.28	6.28	9.42	9.42	-2.09	-21.6
49	110	-1010	-108	310	0	109	140	6.28	6.28	9.42	9.42	-2.18	-22.0
50	110	-1097	-203	285	0	52	127	6.28	6.28	9.42	9.42	-1.98	-21.1
51	110	-864	-154	395	0	100	131	6.28	6.28	9.42	9.42	-2.06	22.7

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	220	-299	-113	345	0	-232	91	6.28	6.28	9.42	9.42	-1.79	52.0
41	220	-430	-133	307	0	-272	-18	6.28	6.28	9.42	9.42	-2.11	55.5
42	220	139	-124	399	0	-430	-17	6.28	6.28	9.42	9.42	-3.06	146.6
43	220	-275	-112	366	0	-192	153	6.28	6.28	9.42	9.42	-2.41	59.9
44	220	-712	-164	244	0	-340	-197	6.28	6.28	9.42	9.42	-3.13	59.6
45	220	454	-131	455	0	-522	-26	6.28	6.28	9.42	9.42	-3.54	199.9
46	220	-533	-152	299	0	-250	-35	6.28	6.28	9.42	9.42	-1.95	42.4
47	220	-559	-157	297	0	-245	-39	6.28	6.28	9.42	9.42	-1.91	39.3
49	220	-515	-150	310	0	-232	-2	6.28	6.28	9.42	9.42	-1.81	38.0
50	220	-602	-161	285	0	-261	-72	6.28	6.28	9.42	9.42	-2.04	41.6
51	220	-369	-154	327	0	-298	-38	6.28	6.28	9.42	9.42	-2.29	67.8

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	330	196	-240	345	0	-612	-104	6.28	6.28	9.42	9.42	-4.36	208.6
41	330	65	-133	307	0	-609	-164	6.28	6.28	9.42	9.42	-4.41	197.9
42	330	634	-124	196	0	-757	-153	6.28	6.28	9.42	9.42	-5.15	288.1
43	330	220	-323	366	0	-594	-87	6.28	6.28	9.42	9.42	-4.22	204.9
44	330	-217	47	244	0	-609	-262	6.28	6.28	9.42	9.42	-4.54	176.8
45	330	949	-131	116	0	-836	-169	6.28	6.28	9.42	9.42	-5.51	337.6
46	330	-38	-152	299	0	-579	-202	6.28	6.28	9.42	9.42	-4.24	180.6
47	330	-64	-157	297	0	-571	-211	6.28	6.28	9.42	9.42	-4.20	176.3
49	330	-20	-192	310	0	-572	-191	6.28	6.28	9.42	9.42	-4.19	179.8
50	330	-107	-118	285	0	-575	-226	6.28	6.28	9.42	9.42	-4.25	174.3
51	330	126	-154	260	0	-621	-207	6.28	6.28	9.42	9.42	-4.47	206.1

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	440	691	-367	345	0	-991	-438	6.28	6.28	9.42	9.42	-6.84	366.6

41	440	560	-133	307	0	-947	-311	6.28	6.28	9.42	9.42	-6.60	342.4
42	440	1129	-124	-8	0	-860	-290	6.28	6.28	9.42	9.42	-5.54	359.3
43	440	715	-535	366	0	-996	-559	6.28	6.28	9.42	9.42	-8.42	370.1
44	440	278	258	244	0	-877	-94	6.28	6.28	9.42	9.42	-6.26	298.8
45	440	1444	-131	-222	0	-778	-313	6.28	6.28	9.42	9.42	-4.62	358.5
46	440	457	-152	299	0	-908	-369	6.28	6.28	9.42	9.42	-6.38	322.2
47	440	431	-157	297	0	-898	-383	6.28	6.28	9.42	9.42	-6.32	317.1
49	440	475	-235	310	0	-913	-426	6.28	6.28	9.42	9.42	-6.44	325.2
50	440	388	-76	285	0	-889	-333	6.28	6.28	9.42	9.42	-6.28	310.9
51	440	621	-154	192	0	-869	-377	6.28	6.28	9.42	9.42	-5.99	322.5

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 5 NI 34 NF 35 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 12C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-10320	-446	457	0	-694	716	6.28	6.28	12.57	12.57	-7.25	-95.5
41	0	-9466	-287	346	0	-502	445	6.28	6.28	12.57	12.57	-5.61	-77.3
42	0	-9469	-280	879	0	-3923	433	6.28	6.28	12.57	12.57	-25.60	578.1
43	0	-10310	-537	451	0	-701	862	6.28	6.28	12.57	12.57	-8.00	-103.9
44	0	-8375	-28	176	0	-206	1	6.28	6.28	12.57	12.57	-3.97	-57.8
45	0	-8884	-260	1153	0	-6083	389	6.28	6.28	12.57	12.57	-40.05	1269.4
46	0	-8528	-263	216	0	-308	389	6.28	6.28	12.57	12.57	-4.99	-67.7
47	0	-8294	-256	184	0	-259	375	6.28	6.28	12.57	12.57	-4.84	-65.6
49	0	-8579	-309	221	0	-323	465	6.28	6.28	12.57	12.57	-5.39	-72.2
50	0	-8193	-208	166	0	-224	293	6.28	6.28	12.57	12.57	-4.40	-60.5
51	0	-8294	-254	362	0	-1399	371	6.28	6.28	12.57	12.57	-8.67	-115.5

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	83	-9826	-446	457	0	-1071	348	6.28	6.28	12.57	12.57	-7.63	-104.9
41	83	-8971	-287	346	0	-787	208	6.28	6.28	12.57	12.57	-6.28	-87.2
42	83	-8974	-280	577	0	-4523	202	6.28	6.28	12.57	12.57	-29.72	787.0
43	83	-9814	-537	451	0	-1073	419	6.28	6.28	12.57	12.57	-7.63	-104.9
44	83	-7880	-28	176	0	-352	-22	6.28	6.28	12.57	12.57	-4.30	-61.4
45	83	-8389	-260	650	0	-6827	175	6.28	6.28	12.57	12.57	-44.88	1533.8
46	83	-8033	-263	216	0	-486	172	6.28	6.28	12.57	12.57	-4.84	-68.3
47	83	-7799	-256	184	0	-411	163	6.28	6.28	12.57	12.57	-4.48	-63.6
49	83	-8084	-309	221	0	-506	210	6.28	6.28	12.57	12.57	-4.93	-69.5
50	83	-7698	-208	166	0	-361	122	6.28	6.28	12.57	12.57	-4.27	-60.8
51	83	-7799	-254	261	0	-1656	161	6.28	6.28	12.57	12.57	-10.19	-132.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	165	-9331	-446	457	0	-1449	-20	6.28	6.28	12.57	12.57	-9.10	-122.2
41	165	-8476	-287	346	0	-1072	-29	6.28	6.28	12.57	12.57	-7.16	-97.6
42	165	-8479	-280	275	0	-4874	-29	6.28	6.28	12.57	12.57	-32.09	925.7
43	165	-9318	-537	451	0	-1445	-24	6.28	6.28	12.57	12.57	-9.08	-122.0
44	165	-7385	-28	176	0	-497	-45	6.28	6.28	12.57	12.57	-4.63	-65.0
45	165	-7894	-260	146	0	-7155	-39	6.28	6.28	12.57	12.57	-46.96	1670.7
46	165	-7538	-263	216	0	-664	-45	6.28	6.28	12.57	12.57	-5.29	-73.4
47	165	-7304	-256	184	0	-562	-48	6.28	6.28	12.57	12.57	-4.84	-67.5
49	165	-7589	-309	221	0	-688	-45	6.28	6.28	12.57	12.57	-5.40	-74.8
50	165	-7203	-208	166	0	-498	-50	6.28	6.28	12.57	12.57	-4.57	-64.0
51	165	-7304	-254	160	0	-1830	-48	6.28	6.28	12.57	12.57	-11.42	-144.1

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	248	-8836	-446	457	0	-1826	-388	6.28	6.28	12.57	12.57	-11.22	-145.9
41	248	-7981	-287	346	0	-1358	-266	6.28	6.28	12.57	12.57	-8.41	-111.9
42	248	-7984	-280	-27	0	-4976	-260	6.28	6.28	12.57	12.57	-32.77	989.9
43	248	-8822	-537	451	0	-1817	-467	6.28	6.28	12.57	12.57	-11.17	-145.2
44	248	-6890	-28	176	0	-642	-68	6.28	6.28	12.57	12.57	-4.96	-68.7
45	248	-7399	-260	-357	0	-7068	-253	6.28	6.28	12.57	12.57	-46.35	1678.7
46	248	-7043	-263	216	0	-843	-261	6.28	6.28	12.57	12.57	-5.75	-78.7
47	248	-6809	-256	184	0	-714	-260	6.28	6.28	12.57	12.57	-5.19	-71.4
49	248	-7094	-309	221	0	-870	-301	6.28	6.28	12.57	12.57	-5.88	-80.3
50	248	-6708	-208	166	0	-636	-221	6.28	6.28	12.57	12.57	-4.87	-67.3
51	248	-6809	-254	60	0	-1920	-258	6.28	6.28	12.57	12.57	-12.14	168.9

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	330	-8342	-446	457	0	-2203	-756	6.28	6.28	12.57	12.57	-13.82	-173.0
41	330	-7486	-287	346	0	-1643	-503	6.28	6.28	12.57	12.57	-10.13	-130.6
42	330	-7489	-280	-330	0	-4829	-491	6.28	6.28	12.57	12.57	-31.80	978.0
43	330	-8326	-537	451	0	-2189	-910	6.28	6.28	12.57	12.57	-13.73	-171.9
44	330	-6395	-28	176	0	-788	-90	6.28	6.28	12.57	12.57	-5.31	-72.5
45	330	-6904	-260	-860	0	-6566	-467	6.28	6.28	12.57	12.57	-43.06	1557.2
46	330	-6548	-263	216	0	-1021	-478	6.28	6.28	12.57	12.57	-6.41	-86.0
47	330	-6314	-256	184	0	-866	-471	6.28	6.28	12.57	12.57	-5.62	-76.2
49	330	-6599	-309	221	0	-1053	-556	6.28	6.28	12.57	12.57	-6.58	-88.2
50	330	-6213	-208	166	0	-773	-392	6.28	6.28	12.57	12.57	-5.19	-70.9
51	330	-6314	-254	-41	0	-1928	-467	6.28	6.28	12.57	12.57	-12.29	193.8

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 6 NI 36 NF 37 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 17C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-10670	-402	505	0	-1167	521	6.28	6.28	12.57	12.57	-8.30	-114.1
41	0	-9976	-244	432	0	-1039	272	6.28	6.28	12.57	12.57	-7.57	-104.3
42	0	-10050	-245	1139	0	-5029	272	6.28	6.28	12.57	12.57	-33.04	870.3
43	0	-10350	-496	454	0	-1017	670	6.28	6.28	12.57	12.57	-7.64	-105.5
44	0	-9034	16	329	0	-870	-143	6.28	6.28	12.57	12.57	-6.61	-91.3

45	0	-9317	-235	1512	0	-7454	254	6.28	6.28	12.57	12.57	-49.01	1663.8
46	0	-8721	-227	273	0	-664	243	6.28	6.28	12.57	12.57	-5.75	-80.2
47	0	-8408	-222	233	0	-570	236	6.28	6.28	12.57	12.57	-5.29	-74.2
49	0	-8639	-275	257	0	-612	319	6.28	6.28	12.57	12.57	-5.53	-77.5
50	0	-8376	-172	232	0	-583	156	6.28	6.28	12.57	12.57	-5.32	-74.6
51	0	-8433	-222	469	0	-1900	236	6.28	6.28	12.57	12.57	-11.74	-150.7

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	83	-10175	-402	505	0	-1583	189	6.28	6.28	12.57	12.57	-9.94	-133.5
41	83	-9481	-244	432	0	-1395	70	6.28	6.28	12.57	12.57	-8.87	-119.7
42	83	-9555	-245	837	0	-5844	70	6.28	6.28	12.57	12.57	-38.49	1150.6
43	83	-9854	-496	454	0	-1392	260	6.28	6.28	12.57	12.57	-8.95	-121.1
44	83	-8539	16	329	0	-1142	-129	6.28	6.28	12.57	12.57	-7.47	-101.5
45	83	-8822	-235	1008	0	-8493	60	6.28	6.28	12.57	12.57	-55.69	2022.0
46	83	-8226	-227	273	0	-889	56	6.28	6.28	12.57	12.57	-6.36	-87.4
47	83	-7913	-222	233	0	-762	52	6.28	6.28	12.57	12.57	-5.79	-80.0
49	83	-8144	-275	257	0	-825	92	6.28	6.28	12.57	12.57	-6.10	-84.1
50	83	-7881	-172	232	0	-775	14	6.28	6.28	12.57	12.57	-5.82	-80.3
51	83	-7938	-222	368	0	-2245	52	6.28	6.28	12.57	12.57	-14.20	198.5

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	165	-9680	-402	505	0	-2000	-143	6.28	6.28	12.57	12.57	-12.29	-159.8
41	165	-8986	-244	432	0	-1752	-132	6.28	6.28	12.57	12.57	-10.76	-140.9
42	165	-9060	-245	535	0	-6410	-133	6.28	6.28	12.57	12.57	-42.20	1358.3
43	165	-9358	-496	454	0	-1766	-149	6.28	6.28	12.57	12.57	-10.86	-142.8
44	165	-8044	16	329	0	-1413	-116	6.28	6.28	12.57	12.57	-8.72	-115.7
45	165	-8327	-235	505	0	-9118	-133	6.28	6.28	12.57	12.57	-59.65	2252.2
46	165	-7731	-227	273	0	-1114	-131	6.28	6.28	12.57	12.57	-7.12	-96.3
47	165	-7418	-222	233	0	-954	-131	6.28	6.28	12.57	12.57	-6.33	-86.2
49	165	-7649	-275	257	0	-1037	-134	6.28	6.28	12.57	12.57	-6.75	-91.7
50	165	-7386	-172	232	0	-966	-128	6.28	6.28	12.57	12.57	-6.37	-86.7
51	165	-7443	-222	268	0	-2508	-131	6.28	6.28	12.57	12.57	-16.13	291.1

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	248	-9184	-402	505	0	-2416	-474	6.28	6.28	12.57	12.57	-15.15	-189.7
41	248	-8491	-244	432	0	-2108	-334	6.28	6.28	12.57	12.57	-13.14	-166.1
42	248	-8566	-245	233	0	-6727	-335	6.28	6.28	12.57	12.57	-44.24	1490.6
43	248	-8863	-496	454	0	-2141	-559	6.28	6.28	12.57	12.57	-13.31	-169.0
44	248	-7549	16	329	0	-1684	-103	6.28	6.28	12.57	12.57	-10.40	-133.6
45	248	-7832	-235	2	0	-9326	-327	6.28	6.28	12.57	12.57	-60.92	2353.1
46	248	-7236	-227	273	0	-1339	-318	6.28	6.28	12.57	12.57	-8.23	-108.6
47	248	-6923	-222	233	0	-1147	-314	6.28	6.28	12.57	12.57	-7.12	-95.1
49	248	-7154	-275	257	0	-1250	-361	6.28	6.28	12.57	12.57	-7.72	-102.4
50	248	-6891	-172	232	0	-1158	-270	6.28	6.28	12.57	12.57	-7.18	-95.7
51	248	-6948	-222	167	0	-2687	-315	6.28	6.28	12.57	12.57	-17.46	368.8

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	330	-8689	-402	505	0	-2832	-806	6.28	6.28	12.57	12.57	-18.17	314.0
41	330	-7996	-244	432	0	-2464	-535	6.28	6.28	12.57	12.57	-15.72	251.3
42	330	-8071	-245	-69	0	-6795	-538	6.28	6.28	12.57	12.57	-44.65	1546.2
43	330	-8367	-496	454	0	-2516	-968	6.28	6.28	12.57	12.57	-16.01	246.8
44	330	-7054	16	329	0	-1955	-89	6.28	6.28	12.57	12.57	-12.33	166.6
45	330	-7337	-235	-502	0	-9120	-520	6.28	6.28	12.57	12.57	-59.52	2324.2
46	330	-6741	-227	273	0	-1564	-505	6.28	6.28	12.57	12.57	-9.69	-123.8
47	330	-6428	-222	233	0	-1339	-497	6.28	6.28	12.57	12.57	-8.23	-106.9
49	330	-6659	-275	257	0	-1462	-588	6.28	6.28	12.57	12.57	-9.02	-116.2
50	330	-6396	-172	232	0	-1350	-412	6.28	6.28	12.57	12.57	-8.31	-107.7
51	330	-6453	-222	66	0	-2783	-498	6.28	6.28	12.57	12.57	-18.19	426.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 7 NI 38 NF 39 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 22C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-11820	-153	339	0	-148	205	6.28	6.28	12.57	12.57	-5.27	-75.2
41	0	-11780	14	362	0	-267	-57	6.28	6.28	12.57	12.57	-5.51	-80.2
42	0	-11840	-4	837	0	-3632	-38	6.28	6.28	12.57	12.57	-23.16	367.8
43	0	-11030	-247	237	0	8	369	6.28	6.28	12.57	12.57	-5.79	-80.1
44	0	-11930	292	417	0	-481	-496	6.28	6.28	12.57	12.57	-6.75	-92.0
45	0	-11060	2	1067	0	-5799	-36	6.28	6.28	12.57	12.57	-38.13	1037.6
46	0	-10460	41	225	0	-144	-74	6.28	6.28	12.57	12.57	-4.56	-67.1
47	0	-10130	48	190	0	-113	-78	6.28	6.28	12.57	12.57	-4.32	-63.8
49	0	-10140	-7	183	0	-73	9	6.28	6.28	12.57	12.57	-4.18	-62.0
50	0	-10320	100	219	0	-171	-164	6.28	6.28	12.57	12.57	-4.60	-67.5
51	0	-10150	43	349	0	-1235	-72	6.28	6.28	12.57	12.57	-8.37	-114.4

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	83	-11326	-153	339	0	-427	79	6.28	6.28	12.57	12.57	-5.91	-84.8
41	83	-11284	14	362	0	-566	-46	6.28	6.28	12.57	12.57	-6.38	-90.7
42	83	-11346	-4	535	0	-4198	-41	6.28	6.28	12.57	12.57	-27.20	548.1
43	83	-10535	-247	237	0	-188	165	6.28	6.28	12.57	12.57	-4.74	-69.5
44	83	-11436	292	417	0	-826	-255	6.28	6.28	12.57	12.57	-7.37	-103.2
45	83	-10566	2	564	0	-6472	-34	6.28	6.28	12.57	12.57	-42.62	1275.1
46	83	-9964	41	225	0	-329	-40	6.28	6.28	12.57	12.57	-5.03	-72.5
47	83	-9634	48	190	0	-270	-39	6.28	6.28	12.57	12.57	-4.69	-67.9
49	83	-9646	-7	183	0	-224	3	6.28	6.28	12.57	12.57	-4.53	-65.9
50	83	-9826	100	219	0	-352	-81	6.28	6.28	12.57	12.57	-5.06	-72.7
51	83	-9655	43	248	0	-1481	-37	6.28	6.28	12.57	12.57	-9.33	-125.4

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	165	-10832	-153	339	0	-707	-48	6.28	6.28	12.57	12.57	-6.72	-94.4
41	165	-10788	14	362	0	-864	-35	6.28	6.28	12.57	12.57	-7.26	-101.2
42	165	-10852	-4	233	0	-4514	-44	6.28	6.28	12.57	12.57	-29.46	667.8
43	165	-10040	-247	237	0	-384	-38	6.28	6.28	12.57	12.57	-5.25	-75.4
44	165	-10942	292	417	0	-1170	-14	6.28	6.28	12.57	12.57	-8.42	-115.8
45	165	-10072	2	60	0	-6729	-32	6.28	6.28	12.57	12.57	-44.31	1387.5

46	165	-9468	41	225	0	-515	-6	6.28	6.28	12.57	12.57	-5.50	-77.9
47	165	-9138	48	190	0	-427	1	6.28	6.28	12.57	12.57	-5.06	-72.1
49	165	-9152	-7	183	0	-375	-3	6.28	6.28	12.57	12.57	-4.88	-69.8
50	165	-9332	100	219	0	-532	2	6.28	6.28	12.57	12.57	-5.51	-77.9
51	165	-9160	43	147	0	-1644	-2	6.28	6.28	12.57	12.57	-10.13	-134.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	248	-10337	-153	339	0	-986	-174	6.28	6.28	12.57	12.57	-7.53	-104.1
41	248	-10291	14	362	0	-1163	-23	6.28	6.28	12.57	12.57	-8.14	-111.7
42	248	-10357	-4	-69	0	-4581	-46	6.28	6.28	12.57	12.57	-29.98	717.5
43	248	-9546	-247	237	0	-579	-242	6.28	6.28	12.57	12.57	-5.76	-81.3
44	248	-10449	292	417	0	-1514	227	6.28	6.28	12.57	12.57	-9.67	-130.6
45	248	-9579	2	-443	0	-6571	-30	6.28	6.28	12.57	12.57	-43.27	1372.5
46	248	-8973	41	225	0	-700	28	6.28	6.28	12.57	12.57	-5.97	-83.3
47	248	-8643	48	190	0	-585	41	6.28	6.28	12.57	12.57	-5.43	-76.3
49	248	-8657	-7	183	0	-526	-9	6.28	6.28	12.57	12.57	-5.23	-73.7
50	248	-8838	100	219	0	-713	85	6.28	6.28	12.57	12.57	-5.97	-83.1
51	248	-8665	43	47	0	-1724	33	6.28	6.28	12.57	12.57	-10.59	-138.4

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	330	-9843	-153	339	0	-1266	-300	6.28	6.28	12.57	12.57	-8.40	-114.4
41	330	-9795	14	362	0	-1462	-12	6.28	6.28	12.57	12.57	-9.27	-124.9
42	330	-9863	-4	-372	0	-4399	-49	6.28	6.28	12.57	12.57	-28.80	694.0
43	330	-9051	-247	237	0	-775	-445	6.28	6.28	12.57	12.57	-6.27	-87.2
44	330	-9955	292	417	0	-1858	468	6.28	6.28	12.57	12.57	-11.42	-150.5
45	330	-9085	2	-946	0	-5998	-28	6.28	6.28	12.57	12.57	-39.50	1229.5
46	330	-8477	41	225	0	-886	62	6.28	6.28	12.57	12.57	-6.45	-88.8
47	330	-8147	48	190	0	-742	81	6.28	6.28	12.57	12.57	-5.80	-80.4
49	330	-8163	-7	183	0	-676	-15	6.28	6.28	12.57	12.57	-5.58	-77.6
50	330	-8344	100	219	0	-893	168	6.28	6.28	12.57	12.57	-6.42	-88.3
51	330	-8170	43	-54	0	-1721	69	6.28	6.28	12.57	12.57	-10.59	-137.3

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 8 NI 40 NF 34 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 12B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-16740	-30	288	0	508	134	6.28	6.28	12.57	12.57	-8.29	-119.8
41	0	-15900	-123	178	0	241	321	6.28	6.28	12.57	12.57	-7.31	-103.7
42	0	-15910	-114	2134	0	1842	298	6.28	6.28	12.57	12.57	-12.76	-174.8
43	0	-16730	35	320	0	628	3	6.28	6.28	12.57	12.57	-8.71	-125.0
44	0	-14840	-280	3	0	-189	638	6.28	6.28	12.57	12.57	-8.50	-115.6
45	0	-15350	-105	3396	0	2850	278	6.28	6.28	12.57	12.57	-17.52	-231.0
46	0	-15000	-119	112	0	147	312	6.28	6.28	12.57	12.57	-6.94	-98.4
47	0	-14770	-117	95	0	123	310	6.28	6.28	12.57	12.57	-6.85	-97.0
49	0	-15050	-86	132	0	212	248	6.28	6.28	12.57	12.57	-6.64	-96.7
50	0	-14670	-149	68	0	49	374	6.28	6.28	12.57	12.57	-7.13	-100.1
51	0	-14770	-114	747	0	657	302	6.28	6.28	12.57	12.57	-8.06	-115.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	110	-16080	-30	288	0	191	101	6.28	6.28	12.57	12.57	-6.90	-101.7
41	110	-15240	-123	178	0	45	186	6.28	6.28	12.57	12.57	-6.41	-92.6
42	110	-15250	-114	1731	0	-284	173	6.28	6.28	12.57	12.57	-6.91	-101.1
43	110	-16070	35	320	0	275	41	6.28	6.28	12.57	12.57	-7.19	-105.5
44	110	-14180	-280	3	0	-192	330	6.28	6.28	12.57	12.57	-6.74	-94.9
45	110	-14690	-105	2725	0	-517	162	6.28	6.28	12.57	12.57	-7.53	-108.3
46	110	-14340	-119	112	0	24	182	6.28	6.28	12.57	12.57	-6.06	-87.6
47	110	-14110	-117	95	0	19	181	6.28	6.28	12.57	12.57	-5.97	-86.3
49	110	-14390	-86	132	0	68	152	6.28	6.28	12.57	12.57	-5.93	-86.4
50	110	-14010	-149	68	0	-26	210	6.28	6.28	12.57	12.57	-6.08	-87.4
51	110	-14110	-114	613	0	-91	177	6.28	6.28	12.57	12.57	-5.95	-86.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	220	-15420	-30	288	0	-126	67	6.28	6.28	12.57	12.57	-6.41	-95.0
41	220	-14580	-123	178	0	-150	50	6.28	6.28	12.57	12.57	-6.17	-91.2
42	220	-14590	-114	1328	0	-1967	48	6.28	6.28	12.57	12.57	-12.83	-174.2
43	220	-15410	35	320	0	-77	80	6.28	6.28	12.57	12.57	-6.23	-92.7
44	220	-13520	-280	3	0	-196	22	6.28	6.28	12.57	12.57	-5.93	-87.1
45	220	-14030	-105	2054	0	-3145	46	6.28	6.28	12.57	12.57	-19.42	-249.5
46	220	-13680	-119	112	0	-98	51	6.28	6.28	12.57	12.57	-5.64	-83.7
47	220	-13450	-117	95	0	-86	52	6.28	6.28	12.57	12.57	-5.50	-81.8
49	220	-13730	-86	132	0	-77	57	6.28	6.28	12.57	12.57	-5.58	-83.0
50	220	-13350	-149	68	0	-101	46	6.28	6.28	12.57	12.57	-5.52	-81.9
51	220	-13450	-114	478	0	-691	51	6.28	6.28	12.57	12.57	-7.67	-108.9

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	330	-14760	-30	288	0	-443	34	6.28	6.28	12.57	12.57	-7.29	-105.3
41	330	-13920	-123	178	0	-346	-85	6.28	6.28	12.57	12.57	-6.62	-96.1
42	330	-13930	-114	926	0	-3206	-78	6.28	6.28	12.57	12.57	-19.84	-253.9
43	330	-14750	35	320	0	-429	118	6.28	6.28	12.57	12.57	-7.23	-104.7
44	330	-12860	-280	3	0	-200	-286	6.28	6.28	12.57	12.57	-6.04	-85.4
45	330	-13370	-105	1383	0	-5035	-69	6.28	6.28	12.57	12.57	-32.67	671.0
46	330	-13020	-119	112	0	-221	-79	6.28	6.28	12.57	12.57	-5.82	-85.3
47	330	-12790	-117	95	0	-190	-78	6.28	6.28	12.57	12.57	-5.62	-82.6
49	330	-13070	-86	132	0	-222	-38	6.28	6.28	12.57	12.57	-5.84	-85.7
50	330	-12690	-149	68	0	-176	-119	6.28	6.28	12.57	12.57	-5.53	-81.4
51	330	-12790	-114	344	0	-1143	-75	6.28	6.28	12.57	12.57	-9.03	-125.3

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	440	-14100	-30	288	0	-760	1	6.28	6.28	12.57	12.57	-8.17	-115.7
41	440	-13260	-123	178	0	-542	-220	6.28	6.28	12.57	12.57	-7.06	-101.1
42	440	-13270	-114	523	0	-4003	-203	6.28	6.28	12.57	12.57	-25.48	394.7
43	440	-14090	35	320	0	-781	156	6.28	6.28	12.57	12.57	-8.24	-116.6
44	440	-12200	-280	3	0	-204	-594	6.28	6.28	12.57	12.57	-7.33	-98.9
45	440	-12710	-105	711	0	-6187	-185	6.28	6.28	12.57	12.57	-40.62	1048.7
46	440	-12360	-119	112	0	-344	-210	6.28	6.28	12.57	12.57	-6.01	-87.0

47	440	-12130	-117	95	0	-294	-207	6.28	6.28	12.57	12.57	-5.74	-83.5
49	440	-12410	-86	132	0	-367	-133	6.28	6.28	12.57	12.57	-6.11	-88.3
50	440	-12030	-149	68	0	-252	-283	6.28	6.28	12.57	12.57	-5.73	-81.0
51	440	-12130	-114	210	0	-1448	-201	6.28	6.28	12.57	12.57	-9.89	-135.4

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 9 NI 41 NF 36 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 17B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-17080	130	496	0	915	-249	6.28	6.28	12.57	12.57	-9.88	-139.9
41	0	-16390	19	430	0	769	-18	6.28	6.28	12.57	12.57	-9.09	-129.4
42	0	-16480	15	2665	0	2840	-11	6.28	6.28	12.57	12.57	-17.56	-233.4
43	0	-16760	198	440	0	829	-389	6.28	6.28	12.57	12.57	-9.44	-134.2
44	0	-15460	-167	339	0	562	364	6.28	6.28	12.57	12.57	-7.99	-114.7
45	0	-15750	7	4056	0	4037	8	6.28	6.28	12.57	12.57	-25.25	-317.5
46	0	-15140	8	270	0	474	4	6.28	6.28	12.57	12.57	-7.55	-109.0
47	0	-14830	5	230	0	401	10	6.28	6.28	12.57	12.57	-7.16	-103.9
49	0	-15060	43	253	0	450	-67	6.28	6.28	12.57	12.57	-7.43	-107.4
50	0	-14800	-31	232	0	396	84	6.28	6.28	12.57	12.57	-7.14	-103.5
51	0	-14850	4	976	0	1091	12	6.28	6.28	12.57	12.57	-9.64	-134.9

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	110	-16420	130	496	0	370	-105	6.28	6.28	12.57	12.57	-7.67	-111.7
41	110	-15730	19	430	0	296	2	6.28	6.28	12.57	12.57	-7.14	-104.4
42	110	-15820	15	2262	0	130	6	6.28	6.28	12.57	12.57	-6.58	-97.5
43	110	-16100	198	440	0	345	-170	6.28	6.28	12.57	12.57	-7.45	-108.7
44	110	-14800	-167	339	0	189	180	6.28	6.28	12.57	12.57	-6.40	-94.2
45	110	-15090	7	3385	0	-55	15	6.28	6.28	12.57	12.57	-6.03	-89.9
46	110	-14480	8	270	0	177	13	6.28	6.28	12.57	12.57	-6.23	-91.8
47	110	-14170	5	230	0	147	16	6.28	6.28	12.57	12.57	-6.00	-88.7
49	110	-14400	43	253	0	172	-20	6.28	6.28	12.57	12.57	-6.18	-91.1
50	110	-14140	-31	232	0	141	50	6.28	6.28	12.57	12.57	-5.97	-88.2
51	110	-14190	4	841	0	92	17	6.28	6.28	12.57	12.57	-5.81	-86.3

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	220	-15760	130	496	0	-175	38	6.28	6.28	12.57	12.57	-6.72	-99.2
41	220	-15070	19	430	0	-176	23	6.28	6.28	12.57	12.57	-6.45	-95.2
42	220	-15160	15	1859	0	-2137	23	6.28	6.28	12.57	12.57	-13.75	-186.1
43	220	-15440	198	440	0	-140	48	6.28	6.28	12.57	12.57	-6.46	-95.7
44	220	-14140	-167	339	0	-183	-3	6.28	6.28	12.57	12.57	-6.12	-90.2
45	220	-14430	7	2714	0	-3408	22	6.28	6.28	12.57	12.57	-21.14	-269.4
46	220	-13820	8	270	0	-120	22	6.28	6.28	12.57	12.57	-5.77	-85.5
47	220	-13510	5	230	0	-106	21	6.28	6.28	12.57	12.57	-5.60	-83.1
49	220	-13740	43	253	0	-106	27	6.28	6.28	12.57	12.57	-5.69	-84.4
50	220	-13480	-31	232	0	-115	16	6.28	6.28	12.57	12.57	-5.62	-83.3
51	220	-13530	4	707	0	-760	21	6.28	6.28	12.57	12.57	-7.95	-112.4

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	330	-15100	130	496	0	-721	182	6.28	6.28	12.57	12.57	-8.41	-119.8
41	330	-14410	19	430	0	-648	43	6.28	6.28	12.57	12.57	-7.89	-112.5
42	330	-14500	15	1457	0	-3960	40	6.28	6.28	12.57	12.57	-24.94	328.3
43	330	-14780	198	440	0	-624	266	6.28	6.28	12.57	12.57	-7.94	-113.6
44	330	-13480	-167	339	0	-556	-187	6.28	6.28	12.57	12.57	-7.20	-103.0
45	330	-13770	7	2042	0	-6023	29	6.28	6.28	12.57	12.57	-39.40	934.0
46	330	-13160	8	270	0	-418	30	6.28	6.28	12.57	12.57	-6.58	-95.0
47	330	-12850	5	230	0	-360	27	6.28	6.28	12.57	12.57	-6.25	-90.6
49	330	-13080	43	253	0	-384	73	6.28	6.28	12.57	12.57	-6.43	-93.0
50	330	-12820	-31	232	0	-370	-17	6.28	6.28	12.57	12.57	-6.28	-90.9
51	330	-12870	4	573	0	-1464	26	6.28	6.28	12.57	12.57	-10.22	-140.2

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	440	-14440	130	496	0	-1266	325	6.28	6.28	12.57	12.57	-10.11	-140.3
41	440	-13750	19	430	0	-1121	63	6.28	6.28	12.57	12.57	-9.33	-129.9
42	440	-13840	15	1054	0	-5341	56	6.28	6.28	12.57	12.57	-34.71	731.4
43	440	-14120	198	440	0	-1108	485	6.28	6.28	12.57	12.57	-9.42	-131.4
44	440	-12820	-167	339	0	-929	-371	6.28	6.28	12.57	12.57	-8.28	-115.9
45	440	-13110	7	1371	0	-7900	36	6.28	6.28	12.57	12.57	-52.02	1542.3
46	440	-12500	8	270	0	-715	39	6.28	6.28	12.57	12.57	-7.39	-104.4
47	440	-12190	5	230	0	-614	33	6.28	6.28	12.57	12.57	-6.91	-98.1
49	440	-12420	43	253	0	-662	120	6.28	6.28	12.57	12.57	-7.17	-101.6
50	440	-12160	-31	232	0	-626	-51	6.28	6.28	12.57	12.57	-6.94	-98.5
51	440	-12210	4	439	0	-2020	31	6.28	6.28	12.57	12.57	-12.55	-167.6

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 10 NI 42 NF 38 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 22B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-18240	207	-11	0	-194	-452	6.28	6.28	12.57	12.57	-8.80	-123.6
41	0	-18200	102	69	0	10	-242	6.28	6.28	12.57	12.57	-7.75	-111.8
42	0	-18270	88	1982	0	1498	-207	6.28	6.28	12.57	12.57	-12.42	-172.9
43	0	-17470	263	-88	0	-357	-566	6.28	6.28	12.57	12.57	-9.09	-125.8
44	0	-18350	-71	208	0	361	104	6.28	6.28	12.57	12.57	-8.38	-122.5
45	0	-17510	65	3233	0	2464	-158	6.28	6.28	12.57	12.57	-15.86	-214.7
46	0	-16910	81	31	0	-32	-202	6.28	6.28	12.57	12.57	-7.09	-102.6
47	0	-16590	75	22	0	-43	-192	6.28	6.28	12.57	12.57	-6.92	-100.3
49	0	-16600	110	-5	0	-111	-261	6.28	6.28	12.57	12.57	-7.27	-104.2
50	0	-16780	43	54	0	33	-127	6.28	6.28	12.57	12.57	-6.67	-98.7
51	0	-16610	70	659	0	453	-180	6.28	6.28	12.57	12.57	-8.04	-116.5

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	110	-17580	207	-11	0	-182	-224	6.28	6.28	12.57	12.57	-7.44	-110.0
41	110	-17540	102	69	0	-66	-130	6.28	6.28	12.57	12.57	-7.01	-104.6
42	110	-17610	88	1579	0	-460	-110	6.28	6.28	12.57	12.57	-8.45	-122.6
43	110	-16810	263	-88	0	-261	-276	6.28	6.28	12.57	12.57	-7.43	-109.1
44	110	-17690	-71	208	0	132	26	6.28	6.28	12.57	12.57	-7.31	-108.4
45	110	-16850	65	2562	0	-723	-86	6.28	6.28	12.57	12.57	-9.10	-130.0
46	110	-16250	81	31	0	-67	-113	6.28	6.28	12.57	12.57	-6.52	-97.1
47	110	-15930	75	22	0	-67	-109	6.28	6.28	12.57	12.57	-6.39	-95.3
49	110	-15940	110	-5	0	-106	-140	6.28	6.28	12.57	12.57	-6.54	-97.1
50	110	-16120	43	54	0	-27	-80	6.28	6.28	12.57	12.57	-6.32	-94.6
51	110	-15950	70	525	0	-198	-102	6.28	6.28	12.57	12.57	-6.87	-101.3

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	220	-16920	207	-11	0	-170	4	6.28	6.28	12.57	12.57	-7.15	-105.7
41	220	-16880	102	69	0	-141	-17	6.28	6.28	12.57	12.57	-7.03	-104.1
42	220	-16950	88	1176	0	-1975	-13	6.28	6.28	12.57	12.57	-13.64	-186.8
43	220	-16150	263	-88	0	-164	13	6.28	6.28	12.57	12.57	-6.83	-100.9
44	220	-17030	-71	208	0	-97	-52	6.28	6.28	12.57	12.57	-6.93	-103.0
45	220	-16190	65	1891	0	-3172	-15	6.28	6.28	12.57	12.57	-19.48	-255.1
46	220	-15590	81	31	0	-101	-24	6.28	6.28	12.57	12.57	-6.38	-94.9
47	220	-15270	75	22	0	-91	-26	6.28	6.28	12.57	12.57	-6.22	-92.5
49	220	-15280	110	-5	0	-100	-19	6.28	6.28	12.57	12.57	-6.26	-93.0
50	220	-15460	43	54	0	-87	-32	6.28	6.28	12.57	12.57	-6.28	-93.5
51	220	-15290	70	391	0	-702	-25	6.28	6.28	12.57	12.57	-8.42	-120.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	330	-16260	207	-11	0	-158	232	6.28	6.28	12.57	12.57	-7.00	-101.3
41	330	-16220	102	69	0	-217	95	6.28	6.28	12.57	12.57	-7.04	-103.7
42	330	-16290	88	773	0	-3047	83	6.28	6.28	12.57	12.57	-18.73	-246.7
43	330	-15490	263	-88	0	-67	303	6.28	6.28	12.57	12.57	-7.08	-100.5
44	330	-16370	-71	208	0	-326	-130	6.28	6.28	12.57	12.57	-7.49	-109.5
45	330	-15530	65	1219	0	-4883	56	6.28	6.28	12.57	12.57	-31.21	513.5
46	330	-14930	81	31	0	-135	65	6.28	6.28	12.57	12.57	-6.25	-92.6
47	330	-14610	75	22	0	-115	57	6.28	6.28	12.57	12.57	-6.05	-89.8
49	330	-14620	110	-5	0	-95	102	6.28	6.28	12.57	12.57	-5.99	-89.0
50	330	-14800	43	54	0	-147	16	6.28	6.28	12.57	12.57	-6.24	-92.3
51	330	-14630	70	257	0	-1058	53	6.28	6.28	12.57	12.57	-9.44	-132.1

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	440	-15600	207	-11	0	-146	459	6.28	6.28	12.57	12.57	-7.89	-109.8
41	440	-15560	102	69	0	-293	208	6.28	6.28	12.57	12.57	-7.06	-103.3
42	440	-15630	88	371	0	-3676	180	6.28	6.28	12.57	12.57	-22.79	-290.6
43	440	-14830	263	-88	0	30	593	6.28	6.28	12.57	12.57	-8.27	-113.1
44	440	-15710	-71	208	0	-555	-207	6.28	6.28	12.57	12.57	-8.06	-115.9
45	440	-14870	65	548	0	-5855	127	6.28	6.28	12.57	12.57	-38.10	819.3
46	440	-14270	81	31	0	-169	153	6.28	6.28	12.57	12.57	-6.12	-90.3
47	440	-13950	75	22	0	-138	140	6.28	6.28	12.57	12.57	-5.88	-87.0
49	440	-13960	110	-5	0	-89	224	6.28	6.28	12.57	12.57	-6.13	-87.8
50	440	-14140	43	54	0	-206	63	6.28	6.28	12.57	12.57	-6.20	-91.2
51	440	-13970	70	122	0	-1266	130	6.28	6.28	12.57	12.57	-9.93	-137.6

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 11 NI 48 NF 49 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 31B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-19620	1456	-87	0	-149	-10540	15.71	15.71	9.42	9.42	-35.64	742.2
41	0	-20620	646	-56	0	-104	-8422	15.71	15.71	9.42	9.42	-28.20	423.1
42	0	-20720	582	117	0	326	-8333	15.71	15.71	9.42	9.42	-27.88	408.9
43	0	-17360	1845	-90	0	-141	-10280	15.71	15.71	9.42	9.42	-34.80	792.1
44	0	-22630	-682	-5	0	-29	-5160	15.71	15.71	9.42	9.42	-17.36	-238.8
45	0	-19180	388	250	0	651	-6601	15.71	15.71	9.42	9.42	-21.91	-290.3
46	0	-18060	404	-28	0	-44	-5745	15.71	15.71	9.42	9.42	-19.01	-254.0
47	0	-17420	343	-20	0	-29	-5075	15.71	15.71	9.42	9.42	-16.77	-226.0
49	0	-17090	613	-31	0	-44	-5781	15.71	15.71	9.42	9.42	-19.18	-254.5
50	0	-18150	108	-14	0	-21	-4758	15.71	15.71	9.42	9.42	-15.77	-214.6
51	0	-17460	322	37	0	115	-5046	15.71	15.71	9.42	9.42	-16.67	-224.9

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	110	-18740	1317	-87	0	-53	-9014	15.71	15.71	9.42	9.42	-30.39	563.3
41	110	-19740	646	-56	0	-42	-7711	15.71	15.71	9.42	9.42	-25.77	361.4
42	110	-19840	582	117	0	198	-7692	15.71	15.71	9.42	9.42	-25.69	356.1
43	110	-16480	1614	-90	0	-43	-8377	15.71	15.71	9.42	9.42	-28.29	557.0
44	110	-21750	-451	-5	0	-23	-5783	15.71	15.71	9.42	9.42	-19.15	-260.3
45	110	-18300	388	250	0	375	-6174	15.71	15.71	9.42	9.42	-20.48	-271.9
46	110	-17180	404	-28	0	-13	-5301	15.71	15.71	9.42	9.42	-17.53	-234.9
47	110	-16540	343	-20	0	-6	-4698	15.71	15.71	9.42	9.42	-15.53	-209.8
49	110	-16210	567	-31	0	-10	-5132	15.71	15.71	9.42	9.42	-16.98	-227.0
50	110	-17270	154	-14	0	-6	-4614	15.71	15.71	9.42	9.42	-15.27	-207.5
51	110	-16580	322	37	0	74	-4692	15.71	15.71	9.42	9.42	-15.51	-209.6

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	220	-17860	1179	-87	0	42	-7641	15.71	15.71	9.42	9.42	-25.64	410.7
41	220	-18860	646	-56	0	20	-7000	15.71	15.71	9.42	9.42	-23.33	-306.5
42	220	-18960	582	117	0	69	-7052	15.71	15.71	9.42	9.42	-23.50	-308.7
43	220	-15600	1383	-90	0	56	-6728	15.71	15.71	9.42	9.42	-22.59	365.7
44	220	-20870	-220	-5	0	-18	-6152	15.71	15.71	9.42	9.42	-20.33	-273.7
45	220	-17420	388	250	0	100	-5746	15.71	15.71	9.42	9.42	-19.04	-253.4
46	220	-16300	404	-28	0	17	-4856	15.71	15.71	9.42	9.42	-16.05	-215.8
47	220	-15660	343	-20	0	16	-4320	15.71	15.71	9.42	9.42	-14.29	-193.5
49	220	-15330	521	-31	0	24	-4534	15.71	15.71	9.42	9.42	-14.98	-201.6
50	220	-16390	200	-14	0	9	-4419	15.71	15.71	9.42	9.42	-14.62	-198.5
51	220	-15700	322	37	0	33	-4338	15.71	15.71	9.42	9.42	-14.34	-194.3

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	330	-16980	1040	-87	0	138	-6420	15.71	15.71	9.42	9.42	-21.42	285.1
41	330	-17980	646	-56	0	81	-6290	15.71	15.71	9.42	9.42	-20.90	-276.4
42	330	-18080	582	117	0	-60	-6412	15.71	15.71	9.42	9.42	-21.32	-281.5
43	330	-14720	1152	-90	0	155	-5334	15.71	15.71	9.42	9.42	-17.75	-233.9
44	330	-19990	11	-5	0	-12	-6267	15.71	15.71	9.42	9.42	-20.73	-277.4
45	330	-16540	388	250	0	-175	-5319	15.71	15.71	9.42	9.42	-17.61	-235.0
46	330	-15420	404	-28	0	47	-4412	15.71	15.71	9.42	9.42	-14.58	-196.9
47	330	-14780	343	-20	0	39	-3943	15.71	15.71	9.42	9.42	-13.05	-177.4
49	330	-14450	475	-31	0	58	-3987	15.71	15.71	9.42	9.42	-13.18	-178.6
50	330	-15510	246	-14	0	24	-4173	15.71	15.71	9.42	9.42	-13.81	-187.5
51	330	-14820	322	37	0	-8	-3983	15.71	15.71	9.42	9.42	-13.18	-179.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	440	-16100	902	-87	0	234	-5352	15.71	15.71	9.42	9.42	-17.74	-235.9
41	440	-17100	646	-56	0	143	-5579	15.71	15.71	9.42	9.42	-18.48	-246.2
42	440	-17200	582	117	0	-188	-5771	15.71	15.71	9.42	9.42	-19.14	-254.2
43	440	-13840	921	-90	0	254	-4193	15.71	15.71	9.42	9.42	-13.86	-186.1
44	440	-19110	242	-5	0	-7	-6128	15.71	15.71	9.42	9.42	-20.29	-270.8
45	440	-15660	388	250	0	-450	-4892	15.71	15.71	9.42	9.42	-16.18	-216.6
46	440	-14540	404	-28	0	78	-3968	15.71	15.71	9.42	9.42	-13.13	-178.0
47	440	-13900	343	-20	0	61	-3566	15.71	15.71	9.42	9.42	-11.83	-161.3
49	440	-13570	428	-31	0	92	-3490	15.71	15.71	9.42	9.42	-11.58	-157.8
50	440	-14630	293	-14	0	40	-3877	15.71	15.71	9.42	9.42	-12.84	-174.6
51	440	-13940	322	37	0	-49	-3629	15.71	15.71	9.42	9.42	-12.03	-163.8

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 12 NI 91 NF 92 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 30B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-22520	2739	-106	0	-269	-21390	15.71	15.71	9.42	9.42	-71.95	2217.9
41	0	-22980	1581	-94	0	-250	-16410	15.71	15.71	9.42	9.42	-55.52	1456.3
42	0	-23020	1589	85	0	190	-16510	15.71	15.71	9.42	9.42	-55.85	1469.3
43	0	-20130	3161	-91	0	-223	-21410	15.71	15.71	9.42	9.42	-71.78	2327.4
44	0	-24170	-294	-75	0	-221	-8651	15.71	15.71	9.42	9.42	-28.78	-379.6
45	0	-20950	1244	227	0	542	-13260	15.71	15.71	9.42	9.42	-44.89	1079.1
46	0	-19630	1021	-57	0	-155	-11120	15.71	15.71	9.42	9.42	-37.63	823.8
47	0	-18800	880	-48	0	-132	-9793	15.71	15.71	9.42	9.42	-33.09	668.3
49	0	-18640	1267	-52	0	-138	-11450	15.71	15.71	9.42	9.42	-38.76	909.8
50	0	-19450	576	-48	0	-138	-8903	15.71	15.71	9.42	9.42	-29.96	523.7
51	0	-18810	883	12	0	15	-9826	15.71	15.71	9.42	9.42	-33.20	672.5

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	110	-21640	2600	-106	0	-153	-18454	15.71	15.71	9.42	9.42	-62.24	1816.6
41	110	-22100	1581	-94	0	-147	-14671	15.71	15.71	9.42	9.42	-49.66	1237.7
42	110	-22140	1589	85	0	96	-14762	15.71	15.71	9.42	9.42	-49.97	1249.3
43	110	-19250	2930	-91	0	-124	-18059	15.71	15.71	9.42	9.42	-60.76	1862.1
44	110	-23290	-63	-75	0	-139	-8848	15.71	15.71	9.42	9.42	-29.52	396.0
45	110	-20070	1244	227	0	292	-11893	15.71	15.71	9.42	9.42	-40.26	917.0
46	110	-18750	1021	-57	0	-93	-9996	15.71	15.71	9.42	9.42	-33.79	698.6
47	110	-17920	880	-48	0	-79	-8824	15.71	15.71	9.42	9.42	-29.77	566.5
49	110	-17760	1221	-52	0	-81	-10083	15.71	15.71	9.42	9.42	-34.12	748.5
50	110	-18570	622	-48	0	-84	-8245	15.71	15.71	9.42	9.42	-27.72	466.1
51	110	-17930	883	12	0	2	-8854	15.71	15.71	9.42	9.42	-29.88	570.3

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	220	-20760	2462	-106	0	-37	-15670	15.71	15.71	9.42	9.42	-52.97	1440.4
41	220	-21220	1581	-94	0	-44	-12932	15.71	15.71	9.42	9.42	-43.78	1020.9
42	220	-21260	1589	85	0	3	-13013	15.71	15.71	9.42	9.42	-44.06	1031.0
43	220	-18370	2699	-91	0	-24	-14962	15.71	15.71	9.42	9.42	-50.51	1437.3
44	220	-22410	168	-75	0	-56	-8790	15.71	15.71	9.42	9.42	-29.38	414.7
45	220	-19190	1244	227	0	42	-10526	15.71	15.71	9.42	9.42	-35.60	756.4
46	220	-17870	1021	-57	0	-30	-8873	15.71	15.71	9.42	9.42	-29.94	575.0
47	220	-17040	880	-48	0	-27	-7856	15.71	15.71	9.42	9.42	-26.45	466.3
49	220	-16880	1174	-52	0	-25	-8767	15.71	15.71	9.42	9.42	-29.62	596.5
50	220	-17690	668	-48	0	-31	-7536	15.71	15.71	9.42	9.42	-25.29	402.5
51	220	-17050	883	12	0	-11	-7883	15.71	15.71	9.42	9.42	-26.54	469.5

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	330	-19880	2324	-106	0	79	-13039	15.71	15.71	9.42	9.42	-44.14	1090.3
41	330	-20340	1581	-94	0	59	-11192	15.71	15.71	9.42	9.42	-37.86	806.8
42	330	-20380	1589	85	0	-91	-11264	15.71	15.71	9.42	9.42	-38.10	815.5
43	330	-17490	2468	-91	0	76	-12120	15.71	15.71	9.42	9.42	-41.01	1054.0
44	330	-21530	399	-75	0	26	-8479	15.71	15.71	9.42	9.42	-28.34	402.5
45	330	-18310	1244	227	0	-207	-9158	15.71	15.71	9.42	9.42	-30.91	598.3
46	330	-16990	1021	-57	0	32	-7750	15.71	15.71	9.42	9.42	-26.08	453.8
47	330	-16160	880	-48	0	25	-6888	15.71	15.71	9.42	9.42	-23.11	368.2
49	330	-16000	1128	-52	0	32	-7502	15.71	15.71	9.42	9.42	-25.27	454.7
50	330	-16810	714	-48	0	22	-6776	15.71	15.71	9.42	9.42	-22.68	333.6
51	330	-16170	883	12	0	-24	-6912	15.71	15.71	9.42	9.42	-23.20	371.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	440	-19000	2185	-106	0	195	-10560	15.71	15.71	9.42	9.42	-35.72	768.5
41	440	-19460	1581	-94	0	162	-9453	15.71	15.71	9.42	9.42	-31.88	597.5
42	440	-19500	1589	85	0	-184	-9516	15.71	15.71	9.42	9.42	-32.10	604.7
43	440	-16610	2237	-91	0	176	-9531	15.71	15.71	9.42	9.42	-32.25	714.3
44	440	-20650	630	-75	0	108	-7913	15.71	15.71	9.42	9.42	-26.41	359.3
45	440	-17430	1244	227	0	-457	-7791	15.71	15.71	9.42	9.42	-26.20	444.4
46	440	-16110	1021	-57	0	95	-6626	15.71	15.71	9.42	9.42	-22.20	336.4
47	440	-15280	880	-48	0	78	-5919	15.71	15.71	9.42	9.42	-19.77	273.6
49	440	-15120	1082	-52	0	89	-6288	15.71	15.71	9.42	9.42	-21.08	324.5
50	440	-15930	760	-48	0	75	-5965	15.71	15.71	9.42	9.42	-19.89	-261.1
51	440	-15290	883	12	0	-38	-5940	15.71	15.71	9.42	9.42	-19.84	275.9

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 13 NI 134 NF 135 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 29B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm²				daN/cm²	
40	0	-22400	3005	-194	0	-539	-22740	15.71	15.71	9.42	9.42	-76.34	2426.3
41	0	-22980	1770	-167	0	-471	-17420	15.71	15.71	9.42	9.42	-58.88	1605.4
42	0	-22920	1754	-11	0	-80	-17260	15.71	15.71	9.42	9.42	-58.35	1584.2
43	0	-19930	3439	-177	0	-486	-22770	15.71	15.71	9.42	9.42	-76.17	2541.9
44	0	-24370	-225	-127	0	-368	-9130	15.71	15.71	9.42	9.42	-30.44	-399.6
45	0	-20790	1354	127	0	279	-13640	15.71	15.71	9.42	9.42	-46.18	1140.8
46	0	-19630	1148	-112	0	-315	-11790	15.71	15.71	9.42	9.42	-39.91	919.5
47	0	-18800	992	-98	0	-276	-10380	15.71	15.71	9.42	9.42	-35.11	750.7
49	0	-18600	1404	-107	0	-299	-12160	15.71	15.71	9.42	9.42	-41.17	1014.4
50	0	-19490	671	-97	0	-275	-9428	15.71	15.71	9.42	9.42	-31.79	593.0
51	0	-18780	987	-46	0	-146	-10330	15.71	15.71	9.42	9.42	-34.94	744.4
apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)													
40	110	-21520	2866	-194	0	-326	-19511	15.71	15.71	9.42	9.42	-65.71	1980.0
41	110	-22100	1770	-167	0	-287	-15472	15.71	15.71	9.42	9.42	-52.35	1355.0
42	110	-22040	1754	-11	0	-67	-15330	15.71	15.71	9.42	9.42	-51.88	1336.7
43	110	-19050	3208	-177	0	-292	-19114	15.71	15.71	9.42	9.42	-64.19	2029.5
44	110	-23490	6	-127	0	-229	-9251	15.71	15.71	9.42	9.42	-30.92	439.2
45	110	-19910	1354	127	0	139	-12150	15.71	15.71	9.42	9.42	-41.13	960.3
46	110	-18750	1148	-112	0	-192	-10527	15.71	15.71	9.42	9.42	-35.62	773.4
47	110	-17920	992	-98	0	-168	-9289	15.71	15.71	9.42	9.42	-31.38	630.7
49	110	-17720	1358	-107	0	-181	-10640	15.71	15.71	9.42	9.42	-36.02	829.7
50	110	-18610	717	-97	0	-168	-8665	15.71	15.71	9.42	9.42	-29.18	520.6
51	110	-17900	987	-46	0	-95	-9245	15.71	15.71	9.42	9.42	-31.23	625.3
apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)													
40	220	-20640	2728	-194	0	-113	-16435	15.71	15.71	9.42	9.42	-55.51	1558.9
41	220	-21220	1770	-167	0	-103	-13524	15.71	15.71	9.42	9.42	-45.78	1106.5
42	220	-21160	1754	-11	0	-55	-13401	15.71	15.71	9.42	9.42	-45.37	1091.1
43	220	-18170	2977	-177	0	-98	-15712	15.71	15.71	9.42	9.42	-52.97	1557.7
44	220	-22610	237	-127	0	-89	-9118	15.71	15.71	9.42	9.42	-30.51	449.2
45	220	-19030	1354	127	0	-2	-10660	15.71	15.71	9.42	9.42	-36.07	781.6
46	220	-17870	1148	-112	0	-69	-9264	15.71	15.71	9.42	9.42	-31.30	629.1
47	220	-17040	992	-98	0	-60	-8198	15.71	15.71	9.42	9.42	-27.64	512.4
49	220	-16840	1311	-107	0	-63	-9171	15.71	15.71	9.42	9.42	-31.02	654.6
50	220	-17730	763	-97	0	-62	-7851	15.71	15.71	9.42	9.42	-26.39	442.3
51	220	-17020	987	-46	0	-44	-8160	15.71	15.71	9.42	9.42	-27.51	507.9
apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)													
40	330	-19760	2590	-194	0	100	-13511	15.71	15.71	9.42	9.42	-45.73	1164.2
41	330	-20340	1770	-167	0	81	-11575	15.71	15.71	9.42	9.42	-39.17	861.1
42	330	-20280	1754	-11	0	-43	-11472	15.71	15.71	9.42	9.42	-38.81	848.7
43	330	-17290	2746	-177	0	96	-12564	15.71	15.71	9.42	9.42	-42.50	1127.7
44	330	-21730	468	-127	0	50	-8730	15.71	15.71	9.42	9.42	-29.21	427.7
45	330	-18150	1354	127	0	-142	-9171	15.71	15.71	9.42	9.42	-30.96	605.9
46	330	-16990	1148	-112	0	55	-8002	15.71	15.71	9.42	9.42	-26.96	487.6
47	330	-16160	992	-98	0	48	-7108	15.71	15.71	9.42	9.42	-23.88	396.8
49	330	-15960	1265	-107	0	54	-7753	15.71	15.71	9.42	9.42	-26.15	490.1
50	330	-16850	809	-97	0	45	-6986	15.71	15.71	9.42	9.42	-23.41	358.8
51	330	-16140	987	-46	0	7	-7074	15.71	15.71	9.42	9.42	-23.77	393.1
apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)													
40	440	-18880	2451	-194	0	313	-10740	15.71	15.71	9.42	9.42	-36.34	798.7
41	440	-19460	1770	-167	0	265	-9627	15.71	15.71	9.42	9.42	-32.49	621.3
42	440	-19400	1754	-11	0	-30	-9542	15.71	15.71	9.42	9.42	-32.19	611.8
43	440	-16410	2515	-177	0	291	-9670	15.71	15.71	9.42	9.42	-32.73	742.0
44	440	-20850	699	-127	0	190	-8089	15.71	15.71	9.42	9.42	-27.02	374.9
45	440	-17270	1354	127	0	-282	-7681	15.71	15.71	9.42	9.42	-25.82	435.3
46	440	-16110	1148	-112	0	178	-6739	15.71	15.71	9.42	9.42	-22.59	350.7
47	440	-15280	992	-98	0	156	-6017	15.71	15.71	9.42	9.42	-20.11	285.6
49	440	-15080	1219	-107	0	172	-6386	15.71	15.71	9.42	9.42	-21.42	338.3
50	440	-15970	856	-97	0	152	-6070	15.71	15.71	9.42	9.42	-20.25	271.9
51	440	-15260	987	-46	0	57	-5989	15.71	15.71	9.42	9.42	-20.02	282.8
apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)													

ASTA NUM. 14 NI 177 NF 178 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 28B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm²				daN/cm²	
40	0	-22320	2818	-233	0	-719	-21590	15.71	15.71	9.42	9.42	-72.58	2256.8
41	0	-22840	1596	-199	0	-617	-16220	15.71	15.71	9.42	9.42	-54.88	1434.2
42	0	-22840	1597	-61	0	-260	-16230	15.71	15.71	9.42	9.42	-54.91	1435.6
43	0	-19910	3276	-211	0	-654	-21860	15.71	15.71	9.42	9.42	-73.22	2405.2
44	0	-24140	-384	-149	0	-464	-7831	15.71	15.71	9.42	9.42	-25.93	-345.8
45	0	-20790	1241	76	0	111	-12930	15.71	15.71	9.42	9.42	-43.78	1037.8
46	0	-19550	1025	-128	0	-405	-10940	15.71	15.71	9.42	9.42	-37.01	801.3
47	0	-18720	882	-110	0	-352	-9615	15.71	15.71	9.42	9.42	-32.48	646.5
49	0	-18550	1290	-122	0	-386	-11400	15.71	15.71	9.42	9.42	-38.59	906.2
50	0	-19390	558	-109	0	-348	-8597	15.71	15.71	9.42	9.42	-28.90	485.2
51	0	-18720	883	-64	0	-233	-9617	15.71	15.71	9.42	9.42	-32.48	646.8
apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)													
40	110	-21440	2680	-233	0	-463	-18566	15.71	15.71	9.42	9.42	-62.59	1842.1
41	110	-21960	1596	-199	0	-398	-14466	15.71	15.71	9.42	9.42	-48.97	1213.5
42	110	-21960	1597	-61	0	-193	-14474	15.71	15.71	9.42	9.42	-49.00	1214.6

43	110	-19030	3045	-211	0	-422	-18384	15.71	15.71	9.42	9.42	-61.81	1920.6
44	110	-23260	-153	-149	0	-300	-8126	15.71	15.71	9.42	9.42	-27.00	-357.1
45	110	-19910	1241	76	0	27	-11566	15.71	15.71	9.42	9.42	-39.14	876.4
46	110	-18670	1025	-128	0	-264	-9812	15.71	15.71	9.42	9.42	-33.16	675.7
47	110	-17840	882	-110	0	-230	-8644	15.71	15.71	9.42	9.42	-29.15	544.8
49	110	-17670	1244	-122	0	-252	-10008	15.71	15.71	9.42	9.42	-33.86	741.2
50	110	-18510	604	-109	0	-228	-7958	15.71	15.71	9.42	9.42	-26.72	430.7
51	110	-17840	883	-64	0	-162	-8646	15.71	15.71	9.42	9.42	-29.16	545.1

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	220	-20560	2541	-233	0	-206	-15695	15.71	15.71	9.42	9.42	-53.05	1452.5
41	220	-21080	1596	-199	0	-178	-12711	15.71	15.71	9.42	9.42	-43.03	994.7
42	220	-21080	1597	-61	0	-126	-12717	15.71	15.71	9.42	9.42	-43.05	995.5
43	220	-18150	2814	-211	0	-190	-15162	15.71	15.71	9.42	9.42	-51.16	1476.5
44	220	-22380	78	-149	0	-137	-8168	15.71	15.71	9.42	9.42	-27.19	-358.0
45	220	-19030	1241	76	0	-56	-10201	15.71	15.71	9.42	9.42	-34.49	716.8
46	220	-17790	1025	-128	0	-123	-8684	15.71	15.71	9.42	9.42	-29.29	551.9
47	220	-16960	882	-110	0	-109	-7674	15.71	15.71	9.42	9.42	-25.82	444.7
49	220	-16790	1197	-122	0	-118	-8666	15.71	15.71	9.42	9.42	-29.28	585.8
50	220	-17630	650	-109	0	-108	-7269	15.71	15.71	9.42	9.42	-24.35	370.3
51	220	-16960	883	-64	0	-91	-7676	15.71	15.71	9.42	9.42	-25.82	444.9

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	330	-19680	2402	-233	0	50	-12976	15.71	15.71	9.42	9.42	-43.93	1089.3
41	330	-20200	1596	-199	0	41	-10956	15.71	15.71	9.42	9.42	-37.05	778.9
42	330	-20200	1597	-61	0	-59	-10960	15.71	15.71	9.42	9.42	-37.06	779.4
43	330	-17270	2583	-211	0	42	-12194	15.71	15.71	9.42	9.42	-41.26	1074.0
44	330	-21500	309	-149	0	27	-7955	15.71	15.71	9.42	9.42	-26.50	-348.4
45	330	-18150	1241	76	0	-140	-8836	15.71	15.71	9.42	9.42	-29.80	560.0
46	330	-16910	1025	-128	0	18	-7555	15.71	15.71	9.42	9.42	-25.40	430.7
47	330	-16080	882	-110	0	12	-6704	15.71	15.71	9.42	9.42	-22.47	347.2
49	330	-15910	1151	-122	0	16	-7376	15.71	15.71	9.42	9.42	-24.84	440.8
50	330	-16750	696	-109	0	13	-6528	15.71	15.71	9.42	9.42	-21.81	304.8
51	330	-16080	883	-64	0	-21	-6705	15.71	15.71	9.42	9.42	-22.48	347.3

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	440	-18800	2264	-233	0	306	-10410	15.71	15.71	9.42	9.42	-35.21	754.9
41	440	-19320	1596	-199	0	260	-9202	15.71	15.71	9.42	9.42	-31.02	568.3
42	440	-19320	1597	-61	0	8	-9204	15.71	15.71	9.42	9.42	-31.02	568.6
43	440	-16390	2352	-211	0	274	-9480	15.71	15.71	9.42	9.42	-32.08	715.6
44	440	-20620	540	-149	0	190	-7488	15.71	15.71	9.42	9.42	-24.93	-328.3
45	440	-17270	1241	76	0	-223	-7472	15.71	15.71	9.42	9.42	-25.09	407.9
46	440	-16030	1025	-128	0	159	-6427	15.71	15.71	9.42	9.42	-21.50	313.8
47	440	-15200	882	-110	0	134	-5733	15.71	15.71	9.42	9.42	-19.12	253.5
49	440	-15030	1105	-122	0	149	-6136	15.71	15.71	9.42	9.42	-20.55	308.0
50	440	-15870	742	-109	0	133	-5737	15.71	15.71	9.42	9.42	-19.09	-251.6
51	440	-15200	883	-64	0	50	-5734	15.71	15.71	9.42	9.42	-19.12	253.6

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 15 NI 220 NF 221 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 27B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-18580	95	-319	0	-756	-11760	15.71	15.71	9.42	9.42	-39.81	957.1
41	0	-19470	-489	-316	0	-716	-7983	15.71	15.71	9.42	9.42	-26.74	403.4
42	0	-19740	-498	-182	0	-382	-8183	15.71	15.71	9.42	9.42	-27.42	420.3
43	0	-16430	544	-282	0	-655	-12540	15.71	15.71	9.42	9.42	-42.38	1160.4
44	0	-21290	-1473	-318	0	-675	-1981	15.71	15.71	9.42	9.42	-9.97	-142.4
45	0	-18360	-445	-53	0	-32	-6582	15.71	15.71	9.42	9.42	-21.90	-288.8
46	0	-16970	-395	-253	0	-514	-5209	15.71	15.71	9.42	9.42	-17.22	-230.9
47	0	-16340	-372	-238	0	-463	-4515	15.71	15.71	9.42	9.42	-14.93	-202.2
49	0	-16040	-177	-239	0	-476	-5773	15.71	15.71	9.42	9.42	-19.21	-253.2
50	0	-17020	-580	-246	0	-480	-3662	15.71	15.71	9.42	9.42	-12.45	-172.0
51	0	-16430	-374	-193	0	-352	-4582	15.71	15.71	9.42	9.42	-15.15	-205.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	110	-17700	-43	-319	0	-404	-11729	15.71	15.71	9.42	9.42	-39.70	988.2
41	110	-18590	-489	-316	0	-369	-8520	15.71	15.71	9.42	9.42	-28.68	501.9
42	110	-18860	-498	-182	0	-182	-8730	15.71	15.71	9.42	9.42	-29.39	520.7
43	110	-15550	313	-282	0	-345	-12069	15.71	15.71	9.42	9.42	-40.78	1128.0
44	110	-20410	-1242	-318	0	-325	-3474	15.71	15.71	9.42	9.42	-12.69	-177.4
45	110	-17480	-445	-53	0	26	-7072	15.71	15.71	9.42	9.42	-23.67	350.1
46	110	-16090	-395	-253	0	-235	-5644	15.71	15.71	9.42	9.42	-18.75	-247.9
47	110	-15460	-372	-238	0	-202	-4924	15.71	15.71	9.42	9.42	-16.30	-217.7
49	110	-15160	-223	-239	0	-214	-5993	15.71	15.71	9.42	9.42	-20.04	286.2
50	110	-16140	-534	-246	0	-210	-4274	15.71	15.71	9.42	9.42	-14.16	-192.5
51	110	-15550	-374	-193	0	-140	-4994	15.71	15.71	9.42	9.42	-16.53	-220.6

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	220	-16820	-182	-319	0	-53	-11850	15.71	15.71	9.42	9.42	-40.10	1042.2
41	220	-17710	-489	-316	0	-21	-9056	15.71	15.71	9.42	9.42	-30.59	606.1
42	220	-17980	-498	-182	0	18	-9276	15.71	15.71	9.42	9.42	-31.34	626.7
43	220	-14670	82	-282	0	-35	-11852	15.71	15.71	9.42	9.42	-40.02	1133.4
44	220	-19530	-1011	-318	0	25	-4713	15.71	15.71	9.42	9.42	-15.73	-215.5
45	220	-16600	-445	-53	0	85	-7561	15.71	15.71	9.42	9.42	-25.44	441.9
46	220	-15210	-395	-253	0	43	-6078	15.71	15.71	9.42	9.42	-20.33	295.3
47	220	-14580	-372	-238	0	59	-5332	15.71	15.71	9.42	9.42	-17.76	-233.7
49	220	-14280	-269	-239	0	49	-6263	15.71	15.71	9.42	9.42	-21.04	348.4
50	220	-15260	-488	-246	0	61	-4836	15.71	15.71	9.42	9.42	-16.00	-213.9
51	220	-14670	-374	-193	0	72	-5406	15.71	15.71	9.42	9.42	-18.01	-236.8

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	330	-15940	-320	-319	0	298	-12124	15.71	15.71	9.42	9.42	-40.98	1119.6
41	330	-16830	-489	-316	0	326	-9593	15.71	15.71	9.42	9.42	-32.46	714.7
42	330	-17100	-498	-182	0	218	-9823	15.71	15.71	9.42	9.42	-33.24	737.0
43	330	-13790	-149	-282	0	276	-11889	15.71	15.71	9.42	9.42	-40.09	1176.9

44	330	-18650	-780	-318	0	376	-5698	15.71	15.71	9.42	9.42	-18.84	-252.7
45	330	-15720	-445	-53	0	143	-8050	15.71	15.71	9.42	9.42	-27.19	539.6
46	330	-14330	-395	-253	0	322	-6512	15.71	15.71	9.42	9.42	-21.91	379.6
47	330	-13700	-372	-238	0	321	-5741	15.71	15.71	9.42	9.42	-19.25	299.6
49	330	-13400	-315	-239	0	311	-6585	15.71	15.71	9.42	9.42	-22.22	421.7
50	330	-14380	-442	-246	0	331	-5347	15.71	15.71	9.42	9.42	-17.82	-234.1
51	330	-13790	-374	-193	0	284	-5817	15.71	15.71	9.42	9.42	-19.51	306.5

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	440	-15060	-459	-319	0	649	-12550	15.71	15.71	9.42	9.42	-42.35	1220.6
41	440	-15950	-489	-316	0	674	-10130	15.71	15.71	9.42	9.42	-34.30	826.6
42	440	-16220	-498	-182	0	418	-10370	15.71	15.71	9.42	9.42	-35.11	850.5
43	440	-12910	-380	-282	0	586	-12180	15.71	15.71	9.42	9.42	-40.98	1259.1
44	440	-17770	-549	-318	0	726	-6429	15.71	15.71	9.42	9.42	-21.40	-281.9
45	440	-14840	-445	-53	0	201	-8540	15.71	15.71	9.42	9.42	-28.90	641.7
46	440	-13450	-395	-253	0	600	-6947	15.71	15.71	9.42	9.42	-23.47	469.9
47	440	-12820	-372	-238	0	582	-6150	15.71	15.71	9.42	9.42	-20.73	383.1
49	440	-12520	-362	-239	0	574	-6957	15.71	15.71	9.42	9.42	-23.53	506.2
50	440	-13500	-395	-246	0	601	-5807	15.71	15.71	9.42	9.42	-19.49	314.5
51	440	-12910	-374	-193	0	496	-6229	15.71	15.71	9.42	9.42	-21.00	390.6

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 16 NI 263 NF 264 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 25B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm		daN		daN*m			cm^2				daN/cm^2	
40	0	-20070	486	-380	0	-959	-598	6.28	6.28	9.42	9.42	-15.13	-206.1
41	0	-18370	57	-303	0	-787	119	6.28	6.28	9.42	9.42	-12.83	-183.4
42	0	-18110	60	-262	0	-445	114	6.28	6.28	9.42	9.42	-11.14	-162.0
43	0	-20340	780	-341	0	-872	-1103	6.28	6.28	9.42	9.42	-19.90	-247.9
44	0	-15410	-660	-198	0	-548	1321	6.28	6.28	9.42	9.42	-20.79	-240.2
45	0	-17070	70	-145	0	-15	84	6.28	6.28	9.42	9.42	-8.97	-130.6
46	0	-16990	70	-158	0	-465	77	6.28	6.28	9.42	9.42	-10.66	-154.7
47	0	-16640	73	-122	0	-384	66	6.28	6.28	9.42	9.42	-10.12	-147.4
49	0	-17210	216	-148	0	-442	-173	6.28	6.28	9.42	9.42	-10.67	-155.0
50	0	-16220	-72	-119	0	-377	312	6.28	6.28	9.42	9.42	-10.65	-145.5
51	0	-16550	74	-108	0	-270	64	6.28	6.28	9.42	9.42	-9.55	-140.2

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	97	-19632	425	-380	0	-588	-154	6.28	6.28	9.42	9.42	-12.56	-181.6
41	97	-17932	57	-303	0	-491	175	6.28	6.28	9.42	9.42	-11.26	-163.3
42	97	-17672	60	-175	0	-232	172	6.28	6.28	9.42	9.42	-10.07	-146.6
43	97	-19902	678	-341	0	-540	-392	6.28	6.28	9.42	9.42	-13.16	-180.9
44	97	-14970	-558	-198	0	-354	727	6.28	6.28	9.42	9.42	-13.87	-174.6
45	97	-16632	70	1	0	53	152	6.28	6.28	9.42	9.42	-9.38	-133.7
46	97	-16550	70	-158	0	-310	145	6.28	6.28	9.42	9.42	-9.74	-142.5
47	97	-16200	73	-122	0	-265	137	6.28	6.28	9.42	9.42	-9.36	-137.3
49	97	-16770	195	-148	0	-298	28	6.28	6.28	9.42	9.42	-9.79	-143.5
50	97	-15780	-52	-119	0	-260	252	6.28	6.28	9.42	9.42	-9.89	-136.8
51	97	-16112	74	-79	0	-179	136	6.28	6.28	9.42	9.42	-8.99	-131.7

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	195	-19195	364	-380	0	-217	230	6.28	6.28	9.42	9.42	-11.33	-159.4
41	195	-17495	57	-303	0	-196	231	6.28	6.28	9.42	9.42	-10.52	-147.2
42	195	-17235	60	-101	0	-99	231	6.28	6.28	9.42	9.42	-10.40	-145.3
43	195	-19465	575	-341	0	-207	219	6.28	6.28	9.42	9.42	-11.35	-160.3
44	195	-14530	-456	-198	0	-161	233	6.28	6.28	9.42	9.42	-9.12	-126.1
45	195	-16195	70	125	0	-9	219	6.28	6.28	9.42	9.42	-9.79	-136.8
46	195	-16110	70	-158	0	-156	213	6.28	6.28	9.42	9.42	-9.69	-135.6
47	195	-15760	73	-122	0	-146	208	6.28	6.28	9.42	9.42	-9.48	-132.7
49	195	-16330	175	-148	0	-154	208	6.28	6.28	9.42	9.42	-9.75	-136.7
50	195	-15340	-31	-119	0	-144	211	6.28	6.28	9.42	9.42	-9.30	-129.9
51	195	-15675	74	-54	0	-114	208	6.28	6.28	9.42	9.42	-9.44	-132.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	292	-18758	302	-380	0	154	555	6.28	6.28	9.42	9.42	-14.10	-186.1
41	292	-17058	57	-303	0	100	287	6.28	6.28	9.42	9.42	-10.83	-149.2
42	292	-16798	60	-39	0	-32	289	6.28	6.28	9.42	9.42	-10.72	-147.6
43	292	-19028	473	-341	0	126	730	6.28	6.28	9.42	9.42	-15.84	-204.1
44	292	-14090	-353	-198	0	32	-161	6.28	6.28	9.42	9.42	-8.25	-116.3
45	292	-15758	70	228	0	-183	287	6.28	6.28	9.42	9.42	-10.20	-139.9
46	292	-15670	70	-158	0	-2	281	6.28	6.28	9.42	9.42	-10.11	-138.7
47	292	-15320	73	-122	0	-27	280	6.28	6.28	9.42	9.42	-9.92	-136.0
49	292	-15890	154	-148	0	-10	369	6.28	6.28	9.42	9.42	-11.02	-148.3
50	292	-14900	-11	-119	0	-28	191	6.28	6.28	9.42	9.42	-8.91	-124.8
51	292	-15238	74	-34	0	-71	280	6.28	6.28	9.42	9.42	-9.89	-135.5

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	390	-18320	241	-380	0	525	820	6.28	6.28	9.42	9.42	-16.33	-207.2
41	390	-16620	57	-303	0	396	343	6.28	6.28	9.42	9.42	-11.13	-151.2
42	390	-16360	60	11	0	-19	348	6.28	6.28	9.42	9.42	-11.05	-149.8
43	390	-18590	371	-341	0	458	1141	6.28	6.28	9.42	9.42	-19.52	-239.5
44	390	-13650	-251	-198	0	226	-456	6.28	6.28	9.42	9.42	-10.74	-140.2
45	390	-15320	70	311	0	-448	355	6.28	6.28	9.42	9.42	-10.62	-142.9
46	390	-15230	70	-158	0	152	349	6.28	6.28	9.42	9.42	-10.52	-141.8
47	390	-14880	73	-122	0	92	351	6.28	6.28	9.42	9.42	-10.37	-139.4
49	390	-15450	134	-148	0	134	509	6.28	6.28	9.42	9.42	-12.10	-158.1
50	390	-14460	10	-119	0	88	190	6.28	6.28	9.42	9.42	-8.69	-121.6
51	390	-14800	74	-17	0	-47	352	6.28	6.28	9.42	9.42	-10.34	-138.9

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 17 NI 49 NF 51 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 31C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-11930	1098	-18	0	-45	-4639	15.71	15.71	9.42	9.42	-15.50	215.8
41	0	-12960	821	-60	0	-105	-4913	15.71	15.71	9.42	9.42	-16.39	219.1
42	0	-13030	854	73	0	49	-5086	15.71	15.71	9.42	9.42	-16.99	238.0
43	0	-9640	1092	11	0	-6	-3426	15.71	15.71	9.42	9.42	-11.39	-150.4
44	0	-15030	386	-126	0	-202	-5542	15.71	15.71	9.42	9.42	-18.46	-242.8
45	0	-11480	686	163	0	151	-4171	15.71	15.71	9.42	9.42	-13.88	-182.9
46	0	-10400	517	-57	0	-106	-3266	15.71	15.71	9.42	9.42	-10.80	-144.5
47	0	-9755	441	-57	0	-106	-2854	15.71	15.71	9.42	9.42	-9.43	-127.1
49	0	-9412	533	-43	0	-86	-2763	15.71	15.71	9.42	9.42	-9.13	-123.0
50	0	-10490	392	-70	0	-126	-3186	15.71	15.71	9.42	9.42	-10.53	-141.4
51	0	-9779	452	-12	0	-55	-2912	15.71	15.71	9.42	9.42	-9.62	-129.4

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	83	-11270	960	-18	0	-30	-3790	15.71	15.71	9.42	9.42	-12.57	-166.9
41	83	-12300	821	-60	0	-56	-4236	15.71	15.71	9.42	9.42	-14.06	-186.3
42	83	-12370	854	73	0	-12	-4382	15.71	15.71	9.42	9.42	-14.57	-192.4
43	83	-8980	863	11	0	-15	-2619	15.71	15.71	9.42	9.42	-8.65	-116.6
44	83	-14370	616	-126	0	-97	-5129	15.71	15.71	9.42	9.42	-17.06	-225.1
45	83	-10820	686	163	0	16	-3605	15.71	15.71	9.42	9.42	-11.95	-158.9
46	83	-9739	517	-57	0	-59	-2840	15.71	15.71	9.42	9.42	-9.38	-126.5
47	83	-9095	441	-57	0	-60	-2490	15.71	15.71	9.42	9.42	-8.24	-111.7
49	83	-8752	488	-43	0	-51	-2342	15.71	15.71	9.42	9.42	-7.75	-105.3
50	83	-9830	438	-70	0	-68	-2844	15.71	15.71	9.42	9.42	-9.40	-126.7
51	83	-9119	452	-12	0	-45	-2539	15.71	15.71	9.42	9.42	-8.39	-113.6

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	165	-10610	823	-18	0	-15	-3054	15.71	15.71	9.42	9.42	-10.09	-136.2
41	165	-11640	821	-60	0	-7	-3559	15.71	15.71	9.42	9.42	-11.77	-157.8
42	165	-11710	854	73	0	-72	-3677	15.71	15.71	9.42	9.42	-12.16	-162.7
43	165	-8320	634	11	0	-23	-2002	15.71	15.71	9.42	9.42	-6.68	-91.6
44	165	-13710	845	-126	0	7	-4526	15.71	15.71	9.42	9.42	-15.00	-199.6
45	165	-10160	686	163	0	-118	-3040	15.71	15.71	9.42	9.42	-10.05	-135.0
46	165	-9078	517	-57	0	-12	-2413	15.71	15.71	9.42	9.42	-7.99	-108.6
47	165	-8435	441	-57	0	-13	-2126	15.71	15.71	9.42	9.42	-7.07	-96.5
49	165	-8092	442	-43	0	-16	-1958	15.71	15.71	9.42	9.42	-6.53	-89.5
50	165	-9170	484	-70	0	-10	-2463	15.71	15.71	9.42	9.42	-8.15	-110.7
51	165	-8459	452	-12	0	-35	-2166	15.71	15.71	9.42	9.42	-7.19	-98.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	248	-9951	685	-18	0	0	-2432	15.71	15.71	9.42	9.42	-8.11	-111.0
41	248	-10980	821	-60	0	43	-2882	15.71	15.71	9.42	9.42	-9.55	-129.9
42	248	-11050	854	73	0	-132	-2972	15.71	15.71	9.42	9.42	-9.84	-133.6
43	248	-7660	404	11	0	-32	-1573	15.71	15.71	9.42	9.42	-5.40	-74.9
44	248	-13050	1075	-126	0	111	-3734	15.71	15.71	9.42	9.42	-12.34	-166.6
45	248	-9499	686	163	0	-253	-2474	15.71	15.71	9.42	9.42	-8.20	-111.7
46	248	-8418	517	-57	0	36	-1986	15.71	15.71	9.42	9.42	-6.65	-91.2
47	248	-7775	441	-57	0	34	-1763	15.71	15.71	9.42	9.42	-5.93	-81.7
49	248	-7432	396	-43	0	20	-1613	15.71	15.71	9.42	9.42	-5.47	-75.6
50	248	-8510	530	-70	0	49	-2045	15.71	15.71	9.42	9.42	-6.83	-93.6
51	248	-7799	452	-12	0	-24	-1793	15.71	15.71	9.42	9.42	-6.02	-82.8

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	330	-9291	547	-18	0	16	-1924	15.71	15.71	9.42	9.42	-6.60	-91.3
41	330	-10320	821	-60	0	92	-2205	15.71	15.71	9.42	9.42	-7.51	-103.7
42	330	-10390	854	73	0	-192	-2268	15.71	15.71	9.42	9.42	-7.69	-106.1
43	330	-7000	175	11	0	-41	-1334	15.71	15.71	9.42	9.42	-4.68	-65.1
44	330	-12390	1304	-126	0	216	-2753	15.71	15.71	9.42	9.42	-9.30	-128.2
45	330	-8839	686	163	0	-388	-1908	15.71	15.71	9.42	9.42	-6.48	-89.5
46	330	-7757	517	-57	0	83	-1560	15.71	15.71	9.42	9.42	-5.39	-74.7
47	330	-7115	441	-57	0	81	-1399	15.71	15.71	9.42	9.42	-4.86	-67.5
49	330	-6772	350	-43	0	55	-1305	15.71	15.71	9.42	9.42	-4.56	-63.4
50	330	-7850	576	-70	0	107	-1589	15.71	15.71	9.42	9.42	-5.48	-76.0
51	330	-7139	452	-12	0	-14	-1420	15.71	15.71	9.42	9.42	-4.92	-68.3

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 18 NI 92 NF 94 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 30C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-15030	2563	-216	0	-319	-10620	15.71	15.71	9.42	9.42	-35.93	935.9
41	0	-15460	1850	-221	0	-339	-9285	15.71	15.71	9.42	9.42	-31.43	724.1
42	0	-15500	1870	-84	0	-150	-9370	15.71	15.71	9.42	9.42	-31.72	734.8
43	0	-12630	2633	-168	0	-241	-9613	15.71	15.71	9.42	9.42	-32.49	888.1
44	0	-16610	728	-234	0	-377	-7386	15.71	15.71	9.42	9.42	-24.83	418.4
45	0	-13430	1479	51	0	42	-7529	15.71	15.71	9.42	9.42	-25.47	552.4
46	0	-12080	1203	-151	0	-234	-6249	15.71	15.71	9.42	9.42	-21.11	423.4
47	0	-11240	1041	-133	0	-208	-5490	15.71	15.71	9.42	9.42	-18.52	349.2
49	0	-11090	1279	-132	0	-202	-5935	15.71	15.71	9.42	9.42	-20.06	416.3
50	0	-11890	898	-145	0	-229	-5490	15.71	15.71	9.42	9.42	-18.48	326.5
51	0	-11250	1048	-88	0	-145	-5518	15.71	15.71	9.42	9.42	-18.62	352.7

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	83	-14370	2425	-216	0	-141	-8562	15.71	15.71	9.42	9.42	-28.98	663.3
41	83	-14800	1850	-221	0	-156	-7758	15.71	15.71	9.42	9.42	-26.22	533.0
42	83	-14840	1870	-84	0	-80	-7827	15.71	15.71	9.42	9.42	-26.45	541.1
43	83	-11970	2404	-168	0	-102	-7535	15.71	15.71	9.42	9.42	-25.51	610.6
44	83	-15950	958	-234	0	-184	-6691	15.71	15.71	9.42	9.42	-22.43	349.6
45	83	-12770	1479	51	0	-0	-6309	15.71	15.71	9.42	9.42	-21.29	406.5
46	83	-11420	1203	-151	0	-110	-5256	15.71	15.71	9.42	9.42	-17.69	311.3
47	83	-10580	1041	-133	0	-98	-4631	15.71	15.71	9.42	9.42	-15.56	256.9
49	83	-10431	1233	-132	0	-93	-4899	15.71	15.71	9.42	9.42	-16.50	297.5

50	83	-11230	944	-145	0	-109	-4730	15.71	15.71	9.42	9.42	-15.86	248.7
51	83	-10591	1048	-88	0	-73	-4654	15.71	15.71	9.42	9.42	-15.64	259.5

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	165	-13710	2288	-216	0	37	-6618	15.71	15.71	9.42	9.42	-22.32	415.3
41	165	-14140	1850	-221	0	26	-6232	15.71	15.71	9.42	9.42	-20.94	348.9
42	165	-14180	1870	-84	0	-10	-6284	15.71	15.71	9.42	9.42	-21.12	354.5
43	165	-11310	2175	-168	0	37	-5646	15.71	15.71	9.42	9.42	-19.06	368.1
44	165	-15290	1187	-234	0	9	-5806	15.71	15.71	9.42	9.42	-19.37	259.7
45	165	-12110	1479	51	0	-42	-5089	15.71	15.71	9.42	9.42	-17.07	266.6
46	165	-10760	1203	-151	0	15	-4264	15.71	15.71	9.42	9.42	-14.26	204.4
47	165	-9919	1041	-133	0	12	-3772	15.71	15.71	9.42	9.42	-12.58	169.0
49	165	-9772	1187	-132	0	15	-3900	15.71	15.71	9.42	9.42	-13.05	189.1
50	165	-10570	989	-145	0	10	-3933	15.71	15.71	9.42	9.42	-13.11	-172.2
51	165	-9932	1048	-88	0	-0	-3789	15.71	15.71	9.42	9.42	-12.64	170.8

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	248	-13050	2150	-216	0	215	-4788	15.71	15.71	9.42	9.42	-15.95	-209.8
41	248	-13480	1850	-221	0	209	-4705	15.71	15.71	9.42	9.42	-15.63	-206.8
42	248	-13520	1870	-84	0	59	-4742	15.71	15.71	9.42	9.42	-15.76	-208.3
43	248	-10651	1945	-168	0	175	-3946	15.71	15.71	9.42	9.42	-13.15	-172.8
44	248	-14630	1417	-234	0	203	-4732	15.71	15.71	9.42	9.42	-15.67	-209.0
45	248	-11450	1479	51	0	-84	-3869	15.71	15.71	9.42	9.42	-12.83	-170.4
46	248	-10101	1203	-151	0	139	-3271	15.71	15.71	9.42	9.42	-10.83	-144.4
47	248	-9258	1041	-133	0	122	-2912	15.71	15.71	9.42	9.42	-9.63	-128.9
49	248	-9114	1141	-132	0	124	-2940	15.71	15.71	9.42	9.42	-9.73	-129.8
50	248	-9911	1035	-145	0	129	-3097	15.71	15.71	9.42	9.42	-10.25	-137.1
51	248	-9273	1048	-88	0	72	-2924	15.71	15.71	9.42	9.42	-9.68	-129.4

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	330	-12390	2012	-216	0	393	-3071	15.71	15.71	9.42	9.42	-10.22	-139.7
41	330	-12820	1850	-221	0	391	-3179	15.71	15.71	9.42	9.42	-10.58	-144.6
42	330	-12860	1870	-84	0	129	-3199	15.71	15.71	9.42	9.42	-10.64	-145.5
43	330	-9991	1716	-168	0	314	-2436	15.71	15.71	9.42	9.42	-8.12	-111.2
44	330	-13970	1646	-234	0	396	-3469	15.71	15.71	9.42	9.42	-11.54	-157.8
45	330	-10790	1479	51	0	-126	-2649	15.71	15.71	9.42	9.42	-8.82	-120.7
46	330	-9441	1203	-151	0	264	-2278	15.71	15.71	9.42	9.42	-7.60	-104.2
47	330	-8598	1041	-133	0	232	-2053	15.71	15.71	9.42	9.42	-6.86	-94.1
49	330	-8455	1095	-132	0	232	-2017	15.71	15.71	9.42	9.42	-6.74	-92.4
50	330	-9251	1081	-145	0	249	-2224	15.71	15.71	9.42	9.42	-7.43	-101.8
51	330	-8614	1048	-88	0	144	-2060	15.71	15.71	9.42	9.42	-6.88	-94.4

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 19 NI 135 NF 137 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 29C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-14830	2491	-439	0	-684	-10410	15.71	15.71	9.42	9.42	-35.22	913.3
41	0	-15400	1812	-404	0	-636	-9197	15.71	15.71	9.42	9.42	-31.13	713.9
42	0	-15340	1782	-249	0	-411	-9087	15.71	15.71	9.42	9.42	-30.76	700.4
43	0	-12350	2546	-379	0	-587	-9335	15.71	15.71	9.42	9.42	-31.56	858.8
44	0	-16790	744	-358	0	-574	-7498	15.71	15.71	9.42	9.42	-25.21	427.2
45	0	-13210	1364	-62	0	-131	-7130	15.71	15.71	9.42	9.42	-24.11	504.4
46	0	-12050	1176	-271	0	-429	-6185	15.71	15.71	9.42	9.42	-20.89	415.6
47	0	-11210	1017	-237	0	-377	-5431	15.71	15.71	9.42	9.42	-18.32	342.2
49	0	-11020	1243	-249	0	-393	-5836	15.71	15.71	9.42	9.42	-19.73	405.1
50	0	-11910	882	-244	0	-391	-5468	15.71	15.71	9.42	9.42	-18.41	322.8
51	0	-11190	1007	-185	0	-302	-5395	15.71	15.71	9.42	9.42	-18.19	338.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	83	-14170	2353	-439	0	-322	-8412	15.71	15.71	9.42	9.42	-28.47	649.6
41	83	-14740	1812	-404	0	-302	-7702	15.71	15.71	9.42	9.42	-26.03	527.3
42	83	-14680	1782	-249	0	-205	-7617	15.71	15.71	9.42	9.42	-25.73	517.7
43	83	-11691	2317	-379	0	-274	-7329	15.71	15.71	9.42	9.42	-24.81	592.0
44	83	-16130	973	-358	0	-279	-6790	15.71	15.71	9.42	9.42	-22.77	356.6
45	83	-12550	1364	-62	0	-79	-6004	15.71	15.71	9.42	9.42	-20.24	372.8
46	83	-11389	1176	-271	0	-206	-5215	15.71	15.71	9.42	9.42	-17.55	306.9
47	83	-10550	1017	-237	0	-182	-4592	15.71	15.71	9.42	9.42	-15.43	252.8
49	83	-10360	1197	-249	0	-188	-4829	15.71	15.71	9.42	9.42	-16.27	290.6
50	83	-11249	928	-244	0	-189	-4721	15.71	15.71	9.42	9.42	-15.83	246.9
51	83	-10530	1007	-185	0	-149	-4564	15.71	15.71	9.42	9.42	-15.33	249.9

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	165	-13510	2216	-439	0	41	-6527	15.71	15.71	9.42	9.42	-22.01	409.9
41	165	-14080	1812	-404	0	31	-6208	15.71	15.71	9.42	9.42	-20.86	347.7
42	165	-14020	1782	-249	0	1	-6146	15.71	15.71	9.42	9.42	-20.65	341.7
43	165	-11032	2088	-379	0	39	-5513	15.71	15.71	9.42	9.42	-18.61	359.7
44	165	-15470	1202	-358	0	16	-5892	15.71	15.71	9.42	9.42	-19.66	264.9
45	165	-11890	1364	-62	0	-28	-4878	15.71	15.71	9.42	9.42	-16.34	246.8
46	165	-10728	1176	-271	0	18	-4245	15.71	15.71	9.42	9.42	-14.19	203.0
47	165	-9889	1017	-237	0	14	-3754	15.71	15.71	9.42	9.42	-12.52	167.8
49	165	-9699	1151	-249	0	17	-3861	15.71	15.71	9.42	9.42	-12.91	186.4
50	165	-10588	974	-244	0	13	-3936	15.71	15.71	9.42	9.42	-13.12	-172.3
51	165	-9869	1007	-185	0	4	-3734	15.71	15.71	9.42	9.42	-12.46	166.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	248	-12850	2078	-439	0	403	-4756	15.71	15.71	9.42	9.42	-15.85	-208.3
41	248	-13420	1812	-404	0	365	-4713	15.71	15.71	9.42	9.42	-15.66	-207.0
42	248	-13360	1782	-249	0	207	-4676	15.71	15.71	9.42	9.42	-15.54	-205.5
43	248	-10374	1858	-379	0	351	-3885	15.71	15.71	9.42	9.42	-12.95	-170.0
44	248	-14810	1432	-358	0	311	-4806	15.71	15.71	9.42	9.42	-15.92	-212.2
45	248	-11230	1364	-62	0	23	-3753	15.71	15.71	9.42	9.42	-12.44	-165.4
46	248	-10068	1176	-271	0	241	-3275	15.71	15.71	9.42	9.42	-10.85	-144.6
47	248	-9228	1017	-237	0	210	-2916	15.71	15.71	9.42	9.42	-9.65	-129.0
49	248	-9038	1105	-249	0	222	-2930	15.71	15.71	9.42	9.42	-9.70	-129.4
50	248	-9926	1020	-244	0	215	-3114	15.71	15.71	9.42	9.42	-10.30	-137.8

51	248	-9208	1007	-185	0	157	-2904	15.71	15.71	9.42	9.42	-9.61	-128.5

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	330	-12190	1940	-439	0	766	-3098	15.71	15.71	9.42	9.42	-10.29	-140.4
41	330	-12760	1812	-404	0	699	-3218	15.71	15.71	9.42	9.42	-10.69	-146.0
42	330	-12700	1782	-249	0	412	-3206	15.71	15.71	9.42	9.42	-10.65	-145.4
43	330	-9715	1629	-379	0	664	-2447	15.71	15.71	9.42	9.42	-8.13	-111.0
44	330	-14150	1661	-358	0	606	-3530	15.71	15.71	9.42	9.42	-11.74	-160.4
45	330	-10570	1364	-62	0	75	-2627	15.71	15.71	9.42	9.42	-8.74	-119.5
46	330	-9407	1176	-271	0	464	-2305	15.71	15.71	9.42	9.42	-7.68	-105.1
47	330	-8568	1017	-237	0	405	-2077	15.71	15.71	9.42	9.42	-6.93	-94.9
49	330	-8378	1059	-249	0	428	-2037	15.71	15.71	9.42	9.42	-6.79	-93.0
50	330	-9265	1066	-244	0	416	-2253	15.71	15.71	9.42	9.42	-7.51	-102.9
51	330	-8548	1007	-185	0	310	-2073	15.71	15.71	9.42	9.42	-6.91	-94.7

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 20 NI 178 NF 180 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 28C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-14650	2424	-507	0	-823	-10250	15.71	15.71	9.42	9.42	-34.68	897.3
41	0	-15180	1722	-476	0	-765	-8897	15.71	15.71	9.42	9.42	-30.11	679.5
42	0	-15190	1720	-296	0	-497	-8897	15.71	15.71	9.42	9.42	-30.11	679.1
43	0	-12230	2509	-425	0	-688	-9318	15.71	15.71	9.42	9.42	-31.50	861.3
44	0	-16490	613	-438	0	-695	-6952	15.71	15.71	9.42	9.42	-23.32	365.9
45	0	-13120	1335	-73	0	-145	-7057	15.71	15.71	9.42	9.42	-23.86	497.5
46	0	-11870	1108	-310	0	-489	-5953	15.71	15.71	9.42	9.42	-20.10	390.1
47	0	-11050	955	-269	0	-420	-5216	15.71	15.71	9.42	9.42	-17.58	318.7
49	0	-10870	1189	-279	0	-439	-5669	15.71	15.71	9.42	9.42	-19.16	387.4
50	0	-11720	810	-282	0	-440	-5196	15.71	15.71	9.42	9.42	-17.47	293.2
51	0	-11050	954	-209	0	-330	-5217	15.71	15.71	9.42	9.42	-17.58	318.8

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	83	-13990	2286	-507	0	-404	-8308	15.71	15.71	9.42	9.42	-28.12	641.7
41	83	-14520	1722	-476	0	-373	-7477	15.71	15.71	9.42	9.42	-25.26	504.1
42	83	-14530	1720	-296	0	-252	-7478	15.71	15.71	9.42	9.42	-25.26	503.9
43	83	-11571	2280	-425	0	-338	-7342	15.71	15.71	9.42	9.42	-24.86	598.7
44	83	-15830	842	-438	0	-333	-6352	15.71	15.71	9.42	9.42	-21.25	310.6
45	83	-12460	1335	-73	0	-85	-5955	15.71	15.71	9.42	9.42	-20.07	369.3
46	83	-11210	1108	-310	0	-233	-5038	15.71	15.71	9.42	9.42	-16.95	289.5
47	83	-10389	955	-269	0	-198	-4428	15.71	15.71	9.42	9.42	-14.86	236.8
49	83	-10210	1143	-279	0	-209	-4707	15.71	15.71	9.42	9.42	-15.85	279.3
50	83	-11060	856	-282	0	-208	-4509	15.71	15.71	9.42	9.42	-15.10	225.9
51	83	-10390	954	-209	0	-158	-4430	15.71	15.71	9.42	9.42	-14.86	236.9

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	165	-13330	2149	-507	0	14	-6479	15.71	15.71	9.42	9.42	-21.85	409.8
41	165	-13860	1722	-476	0	20	-6056	15.71	15.71	9.42	9.42	-20.35	335.2
42	165	-13870	1720	-296	0	-8	-6060	15.71	15.71	9.42	9.42	-20.36	335.2
43	165	-10912	2051	-425	0	13	-5556	15.71	15.71	9.42	9.42	-18.76	370.1
44	165	-15170	1071	-438	0	28	-5563	15.71	15.71	9.42	9.42	-18.53	-243.8
45	165	-11800	1335	-73	0	-25	-4854	15.71	15.71	9.42	9.42	-16.26	246.4
46	165	-10551	1108	-310	0	23	-4124	15.71	15.71	9.42	9.42	-13.78	193.4
47	165	-9728	955	-269	0	24	-3640	15.71	15.71	9.42	9.42	-12.14	-159.3
49	165	-9550	1098	-279	0	22	-3782	15.71	15.71	9.42	9.42	-12.65	181.2
50	165	-10400	902	-282	0	25	-3784	15.71	15.71	9.42	9.42	-12.60	-165.9
51	165	-9729	954	-209	0	14	-3642	15.71	15.71	9.42	9.42	-12.14	-159.4

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	248	-12670	2012	-507	0	433	-4764	15.71	15.71	9.42	9.42	-15.89	209.5
41	248	-13200	1722	-476	0	412	-4636	15.71	15.71	9.42	9.42	-15.41	-203.7
42	248	-13210	1720	-296	0	236	-4641	15.71	15.71	9.42	9.42	-15.42	-203.9
43	248	-10254	1821	-425	0	363	-3959	15.71	15.71	9.42	9.42	-13.22	182.0
44	248	-14510	1301	-438	0	390	-4585	15.71	15.71	9.42	9.42	-15.17	-202.8
45	248	-11140	1335	-73	0	35	-3752	15.71	15.71	9.42	9.42	-12.44	-165.2
46	248	-9892	1108	-310	0	279	-3210	15.71	15.71	9.42	9.42	-10.63	-141.7
47	248	-9066	955	-269	0	246	-2853	15.71	15.71	9.42	9.42	-9.44	-126.2
49	248	-8890	1052	-279	0	252	-2896	15.71	15.71	9.42	9.42	-9.59	-127.8
50	248	-9740	947	-282	0	258	-3022	15.71	15.71	9.42	9.42	-9.99	-133.8
51	248	-9068	954	-209	0	187	-2854	15.71	15.71	9.42	9.42	-9.44	-126.3

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	330	-12010	1874	-507	0	851	-3162	15.71	15.71	9.42	9.42	-10.48	-142.5
41	330	-12540	1722	-476	0	804	-3216	15.71	15.71	9.42	9.42	-10.67	-145.5
42	330	-12550	1720	-296	0	480	-3222	15.71	15.71	9.42	9.42	-10.69	-145.8
43	330	-9595	1592	-425	0	714	-2551	15.71	15.71	9.42	9.42	-8.45	-114.8
44	330	-13850	1530	-438	0	751	-3417	15.71	15.71	9.42	9.42	-11.38	-155.6
45	330	-10480	1335	-73	0	95	-2650	15.71	15.71	9.42	9.42	-8.80	-120.2
46	330	-9232	1108	-310	0	535	-2295	15.71	15.71	9.42	9.42	-7.64	-104.4
47	330	-8405	955	-269	0	467	-2065	15.71	15.71	9.42	9.42	-6.88	-94.1
49	330	-8230	1006	-279	0	483	-2047	15.71	15.71	9.42	9.42	-6.81	-93.1
50	330	-9080	993	-282	0	490	-2221	15.71	15.71	9.42	9.42	-7.40	-101.3
51	330	-8408	954	-209	0	359	-2067	15.71	15.71	9.42	9.42	-6.88	-94.2

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 21 NI 221 NF 223 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 27C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	

40	0	-12890	3385	-1431	0	-2661	-13360	15.71	15.71	9.42	9.42	-44.83	1437.6
41	0	-13660	2280	-1311	0	-2402	-10600	15.71	15.71	9.42	9.42	-35.82	990.6
42	0	-13780	2344	-1111	0	-2064	-10850	15.71	15.71	9.42	9.42	-36.65	1022.6
43	0	-10640	3622	-1245	0	-2411	-13000	15.71	15.71	9.42	9.42	-43.40	1484.8
44	0	-15310	515	-1154	0	-2039	-6354	15.71	15.71	9.42	9.42	-21.30	326.9
45	0	-12130	1887	-711	0	-1417	-8815	15.71	15.71	9.42	9.42	-29.82	791.2
46	0	-10880	1479	-885	0	-1728	-7075	15.71	15.71	9.42	9.42	-23.95	587.8
47	0	-10190	1279	-779	0	-1560	-6194	15.71	15.71	9.42	9.42	-20.97	487.9
49	0	-9931	1648	-819	0	-1646	-7116	15.71	15.71	9.42	9.42	-24.07	632.9
50	0	-10870	1026	-800	0	-1571	-5786	15.71	15.71	9.42	9.42	-19.56	403.7
51	0	-10230	1301	-712	0	-1447	-6278	15.71	15.71	9.42	9.42	-21.25	498.5

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	83	-12230	3247	-1431	0	-1480	-10625	15.71	15.71	9.42	9.42	-35.82	1055.9
41	83	-13000	2280	-1311	0	-1320	-8719	15.71	15.71	9.42	9.42	-29.51	741.1
42	83	-13120	2344	-1111	0	-1148	-8916	15.71	15.71	9.42	9.42	-30.18	764.9
43	83	-9980	3393	-1245	0	-1384	-10108	15.71	15.71	9.42	9.42	-33.94	1077.4
44	83	-14650	745	-1154	0	-1088	-5834	15.71	15.71	9.42	9.42	-19.51	281.9
45	83	-11471	1887	-711	0	-830	-7258	15.71	15.71	9.42	9.42	-24.57	590.5
46	83	-10220	1479	-885	0	-998	-5855	15.71	15.71	9.42	9.42	-19.81	438.1
47	83	-9530	1279	-779	0	-918	-5139	15.71	15.71	9.42	9.42	-17.37	363.2
49	83	-9271	1602	-819	0	-970	-5775	15.71	15.71	9.42	9.42	-19.55	464.2
50	83	-10209	1072	-800	0	-911	-4920	15.71	15.71	9.42	9.42	-16.59	308.2
51	83	-9570	1301	-712	0	-860	-5205	15.71	15.71	9.42	9.42	-17.60	371.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	165	-11570	3110	-1431	0	-299	-8004	15.71	15.71	9.42	9.42	-27.09	695.3
41	165	-12340	2280	-1311	0	-239	-6838	15.71	15.71	9.42	9.42	-23.13	496.3
42	165	-12460	2344	-1111	0	-231	-6982	15.71	15.71	9.42	9.42	-23.62	512.0
43	165	-9320	3164	-1245	0	-356	-7405	15.71	15.71	9.42	9.42	-25.01	701.4
44	165	-13990	974	-1154	0	-136	-5125	15.71	15.71	9.42	9.42	-17.07	-224.6
45	165	-10812	1887	-711	0	-244	-5701	15.71	15.71	9.42	9.42	-19.27	394.0
46	165	-9561	1479	-885	0	-268	-4634	15.71	15.71	9.42	9.42	-15.63	292.2
47	165	-8869	1279	-779	0	-275	-4084	15.71	15.71	9.42	9.42	-13.75	242.0
49	165	-8611	1556	-819	0	-295	-4473	15.71	15.71	9.42	9.42	-15.11	304.3
50	165	-9548	1118	-800	0	-250	-4017	15.71	15.71	9.42	9.42	-13.47	210.8
51	165	-8910	1301	-712	0	-272	-4132	15.71	15.71	9.42	9.42	-13.91	247.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	248	-10910	2972	-1431	0	882	-5496	15.71	15.71	9.42	9.42	-18.56	361.9
41	248	-11680	2280	-1311	0	843	-4958	15.71	15.71	9.42	9.42	-16.63	263.5
42	248	-11800	2344	-1111	0	686	-5048	15.71	15.71	9.42	9.42	-16.94	271.3
43	248	-8661	2934	-1245	0	671	-4891	15.71	15.71	9.42	9.42	-16.55	361.2
44	248	-13330	1204	-1154	0	816	-4227	15.71	15.71	9.42	9.42	-13.99	-186.9
45	248	-10153	1887	-711	0	343	-4144	15.71	15.71	9.42	9.42	-13.88	208.0
46	248	-8902	1479	-885	0	463	-3414	15.71	15.71	9.42	9.42	-11.40	155.3
47	248	-8208	1279	-779	0	368	-3028	15.71	15.71	9.42	9.42	-10.09	-132.6
49	248	-7951	1510	-819	0	381	-3208	15.71	15.71	9.42	9.42	-10.74	158.2
50	248	-8886	1164	-800	0	410	-3075	15.71	15.71	9.42	9.42	-10.21	-135.2
51	248	-8250	1301	-712	0	315	-3058	15.71	15.71	9.42	9.42	-10.19	-133.9

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	330	-10250	2835	-1431	0	2063	-3102	15.71	15.71	9.42	9.42	-12.92	147.1
41	330	-11020	2280	-1311	0	1924	-3077	15.71	15.71	9.42	9.42	-12.05	-139.4
42	330	-11140	2344	-1111	0	1602	-3114	15.71	15.71	9.42	9.42	-10.29	-139.3
43	330	-8001	2705	-1245	0	1698	-2566	15.71	15.71	9.42	9.42	-10.63	130.3
44	330	-12670	1433	-1154	0	1767	-3139	15.71	15.71	9.42	9.42	-11.13	-142.8
45	330	-9494	1887	-711	0	930	-2587	15.71	15.71	9.42	9.42	-8.56	-116.1
46	330	-8242	1479	-885	0	1193	-2194	15.71	15.71	9.42	9.42	-7.50	-98.7
47	330	-7548	1279	-779	0	1010	-1973	15.71	15.71	9.42	9.42	-6.54	-89.0
49	330	-7291	1464	-819	0	1056	-1981	15.71	15.71	9.42	9.42	-6.64	-88.9
50	330	-8225	1210	-800	0	1070	-2096	15.71	15.71	9.42	9.42	-6.96	-94.9
51	330	-7590	1301	-712	0	902	-1985	15.71	15.71	9.42	9.42	-6.58	-89.5

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 22 NI 264 NF 266 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 25C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-9408	425	-326	0	-934	-984	6.28	6.28	9.42	9.42	-15.30	-168.0
41	0	-8091	-14	-276	0	-833	-220	6.28	6.28	9.42	9.42	-7.87	-108.5
42	0	-7922	-12	-306	0	-622	-221	6.28	6.28	9.42	9.42	-6.82	-95.2
43	0	-9655	787	-386	0	-898	-1589	6.28	6.28	9.42	9.42	-25.01	307.7
44	0	-6024	-752	-192	0	-683	1067	6.28	6.28	9.42	9.42	-16.83	225.4
45	0	-7179	60	-353	0	-378	-316	6.28	6.28	9.42	9.42	-6.35	-80.8
46	0	-7084	98	-321	0	-666	-371	6.28	6.28	9.42	9.42	-6.81	-91.4
47	0	-6832	126	-332	0	-625	-409	6.28	6.28	9.42	9.42	-7.07	-87.2
49	0	-7270	272	-348	0	-659	-664	6.28	6.28	9.42	9.42	-10.38	-118.2
50	0	-6544	-36	-310	0	-616	-133	6.28	6.28	9.42	9.42	-6.10	-84.5
51	0	-6775	127	-342	0	-555	-410	6.28	6.28	9.42	9.42	-7.05	-86.7

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	95	-8980	345	-326	0	-625	-618	6.28	6.28	9.42	9.42	-10.17	-122.7
41	95	-7664	-14	-276	0	-570	-233	6.28	6.28	9.42	9.42	-6.45	-90.3
42	95	-7494	-12	-221	0	-373	-232	6.28	6.28	9.42	9.42	-5.73	-77.8
43	95	-9228	655	-386	0	-531	-904	6.28	6.28	9.42	9.42	-14.07	-157.3
44	95	-5596	-620	-192	0	-500	415	6.28	6.28	9.42	9.42	-6.69	-79.7
45	95	-6752	60	-212	0	-111	-259	6.28	6.28	9.42	9.42	-5.62	-72.4
46	95	-6656	98	-321	0	-362	-279	6.28	6.28	9.42	9.42	-5.75	-73.5
47	95	-6404	126	-332	0	-310	-290	6.28	6.28	9.42	9.42	-5.74	-72.7
49	95	-6842	246	-348	0	-328	-418	6.28	6.28	9.42	9.42	-7.17	-88.0
50	95	-6116	-9	-310	0	-322	-155	6.28	6.28	9.42	9.42	-4.54	-64.5
51	95	-6348	127	-314	0	-244	-289	6.28	6.28	9.42	9.42	-5.71	-72.3

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	190	-8553	266	-326	0	-315	-328	6.28	6.28	9.42	9.42	-7.12	-91.7

41	190	-7236	-14	-276	0	-308	-247	6.28	6.28	9.42	9.42	-5.74	-74.8
42	190	-7067	-12	-148	0	-199	-243	6.28	6.28	9.42	9.42	-5.63	-73.2
43	190	-8800	523	-386	0	-164	-344	6.28	6.28	9.42	9.42	-7.38	-95.0
44	190	-5169	-488	-192	0	-318	-112	6.28	6.28	9.42	9.42	-4.05	-57.1
45	190	-6324	60	-90	0	31	-202	6.28	6.28	9.42	9.42	-4.89	-64.1
46	190	-6229	98	-321	0	-57	-186	6.28	6.28	9.42	9.42	-4.70	-61.9
47	190	-5977	126	-332	0	6	-170	6.28	6.28	9.42	9.42	-4.43	-58.7
49	190	-6415	219	-348	0	3	-197	6.28	6.28	9.42	9.42	-4.89	-64.3
50	190	-5689	17	-310	0	-28	-151	6.28	6.28	9.42	9.42	-4.12	-54.8
51	190	-5920	127	-289	0	42	-169	6.28	6.28	9.42	9.42	-4.39	-58.2

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	285	-8126	187	-326	0	-6	-113	6.28	6.28	9.42	9.42	-4.94	-68.9
41	285	-6808	-14	-276	0	-45	-261	6.28	6.28	9.42	9.42	-5.67	-73.0
42	285	-6640	-12	-88	0	-88	-254	6.28	6.28	9.42	9.42	-5.52	-71.2
43	285	-8372	391	-386	0	203	91	6.28	6.28	9.42	9.42	-5.14	-74.8
44	285	-4742	-356	-192	0	-136	-513	6.28	6.28	9.42	9.42	-7.98	-86.8
45	285	-5896	60	10	0	67	-145	6.28	6.28	9.42	9.42	-4.16	-55.8
46	285	-5802	98	-321	0	248	-93	6.28	6.28	9.42	9.42	-4.05	-57.9
47	285	-5550	126	-332	0	321	-51	6.28	6.28	9.42	9.42	-4.26	-60.2
49	285	-5988	193	-348	0	334	-1	6.28	6.28	9.42	9.42	-4.54	-64.2
50	285	-5262	43	-310	0	266	-122	6.28	6.28	9.42	9.42	-3.86	-54.9
51	285	-5492	127	-269	0	307	-49	6.28	6.28	9.42	9.42	-4.16	-58.9

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	380	-7698	108	-326	0	304	27	6.28	6.28	9.42	9.42	-5.26	-75.4
41	380	-6381	-14	-276	0	218	-275	6.28	6.28	9.42	9.42	-5.59	-71.2
42	380	-6212	-12	-39	0	-28	-265	6.28	6.28	9.42	9.42	-5.42	-69.1
43	380	-7945	259	-386	0	571	400	6.28	6.28	9.42	9.42	-7.49	-93.9
44	380	-4314	-224	-192	0	46	-789	6.28	6.28	9.42	9.42	-12.46	172.6
45	380	-5469	60	91	0	17	-87	6.28	6.28	9.42	9.42	-3.43	-47.4
46	380	-5374	98	-321	0	553	0	6.28	6.28	9.42	9.42	-5.22	-72.1
47	380	-5122	126	-332	0	637	69	6.28	6.28	9.42	9.42	-5.50	-75.1
49	380	-5560	166	-348	0	665	169	6.28	6.28	9.42	9.42	-5.84	-80.0
50	380	-4834	70	-310	0	560	-69	6.28	6.28	9.42	9.42	-4.99	-68.4
51	380	-5065	127	-253	0	555	72	6.28	6.28	9.42	9.42	-5.08	-69.8

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 23 NI 298 NF 271 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 20C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-10770	915	-133	0	-2025	-1483	6.28	6.28	12.57	12.57	-12.45	-163.8
41	0	-11170	-229	-160	0	-1943	549	6.28	6.28	12.57	12.57	-12.00	-159.4
42	0	-11100	-231	-520	0	-1303	553	6.28	6.28	12.57	12.57	-8.97	-122.8
43	0	-9783	1730	-71	0	-1609	-2945	6.28	6.28	12.57	12.57	-23.90	406.5
44	0	-12060	-2150	-214	0	-1892	3959	6.28	6.28	12.57	12.57	-32.06	581.6
45	0	-10340	-181	-716	0	-406	448	6.28	6.28	12.57	12.57	-5.94	-80.8
46	0	-10010	-148	-90	0	-1190	377	6.28	6.28	12.57	12.57	-8.15	-111.5
47	0	-9718	-127	-73	0	-1002	334	6.28	6.28	12.57	12.57	-7.34	-101.2
49	0	-9586	254	-64	0	-1029	-344	6.28	6.28	12.57	12.57	-7.39	-101.6
50	0	-10040	-521	-92	0	-1086	1037	6.28	6.28	12.57	12.57	-8.98	-113.9
51	0	-9697	-128	-193	0	-789	335	6.28	6.28	12.57	12.57	-6.57	-91.5

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	95	-10200	915	-133	0	-1898	-614	6.28	6.28	12.57	12.57	-11.67	-153.8
41	95	-10599	-229	-160	0	-1790	331	6.28	6.28	12.57	12.57	-11.10	-147.8
42	95	-10531	-231	-352	0	-891	334	6.28	6.28	12.57	12.57	-7.26	-100.9
43	95	-9213	1730	-71	0	-1542	-1302	6.28	6.28	12.57	12.57	-10.75	-129.9
44	95	-11490	-2150	-214	0	-1688	1917	6.28	6.28	12.57	12.57	-15.71	-184.0
45	95	-9769	-181	-435	0	138	276	6.28	6.28	12.57	12.57	-4.88	-68.1
46	95	-9440	-148	-90	0	-1104	236	6.28	6.28	12.57	12.57	-7.61	-104.2
47	95	-9148	-127	-73	0	-933	213	6.28	6.28	12.57	12.57	-6.87	-94.8
49	95	-9016	254	-64	0	-969	-102	6.28	6.28	12.57	12.57	-6.95	-95.6
50	95	-9470	-521	-92	0	-998	542	6.28	6.28	12.57	12.57	-7.23	-99.6
51	95	-9127	-128	-137	0	-633	214	6.28	6.28	12.57	12.57	-5.79	-81.2

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	190	-9631	915	-133	0	-1772	256	6.28	6.28	12.57	12.57	-10.90	-143.8
41	190	-10028	-229	-160	0	-1638	113	6.28	6.28	12.57	12.57	-10.20	-136.3
42	190	-9962	-231	-208	0	-627	114	6.28	6.28	12.57	12.57	-6.09	-85.8
43	190	-8643	1730	-71	0	-1474	341	6.28	6.28	12.57	12.57	-9.12	-121.4
44	190	-10920	-2150	-214	0	-1484	-126	6.28	6.28	12.57	12.57	-9.66	-131.1
45	190	-9198	-181	-195	0	434	104	6.28	6.28	12.57	12.57	-5.11	-72.7
46	190	-8869	-148	-90	0	-1018	96	6.28	6.28	12.57	12.57	-7.08	-97.0
47	190	-8578	-127	-73	0	-864	92	6.28	6.28	12.57	12.57	-6.41	-88.4
49	190	-8446	254	-64	0	-908	140	6.28	6.28	12.57	12.57	-6.51	-89.6
50	190	-8900	-521	-92	0	-910	46	6.28	6.28	12.57	12.57	-6.70	-92.3
51	190	-8557	-128	-88	0	-527	92	6.28	6.28	12.57	12.57	-5.19	-73.2

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	285	-9062	915	-133	0	-1646	1126	6.28	6.28	12.57	12.57	-10.13	-133.9
41	285	-9458	-229	-160	0	-1486	-105	6.28	6.28	12.57	12.57	-9.31	-124.9
42	285	-9392	-231	-88	0	-489	-105	6.28	6.28	12.57	12.57	-5.38	-76.3
43	285	-8073	1730	-71	0	-1406	1984	6.28	6.28	12.57	12.57	-16.17	228.4
44	285	-10350	-2150	-214	0	-1281	-2168	6.28	6.28	12.57	12.57	-17.70	206.5
45	285	-8626	-181	5	0	521	-68	6.28	6.28	12.57	12.57	-5.20	-73.3
46	285	-8298	-148	-90	0	-933	-44	6.28	6.28	12.57	12.57	-6.55	-89.9
47	285	-8008	-127	-73	0	-794	-29	6.28	6.28	12.57	12.57	-5.94	-82.0
49	285	-7876	254	-64	0	-848	381	6.28	6.28	12.57	12.57	-6.08	-83.6
50	285	-8331	-521	-92	0	-823	-449	6.28	6.28	12.57	12.57	-6.16	-85.1
51	285	-7987	-128	-49	0	-462	-29	6.28	6.28	12.57	12.57	-4.74	-67.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	380	-8492	915	-133	0	-1519	1995	6.28	6.28	12.57	12.57	-16.27	218.8
41	380	-8887	-229	-160	0	-1333	-322	6.28	6.28	12.57	12.57	-8.44	-113.7

42	380	-8823	-231	8	0	-453	-325	6.28	6.28	12.57	12.57	-5.03	-71.4
43	380	-7503	1730	-71	0	-1339	3627	6.28	6.28	12.57	12.57	-29.02	652.8
44	380	-9780	-2150	-214	0	-1077	-4210	6.28	6.28	12.57	12.57	-33.81	720.6
45	380	-8055	-181	164	0	437	-240	6.28	6.28	12.57	12.57	-4.68	-66.3
46	380	-7728	-148	-90	0	-847	-184	6.28	6.28	12.57	12.57	-6.02	-82.7
47	380	-7438	-127	-73	0	-725	-150	6.28	6.28	12.57	12.57	-5.47	-75.6
49	380	-7306	254	-64	0	-787	623	6.28	6.28	12.57	12.57	-5.74	-77.6
50	380	-7761	-521	-92	0	-735	-944	6.28	6.28	12.57	12.57	-7.92	-98.2
51	380	-7417	-128	-17	0	-432	-150	6.28	6.28	12.57	12.57	-4.41	-62.3

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 24 NI 78 NF 77 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 6B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	--												
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-25680	301	50	0	81	10890	15.71	15.71	9.42	9.42	-36.53	578.0
41	0	-22420	-1031	9	0	-6	12590	15.71	15.71	9.42	9.42	-42.60	925.1
42	0	-22540	-931	200	0	447	12360	15.71	15.71	9.42	9.42	-41.80	888.0
43	0	-25860	1392	87	0	168	7441	15.71	15.71	9.42	9.42	-24.59	-331.8
44	0	-17440	-3285	-62	0	-155	15820	15.71	15.71	9.42	9.42	-53.28	1605.8
45	0	-20620	-662	336	0	778	9885	15.71	15.71	9.42	9.42	-33.32	615.2
46	0	-19230	-707	24	0	39	8874	15.71	15.71	9.42	9.42	-29.88	527.3
47	0	-18440	-626	27	0	51	7945	15.71	15.71	9.42	9.42	-26.67	431.2
49	0	-19520	-182	41	0	80	7379	15.71	15.71	9.42	9.42	-24.61	327.5
50	0	-17840	-1118	11	0	16	9055	15.71	15.71	9.42	9.42	-30.58	601.2
51	0	-18470	-593	91	0	202	7868	15.71	15.71	9.42	9.42	-26.40	420.3

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	110	-24800	48	50	0	25	11083	15.71	15.71	9.42	9.42	-37.27	632.0
41	110	-21540	-1031	9	0	-16	11456	15.71	15.71	9.42	9.42	-38.72	798.6
42	110	-21660	-931	200	0	227	11336	15.71	15.71	9.42	9.42	-38.31	777.4
43	110	-24980	970	87	0	71	8740	15.71	15.71	9.42	9.42	-29.04	-384.0
44	110	-16560	-2862	-62	0	-87	12439	15.71	15.71	9.42	9.42	-42.05	1140.0
45	110	-19740	-662	336	0	408	9156	15.71	15.71	9.42	9.42	-30.83	547.6
46	110	-18350	-707	24	0	13	8096	15.71	15.71	9.42	9.42	-27.21	453.9
47	110	-17560	-626	27	0	21	7256	15.71	15.71	9.42	9.42	-24.31	370.9
49	110	-18640	-267	41	0	35	7132	15.71	15.71	9.42	9.42	-23.80	323.0
50	110	-16960	-1033	11	0	3	7872	15.71	15.71	9.42	9.42	-26.51	471.2
51	110	-17590	-593	91	0	102	7216	15.71	15.71	9.42	9.42	-24.17	364.8

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	220	-23920	-206	50	0	-30	10998	15.71	15.71	9.42	9.42	-37.02	650.5
41	220	-20660	-1031	9	0	-26	10322	15.71	15.71	9.42	9.42	-34.84	673.5
42	220	-20780	-931	200	0	8	10312	15.71	15.71	9.42	9.42	-34.80	667.8
43	220	-24100	547	87	0	-25	9574	15.71	15.71	9.42	9.42	-32.02	460.8
44	220	-15680	-2440	-62	0	-19	9523	15.71	15.71	9.42	9.42	-32.24	749.7
45	220	-18860	-662	336	0	38	8428	15.71	15.71	9.42	9.42	-28.34	480.6
46	220	-17470	-707	24	0	-13	7318	15.71	15.71	9.42	9.42	-24.53	381.6
47	220	-16680	-626	27	0	-9	6566	15.71	15.71	9.42	9.42	-21.95	311.6
49	220	-17760	-351	41	0	-11	6792	15.71	15.71	9.42	9.42	-22.67	307.4
50	220	-16080	-949	11	0	-10	6782	15.71	15.71	9.42	9.42	-22.75	357.2
51	220	-16710	-593	91	0	2	6563	15.71	15.71	9.42	9.42	-21.94	310.2

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	330	-23040	-459	50	0	-85	10633	15.71	15.71	9.42	9.42	-35.80	631.9
41	330	-19780	-1031	9	0	-35	9188	15.71	15.71	9.42	9.42	-30.94	550.4
42	330	-19900	-931	200	0	-212	9288	15.71	15.71	9.42	9.42	-31.28	559.7
43	330	-23220	125	87	0	-121	9943	15.71	15.71	9.42	9.42	-33.37	535.1
44	330	-14800	-2018	-62	0	48	7072	15.71	15.71	9.42	9.42	-23.84	438.4
45	330	-17980	-662	336	0	-332	7700	15.71	15.71	9.42	9.42	-25.84	414.4
46	330	-16590	-707	24	0	-39	6539	15.71	15.71	9.42	9.42	-21.86	310.9
47	330	-15800	-626	27	0	-39	5877	15.71	15.71	9.42	9.42	-19.59	-257.3
49	330	-16880	-436	41	0	-56	6359	15.71	15.71	9.42	9.42	-21.21	280.6
50	330	-15200	-864	11	0	-22	5785	15.71	15.71	9.42	9.42	-19.30	259.7
51	330	-15830	-593	91	0	-98	5910	15.71	15.71	9.42	9.42	-19.70	-258.7

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	440	-22160	-712	50	0	-141	9990	15.71	15.71	9.42	9.42	-33.60	576.2
41	440	-18900	-1031	9	0	-45	8054	15.71	15.71	9.42	9.42	-27.03	430.5
42	440	-19020	-931	200	0	-431	8264	15.71	15.71	9.42	9.42	-27.75	453.8
43	440	-22340	-298	87	0	-217	9848	15.71	15.71	9.42	9.42	-33.10	551.5
44	440	-13920	-1595	-62	0	116	5085	15.71	15.71	9.42	9.42	-16.93	-222.9
45	440	-17100	-662	336	0	-701	6971	15.71	15.71	9.42	9.42	-23.34	349.2
46	440	-15710	-707	24	0	-65	5761	15.71	15.71	9.42	9.42	-19.19	-252.4
47	440	-14920	-626	27	0	-70	5188	15.71	15.71	9.42	9.42	-17.23	-228.0
49	440	-16000	-520	41	0	-102	5833	15.71	15.71	9.42	9.42	-19.42	-255.7
50	440	-14320	-780	11	0	-35	4881	15.71	15.71	9.42	9.42	-16.20	-214.8
51	440	-14950	-593	91	0	-198	5258	15.71	15.71	9.42	9.42	-17.47	-231.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 25 NI 121 NF 120 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 5B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	--												
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-27960	-410	-71	0	-201	17880	15.71	15.71	9.42	9.42	-60.53	1466.8
41	0	-24660	-1924	-77	0	-209	21150	15.71	15.71	9.42	9.42	-71.32	2088.2
42	0	-24690	-1926	115	0	245	21180	15.71	15.71	9.42	9.42	-71.42	2091.3
43	0	-27740	998	-47	0	-146	11600	15.71	15.71	9.42	9.42	-38.89	603.4
44	0	-19680	-4514	-91	0	-228	27320	15.71	15.71	9.42	9.42	-90.83	3243.3
45	0	-22280	-1529	262	0	597	17110	15.71	15.71	9.42	9.42	-57.82	1589.1

46	0	-20770	-1286	-48	0	-130	14590	15.71	15.71	9.42	9.42	-49.37	1280.7
47	0	-19800	-1127	-40	0	-110	12950	15.71	15.71	9.42	9.42	-43.84	1080.6
49	0	-20900	-622	-38	0	-107	11860	15.71	15.71	9.42	9.42	-40.13	880.0
50	0	-19290	-1725	-47	0	-123	15000	15.71	15.71	9.42	9.42	-50.68	1403.5
51	0	-19810	-1128	24	0	42	12960	15.71	15.71	9.42	9.42	-43.87	1081.7

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	110	-27080	-663	-71	0	-123	17288	15.71	15.71	9.42	9.42	-58.53	1416.4
41	110	-23780	-1924	-77	0	-124	19032	15.71	15.71	9.42	9.42	-64.27	1810.5
42	110	-23810	-1926	115	0	118	19062	15.71	15.71	9.42	9.42	-64.38	1813.7
43	110	-26860	576	-47	0	-93	12464	15.71	15.71	9.42	9.42	-41.97	745.8
44	110	-18800	-4092	-91	0	-128	22586	15.71	15.71	9.42	9.42	-75.44	2565.3
45	110	-21400	-1529	262	0	308	15428	15.71	15.71	9.42	9.42	-52.19	1377.6
46	110	-19890	-1286	-48	0	-77	13174	15.71	15.71	9.42	9.42	-44.60	1109.7
47	110	-18920	-1127	-40	0	-65	11710	15.71	15.71	9.42	9.42	-39.65	936.2
49	110	-20020	-707	-38	0	-65	11129	15.71	15.71	9.42	9.42	-37.65	810.0
50	110	-18410	-1640	-47	0	-72	13150	15.71	15.71	9.42	9.42	-44.49	1167.2
51	110	-18930	-1128	24	0	15	11720	15.71	15.71	9.42	9.42	-39.68	937.2

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	220	-26200	-916	-71	0	-46	16418	15.71	15.71	9.42	9.42	-55.58	1325.6
41	220	-22900	-1924	-77	0	-39	16915	15.71	15.71	9.42	9.42	-57.20	1534.1
42	220	-22930	-1926	115	0	-9	16945	15.71	15.71	9.42	9.42	-57.30	1537.2
43	220	-25980	153	-47	0	-41	12864	15.71	15.71	9.42	9.42	-43.41	831.1
44	220	-17920	-3670	-91	0	-28	18316	15.71	15.71	9.42	9.42	-61.48	1959.7
45	220	-20520	-1529	262	0	20	13745	15.71	15.71	9.42	9.42	-46.53	1167.2
46	220	-19010	-1286	-48	0	-24	11759	15.71	15.71	9.42	9.42	-39.81	939.7
47	220	-18040	-1127	-40	0	-21	10470	15.71	15.71	9.42	9.42	-35.44	792.7
49	220	-19140	-791	-38	0	-23	10304	15.71	15.71	9.42	9.42	-34.84	727.1
50	220	-17530	-1556	-47	0	-20	11393	15.71	15.71	9.42	9.42	-38.57	946.1
51	220	-18050	-1128	24	0	-11	10479	15.71	15.71	9.42	9.42	-35.47	793.6

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	330	-25320	-1170	-71	0	32	15268	15.71	15.71	9.42	9.42	-51.69	1194.8
41	330	-22020	-1924	-77	0	46	14798	15.71	15.71	9.42	9.42	-50.09	1259.5
42	330	-22050	-1926	115	0	-136	14828	15.71	15.71	9.42	9.42	-50.19	1262.6
43	330	-25100	-269	-47	0	11	12799	15.71	15.71	9.42	9.42	-43.23	854.0
44	330	-17040	-3247	-91	0	72	14511	15.71	15.71	9.42	9.42	-48.94	1427.4
45	330	-19640	-1529	262	0	-269	12062	15.71	15.71	9.42	9.42	-40.84	958.4
46	330	-18130	-1286	-48	0	28	10343	15.71	15.71	9.42	9.42	-35.00	771.2
47	330	-17160	-1127	-40	0	24	9230	15.71	15.71	9.42	9.42	-31.21	650.7
49	330	-18260	-876	-38	0	19	9387	15.71	15.71	9.42	9.42	-31.71	631.8
50	330	-16650	-1472	-47	0	31	9728	15.71	15.71	9.42	9.42	-32.93	741.0
51	330	-17170	-1128	24	0	-37	9238	15.71	15.71	9.42	9.42	-31.24	651.6

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	440	-24440	-1423	-71	0	110	13840	15.71	15.71	9.42	9.42	-46.83	1024.9
41	440	-21140	-1924	-77	0	132	12680	15.71	15.71	9.42	9.42	-42.92	987.8
42	440	-21170	-1926	115	0	-263	12710	15.71	15.71	9.42	9.42	-43.03	991.0
43	440	-24220	-691	-47	0	63	12270	15.71	15.71	9.42	9.42	-41.43	812.9
44	440	-16160	-2825	-91	0	172	11170	15.71	15.71	9.42	9.42	-37.80	969.7
45	440	-18760	-1529	262	0	-558	10380	15.71	15.71	9.42	9.42	-35.11	752.2
46	440	-17250	-1286	-48	0	81	8928	15.71	15.71	9.42	9.42	-30.16	605.2
47	440	-16280	-1127	-40	0	68	7990	15.71	15.71	9.42	9.42	-26.96	511.0
49	440	-17380	-960	-38	0	61	8377	15.71	15.71	9.42	9.42	-28.25	524.7
50	440	-15770	-1387	-47	0	83	8157	15.71	15.71	9.42	9.42	-27.56	552.6
51	440	-16290	-1128	24	0	-63	7998	15.71	15.71	9.42	9.42	-26.98	511.8

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 26 NI 164 NF 163 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 4B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	

40	0	-28260	-614	-80	0	-237	19480	15.71	15.71	9.42	9.42	-65.93	1688.0
41	0	-24850	-2198	-83	0	-233	23130	15.71	15.71	9.42	9.42	-77.84	2376.3
42	0	-24790	-2186	90	0	178	22980	15.71	15.71	9.42	9.42	-77.34	2356.5
43	0	-28060	898	-62	0	-192	12530	15.71	15.71	9.42	9.42	-42.13	713.8
44	0	-19700	-4917	-89	0	-231	30010	15.71	15.71	9.42	9.42	-99.47	3651.4
45	0	-22290	-1723	221	0	500	18360	15.71	15.71	9.42	9.42	-61.97	1774.5
46	0	-20900	-1470	-57	0	-156	15920	15.71	15.71	9.42	9.42	-53.81	1471.4
47	0	-19920	-1288	-50	0	-137	14120	15.71	15.71	9.42	9.42	-47.77	1246.9
49	0	-21050	-760	-50	0	-138	12900	15.71	15.71	9.42	9.42	-43.67	1023.1
50	0	-19380	-1923	-55	0	-146	16390	15.71	15.71	9.42	9.42	-55.29	1606.5
51	0	-19900	-1284	7	0	-0	14060	15.71	15.71	9.42	9.42	-47.57	1238.9

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	110	-27380	-867	-80	0	-148	18666	15.71	15.71	9.42	9.42	-63.18	1605.0
41	110	-23970	-2198	-83	0	-142	20712	15.71	15.71	9.42	9.42	-69.83	2052.8
42	110	-23910	-2186	90	0	80	20575	15.71	15.71	9.42	9.42	-69.38	2034.8
43	110	-27180	475	-62	0	-123	13287	15.71	15.71	9.42	9.42	-44.82	846.0
44	110	-18820	-4494	-89	0	-134	24836	15.71	15.71	9.42	9.42	-82.70	2905.6
45	110	-21410	-1723	221	0	258	16465	15.71	15.71	9.42	9.42	-55.64	1530.5
46	110	-20020	-1470	-57	0	-94	14303	15.71	15.71	9.42	9.42	-48.39	1269.7
47	110	-19040	-1288	-50	0	-82	12702	15.71	15.71	9.42	9.42	-43.00	1075.5
49	110	-20170	-844	-50	0	-84	12017	15.71	15.71	9.42	9.42	-40.68	930.9
50	110	-18500	-1838	-55	0	-86	14323	15.71	15.71	9.42	9.42	-48.40	1336.6
51	110	-19020	-1284	7	0	-8	12649	15.71	15.71	9.42	9.42	-42.82	1068.5

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	220	-26500	-1121	-80	0	-60	17573	15.71	15.71	9.42	9.42	-59.49	1481.3
41	220	-23090	-2198	-83	0	-51	18295	15.71	15.71	9.42	9.42	-61.80	1730.5
42	220	-23030	-2186	90	0	-19	18170	15.71	15.71	9.42	9.42	-61.38	1714.4
43	220	-26300	53	-62	0	-54	13579	15.71	15.71	9.42	9.42	-45.87	918.2
44	220	-17940	-4072	-89	0	-36	20126	15.71	15.71	9.42	9.42	-67.37	2232.0
45	220	-20530	-1723	221	0	15	14570	15.71	15.71	9.42	9.42	-49.29	1287.7
46	220	-19140	-1470	-57	0	-31	12686	15.71	15.71	9.42	9.42	-42.94	1069.0

47	220	-18160	-1288	-50	0	-26	11285	15.71	15.71	9.42	9.42	-38.21	905.1
49	220	-19290	-929	-50	0	-29	11042	15.71	15.71	9.42	9.42	-37.37	825.8
50	220	-17620	-1754	-55	0	-26	12348	15.71	15.71	9.42	9.42	-41.78	1082.2
51	220	-18140	-1284	7	0	-16	11238	15.71	15.71	9.42	9.42	-38.05	899.1

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	330	-25620	-1374	-80	0	28	16201	15.71	15.71	9.42	9.42	-54.85	1317.5
41	330	-22210	-2198	-83	0	40	15878	15.71	15.71	9.42	9.42	-53.71	1410.0
42	330	-22150	-2186	90	0	-117	15765	15.71	15.71	9.42	9.42	-53.34	1396.0
43	330	-25420	-369	-62	0	14	13407	15.71	15.71	9.42	9.42	-45.31	926.7
44	330	-17060	-3650	-89	0	61	15881	15.71	15.71	9.42	9.42	-53.44	1631.6
45	330	-19650	-1723	221	0	-228	12675	15.71	15.71	9.42	9.42	-42.91	1046.7
46	330	-18260	-1470	-57	0	31	11069	15.71	15.71	9.42	9.42	-37.47	870.0
47	330	-17280	-1288	-50	0	29	9867	15.71	15.71	9.42	9.42	-33.39	736.3
49	330	-18410	-1013	-50	0	25	9973	15.71	15.71	9.42	9.42	-33.72	708.1
50	330	-16740	-1670	-55	0	34	10467	15.71	15.71	9.42	9.42	-35.44	843.6
51	330	-17260	-1284	7	0	-23	9826	15.71	15.71	9.42	9.42	-33.25	731.2

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	440	-24740	-1628	-80	0	116	14550	15.71	15.71	9.42	9.42	-49.25	1114.6
41	440	-21330	-2198	-83	0	131	13460	15.71	15.71	9.42	9.42	-45.57	1092.8
42	440	-21270	-2186	90	0	-216	13360	15.71	15.71	9.42	9.42	-45.23	1080.7
43	440	-24540	-792	-62	0	83	12770	15.71	15.71	9.42	9.42	-43.15	870.5
44	440	-16180	-3227	-89	0	158	12100	15.71	15.71	9.42	9.42	-40.91	1105.9
45	440	-18770	-1723	221	0	-471	10780	15.71	15.71	9.42	9.42	-36.48	808.6
46	440	-17380	-1470	-57	0	94	9452	15.71	15.71	9.42	9.42	-31.96	673.7
47	440	-16400	-1288	-50	0	85	8450	15.71	15.71	9.42	9.42	-28.54	570.1
49	440	-17530	-1098	-50	0	80	8812	15.71	15.71	9.42	9.42	-29.75	578.9
50	440	-15860	-1585	-55	0	95	8678	15.71	15.71	9.42	9.42	-29.35	622.2
51	440	-16380	-1284	7	0	-31	8415	15.71	15.71	9.42	9.42	-28.42	566.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 27 NI 207 NF 206 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 3B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-27760	-377	-98	0	-267	17370	15.71	15.71	9.42	9.42	-58.81	1400.9
41	0	-24440	-1947	-93	0	-248	21090	15.71	15.71	9.42	9.42	-71.11	2088.8
42	0	-24440	-1949	64	0	135	21100	15.71	15.71	9.42	9.42	-71.14	2090.3
43	0	-27590	1075	-84	0	-232	10780	15.71	15.71	9.42	9.42	-36.02	505.3
44	0	-19430	-4631	-88	0	-223	28010	15.71	15.71	9.42	9.42	-93.01	3359.7
45	0	-22050	-1545	186	0	438	17000	15.71	15.71	9.42	9.42	-57.45	1582.6
46	0	-20610	-1298	-67	0	-173	14520	15.71	15.71	9.42	9.42	-49.13	1277.0
47	0	-19650	-1135	-60	0	-154	12870	15.71	15.71	9.42	9.42	-43.57	1075.1
49	0	-20760	-612	-62	0	-160	11630	15.71	15.71	9.42	9.42	-39.35	852.7
50	0	-19130	-1753	-63	0	-158	15080	15.71	15.71	9.42	9.42	-50.94	1422.2
51	0	-19650	-1136	-8	0	-26	12880	15.71	15.71	9.42	9.42	-43.60	1076.5

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	110	-26880	-631	-98	0	-159	16816	15.71	15.71	9.42	9.42	-56.93	1355.9
41	110	-23560	-1947	-93	0	-146	18950	15.71	15.71	9.42	9.42	-63.99	1807.7
42	110	-23560	-1949	64	0	64	18958	15.71	15.71	9.42	9.42	-64.01	1808.8
43	110	-26710	653	-84	0	-139	11732	15.71	15.71	9.42	9.42	-39.42	653.8
44	110	-18550	-4208	-88	0	-126	23148	15.71	15.71	9.42	9.42	-77.22	2661.9
45	110	-21170	-1545	186	0	234	15300	15.71	15.71	9.42	9.42	-51.75	1368.5
46	110	-19730	-1298	-67	0	-99	13092	15.71	15.71	9.42	9.42	-44.32	1104.1
47	110	-18770	-1135	-60	0	-87	11622	15.71	15.71	9.42	9.42	-39.35	929.4
49	110	-19880	-697	-62	0	-92	10911	15.71	15.71	9.42	9.42	-36.90	784.6
50	110	-18250	-1668	-63	0	-89	13197	15.71	15.71	9.42	9.42	-44.64	1180.8
51	110	-18770	-1136	-8	0	-17	11629	15.71	15.71	9.42	9.42	-39.37	930.5

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	220	-26000	-884	-98	0	-52	15983	15.71	15.71	9.42	9.42	-54.11	1270.7
41	220	-22680	-1947	-93	0	-43	16810	15.71	15.71	9.42	9.42	-56.84	1527.8
42	220	-22680	-1949	64	0	-6	16815	15.71	15.71	9.42	9.42	-56.86	1528.6
43	220	-25830	230	-84	0	-47	12219	15.71	15.71	9.42	9.42	-41.18	748.6
44	220	-17670	-3786	-88	0	-29	18751	15.71	15.71	9.42	9.42	-62.87	2036.5
45	220	-20290	-1545	186	0	29	13600	15.71	15.71	9.42	9.42	-46.04	1155.4
46	220	-18850	-1298	-67	0	-25	11664	15.71	15.71	9.42	9.42	-39.49	932.3
47	220	-17890	-1135	-60	0	-21	10374	15.71	15.71	9.42	9.42	-35.11	784.8
49	220	-19000	-781	-62	0	-24	10099	15.71	15.71	9.42	9.42	-34.14	703.6
50	220	-17370	-1584	-63	0	-20	11408	15.71	15.71	9.42	9.42	-38.62	954.8
51	220	-17890	-1136	-8	0	-9	10378	15.71	15.71	9.42	9.42	-35.13	785.5

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	330	-25120	-1138	-98	0	56	14871	15.71	15.71	9.42	9.42	-50.34	1145.6
41	330	-21800	-1947	-93	0	60	14670	15.71	15.71	9.42	9.42	-49.66	1249.9
42	330	-21800	-1949	64	0	-77	14672	15.71	15.71	9.42	9.42	-49.66	1250.2
43	330	-24950	-192	-84	0	45	12242	15.71	15.71	9.42	9.42	-41.30	782.7
44	330	-16790	-3364	-88	0	68	14818	15.71	15.71	9.42	9.42	-49.94	1484.2
45	330	-19410	-1545	186	0	-176	11900	15.71	15.71	9.42	9.42	-40.29	944.1
46	330	-17970	-1298	-67	0	48	10235	15.71	15.71	9.42	9.42	-34.63	762.0
47	330	-17010	-1135	-60	0	46	9125	15.71	15.71	9.42	9.42	-30.85	641.7
49	330	-18120	-866	-62	0	44	9194	15.71	15.71	9.42	9.42	-31.05	610.1
50	330	-16490	-1500	-63	0	49	9711	15.71	15.71	9.42	9.42	-32.87	744.7
51	330	-17010	-1136	-8	0	-0	9128	15.71	15.71	9.42	9.42	-30.86	642.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	440	-24240	-1391	-98	0	163	13480	15.71	15.71	9.42	9.42	-45.60	981.5
41	440	-20920	-1947	-93	0	163	12530	15.71	15.71	9.42	9.42	-42.42	975.0
42	440	-20920	-1949	64	0	-148	12530	15.71	15.71	9.42	9.42	-42.42	975.0
43	440	-24070	-615	-84	0	138	11800	15.71	15.71	9.42	9.42	-39.81	753.7
44	440	-15910	-2941	-88	0	165	11350	15.71	15.71	9.42	9.42	-38.40	1006.6
45	440	-18530	-1545	186	0	-380	10200	15.71	15.71	9.42	9.42	-34.50	735.5
46	440	-17090	-1298	-67	0	122	8807	15.71	15.71	9.42	9.42	-29.75	594.3
47	440	-16130	-1135	-60	0	112	7877	15.71	15.71	9.42	9.42	-26.57	500.9

49	440	-17240	-950	-62	0	112	8196	15.71	15.71	9.42	9.42	-27.62	505.1
50	440	-15610	-1415	-63	0	118	8107	15.71	15.71	9.42	9.42	-27.39	551.5
51	440	-16130	-1136	-8	0	8	7877	15.71	15.71	9.42	9.42	-26.57	500.9

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 28 NI 250 NF 249 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 2B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-26260	543	-33	0	-234	9709	15.71	15.71	9.42	9.42	-32.35	-425.2
41	0	-23010	-1016	-24	0	-168	13180	15.71	15.71	9.42	9.42	-44.60	986.3
42	0	-23120	-1023	131	0	202	13380	15.71	15.71	9.42	9.42	-45.28	1010.5
43	0	-26350	1791	-41	0	-251	4889	15.71	15.71	9.42	9.42	-17.30	-241.0
44	0	-18050	-3649	-8	0	-63	19400	15.71	15.71	9.42	9.42	-65.02	2117.4
45	0	-21120	-819	233	0	475	11010	15.71	15.71	9.42	9.42	-37.20	752.0
46	0	-19680	-681	-26	0	-125	9177	15.71	15.71	9.42	9.42	-30.91	552.4
47	0	-18850	-597	-26	0	-115	8175	15.71	15.71	9.42	9.42	-27.45	447.8
49	0	-19940	-78	-29	0	-137	7017	15.71	15.71	9.42	9.42	-23.32	-308.2
50	0	-18280	-1166	-23	0	-99	9919	15.71	15.71	9.42	9.42	-33.54	705.4
51	0	-18890	-600	25	0	8	8241	15.71	15.71	9.42	9.42	-27.68	455.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	110	-25380	289	-33	0	-197	10166	15.71	15.71	9.42	9.42	-34.01	495.7
41	110	-22130	-1016	-24	0	-142	12063	15.71	15.71	9.42	9.42	-40.79	861.7
42	110	-22240	-1023	131	0	58	12254	15.71	15.71	9.42	9.42	-41.45	884.5
43	110	-25470	1369	-41	0	-206	6627	15.71	15.71	9.42	9.42	-21.97	-299.2
44	110	-17170	-3226	-8	0	-54	15619	15.71	15.71	9.42	9.42	-52.59	1587.6
45	110	-20240	-819	233	0	218	10108	15.71	15.71	9.42	9.42	-34.12	659.3
46	110	-18800	-681	-26	0	-97	8428	15.71	15.71	9.42	9.42	-28.34	482.6
47	110	-17970	-597	-26	0	-86	7518	15.71	15.71	9.42	9.42	-25.21	391.3
49	110	-19060	-162	-29	0	-104	6885	15.71	15.71	9.42	9.42	-22.91	-302.0
50	110	-17400	-1081	-23	0	-74	8683	15.71	15.71	9.42	9.42	-29.31	565.9
51	110	-18010	-600	25	0	-20	7581	15.71	15.71	9.42	9.42	-25.43	398.2

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	220	-24500	36	-33	0	-161	10345	15.71	15.71	9.42	9.42	-34.70	545.7
41	220	-21250	-1016	-24	0	-116	10946	15.71	15.71	9.42	9.42	-36.97	738.2
42	220	-21360	-1023	131	0	-87	11128	15.71	15.71	9.42	9.42	-37.60	759.5
43	220	-24590	946	-41	0	-161	7900	15.71	15.71	9.42	9.42	-26.15	-349.1
44	220	-16290	-2804	-8	0	-45	12303	15.71	15.71	9.42	9.42	-41.59	1131.2
45	220	-19360	-819	233	0	-38	9206	15.71	15.71	9.42	9.42	-31.03	567.5
46	220	-17920	-681	-26	0	-69	7678	15.71	15.71	9.42	9.42	-25.77	413.6
47	220	-17090	-597	-26	0	-57	6861	15.71	15.71	9.42	9.42	-22.96	335.7
49	220	-18180	-247	-29	0	-72	6660	15.71	15.71	9.42	9.42	-22.18	-291.9
50	220	-16520	-997	-23	0	-49	7541	15.71	15.71	9.42	9.42	-25.38	441.9
51	220	-17130	-600	25	0	-48	6922	15.71	15.71	9.42	9.42	-23.17	342.1

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	330	-23620	-218	-33	0	-124	10245	15.71	15.71	9.42	9.42	-34.41	561.2
41	330	-20370	-1016	-24	0	-90	9828	15.71	15.71	9.42	9.42	-33.14	616.3
42	330	-20480	-1023	131	0	-231	10002	15.71	15.71	9.42	9.42	-33.74	636.1
43	330	-23710	524	-41	0	-116	8709	15.71	15.71	9.42	9.42	-29.01	-381.6
44	330	-15410	-2382	-8	0	-37	9451	15.71	15.71	9.42	9.42	-32.00	750.0
45	330	-18480	-819	233	0	-294	8305	15.71	15.71	9.42	9.42	-27.93	477.1
46	330	-17040	-681	-26	0	-41	6929	15.71	15.71	9.42	9.42	-23.20	345.8
47	330	-16210	-597	-26	0	-28	6204	15.71	15.71	9.42	9.42	-20.71	281.1
49	330	-17300	-331	-29	0	-40	6343	15.71	15.71	9.42	9.42	-21.12	-277.9
50	330	-15640	-912	-23	0	-24	6491	15.71	15.71	9.42	9.42	-21.75	333.9
51	330	-16250	-600	25	0	-76	6262	15.71	15.71	9.42	9.42	-20.91	287.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	440	-22740	-471	-33	0	-87	9866	15.71	15.71	9.42	9.42	-33.13	540.7
41	440	-19490	-1016	-24	0	-64	8711	15.71	15.71	9.42	9.42	-29.29	496.8
42	440	-19600	-1023	131	0	-375	8876	15.71	15.71	9.42	9.42	-29.86	515.0
43	440	-22830	102	-41	0	-71	9053	15.71	15.71	9.42	9.42	-30.27	434.5
44	440	-14530	-1959	-8	0	-28	7064	15.71	15.71	9.42	9.42	-23.82	446.9
45	440	-17600	-819	233	0	-551	7403	15.71	15.71	9.42	9.42	-24.83	388.4
46	440	-16160	-681	-26	0	-13	6180	15.71	15.71	9.42	9.42	-20.63	279.7
47	440	-15330	-597	-26	0	0	5547	15.71	15.71	9.42	9.42	-18.46	-243.3
49	440	-16420	-416	-29	0	-8	5932	15.71	15.71	9.42	9.42	-19.74	-260.2
50	440	-14760	-828	-23	0	1	5534	15.71	15.71	9.42	9.42	-18.45	242.2
51	440	-15370	-600	25	0	-104	5602	15.71	15.71	9.42	9.42	-18.65	-245.6

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 29 NI 293 NF 292 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 1B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-14820	554	-433	0	-658	-1029	6.28	6.28	9.42	9.42	-16.89	-203.5
41	0	-15040	-40	-342	0	-430	-25	6.28	6.28	9.42	9.42	-9.52	-138.0
42	0	-14800	-38	-375	0	-150	-26	6.28	6.28	9.42	9.42	-8.13	-120.2
43	0	-13780	932	-449	0	-728	-1665	6.28	6.28	9.42	9.42	-25.94	-272.8
44	0	-15550	-1025	-199	0	-65	1641	6.28	6.28	9.42	9.42	-25.52	-279.4
45	0	-13760	-55	-352	0	118	6	6.28	6.28	9.42	9.42	-7.46	-110.5
46	0	-13630	-68	-270	0	-300	28	6.28	6.28	9.42	9.42	-8.22	-119.9
47	0	-13280	-75	-253	0	-267	42	6.28	6.28	9.42	9.42	-7.90	-115.4
49	0	-13200	123	-283	0	-343	-293	6.28	6.28	9.42	9.42	-9.03	-122.0
50	0	-13550	-268	-233	0	-210	368	6.28	6.28	9.42	9.42	-9.89	-131.4
51	0	-13200	-74	-264	0	-174	41	6.28	6.28	9.42	9.42	-7.43	-109.5

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	97	-14380	441	-433	0	-236	-544	6.28	6.28	9.42	9.42	-11.90	-153.5
41	97	-14602	-40	-342	0	-96	-64	6.28	6.28	9.42	9.42	-7.78	-115.6
42	97	-14362	-38	-288	0	172	-64	6.28	6.28	9.42	9.42	-8.01	-118.2
43	97	-13342	745	-449	0	-291	-848	6.28	6.28	9.42	9.42	-14.32	-174.9
44	97	-15112	-838	-199	0	128	733	6.28	6.28	9.42	9.42	-13.99	-176.2
45	97	-13322	-55	-207	0	389	-47	6.28	6.28	9.42	9.42	-8.47	-122.7
46	97	-13190	-68	-270	0	-36	-38	6.28	6.28	9.42	9.42	-6.80	-101.5
47	97	-12840	-75	-253	0	-21	-31	6.28	6.28	9.42	9.42	-6.55	-98.1
49	97	-12762	86	-283	0	-67	-191	6.28	6.28	9.42	9.42	-7.88	-109.5
50	97	-13112	-231	-233	0	16	125	6.28	6.28	9.42	9.42	-7.45	-105.9
51	97	-12760	-74	-234	0	69	-31	6.28	6.28	9.42	9.42	-6.73	-100.2

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	195	-13940	329	-433	0	187	-169	6.28	6.28	9.42	9.42	-8.24	-115.9
41	195	-14165	-40	-342	0	237	-103	6.28	6.28	9.42	9.42	-8.21	-120.4
42	195	-13925	-38	-213	0	416	-101	6.28	6.28	9.42	9.42	-8.90	-128.7
43	195	-12905	557	-449	0	147	-213	6.28	6.28	9.42	9.42	-8.16	-112.5
44	195	-14675	-650	-199	0	322	8	6.28	6.28	9.42	9.42	-8.85	-129.1
45	195	-12885	-55	-83	0	529	-101	6.28	6.28	9.42	9.42	-8.89	-127.3
46	195	-12750	-68	-270	0	228	-104	6.28	6.28	9.42	9.42	-7.45	-109.2
47	195	-12400	-75	-253	0	225	-104	6.28	6.28	9.42	9.42	-7.26	-106.4
49	195	-12325	48	-283	0	208	-126	6.28	6.28	9.42	9.42	-7.15	-104.9
50	195	-12675	-193	-233	0	244	-82	6.28	6.28	9.42	9.42	-7.48	-109.5
51	195	-12320	-74	-210	0	285	-103	6.28	6.28	9.42	9.42	-7.49	-109.2

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	292	-13500	217	-433	0	609	97	6.28	6.28	9.42	9.42	-9.57	-136.6
41	292	-13728	-40	-342	0	571	-142	6.28	6.28	9.42	9.42	-9.51	-136.1
42	292	-13488	-38	-151	0	593	-139	6.28	6.28	9.42	9.42	-9.49	-135.5
43	292	-12468	370	-449	0	585	239	6.28	6.28	9.42	9.42	-8.94	-127.4
44	292	-14238	-463	-199	0	516	-534	6.28	6.28	9.42	9.42	-11.75	-151.6
45	292	-12448	-55	21	0	557	-154	6.28	6.28	9.42	9.42	-8.80	-125.7
46	292	-12310	-68	-270	0	492	-170	6.28	6.28	9.42	9.42	-8.43	-120.9
47	292	-11960	-75	-253	0	472	-177	6.28	6.28	9.42	9.42	-8.17	-117.1
49	292	-11888	11	-283	0	484	-97	6.28	6.28	9.42	9.42	-8.19	-117.3
50	292	-12238	-156	-233	0	470	-252	6.28	6.28	9.42	9.42	-8.30	-119.1
51	292	-11880	-74	-189	0	479	-176	6.28	6.28	9.42	9.42	-8.16	-116.9

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	390	-13060	104	-433	0	1032	254	6.28	6.28	9.42	9.42	-11.27	-157.3
41	390	-13290	-40	-342	0	905	-180	6.28	6.28	9.42	9.42	-10.81	-151.8
42	390	-13050	-38	-102	0	715	-176	6.28	6.28	9.42	9.42	-9.82	-139.2
43	390	-12030	183	-449	0	1023	508	6.28	6.28	9.42	9.42	-10.72	-149.1
44	390	-13800	-276	-199	0	710	-894	6.28	6.28	9.42	9.42	-15.00	-182.7
45	390	-12010	-55	104	0	495	-208	6.28	6.28	9.42	9.42	-8.30	-118.8
46	390	-11870	-68	-270	0	755	-236	6.28	6.28	9.42	9.42	-9.41	-132.6
47	390	-11520	-75	-253	0	718	-250	6.28	6.28	9.42	9.42	-9.07	-127.8
49	390	-11450	-27	-283	0	760	-105	6.28	6.28	9.42	9.42	-9.22	-129.7
50	390	-11800	-118	-233	0	698	-386	6.28	6.28	9.42	9.42	-9.21	-128.8
51	390	-11440	-74	-172	0	655	-248	6.28	6.28	9.42	9.42	-8.74	-123.6

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 30 NI 77 NF 76 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 6C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	--												
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-18160	-809	174	0	97	9467	15.71	15.71	9.42	9.42	-31.99	646.6
41	0	-14850	-1133	181	0	82	7468	15.71	15.71	9.42	9.42	-25.21	490.8
42	0	-14950	-1145	235	0	100	7660	15.71	15.71	9.42	9.42	-25.87	513.7
43	0	-18370	-362	136	0	92	9334	15.71	15.71	9.42	9.42	-31.52	620.4
44	0	-9788	-1711	199	0	63	4398	15.71	15.71	9.42	9.42	-14.79	252.6
45	0	-13010	-922	238	0	98	6321	15.71	15.71	9.42	9.42	-21.32	399.6
46	0	-11640	-764	128	0	60	5122	15.71	15.71	9.42	9.42	-17.21	286.1
47	0	-10840	-672	114	0	55	4536	15.71	15.71	9.42	9.42	-15.21	236.2
49	0	-11940	-564	112	0	60	5202	15.71	15.71	9.42	9.42	-17.47	286.7
50	0	-10230	-834	125	0	54	4215	15.71	15.71	9.42	9.42	-14.12	214.5
51	0	-10870	-676	132	0	61	4600	15.71	15.71	9.42	9.42	-15.43	243.4

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	83	-17500	-1060	174	0	-47	8696	15.71	15.71	9.42	9.42	-29.35	564.0
41	83	-14190	-1133	181	0	-67	6533	15.71	15.71	9.42	9.42	-21.99	387.1
42	83	-14290	-1145	235	0	-94	6716	15.71	15.71	9.42	9.42	-22.62	408.1
43	83	-17710	-781	136	0	-20	8863	15.71	15.71	9.42	9.42	-29.92	579.3
44	83	-9128	-1292	199	0	-102	3159	15.71	15.71	9.42	9.42	-10.49	-138.9
45	83	-12350	-922	238	0	-99	5560	15.71	15.71	9.42	9.42	-18.70	320.1
46	83	-10980	-764	128	0	-45	4492	15.71	15.71	9.42	9.42	-15.04	226.2
47	83	-10179	-672	114	0	-40	3982	15.71	15.71	9.42	9.42	-13.30	187.0
49	83	-11280	-648	112	0	-33	4702	15.71	15.71	9.42	9.42	-15.76	243.5
50	83	-9569	-750	125	0	-49	3562	15.71	15.71	9.42	9.42	-11.87	-155.9
51	83	-10210	-676	132	0	-49	4042	15.71	15.71	9.42	9.42	-13.51	193.5

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	165	-16840	-1311	174	0	-190	7718	15.71	15.71	9.42	9.42	-25.98	454.7
41	165	-13530	-1133	181	0	-216	5598	15.71	15.71	9.42	9.42	-18.76	286.8
42	165	-13630	-1145	235	0	-289	5771	15.71	15.71	9.42	9.42	-19.36	305.6
43	165	-17050	-1200	136	0	-132	8046	15.71	15.71	9.42	9.42	-27.11	491.4
44	165	-8468	-873	199	0	-266	2266	15.71	15.71	9.42	9.42	-7.50	-101.9
45	165	-11690	-922	238	0	-296	4799	15.71	15.71	9.42	9.42	-16.08	242.9
46	165	-10320	-764	128	0	-150	3861	15.71	15.71	9.42	9.42	-12.87	-169.0
47	165	-9518	-672	114	0	-134	3427	15.71	15.71	9.42	9.42	-11.40	-150.3
49	165	-10620	-732	112	0	-125	4133	15.71	15.71	9.42	9.42	-13.81	192.5
50	165	-8908	-666	125	0	-152	2977	15.71	15.71	9.42	9.42	-9.87	-131.2
51	165	-9550	-676	132	0	-158	3484	15.71	15.71	9.42	9.42	-11.60	-152.7

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	248	-16180	-1563	174	0	-334	6532	15.71	15.71	9.42	9.42	-21.86	322.4
41	248	-12870	-1133	181	0	-366	4664	15.71	15.71	9.42	9.42	-15.52	-204.5
42	248	-12970	-1145	235	0	-483	4826	15.71	15.71	9.42	9.42	-16.09	-211.3
43	248	-16390	-1619	136	0	-244	6883	15.71	15.71	9.42	9.42	-23.08	360.2
44	248	-7808	-454	199	0	-431	1719	15.71	15.71	9.42	9.42	-5.82	-80.2
45	248	-11030	-922	238	0	-492	4038	15.71	15.71	9.42	9.42	-13.45	-177.0
46	248	-9660	-764	128	0	-256	3230	15.71	15.71	9.42	9.42	-10.71	-142.3
47	248	-8858	-672	114	0	-228	2872	15.71	15.71	9.42	9.42	-9.51	-126.8
49	248	-9961	-815	112	0	-218	3495	15.71	15.71	9.42	9.42	-11.61	-153.6
50	248	-8247	-582	125	0	-255	2462	15.71	15.71	9.42	9.42	-8.14	-109.4
51	248	-8891	-676	132	0	-267	2926	15.71	15.71	9.42	9.42	-9.70	-129.1

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	330	-15520	-1814	174	0	-478	5139	15.71	15.71	9.42	9.42	-17.03	-226.6
41	330	-12210	-1133	181	0	-515	3729	15.71	15.71	9.42	9.42	-12.33	-165.4
42	330	-12310	-1145	235	0	-677	3882	15.71	15.71	9.42	9.42	-12.84	-171.7
43	330	-15730	-2038	136	0	-356	5374	15.71	15.71	9.42	9.42	-17.84	-236.5
44	330	-7148	-35	199	0	-595	1518	15.71	15.71	9.42	9.42	-5.17	-71.5
45	330	-10370	-922	238	0	-689	3277	15.71	15.71	9.42	9.42	-10.84	-145.0
46	330	-9000	-764	128	0	-361	2600	15.71	15.71	9.42	9.42	-8.59	-115.9
47	330	-8197	-672	114	0	-323	2318	15.71	15.71	9.42	9.42	-7.66	-103.6
49	330	-9301	-899	112	0	-310	2788	15.71	15.71	9.42	9.42	-9.21	-123.8
50	330	-7586	-499	125	0	-358	2016	15.71	15.71	9.42	9.42	-6.68	-90.7
51	330	-8231	-676	132	0	-377	2368	15.71	15.71	9.42	9.42	-7.83	-105.6

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 31 NI 120 NF 119 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 5C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-20400	-1525	-12	0	-159	13360	15.71	15.71	9.42	9.42	-45.23	1115.9
41	0	-17090	-2061	33	0	-101	12280	15.71	15.71	9.42	9.42	-41.54	1094.2
42	0	-17130	-2067	75	0	-56	12330	15.71	15.71	9.42	9.42	-41.71	1099.9
43	0	-20170	-740	-39	0	-166	11650	15.71	15.71	9.42	9.42	-39.43	878.3
44	0	-12120	-3028	108	0	-6	10920	15.71	15.71	9.42	9.42	-36.78	1104.9
45	0	-14720	-1643	106	0	5	9924	15.71	15.71	9.42	9.42	-33.59	846.6
46	0	-13190	-1378	37	0	-49	8388	15.71	15.71	9.42	9.42	-28.40	685.1
47	0	-12220	-1207	38	0	-36	7414	15.71	15.71	9.42	9.42	-25.10	583.1
49	0	-13320	-1028	23	0	-56	7774	15.71	15.71	9.42	9.42	-26.31	591.5
50	0	-11710	-1486	52	0	-24	7629	15.71	15.71	9.42	9.42	-25.83	634.7
51	0	-12230	-1209	52	0	-22	7430	15.71	15.71	9.42	9.42	-25.15	585.1

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	83	-19740	-1776	-12	0	-149	11999	15.71	15.71	9.42	9.42	-40.62	945.2
41	83	-16430	-2061	33	0	-127	10580	15.71	15.71	9.42	9.42	-35.82	872.6
42	83	-16470	-2067	75	0	-119	10624	15.71	15.71	9.42	9.42	-35.97	877.4
43	83	-19510	-1159	-39	0	-134	10866	15.71	15.71	9.42	9.42	-36.76	792.3
44	83	-11459	-2609	108	0	-95	8595	15.71	15.71	9.42	9.42	-29.06	787.0
45	83	-14060	-1643	106	0	-83	8568	15.71	15.71	9.42	9.42	-29.01	676.4
46	83	-12530	-1378	37	0	-79	7251	15.71	15.71	9.42	9.42	-24.54	547.6
47	83	-11559	-1207	38	0	-67	6418	15.71	15.71	9.42	9.42	-21.71	466.6
49	83	-12660	-1112	23	0	-75	6891	15.71	15.71	9.42	9.42	-23.30	491.5
50	83	-11050	-1402	52	0	-67	6438	15.71	15.71	9.42	9.42	-21.79	489.1
51	83	-11570	-1209	52	0	-65	6432	15.71	15.71	9.42	9.42	-21.76	468.2

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	165	-19080	-2028	-12	0	-139	10430	15.71	15.71	9.42	9.42	-35.28	747.2
41	165	-15770	-2061	33	0	-154	8880	15.71	15.71	9.42	9.42	-30.04	654.2
42	165	-15810	-2067	75	0	-181	8919	15.71	15.71	9.42	9.42	-30.18	658.2
43	165	-18850	-1578	-39	0	-101	9737	15.71	15.71	9.42	9.42	-32.89	658.6
44	165	-10798	-2190	108	0	-184	6616	15.71	15.71	9.42	9.42	-22.40	524.6
45	165	-13400	-1643	106	0	-171	7212	15.71	15.71	9.42	9.42	-24.39	508.9
46	165	-11870	-1378	37	0	-110	6114	15.71	15.71	9.42	9.42	-20.65	412.3
47	165	-10898	-1207	38	0	-98	5422	15.71	15.71	9.42	9.42	-18.30	352.1
49	165	-12000	-1196	23	0	-93	5939	15.71	15.71	9.42	9.42	-20.04	383.4
50	165	-10390	-1318	52	0	-110	5315	15.71	15.71	9.42	9.42	-17.95	355.9
51	165	-10910	-1209	52	0	-107	5434	15.71	15.71	9.42	9.42	-18.34	353.4

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	248	-18420	-2279	-12	0	-129	8654	15.71	15.71	9.42	9.42	-29.16	525.8
41	248	-15110	-2061	33	0	-181	7180	15.71	15.71	9.42	9.42	-24.20	442.2
42	248	-15150	-2067	75	0	-243	7214	15.71	15.71	9.42	9.42	-24.31	445.3
43	248	-18190	-1997	-39	0	-69	8261	15.71	15.71	9.42	9.42	-27.80	481.1
44	248	-10138	-1770	108	0	-273	4983	15.71	15.71	9.42	9.42	-16.81	319.2
45	248	-12740	-1643	106	0	-259	5857	15.71	15.71	9.42	9.42	-19.72	346.4
46	248	-11210	-1378	37	0	-140	4977	15.71	15.71	9.42	9.42	-16.73	281.4
47	248	-10238	-1207	38	0	-129	4426	15.71	15.71	9.42	9.42	-14.86	241.4
49	248	-11340	-1280	23	0	-112	4917	15.71	15.71	9.42	9.42	-16.51	269.3
50	248	-9729	-1235	52	0	-153	4262	15.71	15.71	9.42	9.42	-14.32	236.7
51	248	-10249	-1209	52	0	-150	4437	15.71	15.71	9.42	9.42	-14.90	242.4

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	330	-17760	-2530	-12	0	-119	6671	15.71	15.71	9.42	9.42	-22.24	292.9
41	330	-14450	-2061	33	0	-208	5480	15.71	15.71	9.42	9.42	-18.28	244.6
42	330	-14490	-2067	75	0	-305	5508	15.71	15.71	9.42	9.42	-18.38	246.8
43	330	-17530	-2416	-39	0	-37	6440	15.71	15.71	9.42	9.42	-21.45	-282.2
44	330	-9477	-1351	108	0	-363	3695	15.71	15.71	9.42	9.42	-12.34	172.6
45	330	-12080	-1643	106	0	-347	4501	15.71	15.71	9.42	9.42	-15.00	-197.0
46	330	-10550	-1378	37	0	-170	3840	15.71	15.71	9.42	9.42	-12.78	-168.3
47	330	-9577	-1207	38	0	-160	3430	15.71	15.71	9.42	9.42	-11.41	-150.5
49	330	-10680	-1364	23	0	-131	3827	15.71	15.71	9.42	9.42	-12.73	-167.9
50	330	-9069	-1151	52	0	-196	3278	15.71	15.71	9.42	9.42	-10.91	-143.8
51	330	-9589	-1209	52	0	-193	3439	15.71	15.71	9.42	9.42	-11.44	-150.9

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 32 NI 163 NF 162 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 4C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-20650	-1665	-254	0	-379	13970	15.71	15.71	9.42	9.42	-47.28	1194.7
41	0	-17240	-2223	-216	0	-305	12900	15.71	15.71	9.42	9.42	-43.61	1179.4
42	0	-17180	-2200	-151	0	-220	12770	15.71	15.71	9.42	9.42	-43.18	1162.7
43	0	-20460	-832	-225	0	-352	12120	15.71	15.71	9.42	9.42	-41.03	934.2
44	0	-12080	-3233	-160	0	-192	11580	15.71	15.71	9.42	9.42	-38.94	1205.7
45	0	-14670	-1725	-52	0	-87	10130	15.71	15.71	9.42	9.42	-34.28	878.9
46	0	-13290	-1487	-128	0	-182	8807	15.71	15.71	9.42	9.42	-29.81	742.0
47	0	-12300	-1303	-106	0	-151	7784	15.71	15.71	9.42	9.42	-26.35	633.4
49	0	-13440	-1117	-119	0	-176	8140	15.71	15.71	9.42	9.42	-27.56	639.3
50	0	-11770	-1597	-106	0	-144	8032	15.71	15.71	9.42	9.42	-27.18	691.1
51	0	-12290	-1296	-84	0	-123	7742	15.71	15.71	9.42	9.42	-26.21	627.7

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	83	-19990	-1917	-254	0	-169	12492	15.71	15.71	9.42	9.42	-42.29	1006.4
41	83	-16580	-2223	-216	0	-126	11066	15.71	15.71	9.42	9.42	-37.46	937.2
42	83	-16520	-2200	-151	0	-96	10956	15.71	15.71	9.42	9.42	-37.09	923.6
43	83	-19800	-1252	-225	0	-166	11260	15.71	15.71	9.42	9.42	-38.10	837.1
44	83	-11421	-2814	-160	0	-60	9086	15.71	15.71	9.42	9.42	-30.69	861.4
45	83	-14010	-1725	-52	0	-44	8708	15.71	15.71	9.42	9.42	-29.48	698.6
46	83	-12630	-1487	-128	0	-76	7580	15.71	15.71	9.42	9.42	-25.66	590.8
47	83	-11641	-1303	-106	0	-63	6709	15.71	15.71	9.42	9.42	-22.70	504.8
49	83	-12780	-1201	-119	0	-78	7183	15.71	15.71	9.42	9.42	-24.30	528.3
50	83	-11109	-1513	-106	0	-56	6749	15.71	15.71	9.42	9.42	-22.85	531.4
51	83	-11629	-1296	-84	0	-53	6673	15.71	15.71	9.42	9.42	-22.58	500.2

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	165	-19330	-2168	-254	0	41	10806	15.71	15.71	9.42	9.42	-36.56	790.7
41	165	-15920	-2223	-216	0	52	9231	15.71	15.71	9.42	9.42	-31.24	698.4
42	165	-15860	-2200	-151	0	28	9142	15.71	15.71	9.42	9.42	-30.94	688.0
43	165	-19140	-1671	-225	0	19	10054	15.71	15.71	9.42	9.42	-33.98	692.1
44	165	-10762	-2394	-160	0	72	6938	15.71	15.71	9.42	9.42	-23.49	572.8
45	165	-13350	-1725	-52	0	-1	7286	15.71	15.71	9.42	9.42	-24.64	521.1
46	165	-11970	-1487	-128	0	30	6353	15.71	15.71	9.42	9.42	-21.47	442.0
47	165	-10982	-1303	-106	0	24	5634	15.71	15.71	9.42	9.42	-19.03	378.3
49	165	-12120	-1285	-119	0	21	6158	15.71	15.71	9.42	9.42	-20.79	409.3
50	165	-10448	-1430	-106	0	31	5535	15.71	15.71	9.42	9.42	-18.71	384.3
51	165	-10968	-1296	-84	0	17	5604	15.71	15.71	9.42	9.42	-18.93	374.8

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	248	-18670	-2420	-254	0	250	8913	15.71	15.71	9.42	9.42	-30.04	552.0
41	248	-15260	-2223	-216	0	230	7396	15.71	15.71	9.42	9.42	-24.94	466.3
42	248	-15200	-2200	-151	0	153	7328	15.71	15.71	9.42	9.42	-24.71	459.1
43	248	-18480	-2090	-225	0	205	8502	15.71	15.71	9.42	9.42	-28.62	503.3
44	248	-10103	-1975	-160	0	204	5136	15.71	15.71	9.42	9.42	-17.35	341.6
45	248	-12690	-1725	-52	0	42	5864	15.71	15.71	9.42	9.42	-19.74	349.0
46	248	-11310	-1487	-128	0	136	5126	15.71	15.71	9.42	9.42	-17.25	297.7
47	248	-10323	-1303	-106	0	112	4558	15.71	15.71	9.42	9.42	-15.32	255.8
49	248	-11460	-1369	-119	0	119	5063	15.71	15.71	9.42	9.42	-17.02	284.4
50	248	-9788	-1346	-106	0	119	4390	15.71	15.71	9.42	9.42	-14.76	251.5
51	248	-10306	-1296	-84	0	86	4536	15.71	15.71	9.42	9.42	-15.24	253.4

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	330	-18010	-2671	-254	0	460	6812	15.71	15.71	9.42	9.42	-22.72	302.6
41	330	-14600	-2223	-216	0	408	5562	15.71	15.71	9.42	9.42	-18.56	250.1
42	330	-14540	-2200	-151	0	277	5514	15.71	15.71	9.42	9.42	-18.40	246.1
43	330	-17820	-2509	-225	0	391	6605	15.71	15.71	9.42	9.42	-22.01	-289.2
44	330	-9444	-1556	-160	0	336	3680	15.71	15.71	9.42	9.42	-12.29	171.8
45	330	-12030	-1725	-52	0	85	4442	15.71	15.71	9.42	9.42	-14.80	-194.6
46	330	-10650	-1487	-128	0	242	3899	15.71	15.71	9.42	9.42	-12.98	-170.9
47	330	-9664	-1303	-106	0	200	3483	15.71	15.71	9.42	9.42	-11.59	-152.8
49	330	-10800	-1453	-119	0	217	3899	15.71	15.71	9.42	9.42	-12.97	-171.0
50	330	-9127	-1262	-106	0	206	3314	15.71	15.71	9.42	9.42	-11.03	-145.3
51	330	-9645	-1296	-84	0	156	3467	15.71	15.71	9.42	9.42	-11.53	-152.1

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 33 NI 206 NF 205 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 3C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-20220	-1465	-384	0	-540	13000	15.71	15.71	9.42	9.42	-44.01	1070.8
41	0	-16880	-2040	-336	0	-422	12070	15.71	15.71	9.42	9.42	-40.83	1072.1
42	0	-16880	-2039	-239	0	-293	12070	15.71	15.71	9.42	9.42	-40.83	1072.1
43	0	-20050	-656	-335	0	-512	11210	15.71	15.71	9.42	9.42	-37.92	820.4
44	0	-11830	-3070	-270	0	-242	10970	15.71	15.71	9.42	9.42	-36.92	1125.1
45	0	-14480	-1614	-93	0	-100	9669	15.71	15.71	9.42	9.42	-32.73	819.2
46	0	-13030	-1360	-207	0	-251	8232	15.71	15.71	9.42	9.42	-27.87	669.0
47	0	-12070	-1190	-175	0	-209	7271	15.71	15.71	9.42	9.42	-24.61	568.5
49	0	-13180	-998	-191	0	-248	7578	15.71	15.71	9.42	9.42	-25.65	569.0
50	0	-11540	-1481	-178	0	-194	7531	15.71	15.71	9.42	9.42	-25.50	627.4
51	0	-12070	-1190	-142	0	-166	7270	15.71	15.71	9.42	9.42	-24.61	568.4

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	83	-19560	-1716	-384	0	-223	11687	15.71	15.71	9.42	9.42	-39.56	907.5
41	83	-16220	-2040	-336	0	-145	10388	15.71	15.71	9.42	9.42	-35.17	853.2
42	83	-16220	-2039	-239	0	-96	10388	15.71	15.71	9.42	9.42	-35.17	853.2
43	83	-19390	-1075	-335	0	-236	10495	15.71	15.71	9.42	9.42	-35.49	744.5

44	83	-11171	-2651	-270	0	-19	8610	15.71	15.71	9.42	9.42	-29.10	801.4
45	83	-13820	-1614	-93	0	-23	8337	15.71	15.71	9.42	9.42	-28.22	652.6
46	83	-12370	-1360	-207	0	-81	7110	15.71	15.71	9.42	9.42	-24.06	533.7
47	83	-11409	-1190	-175	0	-64	6289	15.71	15.71	9.42	9.42	-21.27	454.1
49	83	-12520	-1082	-191	0	-91	6720	15.71	15.71	9.42	9.42	-22.72	472.7
50	83	-10879	-1397	-178	0	-47	6344	15.71	15.71	9.42	9.42	-21.47	482.3
51	83	-11409	-1190	-142	0	-48	6288	15.71	15.71	9.42	9.42	-21.27	454.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	165	-18900	-1968	-384	0	93	10166	15.71	15.71	9.42	9.42	-34.37	716.8
41	165	-15560	-2040	-336	0	133	8706	15.71	15.71	9.42	9.42	-29.45	637.6
42	165	-15560	-2039	-239	0	101	8706	15.71	15.71	9.42	9.42	-29.45	637.6
43	165	-18730	-1495	-335	0	40	9435	15.71	15.71	9.42	9.42	-31.85	621.2
44	165	-10512	-2232	-270	0	203	6596	15.71	15.71	9.42	9.42	-22.33	533.2
45	165	-13160	-1614	-93	0	53	7005	15.71	15.71	9.42	9.42	-23.68	488.8
46	165	-11710	-1360	-207	0	90	5988	15.71	15.71	9.42	9.42	-20.22	400.7
47	165	-10748	-1190	-175	0	80	5307	15.71	15.71	9.42	9.42	-17.91	341.8
49	165	-11860	-1166	-191	0	67	5792	15.71	15.71	9.42	9.42	-19.54	368.4
50	165	-10218	-1314	-178	0	99	5225	15.71	15.71	9.42	9.42	-17.65	349.7
51	165	-10748	-1190	-142	0	69	5306	15.71	15.71	9.42	9.42	-17.91	341.7

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	248	-18240	-2219	-384	0	410	8438	15.71	15.71	9.42	9.42	-28.41	503.0
41	248	-14900	-2040	-336	0	411	7025	15.71	15.71	9.42	9.42	-23.67	428.6
42	248	-14900	-2039	-239	0	298	7024	15.71	15.71	9.42	9.42	-23.67	428.5
43	248	-18070	-1914	-335	0	316	8028	15.71	15.71	9.42	9.42	-26.99	454.3
44	248	-9852	-1813	-270	0	426	4928	15.71	15.71	9.42	9.42	-16.63	321.9
45	248	-12500	-1614	-93	0	130	5673	15.71	15.71	9.42	9.42	-19.09	330.1
46	248	-11050	-1360	-207	0	261	4865	15.71	15.71	9.42	9.42	-16.35	272.0
47	248	-10086	-1190	-175	0	224	4325	15.71	15.71	9.42	9.42	-14.52	233.2
49	248	-11200	-1250	-191	0	224	4796	15.71	15.71	9.42	9.42	-16.10	258.1
50	248	-9558	-1230	-178	0	246	4176	15.71	15.71	9.42	9.42	-14.03	231.1
51	248	-10088	-1190	-142	0	186	4325	15.71	15.71	9.42	9.42	-14.52	233.1

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	330	-17580	-2470	-384	0	727	6503	15.71	15.71	9.42	9.42	-21.67	-284.8
41	330	-14240	-2040	-336	0	688	5343	15.71	15.71	9.42	9.42	-17.82	234.1
42	330	-14240	-2039	-239	0	495	5342	15.71	15.71	9.42	9.42	-17.81	234.0
43	330	-17410	-2333	-335	0	592	6276	15.71	15.71	9.42	9.42	-20.88	-275.3
44	330	-9193	-1394	-270	0	649	3605	15.71	15.71	9.42	9.42	-12.05	170.0
45	330	-11840	-1614	-93	0	206	4341	15.71	15.71	9.42	9.42	-14.46	-190.2
46	330	-10390	-1360	-207	0	432	3743	15.71	15.71	9.42	9.42	-12.45	-164.2
47	330	-9425	-1190	-175	0	368	3343	15.71	15.71	9.42	9.42	-11.11	-146.8
49	330	-10540	-1334	-191	0	381	3730	15.71	15.71	9.42	9.42	-12.40	-163.8
50	330	-8897	-1146	-178	0	392	3196	15.71	15.71	9.42	9.42	-10.63	-140.2
51	330	-9427	-1190	-142	0	304	3343	15.71	15.71	9.42	9.42	-11.11	-146.8

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 34 NI 249 NF 248 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 2C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-18580	-634	-1065	0	-1079	9348	15.71	15.71	9.42	9.42	-31.56	614.7
41	0	-15310	-1178	-794	0	-758	8230	15.71	15.71	9.42	9.42	-27.83	579.9
42	0	-15420	-1211	-738	0	-643	8417	15.71	15.71	9.42	9.42	-28.47	602.1
43	0	-18690	-22	-1018	0	-1060	8457	15.71	15.71	9.42	9.42	-28.45	490.1
44	0	-10310	-2126	-379	0	-260	6649	15.71	15.71	9.42	9.42	-22.51	549.0
45	0	-13410	-984	-474	0	-334	6905	15.71	15.71	9.42	9.42	-23.32	465.5
46	0	-11980	-779	-431	0	-386	5610	15.71	15.71	9.42	9.42	-18.90	339.5
47	0	-11150	-680	-340	0	-293	4955	15.71	15.71	9.42	9.42	-16.66	280.5
49	0	-12240	-498	-430	0	-400	5328	15.71	15.71	9.42	9.42	-17.90	293.3
50	0	-10570	-919	-302	0	-240	4966	15.71	15.71	9.42	9.42	-16.73	301.7
51	0	-11190	-691	-321	0	-255	5017	15.71	15.71	9.42	9.42	-16.87	287.3

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	83	-17920	-886	-1065	0	-200	8721	15.71	15.71	9.42	9.42	-29.41	552.4
41	83	-14650	-1178	-794	0	-103	7258	15.71	15.71	9.42	9.42	-24.49	469.1
42	83	-14760	-1211	-738	0	-34	7418	15.71	15.71	9.42	9.42	-25.04	487.2
43	83	-18030	-441	-1018	0	-220	8266	15.71	15.71	9.42	9.42	-27.82	487.2
44	83	-9650	-1707	-379	0	53	5068	15.71	15.71	9.42	9.42	-17.13	348.8
45	83	-12750	-984	-474	0	57	6094	15.71	15.71	9.42	9.42	-20.54	377.9
46	83	-11320	-779	-431	0	-31	4967	15.71	15.71	9.42	9.42	-16.69	276.4
47	83	-10490	-680	-340	0	-13	4394	15.71	15.71	9.42	9.42	-14.73	229.2
49	83	-11580	-582	-430	0	-45	4882	15.71	15.71	9.42	9.42	-16.37	257.0
50	83	-9909	-835	-302	0	9	4242	15.71	15.71	9.42	9.42	-14.24	228.2
51	83	-10529	-691	-321	0	10	4447	15.71	15.71	9.42	9.42	-14.92	234.7

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	165	-17260	-1137	-1065	0	678	7887	15.71	15.71	9.42	9.42	-26.54	462.9
41	165	-13990	-1178	-794	0	553	6286	15.71	15.71	9.42	9.42	-21.14	360.9
42	165	-14100	-1211	-738	0	575	6418	15.71	15.71	9.42	9.42	-21.60	374.9
43	165	-17370	-860	-1018	0	620	7730	15.71	15.71	9.42	9.42	-25.99	438.3
44	165	-8990	-1288	-379	0	365	3833	15.71	15.71	9.42	9.42	-12.86	205.0
45	165	-12090	-984	-474	0	447	5282	15.71	15.71	9.42	9.42	-17.74	292.2
46	165	-10660	-779	-431	0	325	4324	15.71	15.71	9.42	9.42	-14.48	215.0
47	165	-9830	-680	-340	0	268	3834	15.71	15.71	9.42	9.42	-12.81	179.2
49	165	-10921	-666	-430	0	310	4367	15.71	15.71	9.42	9.42	-14.61	212.4
50	165	-9248	-751	-302	0	259	3588	15.71	15.71	9.42	9.42	-11.98	166.2
51	165	-9868	-691	-321	0	275	3878	15.71	15.71	9.42	9.42	-12.96	183.4

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	248	-16600	-1388	-1065	0	1557	6845	15.71	15.71	9.42	9.42	-22.93	348.8
41	248	-13330	-1178	-794	0	1208	5313	15.71	15.71	9.42	9.42	-17.77	257.1
42	248	-13440	-1211	-738	0	1184	5419	15.71	15.71	9.42	9.42	-18.14	267.0
43	248	-16710	-1279	-1018	0	1459	6847	15.71	15.71	9.42	9.42	-22.93	345.7
44	248	-8331	-869	-379	0	678	2944	15.71	15.71	9.42	9.42	-9.78	-129.3

45	248	-11430	-984	-474	0	838	4470	15.71	15.71	9.42	9.42	-14.94	209.9
46	248	-10000	-779	-431	0	680	3681	15.71	15.71	9.42	9.42	-12.26	-161.3
47	248	-9169	-680	-340	0	549	3273	15.71	15.71	9.42	9.42	-10.88	-143.6
49	248	-10262	-750	-430	0	665	3783	15.71	15.71	9.42	9.42	-12.60	-165.7
50	248	-8587	-668	-302	0	509	3002	15.71	15.71	9.42	9.42	-9.97	-131.9
51	248	-9206	-691	-321	0	540	3308	15.71	15.71	9.42	9.42	-11.00	-145.1

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	330	-15940	-1640	-1065	0	2436	5596	15.71	15.71	9.42	9.42	-18.60	-245.8
41	330	-12670	-1178	-794	0	1864	4341	15.71	15.71	9.42	9.42	-14.41	-191.0
42	330	-12780	-1211	-738	0	1793	4420	15.71	15.71	9.42	9.42	-14.68	-194.4
43	330	-16050	-1698	-1018	0	2299	5619	15.71	15.71	9.42	9.42	-18.67	-246.9
44	330	-7671	-449	-379	0	991	2400	15.71	15.71	9.42	9.42	-7.94	-106.2
45	330	-10770	-984	-474	0	1229	3659	15.71	15.71	9.42	9.42	-12.14	-161.1
46	330	-9340	-779	-431	0	1036	3038	15.71	15.71	9.42	9.42	-10.06	-134.1
47	330	-8509	-680	-340	0	829	2712	15.71	15.71	9.42	9.42	-8.98	-119.9
49	330	-9602	-834	-430	0	1020	3130	15.71	15.71	9.42	9.42	-10.37	-138.2
50	330	-7926	-584	-302	0	758	2486	15.71	15.71	9.42	9.42	-8.22	-110.0
51	330	-8545	-691	-321	0	806	2738	15.71	15.71	9.42	9.42	-9.06	-121.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 35 NI 302 NF 291 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 1D
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	--												
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-9366	747	304	0	-830	-562	6.28	6.28	9.42	9.42	-9.70	-119.4
41	0	-9072	69	38	0	-874	373	6.28	6.28	9.42	9.42	-8.55	-118.3
42	0	-8909	59	-49	0	-937	379	6.28	6.28	9.42	9.42	-8.76	-120.6
43	0	-8727	1116	298	0	-857	-1122	6.28	6.28	9.42	9.42	-17.51	-180.7
44	0	-8708	-1062	-378	0	-939	1931	6.28	6.28	9.42	9.42	-30.58	503.0
45	0	-7966	-30	-290	0	-1036	446	6.28	6.28	9.42	9.42	-8.78	-119.7
46	0	-7737	-63	-256	0	-964	475	6.28	6.28	9.42	9.42	-8.32	-113.6
47	0	-7403	-96	-330	0	-987	500	6.28	6.28	9.42	9.42	-8.29	-112.8
49	0	-7501	130	-241	0	-972	188	6.28	6.28	9.42	9.42	-8.25	-112.5
50	0	-7497	-306	-376	0	-989	799	6.28	6.28	9.42	9.42	-12.43	-135.7
51	0	-7348	-100	-359	0	-1008	502	6.28	6.28	9.42	9.42	-8.38	-113.8

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	83	-8995	621	304	0	-1081	3	6.28	6.28	9.42	9.42	-9.47	-129.6
41	83	-8701	69	38	0	-906	430	6.28	6.28	9.42	9.42	-8.51	-117.3
42	83	-8538	59	25	0	-929	428	6.28	6.28	9.42	9.42	-8.53	-117.3
43	83	-8356	907	298	0	-1103	-287	6.28	6.28	9.42	9.42	-9.30	-126.6
44	83	-8337	-852	-378	0	-627	1141	6.28	6.28	9.42	9.42	-17.85	-180.6
45	83	-7595	-30	-168	0	-848	421	6.28	6.28	9.42	9.42	-7.69	-105.6
46	83	-7366	-63	-256	0	-753	423	6.28	6.28	9.42	9.42	-7.43	-98.5
47	83	-7032	-96	-330	0	-715	421	6.28	6.28	9.42	9.42	-7.27	-93.8
49	83	-7130	88	-241	0	-774	278	6.28	6.28	9.42	9.42	-7.11	-97.9
50	83	-7126	-264	-376	0	-678	564	6.28	6.28	9.42	9.42	-8.98	-105.6
51	83	-6977	-100	-334	0	-723	420	6.28	6.28	9.42	9.42	-7.24	-93.8

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	165	-8624	496	304	0	-1332	464	6.28	6.28	9.42	9.42	-10.69	-144.0
41	165	-8330	69	38	0	-938	488	6.28	6.28	9.42	9.42	-8.50	-116.3
42	165	-8166	59	88	0	-976	477	6.28	6.28	9.42	9.42	-8.57	-117.4
43	165	-7984	697	298	0	-1348	374	6.28	6.28	9.42	9.42	-10.62	-141.9
44	165	-7966	-643	-378	0	-315	525	6.28	6.28	9.42	9.42	-8.75	-106.3
45	165	-7224	-30	-62	0	-755	397	6.28	6.28	9.42	9.42	-7.12	-97.5
46	165	-6994	-63	-256	0	-542	371	6.28	6.28	9.42	9.42	-6.76	-84.4
47	165	-6660	-96	-330	0	-443	341	6.28	6.28	9.42	9.42	-6.33	-79.3
49	165	-6758	46	-241	0	-575	333	6.28	6.28	9.42	9.42	-6.31	-83.7
50	165	-6754	-222	-376	0	-368	363	6.28	6.28	9.42	9.42	-6.58	-82.0
51	165	-6606	-100	-313	0	-456	338	6.28	6.28	9.42	9.42	-6.27	-78.6

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	248	-8252	370	304	0	-1583	821	6.28	6.28	9.42	9.42	-12.77	-161.8
41	248	-7958	69	38	0	-969	545	6.28	6.28	9.42	9.42	-8.98	-115.5
42	248	-7795	59	141	0	-1072	526	6.28	6.28	9.42	9.42	-8.90	-120.9
43	248	-7613	488	298	0	-1594	863	6.28	6.28	9.42	9.42	-13.43	-160.3
44	248	-7594	-433	-378	0	-2	81	6.28	6.28	9.42	9.42	-4.39	-62.1
45	248	-6852	-30	25	0	-740	372	6.28	6.28	9.42	9.42	-6.82	-93.9
46	248	-6623	-63	-256	0	-331	318	6.28	6.28	9.42	9.42	-6.10	-76.9
47	248	-6289	-96	-330	0	-171	262	6.28	6.28	9.42	9.42	-5.42	-69.3
49	248	-6387	4	-241	0	-376	354	6.28	6.28	9.42	9.42	-6.32	-78.5
50	248	-6383	-180	-376	0	-58	197	6.28	6.28	9.42	9.42	-4.88	-64.1
51	248	-6234	-100	-296	0	-205	255	6.28	6.28	9.42	9.42	-5.34	-68.4

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	330	-7881	244	304	0	-1834	1074	6.28	6.28	9.42	9.42	-16.80	-181.8
41	330	-7587	69	38	0	-1001	602	6.28	6.28	9.42	9.42	-9.58	-114.9
42	330	-7424	59	183	0	-1206	575	6.28	6.28	9.42	9.42	-9.57	-128.3
43	330	-7242	278	298	0	-1839	1179	6.28	6.28	9.42	9.42	-18.55	225.2
44	330	-7223	-224	-378	0	310	-190	6.28	6.28	9.42	9.42	-5.22	-72.1
45	330	-6481	-30	95	0	-791	347	6.28	6.28	9.42	9.42	-6.88	-94.2
46	330	-6252	-63	-256	0	-119	266	6.28	6.28	9.42	9.42	-5.45	-69.5
47	330	-5918	-96	-330	0	101	182	6.28	6.28	9.42	9.42	-4.52	-59.4
49	330	-6016	-38	-241	0	-177	340	6.28	6.28	9.42	9.42	-6.02	-74.6
50	330	-6012	-138	-376	0	253	66	6.28	6.28	9.42	9.42	-4.18	-59.8
51	330	-5863	-100	-282	0	33	173	6.28	6.28	9.42	9.42	-4.41	-58.1

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 36 NI 325 NF 295 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 10D
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-9915	922	-297	0	-2418	-1382	6.28	6.28	12.57	12.57	-15.05	-190.7
41	0	-8993	-242	-216	0	-1972	215	6.28	6.28	12.57	12.57	-12.16	-156.7
42	0	-8971	-242	-539	0	-1305	214	6.28	6.28	12.57	12.57	-8.32	-112.4
43	0	-10180	1781	-299	0	-2265	-2583	6.28	6.28	12.57	12.57	-21.04	307.2
44	0	-7799	-2187	-93	0	-1315	2885	6.28	6.28	12.57	12.57	-23.28	456.5
45	0	-8605	-158	-703	0	-410	76	6.28	6.28	12.57	12.57	-4.79	-68.2
46	0	-8431	-109	-135	0	-1252	-3	6.28	6.28	12.57	12.57	-7.94	-107.1
47	0	-8291	-75	-114	0	-1072	-58	6.28	6.28	12.57	12.57	-7.10	-96.6
49	0	-8598	312	-141	0	-1220	-590	6.28	6.28	12.57	12.57	-7.83	-106.0
50	0	-8122	-481	-100	0	-1030	503	6.28	6.28	12.57	12.57	-6.87	-93.6
51	0	-8283	-75	-222	0	-850	-58	6.28	6.28	12.57	12.57	-6.24	-86.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	83	-9420	922	-297	0	-2173	-622	6.28	6.28	12.57	12.57	-13.45	-172.0
41	83	-8498	-242	-216	0	-1793	15	6.28	6.28	12.57	12.57	-11.03	-143.0
42	83	-8476	-242	-393	0	-922	14	6.28	6.28	12.57	12.57	-6.58	-90.4
43	83	-9684	1781	-299	0	-2018	-1114	6.28	6.28	12.57	12.57	-12.41	-161.1
44	83	-7304	-2187	-93	0	-1238	1081	6.28	6.28	12.57	12.57	-8.90	-106.7
45	83	-8110	-158	-459	0	66	-54	6.28	6.28	12.57	12.57	-3.37	-50.0
46	83	-7936	-109	-135	0	-1141	-93	6.28	6.28	12.57	12.57	-7.30	-98.7
47	83	-7796	-75	-114	0	-978	-120	6.28	6.28	12.57	12.57	-6.55	-89.3
49	83	-8103	312	-141	0	-1104	-332	6.28	6.28	12.57	12.57	-7.18	-97.4
50	83	-7627	-481	-100	0	-948	106	6.28	6.28	12.57	12.57	-6.37	-86.9
51	83	-7788	-75	-173	0	-687	-121	6.28	6.28	12.57	12.57	-5.47	-75.9

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	165	-8925	922	-297	0	-1928	139	6.28	6.28	12.57	12.57	-11.88	-153.4
41	165	-8003	-242	-216	0	-1614	-184	6.28	6.28	12.57	12.57	-9.92	-129.4
42	165	-7981	-242	-268	0	-651	-185	6.28	6.28	12.57	12.57	-5.41	-75.4
43	165	-9189	1781	-299	0	-1771	356	6.28	6.28	12.57	12.57	-10.88	-142.7
44	165	-6809	-2187	-93	0	-1161	-723	6.28	6.28	12.57	12.57	-7.19	-95.6
45	165	-7615	-158	-250	0	357	-185	6.28	6.28	12.57	12.57	-4.22	-60.1
46	165	-7441	-109	-135	0	-1030	-183	6.28	6.28	12.57	12.57	-6.66	-90.3
47	165	-7301	-75	-114	0	-883	-182	6.28	6.28	12.57	12.57	-6.00	-82.0
49	165	-7608	312	-141	0	-988	-75	6.28	6.28	12.57	12.57	-6.53	-88.9
50	165	-7132	-481	-100	0	-865	-290	6.28	6.28	12.57	12.57	-5.87	-80.3
51	165	-7293	-75	-131	0	-562	-183	6.28	6.28	12.57	12.57	-4.83	-67.4

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	248	-8430	922	-297	0	-1683	900	6.28	6.28	12.57	12.57	-10.34	-135.0
41	248	-7508	-242	-216	0	-1436	-383	6.28	6.28	12.57	12.57	-8.82	-115.8
42	248	-7486	-242	-163	0	-475	-384	6.28	6.28	12.57	12.57	-4.59	-64.6
43	248	-8694	1781	-299	0	-1524	1825	6.28	6.28	12.57	12.57	-14.90	174.4
44	248	-6314	-2187	-93	0	-1084	-2527	6.28	6.28	12.57	12.57	-20.34	417.3
45	248	-7120	-158	-77	0	489	-315	6.28	6.28	12.57	12.57	-4.50	-63.2
46	248	-6946	-109	-135	0	-918	-272	6.28	6.28	12.57	12.57	-6.03	-82.0
47	248	-6806	-75	-114	0	-789	-245	6.28	6.28	12.57	12.57	-5.46	-74.8
49	248	-7113	312	-141	0	-871	183	6.28	6.28	12.57	12.57	-5.89	-80.5
50	248	-6637	-481	-100	0	-783	-687	6.28	6.28	12.57	12.57	-5.94	-75.4
51	248	-6798	-75	-97	0	-469	-245	6.28	6.28	12.57	12.57	-4.30	-60.4

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	330	-7935	922	-297	0	-1438	1660	6.28	6.28	12.57	12.57	-13.56	157.9
41	330	-7013	-242	-216	0	-1257	-583	6.28	6.28	12.57	12.57	-7.74	-102.5
42	330	-6991	-242	-80	0	-376	-584	6.28	6.28	12.57	12.57	-5.42	-70.4
43	330	-8198	1781	-299	0	-1277	3294	6.28	6.28	12.57	12.57	-26.51	545.1
44	330	-5819	-2187	-93	0	-1007	-4331	6.28	6.28	12.57	12.57	-34.18	891.6
45	330	-6625	-158	62	0	493	-446	6.28	6.28	12.57	12.57	-4.59	-60.6
46	330	-6451	-109	-135	0	-807	-362	6.28	6.28	12.57	12.57	-5.41	-73.8
47	330	-6311	-75	-114	0	-695	-307	6.28	6.28	12.57	12.57	-4.93	-67.7
49	330	-6618	312	-141	0	-755	441	6.28	6.28	12.57	12.57	-5.26	-72.2
50	330	-6142	-481	-100	0	-701	-1084	6.28	6.28	12.57	12.57	-8.87	-102.8
51	330	-6303	-75	-69	0	-401	-307	6.28	6.28	12.57	12.57	-3.87	-54.5

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 37 NI 296 NF 297 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 15C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-14770	878	-612	0	-2364	-1531	6.28	6.28	12.57	12.57	-14.77	-197.8
41	0	-14400	-250	-534	0	-2022	519	6.28	6.28	12.57	12.57	-13.02	-176.4
42	0	-14250	-251	-1058	0	-1717	522	6.28	6.28	12.57	12.57	-11.69	-159.8
43	0	-13750	1693	-535	0	-2095	-3026	6.28	6.28	12.57	12.57	-24.70	307.3
44	0	-14010	-2137	-429	0	-1548	3951	6.28	6.28	12.57	12.57	-32.11	517.5
45	0	-12870	-189	-1280	0	-1016	396	6.28	6.28	12.57	12.57	-8.61	-120.1
46	0	-12360	-150	-328	0	-1225	315	6.28	6.28	12.57	12.57	-9.16	-126.5
47	0	-11850	-125	-276	0	-1026	264	6.28	6.28	12.57	12.57	-8.25	-114.6
49	0	-11970	251	-302	0	-1140	-420	6.28	6.28	12.57	12.57	-8.71	-120.4
50	0	-12020	-515	-281	0	-1031	976	6.28	6.28	12.57	12.57	-9.17	-119.4
51	0	-11800	-125	-451	0	-924	265	6.28	6.28	12.57	12.57	-7.87	-109.8

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	95	-14200	878	-612	0	-1783	-697	6.28	6.28	12.57	12.57	-11.93	-162.8
41	95	-13830	-250	-534	0	-1515	282	6.28	6.28	12.57	12.57	-10.77	-148.0
42	95	-13680	-251	-890	0	-793	283	6.28	6.28	12.57	12.57	-8.13	-114.8
43	95	-13180	1693	-535	0	-1586	-1418	6.28	6.28	12.57	12.57	-12.15	-153.4
44	95	-13440	-2137	-429	0	-1141	1920	6.28	6.28	12.57	12.57	-15.84	-191.1
45	95	-12300	-189	-999	0	63	216	6.28	6.28	12.57	12.57	-5.49	-78.4
46	95	-11790	-150	-328	0	-914	172	6.28	6.28	12.57	12.57	-7.83	-109.2
47	95	-11280	-125	-276	0	-763	145	6.28	6.28	12.57	12.57	-7.09	-99.5
49	95	-11400	251	-302	0	-853	-181	6.28	6.28	12.57	12.57	-7.46	-104.2
50	95	-11451	-515	-281	0	-764	487	6.28	6.28	12.57	12.57	-7.16	-100.5

51	95	-11229	-125	-395	0	-523	146	6.28	6.28	12.57	12.57	-6.21	-88.5

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	190	-13630	878	-612	0	-1202	138	6.28	6.28	12.57	12.57	-9.57	-132.8
41	190	-13260	-250	-534	0	-1008	44	6.28	6.28	12.57	12.57	-8.73	-122.0
42	190	-13110	-251	-746	0	-18	45	6.28	6.28	12.57	12.57	-5.13	-76.8
43	190	-12610	1693	-535	0	-1078	190	6.28	6.28	12.57	12.57	-8.73	-121.3
44	190	-12870	-2137	-429	0	-733	-110	6.28	6.28	12.57	12.57	-7.60	-107.4
45	190	-11730	-189	-759	0	895	36	6.28	6.28	12.57	12.57	-7.74	-108.0
46	190	-11220	-150	-328	0	-602	30	6.28	6.28	12.57	12.57	-6.49	-92.0
47	190	-10709	-125	-276	0	-501	27	6.28	6.28	12.57	12.57	-5.93	-84.5
49	190	-10831	251	-302	0	-565	58	6.28	6.28	12.57	12.57	-6.21	-88.1
50	190	-10882	-515	-281	0	-497	-2	6.28	6.28	12.57	12.57	-5.98	-85.3
51	190	-10658	-125	-347	0	-171	27	6.28	6.28	12.57	12.57	-4.73	-69.4

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	285	-13060	878	-612	0	-621	972	6.28	6.28	12.57	12.57	-9.50	-124.6
41	285	-12690	-250	-534	0	-501	-193	6.28	6.28	12.57	12.57	-6.70	-96.0
42	285	-12540	-251	-626	0	632	-194	6.28	6.28	12.57	12.57	-7.11	-100.9
43	285	-12040	1693	-535	0	-569	1799	6.28	6.28	12.57	12.57	-14.80	-177.1
44	285	-12300	-2137	-429	0	-326	-2141	6.28	6.28	12.57	12.57	-17.53	-203.6
45	285	-11160	-189	-559	0	1518	-144	6.28	6.28	12.57	12.57	-9.87	-134.0
46	285	-10650	-150	-328	0	-291	-112	6.28	6.28	12.57	12.57	-5.16	-74.7
47	285	-10138	-125	-276	0	-238	-92	6.28	6.28	12.57	12.57	-4.77	-69.4
49	285	-10262	251	-302	0	-278	296	6.28	6.28	12.57	12.57	-5.16	-71.9
50	285	-10314	-515	-281	0	-230	-492	6.28	6.28	12.57	12.57	-6.14	-83.0
51	285	-10088	-125	-307	0	139	-92	6.28	6.28	12.57	12.57	-4.40	-64.7

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	380	-12490	878	-612	0	-40	1806	6.28	6.28	12.57	12.57	-14.89	-179.2
41	380	-12120	-250	-534	0	6	-431	6.28	6.28	12.57	12.57	-6.49	-89.4
42	380	-11970	-251	-530	0	1179	-433	6.28	6.28	12.57	12.57	-8.85	-122.1
43	380	-11470	1693	-535	0	-61	3407	6.28	6.28	12.57	12.57	-27.66	465.4
44	380	-11730	-2137	-429	0	81	-4171	6.28	6.28	12.57	12.57	-33.70	644.9
45	380	-10590	-189	-399	0	1970	-324	6.28	6.28	12.57	12.57	-12.11	-159.6
46	380	-10080	-150	-328	0	21	-255	6.28	6.28	12.57	12.57	-4.89	-68.6
47	380	-9568	-125	-276	0	24	-211	6.28	6.28	12.57	12.57	-4.49	-63.4
49	380	-9692	251	-302	0	9	535	6.28	6.28	12.57	12.57	-6.13	-82.1
50	380	-9745	-515	-281	0	38	-981	6.28	6.28	12.57	12.57	-8.55	-108.8
51	380	-9517	-125	-275	0	415	-211	6.28	6.28	12.57	12.57	-5.16	-73.7

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 38 NI 299 NF 294 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 10B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	--												
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-23030	778	379	0	147	-1849	6.28	6.28	12.57	12.57	-17.46	-227.5
41	0	-22240	21	350	0	217	-52	6.28	6.28	12.57	12.57	-9.37	-138.6
42	0	-22210	24	158	0	-81	-58	6.28	6.28	12.57	12.57	-8.87	-132.3
43	0	-22970	1261	333	0	63	-3009	6.28	6.28	12.57	12.57	-25.00	-306.3
44	0	-20970	-1235	307	0	324	2932	6.28	6.28	12.57	12.57	-24.22	-293.4
45	0	-21610	4	-35	0	-317	-24	6.28	6.28	12.57	12.57	-9.48	-139.4
46	0	-21290	-15	246	0	156	9	6.28	6.28	12.57	12.57	-8.78	-130.4
47	0	-21060	-24	220	0	141	24	6.28	6.28	12.57	12.57	-8.64	-128.4
49	0	-21320	228	230	0	118	-575	6.28	6.28	12.57	12.57	-10.52	-147.1
50	0	-20920	-271	224	0	170	613	6.28	6.28	12.57	12.57	-10.56	-147.1
51	0	-21050	-23	156	0	42	22	6.28	6.28	12.57	12.57	-8.28	-123.8

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	97	-22445	778	379	0	-222	-1090	6.28	6.28	12.57	12.57	-13.47	-181.8
41	97	-21655	21	350	0	-124	-32	6.28	6.28	12.57	12.57	-8.81	-131.1
42	97	-21625	24	158	0	-235	-34	6.28	6.28	12.57	12.57	-9.19	-135.8
43	97	-22385	1261	333	0	-261	-1780	6.28	6.28	12.57	12.57	-16.88	-220.1
44	97	-20385	-1235	307	0	25	1728	6.28	6.28	12.57	12.57	-15.95	-206.8
45	97	-21025	4	-35	0	-283	-20	6.28	6.28	12.57	12.57	-9.14	-134.5
46	97	-20705	-15	246	0	-84	-6	6.28	6.28	12.57	12.57	-8.30	-123.7
47	97	-20475	-24	220	0	-74	0	6.28	6.28	12.57	12.57	-8.17	-121.9
49	97	-20735	228	230	0	-106	-352	6.28	6.28	12.57	12.57	-9.21	-131.6
50	97	-20335	-271	224	0	-49	349	6.28	6.28	12.57	12.57	-9.05	-129.2
51	97	-20465	-23	156	0	-110	-0	6.28	6.28	12.57	12.57	-8.30	-123.5

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	195	-21860	778	379	0	-591	-331	6.28	6.28	12.57	12.57	-10.56	-153.1
41	195	-21070	21	350	0	-466	-11	6.28	6.28	12.57	12.57	-9.81	-143.0
42	195	-21040	24	158	0	-389	-11	6.28	6.28	12.57	12.57	-9.52	-139.3
43	195	-21800	1261	333	0	-586	-550	6.28	6.28	12.57	12.57	-10.57	-152.5
44	195	-19800	-1235	307	0	-275	524	6.28	6.28	12.57	12.57	-9.72	-136.1
45	195	-20440	4	-35	0	-248	-17	6.28	6.28	12.57	12.57	-8.79	-129.6
46	195	-20120	-15	246	0	-324	-21	6.28	6.28	12.57	12.57	-8.93	-131.1
47	195	-19890	-24	220	0	-288	-23	6.28	6.28	12.57	12.57	-8.72	-128.2
49	195	-20150	228	230	0	-330	-130	6.28	6.28	12.57	12.57	-8.97	-131.5
50	195	-19750	-271	224	0	-268	85	6.28	6.28	12.57	12.57	-8.59	-126.4
51	195	-19880	-23	156	0	-263	-23	6.28	6.28	12.57	12.57	-8.62	-127.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	292	-21275	778	379	0	-961	428	6.28	6.28	12.57	12.57	-11.66	-166.3
41	292	-20485	21	350	0	-807	10	6.28	6.28	12.57	12.57	-10.81	-154.9
42	292	-20455	24	158	0	-543	13	6.28	6.28	12.57	12.57	-9.85	-142.8
43	292	-21215	1261	333	0	-910	679	6.28	6.28	12.57	12.57	-11.45	-163.7
44	292	-19215	-1235	307	0	-574	-680	6.28	6.28	12.57	12.57	-10.28	-141.6
45	292	-19855	4	-35	0	-214	-13	6.28	6.28	12.57	12.57	-8.44	-124.6
46	292	-19535	-15	246	0	-564	-35	6.28	6.28	12.57	12.57	-9.57	-138.4
47	292	-19305	-24	220	0	-503	-47	6.28	6.28	12.57	12.57	-9.26	-134.4
49	292	-19565	228	230	0	-554	93	6.28	6.28	12.57	12.57	-9.54	-138.2
50	292	-19165	-271	224	0	-487	-179	6.28	6.28	12.57	12.57	-9.15	-132.8
51	292	-19295	-23	156	0	-415	-45	6.28	6.28	12.57	12.57	-8.94	-130.4

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	390	-20690	778	379	0	-1330	1187	6.28	6.28	12.57	12.57	-13.31	-179.4
41	390	-19900	21	350	0	-1149	30	6.28	6.28	12.57	12.57	-11.80	-166.7
42	390	-19870	24	158	0	-697	36	6.28	6.28	12.57	12.57	-10.17	-146.3
43	390	-20630	1261	333	0	-1234	1908	6.28	6.28	12.57	12.57	-17.06	-219.3
44	390	-18630	-1235	307	0	-874	-1884	6.28	6.28	12.57	12.57	-16.40	-208.6
45	390	-19270	4	-35	0	-180	-10	6.28	6.28	12.57	12.57	-8.09	-119.7
46	390	-18950	-15	246	0	-804	-50	6.28	6.28	12.57	12.57	-10.20	-145.8
47	390	-18720	-24	220	0	-718	-70	6.28	6.28	12.57	12.57	-9.80	-140.6
49	390	-18980	228	230	0	-778	316	6.28	6.28	12.57	12.57	-10.12	-144.8
50	390	-18580	-271	224	0	-706	-443	6.28	6.28	12.57	12.57	-9.70	-139.3
51	390	-18710	-23	156	0	-567	-68	6.28	6.28	12.57	12.57	-9.26	-133.8

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 39 NI 300 NF 296 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 15B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-32330	686	532	0	490	-1242	6.28	6.28	12.57	12.57	-17.78	-243.7
41	0	-31910	133	520	0	518	-175	6.28	6.28	12.57	12.57	-14.18	-208.1
42	0	-31770	136	335	0	252	-180	6.28	6.28	12.57	12.57	-13.17	-195.4
43	0	-30920	1042	502	0	482	-1942	6.28	6.28	12.57	12.57	-20.73	-275.0
44	0	-30910	-786	486	0	530	1600	6.28	6.28	12.57	12.57	-19.04	-255.9
45	0	-29980	126	174	0	84	-172	6.28	6.28	12.57	12.57	-11.88	-177.5
46	0	-29180	114	460	0	533	-157	6.28	6.28	12.57	12.57	-13.18	-193.0
47	0	-28500	109	445	0	537	-152	6.28	6.28	12.57	12.57	-12.93	-189.2
49	0	-28650	293	449	0	528	-508	6.28	6.28	12.57	12.57	-12.96	-189.6
50	0	-28640	-72	446	0	537	200	6.28	6.28	12.57	12.57	-12.99	-190.0
51	0	-28460	110	383	0	448	-154	6.28	6.28	12.57	12.57	-12.60	-185.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	97	-31745	686	532	0	-28	-574	6.28	6.28	12.57	12.57	-14.26	-203.3
41	97	-31325	133	520	0	11	-46	6.28	6.28	12.57	12.57	-12.14	-182.0
42	97	-31185	136	335	0	-75	-48	6.28	6.28	12.57	12.57	-12.32	-184.1
43	97	-30335	1042	502	0	-8	-926	6.28	6.28	12.57	12.57	-15.50	-215.3
44	97	-30325	-786	486	0	56	834	6.28	6.28	12.57	12.57	-15.04	-210.2
45	97	-29395	126	174	0	-86	-49	6.28	6.28	12.57	12.57	-11.66	-174.2
46	97	-28595	114	460	0	85	-46	6.28	6.28	12.57	12.57	-11.35	-169.5
47	97	-27915	109	445	0	103	-46	6.28	6.28	12.57	12.57	-11.15	-166.4
49	97	-28065	293	449	0	90	-222	6.28	6.28	12.57	12.57	-11.20	-166.7
50	97	-28055	-72	446	0	103	130	6.28	6.28	12.57	12.57	-11.21	-167.2
51	97	-27875	110	383	0	74	-47	6.28	6.28	12.57	12.57	-11.04	-164.9

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	195	-31160	686	532	0	-546	95	6.28	6.28	12.57	12.57	-13.99	-205.0
41	195	-30740	133	520	0	-495	84	6.28	6.28	12.57	12.57	-13.65	-200.3
42	195	-30600	136	335	0	-401	85	6.28	6.28	12.57	12.57	-13.26	-195.3
43	195	-29750	1042	502	0	-498	90	6.28	6.28	12.57	12.57	-13.28	-194.7
44	195	-29740	-786	486	0	-418	68	6.28	6.28	12.57	12.57	-12.98	-191.0
45	195	-28810	126	174	0	-256	73	6.28	6.28	12.57	12.57	-12.05	-178.4
46	195	-28010	114	460	0	-363	65	6.28	6.28	12.57	12.57	-12.12	-178.6
47	195	-27330	109	445	0	-330	60	6.28	6.28	12.57	12.57	-11.74	-173.2
49	195	-27480	293	449	0	-348	64	6.28	6.28	12.57	12.57	-11.86	-174.8
50	195	-27470	-72	446	0	-332	59	6.28	6.28	12.57	12.57	-11.80	-174.0
51	195	-27290	110	383	0	-299	60	6.28	6.28	12.57	12.57	-11.61	-171.5

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	292	-30575	686	532	0	-1064	763	6.28	6.28	12.57	12.57	-15.62	-224.8
41	292	-30155	133	520	0	-1002	213	6.28	6.28	12.57	12.57	-15.24	-219.6
42	292	-30015	136	335	0	-728	217	6.28	6.28	12.57	12.57	-14.20	-206.5
43	292	-29165	1042	502	0	-987	1106	6.28	6.28	12.57	12.57	-15.97	-219.0
44	292	-29155	-786	486	0	-891	-698	6.28	6.28	12.57	12.57	-14.45	-208.8
45	292	-28225	126	174	0	-425	196	6.28	6.28	12.57	12.57	-12.43	-182.6
46	292	-27425	114	460	0	-812	176	6.28	6.28	12.57	12.57	-13.50	-195.3
47	292	-26745	109	445	0	-764	166	6.28	6.28	12.57	12.57	-13.07	-189.2
49	292	-26895	293	449	0	-785	350	6.28	6.28	12.57	12.57	-13.20	-191.0
50	292	-26885	-72	446	0	-766	-11	6.28	6.28	12.57	12.57	-13.13	-190.1
51	292	-26705	110	383	0	-673	168	6.28	6.28	12.57	12.57	-12.73	-184.9

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	390	-29990	686	532	0	-1582	1432	6.28	6.28	12.57	12.57	-17.87	-244.6
41	390	-29570	133	520	0	-1508	343	6.28	6.28	12.57	12.57	-16.82	-238.9
42	390	-29430	136	335	0	-1054	349	6.28	6.28	12.57	12.57	-15.14	-217.7
43	390	-28580	1042	502	0	-1477	2122	6.28	6.28	12.57	12.57	-20.78	-272.3
44	390	-28570	-786	486	0	-1365	-1464	6.28	6.28	12.57	12.57	-17.52	-235.7
45	390	-27640	126	174	0	-595	318	6.28	6.28	12.57	12.57	-12.81	-186.8
46	390	-26840	114	460	0	-1260	287	6.28	6.28	12.57	12.57	-14.88	-211.9
47	390	-26160	109	445	0	-1198	273	6.28	6.28	12.57	12.57	-14.40	-205.2
49	390	-26310	293	449	0	-1223	636	6.28	6.28	12.57	12.57	-14.54	-207.2
50	390	-26300	-72	446	0	-1201	-82	6.28	6.28	12.57	12.57	-14.46	-206.2
51	390	-26120	110	383	0	-1047	275	6.28	6.28	12.57	12.57	-13.84	-198.2

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 40 NI 301 NF 298 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 20B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-28900	634	744	0	884	-1272	6.28	6.28	12.57	12.57	-16.69	-226.8

41	0	-29230	124	690	0	808	-242	6.28	6.28	12.57	12.57	-14.19	-205.6
42	0	-29160	128	542	0	647	-247	6.28	6.28	12.57	12.57	-13.58	-197.9
43	0	-27460	960	708	0	884	-1939	6.28	6.28	12.57	12.57	-19.47	-256.1
44	0	-29510	-726	592	0	658	1478	6.28	6.28	12.57	12.57	-17.93	-241.5
45	0	-27910	116	373	0	489	-230	6.28	6.28	12.57	12.57	-12.53	-183.6
46	0	-27310	101	577	0	728	-209	6.28	6.28	12.57	12.57	-13.16	-190.8
47	0	-26820	96	549	0	708	-200	6.28	6.28	12.57	12.57	-12.90	-187.1
49	0	-26710	266	566	0	733	-544	6.28	6.28	12.57	12.57	-12.94	-187.6
50	0	-27120	-71	543	0	688	139	6.28	6.28	12.57	12.57	-12.94	-188.0
51	0	-26800	97	499	0	654	-202	6.28	6.28	12.57	12.57	-12.70	-184.6

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	97	-28315	634	744	0	159	-654	6.28	6.28	12.57	12.57	-13.43	-189.3
41	97	-28645	124	690	0	135	-121	6.28	6.28	12.57	12.57	-11.55	-172.1
42	97	-28575	128	542	0	118	-123	6.28	6.28	12.57	12.57	-11.46	-170.9
43	97	-26875	960	708	0	193	-1004	6.28	6.28	12.57	12.57	-14.64	-200.9
44	97	-28925	-726	592	0	80	770	6.28	6.28	12.57	12.57	-14.22	-199.1
45	97	-27325	116	373	0	126	-117	6.28	6.28	12.57	12.57	-11.01	-164.0
46	97	-26725	101	577	0	165	-110	6.28	6.28	12.57	12.57	-10.92	-162.3
47	97	-26235	96	549	0	173	-107	6.28	6.28	12.57	12.57	-10.75	-159.8
49	97	-26125	266	566	0	181	-285	6.28	6.28	12.57	12.57	-10.82	-159.5
50	97	-26535	-71	543	0	158	70	6.28	6.28	12.57	12.57	-10.82	-160.9
51	97	-26215	97	499	0	167	-108	6.28	6.28	12.57	12.57	-10.73	-159.4

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	195	-27730	634	744	0	-566	-36	6.28	6.28	12.57	12.57	-12.74	-186.0
41	195	-28060	124	690	0	-538	0	6.28	6.28	12.57	12.57	-12.77	-186.7
42	195	-27990	128	542	0	-410	2	6.28	6.28	12.57	12.57	-12.28	-180.6
43	195	-26290	960	708	0	-497	-68	6.28	6.28	12.57	12.57	-11.94	-174.6
44	195	-28340	-726	592	0	-497	63	6.28	6.28	12.57	12.57	-12.73	-186.5
45	195	-26740	116	373	0	-238	-4	6.28	6.28	12.57	12.57	-11.18	-165.6
46	195	-26140	101	577	0	-397	-11	6.28	6.28	12.57	12.57	-11.52	-169.3
47	195	-25650	96	549	0	-362	-14	6.28	6.28	12.57	12.57	-11.21	-164.8
49	195	-25540	266	566	0	-371	-26	6.28	6.28	12.57	12.57	-11.20	-164.6
50	195	-25950	-71	543	0	-371	-0	6.28	6.28	12.57	12.57	-11.36	-167.0
51	195	-25630	97	499	0	-319	-13	6.28	6.28	12.57	12.57	-11.05	-162.8

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	292	-27145	634	744	0	-1291	582	6.28	6.28	12.57	12.57	-15.11	-215.1
41	292	-27475	124	690	0	-1211	121	6.28	6.28	12.57	12.57	-14.95	-213.4
42	292	-27405	128	542	0	-939	127	6.28	6.28	12.57	12.57	-13.95	-200.8
43	292	-25705	960	708	0	-1188	867	6.28	6.28	12.57	12.57	-14.18	-202.1
44	292	-27755	-726	592	0	-1075	-644	6.28	6.28	12.57	12.57	-14.57	-209.0
45	292	-26155	116	373	0	-601	110	6.28	6.28	12.57	12.57	-12.26	-178.5
46	292	-25555	101	577	0	-960	88	6.28	6.28	12.57	12.57	-13.31	-191.1
47	292	-25065	96	549	0	-897	79	6.28	6.28	12.57	12.57	-12.90	-185.4
49	292	-24955	266	566	0	-924	233	6.28	6.28	12.57	12.57	-12.95	-186.0
50	292	-25365	-71	543	0	-901	-70	6.28	6.28	12.57	12.57	-13.03	-187.3
51	292	-25045	97	499	0	-806	81	6.28	6.28	12.57	12.57	-12.56	-181.2

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	390	-26560	634	744	0	-2016	1200	6.28	6.28	12.57	12.57	-17.48	-244.1
41	390	-26890	124	690	0	-1884	242	6.28	6.28	12.57	12.57	-17.13	-240.2
42	390	-26820	128	542	0	-1468	252	6.28	6.28	12.57	12.57	-15.62	-221.1
43	390	-25120	960	708	0	-1878	1803	6.28	6.28	12.57	12.57	-17.95	-235.9
44	390	-27170	-726	592	0	-1653	-1352	6.28	6.28	12.57	12.57	-16.46	-231.4
45	390	-25570	116	373	0	-965	223	6.28	6.28	12.57	12.57	-13.33	-191.4
46	390	-24970	101	577	0	-1523	186	6.28	6.28	12.57	12.57	-15.10	-212.9
47	390	-24480	96	549	0	-1432	172	6.28	6.28	12.57	12.57	-14.58	-206.0
49	390	-24370	266	566	0	-1476	492	6.28	6.28	12.57	12.57	-14.70	-207.3
50	390	-24780	-71	543	0	-1431	-140	6.28	6.28	12.57	12.57	-14.70	-207.6
51	390	-24460	97	499	0	-1293	176	6.28	6.28	12.57	12.57	-14.08	-199.6

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 41 NI 35 NF 31 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 12D
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	--												
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-5665	719	714	0	-2209	-1075	6.28	6.28	12.57	12.57	-14.37	305.9
41	0	-4747	705	584	0	-1634	-967	6.28	6.28	12.57	12.57	-10.53	195.2
42	0	-4723	759	-24	0	-5037	-1022	6.28	6.28	12.57	12.57	-32.97	1235.4
43	0	-5685	778	668	0	-2201	-1192	6.28	6.28	12.57	12.57	-14.31	302.5
44	0	-3552	696	393	0	-758	-807	6.28	6.28	12.57	12.57	-6.58	85.1
45	0	-4116	845	-562	0	-6914	-1104	6.28	6.28	12.57	12.57	-44.86	1867.3
46	0	-3800	785	373	0	-1008	-1039	6.28	6.28	12.57	12.57	-8.45	132.5
47	0	-3563	805	320	0	-852	-1057	6.28	6.28	12.57	12.57	-8.58	144.3
49	0	-3869	809	363	0	-1043	-1093	6.28	6.28	12.57	12.57	-8.88	143.4
50	0	-3443	793	308	0	-755	-1016	6.28	6.28	12.57	12.57	-8.25	138.1
51	0	-3555	822	117	0	-1986	-1076	6.28	6.28	12.57	12.57	-13.07	370.5

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	58	-5318	719	714	0	-2622	-659	6.28	6.28	12.57	12.57	-17.22	448.7
41	58	-4400	705	584	0	-1972	-559	6.28	6.28	12.57	12.57	-12.91	312.4
42	58	-4376	759	-236	0	-4962	-583	6.28	6.28	12.57	12.57	-32.44	1236.8
43	58	-5338	778	668	0	-2587	-742	6.28	6.28	12.57	12.57	-16.98	437.1
44	58	-3205	696	393	0	-985	-404	6.28	6.28	12.57	12.57	-6.28	100.0
45	58	-3769	845	-914	0	-6487	-616	6.28	6.28	12.57	12.57	-42.07	1758.8
46	58	-3453	785	373	0	-1224	-585	6.28	6.28	12.57	12.57	-7.90	151.6
47	58	-3216	805	320	0	-1037	-592	6.28	6.28	12.57	12.57	-6.64	113.2
49	58	-3522	809	363	0	-1253	-625	6.28	6.28	12.57	12.57	-8.10	156.1
50	58	-3096	793	308	0	-933	-558	6.28	6.28	12.57	12.57	-5.94	91.8
51	58	-3208	822	47	0	-2033	-600	6.28	6.28	12.57	12.57	-13.39	408.2

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	116	-4971	719	714	0	-3034	-243	6.28	6.28	12.57	12.57	-19.98	596.8
41	116	-4053	705	584	0	-2310	-152	6.28	6.28	12.57	12.57	-15.20	436.2

42	116	-4029	759	-448	0	-4764	-144	6.28	6.28	12.57	12.57	-31.12	1199.9
43	116	-4991	778	668	0	-2974	-292	6.28	6.28	12.57	12.57	-19.58	576.7
44	116	-2858	696	393	0	-1212	-2	6.28	6.28	12.57	12.57	-7.92	182.7
45	116	-3422	845	-1267	0	-5856	-127	6.28	6.28	12.57	12.57	-37.98	1586.3
46	116	-3106	785	373	0	-1439	-132	6.28	6.28	12.57	12.57	-9.43	234.5
47	116	-2869	805	320	0	-1222	-127	6.28	6.28	12.57	12.57	-7.98	184.9
49	116	-3175	809	363	0	-1463	-157	6.28	6.28	12.57	12.57	-9.59	237.3
50	116	-2749	793	308	0	-1111	-99	6.28	6.28	12.57	12.57	-7.24	159.7
51	116	-2862	822	-24	0	-2040	-124	6.28	6.28	12.57	12.57	-13.43	433.8

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	173	-4624	719	714	0	-3447	173	6.28	6.28	12.57	12.57	-22.68	747.6
41	173	-3706	705	584	0	-2647	256	6.28	6.28	12.57	12.57	-17.43	563.4
42	173	-3682	759	-659	0	-4444	295	6.28	6.28	12.57	12.57	-29.02	1124.7
43	173	-4644	778	668	0	-3360	159	6.28	6.28	12.57	12.57	-22.11	719.1
44	173	-2511	696	393	0	-1440	401	6.28	6.28	12.57	12.57	-9.48	273.0
45	173	-3075	845	-1620	0	-5021	361	6.28	6.28	12.57	12.57	-32.60	1349.8
46	173	-2759	785	373	0	-1654	322	6.28	6.28	12.57	12.57	-10.89	322.1
47	173	-2522	805	320	0	-1407	339	6.28	6.28	12.57	12.57	-9.26	262.3
49	173	-2828	809	363	0	-1673	311	6.28	6.28	12.57	12.57	-11.02	323.2
50	173	-2402	793	308	0	-1289	359	6.28	6.28	12.57	12.57	-8.48	234.3
51	173	-2515	822	-94	0	-2006	351	6.28	6.28	12.57	12.57	-13.19	447.2

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	231	-4277	719	714	0	-3860	589	6.28	6.28	12.57	12.57	-25.34	900.0
41	231	-3359	705	584	0	-2985	664	6.28	6.28	12.57	12.57	-19.60	692.3
42	231	-3335	759	-871	0	-4001	734	6.28	6.28	12.57	12.57	-26.13	1011.3
43	231	-4297	778	668	0	-3746	609	6.28	6.28	12.57	12.57	-24.60	863.1
44	231	-2164	696	393	0	-1667	804	6.28	6.28	12.57	12.57	-10.97	366.5
45	231	-2728	845	-1973	0	-3982	850	6.28	6.28	12.57	12.57	-25.91	1049.3
46	231	-2412	785	373	0	-1870	776	6.28	6.28	12.57	12.57	-12.30	412.2
47	231	-2175	805	320	0	-1592	804	6.28	6.28	12.57	12.57	-10.48	342.5
49	231	-2481	809	363	0	-1883	779	6.28	6.28	12.57	12.57	-12.39	411.4
50	231	-2055	793	308	0	-1467	818	6.28	6.28	12.57	12.57	-9.66	312.1
51	231	-2168	822	-165	0	-1931	827	6.28	6.28	12.57	12.57	-12.68	448.2

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 42 NI 37 NF 43 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 17D
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-5844	403	484	0	-2921	-565	6.28	6.28	12.57	12.57	-19.19	505.1
41	0	-5134	187	402	0	-2541	-222	6.28	6.28	12.57	12.57	-16.69	436.2
42	0	-5208	191	78	0	-6833	-232	6.28	6.28	12.57	12.57	-44.55	1762.3
43	0	-5516	534	445	0	-2599	-768	6.28	6.28	12.57	12.57	-17.05	429.4
44	0	-4163	-160	282	0	-2015	329	6.28	6.28	12.57	12.57	-13.23	340.1
45	0	-4456	180	-230	0	-9119	-213	6.28	6.28	12.57	12.57	-58.96	2534.3
46	0	-3852	164	254	0	-1619	-182	6.28	6.28	12.57	12.57	-10.57	241.9
47	0	-3531	159	217	0	-1389	-171	6.28	6.28	12.57	12.57	-9.04	194.2
49	0	-3768	231	244	0	-1516	-285	6.28	6.28	12.57	12.57	-9.88	216.9
50	0	-3497	92	211	0	-1399	-66	6.28	6.28	12.57	12.57	-9.11	199.0
51	0	-3556	160	109	0	-2820	-174	6.28	6.28	12.57	12.57	-18.54	627.3

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	88	-5313	403	484	0	-3349	-208	6.28	6.28	12.57	12.57	-22.06	670.2
41	88	-4603	187	402	0	-2897	-57	6.28	6.28	12.57	12.57	-19.08	579.2
42	88	-4677	191	-246	0	-6759	-63	6.28	6.28	12.57	12.57	-43.98	1777.7
43	88	-4985	534	445	0	-2993	-295	6.28	6.28	12.57	12.57	-19.71	583.1
44	88	-3632	-160	282	0	-2264	187	6.28	6.28	12.57	12.57	-14.91	450.4
45	88	-3925	180	-771	0	-8676	-54	6.28	6.28	12.57	12.57	-56.02	2434.4
46	88	-3321	164	254	0	-1844	-36	6.28	6.28	12.57	12.57	-12.13	342.6
47	88	-3000	159	217	0	-1581	-31	6.28	6.28	12.57	12.57	-10.40	283.8
49	88	-3237	231	244	0	-1732	-81	6.28	6.28	12.57	12.57	-11.39	314.1
50	88	-2966	92	211	0	-1586	15	6.28	6.28	12.57	12.57	-10.43	287.5
51	88	-3025	160	1	0	-2868	-33	6.28	6.28	12.57	12.57	-18.81	679.6

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	177	-4782	403	484	0	-3777	149	6.28	6.28	12.57	12.57	-24.84	838.8
41	177	-4072	187	402	0	-3252	108	6.28	6.28	12.57	12.57	-21.39	725.5
42	177	-4146	191	-570	0	-6398	106	6.28	6.28	12.57	12.57	-41.58	1703.3
43	177	-4454	534	445	0	-3387	177	6.28	6.28	12.57	12.57	-22.28	740.7
44	177	-3101	-160	282	0	-2513	46	6.28	6.28	12.57	12.57	-16.52	563.7
45	177	-3394	180	-1311	0	-7755	105	6.28	6.28	12.57	12.57	-50.04	2184.4
46	177	-2790	164	254	0	-2068	109	6.28	6.28	12.57	12.57	-13.61	447.4
47	177	-2469	159	217	0	-1772	110	6.28	6.28	12.57	12.57	-11.67	378.1
49	177	-2706	231	244	0	-1948	123	6.28	6.28	12.57	12.57	-12.82	415.9
50	177	-2435	92	211	0	-1772	97	6.28	6.28	12.57	12.57	-11.67	380.4
51	177	-2494	160	-107	0	-2821	109	6.28	6.28	12.57	12.57	-18.44	702.8

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	266	-4251	403	484	0	-4205	506	6.28	6.28	12.57	12.57	-27.56	1009.4
41	266	-3541	187	402	0	-3608	274	6.28	6.28	12.57	12.57	-23.64	873.7
42	266	-3615	191	-894	0	-5750	275	6.28	6.28	12.57	12.57	-37.35	1539.0
43	266	-3923	534	445	0	-3781	650	6.28	6.28	12.57	12.57	-24.79	900.4
44	266	-2570	-160	282	0	-2762	-96	6.28	6.28	12.57	12.57	-18.07	678.9
45	266	-2863	180	-1851	0	-6356	264	6.28	6.28	12.57	12.57	-41.04	1784.3
46	266	-2259	164	254	0	-2292	255	6.28	6.28	12.57	12.57	-15.02	554.5
47	266	-1938	159	217	0	-1964	250	6.28	6.28	12.57	12.57	-12.87	474.9
49	266	-2175	231	244	0	-2163	328	6.28	6.28	12.57	12.57	-14.18	520.1
50	266	-1904	92	211	0	-1959	179	6.28	6.28	12.57	12.57	-12.83	475.8
51	266	-1963	160	-215	0	-2678	251	6.28	6.28	12.57	12.57	-17.45	696.5

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	354	-3720	403	484	0	-4633	863	6.28	6.28	12.57	12.57	-30.23	1181.2
41	354	-3010	187	402	0	-3964	439	6.28	6.28	12.57	12.57	-25.84	1023.2
42	354	-3084	191	-1218	0	-4816	444	6.28	6.28	12.57	12.57	-31.29	1284.8

43	354	-3392	534	445	0	-4175	1122	6.28	6.28	12.57	12.57	-27.25	1061.6
44	354	-2039	-160	282	0	-3011	-237	6.28	6.28	12.57	12.57	-19.58	795.2
45	354	-2332	180	-2391	0	-4479	423	6.28	6.28	12.57	12.57	-28.99	1234.2
46	354	-1728	164	254	0	-2517	400	6.28	6.28	12.57	12.57	-16.38	663.0
47	354	-1407	159	217	0	-2156	391	6.28	6.28	12.57	12.57	-14.01	573.2
49	354	-1644	231	244	0	-2379	532	6.28	6.28	12.57	12.57	-15.48	625.9
50	354	-1373	92	211	0	-2146	260	6.28	6.28	12.57	12.57	-13.94	572.6
51	354	-1432	160	-323	0	-2440	392	6.28	6.28	12.57	12.57	-15.83	660.5

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 43 NI 39 NF 44 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 22D
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-5770	-556	771	0	-1285	148	6.28	6.28	12.57	12.57	-7.93	-102.0
41	0	-5805	-644	734	0	-1476	359	6.28	6.28	12.57	12.57	-9.22	-116.1
42	0	-5841	-661	53	0	-4637	374	6.28	6.28	12.57	12.57	-30.49	1031.9
43	0	-4957	-525	634	0	-789	55	6.28	6.28	12.57	12.57	-4.93	-66.1
44	0	-6094	-803	701	0	-1866	718	6.28	6.28	12.57	12.57	-11.90	188.4
45	0	-5076	-700	-563	0	-6375	433	6.28	6.28	12.57	12.57	-41.59	1628.5
46	0	-4543	-690	475	0	-886	437	6.28	6.28	12.57	12.57	-5.44	-71.3
47	0	-4228	-701	410	0	-738	456	6.28	6.28	12.57	12.57	-4.56	-60.5
49	0	-4216	-672	423	0	-674	386	6.28	6.28	12.57	12.57	-4.21	-56.4
50	0	-4443	-727	436	0	-890	518	6.28	6.28	12.57	12.57	-5.47	-71.4
51	0	-4240	-707	183	0	-1792	461	6.28	6.28	12.57	12.57	-11.70	269.2

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	53	-5453	-556	771	0	-1693	-146	6.28	6.28	12.57	12.57	-10.81	174.6
41	53	-5488	-644	734	0	-1864	19	6.28	6.28	12.57	12.57	-12.00	218.8
42	53	-5524	-661	-141	0	-4614	25	6.28	6.28	12.57	12.57	-30.32	1046.8
43	53	-4640	-525	634	0	-1124	-222	6.28	6.28	12.57	12.57	-6.99	-88.7
44	53	-5777	-803	701	0	-2236	293	6.28	6.28	12.57	12.57	-14.54	307.3
45	53	-4759	-700	-885	0	-5992	62	6.28	6.28	12.57	12.57	-39.09	1531.6
46	53	-4226	-690	475	0	-1137	72	6.28	6.28	12.57	12.57	-7.15	91.6
47	53	-3911	-701	410	0	-955	85	6.28	6.28	12.57	12.57	-5.94	-75.3
49	53	-3899	-672	423	0	-898	31	6.28	6.28	12.57	12.57	-5.56	-71.1
50	53	-4126	-727	436	0	-1120	134	6.28	6.28	12.57	12.57	-7.05	91.9
51	53	-3923	-707	119	0	-1872	88	6.28	6.28	12.57	12.57	-12.28	312.3

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	106	-5136	-556	771	0	-2100	-440	6.28	6.28	12.57	12.57	-13.70	305.6
41	106	-5170	-644	734	0	-2252	-322	6.28	6.28	12.57	12.57	-14.73	348.0
42	106	-5206	-661	-334	0	-4488	-325	6.28	6.28	12.57	12.57	-29.48	1030.0
43	106	-4322	-525	634	0	-1459	-500	6.28	6.28	12.57	12.57	-9.39	169.8
44	106	-5460	-803	701	0	-2607	-132	6.28	6.28	12.57	12.57	-17.11	435.3
45	106	-4442	-700	-1208	0	-5439	-308	6.28	6.28	12.57	12.57	-35.50	1381.3
46	106	-3908	-690	475	0	-1388	-293	6.28	6.28	12.57	12.57	-8.97	172.5
47	106	-3594	-701	410	0	-1172	-285	6.28	6.28	12.57	12.57	-7.52	130.1
49	106	-3582	-672	423	0	-1121	-325	6.28	6.28	12.57	12.57	-7.16	117.1
50	106	-3808	-727	436	0	-1351	-251	6.28	6.28	12.57	12.57	-8.73	167.7
51	106	-3606	-707	54	0	-1917	-286	6.28	6.28	12.57	12.57	-12.61	346.4

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	159	-4818	-556	771	0	-2508	-733	6.28	6.28	12.57	12.57	-16.49	446.6
41	159	-4853	-644	734	0	-2641	-662	6.28	6.28	12.57	12.57	-17.37	484.4
42	159	-4889	-661	-528	0	-4260	-674	6.28	6.28	12.57	12.57	-27.98	981.4
43	159	-4005	-525	634	0	-1794	-777	6.28	6.28	12.57	12.57	-11.75	284.1
44	159	-5142	-803	701	0	-2977	-556	6.28	6.28	12.57	12.57	-19.60	567.9
45	159	-4124	-700	-1530	0	-4715	-679	6.28	6.28	12.57	12.57	-30.82	1177.6
46	159	-3591	-690	475	0	-1639	-657	6.28	6.28	12.57	12.57	-10.74	263.7
47	159	-3276	-701	410	0	-1389	-656	6.28	6.28	12.57	12.57	-9.07	209.3
49	159	-3264	-672	423	0	-1345	-680	6.28	6.28	12.57	12.57	-8.77	197.0
50	159	-3491	-727	436	0	-1581	-635	6.28	6.28	12.57	12.57	-10.36	252.9
51	159	-3288	-707	-10	0	-1929	-659	6.28	6.28	12.57	12.57	-12.70	370.7

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	211	-4501	-556	771	0	-2916	-1027	6.28	6.28	12.57	12.57	-19.20	592.0
41	211	-4536	-644	734	0	-3029	-1003	6.28	6.28	12.57	12.57	-19.95	624.4
42	211	-4572	-661	-721	0	-3930	-1024	6.28	6.28	12.57	12.57	-25.82	901.0
43	211	-3688	-525	634	0	-2129	-1055	6.28	6.28	12.57	12.57	-14.02	405.3
44	211	-4825	-803	701	0	-3348	-981	6.28	6.28	12.57	12.57	-22.04	703.1
45	211	-3807	-700	-1853	0	-3820	-1049	6.28	6.28	12.57	12.57	-25.03	920.9
46	211	-3274	-690	475	0	-1890	-1022	6.28	6.28	12.57	12.57	-12.44	359.8
47	211	-2959	-701	410	0	-1606	-1027	6.28	6.28	12.57	12.57	-10.57	294.1
49	211	-2947	-672	423	0	-1568	-1035	6.28	6.28	12.57	12.57	-10.31	283.4
50	211	-3174	-727	436	0	-1812	-1020	6.28	6.28	12.57	12.57	-11.93	342.7
51	211	-2971	-707	-75	0	-1906	-1033	6.28	6.28	12.57	12.57	-12.55	385.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 44 NI 295 NF 261 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 10E
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-4802	-373	-593	0	-1671	1050	6.28	6.28	12.57	12.57	-10.78	202.4
41	0	-4033	-386	-520	0	-1466	1088	6.28	6.28	12.57	12.57	-9.49	187.5
42	0	-4001	-376	-380	0	-492	1058	6.28	6.28	12.57	12.57	-8.61	130.9
43	0	-4883	-292	-530	0	-1492	821	6.28	6.28	12.57	12.57	-9.51	150.1
44	0	-3093	-405	-420	0	-1183	1139	6.28	6.28	12.57	12.57	-9.19	179.8
45	0	-3550	-297	-174	0	473	835	6.28	6.28	12.57	12.57	-6.81	91.7
46	0	-3343	-270	-341	0	-960	761	6.28	6.28	12.57	12.57	-6.21	87.1

47	0	-3171	-242	-296	0	-834	680	6.28	6.28	12.57	12.57	-5.55	66.7
49	0	-3427	-237	-320	0	-902	667	6.28	6.28	12.57	12.57	-5.66	-70.8
50	0	-3069	-260	-298	0	-840	731	6.28	6.28	12.57	12.57	-5.96	81.4
51	0	-3160	-238	-249	0	-509	670	6.28	6.28	12.57	12.57	-5.47	64.9

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	58	-4455	-373	-593	0	-1328	834	6.28	6.28	12.57	12.57	-8.44	128.4
41	58	-3686	-386	-520	0	-1165	864	6.28	6.28	12.57	12.57	-7.45	123.5
42	58	-3654	-376	-278	0	-302	841	6.28	6.28	12.57	12.57	-6.86	90.0
43	58	-4536	-292	-530	0	-1186	652	6.28	6.28	12.57	12.57	-7.43	-93.1
44	58	-2746	-405	-420	0	-940	905	6.28	6.28	12.57	12.57	-7.33	133.3
45	58	-3203	-297	-4	0	523	663	6.28	6.28	12.57	12.57	-5.42	62.3
46	58	-2996	-270	-341	0	-763	605	6.28	6.28	12.57	12.57	-4.94	-60.0
47	58	-2824	-242	-296	0	-662	540	6.28	6.28	12.57	12.57	-4.41	-52.4
49	58	-3080	-237	-320	0	-717	530	6.28	6.28	12.57	12.57	-4.44	-56.7
50	58	-2722	-260	-298	0	-668	581	6.28	6.28	12.57	12.57	-4.74	56.7
51	58	-2813	-238	-215	0	-375	532	6.28	6.28	12.57	12.57	-4.35	-49.7

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	116	-4108	-373	-593	0	-985	618	6.28	6.28	12.57	12.57	-6.12	-77.8
41	116	-3339	-386	-520	0	-864	641	6.28	6.28	12.57	12.57	-5.41	-67.9
42	116	-3307	-376	-190	0	-168	623	6.28	6.28	12.57	12.57	-5.10	-58.3
43	116	-4189	-292	-530	0	-879	483	6.28	6.28	12.57	12.57	-5.41	-70.2
44	116	-2399	-405	-420	0	-697	671	6.28	6.28	12.57	12.57	-5.46	87.3
45	116	-2856	-297	143	0	482	492	6.28	6.28	12.57	12.57	-4.03	-46.9
46	116	-2649	-270	-341	0	-566	448	6.28	6.28	12.57	12.57	-3.67	-45.1
47	116	-2477	-242	-296	0	-491	400	6.28	6.28	12.57	12.57	-3.28	-39.4
49	116	-2733	-237	-320	0	-532	393	6.28	6.28	12.57	12.57	-3.26	-42.8
50	116	-2375	-260	-298	0	-495	430	6.28	6.28	12.57	12.57	-3.52	-40.6
51	116	-2466	-238	-186	0	-259	395	6.28	6.28	12.57	12.57	-3.24	-38.2

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	173	-3761	-373	-593	0	-642	403	6.28	6.28	12.57	12.57	-3.97	-52.8
41	173	-2992	-386	-520	0	-563	417	6.28	6.28	12.57	12.57	-3.46	-45.5
42	173	-2960	-376	-117	0	-80	406	6.28	6.28	12.57	12.57	-3.36	-40.8
43	173	-3842	-292	-530	0	-573	315	6.28	6.28	12.57	12.57	-3.63	-48.9
44	173	-2052	-405	-420	0	-454	437	6.28	6.28	12.57	12.57	-3.57	42.6
45	173	-2509	-297	264	0	363	320	6.28	6.28	12.57	12.57	-2.67	-32.8
46	173	-2302	-270	-341	0	-369	292	6.28	6.28	12.57	12.57	-2.43	-30.8
47	173	-2130	-242	-296	0	-320	261	6.28	6.28	12.57	12.57	-2.18	-27.3
49	173	-2386	-237	-320	0	-346	256	6.28	6.28	12.57	12.57	-2.21	-29.8
50	173	-2028	-260	-298	0	-323	280	6.28	6.28	12.57	12.57	-2.32	-28.1
51	173	-2119	-238	-161	0	-159	257	6.28	6.28	12.57	12.57	-2.16	-26.7

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	231	-3414	-373	-593	0	-298	187	6.28	6.28	12.57	12.57	-2.39	-33.1
41	231	-2645	-386	-520	0	-262	194	6.28	6.28	12.57	12.57	-1.96	-27.0
42	231	-2613	-376	-59	0	-30	188	6.28	6.28	12.57	12.57	-1.87	-24.6
43	231	-3495	-292	-530	0	-266	146	6.28	6.28	12.57	12.57	-2.30	-32.2
44	231	-1705	-405	-420	0	-211	203	6.28	6.28	12.57	12.57	-1.71	-21.3
45	231	-2162	-297	362	0	181	149	6.28	6.28	12.57	12.57	-1.51	-20.6
46	231	-1955	-270	-341	0	-171	136	6.28	6.28	12.57	12.57	-1.37	-19.0
47	231	-1783	-242	-296	0	-149	121	6.28	6.28	12.57	12.57	-1.24	-17.0
49	231	-2039	-237	-320	0	-161	119	6.28	6.28	12.57	12.57	-1.36	-19.0
50	231	-1681	-260	-298	0	-150	130	6.28	6.28	12.57	12.57	-1.25	-16.5
51	231	-1772	-238	-142	0	-72	119	6.28	6.28	12.57	12.57	-1.23	-16.2

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 45 NI 297 NF 260 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 15D
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	--												
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-8854	-70	24	0	96	282	6.28	6.28	12.57	12.57	-4.58	-63.5
41	0	-8480	-23	32	0	130	93	6.28	6.28	12.57	12.57	-3.74	-55.0
42	0	-8325	-22	17	0	1293	87	6.28	6.28	12.57	12.57	-8.12	-109.1
43	0	-7800	-95	14	0	55	382	6.28	6.28	12.57	12.57	-4.70	-63.4
44	0	-8089	57	47	0	191	-229	6.28	6.28	12.57	12.57	-4.04	-56.4
45	0	-6918	-14	3	0	2050	58	6.28	6.28	12.57	12.57	-13.03	196.3
46	0	-6396	-13	25	0	101	53	6.28	6.28	12.57	12.57	-2.83	-41.6
47	0	-5875	-11	23	0	94	43	6.28	6.28	12.57	12.57	-2.61	-38.3
49	0	-6000	-26	21	0	83	106	6.28	6.28	12.57	12.57	-2.68	-38.5
50	0	-6058	4	27	0	110	-16	6.28	6.28	12.57	12.57	-2.73	-40.0
51	0	-5823	-10	18	0	482	41	6.28	6.28	12.57	12.57	-3.97	-55.3

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	88	-8323	-70	24	0	75	220	6.28	6.28	12.57	12.57	-4.08	-57.2
41	88	-7949	-23	32	0	102	73	6.28	6.28	12.57	12.57	-3.43	-50.6
42	88	-7794	-22	174	0	1207	68	6.28	6.28	12.57	12.57	-7.59	-101.9
43	88	-7269	-95	14	0	43	298	6.28	6.28	12.57	12.57	-4.09	-55.8
44	88	-7558	57	47	0	149	-179	6.28	6.28	12.57	12.57	-3.60	-50.8
45	88	-6387	-14	264	0	1929	45	6.28	6.28	12.57	12.57	-12.28	190.6
46	88	-5865	-13	25	0	79	42	6.28	6.28	12.57	12.57	-2.55	-37.5
47	88	-5344	-11	23	0	73	34	6.28	6.28	12.57	12.57	-2.33	-34.3
49	88	-5469	-26	21	0	64	83	6.28	6.28	12.57	12.57	-2.38	-34.6
50	88	-5527	4	27	0	86	-13	6.28	6.28	12.57	12.57	-2.44	-35.9
51	88	-5292	-10	71	0	442	32	6.28	6.28	12.57	12.57	-3.63	-50.4

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	177	-7792	-70	24	0	54	158	6.28	6.28	12.57	12.57	-3.59	-50.9
41	177	-7418	-23	32	0	73	53	6.28	6.28	12.57	12.57	-3.13	-46.2
42	177	-7263	-22	308	0	992	49	6.28	6.28	12.57	12.57	-6.44	-87.4
43	177	-6738	-95	14	0	31	215	6.28	6.28	12.57	12.57	-3.49	-48.3
44	177	-7027	57	47	0	107	-128	6.28	6.28	12.57	12.57	-3.16	-45.5
45	177	-5856	-14	488	0	1594	33	6.28	6.28	12.57	12.57	-10.04	131.3
46	177	-5334	-13	25	0	57	30	6.28	6.28	12.57	12.57	-2.26	-33.4
47	177	-4813	-11	23	0	53	24	6.28	6.28	12.57	12.57	-2.05	-30.2

49	177	-4938	-26	21	0	46	59	6.28	6.28	12.57	12.57	-2.07	-30.7
50	177	-4996	4	27	0	62	-9	6.28	6.28	12.57	12.57	-2.15	-31.7
51	177	-4761	-10	115	0	359	23	6.28	6.28	12.57	12.57	-3.12	-43.7

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	266	-7261	-70	24	0	32	97	6.28	6.28	12.57	12.57	-3.09	-44.6
41	266	-6887	-23	32	0	44	32	6.28	6.28	12.57	12.57	-2.82	-41.9
42	266	-6732	-22	420	0	668	30	6.28	6.28	12.57	12.57	-4.99	-68.9
43	266	-6207	-95	14	0	18	131	6.28	6.28	12.57	12.57	-2.88	-40.8
44	266	-6496	57	47	0	65	-78	6.28	6.28	12.57	12.57	-2.74	-40.6
45	266	-5325	-14	674	0	1077	20	6.28	6.28	12.57	12.57	-6.62	-86.3
46	266	-4803	-13	25	0	34	18	6.28	6.28	12.57	12.57	-1.98	-29.4
47	266	-4282	-11	23	0	32	15	6.28	6.28	12.57	12.57	-1.77	-26.2
49	266	-4407	-26	21	0	28	36	6.28	6.28	12.57	12.57	-1.80	-26.8
50	266	-4465	4	27	0	37	-6	6.28	6.28	12.57	12.57	-1.86	-27.5
51	266	-4230	-10	153	0	240	14	6.28	6.28	12.57	12.57	-2.49	-35.2

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	354	-6730	-70	24	0	11	35	6.28	6.28	12.57	12.57	-2.64	-39.5
41	354	-6356	-23	32	0	15	12	6.28	6.28	12.57	12.57	-2.51	-37.5
42	354	-6201	-22	509	0	255	11	6.28	6.28	12.57	12.57	-3.31	-47.3
43	354	-5676	-95	14	0	6	47	6.28	6.28	12.57	12.57	-2.28	-33.3
44	354	-5965	57	47	0	23	-28	6.28	6.28	12.57	12.57	-2.39	-35.6
45	354	-4794	-14	823	0	412	7	6.28	6.28	12.57	12.57	-3.33	-46.2
46	354	-4272	-13	25	0	12	7	6.28	6.28	12.57	12.57	-1.69	-25.3
47	354	-3751	-11	23	0	11	5	6.28	6.28	12.57	12.57	-1.49	-22.2
49	354	-3876	-26	21	0	10	13	6.28	6.28	12.57	12.57	-1.53	-22.9
50	354	-3934	4	27	0	13	-2	6.28	6.28	12.57	12.57	-1.57	-23.4
51	354	-3699	-10	182	0	91	5	6.28	6.28	12.57	12.57	-1.75	-25.5

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 46 NI 271 NF 259 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 20D
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-5474	226	-670	0	-1755	-592	6.28	6.28	12.57	12.57	-11.24	190.0
41	0	-5665	220	-599	0	-1569	-576	6.28	6.28	12.57	12.57	-9.90	133.5
42	0	-5597	217	-414	0	-587	-568	6.28	6.28	12.57	12.57	-4.94	-62.8
43	0	-4571	189	-587	0	-1536	-494	6.28	6.28	12.57	12.57	-9.88	177.7
44	0	-6216	214	-504	0	-1319	-560	6.28	6.28	12.57	12.57	-8.12	-105.1
45	0	-4777	174	-159	0	412	-455	6.28	6.28	12.57	12.57	-4.03	-51.6
46	0	-4425	154	-389	0	-1019	-404	6.28	6.28	12.57	12.57	-6.31	-80.7
47	0	-4115	138	-337	0	-881	-360	6.28	6.28	12.57	12.57	-5.43	-70.2
49	0	-4051	140	-360	0	-943	-366	6.28	6.28	12.57	12.57	-5.84	-74.6
50	0	-4380	145	-344	0	-900	-379	6.28	6.28	12.57	12.57	-5.53	-72.0
51	0	-4092	137	-275	0	-554	-358	6.28	6.28	12.57	12.57	-3.61	-49.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	53	-5157	226	-670	0	-1400	-472	6.28	6.28	12.57	12.57	-8.82	114.9
41	53	-5348	220	-599	0	-1252	-460	6.28	6.28	12.57	12.57	-7.76	-99.0
42	53	-5280	217	-320	0	-393	-453	6.28	6.28	12.57	12.57	-4.16	-53.9
43	53	-4254	189	-587	0	-1226	-395	6.28	6.28	12.57	12.57	-7.77	111.9
44	53	-5899	214	-504	0	-1053	-447	6.28	6.28	12.57	12.57	-6.49	-85.9
45	53	-4460	174	-3	0	453	-363	6.28	6.28	12.57	12.57	-3.41	-46.1
46	53	-4108	154	-389	0	-813	-322	6.28	6.28	12.57	12.57	-4.99	-65.3
47	53	-3798	138	-337	0	-703	-287	6.28	6.28	12.57	12.57	-4.32	-57.0
49	53	-3734	140	-360	0	-753	-292	6.28	6.28	12.57	12.57	-4.63	-60.3
50	53	-4063	145	-344	0	-718	-302	6.28	6.28	12.57	12.57	-4.43	-58.7
51	53	-3775	137	-244	0	-417	-285	6.28	6.28	12.57	12.57	-2.95	-40.5

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	106	-4840	226	-670	0	-1046	-353	6.28	6.28	12.57	12.57	-6.44	-83.2
41	106	-5030	220	-599	0	-935	-343	6.28	6.28	12.57	12.57	-5.75	-75.8
42	106	-4962	217	-240	0	-246	-338	6.28	6.28	12.57	12.57	-3.46	-45.6
43	106	-3936	189	-587	0	-915	-295	6.28	6.28	12.57	12.57	-5.67	-72.4
44	106	-5582	214	-504	0	-786	-333	6.28	6.28	12.57	12.57	-5.06	-68.5
45	106	-4142	174	131	0	418	-271	6.28	6.28	12.57	12.57	-3.10	-42.7
46	106	-3790	154	-389	0	-607	-240	6.28	6.28	12.57	12.57	-3.79	-50.8
47	106	-3480	138	-337	0	-525	-215	6.28	6.28	12.57	12.57	-3.32	-44.7
49	106	-3416	140	-360	0	-562	-218	6.28	6.28	12.57	12.57	-3.50	-46.7
50	106	-3746	145	-344	0	-536	-226	6.28	6.28	12.57	12.57	-3.44	-46.5
51	106	-3458	137	-217	0	-296	-213	6.28	6.28	12.57	12.57	-2.39	-33.3

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	159	-4522	226	-670	0	-691	-233	6.28	6.28	12.57	12.57	-4.36	-58.6
41	159	-4713	220	-599	0	-618	-227	6.28	6.28	12.57	12.57	-4.07	-55.4
42	159	-4645	217	-173	0	-137	-224	6.28	6.28	12.57	12.57	-2.78	-37.5
43	159	-3619	189	-587	0	-605	-195	6.28	6.28	12.57	12.57	-3.75	-50.1
44	159	-5264	214	-504	0	-520	-220	6.28	6.28	12.57	12.57	-3.89	-53.8
45	159	-3825	174	242	0	318	-179	6.28	6.28	12.57	12.57	-2.62	-36.4
46	159	-3473	154	-389	0	-401	-159	6.28	6.28	12.57	12.57	-2.78	-38.1
47	159	-3163	138	-337	0	-347	-142	6.28	6.28	12.57	12.57	-2.47	-33.9
49	159	-3099	140	-360	0	-372	-144	6.28	6.28	12.57	12.57	-2.53	-34.7
50	159	-3428	145	-344	0	-355	-149	6.28	6.28	12.57	12.57	-2.59	-35.7
51	159	-3140	137	-195	0	-187	-141	6.28	6.28	12.57	12.57	-1.88	-26.6

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	211	-4205	226	-670	0	-337	-114	6.28	6.28	12.57	12.57	-2.83	-39.4
41	211	-4396	220	-599	0	-301	-110	6.28	6.28	12.57	12.57	-2.78	-39.0
42	211	-4328	217	-120	0	-61	-109	6.28	6.28	12.57	12.57	-2.10	-29.4
43	211	-3302	189	-587	0	-295	-95	6.28	6.28	12.57	12.57	-2.33	-32.3
44	211	-4947	214	-504	0	-253	-107	6.28	6.28	12.57	12.57	-2.82	-40.0
45	211	-3508	174	331	0	166	-87	6.28	6.28	12.57	12.57	-1.95	-27.7
46	211	-3156	154	-389	0	-196	-77	6.28	6.28	12.57	12.57	-1.92	-27.0
47	211	-2846	138	-337	0	-169	-69	6.28	6.28	12.57	12.57	-1.71	-24.1
49	211	-2782	140	-360	0	-181	-70	6.28	6.28	12.57	12.57	-1.72	-24.2

50	211	-3111	145	-344	0	-173	-72	6.28	6.28	12.57	12.57	-1.82	-25.8
51	211	-2823	137	-177	0	-89	-68	6.28	6.28	12.57	12.57	-1.41	-20.3

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 47 NI 129 NF 124 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 9B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-9974	110	-239	0	-437	-492	6.28	6.28	12.57	12.57	-6.02	-81.2
41	0	-9913	-32	-126	0	-226	11	6.28	6.28	12.57	12.57	-4.64	-67.5
42	0	-9858	-33	-218	0	-426	15	6.28	6.28	12.57	12.57	-5.33	-76.2
43	0	-9687	212	-280	0	-519	-852	6.28	6.28	12.57	12.57	-7.76	-100.2
44	0	-9545	-268	45	0	101	853	6.28	6.28	12.57	12.57	-7.72	-99.6
45	0	-9494	-26	-245	0	-500	-7	6.28	6.28	12.57	12.57	-5.46	-77.4
46	0	-9388	-18	-72	0	-130	-29	6.28	6.28	12.57	12.57	-4.09	-60.2
47	0	-9257	-15	-58	0	-106	-38	6.28	6.28	12.57	12.57	-3.96	-58.4
49	0	-9278	32	-96	0	-176	-206	6.28	6.28	12.57	12.57	-4.36	-61.7
50	0	-9249	-64	-31	0	-53	135	6.28	6.28	12.57	12.57	-4.00	-57.5
51	0	-9239	-15	-89	0	-173	-37	6.28	6.28	12.57	12.57	-4.19	-61.3

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	97	-9389	110	-239	0	-205	-386	6.28	6.28	12.57	12.57	-5.29	-72.2
41	97	-9328	-32	-126	0	-102	-20	6.28	6.28	12.57	12.57	-3.97	-58.6
42	97	-9273	-33	-218	0	-214	-18	6.28	6.28	12.57	12.57	-4.35	-63.3
43	97	-9102	212	-280	0	-246	-645	6.28	6.28	12.57	12.57	-6.47	-85.0
44	97	-8960	-268	45	0	57	591	6.28	6.28	12.57	12.57	-6.15	-81.3
45	97	-8909	-26	-245	0	-261	-32	6.28	6.28	12.57	12.57	-4.38	-63.3
46	97	-8803	-18	-72	0	-60	-46	6.28	6.28	12.57	12.57	-3.61	-53.7
47	97	-8672	-15	-58	0	-49	-53	6.28	6.28	12.57	12.57	-3.53	-52.4
49	97	-8693	32	-96	0	-83	-174	6.28	6.28	12.57	12.57	-3.99	-56.7
50	97	-8664	-64	-31	0	-22	73	6.28	6.28	12.57	12.57	-3.48	-51.2
51	97	-8654	-15	-89	0	-86	-52	6.28	6.28	12.57	12.57	-3.65	-54.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	195	-8804	110	-239	0	28	-279	6.28	6.28	12.57	12.57	-4.55	-63.1
41	195	-8743	-32	-126	0	21	-51	6.28	6.28	12.57	12.57	-3.45	-51.6
42	195	-8688	-33	-218	0	-1	-50	6.28	6.28	12.57	12.57	-3.38	-50.4
43	195	-8517	212	-280	0	26	-439	6.28	6.28	12.57	12.57	-5.23	-70.4
44	195	-8375	-268	45	0	14	330	6.28	6.28	12.57	12.57	-4.64	-63.6
45	195	-8324	-26	-245	0	-22	-57	6.28	6.28	12.57	12.57	-3.29	-49.2
46	195	-8218	-18	-72	0	11	-64	6.28	6.28	12.57	12.57	-3.27	-48.1
47	195	-8087	-15	-58	0	8	-67	6.28	6.28	12.57	12.57	-3.24	-47.4
49	195	-8108	32	-96	0	10	-143	6.28	6.28	12.57	12.57	-3.63	-51.7
50	195	-8079	-64	-31	0	8	11	6.28	6.28	12.57	12.57	-3.15	-47.2
51	195	-8069	-15	-89	0	1	-67	6.28	6.28	12.57	12.57	-3.23	-47.3

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	292	-8219	110	-239	0	261	-172	6.28	6.28	12.57	12.57	-4.11	-59.3
41	292	-8158	-32	-126	0	144	-82	6.28	6.28	12.57	12.57	-3.67	-53.7
42	292	-8103	-33	-218	0	212	-83	6.28	6.28	12.57	12.57	-3.89	-56.4
43	292	-7932	212	-280	0	299	-232	6.28	6.28	12.57	12.57	-4.14	-59.4
44	292	-7790	-268	45	0	-30	68	6.28	6.28	12.57	12.57	-3.14	-46.5
45	292	-7739	-26	-245	0	217	-83	6.28	6.28	12.57	12.57	-3.77	-54.6
46	292	-7633	-18	-72	0	81	-81	6.28	6.28	12.57	12.57	-3.24	-47.8
47	292	-7502	-15	-58	0	65	-81	6.28	6.28	12.57	12.57	-3.13	-46.4
49	292	-7523	32	-96	0	104	-111	6.28	6.28	12.57	12.57	-3.28	-48.2
50	292	-7494	-64	-31	0	38	-51	6.28	6.28	12.57	12.57	-3.03	-45.1
51	292	-7484	-15	-89	0	87	-81	6.28	6.28	12.57	12.57	-3.20	-47.3

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	390	-7634	110	-239	0	494	-66	6.28	6.28	12.57	12.57	-4.72	-66.3
41	390	-7573	-32	-126	0	268	-113	6.28	6.28	12.57	12.57	-3.88	-55.9
42	390	-7518	-33	-218	0	424	-115	6.28	6.28	12.57	12.57	-4.42	-62.6
43	390	-7347	212	-280	0	572	-25	6.28	6.28	12.57	12.57	-4.89	-68.2
44	390	-7205	-268	45	0	-73	-194	6.28	6.28	12.57	12.57	-3.55	-49.7
45	390	-7154	-26	-245	0	456	-108	6.28	6.28	12.57	12.57	-4.40	-61.9
46	390	-7048	-18	-72	0	151	-99	6.28	6.28	12.57	12.57	-3.26	-47.6
47	390	-6917	-15	-58	0	122	-96	6.28	6.28	12.57	12.57	-3.11	-45.5
49	390	-6938	32	-96	0	197	-80	6.28	6.28	12.57	12.57	-3.39	-49.0
50	390	-6909	-64	-31	0	68	-113	6.28	6.28	12.57	12.57	-3.05	-43.6
51	390	-6899	-15	-89	0	174	-96	6.28	6.28	12.57	12.57	-3.29	-47.8

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 48 NI 128 NF 125 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 14B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-16060	163	-481	0	-797	-421	6.28	6.28	12.57	12.57	-9.06	-128.7
41	0	-16020	4	-434	0	-728	10	6.28	6.28	12.57	12.57	-8.80	-125.4
42	0	-15970	5	-570	0	-962	7	6.28	6.28	12.57	12.57	-9.61	-135.6
43	0	-15480	274	-434	0	-723	-721	6.28	6.28	12.57	12.57	-9.14	-123.7
44	0	-15420	-262	-374	0	-636	730	6.28	6.28	12.57	12.57	-9.16	-123.8
45	0	-15320	11	-582	0	-998	-8	6.28	6.28	12.57	12.57	-9.49	-133.4
46	0	-15030	12	-309	0	-537	-11	6.28	6.28	12.57	12.57	-7.73	-111.1
47	0	-14790	14	-277	0	-490	-16	6.28	6.28	12.57	12.57	-7.47	-107.6
49	0	-14800	67	-293	0	-512	-160	6.28	6.28	12.57	12.57	-7.55	-108.7
50	0	-14790	-40	-281	0	-495	130	6.28	6.28	12.57	12.57	-7.49	-107.9
51	0	-14770	15	-322	0	-567	-17	6.28	6.28	12.57	12.57	-7.74	-111.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	97	-15475	163	-481	0	-328	-262	6.28	6.28	12.57	12.57	-7.15	-104.3
41	97	-15435	4	-434	0	-305	14	6.28	6.28	12.57	12.57	-7.05	-103.1
42	97	-15385	5	-570	0	-406	12	6.28	6.28	12.57	12.57	-7.40	-107.3
43	97	-14895	274	-434	0	-300	-454	6.28	6.28	12.57	12.57	-7.60	-105.7
44	97	-14835	-262	-374	0	-272	474	6.28	6.28	12.57	12.57	-7.68	-106.5
45	97	-14735	11	-582	0	-431	3	6.28	6.28	12.57	12.57	-7.23	-104.7
46	97	-14445	12	-309	0	-236	1	6.28	6.28	12.57	12.57	-6.43	-94.3
47	97	-14205	14	-277	0	-219	-2	6.28	6.28	12.57	12.57	-6.27	-92.1
49	97	-14215	67	-293	0	-227	-94	6.28	6.28	12.57	12.57	-6.30	-92.5
50	97	-14205	-40	-281	0	-221	91	6.28	6.28	12.57	12.57	-6.28	-92.2
51	97	-14185	15	-322	0	-253	-3	6.28	6.28	12.57	12.57	-6.39	-93.5

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	195	-14890	163	-481	0	141	-103	6.28	6.28	12.57	12.57	-6.26	-92.6
41	195	-14850	4	-434	0	118	18	6.28	6.28	12.57	12.57	-6.16	-91.3
42	195	-14800	5	-570	0	149	17	6.28	6.28	12.57	12.57	-6.25	-92.4
43	195	-14310	274	-434	0	123	-186	6.28	6.28	12.57	12.57	-6.07	-88.4
44	195	-14250	-262	-374	0	93	219	6.28	6.28	12.57	12.57	-6.21	-89.1
45	195	-14150	11	-582	0	136	14	6.28	6.28	12.57	12.57	-5.96	-88.1
46	195	-13860	12	-309	0	65	13	6.28	6.28	12.57	12.57	-5.59	-83.2
47	195	-13620	14	-277	0	51	12	6.28	6.28	12.57	12.57	-5.44	-81.2
49	195	-13630	67	-293	0	59	-28	6.28	6.28	12.57	12.57	-5.48	-81.6
50	195	-13620	-40	-281	0	53	52	6.28	6.28	12.57	12.57	-5.45	-81.3
51	195	-13600	15	-322	0	62	11	6.28	6.28	12.57	12.57	-5.47	-81.6

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	292	-14305	163	-481	0	610	57	6.28	6.28	12.57	12.57	-7.71	-110.2
41	292	-14265	4	-434	0	542	22	6.28	6.28	12.57	12.57	-7.45	-106.9
42	292	-14215	5	-570	0	705	23	6.28	6.28	12.57	12.57	-8.01	-113.9
43	292	-13725	274	-434	0	545	82	6.28	6.28	12.57	12.57	-7.26	-103.9
44	292	-13665	-262	-374	0	458	-37	6.28	6.28	12.57	12.57	-6.92	-99.7
45	292	-13565	11	-582	0	704	25	6.28	6.28	12.57	12.57	-7.76	-110.1
46	292	-13275	12	-309	0	365	25	6.28	6.28	12.57	12.57	-6.44	-93.3
47	292	-13035	14	-277	0	321	25	6.28	6.28	12.57	12.57	-6.19	-89.9
49	292	-13045	67	-293	0	344	37	6.28	6.28	12.57	12.57	-6.27	-91.0
50	292	-13035	-40	-281	0	327	13	6.28	6.28	12.57	12.57	-6.21	-90.2
51	292	-13015	15	-322	0	376	26	6.28	6.28	12.57	12.57	-6.37	-92.2

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	390	-13720	163	-481	0	1079	216	6.28	6.28	12.57	12.57	-9.16	-127.8
41	390	-13680	4	-434	0	965	26	6.28	6.28	12.57	12.57	-8.74	-122.5
42	390	-13630	5	-570	0	1260	28	6.28	6.28	12.57	12.57	-9.78	-135.4
43	390	-13140	274	-434	0	968	349	6.28	6.28	12.57	12.57	-8.54	-119.5
44	390	-13080	-262	-374	0	822	-292	6.28	6.28	12.57	12.57	-8.00	-112.6
45	390	-12980	11	-582	0	1271	36	6.28	6.28	12.57	12.57	-9.57	-132.1
46	390	-12690	12	-309	0	666	37	6.28	6.28	12.57	12.57	-7.29	-103.4
47	390	-12450	14	-277	0	592	39	6.28	6.28	12.57	12.57	-6.93	-98.6
49	390	-12460	67	-293	0	630	103	6.28	6.28	12.57	12.57	-7.07	-100.4
50	390	-12450	-40	-281	0	601	-26	6.28	6.28	12.57	12.57	-6.96	-99.0
51	390	-12430	15	-322	0	690	40	6.28	6.28	12.57	12.57	-7.27	-102.9

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 49 NI 127 NF 126 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 19B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-15810	153	-188	0	-300	-460	6.28	6.28	12.57	12.57	-7.96	-111.0
41	0	-15810	9	-217	0	-348	-47	6.28	6.28	12.57	12.57	-7.35	-107.2
42	0	-15740	10	-274	0	-457	-50	6.28	6.28	12.57	12.57	-7.72	-111.7
43	0	-15210	249	-132	0	-216	-735	6.28	6.28	12.57	12.57	-9.11	-123.0
44	0	-15300	-232	-276	0	-442	642	6.28	6.28	12.57	12.57	-8.68	-118.3
45	0	-15090	10	-275	0	-478	-52	6.28	6.28	12.57	12.57	-7.54	-108.8
46	0	-14860	8	-157	0	-264	-47	6.28	6.28	12.57	12.57	-6.69	-97.9
47	0	-14620	8	-142	0	-243	-47	6.28	6.28	12.57	12.57	-6.52	-95.6
49	0	-14620	56	-132	0	-228	-184	6.28	6.28	12.57	12.57	-6.46	-94.9
50	0	-14640	-40	-161	0	-272	91	6.28	6.28	12.57	12.57	-6.63	-97.0
51	0	-14600	9	-161	0	-280	-48	6.28	6.28	12.57	12.57	-6.64	-97.1

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	97	-15225	153	-188	0	-117	-311	6.28	6.28	12.57	12.57	-7.02	-99.5
41	97	-15225	9	-217	0	-137	-39	6.28	6.28	12.57	12.57	-6.37	-94.4
42	97	-15155	10	-274	0	-190	-40	6.28	6.28	12.57	12.57	-6.54	-96.3
43	97	-14625	249	-132	0	-87	-492	6.28	6.28	12.57	12.57	-7.70	-106.4
44	97	-14715	-232	-276	0	-173	416	6.28	6.28	12.57	12.57	-7.35	-102.6
45	97	-14505	10	-275	0	-209	-42	6.28	6.28	12.57	12.57	-6.35	-93.4
46	97	-14275	8	-157	0	-112	-39	6.28	6.28	12.57	12.57	-5.91	-87.7
47	97	-14035	8	-142	0	-105	-39	6.28	6.28	12.57	12.57	-5.80	-86.0
49	97	-14035	56	-132	0	-98	-130	6.28	6.28	12.57	12.57	-5.77	-85.7
50	97	-14055	-40	-161	0	-116	52	6.28	6.28	12.57	12.57	-5.84	-86.6
51	97	-14015	9	-161	0	-123	-39	6.28	6.28	12.57	12.57	-5.85	-86.7

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	195	-14640	153	-188	0	67	-162	6.28	6.28	12.57	12.57	-6.07	-88.1
41	195	-14640	9	-217	0	74	-30	6.28	6.28	12.57	12.57	-5.92	-88.2
42	195	-14570	10	-274	0	77	-31	6.28	6.28	12.57	12.57	-5.91	-87.9
43	195	-14040	249	-132	0	42	-250	6.28	6.28	12.57	12.57	-6.29	-89.7
44	195	-14130	-232	-276	0	96	190	6.28	6.28	12.57	12.57	-6.03	-86.9
45	195	-13920	10	-275	0	59	-32	6.28	6.28	12.57	12.57	-5.59	-83.3
46	195	-13690	8	-157	0	41	-31	6.28	6.28	12.57	12.57	-5.44	-81.2
47	195	-13450	8	-142	0	33	-31	6.28	6.28	12.57	12.57	-5.31	-79.4
49	195	-13450	56	-132	0	31	-75	6.28	6.28	12.57	12.57	-5.31	-79.3
50	195	-13470	-40	-161	0	42	13	6.28	6.28	12.57	12.57	-5.35	-79.9
51	195	-13430	9	-161	0	34	-31	6.28	6.28	12.57	12.57	-5.31	-79.3

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	292	-14055	153	-188	0	251	-13	6.28	6.28	12.57	12.57	-6.33	-92.7
41	292	-14055	9	-217	0	286	-22	6.28	6.28	12.57	12.57	-6.45	-94.2
42	292	-13985	10	-274	0	345	-21	6.28	6.28	12.57	12.57	-6.64	-96.5
43	292	-13455	249	-132	0	170	-7	6.28	6.28	12.57	12.57	-5.81	-85.6
44	292	-13545	-232	-276	0	365	-36	6.28	6.28	12.57	12.57	-6.54	-94.8
45	292	-13335	10	-275	0	327	-21	6.28	6.28	12.57	12.57	-6.32	-91.9
46	292	-13105	8	-157	0	194	-23	6.28	6.28	12.57	12.57	-5.76	-84.6
47	292	-12865	8	-142	0	171	-23	6.28	6.28	12.57	12.57	-5.58	-82.2
49	292	-12865	56	-132	0	160	-20	6.28	6.28	12.57	12.57	-5.54	-81.7
50	292	-12885	-40	-161	0	198	-26	6.28	6.28	12.57	12.57	-5.69	-83.6
51	292	-12845	9	-161	0	191	-23	6.28	6.28	12.57	12.57	-5.65	-83.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	390	-13470	153	-188	0	435	136	6.28	6.28	12.57	12.57	-6.76	-97.5
41	390	-13470	9	-217	0	497	-13	6.28	6.28	12.57	12.57	-6.98	-100.3
42	390	-13400	10	-274	0	612	-11	6.28	6.28	12.57	12.57	-7.37	-105.0
43	390	-12870	249	-132	0	299	235	6.28	6.28	12.57	12.57	-6.04	-88.0
44	390	-12960	-232	-276	0	634	-263	6.28	6.28	12.57	12.57	-7.28	-103.5
45	390	-12750	10	-275	0	595	-11	6.28	6.28	12.57	12.57	-7.05	-100.5
46	390	-12520	8	-157	0	347	-14	6.28	6.28	12.57	12.57	-6.08	-88.1
47	390	-12280	8	-142	0	309	-15	6.28	6.28	12.57	12.57	-5.85	-85.0
49	390	-12280	56	-132	0	289	35	6.28	6.28	12.57	12.57	-5.78	-84.1
50	390	-12300	-40	-161	0	356	-65	6.28	6.28	12.57	12.57	-6.02	-87.2
51	390	-12260	9	-161	0	348	-14	6.28	6.28	12.57	12.57	-5.98	-86.6

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 50 NI 166 NF 167 SEZ. Rp B= 0.400 H= 0.600 (pilastro)
PIL. NUM. 26B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-9179	-395	-221	0	-587	603	12.57	12.57	6.28	6.28	-6.21	-82.2
41	0	-8666	-648	-173	0	-499	1391	12.57	12.57	6.28	6.28	-8.69	-116.3
42	0	-8667	-658	-47	0	-224	1398	12.57	12.57	6.28	6.28	-8.72	-116.7
43	0	-9208	-96	-170	0	-479	-98	12.57	12.57	6.28	6.28	-5.68	-76.4
44	0	-7737	-1091	-120	0	-399	2735	12.57	12.57	6.28	6.28	-17.67	338.0
45	0	-8356	-535	121	0	126	1227	12.57	12.57	6.28	6.28	-7.81	-105.3
46	0	-8166	-439	-38	0	-232	1111	12.57	12.57	6.28	6.28	-7.23	-98.1
47	0	-8041	-386	-5	0	-166	1040	12.57	12.57	6.28	6.28	-6.88	-93.7
49	0	-8212	-302	-21	0	-195	778	12.57	12.57	6.28	6.28	-5.96	-82.4
50	0	-7918	-501	-11	0	-179	1344	12.57	12.57	6.28	6.28	-8.32	-110.8
51	0	-8042	-390	37	0	-74	1043	12.57	12.57	6.28	6.28	-6.90	-93.9

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	97	-8594	-395	-221	0	-371	218	12.57	12.57	6.28	6.28	-4.93	-67.0
41	97	-8081	-648	-173	0	-330	760	12.57	12.57	6.28	6.28	-5.84	-80.8
42	97	-8082	-658	-47	0	-178	756	12.57	12.57	6.28	6.28	-5.83	-80.7
43	97	-8623	-96	-170	0	-314	-192	12.57	12.57	6.28	6.28	-4.66	-64.0
44	97	-7152	-1091	-120	0	-282	1671	12.57	12.57	6.28	6.28	-10.36	-132.2
45	97	-7771	-535	121	0	9	706	12.57	12.57	6.28	6.28	-5.53	-76.6
46	97	-7581	-439	-38	0	-195	683	12.57	12.57	6.28	6.28	-5.37	-74.5
47	97	-7456	-386	-5	0	-161	663	12.57	12.57	6.28	6.28	-5.26	-72.9
49	97	-7627	-302	-21	0	-175	483	12.57	12.57	6.28	6.28	-4.68	-65.8
50	97	-7333	-501	-11	0	-168	855	12.57	12.57	6.28	6.28	-5.90	-80.9
51	97	-7457	-390	37	0	-110	663	12.57	12.57	6.28	6.28	-5.25	-72.9

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	195	-8009	-395	-221	0	-155	-167	12.57	12.57	6.28	6.28	-3.69	-53.9
41	195	-7496	-648	-173	0	-161	128	12.57	12.57	6.28	6.28	-3.50	-49.5
42	195	-7497	-658	-47	0	-131	114	12.57	12.57	6.28	6.28	-3.35	-48.6
43	195	-8038	-96	-170	0	-149	-286	12.57	12.57	6.28	6.28	-4.13	-59.4
44	195	-6567	-1091	-120	0	-164	608	12.57	12.57	6.28	6.28	-4.71	-65.2
45	195	-7186	-535	121	0	-109	184	12.57	12.57	6.28	6.28	-3.44	-49.9
46	195	-6996	-439	-38	0	-158	255	12.57	12.57	6.28	6.28	-3.62	-52.0
47	195	-6871	-386	-5	0	-157	286	12.57	12.57	6.28	6.28	-3.68	-52.6
49	195	-7042	-302	-21	0	-154	188	12.57	12.57	6.28	6.28	-3.39	-49.2
50	195	-6748	-501	-11	0	-158	366	12.57	12.57	6.28	6.28	-3.92	-55.5
51	195	-6872	-390	37	0	-147	282	12.57	12.57	6.28	6.28	-3.67	-52.5

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	292	-7424	-395	-221	0	61	-552	12.57	12.57	6.28	6.28	-4.85	-67.7
41	292	-6911	-648	-173	0	7	-503	12.57	12.57	6.28	6.28	-4.47	-62.6
42	292	-6912	-658	-47	0	-85	-527	12.57	12.57	6.28	6.28	-4.56	-63.7
43	292	-7453	-96	-170	0	17	-379	12.57	12.57	6.28	6.28	-4.24	-60.2
44	292	-5982	-1091	-120	0	-47	-456	12.57	12.57	6.28	6.28	-3.94	-55.1
45	292	-6601	-535	121	0	-227	-337	12.57	12.57	6.28	6.28	-3.76	-53.3
46	292	-6411	-439	-38	0	-120	-173	12.57	12.57	6.28	6.28	-3.09	-44.9
47	292	-6286	-386	-5	0	-152	-90	12.57	12.57	6.28	6.28	-3.01	-42.4
49	292	-6457	-302	-21	0	-134	-107	12.57	12.57	6.28	6.28	-2.99	-42.3
50	292	-6163	-501	-11	0	-147	-122	12.57	12.57	6.28	6.28	-2.95	-41.5
51	292	-6287	-390	37	0	-183	-98	12.57	12.57	6.28	6.28	-3.17	-44.1

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	390	-6839	-395	-221	0	277	-937	12.57	12.57	6.28	6.28	-6.08	-82.5
41	390	-6326	-648	-173	0	176	-1134	12.57	12.57	6.28	6.28	-6.99	-92.5
42	390	-6327	-658	-47	0	-39	-1169	12.57	12.57	6.28	6.28	-7.19	-94.8
43	390	-6868	-96	-170	0	182	-473	12.57	12.57	6.28	6.28	-4.35	-61.0
44	390	-5397	-1091	-120	0	71	-1520	12.57	12.57	6.28	6.28	-9.61	133.3
45	390	-6016	-535	121	0	-344	-859	12.57	12.57	6.28	6.28	-5.51	-74.5
46	390	-5826	-439	-38	0	-83	-600	12.57	12.57	6.28	6.28	-4.40	-60.6
47	390	-5701	-386	-5	0	-148	-467	12.57	12.57	6.28	6.28	-3.88	-53.9
49	390	-5872	-302	-21	0	-114	-402	12.57	12.57	6.28	6.28	-3.71	-52.0
50	390	-5578	-501	-11	0	-136	-611	12.57	12.57	6.28	6.28	-4.34	-59.7
51	390	-5702	-390	37	0	-219	-479	12.57	12.57	6.28	6.28	-3.92	-54.5

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

ASTA NUM. 51 NI 168 NF 169 SEZ. Rp B= 0.400 H= 0.600 (pilastro)

PIL. NUM. 11B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-5524	1229	380	0	379	-3165	12.57	12.57	6.28	6.28	-20.83	599.8
41	0	-5893	600	354	0	327	-1756	12.57	12.57	6.28	6.28	-11.16	169.7
42	0	-5881	603	324	0	270	-1762	12.57	12.57	6.28	6.28	-11.21	171.8
43	0	-5275	1536	389	0	402	-3865	12.57	12.57	6.28	6.28	-25.44	831.9
44	0	-6400	-430	306	0	240	555	12.57	12.57	6.28	6.28	-4.46	-61.9
45	0	-5869	494	297	0	218	-1526	12.57	12.57	6.28	6.28	-9.56	-119.9
46	0	-5887	421	342	0	307	-1372	12.57	12.57	6.28	6.28	-8.50	-108.5
47	0	-5886	376	338	0	302	-1276	12.57	12.57	6.28	6.28	-7.86	-101.5
49	0	-5763	585	347	0	320	-1746	12.57	12.57	6.28	6.28	-11.12	173.4
50	0	-5988	192	330	0	287	-862	12.57	12.57	6.28	6.28	-5.51	-74.5
51	0	-5882	377	329	0	283	-1278	12.57	12.57	6.28	6.28	-7.88	-101.6

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	97	-4939	1229	380	0	9	-1967	12.57	12.57	6.28	6.28	-12.81	278.5
41	97	-5308	600	354	0	-18	-1171	12.57	12.57	6.28	6.28	-7.22	-93.0
42	97	-5296	603	324	0	-47	-1174	12.57	12.57	6.28	6.28	-7.24	-93.2
43	97	-4690	1536	389	0	22	-2367	12.57	12.57	6.28	6.28	-15.55	412.3
44	97	-5815	-430	306	0	-58	136	12.57	12.57	6.28	6.28	-2.73	-39.8
45	97	-5284	494	297	0	-71	-1045	12.57	12.57	6.28	6.28	-6.42	-83.9
46	97	-5302	421	342	0	-26	-962	12.57	12.57	6.28	6.28	-5.92	-78.3
47	97	-5301	376	338	0	-28	-910	12.57	12.57	6.28	6.28	-5.63	-74.8
49	97	-5178	585	347	0	-19	-1175	12.57	12.57	6.28	6.28	-7.26	-93.1
50	97	-5403	192	330	0	-35	-675	12.57	12.57	6.28	6.28	-4.52	-61.7
51	97	-5297	377	329	0	-38	-911	12.57	12.57	6.28	6.28	-5.63	-74.9

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	195	-4354	1229	380	0	-361	-769	12.57	12.57	6.28	6.28	-4.74	-62.9
41	195	-4723	600	354	0	-363	-586	12.57	12.57	6.28	6.28	-3.94	-53.8
42	195	-4711	603	324	0	-363	-585	12.57	12.57	6.28	6.28	-3.93	-53.7
43	195	-4105	1536	389	0	-357	-870	12.57	12.57	6.28	6.28	-5.35	-69.3
44	195	-5230	-430	306	0	-356	-284	12.57	12.57	6.28	6.28	-3.64	-48.0
45	195	-4699	494	297	0	-360	-563	12.57	12.57	6.28	6.28	-3.84	-52.5
46	195	-4717	421	342	0	-359	-552	12.57	12.57	6.28	6.28	-3.80	-52.1
47	195	-4716	376	338	0	-358	-543	12.57	12.57	6.28	6.28	-3.77	-51.7
49	195	-4593	585	347	0	-357	-604	12.57	12.57	6.28	6.28	-3.98	-54.1
50	195	-4818	192	330	0	-357	-487	12.57	12.57	6.28	6.28	-3.61	-49.7
51	195	-4712	377	329	0	-358	-543	12.57	12.57	6.28	6.28	-3.77	-51.7

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	292	-3769	1229	380	0	-732	429	12.57	12.57	6.28	6.28	-5.98	-68.0
41	292	-4138	600	354	0	-709	-2	12.57	12.57	6.28	6.28	-5.80	-67.6
42	292	-4126	603	324	0	-679	3	12.57	12.57	6.28	6.28	-5.57	-65.4
43	292	-3520	1536	389	0	-737	628	12.57	12.57	6.28	6.28	-6.02	70.1
44	292	-4645	-430	306	0	-653	-703	12.57	12.57	6.28	6.28	-5.40	-65.3
45	292	-4114	494	297	0	-650	-82	12.57	12.57	6.28	6.28	-5.34	-63.2
46	292	-4132	421	342	0	-692	-142	12.57	12.57	6.28	6.28	-5.67	-66.4
47	292	-4131	376	338	0	-688	-177	12.57	12.57	6.28	6.28	-5.64	-66.1
49	292	-4008	585	347	0	-696	-34	12.57	12.57	6.28	6.28	-5.70	-66.2
50	292	-4233	192	330	0	-679	-300	12.57	12.57	6.28	6.28	-5.57	-65.8
51	292	-4127	377	329	0	-678	-176	12.57	12.57	6.28	6.28	-5.56	-65.3

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	390	-3184	1229	380	0	-1102	1627	12.57	12.57	6.28	6.28	-10.69	285.9
41	390	-3553	600	354	0	-1054	583	12.57	12.57	6.28	6.28	-8.56	143.8
42	390	-3541	603	324	0	-996	591	12.57	12.57	6.28	6.28	-8.09	130.1
43	390	-2935	1536	389	0	-1116	2126	12.57	12.57	6.28	6.28	-13.99	455.3
44	390	-4060	-430	306	0	-951	-1123	12.57	12.57	6.28	6.28	-7.76	104.0
45	390	-3529	494	297	0	-939	399	12.57	12.57	6.28	6.28	-7.64	116.9
46	390	-3547	421	342	0	-1025	268	12.57	12.57	6.28	6.28	-8.33	137.0
47	390	-3546	376	338	0	-1018	189	12.57	12.57	6.28	6.28	-8.27	135.3
49	390	-3423	585	347	0	-1034	537	12.57	12.57	6.28	6.28	-8.39	143.1
50	390	-3648	192	330	0	-1001	-113	12.57	12.57	6.28	6.28	-8.14	128.1
51	390	-3542	377	329	0	-999	192	12.57	12.57	6.28	6.28	-8.12	130.8

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

ASTA NUM. 52 NI 170 NF 171 SEZ. Rp B= 0.400 H= 0.600 (pilastro)
PIL. NUM. 16B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-9446	1877	541	0	520	-3385	12.57	12.57	6.28	6.28	-21.89	425.4
41	0	-9467	958	552	0	534	-1665	12.57	12.57	6.28	6.28	-10.27	-136.3
42	0	-9401	963	488	0	424	-1676	12.57	12.57	6.28	6.28	-10.33	-136.8
43	0	-9281	2326	524	0	505	-4237	12.57	12.57	6.28	6.28	-27.76	682.0
44	0	-9300	-547	552	0	538	1153	12.57	12.57	6.28	6.28	-7.76	-105.9
45	0	-9206	803	436	0	346	-1387	12.57	12.57	6.28	6.28	-8.77	-118.1
46	0	-9227	696	538	0	525	-1193	12.57	12.57	6.28	6.28	-7.90	-107.5
47	0	-9167	631	534	0	523	-1075	12.57	12.57	6.28	6.28	-7.40	-101.4
49	0	-9160	937	530	0	518	-1648	12.57	12.57	6.28	6.28	-10.15	-134.3
50	0	-9164	362	536	0	525	-570	12.57	12.57	6.28	6.28	-5.89	-78.7
51	0	-9145	632	513	0	487	-1078	12.57	12.57	6.28	6.28	-7.41	-101.4

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	97	-8861	1877	541	0	-7	-1555	12.57	12.57	6.28	6.28	-9.60	-127.3
41	97	-8882	958	552	0	-5	-731	12.57	12.57	6.28	6.28	-6.05	-84.2
42	97	-8816	963	488	0	-52	-736	12.57	12.57	6.28	6.28	-6.04	-84.1
43	97	-8696	2326	524	0	-5	-1969	12.57	12.57	6.28	6.28	-12.17	-156.1
44	97	-8715	-547	552	0	-0	620	12.57	12.57	6.28	6.28	-5.59	-78.3

45	97	-8621	803	436	0	-79	-604	12.57	12.57	6.28	6.28	-5.49	-77.0
46	97	-8642	696	538	0	1	-514	12.57	12.57	6.28	6.28	-5.18	-73.1
47	97	-8582	631	534	0	2	-460	12.57	12.57	6.28	6.28	-4.96	-70.3
49	97	-8575	937	530	0	1	-734	12.57	12.57	6.28	6.28	-5.94	-82.6
50	97	-8579	362	536	0	2	-217	12.57	12.57	6.28	6.28	-4.09	-59.4
51	97	-8560	632	513	0	-13	-461	12.57	12.57	6.28	6.28	-4.96	-70.2

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	195	-8276	1877	541	0	-535	276	12.57	12.57	6.28	6.28	-5.62	-74.4
41	195	-8297	958	552	0	-544	204	12.57	12.57	6.28	6.28	-5.67	-75.0
42	195	-8231	963	488	0	-527	203	12.57	12.57	6.28	6.28	-5.57	-73.8
43	195	-8111	2326	524	0	-516	299	12.57	12.57	6.28	6.28	-5.47	-72.5
44	195	-8130	-547	552	0	-538	87	12.57	12.57	6.28	6.28	-5.59	-73.8
45	195	-8036	803	436	0	-504	179	12.57	12.57	6.28	6.28	-5.38	-71.4
46	195	-8057	696	538	0	-524	165	12.57	12.57	6.28	6.28	-5.49	-72.6
47	195	-7997	631	534	0	-519	155	12.57	12.57	6.28	6.28	-5.44	-72.0
49	195	-7990	937	530	0	-516	180	12.57	12.57	6.28	6.28	-5.43	-71.8
50	195	-7994	362	536	0	-520	137	12.57	12.57	6.28	6.28	-5.45	-72.1
51	195	-7975	632	513	0	-513	156	12.57	12.57	6.28	6.28	-5.41	-71.6

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	292	-7691	1877	541	0	-1062	2106	12.57	12.57	6.28	6.28	-13.27	175.4
41	292	-7712	958	552	0	-1082	1138	12.57	12.57	6.28	6.28	-8.94	-108.2
42	292	-7646	963	488	0	-1003	1142	12.57	12.57	6.28	6.28	-8.33	-102.1
43	292	-7526	2326	524	0	-1026	2567	12.57	12.57	6.28	6.28	-16.53	302.9
44	292	-7545	-547	552	0	-1076	-446	12.57	12.57	6.28	6.28	-8.88	-107.2
45	292	-7451	803	436	0	-929	962	12.57	12.57	6.28	6.28	-7.76	-95.9
46	292	-7472	696	538	0	-1048	844	12.57	12.57	6.28	6.28	-8.66	-104.8
47	292	-7412	631	534	0	-1040	770	12.57	12.57	6.28	6.28	-8.59	-104.0
49	292	-7405	937	530	0	-1033	1093	12.57	12.57	6.28	6.28	-8.53	-103.4
50	292	-7409	362	536	0	-1043	490	12.57	12.57	6.28	6.28	-8.61	-104.2
51	292	-7390	632	513	0	-1013	772	12.57	12.57	6.28	6.28	-8.38	-101.9

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	390	-7106	1877	541	0	-1589	3936	12.57	12.57	6.28	6.28	-25.90	730.4
41	390	-7127	958	552	0	-1621	2072	12.57	12.57	6.28	6.28	-13.22	192.2
42	390	-7061	963	488	0	-1479	2082	12.57	12.57	6.28	6.28	-13.22	197.7
43	390	-6941	2326	524	0	-1537	4835	12.57	12.57	6.28	6.28	-31.83	1017.2
44	390	-6960	-547	552	0	-1614	-979	12.57	12.57	6.28	6.28	-13.16	174.4
45	390	-6866	803	436	0	-1354	1745	12.57	12.57	6.28	6.28	-11.07	-137.3
46	390	-6887	696	538	0	-1573	1523	12.57	12.57	6.28	6.28	-12.83	167.1
47	390	-6827	631	534	0	-1561	1385	12.57	12.57	6.28	6.28	-12.73	166.0
49	390	-6820	937	530	0	-1550	2007	12.57	12.57	6.28	6.28	-12.74	190.0
50	390	-6824	362	536	0	-1565	844	12.57	12.57	6.28	6.28	-12.77	167.0
51	390	-6805	632	513	0	-1513	1389	12.57	12.57	6.28	6.28	-12.35	155.6

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

ASTA NUM. 53 NI 172 NF 185 SEZ. Rp B= 0.400 H= 0.600 (pilastro)
PIL. NUM. 21B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	--												
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-9467	1808	620	0	659	-3480	12.57	12.57	6.28	6.28	-22.54	451.0
41	0	-9498	865	598	0	620	-1691	12.57	12.57	6.28	6.28	-10.42	-138.1
42	0	-9523	870	573	0	570	-1698	12.57	12.57	6.28	6.28	-10.47	-138.6
43	0	-9292	2261	612	0	656	-4349	12.57	12.57	6.28	6.28	-28.52	714.6
44	0	-9350	-681	544	0	540	1246	12.57	12.57	6.28	6.28	-8.16	-110.9
45	0	-9384	697	533	0	508	-1378	12.57	12.57	6.28	6.28	-8.77	-118.3
46	0	-9251	584	562	0	574	-1172	12.57	12.57	6.28	6.28	-7.82	-106.6
47	0	-9190	514	553	0	562	-1042	12.57	12.57	6.28	6.28	-7.29	-99.9
49	0	-9179	828	560	0	575	-1639	12.57	12.57	6.28	6.28	-10.10	-133.8
50	0	-9191	240	546	0	552	-520	12.57	12.57	6.28	6.28	-6.04	-80.3
51	0	-9198	516	544	0	546	-1045	12.57	12.57	6.28	6.28	-7.30	-100.1

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	97	-8882	1808	620	0	54	-1718	12.57	12.57	6.28	6.28	-10.55	-138.4
41	97	-8913	865	598	0	36	-847	12.57	12.57	6.28	6.28	-6.48	-89.6
42	97	-8938	870	573	0	11	-850	12.57	12.57	6.28	6.28	-6.50	-89.8
43	97	-8707	2261	612	0	60	-2145	12.57	12.57	6.28	6.28	-13.36	-169.1
44	97	-8765	-681	544	0	9	582	12.57	12.57	6.28	6.28	-5.47	-76.9
45	97	-8799	697	533	0	-13	-698	12.57	12.57	6.28	6.28	-5.90	-82.3
46	97	-8666	584	562	0	26	-602	12.57	12.57	6.28	6.28	-5.50	-77.2
47	97	-8605	514	553	0	23	-541	12.57	12.57	6.28	6.28	-5.26	-74.1
49	97	-8594	828	560	0	29	-831	12.57	12.57	6.28	6.28	-6.30	-87.0
50	97	-8606	240	546	0	19	-286	12.57	12.57	6.28	6.28	-4.35	-62.7
51	97	-8613	516	544	0	15	-542	12.57	12.57	6.28	6.28	-5.27	-74.2

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	195	-8297	1808	620	0	-551	45	12.57	12.57	6.28	6.28	-5.71	-75.4
41	195	-8328	865	598	0	-547	-4	12.57	12.57	6.28	6.28	-5.70	-75.4
42	195	-8353	870	573	0	-548	-2	12.57	12.57	6.28	6.28	-5.71	-75.6
43	195	-8122	2261	612	0	-537	59	12.57	12.57	6.28	6.28	-5.58	-73.7
44	195	-8180	-681	544	0	-522	-82	12.57	12.57	6.28	6.28	-5.52	-73.2
45	195	-8214	697	533	0	-533	-19	12.57	12.57	6.28	6.28	-5.59	-74.0
46	195	-8081	584	562	0	-522	-32	12.57	12.57	6.28	6.28	-5.49	-72.6
47	195	-8020	514	553	0	-515	-39	12.57	12.57	6.28	6.28	-5.43	-72.0
49	195	-8009	828	560	0	-516	-24	12.57	12.57	6.28	6.28	-5.44	-72.0
50	195	-8021	240	546	0	-513	-52	12.57	12.57	6.28	6.28	-5.43	-71.9
51	195	-8028	516	544	0	-516	-39	12.57	12.57	6.28	6.28	-5.44	-72.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	292	-7712	1808	620	0	-1155	1807	12.57	12.57	6.28	6.28	-11.20	-142.9
41	292	-7743	865	598	0	-1131	840	12.57	12.57	6.28	6.28	-9.31	-111.9
42	292	-7768	870	573	0	-1106	846	12.57	12.57	6.28	6.28	-9.13	-110.2
43	292	-7537	2261	612	0	-1134	2263	12.57	12.57	6.28	6.28	-14.40	221.4
44	292	-7595	-681	544	0	-1052	-745	12.57	12.57	6.28	6.28	-8.70	-105.5
45	292	-7629	697	533	0	-1053	660	12.57	12.57	6.28	6.28	-8.71	-105.7

46	292	-7496	584	562	0	-1069	537	12.57	12.57	6.28	6.28	-8.82	-106.5
47	292	-7435	514	553	0	-1054	462	12.57	12.57	6.28	6.28	-8.70	-105.1
49	292	-7424	828	560	0	-1062	784	12.57	12.57	6.28	6.28	-8.76	-105.7
50	292	-7436	240	546	0	-1046	183	12.57	12.57	6.28	6.28	-8.64	-104.5
51	292	-7443	516	544	0	-1046	464	12.57	12.57	6.28	6.28	-8.64	-104.6

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	390	-7127	1808	620	0	-1760	3570	12.57	12.57	6.28	6.28	-23.45	618.3
41	390	-7158	865	598	0	-1714	1684	12.57	12.57	6.28	6.28	-13.97	192.0
42	390	-7183	870	573	0	-1665	1694	12.57	12.57	6.28	6.28	-13.58	179.9
43	390	-6952	2261	612	0	-1730	4467	12.57	12.57	6.28	6.28	-29.42	903.1
44	390	-7010	-681	544	0	-1583	-1409	12.57	12.57	6.28	6.28	-12.92	165.9
45	390	-7044	697	533	0	-1573	1340	12.57	12.57	6.28	6.28	-12.84	162.6
46	390	-6911	584	562	0	-1617	1107	12.57	12.57	6.28	6.28	-13.19	176.5
47	390	-6850	514	553	0	-1593	963	12.57	12.57	6.28	6.28	-12.99	172.7
49	390	-6839	828	560	0	-1608	1592	12.57	12.57	6.28	6.28	-13.11	176.5
50	390	-6851	240	546	0	-1579	417	12.57	12.57	6.28	6.28	-12.88	169.5
51	390	-6858	516	544	0	-1577	966	12.57	12.57	6.28	6.28	-12.86	168.8

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

ASTA NUM. 54 NI 167 NF 208 SEZ. Rp B= 0.400 H= 0.600 (pilastro)
PIL. NUM. 26C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-2299	4043	-1298	0	1326	-4206	12.57	12.57	6.28	6.28	-27.25	1151.0
41	0	-2168	2929	-1120	0	1239	-3135	12.57	12.57	6.28	6.28	-20.40	824.6
42	0	-1939	2986	-182	0	1394	-3189	12.57	12.57	6.28	6.28	-20.70	858.3
43	0	-2174	4193	-1115	0	1268	-4298	12.57	12.57	6.28	6.28	-27.80	1189.0
44	0	-1981	1168	-871	0	1101	-1450	12.57	12.57	6.28	6.28	-9.54	312.0
45	0	-1575	2432	744	0	1382	-2604	12.57	12.57	6.28	6.28	-16.90	701.5
46	0	-1829	1982	-637	0	1053	-2140	12.57	12.57	6.28	6.28	-13.98	537.6
47	0	-1745	1745	-516	0	1007	-1892	12.57	12.57	6.28	6.28	-12.38	466.1
49	0	-1788	2116	-576	0	1036	-2249	12.57	12.57	6.28	6.28	-14.67	574.7
50	0	-1750	1511	-527	0	1002	-1679	12.57	12.57	6.28	6.28	-11.01	399.3
51	0	-1668	1764	-204	0	1059	-1910	12.57	12.57	6.28	6.28	-12.48	477.3

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	12	-2224	4043	-1298	0	1488	-3700	12.57	12.57	6.28	6.28	-24.01	997.9
41	12	-2093	2929	-1120	0	1379	-2769	12.57	12.57	6.28	6.28	-18.05	715.3
42	12	-1864	2986	-182	0	1417	-2816	12.57	12.57	6.28	6.28	-18.31	746.7
43	12	-2099	4193	-1115	0	1408	-3774	12.57	12.57	6.28	6.28	-24.45	1030.0
44	12	-1906	1168	-871	0	1210	-1304	12.57	12.57	6.28	6.28	-9.59	272.0
45	12	-1500	2432	744	0	1289	-2300	12.57	12.57	6.28	6.28	-14.95	611.6
46	12	-1754	1982	-637	0	1133	-1892	12.57	12.57	6.28	6.28	-12.38	465.6
47	12	-1670	1745	-516	0	1072	-1674	12.57	12.57	6.28	6.28	-10.97	403.3
49	12	-1713	2116	-576	0	1108	-1984	12.57	12.57	6.28	6.28	-12.97	497.3
50	12	-1675	1511	-527	0	1068	-1490	12.57	12.57	6.28	6.28	-9.78	345.8
51	12	-1593	1764	-204	0	1084	-1690	12.57	12.57	6.28	6.28	-11.06	413.8

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	25	-2149	4043	-1298	0	1650	-3195	12.57	12.57	6.28	6.28	-20.78	844.8
41	25	-2018	2929	-1120	0	1519	-2402	12.57	12.57	6.28	6.28	-15.69	606.1
42	25	-1789	2986	-182	0	1440	-2442	12.57	12.57	6.28	6.28	-15.91	635.2
43	25	-2024	4193	-1115	0	1547	-3250	12.57	12.57	6.28	6.28	-21.10	871.0
44	25	-1831	1168	-871	0	1318	-1158	12.57	12.57	6.28	6.28	-10.41	269.3
45	25	-1425	2432	744	0	1196	-1996	12.57	12.57	6.28	6.28	-13.00	521.8
46	25	-1679	1982	-637	0	1212	-1644	12.57	12.57	6.28	6.28	-10.78	393.6
47	25	-1595	1745	-516	0	1136	-1456	12.57	12.57	6.28	6.28	-9.55	340.6
49	25	-1638	2116	-576	0	1180	-1720	12.57	12.57	6.28	6.28	-11.26	420.1
50	25	-1600	1511	-527	0	1134	-1301	12.57	12.57	6.28	6.28	-8.96	292.3
51	25	-1518	1764	-204	0	1110	-1469	12.57	12.57	6.28	6.28	-9.63	350.3

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	38	-2074	4043	-1298	0	1813	-2690	12.57	12.57	6.28	6.28	-17.54	691.9
41	38	-1943	2929	-1120	0	1659	-2036	12.57	12.57	6.28	6.28	-13.33	497.0
42	38	-1714	2986	-182	0	1463	-2069	12.57	12.57	6.28	6.28	-13.51	523.8
43	38	-1949	4193	-1115	0	1686	-2725	12.57	12.57	6.28	6.28	-17.74	712.2
44	38	-1756	1168	-871	0	1427	-1012	12.57	12.57	6.28	6.28	-11.23	299.7
45	38	-1350	2432	744	0	1103	-1692	12.57	12.57	6.28	6.28	-11.04	432.0
46	38	-1604	1982	-637	0	1292	-1397	12.57	12.57	6.28	6.28	-10.17	321.7
47	38	-1520	1745	-516	0	1200	-1237	12.57	12.57	6.28	6.28	-9.46	278.0
49	38	-1563	2116	-576	0	1252	-1456	12.57	12.57	6.28	6.28	-9.86	342.9
50	38	-1525	1511	-527	0	1200	-1112	12.57	12.57	6.28	6.28	-9.45	250.2
51	38	-1443	1764	-204	0	1136	-1248	12.57	12.57	6.28	6.28	-8.95	286.9

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	50	-1999	4043	-1298	0	1975	-2184	12.57	12.57	6.28	6.28	-15.46	539.2
41	50	-1868	2929	-1120	0	1799	-1670	12.57	12.57	6.28	6.28	-14.09	390.4
42	50	-1639	2986	-182	0	1486	-1696	12.57	12.57	6.28	6.28	-11.66	412.5
43	50	-1874	4193	-1115	0	1826	-2201	12.57	12.57	6.28	6.28	-14.38	553.5
44	50	-1681	1168	-871	0	1536	-866	12.57	12.57	6.28	6.28	-12.05	330.2
45	50	-1275	2432	744	0	1010	-1388	12.57	12.57	6.28	6.28	-9.08	342.3
46	50	-1529	1982	-637	0	1372	-1149	12.57	12.57	6.28	6.28	-10.77	293.9
47	50	-1445	1745	-516	0	1265	-1019	12.57	12.57	6.28	6.28	-9.94	269.7
49	50	-1488	2116	-576	0	1324	-1191	12.57	12.57	6.28	6.28	-10.39	283.2
50	50	-1450	1511	-527	0	1266	-924	12.57	12.57	6.28	6.28	-9.94	269.8
51	50	-1368	1764	-204	0	1161	-1028	12.57	12.57	6.28	6.28	-9.13	246.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

ASTA NUM. 55 NI 122 NF 165 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 24B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf

	--												
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-9435	87	-634	0	-1238	-139	6.28	6.28	9.42	9.42	-10.46	-142.5
41	0	-9394	-9	-518	0	-1019	135	6.28	6.28	9.42	9.42	-9.37	-129.0
42	0	-9382	-10	-298	0	-588	136	6.28	6.28	9.42	9.42	-7.40	-104.3
43	0	-9163	156	-609	0	-1187	-339	6.28	6.28	9.42	9.42	-10.08	-137.4
44	0	-9053	-171	-346	0	-689	594	6.28	6.28	9.42	9.42	-9.92	-120.6
45	0	-9075	-5	-50	0	-102	120	6.28	6.28	9.42	9.42	-5.46	-76.3
46	0	-8916	-1	-356	0	-702	108	6.28	6.28	9.42	9.42	-7.68	-107.3
47	0	-8797	1	-315	0	-623	101	6.28	6.28	9.42	9.42	-7.26	-101.9
49	0	-8810	33	-354	0	-696	10	6.28	6.28	9.42	9.42	-7.60	-106.1
50	0	-8788	-32	-301	0	-596	196	6.28	6.28	9.42	9.42	-7.14	-100.3
51	0	-8793	1	-242	0	-479	102	6.28	6.28	9.42	9.42	-6.61	-93.6

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	97	-8996	87	-634	0	-620	-55	6.28	6.28	9.42	9.42	-7.35	-103.2
41	97	-8955	-9	-518	0	-514	125	6.28	6.28	9.42	9.42	-6.85	-96.8
42	97	-8943	-10	-298	0	-297	126	6.28	6.28	9.42	9.42	-5.85	-84.4
43	97	-8724	156	-609	0	-593	-186	6.28	6.28	9.42	9.42	-7.09	-99.6
44	97	-8614	-171	-346	0	-352	427	6.28	6.28	9.42	9.42	-8.06	-101.3
45	97	-8636	-5	-50	0	-53	114	6.28	6.28	9.42	9.42	-5.20	-72.7
46	97	-8477	-1	-356	0	-355	107	6.28	6.28	9.42	9.42	-5.88	-84.2
47	97	-8358	1	-315	0	-315	102	6.28	6.28	9.42	9.42	-5.64	-81.0
49	97	-8371	33	-354	0	-351	42	6.28	6.28	9.42	9.42	-5.81	-83.2
50	97	-8349	-32	-301	0	-303	165	6.28	6.28	9.42	9.42	-5.58	-80.2
51	97	-8354	1	-242	0	-243	102	6.28	6.28	9.42	9.42	-5.31	-76.9

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	195	-8558	87	-634	0	-2	30	6.28	6.28	9.42	9.42	-4.39	-64.7
41	195	-8516	-9	-518	0	-8	116	6.28	6.28	9.42	9.42	-5.16	-72.0
42	195	-8504	-10	-298	0	-6	116	6.28	6.28	9.42	9.42	-5.15	-71.9
43	195	-8286	156	-609	0	0	-34	6.28	6.28	9.42	9.42	-4.29	-62.8
44	195	-8176	-171	-346	0	-15	260	6.28	6.28	9.42	9.42	-6.32	-82.8
45	195	-8198	-5	-50	0	-4	109	6.28	6.28	9.42	9.42	-4.94	-69.0
46	195	-8038	-1	-356	0	-8	106	6.28	6.28	9.42	9.42	-4.83	-67.6
47	195	-7920	1	-315	0	-8	103	6.28	6.28	9.42	9.42	-4.75	-66.5
49	195	-7932	33	-354	0	-6	74	6.28	6.28	9.42	9.42	-4.49	-63.9
50	195	-7910	-32	-301	0	-9	133	6.28	6.28	9.42	9.42	-5.02	-69.2
51	195	-7916	1	-242	0	-7	103	6.28	6.28	9.42	9.42	-4.74	-66.4

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	292	-8119	87	-634	0	615	115	6.28	6.28	9.42	9.42	-6.89	-96.3
41	292	-8078	-9	-518	0	497	107	6.28	6.28	9.42	9.42	-6.33	-89.3
42	292	-8066	-10	-298	0	285	106	6.28	6.28	9.42	9.42	-5.36	-77.1
43	292	-7847	156	-609	0	594	118	6.28	6.28	9.42	9.42	-6.66	-93.1
44	292	-7737	-171	-346	0	322	94	6.28	6.28	9.42	9.42	-5.36	-76.7
45	292	-7759	-5	-50	0	44	104	6.28	6.28	9.42	9.42	-4.68	-65.4
46	292	-7600	-1	-356	0	339	104	6.28	6.28	9.42	9.42	-5.37	-76.6
47	292	-7481	1	-315	0	299	104	6.28	6.28	9.42	9.42	-5.13	-73.5
49	292	-7494	33	-354	0	339	106	6.28	6.28	9.42	9.42	-5.31	-75.8
50	292	-7472	-32	-301	0	284	101	6.28	6.28	9.42	9.42	-5.05	-72.6
51	292	-7477	1	-242	0	229	103	6.28	6.28	9.42	9.42	-4.80	-69.4

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	390	-7680	87	-634	0	1233	200	6.28	6.28	9.42	9.42	-9.81	-131.7
41	390	-7639	-9	-518	0	1003	98	6.28	6.28	9.42	9.42	-8.47	-115.4
42	390	-7627	-10	-298	0	576	96	6.28	6.28	9.42	9.42	-6.46	-90.4
43	390	-7408	156	-609	0	1188	271	6.28	6.28	9.42	9.42	-9.45	-126.9
44	390	-7298	-171	-346	0	659	-73	6.28	6.28	9.42	9.42	-6.67	-92.6
45	390	-7320	-5	-50	0	93	98	6.28	6.28	9.42	9.42	-4.42	-61.7
46	390	-7161	-1	-356	0	686	103	6.28	6.28	9.42	9.42	-6.73	-93.1
47	390	-7042	1	-315	0	607	105	6.28	6.28	9.42	9.42	-6.31	-87.7
49	390	-7055	33	-354	0	683	138	6.28	6.28	9.42	9.42	-6.66	-92.2
50	390	-7033	-32	-301	0	578	70	6.28	6.28	9.42	9.42	-6.17	-86.0
51	390	-7038	1	-242	0	464	104	6.28	6.28	9.42	9.42	-5.66	-79.6

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 56 NI 209 NF 210 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 23B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	--												
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-6278	138	-907	0	-1412	-151	6.28	6.28	9.42	9.42	-10.87	-140.6
41	0	-6153	80	-837	0	-1254	-23	6.28	6.28	9.42	9.42	-9.68	-126.7
42	0	-6038	87	-677	0	-896	-39	6.28	6.28	9.42	9.42	-7.27	-98.2
43	0	-6190	181	-866	0	-1345	-246	6.28	6.28	9.42	9.42	-10.36	-134.6
44	0	-5829	-18	-712	0	-994	191	6.28	6.28	9.42	9.42	-7.82	-104.3
45	0	-5791	97	-483	0	-486	-59	6.28	6.28	9.42	9.42	-5.13	-71.4
46	0	-5879	86	-698	0	-978	-37	6.28	6.28	9.42	9.42	-7.73	-103.4
47	0	-5811	87	-663	0	-909	-40	6.28	6.28	9.42	9.42	-7.28	-97.9
49	0	-5852	107	-686	0	-962	-83	6.28	6.28	9.42	9.42	-7.62	-102.0
50	0	-5780	67	-655	0	-892	4	6.28	6.28	9.42	9.42	-7.16	-96.4
51	0	-5773	90	-609	0	-790	-46	6.28	6.28	9.42	9.42	-6.57	-89.3

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	97	-5839	138	-907	0	-528	-16	6.28	6.28	9.42	9.42	-5.34	-74.1
41	97	-5714	80	-837	0	-438	55	6.28	6.28	9.42	9.42	-4.87	-68.1
42	97	-5599	87	-677	0	-236	46	6.28	6.28	9.42	9.42	-3.89	-55.7
43	97	-5751	181	-866	0	-501	-69	6.28	6.28	9.42	9.42	-5.18	-71.9
44	97	-5390	-18	-712	0	-300	174	6.28	6.28	9.42	9.42	-4.18	-57.8
45	97	-5352	97	-483	0	-15	36	6.28	6.28	9.42	9.42	-2.90	-41.8
46	97	-5440	86	-698	0	-298	47	6.28	6.28	9.42	9.42	-4.10	-58.0
47	97	-5372	87	-663	0	-263	45	6.28	6.28	9.42	9.42	-3.90	-55.5
49	97	-5413	107	-686	0	-293	21	6.28	6.28	9.42	9.42	-4.06	-57.6
50	97	-5341	67	-655	0	-253	70	6.28	6.28	9.42	9.42	-3.84	-54.7
51	97	-5334	90	-609	0	-196	42	6.28	6.28	9.42	9.42	-3.58	-51.4

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	195	-5400	138	-907	0	356	118	6.28	6.28	9.42	9.42	-4.34	-61.0
41	195	-5276	80	-837	0	378	133	6.28	6.28	9.42	9.42	-4.38	-61.3
42	195	-5160	87	-677	0	423	132	6.28	6.28	9.42	9.42	-4.53	-63.1
43	195	-5312	181	-866	0	344	108	6.28	6.28	9.42	9.42	-4.24	-59.7
44	195	-4952	-18	-712	0	394	156	6.28	6.28	9.42	9.42	-4.29	-59.8
45	195	-4914	97	-483	0	456	130	6.28	6.28	9.42	9.42	-4.55	-63.0
46	195	-5002	86	-698	0	382	131	6.28	6.28	9.42	9.42	-4.26	-59.5
47	195	-4934	87	-663	0	383	130	6.28	6.28	9.42	9.42	-4.23	-59.0
49	195	-4974	107	-686	0	375	125	6.28	6.28	9.42	9.42	-4.21	-58.9
50	195	-4902	67	-655	0	386	135	6.28	6.28	9.42	9.42	-4.22	-59.0
51	195	-4896	90	-609	0	398	130	6.28	6.28	9.42	9.42	-4.28	-59.6

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	292	-4962	138	-907	0	1240	253	6.28	6.28	9.42	9.42	-9.55	-121.8
41	292	-4837	80	-837	0	1194	210	6.28	6.28	9.42	9.42	-9.20	-117.5
42	292	-4722	87	-677	0	1083	217	6.28	6.28	9.42	9.42	-8.34	-107.6
43	292	-4874	181	-866	0	1188	285	6.28	6.28	9.42	9.42	-9.15	-117.0
44	292	-4513	-18	-712	0	1087	138	6.28	6.28	9.42	9.42	-8.37	-107.3
45	292	-4475	97	-483	0	926	224	6.28	6.28	9.42	9.42	-7.14	-93.4
46	292	-4563	86	-698	0	1062	214	6.28	6.28	9.42	9.42	-8.17	-105.3
47	292	-4495	87	-663	0	1029	215	6.28	6.28	9.42	9.42	-7.92	-102.2
49	292	-4536	107	-686	0	1044	230	6.28	6.28	9.42	9.42	-8.04	-103.6
50	292	-4464	67	-655	0	1024	201	6.28	6.28	9.42	9.42	-7.88	-101.7
51	292	-4457	90	-609	0	992	218	6.28	6.28	9.42	9.42	-7.64	-98.9

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	390	-4523	138	-907	0	2124	388	6.28	6.28	9.42	9.42	-16.55	360.2
41	390	-4398	80	-837	0	2010	288	6.28	6.28	9.42	9.42	-15.67	333.6
42	390	-4283	87	-677	0	1743	302	6.28	6.28	9.42	9.42	-13.59	261.4
43	390	-4435	181	-866	0	2032	461	6.28	6.28	9.42	9.42	-15.84	338.0
44	390	-4074	-18	-712	0	1781	120	6.28	6.28	9.42	9.42	-13.89	284.9
45	390	-4036	97	-483	0	1397	318	6.28	6.28	9.42	9.42	-10.86	175.9
46	390	-4124	86	-698	0	1742	298	6.28	6.28	9.42	9.42	-13.58	270.4
47	390	-4056	87	-663	0	1675	301	6.28	6.28	9.42	9.42	-13.06	254.7
49	390	-4097	107	-686	0	1713	334	6.28	6.28	9.42	9.42	-13.35	263.4
50	390	-4025	67	-655	0	1663	266	6.28	6.28	9.42	9.42	-12.96	253.0
51	390	-4018	90	-609	0	1586	306	6.28	6.28	9.42	9.42	-12.36	230.9

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 57 NI 142 NF 123 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 18B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	

40	0	-10760	44	-1046	0	-1077	-165	6.28	6.28	12.57	12.57	-8.01	-110.6
41	0	-10780	-88	-1062	0	-1106	127	6.28	6.28	12.57	12.57	-8.12	-112.0
42	0	-10830	-79	-1122	0	-1223	109	6.28	6.28	12.57	12.57	-8.57	-117.5
43	0	-10470	138	-972	0	-967	-373	6.28	6.28	12.57	12.57	-7.51	-104.0
44	0	-10560	-310	-1051	0	-1121	616	6.28	6.28	12.57	12.57	-8.09	-111.4
45	0	-10590	-66	-1098	0	-1210	83	6.28	6.28	12.57	12.57	-8.43	-115.6
46	0	-10340	-77	-960	0	-960	104	6.28	6.28	12.57	12.57	-7.43	-102.9
47	0	-10230	-74	-934	0	-924	99	6.28	6.28	12.57	12.57	-7.26	-100.6
49	0	-10230	-30	-929	0	-914	2	6.28	6.28	12.57	12.57	-7.23	-100.2
50	0	-10240	-120	-945	0	-945	200	6.28	6.28	12.57	12.57	-7.34	-101.6
51	0	-10250	-71	-954	0	-963	93	6.28	6.28	12.57	12.57	-7.41	-102.5

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	97	-10174	44	-1046	0	-57	-122	6.28	6.28	12.57	12.57	-4.27	-61.8
41	97	-10194	-88	-1062	0	-70	41	6.28	6.28	12.57	12.57	-4.19	-62.2
42	97	-10244	-79	-1122	0	-129	32	6.28	6.28	12.57	12.57	-4.42	-65.1
43	97	-9886	138	-972	0	-20	-238	6.28	6.28	12.57	12.57	-4.74	-66.6
44	97	-9974	-310	-1051	0	-96	314	6.28	6.28	12.57	12.57	-5.14	-71.3
45	97	-10005	-66	-1098	0	-140	18	6.28	6.28	12.57	12.57	-4.36	-64.2
46	97	-9756	-77	-960	0	-24	29	6.28	6.28	12.57	12.57	-3.86	-57.6
47	97	-9646	-74	-934	0	-13	26	6.28	6.28	12.57	12.57	-3.77	-56.5
49	97	-9644	-30	-929	0	-9	-28	6.28	6.28	12.57	12.57	-3.76	-56.3
50	97	-9656	-120	-945	0	-24	82	6.28	6.28	12.57	12.57	-3.88	-57.0
51	97	-9665	-71	-954	0	-33	23	6.28	6.28	12.57	12.57	-3.85	-57.5

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	195	-9588	44	-1046	0	964	-80	6.28	6.28	12.57	12.57	-7.15	-98.7
41	195	-9608	-88	-1062	0	966	-46	6.28	6.28	12.57	12.57	-7.17	-98.9
42	195	-9658	-79	-1122	0	965	-46	6.28	6.28	12.57	12.57	-7.19	-99.2
43	195	-9302	138	-972	0	927	-103	6.28	6.28	12.57	12.57	-6.91	-95.4
44	195	-9388	-310	-1051	0	928	12	6.28	6.28	12.57	12.57	-6.95	-96.0
45	195	-9420	-66	-1098	0	931	-46	6.28	6.28	12.57	12.57	-6.97	-96.3
46	195	-9172	-77	-960	0	911	-46	6.28	6.28	12.57	12.57	-6.81	-93.9
47	195	-9062	-74	-934	0	898	-46	6.28	6.28	12.57	12.57	-6.71	-92.7
49	195	-9059	-30	-929	0	897	-58	6.28	6.28	12.57	12.57	-6.71	-92.6
50	195	-9072	-120	-945	0	897	-35	6.28	6.28	12.57	12.57	-6.72	-92.7
51	195	-9080	-71	-954	0	898	-46	6.28	6.28	12.57	12.57	-6.72	-92.8

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	292	-9003	44	-1046	0	1984	-38	6.28	6.28	12.57	12.57	-12.24	-157.6
41	292	-9022	-88	-1062	0	2001	-132	6.28	6.28	12.57	12.57	-12.35	-158.9
42	292	-9072	-79	-1122	0	2059	-123	6.28	6.28	12.57	12.57	-12.73	-163.2
43	292	-8718	138	-972	0	1875	32	6.28	6.28	12.57	12.57	-11.55	-149.2
44	292	-8801	-310	-1051	0	1953	-290	6.28	6.28	12.57	12.57	-12.05	-155.1
45	292	-8834	-66	-1098	0	2002	-111	6.28	6.28	12.57	12.57	-12.37	-158.7
46	292	-8587	-77	-960	0	1847	-121	6.28	6.28	12.57	12.57	-11.38	-147.0
47	292	-8478	-74	-934	0	1808	-119	6.28	6.28	12.57	12.57	-11.13	-144.1
49	292	-8474	-30	-929	0	1802	-87	6.28	6.28	12.57	12.57	-11.09	-143.6
50	292	-8488	-120	-945	0	1818	-152	6.28	6.28	12.57	12.57	-11.19	-144.8
51	292	-8496	-71	-954	0	1828	-116	6.28	6.28	12.57	12.57	-11.26	-145.5

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	390	-8417	44	-1046	0	3004	5	6.28	6.28	12.57	12.57	-19.42	375.7
41	390	-8436	-88	-1062	0	3037	-218	6.28	6.28	12.57	12.57	-19.64	383.9
42	390	-8486	-79	-1122	0	3153	-200	6.28	6.28	12.57	12.57	-20.44	413.7
43	390	-8134	138	-972	0	2822	166	6.28	6.28	12.57	12.57	-18.20	340.5
44	390	-8215	-310	-1051	0	2978	-592	6.28	6.28	12.57	12.57	-19.27	379.6
45	390	-8249	-66	-1098	0	3072	-176	6.28	6.28	12.57	12.57	-19.92	404.2
46	390	-8003	-77	-960	0	2783	-197	6.28	6.28	12.57	12.57	-17.95	336.8
47	390	-7894	-74	-934	0	2719	-191	6.28	6.28	12.57	12.57	-17.53	325.0
49	390	-7888	-30	-929	0	2708	-117	6.28	6.28	12.57	12.57	-17.45	322.3
50	390	-7904	-120	-945	0	2739	-269	6.28	6.28	12.57	12.57	-17.66	330.0
51	390	-7911	-71	-954	0	2758	-186	6.28	6.28	12.57	12.57	-17.79	334.9

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 58 NI 211 NF 212 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 13B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-10200	111	-1121	0	-1353	-199	6.28	6.28	9.42	9.42	-11.38	-155.0
41	0	-10180	37	-1093	0	-1295	-47	6.28	6.28	9.42	9.42	-11.07	-151.1
42	0	-10270	38	-1196	0	-1498	-50	6.28	6.28	9.42	9.42	-12.21	-165.2
43	0	-9928	165	-1057	0	-1262	-307	6.28	6.28	9.42	9.42	-10.79	-147.3
44	0	-9895	-89	-1016	0	-1175	207	6.28	6.28	9.42	9.42	-10.35	-141.8
45	0	-10050	43	-1182	0	-1504	-59	6.28	6.28	9.42	9.42	-12.17	-164.3
46	0	-9722	42	-960	0	-1086	-58	6.28	6.28	9.42	9.42	-9.84	-135.3
47	0	-9609	44	-927	0	-1034	-61	6.28	6.28	9.42	9.42	-9.55	-131.4
49	0	-9616	68	-936	0	-1053	-112	6.28	6.28	9.42	9.42	-9.64	-132.6
50	0	-9609	18	-928	0	-1036	-9	6.28	6.28	9.42	9.42	-9.56	-131.5
51	0	-9641	44	-961	0	-1102	-62	6.28	6.28	9.42	9.42	-9.88	-135.6

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	97	-9760	111	-1121	0	-260	-90	6.28	6.28	9.42	9.42	-6.09	-88.4
41	97	-9740	37	-1093	0	-229	-11	6.28	6.28	9.42	9.42	-5.94	-86.5
42	97	-9832	38	-1196	0	-332	-13	6.28	6.28	9.42	9.42	-6.46	-93.1
43	97	-9489	165	-1057	0	-231	-147	6.28	6.28	9.42	9.42	-5.90	-84.8
44	97	-9456	-89	-1016	0	-184	121	6.28	6.28	9.42	9.42	-5.65	-81.8
45	97	-9612	43	-1182	0	-351	-17	6.28	6.28	9.42	9.42	-6.44	-92.5
46	97	-9283	42	-960	0	-150	-17	6.28	6.28	9.42	9.42	-5.35	-78.6
47	97	-9170	44	-927	0	-130	-18	6.28	6.28	9.42	9.42	-5.21	-76.6
49	97	-9177	68	-936	0	-140	-45	6.28	6.28	9.42	9.42	-5.25	-77.2
50	97	-9170	18	-928	0	-131	9	6.28	6.28	9.42	9.42	-5.21	-76.6
51	97	-9202	44	-961	0	-164	-19	6.28	6.28	9.42	9.42	-5.38	-78.8

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	195	-9321	111	-1121	0	834	18	6.28	6.28	9.42	9.42	-8.49	-117.8
41	195	-9300	37	-1093	0	836	24	6.28	6.28	9.42	9.42	-8.49	-117.8
42	195	-9394	38	-1196	0	835	24	6.28	6.28	9.42	9.42	-8.53	-118.5
43	195	-9050	165	-1057	0	800	14	6.28	6.28	9.42	9.42	-8.20	-113.8
44	195	-9018	-89	-1016	0	806	34	6.28	6.28	9.42	9.42	-8.21	-114.0
45	195	-9174	43	-1182	0	802	24	6.28	6.28	9.42	9.42	-8.27	-114.9
46	195	-8844	42	-960	0	786	24	6.28	6.28	9.42	9.42	-8.03	-111.5
47	195	-8732	44	-927	0	774	24	6.28	6.28	9.42	9.42	-7.92	-110.0
49	195	-8738	68	-936	0	772	22	6.28	6.28	9.42	9.42	-7.92	-110.0
50	195	-8732	18	-928	0	774	26	6.28	6.28	9.42	9.42	-7.92	-110.0
51	195	-8764	44	-961	0	773	24	6.28	6.28	9.42	9.42	-7.93	-110.2

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	292	-8882	111	-1121	0	1927	127	6.28	6.28	9.42	9.42	-14.84	-192.8
41	292	-8861	37	-1093	0	1902	60	6.28	6.28	9.42	9.42	-14.65	-190.7
42	292	-8955	38	-1196	0	2002	62	6.28	6.28	9.42	9.42	-15.41	-199.4
43	292	-8612	165	-1057	0	1830	175	6.28	6.28	9.42	9.42	-14.10	-183.7
44	292	-8579	-89	-1016	0	1797	-52	6.28	6.28	9.42	9.42	-13.85	-180.8
45	292	-8736	43	-1182	0	1954	66	6.28	6.28	9.42	9.42	-15.04	-194.7
46	292	-8406	42	-960	0	1722	65	6.28	6.28	9.42	9.42	-13.29	-173.9
47	292	-8293	44	-927	0	1677	67	6.28	6.28	9.42	9.42	-12.95	-169.7
49	292	-8300	68	-936	0	1685	89	6.28	6.28	9.42	9.42	-13.01	-170.4
50	292	-8293	18	-928	0	1679	44	6.28	6.28	9.42	9.42	-12.96	-169.9
51	292	-8325	44	-961	0	1710	67	6.28	6.28	9.42	9.42	-13.19	-172.6

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	390	-8442	111	-1121	0	3020	235	6.28	6.28	9.42	9.42	-23.50	395.4
41	390	-8421	37	-1093	0	2968	96	6.28	6.28	9.42	9.42	-23.09	381.9
42	390	-8517	38	-1196	0	3168	99	6.28	6.28	9.42	9.42	-24.67	433.4
43	390	-8173	165	-1057	0	2861	335	6.28	6.28	9.42	9.42	-22.26	365.1
44	390	-8140	-89	-1016	0	2788	-138	6.28	6.28	9.42	9.42	-21.68	346.5
45	390	-8298	43	-1182	0	3107	108	6.28	6.28	9.42	9.42	-24.20	428.1
46	390	-7967	42	-960	0	2658	106	6.28	6.28	9.42	9.42	-20.65	319.5
47	390	-7854	44	-927	0	2581	109	6.28	6.28	9.42	9.42	-20.05	304.2
49	390	-7861	68	-936	0	2598	156	6.28	6.28	9.42	9.42	-20.18	308.5
50	390	-7854	18	-928	0	2584	61	6.28	6.28	9.42	9.42	-20.07	305.0
51	390	-7886	44	-961	0	2648	110	6.28	6.28	9.42	9.42	-20.58	321.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 59 NI 213 NF 214 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 8B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-5833	-27	-596	0	-743	-96	6.28	6.28	9.42	9.42	-6.35	-86.7
41	0	-5855	-88	-534	0	-604	41	6.28	6.28	9.42	9.42	-5.70	-78.6

42	0	-5914	-86	-598	0	-746	37	6.28	6.28	9.42	9.42	-6.40	-87.4
43	0	-5684	16	-603	0	-782	-192	6.28	6.28	9.42	9.42	-6.50	-88.3
44	0	-5774	-190	-417	0	-364	272	6.28	6.28	9.42	9.42	-5.27	-66.5
45	0	-5818	-83	-607	0	-787	31	6.28	6.28	9.42	9.42	-6.57	-89.4
46	0	-5640	-84	-480	0	-518	34	6.28	6.28	9.42	9.42	-5.20	-72.1
47	0	-5586	-83	-467	0	-496	32	6.28	6.28	9.42	9.42	-5.07	-70.4
49	0	-5579	-63	-487	0	-543	-13	6.28	6.28	9.42	9.42	-5.28	-73.0
50	0	-5597	-104	-450	0	-459	79	6.28	6.28	9.42	9.42	-4.91	-68.4
51	0	-5606	-83	-488	0	-544	31	6.28	6.28	9.42	9.42	-5.30	-73.3

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	97	-5394	-27	-596	0	-162	-122	6.28	6.28	9.42	9.42	-3.71	-50.1
41	97	-5416	-88	-534	0	-83	-45	6.28	6.28	9.42	9.42	-3.10	-45.6
42	97	-5475	-86	-598	0	-163	-47	6.28	6.28	9.42	9.42	-3.50	-50.6
43	97	-5245	16	-603	0	-194	-176	6.28	6.28	9.42	9.42	-4.14	-54.0
44	97	-5335	-190	-417	0	42	86	6.28	6.28	9.42	9.42	-3.36	-46.4
45	97	-5379	-83	-607	0	-195	-50	6.28	6.28	9.42	9.42	-3.59	-51.7
46	97	-5201	-84	-480	0	-49	-48	6.28	6.28	9.42	9.42	-2.94	-42.1
47	97	-5147	-83	-467	0	-41	-49	6.28	6.28	9.42	9.42	-2.92	-41.6
49	97	-5140	-63	-487	0	-67	-75	6.28	6.28	9.42	9.42	-3.16	-43.9
50	97	-5158	-104	-450	0	-20	-22	6.28	6.28	9.42	9.42	-2.69	-40.1
51	97	-5167	-83	-488	0	-68	-50	6.28	6.28	9.42	9.42	-2.94	-42.8

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	195	-4956	-27	-596	0	418	-148	6.28	6.28	9.42	9.42	-4.40	-61.2
41	195	-4978	-88	-534	0	437	-130	6.28	6.28	9.42	9.42	-4.50	-62.5
42	195	-5036	-86	-598	0	421	-130	6.28	6.28	9.42	9.42	-4.45	-62.0
43	195	-4806	16	-603	0	394	-161	6.28	6.28	9.42	9.42	-4.21	-58.7
44	195	-4896	-190	-417	0	449	-99	6.28	6.28	9.42	9.42	-4.51	-62.5
45	195	-4940	-83	-607	0	398	-131	6.28	6.28	9.42	9.42	-4.30	-59.9
46	195	-4762	-84	-480	0	419	-130	6.28	6.28	9.42	9.42	-4.30	-59.8
47	195	-4708	-83	-467	0	414	-130	6.28	6.28	9.42	9.42	-4.26	-59.1
49	195	-4702	-63	-487	0	408	-136	6.28	6.28	9.42	9.42	-4.22	-58.7
50	195	-4720	-104	-450	0	419	-124	6.28	6.28	9.42	9.42	-4.28	-59.5
51	195	-4728	-83	-488	0	408	-131	6.28	6.28	9.42	9.42	-4.24	-58.9

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	292	-4517	-27	-596	0	999	-174	6.28	6.28	9.42	9.42	-7.69	-99.7
41	292	-4539	-88	-534	0	958	-215	6.28	6.28	9.42	9.42	-7.38	-96.2
42	292	-4598	-86	-598	0	1004	-214	6.28	6.28	9.42	9.42	-7.73	-100.4
43	292	-4368	16	-603	0	982	-145	6.28	6.28	9.42	9.42	-7.56	-97.8
44	292	-4458	-190	-417	0	856	-284	6.28	6.28	9.42	9.42	-6.63	-87.4
45	292	-4502	-83	-607	0	990	-212	6.28	6.28	9.42	9.42	-7.62	-98.9
46	292	-4324	-84	-480	0	887	-213	6.28	6.28	9.42	9.42	-6.84	-89.5
47	292	-4270	-83	-467	0	869	-212	6.28	6.28	9.42	9.42	-6.71	-87.8
49	292	-4263	-63	-487	0	883	-198	6.28	6.28	9.42	9.42	-6.81	-89.0
50	292	-4281	-104	-450	0	857	-226	6.28	6.28	9.42	9.42	-6.62	-86.9
51	292	-4290	-83	-488	0	884	-211	6.28	6.28	9.42	9.42	-6.82	-89.2

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	390	-4078	-27	-596	0	1580	-200	6.28	6.28	9.42	9.42	-12.31	225.7
41	390	-4100	-88	-534	0	1478	-301	6.28	6.28	9.42	9.42	-11.50	195.2
42	390	-4159	-86	-598	0	1587	-298	6.28	6.28	9.42	9.42	-12.36	223.1
43	390	-3929	16	-603	0	1570	-130	6.28	6.28	9.42	9.42	-12.24	231.3
44	390	-4019	-190	-417	0	1262	-469	6.28	6.28	9.42	9.42	-9.79	139.8
45	390	-4063	-83	-607	0	1582	-292	6.28	6.28	9.42	9.42	-12.33	227.1
46	390	-3885	-84	-480	0	1355	-295	6.28	6.28	9.42	9.42	-10.54	172.2
47	390	-3831	-83	-467	0	1324	-293	6.28	6.28	9.42	9.42	-10.30	166.4
49	390	-3824	-63	-487	0	1358	-260	6.28	6.28	9.42	9.42	-10.57	176.3
50	390	-3842	-104	-450	0	1296	-328	6.28	6.28	9.42	9.42	-10.07	158.0
51	390	-3851	-83	-488	0	1360	-292	6.28	6.28	9.42	9.42	-10.58	175.4

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 60 NI 292 NF 302 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 1C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-13060	104	-433	0	1032	254	6.28	6.28	9.42	9.42	-11.27	-157.3
41	0	-13290	-40	-342	0	905	-180	6.28	6.28	9.42	9.42	-10.81	-151.8
42	0	-13050	-38	-102	0	715	-176	6.28	6.28	9.42	9.42	-9.82	-139.2
43	0	-12030	183	-449	0	1023	508	6.28	6.28	9.42	9.42	-10.72	-149.1
44	0	-13800	-276	-199	0	710	-894	6.28	6.28	9.42	9.42	-15.00	-182.7
45	0	-12010	-55	104	0	495	-208	6.28	6.28	9.42	9.42	-8.30	-118.8
46	0	-11870	-68	-270	0	755	-236	6.28	6.28	9.42	9.42	-9.41	-132.6
47	0	-11520	-75	-253	0	718	-250	6.28	6.28	9.42	9.42	-9.07	-127.8
49	0	-11450	-27	-283	0	760	-105	6.28	6.28	9.42	9.42	-9.22	-129.7
50	0	-11800	-118	-233	0	698	-386	6.28	6.28	9.42	9.42	-9.21	-128.8
51	0	-11440	-74	-172	0	654	-248	6.28	6.28	9.42	9.42	-8.74	-123.6

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	12	-13005	85	-433	0	1086	266	6.28	6.28	9.42	9.42	-11.49	-160.0
41	12	-13232	-40	-342	0	948	-185	6.28	6.28	9.42	9.42	-10.98	-153.8
42	12	-12992	-38	-91	0	727	-181	6.28	6.28	9.42	9.42	-9.85	-139.4
43	12	-11972	151	-449	0	1079	529	6.28	6.28	9.42	9.42	-10.94	-151.8
44	12	-13742	-244	-199	0	734	-927	6.28	6.28	9.42	9.42	-15.35	-185.7
45	12	-11952	-55	122	0	480	-215	6.28	6.28	9.42	9.42	-8.20	-117.6
46	12	-11815	-68	-270	0	789	-244	6.28	6.28	9.42	9.42	-9.54	-134.1
47	12	-11465	-75	-253	0	749	-259	6.28	6.28	9.42	9.42	-9.18	-129.2
49	12	-11392	-33	-283	0	795	-109	6.28	6.28	9.42	9.42	-9.36	-131.3
50	12	-11742	-112	-233	0	727	-400	6.28	6.28	9.42	9.42	-9.31	-130.0
51	12	-11385	-74	-169	0	676	-257	6.28	6.28	9.42	9.42	-8.81	-124.4

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	25	-12950	66	-433	0	1140	275	6.28	6.28	9.42	9.42	-11.71	-162.7
41	25	-13175	-40	-342	0	990	-190	6.28	6.28	9.42	9.42	-11.14	-155.8
42	25	-12935	-38	-81	0	737	-186	6.28	6.28	9.42	9.42	-9.87	-139.6

43	25	-11915	119	-449	0	1135	546	6.28	6.28	9.42	9.42	-11.17	-154.6
44	25	-13685	-212	-199	0	759	-956	6.28	6.28	9.42	9.42	-15.66	-188.5
45	25	-11895	-55	138	0	464	-222	6.28	6.28	9.42	9.42	-8.10	-116.2
46	25	-11760	-68	-270	0	823	-253	6.28	6.28	9.42	9.42	-9.67	-135.6
47	25	-11410	-75	-253	0	781	-268	6.28	6.28	9.42	9.42	-9.30	-130.6
49	25	-11335	-39	-283	0	831	-113	6.28	6.28	9.42	9.42	-9.49	-132.9
50	25	-11685	-106	-233	0	756	-414	6.28	6.28	9.42	9.42	-9.41	-131.2
51	25	-11330	-74	-165	0	697	-267	6.28	6.28	9.42	9.42	-8.88	-125.2

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	38	-12895	47	-433	0	1194	282	6.28	6.28	9.42	9.42	-11.93	-165.3
41	38	-13118	-40	-342	0	1033	-195	6.28	6.28	9.42	9.42	-11.31	-157.9
42	38	-12878	-38	-73	0	747	-190	6.28	6.28	9.42	9.42	-9.88	-139.7
43	38	-11858	88	-449	0	1191	559	6.28	6.28	9.42	9.42	-11.39	-157.3
44	38	-13628	-180	-199	0	784	-980	6.28	6.28	9.42	9.42	-15.94	-190.8
45	38	-11838	-55	151	0	446	-228	6.28	6.28	9.42	9.42	-7.99	-114.7
46	38	-11705	-68	-270	0	857	-261	6.28	6.28	9.42	9.42	-9.79	-137.1
47	38	-11355	-75	-253	0	813	-278	6.28	6.28	9.42	9.42	-9.42	-132.0
49	38	-11278	-46	-283	0	866	-119	6.28	6.28	9.42	9.42	-9.62	-134.5
50	38	-11628	-99	-233	0	785	-426	6.28	6.28	9.42	9.42	-9.50	-132.5
51	38	-11275	-74	-163	0	717	-276	6.28	6.28	9.42	9.42	-8.94	-125.9

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	50	-12840	28	-433	0	1248	287	6.28	6.28	9.42	9.42	-12.15	-168.0
41	50	-13060	-40	-342	0	1076	-200	6.28	6.28	9.42	9.42	-11.47	-159.9
42	50	-12820	-38	-67	0	756	-195	6.28	6.28	9.42	9.42	-9.89	-139.8
43	50	-11800	56	-449	0	1247	568	6.28	6.28	9.42	9.42	-11.62	-160.1
44	50	-13570	-149	-199	0	809	-1001	6.28	6.28	9.42	9.42	-16.17	-192.8
45	50	-11780	-55	162	0	426	-235	6.28	6.28	9.42	9.42	-7.87	-113.2
46	50	-11650	-68	-270	0	890	-270	6.28	6.28	9.42	9.42	-9.92	-138.6
47	50	-11300	-75	-253	0	844	-287	6.28	6.28	9.42	9.42	-9.53	-133.4
49	50	-11220	-52	-283	0	902	-125	6.28	6.28	9.42	9.42	-9.75	-136.0
50	50	-11570	-93	-233	0	814	-438	6.28	6.28	9.42	9.42	-9.58	-133.7
51	50	-11220	-74	-161	0	737	-285	6.28	6.28	9.42	9.42	-9.01	-126.7

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 61 NI 294 NF 325 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 10C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-12760	1376	-250	0	-2406	1314	6.28	6.28	12.57	12.57	-14.79	-194.5
41	0	-11260	-412	-143	0	-1928	2053	6.28	6.28	12.57	12.57	-16.80	-193.3
42	0	-11240	-434	-503	0	-1414	2054	6.28	6.28	12.57	12.57	-16.80	-193.3
43	0	-13420	2649	-287	0	-2275	692	6.28	6.28	12.57	12.57	-14.09	-187.7
44	0	-9105	-3414	28	0	-1220	3297	6.28	6.28	12.57	12.57	-26.62	515.3
45	0	-10880	-367	-709	0	-621	1927	6.28	6.28	12.57	12.57	-15.77	-182.6
46	0	-10730	-282	-87	0	-1210	1847	6.28	6.28	12.57	12.57	-15.13	-176.1
47	0	-10590	-249	-73	0	-1030	1796	6.28	6.28	12.57	12.57	-14.71	-171.8
49	0	-11090	347	-109	0	-1189	1549	6.28	6.28	12.57	12.57	-12.80	-155.0
50	0	-10230	-866	-46	0	-978	2070	6.28	6.28	12.57	12.57	-16.91	-190.6
51	0	-10580	-256	-193	0	-858	1796	6.28	6.28	12.57	12.57	-14.71	-171.8

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	12	-12685	1376	-250	0	-2375	1486	6.28	6.28	12.57	12.57	-14.60	-192.2
41	12	-11185	-412	-143	0	-1910	2002	6.28	6.28	12.57	12.57	-16.38	-189.2
42	12	-11165	-434	-481	0	-1353	2000	6.28	6.28	12.57	12.57	-16.37	-189.0
43	12	-13345	2649	-287	0	-2239	1024	6.28	6.28	12.57	12.57	-13.89	-185.1
44	12	-9030	-3414	28	0	-1224	2870	6.28	6.28	12.57	12.57	-23.26	412.4
45	12	-10805	-367	-672	0	-535	1881	6.28	6.28	12.57	12.57	-15.40	-178.9
46	12	-10655	-282	-87	0	-1199	1812	6.28	6.28	12.57	12.57	-14.84	-173.2
47	12	-10515	-249	-73	0	-1021	1765	6.28	6.28	12.57	12.57	-14.46	-169.2
49	12	-11015	347	-109	0	-1176	1592	6.28	6.28	12.57	12.57	-13.13	-158.0
50	12	-10155	-866	-46	0	-972	1962	6.28	6.28	12.57	12.57	-16.04	-182.4
51	12	-10505	-256	-186	0	-835	1764	6.28	6.28	12.57	12.57	-14.45	-169.1

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	25	-12610	1376	-250	0	-2344	1658	6.28	6.28	12.57	12.57	-14.41	-189.9
41	25	-11110	-412	-143	0	-1892	1950	6.28	6.28	12.57	12.57	-15.96	-185.1
42	25	-11090	-434	-462	0	-1294	1946	6.28	6.28	12.57	12.57	-15.93	-184.8
43	25	-13270	2649	-287	0	-2203	1355	6.28	6.28	12.57	12.57	-13.68	-182.6
44	25	-8955	-3414	28	0	-1227	2444	6.28	6.28	12.57	12.57	-19.87	311.1
45	25	-10730	-367	-640	0	-453	1836	6.28	6.28	12.57	12.57	-15.03	-175.2
46	25	-10580	-282	-87	0	-1188	1776	6.28	6.28	12.57	12.57	-14.56	-170.3
47	25	-10440	-249	-73	0	-1012	1734	6.28	6.28	12.57	12.57	-14.21	-166.6
49	25	-10940	347	-109	0	-1162	1636	6.28	6.28	12.57	12.57	-13.46	-161.0
50	25	-10080	-866	-46	0	-967	1854	6.28	6.28	12.57	12.57	-15.17	-174.2
51	25	-10430	-256	-179	0	-812	1732	6.28	6.28	12.57	12.57	-14.20	-166.5

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	38	-12535	1376	-250	0	-2312	1830	6.28	6.28	12.57	12.57	-15.08	-187.6
41	38	-11035	-412	-143	0	-1875	1898	6.28	6.28	12.57	12.57	-15.55	-181.0
42	38	-11015	-434	-446	0	-1237	1892	6.28	6.28	12.57	12.57	-15.50	-180.5
43	38	-13195	2649	-287	0	-2167	1686	6.28	6.28	12.57	12.57	-14.04	-180.1
44	38	-8880	-3414	28	0	-1230	2017	6.28	6.28	12.57	12.57	-16.45	212.8
45	38	-10655	-367	-614	0	-375	1790	6.28	6.28	12.57	12.57	-14.67	-171.6
46	38	-10505	-282	-87	0	-1177	1741	6.28	6.28	12.57	12.57	-14.27	-167.4
47	38	-10365	-249	-73	0	-1003	1702	6.28	6.28	12.57	12.57	-13.96	-164.0
49	38	-10865	347	-109	0	-1148	1680	6.28	6.28	12.57	12.57	-13.80	-164.0
50	38	-10004	-866	-46	0	-961	1746	6.28	6.28	12.57	12.57	-14.30	-166.0
51	38	-10355	-256	-174	0	-790	1700	6.28	6.28	12.57	12.57	-13.94	-163.8

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	50	-12460	1376	-250	0	-2281	2002	6.28	6.28	12.57	12.57	-16.43	-193.8
41	50	-10960	-412	-143	0	-1857	1847	6.28	6.28	12.57	12.57	-15.13	-176.9
42	50	-10940	-434	-434	0	-1182	1838	6.28	6.28	12.57	12.57	-15.06	-176.2
43	50	-13120	2649	-287	0	-2131	2017	6.28	6.28	12.57	12.57	-16.58	-197.3

44	50	-8805	-3414	28	0	-1234	1590	6.28	6.28	12.57	12.57	-13.01	-150.0
45	50	-10580	-367	-593	0	-300	1744	6.28	6.28	12.57	12.57	-14.30	-167.9
46	50	-10430	-282	-87	0	-1166	1706	6.28	6.28	12.57	12.57	-13.99	-164.5
47	50	-10290	-249	-73	0	-994	1671	6.28	6.28	12.57	12.57	-13.71	-161.4
49	50	-10790	347	-109	0	-1135	1723	6.28	6.28	12.57	12.57	-14.14	-167.1
50	50	-9929	-866	-46	0	-955	1638	6.28	6.28	12.57	12.57	-13.43	-157.6
51	50	-10280	-256	-170	0	-768	1668	6.28	6.28	12.57	12.57	-13.68	-161.1

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 62 NI 1543 NF 1542 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 6
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-4508	645	-526	0	-310	4700	15.71	15.71	9.42	9.42	-15.77	506.9
41	0	-395	202	-714	0	-439	6671	15.71	15.71	9.42	9.42	-21.22	1002.1
42	0	-700	215	-950	0	-452	6472	15.71	15.71	9.42	9.42	-20.67	956.7
43	0	-8509	885	-247	0	-124	2007	15.71	15.71	9.42	9.42	-6.72	-92.2
44	0	6616	-526	-1055	0	-671	10190	15.71	15.71	9.42	9.42	-29.70	1892.5
45	0	-2162	170	-954	0	-360	4960	15.71	15.71	9.42	9.42	-16.24	654.9
46	0	-2409	116	-470	0	-279	4464	15.71	15.71	9.42	9.42	-14.71	567.5
47	0	-2912	94	-408	0	-239	3912	15.71	15.71	9.42	9.42	-13.02	460.1
49	0	-4283	242	-346	0	-196	3255	15.71	15.71	9.42	9.42	-11.00	300.4
50	0	-1259	-41	-507	0	-305	4891	15.71	15.71	9.42	9.42	-15.81	687.6
51	0	-3014	98	-487	0	-243	3846	15.71	15.71	9.42	9.42	-12.82	445.4

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	12	-4408	645	-526	0	-245	4780	15.71	15.71	9.42	9.42	-16.02	523.6
41	12	-295	202	-714	0	-350	6696	15.71	15.71	9.42	9.42	-21.27	1010.9
42	12	-600	215	-950	0	-333	6499	15.71	15.71	9.42	9.42	-20.73	965.8
43	12	-8409	885	-247	0	-93	2118	15.71	15.71	9.42	9.42	-7.04	-96.1
44	12	6716	-526	-1055	0	-539	10123	15.71	15.71	9.42	9.42	-29.44	1887.4
45	12	-2062	170	-954	0	-241	4981	15.71	15.71	9.42	9.42	-16.29	662.9
46	12	-2309	116	-470	0	-220	4478	15.71	15.71	9.42	9.42	-14.73	574.4
47	12	-2812	94	-408	0	-188	3924	15.71	15.71	9.42	9.42	-13.04	466.5
49	12	-4183	242	-346	0	-153	3285	15.71	15.71	9.42	9.42	-11.10	309.2
50	12	-1159	-41	-507	0	-242	4886	15.71	15.71	9.42	9.42	-15.77	691.7
51	12	-2914	98	-487	0	-182	3858	15.71	15.71	9.42	9.42	-12.85	451.8

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	25	-4308	645	-526	0	-179	4861	15.71	15.71	9.42	9.42	-16.27	540.2
41	25	-195	202	-714	0	-261	6722	15.71	15.71	9.42	9.42	-21.32	1019.7
42	25	-500	215	-950	0	-215	6526	15.71	15.71	9.42	9.42	-20.79	974.8
43	25	-8309	885	-247	0	-62	2228	15.71	15.71	9.42	9.42	-7.38	-100.2
44	25	6816	-526	-1055	0	-408	10056	15.71	15.71	9.42	9.42	-29.18	1882.4
45	25	-1962	170	-954	0	-122	5002	15.71	15.71	9.42	9.42	-16.33	670.9
46	25	-2209	116	-470	0	-162	4493	15.71	15.71	9.42	9.42	-14.76	581.4
47	25	-2712	94	-408	0	-137	3936	15.71	15.71	9.42	9.42	-13.07	472.9
49	25	-4083	242	-346	0	-109	3316	15.71	15.71	9.42	9.42	-11.19	318.0
50	25	-1059	-41	-507	0	-178	4881	15.71	15.71	9.42	9.42	-15.73	695.7
51	25	-2814	98	-487	0	-121	3870	15.71	15.71	9.42	9.42	-12.87	458.3

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	38	-4208	645	-526	0	-113	4942	15.71	15.71	9.42	9.42	-16.52	557.0
41	38	-95	202	-714	0	-172	6747	15.71	15.71	9.42	9.42	-21.37	1028.5
42	38	-400	215	-950	0	-96	6553	15.71	15.71	9.42	9.42	-20.84	983.8
43	38	-8209	885	-247	0	-32	2339	15.71	15.71	9.42	9.42	-7.73	-104.4
44	38	6916	-526	-1055	0	-276	9990	15.71	15.71	9.42	9.42	-28.92	1877.3
45	38	-1862	170	-954	0	-2	5024	15.71	15.71	9.42	9.42	-16.38	678.9
46	38	-2109	116	-470	0	-103	4508	15.71	15.71	9.42	9.42	-14.79	588.3
47	38	-2612	94	-408	0	-86	3947	15.71	15.71	9.42	9.42	-13.09	479.3
49	38	-3983	242	-346	0	-66	3346	15.71	15.71	9.42	9.42	-11.29	326.8
50	38	-959	-41	-507	0	-115	4876	15.71	15.71	9.42	9.42	-15.69	699.8
51	38	-2714	98	-487	0	-60	3883	15.71	15.71	9.42	9.42	-12.90	464.8

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	50	-4108	645	-526	0	-48	5022	15.71	15.71	9.42	9.42	-16.76	573.7
41	50	5	202	-714	0	-82	6772	15.71	15.71	9.42	9.42	-21.42	1037.2
42	50	-300	215	-950	0	23	6580	15.71	15.71	9.42	9.42	-20.90	992.9
43	50	-8109	885	-247	0	-1	2450	15.71	15.71	9.42	9.42	-8.10	-108.8
44	50	7016	-526	-1055	0	-144	9923	15.71	15.71	9.42	9.42	-28.65	1872.3
45	50	-1762	170	-954	0	117	5045	15.71	15.71	9.42	9.42	-16.42	687.0
46	50	-2009	116	-470	0	-44	4522	15.71	15.71	9.42	9.42	-14.81	595.3
47	50	-2512	94	-408	0	-35	3959	15.71	15.71	9.42	9.42	-13.11	485.7
49	50	-3883	242	-346	0	-23	3376	15.71	15.71	9.42	9.42	-11.38	335.6
50	50	-859	-41	-507	0	-52	4871	15.71	15.71	9.42	9.42	-15.65	703.9
51	50	-2614	98	-487	0	0	3895	15.71	15.71	9.42	9.42	-12.92	471.3

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 63 NI 1542 NF 78 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 6A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-9261	1917	-257	0	-48	6030	15.71	15.71	9.42	9.42	-20.41	501.5
41	0	-5313	1674	-152	0	-82	7688	15.71	15.71	9.42	9.42	-25.53	923.1
42	0	-5631	1670	-848	0	23	7507	15.71	15.71	9.42	9.42	-24.99	880.9
43	0	-12490	1725	-336	0	-1	3408	15.71	15.71	9.42	9.42	-11.27	-152.9
44	0	1291	1329	22	0	-144	10710	15.71	15.71	9.42	9.42	-33.46	1703.8
45	0	-6441	1313	-1322	0	117	5870	15.71	15.71	9.42	9.42	-19.77	597.2
46	0	-6269	1109	-167	0	-44	5261	15.71	15.71	9.42	9.42	-17.75	513.6
47	0	-6509	967	-171	0	-35	4654	15.71	15.71	9.42	9.42	-15.74	413.4

49	0	-7825	1048	-206	0	-23	4101	15.71	15.71	9.42	9.42	-13.86	281.6
50	0	-5068	969	-134	0	-52	5561	15.71	15.71	9.42	9.42	-18.63	611.7
51	0	-6615	966	-403	0	0	4594	15.71	15.71	9.42	9.42	-15.55	400.1

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	12	-9161	1917	-257	0	-15	6270	15.71	15.71	9.42	9.42	-21.22	540.6
41	12	-5213	1674	-152	0	-63	7897	15.71	15.71	9.42	9.42	-26.18	959.6
42	12	-5531	1670	-848	0	129	7716	15.71	15.71	9.42	9.42	-25.65	917.2
43	12	-12390	1725	-336	0	41	3624	15.71	15.71	9.42	9.42	-11.97	-161.3
44	12	1391	1329	22	0	-146	10875	15.71	15.71	9.42	9.42	-33.95	1734.0
45	12	-6341	1313	-1322	0	282	6034	15.71	15.71	9.42	9.42	-20.29	626.2
46	12	-6169	1109	-167	0	-23	5400	15.71	15.71	9.42	9.42	-18.20	538.6
47	12	-6409	967	-171	0	-13	4775	15.71	15.71	9.42	9.42	-16.14	435.4
49	12	-7725	1048	-206	0	3	4232	15.71	15.71	9.42	9.42	-14.31	303.8
50	12	-4968	969	-134	0	-35	5682	15.71	15.71	9.42	9.42	-19.01	634.6
51	12	-6515	966	-403	0	51	4714	15.71	15.71	9.42	9.42	-15.95	422.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	25	-9061	1917	-257	0	17	6510	15.71	15.71	9.42	9.42	-22.02	580.0
41	25	-5113	1674	-152	0	-44	8106	15.71	15.71	9.42	9.42	-26.84	996.1
42	25	-5431	1670	-848	0	235	7924	15.71	15.71	9.42	9.42	-26.30	953.6
43	25	-12290	1725	-336	0	83	3840	15.71	15.71	9.42	9.42	-12.70	-170.0
44	25	1491	1329	22	0	-149	11040	15.71	15.71	9.42	9.42	-34.44	1764.2
45	25	-6241	1313	-1322	0	447	6198	15.71	15.71	9.42	9.42	-20.82	655.3
46	25	-6069	1109	-167	0	-2	5538	15.71	15.71	9.42	9.42	-18.65	563.7
47	25	-6309	967	-171	0	8	4896	15.71	15.71	9.42	9.42	-16.54	457.5
49	25	-7625	1048	-206	0	28	4363	15.71	15.71	9.42	9.42	-14.76	326.2
50	25	-4868	969	-134	0	-18	5804	15.71	15.71	9.42	9.42	-19.39	657.5
51	25	-6415	966	-403	0	101	4835	15.71	15.71	9.42	9.42	-16.35	444.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	38	-8961	1917	-257	0	49	6749	15.71	15.71	9.42	9.42	-22.82	619.6
41	38	-5013	1674	-152	0	-25	8316	15.71	15.71	9.42	9.42	-27.49	1032.6
42	38	-5331	1670	-848	0	341	8133	15.71	15.71	9.42	9.42	-26.96	990.0
43	38	-12190	1725	-336	0	126	4055	15.71	15.71	9.42	9.42	-13.44	-178.8
44	38	1591	1329	22	0	-152	11205	15.71	15.71	9.42	9.42	-34.93	1794.5
45	38	-6141	1313	-1322	0	612	6362	15.71	15.71	9.42	9.42	-21.35	684.4
46	38	-5969	1109	-167	0	19	5676	15.71	15.71	9.42	9.42	-19.09	588.9
47	38	-6209	967	-171	0	30	5016	15.71	15.71	9.42	9.42	-16.94	479.7
49	38	-7525	1048	-206	0	54	4494	15.71	15.71	9.42	9.42	-15.21	348.8
50	38	-4768	969	-134	0	-1	5925	15.71	15.71	9.42	9.42	-19.77	680.4
51	38	-6315	966	-403	0	152	4956	15.71	15.71	9.42	9.42	-16.74	466.1

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	50	-8861	1917	-257	0	81	6989	15.71	15.71	9.42	9.42	-23.61	659.3
41	50	-4913	1674	-152	0	-6	8525	15.71	15.71	9.42	9.42	-28.14	1069.1
42	50	-5231	1670	-848	0	447	8342	15.71	15.71	9.42	9.42	-27.61	1026.4
43	50	-12090	1725	-336	0	168	4271	15.71	15.71	9.42	9.42	-14.20	-187.6
44	50	1691	1329	22	0	-155	11370	15.71	15.71	9.42	9.42	-35.42	1824.7
45	50	-6041	1313	-1322	0	778	6526	15.71	15.71	9.42	9.42	-21.87	713.7
46	50	-5869	1109	-167	0	39	5815	15.71	15.71	9.42	9.42	-19.54	614.2
47	50	-6109	967	-171	0	51	5137	15.71	15.71	9.42	9.42	-17.33	502.0
49	50	-7425	1048	-206	0	80	4625	15.71	15.71	9.42	9.42	-15.66	371.7
50	50	-4668	969	-134	0	16	6046	15.71	15.71	9.42	9.42	-20.15	703.4
51	50	-6215	966	-403	0	202	5076	15.71	15.71	9.42	9.42	-17.14	488.3

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 64 NI 1581 NF 121 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 5A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-5096	3168	250	0	-76	10760	15.71	15.71	9.42	9.42	-35.31	1401.5
41	0	292	3145	243	0	-88	13530	15.71	15.71	9.42	9.42	-42.70	2086.2
42	0	310	3158	-424	0	33	13540	15.71	15.71	9.42	9.42	-42.73	2088.7
43	0	-10480	2538	196	0	-47	6185	15.71	15.71	9.42	9.42	-20.94	475.2
44	0	9510	3218	236	0	-111	18610	15.71	15.71	9.42	9.42	-55.39	3325.3
45	0	-1475	2521	-928	0	133	10820	15.71	15.71	9.42	9.42	-34.65	1584.6
46	0	-2583	2112	148	0	-56	9152	15.71	15.71	9.42	9.42	-29.65	1275.7
47	0	-3302	1853	124	0	-48	8058	15.71	15.71	9.42	9.42	-26.34	1074.0
49	0	-5098	1861	126	0	-44	7137	15.71	15.71	9.42	9.42	-23.72	849.3
50	0	-1099	1997	134	0	-56	9621	15.71	15.71	9.42	9.42	-30.75	1419.4
51	0	-3296	1858	-98	0	-8	8064	15.71	15.71	9.42	9.42	-26.35	1075.2

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	12	-4996	3168	250	0	-107	11158	15.71	15.71	9.42	9.42	-36.56	1466.9
41	12	392	3145	243	0	-118	13922	15.71	15.71	9.42	9.42	-43.91	2151.3
42	12	410	3158	-424	0	86	13935	15.71	15.71	9.42	9.42	-43.95	2154.1
43	12	-10380	2538	196	0	-72	6502	15.71	15.71	9.42	9.42	-22.01	524.9
44	12	9610	3218	236	0	-140	19012	15.71	15.71	9.42	9.42	-56.64	3391.9
45	12	-1375	2521	-928	0	249	11135	15.71	15.71	9.42	9.42	-35.62	1637.7
46	12	-2483	2112	148	0	-74	9416	15.71	15.71	9.42	9.42	-30.46	1321.0
47	12	-3202	1853	124	0	-63	8290	15.71	15.71	9.42	9.42	-27.05	1114.2
49	12	-4998	1861	126	0	-59	7370	15.71	15.71	9.42	9.42	-24.45	889.2
50	12	-999	1997	134	0	-73	9871	15.71	15.71	9.42	9.42	-31.51	1462.5
51	12	-3196	1858	-98	0	5	8296	15.71	15.71	9.42	9.42	-27.07	1115.4

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	25	-4896	3168	250	0	-138	11555	15.71	15.71	9.42	9.42	-37.80	1532.4
41	25	492	3145	243	0	-148	14315	15.71	15.71	9.42	9.42	-45.12	2216.3
42	25	510	3158	-424	0	139	14330	15.71	15.71	9.42	9.42	-45.16	2219.5
43	25	-10280	2538	196	0	-96	6820	15.71	15.71	9.42	9.42	-23.09	575.0
44	25	9710	3218	236	0	-170	19415	15.71	15.71	9.42	9.42	-57.88	3458.4
45	25	-1275	2521	-928	0	365	11450	15.71	15.71	9.42	9.42	-36.58	1690.8
46	25	-2383	2112	148	0	-93	9681	15.71	15.71	9.42	9.42	-31.28	1366.3
47	25	-3102	1853	124	0	-79	8522	15.71	15.71	9.42	9.42	-27.77	1154.3
49	25	-4898	1861	126	0	-75	7602	15.71	15.71	9.42	9.42	-25.18	929.3

50	25	-899	1997	134	0	-90	10120	15.71	15.71	9.42	9.42	-32.27	1505.7
51	25	-3096	1858	-98	0	17	8528	15.71	15.71	9.42	9.42	-27.79	1155.7

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	38	-4796	3168	250	0	-169	11952	15.71	15.71	9.42	9.42	-39.04	1597.9
41	38	592	3145	243	0	-179	14708	15.71	15.71	9.42	9.42	-46.33	2281.3
42	38	610	3158	-424	0	192	14725	15.71	15.71	9.42	9.42	-46.38	2284.9
43	38	-10180	2538	196	0	-121	7137	15.71	15.71	9.42	9.42	-24.15	625.6
44	38	9810	3218	236	0	-199	19818	15.71	15.71	9.42	9.42	-59.12	3525.0
45	38	-1175	2521	-928	0	481	11765	15.71	15.71	9.42	9.42	-37.55	1744.0
46	38	-2283	2112	148	0	-111	9946	15.71	15.71	9.42	9.42	-32.09	1411.6
47	38	-3002	1853	124	0	-94	8753	15.71	15.71	9.42	9.42	-28.48	1194.6
49	38	-4798	1861	126	0	-91	7834	15.71	15.71	9.42	9.42	-25.91	969.3
50	38	-799	1997	134	0	-107	10370	15.71	15.71	9.42	9.42	-33.03	1548.8
51	38	-2996	1858	-98	0	29	8761	15.71	15.71	9.42	9.42	-28.50	1196.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	50	-4696	3168	250	0	-201	12350	15.71	15.71	9.42	9.42	-40.29	1663.4
41	50	692	3145	243	0	-209	15100	15.71	15.71	9.42	9.42	-47.54	2346.4
42	50	710	3158	-424	0	245	15120	15.71	15.71	9.42	9.42	-47.60	2350.3
43	50	-10080	2538	196	0	-146	7454	15.71	15.71	9.42	9.42	-25.21	676.5
44	50	9910	3218	236	0	-228	20220	15.71	15.71	9.42	9.42	-60.36	3591.5
45	50	-1075	2521	-928	0	597	12080	15.71	15.71	9.42	9.42	-38.52	1797.1
46	50	-2183	2112	148	0	-130	10210	15.71	15.71	9.42	9.42	-32.90	1456.9
47	50	-2902	1853	124	0	-110	8985	15.71	15.71	9.42	9.42	-29.19	1234.8
49	50	-4698	1861	126	0	-107	8067	15.71	15.71	9.42	9.42	-26.64	1009.4
50	50	-699	1997	134	0	-123	10620	15.71	15.71	9.42	9.42	-33.79	1591.9
51	50	-2896	1858	-98	0	42	8993	15.71	15.71	9.42	9.42	-29.22	1236.3

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 65 NI 1601 NF 164 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 4A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-3981	3407	356	0	-58	11890	15.71	15.71	9.42	9.42	-38.66	1627.3
41	0	1833	3407	347	0	-59	14940	15.71	15.71	9.42	9.42	-46.67	2378.3
42	0	1741	3375	-258	0	50	14830	15.71	15.71	9.42	9.42	-46.35	2356.9
43	0	-9977	2710	292	0	-46	6824	15.71	15.71	9.42	9.42	-23.10	588.1
44	0	11820	3529	338	0	-62	20550	15.71	15.71	12.57	12.57	-51.77	2814.2
45	0	-441	2657	-732	0	134	11740	15.71	15.71	9.42	9.42	-37.26	1776.1
46	0	-1560	2292	233	0	-40	10100	15.71	15.71	9.42	9.42	-32.39	1470.3
47	0	-2408	2014	204	0	-35	8887	15.71	15.71	9.42	9.42	-28.76	1243.6
49	0	-4346	2014	208	0	-35	7869	15.71	15.71	9.42	9.42	-25.94	995.7
50	0	13	2177	217	0	-38	10610	15.71	15.71	9.42	9.42	-33.55	1625.3
51	0	-2439	2003	3	0	1	8852	15.71	15.71	9.42	9.42	-28.66	1236.7

apost= 9.42 aant= 9.42 ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	12	-3881	3407	356	0	-103	12315	15.71	15.71	9.42	9.42	-39.99	1697.1
41	12	1933	3407	347	0	-103	15365	15.71	15.71	9.42	9.42	-47.98	2448.4
42	12	1841	3375	-258	0	82	15252	15.71	15.71	9.42	9.42	-47.65	2426.6
43	12	-9877	2710	292	0	-82	7163	15.71	15.71	9.42	9.42	-24.23	642.1
44	12	11920	3529	338	0	-104	20992	15.71	15.71	12.57	12.57	-52.95	2869.0
45	12	-341	2657	-732	0	226	12072	15.71	15.71	9.42	9.42	-38.28	1831.9
46	12	-1460	2292	233	0	-69	10385	15.71	15.71	9.42	9.42	-33.26	1518.8
47	12	-2308	2014	204	0	-60	9139	15.71	15.71	9.42	9.42	-29.54	1286.9
49	12	-4246	2014	208	0	-61	8121	15.71	15.71	9.42	9.42	-26.73	1038.8
50	12	113	2177	217	0	-65	10882	15.71	15.71	9.42	9.42	-34.38	1672.0
51	12	-2339	2003	3	0	1	9102	15.71	15.71	9.42	9.42	-29.43	1279.9

apost= 9.42 aant= 9.42 ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	25	-3781	3407	356	0	-147	12740	15.71	15.71	9.42	9.42	-41.31	1766.9
41	25	2033	3407	347	0	-146	15790	15.71	15.71	9.42	9.42	-49.29	2518.4
42	25	1941	3375	-258	0	114	15675	15.71	15.71	9.42	9.42	-48.96	2496.2
43	25	-9777	2710	292	0	-119	7502	15.71	15.71	9.42	9.42	-25.35	696.4
44	25	12020	3529	338	0	-147	21435	15.71	15.71	12.57	12.57	-54.13	2923.7
45	25	-241	2657	-732	0	317	12405	15.71	15.71	9.42	9.42	-39.31	1887.7
46	25	-1360	2292	233	0	-98	10670	15.71	15.71	9.42	9.42	-34.14	1567.3
47	25	-2208	2014	204	0	-86	9390	15.71	15.71	9.42	9.42	-30.31	1330.3
49	25	-4146	2014	208	0	-86	8372	15.71	15.71	9.42	9.42	-27.51	1082.0
50	25	213	2177	217	0	-92	11155	15.71	15.71	9.42	9.42	-35.22	1718.6
51	25	-2239	2003	3	0	1	9353	15.71	15.71	9.42	9.42	-30.20	1323.0

apost= 9.42 aant= 9.42 ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	38	-3681	3407	356	0	-192	13165	15.71	15.71	9.42	9.42	-42.64	1836.7
41	38	2133	3407	347	0	-189	16215	15.71	15.71	9.42	9.42	-50.60	2588.4
42	38	2041	3375	-258	0	146	16098	15.71	15.71	9.42	9.42	-50.26	2565.9
43	38	-9677	2710	292	0	-155	7840	15.71	15.71	9.42	9.42	-26.47	750.9
44	38	12120	3529	338	0	-189	21878	15.71	15.71	12.57	12.57	-55.31	2978.5
45	38	-141	2657	-732	0	409	12738	15.71	15.71	9.42	9.42	-40.33	1943.5
46	38	-1260	2292	233	0	-127	10955	15.71	15.71	9.42	9.42	-35.01	1615.8
47	38	-2108	2014	204	0	-112	9642	15.71	15.71	9.42	9.42	-31.08	1373.6
49	38	-4046	2014	208	0	-112	8624	15.71	15.71	9.42	9.42	-28.29	1125.1
50	38	313	2177	217	0	-119	11428	15.71	15.71	9.42	9.42	-36.05	1765.3
51	38	-2139	2003	3	0	0	9604	15.71	15.71	9.42	9.42	-30.97	1366.2

apost= 9.42 aant= 9.42 ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	50	-3581	3407	356	0	-237	13590	15.71	15.71	9.42	9.42	-43.96	1906.5
41	50	2233	3407	347	0	-233	16640	15.71	15.71	9.42	9.42	-51.91	2658.4
42	50	2141	3375	-258	0	178	16520	15.71	15.71	9.42	9.42	-51.57	2635.5
43	50	-9577	2710	292	0	-192	8179	15.71	15.71	9.42	9.42	-27.58	805.8
44	50	12220	3529	338	0	-231	22320	15.71	15.71	12.57	12.57	-56.49	3033.2
45	50	-41	2657	-732	0	500	13070	15.71	15.71	9.42	9.42	-41.35	1999.4
46	50	-1160	2292	233	0	-156	11240	15.71	15.71	9.42	9.42	-35.89	1664.3
47	50	-2008	2014	204	0	-137	9894	15.71	15.71	9.42	9.42	-31.86	1417.0
49	50	-3946	2014	208	0	-138	8876	15.71	15.71	9.42	9.42	-29.07	1168.3
50	50	413	2177	217	0	-146	11700	15.71	15.71	9.42	9.42	-36.88	1811.9

51	50	-2039	2003	3	0	-0	9854	15.71	15.71	9.42	9.42	-31.74	1409.4

apost= 9.42 aant= 9.42 ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 66 NI 1621 NF 207 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 3A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-5409	3084	450	0	-42	10430	15.71	15.71	9.42	9.42	-34.32	1336.3
41	0	380	3121	428	0	-34	13510	15.71	15.71	9.42	9.42	-42.61	2087.5
42	0	385	3122	-141	0	65	13520	15.71	15.71	9.42	9.42	-42.64	2089.3
43	0	-11100	2416	382	0	-41	5626	15.71	15.71	9.42	9.42	-19.00	372.9
44	0	10270	3293	403	0	-22	19130	15.71	15.71	9.42	9.42	-56.73	3443.3
45	0	-1441	2479	-603	0	137	10780	15.71	15.71	9.42	9.42	-34.51	1580.2
46	0	-2547	2091	297	0	-24	9120	15.71	15.71	9.42	9.42	-29.54	1272.5
47	0	-3279	1833	265	0	-22	8021	15.71	15.71	9.42	9.42	-26.21	1069.4
49	0	-5208	1821	272	0	-24	6993	15.71	15.71	9.42	9.42	-23.27	822.3
50	0	-935	1997	276	0	-20	9693	15.71	15.71	9.42	9.42	-30.93	1438.4
51	0	-3277	1834	75	0	11	8023	15.71	15.71	9.42	9.42	-26.22	1069.8

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	12	-5309	3084	450	0	-98	10815	15.71	15.71	9.42	9.42	-35.53	1399.8
41	12	480	3121	428	0	-88	13900	15.71	15.71	9.42	9.42	-43.81	2152.1
42	12	485	3122	-141	0	82	13910	15.71	15.71	9.42	9.42	-43.84	2153.9
43	12	-11000	2416	382	0	-89	5928	15.71	15.71	9.42	9.42	-20.04	418.7
44	12	10370	3293	403	0	-72	19542	15.71	15.71	9.42	9.42	-58.00	3511.4
45	12	-1341	2479	-603	0	212	11090	15.71	15.71	9.42	9.42	-35.46	1632.5
46	12	-2447	2091	297	0	-61	9382	15.71	15.71	9.42	9.42	-30.35	1317.5
47	12	-3179	1833	265	0	-55	8250	15.71	15.71	9.42	9.42	-26.92	1109.2
49	12	-5108	1821	272	0	-58	7220	15.71	15.71	9.42	9.42	-23.99	861.5
50	12	-835	1997	276	0	-55	9942	15.71	15.71	9.42	9.42	-31.69	1481.5
51	12	-3177	1834	75	0	2	8252	15.71	15.71	9.42	9.42	-26.93	1109.6

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	25	-5209	3084	450	0	-154	11200	15.71	15.71	9.42	9.42	-36.73	1463.3
41	25	580	3121	428	0	-141	14290	15.71	15.71	9.42	9.42	-45.02	2216.8
42	25	585	3122	-141	0	100	14300	15.71	15.71	9.42	9.42	-45.05	2218.6
43	25	-10900	2416	382	0	-136	6230	15.71	15.71	9.42	9.42	-21.08	465.3
44	25	10470	3293	403	0	-122	19955	15.71	15.71	9.42	9.42	-59.28	3579.5
45	25	-1241	2479	-603	0	288	11400	15.71	15.71	9.42	9.42	-36.42	1684.9
46	25	-2347	2091	297	0	-98	9645	15.71	15.71	9.42	9.42	-31.15	1362.5
47	25	-3079	1833	265	0	-88	8480	15.71	15.71	9.42	9.42	-27.63	1149.0
49	25	-5008	1821	272	0	-92	7448	15.71	15.71	9.42	9.42	-24.71	900.7
50	25	-735	1997	276	0	-89	10192	15.71	15.71	9.42	9.42	-32.45	1524.5
51	25	-3077	1834	75	0	-7	8482	15.71	15.71	9.42	9.42	-27.63	1149.4

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	38	-5109	3084	450	0	-211	11585	15.71	15.71	9.42	9.42	-37.94	1526.9
41	38	680	3121	428	0	-195	14680	15.71	15.71	9.42	9.42	-46.22	2281.4
42	38	685	3122	-141	0	118	14690	15.71	15.71	9.42	9.42	-46.25	2283.2
43	38	-10800	2416	382	0	-184	6532	15.71	15.71	9.42	9.42	-22.11	512.4
44	38	10570	3293	403	0	-173	20368	15.71	15.71	9.42	9.42	-60.55	3647.6
45	38	-1141	2479	-603	0	363	11710	15.71	15.71	9.42	9.42	-37.37	1737.2
46	38	-2247	2091	297	0	-136	9908	15.71	15.71	9.42	9.42	-31.96	1407.5
47	38	-2979	1833	265	0	-121	8709	15.71	15.71	9.42	9.42	-28.33	1188.9
49	38	-4908	1821	272	0	-126	7676	15.71	15.71	9.42	9.42	-25.42	940.0
50	38	-635	1997	276	0	-124	10441	15.71	15.71	9.42	9.42	-33.21	1567.6
51	38	-2977	1834	75	0	-17	8711	15.71	15.71	9.42	9.42	-28.34	1189.3

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	50	-5009	3084	450	0	-267	11970	15.71	15.71	9.42	9.42	-39.14	1590.4
41	50	780	3121	428	0	-248	15070	15.71	15.71	9.42	9.42	-47.42	2346.1
42	50	785	3122	-141	0	135	15080	15.71	15.71	9.42	9.42	-47.45	2347.9
43	50	-10700	2416	382	0	-232	6834	15.71	15.71	9.42	9.42	-23.14	560.1
44	50	10670	3293	403	0	-223	20780	15.71	15.71	12.57	12.57	-52.88	2797.3
45	50	-1041	2479	-603	0	438	12020	15.71	15.71	9.42	9.42	-38.32	1789.6
46	50	-2147	2091	297	0	-173	10170	15.71	15.71	9.42	9.42	-32.77	1452.5
47	50	-2879	1833	265	0	-154	8938	15.71	15.71	9.42	9.42	-29.04	1228.7
49	50	-4808	1821	272	0	-160	7903	15.71	15.71	9.42	9.42	-26.13	979.3
50	50	-535	1997	276	0	-158	10690	15.71	15.71	9.42	9.42	-33.97	1610.7
51	50	-2877	1834	75	0	-26	8940	15.71	15.71	9.42	9.42	-29.04	1229.1

apost= 9.42 aant= 9.42 ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 67 NI 1641 NF 250 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 2A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-10810	1692	542	0	37	5197	15.71	15.71	9.42	9.42	-17.52	324.5
41	0	-5366	1785	432	0	48	8082	15.71	15.71	9.42	9.42	-26.80	980.6
42	0	-5276	1829	-111	0	146	8206	15.71	15.71	9.42	9.42	-27.18	1003.6
43	0	-15110	1240	540	0	19	1636	15.71	15.71	9.42	9.42	-7.53	-106.9
44	0	3737	2004	262	0	68	13170	15.71	15.71	9.42	9.42	-40.39	2202.3
45	0	-5895	1468	-548	0	201	6652	15.71	15.71	9.42	9.42	-22.26	739.3
46	0	-6451	1161	312	0	31	5464	15.71	15.71	9.42	9.42	-18.43	536.0
47	0	-6722	1005	282	0	26	4809	15.71	15.71	9.42	9.42	-16.27	427.3
49	0	-8536	974	318	0	23	3847	15.71	15.71	9.42	9.42	-12.94	221.8
50	0	-4766	1127	263	0	32	6153	15.71	15.71	9.42	9.42	-20.50	715.1
51	0	-6693	1019	101	0	59	4850	15.71	15.71	9.42	9.42	-16.40	434.5

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	12	-10710	1692	542	0	-30	5408	15.71	15.71	9.42	9.42	-18.26	357.1
41	12	-5266	1785	432	0	-6	8305	15.71	15.71	9.42	9.42	-27.50	1019.2
42	12	-5176	1829	-111	0	160	8434	15.71	15.71	9.42	9.42	-27.90	1043.1
43	12	-15010	1240	540	0	-48	1791	15.71	15.71	9.42	9.42	-7.80	-110.4
44	12	3837	2004	262	0	35	13420	15.71	15.71	9.42	9.42	-41.15	2245.6
45	12	-5795	1468	-548	0	269	6835	15.71	15.71	9.42	9.42	-22.84	771.6
46	12	-6351	1161	312	0	-8	5609	15.71	15.71	9.42	9.42	-18.90	562.0
47	12	-6622	1005	282	0	-9	4934	15.71	15.71	9.42	9.42	-16.68	450.0
49	12	-8436	974	318	0	-17	3969	15.71	15.71	9.42	9.42	-13.37	241.5
50	12	-4666	1127	263	0	-0	6294	15.71	15.71	9.42	9.42	-20.94	741.1
51	12	-6593	1019	101	0	46	4978	15.71	15.71	9.42	9.42	-16.83	457.6

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	25	-10610	1692	542	0	-98	5620	15.71	15.71	9.42	9.42	-19.00	390.2
41	25	-5166	1785	432	0	-60	8528	15.71	15.71	9.42	9.42	-28.20	1057.8
42	25	-5076	1829	-111	0	174	8663	15.71	15.71	9.42	9.42	-28.61	1082.5
43	25	-14910	1240	540	0	-116	1946	15.71	15.71	9.42	9.42	-8.07	-114.0
44	25	3937	2004	262	0	3	13670	15.71	15.71	9.42	9.42	-41.91	2288.8
45	25	-5695	1468	-548	0	338	7018	15.71	15.71	9.42	9.42	-23.42	803.9
46	25	-6251	1161	312	0	-47	5754	15.71	15.71	9.42	9.42	-19.37	588.1
47	25	-6522	1005	282	0	-44	5060	15.71	15.71	9.42	9.42	-17.10	472.8
49	25	-8336	974	318	0	-57	4090	15.71	15.71	9.42	9.42	-13.80	261.6
50	25	-4566	1127	263	0	-33	6434	15.71	15.71	9.42	9.42	-21.38	767.1
51	25	-6493	1019	101	0	34	5105	15.71	15.71	9.42	9.42	-17.25	480.7

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	38	-10510	1692	542	0	-166	5832	15.71	15.71	9.42	9.42	-19.73	423.7
41	38	-5066	1785	432	0	-114	8752	15.71	15.71	9.42	9.42	-28.89	1096.5
42	38	-4976	1829	-111	0	188	8892	15.71	15.71	9.42	9.42	-29.32	1122.1
43	38	-14810	1240	540	0	-184	2101	15.71	15.71	9.42	9.42	-8.35	-117.5
44	38	4037	2004	262	0	-30	13920	15.71	15.71	9.42	9.42	-42.66	2332.1
45	38	-5595	1468	-548	0	406	7202	15.71	15.71	9.42	9.42	-24.00	836.2
46	38	-6151	1161	312	0	-86	5899	15.71	15.71	9.42	9.42	-19.84	614.3
47	38	-6422	1005	282	0	-79	5186	15.71	15.71	9.42	9.42	-17.51	495.7
49	38	-8236	974	318	0	-97	4212	15.71	15.71	9.42	9.42	-14.23	281.9
50	38	-4466	1127	263	0	-66	6575	15.71	15.71	9.42	9.42	-21.82	793.1
51	38	-6393	1019	101	0	21	5232	15.71	15.71	9.42	9.42	-17.66	504.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	50	-10410	1692	542	0	-234	6043	15.71	15.71	9.42	9.42	-20.45	457.6
41	50	-4966	1785	432	0	-168	8975	15.71	15.71	9.42	9.42	-29.59	1135.3
42	50	-4876	1829	-111	0	202	9120	15.71	15.71	9.42	9.42	-30.04	1161.6
43	50	-14710	1240	540	0	-251	2256	15.71	15.71	9.42	9.42	-8.62	-121.1
44	50	4137	2004	262	0	-63	14170	15.71	15.71	9.42	9.42	-43.42	2375.4
45	50	-5495	1468	-548	0	475	7385	15.71	15.71	9.42	9.42	-24.58	868.6
46	50	-6051	1161	312	0	-125	6044	15.71	15.71	9.42	9.42	-20.30	640.6
47	50	-6322	1005	282	0	-115	5311	15.71	15.71	9.42	9.42	-17.92	518.7
49	50	-8136	974	318	0	-137	4334	15.71	15.71	9.42	9.42	-14.65	302.6
50	50	-4366	1127	263	0	-99	6716	15.71	15.71	9.42	9.42	-22.25	819.1
51	50	-6293	1019	101	0	8	5360	15.71	15.71	9.42	9.42	-18.08	527.3

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 68 NI 1580 NF 1581 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 5
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	852	1155	-223	0	-187	9000	15.71	15.71	9.42	9.42	-28.20	1420.2
41	0	6700	678	-334	0	-255	12050	15.71	15.71	9.42	9.42	-35.63	2180.7
42	0	6731	698	-550	0	-242	12050	15.71	15.71	9.42	9.42	-35.62	2182.3
43	0	-5829	1343	-79	0	-87	4455	15.71	15.71	9.42	9.42	-15.06	412.6
44	0	16870	-93	-534	0	-378	17570	15.71	15.71	9.42	9.42	-48.45	3544.2
45	0	3968	582	-624	0	-179	9547	15.71	15.71	9.42	9.42	-28.79	1659.8
46	0	2247	470	-222	0	-167	8033	15.71	15.71	9.42	9.42	-24.65	1341.7
47	0	1134	418	-194	0	-145	7029	15.71	15.71	9.42	9.42	-21.87	1132.4
49	0	-815	577	-157	0	-122	6012	15.71	15.71	9.42	9.42	-19.25	880.7
50	0	3725	290	-248	0	-180	8634	15.71	15.71	9.42	9.42	-25.99	1508.0
51	0	1144	425	-266	0	-141	7030	15.71	15.71	9.42	9.42	-21.86	1133.1

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	12	952	1155	-223	0	-159	9144	15.71	15.71	9.42	9.42	-28.62	1447.3
41	12	6800	678	-334	0	-213	12135	15.71	15.71	9.42	9.42	-35.86	2198.7
42	12	6831	698	-550	0	-173	12138	15.71	15.71	9.42	9.42	-35.85	2200.7
43	12	-5729	1343	-79	0	-77	4623	15.71	15.71	9.42	9.42	-15.61	441.8
44	12	16970	-93	-534	0	-311	17558	15.71	15.71	9.42	9.42	-48.36	3547.5
45	12	4068	582	-624	0	-101	9620	15.71	15.71	9.42	9.42	-28.99	1676.0
46	12	2347	470	-222	0	-139	8092	15.71	15.71	9.42	9.42	-24.80	1355.7
47	12	1234	418	-194	0	-121	7081	15.71	15.71	9.42	9.42	-22.00	1145.4
49	12	-715	577	-157	0	-103	6084	15.71	15.71	9.42	9.42	-19.45	896.6
50	12	3825	290	-248	0	-149	8670	15.71	15.71	9.42	9.42	-26.06	1518.6
51	12	1244	425	-266	0	-107	7083	15.71	15.71	9.42	9.42	-22.00	1146.2

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	25	1052	1155	-223	0	-131	9288	15.71	15.71	9.42	9.42	-29.04	1474.3
41	25	6900	678	-334	0	-171	12220	15.71	15.71	9.42	9.42	-36.09	2216.8
42	25	6931	698	-550	0	-105	12225	15.71	15.71	9.42	9.42	-36.09	2219.2
43	25	-5629	1343	-79	0	-67	4790	15.71	15.71	9.42	9.42	-16.16	471.1
44	25	17070	-93	-534	0	-244	17545	15.71	15.71	9.42	9.42	-48.26	3550.8
45	25	4168	582	-624	0	-23	9692	15.71	15.71	9.42	9.42	-29.18	1692.1
46	25	2447	470	-222	0	-111	8150	15.71	15.71	9.42	9.42	-24.95	1369.7
47	25	1334	418	-194	0	-96	7134	15.71	15.71	9.42	9.42	-22.13	1158.4
49	25	-615	577	-157	0	-83	6156	15.71	15.71	9.42	9.42	-19.65	912.5
50	25	3925	290	-248	0	-118	8706	15.71	15.71	9.42	9.42	-26.13	1529.2
51	25	1344	425	-266	0	-74	7136	15.71	15.71	9.42	9.42	-22.13	1159.4

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	38	1152	1155	-223	0	-103	9433	15.71	15.71	9.42	9.42	-29.47	1501.4

41	38	7000	678	-334	0	-129	12305	15.71	15.71	9.42	9.42	-36.32	2234.9
42	38	7031	698	-550	0	-36	12312	15.71	15.71	9.42	9.42	-36.33	2237.6
43	38	-5529	1343	-79	0	-57	4958	15.71	15.71	9.42	9.42	-16.70	500.5
44	38	17170	-93	-534	0	-177	17532	15.71	15.71	9.42	9.42	-48.16	3554.0
45	38	4268	582	-624	0	55	9765	15.71	15.71	9.42	9.42	-29.37	1708.3
46	38	2547	470	-222	0	-83	8209	15.71	15.71	9.42	9.42	-25.10	1383.7
47	38	1434	418	-194	0	-72	7186	15.71	15.71	9.42	9.42	-22.26	1171.4
49	38	-515	577	-157	0	-63	6228	15.71	15.71	9.42	9.42	-19.85	928.4
50	38	4025	290	-248	0	-87	8743	15.71	15.71	9.42	9.42	-26.21	1539.8
51	38	1444	425	-266	0	-41	7190	15.71	15.71	9.42	9.42	-22.27	1172.5

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	50	1252	1155	-223	0	-76	9577	15.71	15.71	9.42	9.42	-29.89	1528.4
41	50	7100	678	-334	0	-88	12390	15.71	15.71	9.42	9.42	-36.54	2252.9
42	50	7131	698	-550	0	33	12400	15.71	15.71	9.42	9.42	-36.56	2256.0
43	50	-5429	1343	-79	0	-47	5126	15.71	15.71	9.42	9.42	-17.24	530.1
44	50	17270	-93	-534	0	-111	17520	15.71	15.71	9.42	9.42	-48.07	3557.3
45	50	4368	582	-624	0	133	9838	15.71	15.71	9.42	9.42	-29.56	1724.5
46	50	2647	470	-222	0	-56	8268	15.71	15.71	9.42	9.42	-25.25	1397.7
47	50	1534	418	-194	0	-48	7238	15.71	15.71	9.42	9.42	-22.39	1184.4
49	50	-415	577	-157	0	-44	6300	15.71	15.71	9.42	9.42	-20.05	944.3
50	50	4125	290	-248	0	-56	8779	15.71	15.71	9.42	9.42	-26.28	1550.4
51	50	1544	425	-266	0	-8	7243	15.71	15.71	9.42	9.42	-22.40	1185.6

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 69 NI 1600 NF 1601 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 4
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	2285	1178	134	0	9	10060	15.71	15.71	9.42	9.42	-31.06	1653.8
41	0	8629	638	107	0	-6	13430	15.71	15.71	9.42	9.42	-39.19	2489.6
42	0	8509	620	-90	0	5	13340	15.71	15.71	9.42	9.42	-38.96	2469.8
43	0	-5132	1422	130	0	19	5025	15.71	15.71	9.42	9.42	-16.89	528.1
44	0	19700	-239	66	0	-29	19510	15.71	15.71	12.57	12.57	-45.20	2996.3
45	0	5241	492	-243	0	13	10480	15.71	15.71	9.42	9.42	-31.24	1866.8
46	0	3530	454	73	0	-3	8950	15.71	15.71	9.42	9.42	-27.07	1546.4
47	0	2255	408	64	0	-3	7831	15.71	15.71	9.42	9.42	-24.01	1311.2
49	0	140	588	73	0	2	6710	15.71	15.71	9.42	9.42	-21.18	1034.4
50	0	5107	256	60	0	-8	9607	15.71	15.71	9.42	9.42	-28.51	1726.6
51	0	2215	402	-1	0	1	7801	15.71	15.71	9.42	9.42	-23.93	1304.6

apost= 9.42 aant= 9.42 ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	12	2385	1178	134	0	-8	10208	15.71	15.71	9.42	9.42	-31.49	1681.3
41	12	8729	638	107	0	-19	13510	15.71	15.71	9.42	9.42	-39.40	2506.9
42	12	8609	620	-90	0	16	13418	15.71	15.71	9.42	9.42	-39.16	2486.7
43	12	-5032	1422	130	0	3	5203	15.71	15.71	9.42	9.42	-17.46	559.3
44	12	19800	-239	66	0	-37	19480	15.71	15.71	12.57	12.57	-45.06	2996.7
45	12	5341	492	-243	0	43	10542	15.71	15.71	9.42	9.42	-31.40	1881.4
46	12	3630	454	73	0	-12	9007	15.71	15.71	9.42	9.42	-27.21	1560.1
47	12	2355	408	64	0	-11	7882	15.71	15.71	9.42	9.42	-24.13	1324.0
49	12	240	588	73	0	-7	6784	15.71	15.71	9.42	9.42	-21.38	1050.6
50	12	5207	256	60	0	-15	9639	15.71	15.71	9.42	9.42	-28.57	1736.6
51	12	2315	402	-1	0	1	7851	15.71	15.71	9.42	9.42	-24.05	1317.3

apost= 9.42 aant= 9.42 ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	25	2485	1178	134	0	-25	10355	15.71	15.71	9.42	9.42	-31.93	1708.9
41	25	8829	638	107	0	-32	13590	15.71	15.71	9.42	9.42	-39.61	2524.3
42	25	8709	620	-90	0	27	13495	15.71	15.71	9.42	9.42	-39.36	2503.6
43	25	-4932	1422	130	0	-13	5380	15.71	15.71	9.42	9.42	-18.03	590.6
44	25	19900	-239	66	0	-46	19450	15.71	15.71	12.57	12.57	-44.93	2997.1
45	25	5441	492	-243	0	74	10605	15.71	15.71	9.42	9.42	-31.56	1896.0
46	25	3730	454	73	0	-21	9064	15.71	15.71	9.42	9.42	-27.35	1573.9
47	25	2455	408	64	0	-19	7933	15.71	15.71	9.42	9.42	-24.26	1336.8
49	25	340	588	73	0	-16	6857	15.71	15.71	9.42	9.42	-21.58	1066.8
50	25	5307	256	60	0	-23	9671	15.71	15.71	9.42	9.42	-28.63	1746.6
51	25	2415	402	-1	0	1	7902	15.71	15.71	9.42	9.42	-24.17	1330.0

apost= 9.42 aant= 9.42 ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	38	2585	1178	134	0	-42	10502	15.71	15.71	9.42	9.42	-32.36	1736.5
41	38	8929	638	107	0	-46	13670	15.71	15.71	9.42	9.42	-39.82	2541.6
42	38	8809	620	-90	0	38	13572	15.71	15.71	9.42	9.42	-39.56	2520.6
43	38	-4832	1422	130	0	-29	5558	15.71	15.71	9.42	9.42	-18.59	622.0
44	38	20000	-239	66	0	-54	19420	15.71	15.71	12.57	12.57	-44.79	2997.6
45	38	5541	492	-243	0	104	10668	15.71	15.71	9.42	9.42	-31.71	1910.7
46	38	3830	454	73	0	-31	9120	15.71	15.71	9.42	9.42	-27.49	1587.6
47	38	2555	408	64	0	-27	7984	15.71	15.71	9.42	9.42	-24.38	1349.6
49	38	440	588	73	0	-25	6930	15.71	15.71	9.42	9.42	-21.78	1083.0
50	38	5407	256	60	0	-30	9703	15.71	15.71	9.42	9.42	-28.69	1756.6
51	38	2515	402	-1	0	1	7952	15.71	15.71	9.42	9.42	-24.29	1342.7

apost= 9.42 aant= 9.42 ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	50	2685	1178	134	0	-58	10650	15.71	15.71	9.42	9.42	-32.79	1764.1
41	50	9029	638	107	0	-59	13750	15.71	15.71	9.42	9.42	-40.03	2558.9
42	50	8909	620	-90	0	50	13650	15.71	15.71	9.42	9.42	-39.77	2537.5
43	50	-4732	1422	130	0	-46	5736	15.71	15.71	9.42	9.42	-19.15	653.4
44	50	20100	-239	66	0	-62	19390	15.71	15.71	12.57	12.57	-44.65	2998.0
45	50	5641	492	-243	0	134	10730	15.71	15.71	9.42	9.42	-31.87	1925.3
46	50	3930	454	73	0	-40	9177	15.71	15.71	9.42	9.42	-27.63	1601.3
47	50	2655	408	64	0	-35	8035	15.71	15.71	9.42	9.42	-24.50	1362.5
49	50	540	588	73	0	-35	7004	15.71	15.71	9.42	9.42	-21.98	1099.2
50	50	5507	256	60	0	-38	9735	15.71	15.71	9.42	9.42	-28.74	1766.5
51	50	2615	402	-1	0	1	8002	15.71	15.71	9.42	9.42	-24.41	1355.4

apost= 9.42 aant= 9.42 ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 70 NI 1620 NF 1621 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 3

armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	453	1142	477	0	196	8687	15.71	15.71	9.42	9.42	-27.33	1352.6
41	0	6783	650	517	0	224	12050	15.71	15.71	9.42	9.42	-35.60	2184.9
42	0	6788	650	320	0	225	12060	15.71	15.71	9.42	9.42	-35.63	2186.7
43	0	-6584	1346	343	0	130	3916	15.71	15.71	9.42	9.42	-13.26	302.9
44	0	17760	-147	601	0	279	18100	15.71	15.71	12.57	12.57	-42.20	2759.8
45	0	3975	527	82	0	178	9538	15.71	15.71	9.42	9.42	-28.76	1658.8
46	0	2277	452	345	0	148	8012	15.71	15.71	9.42	9.42	-24.57	1340.0
47	0	1150	403	302	0	129	7002	15.71	15.71	9.42	9.42	-21.77	1129.1
49	0	-960	567	289	0	120	5879	15.71	15.71	9.42	9.42	-18.87	853.3
50	0	3909	268	340	0	150	8715	15.71	15.71	9.42	9.42	-26.17	1529.6
51	0	1152	403	236	0	130	7004	15.71	15.71	9.42	9.42	-21.78	1129.5

apost= 9.42 aant= 9.42 ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	12	553	1142	477	0	137	8830	15.71	15.71	9.42	9.42	-27.75	1379.4
41	12	6883	650	517	0	160	12132	15.71	15.71	9.42	9.42	-35.82	2202.6
42	12	6888	650	320	0	185	12142	15.71	15.71	9.42	9.42	-35.85	2204.4
43	12	-6484	1346	343	0	88	4084	15.71	15.71	9.42	9.42	-13.83	331.1
44	12	17860	-147	601	0	204	18080	15.71	15.71	12.57	12.57	-42.09	2761.4
45	12	4075	527	82	0	168	9604	15.71	15.71	9.42	9.42	-28.93	1673.9
46	12	2377	452	345	0	105	8068	15.71	15.71	9.42	9.42	-24.71	1353.6
47	12	1250	403	302	0	92	7052	15.71	15.71	9.42	9.42	-21.90	1141.8
49	12	-860	567	289	0	84	5950	15.71	15.71	9.42	9.42	-19.06	869.0
50	12	4009	268	340	0	107	8748	15.71	15.71	9.42	9.42	-26.23	1539.8
51	12	1252	403	236	0	100	7054	15.71	15.71	9.42	9.42	-21.90	1142.2

apost= 9.42 aant= 9.42 ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	25	653	1142	477	0	77	8972	15.71	15.71	9.42	9.42	-28.17	1406.2
41	25	6983	650	517	0	95	12215	15.71	15.71	9.42	9.42	-36.04	2220.3
42	25	6988	650	320	0	145	12225	15.71	15.71	9.42	9.42	-36.07	2222.1
43	25	-6384	1346	343	0	45	4252	15.71	15.71	9.42	9.42	-14.40	359.7
44	25	17960	-147	601	0	129	18060	15.71	15.71	12.57	12.57	-41.98	2762.9
45	25	4175	527	82	0	157	9670	15.71	15.71	9.42	9.42	-29.10	1689.1
46	25	2477	452	345	0	62	8125	15.71	15.71	9.42	9.42	-24.86	1367.3
47	25	1350	403	302	0	54	7102	15.71	15.71	9.42	9.42	-22.02	1154.5
49	25	-760	567	289	0	48	6020	15.71	15.71	9.42	9.42	-19.26	884.7
50	25	4109	268	340	0	65	8782	15.71	15.71	9.42	9.42	-26.30	1550.0
51	25	1352	403	236	0	71	7104	15.71	15.71	9.42	9.42	-22.03	1154.9

apost= 9.42 aant= 9.42 ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	38	753	1142	477	0	18	9115	15.71	15.71	9.42	9.42	-28.59	1433.0
41	38	7083	650	517	0	30	12298	15.71	15.71	9.42	9.42	-36.26	2238.0
42	38	7088	650	320	0	105	12308	15.71	15.71	9.42	9.42	-36.29	2239.7
43	38	-6284	1346	343	0	2	4421	15.71	15.71	9.42	9.42	-14.96	388.4
44	38	18060	-147	601	0	54	18040	15.71	15.71	12.57	12.57	-41.87	2764.5
45	38	4275	527	82	0	147	9736	15.71	15.71	9.42	9.42	-29.27	1704.2
46	38	2577	452	345	0	19	8182	15.71	15.71	9.42	9.42	-25.00	1380.9
47	38	1450	403	302	0	16	7153	15.71	15.71	9.42	9.42	-22.15	1167.1
49	38	-660	567	289	0	12	6091	15.71	15.71	9.42	9.42	-19.46	900.4
50	38	4209	268	340	0	22	8816	15.71	15.71	9.42	9.42	-26.36	1560.2
51	38	1452	403	236	0	41	7155	15.71	15.71	9.42	9.42	-22.15	1167.5

apost= 9.42 aant= 9.42 ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	50	853	1142	477	0	-42	9258	15.71	15.71	9.42	9.42	-29.01	1459.8
41	50	7183	650	517	0	-34	12380	15.71	15.71	9.42	9.42	-36.48	2255.6
42	50	7188	650	320	0	65	12390	15.71	15.71	9.42	9.42	-36.50	2257.4
43	50	-6184	1346	343	0	-41	4589	15.71	15.71	9.42	9.42	-15.52	417.4
44	50	18160	-147	601	0	-22	18020	15.71	15.71	12.57	12.57	-41.77	2766.1
45	50	4375	527	82	0	137	9802	15.71	15.71	9.42	9.42	-29.44	1719.3
46	50	2677	452	345	0	-24	8238	15.71	15.71	9.42	9.42	-25.14	1394.6
47	50	1550	403	302	0	-22	7203	15.71	15.71	9.42	9.42	-22.27	1179.8
49	50	-560	567	289	0	-24	6162	15.71	15.71	9.42	9.42	-19.65	916.1
50	50	4309	268	340	0	-20	8849	15.71	15.71	9.42	9.42	-26.43	1570.4
51	50	1552	403	236	0	11	7205	15.71	15.71	9.42	9.42	-22.28	1180.2

apost= 9.42 aant= 9.42 ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 71 NI 1640 NF 1641 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 2
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-6137	466	597	0	336	3952	15.71	15.71	9.42	9.42	-13.38	325.9
41	0	-296	206	769	0	433	7031	15.71	15.71	9.42	9.42	-22.33	1062.1
42	0	-168	233	596	0	444	7134	15.71	15.71	9.42	9.42	-22.61	1084.2
43	0	-11400	570	305	0	171	414	15.71	15.71	9.42	9.42	-4.08	-59.7
44	0	9612	-219	1086	0	611	12410	15.71	15.71	9.42	9.42	-35.43	2384.5
45	0	-1455	183	304	0	352	5717	15.71	15.71	9.42	9.42	-18.48	804.5
46	0	-2493	95	486	0	273	4655	15.71	15.71	9.42	9.42	-15.33	592.7
47	0	-3042	68	414	0	233	4061	15.71	15.71	9.42	9.42	-13.52	476.7
49	0	-4989	154	357	0	201	3034	15.71	15.71	9.42	9.42	-10.27	239.1
50	0	-786	-3	513	0	289	5434	15.71	15.71	9.42	9.42	-17.41	793.6
51	0	-2999	77	357	0	237	4095	15.71	15.71	9.42	9.42	-13.62	483.9

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	12	-6037	466	597	0	261	4010	15.71	15.71	9.42	9.42	-13.58	338.5
41	12	-196	206	769	0	337	7057	15.71	15.71	9.42	9.42	-22.38	1070.9
42	12	-68	233	596	0	370	7163	15.71	15.71	9.42	9.42	-22.68	1093.6
43	12	-11300	570	305	0	133	485	15.71	15.71	9.42	9.42	-4.19	-61.1
44	12	9712	-219	1086	0	475	12382	15.71	15.71	9.42	9.42	-35.29	2385.4
45	12	-1355	183	304	0	315	5740	15.71	15.71	9.42	9.42	-18.53	812.8

46	12	-2393	95	486	0	213	4667	15.71	15.71	9.42	9.42	-15.35	599.2
47	12	-2942	68	414	0	182	4070	15.71	15.71	9.42	9.42	-13.53	482.6
49	12	-4889	154	357	0	156	3054	15.71	15.71	9.42	9.42	-10.34	245.9
50	12	-686	-3	513	0	225	5434	15.71	15.71	9.42	9.42	-17.38	798.4
51	12	-2899	77	357	0	193	4105	15.71	15.71	9.42	9.42	-13.64	490.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	25	-5937	466	597	0	187	4068	15.71	15.71	9.42	9.42	-13.77	351.1
41	25	-96	206	769	0	241	7082	15.71	15.71	9.42	9.42	-22.43	1079.8
42	25	32	233	596	0	295	7192	15.71	15.71	9.42	9.42	-22.74	1103.0
43	25	-11200	570	305	0	95	557	15.71	15.71	9.42	9.42	-4.30	-62.5
44	25	9811	-219	1086	0	340	12355	15.71	15.71	9.42	9.42	-35.15	2386.3
45	25	-1255	183	304	0	277	5762	15.71	15.71	9.42	9.42	-18.58	821.1
46	25	-2293	95	486	0	152	4679	15.71	15.71	9.42	9.42	-15.37	605.8
47	25	-2842	68	414	0	130	4078	15.71	15.71	9.42	9.42	-13.54	488.5
49	25	-4789	154	357	0	112	3073	15.71	15.71	9.42	9.42	-10.40	252.8
50	25	-586	-3	513	0	161	5433	15.71	15.71	9.42	9.42	-17.35	803.2
51	25	-2799	77	357	0	148	4114	15.71	15.71	9.42	9.42	-13.65	496.1

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	38	-5837	466	597	0	112	4127	15.71	15.71	9.42	9.42	-13.96	363.8
41	38	3	206	769	0	144	7108	15.71	15.71	9.42	9.42	-22.48	1088.7
42	38	132	233	596	0	221	7222	15.71	15.71	9.42	9.42	-22.80	1112.4
43	38	-11100	570	305	0	57	628	15.71	15.71	9.42	9.42	-4.41	-63.9
44	38	9910	-219	1086	0	204	12328	15.71	15.71	9.42	9.42	-35.01	2387.3
45	38	-1155	183	304	0	239	5785	15.71	15.71	9.42	9.42	-18.62	829.5
46	38	-2193	95	486	0	91	4691	15.71	15.71	9.42	9.42	-15.39	612.4
47	38	-2742	68	414	0	78	4086	15.71	15.71	9.42	9.42	-13.55	494.5
49	38	-4689	154	357	0	67	3092	15.71	15.71	9.42	9.42	-10.47	259.7
50	38	-486	-3	513	0	97	5432	15.71	15.71	9.42	9.42	-17.32	808.0
51	38	-2699	77	357	0	104	4124	15.71	15.71	9.42	9.42	-13.67	502.2

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	50	-5737	466	597	0	37	4185	15.71	15.71	9.42	9.42	-14.15	376.6
41	50	104	206	769	0	48	7134	15.71	15.71	9.42	9.42	-22.53	1097.5
42	50	232	233	596	0	146	7251	15.71	15.71	9.42	9.42	-22.86	1121.8
43	50	-11000	570	305	0	19	699	15.71	15.71	9.42	9.42	-4.52	-65.3
44	50	10010	-219	1086	0	68	12300	15.71	15.71	9.42	9.42	-34.87	2388.2
45	50	-1055	183	304	0	201	5808	15.71	15.71	9.42	9.42	-18.67	837.8
46	50	-2093	95	486	0	31	4703	15.71	15.71	9.42	9.42	-15.41	618.9
47	50	-2642	68	414	0	26	4095	15.71	15.71	9.42	9.42	-13.57	500.4
49	50	-4589	154	357	0	23	3112	15.71	15.71	9.42	9.42	-10.53	266.6
50	50	-386	-3	513	0	32	5432	15.71	15.71	9.42	9.42	-17.29	812.9
51	50	-2599	77	357	0	59	4134	15.71	15.71	9.42	9.42	-13.68	508.3

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 72 NI 1663 NF 1664 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 31
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	621	-327	-3004	0	-1636	-5301	15.71	15.71	9.42	9.42	-16.57	842.4
41	0	-2668	-481	-2216	0	-1209	-3604	15.71	15.71	9.42	9.42	-11.99	424.5
42	0	-2829	-448	-2422	0	-1211	-3543	15.71	15.71	9.42	9.42	-11.82	407.9
43	0	1826	-138	-3092	0	-1679	-5515	15.71	15.71	9.42	9.42	-16.82	935.3
44	0	-8043	-749	-978	0	-536	-916	15.71	15.71	9.42	9.42	-4.20	-58.1
45	0	-3924	-340	-2123	0	-970	-2586	15.71	15.71	9.42	9.42	-8.75	217.0
46	0	-4247	-343	-1518	0	-821	-2138	15.71	15.71	9.42	9.42	-7.22	140.7
47	0	-4642	-309	-1344	0	-724	-1772	15.71	15.71	9.42	9.42	-5.91	80.0
49	0	-3546	-257	-1606	0	-866	-2337	15.71	15.71	9.42	9.42	-7.91	196.1
50	0	-5520	-380	-1183	0	-638	-1417	15.71	15.71	9.42	9.42	-4.70	-64.1
51	0	-4696	-298	-1412	0	-724	-1751	15.71	15.71	9.42	9.42	-5.84	-76.7

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	12	721	-327	-3004	0	-1261	-5342	15.71	15.71	9.42	9.42	-16.66	853.6
41	12	-2568	-481	-2216	0	-932	-3664	15.71	15.71	9.42	9.42	-12.17	438.3
42	12	-2729	-448	-2422	0	-908	-3599	15.71	15.71	9.42	9.42	-11.98	421.0
43	12	1926	-138	-3092	0	-1292	-5532	15.71	15.71	9.42	9.42	-16.83	943.0
44	12	-7943	-749	-978	0	-414	-1009	15.71	15.71	9.42	9.42	-4.25	-60.0
45	12	-3824	-340	-2123	0	-704	-2628	15.71	15.71	9.42	9.42	-8.89	227.3
46	12	-4147	-343	-1518	0	-631	-2181	15.71	15.71	9.42	9.42	-7.37	150.3
47	12	-4542	-309	-1344	0	-556	-1810	15.71	15.71	9.42	9.42	-6.06	87.6
49	12	-3446	-257	-1606	0	-666	-2369	15.71	15.71	9.42	9.42	-8.02	204.9
50	12	-5420	-380	-1183	0	-490	-1464	15.71	15.71	9.42	9.42	-4.85	-65.8
51	12	-4596	-298	-1412	0	-548	-1788	15.71	15.71	9.42	9.42	-5.97	83.3

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	25	821	-327	-3004	0	-885	-5382	15.71	15.71	9.42	9.42	-16.76	864.8
41	25	-2468	-481	-2216	0	-655	-3724	15.71	15.71	9.42	9.42	-12.35	452.1
42	25	-2629	-448	-2422	0	-605	-3655	15.71	15.71	9.42	9.42	-12.15	434.1
43	25	2026	-138	-3092	0	-906	-5550	15.71	15.71	9.42	9.42	-16.85	950.7
44	25	-7843	-749	-978	0	-291	-1103	15.71	15.71	9.42	9.42	-4.40	-62.0
45	25	-3724	-340	-2123	0	-439	-2670	15.71	15.71	9.42	9.42	-9.03	237.6
46	25	-4047	-343	-1518	0	-441	-2224	15.71	15.71	9.42	9.42	-7.52	160.1
47	25	-4442	-309	-1344	0	-388	-1849	15.71	15.71	9.42	9.42	-6.20	95.5
49	25	-3346	-257	-1606	0	-465	-2402	15.71	15.71	9.42	9.42	-8.12	213.8
50	25	-5320	-380	-1183	0	-342	-1512	15.71	15.71	9.42	9.42	-5.00	-67.5
51	25	-4496	-298	-1412	0	-371	-1826	15.71	15.71	9.42	9.42	-6.11	90.9

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	38	921	-327	-3004	0	-510	-5423	15.71	15.71	9.42	9.42	-16.85	876.0
41	38	-2368	-481	-2216	0	-378	-3785	15.71	15.71	9.42	9.42	-12.53	465.9
42	38	-2529	-448	-2422	0	-303	-3711	15.71	15.71	9.42	9.42	-12.32	447.2
43	38	2126	-138	-3092	0	-519	-5567	15.71	15.71	9.42	9.42	-16.86	958.3
44	38	-7743	-749	-978	0	-169	-1196	15.71	15.71	9.42	9.42	-4.56	-64.0
45	38	-3624	-340	-2123	0	-174	-2713	15.71	15.71	9.42	9.42	-9.17	248.1
46	38	-3947	-343	-1518	0	-251	-2267	15.71	15.71	9.42	9.42	-7.67	170.1

47	38	-4342	-309	-1344	0	-220	-1888	15.71	15.71	9.42	9.42	-6.34	103.7
49	38	-3246	-257	-1606	0	-264	-2434	15.71	15.71	9.42	9.42	-8.23	222.8
50	38	-5220	-380	-1183	0	-194	-1560	15.71	15.71	9.42	9.42	-5.15	-69.3
51	38	-4396	-298	-1412	0	-195	-1863	15.71	15.71	9.42	9.42	-6.25	98.8

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	50	1021	-327	-3004	0	-134	-5464	15.71	15.71	9.42	9.42	-16.95	887.3
41	50	-2268	-481	-2216	0	-101	-3845	15.71	15.71	9.42	9.42	-12.70	479.8
42	50	-2429	-448	-2422	0	0	-3767	15.71	15.71	9.42	9.42	-12.48	460.4
43	50	2226	-138	-3092	0	-132	-5584	15.71	15.71	9.42	9.42	-16.88	966.0
44	50	-7643	-749	-978	0	-47	-1290	15.71	15.71	9.42	9.42	-4.73	-66.1
45	50	-3524	-340	-2123	0	92	-2755	15.71	15.71	9.42	9.42	-9.31	258.6
46	50	-3847	-343	-1518	0	-62	-2310	15.71	15.71	9.42	9.42	-7.82	180.1
47	50	-4242	-309	-1344	0	-52	-1926	15.71	15.71	9.42	9.42	-6.48	112.1
49	50	-3146	-257	-1606	0	-63	-2466	15.71	15.71	9.42	9.42	-8.33	231.8
50	50	-5120	-380	-1183	0	-46	-1607	15.71	15.71	9.42	9.42	-5.32	-71.1
51	50	-4296	-298	-1412	0	-18	-1900	15.71	15.71	9.42	9.42	-6.39	106.9

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 73 NI 1664 NF 48 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 31A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-4676	-1304	29	0	-134	-6404	15.71	15.71	9.42	9.42	-21.30	757.4
41	0	-7379	-1208	7	0	-101	-4746	15.71	15.71	9.42	9.42	-16.07	391.1
42	0	-7573	-1198	-652	0	0	-4680	15.71	15.71	9.42	9.42	-15.84	373.7
43	0	-3238	-1093	18	0	-132	-6444	15.71	15.71	9.42	9.42	-21.18	830.5
44	0	-11900	-1089	-36	0	-47	-2146	15.71	15.71	9.42	9.42	-7.67	-107.0
45	0	-8068	-916	-1118	0	92	-3570	15.71	15.71	9.42	9.42	-12.00	200.9
46	0	-7963	-766	-36	0	-62	-3040	15.71	15.71	9.42	9.42	-10.15	137.2
47	0	-8109	-656	-47	0	-52	-2614	15.71	15.71	9.42	9.42	-8.65	-115.5
49	0	-7208	-688	-39	0	-63	-3167	15.71	15.71	9.42	9.42	-10.64	176.6
50	0	-8939	-687	-50	0	-46	-2307	15.71	15.71	9.42	9.42	-7.65	-104.3
51	0	-8174	-652	-266	0	-18	-2592	15.71	15.71	9.42	9.42	-8.58	-114.6

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	12	-4576	-1304	29	0	-138	-6567	15.71	15.71	9.42	9.42	-21.81	786.7
41	12	-7279	-1208	7	0	-101	-4897	15.71	15.71	9.42	9.42	-16.58	417.1
42	12	-7473	-1198	-652	0	82	-4830	15.71	15.71	9.42	9.42	-16.35	399.4
43	12	-3138	-1093	18	0	-135	-6580	15.71	15.71	9.42	9.42	-21.60	856.1
44	12	-11800	-1089	-36	0	-42	-2282	15.71	15.71	9.42	9.42	-7.97	-110.8
45	12	-7968	-916	-1118	0	231	-3684	15.71	15.71	9.42	9.42	-12.41	219.5
46	12	-7863	-766	-36	0	-57	-3136	15.71	15.71	9.42	9.42	-10.49	151.9
47	12	-8009	-656	-47	0	-46	-2696	15.71	15.71	9.42	9.42	-8.94	-118.7
49	12	-7108	-688	-39	0	-58	-3253	15.71	15.71	9.42	9.42	-10.95	191.3
50	12	-8839	-687	-50	0	-40	-2393	15.71	15.71	9.42	9.42	-7.92	-107.4
51	12	-8074	-652	-266	0	15	-2674	15.71	15.71	9.42	9.42	-8.86	-117.9

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	25	-4476	-1304	29	0	-142	-6730	15.71	15.71	9.42	9.42	-22.32	816.2
41	25	-7179	-1208	7	0	-102	-5048	15.71	15.71	9.42	9.42	-17.08	443.4
42	25	-7373	-1198	-652	0	163	-4980	15.71	15.71	9.42	9.42	-16.85	425.3
43	25	-3038	-1093	18	0	-137	-6717	15.71	15.71	9.42	9.42	-22.01	881.7
44	25	-11700	-1089	-36	0	-38	-2418	15.71	15.71	9.42	9.42	-8.29	-114.9
45	25	-7868	-916	-1118	0	371	-3799	15.71	15.71	9.42	9.42	-12.81	238.4
46	25	-7763	-766	-36	0	-53	-3232	15.71	15.71	9.42	9.42	-10.83	167.0
47	25	-7909	-656	-47	0	-40	-2778	15.71	15.71	9.42	9.42	-9.23	-122.0
49	25	-7008	-688	-39	0	-53	-3339	15.71	15.71	9.42	9.42	-11.25	206.3
50	25	-8739	-687	-50	0	-34	-2479	15.71	15.71	9.42	9.42	-8.19	-110.7
51	25	-7974	-652	-266	0	48	-2755	15.71	15.71	9.42	9.42	-9.15	-121.1

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	38	-4376	-1304	29	0	-145	-6893	15.71	15.71	9.42	9.42	-22.82	845.6
41	38	-7079	-1208	7	0	-103	-5199	15.71	15.71	9.42	9.42	-17.58	469.8
42	38	-7273	-1198	-652	0	245	-5129	15.71	15.71	9.42	9.42	-17.35	451.4
43	38	-2938	-1093	18	0	-139	-6854	15.71	15.71	9.42	9.42	-22.43	907.3
44	38	-11600	-1089	-36	0	-33	-2554	15.71	15.71	9.42	9.42	-8.64	-119.2
45	38	-7768	-916	-1118	0	511	-3914	15.71	15.71	9.42	9.42	-13.21	257.7
46	38	-7663	-766	-36	0	-48	-3327	15.71	15.71	9.42	9.42	-11.17	182.5
47	38	-7809	-656	-47	0	-34	-2860	15.71	15.71	9.42	9.42	-9.52	-125.3
49	38	-6908	-688	-39	0	-48	-3425	15.71	15.71	9.42	9.42	-11.56	221.6
50	38	-8639	-687	-50	0	-27	-2565	15.71	15.71	9.42	9.42	-8.48	-114.0
51	38	-7874	-652	-266	0	82	-2836	15.71	15.71	9.42	9.42	-9.44	-124.4

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	50	-4276	-1304	29	0	-149	-7056	15.71	15.71	9.42	9.42	-23.33	875.1
41	50	-6979	-1208	7	0	-104	-5350	15.71	15.71	9.42	9.42	-18.08	496.4
42	50	-7173	-1198	-652	0	326	-5279	15.71	15.71	9.42	9.42	-17.85	477.7
43	50	-2838	-1093	18	0	-141	-6990	15.71	15.71	9.42	9.42	-22.84	932.9
44	50	-11500	-1089	-36	0	-29	-2690	15.71	15.71	9.42	9.42	-9.01	-123.8
45	50	-7668	-916	-1118	0	651	-4028	15.71	15.71	9.42	9.42	-13.61	277.3
46	50	-7563	-766	-36	0	-44	-3423	15.71	15.71	9.42	9.42	-11.52	198.4
47	50	-7709	-656	-47	0	-29	-2942	15.71	15.71	9.42	9.42	-9.82	132.7
49	50	-6808	-688	-39	0	-44	-3511	15.71	15.71	9.42	9.42	-11.86	237.1
50	50	-8539	-687	-50	0	-21	-2651	15.71	15.71	9.42	9.42	-8.77	-117.4
51	50	-7774	-652	-266	0	115	-2918	15.71	15.71	9.42	9.42	-9.73	128.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 74 NI 1667 NF 1665 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 30
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf

	cm		daN			daN*m			cm²			daN/cm²	
40	0	10780	-1420	-1606	0	-915	-11600	15.71	15.71	9.42	9.42	-32.18	2321.4
41	0	4626	-1316	-1145	0	-666	-8213	15.71	15.71	9.42	9.42	-24.26	1489.3
42	0	4707	-1343	-1355	0	-655	-8256	15.71	15.71	9.42	9.42	-24.36	1500.0
43	0	12400	-1235	-1689	0	-948	-12000	15.71	15.71	9.42	9.42	-32.60	2466.2
44	0	-5271	-1186	-417	0	-274	-2861	15.71	15.71	9.42	9.42	-9.67	203.5
45	0	2278	-1107	-1271	0	-514	-6423	15.71	15.71	9.42	9.42	-19.53	1096.9
46	0	654	-909	-786	0	-452	-5235	15.71	15.71	9.42	9.42	-16.35	833.9
47	0	-339	-808	-696	0	-399	-4490	15.71	15.71	9.42	9.42	-14.30	670.9
49	0	1713	-842	-850	0	-482	-5621	15.71	15.71	9.42	9.42	-17.20	945.9
50	0	-1822	-832	-595	0	-347	-3792	15.71	15.71	9.42	9.42	-12.45	492.7
51	0	-312	-816	-766	0	-395	-4504	15.71	15.71	9.42	9.42	-14.34	674.4

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	12	10880	-1420	-1606	0	-714	-11778	15.71	15.71	9.42	9.42	-32.71	2353.6
41	12	4726	-1316	-1145	0	-523	-8378	15.71	15.71	9.42	9.42	-24.74	1519.5
42	12	4807	-1343	-1355	0	-486	-8424	15.71	15.71	9.42	9.42	-24.86	1530.8
43	12	12500	-1235	-1689	0	-736	-12155	15.71	15.71	9.42	9.42	-33.05	2494.9
44	12	-5171	-1186	-417	0	-222	-3009	15.71	15.71	9.42	9.42	-10.18	228.4
45	12	2378	-1107	-1271	0	-355	-6562	15.71	15.71	9.42	9.42	-19.93	1123.2
46	12	754	-909	-786	0	-354	-5348	15.71	15.71	9.42	9.42	-16.67	856.3
47	12	-239	-808	-696	0	-312	-4591	15.71	15.71	9.42	9.42	-14.59	691.3
49	12	1813	-842	-850	0	-376	-5726	15.71	15.71	9.42	9.42	-17.49	967.0
50	12	-1722	-832	-595	0	-273	-3896	15.71	15.71	9.42	9.42	-12.76	513.3
51	12	-212	-816	-766	0	-300	-4606	15.71	15.71	9.42	9.42	-14.63	694.9

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	25	10980	-1420	-1606	0	-514	-11955	15.71	15.71	9.42	9.42	-33.24	2385.7
41	25	4826	-1316	-1145	0	-380	-8542	15.71	15.71	9.42	9.42	-25.22	1549.7
42	25	4907	-1343	-1355	0	-316	-8592	15.71	15.71	9.42	9.42	-25.35	1561.5
43	25	12600	-1235	-1689	0	-525	-12310	15.71	15.71	9.42	9.42	-33.51	2523.6
44	25	-5071	-1186	-417	0	-170	-3158	15.71	15.71	9.42	9.42	-10.69	253.7
45	25	2478	-1107	-1271	0	-196	-6700	15.71	15.71	9.42	9.42	-20.33	1149.4
46	25	854	-909	-786	0	-256	-5462	15.71	15.71	9.42	9.42	-17.00	878.6
47	25	-139	-808	-696	0	-225	-4692	15.71	15.71	9.42	9.42	-14.88	711.6
49	25	1913	-842	-850	0	-270	-5832	15.71	15.71	9.42	9.42	-17.79	988.1
50	25	-1622	-832	-595	0	-199	-4000	15.71	15.71	9.42	9.42	-13.07	533.9
51	25	-112	-816	-766	0	-204	-4708	15.71	15.71	9.42	9.42	-14.93	715.5

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	38	11080	-1420	-1606	0	-313	-12132	15.71	15.71	9.42	9.42	-33.77	2417.9
41	38	4926	-1316	-1145	0	-237	-8706	15.71	15.71	9.42	9.42	-25.71	1579.9
42	38	5007	-1343	-1355	0	-147	-8760	15.71	15.71	9.42	9.42	-25.84	1592.2
43	38	12700	-1235	-1689	0	-314	-12465	15.71	15.71	9.42	9.42	-33.97	2552.4
44	38	-4971	-1186	-417	0	-117	-3306	15.71	15.71	9.42	9.42	-11.19	279.2
45	38	2578	-1107	-1271	0	-37	-6838	15.71	15.71	9.42	9.42	-20.73	1175.6
46	38	954	-909	-786	0	-158	-5576	15.71	15.71	9.42	9.42	-17.33	901.0
47	38	-39	-808	-696	0	-138	-4793	15.71	15.71	9.42	9.42	-15.17	732.0
49	38	2013	-842	-850	0	-164	-5937	15.71	15.71	9.42	9.42	-18.08	1009.2
50	38	-1522	-832	-595	0	-124	-4104	15.71	15.71	9.42	9.42	-13.38	554.6
51	38	-12	-816	-766	0	-108	-4811	15.71	15.71	9.42	9.42	-15.22	736.1

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	50	11180	-1420	-1606	0	-112	-12310	15.71	15.71	9.42	9.42	-34.29	2450.1
41	50	5026	-1316	-1145	0	-94	-8871	15.71	15.71	9.42	9.42	-26.19	1610.1
42	50	5107	-1343	-1355	0	23	-8928	15.71	15.71	9.42	9.42	-26.34	1623.0
43	50	12800	-1235	-1689	0	-103	-12620	15.71	15.71	9.42	9.42	-34.42	2581.1
44	50	-4871	-1186	-417	0	-65	-3454	15.71	15.71	9.42	9.42	-11.69	305.1
45	50	2678	-1107	-1271	0	122	-6977	15.71	15.71	9.42	9.42	-21.13	1201.8
46	50	1054	-909	-786	0	-60	-5689	15.71	15.71	9.42	9.42	-17.65	923.3
47	50	61	-808	-696	0	-51	-4894	15.71	15.71	9.42	9.42	-15.46	752.4
49	50	2113	-842	-850	0	-57	-6042	15.71	15.71	9.42	9.42	-18.38	1030.4
50	50	-1422	-832	-595	0	-50	-4208	15.71	15.71	9.42	9.42	-13.69	575.3
51	50	88	-816	-766	0	-12	-4913	15.71	15.71	9.42	9.42	-15.51	756.6

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 75 NI 1684 NF 1683 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 29
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm		daN			daN*m			cm²			daN/cm²	
40	0	12590	-1230	375	0	54	-12620	15.71	15.71	9.42	9.42	-34.54	2570.2
41	0	5899	-1197	347	0	58	-8955	15.71	15.71	9.42	9.42	-26.06	1667.5
42	0	5775	-1171	154	0	65	-8872	15.71	15.71	9.42	9.42	-25.85	1648.5
43	0	14300	-1019	319	0	39	-13060	15.71	15.71	9.42	9.42	-35.01	2725.9
44	0	-4843	-1183	311	0	66	-3169	15.71	15.71	9.42	9.42	-10.73	264.5
45	0	2946	-920	-48	0	57	-6803	15.71	15.71	9.42	9.42	-20.47	1188.7
46	0	1505	-824	230	0	38	-5734	15.71	15.71	9.42	9.42	-17.63	952.7
47	0	406	-730	200	0	33	-4928	15.71	15.71	9.42	9.42	-15.46	774.7
49	0	2636	-741	209	0	31	-6151	15.71	15.71	9.42	9.42	-18.52	1073.4
50	0	-1193	-774	208	0	37	-4174	15.71	15.71	9.42	9.42	-13.53	581.1
51	0	365	-721	136	0	35	-4901	15.71	15.71	9.42	9.42	-15.39	768.5

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	12	12690	-1230	375	0	7	-12775	15.71	15.71	9.42	9.42	-34.99	2598.9
41	12	5999	-1197	347	0	14	-9105	15.71	15.71	9.42	9.42	-26.50	1695.4
42	12	5875	-1171	154	0	46	-9018	15.71	15.71	9.42	9.42	-26.28	1675.9
43	12	14400	-1019	319	0	-1	-13185	15.71	15.71	9.42	9.42	-35.37	2750.0
44	12	-4743	-1183	311	0	27	-3317	15.71	15.71	9.42	9.42	-11.22	290.2
45	12	3046	-920	-48	0	63	-6918	15.71	15.71	9.42	9.42	-20.80	1211.4
46	12	1605	-824	230	0	9	-5837	15.71	15.71	9.42	9.42	-17.92	973.5
47	12	506	-730	200	0	8	-5019	15.71	15.71	9.42	9.42	-15.71	793.6
49	12	2736	-741	209	0	5	-6244	15.71	15.71	9.42	9.42	-18.77	1092.6
50	12	-1093	-774	208	0	11	-4271	15.71	15.71	9.42	9.42	-13.81	600.7
51	12	465	-721	136	0	18	-4991	15.71	15.71	9.42	9.42	-15.64	787.2

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	25	12790	-1230	375	0	-40	-12930	15.71	15.71	9.42	9.42	-35.45	2627.7
41	25	6099	-1197	347	0	-29	-9254	15.71	15.71	9.42	9.42	-26.93	1723.4
42	25	5975	-1171	154	0	26	-9165	15.71	15.71	9.42	9.42	-26.70	1703.4
43	25	14500	-1019	319	0	-41	-13310	15.71	15.71	9.42	9.42	-35.73	2774.2
44	25	-4643	-1183	311	0	-12	-3464	15.71	15.71	9.42	9.42	-11.71	316.2
45	25	3146	-920	-48	0	69	-7033	15.71	15.71	9.42	9.42	-21.12	1234.0
46	25	1705	-824	230	0	-20	-5940	15.71	15.71	9.42	9.42	-18.21	994.3
47	25	606	-730	200	0	-17	-5110	15.71	15.71	9.42	9.42	-15.97	812.5
49	25	2836	-741	209	0	-21	-6336	15.71	15.71	9.42	9.42	-19.03	1111.9
50	25	-993	-774	208	0	-15	-4368	15.71	15.71	9.42	9.42	-14.09	620.3
51	25	565	-721	136	0	1	-5081	15.71	15.71	9.42	9.42	-15.89	806.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	38	12890	-1230	375	0	-86	-13085	15.71	15.71	9.42	9.42	-35.90	2656.4
41	38	6199	-1197	347	0	-73	-9404	15.71	15.71	9.42	9.42	-27.37	1751.3
42	38	6075	-1171	154	0	7	-9312	15.71	15.71	9.42	9.42	-27.13	1730.9
43	38	14600	-1019	319	0	-81	-13435	15.71	15.71	9.42	9.42	-36.08	2798.4
44	38	-4543	-1183	311	0	-51	-3612	15.71	15.71	9.42	9.42	-12.20	342.4
45	38	3246	-920	-48	0	75	-7148	15.71	15.71	9.42	9.42	-21.45	1256.6
46	38	1805	-824	230	0	-48	-6043	15.71	15.71	9.42	9.42	-18.50	1015.1
47	38	706	-730	200	0	-42	-5202	15.71	15.71	9.42	9.42	-16.23	831.5
49	38	2936	-741	209	0	-47	-6429	15.71	15.71	9.42	9.42	-19.28	1131.1
50	38	-893	-774	208	0	-41	-4464	15.71	15.71	9.42	9.42	-14.37	640.0
51	38	665	-721	136	0	-16	-5171	15.71	15.71	9.42	9.42	-16.14	824.7

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	50	12990	-1230	375	0	-133	-13240	15.71	15.71	9.42	9.42	-36.36	2685.1
41	50	6299	-1197	347	0	-116	-9554	15.71	15.71	9.42	9.42	-27.80	1779.3
42	50	6175	-1171	154	0	-12	-9458	15.71	15.71	9.42	9.42	-27.55	1758.3
43	50	14700	-1019	319	0	-120	-13560	15.71	15.71	9.42	9.42	-36.44	2822.5
44	50	-4443	-1183	311	0	-90	-3760	15.71	15.71	9.42	9.42	-12.68	368.7
45	50	3346	-920	-48	0	81	-7263	15.71	15.71	9.42	9.42	-21.77	1279.3
46	50	1905	-824	230	0	-77	-6146	15.71	15.71	9.42	9.42	-18.79	1035.8
47	50	806	-730	200	0	-67	-5293	15.71	15.71	9.42	9.42	-16.48	850.4
49	50	3036	-741	209	0	-73	-6522	15.71	15.71	9.42	9.42	-19.54	1150.3
50	50	-793	-774	208	0	-67	-4561	15.71	15.71	9.42	9.42	-14.65	659.7
51	50	765	-721	136	0	-33	-5261	15.71	15.71	9.42	9.42	-16.39	843.5

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 76 NI 1692 NF 1691 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 28
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	10870	-1653	2334	0	1009	-11660	15.71	15.71	9.42	9.42	-32.33	2335.2
41	0	4345	-1437	1806	0	770	-8059	15.71	15.71	9.42	9.42	-23.89	1451.5
42	0	4344	-1446	1613	0	764	-8061	15.71	15.71	9.42	9.42	-23.90	1451.8
43	0	12750	-1503	2309	0	1011	-12210	15.71	15.71	9.42	9.42	-33.09	2516.2
44	0	-6162	-1128	988	0	397	-2361	15.71	15.71	9.42	9.42	-7.88	107.2
45	0	1883	-1157	1109	0	602	-6217	15.71	15.71	9.42	9.42	-19.02	1045.6
46	0	410	-967	1204	0	517	-5108	15.71	15.71	9.42	9.42	-16.03	802.4
47	0	-573	-849	1054	0	453	-4370	15.71	15.71	9.42	9.42	-13.99	641.1
49	0	1600	-921	1230	0	533	-5569	15.71	15.71	9.42	9.42	-17.07	932.3
50	0	-2183	-846	965	0	410	-3599	15.71	15.71	9.42	9.42	-11.90	446.3
51	0	-574	-852	990	0	452	-4370	15.71	15.71	9.42	9.42	-13.99	641.1

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	12	10970	-1653	2334	0	717	-11865	15.71	15.71	9.42	9.42	-32.95	2371.5
41	12	4445	-1437	1806	0	544	-8239	15.71	15.71	9.42	9.42	-24.42	1484.1
42	12	4444	-1446	1613	0	562	-8242	15.71	15.71	9.42	9.42	-24.43	1484.5
43	12	12850	-1503	2309	0	722	-12398	15.71	15.71	9.42	9.42	-33.66	2549.9
44	12	-6062	-1128	988	0	273	-2502	15.71	15.71	9.42	9.42	-8.38	127.7
45	12	1983	-1157	1109	0	464	-6362	15.71	15.71	9.42	9.42	-19.45	1072.7
46	12	510	-967	1204	0	366	-5229	15.71	15.71	9.42	9.42	-16.38	825.9
47	12	-473	-849	1054	0	322	-4476	15.71	15.71	9.42	9.42	-14.30	662.2
49	12	1700	-921	1230	0	379	-5684	15.71	15.71	9.42	9.42	-17.40	954.9
50	12	-2083	-846	965	0	290	-3705	15.71	15.71	9.42	9.42	-12.22	467.1
51	12	-474	-852	990	0	328	-4476	15.71	15.71	9.42	9.42	-14.30	662.2

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	25	11070	-1653	2334	0	426	-12070	15.71	15.71	9.42	9.42	-33.57	2407.9
41	25	4545	-1437	1806	0	318	-8418	15.71	15.71	9.42	9.42	-24.95	1516.6
42	25	4544	-1446	1613	0	361	-8422	15.71	15.71	9.42	9.42	-24.97	1517.1
43	25	12950	-1503	2309	0	433	-12585	15.71	15.71	9.42	9.42	-34.22	2583.6
44	25	-5962	-1128	988	0	150	-2643	15.71	15.71	9.42	9.42	-8.88	149.1
45	25	2083	-1157	1109	0	325	-6506	15.71	15.71	9.42	9.42	-19.87	1099.9
46	25	610	-967	1204	0	216	-5350	15.71	15.71	9.42	9.42	-16.73	849.3
47	25	-373	-849	1054	0	190	-4582	15.71	15.71	9.42	9.42	-14.60	683.4
49	25	1800	-921	1230	0	226	-5800	15.71	15.71	9.42	9.42	-17.73	977.5
50	25	-1983	-846	965	0	169	-3810	15.71	15.71	9.42	9.42	-12.54	487.9
51	25	-374	-852	990	0	204	-4583	15.71	15.71	9.42	9.42	-14.60	683.4

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	38	11170	-1653	2334	0	134	-12275	15.71	15.71	9.42	9.42	-34.18	2444.2
41	38	4645	-1437	1806	0	92	-8598	15.71	15.71	9.42	9.42	-25.48	1549.1
42	38	4644	-1446	1613	0	159	-8603	15.71	15.71	9.42	9.42	-25.50	1549.8
43	38	13050	-1503	2309	0	145	-12772	15.71	15.71	9.42	9.42	-34.78	2617.2
44	38	-5862	-1128	988	0	27	-2784	15.71	15.71	9.42	9.42	-9.38	171.4
45	38	2183	-1157	1109	0	187	-6651	15.71	15.71	9.42	9.42	-20.29	1127.1
46	38	710	-967	1204	0	65	-5470	15.71	15.71	9.42	9.42	-17.07	872.8
47	38	-273	-849	1054	0	58	-4689	15.71	15.71	9.42	9.42	-14.91	704.6
49	38	1900	-921	1230	0	72	-5915	15.71	15.71	9.42	9.42	-18.06	1000.2
50	38	-1883	-846	965	0	48	-3916	15.71	15.71	9.42	9.42	-12.86	508.8
51	38	-274	-852	990	0	80	-4690	15.71	15.71	9.42	9.42	-14.91	704.6

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	50	11270	-1653	2334	0	-158	-12480	15.71	15.71	9.42	9.42	-34.80	2480.6
41	50	4745	-1437	1806	0	-134	-8778	15.71	15.71	9.42	9.42	-26.02	1581.7
42	50	4744	-1446	1613	0	-43	-8784	15.71	15.71	9.42	9.42	-26.04	1582.5
43	50	13150	-1503	2309	0	-144	-12960	15.71	15.71	9.42	9.42	-35.34	2650.9
44	50	-5762	-1128	988	0	-97	-2925	15.71	15.71	9.42	9.42	-9.88	194.2
45	50	2283	-1157	1109	0	48	-6796	15.71	15.71	9.42	9.42	-20.71	1154.2
46	50	810	-967	1204	0	-86	-5591	15.71	15.71	9.42	9.42	-17.42	896.2
47	50	-173	-849	1054	0	-74	-4795	15.71	15.71	9.42	9.42	-15.22	725.7
49	50	2000	-921	1230	0	-82	-6030	15.71	15.71	9.42	9.42	-18.39	1022.9
50	50	-1783	-846	965	0	-72	-4022	15.71	15.71	9.42	9.42	-13.17	529.6
51	50	-174	-852	990	0	-43	-4796	15.71	15.71	9.42	9.42	-15.22	725.9

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 77 NI 1700 NF 1699 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 27
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	717	-1588	4214	0	2055	-5187	15.71	15.71	9.42	9.42	-16.18	829.7
41	0	-3674	-1110	3105	0	1488	-2829	15.71	15.71	9.42	9.42	-9.56	263.2
42	0	-3634	-1159	2951	0	1500	-2904	15.71	15.71	9.42	9.42	-9.81	276.0
43	0	2804	-1662	4315	0	2122	-5934	15.71	15.71	9.42	9.42	-17.76	1048.7
44	0	-10890	-349	1363	0	593	972	15.71	15.71	9.42	9.42	-5.19	-71.8
45	0	-4448	-947	2209	0	1197	-2129	15.71	15.71	9.42	9.42	-7.49	132.3
46	0	-5017	-719	2083	0	989	-1510	15.71	15.71	9.42	9.42	-6.19	-69.9
47	0	-5353	-621	1827	0	864	-1180	15.71	15.71	9.42	9.42	-5.42	-63.7
49	0	-3889	-780	2197	0	1054	-1966	15.71	15.71	9.42	9.42	-6.64	130.0
50	0	-6629	-517	1606	0	748	-585	15.71	15.71	9.42	9.42	-4.83	-60.5
51	0	-5340	-637	1776	0	869	-1205	15.71	15.71	9.42	9.42	-5.44	-63.9

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	12	817	-1588	4214	0	1528	-5386	15.71	15.71	9.42	9.42	-16.77	865.1
41	12	-3574	-1110	3105	0	1100	-2968	15.71	15.71	9.42	9.42	-10.01	288.1
42	12	-3534	-1159	2951	0	1131	-3049	15.71	15.71	9.42	9.42	-10.28	301.9
43	12	2904	-1662	4315	0	1583	-6142	15.71	15.71	9.42	9.42	-18.38	1085.5
44	12	-10790	-349	1363	0	423	928	15.71	15.71	9.42	9.42	-4.91	-70.2
45	12	-4348	-947	2209	0	921	-2248	15.71	15.71	9.42	9.42	-7.59	152.1
46	12	-4917	-719	2083	0	729	-1600	15.71	15.71	9.42	9.42	-5.30	-70.6
47	12	-5253	-621	1827	0	636	-1258	15.71	15.71	9.42	9.42	-4.20	-57.6
49	12	-3789	-780	2197	0	779	-2064	15.71	15.71	9.42	9.42	-6.98	147.3
50	12	-6529	-517	1606	0	547	-649	15.71	15.71	9.42	9.42	-3.85	-49.9
51	12	-5240	-637	1776	0	647	-1284	15.71	15.71	9.42	9.42	-4.28	-58.6

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	25	917	-1588	4214	0	1002	-5584	15.71	15.71	9.42	9.42	-17.36	900.4
41	25	-3474	-1110	3105	0	712	-3106	15.71	15.71	9.42	9.42	-10.47	313.2
42	25	-3434	-1159	2951	0	762	-3194	15.71	15.71	9.42	9.42	-10.75	328.0
43	25	3004	-1662	4315	0	1043	-6350	15.71	15.71	9.42	9.42	-19.00	1122.4
44	25	-10690	-349	1363	0	252	884	15.71	15.71	9.42	9.42	-4.79	-68.7
45	25	-4248	-947	2209	0	644	-2366	15.71	15.71	9.42	9.42	-8.00	172.5
46	25	-4817	-719	2083	0	468	-1690	15.71	15.71	9.42	9.42	-5.61	-74.2
47	25	-5153	-621	1827	0	408	-1335	15.71	15.71	9.42	9.42	-4.43	-60.3
49	25	-3689	-780	2197	0	505	-2161	15.71	15.71	9.42	9.42	-7.31	165.0
50	25	-6429	-517	1606	0	346	-714	15.71	15.71	9.42	9.42	-3.24	-45.9
51	25	-5140	-637	1776	0	425	-1364	15.71	15.71	9.42	9.42	-4.52	-61.4

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	38	1017	-1588	4214	0	475	-5782	15.71	15.71	9.42	9.42	-17.96	935.8
41	38	-3374	-1110	3105	0	323	-3245	15.71	15.71	9.42	9.42	-10.91	338.4
42	38	-3334	-1159	2951	0	393	-3338	15.71	15.71	9.42	9.42	-11.21	354.2
43	38	3104	-1662	4315	0	504	-6557	15.71	15.71	9.42	9.42	-19.62	1159.2
44	38	-10590	-349	1363	0	82	841	15.71	15.71	9.42	9.42	-4.68	-67.1
45	38	-4148	-947	2209	0	368	-2484	15.71	15.71	9.42	9.42	-8.41	193.3
46	38	-4717	-719	2083	0	208	-1779	15.71	15.71	9.42	9.42	-5.93	78.7
47	38	-5053	-621	1827	0	179	-1412	15.71	15.71	9.42	9.42	-4.67	-63.2
49	38	-3589	-780	2197	0	230	-2258	15.71	15.71	9.42	9.42	-7.65	183.0
50	38	-6329	-517	1606	0	145	-779	15.71	15.71	9.42	9.42	-3.33	-47.2
51	38	-5040	-637	1776	0	203	-1444	15.71	15.71	9.42	9.42	-4.77	-64.4

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	50	1117	-1588	4214	0	-52	-5981	15.71	15.71	9.42	9.42	-18.55	971.2
41	50	-3274	-1110	3105	0	-65	-3384	15.71	15.71	9.42	9.42	-11.36	363.7
42	50	-3234	-1159	2951	0	25	-3483	15.71	15.71	9.42	9.42	-11.67	380.5
43	50	3204	-1662	4315	0	-36	-6765	15.71	15.71	9.42	9.42	-20.24	1196.0
44	50	-10490	-349	1363	0	-88	797	15.71	15.71	9.42	9.42	-4.57	-65.6
45	50	-4048	-947	2209	0	92	-2603	15.71	15.71	9.42	9.42	-8.81	214.4
46	50	-4617	-719	2083	0	-52	-1869	15.71	15.71	9.42	9.42	-6.26	92.6
47	50	-4953	-621	1827	0	-49	-1490	15.71	15.71	9.42	9.42	-4.92	-66.2
49	50	-3489	-780	2197	0	-45	-2356	15.71	15.71	9.42	9.42	-7.97	201.2
50	50	-6229	-517	1606	0	-55	-843	15.71	15.71	9.42	9.42	-3.43	-48.4
51	50	-4940	-637	1776	0	-19	-1523	15.71	15.71	9.42	9.42	-5.04	-67.5

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 78 NI 1665 NF 91 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 30A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	2947	-3346	314	0	-112	-13640	15.71	15.71	9.42	9.42	-42.17	2234.7
41	0	-1956	-2723	312	0	-94	-10060	15.71	15.71	9.42	9.42	-32.37	1444.9
42	0	-1893	-2748	-334	0	23	-10120	15.71	15.71	9.42	9.42	-32.54	1457.2

43	0	4746	-3179	240	0	-103	-13880	15.71	15.71	9.42	9.42	-42.27	2361.6
44	0	-9947	-1780	311	0	-65	-4437	15.71	15.71	9.42	9.42	-14.92	252.4
45	0	-3321	-2183	-840	0	122	-8002	15.71	15.71	9.42	9.42	-26.16	1064.5
46	0	-4307	-1791	191	0	-60	-6611	15.71	15.71	9.42	9.42	-21.91	805.9
47	0	-4895	-1558	161	0	-51	-5749	15.71	15.71	9.42	9.42	-19.22	648.0
49	0	-3260	-1766	161	0	-57	-6943	15.71	15.71	9.42	9.42	-22.78	905.7
50	0	-6199	-1486	176	0	-50	-5056	15.71	15.71	9.42	9.42	-17.07	486.0
51	0	-4874	-1567	-55	0	-12	-5769	15.71	15.71	9.42	9.42	-19.28	652.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	12	3047	-3346	314	0	-152	-14058	15.71	15.71	9.42	9.42	-43.46	2303.6
41	12	-1856	-2723	312	0	-133	-10400	15.71	15.71	9.42	9.42	-33.42	1501.8
42	12	-1793	-2748	-334	0	64	-10462	15.71	15.71	9.42	9.42	-33.60	1514.4
43	12	4846	-3179	240	0	-133	-14278	15.71	15.71	9.42	9.42	-43.49	2427.4
44	12	-9847	-1780	311	0	-104	-4660	15.71	15.71	9.42	9.42	-15.70	285.5
45	12	-3221	-2183	-840	0	227	-8275	15.71	15.71	9.42	9.42	-27.01	1111.0
46	12	-4207	-1791	191	0	-84	-6835	15.71	15.71	9.42	9.42	-22.61	844.6
47	12	-4795	-1558	161	0	-71	-5944	15.71	15.71	9.42	9.42	-19.83	682.1
49	12	-3160	-1766	161	0	-77	-7164	15.71	15.71	9.42	9.42	-23.46	944.1
50	12	-6099	-1486	176	0	-72	-5242	15.71	15.71	9.42	9.42	-17.68	518.1
51	12	-4774	-1567	-55	0	-6	-5965	15.71	15.71	9.42	9.42	-19.90	686.2

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	25	3147	-3346	314	0	-191	-14475	15.71	15.71	9.42	9.42	-44.74	2372.5
41	25	-1756	-2723	312	0	-172	-10740	15.71	15.71	9.42	9.42	-34.47	1558.7
42	25	-1693	-2748	-334	0	106	-10805	15.71	15.71	9.42	9.42	-34.66	1571.7
43	25	4946	-3179	240	0	-163	-14675	15.71	15.71	9.42	9.42	-44.72	2493.2
44	25	-9747	-1780	311	0	-143	-4882	15.71	15.71	9.42	9.42	-16.48	319.4
45	25	-3121	-2183	-840	0	332	-8548	15.71	15.71	9.42	9.42	-27.85	1157.5
46	25	-4107	-1791	191	0	-107	-7058	15.71	15.71	9.42	9.42	-23.31	883.4
47	25	-4695	-1558	161	0	-91	-6138	15.71	15.71	9.42	9.42	-20.45	716.2
49	25	-3060	-1766	161	0	-98	-7384	15.71	15.71	9.42	9.42	-24.14	982.6
50	25	-5999	-1486	176	0	-94	-5428	15.71	15.71	9.42	9.42	-18.28	550.2
51	25	-4674	-1567	-55	0	1	-6160	15.71	15.71	9.42	9.42	-20.52	720.5

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	38	3247	-3346	314	0	-230	-14892	15.71	15.71	9.42	9.42	-46.03	2441.4
41	38	-1656	-2723	312	0	-211	-11080	15.71	15.71	9.42	9.42	-35.52	1615.6
42	38	-1593	-2748	-334	0	148	-11148	15.71	15.71	9.42	9.42	-35.71	1629.0
43	38	5046	-3179	240	0	-193	-15072	15.71	15.71	9.42	9.42	-45.94	2559.1
44	38	-9647	-1780	311	0	-182	-5104	15.71	15.71	9.42	9.42	-17.25	354.0
45	38	-3021	-2183	-840	0	437	-8821	15.71	15.71	9.42	9.42	-28.70	1204.0
46	38	-4007	-1791	191	0	-131	-7282	15.71	15.71	9.42	9.42	-24.00	922.2
47	38	-4595	-1558	161	0	-111	-6333	15.71	15.71	9.42	9.42	-21.06	750.3
49	38	-2960	-1766	161	0	-118	-7605	15.71	15.71	9.42	9.42	-24.82	1021.1
50	38	-5899	-1486	176	0	-116	-5613	15.71	15.71	9.42	9.42	-18.88	582.5
51	38	-4574	-1567	-55	0	8	-6356	15.71	15.71	9.42	9.42	-21.13	754.8

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	50	3347	-3346	314	0	-269	-15310	15.71	15.71	9.42	9.42	-47.32	2510.3
41	50	-1556	-2723	312	0	-250	-11420	15.71	15.71	9.42	9.42	-36.57	1672.6
42	50	-1493	-2748	-334	0	190	-11490	15.71	15.71	9.42	9.42	-36.77	1686.3
43	50	5146	-3179	240	0	-223	-15470	15.71	15.71	9.42	9.42	-47.16	2624.9
44	50	-9547	-1780	311	0	-221	-5327	15.71	15.71	9.42	9.42	-18.02	389.1
45	50	-2921	-2183	-840	0	542	-9094	15.71	15.71	9.42	9.42	-29.54	1250.6
46	50	-3907	-1791	191	0	-155	-7506	15.71	15.71	9.42	9.42	-24.70	961.0
47	50	-4495	-1558	161	0	-132	-6528	15.71	15.71	9.42	9.42	-21.67	784.6
49	50	-2860	-1766	161	0	-138	-7826	15.71	15.71	9.42	9.42	-25.50	1059.6
50	50	-5799	-1486	176	0	-138	-5799	15.71	15.71	9.42	9.42	-19.48	614.9
51	50	-4474	-1567	-55	0	15	-6552	15.71	15.71	9.42	9.42	-21.74	789.2

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 79 NI 1683 NF 134 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 29A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	

40	0	4289	-3440	811	0	-133	-14630	15.71	15.71	9.42	9.42	-44.82	2453.4
41	0	-1030	-2804	710	0	-116	-10790	15.71	15.71	9.42	9.42	-34.43	1601.8
42	0	-1121	-2770	135	0	-12	-10690	15.71	15.71	9.42	9.42	-34.14	1582.0
43	0	6170	-3263	731	0	-120	-14890	15.71	15.71	9.42	9.42	-44.92	2587.8
44	0	-9678	-1845	557	0	-90	-4769	15.71	15.71	9.42	9.42	-16.09	306.4
45	0	-2847	-2147	-395	0	81	-8317	15.71	15.71	9.42	9.42	-27.06	1135.3
46	0	-3693	-1843	476	0	-77	-7102	15.71	15.71	9.42	9.42	-23.37	909.5
47	0	-4359	-1603	417	0	-67	-6180	15.71	15.71	9.42	9.42	-20.53	737.9
49	0	-2586	-1814	451	0	-73	-7460	15.71	15.71	9.42	9.42	-24.28	1016.8
50	0	-5756	-1531	416	0	-67	-5436	15.71	15.71	9.42	9.42	-18.29	562.2
51	0	-4389	-1591	225	0	-33	-6146	15.71	15.71	9.42	9.42	-20.43	731.4

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	12	4389	-3440	811	0	-235	-15060	15.71	15.71	9.42	9.42	-46.15	2524.2
41	12	-930	-2804	710	0	-205	-11140	15.71	15.71	9.42	9.42	-35.51	1660.2
42	12	-1021	-2770	135	0	-29	-11038	15.71	15.71	9.42	9.42	-35.21	1640.1
43	12	6270	-3263	731	0	-212	-15298	15.71	15.71	9.42	9.42	-46.17	2655.1
44	12	-9578	-1845	557	0	-159	-5000	15.71	15.71	9.42	9.42	-16.89	341.9
45	12	-2747	-2147	-395	0	131	-8585	15.71	15.71	9.42	9.42	-27.89	1181.1
46	12	-3593	-1843	476	0	-137	-7332	15.71	15.71	9.42	9.42	-24.09	949.3
47	12	-4259	-1603	417	0	-120	-6380	15.71	15.71	9.42	9.42	-21.16	773.0
49	12	-2486	-1814	451	0	-130	-7687	15.71	15.71	9.42	9.42	-24.98	1056.2
50	12	-5656	-1531	416	0	-119	-5628	15.71	15.71	9.42	9.42	-18.90	595.4
51	12	-4289	-1591	225	0	-61	-6345	15.71	15.71	9.42	9.42	-21.05	766.3

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	25	4489	-3440	811	0	-336	-15490	15.71	15.71	9.42	9.42	-47.47	2595.0
41	25	-830	-2804	710	0	-294	-11490	15.71	15.71	9.42	9.42	-36.58	1718.7
42	25	-921	-2770	135	0	-46	-11385	15.71	15.71	9.42	9.42	-36.28	1698.2
43	25	6370	-3263	731	0	-303	-15705	15.71	15.71	9.42	9.42	-47.43	2722.5

44	25	-9478	-1845	557	0	-229	-5230	15.71	15.71	9.42	9.42	-17.69	378.0
45	25	-2647	-2147	-395	0	180	-8854	15.71	15.71	9.42	9.42	-28.72	1226.9
46	25	-3493	-1843	476	0	-196	-7562	15.71	15.71	9.42	9.42	-24.80	989.2
47	25	-4159	-1603	417	0	-172	-6580	15.71	15.71	9.42	9.42	-21.79	808.2
49	25	-2386	-1814	451	0	-186	-7914	15.71	15.71	9.42	9.42	-25.67	1095.7
50	25	-5556	-1531	416	0	-171	-5819	15.71	15.71	9.42	9.42	-19.52	628.8
51	25	-4189	-1591	225	0	-89	-6544	15.71	15.71	9.42	9.42	-21.67	801.2

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	38	4589	-3440	811	0	-437	-15920	15.71	15.71	9.42	9.42	-48.80	2665.8
41	38	-730	-2804	710	0	-382	-11840	15.71	15.71	9.42	9.42	-37.66	1777.2
42	38	-821	-2770	135	0	-63	-11732	15.71	15.71	9.42	9.42	-37.35	1756.3
43	38	6470	-3263	731	0	-395	-16112	15.71	15.71	9.42	9.42	-48.69	2789.8
44	38	-9378	-1845	557	0	-299	-5460	15.71	15.71	9.42	9.42	-18.48	414.6
45	38	-2547	-2147	-395	0	229	-9122	15.71	15.71	9.42	9.42	-29.54	1272.8
46	38	-3393	-1843	476	0	-256	-7793	15.71	15.71	9.42	9.42	-25.51	1029.1
47	38	-4059	-1603	417	0	-224	-6781	15.71	15.71	9.42	9.42	-22.41	843.3
49	38	-2286	-1814	451	0	-242	-8140	15.71	15.71	9.42	9.42	-26.37	1135.2
50	38	-5456	-1531	416	0	-223	-6010	15.71	15.71	9.42	9.42	-20.13	662.2
51	38	-4089	-1591	225	0	-117	-6743	15.71	15.71	9.42	9.42	-22.29	836.2

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	50	4689	-3440	811	0	-539	-16350	15.71	15.71	9.42	9.42	-50.13	2736.6
41	50	-630	-2804	710	0	-471	-12190	15.71	15.71	9.42	9.42	-38.74	1835.7
42	50	-721	-2770	135	0	-80	-12080	15.71	15.71	9.42	9.42	-38.42	1814.4
43	50	6570	-3263	731	0	-486	-16520	15.71	15.71	9.42	9.42	-49.94	2857.2
44	50	-9278	-1845	557	0	-368	-5691	15.71	15.71	9.42	9.42	-19.27	451.7
45	50	-2447	-2147	-395	0	279	-9390	15.71	15.71	9.42	9.42	-30.37	1318.6
46	50	-3293	-1843	476	0	-315	-8023	15.71	15.71	9.42	9.42	-26.22	1069.1
47	50	-3959	-1603	417	0	-276	-6981	15.71	15.71	9.42	9.42	-23.03	878.5
49	50	-2186	-1814	451	0	-299	-8367	15.71	15.71	9.42	9.42	-27.06	1174.7
50	50	-5356	-1531	416	0	-275	-6202	15.71	15.71	9.42	9.42	-20.74	695.6
51	50	-3989	-1591	225	0	-146	-6942	15.71	15.71	9.42	9.42	-22.91	871.2

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 80 NI 1691 NF 177 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 28A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	3144	-3459	1122	0	-158	-13780	15.71	15.71	9.42	9.42	-42.54	2266.0
41	0	-2106	-2737	966	0	-134	-9937	15.71	15.71	9.42	9.42	-32.02	1418.8
42	0	-2103	-2741	434	0	-43	-9942	15.71	15.71	9.42	9.42	-32.03	1419.7
43	0	5168	-3345	1021	0	-144	-14190	15.71	15.71	9.42	9.42	-43.09	2430.2
44	0	-10670	-1631	734	0	-97	-3883	15.71	15.71	9.42	9.42	-12.93	-170.2
45	0	-3578	-2148	-126	0	48	-7794	15.71	15.71	9.42	9.42	-25.55	1020.5
46	0	-4468	-1782	638	0	-86	-6495	15.71	15.71	9.42	9.42	-21.56	780.8
47	0	-5058	-1544	556	0	-74	-5635	15.71	15.71	9.42	9.42	-18.87	623.4
49	0	-3308	-1785	608	0	-82	-6916	15.71	15.71	9.42	9.42	-22.70	899.3
50	0	-6476	-1442	551	0	-72	-4854	15.71	15.71	9.42	9.42	-16.41	444.3
51	0	-5057	-1545	379	0	-43	-5637	15.71	15.71	9.42	9.42	-18.87	623.7

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	12	3244	-3459	1122	0	-298	-14212	15.71	15.71	9.42	9.42	-43.88	2337.2
41	12	-2006	-2737	966	0	-254	-10280	15.71	15.71	9.42	9.42	-33.08	1476.2
42	12	-2003	-2741	434	0	-97	-10284	15.71	15.71	9.42	9.42	-33.09	1476.9
43	12	5268	-3345	1021	0	-272	-14608	15.71	15.71	9.42	9.42	-44.38	2499.1
44	12	-10570	-1631	734	0	-189	-4087	15.71	15.71	9.42	9.42	-13.65	188.3
45	12	-3478	-2148	-126	0	64	-8062	15.71	15.71	9.42	9.42	-26.39	1066.3
46	12	-4368	-1782	638	0	-165	-6718	15.71	15.71	9.42	9.42	-22.26	819.4
47	12	-4958	-1544	556	0	-143	-5828	15.71	15.71	9.42	9.42	-19.48	657.1
49	12	-3208	-1785	608	0	-158	-7139	15.71	15.71	9.42	9.42	-23.39	938.1
50	12	-6376	-1442	551	0	-141	-5034	15.71	15.71	9.42	9.42	-17.01	475.2
51	12	-4957	-1545	379	0	-91	-5830	15.71	15.71	9.42	9.42	-19.49	657.4

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	25	3344	-3459	1122	0	-438	-14645	15.71	15.71	9.42	9.42	-45.21	2408.4
41	25	-1906	-2737	966	0	-375	-10624	15.71	15.71	9.42	9.42	-34.14	1533.6
42	25	-1903	-2741	434	0	-151	-10626	15.71	15.71	9.42	9.42	-34.15	1534.1
43	25	5368	-3345	1021	0	-399	-15025	15.71	15.71	9.42	9.42	-45.66	2568.0
44	25	-10470	-1631	734	0	-280	-4290	15.71	15.71	9.42	9.42	-14.37	216.6
45	25	-3378	-2148	-126	0	80	-8331	15.71	15.71	9.42	9.42	-27.22	1112.1
46	25	-4268	-1782	638	0	-245	-6941	15.71	15.71	9.42	9.42	-22.96	858.0
47	25	-4858	-1544	556	0	-213	-6021	15.71	15.71	9.42	9.42	-20.09	690.9
49	25	-3108	-1785	608	0	-234	-7362	15.71	15.71	9.42	9.42	-24.08	976.9
50	25	-6276	-1442	551	0	-210	-5214	15.71	15.71	9.42	9.42	-17.60	506.3
51	25	-4857	-1545	379	0	-138	-6023	15.71	15.71	9.42	9.42	-20.10	691.2

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	38	3444	-3459	1122	0	-579	-15078	15.71	15.71	9.42	9.42	-46.55	2479.6
41	38	-1806	-2737	966	0	-496	-10967	15.71	15.71	9.42	9.42	-35.20	1591.0
42	38	-1803	-2741	434	0	-205	-10968	15.71	15.71	9.42	9.42	-35.20	1591.3
43	38	5468	-3345	1021	0	-527	-15442	15.71	15.71	9.42	9.42	-46.95	2636.9
44	38	-10370	-1631	734	0	-372	-4494	15.71	15.71	9.42	9.42	-15.09	245.9
45	38	-3278	-2148	-126	0	95	-8600	15.71	15.71	9.42	9.42	-28.05	1157.9
46	38	-4168	-1782	638	0	-325	-7164	15.71	15.71	9.42	9.42	-23.66	896.6
47	38	-4758	-1544	556	0	-282	-6214	15.71	15.71	9.42	9.42	-20.70	724.7
49	38	-3008	-1785	608	0	-310	-7586	15.71	15.71	9.42	9.42	-24.77	1015.8
50	38	-6176	-1442	551	0	-279	-5395	15.71	15.71	9.42	9.42	-18.18	537.6
51	38	-4757	-1545	379	0	-185	-6216	15.71	15.71	9.42	9.42	-20.71	725.1

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	50	3544	-3459	1122	0	-719	-15510	15.71	15.71	9.42	9.42	-47.88	2550.8
41	50	-1706	-2737	966	0	-617	-11310	15.71	15.71	9.42	9.42	-36.26	1648.4
42	50	-1703	-2741	434	0	-260	-11310	15.71	15.71	9.42	9.42	-36.26	1648.6
43	50	5568	-3345	1021	0	-654	-15860	15.71	15.71	9.42	9.42	-48.24	2705.8
44	50	-10270	-1631	734	0	-464	-4698	15.71	15.71	9.42	9.42	-15.81	276.1

45	50	-3178	-2148	-126	0	111	-8868	15.71	15.71	9.42	9.42	-28.88	1203.7
46	50	-4068	-1782	638	0	-405	-7387	15.71	15.71	9.42	9.42	-24.35	935.3
47	50	-4658	-1544	556	0	-352	-6407	15.71	15.71	9.42	9.42	-21.31	758.6
49	50	-2908	-1785	608	0	-386	-7809	15.71	15.71	9.42	9.42	-25.46	1054.7
50	50	-6076	-1442	551	0	-348	-5575	15.71	15.71	9.42	9.42	-18.77	569.0
51	50	-4657	-1545	379	0	-233	-6409	15.71	15.71	9.42	9.42	-21.31	759.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 81 NI 1699 NF 220 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 27A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-3789	-2583	1407	0	-52	-6859	15.71	15.71	9.42	9.42	-22.61	867.9
41	0	-7621	-1843	1303	0	-65	-4215	15.71	15.71	9.42	9.42	-14.26	305.3
42	0	-7643	-1902	813	0	25	-4326	15.71	15.71	9.42	9.42	-14.64	320.2
43	0	-1558	-2643	1239	0	-36	-7576	15.71	15.71	9.42	9.42	-24.40	1084.0
44	0	-14010	-676	1174	0	-88	26	15.71	15.71	9.42	9.42	-4.15	-61.0
45	0	-7980	-1507	248	0	92	-3353	15.71	15.71	9.42	9.42	-11.24	175.6
46	0	-8139	-1149	923	0	-52	-2540	15.71	15.71	9.42	9.42	-8.40	-112.5
47	0	-8268	-976	828	0	-49	-2122	15.71	15.71	9.42	9.42	-7.04	-96.0
49	0	-6991	-1222	863	0	-45	-3003	15.71	15.71	9.42	9.42	-10.08	162.3
50	0	-9482	-829	850	0	-55	-1483	15.71	15.71	9.42	9.42	-5.62	-78.8
51	0	-8275	-995	665	0	-19	-2159	15.71	15.71	9.42	9.42	-7.16	-97.4

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	12	-3689	-2583	1407	0	-228	-7182	15.71	15.71	9.42	9.42	-23.62	921.9
41	12	-7521	-1843	1303	0	-228	-4445	15.71	15.71	9.42	9.42	-15.05	342.0
42	12	-7543	-1902	813	0	-77	-4564	15.71	15.71	9.42	9.42	-15.45	358.1
43	12	-1458	-2643	1239	0	-191	-7906	15.71	15.71	9.42	9.42	-25.42	1139.4
44	12	-13910	-676	1174	0	-235	-59	15.71	15.71	9.42	9.42	-4.67	-66.8
45	12	-7880	-1507	248	0	61	-3542	15.71	15.71	9.42	9.42	-11.91	203.5
46	12	-8039	-1149	923	0	-168	-2684	15.71	15.71	9.42	9.42	-8.90	-118.3
47	12	-8168	-976	828	0	-153	-2244	15.71	15.71	9.42	9.42	-7.42	-100.6
49	12	-6891	-1222	863	0	-153	-3156	15.71	15.71	9.42	9.42	-10.62	185.7
50	12	-9382	-829	850	0	-162	-1586	15.71	15.71	9.42	9.42	-5.81	-81.3
51	12	-8175	-995	665	0	-102	-2283	15.71	15.71	9.42	9.42	-7.55	-102.1

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	25	-3589	-2583	1407	0	-404	-7505	15.71	15.71	9.42	9.42	-24.63	975.9
41	25	-7421	-1843	1303	0	-390	-4676	15.71	15.71	9.42	9.42	-15.83	379.1
42	25	-7443	-1902	813	0	-179	-4802	15.71	15.71	9.42	9.42	-16.26	396.5
43	25	-1358	-2643	1239	0	-346	-8236	15.71	15.71	9.42	9.42	-26.44	1194.8
44	25	-13810	-676	1174	0	-382	-143	15.71	15.71	9.42	9.42	-5.20	-72.6
45	25	-7780	-1507	248	0	30	-3730	15.71	15.71	9.42	9.42	-12.57	232.2
46	25	-7939	-1149	923	0	-283	-2828	15.71	15.71	9.42	9.42	-9.40	-124.1
47	25	-8068	-976	828	0	-256	-2366	15.71	15.71	9.42	9.42	-7.82	-105.3
49	25	-6791	-1222	863	0	-261	-3308	15.71	15.71	9.42	9.42	-11.16	209.8
50	25	-9282	-829	850	0	-268	-1690	15.71	15.71	9.42	9.42	-6.02	-83.9
51	25	-8075	-995	665	0	-186	-2408	15.71	15.71	9.42	9.42	-7.96	-107.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	38	-3489	-2583	1407	0	-580	-7828	15.71	15.71	9.42	9.42	-25.64	1029.9
41	38	-7321	-1843	1303	0	-553	-4906	15.71	15.71	9.42	9.42	-16.61	416.7
42	38	-7343	-1902	813	0	-280	-5039	15.71	15.71	9.42	9.42	-17.05	435.3
43	38	-1258	-2643	1239	0	-500	-8567	15.71	15.71	9.42	9.42	-27.46	1250.3
44	38	-13710	-676	1174	0	-529	-228	15.71	15.71	9.42	9.42	-5.72	-78.3
45	38	-7680	-1507	248	0	-1	-3918	15.71	15.71	9.42	9.42	-13.23	261.6
46	38	-7839	-1149	923	0	-398	-2971	15.71	15.71	9.42	9.42	-9.91	132.5
47	38	-7968	-976	828	0	-360	-2488	15.71	15.71	9.42	9.42	-8.23	-110.2
49	38	-6691	-1222	863	0	-368	-3461	15.71	15.71	9.42	9.42	-11.69	234.5
50	38	-9182	-829	850	0	-374	-1794	15.71	15.71	9.42	9.42	-6.25	-86.8
51	38	-7975	-995	665	0	-269	-2532	15.71	15.71	9.42	9.42	-8.38	-112.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	50	-3389	-2583	1407	0	-756	-8151	15.71	15.71	9.42	9.42	-26.65	1084.0
41	50	-7221	-1843	1303	0	-716	-5136	15.71	15.71	9.42	9.42	-17.38	454.6
42	50	-7243	-1902	813	0	-382	-5277	15.71	15.71	9.42	9.42	-17.85	474.4
43	50	-1158	-2643	1239	0	-655	-8897	15.71	15.71	9.42	9.42	-28.47	1305.7
44	50	-13610	-676	1174	0	-675	-312	15.71	15.71	9.42	9.42	-6.24	-84.1
45	50	-7580	-1507	248	0	-32	-4107	15.71	15.71	9.42	9.42	-13.89	291.7
46	50	-7739	-1149	923	0	-514	-3115	15.71	15.71	9.42	9.42	-10.42	153.0
47	50	-7868	-976	828	0	-463	-2610	15.71	15.71	9.42	9.42	-8.65	-115.1
49	50	-6591	-1222	863	0	-476	-3614	15.71	15.71	9.42	9.42	-12.22	259.6
50	50	-9082	-829	850	0	-480	-1897	15.71	15.71	9.42	9.42	-6.49	-89.8
51	50	-7875	-995	665	0	-352	-2656	15.71	15.71	9.42	9.42	-8.81	-117.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 82 NI 1351 NF 1360 SEZ. Rp B= 0.400 H= 0.600 (pilastro)
PIL. NUM. 16
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-10050	1877	541	0	1061	-5262	12.57	12.57	6.28	6.28	-34.60	940.6
41	0	-10070	958	552	0	1086	-2624	12.57	12.57	6.28	6.28	-16.44	-206.2
42	0	-10000	963	488	0	912	-2639	12.57	12.57	6.28	6.28	-16.56	-207.2
43	0	-9881	2326	524	0	1029	-6563	12.57	12.57	6.28	6.28	-43.22	1349.4
44	0	-9900	-547	552	0	1089	1700	12.57	12.57	6.28	6.28	-10.51	-139.8
45	0	-9806	803	436	0	782	-2190	12.57	12.57	6.28	6.28	-13.52	-173.8
46	0	-9827	696	538	0	1063	-1889	12.57	12.57	6.28	6.28	-11.60	-152.3
47	0	-9767	631	534	0	1057	-1705	12.57	12.57	6.28	6.28	-10.53	-139.8
49	0	-9760	937	530	0	1049	-2585	12.57	12.57	6.28	6.28	-16.23	-202.9

50	0	-9764	362	536	0	1061	-933	12.57	12.57	6.28	6.28	-9.08	-114.4
51	0	-9745	632	513	0	999	-1711	12.57	12.57	6.28	6.28	-10.56	-140.1

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	12	-9974	1877	541	0	993	-5028	12.57	12.57	6.28	6.28	-33.03	874.8
41	12	-9994	958	552	0	1017	-2504	12.57	12.57	6.28	6.28	-15.62	-197.2
42	12	-9925	963	488	0	851	-2518	12.57	12.57	6.28	6.28	-15.74	-198.2
43	12	-9806	2326	524	0	964	-6272	12.57	12.57	6.28	6.28	-41.31	1265.0
44	12	-9825	-547	552	0	1020	1632	12.57	12.57	6.28	6.28	-10.13	-135.2
45	12	-9731	803	436	0	727	-2090	12.57	12.57	6.28	6.28	-12.87	-166.4
46	12	-9752	696	538	0	996	-1802	12.57	12.57	6.28	6.28	-11.08	-146.2
47	12	-9692	631	534	0	990	-1626	12.57	12.57	6.28	6.28	-10.09	-134.5
49	12	-9685	937	530	0	983	-2468	12.57	12.57	6.28	6.28	-15.43	-194.2
50	12	-9689	362	536	0	994	-887	12.57	12.57	6.28	6.28	-8.62	-109.5
51	12	-9670	632	513	0	935	-1632	12.57	12.57	6.28	6.28	-10.11	-134.7

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	25	-9898	1877	541	0	926	-4793	12.57	12.57	6.28	6.28	-31.46	809.2
41	25	-9918	958	552	0	948	-2384	12.57	12.57	6.28	6.28	-14.81	-188.2
42	25	-9850	963	488	0	790	-2398	12.57	12.57	6.28	6.28	-14.92	-189.2
43	25	-9731	2326	524	0	898	-5982	12.57	12.57	6.28	6.28	-39.39	1180.8
44	25	-9750	-547	552	0	951	1563	12.57	12.57	6.28	6.28	-9.76	-130.7
45	25	-9656	803	436	0	673	-1989	12.57	12.57	6.28	6.28	-12.23	-159.0
46	25	-9677	696	538	0	929	-1715	12.57	12.57	6.28	6.28	-10.58	-140.2
47	25	-9617	631	534	0	924	-1548	12.57	12.57	6.28	6.28	-9.66	-129.3
49	25	-9610	937	530	0	916	-2351	12.57	12.57	6.28	6.28	-14.63	-185.4
50	25	-9614	362	536	0	927	-842	12.57	12.57	6.28	6.28	-8.18	-104.6
51	25	-9595	632	513	0	871	-1552	12.57	12.57	6.28	6.28	-9.68	-129.5

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	37	-9822	1877	541	0	858	-4558	12.57	12.57	6.28	6.28	-29.88	743.9
41	37	-9843	958	552	0	879	-2264	12.57	12.57	6.28	6.28	-14.01	-179.3
42	37	-9776	963	488	0	729	-2278	12.57	12.57	6.28	6.28	-14.11	-180.2
43	37	-9656	2326	524	0	833	-5691	12.57	12.57	6.28	6.28	-37.47	1096.9
44	37	-9675	-547	552	0	882	1494	12.57	12.57	6.28	6.28	-9.40	-126.3
45	37	-9581	803	436	0	618	-1888	12.57	12.57	6.28	6.28	-11.60	-151.7
46	37	-9602	696	538	0	861	-1628	12.57	12.57	6.28	6.28	-10.08	-134.3
47	37	-9542	631	534	0	857	-1469	12.57	12.57	6.28	6.28	-9.24	-124.2
49	37	-9535	937	530	0	850	-2234	12.57	12.57	6.28	6.28	-13.85	-176.7
50	37	-9539	362	536	0	860	-797	12.57	12.57	6.28	6.28	-7.76	-100.0
51	37	-9520	632	513	0	807	-1473	12.57	12.57	6.28	6.28	-9.26	-124.4

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	50	-9746	1877	541	0	790	-4324	12.57	12.57	6.28	6.28	-28.30	679.0
41	50	-9767	958	552	0	810	-2144	12.57	12.57	6.28	6.28	-13.22	-170.4
42	50	-9701	963	488	0	668	-2157	12.57	12.57	6.28	6.28	-13.31	-171.2
43	50	-9581	2326	524	0	767	-5400	12.57	12.57	6.28	6.28	-35.54	1013.1
44	50	-9600	-547	552	0	813	1426	12.57	12.57	6.28	6.28	-9.05	-122.0
45	50	-9506	803	436	0	564	-1788	12.57	12.57	6.28	6.28	-10.99	-144.6
46	50	-9527	696	538	0	794	-1541	12.57	12.57	6.28	6.28	-9.61	-128.6
47	50	-9467	631	534	0	790	-1390	12.57	12.57	6.28	6.28	-8.84	-119.3
49	50	-9460	937	530	0	784	-2117	12.57	12.57	6.28	6.28	-13.07	-168.0
50	50	-9464	362	536	0	793	-751	12.57	12.57	6.28	6.28	-7.35	-95.4
51	50	-9445	632	513	0	743	-1394	12.57	12.57	6.28	6.28	-8.86	-119.5

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

ASTA NUM. 83 NI 1360 NF 170 SEZ. Rp B= 0.400 H= 0.600 (pilastro)
PIL. NUM. 16A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-9746	1877	541	0	790	-4324	12.57	12.57	6.28	6.28	-28.30	679.0
41	0	-9767	958	552	0	810	-2144	12.57	12.57	6.28	6.28	-13.22	-170.4
42	0	-9701	963	488	0	668	-2157	12.57	12.57	6.28	6.28	-13.31	-171.2
43	0	-9581	2326	524	0	767	-5400	12.57	12.57	6.28	6.28	-35.54	1013.1
44	0	-9600	-547	552	0	813	1426	12.57	12.57	6.28	6.28	-9.05	-122.0
45	0	-9506	803	436	0	564	-1788	12.57	12.57	6.28	6.28	-10.99	-144.6
46	0	-9527	696	538	0	794	-1541	12.57	12.57	6.28	6.28	-9.61	-128.6
47	0	-9467	631	534	0	790	-1390	12.57	12.57	6.28	6.28	-8.84	-119.3
49	0	-9460	937	530	0	784	-2117	12.57	12.57	6.28	6.28	-13.07	-168.0
50	0	-9464	362	536	0	793	-751	12.57	12.57	6.28	6.28	-7.35	-95.4
51	0	-9445	632	513	0	743	-1394	12.57	12.57	6.28	6.28	-8.86	-119.5

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	12	-9671	1877	541	0	723	-4089	12.57	12.57	6.28	6.28	-26.71	614.6
41	12	-9692	958	552	0	741	-2024	12.57	12.57	6.28	6.28	-12.45	-161.6
42	12	-9626	963	488	0	607	-2037	12.57	12.57	6.28	6.28	-12.53	-162.4
43	12	-9506	2326	524	0	702	-5109	12.57	12.57	6.28	6.28	-33.61	929.7
44	12	-9525	-547	552	0	744	1358	12.57	12.57	6.28	6.28	-8.71	-117.8
45	12	-9431	803	436	0	510	-1688	12.57	12.57	6.28	6.28	-10.40	-137.7
46	12	-9452	696	538	0	727	-1454	12.57	12.57	6.28	6.28	-9.15	-123.0
47	12	-9392	631	534	0	723	-1311	12.57	12.57	6.28	6.28	-8.46	-114.6
49	12	-9385	937	530	0	717	-2000	12.57	12.57	6.28	6.28	-12.31	-159.3
50	12	-9389	362	536	0	726	-706	12.57	12.57	6.28	6.28	-6.97	-91.1
51	12	-9370	632	513	0	679	-1315	12.57	12.57	6.28	6.28	-8.47	-114.7

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	25	-9596	1877	541	0	655	-3854	12.57	12.57	6.28	6.28	-25.11	550.7
41	25	-9617	958	552	0	672	-1904	12.57	12.57	6.28	6.28	-11.70	-152.9
42	25	-9551	963	488	0	546	-1916	12.57	12.57	6.28	6.28	-11.77	-153.7
43	25	-9431	2326	524	0	636	-4818	12.57	12.57	6.28	6.28	-31.67	846.6
44	25	-9450	-547	552	0	675	1290	12.57	12.57	6.28	6.28	-8.38	-113.7
45	25	-9356	803	436	0	455	-1588	12.57	12.57	6.28	6.28	-9.83	-130.9
46	25	-9377	696	538	0	660	-1367	12.57	12.57	6.28	6.28	-8.71	-117.7
47	25	-9317	631	534	0	657	-1232	12.57	12.57	6.28	6.28	-8.09	-110.0
49	25	-9310	937	530	0	651	-1882	12.57	12.57	6.28	6.28	-11.57	-150.8
50	25	-9314	362	536	0	659	-661	12.57	12.57	6.28	6.28	-6.61	-86.9

51	25	-9295	632	513	0	615	-1236	12.57	12.57	6.28	6.28	-8.10	-110.1

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	38	-9521	1877	541	0	587	-3620	12.57	12.57	6.28	6.28	-23.50	487.6
41	38	-9542	958	552	0	603	-1785	12.57	12.57	6.28	6.28	-10.97	-144.5
42	38	-9476	963	488	0	485	-1796	12.57	12.57	6.28	6.28	-11.04	-145.1
43	38	-9356	2326	524	0	571	-4528	12.57	12.57	6.28	6.28	-29.72	764.0
44	38	-9375	-547	552	0	606	1221	12.57	12.57	6.28	6.28	-8.06	-109.7
45	38	-9281	803	436	0	400	-1487	12.57	12.57	6.28	6.28	-9.29	-124.4
46	38	-9302	696	538	0	592	-1280	12.57	12.57	6.28	6.28	-8.30	-112.5
47	38	-9242	631	534	0	590	-1154	12.57	12.57	6.28	6.28	-7.74	-105.6
49	38	-9235	937	530	0	585	-1765	12.57	12.57	6.28	6.28	-10.84	-142.4
50	38	-9239	362	536	0	592	-615	12.57	12.57	6.28	6.28	-6.25	-82.8
51	38	-9220	632	513	0	551	-1157	12.57	12.57	6.28	6.28	-7.75	-105.7

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	50	-9446	1877	541	0	520	-3385	12.57	12.57	6.28	6.28	-21.89	425.4
41	50	-9467	958	552	0	534	-1665	12.57	12.57	6.28	6.28	-10.27	-136.3
42	50	-9401	963	488	0	424	-1676	12.57	12.57	6.28	6.28	-10.33	-136.8
43	50	-9281	2326	524	0	505	-4237	12.57	12.57	6.28	6.28	-27.76	682.0
44	50	-9300	-547	552	0	538	1153	12.57	12.57	6.28	6.28	-7.76	-105.9
45	50	-9206	803	436	0	346	-1387	12.57	12.57	6.28	6.28	-8.77	-118.1
46	50	-9227	696	538	0	525	-1193	12.57	12.57	6.28	6.28	-7.90	-107.5
47	50	-9167	631	534	0	523	-1075	12.57	12.57	6.28	6.28	-7.40	-101.4
49	50	-9160	937	530	0	518	-1648	12.57	12.57	6.28	6.28	-10.15	-134.3
50	50	-9164	362	536	0	525	-570	12.57	12.57	6.28	6.28	-5.89	-78.7
51	50	-9145	632	513	0	487	-1078	12.57	12.57	6.28	6.28	-7.41	-101.4

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

ASTA NUM. 84 NI 1037 NF 300 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 15A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm²				daN/cm²	
40	0	-32630	686	532	0	756	-1585	6.28	6.28	12.57	12.57	-19.58	-264.3
41	0	-32210	133	520	0	778	-242	6.28	6.28	12.57	12.57	-15.23	-221.5
42	0	-32070	136	335	0	419	-248	6.28	6.28	12.57	12.57	-13.89	-204.6
43	0	-31220	1042	502	0	733	-2463	6.28	6.28	12.57	12.57	-23.44	-305.8
44	0	-31210	-786	486	0	773	1993	6.28	6.28	12.57	12.57	-21.09	-279.4
45	0	-30280	126	174	0	171	-235	6.28	6.28	12.57	12.57	-12.31	-183.1
46	0	-29480	114	460	0	763	-214	6.28	6.28	12.57	12.57	-14.12	-205.0
47	0	-28800	109	445	0	759	-207	6.28	6.28	12.57	12.57	-13.85	-200.9
49	0	-28950	293	449	0	752	-655	6.28	6.28	12.57	12.57	-13.88	-201.4
50	0	-28940	-72	446	0	760	237	6.28	6.28	12.57	12.57	-13.90	-201.7
51	0	-28760	110	383	0	640	-209	6.28	6.28	12.57	12.57	-13.40	-195.3

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	12	-32555	686	532	0	690	-1499	6.28	6.28	12.57	12.57	-19.13	-259.2
41	12	-32135	133	520	0	713	-225	6.28	6.28	12.57	12.57	-14.97	-218.1
42	12	-31995	136	335	0	377	-231	6.28	6.28	12.57	12.57	-13.71	-202.3
43	12	-31145	1042	502	0	670	-2333	6.28	6.28	12.57	12.57	-22.74	-297.9
44	12	-31135	-786	486	0	712	1895	6.28	6.28	12.57	12.57	-20.57	-273.5
45	12	-30205	126	174	0	149	-219	6.28	6.28	12.57	12.57	-12.20	-181.7
46	12	-29405	114	460	0	706	-200	6.28	6.28	12.57	12.57	-13.89	-202.0
47	12	-28725	109	445	0	704	-193	6.28	6.28	12.57	12.57	-13.62	-198.0
49	12	-28875	293	449	0	696	-618	6.28	6.28	12.57	12.57	-13.65	-198.5
50	12	-28865	-72	446	0	705	228	6.28	6.28	12.57	12.57	-13.67	-198.8
51	12	-28685	110	383	0	592	-195	6.28	6.28	12.57	12.57	-13.20	-192.7

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	25	-32480	686	532	0	623	-1414	6.28	6.28	12.57	12.57	-18.68	-254.0
41	25	-32060	133	520	0	648	-208	6.28	6.28	12.57	12.57	-14.70	-214.8
42	25	-31920	136	335	0	335	-214	6.28	6.28	12.57	12.57	-13.53	-200.0
43	25	-31070	1042	502	0	607	-2202	6.28	6.28	12.57	12.57	-22.07	-290.2
44	25	-31060	-786	486	0	651	1796	6.28	6.28	12.57	12.57	-20.06	-267.6
45	25	-30130	126	174	0	128	-203	6.28	6.28	12.57	12.57	-12.10	-180.3
46	25	-29330	114	460	0	648	-185	6.28	6.28	12.57	12.57	-13.65	-199.0
47	25	-28650	109	445	0	648	-180	6.28	6.28	12.57	12.57	-13.39	-195.0
49	25	-28800	293	449	0	640	-581	6.28	6.28	12.57	12.57	-13.42	-195.5
50	25	-28790	-72	446	0	649	218	6.28	6.28	12.57	12.57	-13.45	-195.9
51	25	-28610	110	383	0	544	-181	6.28	6.28	12.57	12.57	-13.00	-190.1

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	38	-32405	686	532	0	557	-1328	6.28	6.28	12.57	12.57	-18.23	-248.8
41	38	-31985	133	520	0	583	-192	6.28	6.28	12.57	12.57	-14.44	-211.4
42	38	-31845	136	335	0	294	-197	6.28	6.28	12.57	12.57	-13.35	-197.7
43	38	-30995	1042	502	0	544	-2072	6.28	6.28	12.57	12.57	-21.40	-282.6
44	38	-30985	-786	486	0	590	1698	6.28	6.28	12.57	12.57	-19.55	-261.8
45	38	-30055	126	174	0	106	-188	6.28	6.28	12.57	12.57	-11.99	-178.9
46	38	-29255	114	460	0	591	-171	6.28	6.28	12.57	12.57	-13.42	-196.0
47	38	-28575	109	445	0	593	-166	6.28	6.28	12.57	12.57	-13.16	-192.1
49	38	-28725	293	449	0	584	-545	6.28	6.28	12.57	12.57	-13.19	-192.6
50	38	-28715	-72	446	0	593	209	6.28	6.28	12.57	12.57	-13.22	-192.9
51	38	-28535	110	383	0	496	-168	6.28	6.28	12.57	12.57	-12.80	-187.6

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	50	-32330	686	532	0	490	-1242	6.28	6.28	12.57	12.57	-17.78	-243.7
41	50	-31910	133	520	0	518	-175	6.28	6.28	12.57	12.57	-14.18	-208.1
42	50	-31770	136	335	0	252	-180	6.28	6.28	12.57	12.57	-13.17	-195.4
43	50	-30920	1042	502	0	482	-1942	6.28	6.28	12.57	12.57	-20.73	-275.0
44	50	-30910	-786	486	0	530	1600	6.28	6.28	12.57	12.57	-19.04	-255.9
45	50	-29980	126	174	0	84	-172	6.28	6.28	12.57	12.57	-11.88	-177.5
46	50	-29180	114	460	0	533	-157	6.28	6.28	12.57	12.57	-13.18	-193.0
47	50	-28500	109	445	0	537	-152	6.28	6.28	12.57	12.57	-12.93	-189.2
49	50	-28650	293	449	0	528	-508	6.28	6.28	12.57	12.57	-12.96	-189.6
50	50	-28640	-72	446	0	537	200	6.28	6.28	12.57	12.57	-12.99	-190.0
51	50	-28460	110	383	0	448	-154	6.28	6.28	12.57	12.57	-12.60	-185.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 85 NI 1033 NF 1037 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 15
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-32930	686	532	0	1022	-1928	6.28	6.28	12.57	12.57	-21.38	-285.0
41	0	-32510	133	520	0	1037	-308	6.28	6.28	12.57	12.57	-16.27	-234.8
42	0	-32370	136	335	0	586	-316	6.28	6.28	12.57	12.57	-14.61	-213.8
43	0	-31520	1042	502	0	984	-2984	6.28	6.28	12.57	12.57	-26.48	-339.5
44	0	-31510	-786	486	0	1015	2385	6.28	6.28	12.57	12.57	-23.14	-302.8
45	0	-30580	126	174	0	258	-298	6.28	6.28	12.57	12.57	-12.74	-188.8
46	0	-29780	114	460	0	993	-271	6.28	6.28	12.57	12.57	-15.06	-217.0
47	0	-29100	109	445	0	982	-261	6.28	6.28	12.57	12.57	-14.76	-212.6
49	0	-29250	293	449	0	977	-801	6.28	6.28	12.57	12.57	-14.80	-213.2
50	0	-29240	-72	446	0	983	273	6.28	6.28	12.57	12.57	-14.82	-213.4
51	0	-29060	110	383	0	832	-264	6.28	6.28	12.57	12.57	-14.20	-205.6

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	12	-32855	686	532	0	956	-1842	6.28	6.28	12.57	12.57	-20.93	-279.9
41	12	-32435	133	520	0	972	-291	6.28	6.28	12.57	12.57	-16.01	-231.5
42	12	-32295	136	335	0	545	-299	6.28	6.28	12.57	12.57	-14.43	-211.5
43	12	-31445	1042	502	0	921	-2854	6.28	6.28	12.57	12.57	-25.68	-330.7
44	12	-31435	-786	486	0	954	2287	6.28	6.28	12.57	12.57	-22.62	-296.9
45	12	-30505	126	174	0	236	-282	6.28	6.28	12.57	12.57	-12.63	-187.4
46	12	-29705	114	460	0	936	-256	6.28	6.28	12.57	12.57	-14.83	-214.0
47	12	-29025	109	445	0	926	-248	6.28	6.28	12.57	12.57	-14.53	-209.7
49	12	-29175	293	449	0	921	-765	6.28	6.28	12.57	12.57	-14.57	-210.3
50	12	-29165	-72	446	0	927	264	6.28	6.28	12.57	12.57	-14.59	-210.5
51	12	-28985	110	383	0	784	-250	6.28	6.28	12.57	12.57	-14.00	-203.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	25	-32780	686	532	0	889	-1756	6.28	6.28	12.57	12.57	-20.48	-274.7
41	25	-32360	133	520	0	907	-275	6.28	6.28	12.57	12.57	-15.75	-228.1
42	25	-32220	136	335	0	503	-282	6.28	6.28	12.57	12.57	-14.25	-209.2
43	25	-31370	1042	502	0	858	-2724	6.28	6.28	12.57	12.57	-24.91	-322.2
44	25	-31360	-786	486	0	894	2189	6.28	6.28	12.57	12.57	-22.11	-291.1
45	25	-30430	126	174	0	215	-266	6.28	6.28	12.57	12.57	-12.52	-185.9
46	25	-29630	114	460	0	878	-242	6.28	6.28	12.57	12.57	-14.59	-211.0
47	25	-28950	109	445	0	871	-234	6.28	6.28	12.57	12.57	-14.30	-206.7
49	25	-29100	293	449	0	864	-728	6.28	6.28	12.57	12.57	-14.34	-207.3
50	25	-29090	-72	446	0	872	255	6.28	6.28	12.57	12.57	-14.36	-207.6
51	25	-28910	110	383	0	736	-236	6.28	6.28	12.57	12.57	-13.80	-200.5

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	38	-32705	686	532	0	822	-1671	6.28	6.28	12.57	12.57	-20.03	-269.5
41	38	-32285	133	520	0	842	-258	6.28	6.28	12.57	12.57	-15.49	-224.8
42	38	-32145	136	335	0	461	-265	6.28	6.28	12.57	12.57	-14.07	-206.9
43	38	-31295	1042	502	0	795	-2593	6.28	6.28	12.57	12.57	-24.16	-313.9
44	38	-31285	-786	486	0	833	2091	6.28	6.28	12.57	12.57	-21.60	-285.2
45	38	-30355	126	174	0	193	-251	6.28	6.28	12.57	12.57	-12.42	-184.5
46	38	-29555	114	460	0	821	-228	6.28	6.28	12.57	12.57	-14.36	-208.0
47	38	-28875	109	445	0	815	-220	6.28	6.28	12.57	12.57	-14.07	-203.8
49	38	-29025	293	449	0	808	-691	6.28	6.28	12.57	12.57	-14.11	-204.4
50	38	-29015	-72	446	0	816	246	6.28	6.28	12.57	12.57	-14.13	-204.7
51	38	-28835	110	383	0	688	-223	6.28	6.28	12.57	12.57	-13.60	-197.9

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	50	-32630	686	532	0	756	-1585	6.28	6.28	12.57	12.57	-19.58	-264.3
41	50	-32210	133	520	0	778	-242	6.28	6.28	12.57	12.57	-15.23	-221.5
42	50	-32070	136	335	0	419	-248	6.28	6.28	12.57	12.57	-13.89	-204.6
43	50	-31220	1042	502	0	733	-2463	6.28	6.28	12.57	12.57	-23.44	-305.8
44	50	-31210	-786	486	0	773	1993	6.28	6.28	12.57	12.57	-21.09	-279.4
45	50	-30280	126	174	0	171	-235	6.28	6.28	12.57	12.57	-12.31	-183.1
46	50	-29480	114	460	0	763	-214	6.28	6.28	12.57	12.57	-14.12	-205.0
47	50	-28800	109	445	0	759	-207	6.28	6.28	12.57	12.57	-13.85	-200.9
49	50	-28950	293	449	0	752	-655	6.28	6.28	12.57	12.57	-13.88	-201.4
50	50	-28940	-72	446	0	760	237	6.28	6.28	12.57	12.57	-13.90	-201.7
51	50	-28760	110	383	0	640	-209	6.28	6.28	12.57	12.57	-13.40	-195.3

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 86 NI 1255 NF 1262 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 14
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-16660	163	-481	0	-1277	-584	6.28	6.28	12.57	12.57	-11.01	-153.7
41	0	-16620	4	-434	0	-1162	6	6.28	6.28	12.57	12.57	-10.58	-148.3
42	0	-16570	5	-570	0	-1531	1	6.28	6.28	12.57	12.57	-11.88	-164.5
43	0	-16080	274	-434	0	-1157	-996	6.28	6.28	12.57	12.57	-10.71	-145.0
44	0	-16020	-262	-374	0	-1011	992	6.28	6.28	12.57	12.57	-10.67	-141.6
45	0	-15920	11	-582	0	-1580	-20	6.28	6.28	12.57	12.57	-11.81	-163.0
46	0	-15630	12	-309	0	-846	-23	6.28	6.28	12.57	12.57	-9.07	-128.4
47	0	-15390	14	-277	0	-767	-30	6.28	6.28	12.57	12.57	-8.69	-123.5
49	0	-15400	67	-293	0	-805	-227	6.28	6.28	12.57	12.57	-8.83	-125.3
50	0	-15390	-40	-281	0	-776	170	6.28	6.28	12.57	12.57	-8.72	-123.9
51	0	-15370	15	-322	0	-890	-32	6.28	6.28	12.57	12.57	-9.12	-128.9

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	12	-16585	163	-481	0	-1217	-564	6.28	6.28	12.57	12.57	-10.76	-150.6

41	12	-16545	4	-434	0	-1108	6	6.28	6.28	12.57	12.57	-10.36	-145.5
42	12	-16495	5	-570	0	-1460	2	6.28	6.28	12.57	12.57	-11.60	-160.9
43	12	-16005	274	-434	0	-1103	-961	6.28	6.28	12.57	12.57	-10.51	-142.1
44	12	-15945	-262	-374	0	-964	959	6.28	6.28	12.57	12.57	-10.48	-139.4
45	12	-15845	11	-582	0	-1507	-18	6.28	6.28	12.57	12.57	-11.52	-159.3
46	12	-15555	12	-309	0	-807	-22	6.28	6.28	12.57	12.57	-8.90	-126.3
47	12	-15315	14	-277	0	-732	-28	6.28	6.28	12.57	12.57	-8.54	-121.5
49	12	-15325	67	-293	0	-769	-218	6.28	6.28	12.57	12.57	-8.67	-123.2
50	12	-15315	-40	-281	0	-741	166	6.28	6.28	12.57	12.57	-8.57	-121.9
51	12	-15295	15	-322	0	-850	-30	6.28	6.28	12.57	12.57	-8.95	-126.7

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	25	-16510	163	-481	0	-1157	-544	6.28	6.28	12.57	12.57	-10.52	-147.5
41	25	-16470	4	-434	0	-1054	7	6.28	6.28	12.57	12.57	-10.14	-142.6
42	25	-16420	5	-570	0	-1389	3	6.28	6.28	12.57	12.57	-11.32	-157.3
43	25	-15930	274	-434	0	-1048	-927	6.28	6.28	12.57	12.57	-10.32	-139.2
44	25	-15870	-262	-374	0	-917	926	6.28	6.28	12.57	12.57	-10.29	-137.2
45	25	-15770	11	-582	0	-1434	-17	6.28	6.28	12.57	12.57	-11.23	-155.6
46	25	-15480	12	-309	0	-769	-20	6.28	6.28	12.57	12.57	-8.73	-124.1
47	25	-15240	14	-277	0	-697	-27	6.28	6.28	12.57	12.57	-8.38	-119.5
49	25	-15250	67	-293	0	-732	-210	6.28	6.28	12.57	12.57	-8.51	-121.1
50	25	-15240	-40	-281	0	-706	160	6.28	6.28	12.57	12.57	-8.41	-119.9
51	25	-15220	15	-322	0	-809	-28	6.28	6.28	12.57	12.57	-8.78	-124.4

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	38	-16435	163	-481	0	-1097	-523	6.28	6.28	12.57	12.57	-10.28	-144.3
41	38	-16395	4	-434	0	-999	7	6.28	6.28	12.57	12.57	-9.91	-139.7
42	38	-16345	5	-570	0	-1318	3	6.28	6.28	12.57	12.57	-11.03	-153.7
43	38	-15855	274	-434	0	-994	-893	6.28	6.28	12.57	12.57	-10.12	-136.4
44	38	-15795	-262	-374	0	-870	893	6.28	6.28	12.57	12.57	-10.10	-135.0
45	38	-15695	11	-582	0	-1362	-15	6.28	6.28	12.57	12.57	-10.94	-151.9
46	38	-15405	12	-309	0	-730	-18	6.28	6.28	12.57	12.57	-8.57	-121.9
47	38	-15165	14	-277	0	-663	-25	6.28	6.28	12.57	12.57	-8.23	-117.5
49	38	-15175	67	-293	0	-695	-202	6.28	6.28	12.57	12.57	-8.35	-119.1
50	38	-15165	-40	-281	0	-671	156	6.28	6.28	12.57	12.57	-8.26	-117.9
51	38	-15145	15	-322	0	-769	-26	6.28	6.28	12.57	12.57	-8.60	-122.2

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	50	-16360	163	-481	0	-1037	-503	6.28	6.28	12.57	12.57	-10.03	-141.2
41	50	-16320	4	-434	0	-945	8	6.28	6.28	12.57	12.57	-9.69	-136.9
42	50	-16270	5	-570	0	-1247	4	6.28	6.28	12.57	12.57	-10.75	-150.1
43	50	-15780	274	-434	0	-940	-858	6.28	6.28	12.57	12.57	-9.92	-133.5
44	50	-15720	-262	-374	0	-824	860	6.28	6.28	12.57	12.57	-9.91	-132.7
45	50	-15620	11	-582	0	-1289	-14	6.28	6.28	12.57	12.57	-10.65	-148.2
46	50	-15330	12	-309	0	-692	-17	6.28	6.28	12.57	12.57	-8.40	-119.8
47	50	-15090	14	-277	0	-628	-23	6.28	6.28	12.57	12.57	-8.08	-115.6
49	50	-15100	67	-293	0	-659	-193	6.28	6.28	12.57	12.57	-8.19	-117.0
50	50	-15090	-40	-281	0	-636	150	6.28	6.28	12.57	12.57	-8.11	-115.9
51	50	-15070	15	-322	0	-729	-24	6.28	6.28	12.57	12.57	-8.43	-119.9

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 87 NI 1262 NF 128 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 14A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	--												
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-16360	163	-481	0	-1037	-503	6.28	6.28	12.57	12.57	-10.03	-141.2
41	0	-16320	4	-434	0	-945	8	6.28	6.28	12.57	12.57	-9.69	-136.9
42	0	-16270	5	-570	0	-1247	4	6.28	6.28	12.57	12.57	-10.75	-150.1
43	0	-15780	274	-434	0	-940	-858	6.28	6.28	12.57	12.57	-9.92	-133.5
44	0	-15720	-262	-374	0	-824	860	6.28	6.28	12.57	12.57	-9.91	-132.7
45	0	-15620	11	-582	0	-1289	-14	6.28	6.28	12.57	12.57	-10.65	-148.2
46	0	-15330	12	-309	0	-692	-17	6.28	6.28	12.57	12.57	-8.40	-119.8
47	0	-15090	14	-277	0	-628	-23	6.28	6.28	12.57	12.57	-8.08	-115.6
49	0	-15100	67	-293	0	-659	-193	6.28	6.28	12.57	12.57	-8.19	-117.0
50	0	-15090	-40	-281	0	-636	150	6.28	6.28	12.57	12.57	-8.11	-115.9
51	0	-15070	15	-322	0	-729	-24	6.28	6.28	12.57	12.57	-8.43	-119.9

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	12	-16285	163	-481	0	-977	-482	6.28	6.28	12.57	12.57	-9.79	-138.1
41	12	-16245	4	-434	0	-891	8	6.28	6.28	12.57	12.57	-9.47	-134.0
42	12	-16195	5	-570	0	-1176	5	6.28	6.28	12.57	12.57	-10.47	-146.5
43	12	-15705	274	-434	0	-886	-824	6.28	6.28	12.57	12.57	-9.73	-130.6
44	12	-15645	-262	-374	0	-777	828	6.28	6.28	12.57	12.57	-9.72	-130.5
45	12	-15545	11	-582	0	-1216	-13	6.28	6.28	12.57	12.57	-10.36	-144.5
46	12	-15255	12	-309	0	-653	-15	6.28	6.28	12.57	12.57	-8.23	-117.6
47	12	-15015	14	-277	0	-593	-21	6.28	6.28	12.57	12.57	-7.93	-113.6
49	12	-15025	67	-293	0	-622	-185	6.28	6.28	12.57	12.57	-8.03	-114.9
50	12	-15015	-40	-281	0	-600	146	6.28	6.28	12.57	12.57	-7.95	-113.9
51	12	-14995	15	-322	0	-688	-23	6.28	6.28	12.57	12.57	-8.26	-117.7

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	25	-16210	163	-481	0	-917	-462	6.28	6.28	12.57	12.57	-9.55	-135.0
41	25	-16170	4	-434	0	-837	9	6.28	6.28	12.57	12.57	-9.24	-131.1
42	25	-16120	5	-570	0	-1104	5	6.28	6.28	12.57	12.57	-10.18	-142.8
43	25	-15630	274	-434	0	-831	-790	6.28	6.28	12.57	12.57	-9.53	-128.3
44	25	-15570	-262	-374	0	-730	795	6.28	6.28	12.57	12.57	-9.53	-128.3
45	25	-15470	11	-582	0	-1144	-11	6.28	6.28	12.57	12.57	-10.07	-140.8
46	25	-15180	12	-309	0	-614	-14	6.28	6.28	12.57	12.57	-8.06	-115.5
47	25	-14940	14	-277	0	-559	-20	6.28	6.28	12.57	12.57	-7.77	-111.6
49	25	-14950	67	-293	0	-586	-176	6.28	6.28	12.57	12.57	-7.87	-112.8
50	25	-14940	-40	-281	0	-565	140	6.28	6.28	12.57	12.57	-7.80	-111.9
51	25	-14920	15	-322	0	-648	-21	6.28	6.28	12.57	12.57	-8.08	-115.5

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	38	-16135	163	-481	0	-857	-441	6.28	6.28	12.57	12.57	-9.30	-131.8
41	38	-16095	4	-434	0	-782	9	6.28	6.28	12.57	12.57	-9.02	-128.3

42	38	-16045	5	-570	0	-1033	6	6.28	6.28	12.57	12.57	-9.90	-139.2
43	38	-15555	274	-434	0	-777	-756	6.28	6.28	12.57	12.57	-9.33	-126.0
44	38	-15495	-262	-374	0	-683	762	6.28	6.28	12.57	12.57	-9.35	-126.1
45	38	-15395	11	-582	0	-1071	-10	6.28	6.28	12.57	12.57	-9.78	-137.1
46	38	-15105	12	-309	0	-576	-12	6.28	6.28	12.57	12.57	-7.90	-113.3
47	38	-14865	14	-277	0	-524	-18	6.28	6.28	12.57	12.57	-7.62	-109.6
49	38	-14875	67	-293	0	-549	-168	6.28	6.28	12.57	12.57	-7.71	-110.8
50	38	-14865	-40	-281	0	-530	136	6.28	6.28	12.57	12.57	-7.64	-109.9
51	38	-14845	15	-322	0	-608	-19	6.28	6.28	12.57	12.57	-7.91	-113.2

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	50	-16060	163	-481	0	-797	-421	6.28	6.28	12.57	12.57	-9.06	-128.7
41	50	-16020	4	-434	0	-728	10	6.28	6.28	12.57	12.57	-8.80	-125.4
42	50	-15970	5	-570	0	-962	7	6.28	6.28	12.57	12.57	-9.61	-135.6
43	50	-15480	274	-434	0	-723	-721	6.28	6.28	12.57	12.57	-9.14	-123.7
44	50	-15420	-262	-374	0	-636	730	6.28	6.28	12.57	12.57	-9.16	-123.8
45	50	-15320	11	-582	0	-998	-8	6.28	6.28	12.57	12.57	-9.49	-133.4
46	50	-15030	12	-309	0	-537	-11	6.28	6.28	12.57	12.57	-7.73	-111.1
47	50	-14790	14	-277	0	-490	-16	6.28	6.28	12.57	12.57	-7.47	-107.6
49	50	-14800	67	-293	0	-512	-160	6.28	6.28	12.57	12.57	-7.55	-108.7
50	50	-14790	-40	-281	0	-495	130	6.28	6.28	12.57	12.57	-7.49	-107.9
51	50	-14770	15	-322	0	-567	-17	6.28	6.28	12.57	12.57	-7.74	-111.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 88 NI 1168 NF 211 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 13A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-5619	-374	258	0	-1022	-12	6.28	6.28	9.42	9.42	-7.96	-105.6
41	0	-5610	-83	238	0	-983	-5	6.28	6.28	9.42	9.42	-7.70	-102.5
42	0	-5655	-88	302	0	-1120	-6	6.28	6.28	9.42	9.42	-8.66	-113.8
43	0	-5480	-582	239	0	-954	-16	6.28	6.28	9.42	9.42	-7.48	-99.7
44	0	-5469	404	206	0	-899	5	6.28	6.28	9.42	9.42	-7.12	-95.3
45	0	-5540	-106	312	0	-1119	-6	6.28	6.28	9.42	9.42	-8.64	-113.3
46	0	-5378	-105	186	0	-834	-6	6.28	6.28	9.42	9.42	-6.69	-90.1
47	0	-5320	-110	173	0	-797	-6	6.28	6.28	9.42	9.42	-6.45	-87.1
49	0	-5323	-208	180	0	-810	-8	6.28	6.28	9.42	9.42	-6.53	-88.0
50	0	-5321	-10	173	0	-799	-3	6.28	6.28	9.42	9.42	-6.46	-87.2
51	0	-5335	-112	194	0	-843	-6	6.28	6.28	9.42	9.42	-6.73	-90.5

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	12	-5563	-374	258	0	-1054	-59	6.28	6.28	9.42	9.42	-8.18	-108.0
41	12	-5554	-83	238	0	-1013	-16	6.28	6.28	9.42	9.42	-7.89	-104.6
42	12	-5599	-88	302	0	-1158	-17	6.28	6.28	9.42	9.42	-8.93	-116.7
43	12	-5424	-582	239	0	-984	-89	6.28	6.28	9.42	9.42	-7.67	-101.8
44	12	-5413	404	206	0	-925	56	6.28	6.28	9.42	9.42	-7.27	-97.0
45	12	-5484	-106	312	0	-1158	-19	6.28	6.28	9.42	9.42	-8.92	-116.4
46	12	-5322	-105	186	0	-857	-19	6.28	6.28	9.42	9.42	-6.82	-91.5
47	12	-5264	-110	173	0	-819	-19	6.28	6.28	9.42	9.42	-6.56	-88.3
49	12	-5267	-208	180	0	-832	-34	6.28	6.28	9.42	9.42	-6.65	-89.3
50	12	-5265	-10	173	0	-820	-5	6.28	6.28	9.42	9.42	-6.57	-88.4
51	12	-5279	-112	194	0	-867	-20	6.28	6.28	9.42	9.42	-6.87	-92.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	25	-5506	-374	258	0	-1086	-105	6.28	6.28	9.42	9.42	-8.40	-110.4
41	25	-5498	-83	238	0	-1042	-26	6.28	6.28	9.42	9.42	-8.09	-106.8
42	25	-5542	-88	302	0	-1196	-28	6.28	6.28	9.42	9.42	-9.21	-119.8
43	25	-5368	-582	239	0	-1014	-162	6.28	6.28	9.42	9.42	-7.87	-104.0
44	25	-5356	404	206	0	-950	106	6.28	6.28	9.42	9.42	-7.43	-98.8
45	25	-5428	-106	312	0	-1197	-33	6.28	6.28	9.42	9.42	-9.22	-119.5
46	25	-5266	-105	186	0	-881	-32	6.28	6.28	9.42	9.42	-6.95	-92.9
47	25	-5208	-110	173	0	-840	-33	6.28	6.28	9.42	9.42	-6.68	-89.6
49	25	-5210	-208	180	0	-855	-60	6.28	6.28	9.42	9.42	-6.77	-90.7
50	25	-5208	-10	173	0	-842	-6	6.28	6.28	9.42	9.42	-6.69	-89.7
51	25	-5222	-112	194	0	-891	-34	6.28	6.28	9.42	9.42	-7.01	-93.6

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	38	-5450	-374	258	0	-1119	-152	6.28	6.28	9.42	9.42	-8.63	-112.9
41	38	-5441	-83	238	0	-1072	-37	6.28	6.28	9.42	9.42	-8.29	-109.0
42	38	-5486	-88	302	0	-1234	-39	6.28	6.28	9.42	9.42	-9.50	-122.9
43	38	-5311	-582	239	0	-1044	-234	6.28	6.28	9.42	9.42	-8.07	-106.2
44	38	-5300	404	206	0	-976	157	6.28	6.28	9.42	9.42	-7.59	-100.6
45	38	-5371	-106	312	0	-1236	-46	6.28	6.28	9.42	9.42	-9.51	-122.7
46	38	-5209	-105	186	0	-904	-45	6.28	6.28	9.42	9.42	-7.09	-94.5
47	38	-5151	-110	173	0	-862	-47	6.28	6.28	9.42	9.42	-6.80	-91.0
49	38	-5154	-208	180	0	-877	-86	6.28	6.28	9.42	9.42	-6.90	-92.1
50	38	-5152	-10	173	0	-864	-7	6.28	6.28	9.42	9.42	-6.81	-91.1
51	38	-5166	-112	194	0	-916	-48	6.28	6.28	9.42	9.42	-7.16	-95.2

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	50	-5394	-374	258	0	-1151	-199	6.28	6.28	9.42	9.42	-8.87	-115.5
41	50	-5385	-83	238	0	-1102	-47	6.28	6.28	9.42	9.42	-8.50	-111.3
42	50	-5430	-88	302	0	-1272	-50	6.28	6.28	9.42	9.42	-9.79	-126.0
43	50	-5255	-582	239	0	-1074	-307	6.28	6.28	9.42	9.42	-8.29	-108.5
44	50	-5244	404	206	0	-1002	207	6.28	6.28	9.42	9.42	-7.77	-102.5
45	50	-5315	-106	312	0	-1275	-59	6.28	6.28	9.42	9.42	-9.82	-125.9
46	50	-5153	-105	186	0	-927	-58	6.28	6.28	9.42	9.42	-7.23	-96.1
47	50	-5095	-110	173	0	-884	-61	6.28	6.28	9.42	9.42	-6.93	-92.4
49	50	-5098	-208	180	0	-900	-112	6.28	6.28	9.42	9.42	-7.04	-93.6
50	50	-5096	-10	173	0	-885	-9	6.28	6.28	9.42	9.42	-6.94	-92.5
51	50	-5110	-112	194	0	-940	-62	6.28	6.28	9.42	9.42	-7.31	-96.9

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 89 NI 1160 NF 1168 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 13
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm²				daN/cm²	
40	0	-3856	-85	-364	0	-1268	31	6.28	6.28	9.42	9.42	-9.85	149.6
41	0	-3854	-32	-363	0	-1228	11	6.28	6.28	9.42	9.42	-9.53	138.8
42	0	-3872	-35	-377	0	-1376	12	6.28	6.28	9.42	9.42	-10.71	178.8
43	0	-3775	-121	-340	0	-1185	44	6.28	6.28	9.42	9.42	-9.19	131.2
44	0	-3776	57	-349	0	-1133	-23	6.28	6.28	9.42	9.42	-8.78	117.4
45	0	-3802	-37	-361	0	-1366	12	6.28	6.28	9.42	9.42	-10.63	179.8
46	0	-3722	-33	-324	0	-1053	11	6.28	6.28	9.42	9.42	-8.14	-102.0
47	0	-3689	-33	-314	0	-1010	11	6.28	6.28	9.42	9.42	-7.80	-98.2
49	0	-3690	-51	-315	0	-1023	18	6.28	6.28	9.42	9.42	-7.90	-99.3
50	0	-3690	-16	-316	0	-1012	4	6.28	6.28	9.42	9.42	-7.82	-98.4
51	0	-3695	-34	-319	0	-1059	11	6.28	6.28	9.42	9.42	-8.19	-102.4

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	12	-3800	-85	-364	0	-1222	20	6.28	6.28	9.42	9.42	-9.49	140.0
41	12	-3798	-32	-363	0	-1183	7	6.28	6.28	9.42	9.42	-9.17	129.4
42	12	-3816	-35	-377	0	-1329	7	6.28	6.28	9.42	9.42	-10.34	168.6
43	12	-3719	-121	-340	0	-1143	29	6.28	6.28	9.42	9.42	-8.86	122.7
44	12	-3720	57	-349	0	-1089	-16	6.28	6.28	9.42	9.42	-8.43	108.7
45	12	-3746	-37	-361	0	-1321	8	6.28	6.28	9.42	9.42	-10.28	170.0
46	12	-3666	-33	-324	0	-1013	7	6.28	6.28	9.42	9.42	-7.82	-98.3
47	12	-3633	-33	-314	0	-971	7	6.28	6.28	9.42	9.42	-7.49	-94.6
49	12	-3634	-51	-315	0	-984	11	6.28	6.28	9.42	9.42	-7.59	-95.8
50	12	-3634	-16	-316	0	-973	2	6.28	6.28	9.42	9.42	-7.51	-94.8
51	12	-3639	-34	-319	0	-1019	7	6.28	6.28	9.42	9.42	-7.88	-98.8

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	25	-3744	-85	-364	0	-1177	9	6.28	6.28	9.42	9.42	-9.13	130.6
41	25	-3742	-32	-363	0	-1138	3	6.28	6.28	9.42	9.42	-8.82	120.2
42	25	-3760	-35	-377	0	-1282	3	6.28	6.28	9.42	9.42	-9.97	158.5
43	25	-3662	-121	-340	0	-1100	14	6.28	6.28	9.42	9.42	-8.53	114.2
44	25	-3664	57	-349	0	-1046	-9	6.28	6.28	9.42	9.42	-8.09	-101.2
45	25	-3690	-37	-361	0	-1276	3	6.28	6.28	9.42	9.42	-9.92	160.3
46	25	-3610	-33	-324	0	-972	3	6.28	6.28	9.42	9.42	-7.50	-94.7
47	25	-3576	-33	-314	0	-931	3	6.28	6.28	9.42	9.42	-7.18	-91.1
49	25	-3578	-51	-315	0	-944	5	6.28	6.28	9.42	9.42	-7.29	-92.2
50	25	-3578	-16	-316	0	-933	0	6.28	6.28	9.42	9.42	-7.20	-91.2
51	25	-3582	-34	-319	0	-979	3	6.28	6.28	9.42	9.42	-7.56	-95.2

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	38	-3687	-85	-364	0	-1132	-1	6.28	6.28	9.42	9.42	-8.77	121.2
41	38	-3685	-32	-363	0	-1092	-1	6.28	6.28	9.42	9.42	-8.46	111.0
42	38	-3703	-35	-377	0	-1235	-2	6.28	6.28	9.42	9.42	-9.60	148.4
43	38	-3606	-121	-340	0	-1058	-1	6.28	6.28	9.42	9.42	-8.19	105.9
44	38	-3607	57	-349	0	-1002	-2	6.28	6.28	9.42	9.42	-7.74	-97.3
45	38	-3633	-37	-361	0	-1230	-2	6.28	6.28	9.42	9.42	-9.56	150.7
46	38	-3553	-33	-324	0	-932	-1	6.28	6.28	9.42	9.42	-7.19	-91.0
47	38	-3520	-33	-314	0	-892	-1	6.28	6.28	9.42	9.42	-6.87	-87.5
49	38	-3521	-51	-315	0	-905	-1	6.28	6.28	9.42	9.42	-6.98	-88.6
50	38	-3521	-16	-316	0	-894	-1	6.28	6.28	9.42	9.42	-6.89	-87.6
51	38	-3526	-34	-319	0	-939	-1	6.28	6.28	9.42	9.42	-7.25	-91.6

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	50	-3631	-85	-364	0	-1086	-12	6.28	6.28	9.42	9.42	-8.41	111.9
41	50	-3629	-32	-363	0	-1047	-5	6.28	6.28	9.42	9.42	-8.10	102.0
42	50	-3647	-35	-377	0	-1188	-6	6.28	6.28	9.42	9.42	-9.23	138.4
43	50	-3550	-121	-340	0	-1016	-16	6.28	6.28	9.42	9.42	-7.86	-98.3
44	50	-3551	57	-349	0	-959	5	6.28	6.28	9.42	9.42	-7.40	-93.3
45	50	-3577	-37	-361	0	-1185	-6	6.28	6.28	9.42	9.42	-9.21	141.2
46	50	-3497	-33	-324	0	-891	-6	6.28	6.28	9.42	9.42	-6.87	-87.4
47	50	-3464	-33	-314	0	-852	-6	6.28	6.28	9.42	9.42	-6.57	-83.9
49	50	-3465	-51	-315	0	-866	-8	6.28	6.28	9.42	9.42	-6.67	-85.0
50	50	-3465	-16	-316	0	-854	-3	6.28	6.28	9.42	9.42	-6.58	-84.1
51	50	-3470	-34	-319	0	-900	-6	6.28	6.28	9.42	9.42	-6.94	-88.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 90 NI 1159 NF 1161 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 18
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm²				daN/cm²	
40	0	-4798	-75	-387	0	-1206	14	6.28	6.28	12.57	12.57	-7.53	-95.0
41	0	-4792	101	-404	0	-1239	-21	6.28	6.28	12.57	12.57	-7.76	-97.4
42	0	-4794	89	-416	0	-1336	-19	6.28	6.28	12.57	12.57	-8.43	115.0
43	0	-4706	-201	-352	0	-1094	39	6.28	6.28	12.57	12.57	-6.78	-86.6
44	0	-4692	394	-415	0	-1253	-80	6.28	6.28	12.57	12.57	-7.87	99.5
45	0	-4700	73	-401	0	-1312	-16	6.28	6.28	12.57	12.57	-8.28	113.3
46	0	-4640	88	-368	0	-1096	-19	6.28	6.28	12.57	12.57	-6.80	-86.6
47	0	-4602	84	-358	0	-1061	-18	6.28	6.28	12.57	12.57	-6.57	-84.0
49	0	-4604	26	-352	0	-1050	-7	6.28	6.28	12.57	12.57	-6.49	-83.2
50	0	-4601	145	-365	0	-1081	-30	6.28	6.28	12.57	12.57	-6.70	-85.5
51	0	-4602	80	-362	0	-1093	-18	6.28	6.28	12.57	12.57	-6.78	-86.4

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	12	-4723	-75	-387	0	-1158	5	6.28	6.28	12.57	12.57	-7.21	-91.3
41	12	-4717	101	-404	0	-1188	-9	6.28	6.28	12.57	12.57	-7.42	-93.6
42	12	-4719	89	-416	0	-1284	-8	6.28	6.28	12.57	12.57	-8.08	105.7
43	12	-4631	-201	-352	0	-1050	14	6.28	6.28	12.57	12.57	-6.49	-83.2
44	12	-4617	394	-415	0	-1201	-31	6.28	6.28	12.57	12.57	-7.52	-94.4
45	12	-4625	73	-401	0	-1262	-7	6.28	6.28	12.57	12.57	-7.95	104.4
46	12	-4565	88	-368	0	-1050	-8	6.28	6.28	12.57	12.57	-6.50	-83.2

47	12	-4527	84	-358	0	-1016	-8	6.28	6.28	12.57	12.57	-6.28	-80.6
49	12	-4529	26	-352	0	-1006	-3	6.28	6.28	12.57	12.57	-6.21	-79.9
50	12	-4526	145	-365	0	-1035	-12	6.28	6.28	12.57	12.57	-6.40	-82.0
51	12	-4527	80	-362	0	-1048	-8	6.28	6.28	12.57	12.57	-6.49	-82.9

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	25	-4648	-75	-387	0	-1109	-4	6.28	6.28	12.57	12.57	-6.89	-87.6
41	25	-4642	101	-404	0	-1138	4	6.28	6.28	12.57	12.57	-7.08	-89.7
42	25	-4644	89	-416	0	-1232	3	6.28	6.28	12.57	12.57	-7.73	-96.7
43	25	-4556	-201	-352	0	-1006	-11	6.28	6.28	12.57	12.57	-6.21	-79.9
44	25	-4542	394	-415	0	-1149	18	6.28	6.28	12.57	12.57	-7.18	-90.4
45	25	-4550	73	-401	0	-1212	2	6.28	6.28	12.57	12.57	-7.61	95.7
46	25	-4490	88	-368	0	-1004	3	6.28	6.28	12.57	12.57	-6.20	-79.7
47	25	-4452	84	-358	0	-971	3	6.28	6.28	12.57	12.57	-5.99	-77.2
49	25	-4454	26	-352	0	-962	-0	6.28	6.28	12.57	12.57	-5.92	-76.5
50	25	-4451	145	-365	0	-990	6	6.28	6.28	12.57	12.57	-6.11	-78.6
51	25	-4452	80	-362	0	-1002	2	6.28	6.28	12.57	12.57	-6.19	-79.5

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	38	-4573	-75	-387	0	-1060	-14	6.28	6.28	12.57	12.57	-6.57	-83.9
41	38	-4567	101	-404	0	-1088	17	6.28	6.28	12.57	12.57	-6.75	-85.9
42	38	-4569	89	-416	0	-1180	14	6.28	6.28	12.57	12.57	-7.39	-92.8
43	38	-4481	-201	-352	0	-962	-36	6.28	6.28	12.57	12.57	-5.92	-76.6
44	38	-4467	394	-415	0	-1097	68	6.28	6.28	12.57	12.57	-6.83	-86.5
45	38	-4475	73	-401	0	-1161	11	6.28	6.28	12.57	12.57	-7.27	-91.3
46	38	-4415	88	-368	0	-958	14	6.28	6.28	12.57	12.57	-5.91	-76.2
47	38	-4377	84	-358	0	-926	13	6.28	6.28	12.57	12.57	-5.70	-73.8
49	38	-4379	26	-352	0	-917	3	6.28	6.28	12.57	12.57	-5.64	-73.2
50	38	-4376	145	-365	0	-944	24	6.28	6.28	12.57	12.57	-5.82	-75.1
51	38	-4377	80	-362	0	-957	13	6.28	6.28	12.57	12.57	-5.90	-76.1

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	50	-4498	-75	-387	0	-1012	-23	6.28	6.28	12.57	12.57	-6.25	-80.3
41	50	-4492	101	-404	0	-1037	29	6.28	6.28	12.57	12.57	-6.42	-82.1
42	50	-4494	89	-416	0	-1128	26	6.28	6.28	12.57	12.57	-7.04	-88.8
43	50	-4406	-201	-352	0	-918	-61	6.28	6.28	12.57	12.57	-5.65	-73.3
44	50	-4392	394	-415	0	-1045	117	6.28	6.28	12.57	12.57	-6.49	-82.6
45	50	-4400	73	-401	0	-1111	21	6.28	6.28	12.57	12.57	-6.94	-87.5
46	50	-4340	88	-368	0	-912	25	6.28	6.28	12.57	12.57	-5.61	-72.8
47	50	-4302	84	-358	0	-881	24	6.28	6.28	12.57	12.57	-5.42	-70.5
49	50	-4304	26	-352	0	-873	6	6.28	6.28	12.57	12.57	-5.37	-69.9
50	50	-4301	145	-365	0	-899	42	6.28	6.28	12.57	12.57	-5.53	-71.7
51	50	-4302	80	-362	0	-912	23	6.28	6.28	12.57	12.57	-5.61	-72.7

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 91 NI 1161 NF 142 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 18A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-6652	-283	69	0	-942	-23	6.28	6.28	12.57	12.57	-6.05	-81.9
41	0	-6651	195	71	0	-965	29	6.28	6.28	12.57	12.57	-6.16	-83.2
42	0	-6669	166	101	0	-1053	26	6.28	6.28	12.57	12.57	-6.59	-88.4
43	0	-6497	-624	53	0	-852	-61	6.28	6.28	12.57	12.57	-5.61	-76.3
44	0	-6503	997	76	0	-975	117	6.28	6.28	12.57	12.57	-6.17	-83.2
45	0	-6524	125	106	0	-1039	21	6.28	6.28	12.57	12.57	-6.50	-87.0
46	0	-6402	159	48	0	-847	25	6.28	6.28	12.57	12.57	-5.56	-75.6
47	0	-6339	150	42	0	-818	24	6.28	6.28	12.57	12.57	-5.42	-73.8
49	0	-6340	-9	42	0	-810	6	6.28	6.28	12.57	12.57	-5.39	-73.4
50	0	-6341	315	46	0	-835	42	6.28	6.28	12.57	12.57	-5.49	-74.7
51	0	-6345	141	52	0	-847	23	6.28	6.28	12.57	12.57	-5.55	-75.4

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	12	-6577	-283	69	0	-950	-59	6.28	6.28	12.57	12.57	-6.07	-82.0
41	12	-6576	195	71	0	-974	54	6.28	6.28	12.57	12.57	-6.19	-83.4
42	12	-6594	166	101	0	-1066	46	6.28	6.28	12.57	12.57	-6.65	-88.9
43	12	-6422	-624	53	0	-859	-139	6.28	6.28	12.57	12.57	-5.62	-76.3
44	12	-6428	997	76	0	-985	242	6.28	6.28	12.57	12.57	-6.20	-83.4
45	12	-6449	125	106	0	-1052	36	6.28	6.28	12.57	12.57	-6.55	-87.6
46	12	-6327	159	48	0	-853	45	6.28	6.28	12.57	12.57	-5.57	-75.6
47	12	-6264	150	42	0	-823	43	6.28	6.28	12.57	12.57	-5.42	-73.7
49	12	-6265	-9	42	0	-815	5	6.28	6.28	12.57	12.57	-5.38	-73.3
50	12	-6266	315	46	0	-840	81	6.28	6.28	12.57	12.57	-5.49	-74.6
51	12	-6270	141	52	0	-854	40	6.28	6.28	12.57	12.57	-5.55	-75.3

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	25	-6502	-283	69	0	-959	-94	6.28	6.28	12.57	12.57	-6.09	-82.2
41	25	-6501	195	71	0	-983	78	6.28	6.28	12.57	12.57	-6.21	-83.6
42	25	-6519	166	101	0	-1078	67	6.28	6.28	12.57	12.57	-6.70	-89.5
43	25	-6347	-624	53	0	-865	-217	6.28	6.28	12.57	12.57	-5.62	-76.3
44	25	-6353	997	76	0	-994	366	6.28	6.28	12.57	12.57	-6.24	-83.7
45	25	-6374	125	106	0	-1066	52	6.28	6.28	12.57	12.57	-6.61	-88.2
46	25	-6252	159	48	0	-859	65	6.28	6.28	12.57	12.57	-5.57	-75.6
47	25	-6189	150	42	0	-829	61	6.28	6.28	12.57	12.57	-5.42	-73.6
49	25	-6190	-9	42	0	-820	4	6.28	6.28	12.57	12.57	-5.38	-73.2
50	25	-6191	315	46	0	-846	121	6.28	6.28	12.57	12.57	-5.50	-74.6
51	25	-6195	141	52	0	-860	58	6.28	6.28	12.57	12.57	-5.56	-75.4

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	38	-6427	-283	69	0	-967	-129	6.28	6.28	12.57	12.57	-6.12	-82.4
41	38	-6426	195	71	0	-992	102	6.28	6.28	12.57	12.57	-6.24	-83.8
42	38	-6444	166	101	0	-1091	88	6.28	6.28	12.57	12.57	-6.76	-90.0
43	38	-6272	-624	53	0	-872	-295	6.28	6.28	12.57	12.57	-5.63	-76.3
44	38	-6278	997	76	0	-1004	491	6.28	6.28	12.57	12.57	-6.27	-84.0
45	38	-6299	125	106	0	-1079	67	6.28	6.28	12.57	12.57	-6.67	-88.8
46	38	-6177	159	48	0	-865	85	6.28	6.28	12.57	12.57	-5.58	-75.5
47	38	-6114	150	42	0	-834	80	6.28	6.28	12.57	12.57	-5.42	-73.5

49	38	-6115	-9	42	0	-826	3	6.28	6.28	12.57	12.57	-5.38	-73.1
50	38	-6116	315	46	0	-852	160	6.28	6.28	12.57	12.57	-5.50	-74.5
51	38	-6120	141	52	0	-867	75	6.28	6.28	12.57	12.57	-5.57	-75.4

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	50	-6352	-283	69	0	-976	-165	6.28	6.28	12.57	12.57	-6.15	-82.6
41	50	-6351	195	71	0	-1001	127	6.28	6.28	12.57	12.57	-6.27	-84.1
42	50	-6369	166	101	0	-1104	109	6.28	6.28	12.57	12.57	-6.82	-90.6
43	50	-6197	-624	53	0	-879	-373	6.28	6.28	12.57	12.57	-5.64	-76.4
44	50	-6203	997	76	0	-1013	616	6.28	6.28	12.57	12.57	-6.31	-84.3
45	50	-6224	125	106	0	-1092	83	6.28	6.28	12.57	12.57	-6.74	-89.4
46	50	-6102	159	48	0	-872	104	6.28	6.28	12.57	12.57	-5.59	-75.5
47	50	-6039	150	42	0	-839	99	6.28	6.28	12.57	12.57	-5.42	-73.5
49	50	-6040	-9	42	0	-831	2	6.28	6.28	12.57	12.57	-5.39	-73.0
50	50	-6041	315	46	0	-858	200	6.28	6.28	12.57	12.57	-5.51	-74.5
51	50	-6045	141	52	0	-874	93	6.28	6.28	12.57	12.57	-5.58	-75.4

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 92 NI 1256 NF 1259 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 19
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	--												
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-16410	153	-188	0	-489	-613	6.28	6.28	12.57	12.57	-8.94	-122.7
41	0	-16410	9	-217	0	-565	-56	6.28	6.28	12.57	12.57	-8.36	-120.4
42	0	-16340	10	-274	0	-731	-60	6.28	6.28	12.57	12.57	-8.93	-127.4
43	0	-15810	249	-132	0	-348	-984	6.28	6.28	12.57	12.57	-10.55	-140.1
44	0	-15900	-232	-276	0	-717	874	6.28	6.28	12.57	12.57	-10.04	-134.5
45	0	-15690	10	-275	0	-752	-62	6.28	6.28	12.57	12.57	-8.76	-124.6
46	0	-15460	8	-157	0	-421	-55	6.28	6.28	12.57	12.57	-7.48	-108.4
47	0	-15220	8	-142	0	-385	-55	6.28	6.28	12.57	12.57	-7.26	-105.4
49	0	-15220	56	-132	0	-360	-241	6.28	6.28	12.57	12.57	-7.17	-104.3
50	0	-15240	-40	-161	0	-434	131	6.28	6.28	12.57	12.57	-7.44	-107.7
51	0	-15200	9	-161	0	-441	-56	6.28	6.28	12.57	12.57	-7.45	-107.8

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	12	-16335	153	-188	0	-466	-594	6.28	6.28	12.57	12.57	-8.81	-121.2
41	12	-16335	9	-217	0	-538	-55	6.28	6.28	12.57	12.57	-8.24	-118.7
42	12	-16265	10	-274	0	-697	-59	6.28	6.28	12.57	12.57	-8.78	-125.5
43	12	-15735	249	-132	0	-332	-952	6.28	6.28	12.57	12.57	-10.37	-137.9
44	12	-15825	-232	-276	0	-683	845	6.28	6.28	12.57	12.57	-9.87	-132.5
45	12	-15615	10	-275	0	-718	-61	6.28	6.28	12.57	12.57	-8.60	-122.6
46	12	-15385	8	-157	0	-402	-54	6.28	6.28	12.57	12.57	-7.38	-107.1
47	12	-15145	8	-142	0	-367	-54	6.28	6.28	12.57	12.57	-7.17	-104.2
49	12	-15145	56	-132	0	-343	-234	6.28	6.28	12.57	12.57	-7.08	-103.1
50	12	-15165	-40	-161	0	-413	126	6.28	6.28	12.57	12.57	-7.34	-106.4
51	12	-15125	9	-161	0	-420	-55	6.28	6.28	12.57	12.57	-7.35	-106.5

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	25	-16260	153	-188	0	-442	-574	6.28	6.28	12.57	12.57	-8.69	-119.8
41	25	-16260	9	-217	0	-511	-54	6.28	6.28	12.57	12.57	-8.11	-117.1
42	25	-16190	10	-274	0	-663	-57	6.28	6.28	12.57	12.57	-8.63	-123.5
43	25	-15660	249	-132	0	-315	-921	6.28	6.28	12.57	12.57	-10.19	-135.8
44	25	-15750	-232	-276	0	-648	816	6.28	6.28	12.57	12.57	-9.70	-130.4
45	25	-15540	10	-275	0	-684	-60	6.28	6.28	12.57	12.57	-8.45	-120.7
46	25	-15310	8	-157	0	-382	-53	6.28	6.28	12.57	12.57	-7.28	-105.8
47	25	-15070	8	-142	0	-350	-53	6.28	6.28	12.57	12.57	-7.07	-103.0
49	25	-15070	56	-132	0	-327	-227	6.28	6.28	12.57	12.57	-6.99	-102.0
50	25	-15090	-40	-161	0	-393	121	6.28	6.28	12.57	12.57	-7.24	-105.0
51	25	-15050	9	-161	0	-400	-54	6.28	6.28	12.57	12.57	-7.25	-105.1

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	38	-16185	153	-188	0	-418	-555	6.28	6.28	12.57	12.57	-8.57	-118.3
41	38	-16185	9	-217	0	-484	-52	6.28	6.28	12.57	12.57	-7.99	-115.4
42	38	-16115	10	-274	0	-629	-56	6.28	6.28	12.57	12.57	-8.48	-121.5
43	38	-15585	249	-132	0	-299	-890	6.28	6.28	12.57	12.57	-10.01	-133.7
44	38	-15675	-232	-276	0	-614	787	6.28	6.28	12.57	12.57	-9.53	-128.4
45	38	-15465	10	-275	0	-649	-58	6.28	6.28	12.57	12.57	-8.30	-118.7
46	38	-15235	8	-157	0	-362	-52	6.28	6.28	12.57	12.57	-7.18	-104.5
47	38	-14995	8	-142	0	-332	-52	6.28	6.28	12.57	12.57	-6.98	-101.8
49	38	-14995	56	-132	0	-310	-220	6.28	6.28	12.57	12.57	-6.90	-100.8
50	38	-15015	-40	-161	0	-373	116	6.28	6.28	12.57	12.57	-7.14	-103.7
51	38	-14975	9	-161	0	-380	-53	6.28	6.28	12.57	12.57	-7.15	-103.8

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	50	-16110	153	-188	0	-395	-536	6.28	6.28	12.57	12.57	-8.45	-116.8
41	50	-16110	9	-217	0	-457	-51	6.28	6.28	12.57	12.57	-7.86	-113.8
42	50	-16040	10	-274	0	-594	-55	6.28	6.28	12.57	12.57	-8.33	-119.6
43	50	-15510	249	-132	0	-282	-859	6.28	6.28	12.57	12.57	-9.83	-131.5
44	50	-15600	-232	-276	0	-579	758	6.28	6.28	12.57	12.57	-9.36	-126.4
45	50	-15390	10	-275	0	-615	-57	6.28	6.28	12.57	12.57	-8.15	-116.7
46	50	-15160	8	-157	0	-343	-51	6.28	6.28	12.57	12.57	-7.08	-103.2
47	50	-14920	8	-142	0	-314	-51	6.28	6.28	12.57	12.57	-6.89	-100.5
49	50	-14920	56	-132	0	-294	-212	6.28	6.28	12.57	12.57	-6.82	-99.6
50	50	-14940	-40	-161	0	-353	111	6.28	6.28	12.57	12.57	-7.04	-102.4
51	50	-14900	9	-161	0	-360	-52	6.28	6.28	12.57	12.57	-7.05	-102.5

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 93 NI 1259 NF 127 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 19A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	--												
	cm		daN			daN*m				cm^2			daN/cm^2

40	0	-16110	153	-188	0	-395	-536	6.28	6.28	12.57	12.57	-8.45	-116.8
41	0	-16110	9	-217	0	-457	-51	6.28	6.28	12.57	12.57	-7.86	-113.8
42	0	-16040	10	-274	0	-594	-55	6.28	6.28	12.57	12.57	-8.33	-119.6
43	0	-15510	249	-132	0	-282	-859	6.28	6.28	12.57	12.57	-9.83	-131.5
44	0	-15600	-232	-276	0	-579	758	6.28	6.28	12.57	12.57	-9.36	-126.4
45	0	-15390	10	-275	0	-615	-57	6.28	6.28	12.57	12.57	-8.15	-116.7
46	0	-15160	8	-157	0	-343	-51	6.28	6.28	12.57	12.57	-7.08	-103.2
47	0	-14920	8	-142	0	-314	-51	6.28	6.28	12.57	12.57	-6.89	-100.5
49	0	-14920	56	-132	0	-294	-212	6.28	6.28	12.57	12.57	-6.82	-99.6
50	0	-14940	-40	-161	0	-353	111	6.28	6.28	12.57	12.57	-7.04	-102.4
51	0	-14900	9	-161	0	-360	-52	6.28	6.28	12.57	12.57	-7.05	-102.5

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	12	-16035	153	-188	0	-371	-517	6.28	6.28	12.57	12.57	-8.33	-115.4
41	12	-16035	9	-217	0	-430	-50	6.28	6.28	12.57	12.57	-7.73	-112.1
42	12	-15965	10	-274	0	-560	-54	6.28	6.28	12.57	12.57	-8.17	-117.6
43	12	-15435	249	-132	0	-266	-828	6.28	6.28	12.57	12.57	-9.65	-129.4
44	12	-15525	-232	-276	0	-545	729	6.28	6.28	12.57	12.57	-9.19	-124.4
45	12	-15315	10	-275	0	-581	-56	6.28	6.28	12.57	12.57	-8.00	-114.7
46	12	-15085	8	-157	0	-323	-50	6.28	6.28	12.57	12.57	-6.98	-101.9
47	12	-14845	8	-142	0	-297	-50	6.28	6.28	12.57	12.57	-6.80	-99.3
49	12	-14845	56	-132	0	-277	-205	6.28	6.28	12.57	12.57	-6.73	-98.4
50	12	-14865	-40	-161	0	-333	106	6.28	6.28	12.57	12.57	-6.93	-101.0
51	12	-14825	9	-161	0	-340	-51	6.28	6.28	12.57	12.57	-6.94	-101.1

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	25	-15960	153	-188	0	-348	-498	6.28	6.28	12.57	12.57	-8.21	-113.9
41	25	-15960	9	-217	0	-402	-49	6.28	6.28	12.57	12.57	-7.61	-110.5
42	25	-15890	10	-274	0	-526	-52	6.28	6.28	12.57	12.57	-8.02	-115.6
43	25	-15360	249	-132	0	-249	-797	6.28	6.28	12.57	12.57	-9.47	-127.3
44	25	-15450	-232	-276	0	-510	700	6.28	6.28	12.57	12.57	-9.02	-122.4
45	25	-15240	10	-275	0	-546	-55	6.28	6.28	12.57	12.57	-7.84	-112.8
46	25	-15010	8	-157	0	-304	-49	6.28	6.28	12.57	12.57	-6.89	-100.6
47	25	-14770	8	-142	0	-279	-49	6.28	6.28	12.57	12.57	-6.70	-98.1
49	25	-14770	56	-132	0	-261	-198	6.28	6.28	12.57	12.57	-6.64	-97.3
50	25	-14790	-40	-161	0	-313	101	6.28	6.28	12.57	12.57	-6.83	-99.7
51	25	-14750	9	-161	0	-320	-50	6.28	6.28	12.57	12.57	-6.84	-99.8

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	38	-15885	153	-188	0	-324	-479	6.28	6.28	12.57	12.57	-8.09	-112.4
41	38	-15885	9	-217	0	-375	-48	6.28	6.28	12.57	12.57	-7.48	-108.9
42	38	-15815	10	-274	0	-492	-51	6.28	6.28	12.57	12.57	-7.87	-113.6
43	38	-15285	249	-132	0	-233	-766	6.28	6.28	12.57	12.57	-9.29	-125.1
44	38	-15375	-232	-276	0	-476	671	6.28	6.28	12.57	12.57	-8.85	-120.4
45	38	-15165	10	-275	0	-512	-53	6.28	6.28	12.57	12.57	-7.69	-110.8
46	38	-14935	8	-157	0	-284	-48	6.28	6.28	12.57	12.57	-6.79	-99.3
47	38	-14695	8	-142	0	-261	-48	6.28	6.28	12.57	12.57	-6.61	-96.8
49	38	-14695	56	-132	0	-244	-191	6.28	6.28	12.57	12.57	-6.55	-96.1
50	38	-14715	-40	-161	0	-293	96	6.28	6.28	12.57	12.57	-6.73	-98.4
51	38	-14675	9	-161	0	-300	-49	6.28	6.28	12.57	12.57	-6.74	-98.5

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	50	-15810	153	-188	0	-300	-460	6.28	6.28	12.57	12.57	-7.96	-111.0
41	50	-15810	9	-217	0	-348	-47	6.28	6.28	12.57	12.57	-7.35	-107.2
42	50	-15740	10	-274	0	-457	-50	6.28	6.28	12.57	12.57	-7.72	-111.7
43	50	-15210	249	-132	0	-216	-735	6.28	6.28	12.57	12.57	-9.11	-123.0
44	50	-15300	-232	-276	0	-442	642	6.28	6.28	12.57	12.57	-8.68	-118.3
45	50	-15090	10	-275	0	-478	-52	6.28	6.28	12.57	12.57	-7.54	-108.8
46	50	-14860	8	-157	0	-264	-47	6.28	6.28	12.57	12.57	-6.69	-97.9
47	50	-14620	8	-142	0	-243	-47	6.28	6.28	12.57	12.57	-6.52	-95.6
49	50	-14620	56	-132	0	-228	-184	6.28	6.28	12.57	12.57	-6.46	-94.9
50	50	-14640	-40	-161	0	-272	91	6.28	6.28	12.57	12.57	-6.63	-97.0
51	50	-14600	9	-161	0	-280	-48	6.28	6.28	12.57	12.57	-6.64	-97.1

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 94 NI 1034 NF 1040 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 20
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	--												
	cm		daN			daN*m				cm^2			daN/cm^2

40	0	-29500	634	744	0	1627	-1906	6.28	6.28	12.57	12.57	-20.04	-265.3
41	0	-29830	124	690	0	1499	-366	6.28	6.28	12.57	12.57	-16.89	-240.0
42	0	-29760	128	542	0	1189	-375	6.28	6.28	12.57	12.57	-15.75	-225.7
43	0	-28060	960	708	0	1592	-2899	6.28	6.28	12.57	12.57	-25.09	-318.4
44	0	-30110	-726	592	0	1251	2203	6.28	6.28	12.57	12.57	-21.73	-285.1
45	0	-28510	116	373	0	862	-347	6.28	6.28	12.57	12.57	-14.10	-203.8
46	0	-27910	101	577	0	1305	-310	6.28	6.28	12.57	12.57	-15.46	-220.1
47	0	-27420	96	549	0	1257	-296	6.28	6.28	12.57	12.57	-15.09	-215.2
49	0	-27310	266	566	0	1300	-810	6.28	6.28	12.57	12.57	-15.21	-216.4
50	0	-27720	-71	543	0	1231	211	6.28	6.28	12.57	12.57	-15.12	-215.7
51	0	-27400	97	499	0	1154	-299	6.28	6.28	12.57	12.57	-14.72	-210.4

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	12	-29425	634	744	0	1534	-1827	6.28	6.28	12.57	12.57	-19.62	-260.5
41	12	-29755	124	690	0	1413	-350	6.28	6.28	12.57	12.57	-16.55	-235.7
42	12	-29685	128	542	0	1121	-359	6.28	6.28	12.57	12.57	-15.48	-222.2
43	12	-27985	960	708	0	1504	-2779	6.28	6.28	12.57	12.57	-24.31	-310.0
44	12	-30035	-726	592	0	1177	2112	6.28	6.28	12.57	12.57	-21.25	-279.6
45	12	-28435	116	373	0	816	-332	6.28	6.28	12.57	12.57	-13.91	-201.3
46	12	-27835	101	577	0	1233	-297	6.28	6.28	12.57	12.57	-15.17	-216.5
47	12	-27345	96	549	0	1188	-284	6.28	6.28	12.57	12.57	-14.82	-211.7
49	12	-27235	266	566	0	1229	-776	6.28	6.28	12.57	12.57	-14.92	-212.8
50	12	-27645	-71	543	0	1163	202	6.28	6.28	12.57	12.57	-14.85	-212.3
51	12	-27325	97	499	0	1092	-287	6.28	6.28	12.57	12.57	-14.46	-207.2

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	25	-29350	634	744	0	1442	-1748	6.28	6.28	12.57	12.57	-19.20	-255.7
41	25	-29680	124	690	0	1326	-335	6.28	6.28	12.57	12.57	-16.22	-231.4
42	25	-29610	128	542	0	1054	-343	6.28	6.28	12.57	12.57	-15.21	-218.7
43	25	-27910	960	708	0	1415	-2659	6.28	6.28	12.57	12.57	-23.55	-301.7
44	25	-29960	-726	592	0	1103	2022	6.28	6.28	12.57	12.57	-20.78	-274.2
45	25	-28360	116	373	0	769	-318	6.28	6.28	12.57	12.57	-13.71	-198.8
46	25	-27760	101	577	0	1161	-285	6.28	6.28	12.57	12.57	-14.88	-212.8
47	25	-27270	96	549	0	1120	-272	6.28	6.28	12.57	12.57	-14.54	-208.1
49	25	-27160	266	566	0	1158	-743	6.28	6.28	12.57	12.57	-14.64	-209.2
50	25	-27570	-71	543	0	1095	193	6.28	6.28	12.57	12.57	-14.57	-208.8
51	25	-27250	97	499	0	1029	-275	6.28	6.28	12.57	12.57	-14.21	-204.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	38	-29275	634	744	0	1349	-1668	6.28	6.28	12.57	12.57	-18.78	-250.9
41	38	-29605	124	690	0	1240	-319	6.28	6.28	12.57	12.57	-15.88	-227.1
42	38	-29535	128	542	0	986	-327	6.28	6.28	12.57	12.57	-14.94	-215.3
43	38	-27835	960	708	0	1326	-2539	6.28	6.28	12.57	12.57	-22.81	-293.6
44	38	-29885	-726	592	0	1029	1932	6.28	6.28	12.57	12.57	-20.30	-268.8
45	38	-28285	116	373	0	722	-303	6.28	6.28	12.57	12.57	-13.51	-196.2
46	38	-27685	101	577	0	1089	-272	6.28	6.28	12.57	12.57	-14.59	-209.2
47	38	-27195	96	549	0	1051	-260	6.28	6.28	12.57	12.57	-14.27	-204.6
49	38	-27085	266	566	0	1087	-710	6.28	6.28	12.57	12.57	-14.36	-205.6
50	38	-27495	-71	543	0	1028	184	6.28	6.28	12.57	12.57	-14.30	-205.3
51	38	-27175	97	499	0	966	-263	6.28	6.28	12.57	12.57	-13.96	-200.7

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	50	-29200	634	744	0	1256	-1589	6.28	6.28	12.57	12.57	-18.37	-246.0
41	50	-29530	124	690	0	1154	-304	6.28	6.28	12.57	12.57	-15.54	-222.8
42	50	-29460	128	542	0	918	-311	6.28	6.28	12.57	12.57	-14.67	-211.8
43	50	-27760	960	708	0	1238	-2419	6.28	6.28	12.57	12.57	-22.09	-285.7
44	50	-29810	-726	592	0	955	1841	6.28	6.28	12.57	12.57	-19.83	-263.3
45	50	-28210	116	373	0	676	-289	6.28	6.28	12.57	12.57	-13.32	-193.7
46	50	-27610	101	577	0	1017	-259	6.28	6.28	12.57	12.57	-14.31	-205.5
47	50	-27120	96	549	0	982	-248	6.28	6.28	12.57	12.57	-13.99	-201.1
49	50	-27010	266	566	0	1016	-677	6.28	6.28	12.57	12.57	-14.07	-202.0
50	50	-27420	-71	543	0	960	175	6.28	6.28	12.57	12.57	-14.03	-201.9
51	50	-27100	97	499	0	904	-251	6.28	6.28	12.57	12.57	-13.71	-197.5

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 95 NI 1040 NF 301 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 20A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-29200	634	744	0	1256	-1589	6.28	6.28	12.57	12.57	-18.37	-246.0
41	0	-29530	124	690	0	1154	-304	6.28	6.28	12.57	12.57	-15.54	-222.8
42	0	-29460	128	542	0	918	-311	6.28	6.28	12.57	12.57	-14.67	-211.8
43	0	-27760	960	708	0	1238	-2419	6.28	6.28	12.57	12.57	-22.09	-285.7
44	0	-29810	-726	592	0	955	1841	6.28	6.28	12.57	12.57	-19.83	-263.3
45	0	-28210	116	373	0	676	-289	6.28	6.28	12.57	12.57	-13.32	-193.7
46	0	-27610	101	577	0	1017	-259	6.28	6.28	12.57	12.57	-14.31	-205.5
47	0	-27120	96	549	0	982	-248	6.28	6.28	12.57	12.57	-13.99	-201.1
49	0	-27010	266	566	0	1016	-677	6.28	6.28	12.57	12.57	-14.07	-202.0
50	0	-27420	-71	543	0	960	175	6.28	6.28	12.57	12.57	-14.03	-201.9
51	0	-27100	97	499	0	904	-251	6.28	6.28	12.57	12.57	-13.71	-197.5

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	12	-29125	634	744	0	1163	-1510	6.28	6.28	12.57	12.57	-17.95	-241.2
41	12	-29455	124	690	0	1068	-288	6.28	6.28	12.57	12.57	-15.20	-218.5
42	12	-29385	128	542	0	850	-295	6.28	6.28	12.57	12.57	-14.40	-208.4
43	12	-27685	960	708	0	1149	-2299	6.28	6.28	12.57	12.57	-21.40	-278.0
44	12	-29735	-726	592	0	881	1750	6.28	6.28	12.57	12.57	-19.35	-257.9
45	12	-28135	116	373	0	629	-274	6.28	6.28	12.57	12.57	-13.12	-191.2
46	12	-27535	101	577	0	945	-247	6.28	6.28	12.57	12.57	-14.02	-201.8
47	12	-27045	96	549	0	914	-236	6.28	6.28	12.57	12.57	-13.72	-197.6
49	12	-26935	266	566	0	945	-644	6.28	6.28	12.57	12.57	-13.79	-198.4
50	12	-27345	-71	543	0	892	166	6.28	6.28	12.57	12.57	-13.76	-198.4
51	12	-27025	97	499	0	842	-239	6.28	6.28	12.57	12.57	-13.45	-194.3

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	25	-29050	634	744	0	1070	-1430	6.28	6.28	12.57	12.57	-17.53	-236.4
41	25	-29380	124	690	0	981	-273	6.28	6.28	12.57	12.57	-14.86	-214.2
42	25	-29310	128	542	0	783	-279	6.28	6.28	12.57	12.57	-14.13	-204.9
43	25	-27610	960	708	0	1061	-2179	6.28	6.28	12.57	12.57	-20.73	-270.5
44	25	-29660	-726	592	0	806	1660	6.28	6.28	12.57	12.57	-18.88	-252.4
45	25	-28060	116	373	0	582	-260	6.28	6.28	12.57	12.57	-12.93	-188.7
46	25	-27460	101	577	0	873	-234	6.28	6.28	12.57	12.57	-13.73	-198.2
47	25	-26970	96	549	0	845	-224	6.28	6.28	12.57	12.57	-13.45	-194.1
49	25	-26860	266	566	0	875	-610	6.28	6.28	12.57	12.57	-13.51	-194.8
50	25	-27270	-71	543	0	824	157	6.28	6.28	12.57	12.57	-13.49	-194.9
51	25	-26950	97	499	0	779	-227	6.28	6.28	12.57	12.57	-13.20	-191.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	38	-28975	634	744	0	977	-1351	6.28	6.28	12.57	12.57	-17.11	-231.6
41	38	-29305	124	690	0	895	-257	6.28	6.28	12.57	12.57	-14.53	-209.9
42	38	-29235	128	542	0	715	-263	6.28	6.28	12.57	12.57	-13.85	-201.4
43	38	-27535	960	708	0	972	-2059	6.28	6.28	12.57	12.57	-20.09	-263.2
44	38	-29585	-726	592	0	732	1569	6.28	6.28	12.57	12.57	-18.40	-247.0
45	38	-27985	116	373	0	536	-245	6.28	6.28	12.57	12.57	-12.73	-186.2
46	38	-27385	101	577	0	800	-221	6.28	6.28	12.57	12.57	-13.45	-194.5
47	38	-26895	96	549	0	777	-212	6.28	6.28	12.57	12.57	-13.17	-190.6
49	38	-26785	266	566	0	804	-577	6.28	6.28	12.57	12.57	-13.23	-191.2
50	38	-27195	-71	543	0	756	148	6.28	6.28	12.57	12.57	-13.21	-191.4
51	38	-26875	97	499	0	717	-214	6.28	6.28	12.57	12.57	-12.95	-187.8

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	50	-28900	634	744	0	884	-1272	6.28	6.28	12.57	12.57	-16.69	-226.8
41	50	-29230	124	690	0	808	-242	6.28	6.28	12.57	12.57	-14.19	-205.6
42	50	-29160	128	542	0	647	-247	6.28	6.28	12.57	12.57	-13.58	-197.9
43	50	-27460	960	708	0	884	-1939	6.28	6.28	12.57	12.57	-19.47	-256.1
44	50	-29510	-726	592	0	658	1478	6.28	6.28	12.57	12.57	-17.93	-241.5
45	50	-27910	116	373	0	489	-230	6.28	6.28	12.57	12.57	-12.53	-183.6
46	50	-27310	101	577	0	728	-209	6.28	6.28	12.57	12.57	-13.16	-190.8
47	50	-26820	96	549	0	708	-200	6.28	6.28	12.57	12.57	-12.90	-187.1
49	50	-26710	266	566	0	733	-544	6.28	6.28	12.57	12.57	-12.94	-187.6
50	50	-27120	-71	543	0	688	139	6.28	6.28	12.57	12.57	-12.94	-188.0
51	50	-26800	97	499	0	654	-202	6.28	6.28	12.57	12.57	-12.70	-184.6

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 96 NI 1352 NF 1355 SEZ. Rp B= 0.400 H= 0.600 (pilastro)
PIL. NUM. 21
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-10070	1808	620	0	1279	-5288	12.57	12.57	6.28	6.28	-34.77	947.2
41	0	-10100	865	598	0	1218	-2556	12.57	12.57	6.28	6.28	-15.97	-201.2
42	0	-10120	870	573	0	1143	-2567	12.57	12.57	6.28	6.28	-16.04	-202.0
43	0	-9892	2261	612	0	1268	-6610	12.57	12.57	6.28	6.28	-43.53	1363.1
44	0	-9950	-681	544	0	1084	1927	12.57	12.57	6.28	6.28	-11.84	-155.2
45	0	-9984	697	533	0	1041	-2075	12.57	12.57	6.28	6.28	-12.76	-165.7
46	0	-9851	584	562	0	1136	-1756	12.57	12.57	6.28	6.28	-10.82	-143.3
47	0	-9790	514	553	0	1115	-1557	12.57	12.57	6.28	6.28	-9.74	-130.5
49	0	-9779	828	560	0	1135	-2467	12.57	12.57	6.28	6.28	-15.40	-194.2
50	0	-9791	240	546	0	1099	-760	12.57	12.57	6.28	6.28	-9.34	-117.2
51	0	-9798	516	544	0	1090	-1560	12.57	12.57	6.28	6.28	-9.75	-130.7

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	12	-9994	1808	620	0	1201	-5062	12.57	12.57	6.28	6.28	-33.26	883.8
41	12	-10024	865	598	0	1143	-2448	12.57	12.57	6.28	6.28	-15.23	-193.1
42	12	-10046	870	573	0	1071	-2458	12.57	12.57	6.28	6.28	-15.30	-193.9
43	12	-9817	2261	612	0	1191	-6328	12.57	12.57	6.28	6.28	-41.67	1281.3
44	12	-9875	-681	544	0	1016	1842	12.57	12.57	6.28	6.28	-11.32	-149.2
45	12	-9909	697	533	0	974	-1988	12.57	12.57	6.28	6.28	-12.21	-159.4
46	12	-9776	584	562	0	1066	-1683	12.57	12.57	6.28	6.28	-10.41	-138.4
47	12	-9715	514	553	0	1046	-1492	12.57	12.57	6.28	6.28	-9.40	-126.3
49	12	-9704	828	560	0	1065	-2364	12.57	12.57	6.28	6.28	-14.70	-186.4
50	12	-9716	240	546	0	1031	-730	12.57	12.57	6.28	6.28	-8.86	-112.1
51	12	-9723	516	544	0	1022	-1496	12.57	12.57	6.28	6.28	-9.41	-126.5

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	25	-9918	1808	620	0	1124	-4836	12.57	12.57	6.28	6.28	-31.75	820.8
41	25	-9949	865	598	0	1068	-2340	12.57	12.57	6.28	6.28	-14.51	-185.0
42	25	-9972	870	573	0	1000	-2350	12.57	12.57	6.28	6.28	-14.57	-185.7
43	25	-9742	2261	612	0	1115	-6045	12.57	12.57	6.28	6.28	-39.81	1199.6
44	25	-9800	-681	544	0	948	1757	12.57	12.57	6.28	6.28	-10.83	-143.3
45	25	-9834	697	533	0	908	-1900	12.57	12.57	6.28	6.28	-11.67	-153.1
46	25	-9701	584	562	0	995	-1610	12.57	12.57	6.28	6.28	-10.00	-133.5
47	25	-9640	514	553	0	977	-1428	12.57	12.57	6.28	6.28	-9.07	-122.3
49	25	-9629	828	560	0	995	-2260	12.57	12.57	6.28	6.28	-14.01	-178.7
50	25	-9641	240	546	0	962	-700	12.57	12.57	6.28	6.28	-8.40	-107.1
51	25	-9648	516	544	0	954	-1431	12.57	12.57	6.28	6.28	-9.08	-122.5

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	37	-9843	1808	620	0	1046	-4610	12.57	12.57	6.28	6.28	-30.23	758.0
41	37	-9873	865	598	0	994	-2231	12.57	12.57	6.28	6.28	-13.79	-176.9
42	37	-9897	870	573	0	928	-2241	12.57	12.57	6.28	6.28	-13.85	-177.6
43	37	-9667	2261	612	0	1038	-5762	12.57	12.57	6.28	6.28	-37.94	1118.1
44	37	-9725	-681	544	0	880	1672	12.57	12.57	6.28	6.28	-10.34	-137.5
45	37	-9759	697	533	0	841	-1813	12.57	12.57	6.28	6.28	-11.15	-146.9
46	37	-9626	584	562	0	925	-1537	12.57	12.57	6.28	6.28	-9.61	-128.7
47	37	-9565	514	553	0	908	-1364	12.57	12.57	6.28	6.28	-8.75	-118.3
49	37	-9554	828	560	0	925	-2156	12.57	12.57	6.28	6.28	-13.33	-171.0
50	37	-9566	240	546	0	894	-670	12.57	12.57	6.28	6.28	-7.96	-102.3
51	37	-9573	516	544	0	886	-1366	12.57	12.57	6.28	6.28	-8.76	-118.5

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	50	-9767	1808	620	0	969	-4384	12.57	12.57	6.28	6.28	-28.71	695.5
41	50	-9798	865	598	0	919	-2123	12.57	12.57	6.28	6.28	-13.08	-168.9
42	50	-9823	870	573	0	856	-2132	12.57	12.57	6.28	6.28	-13.14	-169.6
43	50	-9592	2261	612	0	962	-5480	12.57	12.57	6.28	6.28	-36.07	1036.8
44	50	-9650	-681	544	0	812	1587	12.57	12.57	6.28	6.28	-9.87	-131.8
45	50	-9684	697	533	0	774	-1726	12.57	12.57	6.28	6.28	-10.64	-140.9
46	50	-9551	584	562	0	855	-1464	12.57	12.57	6.28	6.28	-9.22	-124.0
47	50	-9490	514	553	0	839	-1299	12.57	12.57	6.28	6.28	-8.43	-114.4
49	50	-9479	828	560	0	855	-2053	12.57	12.57	6.28	6.28	-12.65	-163.3
50	50	-9491	240	546	0	825	-640	12.57	12.57	6.28	6.28	-7.54	-97.6
51	50	-9498	516	544	0	818	-1302	12.57	12.57	6.28	6.28	-8.45	-114.6

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

ASTA NUM. 97 NI 1355 NF 172 SEZ. Rp B= 0.400 H= 0.600 (pilastro)
PIL. NUM. 21A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-9767	1808	620	0	969	-4384	12.57	12.57	6.28	6.28	-28.71	695.5
41	0	-9798	865	598	0	919	-2123	12.57	12.57	6.28	6.28	-13.08	-168.9
42	0	-9823	870	573	0	856	-2132	12.57	12.57	6.28	6.28	-13.14	-169.6
43	0	-9592	2261	612	0	962	-5480	12.57	12.57	6.28	6.28	-36.07	1036.8

44	0	-9650	-681	544	0	812	1587	12.57	12.57	6.28	6.28	-9.87	-131.8
45	0	-9684	697	533	0	774	-1726	12.57	12.57	6.28	6.28	-10.64	-140.9
46	0	-9551	584	562	0	855	-1464	12.57	12.57	6.28	6.28	-9.22	-124.0
47	0	-9490	514	553	0	839	-1299	12.57	12.57	6.28	6.28	-8.43	-114.4
49	0	-9479	828	560	0	855	-2053	12.57	12.57	6.28	6.28	-12.65	-163.3
50	0	-9491	240	546	0	825	-640	12.57	12.57	6.28	6.28	-7.54	-97.6
51	0	-9498	516	544	0	818	-1302	12.57	12.57	6.28	6.28	-8.45	-114.6

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	12	-9692	1808	620	0	891	-4158	12.57	12.57	6.28	6.28	-27.18	633.4
41	12	-9723	865	598	0	844	-2015	12.57	12.57	6.28	6.28	-12.39	-161.0
42	12	-9748	870	573	0	784	-2024	12.57	12.57	6.28	6.28	-12.44	-161.6
43	12	-9517	2261	612	0	885	-5197	12.57	12.57	6.28	6.28	-34.20	955.7
44	12	-9575	-681	544	0	744	1502	12.57	12.57	6.28	6.28	-9.42	-126.3
45	12	-9609	697	533	0	708	-1639	12.57	12.57	6.28	6.28	-10.15	-135.0
46	12	-9476	584	562	0	784	-1391	12.57	12.57	6.28	6.28	-8.85	-119.4
47	12	-9415	514	553	0	770	-1235	12.57	12.57	6.28	6.28	-8.13	-110.6
49	12	-9404	828	560	0	785	-1950	12.57	12.57	6.28	6.28	-11.99	-155.7
50	12	-9416	240	546	0	757	-610	12.57	12.57	6.28	6.28	-7.14	-93.1
51	12	-9423	516	544	0	750	-1238	12.57	12.57	6.28	6.28	-8.15	-110.8

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	25	-9617	1808	620	0	814	-3932	12.57	12.57	6.28	6.28	-25.64	571.9
41	25	-9648	865	598	0	769	-1907	12.57	12.57	6.28	6.28	-11.71	-153.2
42	25	-9673	870	573	0	713	-1915	12.57	12.57	6.28	6.28	-11.76	-153.8
43	25	-9442	2261	612	0	809	-4914	12.57	12.57	6.28	6.28	-32.31	874.9
44	25	-9500	-681	544	0	676	1416	12.57	12.57	6.28	6.28	-8.98	-121.0
45	25	-9534	697	533	0	641	-1552	12.57	12.57	6.28	6.28	-9.67	-129.3
46	25	-9401	584	562	0	714	-1318	12.57	12.57	6.28	6.28	-8.49	-115.0
47	25	-9340	514	553	0	700	-1170	12.57	12.57	6.28	6.28	-7.84	-107.0
49	25	-9329	828	560	0	715	-1846	12.57	12.57	6.28	6.28	-11.34	-148.3
50	25	-9341	240	546	0	689	-580	12.57	12.57	6.28	6.28	-6.77	-88.7
51	25	-9348	516	544	0	682	-1174	12.57	12.57	6.28	6.28	-7.85	-107.1

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	38	-9542	1808	620	0	736	-3706	12.57	12.57	6.28	6.28	-24.10	511.0
41	38	-9573	865	598	0	694	-1799	12.57	12.57	6.28	6.28	-11.06	-145.5
42	38	-9598	870	573	0	641	-1806	12.57	12.57	6.28	6.28	-11.10	-146.1
43	38	-9367	2261	612	0	732	-4632	12.57	12.57	6.28	6.28	-30.42	794.5
44	38	-9425	-681	544	0	608	1331	12.57	12.57	6.28	6.28	-8.56	-115.9
45	38	-9459	697	533	0	574	-1465	12.57	12.57	6.28	6.28	-9.21	-123.7
46	38	-9326	584	562	0	644	-1245	12.57	12.57	6.28	6.28	-8.15	-110.7
47	38	-9265	514	553	0	631	-1106	12.57	12.57	6.28	6.28	-7.56	-103.4
49	38	-9254	828	560	0	645	-1742	12.57	12.57	6.28	6.28	-10.71	-140.9
50	38	-9266	240	546	0	620	-550	12.57	12.57	6.28	6.28	-6.40	-84.5
51	38	-9273	516	544	0	614	-1109	12.57	12.57	6.28	6.28	-7.57	-103.6

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	50	-9467	1808	620	0	659	-3480	12.57	12.57	6.28	6.28	-22.54	451.0
41	50	-9498	865	598	0	620	-1691	12.57	12.57	6.28	6.28	-10.42	-138.1
42	50	-9523	870	573	0	570	-1698	12.57	12.57	6.28	6.28	-10.47	-138.6
43	50	-9292	2261	612	0	656	-4349	12.57	12.57	6.28	6.28	-28.52	714.6
44	50	-9350	-681	544	0	540	1246	12.57	12.57	6.28	6.28	-8.16	-110.9
45	50	-9384	697	533	0	508	-1378	12.57	12.57	6.28	6.28	-8.77	-118.3
46	50	-9251	584	562	0	574	-1172	12.57	12.57	6.28	6.28	-7.82	-106.6
47	50	-9190	514	553	0	562	-1042	12.57	12.57	6.28	6.28	-7.29	-99.9
49	50	-9179	828	560	0	575	-1639	12.57	12.57	6.28	6.28	-10.10	-133.8
50	50	-9191	240	546	0	552	-520	12.57	12.57	6.28	6.28	-6.04	-80.3
51	50	-9198	516	544	0	546	-1045	12.57	12.57	6.28	6.28	-7.30	-100.1

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

ASTA NUM. 98 NI 479 NF 595 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 7
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-979	45	-327	0	-7	-28	6.28	6.28	9.42	9.42	-0.73	-9.6
41	0	-1069	194	-163	0	33	-76	6.28	6.28	9.42	9.42	-1.25	-14.9
42	0	-770	-98	-1072	0	-409	3	6.28	6.28	9.42	9.42	-3.18	75.7
43	0	-1000	-75	-456	0	-28	21	6.28	6.28	9.42	9.42	-0.68	-9.2
44	0	-1233	447	111	0	96	-160	6.28	6.28	9.42	9.42	-2.50	-25.7
45	0	-651	-313	-1698	0	-698	73	6.28	6.28	9.42	9.42	-5.33	173.7
46	0	-1200	161	-194	0	42	-49	6.28	6.28	9.42	9.42	-1.03	-13.2
47	0	-1232	153	-202	0	44	-42	6.28	6.28	9.42	9.42	-0.98	-12.8
49	0	-1202	103	-257	0	31	-26	6.28	6.28	9.42	9.42	-0.82	-11.1
50	0	-1249	207	-144	0	56	-62	6.28	6.28	9.42	9.42	-1.17	-14.7
51	0	-1132	55	-505	0	-103	-16	6.28	6.28	9.42	9.42	-1.04	-14.4

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	12	-923	45	-327	0	34	-22	6.28	6.28	9.42	9.42	-0.65	-8.9
41	12	-1013	194	-163	0	53	-52	6.28	6.28	9.42	9.42	-0.97	-12.1
42	12	-713	-98	-1072	0	-275	-9	6.28	6.28	9.42	9.42	-2.14	39.1
43	12	-944	-75	-456	0	29	12	6.28	6.28	9.42	9.42	-0.61	-8.8
44	12	-1177	447	111	0	82	-104	6.28	6.28	9.42	9.42	-1.63	-18.7
45	12	-595	-313	-1698	0	-485	34	6.28	6.28	9.42	9.42	-3.74	110.9
46	12	-1144	161	-194	0	66	-29	6.28	6.28	9.42	9.42	-0.88	-12.4
47	12	-1176	153	-202	0	69	-23	6.28	6.28	9.42	9.42	-0.91	-12.8
49	12	-1146	103	-257	0	63	-13	6.28	6.28	9.42	9.42	-0.86	-12.2
50	12	-1193	207	-144	0	74	-36	6.28	6.28	9.42	9.42	-0.94	-13.2
51	12	-1076	55	-505	0	-40	-9	6.28	6.28	9.42	9.42	-0.72	-10.4

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	25	-866	45	-327	0	75	-17	6.28	6.28	9.42	9.42	-0.78	-10.8
41	25	-957	194	-163	0	73	-28	6.28	6.28	9.42	9.42	-0.82	-11.4
42	25	-657	-98	-1072	0	-141	-22	6.28	6.28	9.42	9.42	-1.09	-14.1
43	25	-888	-75	-456	0	86	3	6.28	6.28	9.42	9.42	-0.84	-11.6
44	25	-1120	447	111	0	69	-48	6.28	6.28	9.42	9.42	-0.98	-12.5

45	25	-539	-313	-1698	0	-273	-6	6.28	6.28	9.42	9.42	-2.13	49.0
46	25	-1087	161	-194	0	90	-9	6.28	6.28	9.42	9.42	-0.96	-13.4
47	25	-1120	153	-202	0	95	-4	6.28	6.28	9.42	9.42	-0.99	-13.8
49	25	-1090	103	-257	0	95	-0	6.28	6.28	9.42	9.42	-0.98	-13.6
50	25	-1136	207	-144	0	92	-11	6.28	6.28	9.42	9.42	-0.99	-13.8
51	25	-1020	55	-505	0	23	-2	6.28	6.28	9.42	9.42	-0.62	-9.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	38	-810	45	-327	0	116	-11	6.28	6.28	9.42	9.42	-0.95	-12.8
41	38	-900	194	-163	0	94	-4	6.28	6.28	9.42	9.42	-0.88	-12.1
42	38	-601	-98	-1072	0	-7	-34	6.28	6.28	9.42	9.42	-0.60	-7.4
43	38	-831	-75	-456	0	143	-7	6.28	6.28	9.42	9.42	-1.13	-15.0
44	38	-1064	447	111	0	55	8	6.28	6.28	9.42	9.42	-0.78	-11.1
45	38	-483	-313	-1698	0	-61	-45	6.28	6.28	9.42	9.42	-0.70	-7.9
46	38	-1031	161	-194	0	115	11	6.28	6.28	9.42	9.42	-1.04	-14.3
47	38	-1063	153	-202	0	120	15	6.28	6.28	9.42	9.42	-1.08	-14.9
49	38	-1033	103	-257	0	127	13	6.28	6.28	9.42	9.42	-1.10	-15.1
50	38	-1080	207	-144	0	109	15	6.28	6.28	9.42	9.42	-1.04	-14.4
51	38	-963	55	-505	0	86	5	6.28	6.28	9.42	9.42	-0.88	-12.2

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	50	-754	45	-327	0	156	-5	6.28	6.28	9.42	9.42	-1.21	-15.8
41	50	-844	194	-163	0	114	21	6.28	6.28	9.42	9.42	-0.95	-13.0
42	50	-544	-98	-1072	0	127	-46	6.28	6.28	9.42	9.42	-0.98	-12.6
43	50	-775	-75	-456	0	200	-16	6.28	6.28	9.42	9.42	-1.55	-19.6
44	50	-1008	447	111	0	41	63	6.28	6.28	9.42	9.42	-1.07	-13.1
45	50	-426	-313	-1698	0	152	-84	6.28	6.28	9.42	9.42	-1.33	19.7
46	50	-975	161	-194	0	139	31	6.28	6.28	9.42	9.42	-1.14	-15.5
47	50	-1007	153	-202	0	145	34	6.28	6.28	9.42	9.42	-1.19	-16.1
49	50	-977	103	-257	0	159	25	6.28	6.28	9.42	9.42	-1.26	-16.9
50	50	-1024	207	-144	0	127	41	6.28	6.28	9.42	9.42	-1.10	-15.0
51	50	-907	55	-505	0	150	12	6.28	6.28	9.42	9.42	-1.18	-15.8

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 99 NI 595 NF 23 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 7A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-1069	55	-331	0	246	13	6.28	6.28	9.42	9.42	-1.89	-24.4
41	0	-1206	231	-210	0	193	59	6.28	6.28	9.42	9.42	-1.54	-20.6
42	0	-980	137	-483	0	426	45	6.28	6.28	9.42	9.42	-3.32	67.8
43	0	-1031	-32	-431	0	284	-20	6.28	6.28	9.42	9.42	-2.20	-27.6
44	0	-1466	520	-3	0	105	136	6.28	6.28	9.42	9.42	-2.12	-24.0
45	0	-883	106	-685	0	585	33	6.28	6.28	9.42	9.42	-4.53	122.5
46	0	-1292	281	-242	0	198	54	6.28	6.28	9.42	9.42	-1.59	-21.5
47	0	-1313	293	-250	0	200	53	6.28	6.28	9.42	9.42	-1.61	-21.7
49	0	-1267	234	-290	0	217	37	6.28	6.28	9.42	9.42	-1.71	-22.8
50	0	-1354	345	-204	0	181	69	6.28	6.28	9.42	9.42	-1.52	-20.7
51	0	-1238	262	-340	0	277	48	6.28	6.28	9.42	9.42	-2.13	-27.6

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	12	-1013	55	-331	0	287	20	6.28	6.28	9.42	9.42	-2.22	-27.8
41	12	-1150	231	-210	0	219	88	6.28	6.28	9.42	9.42	-1.70	-22.4
42	12	-924	137	-483	0	486	62	6.28	6.28	9.42	9.42	-3.79	89.5
43	12	-975	-32	-431	0	338	-24	6.28	6.28	9.42	9.42	-2.63	42.7
44	12	-1410	520	-3	0	105	201	6.28	6.28	9.42	9.42	-3.14	31.6
45	12	-827	106	-685	0	671	46	6.28	6.28	9.42	9.42	-5.16	153.0
46	12	-1236	281	-242	0	228	89	6.28	6.28	9.42	9.42	-1.78	-23.5
47	12	-1257	293	-250	0	231	89	6.28	6.28	9.42	9.42	-1.80	-23.8
49	12	-1211	234	-290	0	253	67	6.28	6.28	9.42	9.42	-1.95	-25.5
50	12	-1298	345	-204	0	207	112	6.28	6.28	9.42	9.42	-1.76	-22.1
51	12	-1182	262	-340	0	320	81	6.28	6.28	9.42	9.42	-2.47	-31.1

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	25	-957	55	-331	0	328	27	6.28	6.28	9.42	9.42	-2.55	40.9
41	25	-1094	231	-210	0	245	116	6.28	6.28	9.42	9.42	-1.89	-24.4
42	25	-868	137	-483	0	547	79	6.28	6.28	9.42	9.42	-4.24	111.7
43	25	-919	-32	-431	0	392	-28	6.28	6.28	9.42	9.42	-3.06	61.4
44	25	-1354	520	-3	0	105	266	6.28	6.28	9.42	9.42	-4.20	62.4
45	25	-770	106	-685	0	756	59	6.28	6.28	9.42	9.42	-5.79	183.7
46	25	-1180	281	-242	0	259	124	6.28	6.28	9.42	9.42	-1.99	-25.8
47	25	-1200	293	-250	0	262	126	6.28	6.28	9.42	9.42	-2.02	-26.2
49	25	-1154	234	-290	0	290	96	6.28	6.28	9.42	9.42	-2.23	-28.4
50	25	-1242	345	-204	0	232	155	6.28	6.28	9.42	9.42	-2.41	-25.1
51	25	-1126	262	-340	0	362	113	6.28	6.28	9.42	9.42	-2.81	41.6

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	38	-900	55	-331	0	370	34	6.28	6.28	9.42	9.42	-2.88	55.9
41	38	-1037	231	-210	0	272	145	6.28	6.28	9.42	9.42	-2.27	-26.6
42	38	-811	137	-483	0	607	96	6.28	6.28	9.42	9.42	-4.69	134.3
43	38	-863	-32	-431	0	446	-32	6.28	6.28	9.42	9.42	-3.47	81.0
44	38	-1297	520	-3	0	106	331	6.28	6.28	9.42	9.42	-5.24	95.1
45	38	-714	106	-685	0	842	72	6.28	6.28	9.42	9.42	-6.41	214.6
46	38	-1123	281	-242	0	289	159	6.28	6.28	9.42	9.42	-2.49	-28.3
47	38	-1144	293	-250	0	293	162	6.28	6.28	9.42	9.42	-2.54	-28.7
49	38	-1098	234	-290	0	326	125	6.28	6.28	9.42	9.42	-2.52	33.2
50	38	-1185	345	-204	0	258	198	6.28	6.28	9.42	9.42	-3.12	39.0
51	38	-1069	262	-340	0	405	146	6.28	6.28	9.42	9.42	-3.15	56.5

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	50	-844	55	-331	0	411	41	6.28	6.28	9.42	9.42	-3.20	71.7
41	50	-981	231	-210	0	298	174	6.28	6.28	9.42	9.42	-2.75	36.8
42	50	-755	137	-483	0	668	113	6.28	6.28	9.42	9.42	-5.13	157.0
43	50	-806	-32	-431	0	500	-36	6.28	6.28	9.42	9.42	-3.88	101.2
44	50	-1241	520	-3	0	106	396	6.28	6.28	9.42	9.42	-6.27	128.6
45	50	-658	106	-685	0	927	85	6.28	6.28	9.42	9.42	-7.02	245.6

46	50	-1067	281	-242	0	319	194	6.28	6.28	9.42	9.42	-3.06	42.2
47	50	-1088	293	-250	0	324	199	6.28	6.28	9.42	9.42	-3.14	43.6
49	50	-1042	234	-290	0	362	155	6.28	6.28	9.42	9.42	-2.82	45.8
50	50	-1129	345	-204	0	283	241	6.28	6.28	9.42	9.42	-3.81	60.9
51	50	-1013	262	-340	0	448	179	6.28	6.28	9.42	9.42	-3.49	72.3

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 100 NI 606 NF 624 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 1
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	--												
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-7170	-818	487	0	-199	381	6.28	6.28	9.42	9.42	-6.95	-86.7
41	0	-7855	-525	260	0	-241	336	6.28	6.28	9.42	9.42	-6.86	-87.4
42	0	-7645	-515	131	0	-215	328	6.28	6.28	9.42	9.42	-6.69	-85.2
43	0	-6305	-997	623	0	-141	405	6.28	6.28	9.42	9.42	-6.82	-83.1
44	0	-9065	-43	-114	0	-317	263	6.28	6.28	9.42	9.42	-6.77	-89.4
45	0	-7097	-492	31	0	-168	317	6.28	6.28	9.42	9.42	-6.32	-80.2
46	0	-7203	-501	238	0	-194	326	6.28	6.28	9.42	9.42	-6.45	-81.8
47	0	-7040	-495	232	0	-182	324	6.28	6.28	9.42	9.42	-6.35	-80.4
49	0	-6811	-592	307	0	-168	339	6.28	6.28	9.42	9.42	-6.38	-80.2
50	0	-7363	-402	160	0	-203	310	6.28	6.28	9.42	9.42	-6.39	-81.5
51	0	-6969	-492	189	0	-173	321	6.28	6.28	9.42	9.42	-6.29	-79.7

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	12	-7114	-818	487	0	-260	279	6.28	6.28	9.42	9.42	-5.98	-76.9
41	12	-7799	-525	260	0	-274	270	6.28	6.28	9.42	9.42	-6.23	-81.0
42	12	-7589	-515	131	0	-231	264	6.28	6.28	9.42	9.42	-6.07	-78.9
43	12	-6249	-997	623	0	-219	281	6.28	6.28	9.42	9.42	-5.58	-70.8
44	12	-9009	-43	-114	0	-303	257	6.28	6.28	9.42	9.42	-6.69	-88.5
45	12	-7041	-492	31	0	-172	255	6.28	6.28	9.42	9.42	-5.72	-74.1
46	12	-7147	-501	238	0	-224	263	6.28	6.28	9.42	9.42	-5.85	-75.7
47	12	-6984	-495	232	0	-211	262	6.28	6.28	9.42	9.42	-5.76	-74.3
49	12	-6755	-592	307	0	-206	265	6.28	6.28	9.42	9.42	-5.67	-73.0
50	12	-7307	-402	160	0	-223	260	6.28	6.28	9.42	9.42	-5.90	-76.5
51	12	-6913	-492	189	0	-197	259	6.28	6.28	9.42	9.42	-5.70	-73.6

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	25	-7058	-818	487	0	-320	177	6.28	6.28	9.42	9.42	-5.01	-71.5
41	25	-7742	-525	260	0	-306	205	6.28	6.28	9.42	9.42	-5.60	-75.9
42	25	-7532	-515	131	0	-248	200	6.28	6.28	9.42	9.42	-5.45	-72.6
43	25	-6192	-997	623	0	-297	156	6.28	6.28	9.42	9.42	-4.47	-63.6
44	25	-8952	-43	-114	0	-289	252	6.28	6.28	9.42	9.42	-6.61	-87.6
45	25	-6984	-492	31	0	-175	194	6.28	6.28	9.42	9.42	-5.13	-68.1
46	25	-7090	-501	238	0	-253	201	6.28	6.28	9.42	9.42	-5.25	-69.5
47	25	-6928	-495	232	0	-240	200	6.28	6.28	9.42	9.42	-5.16	-68.2
49	25	-6698	-592	307	0	-245	191	6.28	6.28	9.42	9.42	-4.97	-65.7
50	25	-7250	-402	160	0	-243	210	6.28	6.28	9.42	9.42	-5.41	-71.5
51	25	-6856	-492	189	0	-221	198	6.28	6.28	9.42	9.42	-5.11	-67.6

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	38	-7001	-818	487	0	-381	75	6.28	6.28	9.42	9.42	-5.26	-74.6
41	38	-7686	-525	260	0	-339	139	6.28	6.28	9.42	9.42	-5.41	-77.3
42	38	-7476	-515	131	0	-264	135	6.28	6.28	9.42	9.42	-4.96	-71.4
43	38	-6136	-997	623	0	-375	31	6.28	6.28	9.42	9.42	-4.80	-67.7
44	38	-8896	-43	-114	0	-274	247	6.28	6.28	9.42	9.42	-6.54	-86.7
45	38	-6928	-492	31	0	-179	132	6.28	6.28	9.42	9.42	-4.54	-62.5
46	38	-7034	-501	238	0	-283	138	6.28	6.28	9.42	9.42	-4.83	-69.2
47	38	-6871	-495	232	0	-269	138	6.28	6.28	9.42	9.42	-4.68	-67.2
49	38	-6642	-592	307	0	-283	116	6.28	6.28	9.42	9.42	-4.63	-66.3
50	38	-7194	-402	160	0	-263	160	6.28	6.28	9.42	9.42	-4.92	-69.3
51	38	-6800	-492	189	0	-244	137	6.28	6.28	9.42	9.42	-4.53	-65.2

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	50	-6945	-818	487	0	-442	-28	6.28	6.28	9.42	9.42	-5.51	-77.6
41	50	-7630	-525	260	0	-371	73	6.28	6.28	9.42	9.42	-5.53	-78.7
42	50	-7420	-515	131	0	-280	71	6.28	6.28	9.42	9.42	-5.01	-72.0
43	50	-6080	-997	623	0	-453	-93	6.28	6.28	9.42	9.42	-5.12	-71.7
44	50	-8840	-43	-114	0	-260	241	6.28	6.28	9.42	9.42	-6.46	-85.8
45	50	-6872	-492	31	0	-183	70	6.28	6.28	9.42	9.42	-4.29	-62.3
46	50	-6978	-501	238	0	-313	76	6.28	6.28	9.42	9.42	-4.94	-70.5
47	50	-6815	-495	232	0	-298	76	6.28	6.28	9.42	9.42	-4.79	-68.4
49	50	-6586	-592	307	0	-322	42	6.28	6.28	9.42	9.42	-4.78	-68.0
50	50	-7138	-402	160	0	-283	109	6.28	6.28	9.42	9.42	-4.88	-70.0
51	50	-6744	-492	189	0	-268	75	6.28	6.28	9.42	9.42	-4.61	-66.1

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 101 NI 624 NF 293 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 1A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	--												
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-9032	-1111	190	0	-476	-68	6.28	6.28	9.42	9.42	-6.71	-95.3
41	0	-9591	-105	-34	0	-386	68	6.28	6.28	9.42	9.42	-6.59	-94.4
42	0	-9378	-108	-299	0	-282	67	6.28	6.28	9.42	9.42	-6.00	-86.8
43	0	-8114	-1731	294	0	-494	-163	6.28	6.28	9.42	9.42	-6.34	-89.4
44	0	-10610	1563	-398	0	-245	295	6.28	6.28	9.42	9.42	-7.80	-103.5
45	0	-8692	-59	-521	0	-171	61	6.28	6.28	9.42	9.42	-5.15	-75.3
46	0	-8720	-24	-107	0	-321	60	6.28	6.28	9.42	9.42	-5.85	-84.1
47	0	-8502	-3	-125	0	-304	58	6.28	6.28	9.42	9.42	-5.66	-81.5
49	0	-8316	-339	-51	0	-334	13	6.28	6.28	9.42	9.42	-5.70	-81.8
50	0	-8815	320	-189	0	-284	104	6.28	6.28	9.42	9.42	-5.73	-82.7

51	0	-8432	-4	-214	0	-269	58	6.28	6.28	9.42	9.42	-5.47	-78.9

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	12	-8976	-1111	190	0	-500	-207	6.28	6.28	9.42	9.42	-6.79	-96.2
41	12	-9535	-105	-34	0	-382	55	6.28	6.28	9.42	9.42	-6.54	-93.7
42	12	-9322	-108	-299	0	-244	54	6.28	6.28	9.42	9.42	-5.80	-84.2
43	12	-8058	-1731	294	0	-531	-380	6.28	6.28	9.42	9.42	-7.36	-92.9
44	12	-10552	1563	-398	0	-195	490	6.28	6.28	9.42	9.42	-9.57	-121.0
45	12	-8636	-59	-521	0	-105	54	6.28	6.28	9.42	9.42	-4.82	-71.2
46	12	-8664	-24	-107	0	-307	57	6.28	6.28	9.42	9.42	-5.76	-82.9
47	12	-8446	-3	-125	0	-288	58	6.28	6.28	9.42	9.42	-5.56	-80.2
49	12	-8260	-339	-51	0	-328	-29	6.28	6.28	9.42	9.42	-5.65	-81.0
50	12	-8759	320	-189	0	-260	144	6.28	6.28	9.42	9.42	-5.59	-80.9
51	12	-8376	-4	-214	0	-242	57	6.28	6.28	9.42	9.42	-5.32	-77.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	25	-8920	-1111	190	0	-524	-345	6.28	6.28	9.42	9.42	-7.46	-97.1
41	25	-9478	-105	-34	0	-378	42	6.28	6.28	9.42	9.42	-6.49	-93.0
42	25	-9266	-108	-299	0	-207	40	6.28	6.28	9.42	9.42	-5.60	-81.7
43	25	-8002	-1731	294	0	-568	-596	6.28	6.28	9.42	9.42	-9.61	-114.3
44	25	-10495	1563	-398	0	-145	685	6.28	6.28	9.42	9.42	-11.47	-139.5
45	25	-8580	-59	-521	0	-40	47	6.28	6.28	9.42	9.42	-4.55	-67.0
46	25	-8608	-24	-107	0	-294	54	6.28	6.28	9.42	9.42	-5.67	-81.7
47	25	-8390	-3	-125	0	-273	57	6.28	6.28	9.42	9.42	-5.46	-78.8
49	25	-8204	-339	-51	0	-321	-72	6.28	6.28	9.42	9.42	-5.59	-80.2
50	25	-8702	320	-189	0	-237	184	6.28	6.28	9.42	9.42	-5.87	-79.6
51	25	-8320	-4	-214	0	-216	57	6.28	6.28	9.42	9.42	-5.17	-75.1

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	38	-8863	-1111	190	0	-547	-484	6.28	6.28	9.42	9.42	-8.71	-108.3
41	38	-9422	-105	-34	0	-374	29	6.28	6.28	9.42	9.42	-6.44	-92.4
42	38	-9209	-108	-299	0	-170	27	6.28	6.28	9.42	9.42	-5.40	-79.1
43	38	-7945	-1731	294	0	-605	-813	6.28	6.28	9.42	9.42	-12.64	-139.6
44	38	-10438	1563	-398	0	-95	881	6.28	6.28	9.42	9.42	-13.88	-161.0
45	38	-8523	-59	-521	0	25	39	6.28	6.28	9.42	9.42	-4.45	-65.7
46	38	-8551	-24	-107	0	-280	51	6.28	6.28	9.42	9.42	-5.58	-80.5
47	38	-8333	-3	-125	0	-257	57	6.28	6.28	9.42	9.42	-5.36	-77.5
49	38	-8147	-339	-51	0	-315	-114	6.28	6.28	9.42	9.42	-5.53	-79.4
50	38	-8646	320	-189	0	-213	224	6.28	6.28	9.42	9.42	-6.21	-82.9
51	38	-8263	-4	-214	0	-189	56	6.28	6.28	9.42	9.42	-5.02	-73.1

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	50	-8807	-1111	190	0	-571	-623	6.28	6.28	9.42	9.42	-10.17	-122.2
41	50	-9366	-105	-34	0	-370	16	6.28	6.28	9.42	9.42	-6.40	-91.7
42	50	-9153	-108	-299	0	-132	13	6.28	6.28	9.42	9.42	-5.21	-76.6
43	50	-7889	-1731	294	0	-642	-1029	6.28	6.28	9.42	9.42	-16.07	-165.0
44	50	-10380	1563	-398	0	-46	1076	6.28	6.28	9.42	9.42	-16.73	-184.2
45	50	-8467	-59	-521	0	90	32	6.28	6.28	9.42	9.42	-4.67	-69.0
46	50	-8495	-24	-107	0	-267	48	6.28	6.28	9.42	9.42	-5.49	-79.3
47	50	-8277	-3	-125	0	-241	57	6.28	6.28	9.42	9.42	-5.26	-76.2
49	50	-8091	-339	-51	0	-309	-156	6.28	6.28	9.42	9.42	-5.48	-78.6
50	50	-8590	320	-189	0	-190	264	6.28	6.28	9.42	9.42	-6.55	-86.2
51	50	-8207	-4	-214	0	-162	56	6.28	6.28	9.42	9.42	-4.87	-71.2

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 102 NI 218 NF 132 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 12
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	--												
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-6452	53	-99	0	333	-5	6.28	6.28	12.57	12.57	-3.69	-52.3
41	0	-6179	127	-41	0	172	-11	6.28	6.28	12.57	12.57	-3.00	-43.5
42	0	-6210	112	-206	0	1592	-8	6.28	6.28	12.57	12.57	-9.96	-125.2
43	0	-6430	6	-127	0	399	-3	6.28	6.28	12.57	12.57	-3.91	-55.1
44	0	-5841	250	52	0	-85	-20	6.28	6.28	12.57	12.57	-2.56	-37.6
45	0	-6025	104	-306	0	2497	-7	6.28	6.28	12.57	12.57	-16.29	368.1
46	0	-5852	129	-25	0	106	-13	6.28	6.28	12.57	12.57	-2.64	-38.7
47	0	-5770	130	-21	0	90	-13	6.28	6.28	12.57	12.57	-2.55	-37.5
49	0	-5861	106	-40	0	143	-11	6.28	6.28	12.57	12.57	-2.78	-40.4
50	0	-5744	154	-4	0	47	-15	6.28	6.28	12.57	12.57	-2.39	-35.4
51	0	-5781	125	-75	0	563	-12	6.28	6.28	12.57	12.57	-4.25	-58.7

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	12	-6377	53	-99	0	346	1	6.28	6.28	12.57	12.57	-3.70	-52.4
41	12	-6104	127	-41	0	178	5	6.28	6.28	12.57	12.57	-2.99	-43.3
42	12	-6135	112	-206	0	1618	6	6.28	6.28	12.57	12.57	-10.15	-127.0
43	12	-6355	6	-127	0	415	-2	6.28	6.28	12.57	12.57	-3.94	-55.4
44	12	-5766	250	52	0	-91	12	6.28	6.28	12.57	12.57	-2.55	-37.5
45	12	-5950	104	-306	0	2535	6	6.28	6.28	12.57	12.57	-16.57	383.8
46	12	-5777	129	-25	0	109	4	6.28	6.28	12.57	12.57	-2.62	-38.4
47	12	-5695	130	-21	0	92	3	6.28	6.28	12.57	12.57	-2.53	-37.1
49	12	-5786	106	-40	0	148	2	6.28	6.28	12.57	12.57	-2.77	-40.2
50	12	-5669	154	-4	0	47	5	6.28	6.28	12.57	12.57	-2.36	-35.0
51	12	-5706	125	-75	0	572	4	6.28	6.28	12.57	12.57	-4.25	-58.7

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	25	-6302	53	-99	0	358	8	6.28	6.28	12.57	12.57	-3.72	-52.5
41	25	-6029	127	-41	0	183	21	6.28	6.28	12.57	12.57	-2.98	-43.1
42	25	-6060	112	-206	0	1644	20	6.28	6.28	12.57	12.57	-10.34	134.5
43	25	-6280	6	-127	0	431	-2	6.28	6.28	12.57	12.57	-3.97	-55.7
44	25	-5691	250	52	0	-98	43	6.28	6.28	12.57	12.57	-2.55	-37.4
45	25	-5875	104	-306	0	2574	18	6.28	6.28	12.57	12.57	-16.84	399.6
46	25	-5702	129	-25	0	112	20	6.28	6.28	12.57	12.57	-2.61	-38.1
47	25	-5620	130	-21	0	95	19	6.28	6.28	12.57	12.57	-2.51	-36.8
49	25	-5711	106	-40	0	153	15	6.28	6.28	12.57	12.57	-2.76	-40.0
50	25	-5594	154	-4	0	48	24	6.28	6.28	12.57	12.57	-2.33	-34.5
51	25	-5631	125	-75	0	582	19	6.28	6.28	12.57	12.57	-4.26	-58.7

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	38	-6227	53	-99	0	370	14	6.28	6.28	12.57	12.57	-3.73	-52.7
41	38	-5954	127	-41	0	188	37	6.28	6.28	12.57	12.57	-2.97	-42.9
42	38	-5985	112	-206	0	1669	34	6.28	6.28	12.57	12.57	-10.54	143.9
43	38	-6205	6	-127	0	447	-1	6.28	6.28	12.57	12.57	-4.00	-56.0
44	38	-5616	250	52	0	-104	74	6.28	6.28	12.57	12.57	-2.54	-37.2
45	38	-5800	104	-306	0	2612	31	6.28	6.28	12.57	12.57	-17.10	415.5
46	38	-5627	129	-25	0	116	36	6.28	6.28	12.57	12.57	-2.59	-37.8
47	38	-5545	130	-21	0	97	36	6.28	6.28	12.57	12.57	-2.49	-36.5
49	38	-5636	106	-40	0	158	28	6.28	6.28	12.57	12.57	-2.74	-39.7
50	38	-5519	154	-4	0	48	43	6.28	6.28	12.57	12.57	-2.30	-34.1
51	38	-5556	125	-75	0	591	35	6.28	6.28	12.57	12.57	-4.26	-58.7

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	50	-6152	53	-99	0	383	21	6.28	6.28	12.57	12.57	-3.75	-52.8
41	50	-5879	127	-41	0	193	53	6.28	6.28	12.57	12.57	-2.96	-42.7
42	50	-5910	112	-206	0	1695	48	6.28	6.28	12.57	12.57	-10.73	153.6
43	50	-6130	6	-127	0	463	-0	6.28	6.28	12.57	12.57	-4.02	-56.2
44	50	-5541	250	52	0	-111	106	6.28	6.28	12.57	12.57	-2.54	-37.1
45	50	-5725	104	-306	0	2650	44	6.28	6.28	12.57	12.57	-17.37	431.5
46	50	-5552	129	-25	0	119	52	6.28	6.28	12.57	12.57	-2.57	-37.5
47	50	-5470	130	-21	0	100	52	6.28	6.28	12.57	12.57	-2.47	-36.2
49	50	-5561	106	-40	0	163	42	6.28	6.28	12.57	12.57	-2.73	-39.5
50	50	-5444	154	-4	0	49	63	6.28	6.28	12.57	12.57	-2.28	-33.7
51	50	-5481	125	-75	0	601	50	6.28	6.28	12.57	12.57	-4.27	-58.7

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 103 NI 132 NF 40 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 12A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	

40	0	-9713	225	-175	0	365	21	6.28	6.28	12.57	12.57	-5.06	-72.6
41	0	-9270	537	-72	0	181	53	6.28	6.28	12.57	12.57	-4.23	-61.8
42	0	-9304	501	-347	0	1537	48	6.28	6.28	12.57	12.57	-9.55	-127.5
43	0	-9684	6	-226	0	443	-0	6.28	6.28	12.57	12.57	-5.33	-76.0
44	0	-8718	1065	94	0	-114	106	6.28	6.28	12.57	12.57	-3.77	-55.6
45	0	-9003	466	-512	0	2398	44	6.28	6.28	12.57	12.57	-15.06	189.5
46	0	-8753	520	-43	0	111	52	6.28	6.28	12.57	12.57	-3.78	-55.7
47	0	-8623	516	-36	0	94	52	6.28	6.28	12.57	12.57	-3.67	-54.2
49	0	-8771	412	-70	0	155	42	6.28	6.28	12.57	12.57	-3.94	-57.8
50	0	-8577	624	-6	0	43	63	6.28	6.28	12.57	12.57	-3.47	-51.6
51	0	-8634	504	-128	0	546	50	6.28	6.28	12.57	12.57	-5.29	-74.5

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	12	-9638	225	-175	0	387	49	6.28	6.28	12.57	12.57	-5.11	-73.2
41	12	-9195	537	-72	0	190	120	6.28	6.28	12.57	12.57	-4.23	-61.8
42	12	-9229	501	-347	0	1580	110	6.28	6.28	12.57	12.57	-9.78	-130.1
43	12	-9609	6	-226	0	472	1	6.28	6.28	12.57	12.57	-5.40	-76.8
44	12	-8643	1065	94	0	-125	239	6.28	6.28	12.57	12.57	-4.29	-60.0
45	12	-8928	466	-512	0	2462	103	6.28	6.28	12.57	12.57	-15.52	207.8
46	12	-8678	520	-43	0	116	117	6.28	6.28	12.57	12.57	-3.77	-55.5
47	12	-8548	516	-36	0	98	116	6.28	6.28	12.57	12.57	-3.65	-53.9
49	12	-8696	412	-70	0	163	93	6.28	6.28	12.57	12.57	-3.94	-57.7
50	12	-8502	624	-6	0	44	141	6.28	6.28	12.57	12.57	-3.76	-53.7
51	12	-8559	504	-128	0	562	113	6.28	6.28	12.57	12.57	-5.32	-74.7

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	25	-9563	225	-175	0	408	77	6.28	6.28	12.57	12.57	-5.16	-73.7
41	25	-9120	537	-72	0	199	187	6.28	6.28	12.57	12.57	-4.24	-61.8
42	25	-9154	501	-347	0	1624	173	6.28	6.28	12.57	12.57	-10.01	-132.7
43	25	-9534	6	-226	0	500	1	6.28	6.28	12.57	12.57	-5.47	-77.6
44	25	-8568	1065	94	0	-137	372	6.28	6.28	12.57	12.57	-4.92	-67.0
45	25	-8853	466	-512	0	2526	161	6.28	6.28	12.57	12.57	-15.99	226.8
46	25	-8603	520	-43	0	122	182	6.28	6.28	12.57	12.57	-4.00	-56.6
47	25	-8473	516	-36	0	102	181	6.28	6.28	12.57	12.57	-3.95	-55.8
49	25	-8621	412	-70	0	172	144	6.28	6.28	12.57	12.57	-3.95	-57.7
50	25	-8427	624	-6	0	45	219	6.28	6.28	12.57	12.57	-4.11	-57.7
51	25	-8484	504	-128	0	577	176	6.28	6.28	12.57	12.57	-5.35	-75.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	38	-9488	225	-175	0	430	105	6.28	6.28	12.57	12.57	-5.21	-74.2
41	38	-9045	537	-72	0	208	254	6.28	6.28	12.57	12.57	-4.51	-63.0
42	38	-9079	501	-347	0	1668	236	6.28	6.28	12.57	12.57	-10.26	-135.4
43	38	-9459	6	-226	0	528	2	6.28	6.28	12.57	12.57	-5.54	-78.4
44	38	-8493	1065	94	0	-149	505	6.28	6.28	12.57	12.57	-5.55	-73.9
45	38	-8778	466	-512	0	2590	219	6.28	6.28	12.57	12.57	-16.45	246.3
46	38	-8528	520	-43	0	127	247	6.28	6.28	12.57	12.57	-4.29	-59.8
47	38	-8398	516	-36	0	107	246	6.28	6.28	12.57	12.57	-4.24	-59.0
49	38	-8546	412	-70	0	181	196	6.28	6.28	12.57	12.57	-4.05	-57.6
50	38	-8352	624	-6	0	46	297	6.28	6.28	12.57	12.57	-4.47	-61.6
51	38	-8409	504	-128	0	593	239	6.28	6.28	12.57	12.57	-5.37	-75.3

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	50	-9413	225	-175	0	452	134	6.28	6.28	12.57	12.57	-5.26	-74.8
41	50	-8970	537	-72	0	217	321	6.28	6.28	12.57	12.57	-4.82	-66.3
42	50	-9004	501	-347	0	1711	298	6.28	6.28	12.57	12.57	-10.51	-138.2
43	50	-9384	6	-226	0	556	3	6.28	6.28	12.57	12.57	-5.62	-79.3
44	50	-8418	1065	94	0	-160	638	6.28	6.28	12.57	12.57	-6.19	-81.0
45	50	-8703	466	-512	0	2654	278	6.28	6.28	12.57	12.57	-16.91	266.3
46	50	-8453	520	-43	0	133	312	6.28	6.28	12.57	12.57	-4.59	-63.0
47	50	-8323	516	-36	0	111	310	6.28	6.28	12.57	12.57	-4.53	-62.2
49	50	-8471	412	-70	0	190	248	6.28	6.28	12.57	12.57	-4.27	-59.5
50	50	-8277	624	-6	0	46	374	6.28	6.28	12.57	12.57	-4.83	-65.5
51	50	-8334	504	-128	0	609	302	6.28	6.28	12.57	12.57	-5.40	-75.6

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 104 NI 1350 NF 1445 SEZ. Rp B= 0.400 H= 0.600 (pilastro)
PIL. NUM. 11
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-6124	1229	380	0	759	-4394	12.57	12.57	6.28	6.28	-28.92	937.0
41	0	-6493	600	354	0	682	-2356	12.57	12.57	6.28	6.28	-15.25	300.6
42	0	-6481	603	324	0	594	-2365	12.57	12.57	6.28	6.28	-15.31	303.8
43	0	-5875	1536	389	0	791	-5401	12.57	12.57	6.28	6.28	-35.44	1267.0
44	0	-7000	-430	306	0	546	986	12.57	12.57	6.28	6.28	-6.34	-85.9
45	0	-6469	494	297	0	515	-2020	12.57	12.57	6.28	6.28	-12.90	210.2
46	0	-6487	421	342	0	649	-1793	12.57	12.57	6.28	6.28	-11.31	152.0
47	0	-6486	376	338	0	641	-1652	12.57	12.57	6.28	6.28	-10.33	-130.0
49	0	-6363	585	347	0	667	-2331	12.57	12.57	6.28	6.28	-15.10	300.9
50	0	-6588	192	330	0	618	-1054	12.57	12.57	6.28	6.28	-6.58	-88.2
51	0	-6482	377	329	0	612	-1655	12.57	12.57	6.28	6.28	-10.35	-130.2

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	12	-6049	1229	380	0	712	-4240	12.57	12.57	6.28	6.28	-27.92	894.8
41	12	-6418	600	354	0	637	-2281	12.57	12.57	6.28	6.28	-14.74	283.8
42	12	-6406	603	324	0	554	-2290	12.57	12.57	6.28	6.28	-14.80	286.8
43	12	-5800	1536	389	0	742	-5209	12.57	12.57	6.28	6.28	-34.19	1212.5
44	12	-6925	-430	306	0	507	932	12.57	12.57	6.28	6.28	-6.08	-82.6
45	12	-6394	494	297	0	478	-1958	12.57	12.57	6.28	6.28	-12.49	197.8
46	12	-6412	421	342	0	606	-1740	12.57	12.57	6.28	6.28	-10.95	142.6
47	12	-6411	376	338	0	598	-1605	12.57	12.57	6.28	6.28	-10.01	-126.4
49	12	-6288	585	347	0	623	-2258	12.57	12.57	6.28	6.28	-14.60	284.5
50	12	-6513	192	330	0	576	-1030	12.57	12.57	6.28	6.28	-6.45	-86.5
51	12	-6407	377	329	0	570	-1608	12.57	12.57	6.28	6.28	-10.04	-126.6

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	25	-5974	1229	380	0	664	-4087	12.57	12.57	6.28	6.28	-26.91	852.5
41	25	-6343	600	354	0	593	-2206	12.57	12.57	6.28	6.28	-14.23	267.0
42	25	-6331	603	324	0	513	-2214	12.57	12.57	6.28	6.28	-14.29	269.9
43	25	-5725	1536	389	0	693	-5017	12.57	12.57	6.28	6.28	-32.95	1158.1
44	25	-6850	-430	306	0	469	878	12.57	12.57	6.28	6.28	-5.83	-79.4
45	25	-6319	494	297	0	441	-1897	12.57	12.57	6.28	6.28	-12.07	185.5
46	25	-6337	421	342	0	563	-1688	12.57	12.57	6.28	6.28	-10.60	133.3
47	25	-6336	376	338	0	556	-1558	12.57	12.57	6.28	6.28	-9.70	-122.8
49	25	-6213	585	347	0	580	-2185	12.57	12.57	6.28	6.28	-14.11	268.3
50	25	-6438	192	330	0	535	-1006	12.57	12.57	6.28	6.28	-6.31	-84.7
51	25	-6332	377	329	0	529	-1561	12.57	12.57	6.28	6.28	-9.72	-123.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	37	-5899	1229	380	0	617	-3934	12.57	12.57	6.28	6.28	-25.90	810.3
41	37	-6268	600	354	0	549	-2131	12.57	12.57	6.28	6.28	-13.72	250.4
42	37	-6256	603	324	0	472	-2138	12.57	12.57	6.28	6.28	-13.78	253.1
43	37	-5650	1536	389	0	645	-4825	12.57	12.57	6.28	6.28	-31.70	1103.6
44	37	-6775	-430	306	0	431	824	12.57	12.57	6.28	6.28	-5.59	-76.3
45	37	-6244	494	297	0	404	-1835	12.57	12.57	6.28	6.28	-11.65	173.3
46	37	-6262	421	342	0	521	-1635	12.57	12.57	6.28	6.28	-10.25	-128.4
47	37	-6261	376	338	0	514	-1511	12.57	12.57	6.28	6.28	-9.39	-119.3
49	37	-6138	585	347	0	536	-2112	12.57	12.57	6.28	6.28	-13.61	252.1
50	37	-6363	192	330	0	494	-982	12.57	12.57	6.28	6.28	-6.18	-83.0
51	37	-6257	377	329	0	488	-1514	12.57	12.57	6.28	6.28	-9.41	-119.5

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	50	-5824	1229	380	0	569	-3780	12.57	12.57	6.28	6.28	-24.89	768.2
41	50	-6193	600	354	0	504	-2056	12.57	12.57	6.28	6.28	-13.21	233.9
42	50	-6181	603	324	0	432	-2063	12.57	12.57	6.28	6.28	-13.26	236.4
43	50	-5575	1536	389	0	596	-4633	12.57	12.57	6.28	6.28	-30.45	1049.2
44	50	-6700	-430	306	0	393	770	12.57	12.57	6.28	6.28	-5.35	-73.4
45	50	-6169	494	297	0	367	-1773	12.57	12.57	6.28	6.28	-11.23	161.2
46	50	-6187	421	342	0	478	-1582	12.57	12.57	6.28	6.28	-9.89	-124.4
47	50	-6186	376	338	0	471	-1464	12.57	12.57	6.28	6.28	-9.08	-115.7
49	50	-6063	585	347	0	493	-2039	12.57	12.57	6.28	6.28	-13.12	236.1
50	50	-6288	192	330	0	452	-958	12.57	12.57	6.28	6.28	-6.04	-81.3
51	50	-6182	377	329	0	447	-1467	12.57	12.57	6.28	6.28	-9.10	-115.9

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

ASTA NUM. 105 NI 1445 NF 168 SEZ. Rp B= 0.400 H= 0.600 (pilastro)
PIL. NUM. 11A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-5824	1229	380	0	569	-3780	12.57	12.57	6.28	6.28	-24.89	768.2
41	0	-6193	600	354	0	504	-2056	12.57	12.57	6.28	6.28	-13.21	233.9
42	0	-6181	603	324	0	432	-2063	12.57	12.57	6.28	6.28	-13.26	236.4
43	0	-5575	1536	389	0	596	-4633	12.57	12.57	6.28	6.28	-30.45	1049.2
44	0	-6700	-430	306	0	393	770	12.57	12.57	6.28	6.28	-5.35	-73.4
45	0	-6169	494	297	0	367	-1773	12.57	12.57	6.28	6.28	-11.23	161.2
46	0	-6187	421	342	0	478	-1582	12.57	12.57	6.28	6.28	-9.89	-124.4
47	0	-6186	376	338	0	471	-1464	12.57	12.57	6.28	6.28	-9.08	-115.7
49	0	-6063	585	347	0	493	-2039	12.57	12.57	6.28	6.28	-13.12	236.1
50	0	-6288	192	330	0	452	-958	12.57	12.57	6.28	6.28	-6.04	-81.3
51	0	-6182	377	329	0	447	-1467	12.57	12.57	6.28	6.28	-9.10	-115.9

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	12	-5749	1229	380	0	522	-3626	12.57	12.57	6.28	6.28	-23.88	726.0
41	12	-6118	600	354	0	460	-1981	12.57	12.57	6.28	6.28	-12.70	217.6

42	12	-6106	603	324	0	391	-1988	12.57	12.57	6.28	6.28	-12.75	220.0
43	12	-5500	1536	389	0	547	-4441	12.57	12.57	6.28	6.28	-29.20	994.8
44	12	-6625	-430	306	0	355	717	12.57	12.57	6.28	6.28	-5.13	-70.5
45	12	-6094	494	297	0	330	-1711	12.57	12.57	6.28	6.28	-10.81	149.3
46	12	-6112	421	342	0	435	-1530	12.57	12.57	6.28	6.28	-9.54	-120.5
47	12	-6111	376	338	0	429	-1417	12.57	12.57	6.28	6.28	-8.78	-112.1
49	12	-5988	585	347	0	450	-1966	12.57	12.57	6.28	6.28	-12.62	220.2
50	12	-6213	192	330	0	411	-934	12.57	12.57	6.28	6.28	-5.91	-79.6
51	12	-6107	377	329	0	406	-1420	12.57	12.57	6.28	6.28	-8.79	-112.3

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	25	-5674	1229	380	0	474	-3472	12.57	12.57	6.28	6.28	-22.87	683.9
41	25	-6043	600	354	0	416	-1906	12.57	12.57	6.28	6.28	-12.19	201.4
42	25	-6031	603	324	0	351	-1912	12.57	12.57	6.28	6.28	-12.24	203.7
43	25	-5425	1536	389	0	499	-4249	12.57	12.57	6.28	6.28	-27.95	940.5
44	25	-6550	-430	306	0	316	663	12.57	12.57	6.28	6.28	-4.90	-67.6
45	25	-6019	494	297	0	293	-1650	12.57	12.57	6.28	6.28	-10.39	137.6
46	25	-6037	421	342	0	393	-1477	12.57	12.57	6.28	6.28	-9.19	-116.5
47	25	-6036	376	338	0	387	-1370	12.57	12.57	6.28	6.28	-8.47	-108.6
49	25	-5913	585	347	0	406	-1892	12.57	12.57	6.28	6.28	-12.12	204.4
50	25	-6138	192	330	0	370	-910	12.57	12.57	6.28	6.28	-5.78	-77.9
51	25	-6032	377	329	0	365	-1372	12.57	12.57	6.28	6.28	-8.49	-108.8

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	38	-5599	1229	380	0	427	-3319	12.57	12.57	6.28	6.28	-21.85	641.8
41	38	-5968	600	354	0	372	-1831	12.57	12.57	6.28	6.28	-11.68	185.5
42	38	-5956	603	324	0	310	-1837	12.57	12.57	6.28	6.28	-11.72	187.7
43	38	-5350	1536	389	0	450	-4057	12.57	12.57	6.28	6.28	-26.69	886.2
44	38	-6475	-430	306	0	278	609	12.57	12.57	6.28	6.28	-4.68	-64.8
45	38	-5944	494	297	0	256	-1588	12.57	12.57	6.28	6.28	-9.98	126.1
46	38	-5962	421	342	0	350	-1424	12.57	12.57	6.28	6.28	-8.85	-112.5
47	38	-5961	376	338	0	344	-1323	12.57	12.57	6.28	6.28	-8.16	-105.0
49	38	-5838	585	347	0	363	-1819	12.57	12.57	6.28	6.28	-11.62	188.8
50	38	-6063	192	330	0	328	-886	12.57	12.57	6.28	6.28	-5.64	-76.2
51	38	-5957	377	329	0	324	-1325	12.57	12.57	6.28	6.28	-8.18	-105.2

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	50	-5524	1229	380	0	379	-3165	12.57	12.57	6.28	6.28	-20.83	599.8
41	50	-5893	600	354	0	327	-1756	12.57	12.57	6.28	6.28	-11.16	169.7
42	50	-5881	603	324	0	270	-1762	12.57	12.57	6.28	6.28	-11.21	171.8
43	50	-5275	1536	389	0	402	-3865	12.57	12.57	6.28	6.28	-25.44	831.9
44	50	-6400	-430	306	0	240	555	12.57	12.57	6.28	6.28	-4.46	-61.9
45	50	-5869	494	297	0	218	-1526	12.57	12.57	6.28	6.28	-9.56	-119.9
46	50	-5887	421	342	0	307	-1372	12.57	12.57	6.28	6.28	-8.50	-108.5
47	50	-5886	376	338	0	302	-1276	12.57	12.57	6.28	6.28	-7.86	-101.5
49	50	-5763	585	347	0	320	-1746	12.57	12.57	6.28	6.28	-11.12	173.4
50	50	-5988	192	330	0	287	-862	12.57	12.57	6.28	6.28	-5.51	-74.5
51	50	-5882	377	329	0	283	-1278	12.57	12.57	6.28	6.28	-7.88	-101.6

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

ASTA NUM. 106 NI 1032 NF 1045 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 10
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	--												
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-15260	79	1565	0	1477	-723	6.28	6.28	12.57	12.57	-11.18	-154.5
41	0	-13500	750	1136	0	1208	-634	6.28	6.28	12.57	12.57	-9.54	-132.3
42	0	-13320	753	1254	0	1134	-635	6.28	6.28	12.57	12.57	-9.21	-127.9
43	0	-16090	-304	1792	0	1584	-801	6.28	6.28	12.57	12.57	-11.89	-164.1
44	0	-10610	1859	457	0	781	-486	6.28	6.28	12.57	12.57	-6.90	-96.4
45	0	-12850	819	1274	0	1013	-655	6.28	6.28	12.57	12.57	-8.59	-119.8
46	0	-12950	851	1042	0	1093	-666	6.28	6.28	12.57	12.57	-8.92	-124.0
47	0	-12810	877	1019	0	1064	-674	6.28	6.28	12.57	12.57	-8.76	-121.9
49	0	-13400	653	1162	0	1154	-703	6.28	6.28	12.57	12.57	-9.31	-129.3
50	0	-12300	1086	895	0	993	-640	6.28	6.28	12.57	12.57	-8.31	-115.7
51	0	-12750	878	1058	0	1039	-674	6.28	6.28	12.57	12.57	-8.65	-120.4

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	12	-15185	79	1565	0	1281	-713	6.28	6.28	12.57	12.57	-10.45	-145.3
41	12	-13425	750	1136	0	1066	-541	6.28	6.28	12.57	12.57	-9.00	-125.5
42	12	-13245	753	1254	0	977	-541	6.28	6.28	12.57	12.57	-8.62	-120.5
43	12	-16015	-304	1792	0	1360	-839	6.28	6.28	12.57	12.57	-11.06	-153.7
44	12	-10535	1859	457	0	724	-253	6.28	6.28	12.57	12.57	-6.66	-93.4
45	12	-12775	819	1274	0	854	-552	6.28	6.28	12.57	12.57	-7.99	-112.2
46	12	-12875	851	1042	0	963	-559	6.28	6.28	12.57	12.57	-8.42	-117.7
47	12	-12735	877	1019	0	937	-564	6.28	6.28	12.57	12.57	-8.27	-115.7
49	12	-13325	653	1162	0	1009	-621	6.28	6.28	12.57	12.57	-8.76	-122.4
50	12	-12225	1086	895	0	881	-504	6.28	6.28	12.57	12.57	-7.88	-110.3
51	12	-12675	878	1058	0	907	-564	6.28	6.28	12.57	12.57	-8.14	-114.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	25	-15110	79	1565	0	1086	-703	6.28	6.28	12.57	12.57	-9.72	-136.1
41	25	-13350	750	1136	0	924	-447	6.28	6.28	12.57	12.57	-8.47	-118.7
42	25	-13170	753	1254	0	820	-446	6.28	6.28	12.57	12.57	-8.03	-113.0
43	25	-15940	-304	1792	0	1136	-877	6.28	6.28	12.57	12.57	-10.23	-143.2
44	25	-10460	1859	457	0	667	-21	6.28	6.28	12.57	12.57	-6.43	-90.5
45	25	-12700	819	1274	0	694	-450	6.28	6.28	12.57	12.57	-7.39	-104.7
46	25	-12800	851	1042	0	832	-453	6.28	6.28	12.57	12.57	-7.93	-111.4
47	25	-12660	877	1019	0	809	-454	6.28	6.28	12.57	12.57	-7.79	-109.6
49	25	-13250	653	1162	0	863	-540	6.28	6.28	12.57	12.57	-8.21	-115.4
50	25	-12150	1086	895	0	769	-369	6.28	6.28	12.57	12.57	-7.45	-104.8
51	25	-12600	878	1058	0	775	-454	6.28	6.28	12.57	12.57	-7.64	-107.7

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	38	-15035	79	1565	0	890	-693	6.28	6.28	12.57	12.57	-8.99	-127.0
41	38	-13275	750	1136	0	782	-353	6.28	6.28	12.57	12.57	-7.93	-111.9
42	38	-13095	753	1254	0	664	-352	6.28	6.28	12.57	12.57	-7.43	-105.6

43	38	-15865	-304	1792	0	912	-915	6.28	6.28	12.57	12.57	-10.23	-136.6
44	38	-10385	1859	457	0	610	211	6.28	6.28	12.57	12.57	-6.19	-87.5
45	38	-12625	819	1274	0	535	-348	6.28	6.28	12.57	12.57	-6.79	-97.1
46	38	-12725	851	1042	0	702	-347	6.28	6.28	12.57	12.57	-7.43	-105.2
47	38	-12585	877	1019	0	682	-345	6.28	6.28	12.57	12.57	-7.30	-103.5
49	38	-13175	653	1162	0	718	-458	6.28	6.28	12.57	12.57	-7.66	-108.5
50	38	-12075	1086	895	0	658	-233	6.28	6.28	12.57	12.57	-7.02	-99.4
51	38	-12525	878	1058	0	643	-345	6.28	6.28	12.57	12.57	-7.14	-101.3

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	50	-14960	79	1565	0	694	-683	6.28	6.28	12.57	12.57	-8.76	-118.8
41	50	-13200	750	1136	0	640	-260	6.28	6.28	12.57	12.57	-7.39	-105.1
42	50	-13020	753	1254	0	507	-258	6.28	6.28	12.57	12.57	-6.84	-98.1
43	50	-15790	-304	1792	0	688	-953	6.28	6.28	12.57	12.57	-10.39	-138.3
44	50	-10310	1859	457	0	552	444	6.28	6.28	12.57	12.57	-5.96	-84.5
45	50	-12550	819	1274	0	376	-245	6.28	6.28	12.57	12.57	-6.19	-89.5
46	50	-12650	851	1042	0	572	-240	6.28	6.28	12.57	12.57	-6.93	-98.9
47	50	-12510	877	1019	0	555	-235	6.28	6.28	12.57	12.57	-6.82	-97.3
49	50	-13100	653	1162	0	573	-376	6.28	6.28	12.57	12.57	-7.11	-101.6
50	50	-12000	1086	895	0	546	-97	6.28	6.28	12.57	12.57	-6.59	-94.0
51	50	-12450	878	1058	0	510	-235	6.28	6.28	12.57	12.57	-6.64	-95.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 107 NI 1045 NF 299 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 10A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-16190	-1578	674	0	562	-706	6.28	6.28	12.57	12.57	-9.32	-126.7
41	0	-14910	304	505	0	530	-216	6.28	6.28	12.57	12.57	-7.66	-110.1
42	0	-14800	298	739	0	383	-216	6.28	6.28	12.57	12.57	-7.09	-102.9
43	0	-16630	-2815	796	0	546	-1015	6.28	6.28	12.57	12.57	-11.00	-146.2
44	0	-12830	3434	236	0	477	596	6.28	6.28	12.57	12.57	-7.56	-102.4
45	0	-14320	313	904	0	249	-199	6.28	6.28	12.57	12.57	-6.42	-94.1
46	0	-14260	333	519	0	472	-189	6.28	6.28	12.57	12.57	-7.20	-103.7
47	0	-14100	341	523	0	457	-182	6.28	6.28	12.57	12.57	-7.08	-102.2
49	0	-14530	-287	579	0	468	-345	6.28	6.28	12.57	12.57	-7.29	-105.1
50	0	-13770	963	467	0	454	-23	6.28	6.28	12.57	12.57	-6.94	-100.1
51	0	-14060	339	601	0	408	-182	6.28	6.28	12.57	12.57	-6.89	-99.7

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	12	-16115	-1578	674	0	477	-903	6.28	6.28	12.57	12.57	-10.27	-137.2
41	12	-14835	304	505	0	467	-178	6.28	6.28	12.57	12.57	-7.40	-106.9
42	12	-14725	298	739	0	291	-179	6.28	6.28	12.57	12.57	-6.73	-98.4
43	12	-16555	-2815	796	0	447	-1367	6.28	6.28	12.57	12.57	-12.75	-165.7
44	12	-12755	3434	236	0	448	1025	6.28	6.28	12.57	12.57	-9.68	-126.0
45	12	-14245	313	904	0	136	-159	6.28	6.28	12.57	12.57	-5.99	-88.6
46	12	-14185	333	519	0	407	-147	6.28	6.28	12.57	12.57	-6.94	-100.4
47	12	-14025	341	523	0	392	-139	6.28	6.28	12.57	12.57	-6.82	-98.8
49	12	-14455	-287	579	0	395	-381	6.28	6.28	12.57	12.57	-7.09	-101.5
50	12	-13695	963	467	0	395	98	6.28	6.28	12.57	12.57	-6.71	-97.1
51	12	-13985	339	601	0	333	-139	6.28	6.28	12.57	12.57	-6.60	-95.9

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	25	-16040	-1578	674	0	393	-1100	6.28	6.28	12.57	12.57	-11.21	-147.8
41	25	-14760	304	505	0	404	-140	6.28	6.28	12.57	12.57	-7.15	-103.6
42	25	-14650	298	739	0	199	-142	6.28	6.28	12.57	12.57	-6.37	-93.8
43	25	-16480	-2815	796	0	347	-1718	6.28	6.28	12.57	12.57	-14.84	-188.1
44	25	-12680	3434	236	0	418	1454	6.28	6.28	12.57	12.57	-12.31	-154.0
45	25	-14170	313	904	0	23	-120	6.28	6.28	12.57	12.57	-5.70	-83.2
46	25	-14110	333	519	0	342	-105	6.28	6.28	12.57	12.57	-6.67	-97.1
47	25	-13950	341	523	0	326	-96	6.28	6.28	12.57	12.57	-6.56	-95.4
49	25	-14380	-287	579	0	323	-416	6.28	6.28	12.57	12.57	-7.24	-100.8
50	25	-13620	963	467	0	337	218	6.28	6.28	12.57	12.57	-6.47	-94.0
51	25	-13910	339	601	0	258	-97	6.28	6.28	12.57	12.57	-6.30	-92.2

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	38	-15965	-1578	674	0	309	-1298	6.28	6.28	12.57	12.57	-12.19	-158.6
41	38	-14685	304	505	0	340	-102	6.28	6.28	12.57	12.57	-6.89	-100.3
42	38	-14575	298	739	0	106	-104	6.28	6.28	12.57	12.57	-6.01	-89.2
43	38	-16405	-2815	796	0	248	-2070	6.28	6.28	12.57	12.57	-17.27	-212.9
44	38	-12605	3434	236	0	389	1884	6.28	6.28	12.57	12.57	-15.50	-185.5
45	38	-14095	313	904	0	-90	-81	6.28	6.28	12.57	12.57	-5.77	-85.7
46	38	-14035	333	519	0	277	-64	6.28	6.28	12.57	12.57	-6.41	-93.7
47	38	-13875	341	523	0	261	-54	6.28	6.28	12.57	12.57	-6.29	-92.1
49	38	-14305	-287	579	0	250	-452	6.28	6.28	12.57	12.57	-7.39	-102.4
50	38	-13545	963	467	0	279	338	6.28	6.28	12.57	12.57	-6.55	-92.0
51	38	-13835	339	601	0	183	-54	6.28	6.28	12.57	12.57	-6.00	-88.4

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	50	-15890	-1578	674	0	224	-1495	6.28	6.28	12.57	12.57	-13.29	-170.5
41	50	-14610	304	505	0	277	-64	6.28	6.28	12.57	12.57	-6.64	-97.1
42	50	-14500	298	739	0	14	-67	6.28	6.28	12.57	12.57	-5.65	-84.6
43	50	-16330	-2815	796	0	148	-2422	6.28	6.28	12.57	12.57	-19.94	-238.9
44	50	-12530	3434	236	0	360	2313	6.28	6.28	12.57	12.57	-18.92	-217.2
45	50	-14020	313	904	0	-203	-42	6.28	6.28	12.57	12.57	-6.14	-90.3
46	50	-13960	333	519	0	212	-22	6.28	6.28	12.57	12.57	-6.15	-90.4
47	50	-13800	341	523	0	196	-11	6.28	6.28	12.57	12.57	-6.03	-88.7
49	50	-14230	-287	579	0	178	-488	6.28	6.28	12.57	12.57	-7.54	-104.0
50	50	-13470	963	467	0	220	459	6.28	6.28	12.57	12.57	-7.12	-98.3
51	50	-13760	339	601	0	108	-12	6.28	6.28	12.57	12.57	-5.70	-84.6

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 108 NI 1254 NF 1349 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 9
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-4183	-114	176	0	-60	-168	6.28	6.28	12.57	12.57	-2.34	-31.9
41	0	-4166	1	67	0	-40	9	6.28	6.28	12.57	12.57	-1.75	-25.9
42	0	-4150	1	177	0	-56	10	6.28	6.28	12.57	12.57	-1.80	-26.6
43	0	-4075	-196	218	0	-69	-295	6.28	6.28	12.57	12.57	-2.93	-38.4
44	0	-4043	192	-101	0	-8	305	6.28	6.28	12.57	12.57	-2.96	-38.8
45	0	-4020	-3	219	0	-61	2	6.28	6.28	12.57	12.57	-1.77	-26.0
46	0	-3975	-8	15	0	-31	-6	6.28	6.28	12.57	12.57	-1.65	-24.4
47	0	-3927	-10	3	0	-29	-10	6.28	6.28	12.57	12.57	-1.62	-24.0
49	0	-3933	-48	39	0	-36	-69	6.28	6.28	12.57	12.57	-1.75	-25.1
50	0	-3926	29	-25	0	-24	51	6.28	6.28	12.57	12.57	-1.67	-24.1
51	0	-3922	-10	39	0	-34	-9	6.28	6.28	12.57	12.57	-1.64	-24.3

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	12	-4108	-114	176	0	-83	-182	6.28	6.28	12.57	12.57	-2.38	-32.3
41	12	-4091	1	67	0	-48	9	6.28	6.28	12.57	12.57	-1.75	-25.9
42	12	-4075	1	177	0	-78	10	6.28	6.28	12.57	12.57	-1.85	-27.1
43	12	-4000	-196	218	0	-96	-320	6.28	6.28	12.57	12.57	-3.02	-39.4
44	12	-3968	192	-101	0	5	329	6.28	6.28	12.57	12.57	-3.06	-39.8
45	12	-3945	-3	219	0	-89	2	6.28	6.28	12.57	12.57	-1.84	-26.8
46	12	-3900	-8	15	0	-33	-7	6.28	6.28	12.57	12.57	-1.62	-24.1
47	12	-3852	-10	3	0	-29	-11	6.28	6.28	12.57	12.57	-1.59	-23.6
49	12	-3858	-48	39	0	-41	-75	6.28	6.28	12.57	12.57	-1.76	-25.0
50	12	-3851	29	-25	0	-20	55	6.28	6.28	12.57	12.57	-1.66	-23.9
51	12	-3847	-10	39	0	-39	-10	6.28	6.28	12.57	12.57	-1.63	-24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	25	-4033	-114	176	0	-105	-197	6.28	6.28	12.57	12.57	-2.42	-32.7
41	25	-4016	1	67	0	-57	9	6.28	6.28	12.57	12.57	-1.75	-25.8
42	25	-4000	1	177	0	-100	11	6.28	6.28	12.57	12.57	-1.91	-27.7
43	25	-3925	-196	218	0	-123	-344	6.28	6.28	12.57	12.57	-3.13	-40.5
44	25	-3893	192	-101	0	17	353	6.28	6.28	12.57	12.57	-3.18	-40.9
45	25	-3870	-3	219	0	-116	1	6.28	6.28	12.57	12.57	-1.91	-27.6
46	25	-3825	-8	15	0	-35	-8	6.28	6.28	12.57	12.57	-1.60	-23.7
47	25	-3777	-10	3	0	-29	-12	6.28	6.28	12.57	12.57	-1.56	-23.2
49	25	-3783	-48	39	0	-45	-81	6.28	6.28	12.57	12.57	-1.76	-24.9
50	25	-3776	29	-25	0	-17	59	6.28	6.28	12.57	12.57	-1.65	-23.7
51	25	-3772	-10	39	0	-44	-12	6.28	6.28	12.57	12.57	-1.61	-23.8

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	38	-3958	-114	176	0	-127	-211	6.28	6.28	12.57	12.57	-2.47	-33.1
41	38	-3941	1	67	0	-65	9	6.28	6.28	12.57	12.57	-1.76	-25.7
42	38	-3925	1	177	0	-123	11	6.28	6.28	12.57	12.57	-1.96	-28.2
43	38	-3850	-196	218	0	-150	-368	6.28	6.28	12.57	12.57	-3.26	-41.7
44	38	-3818	192	-101	0	30	377	6.28	6.28	12.57	12.57	-3.30	-42.1
45	38	-3795	-3	219	0	-143	1	6.28	6.28	12.57	12.57	-1.98	-28.4
46	38	-3750	-8	15	0	-37	-9	6.28	6.28	12.57	12.57	-1.58	-23.4
47	38	-3702	-10	3	0	-30	-13	6.28	6.28	12.57	12.57	-1.54	-22.8
49	38	-3708	-48	39	0	-50	-87	6.28	6.28	12.57	12.57	-1.76	-24.8
50	38	-3701	29	-25	0	-14	62	6.28	6.28	12.57	12.57	-1.64	-23.5
51	38	-3697	-10	39	0	-49	-13	6.28	6.28	12.57	12.57	-1.60	-23.6

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	50	-3883	-114	176	0	-149	-225	6.28	6.28	12.57	12.57	-2.51	-33.5
41	50	-3866	1	67	0	-73	9	6.28	6.28	12.57	12.57	-1.76	-25.7
42	50	-3850	1	177	0	-145	11	6.28	6.28	12.57	12.57	-2.01	-28.8
43	50	-3775	-196	218	0	-177	-393	6.28	6.28	12.57	12.57	-3.39	-43.0
44	50	-3743	192	-101	0	42	401	6.28	6.28	12.57	12.57	-3.44	-43.4
45	50	-3720	-3	219	0	-171	1	6.28	6.28	12.57	12.57	-2.05	-29.2
46	50	-3675	-8	15	0	-39	-10	6.28	6.28	12.57	12.57	-1.56	-23.0
47	50	-3627	-10	3	0	-30	-15	6.28	6.28	12.57	12.57	-1.51	-22.4
49	50	-3633	-48	39	0	-55	-93	6.28	6.28	12.57	12.57	-1.77	-24.8
50	50	-3626	29	-25	0	-11	66	6.28	6.28	12.57	12.57	-1.63	-23.3
51	50	-3622	-10	39	0	-54	-14	6.28	6.28	12.57	12.57	-1.59	-23.4

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 109 NI 1349 NF 129 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 9A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-5952	-297	577	0	-149	-214	6.28	6.28	12.57	12.57	-3.20	-44.0
41	0	-5928	5	304	0	-73	7	6.28	6.28	12.57	12.57	-2.55	-37.6
42	0	-5900	8	563	0	-145	9	6.28	6.28	12.57	12.57	-2.80	-40.7
43	0	-5783	-512	683	0	-177	-372	6.28	6.28	12.57	12.57	-3.92	-51.9
44	0	-5737	511	-116	0	42	377	6.28	6.28	12.57	12.57	-3.93	-51.9
45	0	-5695	-5	659	0	-171	-1	6.28	6.28	12.57	12.57	-2.81	-40.6
46	0	-5631	-18	182	0	-39	-11	6.28	6.28	12.57	12.57	-2.31	-34.4
47	0	-5557	-24	152	0	-30	-15	6.28	6.28	12.57	12.57	-2.25	-33.5
49	0	-5565	-124	242	0	-55	-89	6.28	6.28	12.57	12.57	-2.44	-35.0
50	0	-5556	80	83	0	-11	61	6.28	6.28	12.57	12.57	-2.30	-33.4
51	0	-5547	-23	238	0	-54	-15	6.28	6.28	12.57	12.57	-2.34	-34.6

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	12	-5877	-297	577	0	-221	-251	6.28	6.28	12.57	12.57	-3.36	-45.7
41	12	-5853	5	304	0	-111	8	6.28	6.28	12.57	12.57	-2.66	-38.9
42	12	-5825	8	563	0	-215	10	6.28	6.28	12.57	12.57	-3.02	-43.4
43	12	-5708	-512	683	0	-263	-436	6.28	6.28	12.57	12.57	-4.21	-55.1
44	12	-5662	511	-116	0	57	441	6.28	6.28	12.57	12.57	-4.22	-55.1
45	12	-5620	-5	659	0	-253	-2	6.28	6.28	12.57	12.57	-3.08	-43.9
46	12	-5556	-18	182	0	-61	-13	6.28	6.28	12.57	12.57	-2.37	-34.9
47	12	-5482	-24	152	0	-49	-18	6.28	6.28	12.57	12.57	-2.29	-34.0

49	12	-5490	-124	242	0	-85	-104	6.28	6.28	12.57	12.57	-2.49	-35.6
50	12	-5481	80	83	0	-22	71	6.28	6.28	12.57	12.57	-2.33	-33.6
51	12	-5472	-23	238	0	-84	-17	6.28	6.28	12.57	12.57	-2.41	-35.5

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	25	-5802	-297	577	0	-293	-288	6.28	6.28	12.57	12.57	-3.51	-47.4
41	25	-5778	5	304	0	-149	8	6.28	6.28	12.57	12.57	-2.77	-40.2
42	25	-5750	8	563	0	-286	11	6.28	6.28	12.57	12.57	-3.24	-46.1
43	25	-5633	-512	683	0	-348	-500	6.28	6.28	12.57	12.57	-4.54	-58.6
44	25	-5587	511	-116	0	72	505	6.28	6.28	12.57	12.57	-4.55	-58.6
45	25	-5545	-5	659	0	-336	-2	6.28	6.28	12.57	12.57	-3.34	-47.1
46	25	-5481	-18	182	0	-84	-15	6.28	6.28	12.57	12.57	-2.42	-35.5
47	25	-5407	-24	152	0	-68	-21	6.28	6.28	12.57	12.57	-2.33	-34.4
49	25	-5415	-124	242	0	-116	-120	6.28	6.28	12.57	12.57	-2.54	-36.6
50	25	-5406	80	83	0	-32	81	6.28	6.28	12.57	12.57	-2.35	-33.7
51	25	-5397	-23	238	0	-113	-20	6.28	6.28	12.57	12.57	-2.49	-36.3

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	38	-5727	-297	577	0	-365	-325	6.28	6.28	12.57	12.57	-3.67	-49.5
41	38	-5703	5	304	0	-188	9	6.28	6.28	12.57	12.57	-2.87	-41.4
42	38	-5675	8	563	0	-356	12	6.28	6.28	12.57	12.57	-3.47	-48.8
43	38	-5558	-512	683	0	-433	-564	6.28	6.28	12.57	12.57	-4.91	-62.4
44	38	-5512	511	-116	0	86	568	6.28	6.28	12.57	12.57	-4.92	-62.5
45	38	-5470	-5	659	0	-418	-3	6.28	6.28	12.57	12.57	-3.61	-50.4
46	38	-5406	-18	182	0	-107	-17	6.28	6.28	12.57	12.57	-2.47	-36.1
47	38	-5332	-24	152	0	-87	-24	6.28	6.28	12.57	12.57	-2.37	-34.8
49	38	-5340	-124	242	0	-146	-135	6.28	6.28	12.57	12.57	-2.59	-37.5
50	38	-5331	80	83	0	-42	91	6.28	6.28	12.57	12.57	-2.37	-33.9
51	38	-5322	-23	238	0	-143	-23	6.28	6.28	12.57	12.57	-2.57	-37.2

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	50	-5652	-297	577	0	-437	-362	6.28	6.28	12.57	12.57	-3.83	-52.3
41	50	-5628	5	304	0	-226	9	6.28	6.28	12.57	12.57	-2.98	-42.7
42	50	-5600	8	563	0	-426	13	6.28	6.28	12.57	12.57	-3.69	-51.5
43	50	-5483	-512	683	0	-519	-628	6.28	6.28	12.57	12.57	-5.32	-66.5
44	50	-5437	511	-116	0	101	632	6.28	6.28	12.57	12.57	-5.34	-66.6
45	50	-5395	-5	659	0	-500	-3	6.28	6.28	12.57	12.57	-3.88	-53.7
46	50	-5331	-18	182	0	-130	-20	6.28	6.28	12.57	12.57	-2.52	-36.7
47	50	-5257	-24	152	0	-106	-27	6.28	6.28	12.57	12.57	-2.41	-35.2
49	50	-5265	-124	242	0	-176	-151	6.28	6.28	12.57	12.57	-2.67	-38.4
50	50	-5256	80	83	0	-53	101	6.28	6.28	12.57	12.57	-2.39	-34.0
51	50	-5247	-23	238	0	-173	-26	6.28	6.28	12.57	12.57	-2.65	-38.1

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 110 NI 1158 NF 1253 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 8
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm²				daN/cm²	
40	0	-2926	67	426	0	-148	5	6.28	6.28	9.42	9.42	-2.15	-30.5
41	0	-2931	125	337	0	-141	-12	6.28	6.28	9.42	9.42	-2.12	-30.2
42	0	-3009	123	409	0	-155	-11	6.28	6.28	9.42	9.42	-2.22	-31.5
43	0	-2845	23	462	0	-142	17	6.28	6.28	9.42	9.42	-2.08	-29.6
44	0	-2890	220	187	0	-127	-39	6.28	6.28	9.42	9.42	-2.03	-29.0
45	0	-2984	116	433	0	-155	-9	6.28	6.28	9.42	9.42	-2.21	-31.3
46	0	-2808	116	300	0	-126	-10	6.28	6.28	9.42	9.42	-1.99	-28.4
47	0	-2777	114	290	0	-122	-9	6.28	6.28	9.42	9.42	-1.95	-27.9
49	0	-2775	95	320	0	-124	-4	6.28	6.28	9.42	9.42	-1.96	-28.0
50	0	-2784	134	265	0	-121	-15	6.28	6.28	9.42	9.42	-1.95	-27.9
51	0	-2803	113	314	0	-127	-9	6.28	6.28	9.42	9.42	-1.99	-28.4

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	12	-2870	67	426	0	-201	13	6.28	6.28	9.42	9.42	-2.36	-33.1
41	12	-2875	125	337	0	-184	4	6.28	6.28	9.42	9.42	-2.28	-32.2
42	12	-2953	123	409	0	-206	5	6.28	6.28	9.42	9.42	-2.43	-34.0
43	12	-2789	23	462	0	-200	20	6.28	6.28	9.42	9.42	-2.32	-32.5
44	12	-2834	220	187	0	-150	-11	6.28	6.28	9.42	9.42	-2.11	-29.9
45	12	-2928	116	433	0	-209	6	6.28	6.28	9.42	9.42	-2.42	-34.0
46	12	-2752	116	300	0	-163	5	6.28	6.28	9.42	9.42	-2.13	-30.1
47	12	-2721	114	290	0	-158	5	6.28	6.28	9.42	9.42	-2.09	-29.6
49	12	-2719	95	320	0	-164	8	6.28	6.28	9.42	9.42	-2.12	-29.9
50	12	-2728	134	265	0	-154	2	6.28	6.28	9.42	9.42	-2.08	-29.4
51	12	-2747	113	314	0	-166	5	6.28	6.28	9.42	9.42	-2.14	-30.2

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	25	-2814	67	426	0	-254	22	6.28	6.28	9.42	9.42	-2.58	-35.7
41	25	-2818	125	337	0	-226	20	6.28	6.28	9.42	9.42	-2.45	-34.1
42	25	-2896	123	409	0	-257	20	6.28	6.28	9.42	9.42	-2.63	-36.5
43	25	-2732	23	462	0	-258	23	6.28	6.28	9.42	9.42	-2.55	-35.3
44	25	-2778	220	187	0	-173	16	6.28	6.28	9.42	9.42	-2.19	-30.8
45	25	-2872	116	433	0	-263	20	6.28	6.28	9.42	9.42	-2.64	-36.7
46	25	-2696	116	300	0	-201	19	6.28	6.28	9.42	9.42	-2.27	-31.8
47	25	-2664	114	290	0	-195	19	6.28	6.28	9.42	9.42	-2.23	-31.2
49	25	-2662	95	320	0	-204	20	6.28	6.28	9.42	9.42	-2.27	-31.7
50	25	-2672	134	265	0	-187	19	6.28	6.28	9.42	9.42	-2.20	-30.8
51	25	-2690	113	314	0	-205	19	6.28	6.28	9.42	9.42	-2.29	-32.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	38	-2757	67	426	0	-308	30	6.28	6.28	9.42	9.42	-2.79	-38.3
41	38	-2762	125	337	0	-268	35	6.28	6.28	9.42	9.42	-2.61	-36.1
42	38	-2840	123	409	0	-308	36	6.28	6.28	9.42	9.42	-2.84	-39.0
43	38	-2676	23	462	0	-316	25	6.28	6.28	9.42	9.42	-2.79	-38.2
44	38	-2721	220	187	0	-197	44	6.28	6.28	9.42	9.42	-2.27	-31.7
45	38	-2815	116	433	0	-317	35	6.28	6.28	9.42	9.42	-2.86	-39.3
46	38	-2639	116	300	0	-238	34	6.28	6.28	9.42	9.42	-2.41	-33.5
47	38	-2608	114	290	0	-231	34	6.28	6.28	9.42	9.42	-2.37	-32.8
49	38	-2606	95	320	0	-244	32	6.28	6.28	9.42	9.42	-2.42	-33.6

50	38	-2615	134	265	0	-220	35	6.28	6.28	9.42	9.42	-2.32	-32.3
51	38	-2634	113	314	0	-245	34	6.28	6.28	9.42	9.42	-2.44	-33.8

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	50	-2701	67	426	0	-361	38	6.28	6.28	9.42	9.42	-3.03	-41.2
41	50	-2706	125	337	0	-310	51	6.28	6.28	9.42	9.42	-2.78	-38.1
42	50	-2784	123	409	0	-360	51	6.28	6.28	9.42	9.42	-3.06	-41.7
43	50	-2620	23	462	0	-373	28	6.28	6.28	9.42	9.42	-3.07	-41.5
44	50	-2665	220	187	0	-220	71	6.28	6.28	9.42	9.42	-2.34	-32.6
45	50	-2759	116	433	0	-371	49	6.28	6.28	9.42	9.42	-3.11	-42.3
46	50	-2583	116	300	0	-276	48	6.28	6.28	9.42	9.42	-2.56	-35.2
47	50	-2552	114	290	0	-267	48	6.28	6.28	9.42	9.42	-2.50	-34.5
49	50	-2550	95	320	0	-284	44	6.28	6.28	9.42	9.42	-2.58	-35.4
50	50	-2559	134	265	0	-254	52	6.28	6.28	9.42	9.42	-2.44	-33.8
51	50	-2578	113	314	0	-284	48	6.28	6.28	9.42	9.42	-2.59	-35.6

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 111 NI 1253 NF 213 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 8A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-3689	-161	514	0	-395	28	6.28	6.28	9.42	9.42	-3.66	-50.4
41	0	-3714	-23	383	0	-338	47	6.28	6.28	9.42	9.42	-3.41	-47.3
42	0	-3786	-29	504	0	-398	47	6.28	6.28	9.42	9.42	-3.72	-51.2
43	0	-3578	-254	558	0	-409	13	6.28	6.28	9.42	9.42	-3.67	-50.3
44	0	-3687	209	162	0	-237	78	6.28	6.28	9.42	9.42	-2.94	-41.3
45	0	-3740	-35	542	0	-413	45	6.28	6.28	9.42	9.42	-3.77	-51.8
46	0	-3564	-26	314	0	-299	44	6.28	6.28	9.42	9.42	-3.16	-43.9
47	0	-3527	-27	297	0	-289	43	6.28	6.28	9.42	9.42	-3.09	-43.1
49	0	-3518	-73	341	0	-308	37	6.28	6.28	9.42	9.42	-3.17	-44.1
50	0	-3540	20	261	0	-274	50	6.28	6.28	9.42	9.42	-3.03	-42.3
51	0	-3551	-29	338	0	-309	43	6.28	6.28	9.42	9.42	-3.19	-44.4

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	12	-3633	-161	514	0	-460	8	6.28	6.28	9.42	9.42	-3.94	-53.8
41	12	-3658	-23	383	0	-386	44	6.28	6.28	9.42	9.42	-3.60	-49.6
42	12	-3730	-29	504	0	-461	43	6.28	6.28	9.42	9.42	-3.99	-54.5
43	12	-3522	-254	558	0	-479	-19	6.28	6.28	9.42	9.42	-3.99	-54.3
44	12	-3631	209	162	0	-257	104	6.28	6.28	9.42	9.42	-3.00	-42.1
45	12	-3684	-35	542	0	-481	41	6.28	6.28	9.42	9.42	-4.07	-55.5
46	12	-3508	-26	314	0	-338	40	6.28	6.28	9.42	9.42	-3.31	-45.7
47	12	-3471	-27	297	0	-326	40	6.28	6.28	9.42	9.42	-3.23	-44.8
49	12	-3462	-73	341	0	-351	27	6.28	6.28	9.42	9.42	-3.34	-46.1
50	12	-3484	20	261	0	-306	52	6.28	6.28	9.42	9.42	-3.15	-43.7
51	12	-3495	-29	338	0	-351	39	6.28	6.28	9.42	9.42	-3.36	-46.4

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	25	-3576	-161	514	0	-524	-12	6.28	6.28	9.42	9.42	-4.27	-57.7
41	25	-3602	-23	383	0	-434	41	6.28	6.28	9.42	9.42	-3.79	-52.0
42	25	-3674	-29	504	0	-524	40	6.28	6.28	9.42	9.42	-4.30	-58.3
43	25	-3466	-254	558	0	-549	-50	6.28	6.28	9.42	9.42	-4.38	-58.9
44	25	-3574	209	162	0	-278	130	6.28	6.28	9.42	9.42	-3.06	-42.8
45	25	-3628	-35	542	0	-549	37	6.28	6.28	9.42	9.42	-4.43	-59.8
46	25	-3452	-26	314	0	-377	37	6.28	6.28	9.42	9.42	-3.46	-47.5
47	25	-3414	-27	297	0	-363	36	6.28	6.28	9.42	9.42	-3.37	-46.5
49	25	-3406	-73	341	0	-393	18	6.28	6.28	9.42	9.42	-3.51	-48.1
50	25	-3428	20	261	0	-339	54	6.28	6.28	9.42	9.42	-3.27	-45.2
51	25	-3438	-29	338	0	-393	36	6.28	6.28	9.42	9.42	-3.52	-48.4

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	38	-3520	-161	514	0	-588	-32	6.28	6.28	9.42	9.42	-4.64	-62.1
41	38	-3545	-23	383	0	-482	38	6.28	6.28	9.42	9.42	-4.02	-54.6
42	38	-3617	-29	504	0	-587	36	6.28	6.28	9.42	9.42	-4.66	-62.5
43	38	-3409	-254	558	0	-619	-82	6.28	6.28	9.42	9.42	-4.82	-64.0
44	38	-3518	209	162	0	-298	156	6.28	6.28	9.42	9.42	-3.13	-43.5
45	38	-3571	-35	542	0	-617	32	6.28	6.28	9.42	9.42	-4.84	-64.5
46	38	-3395	-26	314	0	-417	34	6.28	6.28	9.42	9.42	-3.62	-49.5
47	38	-3358	-27	297	0	-400	33	6.28	6.28	9.42	9.42	-3.52	-48.2
49	38	-3349	-73	341	0	-436	9	6.28	6.28	9.42	9.42	-3.69	-50.4
50	38	-3371	20	261	0	-372	57	6.28	6.28	9.42	9.42	-3.39	-46.6
51	38	-3382	-29	338	0	-436	32	6.28	6.28	9.42	9.42	-3.71	-50.6

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	50	-3464	-161	514	0	-652	-53	6.28	6.28	9.42	9.42	-5.06	-66.9
41	50	-3489	-23	383	0	-529	35	6.28	6.28	9.42	9.42	-4.27	-57.6
42	50	-3561	-29	504	0	-650	33	6.28	6.28	9.42	9.42	-5.06	-67.1
43	50	-3353	-254	558	0	-688	-114	6.28	6.28	9.42	9.42	-5.31	-69.5
44	50	-3462	209	162	0	-318	182	6.28	6.28	9.42	9.42	-3.34	-44.2
45	50	-3515	-35	542	0	-685	28	6.28	6.28	9.42	9.42	-5.30	-69.8
46	50	-3339	-26	314	0	-456	30	6.28	6.28	9.42	9.42	-3.80	-51.6
47	50	-3302	-27	297	0	-438	29	6.28	6.28	9.42	9.42	-3.68	-50.1
49	50	-3293	-73	341	0	-478	0	6.28	6.28	9.42	9.42	-3.91	-52.8
50	50	-3315	20	261	0	-404	59	6.28	6.28	9.42	9.42	-3.52	-48.1
51	50	-3326	-29	338	0	-478	29	6.28	6.28	9.42	9.42	-3.91	-53.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 112 NI 175 NF 89 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 17
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	

40	0	-6704	-76	-181	0	592	-1	6.28	6.28	12.57	12.57	-4.71	-65.4
41	0	-6463	14	-150	0	502	-7	6.28	6.28	12.57	12.57	-4.30	-59.9
42	0	-6504	18	-401	0	2239	-7	6.28	6.28	12.57	12.57	-14.43	267.5
43	0	-6587	-132	-165	0	533	4	6.28	6.28	12.57	12.57	-4.45	-62.0
44	0	-6139	164	-106	0	376	-18	6.28	6.28	12.57	12.57	-3.72	-52.4
45	0	-6252	24	-531	0	3278	-8	6.28	6.28	12.57	12.57	-21.55	586.5
46	0	-6016	21	-92	0	312	-7	6.28	6.28	12.57	12.57	-3.44	-48.8
47	0	-5905	22	-77	0	264	-7	6.28	6.28	12.57	12.57	-3.23	-46.0
49	0	-5985	-8	-88	0	294	-5	6.28	6.28	12.57	12.57	-3.37	-47.8
50	0	-5896	51	-76	0	263	-9	6.28	6.28	12.57	12.57	-3.22	-45.9
51	0	-5918	23	-161	0	843	-7	6.28	6.28	12.57	12.57	-5.41	-73.1

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	12	-6629	-76	-181	0	615	-10	6.28	6.28	12.57	12.57	-4.76	-65.9
41	12	-6388	14	-150	0	521	-5	6.28	6.28	12.57	12.57	-4.33	-60.3
42	12	-6429	18	-401	0	2289	-5	6.28	6.28	12.57	12.57	-14.79	285.4
43	12	-6512	-132	-165	0	554	-13	6.28	6.28	12.57	12.57	-4.50	-62.5
44	12	-6064	164	-106	0	389	3	6.28	6.28	12.57	12.57	-3.74	-52.6
45	12	-6177	24	-531	0	3344	-5	6.28	6.28	12.57	12.57	-22.00	611.5
46	12	-5941	21	-92	0	323	-4	6.28	6.28	12.57	12.57	-3.45	-48.9
47	12	-5830	22	-77	0	274	-4	6.28	6.28	12.57	12.57	-3.23	-46.0
49	12	-5910	-8	-88	0	305	-6	6.28	6.28	12.57	12.57	-3.38	-47.9
50	12	-5821	51	-76	0	272	-3	6.28	6.28	12.57	12.57	-3.22	-45.9
51	12	-5843	23	-161	0	863	-4	6.28	6.28	12.57	12.57	-5.48	-74.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	25	-6554	-76	-181	0	638	-19	6.28	6.28	12.57	12.57	-4.81	-66.5
41	25	-6313	14	-150	0	540	-3	6.28	6.28	12.57	12.57	-4.37	-60.7
42	25	-6354	18	-401	0	2339	-3	6.28	6.28	12.57	12.57	-15.15	303.6
43	25	-6437	-132	-165	0	574	-29	6.28	6.28	12.57	12.57	-4.54	-63.0
44	25	-5989	164	-106	0	403	23	6.28	6.28	12.57	12.57	-3.76	-52.7
45	25	-6102	24	-531	0	3410	-2	6.28	6.28	12.57	12.57	-22.45	636.5
46	25	-5866	21	-92	0	335	-2	6.28	6.28	12.57	12.57	-3.46	-49.0
47	25	-5755	22	-77	0	283	-1	6.28	6.28	12.57	12.57	-3.24	-46.0
49	25	-5835	-8	-88	0	316	-7	6.28	6.28	12.57	12.57	-3.39	-48.0
50	25	-5746	51	-76	0	282	4	6.28	6.28	12.57	12.57	-3.23	-45.9
51	25	-5768	23	-161	0	883	-1	6.28	6.28	12.57	12.57	-5.57	-74.8

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	38	-6479	-76	-181	0	660	-29	6.28	6.28	12.57	12.57	-4.87	-67.1
41	38	-6238	14	-150	0	559	-2	6.28	6.28	12.57	12.57	-4.41	-61.2
42	38	-6279	18	-401	0	2389	-1	6.28	6.28	12.57	12.57	-15.51	322.1
43	38	-6362	-132	-165	0	595	-45	6.28	6.28	12.57	12.57	-4.59	-63.5
44	38	-5914	164	-106	0	416	44	6.28	6.28	12.57	12.57	-3.77	-52.9
45	38	-6027	24	-531	0	3477	1	6.28	6.28	12.57	12.57	-22.89	661.7
46	38	-5791	21	-92	0	346	1	6.28	6.28	12.57	12.57	-3.48	-49.1
47	38	-5680	22	-77	0	293	2	6.28	6.28	12.57	12.57	-3.24	-46.0
49	38	-5760	-8	-88	0	327	-8	6.28	6.28	12.57	12.57	-3.40	-48.0
50	38	-5671	51	-76	0	291	10	6.28	6.28	12.57	12.57	-3.23	-45.9
51	38	-5693	23	-161	0	903	2	6.28	6.28	12.57	12.57	-5.65	-75.7

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	50	-6404	-76	-181	0	683	-38	6.28	6.28	12.57	12.57	-4.92	-67.7
41	50	-6163	14	-150	0	577	0	6.28	6.28	12.57	12.57	-4.45	-61.6
42	50	-6204	18	-401	0	2439	1	6.28	6.28	12.57	12.57	-15.87	340.7
43	50	-6287	-132	-165	0	616	-62	6.28	6.28	12.57	12.57	-4.63	-64.0
44	50	-5839	164	-106	0	429	64	6.28	6.28	12.57	12.57	-3.79	-53.0
45	50	-5952	24	-531	0	3543	4	6.28	6.28	12.57	12.57	-23.33	686.9
46	50	-5716	21	-92	0	358	4	6.28	6.28	12.57	12.57	-3.49	-49.1
47	50	-5605	22	-77	0	303	4	6.28	6.28	12.57	12.57	-3.25	-46.0
49	50	-5685	-8	-88	0	338	-8	6.28	6.28	12.57	12.57	-3.41	-48.1
50	50	-5596	51	-76	0	301	17	6.28	6.28	12.57	12.57	-3.24	-45.9
51	50	-5618	23	-161	0	923	5	6.28	6.28	12.57	12.57	-5.74	-76.7

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 113 NI 89 NF 41 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 17A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	--												
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-10010	-421	-321	0	652	-38	6.28	6.28	12.57	12.57	-6.20	-87.2
41	0	-9625	-37	-266	0	551	0	6.28	6.28	12.57	12.57	-5.69	-80.4
42	0	-9687	-25	-696	0	2249	1	6.28	6.28	12.57	12.57	-13.93	-178.0
43	0	-9827	-653	-293	0	589	-62	6.28	6.28	12.57	12.57	-5.91	-83.3
44	0	-9104	600	-188	0	407	64	6.28	6.28	12.57	12.57	-4.98	-71.0
45	0	-9286	6	-919	0	3249	4	6.28	6.28	12.57	12.57	-20.97	396.3
46	0	-8916	2	-163	0	341	4	6.28	6.28	12.57	12.57	-4.66	-66.9
47	0	-8739	11	-137	0	288	4	6.28	6.28	12.57	12.57	-4.41	-63.5
49	0	-8868	-117	-155	0	322	-8	6.28	6.28	12.57	12.57	-4.58	-65.8
50	0	-8723	134	-134	0	286	17	6.28	6.28	12.57	12.57	-4.39	-63.3
51	0	-8760	15	-280	0	854	5	6.28	6.28	12.57	12.57	-6.44	-89.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	12	-9936	-421	-321	0	692	-91	6.28	6.28	12.57	12.57	-6.32	-88.6
41	12	-9550	-37	-266	0	584	-4	6.28	6.28	12.57	12.57	-5.78	-81.5
42	12	-9612	-25	-696	0	2336	-2	6.28	6.28	12.57	12.57	-14.53	-184.3
43	12	-9752	-653	-293	0	626	-144	6.28	6.28	12.57	12.57	-6.01	-84.5
44	12	-9029	600	-188	0	431	139	6.28	6.28	12.57	12.57	-5.03	-71.6
45	12	-9211	6	-919	0	3364	5	6.28	6.28	12.57	12.57	-21.78	432.6
46	12	-8841	2	-163	0	361	4	6.28	6.28	12.57	12.57	-4.71	-67.4
47	12	-8664	11	-137	0	305	6	6.28	6.28	12.57	12.57	-4.44	-63.9
49	12	-8793	-117	-155	0	342	-23	6.28	6.28	12.57	12.57	-4.62	-66.2
50	12	-8648	134	-134	0	303	33	6.28	6.28	12.57	12.57	-4.42	-63.7
51	12	-8685	15	-280	0	889	7	6.28	6.28	12.57	12.57	-6.54	-90.1

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	25	-9861	-421	-321	0	733	-144	6.28	6.28	12.57	12.57	-6.43	-89.9
41	25	-9475	-37	-266	0	617	-9	6.28	6.28	12.57	12.57	-5.87	-82.5
42	25	-9537	-25	-696	0	2423	-5	6.28	6.28	12.57	12.57	-15.14	-190.7
43	25	-9677	-653	-293	0	662	-225	6.28	6.28	12.57	12.57	-6.11	-85.7
44	25	-8954	600	-188	0	454	214	6.28	6.28	12.57	12.57	-5.09	-72.2
45	25	-9136	6	-919	0	3479	6	6.28	6.28	12.57	12.57	-22.59	469.4
46	25	-8766	2	-163	0	381	4	6.28	6.28	12.57	12.57	-4.75	-67.9
47	25	-8589	11	-137	0	323	7	6.28	6.28	12.57	12.57	-4.47	-64.2
49	25	-8718	-117	-155	0	361	-38	6.28	6.28	12.57	12.57	-4.66	-66.7
50	25	-8573	134	-134	0	319	50	6.28	6.28	12.57	12.57	-4.46	-64.0
51	25	-8610	15	-280	0	924	9	6.28	6.28	12.57	12.57	-6.64	-91.3

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	38	-9786	-421	-321	0	773	-196	6.28	6.28	12.57	12.57	-6.55	-91.3
41	38	-9400	-37	-266	0	650	-14	6.28	6.28	12.57	12.57	-5.96	-83.6
42	38	-9462	-25	-696	0	2510	-8	6.28	6.28	12.57	12.57	-15.76	-197.0
43	38	-9602	-653	-293	0	699	-307	6.28	6.28	12.57	12.57	-6.21	-86.9
44	38	-8879	600	-188	0	478	289	6.28	6.28	12.57	12.57	-5.14	-72.8
45	38	-9061	6	-919	0	3594	7	6.28	6.28	12.57	12.57	-23.40	506.8
46	38	-8691	2	-163	0	402	4	6.28	6.28	12.57	12.57	-4.80	-68.3
47	38	-8514	11	-137	0	340	9	6.28	6.28	12.57	12.57	-4.51	-64.5
49	38	-8643	-117	-155	0	380	-52	6.28	6.28	12.57	12.57	-4.70	-67.1
50	38	-8498	134	-134	0	336	67	6.28	6.28	12.57	12.57	-4.49	-64.3
51	38	-8535	15	-280	0	959	10	6.28	6.28	12.57	12.57	-6.73	-92.4

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	50	-9712	-421	-321	0	813	-249	6.28	6.28	12.57	12.57	-6.66	-92.7
41	50	-9325	-37	-266	0	684	-18	6.28	6.28	12.57	12.57	-6.05	-84.6
42	50	-9387	-25	-696	0	2597	-11	6.28	6.28	12.57	12.57	-16.38	220.5
43	50	-9527	-653	-293	0	735	-389	6.28	6.28	12.57	12.57	-6.31	-88.1
44	50	-8804	600	-188	0	501	364	6.28	6.28	12.57	12.57	-5.20	-73.5
45	50	-8986	6	-919	0	3709	8	6.28	6.28	12.57	12.57	-24.20	544.6
46	50	-8616	2	-163	0	422	4	6.28	6.28	12.57	12.57	-4.84	-68.8
47	50	-8439	11	-137	0	357	10	6.28	6.28	12.57	12.57	-4.54	-64.9
49	50	-8568	-117	-155	0	400	-67	6.28	6.28	12.57	12.57	-4.74	-67.5
50	50	-8423	134	-134	0	353	84	6.28	6.28	12.57	12.57	-4.52	-64.6
51	50	-8460	15	-280	0	994	12	6.28	6.28	12.57	12.57	-6.84	-93.7

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 114 NI 477 NF 46 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 22
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-7196	-72	52	0	-93	-22	6.28	6.28	12.57	12.57	-3.11	-45.9
41	0	-7135	-7	7	0	29	-22	6.28	6.28	12.57	12.57	-2.86	-42.6
42	0	-7190	13	-130	0	1384	-25	6.28	6.28	12.57	12.57	-8.50	-111.6
43	0	-6932	-119	86	0	-194	-17	6.28	6.28	12.57	12.57	-3.37	-48.9
44	0	-7122	100	-70	0	238	-22	6.28	6.28	12.57	12.57	-3.60	-51.9
45	0	-6922	21	-218	0	2268	-23	6.28	6.28	12.57	12.57	-14.56	253.3
46	0	-6648	-15	13	0	-4	-15	6.28	6.28	12.57	12.57	-2.58	-38.7
47	0	-6527	-17	15	0	-12	-13	6.28	6.28	12.57	12.57	-2.56	-38.4
49	0	-6547	-39	30	0	-52	-13	6.28	6.28	12.57	12.57	-2.72	-40.3
50	0	-6585	5	-1	0	34	-14	6.28	6.28	12.57	12.57	-2.67	-39.7
51	0	-6545	-11	-31	0	440	-14	6.28	6.28	12.57	12.57	-4.10	-57.6

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	12	-7121	-72	52	0	-99	-31	6.28	6.28	12.57	12.57	-3.11	-45.7
41	12	-7060	-7	7	0	28	-22	6.28	6.28	12.57	12.57	-2.83	-42.2
42	12	-7115	13	-130	0	1400	-23	6.28	6.28	12.57	12.57	-8.60	-112.5
43	12	-6857	-119	86	0	-205	-32	6.28	6.28	12.57	12.57	-3.38	-48.9
44	12	-7047	100	-70	0	246	-9	6.28	6.28	12.57	12.57	-3.60	-51.9
45	12	-6847	21	-218	0	2295	-20	6.28	6.28	12.57	12.57	-14.76	264.6
46	12	-6573	-15	13	0	-5	-17	6.28	6.28	12.57	12.57	-2.56	-38.3
47	12	-6452	-17	15	0	-14	-15	6.28	6.28	12.57	12.57	-2.54	-38.0
49	12	-6472	-39	30	0	-56	-18	6.28	6.28	12.57	12.57	-2.70	-40.0
50	12	-6510	5	-1	0	34	-13	6.28	6.28	12.57	12.57	-2.64	-39.2
51	12	-6470	-11	-31	0	444	-15	6.28	6.28	12.57	12.57	-4.09	-57.4

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	25	-7046	-72	52	0	-106	-40	6.28	6.28	12.57	12.57	-3.10	-45.6
41	25	-6985	-7	7	0	27	-23	6.28	6.28	12.57	12.57	-2.80	-41.7
42	25	-7040	13	-130	0	1416	-22	6.28	6.28	12.57	12.57	-8.70	-113.5
43	25	-6782	-119	86	0	-216	-47	6.28	6.28	12.57	12.57	-3.39	-48.9
44	25	-6972	100	-70	0	255	3	6.28	6.28	12.57	12.57	-3.61	-51.8
45	25	-6772	21	-218	0	2322	-17	6.28	6.28	12.57	12.57	-14.96	275.9
46	25	-6498	-15	13	0	-7	-19	6.28	6.28	12.57	12.57	-2.54	-38.0
47	25	-6377	-17	15	0	-16	-17	6.28	6.28	12.57	12.57	-2.52	-37.7
49	25	-6397	-39	30	0	-60	-23	6.28	6.28	12.57	12.57	-2.69	-39.8
50	25	-6435	5	-1	0	34	-13	6.28	6.28	12.57	12.57	-2.61	-38.8
51	25	-6395	-11	-31	0	448	-17	6.28	6.28	12.57	12.57	-4.07	-57.1

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	38	-6971	-72	52	0	-112	-48	6.28	6.28	12.57	12.57	-3.09	-45.4
41	38	-6910	-7	7	0	26	-24	6.28	6.28	12.57	12.57	-2.76	-41.2
42	38	-6965	13	-130	0	1433	-20	6.28	6.28	12.57	12.57	-8.81	-114.6
43	38	-6707	-119	86	0	-226	-62	6.28	6.28	12.57	12.57	-3.40	-49.0
44	38	-6897	100	-70	0	264	16	6.28	6.28	12.57	12.57	-3.61	-51.8
45	38	-6697	21	-218	0	2349	-15	6.28	6.28	12.57	12.57	-15.16	287.5
46	38	-6423	-15	13	0	-9	-20	6.28	6.28	12.57	12.57	-2.51	-37.6
47	38	-6302	-17	15	0	-18	-19	6.28	6.28	12.57	12.57	-2.50	-37.3
49	38	-6322	-39	30	0	-64	-28	6.28	6.28	12.57	12.57	-2.67	-39.5
50	38	-6360	5	-1	0	34	-12	6.28	6.28	12.57	12.57	-2.58	-38.4
51	38	-6320	-11	-31	0	451	-18	6.28	6.28	12.57	12.57	-4.06	-56.8

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	50	-6896	-72	52	0	-119	-57	6.28	6.28	12.57	12.57	-3.09	-45.3

41	50	-6835	-7	7	0	25	-25	6.28	6.28	12.57	12.57	-2.73	-40.7
42	50	-6890	13	-130	0	1449	-18	6.28	6.28	12.57	12.57	-8.91	-115.6
43	50	-6632	-119	86	0	-237	-77	6.28	6.28	12.57	12.57	-3.41	-49.0
44	50	-6822	100	-70	0	272	28	6.28	6.28	12.57	12.57	-3.61	-51.7
45	50	-6622	21	-218	0	2376	-12	6.28	6.28	12.57	12.57	-15.36	299.1
46	50	-6348	-15	13	0	-10	-22	6.28	6.28	12.57	12.57	-2.49	-37.3
47	50	-6227	-17	15	0	-19	-22	6.28	6.28	12.57	12.57	-2.47	-37.0
49	50	-6247	-39	30	0	-67	-32	6.28	6.28	12.57	12.57	-2.65	-39.2
50	50	-6285	5	-1	0	35	-11	6.28	6.28	12.57	12.57	-2.55	-38.0
51	50	-6245	-11	-31	0	455	-19	6.28	6.28	12.57	12.57	-4.04	-56.6

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 115 NI 46 NF 42 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 22A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-10810	-789	93	0	-120	-57	6.28	6.28	12.57	12.57	-4.61	-68.0
41	0	-10730	-434	13	0	20	-25	6.28	6.28	12.57	12.57	-4.22	-63.1
42	0	-10800	-377	-216	0	1300	-18	6.28	6.28	12.57	12.57	-8.85	-121.0
43	0	-10390	-978	153	0	-234	-77	6.28	6.28	12.57	12.57	-4.85	-70.7
44	0	-10740	151	-123	0	259	28	6.28	6.28	12.57	12.57	-5.08	-73.8
45	0	-10370	-291	-362	0	2133	-12	6.28	6.28	12.57	12.57	-13.11	-170.5
46	0	-9969	-359	24	0	-13	-22	6.28	6.28	12.57	12.57	-3.90	-58.4
47	0	-9778	-340	27	0	-22	-22	6.28	6.28	12.57	12.57	-3.86	-57.6
49	0	-9804	-458	53	0	-68	-32	6.28	6.28	12.57	12.57	-4.03	-59.9
50	0	-9874	-232	-2	0	30	-11	6.28	6.28	12.57	12.57	-3.92	-58.6
51	0	-9801	-321	-50	0	405	-19	6.28	6.28	12.57	12.57	-5.24	-74.9

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	12	-10735	-789	93	0	-132	-156	6.28	6.28	12.57	12.57	-4.64	-68.1
41	12	-10655	-434	13	0	18	-80	6.28	6.28	12.57	12.57	-4.23	-62.6
42	12	-10725	-377	-216	0	1327	-65	6.28	6.28	12.57	12.57	-8.93	-122.0
43	12	-10315	-978	153	0	-253	-199	6.28	6.28	12.57	12.57	-4.89	-71.1
44	12	-10665	151	-123	0	275	47	6.28	6.28	12.57	12.57	-5.10	-74.1
45	12	-10295	-291	-362	0	2178	-48	6.28	6.28	12.57	12.57	-13.40	-173.7
46	12	-9894	-359	24	0	-16	-67	6.28	6.28	12.57	12.57	-3.89	-58.1
47	12	-9703	-340	27	0	-25	-64	6.28	6.28	12.57	12.57	-3.84	-57.4
49	12	-9729	-458	53	0	-75	-90	6.28	6.28	12.57	12.57	-4.03	-59.7
50	12	-9799	-232	-2	0	31	-40	6.28	6.28	12.57	12.57	-3.90	-58.2
51	12	-9726	-321	-50	0	411	-59	6.28	6.28	12.57	12.57	-5.23	-74.8

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	25	-10660	-789	93	0	-143	-255	6.28	6.28	12.57	12.57	-5.10	-71.7
41	25	-10580	-434	13	0	16	-134	6.28	6.28	12.57	12.57	-4.47	-64.6
42	25	-10650	-377	-216	0	1354	-113	6.28	6.28	12.57	12.57	-9.02	-122.9
43	25	-10240	-978	153	0	-272	-322	6.28	6.28	12.57	12.57	-5.28	-73.2
44	25	-10590	151	-123	0	290	66	6.28	6.28	12.57	12.57	-5.13	-74.4
45	25	-10220	-291	-362	0	2224	-85	6.28	6.28	12.57	12.57	-13.70	-176.8
46	25	-9819	-359	24	0	-19	-112	6.28	6.28	12.57	12.57	-4.09	-59.3
47	25	-9628	-340	27	0	-28	-107	6.28	6.28	12.57	12.57	-3.99	-57.9
49	25	-9654	-458	53	0	-82	-147	6.28	6.28	12.57	12.57	-4.20	-60.3
50	25	-9724	-232	-2	0	31	-69	6.28	6.28	12.57	12.57	-3.87	-57.7
51	25	-9651	-321	-50	0	417	-99	6.28	6.28	12.57	12.57	-5.22	-74.6

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	38	-10585	-789	93	0	-155	-353	6.28	6.28	12.57	12.57	-5.56	-76.8
41	38	-10505	-434	13	0	15	-188	6.28	6.28	12.57	12.57	-4.71	-67.2
42	38	-10575	-377	-216	0	1381	-160	6.28	6.28	12.57	12.57	-9.11	-123.9
43	38	-10165	-978	153	0	-291	-444	6.28	6.28	12.57	12.57	-5.85	-79.6
44	38	-10515	151	-123	0	306	85	6.28	6.28	12.57	12.57	-5.16	-74.6
45	38	-10145	-291	-362	0	2269	-121	6.28	6.28	12.57	12.57	-14.01	-180.0
46	38	-9744	-359	24	0	-22	-157	6.28	6.28	12.57	12.57	-4.28	-61.4
47	38	-9553	-340	27	0	-32	-149	6.28	6.28	12.57	12.57	-4.18	-59.9
49	38	-9579	-458	53	0	-88	-204	6.28	6.28	12.57	12.57	-4.46	-63.1
50	38	-9649	-232	-2	0	31	-98	6.28	6.28	12.57	12.57	-3.96	-57.6
51	38	-9576	-321	-50	0	424	-140	6.28	6.28	12.57	12.57	-5.22	-74.5

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	50	-10510	-789	93	0	-166	-452	6.28	6.28	12.57	12.57	-6.02	-81.9
41	50	-10430	-434	13	0	13	-242	6.28	6.28	12.57	12.57	-4.95	-69.8
42	50	-10500	-377	-216	0	1408	-207	6.28	6.28	12.57	12.57	-9.20	-125.0
43	50	-10090	-978	153	0	-310	-566	6.28	6.28	12.57	12.57	-6.43	-86.0
44	50	-10440	151	-123	0	321	104	6.28	6.28	12.57	12.57	-5.18	-74.9
45	50	-10070	-291	-362	0	2314	-158	6.28	6.28	12.57	12.57	-14.32	-183.2
46	50	-9669	-359	24	0	-25	-202	6.28	6.28	12.57	12.57	-4.48	-63.4
47	50	-9478	-340	27	0	-35	-192	6.28	6.28	12.57	12.57	-4.36	-61.8
49	50	-9504	-458	53	0	-95	-261	6.28	6.28	12.57	12.57	-4.71	-65.9
50	50	-9574	-232	-2	0	31	-127	6.28	6.28	12.57	12.57	-4.08	-58.8
51	50	-9501	-321	-50	0	430	-180	6.28	6.28	12.57	12.57	-5.21	-74.3

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 116 NI 216 NF 482 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 32
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-2654	-1303	559	0	197	790	6.28	6.28	12.57	12.57	-6.41	108.1
41	0	-2722	-938	323	0	134	580	6.28	6.28	12.57	12.57	-4.73	56.4
42	0	-2486	-595	-670	0	-356	482	6.28	6.28	12.57	12.57	-3.94	-44.7
43	0	-2641	-1401	610	0	228	815	6.28	6.28	12.57	12.57	-6.61	114.6
44	0	-2849	-351	-60	0	31	248	6.28	6.28	12.57	12.57	-2.26	-29.3

45	0	-2360	-221	-1439	0	-694	301	6.28	6.28	12.57	12.57	-4.40	65.5
46	0	-2773	-704	152	0	118	396	6.28	6.28	12.57	12.57	-3.27	-39.4
47	0	-2785	-645	109	0	114	350	6.28	6.28	12.57	12.57	-2.92	-36.0
49	0	-2763	-767	188	0	134	420	6.28	6.28	12.57	12.57	-3.45	-41.2
50	0	-2804	-557	54	0	95	307	6.28	6.28	12.57	12.57	-2.62	-33.0
51	0	-2706	-531	-222	0	-50	317	6.28	6.28	12.57	12.57	-2.68	-33.4

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	12	-2579	-1303	559	0	127	627	6.28	6.28	12.57	12.57	-5.11	71.3
41	12	-2647	-938	323	0	94	462	6.28	6.28	12.57	12.57	-3.79	-43.9
42	12	-2411	-595	-670	0	-272	407	6.28	6.28	12.57	12.57	-3.34	-39.0
43	12	-2566	-1401	610	0	152	640	6.28	6.28	12.57	12.57	-5.21	74.8
44	12	-2774	-351	-60	0	39	204	6.28	6.28	12.57	12.57	-2.01	-26.3
45	12	-2285	-221	-1439	0	-514	274	6.28	6.28	12.57	12.57	-3.17	-40.8
46	12	-2698	-704	152	0	99	308	6.28	6.28	12.57	12.57	-2.61	-32.7
47	12	-2710	-645	109	0	100	269	6.28	6.28	12.57	12.57	-2.36	-30.0
49	12	-2688	-767	188	0	111	324	6.28	6.28	12.57	12.57	-2.72	-33.8
50	12	-2729	-557	54	0	88	237	6.28	6.28	12.57	12.57	-2.17	-28.0
51	12	-2631	-531	-222	0	-22	251	6.28	6.28	12.57	12.57	-2.22	-28.5

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	25	-2504	-1303	559	0	57	464	6.28	6.28	12.57	12.57	-3.79	-43.5
41	25	-2572	-938	323	0	54	345	6.28	6.28	12.57	12.57	-2.86	-34.9
42	25	-2336	-595	-670	0	-189	333	6.28	6.28	12.57	12.57	-2.75	-33.1
43	25	-2491	-1401	610	0	76	465	6.28	6.28	12.57	12.57	-3.80	-43.5
44	25	-2699	-351	-60	0	46	160	6.28	6.28	12.57	12.57	-1.76	-23.5
45	25	-2210	-221	-1439	0	-334	246	6.28	6.28	12.57	12.57	-2.11	-28.4
46	25	-2623	-704	152	0	80	220	6.28	6.28	12.57	12.57	-2.04	-26.5
47	25	-2635	-645	109	0	86	189	6.28	6.28	12.57	12.57	-1.88	-24.7
49	25	-2613	-767	188	0	88	228	6.28	6.28	12.57	12.57	-2.08	-26.9
50	25	-2654	-557	54	0	82	167	6.28	6.28	12.57	12.57	-1.78	-23.6
51	25	-2556	-531	-222	0	6	185	6.28	6.28	12.57	12.57	-1.83	-24.1

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	38	-2429	-1303	559	0	-13	301	6.28	6.28	12.57	12.57	-2.52	-31.1
41	38	-2497	-938	323	0	13	228	6.28	6.28	12.57	12.57	-2.05	-26.4
42	38	-2261	-595	-670	0	-105	258	6.28	6.28	12.57	12.57	-2.19	-27.4
43	38	-2416	-1401	610	0	-0	290	6.28	6.28	12.57	12.57	-2.43	-30.2
44	38	-2624	-351	-60	0	54	116	6.28	6.28	12.57	12.57	-1.52	-20.6
45	38	-2135	-221	-1439	0	-154	219	6.28	6.28	12.57	12.57	-1.90	-24.1
46	38	-2548	-704	152	0	61	132	6.28	6.28	12.57	12.57	-1.57	-21.1
47	38	-2560	-645	109	0	73	108	6.28	6.28	12.57	12.57	-1.46	-19.8
49	38	-2538	-767	188	0	64	132	6.28	6.28	12.57	12.57	-1.57	-21.1
50	38	-2579	-557	54	0	75	98	6.28	6.28	12.57	12.57	-1.41	-19.4
51	38	-2481	-531	-222	0	33	118	6.28	6.28	12.57	12.57	-1.48	-20.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	50	-2354	-1303	559	0	-82	138	6.28	6.28	12.57	12.57	-1.53	-20.4
41	50	-2422	-938	323	0	-27	111	6.28	6.28	12.57	12.57	-1.42	-19.2
42	50	-2186	-595	-670	0	-21	184	6.28	6.28	12.57	12.57	-1.70	-22.1
43	50	-2341	-1401	610	0	-76	115	6.28	6.28	12.57	12.57	-1.41	-19.0
44	50	-2549	-351	-60	0	61	72	6.28	6.28	12.57	12.57	-1.27	-17.8
45	50	-2060	-221	-1439	0	26	191	6.28	6.28	12.57	12.57	-1.71	-21.9
46	50	-2473	-704	152	0	42	44	6.28	6.28	12.57	12.57	-1.11	-16.2
47	50	-2485	-645	109	0	59	27	6.28	6.28	12.57	12.57	-1.17	-17.1
49	50	-2463	-767	188	0	41	37	6.28	6.28	12.57	12.57	-1.10	-16.1
50	50	-2504	-557	54	0	68	28	6.28	6.28	12.57	12.57	-1.21	-17.6
51	50	-2406	-531	-222	0	61	52	6.28	6.28	12.57	12.57	-1.15	-16.7

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 117 NI 482 NF 33 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 32A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-4550	509	332	0	37	-227	6.28	6.28	12.57	12.57	-2.76	-37.2
41	0	-4385	467	252	0	71	-156	6.28	6.28	12.57	12.57	-2.35	-32.4
42	0	-4262	545	-4	0	301	-125	6.28	6.28	12.57	12.57	-2.72	-38.2
43	0	-4493	417	321	0	38	-265	6.28	6.28	12.57	12.57	-2.93	-39.0
44	0	-4164	417	124	0	128	-38	6.28	6.28	12.57	12.57	-2.07	-29.9
45	0	-4013	476	-240	0	478	-94	6.28	6.28	12.57	12.57	-3.27	-44.7
46	0	-4118	273	148	0	110	-140	6.28	6.28	12.57	12.57	-2.17	-30.0
47	0	-4051	224	122	0	119	-135	6.28	6.28	12.57	12.57	-2.13	-29.4
49	0	-4106	238	149	0	108	-159	6.28	6.28	12.57	12.57	-2.27	-31.0
50	0	-4040	239	110	0	126	-114	6.28	6.28	12.57	12.57	-2.02	-29.1
51	0	-4010	250	37	0	196	-125	6.28	6.28	12.57	12.57	-2.25	-32.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	12	-4475	509	332	0	-5	-164	6.28	6.28	12.57	12.57	-2.42	-33.3
41	12	-4310	467	252	0	40	-98	6.28	6.28	12.57	12.57	-2.03	-28.7
42	12	-4187	545	-4	0	301	-57	6.28	6.28	12.57	12.57	-2.70	-37.7
43	12	-4418	417	321	0	-2	-213	6.28	6.28	12.57	12.57	-2.64	-35.7
44	12	-4089	417	124	0	113	14	6.28	6.28	12.57	12.57	-1.98	-28.7
45	12	-3938	476	-240	0	508	-34	6.28	6.28	12.57	12.57	-3.36	-45.8
46	12	-4043	273	148	0	91	-105	6.28	6.28	12.57	12.57	-1.98	-27.7
47	12	-3976	224	122	0	104	-107	6.28	6.28	12.57	12.57	-1.96	-27.7
49	12	-4031	238	149	0	89	-129	6.28	6.28	12.57	12.57	-2.09	-29.0
50	12	-3965	239	110	0	112	-84	6.28	6.28	12.57	12.57	-1.93	-28.0
51	12	-3935	250	37	0	191	-94	6.28	6.28	12.57	12.57	-2.20	-31.4

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	25	-4400	509	332	0	-46	-100	6.28	6.28	12.57	12.57	-2.08	-29.3
41	25	-4235	467	252	0	8	-39	6.28	6.28	12.57	12.57	-1.72	-25.1
42	25	-4112	545	-4	0	302	11	6.28	6.28	12.57	12.57	-2.67	-37.3
43	25	-4343	417	321	0	-43	-161	6.28	6.28	12.57	12.57	-2.36	-32.4
44	25	-4014	417	124	0	97	66	6.28	6.28	12.57	12.57	-1.90	-27.6
45	25	-3863	476	-240	0	538	25	6.28	6.28	12.57	12.57	-3.47	-47.0

46	25	-3968	273	148	0	73	-71	6.28	6.28	12.57	12.57	-1.79	-26.3
47	25	-3901	224	122	0	89	-79	6.28	6.28	12.57	12.57	-1.83	-26.6
49	25	-3956	238	149	0	71	-100	6.28	6.28	12.57	12.57	-1.92	-26.9
50	25	-3890	239	110	0	99	-54	6.28	6.28	12.57	12.57	-1.86	-27.0
51	25	-3860	250	37	0	187	-62	6.28	6.28	12.57	12.57	-2.16	-30.7

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	38	-4325	509	332	0	-88	-36	6.28	6.28	12.57	12.57	-1.99	-29.0
41	38	-4160	467	252	0	-23	19	6.28	6.28	12.57	12.57	-1.69	-25.1
42	38	-4037	545	-4	0	302	80	6.28	6.28	12.57	12.57	-2.64	-36.9
43	38	-4268	417	321	0	-83	-109	6.28	6.28	12.57	12.57	-2.07	-29.1
44	38	-3939	417	124	0	82	118	6.28	6.28	12.57	12.57	-2.00	-27.8
45	38	-3788	476	-240	0	567	85	6.28	6.28	12.57	12.57	-3.59	-48.4
46	38	-3893	273	148	0	54	-37	6.28	6.28	12.57	12.57	-1.70	-25.0
47	38	-3826	224	122	0	74	-51	6.28	6.28	12.57	12.57	-1.74	-25.5
49	38	-3881	238	149	0	52	-70	6.28	6.28	12.57	12.57	-1.74	-24.8
50	38	-3815	239	110	0	85	-25	6.28	6.28	12.57	12.57	-1.78	-25.9
51	38	-3785	250	37	0	182	-31	6.28	6.28	12.57	12.57	-2.11	-30.1

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	50	-4250	509	332	0	-129	27	6.28	6.28	12.57	12.57	-2.11	-30.4
41	50	-4085	467	252	0	-54	77	6.28	6.28	12.57	12.57	-1.85	-26.4
42	50	-3962	545	-4	0	303	148	6.28	6.28	12.57	12.57	-2.61	-36.5
43	50	-4193	417	321	0	-123	-57	6.28	6.28	12.57	12.57	-2.06	-29.8
44	50	-3864	417	124	0	66	170	6.28	6.28	12.57	12.57	-2.23	-30.3
45	50	-3713	476	-240	0	597	144	6.28	6.28	12.57	12.57	-3.73	-49.9
46	50	-3818	273	148	0	36	-3	6.28	6.28	12.57	12.57	-1.60	-23.7
47	50	-3751	224	122	0	58	-23	6.28	6.28	12.57	12.57	-1.66	-24.3
49	50	-3806	238	149	0	33	-40	6.28	6.28	12.57	12.57	-1.59	-23.5
50	50	-3740	239	110	0	71	5	6.28	6.28	12.57	12.57	-1.70	-24.9
51	50	-3710	250	37	0	177	0	6.28	6.28	12.57	12.57	-2.07	-29.4

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 118 NI 803 NF 821 SEZ. Rp B= 0.400 H= 0.600 (pilastro)
PIL. NUM. 26
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-4651	3210	360	0	77	-1607	12.57	12.57	6.28	6.28	-10.36	192.9
41	0	-4686	2019	292	0	63	-254	12.57	12.57	6.28	6.28	-2.72	-38.5
42	0	-4687	2023	170	0	51	-250	12.57	12.57	6.28	6.28	-2.70	-38.3
43	0	-4508	3557	328	0	77	-2364	12.57	12.57	6.28	6.28	-15.54	423.0
44	0	-4711	105	196	0	40	1979	12.57	12.57	6.28	6.28	-12.92	295.6
45	0	-4568	1580	13	0	32	-103	12.57	12.57	6.28	6.28	-2.13	-31.1
46	0	-4495	1306	169	0	47	-24	12.57	12.57	6.28	6.28	-1.85	-27.1
47	0	-4447	1127	138	0	42	33	12.57	12.57	6.28	6.28	-1.84	-27.3
49	0	-4436	1524	161	0	47	-418	12.57	12.57	6.28	6.28	-3.21	-44.4
50	0	-4476	834	134	0	40	451	12.57	12.57	6.28	6.28	-3.34	-46.1
51	0	-4447	1129	98	0	38	35	12.57	12.57	6.28	6.28	-1.84	-27.3

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	12	-4576	3210	360	0	32	-1206	12.57	12.57	6.28	6.28	-7.56	-94.7
41	12	-4611	2019	292	0	27	-2	12.57	12.57	6.28	6.28	-1.79	-26.8
42	12	-4612	2023	170	0	29	3	12.57	12.57	6.28	6.28	-1.81	-26.9
43	12	-4433	3557	328	0	36	-1919	12.57	12.57	6.28	6.28	-12.55	294.9
44	12	-4636	105	196	0	16	1992	12.57	12.57	6.28	6.28	-13.02	303.9
45	12	-4493	1580	13	0	31	95	12.57	12.57	6.28	6.28	-2.08	-30.3
46	12	-4420	1306	169	0	25	139	12.57	12.57	6.28	6.28	-2.21	-31.8
47	12	-4372	1127	138	0	25	174	12.57	12.57	6.28	6.28	-2.31	-33.1
49	12	-4361	1524	161	0	27	-227	12.57	12.57	6.28	6.28	-2.50	-35.4
50	12	-4401	834	134	0	23	555	12.57	12.57	6.28	6.28	-3.71	-50.6
51	12	-4372	1129	98	0	26	176	12.57	12.57	6.28	6.28	-2.32	-33.2

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	25	-4501	3210	360	0	-13	-804	12.57	12.57	6.28	6.28	-4.96	-65.6
41	25	-4536	2019	292	0	-10	250	12.57	12.57	6.28	6.28	-2.65	-37.5
42	25	-4537	2023	170	0	8	256	12.57	12.57	6.28	6.28	-2.67	-37.8
43	25	-4358	3557	328	0	-6	-1475	12.57	12.57	6.28	6.28	-9.49	172.2
44	25	-4561	105	196	0	-9	2005	12.57	12.57	6.28	6.28	-13.12	312.3
45	25	-4418	1580	13	0	29	292	12.57	12.57	6.28	6.28	-2.75	-38.7
46	25	-4345	1306	169	0	4	302	12.57	12.57	6.28	6.28	-2.76	-38.7
47	25	-4297	1127	138	0	8	315	12.57	12.57	6.28	6.28	-2.79	-39.0
49	25	-4286	1524	161	0	7	-36	12.57	12.57	6.28	6.28	-1.79	-26.5
50	25	-4326	834	134	0	6	660	12.57	12.57	6.28	6.28	-4.16	-56.0
51	25	-4297	1129	98	0	14	317	12.57	12.57	6.28	6.28	-2.80	-39.1

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	38	-4426	3210	360	0	-58	-403	12.57	12.57	6.28	6.28	-3.15	-43.7
41	38	-4461	2019	292	0	-46	503	12.57	12.57	6.28	6.28	-3.53	-48.4
42	38	-4462	2023	170	0	-13	509	12.57	12.57	6.28	6.28	-3.55	-48.7
43	38	-4283	3557	328	0	-47	-1030	12.57	12.57	6.28	6.28	-6.40	-81.3
44	38	-4486	105	196	0	-33	2018	12.57	12.57	6.28	6.28	-13.22	320.8
45	38	-4343	1580	13	0	27	490	12.57	12.57	6.28	6.28	-3.43	-47.1
46	38	-4270	1306	169	0	-17	465	12.57	12.57	6.28	6.28	-3.32	-45.6
47	38	-4222	1127	138	0	-9	456	12.57	12.57	6.28	6.28	-3.26	-44.9
49	38	-4211	1524	161	0	-13	154	12.57	12.57	6.28	6.28	-2.18	-31.3
50	38	-4251	834	134	0	-10	764	12.57	12.57	6.28	6.28	-4.71	-62.3
51	38	-4222	1129	98	0	2	458	12.57	12.57	6.28	6.28	-3.27	-45.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	50	-4351	3210	360	0	-102	-2	12.57	12.57	6.28	6.28	-2.07	-29.2
41	50	-4386	2019	292	0	-83	755	12.57	12.57	6.28	6.28	-4.67	-62.1
42	50	-4387	2023	170	0	-34	762	12.57	12.57	6.28	6.28	-4.71	-62.5
43	50	-4208	3557	328	0	-88	-586	12.57	12.57	6.28	6.28	-3.78	-51.2
44	50	-4411	105	196	0	-58	2031	12.57	12.57	6.28	6.28	-13.31	329.3
45	50	-4268	1580	13	0	26	687	12.57	12.57	6.28	6.28	-4.29	-57.4
46	50	-4195	1306	169	0	-38	629	12.57	12.57	6.28	6.28	-3.98	-53.6

47	50	-4147	1127	138	0	-27	597	12.57	12.57	6.28	6.28	-3.82	-51.6
49	50	-4136	1524	161	0	-33	345	12.57	12.57	6.28	6.28	-2.83	-39.4
50	50	-4176	834	134	0	-27	868	12.57	12.57	6.28	6.28	-5.34	-69.3
51	50	-4147	1129	98	0	-11	599	12.57	12.57	6.28	6.28	-3.83	-51.7

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

ASTA NUM. 119 NI 821 NF 166 SEZ. Rp B= 0.400 H= 0.600 (pilastro)
PIL. NUM. 26A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-5896	1340	969	0	-102	-71	12.57	12.57	6.28	6.28	-2.63	-37.5
41	0	-5684	1145	832	0	-83	689	12.57	12.57	6.28	6.28	-4.68	-63.9
42	0	-5683	1147	378	0	-34	695	12.57	12.57	6.28	6.28	-4.70	-64.2
43	0	-5845	1265	783	0	-88	-642	12.57	12.57	6.28	6.28	-4.56	-62.6
44	0	-5286	854	683	0	-58	1968	12.57	12.57	6.28	6.28	-12.76	258.8
45	0	-5490	944	-201	0	26	635	12.57	12.57	6.28	6.28	-4.40	-60.3
46	0	-5376	818	389	0	-38	587	12.57	12.57	6.28	6.28	-4.18	-57.4
47	0	-5300	737	278	0	-27	561	12.57	12.57	6.28	6.28	-4.06	-55.8
49	0	-5370	801	324	0	-33	308	12.57	12.57	6.28	6.28	-3.18	-44.9
50	0	-5258	719	304	0	-27	830	12.57	12.57	6.28	6.28	-5.20	-69.7
51	0	-5299	737	127	0	-11	563	12.57	12.57	6.28	6.28	-4.06	-55.9

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	12	-5821	1340	969	0	-224	96	12.57	12.57	6.28	6.28	-3.20	-43.9
41	12	-5609	1145	832	0	-187	832	12.57	12.57	6.28	6.28	-5.28	-71.2
42	12	-5608	1147	378	0	-82	838	12.57	12.57	6.28	6.28	-5.31	-71.5
43	12	-5770	1265	783	0	-186	-484	12.57	12.57	6.28	6.28	-3.96	-55.1
44	12	-5211	854	683	0	-143	2075	12.57	12.57	6.28	6.28	-13.51	293.7
45	12	-5415	944	-201	0	51	753	12.57	12.57	6.28	6.28	-4.86	-65.9
46	12	-5301	818	389	0	-86	689	12.57	12.57	6.28	6.28	-4.55	-62.0
47	12	-5225	737	278	0	-61	653	12.57	12.57	6.28	6.28	-4.38	-59.8
49	12	-5295	801	324	0	-74	408	12.57	12.57	6.28	6.28	-3.51	-48.9
50	12	-5183	719	304	0	-65	920	12.57	12.57	6.28	6.28	-5.67	-75.1
51	12	-5224	737	127	0	-26	655	12.57	12.57	6.28	6.28	-4.39	-59.9

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	25	-5746	1340	969	0	-345	264	12.57	12.57	6.28	6.28	-3.77	-50.2
41	25	-5534	1145	832	0	-291	976	12.57	12.57	6.28	6.28	-6.02	-79.8
42	25	-5533	1147	378	0	-129	981	12.57	12.57	6.28	6.28	-6.05	-80.2
43	25	-5695	1265	783	0	-283	-326	12.57	12.57	6.28	6.28	-3.45	-47.6
44	25	-5136	854	683	0	-228	2182	12.57	12.57	6.28	6.28	-14.25	329.2
45	25	-5340	944	-201	0	76	870	12.57	12.57	6.28	6.28	-5.42	-72.5
46	25	-5226	818	389	0	-135	791	12.57	12.57	6.28	6.28	-5.00	-67.3
47	25	-5150	737	278	0	-96	745	12.57	12.57	6.28	6.28	-4.76	-64.3
49	25	-5220	801	324	0	-114	508	12.57	12.57	6.28	6.28	-3.84	-53.0
50	25	-5108	719	304	0	-103	1009	12.57	12.57	6.28	6.28	-6.20	-81.1
51	25	-5149	737	127	0	-42	747	12.57	12.57	6.28	6.28	-4.77	-64.4

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	38	-5671	1340	969	0	-466	431	12.57	12.57	6.28	6.28	-4.36	-56.6
41	38	-5459	1145	832	0	-395	1119	12.57	12.57	6.28	6.28	-6.88	-89.5
42	38	-5458	1147	378	0	-176	1125	12.57	12.57	6.28	6.28	-6.91	-89.9
43	38	-5620	1265	783	0	-381	-168	12.57	12.57	6.28	6.28	-3.91	-51.6
44	38	-5061	854	683	0	-314	2288	12.57	12.57	6.28	6.28	-14.99	365.3
45	38	-5265	944	-201	0	101	988	12.57	12.57	6.28	6.28	-6.07	-80.0
46	38	-5151	818	389	0	-184	894	12.57	12.57	6.28	6.28	-5.52	-73.3
47	38	-5075	737	278	0	-131	837	12.57	12.57	6.28	6.28	-5.21	-69.5
49	38	-5145	801	324	0	-155	608	12.57	12.57	6.28	6.28	-4.17	-57.1
50	38	-5033	719	304	0	-141	1099	12.57	12.57	6.28	6.28	-6.78	-87.4
51	38	-5074	737	127	0	-58	840	12.57	12.57	6.28	6.28	-5.22	-69.6

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	50	-5596	1340	969	0	-587	599	12.57	12.57	6.28	6.28	-5.06	-64.1
41	50	-5384	1145	832	0	-499	1262	12.57	12.57	6.28	6.28	-7.82	-99.8
42	50	-5383	1147	378	0	-224	1268	12.57	12.57	6.28	6.28	-7.86	-100.2
43	50	-5545	1265	783	0	-479	-10	12.57	12.57	6.28	6.28	-4.39	-56.8
44	50	-4986	854	683	0	-399	2395	12.57	12.57	6.28	6.28	-15.72	401.8
45	50	-5190	944	-201	0	126	1106	12.57	12.57	6.28	6.28	-6.81	-88.1
46	50	-5076	818	389	0	-232	996	12.57	12.57	6.28	6.28	-6.12	-80.1
47	50	-5000	737	278	0	-166	930	12.57	12.57	6.28	6.28	-5.72	-75.3
49	50	-5070	801	324	0	-195	708	12.57	12.57	6.28	6.28	-4.57	-61.9
50	50	-4958	719	304	0	-179	1189	12.57	12.57	6.28	6.28	-7.39	-93.9
51	50	-4999	737	127	0	-74	932	12.57	12.57	6.28	6.28	-5.73	-75.5

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

ASTA NUM. 120 NI 804 NF 827 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 25
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-7621	330	613	0	7	-358	6.28	6.28	9.42	9.42	-6.94	-87.7
41	0	-7117	189	530	0	17	-68	6.28	6.28	9.42	9.42	-4.04	-57.5
42	0	-7036	189	362	0	34	-69	6.28	6.28	9.42	9.42	-4.02	-57.1
43	0	-7635	383	552	0	6	-538	6.28	6.28	9.42	9.42	-8.79	-105.7
44	0	-6233	-40	417	0	31	413	6.28	6.28	9.42	9.42	-6.88	-83.5
45	0	-6659	148	135	0	51	-58	6.28	6.28	9.42	9.42	-3.73	-53.2
46	0	-6601	123	346	0	26	-47	6.28	6.28	9.42	9.42	-3.60	-51.9
47	0	-6472	107	300	0	28	-42	6.28	6.28	9.42	9.42	-3.50	-50.5
49	0	-6641	154	328	0	25	-139	6.28	6.28	9.42	9.42	-4.46	-60.6
50	0	-6360	69	300	0	30	51	6.28	6.28	9.42	9.42	-3.53	-50.5
51	0	-6445	107	244	0	34	-43	6.28	6.28	9.42	9.42	-3.49	-50.6

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	12	-7565	330	613	0	-70	-316	6.28	6.28	9.42	9.42	-6.54	-83.5
41	12	-7061	189	530	0	-50	-44	6.28	6.28	9.42	9.42	-3.80	-56.1
42	12	-6980	189	362	0	-11	-46	6.28	6.28	9.42	9.42	-3.77	-54.5
43	12	-7579	383	552	0	-63	-490	6.28	6.28	9.42	9.42	-8.23	-100.2
44	12	-6177	-40	417	0	-22	408	6.28	6.28	9.42	9.42	-6.80	-82.6
45	12	-6603	148	135	0	35	-39	6.28	6.28	9.42	9.42	-3.53	-51.8
46	12	-6545	123	346	0	-17	-32	6.28	6.28	9.42	9.42	-3.44	-50.3
47	12	-6416	107	300	0	-9	-29	6.28	6.28	9.42	9.42	-3.35	-48.9
49	12	-6585	154	328	0	-16	-120	6.28	6.28	9.42	9.42	-4.26	-58.4
50	12	-6304	69	300	0	-8	60	6.28	6.28	9.42	9.42	-3.58	-50.9
51	12	-6389	107	244	0	4	-29	6.28	6.28	9.42	9.42	-3.34	-48.7

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	25	-7508	330	613	0	-147	-275	6.28	6.28	9.42	9.42	-6.13	-79.3
41	25	-7004	189	530	0	-116	-21	6.28	6.28	9.42	9.42	-4.05	-59.4
42	25	-6924	189	362	0	-57	-22	6.28	6.28	9.42	9.42	-3.74	-55.5
43	25	-7522	383	552	0	-132	-442	6.28	6.28	9.42	9.42	-7.70	-95.0
44	25	-6120	-40	417	0	-74	403	6.28	6.28	9.42	9.42	-6.73	-81.7
45	25	-6546	148	135	0	18	-21	6.28	6.28	9.42	9.42	-3.37	-50.4
46	25	-6488	123	346	0	-60	-17	6.28	6.28	9.42	9.42	-3.54	-52.4
47	25	-6360	107	300	0	-47	-16	6.28	6.28	9.42	9.42	-3.41	-50.6
49	25	-6528	154	328	0	-57	-100	6.28	6.28	9.42	9.42	-4.06	-56.2
50	25	-6248	69	300	0	-45	69	6.28	6.28	9.42	9.42	-3.63	-51.3
51	25	-6332	107	244	0	-27	-16	6.28	6.28	9.42	9.42	-3.31	-49.3

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	38	-7452	330	613	0	-223	-234	6.28	6.28	9.42	9.42	-5.73	-75.1
41	38	-6948	189	530	0	-182	3	6.28	6.28	9.42	9.42	-4.33	-62.8
42	38	-6867	189	362	0	-102	1	6.28	6.28	9.42	9.42	-3.92	-57.6
43	38	-7466	383	552	0	-202	-394	6.28	6.28	9.42	9.42	-7.21	-90.0
44	38	-6064	-40	417	0	-126	398	6.28	6.28	9.42	9.42	-6.65	-80.8
45	38	-6490	148	135	0	1	-2	6.28	6.28	9.42	9.42	-3.27	-49.0
46	38	-6432	123	346	0	-104	-1	6.28	6.28	9.42	9.42	-3.71	-54.4
47	38	-6303	107	300	0	-84	-2	6.28	6.28	9.42	9.42	-3.55	-52.3
49	38	-6472	154	328	0	-98	-81	6.28	6.28	9.42	9.42	-3.85	-54.4
50	38	-6191	69	300	0	-83	77	6.28	6.28	9.42	9.42	-3.68	-51.7
51	38	-6276	107	244	0	-57	-3	6.28	6.28	9.42	9.42	-3.42	-50.6

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	50	-7396	330	613	0	-300	-192	6.28	6.28	9.42	9.42	-5.32	-72.9
41	50	-6892	189	530	0	-248	27	6.28	6.28	9.42	9.42	-4.60	-66.2
42	50	-6811	189	362	0	-147	25	6.28	6.28	9.42	9.42	-4.10	-59.8
43	50	-7410	383	552	0	-271	-346	6.28	6.28	9.42	9.42	-6.74	-85.2
44	50	-6008	-40	417	0	-178	394	6.28	6.28	9.42	9.42	-6.58	-80.0
45	50	-6434	148	135	0	-16	16	6.28	6.28	9.42	9.42	-3.31	-49.5
46	50	-6376	123	346	0	-147	14	6.28	6.28	9.42	9.42	-3.88	-56.5
47	50	-6247	107	300	0	-122	11	6.28	6.28	9.42	9.42	-3.70	-54.1
49	50	-6416	154	328	0	-139	-62	6.28	6.28	9.42	9.42	-3.86	-56.3
50	50	-6135	69	300	0	-120	86	6.28	6.28	9.42	9.42	-3.74	-53.1
51	50	-6220	107	244	0	-88	11	6.28	6.28	9.42	9.42	-3.53	-51.9

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 121 NI 827 NF 263 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 25A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-10830	-273	1319	0	-300	-190	6.28	6.28	9.42	9.42	-6.95	-98.8
41	0	-9977	105	1077	0	-248	11	6.28	6.28	9.42	9.42	-6.15	-89.4
42	0	-9844	102	595	0	-147	10	6.28	6.28	9.42	9.42	-5.62	-82.6
43	0	-10920	-548	1204	0	-271	-329	6.28	6.28	9.42	9.42	-8.26	-108.9
44	0	-8502	739	740	0	-178	349	6.28	6.28	9.42	9.42	-7.29	-93.3
45	0	-9285	77	-2	0	-16	6	6.28	6.28	9.42	9.42	-4.74	-71.0
46	0	-9224	68	635	0	-147	6	6.28	6.28	9.42	9.42	-5.31	-78.0
47	0	-9035	59	525	0	-122	4	6.28	6.28	9.42	9.42	-5.10	-75.1
49	0	-9318	-67	606	0	-139	-63	6.28	6.28	9.42	9.42	-5.32	-78.2
50	0	-8834	190	513	0	-120	72	6.28	6.28	9.42	9.42	-4.99	-73.5
51	0	-8991	58	364	0	-88	4	6.28	6.28	9.42	9.42	-4.92	-72.8

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	12	-10772	-273	1319	0	-465	-225	6.28	6.28	9.42	9.42	-7.54	-107.8
41	12	-9921	105	1077	0	-383	25	6.28	6.28	9.42	9.42	-6.74	-96.7
42	12	-9788	102	595	0	-222	23	6.28	6.28	9.42	9.42	-5.93	-86.5
43	12	-10862	-548	1204	0	-421	-397	6.28	6.28	9.42	9.42	-8.87	-114.7
44	12	-8446	739	740	0	-270	441	6.28	6.28	9.42	9.42	-8.11	-101.4
45	12	-9229	77	-2	0	-16	15	6.28	6.28	9.42	9.42	-4.71	-70.5
46	12	-9168	68	635	0	-226	14	6.28	6.28	9.42	9.42	-5.64	-82.1
47	12	-8979	59	525	0	-187	12	6.28	6.28	9.42	9.42	-5.37	-78.4
49	12	-9262	-67	606	0	-214	-71	6.28	6.28	9.42	9.42	-5.64	-82.1
50	12	-8778	190	513	0	-184	96	6.28	6.28	9.42	9.42	-5.25	-76.7
51	12	-8935	58	364	0	-133	11	6.28	6.28	9.42	9.42	-5.10	-75.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	25	-10715	-273	1319	0	-630	-259	6.28	6.28	9.42	9.42	-8.26	-116.7
41	25	-9864	105	1077	0	-518	38	6.28	6.28	9.42	9.42	-7.32	-103.9
42	25	-9732	102	595	0	-296	36	6.28	6.28	9.42	9.42	-6.24	-90.3
43	25	-10805	-548	1204	0	-572	-466	6.28	6.28	9.42	9.42	-9.47	-120.6
44	25	-8390	739	740	0	-363	534	6.28	6.28	9.42	9.42	-9.01	-110.0
45	25	-9172	77	-2	0	-16	25	6.28	6.28	9.42	9.42	-4.68	-70.1
46	25	-9112	68	635	0	-306	23	6.28	6.28	9.42	9.42	-5.98	-86.2
47	25	-8922	59	525	0	-253	19	6.28	6.28	9.42	9.42	-5.64	-81.7
49	25	-9206	-67	606	0	-290	-80	6.28	6.28	9.42	9.42	-5.95	-86.0
50	25	-8722	190	513	0	-248	120	6.28	6.28	9.42	9.42	-5.52	-80.0
51	25	-8878	58	364	0	-179	18	6.28	6.28	9.42	9.42	-5.28	-77.2

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	38	-10658	-273	1319	0	-794	-293	6.28	6.28	9.42	9.42	-8.98	-125.7
41	38	-9808	105	1077	0	-652	51	6.28	6.28	9.42	9.42	-7.91	-111.2
42	38	-9675	102	595	0	-370	48	6.28	6.28	9.42	9.42	-6.55	-94.1
43	38	-10748	-548	1204	0	-722	-534	6.28	6.28	9.42	9.42	-10.07	-126.5
44	38	-8333	739	740	0	-455	626	6.28	6.28	9.42	9.42	-10.08	-119.7
45	38	-9116	77	-2	0	-15	34	6.28	6.28	9.42	9.42	-4.69	-69.6
46	38	-9055	68	635	0	-385	31	6.28	6.28	9.42	9.42	-6.31	-90.3
47	38	-8866	59	525	0	-318	26	6.28	6.28	9.42	9.42	-5.91	-85.0
49	38	-9149	-67	606	0	-366	-88	6.28	6.28	9.42	9.42	-6.27	-89.9
50	38	-8665	190	513	0	-312	144	6.28	6.28	9.42	9.42	-5.78	-83.2
51	38	-8822	58	364	0	-224	26	6.28	6.28	9.42	9.42	-5.46	-79.3

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	50	-10600	-273	1319	0	-959	-327	6.28	6.28	9.42	9.42	-9.71	-134.6
41	50	-9752	105	1077	0	-787	64	6.28	6.28	9.42	9.42	-8.49	-118.4
42	50	-9619	102	595	0	-445	61	6.28	6.28	9.42	9.42	-6.87	-97.9
43	50	-10690	-548	1204	0	-872	-603	6.28	6.28	9.42	9.42	-10.68	-132.5
44	50	-8277	739	740	0	-548	719	6.28	6.28	9.42	9.42	-11.29	-130.1
45	50	-9060	77	-2	0	-15	44	6.28	6.28	9.42	9.42	-4.75	-69.3
46	50	-8999	68	635	0	-465	40	6.28	6.28	9.42	9.42	-6.64	-94.4
47	50	-8810	59	525	0	-384	34	6.28	6.28	9.42	9.42	-6.18	-88.4
49	50	-9093	-67	606	0	-442	-97	6.28	6.28	9.42	9.42	-6.59	-93.8
50	50	-8609	190	513	0	-377	168	6.28	6.28	9.42	9.42	-6.05	-86.4
51	50	-8766	58	364	0	-270	33	6.28	6.28	9.42	9.42	-5.64	-81.5

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 122 NI 805 NF 830 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 24
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-3499	-21	597	0	-89	-33	6.28	6.28	9.42	9.42	-2.16	-31.5
41	0	-3458	24	493	0	-72	20	6.28	6.28	9.42	9.42	-2.07	-30.2
42	0	-3445	24	268	0	-47	21	6.28	6.28	9.42	9.42	-1.95	-28.7
43	0	-3417	-53	560	0	-89	-72	6.28	6.28	9.42	9.42	-2.31	-31.3
44	0	-3309	99	340	0	-46	111	6.28	6.28	9.42	9.42	-2.60	-34.0
45	0	-3327	22	12	0	-20	18	6.28	6.28	9.42	9.42	-1.77	-26.2
46	0	-3284	20	322	0	-56	15	6.28	6.28	9.42	9.42	-1.91	-28.0
47	0	-3240	19	279	0	-52	14	6.28	6.28	9.42	9.42	-1.87	-27.4
49	0	-3254	4	314	0	-57	-4	6.28	6.28	9.42	9.42	-1.90	-27.8
50	0	-3232	34	270	0	-49	33	6.28	6.28	9.42	9.42	-1.85	-27.2
51	0	-3236	19	204	0	-43	14	6.28	6.28	9.42	9.42	-1.83	-26.9

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	12	-3443	-21	597	0	-163	-36	6.28	6.28	9.42	9.42	-2.48	-35.3
41	12	-3402	24	493	0	-134	23	6.28	6.28	9.42	9.42	-2.32	-33.3
42	12	-3389	24	268	0	-81	24	6.28	6.28	9.42	9.42	-2.07	-30.2
43	12	-3361	-53	560	0	-159	-79	6.28	6.28	9.42	9.42	-2.42	-34.4
44	12	-3253	99	340	0	-89	123	6.28	6.28	9.42	9.42	-2.69	-34.7
45	12	-3271	22	12	0	-22	20	6.28	6.28	9.42	9.42	-1.76	-25.9
46	12	-3228	20	322	0	-96	18	6.28	6.28	9.42	9.42	-2.06	-29.8
47	12	-3184	19	279	0	-87	16	6.28	6.28	9.42	9.42	-2.00	-29.0
49	12	-3198	4	314	0	-96	-3	6.28	6.28	9.42	9.42	-2.05	-29.6
50	12	-3176	34	270	0	-82	37	6.28	6.28	9.42	9.42	-1.97	-28.7
51	12	-3180	19	204	0	-69	17	6.28	6.28	9.42	9.42	-1.91	-27.9

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	25	-3386	-21	597	0	-238	-39	6.28	6.28	9.42	9.42	-2.79	-39.1
41	25	-3346	24	493	0	-196	26	6.28	6.28	9.42	9.42	-2.57	-36.4
42	25	-3332	24	268	0	-114	27	6.28	6.28	9.42	9.42	-2.20	-31.7
43	25	-3304	-53	560	0	-229	-86	6.28	6.28	9.42	9.42	-2.71	-38.0
44	25	-3196	99	340	0	-131	135	6.28	6.28	9.42	9.42	-2.78	-35.5
45	25	-3214	22	12	0	-23	23	6.28	6.28	9.42	9.42	-1.76	-25.6
46	25	-3172	20	322	0	-136	20	6.28	6.28	9.42	9.42	-2.22	-31.7
47	25	-3128	19	279	0	-122	19	6.28	6.28	9.42	9.42	-2.13	-30.5
49	25	-3142	4	314	0	-136	-3	6.28	6.28	9.42	9.42	-2.20	-31.4
50	25	-3120	34	270	0	-116	41	6.28	6.28	9.42	9.42	-2.10	-30.1
51	25	-3124	19	204	0	-94	19	6.28	6.28	9.42	9.42	-2.00	-28.9

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	38	-3330	-21	597	0	-313	-41	6.28	6.28	9.42	9.42	-3.10	-43.0
41	38	-3289	24	493	0	-257	29	6.28	6.28	9.42	9.42	-2.83	-39.5
42	38	-3276	24	268	0	-148	30	6.28	6.28	9.42	9.42	-2.32	-33.1
43	38	-3248	-53	560	0	-299	-92	6.28	6.28	9.42	9.42	-3.00	-41.6
44	38	-3140	99	340	0	-174	148	6.28	6.28	9.42	9.42	-2.86	-36.2
45	38	-3158	22	12	0	-25	26	6.28	6.28	9.42	9.42	-1.75	-25.2
46	38	-3115	20	322	0	-177	23	6.28	6.28	9.42	9.42	-2.37	-33.6
47	38	-3071	19	279	0	-156	21	6.28	6.28	9.42	9.42	-2.26	-32.1
49	38	-3085	4	314	0	-175	-2	6.28	6.28	9.42	9.42	-2.35	-33.2
50	38	-3063	34	270	0	-150	46	6.28	6.28	9.42	9.42	-2.22	-31.6
51	38	-3067	19	204	0	-120	21	6.28	6.28	9.42	9.42	-2.09	-30.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	50	-3274	-21	597	0	-387	-44	6.28	6.28	9.42	9.42	-3.42	-46.8
41	50	-3233	24	493	0	-319	32	6.28	6.28	9.42	9.42	-3.08	-42.6
42	50	-3220	24	268	0	-181	33	6.28	6.28	9.42	9.42	-2.45	-34.6
43	50	-3192	-53	560	0	-369	-99	6.28	6.28	9.42	9.42	-3.29	-45.2
44	50	-3084	99	340	0	-216	160	6.28	6.28	9.42	9.42	-2.95	-36.9
45	50	-3102	22	12	0	-26	28	6.28	6.28	9.42	9.42	-1.75	-25.0
46	50	-3059	20	322	0	-217	25	6.28	6.28	9.42	9.42	-2.53	-35.4
47	50	-3015	19	279	0	-191	23	6.28	6.28	9.42	9.42	-2.39	-33.7
49	50	-3029	4	314	0	-214	-2	6.28	6.28	9.42	9.42	-2.50	-35.1
50	50	-3007	34	270	0	-184	50	6.28	6.28	9.42	9.42	-2.35	-33.1
51	50	-3011	19	204	0	-146	24	6.28	6.28	9.42	9.42	-2.18	-31.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 123 NI 830 NF 122 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 24A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-5139	-81	1702	0	-387	-36	6.28	6.28	9.42	9.42	-4.35	-60.9
41	0	-5099	86	1400	0	-319	28	6.28	6.28	9.42	9.42	-4.02	-56.6
42	0	-5084	86	813	0	-181	29	6.28	6.28	9.42	9.42	-3.38	-48.7
43	0	-4998	-202	1634	0	-369	-83	6.28	6.28	9.42	9.42	-4.20	-58.8
44	0	-4898	365	945	0	-216	137	6.28	6.28	9.42	9.42	-3.61	-49.3
45	0	-4907	76	153	0	-26	25	6.28	6.28	9.42	9.42	-2.59	-38.5
46	0	-4832	69	970	0	-217	22	6.28	6.28	9.42	9.42	-3.42	-48.8
47	0	-4765	65	862	0	-191	21	6.28	6.28	9.42	9.42	-3.27	-46.9
49	0	-4778	10	963	0	-214	-1	6.28	6.28	9.42	9.42	-3.38	-48.3
50	0	-4758	123	825	0	-184	43	6.28	6.28	9.42	9.42	-3.23	-46.4
51	0	-4760	65	667	0	-146	21	6.28	6.28	9.42	9.42	-3.06	-44.2

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	12	-5083	-81	1702	0	-600	-47	6.28	6.28	9.42	9.42	-5.30	-72.6
41	12	-5043	86	1400	0	-494	39	6.28	6.28	9.42	9.42	-4.79	-66.2
42	12	-5028	86	813	0	-283	40	6.28	6.28	9.42	9.42	-3.82	-54.1
43	12	-4942	-202	1634	0	-574	-109	6.28	6.28	9.42	9.42	-5.10	-70.0
44	12	-4842	365	945	0	-335	183	6.28	6.28	9.42	9.42	-4.00	-55.6
45	12	-4851	76	153	0	-45	35	6.28	6.28	9.42	9.42	-2.65	-39.2
46	12	-4776	69	970	0	-338	31	6.28	6.28	9.42	9.42	-3.94	-55.3
47	12	-4709	65	862	0	-299	29	6.28	6.28	9.42	9.42	-3.73	-52.6
49	12	-4722	10	963	0	-335	0	6.28	6.28	9.42	9.42	-3.90	-54.7
50	12	-4702	123	825	0	-287	59	6.28	6.28	9.42	9.42	-3.67	-51.8
51	12	-4704	65	667	0	-229	29	6.28	6.28	9.42	9.42	-3.41	-48.5

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	25	-5026	-81	1702	0	-813	-57	6.28	6.28	9.42	9.42	-6.46	-86.6
41	25	-4986	86	1400	0	-669	50	6.28	6.28	9.42	9.42	-5.61	-76.3
42	25	-4972	86	813	0	-385	50	6.28	6.28	9.42	9.42	-4.25	-59.4
43	25	-4886	-202	1634	0	-778	-134	6.28	6.28	9.42	9.42	-6.20	-83.3
44	25	-4786	365	945	0	-453	228	6.28	6.28	9.42	9.42	-4.47	-61.9
45	25	-4794	76	153	0	-64	44	6.28	6.28	9.42	9.42	-2.71	-39.8
46	25	-4720	69	970	0	-459	40	6.28	6.28	9.42	9.42	-4.47	-61.8
47	25	-4652	65	862	0	-407	37	6.28	6.28	9.42	9.42	-4.20	-58.3
49	25	-4666	10	963	0	-455	2	6.28	6.28	9.42	9.42	-4.42	-61.1
50	25	-4646	123	825	0	-390	74	6.28	6.28	9.42	9.42	-4.11	-57.3
51	25	-4648	65	667	0	-312	37	6.28	6.28	9.42	9.42	-3.76	-52.9

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	38	-4970	-81	1702	0	-1025	-67	6.28	6.28	9.42	9.42	-7.91	-103.4
41	38	-4930	86	1400	0	-844	61	6.28	6.28	9.42	9.42	-6.63	-88.5
42	38	-4915	86	813	0	-486	61	6.28	6.28	9.42	9.42	-4.69	-64.8
43	38	-4829	-202	1634	0	-983	-159	6.28	6.28	9.42	9.42	-7.58	-99.3
44	38	-4729	365	945	0	-571	274	6.28	6.28	9.42	9.42	-4.99	-68.3
45	38	-4738	76	153	0	-83	54	6.28	6.28	9.42	9.42	-2.77	-40.5
46	38	-4663	69	970	0	-581	48	6.28	6.28	9.42	9.42	-5.01	-68.4
47	38	-4596	65	862	0	-515	45	6.28	6.28	9.42	9.42	-4.66	-64.0
49	38	-4609	10	963	0	-575	3	6.28	6.28	9.42	9.42	-4.96	-67.7
50	38	-4589	123	825	0	-493	89	6.28	6.28	9.42	9.42	-4.56	-62.7
51	38	-4591	65	667	0	-396	45	6.28	6.28	9.42	9.42	-4.11	-57.2

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	50	-4914	-81	1702	0	-1238	-77	6.28	6.28	9.42	9.42	-9.54	-121.5
41	50	-4874	86	1400	0	-1019	71	6.28	6.28	9.42	9.42	-7.85	-102.6
42	50	-4859	86	813	0	-588	72	6.28	6.28	9.42	9.42	-5.13	-70.3
43	50	-4773	-202	1634	0	-1187	-185	6.28	6.28	9.42	9.42	-9.14	-116.7
44	50	-4673	365	945	0	-689	320	6.28	6.28	9.42	9.42	-5.60	-75.7
45	50	-4682	76	153	0	-102	63	6.28	6.28	9.42	9.42	-2.83	-41.2
46	50	-4607	69	970	0	-702	57	6.28	6.28	9.42	9.42	-5.65	-76.2
47	50	-4540	65	862	0	-623	53	6.28	6.28	9.42	9.42	-5.18	-70.3
49	50	-4553	10	963	0	-696	4	6.28	6.28	9.42	9.42	-5.60	-75.5
50	50	-4533	123	825	0	-596	105	6.28	6.28	9.42	9.42	-5.03	-68.6
51	50	-4535	65	667	0	-479	53	6.28	6.28	9.42	9.42	-4.46	-61.5

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 124 NI 806 NF 833 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 23
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-3358	-217	689	0	-233	53	6.28	6.28	9.42	9.42	-2.75	-38.6
41	0	-3215	-153	638	0	-209	32	6.28	6.28	9.42	9.42	-2.57	-36.2
42	0	-3031	-152	475	0	-164	33	6.28	6.28	9.42	9.42	-2.27	-32.2
43	0	-3329	-256	641	0	-228	65	6.28	6.28	9.42	9.42	-2.71	-38.1
44	0	-2930	-44	555	0	-167	-2	6.28	6.28	9.42	9.42	-2.23	-31.6
45	0	-2784	-149	285	0	-112	32	6.28	6.28	9.42	9.42	-1.91	-27.4
46	0	-3015	-148	506	0	-176	30	6.28	6.28	9.42	9.42	-2.32	-32.7
47	0	-2965	-147	474	0	-167	30	6.28	6.28	9.42	9.42	-2.25	-31.9
49	0	-3013	-169	491	0	-175	37	6.28	6.28	9.42	9.42	-2.31	-32.7
50	0	-2933	-126	474	0	-163	23	6.28	6.28	9.42	9.42	-2.22	-31.4
51	0	-2904	-147	419	0	-152	30	6.28	6.28	9.42	9.42	-2.15	-30.6

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	12	-3302	-217	689	0	-320	26	6.28	6.28	9.42	9.42	-3.12	-43.1
41	12	-3159	-153	638	0	-289	13	6.28	6.28	9.42	9.42	-2.91	-40.3
42	12	-2975	-152	475	0	-223	14	6.28	6.28	9.42	9.42	-2.51	-35.2

43	12	-3273	-256	641	0	-308	33	6.28	6.28	9.42	9.42	-3.05	-42.3
44	12	-2874	-44	555	0	-236	-7	6.28	6.28	9.42	9.42	-2.52	-35.2
45	12	-2728	-149	285	0	-147	13	6.28	6.28	9.42	9.42	-2.04	-29.0
46	12	-2959	-148	506	0	-239	12	6.28	6.28	9.42	9.42	-2.58	-35.9
47	12	-2909	-147	474	0	-226	11	6.28	6.28	9.42	9.42	-2.49	-34.8
49	12	-2957	-169	491	0	-236	15	6.28	6.28	9.42	9.42	-2.56	-35.8
50	12	-2877	-126	474	0	-222	7	6.28	6.28	9.42	9.42	-2.46	-34.4
51	12	-2848	-147	419	0	-204	12	6.28	6.28	9.42	9.42	-2.36	-33.1

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	25	-3246	-217	689	0	-406	-2	6.28	6.28	9.42	9.42	-3.49	-47.7
41	25	-3102	-153	638	0	-369	-6	6.28	6.28	9.42	9.42	-3.25	-44.5
42	25	-2918	-152	475	0	-282	-5	6.28	6.28	9.42	9.42	-2.76	-38.1
43	25	-3216	-256	641	0	-388	1	6.28	6.28	9.42	9.42	-3.39	-46.5
44	25	-2818	-44	555	0	-306	-13	6.28	6.28	9.42	9.42	-2.81	-38.7
45	25	-2672	-149	285	0	-183	-5	6.28	6.28	9.42	9.42	-2.18	-30.6
46	25	-2902	-148	506	0	-302	-7	6.28	6.28	9.42	9.42	-2.84	-39.1
47	25	-2852	-147	474	0	-286	-7	6.28	6.28	9.42	9.42	-2.74	-37.8
49	25	-2900	-169	491	0	-298	-6	6.28	6.28	9.42	9.42	-2.82	-38.9
50	25	-2820	-126	474	0	-281	-8	6.28	6.28	9.42	9.42	-2.70	-37.3
51	25	-2792	-147	419	0	-257	-7	6.28	6.28	9.42	9.42	-2.57	-35.7

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	38	-3189	-217	689	0	-492	-29	6.28	6.28	9.42	9.42	-3.95	-53.2
41	38	-3046	-153	638	0	-449	-25	6.28	6.28	9.42	9.42	-3.65	-49.3
42	38	-2862	-152	475	0	-342	-24	6.28	6.28	9.42	9.42	-3.00	-41.1
43	38	-3160	-256	641	0	-469	-31	6.28	6.28	9.42	9.42	-3.80	-51.4
44	38	-2761	-44	555	0	-375	-18	6.28	6.28	9.42	9.42	-3.13	-42.5
45	38	-2615	-149	285	0	-219	-24	6.28	6.28	9.42	9.42	-2.31	-32.2
46	38	-2846	-148	506	0	-365	-25	6.28	6.28	9.42	9.42	-3.11	-42.5
47	38	-2796	-147	474	0	-345	-25	6.28	6.28	9.42	9.42	-2.99	-40.8
49	38	-2844	-169	491	0	-359	-27	6.28	6.28	9.42	9.42	-3.08	-42.1
50	38	-2764	-126	474	0	-340	-24	6.28	6.28	9.42	9.42	-2.95	-40.3
51	38	-2735	-147	419	0	-309	-25	6.28	6.28	9.42	9.42	-2.79	-38.3

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	50	-3133	-217	689	0	-578	-56	6.28	6.28	9.42	9.42	-4.50	-59.5
41	50	-2990	-153	638	0	-528	-44	6.28	6.28	9.42	9.42	-4.13	-55.0
42	50	-2806	-152	475	0	-401	-43	6.28	6.28	9.42	9.42	-3.29	-44.6
43	50	-3104	-256	641	0	-549	-63	6.28	6.28	9.42	9.42	-4.29	-57.1
44	50	-2705	-44	555	0	-445	-24	6.28	6.28	9.42	9.42	-3.52	-47.1
45	50	-2559	-149	285	0	-254	-42	6.28	6.28	9.42	9.42	-2.45	-33.8
46	50	-2790	-148	506	0	-429	-44	6.28	6.28	9.42	9.42	-3.45	-46.4
47	50	-2740	-147	474	0	-404	-44	6.28	6.28	9.42	9.42	-3.28	-44.4
49	50	-2788	-169	491	0	-420	-48	6.28	6.28	9.42	9.42	-3.40	-45.8
50	50	-2708	-126	474	0	-400	-40	6.28	6.28	9.42	9.42	-3.25	-43.9
51	50	-2679	-147	419	0	-362	-44	6.28	6.28	9.42	9.42	-3.02	-41.1

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 125 NI 833 NF 209 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 23A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	--												
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-4201	-42	1041	0	-679	-78	6.28	6.28	9.42	9.42	-5.39	-72.4
41	0	-4041	79	922	0	-612	-57	6.28	6.28	9.42	9.42	-4.94	-66.6
42	0	-3880	64	617	0	-461	-57	6.28	6.28	9.42	9.42	-4.06	-55.6
43	0	-4167	-136	977	0	-649	-91	6.28	6.28	9.42	9.42	-5.20	-70.0
44	0	-3707	280	730	0	-500	-21	6.28	6.28	9.42	9.42	-4.18	-56.8
45	0	-3632	40	272	0	-287	-56	6.28	6.28	9.42	9.42	-3.13	-43.7
46	0	-3815	57	693	0	-493	-55	6.28	6.28	9.42	9.42	-4.19	-57.1
47	0	-3759	52	636	0	-463	-54	6.28	6.28	9.42	9.42	-4.01	-54.9
49	0	-3812	11	676	0	-485	-61	6.28	6.28	9.42	9.42	-4.15	-56.6
50	0	-3721	95	626	0	-455	-48	6.28	6.28	9.42	9.42	-3.96	-54.1
51	0	-3706	46	534	0	-413	-55	6.28	6.28	9.42	9.42	-3.75	-51.5

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	12	-4145	-42	1041	0	-809	-83	6.28	6.28	9.42	9.42	-6.26	-82.4
41	12	-3985	79	922	0	-727	-47	6.28	6.28	9.42	9.42	-5.66	-75.1
42	12	-3824	64	617	0	-539	-49	6.28	6.28	9.42	9.42	-4.44	-60.2
43	12	-4111	-136	977	0	-771	-108	6.28	6.28	9.42	9.42	-5.99	-79.2
44	12	-3651	280	730	0	-591	14	6.28	6.28	9.42	9.42	-4.69	-62.9
45	12	-3576	40	272	0	-321	-52	6.28	6.28	9.42	9.42	-3.26	-45.3
46	12	-3759	57	693	0	-579	-48	6.28	6.28	9.42	9.42	-4.65	-62.7
47	12	-3703	52	636	0	-542	-48	6.28	6.28	9.42	9.42	-4.42	-59.7
49	12	-3756	11	676	0	-570	-60	6.28	6.28	9.42	9.42	-4.59	-62.0
50	12	-3665	95	626	0	-534	-36	6.28	6.28	9.42	9.42	-4.35	-58.9
51	12	-3650	46	534	0	-480	-49	6.28	6.28	9.42	9.42	-4.05	-55.2

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	25	-4088	-42	1041	0	-939	-88	6.28	6.28	9.42	9.42	-7.23	-93.2
41	25	-3928	79	922	0	-842	-37	6.28	6.28	9.42	9.42	-6.49	-84.4
42	25	-3768	64	617	0	-616	-41	6.28	6.28	9.42	9.42	-4.88	-65.4
43	25	-4054	-136	977	0	-894	-125	6.28	6.28	9.42	9.42	-6.88	-89.2
44	25	-3594	280	730	0	-682	49	6.28	6.28	9.42	9.42	-5.29	-69.8
45	25	-3520	40	272	0	-355	-47	6.28	6.28	9.42	9.42	-3.39	-46.8
46	25	-3702	57	693	0	-666	-41	6.28	6.28	9.42	9.42	-5.20	-69.0
47	25	-3646	52	636	0	-622	-42	6.28	6.28	9.42	9.42	-4.89	-65.3
49	25	-3700	11	676	0	-654	-59	6.28	6.28	9.42	9.42	-5.12	-68.0
50	25	-3608	95	626	0	-612	-24	6.28	6.28	9.42	9.42	-4.82	-64.3
51	25	-3594	46	534	0	-546	-43	6.28	6.28	9.42	9.42	-4.40	-59.4

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	38	-4032	-42	1041	0	-1069	-93	6.28	6.28	9.42	9.42	-8.25	-104.3
41	38	-3872	79	922	0	-958	-27	6.28	6.28	9.42	9.42	-7.38	-94.2
42	38	-3711	64	617	0	-693	-33	6.28	6.28	9.42	9.42	-5.38	-71.2
43	38	-3998	-136	977	0	-1016	-142	6.28	6.28	9.42	9.42	-7.83	-99.6

44	38	-3538	280	730	0	-773	84	6.28	6.28	9.42	9.42	-5.95	-77.3
45	38	-3463	40	272	0	-389	-42	6.28	6.28	9.42	9.42	-3.51	-48.3
46	38	-3646	57	693	0	-753	-33	6.28	6.28	9.42	9.42	-5.80	-75.9
47	38	-3590	52	636	0	-701	-35	6.28	6.28	9.42	9.42	-5.43	-71.4
49	38	-3643	11	676	0	-739	-57	6.28	6.28	9.42	9.42	-5.70	-74.7
50	38	-3552	95	626	0	-690	-12	6.28	6.28	9.42	9.42	-5.34	-70.4
51	38	-3537	46	534	0	-613	-37	6.28	6.28	9.42	9.42	-4.81	-64.1

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	50	-3976	-42	1041	0	-1199	-99	6.28	6.28	9.42	9.42	-9.29	125.1
41	50	-3816	79	922	0	-1073	-17	6.28	6.28	9.42	9.42	-8.29	-104.0
42	50	-3655	64	617	0	-770	-25	6.28	6.28	9.42	9.42	-5.93	-77.4
43	50	-3942	-136	977	0	-1138	-159	6.28	6.28	9.42	9.42	-8.80	110.9
44	50	-3482	280	730	0	-864	119	6.28	6.28	9.42	9.42	-6.66	-85.0
45	50	-3407	40	272	0	-423	-37	6.28	6.28	9.42	9.42	-3.65	-49.9
46	50	-3590	57	693	0	-839	-26	6.28	6.28	9.42	9.42	-6.46	-83.1
47	50	-3534	52	636	0	-781	-29	6.28	6.28	9.42	9.42	-6.01	-77.9
49	50	-3587	11	676	0	-823	-56	6.28	6.28	9.42	9.42	-6.34	-81.7
50	50	-3496	95	626	0	-768	-0	6.28	6.28	9.42	9.42	-5.92	-76.8
51	50	-3481	46	534	0	-680	-31	6.28	6.28	9.42	9.42	-5.26	-69.3

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

L E G E N D A

Prima asta	Ultima asta	Nome disegno	Descrizione disegno
1	125	D2403a0002_IP1.YPI	

Delta Ingegneria srl
via Artemide 3 92100 Agrigento - tel 0922 402212
email - g.ferraro@deltaingegneria.it

Lavoro: **D2403a** Intestazione lavoro: **Palestra Campobello**
Elemento: **PILASTRO** Gruppo: **2** Tabella: **Tabella pilastri**
Descrizione: **Pilastri**
Rck: **350.00** daN/cm² fyk: **4580.0** daN/cm² Condizioni ambientali: **Ordinaria**
Copriferro di calcolo: **5.0** cm Copriferro di disegno: **4.0** cm
Diametro staffe: **8** mm Numero braccia: **2**
ρ min.: **1.000** %

ASTA NUM. 1 NI 32 NF 26 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 32C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm²				daN/cm²	
40	0	-1225	1008	185	0	868	-985	6.28	6.28	9.42	9.42	-15.43	413.2
41	0	-910	942	402	0	977	-1078	6.28	6.28	9.42	9.42	-16.82	474.7
42	0	-496	963	773	0	1173	-1094	6.28	6.28	9.42	9.42	-16.98	504.1
43	0	-1084	1050	72	0	810	-956	6.28	6.28	9.42	9.42	-14.97	406.8
44	0	-482	834	760	0	1156	-1233	6.28	6.28	9.42	9.42	-19.13	572.2
45	0	130	974	1052	0	1318	-1138	6.28	6.28	9.42	9.42	-17.52	558.6
46	0	-349	936	455	0	999	-1133	6.28	6.28	9.42	9.42	-17.56	530.7
47	0	-209	934	468	0	1005	-1147	6.28	6.28	9.42	9.42	-17.74	544.9
49	0	-314	957	395	0	969	-1115	6.28	6.28	9.42	9.42	-17.27	523.9
50	0	-193	914	533	0	1038	-1171	6.28	6.28	9.42	9.42	-18.11	557.4
51	0	-71	942	591	0	1070	-1152	6.28	6.28	9.42	9.42	-17.79	554.7
apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)													
40	83	-854	939	185	0	716	-181	6.28	6.28	9.42	9.42	-5.51	165.3
41	83	-539	942	402	0	645	-301	6.28	6.28	9.42	9.42	-4.91	165.1
42	83	-125	963	620	0	598	-300	6.28	6.28	9.42	9.42	-4.65	180.3
43	83	-713	935	72	0	750	-138	6.28	6.28	9.42	9.42	-5.73	185.9
44	83	-111	949	760	0	529	-497	6.28	6.28	9.42	9.42	-7.70	235.3
45	83	501	974	798	0	554	-335	6.28	6.28	9.42	9.42	-5.02	214.0
46	83	22	936	455	0	624	-361	6.28	6.28	9.42	9.42	-5.56	199.4
47	83	162	934	468	0	619	-376	6.28	6.28	9.42	9.42	-5.76	208.3
49	83	57	934	395	0	642	-335	6.28	6.28	9.42	9.42	-5.16	207.9
50	83	178	937	533	0	598	-408	6.28	6.28	9.42	9.42	-6.24	207.1
51	83	300	942	541	0	603	-375	6.28	6.28	9.42	9.42	-5.71	213.8
apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)													
40	165	-482	871	185	0	564	566	6.28	6.28	9.42	9.42	-8.83	248.8
41	165	-167	942	402	0	313	476	6.28	6.28	9.42	9.42	-7.37	221.6
42	165	246	963	468	0	150	494	6.28	6.28	9.42	9.42	-7.57	252.8
43	165	-342	820	72	0	690	586	6.28	6.28	9.42	9.42	-9.11	266.0
44	165	261	1064	760	0	-98	333	6.28	6.28	9.42	9.42	-5.06	175.3
45	165	872	974	544	0	0	468	6.28	6.28	9.42	9.42	-6.96	273.9
46	165	393	936	455	0	249	411	6.28	6.28	9.42	9.42	-6.23	220.3
47	165	534	934	468	0	233	395	6.28	6.28	9.42	9.42	-5.94	220.2
49	165	429	911	395	0	316	425	6.28	6.28	9.42	9.42	-6.45	229.2
50	165	549	959	533	0	159	375	6.28	6.28	9.42	9.42	-5.62	211.2
51	165	671	942	490	0	178	402	6.28	6.28	9.42	9.42	-6.00	230.8
apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)													
40	248	-111	802	185	0	412	1256	6.28	6.28	9.42	9.42	-19.40	602.8
41	248	204	942	402	0	-18	1252	6.28	6.28	9.42	9.42	-19.27	617.9
42	248	617	963	316	0	-173	1289	6.28	6.28	9.42	9.42	-19.72	657.7
43	248	30	706	72	0	631	1215	6.28	6.28	9.42	9.42	-18.74	590.7
44	248	632	1178	760	0	-724	1258	6.28	6.28	9.42	9.42	-19.24	643.3
45	248	1244	974	291	0	-344	1271	6.28	6.28	9.42	9.42	-19.27	682.8
46	248	765	936	455	0	-126	1183	6.28	6.28	9.42	9.42	-18.05	614.3
47	248	905	934	468	0	-153	1166	6.28	6.28	9.42	9.42	-17.75	613.6
49	248	800	888	395	0	-10	1167	6.28	6.28	9.42	9.42	-17.80	608.5
50	248	921	982	533	0	-281	1176	6.28	6.28	9.42	9.42	-17.90	619.3
51	248	1043	942	439	0	-205	1178	6.28	6.28	9.42	9.42	-17.90	627.0
apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)													
40	330	260	733	185	0	259	1889	6.28	6.28	9.42	9.42	-29.08	929.6
41	330	575	942	402	0	-350	2029	6.28	6.28	9.42	9.42	-31.16	1014.2
42	330	989	963	163	0	-371	2083	6.28	6.28	9.42	9.42	-31.88	1062.5
43	330	401	591	72	0	571	1750	6.28	6.28	9.42	9.42	-26.90	869.7
44	330	1003	1293	760	0	-1351	2277	6.28	6.28	9.42	9.42	-34.87	1157.3
45	330	1615	974	37	0	-479	2074	6.28	6.28	9.42	9.42	-31.57	1091.8
46	330	1136	936	455	0	-502	1955	6.28	6.28	9.42	9.42	-29.87	1008.4
47	330	1276	934	468	0	-539	1937	6.28	6.28	9.42	9.42	-29.55	1007.2
49	330	1171	865	395	0	-336	1890	6.28	6.28	9.42	9.42	-28.85	978.7
50	330	1292	1005	533	0	-721	1996	6.28	6.28	9.42	9.42	-30.46	1036.6
51	330	1414	942	388	0	-546	1955	6.28	6.28	9.42	9.42	-29.79	1023.3
apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)													

ASTA NUM. 2 NI 33 NF 32 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 32B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm²				daN/cm²	

40	0	-7177	150	167	0	-10	-123	6.28	6.28	9.42	9.42	-4.58	-63.0
41	0	-6882	10	171	0	40	-17	6.28	6.28	9.42	9.42	-3.64	-54.2
42	0	-6526	-4	656	0	515	15	6.28	6.28	9.42	9.42	-5.63	-78.6
43	0	-7007	265	175	0	-2	-232	6.28	6.28	9.42	9.42	-5.50	-71.8
44	0	-6491	-226	177	0	122	166	6.28	6.28	9.42	9.42	-4.65	-62.0
45	0	-5921	9	989	0	872	-2	6.28	6.28	9.42	9.42	-7.09	-95.9
46	0	-6294	47	186	0	105	-79	6.28	6.28	9.42	9.42	-3.75	-53.4
47	0	-6147	56	190	0	121	-94	6.28	6.28	9.42	9.42	-3.82	-53.3
49	0	-6246	102	189	0	104	-130	6.28	6.28	9.42	9.42	-4.19	-56.9
50	0	-6143	4	190	0	129	-50	6.28	6.28	9.42	9.42	-3.68	-53.7
51	0	-6029	51	352	0	279	-83	6.28	6.28	9.42	9.42	-4.31	-61.4

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	110	-6682	80	167	0	-194	3	6.28	6.28	9.42	9.42	-4.24	-61.5
41	110	-6387	10	171	0	-148	-6	6.28	6.28	9.42	9.42	-3.89	-56.6
42	110	-6031	-4	453	0	-95	11	6.28	6.28	9.42	9.42	-3.47	-50.9
43	110	-6512	150	175	0	-195	-4	6.28	6.28	9.42	9.42	-4.16	-60.2
44	110	-5996	-110	177	0	-73	-19	6.28	6.28	9.42	9.42	-3.35	-49.4
45	110	-5426	9	651	0	-30	8	6.28	6.28	9.42	9.42	-2.86	-42.6
46	110	-5799	47	186	0	-100	-27	6.28	6.28	9.42	9.42	-3.37	-49.5
47	110	-5652	56	190	0	-88	-33	6.28	6.28	9.42	9.42	-3.25	-47.7
49	110	-5751	79	189	0	-104	-29	6.28	6.28	9.42	9.42	-3.37	-49.3
50	110	-5648	27	190	0	-79	-32	6.28	6.28	9.42	9.42	-3.20	-47.1
51	110	-5534	51	284	0	-71	-27	6.28	6.28	9.42	9.42	-3.11	-45.8

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	220	-6187	11	167	0	-378	54	6.28	6.28	9.42	9.42	-4.83	-68.2
41	220	-5892	10	171	0	-336	6	6.28	6.28	9.42	9.42	-4.49	-63.6
42	220	-5536	-4	250	0	-481	6	6.28	6.28	9.42	9.42	-4.98	-69.2
43	220	-6017	34	175	0	-387	97	6.28	6.28	9.42	9.42	-4.79	-67.4
44	220	-5501	5	177	0	-268	-76	6.28	6.28	9.42	9.42	-3.99	-56.8
45	220	-4931	9	312	0	-559	18	6.28	6.28	9.42	9.42	-5.03	-69.1
46	220	-5304	47	186	0	-306	24	6.28	6.28	9.42	9.42	-4.06	-57.4
47	220	-5157	56	190	0	-298	29	6.28	6.28	9.42	9.42	-3.95	-55.9
49	220	-5256	56	189	0	-312	45	6.28	6.28	9.42	9.42	-4.07	-57.4
50	220	-5153	50	190	0	-288	10	6.28	6.28	9.42	9.42	-3.91	-55.3
51	220	-5039	51	217	0	-346	29	6.28	6.28	9.42	9.42	-4.11	-57.8

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	330	-5692	-58	167	0	-562	28	6.28	6.28	9.42	9.42	-5.42	-75.0
41	330	-5397	10	171	0	-524	17	6.28	6.28	9.42	9.42	-5.10	-70.6
42	330	-5041	-4	47	0	-644	2	6.28	6.28	9.42	9.42	-5.50	-75.0
43	330	-5522	-81	175	0	-579	71	6.28	6.28	9.42	9.42	-5.42	-74.7
44	330	-5006	121	177	0	-463	-7	6.28	6.28	9.42	9.42	-4.63	-64.1
45	330	-4436	9	-26	0	-716	28	6.28	6.28	9.42	9.42	-5.69	-76.4
46	330	-4809	47	186	0	-511	76	6.28	6.28	9.42	9.42	-4.75	-65.4
47	330	-4662	56	190	0	-507	91	6.28	6.28	9.42	9.42	-4.66	-64.1
49	330	-4761	33	189	0	-520	94	6.28	6.28	9.42	9.42	-4.77	-65.6
50	330	-4658	74	190	0	-497	79	6.28	6.28	9.42	9.42	-4.61	-63.5
51	330	-4544	51	149	0	-547	86	6.28	6.28	9.42	9.42	-4.79	-65.6

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	440	-5197	-128	167	0	-746	-75	6.28	6.28	9.42	9.42	-6.11	-82.7
41	440	-4902	10	171	0	-712	28	6.28	6.28	9.42	9.42	-5.81	-78.6
42	440	-4546	-4	-157	0	-584	-3	6.28	6.28	9.42	9.42	-4.97	-67.8
43	440	-5027	-197	175	0	-771	-81	6.28	6.28	9.42	9.42	-6.20	-83.6
44	440	-4511	236	177	0	-657	189	6.28	6.28	9.42	9.42	-5.36	-72.5
45	440	-3941	9	-365	0	-501	38	6.28	6.28	9.42	9.42	-4.28	-58.5
46	440	-4314	47	186	0	-716	128	6.28	6.28	9.42	9.42	-5.66	-75.7
47	440	-4167	56	190	0	-717	153	6.28	6.28	9.42	9.42	-5.63	-75.1
49	440	-4266	10	189	0	-728	118	6.28	6.28	9.42	9.42	-5.72	-76.4
50	440	-4163	97	190	0	-705	172	6.28	6.28	9.42	9.42	-5.55	-74.2
51	440	-4049	51	81	0	-674	142	6.28	6.28	9.42	9.42	-5.32	-71.2

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 3 NI 27 NF 25 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 7C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	--												
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	4909	-563	794	0	1160	1030	6.28	6.28	9.42	9.42	-13.88	768.9
41	0	4713	-758	691	0	1076	1053	6.28	6.28	9.42	9.42	-14.37	768.9
42	0	5333	-775	1094	0	1198	1064	6.28	6.28	9.42	9.42	-14.18	809.0
43	0	4945	-443	838	0	1221	1043	6.28	6.28	9.42	9.42	-14.07	780.4
44	0	4331	-1089	520	0	934	1092	6.28	6.28	9.42	9.42	-15.20	766.2
45	0	5653	-796	1337	0	1284	1099	6.28	6.28	9.42	9.42	-14.56	857.8
46	0	4562	-774	651	0	1083	1096	6.28	6.28	9.42	9.42	-15.14	781.1
47	0	4524	-777	641	0	1085	1107	6.28	6.28	9.42	9.42	-15.34	784.2
49	0	4589	-712	676	0	1113	1100	6.28	6.28	9.42	9.42	-15.19	784.5
50	0	4466	-842	612	0	1056	1110	6.28	6.28	9.42	9.42	-15.42	782.4
51	0	4731	-783	775	0	1126	1111	6.28	6.28	9.42	9.42	-15.29	797.7

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	83	5280	-689	794	0	505	513	6.28	6.28	9.42	9.42	-4.49	580.9
41	83	5084	-758	691	0	506	427	6.28	6.28	9.42	9.42	-2.82	565.7
42	83	5704	-775	942	0	359	424	6.28	6.28	9.42	9.42	-1.68	568.1
43	83	5316	-652	838	0	529	591	6.28	6.28	9.42	9.42	-6.00	591.5
44	83	4702	-879	520	0	505	280	6.28	6.28	9.42	9.42	0.00	534.9
45	83	6024	-796	1083	0	286	442	6.28	6.28	9.42	9.42	-1.59	570.4
46	83	4933	-774	651	0	546	458	6.28	6.28	9.42	9.42	-3.72	566.4
47	83	4895	-777	641	0	556	466	6.28	6.28	9.42	9.42	-3.94	566.5
49	83	4960	-754	676	0	556	495	6.28	6.28	9.42	9.42	-4.48	571.5
50	83	4837	-800	612	0	551	433	6.28	6.28	9.42	9.42	-3.30	560.3
51	83	5102	-783	725	0	507	465	6.28	6.28	9.42	9.42	-3.67	567.5

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	165	5652	-815	794	0	-150	-107	6.28	6.28	9.42	9.42	0.00	497.6

41	165	5456	-758	691	0	-64	-198	6.28	6.28	9.42	9.42	0.00	454.5
42	165	6076	-775	789	0	-355	-216	6.28	6.28	9.42	9.42	0.00	596.4
43	165	5688	-862	838	0	-162	-34	6.28	6.28	9.42	9.42	0.00	504.3
44	165	5074	-670	520	0	76	-359	6.28	6.28	9.42	9.42	-0.88	459.0
45	165	6396	-796	829	0	-503	-214	6.28	6.28	9.42	9.42	0.00	669.0
46	165	5304	-774	651	0	9	-180	6.28	6.28	9.42	9.42	0.00	425.0
47	165	5266	-777	641	0	27	-176	6.28	6.28	9.42	9.42	0.00	427.7
49	165	5332	-796	676	0	-2	-145	6.28	6.28	9.42	9.42	0.00	424.9
50	165	5208	-758	612	0	46	-210	6.28	6.28	9.42	9.42	0.00	429.1
51	165	5474	-783	674	0	-70	-181	6.28	6.28	9.42	9.42	0.00	457.8

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	248	6023	-940	794	0	-806	-831	6.28	6.28	9.42	9.42	-9.75	737.2
41	248	5827	-758	691	0	-634	-824	6.28	6.28	9.42	9.42	-9.79	722.8
42	248	6447	-775	637	0	-943	-855	6.28	6.28	9.42	9.42	-9.83	813.1
43	248	6059	-1072	838	0	-854	-831	6.28	6.28	9.42	9.42	-9.73	754.1
44	248	5445	-460	520	0	-354	-825	6.28	6.28	9.42	9.42	-10.10	701.3
45	248	6767	-796	575	0	-1082	-871	6.28	6.28	9.42	9.42	-9.84	883.0
46	248	5676	-774	651	0	-528	-819	6.28	6.28	9.42	9.42	-9.81	711.6
47	248	5638	-777	641	0	-502	-817	6.28	6.28	9.42	9.42	-9.81	708.4
49	248	5703	-838	676	0	-560	-819	6.28	6.28	9.42	9.42	-9.80	713.3
50	248	5580	-716	612	0	-459	-818	6.28	6.28	9.42	9.42	-9.87	705.6
51	248	5845	-783	623	0	-605	-827	6.28	6.28	9.42	9.42	-9.82	725.1

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	330	6394	-1066	794	0	-1461	-1659	6.28	6.28	9.42	9.42	-23.20	1153.7
41	330	6198	-758	691	0	-1204	-1450	6.28	6.28	9.42	9.42	-19.95	1042.5
42	330	6818	-775	484	0	-1405	-1495	6.28	6.28	9.42	9.42	-20.32	1098.8
43	330	6430	-1281	838	0	-1546	-1802	6.28	6.28	9.42	9.42	-25.46	1224.4
44	330	5816	-251	520	0	-783	-1118	6.28	6.28	9.42	9.42	-14.77	862.1
45	330	7138	-796	321	0	-1452	-1528	6.28	6.28	9.42	9.42	-20.67	1132.6
46	330	6047	-774	651	0	-1065	-1457	6.28	6.28	9.42	9.42	-20.14	1037.4
47	330	6009	-777	641	0	-1031	-1458	6.28	6.28	9.42	9.42	-20.18	1035.7
49	330	6074	-880	676	0	-1117	-1528	6.28	6.28	9.42	9.42	-21.27	1072.9
50	330	5951	-674	612	0	-964	-1391	6.28	6.28	9.42	9.42	-19.13	1000.3
51	330	6216	-783	572	0	-1098	-1473	6.28	6.28	9.42	9.42	-20.31	1054.5

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 4 NI 23 NF 27 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 7B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-1289	140	345	0	527	62	6.28	6.28	9.42	9.42	-4.11	79.5
41	0	-1420	-133	307	0	404	274	6.28	6.28	9.42	9.42	-4.34	63.4
42	0	-851	-124	805	0	895	257	6.28	6.28	9.42	9.42	-6.84	221.6
43	0	-1265	310	366	0	612	-65	6.28	6.28	9.42	9.42	-4.77	106.1
44	0	-1702	-586	244	0	196	628	6.28	6.28	9.42	9.42	-9.94	217.2
45	0	-536	-131	1132	0	1224	261	6.28	6.28	9.42	9.42	-9.16	348.2
46	0	-1523	-152	299	0	407	300	6.28	6.28	9.42	9.42	-4.74	70.5
47	0	-1549	-157	297	0	408	306	6.28	6.28	9.42	9.42	-4.84	72.3
49	0	-1505	-66	310	0	449	235	6.28	6.28	9.42	9.42	-3.69	46.1
50	0	-1592	-245	285	0	366	374	6.28	6.28	9.42	9.42	-5.92	101.6
51	0	-1359	-154	463	0	572	300	6.28	6.28	9.42	9.42	-4.76	88.4

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	110	-794	13	345	0	148	146	6.28	6.28	9.42	9.42	-2.30	32.0
41	110	-925	-133	307	0	66	128	6.28	6.28	9.42	9.42	-2.01	-20.2
42	110	-356	-124	602	0	121	120	6.28	6.28	9.42	9.42	-1.90	40.1
43	110	-770	99	366	0	210	160	6.28	6.28	9.42	9.42	-2.54	39.7
44	110	-1207	-375	244	0	-72	99	6.28	6.28	9.42	9.42	-1.57	-18.3
45	110	-41	-131	793	0	165	118	6.28	6.28	9.42	9.42	-1.83	54.9
46	110	-1028	-152	299	0	78	133	6.28	6.28	9.42	9.42	-2.07	-21.3
47	110	-1054	-157	297	0	81	134	6.28	6.28	9.42	9.42	-2.09	-21.6
49	110	-1010	-108	310	0	109	140	6.28	6.28	9.42	9.42	-2.18	-22.0
50	110	-1097	-203	285	0	52	127	6.28	6.28	9.42	9.42	-1.98	-21.1
51	110	-864	-154	395	0	100	131	6.28	6.28	9.42	9.42	-2.06	22.7

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	220	-299	-113	345	0	-232	91	6.28	6.28	9.42	9.42	-1.79	52.0
41	220	-430	-133	307	0	-272	-18	6.28	6.28	9.42	9.42	-2.11	55.5
42	220	139	-124	399	0	-430	-17	6.28	6.28	9.42	9.42	-3.06	146.6
43	220	-275	-112	366	0	-192	153	6.28	6.28	9.42	9.42	-2.41	59.9
44	220	-712	-164	244	0	-340	-197	6.28	6.28	9.42	9.42	-3.13	59.6
45	220	454	-131	455	0	-522	-26	6.28	6.28	9.42	9.42	-3.54	199.9
46	220	-533	-152	299	0	-250	-35	6.28	6.28	9.42	9.42	-1.95	42.4
47	220	-559	-157	297	0	-245	-39	6.28	6.28	9.42	9.42	-1.91	39.3
49	220	-515	-150	310	0	-232	-2	6.28	6.28	9.42	9.42	-1.81	38.0
50	220	-602	-161	285	0	-261	-72	6.28	6.28	9.42	9.42	-2.04	41.6
51	220	-369	-154	327	0	-298	-38	6.28	6.28	9.42	9.42	-2.29	67.8

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	330	196	-240	345	0	-612	-104	6.28	6.28	9.42	9.42	-4.36	208.6
41	330	65	-133	307	0	-609	-164	6.28	6.28	9.42	9.42	-4.41	197.9
42	330	634	-124	196	0	-757	-153	6.28	6.28	9.42	9.42	-5.15	288.1
43	330	220	-323	366	0	-594	-87	6.28	6.28	9.42	9.42	-4.22	204.9
44	330	-217	47	244	0	-609	-262	6.28	6.28	9.42	9.42	-4.54	176.8
45	330	949	-131	116	0	-836	-169	6.28	6.28	9.42	9.42	-5.51	337.6
46	330	-38	-152	299	0	-579	-202	6.28	6.28	9.42	9.42	-4.24	180.6
47	330	-64	-157	297	0	-571	-211	6.28	6.28	9.42	9.42	-4.20	176.3
49	330	-20	-192	310	0	-572	-191	6.28	6.28	9.42	9.42	-4.19	179.8
50	330	-107	-118	285	0	-575	-226	6.28	6.28	9.42	9.42	-4.25	174.3
51	330	126	-154	260	0	-621	-207	6.28	6.28	9.42	9.42	-4.47	206.1

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	440	691	-367	345	0	-991	-438	6.28	6.28	9.42	9.42	-6.84	366.6
41	440	560	-133	307	0	-947	-311	6.28	6.28	9.42	9.42	-6.60	342.4

42	440	1129	-124	-8	0	-860	-290	6.28	6.28	9.42	9.42	-5.54	359.3
43	440	715	-535	366	0	-996	-559	6.28	6.28	9.42	9.42	-8.42	370.1
44	440	278	258	244	0	-877	-94	6.28	6.28	9.42	9.42	-6.26	298.8
45	440	1444	-131	-222	0	-778	-313	6.28	6.28	9.42	9.42	-4.62	358.5
46	440	457	-152	299	0	-908	-369	6.28	6.28	9.42	9.42	-6.38	322.2
47	440	431	-157	297	0	-898	-383	6.28	6.28	9.42	9.42	-6.32	317.1
49	440	475	-235	310	0	-913	-426	6.28	6.28	9.42	9.42	-6.44	325.2
50	440	388	-76	285	0	-889	-333	6.28	6.28	9.42	9.42	-6.28	310.9
51	440	621	-154	192	0	-869	-377	6.28	6.28	9.42	9.42	-5.99	322.5

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 5 NI 34 NF 35 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 12C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-10320	-446	457	0	-694	716	6.28	6.28	12.57	12.57	-7.25	-95.5
41	0	-9466	-287	346	0	-502	445	6.28	6.28	12.57	12.57	-5.61	-77.3
42	0	-9469	-280	879	0	-3923	433	6.28	6.28	12.57	12.57	-25.60	578.1
43	0	-10310	-537	451	0	-701	862	6.28	6.28	12.57	12.57	-8.00	-103.9
44	0	-8375	-28	176	0	-206	1	6.28	6.28	12.57	12.57	-3.97	-57.8
45	0	-8884	-260	1153	0	-6083	389	6.28	6.28	12.57	12.57	-40.05	1269.4
46	0	-8528	-263	216	0	-308	389	6.28	6.28	12.57	12.57	-4.99	-67.7
47	0	-8294	-256	184	0	-259	375	6.28	6.28	12.57	12.57	-4.84	-65.6
49	0	-8579	-309	221	0	-323	465	6.28	6.28	12.57	12.57	-5.39	-72.2
50	0	-8193	-208	166	0	-224	293	6.28	6.28	12.57	12.57	-4.40	-60.5
51	0	-8294	-254	362	0	-1399	371	6.28	6.28	12.57	12.57	-8.67	-115.5

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	83	-9826	-446	457	0	-1071	348	6.28	6.28	12.57	12.57	-7.63	-104.9
41	83	-8971	-287	346	0	-787	208	6.28	6.28	12.57	12.57	-6.28	-87.2
42	83	-8974	-280	577	0	-4523	202	6.28	6.28	12.57	12.57	-29.72	787.0
43	83	-9814	-537	451	0	-1073	419	6.28	6.28	12.57	12.57	-7.63	-104.9
44	83	-7880	-28	176	0	-352	-22	6.28	6.28	12.57	12.57	-4.30	-61.4
45	83	-8389	-260	650	0	-6827	175	6.28	6.28	12.57	12.57	-44.88	1533.8
46	83	-8033	-263	216	0	-486	172	6.28	6.28	12.57	12.57	-4.84	-68.3
47	83	-7799	-256	184	0	-411	163	6.28	6.28	12.57	12.57	-4.48	-63.6
49	83	-8084	-309	221	0	-506	210	6.28	6.28	12.57	12.57	-4.93	-69.5
50	83	-7698	-208	166	0	-361	122	6.28	6.28	12.57	12.57	-4.27	-60.8
51	83	-7799	-254	261	0	-1656	161	6.28	6.28	12.57	12.57	-10.19	-132.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	165	-9331	-446	457	0	-1449	-20	6.28	6.28	12.57	12.57	-9.10	-122.2
41	165	-8476	-287	346	0	-1072	-29	6.28	6.28	12.57	12.57	-7.16	-97.6
42	165	-8479	-280	275	0	-4874	-29	6.28	6.28	12.57	12.57	-32.09	925.7
43	165	-9318	-537	451	0	-1445	-24	6.28	6.28	12.57	12.57	-9.08	-122.0
44	165	-7385	-28	176	0	-497	-45	6.28	6.28	12.57	12.57	-4.63	-65.0
45	165	-7894	-260	146	0	-7155	-39	6.28	6.28	12.57	12.57	-46.96	1670.7
46	165	-7538	-263	216	0	-664	-45	6.28	6.28	12.57	12.57	-5.29	-73.4
47	165	-7304	-256	184	0	-562	-48	6.28	6.28	12.57	12.57	-4.84	-67.5
49	165	-7589	-309	221	0	-688	-45	6.28	6.28	12.57	12.57	-5.40	-74.8
50	165	-7203	-208	166	0	-498	-50	6.28	6.28	12.57	12.57	-4.57	-64.0
51	165	-7304	-254	160	0	-1830	-48	6.28	6.28	12.57	12.57	-11.42	-144.1

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	248	-8836	-446	457	0	-1826	-388	6.28	6.28	12.57	12.57	-11.22	-145.9
41	248	-7981	-287	346	0	-1358	-266	6.28	6.28	12.57	12.57	-8.41	-111.9
42	248	-7984	-280	-27	0	-4976	-260	6.28	6.28	12.57	12.57	-32.77	989.9
43	248	-8822	-537	451	0	-1817	-467	6.28	6.28	12.57	12.57	-11.17	-145.2
44	248	-6890	-28	176	0	-642	-68	6.28	6.28	12.57	12.57	-4.96	-68.7
45	248	-7399	-260	-357	0	-7068	-253	6.28	6.28	12.57	12.57	-46.35	1678.7
46	248	-7043	-263	216	0	-843	-261	6.28	6.28	12.57	12.57	-5.75	-78.7
47	248	-6809	-256	184	0	-714	-260	6.28	6.28	12.57	12.57	-5.19	-71.4
49	248	-7094	-309	221	0	-870	-301	6.28	6.28	12.57	12.57	-5.88	-80.3
50	248	-6708	-208	166	0	-636	-221	6.28	6.28	12.57	12.57	-4.87	-67.3
51	248	-6809	-254	60	0	-1920	-258	6.28	6.28	12.57	12.57	-12.14	168.9

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	330	-8342	-446	457	0	-2203	-756	6.28	6.28	12.57	12.57	-13.82	-173.0
41	330	-7486	-287	346	0	-1643	-503	6.28	6.28	12.57	12.57	-10.13	-130.6
42	330	-7489	-280	-330	0	-4829	-491	6.28	6.28	12.57	12.57	-31.80	978.0
43	330	-8326	-537	451	0	-2189	-910	6.28	6.28	12.57	12.57	-13.73	-171.9
44	330	-6395	-28	176	0	-788	-90	6.28	6.28	12.57	12.57	-5.31	-72.5
45	330	-6904	-260	-860	0	-6566	-467	6.28	6.28	12.57	12.57	-43.06	1557.2
46	330	-6548	-263	216	0	-1021	-478	6.28	6.28	12.57	12.57	-6.41	-86.0
47	330	-6314	-256	184	0	-866	-471	6.28	6.28	12.57	12.57	-5.62	-76.2
49	330	-6599	-309	221	0	-1053	-556	6.28	6.28	12.57	12.57	-6.58	-88.2
50	330	-6213	-208	166	0	-773	-392	6.28	6.28	12.57	12.57	-5.19	-70.9
51	330	-6314	-254	-41	0	-1928	-467	6.28	6.28	12.57	12.57	-12.29	193.8

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 6 NI 36 NF 37 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 17C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-10670	-402	505	0	-1167	521	6.28	6.28	12.57	12.57	-8.30	-114.1
41	0	-9976	-244	432	0	-1039	272	6.28	6.28	12.57	12.57	-7.57	-104.3
42	0	-10050	-245	1139	0	-5029	272	6.28	6.28	12.57	12.57	-33.04	870.3
43	0	-10350	-496	454	0	-1017	670	6.28	6.28	12.57	12.57	-7.64	-105.5
44	0	-9034	16	329	0	-870	-143	6.28	6.28	12.57	12.57	-6.61	-91.3
45	0	-9317	-235	1512	0	-7454	254	6.28	6.28	12.57	12.57	-49.01	1663.8

46	0	-8721	-227	273	0	-664	243	6.28	6.28	12.57	12.57	-5.75	-80.2
47	0	-8408	-222	233	0	-570	236	6.28	6.28	12.57	12.57	-5.29	-74.2
49	0	-8639	-275	257	0	-612	319	6.28	6.28	12.57	12.57	-5.53	-77.5
50	0	-8376	-172	232	0	-583	156	6.28	6.28	12.57	12.57	-5.32	-74.6
51	0	-8433	-222	469	0	-1900	236	6.28	6.28	12.57	12.57	-11.74	-150.7

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	83	-10175	-402	505	0	-1583	189	6.28	6.28	12.57	12.57	-9.94	-133.5
41	83	-9481	-244	432	0	-1395	70	6.28	6.28	12.57	12.57	-8.87	-119.7
42	83	-9555	-245	837	0	-5844	70	6.28	6.28	12.57	12.57	-38.49	1150.6
43	83	-9854	-496	454	0	-1392	260	6.28	6.28	12.57	12.57	-8.95	-121.1
44	83	-8539	16	329	0	-1142	-129	6.28	6.28	12.57	12.57	-7.47	-101.5
45	83	-8822	-235	1008	0	-8493	60	6.28	6.28	12.57	12.57	-55.69	2022.0
46	83	-8226	-227	273	0	-889	56	6.28	6.28	12.57	12.57	-6.36	-87.4
47	83	-7913	-222	233	0	-762	52	6.28	6.28	12.57	12.57	-5.79	-80.0
49	83	-8144	-275	257	0	-825	92	6.28	6.28	12.57	12.57	-6.10	-84.1
50	83	-7881	-172	232	0	-775	14	6.28	6.28	12.57	12.57	-5.82	-80.3
51	83	-7938	-222	368	0	-2245	52	6.28	6.28	12.57	12.57	-14.20	198.5

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	165	-9680	-402	505	0	-2000	-143	6.28	6.28	12.57	12.57	-12.29	-159.8
41	165	-8986	-244	432	0	-1752	-132	6.28	6.28	12.57	12.57	-10.76	-140.9
42	165	-9060	-245	535	0	-6410	-133	6.28	6.28	12.57	12.57	-42.20	1358.3
43	165	-9358	-496	454	0	-1766	-149	6.28	6.28	12.57	12.57	-10.86	-142.8
44	165	-8044	16	329	0	-1413	-116	6.28	6.28	12.57	12.57	-8.72	-115.7
45	165	-8327	-235	505	0	-9118	-133	6.28	6.28	12.57	12.57	-59.65	2252.2
46	165	-7731	-227	273	0	-1114	-131	6.28	6.28	12.57	12.57	-7.12	-96.3
47	165	-7418	-222	233	0	-954	-131	6.28	6.28	12.57	12.57	-6.33	-86.2
49	165	-7649	-275	257	0	-1037	-134	6.28	6.28	12.57	12.57	-6.75	-91.7
50	165	-7386	-172	232	0	-966	-128	6.28	6.28	12.57	12.57	-6.37	-86.7
51	165	-7443	-222	268	0	-2508	-131	6.28	6.28	12.57	12.57	-16.13	291.1

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	248	-9184	-402	505	0	-2416	-474	6.28	6.28	12.57	12.57	-15.15	-189.7
41	248	-8491	-244	432	0	-2108	-334	6.28	6.28	12.57	12.57	-13.14	-166.1
42	248	-8566	-245	233	0	-6727	-335	6.28	6.28	12.57	12.57	-44.24	1490.6
43	248	-8863	-496	454	0	-2141	-559	6.28	6.28	12.57	12.57	-13.31	-169.0
44	248	-7549	16	329	0	-1684	-103	6.28	6.28	12.57	12.57	-10.40	-133.6
45	248	-7832	-235	2	0	-9326	-327	6.28	6.28	12.57	12.57	-60.92	2353.1
46	248	-7236	-227	273	0	-1339	-318	6.28	6.28	12.57	12.57	-8.23	-108.6
47	248	-6923	-222	233	0	-1147	-314	6.28	6.28	12.57	12.57	-7.12	-95.1
49	248	-7154	-275	257	0	-1250	-361	6.28	6.28	12.57	12.57	-7.72	-102.4
50	248	-6891	-172	232	0	-1158	-270	6.28	6.28	12.57	12.57	-7.18	-95.7
51	248	-6948	-222	167	0	-2687	-315	6.28	6.28	12.57	12.57	-17.46	368.8

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	330	-8689	-402	505	0	-2832	-806	6.28	6.28	12.57	12.57	-18.17	314.0
41	330	-7996	-244	432	0	-2464	-535	6.28	6.28	12.57	12.57	-15.72	251.3
42	330	-8071	-245	-69	0	-6795	-538	6.28	6.28	12.57	12.57	-44.65	1546.2
43	330	-8367	-496	454	0	-2516	-968	6.28	6.28	12.57	12.57	-16.01	246.8
44	330	-7054	16	329	0	-1955	-89	6.28	6.28	12.57	12.57	-12.33	166.6
45	330	-7337	-235	-502	0	-9120	-520	6.28	6.28	12.57	12.57	-59.52	2324.2
46	330	-6741	-227	273	0	-1564	-505	6.28	6.28	12.57	12.57	-9.69	-123.8
47	330	-6428	-222	233	0	-1339	-497	6.28	6.28	12.57	12.57	-8.23	-106.9
49	330	-6659	-275	257	0	-1462	-588	6.28	6.28	12.57	12.57	-9.02	-116.2
50	330	-6396	-172	232	0	-1350	-412	6.28	6.28	12.57	12.57	-8.31	-107.7
51	330	-6453	-222	66	0	-2783	-498	6.28	6.28	12.57	12.57	-18.19	426.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 7 NI 38 NF 39 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 22C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	--												
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-11820	-153	339	0	-148	205	6.28	6.28	12.57	12.57	-5.27	-75.2
41	0	-11780	14	362	0	-267	-57	6.28	6.28	12.57	12.57	-5.51	-80.2
42	0	-11840	-4	837	0	-3632	-38	6.28	6.28	12.57	12.57	-23.16	367.8
43	0	-11030	-247	237	0	8	369	6.28	6.28	12.57	12.57	-5.79	-80.1
44	0	-11930	292	417	0	-481	-496	6.28	6.28	12.57	12.57	-6.75	-92.0
45	0	-11060	2	1067	0	-5799	-36	6.28	6.28	12.57	12.57	-38.13	1037.6
46	0	-10460	41	225	0	-144	-74	6.28	6.28	12.57	12.57	-4.56	-67.1
47	0	-10130	48	190	0	-113	-78	6.28	6.28	12.57	12.57	-4.32	-63.8
49	0	-10140	-7	183	0	-73	9	6.28	6.28	12.57	12.57	-4.18	-62.0
50	0	-10320	100	219	0	-171	-164	6.28	6.28	12.57	12.57	-4.60	-67.5
51	0	-10150	43	349	0	-1235	-72	6.28	6.28	12.57	12.57	-8.37	-114.4

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	83	-11326	-153	339	0	-427	79	6.28	6.28	12.57	12.57	-5.91	-84.8
41	83	-11284	14	362	0	-566	-46	6.28	6.28	12.57	12.57	-6.38	-90.7
42	83	-11346	-4	535	0	-4198	-41	6.28	6.28	12.57	12.57	-27.20	548.1
43	83	-10535	-247	237	0	-188	165	6.28	6.28	12.57	12.57	-4.74	-69.5
44	83	-11436	292	417	0	-826	-255	6.28	6.28	12.57	12.57	-7.37	-103.2
45	83	-10566	2	564	0	-6472	-34	6.28	6.28	12.57	12.57	-42.62	1275.1
46	83	-9964	41	225	0	-329	-40	6.28	6.28	12.57	12.57	-5.03	-72.5
47	83	-9634	48	190	0	-270	-39	6.28	6.28	12.57	12.57	-4.69	-67.9
49	83	-9646	-7	183	0	-224	3	6.28	6.28	12.57	12.57	-4.53	-65.9
50	83	-9826	100	219	0	-352	-81	6.28	6.28	12.57	12.57	-5.06	-72.7
51	83	-9655	43	248	0	-1481	-37	6.28	6.28	12.57	12.57	-9.33	-125.4

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	165	-10832	-153	339	0	-707	-48	6.28	6.28	12.57	12.57	-6.72	-94.4
41	165	-10788	14	362	0	-864	-35	6.28	6.28	12.57	12.57	-7.26	-101.2
42	165	-10852	-4	233	0	-4514	-44	6.28	6.28	12.57	12.57	-29.46	667.8
43	165	-10040	-247	237	0	-384	-38	6.28	6.28	12.57	12.57	-5.25	-75.4
44	165	-10942	292	417	0	-1170	-14	6.28	6.28	12.57	12.57	-8.42	-115.8
45	165	-10072	2	60	0	-6729	-32	6.28	6.28	12.57	12.57	-44.31	1387.5
46	165	-9468	41	225	0	-515	-6	6.28	6.28	12.57	12.57	-5.50	-77.9

47	165	-9138	48	190	0	-427	1	6.28	6.28	12.57	12.57	-5.06	-72.1
49	165	-9152	-7	183	0	-375	-3	6.28	6.28	12.57	12.57	-4.88	-69.8
50	165	-9332	100	219	0	-532	2	6.28	6.28	12.57	12.57	-5.51	-77.9
51	165	-9160	43	147	0	-1644	-2	6.28	6.28	12.57	12.57	-10.13	-134.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	248	-10337	-153	339	0	-986	-174	6.28	6.28	12.57	12.57	-7.53	-104.1
41	248	-10291	14	362	0	-1163	-23	6.28	6.28	12.57	12.57	-8.14	-111.7
42	248	-10357	-4	-69	0	-4581	-46	6.28	6.28	12.57	12.57	-29.98	717.5
43	248	-9546	-247	237	0	-579	-242	6.28	6.28	12.57	12.57	-5.76	-81.3
44	248	-10449	292	417	0	-1514	227	6.28	6.28	12.57	12.57	-9.67	-130.6
45	248	-9579	2	-443	0	-6571	-30	6.28	6.28	12.57	12.57	-43.27	1372.5
46	248	-8973	41	225	0	-700	28	6.28	6.28	12.57	12.57	-5.97	-83.3
47	248	-8643	48	190	0	-585	41	6.28	6.28	12.57	12.57	-5.43	-76.3
49	248	-8657	-7	183	0	-526	-9	6.28	6.28	12.57	12.57	-5.23	-73.7
50	248	-8838	100	219	0	-713	85	6.28	6.28	12.57	12.57	-5.97	-83.1
51	248	-8665	43	47	0	-1724	33	6.28	6.28	12.57	12.57	-10.59	-138.4

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	330	-9843	-153	339	0	-1266	-300	6.28	6.28	12.57	12.57	-8.40	-114.4
41	330	-9795	14	362	0	-1462	-12	6.28	6.28	12.57	12.57	-9.27	-124.9
42	330	-9863	-4	-372	0	-4399	-49	6.28	6.28	12.57	12.57	-28.80	694.0
43	330	-9051	-247	237	0	-775	-445	6.28	6.28	12.57	12.57	-6.27	-87.2
44	330	-9955	292	417	0	-1858	468	6.28	6.28	12.57	12.57	-11.42	-150.5
45	330	-9085	2	-946	0	-5998	-28	6.28	6.28	12.57	12.57	-39.50	1229.5
46	330	-8477	41	225	0	-886	62	6.28	6.28	12.57	12.57	-6.45	-88.8
47	330	-8147	48	190	0	-742	81	6.28	6.28	12.57	12.57	-5.80	-80.4
49	330	-8163	-7	183	0	-676	-15	6.28	6.28	12.57	12.57	-5.58	-77.6
50	330	-8344	100	219	0	-893	168	6.28	6.28	12.57	12.57	-6.42	-88.3
51	330	-8170	43	-54	0	-1721	69	6.28	6.28	12.57	12.57	-10.59	-137.3

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 8 NI 40 NF 34 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 12B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-16740	-30	288	0	508	134	6.28	6.28	12.57	12.57	-8.29	-119.8
41	0	-15900	-123	178	0	241	321	6.28	6.28	12.57	12.57	-7.31	-103.7
42	0	-15910	-114	2134	0	1842	298	6.28	6.28	12.57	12.57	-12.76	-174.8
43	0	-16730	35	320	0	628	3	6.28	6.28	12.57	12.57	-8.71	-125.0
44	0	-14840	-280	3	0	-189	638	6.28	6.28	12.57	12.57	-8.50	-115.6
45	0	-15350	-105	3396	0	2850	278	6.28	6.28	12.57	12.57	-17.52	-231.0
46	0	-15000	-119	112	0	147	312	6.28	6.28	12.57	12.57	-6.94	-98.4
47	0	-14770	-117	95	0	123	310	6.28	6.28	12.57	12.57	-6.85	-97.0
49	0	-15050	-86	132	0	212	248	6.28	6.28	12.57	12.57	-6.64	-96.7
50	0	-14670	-149	68	0	49	374	6.28	6.28	12.57	12.57	-7.13	-100.1
51	0	-14770	-114	747	0	657	302	6.28	6.28	12.57	12.57	-8.06	-115.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	110	-16080	-30	288	0	191	101	6.28	6.28	12.57	12.57	-6.90	-101.7
41	110	-15240	-123	178	0	45	186	6.28	6.28	12.57	12.57	-6.41	-92.6
42	110	-15250	-114	1731	0	-284	173	6.28	6.28	12.57	12.57	-6.91	-101.1
43	110	-16070	35	320	0	275	41	6.28	6.28	12.57	12.57	-7.19	-105.5
44	110	-14180	-280	3	0	-192	330	6.28	6.28	12.57	12.57	-6.74	-94.9
45	110	-14690	-105	2725	0	-517	162	6.28	6.28	12.57	12.57	-7.53	-108.3
46	110	-14340	-119	112	0	24	182	6.28	6.28	12.57	12.57	-6.06	-87.6
47	110	-14110	-117	95	0	19	181	6.28	6.28	12.57	12.57	-5.97	-86.3
49	110	-14390	-86	132	0	68	152	6.28	6.28	12.57	12.57	-5.93	-86.4
50	110	-14010	-149	68	0	-26	210	6.28	6.28	12.57	12.57	-6.08	-87.4
51	110	-14110	-114	613	0	-91	177	6.28	6.28	12.57	12.57	-5.95	-86.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	220	-15420	-30	288	0	-126	67	6.28	6.28	12.57	12.57	-6.41	-95.0
41	220	-14580	-123	178	0	-150	50	6.28	6.28	12.57	12.57	-6.17	-91.2
42	220	-14590	-114	1328	0	-1967	48	6.28	6.28	12.57	12.57	-12.83	-174.2
43	220	-15410	35	320	0	-77	80	6.28	6.28	12.57	12.57	-6.23	-92.7
44	220	-13520	-280	3	0	-196	22	6.28	6.28	12.57	12.57	-5.93	-87.1
45	220	-14030	-105	2054	0	-3145	46	6.28	6.28	12.57	12.57	-19.42	-249.5
46	220	-13680	-119	112	0	-98	51	6.28	6.28	12.57	12.57	-5.64	-83.7
47	220	-13450	-117	95	0	-86	52	6.28	6.28	12.57	12.57	-5.50	-81.8
49	220	-13730	-86	132	0	-77	57	6.28	6.28	12.57	12.57	-5.58	-83.0
50	220	-13350	-149	68	0	-101	46	6.28	6.28	12.57	12.57	-5.52	-81.9
51	220	-13450	-114	478	0	-691	51	6.28	6.28	12.57	12.57	-7.67	-108.9

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	330	-14760	-30	288	0	-443	34	6.28	6.28	12.57	12.57	-7.29	-105.3
41	330	-13920	-123	178	0	-346	-85	6.28	6.28	12.57	12.57	-6.62	-96.1
42	330	-13930	-114	926	0	-3206	-78	6.28	6.28	12.57	12.57	-19.84	-253.9
43	330	-14750	35	320	0	-429	118	6.28	6.28	12.57	12.57	-7.23	-104.7
44	330	-12860	-280	3	0	-200	-286	6.28	6.28	12.57	12.57	-6.04	-85.4
45	330	-13370	-105	1383	0	-5035	-69	6.28	6.28	12.57	12.57	-32.67	671.0
46	330	-13020	-119	112	0	-221	-79	6.28	6.28	12.57	12.57	-5.82	-85.3
47	330	-12790	-117	95	0	-190	-78	6.28	6.28	12.57	12.57	-5.62	-82.6
49	330	-13070	-86	132	0	-222	-38	6.28	6.28	12.57	12.57	-5.84	-85.7
50	330	-12690	-149	68	0	-176	-119	6.28	6.28	12.57	12.57	-5.53	-81.4
51	330	-12790	-114	344	0	-1143	-75	6.28	6.28	12.57	12.57	-9.03	-125.3

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	440	-14100	-30	288	0	-760	1	6.28	6.28	12.57	12.57	-8.17	-115.7
41	440	-13260	-123	178	0	-542	-220	6.28	6.28	12.57	12.57	-7.06	-101.1
42	440	-13270	-114	523	0	-4003	-203	6.28	6.28	12.57	12.57	-25.48	394.7
43	440	-14090	35	320	0	-781	156	6.28	6.28	12.57	12.57	-8.24	-116.6
44	440	-12200	-280	3	0	-204	-594	6.28	6.28	12.57	12.57	-7.33	-98.9
45	440	-12710	-105	711	0	-6187	-185	6.28	6.28	12.57	12.57	-40.62	1048.7
46	440	-12360	-119	112	0	-344	-210	6.28	6.28	12.57	12.57	-6.01	-87.0
47	440	-12130	-117	95	0	-294	-207	6.28	6.28	12.57	12.57	-5.74	-83.5

49	440	-12410	-86	132	0	-367	-133	6.28	6.28	12.57	12.57	-6.11	-88.3
50	440	-12030	-149	68	0	-252	-283	6.28	6.28	12.57	12.57	-5.73	-81.0
51	440	-12130	-114	210	0	-1448	-201	6.28	6.28	12.57	12.57	-9.89	-135.4

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 9 NI 41 NF 36 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 17B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-17080	130	496	0	915	-249	6.28	6.28	12.57	12.57	-9.88	-139.9
41	0	-16390	19	430	0	769	-18	6.28	6.28	12.57	12.57	-9.09	-129.4
42	0	-16480	15	2665	0	2840	-11	6.28	6.28	12.57	12.57	-17.56	-233.4
43	0	-16760	198	440	0	829	-389	6.28	6.28	12.57	12.57	-9.44	-134.2
44	0	-15460	-167	339	0	562	364	6.28	6.28	12.57	12.57	-7.99	-114.7
45	0	-15750	7	4056	0	4037	8	6.28	6.28	12.57	12.57	-25.25	-317.5
46	0	-15140	8	270	0	474	4	6.28	6.28	12.57	12.57	-7.55	-109.0
47	0	-14830	5	230	0	401	10	6.28	6.28	12.57	12.57	-7.16	-103.9
49	0	-15060	43	253	0	450	-67	6.28	6.28	12.57	12.57	-7.43	-107.4
50	0	-14800	-31	232	0	396	84	6.28	6.28	12.57	12.57	-7.14	-103.5
51	0	-14850	4	976	0	1091	12	6.28	6.28	12.57	12.57	-9.64	-134.9

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	110	-16420	130	496	0	370	-105	6.28	6.28	12.57	12.57	-7.67	-111.7
41	110	-15730	19	430	0	296	2	6.28	6.28	12.57	12.57	-7.14	-104.4
42	110	-15820	15	2262	0	130	6	6.28	6.28	12.57	12.57	-6.58	-97.5
43	110	-16100	198	440	0	345	-170	6.28	6.28	12.57	12.57	-7.45	-108.7
44	110	-14800	-167	339	0	189	180	6.28	6.28	12.57	12.57	-6.40	-94.2
45	110	-15090	7	3385	0	-55	15	6.28	6.28	12.57	12.57	-6.03	-89.9
46	110	-14480	8	270	0	177	13	6.28	6.28	12.57	12.57	-6.23	-91.8
47	110	-14170	5	230	0	147	16	6.28	6.28	12.57	12.57	-6.00	-88.7
49	110	-14400	43	253	0	172	-20	6.28	6.28	12.57	12.57	-6.18	-91.1
50	110	-14140	-31	232	0	141	50	6.28	6.28	12.57	12.57	-5.97	-88.2
51	110	-14190	4	841	0	92	17	6.28	6.28	12.57	12.57	-5.81	-86.3

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	220	-15760	130	496	0	-175	38	6.28	6.28	12.57	12.57	-6.72	-99.2
41	220	-15070	19	430	0	-176	23	6.28	6.28	12.57	12.57	-6.45	-95.2
42	220	-15160	15	1859	0	-2137	23	6.28	6.28	12.57	12.57	-13.75	-186.1
43	220	-15440	198	440	0	-140	48	6.28	6.28	12.57	12.57	-6.46	-95.7
44	220	-14140	-167	339	0	-183	-3	6.28	6.28	12.57	12.57	-6.12	-90.2
45	220	-14430	7	2714	0	-3408	22	6.28	6.28	12.57	12.57	-21.14	-269.4
46	220	-13820	8	270	0	-120	22	6.28	6.28	12.57	12.57	-5.77	-85.5
47	220	-13510	5	230	0	-106	21	6.28	6.28	12.57	12.57	-5.60	-83.1
49	220	-13740	43	253	0	-106	27	6.28	6.28	12.57	12.57	-5.69	-84.4
50	220	-13480	-31	232	0	-115	16	6.28	6.28	12.57	12.57	-5.62	-83.3
51	220	-13530	4	707	0	-760	21	6.28	6.28	12.57	12.57	-7.95	-112.4

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	330	-15100	130	496	0	-721	182	6.28	6.28	12.57	12.57	-8.41	-119.8
41	330	-14410	19	430	0	-648	43	6.28	6.28	12.57	12.57	-7.89	-112.5
42	330	-14500	15	1457	0	-3960	40	6.28	6.28	12.57	12.57	-24.94	328.3
43	330	-14780	198	440	0	-624	266	6.28	6.28	12.57	12.57	-7.94	-113.6
44	330	-13480	-167	339	0	-556	-187	6.28	6.28	12.57	12.57	-7.20	-103.0
45	330	-13770	7	2042	0	-6023	29	6.28	6.28	12.57	12.57	-39.40	934.0
46	330	-13160	8	270	0	-418	30	6.28	6.28	12.57	12.57	-6.58	-95.0
47	330	-12850	5	230	0	-360	27	6.28	6.28	12.57	12.57	-6.25	-90.6
49	330	-13080	43	253	0	-384	73	6.28	6.28	12.57	12.57	-6.43	-93.0
50	330	-12820	-31	232	0	-370	-17	6.28	6.28	12.57	12.57	-6.28	-90.9
51	330	-12870	4	573	0	-1464	26	6.28	6.28	12.57	12.57	-10.22	-140.2

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	440	-14440	130	496	0	-1266	325	6.28	6.28	12.57	12.57	-10.11	-140.3
41	440	-13750	19	430	0	-1121	63	6.28	6.28	12.57	12.57	-9.33	-129.9
42	440	-13840	15	1054	0	-5341	56	6.28	6.28	12.57	12.57	-34.71	731.4
43	440	-14120	198	440	0	-1108	485	6.28	6.28	12.57	12.57	-9.42	-131.4
44	440	-12820	-167	339	0	-929	-371	6.28	6.28	12.57	12.57	-8.28	-115.9
45	440	-13110	7	1371	0	-7900	36	6.28	6.28	12.57	12.57	-52.02	1542.3
46	440	-12500	8	270	0	-715	39	6.28	6.28	12.57	12.57	-7.39	-104.4
47	440	-12190	5	230	0	-614	33	6.28	6.28	12.57	12.57	-6.91	-98.1
49	440	-12420	43	253	0	-662	120	6.28	6.28	12.57	12.57	-7.17	-101.6
50	440	-12160	-31	232	0	-626	-51	6.28	6.28	12.57	12.57	-6.94	-98.5
51	440	-12210	4	439	0	-2020	31	6.28	6.28	12.57	12.57	-12.55	-167.6

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 10 NI 42 NF 38 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 22B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-18240	207	-11	0	-194	-452	6.28	6.28	12.57	12.57	-8.80	-123.6
41	0	-18200	102	69	0	10	-242	6.28	6.28	12.57	12.57	-7.75	-111.8
42	0	-18270	88	1982	0	1498	-207	6.28	6.28	12.57	12.57	-12.42	-172.9
43	0	-17470	263	-88	0	-357	-566	6.28	6.28	12.57	12.57	-9.09	-125.8
44	0	-18350	-71	208	0	361	104	6.28	6.28	12.57	12.57	-8.38	-122.5
45	0	-17510	65	3233	0	2464	-158	6.28	6.28	12.57	12.57	-15.86	-214.7
46	0	-16910	81	31	0	-32	-202	6.28	6.28	12.57	12.57	-7.09	-102.6
47	0	-16590	75	22	0	-43	-192	6.28	6.28	12.57	12.57	-6.92	-100.3
49	0	-16600	110	-5	0	-111	-261	6.28	6.28	12.57	12.57	-7.27	-104.2
50	0	-16780	43	54	0	33	-127	6.28	6.28	12.57	12.57	-6.67	-98.7
51	0	-16610	70	659	0	453	-180	6.28	6.28	12.57	12.57	-8.04	-116.5

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	110	-17580	207	-11	0	-182	-224	6.28	6.28	12.57	12.57	-7.44	-110.0
41	110	-17540	102	69	0	-66	-130	6.28	6.28	12.57	12.57	-7.01	-104.6
42	110	-17610	88	1579	0	-460	-110	6.28	6.28	12.57	12.57	-8.45	-122.6
43	110	-16810	263	-88	0	-261	-276	6.28	6.28	12.57	12.57	-7.43	-109.1
44	110	-17690	-71	208	0	132	26	6.28	6.28	12.57	12.57	-7.31	-108.4
45	110	-16850	65	2562	0	-723	-86	6.28	6.28	12.57	12.57	-9.10	-130.0
46	110	-16250	81	31	0	-67	-113	6.28	6.28	12.57	12.57	-6.52	-97.1
47	110	-15930	75	22	0	-67	-109	6.28	6.28	12.57	12.57	-6.39	-95.3
49	110	-15940	110	-5	0	-106	-140	6.28	6.28	12.57	12.57	-6.54	-97.1
50	110	-16120	43	54	0	-27	-80	6.28	6.28	12.57	12.57	-6.32	-94.6
51	110	-15950	70	525	0	-198	-102	6.28	6.28	12.57	12.57	-6.87	-101.3

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	220	-16920	207	-11	0	-170	4	6.28	6.28	12.57	12.57	-7.15	-105.7
41	220	-16880	102	69	0	-141	-17	6.28	6.28	12.57	12.57	-7.03	-104.1
42	220	-16950	88	1176	0	-1975	-13	6.28	6.28	12.57	12.57	-13.64	-186.8
43	220	-16150	263	-88	0	-164	13	6.28	6.28	12.57	12.57	-6.83	-100.9
44	220	-17030	-71	208	0	-97	-52	6.28	6.28	12.57	12.57	-6.93	-103.0
45	220	-16190	65	1891	0	-3172	-15	6.28	6.28	12.57	12.57	-19.48	-255.1
46	220	-15590	81	31	0	-101	-24	6.28	6.28	12.57	12.57	-6.38	-94.9
47	220	-15270	75	22	0	-91	-26	6.28	6.28	12.57	12.57	-6.22	-92.5
49	220	-15280	110	-5	0	-100	-19	6.28	6.28	12.57	12.57	-6.26	-93.0
50	220	-15460	43	54	0	-87	-32	6.28	6.28	12.57	12.57	-6.28	-93.5
51	220	-15290	70	391	0	-702	-25	6.28	6.28	12.57	12.57	-8.42	-120.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	330	-16260	207	-11	0	-158	232	6.28	6.28	12.57	12.57	-7.00	-101.3
41	330	-16220	102	69	0	-217	95	6.28	6.28	12.57	12.57	-7.04	-103.7
42	330	-16290	88	773	0	-3047	83	6.28	6.28	12.57	12.57	-18.73	-246.7
43	330	-15490	263	-88	0	-67	303	6.28	6.28	12.57	12.57	-7.08	-100.5
44	330	-16370	-71	208	0	-326	-130	6.28	6.28	12.57	12.57	-7.49	-109.5
45	330	-15530	65	1219	0	-4883	56	6.28	6.28	12.57	12.57	-31.21	513.5
46	330	-14930	81	31	0	-135	65	6.28	6.28	12.57	12.57	-6.25	-92.6
47	330	-14610	75	22	0	-115	57	6.28	6.28	12.57	12.57	-6.05	-89.8
49	330	-14620	110	-5	0	-95	102	6.28	6.28	12.57	12.57	-5.99	-89.0
50	330	-14800	43	54	0	-147	16	6.28	6.28	12.57	12.57	-6.24	-92.3
51	330	-14630	70	257	0	-1058	53	6.28	6.28	12.57	12.57	-9.44	-132.1

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	440	-15600	207	-11	0	-146	459	6.28	6.28	12.57	12.57	-7.89	-109.8
41	440	-15560	102	69	0	-293	208	6.28	6.28	12.57	12.57	-7.06	-103.3
42	440	-15630	88	371	0	-3676	180	6.28	6.28	12.57	12.57	-22.79	-290.6
43	440	-14830	263	-88	0	30	593	6.28	6.28	12.57	12.57	-8.27	-113.1
44	440	-15710	-71	208	0	-555	-207	6.28	6.28	12.57	12.57	-8.06	-115.9
45	440	-14870	65	548	0	-5855	127	6.28	6.28	12.57	12.57	-38.10	819.3
46	440	-14270	81	31	0	-169	153	6.28	6.28	12.57	12.57	-6.12	-90.3
47	440	-13950	75	22	0	-138	140	6.28	6.28	12.57	12.57	-5.88	-87.0
49	440	-13960	110	-5	0	-89	224	6.28	6.28	12.57	12.57	-6.13	-87.8
50	440	-14140	43	54	0	-206	63	6.28	6.28	12.57	12.57	-6.20	-91.2
51	440	-13970	70	122	0	-1266	130	6.28	6.28	12.57	12.57	-9.93	-137.6

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 11 NI 48 NF 49 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 31B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-19620	1456	-87	0	-149	-10540	15.71	15.71	9.42	9.42	-35.64	742.2
41	0	-20620	646	-56	0	-104	-8422	15.71	15.71	9.42	9.42	-28.20	423.1
42	0	-20720	582	117	0	326	-8333	15.71	15.71	9.42	9.42	-27.88	408.9
43	0	-17360	1845	-90	0	-141	-10280	15.71	15.71	9.42	9.42	-34.80	792.1
44	0	-22630	-682	-5	0	-29	-5160	15.71	15.71	9.42	9.42	-17.36	-238.8
45	0	-19180	388	250	0	651	-6601	15.71	15.71	9.42	9.42	-21.91	-290.3
46	0	-18060	404	-28	0	-44	-5745	15.71	15.71	9.42	9.42	-19.01	-254.0
47	0	-17420	343	-20	0	-29	-5075	15.71	15.71	9.42	9.42	-16.77	-226.0
49	0	-17090	613	-31	0	-44	-5781	15.71	15.71	9.42	9.42	-19.18	-254.5
50	0	-18150	108	-14	0	-21	-4758	15.71	15.71	9.42	9.42	-15.77	-214.6
51	0	-17460	322	37	0	115	-5046	15.71	15.71	9.42	9.42	-16.67	-224.9

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	110	-18740	1317	-87	0	-53	-9014	15.71	15.71	9.42	9.42	-30.39	563.3
41	110	-19740	646	-56	0	-42	-7711	15.71	15.71	9.42	9.42	-25.77	361.4
42	110	-19840	582	117	0	198	-7692	15.71	15.71	9.42	9.42	-25.69	356.1
43	110	-16480	1614	-90	0	-43	-8377	15.71	15.71	9.42	9.42	-28.29	557.0
44	110	-21750	-451	-5	0	-23	-5783	15.71	15.71	9.42	9.42	-19.15	-260.3
45	110	-18300	388	250	0	375	-6174	15.71	15.71	9.42	9.42	-20.48	-271.9
46	110	-17180	404	-28	0	-13	-5301	15.71	15.71	9.42	9.42	-17.53	-234.9
47	110	-16540	343	-20	0	-6	-4698	15.71	15.71	9.42	9.42	-15.53	-209.8
49	110	-16210	567	-31	0	-10	-5132	15.71	15.71	9.42	9.42	-16.98	-227.0
50	110	-17270	154	-14	0	-6	-4614	15.71	15.71	9.42	9.42	-15.27	-207.5
51	110	-16580	322	37	0	74	-4692	15.71	15.71	9.42	9.42	-15.51	-209.6

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	220	-17860	1179	-87	0	42	-7641	15.71	15.71	9.42	9.42	-25.64	410.7
41	220	-18860	646	-56	0	20	-7000	15.71	15.71	9.42	9.42	-23.33	-306.5
42	220	-18960	582	117	0	69	-7052	15.71	15.71	9.42	9.42	-23.50	-308.7
43	220	-15600	1383	-90	0	56	-6728	15.71	15.71	9.42	9.42	-22.59	365.7
44	220	-20870	-220	-5	0	-18	-6152	15.71	15.71	9.42	9.42	-20.33	-273.7
45	220	-17420	388	250	0	100	-5746	15.71	15.71	9.42	9.42	-19.04	-253.4
46	220	-16300	404	-28	0	17	-4856	15.71	15.71	9.42	9.42	-16.05	-215.8
47	220	-15660	343	-20	0	16	-4320	15.71	15.71	9.42	9.42	-14.29	-193.5
49	220	-15330	521	-31	0	24	-4534	15.71	15.71	9.42	9.42	-14.98	-201.6
50	220	-16390	200	-14	0	9	-4419	15.71	15.71	9.42	9.42	-14.62	-198.5
51	220	-15700	322	37	0	33	-4338	15.71	15.71	9.42	9.42	-14.34	-194.3

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	330	-16980	1040	-87	0	138	-6420	15.71	15.71	9.42	9.42	-21.42	285.1
41	330	-17980	646	-56	0	81	-6290	15.71	15.71	9.42	9.42	-20.90	-276.4
42	330	-18080	582	117	0	-60	-6412	15.71	15.71	9.42	9.42	-21.32	-281.5
43	330	-14720	1152	-90	0	155	-5334	15.71	15.71	9.42	9.42	-17.75	-233.9
44	330	-19990	11	-5	0	-12	-6267	15.71	15.71	9.42	9.42	-20.73	-277.4
45	330	-16540	388	250	0	-175	-5319	15.71	15.71	9.42	9.42	-17.61	-235.0
46	330	-15420	404	-28	0	47	-4412	15.71	15.71	9.42	9.42	-14.58	-196.9
47	330	-14780	343	-20	0	39	-3943	15.71	15.71	9.42	9.42	-13.05	-177.4
49	330	-14450	475	-31	0	58	-3987	15.71	15.71	9.42	9.42	-13.18	-178.6
50	330	-15510	246	-14	0	24	-4173	15.71	15.71	9.42	9.42	-13.81	-187.5
51	330	-14820	322	37	0	-8	-3983	15.71	15.71	9.42	9.42	-13.18	-179.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	440	-16100	902	-87	0	234	-5352	15.71	15.71	9.42	9.42	-17.74	-235.9
41	440	-17100	646	-56	0	143	-5579	15.71	15.71	9.42	9.42	-18.48	-246.2
42	440	-17200	582	117	0	-188	-5771	15.71	15.71	9.42	9.42	-19.14	-254.2
43	440	-13840	921	-90	0	254	-4193	15.71	15.71	9.42	9.42	-13.86	-186.1
44	440	-19110	242	-5	0	-7	-6128	15.71	15.71	9.42	9.42	-20.29	-270.8
45	440	-15660	388	250	0	-450	-4892	15.71	15.71	9.42	9.42	-16.18	-216.6
46	440	-14540	404	-28	0	78	-3968	15.71	15.71	9.42	9.42	-13.13	-178.0
47	440	-13900	343	-20	0	61	-3566	15.71	15.71	9.42	9.42	-11.83	-161.3
49	440	-13570	428	-31	0	92	-3490	15.71	15.71	9.42	9.42	-11.58	-157.8
50	440	-14630	293	-14	0	40	-3877	15.71	15.71	9.42	9.42	-12.84	-174.6
51	440	-13940	322	37	0	-49	-3629	15.71	15.71	9.42	9.42	-12.03	-163.8

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 12 NI 91 NF 92 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 30B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-22520	2739	-106	0	-269	-21390	15.71	15.71	9.42	9.42	-71.95	2217.9
41	0	-22980	1581	-94	0	-250	-16410	15.71	15.71	9.42	9.42	-55.52	1456.3
42	0	-23020	1589	85	0	190	-16510	15.71	15.71	9.42	9.42	-55.85	1469.3
43	0	-20130	3161	-91	0	-223	-21410	15.71	15.71	9.42	9.42	-71.78	2327.4
44	0	-24170	-294	-75	0	-221	-8651	15.71	15.71	9.42	9.42	-28.78	-379.6
45	0	-20950	1244	227	0	542	-13260	15.71	15.71	9.42	9.42	-44.89	1079.1
46	0	-19630	1021	-57	0	-155	-11120	15.71	15.71	9.42	9.42	-37.63	823.8
47	0	-18800	880	-48	0	-132	-9793	15.71	15.71	9.42	9.42	-33.09	668.3
49	0	-18640	1267	-52	0	-138	-11450	15.71	15.71	9.42	9.42	-38.76	909.8
50	0	-19450	576	-48	0	-138	-8903	15.71	15.71	9.42	9.42	-29.96	523.7
51	0	-18810	883	12	0	15	-9826	15.71	15.71	9.42	9.42	-33.20	672.5

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	110	-21640	2600	-106	0	-153	-18454	15.71	15.71	9.42	9.42	-62.24	1816.6
41	110	-22100	1581	-94	0	-147	-14671	15.71	15.71	9.42	9.42	-49.66	1237.7
42	110	-22140	1589	85	0	96	-14762	15.71	15.71	9.42	9.42	-49.97	1249.3
43	110	-19250	2930	-91	0	-124	-18059	15.71	15.71	9.42	9.42	-60.76	1862.1
44	110	-23290	-63	-75	0	-139	-8848	15.71	15.71	9.42	9.42	-29.52	396.0
45	110	-20070	1244	227	0	292	-11893	15.71	15.71	9.42	9.42	-40.26	917.0
46	110	-18750	1021	-57	0	-93	-9996	15.71	15.71	9.42	9.42	-33.79	698.6
47	110	-17920	880	-48	0	-79	-8824	15.71	15.71	9.42	9.42	-29.77	566.5
49	110	-17760	1221	-52	0	-81	-10083	15.71	15.71	9.42	9.42	-34.12	748.5
50	110	-18570	622	-48	0	-84	-8245	15.71	15.71	9.42	9.42	-27.72	466.1
51	110	-17930	883	12	0	2	-8854	15.71	15.71	9.42	9.42	-29.88	570.3

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	220	-20760	2462	-106	0	-37	-15670	15.71	15.71	9.42	9.42	-52.97	1440.4
41	220	-21220	1581	-94	0	-44	-12932	15.71	15.71	9.42	9.42	-43.78	1020.9
42	220	-21260	1589	85	0	3	-13013	15.71	15.71	9.42	9.42	-44.06	1031.0
43	220	-18370	2699	-91	0	-24	-14962	15.71	15.71	9.42	9.42	-50.51	1437.3
44	220	-22410	168	-75	0	-56	-8790	15.71	15.71	9.42	9.42	-29.38	414.7
45	220	-19190	1244	227	0	42	-10526	15.71	15.71	9.42	9.42	-35.60	756.4
46	220	-17870	1021	-57	0	-30	-8873	15.71	15.71	9.42	9.42	-29.94	575.0
47	220	-17040	880	-48	0	-27	-7856	15.71	15.71	9.42	9.42	-26.45	466.3
49	220	-16880	1174	-52	0	-25	-8767	15.71	15.71	9.42	9.42	-29.62	596.5
50	220	-17690	668	-48	0	-31	-7536	15.71	15.71	9.42	9.42	-25.29	402.5
51	220	-17050	883	12	0	-11	-7883	15.71	15.71	9.42	9.42	-26.54	469.5

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	330	-19880	2324	-106	0	79	-13039	15.71	15.71	9.42	9.42	-44.14	1090.3
41	330	-20340	1581	-94	0	59	-11192	15.71	15.71	9.42	9.42	-37.86	806.8
42	330	-20380	1589	85	0	-91	-11264	15.71	15.71	9.42	9.42	-38.10	815.5
43	330	-17490	2468	-91	0	76	-12120	15.71	15.71	9.42	9.42	-41.01	1054.0
44	330	-21530	399	-75	0	26	-8479	15.71	15.71	9.42	9.42	-28.34	402.5
45	330	-18310	1244	227	0	-207	-9158	15.71	15.71	9.42	9.42	-30.91	598.3
46	330	-16990	1021	-57	0	32	-7750	15.71	15.71	9.42	9.42	-26.08	453.8
47	330	-16160	880	-48	0	25	-6888	15.71	15.71	9.42	9.42	-23.11	368.2
49	330	-16000	1128	-52	0	32	-7502	15.71	15.71	9.42	9.42	-25.27	454.7
50	330	-16810	714	-48	0	22	-6776	15.71	15.71	9.42	9.42	-22.68	333.6
51	330	-16170	883	12	0	-24	-6912	15.71	15.71	9.42	9.42	-23.20	371.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	440	-19000	2185	-106	0	195	-10560	15.71	15.71	9.42	9.42	-35.72	768.5
41	440	-19460	1581	-94	0	162	-9453	15.71	15.71	9.42	9.42	-31.88	597.5
42	440	-19500	1589	85	0	-184	-9516	15.71	15.71	9.42	9.42	-32.10	604.7
43	440	-16610	2237	-91	0	176	-9531	15.71	15.71	9.42	9.42	-32.25	714.3
44	440	-20650	630	-75	0	108	-7913	15.71	15.71	9.42	9.42	-26.41	359.3
45	440	-17430	1244	227	0	-457	-7791	15.71	15.71	9.42	9.42	-26.20	444.4
46	440	-16110	1021	-57	0	95	-6626	15.71	15.71	9.42	9.42	-22.20	336.4
47	440	-15280	880	-48	0	78	-5919	15.71	15.71	9.42	9.42	-19.77	273.6
49	440	-15120	1082	-52	0	89	-6288	15.71	15.71	9.42	9.42	-21.08	324.5
50	440	-15930	760	-48	0	75	-5965	15.71	15.71	9.42	9.42	-19.89	-261.1
51	440	-15290	883	12	0	-38	-5940	15.71	15.71	9.42	9.42	-19.84	275.9

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 13 NI 134 NF 135 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 29B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-22400	3005	-194	0	-539	-22740	15.71	15.71	9.42	9.42	-76.34	2426.3
41	0	-22980	1770	-167	0	-471	-17420	15.71	15.71	9.42	9.42	-58.88	1605.4
42	0	-22920	1754	-11	0	-80	-17260	15.71	15.71	9.42	9.42	-58.35	1584.2
43	0	-19930	3439	-177	0	-486	-22770	15.71	15.71	9.42	9.42	-76.17	2541.9
44	0	-24370	-225	-127	0	-368	-9130	15.71	15.71	9.42	9.42	-30.44	-399.6
45	0	-20790	1354	127	0	279	-13640	15.71	15.71	9.42	9.42	-46.18	1140.8
46	0	-19630	1148	-112	0	-315	-11790	15.71	15.71	9.42	9.42	-39.91	919.5
47	0	-18800	992	-98	0	-276	-10380	15.71	15.71	9.42	9.42	-35.11	750.7
49	0	-18600	1404	-107	0	-299	-12160	15.71	15.71	9.42	9.42	-41.17	1014.4
50	0	-19490	671	-97	0	-275	-9428	15.71	15.71	9.42	9.42	-31.79	593.0
51	0	-18780	987	-46	0	-146	-10330	15.71	15.71	9.42	9.42	-34.94	744.4

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	110	-21520	2866	-194	0	-326	-19511	15.71	15.71	9.42	9.42	-65.71	1980.0
41	110	-22100	1770	-167	0	-287	-15472	15.71	15.71	9.42	9.42	-52.35	1355.0
42	110	-22040	1754	-11	0	-67	-15330	15.71	15.71	9.42	9.42	-51.88	1336.7
43	110	-19050	3208	-177	0	-292	-19114	15.71	15.71	9.42	9.42	-64.19	2029.5
44	110	-23490	6	-127	0	-229	-9251	15.71	15.71	9.42	9.42	-30.92	439.2
45	110	-19910	1354	127	0	139	-12150	15.71	15.71	9.42	9.42	-41.13	960.3
46	110	-18750	1148	-112	0	-192	-10527	15.71	15.71	9.42	9.42	-35.62	773.4
47	110	-17920	992	-98	0	-168	-9289	15.71	15.71	9.42	9.42	-31.38	630.7
49	110	-17720	1358	-107	0	-181	-10640	15.71	15.71	9.42	9.42	-36.02	829.7
50	110	-18610	717	-97	0	-168	-8665	15.71	15.71	9.42	9.42	-29.18	520.6
51	110	-17900	987	-46	0	-95	-9245	15.71	15.71	9.42	9.42	-31.23	625.3

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	220	-20640	2728	-194	0	-113	-16435	15.71	15.71	9.42	9.42	-55.51	1558.9
41	220	-21220	1770	-167	0	-103	-13524	15.71	15.71	9.42	9.42	-45.78	1106.5
42	220	-21160	1754	-11	0	-55	-13401	15.71	15.71	9.42	9.42	-45.37	1091.1
43	220	-18170	2977	-177	0	-98	-15712	15.71	15.71	9.42	9.42	-52.97	1557.7
44	220	-22610	237	-127	0	-89	-9118	15.71	15.71	9.42	9.42	-30.51	449.2
45	220	-19030	1354	127	0	-2	-10660	15.71	15.71	9.42	9.42	-36.07	781.6
46	220	-17870	1148	-112	0	-69	-9264	15.71	15.71	9.42	9.42	-31.30	629.1
47	220	-17040	992	-98	0	-60	-8198	15.71	15.71	9.42	9.42	-27.64	512.4
49	220	-16840	1311	-107	0	-63	-9171	15.71	15.71	9.42	9.42	-31.02	654.6
50	220	-17730	763	-97	0	-62	-7851	15.71	15.71	9.42	9.42	-26.39	442.3
51	220	-17020	987	-46	0	-44	-8160	15.71	15.71	9.42	9.42	-27.51	507.9

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	330	-19760	2590	-194	0	100	-13511	15.71	15.71	9.42	9.42	-45.73	1164.2
41	330	-20340	1770	-167	0	81	-11575	15.71	15.71	9.42	9.42	-39.17	861.1
42	330	-20280	1754	-11	0	-43	-11472	15.71	15.71	9.42	9.42	-38.81	848.7
43	330	-17290	2746	-177	0	96	-12564	15.71	15.71	9.42	9.42	-42.50	1127.7
44	330	-21730	468	-127	0	50	-8730	15.71	15.71	9.42	9.42	-29.21	427.7
45	330	-18150	1354	127	0	-142	-9171	15.71	15.71	9.42	9.42	-30.96	605.9
46	330	-16990	1148	-112	0	55	-8002	15.71	15.71	9.42	9.42	-26.96	487.6
47	330	-16160	992	-98	0	48	-7108	15.71	15.71	9.42	9.42	-23.88	396.8
49	330	-15960	1265	-107	0	54	-7753	15.71	15.71	9.42	9.42	-26.15	490.1
50	330	-16850	809	-97	0	45	-6986	15.71	15.71	9.42	9.42	-23.41	358.8
51	330	-16140	987	-46	0	7	-7074	15.71	15.71	9.42	9.42	-23.77	393.1

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	440	-18880	2451	-194	0	313	-10740	15.71	15.71	9.42	9.42	-36.34	798.7
41	440	-19460	1770	-167	0	265	-9627	15.71	15.71	9.42	9.42	-32.49	621.3
42	440	-19400	1754	-11	0	-30	-9542	15.71	15.71	9.42	9.42	-32.19	611.8
43	440	-16410	2515	-177	0	291	-9670	15.71	15.71	9.42	9.42	-32.73	742.0
44	440	-20850	699	-127	0	190	-8089	15.71	15.71	9.42	9.42	-27.02	374.9
45	440	-17270	1354	127	0	-282	-7681	15.71	15.71	9.42	9.42	-25.82	435.3
46	440	-16110	1148	-112	0	178	-6739	15.71	15.71	9.42	9.42	-22.59	350.7
47	440	-15280	992	-98	0	156	-6017	15.71	15.71	9.42	9.42	-20.11	285.6
49	440	-15080	1219	-107	0	172	-6386	15.71	15.71	9.42	9.42	-21.42	338.3
50	440	-15970	856	-97	0	152	-6070	15.71	15.71	9.42	9.42	-20.25	271.9
51	440	-15260	987	-46	0	57	-5989	15.71	15.71	9.42	9.42	-20.02	282.8

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 14 NI 177 NF 178 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 28B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-22320	2818	-233	0	-719	-21590	15.71	15.71	9.42	9.42	-72.58	2256.8
41	0	-22840	1596	-199	0	-617	-16220	15.71	15.71	9.42	9.42	-54.88	1434.2
42	0	-22840	1597	-61	0	-260	-16230	15.71	15.71	9.42	9.42	-54.91	1435.6
43	0	-19910	3276	-211	0	-654	-21860	15.71	15.71	9.42	9.42	-73.22	2405.2
44	0	-24140	-384	-149	0	-464	-7831	15.71	15.71	9.42	9.42	-25.93	-345.8
45	0	-20790	1241	76	0	111	-12930	15.71	15.71	9.42	9.42	-43.78	1037.8
46	0	-19550	1025	-128	0	-405	-10940	15.71	15.71	9.42	9.42	-37.01	801.3
47	0	-18720	882	-110	0	-352	-9615	15.71	15.71	9.42	9.42	-32.48	646.5
49	0	-18550	1290	-122	0	-386	-11400	15.71	15.71	9.42	9.42	-38.59	906.2
50	0	-19390	558	-109	0	-348	-8597	15.71	15.71	9.42	9.42	-28.90	485.2
51	0	-18720	883	-64	0	-233	-9617	15.71	15.71	9.42	9.42	-32.48	646.8

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	110	-21440	2680	-233	0	-463	-18566	15.71	15.71	9.42	9.42	-62.59	1842.1
41	110	-21960	1596	-199	0	-398	-14466	15.71	15.71	9.42	9.42	-48.97	1213.5
42	110	-21960	1597	-61	0	-193	-14474	15.71	15.71	9.42	9.42	-49.00	1214.6
43	110	-19030	3045	-211	0	-422	-18384	15.71	15.71	9.42	9.42	-61.81	1920.6

44	110	-23260	-153	-149	0	-300	-8126	15.71	15.71	9.42	9.42	-27.00	-357.1
45	110	-19910	1241	76	0	27	-11566	15.71	15.71	9.42	9.42	-39.14	876.4
46	110	-18670	1025	-128	0	-264	-9812	15.71	15.71	9.42	9.42	-33.16	675.7
47	110	-17840	882	-110	0	-230	-8644	15.71	15.71	9.42	9.42	-29.15	544.8
49	110	-17670	1244	-122	0	-252	-10008	15.71	15.71	9.42	9.42	-33.86	741.2
50	110	-18510	604	-109	0	-228	-7958	15.71	15.71	9.42	9.42	-26.72	430.7
51	110	-17840	883	-64	0	-162	-8646	15.71	15.71	9.42	9.42	-29.16	545.1

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	220	-20560	2541	-233	0	-206	-15695	15.71	15.71	9.42	9.42	-53.05	1452.5
41	220	-21080	1596	-199	0	-178	-12711	15.71	15.71	9.42	9.42	-43.03	994.7
42	220	-21080	1597	-61	0	-126	-12717	15.71	15.71	9.42	9.42	-43.05	995.5
43	220	-18150	2814	-211	0	-190	-15162	15.71	15.71	9.42	9.42	-51.16	1476.5
44	220	-22380	78	-149	0	-137	-8168	15.71	15.71	9.42	9.42	-27.19	-358.0
45	220	-19030	1241	76	0	-56	-10201	15.71	15.71	9.42	9.42	-34.49	716.8
46	220	-17790	1025	-128	0	-123	-8684	15.71	15.71	9.42	9.42	-29.29	551.9
47	220	-16960	882	-110	0	-109	-7674	15.71	15.71	9.42	9.42	-25.82	444.7
49	220	-16790	1197	-122	0	-118	-8666	15.71	15.71	9.42	9.42	-29.28	585.8
50	220	-17630	650	-109	0	-108	-7269	15.71	15.71	9.42	9.42	-24.35	370.3
51	220	-16960	883	-64	0	-91	-7676	15.71	15.71	9.42	9.42	-25.82	444.9

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	330	-19680	2402	-233	0	50	-12976	15.71	15.71	9.42	9.42	-43.93	1089.3
41	330	-20200	1596	-199	0	41	-10956	15.71	15.71	9.42	9.42	-37.05	778.9
42	330	-20200	1597	-61	0	-59	-10960	15.71	15.71	9.42	9.42	-37.06	779.4
43	330	-17270	2583	-211	0	42	-12194	15.71	15.71	9.42	9.42	-41.26	1074.0
44	330	-21500	309	-149	0	27	-7955	15.71	15.71	9.42	9.42	-26.50	-348.4
45	330	-18150	1241	76	0	-140	-8836	15.71	15.71	9.42	9.42	-29.80	560.0
46	330	-16910	1025	-128	0	18	-7555	15.71	15.71	9.42	9.42	-25.40	430.7
47	330	-16080	882	-110	0	12	-6704	15.71	15.71	9.42	9.42	-22.47	347.2
49	330	-15910	1151	-122	0	16	-7376	15.71	15.71	9.42	9.42	-24.84	440.8
50	330	-16750	696	-109	0	13	-6528	15.71	15.71	9.42	9.42	-21.81	304.8
51	330	-16080	883	-64	0	-21	-6705	15.71	15.71	9.42	9.42	-22.48	347.3

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	440	-18800	2264	-233	0	306	-10410	15.71	15.71	9.42	9.42	-35.21	754.9
41	440	-19320	1596	-199	0	260	-9202	15.71	15.71	9.42	9.42	-31.02	568.3
42	440	-19320	1597	-61	0	8	-9204	15.71	15.71	9.42	9.42	-31.02	568.6
43	440	-16390	2352	-211	0	274	-9480	15.71	15.71	9.42	9.42	-32.08	715.6
44	440	-20620	540	-149	0	190	-7488	15.71	15.71	9.42	9.42	-24.93	-328.3
45	440	-17270	1241	76	0	-223	-7472	15.71	15.71	9.42	9.42	-25.09	407.9
46	440	-16030	1025	-128	0	159	-6427	15.71	15.71	9.42	9.42	-21.50	313.8
47	440	-15200	882	-110	0	134	-5733	15.71	15.71	9.42	9.42	-19.12	253.5
49	440	-15030	1105	-122	0	149	-6136	15.71	15.71	9.42	9.42	-20.55	308.0
50	440	-15870	742	-109	0	133	-5737	15.71	15.71	9.42	9.42	-19.09	-251.6
51	440	-15200	883	-64	0	50	-5734	15.71	15.71	9.42	9.42	-19.12	253.6

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 15 NI 220 NF 221 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 27B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-18580	95	-319	0	-756	-11760	15.71	15.71	9.42	9.42	-39.81	957.1
41	0	-19470	-489	-316	0	-716	-7983	15.71	15.71	9.42	9.42	-26.74	403.4
42	0	-19740	-498	-182	0	-382	-8183	15.71	15.71	9.42	9.42	-27.42	420.3
43	0	-16430	544	-282	0	-655	-12540	15.71	15.71	9.42	9.42	-42.38	1160.4
44	0	-21290	-1473	-318	0	-675	-1981	15.71	15.71	9.42	9.42	-9.97	-142.4
45	0	-18360	-445	-53	0	-32	-6582	15.71	15.71	9.42	9.42	-21.90	-288.8
46	0	-16970	-395	-253	0	-514	-5209	15.71	15.71	9.42	9.42	-17.22	-230.9
47	0	-16340	-372	-238	0	-463	-4515	15.71	15.71	9.42	9.42	-14.93	-202.2
49	0	-16040	-177	-239	0	-476	-5773	15.71	15.71	9.42	9.42	-19.21	-253.2
50	0	-17020	-580	-246	0	-480	-3662	15.71	15.71	9.42	9.42	-12.45	-172.0
51	0	-16430	-374	-193	0	-352	-4582	15.71	15.71	9.42	9.42	-15.15	-205.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	110	-17700	-43	-319	0	-404	-11729	15.71	15.71	9.42	9.42	-39.70	988.2
41	110	-18590	-489	-316	0	-369	-8520	15.71	15.71	9.42	9.42	-28.68	501.9
42	110	-18860	-498	-182	0	-182	-8730	15.71	15.71	9.42	9.42	-29.39	520.7
43	110	-15550	313	-282	0	-345	-12069	15.71	15.71	9.42	9.42	-40.78	1128.0
44	110	-20410	-1242	-318	0	-325	-3474	15.71	15.71	9.42	9.42	-12.69	-177.4
45	110	-17480	-445	-53	0	26	-7072	15.71	15.71	9.42	9.42	-23.67	350.1
46	110	-16090	-395	-253	0	-235	-5644	15.71	15.71	9.42	9.42	-18.75	-247.9
47	110	-15460	-372	-238	0	-202	-4924	15.71	15.71	9.42	9.42	-16.30	-217.7
49	110	-15160	-223	-239	0	-214	-5993	15.71	15.71	9.42	9.42	-20.04	286.2
50	110	-16140	-534	-246	0	-210	-4274	15.71	15.71	9.42	9.42	-14.16	-192.5
51	110	-15550	-374	-193	0	-140	-4994	15.71	15.71	9.42	9.42	-16.53	-220.6

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	220	-16820	-182	-319	0	-53	-11850	15.71	15.71	9.42	9.42	-40.10	1042.2
41	220	-17710	-489	-316	0	-21	-9056	15.71	15.71	9.42	9.42	-30.59	606.1
42	220	-17980	-498	-182	0	18	-9276	15.71	15.71	9.42	9.42	-31.34	626.7
43	220	-14670	82	-282	0	-35	-11852	15.71	15.71	9.42	9.42	-40.02	1133.4
44	220	-19530	-1011	-318	0	25	-4713	15.71	15.71	9.42	9.42	-15.73	-215.5
45	220	-16600	-445	-53	0	85	-7561	15.71	15.71	9.42	9.42	-25.44	441.9
46	220	-15210	-395	-253	0	43	-6078	15.71	15.71	9.42	9.42	-20.33	295.3
47	220	-14580	-372	-238	0	59	-5332	15.71	15.71	9.42	9.42	-17.76	-233.7
49	220	-14280	-269	-239	0	49	-6263	15.71	15.71	9.42	9.42	-21.04	348.4
50	220	-15260	-488	-246	0	61	-4836	15.71	15.71	9.42	9.42	-16.00	-213.9
51	220	-14670	-374	-193	0	72	-5406	15.71	15.71	9.42	9.42	-18.01	-236.8

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	330	-15940	-320	-319	0	298	-12124	15.71	15.71	9.42	9.42	-40.98	1119.6
41	330	-16830	-489	-316	0	326	-9593	15.71	15.71	9.42	9.42	-32.46	714.7
42	330	-17100	-498	-182	0	218	-9823	15.71	15.71	9.42	9.42	-33.24	737.0
43	330	-13790	-149	-282	0	276	-11889	15.71	15.71	9.42	9.42	-40.09	1176.9
44	330	-18650	-780	-318	0	376	-5698	15.71	15.71	9.42	9.42	-18.84	-252.7

45	330	-15720	-445	-53	0	143	-8050	15.71	15.71	9.42	9.42	-27.19	539.6
46	330	-14330	-395	-253	0	322	-6512	15.71	15.71	9.42	9.42	-21.91	379.6
47	330	-13700	-372	-238	0	321	-5741	15.71	15.71	9.42	9.42	-19.25	299.6
49	330	-13400	-315	-239	0	311	-6585	15.71	15.71	9.42	9.42	-22.22	421.7
50	330	-14380	-442	-246	0	331	-5347	15.71	15.71	9.42	9.42	-17.82	-234.1
51	330	-13790	-374	-193	0	284	-5817	15.71	15.71	9.42	9.42	-19.51	306.5

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	440	-15060	-459	-319	0	649	-12550	15.71	15.71	9.42	9.42	-42.35	1220.6
41	440	-15950	-489	-316	0	674	-10130	15.71	15.71	9.42	9.42	-34.30	826.6
42	440	-16220	-498	-182	0	418	-10370	15.71	15.71	9.42	9.42	-35.11	850.5
43	440	-12910	-380	-282	0	586	-12180	15.71	15.71	9.42	9.42	-40.98	1259.1
44	440	-17770	-549	-318	0	726	-6429	15.71	15.71	9.42	9.42	-21.40	-281.9
45	440	-14840	-445	-53	0	201	-8540	15.71	15.71	9.42	9.42	-28.90	641.7
46	440	-13450	-395	-253	0	600	-6947	15.71	15.71	9.42	9.42	-23.47	469.9
47	440	-12820	-372	-238	0	582	-6150	15.71	15.71	9.42	9.42	-20.73	383.1
49	440	-12520	-362	-239	0	574	-6957	15.71	15.71	9.42	9.42	-23.53	506.2
50	440	-13500	-395	-246	0	601	-5807	15.71	15.71	9.42	9.42	-19.49	314.5
51	440	-12910	-374	-193	0	496	-6229	15.71	15.71	9.42	9.42	-21.00	390.6

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 16 NI 263 NF 264 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 25B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	--												
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-20070	486	-380	0	-959	-598	6.28	6.28	9.42	9.42	-15.13	-206.1
41	0	-18370	57	-303	0	-787	119	6.28	6.28	9.42	9.42	-12.83	-183.4
42	0	-18110	60	-262	0	-445	114	6.28	6.28	9.42	9.42	-11.14	-162.0
43	0	-20340	780	-341	0	-872	-1103	6.28	6.28	9.42	9.42	-19.90	-247.9
44	0	-15410	-660	-198	0	-548	1321	6.28	6.28	9.42	9.42	-20.79	-240.2
45	0	-17070	70	-145	0	-15	84	6.28	6.28	9.42	9.42	-8.97	-130.6
46	0	-16990	70	-158	0	-465	77	6.28	6.28	9.42	9.42	-10.66	-154.7
47	0	-16640	73	-122	0	-384	66	6.28	6.28	9.42	9.42	-10.12	-147.4
49	0	-17210	216	-148	0	-442	-173	6.28	6.28	9.42	9.42	-10.67	-155.0
50	0	-16220	-72	-119	0	-377	312	6.28	6.28	9.42	9.42	-10.65	-145.5
51	0	-16550	74	-108	0	-270	64	6.28	6.28	9.42	9.42	-9.55	-140.2

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	97	-19632	425	-380	0	-588	-154	6.28	6.28	9.42	9.42	-12.56	-181.6
41	97	-17932	57	-303	0	-491	175	6.28	6.28	9.42	9.42	-11.26	-163.3
42	97	-17672	60	-175	0	-232	172	6.28	6.28	9.42	9.42	-10.07	-146.6
43	97	-19902	678	-341	0	-540	-392	6.28	6.28	9.42	9.42	-13.16	-180.9
44	97	-14970	-558	-198	0	-354	727	6.28	6.28	9.42	9.42	-13.87	-174.6
45	97	-16632	70	1	0	53	152	6.28	6.28	9.42	9.42	-9.38	-133.7
46	97	-16550	70	-158	0	-310	145	6.28	6.28	9.42	9.42	-9.74	-142.5
47	97	-16200	73	-122	0	-265	137	6.28	6.28	9.42	9.42	-9.36	-137.3
49	97	-16770	195	-148	0	-298	28	6.28	6.28	9.42	9.42	-9.79	-143.5
50	97	-15780	-52	-119	0	-260	252	6.28	6.28	9.42	9.42	-9.89	-136.8
51	97	-16112	74	-79	0	-179	136	6.28	6.28	9.42	9.42	-8.99	-131.7

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	195	-19195	364	-380	0	-217	230	6.28	6.28	9.42	9.42	-11.33	-159.4
41	195	-17495	57	-303	0	-196	231	6.28	6.28	9.42	9.42	-10.52	-147.2
42	195	-17235	60	-101	0	-99	231	6.28	6.28	9.42	9.42	-10.40	-145.3
43	195	-19465	575	-341	0	-207	219	6.28	6.28	9.42	9.42	-11.35	-160.3
44	195	-14530	-456	-198	0	-161	233	6.28	6.28	9.42	9.42	-9.12	-126.1
45	195	-16195	70	125	0	-9	219	6.28	6.28	9.42	9.42	-9.79	-136.8
46	195	-16110	70	-158	0	-156	213	6.28	6.28	9.42	9.42	-9.69	-135.6
47	195	-15760	73	-122	0	-146	208	6.28	6.28	9.42	9.42	-9.48	-132.7
49	195	-16330	175	-148	0	-154	208	6.28	6.28	9.42	9.42	-9.75	-136.7
50	195	-15340	-31	-119	0	-144	211	6.28	6.28	9.42	9.42	-9.30	-129.9
51	195	-15675	74	-54	0	-114	208	6.28	6.28	9.42	9.42	-9.44	-132.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	292	-18758	302	-380	0	154	555	6.28	6.28	9.42	9.42	-14.10	-186.1
41	292	-17058	57	-303	0	100	287	6.28	6.28	9.42	9.42	-10.83	-149.2
42	292	-16798	60	-39	0	-32	289	6.28	6.28	9.42	9.42	-10.72	-147.6
43	292	-19028	473	-341	0	126	730	6.28	6.28	9.42	9.42	-15.84	-204.1
44	292	-14090	-353	-198	0	32	-161	6.28	6.28	9.42	9.42	-8.25	-116.3
45	292	-15758	70	228	0	-183	287	6.28	6.28	9.42	9.42	-10.20	-139.9
46	292	-15670	70	-158	0	-2	281	6.28	6.28	9.42	9.42	-10.11	-138.7
47	292	-15320	73	-122	0	-27	280	6.28	6.28	9.42	9.42	-9.92	-136.0
49	292	-15890	154	-148	0	-10	369	6.28	6.28	9.42	9.42	-11.02	-148.3
50	292	-14900	-11	-119	0	-28	191	6.28	6.28	9.42	9.42	-8.91	-124.8
51	292	-15238	74	-34	0	-71	280	6.28	6.28	9.42	9.42	-9.89	-135.5

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	390	-18320	241	-380	0	525	820	6.28	6.28	9.42	9.42	-16.33	-207.2
41	390	-16620	57	-303	0	396	343	6.28	6.28	9.42	9.42	-11.13	-151.2
42	390	-16360	60	11	0	-19	348	6.28	6.28	9.42	9.42	-11.05	-149.8
43	390	-18590	371	-341	0	458	1141	6.28	6.28	9.42	9.42	-19.52	-239.5
44	390	-13650	-251	-198	0	226	-456	6.28	6.28	9.42	9.42	-10.74	-140.2
45	390	-15320	70	311	0	-448	355	6.28	6.28	9.42	9.42	-10.62	-142.9
46	390	-15230	70	-158	0	152	349	6.28	6.28	9.42	9.42	-10.52	-141.8
47	390	-14880	73	-122	0	92	351	6.28	6.28	9.42	9.42	-10.37	-139.4
49	390	-15450	134	-148	0	134	509	6.28	6.28	9.42	9.42	-12.10	-158.1
50	390	-14460	10	-119	0	88	190	6.28	6.28	9.42	9.42	-8.69	-121.6
51	390	-14800	74	-17	0	-47	352	6.28	6.28	9.42	9.42	-10.34	-138.9

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 17 NI 49 NF 51 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 31C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-11930	1098	-18	0	-45	-4639	15.71	15.71	9.42	9.42	-15.50	215.8
41	0	-12960	821	-60	0	-105	-4913	15.71	15.71	9.42	9.42	-16.39	219.1
42	0	-13030	854	73	0	49	-5086	15.71	15.71	9.42	9.42	-16.99	238.0
43	0	-9640	1092	11	0	-6	-3426	15.71	15.71	9.42	9.42	-11.39	-150.4
44	0	-15030	386	-126	0	-202	-5542	15.71	15.71	9.42	9.42	-18.46	-242.8
45	0	-11480	686	163	0	151	-4171	15.71	15.71	9.42	9.42	-13.88	-182.9
46	0	-10400	517	-57	0	-106	-3266	15.71	15.71	9.42	9.42	-10.80	-144.5
47	0	-9755	441	-57	0	-106	-2854	15.71	15.71	9.42	9.42	-9.43	-127.1
49	0	-9412	533	-43	0	-86	-2763	15.71	15.71	9.42	9.42	-9.13	-123.0
50	0	-10490	392	-70	0	-126	-3186	15.71	15.71	9.42	9.42	-10.53	-141.4
51	0	-9779	452	-12	0	-55	-2912	15.71	15.71	9.42	9.42	-9.62	-129.4

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	83	-11270	960	-18	0	-30	-3790	15.71	15.71	9.42	9.42	-12.57	-166.9
41	83	-12300	821	-60	0	-56	-4236	15.71	15.71	9.42	9.42	-14.06	-186.3
42	83	-12370	854	73	0	-12	-4382	15.71	15.71	9.42	9.42	-14.57	-192.4
43	83	-8980	863	11	0	-15	-2619	15.71	15.71	9.42	9.42	-8.65	-116.6
44	83	-14370	616	-126	0	-97	-5129	15.71	15.71	9.42	9.42	-17.06	-225.1
45	83	-10820	686	163	0	16	-3605	15.71	15.71	9.42	9.42	-11.95	-158.9
46	83	-9739	517	-57	0	-59	-2840	15.71	15.71	9.42	9.42	-9.38	-126.5
47	83	-9095	441	-57	0	-60	-2490	15.71	15.71	9.42	9.42	-8.24	-111.7
49	83	-8752	488	-43	0	-51	-2342	15.71	15.71	9.42	9.42	-7.75	-105.3
50	83	-9830	438	-70	0	-68	-2844	15.71	15.71	9.42	9.42	-9.40	-126.7
51	83	-9119	452	-12	0	-45	-2539	15.71	15.71	9.42	9.42	-8.39	-113.6

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	165	-10610	823	-18	0	-15	-3054	15.71	15.71	9.42	9.42	-10.09	-136.2
41	165	-11640	821	-60	0	-7	-3559	15.71	15.71	9.42	9.42	-11.77	-157.8
42	165	-11710	854	73	0	-72	-3677	15.71	15.71	9.42	9.42	-12.16	-162.7
43	165	-8320	634	11	0	-23	-2002	15.71	15.71	9.42	9.42	-6.68	-91.6
44	165	-13710	845	-126	0	7	-4526	15.71	15.71	9.42	9.42	-15.00	-199.6
45	165	-10160	686	163	0	-118	-3040	15.71	15.71	9.42	9.42	-10.05	-135.0
46	165	-9078	517	-57	0	-12	-2413	15.71	15.71	9.42	9.42	-7.99	-108.6
47	165	-8435	441	-57	0	-13	-2126	15.71	15.71	9.42	9.42	-7.07	-96.5
49	165	-8092	442	-43	0	-16	-1958	15.71	15.71	9.42	9.42	-6.53	-89.5
50	165	-9170	484	-70	0	-10	-2463	15.71	15.71	9.42	9.42	-8.15	-110.7
51	165	-8459	452	-12	0	-35	-2166	15.71	15.71	9.42	9.42	-7.19	-98.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	248	-9951	685	-18	0	0	-2432	15.71	15.71	9.42	9.42	-8.11	-111.0
41	248	-10980	821	-60	0	43	-2882	15.71	15.71	9.42	9.42	-9.55	-129.9
42	248	-11050	854	73	0	-132	-2972	15.71	15.71	9.42	9.42	-9.84	-133.6
43	248	-7660	404	11	0	-32	-1573	15.71	15.71	9.42	9.42	-5.40	-74.9
44	248	-13050	1075	-126	0	111	-3734	15.71	15.71	9.42	9.42	-12.34	-166.6
45	248	-9499	686	163	0	-253	-2474	15.71	15.71	9.42	9.42	-8.20	-111.7
46	248	-8418	517	-57	0	36	-1986	15.71	15.71	9.42	9.42	-6.65	-91.2
47	248	-7775	441	-57	0	34	-1763	15.71	15.71	9.42	9.42	-5.93	-81.7
49	248	-7432	396	-43	0	20	-1613	15.71	15.71	9.42	9.42	-5.47	-75.6
50	248	-8510	530	-70	0	49	-2045	15.71	15.71	9.42	9.42	-6.83	-93.6
51	248	-7799	452	-12	0	-24	-1793	15.71	15.71	9.42	9.42	-6.02	-82.8

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	330	-9291	547	-18	0	16	-1924	15.71	15.71	9.42	9.42	-6.60	-91.3
41	330	-10320	821	-60	0	92	-2205	15.71	15.71	9.42	9.42	-7.51	-103.7
42	330	-10390	854	73	0	-192	-2268	15.71	15.71	9.42	9.42	-7.69	-106.1
43	330	-7000	175	11	0	-41	-1334	15.71	15.71	9.42	9.42	-4.68	-65.1
44	330	-12390	1304	-126	0	216	-2753	15.71	15.71	9.42	9.42	-9.30	-128.2
45	330	-8839	686	163	0	-388	-1908	15.71	15.71	9.42	9.42	-6.48	-89.5
46	330	-7757	517	-57	0	83	-1560	15.71	15.71	9.42	9.42	-5.39	-74.7
47	330	-7115	441	-57	0	81	-1399	15.71	15.71	9.42	9.42	-4.86	-67.5
49	330	-6772	350	-43	0	55	-1305	15.71	15.71	9.42	9.42	-4.56	-63.4
50	330	-7850	576	-70	0	107	-1589	15.71	15.71	9.42	9.42	-5.48	-76.0
51	330	-7139	452	-12	0	-14	-1420	15.71	15.71	9.42	9.42	-4.92	-68.3

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 18 NI 92 NF 94 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 30C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-15030	2563	-216	0	-319	-10620	15.71	15.71	9.42	9.42	-35.93	935.9
41	0	-15460	1850	-221	0	-339	-9285	15.71	15.71	9.42	9.42	-31.43	724.1
42	0	-15500	1870	-84	0	-150	-9370	15.71	15.71	9.42	9.42	-31.72	734.8
43	0	-12630	2633	-168	0	-241	-9613	15.71	15.71	9.42	9.42	-32.49	888.1
44	0	-16610	728	-234	0	-377	-7386	15.71	15.71	9.42	9.42	-24.83	418.4
45	0	-13430	1479	51	0	42	-7529	15.71	15.71	9.42	9.42	-25.47	552.4
46	0	-12080	1203	-151	0	-234	-6249	15.71	15.71	9.42	9.42	-21.11	423.4
47	0	-11240	1041	-133	0	-208	-5490	15.71	15.71	9.42	9.42	-18.52	349.2
49	0	-11090	1279	-132	0	-202	-5935	15.71	15.71	9.42	9.42	-20.06	416.3
50	0	-11890	898	-145	0	-229	-5490	15.71	15.71	9.42	9.42	-18.48	326.5
51	0	-11250	1048	-88	0	-145	-5518	15.71	15.71	9.42	9.42	-18.62	352.7

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	83	-14370	2425	-216	0	-141	-8562	15.71	15.71	9.42	9.42	-28.98	663.3
41	83	-14800	1850	-221	0	-156	-7758	15.71	15.71	9.42	9.42	-26.22	533.0
42	83	-14840	1870	-84	0	-80	-7827	15.71	15.71	9.42	9.42	-26.45	541.1
43	83	-11970	2404	-168	0	-102	-7535	15.71	15.71	9.42	9.42	-25.51	610.6
44	83	-15950	958	-234	0	-184	-6691	15.71	15.71	9.42	9.42	-22.43	349.6
45	83	-12770	1479	51	0	-0	-6309	15.71	15.71	9.42	9.42	-21.29	406.5
46	83	-11420	1203	-151	0	-110	-5256	15.71	15.71	9.42	9.42	-17.69	311.3
47	83	-10580	1041	-133	0	-98	-4631	15.71	15.71	9.42	9.42	-15.56	256.9
49	83	-10431	1233	-132	0	-93	-4899	15.71	15.71	9.42	9.42	-16.50	297.5
50	83	-11230	944	-145	0	-109	-4730	15.71	15.71	9.42	9.42	-15.86	248.7

51	83	-10591	1048	-88	0	-73	-4654	15.71	15.71	9.42	9.42	-15.64	259.5

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	165	-13710	2288	-216	0	37	-6618	15.71	15.71	9.42	9.42	-22.32	415.3
41	165	-14140	1850	-221	0	26	-6232	15.71	15.71	9.42	9.42	-20.94	348.9
42	165	-14180	1870	-84	0	-10	-6284	15.71	15.71	9.42	9.42	-21.12	354.5
43	165	-11310	2175	-168	0	37	-5646	15.71	15.71	9.42	9.42	-19.06	368.1
44	165	-15290	1187	-234	0	9	-5806	15.71	15.71	9.42	9.42	-19.37	259.7
45	165	-12110	1479	51	0	-42	-5089	15.71	15.71	9.42	9.42	-17.07	266.6
46	165	-10760	1203	-151	0	15	-4264	15.71	15.71	9.42	9.42	-14.26	204.4
47	165	-9919	1041	-133	0	12	-3772	15.71	15.71	9.42	9.42	-12.58	169.0
49	165	-9772	1187	-132	0	15	-3900	15.71	15.71	9.42	9.42	-13.05	189.1
50	165	-10570	989	-145	0	10	-3933	15.71	15.71	9.42	9.42	-13.11	-172.2
51	165	-9932	1048	-88	0	-0	-3789	15.71	15.71	9.42	9.42	-12.64	170.8

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	248	-13050	2150	-216	0	215	-4788	15.71	15.71	9.42	9.42	-15.95	-209.8
41	248	-13480	1850	-221	0	209	-4705	15.71	15.71	9.42	9.42	-15.63	-206.8
42	248	-13520	1870	-84	0	59	-4742	15.71	15.71	9.42	9.42	-15.76	-208.3
43	248	-10651	1945	-168	0	175	-3946	15.71	15.71	9.42	9.42	-13.15	-172.8
44	248	-14630	1417	-234	0	203	-4732	15.71	15.71	9.42	9.42	-15.67	-209.0
45	248	-11450	1479	51	0	-84	-3869	15.71	15.71	9.42	9.42	-12.83	-170.4
46	248	-10101	1203	-151	0	139	-3271	15.71	15.71	9.42	9.42	-10.83	-144.4
47	248	-9258	1041	-133	0	122	-2912	15.71	15.71	9.42	9.42	-9.63	-128.9
49	248	-9114	1141	-132	0	124	-2940	15.71	15.71	9.42	9.42	-9.73	-129.8
50	248	-9911	1035	-145	0	129	-3097	15.71	15.71	9.42	9.42	-10.25	-137.1
51	248	-9273	1048	-88	0	72	-2924	15.71	15.71	9.42	9.42	-9.68	-129.4

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	330	-12390	2012	-216	0	393	-3071	15.71	15.71	9.42	9.42	-10.22	-139.7
41	330	-12820	1850	-221	0	391	-3179	15.71	15.71	9.42	9.42	-10.58	-144.6
42	330	-12860	1870	-84	0	129	-3199	15.71	15.71	9.42	9.42	-10.64	-145.5
43	330	-9991	1716	-168	0	314	-2436	15.71	15.71	9.42	9.42	-8.12	-111.2
44	330	-13970	1646	-234	0	396	-3469	15.71	15.71	9.42	9.42	-11.54	-157.8
45	330	-10790	1479	51	0	-126	-2649	15.71	15.71	9.42	9.42	-8.82	-120.7
46	330	-9441	1203	-151	0	264	-2278	15.71	15.71	9.42	9.42	-7.60	-104.2
47	330	-8598	1041	-133	0	232	-2053	15.71	15.71	9.42	9.42	-6.86	-94.1
49	330	-8455	1095	-132	0	232	-2017	15.71	15.71	9.42	9.42	-6.74	-92.4
50	330	-9251	1081	-145	0	249	-2224	15.71	15.71	9.42	9.42	-7.43	-101.8
51	330	-8614	1048	-88	0	144	-2060	15.71	15.71	9.42	9.42	-6.88	-94.4

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 19 NI 135 NF 137 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 29C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-14830	2491	-439	0	-684	-10410	15.71	15.71	9.42	9.42	-35.22	913.3
41	0	-15400	1812	-404	0	-636	-9197	15.71	15.71	9.42	9.42	-31.13	713.9
42	0	-15340	1782	-249	0	-411	-9087	15.71	15.71	9.42	9.42	-30.76	700.4
43	0	-12350	2546	-379	0	-587	-9335	15.71	15.71	9.42	9.42	-31.56	858.8
44	0	-16790	744	-358	0	-574	-7498	15.71	15.71	9.42	9.42	-25.21	427.2
45	0	-13210	1364	-62	0	-131	-7130	15.71	15.71	9.42	9.42	-24.11	504.4
46	0	-12050	1176	-271	0	-429	-6185	15.71	15.71	9.42	9.42	-20.89	415.6
47	0	-11210	1017	-237	0	-377	-5431	15.71	15.71	9.42	9.42	-18.32	342.2
49	0	-11020	1243	-249	0	-393	-5836	15.71	15.71	9.42	9.42	-19.73	405.1
50	0	-11910	882	-244	0	-391	-5468	15.71	15.71	9.42	9.42	-18.41	322.8
51	0	-11190	1007	-185	0	-302	-5395	15.71	15.71	9.42	9.42	-18.19	338.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	83	-14170	2353	-439	0	-322	-8412	15.71	15.71	9.42	9.42	-28.47	649.6
41	83	-14740	1812	-404	0	-302	-7702	15.71	15.71	9.42	9.42	-26.03	527.3
42	83	-14680	1782	-249	0	-205	-7617	15.71	15.71	9.42	9.42	-25.73	517.7
43	83	-11691	2317	-379	0	-274	-7329	15.71	15.71	9.42	9.42	-24.81	592.0
44	83	-16130	973	-358	0	-279	-6790	15.71	15.71	9.42	9.42	-22.77	356.6
45	83	-12550	1364	-62	0	-79	-6004	15.71	15.71	9.42	9.42	-20.24	372.8
46	83	-11389	1176	-271	0	-206	-5215	15.71	15.71	9.42	9.42	-17.55	306.9
47	83	-10550	1017	-237	0	-182	-4592	15.71	15.71	9.42	9.42	-15.43	252.8
49	83	-10360	1197	-249	0	-188	-4829	15.71	15.71	9.42	9.42	-16.27	290.6
50	83	-11249	928	-244	0	-189	-4721	15.71	15.71	9.42	9.42	-15.83	246.9
51	83	-10530	1007	-185	0	-149	-4564	15.71	15.71	9.42	9.42	-15.33	249.9

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	165	-13510	2216	-439	0	41	-6527	15.71	15.71	9.42	9.42	-22.01	409.9
41	165	-14080	1812	-404	0	31	-6208	15.71	15.71	9.42	9.42	-20.86	347.7
42	165	-14020	1782	-249	0	1	-6146	15.71	15.71	9.42	9.42	-20.65	341.7
43	165	-11032	2088	-379	0	39	-5513	15.71	15.71	9.42	9.42	-18.61	359.7
44	165	-15470	1202	-358	0	16	-5892	15.71	15.71	9.42	9.42	-19.66	264.9
45	165	-11890	1364	-62	0	-28	-4878	15.71	15.71	9.42	9.42	-16.34	246.8
46	165	-10728	1176	-271	0	18	-4245	15.71	15.71	9.42	9.42	-14.19	203.0
47	165	-9889	1017	-237	0	14	-3754	15.71	15.71	9.42	9.42	-12.52	167.8
49	165	-9699	1151	-249	0	17	-3861	15.71	15.71	9.42	9.42	-12.91	186.4
50	165	-10588	974	-244	0	13	-3936	15.71	15.71	9.42	9.42	-13.12	-172.3
51	165	-9869	1007	-185	0	4	-3734	15.71	15.71	9.42	9.42	-12.46	166.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	248	-12850	2078	-439	0	403	-4756	15.71	15.71	9.42	9.42	-15.85	-208.3
41	248	-13420	1812	-404	0	365	-4713	15.71	15.71	9.42	9.42	-15.66	-207.0
42	248	-13360	1782	-249	0	207	-4676	15.71	15.71	9.42	9.42	-15.54	-205.5
43	248	-10374	1858	-379	0	351	-3885	15.71	15.71	9.42	9.42	-12.95	-170.0
44	248	-14810	1432	-358	0	311	-4806	15.71	15.71	9.42	9.42	-15.92	-212.2
45	248	-11230	1364	-62	0	23	-3753	15.71	15.71	9.42	9.42	-12.44	-165.4
46	248	-10068	1176	-271	0	241	-3275	15.71	15.71	9.42	9.42	-10.85	-144.6
47	248	-9228	1017	-237	0	210	-2916	15.71	15.71	9.42	9.42	-9.65	-129.0
49	248	-9038	1105	-249	0	222	-2930	15.71	15.71	9.42	9.42	-9.70	-129.4
50	248	-9926	1020	-244	0	215	-3114	15.71	15.71	9.42	9.42	-10.30	-137.8
51	248	-9208	1007	-185	0	157	-2904	15.71	15.71	9.42	9.42	-9.61	-128.5

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	330	-12190	1940	-439	0	766	-3098	15.71	15.71	9.42	9.42	-10.29	-140.4
41	330	-12760	1812	-404	0	699	-3218	15.71	15.71	9.42	9.42	-10.69	-146.0
42	330	-12700	1782	-249	0	412	-3206	15.71	15.71	9.42	9.42	-10.65	-145.4
43	330	-9715	1629	-379	0	664	-2447	15.71	15.71	9.42	9.42	-8.13	-111.0
44	330	-14150	1661	-358	0	606	-3530	15.71	15.71	9.42	9.42	-11.74	-160.4
45	330	-10570	1364	-62	0	75	-2627	15.71	15.71	9.42	9.42	-8.74	-119.5
46	330	-9407	1176	-271	0	464	-2305	15.71	15.71	9.42	9.42	-7.68	-105.1
47	330	-8568	1017	-237	0	405	-2077	15.71	15.71	9.42	9.42	-6.93	-94.9
49	330	-8378	1059	-249	0	428	-2037	15.71	15.71	9.42	9.42	-6.79	-93.0
50	330	-9265	1066	-244	0	416	-2253	15.71	15.71	9.42	9.42	-7.51	-102.9
51	330	-8548	1007	-185	0	310	-2073	15.71	15.71	9.42	9.42	-6.91	-94.7

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 20 NI 178 NF 180 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 28C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-14650	2424	-507	0	-823	-10250	15.71	15.71	9.42	9.42	-34.68	897.3
41	0	-15180	1722	-476	0	-765	-8897	15.71	15.71	9.42	9.42	-30.11	679.5
42	0	-15190	1720	-296	0	-497	-8897	15.71	15.71	9.42	9.42	-30.11	679.1
43	0	-12230	2509	-425	0	-688	-9318	15.71	15.71	9.42	9.42	-31.50	861.3
44	0	-16490	613	-438	0	-695	-6952	15.71	15.71	9.42	9.42	-23.32	365.9
45	0	-13120	1335	-73	0	-145	-7057	15.71	15.71	9.42	9.42	-23.86	497.5
46	0	-11870	1108	-310	0	-489	-5953	15.71	15.71	9.42	9.42	-20.10	390.1
47	0	-11050	955	-269	0	-420	-5216	15.71	15.71	9.42	9.42	-17.58	318.7
49	0	-10870	1189	-279	0	-439	-5669	15.71	15.71	9.42	9.42	-19.16	387.4
50	0	-11720	810	-282	0	-440	-5196	15.71	15.71	9.42	9.42	-17.47	293.2
51	0	-11050	954	-209	0	-330	-5217	15.71	15.71	9.42	9.42	-17.58	318.8

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	83	-13990	2286	-507	0	-404	-8308	15.71	15.71	9.42	9.42	-28.12	641.7
41	83	-14520	1722	-476	0	-373	-7477	15.71	15.71	9.42	9.42	-25.26	504.1
42	83	-14530	1720	-296	0	-252	-7478	15.71	15.71	9.42	9.42	-25.26	503.9
43	83	-11571	2280	-425	0	-338	-7342	15.71	15.71	9.42	9.42	-24.86	598.7
44	83	-15830	842	-438	0	-333	-6352	15.71	15.71	9.42	9.42	-21.25	310.6
45	83	-12460	1335	-73	0	-85	-5955	15.71	15.71	9.42	9.42	-20.07	369.3
46	83	-11210	1108	-310	0	-233	-5038	15.71	15.71	9.42	9.42	-16.95	289.5
47	83	-10389	955	-269	0	-198	-4428	15.71	15.71	9.42	9.42	-14.86	236.8
49	83	-10210	1143	-279	0	-209	-4707	15.71	15.71	9.42	9.42	-15.85	279.3
50	83	-11060	856	-282	0	-208	-4509	15.71	15.71	9.42	9.42	-15.10	225.9
51	83	-10390	954	-209	0	-158	-4430	15.71	15.71	9.42	9.42	-14.86	236.9

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	165	-13330	2149	-507	0	14	-6479	15.71	15.71	9.42	9.42	-21.85	409.8
41	165	-13860	1722	-476	0	20	-6056	15.71	15.71	9.42	9.42	-20.35	335.2
42	165	-13870	1720	-296	0	-8	-6060	15.71	15.71	9.42	9.42	-20.36	335.2
43	165	-10912	2051	-425	0	13	-5556	15.71	15.71	9.42	9.42	-18.76	370.1
44	165	-15170	1071	-438	0	28	-5563	15.71	15.71	9.42	9.42	-18.53	-243.8
45	165	-11800	1335	-73	0	-25	-4854	15.71	15.71	9.42	9.42	-16.26	246.4
46	165	-10551	1108	-310	0	23	-4124	15.71	15.71	9.42	9.42	-13.78	193.4
47	165	-9728	955	-269	0	24	-3640	15.71	15.71	9.42	9.42	-12.14	-159.3
49	165	-9550	1098	-279	0	22	-3782	15.71	15.71	9.42	9.42	-12.65	181.2
50	165	-10400	902	-282	0	25	-3784	15.71	15.71	9.42	9.42	-12.60	-165.9
51	165	-9729	954	-209	0	14	-3642	15.71	15.71	9.42	9.42	-12.14	-159.4

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	248	-12670	2012	-507	0	433	-4764	15.71	15.71	9.42	9.42	-15.89	209.5
41	248	-13200	1722	-476	0	412	-4636	15.71	15.71	9.42	9.42	-15.41	-203.7
42	248	-13210	1720	-296	0	236	-4641	15.71	15.71	9.42	9.42	-15.42	-203.9
43	248	-10254	1821	-425	0	363	-3959	15.71	15.71	9.42	9.42	-13.22	182.0
44	248	-14510	1301	-438	0	390	-4585	15.71	15.71	9.42	9.42	-15.17	-202.8
45	248	-11140	1335	-73	0	35	-3752	15.71	15.71	9.42	9.42	-12.44	-165.2
46	248	-9892	1108	-310	0	279	-3210	15.71	15.71	9.42	9.42	-10.63	-141.7
47	248	-9066	955	-269	0	246	-2853	15.71	15.71	9.42	9.42	-9.44	-126.2
49	248	-8890	1052	-279	0	252	-2896	15.71	15.71	9.42	9.42	-9.59	-127.8
50	248	-9740	947	-282	0	258	-3022	15.71	15.71	9.42	9.42	-9.99	-133.8
51	248	-9068	954	-209	0	187	-2854	15.71	15.71	9.42	9.42	-9.44	-126.3

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	330	-12010	1874	-507	0	851	-3162	15.71	15.71	9.42	9.42	-10.48	-142.5
41	330	-12540	1722	-476	0	804	-3216	15.71	15.71	9.42	9.42	-10.67	-145.5
42	330	-12550	1720	-296	0	480	-3222	15.71	15.71	9.42	9.42	-10.69	-145.8
43	330	-9595	1592	-425	0	714	-2551	15.71	15.71	9.42	9.42	-8.45	-114.8
44	330	-13850	1530	-438	0	751	-3417	15.71	15.71	9.42	9.42	-11.38	-155.6
45	330	-10480	1335	-73	0	95	-2650	15.71	15.71	9.42	9.42	-8.80	-120.2
46	330	-9232	1108	-310	0	535	-2295	15.71	15.71	9.42	9.42	-7.64	-104.4
47	330	-8405	955	-269	0	467	-2065	15.71	15.71	9.42	9.42	-6.88	-94.1
49	330	-8230	1006	-279	0	483	-2047	15.71	15.71	9.42	9.42	-6.81	-93.1
50	330	-9080	993	-282	0	490	-2221	15.71	15.71	9.42	9.42	-7.40	-101.3
51	330	-8408	954	-209	0	359	-2067	15.71	15.71	9.42	9.42	-6.88	-94.2

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 21 NI 221 NF 223 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 27C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-12890	3385	-1431	0	-2661	-13360	15.71	15.71	9.42	9.42	-44.83	1437.6

41	0	-13660	2280	-1311	0	-2402	-10600	15.71	15.71	9.42	9.42	-35.82	990.6
42	0	-13780	2344	-1111	0	-2064	-10850	15.71	15.71	9.42	9.42	-36.65	1022.6
43	0	-10640	3622	-1245	0	-2411	-13000	15.71	15.71	9.42	9.42	-43.40	1484.8
44	0	-15310	515	-1154	0	-2039	-6354	15.71	15.71	9.42	9.42	-21.30	326.9
45	0	-12130	1887	-711	0	-1417	-8815	15.71	15.71	9.42	9.42	-29.82	791.2
46	0	-10880	1479	-885	0	-1728	-7075	15.71	15.71	9.42	9.42	-23.95	587.8
47	0	-10190	1279	-779	0	-1560	-6194	15.71	15.71	9.42	9.42	-20.97	487.9
49	0	-9931	1648	-819	0	-1646	-7116	15.71	15.71	9.42	9.42	-24.07	632.9
50	0	-10870	1026	-800	0	-1571	-5786	15.71	15.71	9.42	9.42	-19.56	403.7
51	0	-10230	1301	-712	0	-1447	-6278	15.71	15.71	9.42	9.42	-21.25	498.5

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	83	-12230	3247	-1431	0	-1480	-10625	15.71	15.71	9.42	9.42	-35.82	1055.9
41	83	-13000	2280	-1311	0	-1320	-8719	15.71	15.71	9.42	9.42	-29.51	741.1
42	83	-13120	2344	-1111	0	-1148	-8916	15.71	15.71	9.42	9.42	-30.18	764.9
43	83	-9980	3393	-1245	0	-1384	-10108	15.71	15.71	9.42	9.42	-33.94	1077.4
44	83	-14650	745	-1154	0	-1088	-5834	15.71	15.71	9.42	9.42	-19.51	281.9
45	83	-11471	1887	-711	0	-830	-7258	15.71	15.71	9.42	9.42	-24.57	590.5
46	83	-10220	1479	-885	0	-998	-5855	15.71	15.71	9.42	9.42	-19.81	438.1
47	83	-9530	1279	-779	0	-918	-5139	15.71	15.71	9.42	9.42	-17.37	363.2
49	83	-9271	1602	-819	0	-970	-5775	15.71	15.71	9.42	9.42	-19.55	464.2
50	83	-10209	1072	-800	0	-911	-4920	15.71	15.71	9.42	9.42	-16.59	308.2
51	83	-9570	1301	-712	0	-860	-5205	15.71	15.71	9.42	9.42	-17.60	371.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	165	-11570	3110	-1431	0	-299	-8004	15.71	15.71	9.42	9.42	-27.09	695.3
41	165	-12340	2280	-1311	0	-239	-6838	15.71	15.71	9.42	9.42	-23.13	496.3
42	165	-12460	2344	-1111	0	-231	-6982	15.71	15.71	9.42	9.42	-23.62	512.0
43	165	-9320	3164	-1245	0	-356	-7405	15.71	15.71	9.42	9.42	-25.01	701.4
44	165	-13990	974	-1154	0	-136	-5125	15.71	15.71	9.42	9.42	-17.07	-224.6
45	165	-10812	1887	-711	0	-244	-5701	15.71	15.71	9.42	9.42	-19.27	394.0
46	165	-9561	1479	-885	0	-268	-4634	15.71	15.71	9.42	9.42	-15.63	292.2
47	165	-8869	1279	-779	0	-275	-4084	15.71	15.71	9.42	9.42	-13.75	242.0
49	165	-8611	1556	-819	0	-295	-4473	15.71	15.71	9.42	9.42	-15.11	304.3
50	165	-9548	1118	-800	0	-250	-4017	15.71	15.71	9.42	9.42	-13.47	210.8
51	165	-8910	1301	-712	0	-272	-4132	15.71	15.71	9.42	9.42	-13.91	247.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	248	-10910	2972	-1431	0	882	-5496	15.71	15.71	9.42	9.42	-18.56	361.9
41	248	-11680	2280	-1311	0	843	-4958	15.71	15.71	9.42	9.42	-16.63	263.5
42	248	-11800	2344	-1111	0	686	-5048	15.71	15.71	9.42	9.42	-16.94	271.3
43	248	-8661	2934	-1245	0	671	-4891	15.71	15.71	9.42	9.42	-16.55	361.2
44	248	-13330	1204	-1154	0	816	-4227	15.71	15.71	9.42	9.42	-13.99	-186.9
45	248	-10153	1887	-711	0	343	-4144	15.71	15.71	9.42	9.42	-13.88	208.0
46	248	-8902	1479	-885	0	463	-3414	15.71	15.71	9.42	9.42	-11.40	155.3
47	248	-8208	1279	-779	0	368	-3028	15.71	15.71	9.42	9.42	-10.09	-132.6
49	248	-7951	1510	-819	0	381	-3208	15.71	15.71	9.42	9.42	-10.74	158.2
50	248	-8886	1164	-800	0	410	-3075	15.71	15.71	9.42	9.42	-10.21	-135.2
51	248	-8250	1301	-712	0	315	-3058	15.71	15.71	9.42	9.42	-10.19	-133.9

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	330	-10250	2835	-1431	0	2063	-3102	15.71	15.71	9.42	9.42	-12.92	147.1
41	330	-11020	2280	-1311	0	1924	-3077	15.71	15.71	9.42	9.42	-12.05	-139.4
42	330	-11140	2344	-1111	0	1602	-3114	15.71	15.71	9.42	9.42	-10.29	-139.3
43	330	-8001	2705	-1245	0	1698	-2566	15.71	15.71	9.42	9.42	-10.63	130.3
44	330	-12670	1433	-1154	0	1767	-3139	15.71	15.71	9.42	9.42	-11.13	-142.8
45	330	-9494	1887	-711	0	930	-2587	15.71	15.71	9.42	9.42	-8.56	-116.1
46	330	-8242	1479	-885	0	1193	-2194	15.71	15.71	9.42	9.42	-7.50	-98.7
47	330	-7548	1279	-779	0	1010	-1973	15.71	15.71	9.42	9.42	-6.54	-89.0
49	330	-7291	1464	-819	0	1056	-1981	15.71	15.71	9.42	9.42	-6.64	-88.9
50	330	-8225	1210	-800	0	1070	-2096	15.71	15.71	9.42	9.42	-6.96	-94.9
51	330	-7590	1301	-712	0	902	-1985	15.71	15.71	9.42	9.42	-6.58	-89.5

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 22 NI 264 NF 266 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 25C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-9408	425	-326	0	-934	-984	6.28	6.28	9.42	9.42	-15.30	-168.0
41	0	-8091	-14	-276	0	-833	-220	6.28	6.28	9.42	9.42	-7.87	-108.5
42	0	-7922	-12	-306	0	-622	-221	6.28	6.28	9.42	9.42	-6.82	-95.2
43	0	-9655	787	-386	0	-898	-1589	6.28	6.28	9.42	9.42	-25.01	307.7
44	0	-6024	-752	-192	0	-683	1067	6.28	6.28	9.42	9.42	-16.83	225.4
45	0	-7179	60	-353	0	-378	-316	6.28	6.28	9.42	9.42	-6.35	-80.8
46	0	-7084	98	-321	0	-666	-371	6.28	6.28	9.42	9.42	-6.81	-91.4
47	0	-6832	126	-332	0	-625	-409	6.28	6.28	9.42	9.42	-7.07	-87.2
49	0	-7270	272	-348	0	-659	-664	6.28	6.28	9.42	9.42	-10.38	-118.2
50	0	-6544	-36	-310	0	-616	-133	6.28	6.28	9.42	9.42	-6.10	-84.5
51	0	-6775	127	-342	0	-555	-410	6.28	6.28	9.42	9.42	-7.05	-86.7

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	95	-8980	345	-326	0	-625	-618	6.28	6.28	9.42	9.42	-10.17	-122.7
41	95	-7664	-14	-276	0	-570	-233	6.28	6.28	9.42	9.42	-6.45	-90.3
42	95	-7494	-12	-221	0	-373	-232	6.28	6.28	9.42	9.42	-5.73	-77.8
43	95	-9228	655	-386	0	-531	-904	6.28	6.28	9.42	9.42	-14.07	-157.3
44	95	-5596	-620	-192	0	-500	415	6.28	6.28	9.42	9.42	-6.69	-79.7
45	95	-6752	60	-212	0	-111	-259	6.28	6.28	9.42	9.42	-5.62	-72.4
46	95	-6656	98	-321	0	-362	-279	6.28	6.28	9.42	9.42	-5.75	-73.5
47	95	-6404	126	-332	0	-310	-290	6.28	6.28	9.42	9.42	-5.74	-72.7
49	95	-6842	246	-348	0	-328	-418	6.28	6.28	9.42	9.42	-7.17	-88.0
50	95	-6116	-9	-310	0	-322	-155	6.28	6.28	9.42	9.42	-4.54	-64.5
51	95	-6348	127	-314	0	-244	-289	6.28	6.28	9.42	9.42	-5.71	-72.3

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	190	-8553	266	-326	0	-315	-328	6.28	6.28	9.42	9.42	-7.12	-91.7
41	190	-7236	-14	-276	0	-308	-247	6.28	6.28	9.42	9.42	-5.74	-74.8

42	190	-7067	-12	-148	0	-199	-243	6.28	6.28	9.42	9.42	-5.63	-73.2
43	190	-8800	523	-386	0	-164	-344	6.28	6.28	9.42	9.42	-7.38	-95.0
44	190	-5169	-488	-192	0	-318	-112	6.28	6.28	9.42	9.42	-4.05	-57.1
45	190	-6324	60	-90	0	31	-202	6.28	6.28	9.42	9.42	-4.89	-64.1
46	190	-6229	98	-321	0	-57	-186	6.28	6.28	9.42	9.42	-4.70	-61.9
47	190	-5977	126	-332	0	6	-170	6.28	6.28	9.42	9.42	-4.43	-58.7
49	190	-6415	219	-348	0	3	-197	6.28	6.28	9.42	9.42	-4.89	-64.3
50	190	-5689	17	-310	0	-28	-151	6.28	6.28	9.42	9.42	-4.12	-54.8
51	190	-5920	127	-289	0	42	-169	6.28	6.28	9.42	9.42	-4.39	-58.2

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	285	-8126	187	-326	0	-6	-113	6.28	6.28	9.42	9.42	-4.94	-68.9
41	285	-6808	-14	-276	0	-45	-261	6.28	6.28	9.42	9.42	-5.67	-73.0
42	285	-6640	-12	-88	0	-88	-254	6.28	6.28	9.42	9.42	-5.52	-71.2
43	285	-8372	391	-386	0	203	91	6.28	6.28	9.42	9.42	-5.14	-74.8
44	285	-4742	-356	-192	0	-136	-513	6.28	6.28	9.42	9.42	-7.98	-86.8
45	285	-5896	60	10	0	67	-145	6.28	6.28	9.42	9.42	-4.16	-55.8
46	285	-5802	98	-321	0	248	-93	6.28	6.28	9.42	9.42	-4.05	-57.9
47	285	-5550	126	-332	0	321	-51	6.28	6.28	9.42	9.42	-4.26	-60.2
49	285	-5988	193	-348	0	334	-1	6.28	6.28	9.42	9.42	-4.54	-64.2
50	285	-5262	43	-310	0	266	-122	6.28	6.28	9.42	9.42	-3.86	-54.9
51	285	-5492	127	-269	0	307	-49	6.28	6.28	9.42	9.42	-4.16	-58.9

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	380	-7698	108	-326	0	304	27	6.28	6.28	9.42	9.42	-5.26	-75.4
41	380	-6381	-14	-276	0	218	-275	6.28	6.28	9.42	9.42	-5.59	-71.2
42	380	-6212	-12	-39	0	-28	-265	6.28	6.28	9.42	9.42	-5.42	-69.1
43	380	-7945	259	-386	0	571	400	6.28	6.28	9.42	9.42	-7.49	-93.9
44	380	-4314	-224	-192	0	46	-789	6.28	6.28	9.42	9.42	-12.46	172.6
45	380	-5469	60	91	0	17	-87	6.28	6.28	9.42	9.42	-3.43	-47.4
46	380	-5374	98	-321	0	553	0	6.28	6.28	9.42	9.42	-5.22	-72.1
47	380	-5122	126	-332	0	637	69	6.28	6.28	9.42	9.42	-5.50	-75.1
49	380	-5560	166	-348	0	665	169	6.28	6.28	9.42	9.42	-5.84	-80.0
50	380	-4834	70	-310	0	560	-69	6.28	6.28	9.42	9.42	-4.99	-68.4
51	380	-5065	127	-253	0	555	72	6.28	6.28	9.42	9.42	-5.08	-69.8

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 23 NI 298 NF 271 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 20C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-10770	915	-133	0	-2025	-1483	6.28	6.28	12.57	12.57	-12.45	-163.8
41	0	-11170	-229	-160	0	-1943	549	6.28	6.28	12.57	12.57	-12.00	-159.4
42	0	-11100	-231	-520	0	-1303	553	6.28	6.28	12.57	12.57	-8.97	-122.8
43	0	-9783	1730	-71	0	-1609	-2945	6.28	6.28	12.57	12.57	-23.90	406.5
44	0	-12060	-2150	-214	0	-1892	3959	6.28	6.28	12.57	12.57	-32.06	581.6
45	0	-10340	-181	-716	0	-406	448	6.28	6.28	12.57	12.57	-5.94	-80.8
46	0	-10010	-148	-90	0	-1190	377	6.28	6.28	12.57	12.57	-8.15	-111.5
47	0	-9718	-127	-73	0	-1002	334	6.28	6.28	12.57	12.57	-7.34	-101.2
49	0	-9586	254	-64	0	-1029	-344	6.28	6.28	12.57	12.57	-7.39	-101.6
50	0	-10040	-521	-92	0	-1086	1037	6.28	6.28	12.57	12.57	-8.98	-113.9
51	0	-9697	-128	-193	0	-789	335	6.28	6.28	12.57	12.57	-6.57	-91.5

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	95	-10200	915	-133	0	-1898	-614	6.28	6.28	12.57	12.57	-11.67	-153.8
41	95	-10599	-229	-160	0	-1790	331	6.28	6.28	12.57	12.57	-11.10	-147.8
42	95	-10531	-231	-352	0	-891	334	6.28	6.28	12.57	12.57	-7.26	-100.9
43	95	-9213	1730	-71	0	-1542	-1302	6.28	6.28	12.57	12.57	-10.75	-129.9
44	95	-11490	-2150	-214	0	-1688	1917	6.28	6.28	12.57	12.57	-15.71	-184.0
45	95	-9769	-181	-435	0	138	276	6.28	6.28	12.57	12.57	-4.88	-68.1
46	95	-9440	-148	-90	0	-1104	236	6.28	6.28	12.57	12.57	-7.61	-104.2
47	95	-9148	-127	-73	0	-933	213	6.28	6.28	12.57	12.57	-6.87	-94.8
49	95	-9016	254	-64	0	-969	-102	6.28	6.28	12.57	12.57	-6.95	-95.6
50	95	-9470	-521	-92	0	-998	542	6.28	6.28	12.57	12.57	-7.23	-99.6
51	95	-9127	-128	-137	0	-633	214	6.28	6.28	12.57	12.57	-5.79	-81.2

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	190	-9631	915	-133	0	-1772	256	6.28	6.28	12.57	12.57	-10.90	-143.8
41	190	-10028	-229	-160	0	-1638	113	6.28	6.28	12.57	12.57	-10.20	-136.3
42	190	-9962	-231	-208	0	-627	114	6.28	6.28	12.57	12.57	-6.09	-85.8
43	190	-8643	1730	-71	0	-1474	341	6.28	6.28	12.57	12.57	-9.12	-121.4
44	190	-10920	-2150	-214	0	-1484	-126	6.28	6.28	12.57	12.57	-9.66	-131.1
45	190	-9198	-181	-195	0	434	104	6.28	6.28	12.57	12.57	-5.11	-72.7
46	190	-8869	-148	-90	0	-1018	96	6.28	6.28	12.57	12.57	-7.08	-97.0
47	190	-8578	-127	-73	0	-864	92	6.28	6.28	12.57	12.57	-6.41	-88.4
49	190	-8446	254	-64	0	-908	140	6.28	6.28	12.57	12.57	-6.51	-89.6
50	190	-8900	-521	-92	0	-910	46	6.28	6.28	12.57	12.57	-6.70	-92.3
51	190	-8557	-128	-88	0	-527	92	6.28	6.28	12.57	12.57	-5.19	-73.2

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	285	-9062	915	-133	0	-1646	1126	6.28	6.28	12.57	12.57	-10.13	-133.9
41	285	-9458	-229	-160	0	-1486	-105	6.28	6.28	12.57	12.57	-9.31	-124.9
42	285	-9392	-231	-88	0	-489	-105	6.28	6.28	12.57	12.57	-5.38	-76.3
43	285	-8073	1730	-71	0	-1406	1984	6.28	6.28	12.57	12.57	-16.17	228.4
44	285	-10350	-2150	-214	0	-1281	-2168	6.28	6.28	12.57	12.57	-17.70	206.5
45	285	-8626	-181	5	0	521	-68	6.28	6.28	12.57	12.57	-5.20	-73.3
46	285	-8298	-148	-90	0	-933	-44	6.28	6.28	12.57	12.57	-6.55	-89.9
47	285	-8008	-127	-73	0	-794	-29	6.28	6.28	12.57	12.57	-5.94	-82.0
49	285	-7876	254	-64	0	-848	381	6.28	6.28	12.57	12.57	-6.08	-83.6
50	285	-8331	-521	-92	0	-823	-449	6.28	6.28	12.57	12.57	-6.16	-85.1
51	285	-7987	-128	-49	0	-462	-29	6.28	6.28	12.57	12.57	-4.74	-67.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	380	-8492	915	-133	0	-1519	1995	6.28	6.28	12.57	12.57	-16.27	218.8
41	380	-8887	-229	-160	0	-1333	-322	6.28	6.28	12.57	12.57	-8.44	-113.7
42	380	-8823	-231	8	0	-453	-325	6.28	6.28	12.57	12.57	-5.03	-71.4

43	380	-7503	1730	-71	0	-1339	3627	6.28	6.28	12.57	12.57	-29.02	652.8
44	380	-9780	-2150	-214	0	-1077	-4210	6.28	6.28	12.57	12.57	-33.81	720.6
45	380	-8055	-181	164	0	437	-240	6.28	6.28	12.57	12.57	-4.68	-66.3
46	380	-7728	-148	-90	0	-847	-184	6.28	6.28	12.57	12.57	-6.02	-82.7
47	380	-7438	-127	-73	0	-725	-150	6.28	6.28	12.57	12.57	-5.47	-75.6
49	380	-7306	254	-64	0	-787	623	6.28	6.28	12.57	12.57	-5.74	-77.6
50	380	-7761	-521	-92	0	-735	-944	6.28	6.28	12.57	12.57	-7.92	-98.2
51	380	-7417	-128	-17	0	-432	-150	6.28	6.28	12.57	12.57	-4.41	-62.3

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 24 NI 78 NF 77 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 6B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-25680	301	50	0	81	10890	15.71	15.71	9.42	9.42	-36.53	578.0
41	0	-22420	-1031	9	0	-6	12590	15.71	15.71	9.42	9.42	-42.60	925.1
42	0	-22540	-931	200	0	447	12360	15.71	15.71	9.42	9.42	-41.80	888.0
43	0	-25860	1392	87	0	168	7441	15.71	15.71	9.42	9.42	-24.59	-331.8
44	0	-17440	-3285	-62	0	-155	15820	15.71	15.71	9.42	9.42	-53.28	1605.8
45	0	-20620	-662	336	0	778	9885	15.71	15.71	9.42	9.42	-33.32	615.2
46	0	-19230	-707	24	0	39	8874	15.71	15.71	9.42	9.42	-29.88	527.3
47	0	-18440	-626	27	0	51	7945	15.71	15.71	9.42	9.42	-26.67	431.2
49	0	-19520	-182	41	0	80	7379	15.71	15.71	9.42	9.42	-24.61	327.5
50	0	-17840	-1118	11	0	16	9055	15.71	15.71	9.42	9.42	-30.58	601.2
51	0	-18470	-593	91	0	202	7868	15.71	15.71	9.42	9.42	-26.40	420.3

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	110	-24800	48	50	0	25	11083	15.71	15.71	9.42	9.42	-37.27	632.0
41	110	-21540	-1031	9	0	-16	11456	15.71	15.71	9.42	9.42	-38.72	798.6
42	110	-21660	-931	200	0	227	11336	15.71	15.71	9.42	9.42	-38.31	777.4
43	110	-24980	970	87	0	71	8740	15.71	15.71	9.42	9.42	-29.04	-384.0
44	110	-16560	-2862	-62	0	-87	12439	15.71	15.71	9.42	9.42	-42.05	1140.0
45	110	-19740	-662	336	0	408	9156	15.71	15.71	9.42	9.42	-30.83	547.6
46	110	-18350	-707	24	0	13	8096	15.71	15.71	9.42	9.42	-27.21	453.9
47	110	-17560	-626	27	0	21	7256	15.71	15.71	9.42	9.42	-24.31	370.9
49	110	-18640	-267	41	0	35	7132	15.71	15.71	9.42	9.42	-23.80	323.0
50	110	-16960	-1033	11	0	3	7872	15.71	15.71	9.42	9.42	-26.51	471.2
51	110	-17590	-593	91	0	102	7216	15.71	15.71	9.42	9.42	-24.17	364.8

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	220	-23920	-206	50	0	-30	10998	15.71	15.71	9.42	9.42	-37.02	650.5
41	220	-20660	-1031	9	0	-26	10322	15.71	15.71	9.42	9.42	-34.84	673.5
42	220	-20780	-931	200	0	8	10312	15.71	15.71	9.42	9.42	-34.80	667.8
43	220	-24100	547	87	0	-25	9574	15.71	15.71	9.42	9.42	-32.02	460.8
44	220	-15680	-2440	-62	0	-19	9523	15.71	15.71	9.42	9.42	-32.24	749.7
45	220	-18860	-662	336	0	38	8428	15.71	15.71	9.42	9.42	-28.34	480.6
46	220	-17470	-707	24	0	-13	7318	15.71	15.71	9.42	9.42	-24.53	381.6
47	220	-16680	-626	27	0	-9	6566	15.71	15.71	9.42	9.42	-21.95	311.6
49	220	-17760	-351	41	0	-11	6792	15.71	15.71	9.42	9.42	-22.67	307.4
50	220	-16080	-949	11	0	-10	6782	15.71	15.71	9.42	9.42	-22.75	357.2
51	220	-16710	-593	91	0	2	6563	15.71	15.71	9.42	9.42	-21.94	310.2

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	330	-23040	-459	50	0	-85	10633	15.71	15.71	9.42	9.42	-35.80	631.9
41	330	-19780	-1031	9	0	-35	9188	15.71	15.71	9.42	9.42	-30.94	550.4
42	330	-19900	-931	200	0	-212	9288	15.71	15.71	9.42	9.42	-31.28	559.7
43	330	-23220	125	87	0	-121	9943	15.71	15.71	9.42	9.42	-33.37	535.1
44	330	-14800	-2018	-62	0	48	7072	15.71	15.71	9.42	9.42	-23.84	438.4
45	330	-17980	-662	336	0	-332	7700	15.71	15.71	9.42	9.42	-25.84	414.4
46	330	-16590	-707	24	0	-39	6539	15.71	15.71	9.42	9.42	-21.86	310.9
47	330	-15800	-626	27	0	-39	5877	15.71	15.71	9.42	9.42	-19.59	-257.3
49	330	-16880	-436	41	0	-56	6359	15.71	15.71	9.42	9.42	-21.21	280.6
50	330	-15200	-864	11	0	-22	5785	15.71	15.71	9.42	9.42	-19.30	259.7
51	330	-15830	-593	91	0	-98	5910	15.71	15.71	9.42	9.42	-19.70	-258.7

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	440	-22160	-712	50	0	-141	9990	15.71	15.71	9.42	9.42	-33.60	576.2
41	440	-18900	-1031	9	0	-45	8054	15.71	15.71	9.42	9.42	-27.03	430.5
42	440	-19020	-931	200	0	-431	8264	15.71	15.71	9.42	9.42	-27.75	453.8
43	440	-22340	-298	87	0	-217	9848	15.71	15.71	9.42	9.42	-33.10	551.5
44	440	-13920	-1595	-62	0	116	5085	15.71	15.71	9.42	9.42	-16.93	-222.9
45	440	-17100	-662	336	0	-701	6971	15.71	15.71	9.42	9.42	-23.34	349.2
46	440	-15710	-707	24	0	-65	5761	15.71	15.71	9.42	9.42	-19.19	-252.4
47	440	-14920	-626	27	0	-70	5188	15.71	15.71	9.42	9.42	-17.23	-228.0
49	440	-16000	-520	41	0	-102	5833	15.71	15.71	9.42	9.42	-19.42	-255.7
50	440	-14320	-780	11	0	-35	4881	15.71	15.71	9.42	9.42	-16.20	-214.8
51	440	-14950	-593	91	0	-198	5258	15.71	15.71	9.42	9.42	-17.47	-231.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 25 NI 121 NF 120 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 5B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-27960	-410	-71	0	-201	17880	15.71	15.71	9.42	9.42	-60.53	1466.8
41	0	-24660	-1924	-77	0	-209	21150	15.71	15.71	9.42	9.42	-71.32	2088.2
42	0	-24690	-1926	115	0	245	21180	15.71	15.71	9.42	9.42	-71.42	2091.3
43	0	-27740	998	-47	0	-146	11600	15.71	15.71	9.42	9.42	-38.89	603.4
44	0	-19680	-4514	-91	0	-228	27320	15.71	15.71	9.42	9.42	-90.83	3243.3
45	0	-22280	-1529	262	0	597	17110	15.71	15.71	9.42	9.42	-57.82	1589.1
46	0	-20770	-1286	-48	0	-130	14590	15.71	15.71	9.42	9.42	-49.37	1280.7

47	0	-19800	-1127	-40	0	-110	12950	15.71	15.71	9.42	9.42	-43.84	1080.6
49	0	-20900	-622	-38	0	-107	11860	15.71	15.71	9.42	9.42	-40.13	880.0
50	0	-19290	-1725	-47	0	-123	15000	15.71	15.71	9.42	9.42	-50.68	1403.5
51	0	-19810	-1128	24	0	42	12960	15.71	15.71	9.42	9.42	-43.87	1081.7

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	110	-27080	-663	-71	0	-123	17288	15.71	15.71	9.42	9.42	-58.53	1416.4
41	110	-23780	-1924	-77	0	-124	19032	15.71	15.71	9.42	9.42	-64.27	1810.5
42	110	-23810	-1926	115	0	118	19062	15.71	15.71	9.42	9.42	-64.38	1813.7
43	110	-26860	576	-47	0	-93	12464	15.71	15.71	9.42	9.42	-41.97	745.8
44	110	-18800	-4092	-91	0	-128	22586	15.71	15.71	9.42	9.42	-75.44	2565.3
45	110	-21400	-1529	262	0	308	15428	15.71	15.71	9.42	9.42	-52.19	1377.6
46	110	-19890	-1286	-48	0	-77	13174	15.71	15.71	9.42	9.42	-44.60	1109.7
47	110	-18920	-1127	-40	0	-65	11710	15.71	15.71	9.42	9.42	-39.65	936.2
49	110	-20020	-707	-38	0	-65	11129	15.71	15.71	9.42	9.42	-37.65	810.0
50	110	-18410	-1640	-47	0	-72	13150	15.71	15.71	9.42	9.42	-44.49	1167.2
51	110	-18930	-1128	24	0	15	11720	15.71	15.71	9.42	9.42	-39.68	937.2

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	220	-26200	-916	-71	0	-46	16418	15.71	15.71	9.42	9.42	-55.58	1325.6
41	220	-22900	-1924	-77	0	-39	16915	15.71	15.71	9.42	9.42	-57.20	1534.1
42	220	-22930	-1926	115	0	-9	16945	15.71	15.71	9.42	9.42	-57.30	1537.2
43	220	-25980	153	-47	0	-41	12864	15.71	15.71	9.42	9.42	-43.41	831.1
44	220	-17920	-3670	-91	0	-28	18316	15.71	15.71	9.42	9.42	-61.48	1959.7
45	220	-20520	-1529	262	0	20	13745	15.71	15.71	9.42	9.42	-46.53	1167.2
46	220	-19010	-1286	-48	0	-24	11759	15.71	15.71	9.42	9.42	-39.81	939.7
47	220	-18040	-1127	-40	0	-21	10470	15.71	15.71	9.42	9.42	-35.44	792.7
49	220	-19140	-791	-38	0	-23	10304	15.71	15.71	9.42	9.42	-34.84	727.1
50	220	-17530	-1556	-47	0	-20	11393	15.71	15.71	9.42	9.42	-38.57	946.1
51	220	-18050	-1128	24	0	-11	10479	15.71	15.71	9.42	9.42	-35.47	793.6

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	330	-25320	-1170	-71	0	32	15268	15.71	15.71	9.42	9.42	-51.69	1194.8
41	330	-22020	-1924	-77	0	46	14798	15.71	15.71	9.42	9.42	-50.09	1259.5
42	330	-22050	-1926	115	0	-136	14828	15.71	15.71	9.42	9.42	-50.19	1262.6
43	330	-25100	-269	-47	0	11	12799	15.71	15.71	9.42	9.42	-43.23	854.0
44	330	-17040	-3247	-91	0	72	14511	15.71	15.71	9.42	9.42	-48.94	1427.4
45	330	-19640	-1529	262	0	-269	12062	15.71	15.71	9.42	9.42	-40.84	958.4
46	330	-18130	-1286	-48	0	28	10343	15.71	15.71	9.42	9.42	-35.00	771.2
47	330	-17160	-1127	-40	0	24	9230	15.71	15.71	9.42	9.42	-31.21	650.7
49	330	-18260	-876	-38	0	19	9387	15.71	15.71	9.42	9.42	-31.71	631.8
50	330	-16650	-1472	-47	0	31	9728	15.71	15.71	9.42	9.42	-32.93	741.0
51	330	-17170	-1128	24	0	-37	9238	15.71	15.71	9.42	9.42	-31.24	651.6

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	440	-24440	-1423	-71	0	110	13840	15.71	15.71	9.42	9.42	-46.83	1024.9
41	440	-21140	-1924	-77	0	132	12680	15.71	15.71	9.42	9.42	-42.92	987.8
42	440	-21170	-1926	115	0	-263	12710	15.71	15.71	9.42	9.42	-43.03	991.0
43	440	-24220	-691	-47	0	63	12270	15.71	15.71	9.42	9.42	-41.43	812.9
44	440	-16160	-2825	-91	0	172	11170	15.71	15.71	9.42	9.42	-37.80	969.7
45	440	-18760	-1529	262	0	-558	10380	15.71	15.71	9.42	9.42	-35.11	752.2
46	440	-17250	-1286	-48	0	81	8928	15.71	15.71	9.42	9.42	-30.16	605.2
47	440	-16280	-1127	-40	0	68	7990	15.71	15.71	9.42	9.42	-26.96	511.0
49	440	-17380	-960	-38	0	61	8377	15.71	15.71	9.42	9.42	-28.25	524.7
50	440	-15770	-1387	-47	0	83	8157	15.71	15.71	9.42	9.42	-27.56	552.6
51	440	-16290	-1128	24	0	-63	7998	15.71	15.71	9.42	9.42	-26.98	511.8

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 26 NI 164 NF 163 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 4B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	

40	0	-28260	-614	-80	0	-237	19480	15.71	15.71	9.42	9.42	-65.93	1688.0
41	0	-24850	-2198	-83	0	-233	23130	15.71	15.71	9.42	9.42	-77.84	2376.3
42	0	-24790	-2186	90	0	178	22980	15.71	15.71	9.42	9.42	-77.34	2356.5
43	0	-28060	898	-62	0	-192	12530	15.71	15.71	9.42	9.42	-42.13	713.8
44	0	-19700	-4917	-89	0	-231	30010	15.71	15.71	9.42	9.42	-99.47	3651.4
45	0	-22290	-1723	221	0	500	18360	15.71	15.71	9.42	9.42	-61.97	1774.5
46	0	-20900	-1470	-57	0	-156	15920	15.71	15.71	9.42	9.42	-53.81	1471.4
47	0	-19920	-1288	-50	0	-137	14120	15.71	15.71	9.42	9.42	-47.77	1246.9
49	0	-21050	-760	-50	0	-138	12900	15.71	15.71	9.42	9.42	-43.67	1023.1
50	0	-19380	-1923	-55	0	-146	16390	15.71	15.71	9.42	9.42	-55.29	1606.5
51	0	-19900	-1284	7	0	-0	14060	15.71	15.71	9.42	9.42	-47.57	1238.9

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	110	-27380	-867	-80	0	-148	18666	15.71	15.71	9.42	9.42	-63.18	1605.0
41	110	-23970	-2198	-83	0	-142	20712	15.71	15.71	9.42	9.42	-69.83	2052.8
42	110	-23910	-2186	90	0	80	20575	15.71	15.71	9.42	9.42	-69.38	2034.8
43	110	-27180	475	-62	0	-123	13287	15.71	15.71	9.42	9.42	-44.82	846.0
44	110	-18820	-4494	-89	0	-134	24836	15.71	15.71	9.42	9.42	-82.70	2905.6
45	110	-21410	-1723	221	0	258	16465	15.71	15.71	9.42	9.42	-55.64	1530.5
46	110	-20020	-1470	-57	0	-94	14303	15.71	15.71	9.42	9.42	-48.39	1269.7
47	110	-19040	-1288	-50	0	-82	12702	15.71	15.71	9.42	9.42	-43.00	1075.5
49	110	-20170	-844	-50	0	-84	12017	15.71	15.71	9.42	9.42	-40.68	930.9
50	110	-18500	-1838	-55	0	-86	14323	15.71	15.71	9.42	9.42	-48.40	1336.6
51	110	-19020	-1284	7	0	-8	12649	15.71	15.71	9.42	9.42	-42.82	1068.5

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	220	-26500	-1121	-80	0	-60	17573	15.71	15.71	9.42	9.42	-59.49	1481.3
41	220	-23090	-2198	-83	0	-51	18295	15.71	15.71	9.42	9.42	-61.80	1730.5
42	220	-23030	-2186	90	0	-19	18170	15.71	15.71	9.42	9.42	-61.38	1714.4
43	220	-26300	53	-62	0	-54	13579	15.71	15.71	9.42	9.42	-45.87	918.2
44	220	-17940	-4072	-89	0	-36	20126	15.71	15.71	9.42	9.42	-67.37	2232.0
45	220	-20530	-1723	221	0	15	14570	15.71	15.71	9.42	9.42	-49.29	1287.7
46	220	-19140	-1470	-57	0	-31	12686	15.71	15.71	9.42	9.42	-42.94	1069.0
47	220	-18160	-1288	-50	0	-26	11285	15.71	15.71	9.42	9.42	-38.21	905.1

49	220	-19290	-929	-50	0	-29	11042	15.71	15.71	9.42	9.42	-37.37	825.8
50	220	-17620	-1754	-55	0	-26	12348	15.71	15.71	9.42	9.42	-41.78	1082.2
51	220	-18140	-1284	7	0	-16	11238	15.71	15.71	9.42	9.42	-38.05	899.1

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	330	-25620	-1374	-80	0	28	16201	15.71	15.71	9.42	9.42	-54.85	1317.5
41	330	-22210	-2198	-83	0	40	15878	15.71	15.71	9.42	9.42	-53.71	1410.0
42	330	-22150	-2186	90	0	-117	15765	15.71	15.71	9.42	9.42	-53.34	1396.0
43	330	-25420	-369	-62	0	14	13407	15.71	15.71	9.42	9.42	-45.31	926.7
44	330	-17060	-3650	-89	0	61	15881	15.71	15.71	9.42	9.42	-53.44	1631.6
45	330	-19650	-1723	221	0	-228	12675	15.71	15.71	9.42	9.42	-42.91	1046.7
46	330	-18260	-1470	-57	0	31	11069	15.71	15.71	9.42	9.42	-37.47	870.0
47	330	-17280	-1288	-50	0	29	9867	15.71	15.71	9.42	9.42	-33.39	736.3
49	330	-18410	-1013	-50	0	25	9973	15.71	15.71	9.42	9.42	-33.72	708.1
50	330	-16740	-1670	-55	0	34	10467	15.71	15.71	9.42	9.42	-35.44	843.6
51	330	-17260	-1284	7	0	-23	9826	15.71	15.71	9.42	9.42	-33.25	731.2

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	440	-24740	-1628	-80	0	116	14550	15.71	15.71	9.42	9.42	-49.25	1114.6
41	440	-21330	-2198	-83	0	131	13460	15.71	15.71	9.42	9.42	-45.57	1092.8
42	440	-21270	-2186	90	0	-216	13360	15.71	15.71	9.42	9.42	-45.23	1080.7
43	440	-24540	-792	-62	0	83	12770	15.71	15.71	9.42	9.42	-43.15	870.5
44	440	-16180	-3227	-89	0	158	12100	15.71	15.71	9.42	9.42	-40.91	1105.9
45	440	-18770	-1723	221	0	-471	10780	15.71	15.71	9.42	9.42	-36.48	808.6
46	440	-17380	-1470	-57	0	94	9452	15.71	15.71	9.42	9.42	-31.96	673.7
47	440	-16400	-1288	-50	0	85	8450	15.71	15.71	9.42	9.42	-28.54	570.1
49	440	-17530	-1098	-50	0	80	8812	15.71	15.71	9.42	9.42	-29.75	578.9
50	440	-15860	-1585	-55	0	95	8678	15.71	15.71	9.42	9.42	-29.35	622.2
51	440	-16380	-1284	7	0	-31	8415	15.71	15.71	9.42	9.42	-28.42	566.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 27 NI 207 NF 206 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 3B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-27760	-377	-98	0	-267	17370	15.71	15.71	9.42	9.42	-58.81	1400.9
41	0	-24440	-1947	-93	0	-248	21090	15.71	15.71	9.42	9.42	-71.11	2088.8
42	0	-24440	-1949	64	0	135	21100	15.71	15.71	9.42	9.42	-71.14	2090.3
43	0	-27590	1075	-84	0	-232	10780	15.71	15.71	9.42	9.42	-36.02	505.3
44	0	-19430	-4631	-88	0	-223	28010	15.71	15.71	9.42	9.42	-93.01	3359.7
45	0	-22050	-1545	186	0	438	17000	15.71	15.71	9.42	9.42	-57.45	1582.6
46	0	-20610	-1298	-67	0	-173	14520	15.71	15.71	9.42	9.42	-49.13	1277.0
47	0	-19650	-1135	-60	0	-154	12870	15.71	15.71	9.42	9.42	-43.57	1075.1
49	0	-20760	-612	-62	0	-160	11630	15.71	15.71	9.42	9.42	-39.35	852.7
50	0	-19130	-1753	-63	0	-158	15080	15.71	15.71	9.42	9.42	-50.94	1422.2
51	0	-19650	-1136	-8	0	-26	12880	15.71	15.71	9.42	9.42	-43.60	1076.5

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	110	-26880	-631	-98	0	-159	16816	15.71	15.71	9.42	9.42	-56.93	1355.9
41	110	-23560	-1947	-93	0	-146	18950	15.71	15.71	9.42	9.42	-63.99	1807.7
42	110	-23560	-1949	64	0	64	18958	15.71	15.71	9.42	9.42	-64.01	1808.8
43	110	-26710	653	-84	0	-139	11732	15.71	15.71	9.42	9.42	-39.42	653.8
44	110	-18550	-4208	-88	0	-126	23148	15.71	15.71	9.42	9.42	-77.22	2661.9
45	110	-21170	-1545	186	0	234	15300	15.71	15.71	9.42	9.42	-51.75	1368.5
46	110	-19730	-1298	-67	0	-99	13092	15.71	15.71	9.42	9.42	-44.32	1104.1
47	110	-18770	-1135	-60	0	-87	11622	15.71	15.71	9.42	9.42	-39.35	929.4
49	110	-19880	-697	-62	0	-92	10911	15.71	15.71	9.42	9.42	-36.90	784.6
50	110	-18250	-1668	-63	0	-89	13197	15.71	15.71	9.42	9.42	-44.64	1180.8
51	110	-18770	-1136	-8	0	-17	11629	15.71	15.71	9.42	9.42	-39.37	930.5

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	220	-26000	-884	-98	0	-52	15983	15.71	15.71	9.42	9.42	-54.11	1270.7
41	220	-22680	-1947	-93	0	-43	16810	15.71	15.71	9.42	9.42	-56.84	1527.8
42	220	-22680	-1949	64	0	-6	16815	15.71	15.71	9.42	9.42	-56.86	1528.6
43	220	-25830	230	-84	0	-47	12219	15.71	15.71	9.42	9.42	-41.18	748.6
44	220	-17670	-3786	-88	0	-29	18751	15.71	15.71	9.42	9.42	-62.87	2036.5
45	220	-20290	-1545	186	0	29	13600	15.71	15.71	9.42	9.42	-46.04	1155.4
46	220	-18850	-1298	-67	0	-25	11664	15.71	15.71	9.42	9.42	-39.49	932.3
47	220	-17890	-1135	-60	0	-21	10374	15.71	15.71	9.42	9.42	-35.11	784.8
49	220	-19000	-781	-62	0	-24	10099	15.71	15.71	9.42	9.42	-34.14	703.6
50	220	-17370	-1584	-63	0	-20	11408	15.71	15.71	9.42	9.42	-38.62	954.8
51	220	-17890	-1136	-8	0	-9	10378	15.71	15.71	9.42	9.42	-35.13	785.5

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	330	-25120	-1138	-98	0	56	14871	15.71	15.71	9.42	9.42	-50.34	1145.6
41	330	-21800	-1947	-93	0	60	14670	15.71	15.71	9.42	9.42	-49.66	1249.9
42	330	-21800	-1949	64	0	-77	14672	15.71	15.71	9.42	9.42	-49.66	1250.2
43	330	-24950	-192	-84	0	45	12242	15.71	15.71	9.42	9.42	-41.30	782.7
44	330	-16790	-3364	-88	0	68	14818	15.71	15.71	9.42	9.42	-49.94	1484.2
45	330	-19410	-1545	186	0	-176	11900	15.71	15.71	9.42	9.42	-40.29	944.1
46	330	-17970	-1298	-67	0	48	10235	15.71	15.71	9.42	9.42	-34.63	762.0
47	330	-17010	-1135	-60	0	46	9125	15.71	15.71	9.42	9.42	-30.85	641.7
49	330	-18120	-866	-62	0	44	9194	15.71	15.71	9.42	9.42	-31.05	610.1
50	330	-16490	-1500	-63	0	49	9711	15.71	15.71	9.42	9.42	-32.87	744.7
51	330	-17010	-1136	-8	0	-0	9128	15.71	15.71	9.42	9.42	-30.86	642.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	440	-24240	-1391	-98	0	163	13480	15.71	15.71	9.42	9.42	-45.60	981.5
41	440	-20920	-1947	-93	0	163	12530	15.71	15.71	9.42	9.42	-42.42	975.0
42	440	-20920	-1949	64	0	-148	12530	15.71	15.71	9.42	9.42	-42.42	975.0
43	440	-24070	-615	-84	0	138	11800	15.71	15.71	9.42	9.42	-39.81	753.7
44	440	-15910	-2941	-88	0	165	11350	15.71	15.71	9.42	9.42	-38.40	1006.6
45	440	-18530	-1545	186	0	-380	10200	15.71	15.71	9.42	9.42	-34.50	735.5
46	440	-17090	-1298	-67	0	122	8807	15.71	15.71	9.42	9.42	-29.75	594.3
47	440	-16130	-1135	-60	0	112	7877	15.71	15.71	9.42	9.42	-26.57	500.9
49	440	-17240	-950	-62	0	112	8196	15.71	15.71	9.42	9.42	-27.62	505.1

50	440	-15610	-1415	-63	0	118	8107	15.71	15.71	9.42	9.42	-27.39	551.5
51	440	-16130	-1136	-8	0	8	7877	15.71	15.71	9.42	9.42	-26.57	500.9

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 28 NI 250 NF 249 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 2B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-26260	543	-33	0	-234	9709	15.71	15.71	9.42	9.42	-32.35	-425.2
41	0	-23010	-1016	-24	0	-168	13180	15.71	15.71	9.42	9.42	-44.60	986.3
42	0	-23120	-1023	131	0	202	13380	15.71	15.71	9.42	9.42	-45.28	1010.5
43	0	-26350	1791	-41	0	-251	4889	15.71	15.71	9.42	9.42	-17.30	-241.0
44	0	-18050	-3649	-8	0	-63	19400	15.71	15.71	9.42	9.42	-65.02	2117.4
45	0	-21120	-819	233	0	475	11010	15.71	15.71	9.42	9.42	-37.20	752.0
46	0	-19680	-681	-26	0	-125	9177	15.71	15.71	9.42	9.42	-30.91	552.4
47	0	-18850	-597	-26	0	-115	8175	15.71	15.71	9.42	9.42	-27.45	447.8
49	0	-19940	-78	-29	0	-137	7017	15.71	15.71	9.42	9.42	-23.32	-308.2
50	0	-18280	-1166	-23	0	-99	9919	15.71	15.71	9.42	9.42	-33.54	705.4
51	0	-18890	-600	25	0	8	8241	15.71	15.71	9.42	9.42	-27.68	455.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	110	-25380	289	-33	0	-197	10166	15.71	15.71	9.42	9.42	-34.01	495.7
41	110	-22130	-1016	-24	0	-142	12063	15.71	15.71	9.42	9.42	-40.79	861.7
42	110	-22240	-1023	131	0	58	12254	15.71	15.71	9.42	9.42	-41.45	884.5
43	110	-25470	1369	-41	0	-206	6627	15.71	15.71	9.42	9.42	-21.97	-299.2
44	110	-17170	-3226	-8	0	-54	15619	15.71	15.71	9.42	9.42	-52.59	1587.6
45	110	-20240	-819	233	0	218	10108	15.71	15.71	9.42	9.42	-34.12	659.3
46	110	-18800	-681	-26	0	-97	8428	15.71	15.71	9.42	9.42	-28.34	482.6
47	110	-17970	-597	-26	0	-86	7518	15.71	15.71	9.42	9.42	-25.21	391.3
49	110	-19060	-162	-29	0	-104	6885	15.71	15.71	9.42	9.42	-22.91	-302.0
50	110	-17400	-1081	-23	0	-74	8683	15.71	15.71	9.42	9.42	-29.31	565.9
51	110	-18010	-600	25	0	-20	7581	15.71	15.71	9.42	9.42	-25.43	398.2

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	220	-24500	36	-33	0	-161	10345	15.71	15.71	9.42	9.42	-34.70	545.7
41	220	-21250	-1016	-24	0	-116	10946	15.71	15.71	9.42	9.42	-36.97	738.2
42	220	-21360	-1023	131	0	-87	11128	15.71	15.71	9.42	9.42	-37.60	759.5
43	220	-24590	946	-41	0	-161	7900	15.71	15.71	9.42	9.42	-26.15	-349.1
44	220	-16290	-2804	-8	0	-45	12303	15.71	15.71	9.42	9.42	-41.59	1131.2
45	220	-19360	-819	233	0	-38	9206	15.71	15.71	9.42	9.42	-31.03	567.5
46	220	-17920	-681	-26	0	-69	7678	15.71	15.71	9.42	9.42	-25.77	413.6
47	220	-17090	-597	-26	0	-57	6861	15.71	15.71	9.42	9.42	-22.96	335.7
49	220	-18180	-247	-29	0	-72	6660	15.71	15.71	9.42	9.42	-22.18	-291.9
50	220	-16520	-997	-23	0	-49	7541	15.71	15.71	9.42	9.42	-25.38	441.9
51	220	-17130	-600	25	0	-48	6922	15.71	15.71	9.42	9.42	-23.17	342.1

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	330	-23620	-218	-33	0	-124	10245	15.71	15.71	9.42	9.42	-34.41	561.2
41	330	-20370	-1016	-24	0	-90	9828	15.71	15.71	9.42	9.42	-33.14	616.3
42	330	-20480	-1023	131	0	-231	10002	15.71	15.71	9.42	9.42	-33.74	636.1
43	330	-23710	524	-41	0	-116	8709	15.71	15.71	9.42	9.42	-29.01	-381.6
44	330	-15410	-2382	-8	0	-37	9451	15.71	15.71	9.42	9.42	-32.00	750.0
45	330	-18480	-819	233	0	-294	8305	15.71	15.71	9.42	9.42	-27.93	477.1
46	330	-17040	-681	-26	0	-41	6929	15.71	15.71	9.42	9.42	-23.20	345.8
47	330	-16210	-597	-26	0	-28	6204	15.71	15.71	9.42	9.42	-20.71	281.1
49	330	-17300	-331	-29	0	-40	6343	15.71	15.71	9.42	9.42	-21.12	-277.9
50	330	-15640	-912	-23	0	-24	6491	15.71	15.71	9.42	9.42	-21.75	333.9
51	330	-16250	-600	25	0	-76	6262	15.71	15.71	9.42	9.42	-20.91	287.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	440	-22740	-471	-33	0	-87	9866	15.71	15.71	9.42	9.42	-33.13	540.7
41	440	-19490	-1016	-24	0	-64	8711	15.71	15.71	9.42	9.42	-29.29	496.8
42	440	-19600	-1023	131	0	-375	8876	15.71	15.71	9.42	9.42	-29.86	515.0
43	440	-22830	102	-41	0	-71	9053	15.71	15.71	9.42	9.42	-30.27	434.5
44	440	-14530	-1959	-8	0	-28	7064	15.71	15.71	9.42	9.42	-23.82	446.9
45	440	-17600	-819	233	0	-551	7403	15.71	15.71	9.42	9.42	-24.83	388.4
46	440	-16160	-681	-26	0	-13	6180	15.71	15.71	9.42	9.42	-20.63	279.7
47	440	-15330	-597	-26	0	0	5547	15.71	15.71	9.42	9.42	-18.46	-243.3
49	440	-16420	-416	-29	0	-8	5932	15.71	15.71	9.42	9.42	-19.74	-260.2
50	440	-14760	-828	-23	0	1	5534	15.71	15.71	9.42	9.42	-18.45	242.2
51	440	-15370	-600	25	0	-104	5602	15.71	15.71	9.42	9.42	-18.65	-245.6

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 29 NI 293 NF 292 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 1B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-14820	554	-433	0	-658	-1029	6.28	6.28	9.42	9.42	-16.89	-203.5
41	0	-15040	-40	-342	0	-430	-25	6.28	6.28	9.42	9.42	-9.52	-138.0
42	0	-14800	-38	-375	0	-150	-26	6.28	6.28	9.42	9.42	-8.13	-120.2
43	0	-13780	932	-449	0	-728	-1665	6.28	6.28	9.42	9.42	-25.94	-272.8
44	0	-15550	-1025	-199	0	-65	1641	6.28	6.28	9.42	9.42	-25.52	-279.4
45	0	-13760	-55	-352	0	118	6	6.28	6.28	9.42	9.42	-7.46	-110.5
46	0	-13630	-68	-270	0	-300	28	6.28	6.28	9.42	9.42	-8.22	-119.9
47	0	-13280	-75	-253	0	-267	42	6.28	6.28	9.42	9.42	-7.90	-115.4
49	0	-13200	123	-283	0	-343	-293	6.28	6.28	9.42	9.42	-9.03	-122.0
50	0	-13550	-268	-233	0	-210	368	6.28	6.28	9.42	9.42	-9.89	-131.4
51	0	-13200	-74	-264	0	-174	41	6.28	6.28	9.42	9.42	-7.43	-109.5

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	97	-14380	441	-433	0	-236	-544	6.28	6.28	9.42	9.42	-11.90	-153.5
41	97	-14602	-40	-342	0	-96	-64	6.28	6.28	9.42	9.42	-7.78	-115.6
42	97	-14362	-38	-288	0	172	-64	6.28	6.28	9.42	9.42	-8.01	-118.2
43	97	-13342	745	-449	0	-291	-848	6.28	6.28	9.42	9.42	-14.32	-174.9
44	97	-15112	-838	-199	0	128	733	6.28	6.28	9.42	9.42	-13.99	-176.2
45	97	-13322	-55	-207	0	389	-47	6.28	6.28	9.42	9.42	-8.47	-122.7
46	97	-13190	-68	-270	0	-36	-38	6.28	6.28	9.42	9.42	-6.80	-101.5
47	97	-12840	-75	-253	0	-21	-31	6.28	6.28	9.42	9.42	-6.55	-98.1
49	97	-12762	86	-283	0	-67	-191	6.28	6.28	9.42	9.42	-7.88	-109.5
50	97	-13112	-231	-233	0	16	125	6.28	6.28	9.42	9.42	-7.45	-105.9
51	97	-12760	-74	-234	0	69	-31	6.28	6.28	9.42	9.42	-6.73	-100.2

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	195	-13940	329	-433	0	187	-169	6.28	6.28	9.42	9.42	-8.24	-115.9
41	195	-14165	-40	-342	0	237	-103	6.28	6.28	9.42	9.42	-8.21	-120.4
42	195	-13925	-38	-213	0	416	-101	6.28	6.28	9.42	9.42	-8.90	-128.7
43	195	-12905	557	-449	0	147	-213	6.28	6.28	9.42	9.42	-8.16	-112.5
44	195	-14675	-650	-199	0	322	8	6.28	6.28	9.42	9.42	-8.85	-129.1
45	195	-12885	-55	-83	0	529	-101	6.28	6.28	9.42	9.42	-8.89	-127.3
46	195	-12750	-68	-270	0	228	-104	6.28	6.28	9.42	9.42	-7.45	-109.2
47	195	-12400	-75	-253	0	225	-104	6.28	6.28	9.42	9.42	-7.26	-106.4
49	195	-12325	48	-283	0	208	-126	6.28	6.28	9.42	9.42	-7.15	-104.9
50	195	-12675	-193	-233	0	244	-82	6.28	6.28	9.42	9.42	-7.48	-109.5
51	195	-12320	-74	-210	0	285	-103	6.28	6.28	9.42	9.42	-7.49	-109.2

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	292	-13500	217	-433	0	609	97	6.28	6.28	9.42	9.42	-9.57	-136.6
41	292	-13728	-40	-342	0	571	-142	6.28	6.28	9.42	9.42	-9.51	-136.1
42	292	-13488	-38	-151	0	593	-139	6.28	6.28	9.42	9.42	-9.49	-135.5
43	292	-12468	370	-449	0	585	239	6.28	6.28	9.42	9.42	-8.94	-127.4
44	292	-14238	-463	-199	0	516	-534	6.28	6.28	9.42	9.42	-11.75	-151.6
45	292	-12448	-55	21	0	557	-154	6.28	6.28	9.42	9.42	-8.80	-125.7
46	292	-12310	-68	-270	0	492	-170	6.28	6.28	9.42	9.42	-8.43	-120.9
47	292	-11960	-75	-253	0	472	-177	6.28	6.28	9.42	9.42	-8.17	-117.1
49	292	-11888	11	-283	0	484	-97	6.28	6.28	9.42	9.42	-8.19	-117.3
50	292	-12238	-156	-233	0	470	-252	6.28	6.28	9.42	9.42	-8.30	-119.1
51	292	-11880	-74	-189	0	479	-176	6.28	6.28	9.42	9.42	-8.16	-116.9

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	390	-13060	104	-433	0	1032	254	6.28	6.28	9.42	9.42	-11.27	-157.3
41	390	-13290	-40	-342	0	905	-180	6.28	6.28	9.42	9.42	-10.81	-151.8
42	390	-13050	-38	-102	0	715	-176	6.28	6.28	9.42	9.42	-9.82	-139.2
43	390	-12030	183	-449	0	1023	508	6.28	6.28	9.42	9.42	-10.72	-149.1
44	390	-13800	-276	-199	0	710	-894	6.28	6.28	9.42	9.42	-15.00	-182.7
45	390	-12010	-55	104	0	495	-208	6.28	6.28	9.42	9.42	-8.30	-118.8
46	390	-11870	-68	-270	0	755	-236	6.28	6.28	9.42	9.42	-9.41	-132.6
47	390	-11520	-75	-253	0	718	-250	6.28	6.28	9.42	9.42	-9.07	-127.8
49	390	-11450	-27	-283	0	760	-105	6.28	6.28	9.42	9.42	-9.22	-129.7
50	390	-11800	-118	-233	0	698	-386	6.28	6.28	9.42	9.42	-9.21	-128.8
51	390	-11440	-74	-172	0	655	-248	6.28	6.28	9.42	9.42	-8.74	-123.6

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 30 NI 77 NF 76 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 6C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN		daN*m			cm^2				daN/cm^2	
40	0	-18160	-809	174	0	97	9467	15.71	15.71	9.42	9.42	-31.99	646.6
41	0	-14850	-1133	181	0	82	7468	15.71	15.71	9.42	9.42	-25.21	490.8
42	0	-14950	-1145	235	0	100	7660	15.71	15.71	9.42	9.42	-25.87	513.7
43	0	-18370	-362	136	0	92	9334	15.71	15.71	9.42	9.42	-31.52	620.4
44	0	-9788	-1711	199	0	63	4398	15.71	15.71	9.42	9.42	-14.79	252.6
45	0	-13010	-922	238	0	98	6321	15.71	15.71	9.42	9.42	-21.32	399.6
46	0	-11640	-764	128	0	60	5122	15.71	15.71	9.42	9.42	-17.21	286.1
47	0	-10840	-672	114	0	55	4536	15.71	15.71	9.42	9.42	-15.21	236.2
49	0	-11940	-564	112	0	60	5202	15.71	15.71	9.42	9.42	-17.47	286.7
50	0	-10230	-834	125	0	54	4215	15.71	15.71	9.42	9.42	-14.12	214.5
51	0	-10870	-676	132	0	61	4600	15.71	15.71	9.42	9.42	-15.43	243.4

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	83	-17500	-1060	174	0	-47	8696	15.71	15.71	9.42	9.42	-29.35	564.0
41	83	-14190	-1133	181	0	-67	6533	15.71	15.71	9.42	9.42	-21.99	387.1
42	83	-14290	-1145	235	0	-94	6716	15.71	15.71	9.42	9.42	-22.62	408.1
43	83	-17710	-781	136	0	-20	8863	15.71	15.71	9.42	9.42	-29.92	579.3
44	83	-9128	-1292	199	0	-102	3159	15.71	15.71	9.42	9.42	-10.49	-138.9
45	83	-12350	-922	238	0	-99	5560	15.71	15.71	9.42	9.42	-18.70	320.1
46	83	-10980	-764	128	0	-45	4492	15.71	15.71	9.42	9.42	-15.04	226.2
47	83	-10179	-672	114	0	-40	3982	15.71	15.71	9.42	9.42	-13.30	187.0
49	83	-11280	-648	112	0	-33	4702	15.71	15.71	9.42	9.42	-15.76	243.5
50	83	-9569	-750	125	0	-49	3562	15.71	15.71	9.42	9.42	-11.87	-155.9
51	83	-10210	-676	132	0	-49	4042	15.71	15.71	9.42	9.42	-13.51	193.5

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	165	-16840	-1311	174	0	-190	7718	15.71	15.71	9.42	9.42	-25.98	454.7
41	165	-13530	-1133	181	0	-216	5598	15.71	15.71	9.42	9.42	-18.76	286.8
42	165	-13630	-1145	235	0	-289	5771	15.71	15.71	9.42	9.42	-19.36	305.6
43	165	-17050	-1200	136	0	-132	8046	15.71	15.71	9.42	9.42	-27.11	491.4
44	165	-8468	-873	199	0	-266	2266	15.71	15.71	9.42	9.42	-7.50	-101.9
45	165	-11690	-922	238	0	-296	4799	15.71	15.71	9.42	9.42	-16.08	242.9
46	165	-10320	-764	128	0	-150	3861	15.71	15.71	9.42	9.42	-12.87	-169.0
47	165	-9518	-672	114	0	-134	3427	15.71	15.71	9.42	9.42	-11.40	-150.3
49	165	-10620	-732	112	0	-125	4133	15.71	15.71	9.42	9.42	-13.81	192.5
50	165	-8908	-666	125	0	-152	2977	15.71	15.71	9.42	9.42	-9.87	-131.2
51	165	-9550	-676	132	0	-158	3484	15.71	15.71	9.42	9.42	-11.60	-152.7

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	248	-16180	-1563	174	0	-334	6532	15.71	15.71	9.42	9.42	-21.86	322.4
41	248	-12870	-1133	181	0	-366	4664	15.71	15.71	9.42	9.42	-15.52	-204.5
42	248	-12970	-1145	235	0	-483	4826	15.71	15.71	9.42	9.42	-16.09	-211.3
43	248	-16390	-1619	136	0	-244	6883	15.71	15.71	9.42	9.42	-23.08	360.2
44	248	-7808	-454	199	0	-431	1719	15.71	15.71	9.42	9.42	-5.82	-80.2
45	248	-11030	-922	238	0	-492	4038	15.71	15.71	9.42	9.42	-13.45	-177.0
46	248	-9660	-764	128	0	-256	3230	15.71	15.71	9.42	9.42	-10.71	-142.3
47	248	-8858	-672	114	0	-228	2872	15.71	15.71	9.42	9.42	-9.51	-126.8
49	248	-9961	-815	112	0	-218	3495	15.71	15.71	9.42	9.42	-11.61	-153.6
50	248	-8247	-582	125	0	-255	2462	15.71	15.71	9.42	9.42	-8.14	-109.4
51	248	-8891	-676	132	0	-267	2926	15.71	15.71	9.42	9.42	-9.70	-129.1

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	330	-15520	-1814	174	0	-478	5139	15.71	15.71	9.42	9.42	-17.03	-226.6
41	330	-12210	-1133	181	0	-515	3729	15.71	15.71	9.42	9.42	-12.33	-165.4
42	330	-12310	-1145	235	0	-677	3882	15.71	15.71	9.42	9.42	-12.84	-171.7
43	330	-15730	-2038	136	0	-356	5374	15.71	15.71	9.42	9.42	-17.84	-236.5
44	330	-7148	-35	199	0	-595	1518	15.71	15.71	9.42	9.42	-5.17	-71.5
45	330	-10370	-922	238	0	-689	3277	15.71	15.71	9.42	9.42	-10.84	-145.0
46	330	-9000	-764	128	0	-361	2600	15.71	15.71	9.42	9.42	-8.59	-115.9
47	330	-8197	-672	114	0	-323	2318	15.71	15.71	9.42	9.42	-7.66	-103.6
49	330	-9301	-899	112	0	-310	2788	15.71	15.71	9.42	9.42	-9.21	-123.8
50	330	-7586	-499	125	0	-358	2016	15.71	15.71	9.42	9.42	-6.68	-90.7
51	330	-8231	-676	132	0	-377	2368	15.71	15.71	9.42	9.42	-7.83	-105.6

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 31 NI 120 NF 119 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 5C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-20400	-1525	-12	0	-159	13360	15.71	15.71	9.42	9.42	-45.23	1115.9
41	0	-17090	-2061	33	0	-101	12280	15.71	15.71	9.42	9.42	-41.54	1094.2
42	0	-17130	-2067	75	0	-56	12330	15.71	15.71	9.42	9.42	-41.71	1099.9
43	0	-20170	-740	-39	0	-166	11650	15.71	15.71	9.42	9.42	-39.43	878.3
44	0	-12120	-3028	108	0	-6	10920	15.71	15.71	9.42	9.42	-36.78	1104.9
45	0	-14720	-1643	106	0	5	9924	15.71	15.71	9.42	9.42	-33.59	846.6
46	0	-13190	-1378	37	0	-49	8388	15.71	15.71	9.42	9.42	-28.40	685.1
47	0	-12220	-1207	38	0	-36	7414	15.71	15.71	9.42	9.42	-25.10	583.1
49	0	-13320	-1028	23	0	-56	7774	15.71	15.71	9.42	9.42	-26.31	591.5
50	0	-11710	-1486	52	0	-24	7629	15.71	15.71	9.42	9.42	-25.83	634.7
51	0	-12230	-1209	52	0	-22	7430	15.71	15.71	9.42	9.42	-25.15	585.1

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	83	-19740	-1776	-12	0	-149	11999	15.71	15.71	9.42	9.42	-40.62	945.2
41	83	-16430	-2061	33	0	-127	10580	15.71	15.71	9.42	9.42	-35.82	872.6
42	83	-16470	-2067	75	0	-119	10624	15.71	15.71	9.42	9.42	-35.97	877.4
43	83	-19510	-1159	-39	0	-134	10866	15.71	15.71	9.42	9.42	-36.76	792.3
44	83	-11459	-2609	108	0	-95	8595	15.71	15.71	9.42	9.42	-29.06	787.0
45	83	-14060	-1643	106	0	-83	8568	15.71	15.71	9.42	9.42	-29.01	676.4
46	83	-12530	-1378	37	0	-79	7251	15.71	15.71	9.42	9.42	-24.54	547.6
47	83	-11559	-1207	38	0	-67	6418	15.71	15.71	9.42	9.42	-21.71	466.6
49	83	-12660	-1112	23	0	-75	6891	15.71	15.71	9.42	9.42	-23.30	491.5
50	83	-11050	-1402	52	0	-67	6438	15.71	15.71	9.42	9.42	-21.79	489.1
51	83	-11570	-1209	52	0	-65	6432	15.71	15.71	9.42	9.42	-21.76	468.2

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	165	-19080	-2028	-12	0	-139	10430	15.71	15.71	9.42	9.42	-35.28	747.2
41	165	-15770	-2061	33	0	-154	8880	15.71	15.71	9.42	9.42	-30.04	654.2
42	165	-15810	-2067	75	0	-181	8919	15.71	15.71	9.42	9.42	-30.18	658.2
43	165	-18850	-1578	-39	0	-101	9737	15.71	15.71	9.42	9.42	-32.89	658.6
44	165	-10798	-2190	108	0	-184	6616	15.71	15.71	9.42	9.42	-22.40	524.6
45	165	-13400	-1643	106	0	-171	7212	15.71	15.71	9.42	9.42	-24.39	508.9
46	165	-11870	-1378	37	0	-110	6114	15.71	15.71	9.42	9.42	-20.65	412.3
47	165	-10898	-1207	38	0	-98	5422	15.71	15.71	9.42	9.42	-18.30	352.1
49	165	-12000	-1196	23	0	-93	5939	15.71	15.71	9.42	9.42	-20.04	383.4
50	165	-10390	-1318	52	0	-110	5315	15.71	15.71	9.42	9.42	-17.95	355.9
51	165	-10910	-1209	52	0	-107	5434	15.71	15.71	9.42	9.42	-18.34	353.4

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	248	-18420	-2279	-12	0	-129	8654	15.71	15.71	9.42	9.42	-29.16	525.8
41	248	-15110	-2061	33	0	-181	7180	15.71	15.71	9.42	9.42	-24.20	442.2
42	248	-15150	-2067	75	0	-243	7214	15.71	15.71	9.42	9.42	-24.31	445.3
43	248	-18190	-1997	-39	0	-69	8261	15.71	15.71	9.42	9.42	-27.80	481.1
44	248	-10138	-1770	108	0	-273	4983	15.71	15.71	9.42	9.42	-16.81	319.2
45	248	-12740	-1643	106	0	-259	5857	15.71	15.71	9.42	9.42	-19.72	346.4
46	248	-11210	-1378	37	0	-140	4977	15.71	15.71	9.42	9.42	-16.73	281.4
47	248	-10238	-1207	38	0	-129	4426	15.71	15.71	9.42	9.42	-14.86	241.4
49	248	-11340	-1280	23	0	-112	4917	15.71	15.71	9.42	9.42	-16.51	269.3
50	248	-9729	-1235	52	0	-153	4262	15.71	15.71	9.42	9.42	-14.32	236.7
51	248	-10249	-1209	52	0	-150	4437	15.71	15.71	9.42	9.42	-14.90	242.4

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	330	-17760	-2530	-12	0	-119	6671	15.71	15.71	9.42	9.42	-22.24	292.9
41	330	-14450	-2061	33	0	-208	5480	15.71	15.71	9.42	9.42	-18.28	244.6
42	330	-14490	-2067	75	0	-305	5508	15.71	15.71	9.42	9.42	-18.38	246.8
43	330	-17530	-2416	-39	0	-37	6440	15.71	15.71	9.42	9.42	-21.45	-282.2
44	330	-9477	-1351	108	0	-363	3695	15.71	15.71	9.42	9.42	-12.34	172.6
45	330	-12080	-1643	106	0	-347	4501	15.71	15.71	9.42	9.42	-15.00	-197.0
46	330	-10550	-1378	37	0	-170	3840	15.71	15.71	9.42	9.42	-12.78	-168.3
47	330	-9577	-1207	38	0	-160	3430	15.71	15.71	9.42	9.42	-11.41	-150.5
49	330	-10680	-1364	23	0	-131	3827	15.71	15.71	9.42	9.42	-12.73	-167.9
50	330	-9069	-1151	52	0	-196	3278	15.71	15.71	9.42	9.42	-10.91	-143.8
51	330	-9589	-1209	52	0	-193	3439	15.71	15.71	9.42	9.42	-11.44	-150.9

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 32 NI 163 NF 162 SEZ. Rp B= 0.400 H= 0.800 (pilastro)

PIL. NUM. 4C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-20650	-1665	-254	0	-379	13970	15.71	15.71	9.42	9.42	-47.28	1194.7
41	0	-17240	-2223	-216	0	-305	12900	15.71	15.71	9.42	9.42	-43.61	1179.4
42	0	-17180	-2200	-151	0	-220	12770	15.71	15.71	9.42	9.42	-43.18	1162.7
43	0	-20460	-832	-225	0	-352	12120	15.71	15.71	9.42	9.42	-41.03	934.2
44	0	-12080	-3233	-160	0	-192	11580	15.71	15.71	9.42	9.42	-38.94	1205.7
45	0	-14670	-1725	-52	0	-87	10130	15.71	15.71	9.42	9.42	-34.28	878.9
46	0	-13290	-1487	-128	0	-182	8807	15.71	15.71	9.42	9.42	-29.81	742.0
47	0	-12300	-1303	-106	0	-151	7784	15.71	15.71	9.42	9.42	-26.35	633.4
49	0	-13440	-1117	-119	0	-176	8140	15.71	15.71	9.42	9.42	-27.56	639.3
50	0	-11770	-1597	-106	0	-144	8032	15.71	15.71	9.42	9.42	-27.18	691.1
51	0	-12290	-1296	-84	0	-123	7742	15.71	15.71	9.42	9.42	-26.21	627.7

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	83	-19990	-1917	-254	0	-169	12492	15.71	15.71	9.42	9.42	-42.29	1006.4
41	83	-16580	-2223	-216	0	-126	11066	15.71	15.71	9.42	9.42	-37.46	937.2
42	83	-16520	-2200	-151	0	-96	10956	15.71	15.71	9.42	9.42	-37.09	923.6
43	83	-19800	-1252	-225	0	-166	11260	15.71	15.71	9.42	9.42	-38.10	837.1
44	83	-11421	-2814	-160	0	-60	9086	15.71	15.71	9.42	9.42	-30.69	861.4
45	83	-14010	-1725	-52	0	-44	8708	15.71	15.71	9.42	9.42	-29.48	698.6
46	83	-12630	-1487	-128	0	-76	7580	15.71	15.71	9.42	9.42	-25.66	590.8
47	83	-11641	-1303	-106	0	-63	6709	15.71	15.71	9.42	9.42	-22.70	504.8
49	83	-12780	-1201	-119	0	-78	7183	15.71	15.71	9.42	9.42	-24.30	528.3
50	83	-11109	-1513	-106	0	-56	6749	15.71	15.71	9.42	9.42	-22.85	531.4
51	83	-11629	-1296	-84	0	-53	6673	15.71	15.71	9.42	9.42	-22.58	500.2

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	165	-19330	-2168	-254	0	41	10806	15.71	15.71	9.42	9.42	-36.56	790.7
41	165	-15920	-2223	-216	0	52	9231	15.71	15.71	9.42	9.42	-31.24	698.4
42	165	-15860	-2200	-151	0	28	9142	15.71	15.71	9.42	9.42	-30.94	688.0
43	165	-19140	-1671	-225	0	19	10054	15.71	15.71	9.42	9.42	-33.98	692.1
44	165	-10762	-2394	-160	0	72	6938	15.71	15.71	9.42	9.42	-23.49	572.8
45	165	-13350	-1725	-52	0	-1	7286	15.71	15.71	9.42	9.42	-24.64	521.1
46	165	-11970	-1487	-128	0	30	6353	15.71	15.71	9.42	9.42	-21.47	442.0
47	165	-10982	-1303	-106	0	24	5634	15.71	15.71	9.42	9.42	-19.03	378.3
49	165	-12120	-1285	-119	0	21	6158	15.71	15.71	9.42	9.42	-20.79	409.3
50	165	-10448	-1430	-106	0	31	5535	15.71	15.71	9.42	9.42	-18.71	384.3
51	165	-10968	-1296	-84	0	17	5604	15.71	15.71	9.42	9.42	-18.93	374.8

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	248	-18670	-2420	-254	0	250	8913	15.71	15.71	9.42	9.42	-30.04	552.0
41	248	-15260	-2223	-216	0	230	7396	15.71	15.71	9.42	9.42	-24.94	466.3
42	248	-15200	-2200	-151	0	153	7328	15.71	15.71	9.42	9.42	-24.71	459.1
43	248	-18480	-2090	-225	0	205	8502	15.71	15.71	9.42	9.42	-28.62	503.3
44	248	-10103	-1975	-160	0	204	5136	15.71	15.71	9.42	9.42	-17.35	341.6
45	248	-12690	-1725	-52	0	42	5864	15.71	15.71	9.42	9.42	-19.74	349.0
46	248	-11310	-1487	-128	0	136	5126	15.71	15.71	9.42	9.42	-17.25	297.7
47	248	-10323	-1303	-106	0	112	4558	15.71	15.71	9.42	9.42	-15.32	255.8
49	248	-11460	-1369	-119	0	119	5063	15.71	15.71	9.42	9.42	-17.02	284.4
50	248	-9788	-1346	-106	0	119	4390	15.71	15.71	9.42	9.42	-14.76	251.5
51	248	-10306	-1296	-84	0	86	4536	15.71	15.71	9.42	9.42	-15.24	253.4

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	330	-18010	-2671	-254	0	460	6812	15.71	15.71	9.42	9.42	-22.72	302.6
41	330	-14600	-2223	-216	0	408	5562	15.71	15.71	9.42	9.42	-18.56	250.1
42	330	-14540	-2200	-151	0	277	5514	15.71	15.71	9.42	9.42	-18.40	246.1
43	330	-17820	-2509	-225	0	391	6605	15.71	15.71	9.42	9.42	-22.01	-289.2
44	330	-9444	-1556	-160	0	336	3680	15.71	15.71	9.42	9.42	-12.29	171.8
45	330	-12030	-1725	-52	0	85	4442	15.71	15.71	9.42	9.42	-14.80	-194.6
46	330	-10650	-1487	-128	0	242	3899	15.71	15.71	9.42	9.42	-12.98	-170.9
47	330	-9664	-1303	-106	0	200	3483	15.71	15.71	9.42	9.42	-11.59	-152.8
49	330	-10800	-1453	-119	0	217	3899	15.71	15.71	9.42	9.42	-12.97	-171.0
50	330	-9127	-1262	-106	0	206	3314	15.71	15.71	9.42	9.42	-11.03	-145.3
51	330	-9645	-1296	-84	0	156	3467	15.71	15.71	9.42	9.42	-11.53	-152.1

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 33 NI 206 NF 205 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 3C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-20220	-1465	-384	0	-540	13000	15.71	15.71	9.42	9.42	-44.01	1070.8
41	0	-16880	-2040	-336	0	-422	12070	15.71	15.71	9.42	9.42	-40.83	1072.1
42	0	-16880	-2039	-239	0	-293	12070	15.71	15.71	9.42	9.42	-40.83	1072.1
43	0	-20050	-656	-335	0	-512	11210	15.71	15.71	9.42	9.42	-37.92	820.4
44	0	-11830	-3070	-270	0	-242	10970	15.71	15.71	9.42	9.42	-36.92	1125.1
45	0	-14480	-1614	-93	0	-100	9669	15.71	15.71	9.42	9.42	-32.73	819.2
46	0	-13030	-1360	-207	0	-251	8232	15.71	15.71	9.42	9.42	-27.87	669.0
47	0	-12070	-1190	-175	0	-209	7271	15.71	15.71	9.42	9.42	-24.61	568.5
49	0	-13180	-998	-191	0	-248	7578	15.71	15.71	9.42	9.42	-25.65	569.0
50	0	-11540	-1481	-178	0	-194	7531	15.71	15.71	9.42	9.42	-25.50	627.4
51	0	-12070	-1190	-142	0	-166	7270	15.71	15.71	9.42	9.42	-24.61	568.4

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	83	-19560	-1716	-384	0	-223	11687	15.71	15.71	9.42	9.42	-39.56	907.5
41	83	-16220	-2040	-336	0	-145	10388	15.71	15.71	9.42	9.42	-35.17	853.2
42	83	-16220	-2039	-239	0	-96	10388	15.71	15.71	9.42	9.42	-35.17	853.2
43	83	-19390	-1075	-335	0	-236	10495	15.71	15.71	9.42	9.42	-35.49	744.5
44	83	-11171	-2651	-270	0	-19	8610	15.71	15.71	9.42	9.42	-29.10	801.4

45	83	-13820	-1614	-93	0	-23	8337	15.71	15.71	9.42	9.42	-28.22	652.6
46	83	-12370	-1360	-207	0	-81	7110	15.71	15.71	9.42	9.42	-24.06	533.7
47	83	-11409	-1190	-175	0	-64	6289	15.71	15.71	9.42	9.42	-21.27	454.1
49	83	-12520	-1082	-191	0	-91	6720	15.71	15.71	9.42	9.42	-22.72	472.7
50	83	-10879	-1397	-178	0	-47	6344	15.71	15.71	9.42	9.42	-21.47	482.3
51	83	-11409	-1190	-142	0	-48	6288	15.71	15.71	9.42	9.42	-21.27	454.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	165	-18900	-1968	-384	0	93	10166	15.71	15.71	9.42	9.42	-34.37	716.8
41	165	-15560	-2040	-336	0	133	8706	15.71	15.71	9.42	9.42	-29.45	637.6
42	165	-15560	-2039	-239	0	101	8706	15.71	15.71	9.42	9.42	-29.45	637.6
43	165	-18730	-1495	-335	0	40	9435	15.71	15.71	9.42	9.42	-31.85	621.2
44	165	-10512	-2232	-270	0	203	6596	15.71	15.71	9.42	9.42	-22.33	533.2
45	165	-13160	-1614	-93	0	53	7005	15.71	15.71	9.42	9.42	-23.68	488.8
46	165	-11710	-1360	-207	0	90	5988	15.71	15.71	9.42	9.42	-20.22	400.7
47	165	-10748	-1190	-175	0	80	5307	15.71	15.71	9.42	9.42	-17.91	341.8
49	165	-11860	-1166	-191	0	67	5792	15.71	15.71	9.42	9.42	-19.54	368.4
50	165	-10218	-1314	-178	0	99	5225	15.71	15.71	9.42	9.42	-17.65	349.7
51	165	-10748	-1190	-142	0	69	5306	15.71	15.71	9.42	9.42	-17.91	341.7

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	248	-18240	-2219	-384	0	410	8438	15.71	15.71	9.42	9.42	-28.41	503.0
41	248	-14900	-2040	-336	0	411	7025	15.71	15.71	9.42	9.42	-23.67	428.6
42	248	-14900	-2039	-239	0	298	7024	15.71	15.71	9.42	9.42	-23.67	428.5
43	248	-18070	-1914	-335	0	316	8028	15.71	15.71	9.42	9.42	-26.99	454.3
44	248	-9852	-1813	-270	0	426	4928	15.71	15.71	9.42	9.42	-16.63	321.9
45	248	-12500	-1614	-93	0	130	5673	15.71	15.71	9.42	9.42	-19.09	330.1
46	248	-11050	-1360	-207	0	261	4865	15.71	15.71	9.42	9.42	-16.35	272.0
47	248	-10086	-1190	-175	0	224	4325	15.71	15.71	9.42	9.42	-14.52	233.2
49	248	-11200	-1250	-191	0	224	4796	15.71	15.71	9.42	9.42	-16.10	258.1
50	248	-9558	-1230	-178	0	246	4176	15.71	15.71	9.42	9.42	-14.03	231.1
51	248	-10088	-1190	-142	0	186	4325	15.71	15.71	9.42	9.42	-14.52	233.1

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	330	-17580	-2470	-384	0	727	6503	15.71	15.71	9.42	9.42	-21.67	-284.8
41	330	-14240	-2040	-336	0	688	5343	15.71	15.71	9.42	9.42	-17.82	234.1
42	330	-14240	-2039	-239	0	495	5342	15.71	15.71	9.42	9.42	-17.81	234.0
43	330	-17410	-2333	-335	0	592	6276	15.71	15.71	9.42	9.42	-20.88	-275.3
44	330	-9193	-1394	-270	0	649	3605	15.71	15.71	9.42	9.42	-12.05	170.0
45	330	-11840	-1614	-93	0	206	4341	15.71	15.71	9.42	9.42	-14.46	-190.2
46	330	-10390	-1360	-207	0	432	3743	15.71	15.71	9.42	9.42	-12.45	-164.2
47	330	-9425	-1190	-175	0	368	3343	15.71	15.71	9.42	9.42	-11.11	-146.8
49	330	-10540	-1334	-191	0	381	3730	15.71	15.71	9.42	9.42	-12.40	-163.8
50	330	-8897	-1146	-178	0	392	3196	15.71	15.71	9.42	9.42	-10.63	-140.2
51	330	-9427	-1190	-142	0	304	3343	15.71	15.71	9.42	9.42	-11.11	-146.8

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 34 NI 249 NF 248 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 2C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN				daN*m		cm^2				daN/cm^2	
40	0	-18580	-634	-1065	0	-1079	9348	15.71	15.71	9.42	9.42	-31.56	614.7
41	0	-15310	-1178	-794	0	-758	8230	15.71	15.71	9.42	9.42	-27.83	579.9
42	0	-15420	-1211	-738	0	-643	8417	15.71	15.71	9.42	9.42	-28.47	602.1
43	0	-18690	-22	-1018	0	-1060	8457	15.71	15.71	9.42	9.42	-28.45	490.1
44	0	-10310	-2126	-379	0	-260	6649	15.71	15.71	9.42	9.42	-22.51	549.0
45	0	-13410	-984	-474	0	-334	6905	15.71	15.71	9.42	9.42	-23.32	465.5
46	0	-11980	-779	-431	0	-386	5610	15.71	15.71	9.42	9.42	-18.90	339.5
47	0	-11150	-680	-340	0	-293	4955	15.71	15.71	9.42	9.42	-16.66	280.5
49	0	-12240	-498	-430	0	-400	5328	15.71	15.71	9.42	9.42	-17.90	293.3
50	0	-10570	-919	-302	0	-240	4966	15.71	15.71	9.42	9.42	-16.73	301.7
51	0	-11190	-691	-321	0	-255	5017	15.71	15.71	9.42	9.42	-16.87	287.3

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	83	-17920	-886	-1065	0	-200	8721	15.71	15.71	9.42	9.42	-29.41	552.4
41	83	-14650	-1178	-794	0	-103	7258	15.71	15.71	9.42	9.42	-24.49	469.1
42	83	-14760	-1211	-738	0	-34	7418	15.71	15.71	9.42	9.42	-25.04	487.2
43	83	-18030	-441	-1018	0	-220	8266	15.71	15.71	9.42	9.42	-27.82	487.2
44	83	-9650	-1707	-379	0	53	5068	15.71	15.71	9.42	9.42	-17.13	348.8
45	83	-12750	-984	-474	0	57	6094	15.71	15.71	9.42	9.42	-20.54	377.9
46	83	-11320	-779	-431	0	-31	4967	15.71	15.71	9.42	9.42	-16.69	276.4
47	83	-10490	-680	-340	0	-13	4394	15.71	15.71	9.42	9.42	-14.73	229.2
49	83	-11580	-582	-430	0	-45	4882	15.71	15.71	9.42	9.42	-16.37	257.0
50	83	-9909	-835	-302	0	9	4242	15.71	15.71	9.42	9.42	-14.24	228.2
51	83	-10529	-691	-321	0	10	4447	15.71	15.71	9.42	9.42	-14.92	234.7

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	165	-17260	-1137	-1065	0	678	7887	15.71	15.71	9.42	9.42	-26.54	462.9
41	165	-13990	-1178	-794	0	553	6286	15.71	15.71	9.42	9.42	-21.14	360.9
42	165	-14100	-1211	-738	0	575	6418	15.71	15.71	9.42	9.42	-21.60	374.9
43	165	-17370	-860	-1018	0	620	7730	15.71	15.71	9.42	9.42	-25.99	438.3
44	165	-8990	-1288	-379	0	365	3833	15.71	15.71	9.42	9.42	-12.86	205.0
45	165	-12090	-984	-474	0	447	5282	15.71	15.71	9.42	9.42	-17.74	292.2
46	165	-10660	-779	-431	0	325	4324	15.71	15.71	9.42	9.42	-14.48	215.0
47	165	-9830	-680	-340	0	268	3834	15.71	15.71	9.42	9.42	-12.81	179.2
49	165	-10921	-666	-430	0	310	4367	15.71	15.71	9.42	9.42	-14.61	212.4
50	165	-9248	-751	-302	0	259	3588	15.71	15.71	9.42	9.42	-11.98	166.2
51	165	-9868	-691	-321	0	275	3878	15.71	15.71	9.42	9.42	-12.96	183.4

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	248	-16600	-1388	-1065	0	1557	6845	15.71	15.71	9.42	9.42	-22.93	348.8
41	248	-13330	-1178	-794	0	1208	5313	15.71	15.71	9.42	9.42	-17.77	257.1
42	248	-13440	-1211	-738	0	1184	5419	15.71	15.71	9.42	9.42	-18.14	267.0
43	248	-16710	-1279	-1018	0	1459	6847	15.71	15.71	9.42	9.42	-22.93	345.7
44	248	-8331	-869	-379	0	678	2944	15.71	15.71	9.42	9.42	-9.78	-129.3
45	248	-11430	-984	-474	0	838	4470	15.71	15.71	9.42	9.42	-14.94	209.9

46	248	-10000	-779	-431	0	680	3681	15.71	15.71	9.42	9.42	-12.26	-161.3
47	248	-9169	-680	-340	0	549	3273	15.71	15.71	9.42	9.42	-10.88	-143.6
49	248	-10262	-750	-430	0	665	3783	15.71	15.71	9.42	9.42	-12.60	-165.7
50	248	-8587	-668	-302	0	509	3002	15.71	15.71	9.42	9.42	-9.97	-131.9
51	248	-9206	-691	-321	0	540	3308	15.71	15.71	9.42	9.42	-11.00	-145.1

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	330	-15940	-1640	-1065	0	2436	5596	15.71	15.71	9.42	9.42	-18.60	-245.8
41	330	-12670	-1178	-794	0	1864	4341	15.71	15.71	9.42	9.42	-14.41	-191.0
42	330	-12780	-1211	-738	0	1793	4420	15.71	15.71	9.42	9.42	-14.68	-194.4
43	330	-16050	-1698	-1018	0	2299	5619	15.71	15.71	9.42	9.42	-18.67	-246.9
44	330	-7671	-449	-379	0	991	2400	15.71	15.71	9.42	9.42	-7.94	-106.2
45	330	-10770	-984	-474	0	1229	3659	15.71	15.71	9.42	9.42	-12.14	-161.1
46	330	-9340	-779	-431	0	1036	3038	15.71	15.71	9.42	9.42	-10.06	-134.1
47	330	-8509	-680	-340	0	829	2712	15.71	15.71	9.42	9.42	-8.98	-119.9
49	330	-9602	-834	-430	0	1020	3130	15.71	15.71	9.42	9.42	-10.37	-138.2
50	330	-7926	-584	-302	0	758	2486	15.71	15.71	9.42	9.42	-8.22	-110.0
51	330	-8545	-691	-321	0	806	2738	15.71	15.71	9.42	9.42	-9.06	-121.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 35 NI 302 NF 291 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 1D
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-9366	747	304	0	-830	-562	6.28	6.28	9.42	9.42	-9.70	-119.4
41	0	-9072	69	38	0	-874	373	6.28	6.28	9.42	9.42	-8.55	-118.3
42	0	-8909	59	-49	0	-937	379	6.28	6.28	9.42	9.42	-8.76	-120.6
43	0	-8727	1116	298	0	-857	-1122	6.28	6.28	9.42	9.42	-17.51	-180.7
44	0	-8708	-1062	-378	0	-939	1931	6.28	6.28	9.42	9.42	-30.58	503.0
45	0	-7966	-30	-290	0	-1036	446	6.28	6.28	9.42	9.42	-8.78	-119.7
46	0	-7737	-63	-256	0	-964	475	6.28	6.28	9.42	9.42	-8.32	-113.6
47	0	-7403	-96	-330	0	-987	500	6.28	6.28	9.42	9.42	-8.29	-112.8
49	0	-7501	130	-241	0	-972	188	6.28	6.28	9.42	9.42	-8.25	-112.5
50	0	-7497	-306	-376	0	-989	799	6.28	6.28	9.42	9.42	-12.43	-135.7
51	0	-7348	-100	-359	0	-1008	502	6.28	6.28	9.42	9.42	-8.38	-113.8

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	83	-8995	621	304	0	-1081	3	6.28	6.28	9.42	9.42	-9.47	-129.6
41	83	-8701	69	38	0	-906	430	6.28	6.28	9.42	9.42	-8.51	-117.3
42	83	-8538	59	25	0	-929	428	6.28	6.28	9.42	9.42	-8.53	-117.3
43	83	-8356	907	298	0	-1103	-287	6.28	6.28	9.42	9.42	-9.30	-126.6
44	83	-8337	-852	-378	0	-627	1141	6.28	6.28	9.42	9.42	-17.85	-180.6
45	83	-7595	-30	-168	0	-848	421	6.28	6.28	9.42	9.42	-7.69	-105.6
46	83	-7366	-63	-256	0	-753	423	6.28	6.28	9.42	9.42	-7.43	-98.5
47	83	-7032	-96	-330	0	-715	421	6.28	6.28	9.42	9.42	-7.27	-93.8
49	83	-7130	88	-241	0	-774	278	6.28	6.28	9.42	9.42	-7.11	-97.9
50	83	-7126	-264	-376	0	-678	564	6.28	6.28	9.42	9.42	-8.98	-105.6
51	83	-6977	-100	-334	0	-723	420	6.28	6.28	9.42	9.42	-7.24	-93.8

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	165	-8624	496	304	0	-1332	464	6.28	6.28	9.42	9.42	-10.69	-144.0
41	165	-8330	69	38	0	-938	488	6.28	6.28	9.42	9.42	-8.50	-116.3
42	165	-8166	59	88	0	-976	477	6.28	6.28	9.42	9.42	-8.57	-117.4
43	165	-7984	697	298	0	-1348	374	6.28	6.28	9.42	9.42	-10.62	-141.9
44	165	-7966	-643	-378	0	-315	525	6.28	6.28	9.42	9.42	-8.75	-106.3
45	165	-7224	-30	-62	0	-755	397	6.28	6.28	9.42	9.42	-7.12	-97.5
46	165	-6994	-63	-256	0	-542	371	6.28	6.28	9.42	9.42	-6.76	-84.4
47	165	-6660	-96	-330	0	-443	341	6.28	6.28	9.42	9.42	-6.33	-79.3
49	165	-6758	46	-241	0	-575	333	6.28	6.28	9.42	9.42	-6.31	-83.7
50	165	-6754	-222	-376	0	-368	363	6.28	6.28	9.42	9.42	-6.58	-82.0
51	165	-6606	-100	-313	0	-456	338	6.28	6.28	9.42	9.42	-6.27	-78.6

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	248	-8252	370	304	0	-1583	821	6.28	6.28	9.42	9.42	-12.77	-161.8
41	248	-7958	69	38	0	-969	545	6.28	6.28	9.42	9.42	-8.98	-115.5
42	248	-7795	59	141	0	-1072	526	6.28	6.28	9.42	9.42	-8.90	-120.9
43	248	-7613	488	298	0	-1594	863	6.28	6.28	9.42	9.42	-13.43	-160.3
44	248	-7594	-433	-378	0	-2	81	6.28	6.28	9.42	9.42	-4.39	-62.1
45	248	-6852	-30	25	0	-740	372	6.28	6.28	9.42	9.42	-6.82	-93.9
46	248	-6623	-63	-256	0	-331	318	6.28	6.28	9.42	9.42	-6.10	-76.9
47	248	-6289	-96	-330	0	-171	262	6.28	6.28	9.42	9.42	-5.42	-69.3
49	248	-6387	4	-241	0	-376	354	6.28	6.28	9.42	9.42	-6.32	-78.5
50	248	-6383	-180	-376	0	-58	197	6.28	6.28	9.42	9.42	-4.88	-64.1
51	248	-6234	-100	-296	0	-205	255	6.28	6.28	9.42	9.42	-5.34	-68.4

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	330	-7881	244	304	0	-1834	1074	6.28	6.28	9.42	9.42	-16.80	-181.8
41	330	-7587	69	38	0	-1001	602	6.28	6.28	9.42	9.42	-9.58	-114.9
42	330	-7424	59	183	0	-1206	575	6.28	6.28	9.42	9.42	-9.57	-128.3
43	330	-7242	278	298	0	-1839	1179	6.28	6.28	9.42	9.42	-18.55	225.2
44	330	-7223	-224	-378	0	310	-190	6.28	6.28	9.42	9.42	-5.22	-72.1
45	330	-6481	-30	95	0	-791	347	6.28	6.28	9.42	9.42	-6.88	-94.2
46	330	-6252	-63	-256	0	-119	266	6.28	6.28	9.42	9.42	-5.45	-69.5
47	330	-5918	-96	-330	0	101	182	6.28	6.28	9.42	9.42	-4.52	-59.4
49	330	-6016	-38	-241	0	-177	340	6.28	6.28	9.42	9.42	-6.02	-74.6
50	330	-6012	-138	-376	0	253	66	6.28	6.28	9.42	9.42	-4.18	-59.8
51	330	-5863	-100	-282	0	33	173	6.28	6.28	9.42	9.42	-4.41	-58.1

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 36 NI 325 NF 295 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 10D
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf

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	cm		daN		daN*m		cm^2				daN/cm^2	
40	0	-9915	922	-297	0	-2418	-1382	6.28	6.28	12.57	12.57	-15.05	-190.7
41	0	-8993	-242	-216	0	-1972	215	6.28	6.28	12.57	12.57	-12.16	-156.7
42	0	-8971	-242	-539	0	-1305	214	6.28	6.28	12.57	12.57	-8.32	-112.4
43	0	-10180	1781	-299	0	-2265	-2583	6.28	6.28	12.57	12.57	-21.04	307.2
44	0	-7799	-2187	-93	0	-1315	2885	6.28	6.28	12.57	12.57	-23.28	456.5
45	0	-8605	-158	-703	0	-410	76	6.28	6.28	12.57	12.57	-4.79	-68.2
46	0	-8431	-109	-135	0	-1252	-3	6.28	6.28	12.57	12.57	-7.94	-107.1
47	0	-8291	-75	-114	0	-1072	-58	6.28	6.28	12.57	12.57	-7.10	-96.6
49	0	-8598	312	-141	0	-1220	-590	6.28	6.28	12.57	12.57	-7.83	-106.0
50	0	-8122	-481	-100	0	-1030	503	6.28	6.28	12.57	12.57	-6.87	-93.6
51	0	-8283	-75	-222	0	-850	-58	6.28	6.28	12.57	12.57	-6.24	-86.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	83	-9420	922	-297	0	-2173	-622	6.28	6.28	12.57	12.57	-13.45	-172.0
41	83	-8498	-242	-216	0	-1793	15	6.28	6.28	12.57	12.57	-11.03	-143.0
42	83	-8476	-242	-393	0	-922	14	6.28	6.28	12.57	12.57	-6.58	-90.4
43	83	-9684	1781	-299	0	-2018	-1114	6.28	6.28	12.57	12.57	-12.41	-161.1
44	83	-7304	-2187	-93	0	-1238	1081	6.28	6.28	12.57	12.57	-8.90	-106.7
45	83	-8110	-158	-459	0	66	-54	6.28	6.28	12.57	12.57	-3.37	-50.0
46	83	-7936	-109	-135	0	-1141	-93	6.28	6.28	12.57	12.57	-7.30	-98.7
47	83	-7796	-75	-114	0	-978	-120	6.28	6.28	12.57	12.57	-6.55	-89.3
49	83	-8103	312	-141	0	-1104	-332	6.28	6.28	12.57	12.57	-7.18	-97.4
50	83	-7627	-481	-100	0	-948	106	6.28	6.28	12.57	12.57	-6.37	-86.9
51	83	-7788	-75	-173	0	-687	-121	6.28	6.28	12.57	12.57	-5.47	-75.9

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	165	-8925	922	-297	0	-1928	139	6.28	6.28	12.57	12.57	-11.88	-153.4
41	165	-8003	-242	-216	0	-1614	-184	6.28	6.28	12.57	12.57	-9.92	-129.4
42	165	-7981	-242	-268	0	-651	-185	6.28	6.28	12.57	12.57	-5.41	-75.4
43	165	-9189	1781	-299	0	-1771	356	6.28	6.28	12.57	12.57	-10.88	-142.7
44	165	-6809	-2187	-93	0	-1161	-723	6.28	6.28	12.57	12.57	-7.19	-95.6
45	165	-7615	-158	-250	0	357	-185	6.28	6.28	12.57	12.57	-4.22	-60.1
46	165	-7441	-109	-135	0	-1030	-183	6.28	6.28	12.57	12.57	-6.66	-90.3
47	165	-7301	-75	-114	0	-883	-182	6.28	6.28	12.57	12.57	-6.00	-82.0
49	165	-7608	312	-141	0	-988	-75	6.28	6.28	12.57	12.57	-6.53	-88.9
50	165	-7132	-481	-100	0	-865	-290	6.28	6.28	12.57	12.57	-5.87	-80.3
51	165	-7293	-75	-131	0	-562	-183	6.28	6.28	12.57	12.57	-4.83	-67.4

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	248	-8430	922	-297	0	-1683	900	6.28	6.28	12.57	12.57	-10.34	-135.0
41	248	-7508	-242	-216	0	-1436	-383	6.28	6.28	12.57	12.57	-8.82	-115.8
42	248	-7486	-242	-163	0	-475	-384	6.28	6.28	12.57	12.57	-4.59	-64.6
43	248	-8694	1781	-299	0	-1524	1825	6.28	6.28	12.57	12.57	-14.90	174.4
44	248	-6314	-2187	-93	0	-1084	-2527	6.28	6.28	12.57	12.57	-20.34	417.3
45	248	-7120	-158	-77	0	489	-315	6.28	6.28	12.57	12.57	-4.50	-63.2
46	248	-6946	-109	-135	0	-918	-272	6.28	6.28	12.57	12.57	-6.03	-82.0
47	248	-6806	-75	-114	0	-789	-245	6.28	6.28	12.57	12.57	-5.46	-74.8
49	248	-7113	312	-141	0	-871	183	6.28	6.28	12.57	12.57	-5.89	-80.5
50	248	-6637	-481	-100	0	-783	-687	6.28	6.28	12.57	12.57	-5.94	-75.4
51	248	-6798	-75	-97	0	-469	-245	6.28	6.28	12.57	12.57	-4.30	-60.4

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	330	-7935	922	-297	0	-1438	1660	6.28	6.28	12.57	12.57	-13.56	157.9
41	330	-7013	-242	-216	0	-1257	-583	6.28	6.28	12.57	12.57	-7.74	-102.5
42	330	-6991	-242	-80	0	-376	-584	6.28	6.28	12.57	12.57	-5.42	-70.4
43	330	-8198	1781	-299	0	-1277	3294	6.28	6.28	12.57	12.57	-26.51	545.1
44	330	-5819	-2187	-93	0	-1007	-4331	6.28	6.28	12.57	12.57	-34.18	891.6
45	330	-6625	-158	62	0	493	-446	6.28	6.28	12.57	12.57	-4.59	-60.6
46	330	-6451	-109	-135	0	-807	-362	6.28	6.28	12.57	12.57	-5.41	-73.8
47	330	-6311	-75	-114	0	-695	-307	6.28	6.28	12.57	12.57	-4.93	-67.7
49	330	-6618	312	-141	0	-755	441	6.28	6.28	12.57	12.57	-5.26	-72.2
50	330	-6142	-481	-100	0	-701	-1084	6.28	6.28	12.57	12.57	-8.87	-102.8
51	330	-6303	-75	-69	0	-401	-307	6.28	6.28	12.57	12.57	-3.87	-54.5

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 37 NI 296 NF 297 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 15C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
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	cm		daN			daN*m				cm^2		daN/cm^2	
40	0	-14770	878	-612	0	-2364	-1531	6.28	6.28	12.57	12.57	-14.77	-197.8
41	0	-14400	-250	-534	0	-2022	519	6.28	6.28	12.57	12.57	-13.02	-176.4
42	0	-14250	-251	-1058	0	-1717	522	6.28	6.28	12.57	12.57	-11.69	-159.8
43	0	-13750	1693	-535	0	-2095	-3026	6.28	6.28	12.57	12.57	-24.70	307.3
44	0	-14010	-2137	-429	0	-1548	3951	6.28	6.28	12.57	12.57	-32.11	517.5
45	0	-12870	-189	-1280	0	-1016	396	6.28	6.28	12.57	12.57	-8.61	-120.1
46	0	-12360	-150	-328	0	-1225	315	6.28	6.28	12.57	12.57	-9.16	-126.5
47	0	-11850	-125	-276	0	-1026	264	6.28	6.28	12.57	12.57	-8.25	-114.6
49	0	-11970	251	-302	0	-1140	-420	6.28	6.28	12.57	12.57	-8.71	-120.4
50	0	-12020	-515	-281	0	-1031	976	6.28	6.28	12.57	12.57	-9.17	-119.4
51	0	-11800	-125	-451	0	-924	265	6.28	6.28	12.57	12.57	-7.87	-109.8

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	95	-14200	878	-612	0	-1783	-697	6.28	6.28	12.57	12.57	-11.93	-162.8
41	95	-13830	-250	-534	0	-1515	282	6.28	6.28	12.57	12.57	-10.77	-148.0
42	95	-13680	-251	-890	0	-793	283	6.28	6.28	12.57	12.57	-8.13	-114.8
43	95	-13180	1693	-535	0	-1586	-1418	6.28	6.28	12.57	12.57	-12.15	-153.4
44	95	-13440	-2137	-429	0	-1141	1920	6.28	6.28	12.57	12.57	-15.84	-191.1
45	95	-12300	-189	-999	0	63	216	6.28	6.28	12.57	12.57	-5.49	-78.4
46	95	-11790	-150	-328	0	-914	172	6.28	6.28	12.57	12.57	-7.83	-109.2
47	95	-11280	-125	-276	0	-763	145	6.28	6.28	12.57	12.57	-7.09	-99.5
49	95	-11400	251	-302	0	-853	-181	6.28	6.28	12.57	12.57	-7.46	-104.2
50	95	-11451	-515	-281	0	-764	487	6.28	6.28	12.57	12.57	-7.16	-100.5
51	95	-11229	-125	-395	0	-523	146	6.28	6.28	12.57	12.57	-6.21	-88.5

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	190	-13630	878	-612	0	-1202	138	6.28	6.28	12.57	12.57	-9.57	-132.8
41	190	-13260	-250	-534	0	-1008	44	6.28	6.28	12.57	12.57	-8.73	-122.0
42	190	-13110	-251	-746	0	-18	45	6.28	6.28	12.57	12.57	-5.13	-76.8
43	190	-12610	1693	-535	0	-1078	190	6.28	6.28	12.57	12.57	-8.73	-121.3
44	190	-12870	-2137	-429	0	-733	-110	6.28	6.28	12.57	12.57	-7.60	-107.4
45	190	-11730	-189	-759	0	895	36	6.28	6.28	12.57	12.57	-7.74	-108.0
46	190	-11220	-150	-328	0	-602	30	6.28	6.28	12.57	12.57	-6.49	-92.0
47	190	-10709	-125	-276	0	-501	27	6.28	6.28	12.57	12.57	-5.93	-84.5
49	190	-10831	251	-302	0	-565	58	6.28	6.28	12.57	12.57	-6.21	-88.1
50	190	-10882	-515	-281	0	-497	-2	6.28	6.28	12.57	12.57	-5.98	-85.3
51	190	-10658	-125	-347	0	-171	27	6.28	6.28	12.57	12.57	-4.73	-69.4

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	285	-13060	878	-612	0	-621	972	6.28	6.28	12.57	12.57	-9.50	-124.6
41	285	-12690	-250	-534	0	-501	-193	6.28	6.28	12.57	12.57	-6.70	-96.0
42	285	-12540	-251	-626	0	632	-194	6.28	6.28	12.57	12.57	-7.11	-100.9
43	285	-12040	1693	-535	0	-569	1799	6.28	6.28	12.57	12.57	-14.80	-177.1
44	285	-12300	-2137	-429	0	-326	-2141	6.28	6.28	12.57	12.57	-17.53	-203.6
45	285	-11160	-189	-559	0	1518	-144	6.28	6.28	12.57	12.57	-9.87	-134.0
46	285	-10650	-150	-328	0	-291	-112	6.28	6.28	12.57	12.57	-5.16	-74.7
47	285	-10138	-125	-276	0	-238	-92	6.28	6.28	12.57	12.57	-4.77	-69.4
49	285	-10262	251	-302	0	-278	296	6.28	6.28	12.57	12.57	-5.16	-71.9
50	285	-10314	-515	-281	0	-230	-492	6.28	6.28	12.57	12.57	-6.14	-83.0
51	285	-10088	-125	-307	0	139	-92	6.28	6.28	12.57	12.57	-4.40	-64.7

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	380	-12490	878	-612	0	-40	1806	6.28	6.28	12.57	12.57	-14.89	-179.2
41	380	-12120	-250	-534	0	6	-431	6.28	6.28	12.57	12.57	-6.49	-89.4
42	380	-11970	-251	-530	0	1179	-433	6.28	6.28	12.57	12.57	-8.85	-122.1
43	380	-11470	1693	-535	0	-61	3407	6.28	6.28	12.57	12.57	-27.66	465.4
44	380	-11730	-2137	-429	0	81	-4171	6.28	6.28	12.57	12.57	-33.70	644.9
45	380	-10590	-189	-399	0	1970	-324	6.28	6.28	12.57	12.57	-12.11	-159.6
46	380	-10080	-150	-328	0	21	-255	6.28	6.28	12.57	12.57	-4.89	-68.6
47	380	-9568	-125	-276	0	24	-211	6.28	6.28	12.57	12.57	-4.49	-63.4
49	380	-9692	251	-302	0	9	535	6.28	6.28	12.57	12.57	-6.13	-82.1
50	380	-9745	-515	-281	0	38	-981	6.28	6.28	12.57	12.57	-8.55	-108.8
51	380	-9517	-125	-275	0	415	-211	6.28	6.28	12.57	12.57	-5.16	-73.7

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 38 NI 299 NF 294 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 10B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	

40	0	-23030	778	379	0	147	-1849	6.28	6.28	12.57	12.57	-17.46	-227.5
41	0	-22240	21	350	0	217	-52	6.28	6.28	12.57	12.57	-9.37	-138.6
42	0	-22210	24	158	0	-81	-58	6.28	6.28	12.57	12.57	-8.87	-132.3
43	0	-22970	1261	333	0	63	-3009	6.28	6.28	12.57	12.57	-25.00	-306.3
44	0	-20970	-1235	307	0	324	2932	6.28	6.28	12.57	12.57	-24.22	-293.4
45	0	-21610	4	-35	0	-317	-24	6.28	6.28	12.57	12.57	-9.48	-139.4
46	0	-21290	-15	246	0	156	9	6.28	6.28	12.57	12.57	-8.78	-130.4
47	0	-21060	-24	220	0	141	24	6.28	6.28	12.57	12.57	-8.64	-128.4
49	0	-21320	228	230	0	118	-575	6.28	6.28	12.57	12.57	-10.52	-147.1
50	0	-20920	-271	224	0	170	613	6.28	6.28	12.57	12.57	-10.56	-147.1
51	0	-21050	-23	156	0	42	22	6.28	6.28	12.57	12.57	-8.28	-123.8

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	97	-22445	778	379	0	-222	-1090	6.28	6.28	12.57	12.57	-13.47	-181.8
41	97	-21655	21	350	0	-124	-32	6.28	6.28	12.57	12.57	-8.81	-131.1
42	97	-21625	24	158	0	-235	-34	6.28	6.28	12.57	12.57	-9.19	-135.8
43	97	-22385	1261	333	0	-261	-1780	6.28	6.28	12.57	12.57	-16.88	-220.1
44	97	-20385	-1235	307	0	25	1728	6.28	6.28	12.57	12.57	-15.95	-206.8
45	97	-21025	4	-35	0	-283	-20	6.28	6.28	12.57	12.57	-9.14	-134.5
46	97	-20705	-15	246	0	-84	-6	6.28	6.28	12.57	12.57	-8.30	-123.7
47	97	-20475	-24	220	0	-74	0	6.28	6.28	12.57	12.57	-8.17	-121.9
49	97	-20735	228	230	0	-106	-352	6.28	6.28	12.57	12.57	-9.21	-131.6
50	97	-20335	-271	224	0	-49	349	6.28	6.28	12.57	12.57	-9.05	-129.2
51	97	-20465	-23	156	0	-110	-0	6.28	6.28	12.57	12.57	-8.30	-123.5

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	195	-21860	778	379	0	-591	-331	6.28	6.28	12.57	12.57	-10.56	-153.1
41	195	-21070	21	350	0	-466	-11	6.28	6.28	12.57	12.57	-9.81	-143.0
42	195	-21040	24	158	0	-389	-11	6.28	6.28	12.57	12.57	-9.52	-139.3
43	195	-21800	1261	333	0	-586	-550	6.28	6.28	12.57	12.57	-10.57	-152.5
44	195	-19800	-1235	307	0	-275	524	6.28	6.28	12.57	12.57	-9.72	-136.1
45	195	-20440	4	-35	0	-248	-17	6.28	6.28	12.57	12.57	-8.79	-129.6
46	195	-20120	-15	246	0	-324	-21	6.28	6.28	12.57	12.57	-8.93	-131.1
47	195	-19890	-24	220	0	-288	-23	6.28	6.28	12.57	12.57	-8.72	-128.2
49	195	-20150	228	230	0	-330	-130	6.28	6.28	12.57	12.57	-8.97	-131.5
50	195	-19750	-271	224	0	-268	85	6.28	6.28	12.57	12.57	-8.59	-126.4
51	195	-19880	-23	156	0	-263	-23	6.28	6.28	12.57	12.57	-8.62	-127.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	292	-21275	778	379	0	-961	428	6.28	6.28	12.57	12.57	-11.66	-166.3
41	292	-20485	21	350	0	-807	10	6.28	6.28	12.57	12.57	-10.81	-154.9
42	292	-20455	24	158	0	-543	13	6.28	6.28	12.57	12.57	-9.85	-142.8
43	292	-21215	1261	333	0	-910	679	6.28	6.28	12.57	12.57	-11.45	-163.7
44	292	-19215	-1235	307	0	-574	-680	6.28	6.28	12.57	12.57	-10.28	-141.6
45	292	-19855	4	-35	0	-214	-13	6.28	6.28	12.57	12.57	-8.44	-124.6
46	292	-19535	-15	246	0	-564	-35	6.28	6.28	12.57	12.57	-9.57	-138.4
47	292	-19305	-24	220	0	-503	-47	6.28	6.28	12.57	12.57	-9.26	-134.4
49	292	-19565	228	230	0	-554	93	6.28	6.28	12.57	12.57	-9.54	-138.2
50	292	-19165	-271	224	0	-487	-179	6.28	6.28	12.57	12.57	-9.15	-132.8
51	292	-19295	-23	156	0	-415	-45	6.28	6.28	12.57	12.57	-8.94	-130.4

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	390	-20690	778	379	0	-1330	1187	6.28	6.28	12.57	12.57	-13.31	-179.4
41	390	-19900	21	350	0	-1149	30	6.28	6.28	12.57	12.57	-11.80	-166.7
42	390	-19870	24	158	0	-697	36	6.28	6.28	12.57	12.57	-10.17	-146.3
43	390	-20630	1261	333	0	-1234	1908	6.28	6.28	12.57	12.57	-17.06	-219.3
44	390	-18630	-1235	307	0	-874	-1884	6.28	6.28	12.57	12.57	-16.40	-208.6
45	390	-19270	4	-35	0	-180	-10	6.28	6.28	12.57	12.57	-8.09	-119.7
46	390	-18950	-15	246	0	-804	-50	6.28	6.28	12.57	12.57	-10.20	-145.8
47	390	-18720	-24	220	0	-718	-70	6.28	6.28	12.57	12.57	-9.80	-140.6
49	390	-18980	228	230	0	-778	316	6.28	6.28	12.57	12.57	-10.12	-144.8
50	390	-18580	-271	224	0	-706	-443	6.28	6.28	12.57	12.57	-9.70	-139.3
51	390	-18710	-23	156	0	-567	-68	6.28	6.28	12.57	12.57	-9.26	-133.8

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 39 NI 300 NF 296 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 15B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-32330	686	532	0	490	-1242	6.28	6.28	12.57	12.57	-17.78	-243.7
41	0	-31910	133	520	0	518	-175	6.28	6.28	12.57	12.57	-14.18	-208.1
42	0	-31770	136	335	0	252	-180	6.28	6.28	12.57	12.57	-13.17	-195.4
43	0	-30920	1042	502	0	482	-1942	6.28	6.28	12.57	12.57	-20.73	-275.0
44	0	-30910	-786	486	0	530	1600	6.28	6.28	12.57	12.57	-19.04	-255.9
45	0	-29980	126	174	0	84	-172	6.28	6.28	12.57	12.57	-11.88	-177.5
46	0	-29180	114	460	0	533	-157	6.28	6.28	12.57	12.57	-13.18	-193.0
47	0	-28500	109	445	0	537	-152	6.28	6.28	12.57	12.57	-12.93	-189.2
49	0	-28650	293	449	0	528	-508	6.28	6.28	12.57	12.57	-12.96	-189.6
50	0	-28640	-72	446	0	537	200	6.28	6.28	12.57	12.57	-12.99	-190.0
51	0	-28460	110	383	0	448	-154	6.28	6.28	12.57	12.57	-12.60	-185.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	97	-31745	686	532	0	-28	-574	6.28	6.28	12.57	12.57	-14.26	-203.3
41	97	-31325	133	520	0	11	-46	6.28	6.28	12.57	12.57	-12.14	-182.0
42	97	-31185	136	335	0	-75	-48	6.28	6.28	12.57	12.57	-12.32	-184.1
43	97	-30335	1042	502	0	-8	-926	6.28	6.28	12.57	12.57	-15.50	-215.3
44	97	-30325	-786	486	0	56	834	6.28	6.28	12.57	12.57	-15.04	-210.2
45	97	-29395	126	174	0	-86	-49	6.28	6.28	12.57	12.57	-11.66	-174.2
46	97	-28595	114	460	0	85	-46	6.28	6.28	12.57	12.57	-11.35	-169.5
47	97	-27915	109	445	0	103	-46	6.28	6.28	12.57	12.57	-11.15	-166.4
49	97	-28065	293	449	0	90	-222	6.28	6.28	12.57	12.57	-11.20	-166.7
50	97	-28055	-72	446	0	103	130	6.28	6.28	12.57	12.57	-11.21	-167.2
51	97	-27875	110	383	0	74	-47	6.28	6.28	12.57	12.57	-11.04	-164.9

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	195	-31160	686	532	0	-546	95	6.28	6.28	12.57	12.57	-13.99	-205.0
41	195	-30740	133	520	0	-495	84	6.28	6.28	12.57	12.57	-13.65	-200.3
42	195	-30600	136	335	0	-401	85	6.28	6.28	12.57	12.57	-13.26	-195.3
43	195	-29750	1042	502	0	-498	90	6.28	6.28	12.57	12.57	-13.28	-194.7
44	195	-29740	-786	486	0	-418	68	6.28	6.28	12.57	12.57	-12.98	-191.0
45	195	-28810	126	174	0	-256	73	6.28	6.28	12.57	12.57	-12.05	-178.4
46	195	-28010	114	460	0	-363	65	6.28	6.28	12.57	12.57	-12.12	-178.6
47	195	-27330	109	445	0	-330	60	6.28	6.28	12.57	12.57	-11.74	-173.2
49	195	-27480	293	449	0	-348	64	6.28	6.28	12.57	12.57	-11.86	-174.8
50	195	-27470	-72	446	0	-332	59	6.28	6.28	12.57	12.57	-11.80	-174.0
51	195	-27290	110	383	0	-299	60	6.28	6.28	12.57	12.57	-11.61	-171.5

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	292	-30575	686	532	0	-1064	763	6.28	6.28	12.57	12.57	-15.62	-224.8
41	292	-30155	133	520	0	-1002	213	6.28	6.28	12.57	12.57	-15.24	-219.6
42	292	-30015	136	335	0	-728	217	6.28	6.28	12.57	12.57	-14.20	-206.5
43	292	-29165	1042	502	0	-987	1106	6.28	6.28	12.57	12.57	-15.97	-219.0
44	292	-29155	-786	486	0	-891	-698	6.28	6.28	12.57	12.57	-14.45	-208.8
45	292	-28225	126	174	0	-425	196	6.28	6.28	12.57	12.57	-12.43	-182.6
46	292	-27425	114	460	0	-812	176	6.28	6.28	12.57	12.57	-13.50	-195.3
47	292	-26745	109	445	0	-764	166	6.28	6.28	12.57	12.57	-13.07	-189.2
49	292	-26895	293	449	0	-785	350	6.28	6.28	12.57	12.57	-13.20	-191.0
50	292	-26885	-72	446	0	-766	-11	6.28	6.28	12.57	12.57	-13.13	-190.1
51	292	-26705	110	383	0	-673	168	6.28	6.28	12.57	12.57	-12.73	-184.9

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	390	-29990	686	532	0	-1582	1432	6.28	6.28	12.57	12.57	-17.87	-244.6
41	390	-29570	133	520	0	-1508	343	6.28	6.28	12.57	12.57	-16.82	-238.9
42	390	-29430	136	335	0	-1054	349	6.28	6.28	12.57	12.57	-15.14	-217.7
43	390	-28580	1042	502	0	-1477	2122	6.28	6.28	12.57	12.57	-20.78	-272.3
44	390	-28570	-786	486	0	-1365	-1464	6.28	6.28	12.57	12.57	-17.52	-235.7
45	390	-27640	126	174	0	-595	318	6.28	6.28	12.57	12.57	-12.81	-186.8
46	390	-26840	114	460	0	-1260	287	6.28	6.28	12.57	12.57	-14.88	-211.9
47	390	-26160	109	445	0	-1198	273	6.28	6.28	12.57	12.57	-14.40	-205.2
49	390	-26310	293	449	0	-1223	636	6.28	6.28	12.57	12.57	-14.54	-207.2
50	390	-26300	-72	446	0	-1201	-82	6.28	6.28	12.57	12.57	-14.46	-206.2
51	390	-26120	110	383	0	-1047	275	6.28	6.28	12.57	12.57	-13.84	-198.2

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 40 NI 301 NF 298 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 20B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-28900	634	744	0	884	-1272	6.28	6.28	12.57	12.57	-16.69	-226.8
41	0	-29230	124	690	0	808	-242	6.28	6.28	12.57	12.57	-14.19	-205.6

42	0	-29160	128	542	0	647	-247	6.28	6.28	12.57	12.57	-13.58	-197.9
43	0	-27460	960	708	0	884	-1939	6.28	6.28	12.57	12.57	-19.47	-256.1
44	0	-29510	-726	592	0	658	1478	6.28	6.28	12.57	12.57	-17.93	-241.5
45	0	-27910	116	373	0	489	-230	6.28	6.28	12.57	12.57	-12.53	-183.6
46	0	-27310	101	577	0	728	-209	6.28	6.28	12.57	12.57	-13.16	-190.8
47	0	-26820	96	549	0	708	-200	6.28	6.28	12.57	12.57	-12.90	-187.1
49	0	-26710	266	566	0	733	-544	6.28	6.28	12.57	12.57	-12.94	-187.6
50	0	-27120	-71	543	0	688	139	6.28	6.28	12.57	12.57	-12.94	-188.0
51	0	-26800	97	499	0	654	-202	6.28	6.28	12.57	12.57	-12.70	-184.6

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	97	-28315	634	744	0	159	-654	6.28	6.28	12.57	12.57	-13.43	-189.3
41	97	-28645	124	690	0	135	-121	6.28	6.28	12.57	12.57	-11.55	-172.1
42	97	-28575	128	542	0	118	-123	6.28	6.28	12.57	12.57	-11.46	-170.9
43	97	-26875	960	708	0	193	-1004	6.28	6.28	12.57	12.57	-14.64	-200.9
44	97	-28925	-726	592	0	80	770	6.28	6.28	12.57	12.57	-14.22	-199.1
45	97	-27325	116	373	0	126	-117	6.28	6.28	12.57	12.57	-11.01	-164.0
46	97	-26725	101	577	0	165	-110	6.28	6.28	12.57	12.57	-10.92	-162.3
47	97	-26235	96	549	0	173	-107	6.28	6.28	12.57	12.57	-10.75	-159.8
49	97	-26125	266	566	0	181	-285	6.28	6.28	12.57	12.57	-10.82	-159.5
50	97	-26535	-71	543	0	158	70	6.28	6.28	12.57	12.57	-10.82	-160.9
51	97	-26215	97	499	0	167	-108	6.28	6.28	12.57	12.57	-10.73	-159.4

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	195	-27730	634	744	0	-566	-36	6.28	6.28	12.57	12.57	-12.74	-186.0
41	195	-28060	124	690	0	-538	0	6.28	6.28	12.57	12.57	-12.77	-186.7
42	195	-27990	128	542	0	-410	2	6.28	6.28	12.57	12.57	-12.28	-180.6
43	195	-26290	960	708	0	-497	-68	6.28	6.28	12.57	12.57	-11.94	-174.6
44	195	-28340	-726	592	0	-497	63	6.28	6.28	12.57	12.57	-12.73	-186.5
45	195	-26740	116	373	0	-238	-4	6.28	6.28	12.57	12.57	-11.18	-165.6
46	195	-26140	101	577	0	-397	-11	6.28	6.28	12.57	12.57	-11.52	-169.3
47	195	-25650	96	549	0	-362	-14	6.28	6.28	12.57	12.57	-11.21	-164.8
49	195	-25540	266	566	0	-371	-26	6.28	6.28	12.57	12.57	-11.20	-164.6
50	195	-25950	-71	543	0	-371	-0	6.28	6.28	12.57	12.57	-11.36	-167.0
51	195	-25630	97	499	0	-319	-13	6.28	6.28	12.57	12.57	-11.05	-162.8

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	292	-27145	634	744	0	-1291	582	6.28	6.28	12.57	12.57	-15.11	-215.1
41	292	-27475	124	690	0	-1211	121	6.28	6.28	12.57	12.57	-14.95	-213.4
42	292	-27405	128	542	0	-939	127	6.28	6.28	12.57	12.57	-13.95	-200.8
43	292	-25705	960	708	0	-1188	867	6.28	6.28	12.57	12.57	-14.18	-202.1
44	292	-27755	-726	592	0	-1075	-644	6.28	6.28	12.57	12.57	-14.57	-209.0
45	292	-26155	116	373	0	-601	110	6.28	6.28	12.57	12.57	-12.26	-178.5
46	292	-25555	101	577	0	-960	88	6.28	6.28	12.57	12.57	-13.31	-191.1
47	292	-25065	96	549	0	-897	79	6.28	6.28	12.57	12.57	-12.90	-185.4
49	292	-24955	266	566	0	-924	233	6.28	6.28	12.57	12.57	-12.95	-186.0
50	292	-25365	-71	543	0	-901	-70	6.28	6.28	12.57	12.57	-13.03	-187.3
51	292	-25045	97	499	0	-806	81	6.28	6.28	12.57	12.57	-12.56	-181.2

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	390	-26560	634	744	0	-2016	1200	6.28	6.28	12.57	12.57	-17.48	-244.1
41	390	-26890	124	690	0	-1884	242	6.28	6.28	12.57	12.57	-17.13	-240.2
42	390	-26820	128	542	0	-1468	252	6.28	6.28	12.57	12.57	-15.62	-221.1
43	390	-25120	960	708	0	-1878	1803	6.28	6.28	12.57	12.57	-17.95	-235.9
44	390	-27170	-726	592	0	-1653	-1352	6.28	6.28	12.57	12.57	-16.46	-231.4
45	390	-25570	116	373	0	-965	223	6.28	6.28	12.57	12.57	-13.33	-191.4
46	390	-24970	101	577	0	-1523	186	6.28	6.28	12.57	12.57	-15.10	-212.9
47	390	-24480	96	549	0	-1432	172	6.28	6.28	12.57	12.57	-14.58	-206.0
49	390	-24370	266	566	0	-1476	492	6.28	6.28	12.57	12.57	-14.70	-207.3
50	390	-24780	-71	543	0	-1431	-140	6.28	6.28	12.57	12.57	-14.70	-207.6
51	390	-24460	97	499	0	-1293	176	6.28	6.28	12.57	12.57	-14.08	-199.6

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 41 NI 35 NF 31 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 12D
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-5665	719	714	0	-2209	-1075	6.28	6.28	12.57	12.57	-14.37	305.9
41	0	-4747	705	584	0	-1634	-967	6.28	6.28	12.57	12.57	-10.53	195.2
42	0	-4723	759	-24	0	-5037	-1022	6.28	6.28	12.57	12.57	-32.97	1235.4
43	0	-5685	778	668	0	-2201	-1192	6.28	6.28	12.57	12.57	-14.31	302.5
44	0	-3552	696	393	0	-758	-807	6.28	6.28	12.57	12.57	-6.58	85.1
45	0	-4116	845	-562	0	-6914	-1104	6.28	6.28	12.57	12.57	-44.86	1867.3
46	0	-3800	785	373	0	-1008	-1039	6.28	6.28	12.57	12.57	-8.45	132.5
47	0	-3563	805	320	0	-852	-1057	6.28	6.28	12.57	12.57	-8.58	144.3
49	0	-3869	809	363	0	-1043	-1093	6.28	6.28	12.57	12.57	-8.88	143.4
50	0	-3443	793	308	0	-755	-1016	6.28	6.28	12.57	12.57	-8.25	138.1
51	0	-3555	822	117	0	-1986	-1076	6.28	6.28	12.57	12.57	-13.07	370.5

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	58	-5318	719	714	0	-2622	-659	6.28	6.28	12.57	12.57	-17.22	448.7
41	58	-4400	705	584	0	-1972	-559	6.28	6.28	12.57	12.57	-12.91	312.4
42	58	-4376	759	-236	0	-4962	-583	6.28	6.28	12.57	12.57	-32.44	1236.8
43	58	-5338	778	668	0	-2587	-742	6.28	6.28	12.57	12.57	-16.98	437.1
44	58	-3205	696	393	0	-985	-404	6.28	6.28	12.57	12.57	-6.28	100.0
45	58	-3769	845	-914	0	-6487	-616	6.28	6.28	12.57	12.57	-42.07	1758.8
46	58	-3453	785	373	0	-1224	-585	6.28	6.28	12.57	12.57	-7.90	151.6
47	58	-3216	805	320	0	-1037	-592	6.28	6.28	12.57	12.57	-6.64	113.2
49	58	-3522	809	363	0	-1253	-625	6.28	6.28	12.57	12.57	-8.10	156.1
50	58	-3096	793	308	0	-933	-558	6.28	6.28	12.57	12.57	-5.94	91.8
51	58	-3208	822	47	0	-2033	-600	6.28	6.28	12.57	12.57	-13.39	408.2

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	116	-4971	719	714	0	-3034	-243	6.28	6.28	12.57	12.57	-19.98	596.8
41	116	-4053	705	584	0	-2310	-152	6.28	6.28	12.57	12.57	-15.20	436.2
42	116	-4029	759	-448	0	-4764	-144	6.28	6.28	12.57	12.57	-31.12	1199.9

43	116	-4991	778	668	0	-2974	-292	6.28	6.28	12.57	12.57	-19.58	576.7
44	116	-2858	696	393	0	-1212	-2	6.28	6.28	12.57	12.57	-7.92	182.7
45	116	-3422	845	-1267	0	-5856	-127	6.28	6.28	12.57	12.57	-37.98	1586.3
46	116	-3106	785	373	0	-1439	-132	6.28	6.28	12.57	12.57	-9.43	234.5
47	116	-2869	805	320	0	-1222	-127	6.28	6.28	12.57	12.57	-7.98	184.9
49	116	-3175	809	363	0	-1463	-157	6.28	6.28	12.57	12.57	-9.59	237.3
50	116	-2749	793	308	0	-1111	-99	6.28	6.28	12.57	12.57	-7.24	159.7
51	116	-2862	822	-24	0	-2040	-124	6.28	6.28	12.57	12.57	-13.43	433.8

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	173	-4624	719	714	0	-3447	173	6.28	6.28	12.57	12.57	-22.68	747.6
41	173	-3706	705	584	0	-2647	256	6.28	6.28	12.57	12.57	-17.43	563.4
42	173	-3682	759	-659	0	-4444	295	6.28	6.28	12.57	12.57	-29.02	1124.7
43	173	-4644	778	668	0	-3360	159	6.28	6.28	12.57	12.57	-22.11	719.1
44	173	-2511	696	393	0	-1440	401	6.28	6.28	12.57	12.57	-9.48	273.0
45	173	-3075	845	-1620	0	-5021	361	6.28	6.28	12.57	12.57	-32.60	1349.8
46	173	-2759	785	373	0	-1654	322	6.28	6.28	12.57	12.57	-10.89	322.1
47	173	-2522	805	320	0	-1407	339	6.28	6.28	12.57	12.57	-9.26	262.3
49	173	-2828	809	363	0	-1673	311	6.28	6.28	12.57	12.57	-11.02	323.2
50	173	-2402	793	308	0	-1289	359	6.28	6.28	12.57	12.57	-8.48	234.3
51	173	-2515	822	-94	0	-2006	351	6.28	6.28	12.57	12.57	-13.19	447.2

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	231	-4277	719	714	0	-3860	589	6.28	6.28	12.57	12.57	-25.34	900.0
41	231	-3359	705	584	0	-2985	664	6.28	6.28	12.57	12.57	-19.60	692.3
42	231	-3335	759	-871	0	-4001	734	6.28	6.28	12.57	12.57	-26.13	1011.3
43	231	-4297	778	668	0	-3746	609	6.28	6.28	12.57	12.57	-24.60	863.1
44	231	-2164	696	393	0	-1667	804	6.28	6.28	12.57	12.57	-10.97	366.5
45	231	-2728	845	-1973	0	-3982	850	6.28	6.28	12.57	12.57	-25.91	1049.3
46	231	-2412	785	373	0	-1870	776	6.28	6.28	12.57	12.57	-12.30	412.2
47	231	-2175	805	320	0	-1592	804	6.28	6.28	12.57	12.57	-10.48	342.5
49	231	-2481	809	363	0	-1883	779	6.28	6.28	12.57	12.57	-12.39	411.4
50	231	-2055	793	308	0	-1467	818	6.28	6.28	12.57	12.57	-9.66	312.1
51	231	-2168	822	-165	0	-1931	827	6.28	6.28	12.57	12.57	-12.68	448.2

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 42 NI 37 NF 43 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 17D
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-5844	403	484	0	-2921	-565	6.28	6.28	12.57	12.57	-19.19	505.1
41	0	-5134	187	402	0	-2541	-222	6.28	6.28	12.57	12.57	-16.69	436.2
42	0	-5208	191	78	0	-6833	-232	6.28	6.28	12.57	12.57	-44.55	1762.3
43	0	-5516	534	445	0	-2599	-768	6.28	6.28	12.57	12.57	-17.05	429.4
44	0	-4163	-160	282	0	-2015	329	6.28	6.28	12.57	12.57	-13.23	340.1
45	0	-4456	180	-230	0	-9119	-213	6.28	6.28	12.57	12.57	-58.96	2534.3
46	0	-3852	164	254	0	-1619	-182	6.28	6.28	12.57	12.57	-10.57	241.9
47	0	-3531	159	217	0	-1389	-171	6.28	6.28	12.57	12.57	-9.04	194.2
49	0	-3768	231	244	0	-1516	-285	6.28	6.28	12.57	12.57	-9.88	216.9
50	0	-3497	92	211	0	-1399	-66	6.28	6.28	12.57	12.57	-9.11	199.0
51	0	-3556	160	109	0	-2820	-174	6.28	6.28	12.57	12.57	-18.54	627.3

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	88	-5313	403	484	0	-3349	-208	6.28	6.28	12.57	12.57	-22.06	670.2
41	88	-4603	187	402	0	-2897	-57	6.28	6.28	12.57	12.57	-19.08	579.2
42	88	-4677	191	-246	0	-6759	-63	6.28	6.28	12.57	12.57	-43.98	1777.7
43	88	-4985	534	445	0	-2993	-295	6.28	6.28	12.57	12.57	-19.71	583.1
44	88	-3632	-160	282	0	-2264	187	6.28	6.28	12.57	12.57	-14.91	450.4
45	88	-3925	180	-771	0	-8676	-54	6.28	6.28	12.57	12.57	-56.02	2434.4
46	88	-3321	164	254	0	-1844	-36	6.28	6.28	12.57	12.57	-12.13	342.6
47	88	-3000	159	217	0	-1581	-31	6.28	6.28	12.57	12.57	-10.40	283.8
49	88	-3237	231	244	0	-1732	-81	6.28	6.28	12.57	12.57	-11.39	314.1
50	88	-2966	92	211	0	-1586	15	6.28	6.28	12.57	12.57	-10.43	287.5
51	88	-3025	160	1	0	-2868	-33	6.28	6.28	12.57	12.57	-18.81	679.6

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	177	-4782	403	484	0	-3777	149	6.28	6.28	12.57	12.57	-24.84	838.8
41	177	-4072	187	402	0	-3252	108	6.28	6.28	12.57	12.57	-21.39	725.5
42	177	-4146	191	-570	0	-6398	106	6.28	6.28	12.57	12.57	-41.58	1703.3
43	177	-4454	534	445	0	-3387	177	6.28	6.28	12.57	12.57	-22.28	740.7
44	177	-3101	-160	282	0	-2513	46	6.28	6.28	12.57	12.57	-16.52	563.7
45	177	-3394	180	-1311	0	-7755	105	6.28	6.28	12.57	12.57	-50.04	2184.4
46	177	-2790	164	254	0	-2068	109	6.28	6.28	12.57	12.57	-13.61	447.4
47	177	-2469	159	217	0	-1772	110	6.28	6.28	12.57	12.57	-11.67	378.1
49	177	-2706	231	244	0	-1948	123	6.28	6.28	12.57	12.57	-12.82	415.9
50	177	-2435	92	211	0	-1772	97	6.28	6.28	12.57	12.57	-11.67	380.4
51	177	-2494	160	-107	0	-2821	109	6.28	6.28	12.57	12.57	-18.44	702.8

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	266	-4251	403	484	0	-4205	506	6.28	6.28	12.57	12.57	-27.56	1009.4
41	266	-3541	187	402	0	-3608	274	6.28	6.28	12.57	12.57	-23.64	873.7
42	266	-3615	191	-894	0	-5750	275	6.28	6.28	12.57	12.57	-37.35	1539.0
43	266	-3923	534	445	0	-3781	650	6.28	6.28	12.57	12.57	-24.79	900.4
44	266	-2570	-160	282	0	-2762	-96	6.28	6.28	12.57	12.57	-18.07	678.9
45	266	-2863	180	-1851	0	-6356	264	6.28	6.28	12.57	12.57	-41.04	1784.3
46	266	-2259	164	254	0	-2292	255	6.28	6.28	12.57	12.57	-15.02	554.5
47	266	-1938	159	217	0	-1964	250	6.28	6.28	12.57	12.57	-12.87	474.9
49	266	-2175	231	244	0	-2163	328	6.28	6.28	12.57	12.57	-14.18	520.1
50	266	-1904	92	211	0	-1959	179	6.28	6.28	12.57	12.57	-12.83	475.8
51	266	-1963	160	-215	0	-2678	251	6.28	6.28	12.57	12.57	-17.45	696.5

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	354	-3720	403	484	0	-4633	863	6.28	6.28	12.57	12.57	-30.23	1181.2
41	354	-3010	187	402	0	-3964	439	6.28	6.28	12.57	12.57	-25.84	1023.2
42	354	-3084	191	-1218	0	-4816	444	6.28	6.28	12.57	12.57	-31.29	1284.8
43	354	-3392	534	445	0	-4175	1122	6.28	6.28	12.57	12.57	-27.25	1061.6

44	354	-2039	-160	282	0	-3011	-237	6.28	6.28	12.57	12.57	-19.58	795.2
45	354	-2332	180	-2391	0	-4479	423	6.28	6.28	12.57	12.57	-28.99	1234.2
46	354	-1728	164	254	0	-2517	400	6.28	6.28	12.57	12.57	-16.38	663.0
47	354	-1407	159	217	0	-2156	391	6.28	6.28	12.57	12.57	-14.01	573.2
49	354	-1644	231	244	0	-2379	532	6.28	6.28	12.57	12.57	-15.48	625.9
50	354	-1373	92	211	0	-2146	260	6.28	6.28	12.57	12.57	-13.94	572.6
51	354	-1432	160	-323	0	-2440	392	6.28	6.28	12.57	12.57	-15.83	660.5

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 43 NI 39 NF 44 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 22D
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-5770	-556	771	0	-1285	148	6.28	6.28	12.57	12.57	-7.93	-102.0
41	0	-5805	-644	734	0	-1476	359	6.28	6.28	12.57	12.57	-9.22	-116.1
42	0	-5841	-661	53	0	-4637	374	6.28	6.28	12.57	12.57	-30.49	1031.9
43	0	-4957	-525	634	0	-789	55	6.28	6.28	12.57	12.57	-4.93	-66.1
44	0	-6094	-803	701	0	-1866	718	6.28	6.28	12.57	12.57	-11.90	188.4
45	0	-5076	-700	-563	0	-6375	433	6.28	6.28	12.57	12.57	-41.59	1628.5
46	0	-4543	-690	475	0	-886	437	6.28	6.28	12.57	12.57	-5.44	-71.3
47	0	-4228	-701	410	0	-738	456	6.28	6.28	12.57	12.57	-4.56	-60.5
49	0	-4216	-672	423	0	-674	386	6.28	6.28	12.57	12.57	-4.21	-56.4
50	0	-4443	-727	436	0	-890	518	6.28	6.28	12.57	12.57	-5.47	-71.4
51	0	-4240	-707	183	0	-1792	461	6.28	6.28	12.57	12.57	-11.70	269.2

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	53	-5453	-556	771	0	-1693	-146	6.28	6.28	12.57	12.57	-10.81	174.6
41	53	-5488	-644	734	0	-1864	19	6.28	6.28	12.57	12.57	-12.00	218.8
42	53	-5524	-661	-141	0	-4614	25	6.28	6.28	12.57	12.57	-30.32	1046.8
43	53	-4640	-525	634	0	-1124	-222	6.28	6.28	12.57	12.57	-6.99	-88.7
44	53	-5777	-803	701	0	-2236	293	6.28	6.28	12.57	12.57	-14.54	307.3
45	53	-4759	-700	-885	0	-5992	62	6.28	6.28	12.57	12.57	-39.09	1531.6
46	53	-4226	-690	475	0	-1137	72	6.28	6.28	12.57	12.57	-7.15	91.6
47	53	-3911	-701	410	0	-955	85	6.28	6.28	12.57	12.57	-5.94	-75.3
49	53	-3899	-672	423	0	-898	31	6.28	6.28	12.57	12.57	-5.56	-71.1
50	53	-4126	-727	436	0	-1120	134	6.28	6.28	12.57	12.57	-7.05	91.9
51	53	-3923	-707	119	0	-1872	88	6.28	6.28	12.57	12.57	-12.28	312.3

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	106	-5136	-556	771	0	-2100	-440	6.28	6.28	12.57	12.57	-13.70	305.6
41	106	-5170	-644	734	0	-2252	-322	6.28	6.28	12.57	12.57	-14.73	348.0
42	106	-5206	-661	-334	0	-4488	-325	6.28	6.28	12.57	12.57	-29.48	1030.0
43	106	-4322	-525	634	0	-1459	-500	6.28	6.28	12.57	12.57	-9.39	169.8
44	106	-5460	-803	701	0	-2607	-132	6.28	6.28	12.57	12.57	-17.11	435.3
45	106	-4442	-700	-1208	0	-5439	-308	6.28	6.28	12.57	12.57	-35.50	1381.3
46	106	-3908	-690	475	0	-1388	-293	6.28	6.28	12.57	12.57	-8.97	172.5
47	106	-3594	-701	410	0	-1172	-285	6.28	6.28	12.57	12.57	-7.52	130.1
49	106	-3582	-672	423	0	-1121	-325	6.28	6.28	12.57	12.57	-7.16	117.1
50	106	-3808	-727	436	0	-1351	-251	6.28	6.28	12.57	12.57	-8.73	167.7
51	106	-3606	-707	54	0	-1917	-286	6.28	6.28	12.57	12.57	-12.61	346.4

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	159	-4818	-556	771	0	-2508	-733	6.28	6.28	12.57	12.57	-16.49	446.6
41	159	-4853	-644	734	0	-2641	-662	6.28	6.28	12.57	12.57	-17.37	484.4
42	159	-4889	-661	-528	0	-4260	-674	6.28	6.28	12.57	12.57	-27.98	981.4
43	159	-4005	-525	634	0	-1794	-777	6.28	6.28	12.57	12.57	-11.75	284.1
44	159	-5142	-803	701	0	-2977	-556	6.28	6.28	12.57	12.57	-19.60	567.9
45	159	-4124	-700	-1530	0	-4715	-679	6.28	6.28	12.57	12.57	-30.82	1177.6
46	159	-3591	-690	475	0	-1639	-657	6.28	6.28	12.57	12.57	-10.74	263.7
47	159	-3276	-701	410	0	-1389	-656	6.28	6.28	12.57	12.57	-9.07	209.3
49	159	-3264	-672	423	0	-1345	-680	6.28	6.28	12.57	12.57	-8.77	197.0
50	159	-3491	-727	436	0	-1581	-635	6.28	6.28	12.57	12.57	-10.36	252.9
51	159	-3288	-707	-10	0	-1929	-659	6.28	6.28	12.57	12.57	-12.70	370.7

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	211	-4501	-556	771	0	-2916	-1027	6.28	6.28	12.57	12.57	-19.20	592.0
41	211	-4536	-644	734	0	-3029	-1003	6.28	6.28	12.57	12.57	-19.95	624.4
42	211	-4572	-661	-721	0	-3930	-1024	6.28	6.28	12.57	12.57	-25.82	901.0
43	211	-3688	-525	634	0	-2129	-1055	6.28	6.28	12.57	12.57	-14.02	405.3
44	211	-4825	-803	701	0	-3348	-981	6.28	6.28	12.57	12.57	-22.04	703.1
45	211	-3807	-700	-1853	0	-3820	-1049	6.28	6.28	12.57	12.57	-25.03	920.9
46	211	-3274	-690	475	0	-1890	-1022	6.28	6.28	12.57	12.57	-12.44	359.8
47	211	-2959	-701	410	0	-1606	-1027	6.28	6.28	12.57	12.57	-10.57	294.1
49	211	-2947	-672	423	0	-1568	-1035	6.28	6.28	12.57	12.57	-10.31	283.4
50	211	-3174	-727	436	0	-1812	-1020	6.28	6.28	12.57	12.57	-11.93	342.7
51	211	-2971	-707	-75	0	-1906	-1033	6.28	6.28	12.57	12.57	-12.55	385.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 44 NI 295 NF 261 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 10E
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-4802	-373	-593	0	-1671	1050	6.28	6.28	12.57	12.57	-10.78	202.4
41	0	-4033	-386	-520	0	-1466	1088	6.28	6.28	12.57	12.57	-9.49	187.5
42	0	-4001	-376	-380	0	-492	1058	6.28	6.28	12.57	12.57	-8.61	130.9
43	0	-4883	-292	-530	0	-1492	821	6.28	6.28	12.57	12.57	-9.51	150.1
44	0	-3093	-405	-420	0	-1183	1139	6.28	6.28	12.57	12.57	-9.19	179.8
45	0	-3550	-297	-174	0	473	835	6.28	6.28	12.57	12.57	-6.81	91.7
46	0	-3343	-270	-341	0	-960	761	6.28	6.28	12.57	12.57	-6.21	87.1
47	0	-3171	-242	-296	0	-834	680	6.28	6.28	12.57	12.57	-5.55	66.7

49	0	-3427	-237	-320	0	-902	667	6.28	6.28	12.57	12.57	-5.66	-70.8
50	0	-3069	-260	-298	0	-840	731	6.28	6.28	12.57	12.57	-5.96	81.4
51	0	-3160	-238	-249	0	-509	670	6.28	6.28	12.57	12.57	-5.47	64.9

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	58	-4455	-373	-593	0	-1328	834	6.28	6.28	12.57	12.57	-8.44	128.4
41	58	-3686	-386	-520	0	-1165	864	6.28	6.28	12.57	12.57	-7.45	123.5
42	58	-3654	-376	-278	0	-302	841	6.28	6.28	12.57	12.57	-6.86	90.0
43	58	-4536	-292	-530	0	-1186	652	6.28	6.28	12.57	12.57	-7.43	-93.1
44	58	-2746	-405	-420	0	-940	905	6.28	6.28	12.57	12.57	-7.33	133.3
45	58	-3203	-297	-4	0	523	663	6.28	6.28	12.57	12.57	-5.42	62.3
46	58	-2996	-270	-341	0	-763	605	6.28	6.28	12.57	12.57	-4.94	-60.0
47	58	-2824	-242	-296	0	-662	540	6.28	6.28	12.57	12.57	-4.41	-52.4
49	58	-3080	-237	-320	0	-717	530	6.28	6.28	12.57	12.57	-4.44	-56.7
50	58	-2722	-260	-298	0	-668	581	6.28	6.28	12.57	12.57	-4.74	56.7
51	58	-2813	-238	-215	0	-375	532	6.28	6.28	12.57	12.57	-4.35	-49.7

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	116	-4108	-373	-593	0	-985	618	6.28	6.28	12.57	12.57	-6.12	-77.8
41	116	-3339	-386	-520	0	-864	641	6.28	6.28	12.57	12.57	-5.41	-67.9
42	116	-3307	-376	-190	0	-168	623	6.28	6.28	12.57	12.57	-5.10	-58.3
43	116	-4189	-292	-530	0	-879	483	6.28	6.28	12.57	12.57	-5.41	-70.2
44	116	-2399	-405	-420	0	-697	671	6.28	6.28	12.57	12.57	-5.46	87.3
45	116	-2856	-297	143	0	482	492	6.28	6.28	12.57	12.57	-4.03	-46.9
46	116	-2649	-270	-341	0	-566	448	6.28	6.28	12.57	12.57	-3.67	-45.1
47	116	-2477	-242	-296	0	-491	400	6.28	6.28	12.57	12.57	-3.28	-39.4
49	116	-2733	-237	-320	0	-532	393	6.28	6.28	12.57	12.57	-3.26	-42.8
50	116	-2375	-260	-298	0	-495	430	6.28	6.28	12.57	12.57	-3.52	-40.6
51	116	-2466	-238	-186	0	-259	395	6.28	6.28	12.57	12.57	-3.24	-38.2

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	173	-3761	-373	-593	0	-642	403	6.28	6.28	12.57	12.57	-3.97	-52.8
41	173	-2992	-386	-520	0	-563	417	6.28	6.28	12.57	12.57	-3.46	-45.5
42	173	-2960	-376	-117	0	-80	406	6.28	6.28	12.57	12.57	-3.36	-40.8
43	173	-3842	-292	-530	0	-573	315	6.28	6.28	12.57	12.57	-3.63	-48.9
44	173	-2052	-405	-420	0	-454	437	6.28	6.28	12.57	12.57	-3.57	42.6
45	173	-2509	-297	264	0	363	320	6.28	6.28	12.57	12.57	-2.67	-32.8
46	173	-2302	-270	-341	0	-369	292	6.28	6.28	12.57	12.57	-2.43	-30.8
47	173	-2130	-242	-296	0	-320	261	6.28	6.28	12.57	12.57	-2.18	-27.3
49	173	-2386	-237	-320	0	-346	256	6.28	6.28	12.57	12.57	-2.21	-29.8
50	173	-2028	-260	-298	0	-323	280	6.28	6.28	12.57	12.57	-2.32	-28.1
51	173	-2119	-238	-161	0	-159	257	6.28	6.28	12.57	12.57	-2.16	-26.7

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	231	-3414	-373	-593	0	-298	187	6.28	6.28	12.57	12.57	-2.39	-33.1
41	231	-2645	-386	-520	0	-262	194	6.28	6.28	12.57	12.57	-1.96	-27.0
42	231	-2613	-376	-59	0	-30	188	6.28	6.28	12.57	12.57	-1.87	-24.6
43	231	-3495	-292	-530	0	-266	146	6.28	6.28	12.57	12.57	-2.30	-32.2
44	231	-1705	-405	-420	0	-211	203	6.28	6.28	12.57	12.57	-1.71	-21.3
45	231	-2162	-297	362	0	181	149	6.28	6.28	12.57	12.57	-1.51	-20.6
46	231	-1955	-270	-341	0	-171	136	6.28	6.28	12.57	12.57	-1.37	-19.0
47	231	-1783	-242	-296	0	-149	121	6.28	6.28	12.57	12.57	-1.24	-17.0
49	231	-2039	-237	-320	0	-161	119	6.28	6.28	12.57	12.57	-1.36	-19.0
50	231	-1681	-260	-298	0	-150	130	6.28	6.28	12.57	12.57	-1.25	-16.5
51	231	-1772	-238	-142	0	-72	119	6.28	6.28	12.57	12.57	-1.23	-16.2

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 45 NI 297 NF 260 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 15D
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	

40	0	-8854	-70	24	0	96	282	6.28	6.28	12.57	12.57	-4.58	-63.5
41	0	-8480	-23	32	0	130	93	6.28	6.28	12.57	12.57	-3.74	-55.0
42	0	-8325	-22	17	0	1293	87	6.28	6.28	12.57	12.57	-8.12	-109.1
43	0	-7800	-95	14	0	55	382	6.28	6.28	12.57	12.57	-4.70	-63.4
44	0	-8089	57	47	0	191	-229	6.28	6.28	12.57	12.57	-4.04	-56.4
45	0	-6918	-14	3	0	2050	58	6.28	6.28	12.57	12.57	-13.03	196.3
46	0	-6396	-13	25	0	101	53	6.28	6.28	12.57	12.57	-2.83	-41.6
47	0	-5875	-11	23	0	94	43	6.28	6.28	12.57	12.57	-2.61	-38.3
49	0	-6000	-26	21	0	83	106	6.28	6.28	12.57	12.57	-2.68	-38.5
50	0	-6058	4	27	0	110	-16	6.28	6.28	12.57	12.57	-2.73	-40.0
51	0	-5823	-10	18	0	482	41	6.28	6.28	12.57	12.57	-3.97	-55.3

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	88	-8323	-70	24	0	75	220	6.28	6.28	12.57	12.57	-4.08	-57.2
41	88	-7949	-23	32	0	102	73	6.28	6.28	12.57	12.57	-3.43	-50.6
42	88	-7794	-22	174	0	1207	68	6.28	6.28	12.57	12.57	-7.59	-101.9
43	88	-7269	-95	14	0	43	298	6.28	6.28	12.57	12.57	-4.09	-55.8
44	88	-7558	57	47	0	149	-179	6.28	6.28	12.57	12.57	-3.60	-50.8
45	88	-6387	-14	264	0	1929	45	6.28	6.28	12.57	12.57	-12.28	190.6
46	88	-5865	-13	25	0	79	42	6.28	6.28	12.57	12.57	-2.55	-37.5
47	88	-5344	-11	23	0	73	34	6.28	6.28	12.57	12.57	-2.33	-34.3
49	88	-5469	-26	21	0	64	83	6.28	6.28	12.57	12.57	-2.38	-34.6
50	88	-5527	4	27	0	86	-13	6.28	6.28	12.57	12.57	-2.44	-35.9
51	88	-5292	-10	71	0	442	32	6.28	6.28	12.57	12.57	-3.63	-50.4

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	177	-7792	-70	24	0	54	158	6.28	6.28	12.57	12.57	-3.59	-50.9
41	177	-7418	-23	32	0	73	53	6.28	6.28	12.57	12.57	-3.13	-46.2
42	177	-7263	-22	308	0	992	49	6.28	6.28	12.57	12.57	-6.44	-87.4
43	177	-6738	-95	14	0	31	215	6.28	6.28	12.57	12.57	-3.49	-48.3
44	177	-7027	57	47	0	107	-128	6.28	6.28	12.57	12.57	-3.16	-45.5
45	177	-5856	-14	488	0	1594	33	6.28	6.28	12.57	12.57	-10.04	131.3
46	177	-5334	-13	25	0	57	30	6.28	6.28	12.57	12.57	-2.26	-33.4
47	177	-4813	-11	23	0	53	24	6.28	6.28	12.57	12.57	-2.05	-30.2
49	177	-4938	-26	21	0	46	59	6.28	6.28	12.57	12.57	-2.07	-30.7

50	177	-4996	4	27	0	62	-9	6.28	6.28	12.57	12.57	-2.15	-31.7
51	177	-4761	-10	115	0	359	23	6.28	6.28	12.57	12.57	-3.12	-43.7

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	266	-7261	-70	24	0	32	97	6.28	6.28	12.57	12.57	-3.09	-44.6
41	266	-6887	-23	32	0	44	32	6.28	6.28	12.57	12.57	-2.82	-41.9
42	266	-6732	-22	420	0	668	30	6.28	6.28	12.57	12.57	-4.99	-68.9
43	266	-6207	-95	14	0	18	131	6.28	6.28	12.57	12.57	-2.88	-40.8
44	266	-6496	57	47	0	65	-78	6.28	6.28	12.57	12.57	-2.74	-40.6
45	266	-5325	-14	674	0	1077	20	6.28	6.28	12.57	12.57	-6.62	-86.3
46	266	-4803	-13	25	0	34	18	6.28	6.28	12.57	12.57	-1.98	-29.4
47	266	-4282	-11	23	0	32	15	6.28	6.28	12.57	12.57	-1.77	-26.2
49	266	-4407	-26	21	0	28	36	6.28	6.28	12.57	12.57	-1.80	-26.8
50	266	-4465	4	27	0	37	-6	6.28	6.28	12.57	12.57	-1.86	-27.5
51	266	-4230	-10	153	0	240	14	6.28	6.28	12.57	12.57	-2.49	-35.2

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	354	-6730	-70	24	0	11	35	6.28	6.28	12.57	12.57	-2.64	-39.5
41	354	-6356	-23	32	0	15	12	6.28	6.28	12.57	12.57	-2.51	-37.5
42	354	-6201	-22	509	0	255	11	6.28	6.28	12.57	12.57	-3.31	-47.3
43	354	-5676	-95	14	0	6	47	6.28	6.28	12.57	12.57	-2.28	-33.3
44	354	-5965	57	47	0	23	-28	6.28	6.28	12.57	12.57	-2.39	-35.6
45	354	-4794	-14	823	0	412	7	6.28	6.28	12.57	12.57	-3.33	-46.2
46	354	-4272	-13	25	0	12	7	6.28	6.28	12.57	12.57	-1.69	-25.3
47	354	-3751	-11	23	0	11	5	6.28	6.28	12.57	12.57	-1.49	-22.2
49	354	-3876	-26	21	0	10	13	6.28	6.28	12.57	12.57	-1.53	-22.9
50	354	-3934	4	27	0	13	-2	6.28	6.28	12.57	12.57	-1.57	-23.4
51	354	-3699	-10	182	0	91	5	6.28	6.28	12.57	12.57	-1.75	-25.5

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 46 NI 271 NF 259 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 20D
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-5474	226	-670	0	-1755	-592	6.28	6.28	12.57	12.57	-11.24	190.0
41	0	-5665	220	-599	0	-1569	-576	6.28	6.28	12.57	12.57	-9.90	133.5
42	0	-5597	217	-414	0	-587	-568	6.28	6.28	12.57	12.57	-4.94	-62.8
43	0	-4571	189	-587	0	-1536	-494	6.28	6.28	12.57	12.57	-9.88	177.7
44	0	-6216	214	-504	0	-1319	-560	6.28	6.28	12.57	12.57	-8.12	-105.1
45	0	-4777	174	-159	0	412	-455	6.28	6.28	12.57	12.57	-4.03	-51.6
46	0	-4425	154	-389	0	-1019	-404	6.28	6.28	12.57	12.57	-6.31	-80.7
47	0	-4115	138	-337	0	-881	-360	6.28	6.28	12.57	12.57	-5.43	-70.2
49	0	-4051	140	-360	0	-943	-366	6.28	6.28	12.57	12.57	-5.84	-74.6
50	0	-4380	145	-344	0	-900	-379	6.28	6.28	12.57	12.57	-5.53	-72.0
51	0	-4092	137	-275	0	-554	-358	6.28	6.28	12.57	12.57	-3.61	-49.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	53	-5157	226	-670	0	-1400	-472	6.28	6.28	12.57	12.57	-8.82	114.9
41	53	-5348	220	-599	0	-1252	-460	6.28	6.28	12.57	12.57	-7.76	-99.0
42	53	-5280	217	-320	0	-393	-453	6.28	6.28	12.57	12.57	-4.16	-53.9
43	53	-4254	189	-587	0	-1226	-395	6.28	6.28	12.57	12.57	-7.77	111.9
44	53	-5899	214	-504	0	-1053	-447	6.28	6.28	12.57	12.57	-6.49	-85.9
45	53	-4460	174	-3	0	453	-363	6.28	6.28	12.57	12.57	-3.41	-46.1
46	53	-4108	154	-389	0	-813	-322	6.28	6.28	12.57	12.57	-4.99	-65.3
47	53	-3798	138	-337	0	-703	-287	6.28	6.28	12.57	12.57	-4.32	-57.0
49	53	-3734	140	-360	0	-753	-292	6.28	6.28	12.57	12.57	-4.63	-60.3
50	53	-4063	145	-344	0	-718	-302	6.28	6.28	12.57	12.57	-4.43	-58.7
51	53	-3775	137	-244	0	-417	-285	6.28	6.28	12.57	12.57	-2.95	-40.5

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	106	-4840	226	-670	0	-1046	-353	6.28	6.28	12.57	12.57	-6.44	-83.2
41	106	-5030	220	-599	0	-935	-343	6.28	6.28	12.57	12.57	-5.75	-75.8
42	106	-4962	217	-240	0	-246	-338	6.28	6.28	12.57	12.57	-3.46	-45.6
43	106	-3936	189	-587	0	-915	-295	6.28	6.28	12.57	12.57	-5.67	-72.4
44	106	-5582	214	-504	0	-786	-333	6.28	6.28	12.57	12.57	-5.06	-68.5
45	106	-4142	174	131	0	418	-271	6.28	6.28	12.57	12.57	-3.10	-42.7
46	106	-3790	154	-389	0	-607	-240	6.28	6.28	12.57	12.57	-3.79	-50.8
47	106	-3480	138	-337	0	-525	-215	6.28	6.28	12.57	12.57	-3.32	-44.7
49	106	-3416	140	-360	0	-562	-218	6.28	6.28	12.57	12.57	-3.50	-46.7
50	106	-3746	145	-344	0	-536	-226	6.28	6.28	12.57	12.57	-3.44	-46.5
51	106	-3458	137	-217	0	-296	-213	6.28	6.28	12.57	12.57	-2.39	-33.3

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	159	-4522	226	-670	0	-691	-233	6.28	6.28	12.57	12.57	-4.36	-58.6
41	159	-4713	220	-599	0	-618	-227	6.28	6.28	12.57	12.57	-4.07	-55.4
42	159	-4645	217	-173	0	-137	-224	6.28	6.28	12.57	12.57	-2.78	-37.5
43	159	-3619	189	-587	0	-605	-195	6.28	6.28	12.57	12.57	-3.75	-50.1
44	159	-5264	214	-504	0	-520	-220	6.28	6.28	12.57	12.57	-3.89	-53.8
45	159	-3825	174	242	0	318	-179	6.28	6.28	12.57	12.57	-2.62	-36.4
46	159	-3473	154	-389	0	-401	-159	6.28	6.28	12.57	12.57	-2.78	-38.1
47	159	-3163	138	-337	0	-347	-142	6.28	6.28	12.57	12.57	-2.47	-33.9
49	159	-3099	140	-360	0	-372	-144	6.28	6.28	12.57	12.57	-2.53	-34.7
50	159	-3428	145	-344	0	-355	-149	6.28	6.28	12.57	12.57	-2.59	-35.7
51	159	-3140	137	-195	0	-187	-141	6.28	6.28	12.57	12.57	-1.88	-26.6

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	211	-4205	226	-670	0	-337	-114	6.28	6.28	12.57	12.57	-2.83	-39.4
41	211	-4396	220	-599	0	-301	-110	6.28	6.28	12.57	12.57	-2.78	-39.0
42	211	-4328	217	-120	0	-61	-109	6.28	6.28	12.57	12.57	-2.10	-29.4
43	211	-3302	189	-587	0	-295	-95	6.28	6.28	12.57	12.57	-2.33	-32.3
44	211	-4947	214	-504	0	-253	-107	6.28	6.28	12.57	12.57	-2.82	-40.0
45	211	-3508	174	331	0	166	-87	6.28	6.28	12.57	12.57	-1.95	-27.7
46	211	-3156	154	-389	0	-196	-77	6.28	6.28	12.57	12.57	-1.92	-27.0
47	211	-2846	138	-337	0	-169	-69	6.28	6.28	12.57	12.57	-1.71	-24.1
49	211	-2782	140	-360	0	-181	-70	6.28	6.28	12.57	12.57	-1.72	-24.2
50	211	-3111	145	-344	0	-173	-72	6.28	6.28	12.57	12.57	-1.82	-25.8

51	211	-2823	137	-177	0	-89	-68	6.28	6.28	12.57	12.57	-1.41	-20.3

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 47 NI 129 NF 124 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 9B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	--												
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-9974	110	-239	0	-437	-492	6.28	6.28	12.57	12.57	-6.02	-81.2
41	0	-9913	-32	-126	0	-226	11	6.28	6.28	12.57	12.57	-4.64	-67.5
42	0	-9858	-33	-218	0	-426	15	6.28	6.28	12.57	12.57	-5.33	-76.2
43	0	-9687	212	-280	0	-519	-852	6.28	6.28	12.57	12.57	-7.76	-100.2
44	0	-9545	-268	45	0	101	853	6.28	6.28	12.57	12.57	-7.72	-99.6
45	0	-9494	-26	-245	0	-500	-7	6.28	6.28	12.57	12.57	-5.46	-77.4
46	0	-9388	-18	-72	0	-130	-29	6.28	6.28	12.57	12.57	-4.09	-60.2
47	0	-9257	-15	-58	0	-106	-38	6.28	6.28	12.57	12.57	-3.96	-58.4
49	0	-9278	32	-96	0	-176	-206	6.28	6.28	12.57	12.57	-4.36	-61.7
50	0	-9249	-64	-31	0	-53	135	6.28	6.28	12.57	12.57	-4.00	-57.5
51	0	-9239	-15	-89	0	-173	-37	6.28	6.28	12.57	12.57	-4.19	-61.3

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	97	-9389	110	-239	0	-205	-386	6.28	6.28	12.57	12.57	-5.29	-72.2
41	97	-9328	-32	-126	0	-102	-20	6.28	6.28	12.57	12.57	-3.97	-58.6
42	97	-9273	-33	-218	0	-214	-18	6.28	6.28	12.57	12.57	-4.35	-63.3
43	97	-9102	212	-280	0	-246	-645	6.28	6.28	12.57	12.57	-6.47	-85.0
44	97	-8960	-268	45	0	57	591	6.28	6.28	12.57	12.57	-6.15	-81.3
45	97	-8909	-26	-245	0	-261	-32	6.28	6.28	12.57	12.57	-4.38	-63.3
46	97	-8803	-18	-72	0	-60	-46	6.28	6.28	12.57	12.57	-3.61	-53.7
47	97	-8672	-15	-58	0	-49	-53	6.28	6.28	12.57	12.57	-3.53	-52.4
49	97	-8693	32	-96	0	-83	-174	6.28	6.28	12.57	12.57	-3.99	-56.7
50	97	-8664	-64	-31	0	-22	73	6.28	6.28	12.57	12.57	-3.48	-51.2
51	97	-8654	-15	-89	0	-86	-52	6.28	6.28	12.57	12.57	-3.65	-54.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	195	-8804	110	-239	0	28	-279	6.28	6.28	12.57	12.57	-4.55	-63.1
41	195	-8743	-32	-126	0	21	-51	6.28	6.28	12.57	12.57	-3.45	-51.6
42	195	-8688	-33	-218	0	-1	-50	6.28	6.28	12.57	12.57	-3.38	-50.4
43	195	-8517	212	-280	0	26	-439	6.28	6.28	12.57	12.57	-5.23	-70.4
44	195	-8375	-268	45	0	14	330	6.28	6.28	12.57	12.57	-4.64	-63.6
45	195	-8324	-26	-245	0	-22	-57	6.28	6.28	12.57	12.57	-3.29	-49.2
46	195	-8218	-18	-72	0	11	-64	6.28	6.28	12.57	12.57	-3.27	-48.1
47	195	-8087	-15	-58	0	8	-67	6.28	6.28	12.57	12.57	-3.24	-47.4
49	195	-8108	32	-96	0	10	-143	6.28	6.28	12.57	12.57	-3.63	-51.7
50	195	-8079	-64	-31	0	8	11	6.28	6.28	12.57	12.57	-3.15	-47.2
51	195	-8069	-15	-89	0	1	-67	6.28	6.28	12.57	12.57	-3.23	-47.3

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	292	-8219	110	-239	0	261	-172	6.28	6.28	12.57	12.57	-4.11	-59.3
41	292	-8158	-32	-126	0	144	-82	6.28	6.28	12.57	12.57	-3.67	-53.7
42	292	-8103	-33	-218	0	212	-83	6.28	6.28	12.57	12.57	-3.89	-56.4
43	292	-7932	212	-280	0	299	-232	6.28	6.28	12.57	12.57	-4.14	-59.4
44	292	-7790	-268	45	0	-30	68	6.28	6.28	12.57	12.57	-3.14	-46.5
45	292	-7739	-26	-245	0	217	-83	6.28	6.28	12.57	12.57	-3.77	-54.6
46	292	-7633	-18	-72	0	81	-81	6.28	6.28	12.57	12.57	-3.24	-47.8
47	292	-7502	-15	-58	0	65	-81	6.28	6.28	12.57	12.57	-3.13	-46.4
49	292	-7523	32	-96	0	104	-111	6.28	6.28	12.57	12.57	-3.28	-48.2
50	292	-7494	-64	-31	0	38	-51	6.28	6.28	12.57	12.57	-3.03	-45.1
51	292	-7484	-15	-89	0	87	-81	6.28	6.28	12.57	12.57	-3.20	-47.3

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	390	-7634	110	-239	0	494	-66	6.28	6.28	12.57	12.57	-4.72	-66.3
41	390	-7573	-32	-126	0	268	-113	6.28	6.28	12.57	12.57	-3.88	-55.9
42	390	-7518	-33	-218	0	424	-115	6.28	6.28	12.57	12.57	-4.42	-62.6
43	390	-7347	212	-280	0	572	-25	6.28	6.28	12.57	12.57	-4.89	-68.2
44	390	-7205	-268	45	0	-73	-194	6.28	6.28	12.57	12.57	-3.55	-49.7
45	390	-7154	-26	-245	0	456	-108	6.28	6.28	12.57	12.57	-4.40	-61.9
46	390	-7048	-18	-72	0	151	-99	6.28	6.28	12.57	12.57	-3.26	-47.6
47	390	-6917	-15	-58	0	122	-96	6.28	6.28	12.57	12.57	-3.11	-45.5
49	390	-6938	32	-96	0	197	-80	6.28	6.28	12.57	12.57	-3.39	-49.0
50	390	-6909	-64	-31	0	68	-113	6.28	6.28	12.57	12.57	-3.05	-43.6
51	390	-6899	-15	-89	0	174	-96	6.28	6.28	12.57	12.57	-3.29	-47.8

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 48 NI 128 NF 125 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 14B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	--												
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-16060	163	-481	0	-797	-421	6.28	6.28	12.57	12.57	-9.06	-128.7
41	0	-16020	4	-434	0	-728	10	6.28	6.28	12.57	12.57	-8.80	-125.4
42	0	-15970	5	-570	0	-962	7	6.28	6.28	12.57	12.57	-9.61	-135.6
43	0	-15480	274	-434	0	-723	-721	6.28	6.28	12.57	12.57	-9.14	-123.7
44	0	-15420	-262	-374	0	-636	730	6.28	6.28	12.57	12.57	-9.16	-123.8
45	0	-15320	11	-582	0	-998	-8	6.28	6.28	12.57	12.57	-9.49	-133.4
46	0	-15030	12	-309	0	-537	-11	6.28	6.28	12.57	12.57	-7.73	-111.1
47	0	-14790	14	-277	0	-490	-16	6.28	6.28	12.57	12.57	-7.47	-107.6
49	0	-14800	67	-293	0	-512	-160	6.28	6.28	12.57	12.57	-7.55	-108.7
50	0	-14790	-40	-281	0	-495	130	6.28	6.28	12.57	12.57	-7.49	-107.9
51	0	-14770	15	-322	0	-567	-17	6.28	6.28	12.57	12.57	-7.74	-111.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	97	-15475	163	-481	0	-328	-262	6.28	6.28	12.57	12.57	-7.15	-104.3
41	97	-15435	4	-434	0	-305	14	6.28	6.28	12.57	12.57	-7.05	-103.1
42	97	-15385	5	-570	0	-406	12	6.28	6.28	12.57	12.57	-7.40	-107.3
43	97	-14895	274	-434	0	-300	-454	6.28	6.28	12.57	12.57	-7.60	-105.7
44	97	-14835	-262	-374	0	-272	474	6.28	6.28	12.57	12.57	-7.68	-106.5
45	97	-14735	11	-582	0	-431	3	6.28	6.28	12.57	12.57	-7.23	-104.7
46	97	-14445	12	-309	0	-236	1	6.28	6.28	12.57	12.57	-6.43	-94.3
47	97	-14205	14	-277	0	-219	-2	6.28	6.28	12.57	12.57	-6.27	-92.1
49	97	-14215	67	-293	0	-227	-94	6.28	6.28	12.57	12.57	-6.30	-92.5
50	97	-14205	-40	-281	0	-221	91	6.28	6.28	12.57	12.57	-6.28	-92.2
51	97	-14185	15	-322	0	-253	-3	6.28	6.28	12.57	12.57	-6.39	-93.5

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	195	-14890	163	-481	0	141	-103	6.28	6.28	12.57	12.57	-6.26	-92.6
41	195	-14850	4	-434	0	118	18	6.28	6.28	12.57	12.57	-6.16	-91.3
42	195	-14800	5	-570	0	149	17	6.28	6.28	12.57	12.57	-6.25	-92.4
43	195	-14310	274	-434	0	123	-186	6.28	6.28	12.57	12.57	-6.07	-88.4
44	195	-14250	-262	-374	0	93	219	6.28	6.28	12.57	12.57	-6.21	-89.1
45	195	-14150	11	-582	0	136	14	6.28	6.28	12.57	12.57	-5.96	-88.1
46	195	-13860	12	-309	0	65	13	6.28	6.28	12.57	12.57	-5.59	-83.2
47	195	-13620	14	-277	0	51	12	6.28	6.28	12.57	12.57	-5.44	-81.2
49	195	-13630	67	-293	0	59	-28	6.28	6.28	12.57	12.57	-5.48	-81.6
50	195	-13620	-40	-281	0	53	52	6.28	6.28	12.57	12.57	-5.45	-81.3
51	195	-13600	15	-322	0	62	11	6.28	6.28	12.57	12.57	-5.47	-81.6

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	292	-14305	163	-481	0	610	57	6.28	6.28	12.57	12.57	-7.71	-110.2
41	292	-14265	4	-434	0	542	22	6.28	6.28	12.57	12.57	-7.45	-106.9
42	292	-14215	5	-570	0	705	23	6.28	6.28	12.57	12.57	-8.01	-113.9
43	292	-13725	274	-434	0	545	82	6.28	6.28	12.57	12.57	-7.26	-103.9
44	292	-13665	-262	-374	0	458	-37	6.28	6.28	12.57	12.57	-6.92	-99.7
45	292	-13565	11	-582	0	704	25	6.28	6.28	12.57	12.57	-7.76	-110.1
46	292	-13275	12	-309	0	365	25	6.28	6.28	12.57	12.57	-6.44	-93.3
47	292	-13035	14	-277	0	321	25	6.28	6.28	12.57	12.57	-6.19	-89.9
49	292	-13045	67	-293	0	344	37	6.28	6.28	12.57	12.57	-6.27	-91.0
50	292	-13035	-40	-281	0	327	13	6.28	6.28	12.57	12.57	-6.21	-90.2
51	292	-13015	15	-322	0	376	26	6.28	6.28	12.57	12.57	-6.37	-92.2

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	390	-13720	163	-481	0	1079	216	6.28	6.28	12.57	12.57	-9.16	-127.8
41	390	-13680	4	-434	0	965	26	6.28	6.28	12.57	12.57	-8.74	-122.5
42	390	-13630	5	-570	0	1260	28	6.28	6.28	12.57	12.57	-9.78	-135.4
43	390	-13140	274	-434	0	968	349	6.28	6.28	12.57	12.57	-8.54	-119.5
44	390	-13080	-262	-374	0	822	-292	6.28	6.28	12.57	12.57	-8.00	-112.6
45	390	-12980	11	-582	0	1271	36	6.28	6.28	12.57	12.57	-9.57	-132.1
46	390	-12690	12	-309	0	666	37	6.28	6.28	12.57	12.57	-7.29	-103.4
47	390	-12450	14	-277	0	592	39	6.28	6.28	12.57	12.57	-6.93	-98.6
49	390	-12460	67	-293	0	630	103	6.28	6.28	12.57	12.57	-7.07	-100.4
50	390	-12450	-40	-281	0	601	-26	6.28	6.28	12.57	12.57	-6.96	-99.0
51	390	-12430	15	-322	0	690	40	6.28	6.28	12.57	12.57	-7.27	-102.9

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 49 NI 127 NF 126 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 19B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	

40	0	-15810	153	-188	0	-300	-460	6.28	6.28	12.57	12.57	-7.96	-111.0
41	0	-15810	9	-217	0	-348	-47	6.28	6.28	12.57	12.57	-7.35	-107.2
42	0	-15740	10	-274	0	-457	-50	6.28	6.28	12.57	12.57	-7.72	-111.7
43	0	-15210	249	-132	0	-216	-735	6.28	6.28	12.57	12.57	-9.11	-123.0
44	0	-15300	-232	-276	0	-442	642	6.28	6.28	12.57	12.57	-8.68	-118.3
45	0	-15090	10	-275	0	-478	-52	6.28	6.28	12.57	12.57	-7.54	-108.8
46	0	-14860	8	-157	0	-264	-47	6.28	6.28	12.57	12.57	-6.69	-97.9
47	0	-14620	8	-142	0	-243	-47	6.28	6.28	12.57	12.57	-6.52	-95.6
49	0	-14620	56	-132	0	-228	-184	6.28	6.28	12.57	12.57	-6.46	-94.9
50	0	-14640	-40	-161	0	-272	91	6.28	6.28	12.57	12.57	-6.63	-97.0
51	0	-14600	9	-161	0	-280	-48	6.28	6.28	12.57	12.57	-6.64	-97.1

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	97	-15225	153	-188	0	-117	-311	6.28	6.28	12.57	12.57	-7.02	-99.5
41	97	-15225	9	-217	0	-137	-39	6.28	6.28	12.57	12.57	-6.37	-94.4
42	97	-15155	10	-274	0	-190	-40	6.28	6.28	12.57	12.57	-6.54	-96.3
43	97	-14625	249	-132	0	-87	-492	6.28	6.28	12.57	12.57	-7.70	-106.4
44	97	-14715	-232	-276	0	-173	416	6.28	6.28	12.57	12.57	-7.35	-102.6
45	97	-14505	10	-275	0	-209	-42	6.28	6.28	12.57	12.57	-6.35	-93.4
46	97	-14275	8	-157	0	-112	-39	6.28	6.28	12.57	12.57	-5.91	-87.7
47	97	-14035	8	-142	0	-105	-39	6.28	6.28	12.57	12.57	-5.80	-86.0
49	97	-14035	56	-132	0	-98	-130	6.28	6.28	12.57	12.57	-5.77	-85.7
50	97	-14055	-40	-161	0	-116	52	6.28	6.28	12.57	12.57	-5.84	-86.6
51	97	-14015	9	-161	0	-123	-39	6.28	6.28	12.57	12.57	-5.85	-86.7

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	195	-14640	153	-188	0	67	-162	6.28	6.28	12.57	12.57	-6.07	-88.1
41	195	-14640	9	-217	0	74	-30	6.28	6.28	12.57	12.57	-5.92	-88.2
42	195	-14570	10	-274	0	77	-31	6.28	6.28	12.57	12.57	-5.91	-87.9
43	195	-14040	249	-132	0	42	-250	6.28	6.28	12.57	12.57	-6.29	-89.7
44	195	-14130	-232	-276	0	96	190	6.28	6.28	12.57	12.57	-6.03	-86.9
45	195	-13920	10	-275	0	59	-32	6.28	6.28	12.57	12.57	-5.59	-83.3
46	195	-13690	8	-157	0	41	-31	6.28	6.28	12.57	12.57	-5.44	-81.2
47	195	-13450	8	-142	0	33	-31	6.28	6.28	12.57	12.57	-5.31	-79.4
49	195	-13450	56	-132	0	31	-75	6.28	6.28	12.57	12.57	-5.31	-79.3
50	195	-13470	-40	-161	0	42	13	6.28	6.28	12.57	12.57	-5.35	-79.9
51	195	-13430	9	-161	0	34	-31	6.28	6.28	12.57	12.57	-5.31	-79.3

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	292	-14055	153	-188	0	251	-13	6.28	6.28	12.57	12.57	-6.33	-92.7

41	292	-14055	9	-217	0	286	-22	6.28	6.28	12.57	12.57	-6.45	-94.2
42	292	-13985	10	-274	0	345	-21	6.28	6.28	12.57	12.57	-6.64	-96.5
43	292	-13455	249	-132	0	170	-7	6.28	6.28	12.57	12.57	-5.81	-85.6
44	292	-13545	-232	-276	0	365	-36	6.28	6.28	12.57	12.57	-6.54	-94.8
45	292	-13335	10	-275	0	327	-21	6.28	6.28	12.57	12.57	-6.32	-91.9
46	292	-13105	8	-157	0	194	-23	6.28	6.28	12.57	12.57	-5.76	-84.6
47	292	-12865	8	-142	0	171	-23	6.28	6.28	12.57	12.57	-5.58	-82.2
49	292	-12865	56	-132	0	160	-20	6.28	6.28	12.57	12.57	-5.54	-81.7
50	292	-12885	-40	-161	0	198	-26	6.28	6.28	12.57	12.57	-5.69	-83.6
51	292	-12845	9	-161	0	191	-23	6.28	6.28	12.57	12.57	-5.65	-83.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	390	-13470	153	-188	0	435	136	6.28	6.28	12.57	12.57	-6.76	-97.5
41	390	-13470	9	-217	0	497	-13	6.28	6.28	12.57	12.57	-6.98	-100.3
42	390	-13400	10	-274	0	612	-11	6.28	6.28	12.57	12.57	-7.37	-105.0
43	390	-12870	249	-132	0	299	235	6.28	6.28	12.57	12.57	-6.04	-88.0
44	390	-12960	-232	-276	0	634	-263	6.28	6.28	12.57	12.57	-7.28	-103.5
45	390	-12750	10	-275	0	595	-11	6.28	6.28	12.57	12.57	-7.05	-100.5
46	390	-12520	8	-157	0	347	-14	6.28	6.28	12.57	12.57	-6.08	-88.1
47	390	-12280	8	-142	0	309	-15	6.28	6.28	12.57	12.57	-5.85	-85.0
49	390	-12280	56	-132	0	289	35	6.28	6.28	12.57	12.57	-5.78	-84.1
50	390	-12300	-40	-161	0	356	-65	6.28	6.28	12.57	12.57	-6.02	-87.2
51	390	-12260	9	-161	0	348	-14	6.28	6.28	12.57	12.57	-5.98	-86.6

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 50 NI 166 NF 167 SEZ. Rp B= 0.400 H= 0.600 (pilastro)
PIL. NUM. 26B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	--												
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-9179	-395	-221	0	-587	603	12.57	12.57	6.28	6.28	-6.21	-82.2
41	0	-8666	-648	-173	0	-499	1391	12.57	12.57	6.28	6.28	-8.69	-116.3
42	0	-8667	-658	-47	0	-224	1398	12.57	12.57	6.28	6.28	-8.72	-116.7
43	0	-9208	-96	-170	0	-479	-98	12.57	12.57	6.28	6.28	-5.68	-76.4
44	0	-7737	-1091	-120	0	-399	2735	12.57	12.57	6.28	6.28	-17.67	338.0
45	0	-8356	-535	121	0	126	1227	12.57	12.57	6.28	6.28	-7.81	-105.3
46	0	-8166	-439	-38	0	-232	1111	12.57	12.57	6.28	6.28	-7.23	-98.1
47	0	-8041	-386	-5	0	-166	1040	12.57	12.57	6.28	6.28	-6.88	-93.7
49	0	-8212	-302	-21	0	-195	778	12.57	12.57	6.28	6.28	-5.96	-82.4
50	0	-7918	-501	-11	0	-179	1344	12.57	12.57	6.28	6.28	-8.32	-110.8
51	0	-8042	-390	37	0	-74	1043	12.57	12.57	6.28	6.28	-6.90	-93.9

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	97	-8594	-395	-221	0	-371	218	12.57	12.57	6.28	6.28	-4.93	-67.0
41	97	-8081	-648	-173	0	-330	760	12.57	12.57	6.28	6.28	-5.84	-80.8
42	97	-8082	-658	-47	0	-178	756	12.57	12.57	6.28	6.28	-5.83	-80.7
43	97	-8623	-96	-170	0	-314	-192	12.57	12.57	6.28	6.28	-4.66	-64.0
44	97	-7152	-1091	-120	0	-282	1671	12.57	12.57	6.28	6.28	-10.36	-132.2
45	97	-7771	-535	121	0	9	706	12.57	12.57	6.28	6.28	-5.53	-76.6
46	97	-7581	-439	-38	0	-195	683	12.57	12.57	6.28	6.28	-5.37	-74.5
47	97	-7456	-386	-5	0	-161	663	12.57	12.57	6.28	6.28	-5.26	-72.9
49	97	-7627	-302	-21	0	-175	483	12.57	12.57	6.28	6.28	-4.68	-65.8
50	97	-7333	-501	-11	0	-168	855	12.57	12.57	6.28	6.28	-5.90	-80.9
51	97	-7457	-390	37	0	-110	663	12.57	12.57	6.28	6.28	-5.25	-72.9

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	195	-8009	-395	-221	0	-155	-167	12.57	12.57	6.28	6.28	-3.69	-53.9
41	195	-7496	-648	-173	0	-161	128	12.57	12.57	6.28	6.28	-3.50	-49.5
42	195	-7497	-658	-47	0	-131	114	12.57	12.57	6.28	6.28	-3.35	-48.6
43	195	-8038	-96	-170	0	-149	-286	12.57	12.57	6.28	6.28	-4.13	-59.4
44	195	-6567	-1091	-120	0	-164	608	12.57	12.57	6.28	6.28	-4.71	-65.2
45	195	-7186	-535	121	0	-109	184	12.57	12.57	6.28	6.28	-3.44	-49.9
46	195	-6996	-439	-38	0	-158	255	12.57	12.57	6.28	6.28	-3.62	-52.0
47	195	-6871	-386	-5	0	-157	286	12.57	12.57	6.28	6.28	-3.68	-52.6
49	195	-7042	-302	-21	0	-154	188	12.57	12.57	6.28	6.28	-3.39	-49.2
50	195	-6748	-501	-11	0	-158	366	12.57	12.57	6.28	6.28	-3.92	-55.5
51	195	-6872	-390	37	0	-147	282	12.57	12.57	6.28	6.28	-3.67	-52.5

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	292	-7424	-395	-221	0	61	-552	12.57	12.57	6.28	6.28	-4.85	-67.7
41	292	-6911	-648	-173	0	7	-503	12.57	12.57	6.28	6.28	-4.47	-62.6
42	292	-6912	-658	-47	0	-85	-527	12.57	12.57	6.28	6.28	-4.56	-63.7
43	292	-7453	-96	-170	0	17	-379	12.57	12.57	6.28	6.28	-4.24	-60.2
44	292	-5982	-1091	-120	0	-47	-456	12.57	12.57	6.28	6.28	-3.94	-55.1
45	292	-6601	-535	121	0	-227	-337	12.57	12.57	6.28	6.28	-3.76	-53.3
46	292	-6411	-439	-38	0	-120	-173	12.57	12.57	6.28	6.28	-3.09	-44.9
47	292	-6286	-386	-5	0	-152	-90	12.57	12.57	6.28	6.28	-3.01	-42.4
49	292	-6457	-302	-21	0	-134	-107	12.57	12.57	6.28	6.28	-2.99	-42.3
50	292	-6163	-501	-11	0	-147	-122	12.57	12.57	6.28	6.28	-2.95	-41.5
51	292	-6287	-390	37	0	-183	-98	12.57	12.57	6.28	6.28	-3.17	-44.1

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	390	-6839	-395	-221	0	277	-937	12.57	12.57	6.28	6.28	-6.08	-82.5
41	390	-6326	-648	-173	0	176	-1134	12.57	12.57	6.28	6.28	-6.99	-92.5
42	390	-6327	-658	-47	0	-39	-1169	12.57	12.57	6.28	6.28	-7.19	-94.8
43	390	-6868	-96	-170	0	182	-473	12.57	12.57	6.28	6.28	-4.35	-61.0
44	390	-5397	-1091	-120	0	71	-1520	12.57	12.57	6.28	6.28	-9.61	133.3
45	390	-6016	-535	121	0	-344	-859	12.57	12.57	6.28	6.28	-5.51	-74.5
46	390	-5826	-439	-38	0	-83	-600	12.57	12.57	6.28	6.28	-4.40	-60.6
47	390	-5701	-386	-5	0	-148	-467	12.57	12.57	6.28	6.28	-3.88	-53.9
49	390	-5872	-302	-21	0	-114	-402	12.57	12.57	6.28	6.28	-3.71	-52.0
50	390	-5578	-501	-11	0	-136	-611	12.57	12.57	6.28	6.28	-4.34	-59.7
51	390	-5702	-390	37	0	-219	-479	12.57	12.57	6.28	6.28	-3.92	-54.5

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

ASTA NUM. 51 NI 168 NF 169 SEZ. Rp B= 0.400 H= 0.600 (pilastro)
PIL. NUM. 11B

armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-5524	1229	380	0	379	-3165	12.57	12.57	6.28	6.28	-20.83	599.8
41	0	-5893	600	354	0	327	-1756	12.57	12.57	6.28	6.28	-11.16	169.7
42	0	-5881	603	324	0	270	-1762	12.57	12.57	6.28	6.28	-11.21	171.8
43	0	-5275	1536	389	0	402	-3865	12.57	12.57	6.28	6.28	-25.44	831.9
44	0	-6400	-430	306	0	240	555	12.57	12.57	6.28	6.28	-4.46	-61.9
45	0	-5869	494	297	0	218	-1526	12.57	12.57	6.28	6.28	-9.56	-119.9
46	0	-5887	421	342	0	307	-1372	12.57	12.57	6.28	6.28	-8.50	-108.5
47	0	-5886	376	338	0	302	-1276	12.57	12.57	6.28	6.28	-7.86	-101.5
49	0	-5763	585	347	0	320	-1746	12.57	12.57	6.28	6.28	-11.12	173.4
50	0	-5988	192	330	0	287	-862	12.57	12.57	6.28	6.28	-5.51	-74.5
51	0	-5882	377	329	0	283	-1278	12.57	12.57	6.28	6.28	-7.88	-101.6

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	97	-4939	1229	380	0	9	-1967	12.57	12.57	6.28	6.28	-12.81	278.5
41	97	-5308	600	354	0	-18	-1171	12.57	12.57	6.28	6.28	-7.22	-93.0
42	97	-5296	603	324	0	-47	-1174	12.57	12.57	6.28	6.28	-7.24	-93.2
43	97	-4690	1536	389	0	22	-2367	12.57	12.57	6.28	6.28	-15.55	412.3
44	97	-5815	-430	306	0	-58	136	12.57	12.57	6.28	6.28	-2.73	-39.8
45	97	-5284	494	297	0	-71	-1045	12.57	12.57	6.28	6.28	-6.42	-83.9
46	97	-5302	421	342	0	-26	-962	12.57	12.57	6.28	6.28	-5.92	-78.3
47	97	-5301	376	338	0	-28	-910	12.57	12.57	6.28	6.28	-5.63	-74.8
49	97	-5178	585	347	0	-19	-1175	12.57	12.57	6.28	6.28	-7.26	-93.1
50	97	-5403	192	330	0	-35	-675	12.57	12.57	6.28	6.28	-4.52	-61.7
51	97	-5297	377	329	0	-38	-911	12.57	12.57	6.28	6.28	-5.63	-74.9

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	195	-4354	1229	380	0	-361	-769	12.57	12.57	6.28	6.28	-4.74	-62.9
41	195	-4723	600	354	0	-363	-586	12.57	12.57	6.28	6.28	-3.94	-53.8
42	195	-4711	603	324	0	-363	-585	12.57	12.57	6.28	6.28	-3.93	-53.7
43	195	-4105	1536	389	0	-357	-870	12.57	12.57	6.28	6.28	-5.35	-69.3
44	195	-5230	-430	306	0	-356	-284	12.57	12.57	6.28	6.28	-3.64	-48.0
45	195	-4699	494	297	0	-360	-563	12.57	12.57	6.28	6.28	-3.84	-52.5
46	195	-4717	421	342	0	-359	-552	12.57	12.57	6.28	6.28	-3.80	-52.1
47	195	-4716	376	338	0	-358	-543	12.57	12.57	6.28	6.28	-3.77	-51.7
49	195	-4593	585	347	0	-357	-604	12.57	12.57	6.28	6.28	-3.98	-54.1
50	195	-4818	192	330	0	-357	-487	12.57	12.57	6.28	6.28	-3.61	-49.7
51	195	-4712	377	329	0	-358	-543	12.57	12.57	6.28	6.28	-3.77	-51.7

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	292	-3769	1229	380	0	-732	429	12.57	12.57	6.28	6.28	-5.98	-68.0
41	292	-4138	600	354	0	-709	-2	12.57	12.57	6.28	6.28	-5.80	-67.6
42	292	-4126	603	324	0	-679	3	12.57	12.57	6.28	6.28	-5.57	-65.4
43	292	-3520	1536	389	0	-737	628	12.57	12.57	6.28	6.28	-6.02	70.1
44	292	-4645	-430	306	0	-653	-703	12.57	12.57	6.28	6.28	-5.40	-65.3
45	292	-4114	494	297	0	-650	-82	12.57	12.57	6.28	6.28	-5.34	-63.2
46	292	-4132	421	342	0	-692	-142	12.57	12.57	6.28	6.28	-5.67	-66.4
47	292	-4131	376	338	0	-688	-177	12.57	12.57	6.28	6.28	-5.64	-66.1
49	292	-4008	585	347	0	-696	-34	12.57	12.57	6.28	6.28	-5.70	-66.2
50	292	-4233	192	330	0	-679	-300	12.57	12.57	6.28	6.28	-5.57	-65.8
51	292	-4127	377	329	0	-678	-176	12.57	12.57	6.28	6.28	-5.56	-65.3

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	390	-3184	1229	380	0	-1102	1627	12.57	12.57	6.28	6.28	-10.69	285.9
41	390	-3553	600	354	0	-1054	583	12.57	12.57	6.28	6.28	-8.56	143.8
42	390	-3541	603	324	0	-996	591	12.57	12.57	6.28	6.28	-8.09	130.1
43	390	-2935	1536	389	0	-1116	2126	12.57	12.57	6.28	6.28	-13.99	455.3
44	390	-4060	-430	306	0	-951	-1123	12.57	12.57	6.28	6.28	-7.76	104.0
45	390	-3529	494	297	0	-939	399	12.57	12.57	6.28	6.28	-7.64	116.9
46	390	-3547	421	342	0	-1025	268	12.57	12.57	6.28	6.28	-8.33	137.0
47	390	-3546	376	338	0	-1018	189	12.57	12.57	6.28	6.28	-8.27	135.3
49	390	-3423	585	347	0	-1034	537	12.57	12.57	6.28	6.28	-8.39	143.1
50	390	-3648	192	330	0	-1001	-113	12.57	12.57	6.28	6.28	-8.14	128.1
51	390	-3542	377	329	0	-999	192	12.57	12.57	6.28	6.28	-8.12	130.8

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

ASTA NUM. 52 NI 170 NF 171 SEZ. Rp B= 0.400 H= 0.600 (pilastro)
PIL. NUM. 16B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-9446	1877	541	0	520	-3385	12.57	12.57	6.28	6.28	-21.89	425.4
41	0	-9467	958	552	0	534	-1665	12.57	12.57	6.28	6.28	-10.27	-136.3
42	0	-9401	963	488	0	424	-1676	12.57	12.57	6.28	6.28	-10.33	-136.8
43	0	-9281	2326	524	0	505	-4237	12.57	12.57	6.28	6.28	-27.76	682.0
44	0	-9300	-547	552	0	538	1153	12.57	12.57	6.28	6.28	-7.76	-105.9
45	0	-9206	803	436	0	346	-1387	12.57	12.57	6.28	6.28	-8.77	-118.1
46	0	-9227	696	538	0	525	-1193	12.57	12.57	6.28	6.28	-7.90	-107.5
47	0	-9167	631	534	0	523	-1075	12.57	12.57	6.28	6.28	-7.40	-101.4
49	0	-9160	937	530	0	518	-1648	12.57	12.57	6.28	6.28	-10.15	-134.3
50	0	-9164	362	536	0	525	-570	12.57	12.57	6.28	6.28	-5.89	-78.7
51	0	-9145	632	513	0	487	-1078	12.57	12.57	6.28	6.28	-7.41	-101.4

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	97	-8861	1877	541	0	-7	-1555	12.57	12.57	6.28	6.28	-9.60	-127.3
41	97	-8882	958	552	0	-5	-731	12.57	12.57	6.28	6.28	-6.05	-84.2
42	97	-8816	963	488	0	-52	-736	12.57	12.57	6.28	6.28	-6.04	-84.1
43	97	-8696	2326	524	0	-5	-1969	12.57	12.57	6.28	6.28	-12.17	-156.1
44	97	-8715	-547	552	0	-0	620	12.57	12.57	6.28	6.28	-5.59	-78.3
45	97	-8621	803	436	0	-79	-604	12.57	12.57	6.28	6.28	-5.49	-77.0

46	97	-8642	696	538	0	1	-514	12.57	12.57	6.28	6.28	-5.18	-73.1
47	97	-8582	631	534	0	2	-460	12.57	12.57	6.28	6.28	-4.96	-70.3
49	97	-8575	937	530	0	1	-734	12.57	12.57	6.28	6.28	-5.94	-82.6
50	97	-8579	362	536	0	2	-217	12.57	12.57	6.28	6.28	-4.09	-59.4
51	97	-8560	632	513	0	-13	-461	12.57	12.57	6.28	6.28	-4.96	-70.2

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	195	-8276	1877	541	0	-535	276	12.57	12.57	6.28	6.28	-5.62	-74.4
41	195	-8297	958	552	0	-544	204	12.57	12.57	6.28	6.28	-5.67	-75.0
42	195	-8231	963	488	0	-527	203	12.57	12.57	6.28	6.28	-5.57	-73.8
43	195	-8111	2326	524	0	-516	299	12.57	12.57	6.28	6.28	-5.47	-72.5
44	195	-8130	-547	552	0	-538	87	12.57	12.57	6.28	6.28	-5.59	-73.8
45	195	-8036	803	436	0	-504	179	12.57	12.57	6.28	6.28	-5.38	-71.4
46	195	-8057	696	538	0	-524	165	12.57	12.57	6.28	6.28	-5.49	-72.6
47	195	-7997	631	534	0	-519	155	12.57	12.57	6.28	6.28	-5.44	-72.0
49	195	-7990	937	530	0	-516	180	12.57	12.57	6.28	6.28	-5.43	-71.8
50	195	-7994	362	536	0	-520	137	12.57	12.57	6.28	6.28	-5.45	-72.1
51	195	-7975	632	513	0	-513	156	12.57	12.57	6.28	6.28	-5.41	-71.6

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	292	-7691	1877	541	0	-1062	2106	12.57	12.57	6.28	6.28	-13.27	175.4
41	292	-7712	958	552	0	-1082	1138	12.57	12.57	6.28	6.28	-8.94	-108.2
42	292	-7646	963	488	0	-1003	1142	12.57	12.57	6.28	6.28	-8.33	-102.1
43	292	-7526	2326	524	0	-1026	2567	12.57	12.57	6.28	6.28	-16.53	302.9
44	292	-7545	-547	552	0	-1076	-446	12.57	12.57	6.28	6.28	-8.88	-107.2
45	292	-7451	803	436	0	-929	962	12.57	12.57	6.28	6.28	-7.76	-95.9
46	292	-7472	696	538	0	-1048	844	12.57	12.57	6.28	6.28	-8.66	-104.8
47	292	-7412	631	534	0	-1040	770	12.57	12.57	6.28	6.28	-8.59	-104.0
49	292	-7405	937	530	0	-1033	1093	12.57	12.57	6.28	6.28	-8.53	-103.4
50	292	-7409	362	536	0	-1043	490	12.57	12.57	6.28	6.28	-8.61	-104.2
51	292	-7390	632	513	0	-1013	772	12.57	12.57	6.28	6.28	-8.38	-101.9

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	390	-7106	1877	541	0	-1589	3936	12.57	12.57	6.28	6.28	-25.90	730.4
41	390	-7127	958	552	0	-1621	2072	12.57	12.57	6.28	6.28	-13.22	192.2
42	390	-7061	963	488	0	-1479	2082	12.57	12.57	6.28	6.28	-13.22	197.7
43	390	-6941	2326	524	0	-1537	4835	12.57	12.57	6.28	6.28	-31.83	1017.2
44	390	-6960	-547	552	0	-1614	-979	12.57	12.57	6.28	6.28	-13.16	174.4
45	390	-6866	803	436	0	-1354	1745	12.57	12.57	6.28	6.28	-11.07	-137.3
46	390	-6887	696	538	0	-1573	1523	12.57	12.57	6.28	6.28	-12.83	167.1
47	390	-6827	631	534	0	-1561	1385	12.57	12.57	6.28	6.28	-12.73	166.0
49	390	-6820	937	530	0	-1550	2007	12.57	12.57	6.28	6.28	-12.74	190.0
50	390	-6824	362	536	0	-1565	844	12.57	12.57	6.28	6.28	-12.77	167.0
51	390	-6805	632	513	0	-1513	1389	12.57	12.57	6.28	6.28	-12.35	155.6

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

ASTA NUM. 53 NI 172 NF 185 SEZ. Rp B= 0.400 H= 0.600 (pilastro)
PIL. NUM. 21B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-9467	1808	620	0	659	-3480	12.57	12.57	6.28	6.28	-22.54	451.0
41	0	-9498	865	598	0	620	-1691	12.57	12.57	6.28	6.28	-10.42	-138.1
42	0	-9523	870	573	0	570	-1698	12.57	12.57	6.28	6.28	-10.47	-138.6
43	0	-9292	2261	612	0	656	-4349	12.57	12.57	6.28	6.28	-28.52	714.6
44	0	-9350	-681	544	0	540	1246	12.57	12.57	6.28	6.28	-8.16	-110.9
45	0	-9384	697	533	0	508	-1378	12.57	12.57	6.28	6.28	-8.77	-118.3
46	0	-9251	584	562	0	574	-1172	12.57	12.57	6.28	6.28	-7.82	-106.6
47	0	-9190	514	553	0	562	-1042	12.57	12.57	6.28	6.28	-7.29	-99.9
49	0	-9179	828	560	0	575	-1639	12.57	12.57	6.28	6.28	-10.10	-133.8
50	0	-9191	240	546	0	552	-520	12.57	12.57	6.28	6.28	-6.04	-80.3
51	0	-9198	516	544	0	546	-1045	12.57	12.57	6.28	6.28	-7.30	-100.1

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	97	-8882	1808	620	0	54	-1718	12.57	12.57	6.28	6.28	-10.55	-138.4
41	97	-8913	865	598	0	36	-847	12.57	12.57	6.28	6.28	-6.48	-89.6
42	97	-8938	870	573	0	11	-850	12.57	12.57	6.28	6.28	-6.50	-89.8
43	97	-8707	2261	612	0	60	-2145	12.57	12.57	6.28	6.28	-13.36	-169.1
44	97	-8765	-681	544	0	9	582	12.57	12.57	6.28	6.28	-5.47	-76.9
45	97	-8799	697	533	0	-13	-698	12.57	12.57	6.28	6.28	-5.90	-82.3
46	97	-8666	584	562	0	26	-602	12.57	12.57	6.28	6.28	-5.50	-77.2
47	97	-8605	514	553	0	23	-541	12.57	12.57	6.28	6.28	-5.26	-74.1
49	97	-8594	828	560	0	29	-831	12.57	12.57	6.28	6.28	-6.30	-87.0
50	97	-8606	240	546	0	19	-286	12.57	12.57	6.28	6.28	-4.35	-62.7
51	97	-8613	516	544	0	15	-542	12.57	12.57	6.28	6.28	-5.27	-74.2

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	195	-8297	1808	620	0	-551	45	12.57	12.57	6.28	6.28	-5.71	-75.4
41	195	-8328	865	598	0	-547	-4	12.57	12.57	6.28	6.28	-5.70	-75.4
42	195	-8353	870	573	0	-548	-2	12.57	12.57	6.28	6.28	-5.71	-75.6
43	195	-8122	2261	612	0	-537	59	12.57	12.57	6.28	6.28	-5.58	-73.7
44	195	-8180	-681	544	0	-522	-82	12.57	12.57	6.28	6.28	-5.52	-73.2
45	195	-8214	697	533	0	-533	-19	12.57	12.57	6.28	6.28	-5.59	-74.0
46	195	-8081	584	562	0	-522	-32	12.57	12.57	6.28	6.28	-5.49	-72.6
47	195	-8020	514	553	0	-515	-39	12.57	12.57	6.28	6.28	-5.43	-72.0
49	195	-8009	828	560	0	-516	-24	12.57	12.57	6.28	6.28	-5.44	-72.0
50	195	-8021	240	546	0	-513	-52	12.57	12.57	6.28	6.28	-5.43	-71.9
51	195	-8028	516	544	0	-516	-39	12.57	12.57	6.28	6.28	-5.44	-72.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	292	-7712	1808	620	0	-1155	1807	12.57	12.57	6.28	6.28	-11.20	-142.9
41	292	-7743	865	598	0	-1131	840	12.57	12.57	6.28	6.28	-9.31	-111.9
42	292	-7768	870	573	0	-1106	846	12.57	12.57	6.28	6.28	-9.13	-110.2
43	292	-7537	2261	612	0	-1134	2263	12.57	12.57	6.28	6.28	-14.40	221.4
44	292	-7595	-681	544	0	-1052	-745	12.57	12.57	6.28	6.28	-8.70	-105.5
45	292	-7629	697	533	0	-1053	660	12.57	12.57	6.28	6.28	-8.71	-105.7
46	292	-7496	584	562	0	-1069	537	12.57	12.57	6.28	6.28	-8.82	-106.5

47	292	-7435	514	553	0	-1054	462	12.57	12.57	6.28	6.28	-8.70	-105.1
49	292	-7424	828	560	0	-1062	784	12.57	12.57	6.28	6.28	-8.76	-105.7
50	292	-7436	240	546	0	-1046	183	12.57	12.57	6.28	6.28	-8.64	-104.5
51	292	-7443	516	544	0	-1046	464	12.57	12.57	6.28	6.28	-8.64	-104.6

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	390	-7127	1808	620	0	-1760	3570	12.57	12.57	6.28	6.28	-23.45	618.3
41	390	-7158	865	598	0	-1714	1684	12.57	12.57	6.28	6.28	-13.97	192.0
42	390	-7183	870	573	0	-1665	1694	12.57	12.57	6.28	6.28	-13.58	179.9
43	390	-6952	2261	612	0	-1730	4467	12.57	12.57	6.28	6.28	-29.42	903.1
44	390	-7010	-681	544	0	-1583	-1409	12.57	12.57	6.28	6.28	-12.92	165.9
45	390	-7044	697	533	0	-1573	1340	12.57	12.57	6.28	6.28	-12.84	162.6
46	390	-6911	584	562	0	-1617	1107	12.57	12.57	6.28	6.28	-13.19	176.5
47	390	-6850	514	553	0	-1593	963	12.57	12.57	6.28	6.28	-12.99	172.7
49	390	-6839	828	560	0	-1608	1592	12.57	12.57	6.28	6.28	-13.11	176.5
50	390	-6851	240	546	0	-1579	417	12.57	12.57	6.28	6.28	-12.88	169.5
51	390	-6858	516	544	0	-1577	966	12.57	12.57	6.28	6.28	-12.86	168.8

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

ASTA NUM. 54 NI 167 NF 208 SEZ. Rp B= 0.400 H= 0.600 (pilastro)
PIL. NUM. 26C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-2299	4043	-1298	0	1326	-4206	12.57	12.57	6.28	6.28	-27.25	1151.0
41	0	-2168	2929	-1120	0	1239	-3135	12.57	12.57	6.28	6.28	-20.40	824.6
42	0	-1939	2986	-182	0	1394	-3189	12.57	12.57	6.28	6.28	-20.70	858.3
43	0	-2174	4193	-1115	0	1268	-4298	12.57	12.57	6.28	6.28	-27.80	1189.0
44	0	-1981	1168	-871	0	1101	-1450	12.57	12.57	6.28	6.28	-9.54	312.0
45	0	-1575	2432	744	0	1382	-2604	12.57	12.57	6.28	6.28	-16.90	701.5
46	0	-1829	1982	-637	0	1053	-2140	12.57	12.57	6.28	6.28	-13.98	537.6
47	0	-1745	1745	-516	0	1007	-1892	12.57	12.57	6.28	6.28	-12.38	466.1
49	0	-1788	2116	-576	0	1036	-2249	12.57	12.57	6.28	6.28	-14.67	574.7
50	0	-1750	1511	-527	0	1002	-1679	12.57	12.57	6.28	6.28	-11.01	399.3
51	0	-1668	1764	-204	0	1059	-1910	12.57	12.57	6.28	6.28	-12.48	477.3

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	12	-2224	4043	-1298	0	1488	-3700	12.57	12.57	6.28	6.28	-24.01	997.9
41	12	-2093	2929	-1120	0	1379	-2769	12.57	12.57	6.28	6.28	-18.05	715.3
42	12	-1864	2986	-182	0	1417	-2816	12.57	12.57	6.28	6.28	-18.31	746.7
43	12	-2099	4193	-1115	0	1408	-3774	12.57	12.57	6.28	6.28	-24.45	1030.0
44	12	-1906	1168	-871	0	1210	-1304	12.57	12.57	6.28	6.28	-9.59	272.0
45	12	-1500	2432	744	0	1289	-2300	12.57	12.57	6.28	6.28	-14.95	611.6
46	12	-1754	1982	-637	0	1133	-1892	12.57	12.57	6.28	6.28	-12.38	465.6
47	12	-1670	1745	-516	0	1072	-1674	12.57	12.57	6.28	6.28	-10.97	403.3
49	12	-1713	2116	-576	0	1108	-1984	12.57	12.57	6.28	6.28	-12.97	497.3
50	12	-1675	1511	-527	0	1068	-1490	12.57	12.57	6.28	6.28	-9.78	345.8
51	12	-1593	1764	-204	0	1084	-1690	12.57	12.57	6.28	6.28	-11.06	413.8

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	25	-2149	4043	-1298	0	1650	-3195	12.57	12.57	6.28	6.28	-20.78	844.8
41	25	-2018	2929	-1120	0	1519	-2402	12.57	12.57	6.28	6.28	-15.69	606.1
42	25	-1789	2986	-182	0	1440	-2442	12.57	12.57	6.28	6.28	-15.91	635.2
43	25	-2024	4193	-1115	0	1547	-3250	12.57	12.57	6.28	6.28	-21.10	871.0
44	25	-1831	1168	-871	0	1318	-1158	12.57	12.57	6.28	6.28	-10.41	269.3
45	25	-1425	2432	744	0	1196	-1996	12.57	12.57	6.28	6.28	-13.00	521.8
46	25	-1679	1982	-637	0	1212	-1644	12.57	12.57	6.28	6.28	-10.78	393.6
47	25	-1595	1745	-516	0	1136	-1456	12.57	12.57	6.28	6.28	-9.55	340.6
49	25	-1638	2116	-576	0	1180	-1720	12.57	12.57	6.28	6.28	-11.26	420.1
50	25	-1600	1511	-527	0	1134	-1301	12.57	12.57	6.28	6.28	-8.96	292.3
51	25	-1518	1764	-204	0	1110	-1469	12.57	12.57	6.28	6.28	-9.63	350.3

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	38	-2074	4043	-1298	0	1813	-2690	12.57	12.57	6.28	6.28	-17.54	691.9
41	38	-1943	2929	-1120	0	1659	-2036	12.57	12.57	6.28	6.28	-13.33	497.0
42	38	-1714	2986	-182	0	1463	-2069	12.57	12.57	6.28	6.28	-13.51	523.8
43	38	-1949	4193	-1115	0	1686	-2725	12.57	12.57	6.28	6.28	-17.74	712.2
44	38	-1756	1168	-871	0	1427	-1012	12.57	12.57	6.28	6.28	-11.23	299.7
45	38	-1350	2432	744	0	1103	-1692	12.57	12.57	6.28	6.28	-11.04	432.0
46	38	-1604	1982	-637	0	1292	-1397	12.57	12.57	6.28	6.28	-10.17	321.7
47	38	-1520	1745	-516	0	1200	-1237	12.57	12.57	6.28	6.28	-9.46	278.0
49	38	-1563	2116	-576	0	1252	-1456	12.57	12.57	6.28	6.28	-9.86	342.9
50	38	-1525	1511	-527	0	1200	-1112	12.57	12.57	6.28	6.28	-9.45	250.2
51	38	-1443	1764	-204	0	1136	-1248	12.57	12.57	6.28	6.28	-8.95	286.9

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	50	-1999	4043	-1298	0	1975	-2184	12.57	12.57	6.28	6.28	-15.46	539.2
41	50	-1868	2929	-1120	0	1799	-1670	12.57	12.57	6.28	6.28	-14.09	390.4
42	50	-1639	2986	-182	0	1486	-1696	12.57	12.57	6.28	6.28	-11.66	412.5
43	50	-1874	4193	-1115	0	1826	-2201	12.57	12.57	6.28	6.28	-14.38	553.5
44	50	-1681	1168	-871	0	1536	-866	12.57	12.57	6.28	6.28	-12.05	330.2
45	50	-1275	2432	744	0	1010	-1388	12.57	12.57	6.28	6.28	-9.08	342.3
46	50	-1529	1982	-637	0	1372	-1149	12.57	12.57	6.28	6.28	-10.77	293.9
47	50	-1445	1745	-516	0	1265	-1019	12.57	12.57	6.28	6.28	-9.94	269.7
49	50	-1488	2116	-576	0	1324	-1191	12.57	12.57	6.28	6.28	-10.39	283.2
50	50	-1450	1511	-527	0	1266	-924	12.57	12.57	6.28	6.28	-9.94	269.8
51	50	-1368	1764	-204	0	1161	-1028	12.57	12.57	6.28	6.28	-9.13	246.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

ASTA NUM. 55 NI 122 NF 165 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 24B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf

	cm		daN		daN*m			cm²				daN/cm²	
40	0	-9435	87	-634	0	-1238	-139	6.28	6.28	9.42	9.42	-10.46	-142.5
41	0	-9394	-9	-518	0	-1019	135	6.28	6.28	9.42	9.42	-9.37	-129.0
42	0	-9382	-10	-298	0	-588	136	6.28	6.28	9.42	9.42	-7.40	-104.3
43	0	-9163	156	-609	0	-1187	-339	6.28	6.28	9.42	9.42	-10.08	-137.4
44	0	-9053	-171	-346	0	-689	594	6.28	6.28	9.42	9.42	-9.92	-120.6
45	0	-9075	-5	-50	0	-102	120	6.28	6.28	9.42	9.42	-5.46	-76.3
46	0	-8916	-1	-356	0	-702	108	6.28	6.28	9.42	9.42	-7.68	-107.3
47	0	-8797	1	-315	0	-623	101	6.28	6.28	9.42	9.42	-7.26	-101.9
49	0	-8810	33	-354	0	-696	10	6.28	6.28	9.42	9.42	-7.60	-106.1
50	0	-8788	-32	-301	0	-596	196	6.28	6.28	9.42	9.42	-7.14	-100.3
51	0	-8793	1	-242	0	-479	102	6.28	6.28	9.42	9.42	-6.61	-93.6

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	97	-8996	87	-634	0	-620	-55	6.28	6.28	9.42	9.42	-7.35	-103.2
41	97	-8955	-9	-518	0	-514	125	6.28	6.28	9.42	9.42	-6.85	-96.8
42	97	-8943	-10	-298	0	-297	126	6.28	6.28	9.42	9.42	-5.85	-84.4
43	97	-8724	156	-609	0	-593	-186	6.28	6.28	9.42	9.42	-7.09	-99.6
44	97	-8614	-171	-346	0	-352	427	6.28	6.28	9.42	9.42	-8.06	-101.3
45	97	-8636	-5	-50	0	-53	114	6.28	6.28	9.42	9.42	-5.20	-72.7
46	97	-8477	-1	-356	0	-355	107	6.28	6.28	9.42	9.42	-5.88	-84.2
47	97	-8358	1	-315	0	-315	102	6.28	6.28	9.42	9.42	-5.64	-81.0
49	97	-8371	33	-354	0	-351	42	6.28	6.28	9.42	9.42	-5.81	-83.2
50	97	-8349	-32	-301	0	-303	165	6.28	6.28	9.42	9.42	-5.58	-80.2
51	97	-8354	1	-242	0	-243	102	6.28	6.28	9.42	9.42	-5.31	-76.9

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	195	-8558	87	-634	0	-2	30	6.28	6.28	9.42	9.42	-4.39	-64.7
41	195	-8516	-9	-518	0	-8	116	6.28	6.28	9.42	9.42	-5.16	-72.0
42	195	-8504	-10	-298	0	-6	116	6.28	6.28	9.42	9.42	-5.15	-71.9
43	195	-8286	156	-609	0	0	-34	6.28	6.28	9.42	9.42	-4.29	-62.8
44	195	-8176	-171	-346	0	-15	260	6.28	6.28	9.42	9.42	-6.32	-82.8
45	195	-8198	-5	-50	0	-4	109	6.28	6.28	9.42	9.42	-4.94	-69.0
46	195	-8038	-1	-356	0	-8	106	6.28	6.28	9.42	9.42	-4.83	-67.6
47	195	-7920	1	-315	0	-8	103	6.28	6.28	9.42	9.42	-4.75	-66.5
49	195	-7932	33	-354	0	-6	74	6.28	6.28	9.42	9.42	-4.49	-63.9
50	195	-7910	-32	-301	0	-9	133	6.28	6.28	9.42	9.42	-5.02	-69.2
51	195	-7916	1	-242	0	-7	103	6.28	6.28	9.42	9.42	-4.74	-66.4

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	292	-8119	87	-634	0	615	115	6.28	6.28	9.42	9.42	-6.89	-96.3
41	292	-8078	-9	-518	0	497	107	6.28	6.28	9.42	9.42	-6.33	-89.3
42	292	-8066	-10	-298	0	285	106	6.28	6.28	9.42	9.42	-5.36	-77.1
43	292	-7847	156	-609	0	594	118	6.28	6.28	9.42	9.42	-6.66	-93.1
44	292	-7737	-171	-346	0	322	94	6.28	6.28	9.42	9.42	-5.36	-76.7
45	292	-7759	-5	-50	0	44	104	6.28	6.28	9.42	9.42	-4.68	-65.4
46	292	-7600	-1	-356	0	339	104	6.28	6.28	9.42	9.42	-5.37	-76.6
47	292	-7481	1	-315	0	299	104	6.28	6.28	9.42	9.42	-5.13	-73.5
49	292	-7494	33	-354	0	339	106	6.28	6.28	9.42	9.42	-5.31	-75.8
50	292	-7472	-32	-301	0	284	101	6.28	6.28	9.42	9.42	-5.05	-72.6
51	292	-7477	1	-242	0	229	103	6.28	6.28	9.42	9.42	-4.80	-69.4

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	390	-7680	87	-634	0	1233	200	6.28	6.28	9.42	9.42	-9.81	-131.7
41	390	-7639	-9	-518	0	1003	98	6.28	6.28	9.42	9.42	-8.47	-115.4
42	390	-7627	-10	-298	0	576	96	6.28	6.28	9.42	9.42	-6.46	-90.4
43	390	-7408	156	-609	0	1188	271	6.28	6.28	9.42	9.42	-9.45	-126.9
44	390	-7298	-171	-346	0	659	-73	6.28	6.28	9.42	9.42	-6.67	-92.6
45	390	-7320	-5	-50	0	93	98	6.28	6.28	9.42	9.42	-4.42	-61.7
46	390	-7161	-1	-356	0	686	103	6.28	6.28	9.42	9.42	-6.73	-93.1
47	390	-7042	1	-315	0	607	105	6.28	6.28	9.42	9.42	-6.31	-87.7
49	390	-7055	33	-354	0	683	138	6.28	6.28	9.42	9.42	-6.66	-92.2
50	390	-7033	-32	-301	0	578	70	6.28	6.28	9.42	9.42	-6.17	-86.0
51	390	-7038	1	-242	0	464	104	6.28	6.28	9.42	9.42	-5.66	-79.6

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 56 NI 209 NF 210 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 23B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	--												
	cm		daN			daN*m				cm²		daN/cm²	
40	0	-6278	138	-907	0	-1412	-151	6.28	6.28	9.42	9.42	-10.87	-140.6
41	0	-6153	80	-837	0	-1254	-23	6.28	6.28	9.42	9.42	-9.68	-126.7
42	0	-6038	87	-677	0	-896	-39	6.28	6.28	9.42	9.42	-7.27	-98.2
43	0	-6190	181	-866	0	-1345	-246	6.28	6.28	9.42	9.42	-10.36	-134.6
44	0	-5829	-18	-712	0	-994	191	6.28	6.28	9.42	9.42	-7.82	-104.3
45	0	-5791	97	-483	0	-486	-59	6.28	6.28	9.42	9.42	-5.13	-71.4
46	0	-5879	86	-698	0	-978	-37	6.28	6.28	9.42	9.42	-7.73	-103.4
47	0	-5811	87	-663	0	-909	-40	6.28	6.28	9.42	9.42	-7.28	-97.9
49	0	-5852	107	-686	0	-962	-83	6.28	6.28	9.42	9.42	-7.62	-102.0
50	0	-5780	67	-655	0	-892	4	6.28	6.28	9.42	9.42	-7.16	-96.4
51	0	-5773	90	-609	0	-790	-46	6.28	6.28	9.42	9.42	-6.57	-89.3

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	97	-5839	138	-907	0	-528	-16	6.28	6.28	9.42	9.42	-5.34	-74.1
41	97	-5714	80	-837	0	-438	55	6.28	6.28	9.42	9.42	-4.87	-68.1
42	97	-5599	87	-677	0	-236	46	6.28	6.28	9.42	9.42	-3.89	-55.7
43	97	-5751	181	-866	0	-501	-69	6.28	6.28	9.42	9.42	-5.18	-71.9
44	97	-5390	-18	-712	0	-300	174	6.28	6.28	9.42	9.42	-4.18	-57.8
45	97	-5352	97	-483	0	-15	36	6.28	6.28	9.42	9.42	-2.90	-41.8
46	97	-5440	86	-698	0	-298	47	6.28	6.28	9.42	9.42	-4.10	-58.0
47	97	-5372	87	-663	0	-263	45	6.28	6.28	9.42	9.42	-3.90	-55.5
49	97	-5413	107	-686	0	-293	21	6.28	6.28	9.42	9.42	-4.06	-57.6
50	97	-5341	67	-655	0	-253	70	6.28	6.28	9.42	9.42	-3.84	-54.7
51	97	-5334	90	-609	0	-196	42	6.28	6.28	9.42	9.42	-3.58	-51.4

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	195	-5400	138	-907	0	356	118	6.28	6.28	9.42	9.42	-4.34	-61.0
41	195	-5276	80	-837	0	378	133	6.28	6.28	9.42	9.42	-4.38	-61.3
42	195	-5160	87	-677	0	423	132	6.28	6.28	9.42	9.42	-4.53	-63.1
43	195	-5312	181	-866	0	344	108	6.28	6.28	9.42	9.42	-4.24	-59.7
44	195	-4952	-18	-712	0	394	156	6.28	6.28	9.42	9.42	-4.29	-59.8
45	195	-4914	97	-483	0	456	130	6.28	6.28	9.42	9.42	-4.55	-63.0
46	195	-5002	86	-698	0	382	131	6.28	6.28	9.42	9.42	-4.26	-59.5
47	195	-4934	87	-663	0	383	130	6.28	6.28	9.42	9.42	-4.23	-59.0
49	195	-4974	107	-686	0	375	125	6.28	6.28	9.42	9.42	-4.21	-58.9
50	195	-4902	67	-655	0	386	135	6.28	6.28	9.42	9.42	-4.22	-59.0
51	195	-4896	90	-609	0	398	130	6.28	6.28	9.42	9.42	-4.28	-59.6

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	292	-4962	138	-907	0	1240	253	6.28	6.28	9.42	9.42	-9.55	-121.8
41	292	-4837	80	-837	0	1194	210	6.28	6.28	9.42	9.42	-9.20	-117.5
42	292	-4722	87	-677	0	1083	217	6.28	6.28	9.42	9.42	-8.34	-107.6
43	292	-4874	181	-866	0	1188	285	6.28	6.28	9.42	9.42	-9.15	-117.0
44	292	-4513	-18	-712	0	1087	138	6.28	6.28	9.42	9.42	-8.37	-107.3
45	292	-4475	97	-483	0	926	224	6.28	6.28	9.42	9.42	-7.14	-93.4
46	292	-4563	86	-698	0	1062	214	6.28	6.28	9.42	9.42	-8.17	-105.3
47	292	-4495	87	-663	0	1029	215	6.28	6.28	9.42	9.42	-7.92	-102.2
49	292	-4536	107	-686	0	1044	230	6.28	6.28	9.42	9.42	-8.04	-103.6
50	292	-4464	67	-655	0	1024	201	6.28	6.28	9.42	9.42	-7.88	-101.7
51	292	-4457	90	-609	0	992	218	6.28	6.28	9.42	9.42	-7.64	-98.9

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	390	-4523	138	-907	0	2124	388	6.28	6.28	9.42	9.42	-16.55	360.2
41	390	-4398	80	-837	0	2010	288	6.28	6.28	9.42	9.42	-15.67	333.6
42	390	-4283	87	-677	0	1743	302	6.28	6.28	9.42	9.42	-13.59	261.4
43	390	-4435	181	-866	0	2032	461	6.28	6.28	9.42	9.42	-15.84	338.0
44	390	-4074	-18	-712	0	1781	120	6.28	6.28	9.42	9.42	-13.89	284.9
45	390	-4036	97	-483	0	1397	318	6.28	6.28	9.42	9.42	-10.86	175.9
46	390	-4124	86	-698	0	1742	298	6.28	6.28	9.42	9.42	-13.58	270.4
47	390	-4056	87	-663	0	1675	301	6.28	6.28	9.42	9.42	-13.06	254.7
49	390	-4097	107	-686	0	1713	334	6.28	6.28	9.42	9.42	-13.35	263.4
50	390	-4025	67	-655	0	1663	266	6.28	6.28	9.42	9.42	-12.96	253.0
51	390	-4018	90	-609	0	1586	306	6.28	6.28	9.42	9.42	-12.36	230.9

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 57 NI 142 NF 123 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 18B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	--												
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-10760	44	-1046	0	-1077	-165	6.28	6.28	12.57	12.57	-8.01	-110.6
41	0	-10780	-88	-1062	0	-1106	127	6.28	6.28	12.57	12.57	-8.12	-112.0
42	0	-10830	-79	-1122	0	-1223	109	6.28	6.28	12.57	12.57	-8.57	-117.5
43	0	-10470	138	-972	0	-967	-373	6.28	6.28	12.57	12.57	-7.51	-104.0
44	0	-10560	-310	-1051	0	-1121	616	6.28	6.28	12.57	12.57	-8.09	-111.4
45	0	-10590	-66	-1098	0	-1210	83	6.28	6.28	12.57	12.57	-8.43	-115.6
46	0	-10340	-77	-960	0	-960	104	6.28	6.28	12.57	12.57	-7.43	-102.9
47	0	-10230	-74	-934	0	-924	99	6.28	6.28	12.57	12.57	-7.26	-100.6
49	0	-10230	-30	-929	0	-914	2	6.28	6.28	12.57	12.57	-7.23	-100.2
50	0	-10240	-120	-945	0	-945	200	6.28	6.28	12.57	12.57	-7.34	-101.6
51	0	-10250	-71	-954	0	-963	93	6.28	6.28	12.57	12.57	-7.41	-102.5

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	97	-10174	44	-1046	0	-57	-122	6.28	6.28	12.57	12.57	-4.27	-61.8
41	97	-10194	-88	-1062	0	-70	41	6.28	6.28	12.57	12.57	-4.19	-62.2
42	97	-10244	-79	-1122	0	-129	32	6.28	6.28	12.57	12.57	-4.42	-65.1
43	97	-9886	138	-972	0	-20	-238	6.28	6.28	12.57	12.57	-4.74	-66.6
44	97	-9974	-310	-1051	0	-96	314	6.28	6.28	12.57	12.57	-5.14	-71.3
45	97	-10005	-66	-1098	0	-140	18	6.28	6.28	12.57	12.57	-4.36	-64.2
46	97	-9756	-77	-960	0	-24	29	6.28	6.28	12.57	12.57	-3.86	-57.6
47	97	-9646	-74	-934	0	-13	26	6.28	6.28	12.57	12.57	-3.77	-56.5
49	97	-9644	-30	-929	0	-9	-28	6.28	6.28	12.57	12.57	-3.76	-56.3
50	97	-9656	-120	-945	0	-24	82	6.28	6.28	12.57	12.57	-3.88	-57.0
51	97	-9665	-71	-954	0	-33	23	6.28	6.28	12.57	12.57	-3.85	-57.5

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	195	-9588	44	-1046	0	964	-80	6.28	6.28	12.57	12.57	-7.15	-98.7
41	195	-9608	-88	-1062	0	966	-46	6.28	6.28	12.57	12.57	-7.17	-98.9
42	195	-9658	-79	-1122	0	965	-46	6.28	6.28	12.57	12.57	-7.19	-99.2
43	195	-9302	138	-972	0	927	-103	6.28	6.28	12.57	12.57	-6.91	-95.4
44	195	-9388	-310	-1051	0	928	12	6.28	6.28	12.57	12.57	-6.95	-96.0
45	195	-9420	-66	-1098	0	931	-46	6.28	6.28	12.57	12.57	-6.97	-96.3
46	195	-9172	-77	-960	0	911	-46	6.28	6.28	12.57	12.57	-6.81	-93.9
47	195	-9062	-74	-934	0	898	-46	6.28	6.28	12.57	12.57	-6.71	-92.7
49	195	-9059	-30	-929	0	897	-58	6.28	6.28	12.57	12.57	-6.71	-92.6
50	195	-9072	-120	-945	0	897	-35	6.28	6.28	12.57	12.57	-6.72	-92.7
51	195	-9080	-71	-954	0	898	-46	6.28	6.28	12.57	12.57	-6.72	-92.8

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	292	-9003	44	-1046	0	1984	-38	6.28	6.28	12.57	12.57	-12.24	-157.6
41	292	-9022	-88	-1062	0	2001	-132	6.28	6.28	12.57	12.57	-12.35	-158.9
42	292	-9072	-79	-1122	0	2059	-123	6.28	6.28	12.57	12.57	-12.73	-163.2
43	292	-8718	138	-972	0	1875	32	6.28	6.28	12.57	12.57	-11.55	-149.2
44	292	-8801	-310	-1051	0	1953	-290	6.28	6.28	12.57	12.57	-12.05	-155.1
45	292	-8834	-66	-1098	0	2002	-111	6.28	6.28	12.57	12.57	-12.37	-158.7
46	292	-8587	-77	-960	0	1847	-121	6.28	6.28	12.57	12.57	-11.38	-147.0
47	292	-8478	-74	-934	0	1808	-119	6.28	6.28	12.57	12.57	-11.13	-144.1
49	292	-8474	-30	-929	0	1802	-87	6.28	6.28	12.57	12.57	-11.09	-143.6
50	292	-8488	-120	-945	0	1818	-152	6.28	6.28	12.57	12.57	-11.19	-144.8
51	292	-8496	-71	-954	0	1828	-116	6.28	6.28	12.57	12.57	-11.26	-145.5

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	390	-8417	44	-1046	0	3004	5	6.28	6.28	12.57	12.57	-19.42	375.7
41	390	-8436	-88	-1062	0	3037	-218	6.28	6.28	12.57	12.57	-19.64	383.9
42	390	-8486	-79	-1122	0	3153	-200	6.28	6.28	12.57	12.57	-20.44	413.7
43	390	-8134	138	-972	0	2822	166	6.28	6.28	12.57	12.57	-18.20	340.5
44	390	-8215	-310	-1051	0	2978	-592	6.28	6.28	12.57	12.57	-19.27	379.6
45	390	-8249	-66	-1098	0	3072	-176	6.28	6.28	12.57	12.57	-19.92	404.2
46	390	-8003	-77	-960	0	2783	-197	6.28	6.28	12.57	12.57	-17.95	336.8
47	390	-7894	-74	-934	0	2719	-191	6.28	6.28	12.57	12.57	-17.53	325.0
49	390	-7888	-30	-929	0	2708	-117	6.28	6.28	12.57	12.57	-17.45	322.3
50	390	-7904	-120	-945	0	2739	-269	6.28	6.28	12.57	12.57	-17.66	330.0
51	390	-7911	-71	-954	0	2758	-186	6.28	6.28	12.57	12.57	-17.79	334.9

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 58 NI 211 NF 212 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 13B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	--												
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-10200	111	-1121	0	-1353	-199	6.28	6.28	9.42	9.42	-11.38	-155.0
41	0	-10180	37	-1093	0	-1295	-47	6.28	6.28	9.42	9.42	-11.07	-151.1
42	0	-10270	38	-1196	0	-1498	-50	6.28	6.28	9.42	9.42	-12.21	-165.2
43	0	-9928	165	-1057	0	-1262	-307	6.28	6.28	9.42	9.42	-10.79	-147.3
44	0	-9895	-89	-1016	0	-1175	207	6.28	6.28	9.42	9.42	-10.35	-141.8
45	0	-10050	43	-1182	0	-1504	-59	6.28	6.28	9.42	9.42	-12.17	-164.3
46	0	-9722	42	-960	0	-1086	-58	6.28	6.28	9.42	9.42	-9.84	-135.3
47	0	-9609	44	-927	0	-1034	-61	6.28	6.28	9.42	9.42	-9.55	-131.4
49	0	-9616	68	-936	0	-1053	-112	6.28	6.28	9.42	9.42	-9.64	-132.6
50	0	-9609	18	-928	0	-1036	-9	6.28	6.28	9.42	9.42	-9.56	-131.5
51	0	-9641	44	-961	0	-1102	-62	6.28	6.28	9.42	9.42	-9.88	-135.6

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	97	-9760	111	-1121	0	-260	-90	6.28	6.28	9.42	9.42	-6.09	-88.4
41	97	-9740	37	-1093	0	-229	-11	6.28	6.28	9.42	9.42	-5.94	-86.5
42	97	-9832	38	-1196	0	-332	-13	6.28	6.28	9.42	9.42	-6.46	-93.1
43	97	-9489	165	-1057	0	-231	-147	6.28	6.28	9.42	9.42	-5.90	-84.8
44	97	-9456	-89	-1016	0	-184	121	6.28	6.28	9.42	9.42	-5.65	-81.8
45	97	-9612	43	-1182	0	-351	-17	6.28	6.28	9.42	9.42	-6.44	-92.5
46	97	-9283	42	-960	0	-150	-17	6.28	6.28	9.42	9.42	-5.35	-78.6
47	97	-9170	44	-927	0	-130	-18	6.28	6.28	9.42	9.42	-5.21	-76.6
49	97	-9177	68	-936	0	-140	-45	6.28	6.28	9.42	9.42	-5.25	-77.2
50	97	-9170	18	-928	0	-131	9	6.28	6.28	9.42	9.42	-5.21	-76.6
51	97	-9202	44	-961	0	-164	-19	6.28	6.28	9.42	9.42	-5.38	-78.8

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	195	-9321	111	-1121	0	834	18	6.28	6.28	9.42	9.42	-8.49	-117.8
41	195	-9300	37	-1093	0	836	24	6.28	6.28	9.42	9.42	-8.49	-117.8
42	195	-9394	38	-1196	0	835	24	6.28	6.28	9.42	9.42	-8.53	-118.5
43	195	-9050	165	-1057	0	800	14	6.28	6.28	9.42	9.42	-8.20	-113.8
44	195	-9018	-89	-1016	0	806	34	6.28	6.28	9.42	9.42	-8.21	-114.0
45	195	-9174	43	-1182	0	802	24	6.28	6.28	9.42	9.42	-8.27	-114.9
46	195	-8844	42	-960	0	786	24	6.28	6.28	9.42	9.42	-8.03	-111.5
47	195	-8732	44	-927	0	774	24	6.28	6.28	9.42	9.42	-7.92	-110.0
49	195	-8738	68	-936	0	772	22	6.28	6.28	9.42	9.42	-7.92	-110.0
50	195	-8732	18	-928	0	774	26	6.28	6.28	9.42	9.42	-7.92	-110.0
51	195	-8764	44	-961	0	773	24	6.28	6.28	9.42	9.42	-7.93	-110.2

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	292	-8882	111	-1121	0	1927	127	6.28	6.28	9.42	9.42	-14.84	-192.8
41	292	-8861	37	-1093	0	1902	60	6.28	6.28	9.42	9.42	-14.65	-190.7
42	292	-8955	38	-1196	0	2002	62	6.28	6.28	9.42	9.42	-15.41	-199.4
43	292	-8612	165	-1057	0	1830	175	6.28	6.28	9.42	9.42	-14.10	-183.7
44	292	-8579	-89	-1016	0	1797	-52	6.28	6.28	9.42	9.42	-13.85	-180.8
45	292	-8736	43	-1182	0	1954	66	6.28	6.28	9.42	9.42	-15.04	-194.7
46	292	-8406	42	-960	0	1722	65	6.28	6.28	9.42	9.42	-13.29	-173.9
47	292	-8293	44	-927	0	1677	67	6.28	6.28	9.42	9.42	-12.95	-169.7
49	292	-8300	68	-936	0	1685	89	6.28	6.28	9.42	9.42	-13.01	-170.4
50	292	-8293	18	-928	0	1679	44	6.28	6.28	9.42	9.42	-12.96	-169.9
51	292	-8325	44	-961	0	1710	67	6.28	6.28	9.42	9.42	-13.19	-172.6

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	390	-8442	111	-1121	0	3020	235	6.28	6.28	9.42	9.42	-23.50	395.4
41	390	-8421	37	-1093	0	2968	96	6.28	6.28	9.42	9.42	-23.09	381.9
42	390	-8517	38	-1196	0	3168	99	6.28	6.28	9.42	9.42	-24.67	433.4
43	390	-8173	165	-1057	0	2861	335	6.28	6.28	9.42	9.42	-22.26	365.1
44	390	-8140	-89	-1016	0	2788	-138	6.28	6.28	9.42	9.42	-21.68	346.5
45	390	-8298	43	-1182	0	3107	108	6.28	6.28	9.42	9.42	-24.20	428.1
46	390	-7967	42	-960	0	2658	106	6.28	6.28	9.42	9.42	-20.65	319.5
47	390	-7854	44	-927	0	2581	109	6.28	6.28	9.42	9.42	-20.05	304.2
49	390	-7861	68	-936	0	2598	156	6.28	6.28	9.42	9.42	-20.18	308.5
50	390	-7854	18	-928	0	2584	61	6.28	6.28	9.42	9.42	-20.07	305.0
51	390	-7886	44	-961	0	2648	110	6.28	6.28	9.42	9.42	-20.58	321.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 59 NI 213 NF 214 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 8B
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	--												
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-5833	-27	-596	0	-743	-96	6.28	6.28	9.42	9.42	-6.35	-86.7
41	0	-5855	-88	-534	0	-604	41	6.28	6.28	9.42	9.42	-5.70	-78.6
42	0	-5914	-86	-598	0	-746	37	6.28	6.28	9.42	9.42	-6.40	-87.4

43	0	-5684	16	-603	0	-782	-192	6.28	6.28	9.42	9.42	-6.50	-88.3
44	0	-5774	-190	-417	0	-364	272	6.28	6.28	9.42	9.42	-5.27	-66.5
45	0	-5818	-83	-607	0	-787	31	6.28	6.28	9.42	9.42	-6.57	-89.4
46	0	-5640	-84	-480	0	-518	34	6.28	6.28	9.42	9.42	-5.20	-72.1
47	0	-5586	-83	-467	0	-496	32	6.28	6.28	9.42	9.42	-5.07	-70.4
49	0	-5579	-63	-487	0	-543	-13	6.28	6.28	9.42	9.42	-5.28	-73.0
50	0	-5597	-104	-450	0	-459	79	6.28	6.28	9.42	9.42	-4.91	-68.4
51	0	-5606	-83	-488	0	-544	31	6.28	6.28	9.42	9.42	-5.30	-73.3

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	97	-5394	-27	-596	0	-162	-122	6.28	6.28	9.42	9.42	-3.71	-50.1
41	97	-5416	-88	-534	0	-83	-45	6.28	6.28	9.42	9.42	-3.10	-45.6
42	97	-5475	-86	-598	0	-163	-47	6.28	6.28	9.42	9.42	-3.50	-50.6
43	97	-5245	16	-603	0	-194	-176	6.28	6.28	9.42	9.42	-4.14	-54.0
44	97	-5335	-190	-417	0	42	86	6.28	6.28	9.42	9.42	-3.36	-46.4
45	97	-5379	-83	-607	0	-195	-50	6.28	6.28	9.42	9.42	-3.59	-51.7
46	97	-5201	-84	-480	0	-49	-48	6.28	6.28	9.42	9.42	-2.94	-42.1
47	97	-5147	-83	-467	0	-41	-49	6.28	6.28	9.42	9.42	-2.92	-41.6
49	97	-5140	-63	-487	0	-67	-75	6.28	6.28	9.42	9.42	-3.16	-43.9
50	97	-5158	-104	-450	0	-20	-22	6.28	6.28	9.42	9.42	-2.69	-40.1
51	97	-5167	-83	-488	0	-68	-50	6.28	6.28	9.42	9.42	-2.94	-42.8

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	195	-4956	-27	-596	0	418	-148	6.28	6.28	9.42	9.42	-4.40	-61.2
41	195	-4978	-88	-534	0	437	-130	6.28	6.28	9.42	9.42	-4.50	-62.5
42	195	-5036	-86	-598	0	421	-130	6.28	6.28	9.42	9.42	-4.45	-62.0
43	195	-4806	16	-603	0	394	-161	6.28	6.28	9.42	9.42	-4.21	-58.7
44	195	-4896	-190	-417	0	449	-99	6.28	6.28	9.42	9.42	-4.51	-62.5
45	195	-4940	-83	-607	0	398	-131	6.28	6.28	9.42	9.42	-4.30	-59.9
46	195	-4762	-84	-480	0	419	-130	6.28	6.28	9.42	9.42	-4.30	-59.8
47	195	-4708	-83	-467	0	414	-130	6.28	6.28	9.42	9.42	-4.26	-59.1
49	195	-4702	-63	-487	0	408	-136	6.28	6.28	9.42	9.42	-4.22	-58.7
50	195	-4720	-104	-450	0	419	-124	6.28	6.28	9.42	9.42	-4.28	-59.5
51	195	-4728	-83	-488	0	408	-131	6.28	6.28	9.42	9.42	-4.24	-58.9

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	292	-4517	-27	-596	0	999	-174	6.28	6.28	9.42	9.42	-7.69	-99.7
41	292	-4539	-88	-534	0	958	-215	6.28	6.28	9.42	9.42	-7.38	-96.2
42	292	-4598	-86	-598	0	1004	-214	6.28	6.28	9.42	9.42	-7.73	-100.4
43	292	-4368	16	-603	0	982	-145	6.28	6.28	9.42	9.42	-7.56	-97.8
44	292	-4458	-190	-417	0	856	-284	6.28	6.28	9.42	9.42	-6.63	-87.4
45	292	-4502	-83	-607	0	990	-212	6.28	6.28	9.42	9.42	-7.62	-98.9
46	292	-4324	-84	-480	0	887	-213	6.28	6.28	9.42	9.42	-6.84	-89.5
47	292	-4270	-83	-467	0	869	-212	6.28	6.28	9.42	9.42	-6.71	-87.8
49	292	-4263	-63	-487	0	883	-198	6.28	6.28	9.42	9.42	-6.81	-89.0
50	292	-4281	-104	-450	0	857	-226	6.28	6.28	9.42	9.42	-6.62	-86.9
51	292	-4290	-83	-488	0	884	-211	6.28	6.28	9.42	9.42	-6.82	-89.2

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	390	-4078	-27	-596	0	1580	-200	6.28	6.28	9.42	9.42	-12.31	225.7
41	390	-4100	-88	-534	0	1478	-301	6.28	6.28	9.42	9.42	-11.50	195.2
42	390	-4159	-86	-598	0	1587	-298	6.28	6.28	9.42	9.42	-12.36	223.1
43	390	-3929	16	-603	0	1570	-130	6.28	6.28	9.42	9.42	-12.24	231.3
44	390	-4019	-190	-417	0	1262	-469	6.28	6.28	9.42	9.42	-9.79	139.8
45	390	-4063	-83	-607	0	1582	-292	6.28	6.28	9.42	9.42	-12.33	227.1
46	390	-3885	-84	-480	0	1355	-295	6.28	6.28	9.42	9.42	-10.54	172.2
47	390	-3831	-83	-467	0	1324	-293	6.28	6.28	9.42	9.42	-10.30	166.4
49	390	-3824	-63	-487	0	1358	-260	6.28	6.28	9.42	9.42	-10.57	176.3
50	390	-3842	-104	-450	0	1296	-328	6.28	6.28	9.42	9.42	-10.07	158.0
51	390	-3851	-83	-488	0	1360	-292	6.28	6.28	9.42	9.42	-10.58	175.4

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 60 NI 292 NF 302 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 1C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-13060	104	-433	0	1032	254	6.28	6.28	9.42	9.42	-11.27	-157.3
41	0	-13290	-40	-342	0	905	-180	6.28	6.28	9.42	9.42	-10.81	-151.8
42	0	-13050	-38	-102	0	715	-176	6.28	6.28	9.42	9.42	-9.82	-139.2
43	0	-12030	183	-449	0	1023	508	6.28	6.28	9.42	9.42	-10.72	-149.1
44	0	-13800	-276	-199	0	710	-894	6.28	6.28	9.42	9.42	-15.00	-182.7
45	0	-12010	-55	104	0	495	-208	6.28	6.28	9.42	9.42	-8.30	-118.8
46	0	-11870	-68	-270	0	755	-236	6.28	6.28	9.42	9.42	-9.41	-132.6
47	0	-11520	-75	-253	0	718	-250	6.28	6.28	9.42	9.42	-9.07	-127.8
49	0	-11450	-27	-283	0	760	-105	6.28	6.28	9.42	9.42	-9.22	-129.7
50	0	-11800	-118	-233	0	698	-386	6.28	6.28	9.42	9.42	-9.21	-128.8
51	0	-11440	-74	-172	0	654	-248	6.28	6.28	9.42	9.42	-8.74	-123.6

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	12	-13005	85	-433	0	1086	266	6.28	6.28	9.42	9.42	-11.49	-160.0
41	12	-13232	-40	-342	0	948	-185	6.28	6.28	9.42	9.42	-10.98	-153.8
42	12	-12992	-38	-91	0	727	-181	6.28	6.28	9.42	9.42	-9.85	-139.4
43	12	-11972	151	-449	0	1079	529	6.28	6.28	9.42	9.42	-10.94	-151.8
44	12	-13742	-244	-199	0	734	-927	6.28	6.28	9.42	9.42	-15.35	-185.7
45	12	-11952	-55	122	0	480	-215	6.28	6.28	9.42	9.42	-8.20	-117.6
46	12	-11815	-68	-270	0	789	-244	6.28	6.28	9.42	9.42	-9.54	-134.1
47	12	-11465	-75	-253	0	749	-259	6.28	6.28	9.42	9.42	-9.18	-129.2
49	12	-11392	-33	-283	0	795	-109	6.28	6.28	9.42	9.42	-9.36	-131.3
50	12	-11742	-112	-233	0	727	-400	6.28	6.28	9.42	9.42	-9.31	-130.0
51	12	-11385	-74	-169	0	676	-257	6.28	6.28	9.42	9.42	-8.81	-124.4

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	25	-12950	66	-433	0	1140	275	6.28	6.28	9.42	9.42	-11.71	-162.7
41	25	-13175	-40	-342	0	990	-190	6.28	6.28	9.42	9.42	-11.14	-155.8
42	25	-12935	-38	-81	0	737	-186	6.28	6.28	9.42	9.42	-9.87	-139.6
43	25	-11915	119	-449	0	1135	546	6.28	6.28	9.42	9.42	-11.17	-154.6

44	25	-13685	-212	-199	0	759	-956	6.28	6.28	9.42	9.42	-15.66	-188.5
45	25	-11895	-55	138	0	464	-222	6.28	6.28	9.42	9.42	-8.10	-116.2
46	25	-11760	-68	-270	0	823	-253	6.28	6.28	9.42	9.42	-9.67	-135.6
47	25	-11410	-75	-253	0	781	-268	6.28	6.28	9.42	9.42	-9.30	-130.6
49	25	-11335	-39	-283	0	831	-113	6.28	6.28	9.42	9.42	-9.49	-132.9
50	25	-11685	-106	-233	0	756	-414	6.28	6.28	9.42	9.42	-9.41	-131.2
51	25	-11330	-74	-165	0	697	-267	6.28	6.28	9.42	9.42	-8.88	-125.2

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	38	-12895	47	-433	0	1194	282	6.28	6.28	9.42	9.42	-11.93	-165.3
41	38	-13118	-40	-342	0	1033	-195	6.28	6.28	9.42	9.42	-11.31	-157.9
42	38	-12878	-38	-73	0	747	-190	6.28	6.28	9.42	9.42	-9.88	-139.7
43	38	-11858	88	-449	0	1191	559	6.28	6.28	9.42	9.42	-11.39	-157.3
44	38	-13628	-180	-199	0	784	-980	6.28	6.28	9.42	9.42	-15.94	-190.8
45	38	-11838	-55	151	0	446	-228	6.28	6.28	9.42	9.42	-7.99	-114.7
46	38	-11705	-68	-270	0	857	-261	6.28	6.28	9.42	9.42	-9.79	-137.1
47	38	-11355	-75	-253	0	813	-278	6.28	6.28	9.42	9.42	-9.42	-132.0
49	38	-11278	-46	-283	0	866	-119	6.28	6.28	9.42	9.42	-9.62	-134.5
50	38	-11628	-99	-233	0	785	-426	6.28	6.28	9.42	9.42	-9.50	-132.5
51	38	-11275	-74	-163	0	717	-276	6.28	6.28	9.42	9.42	-8.94	-125.9

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	50	-12840	28	-433	0	1248	287	6.28	6.28	9.42	9.42	-12.15	-168.0
41	50	-13060	-40	-342	0	1076	-200	6.28	6.28	9.42	9.42	-11.47	-159.9
42	50	-12820	-38	-67	0	756	-195	6.28	6.28	9.42	9.42	-9.89	-139.8
43	50	-11800	56	-449	0	1247	568	6.28	6.28	9.42	9.42	-11.62	-160.1
44	50	-13570	-149	-199	0	809	-1001	6.28	6.28	9.42	9.42	-16.17	-192.8
45	50	-11780	-55	162	0	426	-235	6.28	6.28	9.42	9.42	-7.87	-113.2
46	50	-11650	-68	-270	0	890	-270	6.28	6.28	9.42	9.42	-9.92	-138.6
47	50	-11300	-75	-253	0	844	-287	6.28	6.28	9.42	9.42	-9.53	-133.4
49	50	-11220	-52	-283	0	902	-125	6.28	6.28	9.42	9.42	-9.75	-136.0
50	50	-11570	-93	-233	0	814	-438	6.28	6.28	9.42	9.42	-9.58	-133.7
51	50	-11220	-74	-161	0	737	-285	6.28	6.28	9.42	9.42	-9.01	-126.7

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 61 NI 294 NF 325 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 10C
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	--												
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-12760	1376	-250	0	-2406	1314	6.28	6.28	12.57	12.57	-14.79	-194.5
41	0	-11260	-412	-143	0	-1928	2053	6.28	6.28	12.57	12.57	-16.80	-193.3
42	0	-11240	-434	-503	0	-1414	2054	6.28	6.28	12.57	12.57	-16.80	-193.3
43	0	-13420	2649	-287	0	-2275	692	6.28	6.28	12.57	12.57	-14.09	-187.7
44	0	-9105	-3414	28	0	-1220	3297	6.28	6.28	12.57	12.57	-26.62	515.3
45	0	-10880	-367	-709	0	-621	1927	6.28	6.28	12.57	12.57	-15.77	-182.6
46	0	-10730	-282	-87	0	-1210	1847	6.28	6.28	12.57	12.57	-15.13	-176.1
47	0	-10590	-249	-73	0	-1030	1796	6.28	6.28	12.57	12.57	-14.71	-171.8
49	0	-11090	347	-109	0	-1189	1549	6.28	6.28	12.57	12.57	-12.80	-155.0
50	0	-10230	-866	-46	0	-978	2070	6.28	6.28	12.57	12.57	-16.91	-190.6
51	0	-10580	-256	-193	0	-858	1796	6.28	6.28	12.57	12.57	-14.71	-171.8

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	12	-12685	1376	-250	0	-2375	1486	6.28	6.28	12.57	12.57	-14.60	-192.2
41	12	-11185	-412	-143	0	-1910	2002	6.28	6.28	12.57	12.57	-16.38	-189.2
42	12	-11165	-434	-481	0	-1353	2000	6.28	6.28	12.57	12.57	-16.37	-189.0
43	12	-13345	2649	-287	0	-2239	1024	6.28	6.28	12.57	12.57	-13.89	-185.1
44	12	-9030	-3414	28	0	-1224	2870	6.28	6.28	12.57	12.57	-23.26	412.4
45	12	-10805	-367	-672	0	-535	1881	6.28	6.28	12.57	12.57	-15.40	-178.9
46	12	-10655	-282	-87	0	-1199	1812	6.28	6.28	12.57	12.57	-14.84	-173.2
47	12	-10515	-249	-73	0	-1021	1765	6.28	6.28	12.57	12.57	-14.46	-169.2
49	12	-11015	347	-109	0	-1176	1592	6.28	6.28	12.57	12.57	-13.13	-158.0
50	12	-10155	-866	-46	0	-972	1962	6.28	6.28	12.57	12.57	-16.04	-182.4
51	12	-10505	-256	-186	0	-835	1764	6.28	6.28	12.57	12.57	-14.45	-169.1

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	25	-12610	1376	-250	0	-2344	1658	6.28	6.28	12.57	12.57	-14.41	-189.9
41	25	-11110	-412	-143	0	-1892	1950	6.28	6.28	12.57	12.57	-15.96	-185.1
42	25	-11090	-434	-462	0	-1294	1946	6.28	6.28	12.57	12.57	-15.93	-184.8
43	25	-13270	2649	-287	0	-2203	1355	6.28	6.28	12.57	12.57	-13.68	-182.6
44	25	-8955	-3414	28	0	-1227	2444	6.28	6.28	12.57	12.57	-19.87	311.1
45	25	-10730	-367	-640	0	-453	1836	6.28	6.28	12.57	12.57	-15.03	-175.2
46	25	-10580	-282	-87	0	-1188	1776	6.28	6.28	12.57	12.57	-14.56	-170.3
47	25	-10440	-249	-73	0	-1012	1734	6.28	6.28	12.57	12.57	-14.21	-166.6
49	25	-10940	347	-109	0	-1162	1636	6.28	6.28	12.57	12.57	-13.46	-161.0
50	25	-10080	-866	-46	0	-967	1854	6.28	6.28	12.57	12.57	-15.17	-174.2
51	25	-10430	-256	-179	0	-812	1732	6.28	6.28	12.57	12.57	-14.20	-166.5

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	38	-12535	1376	-250	0	-2312	1830	6.28	6.28	12.57	12.57	-15.08	-187.6
41	38	-11035	-412	-143	0	-1875	1898	6.28	6.28	12.57	12.57	-15.55	-181.0
42	38	-11015	-434	-446	0	-1237	1892	6.28	6.28	12.57	12.57	-15.50	-180.5
43	38	-13195	2649	-287	0	-2167	1686	6.28	6.28	12.57	12.57	-14.04	-180.1
44	38	-8880	-3414	28	0	-1230	2017	6.28	6.28	12.57	12.57	-16.45	212.8
45	38	-10655	-367	-614	0	-375	1790	6.28	6.28	12.57	12.57	-14.67	-171.6
46	38	-10505	-282	-87	0	-1177	1741	6.28	6.28	12.57	12.57	-14.27	-167.4
47	38	-10365	-249	-73	0	-1003	1702	6.28	6.28	12.57	12.57	-13.96	-164.0
49	38	-10865	347	-109	0	-1148	1680	6.28	6.28	12.57	12.57	-13.80	-164.0
50	38	-10004	-866	-46	0	-961	1746	6.28	6.28	12.57	12.57	-14.30	-166.0
51	38	-10355	-256	-174	0	-790	1700	6.28	6.28	12.57	12.57	-13.94	-163.8

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	50	-12460	1376	-250	0	-2281	2002	6.28	6.28	12.57	12.57	-16.43	-193.8
41	50	-10960	-412	-143	0	-1857	1847	6.28	6.28	12.57	12.57	-15.13	-176.9
42	50	-10940	-434	-434	0	-1182	1838	6.28	6.28	12.57	12.57	-15.06	-176.2
43	50	-13120	2649	-287	0	-2131	2017	6.28	6.28	12.57	12.57	-16.58	-197.3
44	50	-8805	-3414	28	0	-1234	1590	6.28	6.28	12.57	12.57	-13.01	-150.0

45	50	-10580	-367	-593	0	-300	1744	6.28	6.28	12.57	12.57	-14.30	-167.9
46	50	-10430	-282	-87	0	-1166	1706	6.28	6.28	12.57	12.57	-13.99	-164.5
47	50	-10290	-249	-73	0	-994	1671	6.28	6.28	12.57	12.57	-13.71	-161.4
49	50	-10790	347	-109	0	-1135	1723	6.28	6.28	12.57	12.57	-14.14	-167.1
50	50	-9929	-866	-46	0	-955	1638	6.28	6.28	12.57	12.57	-13.43	-157.6
51	50	-10280	-256	-170	0	-768	1668	6.28	6.28	12.57	12.57	-13.68	-161.1

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 62 NI 1543 NF 1542 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 6
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-4508	645	-526	0	-310	4700	15.71	15.71	9.42	9.42	-15.77	506.9
41	0	-395	202	-714	0	-439	6671	15.71	15.71	9.42	9.42	-21.22	1002.1
42	0	-700	215	-950	0	-452	6472	15.71	15.71	9.42	9.42	-20.67	956.7
43	0	-8509	885	-247	0	-124	2007	15.71	15.71	9.42	9.42	-6.72	-92.2
44	0	6616	-526	-1055	0	-671	10190	15.71	15.71	9.42	9.42	-29.70	1892.5
45	0	-2162	170	-954	0	-360	4960	15.71	15.71	9.42	9.42	-16.24	654.9
46	0	-2409	116	-470	0	-279	4464	15.71	15.71	9.42	9.42	-14.71	567.5
47	0	-2912	94	-408	0	-239	3912	15.71	15.71	9.42	9.42	-13.02	460.1
49	0	-4283	242	-346	0	-196	3255	15.71	15.71	9.42	9.42	-11.00	300.4
50	0	-1259	-41	-507	0	-305	4891	15.71	15.71	9.42	9.42	-15.81	687.6
51	0	-3014	98	-487	0	-243	3846	15.71	15.71	9.42	9.42	-12.82	445.4

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	12	-4408	645	-526	0	-245	4780	15.71	15.71	9.42	9.42	-16.02	523.6
41	12	-295	202	-714	0	-350	6696	15.71	15.71	9.42	9.42	-21.27	1010.9
42	12	-600	215	-950	0	-333	6499	15.71	15.71	9.42	9.42	-20.73	965.8
43	12	-8409	885	-247	0	-93	2118	15.71	15.71	9.42	9.42	-7.04	-96.1
44	12	6716	-526	-1055	0	-539	10123	15.71	15.71	9.42	9.42	-29.44	1887.4
45	12	-2062	170	-954	0	-241	4981	15.71	15.71	9.42	9.42	-16.29	662.9
46	12	-2309	116	-470	0	-220	4478	15.71	15.71	9.42	9.42	-14.73	574.4
47	12	-2812	94	-408	0	-188	3924	15.71	15.71	9.42	9.42	-13.04	466.5
49	12	-4183	242	-346	0	-153	3285	15.71	15.71	9.42	9.42	-11.10	309.2
50	12	-1159	-41	-507	0	-242	4886	15.71	15.71	9.42	9.42	-15.77	691.7
51	12	-2914	98	-487	0	-182	3858	15.71	15.71	9.42	9.42	-12.85	451.8

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	25	-4308	645	-526	0	-179	4861	15.71	15.71	9.42	9.42	-16.27	540.2
41	25	-195	202	-714	0	-261	6722	15.71	15.71	9.42	9.42	-21.32	1019.7
42	25	-500	215	-950	0	-215	6526	15.71	15.71	9.42	9.42	-20.79	974.8
43	25	-8309	885	-247	0	-62	2228	15.71	15.71	9.42	9.42	-7.38	-100.2
44	25	6816	-526	-1055	0	-408	10056	15.71	15.71	9.42	9.42	-29.18	1882.4
45	25	-1962	170	-954	0	-122	5002	15.71	15.71	9.42	9.42	-16.33	670.9
46	25	-2209	116	-470	0	-162	4493	15.71	15.71	9.42	9.42	-14.76	581.4
47	25	-2712	94	-408	0	-137	3936	15.71	15.71	9.42	9.42	-13.07	472.9
49	25	-4083	242	-346	0	-109	3316	15.71	15.71	9.42	9.42	-11.19	318.0
50	25	-1059	-41	-507	0	-178	4881	15.71	15.71	9.42	9.42	-15.73	695.7
51	25	-2814	98	-487	0	-121	3870	15.71	15.71	9.42	9.42	-12.87	458.3

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	38	-4208	645	-526	0	-113	4942	15.71	15.71	9.42	9.42	-16.52	557.0
41	38	-95	202	-714	0	-172	6747	15.71	15.71	9.42	9.42	-21.37	1028.5
42	38	-400	215	-950	0	-96	6553	15.71	15.71	9.42	9.42	-20.84	983.8
43	38	-8209	885	-247	0	-32	2339	15.71	15.71	9.42	9.42	-7.73	-104.4
44	38	6916	-526	-1055	0	-276	9990	15.71	15.71	9.42	9.42	-28.92	1877.3
45	38	-1862	170	-954	0	-2	5024	15.71	15.71	9.42	9.42	-16.38	678.9
46	38	-2109	116	-470	0	-103	4508	15.71	15.71	9.42	9.42	-14.79	588.3
47	38	-2612	94	-408	0	-86	3947	15.71	15.71	9.42	9.42	-13.09	479.3
49	38	-3983	242	-346	0	-66	3346	15.71	15.71	9.42	9.42	-11.29	326.8
50	38	-959	-41	-507	0	-115	4876	15.71	15.71	9.42	9.42	-15.69	699.8
51	38	-2714	98	-487	0	-60	3883	15.71	15.71	9.42	9.42	-12.90	464.8

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	50	-4108	645	-526	0	-48	5022	15.71	15.71	9.42	9.42	-16.76	573.7
41	50	5	202	-714	0	-82	6772	15.71	15.71	9.42	9.42	-21.42	1037.2
42	50	-300	215	-950	0	23	6580	15.71	15.71	9.42	9.42	-20.90	992.9
43	50	-8109	885	-247	0	-1	2450	15.71	15.71	9.42	9.42	-8.10	-108.8
44	50	7016	-526	-1055	0	-144	9923	15.71	15.71	9.42	9.42	-28.65	1872.3
45	50	-1762	170	-954	0	117	5045	15.71	15.71	9.42	9.42	-16.42	687.0
46	50	-2009	116	-470	0	-44	4522	15.71	15.71	9.42	9.42	-14.81	595.3
47	50	-2512	94	-408	0	-35	3959	15.71	15.71	9.42	9.42	-13.11	485.7
49	50	-3883	242	-346	0	-23	3376	15.71	15.71	9.42	9.42	-11.38	335.6
50	50	-859	-41	-507	0	-52	4871	15.71	15.71	9.42	9.42	-15.65	703.9
51	50	-2614	98	-487	0	0	3895	15.71	15.71	9.42	9.42	-12.92	471.3

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 63 NI 1542 NF 78 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 6A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-9261	1917	-257	0	-48	6030	15.71	15.71	9.42	9.42	-20.41	501.5
41	0	-5313	1674	-152	0	-82	7688	15.71	15.71	9.42	9.42	-25.53	923.1
42	0	-5631	1670	-848	0	23	7507	15.71	15.71	9.42	9.42	-24.99	880.9
43	0	-12490	1725	-336	0	-1	3408	15.71	15.71	9.42	9.42	-11.27	-152.9
44	0	1291	1329	22	0	-144	10710	15.71	15.71	9.42	9.42	-33.46	1703.8
45	0	-6441	1313	-1322	0	117	5870	15.71	15.71	9.42	9.42	-19.77	597.2
46	0	-6269	1109	-167	0	-44	5261	15.71	15.71	9.42	9.42	-17.75	513.6
47	0	-6509	967	-171	0	-35	4654	15.71	15.71	9.42	9.42	-15.74	413.4
49	0	-7825	1048	-206	0	-23	4101	15.71	15.71	9.42	9.42	-13.86	281.6

50	0	-5068	969	-134	0	-52	5561	15.71	15.71	9.42	9.42	-18.63	611.7
51	0	-6615	966	-403	0	0	4594	15.71	15.71	9.42	9.42	-15.55	400.1

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	12	-9161	1917	-257	0	-15	6270	15.71	15.71	9.42	9.42	-21.22	540.6
41	12	-5213	1674	-152	0	-63	7897	15.71	15.71	9.42	9.42	-26.18	959.6
42	12	-5531	1670	-848	0	129	7716	15.71	15.71	9.42	9.42	-25.65	917.2
43	12	-12390	1725	-336	0	41	3624	15.71	15.71	9.42	9.42	-11.97	-161.3
44	12	1391	1329	22	0	-146	10875	15.71	15.71	9.42	9.42	-33.95	1734.0
45	12	-6341	1313	-1322	0	282	6034	15.71	15.71	9.42	9.42	-20.29	626.2
46	12	-6169	1109	-167	0	-23	5400	15.71	15.71	9.42	9.42	-18.20	538.6
47	12	-6409	967	-171	0	-13	4775	15.71	15.71	9.42	9.42	-16.14	435.4
49	12	-7725	1048	-206	0	3	4232	15.71	15.71	9.42	9.42	-14.31	303.8
50	12	-4968	969	-134	0	-35	5682	15.71	15.71	9.42	9.42	-19.01	634.6
51	12	-6515	966	-403	0	51	4714	15.71	15.71	9.42	9.42	-15.95	422.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	25	-9061	1917	-257	0	17	6510	15.71	15.71	9.42	9.42	-22.02	580.0
41	25	-5113	1674	-152	0	-44	8106	15.71	15.71	9.42	9.42	-26.84	996.1
42	25	-5431	1670	-848	0	235	7924	15.71	15.71	9.42	9.42	-26.30	953.6
43	25	-12290	1725	-336	0	83	3840	15.71	15.71	9.42	9.42	-12.70	-170.0
44	25	1491	1329	22	0	-149	11040	15.71	15.71	9.42	9.42	-34.44	1764.2
45	25	-6241	1313	-1322	0	447	6198	15.71	15.71	9.42	9.42	-20.82	655.3
46	25	-6069	1109	-167	0	-2	5538	15.71	15.71	9.42	9.42	-18.65	563.7
47	25	-6309	967	-171	0	8	4896	15.71	15.71	9.42	9.42	-16.54	457.5
49	25	-7625	1048	-206	0	28	4363	15.71	15.71	9.42	9.42	-14.76	326.2
50	25	-4868	969	-134	0	-18	5804	15.71	15.71	9.42	9.42	-19.39	657.5
51	25	-6415	966	-403	0	101	4835	15.71	15.71	9.42	9.42	-16.35	444.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	38	-8961	1917	-257	0	49	6749	15.71	15.71	9.42	9.42	-22.82	619.6
41	38	-5013	1674	-152	0	-25	8316	15.71	15.71	9.42	9.42	-27.49	1032.6
42	38	-5331	1670	-848	0	341	8133	15.71	15.71	9.42	9.42	-26.96	990.0
43	38	-12190	1725	-336	0	126	4055	15.71	15.71	9.42	9.42	-13.44	-178.8
44	38	1591	1329	22	0	-152	11205	15.71	15.71	9.42	9.42	-34.93	1794.5
45	38	-6141	1313	-1322	0	612	6362	15.71	15.71	9.42	9.42	-21.35	684.4
46	38	-5969	1109	-167	0	19	5676	15.71	15.71	9.42	9.42	-19.09	588.9
47	38	-6209	967	-171	0	30	5016	15.71	15.71	9.42	9.42	-16.94	479.7
49	38	-7525	1048	-206	0	54	4494	15.71	15.71	9.42	9.42	-15.21	348.8
50	38	-4768	969	-134	0	-1	5925	15.71	15.71	9.42	9.42	-19.77	680.4
51	38	-6315	966	-403	0	152	4956	15.71	15.71	9.42	9.42	-16.74	466.1

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	50	-8861	1917	-257	0	81	6989	15.71	15.71	9.42	9.42	-23.61	659.3
41	50	-4913	1674	-152	0	-6	8525	15.71	15.71	9.42	9.42	-28.14	1069.1
42	50	-5231	1670	-848	0	447	8342	15.71	15.71	9.42	9.42	-27.61	1026.4
43	50	-12090	1725	-336	0	168	4271	15.71	15.71	9.42	9.42	-14.20	-187.6
44	50	1691	1329	22	0	-155	11370	15.71	15.71	9.42	9.42	-35.42	1824.7
45	50	-6041	1313	-1322	0	778	6526	15.71	15.71	9.42	9.42	-21.87	713.7
46	50	-5869	1109	-167	0	39	5815	15.71	15.71	9.42	9.42	-19.54	614.2
47	50	-6109	967	-171	0	51	5137	15.71	15.71	9.42	9.42	-17.33	502.0
49	50	-7425	1048	-206	0	80	4625	15.71	15.71	9.42	9.42	-15.66	371.7
50	50	-4668	969	-134	0	16	6046	15.71	15.71	9.42	9.42	-20.15	703.4
51	50	-6215	966	-403	0	202	5076	15.71	15.71	9.42	9.42	-17.14	488.3

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 64 NI 1581 NF 121 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 5A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-5096	3168	250	0	-76	10760	15.71	15.71	9.42	9.42	-35.31	1401.5
41	0	292	3145	243	0	-88	13530	15.71	15.71	9.42	9.42	-42.70	2086.2
42	0	310	3158	-424	0	33	13540	15.71	15.71	9.42	9.42	-42.73	2088.7
43	0	-10480	2538	196	0	-47	6185	15.71	15.71	9.42	9.42	-20.94	475.2
44	0	9510	3218	236	0	-111	18610	15.71	15.71	9.42	9.42	-55.39	3325.3
45	0	-1475	2521	-928	0	133	10820	15.71	15.71	9.42	9.42	-34.65	1584.6
46	0	-2583	2112	148	0	-56	9152	15.71	15.71	9.42	9.42	-29.65	1275.7
47	0	-3302	1853	124	0	-48	8058	15.71	15.71	9.42	9.42	-26.34	1074.0
49	0	-5098	1861	126	0	-44	7137	15.71	15.71	9.42	9.42	-23.72	849.3
50	0	-1099	1997	134	0	-56	9621	15.71	15.71	9.42	9.42	-30.75	1419.4
51	0	-3296	1858	-98	0	-8	8064	15.71	15.71	9.42	9.42	-26.35	1075.2

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	12	-4996	3168	250	0	-107	11158	15.71	15.71	9.42	9.42	-36.56	1466.9
41	12	392	3145	243	0	-118	13922	15.71	15.71	9.42	9.42	-43.91	2151.3
42	12	410	3158	-424	0	86	13935	15.71	15.71	9.42	9.42	-43.95	2154.1
43	12	-10380	2538	196	0	-72	6502	15.71	15.71	9.42	9.42	-22.01	524.9
44	12	9610	3218	236	0	-140	19012	15.71	15.71	9.42	9.42	-56.64	3391.9
45	12	-1375	2521	-928	0	249	11135	15.71	15.71	9.42	9.42	-35.62	1637.7
46	12	-2483	2112	148	0	-74	9416	15.71	15.71	9.42	9.42	-30.46	1321.0
47	12	-3202	1853	124	0	-63	8290	15.71	15.71	9.42	9.42	-27.05	1114.2
49	12	-4998	1861	126	0	-59	7370	15.71	15.71	9.42	9.42	-24.45	889.2
50	12	-999	1997	134	0	-73	9871	15.71	15.71	9.42	9.42	-31.51	1462.5
51	12	-3196	1858	-98	0	5	8296	15.71	15.71	9.42	9.42	-27.07	1115.4

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	25	-4896	3168	250	0	-138	11555	15.71	15.71	9.42	9.42	-37.80	1532.4
41	25	492	3145	243	0	-148	14315	15.71	15.71	9.42	9.42	-45.12	2216.3
42	25	510	3158	-424	0	139	14330	15.71	15.71	9.42	9.42	-45.16	2219.5
43	25	-10280	2538	196	0	-96	6820	15.71	15.71	9.42	9.42	-23.09	575.0
44	25	9710	3218	236	0	-170	19415	15.71	15.71	9.42	9.42	-57.88	3458.4
45	25	-1275	2521	-928	0	365	11450	15.71	15.71	9.42	9.42	-36.58	1690.8
46	25	-2383	2112	148	0	-93	9681	15.71	15.71	9.42	9.42	-31.28	1366.3
47	25	-3102	1853	124	0	-79	8522	15.71	15.71	9.42	9.42	-27.77	1154.3
49	25	-4898	1861	126	0	-75	7602	15.71	15.71	9.42	9.42	-25.18	929.3
50	25	-899	1997	134	0	-90	10120	15.71	15.71	9.42	9.42	-32.27	1505.7

51	25	-3096	1858	-98	0	17	8528	15.71	15.71	9.42	9.42	-27.79	1155.7

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	38	-4796	3168	250	0	-169	11952	15.71	15.71	9.42	9.42	-39.04	1597.9
41	38	592	3145	243	0	-179	14708	15.71	15.71	9.42	9.42	-46.33	2281.3
42	38	610	3158	-424	0	192	14725	15.71	15.71	9.42	9.42	-46.38	2284.9
43	38	-10180	2538	196	0	-121	7137	15.71	15.71	9.42	9.42	-24.15	625.6
44	38	9810	3218	236	0	-199	19818	15.71	15.71	9.42	9.42	-59.12	3525.0
45	38	-1175	2521	-928	0	481	11765	15.71	15.71	9.42	9.42	-37.55	1744.0
46	38	-2283	2112	148	0	-111	9946	15.71	15.71	9.42	9.42	-32.09	1411.6
47	38	-3002	1853	124	0	-94	8753	15.71	15.71	9.42	9.42	-28.48	1194.6
49	38	-4798	1861	126	0	-91	7834	15.71	15.71	9.42	9.42	-25.91	969.3
50	38	-799	1997	134	0	-107	10370	15.71	15.71	9.42	9.42	-33.03	1548.8
51	38	-2996	1858	-98	0	29	8761	15.71	15.71	9.42	9.42	-28.50	1196.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	50	-4696	3168	250	0	-201	12350	15.71	15.71	9.42	9.42	-40.29	1663.4
41	50	692	3145	243	0	-209	15100	15.71	15.71	9.42	9.42	-47.54	2346.4
42	50	710	3158	-424	0	245	15120	15.71	15.71	9.42	9.42	-47.60	2350.3
43	50	-10080	2538	196	0	-146	7454	15.71	15.71	9.42	9.42	-25.21	676.5
44	50	9910	3218	236	0	-228	20220	15.71	15.71	9.42	9.42	-60.36	3591.5
45	50	-1075	2521	-928	0	597	12080	15.71	15.71	9.42	9.42	-38.52	1797.1
46	50	-2183	2112	148	0	-130	10210	15.71	15.71	9.42	9.42	-32.90	1456.9
47	50	-2902	1853	124	0	-110	8985	15.71	15.71	9.42	9.42	-29.19	1234.8
49	50	-4698	1861	126	0	-107	8067	15.71	15.71	9.42	9.42	-26.64	1009.4
50	50	-699	1997	134	0	-123	10620	15.71	15.71	9.42	9.42	-33.79	1591.9
51	50	-2896	1858	-98	0	42	8993	15.71	15.71	9.42	9.42	-29.22	1236.3

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 65 NI 1601 NF 164 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 4A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-3981	3407	356	0	-58	11890	15.71	15.71	9.42	9.42	-38.66	1627.3
41	0	1833	3407	347	0	-59	14940	15.71	15.71	9.42	9.42	-46.67	2378.3
42	0	1741	3375	-258	0	50	14830	15.71	15.71	9.42	9.42	-46.35	2356.9
43	0	-9977	2710	292	0	-46	6824	15.71	15.71	9.42	9.42	-23.10	588.1
44	0	11820	3529	338	0	-62	20550	15.71	15.71	12.57	12.57	-51.77	2814.2
45	0	-441	2657	-732	0	134	11740	15.71	15.71	9.42	9.42	-37.26	1776.1
46	0	-1560	2292	233	0	-40	10100	15.71	15.71	9.42	9.42	-32.39	1470.3
47	0	-2408	2014	204	0	-35	8887	15.71	15.71	9.42	9.42	-28.76	1243.6
49	0	-4346	2014	208	0	-35	7869	15.71	15.71	9.42	9.42	-25.94	995.7
50	0	13	2177	217	0	-38	10610	15.71	15.71	9.42	9.42	-33.55	1625.3
51	0	-2439	2003	3	0	1	8852	15.71	15.71	9.42	9.42	-28.66	1236.7

apost= 9.42 aant= 9.42 ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	12	-3881	3407	356	0	-103	12315	15.71	15.71	9.42	9.42	-39.99	1697.1
41	12	1933	3407	347	0	-103	15365	15.71	15.71	9.42	9.42	-47.98	2448.4
42	12	1841	3375	-258	0	82	15252	15.71	15.71	9.42	9.42	-47.65	2426.6
43	12	-9877	2710	292	0	-82	7163	15.71	15.71	9.42	9.42	-24.23	642.1
44	12	11920	3529	338	0	-104	20992	15.71	15.71	12.57	12.57	-52.95	2869.0
45	12	-341	2657	-732	0	226	12072	15.71	15.71	9.42	9.42	-38.28	1831.9
46	12	-1460	2292	233	0	-69	10385	15.71	15.71	9.42	9.42	-33.26	1518.8
47	12	-2308	2014	204	0	-60	9139	15.71	15.71	9.42	9.42	-29.54	1286.9
49	12	-4246	2014	208	0	-61	8121	15.71	15.71	9.42	9.42	-26.73	1038.8
50	12	113	2177	217	0	-65	10882	15.71	15.71	9.42	9.42	-34.38	1672.0
51	12	-2339	2003	3	0	1	9102	15.71	15.71	9.42	9.42	-29.43	1279.9

apost= 9.42 aant= 9.42 ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	25	-3781	3407	356	0	-147	12740	15.71	15.71	9.42	9.42	-41.31	1766.9
41	25	2033	3407	347	0	-146	15790	15.71	15.71	9.42	9.42	-49.29	2518.4
42	25	1941	3375	-258	0	114	15675	15.71	15.71	9.42	9.42	-48.96	2496.2
43	25	-9777	2710	292	0	-119	7502	15.71	15.71	9.42	9.42	-25.35	696.4
44	25	12020	3529	338	0	-147	21435	15.71	15.71	12.57	12.57	-54.13	2923.7
45	25	-241	2657	-732	0	317	12405	15.71	15.71	9.42	9.42	-39.31	1887.7
46	25	-1360	2292	233	0	-98	10670	15.71	15.71	9.42	9.42	-34.14	1567.3
47	25	-2208	2014	204	0	-86	9390	15.71	15.71	9.42	9.42	-30.31	1330.3
49	25	-4146	2014	208	0	-86	8372	15.71	15.71	9.42	9.42	-27.51	1082.0
50	25	213	2177	217	0	-92	11155	15.71	15.71	9.42	9.42	-35.22	1718.6
51	25	-2239	2003	3	0	1	9353	15.71	15.71	9.42	9.42	-30.20	1323.0

apost= 9.42 aant= 9.42 ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	38	-3681	3407	356	0	-192	13165	15.71	15.71	9.42	9.42	-42.64	1836.7
41	38	2133	3407	347	0	-189	16215	15.71	15.71	9.42	9.42	-50.60	2588.4
42	38	2041	3375	-258	0	146	16098	15.71	15.71	9.42	9.42	-50.26	2565.9
43	38	-9677	2710	292	0	-155	7840	15.71	15.71	9.42	9.42	-26.47	750.9
44	38	12120	3529	338	0	-189	21878	15.71	15.71	12.57	12.57	-55.31	2978.5
45	38	-141	2657	-732	0	409	12738	15.71	15.71	9.42	9.42	-40.33	1943.5
46	38	-1260	2292	233	0	-127	10955	15.71	15.71	9.42	9.42	-35.01	1615.8
47	38	-2108	2014	204	0	-112	9642	15.71	15.71	9.42	9.42	-31.08	1373.6
49	38	-4046	2014	208	0	-112	8624	15.71	15.71	9.42	9.42	-28.29	1125.1
50	38	313	2177	217	0	-119	11428	15.71	15.71	9.42	9.42	-36.05	1765.3
51	38	-2139	2003	3	0	0	9604	15.71	15.71	9.42	9.42	-30.97	1366.2

apost= 9.42 aant= 9.42 ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	50	-3581	3407	356	0	-237	13590	15.71	15.71	9.42	9.42	-43.96	1906.5
41	50	2233	3407	347	0	-233	16640	15.71	15.71	9.42	9.42	-51.91	2658.4
42	50	2141	3375	-258	0	178	16520	15.71	15.71	9.42	9.42	-51.57	2635.5
43	50	-9577	2710	292	0	-192	8179	15.71	15.71	9.42	9.42	-27.58	805.8
44	50	12220	3529	338	0	-231	22320	15.71	15.71	12.57	12.57	-56.49	3033.2
45	50	-41	2657	-732	0	500	13070	15.71	15.71	9.42	9.42	-41.35	1999.4
46	50	-1160	2292	233	0	-156	11240	15.71	15.71	9.42	9.42	-35.89	1664.3
47	50	-2008	2014	204	0	-137	9894	15.71	15.71	9.42	9.42	-31.86	1417.0
49	50	-3946	2014	208	0	-138	8876	15.71	15.71	9.42	9.42	-29.07	1168.3
50	50	413	2177	217	0	-146	11700	15.71	15.71	9.42	9.42	-36.88	1811.9
51	50	-2039	2003	3	0	-0	9854	15.71	15.71	9.42	9.42	-31.74	1409.4

apost= 9.42 aant= 9.42 ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 66 NI 1621 NF 207 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 3A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-5409	3084	450	0	-42	10430	15.71	15.71	9.42	9.42	-34.32	1336.3
41	0	380	3121	428	0	-34	13510	15.71	15.71	9.42	9.42	-42.61	2087.5
42	0	385	3122	-141	0	65	13520	15.71	15.71	9.42	9.42	-42.64	2089.3
43	0	-11100	2416	382	0	-41	5626	15.71	15.71	9.42	9.42	-19.00	372.9
44	0	10270	3293	403	0	-22	19130	15.71	15.71	9.42	9.42	-56.73	3443.3
45	0	-1441	2479	-603	0	137	10780	15.71	15.71	9.42	9.42	-34.51	1580.2
46	0	-2547	2091	297	0	-24	9120	15.71	15.71	9.42	9.42	-29.54	1272.5
47	0	-3279	1833	265	0	-22	8021	15.71	15.71	9.42	9.42	-26.21	1069.4
49	0	-5208	1821	272	0	-24	6993	15.71	15.71	9.42	9.42	-23.27	822.3
50	0	-935	1997	276	0	-20	9693	15.71	15.71	9.42	9.42	-30.93	1438.4
51	0	-3277	1834	75	0	11	8023	15.71	15.71	9.42	9.42	-26.22	1069.8

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	12	-5309	3084	450	0	-98	10815	15.71	15.71	9.42	9.42	-35.53	1399.8
41	12	480	3121	428	0	-88	13900	15.71	15.71	9.42	9.42	-43.81	2152.1
42	12	485	3122	-141	0	82	13910	15.71	15.71	9.42	9.42	-43.84	2153.9
43	12	-11000	2416	382	0	-89	5928	15.71	15.71	9.42	9.42	-20.04	418.7
44	12	10370	3293	403	0	-72	19542	15.71	15.71	9.42	9.42	-58.00	3511.4
45	12	-1341	2479	-603	0	212	11090	15.71	15.71	9.42	9.42	-35.46	1632.5
46	12	-2447	2091	297	0	-61	9382	15.71	15.71	9.42	9.42	-30.35	1317.5
47	12	-3179	1833	265	0	-55	8250	15.71	15.71	9.42	9.42	-26.92	1109.2
49	12	-5108	1821	272	0	-58	7220	15.71	15.71	9.42	9.42	-23.99	861.5
50	12	-835	1997	276	0	-55	9942	15.71	15.71	9.42	9.42	-31.69	1481.5
51	12	-3177	1834	75	0	2	8252	15.71	15.71	9.42	9.42	-26.93	1109.6

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	25	-5209	3084	450	0	-154	11200	15.71	15.71	9.42	9.42	-36.73	1463.3
41	25	580	3121	428	0	-141	14290	15.71	15.71	9.42	9.42	-45.02	2216.8
42	25	585	3122	-141	0	100	14300	15.71	15.71	9.42	9.42	-45.05	2218.6
43	25	-10900	2416	382	0	-136	6230	15.71	15.71	9.42	9.42	-21.08	465.3
44	25	10470	3293	403	0	-122	19955	15.71	15.71	9.42	9.42	-59.28	3579.5
45	25	-1241	2479	-603	0	288	11400	15.71	15.71	9.42	9.42	-36.42	1684.9
46	25	-2347	2091	297	0	-98	9645	15.71	15.71	9.42	9.42	-31.15	1362.5
47	25	-3079	1833	265	0	-88	8480	15.71	15.71	9.42	9.42	-27.63	1149.0
49	25	-5008	1821	272	0	-92	7448	15.71	15.71	9.42	9.42	-24.71	900.7
50	25	-735	1997	276	0	-89	10192	15.71	15.71	9.42	9.42	-32.45	1524.5
51	25	-3077	1834	75	0	-7	8482	15.71	15.71	9.42	9.42	-27.63	1149.4

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	38	-5109	3084	450	0	-211	11585	15.71	15.71	9.42	9.42	-37.94	1526.9
41	38	680	3121	428	0	-195	14680	15.71	15.71	9.42	9.42	-46.22	2281.4
42	38	685	3122	-141	0	118	14690	15.71	15.71	9.42	9.42	-46.25	2283.2
43	38	-10800	2416	382	0	-184	6532	15.71	15.71	9.42	9.42	-22.11	512.4
44	38	10570	3293	403	0	-173	20368	15.71	15.71	9.42	9.42	-60.55	3647.6
45	38	-1141	2479	-603	0	363	11710	15.71	15.71	9.42	9.42	-37.37	1737.2
46	38	-2247	2091	297	0	-136	9908	15.71	15.71	9.42	9.42	-31.96	1407.5
47	38	-2979	1833	265	0	-121	8709	15.71	15.71	9.42	9.42	-28.33	1188.9
49	38	-4908	1821	272	0	-126	7676	15.71	15.71	9.42	9.42	-25.42	940.0
50	38	-635	1997	276	0	-124	10441	15.71	15.71	9.42	9.42	-33.21	1567.6
51	38	-2977	1834	75	0	-17	8711	15.71	15.71	9.42	9.42	-28.34	1189.3

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	50	-5009	3084	450	0	-267	11970	15.71	15.71	9.42	9.42	-39.14	1590.4
41	50	780	3121	428	0	-248	15070	15.71	15.71	9.42	9.42	-47.42	2346.1
42	50	785	3122	-141	0	135	15080	15.71	15.71	9.42	9.42	-47.45	2347.9
43	50	-10700	2416	382	0	-232	6834	15.71	15.71	9.42	9.42	-23.14	560.1
44	50	10670	3293	403	0	-223	20780	15.71	15.71	12.57	12.57	-52.88	2797.3
45	50	-1041	2479	-603	0	438	12020	15.71	15.71	9.42	9.42	-38.32	1789.6
46	50	-2147	2091	297	0	-173	10170	15.71	15.71	9.42	9.42	-32.77	1452.5
47	50	-2879	1833	265	0	-154	8938	15.71	15.71	9.42	9.42	-29.04	1228.7
49	50	-4808	1821	272	0	-160	7903	15.71	15.71	9.42	9.42	-26.13	979.3
50	50	-535	1997	276	0	-158	10690	15.71	15.71	9.42	9.42	-33.97	1610.7
51	50	-2877	1834	75	0	-26	8940	15.71	15.71	9.42	9.42	-29.04	1229.1

apost= 9.42 aant= 9.42 ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 67 NI 1641 NF 250 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 2A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-10810	1692	542	0	37	5197	15.71	15.71	9.42	9.42	-17.52	324.5
41	0	-5366	1785	432	0	48	8082	15.71	15.71	9.42	9.42	-26.80	980.6
42	0	-5276	1829	-111	0	146	8206	15.71	15.71	9.42	9.42	-27.18	1003.6
43	0	-15110	1240	540	0	19	1636	15.71	15.71	9.42	9.42	-7.53	-106.9
44	0	3737	2004	262	0	68	13170	15.71	15.71	9.42	9.42	-40.39	2202.3
45	0	-5895	1468	-548	0	201	6652	15.71	15.71	9.42	9.42	-22.26	739.3
46	0	-6451	1161	312	0	31	5464	15.71	15.71	9.42	9.42	-18.43	536.0
47	0	-6722	1005	282	0	26	4809	15.71	15.71	9.42	9.42	-16.27	427.3
49	0	-8536	974	318	0	23	3847	15.71	15.71	9.42	9.42	-12.94	221.8
50	0	-4766	1127	263	0	32	6153	15.71	15.71	9.42	9.42	-20.50	715.1
51	0	-6693	1019	101	0	59	4850	15.71	15.71	9.42	9.42	-16.40	434.5

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	12	-10710	1692	542	0	-30	5408	15.71	15.71	9.42	9.42	-18.26	357.1

41	12	-5266	1785	432	0	-6	8305	15.71	15.71	9.42	9.42	-27.50	1019.2
42	12	-5176	1829	-111	0	160	8434	15.71	15.71	9.42	9.42	-27.90	1043.1
43	12	-15010	1240	540	0	-48	1791	15.71	15.71	9.42	9.42	-7.80	-110.4
44	12	3837	2004	262	0	35	13420	15.71	15.71	9.42	9.42	-41.15	2245.6
45	12	-5795	1468	-548	0	269	6835	15.71	15.71	9.42	9.42	-22.84	771.6
46	12	-6351	1161	312	0	-8	5609	15.71	15.71	9.42	9.42	-18.90	562.0
47	12	-6622	1005	282	0	-9	4934	15.71	15.71	9.42	9.42	-16.68	450.0
49	12	-8436	974	318	0	-17	3969	15.71	15.71	9.42	9.42	-13.37	241.5
50	12	-4666	1127	263	0	-0	6294	15.71	15.71	9.42	9.42	-20.94	741.1
51	12	-6593	1019	101	0	46	4978	15.71	15.71	9.42	9.42	-16.83	457.6

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	25	-10610	1692	542	0	-98	5620	15.71	15.71	9.42	9.42	-19.00	390.2
41	25	-5166	1785	432	0	-60	8528	15.71	15.71	9.42	9.42	-28.20	1057.8
42	25	-5076	1829	-111	0	174	8663	15.71	15.71	9.42	9.42	-28.61	1082.5
43	25	-14910	1240	540	0	-116	1946	15.71	15.71	9.42	9.42	-8.07	-114.0
44	25	3937	2004	262	0	3	13670	15.71	15.71	9.42	9.42	-41.91	2288.8
45	25	-5695	1468	-548	0	338	7018	15.71	15.71	9.42	9.42	-23.42	803.9
46	25	-6251	1161	312	0	-47	5754	15.71	15.71	9.42	9.42	-19.37	588.1
47	25	-6522	1005	282	0	-44	5060	15.71	15.71	9.42	9.42	-17.10	472.8
49	25	-8336	974	318	0	-57	4090	15.71	15.71	9.42	9.42	-13.80	261.6
50	25	-4566	1127	263	0	-33	6434	15.71	15.71	9.42	9.42	-21.38	767.1
51	25	-6493	1019	101	0	34	5105	15.71	15.71	9.42	9.42	-17.25	480.7

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	38	-10510	1692	542	0	-166	5832	15.71	15.71	9.42	9.42	-19.73	423.7
41	38	-5066	1785	432	0	-114	8752	15.71	15.71	9.42	9.42	-28.89	1096.5
42	38	-4976	1829	-111	0	188	8892	15.71	15.71	9.42	9.42	-29.32	1122.1
43	38	-14810	1240	540	0	-184	2101	15.71	15.71	9.42	9.42	-8.35	-117.5
44	38	4037	2004	262	0	-30	13920	15.71	15.71	9.42	9.42	-42.66	2332.1
45	38	-5595	1468	-548	0	406	7202	15.71	15.71	9.42	9.42	-24.00	836.2
46	38	-6151	1161	312	0	-86	5899	15.71	15.71	9.42	9.42	-19.84	614.3
47	38	-6422	1005	282	0	-79	5186	15.71	15.71	9.42	9.42	-17.51	495.7
49	38	-8236	974	318	0	-97	4212	15.71	15.71	9.42	9.42	-14.23	281.9
50	38	-4466	1127	263	0	-66	6575	15.71	15.71	9.42	9.42	-21.82	793.1
51	38	-6393	1019	101	0	21	5232	15.71	15.71	9.42	9.42	-17.66	504.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	50	-10410	1692	542	0	-234	6043	15.71	15.71	9.42	9.42	-20.45	457.6
41	50	-4966	1785	432	0	-168	8975	15.71	15.71	9.42	9.42	-29.59	1135.3
42	50	-4876	1829	-111	0	202	9120	15.71	15.71	9.42	9.42	-30.04	1161.6
43	50	-14710	1240	540	0	-251	2256	15.71	15.71	9.42	9.42	-8.62	-121.1
44	50	4137	2004	262	0	-63	14170	15.71	15.71	9.42	9.42	-43.42	2375.4
45	50	-5495	1468	-548	0	475	7385	15.71	15.71	9.42	9.42	-24.58	868.6
46	50	-6051	1161	312	0	-125	6044	15.71	15.71	9.42	9.42	-20.30	640.6
47	50	-6322	1005	282	0	-115	5311	15.71	15.71	9.42	9.42	-17.92	518.7
49	50	-8136	974	318	0	-137	4334	15.71	15.71	9.42	9.42	-14.65	302.6
50	50	-4366	1127	263	0	-99	6716	15.71	15.71	9.42	9.42	-22.25	819.1
51	50	-6293	1019	101	0	8	5360	15.71	15.71	9.42	9.42	-18.08	527.3

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 68 NI 1580 NF 1581 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 5
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	852	1155	-223	0	-187	9000	15.71	15.71	9.42	9.42	-28.20	1420.2
41	0	6700	678	-334	0	-255	12050	15.71	15.71	9.42	9.42	-35.63	2180.7
42	0	6731	698	-550	0	-242	12050	15.71	15.71	9.42	9.42	-35.62	2182.3
43	0	-5829	1343	-79	0	-87	4455	15.71	15.71	9.42	9.42	-15.06	412.6
44	0	16870	-93	-534	0	-378	17570	15.71	15.71	9.42	9.42	-48.45	3544.2
45	0	3968	582	-624	0	-179	9547	15.71	15.71	9.42	9.42	-28.79	1659.8
46	0	2247	470	-222	0	-167	8033	15.71	15.71	9.42	9.42	-24.65	1341.7
47	0	1134	418	-194	0	-145	7029	15.71	15.71	9.42	9.42	-21.87	1132.4
49	0	-815	577	-157	0	-122	6012	15.71	15.71	9.42	9.42	-19.25	880.7
50	0	3725	290	-248	0	-180	8634	15.71	15.71	9.42	9.42	-25.99	1508.0
51	0	1144	425	-266	0	-141	7030	15.71	15.71	9.42	9.42	-21.86	1133.1

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	12	952	1155	-223	0	-159	9144	15.71	15.71	9.42	9.42	-28.62	1447.3
41	12	6800	678	-334	0	-213	12135	15.71	15.71	9.42	9.42	-35.86	2198.7
42	12	6831	698	-550	0	-173	12138	15.71	15.71	9.42	9.42	-35.85	2200.7
43	12	-5729	1343	-79	0	-77	4623	15.71	15.71	9.42	9.42	-15.61	441.8
44	12	16970	-93	-534	0	-311	17558	15.71	15.71	9.42	9.42	-48.36	3547.5
45	12	4068	582	-624	0	-101	9620	15.71	15.71	9.42	9.42	-28.99	1676.0
46	12	2347	470	-222	0	-139	8092	15.71	15.71	9.42	9.42	-24.80	1355.7
47	12	1234	418	-194	0	-121	7081	15.71	15.71	9.42	9.42	-22.00	1145.4
49	12	-715	577	-157	0	-103	6084	15.71	15.71	9.42	9.42	-19.45	896.6
50	12	3825	290	-248	0	-149	8670	15.71	15.71	9.42	9.42	-26.06	1518.6
51	12	1244	425	-266	0	-107	7083	15.71	15.71	9.42	9.42	-22.00	1146.2

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	25	1052	1155	-223	0	-131	9288	15.71	15.71	9.42	9.42	-29.04	1474.3
41	25	6900	678	-334	0	-171	12220	15.71	15.71	9.42	9.42	-36.09	2216.8
42	25	6931	698	-550	0	-105	12225	15.71	15.71	9.42	9.42	-36.09	2219.2
43	25	-5629	1343	-79	0	-67	4790	15.71	15.71	9.42	9.42	-16.16	471.1
44	25	17070	-93	-534	0	-244	17545	15.71	15.71	9.42	9.42	-48.26	3550.8
45	25	4168	582	-624	0	-23	9692	15.71	15.71	9.42	9.42	-29.18	1692.1
46	25	2447	470	-222	0	-111	8150	15.71	15.71	9.42	9.42	-24.95	1369.7
47	25	1334	418	-194	0	-96	7134	15.71	15.71	9.42	9.42	-22.13	1158.4
49	25	-615	577	-157	0	-83	6156	15.71	15.71	9.42	9.42	-19.65	912.5
50	25	3925	290	-248	0	-118	8706	15.71	15.71	9.42	9.42	-26.13	1529.2
51	25	1344	425	-266	0	-74	7136	15.71	15.71	9.42	9.42	-22.13	1159.4

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	38	1152	1155	-223	0	-103	9433	15.71	15.71	9.42	9.42	-29.47	1501.4
41	38	7000	678	-334	0	-129	12305	15.71	15.71	9.42	9.42	-36.32	2234.9

42	38	7031	698	-550	0	-36	12312	15.71	15.71	9.42	9.42	-36.33	2237.6
43	38	-5529	1343	-79	0	-57	4958	15.71	15.71	9.42	9.42	-16.70	500.5
44	38	17170	-93	-534	0	-177	17532	15.71	15.71	9.42	9.42	-48.16	3554.0
45	38	4268	582	-624	0	55	9765	15.71	15.71	9.42	9.42	-29.37	1708.3
46	38	2547	470	-222	0	-83	8209	15.71	15.71	9.42	9.42	-25.10	1383.7
47	38	1434	418	-194	0	-72	7186	15.71	15.71	9.42	9.42	-22.26	1171.4
49	38	-515	577	-157	0	-63	6228	15.71	15.71	9.42	9.42	-19.85	928.4
50	38	4025	290	-248	0	-87	8743	15.71	15.71	9.42	9.42	-26.21	1539.8
51	38	1444	425	-266	0	-41	7190	15.71	15.71	9.42	9.42	-22.27	1172.5

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	50	1252	1155	-223	0	-76	9577	15.71	15.71	9.42	9.42	-29.89	1528.4
41	50	7100	678	-334	0	-88	12390	15.71	15.71	9.42	9.42	-36.54	2252.9
42	50	7131	698	-550	0	33	12400	15.71	15.71	9.42	9.42	-36.56	2256.0
43	50	-5429	1343	-79	0	-47	5126	15.71	15.71	9.42	9.42	-17.24	530.1
44	50	17270	-93	-534	0	-111	17520	15.71	15.71	9.42	9.42	-48.07	3557.3
45	50	4368	582	-624	0	133	9838	15.71	15.71	9.42	9.42	-29.56	1724.5
46	50	2647	470	-222	0	-56	8268	15.71	15.71	9.42	9.42	-25.25	1397.7
47	50	1534	418	-194	0	-48	7238	15.71	15.71	9.42	9.42	-22.39	1184.4
49	50	-415	577	-157	0	-44	6300	15.71	15.71	9.42	9.42	-20.05	944.3
50	50	4125	290	-248	0	-56	8779	15.71	15.71	9.42	9.42	-26.28	1550.4
51	50	1544	425	-266	0	-8	7243	15.71	15.71	9.42	9.42	-22.40	1185.6

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 69 NI 1600 NF 1601 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 4
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	2285	1178	134	0	9	10060	15.71	15.71	9.42	9.42	-31.06	1653.8
41	0	8629	638	107	0	-6	13430	15.71	15.71	9.42	9.42	-39.19	2489.6
42	0	8509	620	-90	0	5	13340	15.71	15.71	9.42	9.42	-38.96	2469.8
43	0	-5132	1422	130	0	19	5025	15.71	15.71	9.42	9.42	-16.89	528.1
44	0	19700	-239	66	0	-29	19510	15.71	15.71	12.57	12.57	-45.20	2996.3
45	0	5241	492	-243	0	13	10480	15.71	15.71	9.42	9.42	-31.24	1866.8
46	0	3530	454	73	0	-3	8950	15.71	15.71	9.42	9.42	-27.07	1546.4
47	0	2255	408	64	0	-3	7831	15.71	15.71	9.42	9.42	-24.01	1311.2
49	0	140	588	73	0	2	6710	15.71	15.71	9.42	9.42	-21.18	1034.4
50	0	5107	256	60	0	-8	9607	15.71	15.71	9.42	9.42	-28.51	1726.6
51	0	2215	402	-1	0	1	7801	15.71	15.71	9.42	9.42	-23.93	1304.6

apost= 9.42 aant= 9.42 ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	12	2385	1178	134	0	-8	10208	15.71	15.71	9.42	9.42	-31.49	1681.3
41	12	8729	638	107	0	-19	13510	15.71	15.71	9.42	9.42	-39.40	2506.9
42	12	8609	620	-90	0	16	13418	15.71	15.71	9.42	9.42	-39.16	2486.7
43	12	-5032	1422	130	0	3	5203	15.71	15.71	9.42	9.42	-17.46	559.3
44	12	19800	-239	66	0	-37	19480	15.71	15.71	12.57	12.57	-45.06	2996.7
45	12	5341	492	-243	0	43	10542	15.71	15.71	9.42	9.42	-31.40	1881.4
46	12	3630	454	73	0	-12	9007	15.71	15.71	9.42	9.42	-27.21	1560.1
47	12	2355	408	64	0	-11	7882	15.71	15.71	9.42	9.42	-24.13	1324.0
49	12	240	588	73	0	-7	6784	15.71	15.71	9.42	9.42	-21.38	1050.6
50	12	5207	256	60	0	-15	9639	15.71	15.71	9.42	9.42	-28.57	1736.6
51	12	2315	402	-1	0	1	7851	15.71	15.71	9.42	9.42	-24.05	1317.3

apost= 9.42 aant= 9.42 ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	25	2485	1178	134	0	-25	10355	15.71	15.71	9.42	9.42	-31.93	1708.9
41	25	8829	638	107	0	-32	13590	15.71	15.71	9.42	9.42	-39.61	2524.3
42	25	8709	620	-90	0	27	13495	15.71	15.71	9.42	9.42	-39.36	2503.6
43	25	-4932	1422	130	0	-13	5380	15.71	15.71	9.42	9.42	-18.03	590.6
44	25	19900	-239	66	0	-46	19450	15.71	15.71	12.57	12.57	-44.93	2997.1
45	25	5441	492	-243	0	74	10605	15.71	15.71	9.42	9.42	-31.56	1896.0
46	25	3730	454	73	0	-21	9064	15.71	15.71	9.42	9.42	-27.35	1573.9
47	25	2455	408	64	0	-19	7933	15.71	15.71	9.42	9.42	-24.26	1336.8
49	25	340	588	73	0	-16	6857	15.71	15.71	9.42	9.42	-21.58	1066.8
50	25	5307	256	60	0	-23	9671	15.71	15.71	9.42	9.42	-28.63	1746.6
51	25	2415	402	-1	0	1	7902	15.71	15.71	9.42	9.42	-24.17	1330.0

apost= 9.42 aant= 9.42 ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	38	2585	1178	134	0	-42	10502	15.71	15.71	9.42	9.42	-32.36	1736.5
41	38	8929	638	107	0	-46	13670	15.71	15.71	9.42	9.42	-39.82	2541.6
42	38	8809	620	-90	0	38	13572	15.71	15.71	9.42	9.42	-39.56	2520.6
43	38	-4832	1422	130	0	-29	5558	15.71	15.71	9.42	9.42	-18.59	622.0
44	38	20000	-239	66	0	-54	19420	15.71	15.71	12.57	12.57	-44.79	2997.6
45	38	5541	492	-243	0	104	10668	15.71	15.71	9.42	9.42	-31.71	1910.7
46	38	3830	454	73	0	-31	9120	15.71	15.71	9.42	9.42	-27.49	1587.6
47	38	2555	408	64	0	-27	7984	15.71	15.71	9.42	9.42	-24.38	1349.6
49	38	440	588	73	0	-25	6930	15.71	15.71	9.42	9.42	-21.78	1083.0
50	38	5407	256	60	0	-30	9703	15.71	15.71	9.42	9.42	-28.69	1756.6
51	38	2515	402	-1	0	1	7952	15.71	15.71	9.42	9.42	-24.29	1342.7

apost= 9.42 aant= 9.42 ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	50	2685	1178	134	0	-58	10650	15.71	15.71	9.42	9.42	-32.79	1764.1
41	50	9029	638	107	0	-59	13750	15.71	15.71	9.42	9.42	-40.03	2558.9
42	50	8909	620	-90	0	50	13650	15.71	15.71	9.42	9.42	-39.77	2537.5
43	50	-4732	1422	130	0	-46	5736	15.71	15.71	9.42	9.42	-19.15	653.4
44	50	20100	-239	66	0	-62	19390	15.71	15.71	12.57	12.57	-44.65	2998.0
45	50	5641	492	-243	0	134	10730	15.71	15.71	9.42	9.42	-31.87	1925.3
46	50	3930	454	73	0	-40	9177	15.71	15.71	9.42	9.42	-27.63	1601.3
47	50	2655	408	64	0	-35	8035	15.71	15.71	9.42	9.42	-24.50	1362.5
49	50	540	588	73	0	-35	7004	15.71	15.71	9.42	9.42	-21.98	1099.2
50	50	5507	256	60	0	-38	9735	15.71	15.71	9.42	9.42	-28.74	1766.5
51	50	2615	402	-1	0	1	8002	15.71	15.71	9.42	9.42	-24.41	1355.4

apost= 9.42 aant= 9.42 ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 70 NI 1620 NF 1621 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 3
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm²				daN/cm²	
40	0	453	1142	477	0	196	8687	15.71	15.71	9.42	9.42	-27.33	1352.6
41	0	6783	650	517	0	224	12050	15.71	15.71	9.42	9.42	-35.60	2184.9
42	0	6788	650	320	0	225	12060	15.71	15.71	9.42	9.42	-35.63	2186.7
43	0	-6584	1346	343	0	130	3916	15.71	15.71	9.42	9.42	-13.26	302.9
44	0	17760	-147	601	0	279	18100	15.71	15.71	12.57	12.57	-42.20	2759.8
45	0	3975	527	82	0	178	9538	15.71	15.71	9.42	9.42	-28.76	1658.8
46	0	2277	452	345	0	148	8012	15.71	15.71	9.42	9.42	-24.57	1340.0
47	0	1150	403	302	0	129	7002	15.71	15.71	9.42	9.42	-21.77	1129.1
49	0	-960	567	289	0	120	5879	15.71	15.71	9.42	9.42	-18.87	853.3
50	0	3909	268	340	0	150	8715	15.71	15.71	9.42	9.42	-26.17	1529.6
51	0	1152	403	236	0	130	7004	15.71	15.71	9.42	9.42	-21.78	1129.5

apost= 9.42 aant= 9.42 ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	12	553	1142	477	0	137	8830	15.71	15.71	9.42	9.42	-27.75	1379.4
41	12	6883	650	517	0	160	12132	15.71	15.71	9.42	9.42	-35.82	2202.6
42	12	6888	650	320	0	185	12142	15.71	15.71	9.42	9.42	-35.85	2204.4
43	12	-6484	1346	343	0	88	4084	15.71	15.71	9.42	9.42	-13.83	331.1
44	12	17860	-147	601	0	204	18080	15.71	15.71	12.57	12.57	-42.09	2761.4
45	12	4075	527	82	0	168	9604	15.71	15.71	9.42	9.42	-28.93	1673.9
46	12	2377	452	345	0	105	8068	15.71	15.71	9.42	9.42	-24.71	1353.6
47	12	1250	403	302	0	92	7052	15.71	15.71	9.42	9.42	-21.90	1141.8
49	12	-860	567	289	0	84	5950	15.71	15.71	9.42	9.42	-19.06	869.0
50	12	4009	268	340	0	107	8748	15.71	15.71	9.42	9.42	-26.23	1539.8
51	12	1252	403	236	0	100	7054	15.71	15.71	9.42	9.42	-21.90	1142.2

apost= 9.42 aant= 9.42 ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	25	653	1142	477	0	77	8972	15.71	15.71	9.42	9.42	-28.17	1406.2
41	25	6983	650	517	0	95	12215	15.71	15.71	9.42	9.42	-36.04	2220.3
42	25	6988	650	320	0	145	12225	15.71	15.71	9.42	9.42	-36.07	2222.1
43	25	-6384	1346	343	0	45	4252	15.71	15.71	9.42	9.42	-14.40	359.7
44	25	17960	-147	601	0	129	18060	15.71	15.71	12.57	12.57	-41.98	2762.9
45	25	4175	527	82	0	157	9670	15.71	15.71	9.42	9.42	-29.10	1689.1
46	25	2477	452	345	0	62	8125	15.71	15.71	9.42	9.42	-24.86	1367.3
47	25	1350	403	302	0	54	7102	15.71	15.71	9.42	9.42	-22.02	1154.5
49	25	-760	567	289	0	48	6020	15.71	15.71	9.42	9.42	-19.26	884.7
50	25	4109	268	340	0	65	8782	15.71	15.71	9.42	9.42	-26.30	1550.0
51	25	1352	403	236	0	71	7104	15.71	15.71	9.42	9.42	-22.03	1154.9

apost= 9.42 aant= 9.42 ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	38	753	1142	477	0	18	9115	15.71	15.71	9.42	9.42	-28.59	1433.0
41	38	7083	650	517	0	30	12298	15.71	15.71	9.42	9.42	-36.26	2238.0
42	38	7088	650	320	0	105	12308	15.71	15.71	9.42	9.42	-36.29	2239.7
43	38	-6284	1346	343	0	2	4421	15.71	15.71	9.42	9.42	-14.96	388.4
44	38	18060	-147	601	0	54	18040	15.71	15.71	12.57	12.57	-41.87	2764.5
45	38	4275	527	82	0	147	9736	15.71	15.71	9.42	9.42	-29.27	1704.2
46	38	2577	452	345	0	19	8182	15.71	15.71	9.42	9.42	-25.00	1380.9
47	38	1450	403	302	0	16	7153	15.71	15.71	9.42	9.42	-22.15	1167.1
49	38	-660	567	289	0	12	6091	15.71	15.71	9.42	9.42	-19.46	900.4
50	38	4209	268	340	0	22	8816	15.71	15.71	9.42	9.42	-26.36	1560.2
51	38	1452	403	236	0	41	7155	15.71	15.71	9.42	9.42	-22.15	1167.5

apost= 9.42 aant= 9.42 ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	50	853	1142	477	0	-42	9258	15.71	15.71	9.42	9.42	-29.01	1459.8
41	50	7183	650	517	0	-34	12380	15.71	15.71	9.42	9.42	-36.48	2255.6
42	50	7188	650	320	0	65	12390	15.71	15.71	9.42	9.42	-36.50	2257.4
43	50	-6184	1346	343	0	-41	4589	15.71	15.71	9.42	9.42	-15.52	417.4
44	50	18160	-147	601	0	-22	18020	15.71	15.71	12.57	12.57	-41.77	2766.1
45	50	4375	527	82	0	137	9802	15.71	15.71	9.42	9.42	-29.44	1719.3
46	50	2677	452	345	0	-24	8238	15.71	15.71	9.42	9.42	-25.14	1394.6
47	50	1550	403	302	0	-22	7203	15.71	15.71	9.42	9.42	-22.27	1179.8
49	50	-560	567	289	0	-24	6162	15.71	15.71	9.42	9.42	-19.65	916.1
50	50	4309	268	340	0	-20	8849	15.71	15.71	9.42	9.42	-26.43	1570.4
51	50	1552	403	236	0	11	7205	15.71	15.71	9.42	9.42	-22.28	1180.2

apost= 9.42 aant= 9.42 ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 71 NI 1640 NF 1641 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 2
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm²				daN/cm²	
40	0	-6137	466	597	0	336	3952	15.71	15.71	9.42	9.42	-13.38	325.9
41	0	-296	206	769	0	433	7031	15.71	15.71	9.42	9.42	-22.33	1062.1
42	0	-168	233	596	0	444	7134	15.71	15.71	9.42	9.42	-22.61	1084.2
43	0	-11400	570	305	0	171	414	15.71	15.71	9.42	9.42	-4.08	-59.7
44	0	9612	-219	1086	0	611	12410	15.71	15.71	9.42	9.42	-35.43	2384.5
45	0	-1455	183	304	0	352	5717	15.71	15.71	9.42	9.42	-18.48	804.5
46	0	-2493	95	486	0	273	4655	15.71	15.71	9.42	9.42	-15.33	592.7
47	0	-3042	68	414	0	233	4061	15.71	15.71	9.42	9.42	-13.52	476.7
49	0	-4989	154	357	0	201	3034	15.71	15.71	9.42	9.42	-10.27	239.1
50	0	-786	-3	513	0	289	5434	15.71	15.71	9.42	9.42	-17.41	793.6
51	0	-2999	77	357	0	237	4095	15.71	15.71	9.42	9.42	-13.62	483.9

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	12	-6037	466	597	0	261	4010	15.71	15.71	9.42	9.42	-13.58	338.5
41	12	-196	206	769	0	337	7057	15.71	15.71	9.42	9.42	-22.38	1070.9
42	12	-68	233	596	0	370	7163	15.71	15.71	9.42	9.42	-22.68	1093.6
43	12	-11300	570	305	0	133	485	15.71	15.71	9.42	9.42	-4.19	-61.1
44	12	9712	-219	1086	0	475	12382	15.71	15.71	9.42	9.42	-35.29	2385.4
45	12	-1355	183	304	0	315	5740	15.71	15.71	9.42	9.42	-18.53	812.8
46	12	-2393	95	486	0	213	4667	15.71	15.71	9.42	9.42	-15.35	599.2

47	12	-2942	68	414	0	182	4070	15.71	15.71	9.42	9.42	-13.53	482.6
49	12	-4889	154	357	0	156	3054	15.71	15.71	9.42	9.42	-10.34	245.9
50	12	-686	-3	513	0	225	5434	15.71	15.71	9.42	9.42	-17.38	798.4
51	12	-2899	77	357	0	193	4105	15.71	15.71	9.42	9.42	-13.64	490.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	25	-5937	466	597	0	187	4068	15.71	15.71	9.42	9.42	-13.77	351.1
41	25	-96	206	769	0	241	7082	15.71	15.71	9.42	9.42	-22.43	1079.8
42	25	32	233	596	0	295	7192	15.71	15.71	9.42	9.42	-22.74	1103.0
43	25	-11200	570	305	0	95	557	15.71	15.71	9.42	9.42	-4.30	-62.5
44	25	9811	-219	1086	0	340	12355	15.71	15.71	9.42	9.42	-35.15	2386.3
45	25	-1255	183	304	0	277	5762	15.71	15.71	9.42	9.42	-18.58	821.1
46	25	-2293	95	486	0	152	4679	15.71	15.71	9.42	9.42	-15.37	605.8
47	25	-2842	68	414	0	130	4078	15.71	15.71	9.42	9.42	-13.54	488.5
49	25	-4789	154	357	0	112	3073	15.71	15.71	9.42	9.42	-10.40	252.8
50	25	-586	-3	513	0	161	5433	15.71	15.71	9.42	9.42	-17.35	803.2
51	25	-2799	77	357	0	148	4114	15.71	15.71	9.42	9.42	-13.65	496.1

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	38	-5837	466	597	0	112	4127	15.71	15.71	9.42	9.42	-13.96	363.8
41	38	3	206	769	0	144	7108	15.71	15.71	9.42	9.42	-22.48	1088.7
42	38	132	233	596	0	221	7222	15.71	15.71	9.42	9.42	-22.80	1112.4
43	38	-11100	570	305	0	57	628	15.71	15.71	9.42	9.42	-4.41	-63.9
44	38	9910	-219	1086	0	204	12328	15.71	15.71	9.42	9.42	-35.01	2387.3
45	38	-1155	183	304	0	239	5785	15.71	15.71	9.42	9.42	-18.62	829.5
46	38	-2193	95	486	0	91	4691	15.71	15.71	9.42	9.42	-15.39	612.4
47	38	-2742	68	414	0	78	4086	15.71	15.71	9.42	9.42	-13.55	494.5
49	38	-4689	154	357	0	67	3092	15.71	15.71	9.42	9.42	-10.47	259.7
50	38	-486	-3	513	0	97	5432	15.71	15.71	9.42	9.42	-17.32	808.0
51	38	-2699	77	357	0	104	4124	15.71	15.71	9.42	9.42	-13.67	502.2

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	50	-5737	466	597	0	37	4185	15.71	15.71	9.42	9.42	-14.15	376.6
41	50	104	206	769	0	48	7134	15.71	15.71	9.42	9.42	-22.53	1097.5
42	50	232	233	596	0	146	7251	15.71	15.71	9.42	9.42	-22.86	1121.8
43	50	-11000	570	305	0	19	699	15.71	15.71	9.42	9.42	-4.52	-65.3
44	50	10010	-219	1086	0	68	12300	15.71	15.71	9.42	9.42	-34.87	2388.2
45	50	-1055	183	304	0	201	5808	15.71	15.71	9.42	9.42	-18.67	837.8
46	50	-2093	95	486	0	31	4703	15.71	15.71	9.42	9.42	-15.41	618.9
47	50	-2642	68	414	0	26	4095	15.71	15.71	9.42	9.42	-13.57	500.4
49	50	-4589	154	357	0	23	3112	15.71	15.71	9.42	9.42	-10.53	266.6
50	50	-386	-3	513	0	32	5432	15.71	15.71	9.42	9.42	-17.29	812.9
51	50	-2599	77	357	0	59	4134	15.71	15.71	9.42	9.42	-13.68	508.3

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 72 NI 1663 NF 1664 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 31
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	621	-327	-3004	0	-1636	-5301	15.71	15.71	9.42	9.42	-16.57	842.4
41	0	-2668	-481	-2216	0	-1209	-3604	15.71	15.71	9.42	9.42	-11.99	424.5
42	0	-2829	-448	-2422	0	-1211	-3543	15.71	15.71	9.42	9.42	-11.82	407.9
43	0	1826	-138	-3092	0	-1679	-5515	15.71	15.71	9.42	9.42	-16.82	935.3
44	0	-8043	-749	-978	0	-536	-916	15.71	15.71	9.42	9.42	-4.20	-58.1
45	0	-3924	-340	-2123	0	-970	-2586	15.71	15.71	9.42	9.42	-8.75	217.0
46	0	-4247	-343	-1518	0	-821	-2138	15.71	15.71	9.42	9.42	-7.22	140.7
47	0	-4642	-309	-1344	0	-724	-1772	15.71	15.71	9.42	9.42	-5.91	80.0
49	0	-3546	-257	-1606	0	-866	-2337	15.71	15.71	9.42	9.42	-7.91	196.1
50	0	-5520	-380	-1183	0	-638	-1417	15.71	15.71	9.42	9.42	-4.70	-64.1
51	0	-4696	-298	-1412	0	-724	-1751	15.71	15.71	9.42	9.42	-5.84	-76.7

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	12	721	-327	-3004	0	-1261	-5342	15.71	15.71	9.42	9.42	-16.66	853.6
41	12	-2568	-481	-2216	0	-932	-3664	15.71	15.71	9.42	9.42	-12.17	438.3
42	12	-2729	-448	-2422	0	-908	-3599	15.71	15.71	9.42	9.42	-11.98	421.0
43	12	1926	-138	-3092	0	-1292	-5532	15.71	15.71	9.42	9.42	-16.83	943.0
44	12	-7943	-749	-978	0	-414	-1009	15.71	15.71	9.42	9.42	-4.25	-60.0
45	12	-3824	-340	-2123	0	-704	-2628	15.71	15.71	9.42	9.42	-8.89	227.3
46	12	-4147	-343	-1518	0	-631	-2181	15.71	15.71	9.42	9.42	-7.37	150.3
47	12	-4542	-309	-1344	0	-556	-1810	15.71	15.71	9.42	9.42	-6.06	87.6
49	12	-3446	-257	-1606	0	-666	-2369	15.71	15.71	9.42	9.42	-8.02	204.9
50	12	-5420	-380	-1183	0	-490	-1464	15.71	15.71	9.42	9.42	-4.85	-65.8
51	12	-4596	-298	-1412	0	-548	-1788	15.71	15.71	9.42	9.42	-5.97	83.3

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	25	821	-327	-3004	0	-885	-5382	15.71	15.71	9.42	9.42	-16.76	864.8
41	25	-2468	-481	-2216	0	-655	-3724	15.71	15.71	9.42	9.42	-12.35	452.1
42	25	-2629	-448	-2422	0	-605	-3655	15.71	15.71	9.42	9.42	-12.15	434.1
43	25	2026	-138	-3092	0	-906	-5550	15.71	15.71	9.42	9.42	-16.85	950.7
44	25	-7843	-749	-978	0	-291	-1103	15.71	15.71	9.42	9.42	-4.40	-62.0
45	25	-3724	-340	-2123	0	-439	-2670	15.71	15.71	9.42	9.42	-9.03	237.6
46	25	-4047	-343	-1518	0	-441	-2224	15.71	15.71	9.42	9.42	-7.52	160.1
47	25	-4442	-309	-1344	0	-388	-1849	15.71	15.71	9.42	9.42	-6.20	95.5
49	25	-3346	-257	-1606	0	-465	-2402	15.71	15.71	9.42	9.42	-8.12	213.8
50	25	-5320	-380	-1183	0	-342	-1512	15.71	15.71	9.42	9.42	-5.00	-67.5
51	25	-4496	-298	-1412	0	-371	-1826	15.71	15.71	9.42	9.42	-6.11	90.9

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	38	921	-327	-3004	0	-510	-5423	15.71	15.71	9.42	9.42	-16.85	876.0
41	38	-2368	-481	-2216	0	-378	-3785	15.71	15.71	9.42	9.42	-12.53	465.9
42	38	-2529	-448	-2422	0	-303	-3711	15.71	15.71	9.42	9.42	-12.32	447.2
43	38	2126	-138	-3092	0	-519	-5567	15.71	15.71	9.42	9.42	-16.86	958.3
44	38	-7743	-749	-978	0	-169	-1196	15.71	15.71	9.42	9.42	-4.56	-64.0
45	38	-3624	-340	-2123	0	-174	-2713	15.71	15.71	9.42	9.42	-9.17	248.1
46	38	-3947	-343	-1518	0	-251	-2267	15.71	15.71	9.42	9.42	-7.67	170.1
47	38	-4342	-309	-1344	0	-220	-1888	15.71	15.71	9.42	9.42	-6.34	103.7

49	38	-3246	-257	-1606	0	-264	-2434	15.71	15.71	9.42	9.42	-8.23	222.8
50	38	-5220	-380	-1183	0	-194	-1560	15.71	15.71	9.42	9.42	-5.15	-69.3
51	38	-4396	-298	-1412	0	-195	-1863	15.71	15.71	9.42	9.42	-6.25	98.8

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	50	1021	-327	-3004	0	-134	-5464	15.71	15.71	9.42	9.42	-16.95	887.3
41	50	-2268	-481	-2216	0	-101	-3845	15.71	15.71	9.42	9.42	-12.70	479.8
42	50	-2429	-448	-2422	0	0	-3767	15.71	15.71	9.42	9.42	-12.48	460.4
43	50	2226	-138	-3092	0	-132	-5584	15.71	15.71	9.42	9.42	-16.88	966.0
44	50	-7643	-749	-978	0	-47	-1290	15.71	15.71	9.42	9.42	-4.73	-66.1
45	50	-3524	-340	-2123	0	92	-2755	15.71	15.71	9.42	9.42	-9.31	258.6
46	50	-3847	-343	-1518	0	-62	-2310	15.71	15.71	9.42	9.42	-7.82	180.1
47	50	-4242	-309	-1344	0	-52	-1926	15.71	15.71	9.42	9.42	-6.48	112.1
49	50	-3146	-257	-1606	0	-63	-2466	15.71	15.71	9.42	9.42	-8.33	231.8
50	50	-5120	-380	-1183	0	-46	-1607	15.71	15.71	9.42	9.42	-5.32	-71.1
51	50	-4296	-298	-1412	0	-18	-1900	15.71	15.71	9.42	9.42	-6.39	106.9

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 73 NI 1664 NF 48 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 31A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-4676	-1304	29	0	-134	-6404	15.71	15.71	9.42	9.42	-21.30	757.4
41	0	-7379	-1208	7	0	-101	-4746	15.71	15.71	9.42	9.42	-16.07	391.1
42	0	-7573	-1198	-652	0	0	-4680	15.71	15.71	9.42	9.42	-15.84	373.7
43	0	-3238	-1093	18	0	-132	-6444	15.71	15.71	9.42	9.42	-21.18	830.5
44	0	-11900	-1089	-36	0	-47	-2146	15.71	15.71	9.42	9.42	-7.67	-107.0
45	0	-8068	-916	-1118	0	92	-3570	15.71	15.71	9.42	9.42	-12.00	200.9
46	0	-7963	-766	-36	0	-62	-3040	15.71	15.71	9.42	9.42	-10.15	137.2
47	0	-8109	-656	-47	0	-52	-2614	15.71	15.71	9.42	9.42	-8.65	-115.5
49	0	-7208	-688	-39	0	-63	-3167	15.71	15.71	9.42	9.42	-10.64	176.6
50	0	-8939	-687	-50	0	-46	-2307	15.71	15.71	9.42	9.42	-7.65	-104.3
51	0	-8174	-652	-266	0	-18	-2592	15.71	15.71	9.42	9.42	-8.58	-114.6

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	12	-4576	-1304	29	0	-138	-6567	15.71	15.71	9.42	9.42	-21.81	786.7
41	12	-7279	-1208	7	0	-101	-4897	15.71	15.71	9.42	9.42	-16.58	417.1
42	12	-7473	-1198	-652	0	82	-4830	15.71	15.71	9.42	9.42	-16.35	399.4
43	12	-3138	-1093	18	0	-135	-6580	15.71	15.71	9.42	9.42	-21.60	856.1
44	12	-11800	-1089	-36	0	-42	-2282	15.71	15.71	9.42	9.42	-7.97	-110.8
45	12	-7968	-916	-1118	0	231	-3684	15.71	15.71	9.42	9.42	-12.41	219.5
46	12	-7863	-766	-36	0	-57	-3136	15.71	15.71	9.42	9.42	-10.49	151.9
47	12	-8009	-656	-47	0	-46	-2696	15.71	15.71	9.42	9.42	-8.94	-118.7
49	12	-7108	-688	-39	0	-58	-3253	15.71	15.71	9.42	9.42	-10.95	191.3
50	12	-8839	-687	-50	0	-40	-2393	15.71	15.71	9.42	9.42	-7.92	-107.4
51	12	-8074	-652	-266	0	15	-2674	15.71	15.71	9.42	9.42	-8.86	-117.9

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	25	-4476	-1304	29	0	-142	-6730	15.71	15.71	9.42	9.42	-22.32	816.2
41	25	-7179	-1208	7	0	-102	-5048	15.71	15.71	9.42	9.42	-17.08	443.4
42	25	-7373	-1198	-652	0	163	-4980	15.71	15.71	9.42	9.42	-16.85	425.3
43	25	-3038	-1093	18	0	-137	-6717	15.71	15.71	9.42	9.42	-22.01	881.7
44	25	-11700	-1089	-36	0	-38	-2418	15.71	15.71	9.42	9.42	-8.29	-114.9
45	25	-7868	-916	-1118	0	371	-3799	15.71	15.71	9.42	9.42	-12.81	238.4
46	25	-7763	-766	-36	0	-53	-3232	15.71	15.71	9.42	9.42	-10.83	167.0
47	25	-7909	-656	-47	0	-40	-2778	15.71	15.71	9.42	9.42	-9.23	-122.0
49	25	-7008	-688	-39	0	-53	-3339	15.71	15.71	9.42	9.42	-11.25	206.3
50	25	-8739	-687	-50	0	-34	-2479	15.71	15.71	9.42	9.42	-8.19	-110.7
51	25	-7974	-652	-266	0	48	-2755	15.71	15.71	9.42	9.42	-9.15	-121.1

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	38	-4376	-1304	29	0	-145	-6893	15.71	15.71	9.42	9.42	-22.82	845.6
41	38	-7079	-1208	7	0	-103	-5199	15.71	15.71	9.42	9.42	-17.58	469.8
42	38	-7273	-1198	-652	0	245	-5129	15.71	15.71	9.42	9.42	-17.35	451.4
43	38	-2938	-1093	18	0	-139	-6854	15.71	15.71	9.42	9.42	-22.43	907.3
44	38	-11600	-1089	-36	0	-33	-2554	15.71	15.71	9.42	9.42	-8.64	-119.2
45	38	-7768	-916	-1118	0	511	-3914	15.71	15.71	9.42	9.42	-13.21	257.7
46	38	-7663	-766	-36	0	-48	-3327	15.71	15.71	9.42	9.42	-11.17	182.5
47	38	-7809	-656	-47	0	-34	-2860	15.71	15.71	9.42	9.42	-9.52	-125.3
49	38	-6908	-688	-39	0	-48	-3425	15.71	15.71	9.42	9.42	-11.56	221.6
50	38	-8639	-687	-50	0	-27	-2565	15.71	15.71	9.42	9.42	-8.48	-114.0
51	38	-7874	-652	-266	0	82	-2836	15.71	15.71	9.42	9.42	-9.44	-124.4

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	50	-4276	-1304	29	0	-149	-7056	15.71	15.71	9.42	9.42	-23.33	875.1
41	50	-6979	-1208	7	0	-104	-5350	15.71	15.71	9.42	9.42	-18.08	496.4
42	50	-7173	-1198	-652	0	326	-5279	15.71	15.71	9.42	9.42	-17.85	477.7
43	50	-2838	-1093	18	0	-141	-6990	15.71	15.71	9.42	9.42	-22.84	932.9
44	50	-11500	-1089	-36	0	-29	-2690	15.71	15.71	9.42	9.42	-9.01	-123.8
45	50	-7668	-916	-1118	0	651	-4028	15.71	15.71	9.42	9.42	-13.61	277.3
46	50	-7563	-766	-36	0	-44	-3423	15.71	15.71	9.42	9.42	-11.52	198.4
47	50	-7709	-656	-47	0	-29	-2942	15.71	15.71	9.42	9.42	-9.82	132.7
49	50	-6808	-688	-39	0	-44	-3511	15.71	15.71	9.42	9.42	-11.86	237.1
50	50	-8539	-687	-50	0	-21	-2651	15.71	15.71	9.42	9.42	-8.77	-117.4
51	50	-7774	-652	-266	0	115	-2918	15.71	15.71	9.42	9.42	-9.73	128.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 74 NI 1667 NF 1665 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 30
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	

40	0	10780	-1420	-1606	0	-915	-11600	15.71	15.71	9.42	9.42	-32.18	2321.4
41	0	4626	-1316	-1145	0	-666	-8213	15.71	15.71	9.42	9.42	-24.26	1489.3
42	0	4707	-1343	-1355	0	-655	-8256	15.71	15.71	9.42	9.42	-24.36	1500.0
43	0	12400	-1235	-1689	0	-948	-12000	15.71	15.71	9.42	9.42	-32.60	2466.2
44	0	-5271	-1186	-417	0	-274	-2861	15.71	15.71	9.42	9.42	-9.67	203.5
45	0	2278	-1107	-1271	0	-514	-6423	15.71	15.71	9.42	9.42	-19.53	1096.9
46	0	654	-909	-786	0	-452	-5235	15.71	15.71	9.42	9.42	-16.35	833.9
47	0	-339	-808	-696	0	-399	-4490	15.71	15.71	9.42	9.42	-14.30	670.9
49	0	1713	-842	-850	0	-482	-5621	15.71	15.71	9.42	9.42	-17.20	945.9
50	0	-1822	-832	-595	0	-347	-3792	15.71	15.71	9.42	9.42	-12.45	492.7
51	0	-312	-816	-766	0	-395	-4504	15.71	15.71	9.42	9.42	-14.34	674.4

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	12	10880	-1420	-1606	0	-714	-11778	15.71	15.71	9.42	9.42	-32.71	2353.6
41	12	4726	-1316	-1145	0	-523	-8378	15.71	15.71	9.42	9.42	-24.74	1519.5
42	12	4807	-1343	-1355	0	-486	-8424	15.71	15.71	9.42	9.42	-24.86	1530.8
43	12	12500	-1235	-1689	0	-736	-12155	15.71	15.71	9.42	9.42	-33.05	2494.9
44	12	-5171	-1186	-417	0	-222	-3009	15.71	15.71	9.42	9.42	-10.18	228.4
45	12	2378	-1107	-1271	0	-355	-6562	15.71	15.71	9.42	9.42	-19.93	1123.2
46	12	754	-909	-786	0	-354	-5348	15.71	15.71	9.42	9.42	-16.67	856.3
47	12	-239	-808	-696	0	-312	-4591	15.71	15.71	9.42	9.42	-14.59	691.3
49	12	1813	-842	-850	0	-376	-5726	15.71	15.71	9.42	9.42	-17.49	967.0
50	12	-1722	-832	-595	0	-273	-3896	15.71	15.71	9.42	9.42	-12.76	513.3
51	12	-212	-816	-766	0	-300	-4606	15.71	15.71	9.42	9.42	-14.63	694.9

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	25	10980	-1420	-1606	0	-514	-11955	15.71	15.71	9.42	9.42	-33.24	2385.7
41	25	4826	-1316	-1145	0	-380	-8542	15.71	15.71	9.42	9.42	-25.22	1549.7
42	25	4907	-1343	-1355	0	-316	-8592	15.71	15.71	9.42	9.42	-25.35	1561.5
43	25	12600	-1235	-1689	0	-525	-12310	15.71	15.71	9.42	9.42	-33.51	2523.6
44	25	-5071	-1186	-417	0	-170	-3158	15.71	15.71	9.42	9.42	-10.69	253.7
45	25	2478	-1107	-1271	0	-196	-6700	15.71	15.71	9.42	9.42	-20.33	1149.4
46	25	854	-909	-786	0	-256	-5462	15.71	15.71	9.42	9.42	-17.00	878.6
47	25	-139	-808	-696	0	-225	-4692	15.71	15.71	9.42	9.42	-14.88	711.6
49	25	1913	-842	-850	0	-270	-5832	15.71	15.71	9.42	9.42	-17.79	988.1
50	25	-1622	-832	-595	0	-199	-4000	15.71	15.71	9.42	9.42	-13.07	533.9
51	25	-112	-816	-766	0	-204	-4708	15.71	15.71	9.42	9.42	-14.93	715.5

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	38	11080	-1420	-1606	0	-313	-12132	15.71	15.71	9.42	9.42	-33.77	2417.9
41	38	4926	-1316	-1145	0	-237	-8706	15.71	15.71	9.42	9.42	-25.71	1579.9
42	38	5007	-1343	-1355	0	-147	-8760	15.71	15.71	9.42	9.42	-25.84	1592.2
43	38	12700	-1235	-1689	0	-314	-12465	15.71	15.71	9.42	9.42	-33.97	2552.4
44	38	-4971	-1186	-417	0	-117	-3306	15.71	15.71	9.42	9.42	-11.19	279.2
45	38	2578	-1107	-1271	0	-37	-6838	15.71	15.71	9.42	9.42	-20.73	1175.6
46	38	954	-909	-786	0	-158	-5576	15.71	15.71	9.42	9.42	-17.33	901.0
47	38	-39	-808	-696	0	-138	-4793	15.71	15.71	9.42	9.42	-15.17	732.0
49	38	2013	-842	-850	0	-164	-5937	15.71	15.71	9.42	9.42	-18.08	1009.2
50	38	-1522	-832	-595	0	-124	-4104	15.71	15.71	9.42	9.42	-13.38	554.6
51	38	-12	-816	-766	0	-108	-4811	15.71	15.71	9.42	9.42	-15.22	736.1

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	50	11180	-1420	-1606	0	-112	-12310	15.71	15.71	9.42	9.42	-34.29	2450.1
41	50	5026	-1316	-1145	0	-94	-8871	15.71	15.71	9.42	9.42	-26.19	1610.1
42	50	5107	-1343	-1355	0	23	-8928	15.71	15.71	9.42	9.42	-26.34	1623.0
43	50	12800	-1235	-1689	0	-103	-12620	15.71	15.71	9.42	9.42	-34.42	2581.1
44	50	-4871	-1186	-417	0	-65	-3454	15.71	15.71	9.42	9.42	-11.69	305.1
45	50	2678	-1107	-1271	0	122	-6977	15.71	15.71	9.42	9.42	-21.13	1201.8
46	50	1054	-909	-786	0	-60	-5689	15.71	15.71	9.42	9.42	-17.65	923.3
47	50	61	-808	-696	0	-51	-4894	15.71	15.71	9.42	9.42	-15.46	752.4
49	50	2113	-842	-850	0	-57	-6042	15.71	15.71	9.42	9.42	-18.38	1030.4
50	50	-1422	-832	-595	0	-50	-4208	15.71	15.71	9.42	9.42	-13.69	575.3
51	50	88	-816	-766	0	-12	-4913	15.71	15.71	9.42	9.42	-15.51	756.6

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 75 NI 1684 NF 1683 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 29
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	12590	-1230	375	0	54	-12620	15.71	15.71	9.42	9.42	-34.54	2570.2
41	0	5899	-1197	347	0	58	-8955	15.71	15.71	9.42	9.42	-26.06	1667.5
42	0	5775	-1171	154	0	65	-8872	15.71	15.71	9.42	9.42	-25.85	1648.5
43	0	14300	-1019	319	0	39	-13060	15.71	15.71	9.42	9.42	-35.01	2725.9
44	0	-4843	-1183	311	0	66	-3169	15.71	15.71	9.42	9.42	-10.73	264.5
45	0	2946	-920	-48	0	57	-6803	15.71	15.71	9.42	9.42	-20.47	1188.7
46	0	1505	-824	230	0	38	-5734	15.71	15.71	9.42	9.42	-17.63	952.7
47	0	406	-730	200	0	33	-4928	15.71	15.71	9.42	9.42	-15.46	774.7
49	0	2636	-741	209	0	31	-6151	15.71	15.71	9.42	9.42	-18.52	1073.4
50	0	-1193	-774	208	0	37	-4174	15.71	15.71	9.42	9.42	-13.53	581.1
51	0	365	-721	136	0	35	-4901	15.71	15.71	9.42	9.42	-15.39	768.5

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	12	12690	-1230	375	0	7	-12775	15.71	15.71	9.42	9.42	-34.99	2598.9
41	12	5999	-1197	347	0	14	-9105	15.71	15.71	9.42	9.42	-26.50	1695.4
42	12	5875	-1171	154	0	46	-9018	15.71	15.71	9.42	9.42	-26.28	1675.9
43	12	14400	-1019	319	0	-1	-13185	15.71	15.71	9.42	9.42	-35.37	2750.0
44	12	-4743	-1183	311	0	27	-3317	15.71	15.71	9.42	9.42	-11.22	290.2
45	12	3046	-920	-48	0	63	-6918	15.71	15.71	9.42	9.42	-20.80	1211.4
46	12	1605	-824	230	0	9	-5837	15.71	15.71	9.42	9.42	-17.92	973.5
47	12	506	-730	200	0	8	-5019	15.71	15.71	9.42	9.42	-15.71	793.6
49	12	2736	-741	209	0	5	-6244	15.71	15.71	9.42	9.42	-18.77	1092.6
50	12	-1093	-774	208	0	11	-4271	15.71	15.71	9.42	9.42	-13.81	600.7
51	12	465	-721	136	0	18	-4991	15.71	15.71	9.42	9.42	-15.64	787.2

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	25	12790	-1230	375	0	-40	-12930	15.71	15.71	9.42	9.42	-35.45	2627.7
41	25	6099	-1197	347	0	-29	-9254	15.71	15.71	9.42	9.42	-26.93	1723.4
42	25	5975	-1171	154	0	26	-9165	15.71	15.71	9.42	9.42	-26.70	1703.4
43	25	14500	-1019	319	0	-41	-13310	15.71	15.71	9.42	9.42	-35.73	2774.2
44	25	-4643	-1183	311	0	-12	-3464	15.71	15.71	9.42	9.42	-11.71	316.2
45	25	3146	-920	-48	0	69	-7033	15.71	15.71	9.42	9.42	-21.12	1234.0
46	25	1705	-824	230	0	-20	-5940	15.71	15.71	9.42	9.42	-18.21	994.3
47	25	606	-730	200	0	-17	-5110	15.71	15.71	9.42	9.42	-15.97	812.5
49	25	2836	-741	209	0	-21	-6336	15.71	15.71	9.42	9.42	-19.03	1111.9
50	25	-993	-774	208	0	-15	-4368	15.71	15.71	9.42	9.42	-14.09	620.3
51	25	565	-721	136	0	1	-5081	15.71	15.71	9.42	9.42	-15.89	806.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	38	12890	-1230	375	0	-86	-13085	15.71	15.71	9.42	9.42	-35.90	2656.4
41	38	6199	-1197	347	0	-73	-9404	15.71	15.71	9.42	9.42	-27.37	1751.3
42	38	6075	-1171	154	0	7	-9312	15.71	15.71	9.42	9.42	-27.13	1730.9
43	38	14600	-1019	319	0	-81	-13435	15.71	15.71	9.42	9.42	-36.08	2798.4
44	38	-4543	-1183	311	0	-51	-3612	15.71	15.71	9.42	9.42	-12.20	342.4
45	38	3246	-920	-48	0	75	-7148	15.71	15.71	9.42	9.42	-21.45	1256.6
46	38	1805	-824	230	0	-48	-6043	15.71	15.71	9.42	9.42	-18.50	1015.1
47	38	706	-730	200	0	-42	-5202	15.71	15.71	9.42	9.42	-16.23	831.5
49	38	2936	-741	209	0	-47	-6429	15.71	15.71	9.42	9.42	-19.28	1131.1
50	38	-893	-774	208	0	-41	-4464	15.71	15.71	9.42	9.42	-14.37	640.0
51	38	665	-721	136	0	-16	-5171	15.71	15.71	9.42	9.42	-16.14	824.7

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	50	12990	-1230	375	0	-133	-13240	15.71	15.71	9.42	9.42	-36.36	2685.1
41	50	6299	-1197	347	0	-116	-9554	15.71	15.71	9.42	9.42	-27.80	1779.3
42	50	6175	-1171	154	0	-12	-9458	15.71	15.71	9.42	9.42	-27.55	1758.3
43	50	14700	-1019	319	0	-120	-13560	15.71	15.71	9.42	9.42	-36.44	2822.5
44	50	-4443	-1183	311	0	-90	-3760	15.71	15.71	9.42	9.42	-12.68	368.7
45	50	3346	-920	-48	0	81	-7263	15.71	15.71	9.42	9.42	-21.77	1279.3
46	50	1905	-824	230	0	-77	-6146	15.71	15.71	9.42	9.42	-18.79	1035.8
47	50	806	-730	200	0	-67	-5293	15.71	15.71	9.42	9.42	-16.48	850.4
49	50	3036	-741	209	0	-73	-6522	15.71	15.71	9.42	9.42	-19.54	1150.3
50	50	-793	-774	208	0	-67	-4561	15.71	15.71	9.42	9.42	-14.65	659.7
51	50	765	-721	136	0	-33	-5261	15.71	15.71	9.42	9.42	-16.39	843.5

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 76 NI 1692 NF 1691 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 28
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	10870	-1653	2334	0	1009	-11660	15.71	15.71	9.42	9.42	-32.33	2335.2
41	0	4345	-1437	1806	0	770	-8059	15.71	15.71	9.42	9.42	-23.89	1451.5
42	0	4344	-1446	1613	0	764	-8061	15.71	15.71	9.42	9.42	-23.90	1451.8
43	0	12750	-1503	2309	0	1011	-12210	15.71	15.71	9.42	9.42	-33.09	2516.2
44	0	-6162	-1128	988	0	397	-2361	15.71	15.71	9.42	9.42	-7.88	107.2
45	0	1883	-1157	1109	0	602	-6217	15.71	15.71	9.42	9.42	-19.02	1045.6
46	0	410	-967	1204	0	517	-5108	15.71	15.71	9.42	9.42	-16.03	802.4
47	0	-573	-849	1054	0	453	-4370	15.71	15.71	9.42	9.42	-13.99	641.1
49	0	1600	-921	1230	0	533	-5569	15.71	15.71	9.42	9.42	-17.07	932.3
50	0	-2183	-846	965	0	410	-3599	15.71	15.71	9.42	9.42	-11.90	446.3
51	0	-574	-852	990	0	452	-4370	15.71	15.71	9.42	9.42	-13.99	641.1

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	12	10970	-1653	2334	0	717	-11865	15.71	15.71	9.42	9.42	-32.95	2371.5
41	12	4445	-1437	1806	0	544	-8239	15.71	15.71	9.42	9.42	-24.42	1484.1
42	12	4444	-1446	1613	0	562	-8242	15.71	15.71	9.42	9.42	-24.43	1484.5
43	12	12850	-1503	2309	0	722	-12398	15.71	15.71	9.42	9.42	-33.66	2549.9
44	12	-6062	-1128	988	0	273	-2502	15.71	15.71	9.42	9.42	-8.38	127.7
45	12	1983	-1157	1109	0	464	-6362	15.71	15.71	9.42	9.42	-19.45	1072.7
46	12	510	-967	1204	0	366	-5229	15.71	15.71	9.42	9.42	-16.38	825.9
47	12	-473	-849	1054	0	322	-4476	15.71	15.71	9.42	9.42	-14.30	662.2
49	12	1700	-921	1230	0	379	-5684	15.71	15.71	9.42	9.42	-17.40	954.9
50	12	-2083	-846	965	0	290	-3705	15.71	15.71	9.42	9.42	-12.22	467.1
51	12	-474	-852	990	0	328	-4476	15.71	15.71	9.42	9.42	-14.30	662.2

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	25	11070	-1653	2334	0	426	-12070	15.71	15.71	9.42	9.42	-33.57	2407.9
41	25	4545	-1437	1806	0	318	-8418	15.71	15.71	9.42	9.42	-24.95	1516.6
42	25	4544	-1446	1613	0	361	-8422	15.71	15.71	9.42	9.42	-24.97	1517.1
43	25	12950	-1503	2309	0	433	-12585	15.71	15.71	9.42	9.42	-34.22	2583.6
44	25	-5962	-1128	988	0	150	-2643	15.71	15.71	9.42	9.42	-8.88	149.1
45	25	2083	-1157	1109	0	325	-6506	15.71	15.71	9.42	9.42	-19.87	1099.9
46	25	610	-967	1204	0	216	-5350	15.71	15.71	9.42	9.42	-16.73	849.3
47	25	-373	-849	1054	0	190	-4582	15.71	15.71	9.42	9.42	-14.60	683.4
49	25	1800	-921	1230	0	226	-5800	15.71	15.71	9.42	9.42	-17.73	977.5
50	25	-1983	-846	965	0	169	-3810	15.71	15.71	9.42	9.42	-12.54	487.9
51	25	-374	-852	990	0	204	-4583	15.71	15.71	9.42	9.42	-14.60	683.4

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	38	11170	-1653	2334	0	134	-12275	15.71	15.71	9.42	9.42	-34.18	2444.2
41	38	4645	-1437	1806	0	92	-8598	15.71	15.71	9.42	9.42	-25.48	1549.1
42	38	4644	-1446	1613	0	159	-8603	15.71	15.71	9.42	9.42	-25.50	1549.8
43	38	13050	-1503	2309	0	145	-12772	15.71	15.71	9.42	9.42	-34.78	2617.2
44	38	-5862	-1128	988	0	27	-2784	15.71	15.71	9.42	9.42	-9.38	171.4
45	38	2183	-1157	1109	0	187	-6651	15.71	15.71	9.42	9.42	-20.29	1127.1
46	38	710	-967	1204	0	65	-5470	15.71	15.71	9.42	9.42	-17.07	872.8
47	38	-273	-849	1054	0	58	-4689	15.71	15.71	9.42	9.42	-14.91	704.6
49	38	1900	-921	1230	0	72	-5915	15.71	15.71	9.42	9.42	-18.06	1000.2
50	38	-1883	-846	965	0	48	-3916	15.71	15.71	9.42	9.42	-12.86	508.8
51	38	-274	-852	990	0	80	-4690	15.71	15.71	9.42	9.42	-14.91	704.6

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	50	11270	-1653	2334	0	-158	-12480	15.71	15.71	9.42	9.42	-34.80	2480.6
41	50	4745	-1437	1806	0	-134	-8778	15.71	15.71	9.42	9.42	-26.02	1581.7
42	50	4744	-1446	1613	0	-43	-8784	15.71	15.71	9.42	9.42	-26.04	1582.5
43	50	13150	-1503	2309	0	-144	-12960	15.71	15.71	9.42	9.42	-35.34	2650.9
44	50	-5762	-1128	988	0	-97	-2925	15.71	15.71	9.42	9.42	-9.88	194.2
45	50	2283	-1157	1109	0	48	-6796	15.71	15.71	9.42	9.42	-20.71	1154.2
46	50	810	-967	1204	0	-86	-5591	15.71	15.71	9.42	9.42	-17.42	896.2
47	50	-173	-849	1054	0	-74	-4795	15.71	15.71	9.42	9.42	-15.22	725.7
49	50	2000	-921	1230	0	-82	-6030	15.71	15.71	9.42	9.42	-18.39	1022.9
50	50	-1783	-846	965	0	-72	-4022	15.71	15.71	9.42	9.42	-13.17	529.6
51	50	-174	-852	990	0	-43	-4796	15.71	15.71	9.42	9.42	-15.22	725.9

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 77 NI 1700 NF 1699 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 27
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	717	-1588	4214	0	2055	-5187	15.71	15.71	9.42	9.42	-16.18	829.7
41	0	-3674	-1110	3105	0	1488	-2829	15.71	15.71	9.42	9.42	-9.56	263.2
42	0	-3634	-1159	2951	0	1500	-2904	15.71	15.71	9.42	9.42	-9.81	276.0
43	0	2804	-1662	4315	0	2122	-5934	15.71	15.71	9.42	9.42	-17.76	1048.7
44	0	-10890	-349	1363	0	593	972	15.71	15.71	9.42	9.42	-5.19	-71.8
45	0	-4448	-947	2209	0	1197	-2129	15.71	15.71	9.42	9.42	-7.49	132.3
46	0	-5017	-719	2083	0	989	-1510	15.71	15.71	9.42	9.42	-6.19	-69.9
47	0	-5353	-621	1827	0	864	-1180	15.71	15.71	9.42	9.42	-5.42	-63.7
49	0	-3889	-780	2197	0	1054	-1966	15.71	15.71	9.42	9.42	-6.64	130.0
50	0	-6629	-517	1606	0	748	-585	15.71	15.71	9.42	9.42	-4.83	-60.5
51	0	-5340	-637	1776	0	869	-1205	15.71	15.71	9.42	9.42	-5.44	-63.9

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	12	817	-1588	4214	0	1528	-5386	15.71	15.71	9.42	9.42	-16.77	865.1
41	12	-3574	-1110	3105	0	1100	-2968	15.71	15.71	9.42	9.42	-10.01	288.1
42	12	-3534	-1159	2951	0	1131	-3049	15.71	15.71	9.42	9.42	-10.28	301.9
43	12	2904	-1662	4315	0	1583	-6142	15.71	15.71	9.42	9.42	-18.38	1085.5
44	12	-10790	-349	1363	0	423	928	15.71	15.71	9.42	9.42	-4.91	-70.2
45	12	-4348	-947	2209	0	921	-2248	15.71	15.71	9.42	9.42	-7.59	152.1
46	12	-4917	-719	2083	0	729	-1600	15.71	15.71	9.42	9.42	-5.30	-70.6
47	12	-5253	-621	1827	0	636	-1258	15.71	15.71	9.42	9.42	-4.20	-57.6
49	12	-3789	-780	2197	0	779	-2064	15.71	15.71	9.42	9.42	-6.98	147.3
50	12	-6529	-517	1606	0	547	-649	15.71	15.71	9.42	9.42	-3.85	-49.9
51	12	-5240	-637	1776	0	647	-1284	15.71	15.71	9.42	9.42	-4.28	-58.6

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	25	917	-1588	4214	0	1002	-5584	15.71	15.71	9.42	9.42	-17.36	900.4
41	25	-3474	-1110	3105	0	712	-3106	15.71	15.71	9.42	9.42	-10.47	313.2
42	25	-3434	-1159	2951	0	762	-3194	15.71	15.71	9.42	9.42	-10.75	328.0
43	25	3004	-1662	4315	0	1043	-6350	15.71	15.71	9.42	9.42	-19.00	1122.4
44	25	-10690	-349	1363	0	252	884	15.71	15.71	9.42	9.42	-4.79	-68.7
45	25	-4248	-947	2209	0	644	-2366	15.71	15.71	9.42	9.42	-8.00	172.5
46	25	-4817	-719	2083	0	468	-1690	15.71	15.71	9.42	9.42	-5.61	-74.2
47	25	-5153	-621	1827	0	408	-1335	15.71	15.71	9.42	9.42	-4.43	-60.3
49	25	-3689	-780	2197	0	505	-2161	15.71	15.71	9.42	9.42	-7.31	165.0
50	25	-6429	-517	1606	0	346	-714	15.71	15.71	9.42	9.42	-3.24	-45.9
51	25	-5140	-637	1776	0	425	-1364	15.71	15.71	9.42	9.42	-4.52	-61.4

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	38	1017	-1588	4214	0	475	-5782	15.71	15.71	9.42	9.42	-17.96	935.8
41	38	-3374	-1110	3105	0	323	-3245	15.71	15.71	9.42	9.42	-10.91	338.4
42	38	-3334	-1159	2951	0	393	-3338	15.71	15.71	9.42	9.42	-11.21	354.2
43	38	3104	-1662	4315	0	504	-6557	15.71	15.71	9.42	9.42	-19.62	1159.2
44	38	-10590	-349	1363	0	82	841	15.71	15.71	9.42	9.42	-4.68	-67.1
45	38	-4148	-947	2209	0	368	-2484	15.71	15.71	9.42	9.42	-8.41	193.3
46	38	-4717	-719	2083	0	208	-1779	15.71	15.71	9.42	9.42	-5.93	78.7
47	38	-5053	-621	1827	0	179	-1412	15.71	15.71	9.42	9.42	-4.67	-63.2
49	38	-3589	-780	2197	0	230	-2258	15.71	15.71	9.42	9.42	-7.65	183.0
50	38	-6329	-517	1606	0	145	-779	15.71	15.71	9.42	9.42	-3.33	-47.2
51	38	-5040	-637	1776	0	203	-1444	15.71	15.71	9.42	9.42	-4.77	-64.4

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	50	1117	-1588	4214	0	-52	-5981	15.71	15.71	9.42	9.42	-18.55	971.2
41	50	-3274	-1110	3105	0	-65	-3384	15.71	15.71	9.42	9.42	-11.36	363.7
42	50	-3234	-1159	2951	0	25	-3483	15.71	15.71	9.42	9.42	-11.67	380.5
43	50	3204	-1662	4315	0	-36	-6765	15.71	15.71	9.42	9.42	-20.24	1196.0
44	50	-10490	-349	1363	0	-88	797	15.71	15.71	9.42	9.42	-4.57	-65.6
45	50	-4048	-947	2209	0	92	-2603	15.71	15.71	9.42	9.42	-8.81	214.4
46	50	-4617	-719	2083	0	-52	-1869	15.71	15.71	9.42	9.42	-6.26	92.6
47	50	-4953	-621	1827	0	-49	-1490	15.71	15.71	9.42	9.42	-4.92	-66.2
49	50	-3489	-780	2197	0	-45	-2356	15.71	15.71	9.42	9.42	-7.97	201.2
50	50	-6229	-517	1606	0	-55	-843	15.71	15.71	9.42	9.42	-3.43	-48.4
51	50	-4940	-637	1776	0	-19	-1523	15.71	15.71	9.42	9.42	-5.04	-67.5

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 78 NI 1665 NF 91 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 30A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	2947	-3346	314	0	-112	-13640	15.71	15.71	9.42	9.42	-42.17	2234.7
41	0	-1956	-2723	312	0	-94	-10060	15.71	15.71	9.42	9.42	-32.37	1444.9
42	0	-1893	-2748	-334	0	23	-10120	15.71	15.71	9.42	9.42	-32.54	1457.2
43	0	4746	-3179	240	0	-103	-13880	15.71	15.71	9.42	9.42	-42.27	2361.6

44	0	-9947	-1780	311	0	-65	-4437	15.71	15.71	9.42	9.42	-14.92	252.4
45	0	-3321	-2183	-840	0	122	-8002	15.71	15.71	9.42	9.42	-26.16	1064.5
46	0	-4307	-1791	191	0	-60	-6611	15.71	15.71	9.42	9.42	-21.91	805.9
47	0	-4895	-1558	161	0	-51	-5749	15.71	15.71	9.42	9.42	-19.22	648.0
49	0	-3260	-1766	161	0	-57	-6943	15.71	15.71	9.42	9.42	-22.78	905.7
50	0	-6199	-1486	176	0	-50	-5056	15.71	15.71	9.42	9.42	-17.07	486.0
51	0	-4874	-1567	-55	0	-12	-5769	15.71	15.71	9.42	9.42	-19.28	652.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	12	3047	-3346	314	0	-152	-14058	15.71	15.71	9.42	9.42	-43.46	2303.6
41	12	-1856	-2723	312	0	-133	-10400	15.71	15.71	9.42	9.42	-33.42	1501.8
42	12	-1793	-2748	-334	0	64	-10462	15.71	15.71	9.42	9.42	-33.60	1514.4
43	12	4846	-3179	240	0	-133	-14278	15.71	15.71	9.42	9.42	-43.49	2427.4
44	12	-9847	-1780	311	0	-104	-4660	15.71	15.71	9.42	9.42	-15.70	285.5
45	12	-3221	-2183	-840	0	227	-8275	15.71	15.71	9.42	9.42	-27.01	1111.0
46	12	-4207	-1791	191	0	-84	-6835	15.71	15.71	9.42	9.42	-22.61	844.6
47	12	-4795	-1558	161	0	-71	-5944	15.71	15.71	9.42	9.42	-19.83	682.1
49	12	-3160	-1766	161	0	-77	-7164	15.71	15.71	9.42	9.42	-23.46	944.1
50	12	-6099	-1486	176	0	-72	-5242	15.71	15.71	9.42	9.42	-17.68	518.1
51	12	-4774	-1567	-55	0	-6	-5965	15.71	15.71	9.42	9.42	-19.90	686.2

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	25	3147	-3346	314	0	-191	-14475	15.71	15.71	9.42	9.42	-44.74	2372.5
41	25	-1756	-2723	312	0	-172	-10740	15.71	15.71	9.42	9.42	-34.47	1558.7
42	25	-1693	-2748	-334	0	106	-10805	15.71	15.71	9.42	9.42	-34.66	1571.7
43	25	4946	-3179	240	0	-163	-14675	15.71	15.71	9.42	9.42	-44.72	2493.2
44	25	-9747	-1780	311	0	-143	-4882	15.71	15.71	9.42	9.42	-16.48	319.4
45	25	-3121	-2183	-840	0	332	-8548	15.71	15.71	9.42	9.42	-27.85	1157.5
46	25	-4107	-1791	191	0	-107	-7058	15.71	15.71	9.42	9.42	-23.31	883.4
47	25	-4695	-1558	161	0	-91	-6138	15.71	15.71	9.42	9.42	-20.45	716.2
49	25	-3060	-1766	161	0	-98	-7384	15.71	15.71	9.42	9.42	-24.14	982.6
50	25	-5999	-1486	176	0	-94	-5428	15.71	15.71	9.42	9.42	-18.28	550.2
51	25	-4674	-1567	-55	0	1	-6160	15.71	15.71	9.42	9.42	-20.52	720.5

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	38	3247	-3346	314	0	-230	-14892	15.71	15.71	9.42	9.42	-46.03	2441.4
41	38	-1656	-2723	312	0	-211	-11080	15.71	15.71	9.42	9.42	-35.52	1615.6
42	38	-1593	-2748	-334	0	148	-11148	15.71	15.71	9.42	9.42	-35.71	1629.0
43	38	5046	-3179	240	0	-193	-15072	15.71	15.71	9.42	9.42	-45.94	2559.1
44	38	-9647	-1780	311	0	-182	-5104	15.71	15.71	9.42	9.42	-17.25	354.0
45	38	-3021	-2183	-840	0	437	-8821	15.71	15.71	9.42	9.42	-28.70	1204.0
46	38	-4007	-1791	191	0	-131	-7282	15.71	15.71	9.42	9.42	-24.00	922.2
47	38	-4595	-1558	161	0	-111	-6333	15.71	15.71	9.42	9.42	-21.06	750.3
49	38	-2960	-1766	161	0	-118	-7605	15.71	15.71	9.42	9.42	-24.82	1021.1
50	38	-5899	-1486	176	0	-116	-5613	15.71	15.71	9.42	9.42	-18.88	582.5
51	38	-4574	-1567	-55	0	8	-6356	15.71	15.71	9.42	9.42	-21.13	754.8

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	50	3347	-3346	314	0	-269	-15310	15.71	15.71	9.42	9.42	-47.32	2510.3
41	50	-1556	-2723	312	0	-250	-11420	15.71	15.71	9.42	9.42	-36.57	1672.6
42	50	-1493	-2748	-334	0	190	-11490	15.71	15.71	9.42	9.42	-36.77	1686.3
43	50	5146	-3179	240	0	-223	-15470	15.71	15.71	9.42	9.42	-47.16	2624.9
44	50	-9547	-1780	311	0	-221	-5327	15.71	15.71	9.42	9.42	-18.02	389.1
45	50	-2921	-2183	-840	0	542	-9094	15.71	15.71	9.42	9.42	-29.54	1250.6
46	50	-3907	-1791	191	0	-155	-7506	15.71	15.71	9.42	9.42	-24.70	961.0
47	50	-4495	-1558	161	0	-132	-6528	15.71	15.71	9.42	9.42	-21.67	784.6
49	50	-2860	-1766	161	0	-138	-7826	15.71	15.71	9.42	9.42	-25.50	1059.6
50	50	-5799	-1486	176	0	-138	-5799	15.71	15.71	9.42	9.42	-19.48	614.9
51	50	-4474	-1567	-55	0	15	-6552	15.71	15.71	9.42	9.42	-21.74	789.2

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 79 NI 1683 NF 134 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 29A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	4289	-3440	811	0	-133	-14630	15.71	15.71	9.42	9.42	-44.82	2453.4
41	0	-1030	-2804	710	0	-116	-10790	15.71	15.71	9.42	9.42	-34.43	1601.8
42	0	-1121	-2770	135	0	-12	-10690	15.71	15.71	9.42	9.42	-34.14	1582.0
43	0	6170	-3263	731	0	-120	-14890	15.71	15.71	9.42	9.42	-44.92	2587.8
44	0	-9678	-1845	557	0	-90	-4769	15.71	15.71	9.42	9.42	-16.09	306.4
45	0	-2847	-2147	-395	0	81	-8317	15.71	15.71	9.42	9.42	-27.06	1135.3
46	0	-3693	-1843	476	0	-77	-7102	15.71	15.71	9.42	9.42	-23.37	909.5
47	0	-4359	-1603	417	0	-67	-6180	15.71	15.71	9.42	9.42	-20.53	737.9
49	0	-2586	-1814	451	0	-73	-7460	15.71	15.71	9.42	9.42	-24.28	1016.8
50	0	-5756	-1531	416	0	-67	-5436	15.71	15.71	9.42	9.42	-18.29	562.2
51	0	-4389	-1591	225	0	-33	-6146	15.71	15.71	9.42	9.42	-20.43	731.4

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	12	4389	-3440	811	0	-235	-15060	15.71	15.71	9.42	9.42	-46.15	2524.2
41	12	-930	-2804	710	0	-205	-11140	15.71	15.71	9.42	9.42	-35.51	1660.2
42	12	-1021	-2770	135	0	-29	-11038	15.71	15.71	9.42	9.42	-35.21	1640.1
43	12	6270	-3263	731	0	-212	-15298	15.71	15.71	9.42	9.42	-46.17	2655.1
44	12	-9578	-1845	557	0	-159	-5000	15.71	15.71	9.42	9.42	-16.89	341.9
45	12	-2747	-2147	-395	0	131	-8585	15.71	15.71	9.42	9.42	-27.89	1181.1
46	12	-3593	-1843	476	0	-137	-7332	15.71	15.71	9.42	9.42	-24.09	949.3
47	12	-4259	-1603	417	0	-120	-6380	15.71	15.71	9.42	9.42	-21.16	773.0
49	12	-2486	-1814	451	0	-130	-7687	15.71	15.71	9.42	9.42	-24.98	1056.2
50	12	-5656	-1531	416	0	-119	-5628	15.71	15.71	9.42	9.42	-18.90	595.4
51	12	-4289	-1591	225	0	-61	-6345	15.71	15.71	9.42	9.42	-21.05	766.3

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	25	4489	-3440	811	0	-336	-15490	15.71	15.71	9.42	9.42	-47.47	2595.0
41	25	-830	-2804	710	0	-294	-11490	15.71	15.71	9.42	9.42	-36.58	1718.7
42	25	-921	-2770	135	0	-46	-11385	15.71	15.71	9.42	9.42	-36.28	1698.2
43	25	6370	-3263	731	0	-303	-15705	15.71	15.71	9.42	9.42	-47.43	2722.5
44	25	-9478	-1845	557	0	-229	-5230	15.71	15.71	9.42	9.42	-17.69	378.0

45	25	-2647	-2147	-395	0	180	-8854	15.71	15.71	9.42	9.42	-28.72	1226.9
46	25	-3493	-1843	476	0	-196	-7562	15.71	15.71	9.42	9.42	-24.80	989.2
47	25	-4159	-1603	417	0	-172	-6580	15.71	15.71	9.42	9.42	-21.79	808.2
49	25	-2386	-1814	451	0	-186	-7914	15.71	15.71	9.42	9.42	-25.67	1095.7
50	25	-5556	-1531	416	0	-171	-5819	15.71	15.71	9.42	9.42	-19.52	628.8
51	25	-4189	-1591	225	0	-89	-6544	15.71	15.71	9.42	9.42	-21.67	801.2

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	38	4589	-3440	811	0	-437	-15920	15.71	15.71	9.42	9.42	-48.80	2665.8
41	38	-730	-2804	710	0	-382	-11840	15.71	15.71	9.42	9.42	-37.66	1777.2
42	38	-821	-2770	135	0	-63	-11732	15.71	15.71	9.42	9.42	-37.35	1756.3
43	38	6470	-3263	731	0	-395	-16112	15.71	15.71	9.42	9.42	-48.69	2789.8
44	38	-9378	-1845	557	0	-299	-5460	15.71	15.71	9.42	9.42	-18.48	414.6
45	38	-2547	-2147	-395	0	229	-9122	15.71	15.71	9.42	9.42	-29.54	1272.8
46	38	-3393	-1843	476	0	-256	-7793	15.71	15.71	9.42	9.42	-25.51	1029.1
47	38	-4059	-1603	417	0	-224	-6781	15.71	15.71	9.42	9.42	-22.41	843.3
49	38	-2286	-1814	451	0	-242	-8140	15.71	15.71	9.42	9.42	-26.37	1135.2
50	38	-5456	-1531	416	0	-223	-6010	15.71	15.71	9.42	9.42	-20.13	662.2
51	38	-4089	-1591	225	0	-117	-6743	15.71	15.71	9.42	9.42	-22.29	836.2

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	50	4689	-3440	811	0	-539	-16350	15.71	15.71	9.42	9.42	-50.13	2736.6
41	50	-630	-2804	710	0	-471	-12190	15.71	15.71	9.42	9.42	-38.74	1835.7
42	50	-721	-2770	135	0	-80	-12080	15.71	15.71	9.42	9.42	-38.42	1814.4
43	50	6570	-3263	731	0	-486	-16520	15.71	15.71	9.42	9.42	-49.94	2857.2
44	50	-9278	-1845	557	0	-368	-5691	15.71	15.71	9.42	9.42	-19.27	451.7
45	50	-2447	-2147	-395	0	279	-9390	15.71	15.71	9.42	9.42	-30.37	1318.6
46	50	-3293	-1843	476	0	-315	-8023	15.71	15.71	9.42	9.42	-26.22	1069.1
47	50	-3959	-1603	417	0	-276	-6981	15.71	15.71	9.42	9.42	-23.03	878.5
49	50	-2186	-1814	451	0	-299	-8367	15.71	15.71	9.42	9.42	-27.06	1174.7
50	50	-5356	-1531	416	0	-275	-6202	15.71	15.71	9.42	9.42	-20.74	695.6
51	50	-3989	-1591	225	0	-146	-6942	15.71	15.71	9.42	9.42	-22.91	871.2

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 80 NI 1691 NF 177 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 28A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	3144	-3459	1122	0	-158	-13780	15.71	15.71	9.42	9.42	-42.54	2266.0
41	0	-2106	-2737	966	0	-134	-9937	15.71	15.71	9.42	9.42	-32.02	1418.8
42	0	-2103	-2741	434	0	-43	-9942	15.71	15.71	9.42	9.42	-32.03	1419.7
43	0	5168	-3345	1021	0	-144	-14190	15.71	15.71	9.42	9.42	-43.09	2430.2
44	0	-10670	-1631	734	0	-97	-3883	15.71	15.71	9.42	9.42	-12.93	-170.2
45	0	-3578	-2148	-126	0	48	-7794	15.71	15.71	9.42	9.42	-25.55	1020.5
46	0	-4468	-1782	638	0	-86	-6495	15.71	15.71	9.42	9.42	-21.56	780.8
47	0	-5058	-1544	556	0	-74	-5635	15.71	15.71	9.42	9.42	-18.87	623.4
49	0	-3308	-1785	608	0	-82	-6916	15.71	15.71	9.42	9.42	-22.70	899.3
50	0	-6476	-1442	551	0	-72	-4854	15.71	15.71	9.42	9.42	-16.41	444.3
51	0	-5057	-1545	379	0	-43	-5637	15.71	15.71	9.42	9.42	-18.87	623.7

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	12	3244	-3459	1122	0	-298	-14212	15.71	15.71	9.42	9.42	-43.88	2337.2
41	12	-2006	-2737	966	0	-254	-10280	15.71	15.71	9.42	9.42	-33.08	1476.2
42	12	-2003	-2741	434	0	-97	-10284	15.71	15.71	9.42	9.42	-33.09	1476.9
43	12	5268	-3345	1021	0	-272	-14608	15.71	15.71	9.42	9.42	-44.38	2499.1
44	12	-10570	-1631	734	0	-189	-4087	15.71	15.71	9.42	9.42	-13.65	188.3
45	12	-3478	-2148	-126	0	64	-8062	15.71	15.71	9.42	9.42	-26.39	1066.3
46	12	-4368	-1782	638	0	-165	-6718	15.71	15.71	9.42	9.42	-22.26	819.4
47	12	-4958	-1544	556	0	-143	-5828	15.71	15.71	9.42	9.42	-19.48	657.1
49	12	-3208	-1785	608	0	-158	-7139	15.71	15.71	9.42	9.42	-23.39	938.1
50	12	-6376	-1442	551	0	-141	-5034	15.71	15.71	9.42	9.42	-17.01	475.2
51	12	-4957	-1545	379	0	-91	-5830	15.71	15.71	9.42	9.42	-19.49	657.4

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	25	3344	-3459	1122	0	-438	-14645	15.71	15.71	9.42	9.42	-45.21	2408.4
41	25	-1906	-2737	966	0	-375	-10624	15.71	15.71	9.42	9.42	-34.14	1533.6
42	25	-1903	-2741	434	0	-151	-10626	15.71	15.71	9.42	9.42	-34.15	1534.1
43	25	5368	-3345	1021	0	-399	-15025	15.71	15.71	9.42	9.42	-45.66	2568.0
44	25	-10470	-1631	734	0	-280	-4290	15.71	15.71	9.42	9.42	-14.37	216.6
45	25	-3378	-2148	-126	0	80	-8331	15.71	15.71	9.42	9.42	-27.22	1112.1
46	25	-4268	-1782	638	0	-245	-6941	15.71	15.71	9.42	9.42	-22.96	858.0
47	25	-4858	-1544	556	0	-213	-6021	15.71	15.71	9.42	9.42	-20.09	690.9
49	25	-3108	-1785	608	0	-234	-7362	15.71	15.71	9.42	9.42	-24.08	976.9
50	25	-6276	-1442	551	0	-210	-5214	15.71	15.71	9.42	9.42	-17.60	506.3
51	25	-4857	-1545	379	0	-138	-6023	15.71	15.71	9.42	9.42	-20.10	691.2

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	38	3444	-3459	1122	0	-579	-15078	15.71	15.71	9.42	9.42	-46.55	2479.6
41	38	-1806	-2737	966	0	-496	-10967	15.71	15.71	9.42	9.42	-35.20	1591.0
42	38	-1803	-2741	434	0	-205	-10968	15.71	15.71	9.42	9.42	-35.20	1591.3
43	38	5468	-3345	1021	0	-527	-15442	15.71	15.71	9.42	9.42	-46.95	2636.9
44	38	-10370	-1631	734	0	-372	-4494	15.71	15.71	9.42	9.42	-15.09	245.9
45	38	-3278	-2148	-126	0	95	-8600	15.71	15.71	9.42	9.42	-28.05	1157.9
46	38	-4168	-1782	638	0	-325	-7164	15.71	15.71	9.42	9.42	-23.66	896.6
47	38	-4758	-1544	556	0	-282	-6214	15.71	15.71	9.42	9.42	-20.70	724.7
49	38	-3008	-1785	608	0	-310	-7586	15.71	15.71	9.42	9.42	-24.77	1015.8
50	38	-6176	-1442	551	0	-279	-5395	15.71	15.71	9.42	9.42	-18.18	537.6
51	38	-4757	-1545	379	0	-185	-6216	15.71	15.71	9.42	9.42	-20.71	725.1

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	50	3544	-3459	1122	0	-719	-15510	15.71	15.71	9.42	9.42	-47.88	2550.8
41	50	-1706	-2737	966	0	-617	-11310	15.71	15.71	9.42	9.42	-36.26	1648.4
42	50	-1703	-2741	434	0	-260	-11310	15.71	15.71	9.42	9.42	-36.26	1648.6
43	50	5568	-3345	1021	0	-654	-15860	15.71	15.71	9.42	9.42	-48.24	2705.8
44	50	-10270	-1631	734	0	-464	-4698	15.71	15.71	9.42	9.42	-15.81	276.1
45	50	-3178	-2148	-126	0	111	-8868	15.71	15.71	9.42	9.42	-28.88	1203.7

46	50	-4068	-1782	638	0	-405	-7387	15.71	15.71	9.42	9.42	-24.35	935.3
47	50	-4658	-1544	556	0	-352	-6407	15.71	15.71	9.42	9.42	-21.31	758.6
49	50	-2908	-1785	608	0	-386	-7809	15.71	15.71	9.42	9.42	-25.46	1054.7
50	50	-6076	-1442	551	0	-348	-5575	15.71	15.71	9.42	9.42	-18.77	569.0
51	50	-4657	-1545	379	0	-233	-6409	15.71	15.71	9.42	9.42	-21.31	759.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 81 NI 1699 NF 220 SEZ. Rp B= 0.400 H= 0.800 (pilastro)
PIL. NUM. 27A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-3789	-2583	1407	0	-52	-6859	15.71	15.71	9.42	9.42	-22.61	867.9
41	0	-7621	-1843	1303	0	-65	-4215	15.71	15.71	9.42	9.42	-14.26	305.3
42	0	-7643	-1902	813	0	25	-4326	15.71	15.71	9.42	9.42	-14.64	320.2
43	0	-1558	-2643	1239	0	-36	-7576	15.71	15.71	9.42	9.42	-24.40	1084.0
44	0	-14010	-676	1174	0	-88	26	15.71	15.71	9.42	9.42	-4.15	-61.0
45	0	-7980	-1507	248	0	92	-3353	15.71	15.71	9.42	9.42	-11.24	175.6
46	0	-8139	-1149	923	0	-52	-2540	15.71	15.71	9.42	9.42	-8.40	-112.5
47	0	-8268	-976	828	0	-49	-2122	15.71	15.71	9.42	9.42	-7.04	-96.0
49	0	-6991	-1222	863	0	-45	-3003	15.71	15.71	9.42	9.42	-10.08	162.3
50	0	-9482	-829	850	0	-55	-1483	15.71	15.71	9.42	9.42	-5.62	-78.8
51	0	-8275	-995	665	0	-19	-2159	15.71	15.71	9.42	9.42	-7.16	-97.4

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	12	-3689	-2583	1407	0	-228	-7182	15.71	15.71	9.42	9.42	-23.62	921.9
41	12	-7521	-1843	1303	0	-228	-4445	15.71	15.71	9.42	9.42	-15.05	342.0
42	12	-7543	-1902	813	0	-77	-4564	15.71	15.71	9.42	9.42	-15.45	358.1
43	12	-1458	-2643	1239	0	-191	-7906	15.71	15.71	9.42	9.42	-25.42	1139.4
44	12	-13910	-676	1174	0	-235	-59	15.71	15.71	9.42	9.42	-4.67	-66.8
45	12	-7880	-1507	248	0	61	-3542	15.71	15.71	9.42	9.42	-11.91	203.5
46	12	-8039	-1149	923	0	-168	-2684	15.71	15.71	9.42	9.42	-8.90	-118.3
47	12	-8168	-976	828	0	-153	-2244	15.71	15.71	9.42	9.42	-7.42	-100.6
49	12	-6891	-1222	863	0	-153	-3156	15.71	15.71	9.42	9.42	-10.62	185.7
50	12	-9382	-829	850	0	-162	-1586	15.71	15.71	9.42	9.42	-5.81	-81.3
51	12	-8175	-995	665	0	-102	-2283	15.71	15.71	9.42	9.42	-7.55	-102.1

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	25	-3589	-2583	1407	0	-404	-7505	15.71	15.71	9.42	9.42	-24.63	975.9
41	25	-7421	-1843	1303	0	-390	-4676	15.71	15.71	9.42	9.42	-15.83	379.1
42	25	-7443	-1902	813	0	-179	-4802	15.71	15.71	9.42	9.42	-16.26	396.5
43	25	-1358	-2643	1239	0	-346	-8236	15.71	15.71	9.42	9.42	-26.44	1194.8
44	25	-13810	-676	1174	0	-382	-143	15.71	15.71	9.42	9.42	-5.20	-72.6
45	25	-7780	-1507	248	0	30	-3730	15.71	15.71	9.42	9.42	-12.57	232.2
46	25	-7939	-1149	923	0	-283	-2828	15.71	15.71	9.42	9.42	-9.40	-124.1
47	25	-8068	-976	828	0	-256	-2366	15.71	15.71	9.42	9.42	-7.82	-105.3
49	25	-6791	-1222	863	0	-261	-3308	15.71	15.71	9.42	9.42	-11.16	209.8
50	25	-9282	-829	850	0	-268	-1690	15.71	15.71	9.42	9.42	-6.02	-83.9
51	25	-8075	-995	665	0	-186	-2408	15.71	15.71	9.42	9.42	-7.96	-107.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	38	-3489	-2583	1407	0	-580	-7828	15.71	15.71	9.42	9.42	-25.64	1029.9
41	38	-7321	-1843	1303	0	-553	-4906	15.71	15.71	9.42	9.42	-16.61	416.7
42	38	-7343	-1902	813	0	-280	-5039	15.71	15.71	9.42	9.42	-17.05	435.3
43	38	-1258	-2643	1239	0	-500	-8567	15.71	15.71	9.42	9.42	-27.46	1250.3
44	38	-13710	-676	1174	0	-529	-228	15.71	15.71	9.42	9.42	-5.72	-78.3
45	38	-7680	-1507	248	0	-1	-3918	15.71	15.71	9.42	9.42	-13.23	261.6
46	38	-7839	-1149	923	0	-398	-2971	15.71	15.71	9.42	9.42	-9.91	132.5
47	38	-7968	-976	828	0	-360	-2488	15.71	15.71	9.42	9.42	-8.23	-110.2
49	38	-6691	-1222	863	0	-368	-3461	15.71	15.71	9.42	9.42	-11.69	234.5
50	38	-9182	-829	850	0	-374	-1794	15.71	15.71	9.42	9.42	-6.25	-86.8
51	38	-7975	-995	665	0	-269	-2532	15.71	15.71	9.42	9.42	-8.38	-112.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	50	-3389	-2583	1407	0	-756	-8151	15.71	15.71	9.42	9.42	-26.65	1084.0
41	50	-7221	-1843	1303	0	-716	-5136	15.71	15.71	9.42	9.42	-17.38	454.6
42	50	-7243	-1902	813	0	-382	-5277	15.71	15.71	9.42	9.42	-17.85	474.4
43	50	-1158	-2643	1239	0	-655	-8897	15.71	15.71	9.42	9.42	-28.47	1305.7
44	50	-13610	-676	1174	0	-675	-312	15.71	15.71	9.42	9.42	-6.24	-84.1
45	50	-7580	-1507	248	0	-32	-4107	15.71	15.71	9.42	9.42	-13.89	291.7
46	50	-7739	-1149	923	0	-514	-3115	15.71	15.71	9.42	9.42	-10.42	153.0
47	50	-7868	-976	828	0	-463	-2610	15.71	15.71	9.42	9.42	-8.65	-115.1
49	50	-6591	-1222	863	0	-476	-3614	15.71	15.71	9.42	9.42	-12.22	259.6
50	50	-9082	-829	850	0	-480	-1897	15.71	15.71	9.42	9.42	-6.49	-89.8
51	50	-7875	-995	665	0	-352	-2656	15.71	15.71	9.42	9.42	-8.81	-117.0

apost= 9.42 aant= 9.42 ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 82 NI 1351 NF 1360 SEZ. Rp B= 0.400 H= 0.600 (pilastro)
PIL. NUM. 16
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-10050	1877	541	0	1061	-5262	12.57	12.57	6.28	6.28	-34.60	940.6
41	0	-10070	958	552	0	1086	-2624	12.57	12.57	6.28	6.28	-16.44	-206.2
42	0	-10000	963	488	0	912	-2639	12.57	12.57	6.28	6.28	-16.56	-207.2
43	0	-9881	2326	524	0	1029	-6563	12.57	12.57	6.28	6.28	-43.22	1349.4
44	0	-9900	-547	552	0	1089	1700	12.57	12.57	6.28	6.28	-10.51	-139.8
45	0	-9806	803	436	0	782	-2190	12.57	12.57	6.28	6.28	-13.52	-173.8
46	0	-9827	696	538	0	1063	-1889	12.57	12.57	6.28	6.28	-11.60	-152.3
47	0	-9767	631	534	0	1057	-1705	12.57	12.57	6.28	6.28	-10.53	-139.8
49	0	-9760	937	530	0	1049	-2585	12.57	12.57	6.28	6.28	-16.23	-202.9
50	0	-9764	362	536	0	1061	-933	12.57	12.57	6.28	6.28	-9.08	-114.4

51	0	-9745	632	513	0	999	-1711	12.57	12.57	6.28	6.28	-10.56	-140.1

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	12	-9974	1877	541	0	993	-5028	12.57	12.57	6.28	6.28	-33.03	874.8
41	12	-9994	958	552	0	1017	-2504	12.57	12.57	6.28	6.28	-15.62	-197.2
42	12	-9925	963	488	0	851	-2518	12.57	12.57	6.28	6.28	-15.74	-198.2
43	12	-9806	2326	524	0	964	-6272	12.57	12.57	6.28	6.28	-41.31	1265.0
44	12	-9825	-547	552	0	1020	1632	12.57	12.57	6.28	6.28	-10.13	-135.2
45	12	-9731	803	436	0	727	-2090	12.57	12.57	6.28	6.28	-12.87	-166.4
46	12	-9752	696	538	0	996	-1802	12.57	12.57	6.28	6.28	-11.08	-146.2
47	12	-9692	631	534	0	990	-1626	12.57	12.57	6.28	6.28	-10.09	-134.5
49	12	-9685	937	530	0	983	-2468	12.57	12.57	6.28	6.28	-15.43	-194.2
50	12	-9689	362	536	0	994	-887	12.57	12.57	6.28	6.28	-8.62	-109.5
51	12	-9670	632	513	0	935	-1632	12.57	12.57	6.28	6.28	-10.11	-134.7

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	25	-9898	1877	541	0	926	-4793	12.57	12.57	6.28	6.28	-31.46	809.2
41	25	-9918	958	552	0	948	-2384	12.57	12.57	6.28	6.28	-14.81	-188.2
42	25	-9850	963	488	0	790	-2398	12.57	12.57	6.28	6.28	-14.92	-189.2
43	25	-9731	2326	524	0	898	-5982	12.57	12.57	6.28	6.28	-39.39	1180.8
44	25	-9750	-547	552	0	951	1563	12.57	12.57	6.28	6.28	-9.76	-130.7
45	25	-9656	803	436	0	673	-1989	12.57	12.57	6.28	6.28	-12.23	-159.0
46	25	-9677	696	538	0	929	-1715	12.57	12.57	6.28	6.28	-10.58	-140.2
47	25	-9617	631	534	0	924	-1548	12.57	12.57	6.28	6.28	-9.66	-129.3
49	25	-9610	937	530	0	916	-2351	12.57	12.57	6.28	6.28	-14.63	-185.4
50	25	-9614	362	536	0	927	-842	12.57	12.57	6.28	6.28	-8.18	-104.6
51	25	-9595	632	513	0	871	-1552	12.57	12.57	6.28	6.28	-9.68	-129.5

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	37	-9822	1877	541	0	858	-4558	12.57	12.57	6.28	6.28	-29.88	743.9
41	37	-9843	958	552	0	879	-2264	12.57	12.57	6.28	6.28	-14.01	-179.3
42	37	-9776	963	488	0	729	-2278	12.57	12.57	6.28	6.28	-14.11	-180.2
43	37	-9656	2326	524	0	833	-5691	12.57	12.57	6.28	6.28	-37.47	1096.9
44	37	-9675	-547	552	0	882	1494	12.57	12.57	6.28	6.28	-9.40	-126.3
45	37	-9581	803	436	0	618	-1888	12.57	12.57	6.28	6.28	-11.60	-151.7
46	37	-9602	696	538	0	861	-1628	12.57	12.57	6.28	6.28	-10.08	-134.3
47	37	-9542	631	534	0	857	-1469	12.57	12.57	6.28	6.28	-9.24	-124.2
49	37	-9535	937	530	0	850	-2234	12.57	12.57	6.28	6.28	-13.85	-176.7
50	37	-9539	362	536	0	860	-797	12.57	12.57	6.28	6.28	-7.76	-100.0
51	37	-9520	632	513	0	807	-1473	12.57	12.57	6.28	6.28	-9.26	-124.4

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	50	-9746	1877	541	0	790	-4324	12.57	12.57	6.28	6.28	-28.30	679.0
41	50	-9767	958	552	0	810	-2144	12.57	12.57	6.28	6.28	-13.22	-170.4
42	50	-9701	963	488	0	668	-2157	12.57	12.57	6.28	6.28	-13.31	-171.2
43	50	-9581	2326	524	0	767	-5400	12.57	12.57	6.28	6.28	-35.54	1013.1
44	50	-9600	-547	552	0	813	1426	12.57	12.57	6.28	6.28	-9.05	-122.0
45	50	-9506	803	436	0	564	-1788	12.57	12.57	6.28	6.28	-10.99	-144.6
46	50	-9527	696	538	0	794	-1541	12.57	12.57	6.28	6.28	-9.61	-128.6
47	50	-9467	631	534	0	790	-1390	12.57	12.57	6.28	6.28	-8.84	-119.3
49	50	-9460	937	530	0	784	-2117	12.57	12.57	6.28	6.28	-13.07	-168.0
50	50	-9464	362	536	0	793	-751	12.57	12.57	6.28	6.28	-7.35	-95.4
51	50	-9445	632	513	0	743	-1394	12.57	12.57	6.28	6.28	-8.86	-119.5

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

ASTA NUM. 83 NI 1360 NF 170 SEZ. Rp B= 0.400 H= 0.600 (pilastro)
PIL. NUM. 16A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-9746	1877	541	0	790	-4324	12.57	12.57	6.28	6.28	-28.30	679.0
41	0	-9767	958	552	0	810	-2144	12.57	12.57	6.28	6.28	-13.22	-170.4
42	0	-9701	963	488	0	668	-2157	12.57	12.57	6.28	6.28	-13.31	-171.2
43	0	-9581	2326	524	0	767	-5400	12.57	12.57	6.28	6.28	-35.54	1013.1
44	0	-9600	-547	552	0	813	1426	12.57	12.57	6.28	6.28	-9.05	-122.0
45	0	-9506	803	436	0	564	-1788	12.57	12.57	6.28	6.28	-10.99	-144.6
46	0	-9527	696	538	0	794	-1541	12.57	12.57	6.28	6.28	-9.61	-128.6
47	0	-9467	631	534	0	790	-1390	12.57	12.57	6.28	6.28	-8.84	-119.3
49	0	-9460	937	530	0	784	-2117	12.57	12.57	6.28	6.28	-13.07	-168.0
50	0	-9464	362	536	0	793	-751	12.57	12.57	6.28	6.28	-7.35	-95.4
51	0	-9445	632	513	0	743	-1394	12.57	12.57	6.28	6.28	-8.86	-119.5

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	12	-9671	1877	541	0	723	-4089	12.57	12.57	6.28	6.28	-26.71	614.6
41	12	-9692	958	552	0	741	-2024	12.57	12.57	6.28	6.28	-12.45	-161.6
42	12	-9626	963	488	0	607	-2037	12.57	12.57	6.28	6.28	-12.53	-162.4
43	12	-9506	2326	524	0	702	-5109	12.57	12.57	6.28	6.28	-33.61	929.7
44	12	-9525	-547	552	0	744	1358	12.57	12.57	6.28	6.28	-8.71	-117.8
45	12	-9431	803	436	0	510	-1688	12.57	12.57	6.28	6.28	-10.40	-137.7
46	12	-9452	696	538	0	727	-1454	12.57	12.57	6.28	6.28	-9.15	-123.0
47	12	-9392	631	534	0	723	-1311	12.57	12.57	6.28	6.28	-8.46	-114.6
49	12	-9385	937	530	0	717	-2000	12.57	12.57	6.28	6.28	-12.31	-159.3
50	12	-9389	362	536	0	726	-706	12.57	12.57	6.28	6.28	-6.97	-91.1
51	12	-9370	632	513	0	679	-1315	12.57	12.57	6.28	6.28	-8.47	-114.7

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	25	-9596	1877	541	0	655	-3854	12.57	12.57	6.28	6.28	-25.11	550.7
41	25	-9617	958	552	0	672	-1904	12.57	12.57	6.28	6.28	-11.70	-152.9
42	25	-9551	963	488	0	546	-1916	12.57	12.57	6.28	6.28	-11.77	-153.7
43	25	-9431	2326	524	0	636	-4818	12.57	12.57	6.28	6.28	-31.67	846.6
44	25	-9450	-547	552	0	675	1290	12.57	12.57	6.28	6.28	-8.38	-113.7
45	25	-9356	803	436	0	455	-1588	12.57	12.57	6.28	6.28	-9.83	-130.9
46	25	-9377	696	538	0	660	-1367	12.57	12.57	6.28	6.28	-8.71	-117.7
47	25	-9317	631	534	0	657	-1232	12.57	12.57	6.28	6.28	-8.09	-110.0
49	25	-9310	937	530	0	651	-1882	12.57	12.57	6.28	6.28	-11.57	-150.8
50	25	-9314	362	536	0	659	-661	12.57	12.57	6.28	6.28	-6.61	-86.9
51	25	-9295	632	513	0	615	-1236	12.57	12.57	6.28	6.28	-8.10	-110.1

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	38	-9521	1877	541	0	587	-3620	12.57	12.57	6.28	6.28	-23.50	487.6
41	38	-9542	958	552	0	603	-1785	12.57	12.57	6.28	6.28	-10.97	-144.5
42	38	-9476	963	488	0	485	-1796	12.57	12.57	6.28	6.28	-11.04	-145.1
43	38	-9356	2326	524	0	571	-4528	12.57	12.57	6.28	6.28	-29.72	764.0
44	38	-9375	-547	552	0	606	1221	12.57	12.57	6.28	6.28	-8.06	-109.7
45	38	-9281	803	436	0	400	-1487	12.57	12.57	6.28	6.28	-9.29	-124.4
46	38	-9302	696	538	0	592	-1280	12.57	12.57	6.28	6.28	-8.30	-112.5
47	38	-9242	631	534	0	590	-1154	12.57	12.57	6.28	6.28	-7.74	-105.6
49	38	-9235	937	530	0	585	-1765	12.57	12.57	6.28	6.28	-10.84	-142.4
50	38	-9239	362	536	0	592	-615	12.57	12.57	6.28	6.28	-6.25	-82.8
51	38	-9220	632	513	0	551	-1157	12.57	12.57	6.28	6.28	-7.75	-105.7

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	50	-9446	1877	541	0	520	-3385	12.57	12.57	6.28	6.28	-21.89	425.4
41	50	-9467	958	552	0	534	-1665	12.57	12.57	6.28	6.28	-10.27	-136.3
42	50	-9401	963	488	0	424	-1676	12.57	12.57	6.28	6.28	-10.33	-136.8
43	50	-9281	2326	524	0	505	-4237	12.57	12.57	6.28	6.28	-27.76	682.0
44	50	-9300	-547	552	0	538	1153	12.57	12.57	6.28	6.28	-7.76	-105.9
45	50	-9206	803	436	0	346	-1387	12.57	12.57	6.28	6.28	-8.77	-118.1
46	50	-9227	696	538	0	525	-1193	12.57	12.57	6.28	6.28	-7.90	-107.5
47	50	-9167	631	534	0	523	-1075	12.57	12.57	6.28	6.28	-7.40	-101.4
49	50	-9160	937	530	0	518	-1648	12.57	12.57	6.28	6.28	-10.15	-134.3
50	50	-9164	362	536	0	525	-570	12.57	12.57	6.28	6.28	-5.89	-78.7
51	50	-9145	632	513	0	487	-1078	12.57	12.57	6.28	6.28	-7.41	-101.4

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

ASTA NUM. 84 NI 1037 NF 300 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 15A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-32630	686	532	0	756	-1585	6.28	6.28	12.57	12.57	-19.58	-264.3
41	0	-32210	133	520	0	778	-242	6.28	6.28	12.57	12.57	-15.23	-221.5
42	0	-32070	136	335	0	419	-248	6.28	6.28	12.57	12.57	-13.89	-204.6
43	0	-31220	1042	502	0	733	-2463	6.28	6.28	12.57	12.57	-23.44	-305.8
44	0	-31210	-786	486	0	773	1993	6.28	6.28	12.57	12.57	-21.09	-279.4
45	0	-30280	126	174	0	171	-235	6.28	6.28	12.57	12.57	-12.31	-183.1
46	0	-29480	114	460	0	763	-214	6.28	6.28	12.57	12.57	-14.12	-205.0
47	0	-28800	109	445	0	759	-207	6.28	6.28	12.57	12.57	-13.85	-200.9
49	0	-28950	293	449	0	752	-655	6.28	6.28	12.57	12.57	-13.88	-201.4
50	0	-28940	-72	446	0	760	237	6.28	6.28	12.57	12.57	-13.90	-201.7
51	0	-28760	110	383	0	640	-209	6.28	6.28	12.57	12.57	-13.40	-195.3

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	12	-32555	686	532	0	690	-1499	6.28	6.28	12.57	12.57	-19.13	-259.2
41	12	-32135	133	520	0	713	-225	6.28	6.28	12.57	12.57	-14.97	-218.1
42	12	-31995	136	335	0	377	-231	6.28	6.28	12.57	12.57	-13.71	-202.3
43	12	-31145	1042	502	0	670	-2333	6.28	6.28	12.57	12.57	-22.74	-297.9
44	12	-31135	-786	486	0	712	1895	6.28	6.28	12.57	12.57	-20.57	-273.5
45	12	-30205	126	174	0	149	-219	6.28	6.28	12.57	12.57	-12.20	-181.7
46	12	-29405	114	460	0	706	-200	6.28	6.28	12.57	12.57	-13.89	-202.0
47	12	-28725	109	445	0	704	-193	6.28	6.28	12.57	12.57	-13.62	-198.0
49	12	-28875	293	449	0	696	-618	6.28	6.28	12.57	12.57	-13.65	-198.5
50	12	-28865	-72	446	0	705	228	6.28	6.28	12.57	12.57	-13.67	-198.8
51	12	-28685	110	383	0	592	-195	6.28	6.28	12.57	12.57	-13.20	-192.7

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	25	-32480	686	532	0	623	-1414	6.28	6.28	12.57	12.57	-18.68	-254.0
41	25	-32060	133	520	0	648	-208	6.28	6.28	12.57	12.57	-14.70	-214.8
42	25	-31920	136	335	0	335	-214	6.28	6.28	12.57	12.57	-13.53	-200.0
43	25	-31070	1042	502	0	607	-2202	6.28	6.28	12.57	12.57	-22.07	-290.2
44	25	-31060	-786	486	0	651	1796	6.28	6.28	12.57	12.57	-20.06	-267.6
45	25	-30130	126	174	0	128	-203	6.28	6.28	12.57	12.57	-12.10	-180.3
46	25	-29330	114	460	0	648	-185	6.28	6.28	12.57	12.57	-13.65	-199.0
47	25	-28650	109	445	0	648	-180	6.28	6.28	12.57	12.57	-13.39	-195.0
49	25	-28800	293	449	0	640	-581	6.28	6.28	12.57	12.57	-13.42	-195.5
50	25	-28790	-72	446	0	649	218	6.28	6.28	12.57	12.57	-13.45	-195.9
51	25	-28610	110	383	0	544	-181	6.28	6.28	12.57	12.57	-13.00	-190.1

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	38	-32405	686	532	0	557	-1328	6.28	6.28	12.57	12.57	-18.23	-248.8
41	38	-31985	133	520	0	583	-192	6.28	6.28	12.57	12.57	-14.44	-211.4
42	38	-31845	136	335	0	294	-197	6.28	6.28	12.57	12.57	-13.35	-197.7
43	38	-30995	1042	502	0	544	-2072	6.28	6.28	12.57	12.57	-21.40	-282.6
44	38	-30985	-786	486	0	590	1698	6.28	6.28	12.57	12.57	-19.55	-261.8
45	38	-30055	126	174	0	106	-188	6.28	6.28	12.57	12.57	-11.99	-178.9
46	38	-29255	114	460	0	591	-171	6.28	6.28	12.57	12.57	-13.42	-196.0
47	38	-28575	109	445	0	593	-166	6.28	6.28	12.57	12.57	-13.16	-192.1
49	38	-28725	293	449	0	584	-545	6.28	6.28	12.57	12.57	-13.19	-192.6
50	38	-28715	-72	446	0	593	209	6.28	6.28	12.57	12.57	-13.22	-192.9
51	38	-28535	110	383	0	496	-168	6.28	6.28	12.57	12.57	-12.80	-187.6

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	50	-32330	686	532	0	490	-1242	6.28	6.28	12.57	12.57	-17.78	-243.7
41	50	-31910	133	520	0	518	-175	6.28	6.28	12.57	12.57	-14.18	-208.1
42	50	-31770	136	335	0	252	-180	6.28	6.28	12.57	12.57	-13.17	-195.4
43	50	-30920	1042	502	0	482	-1942	6.28	6.28	12.57	12.57	-20.73	-275.0
44	50	-30910	-786	486	0	530	1600	6.28	6.28	12.57	12.57	-19.04	-255.9
45	50	-29980	126	174	0	84	-172	6.28	6.28	12.57	12.57	-11.88	-177.5
46	50	-29180	114	460	0	533	-157	6.28	6.28	12.57	12.57	-13.18	-193.0
47	50	-28500	109	445	0	537	-152	6.28	6.28	12.57	12.57	-12.93	-189.2
49	50	-28650	293	449	0	528	-508	6.28	6.28	12.57	12.57	-12.96	-189.6
50	50	-28640	-72	446	0	537	200	6.28	6.28	12.57	12.57	-12.99	-190.0
51	50	-28460	110	383	0	448	-154	6.28	6.28	12.57	12.57	-12.60	-185.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 85 NI 1033 NF 1037 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 15
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-32930	686	532	0	1022	-1928	6.28	6.28	12.57	12.57	-21.38	-285.0
41	0	-32510	133	520	0	1037	-308	6.28	6.28	12.57	12.57	-16.27	-234.8
42	0	-32370	136	335	0	586	-316	6.28	6.28	12.57	12.57	-14.61	-213.8
43	0	-31520	1042	502	0	984	-2984	6.28	6.28	12.57	12.57	-26.48	-339.5
44	0	-31510	-786	486	0	1015	2385	6.28	6.28	12.57	12.57	-23.14	-302.8
45	0	-30580	126	174	0	258	-298	6.28	6.28	12.57	12.57	-12.74	-188.8
46	0	-29780	114	460	0	993	-271	6.28	6.28	12.57	12.57	-15.06	-217.0
47	0	-29100	109	445	0	982	-261	6.28	6.28	12.57	12.57	-14.76	-212.6
49	0	-29250	293	449	0	977	-801	6.28	6.28	12.57	12.57	-14.80	-213.2
50	0	-29240	-72	446	0	983	273	6.28	6.28	12.57	12.57	-14.82	-213.4
51	0	-29060	110	383	0	832	-264	6.28	6.28	12.57	12.57	-14.20	-205.6

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	12	-32855	686	532	0	956	-1842	6.28	6.28	12.57	12.57	-20.93	-279.9
41	12	-32435	133	520	0	972	-291	6.28	6.28	12.57	12.57	-16.01	-231.5
42	12	-32295	136	335	0	545	-299	6.28	6.28	12.57	12.57	-14.43	-211.5
43	12	-31445	1042	502	0	921	-2854	6.28	6.28	12.57	12.57	-25.68	-330.7
44	12	-31435	-786	486	0	954	2287	6.28	6.28	12.57	12.57	-22.62	-296.9
45	12	-30505	126	174	0	236	-282	6.28	6.28	12.57	12.57	-12.63	-187.4
46	12	-29705	114	460	0	936	-256	6.28	6.28	12.57	12.57	-14.83	-214.0
47	12	-29025	109	445	0	926	-248	6.28	6.28	12.57	12.57	-14.53	-209.7
49	12	-29175	293	449	0	921	-765	6.28	6.28	12.57	12.57	-14.57	-210.3
50	12	-29165	-72	446	0	927	264	6.28	6.28	12.57	12.57	-14.59	-210.5
51	12	-28985	110	383	0	784	-250	6.28	6.28	12.57	12.57	-14.00	-203.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	25	-32780	686	532	0	889	-1756	6.28	6.28	12.57	12.57	-20.48	-274.7
41	25	-32360	133	520	0	907	-275	6.28	6.28	12.57	12.57	-15.75	-228.1
42	25	-32220	136	335	0	503	-282	6.28	6.28	12.57	12.57	-14.25	-209.2
43	25	-31370	1042	502	0	858	-2724	6.28	6.28	12.57	12.57	-24.91	-322.2
44	25	-31360	-786	486	0	894	2189	6.28	6.28	12.57	12.57	-22.11	-291.1
45	25	-30430	126	174	0	215	-266	6.28	6.28	12.57	12.57	-12.52	-185.9
46	25	-29630	114	460	0	878	-242	6.28	6.28	12.57	12.57	-14.59	-211.0
47	25	-28950	109	445	0	871	-234	6.28	6.28	12.57	12.57	-14.30	-206.7
49	25	-29100	293	449	0	864	-728	6.28	6.28	12.57	12.57	-14.34	-207.3
50	25	-29090	-72	446	0	872	255	6.28	6.28	12.57	12.57	-14.36	-207.6
51	25	-28910	110	383	0	736	-236	6.28	6.28	12.57	12.57	-13.80	-200.5

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	38	-32705	686	532	0	822	-1671	6.28	6.28	12.57	12.57	-20.03	-269.5
41	38	-32285	133	520	0	842	-258	6.28	6.28	12.57	12.57	-15.49	-224.8
42	38	-32145	136	335	0	461	-265	6.28	6.28	12.57	12.57	-14.07	-206.9
43	38	-31295	1042	502	0	795	-2593	6.28	6.28	12.57	12.57	-24.16	-313.9
44	38	-31285	-786	486	0	833	2091	6.28	6.28	12.57	12.57	-21.60	-285.2
45	38	-30355	126	174	0	193	-251	6.28	6.28	12.57	12.57	-12.42	-184.5
46	38	-29555	114	460	0	821	-228	6.28	6.28	12.57	12.57	-14.36	-208.0
47	38	-28875	109	445	0	815	-220	6.28	6.28	12.57	12.57	-14.07	-203.8
49	38	-29025	293	449	0	808	-691	6.28	6.28	12.57	12.57	-14.11	-204.4
50	38	-29015	-72	446	0	816	246	6.28	6.28	12.57	12.57	-14.13	-204.7
51	38	-28835	110	383	0	688	-223	6.28	6.28	12.57	12.57	-13.60	-197.9

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	50	-32630	686	532	0	756	-1585	6.28	6.28	12.57	12.57	-19.58	-264.3
41	50	-32210	133	520	0	778	-242	6.28	6.28	12.57	12.57	-15.23	-221.5
42	50	-32070	136	335	0	419	-248	6.28	6.28	12.57	12.57	-13.89	-204.6
43	50	-31220	1042	502	0	733	-2463	6.28	6.28	12.57	12.57	-23.44	-305.8
44	50	-31210	-786	486	0	773	1993	6.28	6.28	12.57	12.57	-21.09	-279.4
45	50	-30280	126	174	0	171	-235	6.28	6.28	12.57	12.57	-12.31	-183.1
46	50	-29480	114	460	0	763	-214	6.28	6.28	12.57	12.57	-14.12	-205.0
47	50	-28800	109	445	0	759	-207	6.28	6.28	12.57	12.57	-13.85	-200.9
49	50	-28950	293	449	0	752	-655	6.28	6.28	12.57	12.57	-13.88	-201.4
50	50	-28940	-72	446	0	760	237	6.28	6.28	12.57	12.57	-13.90	-201.7
51	50	-28760	110	383	0	640	-209	6.28	6.28	12.57	12.57	-13.40	-195.3

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 86 NI 1255 NF 1262 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 14
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-16660	163	-481	0	-1277	-584	6.28	6.28	12.57	12.57	-11.01	-153.7
41	0	-16620	4	-434	0	-1162	6	6.28	6.28	12.57	12.57	-10.58	-148.3
42	0	-16570	5	-570	0	-1531	1	6.28	6.28	12.57	12.57	-11.88	-164.5
43	0	-16080	274	-434	0	-1157	-996	6.28	6.28	12.57	12.57	-10.71	-145.0
44	0	-16020	-262	-374	0	-1011	992	6.28	6.28	12.57	12.57	-10.67	-141.6
45	0	-15920	11	-582	0	-1580	-20	6.28	6.28	12.57	12.57	-11.81	-163.0
46	0	-15630	12	-309	0	-846	-23	6.28	6.28	12.57	12.57	-9.07	-128.4
47	0	-15390	14	-277	0	-767	-30	6.28	6.28	12.57	12.57	-8.69	-123.5
49	0	-15400	67	-293	0	-805	-227	6.28	6.28	12.57	12.57	-8.83	-125.3
50	0	-15390	-40	-281	0	-776	170	6.28	6.28	12.57	12.57	-8.72	-123.9
51	0	-15370	15	-322	0	-890	-32	6.28	6.28	12.57	12.57	-9.12	-128.9

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	12	-16585	163	-481	0	-1217	-564	6.28	6.28	12.57	12.57	-10.76	-150.6
41	12	-16545	4	-434	0	-1108	6	6.28	6.28	12.57	12.57	-10.36	-145.5

42	12	-16495	5	-570	0	-1460	2	6.28	6.28	12.57	12.57	-11.60	-160.9
43	12	-16005	274	-434	0	-1103	-961	6.28	6.28	12.57	12.57	-10.51	-142.1
44	12	-15945	-262	-374	0	-964	959	6.28	6.28	12.57	12.57	-10.48	-139.4
45	12	-15845	11	-582	0	-1507	-18	6.28	6.28	12.57	12.57	-11.52	-159.3
46	12	-15555	12	-309	0	-807	-22	6.28	6.28	12.57	12.57	-8.90	-126.3
47	12	-15315	14	-277	0	-732	-28	6.28	6.28	12.57	12.57	-8.54	-121.5
49	12	-15325	67	-293	0	-769	-218	6.28	6.28	12.57	12.57	-8.67	-123.2
50	12	-15315	-40	-281	0	-741	166	6.28	6.28	12.57	12.57	-8.57	-121.9
51	12	-15295	15	-322	0	-850	-30	6.28	6.28	12.57	12.57	-8.95	-126.7

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	25	-16510	163	-481	0	-1157	-544	6.28	6.28	12.57	12.57	-10.52	-147.5
41	25	-16470	4	-434	0	-1054	7	6.28	6.28	12.57	12.57	-10.14	-142.6
42	25	-16420	5	-570	0	-1389	3	6.28	6.28	12.57	12.57	-11.32	-157.3
43	25	-15930	274	-434	0	-1048	-927	6.28	6.28	12.57	12.57	-10.32	-139.2
44	25	-15870	-262	-374	0	-917	926	6.28	6.28	12.57	12.57	-10.29	-137.2
45	25	-15770	11	-582	0	-1434	-17	6.28	6.28	12.57	12.57	-11.23	-155.6
46	25	-15480	12	-309	0	-769	-20	6.28	6.28	12.57	12.57	-8.73	-124.1
47	25	-15240	14	-277	0	-697	-27	6.28	6.28	12.57	12.57	-8.38	-119.5
49	25	-15250	67	-293	0	-732	-210	6.28	6.28	12.57	12.57	-8.51	-121.1
50	25	-15240	-40	-281	0	-706	160	6.28	6.28	12.57	12.57	-8.41	-119.9
51	25	-15220	15	-322	0	-809	-28	6.28	6.28	12.57	12.57	-8.78	-124.4

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	38	-16435	163	-481	0	-1097	-523	6.28	6.28	12.57	12.57	-10.28	-144.3
41	38	-16395	4	-434	0	-999	7	6.28	6.28	12.57	12.57	-9.91	-139.7
42	38	-16345	5	-570	0	-1318	3	6.28	6.28	12.57	12.57	-11.03	-153.7
43	38	-15855	274	-434	0	-994	-893	6.28	6.28	12.57	12.57	-10.12	-136.4
44	38	-15795	-262	-374	0	-870	893	6.28	6.28	12.57	12.57	-10.10	-135.0
45	38	-15695	11	-582	0	-1362	-15	6.28	6.28	12.57	12.57	-10.94	-151.9
46	38	-15405	12	-309	0	-730	-18	6.28	6.28	12.57	12.57	-8.57	-121.9
47	38	-15165	14	-277	0	-663	-25	6.28	6.28	12.57	12.57	-8.23	-117.5
49	38	-15175	67	-293	0	-695	-202	6.28	6.28	12.57	12.57	-8.35	-119.1
50	38	-15165	-40	-281	0	-671	156	6.28	6.28	12.57	12.57	-8.26	-117.9
51	38	-15145	15	-322	0	-769	-26	6.28	6.28	12.57	12.57	-8.60	-122.2

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	50	-16360	163	-481	0	-1037	-503	6.28	6.28	12.57	12.57	-10.03	-141.2
41	50	-16320	4	-434	0	-945	8	6.28	6.28	12.57	12.57	-9.69	-136.9
42	50	-16270	5	-570	0	-1247	4	6.28	6.28	12.57	12.57	-10.75	-150.1
43	50	-15780	274	-434	0	-940	-858	6.28	6.28	12.57	12.57	-9.92	-133.5
44	50	-15720	-262	-374	0	-824	860	6.28	6.28	12.57	12.57	-9.91	-132.7
45	50	-15620	11	-582	0	-1289	-14	6.28	6.28	12.57	12.57	-10.65	-148.2
46	50	-15330	12	-309	0	-692	-17	6.28	6.28	12.57	12.57	-8.40	-119.8
47	50	-15090	14	-277	0	-628	-23	6.28	6.28	12.57	12.57	-8.08	-115.6
49	50	-15100	67	-293	0	-659	-193	6.28	6.28	12.57	12.57	-8.19	-117.0
50	50	-15090	-40	-281	0	-636	150	6.28	6.28	12.57	12.57	-8.11	-115.9
51	50	-15070	15	-322	0	-729	-24	6.28	6.28	12.57	12.57	-8.43	-119.9

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 87 NI 1262 NF 128 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 14A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	--												
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-16360	163	-481	0	-1037	-503	6.28	6.28	12.57	12.57	-10.03	-141.2
41	0	-16320	4	-434	0	-945	8	6.28	6.28	12.57	12.57	-9.69	-136.9
42	0	-16270	5	-570	0	-1247	4	6.28	6.28	12.57	12.57	-10.75	-150.1
43	0	-15780	274	-434	0	-940	-858	6.28	6.28	12.57	12.57	-9.92	-133.5
44	0	-15720	-262	-374	0	-824	860	6.28	6.28	12.57	12.57	-9.91	-132.7
45	0	-15620	11	-582	0	-1289	-14	6.28	6.28	12.57	12.57	-10.65	-148.2
46	0	-15330	12	-309	0	-692	-17	6.28	6.28	12.57	12.57	-8.40	-119.8
47	0	-15090	14	-277	0	-628	-23	6.28	6.28	12.57	12.57	-8.08	-115.6
49	0	-15100	67	-293	0	-659	-193	6.28	6.28	12.57	12.57	-8.19	-117.0
50	0	-15090	-40	-281	0	-636	150	6.28	6.28	12.57	12.57	-8.11	-115.9
51	0	-15070	15	-322	0	-729	-24	6.28	6.28	12.57	12.57	-8.43	-119.9

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	12	-16285	163	-481	0	-977	-482	6.28	6.28	12.57	12.57	-9.79	-138.1
41	12	-16245	4	-434	0	-891	8	6.28	6.28	12.57	12.57	-9.47	-134.0
42	12	-16195	5	-570	0	-1176	5	6.28	6.28	12.57	12.57	-10.47	-146.5
43	12	-15705	274	-434	0	-886	-824	6.28	6.28	12.57	12.57	-9.73	-130.6
44	12	-15645	-262	-374	0	-777	828	6.28	6.28	12.57	12.57	-9.72	-130.5
45	12	-15545	11	-582	0	-1216	-13	6.28	6.28	12.57	12.57	-10.36	-144.5
46	12	-15255	12	-309	0	-653	-15	6.28	6.28	12.57	12.57	-8.23	-117.6
47	12	-15015	14	-277	0	-593	-21	6.28	6.28	12.57	12.57	-7.93	-113.6
49	12	-15025	67	-293	0	-622	-185	6.28	6.28	12.57	12.57	-8.03	-114.9
50	12	-15015	-40	-281	0	-600	146	6.28	6.28	12.57	12.57	-7.95	-113.9
51	12	-14995	15	-322	0	-688	-23	6.28	6.28	12.57	12.57	-8.26	-117.7

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	25	-16210	163	-481	0	-917	-462	6.28	6.28	12.57	12.57	-9.55	-135.0
41	25	-16170	4	-434	0	-837	9	6.28	6.28	12.57	12.57	-9.24	-131.1
42	25	-16120	5	-570	0	-1104	5	6.28	6.28	12.57	12.57	-10.18	-142.8
43	25	-15630	274	-434	0	-831	-790	6.28	6.28	12.57	12.57	-9.53	-128.3
44	25	-15570	-262	-374	0	-730	795	6.28	6.28	12.57	12.57	-9.53	-128.3
45	25	-15470	11	-582	0	-1144	-11	6.28	6.28	12.57	12.57	-10.07	-140.8
46	25	-15180	12	-309	0	-614	-14	6.28	6.28	12.57	12.57	-8.06	-115.5
47	25	-14940	14	-277	0	-559	-20	6.28	6.28	12.57	12.57	-7.77	-111.6
49	25	-14950	67	-293	0	-586	-176	6.28	6.28	12.57	12.57	-7.87	-112.8
50	25	-14940	-40	-281	0	-565	140	6.28	6.28	12.57	12.57	-7.80	-111.9
51	25	-14920	15	-322	0	-648	-21	6.28	6.28	12.57	12.57	-8.08	-115.5

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	38	-16135	163	-481	0	-857	-441	6.28	6.28	12.57	12.57	-9.30	-131.8
41	38	-16095	4	-434	0	-782	9	6.28	6.28	12.57	12.57	-9.02	-128.3
42	38	-16045	5	-570	0	-1033	6	6.28	6.28	12.57	12.57	-9.90	-139.2

43	38	-15555	274	-434	0	-777	-756	6.28	6.28	12.57	12.57	-9.33	-126.0
44	38	-15495	-262	-374	0	-683	762	6.28	6.28	12.57	12.57	-9.35	-126.1
45	38	-15395	11	-582	0	-1071	-10	6.28	6.28	12.57	12.57	-9.78	-137.1
46	38	-15105	12	-309	0	-576	-12	6.28	6.28	12.57	12.57	-7.90	-113.3
47	38	-14865	14	-277	0	-524	-18	6.28	6.28	12.57	12.57	-7.62	-109.6
49	38	-14875	67	-293	0	-549	-168	6.28	6.28	12.57	12.57	-7.71	-110.8
50	38	-14865	-40	-281	0	-530	136	6.28	6.28	12.57	12.57	-7.64	-109.9
51	38	-14845	15	-322	0	-608	-19	6.28	6.28	12.57	12.57	-7.91	-113.2

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	50	-16060	163	-481	0	-797	-421	6.28	6.28	12.57	12.57	-9.06	-128.7
41	50	-16020	4	-434	0	-728	10	6.28	6.28	12.57	12.57	-8.80	-125.4
42	50	-15970	5	-570	0	-962	7	6.28	6.28	12.57	12.57	-9.61	-135.6
43	50	-15480	274	-434	0	-723	-721	6.28	6.28	12.57	12.57	-9.14	-123.7
44	50	-15420	-262	-374	0	-636	730	6.28	6.28	12.57	12.57	-9.16	-123.8
45	50	-15320	11	-582	0	-998	-8	6.28	6.28	12.57	12.57	-9.49	-133.4
46	50	-15030	12	-309	0	-537	-11	6.28	6.28	12.57	12.57	-7.73	-111.1
47	50	-14790	14	-277	0	-490	-16	6.28	6.28	12.57	12.57	-7.47	-107.6
49	50	-14800	67	-293	0	-512	-160	6.28	6.28	12.57	12.57	-7.55	-108.7
50	50	-14790	-40	-281	0	-495	130	6.28	6.28	12.57	12.57	-7.49	-107.9
51	50	-14770	15	-322	0	-567	-17	6.28	6.28	12.57	12.57	-7.74	-111.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 88 NI 1168 NF 211 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 13A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-5619	-374	258	0	-1022	-12	6.28	6.28	9.42	9.42	-7.96	-105.6
41	0	-5610	-83	238	0	-983	-5	6.28	6.28	9.42	9.42	-7.70	-102.5
42	0	-5655	-88	302	0	-1120	-6	6.28	6.28	9.42	9.42	-8.66	-113.8
43	0	-5480	-582	239	0	-954	-16	6.28	6.28	9.42	9.42	-7.48	-99.7
44	0	-5469	404	206	0	-899	5	6.28	6.28	9.42	9.42	-7.12	-95.3
45	0	-5540	-106	312	0	-1119	-6	6.28	6.28	9.42	9.42	-8.64	-113.3
46	0	-5378	-105	186	0	-834	-6	6.28	6.28	9.42	9.42	-6.69	-90.1
47	0	-5320	-110	173	0	-797	-6	6.28	6.28	9.42	9.42	-6.45	-87.1
49	0	-5323	-208	180	0	-810	-8	6.28	6.28	9.42	9.42	-6.53	-88.0
50	0	-5321	-10	173	0	-799	-3	6.28	6.28	9.42	9.42	-6.46	-87.2
51	0	-5335	-112	194	0	-843	-6	6.28	6.28	9.42	9.42	-6.73	-90.5

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	12	-5563	-374	258	0	-1054	-59	6.28	6.28	9.42	9.42	-8.18	-108.0
41	12	-5554	-83	238	0	-1013	-16	6.28	6.28	9.42	9.42	-7.89	-104.6
42	12	-5599	-88	302	0	-1158	-17	6.28	6.28	9.42	9.42	-8.93	-116.7
43	12	-5424	-582	239	0	-984	-89	6.28	6.28	9.42	9.42	-7.67	-101.8
44	12	-5413	404	206	0	-925	56	6.28	6.28	9.42	9.42	-7.27	-97.0
45	12	-5484	-106	312	0	-1158	-19	6.28	6.28	9.42	9.42	-8.92	-116.4
46	12	-5322	-105	186	0	-857	-19	6.28	6.28	9.42	9.42	-6.82	-91.5
47	12	-5264	-110	173	0	-819	-19	6.28	6.28	9.42	9.42	-6.56	-88.3
49	12	-5267	-208	180	0	-832	-34	6.28	6.28	9.42	9.42	-6.65	-89.3
50	12	-5265	-10	173	0	-820	-5	6.28	6.28	9.42	9.42	-6.57	-88.4
51	12	-5279	-112	194	0	-867	-20	6.28	6.28	9.42	9.42	-6.87	-92.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	25	-5506	-374	258	0	-1086	-105	6.28	6.28	9.42	9.42	-8.40	-110.4
41	25	-5498	-83	238	0	-1042	-26	6.28	6.28	9.42	9.42	-8.09	-106.8
42	25	-5542	-88	302	0	-1196	-28	6.28	6.28	9.42	9.42	-9.21	-119.8
43	25	-5368	-582	239	0	-1014	-162	6.28	6.28	9.42	9.42	-7.87	-104.0
44	25	-5356	404	206	0	-950	106	6.28	6.28	9.42	9.42	-7.43	-98.8
45	25	-5428	-106	312	0	-1197	-33	6.28	6.28	9.42	9.42	-9.22	-119.5
46	25	-5266	-105	186	0	-881	-32	6.28	6.28	9.42	9.42	-6.95	-92.9
47	25	-5208	-110	173	0	-840	-33	6.28	6.28	9.42	9.42	-6.68	-89.6
49	25	-5210	-208	180	0	-855	-60	6.28	6.28	9.42	9.42	-6.77	-90.7
50	25	-5208	-10	173	0	-842	-6	6.28	6.28	9.42	9.42	-6.69	-89.7
51	25	-5222	-112	194	0	-891	-34	6.28	6.28	9.42	9.42	-7.01	-93.6

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	38	-5450	-374	258	0	-1119	-152	6.28	6.28	9.42	9.42	-8.63	-112.9
41	38	-5441	-83	238	0	-1072	-37	6.28	6.28	9.42	9.42	-8.29	-109.0
42	38	-5486	-88	302	0	-1234	-39	6.28	6.28	9.42	9.42	-9.50	-122.9
43	38	-5311	-582	239	0	-1044	-234	6.28	6.28	9.42	9.42	-8.07	-106.2
44	38	-5300	404	206	0	-976	157	6.28	6.28	9.42	9.42	-7.59	-100.6
45	38	-5371	-106	312	0	-1236	-46	6.28	6.28	9.42	9.42	-9.51	-122.7
46	38	-5209	-105	186	0	-904	-45	6.28	6.28	9.42	9.42	-7.09	-94.5
47	38	-5151	-110	173	0	-862	-47	6.28	6.28	9.42	9.42	-6.80	-91.0
49	38	-5154	-208	180	0	-877	-86	6.28	6.28	9.42	9.42	-6.90	-92.1
50	38	-5152	-10	173	0	-864	-7	6.28	6.28	9.42	9.42	-6.81	-91.1
51	38	-5166	-112	194	0	-916	-48	6.28	6.28	9.42	9.42	-7.16	-95.2

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	50	-5394	-374	258	0	-1151	-199	6.28	6.28	9.42	9.42	-8.87	-115.5
41	50	-5385	-83	238	0	-1102	-47	6.28	6.28	9.42	9.42	-8.50	-111.3
42	50	-5430	-88	302	0	-1272	-50	6.28	6.28	9.42	9.42	-9.79	-126.0
43	50	-5255	-582	239	0	-1074	-307	6.28	6.28	9.42	9.42	-8.29	-108.5
44	50	-5244	404	206	0	-1002	207	6.28	6.28	9.42	9.42	-7.77	-102.5
45	50	-5315	-106	312	0	-1275	-59	6.28	6.28	9.42	9.42	-9.82	-125.9
46	50	-5153	-105	186	0	-927	-58	6.28	6.28	9.42	9.42	-7.23	-96.1
47	50	-5095	-110	173	0	-884	-61	6.28	6.28	9.42	9.42	-6.93	-92.4
49	50	-5098	-208	180	0	-900	-112	6.28	6.28	9.42	9.42	-7.04	-93.6
50	50	-5096	-10	173	0	-885	-9	6.28	6.28	9.42	9.42	-6.94	-92.5
51	50	-5110	-112	194	0	-940	-62	6.28	6.28	9.42	9.42	-7.31	-96.9

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 89 NI 1160 NF 1168 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 13
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-3856	-85	-364	0	-1268	31	6.28	6.28	9.42	9.42	-9.85	149.6
41	0	-3854	-32	-363	0	-1228	11	6.28	6.28	9.42	9.42	-9.53	138.8
42	0	-3872	-35	-377	0	-1376	12	6.28	6.28	9.42	9.42	-10.71	178.8
43	0	-3775	-121	-340	0	-1185	44	6.28	6.28	9.42	9.42	-9.19	131.2
44	0	-3776	57	-349	0	-1133	-23	6.28	6.28	9.42	9.42	-8.78	117.4
45	0	-3802	-37	-361	0	-1366	12	6.28	6.28	9.42	9.42	-10.63	179.8
46	0	-3722	-33	-324	0	-1053	11	6.28	6.28	9.42	9.42	-8.14	-102.0
47	0	-3689	-33	-314	0	-1010	11	6.28	6.28	9.42	9.42	-7.80	-98.2
49	0	-3690	-51	-315	0	-1023	18	6.28	6.28	9.42	9.42	-7.90	-99.3
50	0	-3690	-16	-316	0	-1012	4	6.28	6.28	9.42	9.42	-7.82	-98.4
51	0	-3695	-34	-319	0	-1059	11	6.28	6.28	9.42	9.42	-8.19	-102.4

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	12	-3800	-85	-364	0	-1222	20	6.28	6.28	9.42	9.42	-9.49	140.0
41	12	-3798	-32	-363	0	-1183	7	6.28	6.28	9.42	9.42	-9.17	129.4
42	12	-3816	-35	-377	0	-1329	7	6.28	6.28	9.42	9.42	-10.34	168.6
43	12	-3719	-121	-340	0	-1143	29	6.28	6.28	9.42	9.42	-8.86	122.7
44	12	-3720	57	-349	0	-1089	-16	6.28	6.28	9.42	9.42	-8.43	108.7
45	12	-3746	-37	-361	0	-1321	8	6.28	6.28	9.42	9.42	-10.28	170.0
46	12	-3666	-33	-324	0	-1013	7	6.28	6.28	9.42	9.42	-7.82	-98.3
47	12	-3633	-33	-314	0	-971	7	6.28	6.28	9.42	9.42	-7.49	-94.6
49	12	-3634	-51	-315	0	-984	11	6.28	6.28	9.42	9.42	-7.59	-95.8
50	12	-3634	-16	-316	0	-973	2	6.28	6.28	9.42	9.42	-7.51	-94.8
51	12	-3639	-34	-319	0	-1019	7	6.28	6.28	9.42	9.42	-7.88	-98.8

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	25	-3744	-85	-364	0	-1177	9	6.28	6.28	9.42	9.42	-9.13	130.6
41	25	-3742	-32	-363	0	-1138	3	6.28	6.28	9.42	9.42	-8.82	120.2
42	25	-3760	-35	-377	0	-1282	3	6.28	6.28	9.42	9.42	-9.97	158.5
43	25	-3662	-121	-340	0	-1100	14	6.28	6.28	9.42	9.42	-8.53	114.2
44	25	-3664	57	-349	0	-1046	-9	6.28	6.28	9.42	9.42	-8.09	-101.2
45	25	-3690	-37	-361	0	-1276	3	6.28	6.28	9.42	9.42	-9.92	160.3
46	25	-3610	-33	-324	0	-972	3	6.28	6.28	9.42	9.42	-7.50	-94.7
47	25	-3576	-33	-314	0	-931	3	6.28	6.28	9.42	9.42	-7.18	-91.1
49	25	-3578	-51	-315	0	-944	5	6.28	6.28	9.42	9.42	-7.29	-92.2
50	25	-3578	-16	-316	0	-933	0	6.28	6.28	9.42	9.42	-7.20	-91.2
51	25	-3582	-34	-319	0	-979	3	6.28	6.28	9.42	9.42	-7.56	-95.2

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	38	-3687	-85	-364	0	-1132	-1	6.28	6.28	9.42	9.42	-8.77	121.2
41	38	-3685	-32	-363	0	-1092	-1	6.28	6.28	9.42	9.42	-8.46	111.0
42	38	-3703	-35	-377	0	-1235	-2	6.28	6.28	9.42	9.42	-9.60	148.4
43	38	-3606	-121	-340	0	-1058	-1	6.28	6.28	9.42	9.42	-8.19	105.9
44	38	-3607	57	-349	0	-1002	-2	6.28	6.28	9.42	9.42	-7.74	-97.3
45	38	-3633	-37	-361	0	-1230	-2	6.28	6.28	9.42	9.42	-9.56	150.7
46	38	-3553	-33	-324	0	-932	-1	6.28	6.28	9.42	9.42	-7.19	-91.0
47	38	-3520	-33	-314	0	-892	-1	6.28	6.28	9.42	9.42	-6.87	-87.5
49	38	-3521	-51	-315	0	-905	-1	6.28	6.28	9.42	9.42	-6.98	-88.6
50	38	-3521	-16	-316	0	-894	-1	6.28	6.28	9.42	9.42	-6.89	-87.6
51	38	-3526	-34	-319	0	-939	-1	6.28	6.28	9.42	9.42	-7.25	-91.6

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	50	-3631	-85	-364	0	-1086	-12	6.28	6.28	9.42	9.42	-8.41	111.9
41	50	-3629	-32	-363	0	-1047	-5	6.28	6.28	9.42	9.42	-8.10	102.0
42	50	-3647	-35	-377	0	-1188	-6	6.28	6.28	9.42	9.42	-9.23	138.4
43	50	-3550	-121	-340	0	-1016	-16	6.28	6.28	9.42	9.42	-7.86	-98.3
44	50	-3551	57	-349	0	-959	5	6.28	6.28	9.42	9.42	-7.40	-93.3
45	50	-3577	-37	-361	0	-1185	-6	6.28	6.28	9.42	9.42	-9.21	141.2
46	50	-3497	-33	-324	0	-891	-6	6.28	6.28	9.42	9.42	-6.87	-87.4
47	50	-3464	-33	-314	0	-852	-6	6.28	6.28	9.42	9.42	-6.57	-83.9
49	50	-3465	-51	-315	0	-866	-8	6.28	6.28	9.42	9.42	-6.67	-85.0
50	50	-3465	-16	-316	0	-854	-3	6.28	6.28	9.42	9.42	-6.58	-84.1
51	50	-3470	-34	-319	0	-900	-6	6.28	6.28	9.42	9.42	-6.94	-88.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 90 NI 1159 NF 1161 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 18
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-4798	-75	-387	0	-1206	14	6.28	6.28	12.57	12.57	-7.53	-95.0
41	0	-4792	101	-404	0	-1239	-21	6.28	6.28	12.57	12.57	-7.76	-97.4
42	0	-4794	89	-416	0	-1336	-19	6.28	6.28	12.57	12.57	-8.43	115.0
43	0	-4706	-201	-352	0	-1094	39	6.28	6.28	12.57	12.57	-6.78	-86.6
44	0	-4692	394	-415	0	-1253	-80	6.28	6.28	12.57	12.57	-7.87	99.5
45	0	-4700	73	-401	0	-1312	-16	6.28	6.28	12.57	12.57	-8.28	113.3
46	0	-4640	88	-368	0	-1096	-19	6.28	6.28	12.57	12.57	-6.80	-86.6
47	0	-4602	84	-358	0	-1061	-18	6.28	6.28	12.57	12.57	-6.57	-84.0
49	0	-4604	26	-352	0	-1050	-7	6.28	6.28	12.57	12.57	-6.49	-83.2
50	0	-4601	145	-365	0	-1081	-30	6.28	6.28	12.57	12.57	-6.70	-85.5
51	0	-4602	80	-362	0	-1093	-18	6.28	6.28	12.57	12.57	-6.78	-86.4

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	12	-4723	-75	-387	0	-1158	5	6.28	6.28	12.57	12.57	-7.21	-91.3
41	12	-4717	101	-404	0	-1188	-9	6.28	6.28	12.57	12.57	-7.42	-93.6
42	12	-4719	89	-416	0	-1284	-8	6.28	6.28	12.57	12.57	-8.08	105.7
43	12	-4631	-201	-352	0	-1050	14	6.28	6.28	12.57	12.57	-6.49	-83.2
44	12	-4617	394	-415	0	-1201	-31	6.28	6.28	12.57	12.57	-7.52	-94.4
45	12	-4625	73	-401	0	-1262	-7	6.28	6.28	12.57	12.57	-7.95	104.4
46	12	-4565	88	-368	0	-1050	-8	6.28	6.28	12.57	12.57	-6.50	-83.2
47	12	-4527	84	-358	0	-1016	-8	6.28	6.28	12.57	12.57	-6.28	-80.6

49	12	-4529	26	-352	0	-1006	-3	6.28	6.28	12.57	12.57	-6.21	-79.9
50	12	-4526	145	-365	0	-1035	-12	6.28	6.28	12.57	12.57	-6.40	-82.0
51	12	-4527	80	-362	0	-1048	-8	6.28	6.28	12.57	12.57	-6.49	-82.9

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	25	-4648	-75	-387	0	-1109	-4	6.28	6.28	12.57	12.57	-6.89	-87.6
41	25	-4642	101	-404	0	-1138	4	6.28	6.28	12.57	12.57	-7.08	-89.7
42	25	-4644	89	-416	0	-1232	3	6.28	6.28	12.57	12.57	-7.73	-96.7
43	25	-4556	-201	-352	0	-1006	-11	6.28	6.28	12.57	12.57	-6.21	-79.9
44	25	-4542	394	-415	0	-1149	18	6.28	6.28	12.57	12.57	-7.18	-90.4
45	25	-4550	73	-401	0	-1212	2	6.28	6.28	12.57	12.57	-7.61	95.7
46	25	-4490	88	-368	0	-1004	3	6.28	6.28	12.57	12.57	-6.20	-79.7
47	25	-4452	84	-358	0	-971	3	6.28	6.28	12.57	12.57	-5.99	-77.2
49	25	-4454	26	-352	0	-962	-0	6.28	6.28	12.57	12.57	-5.92	-76.5
50	25	-4451	145	-365	0	-990	6	6.28	6.28	12.57	12.57	-6.11	-78.6
51	25	-4452	80	-362	0	-1002	2	6.28	6.28	12.57	12.57	-6.19	-79.5

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	38	-4573	-75	-387	0	-1060	-14	6.28	6.28	12.57	12.57	-6.57	-83.9
41	38	-4567	101	-404	0	-1088	17	6.28	6.28	12.57	12.57	-6.75	-85.9
42	38	-4569	89	-416	0	-1180	14	6.28	6.28	12.57	12.57	-7.39	-92.8
43	38	-4481	-201	-352	0	-962	-36	6.28	6.28	12.57	12.57	-5.92	-76.6
44	38	-4467	394	-415	0	-1097	68	6.28	6.28	12.57	12.57	-6.83	-86.5
45	38	-4475	73	-401	0	-1161	11	6.28	6.28	12.57	12.57	-7.27	-91.3
46	38	-4415	88	-368	0	-958	14	6.28	6.28	12.57	12.57	-5.91	-76.2
47	38	-4377	84	-358	0	-926	13	6.28	6.28	12.57	12.57	-5.70	-73.8
49	38	-4379	26	-352	0	-917	3	6.28	6.28	12.57	12.57	-5.64	-73.2
50	38	-4376	145	-365	0	-944	24	6.28	6.28	12.57	12.57	-5.82	-75.1
51	38	-4377	80	-362	0	-957	13	6.28	6.28	12.57	12.57	-5.90	-76.1

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	50	-4498	-75	-387	0	-1012	-23	6.28	6.28	12.57	12.57	-6.25	-80.3
41	50	-4492	101	-404	0	-1037	29	6.28	6.28	12.57	12.57	-6.42	-82.1
42	50	-4494	89	-416	0	-1128	26	6.28	6.28	12.57	12.57	-7.04	-88.8
43	50	-4406	-201	-352	0	-918	-61	6.28	6.28	12.57	12.57	-5.65	-73.3
44	50	-4392	394	-415	0	-1045	117	6.28	6.28	12.57	12.57	-6.49	-82.6
45	50	-4400	73	-401	0	-1111	21	6.28	6.28	12.57	12.57	-6.94	-87.5
46	50	-4340	88	-368	0	-912	25	6.28	6.28	12.57	12.57	-5.61	-72.8
47	50	-4302	84	-358	0	-881	24	6.28	6.28	12.57	12.57	-5.42	-70.5
49	50	-4304	26	-352	0	-873	6	6.28	6.28	12.57	12.57	-5.37	-69.9
50	50	-4301	145	-365	0	-899	42	6.28	6.28	12.57	12.57	-5.53	-71.7
51	50	-4302	80	-362	0	-912	23	6.28	6.28	12.57	12.57	-5.61	-72.7

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 91 NI 1161 NF 142 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 18A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm²				daN/cm²	
40	0	-6652	-283	69	0	-942	-23	6.28	6.28	12.57	12.57	-6.05	-81.9
41	0	-6651	195	71	0	-965	29	6.28	6.28	12.57	12.57	-6.16	-83.2
42	0	-6669	166	101	0	-1053	26	6.28	6.28	12.57	12.57	-6.59	-88.4
43	0	-6497	-624	53	0	-852	-61	6.28	6.28	12.57	12.57	-5.61	-76.3
44	0	-6503	997	76	0	-975	117	6.28	6.28	12.57	12.57	-6.17	-83.2
45	0	-6524	125	106	0	-1039	21	6.28	6.28	12.57	12.57	-6.50	-87.0
46	0	-6402	159	48	0	-847	25	6.28	6.28	12.57	12.57	-5.56	-75.6
47	0	-6339	150	42	0	-818	24	6.28	6.28	12.57	12.57	-5.42	-73.8
49	0	-6340	-9	42	0	-810	6	6.28	6.28	12.57	12.57	-5.39	-73.4
50	0	-6341	315	46	0	-835	42	6.28	6.28	12.57	12.57	-5.49	-74.7
51	0	-6345	141	52	0	-847	23	6.28	6.28	12.57	12.57	-5.55	-75.4

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	12	-6577	-283	69	0	-950	-59	6.28	6.28	12.57	12.57	-6.07	-82.0
41	12	-6576	195	71	0	-974	54	6.28	6.28	12.57	12.57	-6.19	-83.4
42	12	-6594	166	101	0	-1066	46	6.28	6.28	12.57	12.57	-6.65	-88.9
43	12	-6422	-624	53	0	-859	-139	6.28	6.28	12.57	12.57	-5.62	-76.3
44	12	-6428	997	76	0	-985	242	6.28	6.28	12.57	12.57	-6.20	-83.4
45	12	-6449	125	106	0	-1052	36	6.28	6.28	12.57	12.57	-6.55	-87.6
46	12	-6327	159	48	0	-853	45	6.28	6.28	12.57	12.57	-5.57	-75.6
47	12	-6264	150	42	0	-823	43	6.28	6.28	12.57	12.57	-5.42	-73.7
49	12	-6265	-9	42	0	-815	5	6.28	6.28	12.57	12.57	-5.38	-73.3
50	12	-6266	315	46	0	-840	81	6.28	6.28	12.57	12.57	-5.49	-74.6
51	12	-6270	141	52	0	-854	40	6.28	6.28	12.57	12.57	-5.55	-75.3

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	25	-6502	-283	69	0	-959	-94	6.28	6.28	12.57	12.57	-6.09	-82.2
41	25	-6501	195	71	0	-983	78	6.28	6.28	12.57	12.57	-6.21	-83.6
42	25	-6519	166	101	0	-1078	67	6.28	6.28	12.57	12.57	-6.70	-89.5
43	25	-6347	-624	53	0	-865	-217	6.28	6.28	12.57	12.57	-5.62	-76.3
44	25	-6353	997	76	0	-994	366	6.28	6.28	12.57	12.57	-6.24	-83.7
45	25	-6374	125	106	0	-1066	52	6.28	6.28	12.57	12.57	-6.61	-88.2
46	25	-6252	159	48	0	-859	65	6.28	6.28	12.57	12.57	-5.57	-75.6
47	25	-6189	150	42	0	-829	61	6.28	6.28	12.57	12.57	-5.42	-73.6
49	25	-6190	-9	42	0	-820	4	6.28	6.28	12.57	12.57	-5.38	-73.2
50	25	-6191	315	46	0	-846	121	6.28	6.28	12.57	12.57	-5.50	-74.6
51	25	-6195	141	52	0	-860	58	6.28	6.28	12.57	12.57	-5.56	-75.4

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	38	-6427	-283	69	0	-967	-129	6.28	6.28	12.57	12.57	-6.12	-82.4
41	38	-6426	195	71	0	-992	102	6.28	6.28	12.57	12.57	-6.24	-83.8
42	38	-6444	166	101	0	-1091	88	6.28	6.28	12.57	12.57	-6.76	-90.0
43	38	-6272	-624	53	0	-872	-295	6.28	6.28	12.57	12.57	-5.63	-76.3
44	38	-6278	997	76	0	-1004	491	6.28	6.28	12.57	12.57	-6.27	-84.0
45	38	-6299	125	106	0	-1079	67	6.28	6.28	12.57	12.57	-6.67	-88.8
46	38	-6177	159	48	0	-865	85	6.28	6.28	12.57	12.57	-5.58	-75.5
47	38	-6114	150	42	0	-834	80	6.28	6.28	12.57	12.57	-5.42	-73.5
49	38	-6115	-9	42	0	-826	3	6.28	6.28	12.57	12.57	-5.38	-73.1

50	38	-6116	315	46	0	-852	160	6.28	6.28	12.57	12.57	-5.50	-74.5
51	38	-6120	141	52	0	-867	75	6.28	6.28	12.57	12.57	-5.57	-75.4

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	50	-6352	-283	69	0	-976	-165	6.28	6.28	12.57	12.57	-6.15	-82.6
41	50	-6351	195	71	0	-1001	127	6.28	6.28	12.57	12.57	-6.27	-84.1
42	50	-6369	166	101	0	-1104	109	6.28	6.28	12.57	12.57	-6.82	-90.6
43	50	-6197	-624	53	0	-879	-373	6.28	6.28	12.57	12.57	-5.64	-76.4
44	50	-6203	997	76	0	-1013	616	6.28	6.28	12.57	12.57	-6.31	-84.3
45	50	-6224	125	106	0	-1092	83	6.28	6.28	12.57	12.57	-6.74	-89.4
46	50	-6102	159	48	0	-872	104	6.28	6.28	12.57	12.57	-5.59	-75.5
47	50	-6039	150	42	0	-839	99	6.28	6.28	12.57	12.57	-5.42	-73.5
49	50	-6040	-9	42	0	-831	2	6.28	6.28	12.57	12.57	-5.39	-73.0
50	50	-6041	315	46	0	-858	200	6.28	6.28	12.57	12.57	-5.51	-74.5
51	50	-6045	141	52	0	-874	93	6.28	6.28	12.57	12.57	-5.58	-75.4

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 92 NI 1256 NF 1259 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 19
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-16410	153	-188	0	-489	-613	6.28	6.28	12.57	12.57	-8.94	-122.7
41	0	-16410	9	-217	0	-565	-56	6.28	6.28	12.57	12.57	-8.36	-120.4
42	0	-16340	10	-274	0	-731	-60	6.28	6.28	12.57	12.57	-8.93	-127.4
43	0	-15810	249	-132	0	-348	-984	6.28	6.28	12.57	12.57	-10.55	-140.1
44	0	-15900	-232	-276	0	-717	874	6.28	6.28	12.57	12.57	-10.04	-134.5
45	0	-15690	10	-275	0	-752	-62	6.28	6.28	12.57	12.57	-8.76	-124.6
46	0	-15460	8	-157	0	-421	-55	6.28	6.28	12.57	12.57	-7.48	-108.4
47	0	-15220	8	-142	0	-385	-55	6.28	6.28	12.57	12.57	-7.26	-105.4
49	0	-15220	56	-132	0	-360	-241	6.28	6.28	12.57	12.57	-7.17	-104.3
50	0	-15240	-40	-161	0	-434	131	6.28	6.28	12.57	12.57	-7.44	-107.7
51	0	-15200	9	-161	0	-441	-56	6.28	6.28	12.57	12.57	-7.45	-107.8

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	12	-16335	153	-188	0	-466	-594	6.28	6.28	12.57	12.57	-8.81	-121.2
41	12	-16335	9	-217	0	-538	-55	6.28	6.28	12.57	12.57	-8.24	-118.7
42	12	-16265	10	-274	0	-697	-59	6.28	6.28	12.57	12.57	-8.78	-125.5
43	12	-15735	249	-132	0	-332	-952	6.28	6.28	12.57	12.57	-10.37	-137.9
44	12	-15825	-232	-276	0	-683	845	6.28	6.28	12.57	12.57	-9.87	-132.5
45	12	-15615	10	-275	0	-718	-61	6.28	6.28	12.57	12.57	-8.60	-122.6
46	12	-15385	8	-157	0	-402	-54	6.28	6.28	12.57	12.57	-7.38	-107.1
47	12	-15145	8	-142	0	-367	-54	6.28	6.28	12.57	12.57	-7.17	-104.2
49	12	-15145	56	-132	0	-343	-234	6.28	6.28	12.57	12.57	-7.08	-103.1
50	12	-15165	-40	-161	0	-413	126	6.28	6.28	12.57	12.57	-7.34	-106.4
51	12	-15125	9	-161	0	-420	-55	6.28	6.28	12.57	12.57	-7.35	-106.5

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	25	-16260	153	-188	0	-442	-574	6.28	6.28	12.57	12.57	-8.69	-119.8
41	25	-16260	9	-217	0	-511	-54	6.28	6.28	12.57	12.57	-8.11	-117.1
42	25	-16190	10	-274	0	-663	-57	6.28	6.28	12.57	12.57	-8.63	-123.5
43	25	-15660	249	-132	0	-315	-921	6.28	6.28	12.57	12.57	-10.19	-135.8
44	25	-15750	-232	-276	0	-648	816	6.28	6.28	12.57	12.57	-9.70	-130.4
45	25	-15540	10	-275	0	-684	-60	6.28	6.28	12.57	12.57	-8.45	-120.7
46	25	-15310	8	-157	0	-382	-53	6.28	6.28	12.57	12.57	-7.28	-105.8
47	25	-15070	8	-142	0	-350	-53	6.28	6.28	12.57	12.57	-7.07	-103.0
49	25	-15070	56	-132	0	-327	-227	6.28	6.28	12.57	12.57	-6.99	-102.0
50	25	-15090	-40	-161	0	-393	121	6.28	6.28	12.57	12.57	-7.24	-105.0
51	25	-15050	9	-161	0	-400	-54	6.28	6.28	12.57	12.57	-7.25	-105.1

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	38	-16185	153	-188	0	-418	-555	6.28	6.28	12.57	12.57	-8.57	-118.3
41	38	-16185	9	-217	0	-484	-52	6.28	6.28	12.57	12.57	-7.99	-115.4
42	38	-16115	10	-274	0	-629	-56	6.28	6.28	12.57	12.57	-8.48	-121.5
43	38	-15585	249	-132	0	-299	-890	6.28	6.28	12.57	12.57	-10.01	-133.7
44	38	-15675	-232	-276	0	-614	787	6.28	6.28	12.57	12.57	-9.53	-128.4
45	38	-15465	10	-275	0	-649	-58	6.28	6.28	12.57	12.57	-8.30	-118.7
46	38	-15235	8	-157	0	-362	-52	6.28	6.28	12.57	12.57	-7.18	-104.5
47	38	-14995	8	-142	0	-332	-52	6.28	6.28	12.57	12.57	-6.98	-101.8
49	38	-14995	56	-132	0	-310	-220	6.28	6.28	12.57	12.57	-6.90	-100.8
50	38	-15015	-40	-161	0	-373	116	6.28	6.28	12.57	12.57	-7.14	-103.7
51	38	-14975	9	-161	0	-380	-53	6.28	6.28	12.57	12.57	-7.15	-103.8

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	50	-16110	153	-188	0	-395	-536	6.28	6.28	12.57	12.57	-8.45	-116.8
41	50	-16110	9	-217	0	-457	-51	6.28	6.28	12.57	12.57	-7.86	-113.8
42	50	-16040	10	-274	0	-594	-55	6.28	6.28	12.57	12.57	-8.33	-119.6
43	50	-15510	249	-132	0	-282	-859	6.28	6.28	12.57	12.57	-9.83	-131.5
44	50	-15600	-232	-276	0	-579	758	6.28	6.28	12.57	12.57	-9.36	-126.4
45	50	-15390	10	-275	0	-615	-57	6.28	6.28	12.57	12.57	-8.15	-116.7
46	50	-15160	8	-157	0	-343	-51	6.28	6.28	12.57	12.57	-7.08	-103.2
47	50	-14920	8	-142	0	-314	-51	6.28	6.28	12.57	12.57	-6.89	-100.5
49	50	-14920	56	-132	0	-294	-212	6.28	6.28	12.57	12.57	-6.82	-99.6
50	50	-14940	-40	-161	0	-353	111	6.28	6.28	12.57	12.57	-7.04	-102.4
51	50	-14900	9	-161	0	-360	-52	6.28	6.28	12.57	12.57	-7.05	-102.5

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 93 NI 1259 NF 127 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 19A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	

40	0	-16110	153	-188	0	-395	-536	6.28	6.28	12.57	12.57	-8.45	-116.8
41	0	-16110	9	-217	0	-457	-51	6.28	6.28	12.57	12.57	-7.86	-113.8
42	0	-16040	10	-274	0	-594	-55	6.28	6.28	12.57	12.57	-8.33	-119.6
43	0	-15510	249	-132	0	-282	-859	6.28	6.28	12.57	12.57	-9.83	-131.5
44	0	-15600	-232	-276	0	-579	758	6.28	6.28	12.57	12.57	-9.36	-126.4
45	0	-15390	10	-275	0	-615	-57	6.28	6.28	12.57	12.57	-8.15	-116.7
46	0	-15160	8	-157	0	-343	-51	6.28	6.28	12.57	12.57	-7.08	-103.2
47	0	-14920	8	-142	0	-314	-51	6.28	6.28	12.57	12.57	-6.89	-100.5
49	0	-14920	56	-132	0	-294	-212	6.28	6.28	12.57	12.57	-6.82	-99.6
50	0	-14940	-40	-161	0	-353	111	6.28	6.28	12.57	12.57	-7.04	-102.4
51	0	-14900	9	-161	0	-360	-52	6.28	6.28	12.57	12.57	-7.05	-102.5

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	12	-16035	153	-188	0	-371	-517	6.28	6.28	12.57	12.57	-8.33	-115.4
41	12	-16035	9	-217	0	-430	-50	6.28	6.28	12.57	12.57	-7.73	-112.1
42	12	-15965	10	-274	0	-560	-54	6.28	6.28	12.57	12.57	-8.17	-117.6
43	12	-15435	249	-132	0	-266	-828	6.28	6.28	12.57	12.57	-9.65	-129.4
44	12	-15525	-232	-276	0	-545	729	6.28	6.28	12.57	12.57	-9.19	-124.4
45	12	-15315	10	-275	0	-581	-56	6.28	6.28	12.57	12.57	-8.00	-114.7
46	12	-15085	8	-157	0	-323	-50	6.28	6.28	12.57	12.57	-6.98	-101.9
47	12	-14845	8	-142	0	-297	-50	6.28	6.28	12.57	12.57	-6.80	-99.3
49	12	-14845	56	-132	0	-277	-205	6.28	6.28	12.57	12.57	-6.73	-98.4
50	12	-14865	-40	-161	0	-333	106	6.28	6.28	12.57	12.57	-6.93	-101.0
51	12	-14825	9	-161	0	-340	-51	6.28	6.28	12.57	12.57	-6.94	-101.1

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	25	-15960	153	-188	0	-348	-498	6.28	6.28	12.57	12.57	-8.21	-113.9
41	25	-15960	9	-217	0	-402	-49	6.28	6.28	12.57	12.57	-7.61	-110.5
42	25	-15890	10	-274	0	-526	-52	6.28	6.28	12.57	12.57	-8.02	-115.6
43	25	-15360	249	-132	0	-249	-797	6.28	6.28	12.57	12.57	-9.47	-127.3
44	25	-15450	-232	-276	0	-510	700	6.28	6.28	12.57	12.57	-9.02	-122.4
45	25	-15240	10	-275	0	-546	-55	6.28	6.28	12.57	12.57	-7.84	-112.8
46	25	-15010	8	-157	0	-304	-49	6.28	6.28	12.57	12.57	-6.89	-100.6
47	25	-14770	8	-142	0	-279	-49	6.28	6.28	12.57	12.57	-6.70	-98.1
49	25	-14770	56	-132	0	-261	-198	6.28	6.28	12.57	12.57	-6.64	-97.3
50	25	-14790	-40	-161	0	-313	101	6.28	6.28	12.57	12.57	-6.83	-99.7
51	25	-14750	9	-161	0	-320	-50	6.28	6.28	12.57	12.57	-6.84	-99.8

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	38	-15885	153	-188	0	-324	-479	6.28	6.28	12.57	12.57	-8.09	-112.4
41	38	-15885	9	-217	0	-375	-48	6.28	6.28	12.57	12.57	-7.48	-108.9
42	38	-15815	10	-274	0	-492	-51	6.28	6.28	12.57	12.57	-7.87	-113.6
43	38	-15285	249	-132	0	-233	-766	6.28	6.28	12.57	12.57	-9.29	-125.1
44	38	-15375	-232	-276	0	-476	671	6.28	6.28	12.57	12.57	-8.85	-120.4
45	38	-15165	10	-275	0	-512	-53	6.28	6.28	12.57	12.57	-7.69	-110.8
46	38	-14935	8	-157	0	-284	-48	6.28	6.28	12.57	12.57	-6.79	-99.3
47	38	-14695	8	-142	0	-261	-48	6.28	6.28	12.57	12.57	-6.61	-96.8
49	38	-14695	56	-132	0	-244	-191	6.28	6.28	12.57	12.57	-6.55	-96.1
50	38	-14715	-40	-161	0	-293	96	6.28	6.28	12.57	12.57	-6.73	-98.4
51	38	-14675	9	-161	0	-300	-49	6.28	6.28	12.57	12.57	-6.74	-98.5

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	50	-15810	153	-188	0	-300	-460	6.28	6.28	12.57	12.57	-7.96	-111.0
41	50	-15810	9	-217	0	-348	-47	6.28	6.28	12.57	12.57	-7.35	-107.2
42	50	-15740	10	-274	0	-457	-50	6.28	6.28	12.57	12.57	-7.72	-111.7
43	50	-15210	249	-132	0	-216	-735	6.28	6.28	12.57	12.57	-9.11	-123.0
44	50	-15300	-232	-276	0	-442	642	6.28	6.28	12.57	12.57	-8.68	-118.3
45	50	-15090	10	-275	0	-478	-52	6.28	6.28	12.57	12.57	-7.54	-108.8
46	50	-14860	8	-157	0	-264	-47	6.28	6.28	12.57	12.57	-6.69	-97.9
47	50	-14620	8	-142	0	-243	-47	6.28	6.28	12.57	12.57	-6.52	-95.6
49	50	-14620	56	-132	0	-228	-184	6.28	6.28	12.57	12.57	-6.46	-94.9
50	50	-14640	-40	-161	0	-272	91	6.28	6.28	12.57	12.57	-6.63	-97.0
51	50	-14600	9	-161	0	-280	-48	6.28	6.28	12.57	12.57	-6.64	-97.1

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 94 NI 1034 NF 1040 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 20
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	--												
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-29500	634	744	0	1627	-1906	6.28	6.28	12.57	12.57	-20.04	-265.3
41	0	-29830	124	690	0	1499	-366	6.28	6.28	12.57	12.57	-16.89	-240.0
42	0	-29760	128	542	0	1189	-375	6.28	6.28	12.57	12.57	-15.75	-225.7
43	0	-28060	960	708	0	1592	-2899	6.28	6.28	12.57	12.57	-25.09	-318.4
44	0	-30110	-726	592	0	1251	2203	6.28	6.28	12.57	12.57	-21.73	-285.1
45	0	-28510	116	373	0	862	-347	6.28	6.28	12.57	12.57	-14.10	-203.8
46	0	-27910	101	577	0	1305	-310	6.28	6.28	12.57	12.57	-15.46	-220.1
47	0	-27420	96	549	0	1257	-296	6.28	6.28	12.57	12.57	-15.09	-215.2
49	0	-27310	266	566	0	1300	-810	6.28	6.28	12.57	12.57	-15.21	-216.4
50	0	-27720	-71	543	0	1231	211	6.28	6.28	12.57	12.57	-15.12	-215.7
51	0	-27400	97	499	0	1154	-299	6.28	6.28	12.57	12.57	-14.72	-210.4

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	12	-29425	634	744	0	1534	-1827	6.28	6.28	12.57	12.57	-19.62	-260.5
41	12	-29755	124	690	0	1413	-350	6.28	6.28	12.57	12.57	-16.55	-235.7
42	12	-29685	128	542	0	1121	-359	6.28	6.28	12.57	12.57	-15.48	-222.2
43	12	-27985	960	708	0	1504	-2779	6.28	6.28	12.57	12.57	-24.31	-310.0
44	12	-30035	-726	592	0	1177	2112	6.28	6.28	12.57	12.57	-21.25	-279.6
45	12	-28435	116	373	0	816	-332	6.28	6.28	12.57	12.57	-13.91	-201.3
46	12	-27835	101	577	0	1233	-297	6.28	6.28	12.57	12.57	-15.17	-216.5
47	12	-27345	96	549	0	1188	-284	6.28	6.28	12.57	12.57	-14.82	-211.7
49	12	-27235	266	566	0	1229	-776	6.28	6.28	12.57	12.57	-14.92	-212.8
50	12	-27645	-71	543	0	1163	202	6.28	6.28	12.57	12.57	-14.85	-212.3
51	12	-27325	97	499	0	1092	-287	6.28	6.28	12.57	12.57	-14.46	-207.2

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	25	-29350	634	744	0	1442	-1748	6.28	6.28	12.57	12.57	-19.20	-255.7
41	25	-29680	124	690	0	1326	-335	6.28	6.28	12.57	12.57	-16.22	-231.4
42	25	-29610	128	542	0	1054	-343	6.28	6.28	12.57	12.57	-15.21	-218.7
43	25	-27910	960	708	0	1415	-2659	6.28	6.28	12.57	12.57	-23.55	-301.7
44	25	-29960	-726	592	0	1103	2022	6.28	6.28	12.57	12.57	-20.78	-274.2
45	25	-28360	116	373	0	769	-318	6.28	6.28	12.57	12.57	-13.71	-198.8
46	25	-27760	101	577	0	1161	-285	6.28	6.28	12.57	12.57	-14.88	-212.8
47	25	-27270	96	549	0	1120	-272	6.28	6.28	12.57	12.57	-14.54	-208.1
49	25	-27160	266	566	0	1158	-743	6.28	6.28	12.57	12.57	-14.64	-209.2
50	25	-27570	-71	543	0	1095	193	6.28	6.28	12.57	12.57	-14.57	-208.8
51	25	-27250	97	499	0	1029	-275	6.28	6.28	12.57	12.57	-14.21	-204.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	38	-29275	634	744	0	1349	-1668	6.28	6.28	12.57	12.57	-18.78	-250.9
41	38	-29605	124	690	0	1240	-319	6.28	6.28	12.57	12.57	-15.88	-227.1
42	38	-29535	128	542	0	986	-327	6.28	6.28	12.57	12.57	-14.94	-215.3
43	38	-27835	960	708	0	1326	-2539	6.28	6.28	12.57	12.57	-22.81	-293.6
44	38	-29885	-726	592	0	1029	1932	6.28	6.28	12.57	12.57	-20.30	-268.8
45	38	-28285	116	373	0	722	-303	6.28	6.28	12.57	12.57	-13.51	-196.2
46	38	-27685	101	577	0	1089	-272	6.28	6.28	12.57	12.57	-14.59	-209.2
47	38	-27195	96	549	0	1051	-260	6.28	6.28	12.57	12.57	-14.27	-204.6
49	38	-27085	266	566	0	1087	-710	6.28	6.28	12.57	12.57	-14.36	-205.6
50	38	-27495	-71	543	0	1028	184	6.28	6.28	12.57	12.57	-14.30	-205.3
51	38	-27175	97	499	0	966	-263	6.28	6.28	12.57	12.57	-13.96	-200.7

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	50	-29200	634	744	0	1256	-1589	6.28	6.28	12.57	12.57	-18.37	-246.0
41	50	-29530	124	690	0	1154	-304	6.28	6.28	12.57	12.57	-15.54	-222.8
42	50	-29460	128	542	0	918	-311	6.28	6.28	12.57	12.57	-14.67	-211.8
43	50	-27760	960	708	0	1238	-2419	6.28	6.28	12.57	12.57	-22.09	-285.7
44	50	-29810	-726	592	0	955	1841	6.28	6.28	12.57	12.57	-19.83	-263.3
45	50	-28210	116	373	0	676	-289	6.28	6.28	12.57	12.57	-13.32	-193.7
46	50	-27610	101	577	0	1017	-259	6.28	6.28	12.57	12.57	-14.31	-205.5
47	50	-27120	96	549	0	982	-248	6.28	6.28	12.57	12.57	-13.99	-201.1
49	50	-27010	266	566	0	1016	-677	6.28	6.28	12.57	12.57	-14.07	-202.0
50	50	-27420	-71	543	0	960	175	6.28	6.28	12.57	12.57	-14.03	-201.9
51	50	-27100	97	499	0	904	-251	6.28	6.28	12.57	12.57	-13.71	-197.5

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 95 NI 1040 NF 301 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 20A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-29200	634	744	0	1256	-1589	6.28	6.28	12.57	12.57	-18.37	-246.0
41	0	-29530	124	690	0	1154	-304	6.28	6.28	12.57	12.57	-15.54	-222.8
42	0	-29460	128	542	0	918	-311	6.28	6.28	12.57	12.57	-14.67	-211.8
43	0	-27760	960	708	0	1238	-2419	6.28	6.28	12.57	12.57	-22.09	-285.7
44	0	-29810	-726	592	0	955	1841	6.28	6.28	12.57	12.57	-19.83	-263.3
45	0	-28210	116	373	0	676	-289	6.28	6.28	12.57	12.57	-13.32	-193.7
46	0	-27610	101	577	0	1017	-259	6.28	6.28	12.57	12.57	-14.31	-205.5
47	0	-27120	96	549	0	982	-248	6.28	6.28	12.57	12.57	-13.99	-201.1
49	0	-27010	266	566	0	1016	-677	6.28	6.28	12.57	12.57	-14.07	-202.0
50	0	-27420	-71	543	0	960	175	6.28	6.28	12.57	12.57	-14.03	-201.9
51	0	-27100	97	499	0	904	-251	6.28	6.28	12.57	12.57	-13.71	-197.5

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	12	-29125	634	744	0	1163	-1510	6.28	6.28	12.57	12.57	-17.95	-241.2
41	12	-29455	124	690	0	1068	-288	6.28	6.28	12.57	12.57	-15.20	-218.5
42	12	-29385	128	542	0	850	-295	6.28	6.28	12.57	12.57	-14.40	-208.4
43	12	-27685	960	708	0	1149	-2299	6.28	6.28	12.57	12.57	-21.40	-278.0
44	12	-29735	-726	592	0	881	1750	6.28	6.28	12.57	12.57	-19.35	-257.9
45	12	-28135	116	373	0	629	-274	6.28	6.28	12.57	12.57	-13.12	-191.2
46	12	-27535	101	577	0	945	-247	6.28	6.28	12.57	12.57	-14.02	-201.8
47	12	-27045	96	549	0	914	-236	6.28	6.28	12.57	12.57	-13.72	-197.6
49	12	-26935	266	566	0	945	-644	6.28	6.28	12.57	12.57	-13.79	-198.4
50	12	-27345	-71	543	0	892	166	6.28	6.28	12.57	12.57	-13.76	-198.4
51	12	-27025	97	499	0	842	-239	6.28	6.28	12.57	12.57	-13.45	-194.3

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	25	-29050	634	744	0	1070	-1430	6.28	6.28	12.57	12.57	-17.53	-236.4
41	25	-29380	124	690	0	981	-273	6.28	6.28	12.57	12.57	-14.86	-214.2
42	25	-29310	128	542	0	783	-279	6.28	6.28	12.57	12.57	-14.13	-204.9
43	25	-27610	960	708	0	1061	-2179	6.28	6.28	12.57	12.57	-20.73	-270.5
44	25	-29660	-726	592	0	806	1660	6.28	6.28	12.57	12.57	-18.88	-252.4
45	25	-28060	116	373	0	582	-260	6.28	6.28	12.57	12.57	-12.93	-188.7
46	25	-27460	101	577	0	873	-234	6.28	6.28	12.57	12.57	-13.73	-198.2
47	25	-26970	96	549	0	845	-224	6.28	6.28	12.57	12.57	-13.45	-194.1
49	25	-26860	266	566	0	875	-610	6.28	6.28	12.57	12.57	-13.51	-194.8
50	25	-27270	-71	543	0	824	157	6.28	6.28	12.57	12.57	-13.49	-194.9
51	25	-26950	97	499	0	779	-227	6.28	6.28	12.57	12.57	-13.20	-191.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	38	-28975	634	744	0	977	-1351	6.28	6.28	12.57	12.57	-17.11	-231.6
41	38	-29305	124	690	0	895	-257	6.28	6.28	12.57	12.57	-14.53	-209.9
42	38	-29235	128	542	0	715	-263	6.28	6.28	12.57	12.57	-13.85	-201.4
43	38	-27535	960	708	0	972	-2059	6.28	6.28	12.57	12.57	-20.09	-263.2
44	38	-29585	-726	592	0	732	1569	6.28	6.28	12.57	12.57	-18.40	-247.0
45	38	-27985	116	373	0	536	-245	6.28	6.28	12.57	12.57	-12.73	-186.2
46	38	-27385	101	577	0	800	-221	6.28	6.28	12.57	12.57	-13.45	-194.5
47	38	-26895	96	549	0	777	-212	6.28	6.28	12.57	12.57	-13.17	-190.6
49	38	-26785	266	566	0	804	-577	6.28	6.28	12.57	12.57	-13.23	-191.2
50	38	-27195	-71	543	0	756	148	6.28	6.28	12.57	12.57	-13.21	-191.4
51	38	-26875	97	499	0	717	-214	6.28	6.28	12.57	12.57	-12.95	-187.8

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	50	-28900	634	744	0	884	-1272	6.28	6.28	12.57	12.57	-16.69	-226.8

41	50	-29230	124	690	0	808	-242	6.28	6.28	12.57	12.57	-14.19	-205.6
42	50	-29160	128	542	0	647	-247	6.28	6.28	12.57	12.57	-13.58	-197.9
43	50	-27460	960	708	0	884	-1939	6.28	6.28	12.57	12.57	-19.47	-256.1
44	50	-29510	-726	592	0	658	1478	6.28	6.28	12.57	12.57	-17.93	-241.5
45	50	-27910	116	373	0	489	-230	6.28	6.28	12.57	12.57	-12.53	-183.6
46	50	-27310	101	577	0	728	-209	6.28	6.28	12.57	12.57	-13.16	-190.8
47	50	-26820	96	549	0	708	-200	6.28	6.28	12.57	12.57	-12.90	-187.1
49	50	-26710	266	566	0	733	-544	6.28	6.28	12.57	12.57	-12.94	-187.6
50	50	-27120	-71	543	0	688	139	6.28	6.28	12.57	12.57	-12.94	-188.0
51	50	-26800	97	499	0	654	-202	6.28	6.28	12.57	12.57	-12.70	-184.6

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 96 NI 1352 NF 1355 SEZ. Rp B= 0.400 H= 0.600 (pilastro)
PIL. NUM. 21
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-10070	1808	620	0	1279	-5288	12.57	12.57	6.28	6.28	-34.77	947.2
41	0	-10100	865	598	0	1218	-2556	12.57	12.57	6.28	6.28	-15.97	-201.2
42	0	-10120	870	573	0	1143	-2567	12.57	12.57	6.28	6.28	-16.04	-202.0
43	0	-9892	2261	612	0	1268	-6610	12.57	12.57	6.28	6.28	-43.53	1363.1
44	0	-9950	-681	544	0	1084	1927	12.57	12.57	6.28	6.28	-11.84	-155.2
45	0	-9984	697	533	0	1041	-2075	12.57	12.57	6.28	6.28	-12.76	-165.7
46	0	-9851	584	562	0	1136	-1756	12.57	12.57	6.28	6.28	-10.82	-143.3
47	0	-9790	514	553	0	1115	-1557	12.57	12.57	6.28	6.28	-9.74	-130.5
49	0	-9779	828	560	0	1135	-2467	12.57	12.57	6.28	6.28	-15.40	-194.2
50	0	-9791	240	546	0	1099	-760	12.57	12.57	6.28	6.28	-9.34	-117.2
51	0	-9798	516	544	0	1090	-1560	12.57	12.57	6.28	6.28	-9.75	-130.7

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	12	-9994	1808	620	0	1201	-5062	12.57	12.57	6.28	6.28	-33.26	883.8
41	12	-10024	865	598	0	1143	-2448	12.57	12.57	6.28	6.28	-15.23	-193.1
42	12	-10046	870	573	0	1071	-2458	12.57	12.57	6.28	6.28	-15.30	-193.9
43	12	-9817	2261	612	0	1191	-6328	12.57	12.57	6.28	6.28	-41.67	1281.3
44	12	-9875	-681	544	0	1016	1842	12.57	12.57	6.28	6.28	-11.32	-149.2
45	12	-9909	697	533	0	974	-1988	12.57	12.57	6.28	6.28	-12.21	-159.4
46	12	-9776	584	562	0	1066	-1683	12.57	12.57	6.28	6.28	-10.41	-138.4
47	12	-9715	514	553	0	1046	-1492	12.57	12.57	6.28	6.28	-9.40	-126.3
49	12	-9704	828	560	0	1065	-2364	12.57	12.57	6.28	6.28	-14.70	-186.4
50	12	-9716	240	546	0	1031	-730	12.57	12.57	6.28	6.28	-8.86	-112.1
51	12	-9723	516	544	0	1022	-1496	12.57	12.57	6.28	6.28	-9.41	-126.5

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	25	-9918	1808	620	0	1124	-4836	12.57	12.57	6.28	6.28	-31.75	820.8
41	25	-9949	865	598	0	1068	-2340	12.57	12.57	6.28	6.28	-14.51	-185.0
42	25	-9972	870	573	0	1000	-2350	12.57	12.57	6.28	6.28	-14.57	-185.7
43	25	-9742	2261	612	0	1115	-6045	12.57	12.57	6.28	6.28	-39.81	1199.6
44	25	-9800	-681	544	0	948	1757	12.57	12.57	6.28	6.28	-10.83	-143.3
45	25	-9834	697	533	0	908	-1900	12.57	12.57	6.28	6.28	-11.67	-153.1
46	25	-9701	584	562	0	995	-1610	12.57	12.57	6.28	6.28	-10.00	-133.5
47	25	-9640	514	553	0	977	-1428	12.57	12.57	6.28	6.28	-9.07	-122.3
49	25	-9629	828	560	0	995	-2260	12.57	12.57	6.28	6.28	-14.01	-178.7
50	25	-9641	240	546	0	962	-700	12.57	12.57	6.28	6.28	-8.40	-107.1
51	25	-9648	516	544	0	954	-1431	12.57	12.57	6.28	6.28	-9.08	-122.5

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	37	-9843	1808	620	0	1046	-4610	12.57	12.57	6.28	6.28	-30.23	758.0
41	37	-9873	865	598	0	994	-2231	12.57	12.57	6.28	6.28	-13.79	-176.9
42	37	-9897	870	573	0	928	-2241	12.57	12.57	6.28	6.28	-13.85	-177.6
43	37	-9667	2261	612	0	1038	-5762	12.57	12.57	6.28	6.28	-37.94	1118.1
44	37	-9725	-681	544	0	880	1672	12.57	12.57	6.28	6.28	-10.34	-137.5
45	37	-9759	697	533	0	841	-1813	12.57	12.57	6.28	6.28	-11.15	-146.9
46	37	-9626	584	562	0	925	-1537	12.57	12.57	6.28	6.28	-9.61	-128.7
47	37	-9565	514	553	0	908	-1364	12.57	12.57	6.28	6.28	-8.75	-118.3
49	37	-9554	828	560	0	925	-2156	12.57	12.57	6.28	6.28	-13.33	-171.0
50	37	-9566	240	546	0	894	-670	12.57	12.57	6.28	6.28	-7.96	-102.3
51	37	-9573	516	544	0	886	-1366	12.57	12.57	6.28	6.28	-8.76	-118.5

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	50	-9767	1808	620	0	969	-4384	12.57	12.57	6.28	6.28	-28.71	695.5
41	50	-9798	865	598	0	919	-2123	12.57	12.57	6.28	6.28	-13.08	-168.9
42	50	-9823	870	573	0	856	-2132	12.57	12.57	6.28	6.28	-13.14	-169.6
43	50	-9592	2261	612	0	962	-5480	12.57	12.57	6.28	6.28	-36.07	1036.8
44	50	-9650	-681	544	0	812	1587	12.57	12.57	6.28	6.28	-9.87	-131.8
45	50	-9684	697	533	0	774	-1726	12.57	12.57	6.28	6.28	-10.64	-140.9
46	50	-9551	584	562	0	855	-1464	12.57	12.57	6.28	6.28	-9.22	-124.0
47	50	-9490	514	553	0	839	-1299	12.57	12.57	6.28	6.28	-8.43	-114.4
49	50	-9479	828	560	0	855	-2053	12.57	12.57	6.28	6.28	-12.65	-163.3
50	50	-9491	240	546	0	825	-640	12.57	12.57	6.28	6.28	-7.54	-97.6
51	50	-9498	516	544	0	818	-1302	12.57	12.57	6.28	6.28	-8.45	-114.6

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

ASTA NUM. 97 NI 1355 NF 172 SEZ. Rp B= 0.400 H= 0.600 (pilastro)
PIL. NUM. 21A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-9767	1808	620	0	969	-4384	12.57	12.57	6.28	6.28	-28.71	695.5
41	0	-9798	865	598	0	919	-2123	12.57	12.57	6.28	6.28	-13.08	-168.9
42	0	-9823	870	573	0	856	-2132	12.57	12.57	6.28	6.28	-13.14	-169.6
43	0	-9592	2261	612	0	962	-5480	12.57	12.57	6.28	6.28	-36.07	1036.8
44	0	-9650	-681	544	0	812	1587	12.57	12.57	6.28	6.28	-9.87	-131.8

45	0	-9684	697	533	0	774	-1726	12.57	12.57	6.28	6.28	-10.64	-140.9
46	0	-9551	584	562	0	855	-1464	12.57	12.57	6.28	6.28	-9.22	-124.0
47	0	-9490	514	553	0	839	-1299	12.57	12.57	6.28	6.28	-8.43	-114.4
49	0	-9479	828	560	0	855	-2053	12.57	12.57	6.28	6.28	-12.65	-163.3
50	0	-9491	240	546	0	825	-640	12.57	12.57	6.28	6.28	-7.54	-97.6
51	0	-9498	516	544	0	818	-1302	12.57	12.57	6.28	6.28	-8.45	-114.6

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	12	-9692	1808	620	0	891	-4158	12.57	12.57	6.28	6.28	-27.18	633.4
41	12	-9723	865	598	0	844	-2015	12.57	12.57	6.28	6.28	-12.39	-161.0
42	12	-9748	870	573	0	784	-2024	12.57	12.57	6.28	6.28	-12.44	-161.6
43	12	-9517	2261	612	0	885	-5197	12.57	12.57	6.28	6.28	-34.20	955.7
44	12	-9575	-681	544	0	744	1502	12.57	12.57	6.28	6.28	-9.42	-126.3
45	12	-9609	697	533	0	708	-1639	12.57	12.57	6.28	6.28	-10.15	-135.0
46	12	-9476	584	562	0	784	-1391	12.57	12.57	6.28	6.28	-8.85	-119.4
47	12	-9415	514	553	0	770	-1235	12.57	12.57	6.28	6.28	-8.13	-110.6
49	12	-9404	828	560	0	785	-1950	12.57	12.57	6.28	6.28	-11.99	-155.7
50	12	-9416	240	546	0	757	-610	12.57	12.57	6.28	6.28	-7.14	-93.1
51	12	-9423	516	544	0	750	-1238	12.57	12.57	6.28	6.28	-8.15	-110.8

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	25	-9617	1808	620	0	814	-3932	12.57	12.57	6.28	6.28	-25.64	571.9
41	25	-9648	865	598	0	769	-1907	12.57	12.57	6.28	6.28	-11.71	-153.2
42	25	-9673	870	573	0	713	-1915	12.57	12.57	6.28	6.28	-11.76	-153.8
43	25	-9442	2261	612	0	809	-4914	12.57	12.57	6.28	6.28	-32.31	874.9
44	25	-9500	-681	544	0	676	1416	12.57	12.57	6.28	6.28	-8.98	-121.0
45	25	-9534	697	533	0	641	-1552	12.57	12.57	6.28	6.28	-9.67	-129.3
46	25	-9401	584	562	0	714	-1318	12.57	12.57	6.28	6.28	-8.49	-115.0
47	25	-9340	514	553	0	700	-1170	12.57	12.57	6.28	6.28	-7.84	-107.0
49	25	-9329	828	560	0	715	-1846	12.57	12.57	6.28	6.28	-11.34	-148.3
50	25	-9341	240	546	0	689	-580	12.57	12.57	6.28	6.28	-6.77	-88.7
51	25	-9348	516	544	0	682	-1174	12.57	12.57	6.28	6.28	-7.85	-107.1

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	38	-9542	1808	620	0	736	-3706	12.57	12.57	6.28	6.28	-24.10	511.0
41	38	-9573	865	598	0	694	-1799	12.57	12.57	6.28	6.28	-11.06	-145.5
42	38	-9598	870	573	0	641	-1806	12.57	12.57	6.28	6.28	-11.10	-146.1
43	38	-9367	2261	612	0	732	-4632	12.57	12.57	6.28	6.28	-30.42	794.5
44	38	-9425	-681	544	0	608	1331	12.57	12.57	6.28	6.28	-8.56	-115.9
45	38	-9459	697	533	0	574	-1465	12.57	12.57	6.28	6.28	-9.21	-123.7
46	38	-9326	584	562	0	644	-1245	12.57	12.57	6.28	6.28	-8.15	-110.7
47	38	-9265	514	553	0	631	-1106	12.57	12.57	6.28	6.28	-7.56	-103.4
49	38	-9254	828	560	0	645	-1742	12.57	12.57	6.28	6.28	-10.71	-140.9
50	38	-9266	240	546	0	620	-550	12.57	12.57	6.28	6.28	-6.40	-84.5
51	38	-9273	516	544	0	614	-1109	12.57	12.57	6.28	6.28	-7.57	-103.6

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	50	-9467	1808	620	0	659	-3480	12.57	12.57	6.28	6.28	-22.54	451.0
41	50	-9498	865	598	0	620	-1691	12.57	12.57	6.28	6.28	-10.42	-138.1
42	50	-9523	870	573	0	570	-1698	12.57	12.57	6.28	6.28	-10.47	-138.6
43	50	-9292	2261	612	0	656	-4349	12.57	12.57	6.28	6.28	-28.52	714.6
44	50	-9350	-681	544	0	540	1246	12.57	12.57	6.28	6.28	-8.16	-110.9
45	50	-9384	697	533	0	508	-1378	12.57	12.57	6.28	6.28	-8.77	-118.3
46	50	-9251	584	562	0	574	-1172	12.57	12.57	6.28	6.28	-7.82	-106.6
47	50	-9190	514	553	0	562	-1042	12.57	12.57	6.28	6.28	-7.29	-99.9
49	50	-9179	828	560	0	575	-1639	12.57	12.57	6.28	6.28	-10.10	-133.8
50	50	-9191	240	546	0	552	-520	12.57	12.57	6.28	6.28	-6.04	-80.3
51	50	-9198	516	544	0	546	-1045	12.57	12.57	6.28	6.28	-7.30	-100.1

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

ASTA NUM. 98 NI 479 NF 595 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 7
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-979	45	-327	0	-7	-28	6.28	6.28	9.42	9.42	-0.73	-9.6
41	0	-1069	194	-163	0	33	-76	6.28	6.28	9.42	9.42	-1.25	-14.9
42	0	-770	-98	-1072	0	-409	3	6.28	6.28	9.42	9.42	-3.18	75.7
43	0	-1000	-75	-456	0	-28	21	6.28	6.28	9.42	9.42	-0.68	-9.2
44	0	-1233	447	111	0	96	-160	6.28	6.28	9.42	9.42	-2.50	-25.7
45	0	-651	-313	-1698	0	-698	73	6.28	6.28	9.42	9.42	-5.33	173.7
46	0	-1200	161	-194	0	42	-49	6.28	6.28	9.42	9.42	-1.03	-13.2
47	0	-1232	153	-202	0	44	-42	6.28	6.28	9.42	9.42	-0.98	-12.8
49	0	-1202	103	-257	0	31	-26	6.28	6.28	9.42	9.42	-0.82	-11.1
50	0	-1249	207	-144	0	56	-62	6.28	6.28	9.42	9.42	-1.17	-14.7
51	0	-1132	55	-505	0	-103	-16	6.28	6.28	9.42	9.42	-1.04	-14.4

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	12	-923	45	-327	0	34	-22	6.28	6.28	9.42	9.42	-0.65	-8.9
41	12	-1013	194	-163	0	53	-52	6.28	6.28	9.42	9.42	-0.97	-12.1
42	12	-713	-98	-1072	0	-275	-9	6.28	6.28	9.42	9.42	-2.14	39.1
43	12	-944	-75	-456	0	29	12	6.28	6.28	9.42	9.42	-0.61	-8.8
44	12	-1177	447	111	0	82	-104	6.28	6.28	9.42	9.42	-1.63	-18.7
45	12	-595	-313	-1698	0	-485	34	6.28	6.28	9.42	9.42	-3.74	110.9
46	12	-1144	161	-194	0	66	-29	6.28	6.28	9.42	9.42	-0.88	-12.4
47	12	-1176	153	-202	0	69	-23	6.28	6.28	9.42	9.42	-0.91	-12.8
49	12	-1146	103	-257	0	63	-13	6.28	6.28	9.42	9.42	-0.86	-12.2
50	12	-1193	207	-144	0	74	-36	6.28	6.28	9.42	9.42	-0.94	-13.2
51	12	-1076	55	-505	0	-40	-9	6.28	6.28	9.42	9.42	-0.72	-10.4

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	25	-866	45	-327	0	75	-17	6.28	6.28	9.42	9.42	-0.78	-10.8
41	25	-957	194	-163	0	73	-28	6.28	6.28	9.42	9.42	-0.82	-11.4
42	25	-657	-98	-1072	0	-141	-22	6.28	6.28	9.42	9.42	-1.09	-14.1
43	25	-888	-75	-456	0	86	3	6.28	6.28	9.42	9.42	-0.84	-11.6
44	25	-1120	447	111	0	69	-48	6.28	6.28	9.42	9.42	-0.98	-12.5
45	25	-539	-313	-1698	0	-273	-6	6.28	6.28	9.42	9.42	-2.13	49.0

46	25	-1087	161	-194	0	90	-9	6.28	6.28	9.42	9.42	-0.96	-13.4
47	25	-1120	153	-202	0	95	-4	6.28	6.28	9.42	9.42	-0.99	-13.8
49	25	-1090	103	-257	0	95	-0	6.28	6.28	9.42	9.42	-0.98	-13.6
50	25	-1136	207	-144	0	92	-11	6.28	6.28	9.42	9.42	-0.99	-13.8
51	25	-1020	55	-505	0	23	-2	6.28	6.28	9.42	9.42	-0.62	-9.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	38	-810	45	-327	0	116	-11	6.28	6.28	9.42	9.42	-0.95	-12.8
41	38	-900	194	-163	0	94	-4	6.28	6.28	9.42	9.42	-0.88	-12.1
42	38	-601	-98	-1072	0	-7	-34	6.28	6.28	9.42	9.42	-0.60	-7.4
43	38	-831	-75	-456	0	143	-7	6.28	6.28	9.42	9.42	-1.13	-15.0
44	38	-1064	447	111	0	55	8	6.28	6.28	9.42	9.42	-0.78	-11.1
45	38	-483	-313	-1698	0	-61	-45	6.28	6.28	9.42	9.42	-0.70	-7.9
46	38	-1031	161	-194	0	115	11	6.28	6.28	9.42	9.42	-1.04	-14.3
47	38	-1063	153	-202	0	120	15	6.28	6.28	9.42	9.42	-1.08	-14.9
49	38	-1033	103	-257	0	127	13	6.28	6.28	9.42	9.42	-1.10	-15.1
50	38	-1080	207	-144	0	109	15	6.28	6.28	9.42	9.42	-1.04	-14.4
51	38	-963	55	-505	0	86	5	6.28	6.28	9.42	9.42	-0.88	-12.2

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	50	-754	45	-327	0	156	-5	6.28	6.28	9.42	9.42	-1.21	-15.8
41	50	-844	194	-163	0	114	21	6.28	6.28	9.42	9.42	-0.95	-13.0
42	50	-544	-98	-1072	0	127	-46	6.28	6.28	9.42	9.42	-0.98	-12.6
43	50	-775	-75	-456	0	200	-16	6.28	6.28	9.42	9.42	-1.55	-19.6
44	50	-1008	447	111	0	41	63	6.28	6.28	9.42	9.42	-1.07	-13.1
45	50	-426	-313	-1698	0	152	-84	6.28	6.28	9.42	9.42	-1.33	19.7
46	50	-975	161	-194	0	139	31	6.28	6.28	9.42	9.42	-1.14	-15.5
47	50	-1007	153	-202	0	145	34	6.28	6.28	9.42	9.42	-1.19	-16.1
49	50	-977	103	-257	0	159	25	6.28	6.28	9.42	9.42	-1.26	-16.9
50	50	-1024	207	-144	0	127	41	6.28	6.28	9.42	9.42	-1.10	-15.0
51	50	-907	55	-505	0	150	12	6.28	6.28	9.42	9.42	-1.18	-15.8

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 99 NI 595 NF 23 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 7A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	--												
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-1069	55	-331	0	246	13	6.28	6.28	9.42	9.42	-1.89	-24.4
41	0	-1206	231	-210	0	193	59	6.28	6.28	9.42	9.42	-1.54	-20.6
42	0	-980	137	-483	0	426	45	6.28	6.28	9.42	9.42	-3.32	67.8
43	0	-1031	-32	-431	0	284	-20	6.28	6.28	9.42	9.42	-2.20	-27.6
44	0	-1466	520	-3	0	105	136	6.28	6.28	9.42	9.42	-2.12	-24.0
45	0	-883	106	-685	0	585	33	6.28	6.28	9.42	9.42	-4.53	122.5
46	0	-1292	281	-242	0	198	54	6.28	6.28	9.42	9.42	-1.59	-21.5
47	0	-1313	293	-250	0	200	53	6.28	6.28	9.42	9.42	-1.61	-21.7
49	0	-1267	234	-290	0	217	37	6.28	6.28	9.42	9.42	-1.71	-22.8
50	0	-1354	345	-204	0	181	69	6.28	6.28	9.42	9.42	-1.52	-20.7
51	0	-1238	262	-340	0	277	48	6.28	6.28	9.42	9.42	-2.13	-27.6

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	12	-1013	55	-331	0	287	20	6.28	6.28	9.42	9.42	-2.22	-27.8
41	12	-1150	231	-210	0	219	88	6.28	6.28	9.42	9.42	-1.70	-22.4
42	12	-924	137	-483	0	486	62	6.28	6.28	9.42	9.42	-3.79	89.5
43	12	-975	-32	-431	0	338	-24	6.28	6.28	9.42	9.42	-2.63	42.7
44	12	-1410	520	-3	0	105	201	6.28	6.28	9.42	9.42	-3.14	31.6
45	12	-827	106	-685	0	671	46	6.28	6.28	9.42	9.42	-5.16	153.0
46	12	-1236	281	-242	0	228	89	6.28	6.28	9.42	9.42	-1.78	-23.5
47	12	-1257	293	-250	0	231	89	6.28	6.28	9.42	9.42	-1.80	-23.8
49	12	-1211	234	-290	0	253	67	6.28	6.28	9.42	9.42	-1.95	-25.5
50	12	-1298	345	-204	0	207	112	6.28	6.28	9.42	9.42	-1.76	-22.1
51	12	-1182	262	-340	0	320	81	6.28	6.28	9.42	9.42	-2.47	-31.1

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	25	-957	55	-331	0	328	27	6.28	6.28	9.42	9.42	-2.55	40.9
41	25	-1094	231	-210	0	245	116	6.28	6.28	9.42	9.42	-1.89	-24.4
42	25	-868	137	-483	0	547	79	6.28	6.28	9.42	9.42	-4.24	111.7
43	25	-919	-32	-431	0	392	-28	6.28	6.28	9.42	9.42	-3.06	61.4
44	25	-1354	520	-3	0	105	266	6.28	6.28	9.42	9.42	-4.20	62.4
45	25	-770	106	-685	0	756	59	6.28	6.28	9.42	9.42	-5.79	183.7
46	25	-1180	281	-242	0	259	124	6.28	6.28	9.42	9.42	-1.99	-25.8
47	25	-1200	293	-250	0	262	126	6.28	6.28	9.42	9.42	-2.02	-26.2
49	25	-1154	234	-290	0	290	96	6.28	6.28	9.42	9.42	-2.23	-28.4
50	25	-1242	345	-204	0	232	155	6.28	6.28	9.42	9.42	-2.41	-25.1
51	25	-1126	262	-340	0	362	113	6.28	6.28	9.42	9.42	-2.81	41.6

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	38	-900	55	-331	0	370	34	6.28	6.28	9.42	9.42	-2.88	55.9
41	38	-1037	231	-210	0	272	145	6.28	6.28	9.42	9.42	-2.27	-26.6
42	38	-811	137	-483	0	607	96	6.28	6.28	9.42	9.42	-4.69	134.3
43	38	-863	-32	-431	0	446	-32	6.28	6.28	9.42	9.42	-3.47	81.0
44	38	-1297	520	-3	0	106	331	6.28	6.28	9.42	9.42	-5.24	95.1
45	38	-714	106	-685	0	842	72	6.28	6.28	9.42	9.42	-6.41	214.6
46	38	-1123	281	-242	0	289	159	6.28	6.28	9.42	9.42	-2.49	-28.3
47	38	-1144	293	-250	0	293	162	6.28	6.28	9.42	9.42	-2.54	-28.7
49	38	-1098	234	-290	0	326	125	6.28	6.28	9.42	9.42	-2.52	33.2
50	38	-1185	345	-204	0	258	198	6.28	6.28	9.42	9.42	-3.12	39.0
51	38	-1069	262	-340	0	405	146	6.28	6.28	9.42	9.42	-3.15	56.5

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	50	-844	55	-331	0	411	41	6.28	6.28	9.42	9.42	-3.20	71.7
41	50	-981	231	-210	0	298	174	6.28	6.28	9.42	9.42	-2.75	36.8
42	50	-755	137	-483	0	668	113	6.28	6.28	9.42	9.42	-5.13	157.0
43	50	-806	-32	-431	0	500	-36	6.28	6.28	9.42	9.42	-3.88	101.2
44	50	-1241	520	-3	0	106	396	6.28	6.28	9.42	9.42	-6.27	128.6
45	50	-658	106	-685	0	927	85	6.28	6.28	9.42	9.42	-7.02	245.6
46	50	-1067	281	-242	0	319	194	6.28	6.28	9.42	9.42	-3.06	42.2

47	50	-1088	293	-250	0	324	199	6.28	6.28	9.42	9.42	-3.14	43.6
49	50	-1042	234	-290	0	362	155	6.28	6.28	9.42	9.42	-2.82	45.8
50	50	-1129	345	-204	0	283	241	6.28	6.28	9.42	9.42	-3.81	60.9
51	50	-1013	262	-340	0	448	179	6.28	6.28	9.42	9.42	-3.49	72.3

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 100 NI 606 NF 624 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 1
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-7170	-818	487	0	-199	381	6.28	6.28	9.42	9.42	-6.95	-86.7
41	0	-7855	-525	260	0	-241	336	6.28	6.28	9.42	9.42	-6.86	-87.4
42	0	-7645	-515	131	0	-215	328	6.28	6.28	9.42	9.42	-6.69	-85.2
43	0	-6305	-997	623	0	-141	405	6.28	6.28	9.42	9.42	-6.82	-83.1
44	0	-9065	-43	-114	0	-317	263	6.28	6.28	9.42	9.42	-6.77	-89.4
45	0	-7097	-492	31	0	-168	317	6.28	6.28	9.42	9.42	-6.32	-80.2
46	0	-7203	-501	238	0	-194	326	6.28	6.28	9.42	9.42	-6.45	-81.8
47	0	-7040	-495	232	0	-182	324	6.28	6.28	9.42	9.42	-6.35	-80.4
49	0	-6811	-592	307	0	-168	339	6.28	6.28	9.42	9.42	-6.38	-80.2
50	0	-7363	-402	160	0	-203	310	6.28	6.28	9.42	9.42	-6.39	-81.5
51	0	-6969	-492	189	0	-173	321	6.28	6.28	9.42	9.42	-6.29	-79.7

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	12	-7114	-818	487	0	-260	279	6.28	6.28	9.42	9.42	-5.98	-76.9
41	12	-7799	-525	260	0	-274	270	6.28	6.28	9.42	9.42	-6.23	-81.0
42	12	-7589	-515	131	0	-231	264	6.28	6.28	9.42	9.42	-6.07	-78.9
43	12	-6249	-997	623	0	-219	281	6.28	6.28	9.42	9.42	-5.58	-70.8
44	12	-9009	-43	-114	0	-303	257	6.28	6.28	9.42	9.42	-6.69	-88.5
45	12	-7041	-492	31	0	-172	255	6.28	6.28	9.42	9.42	-5.72	-74.1
46	12	-7147	-501	238	0	-224	263	6.28	6.28	9.42	9.42	-5.85	-75.7
47	12	-6984	-495	232	0	-211	262	6.28	6.28	9.42	9.42	-5.76	-74.3
49	12	-6755	-592	307	0	-206	265	6.28	6.28	9.42	9.42	-5.67	-73.0
50	12	-7307	-402	160	0	-223	260	6.28	6.28	9.42	9.42	-5.90	-76.5
51	12	-6913	-492	189	0	-197	259	6.28	6.28	9.42	9.42	-5.70	-73.6

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	25	-7058	-818	487	0	-320	177	6.28	6.28	9.42	9.42	-5.01	-71.5
41	25	-7742	-525	260	0	-306	205	6.28	6.28	9.42	9.42	-5.60	-75.9
42	25	-7532	-515	131	0	-248	200	6.28	6.28	9.42	9.42	-5.45	-72.6
43	25	-6192	-997	623	0	-297	156	6.28	6.28	9.42	9.42	-4.47	-63.6
44	25	-8952	-43	-114	0	-289	252	6.28	6.28	9.42	9.42	-6.61	-87.6
45	25	-6984	-492	31	0	-175	194	6.28	6.28	9.42	9.42	-5.13	-68.1
46	25	-7090	-501	238	0	-253	201	6.28	6.28	9.42	9.42	-5.25	-69.5
47	25	-6928	-495	232	0	-240	200	6.28	6.28	9.42	9.42	-5.16	-68.2
49	25	-6698	-592	307	0	-245	191	6.28	6.28	9.42	9.42	-4.97	-65.7
50	25	-7250	-402	160	0	-243	210	6.28	6.28	9.42	9.42	-5.41	-71.5
51	25	-6856	-492	189	0	-221	198	6.28	6.28	9.42	9.42	-5.11	-67.6

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	38	-7001	-818	487	0	-381	75	6.28	6.28	9.42	9.42	-5.26	-74.6
41	38	-7686	-525	260	0	-339	139	6.28	6.28	9.42	9.42	-5.41	-77.3
42	38	-7476	-515	131	0	-264	135	6.28	6.28	9.42	9.42	-4.96	-71.4
43	38	-6136	-997	623	0	-375	31	6.28	6.28	9.42	9.42	-4.80	-67.7
44	38	-8896	-43	-114	0	-274	247	6.28	6.28	9.42	9.42	-6.54	-86.7
45	38	-6928	-492	31	0	-179	132	6.28	6.28	9.42	9.42	-4.54	-62.5
46	38	-7034	-501	238	0	-283	138	6.28	6.28	9.42	9.42	-4.83	-69.2
47	38	-6871	-495	232	0	-269	138	6.28	6.28	9.42	9.42	-4.68	-67.2
49	38	-6642	-592	307	0	-283	116	6.28	6.28	9.42	9.42	-4.63	-66.3
50	38	-7194	-402	160	0	-263	160	6.28	6.28	9.42	9.42	-4.92	-69.3
51	38	-6800	-492	189	0	-244	137	6.28	6.28	9.42	9.42	-4.53	-65.2

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	50	-6945	-818	487	0	-442	-28	6.28	6.28	9.42	9.42	-5.51	-77.6
41	50	-7630	-525	260	0	-371	73	6.28	6.28	9.42	9.42	-5.53	-78.7
42	50	-7420	-515	131	0	-280	71	6.28	6.28	9.42	9.42	-5.01	-72.0
43	50	-6080	-997	623	0	-453	-93	6.28	6.28	9.42	9.42	-5.12	-71.7
44	50	-8840	-43	-114	0	-260	241	6.28	6.28	9.42	9.42	-6.46	-85.8
45	50	-6872	-492	31	0	-183	70	6.28	6.28	9.42	9.42	-4.29	-62.3
46	50	-6978	-501	238	0	-313	76	6.28	6.28	9.42	9.42	-4.94	-70.5
47	50	-6815	-495	232	0	-298	76	6.28	6.28	9.42	9.42	-4.79	-68.4
49	50	-6586	-592	307	0	-322	42	6.28	6.28	9.42	9.42	-4.78	-68.0
50	50	-7138	-402	160	0	-283	109	6.28	6.28	9.42	9.42	-4.88	-70.0
51	50	-6744	-492	189	0	-268	75	6.28	6.28	9.42	9.42	-4.61	-66.1

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 101 NI 624 NF 293 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 1A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-9032	-1111	190	0	-476	-68	6.28	6.28	9.42	9.42	-6.71	-95.3
41	0	-9591	-105	-34	0	-386	68	6.28	6.28	9.42	9.42	-6.59	-94.4
42	0	-9378	-108	-299	0	-282	67	6.28	6.28	9.42	9.42	-6.00	-86.8
43	0	-8114	-1731	294	0	-494	-163	6.28	6.28	9.42	9.42	-6.34	-89.4
44	0	-10610	1563	-398	0	-245	295	6.28	6.28	9.42	9.42	-7.80	-103.5
45	0	-8692	-59	-521	0	-171	61	6.28	6.28	9.42	9.42	-5.15	-75.3
46	0	-8720	-24	-107	0	-321	60	6.28	6.28	9.42	9.42	-5.85	-84.1
47	0	-8502	-3	-125	0	-304	58	6.28	6.28	9.42	9.42	-5.66	-81.5
49	0	-8316	-339	-51	0	-334	13	6.28	6.28	9.42	9.42	-5.70	-81.8
50	0	-8815	320	-189	0	-284	104	6.28	6.28	9.42	9.42	-5.73	-82.7
51	0	-8432	-4	-214	0	-269	58	6.28	6.28	9.42	9.42	-5.47	-78.9

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	12	-8976	-1111	190	0	-500	-207	6.28	6.28	9.42	9.42	-6.79	-96.2
41	12	-9535	-105	-34	0	-382	55	6.28	6.28	9.42	9.42	-6.54	-93.7
42	12	-9322	-108	-299	0	-244	54	6.28	6.28	9.42	9.42	-5.80	-84.2
43	12	-8058	-1731	294	0	-531	-380	6.28	6.28	9.42	9.42	-7.36	-92.9
44	12	-10552	1563	-398	0	-195	490	6.28	6.28	9.42	9.42	-9.57	-121.0
45	12	-8636	-59	-521	0	-105	54	6.28	6.28	9.42	9.42	-4.82	-71.2
46	12	-8664	-24	-107	0	-307	57	6.28	6.28	9.42	9.42	-5.76	-82.9
47	12	-8446	-3	-125	0	-288	58	6.28	6.28	9.42	9.42	-5.56	-80.2
49	12	-8260	-339	-51	0	-328	-29	6.28	6.28	9.42	9.42	-5.65	-81.0
50	12	-8759	320	-189	0	-260	144	6.28	6.28	9.42	9.42	-5.59	-80.9
51	12	-8376	-4	-214	0	-242	57	6.28	6.28	9.42	9.42	-5.32	-77.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	25	-8920	-1111	190	0	-524	-345	6.28	6.28	9.42	9.42	-7.46	-97.1
41	25	-9478	-105	-34	0	-378	42	6.28	6.28	9.42	9.42	-6.49	-93.0
42	25	-9266	-108	-299	0	-207	40	6.28	6.28	9.42	9.42	-5.60	-81.7
43	25	-8002	-1731	294	0	-568	-596	6.28	6.28	9.42	9.42	-9.61	-114.3
44	25	-10495	1563	-398	0	-145	685	6.28	6.28	9.42	9.42	-11.47	-139.5
45	25	-8580	-59	-521	0	-40	47	6.28	6.28	9.42	9.42	-4.55	-67.0
46	25	-8608	-24	-107	0	-294	54	6.28	6.28	9.42	9.42	-5.67	-81.7
47	25	-8390	-3	-125	0	-273	57	6.28	6.28	9.42	9.42	-5.46	-78.8
49	25	-8204	-339	-51	0	-321	-72	6.28	6.28	9.42	9.42	-5.59	-80.2
50	25	-8702	320	-189	0	-237	184	6.28	6.28	9.42	9.42	-5.87	-79.6
51	25	-8320	-4	-214	0	-216	57	6.28	6.28	9.42	9.42	-5.17	-75.1

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	38	-8863	-1111	190	0	-547	-484	6.28	6.28	9.42	9.42	-8.71	-108.3
41	38	-9422	-105	-34	0	-374	29	6.28	6.28	9.42	9.42	-6.44	-92.4
42	38	-9209	-108	-299	0	-170	27	6.28	6.28	9.42	9.42	-5.40	-79.1
43	38	-7945	-1731	294	0	-605	-813	6.28	6.28	9.42	9.42	-12.64	-139.6
44	38	-10438	1563	-398	0	-95	881	6.28	6.28	9.42	9.42	-13.88	-161.0
45	38	-8523	-59	-521	0	25	39	6.28	6.28	9.42	9.42	-4.45	-65.7
46	38	-8551	-24	-107	0	-280	51	6.28	6.28	9.42	9.42	-5.58	-80.5
47	38	-8333	-3	-125	0	-257	57	6.28	6.28	9.42	9.42	-5.36	-77.5
49	38	-8147	-339	-51	0	-315	-114	6.28	6.28	9.42	9.42	-5.53	-79.4
50	38	-8646	320	-189	0	-213	224	6.28	6.28	9.42	9.42	-6.21	-82.9
51	38	-8263	-4	-214	0	-189	56	6.28	6.28	9.42	9.42	-5.02	-73.1

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	50	-8807	-1111	190	0	-571	-623	6.28	6.28	9.42	9.42	-10.17	-122.2
41	50	-9366	-105	-34	0	-370	16	6.28	6.28	9.42	9.42	-6.40	-91.7
42	50	-9153	-108	-299	0	-132	13	6.28	6.28	9.42	9.42	-5.21	-76.6
43	50	-7889	-1731	294	0	-642	-1029	6.28	6.28	9.42	9.42	-16.07	-165.0
44	50	-10380	1563	-398	0	-46	1076	6.28	6.28	9.42	9.42	-16.73	-184.2
45	50	-8467	-59	-521	0	90	32	6.28	6.28	9.42	9.42	-4.67	-69.0
46	50	-8495	-24	-107	0	-267	48	6.28	6.28	9.42	9.42	-5.49	-79.3
47	50	-8277	-3	-125	0	-241	57	6.28	6.28	9.42	9.42	-5.26	-76.2
49	50	-8091	-339	-51	0	-309	-156	6.28	6.28	9.42	9.42	-5.48	-78.6
50	50	-8590	320	-189	0	-190	264	6.28	6.28	9.42	9.42	-6.55	-86.2
51	50	-8207	-4	-214	0	-162	56	6.28	6.28	9.42	9.42	-4.87	-71.2

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 102 NI 218 NF 132 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 12
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	

40	0	-6452	53	-99	0	333	-5	6.28	6.28	12.57	12.57	-3.69	-52.3
41	0	-6179	127	-41	0	172	-11	6.28	6.28	12.57	12.57	-3.00	-43.5
42	0	-6210	112	-206	0	1592	-8	6.28	6.28	12.57	12.57	-9.96	-125.2
43	0	-6430	6	-127	0	399	-3	6.28	6.28	12.57	12.57	-3.91	-55.1
44	0	-5841	250	52	0	-85	-20	6.28	6.28	12.57	12.57	-2.56	-37.6
45	0	-6025	104	-306	0	2497	-7	6.28	6.28	12.57	12.57	-16.29	368.1
46	0	-5852	129	-25	0	106	-13	6.28	6.28	12.57	12.57	-2.64	-38.7
47	0	-5770	130	-21	0	90	-13	6.28	6.28	12.57	12.57	-2.55	-37.5
49	0	-5861	106	-40	0	143	-11	6.28	6.28	12.57	12.57	-2.78	-40.4
50	0	-5744	154	-4	0	47	-15	6.28	6.28	12.57	12.57	-2.39	-35.4
51	0	-5781	125	-75	0	563	-12	6.28	6.28	12.57	12.57	-4.25	-58.7

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	12	-6377	53	-99	0	346	1	6.28	6.28	12.57	12.57	-3.70	-52.4
41	12	-6104	127	-41	0	178	5	6.28	6.28	12.57	12.57	-2.99	-43.3
42	12	-6135	112	-206	0	1618	6	6.28	6.28	12.57	12.57	-10.15	-127.0
43	12	-6355	6	-127	0	415	-2	6.28	6.28	12.57	12.57	-3.94	-55.4
44	12	-5766	250	52	0	-91	12	6.28	6.28	12.57	12.57	-2.55	-37.5
45	12	-5950	104	-306	0	2535	6	6.28	6.28	12.57	12.57	-16.57	383.8
46	12	-5777	129	-25	0	109	4	6.28	6.28	12.57	12.57	-2.62	-38.4
47	12	-5695	130	-21	0	92	3	6.28	6.28	12.57	12.57	-2.53	-37.1
49	12	-5786	106	-40	0	148	2	6.28	6.28	12.57	12.57	-2.77	-40.2
50	12	-5669	154	-4	0	47	5	6.28	6.28	12.57	12.57	-2.36	-35.0
51	12	-5706	125	-75	0	572	4	6.28	6.28	12.57	12.57	-4.25	-58.7

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	25	-6302	53	-99	0	358	8	6.28	6.28	12.57	12.57	-3.72	-52.5
41	25	-6029	127	-41	0	183	21	6.28	6.28	12.57	12.57	-2.98	-43.1
42	25	-6060	112	-206	0	1644	20	6.28	6.28	12.57	12.57	-10.34	134.5
43	25	-6280	6	-127	0	431	-2	6.28	6.28	12.57	12.57	-3.97	-55.7
44	25	-5691	250	52	0	-98	43	6.28	6.28	12.57	12.57	-2.55	-37.4
45	25	-5875	104	-306	0	2574	18	6.28	6.28	12.57	12.57	-16.84	399.6
46	25	-5702	129	-25	0	112	20	6.28	6.28	12.57	12.57	-2.61	-38.1
47	25	-5620	130	-21	0	95	19	6.28	6.28	12.57	12.57	-2.51	-36.8
49	25	-5711	106	-40	0	153	15	6.28	6.28	12.57	12.57	-2.76	-40.0
50	25	-5594	154	-4	0	48	24	6.28	6.28	12.57	12.57	-2.33	-34.5
51	25	-5631	125	-75	0	582	19	6.28	6.28	12.57	12.57	-4.26	-58.7

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	38	-6227	53	-99	0	370	14	6.28	6.28	12.57	12.57	-3.73	-52.7
41	38	-5954	127	-41	0	188	37	6.28	6.28	12.57	12.57	-2.97	-42.9
42	38	-5985	112	-206	0	1669	34	6.28	6.28	12.57	12.57	-10.54	143.9
43	38	-6205	6	-127	0	447	-1	6.28	6.28	12.57	12.57	-4.00	-56.0
44	38	-5616	250	52	0	-104	74	6.28	6.28	12.57	12.57	-2.54	-37.2
45	38	-5800	104	-306	0	2612	31	6.28	6.28	12.57	12.57	-17.10	415.5
46	38	-5627	129	-25	0	116	36	6.28	6.28	12.57	12.57	-2.59	-37.8
47	38	-5545	130	-21	0	97	36	6.28	6.28	12.57	12.57	-2.49	-36.5
49	38	-5636	106	-40	0	158	28	6.28	6.28	12.57	12.57	-2.74	-39.7
50	38	-5519	154	-4	0	48	43	6.28	6.28	12.57	12.57	-2.30	-34.1
51	38	-5556	125	-75	0	591	35	6.28	6.28	12.57	12.57	-4.26	-58.7

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	50	-6152	53	-99	0	383	21	6.28	6.28	12.57	12.57	-3.75	-52.8
41	50	-5879	127	-41	0	193	53	6.28	6.28	12.57	12.57	-2.96	-42.7
42	50	-5910	112	-206	0	1695	48	6.28	6.28	12.57	12.57	-10.73	153.6
43	50	-6130	6	-127	0	463	-0	6.28	6.28	12.57	12.57	-4.02	-56.2
44	50	-5541	250	52	0	-111	106	6.28	6.28	12.57	12.57	-2.54	-37.1
45	50	-5725	104	-306	0	2650	44	6.28	6.28	12.57	12.57	-17.37	431.5
46	50	-5552	129	-25	0	119	52	6.28	6.28	12.57	12.57	-2.57	-37.5
47	50	-5470	130	-21	0	100	52	6.28	6.28	12.57	12.57	-2.47	-36.2
49	50	-5561	106	-40	0	163	42	6.28	6.28	12.57	12.57	-2.73	-39.5
50	50	-5444	154	-4	0	49	63	6.28	6.28	12.57	12.57	-2.28	-33.7
51	50	-5481	125	-75	0	601	50	6.28	6.28	12.57	12.57	-4.27	-58.7

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 103 NI 132 NF 40 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 12A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-9713	225	-175	0	365	21	6.28	6.28	12.57	12.57	-5.06	-72.6
41	0	-9270	537	-72	0	181	53	6.28	6.28	12.57	12.57	-4.23	-61.8
42	0	-9304	501	-347	0	1537	48	6.28	6.28	12.57	12.57	-9.55	-127.5
43	0	-9684	6	-226	0	443	-0	6.28	6.28	12.57	12.57	-5.33	-76.0
44	0	-8718	1065	94	0	-114	106	6.28	6.28	12.57	12.57	-3.77	-55.6
45	0	-9003	466	-512	0	2398	44	6.28	6.28	12.57	12.57	-15.06	189.5
46	0	-8753	520	-43	0	111	52	6.28	6.28	12.57	12.57	-3.78	-55.7
47	0	-8623	516	-36	0	94	52	6.28	6.28	12.57	12.57	-3.67	-54.2
49	0	-8771	412	-70	0	155	42	6.28	6.28	12.57	12.57	-3.94	-57.8
50	0	-8577	624	-6	0	43	63	6.28	6.28	12.57	12.57	-3.47	-51.6
51	0	-8634	504	-128	0	546	50	6.28	6.28	12.57	12.57	-5.29	-74.5

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	12	-9638	225	-175	0	387	49	6.28	6.28	12.57	12.57	-5.11	-73.2
41	12	-9195	537	-72	0	190	120	6.28	6.28	12.57	12.57	-4.23	-61.8
42	12	-9229	501	-347	0	1580	110	6.28	6.28	12.57	12.57	-9.78	-130.1
43	12	-9609	6	-226	0	472	1	6.28	6.28	12.57	12.57	-5.40	-76.8
44	12	-8643	1065	94	0	-125	239	6.28	6.28	12.57	12.57	-4.29	-60.0
45	12	-8928	466	-512	0	2462	103	6.28	6.28	12.57	12.57	-15.52	207.8
46	12	-8678	520	-43	0	116	117	6.28	6.28	12.57	12.57	-3.77	-55.5
47	12	-8548	516	-36	0	98	116	6.28	6.28	12.57	12.57	-3.65	-53.9
49	12	-8696	412	-70	0	163	93	6.28	6.28	12.57	12.57	-3.94	-57.7
50	12	-8502	624	-6	0	44	141	6.28	6.28	12.57	12.57	-3.76	-53.7
51	12	-8559	504	-128	0	562	113	6.28	6.28	12.57	12.57	-5.32	-74.7

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	25	-9563	225	-175	0	408	77	6.28	6.28	12.57	12.57	-5.16	-73.7
41	25	-9120	537	-72	0	199	187	6.28	6.28	12.57	12.57	-4.24	-61.8
42	25	-9154	501	-347	0	1624	173	6.28	6.28	12.57	12.57	-10.01	-132.7
43	25	-9534	6	-226	0	500	1	6.28	6.28	12.57	12.57	-5.47	-77.6
44	25	-8568	1065	94	0	-137	372	6.28	6.28	12.57	12.57	-4.92	-67.0
45	25	-8853	466	-512	0	2526	161	6.28	6.28	12.57	12.57	-15.99	226.8
46	25	-8603	520	-43	0	122	182	6.28	6.28	12.57	12.57	-4.00	-56.6
47	25	-8473	516	-36	0	102	181	6.28	6.28	12.57	12.57	-3.95	-55.8
49	25	-8621	412	-70	0	172	144	6.28	6.28	12.57	12.57	-3.95	-57.7
50	25	-8427	624	-6	0	45	219	6.28	6.28	12.57	12.57	-4.11	-57.7
51	25	-8484	504	-128	0	577	176	6.28	6.28	12.57	12.57	-5.35	-75.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	38	-9488	225	-175	0	430	105	6.28	6.28	12.57	12.57	-5.21	-74.2
41	38	-9045	537	-72	0	208	254	6.28	6.28	12.57	12.57	-4.51	-63.0
42	38	-9079	501	-347	0	1668	236	6.28	6.28	12.57	12.57	-10.26	-135.4
43	38	-9459	6	-226	0	528	2	6.28	6.28	12.57	12.57	-5.54	-78.4
44	38	-8493	1065	94	0	-149	505	6.28	6.28	12.57	12.57	-5.55	-73.9
45	38	-8778	466	-512	0	2590	219	6.28	6.28	12.57	12.57	-16.45	246.3
46	38	-8528	520	-43	0	127	247	6.28	6.28	12.57	12.57	-4.29	-59.8
47	38	-8398	516	-36	0	107	246	6.28	6.28	12.57	12.57	-4.24	-59.0
49	38	-8546	412	-70	0	181	196	6.28	6.28	12.57	12.57	-4.05	-57.6
50	38	-8352	624	-6	0	46	297	6.28	6.28	12.57	12.57	-4.47	-61.6
51	38	-8409	504	-128	0	593	239	6.28	6.28	12.57	12.57	-5.37	-75.3

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	50	-9413	225	-175	0	452	134	6.28	6.28	12.57	12.57	-5.26	-74.8
41	50	-8970	537	-72	0	217	321	6.28	6.28	12.57	12.57	-4.82	-66.3
42	50	-9004	501	-347	0	1711	298	6.28	6.28	12.57	12.57	-10.51	-138.2
43	50	-9384	6	-226	0	556	3	6.28	6.28	12.57	12.57	-5.62	-79.3
44	50	-8418	1065	94	0	-160	638	6.28	6.28	12.57	12.57	-6.19	-81.0
45	50	-8703	466	-512	0	2654	278	6.28	6.28	12.57	12.57	-16.91	266.3
46	50	-8453	520	-43	0	133	312	6.28	6.28	12.57	12.57	-4.59	-63.0
47	50	-8323	516	-36	0	111	310	6.28	6.28	12.57	12.57	-4.53	-62.2
49	50	-8471	412	-70	0	190	248	6.28	6.28	12.57	12.57	-4.27	-59.5
50	50	-8277	624	-6	0	46	374	6.28	6.28	12.57	12.57	-4.83	-65.5
51	50	-8334	504	-128	0	609	302	6.28	6.28	12.57	12.57	-5.40	-75.6

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 104 NI 1350 NF 1445 SEZ. Rp B= 0.400 H= 0.600 (pilastro)
PIL. NUM. 11
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-6124	1229	380	0	759	-4394	12.57	12.57	6.28	6.28	-28.92	937.0
41	0	-6493	600	354	0	682	-2356	12.57	12.57	6.28	6.28	-15.25	300.6
42	0	-6481	603	324	0	594	-2365	12.57	12.57	6.28	6.28	-15.31	303.8
43	0	-5875	1536	389	0	791	-5401	12.57	12.57	6.28	6.28	-35.44	1267.0
44	0	-7000	-430	306	0	546	986	12.57	12.57	6.28	6.28	-6.34	-85.9
45	0	-6469	494	297	0	515	-2020	12.57	12.57	6.28	6.28	-12.90	210.2
46	0	-6487	421	342	0	649	-1793	12.57	12.57	6.28	6.28	-11.31	152.0
47	0	-6486	376	338	0	641	-1652	12.57	12.57	6.28	6.28	-10.33	-130.0
49	0	-6363	585	347	0	667	-2331	12.57	12.57	6.28	6.28	-15.10	300.9
50	0	-6588	192	330	0	618	-1054	12.57	12.57	6.28	6.28	-6.58	-88.2
51	0	-6482	377	329	0	612	-1655	12.57	12.57	6.28	6.28	-10.35	-130.2

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	12	-6049	1229	380	0	712	-4240	12.57	12.57	6.28	6.28	-27.92	894.8
41	12	-6418	600	354	0	637	-2281	12.57	12.57	6.28	6.28	-14.74	283.8
42	12	-6406	603	324	0	554	-2290	12.57	12.57	6.28	6.28	-14.80	286.8
43	12	-5800	1536	389	0	742	-5209	12.57	12.57	6.28	6.28	-34.19	1212.5
44	12	-6925	-430	306	0	507	932	12.57	12.57	6.28	6.28	-6.08	-82.6
45	12	-6394	494	297	0	478	-1958	12.57	12.57	6.28	6.28	-12.49	197.8
46	12	-6412	421	342	0	606	-1740	12.57	12.57	6.28	6.28	-10.95	142.6
47	12	-6411	376	338	0	598	-1605	12.57	12.57	6.28	6.28	-10.01	-126.4
49	12	-6288	585	347	0	623	-2258	12.57	12.57	6.28	6.28	-14.60	284.5
50	12	-6513	192	330	0	576	-1030	12.57	12.57	6.28	6.28	-6.45	-86.5
51	12	-6407	377	329	0	570	-1608	12.57	12.57	6.28	6.28	-10.04	-126.6

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	25	-5974	1229	380	0	664	-4087	12.57	12.57	6.28	6.28	-26.91	852.5
41	25	-6343	600	354	0	593	-2206	12.57	12.57	6.28	6.28	-14.23	267.0
42	25	-6331	603	324	0	513	-2214	12.57	12.57	6.28	6.28	-14.29	269.9
43	25	-5725	1536	389	0	693	-5017	12.57	12.57	6.28	6.28	-32.95	1158.1
44	25	-6850	-430	306	0	469	878	12.57	12.57	6.28	6.28	-5.83	-79.4
45	25	-6319	494	297	0	441	-1897	12.57	12.57	6.28	6.28	-12.07	185.5
46	25	-6337	421	342	0	563	-1688	12.57	12.57	6.28	6.28	-10.60	133.3
47	25	-6336	376	338	0	556	-1558	12.57	12.57	6.28	6.28	-9.70	-122.8
49	25	-6213	585	347	0	580	-2185	12.57	12.57	6.28	6.28	-14.11	268.3
50	25	-6438	192	330	0	535	-1006	12.57	12.57	6.28	6.28	-6.31	-84.7
51	25	-6332	377	329	0	529	-1561	12.57	12.57	6.28	6.28	-9.72	-123.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	37	-5899	1229	380	0	617	-3934	12.57	12.57	6.28	6.28	-25.90	810.3
41	37	-6268	600	354	0	549	-2131	12.57	12.57	6.28	6.28	-13.72	250.4
42	37	-6256	603	324	0	472	-2138	12.57	12.57	6.28	6.28	-13.78	253.1
43	37	-5650	1536	389	0	645	-4825	12.57	12.57	6.28	6.28	-31.70	1103.6
44	37	-6775	-430	306	0	431	824	12.57	12.57	6.28	6.28	-5.59	-76.3
45	37	-6244	494	297	0	404	-1835	12.57	12.57	6.28	6.28	-11.65	173.3
46	37	-6262	421	342	0	521	-1635	12.57	12.57	6.28	6.28	-10.25	-128.4
47	37	-6261	376	338	0	514	-1511	12.57	12.57	6.28	6.28	-9.39	-119.3
49	37	-6138	585	347	0	536	-2112	12.57	12.57	6.28	6.28	-13.61	252.1
50	37	-6363	192	330	0	494	-982	12.57	12.57	6.28	6.28	-6.18	-83.0
51	37	-6257	377	329	0	488	-1514	12.57	12.57	6.28	6.28	-9.41	-119.5

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	50	-5824	1229	380	0	569	-3780	12.57	12.57	6.28	6.28	-24.89	768.2
41	50	-6193	600	354	0	504	-2056	12.57	12.57	6.28	6.28	-13.21	233.9
42	50	-6181	603	324	0	432	-2063	12.57	12.57	6.28	6.28	-13.26	236.4
43	50	-5575	1536	389	0	596	-4633	12.57	12.57	6.28	6.28	-30.45	1049.2
44	50	-6700	-430	306	0	393	770	12.57	12.57	6.28	6.28	-5.35	-73.4
45	50	-6169	494	297	0	367	-1773	12.57	12.57	6.28	6.28	-11.23	161.2
46	50	-6187	421	342	0	478	-1582	12.57	12.57	6.28	6.28	-9.89	-124.4
47	50	-6186	376	338	0	471	-1464	12.57	12.57	6.28	6.28	-9.08	-115.7
49	50	-6063	585	347	0	493	-2039	12.57	12.57	6.28	6.28	-13.12	236.1
50	50	-6288	192	330	0	452	-958	12.57	12.57	6.28	6.28	-6.04	-81.3
51	50	-6182	377	329	0	447	-1467	12.57	12.57	6.28	6.28	-9.10	-115.9

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

ASTA NUM. 105 NI 1445 NF 168 SEZ. Rp B= 0.400 H= 0.600 (pilastro)
PIL. NUM. 11A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-5824	1229	380	0	569	-3780	12.57	12.57	6.28	6.28	-24.89	768.2
41	0	-6193	600	354	0	504	-2056	12.57	12.57	6.28	6.28	-13.21	233.9
42	0	-6181	603	324	0	432	-2063	12.57	12.57	6.28	6.28	-13.26	236.4
43	0	-5575	1536	389	0	596	-4633	12.57	12.57	6.28	6.28	-30.45	1049.2
44	0	-6700	-430	306	0	393	770	12.57	12.57	6.28	6.28	-5.35	-73.4
45	0	-6169	494	297	0	367	-1773	12.57	12.57	6.28	6.28	-11.23	161.2
46	0	-6187	421	342	0	478	-1582	12.57	12.57	6.28	6.28	-9.89	-124.4
47	0	-6186	376	338	0	471	-1464	12.57	12.57	6.28	6.28	-9.08	-115.7
49	0	-6063	585	347	0	493	-2039	12.57	12.57	6.28	6.28	-13.12	236.1
50	0	-6288	192	330	0	452	-958	12.57	12.57	6.28	6.28	-6.04	-81.3
51	0	-6182	377	329	0	447	-1467	12.57	12.57	6.28	6.28	-9.10	-115.9

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	12	-5749	1229	380	0	522	-3626	12.57	12.57	6.28	6.28	-23.88	726.0
41	12	-6118	600	354	0	460	-1981	12.57	12.57	6.28	6.28	-12.70	217.6
42	12	-6106	603	324	0	391	-1988	12.57	12.57	6.28	6.28	-12.75	220.0

43	12	-5500	1536	389	0	547	-4441	12.57	12.57	6.28	6.28	-29.20	994.8
44	12	-6625	-430	306	0	355	717	12.57	12.57	6.28	6.28	-5.13	-70.5
45	12	-6094	494	297	0	330	-1711	12.57	12.57	6.28	6.28	-10.81	149.3
46	12	-6112	421	342	0	435	-1530	12.57	12.57	6.28	6.28	-9.54	-120.5
47	12	-6111	376	338	0	429	-1417	12.57	12.57	6.28	6.28	-8.78	-112.1
49	12	-5988	585	347	0	450	-1966	12.57	12.57	6.28	6.28	-12.62	220.2
50	12	-6213	192	330	0	411	-934	12.57	12.57	6.28	6.28	-5.91	-79.6
51	12	-6107	377	329	0	406	-1420	12.57	12.57	6.28	6.28	-8.79	-112.3

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	25	-5674	1229	380	0	474	-3472	12.57	12.57	6.28	6.28	-22.87	683.9
41	25	-6043	600	354	0	416	-1906	12.57	12.57	6.28	6.28	-12.19	201.4
42	25	-6031	603	324	0	351	-1912	12.57	12.57	6.28	6.28	-12.24	203.7
43	25	-5425	1536	389	0	499	-4249	12.57	12.57	6.28	6.28	-27.95	940.5
44	25	-6550	-430	306	0	316	663	12.57	12.57	6.28	6.28	-4.90	-67.6
45	25	-6019	494	297	0	293	-1650	12.57	12.57	6.28	6.28	-10.39	137.6
46	25	-6037	421	342	0	393	-1477	12.57	12.57	6.28	6.28	-9.19	-116.5
47	25	-6036	376	338	0	387	-1370	12.57	12.57	6.28	6.28	-8.47	-108.6
49	25	-5913	585	347	0	406	-1892	12.57	12.57	6.28	6.28	-12.12	204.4
50	25	-6138	192	330	0	370	-910	12.57	12.57	6.28	6.28	-5.78	-77.9
51	25	-6032	377	329	0	365	-1372	12.57	12.57	6.28	6.28	-8.49	-108.8

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	38	-5599	1229	380	0	427	-3319	12.57	12.57	6.28	6.28	-21.85	641.8
41	38	-5968	600	354	0	372	-1831	12.57	12.57	6.28	6.28	-11.68	185.5
42	38	-5956	603	324	0	310	-1837	12.57	12.57	6.28	6.28	-11.72	187.7
43	38	-5350	1536	389	0	450	-4057	12.57	12.57	6.28	6.28	-26.69	886.2
44	38	-6475	-430	306	0	278	609	12.57	12.57	6.28	6.28	-4.68	-64.8
45	38	-5944	494	297	0	256	-1588	12.57	12.57	6.28	6.28	-9.98	126.1
46	38	-5962	421	342	0	350	-1424	12.57	12.57	6.28	6.28	-8.85	-112.5
47	38	-5961	376	338	0	344	-1323	12.57	12.57	6.28	6.28	-8.16	-105.0
49	38	-5838	585	347	0	363	-1819	12.57	12.57	6.28	6.28	-11.62	188.8
50	38	-6063	192	330	0	328	-886	12.57	12.57	6.28	6.28	-5.64	-76.2
51	38	-5957	377	329	0	324	-1325	12.57	12.57	6.28	6.28	-8.18	-105.2

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	50	-5524	1229	380	0	379	-3165	12.57	12.57	6.28	6.28	-20.83	599.8
41	50	-5893	600	354	0	327	-1756	12.57	12.57	6.28	6.28	-11.16	169.7
42	50	-5881	603	324	0	270	-1762	12.57	12.57	6.28	6.28	-11.21	171.8
43	50	-5275	1536	389	0	402	-3865	12.57	12.57	6.28	6.28	-25.44	831.9
44	50	-6400	-430	306	0	240	555	12.57	12.57	6.28	6.28	-4.46	-61.9
45	50	-5869	494	297	0	218	-1526	12.57	12.57	6.28	6.28	-9.56	-119.9
46	50	-5887	421	342	0	307	-1372	12.57	12.57	6.28	6.28	-8.50	-108.5
47	50	-5886	376	338	0	302	-1276	12.57	12.57	6.28	6.28	-7.86	-101.5
49	50	-5763	585	347	0	320	-1746	12.57	12.57	6.28	6.28	-11.12	173.4
50	50	-5988	192	330	0	287	-862	12.57	12.57	6.28	6.28	-5.51	-74.5
51	50	-5882	377	329	0	283	-1278	12.57	12.57	6.28	6.28	-7.88	-101.6

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

ASTA NUM. 106 NI 1032 NF 1045 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 10
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-15260	79	1565	0	1477	-723	6.28	6.28	12.57	12.57	-11.18	-154.5
41	0	-13500	750	1136	0	1208	-634	6.28	6.28	12.57	12.57	-9.54	-132.3
42	0	-13320	753	1254	0	1134	-635	6.28	6.28	12.57	12.57	-9.21	-127.9
43	0	-16090	-304	1792	0	1584	-801	6.28	6.28	12.57	12.57	-11.89	-164.1
44	0	-10610	1859	457	0	781	-486	6.28	6.28	12.57	12.57	-6.90	-96.4
45	0	-12850	819	1274	0	1013	-655	6.28	6.28	12.57	12.57	-8.59	-119.8
46	0	-12950	851	1042	0	1093	-666	6.28	6.28	12.57	12.57	-8.92	-124.0
47	0	-12810	877	1019	0	1064	-674	6.28	6.28	12.57	12.57	-8.76	-121.9
49	0	-13400	653	1162	0	1154	-703	6.28	6.28	12.57	12.57	-9.31	-129.3
50	0	-12300	1086	895	0	993	-640	6.28	6.28	12.57	12.57	-8.31	-115.7
51	0	-12750	878	1058	0	1039	-674	6.28	6.28	12.57	12.57	-8.65	-120.4

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	12	-15185	79	1565	0	1281	-713	6.28	6.28	12.57	12.57	-10.45	-145.3
41	12	-13425	750	1136	0	1066	-541	6.28	6.28	12.57	12.57	-9.00	-125.5
42	12	-13245	753	1254	0	977	-541	6.28	6.28	12.57	12.57	-8.62	-120.5
43	12	-16015	-304	1792	0	1360	-839	6.28	6.28	12.57	12.57	-11.06	-153.7
44	12	-10535	1859	457	0	724	-253	6.28	6.28	12.57	12.57	-6.66	-93.4
45	12	-12775	819	1274	0	854	-552	6.28	6.28	12.57	12.57	-7.99	-112.2
46	12	-12875	851	1042	0	963	-559	6.28	6.28	12.57	12.57	-8.42	-117.7
47	12	-12735	877	1019	0	937	-564	6.28	6.28	12.57	12.57	-8.27	-115.7
49	12	-13325	653	1162	0	1009	-621	6.28	6.28	12.57	12.57	-8.76	-122.4
50	12	-12225	1086	895	0	881	-504	6.28	6.28	12.57	12.57	-7.88	-110.3
51	12	-12675	878	1058	0	907	-564	6.28	6.28	12.57	12.57	-8.14	-114.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	25	-15110	79	1565	0	1086	-703	6.28	6.28	12.57	12.57	-9.72	-136.1
41	25	-13350	750	1136	0	924	-447	6.28	6.28	12.57	12.57	-8.47	-118.7
42	25	-13170	753	1254	0	820	-446	6.28	6.28	12.57	12.57	-8.03	-113.0
43	25	-15940	-304	1792	0	1136	-877	6.28	6.28	12.57	12.57	-10.23	-143.2
44	25	-10460	1859	457	0	667	-21	6.28	6.28	12.57	12.57	-6.43	-90.5
45	25	-12700	819	1274	0	694	-450	6.28	6.28	12.57	12.57	-7.39	-104.7
46	25	-12800	851	1042	0	832	-453	6.28	6.28	12.57	12.57	-7.93	-111.4
47	25	-12660	877	1019	0	809	-454	6.28	6.28	12.57	12.57	-7.79	-109.6
49	25	-13250	653	1162	0	863	-540	6.28	6.28	12.57	12.57	-8.21	-115.4
50	25	-12150	1086	895	0	769	-369	6.28	6.28	12.57	12.57	-7.45	-104.8
51	25	-12600	878	1058	0	775	-454	6.28	6.28	12.57	12.57	-7.64	-107.7

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	38	-15035	79	1565	0	890	-693	6.28	6.28	12.57	12.57	-8.99	-127.0
41	38	-13275	750	1136	0	782	-353	6.28	6.28	12.57	12.57	-7.93	-111.9
42	38	-13095	753	1254	0	664	-352	6.28	6.28	12.57	12.57	-7.43	-105.6
43	38	-15865	-304	1792	0	912	-915	6.28	6.28	12.57	12.57	-10.23	-136.6

44	38	-10385	1859	457	0	610	211	6.28	6.28	12.57	12.57	-6.19	-87.5
45	38	-12625	819	1274	0	535	-348	6.28	6.28	12.57	12.57	-6.79	-97.1
46	38	-12725	851	1042	0	702	-347	6.28	6.28	12.57	12.57	-7.43	-105.2
47	38	-12585	877	1019	0	682	-345	6.28	6.28	12.57	12.57	-7.30	-103.5
49	38	-13175	653	1162	0	718	-458	6.28	6.28	12.57	12.57	-7.66	-108.5
50	38	-12075	1086	895	0	658	-233	6.28	6.28	12.57	12.57	-7.02	-99.4
51	38	-12525	878	1058	0	643	-345	6.28	6.28	12.57	12.57	-7.14	-101.3

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	50	-14960	79	1565	0	694	-683	6.28	6.28	12.57	12.57	-8.76	-118.8
41	50	-13200	750	1136	0	640	-260	6.28	6.28	12.57	12.57	-7.39	-105.1
42	50	-13020	753	1254	0	507	-258	6.28	6.28	12.57	12.57	-6.84	-98.1
43	50	-15790	-304	1792	0	688	-953	6.28	6.28	12.57	12.57	-10.39	-138.3
44	50	-10310	1859	457	0	552	444	6.28	6.28	12.57	12.57	-5.96	-84.5
45	50	-12550	819	1274	0	376	-245	6.28	6.28	12.57	12.57	-6.19	-89.5
46	50	-12650	851	1042	0	572	-240	6.28	6.28	12.57	12.57	-6.93	-98.9
47	50	-12510	877	1019	0	555	-235	6.28	6.28	12.57	12.57	-6.82	-97.3
49	50	-13100	653	1162	0	573	-376	6.28	6.28	12.57	12.57	-7.11	-101.6
50	50	-12000	1086	895	0	546	-97	6.28	6.28	12.57	12.57	-6.59	-94.0
51	50	-12450	878	1058	0	510	-235	6.28	6.28	12.57	12.57	-6.64	-95.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 107 NI 1045 NF 299 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 10A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-16190	-1578	674	0	562	-706	6.28	6.28	12.57	12.57	-9.32	-126.7
41	0	-14910	304	505	0	530	-216	6.28	6.28	12.57	12.57	-7.66	-110.1
42	0	-14800	298	739	0	383	-216	6.28	6.28	12.57	12.57	-7.09	-102.9
43	0	-16630	-2815	796	0	546	-1015	6.28	6.28	12.57	12.57	-11.00	-146.2
44	0	-12830	3434	236	0	477	596	6.28	6.28	12.57	12.57	-7.56	-102.4
45	0	-14320	313	904	0	249	-199	6.28	6.28	12.57	12.57	-6.42	-94.1
46	0	-14260	333	519	0	472	-189	6.28	6.28	12.57	12.57	-7.20	-103.7
47	0	-14100	341	523	0	457	-182	6.28	6.28	12.57	12.57	-7.08	-102.2
49	0	-14530	-287	579	0	468	-345	6.28	6.28	12.57	12.57	-7.29	-105.1
50	0	-13770	963	467	0	454	-23	6.28	6.28	12.57	12.57	-6.94	-100.1
51	0	-14060	339	601	0	408	-182	6.28	6.28	12.57	12.57	-6.89	-99.7

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	12	-16115	-1578	674	0	477	-903	6.28	6.28	12.57	12.57	-10.27	-137.2
41	12	-14835	304	505	0	467	-178	6.28	6.28	12.57	12.57	-7.40	-106.9
42	12	-14725	298	739	0	291	-179	6.28	6.28	12.57	12.57	-6.73	-98.4
43	12	-16555	-2815	796	0	447	-1367	6.28	6.28	12.57	12.57	-12.75	-165.7
44	12	-12755	3434	236	0	448	1025	6.28	6.28	12.57	12.57	-9.68	-126.0
45	12	-14245	313	904	0	136	-159	6.28	6.28	12.57	12.57	-5.99	-88.6
46	12	-14185	333	519	0	407	-147	6.28	6.28	12.57	12.57	-6.94	-100.4
47	12	-14025	341	523	0	392	-139	6.28	6.28	12.57	12.57	-6.82	-98.8
49	12	-14455	-287	579	0	395	-381	6.28	6.28	12.57	12.57	-7.09	-101.5
50	12	-13695	963	467	0	395	98	6.28	6.28	12.57	12.57	-6.71	-97.1
51	12	-13985	339	601	0	333	-139	6.28	6.28	12.57	12.57	-6.60	-95.9

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	25	-16040	-1578	674	0	393	-1100	6.28	6.28	12.57	12.57	-11.21	-147.8
41	25	-14760	304	505	0	404	-140	6.28	6.28	12.57	12.57	-7.15	-103.6
42	25	-14650	298	739	0	199	-142	6.28	6.28	12.57	12.57	-6.37	-93.8
43	25	-16480	-2815	796	0	347	-1718	6.28	6.28	12.57	12.57	-14.84	-188.1
44	25	-12680	3434	236	0	418	1454	6.28	6.28	12.57	12.57	-12.31	-154.0
45	25	-14170	313	904	0	23	-120	6.28	6.28	12.57	12.57	-5.70	-83.2
46	25	-14110	333	519	0	342	-105	6.28	6.28	12.57	12.57	-6.67	-97.1
47	25	-13950	341	523	0	326	-96	6.28	6.28	12.57	12.57	-6.56	-95.4
49	25	-14380	-287	579	0	323	-416	6.28	6.28	12.57	12.57	-7.24	-100.8
50	25	-13620	963	467	0	337	218	6.28	6.28	12.57	12.57	-6.47	-94.0
51	25	-13910	339	601	0	258	-97	6.28	6.28	12.57	12.57	-6.30	-92.2

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	38	-15965	-1578	674	0	309	-1298	6.28	6.28	12.57	12.57	-12.19	-158.6
41	38	-14685	304	505	0	340	-102	6.28	6.28	12.57	12.57	-6.89	-100.3
42	38	-14575	298	739	0	106	-104	6.28	6.28	12.57	12.57	-6.01	-89.2
43	38	-16405	-2815	796	0	248	-2070	6.28	6.28	12.57	12.57	-17.27	-212.9
44	38	-12605	3434	236	0	389	1884	6.28	6.28	12.57	12.57	-15.50	-185.5
45	38	-14095	313	904	0	-90	-81	6.28	6.28	12.57	12.57	-5.77	-85.7
46	38	-14035	333	519	0	277	-64	6.28	6.28	12.57	12.57	-6.41	-93.7
47	38	-13875	341	523	0	261	-54	6.28	6.28	12.57	12.57	-6.29	-92.1
49	38	-14305	-287	579	0	250	-452	6.28	6.28	12.57	12.57	-7.39	-102.4
50	38	-13545	963	467	0	279	338	6.28	6.28	12.57	12.57	-6.55	-92.0
51	38	-13835	339	601	0	183	-54	6.28	6.28	12.57	12.57	-6.00	-88.4

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	50	-15890	-1578	674	0	224	-1495	6.28	6.28	12.57	12.57	-13.29	-170.5
41	50	-14610	304	505	0	277	-64	6.28	6.28	12.57	12.57	-6.64	-97.1
42	50	-14500	298	739	0	14	-67	6.28	6.28	12.57	12.57	-5.65	-84.6
43	50	-16330	-2815	796	0	148	-2422	6.28	6.28	12.57	12.57	-19.94	-238.9
44	50	-12530	3434	236	0	360	2313	6.28	6.28	12.57	12.57	-18.92	-217.2
45	50	-14020	313	904	0	-203	-42	6.28	6.28	12.57	12.57	-6.14	-90.3
46	50	-13960	333	519	0	212	-22	6.28	6.28	12.57	12.57	-6.15	-90.4
47	50	-13800	341	523	0	196	-11	6.28	6.28	12.57	12.57	-6.03	-88.7
49	50	-14230	-287	579	0	178	-488	6.28	6.28	12.57	12.57	-7.54	-104.0
50	50	-13470	963	467	0	220	459	6.28	6.28	12.57	12.57	-7.12	-98.3
51	50	-13760	339	601	0	108	-12	6.28	6.28	12.57	12.57	-5.70	-84.6

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 108 NI 1254 NF 1349 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 9
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-4183	-114	176	0	-60	-168	6.28	6.28	12.57	12.57	-2.34	-31.9
41	0	-4166	1	67	0	-40	9	6.28	6.28	12.57	12.57	-1.75	-25.9
42	0	-4150	1	177	0	-56	10	6.28	6.28	12.57	12.57	-1.80	-26.6
43	0	-4075	-196	218	0	-69	-295	6.28	6.28	12.57	12.57	-2.93	-38.4
44	0	-4043	192	-101	0	-8	305	6.28	6.28	12.57	12.57	-2.96	-38.8
45	0	-4020	-3	219	0	-61	2	6.28	6.28	12.57	12.57	-1.77	-26.0
46	0	-3975	-8	15	0	-31	-6	6.28	6.28	12.57	12.57	-1.65	-24.4
47	0	-3927	-10	3	0	-29	-10	6.28	6.28	12.57	12.57	-1.62	-24.0
49	0	-3933	-48	39	0	-36	-69	6.28	6.28	12.57	12.57	-1.75	-25.1
50	0	-3926	29	-25	0	-24	51	6.28	6.28	12.57	12.57	-1.67	-24.1
51	0	-3922	-10	39	0	-34	-9	6.28	6.28	12.57	12.57	-1.64	-24.3

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	12	-4108	-114	176	0	-83	-182	6.28	6.28	12.57	12.57	-2.38	-32.3
41	12	-4091	1	67	0	-48	9	6.28	6.28	12.57	12.57	-1.75	-25.9
42	12	-4075	1	177	0	-78	10	6.28	6.28	12.57	12.57	-1.85	-27.1
43	12	-4000	-196	218	0	-96	-320	6.28	6.28	12.57	12.57	-3.02	-39.4
44	12	-3968	192	-101	0	5	329	6.28	6.28	12.57	12.57	-3.06	-39.8
45	12	-3945	-3	219	0	-89	2	6.28	6.28	12.57	12.57	-1.84	-26.8
46	12	-3900	-8	15	0	-33	-7	6.28	6.28	12.57	12.57	-1.62	-24.1
47	12	-3852	-10	3	0	-29	-11	6.28	6.28	12.57	12.57	-1.59	-23.6
49	12	-3858	-48	39	0	-41	-75	6.28	6.28	12.57	12.57	-1.76	-25.0
50	12	-3851	29	-25	0	-20	55	6.28	6.28	12.57	12.57	-1.66	-23.9
51	12	-3847	-10	39	0	-39	-10	6.28	6.28	12.57	12.57	-1.63	-24.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	25	-4033	-114	176	0	-105	-197	6.28	6.28	12.57	12.57	-2.42	-32.7
41	25	-4016	1	67	0	-57	9	6.28	6.28	12.57	12.57	-1.75	-25.8
42	25	-4000	1	177	0	-100	11	6.28	6.28	12.57	12.57	-1.91	-27.7
43	25	-3925	-196	218	0	-123	-344	6.28	6.28	12.57	12.57	-3.13	-40.5
44	25	-3893	192	-101	0	17	353	6.28	6.28	12.57	12.57	-3.18	-40.9
45	25	-3870	-3	219	0	-116	1	6.28	6.28	12.57	12.57	-1.91	-27.6
46	25	-3825	-8	15	0	-35	-8	6.28	6.28	12.57	12.57	-1.60	-23.7
47	25	-3777	-10	3	0	-29	-12	6.28	6.28	12.57	12.57	-1.56	-23.2
49	25	-3783	-48	39	0	-45	-81	6.28	6.28	12.57	12.57	-1.76	-24.9
50	25	-3776	29	-25	0	-17	59	6.28	6.28	12.57	12.57	-1.65	-23.7
51	25	-3772	-10	39	0	-44	-12	6.28	6.28	12.57	12.57	-1.61	-23.8

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	38	-3958	-114	176	0	-127	-211	6.28	6.28	12.57	12.57	-2.47	-33.1
41	38	-3941	1	67	0	-65	9	6.28	6.28	12.57	12.57	-1.76	-25.7
42	38	-3925	1	177	0	-123	11	6.28	6.28	12.57	12.57	-1.96	-28.2
43	38	-3850	-196	218	0	-150	-368	6.28	6.28	12.57	12.57	-3.26	-41.7
44	38	-3818	192	-101	0	30	377	6.28	6.28	12.57	12.57	-3.30	-42.1
45	38	-3795	-3	219	0	-143	1	6.28	6.28	12.57	12.57	-1.98	-28.4
46	38	-3750	-8	15	0	-37	-9	6.28	6.28	12.57	12.57	-1.58	-23.4
47	38	-3702	-10	3	0	-30	-13	6.28	6.28	12.57	12.57	-1.54	-22.8
49	38	-3708	-48	39	0	-50	-87	6.28	6.28	12.57	12.57	-1.76	-24.8
50	38	-3701	29	-25	0	-14	62	6.28	6.28	12.57	12.57	-1.64	-23.5
51	38	-3697	-10	39	0	-49	-13	6.28	6.28	12.57	12.57	-1.60	-23.6

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	50	-3883	-114	176	0	-149	-225	6.28	6.28	12.57	12.57	-2.51	-33.5
41	50	-3866	1	67	0	-73	9	6.28	6.28	12.57	12.57	-1.76	-25.7
42	50	-3850	1	177	0	-145	11	6.28	6.28	12.57	12.57	-2.01	-28.8
43	50	-3775	-196	218	0	-177	-393	6.28	6.28	12.57	12.57	-3.39	-43.0
44	50	-3743	192	-101	0	42	401	6.28	6.28	12.57	12.57	-3.44	-43.4
45	50	-3720	-3	219	0	-171	1	6.28	6.28	12.57	12.57	-2.05	-29.2
46	50	-3675	-8	15	0	-39	-10	6.28	6.28	12.57	12.57	-1.56	-23.0
47	50	-3627	-10	3	0	-30	-15	6.28	6.28	12.57	12.57	-1.51	-22.4
49	50	-3633	-48	39	0	-55	-93	6.28	6.28	12.57	12.57	-1.77	-24.8
50	50	-3626	29	-25	0	-11	66	6.28	6.28	12.57	12.57	-1.63	-23.3
51	50	-3622	-10	39	0	-54	-14	6.28	6.28	12.57	12.57	-1.59	-23.4

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 109 NI 1349 NF 129 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 9A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-5952	-297	577	0	-149	-214	6.28	6.28	12.57	12.57	-3.20	-44.0
41	0	-5928	5	304	0	-73	7	6.28	6.28	12.57	12.57	-2.55	-37.6
42	0	-5900	8	563	0	-145	9	6.28	6.28	12.57	12.57	-2.80	-40.7
43	0	-5783	-512	683	0	-177	-372	6.28	6.28	12.57	12.57	-3.92	-51.9
44	0	-5737	511	-116	0	42	377	6.28	6.28	12.57	12.57	-3.93	-51.9
45	0	-5695	-5	659	0	-171	-1	6.28	6.28	12.57	12.57	-2.81	-40.6
46	0	-5631	-18	182	0	-39	-11	6.28	6.28	12.57	12.57	-2.31	-34.4
47	0	-5557	-24	152	0	-30	-15	6.28	6.28	12.57	12.57	-2.25	-33.5
49	0	-5565	-124	242	0	-55	-89	6.28	6.28	12.57	12.57	-2.44	-35.0
50	0	-5556	80	83	0	-11	61	6.28	6.28	12.57	12.57	-2.30	-33.4
51	0	-5547	-23	238	0	-54	-15	6.28	6.28	12.57	12.57	-2.34	-34.6

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	12	-5877	-297	577	0	-221	-251	6.28	6.28	12.57	12.57	-3.36	-45.7
41	12	-5853	5	304	0	-111	8	6.28	6.28	12.57	12.57	-2.66	-38.9
42	12	-5825	8	563	0	-215	10	6.28	6.28	12.57	12.57	-3.02	-43.4
43	12	-5708	-512	683	0	-263	-436	6.28	6.28	12.57	12.57	-4.21	-55.1
44	12	-5662	511	-116	0	57	441	6.28	6.28	12.57	12.57	-4.22	-55.1
45	12	-5620	-5	659	0	-253	-2	6.28	6.28	12.57	12.57	-3.08	-43.9
46	12	-5556	-18	182	0	-61	-13	6.28	6.28	12.57	12.57	-2.37	-34.9
47	12	-5482	-24	152	0	-49	-18	6.28	6.28	12.57	12.57	-2.29	-34.0
49	12	-5490	-124	242	0	-85	-104	6.28	6.28	12.57	12.57	-2.49	-35.6

50	12	-5481	80	83	0	-22	71	6.28	6.28	12.57	12.57	-2.33	-33.6
51	12	-5472	-23	238	0	-84	-17	6.28	6.28	12.57	12.57	-2.41	-35.5

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	25	-5802	-297	577	0	-293	-288	6.28	6.28	12.57	12.57	-3.51	-47.4
41	25	-5778	5	304	0	-149	8	6.28	6.28	12.57	12.57	-2.77	-40.2
42	25	-5750	8	563	0	-286	11	6.28	6.28	12.57	12.57	-3.24	-46.1
43	25	-5633	-512	683	0	-348	-500	6.28	6.28	12.57	12.57	-4.54	-58.6
44	25	-5587	511	-116	0	72	505	6.28	6.28	12.57	12.57	-4.55	-58.6
45	25	-5545	-5	659	0	-336	-2	6.28	6.28	12.57	12.57	-3.34	-47.1
46	25	-5481	-18	182	0	-84	-15	6.28	6.28	12.57	12.57	-2.42	-35.5
47	25	-5407	-24	152	0	-68	-21	6.28	6.28	12.57	12.57	-2.33	-34.4
49	25	-5415	-124	242	0	-116	-120	6.28	6.28	12.57	12.57	-2.54	-36.6
50	25	-5406	80	83	0	-32	81	6.28	6.28	12.57	12.57	-2.35	-33.7
51	25	-5397	-23	238	0	-113	-20	6.28	6.28	12.57	12.57	-2.49	-36.3

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	38	-5727	-297	577	0	-365	-325	6.28	6.28	12.57	12.57	-3.67	-49.5
41	38	-5703	5	304	0	-188	9	6.28	6.28	12.57	12.57	-2.87	-41.4
42	38	-5675	8	563	0	-356	12	6.28	6.28	12.57	12.57	-3.47	-48.8
43	38	-5558	-512	683	0	-433	-564	6.28	6.28	12.57	12.57	-4.91	-62.4
44	38	-5512	511	-116	0	86	568	6.28	6.28	12.57	12.57	-4.92	-62.5
45	38	-5470	-5	659	0	-418	-3	6.28	6.28	12.57	12.57	-3.61	-50.4
46	38	-5406	-18	182	0	-107	-17	6.28	6.28	12.57	12.57	-2.47	-36.1
47	38	-5332	-24	152	0	-87	-24	6.28	6.28	12.57	12.57	-2.37	-34.8
49	38	-5340	-124	242	0	-146	-135	6.28	6.28	12.57	12.57	-2.59	-37.5
50	38	-5331	80	83	0	-42	91	6.28	6.28	12.57	12.57	-2.37	-33.9
51	38	-5322	-23	238	0	-143	-23	6.28	6.28	12.57	12.57	-2.57	-37.2

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	50	-5652	-297	577	0	-437	-362	6.28	6.28	12.57	12.57	-3.83	-52.3
41	50	-5628	5	304	0	-226	9	6.28	6.28	12.57	12.57	-2.98	-42.7
42	50	-5600	8	563	0	-426	13	6.28	6.28	12.57	12.57	-3.69	-51.5
43	50	-5483	-512	683	0	-519	-628	6.28	6.28	12.57	12.57	-5.32	-66.5
44	50	-5437	511	-116	0	101	632	6.28	6.28	12.57	12.57	-5.34	-66.6
45	50	-5395	-5	659	0	-500	-3	6.28	6.28	12.57	12.57	-3.88	-53.7
46	50	-5331	-18	182	0	-130	-20	6.28	6.28	12.57	12.57	-2.52	-36.7
47	50	-5257	-24	152	0	-106	-27	6.28	6.28	12.57	12.57	-2.41	-35.2
49	50	-5265	-124	242	0	-176	-151	6.28	6.28	12.57	12.57	-2.67	-38.4
50	50	-5256	80	83	0	-53	101	6.28	6.28	12.57	12.57	-2.39	-34.0
51	50	-5247	-23	238	0	-173	-26	6.28	6.28	12.57	12.57	-2.65	-38.1

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 110 NI 1158 NF 1253 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 8
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-2926	67	426	0	-148	5	6.28	6.28	9.42	9.42	-2.15	-30.5
41	0	-2931	125	337	0	-141	-12	6.28	6.28	9.42	9.42	-2.12	-30.2
42	0	-3009	123	409	0	-155	-11	6.28	6.28	9.42	9.42	-2.22	-31.5
43	0	-2845	23	462	0	-142	17	6.28	6.28	9.42	9.42	-2.08	-29.6
44	0	-2890	220	187	0	-127	-39	6.28	6.28	9.42	9.42	-2.03	-29.0
45	0	-2984	116	433	0	-155	-9	6.28	6.28	9.42	9.42	-2.21	-31.3
46	0	-2808	116	300	0	-126	-10	6.28	6.28	9.42	9.42	-1.99	-28.4
47	0	-2777	114	290	0	-122	-9	6.28	6.28	9.42	9.42	-1.95	-27.9
49	0	-2775	95	320	0	-124	-4	6.28	6.28	9.42	9.42	-1.96	-28.0
50	0	-2784	134	265	0	-121	-15	6.28	6.28	9.42	9.42	-1.95	-27.9
51	0	-2803	113	314	0	-127	-9	6.28	6.28	9.42	9.42	-1.99	-28.4

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	12	-2870	67	426	0	-201	13	6.28	6.28	9.42	9.42	-2.36	-33.1
41	12	-2875	125	337	0	-184	4	6.28	6.28	9.42	9.42	-2.28	-32.2
42	12	-2953	123	409	0	-206	5	6.28	6.28	9.42	9.42	-2.43	-34.0
43	12	-2789	23	462	0	-200	20	6.28	6.28	9.42	9.42	-2.32	-32.5
44	12	-2834	220	187	0	-150	-11	6.28	6.28	9.42	9.42	-2.11	-29.9
45	12	-2928	116	433	0	-209	6	6.28	6.28	9.42	9.42	-2.42	-34.0
46	12	-2752	116	300	0	-163	5	6.28	6.28	9.42	9.42	-2.13	-30.1
47	12	-2721	114	290	0	-158	5	6.28	6.28	9.42	9.42	-2.09	-29.6
49	12	-2719	95	320	0	-164	8	6.28	6.28	9.42	9.42	-2.12	-29.9
50	12	-2728	134	265	0	-154	2	6.28	6.28	9.42	9.42	-2.08	-29.4
51	12	-2747	113	314	0	-166	5	6.28	6.28	9.42	9.42	-2.14	-30.2

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	25	-2814	67	426	0	-254	22	6.28	6.28	9.42	9.42	-2.58	-35.7
41	25	-2818	125	337	0	-226	20	6.28	6.28	9.42	9.42	-2.45	-34.1
42	25	-2896	123	409	0	-257	20	6.28	6.28	9.42	9.42	-2.63	-36.5
43	25	-2732	23	462	0	-258	23	6.28	6.28	9.42	9.42	-2.55	-35.3
44	25	-2778	220	187	0	-173	16	6.28	6.28	9.42	9.42	-2.19	-30.8
45	25	-2872	116	433	0	-263	20	6.28	6.28	9.42	9.42	-2.64	-36.7
46	25	-2696	116	300	0	-201	19	6.28	6.28	9.42	9.42	-2.27	-31.8
47	25	-2664	114	290	0	-195	19	6.28	6.28	9.42	9.42	-2.23	-31.2
49	25	-2662	95	320	0	-204	20	6.28	6.28	9.42	9.42	-2.27	-31.7
50	25	-2672	134	265	0	-187	19	6.28	6.28	9.42	9.42	-2.20	-30.8
51	25	-2690	113	314	0	-205	19	6.28	6.28	9.42	9.42	-2.29	-32.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	38	-2757	67	426	0	-308	30	6.28	6.28	9.42	9.42	-2.79	-38.3
41	38	-2762	125	337	0	-268	35	6.28	6.28	9.42	9.42	-2.61	-36.1
42	38	-2840	123	409	0	-308	36	6.28	6.28	9.42	9.42	-2.84	-39.0
43	38	-2676	23	462	0	-316	25	6.28	6.28	9.42	9.42	-2.79	-38.2
44	38	-2721	220	187	0	-197	44	6.28	6.28	9.42	9.42	-2.27	-31.7
45	38	-2815	116	433	0	-317	35	6.28	6.28	9.42	9.42	-2.86	-39.3
46	38	-2639	116	300	0	-238	34	6.28	6.28	9.42	9.42	-2.41	-33.5
47	38	-2608	114	290	0	-231	34	6.28	6.28	9.42	9.42	-2.37	-32.8
49	38	-2606	95	320	0	-244	32	6.28	6.28	9.42	9.42	-2.42	-33.6
50	38	-2615	134	265	0	-220	35	6.28	6.28	9.42	9.42	-2.32	-32.3

51	38	-2634	113	314	0	-245	34	6.28	6.28	9.42	9.42	-2.44	-33.8

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	50	-2701	67	426	0	-361	38	6.28	6.28	9.42	9.42	-3.03	-41.2
41	50	-2706	125	337	0	-310	51	6.28	6.28	9.42	9.42	-2.78	-38.1
42	50	-2784	123	409	0	-360	51	6.28	6.28	9.42	9.42	-3.06	-41.7
43	50	-2620	23	462	0	-373	28	6.28	6.28	9.42	9.42	-3.07	-41.5
44	50	-2665	220	187	0	-220	71	6.28	6.28	9.42	9.42	-2.34	-32.6
45	50	-2759	116	433	0	-371	49	6.28	6.28	9.42	9.42	-3.11	-42.3
46	50	-2583	116	300	0	-276	48	6.28	6.28	9.42	9.42	-2.56	-35.2
47	50	-2552	114	290	0	-267	48	6.28	6.28	9.42	9.42	-2.50	-34.5
49	50	-2550	95	320	0	-284	44	6.28	6.28	9.42	9.42	-2.58	-35.4
50	50	-2559	134	265	0	-254	52	6.28	6.28	9.42	9.42	-2.44	-33.8
51	50	-2578	113	314	0	-284	48	6.28	6.28	9.42	9.42	-2.59	-35.6

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 111 NI 1253 NF 213 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 8A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-3689	-161	514	0	-395	28	6.28	6.28	9.42	9.42	-3.66	-50.4
41	0	-3714	-23	383	0	-338	47	6.28	6.28	9.42	9.42	-3.41	-47.3
42	0	-3786	-29	504	0	-398	47	6.28	6.28	9.42	9.42	-3.72	-51.2
43	0	-3578	-254	558	0	-409	13	6.28	6.28	9.42	9.42	-3.67	-50.3
44	0	-3687	209	162	0	-237	78	6.28	6.28	9.42	9.42	-2.94	-41.3
45	0	-3740	-35	542	0	-413	45	6.28	6.28	9.42	9.42	-3.77	-51.8
46	0	-3564	-26	314	0	-299	44	6.28	6.28	9.42	9.42	-3.16	-43.9
47	0	-3527	-27	297	0	-289	43	6.28	6.28	9.42	9.42	-3.09	-43.1
49	0	-3518	-73	341	0	-308	37	6.28	6.28	9.42	9.42	-3.17	-44.1
50	0	-3540	20	261	0	-274	50	6.28	6.28	9.42	9.42	-3.03	-42.3
51	0	-3551	-29	338	0	-309	43	6.28	6.28	9.42	9.42	-3.19	-44.4

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	12	-3633	-161	514	0	-460	8	6.28	6.28	9.42	9.42	-3.94	-53.8
41	12	-3658	-23	383	0	-386	44	6.28	6.28	9.42	9.42	-3.60	-49.6
42	12	-3730	-29	504	0	-461	43	6.28	6.28	9.42	9.42	-3.99	-54.5
43	12	-3522	-254	558	0	-479	-19	6.28	6.28	9.42	9.42	-3.99	-54.3
44	12	-3631	209	162	0	-257	104	6.28	6.28	9.42	9.42	-3.00	-42.1
45	12	-3684	-35	542	0	-481	41	6.28	6.28	9.42	9.42	-4.07	-55.5
46	12	-3508	-26	314	0	-338	40	6.28	6.28	9.42	9.42	-3.31	-45.7
47	12	-3471	-27	297	0	-326	40	6.28	6.28	9.42	9.42	-3.23	-44.8
49	12	-3462	-73	341	0	-351	27	6.28	6.28	9.42	9.42	-3.34	-46.1
50	12	-3484	20	261	0	-306	52	6.28	6.28	9.42	9.42	-3.15	-43.7
51	12	-3495	-29	338	0	-351	39	6.28	6.28	9.42	9.42	-3.36	-46.4

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	25	-3576	-161	514	0	-524	-12	6.28	6.28	9.42	9.42	-4.27	-57.7
41	25	-3602	-23	383	0	-434	41	6.28	6.28	9.42	9.42	-3.79	-52.0
42	25	-3674	-29	504	0	-524	40	6.28	6.28	9.42	9.42	-4.30	-58.3
43	25	-3466	-254	558	0	-549	-50	6.28	6.28	9.42	9.42	-4.38	-58.9
44	25	-3574	209	162	0	-278	130	6.28	6.28	9.42	9.42	-3.06	-42.8
45	25	-3628	-35	542	0	-549	37	6.28	6.28	9.42	9.42	-4.43	-59.8
46	25	-3452	-26	314	0	-377	37	6.28	6.28	9.42	9.42	-3.46	-47.5
47	25	-3414	-27	297	0	-363	36	6.28	6.28	9.42	9.42	-3.37	-46.5
49	25	-3406	-73	341	0	-393	18	6.28	6.28	9.42	9.42	-3.51	-48.1
50	25	-3428	20	261	0	-339	54	6.28	6.28	9.42	9.42	-3.27	-45.2
51	25	-3438	-29	338	0	-393	36	6.28	6.28	9.42	9.42	-3.52	-48.4

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	38	-3520	-161	514	0	-588	-32	6.28	6.28	9.42	9.42	-4.64	-62.1
41	38	-3545	-23	383	0	-482	38	6.28	6.28	9.42	9.42	-4.02	-54.6
42	38	-3617	-29	504	0	-587	36	6.28	6.28	9.42	9.42	-4.66	-62.5
43	38	-3409	-254	558	0	-619	-82	6.28	6.28	9.42	9.42	-4.82	-64.0
44	38	-3518	209	162	0	-298	156	6.28	6.28	9.42	9.42	-3.13	-43.5
45	38	-3571	-35	542	0	-617	32	6.28	6.28	9.42	9.42	-4.84	-64.5
46	38	-3395	-26	314	0	-417	34	6.28	6.28	9.42	9.42	-3.62	-49.5
47	38	-3358	-27	297	0	-400	33	6.28	6.28	9.42	9.42	-3.52	-48.2
49	38	-3349	-73	341	0	-436	9	6.28	6.28	9.42	9.42	-3.69	-50.4
50	38	-3371	20	261	0	-372	57	6.28	6.28	9.42	9.42	-3.39	-46.6
51	38	-3382	-29	338	0	-436	32	6.28	6.28	9.42	9.42	-3.71	-50.6

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	50	-3464	-161	514	0	-652	-53	6.28	6.28	9.42	9.42	-5.06	-66.9
41	50	-3489	-23	383	0	-529	35	6.28	6.28	9.42	9.42	-4.27	-57.6
42	50	-3561	-29	504	0	-650	33	6.28	6.28	9.42	9.42	-5.06	-67.1
43	50	-3353	-254	558	0	-688	-114	6.28	6.28	9.42	9.42	-5.31	-69.5
44	50	-3462	209	162	0	-318	182	6.28	6.28	9.42	9.42	-3.34	-44.2
45	50	-3515	-35	542	0	-685	28	6.28	6.28	9.42	9.42	-5.30	-69.8
46	50	-3339	-26	314	0	-456	30	6.28	6.28	9.42	9.42	-3.80	-51.6
47	50	-3302	-27	297	0	-438	29	6.28	6.28	9.42	9.42	-3.68	-50.1
49	50	-3293	-73	341	0	-478	0	6.28	6.28	9.42	9.42	-3.91	-52.8
50	50	-3315	20	261	0	-404	59	6.28	6.28	9.42	9.42	-3.52	-48.1
51	50	-3326	-29	338	0	-478	29	6.28	6.28	9.42	9.42	-3.91	-53.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 112 NI 175 NF 89 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 17
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm		daN			daN*m				cm^2			daN/cm^2

40	0	-6704	-76	-181	0	592	-1	6.28	6.28	12.57	12.57	-4.71	-65.4
41	0	-6463	14	-150	0	502	-7	6.28	6.28	12.57	12.57	-4.30	-59.9
42	0	-6504	18	-401	0	2239	-7	6.28	6.28	12.57	12.57	-14.43	267.5
43	0	-6587	-132	-165	0	533	4	6.28	6.28	12.57	12.57	-4.45	-62.0
44	0	-6139	164	-106	0	376	-18	6.28	6.28	12.57	12.57	-3.72	-52.4
45	0	-6252	24	-531	0	3278	-8	6.28	6.28	12.57	12.57	-21.55	586.5
46	0	-6016	21	-92	0	312	-7	6.28	6.28	12.57	12.57	-3.44	-48.8
47	0	-5905	22	-77	0	264	-7	6.28	6.28	12.57	12.57	-3.23	-46.0
49	0	-5985	-8	-88	0	294	-5	6.28	6.28	12.57	12.57	-3.37	-47.8
50	0	-5896	51	-76	0	263	-9	6.28	6.28	12.57	12.57	-3.22	-45.9
51	0	-5918	23	-161	0	843	-7	6.28	6.28	12.57	12.57	-5.41	-73.1

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	12	-6629	-76	-181	0	615	-10	6.28	6.28	12.57	12.57	-4.76	-65.9
41	12	-6388	14	-150	0	521	-5	6.28	6.28	12.57	12.57	-4.33	-60.3
42	12	-6429	18	-401	0	2289	-5	6.28	6.28	12.57	12.57	-14.79	285.4
43	12	-6512	-132	-165	0	554	-13	6.28	6.28	12.57	12.57	-4.50	-62.5
44	12	-6064	164	-106	0	389	3	6.28	6.28	12.57	12.57	-3.74	-52.6
45	12	-6177	24	-531	0	3344	-5	6.28	6.28	12.57	12.57	-22.00	611.5
46	12	-5941	21	-92	0	323	-4	6.28	6.28	12.57	12.57	-3.45	-48.9
47	12	-5830	22	-77	0	274	-4	6.28	6.28	12.57	12.57	-3.23	-46.0
49	12	-5910	-8	-88	0	305	-6	6.28	6.28	12.57	12.57	-3.38	-47.9
50	12	-5821	51	-76	0	272	-3	6.28	6.28	12.57	12.57	-3.22	-45.9
51	12	-5843	23	-161	0	863	-4	6.28	6.28	12.57	12.57	-5.48	-74.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	25	-6554	-76	-181	0	638	-19	6.28	6.28	12.57	12.57	-4.81	-66.5
41	25	-6313	14	-150	0	540	-3	6.28	6.28	12.57	12.57	-4.37	-60.7
42	25	-6354	18	-401	0	2339	-3	6.28	6.28	12.57	12.57	-15.15	303.6
43	25	-6437	-132	-165	0	574	-29	6.28	6.28	12.57	12.57	-4.54	-63.0
44	25	-5989	164	-106	0	403	23	6.28	6.28	12.57	12.57	-3.76	-52.7
45	25	-6102	24	-531	0	3410	-2	6.28	6.28	12.57	12.57	-22.45	636.5
46	25	-5866	21	-92	0	335	-2	6.28	6.28	12.57	12.57	-3.46	-49.0
47	25	-5755	22	-77	0	283	-1	6.28	6.28	12.57	12.57	-3.24	-46.0
49	25	-5835	-8	-88	0	316	-7	6.28	6.28	12.57	12.57	-3.39	-48.0
50	25	-5746	51	-76	0	282	4	6.28	6.28	12.57	12.57	-3.23	-45.9
51	25	-5768	23	-161	0	883	-1	6.28	6.28	12.57	12.57	-5.57	-74.8

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	38	-6479	-76	-181	0	660	-29	6.28	6.28	12.57	12.57	-4.87	-67.1
41	38	-6238	14	-150	0	559	-2	6.28	6.28	12.57	12.57	-4.41	-61.2
42	38	-6279	18	-401	0	2389	-1	6.28	6.28	12.57	12.57	-15.51	322.1
43	38	-6362	-132	-165	0	595	-45	6.28	6.28	12.57	12.57	-4.59	-63.5
44	38	-5914	164	-106	0	416	44	6.28	6.28	12.57	12.57	-3.77	-52.9
45	38	-6027	24	-531	0	3477	1	6.28	6.28	12.57	12.57	-22.89	661.7
46	38	-5791	21	-92	0	346	1	6.28	6.28	12.57	12.57	-3.48	-49.1
47	38	-5680	22	-77	0	293	2	6.28	6.28	12.57	12.57	-3.24	-46.0
49	38	-5760	-8	-88	0	327	-8	6.28	6.28	12.57	12.57	-3.40	-48.0
50	38	-5671	51	-76	0	291	10	6.28	6.28	12.57	12.57	-3.23	-45.9
51	38	-5693	23	-161	0	903	2	6.28	6.28	12.57	12.57	-5.65	-75.7

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	50	-6404	-76	-181	0	683	-38	6.28	6.28	12.57	12.57	-4.92	-67.7
41	50	-6163	14	-150	0	577	0	6.28	6.28	12.57	12.57	-4.45	-61.6
42	50	-6204	18	-401	0	2439	1	6.28	6.28	12.57	12.57	-15.87	340.7
43	50	-6287	-132	-165	0	616	-62	6.28	6.28	12.57	12.57	-4.63	-64.0
44	50	-5839	164	-106	0	429	64	6.28	6.28	12.57	12.57	-3.79	-53.0
45	50	-5952	24	-531	0	3543	4	6.28	6.28	12.57	12.57	-23.33	686.9
46	50	-5716	21	-92	0	358	4	6.28	6.28	12.57	12.57	-3.49	-49.1
47	50	-5605	22	-77	0	303	4	6.28	6.28	12.57	12.57	-3.25	-46.0
49	50	-5685	-8	-88	0	338	-8	6.28	6.28	12.57	12.57	-3.41	-48.1
50	50	-5596	51	-76	0	301	17	6.28	6.28	12.57	12.57	-3.24	-45.9
51	50	-5618	23	-161	0	923	5	6.28	6.28	12.57	12.57	-5.74	-76.7

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 113 NI 89 NF 41 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 17A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-10010	-421	-321	0	652	-38	6.28	6.28	12.57	12.57	-6.20	-87.2
41	0	-9625	-37	-266	0	551	0	6.28	6.28	12.57	12.57	-5.69	-80.4
42	0	-9687	-25	-696	0	2249	1	6.28	6.28	12.57	12.57	-13.93	-178.0
43	0	-9827	-653	-293	0	589	-62	6.28	6.28	12.57	12.57	-5.91	-83.3
44	0	-9104	600	-188	0	407	64	6.28	6.28	12.57	12.57	-4.98	-71.0
45	0	-9286	6	-919	0	3249	4	6.28	6.28	12.57	12.57	-20.97	396.3
46	0	-8916	2	-163	0	341	4	6.28	6.28	12.57	12.57	-4.66	-66.9
47	0	-8739	11	-137	0	288	4	6.28	6.28	12.57	12.57	-4.41	-63.5
49	0	-8868	-117	-155	0	322	-8	6.28	6.28	12.57	12.57	-4.58	-65.8
50	0	-8723	134	-134	0	286	17	6.28	6.28	12.57	12.57	-4.39	-63.3
51	0	-8760	15	-280	0	854	5	6.28	6.28	12.57	12.57	-6.44	-89.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	12	-9936	-421	-321	0	692	-91	6.28	6.28	12.57	12.57	-6.32	-88.6
41	12	-9550	-37	-266	0	584	-4	6.28	6.28	12.57	12.57	-5.78	-81.5
42	12	-9612	-25	-696	0	2336	-2	6.28	6.28	12.57	12.57	-14.53	-184.3
43	12	-9752	-653	-293	0	626	-144	6.28	6.28	12.57	12.57	-6.01	-84.5
44	12	-9029	600	-188	0	431	139	6.28	6.28	12.57	12.57	-5.03	-71.6
45	12	-9211	6	-919	0	3364	5	6.28	6.28	12.57	12.57	-21.78	432.6
46	12	-8841	2	-163	0	361	4	6.28	6.28	12.57	12.57	-4.71	-67.4
47	12	-8664	11	-137	0	305	6	6.28	6.28	12.57	12.57	-4.44	-63.9
49	12	-8793	-117	-155	0	342	-23	6.28	6.28	12.57	12.57	-4.62	-66.2
50	12	-8648	134	-134	0	303	33	6.28	6.28	12.57	12.57	-4.42	-63.7
51	12	-8685	15	-280	0	889	7	6.28	6.28	12.57	12.57	-6.54	-90.1

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	25	-9861	-421	-321	0	733	-144	6.28	6.28	12.57	12.57	-6.43	-89.9

41	25	-9475	-37	-266	0	617	-9	6.28	6.28	12.57	12.57	-5.87	-82.5
42	25	-9537	-25	-696	0	2423	-5	6.28	6.28	12.57	12.57	-15.14	-190.7
43	25	-9677	-653	-293	0	662	-225	6.28	6.28	12.57	12.57	-6.11	-85.7
44	25	-8954	600	-188	0	454	214	6.28	6.28	12.57	12.57	-5.09	-72.2
45	25	-9136	6	-919	0	3479	6	6.28	6.28	12.57	12.57	-22.59	469.4
46	25	-8766	2	-163	0	381	4	6.28	6.28	12.57	12.57	-4.75	-67.9
47	25	-8589	11	-137	0	323	7	6.28	6.28	12.57	12.57	-4.47	-64.2
49	25	-8718	-117	-155	0	361	-38	6.28	6.28	12.57	12.57	-4.66	-66.7
50	25	-8573	134	-134	0	319	50	6.28	6.28	12.57	12.57	-4.46	-64.0
51	25	-8610	15	-280	0	924	9	6.28	6.28	12.57	12.57	-6.64	-91.3

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	38	-9786	-421	-321	0	773	-196	6.28	6.28	12.57	12.57	-6.55	-91.3
41	38	-9400	-37	-266	0	650	-14	6.28	6.28	12.57	12.57	-5.96	-83.6
42	38	-9462	-25	-696	0	2510	-8	6.28	6.28	12.57	12.57	-15.76	-197.0
43	38	-9602	-653	-293	0	699	-307	6.28	6.28	12.57	12.57	-6.21	-86.9
44	38	-8879	600	-188	0	478	289	6.28	6.28	12.57	12.57	-5.14	-72.8
45	38	-9061	6	-919	0	3594	7	6.28	6.28	12.57	12.57	-23.40	506.8
46	38	-8691	2	-163	0	402	4	6.28	6.28	12.57	12.57	-4.80	-68.3
47	38	-8514	11	-137	0	340	9	6.28	6.28	12.57	12.57	-4.51	-64.5
49	38	-8643	-117	-155	0	380	-52	6.28	6.28	12.57	12.57	-4.70	-67.1
50	38	-8498	134	-134	0	336	67	6.28	6.28	12.57	12.57	-4.49	-64.3
51	38	-8535	15	-280	0	959	10	6.28	6.28	12.57	12.57	-6.73	-92.4

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	50	-9712	-421	-321	0	813	-249	6.28	6.28	12.57	12.57	-6.66	-92.7
41	50	-9325	-37	-266	0	684	-18	6.28	6.28	12.57	12.57	-6.05	-84.6
42	50	-9387	-25	-696	0	2597	-11	6.28	6.28	12.57	12.57	-16.38	220.5
43	50	-9527	-653	-293	0	735	-389	6.28	6.28	12.57	12.57	-6.31	-88.1
44	50	-8804	600	-188	0	501	364	6.28	6.28	12.57	12.57	-5.20	-73.5
45	50	-8986	6	-919	0	3709	8	6.28	6.28	12.57	12.57	-24.20	544.6
46	50	-8616	2	-163	0	422	4	6.28	6.28	12.57	12.57	-4.84	-68.8
47	50	-8439	11	-137	0	357	10	6.28	6.28	12.57	12.57	-4.54	-64.9
49	50	-8568	-117	-155	0	400	-67	6.28	6.28	12.57	12.57	-4.74	-67.5
50	50	-8423	134	-134	0	353	84	6.28	6.28	12.57	12.57	-4.52	-64.6
51	50	-8460	15	-280	0	994	12	6.28	6.28	12.57	12.57	-6.84	-93.7

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 114 NI 477 NF 46 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 22
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-7196	-72	52	0	-93	-22	6.28	6.28	12.57	12.57	-3.11	-45.9
41	0	-7135	-7	7	0	29	-22	6.28	6.28	12.57	12.57	-2.86	-42.6
42	0	-7190	13	-130	0	1384	-25	6.28	6.28	12.57	12.57	-8.50	-111.6
43	0	-6932	-119	86	0	-194	-17	6.28	6.28	12.57	12.57	-3.37	-48.9
44	0	-7122	100	-70	0	238	-22	6.28	6.28	12.57	12.57	-3.60	-51.9
45	0	-6922	21	-218	0	2268	-23	6.28	6.28	12.57	12.57	-14.56	253.3
46	0	-6648	-15	13	0	-4	-15	6.28	6.28	12.57	12.57	-2.58	-38.7
47	0	-6527	-17	15	0	-12	-13	6.28	6.28	12.57	12.57	-2.56	-38.4
49	0	-6547	-39	30	0	-52	-13	6.28	6.28	12.57	12.57	-2.72	-40.3
50	0	-6585	5	-1	0	34	-14	6.28	6.28	12.57	12.57	-2.67	-39.7
51	0	-6545	-11	-31	0	440	-14	6.28	6.28	12.57	12.57	-4.10	-57.6

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	12	-7121	-72	52	0	-99	-31	6.28	6.28	12.57	12.57	-3.11	-45.7
41	12	-7060	-7	7	0	28	-22	6.28	6.28	12.57	12.57	-2.83	-42.2
42	12	-7115	13	-130	0	1400	-23	6.28	6.28	12.57	12.57	-8.60	-112.5
43	12	-6857	-119	86	0	-205	-32	6.28	6.28	12.57	12.57	-3.38	-48.9
44	12	-7047	100	-70	0	246	-9	6.28	6.28	12.57	12.57	-3.60	-51.9
45	12	-6847	21	-218	0	2295	-20	6.28	6.28	12.57	12.57	-14.76	264.6
46	12	-6573	-15	13	0	-5	-17	6.28	6.28	12.57	12.57	-2.56	-38.3
47	12	-6452	-17	15	0	-14	-15	6.28	6.28	12.57	12.57	-2.54	-38.0
49	12	-6472	-39	30	0	-56	-18	6.28	6.28	12.57	12.57	-2.70	-40.0
50	12	-6510	5	-1	0	34	-13	6.28	6.28	12.57	12.57	-2.64	-39.2
51	12	-6470	-11	-31	0	444	-15	6.28	6.28	12.57	12.57	-4.09	-57.4

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	25	-7046	-72	52	0	-106	-40	6.28	6.28	12.57	12.57	-3.10	-45.6
41	25	-6985	-7	7	0	27	-23	6.28	6.28	12.57	12.57	-2.80	-41.7
42	25	-7040	13	-130	0	1416	-22	6.28	6.28	12.57	12.57	-8.70	-113.5
43	25	-6782	-119	86	0	-216	-47	6.28	6.28	12.57	12.57	-3.39	-48.9
44	25	-6972	100	-70	0	255	3	6.28	6.28	12.57	12.57	-3.61	-51.8
45	25	-6772	21	-218	0	2322	-17	6.28	6.28	12.57	12.57	-14.96	275.9
46	25	-6498	-15	13	0	-7	-19	6.28	6.28	12.57	12.57	-2.54	-38.0
47	25	-6377	-17	15	0	-16	-17	6.28	6.28	12.57	12.57	-2.52	-37.7
49	25	-6397	-39	30	0	-60	-23	6.28	6.28	12.57	12.57	-2.69	-39.8
50	25	-6435	5	-1	0	34	-13	6.28	6.28	12.57	12.57	-2.61	-38.8
51	25	-6395	-11	-31	0	448	-17	6.28	6.28	12.57	12.57	-4.07	-57.1

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	38	-6971	-72	52	0	-112	-48	6.28	6.28	12.57	12.57	-3.09	-45.4
41	38	-6910	-7	7	0	26	-24	6.28	6.28	12.57	12.57	-2.76	-41.2
42	38	-6965	13	-130	0	1433	-20	6.28	6.28	12.57	12.57	-8.81	-114.6
43	38	-6707	-119	86	0	-226	-62	6.28	6.28	12.57	12.57	-3.40	-49.0
44	38	-6897	100	-70	0	264	16	6.28	6.28	12.57	12.57	-3.61	-51.8
45	38	-6697	21	-218	0	2349	-15	6.28	6.28	12.57	12.57	-15.16	287.5
46	38	-6423	-15	13	0	-9	-20	6.28	6.28	12.57	12.57	-2.51	-37.6
47	38	-6302	-17	15	0	-18	-19	6.28	6.28	12.57	12.57	-2.50	-37.3
49	38	-6322	-39	30	0	-64	-28	6.28	6.28	12.57	12.57	-2.67	-39.5
50	38	-6360	5	-1	0	34	-12	6.28	6.28	12.57	12.57	-2.58	-38.4
51	38	-6320	-11	-31	0	451	-18	6.28	6.28	12.57	12.57	-4.06	-56.8

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	50	-6896	-72	52	0	-119	-57	6.28	6.28	12.57	12.57	-3.09	-45.3
41	50	-6835	-7	7	0	25	-25	6.28	6.28	12.57	12.57	-2.73	-40.7

42	50	-6890	13	-130	0	1449	-18	6.28	6.28	12.57	12.57	-8.91	-115.6
43	50	-6632	-119	86	0	-237	-77	6.28	6.28	12.57	12.57	-3.41	-49.0
44	50	-6822	100	-70	0	272	28	6.28	6.28	12.57	12.57	-3.61	-51.7
45	50	-6622	21	-218	0	2376	-12	6.28	6.28	12.57	12.57	-15.36	299.1
46	50	-6348	-15	13	0	-10	-22	6.28	6.28	12.57	12.57	-2.49	-37.3
47	50	-6227	-17	15	0	-19	-22	6.28	6.28	12.57	12.57	-2.47	-37.0
49	50	-6247	-39	30	0	-67	-32	6.28	6.28	12.57	12.57	-2.65	-39.2
50	50	-6285	5	-1	0	35	-11	6.28	6.28	12.57	12.57	-2.55	-38.0
51	50	-6245	-11	-31	0	455	-19	6.28	6.28	12.57	12.57	-4.04	-56.6

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 115 NI 46 NF 42 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 22A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-10810	-789	93	0	-120	-57	6.28	6.28	12.57	12.57	-4.61	-68.0
41	0	-10730	-434	13	0	20	-25	6.28	6.28	12.57	12.57	-4.22	-63.1
42	0	-10800	-377	-216	0	1300	-18	6.28	6.28	12.57	12.57	-8.85	-121.0
43	0	-10390	-978	153	0	-234	-77	6.28	6.28	12.57	12.57	-4.85	-70.7
44	0	-10740	151	-123	0	259	28	6.28	6.28	12.57	12.57	-5.08	-73.8
45	0	-10370	-291	-362	0	2133	-12	6.28	6.28	12.57	12.57	-13.11	-170.5
46	0	-9969	-359	24	0	-13	-22	6.28	6.28	12.57	12.57	-3.90	-58.4
47	0	-9778	-340	27	0	-22	-22	6.28	6.28	12.57	12.57	-3.86	-57.6
49	0	-9804	-458	53	0	-68	-32	6.28	6.28	12.57	12.57	-4.03	-59.9
50	0	-9874	-232	-2	0	30	-11	6.28	6.28	12.57	12.57	-3.92	-58.6
51	0	-9801	-321	-50	0	405	-19	6.28	6.28	12.57	12.57	-5.24	-74.9

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	12	-10735	-789	93	0	-132	-156	6.28	6.28	12.57	12.57	-4.64	-68.1
41	12	-10655	-434	13	0	18	-80	6.28	6.28	12.57	12.57	-4.23	-62.6
42	12	-10725	-377	-216	0	1327	-65	6.28	6.28	12.57	12.57	-8.93	-122.0
43	12	-10315	-978	153	0	-253	-199	6.28	6.28	12.57	12.57	-4.89	-71.1
44	12	-10665	151	-123	0	275	47	6.28	6.28	12.57	12.57	-5.10	-74.1
45	12	-10295	-291	-362	0	2178	-48	6.28	6.28	12.57	12.57	-13.40	-173.7
46	12	-9894	-359	24	0	-16	-67	6.28	6.28	12.57	12.57	-3.89	-58.1
47	12	-9703	-340	27	0	-25	-64	6.28	6.28	12.57	12.57	-3.84	-57.4
49	12	-9729	-458	53	0	-75	-90	6.28	6.28	12.57	12.57	-4.03	-59.7
50	12	-9799	-232	-2	0	31	-40	6.28	6.28	12.57	12.57	-3.90	-58.2
51	12	-9726	-321	-50	0	411	-59	6.28	6.28	12.57	12.57	-5.23	-74.8

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	25	-10660	-789	93	0	-143	-255	6.28	6.28	12.57	12.57	-5.10	-71.7
41	25	-10580	-434	13	0	16	-134	6.28	6.28	12.57	12.57	-4.47	-64.6
42	25	-10650	-377	-216	0	1354	-113	6.28	6.28	12.57	12.57	-9.02	-122.9
43	25	-10240	-978	153	0	-272	-322	6.28	6.28	12.57	12.57	-5.28	-73.2
44	25	-10590	151	-123	0	290	66	6.28	6.28	12.57	12.57	-5.13	-74.4
45	25	-10220	-291	-362	0	2224	-85	6.28	6.28	12.57	12.57	-13.70	-176.8
46	25	-9819	-359	24	0	-19	-112	6.28	6.28	12.57	12.57	-4.09	-59.3
47	25	-9628	-340	27	0	-28	-107	6.28	6.28	12.57	12.57	-3.99	-57.9
49	25	-9654	-458	53	0	-82	-147	6.28	6.28	12.57	12.57	-4.20	-60.3
50	25	-9724	-232	-2	0	31	-69	6.28	6.28	12.57	12.57	-3.87	-57.7
51	25	-9651	-321	-50	0	417	-99	6.28	6.28	12.57	12.57	-5.22	-74.6

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	38	-10585	-789	93	0	-155	-353	6.28	6.28	12.57	12.57	-5.56	-76.8
41	38	-10505	-434	13	0	15	-188	6.28	6.28	12.57	12.57	-4.71	-67.2
42	38	-10575	-377	-216	0	1381	-160	6.28	6.28	12.57	12.57	-9.11	-123.9
43	38	-10165	-978	153	0	-291	-444	6.28	6.28	12.57	12.57	-5.85	-79.6
44	38	-10515	151	-123	0	306	85	6.28	6.28	12.57	12.57	-5.16	-74.6
45	38	-10145	-291	-362	0	2269	-121	6.28	6.28	12.57	12.57	-14.01	-180.0
46	38	-9744	-359	24	0	-22	-157	6.28	6.28	12.57	12.57	-4.28	-61.4
47	38	-9553	-340	27	0	-32	-149	6.28	6.28	12.57	12.57	-4.18	-59.9
49	38	-9579	-458	53	0	-88	-204	6.28	6.28	12.57	12.57	-4.46	-63.1
50	38	-9649	-232	-2	0	31	-98	6.28	6.28	12.57	12.57	-3.96	-57.6
51	38	-9576	-321	-50	0	424	-140	6.28	6.28	12.57	12.57	-5.22	-74.5

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	50	-10510	-789	93	0	-166	-452	6.28	6.28	12.57	12.57	-6.02	-81.9
41	50	-10430	-434	13	0	13	-242	6.28	6.28	12.57	12.57	-4.95	-69.8
42	50	-10500	-377	-216	0	1408	-207	6.28	6.28	12.57	12.57	-9.20	-125.0
43	50	-10090	-978	153	0	-310	-566	6.28	6.28	12.57	12.57	-6.43	-86.0
44	50	-10440	151	-123	0	321	104	6.28	6.28	12.57	12.57	-5.18	-74.9
45	50	-10070	-291	-362	0	2314	-158	6.28	6.28	12.57	12.57	-14.32	-183.2
46	50	-9669	-359	24	0	-25	-202	6.28	6.28	12.57	12.57	-4.48	-63.4
47	50	-9478	-340	27	0	-35	-192	6.28	6.28	12.57	12.57	-4.36	-61.8
49	50	-9504	-458	53	0	-95	-261	6.28	6.28	12.57	12.57	-4.71	-65.9
50	50	-9574	-232	-2	0	31	-127	6.28	6.28	12.57	12.57	-4.08	-58.8
51	50	-9501	-321	-50	0	430	-180	6.28	6.28	12.57	12.57	-5.21	-74.3

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 116 NI 216 NF 482 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 32
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-2654	-1303	559	0	197	790	6.28	6.28	12.57	12.57	-6.41	108.1
41	0	-2722	-938	323	0	134	580	6.28	6.28	12.57	12.57	-4.73	56.4
42	0	-2486	-595	-670	0	-356	482	6.28	6.28	12.57	12.57	-3.94	-44.7
43	0	-2641	-1401	610	0	228	815	6.28	6.28	12.57	12.57	-6.61	114.6
44	0	-2849	-351	-60	0	31	248	6.28	6.28	12.57	12.57	-2.26	-29.3
45	0	-2360	-221	-1439	0	-694	301	6.28	6.28	12.57	12.57	-4.40	65.5

46	0	-2773	-704	152	0	118	396	6.28	6.28	12.57	12.57	-3.27	-39.4
47	0	-2785	-645	109	0	114	350	6.28	6.28	12.57	12.57	-2.92	-36.0
49	0	-2763	-767	188	0	134	420	6.28	6.28	12.57	12.57	-3.45	-41.2
50	0	-2804	-557	54	0	95	307	6.28	6.28	12.57	12.57	-2.62	-33.0
51	0	-2706	-531	-222	0	-50	317	6.28	6.28	12.57	12.57	-2.68	-33.4

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	12	-2579	-1303	559	0	127	627	6.28	6.28	12.57	12.57	-5.11	71.3
41	12	-2647	-938	323	0	94	462	6.28	6.28	12.57	12.57	-3.79	-43.9
42	12	-2411	-595	-670	0	-272	407	6.28	6.28	12.57	12.57	-3.34	-39.0
43	12	-2566	-1401	610	0	152	640	6.28	6.28	12.57	12.57	-5.21	74.8
44	12	-2774	-351	-60	0	39	204	6.28	6.28	12.57	12.57	-2.01	-26.3
45	12	-2285	-221	-1439	0	-514	274	6.28	6.28	12.57	12.57	-3.17	-40.8
46	12	-2698	-704	152	0	99	308	6.28	6.28	12.57	12.57	-2.61	-32.7
47	12	-2710	-645	109	0	100	269	6.28	6.28	12.57	12.57	-2.36	-30.0
49	12	-2688	-767	188	0	111	324	6.28	6.28	12.57	12.57	-2.72	-33.8
50	12	-2729	-557	54	0	88	237	6.28	6.28	12.57	12.57	-2.17	-28.0
51	12	-2631	-531	-222	0	-22	251	6.28	6.28	12.57	12.57	-2.22	-28.5

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	25	-2504	-1303	559	0	57	464	6.28	6.28	12.57	12.57	-3.79	-43.5
41	25	-2572	-938	323	0	54	345	6.28	6.28	12.57	12.57	-2.86	-34.9
42	25	-2336	-595	-670	0	-189	333	6.28	6.28	12.57	12.57	-2.75	-33.1
43	25	-2491	-1401	610	0	76	465	6.28	6.28	12.57	12.57	-3.80	-43.5
44	25	-2699	-351	-60	0	46	160	6.28	6.28	12.57	12.57	-1.76	-23.5
45	25	-2210	-221	-1439	0	-334	246	6.28	6.28	12.57	12.57	-2.11	-28.4
46	25	-2623	-704	152	0	80	220	6.28	6.28	12.57	12.57	-2.04	-26.5
47	25	-2635	-645	109	0	86	189	6.28	6.28	12.57	12.57	-1.88	-24.7
49	25	-2613	-767	188	0	88	228	6.28	6.28	12.57	12.57	-2.08	-26.9
50	25	-2654	-557	54	0	82	167	6.28	6.28	12.57	12.57	-1.78	-23.6
51	25	-2556	-531	-222	0	6	185	6.28	6.28	12.57	12.57	-1.83	-24.1

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	38	-2429	-1303	559	0	-13	301	6.28	6.28	12.57	12.57	-2.52	-31.1
41	38	-2497	-938	323	0	13	228	6.28	6.28	12.57	12.57	-2.05	-26.4
42	38	-2261	-595	-670	0	-105	258	6.28	6.28	12.57	12.57	-2.19	-27.4
43	38	-2416	-1401	610	0	-0	290	6.28	6.28	12.57	12.57	-2.43	-30.2
44	38	-2624	-351	-60	0	54	116	6.28	6.28	12.57	12.57	-1.52	-20.6
45	38	-2135	-221	-1439	0	-154	219	6.28	6.28	12.57	12.57	-1.90	-24.1
46	38	-2548	-704	152	0	61	132	6.28	6.28	12.57	12.57	-1.57	-21.1
47	38	-2560	-645	109	0	73	108	6.28	6.28	12.57	12.57	-1.46	-19.8
49	38	-2538	-767	188	0	64	132	6.28	6.28	12.57	12.57	-1.57	-21.1
50	38	-2579	-557	54	0	75	98	6.28	6.28	12.57	12.57	-1.41	-19.4
51	38	-2481	-531	-222	0	33	118	6.28	6.28	12.57	12.57	-1.48	-20.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	50	-2354	-1303	559	0	-82	138	6.28	6.28	12.57	12.57	-1.53	-20.4
41	50	-2422	-938	323	0	-27	111	6.28	6.28	12.57	12.57	-1.42	-19.2
42	50	-2186	-595	-670	0	-21	184	6.28	6.28	12.57	12.57	-1.70	-22.1
43	50	-2341	-1401	610	0	-76	115	6.28	6.28	12.57	12.57	-1.41	-19.0
44	50	-2549	-351	-60	0	61	72	6.28	6.28	12.57	12.57	-1.27	-17.8
45	50	-2060	-221	-1439	0	26	191	6.28	6.28	12.57	12.57	-1.71	-21.9
46	50	-2473	-704	152	0	42	44	6.28	6.28	12.57	12.57	-1.11	-16.2
47	50	-2485	-645	109	0	59	27	6.28	6.28	12.57	12.57	-1.17	-17.1
49	50	-2463	-767	188	0	41	37	6.28	6.28	12.57	12.57	-1.10	-16.1
50	50	-2504	-557	54	0	68	28	6.28	6.28	12.57	12.57	-1.21	-17.6
51	50	-2406	-531	-222	0	61	52	6.28	6.28	12.57	12.57	-1.15	-16.7

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 117 NI 482 NF 33 SEZ. Rp B= 0.600 H= 0.400 (pilastro)
PIL. NUM. 32A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-4550	509	332	0	37	-227	6.28	6.28	12.57	12.57	-2.76	-37.2
41	0	-4385	467	252	0	71	-156	6.28	6.28	12.57	12.57	-2.35	-32.4
42	0	-4262	545	-4	0	301	-125	6.28	6.28	12.57	12.57	-2.72	-38.2
43	0	-4493	417	321	0	38	-265	6.28	6.28	12.57	12.57	-2.93	-39.0
44	0	-4164	417	124	0	128	-38	6.28	6.28	12.57	12.57	-2.07	-29.9
45	0	-4013	476	-240	0	478	-94	6.28	6.28	12.57	12.57	-3.27	-44.7
46	0	-4118	273	148	0	110	-140	6.28	6.28	12.57	12.57	-2.17	-30.0
47	0	-4051	224	122	0	119	-135	6.28	6.28	12.57	12.57	-2.13	-29.4
49	0	-4106	238	149	0	108	-159	6.28	6.28	12.57	12.57	-2.27	-31.0
50	0	-4040	239	110	0	126	-114	6.28	6.28	12.57	12.57	-2.02	-29.1
51	0	-4010	250	37	0	196	-125	6.28	6.28	12.57	12.57	-2.25	-32.0

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	12	-4475	509	332	0	-5	-164	6.28	6.28	12.57	12.57	-2.42	-33.3
41	12	-4310	467	252	0	40	-98	6.28	6.28	12.57	12.57	-2.03	-28.7
42	12	-4187	545	-4	0	301	-57	6.28	6.28	12.57	12.57	-2.70	-37.7
43	12	-4418	417	321	0	-2	-213	6.28	6.28	12.57	12.57	-2.64	-35.7
44	12	-4089	417	124	0	113	14	6.28	6.28	12.57	12.57	-1.98	-28.7
45	12	-3938	476	-240	0	508	-34	6.28	6.28	12.57	12.57	-3.36	-45.8
46	12	-4043	273	148	0	91	-105	6.28	6.28	12.57	12.57	-1.98	-27.7
47	12	-3976	224	122	0	104	-107	6.28	6.28	12.57	12.57	-1.96	-27.7
49	12	-4031	238	149	0	89	-129	6.28	6.28	12.57	12.57	-2.09	-29.0
50	12	-3965	239	110	0	112	-84	6.28	6.28	12.57	12.57	-1.93	-28.0
51	12	-3935	250	37	0	191	-94	6.28	6.28	12.57	12.57	-2.20	-31.4

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	25	-4400	509	332	0	-46	-100	6.28	6.28	12.57	12.57	-2.08	-29.3
41	25	-4235	467	252	0	8	-39	6.28	6.28	12.57	12.57	-1.72	-25.1
42	25	-4112	545	-4	0	302	11	6.28	6.28	12.57	12.57	-2.67	-37.3
43	25	-4343	417	321	0	-43	-161	6.28	6.28	12.57	12.57	-2.36	-32.4
44	25	-4014	417	124	0	97	66	6.28	6.28	12.57	12.57	-1.90	-27.6
45	25	-3863	476	-240	0	538	25	6.28	6.28	12.57	12.57	-3.47	-47.0
46	25	-3968	273	148	0	73	-71	6.28	6.28	12.57	12.57	-1.79	-26.3

47	25	-3901	224	122	0	89	-79	6.28	6.28	12.57	12.57	-1.83	-26.6
49	25	-3956	238	149	0	71	-100	6.28	6.28	12.57	12.57	-1.92	-26.9
50	25	-3890	239	110	0	99	-54	6.28	6.28	12.57	12.57	-1.86	-27.0
51	25	-3860	250	37	0	187	-62	6.28	6.28	12.57	12.57	-2.16	-30.7

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	38	-4325	509	332	0	-88	-36	6.28	6.28	12.57	12.57	-1.99	-29.0
41	38	-4160	467	252	0	-23	19	6.28	6.28	12.57	12.57	-1.69	-25.1
42	38	-4037	545	-4	0	302	80	6.28	6.28	12.57	12.57	-2.64	-36.9
43	38	-4268	417	321	0	-83	-109	6.28	6.28	12.57	12.57	-2.07	-29.1
44	38	-3939	417	124	0	82	118	6.28	6.28	12.57	12.57	-2.00	-27.8
45	38	-3788	476	-240	0	567	85	6.28	6.28	12.57	12.57	-3.59	-48.4
46	38	-3893	273	148	0	54	-37	6.28	6.28	12.57	12.57	-1.70	-25.0
47	38	-3826	224	122	0	74	-51	6.28	6.28	12.57	12.57	-1.74	-25.5
49	38	-3881	238	149	0	52	-70	6.28	6.28	12.57	12.57	-1.74	-24.8
50	38	-3815	239	110	0	85	-25	6.28	6.28	12.57	12.57	-1.78	-25.9
51	38	-3785	250	37	0	182	-31	6.28	6.28	12.57	12.57	-2.11	-30.1

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

40	50	-4250	509	332	0	-129	27	6.28	6.28	12.57	12.57	-2.11	-30.4
41	50	-4085	467	252	0	-54	77	6.28	6.28	12.57	12.57	-1.85	-26.4
42	50	-3962	545	-4	0	303	148	6.28	6.28	12.57	12.57	-2.61	-36.5
43	50	-4193	417	321	0	-123	-57	6.28	6.28	12.57	12.57	-2.06	-29.8
44	50	-3864	417	124	0	66	170	6.28	6.28	12.57	12.57	-2.23	-30.3
45	50	-3713	476	-240	0	597	144	6.28	6.28	12.57	12.57	-3.73	-49.9
46	50	-3818	273	148	0	36	-3	6.28	6.28	12.57	12.57	-1.60	-23.7
47	50	-3751	224	122	0	58	-23	6.28	6.28	12.57	12.57	-1.66	-24.3
49	50	-3806	238	149	0	33	-40	6.28	6.28	12.57	12.57	-1.59	-23.5
50	50	-3740	239	110	0	71	5	6.28	6.28	12.57	12.57	-1.70	-24.9
51	50	-3710	250	37	0	177	0	6.28	6.28	12.57	12.57	-2.07	-29.4

apost= -- aant= -- ainf= 6.28 asup= 6.28 (e arm. base= 4 X 3.14)

ASTA NUM. 118 NI 803 NF 821 SEZ. Rp B= 0.400 H= 0.600 (pilastro)
PIL. NUM. 26
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-4651	3210	360	0	77	-1607	12.57	12.57	6.28	6.28	-10.36	192.9
41	0	-4686	2019	292	0	63	-254	12.57	12.57	6.28	6.28	-2.72	-38.5
42	0	-4687	2023	170	0	51	-250	12.57	12.57	6.28	6.28	-2.70	-38.3
43	0	-4508	3557	328	0	77	-2364	12.57	12.57	6.28	6.28	-15.54	423.0
44	0	-4711	105	196	0	40	1979	12.57	12.57	6.28	6.28	-12.92	295.6
45	0	-4568	1580	13	0	32	-103	12.57	12.57	6.28	6.28	-2.13	-31.1
46	0	-4495	1306	169	0	47	-24	12.57	12.57	6.28	6.28	-1.85	-27.1
47	0	-4447	1127	138	0	42	33	12.57	12.57	6.28	6.28	-1.84	-27.3
49	0	-4436	1524	161	0	47	-418	12.57	12.57	6.28	6.28	-3.21	-44.4
50	0	-4476	834	134	0	40	451	12.57	12.57	6.28	6.28	-3.34	-46.1
51	0	-4447	1129	98	0	38	35	12.57	12.57	6.28	6.28	-1.84	-27.3

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	12	-4576	3210	360	0	32	-1206	12.57	12.57	6.28	6.28	-7.56	-94.7
41	12	-4611	2019	292	0	27	-2	12.57	12.57	6.28	6.28	-1.79	-26.8
42	12	-4612	2023	170	0	29	3	12.57	12.57	6.28	6.28	-1.81	-26.9
43	12	-4433	3557	328	0	36	-1919	12.57	12.57	6.28	6.28	-12.55	294.9
44	12	-4636	105	196	0	16	1992	12.57	12.57	6.28	6.28	-13.02	303.9
45	12	-4493	1580	13	0	31	95	12.57	12.57	6.28	6.28	-2.08	-30.3
46	12	-4420	1306	169	0	25	139	12.57	12.57	6.28	6.28	-2.21	-31.8
47	12	-4372	1127	138	0	25	174	12.57	12.57	6.28	6.28	-2.31	-33.1
49	12	-4361	1524	161	0	27	-227	12.57	12.57	6.28	6.28	-2.50	-35.4
50	12	-4401	834	134	0	23	555	12.57	12.57	6.28	6.28	-3.71	-50.6
51	12	-4372	1129	98	0	26	176	12.57	12.57	6.28	6.28	-2.32	-33.2

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	25	-4501	3210	360	0	-13	-804	12.57	12.57	6.28	6.28	-4.96	-65.6
41	25	-4536	2019	292	0	-10	250	12.57	12.57	6.28	6.28	-2.65	-37.5
42	25	-4537	2023	170	0	8	256	12.57	12.57	6.28	6.28	-2.67	-37.8
43	25	-4358	3557	328	0	-6	-1475	12.57	12.57	6.28	6.28	-9.49	172.2
44	25	-4561	105	196	0	-9	2005	12.57	12.57	6.28	6.28	-13.12	312.3
45	25	-4418	1580	13	0	29	292	12.57	12.57	6.28	6.28	-2.75	-38.7
46	25	-4345	1306	169	0	4	302	12.57	12.57	6.28	6.28	-2.76	-38.7
47	25	-4297	1127	138	0	8	315	12.57	12.57	6.28	6.28	-2.79	-39.0
49	25	-4286	1524	161	0	7	-36	12.57	12.57	6.28	6.28	-1.79	-26.5
50	25	-4326	834	134	0	6	660	12.57	12.57	6.28	6.28	-4.16	-56.0
51	25	-4297	1129	98	0	14	317	12.57	12.57	6.28	6.28	-2.80	-39.1

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	38	-4426	3210	360	0	-58	-403	12.57	12.57	6.28	6.28	-3.15	-43.7
41	38	-4461	2019	292	0	-46	503	12.57	12.57	6.28	6.28	-3.53	-48.4
42	38	-4462	2023	170	0	-13	509	12.57	12.57	6.28	6.28	-3.55	-48.7
43	38	-4283	3557	328	0	-47	-1030	12.57	12.57	6.28	6.28	-6.40	-81.3
44	38	-4486	105	196	0	-33	2018	12.57	12.57	6.28	6.28	-13.22	320.8
45	38	-4343	1580	13	0	27	490	12.57	12.57	6.28	6.28	-3.43	-47.1
46	38	-4270	1306	169	0	-17	465	12.57	12.57	6.28	6.28	-3.32	-45.6
47	38	-4222	1127	138	0	-9	456	12.57	12.57	6.28	6.28	-3.26	-44.9
49	38	-4211	1524	161	0	-13	154	12.57	12.57	6.28	6.28	-2.18	-31.3
50	38	-4251	834	134	0	-10	764	12.57	12.57	6.28	6.28	-4.71	-62.3
51	38	-4222	1129	98	0	2	458	12.57	12.57	6.28	6.28	-3.27	-45.0

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	50	-4351	3210	360	0	-102	-2	12.57	12.57	6.28	6.28	-2.07	-29.2
41	50	-4386	2019	292	0	-83	755	12.57	12.57	6.28	6.28	-4.67	-62.1
42	50	-4387	2023	170	0	-34	762	12.57	12.57	6.28	6.28	-4.71	-62.5
43	50	-4208	3557	328	0	-88	-586	12.57	12.57	6.28	6.28	-3.78	-51.2
44	50	-4411	105	196	0	-58	2031	12.57	12.57	6.28	6.28	-13.31	329.3
45	50	-4268	1580	13	0	26	687	12.57	12.57	6.28	6.28	-4.29	-57.4
46	50	-4195	1306	169	0	-38	629	12.57	12.57	6.28	6.28	-3.98	-53.6
47	50	-4147	1127	138	0	-27	597	12.57	12.57	6.28	6.28	-3.82	-51.6

49	50	-4136	1524	161	0	-33	345	12.57	12.57	6.28	6.28	-2.83	-39.4
50	50	-4176	834	134	0	-27	868	12.57	12.57	6.28	6.28	-5.34	-69.3
51	50	-4147	1129	98	0	-11	599	12.57	12.57	6.28	6.28	-3.83	-51.7

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

ASTA NUM. 119 NI 821 NF 166 SEZ. Rp B= 0.400 H= 0.600 (pilastro)
PIL. NUM. 26A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-5896	1340	969	0	-102	-71	12.57	12.57	6.28	6.28	-2.63	-37.5
41	0	-5684	1145	832	0	-83	689	12.57	12.57	6.28	6.28	-4.68	-63.9
42	0	-5683	1147	378	0	-34	695	12.57	12.57	6.28	6.28	-4.70	-64.2
43	0	-5845	1265	783	0	-88	-642	12.57	12.57	6.28	6.28	-4.56	-62.6
44	0	-5286	854	683	0	-58	1968	12.57	12.57	6.28	6.28	-12.76	258.8
45	0	-5490	944	-201	0	26	635	12.57	12.57	6.28	6.28	-4.40	-60.3
46	0	-5376	818	389	0	-38	587	12.57	12.57	6.28	6.28	-4.18	-57.4
47	0	-5300	737	278	0	-27	561	12.57	12.57	6.28	6.28	-4.06	-55.8
49	0	-5370	801	324	0	-33	308	12.57	12.57	6.28	6.28	-3.18	-44.9
50	0	-5258	719	304	0	-27	830	12.57	12.57	6.28	6.28	-5.20	-69.7
51	0	-5299	737	127	0	-11	563	12.57	12.57	6.28	6.28	-4.06	-55.9

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	12	-5821	1340	969	0	-224	96	12.57	12.57	6.28	6.28	-3.20	-43.9
41	12	-5609	1145	832	0	-187	832	12.57	12.57	6.28	6.28	-5.28	-71.2
42	12	-5608	1147	378	0	-82	838	12.57	12.57	6.28	6.28	-5.31	-71.5
43	12	-5770	1265	783	0	-186	-484	12.57	12.57	6.28	6.28	-3.96	-55.1
44	12	-5211	854	683	0	-143	2075	12.57	12.57	6.28	6.28	-13.51	293.7
45	12	-5415	944	-201	0	51	753	12.57	12.57	6.28	6.28	-4.86	-65.9
46	12	-5301	818	389	0	-86	689	12.57	12.57	6.28	6.28	-4.55	-62.0
47	12	-5225	737	278	0	-61	653	12.57	12.57	6.28	6.28	-4.38	-59.8
49	12	-5295	801	324	0	-74	408	12.57	12.57	6.28	6.28	-3.51	-48.9
50	12	-5183	719	304	0	-65	920	12.57	12.57	6.28	6.28	-5.67	-75.1
51	12	-5224	737	127	0	-26	655	12.57	12.57	6.28	6.28	-4.39	-59.9

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	25	-5746	1340	969	0	-345	264	12.57	12.57	6.28	6.28	-3.77	-50.2
41	25	-5534	1145	832	0	-291	976	12.57	12.57	6.28	6.28	-6.02	-79.8
42	25	-5533	1147	378	0	-129	981	12.57	12.57	6.28	6.28	-6.05	-80.2
43	25	-5695	1265	783	0	-283	-326	12.57	12.57	6.28	6.28	-3.45	-47.6
44	25	-5136	854	683	0	-228	2182	12.57	12.57	6.28	6.28	-14.25	329.2
45	25	-5340	944	-201	0	76	870	12.57	12.57	6.28	6.28	-5.42	-72.5
46	25	-5226	818	389	0	-135	791	12.57	12.57	6.28	6.28	-5.00	-67.3
47	25	-5150	737	278	0	-96	745	12.57	12.57	6.28	6.28	-4.76	-64.3
49	25	-5220	801	324	0	-114	508	12.57	12.57	6.28	6.28	-3.84	-53.0
50	25	-5108	719	304	0	-103	1009	12.57	12.57	6.28	6.28	-6.20	-81.1
51	25	-5149	737	127	0	-42	747	12.57	12.57	6.28	6.28	-4.77	-64.4

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	38	-5671	1340	969	0	-466	431	12.57	12.57	6.28	6.28	-4.36	-56.6
41	38	-5459	1145	832	0	-395	1119	12.57	12.57	6.28	6.28	-6.88	-89.5
42	38	-5458	1147	378	0	-176	1125	12.57	12.57	6.28	6.28	-6.91	-89.9
43	38	-5620	1265	783	0	-381	-168	12.57	12.57	6.28	6.28	-3.91	-51.6
44	38	-5061	854	683	0	-314	2288	12.57	12.57	6.28	6.28	-14.99	365.3
45	38	-5265	944	-201	0	101	988	12.57	12.57	6.28	6.28	-6.07	-80.0
46	38	-5151	818	389	0	-184	894	12.57	12.57	6.28	6.28	-5.52	-73.3
47	38	-5075	737	278	0	-131	837	12.57	12.57	6.28	6.28	-5.21	-69.5
49	38	-5145	801	324	0	-155	608	12.57	12.57	6.28	6.28	-4.17	-57.1
50	38	-5033	719	304	0	-141	1099	12.57	12.57	6.28	6.28	-6.78	-87.4
51	38	-5074	737	127	0	-58	840	12.57	12.57	6.28	6.28	-5.22	-69.6

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

40	50	-5596	1340	969	0	-587	599	12.57	12.57	6.28	6.28	-5.06	-64.1
41	50	-5384	1145	832	0	-499	1262	12.57	12.57	6.28	6.28	-7.82	-99.8
42	50	-5383	1147	378	0	-224	1268	12.57	12.57	6.28	6.28	-7.86	-100.2
43	50	-5545	1265	783	0	-479	-10	12.57	12.57	6.28	6.28	-4.39	-56.8
44	50	-4986	854	683	0	-399	2395	12.57	12.57	6.28	6.28	-15.72	401.8
45	50	-5190	944	-201	0	126	1106	12.57	12.57	6.28	6.28	-6.81	-88.1
46	50	-5076	818	389	0	-232	996	12.57	12.57	6.28	6.28	-6.12	-80.1
47	50	-5000	737	278	0	-166	930	12.57	12.57	6.28	6.28	-5.72	-75.3
49	50	-5070	801	324	0	-195	708	12.57	12.57	6.28	6.28	-4.57	-61.9
50	50	-4958	719	304	0	-179	1189	12.57	12.57	6.28	6.28	-7.39	-93.9
51	50	-4999	737	127	0	-74	932	12.57	12.57	6.28	6.28	-5.73	-75.5

apost= 6.28 aant= 6.28 ainf= -- asup= -- (e arm. base= 4 X 3.14)

ASTA NUM. 120 NI 804 NF 827 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 25
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-7621	330	613	0	7	-358	6.28	6.28	9.42	9.42	-6.94	-87.7
41	0	-7117	189	530	0	17	-68	6.28	6.28	9.42	9.42	-4.04	-57.5
42	0	-7036	189	362	0	34	-69	6.28	6.28	9.42	9.42	-4.02	-57.1
43	0	-7635	383	552	0	6	-538	6.28	6.28	9.42	9.42	-8.79	-105.7
44	0	-6233	-40	417	0	31	413	6.28	6.28	9.42	9.42	-6.88	-83.5
45	0	-6659	148	135	0	51	-58	6.28	6.28	9.42	9.42	-3.73	-53.2
46	0	-6601	123	346	0	26	-47	6.28	6.28	9.42	9.42	-3.60	-51.9
47	0	-6472	107	300	0	28	-42	6.28	6.28	9.42	9.42	-3.50	-50.5
49	0	-6641	154	328	0	25	-139	6.28	6.28	9.42	9.42	-4.46	-60.6
50	0	-6360	69	300	0	30	51	6.28	6.28	9.42	9.42	-3.53	-50.5
51	0	-6445	107	244	0	34	-43	6.28	6.28	9.42	9.42	-3.49	-50.6

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	12	-7565	330	613	0	-70	-316	6.28	6.28	9.42	9.42	-6.54	-83.5
41	12	-7061	189	530	0	-50	-44	6.28	6.28	9.42	9.42	-3.80	-56.1
42	12	-6980	189	362	0	-11	-46	6.28	6.28	9.42	9.42	-3.77	-54.5
43	12	-7579	383	552	0	-63	-490	6.28	6.28	9.42	9.42	-8.23	-100.2
44	12	-6177	-40	417	0	-22	408	6.28	6.28	9.42	9.42	-6.80	-82.6
45	12	-6603	148	135	0	35	-39	6.28	6.28	9.42	9.42	-3.53	-51.8
46	12	-6545	123	346	0	-17	-32	6.28	6.28	9.42	9.42	-3.44	-50.3
47	12	-6416	107	300	0	-9	-29	6.28	6.28	9.42	9.42	-3.35	-48.9
49	12	-6585	154	328	0	-16	-120	6.28	6.28	9.42	9.42	-4.26	-58.4
50	12	-6304	69	300	0	-8	60	6.28	6.28	9.42	9.42	-3.58	-50.9
51	12	-6389	107	244	0	4	-29	6.28	6.28	9.42	9.42	-3.34	-48.7

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	25	-7508	330	613	0	-147	-275	6.28	6.28	9.42	9.42	-6.13	-79.3
41	25	-7004	189	530	0	-116	-21	6.28	6.28	9.42	9.42	-4.05	-59.4
42	25	-6924	189	362	0	-57	-22	6.28	6.28	9.42	9.42	-3.74	-55.5
43	25	-7522	383	552	0	-132	-442	6.28	6.28	9.42	9.42	-7.70	-95.0
44	25	-6120	-40	417	0	-74	403	6.28	6.28	9.42	9.42	-6.73	-81.7
45	25	-6546	148	135	0	18	-21	6.28	6.28	9.42	9.42	-3.37	-50.4
46	25	-6488	123	346	0	-60	-17	6.28	6.28	9.42	9.42	-3.54	-52.4
47	25	-6360	107	300	0	-47	-16	6.28	6.28	9.42	9.42	-3.41	-50.6
49	25	-6528	154	328	0	-57	-100	6.28	6.28	9.42	9.42	-4.06	-56.2
50	25	-6248	69	300	0	-45	69	6.28	6.28	9.42	9.42	-3.63	-51.3
51	25	-6332	107	244	0	-27	-16	6.28	6.28	9.42	9.42	-3.31	-49.3

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	38	-7452	330	613	0	-223	-234	6.28	6.28	9.42	9.42	-5.73	-75.1
41	38	-6948	189	530	0	-182	3	6.28	6.28	9.42	9.42	-4.33	-62.8
42	38	-6867	189	362	0	-102	1	6.28	6.28	9.42	9.42	-3.92	-57.6
43	38	-7466	383	552	0	-202	-394	6.28	6.28	9.42	9.42	-7.21	-90.0
44	38	-6064	-40	417	0	-126	398	6.28	6.28	9.42	9.42	-6.65	-80.8
45	38	-6490	148	135	0	1	-2	6.28	6.28	9.42	9.42	-3.27	-49.0
46	38	-6432	123	346	0	-104	-1	6.28	6.28	9.42	9.42	-3.71	-54.4
47	38	-6303	107	300	0	-84	-2	6.28	6.28	9.42	9.42	-3.55	-52.3
49	38	-6472	154	328	0	-98	-81	6.28	6.28	9.42	9.42	-3.85	-54.4
50	38	-6191	69	300	0	-83	77	6.28	6.28	9.42	9.42	-3.68	-51.7
51	38	-6276	107	244	0	-57	-3	6.28	6.28	9.42	9.42	-3.42	-50.6

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	50	-7396	330	613	0	-300	-192	6.28	6.28	9.42	9.42	-5.32	-72.9
41	50	-6892	189	530	0	-248	27	6.28	6.28	9.42	9.42	-4.60	-66.2
42	50	-6811	189	362	0	-147	25	6.28	6.28	9.42	9.42	-4.10	-59.8
43	50	-7410	383	552	0	-271	-346	6.28	6.28	9.42	9.42	-6.74	-85.2
44	50	-6008	-40	417	0	-178	394	6.28	6.28	9.42	9.42	-6.58	-80.0
45	50	-6434	148	135	0	-16	16	6.28	6.28	9.42	9.42	-3.31	-49.5
46	50	-6376	123	346	0	-147	14	6.28	6.28	9.42	9.42	-3.88	-56.5
47	50	-6247	107	300	0	-122	11	6.28	6.28	9.42	9.42	-3.70	-54.1
49	50	-6416	154	328	0	-139	-62	6.28	6.28	9.42	9.42	-3.86	-56.3
50	50	-6135	69	300	0	-120	86	6.28	6.28	9.42	9.42	-3.74	-53.1
51	50	-6220	107	244	0	-88	11	6.28	6.28	9.42	9.42	-3.53	-51.9

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 121 NI 827 NF 263 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 25A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	--												
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-10830	-273	1319	0	-300	-190	6.28	6.28	9.42	9.42	-6.95	-98.8
41	0	-9977	105	1077	0	-248	11	6.28	6.28	9.42	9.42	-6.15	-89.4
42	0	-9844	102	595	0	-147	10	6.28	6.28	9.42	9.42	-5.62	-82.6
43	0	-10920	-548	1204	0	-271	-329	6.28	6.28	9.42	9.42	-8.26	-108.9
44	0	-8502	739	740	0	-178	349	6.28	6.28	9.42	9.42	-7.29	-93.3
45	0	-9285	77	-2	0	-16	6	6.28	6.28	9.42	9.42	-4.74	-71.0
46	0	-9224	68	635	0	-147	6	6.28	6.28	9.42	9.42	-5.31	-78.0
47	0	-9035	59	525	0	-122	4	6.28	6.28	9.42	9.42	-5.10	-75.1
49	0	-9318	-67	606	0	-139	-63	6.28	6.28	9.42	9.42	-5.32	-78.2
50	0	-8834	190	513	0	-120	72	6.28	6.28	9.42	9.42	-4.99	-73.5
51	0	-8991	58	364	0	-88	4	6.28	6.28	9.42	9.42	-4.92	-72.8

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	12	-10772	-273	1319	0	-465	-225	6.28	6.28	9.42	9.42	-7.54	-107.8
41	12	-9921	105	1077	0	-383	25	6.28	6.28	9.42	9.42	-6.74	-96.7
42	12	-9788	102	595	0	-222	23	6.28	6.28	9.42	9.42	-5.93	-86.5
43	12	-10862	-548	1204	0	-421	-397	6.28	6.28	9.42	9.42	-8.87	-114.7
44	12	-8446	739	740	0	-270	441	6.28	6.28	9.42	9.42	-8.11	-101.4
45	12	-9229	77	-2	0	-16	15	6.28	6.28	9.42	9.42	-4.71	-70.5
46	12	-9168	68	635	0	-226	14	6.28	6.28	9.42	9.42	-5.64	-82.1
47	12	-8979	59	525	0	-187	12	6.28	6.28	9.42	9.42	-5.37	-78.4
49	12	-9262	-67	606	0	-214	-71	6.28	6.28	9.42	9.42	-5.64	-82.1
50	12	-8778	190	513	0	-184	96	6.28	6.28	9.42	9.42	-5.25	-76.7
51	12	-8935	58	364	0	-133	11	6.28	6.28	9.42	9.42	-5.10	-75.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	25	-10715	-273	1319	0	-630	-259	6.28	6.28	9.42	9.42	-8.26	-116.7
41	25	-9864	105	1077	0	-518	38	6.28	6.28	9.42	9.42	-7.32	-103.9
42	25	-9732	102	595	0	-296	36	6.28	6.28	9.42	9.42	-6.24	-90.3
43	25	-10805	-548	1204	0	-572	-466	6.28	6.28	9.42	9.42	-9.47	-120.6
44	25	-8390	739	740	0	-363	534	6.28	6.28	9.42	9.42	-9.01	-110.0
45	25	-9172	77	-2	0	-16	25	6.28	6.28	9.42	9.42	-4.68	-70.1
46	25	-9112	68	635	0	-306	23	6.28	6.28	9.42	9.42	-5.98	-86.2
47	25	-8922	59	525	0	-253	19	6.28	6.28	9.42	9.42	-5.64	-81.7
49	25	-9206	-67	606	0	-290	-80	6.28	6.28	9.42	9.42	-5.95	-86.0
50	25	-8722	190	513	0	-248	120	6.28	6.28	9.42	9.42	-5.52	-80.0
51	25	-8878	58	364	0	-179	18	6.28	6.28	9.42	9.42	-5.28	-77.2

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	38	-10658	-273	1319	0	-794	-293	6.28	6.28	9.42	9.42	-8.98	-125.7
41	38	-9808	105	1077	0	-652	51	6.28	6.28	9.42	9.42	-7.91	-111.2
42	38	-9675	102	595	0	-370	48	6.28	6.28	9.42	9.42	-6.55	-94.1
43	38	-10748	-548	1204	0	-722	-534	6.28	6.28	9.42	9.42	-10.07	-126.5
44	38	-8333	739	740	0	-455	626	6.28	6.28	9.42	9.42	-10.08	-119.7
45	38	-9116	77	-2	0	-15	34	6.28	6.28	9.42	9.42	-4.69	-69.6
46	38	-9055	68	635	0	-385	31	6.28	6.28	9.42	9.42	-6.31	-90.3
47	38	-8866	59	525	0	-318	26	6.28	6.28	9.42	9.42	-5.91	-85.0
49	38	-9149	-67	606	0	-366	-88	6.28	6.28	9.42	9.42	-6.27	-89.9
50	38	-8665	190	513	0	-312	144	6.28	6.28	9.42	9.42	-5.78	-83.2
51	38	-8822	58	364	0	-224	26	6.28	6.28	9.42	9.42	-5.46	-79.3

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	50	-10600	-273	1319	0	-959	-327	6.28	6.28	9.42	9.42	-9.71	-134.6
41	50	-9752	105	1077	0	-787	64	6.28	6.28	9.42	9.42	-8.49	-118.4
42	50	-9619	102	595	0	-445	61	6.28	6.28	9.42	9.42	-6.87	-97.9
43	50	-10690	-548	1204	0	-872	-603	6.28	6.28	9.42	9.42	-10.68	-132.5
44	50	-8277	739	740	0	-548	719	6.28	6.28	9.42	9.42	-11.29	-130.1
45	50	-9060	77	-2	0	-15	44	6.28	6.28	9.42	9.42	-4.75	-69.3
46	50	-8999	68	635	0	-465	40	6.28	6.28	9.42	9.42	-6.64	-94.4
47	50	-8810	59	525	0	-384	34	6.28	6.28	9.42	9.42	-6.18	-88.4
49	50	-9093	-67	606	0	-442	-97	6.28	6.28	9.42	9.42	-6.59	-93.8
50	50	-8609	190	513	0	-377	168	6.28	6.28	9.42	9.42	-6.05	-86.4
51	50	-8766	58	364	0	-270	33	6.28	6.28	9.42	9.42	-5.64	-81.5

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 122 NI 805 NF 830 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 24
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm		daN			daN*m				cm^2			daN/cm^2
40	0	-3499	-21	597	0	-89	-33	6.28	6.28	9.42	9.42	-2.16	-31.5
41	0	-3458	24	493	0	-72	20	6.28	6.28	9.42	9.42	-2.07	-30.2
42	0	-3445	24	268	0	-47	21	6.28	6.28	9.42	9.42	-1.95	-28.7
43	0	-3417	-53	560	0	-89	-72	6.28	6.28	9.42	9.42	-2.31	-31.3
44	0	-3309	99	340	0	-46	111	6.28	6.28	9.42	9.42	-2.60	-34.0
45	0	-3327	22	12	0	-20	18	6.28	6.28	9.42	9.42	-1.77	-26.2
46	0	-3284	20	322	0	-56	15	6.28	6.28	9.42	9.42	-1.91	-28.0
47	0	-3240	19	279	0	-52	14	6.28	6.28	9.42	9.42	-1.87	-27.4
49	0	-3254	4	314	0	-57	-4	6.28	6.28	9.42	9.42	-1.90	-27.8
50	0	-3232	34	270	0	-49	33	6.28	6.28	9.42	9.42	-1.85	-27.2
51	0	-3236	19	204	0	-43	14	6.28	6.28	9.42	9.42	-1.83	-26.9

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	12	-3443	-21	597	0	-163	-36	6.28	6.28	9.42	9.42	-2.48	-35.3
41	12	-3402	24	493	0	-134	23	6.28	6.28	9.42	9.42	-2.32	-33.3
42	12	-3389	24	268	0	-81	24	6.28	6.28	9.42	9.42	-2.07	-30.2
43	12	-3361	-53	560	0	-159	-79	6.28	6.28	9.42	9.42	-2.42	-34.4
44	12	-3253	99	340	0	-89	123	6.28	6.28	9.42	9.42	-2.69	-34.7
45	12	-3271	22	12	0	-22	20	6.28	6.28	9.42	9.42	-1.76	-25.9
46	12	-3228	20	322	0	-96	18	6.28	6.28	9.42	9.42	-2.06	-29.8
47	12	-3184	19	279	0	-87	16	6.28	6.28	9.42	9.42	-2.00	-29.0
49	12	-3198	4	314	0	-96	-3	6.28	6.28	9.42	9.42	-2.05	-29.6
50	12	-3176	34	270	0	-82	37	6.28	6.28	9.42	9.42	-1.97	-28.7
51	12	-3180	19	204	0	-69	17	6.28	6.28	9.42	9.42	-1.91	-27.9

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	25	-3386	-21	597	0	-238	-39	6.28	6.28	9.42	9.42	-2.79	-39.1
41	25	-3346	24	493	0	-196	26	6.28	6.28	9.42	9.42	-2.57	-36.4
42	25	-3332	24	268	0	-114	27	6.28	6.28	9.42	9.42	-2.20	-31.7
43	25	-3304	-53	560	0	-229	-86	6.28	6.28	9.42	9.42	-2.71	-38.0
44	25	-3196	99	340	0	-131	135	6.28	6.28	9.42	9.42	-2.78	-35.5
45	25	-3214	22	12	0	-23	23	6.28	6.28	9.42	9.42	-1.76	-25.6
46	25	-3172	20	322	0	-136	20	6.28	6.28	9.42	9.42	-2.22	-31.7
47	25	-3128	19	279	0	-122	19	6.28	6.28	9.42	9.42	-2.13	-30.5
49	25	-3142	4	314	0	-136	-3	6.28	6.28	9.42	9.42	-2.20	-31.4
50	25	-3120	34	270	0	-116	41	6.28	6.28	9.42	9.42	-2.10	-30.1
51	25	-3124	19	204	0	-94	19	6.28	6.28	9.42	9.42	-2.00	-28.9

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	38	-3330	-21	597	0	-313	-41	6.28	6.28	9.42	9.42	-3.10	-43.0
41	38	-3289	24	493	0	-257	29	6.28	6.28	9.42	9.42	-2.83	-39.5
42	38	-3276	24	268	0	-148	30	6.28	6.28	9.42	9.42	-2.32	-33.1
43	38	-3248	-53	560	0	-299	-92	6.28	6.28	9.42	9.42	-3.00	-41.6
44	38	-3140	99	340	0	-174	148	6.28	6.28	9.42	9.42	-2.86	-36.2
45	38	-3158	22	12	0	-25	26	6.28	6.28	9.42	9.42	-1.75	-25.2
46	38	-3115	20	322	0	-177	23	6.28	6.28	9.42	9.42	-2.37	-33.6
47	38	-3071	19	279	0	-156	21	6.28	6.28	9.42	9.42	-2.26	-32.1
49	38	-3085	4	314	0	-175	-2	6.28	6.28	9.42	9.42	-2.35	-33.2
50	38	-3063	34	270	0	-150	46	6.28	6.28	9.42	9.42	-2.22	-31.6
51	38	-3067	19	204	0	-120	21	6.28	6.28	9.42	9.42	-2.09	-30.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	50	-3274	-21	597	0	-387	-44	6.28	6.28	9.42	9.42	-3.42	-46.8
41	50	-3233	24	493	0	-319	32	6.28	6.28	9.42	9.42	-3.08	-42.6
42	50	-3220	24	268	0	-181	33	6.28	6.28	9.42	9.42	-2.45	-34.6
43	50	-3192	-53	560	0	-369	-99	6.28	6.28	9.42	9.42	-3.29	-45.2
44	50	-3084	99	340	0	-216	160	6.28	6.28	9.42	9.42	-2.95	-36.9
45	50	-3102	22	12	0	-26	28	6.28	6.28	9.42	9.42	-1.75	-25.0
46	50	-3059	20	322	0	-217	25	6.28	6.28	9.42	9.42	-2.53	-35.4
47	50	-3015	19	279	0	-191	23	6.28	6.28	9.42	9.42	-2.39	-33.7
49	50	-3029	4	314	0	-214	-2	6.28	6.28	9.42	9.42	-2.50	-35.1
50	50	-3007	34	270	0	-184	50	6.28	6.28	9.42	9.42	-2.35	-33.1
51	50	-3011	19	204	0	-146	24	6.28	6.28	9.42	9.42	-2.18	-31.0

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 123 NI 830 NF 122 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 24A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-5139	-81	1702	0	-387	-36	6.28	6.28	9.42	9.42	-4.35	-60.9
41	0	-5099	86	1400	0	-319	28	6.28	6.28	9.42	9.42	-4.02	-56.6
42	0	-5084	86	813	0	-181	29	6.28	6.28	9.42	9.42	-3.38	-48.7
43	0	-4998	-202	1634	0	-369	-83	6.28	6.28	9.42	9.42	-4.20	-58.8
44	0	-4898	365	945	0	-216	137	6.28	6.28	9.42	9.42	-3.61	-49.3
45	0	-4907	76	153	0	-26	25	6.28	6.28	9.42	9.42	-2.59	-38.5
46	0	-4832	69	970	0	-217	22	6.28	6.28	9.42	9.42	-3.42	-48.8
47	0	-4765	65	862	0	-191	21	6.28	6.28	9.42	9.42	-3.27	-46.9
49	0	-4778	10	963	0	-214	-1	6.28	6.28	9.42	9.42	-3.38	-48.3
50	0	-4758	123	825	0	-184	43	6.28	6.28	9.42	9.42	-3.23	-46.4
51	0	-4760	65	667	0	-146	21	6.28	6.28	9.42	9.42	-3.06	-44.2

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	12	-5083	-81	1702	0	-600	-47	6.28	6.28	9.42	9.42	-5.30	-72.6
41	12	-5043	86	1400	0	-494	39	6.28	6.28	9.42	9.42	-4.79	-66.2
42	12	-5028	86	813	0	-283	40	6.28	6.28	9.42	9.42	-3.82	-54.1
43	12	-4942	-202	1634	0	-574	-109	6.28	6.28	9.42	9.42	-5.10	-70.0
44	12	-4842	365	945	0	-335	183	6.28	6.28	9.42	9.42	-4.00	-55.6
45	12	-4851	76	153	0	-45	35	6.28	6.28	9.42	9.42	-2.65	-39.2
46	12	-4776	69	970	0	-338	31	6.28	6.28	9.42	9.42	-3.94	-55.3
47	12	-4709	65	862	0	-299	29	6.28	6.28	9.42	9.42	-3.73	-52.6
49	12	-4722	10	963	0	-335	0	6.28	6.28	9.42	9.42	-3.90	-54.7
50	12	-4702	123	825	0	-287	59	6.28	6.28	9.42	9.42	-3.67	-51.8
51	12	-4704	65	667	0	-229	29	6.28	6.28	9.42	9.42	-3.41	-48.5

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	25	-5026	-81	1702	0	-813	-57	6.28	6.28	9.42	9.42	-6.46	-86.6
41	25	-4986	86	1400	0	-669	50	6.28	6.28	9.42	9.42	-5.61	-76.3
42	25	-4972	86	813	0	-385	50	6.28	6.28	9.42	9.42	-4.25	-59.4
43	25	-4886	-202	1634	0	-778	-134	6.28	6.28	9.42	9.42	-6.20	-83.3
44	25	-4786	365	945	0	-453	228	6.28	6.28	9.42	9.42	-4.47	-61.9
45	25	-4794	76	153	0	-64	44	6.28	6.28	9.42	9.42	-2.71	-39.8
46	25	-4720	69	970	0	-459	40	6.28	6.28	9.42	9.42	-4.47	-61.8
47	25	-4652	65	862	0	-407	37	6.28	6.28	9.42	9.42	-4.20	-58.3
49	25	-4666	10	963	0	-455	2	6.28	6.28	9.42	9.42	-4.42	-61.1
50	25	-4646	123	825	0	-390	74	6.28	6.28	9.42	9.42	-4.11	-57.3
51	25	-4648	65	667	0	-312	37	6.28	6.28	9.42	9.42	-3.76	-52.9

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	38	-4970	-81	1702	0	-1025	-67	6.28	6.28	9.42	9.42	-7.91	-103.4
41	38	-4930	86	1400	0	-844	61	6.28	6.28	9.42	9.42	-6.63	-88.5
42	38	-4915	86	813	0	-486	61	6.28	6.28	9.42	9.42	-4.69	-64.8
43	38	-4829	-202	1634	0	-983	-159	6.28	6.28	9.42	9.42	-7.58	-99.3
44	38	-4729	365	945	0	-571	274	6.28	6.28	9.42	9.42	-4.99	-68.3
45	38	-4738	76	153	0	-83	54	6.28	6.28	9.42	9.42	-2.77	-40.5
46	38	-4663	69	970	0	-581	48	6.28	6.28	9.42	9.42	-5.01	-68.4
47	38	-4596	65	862	0	-515	45	6.28	6.28	9.42	9.42	-4.66	-64.0
49	38	-4609	10	963	0	-575	3	6.28	6.28	9.42	9.42	-4.96	-67.7
50	38	-4589	123	825	0	-493	89	6.28	6.28	9.42	9.42	-4.56	-62.7
51	38	-4591	65	667	0	-396	45	6.28	6.28	9.42	9.42	-4.11	-57.2

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	50	-4914	-81	1702	0	-1238	-77	6.28	6.28	9.42	9.42	-9.54	-121.5
41	50	-4874	86	1400	0	-1019	71	6.28	6.28	9.42	9.42	-7.85	-102.6
42	50	-4859	86	813	0	-588	72	6.28	6.28	9.42	9.42	-5.13	-70.3
43	50	-4773	-202	1634	0	-1187	-185	6.28	6.28	9.42	9.42	-9.14	-116.7
44	50	-4673	365	945	0	-689	320	6.28	6.28	9.42	9.42	-5.60	-75.7
45	50	-4682	76	153	0	-102	63	6.28	6.28	9.42	9.42	-2.83	-41.2
46	50	-4607	69	970	0	-702	57	6.28	6.28	9.42	9.42	-5.65	-76.2
47	50	-4540	65	862	0	-623	53	6.28	6.28	9.42	9.42	-5.18	-70.3
49	50	-4553	10	963	0	-696	4	6.28	6.28	9.42	9.42	-5.60	-75.5
50	50	-4533	123	825	0	-596	105	6.28	6.28	9.42	9.42	-5.03	-68.6
51	50	-4535	65	667	0	-479	53	6.28	6.28	9.42	9.42	-4.46	-61.5

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 124 NI 806 NF 833 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 23
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-3358	-217	689	0	-233	53	6.28	6.28	9.42	9.42	-2.75	-38.6
41	0	-3215	-153	638	0	-209	32	6.28	6.28	9.42	9.42	-2.57	-36.2
42	0	-3031	-152	475	0	-164	33	6.28	6.28	9.42	9.42	-2.27	-32.2
43	0	-3329	-256	641	0	-228	65	6.28	6.28	9.42	9.42	-2.71	-38.1
44	0	-2930	-44	555	0	-167	-2	6.28	6.28	9.42	9.42	-2.23	-31.6
45	0	-2784	-149	285	0	-112	32	6.28	6.28	9.42	9.42	-1.91	-27.4
46	0	-3015	-148	506	0	-176	30	6.28	6.28	9.42	9.42	-2.32	-32.7
47	0	-2965	-147	474	0	-167	30	6.28	6.28	9.42	9.42	-2.25	-31.9
49	0	-3013	-169	491	0	-175	37	6.28	6.28	9.42	9.42	-2.31	-32.7
50	0	-2933	-126	474	0	-163	23	6.28	6.28	9.42	9.42	-2.22	-31.4
51	0	-2904	-147	419	0	-152	30	6.28	6.28	9.42	9.42	-2.15	-30.6

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	12	-3302	-217	689	0	-320	26	6.28	6.28	9.42	9.42	-3.12	-43.1
41	12	-3159	-153	638	0	-289	13	6.28	6.28	9.42	9.42	-2.91	-40.3
42	12	-2975	-152	475	0	-223	14	6.28	6.28	9.42	9.42	-2.51	-35.2
43	12	-3273	-256	641	0	-308	33	6.28	6.28	9.42	9.42	-3.05	-42.3

44	12	-2874	-44	555	0	-236	-7	6.28	6.28	9.42	9.42	-2.52	-35.2
45	12	-2728	-149	285	0	-147	13	6.28	6.28	9.42	9.42	-2.04	-29.0
46	12	-2959	-148	506	0	-239	12	6.28	6.28	9.42	9.42	-2.58	-35.9
47	12	-2909	-147	474	0	-226	11	6.28	6.28	9.42	9.42	-2.49	-34.8
49	12	-2957	-169	491	0	-236	15	6.28	6.28	9.42	9.42	-2.56	-35.8
50	12	-2877	-126	474	0	-222	7	6.28	6.28	9.42	9.42	-2.46	-34.4
51	12	-2848	-147	419	0	-204	12	6.28	6.28	9.42	9.42	-2.36	-33.1

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	25	-3246	-217	689	0	-406	-2	6.28	6.28	9.42	9.42	-3.49	-47.7
41	25	-3102	-153	638	0	-369	-6	6.28	6.28	9.42	9.42	-3.25	-44.5
42	25	-2918	-152	475	0	-282	-5	6.28	6.28	9.42	9.42	-2.76	-38.1
43	25	-3216	-256	641	0	-388	1	6.28	6.28	9.42	9.42	-3.39	-46.5
44	25	-2818	-44	555	0	-306	-13	6.28	6.28	9.42	9.42	-2.81	-38.7
45	25	-2672	-149	285	0	-183	-5	6.28	6.28	9.42	9.42	-2.18	-30.6
46	25	-2902	-148	506	0	-302	-7	6.28	6.28	9.42	9.42	-2.84	-39.1
47	25	-2852	-147	474	0	-286	-7	6.28	6.28	9.42	9.42	-2.74	-37.8
49	25	-2900	-169	491	0	-298	-6	6.28	6.28	9.42	9.42	-2.82	-38.9
50	25	-2820	-126	474	0	-281	-8	6.28	6.28	9.42	9.42	-2.70	-37.3
51	25	-2792	-147	419	0	-257	-7	6.28	6.28	9.42	9.42	-2.57	-35.7

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	38	-3189	-217	689	0	-492	-29	6.28	6.28	9.42	9.42	-3.95	-53.2
41	38	-3046	-153	638	0	-449	-25	6.28	6.28	9.42	9.42	-3.65	-49.3
42	38	-2862	-152	475	0	-342	-24	6.28	6.28	9.42	9.42	-3.00	-41.1
43	38	-3160	-256	641	0	-469	-31	6.28	6.28	9.42	9.42	-3.80	-51.4
44	38	-2761	-44	555	0	-375	-18	6.28	6.28	9.42	9.42	-3.13	-42.5
45	38	-2615	-149	285	0	-219	-24	6.28	6.28	9.42	9.42	-2.31	-32.2
46	38	-2846	-148	506	0	-365	-25	6.28	6.28	9.42	9.42	-3.11	-42.5
47	38	-2796	-147	474	0	-345	-25	6.28	6.28	9.42	9.42	-2.99	-40.8
49	38	-2844	-169	491	0	-359	-27	6.28	6.28	9.42	9.42	-3.08	-42.1
50	38	-2764	-126	474	0	-340	-24	6.28	6.28	9.42	9.42	-2.95	-40.3
51	38	-2735	-147	419	0	-309	-25	6.28	6.28	9.42	9.42	-2.79	-38.3

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	50	-3133	-217	689	0	-578	-56	6.28	6.28	9.42	9.42	-4.50	-59.5
41	50	-2990	-153	638	0	-528	-44	6.28	6.28	9.42	9.42	-4.13	-55.0
42	50	-2806	-152	475	0	-401	-43	6.28	6.28	9.42	9.42	-3.29	-44.6
43	50	-3104	-256	641	0	-549	-63	6.28	6.28	9.42	9.42	-4.29	-57.1
44	50	-2705	-44	555	0	-445	-24	6.28	6.28	9.42	9.42	-3.52	-47.1
45	50	-2559	-149	285	0	-254	-42	6.28	6.28	9.42	9.42	-2.45	-33.8
46	50	-2790	-148	506	0	-429	-44	6.28	6.28	9.42	9.42	-3.45	-46.4
47	50	-2740	-147	474	0	-404	-44	6.28	6.28	9.42	9.42	-3.28	-44.4
49	50	-2788	-169	491	0	-420	-48	6.28	6.28	9.42	9.42	-3.40	-45.8
50	50	-2708	-126	474	0	-400	-40	6.28	6.28	9.42	9.42	-3.25	-43.9
51	50	-2679	-147	419	0	-362	-44	6.28	6.28	9.42	9.42	-3.02	-41.1

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

ASTA NUM. 125 NI 833 NF 209 SEZ. Rp B= 0.600 H= 0.300 (pilastro)
PIL. NUM. 23A
armatura base = 4 X 3.14 per le armature aggiuntive consultare il tabulato

Fessurazione eseguita mediante calcolo indiretto. Se w fessurazione non è rispettata, viene aggiunta armatura e indicata fra le note laterali

NC	x	Fx	[Fy]	[Fz]	[Mx]	My	Mz	APOST	AANT	AINF	ASUP	Sc	Sf
	cm	daN			daN*m			cm^2				daN/cm^2	
40	0	-4201	-42	1041	0	-679	-78	6.28	6.28	9.42	9.42	-5.39	-72.4
41	0	-4041	79	922	0	-612	-57	6.28	6.28	9.42	9.42	-4.94	-66.6
42	0	-3880	64	617	0	-461	-57	6.28	6.28	9.42	9.42	-4.06	-55.6
43	0	-4167	-136	977	0	-649	-91	6.28	6.28	9.42	9.42	-5.20	-70.0
44	0	-3707	280	730	0	-500	-21	6.28	6.28	9.42	9.42	-4.18	-56.8
45	0	-3632	40	272	0	-287	-56	6.28	6.28	9.42	9.42	-3.13	-43.7
46	0	-3815	57	693	0	-493	-55	6.28	6.28	9.42	9.42	-4.19	-57.1
47	0	-3759	52	636	0	-463	-54	6.28	6.28	9.42	9.42	-4.01	-54.9
49	0	-3812	11	676	0	-485	-61	6.28	6.28	9.42	9.42	-4.15	-56.6
50	0	-3721	95	626	0	-455	-48	6.28	6.28	9.42	9.42	-3.96	-54.1
51	0	-3706	46	534	0	-413	-55	6.28	6.28	9.42	9.42	-3.75	-51.5

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	12	-4145	-42	1041	0	-809	-83	6.28	6.28	9.42	9.42	-6.26	-82.4
41	12	-3985	79	922	0	-727	-47	6.28	6.28	9.42	9.42	-5.66	-75.1
42	12	-3824	64	617	0	-539	-49	6.28	6.28	9.42	9.42	-4.44	-60.2
43	12	-4111	-136	977	0	-771	-108	6.28	6.28	9.42	9.42	-5.99	-79.2
44	12	-3651	280	730	0	-591	14	6.28	6.28	9.42	9.42	-4.69	-62.9
45	12	-3576	40	272	0	-321	-52	6.28	6.28	9.42	9.42	-3.26	-45.3
46	12	-3759	57	693	0	-579	-48	6.28	6.28	9.42	9.42	-4.65	-62.7
47	12	-3703	52	636	0	-542	-48	6.28	6.28	9.42	9.42	-4.42	-59.7
49	12	-3756	11	676	0	-570	-60	6.28	6.28	9.42	9.42	-4.59	-62.0
50	12	-3665	95	626	0	-534	-36	6.28	6.28	9.42	9.42	-4.35	-58.9
51	12	-3650	46	534	0	-480	-49	6.28	6.28	9.42	9.42	-4.05	-55.2

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	25	-4088	-42	1041	0	-939	-88	6.28	6.28	9.42	9.42	-7.23	-93.2
41	25	-3928	79	922	0	-842	-37	6.28	6.28	9.42	9.42	-6.49	-84.4
42	25	-3768	64	617	0	-616	-41	6.28	6.28	9.42	9.42	-4.88	-65.4
43	25	-4054	-136	977	0	-894	-125	6.28	6.28	9.42	9.42	-6.88	-89.2
44	25	-3594	280	730	0	-682	49	6.28	6.28	9.42	9.42	-5.29	-69.8
45	25	-3520	40	272	0	-355	-47	6.28	6.28	9.42	9.42	-3.39	-46.8
46	25	-3702	57	693	0	-666	-41	6.28	6.28	9.42	9.42	-5.20	-69.0
47	25	-3646	52	636	0	-622	-42	6.28	6.28	9.42	9.42	-4.89	-65.3
49	25	-3700	11	676	0	-654	-59	6.28	6.28	9.42	9.42	-5.12	-68.0
50	25	-3608	95	626	0	-612	-24	6.28	6.28	9.42	9.42	-4.82	-64.3
51	25	-3594	46	534	0	-546	-43	6.28	6.28	9.42	9.42	-4.40	-59.4

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	38	-4032	-42	1041	0	-1069	-93	6.28	6.28	9.42	9.42	-8.25	-104.3
41	38	-3872	79	922	0	-958	-27	6.28	6.28	9.42	9.42	-7.38	-94.2
42	38	-3711	64	617	0	-693	-33	6.28	6.28	9.42	9.42	-5.38	-71.2
43	38	-3998	-136	977	0	-1016	-142	6.28	6.28	9.42	9.42	-7.83	-99.6
44	38	-3538	280	730	0	-773	84	6.28	6.28	9.42	9.42	-5.95	-77.3

45	38	-3463	40	272	0	-389	-42	6.28	6.28	9.42	9.42	-3.51	-48.3
46	38	-3646	57	693	0	-753	-33	6.28	6.28	9.42	9.42	-5.80	-75.9
47	38	-3590	52	636	0	-701	-35	6.28	6.28	9.42	9.42	-5.43	-71.4
49	38	-3643	11	676	0	-739	-57	6.28	6.28	9.42	9.42	-5.70	-74.7
50	38	-3552	95	626	0	-690	-12	6.28	6.28	9.42	9.42	-5.34	-70.4
51	38	-3537	46	534	0	-613	-37	6.28	6.28	9.42	9.42	-4.81	-64.1

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

40	50	-3976	-42	1041	0	-1199	-99	6.28	6.28	9.42	9.42	-9.29	125.1
41	50	-3816	79	922	0	-1073	-17	6.28	6.28	9.42	9.42	-8.29	-104.0
42	50	-3655	64	617	0	-770	-25	6.28	6.28	9.42	9.42	-5.93	-77.4
43	50	-3942	-136	977	0	-1138	-159	6.28	6.28	9.42	9.42	-8.80	110.9
44	50	-3482	280	730	0	-864	119	6.28	6.28	9.42	9.42	-6.66	-85.0
45	50	-3407	40	272	0	-423	-37	6.28	6.28	9.42	9.42	-3.65	-49.9
46	50	-3590	57	693	0	-839	-26	6.28	6.28	9.42	9.42	-6.46	-83.1
47	50	-3534	52	636	0	-781	-29	6.28	6.28	9.42	9.42	-6.01	-77.9
49	50	-3587	11	676	0	-823	-56	6.28	6.28	9.42	9.42	-6.34	-81.7
50	50	-3496	95	626	0	-768	-0	6.28	6.28	9.42	9.42	-5.92	-76.8
51	50	-3481	46	534	0	-680	-31	6.28	6.28	9.42	9.42	-5.26	-69.3

apost= -- aant= -- ainf= 3.14 asup= 3.14 (e arm. base= 4 X 3.14)

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Lavoro: **D2403a** Intestazione lavoro: **Palestra Campobello**
Elemento: **TRAVE** Gruppo: **4** Tabella: **Tabella travi**
Descrizione: **Travi copertura palestra**
Rck: **350.00** daN/cm^2 fyk: **4580.0** daN/cm^2
Copriferro superiore: **5.0** cm Copriferro inferiore: **5.0** cm Copriferro laterale: **5.0** cm
Verifica in ottemperanza alle NTC2018
Per le combinazioni sismiche la capacità è valutata in campo elastico o sostanzialmente elastico(§7.4.1 NTC2018)

Diametro staffe: **8** mm Numero braccia: **2**

Nome travata: **Trave_401_IP1** Descrizione: **Trave_4 7-12-17-22-32**
ASTA NUM. 1 NI 25 NF 35 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y Permanente qy tot.
qy medio: 375.00 160.00 535.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	7503	1687	174	0	742	-863	4.02	4.02	4.02	4.02	3	0.23	0.05	0.30	0.00	0.00	22.3
2	0	5809	1303	127	0	556	-692	4.02	4.02	4.02	4.02	2	0.19	0.04	0.23	0.00	0.00	22.3
3	0	5876	1299	112	0	461	-677	4.02	4.02	4.02	4.02	2	0.16	0.04	0.23	0.00	0.00	22.3
4	0	5667	1297	156	0	680	-651	4.02	4.02	4.02	4.02	2	0.23	0.04	0.23	0.00	0.00	22.3
5	0	5735	1293	142	0	585	-635	4.02	4.02	4.02	4.02	2	0.20	0.04	0.23	0.00	0.00	22.3
6	0	5680	1306	154	0	711	-695	4.02	4.02	4.02	4.02	2	0.24	0.04	0.23	0.00	0.00	22.3
7	0	5906	1292	106	0	393	-644	4.02	4.02	4.02	4.02	2	0.13	0.04	0.23	0.00	0.00	22.3
8	0	5638	1304	162	0	748	-683	4.02	4.02	4.02	4.02	2	0.25	0.04	0.23	0.00	0.00	22.3
9	0	5863	1290	115	0	430	-632	4.02	4.02	4.02	4.02	2	0.15	0.04	0.23	0.00	0.00	22.3
10	0	5809	1303	127	0	556	-692	4.02	4.02	4.02	4.02	2	0.19	0.04	0.23	0.00	0.00	22.3
11	0	5876	1299	112	0	461	-677	4.02	4.02	4.02	4.02	2	0.16	0.04	0.23	0.00	0.00	22.3
12	0	5667	1297	156	0	680	-651	4.02	4.02	4.02	4.02	2	0.23	0.04	0.23	0.00	0.00	22.3
13	0	5735	1293	142	0	585	-635	4.02	4.02	4.02	4.02	2	0.20	0.04	0.23	0.00	0.00	22.3
14	0	5680	1306	154	0	711	-695	4.02	4.02	4.02	4.02	2	0.24	0.04	0.23	0.00	0.00	22.3
15	0	5906	1292	106	0	393	-644	4.02	4.02	4.02	4.02	2	0.13	0.04	0.23	0.00	0.00	22.3
16	0	5638	1304	162	0	748	-683	4.02	4.02	4.02	4.02	2	0.25	0.04	0.23	0.00	0.00	22.3
17	0	5863	1290	115	0	430	-632	4.02	4.02	4.02	4.02	2	0.15	0.04	0.23	0.00	0.00	22.3
18	0	8777	1813	330	0	1386	-1242	4.02	4.02	4.02	4.02	3	0.44	0.05	0.32	0.00	0.00	22.3
19	0	8144	1644	377	0	1613	-688	4.02	4.02	4.02	4.02	3	0.50	0.05	0.29	0.00	0.00	22.3
20	0	8672	1681	571	0	2179	-809	4.02	4.02	4.02	4.02	3	0.69	0.05	0.30	0.00	0.00	22.3
37	0	8701	1854	256	0	1062	-1385	4.02	4.02	4.02	4.02	3	0.34	0.05	0.33	0.00	0.00	22.3
38	0	7646	1571	334	0	1440	-463	4.02	4.02	4.02	4.02	3	0.44	0.05	0.28	0.00	0.00	22.3
39	0	8525	1634	658	0	2384	-663	4.02	4.02	4.02	4.02	3	0.76	0.05	0.29	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	56	7503	1336	174	0	643	-684	4.02	4.02	4.02	4.02	3	0.20	0.04	0.24	0.00	0.00	22.3
2	56	5809	1033	127	0	485	-555	4.02	4.02	4.02	4.02	2	0.16	0.03	0.18	0.00	0.00	22.3
3	56	5876	1029	112	0	398	-540	4.02	4.02	4.02	4.02	2	0.14	0.03	0.18	0.00	0.00	22.3
4	56	5667	1027	156	0	592	526	4.02	4.02	4.02	4.02	2	0.20	0.03	0.18	0.00	0.00	22.3
5	56	5735	1023	142	0	505	537	4.02	4.02	4.02	4.02	2	0.17	0.03	0.18	0.00	0.00	22.3
6	56	5680	1036	154	0	624	-558	4.02	4.02	4.02	4.02	2	0.21	0.03	0.18	0.00	0.00	22.3
7	56	5906	1022	106	0	333	527	4.02	4.02	4.02	4.02	2	0.11	0.03	0.18	0.00	0.00	22.3
8	56	5638	1034	162	0	656	-545	4.02	4.02	4.02	4.02	2	0.22	0.03	0.18	0.00	0.00	22.3
9	56	5863	1020	115	0	365	538	4.02	4.02	4.02	4.02	2	0.12	0.03	0.18	0.00	0.00	22.3
10	56	5809	1033	127	0	485	-555	4.02	4.02	4.02	4.02	2	0.16	0.03	0.18	0.00	0.00	22.3
11	56	5876	1029	112	0	398	-540	4.02	4.02	4.02	4.02	2	0.14	0.03	0.18	0.00	0.00	22.3
12	56	5667	1027	156	0	592	526	4.02	4.02	4.02	4.02	2	0.20	0.03	0.18	0.00	0.00	22.3
13	56	5735	1023	142	0	505	537	4.02	4.02	4.02	4.02	2	0.17	0.03	0.18	0.00	0.00	22.3
14	56	5680	1036	154	0	624	-558	4.02	4.02	4.02	4.02	2	0.21	0.03	0.18	0.00	0.00	22.3
15	56	5906	1022	106	0	333	527	4.02	4.02	4.02	4.02	2	0.11	0.03	0.18	0.00	0.00	22.3
16	56	5638	1034	162	0	656	-545	4.02	4.02	4.02	4.02	2	0.22	0.03	0.18	0.00	0.00	22.3
17	56	5863	1020	115	0	365	538	4.02	4.02	4.02	4.02	2	0.12	0.03	0.18	0.00	0.00	22.3
18	56	8777	1462	330	0	1199	-1057	4.02	4.02	4.02	4.02	3	0.38	0.04	0.26	0.00	0.00	22.3
19	56	8144	1293	377	0	1400	796	4.02	4.02	4.02	4.02	3	0.44	0.04	0.23	0.00	0.00	22.3
20	56	8672	1330	571	0	1856	716	4.02	4.02	4.02	4.02	3	0.59	0.04	0.24	0.00	0.00	22.3
37	56	8701	1503	256	0	917	-1197	4.02	4.02	4.02	4.02	3	0.29	0.04	0.27	0.00	0.00	22.3
38	56	7646	1220	334	0	1252	944	4.02	4.02	4.02	4.02	3	0.39	0.04	0.22	0.00	0.00	22.3
39	56	8525	1283	658	0	2012	811	4.02	4.02	4.02	4.02	3	0.64	0.04	0.23	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	113	7503	976	174	0	545	1140	4.02	4.02	4.02	4.02	3	0.21	0.03	0.17	0.00	0.00	22.3
2	113	5809	756	127	0	413	857	4.02	4.02	4.02	4.02	2	0.16	0.02	0.13	0.00	0.00	22.3
3	113	5876	752	112	0	334	866	4.02	4.02	4.02	4.02	2	0.16	0.02	0.13	0.00	0.00	22.3
4	113	5667	750	156	0	504	889	4.02	4.02	4.02	4.02	2	0.17	0.02	0.13	0.00	0.00	22.3
5	113	5735	746	142	0	425	897	4.02	4.02	4.02	4.02	2	0.16	0.02	0.13	0.00	0.00	22.3
6	113	5680	759	154	0	537	858	4.02	4.02	4.02	4.02	2	0.18	0.02	0.14	0.00	0.00	22.3
7	113	5906	745	106	0	273	887	4.02	4.02	4.02	4.02	2	0.16	0.02	0.13	0.00	0.00	22.3
8	113	5638	757	162	0	565	868	4.02	4.02	4.02	4.02	2	0.19	0.02	0.13	0.00	0.00	22.3
9	113	5863	743	115	0	301	896	4.02	4.02	4.02	4.02	2	0.17	0.02	0.13	0.00	0.00	22.3
10	113	5809	756	127	0	413	857	4.02	4.02	4.02	4.02	2	0.16	0.02	0.13	0.00	0.00	22.3
11	113	5876	752	112	0	334	866	4.02	4.02	4.02	4.02	2	0.16	0.02	0.13	0.00	0.00	22.3
12	113	5667	750	156	0	504	889	4.02	4.02	4.02	4.02	2	0.17	0.02	0.13	0.00	0.00	22.3
13	113	5735	746	142	0	425	897	4.02	4.02	4.02	4.02	2	0.16	0.02	0.13	0.00	0.00	22.3
14	113	5680	759	154	0	537	858	4.02	4.02	4.02	4.02	2	0.18	0.02	0.14	0.00	0.00	22.3
15	113	5906	745	106	0	273	887	4.02	4.02	4.02	4.02	2	0.16	0.02	0.13	0.00	0.00	22.3
16	113	5638	757	162	0	565	868	4.02	4.02	4.02	4.02	2	0.19	0.02	0.13	0.00	0.00	22.3
17	113	5863	743	115	0	301	896	4.02	4.02	4.02	4.02	2	0.17	0.02	0.13	0.00	0.00	22.3
18	113	8777	1102	330	0	1013	967	4.02	4.02	4.02	4.02	3	0.32	0.03	0.20	0.00	0.00	22.3
19	113	8144	933	377	0	1187	1243	4.02	4.02	4.02	4.02	3	0.37	0.03	0.17	0.00	0.00	22.3
20	113	8672	970	571	0	1534	1184	4.02	4.02	4.02	4.02	3	0.49	0.03	0.17	0.00	0.00	22.3
37	113	8701	1143	256	0	773	891	4.02	4.02	4.02	4.02	3	0.25	0.03	0.20	0.00	0.00	22.3
38	113	7646	860	334	0	1063	1351	4.02	4.02	4.02	4.02	3	0.33	0.02	0.15	0.00	0.00	22.3

39	113	8525	923	658	0	1641	1253	4.02	4.02	4.02	4.02	3	0.52	0.03	0.16	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	170	7503	607	174	0	446	1350	4.02	4.02	4.02	4.02	3	0.25	0.02	0.11	0.00	0.00	22.3
2	170	5809	472	127	0	342	1024	4.02	4.02	4.02	4.02	2	0.19	0.01	0.08	0.00	0.00	22.3
3	170	5876	468	112	0	271	1028	4.02	4.02	4.02	4.02	2	0.19	0.01	0.08	0.00	0.00	22.3
4	170	5667	466	156	0	416	1049	4.02	4.02	4.02	4.02	2	0.19	0.01	0.08	0.00	0.00	22.3
5	170	5735	462	142	0	344	1052	4.02	4.02	4.02	4.02	2	0.19	0.01	0.08	0.00	0.00	22.3
6	170	5680	475	154	0	451	1029	4.02	4.02	4.02	4.02	2	0.19	0.01	0.08	0.00	0.00	22.3
7	170	5906	461	106	0	213	1041	4.02	4.02	4.02	4.02	2	0.19	0.01	0.08	0.00	0.00	22.3
8	170	5638	473	162	0	473	1036	4.02	4.02	4.02	4.02	2	0.19	0.01	0.08	0.00	0.00	22.3
9	170	5863	459	115	0	236	1048	4.02	4.02	4.02	4.02	2	0.19	0.01	0.08	0.00	0.00	22.3
10	170	5809	472	127	0	342	1024	4.02	4.02	4.02	4.02	2	0.19	0.01	0.08	0.00	0.00	22.3
11	170	5876	468	112	0	271	1028	4.02	4.02	4.02	4.02	2	0.19	0.01	0.08	0.00	0.00	22.3
12	170	5667	466	156	0	416	1049	4.02	4.02	4.02	4.02	2	0.19	0.01	0.08	0.00	0.00	22.3
13	170	5735	462	142	0	344	1052	4.02	4.02	4.02	4.02	2	0.19	0.01	0.08	0.00	0.00	22.3
14	170	5680	475	154	0	451	1029	4.02	4.02	4.02	4.02	2	0.19	0.01	0.08	0.00	0.00	22.3
15	170	5906	461	106	0	213	1041	4.02	4.02	4.02	4.02	2	0.19	0.01	0.08	0.00	0.00	22.3
16	170	5638	473	162	0	473	1036	4.02	4.02	4.02	4.02	2	0.19	0.01	0.08	0.00	0.00	22.3
17	170	5863	459	115	0	236	1048	4.02	4.02	4.02	4.02	2	0.19	0.01	0.08	0.00	0.00	22.3
18	170	8777	733	330	0	826	1298	4.02	4.02	4.02	4.02	3	0.26	0.02	0.13	0.00	0.00	22.3
19	170	8144	564	377	0	974	1406	4.02	4.02	4.02	4.02	3	0.30	0.02	0.10	0.00	0.00	22.3
20	170	8672	601	571	0	1211	1387	4.02	4.02	4.02	4.02	3	0.39	0.02	0.11	0.00	0.00	22.3
37	170	8701	774	256	0	628	1246	4.02	4.02	4.02	4.02	3	0.24	0.02	0.14	0.00	0.00	22.3
38	170	7646	491	334	0	875	1469	4.02	4.02	4.02	4.02	3	0.27	0.01	0.09	0.00	0.00	22.3
39	170	8525	554	658	0	1269	1410	4.02	4.02	4.02	4.02	3	0.40	0.02	0.11	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	226	7503	228	174	0	348	1350	4.02	4.02	4.02	4.02	3	0.25	0.01	0.04	0.00	0.00	22.3
2	226	5809	181	127	0	270	1024	4.02	4.02	4.02	4.02	2	0.19	0.01	0.03	0.00	0.00	22.3
3	226	5876	177	112	0	207	1028	4.02	4.02	4.02	4.02	2	0.19	0.01	0.03	0.00	0.00	22.3
4	226	5667	175	156	0	327	1049	4.02	4.02	4.02	4.02	2	0.19	0.01	0.03	0.00	0.00	22.3
5	226	5735	171	142	0	264	1052	4.02	4.02	4.02	4.02	2	0.19	0.00	0.03	0.00	0.00	22.3
6	226	5680	184	154	0	364	1029	4.02	4.02	4.02	4.02	2	0.19	0.01	0.03	0.00	0.00	22.3
7	226	5906	170	106	0	154	1041	4.02	4.02	4.02	4.02	2	0.19	0.00	0.03	0.00	0.00	22.3
8	226	5638	182	162	0	381	1036	4.02	4.02	4.02	4.02	2	0.19	0.01	0.03	0.00	0.00	22.3
9	226	5863	168	115	0	171	1048	4.02	4.02	4.02	4.02	2	0.19	0.00	0.03	0.00	0.00	22.3
10	226	5809	181	127	0	270	1024	4.02	4.02	4.02	4.02	2	0.19	0.01	0.03	0.00	0.00	22.3
11	226	5876	177	112	0	207	1028	4.02	4.02	4.02	4.02	2	0.19	0.01	0.03	0.00	0.00	22.3
12	226	5667	175	156	0	327	1049	4.02	4.02	4.02	4.02	2	0.19	0.01	0.03	0.00	0.00	22.3
13	226	5735	171	142	0	264	1052	4.02	4.02	4.02	4.02	2	0.19	0.00	0.03	0.00	0.00	22.3
14	226	5680	184	154	0	364	1029	4.02	4.02	4.02	4.02	2	0.19	0.01	0.03	0.00	0.00	22.3
15	226	5906	170	106	0	154	1041	4.02	4.02	4.02	4.02	2	0.19	0.00	0.03	0.00	0.00	22.3
16	226	5638	182	162	0	381	1036	4.02	4.02	4.02	4.02	2	0.19	0.01	0.03	0.00	0.00	22.3
17	226	5863	168	115	0	171	1048	4.02	4.02	4.02	4.02	2	0.19	0.00	0.03	0.00	0.00	22.3
18	226	8777	354	330	0	640	1326	4.02	4.02	4.02	4.02	3	0.26	0.01	0.06	0.00	0.00	22.3
19	226	8144	185	377	0	761	1406	4.02	4.02	4.02	4.02	3	0.26	0.01	0.06	0.00	0.00	22.3
20	226	8672	222	571	0	888	1387	4.02	4.02	4.02	4.02	3	0.28	0.02	0.09	0.00	0.00	22.3
37	226	8701	395	256	0	484	1299	4.02	4.02	4.02	4.02	3	0.25	0.01	0.07	0.00	0.00	22.3
38	226	7646	112	334	0	686	1469	4.02	4.02	4.02	4.02	3	0.27	0.01	0.05	0.00	0.00	22.3
39	226	8525	175	658	0	898	1410	4.02	4.02	4.02	4.02	3	0.28	0.02	0.11	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	282	7503	-160	174	0	249	1350	4.02	4.02	4.02	4.02	3	0.25	0.01	0.03	0.00	0.00	22.3
2	282	5809	-118	127	0	199	1024	4.02	4.02	4.02	4.02	2	0.19	0.00	0.02	0.00	0.00	22.3
3	282	5876	-122	112	0	144	1028	4.02	4.02	4.02	4.02	2	0.19	0.00	0.02	0.00	0.00	22.3
4	282	5667	-124	156	0	239	1049	4.02	4.02	4.02	4.02	2	0.19	0.00	0.03	0.00	0.00	22.3
5	282	5735	-128	142	0	184	1052	4.02	4.02	4.02	4.02	2	0.19	0.00	0.02	0.00	0.00	22.3
6	282	5680	-115	154	0	277	1029	4.02	4.02	4.02	4.02	2	0.19	0.00	0.02	0.00	0.00	22.3
7	282	5906	-129	106	0	94	1041	4.02	4.02	4.02	4.02	2	0.19	0.00	0.02	0.00	0.00	22.3
8	282	5638	-117	162	0	289	1036	4.02	4.02	4.02	4.02	2	0.19	0.01	0.03	0.00	0.00	22.3
9	282	5863	-131	115	0	106	1048	4.02	4.02	4.02	4.02	2	0.19	0.00	0.02	0.00	0.00	22.3
10	282	5809	-118	127	0	199	1024	4.02	4.02	4.02	4.02	2	0.19	0.00	0.02	0.00	0.00	22.3
11	282	5876	-122	112	0	144	1028	4.02	4.02	4.02	4.02	2	0.19	0.00	0.02	0.00	0.00	22.3
12	282	5667	-124	156	0	239	1049	4.02	4.02	4.02	4.02	2	0.19	0.00	0.03	0.00	0.00	22.3
13	282	5735	-128	142	0	184	1052	4.02	4.02	4.02	4.02	2	0.19	0.00	0.02	0.00	0.00	22.3
14	282	5680	-115	154	0	277	1029	4.02	4.02	4.02	4.02	2	0.19	0.00	0.02	0.00	0.00	22.3
15	282	5906	-129	106	0	94	1041	4.02	4.02	4.02	4.02	2	0.19	0.00	0.02	0.00	0.00	22.3
16	282	5638	-117	162	0	289	1036	4.02	4.02	4.02	4.02	2	0.19	0.01	0.03	0.00	0.00	22.3
17	282	5863	-131	115	0	106	1048	4.02	4.02	4.02	4.02	2	0.19	0.00	0.02	0.00	0.00	22.3
18	282	8777	-34	330	0	453	1326	4.02	4.02	4.02	4.02	3	0.26	0.01	0.05	0.00	0.00	22.3
19	282	8144	-203	377	0	548	1406	4.02	4.02	4.02	4.02	3	0.26	0.01	0.06	0.00	0.00	22.3
20	282	8672	-166	571	0	566	1387	4.02	4.02	4.02	4.02	3	0.27	0.02	0.09	0.00	0.00	22.3
37	282	8701	7	256	0	339	1299	4.02	4.02	4.02	4.02	3	0.25	0.01	0.04	0.00	0.00	22.3
38	282	7646	-276	334	0	498	1469	4.02	4.02	4.02	4.02	3	0.27	0.01	0.05	0.00	0.00	22.3
39	282	8525	-213	658	0	526	1410	4.02	4.02	4.02	4.02	3	0.27	0.02	0.11	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	339	7503	-558	174	0	150	1350	4.02	4.02	4.02	4.02	3	0.25	0.02	0.10	0.00	0.00	22.3
2	339	5809	-424	127	0	127	1024	4.02	4.02	4.02	4.02	2	0.19	0.01	0.08	0.00	0.00	22.3
3	339	5876	-428	112	0	80	1028	4.02	4.02	4.02	4.02	2	0.19	0.01	0.08	0.00	0.00	22.3
4	339	5667	-430	156	0	151	1049	4.02	4.02	4.02	4.02	2	0.19	0.01	0.08	0.00	0.00	22.3
5	339	5735	-434	142	0	104	1052	4.02	4.02	4.02	4.02	2	0.19	0.01	0.08	0.00	0.00	22.3
6	339	5680	-421	154	0	190	1029	4.02	4.02	4.02	4.02	2	0.19	0.01	0.07	0.00	0.00	22.3
7	339	5906	-435	106	0	34	1041	4.02	4.02	4.02	4.02	2	0.19	0.01	0.08	0.00	0.00	22.3
8	339	5638	-423	162	0	198	1036	4.02	4.02	4.02	4.02	2	0.19	0.01	0.08	0.00	0.00	22.3
9	339	5863	-437	115	0	41	1048	4.02	4.02	4.02	4.02	2	0.19	0.01	0.08	0.00	0.00	22.3
10	339	5809	-424	127	0	127	1024	4.02	4.02	4.02	4.02	2	0.19	0.01	0.08	0.00	0.00	22.3
11	339	5876	-428	112	0	80	1028	4.02	4.02	4.02	4.02	2	0.19	0.01	0.08	0.00	0.00	22.3
12	339	5667	-430	156	0	151	1049	4.02	4.02	4.02	4.02	2	0.19	0.01	0.08	0.00	0.00	22.3
13	339	5735	-434	142	0	104	1052	4.02	4.02	4.02	4.02	2	0.19	0.01	0.08	0.00	0.00	22.3
14	339	5680	-421	154	0	190	1029	4.02	4.02	4.02	4.02	2	0.19	0.01	0.07	0.00	0.00	22.3
15	339	5906	-435	106	0	34	1041	4.02	4.02	4.02	4.02	2	0.19	0.01	0.08	0.00	0.00	22.3
16	339	5638	-423	162	0	198	1036	4.02	4.02	4.02	4.02	2	0.19	0.01	0.08	0.00	0.00	22.3
17	339	5863	-437	115	0	41	1048	4.02	4.02	4.02	4.02	2	0.19	0.01	0.08	0.00	0.00	22.3
18	339	8777	-432	330	0	267	1326	4.02	4.02	4.02	4.02	3	0.26	0.01	0.08	0.00	0.00	22.3
19	339	8144	-601	377	0	335	1406	4.02	4.02	4.02	4.02	3	0.26	0.02	0.11	0.00	0.00	22.3
20	339	8672	-564	571	0	243	1387	4.02	4.02	4.02	4.02	3	0.27	0.02	0.10	0.00	0.00	22.3
37	339	8701	-391	256	0	195	1299	4.02	4.02	4.02	4.02	3	0.25	0.01	0.07	0.00	0.00	22.3
38	339	7646	-674	334	0	309	1469	4.02	4.02	4.02	4.02	3	0.27	0.02	0.12	0.00	0.00	22.3
39	339	8525	-611	658	0	154	1410	4.02	4.02	4.02	4.02	3	0.27	0.02	0.11	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	396	7503	-965	174	0	52	1206	4.02	4.02	4.02	4.02	3	0.22	0.03	0.17	0.00	0.00	22.3
2	396	5809	-737	127	0	56	917	4.02	4.02	4.02	4.02	2	0.17	0.02	0.13	0.00	0.00	22.3

3	396	5876	-741	112	0	17	918	4.02	4.02	4.02	4.02	2	0.17	0.02	0.13	0.00	0.00	22.3
4	396	5667	-743	156	0	63	938	4.02	4.02	4.02	4.02	2	0.17	0.02	0.13	0.00	0.00	22.3
5	396	5735	-747	142	0	24	939	4.02	4.02	4.02	4.02	2	0.17	0.02	0.13	0.00	0.00	22.3
6	396	5680	-734	154	0	104	923	4.02	4.02	4.02	4.02	2	0.17	0.02	0.13	0.00	0.00	22.3
7	396	5906	-748	106	0	-26	926	4.02	4.02	4.02	4.02	2	0.17	0.02	0.13	0.00	0.00	22.3
8	396	5638	-736	162	0	106	929	4.02	4.02	4.02	4.02	2	0.17	0.02	0.13	0.00	0.00	22.3
9	396	5863	-750	115	0	-24	933	4.02	4.02	4.02	4.02	2	0.17	0.02	0.13	0.00	0.00	22.3
10	396	5809	-737	127	0	56	917	4.02	4.02	4.02	4.02	2	0.17	0.02	0.13	0.00	0.00	22.3
11	396	5876	-741	112	0	17	918	4.02	4.02	4.02	4.02	2	0.17	0.02	0.13	0.00	0.00	22.3
12	396	5667	-743	156	0	63	938	4.02	4.02	4.02	4.02	2	0.17	0.02	0.13	0.00	0.00	22.3
13	396	5735	-747	142	0	24	939	4.02	4.02	4.02	4.02	2	0.17	0.02	0.13	0.00	0.00	22.3
14	396	5680	-734	154	0	104	923	4.02	4.02	4.02	4.02	2	0.17	0.02	0.13	0.00	0.00	22.3
15	396	5906	-748	106	0	-26	926	4.02	4.02	4.02	4.02	2	0.17	0.02	0.13	0.00	0.00	22.3
16	396	5638	-736	162	0	106	929	4.02	4.02	4.02	4.02	2	0.17	0.02	0.13	0.00	0.00	22.3
17	396	5863	-750	115	0	-24	933	4.02	4.02	4.02	4.02	2	0.17	0.02	0.13	0.00	0.00	22.3
18	396	8777	-839	330	0	80	1261	4.02	4.02	4.02	4.02	3	0.24	0.02	0.15	0.00	0.00	22.3
19	396	8144	-1008	377	0	122	1230	4.02	4.02	4.02	4.02	3	0.23	0.03	0.18	0.00	0.00	22.3
20	396	8672	-971	571	0	-80	1240	4.02	4.02	4.02	4.02	3	0.24	0.03	0.17	0.00	0.00	22.3
37	396	8701	-798	256	0	50	1259	4.02	4.02	4.02	4.02	3	0.24	0.02	0.14	0.00	0.00	22.3
38	396	7646	-1081	334	0	121	1207	4.02	4.02	4.02	4.02	3	0.22	0.03	0.19	0.00	0.00	22.3
39	396	8525	-1018	658	0	-217	1223	4.02	4.02	4.02	4.02	3	0.23	0.03	0.18	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	452	7503	-1381	174	0	-47	755	4.02	4.02	4.02	4.02	3	0.14	0.04	0.25	0.00	0.00	22.3
2	452	5809	-1058	127	0	-16	573	4.02	4.02	4.02	4.02	2	0.11	0.03	0.19	0.00	0.00	22.3
3	452	5876	-1062	112	0	-47	571	4.02	4.02	4.02	4.02	2	0.11	0.03	0.19	0.00	0.00	22.3
4	452	5667	-1064	156	0	-25	590	4.02	4.02	4.02	4.02	2	0.11	0.03	0.19	0.00	0.00	22.3
5	452	5735	-1068	142	0	-56	588	4.02	4.02	4.02	4.02	2	0.11	0.03	0.19	0.00	0.00	22.3
6	452	5680	-1055	154	0	17	580	4.02	4.02	4.02	4.02	2	0.11	0.03	0.19	0.00	0.00	22.3
7	452	5906	-1069	106	0	-86	576	4.02	4.02	4.02	4.02	2	0.11	0.03	0.19	0.00	0.00	22.3
8	452	5638	-1057	162	0	14	585	4.02	4.02	4.02	4.02	2	0.11	0.03	0.19	0.00	0.00	22.3
9	452	5863	-1071	115	0	-89	581	4.02	4.02	4.02	4.02	2	0.11	0.03	0.19	0.00	0.00	22.3
10	452	5809	-1058	127	0	-16	573	4.02	4.02	4.02	4.02	2	0.11	0.03	0.19	0.00	0.00	22.3
11	452	5876	-1062	112	0	-47	571	4.02	4.02	4.02	4.02	2	0.11	0.03	0.19	0.00	0.00	22.3
12	452	5667	-1064	156	0	-25	590	4.02	4.02	4.02	4.02	2	0.11	0.03	0.19	0.00	0.00	22.3
13	452	5735	-1068	142	0	-56	588	4.02	4.02	4.02	4.02	2	0.11	0.03	0.19	0.00	0.00	22.3
14	452	5680	-1055	154	0	17	580	4.02	4.02	4.02	4.02	2	0.11	0.03	0.19	0.00	0.00	22.3
15	452	5906	-1069	106	0	-86	576	4.02	4.02	4.02	4.02	2	0.11	0.03	0.19	0.00	0.00	22.3
16	452	5638	-1057	162	0	14	585	4.02	4.02	4.02	4.02	2	0.11	0.03	0.19	0.00	0.00	22.3
17	452	5863	-1071	115	0	-89	581	4.02	4.02	4.02	4.02	2	0.11	0.03	0.19	0.00	0.00	22.3
18	452	8777	-1256	330	0	-106	880	4.02	4.02	4.02	4.02	3	0.17	0.04	0.22	0.00	0.00	22.3
19	452	8144	-1425	377	0	-90	753	4.02	4.02	4.02	4.02	3	0.14	0.04	0.25	0.00	0.00	22.3
20	452	8672	-1387	571	0	-403	785	4.02	4.02	4.02	4.02	3	0.15	0.04	0.25	0.00	0.00	22.3
37	452	8701	-1215	256	0	-94	902	4.02	4.02	4.02	4.02	3	0.17	0.04	0.22	0.00	0.00	22.3
38	452	7646	-1497	334	0	-68	-825	4.02	4.02	4.02	4.02	3	0.15	0.04	0.27	0.00	0.00	22.3
39	452	8525	-1434	658	0	-589	742	4.02	4.02	4.02	4.02	3	0.19	0.04	0.26	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	508	7503	-1807	174	0	-145	-1759	4.02	4.02	4.02	4.02	3	0.32	0.05	0.32	0.00	0.00	22.3
2	508	5809	-1385	127	0	-87	-1353	4.02	4.02	4.02	4.02	2	0.25	0.04	0.25	0.00	0.00	22.3
3	508	5876	-1389	112	0	-110	-1361	4.02	4.02	4.02	4.02	2	0.25	0.04	0.25	0.00	0.00	22.3
4	508	5667	-1391	156	0	-113	-1346	4.02	4.02	4.02	4.02	2	0.25	0.04	0.25	0.00	0.00	22.3
5	508	5735	-1395	142	0	-136	-1354	4.02	4.02	4.02	4.02	2	0.25	0.04	0.25	0.00	0.00	22.3
6	508	5680	-1382	154	0	-70	-1341	4.02	4.02	4.02	4.02	2	0.25	0.04	0.25	0.00	0.00	22.3
7	508	5906	-1396	106	0	-146	-1368	4.02	4.02	4.02	4.02	2	0.25	0.04	0.25	0.00	0.00	22.3
8	508	5638	-1384	162	0	-78	-1339	4.02	4.02	4.02	4.02	2	0.25	0.04	0.25	0.00	0.00	22.3
9	508	5863	-1398	115	0	-154	-1366	4.02	4.02	4.02	4.02	2	0.25	0.04	0.25	0.00	0.00	22.3
10	508	5809	-1385	127	0	-87	-1353	4.02	4.02	4.02	4.02	2	0.25	0.04	0.25	0.00	0.00	22.3
11	508	5876	-1389	112	0	-110	-1361	4.02	4.02	4.02	4.02	2	0.25	0.04	0.25	0.00	0.00	22.3
12	508	5667	-1391	156	0	-113	-1346	4.02	4.02	4.02	4.02	2	0.25	0.04	0.25	0.00	0.00	22.3
13	508	5735	-1395	142	0	-136	-1354	4.02	4.02	4.02	4.02	2	0.25	0.04	0.25	0.00	0.00	22.3
14	508	5680	-1382	154	0	-70	-1341	4.02	4.02	4.02	4.02	2	0.25	0.04	0.25	0.00	0.00	22.3
15	508	5906	-1396	106	0	-146	-1368	4.02	4.02	4.02	4.02	2	0.25	0.04	0.25	0.00	0.00	22.3
16	508	5638	-1384	162	0	-78	-1339	4.02	4.02	4.02	4.02	2	0.25	0.04	0.25	0.00	0.00	22.3
17	508	5863	-1398	115	0	-154	-1366	4.02	4.02	4.02	4.02	2	0.25	0.04	0.25	0.00	0.00	22.3
18	508	8777	-1682	330	0	-293	-1436	4.02	4.02	4.02	4.02	3	0.28	0.05	0.30	0.00	0.00	22.3
19	508	8144	-1851	377	0	-303	-1830	4.02	4.02	4.02	4.02	3	0.34	0.05	0.33	0.00	0.00	22.3
20	508	8672	-1813	571	0	-725	-1739	4.02	4.02	4.02	4.02	3	0.33	0.05	0.32	0.00	0.00	22.3
37	508	8701	-1641	256	0	-239	-1349	4.02	4.02	4.02	4.02	3	0.26	0.05	0.29	0.00	0.00	22.3
38	508	7646	-1923	334	0	-256	-2007	4.02	4.02	4.02	4.02	3	0.37	0.06	0.34	0.00	0.00	22.3
39	508	8525	-1860	658	0	-960	-1856	4.02	4.02	4.02	4.02	3	0.35	0.05	0.33	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	565	7503	-2242	174	0	-244	-1988	4.02	4.02	4.02	4.02	3	0.37	0.07	0.40	0.00	0.00	22.3
2	565	5809	-1720	127	0	-159	-1529	4.02	4.02	4.02	4.02	2	0.28	0.05	0.31	0.00	0.00	22.3
3	565	5876	-1724	112	0	-174	-1537	4.02	4.02	4.02	4.02	2	0.28	0.05	0.31	0.00	0.00	22.3
4	565	5667	-1726	156	0	-201	-1522	4.02	4.02	4.02	4.02	2	0.28	0.05	0.31	0.00	0.00	22.3
5	565	5735	-1730	142	0	-216	-1530	4.02	4.02	4.02	4.02	2	0.28	0.05	0.31	0.00	0.00	22.3
6	565	5680	-1717	154	0	-157	-1517	4.02	4.02	4.02	4.02	2	0.28	0.05	0.31	0.00	0.00	22.3
7	565	5906	-1731	106	0	-206	-1544	4.02	4.02	4.02	4.02	2	0.29	0.05	0.31	0.00	0.00	22.3
8	565	5638	-1719	162	0	-169	-1515	4.02	4.02	4.02	4.02	2	0.28	0.05	0.31	0.00	0.00	22.3
9	565	5863	-1733	115	0	-219	-1542	4.02	4.02	4.02	4.02	2	0.28	0.05	0.31	0.00	0.00	22.3
10	565	5809	-1720	127	0	-159	-1529	4.02	4.02	4.02	4.02	2	0.28	0.05	0.31	0.00	0.00	22.3
11	565	5876	-1724	112	0	-174	-1537	4.02	4.02	4.02	4.02	2	0.28	0.05	0.31	0.00	0.00	22.3
12	565	5667	-1726	156	0	-201	-1522	4.02	4.02	4.02	4.02	2	0.28	0.05	0.31	0.00	0.00	22.3
13	565	5735	-1730	142	0	-216	-1530	4.02	4.02	4.02	4.02	2	0.28	0.05	0.31	0.00	0.00	22.3
14	565	5680	-1717	154	0	-157	-1517	4.02	4.02	4.02	4.02	2	0.28	0.05	0.31	0.00	0.00	22.3
15	565	5906	-1731	106	0	-206	-1544	4.02	4.02	4.02	4.02	2	0.29	0.05	0.31	0.00	0.00	22.3
16	565	5638	-1719	162	0	-169	-1515	4.02	4.02	4.02	4.02	2	0.28	0.05	0.31	0.00	0.00	22.3
17	565	5863	-1733	115	0	-219	-1542	4.02	4.02	4.02	4.02	2	0.28	0.05	0.31	0.00	0.00	22.3
18	565	8777	-2117	330	0	-479	-1657	4.02	4.02	4.02	4.02	3	0.32	0.06	0.38	0.00	0.00	22.3
19	565	8144	-2286	377	0	-516	-2061	4.02	4.02	4.02	4.02	3	0.39	0.07	0.41	0.00	0.00	22.3
20	565	8672	-2248	571	0	-1048	-1968	4.02	4.02	4.02	4.02	3	0.38	0.07	0.40	0.00	0.00	22.3
37	565	8701	-2076	256	0	-383	-1568	4.02	4.02	4.02	4.02	3	0.30	0.06	0.37	0.00	0.00	22.3
38	565	7646	-2358	334	0	-445	-2242	4.02	4.02	4.02	4.02	3	0.41	0.07	0.42	0.00	0.00	22.3
39	565	8525	-2295	658	0	-1332	-2088	4.02	4.02	4.02	4.02	3	0.42	0.07	0.41	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

Nome travata: **Trave_401_IP1** Descrizione: **Trave_4 7-12-17-22-32**
ASTA NUM. 2 NI 35 NF 37 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y qy tot.
qy medio: 375.00 375.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza			aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx		cmq/m		cm
1	0	6124	1333	-2	0	-87	-1227	4.02	4.02	4.02	4.02	3	0.21	0.04	0.24		0.00	0.00	22.3
2	0	4696	1010	-5	0	-68	-902	4.02	4.02	4.02	4.02	2	0.16	0.03	0.18		0.00	0.00	22.3
3	0	4761	1011	-6	0	-85	-904	4.02	4.02	4.02	4.02	2	0.16	0.03	0.18		0.00	0.00	22.3
4	0	4660	1040	2	0	-49	-983	4.02	4.02	4.02	4.02	2	0.17	0.03	0.19		0.00	0.00	22.3
5	0	4726	1041	2	0	-66	-986	4.02	4.02	4.02	4.02	2	0.17	0.03	0.19		0.00	0.00	22.3
6	0	4607	1020	-2	0	-42	-927	4.02	4.02	4.02	4.02	2	0.16	0.03	0.18		0.00	0.00	22.3
7	0	4825	1022	-4	0	-98	-935	4.02	4.02	4.02	4.02	2	0.17	0.03	0.18		0.00	0.00	22.3
8	0	4596	1029	0	0	-36	-952	4.02	4.02	4.02	4.02	2	0.17	0.03	0.18		0.00	0.00	22.3
9	0	4815	1031	-1	0	-92	-960	4.02	4.02	4.02	4.02	2	0.17	0.03	0.18		0.00	0.00	22.3
10	0	4696	1010	-5	0	-68	-902	4.02	4.02	4.02	4.02	2	0.16	0.03	0.18		0.00	0.00	22.3
11	0	4761	1011	-6	0	-85	-904	4.02	4.02	4.02	4.02	2	0.16	0.03	0.18		0.00	0.00	22.3
12	0	4660	1040	2	0	-49	-983	4.02	4.02	4.02	4.02	2	0.17	0.03	0.19		0.00	0.00	22.3
13	0	4726	1041	2	0	-66	-986	4.02	4.02	4.02	4.02	2	0.17	0.03	0.19		0.00	0.00	22.3
14	0	4607	1020	-2	0	-42	-927	4.02	4.02	4.02	4.02	2	0.16	0.03	0.18		0.00	0.00	22.3
15	0	4825	1022	-4	0	-98	-935	4.02	4.02	4.02	4.02	2	0.17	0.03	0.18		0.00	0.00	22.3
16	0	4596	1029	0	0	-36	-952	4.02	4.02	4.02	4.02	2	0.17	0.03	0.18		0.00	0.00	22.3
17	0	4815	1031	-1	0	-92	-960	4.02	4.02	4.02	4.02	2	0.17	0.03	0.18		0.00	0.00	22.3
18	0	7241	1350	-27	0	-295	-1296	4.02	4.02	4.02	4.02	3	0.24	0.04	0.24		0.00	0.00	22.3
19	0	7140	1361	20	0	-81	-1310	4.02	4.02	4.02	4.02	3	0.24	0.04	0.24		0.00	0.00	22.3
20	0	7325	1350	140	0	-120	-1289	4.02	4.02	4.02	4.02	3	0.24	0.04	0.24		0.00	0.00	22.3
37	0	6940	1337	-43	0	-335	-1262	4.02	4.02	4.02	4.02	3	0.23	0.04	0.24		0.00	0.00	22.3
38	0	6772	1356	35	0	21	-1285	4.02	4.02	4.02	4.02	3	0.23	0.04	0.24		0.00	0.00	22.3
39	0	7081	1337	236	0	-44	-1250	4.02	4.02	4.02	4.02	3	0.23	0.04	0.24		0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	56	6124	1058	-2	0	-86	-1087	4.02	4.02	4.02	4.02	3	0.19	0.03	0.19		0.00	0.00	22.3
2	56	4696	798	-5	0	-65	-795	4.02	4.02	4.02	4.02	2	0.14	0.02	0.14		0.00	0.00	22.3
3	56	4761	799	-6	0	-82	-797	4.02	4.02	4.02	4.02	2	0.14	0.02	0.14		0.00	0.00	22.3
4	56	4660	828	2	0	-50	-875	4.02	4.02	4.02	4.02	2	0.15	0.02	0.15		0.00	0.00	22.3
5	56	4726	829	2	0	-67	-877	4.02	4.02	4.02	4.02	2	0.16	0.02	0.15		0.00	0.00	22.3
6	56	4607	808	-2	0	-41	-820	4.02	4.02	4.02	4.02	2	0.14	0.02	0.14		0.00	0.00	22.3
7	56	4825	810	-4	0	-96	-828	4.02	4.02	4.02	4.02	2	0.15	0.02	0.14		0.00	0.00	22.3
8	56	4596	817	0	0	-36	-844	4.02	4.02	4.02	4.02	2	0.15	0.02	0.15		0.00	0.00	22.3
9	56	4815	819	-1	0	-91	-852	4.02	4.02	4.02	4.02	2	0.15	0.02	0.15		0.00	0.00	22.3
10	56	4696	798	-5	0	-65	-795	4.02	4.02	4.02	4.02	2	0.14	0.02	0.14		0.00	0.00	22.3
11	56	4761	799	-6	0	-82	-797	4.02	4.02	4.02	4.02	2	0.14	0.02	0.14		0.00	0.00	22.3
12	56	4660	828	2	0	-50	-875	4.02	4.02	4.02	4.02	2	0.15	0.02	0.15		0.00	0.00	22.3
13	56	4726	829	2	0	-67	-877	4.02	4.02	4.02	4.02	2	0.16	0.02	0.15		0.00	0.00	22.3
14	56	4607	808	-2	0	-41	-820	4.02	4.02	4.02	4.02	2	0.14	0.02	0.14		0.00	0.00	22.3
15	56	4825	810	-4	0	-96	-828	4.02	4.02	4.02	4.02	2	0.15	0.02	0.14		0.00	0.00	22.3
16	56	4596	817	0	0	-36	-844	4.02	4.02	4.02	4.02	2	0.15	0.02	0.15		0.00	0.00	22.3
17	56	4815	819	-1	0	-91	-852	4.02	4.02	4.02	4.02	2	0.15	0.02	0.15		0.00	0.00	22.3
18	56	7241	1074	-27	0	-280	-1155	4.02	4.02	4.02	4.02	3	0.21	0.03	0.19		0.00	0.00	22.3
19	56	7140	1086	20	0	-93	-1168	4.02	4.02	4.02	4.02	3	0.21	0.03	0.19		0.00	0.00	22.3
20	56	7325	1075	140	0	-199	-1148	4.02	4.02	4.02	4.02	3	0.21	0.03	0.19		0.00	0.00	22.3
37	56	6940	1062	-43	0	-311	-1122	4.02	4.02	4.02	4.02	3	0.20	0.03	0.19		0.00	0.00	22.3
38	56	6772	1081	35	0	1	-1143	4.02	4.02	4.02	4.02	3	0.20	0.03	0.19		0.00	0.00	22.3
39	56	7081	1062	236	0	-177	-1110	4.02	4.02	4.02	4.02	3	0.20	0.03	0.19		0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	113	6124	782	-2	0	-85	-428	4.02	4.02	4.02	4.02	3	0.07	0.02	0.14		0.00	0.00	22.3
2	113	4696	586	-5	0	-62	297	4.02	4.02	4.02	4.02	2	0.05	0.02	0.10		0.00	0.00	22.3
3	113	4761	587	-6	0	-78	-298	4.02	4.02	4.02	4.02	2	0.05	0.02	0.10		0.00	0.00	22.3
4	113	4660	616	2	0	-52	-360	4.02	4.02	4.02	4.02	2	0.06	0.02	0.11		0.00	0.00	22.3
5	113	4726	617	2	0	-68	-362	4.02	4.02	4.02	4.02	2	0.06	0.02	0.11		0.00	0.00	22.3
6	113	4607	596	-2	0	-40	-316	4.02	4.02	4.02	4.02	2	0.06	0.02	0.11		0.00	0.00	22.3
7	113	4825	598	-4	0	-94	-323	4.02	4.02	4.02	4.02	2	0.06	0.02	0.11		0.00	0.00	22.3
8	113	4596	605	0	0	-36	-335	4.02	4.02	4.02	4.02	2	0.06	0.02	0.11		0.00	0.00	22.3
9	113	4815	607	-1	0	-90	-342	4.02	4.02	4.02	4.02	2	0.06	0.02	0.11		0.00	0.00	22.3
10	113	4696	586	-5	0	-62	297	4.02	4.02	4.02	4.02	2	0.05	0.02	0.10		0.00	0.00	22.3
11	113	4761	587	-6	0	-78	-298	4.02	4.02	4.02	4.02	2	0.05	0.02	0.10		0.00	0.00	22.3
12	113	4660	616	2	0	-52	-360	4.02	4.02	4.02	4.02	2	0.06	0.02	0.11		0.00	0.00	22.3
13	113	4726	617	2	0	-68	-362	4.02	4.02	4.02	4.02	2	0.06	0.02	0.11		0.00	0.00	22.3
14	113	4607	596	-2	0	-40	-316	4.02	4.02	4.02	4.02	2	0.06	0.02	0.11		0.00	0.00	22.3
15	113	4825	598	-4	0	-94	-323	4.02	4.02	4.02	4.02	2	0.06	0.02	0.11		0.00	0.00	22.3
16	113	4596	605	0	0	-36	-335	4.02	4.02	4.02	4.02	2	0.06	0.02	0.11		0.00	0.00	22.3
17	113	4815	607	-1	0	-90	-342	4.02	4.02	4.02	4.02	2	0.06	0.02	0.11		0.00	0.00	22.3
18	113	7241	799	-27	0	-264	-487	4.02	4.02	4.02	4.02	3	0.09	0.02	0.14		0.00	0.00	22.3
19	113	7140	810	20	0	-104	-493	4.02	4.02	4.02	4.02	3	0.09	0.02	0.14		0.00	0.00	22.3
20	113	7325	799	140	0	-279	-479	4.02	4.02	4.02	4.02	3	0.09	0.02	0.14		0.00	0.00	22.3
37	113	6940	786	-43	0	-287	-461	4.02	4.02	4.02	4.02	3	0.09	0.02	0.14		0.00	0.00	22.3
38	113	6772	805	35	0	-19	-471	4.02	4.02	4.02	4.02	3	0.08	0.02	0.14		0.00	0.00	22.3
39	113	7081	786	236	0	-311	-448	4.02	4.02	4.02	4.02	3	0.09	0.02	0.14		0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	170	6124	507	-2	0	-83	589	4.02	4.02	4.02	4.02	3	0.10	0.01	0.09		0.00	0.00	22.3
2	170	4696	374	-5	0	-59	456	4.02	4.02	4.02	4.02	2	0.08	0.01	0.07		0.00	0.00	22.3
3	170	4761	375	-6	0	-75	455	4.02	4.02	4.02	4.02	2	0.08	0.01	0.07		0.00	0.00	22.3
4	170	4660	404	2	0	-53	445	4.02	4.02	4.02	4.02	2	0.08	0.01	0.07		0.00	0.00	22.3
5	170	4726	405	2	0	-69	445	4.02	4.02	4.02	4.02	2	0.08	0.01	0.07		0.00	0.00	22.3
6	170	4607	384	-2	0	-38	457	4.02	4.02	4.02	4.02	2	0.08	0.01	0.07		0.00	0.00	22.3
7	170	4825	386	-4	0	-91	454	4.02	4.02	4.02	4.02	2	0.08	0.01	0.07		0.00	0.00	22.3
8	170	4596	393	0	0	-37	452	4.02	4.02	4.02	4.02	2	0.08	0.01	0.07		0.00	0.00	22.3
9	170	4815	395	-1	0	-90	449	4.02	4.02	4.02	4.02	2	0.08	0.01	0.07		0.00	0.00	22.3
10	170	4696	374	-5	0	-59	456	4.02	4.02	4.02	4.02	2	0.08	0.01	0.07		0.00	0.00	22.3
11	170	4761	375	-6	0	-75	455	4.02	4.02	4.02	4.02	2	0.08	0.01	0.07		0.00	0.00	22.3
12	170	4660	404	2	0	-53	445	4.02	4.02	4.02	4.02	2	0.08	0.01	0.07		0.00	0.00	22.3
13	170	4726	405	2	0	-69	445	4.02	4.02	4.02	4.02	2	0.08	0.01	0.07		0.00	0.00	22.3
14	170	4607	384	-2	0	-38	457	4.02	4.02	4.02	4.02	2	0.08	0.01	0.07		0.00	0.00	22.3
15	170	4825	386	-4	0	-91	454	4.02	4.02	4.02	4.02	2	0.08	0.01	0.07		0.00	0.00	22.3
16	170	4596	393	0	0	-37	452	4.02	4.02	4.02	4.02	2	0.08	0.01	0.07		0.00	0.00	22.3
17	170	4815	395	-1	0	-90	449	4.02	4.02	4.02	4.02	2	0.08	0.01	0.07		0.00	0.00	22.3
18	170	7241	524	-27	0	-249	556	4.02	4.02	4.02	4.02	3	0.10	0.02	0.09		0.00	0.00	22.3
19	170	7140	535	20	0	-115	568	4.02	4.02	4.02	4.02	3	0.10	0.02	0.10		0.00	0.00	22.3
20	170	7325	524	140	0	-358	564	4.02	4.02	4.02	4.02	3	0.11	0.02	0.09		0.00	0.00	22.3
37	170	6940	510	-43	0	-263	562	4.02	4.02	4.02	4.02	3	0.10	0.01	0.09		0.00	0.00	22.3
38	170	6772	530	35	0	-39	582	4.02	4.02	4.02	4.02	3	0.10	0.02	0.09		0.00	0.00	22.3
39	170	7081	511	236	0	-444	575	4.02	4.02	4.02	4.02	3	0.13	0.01	0.09		0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	226	6124	231	-2	0	-82	594	4.02	4.02	4.02	4.02	3	0.10	0.01	0.04	0.00	0.00	22.3
2	226	4696	162	-5	0	-56	456	4.02	4.02	4.02	4.02	2	0.08	0.00	0.03	0.00	0.00	22.3
3	226	4761	163	-6	0	-72	455	4.02	4.02	4.02	4.02	2	0.08	0.00	0.03	0.00	0.00	22.3
4	226	4660	192	2	0	-54	458	4.02	4.02	4.02	4.02	2	0.08	0.01	0.03	0.00	0.00	22.3
5	226	4726	193	2	0	-70	458	4.02	4.02	4.02	4.02	2	0.08	0.01	0.03	0.00	0.00	22.3
6	226	4607	172	-2	0	-37	458	4.02	4.02	4.02	4.02	2	0.08	0.00	0.03	0.00	0.00	22.3
7	226	4825	174	-4	0	-89	455	4.02	4.02	4.02	4.02	2	0.08	0.01	0.03	0.00	0.00	22.3
8	226	4596	181	0	0	-37	458	4.02	4.02	4.02	4.02	2	0.08	0.01	0.03	0.00	0.00	22.3
9	226	4815	183	-1	0	-89	456	4.02	4.02	4.02	4.02	2	0.08	0.01	0.03	0.00	0.00	22.3
10	226	4696	162	-5	0	-56	456	4.02	4.02	4.02	4.02	2	0.08	0.00	0.03	0.00	0.00	22.3
11	226	4761	163	-6	0	-72	455	4.02	4.02	4.02	4.02	2	0.08	0.00	0.03	0.00	0.00	22.3
12	226	4660	192	2	0	-54	458	4.02	4.02	4.02	4.02	2	0.08	0.01	0.03	0.00	0.00	22.3
13	226	4726	193	2	0	-70	458	4.02	4.02	4.02	4.02	2	0.08	0.01	0.03	0.00	0.00	22.3
14	226	4607	172	-2	0	-37	458	4.02	4.02	4.02	4.02	2	0.08	0.00	0.03	0.00	0.00	22.3
15	226	4825	174	-4	0	-89	455	4.02	4.02	4.02	4.02	2	0.08	0.01	0.03	0.00	0.00	22.3
16	226	4596	181	0	0	-37	458	4.02	4.02	4.02	4.02	2	0.08	0.01	0.03	0.00	0.00	22.3
17	226	4815	183	-1	0	-89	456	4.02	4.02	4.02	4.02	2	0.08	0.01	0.03	0.00	0.00	22.3
18	226	7241	248	-27	0	-234	571	4.02	4.02	4.02	4.02	3	0.10	0.01	0.04	0.00	0.00	22.3
19	226	7140	259	20	0	-126	591	4.02	4.02	4.02	4.02	3	0.11	0.01	0.05	0.00	0.00	22.3
20	226	7325	248	140	0	-437	580	4.02	4.02	4.02	4.02	3	0.13	0.01	0.04	0.00	0.00	22.3
37	226	6940	235	-43	0	-239	569	4.02	4.02	4.02	4.02	3	0.10	0.01	0.04	0.00	0.00	22.3
38	226	6772	254	35	0	-59	602	4.02	4.02	4.02	4.02	3	0.11	0.01	0.05	0.00	0.00	22.3
39	226	7081	235	236	0	-578	583	4.02	4.02	4.02	4.02	3	0.17	0.01	0.04	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	282	6124	-44	-2	0	-81	594	4.02	4.02	4.02	4.02	3	0.10	0.00	0.01	0.00	0.00	22.3
2	282	4696	-50	-5	0	-53	456	4.02	4.02	4.02	4.02	2	0.08	0.00	0.01	0.00	0.00	22.3
3	282	4761	-48	-6	0	-69	455	4.02	4.02	4.02	4.02	2	0.08	0.00	0.01	0.00	0.00	22.3
4	282	4660	-20	2	0	-55	458	4.02	4.02	4.02	4.02	2	0.08	0.00	0.00	0.00	0.00	22.3
5	282	4726	-18	2	0	-71	458	4.02	4.02	4.02	4.02	2	0.08	0.00	0.00	0.00	0.00	22.3
6	282	4607	-40	-2	0	-36	458	4.02	4.02	4.02	4.02	2	0.08	0.00	0.01	0.00	0.00	22.3
7	282	4825	-38	-4	0	-87	455	4.02	4.02	4.02	4.02	2	0.08	0.00	0.01	0.00	0.00	22.3
8	282	4596	-30	0	0	-37	458	4.02	4.02	4.02	4.02	2	0.08	0.00	0.01	0.00	0.00	22.3
9	282	4815	-28	-1	0	-88	456	4.02	4.02	4.02	4.02	2	0.08	0.00	0.01	0.00	0.00	22.3
10	282	4696	-50	-5	0	-53	456	4.02	4.02	4.02	4.02	2	0.08	0.00	0.01	0.00	0.00	22.3
11	282	4761	-48	-6	0	-69	455	4.02	4.02	4.02	4.02	2	0.08	0.00	0.01	0.00	0.00	22.3
12	282	4660	-20	2	0	-55	458	4.02	4.02	4.02	4.02	2	0.08	0.00	0.00	0.00	0.00	22.3
13	282	4726	-18	2	0	-71	458	4.02	4.02	4.02	4.02	2	0.08	0.00	0.00	0.00	0.00	22.3
14	282	4607	-40	-2	0	-36	458	4.02	4.02	4.02	4.02	2	0.08	0.00	0.01	0.00	0.00	22.3
15	282	4825	-38	-4	0	-87	455	4.02	4.02	4.02	4.02	2	0.08	0.00	0.01	0.00	0.00	22.3
16	282	4596	-30	0	0	-37	458	4.02	4.02	4.02	4.02	2	0.08	0.00	0.01	0.00	0.00	22.3
17	282	4815	-28	-1	0	-88	456	4.02	4.02	4.02	4.02	2	0.08	0.00	0.01	0.00	0.00	22.3
18	282	7241	-28	-27	0	-219	571	4.02	4.02	4.02	4.02	3	0.10	0.00	0.00	0.00	0.00	22.3
19	282	7140	-16	20	0	-138	591	4.02	4.02	4.02	4.02	3	0.11	0.00	0.00	0.00	0.00	22.3
20	282	7325	-27	140	0	-517	580	4.02	4.02	4.02	4.02	3	0.16	0.00	0.00	0.00	0.00	22.3
37	282	6940	-40	-43	0	-214	569	4.02	4.02	4.02	4.02	3	0.10	0.00	0.01	0.00	0.00	22.3
38	282	6772	-21	35	0	-79	602	4.02	4.02	4.02	4.02	3	0.11	0.00	0.00	0.00	0.00	22.3
39	282	7081	-40	236	0	-711	583	4.02	4.02	4.02	4.02	3	0.21	0.01	0.04	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	339	6124	-319	-2	0	-79	594	4.02	4.02	4.02	4.02	3	0.10	0.01	0.06	0.00	0.00	22.3
2	339	4696	-261	-5	0	-50	456	4.02	4.02	4.02	4.02	2	0.08	0.01	0.05	0.00	0.00	22.3
3	339	4761	-260	-6	0	-65	455	4.02	4.02	4.02	4.02	2	0.08	0.01	0.05	0.00	0.00	22.3
4	339	4660	-231	2	0	-57	458	4.02	4.02	4.02	4.02	2	0.08	0.01	0.04	0.00	0.00	22.3
5	339	4726	-230	2	0	-72	458	4.02	4.02	4.02	4.02	2	0.08	0.01	0.04	0.00	0.00	22.3
6	339	4607	-251	-2	0	-35	458	4.02	4.02	4.02	4.02	2	0.08	0.01	0.04	0.00	0.00	22.3
7	339	4825	-249	-4	0	-85	455	4.02	4.02	4.02	4.02	2	0.08	0.01	0.04	0.00	0.00	22.3
8	339	4596	-242	0	0	-37	458	4.02	4.02	4.02	4.02	2	0.08	0.01	0.04	0.00	0.00	22.3
9	339	4815	-240	-1	0	-87	456	4.02	4.02	4.02	4.02	2	0.08	0.01	0.04	0.00	0.00	22.3
10	339	4696	-261	-5	0	-50	456	4.02	4.02	4.02	4.02	2	0.08	0.01	0.05	0.00	0.00	22.3
11	339	4761	-260	-6	0	-65	455	4.02	4.02	4.02	4.02	2	0.08	0.01	0.05	0.00	0.00	22.3
12	339	4660	-231	2	0	-57	458	4.02	4.02	4.02	4.02	2	0.08	0.01	0.04	0.00	0.00	22.3
13	339	4726	-230	2	0	-72	458	4.02	4.02	4.02	4.02	2	0.08	0.01	0.04	0.00	0.00	22.3
14	339	4607	-251	-2	0	-35	458	4.02	4.02	4.02	4.02	2	0.08	0.01	0.04	0.00	0.00	22.3
15	339	4825	-249	-4	0	-85	455	4.02	4.02	4.02	4.02	2	0.08	0.01	0.04	0.00	0.00	22.3
16	339	4596	-242	0	0	-37	458	4.02	4.02	4.02	4.02	2	0.08	0.01	0.04	0.00	0.00	22.3
17	339	4815	-240	-1	0	-87	456	4.02	4.02	4.02	4.02	2	0.08	0.01	0.04	0.00	0.00	22.3
18	339	7241	-303	-27	0	-203	571	4.02	4.02	4.02	4.02	3	0.10	0.01	0.05	0.00	0.00	22.3
19	339	7140	-291	20	0	-149	591	4.02	4.02	4.02	4.02	3	0.11	0.01	0.05	0.00	0.00	22.3
20	339	7325	-302	140	0	-596	580	4.02	4.02	4.02	4.02	3	0.18	0.01	0.05	0.00	0.00	22.3
37	339	6940	-316	-43	0	-190	569	4.02	4.02	4.02	4.02	3	0.10	0.01	0.06	0.00	0.00	22.3
38	339	6772	-296	35	0	-99	602	4.02	4.02	4.02	4.02	3	0.11	0.01	0.05	0.00	0.00	22.3
39	339	7081	-315	236	0	-845	583	4.02	4.02	4.02	4.02	3	0.26	0.01	0.06	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	396	6124	-595	-2	0	-78	534	4.02	4.02	4.02	4.02	3	0.09	0.02	0.11	0.00	0.00	22.3
2	396	4696	-473	-5	0	-47	401	4.02	4.02	4.02	4.02	2	0.07	0.01	0.08	0.00	0.00	22.3
3	396	4761	-472	-6	0	-62	400	4.02	4.02	4.02	4.02	2	0.07	0.01	0.08	0.00	0.00	22.3
4	396	4660	-443	2	0	-58	421	4.02	4.02	4.02	4.02	2	0.07	0.01	0.08	0.00	0.00	22.3
5	396	4726	-442	2	0	-73	421	4.02	4.02	4.02	4.02	2	0.07	0.01	0.08	0.00	0.00	22.3
6	396	4607	-463	-2	0	-34	408	4.02	4.02	4.02	4.02	2	0.07	0.01	0.08	0.00	0.00	22.3
7	396	4825	-461	-4	0	-83	407	4.02	4.02	4.02	4.02	2	0.07	0.01	0.08	0.00	0.00	22.3
8	396	4596	-454	0	0	-37	415	4.02	4.02	4.02	4.02	2	0.07	0.01	0.08	0.00	0.00	22.3
9	396	4815	-452	-1	0	-86	413	4.02	4.02	4.02	4.02	2	0.07	0.01	0.08	0.00	0.00	22.3
10	396	4696	-473	-5	0	-47	401	4.02	4.02	4.02	4.02	2	0.07	0.01	0.08	0.00	0.00	22.3
11	396	4761	-472	-6	0	-62	400	4.02	4.02	4.02	4.02	2	0.07	0.01	0.08	0.00	0.00	22.3
12	396	4660	-443	2	0	-58	421	4.02	4.02	4.02	4.02	2	0.07	0.01	0.08	0.00	0.00	22.3
13	396	4726	-442	2	0	-73	421	4.02	4.02	4.02	4.02	2	0.07	0.01	0.08	0.00	0.00	22.3
14	396	4607	-463	-2	0	-34	408	4.02	4.02	4.02	4.02	2	0.07	0.01	0.08	0.00	0.00	22.3
15	396	4825	-461	-4	0	-83	407	4.02	4.02	4.02	4.02	2	0.07	0.01	0.08	0.00	0.00	22.3
16	396	4596	-454	0	0	-37	415	4.02	4.02	4.02	4.02	2	0.07	0.01	0.08	0.00	0.00	22.3
17	396	4815	-452	-1	0	-86	413	4.02	4.02	4.02	4.02	2	0.07	0.01	0.08	0.00	0.00	22.3
18	396	7241	-578	-27	0	-188	522	4.02	4.02	4.02	4.02	3	0.09	0.02	0.10	0.00	0.00	22.3
19	396	7140	-567	20	0	-160	549	4.02	4.02	4.02	4.02	3	0.10	0.02	0.10	0.00	0.00	22.3
20	396	7325	-578	140	0	-675	530	4.02	4.02	4.02	4.02	3	0.21	0.02	0.10	0.00	0.00	22.3
37	396	6940	-591	-43	0	-166	511	4.02	4.02	4.02	4.02	3	0.09	0.02	0.11	0.00	0.00	22.3
38	396	6772	-572	35	0	-119	557	4.02	4.02	4.02	4.02	3	0.10	0.02	0.10	0.00	0.00	22.3
39	396	7081	-591	236	0	-978	526	4.02	4.02	4.02	4.02	3	0.30	0.02	0.11	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	452	6124	-870	-2	0	-77	-622	4.02	4.02	4.02	4.02	3	0.11	0.03	0.15	0.00	0.00	22.3
2	452	4696	-685	-5	0	-44	-513	4.02	4.02	4.02	4.02	2	0.09	0.02	0.12	0.00	0.00	22.3
3	452	4761	-684	-6	0	-59	-513	4.02	4.02	4.02	4.02	2	0.09	0.02	0.12	0.00	0.00	22.3
4	452	4660	-655	2	0	-59	-445	4.02	4.02	4.02	4.02	2	0.08	0.02	0.12	0.00	0.00	22.3
5	452	4726	-654	2	0	-74	-444	4.02	4.02	4.02	4.02	2	0.08	0.02	0.12	0.00	0.00	22.3
6	452	4607	-675	-2	0	-33	-490	4.02	4.02	4.02	4.02	2	0.09	0.02	0.12	0.00	0.00	22.3

7	452	4825	-673	-4	0	-81	-488	4.02	4.02	4.02	4.02	2	0.09	0.02	0.12	0.00	0.00	22.3
8	452	4596	-666	0	0	-37	-469	4.02	4.02	4.02	4.02	2	0.08	0.02	0.12	0.00	0.00	22.3
9	452	4815	-664	-1	0	-86	-468	4.02	4.02	4.02	4.02	2	0.08	0.02	0.12	0.00	0.00	22.3
10	452	4696	-685	-5	0	-44	-513	4.02	4.02	4.02	4.02	2	0.09	0.02	0.12	0.00	0.00	22.3
11	452	4761	-684	-6	0	-59	-513	4.02	4.02	4.02	4.02	2	0.09	0.02	0.12	0.00	0.00	22.3
12	452	4660	-655	2	0	-59	-445	4.02	4.02	4.02	4.02	2	0.08	0.02	0.12	0.00	0.00	22.3
13	452	4726	-654	2	0	-74	-444	4.02	4.02	4.02	4.02	2	0.08	0.02	0.12	0.00	0.00	22.3
14	452	4607	-675	-2	0	-33	-490	4.02	4.02	4.02	4.02	2	0.09	0.02	0.12	0.00	0.00	22.3
15	452	4825	-673	-4	0	-81	-488	4.02	4.02	4.02	4.02	2	0.09	0.02	0.12	0.00	0.00	22.3
16	452	4596	-666	0	0	-37	-469	4.02	4.02	4.02	4.02	2	0.08	0.02	0.12	0.00	0.00	22.3
17	452	4815	-664	-1	0	-86	-468	4.02	4.02	4.02	4.02	2	0.08	0.02	0.12	0.00	0.00	22.3
18	452	7241	-854	-27	0	-173	-608	4.02	4.02	4.02	4.02	3	0.11	0.02	0.15	0.00	0.00	22.3
19	452	7140	-842	20	0	-171	-563	4.02	4.02	4.02	4.02	3	0.10	0.02	0.15	0.00	0.00	22.3
20	452	7325	-853	140	0	-755	-598	4.02	4.02	4.02	4.02	3	0.23	0.02	0.15	0.00	0.00	22.3
37	452	6940	-867	-43	0	-142	-639	4.02	4.02	4.02	4.02	3	0.12	0.03	0.15	0.00	0.00	22.3
38	452	6772	-847	35	0	-140	-563	4.02	4.02	4.02	4.02	3	0.10	0.02	0.15	0.00	0.00	22.3
39	452	7081	-866	236	0	-1112	-623	4.02	4.02	4.02	4.02	3	0.34	0.03	0.15	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	508	6124	-1146	-2	0	-76	-1331	4.02	4.02	4.02	4.02	3	0.23	0.03	0.20	0.00	0.00	22.3
2	508	4696	-897	-5	0	-41	-1067	4.02	4.02	4.02	4.02	2	0.19	0.03	0.16	0.00	0.00	22.3
3	508	4761	-896	-6	0	-56	-1066	4.02	4.02	4.02	4.02	2	0.19	0.03	0.16	0.00	0.00	22.3
4	508	4660	-867	2	0	-61	-982	4.02	4.02	4.02	4.02	2	0.17	0.03	0.15	0.00	0.00	22.3
5	508	4726	-866	2	0	-75	-981	4.02	4.02	4.02	4.02	2	0.17	0.03	0.15	0.00	0.00	22.3
6	508	4607	-887	-2	0	-31	-1038	4.02	4.02	4.02	4.02	2	0.18	0.03	0.16	0.00	0.00	22.3
7	508	4825	-885	-4	0	-79	-1035	4.02	4.02	4.02	4.02	2	0.18	0.03	0.16	0.00	0.00	22.3
8	508	4596	-878	0	0	-37	-1013	4.02	4.02	4.02	4.02	2	0.18	0.03	0.16	0.00	0.00	22.3
9	508	4815	-876	-1	0	-85	-1011	4.02	4.02	4.02	4.02	2	0.18	0.03	0.16	0.00	0.00	22.3
10	508	4696	-897	-5	0	-41	-1067	4.02	4.02	4.02	4.02	2	0.19	0.03	0.16	0.00	0.00	22.3
11	508	4761	-896	-6	0	-56	-1066	4.02	4.02	4.02	4.02	2	0.19	0.03	0.16	0.00	0.00	22.3
12	508	4660	-867	2	0	-61	-982	4.02	4.02	4.02	4.02	2	0.17	0.03	0.15	0.00	0.00	22.3
13	508	4726	-866	2	0	-75	-981	4.02	4.02	4.02	4.02	2	0.17	0.03	0.15	0.00	0.00	22.3
14	508	4607	-887	-2	0	-31	-1038	4.02	4.02	4.02	4.02	2	0.18	0.03	0.16	0.00	0.00	22.3
15	508	4825	-885	-4	0	-79	-1035	4.02	4.02	4.02	4.02	2	0.18	0.03	0.16	0.00	0.00	22.3
16	508	4596	-878	0	0	-37	-1013	4.02	4.02	4.02	4.02	2	0.18	0.03	0.16	0.00	0.00	22.3
17	508	4815	-876	-1	0	-85	-1011	4.02	4.02	4.02	4.02	2	0.18	0.03	0.16	0.00	0.00	22.3
18	508	7241	-1129	-27	0	-158	-1308	4.02	4.02	4.02	4.02	3	0.24	0.03	0.20	0.00	0.00	22.3
19	508	7140	-1118	20	0	-182	-1256	4.02	4.02	4.02	4.02	3	0.23	0.03	0.20	0.00	0.00	22.3
20	508	7325	-1129	140	0	-834	-1298	4.02	4.02	4.02	4.02	3	0.25	0.03	0.20	0.00	0.00	22.3
37	508	6940	-1142	-43	0	-118	-1346	4.02	4.02	4.02	4.02	3	0.24	0.03	0.20	0.00	0.00	22.3
38	508	6772	-1123	35	0	-160	-1258	4.02	4.02	4.02	4.02	3	0.23	0.03	0.20	0.00	0.00	22.3
39	508	7081	-1142	236	0	-1245	-1329	4.02	4.02	4.02	4.02	3	0.38	0.03	0.20	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	565	6124	-1421	-2	0	-74	-1476	4.02	4.02	4.02	4.02	3	0.26	0.04	0.25	0.00	0.00	22.3
2	565	4696	-1109	-5	0	-38	-1179	4.02	4.02	4.02	4.02	2	0.21	0.03	0.20	0.00	0.00	22.3
3	565	4761	-1108	-6	0	-52	-1179	4.02	4.02	4.02	4.02	2	0.21	0.03	0.20	0.00	0.00	22.3
4	565	4660	-1079	2	0	-62	-1093	4.02	4.02	4.02	4.02	2	0.19	0.03	0.19	0.00	0.00	22.3
5	565	4726	-1078	2	0	-76	-1092	4.02	4.02	4.02	4.02	2	0.19	0.03	0.19	0.00	0.00	22.3
6	565	4607	-1099	-2	0	-30	-1150	4.02	4.02	4.02	4.02	2	0.20	0.03	0.20	0.00	0.00	22.3
7	565	4825	-1097	-4	0	-77	-1147	4.02	4.02	4.02	4.02	2	0.20	0.03	0.20	0.00	0.00	22.3
8	565	4596	-1090	0	0	-37	-1124	4.02	4.02	4.02	4.02	2	0.20	0.03	0.19	0.00	0.00	22.3
9	565	4815	-1088	-1	0	-84	-1122	4.02	4.02	4.02	4.02	2	0.20	0.03	0.19	0.00	0.00	22.3
10	565	4696	-1109	-5	0	-38	-1179	4.02	4.02	4.02	4.02	2	0.21	0.03	0.20	0.00	0.00	22.3
11	565	4761	-1108	-6	0	-52	-1179	4.02	4.02	4.02	4.02	2	0.21	0.03	0.20	0.00	0.00	22.3
12	565	4660	-1079	2	0	-62	-1093	4.02	4.02	4.02	4.02	2	0.19	0.03	0.19	0.00	0.00	22.3
13	565	4726	-1078	2	0	-76	-1092	4.02	4.02	4.02	4.02	2	0.19	0.03	0.19	0.00	0.00	22.3
14	565	4607	-1099	-2	0	-30	-1150	4.02	4.02	4.02	4.02	2	0.20	0.03	0.20	0.00	0.00	22.3
15	565	4825	-1097	-4	0	-77	-1147	4.02	4.02	4.02	4.02	2	0.20	0.03	0.20	0.00	0.00	22.3
16	565	4596	-1090	0	0	-37	-1124	4.02	4.02	4.02	4.02	2	0.20	0.03	0.19	0.00	0.00	22.3
17	565	4815	-1088	-1	0	-84	-1122	4.02	4.02	4.02	4.02	2	0.20	0.03	0.19	0.00	0.00	22.3
18	565	7241	-1405	-27	0	-142	-1452	4.02	4.02	4.02	4.02	3	0.26	0.04	0.25	0.00	0.00	22.3
19	565	7140	-1393	20	0	-194	-1399	4.02	4.02	4.02	4.02	3	0.25	0.04	0.25	0.00	0.00	22.3
20	565	7325	-1404	140	0	-913	-1442	4.02	4.02	4.02	4.02	3	0.28	0.04	0.25	0.00	0.00	22.3
37	565	6940	-1418	-43	0	-94	-1491	4.02	4.02	4.02	4.02	3	0.27	0.04	0.25	0.00	0.00	22.3
38	565	6772	-1398	35	0	-180	-1402	4.02	4.02	4.02	4.02	3	0.25	0.04	0.25	0.00	0.00	22.3
39	565	7081	-1417	236	0	-1379	-1474	4.02	4.02	4.02	4.02	3	0.42	0.04	0.25	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

Nome travata: **Trave_401_IP1** Descrizione: **Trave_4 7-12-17-22-32**
ASTA NUM. 3 NI 37 NF 39 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y Permanente qy tot.
qy medio: 375.00 272.00 647.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	5629	2344	19	0	-24	-1900	4.02	4.02	4.02	4.02	3	0.33	0.07	0.42	0.00	0.00	22.3
2	0	4224	1787	10	0	-25	-1417	4.02	4.02	4.02	4.02	2	0.25	0.05	0.32	0.00	0.00	22.3
3	0	4289	1786	13	0	-33	-1416	4.02	4.02	4.02	4.02	2	0.25	0.05	0.32	0.00	0.00	22.3
4	0	4371	1820	17	0	-4	-1508	4.02	4.02	4.02	4.02	2	0.26	0.05	0.32	0.00	0.00	22.3
5	0	4436	1818	20	0	-12	-1506	4.02	4.02	4.02	4.02	2	0.26	0.05	0.32	0.00	0.00	22.3
6	0	4200	1800	9	0	-8	-1451	4.02	4.02	4.02	4.02	2	0.25	0.05	0.32	0.00	0.00	22.3
7	0	4416	1796	19	0	-35	-1446	4.02	4.02	4.02	4.02	2	0.25	0.05	0.32	0.00	0.00	22.3
8	0	4244	1810	11	0	-2	-1478	4.02	4.02	4.02	4.02	2	0.26	0.05	0.32	0.00	0.00	22.3
9	0	4460	1806	21	0	-29	-1473	4.02	4.02	4.02	4.02	2	0.26	0.05	0.32	0.00	0.00	22.3
10	0	4224	1787	10	0	-25	-1417	4.02	4.02	4.02	4.02	2	0.25	0.05	0.32	0.00	0.00	22.3
11	0	4289	1786	13	0	-33	-1416	4.02	4.02	4.02	4.02	2	0.25	0.05	0.32	0.00	0.00	22.3
12	0	4371	1820	17	0	-4	-1508	4.02	4.02	4.02	4.02	2	0.26	0.05	0.32	0.00	0.00	22.3
13	0	4436	1818	20	0	-12	-1506	4.02	4.02	4.02	4.02	2	0.26	0.05	0.32	0.00	0.00	22.3
14	0	4200	1800	9	0	-8	-1451	4.02	4.02	4.02	4.02	2	0.25	0.05	0.32	0.00	0.00	22.3
15	0	4416	1796	19	0	-35	-1446	4.02	4.02	4.02	4.02	2	0.25	0.05	0.32	0.00	0.00	22.3
16	0	4244	1810	11	0	-2	-1478	4.02	4.02	4.02	4.02	2	0.26	0.05	0.32	0.00	0.00	22.3
17	0	4460	1806	21	0	-29	-1473	4.02	4.02	4.02	4.02	2	0.26	0.05	0.32	0.00	0.00	22.3
18	0	6108	2282	2	0	-151	-1749	4.02	4.02	4.02	4.02	3	0.31	0.07	0.41	0.00	0.00	22.3
19	0	7093	2331	83	0	31	-1892	4.02	4.02	4.02	4.02	3	0.34	0.07	0.42	0.00	0.00	22.3
20	0	6747	2310	-83	0	-780	-1835	4.02	4.02	4.02	4.02	3	0.33	0.07	0.41	0.00	0.00	22.3
37	0	5471	2278	-32	0	-200	-1726	4.02	4.02	4.02	4.02	3	0.29	0.07	0.41	0.00	0.00	22.3
38	0	7113	2359	103	0	105	-1964	4.02	4.02	4.02	4.02	3	0.36	0.07	0.42	0.00	0.00	22.3
39	0	6536	2325	-174	0	-1247	-1871	4.02	4.02	4.02	4.02	3	0.37	0.07	0.41	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	57	5629	1837	19	0	-35	-1649	4.02	4.02	4.02	4.02	3	0.28	0.05	0.33	0.00	0.00	22.3
2	57	4224	1397	10	0	-30	-1225	4.02	4.02	4.02	4.02	2	0.21	0.04	0.25	0.00	0.00	22.3
3	57	4289	1396	13	0	-40	-1224	4.02	4.02	4.02	4.02	2	0.21	0.04	0.25	0.00	0.00	22.3
4	57	4371	1430	17	0	-13	-1314	4.02	4.02	4.02	4.02	2	0.23	0.04	0.25	0.00	0.00	22.3
5	57	4436	1428	20	0	-23	-1312	4.02	4.02	4.02	4.02	2	0.23	0.04	0.25	0.00	0.00	22.3
6	57	4200	1410	9	0	-13	-1258	4.02	4.02	4.02	4.02	2	0.22	0.04	0.25	0.00	0.00	22.3
7	57	4416	1406	19	0	-46	-1253	4.02	4.02	4.02	4.02	2	0.22	0.04	0.25	0.00	0.00	22.3
8	57	4244	1420	11	0	-8	-1285	4.02	4.02	4.02	4.02	2	0.22	0.04	0.25	0.00	0.00	22.3
9	57	4460	1416	21	0	-41	-1280	4.02	4.02	4.02	4.02	2	0.22	0.04	0.25	0.00	0.00	22.3
10	57	4224	1397	10	0	-30	-1225	4.02	4.02	4.02	4.02	2	0.21	0.04	0.25	0.00	0.00	22.3
11	57	4289	1396	13	0	-40	-1224	4.02	4.02	4.02	4.02	2	0.21	0.04	0.25	0.00	0.00	22.3
12	57	4371	1430	17	0	-13	-1314	4.02	4.02	4.02	4.02	2	0.23	0.04	0.25	0.00	0.00	22.3
13	57	4436	1428	20	0	-23	-1312	4.02	4.02	4.02	4.02	2	0.23	0.04	0.25	0.00	0.00	22.3
14	57	4200	1410	9	0	-13	-1258	4.02	4.02	4.02	4.02	2	0.22	0.04	0.25	0.00	0.00	22.3
15	57	4416	1406	19	0	-46	-1253	4.02	4.02	4.02	4.02	2	0.22	0.04	0.25	0.00	0.00	22.3
16	57	4244	1420	11	0	-8	-1285	4.02	4.02	4.02	4.02	2	0.22	0.04	0.25	0.00	0.00	22.3
17	57	4460	1416	21	0	-41	-1280	4.02	4.02	4.02	4.02	2	0.22	0.04	0.25	0.00	0.00	22.3
18	57	6108	1775	2	0	-152	-1502	4.02	4.02	4.02	4.02	3	0.26	0.05	0.32	0.00	0.00	22.3
19	57	7093	1824	83	0	-15	-1642	4.02	4.02	4.02	4.02	3	0.30	0.05	0.32	0.00	0.00	22.3
20	57	6747	1803	-83	0	-733	-1586	4.02	4.02	4.02	4.02	3	0.28	0.05	0.32	0.00	0.00	22.3
37	57	5471	1771	-32	0	-181	-1479	4.02	4.02	4.02	4.02	3	0.25	0.05	0.32	0.00	0.00	22.3
38	57	7113	1852	103	0	47	-1712	4.02	4.02	4.02	4.02	3	0.31	0.05	0.33	0.00	0.00	22.3
39	57	6536	1818	-174	0	-1149	-1621	4.02	4.02	4.02	4.02	3	0.34	0.05	0.32	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	113	5629	1337	19	0	-46	854	4.02	4.02	4.02	4.02	3	0.15	0.04	0.24	0.00	0.00	22.3
2	113	4224	1013	10	0	-36	676	4.02	4.02	4.02	4.02	2	0.12	0.03	0.18	0.00	0.00	22.3
3	113	4289	1012	13	0	-48	675	4.02	4.02	4.02	4.02	2	0.12	0.03	0.18	0.00	0.00	22.3
4	113	4371	1045	17	0	-23	638	4.02	4.02	4.02	4.02	2	0.11	0.03	0.19	0.00	0.00	22.3
5	113	4436	1044	20	0	-34	638	4.02	4.02	4.02	4.02	2	0.11	0.03	0.19	0.00	0.00	22.3
6	113	4200	1025	9	0	-18	663	4.02	4.02	4.02	4.02	2	0.12	0.03	0.18	0.00	0.00	22.3
7	113	4416	1022	19	0	-56	661	4.02	4.02	4.02	4.02	2	0.12	0.03	0.18	0.00	0.00	22.3
8	113	4244	1035	11	0	-14	651	4.02	4.02	4.02	4.02	2	0.11	0.03	0.18	0.00	0.00	22.3
9	113	4460	1031	21	0	-52	650	4.02	4.02	4.02	4.02	2	0.11	0.03	0.18	0.00	0.00	22.3
10	113	4224	1013	10	0	-36	676	4.02	4.02	4.02	4.02	2	0.12	0.03	0.18	0.00	0.00	22.3
11	113	4289	1012	13	0	-48	675	4.02	4.02	4.02	4.02	2	0.12	0.03	0.18	0.00	0.00	22.3
12	113	4371	1045	17	0	-23	638	4.02	4.02	4.02	4.02	2	0.11	0.03	0.19	0.00	0.00	22.3
13	113	4436	1044	20	0	-34	638	4.02	4.02	4.02	4.02	2	0.11	0.03	0.19	0.00	0.00	22.3
14	113	4200	1025	9	0	-18	663	4.02	4.02	4.02	4.02	2	0.12	0.03	0.18	0.00	0.00	22.3
15	113	4416	1022	19	0	-56	661	4.02	4.02	4.02	4.02	2	0.12	0.03	0.18	0.00	0.00	22.3
16	113	4244	1035	11	0	-14	651	4.02	4.02	4.02	4.02	2	0.11	0.03	0.18	0.00	0.00	22.3
17	113	4460	1031	21	0	-52	650	4.02	4.02	4.02	4.02	2	0.11	0.03	0.18	0.00	0.00	22.3
18	113	6108	1275	2	0	-153	904	4.02	4.02	4.02	4.02	3	0.16	0.04	0.23	0.00	0.00	22.3
19	113	7093	1324	83	0	-62	841	4.02	4.02	4.02	4.02	3	0.15	0.04	0.24	0.00	0.00	22.3
20	113	6747	1303	-83	0	-685	864	4.02	4.02	4.02	4.02	3	0.20	0.04	0.23	0.00	0.00	22.3
37	113	5471	1271	-32	0	-163	920	4.02	4.02	4.02	4.02	3	0.16	0.04	0.23	0.00	0.00	22.3
38	113	7113	1352	103	0	-12	815	4.02	4.02	4.02	4.02	3	0.15	0.04	0.24	0.00	0.00	22.3
39	113	6536	1318	-174	0	-1050	852	4.02	4.02	4.02	4.02	3	0.31	0.04	0.23	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	170	5629	844	19	0	-57	1199	4.02	4.02	4.02	4.02	3	0.21	0.02	0.15	0.00	0.00	22.3
2	170	4224	634	10	0	-42	923	4.02	4.02	4.02	4.02	2	0.16	0.02	0.11	0.00	0.00	22.3
3	170	4289	633	13	0	-55	921	4.02	4.02	4.02	4.02	2	0.16	0.02	0.11	0.00	0.00	22.3
4	170	4371	666	17	0	-32	923	4.02	4.02	4.02	4.02	2	0.16	0.02	0.12	0.00	0.00	22.3
5	170	4436	665	20	0	-45	922	4.02	4.02	4.02	4.02	2	0.16	0.02	0.12	0.00	0.00	22.3
6	170	4200	646	9	0	-23	925	4.02	4.02	4.02	4.02	2	0.16	0.02	0.12	0.00	0.00	22.3
7	170	4416	643	19	0	-67	919	4.02	4.02	4.02	4.02	2	0.16	0.02	0.11	0.00	0.00	22.3
8	170	4244	656	11	0	-20	925	4.02	4.02	4.02	4.02	2	0.16	0.02	0.12	0.00	0.00	22.3
9	170	4460	652	21	0	-64	920	4.02	4.02	4.02	4.02	2	0.16	0.02	0.12	0.00	0.00	22.3
10	170	4224	634	10	0	-42	923	4.02	4.02	4.02	4.02	2	0.16	0.02	0.11	0.00	0.00	22.3
11	170	4289	633	13	0	-55	921	4.02	4.02	4.02	4.02	2	0.16	0.02	0.11	0.00	0.00	22.3
12	170	4371	666	17	0	-32	923	4.02	4.02	4.02	4.02	2	0.16	0.02	0.12	0.00	0.00	22.3
13	170	4436	665	20	0	-45	922	4.02	4.02	4.02	4.02	2	0.16	0.02	0.12	0.00	0.00	22.3
14	170	4200	646	9	0	-23	925	4.02	4.02	4.02	4.02	2	0.16	0.02	0.12	0.00	0.00	22.3
15	170	4416	643	19	0	-67	919	4.02	4.02	4.02	4.02	2	0.16	0.02	0.11	0.00	0.00	22.3
16	170	4244	656	11	0	-20	925	4.02	4.02	4.02	4.02	2	0.16	0.02	0.12	0.00	0.00	22.3
17	170	4460	652	21	0	-64	920	4.02	4.02	4.02	4.02	2	0.16	0.02	0.12	0.00	0.00	22.3
18	170	6108	782	2	0	-154	1177	4.02	4.02	4.02	4.02	3	0.21	0.02	0.14	0.00	0.00	22.3
19	170	7093	831	83	0	-109	1171	4.02	4.02	4.02	4.02	3	0.21	0.02	0.15	0.00	0.00	22.3
20	170	6747	810	-83	0	-638	1170	4.02	4.02	4.02	4.02	3	0.21	0.02	0.14	0.00	0.00	22.3
37	170	5471	778	-32	0	-145	1187	4.02	4.02	4.02	4.02	3	0.20	0.02	0.14	0.00	0.00	22.3
38	170	7113	859	103	0	-70	1179	4.02	4.02	4.02	4.02	3	0.21	0.02	0.15	0.00	0.00	22.3
39	170	6536	825	-174	0	-952	1175	4.02	4.02	4.02	4.02	3	0.28	0.02	0.15	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	226	5629	359	19	0	-67	1199	4.02	4.02	4.02	4.02	3	0.21	0.01	0.06	0.00	0.00	22.3
2	226	4224	260	10	0	-48	923	4.02	4.02	4.02	4.02	2	0.16	0.01	0.05	0.00	0.00	22.3
3	226	4289	259	13	0	-62	921	4.02	4.02	4.02	4.02	2	0.16	0.01	0.05	0.00	0.00	22.3
4	226	4371	293	17	0	-41	923	4.02	4.02	4.02	4.02	2	0.16	0.01	0.05	0.00	0.00	22.3
5	226	4436	291	20	0	-56	922	4.02	4.02	4.02	4.02	2	0.16	0.01	0.05	0.00	0.00	22.3
6	226	4200	273	9	0	-28	925	4.02	4.02	4.02	4.02	2	0.16	0.01	0.05	0.00	0.00	22.3
7	226	4416	269	19	0	-77	919	4.02	4.02	4.02	4.02	2	0.16	0.01	0.05	0.00	0.00	22.3
8	226	4244	283	11	0	-26	925	4.02	4.02	4.02	4.02	2	0.16	0.01	0.05	0.00	0.00	22.3
9	226	4460	279	21	0	-76	920	4.02	4.02	4.02	4.02	2	0.16	0.01	0.05	0.00	0.00	22.3
10	226	4224	260	10	0	-48	923	4.02	4.02	4.02	4.02	2	0.16	0.01	0.05	0.00	0.00	22.3
11	226	4289	259	13	0	-62	921	4.02	4.02	4.02	4.02	2	0.16	0.01	0.05	0.00	0.00	22.3
12	226	4371	293	17	0	-41	923	4.02	4.02	4.02	4.02	2	0.16	0.01	0.05	0.00	0.00	22.3
13	226	4436	291	20	0	-56	922	4.02	4.02	4.02	4.02	2	0.16	0.01	0.05	0.00	0.00	22.3
14	226	4200	273	9	0	-28	925	4.02	4.02	4.02	4.02	2	0.16	0.01	0.05	0.00	0.00	22.3
15	226	4416	269	19	0	-77	919	4.02	4.02	4.02	4.02	2	0.16	0.01	0.05	0.00	0.00	22.3
16	226	4244	283	11	0	-26	925	4.02	4.02	4.02	4.02	2	0.16	0.01	0.05	0.00	0.00	22.3
17	226	4460	279	21	0	-76	920	4.02	4.02	4.02	4.02	2	0.16	0.01	0.05	0.00	0.00	22.3
18	226	6108	297	2	0	-155	1177	4.02	4.02	4.02	4.02	3	0.21	0.01	0.05	0.00	0.00	22.3
19	226	7093	346	83	0	-156	1171	4.02	4.02	4.02	4.02	3	0.21	0.01	0.06	0.00	0.00	22.3
20	226	6747	325	-83	0	-591	1170	4.02	4.02	4.02	4.02	3	0.21	0.01	0.06	0.00	0.00	22.3
37	226	5471	293	-32	0	-127	1187	4.02	4.02	4.02	4.02	3	0.20	0.01	0.05	0.00	0.00	22.3
38	226	7113	374	103	0	-128	1179	4.02	4.02	4.02	4.02	3	0.21	0.01	0.07	0.00	0.00	22.3
39	226	6536	340	-174	0	-854	1175	4.02	4.02	4.02	4.02	3	0.25	0.01	0.06	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	283	5629	-120	19	0	-78	1199	4.02	4.02	4.02	4.02	3	0.21	0.00	0.02	0.00	0.00	22.3
2	283	4224	-108	10	0	-53	923	4.02	4.02	4.02	4.02	2	0.16	0.00	0.02	0.00	0.00	22.3
3	283	4289	-109	13	0	-70	921	4.02	4.02	4.02	4.02	2	0.16	0.00	0.02	0.00	0.00	22.3
4	283	4371	-76	17	0	-51	923	4.02	4.02	4.02	4.02	2	0.16	0.00	0.01	0.00	0.00	22.3

5	283	4436	-77	20	0	-67	922	4.02	4.02	4.02	4.02	2	0.16	0.00	0.01	0.00	0.00	22.3
6	283	4200	-96	9	0	-33	925	4.02	4.02	4.02	4.02	2	0.16	0.00	0.02	0.00	0.00	22.3
7	283	4416	-99	19	0	-88	919	4.02	4.02	4.02	4.02	2	0.16	0.00	0.02	0.00	0.00	22.3
8	283	4244	-86	11	0	-33	925	4.02	4.02	4.02	4.02	2	0.16	0.00	0.02	0.00	0.00	22.3
9	283	4460	-90	21	0	-87	920	4.02	4.02	4.02	4.02	2	0.16	0.00	0.02	0.00	0.00	22.3
10	283	4224	-108	10	0	-53	923	4.02	4.02	4.02	4.02	2	0.16	0.00	0.02	0.00	0.00	22.3
11	283	4289	-109	13	0	-70	921	4.02	4.02	4.02	4.02	2	0.16	0.00	0.02	0.00	0.00	22.3
12	283	4371	-76	17	0	-51	923	4.02	4.02	4.02	4.02	2	0.16	0.00	0.01	0.00	0.00	22.3
13	283	4436	-77	20	0	-67	922	4.02	4.02	4.02	4.02	2	0.16	0.00	0.01	0.00	0.00	22.3
14	283	4200	-96	9	0	-33	925	4.02	4.02	4.02	4.02	2	0.16	0.00	0.02	0.00	0.00	22.3
15	283	4416	-99	19	0	-88	919	4.02	4.02	4.02	4.02	2	0.16	0.00	0.02	0.00	0.00	22.3
16	283	4244	-86	11	0	-33	925	4.02	4.02	4.02	4.02	2	0.16	0.00	0.02	0.00	0.00	22.3
17	283	4460	-90	21	0	-87	920	4.02	4.02	4.02	4.02	2	0.16	0.00	0.02	0.00	0.00	22.3
18	283	6108	-182	2	0	-156	1177	4.02	4.02	4.02	4.02	3	0.21	0.01	0.03	0.00	0.00	22.3
19	283	7093	-133	83	0	-202	1171	4.02	4.02	4.02	4.02	3	0.21	0.00	0.02	0.00	0.00	22.3
20	283	6747	-154	-83	0	-544	1170	4.02	4.02	4.02	4.02	3	0.21	0.00	0.03	0.00	0.00	22.3
37	283	5471	-186	-32	0	-108	1187	4.02	4.02	4.02	4.02	3	0.20	0.01	0.03	0.00	0.00	22.3
38	283	7113	-105	103	0	-186	1179	4.02	4.02	4.02	4.02	3	0.21	0.00	0.02	0.00	0.00	22.3
39	283	6536	-139	-174	0	-755	1175	4.02	4.02	4.02	4.02	3	0.22	0.01	0.03	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	339	5629	-592	19	0	-89	1199	4.02	4.02	4.02	4.02	3	0.21	0.02	0.11	0.00	0.00	22.3
2	339	4224	-471	10	0	-59	923	4.02	4.02	4.02	4.02	2	0.16	0.01	0.08	0.00	0.00	22.3
3	339	4289	-472	13	0	-77	921	4.02	4.02	4.02	4.02	2	0.16	0.01	0.08	0.00	0.00	22.3
4	339	4371	-439	17	0	-60	923	4.02	4.02	4.02	4.02	2	0.16	0.01	0.08	0.00	0.00	22.3
5	339	4436	-440	20	0	-78	922	4.02	4.02	4.02	4.02	2	0.16	0.01	0.08	0.00	0.00	22.3
6	339	4200	-459	9	0	-38	925	4.02	4.02	4.02	4.02	2	0.16	0.01	0.08	0.00	0.00	22.3
7	339	4416	-462	19	0	-98	919	4.02	4.02	4.02	4.02	2	0.16	0.01	0.08	0.00	0.00	22.3
8	339	4244	-449	11	0	-39	925	4.02	4.02	4.02	4.02	2	0.16	0.01	0.08	0.00	0.00	22.3
9	339	4460	-453	21	0	-99	920	4.02	4.02	4.02	4.02	2	0.16	0.01	0.08	0.00	0.00	22.3
10	339	4224	-471	10	0	-59	923	4.02	4.02	4.02	4.02	2	0.16	0.01	0.08	0.00	0.00	22.3
11	339	4289	-472	13	0	-77	921	4.02	4.02	4.02	4.02	2	0.16	0.01	0.08	0.00	0.00	22.3
12	339	4371	-439	17	0	-60	923	4.02	4.02	4.02	4.02	2	0.16	0.01	0.08	0.00	0.00	22.3
13	339	4436	-440	20	0	-78	922	4.02	4.02	4.02	4.02	2	0.16	0.01	0.08	0.00	0.00	22.3
14	339	4200	-459	9	0	-38	925	4.02	4.02	4.02	4.02	2	0.16	0.01	0.08	0.00	0.00	22.3
15	339	4416	-462	19	0	-98	919	4.02	4.02	4.02	4.02	2	0.16	0.01	0.08	0.00	0.00	22.3
16	339	4244	-449	11	0	-39	925	4.02	4.02	4.02	4.02	2	0.16	0.01	0.08	0.00	0.00	22.3
17	339	4460	-453	21	0	-99	920	4.02	4.02	4.02	4.02	2	0.16	0.01	0.08	0.00	0.00	22.3
18	339	6108	-654	2	0	-157	1177	4.02	4.02	4.02	4.02	3	0.21	0.02	0.12	0.00	0.00	22.3
19	339	7093	-605	83	0	-249	1171	4.02	4.02	4.02	4.02	3	0.21	0.02	0.11	0.00	0.00	22.3
20	339	6747	-626	-83	0	-497	1170	4.02	4.02	4.02	4.02	3	0.21	0.02	0.11	0.00	0.00	22.3
37	339	5471	-658	-32	0	-90	1187	4.02	4.02	4.02	4.02	3	0.20	0.02	0.12	0.00	0.00	22.3
38	339	7113	-577	103	0	-244	1179	4.02	4.02	4.02	4.02	3	0.21	0.02	0.10	0.00	0.00	22.3
39	339	6536	-611	-174	0	-657	1175	4.02	4.02	4.02	4.02	3	0.21	0.02	0.11	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	396	5629	-1056	19	0	-100	1066	4.02	4.02	4.02	4.02	3	0.18	0.03	0.19	0.00	0.00	22.3
2	396	4224	-828	10	0	-65	811	4.02	4.02	4.02	4.02	2	0.14	0.02	0.15	0.00	0.00	22.3
3	396	4289	-829	13	0	-84	809	4.02	4.02	4.02	4.02	2	0.14	0.02	0.15	0.00	0.00	22.3
4	396	4371	-796	17	0	-70	831	4.02	4.02	4.02	4.02	2	0.15	0.02	0.14	0.00	0.00	22.3
5	396	4436	-797	20	0	-89	829	4.02	4.02	4.02	4.02	2	0.15	0.02	0.14	0.00	0.00	22.3
6	396	4200	-816	9	0	-43	821	4.02	4.02	4.02	4.02	2	0.14	0.02	0.15	0.00	0.00	22.3
7	396	4416	-819	19	0	-109	813	4.02	4.02	4.02	4.02	2	0.14	0.02	0.15	0.00	0.00	22.3
8	396	4244	-806	11	0	-45	827	4.02	4.02	4.02	4.02	2	0.14	0.02	0.14	0.00	0.00	22.3
9	396	4460	-810	21	0	-110	820	4.02	4.02	4.02	4.02	2	0.14	0.02	0.14	0.00	0.00	22.3
10	396	4224	-828	10	0	-65	811	4.02	4.02	4.02	4.02	2	0.14	0.02	0.15	0.00	0.00	22.3
11	396	4289	-829	13	0	-84	809	4.02	4.02	4.02	4.02	2	0.14	0.02	0.15	0.00	0.00	22.3
12	396	4371	-796	17	0	-70	831	4.02	4.02	4.02	4.02	2	0.15	0.02	0.14	0.00	0.00	22.3
13	396	4436	-797	20	0	-89	829	4.02	4.02	4.02	4.02	2	0.15	0.02	0.14	0.00	0.00	22.3
14	396	4200	-816	9	0	-43	821	4.02	4.02	4.02	4.02	2	0.14	0.02	0.15	0.00	0.00	22.3
15	396	4416	-819	19	0	-109	813	4.02	4.02	4.02	4.02	2	0.14	0.02	0.15	0.00	0.00	22.3
16	396	4244	-806	11	0	-45	827	4.02	4.02	4.02	4.02	2	0.14	0.02	0.14	0.00	0.00	22.3
17	396	4460	-810	21	0	-110	820	4.02	4.02	4.02	4.02	2	0.14	0.02	0.14	0.00	0.00	22.3
18	396	6108	-1118	2	0	-158	1006	4.02	4.02	4.02	4.02	3	0.18	0.03	0.20	0.00	0.00	22.3
19	396	7093	-1069	83	0	-296	1031	4.02	4.02	4.02	4.02	3	0.19	0.03	0.19	0.00	0.00	22.3
20	396	6747	-1090	-83	0	-450	1016	4.02	4.02	4.02	4.02	3	0.18	0.03	0.19	0.00	0.00	22.3
37	396	5471	-1122	-32	0	-72	1013	4.02	4.02	4.02	4.02	3	0.17	0.03	0.20	0.00	0.00	22.3
38	396	7113	-1041	103	0	-302	1056	4.02	4.02	4.02	4.02	3	0.19	0.03	0.19	0.00	0.00	22.3
39	396	6536	-1075	-174	0	-558	1030	4.02	4.02	4.02	4.02	3	0.18	0.03	0.19	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	452	5629	-1514	19	0	-111	-962	4.02	4.02	4.02	4.02	3	0.17	0.04	0.27	0.00	0.00	22.3
2	452	4224	-1180	10	0	-70	-774	4.02	4.02	4.02	4.02	2	0.13	0.03	0.21	0.00	0.00	22.3
3	452	4289	-1181	13	0	-92	-777	4.02	4.02	4.02	4.02	2	0.14	0.03	0.21	0.00	0.00	22.3
4	452	4371	-1148	17	0	-79	-703	4.02	4.02	4.02	4.02	2	0.12	0.03	0.20	0.00	0.00	22.3
5	452	4436	-1149	20	0	-100	-706	4.02	4.02	4.02	4.02	2	0.12	0.03	0.20	0.00	0.00	22.3
6	452	4200	-1168	9	0	-49	-744	4.02	4.02	4.02	4.02	2	0.13	0.03	0.21	0.00	0.00	22.3
7	452	4416	-1171	19	0	-119	-758	4.02	4.02	4.02	4.02	2	0.13	0.03	0.21	0.00	0.00	22.3
8	452	4244	-1158	11	0	-51	-723	4.02	4.02	4.02	4.02	2	0.13	0.03	0.21	0.00	0.00	22.3
9	452	4460	-1162	21	0	-122	-736	4.02	4.02	4.02	4.02	2	0.13	0.03	0.21	0.00	0.00	22.3
10	452	4224	-1180	10	0	-70	-774	4.02	4.02	4.02	4.02	2	0.13	0.03	0.21	0.00	0.00	22.3
11	452	4289	-1181	13	0	-92	-777	4.02	4.02	4.02	4.02	2	0.14	0.03	0.21	0.00	0.00	22.3
12	452	4371	-1148	17	0	-79	-703	4.02	4.02	4.02	4.02	2	0.12	0.03	0.20	0.00	0.00	22.3
13	452	4436	-1149	20	0	-100	-706	4.02	4.02	4.02	4.02	2	0.12	0.03	0.20	0.00	0.00	22.3
14	452	4200	-1168	9	0	-49	-744	4.02	4.02	4.02	4.02	2	0.13	0.03	0.21	0.00	0.00	22.3
15	452	4416	-1171	19	0	-119	-758	4.02	4.02	4.02	4.02	2	0.13	0.03	0.21	0.00	0.00	22.3
16	452	4244	-1158	11	0	-51	-723	4.02	4.02	4.02	4.02	2	0.13	0.03	0.21	0.00	0.00	22.3
17	452	4460	-1162	21	0	-122	-736	4.02	4.02	4.02	4.02	2	0.13	0.03	0.21	0.00	0.00	22.3
18	452	6108	-1576	2	0	-159	-1120	4.02	4.02	4.02	4.02	3	0.20	0.05	0.28	0.00	0.00	22.3
19	452	7093	-1527	83	0	-343	-1018	4.02	4.02	4.02	4.02	3	0.18	0.04	0.27	0.00	0.00	22.3
20	452	6747	-1548	-83	0	-403	-1065	4.02	4.02	4.02	4.02	3	0.19	0.04	0.28	0.00	0.00	22.3
37	452	5471	-1580	-32	0	-54	-1119	4.02	4.02	4.02	4.02	3	0.19	0.05	0.28	0.00	0.00	22.3
38	452	7113	-1499	103	0	-360	-948	4.02	4.02	4.02	4.02	3	0.17	0.04	0.27	0.00	0.00	22.3
39	452	6536	-1533	-174	0	-460	-1028	4.02	4.02	4.02	4.02	3	0.18	0.04	0.27	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	509	5629	-1965	19	0	-122	-2174	4.02	4.02	4.02	4.02	3	0.37	0.06	0.35	0.00	0.00	22.3
2	509	4224	-1527	10	0	-76	-1715	4.02	4.02	4.02	4.02	2	0.30	0.04	0.27	0.00	0.00	22.3
3	509	4289	-1528	13	0	-99	-1719	4.02	4.02	4.02	4.02	2	0.30	0.04	0.27	0.00	0.00	22.3
4	509	4371	-1495	17	0	-88	-1626	4.02	4.02	4.02	4.02	2	0.28	0.04	0.27	0.00	0.00	22.3
5	509	4436	-1496	20	0	-111	-1629	4.02	4.02	4.02	4.02	2	0.29	0.04	0.27	0.00	0.00	22.3
6	509	4200	-1515	9	0	-54	-1678	4.02	4.02	4.02	4.02	2	0.29	0.04	0.27	0.00	0.00	22.3
7	509	4416	-1518	19	0	-130	-1693	4.02	4.02	4.02	4.02	2	0.30	0.04	0.27	0.00	0.00	22.3
8	509	4244	-1505	11	0	-57	-1651	4.02	4.02	4.02	4.02	2	0.29	0.04	0.27	0.00	0.00	22.3
9	509	4460	-1509	21	0	-134	-1666	4.02	4.02	4.02	4.02	2	0.29	0.04	0.27	0.00	0.00	22.3
10	509	4224	-1527	10	0	-76	-1715	4.02	4.02	4.02	4.02	2	0.30	0.04	0.27	0.00	0.00	22.3

11	509	4289	-1528	13	0	-99	-1719	4.02	4.02	4.02	4.02	2	0.30	0.04	0.27	0.00	0.00	22.3
12	509	4371	-1495	17	0	-88	-1626	4.02	4.02	4.02	4.02	2	0.28	0.04	0.27	0.00	0.00	22.3
13	509	4436	-1496	20	0	-111	-1629	4.02	4.02	4.02	4.02	2	0.29	0.04	0.27	0.00	0.00	22.3
14	509	4200	-1515	9	0	-54	-1678	4.02	4.02	4.02	4.02	2	0.29	0.04	0.27	0.00	0.00	22.3
15	509	4416	-1518	19	0	-130	-1693	4.02	4.02	4.02	4.02	2	0.30	0.04	0.27	0.00	0.00	22.3
16	509	4244	-1505	11	0	-57	-1651	4.02	4.02	4.02	4.02	2	0.29	0.04	0.27	0.00	0.00	22.3
17	509	4460	-1509	21	0	-134	-1666	4.02	4.02	4.02	4.02	2	0.29	0.04	0.27	0.00	0.00	22.3
18	509	6108	-2027	2	0	-160	-2365	4.02	4.02	4.02	4.02	3	0.41	0.06	0.36	0.00	0.00	22.3
19	509	7093	-1978	83	0	-390	-2236	4.02	4.02	4.02	4.02	3	0.40	0.06	0.35	0.00	0.00	22.3
20	509	6747	-1999	-83	0	-355	-2295	4.02	4.02	4.02	4.02	3	0.41	0.06	0.36	0.00	0.00	22.3
37	509	5471	-2031	-32	0	-35	-2367	4.02	4.02	4.02	4.02	3	0.40	0.06	0.36	0.00	0.00	22.3
38	509	7113	-1950	103	0	-419	-2151	4.02	4.02	4.02	4.02	3	0.39	0.06	0.35	0.00	0.00	22.3
39	509	6536	-1984	-174	0	-362	-2250	4.02	4.02	4.02	4.02	3	0.40	0.06	0.35	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	565	5629	-2408	19	0	-133	-2415	4.02	4.02	4.02	4.02	3	0.41	0.07	0.43	0.00	0.00	22.3
2	565	4224	-1868	10	0	-82	-1901	4.02	4.02	4.02	4.02	2	0.33	0.05	0.33	0.00	0.00	22.3
3	565	4289	-1869	13	0	-106	-1905	4.02	4.02	4.02	4.02	2	0.33	0.05	0.33	0.00	0.00	22.3
4	565	4371	-1836	17	0	-98	-1810	4.02	4.02	4.02	4.02	2	0.32	0.05	0.33	0.00	0.00	22.3
5	565	4436	-1837	20	0	-122	-1814	4.02	4.02	4.02	4.02	2	0.32	0.05	0.33	0.00	0.00	22.3
6	565	4200	-1856	9	0	-59	-1863	4.02	4.02	4.02	4.02	2	0.32	0.05	0.33	0.00	0.00	22.3
7	565	4416	-1859	19	0	-141	-1879	4.02	4.02	4.02	4.02	2	0.33	0.05	0.33	0.00	0.00	22.3
8	565	4244	-1846	11	0	-64	-1836	4.02	4.02	4.02	4.02	2	0.32	0.05	0.33	0.00	0.00	22.3
9	565	4460	-1850	21	0	-145	-1851	4.02	4.02	4.02	4.02	2	0.32	0.05	0.33	0.00	0.00	22.3
10	565	4224	-1868	10	0	-82	-1901	4.02	4.02	4.02	4.02	2	0.33	0.05	0.33	0.00	0.00	22.3
11	565	4289	-1869	13	0	-106	-1905	4.02	4.02	4.02	4.02	2	0.33	0.05	0.33	0.00	0.00	22.3
12	565	4371	-1836	17	0	-98	-1810	4.02	4.02	4.02	4.02	2	0.32	0.05	0.33	0.00	0.00	22.3
13	565	4436	-1837	20	0	-122	-1814	4.02	4.02	4.02	4.02	2	0.32	0.05	0.33	0.00	0.00	22.3
14	565	4200	-1856	9	0	-59	-1863	4.02	4.02	4.02	4.02	2	0.32	0.05	0.33	0.00	0.00	22.3
15	565	4416	-1859	19	0	-141	-1879	4.02	4.02	4.02	4.02	2	0.33	0.05	0.33	0.00	0.00	22.3
16	565	4244	-1846	11	0	-64	-1836	4.02	4.02	4.02	4.02	2	0.32	0.05	0.33	0.00	0.00	22.3
17	565	4460	-1850	21	0	-145	-1851	4.02	4.02	4.02	4.02	2	0.32	0.05	0.33	0.00	0.00	22.3
18	565	6108	-2470	2	0	-161	-2610	4.02	4.02	4.02	4.02	3	0.46	0.07	0.44	0.00	0.00	22.3
19	565	7093	-2421	83	0	-436	-2478	4.02	4.02	4.02	4.02	3	0.45	0.07	0.43	0.00	0.00	22.3
20	565	6747	-2442	-83	0	-308	-2538	4.02	4.02	4.02	4.02	3	0.45	0.07	0.43	0.00	0.00	22.3
37	565	5471	-2474	-32	0	-17	-2612	4.02	4.02	4.02	4.02	3	0.45	0.07	0.44	0.00	0.00	22.3
38	565	7113	-2393	103	0	-477	-2391	4.02	4.02	4.02	4.02	3	0.43	0.07	0.43	0.00	0.00	22.3
39	565	6536	-2427	-174	0	-263	-2492	4.02	4.02	4.02	4.02	3	0.44	0.07	0.43	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

Nome travata: **Trave_401_IP1** Descrizione: **Trave_4 7-12-17-22-32**
ASTA NUM. 4 NI 39 NF 26 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y Permanente qy tot.
qy medio: 375.00 160.00 535.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	6603	2687	-266	0	-362	-2903	4.02	4.02	4.02	4.02	3	0.52	0.08	0.48	0.00	0.00	22.3
2	0	4936	2078	-227	0	-292	-2246	4.02	4.02	4.02	4.02	2	0.40	0.06	0.37	0.00	0.00	22.3
3	0	4995	2084	-226	0	-328	-2257	4.02	4.02	4.02	4.02	2	0.40	0.06	0.37	0.00	0.00	22.3
4	0	5163	2049	-184	0	-229	-2208	4.02	4.02	4.02	4.02	2	0.40	0.06	0.36	0.00	0.00	22.3
5	0	5223	2056	-183	0	-265	-2219	4.02	4.02	4.02	4.02	2	0.40	0.06	0.37	0.00	0.00	22.3
6	0	4946	2060	-212	0	-228	-2220	4.02	4.02	4.02	4.02	2	0.40	0.06	0.37	0.00	0.00	22.3
7	0	5144	2081	-211	0	-348	-2257	4.02	4.02	4.02	4.02	2	0.41	0.06	0.37	0.00	0.00	22.3
8	0	5014	2052	-199	0	-209	-2208	4.02	4.02	4.02	4.02	2	0.40	0.06	0.37	0.00	0.00	22.3
9	0	5213	2073	-198	0	-329	-2245	4.02	4.02	4.02	4.02	2	0.40	0.06	0.37	0.00	0.00	22.3
10	0	4936	2078	-227	0	-292	-2246	4.02	4.02	4.02	4.02	2	0.40	0.06	0.37	0.00	0.00	22.3
11	0	4995	2084	-226	0	-328	-2257	4.02	4.02	4.02	4.02	2	0.40	0.06	0.37	0.00	0.00	22.3
12	0	5163	2049	-184	0	-229	-2208	4.02	4.02	4.02	4.02	2	0.40	0.06	0.36	0.00	0.00	22.3
13	0	5223	2056	-183	0	-265	-2219	4.02	4.02	4.02	4.02	2	0.40	0.06	0.37	0.00	0.00	22.3
14	0	4946	2060	-212	0	-228	-2220	4.02	4.02	4.02	4.02	2	0.40	0.06	0.37	0.00	0.00	22.3
15	0	5144	2081	-211	0	-348	-2257	4.02	4.02	4.02	4.02	2	0.41	0.06	0.37	0.00	0.00	22.3
16	0	5014	2052	-199	0	-209	-2208	4.02	4.02	4.02	4.02	2	0.40	0.06	0.37	0.00	0.00	22.3
17	0	5213	2073	-198	0	-329	-2245	4.02	4.02	4.02	4.02	2	0.40	0.06	0.37	0.00	0.00	22.3
18	0	6562	2856	-603	0	-804	-3207	4.02	4.02	4.02	4.02	3	0.57	0.08	0.51	0.00	0.00	22.3
19	0	8282	2696	-420	0	-564	-2849	4.02	4.02	4.02	4.02	3	0.54	0.08	0.48	0.00	0.00	22.3
20	0	7584	2808	-676	0	-1017	-3099	4.02	4.02	4.02	4.02	3	0.57	0.08	0.50	0.00	0.00	22.3
37	0	5739	2882	-583	0	-776	-3288	4.02	4.02	4.02	4.02	3	0.57	0.08	0.51	0.00	0.00	22.3
38	0	8606	2614	-278	0	-376	-2691	4.02	4.02	4.02	4.02	3	0.52	0.08	0.47	0.00	0.00	22.3
39	0	7441	2802	-706	0	-1131	-3108	4.02	4.02	4.02	4.02	3	0.57	0.08	0.50	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	56	6603	2252	-266	0	-212	-2648	4.02	4.02	4.02	4.02	3	0.47	0.07	0.40	0.00	0.00	22.3
2	56	4936	1743	-227	0	-164	-2050	4.02	4.02	4.02	4.02	2	0.37	0.05	0.31	0.00	0.00	22.3
3	56	4995	1749	-226	0	-200	-2060	4.02	4.02	4.02	4.02	2	0.37	0.05	0.31	0.00	0.00	22.3
4	56	5163	1714	-184	0	-125	-2013	4.02	4.02	4.02	4.02	2	0.36	0.05	0.31	0.00	0.00	22.3
5	56	5223	1721	-183	0	-161	-2024	4.02	4.02	4.02	4.02	2	0.36	0.05	0.31	0.00	0.00	22.3
6	56	4946	1725	-212	0	-108	-2024	4.02	4.02	4.02	4.02	2	0.36	0.05	0.31	0.00	0.00	22.3
7	56	5144	1746	-211	0	-229	-2060	4.02	4.02	4.02	4.02	2	0.37	0.05	0.31	0.00	0.00	22.3
8	56	5014	1717	-199	0	-97	-2013	4.02	4.02	4.02	4.02	2	0.36	0.05	0.31	0.00	0.00	22.3
9	56	5213	1738	-198	0	-217	-2049	4.02	4.02	4.02	4.02	2	0.37	0.05	0.31	0.00	0.00	22.3
10	56	4936	1743	-227	0	-164	-2050	4.02	4.02	4.02	4.02	2	0.37	0.05	0.31	0.00	0.00	22.3
11	56	4995	1749	-226	0	-200	-2060	4.02	4.02	4.02	4.02	2	0.37	0.05	0.31	0.00	0.00	22.3
12	56	5163	1714	-184	0	-125	-2013	4.02	4.02	4.02	4.02	2	0.36	0.05	0.31	0.00	0.00	22.3
13	56	5223	1721	-183	0	-161	-2024	4.02	4.02	4.02	4.02	2	0.36	0.05	0.31	0.00	0.00	22.3
14	56	4946	1725	-212	0	-108	-2024	4.02	4.02	4.02	4.02	2	0.36	0.05	0.31	0.00	0.00	22.3
15	56	5144	1746	-211	0	-229	-2060	4.02	4.02	4.02	4.02	2	0.37	0.05	0.31	0.00	0.00	22.3
16	56	5014	1717	-199	0	-97	-2013	4.02	4.02	4.02	4.02	2	0.36	0.05	0.31	0.00	0.00	22.3
17	56	5213	1738	-198	0	-217	-2049	4.02	4.02	4.02	4.02	2	0.37	0.05	0.31	0.00	0.00	22.3
18	56	6562	2421	-603	0	-464	-2942	4.02	4.02	4.02	4.02	3	0.52	0.07	0.43	0.00	0.00	22.3
19	56	8282	2261	-420	0	-327	-2594	4.02	4.02	4.02	4.02	3	0.49	0.07	0.40	0.00	0.00	22.3
20	56	7584	2373	-676	0	-635	-2837	4.02	4.02	4.02	4.02	3	0.52	0.07	0.42	0.00	0.00	22.3
37	56	5739	2447	-583	0	-447	-3022	4.02	4.02	4.02	4.02	3	0.52	0.07	0.44	0.00	0.00	22.3
38	56	8606	2179	-278	0	-219	-2440	4.02	4.02	4.02	4.02	3	0.47	0.06	0.39	0.00	0.00	22.3
39	56	7441	2367	-706	0	-732	-2847	4.02	4.02	4.02	4.02	3	0.52	0.07	0.42	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	113	6603	1826	-266	0	-61	-1281	4.02	4.02	4.02	4.02	3	0.23	0.05	0.33	0.00	0.00	22.3
2	113	4936	1416	-227	0	-36	-992	4.02	4.02	4.02	4.02	2	0.18	0.04	0.25	0.00	0.00	22.3

3	113	4995	1422	-226	0	-73	-999	4.02	4.02	4.02	4.02	2	0.18	0.04	0.25	0.00	0.00	22.3
4	113	5163	1387	-184	0	-21	-971	4.02	4.02	4.02	4.02	2	0.17	0.04	0.25	0.00	0.00	22.3
5	113	5223	1394	-183	0	-58	-978	4.02	4.02	4.02	4.02	2	0.18	0.04	0.25	0.00	0.00	22.3
6	113	4946	1398	-212	0	11	-976	4.02	4.02	4.02	4.02	2	0.17	0.04	0.25	0.00	0.00	22.3
7	113	5144	1419	-211	0	-110	-1000	4.02	4.02	4.02	4.02	2	0.18	0.04	0.25	0.00	0.00	22.3
8	113	5014	1390	-199	0	16	-970	4.02	4.02	4.02	4.02	2	0.17	0.04	0.25	0.00	0.00	22.3
9	113	5213	1411	-198	0	-105	-994	4.02	4.02	4.02	4.02	2	0.18	0.04	0.25	0.00	0.00	22.3
10	113	4936	1416	-227	0	-36	-992	4.02	4.02	4.02	4.02	2	0.18	0.04	0.25	0.00	0.00	22.3
11	113	4995	1422	-226	0	-73	-999	4.02	4.02	4.02	4.02	2	0.18	0.04	0.25	0.00	0.00	22.3
12	113	5163	1387	-184	0	-21	-971	4.02	4.02	4.02	4.02	2	0.17	0.04	0.25	0.00	0.00	22.3
13	113	5223	1394	-183	0	-58	-978	4.02	4.02	4.02	4.02	2	0.18	0.04	0.25	0.00	0.00	22.3
14	113	4946	1398	-212	0	11	-976	4.02	4.02	4.02	4.02	2	0.17	0.04	0.25	0.00	0.00	22.3
15	113	5144	1419	-211	0	-110	-1000	4.02	4.02	4.02	4.02	2	0.18	0.04	0.25	0.00	0.00	22.3
16	113	5014	1390	-199	0	16	-970	4.02	4.02	4.02	4.02	2	0.17	0.04	0.25	0.00	0.00	22.3
17	113	5213	1411	-198	0	-105	-994	4.02	4.02	4.02	4.02	2	0.18	0.04	0.25	0.00	0.00	22.3
18	113	6562	1995	-603	0	-123	-1480	4.02	4.02	4.02	4.02	3	0.26	0.06	0.36	0.00	0.00	22.3
19	113	8282	1835	-420	0	-90	-1222	4.02	4.02	4.02	4.02	3	0.23	0.05	0.33	0.00	0.00	22.3
20	113	7584	1947	-676	0	-253	-1402	4.02	4.02	4.02	4.02	3	0.26	0.06	0.35	0.00	0.00	22.3
37	113	5739	2021	-583	0	-118	-1545	4.02	4.02	4.02	4.02	3	0.27	0.06	0.36	0.00	0.00	22.3
38	113	8606	1753	-278	0	-62	-1115	4.02	4.02	4.02	4.02	3	0.21	0.05	0.31	0.00	0.00	22.3
39	113	7441	1941	-706	0	-333	-1415	4.02	4.02	4.02	4.02	3	0.26	0.06	0.35	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	169	6603	1409	-266	0	90	1270	4.02	4.02	4.02	4.02	3	0.23	0.04	0.25	0.00	0.00	22.3
2	169	4936	1095	-227	0	92	988	4.02	4.02	4.02	4.02	2	0.18	0.03	0.20	0.00	0.00	22.3
3	169	4995	1101	-226	0	55	990	4.02	4.02	4.02	4.02	2	0.18	0.03	0.20	0.00	0.00	22.3
4	169	5163	1066	-184	0	82	964	4.02	4.02	4.02	4.02	2	0.17	0.03	0.19	0.00	0.00	22.3
5	169	5223	1073	-183	0	46	967	4.02	4.02	4.02	4.02	2	0.17	0.03	0.19	0.00	0.00	22.3
6	169	4946	1077	-212	0	131	976	4.02	4.02	4.02	4.02	2	0.17	0.03	0.19	0.00	0.00	22.3
7	169	5144	1098	-211	0	9	985	4.02	4.02	4.02	4.02	2	0.18	0.03	0.20	0.00	0.00	22.3
8	169	5014	1069	-199	0	128	969	4.02	4.02	4.02	4.02	2	0.17	0.03	0.19	0.00	0.00	22.3
9	169	5213	1090	-198	0	7	978	4.02	4.02	4.02	4.02	2	0.18	0.03	0.19	0.00	0.00	22.3
10	169	4936	1095	-227	0	92	988	4.02	4.02	4.02	4.02	2	0.18	0.03	0.20	0.00	0.00	22.3
11	169	4995	1101	-226	0	55	990	4.02	4.02	4.02	4.02	2	0.18	0.03	0.20	0.00	0.00	22.3
12	169	5163	1066	-184	0	82	964	4.02	4.02	4.02	4.02	2	0.17	0.03	0.19	0.00	0.00	22.3
13	169	5223	1073	-183	0	46	967	4.02	4.02	4.02	4.02	2	0.17	0.03	0.19	0.00	0.00	22.3
14	169	4946	1077	-212	0	131	976	4.02	4.02	4.02	4.02	2	0.17	0.03	0.19	0.00	0.00	22.3
15	169	5144	1098	-211	0	9	985	4.02	4.02	4.02	4.02	2	0.18	0.03	0.20	0.00	0.00	22.3
16	169	5014	1069	-199	0	128	969	4.02	4.02	4.02	4.02	2	0.17	0.03	0.19	0.00	0.00	22.3
17	169	5213	1090	-198	0	7	978	4.02	4.02	4.02	4.02	2	0.18	0.03	0.19	0.00	0.00	22.3
18	169	6562	1578	-603	0	217	1338	4.02	4.02	4.02	4.02	3	0.24	0.05	0.28	0.00	0.00	22.3
19	169	8282	1418	-420	0	148	1343	4.02	4.02	4.02	4.02	3	0.25	0.04	0.25	0.00	0.00	22.3
20	169	7584	1531	-676	0	130	1341	4.02	4.02	4.02	4.02	3	0.25	0.04	0.27	0.00	0.00	22.3
37	169	5739	1604	-583	0	212	1314	4.02	4.02	4.02	4.02	3	0.23	0.05	0.29	0.00	0.00	22.3
38	169	8606	1337	-278	0	95	1322	4.02	4.02	4.02	4.02	3	0.25	0.04	0.24	0.00	0.00	22.3
39	169	7441	1524	-706	0	65	1318	4.02	4.02	4.02	4.02	3	0.24	0.04	0.27	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	226	6603	1002	-266	0	240	1744	4.02	4.02	4.02	4.02	3	0.31	0.03	0.18	0.00	0.00	22.3
2	226	4936	782	-227	0	220	1359	4.02	4.02	4.02	4.02	2	0.24	0.02	0.14	0.00	0.00	22.3
3	226	4995	788	-226	0	183	1365	4.02	4.02	4.02	4.02	2	0.24	0.02	0.14	0.00	0.00	22.3
4	226	5163	753	-184	0	186	1319	4.02	4.02	4.02	4.02	2	0.24	0.02	0.13	0.00	0.00	22.3
5	226	5223	760	-183	0	149	1326	4.02	4.02	4.02	4.02	2	0.24	0.02	0.14	0.00	0.00	22.3
6	226	4946	764	-212	0	251	1337	4.02	4.02	4.02	4.02	2	0.24	0.02	0.14	0.00	0.00	22.3
7	226	5144	785	-211	0	129	1358	4.02	4.02	4.02	4.02	2	0.24	0.02	0.14	0.00	0.00	22.3
8	226	5014	756	-199	0	241	1326	4.02	4.02	4.02	4.02	2	0.24	0.02	0.13	0.00	0.00	22.3
9	226	5213	777	-198	0	118	1347	4.02	4.02	4.02	4.02	2	0.24	0.02	0.14	0.00	0.00	22.3
10	226	4936	782	-227	0	220	1359	4.02	4.02	4.02	4.02	2	0.24	0.02	0.14	0.00	0.00	22.3
11	226	4995	788	-226	0	183	1365	4.02	4.02	4.02	4.02	2	0.24	0.02	0.14	0.00	0.00	22.3
12	226	5163	753	-184	0	186	1319	4.02	4.02	4.02	4.02	2	0.24	0.02	0.13	0.00	0.00	22.3
13	226	5223	760	-183	0	149	1326	4.02	4.02	4.02	4.02	2	0.24	0.02	0.14	0.00	0.00	22.3
14	226	4946	764	-212	0	251	1337	4.02	4.02	4.02	4.02	2	0.24	0.02	0.14	0.00	0.00	22.3
15	226	5144	785	-211	0	129	1358	4.02	4.02	4.02	4.02	2	0.24	0.02	0.14	0.00	0.00	22.3
16	226	5014	756	-199	0	241	1326	4.02	4.02	4.02	4.02	2	0.24	0.02	0.13	0.00	0.00	22.3
17	226	5213	777	-198	0	118	1347	4.02	4.02	4.02	4.02	2	0.24	0.02	0.14	0.00	0.00	22.3
18	226	6562	1171	-603	0	558	1909	4.02	4.02	4.02	4.02	3	0.34	0.03	0.21	0.00	0.00	22.3
19	226	8282	1011	-420	0	385	1823	4.02	4.02	4.02	4.02	3	0.35	0.03	0.18	0.00	0.00	22.3
20	226	7584	1124	-676	0	512	1884	4.02	4.02	4.02	4.02	3	0.35	0.03	0.20	0.00	0.00	22.3
37	226	5739	1197	-583	0	541	1899	4.02	4.02	4.02	4.02	3	0.33	0.03	0.21	0.00	0.00	22.3
38	226	8606	930	-278	0	253	1755	4.02	4.02	4.02	4.02	3	0.34	0.03	0.17	0.00	0.00	22.3
39	226	7441	1117	-706	0	464	1857	4.02	4.02	4.02	4.02	3	0.34	0.03	0.20	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	282	6603	604	-266	0	391	1937	4.02	4.02	4.02	4.02	3	0.34	0.02	0.11	0.00	0.00	22.3
2	282	4936	476	-227	0	348	1520	4.02	4.02	4.02	4.02	2	0.27	0.01	0.08	0.00	0.00	22.3
3	282	4995	482	-226	0	311	1533	4.02	4.02	4.02	4.02	2	0.27	0.01	0.09	0.00	0.00	22.3
4	282	5163	447	-184	0	290	1447	4.02	4.02	4.02	4.02	2	0.26	0.01	0.08	0.00	0.00	22.3
5	282	5223	454	-183	0	253	1460	4.02	4.02	4.02	4.02	2	0.26	0.01	0.08	0.00	0.00	22.3
6	282	4946	458	-212	0	371	1478	4.02	4.02	4.02	4.02	2	0.26	0.01	0.08	0.00	0.00	22.3
7	282	5144	479	-211	0	248	1524	4.02	4.02	4.02	4.02	2	0.27	0.01	0.09	0.00	0.00	22.3
8	282	5014	450	-199	0	353	1456	4.02	4.02	4.02	4.02	2	0.26	0.01	0.08	0.00	0.00	22.3
9	282	5213	471	-198	0	230	1502	4.02	4.02	4.02	4.02	2	0.27	0.01	0.08	0.00	0.00	22.3
10	282	4936	476	-227	0	348	1520	4.02	4.02	4.02	4.02	2	0.27	0.01	0.08	0.00	0.00	22.3
11	282	4995	482	-226	0	311	1533	4.02	4.02	4.02	4.02	2	0.27	0.01	0.09	0.00	0.00	22.3
12	282	5163	447	-184	0	290	1447	4.02	4.02	4.02	4.02	2	0.26	0.01	0.08	0.00	0.00	22.3
13	282	5223	454	-183	0	253	1460	4.02	4.02	4.02	4.02	2	0.26	0.01	0.08	0.00	0.00	22.3
14	282	4946	458	-212	0	371	1478	4.02	4.02	4.02	4.02	2	0.26	0.01	0.08	0.00	0.00	22.3
15	282	5144	479	-211	0	248	1524	4.02	4.02	4.02	4.02	2	0.27	0.01	0.09	0.00	0.00	22.3
16	282	5014	450	-199	0	353	1456	4.02	4.02	4.02	4.02	2	0.26	0.01	0.08	0.00	0.00	22.3
17	282	5213	471	-198	0	230	1502	4.02	4.02	4.02	4.02	2	0.27	0.01	0.08	0.00	0.00	22.3
18	282	6562	773	-603	0	898	2256	4.02	4.02	4.02	4.02	3	0.40	0.02	0.14	0.00	0.00	22.3
19	282	8282	613	-420	0	622	2025	4.02	4.02	4.02	4.02	3	0.38	0.02	0.11	0.00	0.00	22.3
20	282	7584	726	-676	0	894	2205	4.02	4.02	4.02	4.02	3	0.41	0.02	0.13	0.00	0.00	22.3
37	282	5739	799	-583	0	870	2261	4.02	4.02	4.02	4.02	3	0.39	0.02	0.14	0.00	0.00	22.3
38	282	8606	532	-278	0	410	1887	4.02	4.02	4.02	4.02	3	0.36	0.02	0.09	0.00	0.00	22.3
39	282	7441	719	-706	0	863	2174	4.02	4.02	4.02	4.02	3	0.40	0.02	0.13	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	339	6603	216	-266	0	542	1937	4.02	4.02	4.02	4.02	3	0.34	0.01	0.04	0.00	0.00	22.3
2	339	4936	177	-227	0	476	1520	4.02	4.02	4.02	4.02	2	0.27	0.01	0.04	0.00	0.00	22.3
3	339	4995	183	-226	0	439	1533	4.02	4.02	4.02	4.02	2	0.27	0.01	0.04	0.00	0.00	22.3
4	339	5163	149	-184	0	394	1447	4.02	4.02	4.02	4.02	2	0.26	0.01	0.03	0.00	0.00	22.3
5	339	5223	155	-183	0	357	1460	4.02	4.02	4.02	4.02	2	0.26	0.01	0.03	0.00	0.00	22.3
6	339	4946	160	-212	0	491	1478	4.02	4.02	4.02	4.02	2	0.26	0.01	0.03	0.00	0.00	22.3
7	339	5144	181	-211	0	367	1524	4.02	4.02	4.02	4.02	2	0.27	0.01	0.03	0.00	0.00	22.3
8	339	5014	152	-199	0	466	1456	4.02	4.02	4.02	4.02	2	0.26	0.01	0.03	0.00	0.00	22.3

9	339	5213	173	-198	0	342	1502	4.02	4.02	4.02	4.02	2	0.27	0.01	0.03	0.00	0.00	22.3
10	339	4936	177	-227	0	476	1520	4.02	4.02	4.02	4.02	2	0.27	0.01	0.04	0.00	0.00	22.3
11	339	4995	183	-226	0	439	1533	4.02	4.02	4.02	4.02	2	0.27	0.01	0.04	0.00	0.00	22.3
12	339	5163	149	-184	0	394	1447	4.02	4.02	4.02	4.02	2	0.26	0.01	0.03	0.00	0.00	22.3
13	339	5223	155	-183	0	357	1460	4.02	4.02	4.02	4.02	2	0.26	0.01	0.03	0.00	0.00	22.3
14	339	4946	160	-212	0	491	1478	4.02	4.02	4.02	4.02	2	0.26	0.01	0.03	0.00	0.00	22.3
15	339	5144	181	-211	0	367	1524	4.02	4.02	4.02	4.02	2	0.27	0.01	0.03	0.00	0.00	22.3
16	339	5014	152	-199	0	466	1456	4.02	4.02	4.02	4.02	2	0.26	0.01	0.03	0.00	0.00	22.3
17	339	5213	173	-198	0	342	1502	4.02	4.02	4.02	4.02	2	0.27	0.01	0.03	0.00	0.00	22.3
18	339	6562	385	-603	0	1238	2302	4.02	4.02	4.02	4.02	3	0.41	0.02	0.10	0.00	0.00	22.3
19	339	8282	225	-420	0	859	2025	4.02	4.02	4.02	4.02	3	0.38	0.01	0.07	0.00	0.00	22.3
20	339	7584	338	-676	0	1276	2220	4.02	4.02	4.02	4.02	3	0.41	0.02	0.11	0.00	0.00	22.3
37	339	5739	411	-583	0	1200	2323	4.02	4.02	4.02	4.02	3	0.40	0.02	0.09	0.00	0.00	22.3
38	339	8606	144	-278	0	567	1887	4.02	4.02	4.02	4.02	3	0.36	0.01	0.04	0.00	0.00	22.3
39	339	7441	331	-706	0	1262	2186	4.02	4.02	4.02	4.02	3	0.40	0.02	0.11	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	395	6603	-163	-266	0	692	1937	4.02	4.02	4.02	4.02	3	0.34	0.01	0.04	0.00	0.00	22.3
2	395	4936	-114	-227	0	604	1520	4.02	4.02	4.02	4.02	2	0.27	0.01	0.04	0.00	0.00	22.3
3	395	4995	-108	-226	0	567	1533	4.02	4.02	4.02	4.02	2	0.27	0.01	0.04	0.00	0.00	22.3
4	395	5163	-143	-184	0	498	1447	4.02	4.02	4.02	4.02	2	0.26	0.01	0.03	0.00	0.00	22.3
5	395	5223	-136	-183	0	460	1460	4.02	4.02	4.02	4.02	2	0.26	0.01	0.03	0.00	0.00	22.3
6	395	4946	-132	-212	0	611	1478	4.02	4.02	4.02	4.02	2	0.26	0.01	0.03	0.00	0.00	22.3
7	395	5144	-111	-211	0	486	1524	4.02	4.02	4.02	4.02	2	0.27	0.01	0.03	0.00	0.00	22.3
8	395	5014	-140	-199	0	578	1456	4.02	4.02	4.02	4.02	2	0.26	0.01	0.03	0.00	0.00	22.3
9	395	5213	-119	-198	0	454	1502	4.02	4.02	4.02	4.02	2	0.27	0.01	0.03	0.00	0.00	22.3
10	395	4936	-114	-227	0	604	1520	4.02	4.02	4.02	4.02	2	0.27	0.01	0.04	0.00	0.00	22.3
11	395	4995	-108	-226	0	567	1533	4.02	4.02	4.02	4.02	2	0.27	0.01	0.04	0.00	0.00	22.3
12	395	5163	-143	-184	0	498	1447	4.02	4.02	4.02	4.02	2	0.26	0.01	0.03	0.00	0.00	22.3
13	395	5223	-136	-183	0	460	1460	4.02	4.02	4.02	4.02	2	0.26	0.01	0.03	0.00	0.00	22.3
14	395	4946	-132	-212	0	611	1478	4.02	4.02	4.02	4.02	2	0.26	0.01	0.03	0.00	0.00	22.3
15	395	5144	-111	-211	0	486	1524	4.02	4.02	4.02	4.02	2	0.27	0.01	0.03	0.00	0.00	22.3
16	395	5014	-140	-199	0	578	1456	4.02	4.02	4.02	4.02	2	0.26	0.01	0.03	0.00	0.00	22.3
17	395	5213	-119	-198	0	454	1502	4.02	4.02	4.02	4.02	2	0.27	0.01	0.03	0.00	0.00	22.3
18	395	6562	6	-603	0	1579	2302	4.02	4.02	4.02	4.02	3	0.47	0.02	0.10	0.00	0.00	22.3
19	395	8282	-154	-420	0	1096	2025	4.02	4.02	4.02	4.02	3	0.38	0.01	0.07	0.00	0.00	22.3
20	395	7584	-41	-676	0	1658	2220	4.02	4.02	4.02	4.02	3	0.51	0.02	0.11	0.00	0.00	22.3
37	395	5739	32	-583	0	1529	2323	4.02	4.02	4.02	4.02	3	0.44	0.02	0.09	0.00	0.00	22.3
38	395	8606	-235	-278	0	724	1887	4.02	4.02	4.02	4.02	3	0.36	0.01	0.04	0.00	0.00	22.3
39	395	7441	-48	-706	0	1661	2186	4.02	4.02	4.02	4.02	3	0.51	0.02	0.11	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	452	6603	-532	-266	0	843	1937	4.02	4.02	4.02	4.02	3	0.34	0.02	0.09	0.00	0.00	22.3
2	452	4936	-398	-227	0	732	1520	4.02	4.02	4.02	4.02	2	0.27	0.01	0.07	0.00	0.00	22.3
3	452	4995	-392	-226	0	695	1533	4.02	4.02	4.02	4.02	2	0.27	0.01	0.07	0.00	0.00	22.3
4	452	5163	-427	-184	0	601	1447	4.02	4.02	4.02	4.02	2	0.26	0.01	0.08	0.00	0.00	22.3
5	452	5223	-420	-183	0	564	1460	4.02	4.02	4.02	4.02	2	0.26	0.01	0.07	0.00	0.00	22.3
6	452	4946	-416	-212	0	730	1478	4.02	4.02	4.02	4.02	2	0.26	0.01	0.07	0.00	0.00	22.3
7	452	5144	-395	-211	0	605	1524	4.02	4.02	4.02	4.02	2	0.27	0.01	0.07	0.00	0.00	22.3
8	452	5014	-424	-199	0	691	1456	4.02	4.02	4.02	4.02	2	0.26	0.01	0.08	0.00	0.00	22.3
9	452	5213	-403	-198	0	566	1502	4.02	4.02	4.02	4.02	2	0.27	0.01	0.07	0.00	0.00	22.3
10	452	4936	-398	-227	0	732	1520	4.02	4.02	4.02	4.02	2	0.27	0.01	0.07	0.00	0.00	22.3
11	452	4995	-392	-226	0	695	1533	4.02	4.02	4.02	4.02	2	0.27	0.01	0.07	0.00	0.00	22.3
12	452	5163	-427	-184	0	601	1447	4.02	4.02	4.02	4.02	2	0.26	0.01	0.08	0.00	0.00	22.3
13	452	5223	-420	-183	0	564	1460	4.02	4.02	4.02	4.02	2	0.26	0.01	0.07	0.00	0.00	22.3
14	452	4946	-416	-212	0	730	1478	4.02	4.02	4.02	4.02	2	0.26	0.01	0.07	0.00	0.00	22.3
15	452	5144	-395	-211	0	605	1524	4.02	4.02	4.02	4.02	2	0.27	0.01	0.07	0.00	0.00	22.3
16	452	5014	-424	-199	0	691	1456	4.02	4.02	4.02	4.02	2	0.26	0.01	0.08	0.00	0.00	22.3
17	452	5213	-403	-198	0	566	1502	4.02	4.02	4.02	4.02	2	0.27	0.01	0.07	0.00	0.00	22.3
18	452	6562	-363	-603	0	1919	2302	4.02	4.02	4.02	4.02	3	0.57	0.02	0.10	0.00	0.00	22.3
19	452	8282	-523	-420	0	1334	2025	4.02	4.02	4.02	4.02	3	0.42	0.02	0.09	0.00	0.00	22.3
20	452	7584	-410	-676	0	2041	2220	4.02	4.02	4.02	4.02	3	0.63	0.02	0.11	0.00	0.00	22.3
37	452	5739	-337	-583	0	1858	2323	4.02	4.02	4.02	4.02	3	0.54	0.02	0.09	0.00	0.00	22.3
38	452	8606	-604	-278	0	882	1887	4.02	4.02	4.02	4.02	3	0.36	0.02	0.11	0.00	0.00	22.3
39	452	7441	-417	-706	0	2059	2186	4.02	4.02	4.02	4.02	3	0.63	0.02	0.11	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	508	6603	-892	-266	0	993	1789	4.02	4.02	4.02	4.02	3	0.32	0.03	0.16	0.00	0.00	22.3
2	508	4936	-675	-227	0	861	1412	4.02	4.02	4.02	4.02	2	0.28	0.02	0.12	0.00	0.00	22.3
3	508	4995	-669	-226	0	823	1430	4.02	4.02	4.02	4.02	2	0.27	0.02	0.12	0.00	0.00	22.3
4	508	5163	-704	-184	0	705	1322	4.02	4.02	4.02	4.02	2	0.24	0.02	0.13	0.00	0.00	22.3
5	508	5223	-697	-183	0	667	1340	4.02	4.02	4.02	4.02	2	0.24	0.02	0.12	0.00	0.00	22.3
6	508	4946	-693	-212	0	850	1360	4.02	4.02	4.02	4.02	2	0.28	0.02	0.12	0.00	0.00	22.3
7	508	5144	-672	-211	0	724	1419	4.02	4.02	4.02	4.02	2	0.26	0.02	0.12	0.00	0.00	22.3
8	508	5014	-701	-199	0	803	1333	4.02	4.02	4.02	4.02	2	0.26	0.02	0.12	0.00	0.00	22.3
9	508	5213	-680	-198	0	678	1392	4.02	4.02	4.02	4.02	2	0.25	0.02	0.12	0.00	0.00	22.3
10	508	4936	-675	-227	0	861	1412	4.02	4.02	4.02	4.02	2	0.28	0.02	0.12	0.00	0.00	22.3
11	508	4995	-669	-226	0	823	1430	4.02	4.02	4.02	4.02	2	0.27	0.02	0.12	0.00	0.00	22.3
12	508	5163	-704	-184	0	705	1322	4.02	4.02	4.02	4.02	2	0.24	0.02	0.13	0.00	0.00	22.3
13	508	5223	-697	-183	0	667	1340	4.02	4.02	4.02	4.02	2	0.24	0.02	0.12	0.00	0.00	22.3
14	508	4946	-693	-212	0	850	1360	4.02	4.02	4.02	4.02	2	0.28	0.02	0.12	0.00	0.00	22.3
15	508	5144	-672	-211	0	724	1419	4.02	4.02	4.02	4.02	2	0.26	0.02	0.12	0.00	0.00	22.3
16	508	5014	-701	-199	0	803	1333	4.02	4.02	4.02	4.02	2	0.26	0.02	0.12	0.00	0.00	22.3
17	508	5213	-680	-198	0	678	1392	4.02	4.02	4.02	4.02	2	0.25	0.02	0.12	0.00	0.00	22.3
18	508	6562	-723	-603	0	2260	2260	4.02	4.02	4.02	4.02	3	0.67	0.02	0.13	0.00	0.00	22.3
19	508	8282	-883	-420	0	1571	1883	4.02	4.02	4.02	4.02	3	0.49	0.03	0.16	0.00	0.00	22.3
20	508	7584	-770	-676	0	2423	2148	4.02	4.02	4.02	4.02	3	0.74	0.02	0.14	0.00	0.00	22.3
37	508	5739	-697	-583	0	2188	2296	4.02	4.02	4.02	4.02	3	0.63	0.02	0.12	0.00	0.00	22.3
38	508	8606	-964	-278	0	1039	1668	4.02	4.02	4.02	4.02	3	0.33	0.03	0.17	0.00	0.00	22.3
39	508	7441	-777	-706	0	2458	2110	4.02	4.02	4.02	4.02	3	0.75	0.02	0.14	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	565	6603	-1243	-266	0	1144	1363	4.02	4.02	4.02	4.02	3	0.34	0.04	0.22	0.00	0.00	22.3
2	565	4936	-945	-227	0	989	1091	4.02	4.02	4.02	4.02	2	0.32	0.03	0.17	0.00	0.00	22.3
3	565	4995	-939	-226	0	951	1112	4.02	4.02	4.02	4.02	2	0.31	0.03	0.17	0.00	0.00	22.3
4	565	5163	-973	-184	0	809	985	4.02	4.02	4.02	4.02	2	0.27	0.03	0.17	0.00	0.00	22.3
5	565	5223	-967	-183	0	771	1006	4.02	4.02	4.02	4.02	2	0.26	0.03	0.17	0.00	0.00	22.3
6	565	4946	-962	-212	0	970	1029	4.02	4.02	4.02	4.02	2	0.32	0.03	0.17	0.00	0.00	22.3
7	565	5144	-941	-211	0	843	1100	4.02	4.02	4.02	4.02	2	0.28	0.03	0.17	0.00	0.00	22.3
8	565	5014	-971	-199	0	916	997	4.02	4.02	4.02	4.02	2	0.30	0.03	0.17	0.00	0.00	22.3
9	565	5213	-950	-198	0	789	1068	4.02	4.02	4.02	4.02	2	0.26	0.03	0.17	0.00	0.00	22.3
10	565	4936	-945	-227	0	989	1091	4.02	4.02	4.02	4.02	2	0.32	0.03	0.17	0.00	0.00	22.3
11	565	4995	-939	-226	0	951	1112	4.02	4.02	4.02	4.02	2	0.31	0.03	0.17	0.00	0.00	22.3
12	565	5163	-973	-184	0	809	985	4.02	4.02	4.02	4.02	2	0.27	0.03	0.17	0.00	0.00	22.3
13	565	5223	-967	-183	0	771	1006	4.02	4.02	4.02	4.02	2	0.26	0.03	0.17	0.00	0.00	22.3
14	565	4946	-962	-212	0	970	1029	4.02	4.02	4.02	4.02	2	0.32	0.03	0.17	0.00	0.00	22.3

15	565	5144	-941	-211	0	843	1100	4.02	4.02	4.02	4.02	2	0.28	0.03	0.17	0.00	0.00	22.3
16	565	5014	-971	-199	0	916	997	4.02	4.02	4.02	4.02	2	0.30	0.03	0.17	0.00	0.00	22.3
17	565	5213	-950	-198	0	789	1068	4.02	4.02	4.02	4.02	2	0.26	0.03	0.17	0.00	0.00	22.3
18	565	6562	-1074	-603	0	2600	1930	4.02	4.02	4.02	4.02	3	0.77	0.03	0.19	0.00	0.00	22.3
19	565	8282	-1234	-420	0	1808	1462	4.02	4.02	4.02	4.02	3	0.57	0.04	0.22	0.00	0.00	22.3
20	565	7584	-1121	-676	0	2805	1791	4.02	4.02	4.02	4.02	3	0.86	0.03	0.20	0.00	0.00	22.3
37	565	5739	-1048	-583	0	2517	1981	4.02	4.02	4.02	4.02	3	0.73	0.03	0.19	0.00	0.00	22.3
38	565	8606	-1315	-278	0	1196	1201	4.02	4.02	4.02	4.02	3	0.38	0.04	0.23	0.00	0.00	22.3
39	565	7441	-1128	-706	0	2857	1749	4.02	4.02	4.02	4.02	3	0.87	0.03	0.20	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

Nome travata: **Trave_402_IP1** Descrizione: **Trave_4 1-10-15-20-25**
ASTA NUM. 5 NI 291 NF 295 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y Permanente qy tot.
qy medio: 375.00 160.00 535.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	3017	2253	-40	0	-427	-3240	4.02	4.02	4.02	4.02	3	0.51	0.07	0.40	0.00	0.00	22.3
2	0	1766	1376	-21	0	-283	-1329	4.02	4.02	4.02	4.02	2	0.21	0.04	0.25	0.00	0.00	22.3
3	0	1709	1373	-16	0	-276	-1314	4.02	4.02	4.02	4.02	2	0.21	0.04	0.24	0.00	0.00	22.3
4	0	2932	2093	-45	0	-381	-3671	4.02	4.02	4.02	4.02	2	0.61	0.06	0.37	0.00	0.00	22.3
5	0	2876	2090	-40	0	-374	-3656	4.02	4.02	4.02	4.02	2	0.61	0.06	0.37	0.00	0.00	22.3
6	0	2240	1631	-35	0	-326	-2166	4.02	4.02	4.02	4.02	2	0.35	0.05	0.29	0.00	0.00	22.3
7	0	2052	1621	-19	0	-301	-2116	4.02	4.02	4.02	4.02	2	0.34	0.05	0.29	0.00	0.00	22.3
8	0	2589	1846	-42	0	-356	-2868	4.02	4.02	4.02	4.02	2	0.47	0.05	0.33	0.00	0.00	22.3
9	0	2402	1836	-26	0	-331	-2819	4.02	4.02	4.02	4.02	2	0.46	0.05	0.33	0.00	0.00	22.3
10	0	1766	1376	-21	0	-283	-1329	4.02	4.02	4.02	4.02	2	0.21	0.04	0.25	0.00	0.00	22.3
11	0	1709	1373	-16	0	-276	-1314	4.02	4.02	4.02	4.02	2	0.21	0.04	0.24	0.00	0.00	22.3
12	0	2932	2093	-45	0	-381	-3671	4.02	4.02	4.02	4.02	2	0.61	0.06	0.37	0.00	0.00	22.3
13	0	2876	2090	-40	0	-374	-3656	4.02	4.02	4.02	4.02	2	0.61	0.06	0.37	0.00	0.00	22.3
14	0	2240	1631	-35	0	-326	-2166	4.02	4.02	4.02	4.02	2	0.35	0.05	0.29	0.00	0.00	22.3
15	0	2052	1621	-19	0	-301	-2116	4.02	4.02	4.02	4.02	2	0.34	0.05	0.29	0.00	0.00	22.3
16	0	2589	1846	-42	0	-356	-2868	4.02	4.02	4.02	4.02	2	0.47	0.05	0.33	0.00	0.00	22.3
17	0	2402	1836	-26	0	-331	-2819	4.02	4.02	4.02	4.02	2	0.46	0.05	0.33	0.00	0.00	22.3
18	0	3981	1836	80	0	-351	-2083	4.02	4.02	4.02	4.02	3	0.34	0.05	0.33	0.00	0.00	22.3
19	0	6933	3481	-118	0	-988	-7368	4.02	4.02	4.02	6.03	3	0.84	0.10	0.54	0.00	0.00	22.3
20	0	5011	2589	-30	0	-688	-4468	4.02	4.02	4.02	4.02	3	0.75	0.08	0.46	0.00	0.00	22.3
37	0	2149	1147	140	0	-58	777	4.02	4.02	4.02	4.02	3	0.12	0.03	0.20	0.00	0.00	22.3
38	0	7070	3888	-189	0	-1119	-8612	4.02	4.02	4.02	6.03	3	0.98	0.11	0.60	0.00	0.00	22.3
39	0	3866	2401	-44	0	-620	-3778	4.02	4.02	4.02	4.02	3	0.61	0.07	0.43	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= 2.01 (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	56	3017	1902	-40	0	-405	-3029	4.02	4.02	4.02	4.02	3	0.48	0.06	0.34	0.00	0.00	22.3
2	56	1766	1106	-21	0	-271	-1187	4.02	4.02	4.02	4.02	2	0.19	0.03	0.20	0.00	0.00	22.3
3	56	1709	1103	-16	0	-267	-1172	4.02	4.02	4.02	4.02	2	0.19	0.03	0.20	0.00	0.00	22.3
4	56	2932	1823	-45	0	-356	-3487	4.02	4.02	4.02	4.02	2	0.58	0.05	0.32	0.00	0.00	22.3
5	56	2876	1820	-40	0	-351	-3472	4.02	4.02	4.02	4.02	2	0.58	0.05	0.32	0.00	0.00	22.3
6	56	2240	1361	-35	0	-306	-2010	4.02	4.02	4.02	4.02	2	0.33	0.04	0.24	0.00	0.00	22.3
7	56	2052	1351	-19	0	-291	-1960	4.02	4.02	4.02	4.02	2	0.32	0.04	0.24	0.00	0.00	22.3
8	56	2589	1576	-42	0	-331	-2699	4.02	4.02	4.02	4.02	2	0.44	0.05	0.28	0.00	0.00	22.3
9	56	2402	1566	-26	0	-316	-2651	4.02	4.02	4.02	4.02	2	0.43	0.05	0.28	0.00	0.00	22.3
10	56	1766	1106	-21	0	-271	-1187	4.02	4.02	4.02	4.02	2	0.19	0.03	0.20	0.00	0.00	22.3
11	56	1709	1103	-16	0	-267	-1172	4.02	4.02	4.02	4.02	2	0.19	0.03	0.20	0.00	0.00	22.3
12	56	2932	1823	-45	0	-356	-3487	4.02	4.02	4.02	4.02	2	0.58	0.05	0.32	0.00	0.00	22.3
13	56	2876	1820	-40	0	-351	-3472	4.02	4.02	4.02	4.02	2	0.58	0.05	0.32	0.00	0.00	22.3
14	56	2240	1361	-35	0	-306	-2010	4.02	4.02	4.02	4.02	2	0.33	0.04	0.24	0.00	0.00	22.3
15	56	2052	1351	-19	0	-291	-1960	4.02	4.02	4.02	4.02	2	0.32	0.04	0.24	0.00	0.00	22.3
16	56	2589	1576	-42	0	-331	-2699	4.02	4.02	4.02	4.02	2	0.44	0.05	0.28	0.00	0.00	22.3
17	56	2402	1566	-26	0	-316	-2651	4.02	4.02	4.02	4.02	2	0.43	0.05	0.28	0.00	0.00	22.3
18	56	3981	1485	80	0	-396	-1896	4.02	4.02	4.02	4.02	3	0.31	0.04	0.26	0.00	0.00	22.3
19	56	6933	3130	-118	0	-921	-7085	4.02	4.02	4.02	6.03	3	0.81	0.09	0.49	0.00	0.00	22.3
20	56	5011	2238	-30	0	-671	-4237	4.02	4.02	4.02	4.02	3	0.71	0.06	0.40	0.00	0.00	22.3
37	56	2149	796	140	0	-137	1149	4.02	4.02	4.02	4.02	3	0.18	0.02	0.14	0.00	0.00	22.3
38	56	7070	3537	-189	0	-1012	-8305	4.02	4.02	4.02	6.03	3	0.95	0.10	0.55	0.00	0.00	22.3
39	56	3866	2050	-44	0	-595	-3558	4.02	4.02	4.02	4.02	3	0.58	0.06	0.37	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= 2.01 (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	113	3017	1542	-40	0	-382	-1873	4.02	4.02	4.02	4.02	3	0.29	0.04	0.27	0.00	0.00	22.3
2	113	1766	829	-21	0	-259	-500	4.02	4.02	4.02	4.02	2	0.08	0.02	0.15	0.00	0.00	22.3
3	113	1709	826	-16	0	-258	-487	4.02	4.02	4.02	4.02	2	0.08	0.02	0.15	0.00	0.00	22.3
4	113	2932	1546	-45	0	-330	-2395	4.02	4.02	4.02	4.02	2	0.40	0.04	0.28	0.00	0.00	22.3
5	113	2876	1543	-40	0	-329	-2382	4.02	4.02	4.02	4.02	2	0.40	0.04	0.27	0.00	0.00	22.3
6	113	2240	1084	-35	0	-286	-1178	4.02	4.02	4.02	4.02	2	0.19	0.03	0.19	0.00	0.00	22.3
7	113	2052	1074	-19	0	-280	-1135	4.02	4.02	4.02	4.02	2	0.18	0.03	0.19	0.00	0.00	22.3
8	113	2589	1299	-42	0	-307	-1746	4.02	4.02	4.02	4.02	2	0.29	0.04	0.23	0.00	0.00	22.3
9	113	2402	1289	-26	0	-302	-1703	4.02	4.02	4.02	4.02	2	0.28	0.04	0.23	0.00	0.00	22.3
10	113	1766	829	-21	0	-259	-500	4.02	4.02	4.02	4.02	2	0.08	0.02	0.15	0.00	0.00	22.3
11	113	1709	826	-16	0	-258	-487	4.02	4.02	4.02	4.02	2	0.08	0.02	0.15	0.00	0.00	22.3
12	113	2932	1546	-45	0	-330	-2395	4.02	4.02	4.02	4.02	2	0.40	0.04	0.28	0.00	0.00	22.3
13	113	2876	1543	-40	0	-329	-2382	4.02	4.02	4.02	4.02	2	0.40	0.04	0.27	0.00	0.00	22.3
14	113	2240	1084	-35	0	-286	-1178	4.02	4.02	4.02	4.02	2	0.19	0.03	0.19	0.00	0.00	22.3
15	113	2052	1074	-19	0	-280	-1135	4.02	4.02	4.02	4.02	2	0.18	0.03	0.19	0.00	0.00	22.3
16	113	2589	1299	-42	0	-307	-1746	4.02	4.02	4.02	4.02	2	0.29	0.04	0.23	0.00	0.00	22.3
17	113	2402	1289	-26	0	-302	-1703	4.02	4.02	4.02	4.02	2	0.28	0.04	0.23	0.00	0.00	22.3
18	113	3981	1125	80	0	-441	-976	4.02	4.02	4.02	4.02	3	0.16	0.03	0.20	0.00	0.00	22.3
19	113	6933	2770	-118	0	-855	-5235	4.02	4.02	4.02	4.02	3	0.94	0.08	0.49	0.00	0.00	22.3
20	113	5011	1878	-30	0	-654	-2892	4.02	4.02	4.02	4.02	3	0.49	0.05	0.33	0.00	0.00	22.3
37	113	2149	436	140	0	-216	1237	4.02	4.02	4.02	4.02	3	0.19	0.01	0.08	0.00	0.00	22.3
38	113	7070	3177	-189	0	-905	-6225	4.02	4.02	4.02	6.03	3	0.71	0.09	0.49	0.00	0.00	22.3
39	113	3866	1690	-44	0	-570	-2318	4.02	4.02	4.02	4.02	3	0.37	0.05	0.30	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= 2.01 (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	170	3017	1173	-40	0	-360	-918	4.02	4.02	4.02	4.02	3	0.14	0.03	0.21	0.00	0.00	22.3
2	170	1766	545	-21	0	-247	585	4.02	4.02	4.02	4.02	2	0.09	0.02	0.10	0.00	0.00	22.3
3	170	1709	542	-16	0	-248	594	4.02	4.02	4.02	4.02	2	0.09	0.02	0.10	0.00	0.00	22.3
4	170	2932	1262	-45	0	-305	-1457	4.02	4.02	4.02	4.02	2	0.24	0.04	0.22	0.00	0.00	22.3
5	170	2876	1259	-40	0	-306	-1445	4.02	4.02	4.02	4.02	2	0.24	0.04	0.22	0.00	0.00	22.3
6	170	2240	800	-35	0	-266	-502	4.02	4.02	4.02	4.02	2	0.08	0.02	0.14	0.00	0.00	22.3

7	170	2052	790	-19	0	-270	-464	4.02	4.02	4.02	4.02	2	0.08	0.02	0.14	0.00	0.00	22.3
8	170	2589	1015	-42	0	-283	-948	4.02	4.02	4.02	4.02	2	0.16	0.03	0.18	0.00	0.00	22.3
9	170	2402	1005	-26	0	-287	-911	4.02	4.02	4.02	4.02	2	0.15	0.03	0.18	0.00	0.00	22.3
10	170	1766	545	-21	0	-247	585	4.02	4.02	4.02	4.02	2	0.09	0.02	0.10	0.00	0.00	22.3
11	170	1709	542	-16	0	-248	594	4.02	4.02	4.02	4.02	2	0.09	0.02	0.10	0.00	0.00	22.3
12	170	2932	1262	-45	0	-305	-1457	4.02	4.02	4.02	4.02	2	0.24	0.04	0.22	0.00	0.00	22.3
13	170	2876	1259	-40	0	-306	-1445	4.02	4.02	4.02	4.02	2	0.24	0.04	0.22	0.00	0.00	22.3
14	170	2240	800	-35	0	-266	-502	4.02	4.02	4.02	4.02	2	0.08	0.02	0.14	0.00	0.00	22.3
15	170	2052	790	-19	0	-270	-464	4.02	4.02	4.02	4.02	2	0.08	0.02	0.14	0.00	0.00	22.3
16	170	2589	1015	-42	0	-283	-948	4.02	4.02	4.02	4.02	2	0.16	0.03	0.18	0.00	0.00	22.3
17	170	2402	1005	-26	0	-287	-911	4.02	4.02	4.02	4.02	2	0.15	0.03	0.18	0.00	0.00	22.3
18	170	3981	756	80	0	-486	508	4.02	4.02	4.02	4.02	3	0.13	0.02	0.13	0.00	0.00	22.3
19	170	6933	2401	-118	0	-789	-3587	4.02	4.02	4.02	4.02	3	0.65	0.07	0.43	0.00	0.00	22.3
20	170	5011	1509	-30	0	-637	-1747	4.02	4.02	4.02	4.02	3	0.29	0.04	0.27	0.00	0.00	22.3
37	170	2149	67	140	0	-295	1237	4.02	4.02	4.02	4.02	3	0.19	0.00	0.01	0.00	0.00	22.3
38	170	7070	2808	-189	0	-798	-4347	4.02	4.02	4.02	4.02	3	0.79	0.08	0.50	0.00	0.00	22.3
39	170	3866	1321	-44	0	-545	-1280	4.02	4.02	4.02	4.02	3	0.21	0.04	0.24	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	226	3017	794	-40	0	-337	634	4.02	4.02	4.02	4.02	3	0.10	0.02	0.14	0.00	0.00	22.3
2	226	1766	254	-21	0	-235	595	4.02	4.02	4.02	4.02	2	0.10	0.01	0.05	0.00	0.00	22.3
3	226	1709	251	-16	0	-239	601	4.02	4.02	4.02	4.02	2	0.10	0.01	0.04	0.00	0.00	22.3
4	226	2932	971	-45	0	-280	-678	4.02	4.02	4.02	4.02	2	0.11	0.03	0.17	0.00	0.00	22.3
5	226	2876	968	-40	0	-284	-668	4.02	4.02	4.02	4.02	2	0.11	0.03	0.17	0.00	0.00	22.3
6	226	2240	509	-35	0	-246	509	4.02	4.02	4.02	4.02	2	0.08	0.01	0.09	0.00	0.00	22.3
7	226	2052	499	-19	0	-260	525	4.02	4.02	4.02	4.02	2	0.08	0.01	0.09	0.00	0.00	22.3
8	226	2589	724	-42	0	-259	423	4.02	4.02	4.02	4.02	2	0.08	0.02	0.13	0.00	0.00	22.3
9	226	2402	714	-26	0	-273	445	4.02	4.02	4.02	4.02	2	0.08	0.02	0.13	0.00	0.00	22.3
10	226	1766	254	-21	0	-235	595	4.02	4.02	4.02	4.02	2	0.10	0.01	0.05	0.00	0.00	22.3
11	226	1709	251	-16	0	-239	601	4.02	4.02	4.02	4.02	2	0.10	0.01	0.04	0.00	0.00	22.3
12	226	2932	971	-45	0	-280	-678	4.02	4.02	4.02	4.02	2	0.11	0.03	0.17	0.00	0.00	22.3
13	226	2876	968	-40	0	-284	-668	4.02	4.02	4.02	4.02	2	0.11	0.03	0.17	0.00	0.00	22.3
14	226	2240	509	-35	0	-246	509	4.02	4.02	4.02	4.02	2	0.08	0.01	0.09	0.00	0.00	22.3
15	226	2052	499	-19	0	-260	525	4.02	4.02	4.02	4.02	2	0.08	0.01	0.09	0.00	0.00	22.3
16	226	2589	724	-42	0	-259	423	4.02	4.02	4.02	4.02	2	0.08	0.02	0.13	0.00	0.00	22.3
17	226	2402	714	-26	0	-273	445	4.02	4.02	4.02	4.02	2	0.08	0.02	0.13	0.00	0.00	22.3
18	226	3981	377	80	0	-531	550	4.02	4.02	4.02	4.02	3	0.15	0.01	0.07	0.00	0.00	22.3
19	226	6933	2022	-118	0	-722	-2146	4.02	4.02	4.02	4.02	3	0.39	0.06	0.36	0.00	0.00	22.3
20	226	5011	1130	-30	0	-620	-810	4.02	4.02	4.02	4.02	3	0.18	0.03	0.20	0.00	0.00	22.3
37	226	2149	-312	140	0	-373	1237	4.02	4.02	4.02	4.02	3	0.19	0.01	0.06	0.00	0.00	22.3
38	226	7070	2429	-189	0	-691	-2675	4.02	4.02	4.02	4.02	3	0.48	0.07	0.43	0.00	0.00	22.3
39	226	3866	942	-44	0	-521	505	4.02	4.02	4.02	4.02	3	0.14	0.03	0.17	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	282	3017	406	-40	0	-315	689	4.02	4.02	4.02	4.02	3	0.11	0.01	0.07	0.00	0.00	22.3
2	282	1766	-45	-21	0	-223	595	4.02	4.02	4.02	4.02	2	0.10	0.00	0.01	0.00	0.00	22.3
3	282	1709	-48	-16	0	-230	601	4.02	4.02	4.02	4.02	2	0.10	0.00	0.01	0.00	0.00	22.3
4	282	2932	672	-45	0	-254	618	4.02	4.02	4.02	4.02	2	0.10	0.02	0.12	0.00	0.00	22.3
5	282	2876	669	-40	0	-261	623	4.02	4.02	4.02	4.02	2	0.10	0.02	0.12	0.00	0.00	22.3
6	282	2240	210	-35	0	-226	509	4.02	4.02	4.02	4.02	2	0.08	0.01	0.04	0.00	0.00	22.3
7	282	2052	200	-19	0	-249	525	4.02	4.02	4.02	4.02	2	0.08	0.01	0.04	0.00	0.00	22.3
8	282	2589	425	-42	0	-235	536	4.02	4.02	4.02	4.02	2	0.09	0.01	0.08	0.00	0.00	22.3
9	282	2402	415	-26	0	-258	551	4.02	4.02	4.02	4.02	2	0.09	0.01	0.07	0.00	0.00	22.3
10	282	1766	-45	-21	0	-223	595	4.02	4.02	4.02	4.02	2	0.10	0.00	0.01	0.00	0.00	22.3
11	282	1709	-48	-16	0	-230	601	4.02	4.02	4.02	4.02	2	0.10	0.00	0.01	0.00	0.00	22.3
12	282	2932	672	-45	0	-254	618	4.02	4.02	4.02	4.02	2	0.10	0.02	0.12	0.00	0.00	22.3
13	282	2876	669	-40	0	-261	623	4.02	4.02	4.02	4.02	2	0.10	0.02	0.12	0.00	0.00	22.3
14	282	2240	210	-35	0	-226	509	4.02	4.02	4.02	4.02	2	0.08	0.01	0.04	0.00	0.00	22.3
15	282	2052	200	-19	0	-249	525	4.02	4.02	4.02	4.02	2	0.08	0.01	0.04	0.00	0.00	22.3
16	282	2589	425	-42	0	-235	536	4.02	4.02	4.02	4.02	2	0.09	0.01	0.08	0.00	0.00	22.3
17	282	2402	415	-26	0	-258	551	4.02	4.02	4.02	4.02	2	0.09	0.01	0.07	0.00	0.00	22.3
18	282	3981	-11	80	0	-577	550	4.02	4.02	4.02	4.02	3	0.16	0.00	0.00	0.00	0.00	22.3
19	282	6933	1634	-118	0	-656	-916	4.02	4.02	4.02	4.02	3	0.20	0.05	0.29	0.00	0.00	22.3
20	282	5011	742	-30	0	-603	667	4.02	4.02	4.02	4.02	3	0.17	0.02	0.13	0.00	0.00	22.3
37	282	2149	-700	140	0	-452	1237	4.02	4.02	4.02	4.02	3	0.19	0.02	0.12	0.00	0.00	22.3
38	282	7070	2041	-189	0	-584	-1216	4.02	4.02	4.02	4.02	3	0.22	0.06	0.36	0.00	0.00	22.3
39	282	3866	554	-44	0	-496	652	4.02	4.02	4.02	4.02	3	0.14	0.02	0.10	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	339	3017	8	-40	0	-293	689	4.02	4.02	4.02	4.02	3	0.11	0.00	0.00	0.00	0.00	22.3
2	339	1766	-350	-21	0	-211	595	4.02	4.02	4.02	4.02	2	0.10	0.01	0.06	0.00	0.00	22.3
3	339	1709	-353	-16	0	-221	601	4.02	4.02	4.02	4.02	2	0.10	0.01	0.06	0.00	0.00	22.3
4	339	2932	366	-45	0	-229	691	4.02	4.02	4.02	4.02	2	0.11	0.01	0.07	0.00	0.00	22.3
5	339	2876	363	-40	0	-239	694	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
6	339	2240	-96	-35	0	-206	509	4.02	4.02	4.02	4.02	2	0.08	0.00	0.02	0.00	0.00	22.3
7	339	2052	-106	-19	0	-239	525	4.02	4.02	4.02	4.02	2	0.08	0.00	0.02	0.00	0.00	22.3
8	339	2589	119	-42	0	-211	536	4.02	4.02	4.02	4.02	2	0.09	0.00	0.02	0.00	0.00	22.3
9	339	2402	109	-26	0	-244	551	4.02	4.02	4.02	4.02	2	0.09	0.00	0.02	0.00	0.00	22.3
10	339	1766	-350	-21	0	-211	595	4.02	4.02	4.02	4.02	2	0.10	0.01	0.06	0.00	0.00	22.3
11	339	1709	-353	-16	0	-221	601	4.02	4.02	4.02	4.02	2	0.10	0.01	0.06	0.00	0.00	22.3
12	339	2932	366	-45	0	-229	691	4.02	4.02	4.02	4.02	2	0.11	0.01	0.07	0.00	0.00	22.3
13	339	2876	363	-40	0	-239	694	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
14	339	2240	-96	-35	0	-206	509	4.02	4.02	4.02	4.02	2	0.08	0.00	0.02	0.00	0.00	22.3
15	339	2052	-106	-19	0	-239	525	4.02	4.02	4.02	4.02	2	0.08	0.00	0.02	0.00	0.00	22.3
16	339	2589	119	-42	0	-211	536	4.02	4.02	4.02	4.02	2	0.09	0.00	0.02	0.00	0.00	22.3
17	339	2402	109	-26	0	-244	551	4.02	4.02	4.02	4.02	2	0.09	0.00	0.02	0.00	0.00	22.3
18	339	3981	-409	80	0	-622	550	4.02	4.02	4.02	4.02	3	0.17	0.01	0.07	0.00	0.00	22.3
19	339	6933	1236	-118	0	-589	1347	4.02	4.02	4.02	4.02	3	0.24	0.04	0.22	0.00	0.00	22.3
20	339	5011	344	-30	0	-586	678	4.02	4.02	4.02	4.02	3	0.17	0.01	0.06	0.00	0.00	22.3
37	339	2149	-1098	140	0	-531	931	4.02	4.02	4.02	4.02	3	0.14	0.03	0.20	0.00	0.00	22.3
38	339	7070	1643	-189	0	-477	1690	4.02	4.02	4.02	4.02	3	0.31	0.05	0.29	0.00	0.00	22.3
39	339	3866	156	-44	0	-471	652	4.02	4.02	4.02	4.02	3	0.13	0.00	0.03	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	396	3017	-399	-40	0	-270	689	4.02	4.02	4.02	4.02	3	0.11	0.01	0.07	0.00	0.00	22.3
2	396	1766	-663	-21	0	-199	533	4.02	4.02	4.02	4.02	2	0.09	0.02	0.12	0.00	0.00	22.3
3	396	1709	-666	-16	0	-212	538	4.02	4.02	4.02	4.02	2	0.09	0.02	0.12	0.00	0.00	22.3
4	396	2932	53	-45	0	-204	691	4.02	4.02	4.02	4.02	2	0.11	0.00	0.01	0.00	0.00	22.3
5	396	2876	50	-40	0	-216	694	4.02	4.02	4.02	4.02	2	0.12	0.00	0.01	0.00	0.00	22.3
6	396	2240	-409	-35	0	-186	509	4.02	4.02	4.02	4.02	2	0.08	0.01	0.07	0.00	0.00	22.3
7	396	2052	-419	-19	0	-228	525	4.02	4.02	4.02	4.02	2	0.08	0.01	0.07	0.00	0.00	22.3
8	396	2589	-194	-42	0	-187	536	4.02	4.02	4.02	4.02	2	0.09	0.01	0.03	0.00	0.00	22.3
9	396	2402	-204	-26	0	-229	551	4.02	4.02	4.02	4.02	2	0.09	0.01	0.04	0.00	0.00	22.3
10	396	1766	-663	-21	0	-199	533	4.02	4.02	4.02	4.02	2	0.09	0.02	0.12	0.00	0.00	22.3
11	396	1709	-666	-16	0	-212	538	4.02	4.02	4.02	4.02	2	0.09	0.02	0.12	0.00	0.00	22.3
12	396	2932	53	-45	0	-204	691	4.02	4.02	4.02	4.02	2	0.11	0.00	0.01	0.00	0.00	22.3

13	396	2876	50	-40	0	-216	694	4.02	4.02	4.02	4.02	2	0.12	0.00	0.01	0.00	0.00	22.3
14	396	2240	-409	-35	0	-186	509	4.02	4.02	4.02	4.02	2	0.08	0.01	0.07	0.00	0.00	22.3
15	396	2052	-419	-19	0	-228	525	4.02	4.02	4.02	4.02	2	0.08	0.01	0.07	0.00	0.00	22.3
16	396	2589	-194	-42	0	-187	536	4.02	4.02	4.02	4.02	2	0.09	0.01	0.03	0.00	0.00	22.3
17	396	2402	-204	-26	0	-229	551	4.02	4.02	4.02	4.02	2	0.09	0.01	0.04	0.00	0.00	22.3
18	396	3981	-816	80	0	-667	499	4.02	4.02	4.02	4.02	3	0.18	0.02	0.15	0.00	0.00	22.3
19	396	6933	829	-118	0	-523	1725	4.02	4.02	4.02	4.02	3	0.31	0.02	0.15	0.00	0.00	22.3
20	396	5011	-63	-30	0	-569	678	4.02	4.02	4.02	4.02	3	0.16	0.00	0.01	0.00	0.00	22.3
37	396	2149	-1505	140	0	-610	-1122	4.02	4.02	4.02	4.02	3	0.17	0.04	0.27	0.00	0.00	22.3
38	396	7070	1236	-189	0	-370	2298	4.02	4.02	4.02	4.02	3	0.42	0.04	0.22	0.00	0.00	22.3
39	396	3866	-251	-44	0	-446	652	4.02	4.02	4.02	4.02	3	0.12	0.01	0.04	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	452	3017	-815	-40	0	-248	650	4.02	4.02	4.02	4.02	3	0.10	0.02	0.15	0.00	0.00	22.3
2	452	1766	-984	-21	0	-187	-766	4.02	4.02	4.02	4.02	2	0.12	0.03	0.18	0.00	0.00	22.3
3	452	1709	-987	-16	0	-203	-766	4.02	4.02	4.02	4.02	2	0.12	0.03	0.18	0.00	0.00	22.3
4	452	2932	-267	-45	0	-178	691	4.02	4.02	4.02	4.02	2	0.11	0.01	0.05	0.00	0.00	22.3
5	452	2876	-270	-40	0	-194	694	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
6	452	2240	-730	-35	0	-166	415	4.02	4.02	4.02	4.02	2	0.07	0.02	0.13	0.00	0.00	22.3
7	452	2052	-740	-19	0	-218	424	4.02	4.02	4.02	4.02	2	0.07	0.02	0.13	0.00	0.00	22.3
8	452	2589	-515	-42	0	-163	536	4.02	4.02	4.02	4.02	2	0.09	0.01	0.09	0.00	0.00	22.3
9	452	2402	-525	-26	0	-215	551	4.02	4.02	4.02	4.02	2	0.09	0.02	0.09	0.00	0.00	22.3
10	452	1766	-984	-21	0	-187	-766	4.02	4.02	4.02	4.02	2	0.12	0.03	0.18	0.00	0.00	22.3
11	452	1709	-987	-16	0	-203	-766	4.02	4.02	4.02	4.02	2	0.12	0.03	0.18	0.00	0.00	22.3
12	452	2932	-267	-45	0	-178	691	4.02	4.02	4.02	4.02	2	0.11	0.01	0.05	0.00	0.00	22.3
13	452	2876	-270	-40	0	-194	694	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
14	452	2240	-730	-35	0	-166	415	4.02	4.02	4.02	4.02	2	0.07	0.02	0.13	0.00	0.00	22.3
15	452	2052	-740	-19	0	-218	424	4.02	4.02	4.02	4.02	2	0.07	0.02	0.13	0.00	0.00	22.3
16	452	2589	-515	-42	0	-163	536	4.02	4.02	4.02	4.02	2	0.09	0.01	0.09	0.00	0.00	22.3
17	452	2402	-525	-26	0	-215	551	4.02	4.02	4.02	4.02	2	0.09	0.02	0.09	0.00	0.00	22.3
18	452	3981	-1232	80	0	-712	-1116	4.02	4.02	4.02	4.02	3	0.20	0.04	0.22	0.00	0.00	22.3
19	452	6933	412	-118	0	-457	1769	4.02	4.02	4.02	4.02	3	0.32	0.01	0.07	0.00	0.00	22.3
20	452	5011	-480	-30	0	-551	678	4.02	4.02	4.02	4.02	3	0.16	0.01	0.09	0.00	0.00	22.3
37	452	2149	-1922	140	0	-689	-2301	4.02	4.02	4.02	4.02	3	0.35	0.06	0.34	0.00	0.00	22.3
38	452	7070	819	-189	0	-263	2668	4.02	4.02	4.02	4.02	3	0.48	0.02	0.15	0.00	0.00	22.3
39	452	3866	-667	-44	0	-422	652	4.02	4.02	4.02	4.02	3	0.12	0.02	0.12	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	508	3017	-1241	-40	0	-225	-971	4.02	4.02	4.02	4.02	3	0.15	0.04	0.22	0.00	0.00	22.3
2	508	1766	-1311	-21	0	-175	-1580	4.02	4.02	4.02	4.02	2	0.25	0.04	0.23	0.00	0.00	22.3
3	508	1709	-1314	-16	0	-194	-1581	4.02	4.02	4.02	4.02	2	0.25	0.04	0.23	0.00	0.00	22.3
4	508	2932	-595	-45	0	-153	689	4.02	4.02	4.02	4.02	2	0.11	0.02	0.11	0.00	0.00	22.3
5	508	2876	-598	-40	0	-171	690	4.02	4.02	4.02	4.02	2	0.11	0.02	0.11	0.00	0.00	22.3
6	508	2240	-1057	-35	0	-146	-994	4.02	4.02	4.02	4.02	2	0.16	0.03	0.19	0.00	0.00	22.3
7	508	2052	-1067	-19	0	-207	-1001	4.02	4.02	4.02	4.02	2	0.16	0.03	0.19	0.00	0.00	22.3
8	508	2589	-842	-42	0	-139	-494	4.02	4.02	4.02	4.02	2	0.08	0.02	0.15	0.00	0.00	22.3
9	508	2402	-852	-26	0	-200	-501	4.02	4.02	4.02	4.02	2	0.08	0.02	0.15	0.00	0.00	22.3
10	508	1766	-1311	-21	0	-175	-1580	4.02	4.02	4.02	4.02	2	0.25	0.04	0.23	0.00	0.00	22.3
11	508	1709	-1314	-16	0	-194	-1581	4.02	4.02	4.02	4.02	2	0.25	0.04	0.23	0.00	0.00	22.3
12	508	2932	-595	-45	0	-153	689	4.02	4.02	4.02	4.02	2	0.11	0.02	0.11	0.00	0.00	22.3
13	508	2876	-598	-40	0	-171	690	4.02	4.02	4.02	4.02	2	0.11	0.02	0.11	0.00	0.00	22.3
14	508	2240	-1057	-35	0	-146	-994	4.02	4.02	4.02	4.02	2	0.16	0.03	0.19	0.00	0.00	22.3
15	508	2052	-1067	-19	0	-207	-1001	4.02	4.02	4.02	4.02	2	0.16	0.03	0.19	0.00	0.00	22.3
16	508	2589	-842	-42	0	-139	-494	4.02	4.02	4.02	4.02	2	0.08	0.02	0.15	0.00	0.00	22.3
17	508	2402	-852	-26	0	-200	-501	4.02	4.02	4.02	4.02	2	0.08	0.02	0.15	0.00	0.00	22.3
18	508	3981	-1658	80	0	-757	-2148	4.02	4.02	4.02	4.02	3	0.35	0.05	0.30	0.00	0.00	22.3
19	508	6933	-14	-118	0	-390	1769	4.02	4.02	4.02	4.02	3	0.32	0.00	0.00	0.00	0.00	22.3
20	508	5011	-906	-30	0	-534	592	4.02	4.02	4.02	4.02	3	0.15	0.03	0.16	0.00	0.00	22.3
37	508	2149	-2348	140	0	-768	-3722	4.02	4.02	4.02	4.02	3	0.57	0.07	0.42	0.00	0.00	22.3
38	508	7070	394	-189	0	-157	2696	4.02	4.02	4.02	4.02	3	0.49	0.01	0.07	0.00	0.00	22.3
39	508	3866	-1093	-44	0	-397	-683	4.02	4.02	4.02	4.02	3	0.11	0.03	0.19	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	565	3017	-1676	-40	0	-203	-1167	4.02	4.02	4.02	4.02	3	0.18	0.05	0.30	0.00	0.00	22.3
2	565	1766	-1646	-21	0	-164	-1751	4.02	4.02	4.02	4.02	2	0.28	0.05	0.29	0.00	0.00	22.3
3	565	1709	-1649	-16	0	-185	-1753	4.02	4.02	4.02	4.02	2	0.28	0.05	0.29	0.00	0.00	22.3
4	565	2932	-930	-45	0	-128	-43	4.02	4.02	4.02	4.02	2	0.04	0.03	0.17	0.00	0.00	22.3
5	565	2876	-933	-40	0	-149	-45	4.02	4.02	4.02	4.02	2	0.05	0.03	0.17	0.00	0.00	22.3
6	565	2240	-1392	-35	0	-126	-1150	4.02	4.02	4.02	4.02	2	0.19	0.04	0.25	0.00	0.00	22.3
7	565	2052	-1402	-19	0	-197	-1158	4.02	4.02	4.02	4.02	2	0.19	0.04	0.25	0.00	0.00	22.3
8	565	2589	-1177	-42	0	-115	-638	4.02	4.02	4.02	4.02	2	0.10	0.03	0.21	0.00	0.00	22.3
9	565	2402	-1187	-26	0	-186	-646	4.02	4.02	4.02	4.02	2	0.11	0.03	0.21	0.00	0.00	22.3
10	565	1766	-1646	-21	0	-164	-1751	4.02	4.02	4.02	4.02	2	0.28	0.05	0.29	0.00	0.00	22.3
11	565	1709	-1649	-16	0	-185	-1753	4.02	4.02	4.02	4.02	2	0.28	0.05	0.29	0.00	0.00	22.3
12	565	2932	-930	-45	0	-128	-43	4.02	4.02	4.02	4.02	2	0.04	0.03	0.17	0.00	0.00	22.3
13	565	2876	-933	-40	0	-149	-45	4.02	4.02	4.02	4.02	2	0.05	0.03	0.17	0.00	0.00	22.3
14	565	2240	-1392	-35	0	-126	-1150	4.02	4.02	4.02	4.02	2	0.19	0.04	0.25	0.00	0.00	22.3
15	565	2052	-1402	-19	0	-197	-1158	4.02	4.02	4.02	4.02	2	0.19	0.04	0.25	0.00	0.00	22.3
16	565	2589	-1177	-42	0	-115	-638	4.02	4.02	4.02	4.02	2	0.10	0.03	0.21	0.00	0.00	22.3
17	565	2402	-1187	-26	0	-186	-646	4.02	4.02	4.02	4.02	2	0.11	0.03	0.21	0.00	0.00	22.3
18	565	3981	-2093	80	0	-802	-2368	4.02	4.02	4.02	4.02	3	0.38	0.06	0.37	0.00	0.00	22.3
19	565	6933	-449	-118	0	-324	1769	4.02	4.02	4.02	4.02	3	0.32	0.01	0.08	0.00	0.00	22.3
20	565	5011	-1341	-30	0	-517	-500	4.02	4.02	4.02	4.02	3	0.15	0.04	0.24	0.00	0.00	22.3
37	565	2149	-2783	140	0	-846	-3982	4.02	4.02	4.02	4.02	3	0.61	0.08	0.50	0.00	0.00	22.3
38	565	7070	-42	-189	0	-50	2696	4.02	4.02	4.02	4.02	3	0.49	0.01	0.03	0.00	0.00	22.3
39	565	3866	-1528	-44	0	-372	-870	4.02	4.02	4.02	4.02	3	0.14	0.04	0.27	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

Nome travata: **Trave_402_IP1** Descrizione: **Trave_4 1-10-15-20-25**
ASTA NUM. 6 NI 295 NF 297 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y Permanente qy tot.
qy medio: 375.00 272.00 647.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	3233	2406	197	0	731	-2450	4.02	4.02	4.02	4.02	3	0.39	0.07	0.43	0.00	0.00	22.3
2	0	2621	1629	154	0	574	-1260	4.02	4.02	4.02	4.02	2	0.21	0.05	0.29	0.00	0.00	22.3
3	0	2550	1629	148	0	548	-1257	4.02	4.02	4.02	4.02	2	0.21	0.05	0.29	0.00	0.00	22.3
4	0	2424	2072	155	0	576	-2512	4.02	4.02	4.02	4.02	2	0.41	0.06	0.37	0.00	0.00	22.3

5	0	2352	2072	148	0	551	-2509	4.02	4.02	4.02	4.02	2	0.41	0.06	0.37	0.00	0.00	22.3
6	0	2636	1785	162	0	605	-1701	4.02	4.02	4.02	4.02	2	0.28	0.05	0.32	0.00	0.00	22.3
7	0	2397	1783	140	0	519	-1692	4.02	4.02	4.02	4.02	2	0.28	0.05	0.32	0.00	0.00	22.3
8	0	2577	1918	162	0	606	-2077	4.02	4.02	4.02	4.02	2	0.34	0.06	0.34	0.00	0.00	22.3
9	0	2338	1916	140	0	520	-2067	4.02	4.02	4.02	4.02	2	0.34	0.06	0.34	0.00	0.00	22.3
10	0	2621	1629	154	0	574	-1260	4.02	4.02	4.02	4.02	2	0.21	0.05	0.29	0.00	0.00	22.3
11	0	2550	1629	148	0	548	-1257	4.02	4.02	4.02	4.02	2	0.21	0.05	0.29	0.00	0.00	22.3
12	0	2424	2072	155	0	576	-2512	4.02	4.02	4.02	4.02	2	0.41	0.06	0.37	0.00	0.00	22.3
13	0	2352	2072	148	0	551	-2509	4.02	4.02	4.02	4.02	2	0.41	0.06	0.37	0.00	0.00	22.3
14	0	2636	1785	162	0	605	-1701	4.02	4.02	4.02	4.02	2	0.28	0.05	0.32	0.00	0.00	22.3
15	0	2397	1783	140	0	519	-1692	4.02	4.02	4.02	4.02	2	0.28	0.05	0.32	0.00	0.00	22.3
16	0	2577	1918	162	0	606	-2077	4.02	4.02	4.02	4.02	2	0.34	0.06	0.34	0.00	0.00	22.3
17	0	2338	1916	140	0	520	-2067	4.02	4.02	4.02	4.02	2	0.34	0.06	0.34	0.00	0.00	22.3
18	0	5890	1978	488	0	1827	-1255	4.02	4.02	4.02	4.02	3	0.53	0.06	0.35	0.00	0.00	22.3
19	0	5373	3093	377	0	1369	-4397	4.02	4.02	4.02	4.02	3	0.75	0.09	0.55	0.00	0.00	22.3
20	0	5180	2515	383	0	1445	-2766	4.02	4.02	4.02	4.02	3	0.47	0.07	0.45	0.00	0.00	22.3
37	0	5224	1561	449	0	1701	-75	4.02	4.02	4.02	4.02	3	0.48	0.05	0.28	0.00	0.00	22.3
38	0	4363	3419	264	0	936	-5313	4.02	4.02	4.02	4.02	3	0.87	0.10	0.61	0.00	0.00	22.3
39	0	4041	2456	274	0	1063	-2594	4.02	4.02	4.02	4.02	3	0.42	0.07	0.44	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	56	3233	1963	197	0	620	-2209	4.02	4.02	4.02	4.02	3	0.35	0.06	0.35	0.00	0.00	22.3
2	56	2621	1288	154	0	487	-1087	4.02	4.02	4.02	4.02	2	0.18	0.04	0.23	0.00	0.00	22.3
3	56	2550	1288	148	0	465	-1085	4.02	4.02	4.02	4.02	2	0.18	0.04	0.23	0.00	0.00	22.3
4	56	2424	1731	155	0	489	-2313	4.02	4.02	4.02	4.02	2	0.38	0.05	0.31	0.00	0.00	22.3
5	56	2352	1731	148	0	467	-2311	4.02	4.02	4.02	4.02	2	0.38	0.05	0.31	0.00	0.00	22.3
6	56	2636	1444	162	0	513	-1519	4.02	4.02	4.02	4.02	2	0.25	0.04	0.26	0.00	0.00	22.3
7	56	2397	1442	140	0	440	-1511	4.02	4.02	4.02	4.02	2	0.25	0.04	0.26	0.00	0.00	22.3
8	56	2577	1577	162	0	514	-1888	4.02	4.02	4.02	4.02	2	0.31	0.05	0.28	0.00	0.00	22.3
9	56	2338	1575	140	0	440	-1878	4.02	4.02	4.02	4.02	2	0.31	0.05	0.28	0.00	0.00	22.3
10	56	2621	1288	154	0	487	-1087	4.02	4.02	4.02	4.02	2	0.18	0.04	0.23	0.00	0.00	22.3
11	56	2550	1288	148	0	465	-1085	4.02	4.02	4.02	4.02	2	0.18	0.04	0.23	0.00	0.00	22.3
12	56	2424	1731	155	0	489	-2313	4.02	4.02	4.02	4.02	2	0.38	0.05	0.31	0.00	0.00	22.3
13	56	2352	1731	148	0	467	-2311	4.02	4.02	4.02	4.02	2	0.38	0.05	0.31	0.00	0.00	22.3
14	56	2636	1444	162	0	513	-1519	4.02	4.02	4.02	4.02	2	0.25	0.04	0.26	0.00	0.00	22.3
15	56	2397	1442	140	0	440	-1511	4.02	4.02	4.02	4.02	2	0.25	0.04	0.26	0.00	0.00	22.3
16	56	2577	1577	162	0	514	-1888	4.02	4.02	4.02	4.02	2	0.31	0.05	0.28	0.00	0.00	22.3
17	56	2338	1575	140	0	440	-1878	4.02	4.02	4.02	4.02	2	0.31	0.05	0.28	0.00	0.00	22.3
18	56	5890	1535	488	0	1551	-1039	4.02	4.02	4.02	4.02	3	0.45	0.04	0.27	0.00	0.00	22.3
19	56	5373	2650	377	0	1156	-4116	4.02	4.02	4.02	4.02	3	0.70	0.08	0.47	0.00	0.00	22.3
20	56	5180	2072	383	0	1228	-2518	4.02	4.02	4.02	4.02	3	0.43	0.06	0.37	0.00	0.00	22.3
37	56	5224	1118	449	0	1447	1248	4.02	4.02	4.02	4.02	3	0.41	0.03	0.20	0.00	0.00	22.3
38	56	4363	2976	264	0	787	-5013	4.02	4.02	4.02	4.02	3	0.82	0.09	0.53	0.00	0.00	22.3
39	56	4041	2013	274	0	908	-2350	4.02	4.02	4.02	4.02	3	0.38	0.06	0.36	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	113	3233	1512	197	0	509	-999	4.02	4.02	4.02	4.02	3	0.16	0.04	0.27	0.00	0.00	22.3
2	113	2621	941	154	0	399	671	4.02	4.02	4.02	4.02	2	0.12	0.03	0.17	0.00	0.00	22.3
3	113	2550	941	148	0	381	673	4.02	4.02	4.02	4.02	2	0.11	0.03	0.17	0.00	0.00	22.3
4	113	2424	1384	155	0	401	-1258	4.02	4.02	4.02	4.02	2	0.21	0.04	0.25	0.00	0.00	22.3
5	113	2352	1384	148	0	383	-1255	4.02	4.02	4.02	4.02	2	0.20	0.04	0.25	0.00	0.00	22.3
6	113	2636	1097	162	0	422	-626	4.02	4.02	4.02	4.02	2	0.13	0.03	0.20	0.00	0.00	22.3
7	113	2397	1095	140	0	360	-618	4.02	4.02	4.02	4.02	2	0.11	0.03	0.20	0.00	0.00	22.3
8	113	2577	1230	162	0	422	-919	4.02	4.02	4.02	4.02	2	0.15	0.04	0.22	0.00	0.00	22.3
9	113	2338	1228	140	0	361	-910	4.02	4.02	4.02	4.02	2	0.15	0.04	0.22	0.00	0.00	22.3
10	113	2621	941	154	0	399	671	4.02	4.02	4.02	4.02	2	0.12	0.03	0.17	0.00	0.00	22.3
11	113	2550	941	148	0	381	673	4.02	4.02	4.02	4.02	2	0.11	0.03	0.17	0.00	0.00	22.3
12	113	2424	1384	155	0	401	-1258	4.02	4.02	4.02	4.02	2	0.21	0.04	0.25	0.00	0.00	22.3
13	113	2352	1384	148	0	383	-1255	4.02	4.02	4.02	4.02	2	0.20	0.04	0.25	0.00	0.00	22.3
14	113	2636	1097	162	0	422	-626	4.02	4.02	4.02	4.02	2	0.13	0.03	0.20	0.00	0.00	22.3
15	113	2397	1095	140	0	360	-618	4.02	4.02	4.02	4.02	2	0.11	0.03	0.20	0.00	0.00	22.3
16	113	2577	1230	162	0	422	-919	4.02	4.02	4.02	4.02	2	0.15	0.04	0.22	0.00	0.00	22.3
17	113	2338	1228	140	0	361	-910	4.02	4.02	4.02	4.02	2	0.15	0.04	0.22	0.00	0.00	22.3
18	113	5890	1084	488	0	1276	1027	4.02	4.02	4.02	4.02	3	0.37	0.03	0.19	0.00	0.00	22.3
19	113	5373	2199	377	0	942	-2518	4.02	4.02	4.02	4.02	3	0.43	0.06	0.39	0.00	0.00	22.3
20	113	5180	1621	383	0	1012	-1247	4.02	4.02	4.02	4.02	3	0.29	0.05	0.29	0.00	0.00	22.3
37	113	5224	667	449	0	1194	1435	4.02	4.02	4.02	4.02	3	0.34	0.02	0.12	0.00	0.00	22.3
38	113	4363	2525	264	0	637	-3230	4.02	4.02	4.02	4.02	3	0.53	0.07	0.45	0.00	0.00	22.3
39	113	4041	1562	274	0	753	-1112	4.02	4.02	4.02	4.02	3	0.21	0.05	0.28	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	170	3233	1054	197	0	397	1025	4.02	4.02	4.02	4.02	3	0.16	0.03	0.19	0.00	0.00	22.3
2	170	2621	589	154	0	312	889	4.02	4.02	4.02	4.02	2	0.15	0.02	0.10	0.00	0.00	22.3
3	170	2550	589	148	0	298	890	4.02	4.02	4.02	4.02	2	0.15	0.02	0.10	0.00	0.00	22.3
4	170	2424	1032	155	0	314	649	4.02	4.02	4.02	4.02	2	0.11	0.03	0.18	0.00	0.00	22.3
5	170	2352	1032	148	0	299	651	4.02	4.02	4.02	4.02	2	0.11	0.03	0.18	0.00	0.00	22.3
6	170	2636	745	162	0	330	828	4.02	4.02	4.02	4.02	2	0.14	0.02	0.13	0.00	0.00	22.3
7	170	2397	743	140	0	281	832	4.02	4.02	4.02	4.02	2	0.14	0.02	0.13	0.00	0.00	22.3
8	170	2577	878	162	0	330	745	4.02	4.02	4.02	4.02	2	0.12	0.03	0.16	0.00	0.00	22.3
9	170	2338	876	140	0	282	750	4.02	4.02	4.02	4.02	2	0.12	0.03	0.16	0.00	0.00	22.3
10	170	2621	589	154	0	312	889	4.02	4.02	4.02	4.02	2	0.15	0.02	0.10	0.00	0.00	22.3
11	170	2550	589	148	0	298	890	4.02	4.02	4.02	4.02	2	0.15	0.02	0.10	0.00	0.00	22.3
12	170	2424	1032	155	0	314	649	4.02	4.02	4.02	4.02	2	0.11	0.03	0.18	0.00	0.00	22.3
13	170	2352	1032	148	0	299	651	4.02	4.02	4.02	4.02	2	0.11	0.03	0.18	0.00	0.00	22.3
14	170	2636	745	162	0	330	828	4.02	4.02	4.02	4.02	2	0.14	0.02	0.13	0.00	0.00	22.3
15	170	2397	743	140	0	281	832	4.02	4.02	4.02	4.02	2	0.14	0.02	0.13	0.00	0.00	22.3
16	170	2577	878	162	0	330	745	4.02	4.02	4.02	4.02	2	0.12	0.03	0.16	0.00	0.00	22.3
17	170	2338	876	140	0	282	750	4.02	4.02	4.02	4.02	2	0.12	0.03	0.16	0.00	0.00	22.3
18	170	5890	626	488	0	1000	1185	4.02	4.02	4.02	4.02	3	0.29	0.02	0.11	0.00	0.00	22.3
19	170	5373	1741	377	0	729	-1172	4.02	4.02	4.02	4.02	3	0.21	0.05	0.31	0.00	0.00	22.3
20	170	5180	1163	383	0	795	950	4.02	4.02	4.02	4.02	3	0.23	0.03	0.21	0.00	0.00	22.3
37	170	5224	209	449	0	940	1435	4.02	4.02	4.02	4.02	3	0.27	0.01	0.07	0.00	0.00	22.3
38	170	4363	2067	264	0	488	-1701	4.02	4.02	4.02	4.02	3	0.28	0.06	0.37	0.00	0.00	22.3
39	170	4041	1104	274	0	599	992	4.02	4.02	4.02	4.02	3	0.16	0.03	0.20	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	226	3233	590	197	0	286	1156	4.02	4.02	4.02	4.02	3	0.18	0.02	0.11	0.00	0.00	22.3
2	226	2621	232	154	0	225	889	4.02	4.02	4.02	4.02	2	0.15	0.01	0.04	0.00	0.00	22.3
3	226	2550	232	148	0	214	890	4.02	4.02	4.02	4.02	2	0.15	0.01	0.04	0.00	0.00	22.3
4	226	2424	675	155	0	226	951	4.02	4.02	4.02	4.02	2	0.16	0.02	0.12	0.00	0.00	22.3
5	226	2352	675	148	0	215	952	4.02	4.02	4.02	4.02	2	0.16	0.02	0.12	0.00	0.00	22.3
6	226	2636	388	162	0	238	888	4.02	4.02	4.02	4.02	2	0.15	0.01	0.07	0.00	0.00	22.3
7	226	2397	386	140	0	202	891	4.02	4.02	4.02	4.02	2	0.15	0.01	0.07	0.00	0.00	22.3
8	226	2577	521	162	0	239	888	4.02	4.02	4.02	4.02	2	0.15	0.02	0.09	0.00	0.00	22.3
9	226	2338	519	140	0	202	891	4.02	4.02	4.02	4.02	2	0.15	0.02	0.09	0.00	0.00	22.3
10	226	2621	232	154	0	225	889	4.02	4.02	4.02	4.02	2	0.15	0.01	0.04	0.00	0.00	22.3

11	226	2550	232	148	0	214	890	4.02	4.02	4.02	4.02	2	0.15	0.01	0.04	0.00	0.00	22.3
12	226	2424	675	155	0	226	951	4.02	4.02	4.02	4.02	2	0.16	0.02	0.12	0.00	0.00	22.3
13	226	2352	675	148	0	215	952	4.02	4.02	4.02	4.02	2	0.16	0.02	0.12	0.00	0.00	22.3
14	226	2636	388	162	0	238	888	4.02	4.02	4.02	4.02	2	0.15	0.01	0.07	0.00	0.00	22.3
15	226	2397	386	140	0	202	891	4.02	4.02	4.02	4.02	2	0.15	0.01	0.07	0.00	0.00	22.3
16	226	2577	521	162	0	239	888	4.02	4.02	4.02	4.02	2	0.15	0.02	0.09	0.00	0.00	22.3
17	226	2338	519	140	0	202	891	4.02	4.02	4.02	4.02	2	0.15	0.02	0.09	0.00	0.00	22.3
18	226	5890	162	488	0	724	1185	4.02	4.02	4.02	4.02	3	0.21	0.02	0.08	0.00	0.00	22.3
19	226	5373	1277	377	0	516	1209	4.02	4.02	4.02	4.02	3	0.21	0.04	0.23	0.00	0.00	22.3
20	226	5180	699	383	0	579	1150	4.02	4.02	4.02	4.02	3	0.19	0.02	0.12	0.00	0.00	22.3
37	226	5224	-255	449	0	686	1435	4.02	4.02	4.02	4.02	3	0.24	0.01	0.07	0.00	0.00	22.3
38	226	4363	1603	264	0	339	1194	4.02	4.02	4.02	4.02	3	0.20	0.05	0.29	0.00	0.00	22.3
39	226	4041	640	274	0	444	1155	4.02	4.02	4.02	4.02	3	0.19	0.02	0.11	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	282	3233	118	197	0	175	1156	4.02	4.02	4.02	4.02	3	0.18	0.01	0.03	0.00	0.00	22.3
2	282	2621	-131	154	0	138	889	4.02	4.02	4.02	4.02	2	0.15	0.00	0.02	0.00	0.00	22.3
3	282	2550	-131	148	0	131	890	4.02	4.02	4.02	4.02	2	0.15	0.00	0.02	0.00	0.00	22.3
4	282	2424	312	155	0	139	961	4.02	4.02	4.02	4.02	2	0.16	0.01	0.06	0.00	0.00	22.3
5	282	2352	312	148	0	131	962	4.02	4.02	4.02	4.02	2	0.16	0.01	0.06	0.00	0.00	22.3
6	282	2636	25	162	0	147	888	4.02	4.02	4.02	4.02	2	0.15	0.01	0.03	0.00	0.00	22.3
7	282	2397	23	140	0	123	891	4.02	4.02	4.02	4.02	2	0.15	0.00	0.00	0.00	0.00	22.3
8	282	2577	158	162	0	147	888	4.02	4.02	4.02	4.02	2	0.15	0.01	0.03	0.00	0.00	22.3
9	282	2338	156	140	0	123	891	4.02	4.02	4.02	4.02	2	0.15	0.00	0.03	0.00	0.00	22.3
10	282	2621	-131	154	0	138	889	4.02	4.02	4.02	4.02	2	0.15	0.00	0.02	0.00	0.00	22.3
11	282	2550	-131	148	0	131	890	4.02	4.02	4.02	4.02	2	0.15	0.00	0.02	0.00	0.00	22.3
12	282	2424	312	155	0	139	961	4.02	4.02	4.02	4.02	2	0.16	0.01	0.06	0.00	0.00	22.3
13	282	2352	312	148	0	131	962	4.02	4.02	4.02	4.02	2	0.16	0.01	0.06	0.00	0.00	22.3
14	282	2636	25	162	0	147	888	4.02	4.02	4.02	4.02	2	0.15	0.01	0.03	0.00	0.00	22.3
15	282	2397	23	140	0	123	891	4.02	4.02	4.02	4.02	2	0.15	0.00	0.00	0.00	0.00	22.3
16	282	2577	158	162	0	147	888	4.02	4.02	4.02	4.02	2	0.15	0.01	0.03	0.00	0.00	22.3
17	282	2338	156	140	0	123	891	4.02	4.02	4.02	4.02	2	0.15	0.00	0.03	0.00	0.00	22.3
18	282	5890	-310	488	0	448	1185	4.02	4.02	4.02	4.02	3	0.21	0.02	0.08	0.00	0.00	22.3
19	282	5373	805	377	0	303	1518	4.02	4.02	4.02	4.02	3	0.26	0.02	0.14	0.00	0.00	22.3
20	282	5180	227	383	0	362	1150	4.02	4.02	4.02	4.02	3	0.19	0.01	0.06	0.00	0.00	22.3
37	282	5224	-727	449	0	433	1435	4.02	4.02	4.02	4.02	3	0.24	0.02	0.13	0.00	0.00	22.3
38	282	4363	1131	264	0	189	1728	4.02	4.02	4.02	4.02	3	0.28	0.03	0.20	0.00	0.00	22.3
39	282	4041	168	274	0	289	1155	4.02	4.02	4.02	4.02	3	0.19	0.01	0.04	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	339	3233	-361	197	0	64	1156	4.02	4.02	4.02	4.02	3	0.18	0.01	0.06	0.00	0.00	22.3
2	339	2621	-499	154	0	51	889	4.02	4.02	4.02	4.02	2	0.15	0.01	0.09	0.00	0.00	22.3
3	339	2550	-500	148	0	48	890	4.02	4.02	4.02	4.02	2	0.15	0.01	0.09	0.00	0.00	22.3
4	339	2424	-56	155	0	51	961	4.02	4.02	4.02	4.02	2	0.16	0.00	0.02	0.00	0.00	22.3
5	339	2352	-57	148	0	47	962	4.02	4.02	4.02	4.02	2	0.16	0.00	0.01	0.00	0.00	22.3
6	339	2636	-343	162	0	55	888	4.02	4.02	4.02	4.02	2	0.15	0.01	0.06	0.00	0.00	22.3
7	339	2397	-346	140	0	44	891	4.02	4.02	4.02	4.02	2	0.15	0.01	0.06	0.00	0.00	22.3
8	339	2577	-210	162	0	55	888	4.02	4.02	4.02	4.02	2	0.15	0.01	0.04	0.00	0.00	22.3
9	339	2338	-213	140	0	44	891	4.02	4.02	4.02	4.02	2	0.15	0.01	0.04	0.00	0.00	22.3
10	339	2621	-499	154	0	51	889	4.02	4.02	4.02	4.02	2	0.15	0.01	0.09	0.00	0.00	22.3
11	339	2550	-500	148	0	48	890	4.02	4.02	4.02	4.02	2	0.15	0.01	0.09	0.00	0.00	22.3
12	339	2424	-56	155	0	51	961	4.02	4.02	4.02	4.02	2	0.16	0.00	0.02	0.00	0.00	22.3
13	339	2352	-57	148	0	47	962	4.02	4.02	4.02	4.02	2	0.16	0.00	0.01	0.00	0.00	22.3
14	339	2636	-343	162	0	55	888	4.02	4.02	4.02	4.02	2	0.15	0.01	0.06	0.00	0.00	22.3
15	339	2397	-346	140	0	44	891	4.02	4.02	4.02	4.02	2	0.15	0.01	0.06	0.00	0.00	22.3
16	339	2577	-210	162	0	55	888	4.02	4.02	4.02	4.02	2	0.15	0.01	0.04	0.00	0.00	22.3
17	339	2338	-213	140	0	44	891	4.02	4.02	4.02	4.02	2	0.15	0.01	0.04	0.00	0.00	22.3
18	339	5890	-789	488	0	172	1185	4.02	4.02	4.02	4.02	3	0.21	0.02	0.14	0.00	0.00	22.3
19	339	5373	326	377	0	89	1518	4.02	4.02	4.02	4.02	3	0.26	0.01	0.06	0.00	0.00	22.3
20	339	5180	-252	383	0	146	1150	4.02	4.02	4.02	4.02	3	0.19	0.01	0.06	0.00	0.00	22.3
37	339	5224	-1206	449	0	179	1210	4.02	4.02	4.02	4.02	3	0.20	0.03	0.21	0.00	0.00	22.3
38	339	4363	652	264	0	40	1891	4.02	4.02	4.02	4.02	3	0.31	0.02	0.12	0.00	0.00	22.3
39	339	4041	-311	274	0	134	1155	4.02	4.02	4.02	4.02	3	0.19	0.01	0.06	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	396	3233	-846	197	0	-47	1156	4.02	4.02	4.02	4.02	3	0.18	0.02	0.15	0.00	0.00	22.3
2	396	2621	-873	154	0	-36	766	4.02	4.02	4.02	4.02	2	0.13	0.03	0.16	0.00	0.00	22.3
3	396	2550	-873	148	0	-36	767	4.02	4.02	4.02	4.02	2	0.13	0.03	0.16	0.00	0.00	22.3
4	396	2424	-430	155	0	-37	961	4.02	4.02	4.02	4.02	2	0.16	0.01	0.08	0.00	0.00	22.3
5	396	2352	-430	148	0	-36	962	4.02	4.02	4.02	4.02	2	0.16	0.01	0.08	0.00	0.00	22.3
6	396	2636	-717	162	0	-36	862	4.02	4.02	4.02	4.02	2	0.14	0.02	0.13	0.00	0.00	22.3
7	396	2397	-719	140	0	-36	864	4.02	4.02	4.02	4.02	2	0.14	0.02	0.13	0.00	0.00	22.3
8	396	2577	-584	162	0	-37	888	4.02	4.02	4.02	4.02	2	0.15	0.02	0.10	0.00	0.00	22.3
9	396	2338	-586	140	0	-36	891	4.02	4.02	4.02	4.02	2	0.15	0.02	0.10	0.00	0.00	22.3
10	396	2621	-873	154	0	-36	766	4.02	4.02	4.02	4.02	2	0.13	0.03	0.16	0.00	0.00	22.3
11	396	2550	-873	148	0	-36	767	4.02	4.02	4.02	4.02	2	0.13	0.03	0.16	0.00	0.00	22.3
12	396	2424	-430	155	0	-37	961	4.02	4.02	4.02	4.02	2	0.16	0.01	0.08	0.00	0.00	22.3
13	396	2352	-430	148	0	-36	962	4.02	4.02	4.02	4.02	2	0.16	0.01	0.08	0.00	0.00	22.3
14	396	2636	-717	162	0	-36	862	4.02	4.02	4.02	4.02	2	0.14	0.02	0.13	0.00	0.00	22.3
15	396	2397	-719	140	0	-36	864	4.02	4.02	4.02	4.02	2	0.14	0.02	0.13	0.00	0.00	22.3
16	396	2577	-584	162	0	-37	888	4.02	4.02	4.02	4.02	2	0.15	0.02	0.10	0.00	0.00	22.3
17	396	2338	-586	140	0	-36	891	4.02	4.02	4.02	4.02	2	0.15	0.02	0.10	0.00	0.00	22.3
18	396	5890	-1274	488	0	-103	897	4.02	4.02	4.02	4.02	3	0.16	0.04	0.23	0.00	0.00	22.3
19	396	5373	-159	377	0	-124	1518	4.02	4.02	4.02	4.02	3	0.26	0.01	0.06	0.00	0.00	22.3
20	396	5180	-737	383	0	-71	1150	4.02	4.02	4.02	4.02	3	0.19	0.02	0.13	0.00	0.00	22.3
37	396	5224	-1691	449	0	-74	-1075	4.02	4.02	4.02	4.02	3	0.18	0.05	0.30	0.00	0.00	22.3
38	396	4363	167	264	0	-109	1891	4.02	4.02	4.02	4.02	3	0.31	0.01	0.04	0.00	0.00	22.3
39	396	4041	-796	274	0	-21	1155	4.02	4.02	4.02	4.02	3	0.19	0.02	0.14	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	452	3233	-1339	197	0	-158	808	4.02	4.02	4.02	4.02	3	0.13	0.04	0.24	0.00	0.00	22.3
2	452	2621	-1252	154	0	-123	-909	4.02	4.02	4.02	4.02	2	0.15	0.04	0.22	0.00	0.00	22.3
3	452	2550	-1252	148	0	-119	-909	4.02	4.02	4.02	4.02	2	0.15	0.04	0.22	0.00	0.00	22.3
4	452	2424	-809	155	0	-124	884	4.02	4.02	4.02	4.02	2	0.14	0.02	0.14	0.00	0.00	22.3
5	452	2352	-809	148	0	-120	884	4.02	4.02	4.02	4.02	2	0.14	0.02	0.14	0.00	0.00	22.3
6	452	2636	-1096	162	0	-128	-567	4.02	4.02	4.02	4.02	2	0.09	0.03	0.20	0.00	0.00	22.3
7	452	2397	-1098	140	0	-115	-569	4.02	4.02	4.02	4.02	2	0.09	0.03	0.20	0.00	0.00	22.3
8	452	2577	-963	162	0	-128	700	4.02	4.02	4.02	4.02	2	0.12	0.03	0.17	0.00	0.00	22.3
9	452	2338	-965	140	0	-115	701	4.02	4.02	4.02	4.02	2	0.11	0.03	0.17	0.00	0.00	22.3
10	452	2621	-1252	154	0	-123	-909	4.02	4.02	4.02	4.02	2	0.15	0.04	0.22	0.00	0.00	22.3
11	452	2550	-1252	148	0	-119	-909	4.02	4.02	4.02	4.02	2	0.15	0.04	0.22	0.00	0.00	22.3
12	452	2424	-809	155	0	-124	884	4.02	4.02	4.02	4.02	2	0.14	0.02	0.14	0.00	0.00	22.3
13	452	2352	-809	148	0	-120	884	4.02	4.02	4.02	4.02	2	0.14	0.02	0.14	0.00	0.00	22.3
14	452	2636	-1096	162	0	-128	-567	4.02	4.02	4.02	4.02	2	0.09	0.03	0.20	0.00	0.00	22.3
15	452	2397	-1098	140	0	-115	-569	4.02	4.02	4.02	4.02	2	0.09	0.03	0.20	0.00	0.00	22.3
16	452	2577	-963	162	0	-128	700	4.02	4.02	4.02	4.02	2	0.12	0.03	0.17	0.00	0.00	22.3

17	452	2338	-965	140	0	-115	701	4.02	4.02	4.02	4.02	2	0.11	0.03	0.17	0.00	0.00	22.3
18	452	5890	-1767	488	0	-379	-1501	4.02	4.02	4.02	4.02	3	0.26	0.05	0.31	0.00	0.00	22.3
19	452	5373	-652	377	0	-337	1518	4.02	4.02	4.02	4.02	3	0.26	0.02	0.12	0.00	0.00	22.3
20	452	5180	-1230	383	0	-287	932	4.02	4.02	4.02	4.02	3	0.16	0.04	0.22	0.00	0.00	22.3
37	452	5224	-2184	449	0	-328	-2418	4.02	4.02	4.02	4.02	3	0.41	0.06	0.39	0.00	0.00	22.3
38	452	4363	-326	264	0	-259	1891	4.02	4.02	4.02	4.02	3	0.31	0.01	0.06	0.00	0.00	22.3
39	452	4041	-1289	274	0	-176	867	4.02	4.02	4.02	4.02	3	0.14	0.04	0.23	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	508	3233	-1839	197	0	-269	-1699	4.02	4.02	4.02	4.02	3	0.27	0.05	0.33	0.00	0.00	22.3
2	508	2621	-1636	154	0	-210	-1919	4.02	4.02	4.02	4.02	2	0.32	0.05	0.29	0.00	0.00	22.3
3	508	2550	-1637	148	0	-202	-1920	4.02	4.02	4.02	4.02	2	0.32	0.05	0.29	0.00	0.00	22.3
4	508	2424	-1193	155	0	-212	-694	4.02	4.02	4.02	4.02	2	0.11	0.03	0.21	0.00	0.00	22.3
5	508	2352	-1194	148	0	-204	-695	4.02	4.02	4.02	4.02	2	0.11	0.03	0.21	0.00	0.00	22.3
6	508	2636	-1480	162	0	-220	-1489	4.02	4.02	4.02	4.02	2	0.25	0.04	0.26	0.00	0.00	22.3
7	508	2397	-1483	140	0	-194	-1492	4.02	4.02	4.02	4.02	2	0.24	0.04	0.26	0.00	0.00	22.3
8	508	2577	-1347	162	0	-220	-1122	4.02	4.02	4.02	4.02	2	0.18	0.04	0.24	0.00	0.00	22.3
9	508	2338	-1350	140	0	-194	-1125	4.02	4.02	4.02	4.02	2	0.18	0.04	0.24	0.00	0.00	22.3
10	508	2621	-1636	154	0	-210	-1919	4.02	4.02	4.02	4.02	2	0.32	0.05	0.29	0.00	0.00	22.3
11	508	2550	-1637	148	0	-202	-1920	4.02	4.02	4.02	4.02	2	0.32	0.05	0.29	0.00	0.00	22.3
12	508	2424	-1193	155	0	-212	-694	4.02	4.02	4.02	4.02	2	0.11	0.03	0.21	0.00	0.00	22.3
13	508	2352	-1194	148	0	-204	-695	4.02	4.02	4.02	4.02	2	0.11	0.03	0.21	0.00	0.00	22.3
14	508	2636	-1480	162	0	-220	-1489	4.02	4.02	4.02	4.02	2	0.25	0.04	0.26	0.00	0.00	22.3
15	508	2397	-1483	140	0	-194	-1492	4.02	4.02	4.02	4.02	2	0.24	0.04	0.26	0.00	0.00	22.3
16	508	2577	-1347	162	0	-220	-1122	4.02	4.02	4.02	4.02	2	0.18	0.04	0.24	0.00	0.00	22.3
17	508	2338	-1350	140	0	-194	-1125	4.02	4.02	4.02	4.02	2	0.18	0.04	0.24	0.00	0.00	22.3
18	508	5890	-2267	488	0	-655	-2893	4.02	4.02	4.02	4.02	3	0.50	0.07	0.40	0.00	0.00	22.3
19	508	5373	-1152	377	0	-551	1363	4.02	4.02	4.02	4.02	3	0.23	0.03	0.21	0.00	0.00	22.3
20	508	5180	-1730	383	0	-504	-1403	4.02	4.02	4.02	4.02	3	0.24	0.05	0.31	0.00	0.00	22.3
37	508	5224	-2684	449	0	-582	-4046	4.02	4.02	4.02	4.02	3	0.69	0.08	0.48	0.00	0.00	22.3
38	508	4363	-826	264	0	-408	1891	4.02	4.02	4.02	4.02	3	0.31	0.02	0.15	0.00	0.00	22.3
39	508	4041	-1789	274	0	-330	-1561	4.02	4.02	4.02	4.02	3	0.25	0.05	0.32	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	565	3233	-2346	197	0	-380	-1950	4.02	4.02	4.02	4.02	3	0.31	0.07	0.42	0.00	0.00	22.3
2	565	2621	-2026	154	0	-297	-2125	4.02	4.02	4.02	4.02	2	0.35	0.06	0.36	0.00	0.00	22.3
3	565	2550	-2027	148	0	-286	-2126	4.02	4.02	4.02	4.02	2	0.35	0.06	0.36	0.00	0.00	22.3
4	565	2424	-1583	155	0	-299	-874	4.02	4.02	4.02	4.02	2	0.14	0.05	0.28	0.00	0.00	22.3
5	565	2352	-1584	148	0	-288	-875	4.02	4.02	4.02	4.02	2	0.14	0.05	0.28	0.00	0.00	22.3
6	565	2636	-1870	162	0	-311	-1686	4.02	4.02	4.02	4.02	2	0.28	0.05	0.33	0.00	0.00	22.3
7	565	2397	-1873	140	0	-273	-1689	4.02	4.02	4.02	4.02	2	0.28	0.05	0.33	0.00	0.00	22.3
8	565	2577	-1737	162	0	-312	-1311	4.02	4.02	4.02	4.02	2	0.22	0.05	0.31	0.00	0.00	22.3
9	565	2338	-1740	140	0	-274	-1314	4.02	4.02	4.02	4.02	2	0.21	0.05	0.31	0.00	0.00	22.3
10	565	2621	-2026	154	0	-297	-2125	4.02	4.02	4.02	4.02	2	0.35	0.06	0.36	0.00	0.00	22.3
11	565	2550	-2027	148	0	-286	-2126	4.02	4.02	4.02	4.02	2	0.35	0.06	0.36	0.00	0.00	22.3
12	565	2424	-1583	155	0	-299	-874	4.02	4.02	4.02	4.02	2	0.14	0.05	0.28	0.00	0.00	22.3
13	565	2352	-1584	148	0	-288	-875	4.02	4.02	4.02	4.02	2	0.14	0.05	0.28	0.00	0.00	22.3
14	565	2636	-1870	162	0	-311	-1686	4.02	4.02	4.02	4.02	2	0.28	0.05	0.33	0.00	0.00	22.3
15	565	2397	-1873	140	0	-273	-1689	4.02	4.02	4.02	4.02	2	0.28	0.05	0.33	0.00	0.00	22.3
16	565	2577	-1737	162	0	-312	-1311	4.02	4.02	4.02	4.02	2	0.22	0.05	0.31	0.00	0.00	22.3
17	565	2338	-1740	140	0	-274	-1314	4.02	4.02	4.02	4.02	2	0.21	0.05	0.31	0.00	0.00	22.3
18	565	5890	-2774	488	0	-930	-3169	4.02	4.02	4.02	4.02	3	0.55	0.08	0.49	0.00	0.00	22.3
19	565	5373	-1659	377	0	-764	-14	4.02	4.02	4.02	4.02	3	0.22	0.05	0.30	0.00	0.00	22.3
20	565	5180	-2237	383	0	-720	-1647	4.02	4.02	4.02	4.02	3	0.28	0.06	0.40	0.00	0.00	22.3
37	565	5224	-3191	449	0	-835	-4347	4.02	4.02	4.02	4.02	3	0.74	0.09	0.57	0.00	0.00	22.3
38	565	4363	-1333	264	0	-558	1587	4.02	4.02	4.02	4.02	3	0.26	0.04	0.24	0.00	0.00	22.3
39	565	4041	-2296	274	0	-485	-1809	4.02	4.02	4.02	4.02	3	0.29	0.07	0.41	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

Nome travata: **Trave_402_IP1** Descrizione: **Trave_4 1-10-15-20-25**
ASTA NUM. 7 NI 297 NF 271 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y Permanente qy tot.
qy medio: 375.00 272.00 647.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	3084	2454	-193	0	-332	-2280	4.02	4.02	4.02	4.02	3	0.36	0.07	0.44	0.00	0.00	22.3
2	0	3201	1679	-152	0	-263	-1159	4.02	4.02	4.02	4.02	2	0.19	0.05	0.30	0.00	0.00	22.3
3	0	3121	1681	-143	0	-245	-1165	4.02	4.02	4.02	4.02	2	0.20	0.05	0.30	0.00	0.00	22.3
4	0	1624	2093	-154	0	-266	-2343	4.02	4.02	4.02	4.02	2	0.37	0.06	0.37	0.00	0.00	22.3
5	0	1544	2096	-145	0	-247	-2349	4.02	4.02	4.02	4.02	2	0.37	0.06	0.37	0.00	0.00	22.3
6	0	2742	1821	-162	0	-285	-1566	4.02	4.02	4.02	4.02	2	0.26	0.05	0.32	0.00	0.00	22.3
7	0	2476	1829	-134	0	-225	-1587	4.02	4.02	4.02	4.02	2	0.26	0.05	0.33	0.00	0.00	22.3
8	0	2269	1946	-163	0	-286	-1921	4.02	4.02	4.02	4.02	2	0.31	0.06	0.35	0.00	0.00	22.3
9	0	2003	1953	-135	0	-225	-1942	4.02	4.02	4.02	4.02	2	0.31	0.06	0.35	0.00	0.00	22.3
10	0	3201	1679	-152	0	-263	-1159	4.02	4.02	4.02	4.02	2	0.19	0.05	0.30	0.00	0.00	22.3
11	0	3121	1681	-143	0	-245	-1165	4.02	4.02	4.02	4.02	2	0.20	0.05	0.30	0.00	0.00	22.3
12	0	1624	2093	-154	0	-266	-2343	4.02	4.02	4.02	4.02	2	0.37	0.06	0.37	0.00	0.00	22.3
13	0	1544	2096	-145	0	-247	-2349	4.02	4.02	4.02	4.02	2	0.37	0.06	0.37	0.00	0.00	22.3
14	0	2742	1821	-162	0	-285	-1566	4.02	4.02	4.02	4.02	2	0.26	0.05	0.32	0.00	0.00	22.3
15	0	2476	1829	-134	0	-225	-1587	4.02	4.02	4.02	4.02	2	0.26	0.05	0.33	0.00	0.00	22.3
16	0	2269	1946	-163	0	-286	-1921	4.02	4.02	4.02	4.02	2	0.31	0.06	0.35	0.00	0.00	22.3
17	0	2003	1953	-135	0	-225	-1942	4.02	4.02	4.02	4.02	2	0.31	0.06	0.35	0.00	0.00	22.3
18	0	7335	1945	-406	0	-722	-833	4.02	4.02	4.02	4.02	3	0.22	0.06	0.35	0.00	0.00	22.3
19	0	3234	3038	-451	0	-764	-3948	4.02	4.02	4.02	4.02	3	0.63	0.09	0.54	0.00	0.00	22.3
20	0	4858	2487	-378	0	-614	-2376	4.02	4.02	4.02	4.02	3	0.40	0.07	0.44	0.00	0.00	22.3
37	0	7929	1569	-315	0	-575	1035	4.02	4.02	4.02	4.02	3	0.19	0.05	0.28	0.00	0.00	22.3
38	0	1095	3390	-390	0	-646	-4951	4.02	4.02	4.02	4.02	3	0.73	0.10	0.60	0.00	0.00	22.3
39	0	3801	2472	-269	0	-395	-2331	4.02	4.02	4.02	4.02	3	0.38	0.07	0.44	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	57	3084	1947	-193	0	-223	-2023	4.02	4.02	4.02	4.02	3	0.32	0.06	0.35	0.00	0.00	22.3
2	57	3201	1289	-152	0	-178	-973	4.02	4.02	4.02	4.02	2	0.16	0.04	0.23	0.00	0.00	22.3
3	57	3121	1291	-143	0	-164	-979	4.02	4.02	4.02	4.02	2	0.16	0.04	0.23	0.00	0.00	22.3
4	57	1624	1703	-154	0	-179	-2133	4.02	4.02	4.02	4.02	2	0.34	0.05	0.30	0.00	0.00	22.3
5	57	1544	1706	-145	0	-165	-2139	4.02	4.02	4.02	4.02	2	0.34	0.05	0.30	0.00	0.00	22.3
6	57	2742	1431	-162	0	-193	-1372	4.02	4.02	4.02	4.02	2	0.23	0.04	0.25	0.00	0.00	22.3
7	57	2476	1439	-134	0	-149	-1393	4.02	4.02	4.02	4.02	2	0.23	0.04	0.26	0.00	0.00	22.3
8	57	2269	1556	-163	0	-194	-1720	4.02	4.02	4.02	4.02	2	0.28	0.05	0.28	0.00	0.00	22.3

9	57	2003	1563	-135	0	-149	-1740	4.02	4.02	4.02	4.02	2	0.28	0.05	0.28	0.00	0.00	22.3
10	57	3201	1289	-152	0	-178	-973	4.02	4.02	4.02	4.02	2	0.16	0.04	0.23	0.00	0.00	22.3
11	57	3121	1291	-143	0	-164	-979	4.02	4.02	4.02	4.02	2	0.16	0.04	0.23	0.00	0.00	22.3
12	57	1624	1703	-154	0	-179	-2133	4.02	4.02	4.02	4.02	2	0.34	0.05	0.30	0.00	0.00	22.3
13	57	1544	1706	-145	0	-165	-2139	4.02	4.02	4.02	4.02	2	0.34	0.05	0.30	0.00	0.00	22.3
14	57	2742	1431	-162	0	-193	-1372	4.02	4.02	4.02	4.02	2	0.23	0.04	0.25	0.00	0.00	22.3
15	57	2476	1439	-134	0	-149	-1393	4.02	4.02	4.02	4.02	2	0.23	0.04	0.26	0.00	0.00	22.3
16	57	2269	1556	-163	0	-194	-1720	4.02	4.02	4.02	4.02	2	0.28	0.05	0.28	0.00	0.00	22.3
17	57	2003	1563	-135	0	-149	-1740	4.02	4.02	4.02	4.02	2	0.28	0.05	0.28	0.00	0.00	22.3
18	57	7335	1438	-406	0	-492	851	4.02	4.02	4.02	4.02	3	0.16	0.04	0.26	0.00	0.00	22.3
19	57	3234	2531	-451	0	-510	-3657	4.02	4.02	4.02	4.02	3	0.58	0.07	0.45	0.00	0.00	22.3
20	57	4858	1980	-378	0	-400	-2117	4.02	4.02	4.02	4.02	3	0.35	0.06	0.35	0.00	0.00	22.3
37	57	7929	1062	-315	0	-397	1521	4.02	4.02	4.02	4.02	3	0.28	0.03	0.19	0.00	0.00	22.3
38	57	1095	2883	-390	0	-426	-4639	4.02	4.02	4.02	4.02	3	0.69	0.08	0.51	0.00	0.00	22.3
39	57	3801	1965	-269	0	-243	-2073	4.02	4.02	4.02	4.02	3	0.33	0.06	0.35	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	113	3084	1447	-193	0	-114	-812	4.02	4.02	4.02	4.02	3	0.13	0.04	0.26	0.00	0.00	22.3
2	113	3201	904	-152	0	-92	756	4.02	4.02	4.02	4.02	2	0.13	0.03	0.16	0.00	0.00	22.3
3	113	3121	907	-143	0	-83	754	4.02	4.02	4.02	4.02	2	0.13	0.03	0.16	0.00	0.00	22.3
4	113	1624	1319	-154	0	-92	-1085	4.02	4.02	4.02	4.02	2	0.17	0.04	0.23	0.00	0.00	22.3
5	113	1544	1321	-145	0	-83	-1089	4.02	4.02	4.02	4.02	2	0.17	0.04	0.24	0.00	0.00	22.3
6	113	2742	1047	-162	0	-102	582	4.02	4.02	4.02	4.02	2	0.10	0.03	0.19	0.00	0.00	22.3
7	113	2476	1055	-134	0	-73	574	4.02	4.02	4.02	4.02	2	0.09	0.03	0.19	0.00	0.00	22.3
8	113	2269	1171	-163	0	-102	-755	4.02	4.02	4.02	4.02	2	0.12	0.03	0.21	0.00	0.00	22.3
9	113	2003	1179	-135	0	-73	-771	4.02	4.02	4.02	4.02	2	0.12	0.03	0.21	0.00	0.00	22.3
10	113	3201	904	-152	0	-92	756	4.02	4.02	4.02	4.02	2	0.13	0.03	0.16	0.00	0.00	22.3
11	113	3121	907	-143	0	-83	754	4.02	4.02	4.02	4.02	2	0.13	0.03	0.16	0.00	0.00	22.3
12	113	1624	1319	-154	0	-92	-1085	4.02	4.02	4.02	4.02	2	0.17	0.04	0.23	0.00	0.00	22.3
13	113	1544	1321	-145	0	-83	-1089	4.02	4.02	4.02	4.02	2	0.17	0.04	0.24	0.00	0.00	22.3
14	113	2742	1047	-162	0	-102	582	4.02	4.02	4.02	4.02	2	0.10	0.03	0.19	0.00	0.00	22.3
15	113	2476	1055	-134	0	-73	574	4.02	4.02	4.02	4.02	2	0.09	0.03	0.19	0.00	0.00	22.3
16	113	2269	1171	-163	0	-102	-755	4.02	4.02	4.02	4.02	2	0.12	0.03	0.21	0.00	0.00	22.3
17	113	2003	1179	-135	0	-73	-771	4.02	4.02	4.02	4.02	2	0.12	0.03	0.21	0.00	0.00	22.3
18	113	7335	938	-406	0	-263	1269	4.02	4.02	4.02	4.02	3	0.23	0.03	0.17	0.00	0.00	22.3
19	113	3234	2031	-451	0	-255	-2115	4.02	4.02	4.02	4.02	3	0.34	0.06	0.36	0.00	0.00	22.3
20	113	4858	1480	-378	0	-186	-886	4.02	4.02	4.02	4.02	3	0.15	0.04	0.26	0.00	0.00	22.3
37	113	7929	562	-315	0	-219	1620	4.02	4.02	4.02	4.02	3	0.30	0.02	0.10	0.00	0.00	22.3
38	113	1095	2383	-390	0	-206	-2899	4.02	4.02	4.02	4.02	3	0.43	0.07	0.42	0.00	0.00	22.3
39	113	3801	1465	-269	0	-91	-851	4.02	4.02	4.02	4.02	3	0.14	0.04	0.26	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	170	3084	954	-193	0	-5	1082	4.02	4.02	4.02	4.02	3	0.17	0.03	0.17	0.00	0.00	22.3
2	170	3201	525	-152	0	-6	893	4.02	4.02	4.02	4.02	2	0.15	0.02	0.09	0.00	0.00	22.3
3	170	3121	528	-143	0	-2	893	4.02	4.02	4.02	4.02	2	0.15	0.02	0.09	0.00	0.00	22.3
4	170	1624	940	-154	0	-5	697	4.02	4.02	4.02	4.02	2	0.11	0.03	0.17	0.00	0.00	22.3
5	170	1544	942	-145	0	-1	696	4.02	4.02	4.02	4.02	2	0.11	0.03	0.17	0.00	0.00	22.3
6	170	2742	668	-162	0	-10	870	4.02	4.02	4.02	4.02	2	0.14	0.02	0.12	0.00	0.00	22.3
7	170	2476	676	-134	0	3	871	4.02	4.02	4.02	4.02	2	0.14	0.02	0.12	0.00	0.00	22.3
8	170	2269	792	-163	0	-10	793	4.02	4.02	4.02	4.02	2	0.13	0.02	0.14	0.00	0.00	22.3
9	170	2003	800	-135	0	3	789	4.02	4.02	4.02	4.02	2	0.13	0.02	0.14	0.00	0.00	22.3
10	170	3201	525	-152	0	-6	893	4.02	4.02	4.02	4.02	2	0.15	0.02	0.09	0.00	0.00	22.3
11	170	3121	528	-143	0	-2	893	4.02	4.02	4.02	4.02	2	0.15	0.02	0.09	0.00	0.00	22.3
12	170	1624	940	-154	0	-5	697	4.02	4.02	4.02	4.02	2	0.11	0.03	0.17	0.00	0.00	22.3
13	170	1544	942	-145	0	-1	696	4.02	4.02	4.02	4.02	2	0.11	0.03	0.17	0.00	0.00	22.3
14	170	2742	668	-162	0	-10	870	4.02	4.02	4.02	4.02	2	0.14	0.02	0.12	0.00	0.00	22.3
15	170	2476	676	-134	0	3	871	4.02	4.02	4.02	4.02	2	0.14	0.02	0.12	0.00	0.00	22.3
16	170	2269	792	-163	0	-10	793	4.02	4.02	4.02	4.02	2	0.13	0.02	0.14	0.00	0.00	22.3
17	170	2003	800	-135	0	3	789	4.02	4.02	4.02	4.02	2	0.13	0.02	0.14	0.00	0.00	22.3
18	170	7335	445	-406	0	-34	1299	4.02	4.02	4.02	4.02	3	0.24	0.01	0.08	0.00	0.00	22.3
19	170	3234	1538	-451	0	-0	-858	4.02	4.02	4.02	4.02	3	0.14	0.04	0.27	0.00	0.00	22.3
20	170	4858	987	-378	0	27	1059	4.02	4.02	4.02	4.02	3	0.18	0.03	0.18	0.00	0.00	22.3
37	170	7929	69	-315	0	-41	1620	4.02	4.02	4.02	4.02	3	0.30	0.01	0.05	0.00	0.00	22.3
38	170	1095	1890	-390	0	15	-1442	4.02	4.02	4.02	4.02	3	0.21	0.05	0.34	0.00	0.00	22.3
39	170	3801	972	-269	0	61	1071	4.02	4.02	4.02	4.02	3	0.17	0.03	0.17	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	226	3084	468	-193	0	105	1129	4.02	4.02	4.02	4.02	3	0.18	0.01	0.08	0.00	0.00	22.3
2	226	3201	152	-152	0	79	893	4.02	4.02	4.02	4.02	2	0.15	0.00	0.03	0.00	0.00	22.3
3	226	3121	154	-143	0	78	893	4.02	4.02	4.02	4.02	2	0.15	0.00	0.03	0.00	0.00	22.3
4	226	1624	566	-154	0	82	871	4.02	4.02	4.02	4.02	2	0.14	0.02	0.10	0.00	0.00	22.3
5	226	1544	569	-145	0	81	873	4.02	4.02	4.02	4.02	2	0.14	0.02	0.10	0.00	0.00	22.3
6	226	2742	294	-162	0	82	870	4.02	4.02	4.02	4.02	2	0.14	0.01	0.05	0.00	0.00	22.3
7	226	2476	302	-134	0	78	871	4.02	4.02	4.02	4.02	2	0.14	0.01	0.05	0.00	0.00	22.3
8	226	2269	419	-163	0	83	866	4.02	4.02	4.02	4.02	2	0.14	0.01	0.07	0.00	0.00	22.3
9	226	2003	426	-135	0	79	867	4.02	4.02	4.02	4.02	2	0.14	0.01	0.08	0.00	0.00	22.3
10	226	3201	152	-152	0	79	893	4.02	4.02	4.02	4.02	2	0.15	0.00	0.03	0.00	0.00	22.3
11	226	3121	154	-143	0	78	893	4.02	4.02	4.02	4.02	2	0.15	0.00	0.03	0.00	0.00	22.3
12	226	1624	566	-154	0	82	871	4.02	4.02	4.02	4.02	2	0.14	0.02	0.10	0.00	0.00	22.3
13	226	1544	569	-145	0	81	873	4.02	4.02	4.02	4.02	2	0.14	0.02	0.10	0.00	0.00	22.3
14	226	2742	294	-162	0	82	870	4.02	4.02	4.02	4.02	2	0.14	0.01	0.05	0.00	0.00	22.3
15	226	2476	302	-134	0	78	871	4.02	4.02	4.02	4.02	2	0.14	0.01	0.05	0.00	0.00	22.3
16	226	2269	419	-163	0	83	866	4.02	4.02	4.02	4.02	2	0.14	0.01	0.07	0.00	0.00	22.3
17	226	2003	426	-135	0	79	867	4.02	4.02	4.02	4.02	2	0.14	0.01	0.08	0.00	0.00	22.3
18	226	7335	-40	-406	0	195	1299	4.02	4.02	4.02	4.02	3	0.24	0.01	0.07	0.00	0.00	22.3
19	226	3234	1053	-451	0	255	1185	4.02	4.02	4.02	4.02	3	0.19	0.03	0.19	0.00	0.00	22.3
20	226	4858	502	-378	0	241	1128	4.02	4.02	4.02	4.02	3	0.19	0.01	0.09	0.00	0.00	22.3
37	226	7929	-416	-315	0	137	1620	4.02	4.02	4.02	4.02	3	0.30	0.01	0.07	0.00	0.00	22.3
38	226	1095	1404	-390	0	235	1156	4.02	4.02	4.02	4.02	3	0.17	0.04	0.25	0.00	0.00	22.3
39	226	3801	487	-269	0	213	1130	4.02	4.02	4.02	4.02	3	0.18	0.01	0.09	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	283	3084	-11	-193	0	214	1129	4.02	4.02	4.02	4.02	3	0.18	0.01	0.03	0.00	0.00	22.3
2	283	3201	-217	-152	0	165	893	4.02	4.02	4.02	4.02	2	0.15	0.01	0.04	0.00	0.00	22.3
3	283	3121	-214	-143	0	159	893	4.02	4.02	4.02	4.02	2	0.15	0.01	0.04	0.00	0.00	22.3
4	283	1624	198	-154	0	169	871	4.02	4.02	4.02	4.02	2	0.14	0.01	0.04	0.00	0.00	22.3
5	283	1544	200	-145	0	163	873	4.02	4.02	4.02	4.02	2	0.14	0.01	0.04	0.00	0.00	22.3
6	283	2742	-74	-162	0	173	870	4.02	4.02	4.02	4.02	2	0.14	0.01	0.03	0.00	0.00	22.3
7	283	2476	-66	-134	0	154	871	4.02	4.02	4.02	4.02	2	0.14	0.00	0.01	0.00	0.00	22.3
8	283	2269	50	-163	0	175	866	4.02	4.02	4.02	4.02	2	0.14	0.01	0.03	0.00	0.00	22.3
9	283	2003	58	-135	0	155	867	4.02	4.02	4.02	4.02	2	0.14	0.00	0.01	0.00	0.00	22.3
10	283	3201	-217	-152	0	165	893	4.02	4.02	4.02	4.02	2	0.15	0.01	0.04	0.00	0.00	22.3
11	283	3121	-214	-143	0	159	893	4.02	4.02	4.02	4.02	2	0.15	0.01	0.04	0.00	0.00	22.3
12	283	1624	198	-154	0	169	871	4.02	4.02	4.02	4.02	2	0.14	0.01	0.04	0.00	0.00	22.3
13	283	1544	200	-145	0	163	873	4.02	4.02	4.02	4.02	2	0.14	0.01	0.04	0.00	0.00	22.3
14	283	2742	-74	-162	0	173	870	4.02	4.02	4.02	4.02	2	0.14	0.01	0.03	0.00	0.00	22.3

15	283	2476	-66	-134	0	154	871	4.02	4.02	4.02	4.02	2	0.14	0.00	0.01	0.00	0.00	22.3
16	283	2269	50	-163	0	175	866	4.02	4.02	4.02	4.02	2	0.14	0.01	0.03	0.00	0.00	22.3
17	283	2003	58	-135	0	155	867	4.02	4.02	4.02	4.02	2	0.14	0.00	0.01	0.00	0.00	22.3
18	283	7335	-519	-406	0	425	1299	4.02	4.02	4.02	4.02	3	0.24	0.02	0.09	0.00	0.00	22.3
19	283	3234	574	-451	0	509	1302	4.02	4.02	4.02	4.02	3	0.21	0.02	0.10	0.00	0.00	22.3
20	283	4858	23	-378	0	454	1128	4.02	4.02	4.02	4.02	3	0.19	0.01	0.06	0.00	0.00	22.3
37	283	7929	-895	-315	0	315	1603	4.02	4.02	4.02	4.02	3	0.30	0.03	0.16	0.00	0.00	22.3
38	283	1095	925	-390	0	456	1571	4.02	4.02	4.02	4.02	3	0.23	0.03	0.16	0.00	0.00	22.3
39	283	3801	8	-269	0	364	1130	4.02	4.02	4.02	4.02	3	0.18	0.01	0.04	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	339	3084	-482	-193	0	323	1129	4.02	4.02	4.02	4.02	3	0.18	0.01	0.09	0.00	0.00	22.3
2	339	3201	-580	-152	0	251	893	4.02	4.02	4.02	4.02	2	0.15	0.02	0.10	0.00	0.00	22.3
3	339	3121	-577	-143	0	240	893	4.02	4.02	4.02	4.02	2	0.15	0.02	0.10	0.00	0.00	22.3
4	339	1624	-165	-154	0	256	871	4.02	4.02	4.02	4.02	2	0.14	0.00	0.03	0.00	0.00	22.3
5	339	1544	-163	-145	0	246	873	4.02	4.02	4.02	4.02	2	0.14	0.00	0.03	0.00	0.00	22.3
6	339	2742	-437	-162	0	265	870	4.02	4.02	4.02	4.02	2	0.14	0.01	0.08	0.00	0.00	22.3
7	339	2476	-429	-134	0	230	871	4.02	4.02	4.02	4.02	2	0.14	0.01	0.08	0.00	0.00	22.3
8	339	2269	-313	-163	0	267	866	4.02	4.02	4.02	4.02	2	0.14	0.01	0.06	0.00	0.00	22.3
9	339	2003	-305	-135	0	231	867	4.02	4.02	4.02	4.02	2	0.14	0.01	0.05	0.00	0.00	22.3
10	339	3201	-580	-152	0	251	893	4.02	4.02	4.02	4.02	2	0.15	0.02	0.10	0.00	0.00	22.3
11	339	3121	-577	-143	0	240	893	4.02	4.02	4.02	4.02	2	0.15	0.02	0.10	0.00	0.00	22.3
12	339	1624	-165	-154	0	256	871	4.02	4.02	4.02	4.02	2	0.14	0.00	0.03	0.00	0.00	22.3
13	339	1544	-163	-145	0	246	873	4.02	4.02	4.02	4.02	2	0.14	0.00	0.03	0.00	0.00	22.3
14	339	2742	-437	-162	0	265	870	4.02	4.02	4.02	4.02	2	0.14	0.01	0.08	0.00	0.00	22.3
15	339	2476	-429	-134	0	230	871	4.02	4.02	4.02	4.02	2	0.14	0.01	0.08	0.00	0.00	22.3
16	339	2269	-313	-163	0	267	866	4.02	4.02	4.02	4.02	2	0.14	0.01	0.06	0.00	0.00	22.3
17	339	2003	-305	-135	0	231	867	4.02	4.02	4.02	4.02	2	0.14	0.01	0.05	0.00	0.00	22.3
18	339	7335	-991	-406	0	654	1215	4.02	4.02	4.02	4.02	3	0.22	0.03	0.18	0.00	0.00	22.3
19	339	3234	102	-451	0	764	1302	4.02	4.02	4.02	4.02	3	0.21	0.01	0.07	0.00	0.00	22.3
20	339	4858	-449	-378	0	668	1128	4.02	4.02	4.02	4.02	3	0.19	0.01	0.08	0.00	0.00	22.3
37	339	7929	-1367	-315	0	493	1202	4.02	4.02	4.02	4.02	3	0.22	0.04	0.24	0.00	0.00	22.3
38	339	1095	454	-390	0	676	1616	4.02	4.02	4.02	4.02	3	0.24	0.01	0.08	0.00	0.00	22.3
39	339	3801	-464	-269	0	516	1130	4.02	4.02	4.02	4.02	3	0.18	0.01	0.08	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	396	3084	-947	-193	0	432	1064	4.02	4.02	4.02	4.02	3	0.17	0.03	0.17	0.00	0.00	22.3
2	396	3201	-937	-152	0	336	695	4.02	4.02	4.02	4.02	2	0.12	0.03	0.17	0.00	0.00	22.3
3	396	3121	-934	-143	0	321	697	4.02	4.02	4.02	4.02	2	0.12	0.03	0.17	0.00	0.00	22.3
4	396	1624	-522	-154	0	343	871	4.02	4.02	4.02	4.02	2	0.14	0.02	0.09	0.00	0.00	22.3
5	396	1544	-520	-145	0	328	873	4.02	4.02	4.02	4.02	2	0.14	0.02	0.09	0.00	0.00	22.3
6	396	2742	-794	-162	0	357	779	4.02	4.02	4.02	4.02	2	0.13	0.02	0.14	0.00	0.00	22.3
7	396	2476	-786	-134	0	305	785	4.02	4.02	4.02	4.02	2	0.13	0.02	0.14	0.00	0.00	22.3
8	396	2269	-670	-163	0	359	852	4.02	4.02	4.02	4.02	2	0.14	0.02	0.12	0.00	0.00	22.3
9	396	2003	-662	-135	0	307	859	4.02	4.02	4.02	4.02	2	0.14	0.02	0.12	0.00	0.00	22.3
10	396	3201	-937	-152	0	336	695	4.02	4.02	4.02	4.02	2	0.12	0.03	0.17	0.00	0.00	22.3
11	396	3121	-934	-143	0	321	697	4.02	4.02	4.02	4.02	2	0.12	0.03	0.17	0.00	0.00	22.3
12	396	1624	-522	-154	0	343	871	4.02	4.02	4.02	4.02	2	0.14	0.02	0.09	0.00	0.00	22.3
13	396	1544	-520	-145	0	328	873	4.02	4.02	4.02	4.02	2	0.14	0.02	0.09	0.00	0.00	22.3
14	396	2742	-794	-162	0	357	779	4.02	4.02	4.02	4.02	2	0.13	0.02	0.14	0.00	0.00	22.3
15	396	2476	-786	-134	0	305	785	4.02	4.02	4.02	4.02	2	0.13	0.02	0.14	0.00	0.00	22.3
16	396	2269	-670	-163	0	359	852	4.02	4.02	4.02	4.02	2	0.14	0.02	0.12	0.00	0.00	22.3
17	396	2003	-662	-135	0	307	859	4.02	4.02	4.02	4.02	2	0.14	0.02	0.12	0.00	0.00	22.3
18	396	7335	-1455	-406	0	883	759	4.02	4.02	4.02	4.02	3	0.27	0.04	0.26	0.00	0.00	22.3
19	396	3234	-362	-451	0	1019	1302	4.02	4.02	4.02	4.02	3	0.27	0.01	0.07	0.00	0.00	22.3
20	396	4858	-913	-378	0	881	1084	4.02	4.02	4.02	4.02	3	0.25	0.03	0.16	0.00	0.00	22.3
37	396	7929	-1831	-315	0	671	-1321	4.02	4.02	4.02	4.02	3	0.25	0.05	0.33	0.00	0.00	22.3
38	396	1095	-11	-390	0	897	1616	4.02	4.02	4.02	4.02	3	0.24	0.01	0.06	0.00	0.00	22.3
39	396	3801	-928	-269	0	668	1077	4.02	4.02	4.02	4.02	3	0.18	0.03	0.17	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	452	3084	-1405	-193	0	541	-791	4.02	4.02	4.02	4.02	3	0.14	0.04	0.25	0.00	0.00	22.3
2	452	3201	-1289	-152	0	422	-1061	4.02	4.02	4.02	4.02	2	0.18	0.04	0.23	0.00	0.00	22.3
3	452	3121	-1286	-143	0	402	-1055	4.02	4.02	4.02	4.02	2	0.18	0.04	0.23	0.00	0.00	22.3
4	452	1624	-874	-154	0	430	724	4.02	4.02	4.02	4.02	2	0.13	0.03	0.16	0.00	0.00	22.3
5	452	1544	-872	-145	0	410	728	4.02	4.02	4.02	4.02	2	0.12	0.03	0.16	0.00	0.00	22.3
6	452	2742	-1146	-162	0	449	-752	4.02	4.02	4.02	4.02	2	0.14	0.03	0.20	0.00	0.00	22.3
7	452	2476	-1138	-134	0	381	-734	4.02	4.02	4.02	4.02	2	0.12	0.03	0.20	0.00	0.00	22.3
8	452	2269	-1022	-163	0	451	552	4.02	4.02	4.02	4.02	2	0.13	0.03	0.18	0.00	0.00	22.3
9	452	2003	-1014	-135	0	383	563	4.02	4.02	4.02	4.02	2	0.11	0.03	0.18	0.00	0.00	22.3
10	452	3201	-1289	-152	0	422	-1061	4.02	4.02	4.02	4.02	2	0.18	0.04	0.23	0.00	0.00	22.3
11	452	3121	-1286	-143	0	402	-1055	4.02	4.02	4.02	4.02	2	0.18	0.04	0.23	0.00	0.00	22.3
12	452	1624	-874	-154	0	430	724	4.02	4.02	4.02	4.02	2	0.13	0.03	0.16	0.00	0.00	22.3
13	452	1544	-872	-145	0	410	728	4.02	4.02	4.02	4.02	2	0.12	0.03	0.16	0.00	0.00	22.3
14	452	2742	-1146	-162	0	449	-752	4.02	4.02	4.02	4.02	2	0.14	0.03	0.20	0.00	0.00	22.3
15	452	2476	-1138	-134	0	381	-734	4.02	4.02	4.02	4.02	2	0.12	0.03	0.20	0.00	0.00	22.3
16	452	2269	-1022	-163	0	451	552	4.02	4.02	4.02	4.02	2	0.13	0.03	0.18	0.00	0.00	22.3
17	452	2003	-1014	-135	0	383	563	4.02	4.02	4.02	4.02	2	0.11	0.03	0.18	0.00	0.00	22.3
18	452	7335	-1913	-406	0	1112	-1898	4.02	4.02	4.02	4.02	3	0.35	0.06	0.34	0.00	0.00	22.3
19	452	3234	-820	-451	0	1274	1302	4.02	4.02	4.02	4.02	3	0.34	0.02	0.15	0.00	0.00	22.3
20	452	4858	-1371	-378	0	1095	-718	4.02	4.02	4.02	4.02	3	0.31	0.04	0.24	0.00	0.00	22.3
37	452	7929	-2289	-315	0	849	-2717	4.02	4.02	4.02	4.02	3	0.51	0.07	0.41	0.00	0.00	22.3
38	452	1095	-469	-390	0	1117	1616	4.02	4.02	4.02	4.02	3	0.28	0.01	0.08	0.00	0.00	22.3
39	452	3801	-1386	-269	0	820	-749	4.02	4.02	4.02	4.02	3	0.22	0.04	0.25	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	509	3084	-1855	-193	0	650	-1940	4.02	4.02	4.02	4.02	3	0.31	0.05	0.33	0.00	0.00	22.3
2	509	3201	-1636	-152	0	508	-2063	4.02	4.02	4.02	4.02	2	0.35	0.05	0.29	0.00	0.00	22.3
3	509	3121	-1633	-143	0	483	-2055	4.02	4.02	4.02	4.02	2	0.34	0.05	0.29	0.00	0.00	22.3
4	509	1624	-1221	-154	0	517	-929	4.02	4.02	4.02	4.02	2	0.15	0.04	0.22	0.00	0.00	22.3
5	509	1544	-1219	-145	0	492	-922	4.02	4.02	4.02	4.02	2	0.15	0.04	0.22	0.00	0.00	22.3
6	509	2742	-1493	-162	0	540	-1674	4.02	4.02	4.02	4.02	2	0.28	0.04	0.27	0.00	0.00	22.3
7	509	2476	-1485	-134	0	457	-1651	4.02	4.02	4.02	4.02	2	0.27	0.04	0.26	0.00	0.00	22.3
8	509	2269	-1369	-163	0	543	-1334	4.02	4.02	4.02	4.02	2	0.22	0.04	0.24	0.00	0.00	22.3
9	509	2003	-1361	-135	0	459	-1310	4.02	4.02	4.02	4.02	2	0.21	0.04	0.24	0.00	0.00	22.3
10	509	3201	-1636	-152	0	508	-2063	4.02	4.02	4.02	4.02	2	0.35	0.05	0.29	0.00	0.00	22.3
11	509	3121	-1633	-143	0	483	-2055	4.02	4.02	4.02	4.02	2	0.34	0.05	0.29	0.00	0.00	22.3
12	509	1624	-1221	-154	0	517	-929	4.02	4.02	4.02	4.02	2	0.15	0.04	0.22	0.00	0.00	22.3
13	509	1544	-1219	-145	0	492	-922	4.02	4.02	4.02	4.02	2	0.15	0.04	0.22	0.00	0.00	22.3
14	509	2742	-1493	-162	0	540	-1674	4.02	4.02	4.02	4.02	2	0.28	0.04	0.27	0.00	0.00	22.3
15	509	2476	-1485	-134	0	457	-1651	4.02	4.02	4.02	4.02	2	0.27	0.04	0.26	0.00	0.00	22.3
16	509	2269	-1369	-163	0	543	-1334	4.02	4.02	4.02	4.02	2	0.22	0.04	0.24	0.00	0.00	22.3
17	509	2003	-1361	-135	0	459	-1310	4.02	4.02	4.02	4.02	2	0.21	0.04	0.24	0.00	0.00	22.3
18	509	7335	-2364	-406	0	1342	-3335	4.02	4.02	4.02	4.02	3	0.61	0.07	0.42	0.00	0.00	22.3
19	509	3234	-1271	-451	0	1528	946	4.02	4.02	4.02	4.02	3	0.41	0.04	0.23	0.00	0.00	22.3
20	509	4858	-1822	-378	0	1308	-1848	4.02	4.02	4.02	4.02	3	0.37	0.05	0.32	0.00	0.00	22.3

37	509	7929	-2740	-315	0	1027	-4366	4.02	4.02	4.02	4.02	3	0.82	0.08	0.49	0.00	0.00	22.3
38	509	1095	-919	-390	0	1338	1554	4.02	4.02	4.02	4.02	3	0.34	0.03	0.16	0.00	0.00	22.3
39	509	3801	-1837	-269	0	972	-1888	4.02	4.02	4.02	4.02	3	0.30	0.05	0.33	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	565	3084	-2299	-193	0	759	-2175	4.02	4.02	4.02	4.02	3	0.34	0.07	0.41	0.00	0.00	22.3
2	565	3201	-1977	-152	0	593	-2256	4.02	4.02	4.02	4.02	2	0.38	0.06	0.35	0.00	0.00	22.3
3	565	3121	-1974	-143	0	564	-2248	4.02	4.02	4.02	4.02	2	0.38	0.06	0.35	0.00	0.00	22.3
4	565	1624	-1562	-154	0	604	-1097	4.02	4.02	4.02	4.02	2	0.18	0.05	0.28	0.00	0.00	22.3
5	565	1544	-1560	-145	0	574	-1090	4.02	4.02	4.02	4.02	2	0.17	0.05	0.28	0.00	0.00	22.3
6	565	2742	-1834	-162	0	632	-1858	4.02	4.02	4.02	4.02	2	0.31	0.05	0.33	0.00	0.00	22.3
7	565	2476	-1826	-134	0	532	-1835	4.02	4.02	4.02	4.02	2	0.30	0.05	0.33	0.00	0.00	22.3
8	565	2269	-1710	-163	0	635	-1511	4.02	4.02	4.02	4.02	2	0.25	0.05	0.30	0.00	0.00	22.3
9	565	2003	-1702	-135	0	536	-1487	4.02	4.02	4.02	4.02	2	0.24	0.05	0.30	0.00	0.00	22.3
10	565	3201	-1977	-152	0	593	-2256	4.02	4.02	4.02	4.02	2	0.38	0.06	0.35	0.00	0.00	22.3
11	565	3121	-1974	-143	0	564	-2248	4.02	4.02	4.02	4.02	2	0.38	0.06	0.35	0.00	0.00	22.3
12	565	1624	-1562	-154	0	604	-1097	4.02	4.02	4.02	4.02	2	0.18	0.05	0.28	0.00	0.00	22.3
13	565	1544	-1560	-145	0	574	-1090	4.02	4.02	4.02	4.02	2	0.17	0.05	0.28	0.00	0.00	22.3
14	565	2742	-1834	-162	0	632	-1858	4.02	4.02	4.02	4.02	2	0.31	0.05	0.33	0.00	0.00	22.3
15	565	2476	-1826	-134	0	532	-1835	4.02	4.02	4.02	4.02	2	0.30	0.05	0.33	0.00	0.00	22.3
16	565	2269	-1710	-163	0	635	-1511	4.02	4.02	4.02	4.02	2	0.25	0.05	0.30	0.00	0.00	22.3
17	565	2003	-1702	-135	0	536	-1487	4.02	4.02	4.02	4.02	2	0.24	0.05	0.30	0.00	0.00	22.3
18	565	7335	-2807	-406	0	1571	-3599	4.02	4.02	4.02	4.02	3	0.66	0.08	0.50	0.00	0.00	22.3
19	565	3234	-1714	-451	0	1783	-541	4.02	4.02	4.02	4.02	3	0.48	0.05	0.31	0.00	0.00	22.3
20	565	4858	-2265	-378	0	1522	-2081	4.02	4.02	4.02	4.02	3	0.43	0.07	0.40	0.00	0.00	22.3
37	565	7929	-3183	-315	0	1205	-4653	4.02	4.02	4.02	4.02	3	0.87	0.09	0.57	0.00	0.00	22.3
38	565	1095	-1363	-390	0	1558	1133	4.02	4.02	4.02	4.02	3	0.39	0.04	0.24	0.00	0.00	22.3
39	565	3801	-2280	-269	0	1124	-2122	4.02	4.02	4.02	4.02	3	0.34	0.07	0.41	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

Nome travata: **Trave_402_IP1** Descrizione: **Trave_4 1-10-15-20-25**
ASTA NUM. 8 NI 271 NF 266 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y Permanente qy tot.
qy medio: 375.00 160.00 535.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	2740	2021	150	0	-68	-1901	4.02	4.02	4.02	4.02	3	0.30	0.06	0.36	0.00	0.00	22.3
2	0	3613	1216	140	0	2	-665	4.02	4.02	4.02	4.02	2	0.11	0.04	0.22	0.00	0.00	22.3
3	0	3529	1222	130	0	-35	-677	4.02	4.02	4.02	4.02	2	0.11	0.04	0.22	0.00	0.00	22.3
4	0	687	1888	101	0	-69	-2247	4.02	4.02	4.02	4.02	2	0.35	0.05	0.34	0.00	0.00	22.3
5	0	602	1894	91	0	-106	-2259	4.02	4.02	4.02	4.02	2	0.35	0.05	0.34	0.00	0.00	22.3
6	0	2687	1444	138	0	21	-1206	4.02	4.02	4.02	4.02	2	0.20	0.04	0.26	0.00	0.00	22.3
7	0	2406	1464	105	0	-103	-1244	4.02	4.02	4.02	4.02	2	0.20	0.04	0.26	0.00	0.00	22.3
8	0	1809	1646	126	0	-1	-1680	4.02	4.02	4.02	4.02	2	0.27	0.05	0.29	0.00	0.00	22.3
9	0	1528	1666	93	0	-124	-1719	4.02	4.02	4.02	4.02	2	0.27	0.05	0.30	0.00	0.00	22.3
10	0	3613	1216	140	0	2	-665	4.02	4.02	4.02	4.02	2	0.11	0.04	0.22	0.00	0.00	22.3
11	0	3529	1222	130	0	-35	-677	4.02	4.02	4.02	4.02	2	0.11	0.04	0.22	0.00	0.00	22.3
12	0	687	1888	101	0	-69	-2247	4.02	4.02	4.02	4.02	2	0.35	0.05	0.34	0.00	0.00	22.3
13	0	602	1894	91	0	-106	-2259	4.02	4.02	4.02	4.02	2	0.35	0.05	0.34	0.00	0.00	22.3
14	0	2687	1444	138	0	21	-1206	4.02	4.02	4.02	4.02	2	0.20	0.04	0.26	0.00	0.00	22.3
15	0	2406	1464	105	0	-103	-1244	4.02	4.02	4.02	4.02	2	0.20	0.04	0.26	0.00	0.00	22.3
16	0	1809	1646	126	0	-1	-1680	4.02	4.02	4.02	4.02	2	0.27	0.05	0.29	0.00	0.00	22.3
17	0	1528	1666	93	0	-124	-1719	4.02	4.02	4.02	4.02	2	0.27	0.05	0.30	0.00	0.00	22.3
18	0	8421	1054	347	0	-108	773	4.02	4.02	4.02	4.02	3	0.15	0.03	0.19	0.00	0.00	22.3
19	0	807	2716	99	0	-601	-3696	4.02	4.02	4.02	4.02	3	0.54	0.08	0.48	0.00	0.00	22.3
20	0	4239	1908	202	0	-392	-1758	4.02	4.02	4.02	4.02	3	0.29	0.06	0.34	0.00	0.00	22.3
37	0	10290	550	405	0	146	1674	4.02	4.02	4.02	4.02	3	0.34	0.02	0.10	0.00	0.00	22.3
38	0	-2398	3319	-9	0	-675	-5073	4.02	4.02	4.02	4.02	3	0.68	0.10	0.56	0.00	0.00	22.3
39	0	3322	1973	163	0	-328	-1843	4.02	4.02	4.02	4.02	3	0.29	0.06	0.35	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	56	2740	1586	150	0	-152	-1685	4.02	4.02	4.02	4.02	3	0.26	0.05	0.28	0.00	0.00	22.3
2	56	3613	881	140	0	-77	-519	4.02	4.02	4.02	4.02	2	0.09	0.03	0.16	0.00	0.00	22.3
3	56	3529	887	130	0	-109	-531	4.02	4.02	4.02	4.02	2	0.09	0.03	0.16	0.00	0.00	22.3
4	56	687	1553	101	0	-126	-2062	4.02	4.02	4.02	4.02	2	0.32	0.05	0.28	0.00	0.00	22.3
5	56	602	1559	91	0	-157	-2073	4.02	4.02	4.02	4.02	2	0.32	0.05	0.28	0.00	0.00	22.3
6	56	2687	1109	138	0	-57	-1046	4.02	4.02	4.02	4.02	2	0.17	0.03	0.20	0.00	0.00	22.3
7	56	2406	1129	105	0	-163	-1083	4.02	4.02	4.02	4.02	2	0.18	0.03	0.20	0.00	0.00	22.3
8	56	1809	1311	126	0	-72	-1509	4.02	4.02	4.02	4.02	2	0.24	0.04	0.23	0.00	0.00	22.3
9	56	1528	1331	93	0	-177	-1547	4.02	4.02	4.02	4.02	2	0.25	0.04	0.24	0.00	0.00	22.3
10	56	3613	881	140	0	-77	-519	4.02	4.02	4.02	4.02	2	0.09	0.03	0.16	0.00	0.00	22.3
11	56	3529	887	130	0	-109	-531	4.02	4.02	4.02	4.02	2	0.09	0.03	0.16	0.00	0.00	22.3
12	56	687	1553	101	0	-126	-2062	4.02	4.02	4.02	4.02	2	0.32	0.05	0.28	0.00	0.00	22.3
13	56	602	1559	91	0	-157	-2073	4.02	4.02	4.02	4.02	2	0.32	0.05	0.28	0.00	0.00	22.3
14	56	2687	1109	138	0	-57	-1046	4.02	4.02	4.02	4.02	2	0.17	0.03	0.20	0.00	0.00	22.3
15	56	2406	1129	105	0	-163	-1083	4.02	4.02	4.02	4.02	2	0.18	0.03	0.20	0.00	0.00	22.3
16	56	1809	1311	126	0	-72	-1509	4.02	4.02	4.02	4.02	2	0.24	0.04	0.23	0.00	0.00	22.3
17	56	1528	1331	93	0	-177	-1547	4.02	4.02	4.02	4.02	2	0.25	0.04	0.24	0.00	0.00	22.3
18	56	8421	619	347	0	-305	941	4.02	4.02	4.02	4.02	3	0.18	0.02	0.11	0.00	0.00	22.3
19	56	807	2281	99	0	-656	-3440	4.02	4.02	4.02	4.02	3	0.51	0.07	0.41	0.00	0.00	22.3
20	56	4239	1473	202	0	-506	-1549	4.02	4.02	4.02	4.02	3	0.25	0.04	0.26	0.00	0.00	22.3
37	56	10290	115	405	0	-83	1674	4.02	4.02	4.02	4.02	3	0.34	0.01	0.07	0.00	0.00	22.3
38	56	-2398	2884	-9	0	-670	-4781	4.02	4.02	4.02	4.02	3	0.64	0.08	0.49	0.00	0.00	22.3
39	56	3322	1538	163	0	-420	-1630	4.02	4.02	4.02	4.02	3	0.26	0.04	0.27	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	113	2740	1160	150	0	-237	-694	4.02	4.02	4.02	4.02	3	0.11	0.03	0.21	0.00	0.00	22.3
2	113	3613	554	140	0	-156	597	4.02	4.02	4.02	4.02	2	0.10	0.02	0.10	0.00	0.00	22.3
3	113	3529	560	130	0	-182	599	4.02	4.02	4.02	4.02	2	0.10	0.02	0.10	0.00	0.00	22.3
4	113	687	1226	101	0	-182	-1112	4.02	4.02	4.02	4.02	2	0.17	0.04	0.22	0.00	0.00	22.3
5	113	602	1232	91	0	-209	-1120	4.02	4.02	4.02	4.02	2	0.17	0.04	0.22	0.00	0.00	22.3
6	113	2687	782	138	0	-135	445	4.02	4.02	4.02	4.02	2	0.07	0.02	0.14	0.00	0.00	22.3
7	113	2406	802	105	0	-222	439	4.02	4.02	4.02	4.02	2	0.07	0.02	0.14	0.00	0.00	22.3
8	113	1809	984	126	0	-143	-695	4.02	4.02	4.02	4.02	2	0.11	0.03	0.18	0.00	0.00	22.3
9	113	1528	1004	93	0	-230	-722	4.02	4.02	4.02	4.02	2	0.11	0.03	0.18	0.00	0.00	22.3
10	113	3613	554	140	0	-156	597	4.02	4.02	4.02	4.02	2	0.10	0.02	0.10	0.00	0.00	22.3
11	113	3529	560	130	0	-182	599	4.02	4.02	4.02	4.02	2	0.10	0.02	0.10	0.00	0.00	22.3
12	113	687	1226	101	0	-182	-1112	4.02	4.02	4.02	4.02	2	0.17	0.04	0.22	0.00	0.00	22.3

13	113	602	1232	91	0	-209	-1120	4.02	4.02	4.02	4.02	2	0.17	0.04	0.22	0.00	0.00	22.3
14	113	2687	782	138	0	-135	445	4.02	4.02	4.02	4.02	2	0.07	0.02	0.14	0.00	0.00	22.3
15	113	2406	802	105	0	-222	439	4.02	4.02	4.02	4.02	2	0.07	0.02	0.14	0.00	0.00	22.3
16	113	1809	984	126	0	-143	-695	4.02	4.02	4.02	4.02	2	0.11	0.03	0.18	0.00	0.00	22.3
17	113	1528	1004	93	0	-230	-722	4.02	4.02	4.02	4.02	2	0.11	0.03	0.18	0.00	0.00	22.3
18	113	8421	193	347	0	-501	941	4.02	4.02	4.02	4.02	3	0.18	0.01	0.06	0.00	0.00	22.3
19	113	807	1855	99	0	-712	-2056	4.02	4.02	4.02	4.02	3	0.30	0.05	0.33	0.00	0.00	22.3
20	113	4239	1047	202	0	-621	-622	4.02	4.02	4.02	4.02	3	0.17	0.03	0.19	0.00	0.00	22.3
37	113	10290	-311	405	0	-313	1674	4.02	4.02	4.02	4.02	3	0.34	0.01	0.07	0.00	0.00	22.3
38	113	-2398	2458	-9	0	-665	-3057	4.02	4.02	4.02	4.02	3	0.41	0.07	0.41	0.00	0.00	22.3
39	113	3322	1112	163	0	-512	-667	4.02	4.02	4.02	4.02	3	0.14	0.03	0.20	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	169	2740	744	150	0	-322	807	4.02	4.02	4.02	4.02	3	0.13	0.02	0.13	0.00	0.00	22.3
2	169	3613	233	140	0	-235	597	4.02	4.02	4.02	4.02	2	0.10	0.01	0.04	0.00	0.00	22.3
3	169	3529	239	130	0	-256	599	4.02	4.02	4.02	4.02	2	0.10	0.01	0.04	0.00	0.00	22.3
4	169	687	905	101	0	-239	568	4.02	4.02	4.02	4.02	2	0.09	0.03	0.16	0.00	0.00	22.3
5	169	602	911	91	0	-260	570	4.02	4.02	4.02	4.02	2	0.09	0.03	0.16	0.00	0.00	22.3
6	169	2687	461	138	0	-212	572	4.02	4.02	4.02	4.02	2	0.09	0.01	0.08	0.00	0.00	22.3
7	169	2406	481	105	0	-281	587	4.02	4.02	4.02	4.02	2	0.10	0.01	0.09	0.00	0.00	22.3
8	169	1809	663	126	0	-214	603	4.02	4.02	4.02	4.02	2	0.10	0.02	0.12	0.00	0.00	22.3
9	169	1528	683	93	0	-282	608	4.02	4.02	4.02	4.02	2	0.10	0.02	0.12	0.00	0.00	22.3
10	169	3613	233	140	0	-235	597	4.02	4.02	4.02	4.02	2	0.10	0.01	0.04	0.00	0.00	22.3
11	169	3529	239	130	0	-256	599	4.02	4.02	4.02	4.02	2	0.10	0.01	0.04	0.00	0.00	22.3
12	169	687	905	101	0	-239	568	4.02	4.02	4.02	4.02	2	0.09	0.03	0.16	0.00	0.00	22.3
13	169	602	911	91	0	-260	570	4.02	4.02	4.02	4.02	2	0.09	0.03	0.16	0.00	0.00	22.3
14	169	2687	461	138	0	-212	572	4.02	4.02	4.02	4.02	2	0.09	0.01	0.08	0.00	0.00	22.3
15	169	2406	481	105	0	-281	587	4.02	4.02	4.02	4.02	2	0.10	0.01	0.09	0.00	0.00	22.3
16	169	1809	663	126	0	-214	603	4.02	4.02	4.02	4.02	2	0.10	0.02	0.12	0.00	0.00	22.3
17	169	1528	683	93	0	-282	608	4.02	4.02	4.02	4.02	2	0.10	0.02	0.12	0.00	0.00	22.3
18	169	8421	-223	347	0	-697	941	4.02	4.02	4.02	4.02	3	0.22	0.01	0.06	0.00	0.00	22.3
19	169	807	1438	99	0	-768	-916	4.02	4.02	4.02	4.02	3	0.19	0.04	0.26	0.00	0.00	22.3
20	169	4239	631	202	0	-735	636	4.02	4.02	4.02	4.02	3	0.20	0.02	0.11	0.00	0.00	22.3
37	169	10290	-728	405	0	-542	1674	4.02	4.02	4.02	4.02	3	0.34	0.02	0.13	0.00	0.00	22.3
38	169	-2398	2041	-9	0	-659	-1576	4.02	4.02	4.02	4.02	3	0.21	0.06	0.34	0.00	0.00	22.3
39	169	3322	695	163	0	-604	733	4.02	4.02	4.02	4.02	3	0.16	0.02	0.12	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	226	2740	337	150	0	-406	813	4.02	4.02	4.02	4.02	3	0.13	0.01	0.06	0.00	0.00	22.3
2	226	3613	-80	140	0	-314	597	4.02	4.02	4.02	4.02	2	0.10	0.00	0.01	0.00	0.00	22.3
3	226	3529	-74	130	0	-329	599	4.02	4.02	4.02	4.02	2	0.10	0.00	0.01	0.00	0.00	22.3
4	226	687	592	101	0	-296	832	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
5	226	602	598	91	0	-311	837	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
6	226	2687	148	138	0	-290	572	4.02	4.02	4.02	4.02	2	0.09	0.00	0.03	0.00	0.00	22.3
7	226	2406	168	105	0	-340	587	4.02	4.02	4.02	4.02	2	0.10	0.00	0.03	0.00	0.00	22.3
8	226	1809	350	126	0	-285	664	4.02	4.02	4.02	4.02	2	0.11	0.01	0.06	0.00	0.00	22.3
9	226	1528	370	93	0	-335	681	4.02	4.02	4.02	4.02	2	0.11	0.01	0.07	0.00	0.00	22.3
10	226	3613	-80	140	0	-314	597	4.02	4.02	4.02	4.02	2	0.10	0.00	0.01	0.00	0.00	22.3
11	226	3529	-74	130	0	-329	599	4.02	4.02	4.02	4.02	2	0.10	0.00	0.01	0.00	0.00	22.3
12	226	687	592	101	0	-296	832	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
13	226	602	598	91	0	-311	837	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
14	226	2687	148	138	0	-290	572	4.02	4.02	4.02	4.02	2	0.09	0.00	0.03	0.00	0.00	22.3
15	226	2406	168	105	0	-340	587	4.02	4.02	4.02	4.02	2	0.10	0.00	0.03	0.00	0.00	22.3
16	226	1809	350	126	0	-285	664	4.02	4.02	4.02	4.02	2	0.11	0.01	0.06	0.00	0.00	22.3
17	226	1528	370	93	0	-335	681	4.02	4.02	4.02	4.02	2	0.11	0.01	0.07	0.00	0.00	22.3
18	226	8421	-630	347	0	-893	941	4.02	4.02	4.02	4.02	3	0.28	0.02	0.11	0.00	0.00	22.3
19	226	807	1031	99	0	-824	1031	4.02	4.02	4.02	4.02	3	0.21	0.03	0.18	0.00	0.00	22.3
20	226	4239	224	202	0	-849	636	4.02	4.02	4.02	4.02	3	0.23	0.01	0.04	0.00	0.00	22.3
37	226	10290	-1135	405	0	-771	1372	4.02	4.02	4.02	4.02	3	0.28	0.03	0.20	0.00	0.00	22.3
38	226	-2398	1634	-9	0	-654	1322	4.02	4.02	4.02	4.02	3	0.18	0.05	0.28	0.00	0.00	22.3
39	226	3322	288	163	0	-696	733	4.02	4.02	4.02	4.02	3	0.19	0.01	0.05	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	282	2740	-61	150	0	-491	813	4.02	4.02	4.02	4.02	3	0.13	0.00	0.01	0.00	0.00	22.3
2	282	3613	-385	140	0	-393	597	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
3	282	3529	-379	130	0	-402	599	4.02	4.02	4.02	4.02	2	0.13	0.01	0.07	0.00	0.00	22.3
4	282	687	286	101	0	-353	857	4.02	4.02	4.02	4.02	2	0.13	0.01	0.05	0.00	0.00	22.3
5	282	602	292	91	0	-363	865	4.02	4.02	4.02	4.02	2	0.13	0.01	0.05	0.00	0.00	22.3
6	282	2687	-158	138	0	-368	572	4.02	4.02	4.02	4.02	2	0.11	0.00	0.03	0.00	0.00	22.3
7	282	2406	-137	105	0	-400	587	4.02	4.02	4.02	4.02	2	0.12	0.00	0.02	0.00	0.00	22.3
8	282	1809	44	126	0	-356	664	4.02	4.02	4.02	4.02	2	0.11	0.00	0.01	0.00	0.00	22.3
9	282	1528	64	93	0	-388	681	4.02	4.02	4.02	4.02	2	0.11	0.00	0.01	0.00	0.00	22.3
10	282	3613	-385	140	0	-393	597	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
11	282	3529	-379	130	0	-402	599	4.02	4.02	4.02	4.02	2	0.13	0.01	0.07	0.00	0.00	22.3
12	282	687	286	101	0	-353	857	4.02	4.02	4.02	4.02	2	0.13	0.01	0.05	0.00	0.00	22.3
13	282	602	292	91	0	-363	865	4.02	4.02	4.02	4.02	2	0.13	0.01	0.05	0.00	0.00	22.3
14	282	2687	-158	138	0	-368	572	4.02	4.02	4.02	4.02	2	0.11	0.00	0.03	0.00	0.00	22.3
15	282	2406	-137	105	0	-400	587	4.02	4.02	4.02	4.02	2	0.12	0.00	0.02	0.00	0.00	22.3
16	282	1809	44	126	0	-356	664	4.02	4.02	4.02	4.02	2	0.11	0.00	0.01	0.00	0.00	22.3
17	282	1528	64	93	0	-388	681	4.02	4.02	4.02	4.02	2	0.11	0.00	0.01	0.00	0.00	22.3
18	282	8421	-1028	347	0	-1090	742	4.02	4.02	4.02	4.02	3	0.34	0.03	0.18	0.00	0.00	22.3
19	282	807	633	99	0	-880	1258	4.02	4.02	4.02	4.02	3	0.22	0.02	0.11	0.00	0.00	22.3
20	282	4239	-174	202	0	-963	636	4.02	4.02	4.02	4.02	3	0.27	0.01	0.03	0.00	0.00	22.3
37	282	10290	-1533	405	0	-1000	820	4.02	4.02	4.02	4.02	3	0.34	0.04	0.27	0.00	0.00	22.3
38	282	-2398	1236	-9	0	-649	1931	4.02	4.02	4.02	4.02	3	0.26	0.04	0.21	0.00	0.00	22.3
39	282	3322	-110	163	0	-788	733	4.02	4.02	4.02	4.02	3	0.21	0.01	0.03	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	339	2740	-449	150	0	-576	813	4.02	4.02	4.02	4.02	3	0.15	0.01	0.08	0.00	0.00	22.3
2	339	3613	-684	140	0	-472	509	4.02	4.02	4.02	4.02	2	0.15	0.02	0.12	0.00	0.00	22.3
3	339	3529	-678	130	0	-476	515	4.02	4.02	4.02	4.02	2	0.15	0.02	0.12	0.00	0.00	22.3
4	339	687	-13	101	0	-410	857	4.02	4.02	4.02	4.02	2	0.13	0.00	0.00	0.00	0.00	22.3
5	339	602	-7	91	0	-414	865	4.02	4.02	4.02	4.02	2	0.13	0.00	0.00	0.00	0.00	22.3
6	339	2687	-457	138	0	-445	572	4.02	4.02	4.02	4.02	2	0.13	0.01	0.08	0.00	0.00	22.3
7	339	2406	-436	105	0	-459	587	4.02	4.02	4.02	4.02	2	0.14	0.01	0.08	0.00	0.00	22.3
8	339	1809	-255	126	0	-427	664	4.02	4.02	4.02	4.02	2	0.13	0.01	0.05	0.00	0.00	22.3
9	339	1528	-235	93	0	-440	681	4.02	4.02	4.02	4.02	2	0.13	0.01	0.04	0.00	0.00	22.3
10	339	3613	-684	140	0	-472	509	4.02	4.02	4.02	4.02	2	0.15	0.02	0.12	0.00	0.00	22.3
11	339	3529	-678	130	0	-476	515	4.02	4.02	4.02	4.02	2	0.15	0.02	0.12	0.00	0.00	22.3
12	339	687	-13	101	0	-410	857	4.02	4.02	4.02	4.02	2	0.13	0.00	0.00	0.00	0.00	22.3
13	339	602	-7	91	0	-414	865	4.02	4.02	4.02	4.02	2	0.13	0.00	0.00	0.00	0.00	22.3
14	339	2687	-457	138	0	-445	572	4.02	4.02	4.02	4.02	2	0.13	0.01	0.08	0.00	0.00	22.3
15	339	2406	-436	105	0	-459	587	4.02	4.02	4.02	4.02	2	0.14	0.01	0.08	0.00	0.00	22.3
16	339	1809	-255	126	0	-427	664	4.02	4.02	4.02	4.02	2	0.13	0.01	0.05	0.00	0.00	22.3
17	339	1528	-235	93	0	-440	681	4.02	4.02	4.02	4.02	2	0.13	0.01	0.04	0.00	0.00	22.3
18	339	8421	-1416	347	0	-1286	-1186	4.02	4.02	4.02	4.02	3	0.41	0.04	0.25	0.00	0.00	22.3

19	339	807	245	99	0	-936	1258	4.02	4.02	4.02	4.02	3	0.23	0.01	0.04	0.00	0.00	22.3
20	339	4239	-562	202	0	-1077	636	4.02	4.02	4.02	4.02	3	0.30	0.02	0.10	0.00	0.00	22.3
37	339	10290	-1921	405	0	-1229	-1905	4.02	4.02	4.02	4.02	3	0.41	0.06	0.34	0.00	0.00	22.3
38	339	-2398	848	-9	0	-644	2323	4.02	4.02	4.02	4.02	3	0.31	0.02	0.14	0.00	0.00	22.3
39	339	3322	-498	163	0	-880	733	4.02	4.02	4.02	4.02	3	0.24	0.01	0.09	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	395	2740	-828	150	0	-661	727	4.02	4.02	4.02	4.02	3	0.18	0.02	0.15	0.00	0.00	22.3
2	395	3613	-975	140	0	-551	-800	4.02	4.02	4.02	4.02	2	0.17	0.03	0.17	0.00	0.00	22.3
3	395	3529	-969	130	0	-549	-785	4.02	4.02	4.02	4.02	2	0.17	0.03	0.17	0.00	0.00	22.3
4	395	687	-304	101	0	-467	857	4.02	4.02	4.02	4.02	2	0.13	0.01	0.05	0.00	0.00	22.3
5	395	602	-298	91	0	-466	865	4.02	4.02	4.02	4.02	2	0.13	0.01	0.05	0.00	0.00	22.3
6	395	2687	-748	137	0	-523	434	4.02	4.02	4.02	4.02	2	0.16	0.02	0.13	0.00	0.00	22.3
7	395	2406	-727	105	0	-518	464	4.02	4.02	4.02	4.02	2	0.15	0.02	0.13	0.00	0.00	22.3
8	395	1809	-546	126	0	-498	654	4.02	4.02	4.02	4.02	2	0.15	0.02	0.10	0.00	0.00	22.3
9	395	1528	-526	93	0	-493	681	4.02	4.02	4.02	4.02	2	0.14	0.02	0.09	0.00	0.00	22.3
10	395	3613	-975	140	0	-551	-800	4.02	4.02	4.02	4.02	2	0.17	0.03	0.17	0.00	0.00	22.3
11	395	3529	-969	130	0	-549	-785	4.02	4.02	4.02	4.02	2	0.17	0.03	0.17	0.00	0.00	22.3
12	395	687	-304	101	0	-467	857	4.02	4.02	4.02	4.02	2	0.13	0.01	0.05	0.00	0.00	22.3
13	395	602	-298	91	0	-466	865	4.02	4.02	4.02	4.02	2	0.13	0.01	0.05	0.00	0.00	22.3
14	395	2687	-748	137	0	-523	434	4.02	4.02	4.02	4.02	2	0.16	0.02	0.13	0.00	0.00	22.3
15	395	2406	-727	105	0	-518	464	4.02	4.02	4.02	4.02	2	0.15	0.02	0.13	0.00	0.00	22.3
16	395	1809	-546	126	0	-498	654	4.02	4.02	4.02	4.02	2	0.15	0.02	0.10	0.00	0.00	22.3
17	395	1528	-526	93	0	-493	681	4.02	4.02	4.02	4.02	2	0.14	0.02	0.09	0.00	0.00	22.3
18	395	8421	-1795	347	0	-1482	-2285	4.02	4.02	4.02	4.02	3	0.47	0.05	0.32	0.00	0.00	22.3
19	395	807	-134	99	0	-991	1258	4.02	4.02	4.02	4.02	3	0.25	0.00	0.02	0.00	0.00	22.3
20	395	4239	-941	202	0	-1191	478	4.02	4.02	4.02	4.02	3	0.33	0.03	0.17	0.00	0.00	22.3
37	395	10290	-2300	405	0	-1458	-3289	4.02	4.02	4.02	4.02	3	0.68	0.07	0.41	0.00	0.00	22.3
38	395	-2398	469	-9	0	-639	2425	4.02	4.02	4.02	4.02	3	0.32	0.01	0.08	0.00	0.00	22.3
39	395	3322	-877	163	0	-973	616	4.02	4.02	4.02	4.02	3	0.26	0.03	0.16	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	452	2740	-1197	150	0	-745	-871	4.02	4.02	4.02	4.02	3	0.20	0.03	0.21	0.00	0.00	22.3
2	452	3613	-1259	140	0	-630	-1575	4.02	4.02	4.02	4.02	2	0.27	0.04	0.22	0.00	0.00	22.3
3	452	3529	-1253	130	0	-623	-1557	4.02	4.02	4.02	4.02	2	0.26	0.04	0.22	0.00	0.00	22.3
4	452	687	-588	101	0	-524	812	4.02	4.02	4.02	4.02	2	0.15	0.02	0.10	0.00	0.00	22.3
5	452	602	-582	91	0	-517	825	4.02	4.02	4.02	4.02	2	0.15	0.02	0.10	0.00	0.00	22.3
6	452	2687	-1032	138	0	-601	-970	4.02	4.02	4.02	4.02	2	0.18	0.03	0.18	0.00	0.00	22.3
7	452	2406	-1011	105	0	-577	-908	4.02	4.02	4.02	4.02	2	0.17	0.03	0.18	0.00	0.00	22.3
8	452	1809	-830	126	0	-569	-432	4.02	4.02	4.02	4.02	2	0.17	0.02	0.15	0.00	0.00	22.3
9	452	1528	-810	93	0	-546	450	4.02	4.02	4.02	4.02	2	0.16	0.02	0.14	0.00	0.00	22.3
10	452	3613	-1259	140	0	-630	-1575	4.02	4.02	4.02	4.02	2	0.27	0.04	0.22	0.00	0.00	22.3
11	452	3529	-1253	130	0	-623	-1557	4.02	4.02	4.02	4.02	2	0.26	0.04	0.22	0.00	0.00	22.3
12	452	687	-588	101	0	-524	812	4.02	4.02	4.02	4.02	2	0.15	0.02	0.10	0.00	0.00	22.3
13	452	602	-582	91	0	-517	825	4.02	4.02	4.02	4.02	2	0.15	0.02	0.10	0.00	0.00	22.3
14	452	2687	-1032	138	0	-601	-970	4.02	4.02	4.02	4.02	2	0.18	0.03	0.18	0.00	0.00	22.3
15	452	2406	-1011	105	0	-577	-908	4.02	4.02	4.02	4.02	2	0.17	0.03	0.18	0.00	0.00	22.3
16	452	1809	-830	126	0	-569	-432	4.02	4.02	4.02	4.02	2	0.17	0.02	0.15	0.00	0.00	22.3
17	452	1528	-810	93	0	-546	450	4.02	4.02	4.02	4.02	2	0.16	0.02	0.14	0.00	0.00	22.3
18	452	8421	-2164	347	0	-1678	-3591	4.02	4.02	4.02	4.02	3	0.68	0.06	0.39	0.00	0.00	22.3
19	452	807	-503	99	0	-1047	1258	4.02	4.02	4.02	4.02	3	0.26	0.01	0.09	0.00	0.00	22.3
20	452	4239	-1310	202	0	-1305	-1298	4.02	4.02	4.02	4.02	3	0.36	0.04	0.23	0.00	0.00	22.3
37	452	10290	-2669	405	0	-1687	-4880	4.02	4.02	4.02	6.03	3	0.60	0.08	0.42	0.00	0.00	22.3
38	452	-2398	100	-9	0	-634	2425	4.02	4.02	4.02	4.02	3	0.32	0.00	0.02	0.00	0.00	22.3
39	452	3322	-1246	163	0	-1065	-1059	4.02	4.02	4.02	4.02	3	0.29	0.04	0.22	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= 2.01 (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	508	2740	-1557	150	0	-830	-1832	4.02	4.02	4.02	4.02	3	0.29	0.05	0.28	0.00	0.00	22.3
2	508	3613	-1536	140	0	-708	-2506	4.02	4.02	4.02	4.02	2	0.43	0.04	0.27	0.00	0.00	22.3
3	508	3529	-1530	130	0	-696	-2484	4.02	4.02	4.02	4.02	2	0.42	0.04	0.27	0.00	0.00	22.3
4	508	687	-865	101	0	-581	541	4.02	4.02	4.02	4.02	2	0.16	0.03	0.15	0.00	0.00	22.3
5	508	602	-859	91	0	-568	557	4.02	4.02	4.02	4.02	2	0.16	0.02	0.15	0.00	0.00	22.3
6	508	2687	-1309	138	0	-679	-1772	4.02	4.02	4.02	4.02	2	0.29	0.04	0.23	0.00	0.00	22.3
7	508	2406	-1288	105	0	-637	-1699	4.02	4.02	4.02	4.02	2	0.28	0.04	0.23	0.00	0.00	22.3
8	508	1809	-1107	126	0	-640	-1120	4.02	4.02	4.02	4.02	2	0.19	0.03	0.20	0.00	0.00	22.3
9	508	1528	-1087	93	0	-598	-1047	4.02	4.02	4.02	4.02	2	0.17	0.03	0.19	0.00	0.00	22.3
10	508	3613	-1536	140	0	-708	-2506	4.02	4.02	4.02	4.02	2	0.43	0.04	0.27	0.00	0.00	22.3
11	508	3529	-1530	130	0	-696	-2484	4.02	4.02	4.02	4.02	2	0.42	0.04	0.27	0.00	0.00	22.3
12	508	687	-865	101	0	-581	541	4.02	4.02	4.02	4.02	2	0.16	0.03	0.15	0.00	0.00	22.3
13	508	602	-859	91	0	-568	557	4.02	4.02	4.02	4.02	2	0.16	0.02	0.15	0.00	0.00	22.3
14	508	2687	-1309	138	0	-679	-1772	4.02	4.02	4.02	4.02	2	0.29	0.04	0.23	0.00	0.00	22.3
15	508	2406	-1288	105	0	-637	-1699	4.02	4.02	4.02	4.02	2	0.28	0.04	0.23	0.00	0.00	22.3
16	508	1809	-1107	126	0	-640	-1120	4.02	4.02	4.02	4.02	2	0.19	0.03	0.20	0.00	0.00	22.3
17	508	1528	-1087	93	0	-598	-1047	4.02	4.02	4.02	4.02	2	0.17	0.03	0.19	0.00	0.00	22.3
18	508	8421	-2524	347	0	-1875	-5098	4.02	4.02	4.02	4.02	3	0.97	0.07	0.45	0.00	0.00	22.3
19	508	807	-863	99	0	-1103	1128	4.02	4.02	4.02	4.02	3	0.28	0.03	0.15	0.00	0.00	22.3
20	508	4239	-1670	202	0	-1419	-2323	4.02	4.02	4.02	4.02	3	0.39	0.05	0.30	0.00	0.00	22.3
37	508	10290	-3029	405	0	-1916	-6673	4.02	4.02	4.02	6.03	3	0.82	0.09	0.47	0.00	0.00	22.3
38	508	-2398	-260	-9	0	-629	2425	4.02	4.02	4.02	4.02	3	0.32	0.01	0.04	0.00	0.00	22.3
39	508	3322	-1606	163	0	-1157	-2047	4.02	4.02	4.02	4.02	3	0.33	0.05	0.29	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= 2.01 (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	565	2740	-1908	150	0	-915	-2023	4.02	4.02	4.02	4.02	3	0.32	0.06	0.34	0.00	0.00	22.3
2	565	3613	-1806	140	0	-787	-2673	4.02	4.02	4.02	4.02	2	0.46	0.05	0.32	0.00	0.00	22.3
3	565	3529	-1800	130	0	-769	-2651	4.02	4.02	4.02	4.02	2	0.45	0.05	0.32	0.00	0.00	22.3
4	565	687	-1135	101	0	-638	-462	4.02	4.02	4.02	4.02	2	0.18	0.03	0.20	0.00	0.00	22.3
5	565	602	-1129	91	0	-620	-440	4.02	4.02	4.02	4.02	2	0.17	0.03	0.20	0.00	0.00	22.3
6	565	2687	-1579	138	0	-756	-1925	4.02	4.02	4.02	4.02	2	0.32	0.05	0.28	0.00	0.00	22.3
7	565	2406	-1558	105	0	-696	-1851	4.02	4.02	4.02	4.02	2	0.30	0.05	0.28	0.00	0.00	22.3
8	565	1809	-1377	126	0	-711	-1262	4.02	4.02	4.02	4.02	2	0.21	0.04	0.25	0.00	0.00	22.3
9	565	1528	-1357	93	0	-651	-1188	4.02	4.02	4.02	4.02	2	0.19	0.04	0.24	0.00	0.00	22.3
10	565	3613	-1806	140	0	-787	-2673	4.02	4.02	4.02	4.02	2	0.46	0.05	0.32	0.00	0.00	22.3
11	565	3529	-1800	130	0	-769	-2651	4.02	4.02	4.02	4.02	2	0.45	0.05	0.32	0.00	0.00	22.3
12	565	687	-1135	101	0	-638	-462	4.02	4.02	4.02	4.02	2	0.18	0.03	0.20	0.00	0.00	22.3
13	565	602	-1129	91	0	-620	-440	4.02	4.02	4.02	4.02	2	0.17	0.03	0.20	0.00	0.00	22.3
14	565	2687	-1579	138	0	-756	-1925	4.02	4.02	4.02	4.02	2	0.32	0.05	0.28	0.00	0.00	22.3
15	565	2406	-1558	105	0	-696	-1851	4.02	4.02	4.02	4.02	2	0.30	0.05	0.28	0.00	0.00	22.3
16	565	1809	-1377	126	0	-711	-1262	4.02	4.02	4.02	4.02	2	0.21	0.04	0.25	0.00	0.00	22.3
17	565	1528	-1357	93	0	-651	-1188	4.02	4.02	4.02	4.02	2	0.19	0.04	0.24	0.00	0.00	22.3
18	565	8421	-2875	347	0	-2071	-5346	4.02	4.02	4.02	6.03	3	0.65	0.08	0.45	0.00	0.00	22.3
19	565	807	-1214	99	0	-1159	718	4.02	4.02	4.02	4.02	3	0.29	0.04	0.22	0.00	0.00	22.3
20	565	4239	-2021	202	0	-1533	-2521	4.02	4.02	4.02	4.02	3	0.42	0.06	0.36	0.00	0.00	22.3
37	565	10290	-3380	405	0	-2145	-6950	4.02	4.02	4.02	6.03	3	0.86	0.10	0.53	0.00	0.00	22.3
38	565	-2398	-611	-9	0	-624	2425	4.02	4.02	4.02	4.02	3	0.32	0.02	0.10	0.00	0.00	22.3
39	565	3322	-1957	163	0	-1249	-2241	4.02	4.02	4.02	4.02	3	0.36	0.06	0.35	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= 2.01 (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

Nome travata: **Trave_403_IP1** Descrizione: **Trave_4 7-6-5-4-3-2-1**
ASTA NUM. 9 NI 25 NF 215 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y Permanente qy tot.
qy medio: 375.00 132.00 507.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	165	2018	-671	0	-2093	-2084	4.02	4.02	4.02	4.02	3	0.52	0.06	0.36	0.00	0.00	22.3
2	0	635	1557	-408	0	-1220	-1616	4.02	4.02	4.02	4.02	2	0.34	0.05	0.28	0.00	0.00	22.3
3	0	-73	1583	-464	0	-1446	-1674	4.02	4.02	4.02	4.02	2	0.40	0.05	0.28	0.00	0.00	22.3
4	0	327	1522	-568	0	-1774	-1532	4.02	4.02	4.02	4.02	2	0.49	0.04	0.27	0.00	0.00	22.3
5	0	-381	1548	-623	0	-2001	-1591	4.02	4.02	4.02	4.02	2	0.55	0.04	0.27	0.00	0.00	22.3
6	0	1353	1514	-400	0	-1150	-1519	4.02	4.02	4.02	4.02	2	0.33	0.04	0.27	0.00	0.00	22.3
7	0	-1007	1601	-584	0	-1905	-1713	4.02	4.02	4.02	4.02	2	0.51	0.05	0.28	0.00	0.00	22.3
8	0	1261	1503	-448	0	-1316	-1494	4.02	4.02	4.02	4.02	2	0.38	0.04	0.27	0.00	0.00	22.3
9	0	-1100	1591	-632	0	-2071	-1688	4.02	4.02	4.02	4.02	2	0.55	0.05	0.28	0.00	0.00	22.3
10	0	635	1557	-408	0	-1220	-1616	4.02	4.02	4.02	4.02	2	0.34	0.05	0.28	0.00	0.00	22.3
11	0	-73	1583	-464	0	-1446	-1674	4.02	4.02	4.02	4.02	2	0.40	0.05	0.28	0.00	0.00	22.3
12	0	327	1522	-568	0	-1774	-1532	4.02	4.02	4.02	4.02	2	0.49	0.04	0.27	0.00	0.00	22.3
13	0	-381	1548	-623	0	-2001	-1591	4.02	4.02	4.02	4.02	2	0.55	0.04	0.27	0.00	0.00	22.3
14	0	1353	1514	-400	0	-1150	-1519	4.02	4.02	4.02	4.02	2	0.33	0.04	0.27	0.00	0.00	22.3
15	0	-1007	1601	-584	0	-1905	-1713	4.02	4.02	4.02	4.02	2	0.51	0.05	0.28	0.00	0.00	22.3
16	0	1261	1503	-448	0	-1316	-1494	4.02	4.02	4.02	4.02	2	0.38	0.04	0.27	0.00	0.00	22.3
17	0	-1100	1591	-632	0	-2071	-1688	4.02	4.02	4.02	4.02	2	0.55	0.05	0.28	0.00	0.00	22.3
18	0	1460	2060	-1186	0	-3643	-2182	4.02	4.02	4.02	4.02	3	0.93	0.06	0.37	0.00	0.00	22.3
19	0	-21	1903	-1552	0	-4938	-1809	4.02	6.03	4.02	4.02	3	0.86	0.06	0.34	0.00	0.00	22.3
20	0	658	1941	-1471	0	-4811	-1824	4.02	6.03	4.02	4.02	3	0.85	0.06	0.35	0.00	0.00	22.3
37	0	1770	2124	-837	0	-2499	-2337	4.02	4.02	4.02	4.02	3	0.64	0.06	0.38	0.00	0.00	22.3
38	0	-698	1864	-1447	0	-4656	-1715	4.02	6.03	4.02	4.02	3	0.80	0.05	0.33	0.00	0.00	22.3
39	0	433	1925	-1311	0	-4444	-1741	4.02	6.03	4.02	4.02	3	0.78	0.06	0.34	0.00	0.00	22.3

apost= -- aant= 2.01 ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	60	165	1622	-671	0	-1691	-1813	4.02	4.02	4.02	4.02	3	0.42	0.05	0.29	0.00	0.00	22.3
2	60	635	1253	-408	0	-975	-1408	4.02	4.02	4.02	4.02	2	0.27	0.04	0.22	0.00	0.00	22.3
3	60	-73	1279	-464	0	-1168	-1463	4.02	4.02	4.02	4.02	2	0.32	0.04	0.23	0.00	0.00	22.3
4	60	327	1218	-568	0	-1433	-1327	4.02	4.02	4.02	4.02	2	0.40	0.04	0.22	0.00	0.00	22.3
5	60	-381	1244	-623	0	-1627	-1383	4.02	4.02	4.02	4.02	2	0.44	0.04	0.22	0.00	0.00	22.3
6	60	1353	1210	-400	0	-910	-1315	4.02	4.02	4.02	4.02	2	0.26	0.04	0.22	0.00	0.00	22.3
7	60	-1007	1297	-584	0	-1555	-1500	4.02	4.02	4.02	4.02	2	0.42	0.04	0.23	0.00	0.00	22.3
8	60	1261	1199	-448	0	-1047	-1290	4.02	4.02	4.02	4.02	2	0.30	0.03	0.21	0.00	0.00	22.3
9	60	-1100	1287	-632	0	-1692	-1476	4.02	4.02	4.02	4.02	2	0.45	0.04	0.22	0.00	0.00	22.3
10	60	635	1253	-408	0	-975	-1408	4.02	4.02	4.02	4.02	2	0.27	0.04	0.22	0.00	0.00	22.3
11	60	-73	1279	-464	0	-1168	-1463	4.02	4.02	4.02	4.02	2	0.32	0.04	0.23	0.00	0.00	22.3
12	60	327	1218	-568	0	-1433	-1327	4.02	4.02	4.02	4.02	2	0.40	0.04	0.22	0.00	0.00	22.3
13	60	-381	1244	-623	0	-1627	-1383	4.02	4.02	4.02	4.02	2	0.44	0.04	0.22	0.00	0.00	22.3
14	60	1353	1210	-400	0	-910	-1315	4.02	4.02	4.02	4.02	2	0.26	0.04	0.22	0.00	0.00	22.3
15	60	-1007	1297	-584	0	-1555	-1500	4.02	4.02	4.02	4.02	2	0.42	0.04	0.23	0.00	0.00	22.3
16	60	1261	1199	-448	0	-1047	-1290	4.02	4.02	4.02	4.02	2	0.30	0.03	0.21	0.00	0.00	22.3
17	60	-1100	1287	-632	0	-1692	-1476	4.02	4.02	4.02	4.02	2	0.45	0.04	0.22	0.00	0.00	22.3
18	60	1460	1664	-1186	0	-2931	-1907	4.02	4.02	4.02	4.02	3	0.75	0.05	0.30	0.00	0.00	22.3
19	60	-21	1508	-1552	0	-4007	-1549	4.02	4.02	4.02	4.02	3	0.98	0.05	0.27	0.00	0.00	22.3
20	60	658	1546	-1471	0	-3929	-1561	4.02	4.02	4.02	4.02	3	0.98	0.05	0.28	0.00	0.00	22.3
37	60	1770	1729	-837	0	-1997	-2056	4.02	4.02	4.02	4.02	3	0.51	0.05	0.31	0.00	0.00	22.3
38	60	-698	1468	-1447	0	-3788	-1459	4.02	4.02	4.02	4.02	3	0.91	0.05	0.26	0.00	0.00	22.3
39	60	433	1530	-1311	0	-3657	-1479	4.02	4.02	4.02	4.02	3	0.91	0.04	0.27	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	120	165	1227	-671	0	-1288	-758	4.02	4.02	4.02	4.02	3	0.32	0.04	0.22	0.00	0.00	22.3
2	120	635	949	-408	0	-730	-593	4.02	4.02	4.02	4.02	2	0.21	0.03	0.17	0.00	0.00	22.3
3	120	-73	975	-464	0	-890	-633	4.02	4.02	4.02	4.02	2	0.24	0.03	0.17	0.00	0.00	22.3
4	120	327	914	-568	0	-1092	-534	4.02	4.02	4.02	4.02	2	0.30	0.03	0.16	0.00	0.00	22.3
5	120	-381	940	-623	0	-1253	-574	4.02	4.02	4.02	4.02	2	0.34	0.03	0.17	0.00	0.00	22.3
6	120	1353	906	-400	0	-670	-526	4.02	4.02	4.02	4.02	2	0.19	0.03	0.16	0.00	0.00	22.3
7	120	-1007	993	-584	0	-1204	-659	4.02	4.02	4.02	4.02	2	0.32	0.03	0.17	0.00	0.00	22.3
8	120	1261	895	-448	0	-779	-508	4.02	4.02	4.02	4.02	2	0.22	0.03	0.16	0.00	0.00	22.3
9	120	-1100	983	-632	0	-1313	-641	4.02	4.02	4.02	4.02	2	0.35	0.03	0.17	0.00	0.00	22.3
10	120	635	949	-408	0	-730	-593	4.02	4.02	4.02	4.02	2	0.21	0.03	0.17	0.00	0.00	22.3
11	120	-73	975	-464	0	-890	-633	4.02	4.02	4.02	4.02	2	0.24	0.03	0.17	0.00	0.00	22.3
12	120	327	914	-568	0	-1092	-534	4.02	4.02	4.02	4.02	2	0.30	0.03	0.16	0.00	0.00	22.3
13	120	-381	940	-623	0	-1253	-574	4.02	4.02	4.02	4.02	2	0.34	0.03	0.17	0.00	0.00	22.3
14	120	1353	906	-400	0	-670	-526	4.02	4.02	4.02	4.02	2	0.19	0.03	0.16	0.00	0.00	22.3
15	120	-1007	993	-584	0	-1204	-659	4.02	4.02	4.02	4.02	2	0.32	0.03	0.17	0.00	0.00	22.3
16	120	1261	895	-448	0	-779	-508	4.02	4.02	4.02	4.02	2	0.22	0.03	0.16	0.00	0.00	22.3
17	120	-1100	983	-632	0	-1313	-641	4.02	4.02	4.02	4.02	2	0.35	0.03	0.17	0.00	0.00	22.3
18	120	1460	1269	-1186	0	-2220	-827	4.02	4.02	4.02	4.02	3	0.57	0.04	0.23	0.00	0.00	22.3
19	120	-21	1112	-1552	0	-3075	564	4.02	4.02	4.02	4.02	3	0.76	0.05	0.25	0.00	0.00	22.3
20	120	658	1150	-1471	0	-3046	612	4.02	4.02	4.02	4.02	3	0.76	0.05	0.24	0.00	0.00	22.3
37	120	1770	1333	-837	0	-1494	-937	4.02	4.02	4.02	4.02	3	0.39	0.04	0.24	0.00	0.00	22.3
38	120	-698	1073	-1447	0	-2919	590	4.02	4.02	4.02	4.02	3	0.70	0.05	0.23	0.00	0.00	22.3
39	120	433	1134	-1311	0	-2870	669	4.02	4.02	4.02	4.02	3	0.71	0.04	0.21	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	180	165	832	-671	0	-886	902	4.02	4.02	4.02	4.02	3	0.22	0.02	0.15	0.00	0.00	22.3
2	180	635	644	-408	0	-485	691	4.02	4.02	4.02	4.02	2	0.14	0.02	0.11	0.00	0.00	22.3
3	180	-73	670	-464	0	-612	693	4.02	4.02	4.02	4.02	2	0.17	0.02	0.12	0.00	0.00	22.3
4	180	327	609	-568	0	-751	694	4.02	4.02	4.02	4.02	2	0.21	0.02	0.11	0.00	0.00	22.3
5	180	-381	635	-623	0	-879	696	4.02	4.02	4.02	4.02	2	0.24	0.02	0.11	0.00	0.00	22.3
6	180	1353	601	-400	0	-430	689	4.02	4.02	4.02	4.02	2	0.12	0.02	0.11	0.00	0.00	22.3
7	180	-1007	688	-584	0	-854	697	4.02	4.02	4.02	4.02	2	0.23	0.02	0.12	0.00	0.00	22.3
8	180	1261	590	-448	0	-510	689	4.02	4.02	4.02	4.02	2	0.15	0.02	0.11	0.00	0.00	22.3
9	180	-1100	678	-632	0	-933	698	4.02	4.02	4.02	4.02	2	0.25	0.02	0.12	0.00	0.00	22.3
10	180	635	644	-408	0	-485	691	4.02	4.02	4.02	4.02	2	0.14	0.02	0.11	0.00	0.00	22.3
11	180	-73	670	-464	0	-612	693	4.02	4.02	4.02	4.02	2	0.17	0.02	0.12	0.00	0.00	22.3
12	180	327	609	-568	0	-751	694	4.02	4.02	4.02	4.02	2	0.21	0.02	0.11	0.00	0.00	22.3
13	180	-381	635	-623	0	-879	696	4.02	4.02	4.02	4.02	2	0.24	0.02	0.11	0.00	0.00	22.3
14	180	1353	601	-400	0	-430	689	4.02	4.02	4.02	4.02	2	0.12	0.02	0.11	0.00	0.00	22.3
15	180	-1007	688	-584	0	-854	697	4.02	4.02	4.02	4.02	2	0.23	0.02	0.12	0.00	0.00	22.3
16	180	1261	590	-448	0	-510	689	4.02	4.02	4.02	4.02	2	0.15	0.02	0.11	0.00	0.00	22.3

17	180	-1100	678	-632	0	-933	698	4.02	4.02	4.02	4.02	2	0.25	0.02	0.12	0.00	0.00	22.3
18	180	1460	874	-1186	0	-1508	900	4.02	4.02	4.02	4.02	3	0.39	0.04	0.19	0.00	0.00	22.3
19	180	-21	717	-1552	0	-2144	912	4.02	4.02	4.02	4.02	3	0.53	0.05	0.25	0.00	0.00	22.3
20	180	658	755	-1471	0	-2164	983	4.02	4.02	4.02	4.02	3	0.54	0.05	0.24	0.00	0.00	22.3
37	180	1770	938	-837	0	-992	894	4.02	4.02	4.02	4.02	3	0.26	0.03	0.17	0.00	0.00	22.3
38	180	-698	677	-1447	0	-2050	909	4.02	4.02	4.02	4.02	3	0.49	0.05	0.23	0.00	0.00	22.3
39	180	433	739	-1311	0	-2084	1031	4.02	4.02	4.02	4.02	3	0.52	0.04	0.21	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	240	165	436	-671	0	-484	1004	4.02	4.02	4.02	4.02	3	0.14	0.02	0.11	0.00	0.00	22.3
2	240	635	340	-408	0	-240	772	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
3	240	-73	366	-464	0	-334	793	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
4	240	327	305	-568	0	-410	752	4.02	4.02	4.02	4.02	2	0.12	0.02	0.09	0.00	0.00	22.3
5	240	-381	331	-623	0	-505	772	4.02	4.02	4.02	4.02	2	0.14	0.02	0.10	0.00	0.00	22.3
6	240	1353	297	-400	0	-190	741	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
7	240	-1007	384	-584	0	-503	810	4.02	4.02	4.02	4.02	2	0.13	0.02	0.09	0.00	0.00	22.3
8	240	1261	286	-448	0	-241	734	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
9	240	-1100	374	-632	0	-554	804	4.02	4.02	4.02	4.02	2	0.15	0.02	0.10	0.00	0.00	22.3
10	240	635	340	-408	0	-240	772	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
11	240	-73	366	-464	0	-334	793	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
12	240	327	305	-568	0	-410	752	4.02	4.02	4.02	4.02	2	0.12	0.02	0.09	0.00	0.00	22.3
13	240	-381	331	-623	0	-505	772	4.02	4.02	4.02	4.02	2	0.14	0.02	0.10	0.00	0.00	22.3
14	240	1353	297	-400	0	-190	741	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
15	240	-1007	384	-584	0	-503	810	4.02	4.02	4.02	4.02	2	0.13	0.02	0.09	0.00	0.00	22.3
16	240	1261	286	-448	0	-241	734	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
17	240	-1100	374	-632	0	-554	804	4.02	4.02	4.02	4.02	2	0.15	0.02	0.10	0.00	0.00	22.3
18	240	1460	478	-1186	0	-796	1031	4.02	4.02	4.02	4.02	3	0.20	0.04	0.19	0.00	0.00	22.3
19	240	-21	321	-1552	0	-1212	935	4.02	4.02	4.02	4.02	3	0.30	0.05	0.25	0.00	0.00	22.3
20	240	658	359	-1471	0	-1281	1031	4.02	4.02	4.02	4.02	3	0.32	0.05	0.24	0.00	0.00	22.3
37	240	1770	542	-837	0	-490	1070	4.02	4.02	4.02	4.02	3	0.16	0.03	0.13	0.00	0.00	22.3
38	240	-698	282	-1447	0	-1182	909	4.02	4.02	4.02	4.02	3	0.29	0.05	0.23	0.00	0.00	22.3
39	240	433	343	-1311	0	-1297	1069	4.02	4.02	4.02	4.02	3	0.32	0.04	0.21	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	300	165	40	-671	0	-82	1004	4.02	4.02	4.02	4.02	3	0.14	0.02	0.11	0.00	0.00	22.3
2	300	635	36	-408	0	5	772	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
3	300	-73	62	-464	0	-56	793	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
4	300	327	1	-568	0	-70	752	4.02	4.02	4.02	4.02	2	0.12	0.02	0.09	0.00	0.00	22.3
5	300	-381	27	-623	0	-130	772	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
6	300	1353	-7	-400	0	50	741	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
7	300	-1007	80	-584	0	-153	810	4.02	4.02	4.02	4.02	2	0.12	0.02	0.09	0.00	0.00	22.3
8	300	1261	-18	-448	0	27	734	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
9	300	-1100	70	-632	0	-175	804	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
10	300	635	36	-408	0	5	772	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
11	300	-73	62	-464	0	-56	793	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
12	300	327	1	-568	0	-70	752	4.02	4.02	4.02	4.02	2	0.12	0.02	0.09	0.00	0.00	22.3
13	300	-381	27	-623	0	-130	772	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
14	300	1353	-7	-400	0	50	741	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
15	300	-1007	80	-584	0	-153	810	4.02	4.02	4.02	4.02	2	0.12	0.02	0.09	0.00	0.00	22.3
16	300	1261	-18	-448	0	27	734	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
17	300	-1100	70	-632	0	-175	804	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
18	300	1460	82	-1186	0	-85	1031	4.02	4.02	4.02	4.02	3	0.15	0.04	0.19	0.00	0.00	22.3
19	300	-21	-74	-1552	0	-281	935	4.02	4.02	4.02	4.02	3	0.13	0.05	0.25	0.00	0.00	22.3
20	300	658	-36	-1471	0	-399	1031	4.02	4.02	4.02	4.02	3	0.15	0.05	0.24	0.00	0.00	22.3
37	300	1770	147	-837	0	12	1070	4.02	4.02	4.02	4.02	3	0.16	0.03	0.13	0.00	0.00	22.3
38	300	-698	-114	-1447	0	-314	909	4.02	4.02	4.02	4.02	3	0.13	0.05	0.23	0.00	0.00	22.3
39	300	433	-52	-1311	0	-510	1069	4.02	4.02	4.02	4.02	3	0.16	0.04	0.21	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	360	165	-355	-671	0	321	1004	4.02	4.02	4.02	4.02	3	0.14	0.02	0.11	0.00	0.00	22.3
2	360	635	-268	-408	0	250	772	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
3	360	-73	-242	-464	0	223	793	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
4	360	327	-303	-568	0	271	752	4.02	4.02	4.02	4.02	2	0.12	0.02	0.09	0.00	0.00	22.3
5	360	-381	-277	-623	0	244	772	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
6	360	1353	-311	-400	0	289	741	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
7	360	-1007	-224	-584	0	197	810	4.02	4.02	4.02	4.02	2	0.12	0.02	0.09	0.00	0.00	22.3
8	360	1261	-322	-448	0	296	734	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
9	360	-1100	-234	-632	0	204	804	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
10	360	635	-268	-408	0	250	772	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
11	360	-73	-242	-464	0	223	793	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
12	360	327	-303	-568	0	271	752	4.02	4.02	4.02	4.02	2	0.12	0.02	0.09	0.00	0.00	22.3
13	360	-381	-277	-623	0	244	772	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
14	360	1353	-311	-400	0	289	741	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
15	360	-1007	-224	-584	0	197	810	4.02	4.02	4.02	4.02	2	0.12	0.02	0.09	0.00	0.00	22.3
16	360	1261	-322	-448	0	296	734	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
17	360	-1100	-234	-632	0	204	804	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
18	360	1460	-313	-1186	0	627	1031	4.02	4.02	4.02	4.02	3	0.16	0.04	0.19	0.00	0.00	22.3
19	360	-21	-469	-1552	0	650	935	4.02	4.02	4.02	4.02	3	0.16	0.05	0.25	0.00	0.00	22.3
20	360	658	-432	-1471	0	483	1031	4.02	4.02	4.02	4.02	3	0.15	0.05	0.24	0.00	0.00	22.3
37	360	1770	-248	-837	0	515	1070	4.02	4.02	4.02	4.02	3	0.16	0.03	0.13	0.00	0.00	22.3
38	360	-698	-509	-1447	0	555	909	4.02	4.02	4.02	4.02	3	0.13	0.05	0.23	0.00	0.00	22.3
39	360	433	-447	-1311	0	277	1069	4.02	4.02	4.02	4.02	3	0.16	0.04	0.21	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	420	165	-750	-671	0	723	958	4.02	4.02	4.02	4.02	3	0.18	0.02	0.13	0.00	0.00	22.3
2	420	635	-572	-408	0	495	739	4.02	4.02	4.02	4.02	2	0.14	0.02	0.10	0.00	0.00	22.3
3	420	-73	-546	-464	0	501	779	4.02	4.02	4.02	4.02	2	0.14	0.02	0.10	0.00	0.00	22.3
4	420	327	-607	-568	0	612	695	4.02	4.02	4.02	4.02	2	0.17	0.02	0.11	0.00	0.00	22.3
5	420	-381	-581	-623	0	618	734	4.02	4.02	4.02	4.02	2	0.17	0.02	0.10	0.00	0.00	22.3
6	420	1353	-615	-400	0	529	678	4.02	4.02	4.02	4.02	2	0.15	0.02	0.11	0.00	0.00	22.3
7	420	-1007	-528	-584	0	548	809	4.02	4.02	4.02	4.02	2	0.15	0.02	0.09	0.00	0.00	22.3
8	420	1261	-626	-448	0	565	665	4.02	4.02	4.02	4.02	2	0.16	0.02	0.11	0.00	0.00	22.3
9	420	-1100	-538	-632	0	583	795	4.02	4.02	4.02	4.02	2	0.16	0.02	0.10	0.00	0.00	22.3
10	420	635	-572	-408	0	495	739	4.02	4.02	4.02	4.02	2	0.14	0.02	0.10	0.00	0.00	22.3
11	420	-73	-546	-464	0	501	779	4.02	4.02	4.02	4.02	2	0.14	0.02	0.10	0.00	0.00	22.3
12	420	327	-607	-568	0	612	695	4.02	4.02	4.02	4.02	2	0.17	0.02	0.11	0.00	0.00	22.3
13	420	-381	-581	-623	0	618	734	4.02	4.02	4.02	4.02	2	0.17	0.02	0.10	0.00	0.00	22.3
14	420	1353	-615	-400	0	529	678	4.02	4.02	4.02	4.02	2	0.15	0.02	0.11	0.00	0.00	22.3
15	420	-1007	-528	-584	0	548	809	4.02	4.02	4.02	4.02	2	0.15	0.02	0.09	0.00	0.00	22.3
16	420	1261	-626	-448	0	565	665	4.02	4.02	4.02	4.02	2	0.16	0.02	0.11	0.00	0.00	22.3
17	420	-1100	-538	-632	0	583	795	4.02	4.02	4.02	4.02	2	0.16	0.02	0.10	0.00	0.00	22.3
18	420	1460	-708	-1186	0	1339	1015	4.02	4.02	4.02	4.02	3	0.34	0.04	0.19	0.00	0.00	22.3
19	420	-21	-865	-1552	0	1582	810	4.02	4.02	4.02	4.02	3	0.39	0.05	0.25	0.00	0.00	22.3
20	420	658	-827	-1471	0	1366	932	4.02	4.02	4.02	4.02	3	0.34	0.05	0.24	0.00	0.00	22.3
37	420	1770	-644	-837	0	1017	1070	4.02	4.02	4.02	4.02	3	0.26	0.03	0.13	0.00	0.00	22.3
38	420	-698	-904	-1447	0	1424	756	4.02	4.02	4.02	4.02	3	0.34	0.05	0.23	0.00	0.00	22.3

39	420	433	-843	-1311	0	1064	959	4.02	4.02	4.02	4.02	3	0.26	0.04	0.21	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	480	165	-1146	-671	0	1125	590	4.02	4.02	4.02	4.02	3	0.28	0.03	0.20	0.00	0.00	22.3
2	480	635	-877	-408	0	740	458	4.02	4.02	4.02	4.02	2	0.21	0.03	0.16	0.00	0.00	22.3
3	480	-73	-851	-464	0	779	514	4.02	4.02	4.02	4.02	2	0.21	0.02	0.15	0.00	0.00	22.3
4	480	327	-912	-568	0	953	-530	4.02	4.02	4.02	4.02	2	0.27	0.03	0.16	0.00	0.00	22.3
5	480	-381	-886	-623	0	992	-449	4.02	4.02	4.02	4.02	2	0.27	0.03	0.16	0.00	0.00	22.3
6	480	1353	-920	-400	0	769	-560	4.02	4.02	4.02	4.02	2	0.22	0.03	0.16	0.00	0.00	22.3
7	480	-1007	-833	-584	0	898	555	4.02	4.02	4.02	4.02	2	0.24	0.02	0.14	0.00	0.00	22.3
8	480	1261	-931	-448	0	834	-591	4.02	4.02	4.02	4.02	2	0.24	0.03	0.17	0.00	0.00	22.3
9	480	-1100	-843	-632	0	963	535	4.02	4.02	4.02	4.02	2	0.26	0.02	0.15	0.00	0.00	22.3
10	480	635	-877	-408	0	740	458	4.02	4.02	4.02	4.02	2	0.21	0.03	0.16	0.00	0.00	22.3
11	480	-73	-851	-464	0	779	514	4.02	4.02	4.02	4.02	2	0.21	0.02	0.15	0.00	0.00	22.3
12	480	327	-912	-568	0	953	-530	4.02	4.02	4.02	4.02	2	0.27	0.03	0.16	0.00	0.00	22.3
13	480	-381	-886	-623	0	992	-449	4.02	4.02	4.02	4.02	2	0.27	0.03	0.16	0.00	0.00	22.3
14	480	1353	-920	-400	0	769	-560	4.02	4.02	4.02	4.02	2	0.22	0.03	0.16	0.00	0.00	22.3
15	480	-1007	-833	-584	0	898	555	4.02	4.02	4.02	4.02	2	0.24	0.02	0.14	0.00	0.00	22.3
16	480	1261	-931	-448	0	834	-591	4.02	4.02	4.02	4.02	2	0.24	0.03	0.17	0.00	0.00	22.3
17	480	-1100	-843	-632	0	963	535	4.02	4.02	4.02	4.02	2	0.26	0.02	0.15	0.00	0.00	22.3
18	480	1460	-1104	-1186	0	2051	671	4.02	4.02	4.02	4.02	3	0.52	0.04	0.20	0.00	0.00	22.3
19	480	-21	-1260	-1552	0	2513	-903	4.02	4.02	4.02	4.02	3	0.62	0.05	0.25	0.00	0.00	22.3
20	480	658	-1223	-1471	0	2248	-722	4.02	4.02	4.02	4.02	3	0.56	0.05	0.24	0.00	0.00	22.3
37	480	1770	-1039	-837	0	1519	793	4.02	4.02	4.02	4.02	3	0.39	0.03	0.19	0.00	0.00	22.3
38	480	-698	-1300	-1447	0	2292	-1021	4.02	4.02	4.02	4.02	3	0.55	0.05	0.23	0.00	0.00	22.3
39	480	433	-1238	-1311	0	1850	-718	4.02	4.02	4.02	4.02	3	0.46	0.04	0.22	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	540	165	-1541	-671	0	1528	-1577	4.02	4.02	4.02	4.02	3	0.38	0.04	0.27	0.00	0.00	22.3
2	540	635	-1181	-408	0	985	-1201	4.02	4.02	4.02	4.02	2	0.28	0.03	0.21	0.00	0.00	22.3
3	540	-73	-1155	-464	0	1057	-1103	4.02	4.02	4.02	4.02	2	0.29	0.03	0.21	0.00	0.00	22.3
4	540	327	-1216	-568	0	1294	-1323	4.02	4.02	4.02	4.02	2	0.36	0.04	0.22	0.00	0.00	22.3
5	540	-381	-1190	-623	0	1366	-1225	4.02	4.02	4.02	4.02	2	0.37	0.03	0.21	0.00	0.00	22.3
6	540	1353	-1224	-400	0	1009	-1357	4.02	4.02	4.02	4.02	2	0.29	0.04	0.22	0.00	0.00	22.3
7	540	-1007	-1137	-584	0	1249	-1032	4.02	4.02	4.02	4.02	2	0.33	0.03	0.20	0.00	0.00	22.3
8	540	1261	-1235	-448	0	1102	-1394	4.02	4.02	4.02	4.02	2	0.32	0.04	0.22	0.00	0.00	22.3
9	540	-1100	-1147	-632	0	1342	-1069	4.02	4.02	4.02	4.02	2	0.36	0.03	0.20	0.00	0.00	22.3
10	540	635	-1181	-408	0	985	-1201	4.02	4.02	4.02	4.02	2	0.28	0.03	0.21	0.00	0.00	22.3
11	540	-73	-1155	-464	0	1057	-1103	4.02	4.02	4.02	4.02	2	0.29	0.03	0.21	0.00	0.00	22.3
12	540	327	-1216	-568	0	1294	-1323	4.02	4.02	4.02	4.02	2	0.36	0.04	0.22	0.00	0.00	22.3
13	540	-381	-1190	-623	0	1366	-1225	4.02	4.02	4.02	4.02	2	0.37	0.03	0.21	0.00	0.00	22.3
14	540	1353	-1224	-400	0	1009	-1357	4.02	4.02	4.02	4.02	2	0.29	0.04	0.22	0.00	0.00	22.3
15	540	-1007	-1137	-584	0	1249	-1032	4.02	4.02	4.02	4.02	2	0.33	0.03	0.20	0.00	0.00	22.3
16	540	1261	-1235	-448	0	1102	-1394	4.02	4.02	4.02	4.02	2	0.32	0.04	0.22	0.00	0.00	22.3
17	540	-1100	-1147	-632	0	1342	-1069	4.02	4.02	4.02	4.02	2	0.36	0.03	0.20	0.00	0.00	22.3
18	540	1460	-1499	-1186	0	2762	-1428	4.02	4.02	4.02	4.02	3	0.71	0.04	0.27	0.00	0.00	22.3
19	540	-21	-1656	-1552	0	3445	-1978	4.02	4.02	4.02	4.02	3	0.85	0.05	0.29	0.00	0.00	22.3
20	540	658	-1618	-1471	0	3131	-1775	4.02	4.02	4.02	4.02	3	0.78	0.05	0.29	0.00	0.00	22.3
37	540	1770	-1435	-837	0	2022	-1202	4.02	4.02	4.02	4.02	3	0.52	0.04	0.26	0.00	0.00	22.3
38	540	-698	-1695	-1447	0	3160	-2120	4.02	4.02	4.02	4.02	3	0.76	0.05	0.30	0.00	0.00	22.3
39	540	433	-1634	-1311	0	2637	-1780	4.02	4.02	4.02	4.02	3	0.66	0.05	0.29	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	600	165	-1937	-671	0	1930	-1840	4.02	4.02	4.02	4.02	3	0.48	0.06	0.35	0.00	0.00	22.3
2	600	635	-1485	-408	0	1230	-1403	4.02	4.02	4.02	4.02	2	0.35	0.04	0.26	0.00	0.00	22.3
3	600	-73	-1459	-464	0	1335	-1303	4.02	4.02	4.02	4.02	2	0.37	0.04	0.26	0.00	0.00	22.3
4	600	327	-1520	-568	0	1635	-1528	4.02	4.02	4.02	4.02	2	0.46	0.04	0.27	0.00	0.00	22.3
5	600	-381	-1494	-623	0	1740	-1428	4.02	4.02	4.02	4.02	2	0.47	0.04	0.26	0.00	0.00	22.3
6	600	1353	-1528	-400	0	1249	-1563	4.02	4.02	4.02	4.02	2	0.36	0.04	0.27	0.00	0.00	22.3
7	600	-1007	-1441	-584	0	1599	-1230	4.02	4.02	4.02	4.02	2	0.43	0.04	0.25	0.00	0.00	22.3
8	600	1261	-1539	-448	0	1371	-1601	4.02	4.02	4.02	4.02	2	0.39	0.04	0.27	0.00	0.00	22.3
9	600	-1100	-1451	-632	0	1721	-1268	4.02	4.02	4.02	4.02	2	0.46	0.04	0.25	0.00	0.00	22.3
10	600	635	-1485	-408	0	1230	-1403	4.02	4.02	4.02	4.02	2	0.35	0.04	0.26	0.00	0.00	22.3
11	600	-73	-1459	-464	0	1335	-1303	4.02	4.02	4.02	4.02	2	0.37	0.04	0.26	0.00	0.00	22.3
12	600	327	-1520	-568	0	1635	-1528	4.02	4.02	4.02	4.02	2	0.46	0.04	0.27	0.00	0.00	22.3
13	600	-381	-1494	-623	0	1740	-1428	4.02	4.02	4.02	4.02	2	0.47	0.04	0.26	0.00	0.00	22.3
14	600	1353	-1528	-400	0	1249	-1563	4.02	4.02	4.02	4.02	2	0.36	0.04	0.27	0.00	0.00	22.3
15	600	-1007	-1441	-584	0	1599	-1230	4.02	4.02	4.02	4.02	2	0.43	0.04	0.25	0.00	0.00	22.3
16	600	1261	-1539	-448	0	1371	-1601	4.02	4.02	4.02	4.02	2	0.39	0.04	0.27	0.00	0.00	22.3
17	600	-1100	-1451	-632	0	1721	-1268	4.02	4.02	4.02	4.02	2	0.46	0.04	0.25	0.00	0.00	22.3
18	600	1460	-1895	-1186	0	3474	-1687	4.02	4.02	4.02	4.02	3	0.89	0.05	0.34	0.00	0.00	22.3
19	600	-21	-2051	-1552	0	4376	-2252	6.03	4.02	4.02	4.02	3	0.76	0.06	0.37	0.00	0.00	22.3
20	600	658	-2014	-1471	0	4013	-2045	6.03	4.02	4.02	4.02	3	0.71	0.06	0.36	0.00	0.00	22.3
37	600	1770	-1830	-837	0	2524	-1455	4.02	4.02	4.02	4.02	3	0.65	0.05	0.33	0.00	0.00	22.3
38	600	-698	-2091	-1447	0	4029	-2398	4.02	4.02	4.02	4.02	3	0.97	0.06	0.37	0.00	0.00	22.3
39	600	433	-2029	-1311	0	3424	-2052	4.02	4.02	4.02	4.02	3	0.85	0.06	0.36	0.00	0.00	22.3

apost= 2.01 aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

Nome travata: **Trave_403_IP1** Descrizione: **Trave_4 7-6-5-4-3-2-1**
ASTA NUM. 10 NI 215 NF 228 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y Permanente qy tot.
qy medio: 375.00 132.00 507.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-491	1878	-472	0	-1306	-1648	4.02	4.02	4.02	4.02	3	0.32	0.05	0.33	0.00	0.00	22.3
2	0	282	1429	-253	0	-695	-1231	4.02	4.02	4.02	4.02	2	0.19	0.04	0.25	0.00	0.00	22.3
3	0	-372	1486	-286	0	-791	-1396	4.02	4.02	4.02	4.02	2	0.22	0.04	0.26	0.00	0.00	22.3
4	0	-383	1404	-440	0	-1218	-1140	4.02	4.02	4.02	4.02	2	0.33	0.04	0.25	0.00	0.00	22.3
5	0	-1037	1460	-473	0	-1313	-1305	4.02	4.02	4.02	4.02	2	0.35	0.04	0.25	0.00	0.00	22.3
6	0	813	1355	-280	0	-767	-1007	4.02	4.02	4.02	4.02	2	0.22	0.04	0.24	0.00	0.00	22.3
7	0	-1369	1542	-390	0	-1085	-1557	4.02	4.02	4.02	4.02	2	0.29	0.04	0.27	0.00	0.00	22.3
8	0	613	1347	-336	0	-923	-979	4.02	4.02	4.02	4.02	2	0.26	0.04	0.24	0.00	0.00	22.3
9	0	-1568	1535	-446	0	-1242	-1529	4.02	4.02	4.02	4.02	2	0.33	0.04	0.26	0.00	0.00	22.3
10	0	282	1429	-253	0	-695	-1231	4.02	4.02	4.02	4.02	2	0.19	0.04	0.25	0.00	0.00	22.3
11	0	-372	1486	-286	0	-791	-1396	4.02	4.02	4.02	4.02	2	0.22	0.04	0.26	0.00	0.00	22.3
12	0	-383	1404	-440	0	-1218	-1140	4.02	4.02	4.02	4.02	2	0.33	0.04	0.25	0.00	0.00	22.3
13	0	-1037	1460	-473	0	-1313	-1305	4.02	4.02	4.02	4.02	2	0.35	0.04	0.25	0.00	0.00	22.3
14	0	813	1355	-280	0	-767	-1007	4.02	4.02	4.02	4.02	2	0.22	0.04	0.24	0.00	0.00	22.3

15	0	-1369	1542	-390	0	-1085	-1557	4.02	4.02	4.02	4.02	2	0.29	0.04	0.27	0.00	0.00	22.3
16	0	613	1347	-336	0	-923	-979	4.02	4.02	4.02	4.02	2	0.26	0.04	0.24	0.00	0.00	22.3
17	0	-1568	1535	-446	0	-1242	-1529	4.02	4.02	4.02	4.02	2	0.33	0.04	0.26	0.00	0.00	22.3
18	0	440	1801	-693	0	-1907	-1396	4.02	4.02	4.02	4.02	3	0.47	0.05	0.32	0.00	0.00	22.3
19	0	-1879	1754	-1169	0	-3216	-1236	4.02	4.02	4.02	4.02	3	0.75	0.05	0.30	0.00	0.00	22.3
20	0	-909	1848	-913	0	-2498	-1506	4.02	4.02	4.02	4.02	3	0.60	0.05	0.32	0.00	0.00	22.3
37	0	1286	1850	-386	0	-1064	-1559	4.02	4.02	4.02	4.02	3	0.27	0.05	0.33	0.00	0.00	22.3
38	0	-2580	1771	-1179	0	-3246	-1291	4.02	4.02	4.02	4.02	3	0.75	0.05	0.30	0.00	0.00	22.3
39	0	-964	1927	-753	0	-2049	-1741	4.02	4.02	4.02	4.02	3	0.49	0.06	0.34	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	60	-491	1483	-472	0	-1023	-1390	4.02	4.02	4.02	4.02	3	0.25	0.04	0.26	0.00	0.00	22.3
2	60	282	1125	-253	0	-543	-1034	4.02	4.02	4.02	4.02	2	0.16	0.03	0.20	0.00	0.00	22.3
3	60	-372	1182	-286	0	-619	-1194	4.02	4.02	4.02	4.02	2	0.18	0.03	0.21	0.00	0.00	22.3
4	60	-383	1100	-440	0	-954	-946	4.02	4.02	4.02	4.02	2	0.26	0.03	0.19	0.00	0.00	22.3
5	60	-1037	1156	-473	0	-1029	-1105	4.02	4.02	4.02	4.02	2	0.27	0.03	0.20	0.00	0.00	22.3
6	60	813	1051	-280	0	-598	-817	4.02	4.02	4.02	4.02	2	0.17	0.03	0.19	0.00	0.00	22.3
7	60	-1369	1238	-390	0	-851	-1349	4.02	4.02	4.02	4.02	2	0.23	0.04	0.21	0.00	0.00	22.3
8	60	613	1043	-336	0	-721	-790	4.02	4.02	4.02	4.02	2	0.20	0.03	0.19	0.00	0.00	22.3
9	60	-1568	1231	-446	0	-974	-1322	4.02	4.02	4.02	4.02	2	0.26	0.04	0.21	0.00	0.00	22.3
10	60	282	1125	-253	0	-543	-1034	4.02	4.02	4.02	4.02	2	0.16	0.03	0.20	0.00	0.00	22.3
11	60	-372	1182	-286	0	-619	-1194	4.02	4.02	4.02	4.02	2	0.18	0.03	0.21	0.00	0.00	22.3
12	60	-383	1100	-440	0	-954	-946	4.02	4.02	4.02	4.02	2	0.26	0.03	0.19	0.00	0.00	22.3
13	60	-1037	1156	-473	0	-1029	-1105	4.02	4.02	4.02	4.02	2	0.27	0.03	0.20	0.00	0.00	22.3
14	60	813	1051	-280	0	-598	-817	4.02	4.02	4.02	4.02	2	0.17	0.03	0.19	0.00	0.00	22.3
15	60	-1369	1238	-390	0	-851	-1349	4.02	4.02	4.02	4.02	2	0.23	0.04	0.21	0.00	0.00	22.3
16	60	613	1043	-336	0	-721	-790	4.02	4.02	4.02	4.02	2	0.20	0.03	0.19	0.00	0.00	22.3
17	60	-1568	1231	-446	0	-974	-1322	4.02	4.02	4.02	4.02	2	0.26	0.04	0.21	0.00	0.00	22.3
18	60	440	1406	-693	0	-1491	-1145	4.02	4.02	4.02	4.02	3	0.37	0.04	0.25	0.00	0.00	22.3
19	60	-1879	1358	-1169	0	-2515	-990	4.02	4.02	4.02	4.02	3	0.59	0.04	0.23	0.00	0.00	22.3
20	60	-909	1452	-913	0	-1950	-1251	4.02	4.02	4.02	4.02	3	0.47	0.04	0.25	0.00	0.00	22.3
37	60	1286	1455	-386	0	-833	-1304	4.02	4.02	4.02	4.02	3	0.21	0.04	0.26	0.00	0.00	22.3
38	60	-2580	1376	-1179	0	-2539	-1043	4.02	4.02	4.02	4.02	3	0.58	0.04	0.23	0.00	0.00	22.3
39	60	-964	1532	-753	0	-1597	-1479	4.02	4.02	4.02	4.02	3	0.38	0.04	0.27	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	120	-491	1087	-472	0	-739	682	4.02	4.02	4.02	4.02	3	0.18	0.03	0.19	0.00	0.00	22.3
2	120	282	821	-253	0	-391	535	4.02	4.02	4.02	4.02	2	0.11	0.02	0.15	0.00	0.00	22.3
3	120	-372	878	-286	0	-448	466	4.02	4.02	4.02	4.02	2	0.12	0.03	0.15	0.00	0.00	22.3
4	120	-383	796	-440	0	-690	582	4.02	4.02	4.02	4.02	2	0.19	0.02	0.14	0.00	0.00	22.3
5	120	-1037	852	-473	0	-745	513	4.02	4.02	4.02	4.02	2	0.20	0.02	0.15	0.00	0.00	22.3
6	120	813	747	-280	0	-430	632	4.02	4.02	4.02	4.02	2	0.12	0.02	0.13	0.00	0.00	22.3
7	120	-1369	934	-390	0	-617	-544	4.02	4.02	4.02	4.02	2	0.16	0.03	0.16	0.00	0.00	22.3
8	120	613	739	-336	0	-519	646	4.02	4.02	4.02	4.02	2	0.15	0.02	0.13	0.00	0.00	22.3
9	120	-1568	927	-446	0	-707	-521	4.02	4.02	4.02	4.02	2	0.19	0.03	0.16	0.00	0.00	22.3
10	120	282	821	-253	0	-391	535	4.02	4.02	4.02	4.02	2	0.11	0.02	0.15	0.00	0.00	22.3
11	120	-372	878	-286	0	-448	466	4.02	4.02	4.02	4.02	2	0.12	0.03	0.15	0.00	0.00	22.3
12	120	-383	796	-440	0	-690	582	4.02	4.02	4.02	4.02	2	0.19	0.02	0.14	0.00	0.00	22.3
13	120	-1037	852	-473	0	-745	513	4.02	4.02	4.02	4.02	2	0.20	0.02	0.15	0.00	0.00	22.3
14	120	813	747	-280	0	-430	632	4.02	4.02	4.02	4.02	2	0.12	0.02	0.13	0.00	0.00	22.3
15	120	-1369	934	-390	0	-617	-544	4.02	4.02	4.02	4.02	2	0.16	0.03	0.16	0.00	0.00	22.3
16	120	613	739	-336	0	-519	646	4.02	4.02	4.02	4.02	2	0.15	0.02	0.13	0.00	0.00	22.3
17	120	-1568	927	-446	0	-707	-521	4.02	4.02	4.02	4.02	2	0.19	0.03	0.16	0.00	0.00	22.3
18	120	440	1010	-693	0	-1075	802	4.02	4.02	4.02	4.02	3	0.27	0.03	0.18	0.00	0.00	22.3
19	120	-1879	963	-1169	0	-1813	882	4.02	4.02	4.02	4.02	3	0.42	0.04	0.18	0.00	0.00	22.3
20	120	-909	1057	-913	0	-1402	772	4.02	4.02	4.02	4.02	3	0.34	0.03	0.18	0.00	0.00	22.3
37	120	1286	1059	-386	0	-601	723	4.02	4.02	4.02	4.02	3	0.15	0.03	0.19	0.00	0.00	22.3
38	120	-2580	980	-1179	0	-1831	856	4.02	4.02	4.02	4.02	3	0.42	0.04	0.18	0.00	0.00	22.3
39	120	-964	1136	-753	0	-1145	672	4.02	4.02	4.02	4.02	3	0.27	0.03	0.20	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	180	-491	692	-472	0	-456	1015	4.02	4.02	4.02	4.02	3	0.14	0.02	0.12	0.00	0.00	22.3
2	180	282	516	-253	0	-239	776	4.02	4.02	4.02	4.02	2	0.12	0.01	0.09	0.00	0.00	22.3
3	180	-372	573	-286	0	-276	747	4.02	4.02	4.02	4.02	2	0.11	0.02	0.10	0.00	0.00	22.3
4	180	-383	491	-440	0	-425	790	4.02	4.02	4.02	4.02	2	0.12	0.01	0.09	0.00	0.00	22.3
5	180	-1037	547	-473	0	-462	779	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
6	180	813	442	-280	0	-262	784	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
7	180	-1369	629	-390	0	-383	717	4.02	4.02	4.02	4.02	2	0.10	0.02	0.11	0.00	0.00	22.3
8	180	613	434	-336	0	-318	793	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
9	180	-1568	622	-446	0	-439	727	4.02	4.02	4.02	4.02	2	0.12	0.02	0.11	0.00	0.00	22.3
10	180	282	516	-253	0	-239	776	4.02	4.02	4.02	4.02	2	0.12	0.01	0.09	0.00	0.00	22.3
11	180	-372	573	-286	0	-276	747	4.02	4.02	4.02	4.02	2	0.11	0.02	0.10	0.00	0.00	22.3
12	180	-383	491	-440	0	-425	790	4.02	4.02	4.02	4.02	2	0.12	0.01	0.09	0.00	0.00	22.3
13	180	-1037	547	-473	0	-462	779	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
14	180	813	442	-280	0	-262	784	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
15	180	-1369	629	-390	0	-383	717	4.02	4.02	4.02	4.02	2	0.10	0.02	0.11	0.00	0.00	22.3
16	180	613	434	-336	0	-318	793	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
17	180	-1568	622	-446	0	-439	727	4.02	4.02	4.02	4.02	2	0.12	0.02	0.11	0.00	0.00	22.3
18	180	440	615	-693	0	-660	1042	4.02	4.02	4.02	4.02	3	0.16	0.02	0.11	0.00	0.00	22.3
19	180	-1879	567	-1169	0	-1112	1076	4.02	4.02	4.02	4.02	3	0.26	0.04	0.18	0.00	0.00	22.3
20	180	-909	661	-913	0	-854	1071	4.02	4.02	4.02	4.02	3	0.20	0.03	0.14	0.00	0.00	22.3
37	180	1286	664	-386	0	-370	1025	4.02	4.02	4.02	4.02	3	0.15	0.02	0.12	0.00	0.00	22.3
38	180	-2580	585	-1179	0	-1124	1062	4.02	4.02	4.02	4.02	3	0.26	0.04	0.18	0.00	0.00	22.3
39	180	-964	741	-753	0	-693	1035	4.02	4.02	4.02	4.02	3	0.17	0.02	0.13	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	240	-491	296	-472	0	-173	1020	4.02	4.02	4.02	4.02	3	0.14	0.01	0.08	0.00	0.00	22.3
2	240	282	212	-253	0	-87	776	4.02	4.02	4.02	4.02	2	0.12	0.01	0.04	0.00	0.00	22.3
3	240	-372	269	-286	0	-104	780	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
4	240	-383	187	-440	0	-161	790	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
5	240	-1037	243	-473	0	-178	794	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
6	240	813	138	-280	0	-94	784	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
7	240	-1369	325	-390	0	-149	789	4.02	4.02	4.02	4.02	2	0.11	0.01	0.06	0.00	0.00	22.3
8	240	613	130	-336	0	-116	793	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
9	240	-1568	318	-446	0	-172	794	4.02	4.02	4.02	4.02	2	0.11	0.01	0.07	0.00	0.00	22.3
10	240	282	212	-253	0	-87	776	4.02	4.02	4.02	4.02	2	0.12	0.01	0.04	0.00	0.00	22.3
11	240	-372	269	-286	0	-104	780	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
12	240	-383	187	-440	0	-161	790	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
13	240	-1037	243	-473	0	-178	794	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
14	240	813	138	-280	0	-94	784	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
15	240	-1369	325	-390	0	-149	789	4.02	4.02	4.02	4.02	2	0.11	0.01	0.06	0.00	0.00	22.3
16	240	613	130	-336	0	-116	793	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
17	240	-1568	318	-446	0	-172	794	4.02	4.02	4.02	4.02	2	0.11	0.01	0.07	0.00	0.00	22.3
18	240	440	219	-693	0	-244	1042	4.02	4.02	4.02	4.02	3	0.15	0.02	0.11	0.00	0.00	22.3
19	240	-1879	172	-1169	0	-411	1076	4.02	4.02	4.02	4.02	3	0.15	0.04	0.18	0.00	0.00	22.3
20	240	-909	266	-913	0	-306	1071	4.02	4.02	4.02	4.02	3	0.15	0.03	0.14	0.00	0.00	22.3

37	240	1286	268	-386	0	-138	1025	4.02	4.02	4.02	4.02	3	0.15	0.01	0.06	0.00	0.00	22.3
38	240	-2580	189	-1179	0	-417	1062	4.02	4.02	4.02	4.02	3	0.14	0.04	0.18	0.00	0.00	22.3
39	240	-964	345	-753	0	-241	1074	4.02	4.02	4.02	4.02	3	0.15	0.02	0.12	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	300	-491	-99	-472	0	110	1020	4.02	4.02	4.02	4.02	3	0.14	0.01	0.08	0.00	0.00	22.3
2	300	282	-92	-253	0	64	776	4.02	4.02	4.02	4.02	2	0.12	0.01	0.04	0.00	0.00	22.3
3	300	-372	-35	-286	0	67	780	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
4	300	-383	-117	-440	0	103	790	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
5	300	-1037	-61	-473	0	106	794	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
6	300	813	-166	-280	0	75	784	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
7	300	-1369	21	-390	0	85	789	4.02	4.02	4.02	4.02	2	0.11	0.01	0.06	0.00	0.00	22.3
8	300	613	-174	-336	0	86	793	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
9	300	-1568	14	-446	0	96	794	4.02	4.02	4.02	4.02	2	0.11	0.01	0.07	0.00	0.00	22.3
10	300	282	-92	-253	0	64	776	4.02	4.02	4.02	4.02	2	0.12	0.01	0.04	0.00	0.00	22.3
11	300	-372	-35	-286	0	67	780	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
12	300	-383	-117	-440	0	103	790	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
13	300	-1037	-61	-473	0	106	794	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
14	300	813	-166	-280	0	75	784	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
15	300	-1369	21	-390	0	85	789	4.02	4.02	4.02	4.02	2	0.11	0.01	0.06	0.00	0.00	22.3
16	300	613	-174	-336	0	86	793	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
17	300	-1568	14	-446	0	96	794	4.02	4.02	4.02	4.02	2	0.11	0.01	0.07	0.00	0.00	22.3
18	300	440	-176	-693	0	172	1042	4.02	4.02	4.02	4.02	3	0.15	0.02	0.11	0.00	0.00	22.3
19	300	-1879	-224	-1169	0	290	1076	4.02	4.02	4.02	4.02	3	0.15	0.04	0.18	0.00	0.00	22.3
20	300	-909	-130	-913	0	243	1071	4.02	4.02	4.02	4.02	3	0.15	0.03	0.14	0.00	0.00	22.3
37	300	1286	-127	-386	0	93	1025	4.02	4.02	4.02	4.02	3	0.15	0.01	0.06	0.00	0.00	22.3
38	300	-2580	-206	-1179	0	290	1062	4.02	4.02	4.02	4.02	3	0.14	0.04	0.18	0.00	0.00	22.3
39	300	-964	-50	-753	0	210	1074	4.02	4.02	4.02	4.02	3	0.15	0.02	0.12	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	360	-491	-494	-472	0	394	1020	4.02	4.02	4.02	4.02	3	0.14	0.01	0.09	0.00	0.00	22.3
2	360	282	-396	-253	0	216	776	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
3	360	-372	-339	-286	0	239	780	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
4	360	-383	-421	-440	0	367	790	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
5	360	-1037	-365	-473	0	390	794	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
6	360	813	-470	-280	0	243	784	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
7	360	-1369	-283	-390	0	318	789	4.02	4.02	4.02	4.02	2	0.11	0.01	0.06	0.00	0.00	22.3
8	360	613	-478	-336	0	288	793	4.02	4.02	4.02	4.02	2	0.12	0.01	0.09	0.00	0.00	22.3
9	360	-1568	-290	-446	0	364	794	4.02	4.02	4.02	4.02	2	0.11	0.01	0.07	0.00	0.00	22.3
10	360	282	-396	-253	0	216	776	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
11	360	-372	-339	-286	0	239	780	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
12	360	-383	-421	-440	0	367	790	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
13	360	-1037	-365	-473	0	390	794	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
14	360	813	-470	-280	0	243	784	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
15	360	-1369	-283	-390	0	318	789	4.02	4.02	4.02	4.02	2	0.11	0.01	0.06	0.00	0.00	22.3
16	360	613	-478	-336	0	288	793	4.02	4.02	4.02	4.02	2	0.12	0.01	0.09	0.00	0.00	22.3
17	360	-1568	-290	-446	0	364	794	4.02	4.02	4.02	4.02	2	0.11	0.01	0.07	0.00	0.00	22.3
18	360	440	-571	-693	0	588	1042	4.02	4.02	4.02	4.02	3	0.15	0.02	0.11	0.00	0.00	22.3
19	360	-1879	-619	-1169	0	992	1076	4.02	4.02	4.02	4.02	3	0.23	0.04	0.18	0.00	0.00	22.3
20	360	-909	-525	-913	0	791	1071	4.02	4.02	4.02	4.02	3	0.19	0.03	0.14	0.00	0.00	22.3
37	360	1286	-522	-386	0	324	1025	4.02	4.02	4.02	4.02	3	0.15	0.02	0.09	0.00	0.00	22.3
38	360	-2580	-601	-1179	0	998	1062	4.02	4.02	4.02	4.02	3	0.23	0.04	0.18	0.00	0.00	22.3
39	360	-964	-445	-753	0	662	1074	4.02	4.02	4.02	4.02	3	0.16	0.02	0.12	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	420	-491	-890	-472	0	677	877	4.02	4.02	4.02	4.02	3	0.16	0.03	0.16	0.00	0.00	22.3
2	420	282	-700	-253	0	368	655	4.02	4.02	4.02	4.02	2	0.10	0.02	0.12	0.00	0.00	22.3
3	420	-372	-643	-286	0	411	698	4.02	4.02	4.02	4.02	2	0.11	0.02	0.11	0.00	0.00	22.3
4	420	-383	-725	-440	0	631	652	4.02	4.02	4.02	4.02	2	0.17	0.02	0.13	0.00	0.00	22.3
5	420	-1037	-669	-473	0	674	695	4.02	4.02	4.02	4.02	2	0.18	0.02	0.12	0.00	0.00	22.3
6	420	813	-774	-280	0	411	604	4.02	4.02	4.02	4.02	2	0.12	0.02	0.14	0.00	0.00	22.3
7	420	-1369	-587	-390	0	552	747	4.02	4.02	4.02	4.02	2	0.15	0.02	0.10	0.00	0.00	22.3
8	420	613	-782	-336	0	490	603	4.02	4.02	4.02	4.02	2	0.14	0.02	0.14	0.00	0.00	22.3
9	420	-1568	-594	-446	0	631	746	4.02	4.02	4.02	4.02	2	0.17	0.02	0.10	0.00	0.00	22.3
10	420	282	-700	-253	0	368	655	4.02	4.02	4.02	4.02	2	0.10	0.02	0.12	0.00	0.00	22.3
11	420	-372	-643	-286	0	411	698	4.02	4.02	4.02	4.02	2	0.11	0.02	0.11	0.00	0.00	22.3
12	420	-383	-725	-440	0	631	652	4.02	4.02	4.02	4.02	2	0.17	0.02	0.13	0.00	0.00	22.3
13	420	-1037	-669	-473	0	674	695	4.02	4.02	4.02	4.02	2	0.18	0.02	0.12	0.00	0.00	22.3
14	420	813	-774	-280	0	411	604	4.02	4.02	4.02	4.02	2	0.12	0.02	0.14	0.00	0.00	22.3
15	420	-1369	-587	-390	0	552	747	4.02	4.02	4.02	4.02	2	0.15	0.02	0.10	0.00	0.00	22.3
16	420	613	-782	-336	0	490	603	4.02	4.02	4.02	4.02	2	0.14	0.02	0.14	0.00	0.00	22.3
17	420	-1568	-594	-446	0	631	746	4.02	4.02	4.02	4.02	2	0.17	0.02	0.10	0.00	0.00	22.3
18	420	440	-967	-693	0	1004	846	4.02	4.02	4.02	4.02	3	0.25	0.03	0.17	0.00	0.00	22.3
19	420	-1879	-1014	-1169	0	1693	832	4.02	4.02	4.02	4.02	3	0.40	0.04	0.18	0.00	0.00	22.3
20	420	-909	-920	-913	0	1339	907	4.02	4.02	4.02	4.02	3	0.32	0.03	0.16	0.00	0.00	22.3
37	420	1286	-918	-386	0	556	863	4.02	4.02	4.02	4.02	3	0.14	0.03	0.16	0.00	0.00	22.3
38	420	-2580	-997	-1179	0	1705	840	4.02	4.02	4.02	4.02	3	0.39	0.04	0.18	0.00	0.00	22.3
39	420	-964	-841	-753	0	1114	965	4.02	4.02	4.02	4.02	3	0.27	0.02	0.15	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	480	-491	-1285	-472	0	960	-876	4.02	4.02	4.02	4.02	3	0.23	0.04	0.23	0.00	0.00	22.3
2	480	282	-1005	-253	0	520	-719	4.02	4.02	4.02	4.02	2	0.14	0.03	0.18	0.00	0.00	22.3
3	480	-372	-948	-286	0	582	-585	4.02	4.02	4.02	4.02	2	0.16	0.03	0.17	0.00	0.00	22.3
4	480	-383	-1030	-440	0	896	-763	4.02	4.02	4.02	4.02	2	0.24	0.03	0.18	0.00	0.00	22.3
5	480	-1037	-974	-473	0	957	-630	4.02	4.02	4.02	4.02	2	0.26	0.03	0.17	0.00	0.00	22.3
6	480	813	-1079	-280	0	579	-890	4.02	4.02	4.02	4.02	2	0.16	0.03	0.19	0.00	0.00	22.3
7	480	-1369	-892	-390	0	786	458	4.02	4.02	4.02	4.02	2	0.21	0.03	0.15	0.00	0.00	22.3
8	480	613	-1087	-336	0	692	-904	4.02	4.02	4.02	4.02	2	0.19	0.03	0.19	0.00	0.00	22.3
9	480	-1568	-899	-446	0	899	-457	4.02	4.02	4.02	4.02	2	0.24	0.03	0.15	0.00	0.00	22.3
10	480	282	-1005	-253	0	520	-719	4.02	4.02	4.02	4.02	2	0.14	0.03	0.18	0.00	0.00	22.3
11	480	-372	-948	-286	0	582	-585	4.02	4.02	4.02	4.02	2	0.16	0.03	0.17	0.00	0.00	22.3
12	480	-383	-1030	-440	0	896	-763	4.02	4.02	4.02	4.02	2	0.24	0.03	0.18	0.00	0.00	22.3
13	480	-1037	-974	-473	0	957	-630	4.02	4.02	4.02	4.02	2	0.26	0.03	0.17	0.00	0.00	22.3
14	480	813	-1079	-280	0	579	-890	4.02	4.02	4.02	4.02	2	0.16	0.03	0.19	0.00	0.00	22.3
15	480	-1369	-892	-390	0	786	458	4.02	4.02	4.02	4.02	2	0.21	0.03	0.15	0.00	0.00	22.3
16	480	613	-1087	-336	0	692	-904	4.02	4.02	4.02	4.02	2	0.19	0.03	0.19	0.00	0.00	22.3
17	480	-1568	-899	-446	0	899	-457	4.02	4.02	4.02	4.02	2	0.24	0.03	0.15	0.00	0.00	22.3
18	480	440	-1362	-693	0	1419	-1032	4.02	4.02	4.02	4.02	3	0.35	0.04	0.24	0.00	0.00	22.3
19	480	-1879	-1410	-1169	0	2394	-1123	4.02	4.02	4.02	4.02	3	0.56	0.04	0.24	0.00	0.00	22.3
20	480	-909	-1316	-913	0	1887	-896	4.02	4.02	4.02	4.02	3	0.45	0.04	0.23	0.00	0.00	22.3
37	480	1286	-1313	-386	0	787	-936	4.02	4.02	4.02	4.02	3	0.20	0.04	0.23	0.00	0.00	22.3
38	480	-2580	-1392	-1179	0	2412	-1086	4.02	4.02	4.02	4.02	3	0.56	0.04	0.23	0.00	0.00	22.3
39	480	-964	-1236	-753	0	1566	-709	4.02	4.02	4.02	4.02	3	0.38	0.04	0.22	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	540	-491	-1681	-472	0	1244	-1967	4.02	4.02	4.02	4.02	3	0.30	0.05	0.30	0.00	0.00	22.3
2	540	282	-1309	-253	0	672	-1567	4.02	4.02	4.02	4.02	2	0.24	0.04	0.23	0.00	0.00	22.3
3	540	-372	-1252	-286	0	754	-1399	4.02	4.02	4.02	4.02	2	0.21	0.04	0.22	0.00	0.00	22.3
4	540	-383	-1334	-440	0	1160	-1627	4.02	4.02	4.02	4.02	2	0.32	0.04	0.24	0.00	0.00	22.3
5	540	-1037	-1278	-473	0	1241	-1459	4.02	4.02	4.02	4.02	2	0.33	0.04	0.22	0.00	0.00	22.3
6	540	813	-1383	-280	0	748	-1783	4.02	4.02	4.02	4.02	2	0.28	0.04	0.25	0.00	0.00	22.3
7	540	-1369	-1196	-390	0	1020	-1225	4.02	4.02	4.02	4.02	2	0.27	0.03	0.21	0.00	0.00	22.3
8	540	613	-1391	-336	0	894	-1801	4.02	4.02	4.02	4.02	2	0.28	0.04	0.25	0.00	0.00	22.3
9	540	-1568	-1203	-446	0	1166	-1242	4.02	4.02	4.02	4.02	2	0.31	0.03	0.21	0.00	0.00	22.3
10	540	282	-1309	-253	0	672	-1567	4.02	4.02	4.02	4.02	2	0.24	0.04	0.23	0.00	0.00	22.3
11	540	-372	-1252	-286	0	754	-1399	4.02	4.02	4.02	4.02	2	0.21	0.04	0.22	0.00	0.00	22.3
12	540	-383	-1334	-440	0	1160	-1627	4.02	4.02	4.02	4.02	2	0.32	0.04	0.24	0.00	0.00	22.3
13	540	-1037	-1278	-473	0	1241	-1459	4.02	4.02	4.02	4.02	2	0.33	0.04	0.22	0.00	0.00	22.3
14	540	813	-1383	-280	0	748	-1783	4.02	4.02	4.02	4.02	2	0.28	0.04	0.25	0.00	0.00	22.3
15	540	-1369	-1196	-390	0	1020	-1225	4.02	4.02	4.02	4.02	2	0.27	0.03	0.21	0.00	0.00	22.3
16	540	613	-1391	-336	0	894	-1801	4.02	4.02	4.02	4.02	2	0.28	0.04	0.25	0.00	0.00	22.3
17	540	-1568	-1203	-446	0	1166	-1242	4.02	4.02	4.02	4.02	2	0.31	0.03	0.21	0.00	0.00	22.3
18	540	440	-1758	-693	0	1835	-2168	4.02	4.02	4.02	4.02	3	0.46	0.05	0.31	0.00	0.00	22.3
19	540	-1879	-1806	-1169	0	3096	-2287	4.02	4.02	4.02	4.02	3	0.72	0.05	0.31	0.00	0.00	22.3
20	540	-909	-1711	-913	0	2435	-2005	4.02	4.02	4.02	4.02	3	0.58	0.05	0.30	0.00	0.00	22.3
37	540	1286	-1709	-386	0	1019	-2043	4.02	4.02	4.02	4.02	3	0.30	0.05	0.30	0.00	0.00	22.3
38	540	-2580	-1788	-1179	0	3120	-2241	4.02	4.02	4.02	4.02	3	0.72	0.05	0.30	0.00	0.00	22.3
39	540	-964	-1632	-753	0	2018	-1770	4.02	4.02	4.02	4.02	3	0.48	0.05	0.28	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	600	-491	-2076	-472	0	1527	-2243	4.02	4.02	4.02	4.02	3	0.37	0.06	0.37	0.00	0.00	22.3
2	600	282	-1613	-253	0	824	-1781	4.02	4.02	4.02	4.02	2	0.27	0.05	0.29	0.00	0.00	22.3
3	600	-372	-1556	-286	0	926	-1608	4.02	4.02	4.02	4.02	2	0.25	0.05	0.27	0.00	0.00	22.3
4	600	-383	-1638	-440	0	1424	-1843	4.02	4.02	4.02	4.02	2	0.39	0.05	0.29	0.00	0.00	22.3
5	600	-1037	-1582	-473	0	1525	-1670	4.02	4.02	4.02	4.02	2	0.41	0.05	0.27	0.00	0.00	22.3
6	600	813	-1687	-280	0	916	-2004	4.02	4.02	4.02	4.02	2	0.31	0.05	0.30	0.00	0.00	22.3
7	600	-1369	-1500	-390	0	1254	-1428	4.02	4.02	4.02	4.02	2	0.33	0.04	0.26	0.00	0.00	22.3
8	600	613	-1695	-336	0	1096	-2023	4.02	4.02	4.02	4.02	2	0.31	0.05	0.30	0.00	0.00	22.3
9	600	-1568	-1507	-446	0	1434	-1446	4.02	4.02	4.02	4.02	2	0.38	0.04	0.26	0.00	0.00	22.3
10	600	282	-1613	-253	0	824	-1781	4.02	4.02	4.02	4.02	2	0.27	0.05	0.29	0.00	0.00	22.3
11	600	-372	-1556	-286	0	926	-1608	4.02	4.02	4.02	4.02	2	0.25	0.05	0.27	0.00	0.00	22.3
12	600	-383	-1638	-440	0	1424	-1843	4.02	4.02	4.02	4.02	2	0.39	0.05	0.29	0.00	0.00	22.3
13	600	-1037	-1582	-473	0	1525	-1670	4.02	4.02	4.02	4.02	2	0.41	0.05	0.27	0.00	0.00	22.3
14	600	813	-1687	-280	0	916	-2004	4.02	4.02	4.02	4.02	2	0.31	0.05	0.30	0.00	0.00	22.3
15	600	-1369	-1500	-390	0	1254	-1428	4.02	4.02	4.02	4.02	2	0.33	0.04	0.26	0.00	0.00	22.3
16	600	613	-1695	-336	0	1096	-2023	4.02	4.02	4.02	4.02	2	0.31	0.05	0.30	0.00	0.00	22.3
17	600	-1568	-1507	-446	0	1434	-1446	4.02	4.02	4.02	4.02	2	0.38	0.04	0.26	0.00	0.00	22.3
18	600	440	-2153	-693	0	2251	-2452	4.02	4.02	4.02	4.02	3	0.56	0.06	0.38	0.00	0.00	22.3
19	600	-1879	-2201	-1169	0	3797	-2575	4.02	4.02	4.02	4.02	3	0.89	0.06	0.38	0.00	0.00	22.3
20	600	-909	-2107	-913	0	2983	-2284	4.02	4.02	4.02	4.02	3	0.72	0.06	0.37	0.00	0.00	22.3
37	600	1286	-2104	-386	0	1250	-2322	4.02	4.02	4.02	4.02	3	0.35	0.06	0.37	0.00	0.00	22.3
38	600	-2580	-2183	-1179	0	3827	-2527	4.02	4.02	4.02	4.02	3	0.88	0.06	0.37	0.00	0.00	22.3
39	600	-964	-2027	-753	0	2470	-2042	4.02	4.02	4.02	4.02	3	0.59	0.06	0.35	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

Nome travata: **Trave_403_IP1** Descrizione: **Trave_4 7-6-5-4-3-2-1**
ASTA NUM. 11 NI 228 NF 251 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y Permanente qy tot.
qy medio: 375.00 132.00 507.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-1201	1894	-65	0	-58	-1655	4.02	4.02	4.02	4.02	3	0.23	0.05	0.33	0.00	0.00	22.3
2	0	-216	1430	-45	0	-58	-1209	4.02	4.02	4.02	4.02	2	0.18	0.04	0.25	0.00	0.00	22.3
3	0	-763	1491	-48	0	-67	-1386	4.02	4.02	4.02	4.02	2	0.21	0.04	0.26	0.00	0.00	22.3
4	0	-1084	1423	-52	0	-23	-1160	4.02	4.02	4.02	4.02	2	0.17	0.04	0.25	0.00	0.00	22.3
5	0	-1631	1483	-55	0	-31	-1337	4.02	4.02	4.02	4.02	2	0.19	0.04	0.25	0.00	0.00	22.3
6	0	118	1357	-44	0	-36	-986	4.02	4.02	4.02	4.02	2	0.15	0.04	0.24	0.00	0.00	22.3
7	0	-1705	1558	-53	0	-65	-1575	4.02	4.02	4.02	4.02	2	0.23	0.04	0.27	0.00	0.00	22.3
8	0	-142	1355	-47	0	-25	-971	4.02	4.02	4.02	4.02	2	0.15	0.04	0.24	0.00	0.00	22.3
9	0	-1965	1556	-56	0	-54	-1561	4.02	4.02	4.02	4.02	2	0.22	0.04	0.26	0.00	0.00	22.3
10	0	-216	1430	-45	0	-58	-1209	4.02	4.02	4.02	4.02	2	0.18	0.04	0.25	0.00	0.00	22.3
11	0	-763	1491	-48	0	-67	-1386	4.02	4.02	4.02	4.02	2	0.21	0.04	0.26	0.00	0.00	22.3
12	0	-1084	1423	-52	0	-23	-1160	4.02	4.02	4.02	4.02	2	0.17	0.04	0.25	0.00	0.00	22.3
13	0	-1631	1483	-55	0	-31	-1337	4.02	4.02	4.02	4.02	2	0.19	0.04	0.25	0.00	0.00	22.3
14	0	118	1357	-44	0	-36	-986	4.02	4.02	4.02	4.02	2	0.15	0.04	0.24	0.00	0.00	22.3
15	0	-1705	1558	-53	0	-65	-1575	4.02	4.02	4.02	4.02	2	0.23	0.04	0.27	0.00	0.00	22.3
16	0	-142	1355	-47	0	-25	-971	4.02	4.02	4.02	4.02	2	0.15	0.04	0.24	0.00	0.00	22.3
17	0	-1965	1556	-56	0	-54	-1561	4.02	4.02	4.02	4.02	2	0.22	0.04	0.26	0.00	0.00	22.3
18	0	-521	1823	-126	0	-186	-1410	4.02	4.02	4.02	4.02	3	0.20	0.05	0.32	0.00	0.00	22.3
19	0	-3381	1818	-136	0	-61	-1335	4.02	4.02	4.02	4.02	3	0.17	0.05	0.30	0.00	0.00	22.3
20	0	-1908	1906	-134	0	-159	-1634	4.02	4.02	4.02	4.02	3	0.22	0.05	0.32	0.00	0.00	22.3
37	0	674	1849	-101	0	-206	-1527	4.02	4.02	4.02	4.02	3	0.22	0.05	0.33	0.00	0.00	22.3
38	0	-4093	1840	-117	0	3	-1402	4.02	4.02	4.02	4.02	3	0.18	0.05	0.30	0.00	0.00	22.3
39	0	-1638	1986	-114	0	-161	-1901	4.02	4.02	4.02	4.02	3	0.26	0.06	0.34	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	60	-1201	1498	-65	0	-19	-1396	4.02	4.02	4.02	4.02	3	0.19	0.04	0.26	0.00	0.00	22.3
2	60	-216	1126	-45	0	-31	-1012	4.02	4.02	4.02	4.02	2	0.15	0.03	0.20	0.00	0.00	22.3
3	60	-763	1187	-48	0	-38	-1184	4.02	4.02	4.02	4.02	2	0.18	0.03	0.21	0.00	0.00	22.3
4	60	-1084	1119	-52	0	9	-964	4.02	4.02	4.02	4.02	2	0.14	0.03	0.19	0.00	0.00	22.3
5	60	-1631	1179	-55	0	2	-1135	4.02	4.02	4.02	4.02	2	0.16	0.03	0.20	0.00	0.00	22.3
6	60	118	1053	-44	0	-9	-796	4.02	4.02	4.02	4.02	2	0.12	0.03	0.19	0.00	0.00	22.3
7	60	-1705	1254	-53	0	-33	-1366	4.02	4.02	4.02	4.02	2	0.20	0.04	0.21	0.00	0.00	22.3
8	60	-142	1051	-47	0	3	-781	4.02	4.02	4.02	4.02	2	0.12	0.03	0.19	0.00	0.00	22.3
9	60	-1965	1252	-56	0	-21	-1352	4.02	4.02	4.02	4.02	2	0.19	0.04	0.21	0.00	0.00	22.3
10	60	-216	1126	-45	0	-31	-1012	4.02	4.02	4.02	4.02	2	0.15	0.03	0.20	0.00	0.00	22.3
11	60	-763	1187	-48	0	-38	-1184	4.02	4.02	4.02	4.02	2	0.18	0.03	0.21	0.00	0.00	22.3
12	60	-1084	1119	-52	0	9	-964	4.02	4.02	4.02	4.02	2	0.14	0.03	0.19	0.00	0.00	22.3
13	60	-1631	1179	-55	0	2	-1135	4.02	4.02	4.02	4.02	2	0.16	0.03	0.20	0.00	0.00	22.3
14	60	118	1053	-44	0	-9	-796	4.02	4.02	4.02	4.02	2	0.12	0.03	0.19	0.00	0.00	22.3
15	60	-1705	1254	-53	0	-33	-1366	4.02	4.02	4.02	4.02	2	0.20	0.04	0.21	0.00	0.00	22.3
16	60	-142	1051	-47	0	3	-781	4.02	4.02	4.02	4.02	2	0.12	0.03	0.19	0.00	0.00	22.3
17	60	-1965	1252	-56	0	-21	-1352	4.02	4.02	4.02	4.02	2	0.19	0.04	0.21	0.00	0.00	22.3
18	60	-521	1428	-126	0	-110	-1157	4.02	4.02	4.02	4.02	3	0.16	0.04	0.25	0.00	0.00	22.3

19	60	-3381	1422	-136	0	21	-1083	4.02	4.02	4.02	4.02	3	0.14	0.04	0.23	0.00	0.00	22.3
20	60	-1908	1510	-134	0	-79	-1374	4.02	4.02	4.02	4.02	3	0.19	0.04	0.26	0.00	0.00	22.3
37	60	674	1454	-101	0	-146	-1272	4.02	4.02	4.02	4.02	3	0.19	0.04	0.26	0.00	0.00	22.3
38	60	-4093	1445	-117	0	73	-1148	4.02	4.02	4.02	4.02	3	0.15	0.04	0.23	0.00	0.00	22.3
39	60	-1638	1591	-114	0	-93	-1633	4.02	4.02	4.02	4.02	3	0.22	0.05	0.27	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	120	-1201	1103	-65	0	20	701	4.02	4.02	4.02	4.02	3	0.10	0.03	0.19	0.00	0.00	22.3
2	120	-216	822	-45	0	-4	558	4.02	4.02	4.02	4.02	2	0.08	0.02	0.15	0.00	0.00	22.3
3	120	-763	883	-48	0	-10	485	4.02	4.02	4.02	4.02	2	0.07	0.03	0.15	0.00	0.00	22.3
4	120	-1084	815	-52	0	40	595	4.02	4.02	4.02	4.02	2	0.09	0.02	0.14	0.00	0.00	22.3
5	120	-1631	875	-55	0	35	521	4.02	4.02	4.02	4.02	2	0.08	0.03	0.15	0.00	0.00	22.3
6	120	118	749	-44	0	18	657	4.02	4.02	4.02	4.02	2	0.10	0.02	0.13	0.00	0.00	22.3
7	120	-1705	950	-53	0	-1	-551	4.02	4.02	4.02	4.02	2	0.08	0.03	0.16	0.00	0.00	22.3
8	120	-142	747	-47	0	31	668	4.02	4.02	4.02	4.02	2	0.10	0.02	0.13	0.00	0.00	22.3
9	120	-1965	948	-56	0	13	-538	4.02	4.02	4.02	4.02	2	0.08	0.03	0.16	0.00	0.00	22.3
10	120	-216	822	-45	0	-4	558	4.02	4.02	4.02	4.02	2	0.08	0.02	0.15	0.00	0.00	22.3
11	120	-763	883	-48	0	-10	485	4.02	4.02	4.02	4.02	2	0.07	0.03	0.15	0.00	0.00	22.3
12	120	-1084	815	-52	0	40	595	4.02	4.02	4.02	4.02	2	0.09	0.02	0.14	0.00	0.00	22.3
13	120	-1631	875	-55	0	35	521	4.02	4.02	4.02	4.02	2	0.08	0.03	0.15	0.00	0.00	22.3
14	120	118	749	-44	0	18	657	4.02	4.02	4.02	4.02	2	0.10	0.02	0.13	0.00	0.00	22.3
15	120	-1705	950	-53	0	-1	-551	4.02	4.02	4.02	4.02	2	0.08	0.03	0.16	0.00	0.00	22.3
16	120	-142	747	-47	0	31	668	4.02	4.02	4.02	4.02	2	0.10	0.02	0.13	0.00	0.00	22.3
17	120	-1965	948	-56	0	13	-538	4.02	4.02	4.02	4.02	2	0.08	0.03	0.16	0.00	0.00	22.3
18	120	-521	1032	-126	0	-35	826	4.02	4.02	4.02	4.02	3	0.12	0.03	0.18	0.00	0.00	22.3
19	120	-3381	1027	-136	0	102	892	4.02	4.02	4.02	4.02	3	0.12	0.03	0.17	0.00	0.00	22.3
20	120	-1908	1115	-134	0	2	743	4.02	4.02	4.02	4.02	3	0.10	0.03	0.19	0.00	0.00	22.3
37	120	674	1058	-101	0	-85	753	4.02	4.02	4.02	4.02	3	0.11	0.03	0.19	0.00	0.00	22.3
38	120	-4093	1049	-117	0	143	863	4.02	4.02	4.02	4.02	3	0.11	0.03	0.17	0.00	0.00	22.3
39	120	-1638	1195	-114	0	-24	613	4.02	4.02	4.02	4.02	3	0.08	0.03	0.20	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	180	-1201	707	-65	0	59	1044	4.02	4.02	4.02	4.02	3	0.14	0.02	0.12	0.00	0.00	22.3
2	180	-216	517	-45	0	23	800	4.02	4.02	4.02	4.02	2	0.12	0.01	0.09	0.00	0.00	22.3
3	180	-763	578	-48	0	19	769	4.02	4.02	4.02	4.02	2	0.11	0.02	0.10	0.00	0.00	22.3
4	180	-1084	510	-52	0	71	827	4.02	4.02	4.02	4.02	2	0.12	0.01	0.09	0.00	0.00	22.3
5	180	-1631	570	-55	0	68	800	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
6	180	118	444	-44	0	44	811	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
7	180	-1705	645	-53	0	31	735	4.02	4.02	4.02	4.02	2	0.11	0.02	0.11	0.00	0.00	22.3
8	180	-142	442	-47	0	59	821	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
9	180	-1965	643	-56	0	46	745	4.02	4.02	4.02	4.02	2	0.11	0.02	0.11	0.00	0.00	22.3
10	180	-216	517	-45	0	23	800	4.02	4.02	4.02	4.02	2	0.12	0.01	0.09	0.00	0.00	22.3
11	180	-763	578	-48	0	19	769	4.02	4.02	4.02	4.02	2	0.11	0.02	0.10	0.00	0.00	22.3
12	180	-1084	510	-52	0	71	827	4.02	4.02	4.02	4.02	2	0.12	0.01	0.09	0.00	0.00	22.3
13	180	-1631	570	-55	0	68	800	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
14	180	118	444	-44	0	44	811	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
15	180	-1705	645	-53	0	31	735	4.02	4.02	4.02	4.02	2	0.11	0.02	0.11	0.00	0.00	22.3
16	180	-142	442	-47	0	59	821	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
17	180	-1965	643	-56	0	46	745	4.02	4.02	4.02	4.02	2	0.11	0.02	0.11	0.00	0.00	22.3
18	180	-521	636	-126	0	41	1093	4.02	4.02	4.02	4.02	3	0.15	0.02	0.11	0.00	0.00	22.3
19	180	-3381	631	-136	0	184	1153	4.02	4.02	4.02	4.02	3	0.15	0.02	0.10	0.00	0.00	22.3
20	180	-1908	720	-134	0	82	1093	4.02	4.02	4.02	4.02	3	0.15	0.02	0.12	0.00	0.00	22.3
37	180	674	662	-101	0	-24	1053	4.02	4.02	4.02	4.02	3	0.15	0.02	0.12	0.00	0.00	22.3
38	180	-4093	654	-117	0	214	1152	4.02	4.02	4.02	4.02	3	0.15	0.02	0.11	0.00	0.00	22.3
39	180	-1638	800	-114	0	44	1012	4.02	4.02	4.02	4.02	3	0.14	0.02	0.14	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	240	-1201	312	-65	0	98	1060	4.02	4.02	4.02	4.02	3	0.15	0.01	0.05	0.00	0.00	22.3
2	240	-216	213	-45	0	50	800	4.02	4.02	4.02	4.02	2	0.12	0.01	0.04	0.00	0.00	22.3
3	240	-763	274	-48	0	48	805	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
4	240	-1084	206	-52	0	103	827	4.02	4.02	4.02	4.02	2	0.12	0.01	0.04	0.00	0.00	22.3
5	240	-1631	266	-55	0	100	831	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
6	240	118	140	-44	0	71	811	4.02	4.02	4.02	4.02	2	0.12	0.00	0.02	0.00	0.00	22.3
7	240	-1705	341	-53	0	64	819	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
8	240	-142	138	-47	0	87	821	4.02	4.02	4.02	4.02	2	0.12	0.00	0.02	0.00	0.00	22.3
9	240	-1965	339	-56	0	79	827	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
10	240	-216	213	-45	0	50	800	4.02	4.02	4.02	4.02	2	0.12	0.01	0.04	0.00	0.00	22.3
11	240	-763	274	-48	0	48	805	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
12	240	-1084	206	-52	0	103	827	4.02	4.02	4.02	4.02	2	0.12	0.01	0.04	0.00	0.00	22.3
13	240	-1631	266	-55	0	100	831	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
14	240	118	140	-44	0	71	811	4.02	4.02	4.02	4.02	2	0.12	0.00	0.02	0.00	0.00	22.3
15	240	-1705	341	-53	0	64	819	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
16	240	-142	138	-47	0	87	821	4.02	4.02	4.02	4.02	2	0.12	0.00	0.02	0.00	0.00	22.3
17	240	-1965	339	-56	0	79	827	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
18	240	-521	241	-126	0	116	1093	4.02	4.02	4.02	4.02	3	0.15	0.01	0.04	0.00	0.00	22.3
19	240	-3381	236	-136	0	265	1153	4.02	4.02	4.02	4.02	3	0.15	0.01	0.04	0.00	0.00	22.3
20	240	-1908	324	-134	0	162	1117	4.02	4.02	4.02	4.02	3	0.15	0.01	0.06	0.00	0.00	22.3
37	240	674	267	-101	0	37	1053	4.02	4.02	4.02	4.02	3	0.15	0.01	0.05	0.00	0.00	22.3
38	240	-4093	258	-117	0	284	1152	4.02	4.02	4.02	4.02	3	0.15	0.01	0.04	0.00	0.00	22.3
39	240	-1638	404	-114	0	113	1092	4.02	4.02	4.02	4.02	3	0.15	0.01	0.07	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	300	-1201	-84	-65	0	137	1060	4.02	4.02	4.02	4.02	3	0.15	0.00	0.01	0.00	0.00	22.3
2	300	-216	-91	-45	0	77	800	4.02	4.02	4.02	4.02	2	0.12	0.00	0.02	0.00	0.00	22.3
3	300	-763	-30	-48	0	76	805	4.02	4.02	4.02	4.02	2	0.12	0.00	0.01	0.00	0.00	22.3
4	300	-1084	-98	-52	0	134	827	4.02	4.02	4.02	4.02	2	0.12	0.00	0.02	0.00	0.00	22.3
5	300	-1631	-38	-55	0	133	831	4.02	4.02	4.02	4.02	2	0.12	0.00	0.01	0.00	0.00	22.3
6	300	118	-164	-44	0	98	811	4.02	4.02	4.02	4.02	2	0.12	0.00	0.03	0.00	0.00	22.3
7	300	-1705	37	-53	0	96	819	4.02	4.02	4.02	4.02	2	0.12	0.00	0.01	0.00	0.00	22.3
8	300	-142	-166	-47	0	115	821	4.02	4.02	4.02	4.02	2	0.12	0.00	0.03	0.00	0.00	22.3
9	300	-1965	35	-56	0	113	827	4.02	4.02	4.02	4.02	2	0.12	0.00	0.01	0.00	0.00	22.3
10	300	-216	-91	-45	0	77	800	4.02	4.02	4.02	4.02	2	0.12	0.00	0.02	0.00	0.00	22.3
11	300	-763	-30	-48	0	76	805	4.02	4.02	4.02	4.02	2	0.12	0.00	0.01	0.00	0.00	22.3
12	300	-1084	-98	-52	0	134	827	4.02	4.02	4.02	4.02	2	0.12	0.00	0.02	0.00	0.00	22.3
13	300	-1631	-38	-55	0	133	831	4.02	4.02	4.02	4.02	2	0.12	0.00	0.01	0.00	0.00	22.3
14	300	118	-164	-44	0	98	811	4.02	4.02	4.02	4.02	2	0.12	0.00	0.03	0.00	0.00	22.3
15	300	-1705	37	-53	0	96	819	4.02	4.02	4.02	4.02	2	0.12	0.00	0.01	0.00	0.00	22.3
16	300	-142	-166	-47	0	115	821	4.02	4.02	4.02	4.02	2	0.12	0.00	0.03	0.00	0.00	22.3
17	300	-1965	35	-56	0	113	827	4.02	4.02	4.02	4.02	2	0.12	0.00	0.01	0.00	0.00	22.3
18	300	-521	-155	-126	0	192	1093	4.02	4.02	4.02	4.02	3	0.15	0.00	0.03	0.00	0.00	22.3
19	300	-3381	-160	-136	0	346	1153	4.02	4.02	4.02	4.02	3	0.15	0.00	0.03	0.00	0.00	22.3
20	300	-1908	-72	-134	0	242	1117	4.02	4.02	4.02	4.02	3	0.15	0.00	0.01	0.00	0.00	22.3
37	300	674	-129	-101	0	98	1053	4.02	4.02	4.02	4.02	3	0.15	0.00	0.02	0.00	0.00	22.3
38	300	-4093	-137	-117	0	355	1152	4.02	4.02	4.02	4.02	3	0.15	0.00	0.02	0.00	0.00	22.3
39	300	-1638	9	-114	0	181	1092	4.02	4.02	4.02	4.02	3	0.15	0.00	0.00	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	360	-1201	-479	-65	0	176	1060	4.02	4.02	4.02	4.02	3	0.15	0.01	0.08	0.00	0.00	22.3
2	360	-216	-395	-45	0	104	800	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
3	360	-763	-334	-48	0	105	805	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
4	360	-1084	-402	-52	0	165	827	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
5	360	-1631	-342	-55	0	166	831	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
6	360	118	-468	-44	0	124	811	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
7	360	-1705	-267	-53	0	128	819	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
8	360	-142	-470	-47	0	143	821	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
9	360	-1965	-269	-56	0	146	827	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
10	360	-216	-395	-45	0	104	800	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
11	360	-763	-334	-48	0	105	805	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
12	360	-1084	-402	-52	0	165	827	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
13	360	-1631	-342	-55	0	166	831	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
14	360	118	-468	-44	0	124	811	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
15	360	-1705	-267	-53	0	128	819	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
16	360	-142	-470	-47	0	143	821	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
17	360	-1965	-269	-56	0	146	827	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
18	360	-521	-550	-126	0	268	1093	4.02	4.02	4.02	4.02	3	0.15	0.02	0.10	0.00	0.00	22.3
19	360	-3381	-555	-136	0	428	1153	4.02	4.02	4.02	4.02	3	0.15	0.02	0.09	0.00	0.00	22.3
20	360	-1908	-467	-134	0	323	1117	4.02	4.02	4.02	4.02	3	0.15	0.01	0.08	0.00	0.00	22.3
37	360	674	-524	-101	0	159	1053	4.02	4.02	4.02	4.02	3	0.15	0.02	0.09	0.00	0.00	22.3
38	360	-4093	-532	-117	0	425	1152	4.02	4.02	4.02	4.02	3	0.15	0.02	0.09	0.00	0.00	22.3
39	360	-1638	-386	-114	0	250	1092	4.02	4.02	4.02	4.02	3	0.15	0.01	0.07	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	420	-1201	-874	-65	0	215	928	4.02	4.02	4.02	4.02	3	0.13	0.03	0.15	0.00	0.00	22.3
2	420	-216	-699	-45	0	131	680	4.02	4.02	4.02	4.02	2	0.10	0.02	0.12	0.00	0.00	22.3
3	420	-763	-638	-48	0	134	726	4.02	4.02	4.02	4.02	2	0.11	0.02	0.11	0.00	0.00	22.3
4	420	-1084	-706	-52	0	197	701	4.02	4.02	4.02	4.02	2	0.10	0.02	0.12	0.00	0.00	22.3
5	420	-1631	-646	-55	0	199	748	4.02	4.02	4.02	4.02	2	0.11	0.02	0.11	0.00	0.00	22.3
6	420	118	-772	-44	0	151	634	4.02	4.02	4.02	4.02	2	0.10	0.02	0.14	0.00	0.00	22.3
7	420	-1705	-571	-53	0	160	788	4.02	4.02	4.02	4.02	2	0.11	0.02	0.10	0.00	0.00	22.3
8	420	-142	-774	-47	0	171	640	4.02	4.02	4.02	4.02	2	0.10	0.02	0.14	0.00	0.00	22.3
9	420	-1965	-573	-56	0	179	794	4.02	4.02	4.02	4.02	2	0.11	0.02	0.10	0.00	0.00	22.3
10	420	-216	-699	-45	0	131	680	4.02	4.02	4.02	4.02	2	0.10	0.02	0.12	0.00	0.00	22.3
11	420	-763	-638	-48	0	134	726	4.02	4.02	4.02	4.02	2	0.11	0.02	0.11	0.00	0.00	22.3
12	420	-1084	-706	-52	0	197	701	4.02	4.02	4.02	4.02	2	0.10	0.02	0.12	0.00	0.00	22.3
13	420	-1631	-646	-55	0	199	748	4.02	4.02	4.02	4.02	2	0.11	0.02	0.11	0.00	0.00	22.3
14	420	118	-772	-44	0	151	634	4.02	4.02	4.02	4.02	2	0.10	0.02	0.14	0.00	0.00	22.3
15	420	-1705	-571	-53	0	160	788	4.02	4.02	4.02	4.02	2	0.11	0.02	0.10	0.00	0.00	22.3
16	420	-142	-774	-47	0	171	640	4.02	4.02	4.02	4.02	2	0.10	0.02	0.14	0.00	0.00	22.3
17	420	-1965	-573	-56	0	179	794	4.02	4.02	4.02	4.02	2	0.11	0.02	0.10	0.00	0.00	22.3
18	420	-521	-946	-126	0	343	913	4.02	4.02	4.02	4.02	3	0.13	0.03	0.17	0.00	0.00	22.3
19	420	-3381	-950	-136	0	509	968	4.02	4.02	4.02	4.02	3	0.13	0.03	0.16	0.00	0.00	22.3
20	420	-1908	-862	-134	0	403	993	4.02	4.02	4.02	4.02	3	0.13	0.02	0.15	0.00	0.00	22.3
37	420	674	-920	-101	0	219	890	4.02	4.02	4.02	4.02	3	0.13	0.03	0.16	0.00	0.00	22.3
38	420	-4093	-928	-117	0	495	983	4.02	4.02	4.02	4.02	3	0.13	0.03	0.15	0.00	0.00	22.3
39	420	-1638	-782	-114	0	319	1025	4.02	4.02	4.02	4.02	3	0.14	0.02	0.13	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	480	-1201	-1270	-65	0	254	-801	4.02	4.02	4.02	4.02	3	0.11	0.04	0.22	0.00	0.00	22.3
2	480	-216	-1004	-45	0	158	-693	4.02	4.02	4.02	4.02	2	0.10	0.03	0.18	0.00	0.00	22.3
3	480	-763	-943	-48	0	162	-549	4.02	4.02	4.02	4.02	2	0.08	0.03	0.16	0.00	0.00	22.3
4	480	-1084	-1011	-52	0	228	-683	4.02	4.02	4.02	4.02	2	0.10	0.03	0.18	0.00	0.00	22.3
5	480	-1631	-951	-55	0	232	-540	4.02	4.02	4.02	4.02	2	0.08	0.03	0.16	0.00	0.00	22.3
6	480	118	-1077	-44	0	178	-857	4.02	4.02	4.02	4.02	2	0.13	0.03	0.19	0.00	0.00	22.3
7	480	-1705	-876	-53	0	192	508	4.02	4.02	4.02	4.02	2	0.07	0.03	0.15	0.00	0.00	22.3
8	480	-142	-1079	-47	0	199	-854	4.02	4.02	4.02	4.02	2	0.13	0.03	0.19	0.00	0.00	22.3
9	480	-1965	-878	-56	0	213	513	4.02	4.02	4.02	4.02	2	0.07	0.03	0.15	0.00	0.00	22.3
10	480	-216	-1004	-45	0	158	-693	4.02	4.02	4.02	4.02	2	0.10	0.03	0.18	0.00	0.00	22.3
11	480	-763	-943	-48	0	162	-549	4.02	4.02	4.02	4.02	2	0.08	0.03	0.16	0.00	0.00	22.3
12	480	-1084	-1011	-52	0	228	-683	4.02	4.02	4.02	4.02	2	0.10	0.03	0.18	0.00	0.00	22.3
13	480	-1631	-951	-55	0	232	-540	4.02	4.02	4.02	4.02	2	0.08	0.03	0.16	0.00	0.00	22.3
14	480	118	-1077	-44	0	178	-857	4.02	4.02	4.02	4.02	2	0.13	0.03	0.19	0.00	0.00	22.3
15	480	-1705	-876	-53	0	192	508	4.02	4.02	4.02	4.02	2	0.07	0.03	0.15	0.00	0.00	22.3
16	480	-142	-1079	-47	0	199	-854	4.02	4.02	4.02	4.02	2	0.13	0.03	0.19	0.00	0.00	22.3
17	480	-1965	-878	-56	0	213	513	4.02	4.02	4.02	4.02	2	0.07	0.03	0.15	0.00	0.00	22.3
18	480	-521	-1341	-126	0	419	-931	4.02	4.02	4.02	4.02	3	0.13	0.04	0.24	0.00	0.00	22.3
19	480	-3381	-1346	-136	0	590	-883	4.02	4.02	4.02	4.02	3	0.13	0.04	0.22	0.00	0.00	22.3
20	480	-1908	-1258	-134	0	483	-717	4.02	4.02	4.02	4.02	3	0.11	0.04	0.21	0.00	0.00	22.3
37	480	674	-1315	-101	0	280	-911	4.02	4.02	4.02	4.02	3	0.13	0.04	0.23	0.00	0.00	22.3
38	480	-4093	-1323	-117	0	566	-832	4.02	4.02	4.02	4.02	3	0.13	0.04	0.21	0.00	0.00	22.3
39	480	-1638	-1177	-114	0	387	637	4.02	4.02	4.02	4.02	3	0.09	0.03	0.20	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	540	-1201	-1665	-65	0	293	-1882	4.02	4.02	4.02	4.02	3	0.26	0.05	0.29	0.00	0.00	22.3
2	540	-216	-1308	-45	0	185	-1540	4.02	4.02	4.02	4.02	2	0.23	0.04	0.23	0.00	0.00	22.3
3	540	-763	-1247	-48	0	191	-1360	4.02	4.02	4.02	4.02	2	0.20	0.04	0.22	0.00	0.00	22.3
4	540	-1084	-1315	-52	0	259	-1535	4.02	4.02	4.02	4.02	2	0.23	0.04	0.23	0.00	0.00	22.3
5	540	-1631	-1255	-55	0	265	-1355	4.02	4.02	4.02	4.02	2	0.20	0.04	0.22	0.00	0.00	22.3
6	540	118	-1381	-44	0	205	-1748	4.02	4.02	4.02	4.02	2	0.27	0.04	0.25	0.00	0.00	22.3
7	540	-1705	-1180	-53	0	224	-1149	4.02	4.02	4.02	4.02	2	0.17	0.03	0.20	0.00	0.00	22.3
8	540	-142	-1383	-47	0	227	-1746	4.02	4.02	4.02	4.02	2	0.26	0.04	0.25	0.00	0.00	22.3
9	540	-1965	-1182	-56	0	246	-1147	4.02	4.02	4.02	4.02	2	0.16	0.03	0.20	0.00	0.00	22.3
10	540	-216	-1308	-45	0	185	-1540	4.02	4.02	4.02	4.02	2	0.23	0.04	0.23	0.00	0.00	22.3
11	540	-763	-1247	-48	0	191	-1360	4.02	4.02	4.02	4.02	2	0.20	0.04	0.22	0.00	0.00	22.3
12	540	-1084	-1315	-52	0	259	-1535	4.02	4.02	4.02	4.02	2	0.23	0.04	0.23	0.00	0.00	22.3
13	540	-1631	-1255	-55	0	265	-1355	4.02	4.02	4.02	4.02	2	0.20	0.04	0.22	0.00	0.00	22.3
14	540	118	-1381	-44	0	205	-1748	4.02	4.02	4.02	4.02	2	0.27	0.04	0.25	0.00	0.00	22.3
15	540	-1705	-1180	-53	0	224	-1149	4.02	4.02	4.02	4.02	2	0.17	0.03	0.20	0.00	0.00	22.3
16	540	-142	-1383	-47	0	227	-1746	4.02	4.02	4.02	4.02	2	0.26	0.04	0.25	0.00	0.00	22.3
17	540	-1965	-1182	-56	0	246	-1147	4.02	4.02	4.02	4.02	2	0.16	0.03	0.20	0.00	0.00	22.3
18	540	-521	-1736	-126	0	494	-2054	4.02	4.02	4.02	4.02	3	0.29	0.05	0.31	0.00	0.00	22.3
19	540	-3381	-1741	-136	0	672	-2009	4.02	4.02	4.02	4.02	3	0.26	0.05	0.29	0.00	0.00	22.3
20	540	-1908	-1653	-134	0	563	-1790	4.02	4.02	4.02	4.02	3	0.24	0.05	0.28	0.00	0.00	22.3
37	540	674	-1710	-101	0	341	-2019	4.02	4.02	4.02	4.02	3	0.30	0.05	0.30	0.00	0.00	22.3
38	540	-4093	-1719	-117	0	636	-1945	4.02	4.02	4.02	4.02	3	0.25	0.05	0.28	0.00	0.00	22.3
39	540	-1638	-1573	-114	0	456	-1580	4.02	4.02	4.02	4.02	3	0.22	0.05	0.27	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	600	-1201	-2061	-65	0	332	-2157	4.02	4.02	4.02	4.02	3	0.30	0.06	0.36	0.00	0.00	22.3
2	600	-216	-1612	-45	0	213	-1754	4.02	4.02	4.02	4.02	2	0.26	0.05	0.29	0.00	0.00	22.3
3	600	-763	-1551	-48	0	220	-1568	4.02	4.02	4.02	4.02	2	0.23	0.04	0.27	0.00	0.00	22.3
4	600	-1084	-1619	-52	0	291	-1750	4.02	4.02	4.02	4.02	2	0.26	0.05	0.28	0.00	0.00	22.3

5	600	-1631	-1559	-55	0	298	-1564	4.02	4.02	4.02	4.02	2	0.23	0.04	0.27	0.00	0.00	22.3
6	600	118	-1685	-44	0	231	-1969	4.02	4.02	4.02	4.02	2	0.30	0.05	0.30	0.00	0.00	22.3
7	600	-1705	-1484	-53	0	256	-1351	4.02	4.02	4.02	4.02	2	0.19	0.04	0.25	0.00	0.00	22.3
8	600	-142	-1687	-47	0	255	-1967	4.02	4.02	4.02	4.02	2	0.30	0.05	0.30	0.00	0.00	22.3
9	600	-1965	-1486	-56	0	279	-1349	4.02	4.02	4.02	4.02	2	0.19	0.04	0.25	0.00	0.00	22.3
10	600	-216	-1612	-45	0	213	-1754	4.02	4.02	4.02	4.02	2	0.26	0.05	0.29	0.00	0.00	22.3
11	600	-763	-1551	-48	0	220	-1568	4.02	4.02	4.02	4.02	2	0.23	0.04	0.27	0.00	0.00	22.3
12	600	-1084	-1619	-52	0	291	-1750	4.02	4.02	4.02	4.02	2	0.26	0.05	0.28	0.00	0.00	22.3
13	600	-1631	-1559	-55	0	298	-1564	4.02	4.02	4.02	4.02	2	0.23	0.04	0.27	0.00	0.00	22.3
14	600	118	-1685	-44	0	231	-1969	4.02	4.02	4.02	4.02	2	0.30	0.05	0.30	0.00	0.00	22.3
15	600	-1705	-1484	-53	0	256	-1351	4.02	4.02	4.02	4.02	2	0.19	0.04	0.25	0.00	0.00	22.3
16	600	-142	-1687	-47	0	255	-1967	4.02	4.02	4.02	4.02	2	0.30	0.05	0.30	0.00	0.00	22.3
17	600	-1965	-1486	-56	0	279	-1349	4.02	4.02	4.02	4.02	2	0.19	0.04	0.25	0.00	0.00	22.3
18	600	-521	-2132	-126	0	570	-2335	4.02	4.02	4.02	4.02	3	0.33	0.06	0.38	0.00	0.00	22.3
19	600	-3381	-2137	-136	0	753	-2291	4.02	4.02	4.02	4.02	3	0.30	0.06	0.35	0.00	0.00	22.3
20	600	-1908	-2049	-134	0	644	-2064	4.02	4.02	4.02	4.02	3	0.28	0.06	0.35	0.00	0.00	22.3
37	600	674	-2106	-101	0	402	-2298	4.02	4.02	4.02	4.02	3	0.34	0.06	0.38	0.00	0.00	22.3
38	600	-4093	-2114	-117	0	707	-2225	4.02	4.02	4.02	4.02	3	0.28	0.06	0.34	0.00	0.00	22.3
39	600	-1638	-1968	-114	0	524	-1846	4.02	4.02	4.02	4.02	3	0.25	0.06	0.34	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

Nome travata: **Trave_403_IP1** Descrizione: **Trave_4 7-6-5-4-3-2-1**
ASTA NUM. 12 NI 251 NF 252 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y Permanente qy tot.
qy medio: 375.00 132.00 507.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-1037	1974	111	0	453	-1928	4.02	4.02	4.02	4.02	3	0.27	0.06	0.34	0.00	0.00	22.3
2	0	-221	1469	95	0	361	-1342	4.02	4.02	4.02	4.02	2	0.20	0.04	0.26	0.00	0.00	22.3
3	0	-637	1537	70	0	279	-1545	4.02	4.02	4.02	4.02	2	0.23	0.04	0.27	0.00	0.00	22.3
4	0	-958	1501	101	0	418	-1421	4.02	4.02	4.02	4.02	2	0.21	0.04	0.26	0.00	0.00	22.3
5	0	-1374	1568	76	0	336	-1624	4.02	4.02	4.02	4.02	2	0.24	0.05	0.27	0.00	0.00	22.3
6	0	6	1402	127	0	477	-1134	4.02	4.02	4.02	4.02	2	0.17	0.04	0.25	0.00	0.00	22.3
7	0	-1380	1626	42	0	203	-1809	4.02	4.02	4.02	4.02	2	0.26	0.05	0.28	0.00	0.00	22.3
8	0	-215	1411	129	0	494	-1157	4.02	4.02	4.02	4.02	2	0.17	0.04	0.25	0.00	0.00	22.3
9	0	-1602	1635	44	0	220	-1832	4.02	4.02	4.02	4.02	2	0.27	0.05	0.28	0.00	0.00	22.3
10	0	-221	1469	95	0	361	-1342	4.02	4.02	4.02	4.02	2	0.20	0.04	0.26	0.00	0.00	22.3
11	0	-637	1537	70	0	279	-1545	4.02	4.02	4.02	4.02	2	0.23	0.04	0.27	0.00	0.00	22.3
12	0	-958	1501	101	0	418	-1421	4.02	4.02	4.02	4.02	2	0.21	0.04	0.26	0.00	0.00	22.3
13	0	-1374	1568	76	0	336	-1624	4.02	4.02	4.02	4.02	2	0.24	0.05	0.27	0.00	0.00	22.3
14	0	6	1402	127	0	477	-1134	4.02	4.02	4.02	4.02	2	0.17	0.04	0.25	0.00	0.00	22.3
15	0	-1380	1626	42	0	203	-1809	4.02	4.02	4.02	4.02	2	0.26	0.05	0.28	0.00	0.00	22.3
16	0	-215	1411	129	0	494	-1157	4.02	4.02	4.02	4.02	2	0.17	0.04	0.25	0.00	0.00	22.3
17	0	-1602	1635	44	0	220	-1832	4.02	4.02	4.02	4.02	2	0.27	0.05	0.28	0.00	0.00	22.3
18	0	-100	1919	204	0	788	-1758	4.02	4.02	4.02	4.02	3	0.25	0.06	0.34	0.00	0.00	22.3
19	0	-2820	2016	208	0	912	-2002	4.02	4.02	4.02	4.02	3	0.27	0.06	0.34	0.00	0.00	22.3
20	0	-1339	2047	131	0	593	-2127	4.02	4.02	4.02	4.02	3	0.29	0.06	0.35	0.00	0.00	22.3
37	0	940	1890	172	0	617	-1692	4.02	4.02	4.02	4.02	3	0.25	0.05	0.34	0.00	0.00	22.3
38	0	-3593	2050	178	0	824	-2100	4.02	4.02	4.02	4.02	3	0.27	0.06	0.34	0.00	0.00	22.3
39	0	-1125	2103	50	0	294	-2308	4.02	4.02	4.02	4.02	3	0.32	0.06	0.36	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	60	-1037	1579	111	0	386	-1661	4.02	4.02	4.02	4.02	3	0.23	0.05	0.27	0.00	0.00	22.3
2	60	-221	1165	95	0	304	-1141	4.02	4.02	4.02	4.02	2	0.17	0.03	0.21	0.00	0.00	22.3
3	60	-637	1233	70	0	237	-1338	4.02	4.02	4.02	4.02	2	0.20	0.04	0.22	0.00	0.00	22.3
4	60	-958	1197	101	0	357	-1218	4.02	4.02	4.02	4.02	2	0.18	0.03	0.21	0.00	0.00	22.3
5	60	-1374	1264	76	0	291	-1414	4.02	4.02	4.02	4.02	2	0.21	0.04	0.22	0.00	0.00	22.3
6	60	6	1098	127	0	400	-940	4.02	4.02	4.02	4.02	2	0.14	0.03	0.20	0.00	0.00	22.3
7	60	-1380	1322	42	0	178	-1594	4.02	4.02	4.02	4.02	2	0.23	0.04	0.23	0.00	0.00	22.3
8	60	-215	1107	129	0	416	-962	4.02	4.02	4.02	4.02	2	0.14	0.03	0.20	0.00	0.00	22.3
9	60	-1602	1331	44	0	194	-1616	4.02	4.02	4.02	4.02	2	0.23	0.04	0.23	0.00	0.00	22.3
10	60	-221	1165	95	0	304	-1141	4.02	4.02	4.02	4.02	2	0.17	0.03	0.21	0.00	0.00	22.3
11	60	-637	1233	70	0	237	-1338	4.02	4.02	4.02	4.02	2	0.20	0.04	0.22	0.00	0.00	22.3
12	60	-958	1197	101	0	357	-1218	4.02	4.02	4.02	4.02	2	0.18	0.03	0.21	0.00	0.00	22.3
13	60	-1374	1264	76	0	291	-1414	4.02	4.02	4.02	4.02	2	0.21	0.04	0.22	0.00	0.00	22.3
14	60	6	1098	127	0	400	-940	4.02	4.02	4.02	4.02	2	0.14	0.03	0.20	0.00	0.00	22.3
15	60	-1380	1322	42	0	178	-1594	4.02	4.02	4.02	4.02	2	0.23	0.04	0.23	0.00	0.00	22.3
16	60	-215	1107	129	0	416	-962	4.02	4.02	4.02	4.02	2	0.14	0.03	0.20	0.00	0.00	22.3
17	60	-1602	1331	44	0	194	-1616	4.02	4.02	4.02	4.02	2	0.23	0.04	0.23	0.00	0.00	22.3
18	60	-100	1524	204	0	665	-1496	4.02	4.02	4.02	4.02	3	0.21	0.04	0.27	0.00	0.00	22.3
19	60	-2820	1620	208	0	787	-1732	4.02	4.02	4.02	4.02	3	0.23	0.05	0.27	0.00	0.00	22.3
20	60	-1339	1652	131	0	515	-1853	4.02	4.02	4.02	4.02	3	0.26	0.05	0.28	0.00	0.00	22.3
37	60	940	1494	172	0	514	-1433	4.02	4.02	4.02	4.02	3	0.21	0.04	0.27	0.00	0.00	22.3
38	60	-3593	1655	178	0	717	-1826	4.02	4.02	4.02	4.02	3	0.24	0.05	0.27	0.00	0.00	22.3
39	60	-1125	1708	50	0	264	-2029	4.02	4.02	4.02	4.02	3	0.28	0.05	0.30	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	120	-1037	1183	111	0	319	-633	4.02	4.02	4.02	4.02	3	0.09	0.03	0.21	0.00	0.00	22.3
2	120	-221	861	95	0	246	492	4.02	4.02	4.02	4.02	2	0.07	0.02	0.15	0.00	0.00	22.3
3	120	-637	929	70	0	195	-536	4.02	4.02	4.02	4.02	2	0.08	0.03	0.16	0.00	0.00	22.3
4	120	-958	893	101	0	297	466	4.02	4.02	4.02	4.02	2	0.08	0.03	0.16	0.00	0.00	22.3
5	120	-1374	960	76	0	245	-593	4.02	4.02	4.02	4.02	2	0.09	0.03	0.17	0.00	0.00	22.3
6	120	6	794	127	0	324	585	4.02	4.02	4.02	4.02	2	0.09	0.02	0.14	0.00	0.00	22.3
7	120	-1380	1018	42	0	153	-738	4.02	4.02	4.02	4.02	2	0.11	0.03	0.18	0.00	0.00	22.3
8	120	-215	803	129	0	339	578	4.02	4.02	4.02	4.02	2	0.09	0.02	0.14	0.00	0.00	22.3
9	120	-1602	1027	44	0	168	-755	4.02	4.02	4.02	4.02	2	0.11	0.03	0.18	0.00	0.00	22.3
10	120	-221	861	95	0	246	492	4.02	4.02	4.02	4.02	2	0.07	0.02	0.15	0.00	0.00	22.3
11	120	-637	929	70	0	195	-536	4.02	4.02	4.02	4.02	2	0.08	0.03	0.16	0.00	0.00	22.3
12	120	-958	893	101	0	297	466	4.02	4.02	4.02	4.02	2	0.08	0.03	0.16	0.00	0.00	22.3
13	120	-1374	960	76	0	245	-593	4.02	4.02	4.02	4.02	2	0.09	0.03	0.17	0.00	0.00	22.3
14	120	6	794	127	0	324	585	4.02	4.02	4.02	4.02	2	0.09	0.02	0.14	0.00	0.00	22.3
15	120	-1380	1018	42	0	153	-738	4.02	4.02	4.02	4.02	2	0.11	0.03	0.18	0.00	0.00	22.3
16	120	-215	803	129	0	339	578	4.02	4.02	4.02	4.02	2	0.09	0.02	0.14	0.00	0.00	22.3
17	120	-1602	1027	44	0	168	-755	4.02	4.02	4.02	4.02	2	0.11	0.03	0.18	0.00	0.00	22.3
18	120	-100	1128	204	0	543	642	4.02	4.02	4.02	4.02	3	0.13	0.03	0.20	0.00	0.00	22.3
19	120	-2820	1225	208	0	662	-678	4.02	4.02	4.02	4.02	3	0.15	0.04	0.20	0.00	0.00	22.3
20	120	-1339	1256	131	0	437	-781	4.02	4.02	4.02	4.02	3	0.11	0.04	0.22	0.00	0.00	22.3
37	120	940	1099	172	0	411	657	4.02	4.02	4.02	4.02	3	0.10	0.03	0.20	0.00	0.00	22.3
38	120	-3593	1259	178	0	609	-752	4.02	4.02	4.02	4.02	3	0.14	0.04	0.21	0.00	0.00	22.3

39	120	-1125	1312	50	0	234	-923	4.02	4.02	4.02	4.02	3	0.13	0.04	0.23	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	180	-1037	788	111	0	253	957	4.02	4.02	4.02	4.02	3	0.13	0.02	0.14	0.00	0.00	22.3
2	180	-221	556	95	0	189	763	4.02	4.02	4.02	4.02	2	0.11	0.02	0.10	0.00	0.00	22.3
3	180	-637	624	70	0	153	716	4.02	4.02	4.02	4.02	2	0.11	0.02	0.11	0.00	0.00	22.3
4	180	-958	588	101	0	236	756	4.02	4.02	4.02	4.02	2	0.11	0.02	0.10	0.00	0.00	22.3
5	180	-1374	655	76	0	200	709	4.02	4.02	4.02	4.02	2	0.10	0.02	0.11	0.00	0.00	22.3
6	180	6	489	127	0	247	791	4.02	4.02	4.02	4.02	2	0.12	0.01	0.09	0.00	0.00	22.3
7	180	-1380	713	42	0	128	657	4.02	4.02	4.02	4.02	2	0.10	0.02	0.12	0.00	0.00	22.3
8	180	-215	498	129	0	261	796	4.02	4.02	4.02	4.02	2	0.12	0.01	0.09	0.00	0.00	22.3
9	180	-1602	722	44	0	142	656	4.02	4.02	4.02	4.02	2	0.09	0.02	0.12	0.00	0.00	22.3
10	180	-221	556	95	0	189	763	4.02	4.02	4.02	4.02	2	0.11	0.02	0.10	0.00	0.00	22.3
11	180	-637	624	70	0	153	716	4.02	4.02	4.02	4.02	2	0.11	0.02	0.11	0.00	0.00	22.3
12	180	-958	588	101	0	236	756	4.02	4.02	4.02	4.02	2	0.11	0.02	0.10	0.00	0.00	22.3
13	180	-1374	655	76	0	200	709	4.02	4.02	4.02	4.02	2	0.10	0.02	0.11	0.00	0.00	22.3
14	180	6	489	127	0	247	791	4.02	4.02	4.02	4.02	2	0.12	0.01	0.09	0.00	0.00	22.3
15	180	-1380	713	42	0	128	657	4.02	4.02	4.02	4.02	2	0.10	0.02	0.12	0.00	0.00	22.3
16	180	-215	498	129	0	261	796	4.02	4.02	4.02	4.02	2	0.12	0.01	0.09	0.00	0.00	22.3
17	180	-1602	722	44	0	142	656	4.02	4.02	4.02	4.02	2	0.09	0.02	0.12	0.00	0.00	22.3
18	180	-100	733	204	0	421	1000	4.02	4.02	4.02	4.02	3	0.14	0.02	0.13	0.00	0.00	22.3
19	180	-2820	830	208	0	537	978	4.02	4.02	4.02	4.02	3	0.13	0.02	0.14	0.00	0.00	22.3
20	180	-1339	861	131	0	358	926	4.02	4.02	4.02	4.02	3	0.13	0.02	0.15	0.00	0.00	22.3
37	180	940	703	172	0	308	998	4.02	4.02	4.02	4.02	3	0.15	0.02	0.13	0.00	0.00	22.3
38	180	-3593	864	178	0	502	960	4.02	4.02	4.02	4.02	3	0.12	0.02	0.14	0.00	0.00	22.3
39	180	-1125	917	50	0	204	873	4.02	4.02	4.02	4.02	3	0.12	0.03	0.16	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	240	-1037	392	111	0	186	1028	4.02	4.02	4.02	4.02	3	0.14	0.01	0.07	0.00	0.00	22.3
2	240	-221	252	95	0	132	785	4.02	4.02	4.02	4.02	2	0.12	0.01	0.04	0.00	0.00	22.3
3	240	-637	320	70	0	111	784	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
4	240	-958	284	101	0	175	799	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
5	240	-1374	351	76	0	154	798	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
6	240	6	185	127	0	171	791	4.02	4.02	4.02	4.02	2	0.12	0.01	0.03	0.00	0.00	22.3
7	240	-1380	409	42	0	103	787	4.02	4.02	4.02	4.02	2	0.11	0.01	0.07	0.00	0.00	22.3
8	240	-215	194	129	0	184	796	4.02	4.02	4.02	4.02	2	0.12	0.01	0.03	0.00	0.00	22.3
9	240	-1602	418	44	0	116	792	4.02	4.02	4.02	4.02	2	0.11	0.01	0.07	0.00	0.00	22.3
10	240	-221	252	95	0	132	785	4.02	4.02	4.02	4.02	2	0.12	0.01	0.04	0.00	0.00	22.3
11	240	-637	320	70	0	111	784	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
12	240	-958	284	101	0	175	799	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
13	240	-1374	351	76	0	154	798	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
14	240	6	185	127	0	171	791	4.02	4.02	4.02	4.02	2	0.12	0.01	0.03	0.00	0.00	22.3
15	240	-1380	409	42	0	103	787	4.02	4.02	4.02	4.02	2	0.11	0.01	0.07	0.00	0.00	22.3
16	240	-215	194	129	0	184	796	4.02	4.02	4.02	4.02	2	0.12	0.01	0.03	0.00	0.00	22.3
17	240	-1602	418	44	0	116	792	4.02	4.02	4.02	4.02	2	0.11	0.01	0.07	0.00	0.00	22.3
18	240	-100	337	204	0	298	1034	4.02	4.02	4.02	4.02	3	0.15	0.01	0.06	0.00	0.00	22.3
19	240	-2820	434	208	0	412	1079	4.02	4.02	4.02	4.02	3	0.14	0.01	0.07	0.00	0.00	22.3
20	240	-1339	465	131	0	280	1048	4.02	4.02	4.02	4.02	3	0.14	0.01	0.08	0.00	0.00	22.3
37	240	940	308	172	0	205	1011	4.02	4.02	4.02	4.02	3	0.15	0.01	0.05	0.00	0.00	22.3
38	240	-3593	468	178	0	395	1085	4.02	4.02	4.02	4.02	3	0.14	0.01	0.08	0.00	0.00	22.3
39	240	-1125	521	50	0	175	1034	4.02	4.02	4.02	4.02	3	0.14	0.02	0.09	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	300	-1037	-3	111	0	119	1028	4.02	4.02	4.02	4.02	3	0.14	0.00	0.00	0.00	0.00	22.3
2	300	-221	-52	95	0	74	785	4.02	4.02	4.02	4.02	2	0.12	0.00	0.01	0.00	0.00	22.3
3	300	-637	16	70	0	69	784	4.02	4.02	4.02	4.02	2	0.12	0.00	0.00	0.00	0.00	22.3
4	300	-958	-20	101	0	114	799	4.02	4.02	4.02	4.02	2	0.12	0.00	0.00	0.00	0.00	22.3
5	300	-1374	47	76	0	109	798	4.02	4.02	4.02	4.02	2	0.12	0.00	0.01	0.00	0.00	22.3
6	300	6	-119	127	0	94	791	4.02	4.02	4.02	4.02	2	0.12	0.00	0.02	0.00	0.00	22.3
7	300	-1380	105	42	0	77	787	4.02	4.02	4.02	4.02	2	0.11	0.00	0.02	0.00	0.00	22.3
8	300	-215	-110	129	0	106	796	4.02	4.02	4.02	4.02	2	0.12	0.00	0.02	0.00	0.00	22.3
9	300	-1602	114	44	0	89	792	4.02	4.02	4.02	4.02	2	0.11	0.00	0.02	0.00	0.00	22.3
10	300	-221	-52	95	0	74	785	4.02	4.02	4.02	4.02	2	0.12	0.00	0.01	0.00	0.00	22.3
11	300	-637	16	70	0	69	784	4.02	4.02	4.02	4.02	2	0.12	0.00	0.00	0.00	0.00	22.3
12	300	-958	-20	101	0	114	799	4.02	4.02	4.02	4.02	2	0.12	0.00	0.00	0.00	0.00	22.3
13	300	-1374	47	76	0	109	798	4.02	4.02	4.02	4.02	2	0.12	0.00	0.01	0.00	0.00	22.3
14	300	6	-119	127	0	94	791	4.02	4.02	4.02	4.02	2	0.12	0.00	0.02	0.00	0.00	22.3
15	300	-1380	105	42	0	77	787	4.02	4.02	4.02	4.02	2	0.11	0.00	0.02	0.00	0.00	22.3
16	300	-215	-110	129	0	106	796	4.02	4.02	4.02	4.02	2	0.12	0.00	0.02	0.00	0.00	22.3
17	300	-1602	114	44	0	89	792	4.02	4.02	4.02	4.02	2	0.11	0.00	0.02	0.00	0.00	22.3
18	300	-100	-58	204	0	176	1034	4.02	4.02	4.02	4.02	3	0.15	0.01	0.03	0.00	0.00	22.3
19	300	-2820	38	208	0	287	1079	4.02	4.02	4.02	4.02	3	0.14	0.01	0.03	0.00	0.00	22.3
20	300	-1339	70	131	0	202	1048	4.02	4.02	4.02	4.02	3	0.14	0.00	0.01	0.00	0.00	22.3
37	300	940	-88	172	0	102	1011	4.02	4.02	4.02	4.02	3	0.15	0.01	0.03	0.00	0.00	22.3
38	300	-3593	73	178	0	288	1085	4.02	4.02	4.02	4.02	3	0.14	0.01	0.03	0.00	0.00	22.3
39	300	-1125	126	50	0	145	1034	4.02	4.02	4.02	4.02	3	0.14	0.00	0.02	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	360	-1037	-398	111	0	53	1028	4.02	4.02	4.02	4.02	3	0.14	0.01	0.07	0.00	0.00	22.3
2	360	-221	-356	95	0	17	785	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
3	360	-637	-288	70	0	28	784	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
4	360	-958	-324	101	0	53	799	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
5	360	-1374	-257	76	0	64	798	4.02	4.02	4.02	4.02	2	0.12	0.01	0.04	0.00	0.00	22.3
6	360	6	-423	127	0	18	791	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
7	360	-1380	-199	42	0	52	787	4.02	4.02	4.02	4.02	2	0.11	0.01	0.03	0.00	0.00	22.3
8	360	-215	-414	129	0	29	796	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
9	360	-1602	-190	44	0	63	792	4.02	4.02	4.02	4.02	2	0.11	0.01	0.03	0.00	0.00	22.3
10	360	-221	-356	95	0	17	785	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
11	360	-637	-288	70	0	28	784	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
12	360	-958	-324	101	0	53	799	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
13	360	-1374	-257	76	0	64	798	4.02	4.02	4.02	4.02	2	0.12	0.01	0.04	0.00	0.00	22.3
14	360	6	-423	127	0	18	791	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
15	360	-1380	-199	42	0	52	787	4.02	4.02	4.02	4.02	2	0.11	0.01	0.03	0.00	0.00	22.3
16	360	-215	-414	129	0	29	796	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
17	360	-1602	-190	44	0	63	792	4.02	4.02	4.02	4.02	2	0.11	0.01	0.03	0.00	0.00	22.3
18	360	-100	-453	204	0	54	1034	4.02	4.02	4.02	4.02	3	0.15	0.01	0.08	0.00	0.00	22.3
19	360	-2820	-357	208	0	163	1079	4.02	4.02	4.02	4.02	3	0.14	0.01	0.06	0.00	0.00	22.3
20	360	-1339	-325	131	0	123	1048	4.02	4.02	4.02	4.02	3	0.14	0.01	0.06	0.00	0.00	22.3
37	360	940	-483	172	0	-1	1011	4.02	4.02	4.02	4.02	3	0.15	0.01	0.09	0.00	0.00	22.3
38	360	-3593	-322	178	0	181	1085	4.02	4.02	4.02	4.02	3	0.14	0.01	0.05	0.00	0.00	22.3
39	360	-1125	-270	50	0	115	1034	4.02	4.02	4.02	4.02	3	0.14	0.01	0.05	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	420	-1037	-794	111	0	-14	952	4.02	4.02	4.02	4.02	3	0.13	0.02	0.14	0.00	0.00	22.3
2	420	-221	-660	95	0	-40	692	4.02	4.02	4.02	4.02	2	0.10	0.02	0.12	0.00	0.00	22.3

3	420	-637	-592	70	0	-14	737	4.02	4.02	4.02	4.02	2	0.11	0.02	0.10	0.00	0.00	22.3
4	420	-958	-628	101	0	-7	727	4.02	4.02	4.02	4.02	2	0.11	0.02	0.11	0.00	0.00	22.3
5	420	-1374	-561	76	0	18	773	4.02	4.02	4.02	4.02	2	0.11	0.02	0.10	0.00	0.00	22.3
6	420	6	-727	127	0	-59	652	4.02	4.02	4.02	4.02	2	0.10	0.02	0.13	0.00	0.00	22.3
7	420	-1380	-503	42	0	27	787	4.02	4.02	4.02	4.02	2	0.11	0.01	0.09	0.00	0.00	22.3
8	420	-215	-718	129	0	-49	663	4.02	4.02	4.02	4.02	2	0.10	0.02	0.13	0.00	0.00	22.3
9	420	-1602	-494	44	0	37	792	4.02	4.02	4.02	4.02	2	0.11	0.01	0.08	0.00	0.00	22.3
10	420	-221	-660	95	0	-40	692	4.02	4.02	4.02	4.02	2	0.10	0.02	0.12	0.00	0.00	22.3
11	420	-637	-592	70	0	-14	737	4.02	4.02	4.02	4.02	2	0.11	0.02	0.10	0.00	0.00	22.3
12	420	-958	-628	101	0	-7	727	4.02	4.02	4.02	4.02	2	0.11	0.02	0.11	0.00	0.00	22.3
13	420	-1374	-561	76	0	18	773	4.02	4.02	4.02	4.02	2	0.11	0.02	0.10	0.00	0.00	22.3
14	420	6	-727	127	0	-59	652	4.02	4.02	4.02	4.02	2	0.10	0.02	0.13	0.00	0.00	22.3
15	420	-1380	-503	42	0	27	787	4.02	4.02	4.02	4.02	2	0.11	0.01	0.09	0.00	0.00	22.3
16	420	-215	-718	129	0	-49	663	4.02	4.02	4.02	4.02	2	0.10	0.02	0.13	0.00	0.00	22.3
17	420	-1602	-494	44	0	37	792	4.02	4.02	4.02	4.02	2	0.11	0.01	0.08	0.00	0.00	22.3
18	420	-100	-849	204	0	-69	920	4.02	4.02	4.02	4.02	3	0.13	0.02	0.15	0.00	0.00	22.3
19	420	-2820	-752	208	0	38	1031	4.02	4.02	4.02	4.02	3	0.14	0.02	0.13	0.00	0.00	22.3
20	420	-1339	-721	131	0	45	1023	4.02	4.02	4.02	4.02	3	0.14	0.02	0.12	0.00	0.00	22.3
37	420	940	-878	172	0	-104	876	4.02	4.02	4.02	4.02	3	0.13	0.03	0.16	0.00	0.00	22.3
38	420	-3593	-718	178	0	74	1061	4.02	4.02	4.02	4.02	3	0.14	0.02	0.12	0.00	0.00	22.3
39	420	-1125	-665	50	0	86	1034	4.02	4.02	4.02	4.02	3	0.14	0.02	0.12	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	480	-1037	-1189	111	0	-81	-647	4.02	4.02	4.02	4.02	3	0.09	0.03	0.21	0.00	0.00	22.3
2	480	-221	-965	95	0	-97	-617	4.02	4.02	4.02	4.02	2	0.09	0.03	0.17	0.00	0.00	22.3
3	480	-637	-897	70	0	-56	-464	4.02	4.02	4.02	4.02	2	0.07	0.03	0.16	0.00	0.00	22.3
4	480	-958	-933	101	0	-68	-531	4.02	4.02	4.02	4.02	2	0.08	0.03	0.16	0.00	0.00	22.3
5	480	-1374	-866	76	0	-27	499	4.02	4.02	4.02	4.02	2	0.07	0.02	0.15	0.00	0.00	22.3
6	480	6	-1032	127	0	-135	-766	4.02	4.02	4.02	4.02	2	0.12	0.03	0.18	0.00	0.00	22.3
7	480	-1380	-808	42	0	2	563	4.02	4.02	4.02	4.02	2	0.08	0.02	0.14	0.00	0.00	22.3
8	480	-215	-1023	129	0	-126	-741	4.02	4.02	4.02	4.02	2	0.11	0.03	0.18	0.00	0.00	22.3
9	480	-1602	-799	44	0	11	580	4.02	4.02	4.02	4.02	2	0.08	0.02	0.14	0.00	0.00	22.3
10	480	-221	-965	95	0	-97	-617	4.02	4.02	4.02	4.02	2	0.09	0.03	0.17	0.00	0.00	22.3
11	480	-637	-897	70	0	-56	-464	4.02	4.02	4.02	4.02	2	0.07	0.03	0.16	0.00	0.00	22.3
12	480	-958	-933	101	0	-68	-531	4.02	4.02	4.02	4.02	2	0.08	0.03	0.16	0.00	0.00	22.3
13	480	-1374	-866	76	0	-27	499	4.02	4.02	4.02	4.02	2	0.07	0.02	0.15	0.00	0.00	22.3
14	480	6	-1032	127	0	-135	-766	4.02	4.02	4.02	4.02	2	0.12	0.03	0.18	0.00	0.00	22.3
15	480	-1380	-808	42	0	2	563	4.02	4.02	4.02	4.02	2	0.08	0.02	0.14	0.00	0.00	22.3
16	480	-215	-1023	129	0	-126	-741	4.02	4.02	4.02	4.02	2	0.11	0.03	0.18	0.00	0.00	22.3
17	480	-1602	-799	44	0	11	580	4.02	4.02	4.02	4.02	2	0.08	0.02	0.14	0.00	0.00	22.3
18	480	-100	-1244	204	0	-191	-767	4.02	4.02	4.02	4.02	3	0.11	0.04	0.22	0.00	0.00	22.3
19	480	-2820	-1148	208	0	-87	661	4.02	4.02	4.02	4.02	3	0.09	0.03	0.19	0.00	0.00	22.3
20	480	-1339	-1116	131	0	-34	671	4.02	4.02	4.02	4.02	3	0.09	0.03	0.19	0.00	0.00	22.3
37	480	940	-1274	172	0	-207	-860	4.02	4.02	4.02	4.02	3	0.13	0.04	0.23	0.00	0.00	22.3
38	480	-3593	-1113	178	0	-33	712	4.02	4.02	4.02	4.02	3	0.09	0.03	0.18	0.00	0.00	22.3
39	480	-1125	-1061	50	0	56	730	4.02	4.02	4.02	4.02	3	0.10	0.03	0.18	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	540	-1037	-1585	111	0	-148	-1680	4.02	4.02	4.02	4.02	3	0.23	0.05	0.28	0.00	0.00	22.3
2	540	-221	-1269	95	0	-155	-1441	4.02	4.02	4.02	4.02	2	0.22	0.04	0.22	0.00	0.00	22.3
3	540	-637	-1201	70	0	-98	-1247	4.02	4.02	4.02	4.02	2	0.19	0.03	0.21	0.00	0.00	22.3
4	540	-958	-1237	101	0	-129	-1336	4.02	4.02	4.02	4.02	2	0.20	0.04	0.22	0.00	0.00	22.3
5	540	-1374	-1170	76	0	-72	-1142	4.02	4.02	4.02	4.02	2	0.17	0.03	0.20	0.00	0.00	22.3
6	540	6	-1336	127	0	-212	-1631	4.02	4.02	4.02	4.02	2	0.25	0.04	0.24	0.00	0.00	22.3
7	540	-1380	-1112	42	0	-23	-984	4.02	4.02	4.02	4.02	2	0.14	0.03	0.19	0.00	0.00	22.3
8	540	-215	-1327	129	0	-204	-1600	4.02	4.02	4.02	4.02	2	0.24	0.04	0.24	0.00	0.00	22.3
9	540	-1602	-1103	44	0	-15	-952	4.02	4.02	4.02	4.02	2	0.14	0.03	0.19	0.00	0.00	22.3
10	540	-221	-1269	95	0	-155	-1441	4.02	4.02	4.02	4.02	2	0.22	0.04	0.22	0.00	0.00	22.3
11	540	-637	-1201	70	0	-98	-1247	4.02	4.02	4.02	4.02	2	0.19	0.03	0.21	0.00	0.00	22.3
12	540	-958	-1237	101	0	-129	-1336	4.02	4.02	4.02	4.02	2	0.20	0.04	0.22	0.00	0.00	22.3
13	540	-1374	-1170	76	0	-72	-1142	4.02	4.02	4.02	4.02	2	0.17	0.03	0.20	0.00	0.00	22.3
14	540	6	-1336	127	0	-212	-1631	4.02	4.02	4.02	4.02	2	0.25	0.04	0.24	0.00	0.00	22.3
15	540	-1380	-1112	42	0	-23	-984	4.02	4.02	4.02	4.02	2	0.14	0.03	0.19	0.00	0.00	22.3
16	540	-215	-1327	129	0	-204	-1600	4.02	4.02	4.02	4.02	2	0.24	0.04	0.24	0.00	0.00	22.3
17	540	-1602	-1103	44	0	-15	-952	4.02	4.02	4.02	4.02	2	0.14	0.03	0.19	0.00	0.00	22.3
18	540	-100	-1640	204	0	-313	-1833	4.02	4.02	4.02	4.02	3	0.26	0.05	0.29	0.00	0.00	22.3
19	540	-2820	-1543	208	0	-212	-1509	4.02	4.02	4.02	4.02	3	0.20	0.04	0.26	0.00	0.00	22.3
20	540	-1339	-1512	131	0	-112	-1447	4.02	4.02	4.02	4.02	3	0.20	0.04	0.26	0.00	0.00	22.3
37	540	940	-1669	172	0	-310	-1943	4.02	4.02	4.02	4.02	3	0.29	0.05	0.30	0.00	0.00	22.3
38	540	-3593	-1509	178	0	-140	-1402	4.02	4.02	4.02	4.02	3	0.18	0.04	0.25	0.00	0.00	22.3
39	540	-1125	-1456	50	0	26	-1300	4.02	4.02	4.02	4.02	3	0.18	0.04	0.25	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	600	-1037	-1980	111	0	-214	-1947	4.02	4.02	4.02	4.02	3	0.27	0.06	0.34	0.00	0.00	22.3
2	600	-221	-1573	95	0	-212	-1651	4.02	4.02	4.02	4.02	2	0.25	0.05	0.28	0.00	0.00	22.3
3	600	-637	-1505	70	0	-140	-1451	4.02	4.02	4.02	4.02	2	0.22	0.04	0.26	0.00	0.00	22.3
4	600	-958	-1541	101	0	-190	-1544	4.02	4.02	4.02	4.02	2	0.23	0.04	0.27	0.00	0.00	22.3
5	600	-1374	-1474	76	0	-118	-1343	4.02	4.02	4.02	4.02	2	0.20	0.04	0.25	0.00	0.00	22.3
6	600	6	-1640	127	0	-288	-1847	4.02	4.02	4.02	4.02	2	0.28	0.05	0.29	0.00	0.00	22.3
7	600	-1380	-1416	42	0	-48	-1180	4.02	4.02	4.02	4.02	2	0.17	0.04	0.24	0.00	0.00	22.3
8	600	-215	-1631	129	0	-281	-1815	4.02	4.02	4.02	4.02	2	0.27	0.05	0.29	0.00	0.00	22.3
9	600	-1602	-1407	44	0	-42	-1147	4.02	4.02	4.02	4.02	2	0.17	0.04	0.24	0.00	0.00	22.3
10	600	-221	-1573	95	0	-212	-1651	4.02	4.02	4.02	4.02	2	0.25	0.05	0.28	0.00	0.00	22.3
11	600	-637	-1505	70	0	-140	-1451	4.02	4.02	4.02	4.02	2	0.22	0.04	0.26	0.00	0.00	22.3
12	600	-958	-1541	101	0	-190	-1544	4.02	4.02	4.02	4.02	2	0.23	0.04	0.27	0.00	0.00	22.3
13	600	-1374	-1474	76	0	-118	-1343	4.02	4.02	4.02	4.02	2	0.20	0.04	0.25	0.00	0.00	22.3
14	600	6	-1640	127	0	-288	-1847	4.02	4.02	4.02	4.02	2	0.28	0.05	0.29	0.00	0.00	22.3
15	600	-1380	-1416	42	0	-48	-1180	4.02	4.02	4.02	4.02	2	0.17	0.04	0.24	0.00	0.00	22.3
16	600	-215	-1631	129	0	-281	-1815	4.02	4.02	4.02	4.02	2	0.27	0.05	0.29	0.00	0.00	22.3
17	600	-1602	-1407	44	0	-42	-1147	4.02	4.02	4.02	4.02	2	0.17	0.04	0.24	0.00	0.00	22.3
18	600	-100	-2035	204	0	-436	-2105	4.02	4.02	4.02	4.02	3	0.30	0.06	0.36	0.00	0.00	22.3
19	600	-2820	-1939	208	0	-337	-1772	4.02	4.02	4.02	4.02	3	0.23	0.06	0.32	0.00	0.00	22.3
20	600	-1339	-1907	131	0	-190	-1708	4.02	4.02	4.02	4.02	3	0.24	0.06	0.33	0.00	0.00	22.3
37	600	940	-2065	172	0	-413	-2218	4.02	4.02	4.02	4.02	3	0.33	0.06	0.37	0.00	0.00	22.3
38	600	-3593	-1904	178	0	-248	-1662	4.02	4.02	4.02	4.02	3	0.22	0.05	0.31	0.00	0.00	22.3
39	600	-1125	-1852	50	0	-4	-1555	4.02	4.02	4.02	4.02	3	0.22	0.05	0.32	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

Nome travata: **Trave_403_IP1** Descrizione: **Trave_4 7-6-5-4-3-2-1**
ASTA NUM. 13 NI 252 NF 253 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y Permanente qy tot.
qy medio: 375.00 132.00 507.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-283	2048	420	0	1404	-2103	4.02	4.02	4.02	4.02	3	0.34	0.06	0.36	0.00	0.00	22.3
2	0	154	1517	282	0	941	-1448	4.02	4.02	4.02	4.02	2	0.26	0.04	0.27	0.00	0.00	22.3
3	0	-163	1590	256	0	867	-1660	4.02	4.02	4.02	4.02	2	0.25	0.05	0.28	0.00	0.00	22.3
4	0	-272	1561	390	0	1293	-1575	4.02	4.02	4.02	4.02	2	0.35	0.05	0.28	0.00	0.00	22.3
5	0	-590	1633	364	0	1219	-1787	4.02	4.02	4.02	4.02	2	0.33	0.05	0.29	0.00	0.00	22.3
6	0	376	1447	350	0	1149	-1246	4.02	4.02	4.02	4.02	2	0.32	0.04	0.26	0.00	0.00	22.3
7	0	-683	1690	264	0	905	-1951	4.02	4.02	4.02	4.02	2	0.29	0.05	0.30	0.00	0.00	22.3
8	0	247	1460	382	0	1255	-1284	4.02	4.02	4.02	4.02	2	0.35	0.04	0.26	0.00	0.00	22.3
9	0	-811	1703	296	0	1010	-1989	4.02	4.02	4.02	4.02	2	0.29	0.05	0.30	0.00	0.00	22.3
10	0	154	1517	282	0	941	-1448	4.02	4.02	4.02	4.02	2	0.26	0.04	0.27	0.00	0.00	22.3
11	0	-163	1590	256	0	867	-1660	4.02	4.02	4.02	4.02	2	0.25	0.05	0.28	0.00	0.00	22.3
12	0	-272	1561	390	0	1293	-1575	4.02	4.02	4.02	4.02	2	0.35	0.05	0.28	0.00	0.00	22.3
13	0	-590	1633	364	0	1219	-1787	4.02	4.02	4.02	4.02	2	0.33	0.05	0.29	0.00	0.00	22.3
14	0	376	1447	350	0	1149	-1246	4.02	4.02	4.02	4.02	2	0.32	0.04	0.26	0.00	0.00	22.3
15	0	-683	1690	264	0	905	-1951	4.02	4.02	4.02	4.02	2	0.29	0.05	0.30	0.00	0.00	22.3
16	0	247	1460	382	0	1255	-1284	4.02	4.02	4.02	4.02	2	0.35	0.04	0.26	0.00	0.00	22.3
17	0	-811	1703	296	0	1010	-1989	4.02	4.02	4.02	4.02	2	0.29	0.05	0.30	0.00	0.00	22.3
18	0	1374	2153	664	0	2270	-2214	4.02	4.02	4.02	4.02	3	0.58	0.06	0.38	0.00	0.00	22.3
19	0	-922	2178	943	0	3166	-2409	4.02	4.02	4.02	4.02	3	0.76	0.06	0.38	0.00	0.00	22.3
20	0	248	2251	677	0	2327	-2562	4.02	4.02	4.02	4.02	3	0.58	0.07	0.40	0.00	0.00	22.3
37	0	1969	2106	446	0	1545	-2080	4.02	4.02	4.02	4.02	3	0.40	0.06	0.38	0.00	0.00	22.3
38	0	-1859	2148	912	0	3038	-2406	4.02	4.02	4.02	4.02	3	0.71	0.06	0.37	0.00	0.00	22.3
39	0	92	2270	468	0	1641	-2661	4.02	4.02	4.02	4.02	3	0.40	0.07	0.40	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	60	-283	1652	420	0	1152	-1830	4.02	4.02	4.02	4.02	3	0.28	0.05	0.29	0.00	0.00	22.3
2	60	154	1213	282	0	772	-1243	4.02	4.02	4.02	4.02	2	0.21	0.04	0.22	0.00	0.00	22.3
3	60	-163	1286	256	0	714	-1448	4.02	4.02	4.02	4.02	2	0.22	0.04	0.23	0.00	0.00	22.3
4	60	-272	1257	390	0	1059	-1366	4.02	4.02	4.02	4.02	2	0.29	0.04	0.22	0.00	0.00	22.3
5	60	-590	1329	364	0	1001	-1571	4.02	4.02	4.02	4.02	2	0.27	0.04	0.23	0.00	0.00	22.3
6	60	376	1143	350	0	939	-1047	4.02	4.02	4.02	4.02	2	0.26	0.03	0.20	0.00	0.00	22.3
7	60	-683	1386	264	0	747	-1730	4.02	4.02	4.02	4.02	2	0.26	0.04	0.24	0.00	0.00	22.3
8	60	247	1156	382	0	1026	-1084	4.02	4.02	4.02	4.02	2	0.29	0.03	0.21	0.00	0.00	22.3
9	60	-811	1399	296	0	832	-1767	4.02	4.02	4.02	4.02	2	0.26	0.04	0.24	0.00	0.00	22.3
10	60	154	1213	282	0	772	-1243	4.02	4.02	4.02	4.02	2	0.21	0.04	0.22	0.00	0.00	22.3
11	60	-163	1286	256	0	714	-1448	4.02	4.02	4.02	4.02	2	0.22	0.04	0.23	0.00	0.00	22.3
12	60	-272	1257	390	0	1059	-1366	4.02	4.02	4.02	4.02	2	0.29	0.04	0.22	0.00	0.00	22.3
13	60	-590	1329	364	0	1001	-1571	4.02	4.02	4.02	4.02	2	0.27	0.04	0.23	0.00	0.00	22.3
14	60	376	1143	350	0	939	-1047	4.02	4.02	4.02	4.02	2	0.26	0.03	0.20	0.00	0.00	22.3
15	60	-683	1386	264	0	747	-1730	4.02	4.02	4.02	4.02	2	0.26	0.04	0.24	0.00	0.00	22.3
16	60	247	1156	382	0	1026	-1084	4.02	4.02	4.02	4.02	2	0.29	0.03	0.21	0.00	0.00	22.3
17	60	-811	1399	296	0	832	-1767	4.02	4.02	4.02	4.02	2	0.26	0.04	0.24	0.00	0.00	22.3
18	60	1374	1758	664	0	1872	-1930	4.02	4.02	4.02	4.02	3	0.48	0.05	0.31	0.00	0.00	22.3
19	60	-922	1783	943	0	2600	-2123	4.02	4.02	4.02	4.02	3	0.62	0.05	0.31	0.00	0.00	22.3
20	60	248	1856	677	0	1921	-2269	4.02	4.02	4.02	4.02	3	0.48	0.05	0.33	0.00	0.00	22.3
37	60	1969	1710	446	0	1277	-1801	4.02	4.02	4.02	4.02	3	0.33	0.05	0.30	0.00	0.00	22.3
38	60	-1859	1753	912	0	2491	-2123	4.02	4.02	4.02	4.02	3	0.58	0.05	0.30	0.00	0.00	22.3
39	60	92	1874	468	0	1360	-2367	4.02	4.02	4.02	4.02	3	0.34	0.05	0.33	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	120	-283	1257	420	0	901	-757	4.02	4.02	4.02	4.02	3	0.22	0.04	0.22	0.00	0.00	22.3
2	120	154	909	282	0	603	467	4.02	4.02	4.02	4.02	2	0.17	0.03	0.16	0.00	0.00	22.3
3	120	-163	982	256	0	560	-615	4.02	4.02	4.02	4.02	2	0.15	0.03	0.17	0.00	0.00	22.3
4	120	-272	953	390	0	825	-549	4.02	4.02	4.02	4.02	2	0.23	0.03	0.17	0.00	0.00	22.3
5	120	-590	1025	364	0	782	-711	4.02	4.02	4.02	4.02	2	0.21	0.03	0.18	0.00	0.00	22.3
6	120	376	839	350	0	730	550	4.02	4.02	4.02	4.02	2	0.20	0.02	0.15	0.00	0.00	22.3
7	120	-683	1082	264	0	589	-836	4.02	4.02	4.02	4.02	2	0.16	0.03	0.19	0.00	0.00	22.3
8	120	247	852	382	0	797	535	4.02	4.02	4.02	4.02	2	0.22	0.02	0.15	0.00	0.00	22.3
9	120	-811	1095	296	0	655	-865	4.02	4.02	4.02	4.02	2	0.18	0.03	0.19	0.00	0.00	22.3
10	120	154	909	282	0	603	467	4.02	4.02	4.02	4.02	2	0.17	0.03	0.16	0.00	0.00	22.3
11	120	-163	982	256	0	560	-615	4.02	4.02	4.02	4.02	2	0.15	0.03	0.17	0.00	0.00	22.3
12	120	-272	953	390	0	825	-549	4.02	4.02	4.02	4.02	2	0.23	0.03	0.17	0.00	0.00	22.3
13	120	-590	1025	364	0	782	-711	4.02	4.02	4.02	4.02	2	0.21	0.03	0.18	0.00	0.00	22.3
14	120	376	839	350	0	730	550	4.02	4.02	4.02	4.02	2	0.20	0.02	0.15	0.00	0.00	22.3
15	120	-683	1082	264	0	589	-836	4.02	4.02	4.02	4.02	2	0.16	0.03	0.19	0.00	0.00	22.3
16	120	247	852	382	0	797	535	4.02	4.02	4.02	4.02	2	0.22	0.02	0.15	0.00	0.00	22.3
17	120	-811	1095	296	0	655	-865	4.02	4.02	4.02	4.02	2	0.18	0.03	0.19	0.00	0.00	22.3
18	120	1374	1362	664	0	1473	-794	4.02	4.02	4.02	4.02	3	0.38	0.04	0.24	0.00	0.00	22.3
19	120	-922	1387	943	0	2034	-972	4.02	4.02	4.02	4.02	3	0.49	0.04	0.24	0.00	0.00	22.3
20	120	248	1460	677	0	1515	-1074	4.02	4.02	4.02	4.02	3	0.37	0.04	0.26	0.00	0.00	22.3
37	120	1969	1315	446	0	1009	-693	4.02	4.02	4.02	4.02	3	0.26	0.04	0.23	0.00	0.00	22.3
38	120	-1859	1357	912	0	1943	-990	4.02	4.02	4.02	4.02	3	0.46	0.04	0.23	0.00	0.00	22.3
39	120	92	1479	468	0	1080	-1160	4.02	4.02	4.02	4.02	3	0.27	0.04	0.26	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	180	-283	862	420	0	649	951	4.02	4.02	4.02	4.02	3	0.16	0.02	0.15	0.00	0.00	22.3
2	180	154	604	282	0	434	767	4.02	4.02	4.02	4.02	2	0.12	0.02	0.11	0.00	0.00	22.3
3	180	-163	677	256	0	407	723	4.02	4.02	4.02	4.02	2	0.11	0.02	0.12	0.00	0.00	22.3
4	180	-272	648	390	0	591	741	4.02	4.02	4.02	4.02	2	0.16	0.02	0.11	0.00	0.00	22.3
5	180	-590	720	364	0	564	697	4.02	4.02	4.02	4.02	2	0.15	0.02	0.13	0.00	0.00	22.3
6	180	376	534	350	0	520	808	4.02	4.02	4.02	4.02	2	0.15	0.02	0.10	0.00	0.00	22.3
7	180	-683	777	264	0	431	663	4.02	4.02	4.02	4.02	2	0.12	0.02	0.14	0.00	0.00	22.3
8	180	247	547	382	0	567	801	4.02	4.02	4.02	4.02	2	0.16	0.02	0.10	0.00	0.00	22.3
9	180	-811	790	296	0	477	655	4.02	4.02	4.02	4.02	2	0.13	0.02	0.14	0.00	0.00	22.3
10	180	154	604	282	0	434	767	4.02	4.02	4.02	4.02	2	0.12	0.02	0.11	0.00	0.00	22.3
11	180	-163	677	256	0	407	723	4.02	4.02	4.02	4.02	2	0.11	0.02	0.12	0.00	0.00	22.3
12	180	-272	648	390	0	591	741	4.02	4.02	4.02	4.02	2	0.16	0.02	0.11	0.00	0.00	22.3
13	180	-590	720	364	0	564	697	4.02	4.02	4.02	4.02	2	0.15	0.02	0.13	0.00	0.00	22.3
14	180	376	534	350	0	520	808	4.02	4.02	4.02	4.02	2	0.15	0.02	0.10	0.00	0.00	22.3
15	180	-683	777	264	0	431	663	4.02	4.02	4.02	4.02	2	0.12	0.02	0.14	0.00	0.00	22.3
16	180	247	547	382	0	567	801	4.02	4.02	4.02	4.02	2	0.16	0.02	0.10	0.00	0.00	22.3
17	180	-811	790	296	0	477	655	4.02	4.02	4.02	4.02	2	0.13	0.02	0.14	0.00	0.00	22.3
18	180	1374	967	664	0	1075	1084	4.02	4.02	4.02	4.02	3	0.27	0.03	0.17	0.00	0.00	22.3
19	180	-922	992	943	0	1468	946	4.02	4.02	4.02	4.02	3	0.35	0.03	0.17	0.00	0.00	22.3
20	180	248	1065	677	0	1109	962	4.02	4.02	4.02	4.02	3	0.27	0.03	0.19	0.00	0.00	22.3
37	180	1969	920	446	0	742	1109	4.02	4.02	4.02	4.02	3	0.19	0.03	0.16	0.00	0.00	22.3
38	180	-1859	962	912	0	1396	880	4.02	4.02	4.02	4.02	3	0.33	0.03	0.16	0.00	0.00	22.3
39	180	92	1084	468	0	799	906	4.02	4.02	4.02	4.02	3	0.20	0.03	0.19	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	240	-283	466	420	0	397	1074	4.02	4.02	4.02	4.02	3	0.15	0.01	0.08	0.00	0.00	22.3
2	240	154	300	282	0	265	821	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
3	240	-163	373	256	0	254	827	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
4	240	-272	344	390	0	357	826	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
5	240	-590	416	364	0	346	832	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
6	240	376	230	350	0	310	815	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
7	240	-683	473	264	0	272	847	4.02	4.02	4.02	4.02	2	0.13	0.01	0.08	0.00	0.00	22.3
8	240	247	243	382	0	338	816	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
9	240	-811	486	296	0	300	856	4.02	4.02	4.02	4.02	2	0.13	0.01	0.08	0.00	0.00	22.3
10	240	154	300	282	0	265	821	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
11	240	-163	373	256	0	254	827	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
12	240	-272	344	390	0	357	826	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
13	240	-590	416	364	0	346	832	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
14	240	376	230	350	0	310	815	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
15	240	-683	473	264	0	272	847	4.02	4.02	4.02	4.02	2	0.13	0.01	0.08	0.00	0.00	22.3
16	240	247	243	382	0	338	816	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
17	240	-811	486	296	0	300	856	4.02	4.02	4.02	4.02	2	0.13	0.01	0.08	0.00	0.00	22.3
18	240	1374	571	664	0	677	1280	4.02	4.02	4.02	4.02	3	0.19	0.02	0.11	0.00	0.00	22.3
19	240	-922	596	943	0	902	1162	4.02	4.02	4.02	4.02	3	0.22	0.03	0.15	0.00	0.00	22.3
20	240	248	669	677	0	703	1272	4.02	4.02	4.02	4.02	3	0.18	0.02	0.12	0.00	0.00	22.3
37	240	1969	524	446	0	474	1272	4.02	4.02	4.02	4.02	3	0.19	0.02	0.09	0.00	0.00	22.3
38	240	-1859	566	912	0	849	1072	4.02	4.02	4.02	4.02	3	0.20	0.03	0.14	0.00	0.00	22.3
39	240	92	688	468	0	518	1237	4.02	4.02	4.02	4.02	3	0.18	0.02	0.12	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	300	-283	70	420	0	146	1074	4.02	4.02	4.02	4.02	3	0.15	0.01	0.07	0.00	0.00	22.3
2	300	154	-4	282	0	96	821	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
3	300	-163	69	256	0	100	827	4.02	4.02	4.02	4.02	2	0.12	0.01	0.04	0.00	0.00	22.3
4	300	-272	40	390	0	123	826	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
5	300	-590	112	364	0	127	832	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
6	300	376	-74	350	0	101	815	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
7	300	-683	169	264	0	114	847	4.02	4.02	4.02	4.02	2	0.13	0.01	0.04	0.00	0.00	22.3
8	300	247	-61	382	0	109	816	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
9	300	-811	182	296	0	122	856	4.02	4.02	4.02	4.02	2	0.13	0.01	0.05	0.00	0.00	22.3
10	300	154	-4	282	0	96	821	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
11	300	-163	69	256	0	100	827	4.02	4.02	4.02	4.02	2	0.12	0.01	0.04	0.00	0.00	22.3
12	300	-272	40	390	0	123	826	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
13	300	-590	112	364	0	127	832	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
14	300	376	-74	350	0	101	815	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
15	300	-683	169	264	0	114	847	4.02	4.02	4.02	4.02	2	0.13	0.01	0.04	0.00	0.00	22.3
16	300	247	-61	382	0	109	816	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
17	300	-811	182	296	0	122	856	4.02	4.02	4.02	4.02	2	0.13	0.01	0.05	0.00	0.00	22.3
18	300	1374	176	664	0	278	1280	4.02	4.02	4.02	4.02	3	0.19	0.02	0.11	0.00	0.00	22.3
19	300	-922	201	943	0	335	1162	4.02	4.02	4.02	4.02	3	0.16	0.03	0.15	0.00	0.00	22.3
20	300	248	274	677	0	297	1272	4.02	4.02	4.02	4.02	3	0.18	0.02	0.11	0.00	0.00	22.3
37	300	1969	128	446	0	206	1272	4.02	4.02	4.02	4.02	3	0.19	0.01	0.07	0.00	0.00	22.3
38	300	-1859	171	912	0	302	1072	4.02	4.02	4.02	4.02	3	0.15	0.03	0.14	0.00	0.00	22.3
39	300	92	292	468	0	237	1240	4.02	4.02	4.02	4.02	3	0.18	0.01	0.08	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	360	-283	-325	420	0	-106	1074	4.02	4.02	4.02	4.02	3	0.15	0.01	0.07	0.00	0.00	22.3
2	360	154	-308	282	0	-73	821	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
3	360	-163	-235	256	0	-53	827	4.02	4.02	4.02	4.02	2	0.12	0.01	0.04	0.00	0.00	22.3
4	360	-272	-264	390	0	-110	826	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
5	360	-590	-192	364	0	-91	832	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
6	360	376	-378	350	0	-109	815	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
7	360	-683	-135	264	0	-44	847	4.02	4.02	4.02	4.02	2	0.13	0.01	0.04	0.00	0.00	22.3
8	360	247	-365	382	0	-120	816	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
9	360	-811	-122	296	0	-55	856	4.02	4.02	4.02	4.02	2	0.13	0.01	0.05	0.00	0.00	22.3
10	360	154	-308	282	0	-73	821	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
11	360	-163	-235	256	0	-53	827	4.02	4.02	4.02	4.02	2	0.12	0.01	0.04	0.00	0.00	22.3
12	360	-272	-264	390	0	-110	826	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
13	360	-590	-192	364	0	-91	832	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
14	360	376	-378	350	0	-109	815	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
15	360	-683	-135	264	0	-44	847	4.02	4.02	4.02	4.02	2	0.13	0.01	0.04	0.00	0.00	22.3
16	360	247	-365	382	0	-120	816	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
17	360	-811	-122	296	0	-55	856	4.02	4.02	4.02	4.02	2	0.13	0.01	0.05	0.00	0.00	22.3
18	360	1374	-219	664	0	-120	1280	4.02	4.02	4.02	4.02	3	0.19	0.02	0.11	0.00	0.00	22.3
19	360	-922	-194	943	0	-231	1162	4.02	4.02	4.02	4.02	3	0.16	0.03	0.15	0.00	0.00	22.3
20	360	248	-121	677	0	-109	1272	4.02	4.02	4.02	4.02	3	0.18	0.02	0.11	0.00	0.00	22.3
37	360	1969	-267	446	0	-62	1272	4.02	4.02	4.02	4.02	3	0.19	0.01	0.07	0.00	0.00	22.3
38	360	-1859	-224	912	0	-246	1072	4.02	4.02	4.02	4.02	3	0.15	0.03	0.14	0.00	0.00	22.3
39	360	92	-103	468	0	-43	1240	4.02	4.02	4.02	4.02	3	0.18	0.01	0.08	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	420	-283	-720	420	0	-358	1049	4.02	4.02	4.02	4.02	3	0.15	0.02	0.13	0.00	0.00	22.3
2	420	154	-612	282	0	-242	760	4.02	4.02	4.02	4.02	2	0.12	0.02	0.11	0.00	0.00	22.3
3	420	-163	-539	256	0	-207	817	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
4	420	-272	-568	390	0	-344	796	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
5	420	-590	-496	364	0	-309	832	4.02	4.02	4.02	4.02	2	0.12	0.01	0.09	0.00	0.00	22.3
6	420	376	-682	350	0	-318	707	4.02	4.02	4.02	4.02	2	0.11	0.02	0.12	0.00	0.00	22.3
7	420	-683	-439	264	0	-202	847	4.02	4.02	4.02	4.02	2	0.13	0.01	0.08	0.00	0.00	22.3
8	420	247	-669	382	0	-349	717	4.02	4.02	4.02	4.02	2	0.11	0.02	0.12	0.00	0.00	22.3
9	420	-811	-426	296	0	-233	856	4.02	4.02	4.02	4.02	2	0.13	0.01	0.07	0.00	0.00	22.3
10	420	154	-612	282	0	-242	760	4.02	4.02	4.02	4.02	2	0.12	0.02	0.11	0.00	0.00	22.3
11	420	-163	-539	256	0	-207	817	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
12	420	-272	-568	390	0	-344	796	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
13	420	-590	-496	364	0	-309	832	4.02	4.02	4.02	4.02	2	0.12	0.01	0.09	0.00	0.00	22.3
14	420	376	-682	350	0	-318	707	4.02	4.02	4.02	4.02	2	0.11	0.02	0.12	0.00	0.00	22.3
15	420	-683	-439	264	0	-202	847	4.02	4.02	4.02	4.02	2	0.13	0.01	0.08	0.00	0.00	22.3
16	420	247	-669	382	0	-349	717	4.02	4.02	4.02	4.02	2	0.11	0.02	0.12	0.00	0.00	22.3
17	420	-811	-426	296	0	-233	856	4.02	4.02	4.02	4.02	2	0.13	0.01	0.07	0.00	0.00	22.3
18	420	1374	-615	664	0	-518	1280	4.02	4.02	4.02	4.02	3	0.19	0.02	0.11	0.00	0.00	22.3
19	420	-922	-590	943	0	-797	1162	4.02	4.02	4.02	4.02	3	0.19	0.03	0.15	0.00	0.00	22.3
20	420	248	-517	677	0	-515	1272	4.02	4.02	4.02	4.02	3	0.18	0.02	0.11	0.00	0.00	22.3
37	420	1969	-662	446	0	-330	1272	4.02	4.02	4.02	4.02	3	0.19	0.02	0.12	0.00	0.00	22.3
38	420	-1859	-620	912	0	-793	1072	4.02	4.02	4.02	4.02	3	0.19	0.03	0.14	0.00	0.00	22.3
39	420	92	-498	468	0	-324	1240	4.02	4.02	4.02	4.02	3	0.18	0.01	0.09	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	480	-283	-1116	420	0	-610	698	4.02	4.02	4.02	4.02	3	0.15	0.03	0.20	0.00	0.00	22.3
2	480	154	-917	282	0	-411	-473	4.02	4.02	4.02	4.02	2	0.11	0.03	0.16	0.00	0.00	22.3
3	480	-163	-844	256	0	-360	556	4.02	4.02	4.02	4.02	2	0.10	0.02	0.15	0.00	0.00	22.3
4	480	-272	-873	390	0	-578	517	4.02	4.02	4.02	4.02	2	0.16	0.03	0.15	0.00	0.00	22.3
5	480	-590	-801	364	0	-528	618	4.02	4.02	4.02	4.02	2	0.14	0.02	0.14	0.00	0.00	22.3
6	480	376	-987	350	0	-528	-639	4.02	4.02	4.02	4.02	2	0.15	0.03	0.18	0.00	0.00	22.3

7	480	-683	-744	264	0	-360	696	4.02	4.02	4.02	4.02	2	0.10	0.02	0.13	0.00	0.00	22.3
8	480	247	-974	382	0	-579	-607	4.02	4.02	4.02	4.02	2	0.16	0.03	0.17	0.00	0.00	22.3
9	480	-811	-731	296	0	-410	714	4.02	4.02	4.02	4.02	2	0.11	0.02	0.13	0.00	0.00	22.3
10	480	154	-917	282	0	-411	-473	4.02	4.02	4.02	4.02	2	0.11	0.03	0.16	0.00	0.00	22.3
11	480	-163	-844	256	0	-360	556	4.02	4.02	4.02	4.02	2	0.10	0.02	0.15	0.00	0.00	22.3
12	480	-272	-873	390	0	-578	517	4.02	4.02	4.02	4.02	2	0.16	0.03	0.15	0.00	0.00	22.3
13	480	-590	-801	364	0	-528	618	4.02	4.02	4.02	4.02	2	0.14	0.02	0.14	0.00	0.00	22.3
14	480	376	-987	350	0	-528	-639	4.02	4.02	4.02	4.02	2	0.15	0.03	0.18	0.00	0.00	22.3
15	480	-683	-744	264	0	-360	696	4.02	4.02	4.02	4.02	2	0.10	0.02	0.13	0.00	0.00	22.3
16	480	247	-974	382	0	-579	-607	4.02	4.02	4.02	4.02	2	0.16	0.03	0.17	0.00	0.00	22.3
17	480	-811	-731	296	0	-410	714	4.02	4.02	4.02	4.02	2	0.11	0.02	0.13	0.00	0.00	22.3
18	480	1374	-1010	664	0	-916	1040	4.02	4.02	4.02	4.02	3	0.23	0.03	0.18	0.00	0.00	22.3
19	480	-922	-985	943	0	-1363	953	4.02	4.02	4.02	4.02	3	0.33	0.03	0.17	0.00	0.00	22.3
20	480	248	-912	677	0	-921	1114	4.02	4.02	4.02	4.02	3	0.23	0.03	0.16	0.00	0.00	22.3
37	480	1969	-1058	446	0	-597	972	4.02	4.02	4.02	4.02	3	0.15	0.03	0.19	0.00	0.00	22.3
38	480	-1859	-1015	912	0	-1340	826	4.02	4.02	4.02	4.02	3	0.31	0.03	0.17	0.00	0.00	22.3
39	480	92	-894	468	0	-605	1094	4.02	4.02	4.02	4.02	3	0.16	0.03	0.16	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	540	-283	-1511	420	0	-861	-1421	4.02	4.02	4.02	4.02	3	0.21	0.04	0.27	0.00	0.00	22.3
2	540	154	-1221	282	0	-579	-1268	4.02	4.02	4.02	4.02	2	0.19	0.04	0.22	0.00	0.00	22.3
3	540	-163	-1148	256	0	-513	-1050	4.02	4.02	4.02	4.02	2	0.16	0.03	0.20	0.00	0.00	22.3
4	540	-272	-1177	390	0	-812	-1135	4.02	4.02	4.02	4.02	2	0.22	0.03	0.21	0.00	0.00	22.3
5	540	-590	-1105	364	0	-746	-917	4.02	4.02	4.02	4.02	2	0.20	0.03	0.19	0.00	0.00	22.3
6	540	376	-1291	350	0	-738	-1476	4.02	4.02	4.02	4.02	2	0.23	0.04	0.23	0.00	0.00	22.3
7	540	-683	-1048	264	0	-518	-749	4.02	4.02	4.02	4.02	2	0.14	0.03	0.18	0.00	0.00	22.3
8	540	247	-1278	382	0	-808	-1436	4.02	4.02	4.02	4.02	2	0.22	0.04	0.23	0.00	0.00	22.3
9	540	-811	-1035	296	0	-588	-709	4.02	4.02	4.02	4.02	2	0.16	0.03	0.18	0.00	0.00	22.3
10	540	154	-1221	282	0	-579	-1268	4.02	4.02	4.02	4.02	2	0.19	0.04	0.22	0.00	0.00	22.3
11	540	-163	-1148	256	0	-513	-1050	4.02	4.02	4.02	4.02	2	0.16	0.03	0.20	0.00	0.00	22.3
12	540	-272	-1177	390	0	-812	-1135	4.02	4.02	4.02	4.02	2	0.22	0.03	0.21	0.00	0.00	22.3
13	540	-590	-1105	364	0	-746	-917	4.02	4.02	4.02	4.02	2	0.20	0.03	0.19	0.00	0.00	22.3
14	540	376	-1291	350	0	-738	-1476	4.02	4.02	4.02	4.02	2	0.23	0.04	0.23	0.00	0.00	22.3
15	540	-683	-1048	264	0	-518	-749	4.02	4.02	4.02	4.02	2	0.14	0.03	0.18	0.00	0.00	22.3
16	540	247	-1278	382	0	-808	-1436	4.02	4.02	4.02	4.02	2	0.22	0.04	0.23	0.00	0.00	22.3
17	540	-811	-1035	296	0	-588	-709	4.02	4.02	4.02	4.02	2	0.16	0.03	0.18	0.00	0.00	22.3
18	540	1374	-1406	664	0	-1315	-907	4.02	4.02	4.02	4.02	3	0.34	0.04	0.25	0.00	0.00	22.3
19	540	-922	-1381	943	0	-1929	-955	4.02	4.02	4.02	4.02	3	0.46	0.04	0.24	0.00	0.00	22.3
20	540	248	-1308	677	0	-1327	-676	4.02	4.02	4.02	4.02	3	0.33	0.04	0.23	0.00	0.00	22.3
37	540	1969	-1453	446	0	-865	-1052	4.02	4.02	4.02	4.02	3	0.22	0.04	0.26	0.00	0.00	22.3
38	540	-1859	-1411	912	0	-1888	-1130	4.02	4.02	4.02	4.02	3	0.44	0.04	0.24	0.00	0.00	22.3
39	540	92	-1289	468	0	-885	-666	4.02	4.02	4.02	4.02	3	0.22	0.04	0.23	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	600	-283	-1907	420	0	-1113	-1681	4.02	4.02	4.02	4.02	3	0.27	0.06	0.34	0.00	0.00	22.3
2	600	154	-1525	282	0	-748	-1474	4.02	4.02	4.02	4.02	2	0.22	0.04	0.27	0.00	0.00	22.3
3	600	-163	-1452	256	0	-667	-1249	4.02	4.02	4.02	4.02	2	0.19	0.04	0.26	0.00	0.00	22.3
4	600	-272	-1481	390	0	-1046	-1337	4.02	4.02	4.02	4.02	2	0.29	0.04	0.26	0.00	0.00	22.3
5	600	-590	-1409	364	0	-964	-1112	4.02	4.02	4.02	4.02	2	0.26	0.04	0.25	0.00	0.00	22.3
6	600	376	-1595	350	0	-947	-1688	4.02	4.02	4.02	4.02	2	0.26	0.05	0.28	0.00	0.00	22.3
7	600	-683	-1352	264	0	-676	-938	4.02	4.02	4.02	4.02	2	0.18	0.04	0.24	0.00	0.00	22.3
8	600	247	-1582	382	0	-1037	-1647	4.02	4.02	4.02	4.02	2	0.29	0.05	0.28	0.00	0.00	22.3
9	600	-811	-1339	296	0	-765	-897	4.02	4.02	4.02	4.02	2	0.21	0.04	0.23	0.00	0.00	22.3
10	600	154	-1525	282	0	-748	-1474	4.02	4.02	4.02	4.02	2	0.22	0.04	0.27	0.00	0.00	22.3
11	600	-163	-1452	256	0	-667	-1249	4.02	4.02	4.02	4.02	2	0.19	0.04	0.26	0.00	0.00	22.3
12	600	-272	-1481	390	0	-1046	-1337	4.02	4.02	4.02	4.02	2	0.29	0.04	0.26	0.00	0.00	22.3
13	600	-590	-1409	364	0	-964	-1112	4.02	4.02	4.02	4.02	2	0.26	0.04	0.25	0.00	0.00	22.3
14	600	376	-1595	350	0	-947	-1688	4.02	4.02	4.02	4.02	2	0.26	0.05	0.28	0.00	0.00	22.3
15	600	-683	-1352	264	0	-676	-938	4.02	4.02	4.02	4.02	2	0.18	0.04	0.24	0.00	0.00	22.3
16	600	247	-1582	382	0	-1037	-1647	4.02	4.02	4.02	4.02	2	0.29	0.05	0.28	0.00	0.00	22.3
17	600	-811	-1339	296	0	-765	-897	4.02	4.02	4.02	4.02	2	0.21	0.04	0.23	0.00	0.00	22.3
18	600	1374	-1801	664	0	-1713	-1158	4.02	4.02	4.02	4.02	3	0.44	0.05	0.32	0.00	0.00	22.3
19	600	-922	-1776	943	0	-2495	-1203	4.02	4.02	4.02	4.02	3	0.60	0.05	0.31	0.00	0.00	22.3
20	600	248	-1703	677	0	-1733	-917	4.02	4.02	4.02	4.02	3	0.43	0.05	0.30	0.00	0.00	22.3
37	600	1969	-1849	446	0	-1133	-1307	4.02	4.02	4.02	4.02	3	0.29	0.05	0.33	0.00	0.00	22.3
38	600	-1859	-1806	912	0	-2435	-1381	4.02	4.02	4.02	4.02	3	0.57	0.05	0.31	0.00	0.00	22.3
39	600	92	-1685	468	0	-1166	-905	4.02	4.02	4.02	4.02	3	0.29	0.05	0.30	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

Nome travata: **Trave_403_IP1** Descrizione: **Trave_4 7-6-5-4-3-2-1**
ASTA NUM. 14 NI 253 NF 291 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y Permanente qy tot.
qy medio: 375.00 132.00 507.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	1321	1923	808	0	2283	-2002	4.02	4.02	4.02	4.02	3	0.58	0.06	0.34	0.00	0.00	22.3
2	0	1134	1416	575	0	1625	-1352	4.02	4.02	4.02	4.02	2	0.47	0.04	0.25	0.00	0.00	22.3
3	0	992	1498	570	0	1617	-1588	4.02	4.02	4.02	4.02	2	0.46	0.04	0.27	0.00	0.00	22.3
4	0	1040	1459	673	0	1895	-1493	4.02	4.02	4.02	4.02	2	0.54	0.04	0.26	0.00	0.00	22.3
5	0	898	1541	668	0	1887	-1729	4.02	4.02	4.02	4.02	2	0.54	0.04	0.27	0.00	0.00	22.3
6	0	1267	1336	615	0	1729	-1126	4.02	4.02	4.02	4.02	2	0.50	0.04	0.24	0.00	0.00	22.3
7	0	793	1609	599	0	1702	-1912	4.02	4.02	4.02	4.02	2	0.48	0.05	0.29	0.00	0.00	22.3
8	0	1239	1349	645	0	1810	-1168	4.02	4.02	4.02	4.02	2	0.52	0.04	0.24	0.00	0.00	22.3
9	0	765	1622	628	0	1783	-1955	4.02	4.02	4.02	4.02	2	0.50	0.05	0.29	0.00	0.00	22.3
10	0	1134	1416	575	0	1625	-1352	4.02	4.02	4.02	4.02	2	0.47	0.04	0.25	0.00	0.00	22.3
11	0	992	1498	570	0	1617	-1588	4.02	4.02	4.02	4.02	2	0.46	0.04	0.27	0.00	0.00	22.3
12	0	1040	1459	673	0	1895	-1493	4.02	4.02	4.02	4.02	2	0.54	0.04	0.26	0.00	0.00	22.3
13	0	898	1541	668	0	1887	-1729	4.02	4.02	4.02	4.02	2	0.54	0.04	0.27	0.00	0.00	22.3
14	0	1267	1336	615	0	1729	-1126	4.02	4.02	4.02	4.02	2	0.50	0.04	0.24	0.00	0.00	22.3
15	0	793	1609	599	0	1702	-1912	4.02	4.02	4.02	4.02	2	0.48	0.05	0.29	0.00	0.00	22.3
16	0	1239	1349	645	0	1810	-1168	4.02	4.02	4.02	4.02	2	0.52	0.04	0.24	0.00	0.00	22.3
17	0	765	1622	628	0	1783	-1955	4.02	4.02	4.02	4.02	2	0.50	0.05	0.29	0.00	0.00	22.3
18	0	6001	1523	1567	0	4356	-1403	6.03	4.02	4.02	4.02	3	0.86	0.05	0.27	0.00	0.00	22.3
19	0	2755	1894	1682	0	4731	-2173	6.03	4.02	4.02	4.02	3	0.87	0.05	0.34	0.00	0.00	22.3
20	0	4382	1834	1507	0	4213	-2123	6.03	4.02	4.02	4.02	3	0.80	0.05	0.33	0.00	0.00	22.3
37	0	6077	1469	1263	0	3496	-1216	6.03	4.02	4.02	4.02	3	0.69	0.04	0.26	0.00	0.00	22.3
38	0	666	2088	1454	0	4120	-2499	6.03	4.02	4.02	4.02	3	0.73	0.06	0.37	0.00	0.00	22.3
39	0	3378	1987	1163	0	3256	-2414	4.02	4.02	4.02	4.02	3	0.88	0.06	0.35	0.00	0.00	22.3

apost= 2.01 aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	60	1321	1528	808	0	1798	-1740	4.02	4.02	4.02	4.02	3	0.46	0.04	0.27	0.00	0.00	22.3
2	60	1134	1112	575	0	1280	-1156	4.02	4.02	4.02	4.02	2	0.37	0.03	0.20	0.00	0.00	22.3
3	60	992	1194	570	0	1275	-1385	4.02	4.02	4.02	4.02	2	0.36	0.03	0.21	0.00	0.00	22.3
4	60	1040	1155	673	0	1491	-1293	4.02	4.02	4.02	4.02	2	0.43	0.03	0.21	0.00	0.00	22.3
5	60	898	1237	668	0	1486	-1522	4.02	4.02	4.02	4.02	2	0.42	0.04	0.22	0.00	0.00	22.3
6	60	1267	1032	615	0	1360	-938	4.02	4.02	4.02	4.02	2	0.39	0.03	0.18	0.00	0.00	22.3
7	60	793	1305	599	0	1343	-1698	4.02	4.02	4.02	4.02	2	0.38	0.04	0.23	0.00	0.00	22.3
8	60	1239	1045	645	0	1423	-979	4.02	4.02	4.02	4.02	2	0.41	0.03	0.19	0.00	0.00	22.3
9	60	765	1318	628	0	1406	-1740	4.02	4.02	4.02	4.02	2	0.40	0.04	0.23	0.00	0.00	22.3
10	60	1134	1112	575	0	1280	-1156	4.02	4.02	4.02	4.02	2	0.37	0.03	0.20	0.00	0.00	22.3
11	60	992	1194	570	0	1275	-1385	4.02	4.02	4.02	4.02	2	0.36	0.03	0.21	0.00	0.00	22.3
12	60	1040	1155	673	0	1491	-1293	4.02	4.02	4.02	4.02	2	0.43	0.03	0.21	0.00	0.00	22.3
13	60	898	1237	668	0	1486	-1522	4.02	4.02	4.02	4.02	2	0.42	0.04	0.22	0.00	0.00	22.3
14	60	1267	1032	615	0	1360	-938	4.02	4.02	4.02	4.02	2	0.39	0.03	0.18	0.00	0.00	22.3
15	60	793	1305	599	0	1343	-1698	4.02	4.02	4.02	4.02	2	0.38	0.04	0.23	0.00	0.00	22.3
16	60	1239	1045	645	0	1423	-979	4.02	4.02	4.02	4.02	2	0.41	0.03	0.19	0.00	0.00	22.3
17	60	765	1318	628	0	1406	-1740	4.02	4.02	4.02	4.02	2	0.40	0.04	0.23	0.00	0.00	22.3
18	60	6001	1128	1567	0	3416	-1179	4.02	4.02	4.02	4.02	3	1.00	0.05	0.25	0.00	0.00	22.3
19	60	2755	1499	1682	0	3722	-1914	4.02	4.02	4.02	4.02	3	0.99	0.05	0.27	0.00	0.00	22.3
20	60	4382	1438	1507	0	3309	-1870	4.02	4.02	4.02	4.02	3	0.92	0.05	0.26	0.00	0.00	22.3
37	60	6077	1074	1263	0	2738	-997	4.02	4.02	4.02	4.02	3	0.80	0.04	0.20	0.00	0.00	22.3
38	60	666	1692	1454	0	3247	-2222	4.02	4.02	4.02	4.02	3	0.81	0.05	0.30	0.00	0.00	22.3
39	60	3378	1592	1163	0	2558	-2146	4.02	4.02	4.02	4.02	3	0.69	0.05	0.28	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	120	1321	1132	808	0	1313	-743	4.02	4.02	4.02	4.02	3	0.33	0.03	0.20	0.00	0.00	22.3
2	120	1134	808	575	0	935	-426	4.02	4.02	4.02	4.02	2	0.27	0.02	0.14	0.00	0.00	22.3
3	120	992	890	570	0	933	-605	4.02	4.02	4.02	4.02	2	0.27	0.03	0.16	0.00	0.00	22.3
4	120	1040	851	673	0	1087	-537	4.02	4.02	4.02	4.02	2	0.31	0.02	0.15	0.00	0.00	22.3
5	120	898	933	668	0	1085	-717	4.02	4.02	4.02	4.02	2	0.31	0.03	0.17	0.00	0.00	22.3
6	120	1267	728	615	0	991	480	4.02	4.02	4.02	4.02	2	0.28	0.02	0.13	0.00	0.00	22.3
7	120	793	1001	599	0	983	-853	4.02	4.02	4.02	4.02	2	0.28	0.03	0.18	0.00	0.00	22.3
8	120	1239	741	645	0	1036	460	4.02	4.02	4.02	4.02	2	0.30	0.02	0.13	0.00	0.00	22.3
9	120	765	1014	628	0	1029	-887	4.02	4.02	4.02	4.02	2	0.29	0.03	0.18	0.00	0.00	22.3
10	120	1134	808	575	0	935	-426	4.02	4.02	4.02	4.02	2	0.27	0.02	0.14	0.00	0.00	22.3
11	120	992	890	570	0	933	-605	4.02	4.02	4.02	4.02	2	0.27	0.03	0.16	0.00	0.00	22.3
12	120	1040	851	673	0	1087	-537	4.02	4.02	4.02	4.02	2	0.31	0.02	0.15	0.00	0.00	22.3
13	120	898	933	668	0	1085	-717	4.02	4.02	4.02	4.02	2	0.31	0.03	0.17	0.00	0.00	22.3
14	120	1267	728	615	0	991	480	4.02	4.02	4.02	4.02	2	0.28	0.02	0.13	0.00	0.00	22.3
15	120	793	1001	599	0	983	-853	4.02	4.02	4.02	4.02	2	0.28	0.03	0.18	0.00	0.00	22.3
16	120	1239	741	645	0	1036	460	4.02	4.02	4.02	4.02	2	0.30	0.02	0.13	0.00	0.00	22.3
17	120	765	1014	628	0	1029	-887	4.02	4.02	4.02	4.02	2	0.29	0.03	0.18	0.00	0.00	22.3
18	120	6001	732	1567	0	2475	-421	4.02	4.02	4.02	4.02	3	0.72	0.05	0.25	0.00	0.00	22.3
19	120	2755	1103	1682	0	2713	-933	4.02	4.02	4.02	4.02	3	0.72	0.05	0.27	0.00	0.00	22.3
20	120	4382	1043	1507	0	2405	-925	4.02	4.02	4.02	4.02	3	0.67	0.05	0.24	0.00	0.00	22.3
37	120	6077	678	1263	0	1980	412	4.02	4.02	4.02	4.02	3	0.58	0.04	0.20	0.00	0.00	22.3
38	120	666	1297	1454	0	2375	-1125	4.02	4.02	4.02	4.02	3	0.59	0.05	0.23	0.00	0.00	22.3
39	120	3378	1196	1163	0	1861	-1110	4.02	4.02	4.02	4.02	3	0.50	0.04	0.21	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	180	1321	737	808	0	828	764	4.02	4.02	4.02	4.02	3	0.21	0.03	0.13	0.00	0.00	22.3
2	180	1134	503	575	0	590	616	4.02	4.02	4.02	4.02	2	0.17	0.02	0.09	0.00	0.00	22.3
3	180	992	585	570	0	591	584	4.02	4.02	4.02	4.02	2	0.17	0.02	0.10	0.00	0.00	22.3
4	180	1040	546	673	0	683	589	4.02	4.02	4.02	4.02	2	0.19	0.02	0.11	0.00	0.00	22.3
5	180	898	628	668	0	683	542	4.02	4.02	4.02	4.02	2	0.19	0.02	0.11	0.00	0.00	22.3
6	180	1267	423	615	0	622	620	4.02	4.02	4.02	4.02	2	0.18	0.02	0.10	0.00	0.00	22.3
7	180	793	696	599	0	624	515	4.02	4.02	4.02	4.02	2	0.18	0.02	0.12	0.00	0.00	22.3
8	180	1239	436	645	0	650	609	4.02	4.02	4.02	4.02	2	0.19	0.02	0.10	0.00	0.00	22.3
9	180	765	709	628	0	652	502	4.02	4.02	4.02	4.02	2	0.18	0.02	0.13	0.00	0.00	22.3
10	180	1134	503	575	0	590	616	4.02	4.02	4.02	4.02	2	0.17	0.02	0.09	0.00	0.00	22.3
11	180	992	585	570	0	591	584	4.02	4.02	4.02	4.02	2	0.17	0.02	0.10	0.00	0.00	22.3
12	180	1040	546	673	0	683	589	4.02	4.02	4.02	4.02	2	0.19	0.02	0.11	0.00	0.00	22.3
13	180	898	628	668	0	683	542	4.02	4.02	4.02	4.02	2	0.19	0.02	0.11	0.00	0.00	22.3
14	180	1267	423	615	0	622	620	4.02	4.02	4.02	4.02	2	0.18	0.02	0.10	0.00	0.00	22.3
15	180	793	696	599	0	624	515	4.02	4.02	4.02	4.02	2	0.18	0.02	0.12	0.00	0.00	22.3
16	180	1239	436	645	0	650	609	4.02	4.02	4.02	4.02	2	0.19	0.02	0.10	0.00	0.00	22.3
17	180	765	709	628	0	652	502	4.02	4.02	4.02	4.02	2	0.18	0.02	0.13	0.00	0.00	22.3
18	180	6001	336	1567	0	1535	354	4.02	4.02	4.02	4.02	3	0.45	0.05	0.25	0.00	0.00	22.3
19	180	2755	708	1682	0	1704	527	4.02	4.02	4.02	4.02	3	0.45	0.05	0.27	0.00	0.00	22.3
20	180	4382	647	1507	0	1501	412	4.02	4.02	4.02	4.02	3	0.42	0.05	0.24	0.00	0.00	22.3
37	180	6077	282	1263	0	1222	412	4.02	4.02	4.02	4.02	3	0.36	0.04	0.20	0.00	0.00	22.3
38	180	666	902	1454	0	1502	648	4.02	4.02	4.02	4.02	3	0.38	0.05	0.23	0.00	0.00	22.3
39	180	3378	801	1163	0	1163	500	4.02	4.02	4.02	4.02	3	0.31	0.04	0.19	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	240	1321	341	808	0	343	799	4.02	4.02	4.02	4.02	3	0.12	0.03	0.13	0.00	0.00	22.3
2	240	1134	199	575	0	245	616	4.02	4.02	4.02	4.02	2	0.10	0.02	0.09	0.00	0.00	22.3
3	240	992	281	570	0	249	626	4.02	4.02	4.02	4.02	2	0.10	0.02	0.09	0.00	0.00	22.3
4	240	1040	242	673	0	279	604	4.02	4.02	4.02	4.02	2	0.09	0.02	0.11	0.00	0.00	22.3
5	240	898	324	668	0	282	614	4.02	4.02	4.02	4.02	2	0.10	0.02	0.11	0.00	0.00	22.3
6	240	1267	119	615	0	253	620	4.02	4.02	4.02	4.02	2	0.10	0.02	0.10	0.00	0.00	22.3
7	240	793	392	599	0	265	634	4.02	4.02	4.02	4.02	2	0.10	0.02	0.10	0.00	0.00	22.3
8	240	1239	132	645	0	263	609	4.02	4.02	4.02	4.02	2	0.10	0.02	0.10	0.00	0.00	22.3
9	240	765	405	628	0	275	630	4.02	4.02	4.02	4.02	2	0.10	0.02	0.10	0.00	0.00	22.3
10	240	1134	199	575	0	245	616	4.02	4.02	4.02	4.02	2	0.10	0.02	0.09	0.00	0.00	22.3
11	240	992	281	570	0	249	626	4.02	4.02	4.02	4.02	2	0.10	0.02	0.09	0.00	0.00	22.3
12	240	1040	242	673	0	279	604	4.02	4.02	4.02	4.02	2	0.09	0.02	0.11	0.00	0.00	22.3
13	240	898	324	668	0	282	614	4.02	4.02	4.02	4.02	2	0.10	0.02	0.11	0.00	0.00	22.3
14	240	1267	119	615	0	253	620	4.02	4.02	4.02	4.02	2	0.10	0.02	0.10	0.00	0.00	22.3
15	240	793	392	599	0	265	634	4.02	4.02	4.02	4.02	2	0.10	0.02	0.10	0.00	0.00	22.3
16	240	1239	132	645	0	263	609	4.02	4.02	4.02	4.02	2	0.10	0.02	0.10	0.00	0.00	22.3
17	240	765	405	628	0	275	630	4.02	4.02	4.02	4.02	2	0.10	0.02	0.10	0.00	0.00	22.3
18	240	6001	-59	1567	0	595	354	4.02	4.02	4.02	4.02	3	0.17	0.05	0.25	0.00	0.00	22.3
19	240	2755	312	1682	0	695	544	4.02	4.02	4.02	4.02	3	0.18	0.05	0.27	0.00	0.00	22.3
20	240	4382	252	1507	0	597	412	4.02	4.02	4.02	4.02	3	0.17	0.05	0.24	0.00	0.00	22.3
37	240	6077	-113	1263	0	464	412	4.02	4.02	4.02	4.02	3	0.14	0.04	0.20	0.00	0.00	22.3
38	240	666	506	1454	0	630	799	4.02	4.02	4.02	4.02	3	0.16	0.05	0.23	0.00	0.00	22.3
39	240	3378	405	1163	0	466	581	4.02	4.02	4.02	4.02	3	0.13	0.04	0.19	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	300	1321	-54	808	0	-141	799	4.02	4.02	4.02	4.02	3	0.12	0.03	0.13	0.00	0.00	22.3
2	300	1134	-105	575	0	-100	616	4.02	4.02	4.02	4.02	2	0.10	0.02	0.09	0.00	0.00	22.3
3	300	992	-23	570	0	-93	626	4.02	4.02	4.02	4.02	2	0.10	0.02	0.09	0.00	0.00	22.3
4	300	1040	-62	673	0	-126	604	4.02	4.02	4.02	4.02	2	0.09	0.02	0.11	0.00	0.00	22.3

5	300	898	20	668	0	-119	614	4.02	4.02	4.02	4.02	2	0.10	0.02	0.11	0.00	0.00	22.3
6	300	1267	-185	615	0	-116	620	4.02	4.02	4.02	4.02	2	0.10	0.02	0.10	0.00	0.00	22.3
7	300	793	88	599	0	-94	634	4.02	4.02	4.02	4.02	2	0.10	0.02	0.10	0.00	0.00	22.3
8	300	1239	-172	645	0	-124	609	4.02	4.02	4.02	4.02	2	0.10	0.02	0.10	0.00	0.00	22.3
9	300	765	101	628	0	-102	630	4.02	4.02	4.02	4.02	2	0.10	0.02	0.10	0.00	0.00	22.3
10	300	1134	-105	575	0	-100	616	4.02	4.02	4.02	4.02	2	0.10	0.02	0.09	0.00	0.00	22.3
11	300	992	-23	570	0	-93	626	4.02	4.02	4.02	4.02	2	0.10	0.02	0.09	0.00	0.00	22.3
12	300	1040	-62	673	0	-126	604	4.02	4.02	4.02	4.02	2	0.09	0.02	0.11	0.00	0.00	22.3
13	300	898	20	668	0	-119	614	4.02	4.02	4.02	4.02	2	0.10	0.02	0.11	0.00	0.00	22.3
14	300	1267	-185	615	0	-116	620	4.02	4.02	4.02	4.02	2	0.10	0.02	0.10	0.00	0.00	22.3
15	300	793	88	599	0	-94	634	4.02	4.02	4.02	4.02	2	0.10	0.02	0.10	0.00	0.00	22.3
16	300	1239	-172	645	0	-124	609	4.02	4.02	4.02	4.02	2	0.10	0.02	0.10	0.00	0.00	22.3
17	300	765	101	628	0	-102	630	4.02	4.02	4.02	4.02	2	0.10	0.02	0.10	0.00	0.00	22.3
18	300	6001	-455	1567	0	-346	354	4.02	4.02	4.02	4.02	3	0.10	0.05	0.25	0.00	0.00	22.3
19	300	2755	-83	1682	0	-314	544	4.02	4.02	4.02	4.02	3	0.08	0.05	0.27	0.00	0.00	22.3
20	300	4382	-144	1507	0	-308	412	4.02	4.02	4.02	4.02	3	0.09	0.05	0.24	0.00	0.00	22.3
37	300	6077	-509	1263	0	-295	412	4.02	4.02	4.02	4.02	3	0.09	0.04	0.20	0.00	0.00	22.3
38	300	666	110	1454	0	-243	799	4.02	4.02	4.02	4.02	3	0.12	0.05	0.23	0.00	0.00	22.3
39	300	3378	10	1163	0	-232	581	4.02	4.02	4.02	4.02	3	0.09	0.04	0.19	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	360	1321	-450	808	0	-626	799	4.02	4.02	4.02	4.02	3	0.16	0.03	0.13	0.00	0.00	22.3
2	360	1134	-409	575	0	-444	616	4.02	4.02	4.02	4.02	2	0.13	0.02	0.09	0.00	0.00	22.3
3	360	992	-327	570	0	-435	626	4.02	4.02	4.02	4.02	2	0.12	0.02	0.09	0.00	0.00	22.3
4	360	1040	-366	673	0	-530	604	4.02	4.02	4.02	4.02	2	0.15	0.02	0.11	0.00	0.00	22.3
5	360	898	-284	668	0	-520	614	4.02	4.02	4.02	4.02	2	0.15	0.02	0.11	0.00	0.00	22.3
6	360	1267	-489	615	0	-485	620	4.02	4.02	4.02	4.02	2	0.14	0.02	0.10	0.00	0.00	22.3
7	360	793	-216	599	0	-454	634	4.02	4.02	4.02	4.02	2	0.13	0.02	0.10	0.00	0.00	22.3
8	360	1239	-476	645	0	-511	609	4.02	4.02	4.02	4.02	2	0.15	0.02	0.10	0.00	0.00	22.3
9	360	765	-203	628	0	-479	630	4.02	4.02	4.02	4.02	2	0.14	0.02	0.10	0.00	0.00	22.3
10	360	1134	-409	575	0	-444	616	4.02	4.02	4.02	4.02	2	0.13	0.02	0.09	0.00	0.00	22.3
11	360	992	-327	570	0	-435	626	4.02	4.02	4.02	4.02	2	0.12	0.02	0.09	0.00	0.00	22.3
12	360	1040	-366	673	0	-530	604	4.02	4.02	4.02	4.02	2	0.15	0.02	0.11	0.00	0.00	22.3
13	360	898	-284	668	0	-520	614	4.02	4.02	4.02	4.02	2	0.15	0.02	0.11	0.00	0.00	22.3
14	360	1267	-489	615	0	-485	620	4.02	4.02	4.02	4.02	2	0.14	0.02	0.10	0.00	0.00	22.3
15	360	793	-216	599	0	-454	634	4.02	4.02	4.02	4.02	2	0.13	0.02	0.10	0.00	0.00	22.3
16	360	1239	-476	645	0	-511	609	4.02	4.02	4.02	4.02	2	0.15	0.02	0.10	0.00	0.00	22.3
17	360	765	-203	628	0	-479	630	4.02	4.02	4.02	4.02	2	0.14	0.02	0.10	0.00	0.00	22.3
18	360	6001	-850	1567	0	-1286	-622	4.02	4.02	4.02	4.02	3	0.38	0.05	0.25	0.00	0.00	22.3
19	360	2755	-478	1682	0	-1324	544	4.02	4.02	4.02	4.02	3	0.35	0.05	0.27	0.00	0.00	22.3
20	360	4382	-539	1507	0	-1212	412	4.02	4.02	4.02	4.02	3	0.34	0.05	0.24	0.00	0.00	22.3
37	360	6077	-904	1263	0	-1053	-656	4.02	4.02	4.02	4.02	3	0.31	0.04	0.20	0.00	0.00	22.3
38	360	666	-285	1454	0	-1116	799	4.02	4.02	4.02	4.02	3	0.28	0.05	0.23	0.00	0.00	22.3
39	360	3378	-385	1163	0	-930	581	4.02	4.02	4.02	4.02	3	0.25	0.04	0.19	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	420	1321	-845	808	0	-1111	687	4.02	4.02	4.02	4.02	3	0.28	0.03	0.15	0.00	0.00	22.3
2	420	1134	-713	575	0	-789	487	4.02	4.02	4.02	4.02	2	0.23	0.02	0.13	0.00	0.00	22.3
3	420	992	-631	570	0	-777	553	4.02	4.02	4.02	4.02	2	0.22	0.02	0.11	0.00	0.00	22.3
4	420	1040	-670	673	0	-934	505	4.02	4.02	4.02	4.02	2	0.27	0.02	0.12	0.00	0.00	22.3
5	420	898	-588	668	0	-921	571	4.02	4.02	4.02	4.02	2	0.26	0.02	0.11	0.00	0.00	22.3
6	420	1267	-793	615	0	-854	414	4.02	4.02	4.02	4.02	2	0.25	0.02	0.14	0.00	0.00	22.3
7	420	793	-520	599	0	-813	634	4.02	4.02	4.02	4.02	2	0.23	0.02	0.10	0.00	0.00	22.3
8	420	1239	-780	645	0	-898	420	4.02	4.02	4.02	4.02	2	0.26	0.02	0.14	0.00	0.00	22.3
9	420	765	-507	628	0	-856	630	4.02	4.02	4.02	4.02	2	0.24	0.02	0.10	0.00	0.00	22.3
10	420	1134	-713	575	0	-789	487	4.02	4.02	4.02	4.02	2	0.23	0.02	0.13	0.00	0.00	22.3
11	420	992	-631	570	0	-777	553	4.02	4.02	4.02	4.02	2	0.22	0.02	0.11	0.00	0.00	22.3
12	420	1040	-670	673	0	-934	505	4.02	4.02	4.02	4.02	2	0.27	0.02	0.12	0.00	0.00	22.3
13	420	898	-588	668	0	-921	571	4.02	4.02	4.02	4.02	2	0.26	0.02	0.11	0.00	0.00	22.3
14	420	1267	-793	615	0	-854	414	4.02	4.02	4.02	4.02	2	0.25	0.02	0.14	0.00	0.00	22.3
15	420	793	-520	599	0	-813	634	4.02	4.02	4.02	4.02	2	0.23	0.02	0.10	0.00	0.00	22.3
16	420	1239	-780	645	0	-898	420	4.02	4.02	4.02	4.02	2	0.26	0.02	0.14	0.00	0.00	22.3
17	420	765	-507	628	0	-856	630	4.02	4.02	4.02	4.02	2	0.24	0.02	0.10	0.00	0.00	22.3
18	420	6001	-1246	1567	0	-2226	-1450	4.02	4.02	4.02	4.02	3	0.65	0.05	0.25	0.00	0.00	22.3
19	420	2755	-874	1682	0	-2333	-473	4.02	4.02	4.02	4.02	3	0.62	0.05	0.27	0.00	0.00	22.3
20	420	4382	-934	1507	0	-2116	-707	4.02	4.02	4.02	4.02	3	0.59	0.05	0.24	0.00	0.00	22.3
37	420	6077	-1300	1263	0	-1811	-1517	4.02	4.02	4.02	4.02	3	0.53	0.04	0.23	0.00	0.00	22.3
38	420	666	-680	1454	0	-1988	799	4.02	4.02	4.02	4.02	3	0.50	0.05	0.23	0.00	0.00	22.3
39	420	3378	-781	1163	0	-1627	513	4.02	4.02	4.02	4.02	3	0.44	0.04	0.19	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	480	1321	-1241	808	0	-1596	-995	4.02	4.02	4.02	4.02	3	0.41	0.04	0.22	0.00	0.00	22.3
2	480	1134	-1018	575	0	-1134	-909	4.02	4.02	4.02	4.02	2	0.32	0.03	0.18	0.00	0.00	22.3
3	480	992	-936	570	0	-1119	-710	4.02	4.02	4.02	4.02	2	0.32	0.03	0.17	0.00	0.00	22.3
4	480	1040	-975	673	0	-1338	-821	4.02	4.02	4.02	4.02	2	0.38	0.03	0.17	0.00	0.00	22.3
5	480	898	-893	668	0	-1323	-623	4.02	4.02	4.02	4.02	2	0.38	0.03	0.16	0.00	0.00	22.3
6	480	1267	-1098	615	0	-1223	-1110	4.02	4.02	4.02	4.02	2	0.35	0.03	0.20	0.00	0.00	22.3
7	480	793	-825	599	0	-1172	-447	4.02	4.02	4.02	4.02	2	0.33	0.02	0.15	0.00	0.00	22.3
8	480	1239	-1085	645	0	-1284	-1084	4.02	4.02	4.02	4.02	2	0.37	0.03	0.19	0.00	0.00	22.3
9	480	765	-812	628	0	-1233	-421	4.02	4.02	4.02	4.02	2	0.35	0.02	0.14	0.00	0.00	22.3
10	480	1134	-1018	575	0	-1134	-909	4.02	4.02	4.02	4.02	2	0.32	0.03	0.18	0.00	0.00	22.3
11	480	992	-936	570	0	-1119	-710	4.02	4.02	4.02	4.02	2	0.32	0.03	0.17	0.00	0.00	22.3
12	480	1040	-975	673	0	-1338	-821	4.02	4.02	4.02	4.02	2	0.38	0.03	0.17	0.00	0.00	22.3
13	480	898	-893	668	0	-1323	-623	4.02	4.02	4.02	4.02	2	0.38	0.03	0.16	0.00	0.00	22.3
14	480	1267	-1098	615	0	-1223	-1110	4.02	4.02	4.02	4.02	2	0.35	0.03	0.20	0.00	0.00	22.3
15	480	793	-825	599	0	-1172	-447	4.02	4.02	4.02	4.02	2	0.33	0.02	0.15	0.00	0.00	22.3
16	480	1239	-1085	645	0	-1284	-1084	4.02	4.02	4.02	4.02	2	0.37	0.03	0.19	0.00	0.00	22.3
17	480	765	-812	628	0	-1233	-421	4.02	4.02	4.02	4.02	2	0.35	0.02	0.14	0.00	0.00	22.3
18	480	6001	-1641	1567	0	-3166	-2516	4.02	4.02	4.02	4.02	3	0.92	0.05	0.29	0.00	0.00	22.3
19	480	2755	-1269	1682	0	-3342	-1316	4.02	4.02	4.02	4.02	3	0.89	0.05	0.27	0.00	0.00	22.3
20	480	4382	-1330	1507	0	-3020	-1587	4.02	4.02	4.02	4.02	3	0.84	0.05	0.24	0.00	0.00	22.3
37	480	6077	-1695	1263	0	-2569	-2615	4.02	4.02	4.02	4.02	3	0.75	0.05	0.30	0.00	0.00	22.3
38	480	666	-1076	1454	0	-2861	-614	4.02	4.02	4.02	4.02	3	0.72	0.05	0.23	0.00	0.00	22.3
39	480	3378	-1176	1163	0	-2325	-1065	4.02	4.02	4.02	4.02	3	0.63	0.04	0.21	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	540	1321	-1636	808	0	-2081	-2059	4.02	4.02	4.02	4.02	3	0.53	0.05	0.29	0.00	0.00	22.3
2	540	1134	-1322	575	0	-1479	-1764	4.02	4.02	4.02	4.02	2	0.42	0.04	0.24	0.00	0.00	22.3
3	540	992	-1240	570	0	-1461	-1517	4.02	4.02	4.02	4.02	2	0.42	0.04	0.22	0.00	0.00	22.3
4	540	1040	-1279	673	0	-1742	-1651	4.02	4.02	4.02	4.02	2	0.50	0.04	0.23	0.00	0.00	22.3
5	540	898	-1197	668	0	-1724	-1404	4.02	4.02	4.02	4.02	2	0.49	0.03	0.21	0.00	0.00	22.3
6	540	1267	-1402	615	0	-1592	-2014	4.02	4.02	4.02	4.02	2	0.46	0.04	0.25	0.00	0.00	22.3
7	540	793	-1129	599	0	-1532	-1187	4.02	4.02	4.02	4.02	2	0.43	0.03	0.20	0.00	0.00	22.3
8	540	1239	-1389	645	0	-1671	-1980	4.02	4.02	4.02	4.02	2	0.48	0.04	0.25	0.00	0.00	22.3
9	540	765	-1116	628	0	-1610	-1153	4.02	4.02	4.02	4.02	2	0.46	0.03	0.20	0.00	0.00	22.3
10	540	1134	-1322	575	0	-1479	-1764	4.02	4.02	4.02	4.02	2	0.42	0.04	0.24	0.00	0.00	22.3

11	540	992	-1240	570	0	-1461	-1517	4.02	4.02	4.02	4.02	2	0.42	0.04	0.22	0.00	0.00	22.3
12	540	1040	-1279	673	0	-1742	-1651	4.02	4.02	4.02	4.02	2	0.50	0.04	0.23	0.00	0.00	22.3
13	540	898	-1197	668	0	-1724	-1404	4.02	4.02	4.02	4.02	2	0.49	0.03	0.21	0.00	0.00	22.3
14	540	1267	-1402	615	0	-1592	-2014	4.02	4.02	4.02	4.02	2	0.46	0.04	0.25	0.00	0.00	22.3
15	540	793	-1129	599	0	-1532	-1187	4.02	4.02	4.02	4.02	2	0.43	0.03	0.20	0.00	0.00	22.3
16	540	1239	-1389	645	0	-1671	-1980	4.02	4.02	4.02	4.02	2	0.48	0.04	0.25	0.00	0.00	22.3
17	540	765	-1116	628	0	-1610	-1153	4.02	4.02	4.02	4.02	2	0.46	0.03	0.20	0.00	0.00	22.3
18	540	6001	-2036	1567	0	-4107	-3820	4.02	6.03	4.02	4.02	3	0.81	0.06	0.36	0.00	0.00	22.3
19	540	2755	-1665	1682	0	-4351	-2396	4.02	6.03	4.02	4.02	3	0.80	0.05	0.30	0.00	0.00	22.3
20	540	4382	-1725	1507	0	-3924	-2704	4.02	6.03	4.02	4.02	3	0.75	0.05	0.31	0.00	0.00	22.3
37	540	6077	-2090	1263	0	-3327	-3951	4.02	4.02	4.02	4.02	3	0.97	0.06	0.37	0.00	0.00	22.3
38	540	666	-1471	1454	0	-3733	-1579	4.02	4.02	4.02	4.02	3	0.93	0.05	0.26	0.00	0.00	22.3
39	540	3378	-1572	1163	0	-3022	-2090	4.02	4.02	4.02	4.02	3	0.82	0.05	0.28	0.00	0.00	22.3

apost= -- aant= 2.01 ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	600	1321	-2032	808	0	-2566	-2331	4.02	4.02	4.02	4.02	3	0.65	0.06	0.36	0.00	0.00	22.3
2	600	1134	-1626	575	0	-1824	-1979	4.02	4.02	4.02	4.02	2	0.52	0.05	0.29	0.00	0.00	22.3
3	600	992	-1544	570	0	-1803	-1724	4.02	4.02	4.02	4.02	2	0.51	0.04	0.28	0.00	0.00	22.3
4	600	1040	-1583	673	0	-2146	-1862	4.02	4.02	4.02	4.02	2	0.61	0.05	0.28	0.00	0.00	22.3
5	600	898	-1501	668	0	-2125	-1607	4.02	4.02	4.02	4.02	2	0.60	0.04	0.27	0.00	0.00	22.3
6	600	1267	-1706	615	0	-1961	-2237	4.02	4.02	4.02	4.02	2	0.56	0.05	0.30	0.00	0.00	22.3
7	600	793	-1433	599	0	-1891	-1384	4.02	4.02	4.02	4.02	2	0.54	0.04	0.26	0.00	0.00	22.3
8	600	1239	-1693	645	0	-2058	-2202	4.02	4.02	4.02	4.02	2	0.59	0.05	0.30	0.00	0.00	22.3
9	600	765	-1420	628	0	-1987	-1349	4.02	4.02	4.02	4.02	2	0.56	0.04	0.25	0.00	0.00	22.3
10	600	1134	-1626	575	0	-1824	-1979	4.02	4.02	4.02	4.02	2	0.52	0.05	0.29	0.00	0.00	22.3
11	600	992	-1544	570	0	-1803	-1724	4.02	4.02	4.02	4.02	2	0.51	0.04	0.28	0.00	0.00	22.3
12	600	1040	-1583	673	0	-2146	-1862	4.02	4.02	4.02	4.02	2	0.61	0.05	0.28	0.00	0.00	22.3
13	600	898	-1501	668	0	-2125	-1607	4.02	4.02	4.02	4.02	2	0.60	0.04	0.27	0.00	0.00	22.3
14	600	1267	-1706	615	0	-1961	-2237	4.02	4.02	4.02	4.02	2	0.56	0.05	0.30	0.00	0.00	22.3
15	600	793	-1433	599	0	-1891	-1384	4.02	4.02	4.02	4.02	2	0.54	0.04	0.26	0.00	0.00	22.3
16	600	1239	-1693	645	0	-2058	-2202	4.02	4.02	4.02	4.02	2	0.59	0.05	0.30	0.00	0.00	22.3
17	600	765	-1420	628	0	-1987	-1349	4.02	4.02	4.02	4.02	2	0.56	0.04	0.25	0.00	0.00	22.3
18	600	6001	-2432	1567	0	-5047	-4129	4.02	6.03	4.02	4.02	3	0.99	0.07	0.43	0.00	0.00	22.3
19	600	2755	-2060	1682	0	-5360	-2671	4.02	6.03	4.02	4.02	3	0.99	0.06	0.37	0.00	0.00	22.3
20	600	4382	-2121	1507	0	-4828	-2984	4.02	6.03	4.02	4.02	3	0.92	0.06	0.38	0.00	0.00	22.3
37	600	6077	-2486	1263	0	-4085	-4265	4.02	6.03	4.02	4.02	3	0.80	0.07	0.44	0.00	0.00	22.3
38	600	666	-1867	1454	0	-4606	-1835	4.02	6.03	4.02	4.02	3	0.81	0.05	0.33	0.00	0.00	22.3
39	600	3378	-1967	1163	0	-3720	-2356	4.02	6.03	4.02	4.02	3	0.69	0.06	0.35	0.00	0.00	22.3

apost= -- aant= 2.01 ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

Nome travata: **Trave_404_IP1** Descrizione: **Trave_4 32-25**
ASTA NUM. 15 NI 26 NF 254 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y Permanente qy tot.
qy medio: 375.00 132.00 507.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	1274	2019	984	0	3130	-2106	4.02	4.02	4.02	4.02	3	0.80	0.06	0.36	0.00	0.00	22.3
2	0	1200	1535	818	0	2609	-1575	4.02	4.02	4.02	4.02	2	0.75	0.04	0.27	0.00	0.00	22.3
3	0	930	1599	859	0	2770	-1791	4.02	4.02	4.02	4.02	2	0.79	0.05	0.28	0.00	0.00	22.3
4	0	1030	1507	655	0	2045	-1449	4.02	4.02	4.02	4.02	2	0.58	0.04	0.27	0.00	0.00	22.3
5	0	760	1572	696	0	2207	-1664	4.02	4.02	4.02	4.02	2	0.62	0.05	0.28	0.00	0.00	22.3
6	0	1455	1450	713	0	2223	-1279	4.02	4.02	4.02	4.02	2	0.64	0.04	0.26	0.00	0.00	22.3
7	0	556	1665	850	0	2761	-1998	4.02	4.02	4.02	4.02	2	0.78	0.05	0.30	0.00	0.00	22.3
8	0	1404	1442	664	0	2054	-1241	4.02	4.02	4.02	4.02	2	0.59	0.04	0.26	0.00	0.00	22.3
9	0	504	1657	801	0	2592	-1960	4.02	4.02	4.02	4.02	2	0.73	0.05	0.30	0.00	0.00	22.3
10	0	1200	1535	818	0	2609	-1575	4.02	4.02	4.02	4.02	2	0.75	0.04	0.27	0.00	0.00	22.3
11	0	930	1599	859	0	2770	-1791	4.02	4.02	4.02	4.02	2	0.79	0.05	0.28	0.00	0.00	22.3
12	0	1030	1507	655	0	2045	-1449	4.02	4.02	4.02	4.02	2	0.58	0.04	0.27	0.00	0.00	22.3
13	0	760	1572	696	0	2207	-1664	4.02	4.02	4.02	4.02	2	0.62	0.05	0.28	0.00	0.00	22.3
14	0	1455	1450	713	0	2223	-1279	4.02	4.02	4.02	4.02	2	0.64	0.04	0.26	0.00	0.00	22.3
15	0	556	1665	850	0	2761	-1998	4.02	4.02	4.02	4.02	2	0.78	0.05	0.30	0.00	0.00	22.3
16	0	1404	1442	664	0	2054	-1241	4.02	4.02	4.02	4.02	2	0.59	0.04	0.26	0.00	0.00	22.3
17	0	504	1657	801	0	2592	-1960	4.02	4.02	4.02	4.02	2	0.73	0.05	0.30	0.00	0.00	22.3
18	0	3300	2140	2274	0	7303	-2626	10.05	4.02	4.02	4.02	3	0.84	0.07	0.38	0.00	0.00	22.3
19	0	2815	2023	1572	0	4945	-2061	6.03	4.02	4.02	4.02	3	0.91	0.06	0.36	0.00	0.00	22.3
20	0	3493	2101	1961	0	6379	-2399	8.04	4.02	4.02	4.02	3	0.91	0.06	0.37	0.00	0.00	22.3
37	0	2876	2159	2201	0	7110	-2738	10.05	4.02	4.02	4.02	3	0.82	0.07	0.38	0.00	0.00	22.3
38	0	2068	1964	1031	0	3181	-1797	4.02	4.02	4.02	4.02	3	0.83	0.06	0.35	0.00	0.00	22.3
39	0	3198	2094	1679	0	5570	-2360	8.04	4.02	4.02	4.02	3	0.79	0.06	0.37	0.00	0.00	22.3

apost= 6.03 aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	60	1274	1624	984	0	2540	-1835	4.02	4.02	4.02	4.02	3	0.65	0.05	0.29	0.00	0.00	22.3
2	60	1200	1231	818	0	2118	-1369	4.02	4.02	4.02	4.02	2	0.61	0.04	0.22	0.00	0.00	22.3
3	60	930	1295	859	0	2254	-1578	4.02	4.02	4.02	4.02	2	0.64	0.04	0.23	0.00	0.00	22.3
4	60	1030	1203	655	0	1652	-1245	4.02	4.02	4.02	4.02	2	0.47	0.03	0.21	0.00	0.00	22.3
5	60	760	1268	696	0	1790	-1454	4.02	4.02	4.02	4.02	2	0.51	0.04	0.23	0.00	0.00	22.3
6	60	1455	1146	713	0	1795	-1081	4.02	4.02	4.02	4.02	2	0.52	0.03	0.20	0.00	0.00	22.3
7	60	556	1361	850	0	2251	-1779	4.02	4.02	4.02	4.02	2	0.63	0.04	0.24	0.00	0.00	22.3
8	60	1404	1138	664	0	1655	-1043	4.02	4.02	4.02	4.02	2	0.48	0.03	0.20	0.00	0.00	22.3
9	60	504	1353	801	0	2112	-1742	4.02	4.02	4.02	4.02	2	0.59	0.04	0.24	0.00	0.00	22.3
10	60	1200	1231	818	0	2118	-1369	4.02	4.02	4.02	4.02	2	0.61	0.04	0.22	0.00	0.00	22.3
11	60	930	1295	859	0	2254	-1578	4.02	4.02	4.02	4.02	2	0.64	0.04	0.23	0.00	0.00	22.3
12	60	1030	1203	655	0	1652	-1245	4.02	4.02	4.02	4.02	2	0.47	0.03	0.21	0.00	0.00	22.3
13	60	760	1268	696	0	1790	-1454	4.02	4.02	4.02	4.02	2	0.51	0.04	0.23	0.00	0.00	22.3
14	60	1455	1146	713	0	1795	-1081	4.02	4.02	4.02	4.02	2	0.52	0.03	0.20	0.00	0.00	22.3
15	60	556	1361	850	0	2251	-1779	4.02	4.02	4.02	4.02	2	0.63	0.04	0.24	0.00	0.00	22.3
16	60	1404	1138	664	0	1655	-1043	4.02	4.02	4.02	4.02	2	0.48	0.03	0.20	0.00	0.00	22.3
17	60	504	1353	801	0	2112	-1742	4.02	4.02	4.02	4.02	2	0.59	0.04	0.24	0.00	0.00	22.3
18	60	3300	1744	2274	0	5938	-2344	8.04	4.02	4.02	4.02	3	0.85	0.07	0.37	0.00	0.00	22.3
19	60	2815	1628	1572	0	4002	-1790	6.03	4.02	4.02	4.02	3	0.74	0.05	0.29	0.00	0.00	22.3
20	60	3493	1706	1961	0	5203	-2121	6.03	4.02	4.02	4.02	3	0.97	0.06	0.32	0.00	0.00	22.3
37	60	2876	1764	2201	0	5789	-2454	8.04	4.02	4.02	4.02	3	0.82	0.07	0.35	0.00	0.00	22.3
38	60	2068	1569	1031	0	2562	-1531	4.02	4.02	4.02	4.02	3	0.67	0.05	0.28	0.00	0.00	22.3
39	60	3198	1698	1679	0	4563	-2082	6.03	4.02	4.02	4.02	3	0.85	0.05	0.30	0.00	0.00	22.3

apost= 4.02 aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	120	1274	1228	984	0	1949	-779	4.02	4.02	4.02	4.02	3	0.50	0.04	0.22	0.00	0.00	22.3
2	120	1200	927	818	0	1627	-568	4.02	4.02	4.02	4.02	2	0.47	0.03	0.17	0.00	0.00	22.3

3	120	930	991	859	0	1739	-738	4.02	4.02	4.02	4.02	2	0.49	0.03	0.18	0.00	0.00	22.3
4	120	1030	899	655	0	1259	-460	4.02	4.02	4.02	4.02	2	0.36	0.03	0.16	0.00	0.00	22.3
5	120	760	964	696	0	1372	-630	4.02	4.02	4.02	4.02	2	0.39	0.03	0.17	0.00	0.00	22.3
6	120	1455	842	713	0	1367	522	4.02	4.02	4.02	4.02	2	0.40	0.02	0.15	0.00	0.00	22.3
7	120	556	1057	850	0	1741	-900	4.02	4.02	4.02	4.02	2	0.49	0.03	0.19	0.00	0.00	22.3
8	120	1404	834	664	0	1257	546	4.02	4.02	4.02	4.02	2	0.36	0.02	0.15	0.00	0.00	22.3
9	120	504	1049	801	0	1631	-867	4.02	4.02	4.02	4.02	2	0.46	0.03	0.19	0.00	0.00	22.3
10	120	1200	927	818	0	1627	-568	4.02	4.02	4.02	4.02	2	0.47	0.03	0.17	0.00	0.00	22.3
11	120	930	991	859	0	1739	-738	4.02	4.02	4.02	4.02	2	0.49	0.03	0.18	0.00	0.00	22.3
12	120	1030	899	655	0	1259	-460	4.02	4.02	4.02	4.02	2	0.36	0.03	0.16	0.00	0.00	22.3
13	120	760	964	696	0	1372	-630	4.02	4.02	4.02	4.02	2	0.39	0.03	0.17	0.00	0.00	22.3
14	120	1455	842	713	0	1367	522	4.02	4.02	4.02	4.02	2	0.40	0.02	0.15	0.00	0.00	22.3
15	120	556	1057	850	0	1741	-900	4.02	4.02	4.02	4.02	2	0.49	0.03	0.19	0.00	0.00	22.3
16	120	1404	834	664	0	1257	546	4.02	4.02	4.02	4.02	2	0.36	0.02	0.15	0.00	0.00	22.3
17	120	504	1049	801	0	1631	-867	4.02	4.02	4.02	4.02	2	0.46	0.03	0.19	0.00	0.00	22.3
18	120	3300	1349	2274	0	4574	-1216	6.03	4.02	4.02	4.02	3	0.85	0.07	0.37	0.00	0.00	22.3
19	120	2815	1232	1572	0	3058	-732	4.02	4.02	4.02	4.02	3	0.81	0.05	0.25	0.00	0.00	22.3
20	120	3493	1310	1961	0	4026	-1016	6.03	4.02	4.02	4.02	3	0.75	0.06	0.32	0.00	0.00	22.3
37	120	2876	1368	2201	0	4468	-1314	6.03	4.02	4.02	4.02	3	0.82	0.07	0.35	0.00	0.00	22.3
38	120	2068	1173	1031	0	1943	679	4.02	4.02	4.02	4.02	3	0.51	0.03	0.21	0.00	0.00	22.3
39	120	3198	1303	1679	0	3556	-981	4.02	4.02	4.02	4.02	3	0.95	0.05	0.27	0.00	0.00	22.3

apost= 2.01 aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	180	1274	833	984	0	1359	883	4.02	4.02	4.02	4.02	3	0.35	0.03	0.16	0.00	0.00	22.3
2	180	1200	622	818	0	1136	681	4.02	4.02	4.02	4.02	2	0.33	0.03	0.13	0.00	0.00	22.3
3	180	930	686	859	0	1224	614	4.02	4.02	4.02	4.02	2	0.35	0.03	0.14	0.00	0.00	22.3
4	180	1030	594	655	0	867	744	4.02	4.02	4.02	4.02	2	0.25	0.02	0.11	0.00	0.00	22.3
5	180	760	659	696	0	955	678	4.02	4.02	4.02	4.02	2	0.27	0.02	0.12	0.00	0.00	22.3
6	180	1455	537	713	0	939	781	4.02	4.02	4.02	4.02	2	0.27	0.02	0.11	0.00	0.00	22.3
7	180	556	752	850	0	1232	559	4.02	4.02	4.02	4.02	2	0.35	0.03	0.14	0.00	0.00	22.3
8	180	1404	529	664	0	859	800	4.02	4.02	4.02	4.02	2	0.25	0.02	0.11	0.00	0.00	22.3
9	180	504	744	801	0	1151	578	4.02	4.02	4.02	4.02	2	0.32	0.03	0.13	0.00	0.00	22.3
10	180	1200	622	818	0	1136	681	4.02	4.02	4.02	4.02	2	0.33	0.03	0.13	0.00	0.00	22.3
11	180	930	686	859	0	1224	614	4.02	4.02	4.02	4.02	2	0.35	0.03	0.14	0.00	0.00	22.3
12	180	1030	594	655	0	867	744	4.02	4.02	4.02	4.02	2	0.25	0.02	0.11	0.00	0.00	22.3
13	180	760	659	696	0	955	678	4.02	4.02	4.02	4.02	2	0.27	0.02	0.12	0.00	0.00	22.3
14	180	1455	537	713	0	939	781	4.02	4.02	4.02	4.02	2	0.27	0.02	0.11	0.00	0.00	22.3
15	180	556	752	850	0	1232	559	4.02	4.02	4.02	4.02	2	0.35	0.03	0.14	0.00	0.00	22.3
16	180	1404	529	664	0	859	800	4.02	4.02	4.02	4.02	2	0.25	0.02	0.11	0.00	0.00	22.3
17	180	504	744	801	0	1151	578	4.02	4.02	4.02	4.02	2	0.32	0.03	0.13	0.00	0.00	22.3
18	180	3300	954	2274	0	3209	640	4.02	4.02	4.02	4.02	3	0.86	0.07	0.37	0.00	0.00	22.3
19	180	2815	837	1572	0	2115	936	4.02	4.02	4.02	4.02	3	0.56	0.05	0.25	0.00	0.00	22.3
20	180	3493	915	1961	0	2850	777	4.02	4.02	4.02	4.02	3	0.77	0.06	0.32	0.00	0.00	22.3
37	180	2876	973	2201	0	3148	573	4.02	4.02	4.02	4.02	3	0.84	0.07	0.35	0.00	0.00	22.3
38	180	2068	778	1031	0	1325	1064	4.02	4.02	4.02	4.02	3	0.34	0.03	0.17	0.00	0.00	22.3
39	180	3198	908	1679	0	2548	801	4.02	4.02	4.02	4.02	3	0.68	0.05	0.27	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	240	1274	437	984	0	768	986	4.02	4.02	4.02	4.02	3	0.20	0.03	0.16	0.00	0.00	22.3
2	240	1200	318	818	0	645	748	4.02	4.02	4.02	4.02	2	0.19	0.03	0.13	0.00	0.00	22.3
3	240	930	382	859	0	708	726	4.02	4.02	4.02	4.02	2	0.20	0.03	0.14	0.00	0.00	22.3
4	240	1030	290	655	0	474	792	4.02	4.02	4.02	4.02	2	0.14	0.02	0.11	0.00	0.00	22.3
5	240	760	355	696	0	537	771	4.02	4.02	4.02	4.02	2	0.15	0.02	0.11	0.00	0.00	22.3
6	240	1455	233	713	0	511	789	4.02	4.02	4.02	4.02	2	0.15	0.02	0.11	0.00	0.00	22.3
7	240	556	448	850	0	722	716	4.02	4.02	4.02	4.02	2	0.20	0.03	0.14	0.00	0.00	22.3
8	240	1404	225	664	0	460	802	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
9	240	504	440	801	0	670	730	4.02	4.02	4.02	4.02	2	0.19	0.03	0.13	0.00	0.00	22.3
10	240	1200	318	818	0	645	748	4.02	4.02	4.02	4.02	2	0.19	0.03	0.13	0.00	0.00	22.3
11	240	930	382	859	0	708	726	4.02	4.02	4.02	4.02	2	0.20	0.03	0.14	0.00	0.00	22.3
12	240	1030	290	655	0	474	792	4.02	4.02	4.02	4.02	2	0.14	0.02	0.11	0.00	0.00	22.3
13	240	760	355	696	0	537	771	4.02	4.02	4.02	4.02	2	0.15	0.02	0.11	0.00	0.00	22.3
14	240	1455	233	713	0	511	789	4.02	4.02	4.02	4.02	2	0.15	0.02	0.11	0.00	0.00	22.3
15	240	556	448	850	0	722	716	4.02	4.02	4.02	4.02	2	0.20	0.03	0.14	0.00	0.00	22.3
16	240	1404	225	664	0	460	802	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
17	240	504	440	801	0	670	730	4.02	4.02	4.02	4.02	2	0.19	0.03	0.13	0.00	0.00	22.3
18	240	3300	558	2274	0	1844	827	4.02	4.02	4.02	4.02	3	0.50	0.07	0.37	0.00	0.00	22.3
19	240	2815	441	1572	0	1171	1041	4.02	4.02	4.02	4.02	3	0.31	0.05	0.25	0.00	0.00	22.3
20	240	3493	519	1961	0	1673	937	4.02	4.02	4.02	4.02	3	0.45	0.06	0.32	0.00	0.00	22.3
37	240	2876	577	2201	0	1827	773	4.02	4.02	4.02	4.02	3	0.49	0.07	0.35	0.00	0.00	22.3
38	240	2068	382	1031	0	706	1129	4.02	4.02	4.02	4.02	3	0.18	0.03	0.17	0.00	0.00	22.3
39	240	3198	512	1679	0	1541	956	4.02	4.02	4.02	4.02	3	0.41	0.05	0.27	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	300	1274	42	984	0	178	986	4.02	4.02	4.02	4.02	3	0.15	0.03	0.16	0.00	0.00	22.3
2	300	1200	14	818	0	155	748	4.02	4.02	4.02	4.02	2	0.12	0.03	0.13	0.00	0.00	22.3
3	300	930	78	859	0	193	726	4.02	4.02	4.02	4.02	2	0.11	0.03	0.14	0.00	0.00	22.3
4	300	1030	-14	655	0	81	792	4.02	4.02	4.02	4.02	2	0.12	0.02	0.11	0.00	0.00	22.3
5	300	760	51	696	0	120	771	4.02	4.02	4.02	4.02	2	0.12	0.02	0.11	0.00	0.00	22.3
6	300	1455	-71	713	0	84	789	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
7	300	556	144	850	0	212	716	4.02	4.02	4.02	4.02	2	0.11	0.03	0.14	0.00	0.00	22.3
8	300	1404	-79	664	0	62	802	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
9	300	504	136	801	0	190	730	4.02	4.02	4.02	4.02	2	0.11	0.03	0.13	0.00	0.00	22.3
10	300	1200	14	818	0	155	748	4.02	4.02	4.02	4.02	2	0.12	0.03	0.13	0.00	0.00	22.3
11	300	930	78	859	0	193	726	4.02	4.02	4.02	4.02	2	0.11	0.03	0.14	0.00	0.00	22.3
12	300	1030	-14	655	0	81	792	4.02	4.02	4.02	4.02	2	0.12	0.02	0.11	0.00	0.00	22.3
13	300	760	51	696	0	120	771	4.02	4.02	4.02	4.02	2	0.12	0.02	0.11	0.00	0.00	22.3
14	300	1455	-71	713	0	84	789	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
15	300	556	144	850	0	212	716	4.02	4.02	4.02	4.02	2	0.11	0.03	0.14	0.00	0.00	22.3
16	300	1404	-79	664	0	62	802	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
17	300	504	136	801	0	190	730	4.02	4.02	4.02	4.02	2	0.11	0.03	0.13	0.00	0.00	22.3
18	300	3300	162	2274	0	479	827	4.02	4.02	4.02	4.02	3	0.13	0.07	0.37	0.00	0.00	22.3
19	300	2815	46	1572	0	228	1041	4.02	4.02	4.02	4.02	3	0.16	0.05	0.25	0.00	0.00	22.3
20	300	3493	124	1961	0	496	937	4.02	4.02	4.02	4.02	3	0.15	0.06	0.32	0.00	0.00	22.3
37	300	2876	182	2201	0	506	773	4.02	4.02	4.02	4.02	3	0.13	0.07	0.35	0.00	0.00	22.3
38	300	2068	-13	1031	0	87	1129	4.02	4.02	4.02	4.02	3	0.17	0.03	0.17	0.00	0.00	22.3
39	300	3198	116	1679	0	534	956	4.02	4.02	4.02	4.02	3	0.15	0.05	0.27	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	360	1274	-353	984	0	-412	986	4.02	4.02	4.02	4.02	3	0.15	0.03	0.16	0.00	0.00	22.3
2	360	1200	-290	818	0	-336	748	4.02	4.02	4.02	4.02	2	0.12	0.03	0.13	0.00	0.00	22.3
3	360	930	-226	859	0	-323	726	4.02	4.02	4.02	4.02	2	0.11	0.03	0.14	0.00	0.00	22.3
4	360	1030	-318	655	0	-312	792	4.02	4.02	4.02	4.02	2	0.12	0.02	0.11	0.00	0.00	22.3
5	360	760	-253	696	0	-298	771	4.02	4.02	4.02	4.02	2	0.12	0.02	0.11	0.00	0.00	22.3
6	360	1455	-375	713	0	-344	789	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
7	360	556	-160	850	0	-298	716	4.02	4.02	4.02	4.02	2	0.11	0.03	0.14	0.00	0.00	22.3
8	360	1404	-383	664	0	-337	802	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3

9	360	504	-168	801	0	-290	730	4.02	4.02	4.02	4.02	2	0.11	0.03	0.13	0.00	0.00	22.3
10	360	1200	-290	818	0	-336	748	4.02	4.02	4.02	4.02	2	0.12	0.03	0.13	0.00	0.00	22.3
11	360	930	-226	859	0	-323	726	4.02	4.02	4.02	4.02	2	0.11	0.03	0.14	0.00	0.00	22.3
12	360	1030	-318	655	0	-312	792	4.02	4.02	4.02	4.02	2	0.12	0.02	0.11	0.00	0.00	22.3
13	360	760	-253	696	0	-298	771	4.02	4.02	4.02	4.02	2	0.12	0.02	0.11	0.00	0.00	22.3
14	360	1455	-375	713	0	-344	789	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
15	360	556	-160	850	0	-298	716	4.02	4.02	4.02	4.02	2	0.11	0.03	0.14	0.00	0.00	22.3
16	360	1404	-383	664	0	-337	802	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
17	360	504	-168	801	0	-290	730	4.02	4.02	4.02	4.02	2	0.11	0.03	0.13	0.00	0.00	22.3
18	360	3300	-233	2274	0	-885	827	4.02	4.02	4.02	4.02	3	0.24	0.07	0.37	0.00	0.00	22.3
19	360	2815	-350	1572	0	-715	1041	4.02	4.02	4.02	4.02	3	0.19	0.05	0.25	0.00	0.00	22.3
20	360	3493	-272	1961	0	-680	937	4.02	4.02	4.02	4.02	3	0.18	0.06	0.32	0.00	0.00	22.3
37	360	2876	-214	2201	0	-815	773	4.02	4.02	4.02	4.02	3	0.22	0.07	0.35	0.00	0.00	22.3
38	360	2068	-408	1031	0	-532	1129	4.02	4.02	4.02	4.02	3	0.17	0.03	0.17	0.00	0.00	22.3
39	360	3198	-279	1679	0	-473	956	4.02	4.02	4.02	4.02	3	0.15	0.05	0.27	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	420	1274	-749	984	0	-1003	942	4.02	4.02	4.02	4.02	3	0.26	0.03	0.16	0.00	0.00	22.3
2	420	1200	-594	818	0	-827	700	4.02	4.02	4.02	4.02	2	0.24	0.03	0.13	0.00	0.00	22.3
3	420	930	-530	859	0	-838	723	4.02	4.02	4.02	4.02	2	0.24	0.03	0.14	0.00	0.00	22.3
4	420	1030	-622	655	0	-705	726	4.02	4.02	4.02	4.02	2	0.20	0.02	0.11	0.00	0.00	22.3
5	420	760	-557	696	0	-716	749	4.02	4.02	4.02	4.02	2	0.20	0.02	0.11	0.00	0.00	22.3
6	420	1455	-679	713	0	-772	682	4.02	4.02	4.02	4.02	2	0.22	0.02	0.12	0.00	0.00	22.3
7	420	556	-464	850	0	-808	716	4.02	4.02	4.02	4.02	2	0.23	0.03	0.14	0.00	0.00	22.3
8	420	1404	-687	664	0	-735	690	4.02	4.02	4.02	4.02	2	0.21	0.02	0.12	0.00	0.00	22.3
9	420	504	-472	801	0	-771	730	4.02	4.02	4.02	4.02	2	0.22	0.03	0.13	0.00	0.00	22.3
10	420	1200	-594	818	0	-827	700	4.02	4.02	4.02	4.02	2	0.24	0.03	0.13	0.00	0.00	22.3
11	420	930	-530	859	0	-838	723	4.02	4.02	4.02	4.02	2	0.24	0.03	0.14	0.00	0.00	22.3
12	420	1030	-622	655	0	-705	726	4.02	4.02	4.02	4.02	2	0.20	0.02	0.11	0.00	0.00	22.3
13	420	760	-557	696	0	-716	749	4.02	4.02	4.02	4.02	2	0.20	0.02	0.11	0.00	0.00	22.3
14	420	1455	-679	713	0	-772	682	4.02	4.02	4.02	4.02	2	0.22	0.02	0.12	0.00	0.00	22.3
15	420	556	-464	850	0	-808	716	4.02	4.02	4.02	4.02	2	0.23	0.03	0.14	0.00	0.00	22.3
16	420	1404	-687	664	0	-735	690	4.02	4.02	4.02	4.02	2	0.21	0.02	0.12	0.00	0.00	22.3
17	420	504	-472	801	0	-771	730	4.02	4.02	4.02	4.02	2	0.22	0.03	0.13	0.00	0.00	22.3
18	420	3300	-628	2274	0	-2250	827	4.02	4.02	4.02	4.02	3	0.61	0.07	0.37	0.00	0.00	22.3
19	420	2815	-745	1572	0	-1659	999	4.02	4.02	4.02	4.02	3	0.44	0.05	0.25	0.00	0.00	22.3
20	420	3493	-667	1961	0	-1857	937	4.02	4.02	4.02	4.02	3	0.50	0.06	0.32	0.00	0.00	22.3
37	420	2876	-609	2201	0	-2136	773	4.02	4.02	4.02	4.02	3	0.57	0.07	0.35	0.00	0.00	22.3
38	420	2068	-804	1031	0	-1151	1046	4.02	4.02	4.02	4.02	3	0.30	0.03	0.17	0.00	0.00	22.3
39	420	3198	-674	1679	0	-1480	956	4.02	4.02	4.02	4.02	3	0.40	0.05	0.27	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	480	1274	-1144	984	0	-1593	-585	4.02	4.02	4.02	4.02	3	0.41	0.03	0.20	0.00	0.00	22.3
2	480	1200	-899	818	0	-1318	-504	4.02	4.02	4.02	4.02	2	0.38	0.03	0.16	0.00	0.00	22.3
3	480	930	-835	859	0	-1354	468	4.02	4.02	4.02	4.02	2	0.38	0.03	0.15	0.00	0.00	22.3
4	480	1030	-927	655	0	-1097	-523	4.02	4.02	4.02	4.02	2	0.31	0.03	0.17	0.00	0.00	22.3
5	480	760	-862	696	0	-1133	477	4.02	4.02	4.02	4.02	2	0.32	0.02	0.15	0.00	0.00	22.3
6	480	1455	-984	713	0	-1200	-659	4.02	4.02	4.02	4.02	2	0.35	0.03	0.18	0.00	0.00	22.3
7	480	556	-769	850	0	-1317	543	4.02	4.02	4.02	4.02	2	0.37	0.03	0.14	0.00	0.00	22.3
8	480	1404	-992	664	0	-1134	-664	4.02	4.02	4.02	4.02	2	0.33	0.03	0.18	0.00	0.00	22.3
9	480	504	-777	801	0	-1251	546	4.02	4.02	4.02	4.02	2	0.35	0.03	0.14	0.00	0.00	22.3
10	480	1200	-899	818	0	-1318	-504	4.02	4.02	4.02	4.02	2	0.38	0.03	0.16	0.00	0.00	22.3
11	480	930	-835	859	0	-1354	468	4.02	4.02	4.02	4.02	2	0.38	0.03	0.15	0.00	0.00	22.3
12	480	1030	-927	655	0	-1097	-523	4.02	4.02	4.02	4.02	2	0.31	0.03	0.17	0.00	0.00	22.3
13	480	760	-862	696	0	-1133	477	4.02	4.02	4.02	4.02	2	0.32	0.02	0.15	0.00	0.00	22.3
14	480	1455	-984	713	0	-1200	-659	4.02	4.02	4.02	4.02	2	0.35	0.03	0.18	0.00	0.00	22.3
15	480	556	-769	850	0	-1317	543	4.02	4.02	4.02	4.02	2	0.37	0.03	0.14	0.00	0.00	22.3
16	480	1404	-992	664	0	-1134	-664	4.02	4.02	4.02	4.02	2	0.33	0.03	0.18	0.00	0.00	22.3
17	480	504	-777	801	0	-1251	546	4.02	4.02	4.02	4.02	2	0.35	0.03	0.14	0.00	0.00	22.3
18	480	3300	-1024	2274	0	-3615	570	4.02	4.02	4.02	4.02	3	0.97	0.07	0.37	0.00	0.00	22.3
19	480	2815	-1141	1572	0	-2602	633	4.02	4.02	4.02	4.02	3	0.69	0.05	0.25	0.00	0.00	22.3
20	480	3493	-1063	1961	0	-3033	629	4.02	4.02	4.02	4.02	3	0.82	0.06	0.32	0.00	0.00	22.3
37	480	2876	-1005	2201	0	-3456	541	4.02	4.02	4.02	4.02	3	0.92	0.07	0.35	0.00	0.00	22.3
38	480	2068	-1199	1031	0	-1769	645	4.02	4.02	4.02	4.02	3	0.46	0.03	0.21	0.00	0.00	22.3
39	480	3198	-1070	1679	0	-2488	640	4.02	4.02	4.02	4.02	3	0.67	0.05	0.27	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	540	1274	-1540	984	0	-2184	-1590	4.02	4.02	4.02	4.02	3	0.56	0.04	0.27	0.00	0.00	22.3
2	540	1200	-1203	818	0	-1809	-1289	4.02	4.02	4.02	4.02	2	0.52	0.03	0.21	0.00	0.00	22.3
3	540	930	-1139	859	0	-1870	-1123	4.02	4.02	4.02	4.02	2	0.53	0.03	0.20	0.00	0.00	22.3
4	540	1030	-1231	655	0	-1490	-1324	4.02	4.02	4.02	4.02	2	0.43	0.04	0.22	0.00	0.00	22.3
5	540	760	-1166	696	0	-1550	-1157	4.02	4.02	4.02	4.02	2	0.44	0.03	0.21	0.00	0.00	22.3
6	540	1455	-1288	713	0	-1628	-1495	4.02	4.02	4.02	4.02	2	0.47	0.04	0.23	0.00	0.00	22.3
7	540	556	-1073	850	0	-1827	-941	4.02	4.02	4.02	4.02	2	0.51	0.03	0.19	0.00	0.00	22.3
8	540	1404	-1296	664	0	-1532	-1505	4.02	4.02	4.02	4.02	2	0.44	0.04	0.23	0.00	0.00	22.3
9	540	504	-1081	801	0	-1732	-951	4.02	4.02	4.02	4.02	2	0.49	0.03	0.19	0.00	0.00	22.3
10	540	1200	-1203	818	0	-1809	-1289	4.02	4.02	4.02	4.02	2	0.52	0.03	0.21	0.00	0.00	22.3
11	540	930	-1139	859	0	-1870	-1123	4.02	4.02	4.02	4.02	2	0.53	0.03	0.20	0.00	0.00	22.3
12	540	1030	-1231	655	0	-1490	-1324	4.02	4.02	4.02	4.02	2	0.43	0.04	0.22	0.00	0.00	22.3
13	540	760	-1166	696	0	-1550	-1157	4.02	4.02	4.02	4.02	2	0.44	0.03	0.21	0.00	0.00	22.3
14	540	1455	-1288	713	0	-1628	-1495	4.02	4.02	4.02	4.02	2	0.47	0.04	0.23	0.00	0.00	22.3
15	540	556	-1073	850	0	-1827	-941	4.02	4.02	4.02	4.02	2	0.51	0.03	0.19	0.00	0.00	22.3
16	540	1404	-1296	664	0	-1532	-1505	4.02	4.02	4.02	4.02	2	0.44	0.04	0.23	0.00	0.00	22.3
17	540	504	-1081	801	0	-1732	-951	4.02	4.02	4.02	4.02	2	0.49	0.03	0.19	0.00	0.00	22.3
18	540	3300	-1419	2274	0	-4979	-1400	4.02	6.03	4.02	4.02	3	0.93	0.07	0.37	0.00	0.00	22.3
19	540	2815	-1536	1572	0	-3546	-1525	4.02	4.02	4.02	4.02	3	0.94	0.05	0.27	0.00	0.00	22.3
20	540	3493	-1458	1961	0	-4210	-1404	4.02	6.03	4.02	4.02	3	0.79	0.06	0.32	0.00	0.00	22.3
37	540	2876	-1400	2201	0	-4777	-1398	4.02	6.03	4.02	4.02	3	0.88	0.07	0.35	0.00	0.00	22.3
38	540	2068	-1595	1031	0	-2388	-1608	4.02	4.02	4.02	4.02	3	0.62	0.05	0.28	0.00	0.00	22.3
39	540	3198	-1465	1679	0	-3495	-1404	4.02	4.02	4.02	4.02	3	0.94	0.05	0.27	0.00	0.00	22.3

apost= -- aant= 2.01 ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	600	1274	-1935	984	0	-2774	-1853	4.02	4.02	4.02	4.02	3	0.71	0.06	0.34	0.00	0.00	22.3
2	600	1200	-1507	818	0	-2300	-1493	4.02	4.02	4.02	4.02	2	0.66	0.04	0.27	0.00	0.00	22.3
3	600	930	-1443	859	0	-2385	-1321	4.02	4.02	4.02	4.02	2	0.68	0.04	0.26	0.00	0.00	22.3
4	600	1030	-1535	655	0	-1883	-1530	4.02	4.02	4.02	4.02	2	0.54	0.04	0.27	0.00	0.00	22.3
5	600	760	-1470	696	0	-1968	-1358	4.02	4.02	4.02	4.02	2	0.56	0.04	0.26	0.00	0.00	22.3
6	600	1455	-1592	713	0	-2056	-1707	4.02	4.02	4.02	4.02	2	0.59	0.05	0.28	0.00	0.00	22.3
7	600	556	-1377	850	0	-2337	-1133	4.02	4.02	4.02	4.02	2	0.66	0.04	0.25	0.00	0.00	22.3
8	600	1404	-1600	664	0	-1931	-1718	4.02	4.02	4.02	4.02	2	0.56	0.05	0.28	0.00	0.00	22.3
9	600	504	-1385	801	0	-2212	-1144	4.02	4.02	4.02	4.02	2	0.62	0.04	0.25	0.00	0.00	22.3
10	600	1200	-1507	818	0	-2300	-1493	4.02	4.02	4.02	4.02	2	0.66	0.04	0.27	0.00	0.00	22.3
11	600	930	-1443	859	0	-2385	-1321	4.02	4.02	4.02	4.02	2	0.68	0.04	0.26	0.00	0.00	22.3
12	600	1030	-1535	655	0	-1883	-1530	4.02	4.02	4.02	4.02	2	0.54	0.04	0.27	0.00	0.00	22.3
13	600	760	-1470	696	0	-1968	-1358	4.02	4.02	4.02	4.02	2	0.56	0.04	0.26	0.00	0.00	22.3
14	600	1455	-1592	713	0	-2056	-1707	4.02	4.02	4.02	4.02	2	0.59	0.05	0.28	0.00	0.00	22.3

15	600	556	-1377	850	0	-2337	-1133	4.02	4.02	4.02	4.02	2	0.66	0.04	0.25	0.00	0.00	22.3
16	600	1404	-1600	664	0	-1931	-1718	4.02	4.02	4.02	4.02	2	0.56	0.05	0.28	0.00	0.00	22.3
17	600	504	-1385	801	0	-2212	-1144	4.02	4.02	4.02	4.02	2	0.62	0.04	0.25	0.00	0.00	22.3
18	600	3300	-1815	2274	0	-6344	-1652	4.02	8.04	4.02	4.02	3	0.90	0.07	0.37	0.00	0.00	22.3
19	600	2815	-1932	1572	0	-4489	-1788	4.02	6.03	4.02	4.02	3	0.83	0.06	0.34	0.00	0.00	22.3
20	600	3493	-1854	1961	0	-5386	-1659	4.02	8.04	4.02	4.02	3	0.77	0.06	0.33	0.00	0.00	22.3
37	600	2876	-1796	2201	0	-6098	-1648	4.02	8.04	4.02	4.02	3	0.86	0.07	0.35	0.00	0.00	22.3
38	600	2068	-1990	1031	0	-3007	-1876	4.02	4.02	4.02	4.02	3	0.78	0.06	0.35	0.00	0.00	22.3
39	600	3198	-1861	1679	0	-4502	-1660	4.02	6.03	4.02	4.02	3	0.84	0.05	0.33	0.00	0.00	22.3

apost= -- aant= 4.02 ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

Nome travata: **Trave_404_IP1** Descrizione: **Trave_4 32-25**
ASTA NUM. 16 NI 254 NF 255 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y Permanente qy tot.
qy medio: 375.00 132.00 507.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	1757	1974	744	0	2026	-1953	4.02	4.02	4.02	4.02	3	0.52	0.06	0.35	0.00	0.00	22.3
2	0	1523	1498	661	0	1801	-1438	4.02	4.02	4.02	4.02	2	0.52	0.04	0.27	0.00	0.00	22.3
3	0	1247	1553	698	0	1914	-1599	4.02	4.02	4.02	4.02	2	0.55	0.05	0.28	0.00	0.00	22.3
4	0	1456	1484	448	0	1202	-1405	4.02	4.02	4.02	4.02	2	0.35	0.04	0.26	0.00	0.00	22.3
5	0	1180	1539	485	0	1316	-1566	4.02	4.02	4.02	4.02	2	0.38	0.04	0.27	0.00	0.00	22.3
6	0	1820	1429	542	0	1458	-1239	4.02	4.02	4.02	4.02	2	0.43	0.04	0.25	0.00	0.00	22.3
7	0	903	1612	667	0	1838	-1775	4.02	4.02	4.02	4.02	2	0.52	0.05	0.29	0.00	0.00	22.3
8	0	1800	1425	478	0	1279	-1229	4.02	4.02	4.02	4.02	2	0.37	0.04	0.25	0.00	0.00	22.3
9	0	882	1608	603	0	1658	-1765	4.02	4.02	4.02	4.02	2	0.47	0.05	0.29	0.00	0.00	22.3
10	0	1523	1498	661	0	1801	-1438	4.02	4.02	4.02	4.02	2	0.52	0.04	0.27	0.00	0.00	22.3
11	0	1247	1553	698	0	1914	-1599	4.02	4.02	4.02	4.02	2	0.55	0.05	0.28	0.00	0.00	22.3
12	0	1456	1484	448	0	1202	-1405	4.02	4.02	4.02	4.02	2	0.35	0.04	0.26	0.00	0.00	22.3
13	0	1180	1539	485	0	1316	-1566	4.02	4.02	4.02	4.02	2	0.38	0.04	0.27	0.00	0.00	22.3
14	0	1820	1429	542	0	1458	-1239	4.02	4.02	4.02	4.02	2	0.43	0.04	0.25	0.00	0.00	22.3
15	0	903	1612	667	0	1838	-1775	4.02	4.02	4.02	4.02	2	0.52	0.05	0.29	0.00	0.00	22.3
16	0	1800	1425	478	0	1279	-1229	4.02	4.02	4.02	4.02	2	0.37	0.04	0.25	0.00	0.00	22.3
17	0	882	1608	603	0	1658	-1765	4.02	4.02	4.02	4.02	2	0.47	0.05	0.29	0.00	0.00	22.3
18	0	4056	2002	1831	0	5001	-2015	6.03	4.02	4.02	4.02	3	0.94	0.06	0.36	0.00	0.00	22.3
19	0	3576	1944	1026	0	2775	-1860	4.02	4.02	4.02	4.02	3	0.75	0.06	0.35	0.00	0.00	22.3
20	0	3774	2052	1395	0	3806	-2164	6.03	4.02	4.02	4.02	3	0.71	0.06	0.37	0.00	0.00	22.3
37	0	3542	2022	1877	0	5137	-2072	6.03	4.02	4.02	4.02	3	0.96	0.06	0.36	0.00	0.00	22.3
38	0	2740	1926	535	0	1428	-1815	4.02	4.02	4.02	4.02	3	0.38	0.06	0.34	0.00	0.00	22.3
39	0	3070	2106	1151	0	3147	-2322	4.02	4.02	4.02	4.02	3	0.84	0.06	0.38	0.00	0.00	22.3

apost= 2.01 aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	60	1757	1578	744	0	1579	-1686	4.02	4.02	4.02	4.02	3	0.41	0.05	0.28	0.00	0.00	22.3
2	60	1523	1194	661	0	1405	-1235	4.02	4.02	4.02	4.02	2	0.41	0.03	0.21	0.00	0.00	22.3
3	60	1247	1249	698	0	1495	-1391	4.02	4.02	4.02	4.02	2	0.43	0.04	0.22	0.00	0.00	22.3
4	60	1456	1180	448	0	934	-1203	4.02	4.02	4.02	4.02	2	0.27	0.03	0.21	0.00	0.00	22.3
5	60	1180	1235	485	0	1025	-1359	4.02	4.02	4.02	4.02	2	0.29	0.04	0.22	0.00	0.00	22.3
6	60	1820	1125	542	0	1133	-1042	4.02	4.02	4.02	4.02	2	0.33	0.03	0.20	0.00	0.00	22.3
7	60	903	1308	667	0	1438	-1561	4.02	4.02	4.02	4.02	2	0.41	0.04	0.23	0.00	0.00	22.3
8	60	1800	1121	478	0	992	-1033	4.02	4.02	4.02	4.02	2	0.29	0.03	0.20	0.00	0.00	22.3
9	60	882	1304	603	0	1296	-1552	4.02	4.02	4.02	4.02	2	0.37	0.04	0.23	0.00	0.00	22.3
10	60	1523	1194	661	0	1405	-1235	4.02	4.02	4.02	4.02	2	0.41	0.03	0.21	0.00	0.00	22.3
11	60	1247	1249	698	0	1495	-1391	4.02	4.02	4.02	4.02	2	0.43	0.04	0.22	0.00	0.00	22.3
12	60	1456	1180	448	0	934	-1203	4.02	4.02	4.02	4.02	2	0.27	0.03	0.21	0.00	0.00	22.3
13	60	1180	1235	485	0	1025	-1359	4.02	4.02	4.02	4.02	2	0.29	0.04	0.22	0.00	0.00	22.3
14	60	1820	1125	542	0	1133	-1042	4.02	4.02	4.02	4.02	2	0.33	0.03	0.20	0.00	0.00	22.3
15	60	903	1308	667	0	1438	-1561	4.02	4.02	4.02	4.02	2	0.41	0.04	0.23	0.00	0.00	22.3
16	60	1800	1121	478	0	992	-1033	4.02	4.02	4.02	4.02	2	0.29	0.03	0.20	0.00	0.00	22.3
17	60	882	1304	603	0	1296	-1552	4.02	4.02	4.02	4.02	2	0.37	0.04	0.23	0.00	0.00	22.3
18	60	4056	1606	1831	0	3902	-1746	6.03	4.02	4.02	4.02	3	0.74	0.06	0.29	0.00	0.00	22.3
19	60	3576	1549	1026	0	2159	-1596	4.02	4.02	4.02	4.02	3	0.59	0.04	0.28	0.00	0.00	22.3
20	60	3774	1657	1395	0	2969	-1890	4.02	4.02	4.02	4.02	3	0.81	0.05	0.30	0.00	0.00	22.3
37	60	3542	1626	1877	0	4011	-1801	6.03	4.02	4.02	4.02	3	0.75	0.06	0.30	0.00	0.00	22.3
38	60	2740	1530	535	0	1107	-1553	4.02	4.02	4.02	4.02	3	0.29	0.04	0.27	0.00	0.00	22.3
39	60	3070	1710	1151	0	2457	-2043	4.02	4.02	4.02	4.02	3	0.66	0.05	0.30	0.00	0.00	22.3

apost= 2.01 aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	120	1757	1183	744	0	1133	-657	4.02	4.02	4.02	4.02	3	0.29	0.03	0.21	0.00	0.00	22.3
2	120	1523	890	661	0	1008	-456	4.02	4.02	4.02	4.02	2	0.29	0.03	0.16	0.00	0.00	22.3
3	120	1247	945	698	0	1077	-579	4.02	4.02	4.02	4.02	2	0.31	0.03	0.17	0.00	0.00	22.3
4	120	1456	876	448	0	665	454	4.02	4.02	4.02	4.02	2	0.19	0.03	0.16	0.00	0.00	22.3
5	120	1180	931	485	0	734	-555	4.02	4.02	4.02	4.02	2	0.21	0.03	0.17	0.00	0.00	22.3
6	120	1820	821	542	0	807	526	4.02	4.02	4.02	4.02	2	0.24	0.02	0.15	0.00	0.00	22.3
7	120	903	1004	667	0	1038	-714	4.02	4.02	4.02	4.02	2	0.29	0.03	0.18	0.00	0.00	22.3
8	120	1800	817	478	0	705	529	4.02	4.02	4.02	4.02	2	0.21	0.02	0.15	0.00	0.00	22.3
9	120	882	1000	603	0	935	-707	4.02	4.02	4.02	4.02	2	0.27	0.03	0.18	0.00	0.00	22.3
10	120	1523	890	661	0	1008	-456	4.02	4.02	4.02	4.02	2	0.29	0.03	0.16	0.00	0.00	22.3
11	120	1247	945	698	0	1077	-579	4.02	4.02	4.02	4.02	2	0.31	0.03	0.17	0.00	0.00	22.3
12	120	1456	876	448	0	665	454	4.02	4.02	4.02	4.02	2	0.19	0.03	0.16	0.00	0.00	22.3
13	120	1180	931	485	0	734	-555	4.02	4.02	4.02	4.02	2	0.21	0.03	0.17	0.00	0.00	22.3
14	120	1820	821	542	0	807	526	4.02	4.02	4.02	4.02	2	0.24	0.02	0.15	0.00	0.00	22.3
15	120	903	1004	667	0	1038	-714	4.02	4.02	4.02	4.02	2	0.29	0.03	0.18	0.00	0.00	22.3
16	120	1800	817	478	0	705	529	4.02	4.02	4.02	4.02	2	0.21	0.02	0.15	0.00	0.00	22.3
17	120	882	1000	603	0	935	-707	4.02	4.02	4.02	4.02	2	0.27	0.03	0.18	0.00	0.00	22.3
18	120	4056	1211	1831	0	2803	-700	4.02	4.02	4.02	4.02	3	0.77	0.06	0.29	0.00	0.00	22.3
19	120	3576	1153	1026	0	1544	-585	4.02	4.02	4.02	4.02	3	0.42	0.03	0.21	0.00	0.00	22.3
20	120	3774	1261	1395	0	2132	-814	4.02	4.02	4.02	4.02	3	0.58	0.04	0.22	0.00	0.00	22.3
37	120	3542	1231	1877	0	2885	-744	4.02	4.02	4.02	4.02	3	0.78	0.06	0.30	0.00	0.00	22.3
38	120	2740	1135	535	0	786	596	4.02	4.02	4.02	4.02	3	0.21	0.03	0.20	0.00	0.00	22.3
39	120	3070	1315	1151	0	1766	-935	4.02	4.02	4.02	4.02	3	0.47	0.04	0.23	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	180	1757	788	744	0	686	931	4.02	4.02	4.02	4.02	3	0.18	0.02	0.14	0.00	0.00	22.3
2	180	1523	585	661	0	612	733	4.02	4.02	4.02	4.02	2	0.18	0.02	0.11	0.00	0.00	22.3
3	180	1247	640	698	0	658	699	4.02	4.02	4.02	4.02	2	0.19	0.02	0.11	0.00	0.00	22.3
4	180	1456	571	448	0	397	734	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
5	180	1180	626	485	0	443	700	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
6	180	1820	516	542	0	482	767	4.02	4.02	4.02	4.02	2	0.14	0.02	0.09	0.00	0.00	22.3

7	180	903	699	667	0	638	659	4.02	4.02	4.02	4.02	2	0.18	0.02	0.12	0.00	0.00	22.3
8	180	1800	512	478	0	418	765	4.02	4.02	4.02	4.02	2	0.12	0.01	0.09	0.00	0.00	22.3
9	180	882	695	603	0	573	660	4.02	4.02	4.02	4.02	2	0.16	0.02	0.12	0.00	0.00	22.3
10	180	1523	585	661	0	612	733	4.02	4.02	4.02	4.02	2	0.18	0.02	0.11	0.00	0.00	22.3
11	180	1247	640	698	0	658	699	4.02	4.02	4.02	4.02	2	0.19	0.02	0.11	0.00	0.00	22.3
12	180	1456	571	448	0	397	734	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
13	180	1180	626	485	0	443	700	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
14	180	1820	516	542	0	482	767	4.02	4.02	4.02	4.02	2	0.14	0.02	0.09	0.00	0.00	22.3
15	180	903	699	667	0	638	659	4.02	4.02	4.02	4.02	2	0.18	0.02	0.12	0.00	0.00	22.3
16	180	1800	512	478	0	418	765	4.02	4.02	4.02	4.02	2	0.12	0.01	0.09	0.00	0.00	22.3
17	180	882	695	603	0	573	660	4.02	4.02	4.02	4.02	2	0.16	0.02	0.12	0.00	0.00	22.3
18	180	4056	816	1831	0	1705	933	4.02	4.02	4.02	4.02	3	0.47	0.06	0.29	0.00	0.00	22.3
19	180	3576	758	1026	0	928	956	4.02	4.02	4.02	4.02	3	0.25	0.03	0.17	0.00	0.00	22.3
20	180	3774	866	1395	0	1294	900	4.02	4.02	4.02	4.02	3	0.35	0.04	0.22	0.00	0.00	22.3
37	180	3542	836	1877	0	1758	922	4.02	4.02	4.02	4.02	3	0.48	0.06	0.30	0.00	0.00	22.3
38	180	2740	740	535	0	464	958	4.02	4.02	4.02	4.02	3	0.15	0.02	0.13	0.00	0.00	22.3
39	180	3070	920	1151	0	1076	866	4.02	4.02	4.02	4.02	3	0.29	0.04	0.19	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	240	1757	392	744	0	239	1003	4.02	4.02	4.02	4.02	3	0.15	0.02	0.12	0.00	0.00	22.3
2	240	1523	281	661	0	215	774	4.02	4.02	4.02	4.02	2	0.12	0.02	0.11	0.00	0.00	22.3
3	240	1247	336	698	0	239	778	4.02	4.02	4.02	4.02	2	0.12	0.02	0.11	0.00	0.00	22.3
4	240	1456	267	448	0	128	766	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
5	240	1180	322	485	0	152	770	4.02	4.02	4.02	4.02	2	0.12	0.02	0.08	0.00	0.00	22.3
6	240	1820	212	542	0	156	767	4.02	4.02	4.02	4.02	2	0.12	0.02	0.09	0.00	0.00	22.3
7	240	903	395	667	0	238	779	4.02	4.02	4.02	4.02	2	0.12	0.02	0.11	0.00	0.00	22.3
8	240	1800	208	478	0	131	765	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
9	240	882	391	603	0	211	777	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
10	240	1523	281	661	0	215	774	4.02	4.02	4.02	4.02	2	0.12	0.02	0.11	0.00	0.00	22.3
11	240	1247	336	698	0	239	778	4.02	4.02	4.02	4.02	2	0.12	0.02	0.11	0.00	0.00	22.3
12	240	1456	267	448	0	128	766	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
13	240	1180	322	485	0	152	770	4.02	4.02	4.02	4.02	2	0.12	0.02	0.08	0.00	0.00	22.3
14	240	1820	212	542	0	156	767	4.02	4.02	4.02	4.02	2	0.12	0.02	0.09	0.00	0.00	22.3
15	240	903	395	667	0	238	779	4.02	4.02	4.02	4.02	2	0.12	0.02	0.11	0.00	0.00	22.3
16	240	1800	208	478	0	131	765	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
17	240	882	391	603	0	211	777	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
18	240	4056	420	1831	0	606	1024	4.02	4.02	4.02	4.02	3	0.17	0.06	0.29	0.00	0.00	22.3
19	240	3576	362	1026	0	312	1007	4.02	4.02	4.02	4.02	3	0.16	0.03	0.17	0.00	0.00	22.3
20	240	3774	470	1395	0	457	1026	4.02	4.02	4.02	4.02	3	0.17	0.04	0.22	0.00	0.00	22.3
37	240	3542	440	1877	0	632	1026	4.02	4.02	4.02	4.02	3	0.17	0.06	0.30	0.00	0.00	22.3
38	240	2740	344	535	0	143	997	4.02	4.02	4.02	4.02	3	0.16	0.02	0.09	0.00	0.00	22.3
39	240	3070	524	1151	0	385	1029	4.02	4.02	4.02	4.02	3	0.16	0.04	0.19	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	300	1757	-4	744	0	-207	1003	4.02	4.02	4.02	4.02	3	0.15	0.02	0.12	0.00	0.00	22.3
2	300	1523	-23	661	0	-181	774	4.02	4.02	4.02	4.02	2	0.12	0.02	0.11	0.00	0.00	22.3
3	300	1247	32	698	0	-179	778	4.02	4.02	4.02	4.02	2	0.12	0.02	0.11	0.00	0.00	22.3
4	300	1456	-37	448	0	-140	766	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
5	300	1180	18	485	0	-138	770	4.02	4.02	4.02	4.02	2	0.12	0.02	0.08	0.00	0.00	22.3
6	300	1820	-92	542	0	-169	767	4.02	4.02	4.02	4.02	2	0.12	0.02	0.09	0.00	0.00	22.3
7	300	903	91	667	0	-162	779	4.02	4.02	4.02	4.02	2	0.12	0.02	0.11	0.00	0.00	22.3
8	300	1800	-96	478	0	-156	765	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
9	300	882	87	603	0	-150	777	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
10	300	1523	-23	661	0	-181	774	4.02	4.02	4.02	4.02	2	0.12	0.02	0.11	0.00	0.00	22.3
11	300	1247	32	698	0	-179	778	4.02	4.02	4.02	4.02	2	0.12	0.02	0.11	0.00	0.00	22.3
12	300	1456	-37	448	0	-140	766	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
13	300	1180	18	485	0	-138	770	4.02	4.02	4.02	4.02	2	0.12	0.02	0.08	0.00	0.00	22.3
14	300	1820	-92	542	0	-169	767	4.02	4.02	4.02	4.02	2	0.12	0.02	0.09	0.00	0.00	22.3
15	300	903	91	667	0	-162	779	4.02	4.02	4.02	4.02	2	0.12	0.02	0.11	0.00	0.00	22.3
16	300	1800	-96	478	0	-156	765	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
17	300	882	87	603	0	-150	777	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
18	300	4056	24	1831	0	-493	1024	4.02	4.02	4.02	4.02	3	0.17	0.06	0.29	0.00	0.00	22.3
19	300	3576	-33	1026	0	-303	1007	4.02	4.02	4.02	4.02	3	0.16	0.03	0.17	0.00	0.00	22.3
20	300	3774	75	1395	0	-380	1026	4.02	4.02	4.02	4.02	3	0.17	0.04	0.22	0.00	0.00	22.3
37	300	3542	44	1877	0	-494	1026	4.02	4.02	4.02	4.02	3	0.16	0.06	0.30	0.00	0.00	22.3
38	300	2740	-52	535	0	-178	997	4.02	4.02	4.02	4.02	3	0.16	0.02	0.09	0.00	0.00	22.3
39	300	3070	128	1151	0	-305	1029	4.02	4.02	4.02	4.02	3	0.16	0.04	0.19	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	360	1757	-399	744	0	-654	1003	4.02	4.02	4.02	4.02	3	0.17	0.02	0.12	0.00	0.00	22.3
2	360	1523	-327	661	0	-577	774	4.02	4.02	4.02	4.02	2	0.17	0.02	0.11	0.00	0.00	22.3
3	360	1247	-272	698	0	-598	778	4.02	4.02	4.02	4.02	2	0.17	0.02	0.11	0.00	0.00	22.3
4	360	1456	-341	448	0	-408	766	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
5	360	1180	-286	485	0	-429	770	4.02	4.02	4.02	4.02	2	0.12	0.02	0.08	0.00	0.00	22.3
6	360	1820	-396	542	0	-494	767	4.02	4.02	4.02	4.02	2	0.14	0.02	0.09	0.00	0.00	22.3
7	360	903	-213	667	0	-563	779	4.02	4.02	4.02	4.02	2	0.16	0.02	0.11	0.00	0.00	22.3
8	360	1800	-400	478	0	-444	765	4.02	4.02	4.02	4.02	2	0.13	0.01	0.08	0.00	0.00	22.3
9	360	882	-217	603	0	-512	777	4.02	4.02	4.02	4.02	2	0.15	0.02	0.10	0.00	0.00	22.3
10	360	1523	-327	661	0	-577	774	4.02	4.02	4.02	4.02	2	0.17	0.02	0.11	0.00	0.00	22.3
11	360	1247	-272	698	0	-598	778	4.02	4.02	4.02	4.02	2	0.17	0.02	0.11	0.00	0.00	22.3
12	360	1456	-341	448	0	-408	766	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
13	360	1180	-286	485	0	-429	770	4.02	4.02	4.02	4.02	2	0.12	0.02	0.08	0.00	0.00	22.3
14	360	1820	-396	542	0	-494	767	4.02	4.02	4.02	4.02	2	0.14	0.02	0.09	0.00	0.00	22.3
15	360	903	-213	667	0	-563	779	4.02	4.02	4.02	4.02	2	0.16	0.02	0.11	0.00	0.00	22.3
16	360	1800	-400	478	0	-444	765	4.02	4.02	4.02	4.02	2	0.13	0.01	0.08	0.00	0.00	22.3
17	360	882	-217	603	0	-512	777	4.02	4.02	4.02	4.02	2	0.15	0.02	0.10	0.00	0.00	22.3
18	360	4056	-371	1831	0	-1592	1024	4.02	4.02	4.02	4.02	3	0.44	0.06	0.29	0.00	0.00	22.3
19	360	3576	-428	1026	0	-919	1007	4.02	4.02	4.02	4.02	3	0.25	0.03	0.17	0.00	0.00	22.3
20	360	3774	-320	1395	0	-1217	1026	4.02	4.02	4.02	4.02	3	0.33	0.04	0.22	0.00	0.00	22.3
37	360	3542	-351	1877	0	-1620	1026	4.02	4.02	4.02	4.02	3	0.44	0.06	0.30	0.00	0.00	22.3
38	360	2740	-447	535	0	-499	997	4.02	4.02	4.02	4.02	3	0.16	0.02	0.09	0.00	0.00	22.3
39	360	3070	-267	1151	0	-995	1029	4.02	4.02	4.02	4.02	3	0.27	0.04	0.19	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	420	1757	-794	744	0	-1101	927	4.02	4.02	4.02	4.02	3	0.28	0.02	0.14	0.00	0.00	22.3
2	420	1523	-631	661	0	-974	701	4.02	4.02	4.02	4.02	2	0.28	0.02	0.11	0.00	0.00	22.3
3	420	1247	-576	698	0	-1017	742	4.02	4.02	4.02	4.02	2	0.29	0.02	0.11	0.00	0.00	22.3
4	420	1456	-645	448	0	-677	683	4.02	4.02	4.02	4.02	2	0.20	0.02	0.11	0.00	0.00	22.3
5	420	1180	-590	485	0	-720	725	4.02	4.02	4.02	4.02	2	0.21	0.02	0.11	0.00	0.00	22.3
6	420	1820	-700	542	0	-820	646	4.02	4.02	4.02	4.02	2	0.24	0.02	0.12	0.00	0.00	22.3
7	420	903	-517	667	0	-963	779	4.02	4.02	4.02	4.02	2	0.27	0.02	0.11	0.00	0.00	22.3
8	420	1800	-704	478	0	-731	641	4.02	4.02	4.02	4.02	2	0.21	0.02	0.13	0.00	0.00	22.3
9	420	882	-521	603	0	-874	777	4.02	4.02	4.02	4.02	2	0.25	0.02	0.10	0.00	0.00	22.3
10	420	1523	-631	661	0	-974	701	4.02	4.02	4.02	4.02	2	0.28	0.02	0.11	0.00	0.00	22.3
11	420	1247	-576	698	0	-1017	742	4.02	4.02	4.02	4.02	2	0.29	0.02	0.11	0.00	0.00	22.3
12	420	1456	-645	448	0	-677	683	4.02	4.02	4.02	4.02	2	0.20	0.02	0.11	0.00	0.00	22.3

13	420	1180	-590	485	0	-720	725	4.02	4.02	4.02	4.02	2	0.21	0.02	0.11	0.00	0.00	22.3
14	420	1820	-700	542	0	-820	646	4.02	4.02	4.02	4.02	2	0.24	0.02	0.12	0.00	0.00	22.3
15	420	903	-517	667	0	-963	779	4.02	4.02	4.02	4.02	2	0.27	0.02	0.11	0.00	0.00	22.3
16	420	1800	-704	478	0	-731	641	4.02	4.02	4.02	4.02	2	0.21	0.02	0.13	0.00	0.00	22.3
17	420	882	-521	603	0	-874	777	4.02	4.02	4.02	4.02	2	0.25	0.02	0.10	0.00	0.00	22.3
18	420	4056	-766	1831	0	-2691	967	4.02	4.02	4.02	4.02	3	0.74	0.06	0.29	0.00	0.00	22.3
19	420	3576	-824	1026	0	-1535	910	4.02	4.02	4.02	4.02	3	0.42	0.03	0.17	0.00	0.00	22.3
20	420	3774	-716	1395	0	-2054	1004	4.02	4.02	4.02	4.02	3	0.56	0.04	0.22	0.00	0.00	22.3
37	420	3542	-746	1877	0	-2746	983	4.02	4.02	4.02	4.02	3	0.74	0.06	0.30	0.00	0.00	22.3
38	420	2740	-842	535	0	-820	887	4.02	4.02	4.02	4.02	3	0.22	0.02	0.15	0.00	0.00	22.3
39	420	3070	-662	1151	0	-1686	1029	4.02	4.02	4.02	4.02	3	0.45	0.04	0.19	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	480	1757	-1190	744	0	-1548	-672	4.02	4.02	4.02	4.02	3	0.40	0.03	0.21	0.00	0.00	22.3
2	480	1523	-936	661	0	-1370	-563	4.02	4.02	4.02	4.02	2	0.40	0.03	0.17	0.00	0.00	22.3
3	480	1247	-881	698	0	-1436	459	4.02	4.02	4.02	4.02	2	0.41	0.03	0.16	0.00	0.00	22.3
4	480	1456	-950	448	0	-945	-602	4.02	4.02	4.02	4.02	2	0.27	0.03	0.17	0.00	0.00	22.3
5	480	1180	-895	485	0	-1011	-472	4.02	4.02	4.02	4.02	2	0.29	0.03	0.16	0.00	0.00	22.3
6	480	1820	-1005	542	0	-1145	-728	4.02	4.02	4.02	4.02	2	0.34	0.03	0.18	0.00	0.00	22.3
7	480	903	-822	667	0	-1363	537	4.02	4.02	4.02	4.02	2	0.39	0.02	0.15	0.00	0.00	22.3
8	480	1800	-1009	479	0	-1018	-740	4.02	4.02	4.02	4.02	2	0.30	0.03	0.18	0.00	0.00	22.3
9	480	882	-826	603	0	-1236	529	4.02	4.02	4.02	4.02	2	0.35	0.02	0.15	0.00	0.00	22.3
10	480	1523	-936	661	0	-1370	-563	4.02	4.02	4.02	4.02	2	0.40	0.03	0.17	0.00	0.00	22.3
11	480	1247	-881	698	0	-1436	459	4.02	4.02	4.02	4.02	2	0.41	0.03	0.16	0.00	0.00	22.3
12	480	1456	-950	448	0	-945	-602	4.02	4.02	4.02	4.02	2	0.27	0.03	0.17	0.00	0.00	22.3
13	480	1180	-895	485	0	-1011	-472	4.02	4.02	4.02	4.02	2	0.29	0.03	0.16	0.00	0.00	22.3
14	480	1820	-1005	542	0	-1145	-728	4.02	4.02	4.02	4.02	2	0.34	0.03	0.18	0.00	0.00	22.3
15	480	903	-822	667	0	-1363	537	4.02	4.02	4.02	4.02	2	0.39	0.02	0.15	0.00	0.00	22.3
16	480	1800	-1009	479	0	-1018	-740	4.02	4.02	4.02	4.02	2	0.30	0.03	0.18	0.00	0.00	22.3
17	480	882	-826	603	0	-1236	529	4.02	4.02	4.02	4.02	2	0.35	0.02	0.15	0.00	0.00	22.3
18	480	4056	-1162	1831	0	-3789	589	4.02	6.03	4.02	4.02	3	0.72	0.06	0.29	0.00	0.00	22.3
19	480	3576	-1219	1026	0	-2151	-737	4.02	4.02	4.02	4.02	3	0.58	0.04	0.22	0.00	0.00	22.3
20	480	3774	-1111	1395	0	-2892	656	4.02	4.02	4.02	4.02	3	0.79	0.04	0.22	0.00	0.00	22.3
37	480	3542	-1142	1877	0	-3873	616	4.02	6.03	4.02	4.02	3	0.72	0.06	0.30	0.00	0.00	22.3
38	480	2740	-1238	535	0	-1142	-790	4.02	4.02	4.02	4.02	3	0.30	0.04	0.22	0.00	0.00	22.3
39	480	3070	-1058	1151	0	-2376	729	4.02	4.02	4.02	4.02	3	0.64	0.04	0.19	0.00	0.00	22.3

apost= -- aant= 2.01 ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	540	1757	-1585	744	0	-1994	-1705	4.02	4.02	4.02	4.02	3	0.51	0.05	0.28	0.00	0.00	22.3
2	540	1523	-1240	661	0	-1767	-1369	4.02	4.02	4.02	4.02	2	0.51	0.04	0.22	0.00	0.00	22.3
3	540	1247	-1185	698	0	-1854	-1206	4.02	4.02	4.02	4.02	2	0.53	0.03	0.21	0.00	0.00	22.3
4	540	1456	-1254	448	0	-1214	-1417	4.02	4.02	4.02	4.02	2	0.35	0.04	0.22	0.00	0.00	22.3
5	540	1180	-1199	485	0	-1302	-1254	4.02	4.02	4.02	4.02	2	0.37	0.03	0.21	0.00	0.00	22.3
6	540	1820	-1309	542	0	-1471	-1576	4.02	4.02	4.02	4.02	2	0.43	0.04	0.23	0.00	0.00	22.3
7	540	903	-1126	667	0	-1763	-1033	4.02	4.02	4.02	4.02	2	0.50	0.03	0.20	0.00	0.00	22.3
8	540	1800	-1313	478	0	-1305	-1591	4.02	4.02	4.02	4.02	2	0.38	0.04	0.23	0.00	0.00	22.3
9	540	882	-1130	603	0	-1597	-1048	4.02	4.02	4.02	4.02	2	0.45	0.03	0.20	0.00	0.00	22.3
10	540	1523	-1240	661	0	-1767	-1369	4.02	4.02	4.02	4.02	2	0.51	0.04	0.22	0.00	0.00	22.3
11	540	1247	-1185	698	0	-1854	-1206	4.02	4.02	4.02	4.02	2	0.53	0.03	0.21	0.00	0.00	22.3
12	540	1456	-1254	448	0	-1214	-1417	4.02	4.02	4.02	4.02	2	0.35	0.04	0.22	0.00	0.00	22.3
13	540	1180	-1199	485	0	-1302	-1254	4.02	4.02	4.02	4.02	2	0.37	0.03	0.21	0.00	0.00	22.3
14	540	1820	-1309	542	0	-1471	-1576	4.02	4.02	4.02	4.02	2	0.43	0.04	0.23	0.00	0.00	22.3
15	540	903	-1126	667	0	-1763	-1033	4.02	4.02	4.02	4.02	2	0.50	0.03	0.20	0.00	0.00	22.3
16	540	1800	-1313	478	0	-1305	-1591	4.02	4.02	4.02	4.02	2	0.38	0.04	0.23	0.00	0.00	22.3
17	540	882	-1130	603	0	-1597	-1048	4.02	4.02	4.02	4.02	2	0.45	0.03	0.20	0.00	0.00	22.3
18	540	4056	-1557	1831	0	-4888	-1603	4.02	6.03	4.02	4.02	3	0.92	0.06	0.29	0.00	0.00	22.3
19	540	3576	-1615	1026	0	-2766	-1788	4.02	4.02	4.02	4.02	3	0.75	0.05	0.29	0.00	0.00	22.3
20	540	3774	-1507	1395	0	-3729	-1455	4.02	6.03	4.02	4.02	3	0.70	0.04	0.27	0.00	0.00	22.3
37	540	3542	-1537	1877	0	-4999	-1544	4.02	6.03	4.02	4.02	3	0.93	0.06	0.30	0.00	0.00	22.3
38	540	2740	-1633	535	0	-1463	-1851	4.02	4.02	4.02	4.02	3	0.39	0.05	0.29	0.00	0.00	22.3
39	540	3070	-1453	1151	0	-3067	-1296	4.02	4.02	4.02	4.02	3	0.82	0.04	0.26	0.00	0.00	22.3

apost= -- aant= 2.01 ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	600	1757	-1981	744	0	-2441	-1972	4.02	4.02	4.02	4.02	3	0.63	0.06	0.35	0.00	0.00	22.3
2	600	1523	-1544	661	0	-2163	-1577	4.02	4.02	4.02	4.02	2	0.63	0.04	0.28	0.00	0.00	22.3
3	600	1247	-1489	698	0	-2273	-1409	4.02	4.02	4.02	4.02	2	0.65	0.04	0.27	0.00	0.00	22.3
4	600	1456	-1558	448	0	-1482	-1626	4.02	4.02	4.02	4.02	2	0.43	0.05	0.28	0.00	0.00	22.3
5	600	1180	-1503	485	0	-1593	-1458	4.02	4.02	4.02	4.02	2	0.46	0.04	0.27	0.00	0.00	22.3
6	600	1820	-1613	542	0	-1796	-1790	4.02	4.02	4.02	4.02	2	0.53	0.05	0.29	0.00	0.00	22.3
7	600	903	-1430	667	0	-2163	-1230	4.02	4.02	4.02	4.02	2	0.61	0.04	0.25	0.00	0.00	22.3
8	600	1800	-1617	478	0	-1592	-1805	4.02	4.02	4.02	4.02	2	0.47	0.05	0.29	0.00	0.00	22.3
9	600	882	-1434	603	0	-1959	-1245	4.02	4.02	4.02	4.02	2	0.56	0.04	0.26	0.00	0.00	22.3
10	600	1523	-1544	661	0	-2163	-1577	4.02	4.02	4.02	4.02	2	0.63	0.04	0.28	0.00	0.00	22.3
11	600	1247	-1489	698	0	-2273	-1409	4.02	4.02	4.02	4.02	2	0.65	0.04	0.27	0.00	0.00	22.3
12	600	1456	-1558	448	0	-1482	-1626	4.02	4.02	4.02	4.02	2	0.43	0.05	0.28	0.00	0.00	22.3
13	600	1180	-1503	485	0	-1593	-1458	4.02	4.02	4.02	4.02	2	0.46	0.04	0.27	0.00	0.00	22.3
14	600	1820	-1613	542	0	-1796	-1790	4.02	4.02	4.02	4.02	2	0.53	0.05	0.29	0.00	0.00	22.3
15	600	903	-1430	667	0	-2163	-1230	4.02	4.02	4.02	4.02	2	0.61	0.04	0.25	0.00	0.00	22.3
16	600	1800	-1617	478	0	-1592	-1805	4.02	4.02	4.02	4.02	2	0.47	0.05	0.29	0.00	0.00	22.3
17	600	882	-1434	603	0	-1959	-1245	4.02	4.02	4.02	4.02	2	0.56	0.04	0.26	0.00	0.00	22.3
18	600	4056	-1953	1831	0	-5987	-1868	4.02	8.04	4.02	4.02	3	0.86	0.06	0.35	0.00	0.00	22.3
19	600	3576	-2010	1026	0	-3382	-2058	4.02	4.02	4.02	4.02	3	0.92	0.06	0.36	0.00	0.00	22.3
20	600	3774	-1902	1395	0	-4566	-1715	4.02	6.03	4.02	4.02	3	0.86	0.06	0.34	0.00	0.00	22.3
37	600	3542	-1933	1877	0	-6125	-1807	4.02	8.04	4.02	4.02	3	0.87	0.06	0.34	0.00	0.00	22.3
38	600	2740	-2029	535	0	-1784	-2123	4.02	4.02	4.02	4.02	3	0.47	0.06	0.36	0.00	0.00	22.3
39	600	3070	-1849	1151	0	-3757	-1551	4.02	6.03	4.02	4.02	3	0.70	0.05	0.33	0.00	0.00	22.3

apost= -- aant= 4.02 ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

Nome travata: **Trave_404_IP1** Descrizione: **Trave_4 32-25**
ASTA NUM. 17 NI 255 NF 256 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y Permanente qy tot.
qy medio: 375.00 132.00 507.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	1995	1891	88	0	-19	-1703	4.02	4.02	4.02	4.02	3	0.26	0.05	0.34	0.00	0.00	22.3
2	0	1699	1428	72	0	-39	-1227	4.02	4.02	4.02	4.02	2	0.20	0.04	0.25	0.00	0.00	22.3
3	0	1454	1484	72	0	-38	-1394	4.02	4.02	4.02	4.02	2	0.22	0.04	0.26	0.00	0.00	22.3
4	0	1615	1426	64	0	9	-1227	4.02	4.02	4.02	4.02	2	0.20	0.04	0.25	0.00	0.00	22.3

5	0	1370	1482	64	0	11	-1394	4.02	4.02	4.02	4.02	2	0.22	0.04	0.26	0.00	0.00	22.3
6	0	1956	1361	70	0	-24	-1032	4.02	4.02	4.02	4.02	2	0.17	0.04	0.24	0.00	0.00	22.3
7	0	1139	1549	69	0	-19	-1589	4.02	4.02	4.02	4.02	2	0.25	0.04	0.28	0.00	0.00	22.3
8	0	1931	1361	67	0	-10	-1032	4.02	4.02	4.02	4.02	2	0.17	0.04	0.24	0.00	0.00	22.3
9	0	1114	1548	66	0	-4	-1589	4.02	4.02	4.02	4.02	2	0.25	0.04	0.28	0.00	0.00	22.3
10	0	1699	1428	72	0	-39	-1227	4.02	4.02	4.02	4.02	2	0.20	0.04	0.25	0.00	0.00	22.3
11	0	1454	1484	72	0	-38	-1394	4.02	4.02	4.02	4.02	2	0.22	0.04	0.26	0.00	0.00	22.3
12	0	1615	1426	64	0	9	-1227	4.02	4.02	4.02	4.02	2	0.20	0.04	0.25	0.00	0.00	22.3
13	0	1370	1482	64	0	11	-1394	4.02	4.02	4.02	4.02	2	0.22	0.04	0.26	0.00	0.00	22.3
14	0	1956	1361	70	0	-24	-1032	4.02	4.02	4.02	4.02	2	0.17	0.04	0.24	0.00	0.00	22.3
15	0	1139	1549	69	0	-19	-1589	4.02	4.02	4.02	4.02	2	0.25	0.04	0.28	0.00	0.00	22.3
16	0	1931	1361	67	0	-10	-1032	4.02	4.02	4.02	4.02	2	0.17	0.04	0.24	0.00	0.00	22.3
17	0	1114	1548	66	0	-4	-1589	4.02	4.02	4.02	4.02	2	0.25	0.04	0.28	0.00	0.00	22.3
18	0	4644	1820	195	0	-106	-1471	4.02	4.02	4.02	4.02	3	0.24	0.05	0.32	0.00	0.00	22.3
19	0	4015	1820	150	0	57	-1483	4.02	4.02	4.02	4.02	3	0.24	0.05	0.32	0.00	0.00	22.3
20	0	4272	1917	162	0	-7	-1767	4.02	4.02	4.02	4.02	3	0.29	0.06	0.34	0.00	0.00	22.3
37	0	4087	1844	183	0	-159	-1541	4.02	4.02	4.02	4.02	3	0.25	0.05	0.33	0.00	0.00	22.3
38	0	3039	1843	108	0	113	-1563	4.02	4.02	4.02	4.02	3	0.25	0.05	0.33	0.00	0.00	22.3
39	0	3467	2006	128	0	7	-2036	4.02	4.02	4.02	4.02	3	0.32	0.06	0.36	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	60	1995	1496	88	0	-72	-1444	4.02	4.02	4.02	4.02	3	0.22	0.04	0.27	0.00	0.00	22.3
2	60	1699	1124	72	0	-83	-1031	4.02	4.02	4.02	4.02	2	0.16	0.03	0.20	0.00	0.00	22.3
3	60	1454	1180	72	0	-81	-1192	4.02	4.02	4.02	4.02	2	0.19	0.03	0.21	0.00	0.00	22.3
4	60	1615	1122	64	0	-29	-1031	4.02	4.02	4.02	4.02	2	0.16	0.03	0.20	0.00	0.00	22.3
5	60	1370	1178	64	0	-27	-1192	4.02	4.02	4.02	4.02	2	0.19	0.03	0.21	0.00	0.00	22.3
6	60	1956	1057	70	0	-66	-841	4.02	4.02	4.02	4.02	2	0.14	0.03	0.19	0.00	0.00	22.3
7	60	1139	1245	69	0	-60	-1381	4.02	4.02	4.02	4.02	2	0.22	0.04	0.22	0.00	0.00	22.3
8	60	1931	1057	67	0	-50	-842	4.02	4.02	4.02	4.02	2	0.14	0.03	0.19	0.00	0.00	22.3
9	60	1114	1244	66	0	-44	-1381	4.02	4.02	4.02	4.02	2	0.22	0.04	0.22	0.00	0.00	22.3
10	60	1699	1124	72	0	-83	-1031	4.02	4.02	4.02	4.02	2	0.16	0.03	0.20	0.00	0.00	22.3
11	60	1454	1180	72	0	-81	-1192	4.02	4.02	4.02	4.02	2	0.19	0.03	0.21	0.00	0.00	22.3
12	60	1615	1122	64	0	-29	-1031	4.02	4.02	4.02	4.02	2	0.16	0.03	0.20	0.00	0.00	22.3
13	60	1370	1178	64	0	-27	-1192	4.02	4.02	4.02	4.02	2	0.19	0.03	0.21	0.00	0.00	22.3
14	60	1956	1057	70	0	-66	-841	4.02	4.02	4.02	4.02	2	0.14	0.03	0.19	0.00	0.00	22.3
15	60	1139	1245	69	0	-60	-1381	4.02	4.02	4.02	4.02	2	0.22	0.04	0.22	0.00	0.00	22.3
16	60	1931	1057	67	0	-50	-842	4.02	4.02	4.02	4.02	2	0.14	0.03	0.19	0.00	0.00	22.3
17	60	1114	1244	66	0	-44	-1381	4.02	4.02	4.02	4.02	2	0.22	0.04	0.22	0.00	0.00	22.3
18	60	4644	1425	195	0	-223	-1219	4.02	4.02	4.02	4.02	3	0.20	0.04	0.25	0.00	0.00	22.3
19	60	4015	1424	150	0	-33	-1231	4.02	4.02	4.02	4.02	3	0.20	0.04	0.25	0.00	0.00	22.3
20	60	4272	1522	162	0	-104	-1506	4.02	4.02	4.02	4.02	3	0.25	0.04	0.27	0.00	0.00	22.3
37	60	4087	1448	183	0	-268	-1287	4.02	4.02	4.02	4.02	3	0.21	0.04	0.26	0.00	0.00	22.3
38	60	3039	1448	108	0	49	-1308	4.02	4.02	4.02	4.02	3	0.21	0.04	0.26	0.00	0.00	22.3
39	60	3467	1610	128	0	-70	-1766	4.02	4.02	4.02	4.02	3	0.28	0.05	0.29	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	120	1995	1100	88	0	-125	649	4.02	4.02	4.02	4.02	3	0.10	0.03	0.20	0.00	0.00	22.3
2	120	1699	820	72	0	-126	536	4.02	4.02	4.02	4.02	2	0.09	0.02	0.15	0.00	0.00	22.3
3	120	1454	876	72	0	-124	465	4.02	4.02	4.02	4.02	2	0.07	0.03	0.16	0.00	0.00	22.3
4	120	1615	818	64	0	-68	533	4.02	4.02	4.02	4.02	2	0.08	0.02	0.15	0.00	0.00	22.3
5	120	1370	874	64	0	-66	462	4.02	4.02	4.02	4.02	2	0.07	0.03	0.16	0.00	0.00	22.3
6	120	1956	753	70	0	-108	618	4.02	4.02	4.02	4.02	2	0.10	0.02	0.13	0.00	0.00	22.3
7	120	1139	941	69	0	-101	-571	4.02	4.02	4.02	4.02	2	0.09	0.03	0.17	0.00	0.00	22.3
8	120	1931	753	67	0	-91	617	4.02	4.02	4.02	4.02	2	0.10	0.02	0.13	0.00	0.00	22.3
9	120	1114	940	66	0	-84	-572	4.02	4.02	4.02	4.02	2	0.09	0.03	0.17	0.00	0.00	22.3
10	120	1699	820	72	0	-126	536	4.02	4.02	4.02	4.02	2	0.09	0.02	0.15	0.00	0.00	22.3
11	120	1454	876	72	0	-124	465	4.02	4.02	4.02	4.02	2	0.07	0.03	0.16	0.00	0.00	22.3
12	120	1615	818	64	0	-68	533	4.02	4.02	4.02	4.02	2	0.08	0.02	0.15	0.00	0.00	22.3
13	120	1370	874	64	0	-66	462	4.02	4.02	4.02	4.02	2	0.07	0.03	0.16	0.00	0.00	22.3
14	120	1956	753	70	0	-108	618	4.02	4.02	4.02	4.02	2	0.10	0.02	0.13	0.00	0.00	22.3
15	120	1139	941	69	0	-101	-571	4.02	4.02	4.02	4.02	2	0.09	0.03	0.17	0.00	0.00	22.3
16	120	1931	753	67	0	-91	617	4.02	4.02	4.02	4.02	2	0.10	0.02	0.13	0.00	0.00	22.3
17	120	1114	940	66	0	-84	-572	4.02	4.02	4.02	4.02	2	0.09	0.03	0.17	0.00	0.00	22.3
18	120	4644	1029	195	0	-340	760	4.02	4.02	4.02	4.02	3	0.13	0.03	0.18	0.00	0.00	22.3
19	120	4015	1029	150	0	-123	747	4.02	4.02	4.02	4.02	3	0.12	0.03	0.18	0.00	0.00	22.3
20	120	4272	1126	162	0	-201	629	4.02	4.02	4.02	4.02	3	0.10	0.03	0.20	0.00	0.00	22.3
37	120	4087	1053	183	0	-378	730	4.02	4.02	4.02	4.02	3	0.12	0.03	0.19	0.00	0.00	22.3
38	120	3039	1052	108	0	-16	707	4.02	4.02	4.02	4.02	3	0.11	0.03	0.19	0.00	0.00	22.3
39	120	3467	1215	128	0	-147	-718	4.02	4.02	4.02	4.02	3	0.11	0.04	0.22	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	180	1995	705	88	0	-178	990	4.02	4.02	4.02	4.02	3	0.15	0.02	0.13	0.00	0.00	22.3
2	180	1699	515	72	0	-170	775	4.02	4.02	4.02	4.02	2	0.12	0.01	0.09	0.00	0.00	22.3
3	180	1454	571	72	0	-167	745	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
4	180	1615	513	64	0	-106	769	4.02	4.02	4.02	4.02	2	0.12	0.01	0.09	0.00	0.00	22.3
5	180	1370	569	64	0	-104	741	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
6	180	1956	448	70	0	-150	775	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
7	180	1139	636	69	0	-142	700	4.02	4.02	4.02	4.02	2	0.11	0.02	0.11	0.00	0.00	22.3
8	180	1931	448	67	0	-131	774	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
9	180	1114	635	66	0	-123	699	4.02	4.02	4.02	4.02	2	0.11	0.02	0.11	0.00	0.00	22.3
10	180	1699	515	72	0	-170	775	4.02	4.02	4.02	4.02	2	0.12	0.01	0.09	0.00	0.00	22.3
11	180	1454	571	72	0	-167	745	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
12	180	1615	513	64	0	-106	769	4.02	4.02	4.02	4.02	2	0.12	0.01	0.09	0.00	0.00	22.3
13	180	1370	569	64	0	-104	741	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
14	180	1956	448	70	0	-150	775	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
15	180	1139	636	69	0	-142	700	4.02	4.02	4.02	4.02	2	0.11	0.02	0.11	0.00	0.00	22.3
16	180	1931	448	67	0	-131	774	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
17	180	1114	635	66	0	-123	699	4.02	4.02	4.02	4.02	2	0.11	0.02	0.11	0.00	0.00	22.3
18	180	4644	634	195	0	-457	1024	4.02	4.02	4.02	4.02	3	0.17	0.02	0.11	0.00	0.00	22.3
19	180	4015	633	150	0	-213	1010	4.02	4.02	4.02	4.02	3	0.16	0.02	0.11	0.00	0.00	22.3
20	180	4272	731	162	0	-299	986	4.02	4.02	4.02	4.02	3	0.16	0.02	0.13	0.00	0.00	22.3
37	180	4087	657	183	0	-487	1025	4.02	4.02	4.02	4.02	3	0.17	0.02	0.12	0.00	0.00	22.3
38	180	3039	657	108	0	-80	1001	4.02	4.02	4.02	4.02	3	0.16	0.02	0.12	0.00	0.00	22.3
39	180	3467	820	128	0	-223	922	4.02	4.02	4.02	4.02	3	0.15	0.02	0.15	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	240	1995	309	88	0	-231	1005	4.02	4.02	4.02	4.02	3	0.15	0.01	0.06	0.00	0.00	22.3
2	240	1699	211	72	0	-213	775	4.02	4.02	4.02	4.02	2	0.12	0.01	0.04	0.00	0.00	22.3
3	240	1454	267	72	0	-211	777	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
4	240	1615	209	64	0	-145	769	4.02	4.02	4.02	4.02	2	0.12	0.01	0.04	0.00	0.00	22.3
5	240	1370	265	64	0	-142	771	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
6	240	1956	144	70	0	-192	775	4.02	4.02	4.02	4.02	2	0.12	0.00	0.03	0.00	0.00	22.3
7	240	1139	332	69	0	-183	777	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
8	240	1931	144	67	0	-172	774	4.02	4.02	4.02	4.02	2	0.12	0.00	0.03	0.00	0.00	22.3
9	240	1114	331	66	0	-163	775	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
10	240	1699	211	72	0	-213	775	4.02	4.02	4.02	4.02	2	0.12	0.01	0.04	0.00	0.00	22.3

11	240	1454	267	72	0	-211	777	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
12	240	1615	209	64	0	-145	769	4.02	4.02	4.02	4.02	2	0.12	0.01	0.04	0.00	0.00	22.3
13	240	1370	265	64	0	-142	771	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
14	240	1956	144	70	0	-192	775	4.02	4.02	4.02	4.02	2	0.12	0.00	0.03	0.00	0.00	22.3
15	240	1139	332	69	0	-183	777	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
16	240	1931	144	67	0	-172	774	4.02	4.02	4.02	4.02	2	0.12	0.00	0.03	0.00	0.00	22.3
17	240	1114	331	66	0	-163	775	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
18	240	4644	238	195	0	-574	1024	4.02	4.02	4.02	4.02	3	0.17	0.01	0.04	0.00	0.00	22.3
19	240	4015	238	150	0	-303	1010	4.02	4.02	4.02	4.02	3	0.16	0.01	0.04	0.00	0.00	22.3
20	240	4272	335	162	0	-396	1019	4.02	4.02	4.02	4.02	3	0.17	0.01	0.06	0.00	0.00	22.3
37	240	4087	262	183	0	-597	1025	4.02	4.02	4.02	4.02	3	0.17	0.01	0.05	0.00	0.00	22.3
38	240	3039	261	108	0	-145	1001	4.02	4.02	4.02	4.02	3	0.16	0.01	0.05	0.00	0.00	22.3
39	240	3467	424	128	0	-300	1016	4.02	4.02	4.02	4.02	3	0.16	0.01	0.08	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	300	1995	-86	88	0	-284	1005	4.02	4.02	4.02	4.02	3	0.15	0.00	0.02	0.00	0.00	22.3
2	300	1699	-93	72	0	-257	775	4.02	4.02	4.02	4.02	2	0.12	0.00	0.02	0.00	0.00	22.3
3	300	1454	-37	72	0	-254	777	4.02	4.02	4.02	4.02	2	0.12	0.00	0.01	0.00	0.00	22.3
4	300	1615	-95	64	0	-183	769	4.02	4.02	4.02	4.02	2	0.12	0.00	0.02	0.00	0.00	22.3
5	300	1370	-39	64	0	-180	771	4.02	4.02	4.02	4.02	2	0.12	0.00	0.01	0.00	0.00	22.3
6	300	1956	-160	70	0	-234	775	4.02	4.02	4.02	4.02	2	0.12	0.00	0.03	0.00	0.00	22.3
7	300	1139	28	69	0	-225	777	4.02	4.02	4.02	4.02	2	0.12	0.00	0.00	0.00	0.00	22.3
8	300	1931	-160	67	0	-212	774	4.02	4.02	4.02	4.02	2	0.12	0.00	0.03	0.00	0.00	22.3
9	300	1114	27	66	0	-202	775	4.02	4.02	4.02	4.02	2	0.12	0.00	0.00	0.00	0.00	22.3
10	300	1699	-93	72	0	-257	775	4.02	4.02	4.02	4.02	2	0.12	0.00	0.02	0.00	0.00	22.3
11	300	1454	-37	72	0	-254	777	4.02	4.02	4.02	4.02	2	0.12	0.00	0.01	0.00	0.00	22.3
12	300	1615	-95	64	0	-183	769	4.02	4.02	4.02	4.02	2	0.12	0.00	0.02	0.00	0.00	22.3
13	300	1370	-39	64	0	-180	771	4.02	4.02	4.02	4.02	2	0.12	0.00	0.01	0.00	0.00	22.3
14	300	1956	-160	70	0	-234	775	4.02	4.02	4.02	4.02	2	0.12	0.00	0.03	0.00	0.00	22.3
15	300	1139	28	69	0	-225	777	4.02	4.02	4.02	4.02	2	0.12	0.00	0.00	0.00	0.00	22.3
16	300	1931	-160	67	0	-212	774	4.02	4.02	4.02	4.02	2	0.12	0.00	0.03	0.00	0.00	22.3
17	300	1114	27	66	0	-202	775	4.02	4.02	4.02	4.02	2	0.12	0.00	0.00	0.00	0.00	22.3
18	300	4644	-157	195	0	-691	1024	4.02	4.02	4.02	4.02	3	0.19	0.01	0.03	0.00	0.00	22.3
19	300	4015	-158	150	0	-393	1010	4.02	4.02	4.02	4.02	3	0.16	0.00	0.03	0.00	0.00	22.3
20	300	4272	-60	162	0	-493	1019	4.02	4.02	4.02	4.02	3	0.17	0.01	0.03	0.00	0.00	22.3
37	300	4087	-134	183	0	-706	1025	4.02	4.02	4.02	4.02	3	0.19	0.01	0.03	0.00	0.00	22.3
38	300	3039	-134	108	0	-209	1001	4.02	4.02	4.02	4.02	3	0.16	0.00	0.02	0.00	0.00	22.3
39	300	3467	28	128	0	-377	1016	4.02	4.02	4.02	4.02	3	0.16	0.00	0.01	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	360	1995	-481	88	0	-337	1005	4.02	4.02	4.02	4.02	3	0.15	0.01	0.09	0.00	0.00	22.3
2	360	1699	-397	72	0	-300	775	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
3	360	1454	-341	72	0	-297	777	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
4	360	1615	-399	64	0	-221	769	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
5	360	1370	-343	64	0	-218	771	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
6	360	1956	-464	70	0	-276	775	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
7	360	1139	-276	69	0	-266	777	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
8	360	1931	-464	67	0	-253	774	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
9	360	1114	-277	66	0	-242	775	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
10	360	1699	-397	72	0	-300	775	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
11	360	1454	-341	72	0	-297	777	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
12	360	1615	-399	64	0	-221	769	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
13	360	1370	-343	64	0	-218	771	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
14	360	1956	-464	70	0	-276	775	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
15	360	1139	-276	69	0	-266	777	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
16	360	1931	-464	67	0	-253	774	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
17	360	1114	-277	66	0	-242	775	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
18	360	4644	-552	195	0	-808	1024	4.02	4.02	4.02	4.02	3	0.23	0.02	0.10	0.00	0.00	22.3
19	360	4015	-553	150	0	-483	1010	4.02	4.02	4.02	4.02	3	0.16	0.02	0.10	0.00	0.00	22.3
20	360	4272	-455	162	0	-590	1019	4.02	4.02	4.02	4.02	3	0.17	0.01	0.08	0.00	0.00	22.3
37	360	4087	-529	183	0	-816	1025	4.02	4.02	4.02	4.02	3	0.22	0.02	0.09	0.00	0.00	22.3
38	360	3039	-529	108	0	-274	1001	4.02	4.02	4.02	4.02	3	0.16	0.02	0.09	0.00	0.00	22.3
39	360	3467	-367	128	0	-453	1016	4.02	4.02	4.02	4.02	3	0.16	0.01	0.07	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	420	1995	-877	88	0	-390	871	4.02	4.02	4.02	4.02	3	0.13	0.03	0.16	0.00	0.00	22.3
2	420	1699	-701	72	0	-344	653	4.02	4.02	4.02	4.02	2	0.10	0.02	0.12	0.00	0.00	22.3
3	420	1454	-645	72	0	-340	694	4.02	4.02	4.02	4.02	2	0.11	0.02	0.11	0.00	0.00	22.3
4	420	1615	-703	64	0	-260	646	4.02	4.02	4.02	4.02	2	0.10	0.02	0.13	0.00	0.00	22.3
5	420	1370	-647	64	0	-256	687	4.02	4.02	4.02	4.02	2	0.11	0.02	0.12	0.00	0.00	22.3
6	420	1956	-768	70	0	-318	603	4.02	4.02	4.02	4.02	2	0.10	0.02	0.14	0.00	0.00	22.3
7	420	1139	-580	69	0	-307	739	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
8	420	1931	-768	67	0	-293	601	4.02	4.02	4.02	4.02	2	0.10	0.02	0.14	0.00	0.00	22.3
9	420	1114	-581	66	0	-282	737	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
10	420	1699	-701	72	0	-344	653	4.02	4.02	4.02	4.02	2	0.10	0.02	0.12	0.00	0.00	22.3
11	420	1454	-645	72	0	-340	694	4.02	4.02	4.02	4.02	2	0.11	0.02	0.11	0.00	0.00	22.3
12	420	1615	-703	64	0	-260	646	4.02	4.02	4.02	4.02	2	0.10	0.02	0.13	0.00	0.00	22.3
13	420	1370	-647	64	0	-256	687	4.02	4.02	4.02	4.02	2	0.11	0.02	0.12	0.00	0.00	22.3
14	420	1956	-768	70	0	-318	603	4.02	4.02	4.02	4.02	2	0.10	0.02	0.14	0.00	0.00	22.3
15	420	1139	-580	69	0	-307	739	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
16	420	1931	-768	67	0	-293	601	4.02	4.02	4.02	4.02	2	0.10	0.02	0.14	0.00	0.00	22.3
17	420	1114	-581	66	0	-282	737	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
18	420	4644	-948	195	0	-925	841	4.02	4.02	4.02	4.02	3	0.26	0.03	0.17	0.00	0.00	22.3
19	420	4015	-948	150	0	-573	827	4.02	4.02	4.02	4.02	3	0.16	0.03	0.17	0.00	0.00	22.3
20	420	4272	-851	162	0	-688	903	4.02	4.02	4.02	4.02	3	0.19	0.02	0.15	0.00	0.00	22.3
37	420	4087	-924	183	0	-925	858	4.02	4.02	4.02	4.02	3	0.25	0.03	0.16	0.00	0.00	22.3
38	420	3039	-925	108	0	-338	834	4.02	4.02	4.02	4.02	3	0.13	0.03	0.16	0.00	0.00	22.3
39	420	3467	-762	128	0	-530	963	4.02	4.02	4.02	4.02	3	0.15	0.02	0.14	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	480	1995	-1272	88	0	-443	-862	4.02	4.02	4.02	4.02	3	0.13	0.04	0.23	0.00	0.00	22.3
2	480	1699	-1006	72	0	-387	-724	4.02	4.02	4.02	4.02	2	0.12	0.03	0.18	0.00	0.00	22.3
3	480	1454	-950	72	0	-383	-592	4.02	4.02	4.02	4.02	2	0.11	0.03	0.17	0.00	0.00	22.3
4	480	1615	-1008	64	0	-298	-734	4.02	4.02	4.02	4.02	2	0.12	0.03	0.18	0.00	0.00	22.3
5	480	1370	-952	64	0	-295	-602	4.02	4.02	4.02	4.02	2	0.10	0.03	0.17	0.00	0.00	22.3
6	480	1956	-1073	70	0	-360	-881	4.02	4.02	4.02	4.02	2	0.14	0.03	0.19	0.00	0.00	22.3
7	480	1139	-885	69	0	-348	453	4.02	4.02	4.02	4.02	2	0.10	0.03	0.16	0.00	0.00	22.3
8	480	1931	-1073	67	0	-334	-884	4.02	4.02	4.02	4.02	2	0.14	0.03	0.19	0.00	0.00	22.3
9	480	1114	-886	66	0	-321	451	4.02	4.02	4.02	4.02	2	0.09	0.03	0.16	0.00	0.00	22.3
10	480	1699	-1006	72	0	-387	-724	4.02	4.02	4.02	4.02	2	0.12	0.03	0.18	0.00	0.00	22.3
11	480	1454	-950	72	0	-383	-592	4.02	4.02	4.02	4.02	2	0.11	0.03	0.17	0.00	0.00	22.3
12	480	1615	-1008	64	0	-298	-734	4.02	4.02	4.02	4.02	2	0.12	0.03	0.18	0.00	0.00	22.3
13	480	1370	-952	64	0	-295	-602	4.02	4.02	4.02	4.02	2	0.10	0.03	0.17	0.00	0.00	22.3
14	480	1956	-1073	70	0	-360	-881	4.02	4.02	4.02	4.02	2	0.14	0.03	0.19	0.00	0.00	22.3
15	480	1139	-885	69	0	-348	453	4.02	4.02	4.02	4.02	2	0.10	0.03	0.16	0.00	0.00	22.3
16	480	1931	-1073	67	0	-334	-884	4.02	4.02	4.02	4.02	2	0.14	0.03	0.19	0.00	0.00	22.3

17	480	1114	-886	66	0	-321	451	4.02	4.02	4.02	4.02	2	0.09	0.03	0.16	0.00	0.00	22.3
18	480	4644	-1343	195	0	-1042	-1006	4.02	4.02	4.02	4.02	3	0.29	0.04	0.24	0.00	0.00	22.3
19	480	4015	-1344	150	0	-663	-1021	4.02	4.02	4.02	4.02	3	0.18	0.04	0.24	0.00	0.00	22.3
20	480	4272	-1246	162	0	-785	-788	4.02	4.02	4.02	4.02	3	0.22	0.04	0.22	0.00	0.00	22.3
37	480	4087	-1320	183	0	-1035	-951	4.02	4.02	4.02	4.02	3	0.29	0.04	0.24	0.00	0.00	22.3
38	480	3039	-1320	108	0	-403	-976	4.02	4.02	4.02	4.02	3	0.15	0.04	0.24	0.00	0.00	22.3
39	480	3467	-1158	128	0	-607	587	4.02	4.02	4.02	4.02	3	0.16	0.03	0.21	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	540	1995	-1668	88	0	-496	-1944	4.02	4.02	4.02	4.02	3	0.30	0.05	0.30	0.00	0.00	22.3
2	540	1699	-1310	72	0	-431	-1573	4.02	4.02	4.02	4.02	2	0.25	0.04	0.23	0.00	0.00	22.3
3	540	1454	-1254	72	0	-427	-1407	4.02	4.02	4.02	4.02	2	0.22	0.04	0.22	0.00	0.00	22.3
4	540	1615	-1312	64	0	-337	-1584	4.02	4.02	4.02	4.02	2	0.25	0.04	0.23	0.00	0.00	22.3
5	540	1370	-1256	64	0	-333	-1418	4.02	4.02	4.02	4.02	2	0.22	0.04	0.22	0.00	0.00	22.3
6	540	1956	-1377	70	0	-402	-1770	4.02	4.02	4.02	4.02	2	0.29	0.04	0.25	0.00	0.00	22.3
7	540	1139	-1189	69	0	-389	-1218	4.02	4.02	4.02	4.02	2	0.19	0.03	0.21	0.00	0.00	22.3
8	540	1931	-1377	67	0	-374	-1773	4.02	4.02	4.02	4.02	2	0.29	0.04	0.25	0.00	0.00	22.3
9	540	1114	-1190	66	0	-361	-1221	4.02	4.02	4.02	4.02	2	0.19	0.03	0.21	0.00	0.00	22.3
10	540	1699	-1310	72	0	-431	-1573	4.02	4.02	4.02	4.02	2	0.25	0.04	0.23	0.00	0.00	22.3
11	540	1454	-1254	72	0	-427	-1407	4.02	4.02	4.02	4.02	2	0.22	0.04	0.22	0.00	0.00	22.3
12	540	1615	-1312	64	0	-337	-1584	4.02	4.02	4.02	4.02	2	0.25	0.04	0.23	0.00	0.00	22.3
13	540	1370	-1256	64	0	-333	-1418	4.02	4.02	4.02	4.02	2	0.22	0.04	0.22	0.00	0.00	22.3
14	540	1956	-1377	70	0	-402	-1770	4.02	4.02	4.02	4.02	2	0.29	0.04	0.25	0.00	0.00	22.3
15	540	1139	-1189	69	0	-389	-1218	4.02	4.02	4.02	4.02	2	0.19	0.03	0.21	0.00	0.00	22.3
16	540	1931	-1377	67	0	-374	-1773	4.02	4.02	4.02	4.02	2	0.29	0.04	0.25	0.00	0.00	22.3
17	540	1114	-1190	66	0	-361	-1221	4.02	4.02	4.02	4.02	2	0.19	0.03	0.21	0.00	0.00	22.3
18	540	4644	-1739	195	0	-1159	-2131	4.02	4.02	4.02	4.02	3	0.35	0.05	0.31	0.00	0.00	22.3
19	540	4015	-1740	150	0	-753	-2146	4.02	4.02	4.02	4.02	3	0.35	0.05	0.31	0.00	0.00	22.3
20	540	4272	-1642	162	0	-882	-1854	4.02	4.02	4.02	4.02	3	0.30	0.05	0.29	0.00	0.00	22.3
37	540	4087	-1716	183	0	-1144	-2062	4.02	4.02	4.02	4.02	3	0.34	0.05	0.31	0.00	0.00	22.3
38	540	3039	-1716	108	0	-467	-2086	4.02	4.02	4.02	4.02	3	0.33	0.05	0.31	0.00	0.00	22.3
39	540	3467	-1553	128	0	-683	-1599	4.02	4.02	4.02	4.02	3	0.26	0.05	0.28	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	600	1995	-2063	88	0	-549	-2219	4.02	4.02	4.02	4.02	3	0.34	0.06	0.37	0.00	0.00	22.3
2	600	1699	-1614	72	0	-474	-1787	4.02	4.02	4.02	4.02	2	0.29	0.05	0.29	0.00	0.00	22.3
3	600	1454	-1558	72	0	-470	-1616	4.02	4.02	4.02	4.02	2	0.26	0.05	0.28	0.00	0.00	22.3
4	600	1615	-1616	64	0	-375	-1798	4.02	4.02	4.02	4.02	2	0.29	0.05	0.29	0.00	0.00	22.3
5	600	1370	-1560	64	0	-371	-1627	4.02	4.02	4.02	4.02	2	0.26	0.05	0.28	0.00	0.00	22.3
6	600	1956	-1681	70	0	-444	-1990	4.02	4.02	4.02	4.02	2	0.32	0.05	0.30	0.00	0.00	22.3
7	600	1139	-1493	69	0	-430	-1421	4.02	4.02	4.02	4.02	2	0.22	0.04	0.27	0.00	0.00	22.3
8	600	1931	-1681	67	0	-415	-1993	4.02	4.02	4.02	4.02	2	0.32	0.05	0.30	0.00	0.00	22.3
9	600	1114	-1494	66	0	-400	-1424	4.02	4.02	4.02	4.02	2	0.22	0.04	0.27	0.00	0.00	22.3
10	600	1699	-1614	72	0	-474	-1787	4.02	4.02	4.02	4.02	2	0.29	0.05	0.29	0.00	0.00	22.3
11	600	1454	-1558	72	0	-470	-1616	4.02	4.02	4.02	4.02	2	0.26	0.05	0.28	0.00	0.00	22.3
12	600	1615	-1616	64	0	-375	-1798	4.02	4.02	4.02	4.02	2	0.29	0.05	0.29	0.00	0.00	22.3
13	600	1370	-1560	64	0	-371	-1627	4.02	4.02	4.02	4.02	2	0.26	0.05	0.28	0.00	0.00	22.3
14	600	1956	-1681	70	0	-444	-1990	4.02	4.02	4.02	4.02	2	0.32	0.05	0.30	0.00	0.00	22.3
15	600	1139	-1493	69	0	-430	-1421	4.02	4.02	4.02	4.02	2	0.22	0.04	0.27	0.00	0.00	22.3
16	600	1931	-1681	67	0	-415	-1993	4.02	4.02	4.02	4.02	2	0.32	0.05	0.30	0.00	0.00	22.3
17	600	1114	-1494	66	0	-400	-1424	4.02	4.02	4.02	4.02	2	0.22	0.04	0.27	0.00	0.00	22.3
18	600	4644	-2134	195	0	-1276	-2413	4.02	4.02	4.02	4.02	3	0.40	0.06	0.38	0.00	0.00	22.3
19	600	4015	-2135	150	0	-843	-2428	4.02	4.02	4.02	4.02	3	0.39	0.06	0.38	0.00	0.00	22.3
20	600	4272	-2037	162	0	-980	-2127	4.02	4.02	4.02	4.02	3	0.35	0.06	0.36	0.00	0.00	22.3
37	600	4087	-2111	183	0	-1254	-2341	4.02	4.02	4.02	4.02	3	0.38	0.06	0.38	0.00	0.00	22.3
38	600	3039	-2111	108	0	-532	-2366	4.02	4.02	4.02	4.02	3	0.37	0.06	0.38	0.00	0.00	22.3
39	600	3467	-1949	128	0	-760	-1863	4.02	4.02	4.02	4.02	3	0.30	0.06	0.35	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

Nome travata: **Trave_404_IP1** Descrizione: **Trave_4 32-25**
ASTA NUM. 18 NI 256 NF 257 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y Permanente qy tot.
qy medio: 375.00 132.00 507.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	2151	1858	-121	0	-619	-1616	4.02	4.02	4.02	4.02	3	0.25	0.05	0.33	0.00	0.00	22.3
2	0	1821	1399	-106	0	-544	-1152	4.02	4.02	4.02	4.02	2	0.18	0.04	0.25	0.00	0.00	22.3
3	0	1634	1461	-82	0	-466	-1339	4.02	4.02	4.02	4.02	2	0.21	0.04	0.26	0.00	0.00	22.3
4	0	1676	1398	-104	0	-485	-1147	4.02	4.02	4.02	4.02	2	0.18	0.04	0.25	0.00	0.00	22.3
5	0	1489	1460	-81	0	-408	-1333	4.02	4.02	4.02	4.02	2	0.21	0.04	0.26	0.00	0.00	22.3
6	0	1989	1326	-132	0	-614	-933	4.02	4.02	4.02	4.02	2	0.18	0.04	0.24	0.00	0.00	22.3
7	0	1364	1534	-54	0	-355	-1555	4.02	4.02	4.02	4.02	2	0.25	0.04	0.27	0.00	0.00	22.3
8	0	1946	1325	-132	0	-597	-931	4.02	4.02	4.02	4.02	2	0.18	0.04	0.24	0.00	0.00	22.3
9	0	1321	1533	-54	0	-338	-1553	4.02	4.02	4.02	4.02	2	0.25	0.04	0.27	0.00	0.00	22.3
10	0	1821	1399	-106	0	-544	-1152	4.02	4.02	4.02	4.02	2	0.18	0.04	0.25	0.00	0.00	22.3
11	0	1634	1461	-82	0	-466	-1339	4.02	4.02	4.02	4.02	2	0.21	0.04	0.26	0.00	0.00	22.3
12	0	1676	1398	-104	0	-485	-1147	4.02	4.02	4.02	4.02	2	0.18	0.04	0.25	0.00	0.00	22.3
13	0	1489	1460	-81	0	-408	-1333	4.02	4.02	4.02	4.02	2	0.21	0.04	0.26	0.00	0.00	22.3
14	0	1989	1326	-132	0	-614	-933	4.02	4.02	4.02	4.02	2	0.18	0.04	0.24	0.00	0.00	22.3
15	0	1364	1534	-54	0	-355	-1555	4.02	4.02	4.02	4.02	2	0.25	0.04	0.27	0.00	0.00	22.3
16	0	1946	1325	-132	0	-597	-931	4.02	4.02	4.02	4.02	2	0.18	0.04	0.24	0.00	0.00	22.3
17	0	1321	1533	-54	0	-338	-1553	4.02	4.02	4.02	4.02	2	0.25	0.04	0.27	0.00	0.00	22.3
18	0	5081	1735	-244	0	-1340	-1258	4.02	4.02	4.02	4.02	3	0.38	0.05	0.31	0.00	0.00	22.3
19	0	4387	1752	-211	0	-1001	-1302	4.02	4.02	4.02	4.02	3	0.28	0.05	0.31	0.00	0.00	22.3
20	0	4665	1859	-155	0	-901	-1622	4.02	4.02	4.02	4.02	3	0.27	0.05	0.33	0.00	0.00	22.3
37	0	4463	1768	-221	0	-1273	-1354	4.02	4.02	4.02	4.02	3	0.35	0.05	0.31	0.00	0.00	22.3
38	0	3308	1796	-165	0	-708	-1428	4.02	4.02	4.02	4.02	3	0.23	0.05	0.32	0.00	0.00	22.3
39	0	3771	1973	-73	0	-541	-1961	4.02	4.02	4.02	4.02	3	0.32	0.06	0.35	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	60	2151	1463	-121	0	-546	-1360	4.02	4.02	4.02	4.02	3	0.21	0.04	0.26	0.00	0.00	22.3
2	60	1821	1095	-106	0	-481	-958	4.02	4.02	4.02	4.02	2	0.15	0.03	0.19	0.00	0.00	22.3
3	60	1634	1157	-82	0	-417	-1139	4.02	4.02	4.02	4.02	2	0.18	0.03	0.21	0.00	0.00	22.3
4	60	1676	1094	-104	0	-423	-953	4.02	4.02	4.02	4.02	2	0.15	0.03	0.19	0.00	0.00	22.3
5	60	1489	1156	-81	0	-359	-1133	4.02	4.02	4.02	4.02	2	0.18	0.03	0.21	0.00	0.00	22.3
6	60	1989	1022	-132	0	-535	-746	4.02	4.02	4.02	4.02	2	0.16	0.03	0.18	0.00	0.00	22.3
7	60	1364	1230	-54	0	-323	-1349	4.02	4.02	4.02	4.02	2	0.21	0.04	0.22	0.00	0.00	22.3
8	60	1946	1021	-132	0	-517	-744	4.02	4.02	4.02	4.02	2	0.15	0.03	0.18	0.00	0.00	22.3

9	60	1321	1229	-54	0	-305	-1346	4.02	4.02	4.02	4.02	2	0.21	0.04	0.22	0.00	0.00	22.3
10	60	1821	1095	-106	0	-481	-958	4.02	4.02	4.02	4.02	2	0.15	0.03	0.19	0.00	0.00	22.3
11	60	1634	1157	-82	0	-417	-1139	4.02	4.02	4.02	4.02	2	0.18	0.03	0.21	0.00	0.00	22.3
12	60	1676	1094	-104	0	-423	-953	4.02	4.02	4.02	4.02	2	0.15	0.03	0.19	0.00	0.00	22.3
13	60	1489	1156	-81	0	-359	-1133	4.02	4.02	4.02	4.02	2	0.18	0.03	0.21	0.00	0.00	22.3
14	60	1989	1022	-132	0	-535	-746	4.02	4.02	4.02	4.02	2	0.16	0.03	0.18	0.00	0.00	22.3
15	60	1364	1230	-54	0	-323	-1349	4.02	4.02	4.02	4.02	2	0.21	0.04	0.22	0.00	0.00	22.3
16	60	1946	1021	-132	0	-517	-744	4.02	4.02	4.02	4.02	2	0.15	0.03	0.18	0.00	0.00	22.3
17	60	1321	1229	-54	0	-305	-1346	4.02	4.02	4.02	4.02	2	0.21	0.04	0.22	0.00	0.00	22.3
18	60	5081	1340	-244	0	-1193	-1014	4.02	4.02	4.02	4.02	3	0.34	0.04	0.24	0.00	0.00	22.3
19	60	4387	1357	-211	0	-875	-1056	4.02	4.02	4.02	4.02	3	0.24	0.04	0.24	0.00	0.00	22.3
20	60	4665	1464	-155	0	-807	-1366	4.02	4.02	4.02	4.02	3	0.23	0.04	0.26	0.00	0.00	22.3
37	60	4463	1372	-221	0	-1140	-1107	4.02	4.02	4.02	4.02	3	0.32	0.04	0.24	0.00	0.00	22.3
38	60	3308	1400	-165	0	-609	-1178	4.02	4.02	4.02	4.02	3	0.19	0.04	0.25	0.00	0.00	22.3
39	60	3771	1578	-73	0	-498	-1694	4.02	4.02	4.02	4.02	3	0.27	0.05	0.28	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	120	2151	1067	-121	0	-473	680	4.02	4.02	4.02	4.02	3	0.12	0.03	0.19	0.00	0.00	22.3
2	120	1821	791	-106	0	-417	562	4.02	4.02	4.02	4.02	2	0.12	0.02	0.14	0.00	0.00	22.3
3	120	1634	853	-82	0	-368	481	4.02	4.02	4.02	4.02	2	0.11	0.02	0.15	0.00	0.00	22.3
4	120	1676	790	-104	0	-360	565	4.02	4.02	4.02	4.02	2	0.11	0.02	0.14	0.00	0.00	22.3
5	120	1489	852	-81	0	-311	485	4.02	4.02	4.02	4.02	2	0.09	0.02	0.15	0.00	0.00	22.3
6	120	1989	718	-132	0	-455	657	4.02	4.02	4.02	4.02	2	0.13	0.02	0.13	0.00	0.00	22.3
7	120	1364	926	-54	0	-290	-548	4.02	4.02	4.02	4.02	2	0.09	0.03	0.16	0.00	0.00	22.3
8	120	1946	717	-132	0	-438	657	4.02	4.02	4.02	4.02	2	0.13	0.02	0.13	0.00	0.00	22.3
9	120	1321	925	-54	0	-273	-546	4.02	4.02	4.02	4.02	2	0.09	0.03	0.16	0.00	0.00	22.3
10	120	1821	791	-106	0	-417	562	4.02	4.02	4.02	4.02	2	0.12	0.02	0.14	0.00	0.00	22.3
11	120	1634	853	-82	0	-368	481	4.02	4.02	4.02	4.02	2	0.11	0.02	0.15	0.00	0.00	22.3
12	120	1676	790	-104	0	-360	565	4.02	4.02	4.02	4.02	2	0.11	0.02	0.14	0.00	0.00	22.3
13	120	1489	852	-81	0	-311	485	4.02	4.02	4.02	4.02	2	0.09	0.02	0.15	0.00	0.00	22.3
14	120	1989	718	-132	0	-455	657	4.02	4.02	4.02	4.02	2	0.13	0.02	0.13	0.00	0.00	22.3
15	120	1364	926	-54	0	-290	-548	4.02	4.02	4.02	4.02	2	0.09	0.03	0.16	0.00	0.00	22.3
16	120	1946	717	-132	0	-438	657	4.02	4.02	4.02	4.02	2	0.13	0.02	0.13	0.00	0.00	22.3
17	120	1321	925	-54	0	-273	-546	4.02	4.02	4.02	4.02	2	0.09	0.03	0.16	0.00	0.00	22.3
18	120	5081	944	-244	0	-1046	828	4.02	4.02	4.02	4.02	3	0.30	0.03	0.17	0.00	0.00	22.3
19	120	4387	961	-211	0	-748	813	4.02	4.02	4.02	4.02	3	0.21	0.03	0.17	0.00	0.00	22.3
20	120	4665	1068	-155	0	-714	675	4.02	4.02	4.02	4.02	3	0.20	0.03	0.19	0.00	0.00	22.3
37	120	4463	977	-221	0	-1008	787	4.02	4.02	4.02	4.02	3	0.28	0.03	0.17	0.00	0.00	22.3
38	120	3308	1005	-165	0	-511	761	4.02	4.02	4.02	4.02	3	0.14	0.03	0.18	0.00	0.00	22.3
39	120	3771	1182	-73	0	-454	-666	4.02	4.02	4.02	4.02	3	0.12	0.03	0.21	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	180	2151	672	-121	0	-401	993	4.02	4.02	4.02	4.02	3	0.15	0.02	0.12	0.00	0.00	22.3
2	180	1821	486	-106	0	-354	764	4.02	4.02	4.02	4.02	2	0.12	0.01	0.09	0.00	0.00	22.3
3	180	1634	548	-82	0	-319	748	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
4	180	1676	485	-104	0	-298	765	4.02	4.02	4.02	4.02	2	0.12	0.01	0.09	0.00	0.00	22.3
5	180	1489	547	-81	0	-262	751	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
6	180	1989	413	-132	0	-376	789	4.02	4.02	4.02	4.02	2	0.13	0.01	0.07	0.00	0.00	22.3
7	180	1364	621	-54	0	-258	699	4.02	4.02	4.02	4.02	2	0.11	0.02	0.11	0.00	0.00	22.3
8	180	1946	412	-132	0	-359	790	4.02	4.02	4.02	4.02	2	0.13	0.01	0.07	0.00	0.00	22.3
9	180	1321	620	-54	0	-241	700	4.02	4.02	4.02	4.02	2	0.11	0.02	0.11	0.00	0.00	22.3
10	180	1821	486	-106	0	-354	764	4.02	4.02	4.02	4.02	2	0.12	0.01	0.09	0.00	0.00	22.3
11	180	1634	548	-82	0	-319	748	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
12	180	1676	485	-104	0	-298	765	4.02	4.02	4.02	4.02	2	0.12	0.01	0.09	0.00	0.00	22.3
13	180	1489	547	-81	0	-262	751	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
14	180	1989	413	-132	0	-376	789	4.02	4.02	4.02	4.02	2	0.13	0.01	0.07	0.00	0.00	22.3
15	180	1364	621	-54	0	-258	699	4.02	4.02	4.02	4.02	2	0.11	0.02	0.11	0.00	0.00	22.3
16	180	1946	412	-132	0	-359	790	4.02	4.02	4.02	4.02	2	0.13	0.01	0.07	0.00	0.00	22.3
17	180	1321	620	-54	0	-241	700	4.02	4.02	4.02	4.02	2	0.11	0.02	0.11	0.00	0.00	22.3
18	180	5081	549	-244	0	-900	1009	4.02	4.02	4.02	4.02	3	0.26	0.02	0.10	0.00	0.00	22.3
19	180	4387	566	-211	0	-622	1006	4.02	4.02	4.02	4.02	3	0.17	0.02	0.10	0.00	0.00	22.3
20	180	4665	672	-155	0	-621	988	4.02	4.02	4.02	4.02	3	0.17	0.02	0.12	0.00	0.00	22.3
37	180	4463	581	-221	0	-875	990	4.02	4.02	4.02	4.02	3	0.24	0.02	0.10	0.00	0.00	22.3
38	180	3308	609	-165	0	-412	994	4.02	4.02	4.02	4.02	3	0.16	0.02	0.11	0.00	0.00	22.3
39	180	3771	787	-73	0	-411	921	4.02	4.02	4.02	4.02	3	0.15	0.02	0.14	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	240	2151	276	-121	0	-328	993	4.02	4.02	4.02	4.02	3	0.15	0.01	0.05	0.00	0.00	22.3
2	240	1821	182	-106	0	-291	764	4.02	4.02	4.02	4.02	2	0.12	0.01	0.03	0.00	0.00	22.3
3	240	1634	244	-82	0	-270	764	4.02	4.02	4.02	4.02	2	0.12	0.01	0.04	0.00	0.00	22.3
4	240	1676	181	-104	0	-235	765	4.02	4.02	4.02	4.02	2	0.12	0.01	0.03	0.00	0.00	22.3
5	240	1489	243	-81	0	-214	766	4.02	4.02	4.02	4.02	2	0.12	0.01	0.04	0.00	0.00	22.3
6	240	1989	109	-132	0	-296	789	4.02	4.02	4.02	4.02	2	0.13	0.00	0.02	0.00	0.00	22.3
7	240	1364	317	-54	0	-225	765	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
8	240	1946	108	-132	0	-279	790	4.02	4.02	4.02	4.02	2	0.13	0.00	0.02	0.00	0.00	22.3
9	240	1321	316	-54	0	-209	766	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
10	240	1821	182	-106	0	-291	764	4.02	4.02	4.02	4.02	2	0.12	0.01	0.03	0.00	0.00	22.3
11	240	1634	244	-82	0	-270	764	4.02	4.02	4.02	4.02	2	0.12	0.01	0.04	0.00	0.00	22.3
12	240	1676	181	-104	0	-235	765	4.02	4.02	4.02	4.02	2	0.12	0.01	0.03	0.00	0.00	22.3
13	240	1489	243	-81	0	-214	766	4.02	4.02	4.02	4.02	2	0.12	0.01	0.04	0.00	0.00	22.3
14	240	1989	109	-132	0	-296	789	4.02	4.02	4.02	4.02	2	0.13	0.00	0.02	0.00	0.00	22.3
15	240	1364	317	-54	0	-225	765	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
16	240	1946	108	-132	0	-279	790	4.02	4.02	4.02	4.02	2	0.13	0.00	0.02	0.00	0.00	22.3
17	240	1321	316	-54	0	-209	766	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
18	240	5081	153	-244	0	-753	1009	4.02	4.02	4.02	4.02	3	0.21	0.01	0.04	0.00	0.00	22.3
19	240	4387	170	-211	0	-495	1006	4.02	4.02	4.02	4.02	3	0.17	0.01	0.03	0.00	0.00	22.3
20	240	4665	277	-155	0	-528	988	4.02	4.02	4.02	4.02	3	0.16	0.01	0.05	0.00	0.00	22.3
37	240	4463	186	-221	0	-742	990	4.02	4.02	4.02	4.02	3	0.21	0.01	0.04	0.00	0.00	22.3
38	240	3308	214	-165	0	-313	994	4.02	4.02	4.02	4.02	3	0.16	0.01	0.04	0.00	0.00	22.3
39	240	3771	391	-73	0	-367	992	4.02	4.02	4.02	4.02	3	0.16	0.01	0.07	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	300	2151	-119	-121	0	-255	993	4.02	4.02	4.02	4.02	3	0.15	0.00	0.02	0.00	0.00	22.3
2	300	1821	-122	-106	0	-227	764	4.02	4.02	4.02	4.02	2	0.12	0.00	0.02	0.00	0.00	22.3
3	300	1634	-60	-82	0	-220	764	4.02	4.02	4.02	4.02	2	0.12	0.00	0.01	0.00	0.00	22.3
4	300	1676	-123	-104	0	-173	765	4.02	4.02	4.02	4.02	2	0.12	0.00	0.02	0.00	0.00	22.3
5	300	1489	-61	-81	0	-165	766	4.02	4.02	4.02	4.02	2	0.12	0.00	0.01	0.00	0.00	22.3
6	300	1989	-195	-132	0	-217	789	4.02	4.02	4.02	4.02	2	0.13	0.01	0.03	0.00	0.00	22.3
7	300	1364	13	-54	0	-193	765	4.02	4.02	4.02	4.02	2	0.12	0.00	0.00	0.00	0.00	22.3
8	300	1946	-196	-132	0	-200	790	4.02	4.02	4.02	4.02	2	0.13	0.01	0.03	0.00	0.00	22.3
9	300	1321	12	-54	0	-176	766	4.02	4.02	4.02	4.02	2	0.12	0.00	0.00	0.00	0.00	22.3
10	300	1821	-122	-106	0	-227	764	4.02	4.02	4.02	4.02	2	0.12	0.00	0.02	0.00	0.00	22.3
11	300	1634	-60	-82	0	-220	764	4.02	4.02	4.02	4.02	2	0.12	0.00	0.01	0.00	0.00	22.3
12	300	1676	-123	-104	0	-173	765	4.02	4.02	4.02	4.02	2	0.12	0.00	0.02	0.00	0.00	22.3
13	300	1489	-61	-81	0	-165	766	4.02	4.02	4.02	4.02	2	0.12	0.00	0.01	0.00	0.00	22.3
14	300	1989	-195	-132	0	-217	789	4.02	4.02	4.02	4.02	2	0.13	0.01	0.03	0.00	0.00	22.3

15	300	1364	13	-54	0	-193	765	4.02	4.02	4.02	4.02	2	0.12	0.00	0.00	0.00	0.00	22.3
16	300	1946	-196	-132	0	-200	790	4.02	4.02	4.02	4.02	2	0.13	0.01	0.03	0.00	0.00	22.3
17	300	1321	12	-54	0	-176	766	4.02	4.02	4.02	4.02	2	0.12	0.00	0.00	0.00	0.00	22.3
18	300	5081	-242	-244	0	-606	1009	4.02	4.02	4.02	4.02	3	0.17	0.01	0.04	0.00	0.00	22.3
19	300	4387	-225	-211	0	-369	1006	4.02	4.02	4.02	4.02	3	0.17	0.01	0.04	0.00	0.00	22.3
20	300	4665	-119	-155	0	-434	988	4.02	4.02	4.02	4.02	3	0.16	0.00	0.03	0.00	0.00	22.3
37	300	4463	-210	-221	0	-610	990	4.02	4.02	4.02	4.02	3	0.17	0.01	0.04	0.00	0.00	22.3
38	300	3308	-182	-165	0	-214	994	4.02	4.02	4.02	4.02	3	0.16	0.01	0.03	0.00	0.00	22.3
39	300	3771	-4	-73	0	-323	992	4.02	4.02	4.02	4.02	3	0.16	0.00	0.00	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	360	2151	-514	-121	0	-183	993	4.02	4.02	4.02	4.02	3	0.15	0.01	0.09	0.00	0.00	22.3
2	360	1821	-426	-106	0	-164	764	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
3	360	1634	-364	-82	0	-171	764	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
4	360	1676	-427	-104	0	-110	765	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
5	360	1489	-365	-81	0	-117	766	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
6	360	1989	-499	-132	0	-137	789	4.02	4.02	4.02	4.02	2	0.13	0.01	0.09	0.00	0.00	22.3
7	360	1364	-291	-54	0	-160	765	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
8	360	1946	-500	-132	0	-121	790	4.02	4.02	4.02	4.02	2	0.13	0.01	0.09	0.00	0.00	22.3
9	360	1321	-292	-54	0	-144	766	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
10	360	1821	-426	-106	0	-164	764	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
11	360	1634	-364	-82	0	-171	764	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
12	360	1676	-427	-104	0	-110	765	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
13	360	1489	-365	-81	0	-117	766	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
14	360	1989	-499	-132	0	-137	789	4.02	4.02	4.02	4.02	2	0.13	0.01	0.09	0.00	0.00	22.3
15	360	1364	-291	-54	0	-160	765	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
16	360	1946	-500	-132	0	-121	790	4.02	4.02	4.02	4.02	2	0.13	0.01	0.09	0.00	0.00	22.3
17	360	1321	-292	-54	0	-144	766	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
18	360	5081	-637	-244	0	-459	1009	4.02	4.02	4.02	4.02	3	0.17	0.02	0.11	0.00	0.00	22.3
19	360	4387	-620	-211	0	-242	1006	4.02	4.02	4.02	4.02	3	0.17	0.02	0.11	0.00	0.00	22.3
20	360	4665	-514	-155	0	-341	988	4.02	4.02	4.02	4.02	3	0.16	0.01	0.09	0.00	0.00	22.3
37	360	4463	-605	-221	0	-477	990	4.02	4.02	4.02	4.02	3	0.16	0.02	0.11	0.00	0.00	22.3
38	360	3308	-577	-165	0	-115	994	4.02	4.02	4.02	4.02	3	0.16	0.02	0.10	0.00	0.00	22.3
39	360	3771	-399	-73	0	-280	992	4.02	4.02	4.02	4.02	3	0.16	0.01	0.07	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	420	2151	-910	-121	0	-110	837	4.02	4.02	4.02	4.02	3	0.13	0.03	0.16	0.00	0.00	22.3
2	420	1821	-730	-106	0	-101	622	4.02	4.02	4.02	4.02	2	0.10	0.02	0.13	0.00	0.00	22.3
3	420	1634	-668	-82	0	-122	665	4.02	4.02	4.02	4.02	2	0.11	0.02	0.12	0.00	0.00	22.3
4	420	1676	-731	-104	0	-47	622	4.02	4.02	4.02	4.02	2	0.10	0.02	0.13	0.00	0.00	22.3
5	420	1489	-669	-81	0	-68	666	4.02	4.02	4.02	4.02	2	0.11	0.02	0.12	0.00	0.00	22.3
6	420	1989	-803	-132	0	-58	571	4.02	4.02	4.02	4.02	2	0.09	0.02	0.14	0.00	0.00	22.3
7	420	1364	-595	-54	0	-128	716	4.02	4.02	4.02	4.02	2	0.11	0.02	0.11	0.00	0.00	22.3
8	420	1946	-804	-132	0	-42	571	4.02	4.02	4.02	4.02	2	0.09	0.02	0.14	0.00	0.00	22.3
9	420	1321	-596	-54	0	-112	717	4.02	4.02	4.02	4.02	2	0.11	0.02	0.11	0.00	0.00	22.3
10	420	1821	-730	-106	0	-101	622	4.02	4.02	4.02	4.02	2	0.10	0.02	0.13	0.00	0.00	22.3
11	420	1634	-668	-82	0	-122	665	4.02	4.02	4.02	4.02	2	0.11	0.02	0.12	0.00	0.00	22.3
12	420	1676	-731	-104	0	-47	622	4.02	4.02	4.02	4.02	2	0.10	0.02	0.13	0.00	0.00	22.3
13	420	1489	-669	-81	0	-68	666	4.02	4.02	4.02	4.02	2	0.11	0.02	0.12	0.00	0.00	22.3
14	420	1989	-803	-132	0	-58	571	4.02	4.02	4.02	4.02	2	0.09	0.02	0.14	0.00	0.00	22.3
15	420	1364	-595	-54	0	-128	716	4.02	4.02	4.02	4.02	2	0.11	0.02	0.11	0.00	0.00	22.3
16	420	1946	-804	-132	0	-42	571	4.02	4.02	4.02	4.02	2	0.09	0.02	0.14	0.00	0.00	22.3
17	420	1321	-596	-54	0	-112	717	4.02	4.02	4.02	4.02	2	0.11	0.02	0.11	0.00	0.00	22.3
18	420	5081	-1033	-244	0	-313	741	4.02	4.02	4.02	4.02	3	0.12	0.03	0.18	0.00	0.00	22.3
19	420	4387	-1016	-211	0	-116	759	4.02	4.02	4.02	4.02	3	0.12	0.03	0.18	0.00	0.00	22.3
20	420	4665	-910	-155	0	-248	832	4.02	4.02	4.02	4.02	3	0.14	0.03	0.16	0.00	0.00	22.3
37	420	4463	-1000	-221	0	-344	763	4.02	4.02	4.02	4.02	3	0.13	0.03	0.18	0.00	0.00	22.3
38	420	3308	-972	-165	0	-16	794	4.02	4.02	4.02	4.02	3	0.13	0.03	0.17	0.00	0.00	22.3
39	420	3771	-795	-73	0	-236	915	4.02	4.02	4.02	4.02	3	0.15	0.02	0.14	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	480	2151	-1305	-121	0	-37	-949	4.02	4.02	4.02	4.02	3	0.15	0.04	0.23	0.00	0.00	22.3
2	480	1821	-1035	-106	0	-38	-801	4.02	4.02	4.02	4.02	2	0.13	0.03	0.18	0.00	0.00	22.3
3	480	1634	-973	-82	0	-73	-658	4.02	4.02	4.02	4.02	2	0.10	0.03	0.17	0.00	0.00	22.3
4	480	1676	-1036	-104	0	15	-803	4.02	4.02	4.02	4.02	2	0.13	0.03	0.18	0.00	0.00	22.3
5	480	1489	-974	-81	0	-20	-659	4.02	4.02	4.02	4.02	2	0.10	0.03	0.17	0.00	0.00	22.3
6	480	1989	-1108	-133	0	22	-970	4.02	4.02	4.02	4.02	2	0.16	0.03	0.20	0.00	0.00	22.3
7	480	1364	-900	-54	0	-95	-489	4.02	4.02	4.02	4.02	2	0.08	0.03	0.16	0.00	0.00	22.3
8	480	1946	-1109	-132	0	38	-971	4.02	4.02	4.02	4.02	2	0.16	0.03	0.20	0.00	0.00	22.3
9	480	1321	-901	-54	0	-79	-490	4.02	4.02	4.02	4.02	2	0.08	0.03	0.16	0.00	0.00	22.3
10	480	1821	-1035	-106	0	-38	-801	4.02	4.02	4.02	4.02	2	0.13	0.03	0.18	0.00	0.00	22.3
11	480	1634	-973	-82	0	-73	-658	4.02	4.02	4.02	4.02	2	0.10	0.03	0.17	0.00	0.00	22.3
12	480	1676	-1036	-104	0	15	-803	4.02	4.02	4.02	4.02	2	0.13	0.03	0.18	0.00	0.00	22.3
13	480	1489	-974	-81	0	-20	-659	4.02	4.02	4.02	4.02	2	0.10	0.03	0.17	0.00	0.00	22.3
14	480	1989	-1108	-133	0	22	-970	4.02	4.02	4.02	4.02	2	0.16	0.03	0.20	0.00	0.00	22.3
15	480	1364	-900	-54	0	-95	-489	4.02	4.02	4.02	4.02	2	0.08	0.03	0.16	0.00	0.00	22.3
16	480	1946	-1109	-132	0	38	-971	4.02	4.02	4.02	4.02	2	0.16	0.03	0.20	0.00	0.00	22.3
17	480	1321	-901	-54	0	-79	-490	4.02	4.02	4.02	4.02	2	0.08	0.03	0.16	0.00	0.00	22.3
18	480	5081	-1428	-244	0	-166	-1244	4.02	4.02	4.02	4.02	3	0.21	0.04	0.25	0.00	0.00	22.3
19	480	4387	-1411	-211	0	10	-1197	4.02	4.02	4.02	4.02	3	0.20	0.04	0.25	0.00	0.00	22.3
20	480	4665	-1305	-155	0	-155	-953	4.02	4.02	4.02	4.02	3	0.16	0.04	0.23	0.00	0.00	22.3
37	480	4463	-1396	-221	0	-212	-1170	4.02	4.02	4.02	4.02	3	0.19	0.04	0.25	0.00	0.00	22.3
38	480	3308	-1368	-165	0	83	-1093	4.02	4.02	4.02	4.02	3	0.17	0.04	0.24	0.00	0.00	22.3
39	480	3771	-1190	-73	0	-193	-685	4.02	4.02	4.02	4.02	3	0.11	0.03	0.21	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	540	2151	-1701	-121	0	35	-2051	4.02	4.02	4.02	4.02	3	0.31	0.05	0.30	0.00	0.00	22.3
2	540	1821	-1339	-106	0	26	-1667	4.02	4.02	4.02	4.02	2	0.27	0.04	0.24	0.00	0.00	22.3
3	540	1634	-1277	-82	0	-23	-1486	4.02	4.02	4.02	4.02	2	0.24	0.04	0.23	0.00	0.00	22.3
4	540	1676	-1340	-104	0	78	-1670	4.02	4.02	4.02	4.02	2	0.27	0.04	0.24	0.00	0.00	22.3
5	540	1489	-1278	-81	0	28	-1488	4.02	4.02	4.02	4.02	2	0.24	0.04	0.23	0.00	0.00	22.3
6	540	1989	-1412	-132	0	101	-1880	4.02	4.02	4.02	4.02	2	0.30	0.04	0.25	0.00	0.00	22.3
7	540	1364	-1204	-54	0	-63	-1275	4.02	4.02	4.02	4.02	2	0.20	0.03	0.21	0.00	0.00	22.3
8	540	1946	-1413	-132	0	117	-1881	4.02	4.02	4.02	4.02	2	0.30	0.04	0.25	0.00	0.00	22.3
9	540	1321	-1205	-54	0	-47	-1275	4.02	4.02	4.02	4.02	2	0.20	0.03	0.21	0.00	0.00	22.3
10	540	1821	-1339	-106	0	26	-1667	4.02	4.02	4.02	4.02	2	0.27	0.04	0.24	0.00	0.00	22.3
11	540	1634	-1277	-82	0	-23	-1486	4.02	4.02	4.02	4.02	2	0.24	0.04	0.23	0.00	0.00	22.3
12	540	1676	-1340	-104	0	78	-1670	4.02	4.02	4.02	4.02	2	0.27	0.04	0.24	0.00	0.00	22.3
13	540	1489	-1278	-81	0	28	-1488	4.02	4.02	4.02	4.02	2	0.24	0.04	0.23	0.00	0.00	22.3
14	540	1989	-1412	-132	0	101	-1880	4.02	4.02	4.02	4.02	2	0.30	0.04	0.25	0.00	0.00	22.3
15	540	1364	-1204	-54	0	-63	-1275	4.02	4.02	4.02	4.02	2	0.20	0.03	0.21	0.00	0.00	22.3
16	540	1946	-1413	-132	0	117	-1881	4.02	4.02	4.02	4.02	2	0.30	0.04	0.25	0.00	0.00	22.3
17	540	1321	-1205	-54	0	-47	-1275	4.02	4.02	4.02	4.02	2	0.20	0.03	0.21	0.00	0.00	22.3
18	540	5081	-1824	-244	0	-19	-2419	4.02	4.02	4.02	4.02	3	0.41	0.05	0.32	0.00	0.00	22.3
19	540	4387	-1807	-211	0	137	-2363	4.02	4.02	4.02	4.02	3	0.39	0.05	0.32	0.00	0.00	22.3
20	540	4665	-1700	-155	0	-61	-2055	4.02	4.02	4.02	4.02	3	0.34	0.05	0.30	0.00	0.00	22.3

37	540	4463	-1791	-221	0	-79	-2326	4.02	4.02	4.02	4.02	3	0.38	0.05	0.32	0.00	0.00	22.3
38	540	3308	-1764	-165	0	181	-2232	4.02	4.02	4.02	4.02	3	0.35	0.05	0.31	0.00	0.00	22.3
39	540	3771	-1586	-73	0	-149	-1718	4.02	4.02	4.02	4.02	3	0.28	0.05	0.28	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	600	2151	-2096	-121	0	108	-2329	4.02	4.02	4.02	4.02	3	0.36	0.06	0.37	0.00	0.00	22.3
2	600	1821	-1643	-106	0	89	-1884	4.02	4.02	4.02	4.02	2	0.30	0.05	0.29	0.00	0.00	22.3
3	600	1634	-1581	-82	0	26	-1697	4.02	4.02	4.02	4.02	2	0.27	0.05	0.28	0.00	0.00	22.3
4	600	1676	-1644	-104	0	140	-1887	4.02	4.02	4.02	4.02	2	0.30	0.05	0.29	0.00	0.00	22.3
5	600	1489	-1582	-81	0	77	-1699	4.02	4.02	4.02	4.02	2	0.27	0.05	0.28	0.00	0.00	22.3
6	600	1989	-1716	-132	0	181	-2104	4.02	4.02	4.02	4.02	2	0.34	0.05	0.31	0.00	0.00	22.3
7	600	1364	-1508	-54	0	-30	-1479	4.02	4.02	4.02	4.02	2	0.23	0.04	0.27	0.00	0.00	22.3
8	600	1946	-1717	-132	0	196	-2105	4.02	4.02	4.02	4.02	2	0.34	0.05	0.31	0.00	0.00	22.3
9	600	1321	-1509	-54	0	-15	-1479	4.02	4.02	4.02	4.02	2	0.23	0.04	0.27	0.00	0.00	22.3
10	600	1821	-1643	-106	0	89	-1884	4.02	4.02	4.02	4.02	2	0.30	0.05	0.29	0.00	0.00	22.3
11	600	1634	-1581	-82	0	26	-1697	4.02	4.02	4.02	4.02	2	0.27	0.05	0.28	0.00	0.00	22.3
12	600	1676	-1644	-104	0	140	-1887	4.02	4.02	4.02	4.02	2	0.30	0.05	0.29	0.00	0.00	22.3
13	600	1489	-1582	-81	0	77	-1699	4.02	4.02	4.02	4.02	2	0.27	0.05	0.28	0.00	0.00	22.3
14	600	1989	-1716	-132	0	181	-2104	4.02	4.02	4.02	4.02	2	0.34	0.05	0.31	0.00	0.00	22.3
15	600	1364	-1508	-54	0	-30	-1479	4.02	4.02	4.02	4.02	2	0.23	0.04	0.27	0.00	0.00	22.3
16	600	1946	-1717	-132	0	196	-2105	4.02	4.02	4.02	4.02	2	0.34	0.05	0.31	0.00	0.00	22.3
17	600	1321	-1509	-54	0	-15	-1479	4.02	4.02	4.02	4.02	2	0.23	0.04	0.27	0.00	0.00	22.3
18	600	5081	-2219	-244	0	128	-2709	4.02	4.02	4.02	4.02	3	0.46	0.06	0.40	0.00	0.00	22.3
19	600	4387	-2202	-211	0	263	-2651	4.02	4.02	4.02	4.02	3	0.44	0.06	0.39	0.00	0.00	22.3
20	600	4665	-2096	-155	0	32	-2333	4.02	4.02	4.02	4.02	3	0.39	0.06	0.37	0.00	0.00	22.3
37	600	4463	-2187	-221	0	54	-2613	4.02	4.02	4.02	4.02	3	0.43	0.06	0.39	0.00	0.00	22.3
38	600	3308	-2159	-165	0	280	-2516	4.02	4.02	4.02	4.02	3	0.40	0.06	0.38	0.00	0.00	22.3
39	600	3771	-1981	-73	0	-106	-1986	4.02	4.02	4.02	4.02	3	0.32	0.06	0.35	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

Nome travata: **Trave_404_IP1** Descrizione: **Trave_4 32-25**
ASTA NUM. 19 NI 257 NF 258 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y Permanente qy tot.
qy medio: 375.00 132.00 507.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	1944	1790	-623	0	-2093	-1443	4.02	4.02	4.02	4.02	3	0.54	0.05	0.32	0.00	0.00	22.3
2	0	1620	1343	-546	0	-1831	-1012	4.02	4.02	4.02	4.02	2	0.53	0.04	0.24	0.00	0.00	22.3
3	0	1489	1410	-523	0	-1768	-1209	4.02	4.02	4.02	4.02	2	0.51	0.04	0.25	0.00	0.00	22.3
4	0	1502	1344	-435	0	-1452	-1011	4.02	4.02	4.02	4.02	2	0.42	0.04	0.24	0.00	0.00	22.3
5	0	1372	1411	-412	0	-1389	-1209	4.02	4.02	4.02	4.02	2	0.40	0.04	0.25	0.00	0.00	22.3
6	0	1730	1265	-534	0	-1772	-781	4.02	4.02	4.02	4.02	2	0.52	0.04	0.23	0.00	0.00	22.3
7	0	1296	1488	-458	0	-1562	-1440	4.02	4.02	4.02	4.02	2	0.45	0.04	0.27	0.00	0.00	22.3
8	0	1695	1265	-501	0	-1659	-781	4.02	4.02	4.02	4.02	2	0.48	0.04	0.23	0.00	0.00	22.3
9	0	1261	1488	-425	0	-1448	-1439	4.02	4.02	4.02	4.02	2	0.42	0.04	0.27	0.00	0.00	22.3
10	0	1620	1343	-546	0	-1831	-1012	4.02	4.02	4.02	4.02	2	0.53	0.04	0.24	0.00	0.00	22.3
11	0	1489	1410	-523	0	-1768	-1209	4.02	4.02	4.02	4.02	2	0.51	0.04	0.25	0.00	0.00	22.3
12	0	1502	1344	-435	0	-1452	-1011	4.02	4.02	4.02	4.02	2	0.42	0.04	0.24	0.00	0.00	22.3
13	0	1372	1411	-412	0	-1389	-1209	4.02	4.02	4.02	4.02	2	0.40	0.04	0.25	0.00	0.00	22.3
14	0	1730	1265	-534	0	-1772	-781	4.02	4.02	4.02	4.02	2	0.52	0.04	0.23	0.00	0.00	22.3
15	0	1296	1488	-458	0	-1562	-1440	4.02	4.02	4.02	4.02	2	0.45	0.04	0.27	0.00	0.00	22.3
16	0	1695	1265	-501	0	-1659	-781	4.02	4.02	4.02	4.02	2	0.48	0.04	0.23	0.00	0.00	22.3
17	0	1261	1488	-425	0	-1448	-1439	4.02	4.02	4.02	4.02	2	0.42	0.04	0.27	0.00	0.00	22.3
18	0	4626	1632	-1430	0	-4834	-945	4.02	6.03	4.02	4.02	3	0.92	0.05	0.29	0.00	0.00	22.3
19	0	4431	1699	-951	0	-3179	-1096	4.02	4.02	4.02	4.02	3	0.88	0.05	0.30	0.00	0.00	22.3
20	0	4474	1799	-1046	0	-3555	-1416	4.02	4.02	4.02	4.02	3	0.99	0.05	0.32	0.00	0.00	22.3
37	0	3843	1650	-1406	0	-4763	-1034	4.02	6.03	4.02	4.02	3	0.90	0.05	0.29	0.00	0.00	22.3
38	0	3518	1762	-606	0	-2004	-1285	4.02	4.02	4.02	4.02	3	0.54	0.05	0.31	0.00	0.00	22.3
39	0	3590	1929	-765	0	-2632	-1817	4.02	4.02	4.02	4.02	3	0.71	0.06	0.34	0.00	0.00	22.3

apost= -- aant= 2.01 ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	60	1944	1394	-623	0	-1719	-1194	4.02	4.02	4.02	4.02	3	0.45	0.04	0.25	0.00	0.00	22.3
2	60	1620	1039	-546	0	-1503	-823	4.02	4.02	4.02	4.02	2	0.44	0.03	0.19	0.00	0.00	22.3
3	60	1489	1106	-523	0	-1454	-1014	4.02	4.02	4.02	4.02	2	0.42	0.03	0.20	0.00	0.00	22.3
4	60	1502	1040	-435	0	-1191	-822	4.02	4.02	4.02	4.02	2	0.35	0.03	0.19	0.00	0.00	22.3
5	60	1372	1107	-412	0	-1142	-1014	4.02	4.02	4.02	4.02	2	0.33	0.03	0.20	0.00	0.00	22.3
6	60	1730	961	-534	0	-1452	-600	4.02	4.02	4.02	4.02	2	0.42	0.03	0.17	0.00	0.00	22.3
7	60	1296	1184	-458	0	-1287	-1238	4.02	4.02	4.02	4.02	2	0.37	0.03	0.21	0.00	0.00	22.3
8	60	1695	961	-501	0	-1358	-600	4.02	4.02	4.02	4.02	2	0.40	0.03	0.17	0.00	0.00	22.3
9	60	1261	1184	-425	0	-1193	-1237	4.02	4.02	4.02	4.02	2	0.34	0.03	0.21	0.00	0.00	22.3
10	60	1620	1039	-546	0	-1503	-823	4.02	4.02	4.02	4.02	2	0.44	0.03	0.19	0.00	0.00	22.3
11	60	1489	1106	-523	0	-1454	-1014	4.02	4.02	4.02	4.02	2	0.42	0.03	0.20	0.00	0.00	22.3
12	60	1502	1040	-435	0	-1191	-822	4.02	4.02	4.02	4.02	2	0.35	0.03	0.19	0.00	0.00	22.3
13	60	1372	1107	-412	0	-1142	-1014	4.02	4.02	4.02	4.02	2	0.33	0.03	0.20	0.00	0.00	22.3
14	60	1730	961	-534	0	-1452	-600	4.02	4.02	4.02	4.02	2	0.42	0.03	0.17	0.00	0.00	22.3
15	60	1296	1184	-458	0	-1287	-1238	4.02	4.02	4.02	4.02	2	0.37	0.03	0.21	0.00	0.00	22.3
16	60	1695	961	-501	0	-1358	-600	4.02	4.02	4.02	4.02	2	0.40	0.03	0.17	0.00	0.00	22.3
17	60	1261	1184	-425	0	-1193	-1237	4.02	4.02	4.02	4.02	2	0.34	0.03	0.21	0.00	0.00	22.3
18	60	4626	1236	-1430	0	-3976	-711	4.02	6.03	4.02	4.02	3	0.76	0.04	0.23	0.00	0.00	22.3
19	60	4431	1304	-951	0	-2609	-855	4.02	4.02	4.02	4.02	3	0.73	0.04	0.23	0.00	0.00	22.3
20	60	4474	1404	-1046	0	-2928	-1166	4.02	4.02	4.02	4.02	3	0.82	0.04	0.25	0.00	0.00	22.3
37	60	3843	1255	-1406	0	-3920	-798	4.02	6.03	4.02	4.02	3	0.74	0.04	0.23	0.00	0.00	22.3
38	60	3518	1367	-606	0	-1640	-1038	4.02	4.02	4.02	4.02	3	0.44	0.04	0.24	0.00	0.00	22.3
39	60	3590	1534	-765	0	-2173	-1555	4.02	4.02	4.02	4.02	3	0.59	0.04	0.27	0.00	0.00	22.3

apost= -- aant= 2.01 ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	120	1944	999	-623	0	-1345	736	4.02	4.02	4.02	4.02	3	0.35	0.03	0.18	0.00	0.00	22.3
2	120	1620	735	-546	0	-1176	607	4.02	4.02	4.02	4.02	2	0.34	0.02	0.13	0.00	0.00	22.3
3	120	1489	802	-523	0	-1140	524	4.02	4.02	4.02	4.02	2	0.33	0.02	0.14	0.00	0.00	22.3
4	120	1502	736	-435	0	-930	609	4.02	4.02	4.02	4.02	2	0.27	0.02	0.13	0.00	0.00	22.3
5	120	1372	803	-412	0	-894	525	4.02	4.02	4.02	4.02	2	0.26	0.02	0.14	0.00	0.00	22.3
6	120	1730	657	-534	0	-1131	704	4.02	4.02	4.02	4.02	2	0.33	0.02	0.12	0.00	0.00	22.3
7	120	1296	880	-458	0	-1013	-464	4.02	4.02	4.02	4.02	2	0.29	0.03	0.16	0.00	0.00	22.3
8	120	1695	657	-501	0	-1058	705	4.02	4.02	4.02	4.02	2	0.31	0.02	0.12	0.00	0.00	22.3
9	120	1261	880	-425	0	-939	-463	4.02	4.02	4.02	4.02	2	0.27	0.03	0.16	0.00	0.00	22.3
10	120	1620	735	-546	0	-1176	607	4.02	4.02	4.02	4.02	2	0.34	0.02	0.13	0.00	0.00	22.3
11	120	1489	802	-523	0	-1140	524	4.02	4.02	4.02	4.02	2	0.33	0.02	0.14	0.00	0.00	22.3
12	120	1502	736	-435	0	-930	609	4.02	4.02	4.02	4.02	2	0.27	0.02	0.13	0.00	0.00	22.3

13	120	1372	803	-412	0	-894	525	4.02	4.02	4.02	4.02	2	0.26	0.02	0.14	0.00	0.00	22.3
14	120	1730	657	-534	0	-1131	704	4.02	4.02	4.02	4.02	2	0.33	0.02	0.12	0.00	0.00	22.3
15	120	1296	880	-458	0	-1013	-464	4.02	4.02	4.02	4.02	2	0.29	0.03	0.16	0.00	0.00	22.3
16	120	1695	657	-501	0	-1058	705	4.02	4.02	4.02	4.02	2	0.31	0.02	0.12	0.00	0.00	22.3
17	120	1261	880	-425	0	-939	-463	4.02	4.02	4.02	4.02	2	0.27	0.03	0.16	0.00	0.00	22.3
18	120	4626	841	-1430	0	-3118	964	4.02	4.02	4.02	4.02	3	0.87	0.04	0.23	0.00	0.00	22.3
19	120	4431	908	-951	0	-2038	928	4.02	4.02	4.02	4.02	3	0.57	0.03	0.16	0.00	0.00	22.3
20	120	4474	1008	-1046	0	-2300	779	4.02	4.02	4.02	4.02	3	0.64	0.03	0.18	0.00	0.00	22.3
37	120	3843	859	-1406	0	-3076	907	4.02	4.02	4.02	4.02	3	0.84	0.04	0.23	0.00	0.00	22.3
38	120	3518	971	-606	0	-1276	847	4.02	4.02	4.02	4.02	3	0.35	0.03	0.17	0.00	0.00	22.3
39	120	3590	1138	-765	0	-1714	599	4.02	4.02	4.02	4.02	3	0.47	0.03	0.20	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	180	1944	603	-623	0	-972	960	4.02	4.02	4.02	4.02	3	0.25	0.02	0.11	0.00	0.00	22.3
2	180	1620	430	-546	0	-848	751	4.02	4.02	4.02	4.02	2	0.25	0.02	0.09	0.00	0.00	22.3
3	180	1489	497	-523	0	-826	740	4.02	4.02	4.02	4.02	2	0.24	0.02	0.09	0.00	0.00	22.3
4	180	1502	431	-435	0	-668	754	4.02	4.02	4.02	4.02	2	0.19	0.01	0.08	0.00	0.00	22.3
5	180	1372	498	-412	0	-646	742	4.02	4.02	4.02	4.02	2	0.19	0.01	0.09	0.00	0.00	22.3
6	180	1730	352	-534	0	-811	795	4.02	4.02	4.02	4.02	2	0.24	0.02	0.09	0.00	0.00	22.3
7	180	1296	575	-458	0	-738	709	4.02	4.02	4.02	4.02	2	0.21	0.02	0.10	0.00	0.00	22.3
8	180	1695	352	-501	0	-757	796	4.02	4.02	4.02	4.02	2	0.22	0.02	0.08	0.00	0.00	22.3
9	180	1261	575	-425	0	-684	710	4.02	4.02	4.02	4.02	2	0.20	0.02	0.10	0.00	0.00	22.3
10	180	1620	430	-546	0	-848	751	4.02	4.02	4.02	4.02	2	0.25	0.02	0.09	0.00	0.00	22.3
11	180	1489	497	-523	0	-826	740	4.02	4.02	4.02	4.02	2	0.24	0.02	0.09	0.00	0.00	22.3
12	180	1502	431	-435	0	-668	754	4.02	4.02	4.02	4.02	2	0.19	0.01	0.08	0.00	0.00	22.3
13	180	1372	498	-412	0	-646	742	4.02	4.02	4.02	4.02	2	0.19	0.01	0.09	0.00	0.00	22.3
14	180	1730	352	-534	0	-811	795	4.02	4.02	4.02	4.02	2	0.24	0.02	0.09	0.00	0.00	22.3
15	180	1296	575	-458	0	-738	709	4.02	4.02	4.02	4.02	2	0.21	0.02	0.10	0.00	0.00	22.3
16	180	1695	352	-501	0	-757	796	4.02	4.02	4.02	4.02	2	0.22	0.02	0.08	0.00	0.00	22.3
17	180	1261	575	-425	0	-684	710	4.02	4.02	4.02	4.02	2	0.20	0.02	0.10	0.00	0.00	22.3
18	180	4626	445	-1430	0	-2260	1073	4.02	4.02	4.02	4.02	3	0.63	0.04	0.23	0.00	0.00	22.3
19	180	4431	513	-951	0	-1468	1084	4.02	4.02	4.02	4.02	3	0.41	0.03	0.15	0.00	0.00	22.3
20	180	4474	612	-1046	0	-1672	1015	4.02	4.02	4.02	4.02	3	0.47	0.03	0.17	0.00	0.00	22.3
37	180	3843	464	-1406	0	-2233	1029	4.02	4.02	4.02	4.02	3	0.61	0.04	0.23	0.00	0.00	22.3
38	180	3518	576	-606	0	-913	1047	4.02	4.02	4.02	4.02	3	0.25	0.02	0.10	0.00	0.00	22.3
39	180	3590	743	-765	0	-1255	963	4.02	4.02	4.02	4.02	3	0.34	0.02	0.13	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	240	1944	208	-623	0	-598	960	4.02	4.02	4.02	4.02	3	0.15	0.02	0.10	0.00	0.00	22.3
2	240	1620	126	-546	0	-521	751	4.02	4.02	4.02	4.02	2	0.15	0.02	0.09	0.00	0.00	22.3
3	240	1489	193	-523	0	-512	740	4.02	4.02	4.02	4.02	2	0.15	0.02	0.08	0.00	0.00	22.3
4	240	1502	127	-435	0	-407	754	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
5	240	1372	194	-412	0	-399	742	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
6	240	1730	48	-534	0	-490	795	4.02	4.02	4.02	4.02	2	0.14	0.02	0.09	0.00	0.00	22.3
7	240	1296	271	-458	0	-463	744	4.02	4.02	4.02	4.02	2	0.13	0.01	0.07	0.00	0.00	22.3
8	240	1695	48	-501	0	-457	796	4.02	4.02	4.02	4.02	2	0.13	0.02	0.08	0.00	0.00	22.3
9	240	1261	271	-425	0	-429	745	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
10	240	1620	126	-546	0	-521	751	4.02	4.02	4.02	4.02	2	0.15	0.02	0.09	0.00	0.00	22.3
11	240	1489	193	-523	0	-512	740	4.02	4.02	4.02	4.02	2	0.15	0.02	0.08	0.00	0.00	22.3
12	240	1502	127	-435	0	-407	754	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
13	240	1372	194	-412	0	-399	742	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
14	240	1730	48	-534	0	-490	795	4.02	4.02	4.02	4.02	2	0.14	0.02	0.09	0.00	0.00	22.3
15	240	1296	271	-458	0	-463	744	4.02	4.02	4.02	4.02	2	0.13	0.01	0.07	0.00	0.00	22.3
16	240	1695	48	-501	0	-457	796	4.02	4.02	4.02	4.02	2	0.13	0.02	0.08	0.00	0.00	22.3
17	240	1261	271	-425	0	-429	745	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
18	240	4626	50	-1430	0	-1402	1073	4.02	4.02	4.02	4.02	3	0.39	0.04	0.23	0.00	0.00	22.3
19	240	4431	117	-951	0	-897	1084	4.02	4.02	4.02	4.02	3	0.25	0.03	0.15	0.00	0.00	22.3
20	240	4474	217	-1046	0	-1045	1015	4.02	4.02	4.02	4.02	3	0.29	0.03	0.17	0.00	0.00	22.3
37	240	3843	68	-1406	0	-1390	1029	4.02	4.02	4.02	4.02	3	0.38	0.04	0.23	0.00	0.00	22.3
38	240	3518	180	-606	0	-549	1047	4.02	4.02	4.02	4.02	3	0.17	0.02	0.10	0.00	0.00	22.3
39	240	3590	347	-765	0	-796	1003	4.02	4.02	4.02	4.02	3	0.22	0.02	0.12	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	300	1944	-188	-623	0	-224	960	4.02	4.02	4.02	4.02	3	0.15	0.02	0.10	0.00	0.00	22.3
2	300	1620	-178	-546	0	-193	751	4.02	4.02	4.02	4.02	2	0.12	0.02	0.09	0.00	0.00	22.3
3	300	1489	-111	-523	0	-198	740	4.02	4.02	4.02	4.02	2	0.12	0.02	0.08	0.00	0.00	22.3
4	300	1502	-177	-435	0	-146	754	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
5	300	1372	-110	-412	0	-151	742	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
6	300	1730	-256	-534	0	-170	795	4.02	4.02	4.02	4.02	2	0.13	0.02	0.09	0.00	0.00	22.3
7	300	1296	-33	-458	0	-188	744	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
8	300	1695	-256	-501	0	-156	796	4.02	4.02	4.02	4.02	2	0.13	0.02	0.08	0.00	0.00	22.3
9	300	1261	-33	-425	0	-174	745	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
10	300	1620	-178	-546	0	-193	751	4.02	4.02	4.02	4.02	2	0.12	0.02	0.09	0.00	0.00	22.3
11	300	1489	-111	-523	0	-198	740	4.02	4.02	4.02	4.02	2	0.12	0.02	0.08	0.00	0.00	22.3
12	300	1502	-177	-435	0	-146	754	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
13	300	1372	-110	-412	0	-151	742	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
14	300	1730	-256	-534	0	-170	795	4.02	4.02	4.02	4.02	2	0.13	0.02	0.09	0.00	0.00	22.3
15	300	1296	-33	-458	0	-188	744	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
16	300	1695	-256	-501	0	-156	796	4.02	4.02	4.02	4.02	2	0.13	0.02	0.08	0.00	0.00	22.3
17	300	1261	-33	-425	0	-174	745	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
18	300	4626	-346	-1430	0	-543	1073	4.02	4.02	4.02	4.02	3	0.18	0.04	0.23	0.00	0.00	22.3
19	300	4431	-278	-951	0	-327	1084	4.02	4.02	4.02	4.02	3	0.18	0.03	0.15	0.00	0.00	22.3
20	300	4474	-179	-1046	0	-417	1015	4.02	4.02	4.02	4.02	3	0.17	0.03	0.17	0.00	0.00	22.3
37	300	3843	-327	-1406	0	-546	1029	4.02	4.02	4.02	4.02	3	0.17	0.04	0.23	0.00	0.00	22.3
38	300	3518	-215	-606	0	-185	1047	4.02	4.02	4.02	4.02	3	0.17	0.02	0.10	0.00	0.00	22.3
39	300	3590	-48	-765	0	-337	1003	4.02	4.02	4.02	4.02	3	0.16	0.02	0.12	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	360	1944	-583	-623	0	150	960	4.02	4.02	4.02	4.02	3	0.15	0.02	0.10	0.00	0.00	22.3
2	360	1620	-482	-546	0	135	751	4.02	4.02	4.02	4.02	2	0.12	0.02	0.09	0.00	0.00	22.3
3	360	1489	-415	-523	0	115	740	4.02	4.02	4.02	4.02	2	0.12	0.02	0.08	0.00	0.00	22.3
4	360	1502	-481	-435	0	115	754	4.02	4.02	4.02	4.02	2	0.12	0.01	0.09	0.00	0.00	22.3
5	360	1372	-414	-412	0	96	742	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
6	360	1730	-560	-534	0	150	772	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
7	360	1296	-337	-458	0	86	744	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
8	360	1695	-560	-501	0	144	773	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
9	360	1261	-337	-425	0	80	745	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
10	360	1620	-482	-546	0	135	751	4.02	4.02	4.02	4.02	2	0.12	0.02	0.09	0.00	0.00	22.3
11	360	1489	-415	-523	0	115	740	4.02	4.02	4.02	4.02	2	0.12	0.02	0.08	0.00	0.00	22.3
12	360	1502	-481	-435	0	115	754	4.02	4.02	4.02	4.02	2	0.12	0.01	0.09	0.00	0.00	22.3
13	360	1372	-414	-412	0	96	742	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
14	360	1730	-560	-534	0	150	772	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
15	360	1296	-337	-458	0	86	744	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
16	360	1695	-560	-501	0	144	773	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
17	360	1261	-337	-425	0	80	745	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
18	360	4626	-741	-1430	0	315	1033	4.02	4.02	4.02	4.02	3	0.17	0.04	0.23	0.00	0.00	22.3

19	360	4431	-673	-951	0	243	1084	4.02	4.02	4.02	4.02	3	0.18	0.03	0.15	0.00	0.00	22.3
20	360	4474	-574	-1046	0	210	1015	4.02	4.02	4.02	4.02	3	0.17	0.03	0.17	0.00	0.00	22.3
37	360	3843	-722	-1406	0	297	1002	4.02	4.02	4.02	4.02	3	0.16	0.04	0.23	0.00	0.00	22.3
38	360	3518	-610	-606	0	179	1047	4.02	4.02	4.02	4.02	3	0.17	0.02	0.11	0.00	0.00	22.3
39	360	3590	-444	-765	0	122	1003	4.02	4.02	4.02	4.02	3	0.16	0.02	0.12	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	420	1944	-978	-623	0	524	756	4.02	4.02	4.02	4.02	3	0.14	0.03	0.17	0.00	0.00	22.3
2	420	1620	-786	-546	0	462	556	4.02	4.02	4.02	4.02	2	0.13	0.02	0.14	0.00	0.00	22.3
3	420	1489	-719	-523	0	429	605	4.02	4.02	4.02	4.02	2	0.12	0.02	0.13	0.00	0.00	22.3
4	420	1502	-785	-435	0	376	558	4.02	4.02	4.02	4.02	2	0.11	0.02	0.14	0.00	0.00	22.3
5	420	1372	-718	-412	0	344	608	4.02	4.02	4.02	4.02	2	0.10	0.02	0.13	0.00	0.00	22.3
6	420	1730	-864	-534	0	471	498	4.02	4.02	4.02	4.02	2	0.14	0.03	0.15	0.00	0.00	22.3
7	420	1296	-641	-458	0	361	664	4.02	4.02	4.02	4.02	2	0.10	0.02	0.11	0.00	0.00	22.3
8	420	1695	-864	-501	0	445	500	4.02	4.02	4.02	4.02	2	0.13	0.03	0.15	0.00	0.00	22.3
9	420	1261	-641	-425	0	335	665	4.02	4.02	4.02	4.02	2	0.10	0.02	0.11	0.00	0.00	22.3
10	420	1620	-786	-546	0	462	556	4.02	4.02	4.02	4.02	2	0.13	0.02	0.14	0.00	0.00	22.3
11	420	1489	-719	-523	0	429	605	4.02	4.02	4.02	4.02	2	0.12	0.02	0.13	0.00	0.00	22.3
12	420	1502	-785	-435	0	376	558	4.02	4.02	4.02	4.02	2	0.11	0.02	0.14	0.00	0.00	22.3
13	420	1372	-718	-412	0	344	608	4.02	4.02	4.02	4.02	2	0.10	0.02	0.13	0.00	0.00	22.3
14	420	1730	-864	-534	0	471	498	4.02	4.02	4.02	4.02	2	0.14	0.03	0.15	0.00	0.00	22.3
15	420	1296	-641	-458	0	361	664	4.02	4.02	4.02	4.02	2	0.10	0.02	0.11	0.00	0.00	22.3
16	420	1695	-864	-501	0	445	500	4.02	4.02	4.02	4.02	2	0.13	0.03	0.15	0.00	0.00	22.3
17	420	1261	-641	-425	0	335	665	4.02	4.02	4.02	4.02	2	0.10	0.02	0.11	0.00	0.00	22.3
18	420	4626	-1136	-1430	0	1173	671	4.02	4.02	4.02	4.02	3	0.33	0.04	0.23	0.00	0.00	22.3
19	420	4431	-1069	-951	0	814	768	4.02	4.02	4.02	4.02	3	0.23	0.03	0.19	0.00	0.00	22.3
20	420	4474	-970	-1046	0	838	817	4.02	4.02	4.02	4.02	3	0.23	0.03	0.17	0.00	0.00	22.3
37	420	3843	-1118	-1406	0	1140	650	4.02	4.02	4.02	4.02	3	0.31	0.04	0.23	0.00	0.00	22.3
38	420	3518	-1006	-606	0	543	813	4.02	4.02	4.02	4.02	3	0.15	0.03	0.18	0.00	0.00	22.3
39	420	3590	-839	-765	0	581	895	4.02	4.02	4.02	4.02	3	0.16	0.02	0.15	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	480	1944	-1374	-623	0	897	-1140	4.02	4.02	4.02	4.02	3	0.23	0.04	0.24	0.00	0.00	22.3
2	480	1620	-1091	-546	0	790	-958	4.02	4.02	4.02	4.02	2	0.23	0.03	0.19	0.00	0.00	22.3
3	480	1489	-1024	-523	0	743	-800	4.02	4.02	4.02	4.02	2	0.22	0.03	0.18	0.00	0.00	22.3
4	480	1502	-1090	-435	0	638	-954	4.02	4.02	4.02	4.02	2	0.18	0.03	0.19	0.00	0.00	22.3
5	480	1372	-1023	-412	0	591	-796	4.02	4.02	4.02	4.02	2	0.17	0.03	0.18	0.00	0.00	22.3
6	480	1730	-1169	-534	0	791	-1141	4.02	4.02	4.02	4.02	2	0.23	0.03	0.21	0.00	0.00	22.3
7	480	1296	-946	-458	0	636	-615	4.02	4.02	4.02	4.02	2	0.18	0.03	0.17	0.00	0.00	22.3
8	480	1695	-1169	-501	0	745	-1139	4.02	4.02	4.02	4.02	2	0.22	0.03	0.21	0.00	0.00	22.3
9	480	1261	-946	-425	0	590	-614	4.02	4.02	4.02	4.02	2	0.17	0.03	0.17	0.00	0.00	22.3
10	480	1620	-1091	-546	0	790	-958	4.02	4.02	4.02	4.02	2	0.23	0.03	0.19	0.00	0.00	22.3
11	480	1489	-1024	-523	0	743	-800	4.02	4.02	4.02	4.02	2	0.22	0.03	0.18	0.00	0.00	22.3
12	480	1502	-1090	-435	0	638	-954	4.02	4.02	4.02	4.02	2	0.18	0.03	0.19	0.00	0.00	22.3
13	480	1372	-1023	-412	0	591	-796	4.02	4.02	4.02	4.02	2	0.17	0.03	0.18	0.00	0.00	22.3
14	480	1730	-1169	-534	0	791	-1141	4.02	4.02	4.02	4.02	2	0.23	0.03	0.21	0.00	0.00	22.3
15	480	1296	-946	-458	0	636	-615	4.02	4.02	4.02	4.02	2	0.18	0.03	0.17	0.00	0.00	22.3
16	480	1695	-1169	-501	0	745	-1139	4.02	4.02	4.02	4.02	2	0.22	0.03	0.21	0.00	0.00	22.3
17	480	1261	-946	-425	0	590	-614	4.02	4.02	4.02	4.02	2	0.17	0.03	0.17	0.00	0.00	22.3
18	480	4626	-1532	-1430	0	2031	-1481	4.02	4.02	4.02	4.02	3	0.57	0.04	0.27	0.00	0.00	22.3
19	480	4431	-1464	-951	0	1384	-1274	4.02	4.02	4.02	4.02	3	0.39	0.04	0.26	0.00	0.00	22.3
20	480	4474	-1365	-1046	0	1465	-1065	4.02	4.02	4.02	4.02	3	0.41	0.04	0.24	0.00	0.00	22.3
37	480	3843	-1513	-1406	0	1983	-1471	4.02	4.02	4.02	4.02	3	0.54	0.04	0.27	0.00	0.00	22.3
38	480	3518	-1401	-606	0	906	-1127	4.02	4.02	4.02	4.02	3	0.25	0.04	0.25	0.00	0.00	22.3
39	480	3590	-1235	-765	0	1040	-778	4.02	4.02	4.02	4.02	3	0.28	0.04	0.22	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	540	1944	-1770	-623	0	1271	-2284	4.02	4.02	4.02	4.02	3	0.35	0.05	0.32	0.00	0.00	22.3
2	540	1620	-1395	-546	0	1117	-1857	4.02	4.02	4.02	4.02	2	0.33	0.04	0.25	0.00	0.00	22.3
3	540	1489	-1328	-523	0	1057	-1659	4.02	4.02	4.02	4.02	2	0.31	0.04	0.24	0.00	0.00	22.3
4	540	1502	-1394	-435	0	899	-1853	4.02	4.02	4.02	4.02	2	0.29	0.04	0.25	0.00	0.00	22.3
5	540	1372	-1327	-412	0	838	-1655	4.02	4.02	4.02	4.02	2	0.26	0.04	0.24	0.00	0.00	22.3
6	540	1730	-1473	-534	0	1112	-2087	4.02	4.02	4.02	4.02	2	0.33	0.04	0.26	0.00	0.00	22.3
7	540	1296	-1250	-458	0	910	-1428	4.02	4.02	4.02	4.02	2	0.26	0.04	0.22	0.00	0.00	22.3
8	540	1695	-1473	-501	0	1046	-2085	4.02	4.02	4.02	4.02	2	0.33	0.04	0.26	0.00	0.00	22.3
9	540	1261	-1250	-425	0	844	-1427	4.02	4.02	4.02	4.02	2	0.24	0.04	0.22	0.00	0.00	22.3
10	540	1620	-1395	-546	0	1117	-1857	4.02	4.02	4.02	4.02	2	0.33	0.04	0.25	0.00	0.00	22.3
11	540	1489	-1328	-523	0	1057	-1659	4.02	4.02	4.02	4.02	2	0.31	0.04	0.24	0.00	0.00	22.3
12	540	1502	-1394	-435	0	899	-1853	4.02	4.02	4.02	4.02	2	0.29	0.04	0.25	0.00	0.00	22.3
13	540	1372	-1327	-412	0	838	-1655	4.02	4.02	4.02	4.02	2	0.26	0.04	0.24	0.00	0.00	22.3
14	540	1730	-1473	-534	0	1112	-2087	4.02	4.02	4.02	4.02	2	0.33	0.04	0.26	0.00	0.00	22.3
15	540	1296	-1250	-458	0	910	-1428	4.02	4.02	4.02	4.02	2	0.26	0.04	0.22	0.00	0.00	22.3
16	540	1695	-1473	-501	0	1046	-2085	4.02	4.02	4.02	4.02	2	0.33	0.04	0.26	0.00	0.00	22.3
17	540	1261	-1250	-425	0	844	-1427	4.02	4.02	4.02	4.02	2	0.24	0.04	0.22	0.00	0.00	22.3
18	540	4626	-1927	-1430	0	2889	-2719	4.02	4.02	4.02	4.02	3	0.81	0.06	0.34	0.00	0.00	22.3
19	540	4431	-1860	-951	0	1955	-2472	4.02	4.02	4.02	4.02	3	0.54	0.05	0.33	0.00	0.00	22.3
20	540	4474	-1760	-1046	0	2093	-2203	4.02	4.02	4.02	4.02	3	0.58	0.05	0.31	0.00	0.00	22.3
37	540	3843	-1909	-1406	0	2827	-2698	4.02	4.02	4.02	4.02	3	0.77	0.06	0.34	0.00	0.00	22.3
38	540	3518	-1797	-606	0	1270	-2287	4.02	4.02	4.02	4.02	3	0.37	0.05	0.32	0.00	0.00	22.3
39	540	3590	-1630	-765	0	1499	-1837	4.02	4.02	4.02	4.02	3	0.41	0.05	0.29	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	600	1944	-2165	-623	0	1645	-2568	4.02	4.02	4.02	4.02	3	0.43	0.06	0.39	0.00	0.00	22.3
2	600	1620	-1699	-546	0	1445	-2079	4.02	4.02	4.02	4.02	2	0.42	0.05	0.30	0.00	0.00	22.3
3	600	1489	-1632	-523	0	1371	-1875	4.02	4.02	4.02	4.02	2	0.40	0.05	0.29	0.00	0.00	22.3
4	600	1502	-1698	-435	0	1160	-2075	4.02	4.02	4.02	4.02	2	0.34	0.05	0.30	0.00	0.00	22.3
5	600	1372	-1631	-412	0	1086	-1871	4.02	4.02	4.02	4.02	2	0.31	0.05	0.29	0.00	0.00	22.3
6	600	1730	-1777	-534	0	1432	-2316	4.02	4.02	4.02	4.02	2	0.42	0.05	0.32	0.00	0.00	22.3
7	600	1296	-1554	-458	0	1185	-1636	4.02	4.02	4.02	4.02	2	0.34	0.05	0.28	0.00	0.00	22.3
8	600	1695	-1777	-501	0	1346	-2314	4.02	4.02	4.02	4.02	2	0.39	0.05	0.32	0.00	0.00	22.3
9	600	1261	-1554	-425	0	1099	-1635	4.02	4.02	4.02	4.02	2	0.32	0.05	0.28	0.00	0.00	22.3
10	600	1620	-1699	-546	0	1445	-2079	4.02	4.02	4.02	4.02	2	0.42	0.05	0.30	0.00	0.00	22.3
11	600	1489	-1632	-523	0	1371	-1875	4.02	4.02	4.02	4.02	2	0.40	0.05	0.29	0.00	0.00	22.3
12	600	1502	-1698	-435	0	1160	-2075	4.02	4.02	4.02	4.02	2	0.34	0.05	0.30	0.00	0.00	22.3
13	600	1372	-1631	-412	0	1086	-1871	4.02	4.02	4.02	4.02	2	0.31	0.05	0.29	0.00	0.00	22.3
14	600	1730	-1777	-534	0	1432	-2316	4.02	4.02	4.02	4.02	2	0.42	0.05	0.32	0.00	0.00	22.3
15	600	1296	-1554	-458	0	1185	-1636	4.02	4.02	4.02	4.02	2	0.34	0.05	0.28	0.00	0.00	22.3
16	600	1695	-1777	-501	0	1346	-2314	4.02	4.02	4.02	4.02	2	0.39	0.05	0.32	0.00	0.00	22.3
17	600	1261	-1554	-425	0	1099	-1635	4.02	4.02	4.02	4.02	2	0.32	0.05	0.28	0.00	0.00	22.3
18	600	4626	-2323	-1430	0	3747	-3018	6.03	4.02	4.02	4.02	3	0.72	0.07	0.41	0.00	0.00	22.3
19	600	4431	-2255	-951	0	2525	-2765	4.02	4.02	4.02	4.02	3	0.70	0.07	0.40	0.00	0.00	22.3
20	600	4474	-2156	-1046	0	2720	-2486	4.02	4.02	4.02	4.02	3	0.76	0.06	0.38	0.00	0.00	22.3
37	600	3843	-2304	-1406	0	3670	-2996	6.03	4.02	4.02	4.02	3	0.69	0.07	0.41	0.00	0.00	22.3
38	600	3518	-2192	-606	0	1634	-2574	4.02	4.02	4.02	4.02	3	0.44	0.06	0.39	0.00	0.00	22.3
39	600	3590	-2026	-765	0	1958	-2109	4.02	4.02	4.02	4.02	3	0.53	0.06	0.36	0.00	0.00	22.3

apost= 2.01 aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

Nome travata: **Trave_404_IP1** Descrizione: **Trave_4 32-25**
ASTA NUM. 20 NI 258 NF 266 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y Permanente qy tot.
qy medio: 375.00 132.00 507.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	3063	1753	-846	0	-2302	-1308	4.02	4.02	4.02	4.02	3	0.62	0.05	0.31	0.00	0.00	22.3
2	0	2499	1299	-677	0	-1817	-866	4.02	4.02	4.02	4.02	2	0.54	0.04	0.23	0.00	0.00	22.3
3	0	2453	1376	-676	0	-1825	-1082	4.02	4.02	4.02	4.02	2	0.55	0.04	0.25	0.00	0.00	22.3
4	0	2259	1322	-625	0	-1716	-931	4.02	4.02	4.02	4.02	2	0.51	0.04	0.24	0.00	0.00	22.3
5	0	2213	1399	-625	0	-1724	-1147	4.02	4.02	4.02	4.02	2	0.51	0.04	0.25	0.00	0.00	22.3
6	0	2469	1217	-660	0	-1773	-637	4.02	4.02	4.02	4.02	2	0.53	0.04	0.22	0.00	0.00	22.3
7	0	2316	1474	-658	0	-1798	-1356	4.02	4.02	4.02	4.02	2	0.54	0.04	0.26	0.00	0.00	22.3
8	0	2397	1224	-644	0	-1743	-656	4.02	4.02	4.02	4.02	2	0.52	0.04	0.22	0.00	0.00	22.3
9	0	2244	1481	-642	0	-1768	-1376	4.02	4.02	4.02	4.02	2	0.53	0.04	0.26	0.00	0.00	22.3
10	0	2499	1299	-677	0	-1817	-866	4.02	4.02	4.02	4.02	2	0.54	0.04	0.23	0.00	0.00	22.3
11	0	2453	1376	-676	0	-1825	-1082	4.02	4.02	4.02	4.02	2	0.55	0.04	0.25	0.00	0.00	22.3
12	0	2259	1322	-625	0	-1716	-931	4.02	4.02	4.02	4.02	2	0.51	0.04	0.24	0.00	0.00	22.3
13	0	2213	1399	-625	0	-1724	-1147	4.02	4.02	4.02	4.02	2	0.51	0.04	0.25	0.00	0.00	22.3
14	0	2469	1217	-660	0	-1773	-637	4.02	4.02	4.02	4.02	2	0.53	0.04	0.22	0.00	0.00	22.3
15	0	2316	1474	-658	0	-1798	-1356	4.02	4.02	4.02	4.02	2	0.54	0.04	0.26	0.00	0.00	22.3
16	0	2397	1224	-644	0	-1743	-656	4.02	4.02	4.02	4.02	2	0.52	0.04	0.22	0.00	0.00	22.3
17	0	2244	1481	-642	0	-1768	-1376	4.02	4.02	4.02	4.02	2	0.53	0.04	0.26	0.00	0.00	22.3
18	0	6918	1344	-1824	0	-4897	-276	4.02	6.03	4.02	4.02	3	0.98	0.06	0.29	0.00	0.00	22.3
19	0	7739	1389	-1515	0	-4180	-510	4.02	6.03	4.02	4.02	3	0.85	0.05	0.25	0.00	0.00	22.3
20	0	7226	1559	-1559	0	-4250	-906	4.02	6.03	4.02	4.02	3	0.86	0.05	0.28	0.00	0.00	22.3
37	0	5246	1455	-1659	0	-4406	-495	4.02	6.03	4.02	4.02	3	0.85	0.05	0.27	0.00	0.00	22.3
38	0	6613	1530	-1143	0	-3211	-885	4.02	4.02	4.02	4.02	3	0.96	0.04	0.27	0.00	0.00	22.3
39	0	5759	1813	-1216	0	-3328	-1545	4.02	4.02	4.02	4.02	3	0.96	0.05	0.32	0.00	0.00	22.3

apost= -- aant= 2.01 ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	60	3063	1358	-846	0	-1794	-1062	4.02	4.02	4.02	4.02	3	0.48	0.04	0.24	0.00	0.00	22.3
2	60	2499	995	-677	0	-1411	-682	4.02	4.02	4.02	4.02	2	0.42	0.03	0.18	0.00	0.00	22.3
3	60	2453	1072	-676	0	-1419	-890	4.02	4.02	4.02	4.02	2	0.42	0.03	0.19	0.00	0.00	22.3
4	60	2259	1018	-625	0	-1341	-745	4.02	4.02	4.02	4.02	2	0.40	0.03	0.18	0.00	0.00	22.3
5	60	2213	1095	-625	0	-1349	-953	4.02	4.02	4.02	4.02	2	0.40	0.03	0.19	0.00	0.00	22.3
6	60	2469	913	-660	0	-1377	464	4.02	4.02	4.02	4.02	2	0.41	0.03	0.16	0.00	0.00	22.3
7	60	2316	1170	-658	0	-1403	-1155	4.02	4.02	4.02	4.02	2	0.42	0.03	0.21	0.00	0.00	22.3
8	60	2397	920	-644	0	-1357	-479	4.02	4.02	4.02	4.02	2	0.41	0.03	0.16	0.00	0.00	22.3
9	60	2244	1177	-642	0	-1383	-1175	4.02	4.02	4.02	4.02	2	0.41	0.03	0.21	0.00	0.00	22.3
10	60	2499	995	-677	0	-1411	-682	4.02	4.02	4.02	4.02	2	0.42	0.03	0.18	0.00	0.00	22.3
11	60	2453	1072	-676	0	-1419	-890	4.02	4.02	4.02	4.02	2	0.42	0.03	0.19	0.00	0.00	22.3
12	60	2259	1018	-625	0	-1341	-745	4.02	4.02	4.02	4.02	2	0.40	0.03	0.18	0.00	0.00	22.3
13	60	2213	1095	-625	0	-1349	-953	4.02	4.02	4.02	4.02	2	0.40	0.03	0.19	0.00	0.00	22.3
14	60	2469	913	-660	0	-1377	464	4.02	4.02	4.02	4.02	2	0.41	0.03	0.16	0.00	0.00	22.3
15	60	2316	1170	-658	0	-1403	-1155	4.02	4.02	4.02	4.02	2	0.42	0.03	0.21	0.00	0.00	22.3
16	60	2397	920	-644	0	-1357	-479	4.02	4.02	4.02	4.02	2	0.41	0.03	0.16	0.00	0.00	22.3
17	60	2244	1177	-642	0	-1383	-1175	4.02	4.02	4.02	4.02	2	0.41	0.03	0.21	0.00	0.00	22.3
18	60	6918	949	-1824	0	-3802	892	4.02	6.03	4.02	4.02	3	0.76	0.06	0.29	0.00	0.00	22.3
19	60	7739	994	-1515	0	-3271	708	4.02	6.03	4.02	4.02	3	0.67	0.05	0.24	0.00	0.00	22.3
20	60	7226	1164	-1559	0	-3315	-679	4.02	6.03	4.02	4.02	3	0.67	0.05	0.25	0.00	0.00	22.3
37	60	5246	1060	-1659	0	-3411	795	4.02	4.02	4.02	4.02	3	0.97	0.05	0.27	0.00	0.00	22.3
38	60	6613	1135	-1143	0	-2525	-660	4.02	4.02	4.02	4.02	3	0.75	0.04	0.20	0.00	0.00	22.3
39	60	5759	1418	-1216	0	-2598	-1294	4.02	4.02	4.02	4.02	3	0.75	0.04	0.25	0.00	0.00	22.3

apost= -- aant= 2.01 ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	120	3063	962	-846	0	-1287	808	4.02	4.02	4.02	4.02	3	0.34	0.03	0.17	0.00	0.00	22.3
2	120	2499	691	-677	0	-1005	677	4.02	4.02	4.02	4.02	2	0.30	0.02	0.12	0.00	0.00	22.3
3	120	2453	768	-676	0	-1013	593	4.02	4.02	4.02	4.02	2	0.30	0.02	0.14	0.00	0.00	22.3
4	120	2259	714	-625	0	-966	651	4.02	4.02	4.02	4.02	2	0.29	0.02	0.13	0.00	0.00	22.3
5	120	2213	791	-625	0	-974	567	4.02	4.02	4.02	4.02	2	0.29	0.02	0.14	0.00	0.00	22.3
6	120	2469	609	-660	0	-982	766	4.02	4.02	4.02	4.02	2	0.29	0.02	0.11	0.00	0.00	22.3
7	120	2316	866	-658	0	-1009	486	4.02	4.02	4.02	4.02	2	0.30	0.03	0.15	0.00	0.00	22.3
8	120	2397	616	-644	0	-970	758	4.02	4.02	4.02	4.02	2	0.29	0.02	0.11	0.00	0.00	22.3
9	120	2244	873	-642	0	-997	478	4.02	4.02	4.02	4.02	2	0.30	0.03	0.16	0.00	0.00	22.3
10	120	2499	691	-677	0	-1005	677	4.02	4.02	4.02	4.02	2	0.30	0.02	0.12	0.00	0.00	22.3
11	120	2453	768	-676	0	-1013	593	4.02	4.02	4.02	4.02	2	0.30	0.02	0.14	0.00	0.00	22.3
12	120	2259	714	-625	0	-966	651	4.02	4.02	4.02	4.02	2	0.29	0.02	0.13	0.00	0.00	22.3
13	120	2213	791	-625	0	-974	567	4.02	4.02	4.02	4.02	2	0.29	0.02	0.14	0.00	0.00	22.3
14	120	2469	609	-660	0	-982	766	4.02	4.02	4.02	4.02	2	0.29	0.02	0.11	0.00	0.00	22.3
15	120	2316	866	-658	0	-1009	486	4.02	4.02	4.02	4.02	2	0.30	0.03	0.15	0.00	0.00	22.3
16	120	2397	616	-644	0	-970	758	4.02	4.02	4.02	4.02	2	0.29	0.02	0.11	0.00	0.00	22.3
17	120	2244	873	-642	0	-997	478	4.02	4.02	4.02	4.02	2	0.30	0.03	0.16	0.00	0.00	22.3
18	120	6918	553	-1824	0	-2708	1076	4.02	4.02	4.02	4.02	3	0.81	0.06	0.29	0.00	0.00	22.3
19	120	7739	598	-1515	0	-2362	926	4.02	4.02	4.02	4.02	3	0.73	0.05	0.24	0.00	0.00	22.3
20	120	7226	768	-1559	0	-2380	879	4.02	4.02	4.02	4.02	3	0.72	0.05	0.25	0.00	0.00	22.3
37	120	5246	664	-1659	0	-2416	1099	4.02	4.02	4.02	4.02	3	0.69	0.05	0.27	0.00	0.00	22.3
38	120	6613	739	-1143	0	-1839	851	4.02	4.02	4.02	4.02	3	0.55	0.04	0.18	0.00	0.00	22.3
39	120	5759	1022	-1216	0	-1869	673	4.02	4.02	4.02	4.02	3	0.54	0.04	0.20	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	180	3063	567	-846	0	-779	1001	4.02	4.02	4.02	4.02	3	0.21	0.03	0.14	0.00	0.00	22.3
2	180	2499	386	-677	0	-599	791	4.02	4.02	4.02	4.02	2	0.18	0.02	0.11	0.00	0.00	22.3
3	180	2453	463	-676	0	-608	764	4.02	4.02	4.02	4.02	2	0.18	0.02	0.11	0.00	0.00	22.3
4	180	2259	409	-625	0	-591	781	4.02	4.02	4.02	4.02	2	0.18	0.02	0.10	0.00	0.00	22.3
5	180	2213	486	-625	0	-600	768	4.02	4.02	4.02	4.02	2	0.18	0.02	0.10	0.00	0.00	22.3
6	180	2469	304	-660	0	-586	823	4.02	4.02	4.02	4.02	2	0.18	0.02	0.11	0.00	0.00	22.3
7	180	2316	561	-658	0	-615	759	4.02	4.02	4.02	4.02	2	0.18	0.02	0.11	0.00	0.00	22.3
8	180	2397	311	-644	0	-584	820	4.02	4.02	4.02	4.02	2	0.17	0.02	0.10	0.00	0.00	22.3
9	180	2244	568	-642	0	-612	756	4.02	4.02	4.02	4.02	2	0.18	0.02	0.10	0.00	0.00	22.3
10	180	2499	386	-677	0	-599	791	4.02	4.02	4.02	4.02	2	0.18	0.02	0.11	0.00	0.00	22.3
11	180	2453	463	-676	0	-608	764	4.02	4.02	4.02	4.02	2	0.18	0.02	0.11	0.00	0.00	22.3
12	180	2259	409	-625	0	-591	781	4.02	4.02	4.02	4.02	2	0.18	0.02	0.10	0.00	0.00	22.3
13	180	2213	486	-625	0	-600	768	4.02	4.02	4.02	4.02	2	0.18	0.02	0.10	0.00	0.00	22.3
14	180	2469	304	-660	0	-586	823	4.02	4.02	4.02	4.02	2	0.18	0.02	0.11	0.00	0.00	22.3
15	180	2316	561	-658	0	-615	759	4.02	4.02	4.02	4.02	2	0.18	0.02	0.11	0.00	0.00	22.3
16	180	2397	311	-644	0	-584	820	4.02	4.02	4.02	4.02	2	0.17	0.02	0.10	0.00	0.00	22.3

17	180	2244	568	-642	0	-612	756	4.02	4.02	4.02	4.02	2	0.18	0.02	0.10	0.00	0.00	22.3
18	180	6918	158	-1824	0	-1613	1076	4.02	4.02	4.02	4.02	3	0.49	0.06	0.29	0.00	0.00	22.3
19	180	7739	203	-1515	0	-1453	926	4.02	4.02	4.02	4.02	3	0.45	0.05	0.24	0.00	0.00	22.3
20	180	7226	372	-1559	0	-1445	937	4.02	4.02	4.02	4.02	3	0.44	0.05	0.25	0.00	0.00	22.3
37	180	5246	268	-1659	0	-1421	1099	4.02	4.02	4.02	4.02	3	0.41	0.05	0.27	0.00	0.00	22.3
38	180	6613	344	-1143	0	-1153	889	4.02	4.02	4.02	4.02	3	0.34	0.04	0.18	0.00	0.00	22.3
39	180	5759	626	-1216	0	-1139	927	4.02	4.02	4.02	4.02	3	0.33	0.04	0.20	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	240	3063	171	-846	0	-272	1001	4.02	4.02	4.02	4.02	3	0.16	0.03	0.14	0.00	0.00	22.3
2	240	2499	82	-677	0	-193	791	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
3	240	2453	159	-676	0	-202	764	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
4	240	2259	105	-625	0	-216	781	4.02	4.02	4.02	4.02	2	0.13	0.02	0.10	0.00	0.00	22.3
5	240	2213	182	-625	0	-225	768	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
6	240	2469	0	-660	0	-190	823	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
7	240	2316	257	-658	0	-220	784	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
8	240	2397	7	-644	0	-197	820	4.02	4.02	4.02	4.02	2	0.13	0.02	0.10	0.00	0.00	22.3
9	240	2244	264	-642	0	-227	785	4.02	4.02	4.02	4.02	2	0.13	0.02	0.10	0.00	0.00	22.3
10	240	2499	82	-677	0	-193	791	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
11	240	2453	159	-676	0	-202	764	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
12	240	2259	105	-625	0	-216	781	4.02	4.02	4.02	4.02	2	0.13	0.02	0.10	0.00	0.00	22.3
13	240	2213	182	-625	0	-225	768	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
14	240	2469	0	-660	0	-190	823	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
15	240	2316	257	-658	0	-220	784	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
16	240	2397	7	-644	0	-197	820	4.02	4.02	4.02	4.02	2	0.13	0.02	0.10	0.00	0.00	22.3
17	240	2244	264	-642	0	-227	785	4.02	4.02	4.02	4.02	2	0.13	0.02	0.10	0.00	0.00	22.3
18	240	6918	-238	-1824	0	-519	1076	4.02	4.02	4.02	4.02	3	0.19	0.06	0.29	0.00	0.00	22.3
19	240	7739	-193	-1515	0	-544	926	4.02	4.02	4.02	4.02	3	0.17	0.05	0.24	0.00	0.00	22.3
20	240	7226	-23	-1559	0	-510	937	4.02	4.02	4.02	4.02	3	0.17	0.05	0.25	0.00	0.00	22.3
37	240	5246	-127	-1659	0	-426	1099	4.02	4.02	4.02	4.02	3	0.19	0.05	0.27	0.00	0.00	22.3
38	240	6613	-52	-1143	0	-467	889	4.02	4.02	4.02	4.02	3	0.16	0.04	0.18	0.00	0.00	22.3
39	240	5759	231	-1216	0	-410	927	4.02	4.02	4.02	4.02	3	0.16	0.04	0.20	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	300	3063	-224	-846	0	236	1001	4.02	4.02	4.02	4.02	3	0.16	0.03	0.14	0.00	0.00	22.3
2	300	2499	-222	-677	0	214	791	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
3	300	2453	-145	-676	0	204	764	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
4	300	2259	-199	-625	0	160	781	4.02	4.02	4.02	4.02	2	0.13	0.02	0.10	0.00	0.00	22.3
5	300	2213	-122	-625	0	150	768	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
6	300	2469	-304	-660	0	206	823	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
7	300	2316	-47	-658	0	175	784	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
8	300	2397	-297	-644	0	189	820	4.02	4.02	4.02	4.02	2	0.13	0.02	0.10	0.00	0.00	22.3
9	300	2244	-40	-642	0	159	785	4.02	4.02	4.02	4.02	2	0.13	0.02	0.10	0.00	0.00	22.3
10	300	2499	-222	-677	0	214	791	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
11	300	2453	-145	-676	0	204	764	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
12	300	2259	-199	-625	0	160	781	4.02	4.02	4.02	4.02	2	0.13	0.02	0.10	0.00	0.00	22.3
13	300	2213	-122	-625	0	150	768	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
14	300	2469	-304	-660	0	206	823	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
15	300	2316	-47	-658	0	175	784	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
16	300	2397	-297	-644	0	189	820	4.02	4.02	4.02	4.02	2	0.13	0.02	0.10	0.00	0.00	22.3
17	300	2244	-40	-642	0	159	785	4.02	4.02	4.02	4.02	2	0.13	0.02	0.10	0.00	0.00	22.3
18	300	6918	-633	-1824	0	575	1076	4.02	4.02	4.02	4.02	3	0.19	0.06	0.29	0.00	0.00	22.3
19	300	7739	-588	-1515	0	365	926	4.02	4.02	4.02	4.02	3	0.17	0.05	0.24	0.00	0.00	22.3
20	300	7226	-419	-1559	0	426	937	4.02	4.02	4.02	4.02	3	0.17	0.05	0.25	0.00	0.00	22.3
37	300	5246	-523	-1659	0	569	1099	4.02	4.02	4.02	4.02	3	0.19	0.05	0.27	0.00	0.00	22.3
38	300	6613	-447	-1143	0	219	889	4.02	4.02	4.02	4.02	3	0.16	0.04	0.18	0.00	0.00	22.3
39	300	5759	-165	-1216	0	320	927	4.02	4.02	4.02	4.02	3	0.16	0.04	0.20	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	360	3063	-619	-846	0	744	1001	4.02	4.02	4.02	4.02	3	0.20	0.03	0.14	0.00	0.00	22.3
2	360	2499	-526	-677	0	620	790	4.02	4.02	4.02	4.02	2	0.19	0.02	0.11	0.00	0.00	22.3
3	360	2453	-449	-676	0	610	764	4.02	4.02	4.02	4.02	2	0.18	0.02	0.11	0.00	0.00	22.3
4	360	2259	-503	-625	0	535	781	4.02	4.02	4.02	4.02	2	0.16	0.02	0.10	0.00	0.00	22.3
5	360	2213	-426	-625	0	525	768	4.02	4.02	4.02	4.02	2	0.16	0.02	0.10	0.00	0.00	22.3
6	360	2469	-608	-660	0	601	766	4.02	4.02	4.02	4.02	2	0.18	0.02	0.11	0.00	0.00	22.3
7	360	2316	-351	-658	0	569	784	4.02	4.02	4.02	4.02	2	0.17	0.02	0.11	0.00	0.00	22.3
8	360	2397	-601	-644	0	575	767	4.02	4.02	4.02	4.02	2	0.17	0.02	0.11	0.00	0.00	22.3
9	360	2244	-344	-642	0	544	785	4.02	4.02	4.02	4.02	2	0.16	0.02	0.10	0.00	0.00	22.3
10	360	2499	-526	-677	0	620	790	4.02	4.02	4.02	4.02	2	0.19	0.02	0.11	0.00	0.00	22.3
11	360	2453	-449	-676	0	610	764	4.02	4.02	4.02	4.02	2	0.18	0.02	0.11	0.00	0.00	22.3
12	360	2259	-503	-625	0	535	781	4.02	4.02	4.02	4.02	2	0.16	0.02	0.10	0.00	0.00	22.3
13	360	2213	-426	-625	0	525	768	4.02	4.02	4.02	4.02	2	0.16	0.02	0.10	0.00	0.00	22.3
14	360	2469	-608	-660	0	601	766	4.02	4.02	4.02	4.02	2	0.18	0.02	0.11	0.00	0.00	22.3
15	360	2316	-351	-658	0	569	784	4.02	4.02	4.02	4.02	2	0.17	0.02	0.11	0.00	0.00	22.3
16	360	2397	-601	-644	0	575	767	4.02	4.02	4.02	4.02	2	0.17	0.02	0.11	0.00	0.00	22.3
17	360	2244	-344	-642	0	544	785	4.02	4.02	4.02	4.02	2	0.16	0.02	0.10	0.00	0.00	22.3
18	360	6918	-1028	-1824	0	1670	813	4.02	4.02	4.02	4.02	3	0.50	0.06	0.29	0.00	0.00	22.3
19	360	7739	-983	-1515	0	1274	718	4.02	4.02	4.02	4.02	3	0.39	0.05	0.24	0.00	0.00	22.3
20	360	7226	-814	-1559	0	1361	847	4.02	4.02	4.02	4.02	3	0.41	0.05	0.25	0.00	0.00	22.3
37	360	5246	-918	-1659	0	1565	937	4.02	4.02	4.02	4.02	3	0.45	0.05	0.27	0.00	0.00	22.3
38	360	6613	-842	-1143	0	904	779	4.02	4.02	4.02	4.02	3	0.27	0.04	0.18	0.00	0.00	22.3
39	360	5759	-560	-1216	0	1049	927	4.02	4.02	4.02	4.02	3	0.30	0.04	0.20	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	420	3063	-1015	-846	0	1251	756	4.02	4.02	4.02	4.02	3	0.33	0.03	0.18	0.00	0.00	22.3
2	420	2499	-830	-677	0	1026	537	4.02	4.02	4.02	4.02	2	0.31	0.02	0.15	0.00	0.00	22.3
3	420	2453	-753	-676	0	1016	606	4.02	4.02	4.02	4.02	2	0.30	0.02	0.13	0.00	0.00	22.3
4	420	2259	-807	-625	0	910	556	4.02	4.02	4.02	4.02	2	0.27	0.02	0.14	0.00	0.00	22.3
5	420	2213	-730	-625	0	900	625	4.02	4.02	4.02	4.02	2	0.27	0.02	0.13	0.00	0.00	22.3
6	420	2469	-912	-660	0	997	463	4.02	4.02	4.02	4.02	2	0.30	0.03	0.16	0.00	0.00	22.3
7	420	2316	-655	-658	0	963	693	4.02	4.02	4.02	4.02	2	0.29	0.02	0.12	0.00	0.00	22.3
8	420	2397	-905	-644	0	962	469	4.02	4.02	4.02	4.02	2	0.29	0.03	0.16	0.00	0.00	22.3
9	420	2244	-648	-642	0	929	699	4.02	4.02	4.02	4.02	2	0.28	0.02	0.12	0.00	0.00	22.3
10	420	2499	-830	-677	0	1026	537	4.02	4.02	4.02	4.02	2	0.31	0.02	0.15	0.00	0.00	22.3
11	420	2453	-753	-676	0	1016	606	4.02	4.02	4.02	4.02	2	0.30	0.02	0.13	0.00	0.00	22.3
12	420	2259	-807	-625	0	910	556	4.02	4.02	4.02	4.02	2	0.27	0.02	0.14	0.00	0.00	22.3
13	420	2213	-730	-625	0	900	625	4.02	4.02	4.02	4.02	2	0.27	0.02	0.13	0.00	0.00	22.3
14	420	2469	-912	-660	0	997	463	4.02	4.02	4.02	4.02	2	0.30	0.03	0.16	0.00	0.00	22.3
15	420	2316	-655	-658	0	963	693	4.02	4.02	4.02	4.02	2	0.29	0.02	0.12	0.00	0.00	22.3
16	420	2397	-905	-644	0	962	469	4.02	4.02	4.02	4.02	2	0.29	0.03	0.16	0.00	0.00	22.3
17	420	2244	-648	-642	0	929	699	4.02	4.02	4.02	4.02	2	0.28	0.02	0.12	0.00	0.00	22.3
18	420	6918	-1424	-1824	0	2764	-1164	4.02	4.02	4.02	4.02	3	0.83	0.06	0.29	0.00	0.00	22.3
19	420	7739	-1379	-1515	0	2183	-1186	4.02	4.02	4.02	4.02	3	0.67	0.05	0.25	0.00	0.00	22.3
20	420	7226	-1210	-1559	0	2296	-785	4.02	4.02	4.02	4.02	3	0.70	0.05	0.25	0.00	0.00	22.3
37	420	5246	-1314	-1659	0	2560	-862	4.02	4.02	4.02	4.02	3	0.73	0.05	0.27	0.00	0.00	22.3
38	420	6613	-1238	-1143	0	1590	-898	4.02	4.02	4.02	4.02	3	0.47	0.04	0.22	0.00	0.00	22.3

39	420	5759	-956	-1216	0	1778	739	4.02	4.02	4.02	4.02	3	0.52	0.04	0.20	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	480	3063	-1410	-846	0	1759	-1200	4.02	4.02	4.02	4.02	3	0.47	0.04	0.25	0.00	0.00	22.3
2	480	2499	-1135	-677	0	1432	-1047	4.02	4.02	4.02	4.02	2	0.43	0.03	0.20	0.00	0.00	22.3
3	480	2453	-1058	-676	0	1421	-854	4.02	4.02	4.02	4.02	2	0.43	0.03	0.19	0.00	0.00	22.3
4	480	2259	-1112	-625	0	1285	-991	4.02	4.02	4.02	4.02	2	0.38	0.03	0.20	0.00	0.00	22.3
5	480	2213	-1035	-625	0	1274	-798	4.02	4.02	4.02	4.02	2	0.38	0.03	0.18	0.00	0.00	22.3
6	480	2469	-1217	-660	0	1393	-1254	4.02	4.02	4.02	4.02	2	0.42	0.04	0.22	0.00	0.00	22.3
7	480	2316	-960	-658	0	1358	-609	4.02	4.02	4.02	4.02	2	0.40	0.03	0.17	0.00	0.00	22.3
8	480	2397	-1210	-644	0	1348	-1236	4.02	4.02	4.02	4.02	2	0.40	0.04	0.22	0.00	0.00	22.3
9	480	2244	-953	-642	0	1314	-592	4.02	4.02	4.02	4.02	2	0.39	0.03	0.17	0.00	0.00	22.3
10	480	2499	-1135	-677	0	1432	-1047	4.02	4.02	4.02	4.02	2	0.43	0.03	0.20	0.00	0.00	22.3
11	480	2453	-1058	-676	0	1421	-854	4.02	4.02	4.02	4.02	2	0.43	0.03	0.19	0.00	0.00	22.3
12	480	2259	-1112	-625	0	1285	-991	4.02	4.02	4.02	4.02	2	0.38	0.03	0.20	0.00	0.00	22.3
13	480	2213	-1035	-625	0	1274	-798	4.02	4.02	4.02	4.02	2	0.38	0.03	0.18	0.00	0.00	22.3
14	480	2469	-1217	-660	0	1393	-1254	4.02	4.02	4.02	4.02	2	0.42	0.04	0.22	0.00	0.00	22.3
15	480	2316	-960	-658	0	1358	-609	4.02	4.02	4.02	4.02	2	0.40	0.03	0.17	0.00	0.00	22.3
16	480	2397	-1210	-644	0	1348	-1236	4.02	4.02	4.02	4.02	2	0.40	0.04	0.22	0.00	0.00	22.3
17	480	2244	-953	-642	0	1314	-592	4.02	4.02	4.02	4.02	2	0.39	0.03	0.17	0.00	0.00	22.3
18	480	6918	-1819	-1824	0	3859	-2337	6.03	4.02	4.02	4.02	3	0.77	0.06	0.32	0.00	0.00	22.3
19	480	7739	-1774	-1515	0	3092	-2332	4.02	4.02	4.02	4.02	3	0.95	0.05	0.32	0.00	0.00	22.3
20	480	7226	-1605	-1559	0	3231	-1829	4.02	4.02	4.02	4.02	3	0.98	0.05	0.29	0.00	0.00	22.3
37	480	5246	-1709	-1659	0	3555	-1969	6.03	4.02	4.02	4.02	3	0.69	0.05	0.30	0.00	0.00	22.3
38	480	6613	-1633	-1143	0	2276	-1960	4.02	4.02	4.02	4.02	3	0.68	0.05	0.29	0.00	0.00	22.3
39	480	5759	-1351	-1216	0	2508	-1121	4.02	4.02	4.02	4.02	3	0.73	0.04	0.24	0.00	0.00	22.3

apost= 2.01 aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	540	3063	-1806	-846	0	2266	-2365	4.02	4.02	4.02	4.02	3	0.61	0.05	0.32	0.00	0.00	22.3
2	540	2499	-1439	-677	0	1838	-1974	4.02	4.02	4.02	4.02	2	0.55	0.04	0.26	0.00	0.00	22.3
3	540	2453	-1362	-676	0	1827	-1734	4.02	4.02	4.02	4.02	2	0.55	0.04	0.24	0.00	0.00	22.3
4	540	2259	-1416	-625	0	1660	-1904	4.02	4.02	4.02	4.02	2	0.49	0.04	0.25	0.00	0.00	22.3
5	540	2213	-1339	-625	0	1649	-1664	4.02	4.02	4.02	4.02	2	0.49	0.04	0.24	0.00	0.00	22.3
6	540	2469	-1521	-660	0	1788	-2229	4.02	4.02	4.02	4.02	2	0.54	0.04	0.27	0.00	0.00	22.3
7	540	2316	-1264	-658	0	1753	-1430	4.02	4.02	4.02	4.02	2	0.52	0.04	0.23	0.00	0.00	22.3
8	540	2397	-1514	-644	0	1735	-2208	4.02	4.02	4.02	4.02	2	0.52	0.04	0.27	0.00	0.00	22.3
9	540	2244	-1257	-642	0	1700	-1409	4.02	4.02	4.02	4.02	2	0.51	0.04	0.22	0.00	0.00	22.3
10	540	2499	-1439	-677	0	1838	-1974	4.02	4.02	4.02	4.02	2	0.55	0.04	0.26	0.00	0.00	22.3
11	540	2453	-1362	-676	0	1827	-1734	4.02	4.02	4.02	4.02	2	0.55	0.04	0.24	0.00	0.00	22.3
12	540	2259	-1416	-625	0	1660	-1904	4.02	4.02	4.02	4.02	2	0.49	0.04	0.25	0.00	0.00	22.3
13	540	2213	-1339	-625	0	1649	-1664	4.02	4.02	4.02	4.02	2	0.49	0.04	0.24	0.00	0.00	22.3
14	540	2469	-1521	-660	0	1788	-2229	4.02	4.02	4.02	4.02	2	0.54	0.04	0.27	0.00	0.00	22.3
15	540	2316	-1264	-658	0	1753	-1430	4.02	4.02	4.02	4.02	2	0.52	0.04	0.23	0.00	0.00	22.3
16	540	2397	-1514	-644	0	1735	-2208	4.02	4.02	4.02	4.02	2	0.52	0.04	0.27	0.00	0.00	22.3
17	540	2244	-1257	-642	0	1700	-1409	4.02	4.02	4.02	4.02	2	0.51	0.04	0.22	0.00	0.00	22.3
18	540	6918	-2215	-1824	0	4953	-3748	6.03	4.02	4.02	4.02	3	0.99	0.06	0.39	0.00	0.00	22.3
19	540	7739	-2170	-1515	0	4001	-3716	6.03	4.02	4.02	4.02	3	0.82	0.06	0.39	0.00	0.00	22.3
20	540	7226	-2000	-1559	0	4166	-3111	6.03	4.02	4.02	4.02	3	0.84	0.06	0.36	0.00	0.00	22.3
37	540	5246	-2104	-1659	0	4550	-3313	6.03	4.02	4.02	4.02	3	0.88	0.06	0.37	0.00	0.00	22.3
38	540	6613	-2029	-1143	0	2962	-3259	4.02	4.02	4.02	4.02	3	0.88	0.06	0.36	0.00	0.00	22.3
39	540	5759	-1746	-1216	0	3237	-2251	4.02	4.02	4.02	4.02	3	0.94	0.05	0.31	0.00	0.00	22.3

apost= 2.01 aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	600	3063	-2201	-846	0	2774	-2653	4.02	4.02	4.02	4.02	3	0.74	0.06	0.39	0.00	0.00	22.3
2	600	2499	-1743	-677	0	2244	-2200	4.02	4.02	4.02	4.02	2	0.67	0.05	0.31	0.00	0.00	22.3
3	600	2453	-1666	-676	0	2233	-1953	4.02	4.02	4.02	4.02	2	0.67	0.05	0.30	0.00	0.00	22.3
4	600	2259	-1720	-625	0	2035	-2128	4.02	4.02	4.02	4.02	2	0.61	0.05	0.31	0.00	0.00	22.3
5	600	2213	-1643	-625	0	2024	-1881	4.02	4.02	4.02	4.02	2	0.60	0.05	0.29	0.00	0.00	22.3
6	600	2469	-1825	-660	0	2184	-2463	4.02	4.02	4.02	4.02	2	0.65	0.05	0.33	0.00	0.00	22.3
7	600	2316	-1568	-658	0	2147	-1640	4.02	4.02	4.02	4.02	2	0.64	0.05	0.28	0.00	0.00	22.3
8	600	2397	-1818	-644	0	2121	-2441	4.02	4.02	4.02	4.02	2	0.63	0.05	0.32	0.00	0.00	22.3
9	600	2244	-1561	-642	0	2085	-1618	4.02	4.02	4.02	4.02	2	0.62	0.05	0.28	0.00	0.00	22.3
10	600	2499	-1743	-677	0	2244	-2200	4.02	4.02	4.02	4.02	2	0.67	0.05	0.31	0.00	0.00	22.3
11	600	2453	-1666	-676	0	2233	-1953	4.02	4.02	4.02	4.02	2	0.67	0.05	0.30	0.00	0.00	22.3
12	600	2259	-1720	-625	0	2035	-2128	4.02	4.02	4.02	4.02	2	0.61	0.05	0.31	0.00	0.00	22.3
13	600	2213	-1643	-625	0	2024	-1881	4.02	4.02	4.02	4.02	2	0.60	0.05	0.29	0.00	0.00	22.3
14	600	2469	-1825	-660	0	2184	-2463	4.02	4.02	4.02	4.02	2	0.65	0.05	0.33	0.00	0.00	22.3
15	600	2316	-1568	-658	0	2147	-1640	4.02	4.02	4.02	4.02	2	0.64	0.05	0.28	0.00	0.00	22.3
16	600	2397	-1818	-644	0	2121	-2441	4.02	4.02	4.02	4.02	2	0.63	0.05	0.32	0.00	0.00	22.3
17	600	2244	-1561	-642	0	2085	-1618	4.02	4.02	4.02	4.02	2	0.62	0.05	0.28	0.00	0.00	22.3
18	600	6918	-2610	-1824	0	6048	-4074	8.04	4.02	4.02	4.02	3	0.91	0.08	0.46	0.00	0.00	22.3
19	600	7739	-2565	-1515	0	4910	-4038	8.04	4.02	4.02	4.02	3	0.75	0.07	0.46	0.00	0.00	22.3
20	600	7226	-2396	-1559	0	5101	-3417	8.04	4.02	4.02	4.02	3	0.77	0.07	0.43	0.00	0.00	22.3
37	600	5246	-2500	-1659	0	5545	-3629	8.04	4.02	4.02	4.02	3	0.81	0.07	0.45	0.00	0.00	22.3
38	600	6613	-2424	-1143	0	3648	-3568	6.03	4.02	4.02	4.02	3	0.73	0.07	0.43	0.00	0.00	22.3
39	600	5759	-2142	-1216	0	3967	-2533	6.03	4.02	4.02	4.02	3	0.78	0.06	0.38	0.00	0.00	22.3

apost= 4.02 aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

Delta Ingegneria srl
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Lavoro: **D2403a** Intestazione lavoro: **Palestra Campobello**
Elemento: **TRAVE** Gruppo: **4** Tabella: **Tabella travi**
Descrizione: **Travi copertura palestra**
Rck: **350.00** daN/cm^2 fyk: **4580.0** daN/cm^2
Copriferro superiore: **5.0** cm Copriferro inferiore: **5.0** cm Copriferro laterale: **5.0** cm
Verifica in ottemperanza alle NTC2018
Per le combinazioni sismiche la capacità è valutata in campo elastico o sostanzialmente elastico(§7.4.1 NTC2018)

Diametro staffe: **8** mm Numero braccia: **2**

Nome travata: **Trave_401_IP1** Descrizione: **Trave_4 7-12-17-22-32**
ASTA NUM. 1 NI 25 NF 35 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y Permanente qy tot.
qy medio: 375.00 160.00 535.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	7503	1687	174	0	742	-863	4.02	4.02	4.02	4.02	3	0.23	0.05	0.30	0.00	0.00	22.3
2	0	5809	1303	127	0	556	-692	4.02	4.02	4.02	4.02	2	0.19	0.04	0.23	0.00	0.00	22.3
3	0	5876	1299	112	0	461	-677	4.02	4.02	4.02	4.02	2	0.16	0.04	0.23	0.00	0.00	22.3
4	0	5667	1297	156	0	680	-651	4.02	4.02	4.02	4.02	2	0.23	0.04	0.23	0.00	0.00	22.3
5	0	5735	1293	142	0	585	-635	4.02	4.02	4.02	4.02	2	0.20	0.04	0.23	0.00	0.00	22.3
6	0	5680	1306	154	0	711	-695	4.02	4.02	4.02	4.02	2	0.24	0.04	0.23	0.00	0.00	22.3
7	0	5906	1292	106	0	393	-644	4.02	4.02	4.02	4.02	2	0.13	0.04	0.23	0.00	0.00	22.3
8	0	5638	1304	162	0	748	-683	4.02	4.02	4.02	4.02	2	0.25	0.04	0.23	0.00	0.00	22.3
9	0	5863	1290	115	0	430	-632	4.02	4.02	4.02	4.02	2	0.15	0.04	0.23	0.00	0.00	22.3
10	0	5809	1303	127	0	556	-692	4.02	4.02	4.02	4.02	2	0.19	0.04	0.23	0.00	0.00	22.3
11	0	5876	1299	112	0	461	-677	4.02	4.02	4.02	4.02	2	0.16	0.04	0.23	0.00	0.00	22.3
12	0	5667	1297	156	0	680	-651	4.02	4.02	4.02	4.02	2	0.23	0.04	0.23	0.00	0.00	22.3
13	0	5735	1293	142	0	585	-635	4.02	4.02	4.02	4.02	2	0.20	0.04	0.23	0.00	0.00	22.3
14	0	5680	1306	154	0	711	-695	4.02	4.02	4.02	4.02	2	0.24	0.04	0.23	0.00	0.00	22.3
15	0	5906	1292	106	0	393	-644	4.02	4.02	4.02	4.02	2	0.13	0.04	0.23	0.00	0.00	22.3
16	0	5638	1304	162	0	748	-683	4.02	4.02	4.02	4.02	2	0.25	0.04	0.23	0.00	0.00	22.3
17	0	5863	1290	115	0	430	-632	4.02	4.02	4.02	4.02	2	0.15	0.04	0.23	0.00	0.00	22.3
18	0	8777	1813	330	0	1386	-1242	4.02	4.02	4.02	4.02	3	0.44	0.05	0.32	0.00	0.00	22.3
19	0	8144	1644	377	0	1613	-688	4.02	4.02	4.02	4.02	3	0.50	0.05	0.29	0.00	0.00	22.3
20	0	8672	1681	571	0	2179	-809	4.02	4.02	4.02	4.02	3	0.69	0.05	0.30	0.00	0.00	22.3
37	0	8701	1854	256	0	1062	-1385	4.02	4.02	4.02	4.02	3	0.34	0.05	0.33	0.00	0.00	22.3
38	0	7646	1571	334	0	1440	-463	4.02	4.02	4.02	4.02	3	0.44	0.05	0.28	0.00	0.00	22.3
39	0	8525	1634	658	0	2384	-663	4.02	4.02	4.02	4.02	3	0.76	0.05	0.29	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	56	7503	1336	174	0	643	-684	4.02	4.02	4.02	4.02	3	0.20	0.04	0.24	0.00	0.00	22.3
2	56	5809	1033	127	0	485	-555	4.02	4.02	4.02	4.02	2	0.16	0.03	0.18	0.00	0.00	22.3
3	56	5876	1029	112	0	398	-540	4.02	4.02	4.02	4.02	2	0.14	0.03	0.18	0.00	0.00	22.3
4	56	5667	1027	156	0	592	526	4.02	4.02	4.02	4.02	2	0.20	0.03	0.18	0.00	0.00	22.3
5	56	5735	1023	142	0	505	537	4.02	4.02	4.02	4.02	2	0.17	0.03	0.18	0.00	0.00	22.3
6	56	5680	1036	154	0	624	-558	4.02	4.02	4.02	4.02	2	0.21	0.03	0.18	0.00	0.00	22.3
7	56	5906	1022	106	0	333	527	4.02	4.02	4.02	4.02	2	0.11	0.03	0.18	0.00	0.00	22.3
8	56	5638	1034	162	0	656	-545	4.02	4.02	4.02	4.02	2	0.22	0.03	0.18	0.00	0.00	22.3
9	56	5863	1020	115	0	365	538	4.02	4.02	4.02	4.02	2	0.12	0.03	0.18	0.00	0.00	22.3
10	56	5809	1033	127	0	485	-555	4.02	4.02	4.02	4.02	2	0.16	0.03	0.18	0.00	0.00	22.3
11	56	5876	1029	112	0	398	-540	4.02	4.02	4.02	4.02	2	0.14	0.03	0.18	0.00	0.00	22.3
12	56	5667	1027	156	0	592	526	4.02	4.02	4.02	4.02	2	0.20	0.03	0.18	0.00	0.00	22.3
13	56	5735	1023	142	0	505	537	4.02	4.02	4.02	4.02	2	0.17	0.03	0.18	0.00	0.00	22.3
14	56	5680	1036	154	0	624	-558	4.02	4.02	4.02	4.02	2	0.21	0.03	0.18	0.00	0.00	22.3
15	56	5906	1022	106	0	333	527	4.02	4.02	4.02	4.02	2	0.11	0.03	0.18	0.00	0.00	22.3
16	56	5638	1034	162	0	656	-545	4.02	4.02	4.02	4.02	2	0.22	0.03	0.18	0.00	0.00	22.3
17	56	5863	1020	115	0	365	538	4.02	4.02	4.02	4.02	2	0.12	0.03	0.18	0.00	0.00	22.3
18	56	8777	1462	330	0	1199	-1057	4.02	4.02	4.02	4.02	3	0.38	0.04	0.26	0.00	0.00	22.3
19	56	8144	1293	377	0	1400	796	4.02	4.02	4.02	4.02	3	0.44	0.04	0.23	0.00	0.00	22.3
20	56	8672	1330	571	0	1856	716	4.02	4.02	4.02	4.02	3	0.59	0.04	0.24	0.00	0.00	22.3
37	56	8701	1503	256	0	917	-1197	4.02	4.02	4.02	4.02	3	0.29	0.04	0.27	0.00	0.00	22.3
38	56	7646	1220	334	0	1252	944	4.02	4.02	4.02	4.02	3	0.39	0.04	0.22	0.00	0.00	22.3
39	56	8525	1283	658	0	2012	811	4.02	4.02	4.02	4.02	3	0.64	0.04	0.23	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	113	7503	976	174	0	545	1140	4.02	4.02	4.02	4.02	3	0.21	0.03	0.17	0.00	0.00	22.3
2	113	5809	756	127	0	413	857	4.02	4.02	4.02	4.02	2	0.16	0.02	0.13	0.00	0.00	22.3
3	113	5876	752	112	0	334	866	4.02	4.02	4.02	4.02	2	0.16	0.02	0.13	0.00	0.00	22.3
4	113	5667	750	156	0	504	889	4.02	4.02	4.02	4.02	2	0.17	0.02	0.13	0.00	0.00	22.3
5	113	5735	746	142	0	425	897	4.02	4.02	4.02	4.02	2	0.16	0.02	0.13	0.00	0.00	22.3
6	113	5680	759	154	0	537	858	4.02	4.02	4.02	4.02	2	0.18	0.02	0.14	0.00	0.00	22.3
7	113	5906	745	106	0	273	887	4.02	4.02	4.02	4.02	2	0.16	0.02	0.13	0.00	0.00	22.3
8	113	5638	757	162	0	565	868	4.02	4.02	4.02	4.02	2	0.19	0.02	0.13	0.00	0.00	22.3
9	113	5863	743	115	0	301	896	4.02	4.02	4.02	4.02	2	0.17	0.02	0.13	0.00	0.00	22.3
10	113	5809	756	127	0	413	857	4.02	4.02	4.02	4.02	2	0.16	0.02	0.13	0.00	0.00	22.3
11	113	5876	752	112	0	334	866	4.02	4.02	4.02	4.02	2	0.16	0.02	0.13	0.00	0.00	22.3
12	113	5667	750	156	0	504	889	4.02	4.02	4.02	4.02	2	0.17	0.02	0.13	0.00	0.00	22.3
13	113	5735	746	142	0	425	897	4.02	4.02	4.02	4.02	2	0.16	0.02	0.13	0.00	0.00	22.3
14	113	5680	759	154	0	537	858	4.02	4.02	4.02	4.02	2	0.18	0.02	0.14	0.00	0.00	22.3
15	113	5906	745	106	0	273	887	4.02	4.02	4.02	4.02	2	0.16	0.02	0.13	0.00	0.00	22.3
16	113	5638	757	162	0	565	868	4.02	4.02	4.02	4.02	2	0.19	0.02	0.13	0.00	0.00	22.3
17	113	5863	743	115	0	301	896	4.02	4.02	4.02	4.02	2	0.17	0.02	0.13	0.00	0.00	22.3
18	113	8777	1102	330	0	1013	967	4.02	4.02	4.02	4.02	3	0.32	0.03	0.20	0.00	0.00	22.3
19	113	8144	933	377	0	1187	1243	4.02	4.02	4.02	4.02	3	0.37	0.03	0.17	0.00	0.00	22.3
20	113	8672	970	571	0	1534	1184	4.02	4.02	4.02	4.02	3	0.49	0.03	0.17	0.00	0.00	22.3
37	113	8701	1143	256	0	773	891	4.02	4.02	4.02	4.02	3	0.25	0.03	0.20	0.00	0.00	22.3
38	113	7646	860	334	0	1063	1351	4.02	4.02	4.02	4.02	3	0.33	0.02	0.15	0.00	0.00	22.3

39	113	8525	923	658	0	1641	1253	4.02	4.02	4.02	4.02	3	0.52	0.03	0.16	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	170	7503	607	174	0	446	1350	4.02	4.02	4.02	4.02	3	0.25	0.02	0.11	0.00	0.00	22.3
2	170	5809	472	127	0	342	1024	4.02	4.02	4.02	4.02	2	0.19	0.01	0.08	0.00	0.00	22.3
3	170	5876	468	112	0	271	1028	4.02	4.02	4.02	4.02	2	0.19	0.01	0.08	0.00	0.00	22.3
4	170	5667	466	156	0	416	1049	4.02	4.02	4.02	4.02	2	0.19	0.01	0.08	0.00	0.00	22.3
5	170	5735	462	142	0	344	1052	4.02	4.02	4.02	4.02	2	0.19	0.01	0.08	0.00	0.00	22.3
6	170	5680	475	154	0	451	1029	4.02	4.02	4.02	4.02	2	0.19	0.01	0.08	0.00	0.00	22.3
7	170	5906	461	106	0	213	1041	4.02	4.02	4.02	4.02	2	0.19	0.01	0.08	0.00	0.00	22.3
8	170	5638	473	162	0	473	1036	4.02	4.02	4.02	4.02	2	0.19	0.01	0.08	0.00	0.00	22.3
9	170	5863	459	115	0	236	1048	4.02	4.02	4.02	4.02	2	0.19	0.01	0.08	0.00	0.00	22.3
10	170	5809	472	127	0	342	1024	4.02	4.02	4.02	4.02	2	0.19	0.01	0.08	0.00	0.00	22.3
11	170	5876	468	112	0	271	1028	4.02	4.02	4.02	4.02	2	0.19	0.01	0.08	0.00	0.00	22.3
12	170	5667	466	156	0	416	1049	4.02	4.02	4.02	4.02	2	0.19	0.01	0.08	0.00	0.00	22.3
13	170	5735	462	142	0	344	1052	4.02	4.02	4.02	4.02	2	0.19	0.01	0.08	0.00	0.00	22.3
14	170	5680	475	154	0	451	1029	4.02	4.02	4.02	4.02	2	0.19	0.01	0.08	0.00	0.00	22.3
15	170	5906	461	106	0	213	1041	4.02	4.02	4.02	4.02	2	0.19	0.01	0.08	0.00	0.00	22.3
16	170	5638	473	162	0	473	1036	4.02	4.02	4.02	4.02	2	0.19	0.01	0.08	0.00	0.00	22.3
17	170	5863	459	115	0	236	1048	4.02	4.02	4.02	4.02	2	0.19	0.01	0.08	0.00	0.00	22.3
18	170	8777	733	330	0	826	1298	4.02	4.02	4.02	4.02	3	0.26	0.02	0.13	0.00	0.00	22.3
19	170	8144	564	377	0	974	1406	4.02	4.02	4.02	4.02	3	0.30	0.02	0.10	0.00	0.00	22.3
20	170	8672	601	571	0	1211	1387	4.02	4.02	4.02	4.02	3	0.39	0.02	0.11	0.00	0.00	22.3
37	170	8701	774	256	0	628	1246	4.02	4.02	4.02	4.02	3	0.24	0.02	0.14	0.00	0.00	22.3
38	170	7646	491	334	0	875	1469	4.02	4.02	4.02	4.02	3	0.27	0.01	0.09	0.00	0.00	22.3
39	170	8525	554	658	0	1269	1410	4.02	4.02	4.02	4.02	3	0.40	0.02	0.11	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	226	7503	228	174	0	348	1350	4.02	4.02	4.02	4.02	3	0.25	0.01	0.04	0.00	0.00	22.3
2	226	5809	181	127	0	270	1024	4.02	4.02	4.02	4.02	2	0.19	0.01	0.03	0.00	0.00	22.3
3	226	5876	177	112	0	207	1028	4.02	4.02	4.02	4.02	2	0.19	0.01	0.03	0.00	0.00	22.3
4	226	5667	175	156	0	327	1049	4.02	4.02	4.02	4.02	2	0.19	0.01	0.03	0.00	0.00	22.3
5	226	5735	171	142	0	264	1052	4.02	4.02	4.02	4.02	2	0.19	0.00	0.03	0.00	0.00	22.3
6	226	5680	184	154	0	364	1029	4.02	4.02	4.02	4.02	2	0.19	0.01	0.03	0.00	0.00	22.3
7	226	5906	170	106	0	154	1041	4.02	4.02	4.02	4.02	2	0.19	0.00	0.03	0.00	0.00	22.3
8	226	5638	182	162	0	381	1036	4.02	4.02	4.02	4.02	2	0.19	0.01	0.03	0.00	0.00	22.3
9	226	5863	168	115	0	171	1048	4.02	4.02	4.02	4.02	2	0.19	0.00	0.03	0.00	0.00	22.3
10	226	5809	181	127	0	270	1024	4.02	4.02	4.02	4.02	2	0.19	0.01	0.03	0.00	0.00	22.3
11	226	5876	177	112	0	207	1028	4.02	4.02	4.02	4.02	2	0.19	0.01	0.03	0.00	0.00	22.3
12	226	5667	175	156	0	327	1049	4.02	4.02	4.02	4.02	2	0.19	0.01	0.03	0.00	0.00	22.3
13	226	5735	171	142	0	264	1052	4.02	4.02	4.02	4.02	2	0.19	0.00	0.03	0.00	0.00	22.3
14	226	5680	184	154	0	364	1029	4.02	4.02	4.02	4.02	2	0.19	0.01	0.03	0.00	0.00	22.3
15	226	5906	170	106	0	154	1041	4.02	4.02	4.02	4.02	2	0.19	0.00	0.03	0.00	0.00	22.3
16	226	5638	182	162	0	381	1036	4.02	4.02	4.02	4.02	2	0.19	0.01	0.03	0.00	0.00	22.3
17	226	5863	168	115	0	171	1048	4.02	4.02	4.02	4.02	2	0.19	0.00	0.03	0.00	0.00	22.3
18	226	8777	354	330	0	640	1326	4.02	4.02	4.02	4.02	3	0.26	0.01	0.06	0.00	0.00	22.3
19	226	8144	185	377	0	761	1406	4.02	4.02	4.02	4.02	3	0.26	0.01	0.06	0.00	0.00	22.3
20	226	8672	222	571	0	888	1387	4.02	4.02	4.02	4.02	3	0.28	0.02	0.09	0.00	0.00	22.3
37	226	8701	395	256	0	484	1299	4.02	4.02	4.02	4.02	3	0.25	0.01	0.07	0.00	0.00	22.3
38	226	7646	112	334	0	686	1469	4.02	4.02	4.02	4.02	3	0.27	0.01	0.05	0.00	0.00	22.3
39	226	8525	175	658	0	898	1410	4.02	4.02	4.02	4.02	3	0.28	0.02	0.11	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	282	7503	-160	174	0	249	1350	4.02	4.02	4.02	4.02	3	0.25	0.01	0.03	0.00	0.00	22.3
2	282	5809	-118	127	0	199	1024	4.02	4.02	4.02	4.02	2	0.19	0.00	0.02	0.00	0.00	22.3
3	282	5876	-122	112	0	144	1028	4.02	4.02	4.02	4.02	2	0.19	0.00	0.02	0.00	0.00	22.3
4	282	5667	-124	156	0	239	1049	4.02	4.02	4.02	4.02	2	0.19	0.00	0.03	0.00	0.00	22.3
5	282	5735	-128	142	0	184	1052	4.02	4.02	4.02	4.02	2	0.19	0.00	0.02	0.00	0.00	22.3
6	282	5680	-115	154	0	277	1029	4.02	4.02	4.02	4.02	2	0.19	0.00	0.02	0.00	0.00	22.3
7	282	5906	-129	106	0	94	1041	4.02	4.02	4.02	4.02	2	0.19	0.00	0.02	0.00	0.00	22.3
8	282	5638	-117	162	0	289	1036	4.02	4.02	4.02	4.02	2	0.19	0.01	0.03	0.00	0.00	22.3
9	282	5863	-131	115	0	106	1048	4.02	4.02	4.02	4.02	2	0.19	0.00	0.02	0.00	0.00	22.3
10	282	5809	-118	127	0	199	1024	4.02	4.02	4.02	4.02	2	0.19	0.00	0.02	0.00	0.00	22.3
11	282	5876	-122	112	0	144	1028	4.02	4.02	4.02	4.02	2	0.19	0.00	0.02	0.00	0.00	22.3
12	282	5667	-124	156	0	239	1049	4.02	4.02	4.02	4.02	2	0.19	0.00	0.03	0.00	0.00	22.3
13	282	5735	-128	142	0	184	1052	4.02	4.02	4.02	4.02	2	0.19	0.00	0.02	0.00	0.00	22.3
14	282	5680	-115	154	0	277	1029	4.02	4.02	4.02	4.02	2	0.19	0.00	0.02	0.00	0.00	22.3
15	282	5906	-129	106	0	94	1041	4.02	4.02	4.02	4.02	2	0.19	0.00	0.02	0.00	0.00	22.3
16	282	5638	-117	162	0	289	1036	4.02	4.02	4.02	4.02	2	0.19	0.01	0.03	0.00	0.00	22.3
17	282	5863	-131	115	0	106	1048	4.02	4.02	4.02	4.02	2	0.19	0.00	0.02	0.00	0.00	22.3
18	282	8777	-34	330	0	453	1326	4.02	4.02	4.02	4.02	3	0.26	0.01	0.05	0.00	0.00	22.3
19	282	8144	-203	377	0	548	1406	4.02	4.02	4.02	4.02	3	0.26	0.01	0.06	0.00	0.00	22.3
20	282	8672	-166	571	0	566	1387	4.02	4.02	4.02	4.02	3	0.27	0.02	0.09	0.00	0.00	22.3
37	282	8701	7	256	0	339	1299	4.02	4.02	4.02	4.02	3	0.25	0.01	0.04	0.00	0.00	22.3
38	282	7646	-276	334	0	498	1469	4.02	4.02	4.02	4.02	3	0.27	0.01	0.05	0.00	0.00	22.3
39	282	8525	-213	658	0	526	1410	4.02	4.02	4.02	4.02	3	0.27	0.02	0.11	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	339	7503	-558	174	0	150	1350	4.02	4.02	4.02	4.02	3	0.25	0.02	0.10	0.00	0.00	22.3
2	339	5809	-424	127	0	127	1024	4.02	4.02	4.02	4.02	2	0.19	0.01	0.08	0.00	0.00	22.3
3	339	5876	-428	112	0	80	1028	4.02	4.02	4.02	4.02	2	0.19	0.01	0.08	0.00	0.00	22.3
4	339	5667	-430	156	0	151	1049	4.02	4.02	4.02	4.02	2	0.19	0.01	0.08	0.00	0.00	22.3
5	339	5735	-434	142	0	104	1052	4.02	4.02	4.02	4.02	2	0.19	0.01	0.08	0.00	0.00	22.3
6	339	5680	-421	154	0	190	1029	4.02	4.02	4.02	4.02	2	0.19	0.01	0.07	0.00	0.00	22.3
7	339	5906	-435	106	0	34	1041	4.02	4.02	4.02	4.02	2	0.19	0.01	0.08	0.00	0.00	22.3
8	339	5638	-423	162	0	198	1036	4.02	4.02	4.02	4.02	2	0.19	0.01	0.08	0.00	0.00	22.3
9	339	5863	-437	115	0	41	1048	4.02	4.02	4.02	4.02	2	0.19	0.01	0.08	0.00	0.00	22.3
10	339	5809	-424	127	0	127	1024	4.02	4.02	4.02	4.02	2	0.19	0.01	0.08	0.00	0.00	22.3
11	339	5876	-428	112	0	80	1028	4.02	4.02	4.02	4.02	2	0.19	0.01	0.08	0.00	0.00	22.3
12	339	5667	-430	156	0	151	1049	4.02	4.02	4.02	4.02	2	0.19	0.01	0.08	0.00	0.00	22.3
13	339	5735	-434	142	0	104	1052	4.02	4.02	4.02	4.02	2	0.19	0.01	0.08	0.00	0.00	22.3
14	339	5680	-421	154	0	190	1029	4.02	4.02	4.02	4.02	2	0.19	0.01	0.07	0.00	0.00	22.3
15	339	5906	-435	106	0	34	1041	4.02	4.02	4.02	4.02	2	0.19	0.01	0.08	0.00	0.00	22.3
16	339	5638	-423	162	0	198	1036	4.02	4.02	4.02	4.02	2	0.19	0.01	0.08	0.00	0.00	22.3
17	339	5863	-437	115	0	41	1048	4.02	4.02	4.02	4.02	2	0.19	0.01	0.08	0.00	0.00	22.3
18	339	8777	-432	330	0	267	1326	4.02	4.02	4.02	4.02	3	0.26	0.01	0.08	0.00	0.00	22.3
19	339	8144	-601	377	0	335	1406	4.02	4.02	4.02	4.02	3	0.26	0.02	0.11	0.00	0.00	22.3
20	339	8672	-564	571	0	243	1387	4.02	4.02	4.02	4.02	3	0.27	0.02	0.10	0.00	0.00	22.3
37	339	8701	-391	256	0	195	1299	4.02	4.02	4.02	4.02	3	0.25	0.01	0.07	0.00	0.00	22.3
38	339	7646	-674	334	0	309	1469	4.02	4.02	4.02	4.02	3	0.27	0.02	0.12	0.00	0.00	22.3
39	339	8525	-611	658	0	154	1410	4.02	4.02	4.02	4.02	3	0.27	0.02	0.11	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	396	7503	-965	174	0	52	1206	4.02	4.02	4.02	4.02	3	0.22	0.03	0.17	0.00	0.00	22.3
2	396	5809	-737	127	0	56	917	4.02	4.02	4.02	4.02	2	0.17	0.02	0.13	0.00	0.00	22.3

3	396	5876	-741	112	0	17	918	4.02	4.02	4.02	4.02	2	0.17	0.02	0.13	0.00	0.00	22.3
4	396	5667	-743	156	0	63	938	4.02	4.02	4.02	4.02	2	0.17	0.02	0.13	0.00	0.00	22.3
5	396	5735	-747	142	0	24	939	4.02	4.02	4.02	4.02	2	0.17	0.02	0.13	0.00	0.00	22.3
6	396	5680	-734	154	0	104	923	4.02	4.02	4.02	4.02	2	0.17	0.02	0.13	0.00	0.00	22.3
7	396	5906	-748	106	0	-26	926	4.02	4.02	4.02	4.02	2	0.17	0.02	0.13	0.00	0.00	22.3
8	396	5638	-736	162	0	106	929	4.02	4.02	4.02	4.02	2	0.17	0.02	0.13	0.00	0.00	22.3
9	396	5863	-750	115	0	-24	933	4.02	4.02	4.02	4.02	2	0.17	0.02	0.13	0.00	0.00	22.3
10	396	5809	-737	127	0	56	917	4.02	4.02	4.02	4.02	2	0.17	0.02	0.13	0.00	0.00	22.3
11	396	5876	-741	112	0	17	918	4.02	4.02	4.02	4.02	2	0.17	0.02	0.13	0.00	0.00	22.3
12	396	5667	-743	156	0	63	938	4.02	4.02	4.02	4.02	2	0.17	0.02	0.13	0.00	0.00	22.3
13	396	5735	-747	142	0	24	939	4.02	4.02	4.02	4.02	2	0.17	0.02	0.13	0.00	0.00	22.3
14	396	5680	-734	154	0	104	923	4.02	4.02	4.02	4.02	2	0.17	0.02	0.13	0.00	0.00	22.3
15	396	5906	-748	106	0	-26	926	4.02	4.02	4.02	4.02	2	0.17	0.02	0.13	0.00	0.00	22.3
16	396	5638	-736	162	0	106	929	4.02	4.02	4.02	4.02	2	0.17	0.02	0.13	0.00	0.00	22.3
17	396	5863	-750	115	0	-24	933	4.02	4.02	4.02	4.02	2	0.17	0.02	0.13	0.00	0.00	22.3
18	396	8777	-839	330	0	80	1261	4.02	4.02	4.02	4.02	3	0.24	0.02	0.15	0.00	0.00	22.3
19	396	8144	-1008	377	0	122	1230	4.02	4.02	4.02	4.02	3	0.23	0.03	0.18	0.00	0.00	22.3
20	396	8672	-971	571	0	-80	1240	4.02	4.02	4.02	4.02	3	0.24	0.03	0.17	0.00	0.00	22.3
37	396	8701	-798	256	0	50	1259	4.02	4.02	4.02	4.02	3	0.24	0.02	0.14	0.00	0.00	22.3
38	396	7646	-1081	334	0	121	1207	4.02	4.02	4.02	4.02	3	0.22	0.03	0.19	0.00	0.00	22.3
39	396	8525	-1018	658	0	-217	1223	4.02	4.02	4.02	4.02	3	0.23	0.03	0.18	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	452	7503	-1381	174	0	-47	755	4.02	4.02	4.02	4.02	3	0.14	0.04	0.25	0.00	0.00	22.3
2	452	5809	-1058	127	0	-16	573	4.02	4.02	4.02	4.02	2	0.11	0.03	0.19	0.00	0.00	22.3
3	452	5876	-1062	112	0	-47	571	4.02	4.02	4.02	4.02	2	0.11	0.03	0.19	0.00	0.00	22.3
4	452	5667	-1064	156	0	-25	590	4.02	4.02	4.02	4.02	2	0.11	0.03	0.19	0.00	0.00	22.3
5	452	5735	-1068	142	0	-56	588	4.02	4.02	4.02	4.02	2	0.11	0.03	0.19	0.00	0.00	22.3
6	452	5680	-1055	154	0	17	580	4.02	4.02	4.02	4.02	2	0.11	0.03	0.19	0.00	0.00	22.3
7	452	5906	-1069	106	0	-86	576	4.02	4.02	4.02	4.02	2	0.11	0.03	0.19	0.00	0.00	22.3
8	452	5638	-1057	162	0	14	585	4.02	4.02	4.02	4.02	2	0.11	0.03	0.19	0.00	0.00	22.3
9	452	5863	-1071	115	0	-89	581	4.02	4.02	4.02	4.02	2	0.11	0.03	0.19	0.00	0.00	22.3
10	452	5809	-1058	127	0	-16	573	4.02	4.02	4.02	4.02	2	0.11	0.03	0.19	0.00	0.00	22.3
11	452	5876	-1062	112	0	-47	571	4.02	4.02	4.02	4.02	2	0.11	0.03	0.19	0.00	0.00	22.3
12	452	5667	-1064	156	0	-25	590	4.02	4.02	4.02	4.02	2	0.11	0.03	0.19	0.00	0.00	22.3
13	452	5735	-1068	142	0	-56	588	4.02	4.02	4.02	4.02	2	0.11	0.03	0.19	0.00	0.00	22.3
14	452	5680	-1055	154	0	17	580	4.02	4.02	4.02	4.02	2	0.11	0.03	0.19	0.00	0.00	22.3
15	452	5906	-1069	106	0	-86	576	4.02	4.02	4.02	4.02	2	0.11	0.03	0.19	0.00	0.00	22.3
16	452	5638	-1057	162	0	14	585	4.02	4.02	4.02	4.02	2	0.11	0.03	0.19	0.00	0.00	22.3
17	452	5863	-1071	115	0	-89	581	4.02	4.02	4.02	4.02	2	0.11	0.03	0.19	0.00	0.00	22.3
18	452	8777	-1256	330	0	-106	880	4.02	4.02	4.02	4.02	3	0.17	0.04	0.22	0.00	0.00	22.3
19	452	8144	-1425	377	0	-90	753	4.02	4.02	4.02	4.02	3	0.14	0.04	0.25	0.00	0.00	22.3
20	452	8672	-1387	571	0	-403	785	4.02	4.02	4.02	4.02	3	0.15	0.04	0.25	0.00	0.00	22.3
37	452	8701	-1215	256	0	-94	902	4.02	4.02	4.02	4.02	3	0.17	0.04	0.22	0.00	0.00	22.3
38	452	7646	-1497	334	0	-68	-825	4.02	4.02	4.02	4.02	3	0.15	0.04	0.27	0.00	0.00	22.3
39	452	8525	-1434	658	0	-589	742	4.02	4.02	4.02	4.02	3	0.19	0.04	0.26	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	508	7503	-1807	174	0	-145	-1759	4.02	4.02	4.02	4.02	3	0.32	0.05	0.32	0.00	0.00	22.3
2	508	5809	-1385	127	0	-87	-1353	4.02	4.02	4.02	4.02	2	0.25	0.04	0.25	0.00	0.00	22.3
3	508	5876	-1389	112	0	-110	-1361	4.02	4.02	4.02	4.02	2	0.25	0.04	0.25	0.00	0.00	22.3
4	508	5667	-1391	156	0	-113	-1346	4.02	4.02	4.02	4.02	2	0.25	0.04	0.25	0.00	0.00	22.3
5	508	5735	-1395	142	0	-136	-1354	4.02	4.02	4.02	4.02	2	0.25	0.04	0.25	0.00	0.00	22.3
6	508	5680	-1382	154	0	-70	-1341	4.02	4.02	4.02	4.02	2	0.25	0.04	0.25	0.00	0.00	22.3
7	508	5906	-1396	106	0	-146	-1368	4.02	4.02	4.02	4.02	2	0.25	0.04	0.25	0.00	0.00	22.3
8	508	5638	-1384	162	0	-78	-1339	4.02	4.02	4.02	4.02	2	0.25	0.04	0.25	0.00	0.00	22.3
9	508	5863	-1398	115	0	-154	-1366	4.02	4.02	4.02	4.02	2	0.25	0.04	0.25	0.00	0.00	22.3
10	508	5809	-1385	127	0	-87	-1353	4.02	4.02	4.02	4.02	2	0.25	0.04	0.25	0.00	0.00	22.3
11	508	5876	-1389	112	0	-110	-1361	4.02	4.02	4.02	4.02	2	0.25	0.04	0.25	0.00	0.00	22.3
12	508	5667	-1391	156	0	-113	-1346	4.02	4.02	4.02	4.02	2	0.25	0.04	0.25	0.00	0.00	22.3
13	508	5735	-1395	142	0	-136	-1354	4.02	4.02	4.02	4.02	2	0.25	0.04	0.25	0.00	0.00	22.3
14	508	5680	-1382	154	0	-70	-1341	4.02	4.02	4.02	4.02	2	0.25	0.04	0.25	0.00	0.00	22.3
15	508	5906	-1396	106	0	-146	-1368	4.02	4.02	4.02	4.02	2	0.25	0.04	0.25	0.00	0.00	22.3
16	508	5638	-1384	162	0	-78	-1339	4.02	4.02	4.02	4.02	2	0.25	0.04	0.25	0.00	0.00	22.3
17	508	5863	-1398	115	0	-154	-1366	4.02	4.02	4.02	4.02	2	0.25	0.04	0.25	0.00	0.00	22.3
18	508	8777	-1682	330	0	-293	-1436	4.02	4.02	4.02	4.02	3	0.28	0.05	0.30	0.00	0.00	22.3
19	508	8144	-1851	377	0	-303	-1830	4.02	4.02	4.02	4.02	3	0.34	0.05	0.33	0.00	0.00	22.3
20	508	8672	-1813	571	0	-725	-1739	4.02	4.02	4.02	4.02	3	0.33	0.05	0.32	0.00	0.00	22.3
37	508	8701	-1641	256	0	-239	-1349	4.02	4.02	4.02	4.02	3	0.26	0.05	0.29	0.00	0.00	22.3
38	508	7646	-1923	334	0	-256	-2007	4.02	4.02	4.02	4.02	3	0.37	0.06	0.34	0.00	0.00	22.3
39	508	8525	-1860	658	0	-960	-1856	4.02	4.02	4.02	4.02	3	0.35	0.05	0.33	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	565	7503	-2242	174	0	-244	-1988	4.02	4.02	4.02	4.02	3	0.37	0.07	0.40	0.00	0.00	22.3
2	565	5809	-1720	127	0	-159	-1529	4.02	4.02	4.02	4.02	2	0.28	0.05	0.31	0.00	0.00	22.3
3	565	5876	-1724	112	0	-174	-1537	4.02	4.02	4.02	4.02	2	0.28	0.05	0.31	0.00	0.00	22.3
4	565	5667	-1726	156	0	-201	-1522	4.02	4.02	4.02	4.02	2	0.28	0.05	0.31	0.00	0.00	22.3
5	565	5735	-1730	142	0	-216	-1530	4.02	4.02	4.02	4.02	2	0.28	0.05	0.31	0.00	0.00	22.3
6	565	5680	-1717	154	0	-157	-1517	4.02	4.02	4.02	4.02	2	0.28	0.05	0.31	0.00	0.00	22.3
7	565	5906	-1731	106	0	-206	-1544	4.02	4.02	4.02	4.02	2	0.29	0.05	0.31	0.00	0.00	22.3
8	565	5638	-1719	162	0	-169	-1515	4.02	4.02	4.02	4.02	2	0.28	0.05	0.31	0.00	0.00	22.3
9	565	5863	-1733	115	0	-219	-1542	4.02	4.02	4.02	4.02	2	0.28	0.05	0.31	0.00	0.00	22.3
10	565	5809	-1720	127	0	-159	-1529	4.02	4.02	4.02	4.02	2	0.28	0.05	0.31	0.00	0.00	22.3
11	565	5876	-1724	112	0	-174	-1537	4.02	4.02	4.02	4.02	2	0.28	0.05	0.31	0.00	0.00	22.3
12	565	5667	-1726	156	0	-201	-1522	4.02	4.02	4.02	4.02	2	0.28	0.05	0.31	0.00	0.00	22.3
13	565	5735	-1730	142	0	-216	-1530	4.02	4.02	4.02	4.02	2	0.28	0.05	0.31	0.00	0.00	22.3
14	565	5680	-1717	154	0	-157	-1517	4.02	4.02	4.02	4.02	2	0.28	0.05	0.31	0.00	0.00	22.3
15	565	5906	-1731	106	0	-206	-1544	4.02	4.02	4.02	4.02	2	0.29	0.05	0.31	0.00	0.00	22.3
16	565	5638	-1719	162	0	-169	-1515	4.02	4.02	4.02	4.02	2	0.28	0.05	0.31	0.00	0.00	22.3
17	565	5863	-1733	115	0	-219	-1542	4.02	4.02	4.02	4.02	2	0.28	0.05	0.31	0.00	0.00	22.3
18	565	8777	-2117	330	0	-479	-1657	4.02	4.02	4.02	4.02	3	0.32	0.06	0.38	0.00	0.00	22.3
19	565	8144	-2286	377	0	-516	-2061	4.02	4.02	4.02	4.02	3	0.39	0.07	0.41	0.00	0.00	22.3
20	565	8672	-2248	571	0	-1048	-1968	4.02	4.02	4.02	4.02	3	0.38	0.07	0.40	0.00	0.00	22.3
37	565	8701	-2076	256	0	-383	-1568	4.02	4.02	4.02	4.02	3	0.30	0.06	0.37	0.00	0.00	22.3
38	565	7646	-2358	334	0	-445	-2242	4.02	4.02	4.02	4.02	3	0.41	0.07	0.42	0.00	0.00	22.3
39	565	8525	-2295	658	0	-1332	-2088	4.02	4.02	4.02	4.02	3	0.42	0.07	0.41	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

Nome travata: **Trave_401_IP1** Descrizione: **Trave_4 7-12-17-22-32**
ASTA NUM. 2 NI 35 NF 37 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y qy tot.
qy medio: 375.00 375.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	6124	1333	-2	0	-87	-1227	4.02	4.02	4.02	4.02	3	0.21	0.04	0.24	0.00	0.00	22.3
2	0	4696	1010	-5	0	-68	-902	4.02	4.02	4.02	4.02	2	0.16	0.03	0.18	0.00	0.00	22.3
3	0	4761	1011	-6	0	-85	-904	4.02	4.02	4.02	4.02	2	0.16	0.03	0.18	0.00	0.00	22.3
4	0	4660	1040	2	0	-49	-983	4.02	4.02	4.02	4.02	2	0.17	0.03	0.19	0.00	0.00	22.3
5	0	4726	1041	2	0	-66	-986	4.02	4.02	4.02	4.02	2	0.17	0.03	0.19	0.00	0.00	22.3
6	0	4607	1020	-2	0	-42	-927	4.02	4.02	4.02	4.02	2	0.16	0.03	0.18	0.00	0.00	22.3
7	0	4825	1022	-4	0	-98	-935	4.02	4.02	4.02	4.02	2	0.17	0.03	0.18	0.00	0.00	22.3
8	0	4596	1029	0	0	-36	-952	4.02	4.02	4.02	4.02	2	0.17	0.03	0.18	0.00	0.00	22.3
9	0	4815	1031	-1	0	-92	-960	4.02	4.02	4.02	4.02	2	0.17	0.03	0.18	0.00	0.00	22.3
10	0	4696	1010	-5	0	-68	-902	4.02	4.02	4.02	4.02	2	0.16	0.03	0.18	0.00	0.00	22.3
11	0	4761	1011	-6	0	-85	-904	4.02	4.02	4.02	4.02	2	0.16	0.03	0.18	0.00	0.00	22.3
12	0	4660	1040	2	0	-49	-983	4.02	4.02	4.02	4.02	2	0.17	0.03	0.19	0.00	0.00	22.3
13	0	4726	1041	2	0	-66	-986	4.02	4.02	4.02	4.02	2	0.17	0.03	0.19	0.00	0.00	22.3
14	0	4607	1020	-2	0	-42	-927	4.02	4.02	4.02	4.02	2	0.16	0.03	0.18	0.00	0.00	22.3
15	0	4825	1022	-4	0	-98	-935	4.02	4.02	4.02	4.02	2	0.17	0.03	0.18	0.00	0.00	22.3
16	0	4596	1029	0	0	-36	-952	4.02	4.02	4.02	4.02	2	0.17	0.03	0.18	0.00	0.00	22.3
17	0	4815	1031	-1	0	-92	-960	4.02	4.02	4.02	4.02	2	0.17	0.03	0.18	0.00	0.00	22.3
18	0	7241	1350	-27	0	-295	-1296	4.02	4.02	4.02	4.02	3	0.24	0.04	0.24	0.00	0.00	22.3
19	0	7140	1361	20	0	-81	-1310	4.02	4.02	4.02	4.02	3	0.24	0.04	0.24	0.00	0.00	22.3
20	0	7325	1350	140	0	-120	-1289	4.02	4.02	4.02	4.02	3	0.24	0.04	0.24	0.00	0.00	22.3
37	0	6940	1337	-43	0	-335	-1262	4.02	4.02	4.02	4.02	3	0.23	0.04	0.24	0.00	0.00	22.3
38	0	6772	1356	35	0	21	-1285	4.02	4.02	4.02	4.02	3	0.23	0.04	0.24	0.00	0.00	22.3
39	0	7081	1337	236	0	-44	-1250	4.02	4.02	4.02	4.02	3	0.23	0.04	0.24	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	56	6124	1058	-2	0	-86	-1087	4.02	4.02	4.02	4.02	3	0.19	0.03	0.19	0.00	0.00	22.3
2	56	4696	798	-5	0	-65	-795	4.02	4.02	4.02	4.02	2	0.14	0.02	0.14	0.00	0.00	22.3
3	56	4761	799	-6	0	-82	-797	4.02	4.02	4.02	4.02	2	0.14	0.02	0.14	0.00	0.00	22.3
4	56	4660	828	2	0	-50	-875	4.02	4.02	4.02	4.02	2	0.15	0.02	0.15	0.00	0.00	22.3
5	56	4726	829	2	0	-67	-877	4.02	4.02	4.02	4.02	2	0.16	0.02	0.15	0.00	0.00	22.3
6	56	4607	808	-2	0	-41	-820	4.02	4.02	4.02	4.02	2	0.14	0.02	0.14	0.00	0.00	22.3
7	56	4825	810	-4	0	-96	-828	4.02	4.02	4.02	4.02	2	0.15	0.02	0.14	0.00	0.00	22.3
8	56	4596	817	0	0	-36	-844	4.02	4.02	4.02	4.02	2	0.15	0.02	0.15	0.00	0.00	22.3
9	56	4815	819	-1	0	-91	-852	4.02	4.02	4.02	4.02	2	0.15	0.02	0.15	0.00	0.00	22.3
10	56	4696	798	-5	0	-65	-795	4.02	4.02	4.02	4.02	2	0.14	0.02	0.14	0.00	0.00	22.3
11	56	4761	799	-6	0	-82	-797	4.02	4.02	4.02	4.02	2	0.14	0.02	0.14	0.00	0.00	22.3
12	56	4660	828	2	0	-50	-875	4.02	4.02	4.02	4.02	2	0.15	0.02	0.15	0.00	0.00	22.3
13	56	4726	829	2	0	-67	-877	4.02	4.02	4.02	4.02	2	0.16	0.02	0.15	0.00	0.00	22.3
14	56	4607	808	-2	0	-41	-820	4.02	4.02	4.02	4.02	2	0.14	0.02	0.14	0.00	0.00	22.3
15	56	4825	810	-4	0	-96	-828	4.02	4.02	4.02	4.02	2	0.15	0.02	0.14	0.00	0.00	22.3
16	56	4596	817	0	0	-36	-844	4.02	4.02	4.02	4.02	2	0.15	0.02	0.15	0.00	0.00	22.3
17	56	4815	819	-1	0	-91	-852	4.02	4.02	4.02	4.02	2	0.15	0.02	0.15	0.00	0.00	22.3
18	56	7241	1074	-27	0	-280	-1155	4.02	4.02	4.02	4.02	3	0.21	0.03	0.19	0.00	0.00	22.3
19	56	7140	1086	20	0	-93	-1168	4.02	4.02	4.02	4.02	3	0.21	0.03	0.19	0.00	0.00	22.3
20	56	7325	1075	140	0	-199	-1148	4.02	4.02	4.02	4.02	3	0.21	0.03	0.19	0.00	0.00	22.3
37	56	6940	1062	-43	0	-311	-1122	4.02	4.02	4.02	4.02	3	0.20	0.03	0.19	0.00	0.00	22.3
38	56	6772	1081	35	0	1	-1143	4.02	4.02	4.02	4.02	3	0.20	0.03	0.19	0.00	0.00	22.3
39	56	7081	1062	236	0	-177	-1110	4.02	4.02	4.02	4.02	3	0.20	0.03	0.19	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	113	6124	782	-2	0	-85	-428	4.02	4.02	4.02	4.02	3	0.07	0.02	0.14	0.00	0.00	22.3
2	113	4696	586	-5	0	-62	297	4.02	4.02	4.02	4.02	2	0.05	0.02	0.10	0.00	0.00	22.3
3	113	4761	587	-6	0	-78	-298	4.02	4.02	4.02	4.02	2	0.05	0.02	0.10	0.00	0.00	22.3
4	113	4660	616	2	0	-52	-360	4.02	4.02	4.02	4.02	2	0.06	0.02	0.11	0.00	0.00	22.3
5	113	4726	617	2	0	-68	-362	4.02	4.02	4.02	4.02	2	0.06	0.02	0.11	0.00	0.00	22.3
6	113	4607	596	-2	0	-40	-316	4.02	4.02	4.02	4.02	2	0.06	0.02	0.11	0.00	0.00	22.3
7	113	4825	598	-4	0	-94	-323	4.02	4.02	4.02	4.02	2	0.06	0.02	0.11	0.00	0.00	22.3
8	113	4596	605	0	0	-36	-335	4.02	4.02	4.02	4.02	2	0.06	0.02	0.11	0.00	0.00	22.3
9	113	4815	607	-1	0	-90	-342	4.02	4.02	4.02	4.02	2	0.06	0.02	0.11	0.00	0.00	22.3
10	113	4696	586	-5	0	-62	297	4.02	4.02	4.02	4.02	2	0.05	0.02	0.10	0.00	0.00	22.3
11	113	4761	587	-6	0	-78	-298	4.02	4.02	4.02	4.02	2	0.05	0.02	0.10	0.00	0.00	22.3
12	113	4660	616	2	0	-52	-360	4.02	4.02	4.02	4.02	2	0.06	0.02	0.11	0.00	0.00	22.3
13	113	4726	617	2	0	-68	-362	4.02	4.02	4.02	4.02	2	0.06	0.02	0.11	0.00	0.00	22.3
14	113	4607	596	-2	0	-40	-316	4.02	4.02	4.02	4.02	2	0.06	0.02	0.11	0.00	0.00	22.3
15	113	4825	598	-4	0	-94	-323	4.02	4.02	4.02	4.02	2	0.06	0.02	0.11	0.00	0.00	22.3
16	113	4596	605	0	0	-36	-335	4.02	4.02	4.02	4.02	2	0.06	0.02	0.11	0.00	0.00	22.3
17	113	4815	607	-1	0	-90	-342	4.02	4.02	4.02	4.02	2	0.06	0.02	0.11	0.00	0.00	22.3
18	113	7241	799	-27	0	-264	-487	4.02	4.02	4.02	4.02	3	0.09	0.02	0.14	0.00	0.00	22.3
19	113	7140	810	20	0	-104	-493	4.02	4.02	4.02	4.02	3	0.09	0.02	0.14	0.00	0.00	22.3
20	113	7325	799	140	0	-279	-479	4.02	4.02	4.02	4.02	3	0.09	0.02	0.14	0.00	0.00	22.3
37	113	6940	786	-43	0	-287	-461	4.02	4.02	4.02	4.02	3	0.09	0.02	0.14	0.00	0.00	22.3
38	113	6772	805	35	0	-19	-471	4.02	4.02	4.02	4.02	3	0.08	0.02	0.14	0.00	0.00	22.3
39	113	7081	786	236	0	-311	-448	4.02	4.02	4.02	4.02	3	0.09	0.02	0.14	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	170	6124	507	-2	0	-83	589	4.02	4.02	4.02	4.02	3	0.10	0.01	0.09	0.00	0.00	22.3
2	170	4696	374	-5	0	-59	456	4.02	4.02	4.02	4.02	2	0.08	0.01	0.07	0.00	0.00	22.3
3	170	4761	375	-6	0	-75	455	4.02	4.02	4.02	4.02	2	0.08	0.01	0.07	0.00	0.00	22.3
4	170	4660	404	2	0	-53	445	4.02	4.02	4.02	4.02	2	0.08	0.01	0.07	0.00	0.00	22.3
5	170	4726	405	2	0	-69	445	4.02	4.02	4.02	4.02	2	0.08	0.01	0.07	0.00	0.00	22.3
6	170	4607	384	-2	0	-38	457	4.02	4.02	4.02	4.02	2	0.08	0.01	0.07	0.00	0.00	22.3
7	170	4825	386	-4	0	-91	454	4.02	4.02	4.02	4.02	2	0.08	0.01	0.07	0.00	0.00	22.3
8	170	4596	393	0	0	-37	452	4.02	4.02	4.02	4.02	2	0.08	0.01	0.07	0.00	0.00	22.3
9	170	4815	395	-1	0	-90	449	4.02	4.02	4.02	4.02	2	0.08	0.01	0.07	0.00	0.00	22.3
10	170	4696	374	-5	0	-59	456	4.02	4.02	4.02	4.02	2	0.08	0.01	0.07	0.00	0.00	22.3
11	170	4761	375	-6	0	-75	455	4.02	4.02	4.02	4.02	2	0.08	0.01	0.07	0.00	0.00	22.3
12	170	4660	404	2	0	-53	445	4.02	4.02	4.02	4.02	2	0.08	0.01	0.07	0.00	0.00	22.3
13	170	4726	405	2	0	-69	445	4.02	4.02	4.02	4.02	2	0.08	0.01	0.07	0.00	0.00	22.3
14	170	4607	384	-2	0	-38	457	4.02	4.02	4.02	4.02	2	0.08	0.01	0.07	0.00	0.00	22.3
15	170	4825	386	-4	0	-91	454	4.02	4.02	4.02	4.02	2	0.08	0.01	0.07	0.00	0.00	22.3
16	170	4596	393	0	0	-37	452	4.02	4.02	4.02	4.02	2	0.08	0.01	0.07	0.00	0.00	22.3
17	170	4815	395	-1	0	-90	449	4.02	4.02	4.02	4.02	2	0.08	0.01	0.07	0.00	0.00	22.3
18	170	7241	524	-27	0	-249	556	4.02	4.02	4.02	4.02	3	0.10	0.02	0.09	0.00	0.00	22.3
19	170	7140	535	20	0	-115	568	4.02	4.02	4.02	4.02	3	0.10	0.02	0.10	0.00	0.00	22.3
20	170	7325	524	140	0	-358	564	4.02	4.02	4.02	4.02	3	0.11	0.02	0.09	0.00	0.00	22.3
37	170	6940	510	-43	0	-263	562	4.02	4.02	4.02	4.02	3	0.10	0.01	0.09	0.00	0.00	22.3
38	170	6772	530	35	0	-39	582	4.02	4.02	4.02	4.02	3	0.10	0.02	0.09	0.00	0.00	22.3
39	170	7081	511	236	0	-444	575	4.02	4.02	4.02	4.02	3	0.13	0.01	0.09	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	226	6124	231	-2	0	-82	594	4.02	4.02	4.02	4.02	3	0.10	0.01	0.04	0.00	0.00	22.3
2	226	4696	162	-5	0	-56	456	4.02	4.02	4.02	4.02	2	0.08	0.00	0.03	0.00	0.00	22.3
3	226	4761	163	-6	0	-72	455	4.02	4.02	4.02	4.02	2	0.08	0.00	0.03	0.00	0.00	22.3
4	226	4660	192	2	0	-54	458	4.02	4.02	4.02	4.02	2	0.08	0.01	0.03	0.00	0.00	22.3
5	226	4726	193	2	0	-70	458	4.02	4.02	4.02	4.02	2	0.08	0.01	0.03	0.00	0.00	22.3
6	226	4607	172	-2	0	-37	458	4.02	4.02	4.02	4.02	2	0.08	0.00	0.03	0.00	0.00	22.3
7	226	4825	174	-4	0	-89	455	4.02	4.02	4.02	4.02	2	0.08	0.01	0.03	0.00	0.00	22.3
8	226	4596	181	0	0	-37	458	4.02	4.02	4.02	4.02	2	0.08	0.01	0.03	0.00	0.00	22.3
9	226	4815	183	-1	0	-89	456	4.02	4.02	4.02	4.02	2	0.08	0.01	0.03	0.00	0.00	22.3
10	226	4696	162	-5	0	-56	456	4.02	4.02	4.02	4.02	2	0.08	0.00	0.03	0.00	0.00	22.3
11	226	4761	163	-6	0	-72	455	4.02	4.02	4.02	4.02	2	0.08	0.00	0.03	0.00	0.00	22.3
12	226	4660	192	2	0	-54	458	4.02	4.02	4.02	4.02	2	0.08	0.01	0.03	0.00	0.00	22.3
13	226	4726	193	2	0	-70	458	4.02	4.02	4.02	4.02	2	0.08	0.01	0.03	0.00	0.00	22.3
14	226	4607	172	-2	0	-37	458	4.02	4.02	4.02	4.02	2	0.08	0.00	0.03	0.00	0.00	22.3
15	226	4825	174	-4	0	-89	455	4.02	4.02	4.02	4.02	2	0.08	0.01	0.03	0.00	0.00	22.3
16	226	4596	181	0	0	-37	458	4.02	4.02	4.02	4.02	2	0.08	0.01	0.03	0.00	0.00	22.3
17	226	4815	183	-1	0	-89	456	4.02	4.02	4.02	4.02	2	0.08	0.01	0.03	0.00	0.00	22.3
18	226	7241	248	-27	0	-234	571	4.02	4.02	4.02	4.02	3	0.10	0.01	0.04	0.00	0.00	22.3
19	226	7140	259	20	0	-126	591	4.02	4.02	4.02	4.02	3	0.11	0.01	0.05	0.00	0.00	22.3
20	226	7325	248	140	0	-437	580	4.02	4.02	4.02	4.02	3	0.13	0.01	0.04	0.00	0.00	22.3
37	226	6940	235	-43	0	-239	569	4.02	4.02	4.02	4.02	3	0.10	0.01	0.04	0.00	0.00	22.3
38	226	6772	254	35	0	-59	602	4.02	4.02	4.02	4.02	3	0.11	0.01	0.05	0.00	0.00	22.3
39	226	7081	235	236	0	-578	583	4.02	4.02	4.02	4.02	3	0.17	0.01	0.04	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	282	6124	-44	-2	0	-81	594	4.02	4.02	4.02	4.02	3	0.10	0.00	0.01	0.00	0.00	22.3
2	282	4696	-50	-5	0	-53	456	4.02	4.02	4.02	4.02	2	0.08	0.00	0.01	0.00	0.00	22.3
3	282	4761	-48	-6	0	-69	455	4.02	4.02	4.02	4.02	2	0.08	0.00	0.01	0.00	0.00	22.3
4	282	4660	-20	2	0	-55	458	4.02	4.02	4.02	4.02	2	0.08	0.00	0.00	0.00	0.00	22.3
5	282	4726	-18	2	0	-71	458	4.02	4.02	4.02	4.02	2	0.08	0.00	0.00	0.00	0.00	22.3
6	282	4607	-40	-2	0	-36	458	4.02	4.02	4.02	4.02	2	0.08	0.00	0.01	0.00	0.00	22.3
7	282	4825	-38	-4	0	-87	455	4.02	4.02	4.02	4.02	2	0.08	0.00	0.01	0.00	0.00	22.3
8	282	4596	-30	0	0	-37	458	4.02	4.02	4.02	4.02	2	0.08	0.00	0.01	0.00	0.00	22.3
9	282	4815	-28	-1	0	-88	456	4.02	4.02	4.02	4.02	2	0.08	0.00	0.01	0.00	0.00	22.3
10	282	4696	-50	-5	0	-53	456	4.02	4.02	4.02	4.02	2	0.08	0.00	0.01	0.00	0.00	22.3
11	282	4761	-48	-6	0	-69	455	4.02	4.02	4.02	4.02	2	0.08	0.00	0.01	0.00	0.00	22.3
12	282	4660	-20	2	0	-55	458	4.02	4.02	4.02	4.02	2	0.08	0.00	0.00	0.00	0.00	22.3
13	282	4726	-18	2	0	-71	458	4.02	4.02	4.02	4.02	2	0.08	0.00	0.00	0.00	0.00	22.3
14	282	4607	-40	-2	0	-36	458	4.02	4.02	4.02	4.02	2	0.08	0.00	0.01	0.00	0.00	22.3
15	282	4825	-38	-4	0	-87	455	4.02	4.02	4.02	4.02	2	0.08	0.00	0.01	0.00	0.00	22.3
16	282	4596	-30	0	0	-37	458	4.02	4.02	4.02	4.02	2	0.08	0.00	0.01	0.00	0.00	22.3
17	282	4815	-28	-1	0	-88	456	4.02	4.02	4.02	4.02	2	0.08	0.00	0.01	0.00	0.00	22.3
18	282	7241	-28	-27	0	-219	571	4.02	4.02	4.02	4.02	3	0.10	0.00	0.00	0.00	0.00	22.3
19	282	7140	-16	20	0	-138	591	4.02	4.02	4.02	4.02	3	0.11	0.00	0.00	0.00	0.00	22.3
20	282	7325	-27	140	0	-517	580	4.02	4.02	4.02	4.02	3	0.16	0.00	0.00	0.00	0.00	22.3
37	282	6940	-40	-43	0	-214	569	4.02	4.02	4.02	4.02	3	0.10	0.00	0.01	0.00	0.00	22.3
38	282	6772	-21	35	0	-79	602	4.02	4.02	4.02	4.02	3	0.11	0.00	0.00	0.00	0.00	22.3
39	282	7081	-40	236	0	-711	583	4.02	4.02	4.02	4.02	3	0.21	0.01	0.04	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	339	6124	-319	-2	0	-79	594	4.02	4.02	4.02	4.02	3	0.10	0.01	0.06	0.00	0.00	22.3
2	339	4696	-261	-5	0	-50	456	4.02	4.02	4.02	4.02	2	0.08	0.01	0.05	0.00	0.00	22.3
3	339	4761	-260	-6	0	-65	455	4.02	4.02	4.02	4.02	2	0.08	0.01	0.05	0.00	0.00	22.3
4	339	4660	-231	2	0	-57	458	4.02	4.02	4.02	4.02	2	0.08	0.01	0.04	0.00	0.00	22.3
5	339	4726	-230	2	0	-72	458	4.02	4.02	4.02	4.02	2	0.08	0.01	0.04	0.00	0.00	22.3
6	339	4607	-251	-2	0	-35	458	4.02	4.02	4.02	4.02	2	0.08	0.01	0.04	0.00	0.00	22.3
7	339	4825	-249	-4	0	-85	455	4.02	4.02	4.02	4.02	2	0.08	0.01	0.04	0.00	0.00	22.3
8	339	4596	-242	0	0	-37	458	4.02	4.02	4.02	4.02	2	0.08	0.01	0.04	0.00	0.00	22.3
9	339	4815	-240	-1	0	-87	456	4.02	4.02	4.02	4.02	2	0.08	0.01	0.04	0.00	0.00	22.3
10	339	4696	-261	-5	0	-50	456	4.02	4.02	4.02	4.02	2	0.08	0.01	0.05	0.00	0.00	22.3
11	339	4761	-260	-6	0	-65	455	4.02	4.02	4.02	4.02	2	0.08	0.01	0.05	0.00	0.00	22.3
12	339	4660	-231	2	0	-57	458	4.02	4.02	4.02	4.02	2	0.08	0.01	0.04	0.00	0.00	22.3
13	339	4726	-230	2	0	-72	458	4.02	4.02	4.02	4.02	2	0.08	0.01	0.04	0.00	0.00	22.3
14	339	4607	-251	-2	0	-35	458	4.02	4.02	4.02	4.02	2	0.08	0.01	0.04	0.00	0.00	22.3
15	339	4825	-249	-4	0	-85	455	4.02	4.02	4.02	4.02	2	0.08	0.01	0.04	0.00	0.00	22.3
16	339	4596	-242	0	0	-37	458	4.02	4.02	4.02	4.02	2	0.08	0.01	0.04	0.00	0.00	22.3
17	339	4815	-240	-1	0	-87	456	4.02	4.02	4.02	4.02	2	0.08	0.01	0.04	0.00	0.00	22.3
18	339	7241	-303	-27	0	-203	571	4.02	4.02	4.02	4.02	3	0.10	0.01	0.05	0.00	0.00	22.3
19	339	7140	-291	20	0	-149	591	4.02	4.02	4.02	4.02	3	0.11	0.01	0.05	0.00	0.00	22.3
20	339	7325	-302	140	0	-596	580	4.02	4.02	4.02	4.02	3	0.18	0.01	0.05	0.00	0.00	22.3
37	339	6940	-316	-43	0	-190	569	4.02	4.02	4.02	4.02	3	0.10	0.01	0.06	0.00	0.00	22.3
38	339	6772	-296	35	0	-99	602	4.02	4.02	4.02	4.02	3	0.11	0.01	0.05	0.00	0.00	22.3
39	339	7081	-315	236	0	-845	583	4.02	4.02	4.02	4.02	3	0.26	0.01	0.06	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	396	6124	-595	-2	0	-78	534	4.02	4.02	4.02	4.02	3	0.09	0.02	0.11	0.00	0.00	22.3
2	396	4696	-473	-5	0	-47	401	4.02	4.02	4.02	4.02	2	0.07	0.01	0.08	0.00	0.00	22.3
3	396	4761	-472	-6	0	-62	400	4.02	4.02	4.02	4.02	2	0.07	0.01	0.08	0.00	0.00	22.3
4	396	4660	-443	2	0	-58	421	4.02	4.02	4.02	4.02	2	0.07	0.01	0.08	0.00	0.00	22.3
5	396	4726	-442	2	0	-73	421	4.02	4.02	4.02	4.02	2	0.07	0.01	0.08	0.00	0.00	22.3
6	396	4607	-463	-2	0	-34	408	4.02	4.02	4.02	4.02	2	0.07	0.01	0.08	0.00	0.00	22.3
7	396	4825	-461	-4	0	-83	407	4.02	4.02	4.02	4.02	2	0.07	0.01	0.08	0.00	0.00	22.3
8	396	4596	-454	0	0	-37	415	4.02	4.02	4.02	4.02	2	0.07	0.01	0.08	0.00	0.00	22.3
9	396	4815	-452	-1	0	-86	413	4.02	4.02	4.02	4.02	2	0.07	0.01	0.08	0.00	0.00	22.3
10	396	4696	-473	-5	0	-47	401	4.02	4.02	4.02	4.02	2	0.07	0.01	0.08	0.00	0.00	22.3
11	396	4761	-472	-6	0	-62	400	4.02	4.02	4.02	4.02	2	0.07	0.01	0.08	0.00	0.00	22.3
12	396	4660	-443	2	0	-58	421	4.02	4.02	4.02	4.02	2	0.07	0.01	0.08	0.00	0.00	22.3
13	396	4726	-442	2	0	-73	421	4.02	4.02	4.02	4.02	2	0.07	0.01	0.08	0.00	0.00	22.3
14	396	4607	-463	-2	0	-34	408	4.02	4.02	4.02	4.02	2	0.07	0.01	0.08	0.00	0.00	22.3
15	396	4825	-461	-4	0	-83	407	4.02	4.02	4.02	4.02	2	0.07	0.01	0.08	0.00	0.00	22.3
16	396	4596	-454	0	0	-37	415	4.02	4.02	4.02	4.02	2	0.07	0.01	0.08	0.00	0.00	22.3
17	396	4815	-452	-1	0	-86	413	4.02	4.02	4.02	4.02	2	0.07	0.01	0.08	0.00	0.00	22.3
18	396	7241	-578	-27	0	-188	522	4.02	4.02	4.02	4.02	3	0.09	0.02	0.10	0.00	0.00	22.3
19	396	7140	-567	20	0	-160	549	4.02	4.02	4.02	4.02	3	0.10	0.02	0.10	0.00	0.00	22.3
20	396	7325	-578	140	0	-675	530	4.02	4.02	4.02	4.02	3	0.21	0.02	0.10	0.00	0.00	22.3
37	396	6940	-591	-43	0	-166	511	4.02	4.02	4.02	4.02	3	0.09	0.02	0.11	0.00	0.00	22.3
38	396	6772	-572	35	0	-119	557	4.02	4.02	4.02	4.02	3	0.10	0.02	0.10	0.00	0.00	22.3
39	396	7081	-591	236	0	-978	526	4.02	4.02	4.02	4.02	3	0.30	0.02	0.11	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	452	6124	-870	-2	0	-77	-622	4.02	4.02	4.02	4.02	3	0.11	0.03	0.15	0.00	0.00	22.3
2	452	4696	-685	-5	0	-44	-513	4.02	4.02	4.02	4.02	2	0.09	0.02	0.12	0.00	0.00	22.3
3	452	4761	-684	-6	0	-59	-513	4.02	4.02	4.02	4.02	2	0.09	0.02	0.12	0.00	0.00	22.3
4	452	4660	-655	2	0	-59	-445	4.02	4.02	4.02	4.02	2	0.08	0.02	0.12	0.00	0.00	22.3
5	452	4726	-654	2	0	-74	-444	4.02	4.02	4.02	4.02	2	0.08	0.02	0.12	0.00	0.00	22.3
6	452	4607	-675	-2	0	-33	-490	4.02	4.02	4.02	4.02	2	0.09	0.02	0.12	0.00	0.00	22.3

7	452	4825	-673	-4	0	-81	-488	4.02	4.02	4.02	4.02	2	0.09	0.02	0.12	0.00	0.00	22.3
8	452	4596	-666	0	0	-37	-469	4.02	4.02	4.02	4.02	2	0.08	0.02	0.12	0.00	0.00	22.3
9	452	4815	-664	-1	0	-86	-468	4.02	4.02	4.02	4.02	2	0.08	0.02	0.12	0.00	0.00	22.3
10	452	4696	-685	-5	0	-44	-513	4.02	4.02	4.02	4.02	2	0.09	0.02	0.12	0.00	0.00	22.3
11	452	4761	-684	-6	0	-59	-513	4.02	4.02	4.02	4.02	2	0.09	0.02	0.12	0.00	0.00	22.3
12	452	4660	-655	2	0	-59	-445	4.02	4.02	4.02	4.02	2	0.08	0.02	0.12	0.00	0.00	22.3
13	452	4726	-654	2	0	-74	-444	4.02	4.02	4.02	4.02	2	0.08	0.02	0.12	0.00	0.00	22.3
14	452	4607	-675	-2	0	-33	-490	4.02	4.02	4.02	4.02	2	0.09	0.02	0.12	0.00	0.00	22.3
15	452	4825	-673	-4	0	-81	-488	4.02	4.02	4.02	4.02	2	0.09	0.02	0.12	0.00	0.00	22.3
16	452	4596	-666	0	0	-37	-469	4.02	4.02	4.02	4.02	2	0.08	0.02	0.12	0.00	0.00	22.3
17	452	4815	-664	-1	0	-86	-468	4.02	4.02	4.02	4.02	2	0.08	0.02	0.12	0.00	0.00	22.3
18	452	7241	-854	-27	0	-173	-608	4.02	4.02	4.02	4.02	3	0.11	0.02	0.15	0.00	0.00	22.3
19	452	7140	-842	20	0	-171	-563	4.02	4.02	4.02	4.02	3	0.10	0.02	0.15	0.00	0.00	22.3
20	452	7325	-853	140	0	-755	-598	4.02	4.02	4.02	4.02	3	0.23	0.02	0.15	0.00	0.00	22.3
37	452	6940	-867	-43	0	-142	-639	4.02	4.02	4.02	4.02	3	0.12	0.03	0.15	0.00	0.00	22.3
38	452	6772	-847	35	0	-140	-563	4.02	4.02	4.02	4.02	3	0.10	0.02	0.15	0.00	0.00	22.3
39	452	7081	-866	236	0	-1112	-623	4.02	4.02	4.02	4.02	3	0.34	0.03	0.15	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	508	6124	-1146	-2	0	-76	-1331	4.02	4.02	4.02	4.02	3	0.23	0.03	0.20	0.00	0.00	22.3
2	508	4696	-897	-5	0	-41	-1067	4.02	4.02	4.02	4.02	2	0.19	0.03	0.16	0.00	0.00	22.3
3	508	4761	-896	-6	0	-56	-1066	4.02	4.02	4.02	4.02	2	0.19	0.03	0.16	0.00	0.00	22.3
4	508	4660	-867	2	0	-61	-982	4.02	4.02	4.02	4.02	2	0.17	0.03	0.15	0.00	0.00	22.3
5	508	4726	-866	2	0	-75	-981	4.02	4.02	4.02	4.02	2	0.17	0.03	0.15	0.00	0.00	22.3
6	508	4607	-887	-2	0	-31	-1038	4.02	4.02	4.02	4.02	2	0.18	0.03	0.16	0.00	0.00	22.3
7	508	4825	-885	-4	0	-79	-1035	4.02	4.02	4.02	4.02	2	0.18	0.03	0.16	0.00	0.00	22.3
8	508	4596	-878	0	0	-37	-1013	4.02	4.02	4.02	4.02	2	0.18	0.03	0.16	0.00	0.00	22.3
9	508	4815	-876	-1	0	-85	-1011	4.02	4.02	4.02	4.02	2	0.18	0.03	0.16	0.00	0.00	22.3
10	508	4696	-897	-5	0	-41	-1067	4.02	4.02	4.02	4.02	2	0.19	0.03	0.16	0.00	0.00	22.3
11	508	4761	-896	-6	0	-56	-1066	4.02	4.02	4.02	4.02	2	0.19	0.03	0.16	0.00	0.00	22.3
12	508	4660	-867	2	0	-61	-982	4.02	4.02	4.02	4.02	2	0.17	0.03	0.15	0.00	0.00	22.3
13	508	4726	-866	2	0	-75	-981	4.02	4.02	4.02	4.02	2	0.17	0.03	0.15	0.00	0.00	22.3
14	508	4607	-887	-2	0	-31	-1038	4.02	4.02	4.02	4.02	2	0.18	0.03	0.16	0.00	0.00	22.3
15	508	4825	-885	-4	0	-79	-1035	4.02	4.02	4.02	4.02	2	0.18	0.03	0.16	0.00	0.00	22.3
16	508	4596	-878	0	0	-37	-1013	4.02	4.02	4.02	4.02	2	0.18	0.03	0.16	0.00	0.00	22.3
17	508	4815	-876	-1	0	-85	-1011	4.02	4.02	4.02	4.02	2	0.18	0.03	0.16	0.00	0.00	22.3
18	508	7241	-1129	-27	0	-158	-1308	4.02	4.02	4.02	4.02	3	0.24	0.03	0.20	0.00	0.00	22.3
19	508	7140	-1118	20	0	-182	-1256	4.02	4.02	4.02	4.02	3	0.23	0.03	0.20	0.00	0.00	22.3
20	508	7325	-1129	140	0	-834	-1298	4.02	4.02	4.02	4.02	3	0.25	0.03	0.20	0.00	0.00	22.3
37	508	6940	-1142	-43	0	-118	-1346	4.02	4.02	4.02	4.02	3	0.24	0.03	0.20	0.00	0.00	22.3
38	508	6772	-1123	35	0	-160	-1258	4.02	4.02	4.02	4.02	3	0.23	0.03	0.20	0.00	0.00	22.3
39	508	7081	-1142	236	0	-1245	-1329	4.02	4.02	4.02	4.02	3	0.38	0.03	0.20	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	565	6124	-1421	-2	0	-74	-1476	4.02	4.02	4.02	4.02	3	0.26	0.04	0.25	0.00	0.00	22.3
2	565	4696	-1109	-5	0	-38	-1179	4.02	4.02	4.02	4.02	2	0.21	0.03	0.20	0.00	0.00	22.3
3	565	4761	-1108	-6	0	-52	-1179	4.02	4.02	4.02	4.02	2	0.21	0.03	0.20	0.00	0.00	22.3
4	565	4660	-1079	2	0	-62	-1093	4.02	4.02	4.02	4.02	2	0.19	0.03	0.19	0.00	0.00	22.3
5	565	4726	-1078	2	0	-76	-1092	4.02	4.02	4.02	4.02	2	0.19	0.03	0.19	0.00	0.00	22.3
6	565	4607	-1099	-2	0	-30	-1150	4.02	4.02	4.02	4.02	2	0.20	0.03	0.20	0.00	0.00	22.3
7	565	4825	-1097	-4	0	-77	-1147	4.02	4.02	4.02	4.02	2	0.20	0.03	0.20	0.00	0.00	22.3
8	565	4596	-1090	0	0	-37	-1124	4.02	4.02	4.02	4.02	2	0.20	0.03	0.19	0.00	0.00	22.3
9	565	4815	-1088	-1	0	-84	-1122	4.02	4.02	4.02	4.02	2	0.20	0.03	0.19	0.00	0.00	22.3
10	565	4696	-1109	-5	0	-38	-1179	4.02	4.02	4.02	4.02	2	0.21	0.03	0.20	0.00	0.00	22.3
11	565	4761	-1108	-6	0	-52	-1179	4.02	4.02	4.02	4.02	2	0.21	0.03	0.20	0.00	0.00	22.3
12	565	4660	-1079	2	0	-62	-1093	4.02	4.02	4.02	4.02	2	0.19	0.03	0.19	0.00	0.00	22.3
13	565	4726	-1078	2	0	-76	-1092	4.02	4.02	4.02	4.02	2	0.19	0.03	0.19	0.00	0.00	22.3
14	565	4607	-1099	-2	0	-30	-1150	4.02	4.02	4.02	4.02	2	0.20	0.03	0.20	0.00	0.00	22.3
15	565	4825	-1097	-4	0	-77	-1147	4.02	4.02	4.02	4.02	2	0.20	0.03	0.20	0.00	0.00	22.3
16	565	4596	-1090	0	0	-37	-1124	4.02	4.02	4.02	4.02	2	0.20	0.03	0.19	0.00	0.00	22.3
17	565	4815	-1088	-1	0	-84	-1122	4.02	4.02	4.02	4.02	2	0.20	0.03	0.19	0.00	0.00	22.3
18	565	7241	-1405	-27	0	-142	-1452	4.02	4.02	4.02	4.02	3	0.26	0.04	0.25	0.00	0.00	22.3
19	565	7140	-1393	20	0	-194	-1399	4.02	4.02	4.02	4.02	3	0.25	0.04	0.25	0.00	0.00	22.3
20	565	7325	-1404	140	0	-913	-1442	4.02	4.02	4.02	4.02	3	0.28	0.04	0.25	0.00	0.00	22.3
37	565	6940	-1418	-43	0	-94	-1491	4.02	4.02	4.02	4.02	3	0.27	0.04	0.25	0.00	0.00	22.3
38	565	6772	-1398	35	0	-180	-1402	4.02	4.02	4.02	4.02	3	0.25	0.04	0.25	0.00	0.00	22.3
39	565	7081	-1417	236	0	-1379	-1474	4.02	4.02	4.02	4.02	3	0.42	0.04	0.25	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

Nome travata: **Trave_401_IP1** Descrizione: **Trave_4 7-12-17-22-32**
ASTA NUM. 3 NI 37 NF 39 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y Permanente qy tot.
qy medio: 375.00 272.00 647.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	5629	2344	19	0	-24	-1900	4.02	4.02	4.02	4.02	3	0.33	0.07	0.42	0.00	0.00	22.3
2	0	4224	1787	10	0	-25	-1417	4.02	4.02	4.02	4.02	2	0.25	0.05	0.32	0.00	0.00	22.3
3	0	4289	1786	13	0	-33	-1416	4.02	4.02	4.02	4.02	2	0.25	0.05	0.32	0.00	0.00	22.3
4	0	4371	1820	17	0	-4	-1508	4.02	4.02	4.02	4.02	2	0.26	0.05	0.32	0.00	0.00	22.3
5	0	4436	1818	20	0	-12	-1506	4.02	4.02	4.02	4.02	2	0.26	0.05	0.32	0.00	0.00	22.3
6	0	4200	1800	9	0	-8	-1451	4.02	4.02	4.02	4.02	2	0.25	0.05	0.32	0.00	0.00	22.3
7	0	4416	1796	19	0	-35	-1446	4.02	4.02	4.02	4.02	2	0.25	0.05	0.32	0.00	0.00	22.3
8	0	4244	1810	11	0	-2	-1478	4.02	4.02	4.02	4.02	2	0.26	0.05	0.32	0.00	0.00	22.3
9	0	4460	1806	21	0	-29	-1473	4.02	4.02	4.02	4.02	2	0.26	0.05	0.32	0.00	0.00	22.3
10	0	4224	1787	10	0	-25	-1417	4.02	4.02	4.02	4.02	2	0.25	0.05	0.32	0.00	0.00	22.3
11	0	4289	1786	13	0	-33	-1416	4.02	4.02	4.02	4.02	2	0.25	0.05	0.32	0.00	0.00	22.3
12	0	4371	1820	17	0	-4	-1508	4.02	4.02	4.02	4.02	2	0.26	0.05	0.32	0.00	0.00	22.3
13	0	4436	1818	20	0	-12	-1506	4.02	4.02	4.02	4.02	2	0.26	0.05	0.32	0.00	0.00	22.3
14	0	4200	1800	9	0	-8	-1451	4.02	4.02	4.02	4.02	2	0.25	0.05	0.32	0.00	0.00	22.3
15	0	4416	1796	19	0	-35	-1446	4.02	4.02	4.02	4.02	2	0.25	0.05	0.32	0.00	0.00	22.3
16	0	4244	1810	11	0	-2	-1478	4.02	4.02	4.02	4.02	2	0.26	0.05	0.32	0.00	0.00	22.3
17	0	4460	1806	21	0	-29	-1473	4.02	4.02	4.02	4.02	2	0.26	0.05	0.32	0.00	0.00	22.3
18	0	6108	2282	2	0	-151	-1749	4.02	4.02	4.02	4.02	3	0.31	0.07	0.41	0.00	0.00	22.3
19	0	7093	2331	83	0	31	-1892	4.02	4.02	4.02	4.02	3	0.34	0.07	0.42	0.00	0.00	22.3
20	0	6747	2310	-83	0	-780	-1835	4.02	4.02	4.02	4.02	3	0.33	0.07	0.41	0.00	0.00	22.3
37	0	5471	2278	-32	0	-200	-1726	4.02	4.02	4.02	4.02	3	0.29	0.07	0.41	0.00	0.00	22.3
38	0	7113	2359	103	0	105	-1964	4.02	4.02	4.02	4.02	3	0.36	0.07	0.42	0.00	0.00	22.3
39	0	6536	2325	-174	0	-1247	-1871	4.02	4.02	4.02	4.02	3	0.37	0.07	0.41	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	57	5629	1837	19	0	-35	-1649	4.02	4.02	4.02	4.02	3	0.28	0.05	0.33	0.00	0.00	22.3
2	57	4224	1397	10	0	-30	-1225	4.02	4.02	4.02	4.02	2	0.21	0.04	0.25	0.00	0.00	22.3
3	57	4289	1396	13	0	-40	-1224	4.02	4.02	4.02	4.02	2	0.21	0.04	0.25	0.00	0.00	22.3
4	57	4371	1430	17	0	-13	-1314	4.02	4.02	4.02	4.02	2	0.23	0.04	0.25	0.00	0.00	22.3
5	57	4436	1428	20	0	-23	-1312	4.02	4.02	4.02	4.02	2	0.23	0.04	0.25	0.00	0.00	22.3
6	57	4200	1410	9	0	-13	-1258	4.02	4.02	4.02	4.02	2	0.22	0.04	0.25	0.00	0.00	22.3
7	57	4416	1406	19	0	-46	-1253	4.02	4.02	4.02	4.02	2	0.22	0.04	0.25	0.00	0.00	22.3
8	57	4244	1420	11	0	-8	-1285	4.02	4.02	4.02	4.02	2	0.22	0.04	0.25	0.00	0.00	22.3
9	57	4460	1416	21	0	-41	-1280	4.02	4.02	4.02	4.02	2	0.22	0.04	0.25	0.00	0.00	22.3
10	57	4224	1397	10	0	-30	-1225	4.02	4.02	4.02	4.02	2	0.21	0.04	0.25	0.00	0.00	22.3
11	57	4289	1396	13	0	-40	-1224	4.02	4.02	4.02	4.02	2	0.21	0.04	0.25	0.00	0.00	22.3
12	57	4371	1430	17	0	-13	-1314	4.02	4.02	4.02	4.02	2	0.23	0.04	0.25	0.00	0.00	22.3
13	57	4436	1428	20	0	-23	-1312	4.02	4.02	4.02	4.02	2	0.23	0.04	0.25	0.00	0.00	22.3
14	57	4200	1410	9	0	-13	-1258	4.02	4.02	4.02	4.02	2	0.22	0.04	0.25	0.00	0.00	22.3
15	57	4416	1406	19	0	-46	-1253	4.02	4.02	4.02	4.02	2	0.22	0.04	0.25	0.00	0.00	22.3
16	57	4244	1420	11	0	-8	-1285	4.02	4.02	4.02	4.02	2	0.22	0.04	0.25	0.00	0.00	22.3
17	57	4460	1416	21	0	-41	-1280	4.02	4.02	4.02	4.02	2	0.22	0.04	0.25	0.00	0.00	22.3
18	57	6108	1775	2	0	-152	-1502	4.02	4.02	4.02	4.02	3	0.26	0.05	0.32	0.00	0.00	22.3
19	57	7093	1824	83	0	-15	-1642	4.02	4.02	4.02	4.02	3	0.30	0.05	0.32	0.00	0.00	22.3
20	57	6747	1803	-83	0	-733	-1586	4.02	4.02	4.02	4.02	3	0.28	0.05	0.32	0.00	0.00	22.3
37	57	5471	1771	-32	0	-181	-1479	4.02	4.02	4.02	4.02	3	0.25	0.05	0.32	0.00	0.00	22.3
38	57	7113	1852	103	0	47	-1712	4.02	4.02	4.02	4.02	3	0.31	0.05	0.33	0.00	0.00	22.3
39	57	6536	1818	-174	0	-1149	-1621	4.02	4.02	4.02	4.02	3	0.34	0.05	0.32	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	113	5629	1337	19	0	-46	854	4.02	4.02	4.02	4.02	3	0.15	0.04	0.24	0.00	0.00	22.3
2	113	4224	1013	10	0	-36	676	4.02	4.02	4.02	4.02	2	0.12	0.03	0.18	0.00	0.00	22.3
3	113	4289	1012	13	0	-48	675	4.02	4.02	4.02	4.02	2	0.12	0.03	0.18	0.00	0.00	22.3
4	113	4371	1045	17	0	-23	638	4.02	4.02	4.02	4.02	2	0.11	0.03	0.19	0.00	0.00	22.3
5	113	4436	1044	20	0	-34	638	4.02	4.02	4.02	4.02	2	0.11	0.03	0.19	0.00	0.00	22.3
6	113	4200	1025	9	0	-18	663	4.02	4.02	4.02	4.02	2	0.12	0.03	0.18	0.00	0.00	22.3
7	113	4416	1022	19	0	-56	661	4.02	4.02	4.02	4.02	2	0.12	0.03	0.18	0.00	0.00	22.3
8	113	4244	1035	11	0	-14	651	4.02	4.02	4.02	4.02	2	0.11	0.03	0.18	0.00	0.00	22.3
9	113	4460	1031	21	0	-52	650	4.02	4.02	4.02	4.02	2	0.11	0.03	0.18	0.00	0.00	22.3
10	113	4224	1013	10	0	-36	676	4.02	4.02	4.02	4.02	2	0.12	0.03	0.18	0.00	0.00	22.3
11	113	4289	1012	13	0	-48	675	4.02	4.02	4.02	4.02	2	0.12	0.03	0.18	0.00	0.00	22.3
12	113	4371	1045	17	0	-23	638	4.02	4.02	4.02	4.02	2	0.11	0.03	0.19	0.00	0.00	22.3
13	113	4436	1044	20	0	-34	638	4.02	4.02	4.02	4.02	2	0.11	0.03	0.19	0.00	0.00	22.3
14	113	4200	1025	9	0	-18	663	4.02	4.02	4.02	4.02	2	0.12	0.03	0.18	0.00	0.00	22.3
15	113	4416	1022	19	0	-56	661	4.02	4.02	4.02	4.02	2	0.12	0.03	0.18	0.00	0.00	22.3
16	113	4244	1035	11	0	-14	651	4.02	4.02	4.02	4.02	2	0.11	0.03	0.18	0.00	0.00	22.3
17	113	4460	1031	21	0	-52	650	4.02	4.02	4.02	4.02	2	0.11	0.03	0.18	0.00	0.00	22.3
18	113	6108	1275	2	0	-153	904	4.02	4.02	4.02	4.02	3	0.16	0.04	0.23	0.00	0.00	22.3
19	113	7093	1324	83	0	-62	841	4.02	4.02	4.02	4.02	3	0.15	0.04	0.24	0.00	0.00	22.3
20	113	6747	1303	-83	0	-685	864	4.02	4.02	4.02	4.02	3	0.20	0.04	0.23	0.00	0.00	22.3
37	113	5471	1271	-32	0	-163	920	4.02	4.02	4.02	4.02	3	0.16	0.04	0.23	0.00	0.00	22.3
38	113	7113	1352	103	0	-12	815	4.02	4.02	4.02	4.02	3	0.15	0.04	0.24	0.00	0.00	22.3
39	113	6536	1318	-174	0	-1050	852	4.02	4.02	4.02	4.02	3	0.31	0.04	0.23	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	170	5629	844	19	0	-57	1199	4.02	4.02	4.02	4.02	3	0.21	0.02	0.15	0.00	0.00	22.3
2	170	4224	634	10	0	-42	923	4.02	4.02	4.02	4.02	2	0.16	0.02	0.11	0.00	0.00	22.3
3	170	4289	633	13	0	-55	921	4.02	4.02	4.02	4.02	2	0.16	0.02	0.11	0.00	0.00	22.3
4	170	4371	666	17	0	-32	923	4.02	4.02	4.02	4.02	2	0.16	0.02	0.12	0.00	0.00	22.3
5	170	4436	665	20	0	-45	922	4.02	4.02	4.02	4.02	2	0.16	0.02	0.12	0.00	0.00	22.3
6	170	4200	646	9	0	-23	925	4.02	4.02	4.02	4.02	2	0.16	0.02	0.12	0.00	0.00	22.3
7	170	4416	643	19	0	-67	919	4.02	4.02	4.02	4.02	2	0.16	0.02	0.11	0.00	0.00	22.3
8	170	4244	656	11	0	-20	925	4.02	4.02	4.02	4.02	2	0.16	0.02	0.12	0.00	0.00	22.3
9	170	4460	652	21	0	-64	920	4.02	4.02	4.02	4.02	2	0.16	0.02	0.12	0.00	0.00	22.3
10	170	4224	634	10	0	-42	923	4.02	4.02	4.02	4.02	2	0.16	0.02	0.11	0.00	0.00	22.3
11	170	4289	633	13	0	-55	921	4.02	4.02	4.02	4.02	2	0.16	0.02	0.11	0.00	0.00	22.3
12	170	4371	666	17	0	-32	923	4.02	4.02	4.02	4.02	2	0.16	0.02	0.12	0.00	0.00	22.3
13	170	4436	665	20	0	-45	922	4.02	4.02	4.02	4.02	2	0.16	0.02	0.12	0.00	0.00	22.3
14	170	4200	646	9	0	-23	925	4.02	4.02	4.02	4.02	2	0.16	0.02	0.12	0.00	0.00	22.3
15	170	4416	643	19	0	-67	919	4.02	4.02	4.02	4.02	2	0.16	0.02	0.11	0.00	0.00	22.3
16	170	4244	656	11	0	-20	925	4.02	4.02	4.02	4.02	2	0.16	0.02	0.12	0.00	0.00	22.3
17	170	4460	652	21	0	-64	920	4.02	4.02	4.02	4.02	2	0.16	0.02	0.12	0.00	0.00	22.3
18	170	6108	782	2	0	-154	1177	4.02	4.02	4.02	4.02	3	0.21	0.02	0.14	0.00	0.00	22.3
19	170	7093	831	83	0	-109	1171	4.02	4.02	4.02	4.02	3	0.21	0.02	0.15	0.00	0.00	22.3
20	170	6747	810	-83	0	-638	1170	4.02	4.02	4.02	4.02	3	0.21	0.02	0.14	0.00	0.00	22.3
37	170	5471	778	-32	0	-145	1187	4.02	4.02	4.02	4.02	3	0.20	0.02	0.14	0.00	0.00	22.3
38	170	7113	859	103	0	-70	1179	4.02	4.02	4.02	4.02	3	0.21	0.02	0.15	0.00	0.00	22.3
39	170	6536	825	-174	0	-952	1175	4.02	4.02	4.02	4.02	3	0.28	0.02	0.15	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	226	5629	359	19	0	-67	1199	4.02	4.02	4.02	4.02	3	0.21	0.01	0.06	0.00	0.00	22.3
2	226	4224	260	10	0	-48	923	4.02	4.02	4.02	4.02	2	0.16	0.01	0.05	0.00	0.00	22.3
3	226	4289	259	13	0	-62	921	4.02	4.02	4.02	4.02	2	0.16	0.01	0.05	0.00	0.00	22.3
4	226	4371	293	17	0	-41	923	4.02	4.02	4.02	4.02	2	0.16	0.01	0.05	0.00	0.00	22.3
5	226	4436	291	20	0	-56	922	4.02	4.02	4.02	4.02	2	0.16	0.01	0.05	0.00	0.00	22.3
6	226	4200	273	9	0	-28	925	4.02	4.02	4.02	4.02	2	0.16	0.01	0.05	0.00	0.00	22.3
7	226	4416	269	19	0	-77	919	4.02	4.02	4.02	4.02	2	0.16	0.01	0.05	0.00	0.00	22.3
8	226	4244	283	11	0	-26	925	4.02	4.02	4.02	4.02	2	0.16	0.01	0.05	0.00	0.00	22.3
9	226	4460	279	21	0	-76	920	4.02	4.02	4.02	4.02	2	0.16	0.01	0.05	0.00	0.00	22.3
10	226	4224	260	10	0	-48	923	4.02	4.02	4.02	4.02	2	0.16	0.01	0.05	0.00	0.00	22.3
11	226	4289	259	13	0	-62	921	4.02	4.02	4.02	4.02	2	0.16	0.01	0.05	0.00	0.00	22.3
12	226	4371	293	17	0	-41	923	4.02	4.02	4.02	4.02	2	0.16	0.01	0.05	0.00	0.00	22.3
13	226	4436	291	20	0	-56	922	4.02	4.02	4.02	4.02	2	0.16	0.01	0.05	0.00	0.00	22.3
14	226	4200	273	9	0	-28	925	4.02	4.02	4.02	4.02	2	0.16	0.01	0.05	0.00	0.00	22.3
15	226	4416	269	19	0	-77	919	4.02	4.02	4.02	4.02	2	0.16	0.01	0.05	0.00	0.00	22.3
16	226	4244	283	11	0	-26	925	4.02	4.02	4.02	4.02	2	0.16	0.01	0.05	0.00	0.00	22.3
17	226	4460	279	21	0	-76	920	4.02	4.02	4.02	4.02	2	0.16	0.01	0.05	0.00	0.00	22.3
18	226	6108	297	2	0	-155	1177	4.02	4.02	4.02	4.02	3	0.21	0.01	0.05	0.00	0.00	22.3
19	226	7093	346	83	0	-156	1171	4.02	4.02	4.02	4.02	3	0.21	0.01	0.06	0.00	0.00	22.3
20	226	6747	325	-83	0	-591	1170	4.02	4.02	4.02	4.02	3	0.21	0.01	0.06	0.00	0.00	22.3
37	226	5471	293	-32	0	-127	1187	4.02	4.02	4.02	4.02	3	0.20	0.01	0.05	0.00	0.00	22.3
38	226	7113	374	103	0	-128	1179	4.02	4.02	4.02	4.02	3	0.21	0.01	0.07	0.00	0.00	22.3
39	226	6536	340	-174	0	-854	1175	4.02	4.02	4.02	4.02	3	0.25	0.01	0.06	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	283	5629	-120	19	0	-78	1199	4.02	4.02	4.02	4.02	3	0.21	0.00	0.02	0.00	0.00	22.3
2	283	4224	-108	10	0	-53	923	4.02	4.02	4.02	4.02	2	0.16	0.00	0.02	0.00	0.00	22.3
3	283	4289	-109	13	0	-70	921	4.02	4.02	4.02	4.02	2	0.16	0.00	0.02	0.00	0.00	22.3
4	283	4371	-76	17	0	-51	923	4.02	4.02	4.02	4.02	2	0.16	0.00	0.01	0.00	0.00	22.3

5	283	4436	-77	20	0	-67	922	4.02	4.02	4.02	4.02	2	0.16	0.00	0.01	0.00	0.00	22.3
6	283	4200	-96	9	0	-33	925	4.02	4.02	4.02	4.02	2	0.16	0.00	0.02	0.00	0.00	22.3
7	283	4416	-99	19	0	-88	919	4.02	4.02	4.02	4.02	2	0.16	0.00	0.02	0.00	0.00	22.3
8	283	4244	-86	11	0	-33	925	4.02	4.02	4.02	4.02	2	0.16	0.00	0.02	0.00	0.00	22.3
9	283	4460	-90	21	0	-87	920	4.02	4.02	4.02	4.02	2	0.16	0.00	0.02	0.00	0.00	22.3
10	283	4224	-108	10	0	-53	923	4.02	4.02	4.02	4.02	2	0.16	0.00	0.02	0.00	0.00	22.3
11	283	4289	-109	13	0	-70	921	4.02	4.02	4.02	4.02	2	0.16	0.00	0.02	0.00	0.00	22.3
12	283	4371	-76	17	0	-51	923	4.02	4.02	4.02	4.02	2	0.16	0.00	0.01	0.00	0.00	22.3
13	283	4436	-77	20	0	-67	922	4.02	4.02	4.02	4.02	2	0.16	0.00	0.01	0.00	0.00	22.3
14	283	4200	-96	9	0	-33	925	4.02	4.02	4.02	4.02	2	0.16	0.00	0.02	0.00	0.00	22.3
15	283	4416	-99	19	0	-88	919	4.02	4.02	4.02	4.02	2	0.16	0.00	0.02	0.00	0.00	22.3
16	283	4244	-86	11	0	-33	925	4.02	4.02	4.02	4.02	2	0.16	0.00	0.02	0.00	0.00	22.3
17	283	4460	-90	21	0	-87	920	4.02	4.02	4.02	4.02	2	0.16	0.00	0.02	0.00	0.00	22.3
18	283	6108	-182	2	0	-156	1177	4.02	4.02	4.02	4.02	3	0.21	0.01	0.03	0.00	0.00	22.3
19	283	7093	-133	83	0	-202	1171	4.02	4.02	4.02	4.02	3	0.21	0.00	0.02	0.00	0.00	22.3
20	283	6747	-154	-83	0	-544	1170	4.02	4.02	4.02	4.02	3	0.21	0.00	0.03	0.00	0.00	22.3
37	283	5471	-186	-32	0	-108	1187	4.02	4.02	4.02	4.02	3	0.20	0.01	0.03	0.00	0.00	22.3
38	283	7113	-105	103	0	-186	1179	4.02	4.02	4.02	4.02	3	0.21	0.00	0.02	0.00	0.00	22.3
39	283	6536	-139	-174	0	-755	1175	4.02	4.02	4.02	4.02	3	0.22	0.01	0.03	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	339	5629	-592	19	0	-89	1199	4.02	4.02	4.02	4.02	3	0.21	0.02	0.11	0.00	0.00	22.3
2	339	4224	-471	10	0	-59	923	4.02	4.02	4.02	4.02	2	0.16	0.01	0.08	0.00	0.00	22.3
3	339	4289	-472	13	0	-77	921	4.02	4.02	4.02	4.02	2	0.16	0.01	0.08	0.00	0.00	22.3
4	339	4371	-439	17	0	-60	923	4.02	4.02	4.02	4.02	2	0.16	0.01	0.08	0.00	0.00	22.3
5	339	4436	-440	20	0	-78	922	4.02	4.02	4.02	4.02	2	0.16	0.01	0.08	0.00	0.00	22.3
6	339	4200	-459	9	0	-38	925	4.02	4.02	4.02	4.02	2	0.16	0.01	0.08	0.00	0.00	22.3
7	339	4416	-462	19	0	-98	919	4.02	4.02	4.02	4.02	2	0.16	0.01	0.08	0.00	0.00	22.3
8	339	4244	-449	11	0	-39	925	4.02	4.02	4.02	4.02	2	0.16	0.01	0.08	0.00	0.00	22.3
9	339	4460	-453	21	0	-99	920	4.02	4.02	4.02	4.02	2	0.16	0.01	0.08	0.00	0.00	22.3
10	339	4224	-471	10	0	-59	923	4.02	4.02	4.02	4.02	2	0.16	0.01	0.08	0.00	0.00	22.3
11	339	4289	-472	13	0	-77	921	4.02	4.02	4.02	4.02	2	0.16	0.01	0.08	0.00	0.00	22.3
12	339	4371	-439	17	0	-60	923	4.02	4.02	4.02	4.02	2	0.16	0.01	0.08	0.00	0.00	22.3
13	339	4436	-440	20	0	-78	922	4.02	4.02	4.02	4.02	2	0.16	0.01	0.08	0.00	0.00	22.3
14	339	4200	-459	9	0	-38	925	4.02	4.02	4.02	4.02	2	0.16	0.01	0.08	0.00	0.00	22.3
15	339	4416	-462	19	0	-98	919	4.02	4.02	4.02	4.02	2	0.16	0.01	0.08	0.00	0.00	22.3
16	339	4244	-449	11	0	-39	925	4.02	4.02	4.02	4.02	2	0.16	0.01	0.08	0.00	0.00	22.3
17	339	4460	-453	21	0	-99	920	4.02	4.02	4.02	4.02	2	0.16	0.01	0.08	0.00	0.00	22.3
18	339	6108	-654	2	0	-157	1177	4.02	4.02	4.02	4.02	3	0.21	0.02	0.12	0.00	0.00	22.3
19	339	7093	-605	83	0	-249	1171	4.02	4.02	4.02	4.02	3	0.21	0.02	0.11	0.00	0.00	22.3
20	339	6747	-626	-83	0	-497	1170	4.02	4.02	4.02	4.02	3	0.21	0.02	0.11	0.00	0.00	22.3
37	339	5471	-658	-32	0	-90	1187	4.02	4.02	4.02	4.02	3	0.20	0.02	0.12	0.00	0.00	22.3
38	339	7113	-577	103	0	-244	1179	4.02	4.02	4.02	4.02	3	0.21	0.02	0.10	0.00	0.00	22.3
39	339	6536	-611	-174	0	-657	1175	4.02	4.02	4.02	4.02	3	0.21	0.02	0.11	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	396	5629	-1056	19	0	-100	1066	4.02	4.02	4.02	4.02	3	0.18	0.03	0.19	0.00	0.00	22.3
2	396	4224	-828	10	0	-65	811	4.02	4.02	4.02	4.02	2	0.14	0.02	0.15	0.00	0.00	22.3
3	396	4289	-829	13	0	-84	809	4.02	4.02	4.02	4.02	2	0.14	0.02	0.15	0.00	0.00	22.3
4	396	4371	-796	17	0	-70	831	4.02	4.02	4.02	4.02	2	0.15	0.02	0.14	0.00	0.00	22.3
5	396	4436	-797	20	0	-89	829	4.02	4.02	4.02	4.02	2	0.15	0.02	0.14	0.00	0.00	22.3
6	396	4200	-816	9	0	-43	821	4.02	4.02	4.02	4.02	2	0.14	0.02	0.15	0.00	0.00	22.3
7	396	4416	-819	19	0	-109	813	4.02	4.02	4.02	4.02	2	0.14	0.02	0.15	0.00	0.00	22.3
8	396	4244	-806	11	0	-45	827	4.02	4.02	4.02	4.02	2	0.14	0.02	0.14	0.00	0.00	22.3
9	396	4460	-810	21	0	-110	820	4.02	4.02	4.02	4.02	2	0.14	0.02	0.14	0.00	0.00	22.3
10	396	4224	-828	10	0	-65	811	4.02	4.02	4.02	4.02	2	0.14	0.02	0.15	0.00	0.00	22.3
11	396	4289	-829	13	0	-84	809	4.02	4.02	4.02	4.02	2	0.14	0.02	0.15	0.00	0.00	22.3
12	396	4371	-796	17	0	-70	831	4.02	4.02	4.02	4.02	2	0.15	0.02	0.14	0.00	0.00	22.3
13	396	4436	-797	20	0	-89	829	4.02	4.02	4.02	4.02	2	0.15	0.02	0.14	0.00	0.00	22.3
14	396	4200	-816	9	0	-43	821	4.02	4.02	4.02	4.02	2	0.14	0.02	0.15	0.00	0.00	22.3
15	396	4416	-819	19	0	-109	813	4.02	4.02	4.02	4.02	2	0.14	0.02	0.15	0.00	0.00	22.3
16	396	4244	-806	11	0	-45	827	4.02	4.02	4.02	4.02	2	0.14	0.02	0.14	0.00	0.00	22.3
17	396	4460	-810	21	0	-110	820	4.02	4.02	4.02	4.02	2	0.14	0.02	0.14	0.00	0.00	22.3
18	396	6108	-1118	2	0	-158	1006	4.02	4.02	4.02	4.02	3	0.18	0.03	0.20	0.00	0.00	22.3
19	396	7093	-1069	83	0	-296	1031	4.02	4.02	4.02	4.02	3	0.19	0.03	0.19	0.00	0.00	22.3
20	396	6747	-1090	-83	0	-450	1016	4.02	4.02	4.02	4.02	3	0.18	0.03	0.19	0.00	0.00	22.3
37	396	5471	-1122	-32	0	-72	1013	4.02	4.02	4.02	4.02	3	0.17	0.03	0.20	0.00	0.00	22.3
38	396	7113	-1041	103	0	-302	1056	4.02	4.02	4.02	4.02	3	0.19	0.03	0.19	0.00	0.00	22.3
39	396	6536	-1075	-174	0	-558	1030	4.02	4.02	4.02	4.02	3	0.18	0.03	0.19	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	452	5629	-1514	19	0	-111	-962	4.02	4.02	4.02	4.02	3	0.17	0.04	0.27	0.00	0.00	22.3
2	452	4224	-1180	10	0	-70	-774	4.02	4.02	4.02	4.02	2	0.13	0.03	0.21	0.00	0.00	22.3
3	452	4289	-1181	13	0	-92	-777	4.02	4.02	4.02	4.02	2	0.14	0.03	0.21	0.00	0.00	22.3
4	452	4371	-1148	17	0	-79	-703	4.02	4.02	4.02	4.02	2	0.12	0.03	0.20	0.00	0.00	22.3
5	452	4436	-1149	20	0	-100	-706	4.02	4.02	4.02	4.02	2	0.12	0.03	0.20	0.00	0.00	22.3
6	452	4200	-1168	9	0	-49	-744	4.02	4.02	4.02	4.02	2	0.13	0.03	0.21	0.00	0.00	22.3
7	452	4416	-1171	19	0	-119	-758	4.02	4.02	4.02	4.02	2	0.13	0.03	0.21	0.00	0.00	22.3
8	452	4244	-1158	11	0	-51	-723	4.02	4.02	4.02	4.02	2	0.13	0.03	0.21	0.00	0.00	22.3
9	452	4460	-1162	21	0	-122	-736	4.02	4.02	4.02	4.02	2	0.13	0.03	0.21	0.00	0.00	22.3
10	452	4224	-1180	10	0	-70	-774	4.02	4.02	4.02	4.02	2	0.13	0.03	0.21	0.00	0.00	22.3
11	452	4289	-1181	13	0	-92	-777	4.02	4.02	4.02	4.02	2	0.14	0.03	0.21	0.00	0.00	22.3
12	452	4371	-1148	17	0	-79	-703	4.02	4.02	4.02	4.02	2	0.12	0.03	0.20	0.00	0.00	22.3
13	452	4436	-1149	20	0	-100	-706	4.02	4.02	4.02	4.02	2	0.12	0.03	0.20	0.00	0.00	22.3
14	452	4200	-1168	9	0	-49	-744	4.02	4.02	4.02	4.02	2	0.13	0.03	0.21	0.00	0.00	22.3
15	452	4416	-1171	19	0	-119	-758	4.02	4.02	4.02	4.02	2	0.13	0.03	0.21	0.00	0.00	22.3
16	452	4244	-1158	11	0	-51	-723	4.02	4.02	4.02	4.02	2	0.13	0.03	0.21	0.00	0.00	22.3
17	452	4460	-1162	21	0	-122	-736	4.02	4.02	4.02	4.02	2	0.13	0.03	0.21	0.00	0.00	22.3
18	452	6108	-1576	2	0	-159	-1120	4.02	4.02	4.02	4.02	3	0.20	0.05	0.28	0.00	0.00	22.3
19	452	7093	-1527	83	0	-343	-1018	4.02	4.02	4.02	4.02	3	0.18	0.04	0.27	0.00	0.00	22.3
20	452	6747	-1548	-83	0	-403	-1065	4.02	4.02	4.02	4.02	3	0.19	0.04	0.28	0.00	0.00	22.3
37	452	5471	-1580	-32	0	-54	-1119	4.02	4.02	4.02	4.02	3	0.19	0.05	0.28	0.00	0.00	22.3
38	452	7113	-1499	103	0	-360	-948	4.02	4.02	4.02	4.02	3	0.17	0.04	0.27	0.00	0.00	22.3
39	452	6536	-1533	-174	0	-460	-1028	4.02	4.02	4.02	4.02	3	0.18	0.04	0.27	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	509	5629	-1965	19	0	-122	-2174	4.02	4.02	4.02	4.02	3	0.37	0.06	0.35	0.00	0.00	22.3
2	509	4224	-1527	10	0	-76	-1715	4.02	4.02	4.02	4.02	2	0.30	0.04	0.27	0.00	0.00	22.3
3	509	4289	-1528	13	0	-99	-1719	4.02	4.02	4.02	4.02	2	0.30	0.04	0.27	0.00	0.00	22.3
4	509	4371	-1495	17	0	-88	-1626	4.02	4.02	4.02	4.02	2	0.28	0.04	0.27	0.00	0.00	22.3
5	509	4436	-1496	20	0	-111	-1629	4.02	4.02	4.02	4.02	2	0.29	0.04	0.27	0.00	0.00	22.3
6	509	4200	-1515	9	0	-54	-1678	4.02	4.02	4.02	4.02	2	0.29	0.04	0.27	0.00	0.00	22.3
7	509	4416	-1518	19	0	-130	-1693	4.02	4.02	4.02	4.02	2	0.30	0.04	0.27	0.00	0.00	22.3
8	509	4244	-1505	11	0	-57	-1651	4.02	4.02	4.02	4.02	2	0.29	0.04	0.27	0.00	0.00	22.3
9	509	4460	-1509	21	0	-134	-1666	4.02	4.02	4.02	4.02	2	0.29	0.04	0.27	0.00	0.00	22.3
10	509	4224	-1527	10	0	-76	-1715	4.02	4.02	4.02	4.02	2	0.30	0.04	0.27	0.00	0.00	22.3

11	509	4289	-1528	13	0	-99	-1719	4.02	4.02	4.02	4.02	2	0.30	0.04	0.27	0.00	0.00	22.3
12	509	4371	-1495	17	0	-88	-1626	4.02	4.02	4.02	4.02	2	0.28	0.04	0.27	0.00	0.00	22.3
13	509	4436	-1496	20	0	-111	-1629	4.02	4.02	4.02	4.02	2	0.29	0.04	0.27	0.00	0.00	22.3
14	509	4200	-1515	9	0	-54	-1678	4.02	4.02	4.02	4.02	2	0.29	0.04	0.27	0.00	0.00	22.3
15	509	4416	-1518	19	0	-130	-1693	4.02	4.02	4.02	4.02	2	0.30	0.04	0.27	0.00	0.00	22.3
16	509	4244	-1505	11	0	-57	-1651	4.02	4.02	4.02	4.02	2	0.29	0.04	0.27	0.00	0.00	22.3
17	509	4460	-1509	21	0	-134	-1666	4.02	4.02	4.02	4.02	2	0.29	0.04	0.27	0.00	0.00	22.3
18	509	6108	-2027	2	0	-160	-2365	4.02	4.02	4.02	4.02	3	0.41	0.06	0.36	0.00	0.00	22.3
19	509	7093	-1978	83	0	-390	-2236	4.02	4.02	4.02	4.02	3	0.40	0.06	0.35	0.00	0.00	22.3
20	509	6747	-1999	-83	0	-355	-2295	4.02	4.02	4.02	4.02	3	0.41	0.06	0.36	0.00	0.00	22.3
37	509	5471	-2031	-32	0	-35	-2367	4.02	4.02	4.02	4.02	3	0.40	0.06	0.36	0.00	0.00	22.3
38	509	7113	-1950	103	0	-419	-2151	4.02	4.02	4.02	4.02	3	0.39	0.06	0.35	0.00	0.00	22.3
39	509	6536	-1984	-174	0	-362	-2250	4.02	4.02	4.02	4.02	3	0.40	0.06	0.35	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	565	5629	-2408	19	0	-133	-2415	4.02	4.02	4.02	4.02	3	0.41	0.07	0.43	0.00	0.00	22.3
2	565	4224	-1868	10	0	-82	-1901	4.02	4.02	4.02	4.02	2	0.33	0.05	0.33	0.00	0.00	22.3
3	565	4289	-1869	13	0	-106	-1905	4.02	4.02	4.02	4.02	2	0.33	0.05	0.33	0.00	0.00	22.3
4	565	4371	-1836	17	0	-98	-1810	4.02	4.02	4.02	4.02	2	0.32	0.05	0.33	0.00	0.00	22.3
5	565	4436	-1837	20	0	-122	-1814	4.02	4.02	4.02	4.02	2	0.32	0.05	0.33	0.00	0.00	22.3
6	565	4200	-1856	9	0	-59	-1863	4.02	4.02	4.02	4.02	2	0.32	0.05	0.33	0.00	0.00	22.3
7	565	4416	-1859	19	0	-141	-1879	4.02	4.02	4.02	4.02	2	0.33	0.05	0.33	0.00	0.00	22.3
8	565	4244	-1846	11	0	-64	-1836	4.02	4.02	4.02	4.02	2	0.32	0.05	0.33	0.00	0.00	22.3
9	565	4460	-1850	21	0	-145	-1851	4.02	4.02	4.02	4.02	2	0.32	0.05	0.33	0.00	0.00	22.3
10	565	4224	-1868	10	0	-82	-1901	4.02	4.02	4.02	4.02	2	0.33	0.05	0.33	0.00	0.00	22.3
11	565	4289	-1869	13	0	-106	-1905	4.02	4.02	4.02	4.02	2	0.33	0.05	0.33	0.00	0.00	22.3
12	565	4371	-1836	17	0	-98	-1810	4.02	4.02	4.02	4.02	2	0.32	0.05	0.33	0.00	0.00	22.3
13	565	4436	-1837	20	0	-122	-1814	4.02	4.02	4.02	4.02	2	0.32	0.05	0.33	0.00	0.00	22.3
14	565	4200	-1856	9	0	-59	-1863	4.02	4.02	4.02	4.02	2	0.32	0.05	0.33	0.00	0.00	22.3
15	565	4416	-1859	19	0	-141	-1879	4.02	4.02	4.02	4.02	2	0.33	0.05	0.33	0.00	0.00	22.3
16	565	4244	-1846	11	0	-64	-1836	4.02	4.02	4.02	4.02	2	0.32	0.05	0.33	0.00	0.00	22.3
17	565	4460	-1850	21	0	-145	-1851	4.02	4.02	4.02	4.02	2	0.32	0.05	0.33	0.00	0.00	22.3
18	565	6108	-2470	2	0	-161	-2610	4.02	4.02	4.02	4.02	3	0.46	0.07	0.44	0.00	0.00	22.3
19	565	7093	-2421	83	0	-436	-2478	4.02	4.02	4.02	4.02	3	0.45	0.07	0.43	0.00	0.00	22.3
20	565	6747	-2442	-83	0	-308	-2538	4.02	4.02	4.02	4.02	3	0.45	0.07	0.43	0.00	0.00	22.3
37	565	5471	-2474	-32	0	-17	-2612	4.02	4.02	4.02	4.02	3	0.45	0.07	0.44	0.00	0.00	22.3
38	565	7113	-2393	103	0	-477	-2391	4.02	4.02	4.02	4.02	3	0.43	0.07	0.43	0.00	0.00	22.3
39	565	6536	-2427	-174	0	-263	-2492	4.02	4.02	4.02	4.02	3	0.44	0.07	0.43	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

Nome travata: **Trave_401_IP1** Descrizione: **Trave_4 7-12-17-22-32**
ASTA NUM. 4 NI 39 NF 26 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y Permanente qy tot.
qy medio: 375.00 160.00 535.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	6603	2687	-266	0	-362	-2903	4.02	4.02	4.02	4.02	3	0.52	0.08	0.48	0.00	0.00	22.3
2	0	4936	2078	-227	0	-292	-2246	4.02	4.02	4.02	4.02	2	0.40	0.06	0.37	0.00	0.00	22.3
3	0	4995	2084	-226	0	-328	-2257	4.02	4.02	4.02	4.02	2	0.40	0.06	0.37	0.00	0.00	22.3
4	0	5163	2049	-184	0	-229	-2208	4.02	4.02	4.02	4.02	2	0.40	0.06	0.36	0.00	0.00	22.3
5	0	5223	2056	-183	0	-265	-2219	4.02	4.02	4.02	4.02	2	0.40	0.06	0.37	0.00	0.00	22.3
6	0	4946	2060	-212	0	-228	-2220	4.02	4.02	4.02	4.02	2	0.40	0.06	0.37	0.00	0.00	22.3
7	0	5144	2081	-211	0	-348	-2257	4.02	4.02	4.02	4.02	2	0.41	0.06	0.37	0.00	0.00	22.3
8	0	5014	2052	-199	0	-209	-2208	4.02	4.02	4.02	4.02	2	0.40	0.06	0.37	0.00	0.00	22.3
9	0	5213	2073	-198	0	-329	-2245	4.02	4.02	4.02	4.02	2	0.40	0.06	0.37	0.00	0.00	22.3
10	0	4936	2078	-227	0	-292	-2246	4.02	4.02	4.02	4.02	2	0.40	0.06	0.37	0.00	0.00	22.3
11	0	4995	2084	-226	0	-328	-2257	4.02	4.02	4.02	4.02	2	0.40	0.06	0.37	0.00	0.00	22.3
12	0	5163	2049	-184	0	-229	-2208	4.02	4.02	4.02	4.02	2	0.40	0.06	0.36	0.00	0.00	22.3
13	0	5223	2056	-183	0	-265	-2219	4.02	4.02	4.02	4.02	2	0.40	0.06	0.37	0.00	0.00	22.3
14	0	4946	2060	-212	0	-228	-2220	4.02	4.02	4.02	4.02	2	0.40	0.06	0.37	0.00	0.00	22.3
15	0	5144	2081	-211	0	-348	-2257	4.02	4.02	4.02	4.02	2	0.41	0.06	0.37	0.00	0.00	22.3
16	0	5014	2052	-199	0	-209	-2208	4.02	4.02	4.02	4.02	2	0.40	0.06	0.37	0.00	0.00	22.3
17	0	5213	2073	-198	0	-329	-2245	4.02	4.02	4.02	4.02	2	0.40	0.06	0.37	0.00	0.00	22.3
18	0	6562	2856	-603	0	-804	-3207	4.02	4.02	4.02	4.02	3	0.57	0.08	0.51	0.00	0.00	22.3
19	0	8282	2696	-420	0	-564	-2849	4.02	4.02	4.02	4.02	3	0.54	0.08	0.48	0.00	0.00	22.3
20	0	7584	2808	-676	0	-1017	-3099	4.02	4.02	4.02	4.02	3	0.57	0.08	0.50	0.00	0.00	22.3
37	0	5739	2882	-583	0	-776	-3288	4.02	4.02	4.02	4.02	3	0.57	0.08	0.51	0.00	0.00	22.3
38	0	8606	2614	-278	0	-376	-2691	4.02	4.02	4.02	4.02	3	0.52	0.08	0.47	0.00	0.00	22.3
39	0	7441	2802	-706	0	-1131	-3108	4.02	4.02	4.02	4.02	3	0.57	0.08	0.50	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	56	6603	2252	-266	0	-212	-2648	4.02	4.02	4.02	4.02	3	0.47	0.07	0.40	0.00	0.00	22.3
2	56	4936	1743	-227	0	-164	-2050	4.02	4.02	4.02	4.02	2	0.37	0.05	0.31	0.00	0.00	22.3
3	56	4995	1749	-226	0	-200	-2060	4.02	4.02	4.02	4.02	2	0.37	0.05	0.31	0.00	0.00	22.3
4	56	5163	1714	-184	0	-125	-2013	4.02	4.02	4.02	4.02	2	0.36	0.05	0.31	0.00	0.00	22.3
5	56	5223	1721	-183	0	-161	-2024	4.02	4.02	4.02	4.02	2	0.36	0.05	0.31	0.00	0.00	22.3
6	56	4946	1725	-212	0	-108	-2024	4.02	4.02	4.02	4.02	2	0.36	0.05	0.31	0.00	0.00	22.3
7	56	5144	1746	-211	0	-229	-2060	4.02	4.02	4.02	4.02	2	0.37	0.05	0.31	0.00	0.00	22.3
8	56	5014	1717	-199	0	-97	-2013	4.02	4.02	4.02	4.02	2	0.36	0.05	0.31	0.00	0.00	22.3
9	56	5213	1738	-198	0	-217	-2049	4.02	4.02	4.02	4.02	2	0.37	0.05	0.31	0.00	0.00	22.3
10	56	4936	1743	-227	0	-164	-2050	4.02	4.02	4.02	4.02	2	0.37	0.05	0.31	0.00	0.00	22.3
11	56	4995	1749	-226	0	-200	-2060	4.02	4.02	4.02	4.02	2	0.37	0.05	0.31	0.00	0.00	22.3
12	56	5163	1714	-184	0	-125	-2013	4.02	4.02	4.02	4.02	2	0.36	0.05	0.31	0.00	0.00	22.3
13	56	5223	1721	-183	0	-161	-2024	4.02	4.02	4.02	4.02	2	0.36	0.05	0.31	0.00	0.00	22.3
14	56	4946	1725	-212	0	-108	-2024	4.02	4.02	4.02	4.02	2	0.36	0.05	0.31	0.00	0.00	22.3
15	56	5144	1746	-211	0	-229	-2060	4.02	4.02	4.02	4.02	2	0.37	0.05	0.31	0.00	0.00	22.3
16	56	5014	1717	-199	0	-97	-2013	4.02	4.02	4.02	4.02	2	0.36	0.05	0.31	0.00	0.00	22.3
17	56	5213	1738	-198	0	-217	-2049	4.02	4.02	4.02	4.02	2	0.37	0.05	0.31	0.00	0.00	22.3
18	56	6562	2421	-603	0	-464	-2942	4.02	4.02	4.02	4.02	3	0.52	0.07	0.43	0.00	0.00	22.3
19	56	8282	2261	-420	0	-327	-2594	4.02	4.02	4.02	4.02	3	0.49	0.07	0.40	0.00	0.00	22.3
20	56	7584	2373	-676	0	-635	-2837	4.02	4.02	4.02	4.02	3	0.52	0.07	0.42	0.00	0.00	22.3
37	56	5739	2447	-583	0	-447	-3022	4.02	4.02	4.02	4.02	3	0.52	0.07	0.44	0.00	0.00	22.3
38	56	8606	2179	-278	0	-219	-2440	4.02	4.02	4.02	4.02	3	0.47	0.06	0.39	0.00	0.00	22.3
39	56	7441	2367	-706	0	-732	-2847	4.02	4.02	4.02	4.02	3	0.52	0.07	0.42	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	113	6603	1826	-266	0	-61	-1281	4.02	4.02	4.02	4.02	3	0.23	0.05	0.33	0.00	0.00	22.3
2	113	4936	1416	-227	0	-36	-992	4.02	4.02	4.02	4.02	2	0.18	0.04	0.25	0.00	0.00	22.3

3	113	4995	1422	-226	0	-73	-999	4.02	4.02	4.02	4.02	2	0.18	0.04	0.25	0.00	0.00	22.3
4	113	5163	1387	-184	0	-21	-971	4.02	4.02	4.02	4.02	2	0.17	0.04	0.25	0.00	0.00	22.3
5	113	5223	1394	-183	0	-58	-978	4.02	4.02	4.02	4.02	2	0.18	0.04	0.25	0.00	0.00	22.3
6	113	4946	1398	-212	0	11	-976	4.02	4.02	4.02	4.02	2	0.17	0.04	0.25	0.00	0.00	22.3
7	113	5144	1419	-211	0	-110	-1000	4.02	4.02	4.02	4.02	2	0.18	0.04	0.25	0.00	0.00	22.3
8	113	5014	1390	-199	0	16	-970	4.02	4.02	4.02	4.02	2	0.17	0.04	0.25	0.00	0.00	22.3
9	113	5213	1411	-198	0	-105	-994	4.02	4.02	4.02	4.02	2	0.18	0.04	0.25	0.00	0.00	22.3
10	113	4936	1416	-227	0	-36	-992	4.02	4.02	4.02	4.02	2	0.18	0.04	0.25	0.00	0.00	22.3
11	113	4995	1422	-226	0	-73	-999	4.02	4.02	4.02	4.02	2	0.18	0.04	0.25	0.00	0.00	22.3
12	113	5163	1387	-184	0	-21	-971	4.02	4.02	4.02	4.02	2	0.17	0.04	0.25	0.00	0.00	22.3
13	113	5223	1394	-183	0	-58	-978	4.02	4.02	4.02	4.02	2	0.18	0.04	0.25	0.00	0.00	22.3
14	113	4946	1398	-212	0	11	-976	4.02	4.02	4.02	4.02	2	0.17	0.04	0.25	0.00	0.00	22.3
15	113	5144	1419	-211	0	-110	-1000	4.02	4.02	4.02	4.02	2	0.18	0.04	0.25	0.00	0.00	22.3
16	113	5014	1390	-199	0	16	-970	4.02	4.02	4.02	4.02	2	0.17	0.04	0.25	0.00	0.00	22.3
17	113	5213	1411	-198	0	-105	-994	4.02	4.02	4.02	4.02	2	0.18	0.04	0.25	0.00	0.00	22.3
18	113	6562	1995	-603	0	-123	-1480	4.02	4.02	4.02	4.02	3	0.26	0.06	0.36	0.00	0.00	22.3
19	113	8282	1835	-420	0	-90	-1222	4.02	4.02	4.02	4.02	3	0.23	0.05	0.33	0.00	0.00	22.3
20	113	7584	1947	-676	0	-253	-1402	4.02	4.02	4.02	4.02	3	0.26	0.06	0.35	0.00	0.00	22.3
37	113	5739	2021	-583	0	-118	-1545	4.02	4.02	4.02	4.02	3	0.27	0.06	0.36	0.00	0.00	22.3
38	113	8606	1753	-278	0	-62	-1115	4.02	4.02	4.02	4.02	3	0.21	0.05	0.31	0.00	0.00	22.3
39	113	7441	1941	-706	0	-333	-1415	4.02	4.02	4.02	4.02	3	0.26	0.06	0.35	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	169	6603	1409	-266	0	90	1270	4.02	4.02	4.02	4.02	3	0.23	0.04	0.25	0.00	0.00	22.3
2	169	4936	1095	-227	0	92	988	4.02	4.02	4.02	4.02	2	0.18	0.03	0.20	0.00	0.00	22.3
3	169	4995	1101	-226	0	55	990	4.02	4.02	4.02	4.02	2	0.18	0.03	0.20	0.00	0.00	22.3
4	169	5163	1066	-184	0	82	964	4.02	4.02	4.02	4.02	2	0.17	0.03	0.19	0.00	0.00	22.3
5	169	5223	1073	-183	0	46	967	4.02	4.02	4.02	4.02	2	0.17	0.03	0.19	0.00	0.00	22.3
6	169	4946	1077	-212	0	131	976	4.02	4.02	4.02	4.02	2	0.17	0.03	0.19	0.00	0.00	22.3
7	169	5144	1098	-211	0	9	985	4.02	4.02	4.02	4.02	2	0.18	0.03	0.20	0.00	0.00	22.3
8	169	5014	1069	-199	0	128	969	4.02	4.02	4.02	4.02	2	0.17	0.03	0.19	0.00	0.00	22.3
9	169	5213	1090	-198	0	7	978	4.02	4.02	4.02	4.02	2	0.18	0.03	0.19	0.00	0.00	22.3
10	169	4936	1095	-227	0	92	988	4.02	4.02	4.02	4.02	2	0.18	0.03	0.20	0.00	0.00	22.3
11	169	4995	1101	-226	0	55	990	4.02	4.02	4.02	4.02	2	0.18	0.03	0.20	0.00	0.00	22.3
12	169	5163	1066	-184	0	82	964	4.02	4.02	4.02	4.02	2	0.17	0.03	0.19	0.00	0.00	22.3
13	169	5223	1073	-183	0	46	967	4.02	4.02	4.02	4.02	2	0.17	0.03	0.19	0.00	0.00	22.3
14	169	4946	1077	-212	0	131	976	4.02	4.02	4.02	4.02	2	0.17	0.03	0.19	0.00	0.00	22.3
15	169	5144	1098	-211	0	9	985	4.02	4.02	4.02	4.02	2	0.18	0.03	0.20	0.00	0.00	22.3
16	169	5014	1069	-199	0	128	969	4.02	4.02	4.02	4.02	2	0.17	0.03	0.19	0.00	0.00	22.3
17	169	5213	1090	-198	0	7	978	4.02	4.02	4.02	4.02	2	0.18	0.03	0.19	0.00	0.00	22.3
18	169	6562	1578	-603	0	217	1338	4.02	4.02	4.02	4.02	3	0.24	0.05	0.28	0.00	0.00	22.3
19	169	8282	1418	-420	0	148	1343	4.02	4.02	4.02	4.02	3	0.25	0.04	0.25	0.00	0.00	22.3
20	169	7584	1531	-676	0	130	1341	4.02	4.02	4.02	4.02	3	0.25	0.04	0.27	0.00	0.00	22.3
37	169	5739	1604	-583	0	212	1314	4.02	4.02	4.02	4.02	3	0.23	0.05	0.29	0.00	0.00	22.3
38	169	8606	1337	-278	0	95	1322	4.02	4.02	4.02	4.02	3	0.25	0.04	0.24	0.00	0.00	22.3
39	169	7441	1524	-706	0	65	1318	4.02	4.02	4.02	4.02	3	0.24	0.04	0.27	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	226	6603	1002	-266	0	240	1744	4.02	4.02	4.02	4.02	3	0.31	0.03	0.18	0.00	0.00	22.3
2	226	4936	782	-227	0	220	1359	4.02	4.02	4.02	4.02	2	0.24	0.02	0.14	0.00	0.00	22.3
3	226	4995	788	-226	0	183	1365	4.02	4.02	4.02	4.02	2	0.24	0.02	0.14	0.00	0.00	22.3
4	226	5163	753	-184	0	186	1319	4.02	4.02	4.02	4.02	2	0.24	0.02	0.13	0.00	0.00	22.3
5	226	5223	760	-183	0	149	1326	4.02	4.02	4.02	4.02	2	0.24	0.02	0.14	0.00	0.00	22.3
6	226	4946	764	-212	0	251	1337	4.02	4.02	4.02	4.02	2	0.24	0.02	0.14	0.00	0.00	22.3
7	226	5144	785	-211	0	129	1358	4.02	4.02	4.02	4.02	2	0.24	0.02	0.14	0.00	0.00	22.3
8	226	5014	756	-199	0	241	1326	4.02	4.02	4.02	4.02	2	0.24	0.02	0.13	0.00	0.00	22.3
9	226	5213	777	-198	0	118	1347	4.02	4.02	4.02	4.02	2	0.24	0.02	0.14	0.00	0.00	22.3
10	226	4936	782	-227	0	220	1359	4.02	4.02	4.02	4.02	2	0.24	0.02	0.14	0.00	0.00	22.3
11	226	4995	788	-226	0	183	1365	4.02	4.02	4.02	4.02	2	0.24	0.02	0.14	0.00	0.00	22.3
12	226	5163	753	-184	0	186	1319	4.02	4.02	4.02	4.02	2	0.24	0.02	0.13	0.00	0.00	22.3
13	226	5223	760	-183	0	149	1326	4.02	4.02	4.02	4.02	2	0.24	0.02	0.14	0.00	0.00	22.3
14	226	4946	764	-212	0	251	1337	4.02	4.02	4.02	4.02	2	0.24	0.02	0.14	0.00	0.00	22.3
15	226	5144	785	-211	0	129	1358	4.02	4.02	4.02	4.02	2	0.24	0.02	0.14	0.00	0.00	22.3
16	226	5014	756	-199	0	241	1326	4.02	4.02	4.02	4.02	2	0.24	0.02	0.13	0.00	0.00	22.3
17	226	5213	777	-198	0	118	1347	4.02	4.02	4.02	4.02	2	0.24	0.02	0.14	0.00	0.00	22.3
18	226	6562	1171	-603	0	558	1909	4.02	4.02	4.02	4.02	3	0.34	0.03	0.21	0.00	0.00	22.3
19	226	8282	1011	-420	0	385	1823	4.02	4.02	4.02	4.02	3	0.35	0.03	0.18	0.00	0.00	22.3
20	226	7584	1124	-676	0	512	1884	4.02	4.02	4.02	4.02	3	0.35	0.03	0.20	0.00	0.00	22.3
37	226	5739	1197	-583	0	541	1899	4.02	4.02	4.02	4.02	3	0.33	0.03	0.21	0.00	0.00	22.3
38	226	8606	930	-278	0	253	1755	4.02	4.02	4.02	4.02	3	0.34	0.03	0.17	0.00	0.00	22.3
39	226	7441	1117	-706	0	464	1857	4.02	4.02	4.02	4.02	3	0.34	0.03	0.20	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	282	6603	604	-266	0	391	1937	4.02	4.02	4.02	4.02	3	0.34	0.02	0.11	0.00	0.00	22.3
2	282	4936	476	-227	0	348	1520	4.02	4.02	4.02	4.02	2	0.27	0.01	0.08	0.00	0.00	22.3
3	282	4995	482	-226	0	311	1533	4.02	4.02	4.02	4.02	2	0.27	0.01	0.09	0.00	0.00	22.3
4	282	5163	447	-184	0	290	1447	4.02	4.02	4.02	4.02	2	0.26	0.01	0.08	0.00	0.00	22.3
5	282	5223	454	-183	0	253	1460	4.02	4.02	4.02	4.02	2	0.26	0.01	0.08	0.00	0.00	22.3
6	282	4946	458	-212	0	371	1478	4.02	4.02	4.02	4.02	2	0.26	0.01	0.08	0.00	0.00	22.3
7	282	5144	479	-211	0	248	1524	4.02	4.02	4.02	4.02	2	0.27	0.01	0.09	0.00	0.00	22.3
8	282	5014	450	-199	0	353	1456	4.02	4.02	4.02	4.02	2	0.26	0.01	0.08	0.00	0.00	22.3
9	282	5213	471	-198	0	230	1502	4.02	4.02	4.02	4.02	2	0.27	0.01	0.08	0.00	0.00	22.3
10	282	4936	476	-227	0	348	1520	4.02	4.02	4.02	4.02	2	0.27	0.01	0.08	0.00	0.00	22.3
11	282	4995	482	-226	0	311	1533	4.02	4.02	4.02	4.02	2	0.27	0.01	0.09	0.00	0.00	22.3
12	282	5163	447	-184	0	290	1447	4.02	4.02	4.02	4.02	2	0.26	0.01	0.08	0.00	0.00	22.3
13	282	5223	454	-183	0	253	1460	4.02	4.02	4.02	4.02	2	0.26	0.01	0.08	0.00	0.00	22.3
14	282	4946	458	-212	0	371	1478	4.02	4.02	4.02	4.02	2	0.26	0.01	0.08	0.00	0.00	22.3
15	282	5144	479	-211	0	248	1524	4.02	4.02	4.02	4.02	2	0.27	0.01	0.09	0.00	0.00	22.3
16	282	5014	450	-199	0	353	1456	4.02	4.02	4.02	4.02	2	0.26	0.01	0.08	0.00	0.00	22.3
17	282	5213	471	-198	0	230	1502	4.02	4.02	4.02	4.02	2	0.27	0.01	0.08	0.00	0.00	22.3
18	282	6562	773	-603	0	898	2256	4.02	4.02	4.02	4.02	3	0.40	0.02	0.14	0.00	0.00	22.3
19	282	8282	613	-420	0	622	2025	4.02	4.02	4.02	4.02	3	0.38	0.02	0.11	0.00	0.00	22.3
20	282	7584	726	-676	0	894	2205	4.02	4.02	4.02	4.02	3	0.41	0.02	0.13	0.00	0.00	22.3
37	282	5739	799	-583	0	870	2261	4.02	4.02	4.02	4.02	3	0.39	0.02	0.14	0.00	0.00	22.3
38	282	8606	532	-278	0	410	1887	4.02	4.02	4.02	4.02	3	0.36	0.02	0.09	0.00	0.00	22.3
39	282	7441	719	-706	0	863	2174	4.02	4.02	4.02	4.02	3	0.40	0.02	0.13	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	339	6603	216	-266	0	542	1937	4.02	4.02	4.02	4.02	3	0.34	0.01	0.04	0.00	0.00	22.3
2	339	4936	177	-227	0	476	1520	4.02	4.02	4.02	4.02	2	0.27	0.01	0.04	0.00	0.00	22.3
3	339	4995	183	-226	0	439	1533	4.02	4.02	4.02	4.02	2	0.27	0.01	0.04	0.00	0.00	22.3
4	339	5163	149	-184	0	394	1447	4.02	4.02	4.02	4.02	2	0.26	0.01	0.03	0.00	0.00	22.3
5	339	5223	155	-183	0	357	1460	4.02	4.02	4.02	4.02	2	0.26	0.01	0.03	0.00	0.00	22.3
6	339	4946	160	-212	0	491	1478	4.02	4.02	4.02	4.02	2	0.26	0.01	0.03	0.00	0.00	22.3
7	339	5144	181	-211	0	367	1524	4.02	4.02	4.02	4.02	2	0.27	0.01	0.03	0.00	0.00	22.3
8	339	5014	152	-199	0	466	1456	4.02	4.02	4.02	4.02	2	0.26	0.01	0.03	0.00	0.00	22.3

9	339	5213	173	-198	0	342	1502	4.02	4.02	4.02	4.02	2	0.27	0.01	0.03	0.00	0.00	22.3
10	339	4936	177	-227	0	476	1520	4.02	4.02	4.02	4.02	2	0.27	0.01	0.04	0.00	0.00	22.3
11	339	4995	183	-226	0	439	1533	4.02	4.02	4.02	4.02	2	0.27	0.01	0.04	0.00	0.00	22.3
12	339	5163	149	-184	0	394	1447	4.02	4.02	4.02	4.02	2	0.26	0.01	0.03	0.00	0.00	22.3
13	339	5223	155	-183	0	357	1460	4.02	4.02	4.02	4.02	2	0.26	0.01	0.03	0.00	0.00	22.3
14	339	4946	160	-212	0	491	1478	4.02	4.02	4.02	4.02	2	0.26	0.01	0.03	0.00	0.00	22.3
15	339	5144	181	-211	0	367	1524	4.02	4.02	4.02	4.02	2	0.27	0.01	0.03	0.00	0.00	22.3
16	339	5014	152	-199	0	466	1456	4.02	4.02	4.02	4.02	2	0.26	0.01	0.03	0.00	0.00	22.3
17	339	5213	173	-198	0	342	1502	4.02	4.02	4.02	4.02	2	0.27	0.01	0.03	0.00	0.00	22.3
18	339	6562	385	-603	0	1238	2302	4.02	4.02	4.02	4.02	3	0.41	0.02	0.10	0.00	0.00	22.3
19	339	8282	225	-420	0	859	2025	4.02	4.02	4.02	4.02	3	0.38	0.01	0.07	0.00	0.00	22.3
20	339	7584	338	-676	0	1276	2220	4.02	4.02	4.02	4.02	3	0.41	0.02	0.11	0.00	0.00	22.3
37	339	5739	411	-583	0	1200	2323	4.02	4.02	4.02	4.02	3	0.40	0.02	0.09	0.00	0.00	22.3
38	339	8606	144	-278	0	567	1887	4.02	4.02	4.02	4.02	3	0.36	0.01	0.04	0.00	0.00	22.3
39	339	7441	331	-706	0	1262	2186	4.02	4.02	4.02	4.02	3	0.40	0.02	0.11	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	395	6603	-163	-266	0	692	1937	4.02	4.02	4.02	4.02	3	0.34	0.01	0.04	0.00	0.00	22.3
2	395	4936	-114	-227	0	604	1520	4.02	4.02	4.02	4.02	2	0.27	0.01	0.04	0.00	0.00	22.3
3	395	4995	-108	-226	0	567	1533	4.02	4.02	4.02	4.02	2	0.27	0.01	0.04	0.00	0.00	22.3
4	395	5163	-143	-184	0	498	1447	4.02	4.02	4.02	4.02	2	0.26	0.01	0.03	0.00	0.00	22.3
5	395	5223	-136	-183	0	460	1460	4.02	4.02	4.02	4.02	2	0.26	0.01	0.03	0.00	0.00	22.3
6	395	4946	-132	-212	0	611	1478	4.02	4.02	4.02	4.02	2	0.26	0.01	0.03	0.00	0.00	22.3
7	395	5144	-111	-211	0	486	1524	4.02	4.02	4.02	4.02	2	0.27	0.01	0.03	0.00	0.00	22.3
8	395	5014	-140	-199	0	578	1456	4.02	4.02	4.02	4.02	2	0.26	0.01	0.03	0.00	0.00	22.3
9	395	5213	-119	-198	0	454	1502	4.02	4.02	4.02	4.02	2	0.27	0.01	0.03	0.00	0.00	22.3
10	395	4936	-114	-227	0	604	1520	4.02	4.02	4.02	4.02	2	0.27	0.01	0.04	0.00	0.00	22.3
11	395	4995	-108	-226	0	567	1533	4.02	4.02	4.02	4.02	2	0.27	0.01	0.04	0.00	0.00	22.3
12	395	5163	-143	-184	0	498	1447	4.02	4.02	4.02	4.02	2	0.26	0.01	0.03	0.00	0.00	22.3
13	395	5223	-136	-183	0	460	1460	4.02	4.02	4.02	4.02	2	0.26	0.01	0.03	0.00	0.00	22.3
14	395	4946	-132	-212	0	611	1478	4.02	4.02	4.02	4.02	2	0.26	0.01	0.03	0.00	0.00	22.3
15	395	5144	-111	-211	0	486	1524	4.02	4.02	4.02	4.02	2	0.27	0.01	0.03	0.00	0.00	22.3
16	395	5014	-140	-199	0	578	1456	4.02	4.02	4.02	4.02	2	0.26	0.01	0.03	0.00	0.00	22.3
17	395	5213	-119	-198	0	454	1502	4.02	4.02	4.02	4.02	2	0.27	0.01	0.03	0.00	0.00	22.3
18	395	6562	6	-603	0	1579	2302	4.02	4.02	4.02	4.02	3	0.47	0.02	0.10	0.00	0.00	22.3
19	395	8282	-154	-420	0	1096	2025	4.02	4.02	4.02	4.02	3	0.38	0.01	0.07	0.00	0.00	22.3
20	395	7584	-41	-676	0	1658	2220	4.02	4.02	4.02	4.02	3	0.51	0.02	0.11	0.00	0.00	22.3
37	395	5739	32	-583	0	1529	2323	4.02	4.02	4.02	4.02	3	0.44	0.02	0.09	0.00	0.00	22.3
38	395	8606	-235	-278	0	724	1887	4.02	4.02	4.02	4.02	3	0.36	0.01	0.04	0.00	0.00	22.3
39	395	7441	-48	-706	0	1661	2186	4.02	4.02	4.02	4.02	3	0.51	0.02	0.11	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	452	6603	-532	-266	0	843	1937	4.02	4.02	4.02	4.02	3	0.34	0.02	0.09	0.00	0.00	22.3
2	452	4936	-398	-227	0	732	1520	4.02	4.02	4.02	4.02	2	0.27	0.01	0.07	0.00	0.00	22.3
3	452	4995	-392	-226	0	695	1533	4.02	4.02	4.02	4.02	2	0.27	0.01	0.07	0.00	0.00	22.3
4	452	5163	-427	-184	0	601	1447	4.02	4.02	4.02	4.02	2	0.26	0.01	0.08	0.00	0.00	22.3
5	452	5223	-420	-183	0	564	1460	4.02	4.02	4.02	4.02	2	0.26	0.01	0.07	0.00	0.00	22.3
6	452	4946	-416	-212	0	730	1478	4.02	4.02	4.02	4.02	2	0.26	0.01	0.07	0.00	0.00	22.3
7	452	5144	-395	-211	0	605	1524	4.02	4.02	4.02	4.02	2	0.27	0.01	0.07	0.00	0.00	22.3
8	452	5014	-424	-199	0	691	1456	4.02	4.02	4.02	4.02	2	0.26	0.01	0.08	0.00	0.00	22.3
9	452	5213	-403	-198	0	566	1502	4.02	4.02	4.02	4.02	2	0.27	0.01	0.07	0.00	0.00	22.3
10	452	4936	-398	-227	0	732	1520	4.02	4.02	4.02	4.02	2	0.27	0.01	0.07	0.00	0.00	22.3
11	452	4995	-392	-226	0	695	1533	4.02	4.02	4.02	4.02	2	0.27	0.01	0.07	0.00	0.00	22.3
12	452	5163	-427	-184	0	601	1447	4.02	4.02	4.02	4.02	2	0.26	0.01	0.08	0.00	0.00	22.3
13	452	5223	-420	-183	0	564	1460	4.02	4.02	4.02	4.02	2	0.26	0.01	0.07	0.00	0.00	22.3
14	452	4946	-416	-212	0	730	1478	4.02	4.02	4.02	4.02	2	0.26	0.01	0.07	0.00	0.00	22.3
15	452	5144	-395	-211	0	605	1524	4.02	4.02	4.02	4.02	2	0.27	0.01	0.07	0.00	0.00	22.3
16	452	5014	-424	-199	0	691	1456	4.02	4.02	4.02	4.02	2	0.26	0.01	0.08	0.00	0.00	22.3
17	452	5213	-403	-198	0	566	1502	4.02	4.02	4.02	4.02	2	0.27	0.01	0.07	0.00	0.00	22.3
18	452	6562	-363	-603	0	1919	2302	4.02	4.02	4.02	4.02	3	0.57	0.02	0.10	0.00	0.00	22.3
19	452	8282	-523	-420	0	1334	2025	4.02	4.02	4.02	4.02	3	0.42	0.02	0.09	0.00	0.00	22.3
20	452	7584	-410	-676	0	2041	2220	4.02	4.02	4.02	4.02	3	0.63	0.02	0.11	0.00	0.00	22.3
37	452	5739	-337	-583	0	1858	2323	4.02	4.02	4.02	4.02	3	0.54	0.02	0.09	0.00	0.00	22.3
38	452	8606	-604	-278	0	882	1887	4.02	4.02	4.02	4.02	3	0.36	0.02	0.11	0.00	0.00	22.3
39	452	7441	-417	-706	0	2059	2186	4.02	4.02	4.02	4.02	3	0.63	0.02	0.11	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	508	6603	-892	-266	0	993	1789	4.02	4.02	4.02	4.02	3	0.32	0.03	0.16	0.00	0.00	22.3
2	508	4936	-675	-227	0	861	1412	4.02	4.02	4.02	4.02	2	0.28	0.02	0.12	0.00	0.00	22.3
3	508	4995	-669	-226	0	823	1430	4.02	4.02	4.02	4.02	2	0.27	0.02	0.12	0.00	0.00	22.3
4	508	5163	-704	-184	0	705	1322	4.02	4.02	4.02	4.02	2	0.24	0.02	0.13	0.00	0.00	22.3
5	508	5223	-697	-183	0	667	1340	4.02	4.02	4.02	4.02	2	0.24	0.02	0.12	0.00	0.00	22.3
6	508	4946	-693	-212	0	850	1360	4.02	4.02	4.02	4.02	2	0.28	0.02	0.12	0.00	0.00	22.3
7	508	5144	-672	-211	0	724	1419	4.02	4.02	4.02	4.02	2	0.26	0.02	0.12	0.00	0.00	22.3
8	508	5014	-701	-199	0	803	1333	4.02	4.02	4.02	4.02	2	0.26	0.02	0.12	0.00	0.00	22.3
9	508	5213	-680	-198	0	678	1392	4.02	4.02	4.02	4.02	2	0.25	0.02	0.12	0.00	0.00	22.3
10	508	4936	-675	-227	0	861	1412	4.02	4.02	4.02	4.02	2	0.28	0.02	0.12	0.00	0.00	22.3
11	508	4995	-669	-226	0	823	1430	4.02	4.02	4.02	4.02	2	0.27	0.02	0.12	0.00	0.00	22.3
12	508	5163	-704	-184	0	705	1322	4.02	4.02	4.02	4.02	2	0.24	0.02	0.13	0.00	0.00	22.3
13	508	5223	-697	-183	0	667	1340	4.02	4.02	4.02	4.02	2	0.24	0.02	0.12	0.00	0.00	22.3
14	508	4946	-693	-212	0	850	1360	4.02	4.02	4.02	4.02	2	0.28	0.02	0.12	0.00	0.00	22.3
15	508	5144	-672	-211	0	724	1419	4.02	4.02	4.02	4.02	2	0.26	0.02	0.12	0.00	0.00	22.3
16	508	5014	-701	-199	0	803	1333	4.02	4.02	4.02	4.02	2	0.26	0.02	0.12	0.00	0.00	22.3
17	508	5213	-680	-198	0	678	1392	4.02	4.02	4.02	4.02	2	0.25	0.02	0.12	0.00	0.00	22.3
18	508	6562	-723	-603	0	2260	2260	4.02	4.02	4.02	4.02	3	0.67	0.02	0.13	0.00	0.00	22.3
19	508	8282	-883	-420	0	1571	1883	4.02	4.02	4.02	4.02	3	0.49	0.03	0.16	0.00	0.00	22.3
20	508	7584	-770	-676	0	2423	2148	4.02	4.02	4.02	4.02	3	0.74	0.02	0.14	0.00	0.00	22.3
37	508	5739	-697	-583	0	2188	2296	4.02	4.02	4.02	4.02	3	0.63	0.02	0.12	0.00	0.00	22.3
38	508	8606	-964	-278	0	1039	1668	4.02	4.02	4.02	4.02	3	0.33	0.03	0.17	0.00	0.00	22.3
39	508	7441	-777	-706	0	2458	2110	4.02	4.02	4.02	4.02	3	0.75	0.02	0.14	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	565	6603	-1243	-266	0	1144	1363	4.02	4.02	4.02	4.02	3	0.34	0.04	0.22	0.00	0.00	22.3
2	565	4936	-945	-227	0	989	1091	4.02	4.02	4.02	4.02	2	0.32	0.03	0.17	0.00	0.00	22.3
3	565	4995	-939	-226	0	951	1112	4.02	4.02	4.02	4.02	2	0.31	0.03	0.17	0.00	0.00	22.3
4	565	5163	-973	-184	0	809	985	4.02	4.02	4.02	4.02	2	0.27	0.03	0.17	0.00	0.00	22.3
5	565	5223	-967	-183	0	771	1006	4.02	4.02	4.02	4.02	2	0.26	0.03	0.17	0.00	0.00	22.3
6	565	4946	-962	-212	0	970	1029	4.02	4.02	4.02	4.02	2	0.32	0.03	0.17	0.00	0.00	22.3
7	565	5144	-941	-211	0	843	1100	4.02	4.02	4.02	4.02	2	0.28	0.03	0.17	0.00	0.00	22.3
8	565	5014	-971	-199	0	916	997	4.02	4.02	4.02	4.02	2	0.30	0.03	0.17	0.00	0.00	22.3
9	565	5213	-950	-198	0	789	1068	4.02	4.02	4.02	4.02	2	0.26	0.03	0.17	0.00	0.00	22.3
10	565	4936	-945	-227	0	989	1091	4.02	4.02	4.02	4.02	2	0.32	0.03	0.17	0.00	0.00	22.3
11	565	4995	-939	-226	0	951	1112	4.02	4.02	4.02	4.02	2	0.31	0.03	0.17	0.00	0.00	22.3
12	565	5163	-973	-184	0	809	985	4.02	4.02	4.02	4.02	2	0.27	0.03	0.17	0.00	0.00	22.3
13	565	5223	-967	-183	0	771	1006	4.02	4.02	4.02	4.02	2	0.26	0.03	0.17	0.00	0.00	22.3
14	565	4946	-962	-212	0	970	1029	4.02	4.02	4.02	4.02	2	0.32	0.03	0.17	0.00	0.00	22.3

15	565	5144	-941	-211	0	843	1100	4.02	4.02	4.02	4.02	2	0.28	0.03	0.17	0.00	0.00	22.3
16	565	5014	-971	-199	0	916	997	4.02	4.02	4.02	4.02	2	0.30	0.03	0.17	0.00	0.00	22.3
17	565	5213	-950	-198	0	789	1068	4.02	4.02	4.02	4.02	2	0.26	0.03	0.17	0.00	0.00	22.3
18	565	6562	-1074	-603	0	2600	1930	4.02	4.02	4.02	4.02	3	0.77	0.03	0.19	0.00	0.00	22.3
19	565	8282	-1234	-420	0	1808	1462	4.02	4.02	4.02	4.02	3	0.57	0.04	0.22	0.00	0.00	22.3
20	565	7584	-1121	-676	0	2805	1791	4.02	4.02	4.02	4.02	3	0.86	0.03	0.20	0.00	0.00	22.3
37	565	5739	-1048	-583	0	2517	1981	4.02	4.02	4.02	4.02	3	0.73	0.03	0.19	0.00	0.00	22.3
38	565	8606	-1315	-278	0	1196	1201	4.02	4.02	4.02	4.02	3	0.38	0.04	0.23	0.00	0.00	22.3
39	565	7441	-1128	-706	0	2857	1749	4.02	4.02	4.02	4.02	3	0.87	0.03	0.20	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

Nome travata: **Trave_402_IP1** Descrizione: **Trave_4 1-10-15-20-25**
ASTA NUM. 5 NI 291 NF 295 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y Permanente qy tot.
qy medio: 375.00 160.00 535.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	3017	2253	-40	0	-427	-3240	4.02	4.02	4.02	4.02	3	0.51	0.07	0.40	0.00	0.00	22.3
2	0	1766	1376	-21	0	-283	-1329	4.02	4.02	4.02	4.02	2	0.21	0.04	0.25	0.00	0.00	22.3
3	0	1709	1373	-16	0	-276	-1314	4.02	4.02	4.02	4.02	2	0.21	0.04	0.24	0.00	0.00	22.3
4	0	2932	2093	-45	0	-381	-3671	4.02	4.02	4.02	4.02	2	0.61	0.06	0.37	0.00	0.00	22.3
5	0	2876	2090	-40	0	-374	-3656	4.02	4.02	4.02	4.02	2	0.61	0.06	0.37	0.00	0.00	22.3
6	0	2240	1631	-35	0	-326	-2166	4.02	4.02	4.02	4.02	2	0.35	0.05	0.29	0.00	0.00	22.3
7	0	2052	1621	-19	0	-301	-2116	4.02	4.02	4.02	4.02	2	0.34	0.05	0.29	0.00	0.00	22.3
8	0	2589	1846	-42	0	-356	-2868	4.02	4.02	4.02	4.02	2	0.47	0.05	0.33	0.00	0.00	22.3
9	0	2402	1836	-26	0	-331	-2819	4.02	4.02	4.02	4.02	2	0.46	0.05	0.33	0.00	0.00	22.3
10	0	1766	1376	-21	0	-283	-1329	4.02	4.02	4.02	4.02	2	0.21	0.04	0.25	0.00	0.00	22.3
11	0	1709	1373	-16	0	-276	-1314	4.02	4.02	4.02	4.02	2	0.21	0.04	0.24	0.00	0.00	22.3
12	0	2932	2093	-45	0	-381	-3671	4.02	4.02	4.02	4.02	2	0.61	0.06	0.37	0.00	0.00	22.3
13	0	2876	2090	-40	0	-374	-3656	4.02	4.02	4.02	4.02	2	0.61	0.06	0.37	0.00	0.00	22.3
14	0	2240	1631	-35	0	-326	-2166	4.02	4.02	4.02	4.02	2	0.35	0.05	0.29	0.00	0.00	22.3
15	0	2052	1621	-19	0	-301	-2116	4.02	4.02	4.02	4.02	2	0.34	0.05	0.29	0.00	0.00	22.3
16	0	2589	1846	-42	0	-356	-2868	4.02	4.02	4.02	4.02	2	0.47	0.05	0.33	0.00	0.00	22.3
17	0	2402	1836	-26	0	-331	-2819	4.02	4.02	4.02	4.02	2	0.46	0.05	0.33	0.00	0.00	22.3
18	0	3981	1836	80	0	-351	-2083	4.02	4.02	4.02	4.02	3	0.34	0.05	0.33	0.00	0.00	22.3
19	0	6933	3481	-118	0	-988	-7368	4.02	4.02	4.02	6.03	3	0.84	0.10	0.54	0.00	0.00	22.3
20	0	5011	2589	-30	0	-688	-4468	4.02	4.02	4.02	4.02	3	0.75	0.08	0.46	0.00	0.00	22.3
37	0	2149	1147	140	0	-58	777	4.02	4.02	4.02	4.02	3	0.12	0.03	0.20	0.00	0.00	22.3
38	0	7070	3888	-189	0	-1119	-8612	4.02	4.02	4.02	6.03	3	0.98	0.11	0.60	0.00	0.00	22.3
39	0	3866	2401	-44	0	-620	-3778	4.02	4.02	4.02	4.02	3	0.61	0.07	0.43	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= 2.01 (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	56	3017	1902	-40	0	-405	-3029	4.02	4.02	4.02	4.02	3	0.48	0.06	0.34	0.00	0.00	22.3
2	56	1766	1106	-21	0	-271	-1187	4.02	4.02	4.02	4.02	2	0.19	0.03	0.20	0.00	0.00	22.3
3	56	1709	1103	-16	0	-267	-1172	4.02	4.02	4.02	4.02	2	0.19	0.03	0.20	0.00	0.00	22.3
4	56	2932	1823	-45	0	-356	-3487	4.02	4.02	4.02	4.02	2	0.58	0.05	0.32	0.00	0.00	22.3
5	56	2876	1820	-40	0	-351	-3472	4.02	4.02	4.02	4.02	2	0.58	0.05	0.32	0.00	0.00	22.3
6	56	2240	1361	-35	0	-306	-2010	4.02	4.02	4.02	4.02	2	0.33	0.04	0.24	0.00	0.00	22.3
7	56	2052	1351	-19	0	-291	-1960	4.02	4.02	4.02	4.02	2	0.32	0.04	0.24	0.00	0.00	22.3
8	56	2589	1576	-42	0	-331	-2699	4.02	4.02	4.02	4.02	2	0.44	0.05	0.28	0.00	0.00	22.3
9	56	2402	1566	-26	0	-316	-2651	4.02	4.02	4.02	4.02	2	0.43	0.05	0.28	0.00	0.00	22.3
10	56	1766	1106	-21	0	-271	-1187	4.02	4.02	4.02	4.02	2	0.19	0.03	0.20	0.00	0.00	22.3
11	56	1709	1103	-16	0	-267	-1172	4.02	4.02	4.02	4.02	2	0.19	0.03	0.20	0.00	0.00	22.3
12	56	2932	1823	-45	0	-356	-3487	4.02	4.02	4.02	4.02	2	0.58	0.05	0.32	0.00	0.00	22.3
13	56	2876	1820	-40	0	-351	-3472	4.02	4.02	4.02	4.02	2	0.58	0.05	0.32	0.00	0.00	22.3
14	56	2240	1361	-35	0	-306	-2010	4.02	4.02	4.02	4.02	2	0.33	0.04	0.24	0.00	0.00	22.3
15	56	2052	1351	-19	0	-291	-1960	4.02	4.02	4.02	4.02	2	0.32	0.04	0.24	0.00	0.00	22.3
16	56	2589	1576	-42	0	-331	-2699	4.02	4.02	4.02	4.02	2	0.44	0.05	0.28	0.00	0.00	22.3
17	56	2402	1566	-26	0	-316	-2651	4.02	4.02	4.02	4.02	2	0.43	0.05	0.28	0.00	0.00	22.3
18	56	3981	1485	80	0	-396	-1896	4.02	4.02	4.02	4.02	3	0.31	0.04	0.26	0.00	0.00	22.3
19	56	6933	3130	-118	0	-921	-7085	4.02	4.02	4.02	6.03	3	0.81	0.09	0.49	0.00	0.00	22.3
20	56	5011	2238	-30	0	-671	-4237	4.02	4.02	4.02	4.02	3	0.71	0.06	0.40	0.00	0.00	22.3
37	56	2149	796	140	0	-137	1149	4.02	4.02	4.02	4.02	3	0.18	0.02	0.14	0.00	0.00	22.3
38	56	7070	3537	-189	0	-1012	-8305	4.02	4.02	4.02	6.03	3	0.95	0.10	0.55	0.00	0.00	22.3
39	56	3866	2050	-44	0	-595	-3558	4.02	4.02	4.02	4.02	3	0.58	0.06	0.37	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= 2.01 (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	113	3017	1542	-40	0	-382	-1873	4.02	4.02	4.02	4.02	3	0.29	0.04	0.27	0.00	0.00	22.3
2	113	1766	829	-21	0	-259	-500	4.02	4.02	4.02	4.02	2	0.08	0.02	0.15	0.00	0.00	22.3
3	113	1709	826	-16	0	-258	-487	4.02	4.02	4.02	4.02	2	0.08	0.02	0.15	0.00	0.00	22.3
4	113	2932	1546	-45	0	-330	-2395	4.02	4.02	4.02	4.02	2	0.40	0.04	0.28	0.00	0.00	22.3
5	113	2876	1543	-40	0	-329	-2382	4.02	4.02	4.02	4.02	2	0.40	0.04	0.27	0.00	0.00	22.3
6	113	2240	1084	-35	0	-286	-1178	4.02	4.02	4.02	4.02	2	0.19	0.03	0.19	0.00	0.00	22.3
7	113	2052	1074	-19	0	-280	-1135	4.02	4.02	4.02	4.02	2	0.18	0.03	0.19	0.00	0.00	22.3
8	113	2589	1299	-42	0	-307	-1746	4.02	4.02	4.02	4.02	2	0.29	0.04	0.23	0.00	0.00	22.3
9	113	2402	1289	-26	0	-302	-1703	4.02	4.02	4.02	4.02	2	0.28	0.04	0.23	0.00	0.00	22.3
10	113	1766	829	-21	0	-259	-500	4.02	4.02	4.02	4.02	2	0.08	0.02	0.15	0.00	0.00	22.3
11	113	1709	826	-16	0	-258	-487	4.02	4.02	4.02	4.02	2	0.08	0.02	0.15	0.00	0.00	22.3
12	113	2932	1546	-45	0	-330	-2395	4.02	4.02	4.02	4.02	2	0.40	0.04	0.28	0.00	0.00	22.3
13	113	2876	1543	-40	0	-329	-2382	4.02	4.02	4.02	4.02	2	0.40	0.04	0.27	0.00	0.00	22.3
14	113	2240	1084	-35	0	-286	-1178	4.02	4.02	4.02	4.02	2	0.19	0.03	0.19	0.00	0.00	22.3
15	113	2052	1074	-19	0	-280	-1135	4.02	4.02	4.02	4.02	2	0.18	0.03	0.19	0.00	0.00	22.3
16	113	2589	1299	-42	0	-307	-1746	4.02	4.02	4.02	4.02	2	0.29	0.04	0.23	0.00	0.00	22.3
17	113	2402	1289	-26	0	-302	-1703	4.02	4.02	4.02	4.02	2	0.28	0.04	0.23	0.00	0.00	22.3
18	113	3981	1125	80	0	-441	-976	4.02	4.02	4.02	4.02	3	0.16	0.03	0.20	0.00	0.00	22.3
19	113	6933	2770	-118	0	-855	-5235	4.02	4.02	4.02	4.02	3	0.94	0.08	0.49	0.00	0.00	22.3
20	113	5011	1878	-30	0	-654	-2892	4.02	4.02	4.02	4.02	3	0.49	0.05	0.33	0.00	0.00	22.3
37	113	2149	436	140	0	-216	1237	4.02	4.02	4.02	4.02	3	0.19	0.01	0.08	0.00	0.00	22.3
38	113	7070	3177	-189	0	-905	-6225	4.02	4.02	4.02	6.03	3	0.71	0.09	0.49	0.00	0.00	22.3
39	113	3866	1690	-44	0	-570	-2318	4.02	4.02	4.02	4.02	3	0.37	0.05	0.30	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= 2.01 (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	170	3017	1173	-40	0	-360	-918	4.02	4.02	4.02	4.02	3	0.14	0.03	0.21	0.00	0.00	22.3
2	170	1766	545	-21	0	-247	585	4.02	4.02	4.02	4.02	2	0.09	0.02	0.10	0.00	0.00	22.3
3	170	1709	542	-16	0	-248	594	4.02	4.02	4.02	4.02	2	0.09	0.02	0.10	0.00	0.00	22.3
4	170	2932	1262	-45	0	-305	-1457	4.02	4.02	4.02	4.02	2	0.24	0.04	0.22	0.00	0.00	22.3
5	170	2876	1259	-40	0	-306	-1445	4.02	4.02	4.02	4.02	2	0.24	0.04	0.22	0.00	0.00	22.3
6	170	2240	800	-35	0	-266	-502	4.02	4.02	4.02	4.02	2	0.08	0.02	0.14	0.00	0.00	22.3

7	170	2052	790	-19	0	-270	-464	4.02	4.02	4.02	4.02	2	0.08	0.02	0.14	0.00	0.00	22.3
8	170	2589	1015	-42	0	-283	-948	4.02	4.02	4.02	4.02	2	0.16	0.03	0.18	0.00	0.00	22.3
9	170	2402	1005	-26	0	-287	-911	4.02	4.02	4.02	4.02	2	0.15	0.03	0.18	0.00	0.00	22.3
10	170	1766	545	-21	0	-247	585	4.02	4.02	4.02	4.02	2	0.09	0.02	0.10	0.00	0.00	22.3
11	170	1709	542	-16	0	-248	594	4.02	4.02	4.02	4.02	2	0.09	0.02	0.10	0.00	0.00	22.3
12	170	2932	1262	-45	0	-305	-1457	4.02	4.02	4.02	4.02	2	0.24	0.04	0.22	0.00	0.00	22.3
13	170	2876	1259	-40	0	-306	-1445	4.02	4.02	4.02	4.02	2	0.24	0.04	0.22	0.00	0.00	22.3
14	170	2240	800	-35	0	-266	-502	4.02	4.02	4.02	4.02	2	0.08	0.02	0.14	0.00	0.00	22.3
15	170	2052	790	-19	0	-270	-464	4.02	4.02	4.02	4.02	2	0.08	0.02	0.14	0.00	0.00	22.3
16	170	2589	1015	-42	0	-283	-948	4.02	4.02	4.02	4.02	2	0.16	0.03	0.18	0.00	0.00	22.3
17	170	2402	1005	-26	0	-287	-911	4.02	4.02	4.02	4.02	2	0.15	0.03	0.18	0.00	0.00	22.3
18	170	3981	756	80	0	-486	508	4.02	4.02	4.02	4.02	3	0.13	0.02	0.13	0.00	0.00	22.3
19	170	6933	2401	-118	0	-789	-3587	4.02	4.02	4.02	4.02	3	0.65	0.07	0.43	0.00	0.00	22.3
20	170	5011	1509	-30	0	-637	-1747	4.02	4.02	4.02	4.02	3	0.29	0.04	0.27	0.00	0.00	22.3
37	170	2149	67	140	0	-295	1237	4.02	4.02	4.02	4.02	3	0.19	0.00	0.01	0.00	0.00	22.3
38	170	7070	2808	-189	0	-798	-4347	4.02	4.02	4.02	4.02	3	0.79	0.08	0.50	0.00	0.00	22.3
39	170	3866	1321	-44	0	-545	-1280	4.02	4.02	4.02	4.02	3	0.21	0.04	0.24	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	226	3017	794	-40	0	-337	634	4.02	4.02	4.02	4.02	3	0.10	0.02	0.14	0.00	0.00	22.3
2	226	1766	254	-21	0	-235	595	4.02	4.02	4.02	4.02	2	0.10	0.01	0.05	0.00	0.00	22.3
3	226	1709	251	-16	0	-239	601	4.02	4.02	4.02	4.02	2	0.10	0.01	0.04	0.00	0.00	22.3
4	226	2932	971	-45	0	-280	-678	4.02	4.02	4.02	4.02	2	0.11	0.03	0.17	0.00	0.00	22.3
5	226	2876	968	-40	0	-284	-668	4.02	4.02	4.02	4.02	2	0.11	0.03	0.17	0.00	0.00	22.3
6	226	2240	509	-35	0	-246	509	4.02	4.02	4.02	4.02	2	0.08	0.01	0.09	0.00	0.00	22.3
7	226	2052	499	-19	0	-260	525	4.02	4.02	4.02	4.02	2	0.08	0.01	0.09	0.00	0.00	22.3
8	226	2589	724	-42	0	-259	423	4.02	4.02	4.02	4.02	2	0.08	0.02	0.13	0.00	0.00	22.3
9	226	2402	714	-26	0	-273	445	4.02	4.02	4.02	4.02	2	0.08	0.02	0.13	0.00	0.00	22.3
10	226	1766	254	-21	0	-235	595	4.02	4.02	4.02	4.02	2	0.10	0.01	0.05	0.00	0.00	22.3
11	226	1709	251	-16	0	-239	601	4.02	4.02	4.02	4.02	2	0.10	0.01	0.04	0.00	0.00	22.3
12	226	2932	971	-45	0	-280	-678	4.02	4.02	4.02	4.02	2	0.11	0.03	0.17	0.00	0.00	22.3
13	226	2876	968	-40	0	-284	-668	4.02	4.02	4.02	4.02	2	0.11	0.03	0.17	0.00	0.00	22.3
14	226	2240	509	-35	0	-246	509	4.02	4.02	4.02	4.02	2	0.08	0.01	0.09	0.00	0.00	22.3
15	226	2052	499	-19	0	-260	525	4.02	4.02	4.02	4.02	2	0.08	0.01	0.09	0.00	0.00	22.3
16	226	2589	724	-42	0	-259	423	4.02	4.02	4.02	4.02	2	0.08	0.02	0.13	0.00	0.00	22.3
17	226	2402	714	-26	0	-273	445	4.02	4.02	4.02	4.02	2	0.08	0.02	0.13	0.00	0.00	22.3
18	226	3981	377	80	0	-531	550	4.02	4.02	4.02	4.02	3	0.15	0.01	0.07	0.00	0.00	22.3
19	226	6933	2022	-118	0	-722	-2146	4.02	4.02	4.02	4.02	3	0.39	0.06	0.36	0.00	0.00	22.3
20	226	5011	1130	-30	0	-620	-810	4.02	4.02	4.02	4.02	3	0.18	0.03	0.20	0.00	0.00	22.3
37	226	2149	-312	140	0	-373	1237	4.02	4.02	4.02	4.02	3	0.19	0.01	0.06	0.00	0.00	22.3
38	226	7070	2429	-189	0	-691	-2675	4.02	4.02	4.02	4.02	3	0.48	0.07	0.43	0.00	0.00	22.3
39	226	3866	942	-44	0	-521	505	4.02	4.02	4.02	4.02	3	0.14	0.03	0.17	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	282	3017	406	-40	0	-315	689	4.02	4.02	4.02	4.02	3	0.11	0.01	0.07	0.00	0.00	22.3
2	282	1766	-45	-21	0	-223	595	4.02	4.02	4.02	4.02	2	0.10	0.00	0.01	0.00	0.00	22.3
3	282	1709	-48	-16	0	-230	601	4.02	4.02	4.02	4.02	2	0.10	0.00	0.01	0.00	0.00	22.3
4	282	2932	672	-45	0	-254	618	4.02	4.02	4.02	4.02	2	0.10	0.02	0.12	0.00	0.00	22.3
5	282	2876	669	-40	0	-261	623	4.02	4.02	4.02	4.02	2	0.10	0.02	0.12	0.00	0.00	22.3
6	282	2240	210	-35	0	-226	509	4.02	4.02	4.02	4.02	2	0.08	0.01	0.04	0.00	0.00	22.3
7	282	2052	200	-19	0	-249	525	4.02	4.02	4.02	4.02	2	0.08	0.01	0.04	0.00	0.00	22.3
8	282	2589	425	-42	0	-235	536	4.02	4.02	4.02	4.02	2	0.09	0.01	0.08	0.00	0.00	22.3
9	282	2402	415	-26	0	-258	551	4.02	4.02	4.02	4.02	2	0.09	0.01	0.07	0.00	0.00	22.3
10	282	1766	-45	-21	0	-223	595	4.02	4.02	4.02	4.02	2	0.10	0.00	0.01	0.00	0.00	22.3
11	282	1709	-48	-16	0	-230	601	4.02	4.02	4.02	4.02	2	0.10	0.00	0.01	0.00	0.00	22.3
12	282	2932	672	-45	0	-254	618	4.02	4.02	4.02	4.02	2	0.10	0.02	0.12	0.00	0.00	22.3
13	282	2876	669	-40	0	-261	623	4.02	4.02	4.02	4.02	2	0.10	0.02	0.12	0.00	0.00	22.3
14	282	2240	210	-35	0	-226	509	4.02	4.02	4.02	4.02	2	0.08	0.01	0.04	0.00	0.00	22.3
15	282	2052	200	-19	0	-249	525	4.02	4.02	4.02	4.02	2	0.08	0.01	0.04	0.00	0.00	22.3
16	282	2589	425	-42	0	-235	536	4.02	4.02	4.02	4.02	2	0.09	0.01	0.08	0.00	0.00	22.3
17	282	2402	415	-26	0	-258	551	4.02	4.02	4.02	4.02	2	0.09	0.01	0.07	0.00	0.00	22.3
18	282	3981	-11	80	0	-577	550	4.02	4.02	4.02	4.02	3	0.16	0.00	0.00	0.00	0.00	22.3
19	282	6933	1634	-118	0	-656	-916	4.02	4.02	4.02	4.02	3	0.20	0.05	0.29	0.00	0.00	22.3
20	282	5011	742	-30	0	-603	667	4.02	4.02	4.02	4.02	3	0.17	0.02	0.13	0.00	0.00	22.3
37	282	2149	-700	140	0	-452	1237	4.02	4.02	4.02	4.02	3	0.19	0.02	0.12	0.00	0.00	22.3
38	282	7070	2041	-189	0	-584	-1216	4.02	4.02	4.02	4.02	3	0.22	0.06	0.36	0.00	0.00	22.3
39	282	3866	554	-44	0	-496	652	4.02	4.02	4.02	4.02	3	0.14	0.02	0.10	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	339	3017	8	-40	0	-293	689	4.02	4.02	4.02	4.02	3	0.11	0.00	0.00	0.00	0.00	22.3
2	339	1766	-350	-21	0	-211	595	4.02	4.02	4.02	4.02	2	0.10	0.01	0.06	0.00	0.00	22.3
3	339	1709	-353	-16	0	-221	601	4.02	4.02	4.02	4.02	2	0.10	0.01	0.06	0.00	0.00	22.3
4	339	2932	366	-45	0	-229	691	4.02	4.02	4.02	4.02	2	0.11	0.01	0.07	0.00	0.00	22.3
5	339	2876	363	-40	0	-239	694	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
6	339	2240	-96	-35	0	-206	509	4.02	4.02	4.02	4.02	2	0.08	0.00	0.02	0.00	0.00	22.3
7	339	2052	-106	-19	0	-239	525	4.02	4.02	4.02	4.02	2	0.08	0.00	0.02	0.00	0.00	22.3
8	339	2589	119	-42	0	-211	536	4.02	4.02	4.02	4.02	2	0.09	0.00	0.02	0.00	0.00	22.3
9	339	2402	109	-26	0	-244	551	4.02	4.02	4.02	4.02	2	0.09	0.00	0.02	0.00	0.00	22.3
10	339	1766	-350	-21	0	-211	595	4.02	4.02	4.02	4.02	2	0.10	0.01	0.06	0.00	0.00	22.3
11	339	1709	-353	-16	0	-221	601	4.02	4.02	4.02	4.02	2	0.10	0.01	0.06	0.00	0.00	22.3
12	339	2932	366	-45	0	-229	691	4.02	4.02	4.02	4.02	2	0.11	0.01	0.07	0.00	0.00	22.3
13	339	2876	363	-40	0	-239	694	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
14	339	2240	-96	-35	0	-206	509	4.02	4.02	4.02	4.02	2	0.08	0.00	0.02	0.00	0.00	22.3
15	339	2052	-106	-19	0	-239	525	4.02	4.02	4.02	4.02	2	0.08	0.00	0.02	0.00	0.00	22.3
16	339	2589	119	-42	0	-211	536	4.02	4.02	4.02	4.02	2	0.09	0.00	0.02	0.00	0.00	22.3
17	339	2402	109	-26	0	-244	551	4.02	4.02	4.02	4.02	2	0.09	0.00	0.02	0.00	0.00	22.3
18	339	3981	-409	80	0	-622	550	4.02	4.02	4.02	4.02	3	0.17	0.01	0.07	0.00	0.00	22.3
19	339	6933	1236	-118	0	-589	1347	4.02	4.02	4.02	4.02	3	0.24	0.04	0.22	0.00	0.00	22.3
20	339	5011	344	-30	0	-586	678	4.02	4.02	4.02	4.02	3	0.17	0.01	0.06	0.00	0.00	22.3
37	339	2149	-1098	140	0	-531	931	4.02	4.02	4.02	4.02	3	0.14	0.03	0.20	0.00	0.00	22.3
38	339	7070	1643	-189	0	-477	1690	4.02	4.02	4.02	4.02	3	0.31	0.05	0.29	0.00	0.00	22.3
39	339	3866	156	-44	0	-471	652	4.02	4.02	4.02	4.02	3	0.13	0.00	0.03	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	396	3017	-399	-40	0	-270	689	4.02	4.02	4.02	4.02	3	0.11	0.01	0.07	0.00	0.00	22.3
2	396	1766	-663	-21	0	-199	533	4.02	4.02	4.02	4.02	2	0.09	0.02	0.12	0.00	0.00	22.3
3	396	1709	-666	-16	0	-212	538	4.02	4.02	4.02	4.02	2	0.09	0.02	0.12	0.00	0.00	22.3
4	396	2932	53	-45	0	-204	691	4.02	4.02	4.02	4.02	2	0.11	0.00	0.01	0.00	0.00	22.3
5	396	2876	50	-40	0	-216	694	4.02	4.02	4.02	4.02	2	0.12	0.00	0.01	0.00	0.00	22.3
6	396	2240	-409	-35	0	-186	509	4.02	4.02	4.02	4.02	2	0.08	0.01	0.07	0.00	0.00	22.3
7	396	2052	-419	-19	0	-228	525	4.02	4.02	4.02	4.02	2	0.08	0.01	0.07	0.00	0.00	22.3
8	396	2589	-194	-42	0	-187	536	4.02	4.02	4.02	4.02	2	0.09	0.01	0.03	0.00	0.00	22.3
9	396	2402	-204	-26	0	-229	551	4.02	4.02	4.02	4.02	2	0.09	0.01	0.04	0.00	0.00	22.3
10	396	1766	-663	-21	0	-199	533	4.02	4.02	4.02	4.02	2	0.09	0.02	0.12	0.00	0.00	22.3
11	396	1709	-666	-16	0	-212	538	4.02	4.02	4.02	4.02	2	0.09	0.02	0.12	0.00	0.00	22.3
12	396	2932	53	-45	0	-204	691	4.02	4.02	4.02	4.02	2	0.11	0.00	0.01	0.00	0.00	22.3

13	396	2876	50	-40	0	-216	694	4.02	4.02	4.02	4.02	2	0.12	0.00	0.01	0.00	0.00	22.3
14	396	2240	-409	-35	0	-186	509	4.02	4.02	4.02	4.02	2	0.08	0.01	0.07	0.00	0.00	22.3
15	396	2052	-419	-19	0	-228	525	4.02	4.02	4.02	4.02	2	0.08	0.01	0.07	0.00	0.00	22.3
16	396	2589	-194	-42	0	-187	536	4.02	4.02	4.02	4.02	2	0.09	0.01	0.03	0.00	0.00	22.3
17	396	2402	-204	-26	0	-229	551	4.02	4.02	4.02	4.02	2	0.09	0.01	0.04	0.00	0.00	22.3
18	396	3981	-816	80	0	-667	499	4.02	4.02	4.02	4.02	3	0.18	0.02	0.15	0.00	0.00	22.3
19	396	6933	829	-118	0	-523	1725	4.02	4.02	4.02	4.02	3	0.31	0.02	0.15	0.00	0.00	22.3
20	396	5011	-63	-30	0	-569	678	4.02	4.02	4.02	4.02	3	0.16	0.00	0.01	0.00	0.00	22.3
37	396	2149	-1505	140	0	-610	-1122	4.02	4.02	4.02	4.02	3	0.17	0.04	0.27	0.00	0.00	22.3
38	396	7070	1236	-189	0	-370	2298	4.02	4.02	4.02	4.02	3	0.42	0.04	0.22	0.00	0.00	22.3
39	396	3866	-251	-44	0	-446	652	4.02	4.02	4.02	4.02	3	0.12	0.01	0.04	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	452	3017	-815	-40	0	-248	650	4.02	4.02	4.02	4.02	3	0.10	0.02	0.15	0.00	0.00	22.3
2	452	1766	-984	-21	0	-187	-766	4.02	4.02	4.02	4.02	2	0.12	0.03	0.18	0.00	0.00	22.3
3	452	1709	-987	-16	0	-203	-766	4.02	4.02	4.02	4.02	2	0.12	0.03	0.18	0.00	0.00	22.3
4	452	2932	-267	-45	0	-178	691	4.02	4.02	4.02	4.02	2	0.11	0.01	0.05	0.00	0.00	22.3
5	452	2876	-270	-40	0	-194	694	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
6	452	2240	-730	-35	0	-166	415	4.02	4.02	4.02	4.02	2	0.07	0.02	0.13	0.00	0.00	22.3
7	452	2052	-740	-19	0	-218	424	4.02	4.02	4.02	4.02	2	0.07	0.02	0.13	0.00	0.00	22.3
8	452	2589	-515	-42	0	-163	536	4.02	4.02	4.02	4.02	2	0.09	0.01	0.09	0.00	0.00	22.3
9	452	2402	-525	-26	0	-215	551	4.02	4.02	4.02	4.02	2	0.09	0.02	0.09	0.00	0.00	22.3
10	452	1766	-984	-21	0	-187	-766	4.02	4.02	4.02	4.02	2	0.12	0.03	0.18	0.00	0.00	22.3
11	452	1709	-987	-16	0	-203	-766	4.02	4.02	4.02	4.02	2	0.12	0.03	0.18	0.00	0.00	22.3
12	452	2932	-267	-45	0	-178	691	4.02	4.02	4.02	4.02	2	0.11	0.01	0.05	0.00	0.00	22.3
13	452	2876	-270	-40	0	-194	694	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
14	452	2240	-730	-35	0	-166	415	4.02	4.02	4.02	4.02	2	0.07	0.02	0.13	0.00	0.00	22.3
15	452	2052	-740	-19	0	-218	424	4.02	4.02	4.02	4.02	2	0.07	0.02	0.13	0.00	0.00	22.3
16	452	2589	-515	-42	0	-163	536	4.02	4.02	4.02	4.02	2	0.09	0.01	0.09	0.00	0.00	22.3
17	452	2402	-525	-26	0	-215	551	4.02	4.02	4.02	4.02	2	0.09	0.02	0.09	0.00	0.00	22.3
18	452	3981	-1232	80	0	-712	-1116	4.02	4.02	4.02	4.02	3	0.20	0.04	0.22	0.00	0.00	22.3
19	452	6933	412	-118	0	-457	1769	4.02	4.02	4.02	4.02	3	0.32	0.01	0.07	0.00	0.00	22.3
20	452	5011	-480	-30	0	-551	678	4.02	4.02	4.02	4.02	3	0.16	0.01	0.09	0.00	0.00	22.3
37	452	2149	-1922	140	0	-689	-2301	4.02	4.02	4.02	4.02	3	0.35	0.06	0.34	0.00	0.00	22.3
38	452	7070	819	-189	0	-263	2668	4.02	4.02	4.02	4.02	3	0.48	0.02	0.15	0.00	0.00	22.3
39	452	3866	-667	-44	0	-422	652	4.02	4.02	4.02	4.02	3	0.12	0.02	0.12	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	508	3017	-1241	-40	0	-225	-971	4.02	4.02	4.02	4.02	3	0.15	0.04	0.22	0.00	0.00	22.3
2	508	1766	-1311	-21	0	-175	-1580	4.02	4.02	4.02	4.02	2	0.25	0.04	0.23	0.00	0.00	22.3
3	508	1709	-1314	-16	0	-194	-1581	4.02	4.02	4.02	4.02	2	0.25	0.04	0.23	0.00	0.00	22.3
4	508	2932	-595	-45	0	-153	689	4.02	4.02	4.02	4.02	2	0.11	0.02	0.11	0.00	0.00	22.3
5	508	2876	-598	-40	0	-171	690	4.02	4.02	4.02	4.02	2	0.11	0.02	0.11	0.00	0.00	22.3
6	508	2240	-1057	-35	0	-146	-994	4.02	4.02	4.02	4.02	2	0.16	0.03	0.19	0.00	0.00	22.3
7	508	2052	-1067	-19	0	-207	-1001	4.02	4.02	4.02	4.02	2	0.16	0.03	0.19	0.00	0.00	22.3
8	508	2589	-842	-42	0	-139	-494	4.02	4.02	4.02	4.02	2	0.08	0.02	0.15	0.00	0.00	22.3
9	508	2402	-852	-26	0	-200	-501	4.02	4.02	4.02	4.02	2	0.08	0.02	0.15	0.00	0.00	22.3
10	508	1766	-1311	-21	0	-175	-1580	4.02	4.02	4.02	4.02	2	0.25	0.04	0.23	0.00	0.00	22.3
11	508	1709	-1314	-16	0	-194	-1581	4.02	4.02	4.02	4.02	2	0.25	0.04	0.23	0.00	0.00	22.3
12	508	2932	-595	-45	0	-153	689	4.02	4.02	4.02	4.02	2	0.11	0.02	0.11	0.00	0.00	22.3
13	508	2876	-598	-40	0	-171	690	4.02	4.02	4.02	4.02	2	0.11	0.02	0.11	0.00	0.00	22.3
14	508	2240	-1057	-35	0	-146	-994	4.02	4.02	4.02	4.02	2	0.16	0.03	0.19	0.00	0.00	22.3
15	508	2052	-1067	-19	0	-207	-1001	4.02	4.02	4.02	4.02	2	0.16	0.03	0.19	0.00	0.00	22.3
16	508	2589	-842	-42	0	-139	-494	4.02	4.02	4.02	4.02	2	0.08	0.02	0.15	0.00	0.00	22.3
17	508	2402	-852	-26	0	-200	-501	4.02	4.02	4.02	4.02	2	0.08	0.02	0.15	0.00	0.00	22.3
18	508	3981	-1658	80	0	-757	-2148	4.02	4.02	4.02	4.02	3	0.35	0.05	0.30	0.00	0.00	22.3
19	508	6933	-14	-118	0	-390	1769	4.02	4.02	4.02	4.02	3	0.32	0.00	0.00	0.00	0.00	22.3
20	508	5011	-906	-30	0	-534	592	4.02	4.02	4.02	4.02	3	0.15	0.03	0.16	0.00	0.00	22.3
37	508	2149	-2348	140	0	-768	-3722	4.02	4.02	4.02	4.02	3	0.57	0.07	0.42	0.00	0.00	22.3
38	508	7070	394	-189	0	-157	2696	4.02	4.02	4.02	4.02	3	0.49	0.01	0.07	0.00	0.00	22.3
39	508	3866	-1093	-44	0	-397	-683	4.02	4.02	4.02	4.02	3	0.11	0.03	0.19	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	565	3017	-1676	-40	0	-203	-1167	4.02	4.02	4.02	4.02	3	0.18	0.05	0.30	0.00	0.00	22.3
2	565	1766	-1646	-21	0	-164	-1751	4.02	4.02	4.02	4.02	2	0.28	0.05	0.29	0.00	0.00	22.3
3	565	1709	-1649	-16	0	-185	-1753	4.02	4.02	4.02	4.02	2	0.28	0.05	0.29	0.00	0.00	22.3
4	565	2932	-930	-45	0	-128	-43	4.02	4.02	4.02	4.02	2	0.04	0.03	0.17	0.00	0.00	22.3
5	565	2876	-933	-40	0	-149	-45	4.02	4.02	4.02	4.02	2	0.05	0.03	0.17	0.00	0.00	22.3
6	565	2240	-1392	-35	0	-126	-1150	4.02	4.02	4.02	4.02	2	0.19	0.04	0.25	0.00	0.00	22.3
7	565	2052	-1402	-19	0	-197	-1158	4.02	4.02	4.02	4.02	2	0.19	0.04	0.25	0.00	0.00	22.3
8	565	2589	-1177	-42	0	-115	-638	4.02	4.02	4.02	4.02	2	0.10	0.03	0.21	0.00	0.00	22.3
9	565	2402	-1187	-26	0	-186	-646	4.02	4.02	4.02	4.02	2	0.11	0.03	0.21	0.00	0.00	22.3
10	565	1766	-1646	-21	0	-164	-1751	4.02	4.02	4.02	4.02	2	0.28	0.05	0.29	0.00	0.00	22.3
11	565	1709	-1649	-16	0	-185	-1753	4.02	4.02	4.02	4.02	2	0.28	0.05	0.29	0.00	0.00	22.3
12	565	2932	-930	-45	0	-128	-43	4.02	4.02	4.02	4.02	2	0.04	0.03	0.17	0.00	0.00	22.3
13	565	2876	-933	-40	0	-149	-45	4.02	4.02	4.02	4.02	2	0.05	0.03	0.17	0.00	0.00	22.3
14	565	2240	-1392	-35	0	-126	-1150	4.02	4.02	4.02	4.02	2	0.19	0.04	0.25	0.00	0.00	22.3
15	565	2052	-1402	-19	0	-197	-1158	4.02	4.02	4.02	4.02	2	0.19	0.04	0.25	0.00	0.00	22.3
16	565	2589	-1177	-42	0	-115	-638	4.02	4.02	4.02	4.02	2	0.10	0.03	0.21	0.00	0.00	22.3
17	565	2402	-1187	-26	0	-186	-646	4.02	4.02	4.02	4.02	2	0.11	0.03	0.21	0.00	0.00	22.3
18	565	3981	-2093	80	0	-802	-2368	4.02	4.02	4.02	4.02	3	0.38	0.06	0.37	0.00	0.00	22.3
19	565	6933	-449	-118	0	-324	1769	4.02	4.02	4.02	4.02	3	0.32	0.01	0.08	0.00	0.00	22.3
20	565	5011	-1341	-30	0	-517	-500	4.02	4.02	4.02	4.02	3	0.15	0.04	0.24	0.00	0.00	22.3
37	565	2149	-2783	140	0	-846	-3982	4.02	4.02	4.02	4.02	3	0.61	0.08	0.50	0.00	0.00	22.3
38	565	7070	-42	-189	0	-50	2696	4.02	4.02	4.02	4.02	3	0.49	0.01	0.03	0.00	0.00	22.3
39	565	3866	-1528	-44	0	-372	-870	4.02	4.02	4.02	4.02	3	0.14	0.04	0.27	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

Nome travata: **Trave_402_IP1** Descrizione: **Trave_4 1-10-15-20-25**
ASTA NUM. 6 NI 295 NF 297 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y Permanente qy tot.
qy medio: 375.00 272.00 647.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	3233	2406	197	0	731	-2450	4.02	4.02	4.02	4.02	3	0.39	0.07	0.43	0.00	0.00	22.3
2	0	2621	1629	154	0	574	-1260	4.02	4.02	4.02	4.02	2	0.21	0.05	0.29	0.00	0.00	22.3
3	0	2550	1629	148	0	548	-1257	4.02	4.02	4.02	4.02	2	0.21	0.05	0.29	0.00	0.00	22.3
4	0	2424	2072	155	0	576	-2512	4.02	4.02	4.02	4.02	2	0.41	0.06	0.37	0.00	0.00	22.3

5	0	2352	2072	148	0	551	-2509	4.02	4.02	4.02	4.02	2	0.41	0.06	0.37	0.00	0.00	22.3
6	0	2636	1785	162	0	605	-1701	4.02	4.02	4.02	4.02	2	0.28	0.05	0.32	0.00	0.00	22.3
7	0	2397	1783	140	0	519	-1692	4.02	4.02	4.02	4.02	2	0.28	0.05	0.32	0.00	0.00	22.3
8	0	2577	1918	162	0	606	-2077	4.02	4.02	4.02	4.02	2	0.34	0.06	0.34	0.00	0.00	22.3
9	0	2338	1916	140	0	520	-2067	4.02	4.02	4.02	4.02	2	0.34	0.06	0.34	0.00	0.00	22.3
10	0	2621	1629	154	0	574	-1260	4.02	4.02	4.02	4.02	2	0.21	0.05	0.29	0.00	0.00	22.3
11	0	2550	1629	148	0	548	-1257	4.02	4.02	4.02	4.02	2	0.21	0.05	0.29	0.00	0.00	22.3
12	0	2424	2072	155	0	576	-2512	4.02	4.02	4.02	4.02	2	0.41	0.06	0.37	0.00	0.00	22.3
13	0	2352	2072	148	0	551	-2509	4.02	4.02	4.02	4.02	2	0.41	0.06	0.37	0.00	0.00	22.3
14	0	2636	1785	162	0	605	-1701	4.02	4.02	4.02	4.02	2	0.28	0.05	0.32	0.00	0.00	22.3
15	0	2397	1783	140	0	519	-1692	4.02	4.02	4.02	4.02	2	0.28	0.05	0.32	0.00	0.00	22.3
16	0	2577	1918	162	0	606	-2077	4.02	4.02	4.02	4.02	2	0.34	0.06	0.34	0.00	0.00	22.3
17	0	2338	1916	140	0	520	-2067	4.02	4.02	4.02	4.02	2	0.34	0.06	0.34	0.00	0.00	22.3
18	0	5890	1978	488	0	1827	-1255	4.02	4.02	4.02	4.02	3	0.53	0.06	0.35	0.00	0.00	22.3
19	0	5373	3093	377	0	1369	-4397	4.02	4.02	4.02	4.02	3	0.75	0.09	0.55	0.00	0.00	22.3
20	0	5180	2515	383	0	1445	-2766	4.02	4.02	4.02	4.02	3	0.47	0.07	0.45	0.00	0.00	22.3
37	0	5224	1561	449	0	1701	-75	4.02	4.02	4.02	4.02	3	0.48	0.05	0.28	0.00	0.00	22.3
38	0	4363	3419	264	0	936	-5313	4.02	4.02	4.02	4.02	3	0.87	0.10	0.61	0.00	0.00	22.3
39	0	4041	2456	274	0	1063	-2594	4.02	4.02	4.02	4.02	3	0.42	0.07	0.44	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	56	3233	1963	197	0	620	-2209	4.02	4.02	4.02	4.02	3	0.35	0.06	0.35	0.00	0.00	22.3
2	56	2621	1288	154	0	487	-1087	4.02	4.02	4.02	4.02	2	0.18	0.04	0.23	0.00	0.00	22.3
3	56	2550	1288	148	0	465	-1085	4.02	4.02	4.02	4.02	2	0.18	0.04	0.23	0.00	0.00	22.3
4	56	2424	1731	155	0	489	-2313	4.02	4.02	4.02	4.02	2	0.38	0.05	0.31	0.00	0.00	22.3
5	56	2352	1731	148	0	467	-2311	4.02	4.02	4.02	4.02	2	0.38	0.05	0.31	0.00	0.00	22.3
6	56	2636	1444	162	0	513	-1519	4.02	4.02	4.02	4.02	2	0.25	0.04	0.26	0.00	0.00	22.3
7	56	2397	1442	140	0	440	-1511	4.02	4.02	4.02	4.02	2	0.25	0.04	0.26	0.00	0.00	22.3
8	56	2577	1577	162	0	514	-1888	4.02	4.02	4.02	4.02	2	0.31	0.05	0.28	0.00	0.00	22.3
9	56	2338	1575	140	0	440	-1878	4.02	4.02	4.02	4.02	2	0.31	0.05	0.28	0.00	0.00	22.3
10	56	2621	1288	154	0	487	-1087	4.02	4.02	4.02	4.02	2	0.18	0.04	0.23	0.00	0.00	22.3
11	56	2550	1288	148	0	465	-1085	4.02	4.02	4.02	4.02	2	0.18	0.04	0.23	0.00	0.00	22.3
12	56	2424	1731	155	0	489	-2313	4.02	4.02	4.02	4.02	2	0.38	0.05	0.31	0.00	0.00	22.3
13	56	2352	1731	148	0	467	-2311	4.02	4.02	4.02	4.02	2	0.38	0.05	0.31	0.00	0.00	22.3
14	56	2636	1444	162	0	513	-1519	4.02	4.02	4.02	4.02	2	0.25	0.04	0.26	0.00	0.00	22.3
15	56	2397	1442	140	0	440	-1511	4.02	4.02	4.02	4.02	2	0.25	0.04	0.26	0.00	0.00	22.3
16	56	2577	1577	162	0	514	-1888	4.02	4.02	4.02	4.02	2	0.31	0.05	0.28	0.00	0.00	22.3
17	56	2338	1575	140	0	440	-1878	4.02	4.02	4.02	4.02	2	0.31	0.05	0.28	0.00	0.00	22.3
18	56	5890	1535	488	0	1551	-1039	4.02	4.02	4.02	4.02	3	0.45	0.04	0.27	0.00	0.00	22.3
19	56	5373	2650	377	0	1156	-4116	4.02	4.02	4.02	4.02	3	0.70	0.08	0.47	0.00	0.00	22.3
20	56	5180	2072	383	0	1228	-2518	4.02	4.02	4.02	4.02	3	0.43	0.06	0.37	0.00	0.00	22.3
37	56	5224	1118	449	0	1447	1248	4.02	4.02	4.02	4.02	3	0.41	0.03	0.20	0.00	0.00	22.3
38	56	4363	2976	264	0	787	-5013	4.02	4.02	4.02	4.02	3	0.82	0.09	0.53	0.00	0.00	22.3
39	56	4041	2013	274	0	908	-2350	4.02	4.02	4.02	4.02	3	0.38	0.06	0.36	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	113	3233	1512	197	0	509	-999	4.02	4.02	4.02	4.02	3	0.16	0.04	0.27	0.00	0.00	22.3
2	113	2621	941	154	0	399	671	4.02	4.02	4.02	4.02	2	0.12	0.03	0.17	0.00	0.00	22.3
3	113	2550	941	148	0	381	673	4.02	4.02	4.02	4.02	2	0.11	0.03	0.17	0.00	0.00	22.3
4	113	2424	1384	155	0	401	-1258	4.02	4.02	4.02	4.02	2	0.21	0.04	0.25	0.00	0.00	22.3
5	113	2352	1384	148	0	383	-1255	4.02	4.02	4.02	4.02	2	0.20	0.04	0.25	0.00	0.00	22.3
6	113	2636	1097	162	0	422	-626	4.02	4.02	4.02	4.02	2	0.13	0.03	0.20	0.00	0.00	22.3
7	113	2397	1095	140	0	360	-618	4.02	4.02	4.02	4.02	2	0.11	0.03	0.20	0.00	0.00	22.3
8	113	2577	1230	162	0	422	-919	4.02	4.02	4.02	4.02	2	0.15	0.04	0.22	0.00	0.00	22.3
9	113	2338	1228	140	0	361	-910	4.02	4.02	4.02	4.02	2	0.15	0.04	0.22	0.00	0.00	22.3
10	113	2621	941	154	0	399	671	4.02	4.02	4.02	4.02	2	0.12	0.03	0.17	0.00	0.00	22.3
11	113	2550	941	148	0	381	673	4.02	4.02	4.02	4.02	2	0.11	0.03	0.17	0.00	0.00	22.3
12	113	2424	1384	155	0	401	-1258	4.02	4.02	4.02	4.02	2	0.21	0.04	0.25	0.00	0.00	22.3
13	113	2352	1384	148	0	383	-1255	4.02	4.02	4.02	4.02	2	0.20	0.04	0.25	0.00	0.00	22.3
14	113	2636	1097	162	0	422	-626	4.02	4.02	4.02	4.02	2	0.13	0.03	0.20	0.00	0.00	22.3
15	113	2397	1095	140	0	360	-618	4.02	4.02	4.02	4.02	2	0.11	0.03	0.20	0.00	0.00	22.3
16	113	2577	1230	162	0	422	-919	4.02	4.02	4.02	4.02	2	0.15	0.04	0.22	0.00	0.00	22.3
17	113	2338	1228	140	0	361	-910	4.02	4.02	4.02	4.02	2	0.15	0.04	0.22	0.00	0.00	22.3
18	113	5890	1084	488	0	1276	1027	4.02	4.02	4.02	4.02	3	0.37	0.03	0.19	0.00	0.00	22.3
19	113	5373	2199	377	0	942	-2518	4.02	4.02	4.02	4.02	3	0.43	0.06	0.39	0.00	0.00	22.3
20	113	5180	1621	383	0	1012	-1247	4.02	4.02	4.02	4.02	3	0.29	0.05	0.29	0.00	0.00	22.3
37	113	5224	667	449	0	1194	1435	4.02	4.02	4.02	4.02	3	0.34	0.02	0.12	0.00	0.00	22.3
38	113	4363	2525	264	0	637	-3230	4.02	4.02	4.02	4.02	3	0.53	0.07	0.45	0.00	0.00	22.3
39	113	4041	1562	274	0	753	-1112	4.02	4.02	4.02	4.02	3	0.21	0.05	0.28	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	170	3233	1054	197	0	397	1025	4.02	4.02	4.02	4.02	3	0.16	0.03	0.19	0.00	0.00	22.3
2	170	2621	589	154	0	312	889	4.02	4.02	4.02	4.02	2	0.15	0.02	0.10	0.00	0.00	22.3
3	170	2550	589	148	0	298	890	4.02	4.02	4.02	4.02	2	0.15	0.02	0.10	0.00	0.00	22.3
4	170	2424	1032	155	0	314	649	4.02	4.02	4.02	4.02	2	0.11	0.03	0.18	0.00	0.00	22.3
5	170	2352	1032	148	0	299	651	4.02	4.02	4.02	4.02	2	0.11	0.03	0.18	0.00	0.00	22.3
6	170	2636	745	162	0	330	828	4.02	4.02	4.02	4.02	2	0.14	0.02	0.13	0.00	0.00	22.3
7	170	2397	743	140	0	281	832	4.02	4.02	4.02	4.02	2	0.14	0.02	0.13	0.00	0.00	22.3
8	170	2577	878	162	0	330	745	4.02	4.02	4.02	4.02	2	0.12	0.03	0.16	0.00	0.00	22.3
9	170	2338	876	140	0	282	750	4.02	4.02	4.02	4.02	2	0.12	0.03	0.16	0.00	0.00	22.3
10	170	2621	589	154	0	312	889	4.02	4.02	4.02	4.02	2	0.15	0.02	0.10	0.00	0.00	22.3
11	170	2550	589	148	0	298	890	4.02	4.02	4.02	4.02	2	0.15	0.02	0.10	0.00	0.00	22.3
12	170	2424	1032	155	0	314	649	4.02	4.02	4.02	4.02	2	0.11	0.03	0.18	0.00	0.00	22.3
13	170	2352	1032	148	0	299	651	4.02	4.02	4.02	4.02	2	0.11	0.03	0.18	0.00	0.00	22.3
14	170	2636	745	162	0	330	828	4.02	4.02	4.02	4.02	2	0.14	0.02	0.13	0.00	0.00	22.3
15	170	2397	743	140	0	281	832	4.02	4.02	4.02	4.02	2	0.14	0.02	0.13	0.00	0.00	22.3
16	170	2577	878	162	0	330	745	4.02	4.02	4.02	4.02	2	0.12	0.03	0.16	0.00	0.00	22.3
17	170	2338	876	140	0	282	750	4.02	4.02	4.02	4.02	2	0.12	0.03	0.16	0.00	0.00	22.3
18	170	5890	626	488	0	1000	1185	4.02	4.02	4.02	4.02	3	0.29	0.02	0.11	0.00	0.00	22.3
19	170	5373	1741	377	0	729	-1172	4.02	4.02	4.02	4.02	3	0.21	0.05	0.31	0.00	0.00	22.3
20	170	5180	1163	383	0	795	950	4.02	4.02	4.02	4.02	3	0.23	0.03	0.21	0.00	0.00	22.3
37	170	5224	209	449	0	940	1435	4.02	4.02	4.02	4.02	3	0.27	0.01	0.07	0.00	0.00	22.3
38	170	4363	2067	264	0	488	-1701	4.02	4.02	4.02	4.02	3	0.28	0.06	0.37	0.00	0.00	22.3
39	170	4041	1104	274	0	599	992	4.02	4.02	4.02	4.02	3	0.16	0.03	0.20	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	226	3233	590	197	0	286	1156	4.02	4.02	4.02	4.02	3	0.18	0.02	0.11	0.00	0.00	22.3
2	226	2621	232	154	0	225	889	4.02	4.02	4.02	4.02	2	0.15	0.01	0.04	0.00	0.00	22.3
3	226	2550	232	148	0	214	890	4.02	4.02	4.02	4.02	2	0.15	0.01	0.04	0.00	0.00	22.3
4	226	2424	675	155	0	226	951	4.02	4.02	4.02	4.02	2	0.16	0.02	0.12	0.00	0.00	22.3
5	226	2352	675	148	0	215	952	4.02	4.02	4.02	4.02	2	0.16	0.02	0.12	0.00	0.00	22.3
6	226	2636	388	162	0	238	888	4.02	4.02	4.02	4.02	2	0.15	0.01	0.07	0.00	0.00	22.3
7	226	2397	386	140	0	202	891	4.02	4.02	4.02	4.02	2	0.15	0.01	0.07	0.00	0.00	22.3
8	226	2577	521	162	0	239	888	4.02	4.02	4.02	4.02	2	0.15	0.02	0.09	0.00	0.00	22.3
9	226	2338	519	140	0	202	891	4.02	4.02	4.02	4.02	2	0.15	0.02	0.09	0.00	0.00	22.3
10	226	2621	232	154	0	225	889	4.02	4.02	4.02	4.02	2	0.15	0.01	0.04	0.00	0.00	22.3

11	226	2550	232	148	0	214	890	4.02	4.02	4.02	4.02	2	0.15	0.01	0.04	0.00	0.00	22.3
12	226	2424	675	155	0	226	951	4.02	4.02	4.02	4.02	2	0.16	0.02	0.12	0.00	0.00	22.3
13	226	2352	675	148	0	215	952	4.02	4.02	4.02	4.02	2	0.16	0.02	0.12	0.00	0.00	22.3
14	226	2636	388	162	0	238	888	4.02	4.02	4.02	4.02	2	0.15	0.01	0.07	0.00	0.00	22.3
15	226	2397	386	140	0	202	891	4.02	4.02	4.02	4.02	2	0.15	0.01	0.07	0.00	0.00	22.3
16	226	2577	521	162	0	239	888	4.02	4.02	4.02	4.02	2	0.15	0.02	0.09	0.00	0.00	22.3
17	226	2338	519	140	0	202	891	4.02	4.02	4.02	4.02	2	0.15	0.02	0.09	0.00	0.00	22.3
18	226	5890	162	488	0	724	1185	4.02	4.02	4.02	4.02	3	0.21	0.02	0.08	0.00	0.00	22.3
19	226	5373	1277	377	0	516	1209	4.02	4.02	4.02	4.02	3	0.21	0.04	0.23	0.00	0.00	22.3
20	226	5180	699	383	0	579	1150	4.02	4.02	4.02	4.02	3	0.19	0.02	0.12	0.00	0.00	22.3
37	226	5224	-255	449	0	686	1435	4.02	4.02	4.02	4.02	3	0.24	0.01	0.07	0.00	0.00	22.3
38	226	4363	1603	264	0	339	1194	4.02	4.02	4.02	4.02	3	0.20	0.05	0.29	0.00	0.00	22.3
39	226	4041	640	274	0	444	1155	4.02	4.02	4.02	4.02	3	0.19	0.02	0.11	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	282	3233	118	197	0	175	1156	4.02	4.02	4.02	4.02	3	0.18	0.01	0.03	0.00	0.00	22.3
2	282	2621	-131	154	0	138	889	4.02	4.02	4.02	4.02	2	0.15	0.00	0.02	0.00	0.00	22.3
3	282	2550	-131	148	0	131	890	4.02	4.02	4.02	4.02	2	0.15	0.00	0.02	0.00	0.00	22.3
4	282	2424	312	155	0	139	961	4.02	4.02	4.02	4.02	2	0.16	0.01	0.06	0.00	0.00	22.3
5	282	2352	312	148	0	131	962	4.02	4.02	4.02	4.02	2	0.16	0.01	0.06	0.00	0.00	22.3
6	282	2636	25	162	0	147	888	4.02	4.02	4.02	4.02	2	0.15	0.01	0.03	0.00	0.00	22.3
7	282	2397	23	140	0	123	891	4.02	4.02	4.02	4.02	2	0.15	0.00	0.00	0.00	0.00	22.3
8	282	2577	158	162	0	147	888	4.02	4.02	4.02	4.02	2	0.15	0.01	0.03	0.00	0.00	22.3
9	282	2338	156	140	0	123	891	4.02	4.02	4.02	4.02	2	0.15	0.00	0.03	0.00	0.00	22.3
10	282	2621	-131	154	0	138	889	4.02	4.02	4.02	4.02	2	0.15	0.00	0.02	0.00	0.00	22.3
11	282	2550	-131	148	0	131	890	4.02	4.02	4.02	4.02	2	0.15	0.00	0.02	0.00	0.00	22.3
12	282	2424	312	155	0	139	961	4.02	4.02	4.02	4.02	2	0.16	0.01	0.06	0.00	0.00	22.3
13	282	2352	312	148	0	131	962	4.02	4.02	4.02	4.02	2	0.16	0.01	0.06	0.00	0.00	22.3
14	282	2636	25	162	0	147	888	4.02	4.02	4.02	4.02	2	0.15	0.01	0.03	0.00	0.00	22.3
15	282	2397	23	140	0	123	891	4.02	4.02	4.02	4.02	2	0.15	0.00	0.00	0.00	0.00	22.3
16	282	2577	158	162	0	147	888	4.02	4.02	4.02	4.02	2	0.15	0.01	0.03	0.00	0.00	22.3
17	282	2338	156	140	0	123	891	4.02	4.02	4.02	4.02	2	0.15	0.00	0.03	0.00	0.00	22.3
18	282	5890	-310	488	0	448	1185	4.02	4.02	4.02	4.02	3	0.21	0.02	0.08	0.00	0.00	22.3
19	282	5373	805	377	0	303	1518	4.02	4.02	4.02	4.02	3	0.26	0.02	0.14	0.00	0.00	22.3
20	282	5180	227	383	0	362	1150	4.02	4.02	4.02	4.02	3	0.19	0.01	0.06	0.00	0.00	22.3
37	282	5224	-727	449	0	433	1435	4.02	4.02	4.02	4.02	3	0.24	0.02	0.13	0.00	0.00	22.3
38	282	4363	1131	264	0	189	1728	4.02	4.02	4.02	4.02	3	0.28	0.03	0.20	0.00	0.00	22.3
39	282	4041	168	274	0	289	1155	4.02	4.02	4.02	4.02	3	0.19	0.01	0.04	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	339	3233	-361	197	0	64	1156	4.02	4.02	4.02	4.02	3	0.18	0.01	0.06	0.00	0.00	22.3
2	339	2621	-499	154	0	51	889	4.02	4.02	4.02	4.02	2	0.15	0.01	0.09	0.00	0.00	22.3
3	339	2550	-500	148	0	48	890	4.02	4.02	4.02	4.02	2	0.15	0.01	0.09	0.00	0.00	22.3
4	339	2424	-56	155	0	51	961	4.02	4.02	4.02	4.02	2	0.16	0.00	0.02	0.00	0.00	22.3
5	339	2352	-57	148	0	47	962	4.02	4.02	4.02	4.02	2	0.16	0.00	0.01	0.00	0.00	22.3
6	339	2636	-343	162	0	55	888	4.02	4.02	4.02	4.02	2	0.15	0.01	0.06	0.00	0.00	22.3
7	339	2397	-346	140	0	44	891	4.02	4.02	4.02	4.02	2	0.15	0.01	0.06	0.00	0.00	22.3
8	339	2577	-210	162	0	55	888	4.02	4.02	4.02	4.02	2	0.15	0.01	0.04	0.00	0.00	22.3
9	339	2338	-213	140	0	44	891	4.02	4.02	4.02	4.02	2	0.15	0.01	0.04	0.00	0.00	22.3
10	339	2621	-499	154	0	51	889	4.02	4.02	4.02	4.02	2	0.15	0.01	0.09	0.00	0.00	22.3
11	339	2550	-500	148	0	48	890	4.02	4.02	4.02	4.02	2	0.15	0.01	0.09	0.00	0.00	22.3
12	339	2424	-56	155	0	51	961	4.02	4.02	4.02	4.02	2	0.16	0.00	0.02	0.00	0.00	22.3
13	339	2352	-57	148	0	47	962	4.02	4.02	4.02	4.02	2	0.16	0.00	0.01	0.00	0.00	22.3
14	339	2636	-343	162	0	55	888	4.02	4.02	4.02	4.02	2	0.15	0.01	0.06	0.00	0.00	22.3
15	339	2397	-346	140	0	44	891	4.02	4.02	4.02	4.02	2	0.15	0.01	0.06	0.00	0.00	22.3
16	339	2577	-210	162	0	55	888	4.02	4.02	4.02	4.02	2	0.15	0.01	0.04	0.00	0.00	22.3
17	339	2338	-213	140	0	44	891	4.02	4.02	4.02	4.02	2	0.15	0.01	0.04	0.00	0.00	22.3
18	339	5890	-789	488	0	172	1185	4.02	4.02	4.02	4.02	3	0.21	0.02	0.14	0.00	0.00	22.3
19	339	5373	326	377	0	89	1518	4.02	4.02	4.02	4.02	3	0.26	0.01	0.06	0.00	0.00	22.3
20	339	5180	-252	383	0	146	1150	4.02	4.02	4.02	4.02	3	0.19	0.01	0.06	0.00	0.00	22.3
37	339	5224	-1206	449	0	179	1210	4.02	4.02	4.02	4.02	3	0.20	0.03	0.21	0.00	0.00	22.3
38	339	4363	652	264	0	40	1891	4.02	4.02	4.02	4.02	3	0.31	0.02	0.12	0.00	0.00	22.3
39	339	4041	-311	274	0	134	1155	4.02	4.02	4.02	4.02	3	0.19	0.01	0.06	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	396	3233	-846	197	0	-47	1156	4.02	4.02	4.02	4.02	3	0.18	0.02	0.15	0.00	0.00	22.3
2	396	2621	-873	154	0	-36	766	4.02	4.02	4.02	4.02	2	0.13	0.03	0.16	0.00	0.00	22.3
3	396	2550	-873	148	0	-36	767	4.02	4.02	4.02	4.02	2	0.13	0.03	0.16	0.00	0.00	22.3
4	396	2424	-430	155	0	-37	961	4.02	4.02	4.02	4.02	2	0.16	0.01	0.08	0.00	0.00	22.3
5	396	2352	-430	148	0	-36	962	4.02	4.02	4.02	4.02	2	0.16	0.01	0.08	0.00	0.00	22.3
6	396	2636	-717	162	0	-36	862	4.02	4.02	4.02	4.02	2	0.14	0.02	0.13	0.00	0.00	22.3
7	396	2397	-719	140	0	-36	864	4.02	4.02	4.02	4.02	2	0.14	0.02	0.13	0.00	0.00	22.3
8	396	2577	-584	162	0	-37	888	4.02	4.02	4.02	4.02	2	0.15	0.02	0.10	0.00	0.00	22.3
9	396	2338	-586	140	0	-36	891	4.02	4.02	4.02	4.02	2	0.15	0.02	0.10	0.00	0.00	22.3
10	396	2621	-873	154	0	-36	766	4.02	4.02	4.02	4.02	2	0.13	0.03	0.16	0.00	0.00	22.3
11	396	2550	-873	148	0	-36	767	4.02	4.02	4.02	4.02	2	0.13	0.03	0.16	0.00	0.00	22.3
12	396	2424	-430	155	0	-37	961	4.02	4.02	4.02	4.02	2	0.16	0.01	0.08	0.00	0.00	22.3
13	396	2352	-430	148	0	-36	962	4.02	4.02	4.02	4.02	2	0.16	0.01	0.08	0.00	0.00	22.3
14	396	2636	-717	162	0	-36	862	4.02	4.02	4.02	4.02	2	0.14	0.02	0.13	0.00	0.00	22.3
15	396	2397	-719	140	0	-36	864	4.02	4.02	4.02	4.02	2	0.14	0.02	0.13	0.00	0.00	22.3
16	396	2577	-584	162	0	-37	888	4.02	4.02	4.02	4.02	2	0.15	0.02	0.10	0.00	0.00	22.3
17	396	2338	-586	140	0	-36	891	4.02	4.02	4.02	4.02	2	0.15	0.02	0.10	0.00	0.00	22.3
18	396	5890	-1274	488	0	-103	897	4.02	4.02	4.02	4.02	3	0.16	0.04	0.23	0.00	0.00	22.3
19	396	5373	-159	377	0	-124	1518	4.02	4.02	4.02	4.02	3	0.26	0.01	0.06	0.00	0.00	22.3
20	396	5180	-737	383	0	-71	1150	4.02	4.02	4.02	4.02	3	0.19	0.02	0.13	0.00	0.00	22.3
37	396	5224	-1691	449	0	-74	-1075	4.02	4.02	4.02	4.02	3	0.18	0.05	0.30	0.00	0.00	22.3
38	396	4363	167	264	0	-109	1891	4.02	4.02	4.02	4.02	3	0.31	0.01	0.04	0.00	0.00	22.3
39	396	4041	-796	274	0	-21	1155	4.02	4.02	4.02	4.02	3	0.19	0.02	0.14	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	452	3233	-1339	197	0	-158	808	4.02	4.02	4.02	4.02	3	0.13	0.04	0.24	0.00	0.00	22.3
2	452	2621	-1252	154	0	-123	-909	4.02	4.02	4.02	4.02	2	0.15	0.04	0.22	0.00	0.00	22.3
3	452	2550	-1252	148	0	-119	-909	4.02	4.02	4.02	4.02	2	0.15	0.04	0.22	0.00	0.00	22.3
4	452	2424	-809	155	0	-124	884	4.02	4.02	4.02	4.02	2	0.14	0.02	0.14	0.00	0.00	22.3
5	452	2352	-809	148	0	-120	884	4.02	4.02	4.02	4.02	2	0.14	0.02	0.14	0.00	0.00	22.3
6	452	2636	-1096	162	0	-128	-567	4.02	4.02	4.02	4.02	2	0.09	0.03	0.20	0.00	0.00	22.3
7	452	2397	-1098	140	0	-115	-569	4.02	4.02	4.02	4.02	2	0.09	0.03	0.20	0.00	0.00	22.3
8	452	2577	-963	162	0	-128	700	4.02	4.02	4.02	4.02	2	0.12	0.03	0.17	0.00	0.00	22.3
9	452	2338	-965	140	0	-115	701	4.02	4.02	4.02	4.02	2	0.11	0.03	0.17	0.00	0.00	22.3
10	452	2621	-1252	154	0	-123	-909	4.02	4.02	4.02	4.02	2	0.15	0.04	0.22	0.00	0.00	22.3
11	452	2550	-1252	148	0	-119	-909	4.02	4.02	4.02	4.02	2	0.15	0.04	0.22	0.00	0.00	22.3
12	452	2424	-809	155	0	-124	884	4.02	4.02	4.02	4.02	2	0.14	0.02	0.14	0.00	0.00	22.3
13	452	2352	-809	148	0	-120	884	4.02	4.02	4.02	4.02	2	0.14	0.02	0.14	0.00	0.00	22.3
14	452	2636	-1096	162	0	-128	-567	4.02	4.02	4.02	4.02	2	0.09	0.03	0.20	0.00	0.00	22.3
15	452	2397	-1098	140	0	-115	-569	4.02	4.02	4.02	4.02	2	0.09	0.03	0.20	0.00	0.00	22.3
16	452	2577	-963	162	0	-128	700	4.02	4.02	4.02	4.02	2	0.12	0.03	0.17	0.00	0.00	22.3

17	452	2338	-965	140	0	-115	701	4.02	4.02	4.02	4.02	2	0.11	0.03	0.17	0.00	0.00	22.3
18	452	5890	-1767	488	0	-379	-1501	4.02	4.02	4.02	4.02	3	0.26	0.05	0.31	0.00	0.00	22.3
19	452	5373	-652	377	0	-337	1518	4.02	4.02	4.02	4.02	3	0.26	0.02	0.12	0.00	0.00	22.3
20	452	5180	-1230	383	0	-287	932	4.02	4.02	4.02	4.02	3	0.16	0.04	0.22	0.00	0.00	22.3
37	452	5224	-2184	449	0	-328	-2418	4.02	4.02	4.02	4.02	3	0.41	0.06	0.39	0.00	0.00	22.3
38	452	4363	-326	264	0	-259	1891	4.02	4.02	4.02	4.02	3	0.31	0.01	0.06	0.00	0.00	22.3
39	452	4041	-1289	274	0	-176	867	4.02	4.02	4.02	4.02	3	0.14	0.04	0.23	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	508	3233	-1839	197	0	-269	-1699	4.02	4.02	4.02	4.02	3	0.27	0.05	0.33	0.00	0.00	22.3
2	508	2621	-1636	154	0	-210	-1919	4.02	4.02	4.02	4.02	2	0.32	0.05	0.29	0.00	0.00	22.3
3	508	2550	-1637	148	0	-202	-1920	4.02	4.02	4.02	4.02	2	0.32	0.05	0.29	0.00	0.00	22.3
4	508	2424	-1193	155	0	-212	-694	4.02	4.02	4.02	4.02	2	0.11	0.03	0.21	0.00	0.00	22.3
5	508	2352	-1194	148	0	-204	-695	4.02	4.02	4.02	4.02	2	0.11	0.03	0.21	0.00	0.00	22.3
6	508	2636	-1480	162	0	-220	-1489	4.02	4.02	4.02	4.02	2	0.25	0.04	0.26	0.00	0.00	22.3
7	508	2397	-1483	140	0	-194	-1492	4.02	4.02	4.02	4.02	2	0.24	0.04	0.26	0.00	0.00	22.3
8	508	2577	-1347	162	0	-220	-1122	4.02	4.02	4.02	4.02	2	0.18	0.04	0.24	0.00	0.00	22.3
9	508	2338	-1350	140	0	-194	-1125	4.02	4.02	4.02	4.02	2	0.18	0.04	0.24	0.00	0.00	22.3
10	508	2621	-1636	154	0	-210	-1919	4.02	4.02	4.02	4.02	2	0.32	0.05	0.29	0.00	0.00	22.3
11	508	2550	-1637	148	0	-202	-1920	4.02	4.02	4.02	4.02	2	0.32	0.05	0.29	0.00	0.00	22.3
12	508	2424	-1193	155	0	-212	-694	4.02	4.02	4.02	4.02	2	0.11	0.03	0.21	0.00	0.00	22.3
13	508	2352	-1194	148	0	-204	-695	4.02	4.02	4.02	4.02	2	0.11	0.03	0.21	0.00	0.00	22.3
14	508	2636	-1480	162	0	-220	-1489	4.02	4.02	4.02	4.02	2	0.25	0.04	0.26	0.00	0.00	22.3
15	508	2397	-1483	140	0	-194	-1492	4.02	4.02	4.02	4.02	2	0.24	0.04	0.26	0.00	0.00	22.3
16	508	2577	-1347	162	0	-220	-1122	4.02	4.02	4.02	4.02	2	0.18	0.04	0.24	0.00	0.00	22.3
17	508	2338	-1350	140	0	-194	-1125	4.02	4.02	4.02	4.02	2	0.18	0.04	0.24	0.00	0.00	22.3
18	508	5890	-2267	488	0	-655	-2893	4.02	4.02	4.02	4.02	3	0.50	0.07	0.40	0.00	0.00	22.3
19	508	5373	-1152	377	0	-551	1363	4.02	4.02	4.02	4.02	3	0.23	0.03	0.21	0.00	0.00	22.3
20	508	5180	-1730	383	0	-504	-1403	4.02	4.02	4.02	4.02	3	0.24	0.05	0.31	0.00	0.00	22.3
37	508	5224	-2684	449	0	-582	-4046	4.02	4.02	4.02	4.02	3	0.69	0.08	0.48	0.00	0.00	22.3
38	508	4363	-826	264	0	-408	1891	4.02	4.02	4.02	4.02	3	0.31	0.02	0.15	0.00	0.00	22.3
39	508	4041	-1789	274	0	-330	-1561	4.02	4.02	4.02	4.02	3	0.25	0.05	0.32	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	565	3233	-2346	197	0	-380	-1950	4.02	4.02	4.02	4.02	3	0.31	0.07	0.42	0.00	0.00	22.3
2	565	2621	-2026	154	0	-297	-2125	4.02	4.02	4.02	4.02	2	0.35	0.06	0.36	0.00	0.00	22.3
3	565	2550	-2027	148	0	-286	-2126	4.02	4.02	4.02	4.02	2	0.35	0.06	0.36	0.00	0.00	22.3
4	565	2424	-1583	155	0	-299	-874	4.02	4.02	4.02	4.02	2	0.14	0.05	0.28	0.00	0.00	22.3
5	565	2352	-1584	148	0	-288	-875	4.02	4.02	4.02	4.02	2	0.14	0.05	0.28	0.00	0.00	22.3
6	565	2636	-1870	162	0	-311	-1686	4.02	4.02	4.02	4.02	2	0.28	0.05	0.33	0.00	0.00	22.3
7	565	2397	-1873	140	0	-273	-1689	4.02	4.02	4.02	4.02	2	0.28	0.05	0.33	0.00	0.00	22.3
8	565	2577	-1737	162	0	-312	-1311	4.02	4.02	4.02	4.02	2	0.22	0.05	0.31	0.00	0.00	22.3
9	565	2338	-1740	140	0	-274	-1314	4.02	4.02	4.02	4.02	2	0.21	0.05	0.31	0.00	0.00	22.3
10	565	2621	-2026	154	0	-297	-2125	4.02	4.02	4.02	4.02	2	0.35	0.06	0.36	0.00	0.00	22.3
11	565	2550	-2027	148	0	-286	-2126	4.02	4.02	4.02	4.02	2	0.35	0.06	0.36	0.00	0.00	22.3
12	565	2424	-1583	155	0	-299	-874	4.02	4.02	4.02	4.02	2	0.14	0.05	0.28	0.00	0.00	22.3
13	565	2352	-1584	148	0	-288	-875	4.02	4.02	4.02	4.02	2	0.14	0.05	0.28	0.00	0.00	22.3
14	565	2636	-1870	162	0	-311	-1686	4.02	4.02	4.02	4.02	2	0.28	0.05	0.33	0.00	0.00	22.3
15	565	2397	-1873	140	0	-273	-1689	4.02	4.02	4.02	4.02	2	0.28	0.05	0.33	0.00	0.00	22.3
16	565	2577	-1737	162	0	-312	-1311	4.02	4.02	4.02	4.02	2	0.22	0.05	0.31	0.00	0.00	22.3
17	565	2338	-1740	140	0	-274	-1314	4.02	4.02	4.02	4.02	2	0.21	0.05	0.31	0.00	0.00	22.3
18	565	5890	-2774	488	0	-930	-3169	4.02	4.02	4.02	4.02	3	0.55	0.08	0.49	0.00	0.00	22.3
19	565	5373	-1659	377	0	-764	-14	4.02	4.02	4.02	4.02	3	0.22	0.05	0.30	0.00	0.00	22.3
20	565	5180	-2237	383	0	-720	-1647	4.02	4.02	4.02	4.02	3	0.28	0.06	0.40	0.00	0.00	22.3
37	565	5224	-3191	449	0	-835	-4347	4.02	4.02	4.02	4.02	3	0.74	0.09	0.57	0.00	0.00	22.3
38	565	4363	-1333	264	0	-558	1587	4.02	4.02	4.02	4.02	3	0.26	0.04	0.24	0.00	0.00	22.3
39	565	4041	-2296	274	0	-485	-1809	4.02	4.02	4.02	4.02	3	0.29	0.07	0.41	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

Nome travata: **Trave_402_IP1** Descrizione: **Trave_4 1-10-15-20-25**
ASTA NUM. 7 NI 297 NF 271 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y Permanente qy tot.
qy medio: 375.00 272.00 647.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	3084	2454	-193	0	-332	-2280	4.02	4.02	4.02	4.02	3	0.36	0.07	0.44	0.00	0.00	22.3
2	0	3201	1679	-152	0	-263	-1159	4.02	4.02	4.02	4.02	2	0.19	0.05	0.30	0.00	0.00	22.3
3	0	3121	1681	-143	0	-245	-1165	4.02	4.02	4.02	4.02	2	0.20	0.05	0.30	0.00	0.00	22.3
4	0	1624	2093	-154	0	-266	-2343	4.02	4.02	4.02	4.02	2	0.37	0.06	0.37	0.00	0.00	22.3
5	0	1544	2096	-145	0	-247	-2349	4.02	4.02	4.02	4.02	2	0.37	0.06	0.37	0.00	0.00	22.3
6	0	2742	1821	-162	0	-285	-1566	4.02	4.02	4.02	4.02	2	0.26	0.05	0.32	0.00	0.00	22.3
7	0	2476	1829	-134	0	-225	-1587	4.02	4.02	4.02	4.02	2	0.26	0.05	0.33	0.00	0.00	22.3
8	0	2269	1946	-163	0	-286	-1921	4.02	4.02	4.02	4.02	2	0.31	0.06	0.35	0.00	0.00	22.3
9	0	2003	1953	-135	0	-225	-1942	4.02	4.02	4.02	4.02	2	0.31	0.06	0.35	0.00	0.00	22.3
10	0	3201	1679	-152	0	-263	-1159	4.02	4.02	4.02	4.02	2	0.19	0.05	0.30	0.00	0.00	22.3
11	0	3121	1681	-143	0	-245	-1165	4.02	4.02	4.02	4.02	2	0.20	0.05	0.30	0.00	0.00	22.3
12	0	1624	2093	-154	0	-266	-2343	4.02	4.02	4.02	4.02	2	0.37	0.06	0.37	0.00	0.00	22.3
13	0	1544	2096	-145	0	-247	-2349	4.02	4.02	4.02	4.02	2	0.37	0.06	0.37	0.00	0.00	22.3
14	0	2742	1821	-162	0	-285	-1566	4.02	4.02	4.02	4.02	2	0.26	0.05	0.32	0.00	0.00	22.3
15	0	2476	1829	-134	0	-225	-1587	4.02	4.02	4.02	4.02	2	0.26	0.05	0.33	0.00	0.00	22.3
16	0	2269	1946	-163	0	-286	-1921	4.02	4.02	4.02	4.02	2	0.31	0.06	0.35	0.00	0.00	22.3
17	0	2003	1953	-135	0	-225	-1942	4.02	4.02	4.02	4.02	2	0.31	0.06	0.35	0.00	0.00	22.3
18	0	7335	1945	-406	0	-722	-833	4.02	4.02	4.02	4.02	3	0.22	0.06	0.35	0.00	0.00	22.3
19	0	3234	3038	-451	0	-764	-3948	4.02	4.02	4.02	4.02	3	0.63	0.09	0.54	0.00	0.00	22.3
20	0	4858	2487	-378	0	-614	-2376	4.02	4.02	4.02	4.02	3	0.40	0.07	0.44	0.00	0.00	22.3
37	0	7929	1569	-315	0	-575	1035	4.02	4.02	4.02	4.02	3	0.19	0.05	0.28	0.00	0.00	22.3
38	0	1095	3390	-390	0	-646	-4951	4.02	4.02	4.02	4.02	3	0.73	0.10	0.60	0.00	0.00	22.3
39	0	3801	2472	-269	0	-395	-2331	4.02	4.02	4.02	4.02	3	0.38	0.07	0.44	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	57	3084	1947	-193	0	-223	-2023	4.02	4.02	4.02	4.02	3	0.32	0.06	0.35	0.00	0.00	22.3
2	57	3201	1289	-152	0	-178	-973	4.02	4.02	4.02	4.02	2	0.16	0.04	0.23	0.00	0.00	22.3
3	57	3121	1291	-143	0	-164	-979	4.02	4.02	4.02	4.02	2	0.16	0.04	0.23	0.00	0.00	22.3
4	57	1624	1703	-154	0	-179	-2133	4.02	4.02	4.02	4.02	2	0.34	0.05	0.30	0.00	0.00	22.3
5	57	1544	1706	-145	0	-165	-2139	4.02	4.02	4.02	4.02	2	0.34	0.05	0.30	0.00	0.00	22.3
6	57	2742	1431	-162	0	-193	-1372	4.02	4.02	4.02	4.02	2	0.23	0.04	0.25	0.00	0.00	22.3
7	57	2476	1439	-134	0	-149	-1393	4.02	4.02	4.02	4.02	2	0.23	0.04	0.26	0.00	0.00	22.3
8	57	2269	1556	-163	0	-194	-1720	4.02	4.02	4.02	4.02	2	0.28	0.05	0.28	0.00	0.00	22.3

9	57	2003	1563	-135	0	-149	-1740	4.02	4.02	4.02	4.02	2	0.28	0.05	0.28	0.00	0.00	22.3
10	57	3201	1289	-152	0	-178	-973	4.02	4.02	4.02	4.02	2	0.16	0.04	0.23	0.00	0.00	22.3
11	57	3121	1291	-143	0	-164	-979	4.02	4.02	4.02	4.02	2	0.16	0.04	0.23	0.00	0.00	22.3
12	57	1624	1703	-154	0	-179	-2133	4.02	4.02	4.02	4.02	2	0.34	0.05	0.30	0.00	0.00	22.3
13	57	1544	1706	-145	0	-165	-2139	4.02	4.02	4.02	4.02	2	0.34	0.05	0.30	0.00	0.00	22.3
14	57	2742	1431	-162	0	-193	-1372	4.02	4.02	4.02	4.02	2	0.23	0.04	0.25	0.00	0.00	22.3
15	57	2476	1439	-134	0	-149	-1393	4.02	4.02	4.02	4.02	2	0.23	0.04	0.26	0.00	0.00	22.3
16	57	2269	1556	-163	0	-194	-1720	4.02	4.02	4.02	4.02	2	0.28	0.05	0.28	0.00	0.00	22.3
17	57	2003	1563	-135	0	-149	-1740	4.02	4.02	4.02	4.02	2	0.28	0.05	0.28	0.00	0.00	22.3
18	57	7335	1438	-406	0	-492	851	4.02	4.02	4.02	4.02	3	0.16	0.04	0.26	0.00	0.00	22.3
19	57	3234	2531	-451	0	-510	-3657	4.02	4.02	4.02	4.02	3	0.58	0.07	0.45	0.00	0.00	22.3
20	57	4858	1980	-378	0	-400	-2117	4.02	4.02	4.02	4.02	3	0.35	0.06	0.35	0.00	0.00	22.3
37	57	7929	1062	-315	0	-397	1521	4.02	4.02	4.02	4.02	3	0.28	0.03	0.19	0.00	0.00	22.3
38	57	1095	2883	-390	0	-426	-4639	4.02	4.02	4.02	4.02	3	0.69	0.08	0.51	0.00	0.00	22.3
39	57	3801	1965	-269	0	-243	-2073	4.02	4.02	4.02	4.02	3	0.33	0.06	0.35	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	113	3084	1447	-193	0	-114	-812	4.02	4.02	4.02	4.02	3	0.13	0.04	0.26	0.00	0.00	22.3
2	113	3201	904	-152	0	-92	756	4.02	4.02	4.02	4.02	2	0.13	0.03	0.16	0.00	0.00	22.3
3	113	3121	907	-143	0	-83	754	4.02	4.02	4.02	4.02	2	0.13	0.03	0.16	0.00	0.00	22.3
4	113	1624	1319	-154	0	-92	-1085	4.02	4.02	4.02	4.02	2	0.17	0.04	0.23	0.00	0.00	22.3
5	113	1544	1321	-145	0	-83	-1089	4.02	4.02	4.02	4.02	2	0.17	0.04	0.24	0.00	0.00	22.3
6	113	2742	1047	-162	0	-102	582	4.02	4.02	4.02	4.02	2	0.10	0.03	0.19	0.00	0.00	22.3
7	113	2476	1055	-134	0	-73	574	4.02	4.02	4.02	4.02	2	0.09	0.03	0.19	0.00	0.00	22.3
8	113	2269	1171	-163	0	-102	-755	4.02	4.02	4.02	4.02	2	0.12	0.03	0.21	0.00	0.00	22.3
9	113	2003	1179	-135	0	-73	-771	4.02	4.02	4.02	4.02	2	0.12	0.03	0.21	0.00	0.00	22.3
10	113	3201	904	-152	0	-92	756	4.02	4.02	4.02	4.02	2	0.13	0.03	0.16	0.00	0.00	22.3
11	113	3121	907	-143	0	-83	754	4.02	4.02	4.02	4.02	2	0.13	0.03	0.16	0.00	0.00	22.3
12	113	1624	1319	-154	0	-92	-1085	4.02	4.02	4.02	4.02	2	0.17	0.04	0.23	0.00	0.00	22.3
13	113	1544	1321	-145	0	-83	-1089	4.02	4.02	4.02	4.02	2	0.17	0.04	0.24	0.00	0.00	22.3
14	113	2742	1047	-162	0	-102	582	4.02	4.02	4.02	4.02	2	0.10	0.03	0.19	0.00	0.00	22.3
15	113	2476	1055	-134	0	-73	574	4.02	4.02	4.02	4.02	2	0.09	0.03	0.19	0.00	0.00	22.3
16	113	2269	1171	-163	0	-102	-755	4.02	4.02	4.02	4.02	2	0.12	0.03	0.21	0.00	0.00	22.3
17	113	2003	1179	-135	0	-73	-771	4.02	4.02	4.02	4.02	2	0.12	0.03	0.21	0.00	0.00	22.3
18	113	7335	938	-406	0	-263	1269	4.02	4.02	4.02	4.02	3	0.23	0.03	0.17	0.00	0.00	22.3
19	113	3234	2031	-451	0	-255	-2115	4.02	4.02	4.02	4.02	3	0.34	0.06	0.36	0.00	0.00	22.3
20	113	4858	1480	-378	0	-186	-886	4.02	4.02	4.02	4.02	3	0.15	0.04	0.26	0.00	0.00	22.3
37	113	7929	562	-315	0	-219	1620	4.02	4.02	4.02	4.02	3	0.30	0.02	0.10	0.00	0.00	22.3
38	113	1095	2383	-390	0	-206	-2899	4.02	4.02	4.02	4.02	3	0.43	0.07	0.42	0.00	0.00	22.3
39	113	3801	1465	-269	0	-91	-851	4.02	4.02	4.02	4.02	3	0.14	0.04	0.26	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	170	3084	954	-193	0	-5	1082	4.02	4.02	4.02	4.02	3	0.17	0.03	0.17	0.00	0.00	22.3
2	170	3201	525	-152	0	-6	893	4.02	4.02	4.02	4.02	2	0.15	0.02	0.09	0.00	0.00	22.3
3	170	3121	528	-143	0	-2	893	4.02	4.02	4.02	4.02	2	0.15	0.02	0.09	0.00	0.00	22.3
4	170	1624	940	-154	0	-5	697	4.02	4.02	4.02	4.02	2	0.11	0.03	0.17	0.00	0.00	22.3
5	170	1544	942	-145	0	-1	696	4.02	4.02	4.02	4.02	2	0.11	0.03	0.17	0.00	0.00	22.3
6	170	2742	668	-162	0	-10	870	4.02	4.02	4.02	4.02	2	0.14	0.02	0.12	0.00	0.00	22.3
7	170	2476	676	-134	0	3	871	4.02	4.02	4.02	4.02	2	0.14	0.02	0.12	0.00	0.00	22.3
8	170	2269	792	-163	0	-10	793	4.02	4.02	4.02	4.02	2	0.13	0.02	0.14	0.00	0.00	22.3
9	170	2003	800	-135	0	3	789	4.02	4.02	4.02	4.02	2	0.13	0.02	0.14	0.00	0.00	22.3
10	170	3201	525	-152	0	-6	893	4.02	4.02	4.02	4.02	2	0.15	0.02	0.09	0.00	0.00	22.3
11	170	3121	528	-143	0	-2	893	4.02	4.02	4.02	4.02	2	0.15	0.02	0.09	0.00	0.00	22.3
12	170	1624	940	-154	0	-5	697	4.02	4.02	4.02	4.02	2	0.11	0.03	0.17	0.00	0.00	22.3
13	170	1544	942	-145	0	-1	696	4.02	4.02	4.02	4.02	2	0.11	0.03	0.17	0.00	0.00	22.3
14	170	2742	668	-162	0	-10	870	4.02	4.02	4.02	4.02	2	0.14	0.02	0.12	0.00	0.00	22.3
15	170	2476	676	-134	0	3	871	4.02	4.02	4.02	4.02	2	0.14	0.02	0.12	0.00	0.00	22.3
16	170	2269	792	-163	0	-10	793	4.02	4.02	4.02	4.02	2	0.13	0.02	0.14	0.00	0.00	22.3
17	170	2003	800	-135	0	3	789	4.02	4.02	4.02	4.02	2	0.13	0.02	0.14	0.00	0.00	22.3
18	170	7335	445	-406	0	-34	1299	4.02	4.02	4.02	4.02	3	0.24	0.01	0.08	0.00	0.00	22.3
19	170	3234	1538	-451	0	-0	-858	4.02	4.02	4.02	4.02	3	0.14	0.04	0.27	0.00	0.00	22.3
20	170	4858	987	-378	0	27	1059	4.02	4.02	4.02	4.02	3	0.18	0.03	0.18	0.00	0.00	22.3
37	170	7929	69	-315	0	-41	1620	4.02	4.02	4.02	4.02	3	0.30	0.01	0.05	0.00	0.00	22.3
38	170	1095	1890	-390	0	15	-1442	4.02	4.02	4.02	4.02	3	0.21	0.05	0.34	0.00	0.00	22.3
39	170	3801	972	-269	0	61	1071	4.02	4.02	4.02	4.02	3	0.17	0.03	0.17	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	226	3084	468	-193	0	105	1129	4.02	4.02	4.02	4.02	3	0.18	0.01	0.08	0.00	0.00	22.3
2	226	3201	152	-152	0	79	893	4.02	4.02	4.02	4.02	2	0.15	0.00	0.03	0.00	0.00	22.3
3	226	3121	154	-143	0	78	893	4.02	4.02	4.02	4.02	2	0.15	0.00	0.03	0.00	0.00	22.3
4	226	1624	566	-154	0	82	871	4.02	4.02	4.02	4.02	2	0.14	0.02	0.10	0.00	0.00	22.3
5	226	1544	569	-145	0	81	873	4.02	4.02	4.02	4.02	2	0.14	0.02	0.10	0.00	0.00	22.3
6	226	2742	294	-162	0	82	870	4.02	4.02	4.02	4.02	2	0.14	0.01	0.05	0.00	0.00	22.3
7	226	2476	302	-134	0	78	871	4.02	4.02	4.02	4.02	2	0.14	0.01	0.05	0.00	0.00	22.3
8	226	2269	419	-163	0	83	866	4.02	4.02	4.02	4.02	2	0.14	0.01	0.07	0.00	0.00	22.3
9	226	2003	426	-135	0	79	867	4.02	4.02	4.02	4.02	2	0.14	0.01	0.08	0.00	0.00	22.3
10	226	3201	152	-152	0	79	893	4.02	4.02	4.02	4.02	2	0.15	0.00	0.03	0.00	0.00	22.3
11	226	3121	154	-143	0	78	893	4.02	4.02	4.02	4.02	2	0.15	0.00	0.03	0.00	0.00	22.3
12	226	1624	566	-154	0	82	871	4.02	4.02	4.02	4.02	2	0.14	0.02	0.10	0.00	0.00	22.3
13	226	1544	569	-145	0	81	873	4.02	4.02	4.02	4.02	2	0.14	0.02	0.10	0.00	0.00	22.3
14	226	2742	294	-162	0	82	870	4.02	4.02	4.02	4.02	2	0.14	0.01	0.05	0.00	0.00	22.3
15	226	2476	302	-134	0	78	871	4.02	4.02	4.02	4.02	2	0.14	0.01	0.05	0.00	0.00	22.3
16	226	2269	419	-163	0	83	866	4.02	4.02	4.02	4.02	2	0.14	0.01	0.07	0.00	0.00	22.3
17	226	2003	426	-135	0	79	867	4.02	4.02	4.02	4.02	2	0.14	0.01	0.08	0.00	0.00	22.3
18	226	7335	-40	-406	0	195	1299	4.02	4.02	4.02	4.02	3	0.24	0.01	0.07	0.00	0.00	22.3
19	226	3234	1053	-451	0	255	1185	4.02	4.02	4.02	4.02	3	0.19	0.03	0.19	0.00	0.00	22.3
20	226	4858	502	-378	0	241	1128	4.02	4.02	4.02	4.02	3	0.19	0.01	0.09	0.00	0.00	22.3
37	226	7929	-416	-315	0	137	1620	4.02	4.02	4.02	4.02	3	0.30	0.01	0.07	0.00	0.00	22.3
38	226	1095	1404	-390	0	235	1156	4.02	4.02	4.02	4.02	3	0.17	0.04	0.25	0.00	0.00	22.3
39	226	3801	487	-269	0	213	1130	4.02	4.02	4.02	4.02	3	0.18	0.01	0.09	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	283	3084	-11	-193	0	214	1129	4.02	4.02	4.02	4.02	3	0.18	0.01	0.03	0.00	0.00	22.3
2	283	3201	-217	-152	0	165	893	4.02	4.02	4.02	4.02	2	0.15	0.01	0.04	0.00	0.00	22.3
3	283	3121	-214	-143	0	159	893	4.02	4.02	4.02	4.02	2	0.15	0.01	0.04	0.00	0.00	22.3
4	283	1624	198	-154	0	169	871	4.02	4.02	4.02	4.02	2	0.14	0.01	0.04	0.00	0.00	22.3
5	283	1544	200	-145	0	163	873	4.02	4.02	4.02	4.02	2	0.14	0.01	0.04	0.00	0.00	22.3
6	283	2742	-74	-162	0	173	870	4.02	4.02	4.02	4.02	2	0.14	0.01	0.03	0.00	0.00	22.3
7	283	2476	-66	-134	0	154	871	4.02	4.02	4.02	4.02	2	0.14	0.00	0.01	0.00	0.00	22.3
8	283	2269	50	-163	0	175	866	4.02	4.02	4.02	4.02	2	0.14	0.01	0.03	0.00	0.00	22.3
9	283	2003	58	-135	0	155	867	4.02	4.02	4.02	4.02	2	0.14	0.00	0.01	0.00	0.00	22.3
10	283	3201	-217	-152	0	165	893	4.02	4.02	4.02	4.02	2	0.15	0.01	0.04	0.00	0.00	22.3
11	283	3121	-214	-143	0	159	893	4.02	4.02	4.02	4.02	2	0.15	0.01	0.04	0.00	0.00	22.3
12	283	1624	198	-154	0	169	871	4.02	4.02	4.02	4.02	2	0.14	0.01	0.04	0.00	0.00	22.3
13	283	1544	200	-145	0	163	873	4.02	4.02	4.02	4.02	2	0.14	0.01	0.04	0.00	0.00	22.3
14	283	2742	-74	-162	0	173	870	4.02	4.02	4.02	4.02	2	0.14	0.01	0.03	0.00	0.00	22.3

15	283	2476	-66	-134	0	154	871	4.02	4.02	4.02	4.02	2	0.14	0.00	0.01	0.00	0.00	22.3
16	283	2269	50	-163	0	175	866	4.02	4.02	4.02	4.02	2	0.14	0.01	0.03	0.00	0.00	22.3
17	283	2003	58	-135	0	155	867	4.02	4.02	4.02	4.02	2	0.14	0.00	0.01	0.00	0.00	22.3
18	283	7335	-519	-406	0	425	1299	4.02	4.02	4.02	4.02	3	0.24	0.02	0.09	0.00	0.00	22.3
19	283	3234	574	-451	0	509	1302	4.02	4.02	4.02	4.02	3	0.21	0.02	0.10	0.00	0.00	22.3
20	283	4858	23	-378	0	454	1128	4.02	4.02	4.02	4.02	3	0.19	0.01	0.06	0.00	0.00	22.3
37	283	7929	-895	-315	0	315	1603	4.02	4.02	4.02	4.02	3	0.30	0.03	0.16	0.00	0.00	22.3
38	283	1095	925	-390	0	456	1571	4.02	4.02	4.02	4.02	3	0.23	0.03	0.16	0.00	0.00	22.3
39	283	3801	8	-269	0	364	1130	4.02	4.02	4.02	4.02	3	0.18	0.01	0.04	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	339	3084	-482	-193	0	323	1129	4.02	4.02	4.02	4.02	3	0.18	0.01	0.09	0.00	0.00	22.3
2	339	3201	-580	-152	0	251	893	4.02	4.02	4.02	4.02	2	0.15	0.02	0.10	0.00	0.00	22.3
3	339	3121	-577	-143	0	240	893	4.02	4.02	4.02	4.02	2	0.15	0.02	0.10	0.00	0.00	22.3
4	339	1624	-165	-154	0	256	871	4.02	4.02	4.02	4.02	2	0.14	0.00	0.03	0.00	0.00	22.3
5	339	1544	-163	-145	0	246	873	4.02	4.02	4.02	4.02	2	0.14	0.00	0.03	0.00	0.00	22.3
6	339	2742	-437	-162	0	265	870	4.02	4.02	4.02	4.02	2	0.14	0.01	0.08	0.00	0.00	22.3
7	339	2476	-429	-134	0	230	871	4.02	4.02	4.02	4.02	2	0.14	0.01	0.08	0.00	0.00	22.3
8	339	2269	-313	-163	0	267	866	4.02	4.02	4.02	4.02	2	0.14	0.01	0.06	0.00	0.00	22.3
9	339	2003	-305	-135	0	231	867	4.02	4.02	4.02	4.02	2	0.14	0.01	0.05	0.00	0.00	22.3
10	339	3201	-580	-152	0	251	893	4.02	4.02	4.02	4.02	2	0.15	0.02	0.10	0.00	0.00	22.3
11	339	3121	-577	-143	0	240	893	4.02	4.02	4.02	4.02	2	0.15	0.02	0.10	0.00	0.00	22.3
12	339	1624	-165	-154	0	256	871	4.02	4.02	4.02	4.02	2	0.14	0.00	0.03	0.00	0.00	22.3
13	339	1544	-163	-145	0	246	873	4.02	4.02	4.02	4.02	2	0.14	0.00	0.03	0.00	0.00	22.3
14	339	2742	-437	-162	0	265	870	4.02	4.02	4.02	4.02	2	0.14	0.01	0.08	0.00	0.00	22.3
15	339	2476	-429	-134	0	230	871	4.02	4.02	4.02	4.02	2	0.14	0.01	0.08	0.00	0.00	22.3
16	339	2269	-313	-163	0	267	866	4.02	4.02	4.02	4.02	2	0.14	0.01	0.06	0.00	0.00	22.3
17	339	2003	-305	-135	0	231	867	4.02	4.02	4.02	4.02	2	0.14	0.01	0.05	0.00	0.00	22.3
18	339	7335	-991	-406	0	654	1215	4.02	4.02	4.02	4.02	3	0.22	0.03	0.18	0.00	0.00	22.3
19	339	3234	102	-451	0	764	1302	4.02	4.02	4.02	4.02	3	0.21	0.01	0.07	0.00	0.00	22.3
20	339	4858	-449	-378	0	668	1128	4.02	4.02	4.02	4.02	3	0.19	0.01	0.08	0.00	0.00	22.3
37	339	7929	-1367	-315	0	493	1202	4.02	4.02	4.02	4.02	3	0.22	0.04	0.24	0.00	0.00	22.3
38	339	1095	454	-390	0	676	1616	4.02	4.02	4.02	4.02	3	0.24	0.01	0.08	0.00	0.00	22.3
39	339	3801	-464	-269	0	516	1130	4.02	4.02	4.02	4.02	3	0.18	0.01	0.08	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	396	3084	-947	-193	0	432	1064	4.02	4.02	4.02	4.02	3	0.17	0.03	0.17	0.00	0.00	22.3
2	396	3201	-937	-152	0	336	695	4.02	4.02	4.02	4.02	2	0.12	0.03	0.17	0.00	0.00	22.3
3	396	3121	-934	-143	0	321	697	4.02	4.02	4.02	4.02	2	0.12	0.03	0.17	0.00	0.00	22.3
4	396	1624	-522	-154	0	343	871	4.02	4.02	4.02	4.02	2	0.14	0.02	0.09	0.00	0.00	22.3
5	396	1544	-520	-145	0	328	873	4.02	4.02	4.02	4.02	2	0.14	0.02	0.09	0.00	0.00	22.3
6	396	2742	-794	-162	0	357	779	4.02	4.02	4.02	4.02	2	0.13	0.02	0.14	0.00	0.00	22.3
7	396	2476	-786	-134	0	305	785	4.02	4.02	4.02	4.02	2	0.13	0.02	0.14	0.00	0.00	22.3
8	396	2269	-670	-163	0	359	852	4.02	4.02	4.02	4.02	2	0.14	0.02	0.12	0.00	0.00	22.3
9	396	2003	-662	-135	0	307	859	4.02	4.02	4.02	4.02	2	0.14	0.02	0.12	0.00	0.00	22.3
10	396	3201	-937	-152	0	336	695	4.02	4.02	4.02	4.02	2	0.12	0.03	0.17	0.00	0.00	22.3
11	396	3121	-934	-143	0	321	697	4.02	4.02	4.02	4.02	2	0.12	0.03	0.17	0.00	0.00	22.3
12	396	1624	-522	-154	0	343	871	4.02	4.02	4.02	4.02	2	0.14	0.02	0.09	0.00	0.00	22.3
13	396	1544	-520	-145	0	328	873	4.02	4.02	4.02	4.02	2	0.14	0.02	0.09	0.00	0.00	22.3
14	396	2742	-794	-162	0	357	779	4.02	4.02	4.02	4.02	2	0.13	0.02	0.14	0.00	0.00	22.3
15	396	2476	-786	-134	0	305	785	4.02	4.02	4.02	4.02	2	0.13	0.02	0.14	0.00	0.00	22.3
16	396	2269	-670	-163	0	359	852	4.02	4.02	4.02	4.02	2	0.14	0.02	0.12	0.00	0.00	22.3
17	396	2003	-662	-135	0	307	859	4.02	4.02	4.02	4.02	2	0.14	0.02	0.12	0.00	0.00	22.3
18	396	7335	-1455	-406	0	883	759	4.02	4.02	4.02	4.02	3	0.27	0.04	0.26	0.00	0.00	22.3
19	396	3234	-362	-451	0	1019	1302	4.02	4.02	4.02	4.02	3	0.27	0.01	0.07	0.00	0.00	22.3
20	396	4858	-913	-378	0	881	1084	4.02	4.02	4.02	4.02	3	0.25	0.03	0.16	0.00	0.00	22.3
37	396	7929	-1831	-315	0	671	-1321	4.02	4.02	4.02	4.02	3	0.25	0.05	0.33	0.00	0.00	22.3
38	396	1095	-11	-390	0	897	1616	4.02	4.02	4.02	4.02	3	0.24	0.01	0.06	0.00	0.00	22.3
39	396	3801	-928	-269	0	668	1077	4.02	4.02	4.02	4.02	3	0.18	0.03	0.17	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	452	3084	-1405	-193	0	541	-791	4.02	4.02	4.02	4.02	3	0.14	0.04	0.25	0.00	0.00	22.3
2	452	3201	-1289	-152	0	422	-1061	4.02	4.02	4.02	4.02	2	0.18	0.04	0.23	0.00	0.00	22.3
3	452	3121	-1286	-143	0	402	-1055	4.02	4.02	4.02	4.02	2	0.18	0.04	0.23	0.00	0.00	22.3
4	452	1624	-874	-154	0	430	724	4.02	4.02	4.02	4.02	2	0.13	0.03	0.16	0.00	0.00	22.3
5	452	1544	-872	-145	0	410	728	4.02	4.02	4.02	4.02	2	0.12	0.03	0.16	0.00	0.00	22.3
6	452	2742	-1146	-162	0	449	-752	4.02	4.02	4.02	4.02	2	0.14	0.03	0.20	0.00	0.00	22.3
7	452	2476	-1138	-134	0	381	-734	4.02	4.02	4.02	4.02	2	0.12	0.03	0.20	0.00	0.00	22.3
8	452	2269	-1022	-163	0	451	552	4.02	4.02	4.02	4.02	2	0.13	0.03	0.18	0.00	0.00	22.3
9	452	2003	-1014	-135	0	383	563	4.02	4.02	4.02	4.02	2	0.11	0.03	0.18	0.00	0.00	22.3
10	452	3201	-1289	-152	0	422	-1061	4.02	4.02	4.02	4.02	2	0.18	0.04	0.23	0.00	0.00	22.3
11	452	3121	-1286	-143	0	402	-1055	4.02	4.02	4.02	4.02	2	0.18	0.04	0.23	0.00	0.00	22.3
12	452	1624	-874	-154	0	430	724	4.02	4.02	4.02	4.02	2	0.13	0.03	0.16	0.00	0.00	22.3
13	452	1544	-872	-145	0	410	728	4.02	4.02	4.02	4.02	2	0.12	0.03	0.16	0.00	0.00	22.3
14	452	2742	-1146	-162	0	449	-752	4.02	4.02	4.02	4.02	2	0.14	0.03	0.20	0.00	0.00	22.3
15	452	2476	-1138	-134	0	381	-734	4.02	4.02	4.02	4.02	2	0.12	0.03	0.20	0.00	0.00	22.3
16	452	2269	-1022	-163	0	451	552	4.02	4.02	4.02	4.02	2	0.13	0.03	0.18	0.00	0.00	22.3
17	452	2003	-1014	-135	0	383	563	4.02	4.02	4.02	4.02	2	0.11	0.03	0.18	0.00	0.00	22.3
18	452	7335	-1913	-406	0	1112	-1898	4.02	4.02	4.02	4.02	3	0.35	0.06	0.34	0.00	0.00	22.3
19	452	3234	-820	-451	0	1274	1302	4.02	4.02	4.02	4.02	3	0.34	0.02	0.15	0.00	0.00	22.3
20	452	4858	-1371	-378	0	1095	-718	4.02	4.02	4.02	4.02	3	0.31	0.04	0.24	0.00	0.00	22.3
37	452	7929	-2289	-315	0	849	-2717	4.02	4.02	4.02	4.02	3	0.51	0.07	0.41	0.00	0.00	22.3
38	452	1095	-469	-390	0	1117	1616	4.02	4.02	4.02	4.02	3	0.28	0.01	0.08	0.00	0.00	22.3
39	452	3801	-1386	-269	0	820	-749	4.02	4.02	4.02	4.02	3	0.22	0.04	0.25	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	509	3084	-1855	-193	0	650	-1940	4.02	4.02	4.02	4.02	3	0.31	0.05	0.33	0.00	0.00	22.3
2	509	3201	-1636	-152	0	508	-2063	4.02	4.02	4.02	4.02	2	0.35	0.05	0.29	0.00	0.00	22.3
3	509	3121	-1633	-143	0	483	-2055	4.02	4.02	4.02	4.02	2	0.34	0.05	0.29	0.00	0.00	22.3
4	509	1624	-1221	-154	0	517	-929	4.02	4.02	4.02	4.02	2	0.15	0.04	0.22	0.00	0.00	22.3
5	509	1544	-1219	-145	0	492	-922	4.02	4.02	4.02	4.02	2	0.15	0.04	0.22	0.00	0.00	22.3
6	509	2742	-1493	-162	0	540	-1674	4.02	4.02	4.02	4.02	2	0.28	0.04	0.27	0.00	0.00	22.3
7	509	2476	-1485	-134	0	457	-1651	4.02	4.02	4.02	4.02	2	0.27	0.04	0.26	0.00	0.00	22.3
8	509	2269	-1369	-163	0	543	-1334	4.02	4.02	4.02	4.02	2	0.22	0.04	0.24	0.00	0.00	22.3
9	509	2003	-1361	-135	0	459	-1310	4.02	4.02	4.02	4.02	2	0.21	0.04	0.24	0.00	0.00	22.3
10	509	3201	-1636	-152	0	508	-2063	4.02	4.02	4.02	4.02	2	0.35	0.05	0.29	0.00	0.00	22.3
11	509	3121	-1633	-143	0	483	-2055	4.02	4.02	4.02	4.02	2	0.34	0.05	0.29	0.00	0.00	22.3
12	509	1624	-1221	-154	0	517	-929	4.02	4.02	4.02	4.02	2	0.15	0.04	0.22	0.00	0.00	22.3
13	509	1544	-1219	-145	0	492	-922	4.02	4.02	4.02	4.02	2	0.15	0.04	0.22	0.00	0.00	22.3
14	509	2742	-1493	-162	0	540	-1674	4.02	4.02	4.02	4.02	2	0.28	0.04	0.27	0.00	0.00	22.3
15	509	2476	-1485	-134	0	457	-1651	4.02	4.02	4.02	4.02	2	0.27	0.04	0.26	0.00	0.00	22.3
16	509	2269	-1369	-163	0	543	-1334	4.02	4.02	4.02	4.02	2	0.22	0.04	0.24	0.00	0.00	22.3
17	509	2003	-1361	-135	0	459	-1310	4.02	4.02	4.02	4.02	2	0.21	0.04	0.24	0.00	0.00	22.3
18	509	7335	-2364	-406	0	1342	-3335	4.02	4.02	4.02	4.02	3	0.61	0.07	0.42	0.00	0.00	22.3
19	509	3234	-1271	-451	0	1528	946	4.02	4.02	4.02	4.02	3	0.41	0.04	0.23	0.00	0.00	22.3
20	509	4858	-1822	-378	0	1308	-1848	4.02	4.02	4.02	4.02	3	0.37	0.05	0.32	0.00	0.00	22.3

37	509	7929	-2740	-315	0	1027	-4366	4.02	4.02	4.02	4.02	3	0.82	0.08	0.49	0.00	0.00	22.3
38	509	1095	-919	-390	0	1338	1554	4.02	4.02	4.02	4.02	3	0.34	0.03	0.16	0.00	0.00	22.3
39	509	3801	-1837	-269	0	972	-1888	4.02	4.02	4.02	4.02	3	0.30	0.05	0.33	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	565	3084	-2299	-193	0	759	-2175	4.02	4.02	4.02	4.02	3	0.34	0.07	0.41	0.00	0.00	22.3
2	565	3201	-1977	-152	0	593	-2256	4.02	4.02	4.02	4.02	2	0.38	0.06	0.35	0.00	0.00	22.3
3	565	3121	-1974	-143	0	564	-2248	4.02	4.02	4.02	4.02	2	0.38	0.06	0.35	0.00	0.00	22.3
4	565	1624	-1562	-154	0	604	-1097	4.02	4.02	4.02	4.02	2	0.18	0.05	0.28	0.00	0.00	22.3
5	565	1544	-1560	-145	0	574	-1090	4.02	4.02	4.02	4.02	2	0.17	0.05	0.28	0.00	0.00	22.3
6	565	2742	-1834	-162	0	632	-1858	4.02	4.02	4.02	4.02	2	0.31	0.05	0.33	0.00	0.00	22.3
7	565	2476	-1826	-134	0	532	-1835	4.02	4.02	4.02	4.02	2	0.30	0.05	0.33	0.00	0.00	22.3
8	565	2269	-1710	-163	0	635	-1511	4.02	4.02	4.02	4.02	2	0.25	0.05	0.30	0.00	0.00	22.3
9	565	2003	-1702	-135	0	536	-1487	4.02	4.02	4.02	4.02	2	0.24	0.05	0.30	0.00	0.00	22.3
10	565	3201	-1977	-152	0	593	-2256	4.02	4.02	4.02	4.02	2	0.38	0.06	0.35	0.00	0.00	22.3
11	565	3121	-1974	-143	0	564	-2248	4.02	4.02	4.02	4.02	2	0.38	0.06	0.35	0.00	0.00	22.3
12	565	1624	-1562	-154	0	604	-1097	4.02	4.02	4.02	4.02	2	0.18	0.05	0.28	0.00	0.00	22.3
13	565	1544	-1560	-145	0	574	-1090	4.02	4.02	4.02	4.02	2	0.17	0.05	0.28	0.00	0.00	22.3
14	565	2742	-1834	-162	0	632	-1858	4.02	4.02	4.02	4.02	2	0.31	0.05	0.33	0.00	0.00	22.3
15	565	2476	-1826	-134	0	532	-1835	4.02	4.02	4.02	4.02	2	0.30	0.05	0.33	0.00	0.00	22.3
16	565	2269	-1710	-163	0	635	-1511	4.02	4.02	4.02	4.02	2	0.25	0.05	0.30	0.00	0.00	22.3
17	565	2003	-1702	-135	0	536	-1487	4.02	4.02	4.02	4.02	2	0.24	0.05	0.30	0.00	0.00	22.3
18	565	7335	-2807	-406	0	1571	-3599	4.02	4.02	4.02	4.02	3	0.66	0.08	0.50	0.00	0.00	22.3
19	565	3234	-1714	-451	0	1783	-541	4.02	4.02	4.02	4.02	3	0.48	0.05	0.31	0.00	0.00	22.3
20	565	4858	-2265	-378	0	1522	-2081	4.02	4.02	4.02	4.02	3	0.43	0.07	0.40	0.00	0.00	22.3
37	565	7929	-3183	-315	0	1205	-4653	4.02	4.02	4.02	4.02	3	0.87	0.09	0.57	0.00	0.00	22.3
38	565	1095	-1363	-390	0	1558	1133	4.02	4.02	4.02	4.02	3	0.39	0.04	0.24	0.00	0.00	22.3
39	565	3801	-2280	-269	0	1124	-2122	4.02	4.02	4.02	4.02	3	0.34	0.07	0.41	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

Nome travata: **Trave_402_IP1** Descrizione: **Trave_4 1-10-15-20-25**
ASTA NUM. 8 NI 271 NF 266 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y Permanente qy tot.
qy medio: 375.00 160.00 535.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	2740	2021	150	0	-68	-1901	4.02	4.02	4.02	4.02	3	0.30	0.06	0.36	0.00	0.00	22.3
2	0	3613	1216	140	0	2	-665	4.02	4.02	4.02	4.02	2	0.11	0.04	0.22	0.00	0.00	22.3
3	0	3529	1222	130	0	-35	-677	4.02	4.02	4.02	4.02	2	0.11	0.04	0.22	0.00	0.00	22.3
4	0	687	1888	101	0	-69	-2247	4.02	4.02	4.02	4.02	2	0.35	0.05	0.34	0.00	0.00	22.3
5	0	602	1894	91	0	-106	-2259	4.02	4.02	4.02	4.02	2	0.35	0.05	0.34	0.00	0.00	22.3
6	0	2687	1444	138	0	21	-1206	4.02	4.02	4.02	4.02	2	0.20	0.04	0.26	0.00	0.00	22.3
7	0	2406	1464	105	0	-103	-1244	4.02	4.02	4.02	4.02	2	0.20	0.04	0.26	0.00	0.00	22.3
8	0	1809	1646	126	0	-1	-1680	4.02	4.02	4.02	4.02	2	0.27	0.05	0.29	0.00	0.00	22.3
9	0	1528	1666	93	0	-124	-1719	4.02	4.02	4.02	4.02	2	0.27	0.05	0.30	0.00	0.00	22.3
10	0	3613	1216	140	0	2	-665	4.02	4.02	4.02	4.02	2	0.11	0.04	0.22	0.00	0.00	22.3
11	0	3529	1222	130	0	-35	-677	4.02	4.02	4.02	4.02	2	0.11	0.04	0.22	0.00	0.00	22.3
12	0	687	1888	101	0	-69	-2247	4.02	4.02	4.02	4.02	2	0.35	0.05	0.34	0.00	0.00	22.3
13	0	602	1894	91	0	-106	-2259	4.02	4.02	4.02	4.02	2	0.35	0.05	0.34	0.00	0.00	22.3
14	0	2687	1444	138	0	21	-1206	4.02	4.02	4.02	4.02	2	0.20	0.04	0.26	0.00	0.00	22.3
15	0	2406	1464	105	0	-103	-1244	4.02	4.02	4.02	4.02	2	0.20	0.04	0.26	0.00	0.00	22.3
16	0	1809	1646	126	0	-1	-1680	4.02	4.02	4.02	4.02	2	0.27	0.05	0.29	0.00	0.00	22.3
17	0	1528	1666	93	0	-124	-1719	4.02	4.02	4.02	4.02	2	0.27	0.05	0.30	0.00	0.00	22.3
18	0	8421	1054	347	0	-108	773	4.02	4.02	4.02	4.02	3	0.15	0.03	0.19	0.00	0.00	22.3
19	0	807	2716	99	0	-601	-3696	4.02	4.02	4.02	4.02	3	0.54	0.08	0.48	0.00	0.00	22.3
20	0	4239	1908	202	0	-392	-1758	4.02	4.02	4.02	4.02	3	0.29	0.06	0.34	0.00	0.00	22.3
37	0	10290	550	405	0	146	1674	4.02	4.02	4.02	4.02	3	0.34	0.02	0.10	0.00	0.00	22.3
38	0	-2398	3319	-9	0	-675	-5073	4.02	4.02	4.02	4.02	3	0.68	0.10	0.56	0.00	0.00	22.3
39	0	3322	1973	163	0	-328	-1843	4.02	4.02	4.02	4.02	3	0.29	0.06	0.35	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	56	2740	1586	150	0	-152	-1685	4.02	4.02	4.02	4.02	3	0.26	0.05	0.28	0.00	0.00	22.3
2	56	3613	881	140	0	-77	-519	4.02	4.02	4.02	4.02	2	0.09	0.03	0.16	0.00	0.00	22.3
3	56	3529	887	130	0	-109	-531	4.02	4.02	4.02	4.02	2	0.09	0.03	0.16	0.00	0.00	22.3
4	56	687	1553	101	0	-126	-2062	4.02	4.02	4.02	4.02	2	0.32	0.05	0.28	0.00	0.00	22.3
5	56	602	1559	91	0	-157	-2073	4.02	4.02	4.02	4.02	2	0.32	0.05	0.28	0.00	0.00	22.3
6	56	2687	1109	138	0	-57	-1046	4.02	4.02	4.02	4.02	2	0.17	0.03	0.20	0.00	0.00	22.3
7	56	2406	1129	105	0	-163	-1083	4.02	4.02	4.02	4.02	2	0.18	0.03	0.20	0.00	0.00	22.3
8	56	1809	1311	126	0	-72	-1509	4.02	4.02	4.02	4.02	2	0.24	0.04	0.23	0.00	0.00	22.3
9	56	1528	1331	93	0	-177	-1547	4.02	4.02	4.02	4.02	2	0.25	0.04	0.24	0.00	0.00	22.3
10	56	3613	881	140	0	-77	-519	4.02	4.02	4.02	4.02	2	0.09	0.03	0.16	0.00	0.00	22.3
11	56	3529	887	130	0	-109	-531	4.02	4.02	4.02	4.02	2	0.09	0.03	0.16	0.00	0.00	22.3
12	56	687	1553	101	0	-126	-2062	4.02	4.02	4.02	4.02	2	0.32	0.05	0.28	0.00	0.00	22.3
13	56	602	1559	91	0	-157	-2073	4.02	4.02	4.02	4.02	2	0.32	0.05	0.28	0.00	0.00	22.3
14	56	2687	1109	138	0	-57	-1046	4.02	4.02	4.02	4.02	2	0.17	0.03	0.20	0.00	0.00	22.3
15	56	2406	1129	105	0	-163	-1083	4.02	4.02	4.02	4.02	2	0.18	0.03	0.20	0.00	0.00	22.3
16	56	1809	1311	126	0	-72	-1509	4.02	4.02	4.02	4.02	2	0.24	0.04	0.23	0.00	0.00	22.3
17	56	1528	1331	93	0	-177	-1547	4.02	4.02	4.02	4.02	2	0.25	0.04	0.24	0.00	0.00	22.3
18	56	8421	619	347	0	-305	941	4.02	4.02	4.02	4.02	3	0.18	0.02	0.11	0.00	0.00	22.3
19	56	807	2281	99	0	-656	-3440	4.02	4.02	4.02	4.02	3	0.51	0.07	0.41	0.00	0.00	22.3
20	56	4239	1473	202	0	-506	-1549	4.02	4.02	4.02	4.02	3	0.25	0.04	0.26	0.00	0.00	22.3
37	56	10290	115	405	0	-83	1674	4.02	4.02	4.02	4.02	3	0.34	0.01	0.07	0.00	0.00	22.3
38	56	-2398	2884	-9	0	-670	-4781	4.02	4.02	4.02	4.02	3	0.64	0.08	0.49	0.00	0.00	22.3
39	56	3322	1538	163	0	-420	-1630	4.02	4.02	4.02	4.02	3	0.26	0.04	0.27	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	113	2740	1160	150	0	-237	-694	4.02	4.02	4.02	4.02	3	0.11	0.03	0.21	0.00	0.00	22.3
2	113	3613	554	140	0	-156	597	4.02	4.02	4.02	4.02	2	0.10	0.02	0.10	0.00	0.00	22.3
3	113	3529	560	130	0	-182	599	4.02	4.02	4.02	4.02	2	0.10	0.02	0.10	0.00	0.00	22.3
4	113	687	1226	101	0	-182	-1112	4.02	4.02	4.02	4.02	2	0.17	0.04	0.22	0.00	0.00	22.3
5	113	602	1232	91	0	-209	-1120	4.02	4.02	4.02	4.02	2	0.17	0.04	0.22	0.00	0.00	22.3
6	113	2687	782	138	0	-135	445	4.02	4.02	4.02	4.02	2	0.07	0.02	0.14	0.00	0.00	22.3
7	113	2406	802	105	0	-222	439	4.02	4.02	4.02	4.02	2	0.07	0.02	0.14	0.00	0.00	22.3
8	113	1809	984	126	0	-143	-695	4.02	4.02	4.02	4.02	2	0.11	0.03	0.18	0.00	0.00	22.3
9	113	1528	1004	93	0	-230	-722	4.02	4.02	4.02	4.02	2	0.11	0.03	0.18	0.00	0.00	22.3
10	113	3613	554	140	0	-156	597	4.02	4.02	4.02	4.02	2	0.10	0.02	0.10	0.00	0.00	22.3
11	113	3529	560	130	0	-182	599	4.02	4.02	4.02	4.02	2	0.10	0.02	0.10	0.00	0.00	22.3
12	113	687	1226	101	0	-182	-1112	4.02	4.02	4.02	4.02	2	0.17	0.04	0.22	0.00	0.00	22.3

13	113	602	1232	91	0	-209	-1120	4.02	4.02	4.02	4.02	2	0.17	0.04	0.22	0.00	0.00	22.3
14	113	2687	782	138	0	-135	445	4.02	4.02	4.02	4.02	2	0.07	0.02	0.14	0.00	0.00	22.3
15	113	2406	802	105	0	-222	439	4.02	4.02	4.02	4.02	2	0.07	0.02	0.14	0.00	0.00	22.3
16	113	1809	984	126	0	-143	-695	4.02	4.02	4.02	4.02	2	0.11	0.03	0.18	0.00	0.00	22.3
17	113	1528	1004	93	0	-230	-722	4.02	4.02	4.02	4.02	2	0.11	0.03	0.18	0.00	0.00	22.3
18	113	8421	193	347	0	-501	941	4.02	4.02	4.02	4.02	3	0.18	0.01	0.06	0.00	0.00	22.3
19	113	807	1855	99	0	-712	-2056	4.02	4.02	4.02	4.02	3	0.30	0.05	0.33	0.00	0.00	22.3
20	113	4239	1047	202	0	-621	-622	4.02	4.02	4.02	4.02	3	0.17	0.03	0.19	0.00	0.00	22.3
37	113	10290	-311	405	0	-313	1674	4.02	4.02	4.02	4.02	3	0.34	0.01	0.07	0.00	0.00	22.3
38	113	-2398	2458	-9	0	-665	-3057	4.02	4.02	4.02	4.02	3	0.41	0.07	0.41	0.00	0.00	22.3
39	113	3322	1112	163	0	-512	-667	4.02	4.02	4.02	4.02	3	0.14	0.03	0.20	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	169	2740	744	150	0	-322	807	4.02	4.02	4.02	4.02	3	0.13	0.02	0.13	0.00	0.00	22.3
2	169	3613	233	140	0	-235	597	4.02	4.02	4.02	4.02	2	0.10	0.01	0.04	0.00	0.00	22.3
3	169	3529	239	130	0	-256	599	4.02	4.02	4.02	4.02	2	0.10	0.01	0.04	0.00	0.00	22.3
4	169	687	905	101	0	-239	568	4.02	4.02	4.02	4.02	2	0.09	0.03	0.16	0.00	0.00	22.3
5	169	602	911	91	0	-260	570	4.02	4.02	4.02	4.02	2	0.09	0.03	0.16	0.00	0.00	22.3
6	169	2687	461	138	0	-212	572	4.02	4.02	4.02	4.02	2	0.09	0.01	0.08	0.00	0.00	22.3
7	169	2406	481	105	0	-281	587	4.02	4.02	4.02	4.02	2	0.10	0.01	0.09	0.00	0.00	22.3
8	169	1809	663	126	0	-214	603	4.02	4.02	4.02	4.02	2	0.10	0.02	0.12	0.00	0.00	22.3
9	169	1528	683	93	0	-282	608	4.02	4.02	4.02	4.02	2	0.10	0.02	0.12	0.00	0.00	22.3
10	169	3613	233	140	0	-235	597	4.02	4.02	4.02	4.02	2	0.10	0.01	0.04	0.00	0.00	22.3
11	169	3529	239	130	0	-256	599	4.02	4.02	4.02	4.02	2	0.10	0.01	0.04	0.00	0.00	22.3
12	169	687	905	101	0	-239	568	4.02	4.02	4.02	4.02	2	0.09	0.03	0.16	0.00	0.00	22.3
13	169	602	911	91	0	-260	570	4.02	4.02	4.02	4.02	2	0.09	0.03	0.16	0.00	0.00	22.3
14	169	2687	461	138	0	-212	572	4.02	4.02	4.02	4.02	2	0.09	0.01	0.08	0.00	0.00	22.3
15	169	2406	481	105	0	-281	587	4.02	4.02	4.02	4.02	2	0.10	0.01	0.09	0.00	0.00	22.3
16	169	1809	663	126	0	-214	603	4.02	4.02	4.02	4.02	2	0.10	0.02	0.12	0.00	0.00	22.3
17	169	1528	683	93	0	-282	608	4.02	4.02	4.02	4.02	2	0.10	0.02	0.12	0.00	0.00	22.3
18	169	8421	-223	347	0	-697	941	4.02	4.02	4.02	4.02	3	0.22	0.01	0.06	0.00	0.00	22.3
19	169	807	1438	99	0	-768	-916	4.02	4.02	4.02	4.02	3	0.19	0.04	0.26	0.00	0.00	22.3
20	169	4239	631	202	0	-735	636	4.02	4.02	4.02	4.02	3	0.20	0.02	0.11	0.00	0.00	22.3
37	169	10290	-728	405	0	-542	1674	4.02	4.02	4.02	4.02	3	0.34	0.02	0.13	0.00	0.00	22.3
38	169	-2398	2041	-9	0	-659	-1576	4.02	4.02	4.02	4.02	3	0.21	0.06	0.34	0.00	0.00	22.3
39	169	3322	695	163	0	-604	733	4.02	4.02	4.02	4.02	3	0.16	0.02	0.12	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	226	2740	337	150	0	-406	813	4.02	4.02	4.02	4.02	3	0.13	0.01	0.06	0.00	0.00	22.3
2	226	3613	-80	140	0	-314	597	4.02	4.02	4.02	4.02	2	0.10	0.00	0.01	0.00	0.00	22.3
3	226	3529	-74	130	0	-329	599	4.02	4.02	4.02	4.02	2	0.10	0.00	0.01	0.00	0.00	22.3
4	226	687	592	101	0	-296	832	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
5	226	602	598	91	0	-311	837	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
6	226	2687	148	138	0	-290	572	4.02	4.02	4.02	4.02	2	0.09	0.00	0.03	0.00	0.00	22.3
7	226	2406	168	105	0	-340	587	4.02	4.02	4.02	4.02	2	0.10	0.00	0.03	0.00	0.00	22.3
8	226	1809	350	126	0	-285	664	4.02	4.02	4.02	4.02	2	0.11	0.01	0.06	0.00	0.00	22.3
9	226	1528	370	93	0	-335	681	4.02	4.02	4.02	4.02	2	0.11	0.01	0.07	0.00	0.00	22.3
10	226	3613	-80	140	0	-314	597	4.02	4.02	4.02	4.02	2	0.10	0.00	0.01	0.00	0.00	22.3
11	226	3529	-74	130	0	-329	599	4.02	4.02	4.02	4.02	2	0.10	0.00	0.01	0.00	0.00	22.3
12	226	687	592	101	0	-296	832	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
13	226	602	598	91	0	-311	837	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
14	226	2687	148	138	0	-290	572	4.02	4.02	4.02	4.02	2	0.09	0.00	0.03	0.00	0.00	22.3
15	226	2406	168	105	0	-340	587	4.02	4.02	4.02	4.02	2	0.10	0.00	0.03	0.00	0.00	22.3
16	226	1809	350	126	0	-285	664	4.02	4.02	4.02	4.02	2	0.11	0.01	0.06	0.00	0.00	22.3
17	226	1528	370	93	0	-335	681	4.02	4.02	4.02	4.02	2	0.11	0.01	0.07	0.00	0.00	22.3
18	226	8421	-630	347	0	-893	941	4.02	4.02	4.02	4.02	3	0.28	0.02	0.11	0.00	0.00	22.3
19	226	807	1031	99	0	-824	1031	4.02	4.02	4.02	4.02	3	0.21	0.03	0.18	0.00	0.00	22.3
20	226	4239	224	202	0	-849	636	4.02	4.02	4.02	4.02	3	0.23	0.01	0.04	0.00	0.00	22.3
37	226	10290	-1135	405	0	-771	1372	4.02	4.02	4.02	4.02	3	0.28	0.03	0.20	0.00	0.00	22.3
38	226	-2398	1634	-9	0	-654	1322	4.02	4.02	4.02	4.02	3	0.18	0.05	0.28	0.00	0.00	22.3
39	226	3322	288	163	0	-696	733	4.02	4.02	4.02	4.02	3	0.19	0.01	0.05	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	282	2740	-61	150	0	-491	813	4.02	4.02	4.02	4.02	3	0.13	0.00	0.01	0.00	0.00	22.3
2	282	3613	-385	140	0	-393	597	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
3	282	3529	-379	130	0	-402	599	4.02	4.02	4.02	4.02	2	0.13	0.01	0.07	0.00	0.00	22.3
4	282	687	286	101	0	-353	857	4.02	4.02	4.02	4.02	2	0.13	0.01	0.05	0.00	0.00	22.3
5	282	602	292	91	0	-363	865	4.02	4.02	4.02	4.02	2	0.13	0.01	0.05	0.00	0.00	22.3
6	282	2687	-158	138	0	-368	572	4.02	4.02	4.02	4.02	2	0.11	0.00	0.03	0.00	0.00	22.3
7	282	2406	-137	105	0	-400	587	4.02	4.02	4.02	4.02	2	0.12	0.00	0.02	0.00	0.00	22.3
8	282	1809	44	126	0	-356	664	4.02	4.02	4.02	4.02	2	0.11	0.00	0.01	0.00	0.00	22.3
9	282	1528	64	93	0	-388	681	4.02	4.02	4.02	4.02	2	0.11	0.00	0.01	0.00	0.00	22.3
10	282	3613	-385	140	0	-393	597	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
11	282	3529	-379	130	0	-402	599	4.02	4.02	4.02	4.02	2	0.13	0.01	0.07	0.00	0.00	22.3
12	282	687	286	101	0	-353	857	4.02	4.02	4.02	4.02	2	0.13	0.01	0.05	0.00	0.00	22.3
13	282	602	292	91	0	-363	865	4.02	4.02	4.02	4.02	2	0.13	0.01	0.05	0.00	0.00	22.3
14	282	2687	-158	138	0	-368	572	4.02	4.02	4.02	4.02	2	0.11	0.00	0.03	0.00	0.00	22.3
15	282	2406	-137	105	0	-400	587	4.02	4.02	4.02	4.02	2	0.12	0.00	0.02	0.00	0.00	22.3
16	282	1809	44	126	0	-356	664	4.02	4.02	4.02	4.02	2	0.11	0.00	0.01	0.00	0.00	22.3
17	282	1528	64	93	0	-388	681	4.02	4.02	4.02	4.02	2	0.11	0.00	0.01	0.00	0.00	22.3
18	282	8421	-1028	347	0	-1090	742	4.02	4.02	4.02	4.02	3	0.34	0.03	0.18	0.00	0.00	22.3
19	282	807	633	99	0	-880	1258	4.02	4.02	4.02	4.02	3	0.22	0.02	0.11	0.00	0.00	22.3
20	282	4239	-174	202	0	-963	636	4.02	4.02	4.02	4.02	3	0.27	0.01	0.03	0.00	0.00	22.3
37	282	10290	-1533	405	0	-1000	820	4.02	4.02	4.02	4.02	3	0.34	0.04	0.27	0.00	0.00	22.3
38	282	-2398	1236	-9	0	-649	1931	4.02	4.02	4.02	4.02	3	0.26	0.04	0.21	0.00	0.00	22.3
39	282	3322	-110	163	0	-788	733	4.02	4.02	4.02	4.02	3	0.21	0.01	0.03	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	339	2740	-449	150	0	-576	813	4.02	4.02	4.02	4.02	3	0.15	0.01	0.08	0.00	0.00	22.3
2	339	3613	-684	140	0	-472	509	4.02	4.02	4.02	4.02	2	0.15	0.02	0.12	0.00	0.00	22.3
3	339	3529	-678	130	0	-476	515	4.02	4.02	4.02	4.02	2	0.15	0.02	0.12	0.00	0.00	22.3
4	339	687	-13	101	0	-410	857	4.02	4.02	4.02	4.02	2	0.13	0.00	0.00	0.00	0.00	22.3
5	339	602	-7	91	0	-414	865	4.02	4.02	4.02	4.02	2	0.13	0.00	0.00	0.00	0.00	22.3
6	339	2687	-457	138	0	-445	572	4.02	4.02	4.02	4.02	2	0.13	0.01	0.08	0.00	0.00	22.3
7	339	2406	-436	105	0	-459	587	4.02	4.02	4.02	4.02	2	0.14	0.01	0.08	0.00	0.00	22.3
8	339	1809	-255	126	0	-427	664	4.02	4.02	4.02	4.02	2	0.13	0.01	0.05	0.00	0.00	22.3
9	339	1528	-235	93	0	-440	681	4.02	4.02	4.02	4.02	2	0.13	0.01	0.04	0.00	0.00	22.3
10	339	3613	-684	140	0	-472	509	4.02	4.02	4.02	4.02	2	0.15	0.02	0.12	0.00	0.00	22.3
11	339	3529	-678	130	0	-476	515	4.02	4.02	4.02	4.02	2	0.15	0.02	0.12	0.00	0.00	22.3
12	339	687	-13	101	0	-410	857	4.02	4.02	4.02	4.02	2	0.13	0.00	0.00	0.00	0.00	22.3
13	339	602	-7	91	0	-414	865	4.02	4.02	4.02	4.02	2	0.13	0.00	0.00	0.00	0.00	22.3
14	339	2687	-457	138	0	-445	572	4.02	4.02	4.02	4.02	2	0.13	0.01	0.08	0.00	0.00	22.3
15	339	2406	-436	105	0	-459	587	4.02	4.02	4.02	4.02	2	0.14	0.01	0.08	0.00	0.00	22.3
16	339	1809	-255	126	0	-427	664	4.02	4.02	4.02	4.02	2	0.13	0.01	0.05	0.00	0.00	22.3
17	339	1528	-235	93	0	-440	681	4.02	4.02	4.02	4.02	2	0.13	0.01	0.04	0.00	0.00	22.3
18	339	8421	-1416	347	0	-1286	-1186	4.02	4.02	4.02	4.02	3	0.41	0.04	0.25	0.00	0.00	22.3

19	339	807	245	99	0	-936	1258	4.02	4.02	4.02	4.02	3	0.23	0.01	0.04	0.00	0.00	22.3
20	339	4239	-562	202	0	-1077	636	4.02	4.02	4.02	4.02	3	0.30	0.02	0.10	0.00	0.00	22.3
37	339	10290	-1921	405	0	-1229	-1905	4.02	4.02	4.02	4.02	3	0.41	0.06	0.34	0.00	0.00	22.3
38	339	-2398	848	-9	0	-644	2323	4.02	4.02	4.02	4.02	3	0.31	0.02	0.14	0.00	0.00	22.3
39	339	3322	-498	163	0	-880	733	4.02	4.02	4.02	4.02	3	0.24	0.01	0.09	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	395	2740	-828	150	0	-661	727	4.02	4.02	4.02	4.02	3	0.18	0.02	0.15	0.00	0.00	22.3
2	395	3613	-975	140	0	-551	-800	4.02	4.02	4.02	4.02	2	0.17	0.03	0.17	0.00	0.00	22.3
3	395	3529	-969	130	0	-549	-785	4.02	4.02	4.02	4.02	2	0.17	0.03	0.17	0.00	0.00	22.3
4	395	687	-304	101	0	-467	857	4.02	4.02	4.02	4.02	2	0.13	0.01	0.05	0.00	0.00	22.3
5	395	602	-298	91	0	-466	865	4.02	4.02	4.02	4.02	2	0.13	0.01	0.05	0.00	0.00	22.3
6	395	2687	-748	137	0	-523	434	4.02	4.02	4.02	4.02	2	0.16	0.02	0.13	0.00	0.00	22.3
7	395	2406	-727	105	0	-518	464	4.02	4.02	4.02	4.02	2	0.15	0.02	0.13	0.00	0.00	22.3
8	395	1809	-546	126	0	-498	654	4.02	4.02	4.02	4.02	2	0.15	0.02	0.10	0.00	0.00	22.3
9	395	1528	-526	93	0	-493	681	4.02	4.02	4.02	4.02	2	0.14	0.02	0.09	0.00	0.00	22.3
10	395	3613	-975	140	0	-551	-800	4.02	4.02	4.02	4.02	2	0.17	0.03	0.17	0.00	0.00	22.3
11	395	3529	-969	130	0	-549	-785	4.02	4.02	4.02	4.02	2	0.17	0.03	0.17	0.00	0.00	22.3
12	395	687	-304	101	0	-467	857	4.02	4.02	4.02	4.02	2	0.13	0.01	0.05	0.00	0.00	22.3
13	395	602	-298	91	0	-466	865	4.02	4.02	4.02	4.02	2	0.13	0.01	0.05	0.00	0.00	22.3
14	395	2687	-748	137	0	-523	434	4.02	4.02	4.02	4.02	2	0.16	0.02	0.13	0.00	0.00	22.3
15	395	2406	-727	105	0	-518	464	4.02	4.02	4.02	4.02	2	0.15	0.02	0.13	0.00	0.00	22.3
16	395	1809	-546	126	0	-498	654	4.02	4.02	4.02	4.02	2	0.15	0.02	0.10	0.00	0.00	22.3
17	395	1528	-526	93	0	-493	681	4.02	4.02	4.02	4.02	2	0.14	0.02	0.09	0.00	0.00	22.3
18	395	8421	-1795	347	0	-1482	-2285	4.02	4.02	4.02	4.02	3	0.47	0.05	0.32	0.00	0.00	22.3
19	395	807	-134	99	0	-991	1258	4.02	4.02	4.02	4.02	3	0.25	0.00	0.02	0.00	0.00	22.3
20	395	4239	-941	202	0	-1191	478	4.02	4.02	4.02	4.02	3	0.33	0.03	0.17	0.00	0.00	22.3
37	395	10290	-2300	405	0	-1458	-3289	4.02	4.02	4.02	4.02	3	0.68	0.07	0.41	0.00	0.00	22.3
38	395	-2398	469	-9	0	-639	2425	4.02	4.02	4.02	4.02	3	0.32	0.01	0.08	0.00	0.00	22.3
39	395	3322	-877	163	0	-973	616	4.02	4.02	4.02	4.02	3	0.26	0.03	0.16	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	452	2740	-1197	150	0	-745	-871	4.02	4.02	4.02	4.02	3	0.20	0.03	0.21	0.00	0.00	22.3
2	452	3613	-1259	140	0	-630	-1575	4.02	4.02	4.02	4.02	2	0.27	0.04	0.22	0.00	0.00	22.3
3	452	3529	-1253	130	0	-623	-1557	4.02	4.02	4.02	4.02	2	0.26	0.04	0.22	0.00	0.00	22.3
4	452	687	-588	101	0	-524	812	4.02	4.02	4.02	4.02	2	0.15	0.02	0.10	0.00	0.00	22.3
5	452	602	-582	91	0	-517	825	4.02	4.02	4.02	4.02	2	0.15	0.02	0.10	0.00	0.00	22.3
6	452	2687	-1032	138	0	-601	-970	4.02	4.02	4.02	4.02	2	0.18	0.03	0.18	0.00	0.00	22.3
7	452	2406	-1011	105	0	-577	-908	4.02	4.02	4.02	4.02	2	0.17	0.03	0.18	0.00	0.00	22.3
8	452	1809	-830	126	0	-569	-432	4.02	4.02	4.02	4.02	2	0.17	0.02	0.15	0.00	0.00	22.3
9	452	1528	-810	93	0	-546	450	4.02	4.02	4.02	4.02	2	0.16	0.02	0.14	0.00	0.00	22.3
10	452	3613	-1259	140	0	-630	-1575	4.02	4.02	4.02	4.02	2	0.27	0.04	0.22	0.00	0.00	22.3
11	452	3529	-1253	130	0	-623	-1557	4.02	4.02	4.02	4.02	2	0.26	0.04	0.22	0.00	0.00	22.3
12	452	687	-588	101	0	-524	812	4.02	4.02	4.02	4.02	2	0.15	0.02	0.10	0.00	0.00	22.3
13	452	602	-582	91	0	-517	825	4.02	4.02	4.02	4.02	2	0.15	0.02	0.10	0.00	0.00	22.3
14	452	2687	-1032	138	0	-601	-970	4.02	4.02	4.02	4.02	2	0.18	0.03	0.18	0.00	0.00	22.3
15	452	2406	-1011	105	0	-577	-908	4.02	4.02	4.02	4.02	2	0.17	0.03	0.18	0.00	0.00	22.3
16	452	1809	-830	126	0	-569	-432	4.02	4.02	4.02	4.02	2	0.17	0.02	0.15	0.00	0.00	22.3
17	452	1528	-810	93	0	-546	450	4.02	4.02	4.02	4.02	2	0.16	0.02	0.14	0.00	0.00	22.3
18	452	8421	-2164	347	0	-1678	-3591	4.02	4.02	4.02	4.02	3	0.68	0.06	0.39	0.00	0.00	22.3
19	452	807	-503	99	0	-1047	1258	4.02	4.02	4.02	4.02	3	0.26	0.01	0.09	0.00	0.00	22.3
20	452	4239	-1310	202	0	-1305	-1298	4.02	4.02	4.02	4.02	3	0.36	0.04	0.23	0.00	0.00	22.3
37	452	10290	-2669	405	0	-1687	-4880	4.02	4.02	4.02	6.03	3	0.60	0.08	0.42	0.00	0.00	22.3
38	452	-2398	100	-9	0	-634	2425	4.02	4.02	4.02	4.02	3	0.32	0.00	0.02	0.00	0.00	22.3
39	452	3322	-1246	163	0	-1065	-1059	4.02	4.02	4.02	4.02	3	0.29	0.04	0.22	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= 2.01 (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	508	2740	-1557	150	0	-830	-1832	4.02	4.02	4.02	4.02	3	0.29	0.05	0.28	0.00	0.00	22.3
2	508	3613	-1536	140	0	-708	-2506	4.02	4.02	4.02	4.02	2	0.43	0.04	0.27	0.00	0.00	22.3
3	508	3529	-1530	130	0	-696	-2484	4.02	4.02	4.02	4.02	2	0.42	0.04	0.27	0.00	0.00	22.3
4	508	687	-865	101	0	-581	541	4.02	4.02	4.02	4.02	2	0.16	0.03	0.15	0.00	0.00	22.3
5	508	602	-859	91	0	-568	557	4.02	4.02	4.02	4.02	2	0.16	0.02	0.15	0.00	0.00	22.3
6	508	2687	-1309	138	0	-679	-1772	4.02	4.02	4.02	4.02	2	0.29	0.04	0.23	0.00	0.00	22.3
7	508	2406	-1288	105	0	-637	-1699	4.02	4.02	4.02	4.02	2	0.28	0.04	0.23	0.00	0.00	22.3
8	508	1809	-1107	126	0	-640	-1120	4.02	4.02	4.02	4.02	2	0.19	0.03	0.20	0.00	0.00	22.3
9	508	1528	-1087	93	0	-598	-1047	4.02	4.02	4.02	4.02	2	0.17	0.03	0.19	0.00	0.00	22.3
10	508	3613	-1536	140	0	-708	-2506	4.02	4.02	4.02	4.02	2	0.43	0.04	0.27	0.00	0.00	22.3
11	508	3529	-1530	130	0	-696	-2484	4.02	4.02	4.02	4.02	2	0.42	0.04	0.27	0.00	0.00	22.3
12	508	687	-865	101	0	-581	541	4.02	4.02	4.02	4.02	2	0.16	0.03	0.15	0.00	0.00	22.3
13	508	602	-859	91	0	-568	557	4.02	4.02	4.02	4.02	2	0.16	0.02	0.15	0.00	0.00	22.3
14	508	2687	-1309	138	0	-679	-1772	4.02	4.02	4.02	4.02	2	0.29	0.04	0.23	0.00	0.00	22.3
15	508	2406	-1288	105	0	-637	-1699	4.02	4.02	4.02	4.02	2	0.28	0.04	0.23	0.00	0.00	22.3
16	508	1809	-1107	126	0	-640	-1120	4.02	4.02	4.02	4.02	2	0.19	0.03	0.20	0.00	0.00	22.3
17	508	1528	-1087	93	0	-598	-1047	4.02	4.02	4.02	4.02	2	0.17	0.03	0.19	0.00	0.00	22.3
18	508	8421	-2524	347	0	-1875	-5098	4.02	4.02	4.02	4.02	3	0.97	0.07	0.45	0.00	0.00	22.3
19	508	807	-863	99	0	-1103	1128	4.02	4.02	4.02	4.02	3	0.28	0.03	0.15	0.00	0.00	22.3
20	508	4239	-1670	202	0	-1419	-2323	4.02	4.02	4.02	4.02	3	0.39	0.05	0.30	0.00	0.00	22.3
37	508	10290	-3029	405	0	-1916	-6673	4.02	4.02	4.02	6.03	3	0.82	0.09	0.47	0.00	0.00	22.3
38	508	-2398	-260	-9	0	-629	2425	4.02	4.02	4.02	4.02	3	0.32	0.01	0.04	0.00	0.00	22.3
39	508	3322	-1606	163	0	-1157	-2047	4.02	4.02	4.02	4.02	3	0.33	0.05	0.29	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= 2.01 (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	565	2740	-1908	150	0	-915	-2023	4.02	4.02	4.02	4.02	3	0.32	0.06	0.34	0.00	0.00	22.3
2	565	3613	-1806	140	0	-787	-2673	4.02	4.02	4.02	4.02	2	0.46	0.05	0.32	0.00	0.00	22.3
3	565	3529	-1800	130	0	-769	-2651	4.02	4.02	4.02	4.02	2	0.45	0.05	0.32	0.00	0.00	22.3
4	565	687	-1135	101	0	-638	-462	4.02	4.02	4.02	4.02	2	0.18	0.03	0.20	0.00	0.00	22.3
5	565	602	-1129	91	0	-620	-440	4.02	4.02	4.02	4.02	2	0.17	0.03	0.20	0.00	0.00	22.3
6	565	2687	-1579	138	0	-756	-1925	4.02	4.02	4.02	4.02	2	0.32	0.05	0.28	0.00	0.00	22.3
7	565	2406	-1558	105	0	-696	-1851	4.02	4.02	4.02	4.02	2	0.30	0.05	0.28	0.00	0.00	22.3
8	565	1809	-1377	126	0	-711	-1262	4.02	4.02	4.02	4.02	2	0.21	0.04	0.25	0.00	0.00	22.3
9	565	1528	-1357	93	0	-651	-1188	4.02	4.02	4.02	4.02	2	0.19	0.04	0.24	0.00	0.00	22.3
10	565	3613	-1806	140	0	-787	-2673	4.02	4.02	4.02	4.02	2	0.46	0.05	0.32	0.00	0.00	22.3
11	565	3529	-1800	130	0	-769	-2651	4.02	4.02	4.02	4.02	2	0.45	0.05	0.32	0.00	0.00	22.3
12	565	687	-1135	101	0	-638	-462	4.02	4.02	4.02	4.02	2	0.18	0.03	0.20	0.00	0.00	22.3
13	565	602	-1129	91	0	-620	-440	4.02	4.02	4.02	4.02	2	0.17	0.03	0.20	0.00	0.00	22.3
14	565	2687	-1579	138	0	-756	-1925	4.02	4.02	4.02	4.02	2	0.32	0.05	0.28	0.00	0.00	22.3
15	565	2406	-1558	105	0	-696	-1851	4.02	4.02	4.02	4.02	2	0.30	0.05	0.28	0.00	0.00	22.3
16	565	1809	-1377	126	0	-711	-1262	4.02	4.02	4.02	4.02	2	0.21	0.04	0.25	0.00	0.00	22.3
17	565	1528	-1357	93	0	-651	-1188	4.02	4.02	4.02	4.02	2	0.19	0.04	0.24	0.00	0.00	22.3
18	565	8421	-2875	347	0	-2071	-5346	4.02	4.02	4.02	6.03	3	0.65	0.08	0.45	0.00	0.00	22.3
19	565	807	-1214	99	0	-1159	718	4.02	4.02	4.02	4.02	3	0.29	0.04	0.22	0.00	0.00	22.3
20	565	4239	-2021	202	0	-1533	-2521	4.02	4.02	4.02	4.02	3	0.42	0.06	0.36	0.00	0.00	22.3
37	565	10290	-3380	405	0	-2145	-6950	4.02	4.02	4.02	6.03	3	0.86	0.10	0.53	0.00	0.00	22.3
38	565	-2398	-611	-9	0	-624	2425	4.02	4.02	4.02	4.02	3	0.32	0.02	0.10	0.00	0.00	22.3
39	565	3322	-1957	163	0	-1249	-2241	4.02	4.02	4.02	4.02	3	0.36	0.06	0.35	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= 2.01 (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

Nome travata: **Trave_403_IP1** Descrizione: **Trave_4 7-6-5-4-3-2-1**
ASTA NUM. 9 NI 25 NF 215 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y Permanente qy tot.
qy medio: 375.00 132.00 507.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	165	2018	-671	0	-2093	-2084	4.02	4.02	4.02	4.02	3	0.52	0.06	0.36	0.00	0.00	22.3
2	0	635	1557	-408	0	-1220	-1616	4.02	4.02	4.02	4.02	2	0.34	0.05	0.28	0.00	0.00	22.3
3	0	-73	1583	-464	0	-1446	-1674	4.02	4.02	4.02	4.02	2	0.40	0.05	0.28	0.00	0.00	22.3
4	0	327	1522	-568	0	-1774	-1532	4.02	4.02	4.02	4.02	2	0.49	0.04	0.27	0.00	0.00	22.3
5	0	-381	1548	-623	0	-2001	-1591	4.02	4.02	4.02	4.02	2	0.55	0.04	0.27	0.00	0.00	22.3
6	0	1353	1514	-400	0	-1150	-1519	4.02	4.02	4.02	4.02	2	0.33	0.04	0.27	0.00	0.00	22.3
7	0	-1007	1601	-584	0	-1905	-1713	4.02	4.02	4.02	4.02	2	0.51	0.05	0.28	0.00	0.00	22.3
8	0	1261	1503	-448	0	-1316	-1494	4.02	4.02	4.02	4.02	2	0.38	0.04	0.27	0.00	0.00	22.3
9	0	-1100	1591	-632	0	-2071	-1688	4.02	4.02	4.02	4.02	2	0.55	0.05	0.28	0.00	0.00	22.3
10	0	635	1557	-408	0	-1220	-1616	4.02	4.02	4.02	4.02	2	0.34	0.05	0.28	0.00	0.00	22.3
11	0	-73	1583	-464	0	-1446	-1674	4.02	4.02	4.02	4.02	2	0.40	0.05	0.28	0.00	0.00	22.3
12	0	327	1522	-568	0	-1774	-1532	4.02	4.02	4.02	4.02	2	0.49	0.04	0.27	0.00	0.00	22.3
13	0	-381	1548	-623	0	-2001	-1591	4.02	4.02	4.02	4.02	2	0.55	0.04	0.27	0.00	0.00	22.3
14	0	1353	1514	-400	0	-1150	-1519	4.02	4.02	4.02	4.02	2	0.33	0.04	0.27	0.00	0.00	22.3
15	0	-1007	1601	-584	0	-1905	-1713	4.02	4.02	4.02	4.02	2	0.51	0.05	0.28	0.00	0.00	22.3
16	0	1261	1503	-448	0	-1316	-1494	4.02	4.02	4.02	4.02	2	0.38	0.04	0.27	0.00	0.00	22.3
17	0	-1100	1591	-632	0	-2071	-1688	4.02	4.02	4.02	4.02	2	0.55	0.05	0.28	0.00	0.00	22.3
18	0	1460	2060	-1186	0	-3643	-2182	4.02	4.02	4.02	4.02	3	0.93	0.06	0.37	0.00	0.00	22.3
19	0	-21	1903	-1552	0	-4938	-1809	4.02	6.03	4.02	4.02	3	0.86	0.06	0.34	0.00	0.00	22.3
20	0	658	1941	-1471	0	-4811	-1824	4.02	6.03	4.02	4.02	3	0.85	0.06	0.35	0.00	0.00	22.3
37	0	1770	2124	-837	0	-2499	-2337	4.02	4.02	4.02	4.02	3	0.64	0.06	0.38	0.00	0.00	22.3
38	0	-698	1864	-1447	0	-4656	-1715	4.02	6.03	4.02	4.02	3	0.80	0.05	0.33	0.00	0.00	22.3
39	0	433	1925	-1311	0	-4444	-1741	4.02	6.03	4.02	4.02	3	0.78	0.06	0.34	0.00	0.00	22.3

apost= -- aant= 2.01 ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	60	165	1622	-671	0	-1691	-1813	4.02	4.02	4.02	4.02	3	0.42	0.05	0.29	0.00	0.00	22.3
2	60	635	1253	-408	0	-975	-1408	4.02	4.02	4.02	4.02	2	0.27	0.04	0.22	0.00	0.00	22.3
3	60	-73	1279	-464	0	-1168	-1463	4.02	4.02	4.02	4.02	2	0.32	0.04	0.23	0.00	0.00	22.3
4	60	327	1218	-568	0	-1433	-1327	4.02	4.02	4.02	4.02	2	0.40	0.04	0.22	0.00	0.00	22.3
5	60	-381	1244	-623	0	-1627	-1383	4.02	4.02	4.02	4.02	2	0.44	0.04	0.22	0.00	0.00	22.3
6	60	1353	1210	-400	0	-910	-1315	4.02	4.02	4.02	4.02	2	0.26	0.04	0.22	0.00	0.00	22.3
7	60	-1007	1297	-584	0	-1555	-1500	4.02	4.02	4.02	4.02	2	0.42	0.04	0.23	0.00	0.00	22.3
8	60	1261	1199	-448	0	-1047	-1290	4.02	4.02	4.02	4.02	2	0.30	0.03	0.21	0.00	0.00	22.3
9	60	-1100	1287	-632	0	-1692	-1476	4.02	4.02	4.02	4.02	2	0.45	0.04	0.22	0.00	0.00	22.3
10	60	635	1253	-408	0	-975	-1408	4.02	4.02	4.02	4.02	2	0.27	0.04	0.22	0.00	0.00	22.3
11	60	-73	1279	-464	0	-1168	-1463	4.02	4.02	4.02	4.02	2	0.32	0.04	0.23	0.00	0.00	22.3
12	60	327	1218	-568	0	-1433	-1327	4.02	4.02	4.02	4.02	2	0.40	0.04	0.22	0.00	0.00	22.3
13	60	-381	1244	-623	0	-1627	-1383	4.02	4.02	4.02	4.02	2	0.44	0.04	0.22	0.00	0.00	22.3
14	60	1353	1210	-400	0	-910	-1315	4.02	4.02	4.02	4.02	2	0.26	0.04	0.22	0.00	0.00	22.3
15	60	-1007	1297	-584	0	-1555	-1500	4.02	4.02	4.02	4.02	2	0.42	0.04	0.23	0.00	0.00	22.3
16	60	1261	1199	-448	0	-1047	-1290	4.02	4.02	4.02	4.02	2	0.30	0.03	0.21	0.00	0.00	22.3
17	60	-1100	1287	-632	0	-1692	-1476	4.02	4.02	4.02	4.02	2	0.45	0.04	0.22	0.00	0.00	22.3
18	60	1460	1664	-1186	0	-2931	-1907	4.02	4.02	4.02	4.02	3	0.75	0.05	0.30	0.00	0.00	22.3
19	60	-21	1508	-1552	0	-4007	-1549	4.02	4.02	4.02	4.02	3	0.98	0.05	0.27	0.00	0.00	22.3
20	60	658	1546	-1471	0	-3929	-1561	4.02	4.02	4.02	4.02	3	0.98	0.05	0.28	0.00	0.00	22.3
37	60	1770	1729	-837	0	-1997	-2056	4.02	4.02	4.02	4.02	3	0.51	0.05	0.31	0.00	0.00	22.3
38	60	-698	1468	-1447	0	-3788	-1459	4.02	4.02	4.02	4.02	3	0.91	0.05	0.26	0.00	0.00	22.3
39	60	433	1530	-1311	0	-3657	-1479	4.02	4.02	4.02	4.02	3	0.91	0.04	0.27	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	120	165	1227	-671	0	-1288	-758	4.02	4.02	4.02	4.02	3	0.32	0.04	0.22	0.00	0.00	22.3
2	120	635	949	-408	0	-730	-593	4.02	4.02	4.02	4.02	2	0.21	0.03	0.17	0.00	0.00	22.3
3	120	-73	975	-464	0	-890	-633	4.02	4.02	4.02	4.02	2	0.24	0.03	0.17	0.00	0.00	22.3
4	120	327	914	-568	0	-1092	-534	4.02	4.02	4.02	4.02	2	0.30	0.03	0.16	0.00	0.00	22.3
5	120	-381	940	-623	0	-1253	-574	4.02	4.02	4.02	4.02	2	0.34	0.03	0.17	0.00	0.00	22.3
6	120	1353	906	-400	0	-670	-526	4.02	4.02	4.02	4.02	2	0.19	0.03	0.16	0.00	0.00	22.3
7	120	-1007	993	-584	0	-1204	-659	4.02	4.02	4.02	4.02	2	0.32	0.03	0.17	0.00	0.00	22.3
8	120	1261	895	-448	0	-779	-508	4.02	4.02	4.02	4.02	2	0.22	0.03	0.16	0.00	0.00	22.3
9	120	-1100	983	-632	0	-1313	-641	4.02	4.02	4.02	4.02	2	0.35	0.03	0.17	0.00	0.00	22.3
10	120	635	949	-408	0	-730	-593	4.02	4.02	4.02	4.02	2	0.21	0.03	0.17	0.00	0.00	22.3
11	120	-73	975	-464	0	-890	-633	4.02	4.02	4.02	4.02	2	0.24	0.03	0.17	0.00	0.00	22.3
12	120	327	914	-568	0	-1092	-534	4.02	4.02	4.02	4.02	2	0.30	0.03	0.16	0.00	0.00	22.3
13	120	-381	940	-623	0	-1253	-574	4.02	4.02	4.02	4.02	2	0.34	0.03	0.17	0.00	0.00	22.3
14	120	1353	906	-400	0	-670	-526	4.02	4.02	4.02	4.02	2	0.19	0.03	0.16	0.00	0.00	22.3
15	120	-1007	993	-584	0	-1204	-659	4.02	4.02	4.02	4.02	2	0.32	0.03	0.17	0.00	0.00	22.3
16	120	1261	895	-448	0	-779	-508	4.02	4.02	4.02	4.02	2	0.22	0.03	0.16	0.00	0.00	22.3
17	120	-1100	983	-632	0	-1313	-641	4.02	4.02	4.02	4.02	2	0.35	0.03	0.17	0.00	0.00	22.3
18	120	1460	1269	-1186	0	-2220	-827	4.02	4.02	4.02	4.02	3	0.57	0.04	0.23	0.00	0.00	22.3
19	120	-21	1112	-1552	0	-3075	564	4.02	4.02	4.02	4.02	3	0.76	0.05	0.25	0.00	0.00	22.3
20	120	658	1150	-1471	0	-3046	612	4.02	4.02	4.02	4.02	3	0.76	0.05	0.24	0.00	0.00	22.3
37	120	1770	1333	-837	0	-1494	-937	4.02	4.02	4.02	4.02	3	0.39	0.04	0.24	0.00	0.00	22.3
38	120	-698	1073	-1447	0	-2919	590	4.02	4.02	4.02	4.02	3	0.70	0.05	0.23	0.00	0.00	22.3
39	120	433	1134	-1311	0	-2870	669	4.02	4.02	4.02	4.02	3	0.71	0.04	0.21	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	180	165	832	-671	0	-886	902	4.02	4.02	4.02	4.02	3	0.22	0.02	0.15	0.00	0.00	22.3
2	180	635	644	-408	0	-485	691	4.02	4.02	4.02	4.02	2	0.14	0.02	0.11	0.00	0.00	22.3
3	180	-73	670	-464	0	-612	693	4.02	4.02	4.02	4.02	2	0.17	0.02	0.12	0.00	0.00	22.3
4	180	327	609	-568	0	-751	694	4.02	4.02	4.02	4.02	2	0.21	0.02	0.11	0.00	0.00	22.3
5	180	-381	635	-623	0	-879	696	4.02	4.02	4.02	4.02	2	0.24	0.02	0.11	0.00	0.00	22.3
6	180	1353	601	-400	0	-430	689	4.02	4.02	4.02	4.02	2	0.12	0.02	0.11	0.00	0.00	22.3
7	180	-1007	688	-584	0	-854	697	4.02	4.02	4.02	4.02	2	0.23	0.02	0.12	0.00	0.00	22.3
8	180	1261	590	-448	0	-510	689	4.02	4.02	4.02	4.02	2	0.15	0.02	0.11	0.00	0.00	22.3
9	180	-1100	678	-632	0	-933	698	4.02	4.02	4.02	4.02	2	0.25	0.02	0.12	0.00	0.00	22.3
10	180	635	644	-408	0	-485	691	4.02	4.02	4.02	4.02	2	0.14	0.02	0.11	0.00	0.00	22.3
11	180	-73	670	-464	0	-612	693	4.02	4.02	4.02	4.02	2	0.17	0.02	0.12	0.00	0.00	22.3
12	180	327	609	-568	0	-751	694	4.02	4.02	4.02	4.02	2	0.21	0.02	0.11	0.00	0.00	22.3
13	180	-381	635	-623	0	-879	696	4.02	4.02	4.02	4.02	2	0.24	0.02	0.11	0.00	0.00	22.3
14	180	1353	601	-400	0	-430	689	4.02	4.02	4.02	4.02	2	0.12	0.02	0.11	0.00	0.00	22.3
15	180	-1007	688	-584	0	-854	697	4.02	4.02	4.02	4.02	2	0.23	0.02	0.12	0.00	0.00	22.3
16	180	1261	590	-448	0	-510	689	4.02	4.02	4.02	4.02	2	0.15	0.02	0.11	0.00	0.00	22.3

17	180	-1100	678	-632	0	-933	698	4.02	4.02	4.02	4.02	2	0.25	0.02	0.12	0.00	0.00	22.3
18	180	1460	874	-1186	0	-1508	900	4.02	4.02	4.02	4.02	3	0.39	0.04	0.19	0.00	0.00	22.3
19	180	-21	717	-1552	0	-2144	912	4.02	4.02	4.02	4.02	3	0.53	0.05	0.25	0.00	0.00	22.3
20	180	658	755	-1471	0	-2164	983	4.02	4.02	4.02	4.02	3	0.54	0.05	0.24	0.00	0.00	22.3
37	180	1770	938	-837	0	-992	894	4.02	4.02	4.02	4.02	3	0.26	0.03	0.17	0.00	0.00	22.3
38	180	-698	677	-1447	0	-2050	909	4.02	4.02	4.02	4.02	3	0.49	0.05	0.23	0.00	0.00	22.3
39	180	433	739	-1311	0	-2084	1031	4.02	4.02	4.02	4.02	3	0.52	0.04	0.21	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	240	165	436	-671	0	-484	1004	4.02	4.02	4.02	4.02	3	0.14	0.02	0.11	0.00	0.00	22.3
2	240	635	340	-408	0	-240	772	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
3	240	-73	366	-464	0	-334	793	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
4	240	327	305	-568	0	-410	752	4.02	4.02	4.02	4.02	2	0.12	0.02	0.09	0.00	0.00	22.3
5	240	-381	331	-623	0	-505	772	4.02	4.02	4.02	4.02	2	0.14	0.02	0.10	0.00	0.00	22.3
6	240	1353	297	-400	0	-190	741	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
7	240	-1007	384	-584	0	-503	810	4.02	4.02	4.02	4.02	2	0.13	0.02	0.09	0.00	0.00	22.3
8	240	1261	286	-448	0	-241	734	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
9	240	-1100	374	-632	0	-554	804	4.02	4.02	4.02	4.02	2	0.15	0.02	0.10	0.00	0.00	22.3
10	240	635	340	-408	0	-240	772	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
11	240	-73	366	-464	0	-334	793	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
12	240	327	305	-568	0	-410	752	4.02	4.02	4.02	4.02	2	0.12	0.02	0.09	0.00	0.00	22.3
13	240	-381	331	-623	0	-505	772	4.02	4.02	4.02	4.02	2	0.14	0.02	0.10	0.00	0.00	22.3
14	240	1353	297	-400	0	-190	741	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
15	240	-1007	384	-584	0	-503	810	4.02	4.02	4.02	4.02	2	0.13	0.02	0.09	0.00	0.00	22.3
16	240	1261	286	-448	0	-241	734	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
17	240	-1100	374	-632	0	-554	804	4.02	4.02	4.02	4.02	2	0.15	0.02	0.10	0.00	0.00	22.3
18	240	1460	478	-1186	0	-796	1031	4.02	4.02	4.02	4.02	3	0.20	0.04	0.19	0.00	0.00	22.3
19	240	-21	321	-1552	0	-1212	935	4.02	4.02	4.02	4.02	3	0.30	0.05	0.25	0.00	0.00	22.3
20	240	658	359	-1471	0	-1281	1031	4.02	4.02	4.02	4.02	3	0.32	0.05	0.24	0.00	0.00	22.3
37	240	1770	542	-837	0	-490	1070	4.02	4.02	4.02	4.02	3	0.16	0.03	0.13	0.00	0.00	22.3
38	240	-698	282	-1447	0	-1182	909	4.02	4.02	4.02	4.02	3	0.29	0.05	0.23	0.00	0.00	22.3
39	240	433	343	-1311	0	-1297	1069	4.02	4.02	4.02	4.02	3	0.32	0.04	0.21	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	300	165	40	-671	0	-82	1004	4.02	4.02	4.02	4.02	3	0.14	0.02	0.11	0.00	0.00	22.3
2	300	635	36	-408	0	5	772	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
3	300	-73	62	-464	0	-56	793	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
4	300	327	1	-568	0	-70	752	4.02	4.02	4.02	4.02	2	0.12	0.02	0.09	0.00	0.00	22.3
5	300	-381	27	-623	0	-130	772	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
6	300	1353	-7	-400	0	50	741	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
7	300	-1007	80	-584	0	-153	810	4.02	4.02	4.02	4.02	2	0.12	0.02	0.09	0.00	0.00	22.3
8	300	1261	-18	-448	0	27	734	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
9	300	-1100	70	-632	0	-175	804	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
10	300	635	36	-408	0	5	772	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
11	300	-73	62	-464	0	-56	793	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
12	300	327	1	-568	0	-70	752	4.02	4.02	4.02	4.02	2	0.12	0.02	0.09	0.00	0.00	22.3
13	300	-381	27	-623	0	-130	772	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
14	300	1353	-7	-400	0	50	741	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
15	300	-1007	80	-584	0	-153	810	4.02	4.02	4.02	4.02	2	0.12	0.02	0.09	0.00	0.00	22.3
16	300	1261	-18	-448	0	27	734	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
17	300	-1100	70	-632	0	-175	804	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
18	300	1460	82	-1186	0	-85	1031	4.02	4.02	4.02	4.02	3	0.15	0.04	0.19	0.00	0.00	22.3
19	300	-21	-74	-1552	0	-281	935	4.02	4.02	4.02	4.02	3	0.13	0.05	0.25	0.00	0.00	22.3
20	300	658	-36	-1471	0	-399	1031	4.02	4.02	4.02	4.02	3	0.15	0.05	0.24	0.00	0.00	22.3
37	300	1770	147	-837	0	12	1070	4.02	4.02	4.02	4.02	3	0.16	0.03	0.13	0.00	0.00	22.3
38	300	-698	-114	-1447	0	-314	909	4.02	4.02	4.02	4.02	3	0.13	0.05	0.23	0.00	0.00	22.3
39	300	433	-52	-1311	0	-510	1069	4.02	4.02	4.02	4.02	3	0.16	0.04	0.21	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	360	165	-355	-671	0	321	1004	4.02	4.02	4.02	4.02	3	0.14	0.02	0.11	0.00	0.00	22.3
2	360	635	-268	-408	0	250	772	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
3	360	-73	-242	-464	0	223	793	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
4	360	327	-303	-568	0	271	752	4.02	4.02	4.02	4.02	2	0.12	0.02	0.09	0.00	0.00	22.3
5	360	-381	-277	-623	0	244	772	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
6	360	1353	-311	-400	0	289	741	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
7	360	-1007	-224	-584	0	197	810	4.02	4.02	4.02	4.02	2	0.12	0.02	0.09	0.00	0.00	22.3
8	360	1261	-322	-448	0	296	734	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
9	360	-1100	-234	-632	0	204	804	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
10	360	635	-268	-408	0	250	772	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
11	360	-73	-242	-464	0	223	793	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
12	360	327	-303	-568	0	271	752	4.02	4.02	4.02	4.02	2	0.12	0.02	0.09	0.00	0.00	22.3
13	360	-381	-277	-623	0	244	772	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
14	360	1353	-311	-400	0	289	741	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
15	360	-1007	-224	-584	0	197	810	4.02	4.02	4.02	4.02	2	0.12	0.02	0.09	0.00	0.00	22.3
16	360	1261	-322	-448	0	296	734	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
17	360	-1100	-234	-632	0	204	804	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
18	360	1460	-313	-1186	0	627	1031	4.02	4.02	4.02	4.02	3	0.16	0.04	0.19	0.00	0.00	22.3
19	360	-21	-469	-1552	0	650	935	4.02	4.02	4.02	4.02	3	0.16	0.05	0.25	0.00	0.00	22.3
20	360	658	-432	-1471	0	483	1031	4.02	4.02	4.02	4.02	3	0.15	0.05	0.24	0.00	0.00	22.3
37	360	1770	-248	-837	0	515	1070	4.02	4.02	4.02	4.02	3	0.16	0.03	0.13	0.00	0.00	22.3
38	360	-698	-509	-1447	0	555	909	4.02	4.02	4.02	4.02	3	0.13	0.05	0.23	0.00	0.00	22.3
39	360	433	-447	-1311	0	277	1069	4.02	4.02	4.02	4.02	3	0.16	0.04	0.21	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	420	165	-750	-671	0	723	958	4.02	4.02	4.02	4.02	3	0.18	0.02	0.13	0.00	0.00	22.3
2	420	635	-572	-408	0	495	739	4.02	4.02	4.02	4.02	2	0.14	0.02	0.10	0.00	0.00	22.3
3	420	-73	-546	-464	0	501	779	4.02	4.02	4.02	4.02	2	0.14	0.02	0.10	0.00	0.00	22.3
4	420	327	-607	-568	0	612	695	4.02	4.02	4.02	4.02	2	0.17	0.02	0.11	0.00	0.00	22.3
5	420	-381	-581	-623	0	618	734	4.02	4.02	4.02	4.02	2	0.17	0.02	0.10	0.00	0.00	22.3
6	420	1353	-615	-400	0	529	678	4.02	4.02	4.02	4.02	2	0.15	0.02	0.11	0.00	0.00	22.3
7	420	-1007	-528	-584	0	548	809	4.02	4.02	4.02	4.02	2	0.15	0.02	0.09	0.00	0.00	22.3
8	420	1261	-626	-448	0	565	665	4.02	4.02	4.02	4.02	2	0.16	0.02	0.11	0.00	0.00	22.3
9	420	-1100	-538	-632	0	583	795	4.02	4.02	4.02	4.02	2	0.16	0.02	0.10	0.00	0.00	22.3
10	420	635	-572	-408	0	495	739	4.02	4.02	4.02	4.02	2	0.14	0.02	0.10	0.00	0.00	22.3
11	420	-73	-546	-464	0	501	779	4.02	4.02	4.02	4.02	2	0.14	0.02	0.10	0.00	0.00	22.3
12	420	327	-607	-568	0	612	695	4.02	4.02	4.02	4.02	2	0.17	0.02	0.11	0.00	0.00	22.3
13	420	-381	-581	-623	0	618	734	4.02	4.02	4.02	4.02	2	0.17	0.02	0.10	0.00	0.00	22.3
14	420	1353	-615	-400	0	529	678	4.02	4.02	4.02	4.02	2	0.15	0.02	0.11	0.00	0.00	22.3
15	420	-1007	-528	-584	0	548	809	4.02	4.02	4.02	4.02	2	0.15	0.02	0.09	0.00	0.00	22.3
16	420	1261	-626	-448	0	565	665	4.02	4.02	4.02	4.02	2	0.16	0.02	0.11	0.00	0.00	22.3
17	420	-1100	-538	-632	0	583	795	4.02	4.02	4.02	4.02	2	0.16	0.02	0.10	0.00	0.00	22.3
18	420	1460	-708	-1186	0	1339	1015	4.02	4.02	4.02	4.02	3	0.34	0.04	0.19	0.00	0.00	22.3
19	420	-21	-865	-1552	0	1582	810	4.02	4.02	4.02	4.02	3	0.39	0.05	0.25	0.00	0.00	22.3
20	420	658	-827	-1471	0	1366	932	4.02	4.02	4.02	4.02	3	0.34	0.05	0.24	0.00	0.00	22.3
37	420	1770	-644	-837	0	1017	1070	4.02	4.02	4.02	4.02	3	0.26	0.03	0.13	0.00	0.00	22.3
38	420	-698	-904	-1447	0	1424	756	4.02	4.02	4.02	4.02	3	0.34	0.05	0.23	0.00	0.00	22.3

39	420	433	-843	-1311	0	1064	959	4.02	4.02	4.02	4.02	3	0.26	0.04	0.21	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	480	165	-1146	-671	0	1125	590	4.02	4.02	4.02	4.02	3	0.28	0.03	0.20	0.00	0.00	22.3
2	480	635	-877	-408	0	740	458	4.02	4.02	4.02	4.02	2	0.21	0.03	0.16	0.00	0.00	22.3
3	480	-73	-851	-464	0	779	514	4.02	4.02	4.02	4.02	2	0.21	0.02	0.15	0.00	0.00	22.3
4	480	327	-912	-568	0	953	-530	4.02	4.02	4.02	4.02	2	0.27	0.03	0.16	0.00	0.00	22.3
5	480	-381	-886	-623	0	992	-449	4.02	4.02	4.02	4.02	2	0.27	0.03	0.16	0.00	0.00	22.3
6	480	1353	-920	-400	0	769	-560	4.02	4.02	4.02	4.02	2	0.22	0.03	0.16	0.00	0.00	22.3
7	480	-1007	-833	-584	0	898	555	4.02	4.02	4.02	4.02	2	0.24	0.02	0.14	0.00	0.00	22.3
8	480	1261	-931	-448	0	834	-591	4.02	4.02	4.02	4.02	2	0.24	0.03	0.17	0.00	0.00	22.3
9	480	-1100	-843	-632	0	963	535	4.02	4.02	4.02	4.02	2	0.26	0.02	0.15	0.00	0.00	22.3
10	480	635	-877	-408	0	740	458	4.02	4.02	4.02	4.02	2	0.21	0.03	0.16	0.00	0.00	22.3
11	480	-73	-851	-464	0	779	514	4.02	4.02	4.02	4.02	2	0.21	0.02	0.15	0.00	0.00	22.3
12	480	327	-912	-568	0	953	-530	4.02	4.02	4.02	4.02	2	0.27	0.03	0.16	0.00	0.00	22.3
13	480	-381	-886	-623	0	992	-449	4.02	4.02	4.02	4.02	2	0.27	0.03	0.16	0.00	0.00	22.3
14	480	1353	-920	-400	0	769	-560	4.02	4.02	4.02	4.02	2	0.22	0.03	0.16	0.00	0.00	22.3
15	480	-1007	-833	-584	0	898	555	4.02	4.02	4.02	4.02	2	0.24	0.02	0.14	0.00	0.00	22.3
16	480	1261	-931	-448	0	834	-591	4.02	4.02	4.02	4.02	2	0.24	0.03	0.17	0.00	0.00	22.3
17	480	-1100	-843	-632	0	963	535	4.02	4.02	4.02	4.02	2	0.26	0.02	0.15	0.00	0.00	22.3
18	480	1460	-1104	-1186	0	2051	671	4.02	4.02	4.02	4.02	3	0.52	0.04	0.20	0.00	0.00	22.3
19	480	-21	-1260	-1552	0	2513	-903	4.02	4.02	4.02	4.02	3	0.62	0.05	0.25	0.00	0.00	22.3
20	480	658	-1223	-1471	0	2248	-722	4.02	4.02	4.02	4.02	3	0.56	0.05	0.24	0.00	0.00	22.3
37	480	1770	-1039	-837	0	1519	793	4.02	4.02	4.02	4.02	3	0.39	0.03	0.19	0.00	0.00	22.3
38	480	-698	-1300	-1447	0	2292	-1021	4.02	4.02	4.02	4.02	3	0.55	0.05	0.23	0.00	0.00	22.3
39	480	433	-1238	-1311	0	1850	-718	4.02	4.02	4.02	4.02	3	0.46	0.04	0.22	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	540	165	-1541	-671	0	1528	-1577	4.02	4.02	4.02	4.02	3	0.38	0.04	0.27	0.00	0.00	22.3
2	540	635	-1181	-408	0	985	-1201	4.02	4.02	4.02	4.02	2	0.28	0.03	0.21	0.00	0.00	22.3
3	540	-73	-1155	-464	0	1057	-1103	4.02	4.02	4.02	4.02	2	0.29	0.03	0.21	0.00	0.00	22.3
4	540	327	-1216	-568	0	1294	-1323	4.02	4.02	4.02	4.02	2	0.36	0.04	0.22	0.00	0.00	22.3
5	540	-381	-1190	-623	0	1366	-1225	4.02	4.02	4.02	4.02	2	0.37	0.03	0.21	0.00	0.00	22.3
6	540	1353	-1224	-400	0	1009	-1357	4.02	4.02	4.02	4.02	2	0.29	0.04	0.22	0.00	0.00	22.3
7	540	-1007	-1137	-584	0	1249	-1032	4.02	4.02	4.02	4.02	2	0.33	0.03	0.20	0.00	0.00	22.3
8	540	1261	-1235	-448	0	1102	-1394	4.02	4.02	4.02	4.02	2	0.32	0.04	0.22	0.00	0.00	22.3
9	540	-1100	-1147	-632	0	1342	-1069	4.02	4.02	4.02	4.02	2	0.36	0.03	0.20	0.00	0.00	22.3
10	540	635	-1181	-408	0	985	-1201	4.02	4.02	4.02	4.02	2	0.28	0.03	0.21	0.00	0.00	22.3
11	540	-73	-1155	-464	0	1057	-1103	4.02	4.02	4.02	4.02	2	0.29	0.03	0.21	0.00	0.00	22.3
12	540	327	-1216	-568	0	1294	-1323	4.02	4.02	4.02	4.02	2	0.36	0.04	0.22	0.00	0.00	22.3
13	540	-381	-1190	-623	0	1366	-1225	4.02	4.02	4.02	4.02	2	0.37	0.03	0.21	0.00	0.00	22.3
14	540	1353	-1224	-400	0	1009	-1357	4.02	4.02	4.02	4.02	2	0.29	0.04	0.22	0.00	0.00	22.3
15	540	-1007	-1137	-584	0	1249	-1032	4.02	4.02	4.02	4.02	2	0.33	0.03	0.20	0.00	0.00	22.3
16	540	1261	-1235	-448	0	1102	-1394	4.02	4.02	4.02	4.02	2	0.32	0.04	0.22	0.00	0.00	22.3
17	540	-1100	-1147	-632	0	1342	-1069	4.02	4.02	4.02	4.02	2	0.36	0.03	0.20	0.00	0.00	22.3
18	540	1460	-1499	-1186	0	2762	-1428	4.02	4.02	4.02	4.02	3	0.71	0.04	0.27	0.00	0.00	22.3
19	540	-21	-1656	-1552	0	3445	-1978	4.02	4.02	4.02	4.02	3	0.85	0.05	0.29	0.00	0.00	22.3
20	540	658	-1618	-1471	0	3131	-1775	4.02	4.02	4.02	4.02	3	0.78	0.05	0.29	0.00	0.00	22.3
37	540	1770	-1435	-837	0	2022	-1202	4.02	4.02	4.02	4.02	3	0.52	0.04	0.26	0.00	0.00	22.3
38	540	-698	-1695	-1447	0	3160	-2120	4.02	4.02	4.02	4.02	3	0.76	0.05	0.30	0.00	0.00	22.3
39	540	433	-1634	-1311	0	2637	-1780	4.02	4.02	4.02	4.02	3	0.66	0.05	0.29	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	600	165	-1937	-671	0	1930	-1840	4.02	4.02	4.02	4.02	3	0.48	0.06	0.35	0.00	0.00	22.3
2	600	635	-1485	-408	0	1230	-1403	4.02	4.02	4.02	4.02	2	0.35	0.04	0.26	0.00	0.00	22.3
3	600	-73	-1459	-464	0	1335	-1303	4.02	4.02	4.02	4.02	2	0.37	0.04	0.26	0.00	0.00	22.3
4	600	327	-1520	-568	0	1635	-1528	4.02	4.02	4.02	4.02	2	0.46	0.04	0.27	0.00	0.00	22.3
5	600	-381	-1494	-623	0	1740	-1428	4.02	4.02	4.02	4.02	2	0.47	0.04	0.26	0.00	0.00	22.3
6	600	1353	-1528	-400	0	1249	-1563	4.02	4.02	4.02	4.02	2	0.36	0.04	0.27	0.00	0.00	22.3
7	600	-1007	-1441	-584	0	1599	-1230	4.02	4.02	4.02	4.02	2	0.43	0.04	0.25	0.00	0.00	22.3
8	600	1261	-1539	-448	0	1371	-1601	4.02	4.02	4.02	4.02	2	0.39	0.04	0.27	0.00	0.00	22.3
9	600	-1100	-1451	-632	0	1721	-1268	4.02	4.02	4.02	4.02	2	0.46	0.04	0.25	0.00	0.00	22.3
10	600	635	-1485	-408	0	1230	-1403	4.02	4.02	4.02	4.02	2	0.35	0.04	0.26	0.00	0.00	22.3
11	600	-73	-1459	-464	0	1335	-1303	4.02	4.02	4.02	4.02	2	0.37	0.04	0.26	0.00	0.00	22.3
12	600	327	-1520	-568	0	1635	-1528	4.02	4.02	4.02	4.02	2	0.46	0.04	0.27	0.00	0.00	22.3
13	600	-381	-1494	-623	0	1740	-1428	4.02	4.02	4.02	4.02	2	0.47	0.04	0.26	0.00	0.00	22.3
14	600	1353	-1528	-400	0	1249	-1563	4.02	4.02	4.02	4.02	2	0.36	0.04	0.27	0.00	0.00	22.3
15	600	-1007	-1441	-584	0	1599	-1230	4.02	4.02	4.02	4.02	2	0.43	0.04	0.25	0.00	0.00	22.3
16	600	1261	-1539	-448	0	1371	-1601	4.02	4.02	4.02	4.02	2	0.39	0.04	0.27	0.00	0.00	22.3
17	600	-1100	-1451	-632	0	1721	-1268	4.02	4.02	4.02	4.02	2	0.46	0.04	0.25	0.00	0.00	22.3
18	600	1460	-1895	-1186	0	3474	-1687	4.02	4.02	4.02	4.02	3	0.89	0.05	0.34	0.00	0.00	22.3
19	600	-21	-2051	-1552	0	4376	-2252	6.03	4.02	4.02	4.02	3	0.76	0.06	0.37	0.00	0.00	22.3
20	600	658	-2014	-1471	0	4013	-2045	6.03	4.02	4.02	4.02	3	0.71	0.06	0.36	0.00	0.00	22.3
37	600	1770	-1830	-837	0	2524	-1455	4.02	4.02	4.02	4.02	3	0.65	0.05	0.33	0.00	0.00	22.3
38	600	-698	-2091	-1447	0	4029	-2398	4.02	4.02	4.02	4.02	3	0.97	0.06	0.37	0.00	0.00	22.3
39	600	433	-2029	-1311	0	3424	-2052	4.02	4.02	4.02	4.02	3	0.85	0.06	0.36	0.00	0.00	22.3

apost= 2.01 aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

Nome travata: **Trave_403_IP1** Descrizione: **Trave_4 7-6-5-4-3-2-1**
ASTA NUM. 10 NI 215 NF 228 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y Permanente qy tot.
qy medio: 375.00 132.00 507.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-491	1878	-472	0	-1306	-1648	4.02	4.02	4.02	4.02	3	0.32	0.05	0.33	0.00	0.00	22.3
2	0	282	1429	-253	0	-695	-1231	4.02	4.02	4.02	4.02	2	0.19	0.04	0.25	0.00	0.00	22.3
3	0	-372	1486	-286	0	-791	-1396	4.02	4.02	4.02	4.02	2	0.22	0.04	0.26	0.00	0.00	22.3
4	0	-383	1404	-440	0	-1218	-1140	4.02	4.02	4.02	4.02	2	0.33	0.04	0.25	0.00	0.00	22.3
5	0	-1037	1460	-473	0	-1313	-1305	4.02	4.02	4.02	4.02	2	0.35	0.04	0.25	0.00	0.00	22.3
6	0	813	1355	-280	0	-767	-1007	4.02	4.02	4.02	4.02	2	0.22	0.04	0.24	0.00	0.00	22.3
7	0	-1369	1542	-390	0	-1085	-1557	4.02	4.02	4.02	4.02	2	0.29	0.04	0.27	0.00	0.00	22.3
8	0	613	1347	-336	0	-923	-979	4.02	4.02	4.02	4.02	2	0.26	0.04	0.24	0.00	0.00	22.3
9	0	-1568	1535	-446	0	-1242	-1529	4.02	4.02	4.02	4.02	2	0.33	0.04	0.26	0.00	0.00	22.3
10	0	282	1429	-253	0	-695	-1231	4.02	4.02	4.02	4.02	2	0.19	0.04	0.25	0.00	0.00	22.3
11	0	-372	1486	-286	0	-791	-1396	4.02	4.02	4.02	4.02	2	0.22	0.04	0.26	0.00	0.00	22.3
12	0	-383	1404	-440	0	-1218	-1140	4.02	4.02	4.02	4.02	2	0.33	0.04	0.25	0.00	0.00	22.3
13	0	-1037	1460	-473	0	-1313	-1305	4.02	4.02	4.02	4.02	2	0.35	0.04	0.25	0.00	0.00	22.3
14	0	813	1355	-280	0	-767	-1007	4.02	4.02	4.02	4.02	2	0.22	0.04	0.24	0.00	0.00	22.3

15	0	-1369	1542	-390	0	-1085	-1557	4.02	4.02	4.02	4.02	2	0.29	0.04	0.27	0.00	0.00	22.3
16	0	613	1347	-336	0	-923	-979	4.02	4.02	4.02	4.02	2	0.26	0.04	0.24	0.00	0.00	22.3
17	0	-1568	1535	-446	0	-1242	-1529	4.02	4.02	4.02	4.02	2	0.33	0.04	0.26	0.00	0.00	22.3
18	0	440	1801	-693	0	-1907	-1396	4.02	4.02	4.02	4.02	3	0.47	0.05	0.32	0.00	0.00	22.3
19	0	-1879	1754	-1169	0	-3216	-1236	4.02	4.02	4.02	4.02	3	0.75	0.05	0.30	0.00	0.00	22.3
20	0	-909	1848	-913	0	-2498	-1506	4.02	4.02	4.02	4.02	3	0.60	0.05	0.32	0.00	0.00	22.3
37	0	1286	1850	-386	0	-1064	-1559	4.02	4.02	4.02	4.02	3	0.27	0.05	0.33	0.00	0.00	22.3
38	0	-2580	1771	-1179	0	-3246	-1291	4.02	4.02	4.02	4.02	3	0.75	0.05	0.30	0.00	0.00	22.3
39	0	-964	1927	-753	0	-2049	-1741	4.02	4.02	4.02	4.02	3	0.49	0.06	0.34	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	60	-491	1483	-472	0	-1023	-1390	4.02	4.02	4.02	4.02	3	0.25	0.04	0.26	0.00	0.00	22.3
2	60	282	1125	-253	0	-543	-1034	4.02	4.02	4.02	4.02	2	0.16	0.03	0.20	0.00	0.00	22.3
3	60	-372	1182	-286	0	-619	-1194	4.02	4.02	4.02	4.02	2	0.18	0.03	0.21	0.00	0.00	22.3
4	60	-383	1100	-440	0	-954	-946	4.02	4.02	4.02	4.02	2	0.26	0.03	0.19	0.00	0.00	22.3
5	60	-1037	1156	-473	0	-1029	-1105	4.02	4.02	4.02	4.02	2	0.27	0.03	0.20	0.00	0.00	22.3
6	60	813	1051	-280	0	-598	-817	4.02	4.02	4.02	4.02	2	0.17	0.03	0.19	0.00	0.00	22.3
7	60	-1369	1238	-390	0	-851	-1349	4.02	4.02	4.02	4.02	2	0.23	0.04	0.21	0.00	0.00	22.3
8	60	613	1043	-336	0	-721	-790	4.02	4.02	4.02	4.02	2	0.20	0.03	0.19	0.00	0.00	22.3
9	60	-1568	1231	-446	0	-974	-1322	4.02	4.02	4.02	4.02	2	0.26	0.04	0.21	0.00	0.00	22.3
10	60	282	1125	-253	0	-543	-1034	4.02	4.02	4.02	4.02	2	0.16	0.03	0.20	0.00	0.00	22.3
11	60	-372	1182	-286	0	-619	-1194	4.02	4.02	4.02	4.02	2	0.18	0.03	0.21	0.00	0.00	22.3
12	60	-383	1100	-440	0	-954	-946	4.02	4.02	4.02	4.02	2	0.26	0.03	0.19	0.00	0.00	22.3
13	60	-1037	1156	-473	0	-1029	-1105	4.02	4.02	4.02	4.02	2	0.27	0.03	0.20	0.00	0.00	22.3
14	60	813	1051	-280	0	-598	-817	4.02	4.02	4.02	4.02	2	0.17	0.03	0.19	0.00	0.00	22.3
15	60	-1369	1238	-390	0	-851	-1349	4.02	4.02	4.02	4.02	2	0.23	0.04	0.21	0.00	0.00	22.3
16	60	613	1043	-336	0	-721	-790	4.02	4.02	4.02	4.02	2	0.20	0.03	0.19	0.00	0.00	22.3
17	60	-1568	1231	-446	0	-974	-1322	4.02	4.02	4.02	4.02	2	0.26	0.04	0.21	0.00	0.00	22.3
18	60	440	1406	-693	0	-1491	-1145	4.02	4.02	4.02	4.02	3	0.37	0.04	0.25	0.00	0.00	22.3
19	60	-1879	1358	-1169	0	-2515	-990	4.02	4.02	4.02	4.02	3	0.59	0.04	0.23	0.00	0.00	22.3
20	60	-909	1452	-913	0	-1950	-1251	4.02	4.02	4.02	4.02	3	0.47	0.04	0.25	0.00	0.00	22.3
37	60	1286	1455	-386	0	-833	-1304	4.02	4.02	4.02	4.02	3	0.21	0.04	0.26	0.00	0.00	22.3
38	60	-2580	1376	-1179	0	-2539	-1043	4.02	4.02	4.02	4.02	3	0.58	0.04	0.23	0.00	0.00	22.3
39	60	-964	1532	-753	0	-1597	-1479	4.02	4.02	4.02	4.02	3	0.38	0.04	0.27	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	120	-491	1087	-472	0	-739	682	4.02	4.02	4.02	4.02	3	0.18	0.03	0.19	0.00	0.00	22.3
2	120	282	821	-253	0	-391	535	4.02	4.02	4.02	4.02	2	0.11	0.02	0.15	0.00	0.00	22.3
3	120	-372	878	-286	0	-448	466	4.02	4.02	4.02	4.02	2	0.12	0.03	0.15	0.00	0.00	22.3
4	120	-383	796	-440	0	-690	582	4.02	4.02	4.02	4.02	2	0.19	0.02	0.14	0.00	0.00	22.3
5	120	-1037	852	-473	0	-745	513	4.02	4.02	4.02	4.02	2	0.20	0.02	0.15	0.00	0.00	22.3
6	120	813	747	-280	0	-430	632	4.02	4.02	4.02	4.02	2	0.12	0.02	0.13	0.00	0.00	22.3
7	120	-1369	934	-390	0	-617	-544	4.02	4.02	4.02	4.02	2	0.16	0.03	0.16	0.00	0.00	22.3
8	120	613	739	-336	0	-519	646	4.02	4.02	4.02	4.02	2	0.15	0.02	0.13	0.00	0.00	22.3
9	120	-1568	927	-446	0	-707	-521	4.02	4.02	4.02	4.02	2	0.19	0.03	0.16	0.00	0.00	22.3
10	120	282	821	-253	0	-391	535	4.02	4.02	4.02	4.02	2	0.11	0.02	0.15	0.00	0.00	22.3
11	120	-372	878	-286	0	-448	466	4.02	4.02	4.02	4.02	2	0.12	0.03	0.15	0.00	0.00	22.3
12	120	-383	796	-440	0	-690	582	4.02	4.02	4.02	4.02	2	0.19	0.02	0.14	0.00	0.00	22.3
13	120	-1037	852	-473	0	-745	513	4.02	4.02	4.02	4.02	2	0.20	0.02	0.15	0.00	0.00	22.3
14	120	813	747	-280	0	-430	632	4.02	4.02	4.02	4.02	2	0.12	0.02	0.13	0.00	0.00	22.3
15	120	-1369	934	-390	0	-617	-544	4.02	4.02	4.02	4.02	2	0.16	0.03	0.16	0.00	0.00	22.3
16	120	613	739	-336	0	-519	646	4.02	4.02	4.02	4.02	2	0.15	0.02	0.13	0.00	0.00	22.3
17	120	-1568	927	-446	0	-707	-521	4.02	4.02	4.02	4.02	2	0.19	0.03	0.16	0.00	0.00	22.3
18	120	440	1010	-693	0	-1075	802	4.02	4.02	4.02	4.02	3	0.27	0.03	0.18	0.00	0.00	22.3
19	120	-1879	963	-1169	0	-1813	882	4.02	4.02	4.02	4.02	3	0.42	0.04	0.18	0.00	0.00	22.3
20	120	-909	1057	-913	0	-1402	772	4.02	4.02	4.02	4.02	3	0.34	0.03	0.18	0.00	0.00	22.3
37	120	1286	1059	-386	0	-601	723	4.02	4.02	4.02	4.02	3	0.15	0.03	0.19	0.00	0.00	22.3
38	120	-2580	980	-1179	0	-1831	856	4.02	4.02	4.02	4.02	3	0.42	0.04	0.18	0.00	0.00	22.3
39	120	-964	1136	-753	0	-1145	672	4.02	4.02	4.02	4.02	3	0.27	0.03	0.20	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	180	-491	692	-472	0	-456	1015	4.02	4.02	4.02	4.02	3	0.14	0.02	0.12	0.00	0.00	22.3
2	180	282	516	-253	0	-239	776	4.02	4.02	4.02	4.02	2	0.12	0.01	0.09	0.00	0.00	22.3
3	180	-372	573	-286	0	-276	747	4.02	4.02	4.02	4.02	2	0.11	0.02	0.10	0.00	0.00	22.3
4	180	-383	491	-440	0	-425	790	4.02	4.02	4.02	4.02	2	0.12	0.01	0.09	0.00	0.00	22.3
5	180	-1037	547	-473	0	-462	779	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
6	180	813	442	-280	0	-262	784	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
7	180	-1369	629	-390	0	-383	717	4.02	4.02	4.02	4.02	2	0.10	0.02	0.11	0.00	0.00	22.3
8	180	613	434	-336	0	-318	793	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
9	180	-1568	622	-446	0	-439	727	4.02	4.02	4.02	4.02	2	0.12	0.02	0.11	0.00	0.00	22.3
10	180	282	516	-253	0	-239	776	4.02	4.02	4.02	4.02	2	0.12	0.01	0.09	0.00	0.00	22.3
11	180	-372	573	-286	0	-276	747	4.02	4.02	4.02	4.02	2	0.11	0.02	0.10	0.00	0.00	22.3
12	180	-383	491	-440	0	-425	790	4.02	4.02	4.02	4.02	2	0.12	0.01	0.09	0.00	0.00	22.3
13	180	-1037	547	-473	0	-462	779	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
14	180	813	442	-280	0	-262	784	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
15	180	-1369	629	-390	0	-383	717	4.02	4.02	4.02	4.02	2	0.10	0.02	0.11	0.00	0.00	22.3
16	180	613	434	-336	0	-318	793	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
17	180	-1568	622	-446	0	-439	727	4.02	4.02	4.02	4.02	2	0.12	0.02	0.11	0.00	0.00	22.3
18	180	440	615	-693	0	-660	1042	4.02	4.02	4.02	4.02	3	0.16	0.02	0.11	0.00	0.00	22.3
19	180	-1879	567	-1169	0	-1112	1076	4.02	4.02	4.02	4.02	3	0.26	0.04	0.18	0.00	0.00	22.3
20	180	-909	661	-913	0	-854	1071	4.02	4.02	4.02	4.02	3	0.20	0.03	0.14	0.00	0.00	22.3
37	180	1286	664	-386	0	-370	1025	4.02	4.02	4.02	4.02	3	0.15	0.02	0.12	0.00	0.00	22.3
38	180	-2580	585	-1179	0	-1124	1062	4.02	4.02	4.02	4.02	3	0.26	0.04	0.18	0.00	0.00	22.3
39	180	-964	741	-753	0	-693	1035	4.02	4.02	4.02	4.02	3	0.17	0.02	0.13	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	240	-491	296	-472	0	-173	1020	4.02	4.02	4.02	4.02	3	0.14	0.01	0.08	0.00	0.00	22.3
2	240	282	212	-253	0	-87	776	4.02	4.02	4.02	4.02	2	0.12	0.01	0.04	0.00	0.00	22.3
3	240	-372	269	-286	0	-104	780	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
4	240	-383	187	-440	0	-161	790	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
5	240	-1037	243	-473	0	-178	794	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
6	240	813	138	-280	0	-94	784	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
7	240	-1369	325	-390	0	-149	789	4.02	4.02	4.02	4.02	2	0.11	0.01	0.06	0.00	0.00	22.3
8	240	613	130	-336	0	-116	793	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
9	240	-1568	318	-446	0	-172	794	4.02	4.02	4.02	4.02	2	0.11	0.01	0.07	0.00	0.00	22.3
10	240	282	212	-253	0	-87	776	4.02	4.02	4.02	4.02	2	0.12	0.01	0.04	0.00	0.00	22.3
11	240	-372	269	-286	0	-104	780	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
12	240	-383	187	-440	0	-161	790	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
13	240	-1037	243	-473	0	-178	794	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
14	240	813	138	-280	0	-94	784	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
15	240	-1369	325	-390	0	-149	789	4.02	4.02	4.02	4.02	2	0.11	0.01	0.06	0.00	0.00	22.3
16	240	613	130	-336	0	-116	793	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
17	240	-1568	318	-446	0	-172	794	4.02	4.02	4.02	4.02	2	0.11	0.01	0.07	0.00	0.00	22.3
18	240	440	219	-693	0	-244	1042	4.02	4.02	4.02	4.02	3	0.15	0.02	0.11	0.00	0.00	22.3
19	240	-1879	172	-1169	0	-411	1076	4.02	4.02	4.02	4.02	3	0.15	0.04	0.18	0.00	0.00	22.3
20	240	-909	266	-913	0	-306	1071	4.02	4.02	4.02	4.02	3	0.15	0.03	0.14	0.00	0.00	22.3

37	240	1286	268	-386	0	-138	1025	4.02	4.02	4.02	4.02	3	0.15	0.01	0.06	0.00	0.00	22.3
38	240	-2580	189	-1179	0	-417	1062	4.02	4.02	4.02	4.02	3	0.14	0.04	0.18	0.00	0.00	22.3
39	240	-964	345	-753	0	-241	1074	4.02	4.02	4.02	4.02	3	0.15	0.02	0.12	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	300	-491	-99	-472	0	110	1020	4.02	4.02	4.02	4.02	3	0.14	0.01	0.08	0.00	0.00	22.3
2	300	282	-92	-253	0	64	776	4.02	4.02	4.02	4.02	2	0.12	0.01	0.04	0.00	0.00	22.3
3	300	-372	-35	-286	0	67	780	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
4	300	-383	-117	-440	0	103	790	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
5	300	-1037	-61	-473	0	106	794	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
6	300	813	-166	-280	0	75	784	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
7	300	-1369	21	-390	0	85	789	4.02	4.02	4.02	4.02	2	0.11	0.01	0.06	0.00	0.00	22.3
8	300	613	-174	-336	0	86	793	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
9	300	-1568	14	-446	0	96	794	4.02	4.02	4.02	4.02	2	0.11	0.01	0.07	0.00	0.00	22.3
10	300	282	-92	-253	0	64	776	4.02	4.02	4.02	4.02	2	0.12	0.01	0.04	0.00	0.00	22.3
11	300	-372	-35	-286	0	67	780	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
12	300	-383	-117	-440	0	103	790	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
13	300	-1037	-61	-473	0	106	794	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
14	300	813	-166	-280	0	75	784	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
15	300	-1369	21	-390	0	85	789	4.02	4.02	4.02	4.02	2	0.11	0.01	0.06	0.00	0.00	22.3
16	300	613	-174	-336	0	86	793	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
17	300	-1568	14	-446	0	96	794	4.02	4.02	4.02	4.02	2	0.11	0.01	0.07	0.00	0.00	22.3
18	300	440	-176	-693	0	172	1042	4.02	4.02	4.02	4.02	3	0.15	0.02	0.11	0.00	0.00	22.3
19	300	-1879	-224	-1169	0	290	1076	4.02	4.02	4.02	4.02	3	0.15	0.04	0.18	0.00	0.00	22.3
20	300	-909	-130	-913	0	243	1071	4.02	4.02	4.02	4.02	3	0.15	0.03	0.14	0.00	0.00	22.3
37	300	1286	-127	-386	0	93	1025	4.02	4.02	4.02	4.02	3	0.15	0.01	0.06	0.00	0.00	22.3
38	300	-2580	-206	-1179	0	290	1062	4.02	4.02	4.02	4.02	3	0.14	0.04	0.18	0.00	0.00	22.3
39	300	-964	-50	-753	0	210	1074	4.02	4.02	4.02	4.02	3	0.15	0.02	0.12	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	360	-491	-494	-472	0	394	1020	4.02	4.02	4.02	4.02	3	0.14	0.01	0.09	0.00	0.00	22.3
2	360	282	-396	-253	0	216	776	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
3	360	-372	-339	-286	0	239	780	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
4	360	-383	-421	-440	0	367	790	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
5	360	-1037	-365	-473	0	390	794	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
6	360	813	-470	-280	0	243	784	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
7	360	-1369	-283	-390	0	318	789	4.02	4.02	4.02	4.02	2	0.11	0.01	0.06	0.00	0.00	22.3
8	360	613	-478	-336	0	288	793	4.02	4.02	4.02	4.02	2	0.12	0.01	0.09	0.00	0.00	22.3
9	360	-1568	-290	-446	0	364	794	4.02	4.02	4.02	4.02	2	0.11	0.01	0.07	0.00	0.00	22.3
10	360	282	-396	-253	0	216	776	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
11	360	-372	-339	-286	0	239	780	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
12	360	-383	-421	-440	0	367	790	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
13	360	-1037	-365	-473	0	390	794	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
14	360	813	-470	-280	0	243	784	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
15	360	-1369	-283	-390	0	318	789	4.02	4.02	4.02	4.02	2	0.11	0.01	0.06	0.00	0.00	22.3
16	360	613	-478	-336	0	288	793	4.02	4.02	4.02	4.02	2	0.12	0.01	0.09	0.00	0.00	22.3
17	360	-1568	-290	-446	0	364	794	4.02	4.02	4.02	4.02	2	0.11	0.01	0.07	0.00	0.00	22.3
18	360	440	-571	-693	0	588	1042	4.02	4.02	4.02	4.02	3	0.15	0.02	0.11	0.00	0.00	22.3
19	360	-1879	-619	-1169	0	992	1076	4.02	4.02	4.02	4.02	3	0.23	0.04	0.18	0.00	0.00	22.3
20	360	-909	-525	-913	0	791	1071	4.02	4.02	4.02	4.02	3	0.19	0.03	0.14	0.00	0.00	22.3
37	360	1286	-522	-386	0	324	1025	4.02	4.02	4.02	4.02	3	0.15	0.02	0.09	0.00	0.00	22.3
38	360	-2580	-601	-1179	0	998	1062	4.02	4.02	4.02	4.02	3	0.23	0.04	0.18	0.00	0.00	22.3
39	360	-964	-445	-753	0	662	1074	4.02	4.02	4.02	4.02	3	0.16	0.02	0.12	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	420	-491	-890	-472	0	677	877	4.02	4.02	4.02	4.02	3	0.16	0.03	0.16	0.00	0.00	22.3
2	420	282	-700	-253	0	368	655	4.02	4.02	4.02	4.02	2	0.10	0.02	0.12	0.00	0.00	22.3
3	420	-372	-643	-286	0	411	698	4.02	4.02	4.02	4.02	2	0.11	0.02	0.11	0.00	0.00	22.3
4	420	-383	-725	-440	0	631	652	4.02	4.02	4.02	4.02	2	0.17	0.02	0.13	0.00	0.00	22.3
5	420	-1037	-669	-473	0	674	695	4.02	4.02	4.02	4.02	2	0.18	0.02	0.12	0.00	0.00	22.3
6	420	813	-774	-280	0	411	604	4.02	4.02	4.02	4.02	2	0.12	0.02	0.14	0.00	0.00	22.3
7	420	-1369	-587	-390	0	552	747	4.02	4.02	4.02	4.02	2	0.15	0.02	0.10	0.00	0.00	22.3
8	420	613	-782	-336	0	490	603	4.02	4.02	4.02	4.02	2	0.14	0.02	0.14	0.00	0.00	22.3
9	420	-1568	-594	-446	0	631	746	4.02	4.02	4.02	4.02	2	0.17	0.02	0.10	0.00	0.00	22.3
10	420	282	-700	-253	0	368	655	4.02	4.02	4.02	4.02	2	0.10	0.02	0.12	0.00	0.00	22.3
11	420	-372	-643	-286	0	411	698	4.02	4.02	4.02	4.02	2	0.11	0.02	0.11	0.00	0.00	22.3
12	420	-383	-725	-440	0	631	652	4.02	4.02	4.02	4.02	2	0.17	0.02	0.13	0.00	0.00	22.3
13	420	-1037	-669	-473	0	674	695	4.02	4.02	4.02	4.02	2	0.18	0.02	0.12	0.00	0.00	22.3
14	420	813	-774	-280	0	411	604	4.02	4.02	4.02	4.02	2	0.12	0.02	0.14	0.00	0.00	22.3
15	420	-1369	-587	-390	0	552	747	4.02	4.02	4.02	4.02	2	0.15	0.02	0.10	0.00	0.00	22.3
16	420	613	-782	-336	0	490	603	4.02	4.02	4.02	4.02	2	0.14	0.02	0.14	0.00	0.00	22.3
17	420	-1568	-594	-446	0	631	746	4.02	4.02	4.02	4.02	2	0.17	0.02	0.10	0.00	0.00	22.3
18	420	440	-967	-693	0	1004	846	4.02	4.02	4.02	4.02	3	0.25	0.03	0.17	0.00	0.00	22.3
19	420	-1879	-1014	-1169	0	1693	832	4.02	4.02	4.02	4.02	3	0.40	0.04	0.18	0.00	0.00	22.3
20	420	-909	-920	-913	0	1339	907	4.02	4.02	4.02	4.02	3	0.32	0.03	0.16	0.00	0.00	22.3
37	420	1286	-918	-386	0	556	863	4.02	4.02	4.02	4.02	3	0.14	0.03	0.16	0.00	0.00	22.3
38	420	-2580	-997	-1179	0	1705	840	4.02	4.02	4.02	4.02	3	0.39	0.04	0.18	0.00	0.00	22.3
39	420	-964	-841	-753	0	1114	965	4.02	4.02	4.02	4.02	3	0.27	0.02	0.15	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	480	-491	-1285	-472	0	960	-876	4.02	4.02	4.02	4.02	3	0.23	0.04	0.23	0.00	0.00	22.3
2	480	282	-1005	-253	0	520	-719	4.02	4.02	4.02	4.02	2	0.14	0.03	0.18	0.00	0.00	22.3
3	480	-372	-948	-286	0	582	-585	4.02	4.02	4.02	4.02	2	0.16	0.03	0.17	0.00	0.00	22.3
4	480	-383	-1030	-440	0	896	-763	4.02	4.02	4.02	4.02	2	0.24	0.03	0.18	0.00	0.00	22.3
5	480	-1037	-974	-473	0	957	-630	4.02	4.02	4.02	4.02	2	0.26	0.03	0.17	0.00	0.00	22.3
6	480	813	-1079	-280	0	579	-890	4.02	4.02	4.02	4.02	2	0.16	0.03	0.19	0.00	0.00	22.3
7	480	-1369	-892	-390	0	786	458	4.02	4.02	4.02	4.02	2	0.21	0.03	0.15	0.00	0.00	22.3
8	480	613	-1087	-336	0	692	-904	4.02	4.02	4.02	4.02	2	0.19	0.03	0.19	0.00	0.00	22.3
9	480	-1568	-899	-446	0	899	-457	4.02	4.02	4.02	4.02	2	0.24	0.03	0.15	0.00	0.00	22.3
10	480	282	-1005	-253	0	520	-719	4.02	4.02	4.02	4.02	2	0.14	0.03	0.18	0.00	0.00	22.3
11	480	-372	-948	-286	0	582	-585	4.02	4.02	4.02	4.02	2	0.16	0.03	0.17	0.00	0.00	22.3
12	480	-383	-1030	-440	0	896	-763	4.02	4.02	4.02	4.02	2	0.24	0.03	0.18	0.00	0.00	22.3
13	480	-1037	-974	-473	0	957	-630	4.02	4.02	4.02	4.02	2	0.26	0.03	0.17	0.00	0.00	22.3
14	480	813	-1079	-280	0	579	-890	4.02	4.02	4.02	4.02	2	0.16	0.03	0.19	0.00	0.00	22.3
15	480	-1369	-892	-390	0	786	458	4.02	4.02	4.02	4.02	2	0.21	0.03	0.15	0.00	0.00	22.3
16	480	613	-1087	-336	0	692	-904	4.02	4.02	4.02	4.02	2	0.19	0.03	0.19	0.00	0.00	22.3
17	480	-1568	-899	-446	0	899	-457	4.02	4.02	4.02	4.02	2	0.24	0.03	0.15	0.00	0.00	22.3
18	480	440	-1362	-693	0	1419	-1032	4.02	4.02	4.02	4.02	3	0.35	0.04	0.24	0.00	0.00	22.3
19	480	-1879	-1410	-1169	0	2394	-1123	4.02	4.02	4.02	4.02	3	0.56	0.04	0.24	0.00	0.00	22.3
20	480	-909	-1316	-913	0	1887	-896	4.02	4.02	4.02	4.02	3	0.45	0.04	0.23	0.00	0.00	22.3
37	480	1286	-1313	-386	0	787	-936	4.02	4.02	4.02	4.02	3	0.20	0.04	0.23	0.00	0.00	22.3
38	480	-2580	-1392	-1179	0	2412	-1086	4.02	4.02	4.02	4.02	3	0.56	0.04	0.23	0.00	0.00	22.3
39	480	-964	-1236	-753	0	1566	-709	4.02	4.02	4.02	4.02	3	0.38	0.04	0.22	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	540	-491	-1681	-472	0	1244	-1967	4.02	4.02	4.02	4.02	3	0.30	0.05	0.30	0.00	0.00	22.3
2	540	282	-1309	-253	0	672	-1567	4.02	4.02	4.02	4.02	2	0.24	0.04	0.23	0.00	0.00	22.3
3	540	-372	-1252	-286	0	754	-1399	4.02	4.02	4.02	4.02	2	0.21	0.04	0.22	0.00	0.00	22.3
4	540	-383	-1334	-440	0	1160	-1627	4.02	4.02	4.02	4.02	2	0.32	0.04	0.24	0.00	0.00	22.3
5	540	-1037	-1278	-473	0	1241	-1459	4.02	4.02	4.02	4.02	2	0.33	0.04	0.22	0.00	0.00	22.3
6	540	813	-1383	-280	0	748	-1783	4.02	4.02	4.02	4.02	2	0.28	0.04	0.25	0.00	0.00	22.3
7	540	-1369	-1196	-390	0	1020	-1225	4.02	4.02	4.02	4.02	2	0.27	0.03	0.21	0.00	0.00	22.3
8	540	613	-1391	-336	0	894	-1801	4.02	4.02	4.02	4.02	2	0.28	0.04	0.25	0.00	0.00	22.3
9	540	-1568	-1203	-446	0	1166	-1242	4.02	4.02	4.02	4.02	2	0.31	0.03	0.21	0.00	0.00	22.3
10	540	282	-1309	-253	0	672	-1567	4.02	4.02	4.02	4.02	2	0.24	0.04	0.23	0.00	0.00	22.3
11	540	-372	-1252	-286	0	754	-1399	4.02	4.02	4.02	4.02	2	0.21	0.04	0.22	0.00	0.00	22.3
12	540	-383	-1334	-440	0	1160	-1627	4.02	4.02	4.02	4.02	2	0.32	0.04	0.24	0.00	0.00	22.3
13	540	-1037	-1278	-473	0	1241	-1459	4.02	4.02	4.02	4.02	2	0.33	0.04	0.22	0.00	0.00	22.3
14	540	813	-1383	-280	0	748	-1783	4.02	4.02	4.02	4.02	2	0.28	0.04	0.25	0.00	0.00	22.3
15	540	-1369	-1196	-390	0	1020	-1225	4.02	4.02	4.02	4.02	2	0.27	0.03	0.21	0.00	0.00	22.3
16	540	613	-1391	-336	0	894	-1801	4.02	4.02	4.02	4.02	2	0.28	0.04	0.25	0.00	0.00	22.3
17	540	-1568	-1203	-446	0	1166	-1242	4.02	4.02	4.02	4.02	2	0.31	0.03	0.21	0.00	0.00	22.3
18	540	440	-1758	-693	0	1835	-2168	4.02	4.02	4.02	4.02	3	0.46	0.05	0.31	0.00	0.00	22.3
19	540	-1879	-1806	-1169	0	3096	-2287	4.02	4.02	4.02	4.02	3	0.72	0.05	0.31	0.00	0.00	22.3
20	540	-909	-1711	-913	0	2435	-2005	4.02	4.02	4.02	4.02	3	0.58	0.05	0.30	0.00	0.00	22.3
37	540	1286	-1709	-386	0	1019	-2043	4.02	4.02	4.02	4.02	3	0.30	0.05	0.30	0.00	0.00	22.3
38	540	-2580	-1788	-1179	0	3120	-2241	4.02	4.02	4.02	4.02	3	0.72	0.05	0.30	0.00	0.00	22.3
39	540	-964	-1632	-753	0	2018	-1770	4.02	4.02	4.02	4.02	3	0.48	0.05	0.28	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	600	-491	-2076	-472	0	1527	-2243	4.02	4.02	4.02	4.02	3	0.37	0.06	0.37	0.00	0.00	22.3
2	600	282	-1613	-253	0	824	-1781	4.02	4.02	4.02	4.02	2	0.27	0.05	0.29	0.00	0.00	22.3
3	600	-372	-1556	-286	0	926	-1608	4.02	4.02	4.02	4.02	2	0.25	0.05	0.27	0.00	0.00	22.3
4	600	-383	-1638	-440	0	1424	-1843	4.02	4.02	4.02	4.02	2	0.39	0.05	0.29	0.00	0.00	22.3
5	600	-1037	-1582	-473	0	1525	-1670	4.02	4.02	4.02	4.02	2	0.41	0.05	0.27	0.00	0.00	22.3
6	600	813	-1687	-280	0	916	-2004	4.02	4.02	4.02	4.02	2	0.31	0.05	0.30	0.00	0.00	22.3
7	600	-1369	-1500	-390	0	1254	-1428	4.02	4.02	4.02	4.02	2	0.33	0.04	0.26	0.00	0.00	22.3
8	600	613	-1695	-336	0	1096	-2023	4.02	4.02	4.02	4.02	2	0.31	0.05	0.30	0.00	0.00	22.3
9	600	-1568	-1507	-446	0	1434	-1446	4.02	4.02	4.02	4.02	2	0.38	0.04	0.26	0.00	0.00	22.3
10	600	282	-1613	-253	0	824	-1781	4.02	4.02	4.02	4.02	2	0.27	0.05	0.29	0.00	0.00	22.3
11	600	-372	-1556	-286	0	926	-1608	4.02	4.02	4.02	4.02	2	0.25	0.05	0.27	0.00	0.00	22.3
12	600	-383	-1638	-440	0	1424	-1843	4.02	4.02	4.02	4.02	2	0.39	0.05	0.29	0.00	0.00	22.3
13	600	-1037	-1582	-473	0	1525	-1670	4.02	4.02	4.02	4.02	2	0.41	0.05	0.27	0.00	0.00	22.3
14	600	813	-1687	-280	0	916	-2004	4.02	4.02	4.02	4.02	2	0.31	0.05	0.30	0.00	0.00	22.3
15	600	-1369	-1500	-390	0	1254	-1428	4.02	4.02	4.02	4.02	2	0.33	0.04	0.26	0.00	0.00	22.3
16	600	613	-1695	-336	0	1096	-2023	4.02	4.02	4.02	4.02	2	0.31	0.05	0.30	0.00	0.00	22.3
17	600	-1568	-1507	-446	0	1434	-1446	4.02	4.02	4.02	4.02	2	0.38	0.04	0.26	0.00	0.00	22.3
18	600	440	-2153	-693	0	2251	-2452	4.02	4.02	4.02	4.02	3	0.56	0.06	0.38	0.00	0.00	22.3
19	600	-1879	-2201	-1169	0	3797	-2575	4.02	4.02	4.02	4.02	3	0.89	0.06	0.38	0.00	0.00	22.3
20	600	-909	-2107	-913	0	2983	-2284	4.02	4.02	4.02	4.02	3	0.72	0.06	0.37	0.00	0.00	22.3
37	600	1286	-2104	-386	0	1250	-2322	4.02	4.02	4.02	4.02	3	0.35	0.06	0.37	0.00	0.00	22.3
38	600	-2580	-2183	-1179	0	3827	-2527	4.02	4.02	4.02	4.02	3	0.88	0.06	0.37	0.00	0.00	22.3
39	600	-964	-2027	-753	0	2470	-2042	4.02	4.02	4.02	4.02	3	0.59	0.06	0.35	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

Nome travata: **Trave_403_IP1** Descrizione: **Trave_4 7-6-5-4-3-2-1**
ASTA NUM. 11 NI 228 NF 251 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y Permanente qy tot.
qy medio: 375.00 132.00 507.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-1201	1894	-65	0	-58	-1655	4.02	4.02	4.02	4.02	3	0.23	0.05	0.33	0.00	0.00	22.3
2	0	-216	1430	-45	0	-58	-1209	4.02	4.02	4.02	4.02	2	0.18	0.04	0.25	0.00	0.00	22.3
3	0	-763	1491	-48	0	-67	-1386	4.02	4.02	4.02	4.02	2	0.21	0.04	0.26	0.00	0.00	22.3
4	0	-1084	1423	-52	0	-23	-1160	4.02	4.02	4.02	4.02	2	0.17	0.04	0.25	0.00	0.00	22.3
5	0	-1631	1483	-55	0	-31	-1337	4.02	4.02	4.02	4.02	2	0.19	0.04	0.25	0.00	0.00	22.3
6	0	118	1357	-44	0	-36	-986	4.02	4.02	4.02	4.02	2	0.15	0.04	0.24	0.00	0.00	22.3
7	0	-1705	1558	-53	0	-65	-1575	4.02	4.02	4.02	4.02	2	0.23	0.04	0.27	0.00	0.00	22.3
8	0	-142	1355	-47	0	-25	-971	4.02	4.02	4.02	4.02	2	0.15	0.04	0.24	0.00	0.00	22.3
9	0	-1965	1556	-56	0	-54	-1561	4.02	4.02	4.02	4.02	2	0.22	0.04	0.26	0.00	0.00	22.3
10	0	-216	1430	-45	0	-58	-1209	4.02	4.02	4.02	4.02	2	0.18	0.04	0.25	0.00	0.00	22.3
11	0	-763	1491	-48	0	-67	-1386	4.02	4.02	4.02	4.02	2	0.21	0.04	0.26	0.00	0.00	22.3
12	0	-1084	1423	-52	0	-23	-1160	4.02	4.02	4.02	4.02	2	0.17	0.04	0.25	0.00	0.00	22.3
13	0	-1631	1483	-55	0	-31	-1337	4.02	4.02	4.02	4.02	2	0.19	0.04	0.25	0.00	0.00	22.3
14	0	118	1357	-44	0	-36	-986	4.02	4.02	4.02	4.02	2	0.15	0.04	0.24	0.00	0.00	22.3
15	0	-1705	1558	-53	0	-65	-1575	4.02	4.02	4.02	4.02	2	0.23	0.04	0.27	0.00	0.00	22.3
16	0	-142	1355	-47	0	-25	-971	4.02	4.02	4.02	4.02	2	0.15	0.04	0.24	0.00	0.00	22.3
17	0	-1965	1556	-56	0	-54	-1561	4.02	4.02	4.02	4.02	2	0.22	0.04	0.26	0.00	0.00	22.3
18	0	-521	1823	-126	0	-186	-1410	4.02	4.02	4.02	4.02	3	0.20	0.05	0.32	0.00	0.00	22.3
19	0	-3381	1818	-136	0	-61	-1335	4.02	4.02	4.02	4.02	3	0.17	0.05	0.30	0.00	0.00	22.3
20	0	-1908	1906	-134	0	-159	-1634	4.02	4.02	4.02	4.02	3	0.22	0.05	0.32	0.00	0.00	22.3
37	0	674	1849	-101	0	-206	-1527	4.02	4.02	4.02	4.02	3	0.22	0.05	0.33	0.00	0.00	22.3
38	0	-4093	1840	-117	0	3	-1402	4.02	4.02	4.02	4.02	3	0.18	0.05	0.30	0.00	0.00	22.3
39	0	-1638	1986	-114	0	-161	-1901	4.02	4.02	4.02	4.02	3	0.26	0.06	0.34	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	60	-1201	1498	-65	0	-19	-1396	4.02	4.02	4.02	4.02	3	0.19	0.04	0.26	0.00	0.00	22.3
2	60	-216	1126	-45	0	-31	-1012	4.02	4.02	4.02	4.02	2	0.15	0.03	0.20	0.00	0.00	22.3
3	60	-763	1187	-48	0	-38	-1184	4.02	4.02	4.02	4.02	2	0.18	0.03	0.21	0.00	0.00	22.3
4	60	-1084	1119	-52	0	9	-964	4.02	4.02	4.02	4.02	2	0.14	0.03	0.19	0.00	0.00	22.3
5	60	-1631	1179	-55	0	2	-1135	4.02	4.02	4.02	4.02	2	0.16	0.03	0.20	0.00	0.00	22.3
6	60	118	1053	-44	0	-9	-796	4.02	4.02	4.02	4.02	2	0.12	0.03	0.19	0.00	0.00	22.3
7	60	-1705	1254	-53	0	-33	-1366	4.02	4.02	4.02	4.02	2	0.20	0.04	0.21	0.00	0.00	22.3
8	60	-142	1051	-47	0	3	-781	4.02	4.02	4.02	4.02	2	0.12	0.03	0.19	0.00	0.00	22.3
9	60	-1965	1252	-56	0	-21	-1352	4.02	4.02	4.02	4.02	2	0.19	0.04	0.21	0.00	0.00	22.3
10	60	-216	1126	-45	0	-31	-1012	4.02	4.02	4.02	4.02	2	0.15	0.03	0.20	0.00	0.00	22.3
11	60	-763	1187	-48	0	-38	-1184	4.02	4.02	4.02	4.02	2	0.18	0.03	0.21	0.00	0.00	22.3
12	60	-1084	1119	-52	0	9	-964	4.02	4.02	4.02	4.02	2	0.14	0.03	0.19	0.00	0.00	22.3
13	60	-1631	1179	-55	0	2	-1135	4.02	4.02	4.02	4.02	2	0.16	0.03	0.20	0.00	0.00	22.3
14	60	118	1053	-44	0	-9	-796	4.02	4.02	4.02	4.02	2	0.12	0.03	0.19	0.00	0.00	22.3
15	60	-1705	1254	-53	0	-33	-1366	4.02	4.02	4.02	4.02	2	0.20	0.04	0.21	0.00	0.00	22.3
16	60	-142	1051	-47	0	3	-781	4.02	4.02	4.02	4.02	2	0.12	0.03	0.19	0.00	0.00	22.3
17	60	-1965	1252	-56	0	-21	-1352	4.02	4.02	4.02	4.02	2	0.19	0.04	0.21	0.00	0.00	22.3
18	60	-521	1428	-126	0	-110	-1157	4.02	4.02	4.02	4.02	3	0.16	0.04	0.25	0.00	0.00	22.3

19	60	-3381	1422	-136	0	21	-1083	4.02	4.02	4.02	4.02	3	0.14	0.04	0.23	0.00	0.00	22.3
20	60	-1908	1510	-134	0	-79	-1374	4.02	4.02	4.02	4.02	3	0.19	0.04	0.26	0.00	0.00	22.3
37	60	674	1454	-101	0	-146	-1272	4.02	4.02	4.02	4.02	3	0.19	0.04	0.26	0.00	0.00	22.3
38	60	-4093	1445	-117	0	73	-1148	4.02	4.02	4.02	4.02	3	0.15	0.04	0.23	0.00	0.00	22.3
39	60	-1638	1591	-114	0	-93	-1633	4.02	4.02	4.02	4.02	3	0.22	0.05	0.27	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	120	-1201	1103	-65	0	20	701	4.02	4.02	4.02	4.02	3	0.10	0.03	0.19	0.00	0.00	22.3
2	120	-216	822	-45	0	-4	558	4.02	4.02	4.02	4.02	2	0.08	0.02	0.15	0.00	0.00	22.3
3	120	-763	883	-48	0	-10	485	4.02	4.02	4.02	4.02	2	0.07	0.03	0.15	0.00	0.00	22.3
4	120	-1084	815	-52	0	40	595	4.02	4.02	4.02	4.02	2	0.09	0.02	0.14	0.00	0.00	22.3
5	120	-1631	875	-55	0	35	521	4.02	4.02	4.02	4.02	2	0.08	0.03	0.15	0.00	0.00	22.3
6	120	118	749	-44	0	18	657	4.02	4.02	4.02	4.02	2	0.10	0.02	0.13	0.00	0.00	22.3
7	120	-1705	950	-53	0	-1	-551	4.02	4.02	4.02	4.02	2	0.08	0.03	0.16	0.00	0.00	22.3
8	120	-142	747	-47	0	31	668	4.02	4.02	4.02	4.02	2	0.10	0.02	0.13	0.00	0.00	22.3
9	120	-1965	948	-56	0	13	-538	4.02	4.02	4.02	4.02	2	0.08	0.03	0.16	0.00	0.00	22.3
10	120	-216	822	-45	0	-4	558	4.02	4.02	4.02	4.02	2	0.08	0.02	0.15	0.00	0.00	22.3
11	120	-763	883	-48	0	-10	485	4.02	4.02	4.02	4.02	2	0.07	0.03	0.15	0.00	0.00	22.3
12	120	-1084	815	-52	0	40	595	4.02	4.02	4.02	4.02	2	0.09	0.02	0.14	0.00	0.00	22.3
13	120	-1631	875	-55	0	35	521	4.02	4.02	4.02	4.02	2	0.08	0.03	0.15	0.00	0.00	22.3
14	120	118	749	-44	0	18	657	4.02	4.02	4.02	4.02	2	0.10	0.02	0.13	0.00	0.00	22.3
15	120	-1705	950	-53	0	-1	-551	4.02	4.02	4.02	4.02	2	0.08	0.03	0.16	0.00	0.00	22.3
16	120	-142	747	-47	0	31	668	4.02	4.02	4.02	4.02	2	0.10	0.02	0.13	0.00	0.00	22.3
17	120	-1965	948	-56	0	13	-538	4.02	4.02	4.02	4.02	2	0.08	0.03	0.16	0.00	0.00	22.3
18	120	-521	1032	-126	0	-35	826	4.02	4.02	4.02	4.02	3	0.12	0.03	0.18	0.00	0.00	22.3
19	120	-3381	1027	-136	0	102	892	4.02	4.02	4.02	4.02	3	0.12	0.03	0.17	0.00	0.00	22.3
20	120	-1908	1115	-134	0	2	743	4.02	4.02	4.02	4.02	3	0.10	0.03	0.19	0.00	0.00	22.3
37	120	674	1058	-101	0	-85	753	4.02	4.02	4.02	4.02	3	0.11	0.03	0.19	0.00	0.00	22.3
38	120	-4093	1049	-117	0	143	863	4.02	4.02	4.02	4.02	3	0.11	0.03	0.17	0.00	0.00	22.3
39	120	-1638	1195	-114	0	-24	613	4.02	4.02	4.02	4.02	3	0.08	0.03	0.20	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	180	-1201	707	-65	0	59	1044	4.02	4.02	4.02	4.02	3	0.14	0.02	0.12	0.00	0.00	22.3
2	180	-216	517	-45	0	23	800	4.02	4.02	4.02	4.02	2	0.12	0.01	0.09	0.00	0.00	22.3
3	180	-763	578	-48	0	19	769	4.02	4.02	4.02	4.02	2	0.11	0.02	0.10	0.00	0.00	22.3
4	180	-1084	510	-52	0	71	827	4.02	4.02	4.02	4.02	2	0.12	0.01	0.09	0.00	0.00	22.3
5	180	-1631	570	-55	0	68	800	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
6	180	118	444	-44	0	44	811	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
7	180	-1705	645	-53	0	31	735	4.02	4.02	4.02	4.02	2	0.11	0.02	0.11	0.00	0.00	22.3
8	180	-142	442	-47	0	59	821	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
9	180	-1965	643	-56	0	46	745	4.02	4.02	4.02	4.02	2	0.11	0.02	0.11	0.00	0.00	22.3
10	180	-216	517	-45	0	23	800	4.02	4.02	4.02	4.02	2	0.12	0.01	0.09	0.00	0.00	22.3
11	180	-763	578	-48	0	19	769	4.02	4.02	4.02	4.02	2	0.11	0.02	0.10	0.00	0.00	22.3
12	180	-1084	510	-52	0	71	827	4.02	4.02	4.02	4.02	2	0.12	0.01	0.09	0.00	0.00	22.3
13	180	-1631	570	-55	0	68	800	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
14	180	118	444	-44	0	44	811	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
15	180	-1705	645	-53	0	31	735	4.02	4.02	4.02	4.02	2	0.11	0.02	0.11	0.00	0.00	22.3
16	180	-142	442	-47	0	59	821	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
17	180	-1965	643	-56	0	46	745	4.02	4.02	4.02	4.02	2	0.11	0.02	0.11	0.00	0.00	22.3
18	180	-521	636	-126	0	41	1093	4.02	4.02	4.02	4.02	3	0.15	0.02	0.11	0.00	0.00	22.3
19	180	-3381	631	-136	0	184	1153	4.02	4.02	4.02	4.02	3	0.15	0.02	0.10	0.00	0.00	22.3
20	180	-1908	720	-134	0	82	1093	4.02	4.02	4.02	4.02	3	0.15	0.02	0.12	0.00	0.00	22.3
37	180	674	662	-101	0	-24	1053	4.02	4.02	4.02	4.02	3	0.15	0.02	0.12	0.00	0.00	22.3
38	180	-4093	654	-117	0	214	1152	4.02	4.02	4.02	4.02	3	0.15	0.02	0.11	0.00	0.00	22.3
39	180	-1638	800	-114	0	44	1012	4.02	4.02	4.02	4.02	3	0.14	0.02	0.14	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	240	-1201	312	-65	0	98	1060	4.02	4.02	4.02	4.02	3	0.15	0.01	0.05	0.00	0.00	22.3
2	240	-216	213	-45	0	50	800	4.02	4.02	4.02	4.02	2	0.12	0.01	0.04	0.00	0.00	22.3
3	240	-763	274	-48	0	48	805	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
4	240	-1084	206	-52	0	103	827	4.02	4.02	4.02	4.02	2	0.12	0.01	0.04	0.00	0.00	22.3
5	240	-1631	266	-55	0	100	831	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
6	240	118	140	-44	0	71	811	4.02	4.02	4.02	4.02	2	0.12	0.00	0.02	0.00	0.00	22.3
7	240	-1705	341	-53	0	64	819	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
8	240	-142	138	-47	0	87	821	4.02	4.02	4.02	4.02	2	0.12	0.00	0.02	0.00	0.00	22.3
9	240	-1965	339	-56	0	79	827	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
10	240	-216	213	-45	0	50	800	4.02	4.02	4.02	4.02	2	0.12	0.01	0.04	0.00	0.00	22.3
11	240	-763	274	-48	0	48	805	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
12	240	-1084	206	-52	0	103	827	4.02	4.02	4.02	4.02	2	0.12	0.01	0.04	0.00	0.00	22.3
13	240	-1631	266	-55	0	100	831	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
14	240	118	140	-44	0	71	811	4.02	4.02	4.02	4.02	2	0.12	0.00	0.02	0.00	0.00	22.3
15	240	-1705	341	-53	0	64	819	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
16	240	-142	138	-47	0	87	821	4.02	4.02	4.02	4.02	2	0.12	0.00	0.02	0.00	0.00	22.3
17	240	-1965	339	-56	0	79	827	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
18	240	-521	241	-126	0	116	1093	4.02	4.02	4.02	4.02	3	0.15	0.01	0.04	0.00	0.00	22.3
19	240	-3381	236	-136	0	265	1153	4.02	4.02	4.02	4.02	3	0.15	0.01	0.04	0.00	0.00	22.3
20	240	-1908	324	-134	0	162	1117	4.02	4.02	4.02	4.02	3	0.15	0.01	0.06	0.00	0.00	22.3
37	240	674	267	-101	0	37	1053	4.02	4.02	4.02	4.02	3	0.15	0.01	0.05	0.00	0.00	22.3
38	240	-4093	258	-117	0	284	1152	4.02	4.02	4.02	4.02	3	0.15	0.01	0.04	0.00	0.00	22.3
39	240	-1638	404	-114	0	113	1092	4.02	4.02	4.02	4.02	3	0.15	0.01	0.07	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	300	-1201	-84	-65	0	137	1060	4.02	4.02	4.02	4.02	3	0.15	0.00	0.01	0.00	0.00	22.3
2	300	-216	-91	-45	0	77	800	4.02	4.02	4.02	4.02	2	0.12	0.00	0.02	0.00	0.00	22.3
3	300	-763	-30	-48	0	76	805	4.02	4.02	4.02	4.02	2	0.12	0.00	0.01	0.00	0.00	22.3
4	300	-1084	-98	-52	0	134	827	4.02	4.02	4.02	4.02	2	0.12	0.00	0.02	0.00	0.00	22.3
5	300	-1631	-38	-55	0	133	831	4.02	4.02	4.02	4.02	2	0.12	0.00	0.01	0.00	0.00	22.3
6	300	118	-164	-44	0	98	811	4.02	4.02	4.02	4.02	2	0.12	0.00	0.03	0.00	0.00	22.3
7	300	-1705	37	-53	0	96	819	4.02	4.02	4.02	4.02	2	0.12	0.00	0.01	0.00	0.00	22.3
8	300	-142	-166	-47	0	115	821	4.02	4.02	4.02	4.02	2	0.12	0.00	0.03	0.00	0.00	22.3
9	300	-1965	35	-56	0	113	827	4.02	4.02	4.02	4.02	2	0.12	0.00	0.01	0.00	0.00	22.3
10	300	-216	-91	-45	0	77	800	4.02	4.02	4.02	4.02	2	0.12	0.00	0.02	0.00	0.00	22.3
11	300	-763	-30	-48	0	76	805	4.02	4.02	4.02	4.02	2	0.12	0.00	0.01	0.00	0.00	22.3
12	300	-1084	-98	-52	0	134	827	4.02	4.02	4.02	4.02	2	0.12	0.00	0.02	0.00	0.00	22.3
13	300	-1631	-38	-55	0	133	831	4.02	4.02	4.02	4.02	2	0.12	0.00	0.01	0.00	0.00	22.3
14	300	118	-164	-44	0	98	811	4.02	4.02	4.02	4.02	2	0.12	0.00	0.03	0.00	0.00	22.3
15	300	-1705	37	-53	0	96	819	4.02	4.02	4.02	4.02	2	0.12	0.00	0.01	0.00	0.00	22.3
16	300	-142	-166	-47	0	115	821	4.02	4.02	4.02	4.02	2	0.12	0.00	0.03	0.00	0.00	22.3
17	300	-1965	35	-56	0	113	827	4.02	4.02	4.02	4.02	2	0.12	0.00	0.01	0.00	0.00	22.3
18	300	-521	-155	-126	0	192	1093	4.02	4.02	4.02	4.02	3	0.15	0.00	0.03	0.00	0.00	22.3
19	300	-3381	-160	-136	0	346	1153	4.02	4.02	4.02	4.02	3	0.15	0.00	0.03	0.00	0.00	22.3
20	300	-1908	-72	-134	0	242	1117	4.02	4.02	4.02	4.02	3	0.15	0.00	0.01	0.00	0.00	22.3
37	300	674	-129	-101	0	98	1053	4.02	4.02	4.02	4.02	3	0.15	0.00	0.02	0.00	0.00	22.3
38	300	-4093	-137	-117	0	355	1152	4.02	4.02	4.02	4.02	3	0.15	0.00	0.02	0.00	0.00	22.3
39	300	-1638	9	-114	0	181	1092	4.02	4.02	4.02	4.02	3	0.15	0.00	0.00	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	360	-1201	-479	-65	0	176	1060	4.02	4.02	4.02	4.02	3	0.15	0.01	0.08	0.00	0.00	22.3
2	360	-216	-395	-45	0	104	800	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
3	360	-763	-334	-48	0	105	805	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
4	360	-1084	-402	-52	0	165	827	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
5	360	-1631	-342	-55	0	166	831	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
6	360	118	-468	-44	0	124	811	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
7	360	-1705	-267	-53	0	128	819	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
8	360	-142	-470	-47	0	143	821	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
9	360	-1965	-269	-56	0	146	827	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
10	360	-216	-395	-45	0	104	800	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
11	360	-763	-334	-48	0	105	805	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
12	360	-1084	-402	-52	0	165	827	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
13	360	-1631	-342	-55	0	166	831	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
14	360	118	-468	-44	0	124	811	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
15	360	-1705	-267	-53	0	128	819	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
16	360	-142	-470	-47	0	143	821	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
17	360	-1965	-269	-56	0	146	827	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
18	360	-521	-550	-126	0	268	1093	4.02	4.02	4.02	4.02	3	0.15	0.02	0.10	0.00	0.00	22.3
19	360	-3381	-555	-136	0	428	1153	4.02	4.02	4.02	4.02	3	0.15	0.02	0.09	0.00	0.00	22.3
20	360	-1908	-467	-134	0	323	1117	4.02	4.02	4.02	4.02	3	0.15	0.01	0.08	0.00	0.00	22.3
37	360	674	-524	-101	0	159	1053	4.02	4.02	4.02	4.02	3	0.15	0.02	0.09	0.00	0.00	22.3
38	360	-4093	-532	-117	0	425	1152	4.02	4.02	4.02	4.02	3	0.15	0.02	0.09	0.00	0.00	22.3
39	360	-1638	-386	-114	0	250	1092	4.02	4.02	4.02	4.02	3	0.15	0.01	0.07	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	420	-1201	-874	-65	0	215	928	4.02	4.02	4.02	4.02	3	0.13	0.03	0.15	0.00	0.00	22.3
2	420	-216	-699	-45	0	131	680	4.02	4.02	4.02	4.02	2	0.10	0.02	0.12	0.00	0.00	22.3
3	420	-763	-638	-48	0	134	726	4.02	4.02	4.02	4.02	2	0.11	0.02	0.11	0.00	0.00	22.3
4	420	-1084	-706	-52	0	197	701	4.02	4.02	4.02	4.02	2	0.10	0.02	0.12	0.00	0.00	22.3
5	420	-1631	-646	-55	0	199	748	4.02	4.02	4.02	4.02	2	0.11	0.02	0.11	0.00	0.00	22.3
6	420	118	-772	-44	0	151	634	4.02	4.02	4.02	4.02	2	0.10	0.02	0.14	0.00	0.00	22.3
7	420	-1705	-571	-53	0	160	788	4.02	4.02	4.02	4.02	2	0.11	0.02	0.10	0.00	0.00	22.3
8	420	-142	-774	-47	0	171	640	4.02	4.02	4.02	4.02	2	0.10	0.02	0.14	0.00	0.00	22.3
9	420	-1965	-573	-56	0	179	794	4.02	4.02	4.02	4.02	2	0.11	0.02	0.10	0.00	0.00	22.3
10	420	-216	-699	-45	0	131	680	4.02	4.02	4.02	4.02	2	0.10	0.02	0.12	0.00	0.00	22.3
11	420	-763	-638	-48	0	134	726	4.02	4.02	4.02	4.02	2	0.11	0.02	0.11	0.00	0.00	22.3
12	420	-1084	-706	-52	0	197	701	4.02	4.02	4.02	4.02	2	0.10	0.02	0.12	0.00	0.00	22.3
13	420	-1631	-646	-55	0	199	748	4.02	4.02	4.02	4.02	2	0.11	0.02	0.11	0.00	0.00	22.3
14	420	118	-772	-44	0	151	634	4.02	4.02	4.02	4.02	2	0.10	0.02	0.14	0.00	0.00	22.3
15	420	-1705	-571	-53	0	160	788	4.02	4.02	4.02	4.02	2	0.11	0.02	0.10	0.00	0.00	22.3
16	420	-142	-774	-47	0	171	640	4.02	4.02	4.02	4.02	2	0.10	0.02	0.14	0.00	0.00	22.3
17	420	-1965	-573	-56	0	179	794	4.02	4.02	4.02	4.02	2	0.11	0.02	0.10	0.00	0.00	22.3
18	420	-521	-946	-126	0	343	913	4.02	4.02	4.02	4.02	3	0.13	0.03	0.17	0.00	0.00	22.3
19	420	-3381	-950	-136	0	509	968	4.02	4.02	4.02	4.02	3	0.13	0.03	0.16	0.00	0.00	22.3
20	420	-1908	-862	-134	0	403	993	4.02	4.02	4.02	4.02	3	0.13	0.02	0.15	0.00	0.00	22.3
37	420	674	-920	-101	0	219	890	4.02	4.02	4.02	4.02	3	0.13	0.03	0.16	0.00	0.00	22.3
38	420	-4093	-928	-117	0	495	983	4.02	4.02	4.02	4.02	3	0.13	0.03	0.15	0.00	0.00	22.3
39	420	-1638	-782	-114	0	319	1025	4.02	4.02	4.02	4.02	3	0.14	0.02	0.13	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	480	-1201	-1270	-65	0	254	-801	4.02	4.02	4.02	4.02	3	0.11	0.04	0.22	0.00	0.00	22.3
2	480	-216	-1004	-45	0	158	-693	4.02	4.02	4.02	4.02	2	0.10	0.03	0.18	0.00	0.00	22.3
3	480	-763	-943	-48	0	162	-549	4.02	4.02	4.02	4.02	2	0.08	0.03	0.16	0.00	0.00	22.3
4	480	-1084	-1011	-52	0	228	-683	4.02	4.02	4.02	4.02	2	0.10	0.03	0.18	0.00	0.00	22.3
5	480	-1631	-951	-55	0	232	-540	4.02	4.02	4.02	4.02	2	0.08	0.03	0.16	0.00	0.00	22.3
6	480	118	-1077	-44	0	178	-857	4.02	4.02	4.02	4.02	2	0.13	0.03	0.19	0.00	0.00	22.3
7	480	-1705	-876	-53	0	192	508	4.02	4.02	4.02	4.02	2	0.07	0.03	0.15	0.00	0.00	22.3
8	480	-142	-1079	-47	0	199	-854	4.02	4.02	4.02	4.02	2	0.13	0.03	0.19	0.00	0.00	22.3
9	480	-1965	-878	-56	0	213	513	4.02	4.02	4.02	4.02	2	0.07	0.03	0.15	0.00	0.00	22.3
10	480	-216	-1004	-45	0	158	-693	4.02	4.02	4.02	4.02	2	0.10	0.03	0.18	0.00	0.00	22.3
11	480	-763	-943	-48	0	162	-549	4.02	4.02	4.02	4.02	2	0.08	0.03	0.16	0.00	0.00	22.3
12	480	-1084	-1011	-52	0	228	-683	4.02	4.02	4.02	4.02	2	0.10	0.03	0.18	0.00	0.00	22.3
13	480	-1631	-951	-55	0	232	-540	4.02	4.02	4.02	4.02	2	0.08	0.03	0.16	0.00	0.00	22.3
14	480	118	-1077	-44	0	178	-857	4.02	4.02	4.02	4.02	2	0.13	0.03	0.19	0.00	0.00	22.3
15	480	-1705	-876	-53	0	192	508	4.02	4.02	4.02	4.02	2	0.07	0.03	0.15	0.00	0.00	22.3
16	480	-142	-1079	-47	0	199	-854	4.02	4.02	4.02	4.02	2	0.13	0.03	0.19	0.00	0.00	22.3
17	480	-1965	-878	-56	0	213	513	4.02	4.02	4.02	4.02	2	0.07	0.03	0.15	0.00	0.00	22.3
18	480	-521	-1341	-126	0	419	-931	4.02	4.02	4.02	4.02	3	0.13	0.04	0.24	0.00	0.00	22.3
19	480	-3381	-1346	-136	0	590	-883	4.02	4.02	4.02	4.02	3	0.13	0.04	0.22	0.00	0.00	22.3
20	480	-1908	-1258	-134	0	483	-717	4.02	4.02	4.02	4.02	3	0.11	0.04	0.21	0.00	0.00	22.3
37	480	674	-1315	-101	0	280	-911	4.02	4.02	4.02	4.02	3	0.13	0.04	0.23	0.00	0.00	22.3
38	480	-4093	-1323	-117	0	566	-832	4.02	4.02	4.02	4.02	3	0.13	0.04	0.21	0.00	0.00	22.3
39	480	-1638	-1177	-114	0	387	637	4.02	4.02	4.02	4.02	3	0.09	0.03	0.20	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	540	-1201	-1665	-65	0	293	-1882	4.02	4.02	4.02	4.02	3	0.26	0.05	0.29	0.00	0.00	22.3
2	540	-216	-1308	-45	0	185	-1540	4.02	4.02	4.02	4.02	2	0.23	0.04	0.23	0.00	0.00	22.3
3	540	-763	-1247	-48	0	191	-1360	4.02	4.02	4.02	4.02	2	0.20	0.04	0.22	0.00	0.00	22.3
4	540	-1084	-1315	-52	0	259	-1535	4.02	4.02	4.02	4.02	2	0.23	0.04	0.23	0.00	0.00	22.3
5	540	-1631	-1255	-55	0	265	-1355	4.02	4.02	4.02	4.02	2	0.20	0.04	0.22	0.00	0.00	22.3
6	540	118	-1381	-44	0	205	-1748	4.02	4.02	4.02	4.02	2	0.27	0.04	0.25	0.00	0.00	22.3
7	540	-1705	-1180	-53	0	224	-1149	4.02	4.02	4.02	4.02	2	0.17	0.03	0.20	0.00	0.00	22.3
8	540	-142	-1383	-47	0	227	-1746	4.02	4.02	4.02	4.02	2	0.26	0.04	0.25	0.00	0.00	22.3
9	540	-1965	-1182	-56	0	246	-1147	4.02	4.02	4.02	4.02	2	0.16	0.03	0.20	0.00	0.00	22.3
10	540	-216	-1308	-45	0	185	-1540	4.02	4.02	4.02	4.02	2	0.23	0.04	0.23	0.00	0.00	22.3
11	540	-763	-1247	-48	0	191	-1360	4.02	4.02	4.02	4.02	2	0.20	0.04	0.22	0.00	0.00	22.3
12	540	-1084	-1315	-52	0	259	-1535	4.02	4.02	4.02	4.02	2	0.23	0.04	0.23	0.00	0.00	22.3
13	540	-1631	-1255	-55	0	265	-1355	4.02	4.02	4.02	4.02	2	0.20	0.04	0.22	0.00	0.00	22.3
14	540	118	-1381	-44	0	205	-1748	4.02	4.02	4.02	4.02	2	0.27	0.04	0.25	0.00	0.00	22.3
15	540	-1705	-1180	-53	0	224	-1149	4.02	4.02	4.02	4.02	2	0.17	0.03	0.20	0.00	0.00	22.3
16	540	-142	-1383	-47	0	227	-1746	4.02	4.02	4.02	4.02	2	0.26	0.04	0.25	0.00	0.00	22.3
17	540	-1965	-1182	-56	0	246	-1147	4.02	4.02	4.02	4.02	2	0.16	0.03	0.20	0.00	0.00	22.3
18	540	-521	-1736	-126	0	494	-2054	4.02	4.02	4.02	4.02	3	0.29	0.05	0.31	0.00	0.00	22.3
19	540	-3381	-1741	-136	0	672	-2009	4.02	4.02	4.02	4.02	3	0.26	0.05	0.29	0.00	0.00	22.3
20	540	-1908	-1653	-134	0	563	-1790	4.02	4.02	4.02	4.02	3	0.24	0.05	0.28	0.00	0.00	22.3
37	540	674	-1710	-101	0	341	-2019	4.02	4.02	4.02	4.02	3	0.30	0.05	0.30	0.00	0.00	22.3
38	540	-4093	-1719	-117	0	636	-1945	4.02	4.02	4.02	4.02	3	0.25	0.05	0.28	0.00	0.00	22.3
39	540	-1638	-1573	-114	0	456	-1580	4.02	4.02	4.02	4.02	3	0.22	0.05	0.27	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	600	-1201	-2061	-65	0	332	-2157	4.02	4.02	4.02	4.02	3	0.30	0.06	0.36	0.00	0.00	22.3
2	600	-216	-1612	-45	0	213	-1754	4.02	4.02	4.02	4.02	2	0.26	0.05	0.29	0.00	0.00	22.3
3	600	-763	-1551	-48	0	220	-1568	4.02	4.02	4.02	4.02	2	0.23	0.04	0.27	0.00	0.00	22.3
4	600	-1084	-1619	-52	0	291	-1750	4.02	4.02	4.02	4.02	2	0.26	0.05	0.28	0.00	0.00	22.3

5	600	-1631	-1559	-55	0	298	-1564	4.02	4.02	4.02	4.02	2	0.23	0.04	0.27	0.00	0.00	22.3
6	600	118	-1685	-44	0	231	-1969	4.02	4.02	4.02	4.02	2	0.30	0.05	0.30	0.00	0.00	22.3
7	600	-1705	-1484	-53	0	256	-1351	4.02	4.02	4.02	4.02	2	0.19	0.04	0.25	0.00	0.00	22.3
8	600	-142	-1687	-47	0	255	-1967	4.02	4.02	4.02	4.02	2	0.30	0.05	0.30	0.00	0.00	22.3
9	600	-1965	-1486	-56	0	279	-1349	4.02	4.02	4.02	4.02	2	0.19	0.04	0.25	0.00	0.00	22.3
10	600	-216	-1612	-45	0	213	-1754	4.02	4.02	4.02	4.02	2	0.26	0.05	0.29	0.00	0.00	22.3
11	600	-763	-1551	-48	0	220	-1568	4.02	4.02	4.02	4.02	2	0.23	0.04	0.27	0.00	0.00	22.3
12	600	-1084	-1619	-52	0	291	-1750	4.02	4.02	4.02	4.02	2	0.26	0.05	0.28	0.00	0.00	22.3
13	600	-1631	-1559	-55	0	298	-1564	4.02	4.02	4.02	4.02	2	0.23	0.04	0.27	0.00	0.00	22.3
14	600	118	-1685	-44	0	231	-1969	4.02	4.02	4.02	4.02	2	0.30	0.05	0.30	0.00	0.00	22.3
15	600	-1705	-1484	-53	0	256	-1351	4.02	4.02	4.02	4.02	2	0.19	0.04	0.25	0.00	0.00	22.3
16	600	-142	-1687	-47	0	255	-1967	4.02	4.02	4.02	4.02	2	0.30	0.05	0.30	0.00	0.00	22.3
17	600	-1965	-1486	-56	0	279	-1349	4.02	4.02	4.02	4.02	2	0.19	0.04	0.25	0.00	0.00	22.3
18	600	-521	-2132	-126	0	570	-2335	4.02	4.02	4.02	4.02	3	0.33	0.06	0.38	0.00	0.00	22.3
19	600	-3381	-2137	-136	0	753	-2291	4.02	4.02	4.02	4.02	3	0.30	0.06	0.35	0.00	0.00	22.3
20	600	-1908	-2049	-134	0	644	-2064	4.02	4.02	4.02	4.02	3	0.28	0.06	0.35	0.00	0.00	22.3
37	600	674	-2106	-101	0	402	-2298	4.02	4.02	4.02	4.02	3	0.34	0.06	0.38	0.00	0.00	22.3
38	600	-4093	-2114	-117	0	707	-2225	4.02	4.02	4.02	4.02	3	0.28	0.06	0.34	0.00	0.00	22.3
39	600	-1638	-1968	-114	0	524	-1846	4.02	4.02	4.02	4.02	3	0.25	0.06	0.34	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

Nome travata: **Trave_403_IP1** Descrizione: **Trave_4 7-6-5-4-3-2-1**
ASTA NUM. 12 NI 251 NF 252 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y Permanente qy tot.
qy medio: 375.00 132.00 507.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-1037	1974	111	0	453	-1928	4.02	4.02	4.02	4.02	3	0.27	0.06	0.34	0.00	0.00	22.3
2	0	-221	1469	95	0	361	-1342	4.02	4.02	4.02	4.02	2	0.20	0.04	0.26	0.00	0.00	22.3
3	0	-637	1537	70	0	279	-1545	4.02	4.02	4.02	4.02	2	0.23	0.04	0.27	0.00	0.00	22.3
4	0	-958	1501	101	0	418	-1421	4.02	4.02	4.02	4.02	2	0.21	0.04	0.26	0.00	0.00	22.3
5	0	-1374	1568	76	0	336	-1624	4.02	4.02	4.02	4.02	2	0.24	0.05	0.27	0.00	0.00	22.3
6	0	6	1402	127	0	477	-1134	4.02	4.02	4.02	4.02	2	0.17	0.04	0.25	0.00	0.00	22.3
7	0	-1380	1626	42	0	203	-1809	4.02	4.02	4.02	4.02	2	0.26	0.05	0.28	0.00	0.00	22.3
8	0	-215	1411	129	0	494	-1157	4.02	4.02	4.02	4.02	2	0.17	0.04	0.25	0.00	0.00	22.3
9	0	-1602	1635	44	0	220	-1832	4.02	4.02	4.02	4.02	2	0.27	0.05	0.28	0.00	0.00	22.3
10	0	-221	1469	95	0	361	-1342	4.02	4.02	4.02	4.02	2	0.20	0.04	0.26	0.00	0.00	22.3
11	0	-637	1537	70	0	279	-1545	4.02	4.02	4.02	4.02	2	0.23	0.04	0.27	0.00	0.00	22.3
12	0	-958	1501	101	0	418	-1421	4.02	4.02	4.02	4.02	2	0.21	0.04	0.26	0.00	0.00	22.3
13	0	-1374	1568	76	0	336	-1624	4.02	4.02	4.02	4.02	2	0.24	0.05	0.27	0.00	0.00	22.3
14	0	6	1402	127	0	477	-1134	4.02	4.02	4.02	4.02	2	0.17	0.04	0.25	0.00	0.00	22.3
15	0	-1380	1626	42	0	203	-1809	4.02	4.02	4.02	4.02	2	0.26	0.05	0.28	0.00	0.00	22.3
16	0	-215	1411	129	0	494	-1157	4.02	4.02	4.02	4.02	2	0.17	0.04	0.25	0.00	0.00	22.3
17	0	-1602	1635	44	0	220	-1832	4.02	4.02	4.02	4.02	2	0.27	0.05	0.28	0.00	0.00	22.3
18	0	-100	1919	204	0	788	-1758	4.02	4.02	4.02	4.02	3	0.25	0.06	0.34	0.00	0.00	22.3
19	0	-2820	2016	208	0	912	-2002	4.02	4.02	4.02	4.02	3	0.27	0.06	0.34	0.00	0.00	22.3
20	0	-1339	2047	131	0	593	-2127	4.02	4.02	4.02	4.02	3	0.29	0.06	0.35	0.00	0.00	22.3
37	0	940	1890	172	0	617	-1692	4.02	4.02	4.02	4.02	3	0.25	0.05	0.34	0.00	0.00	22.3
38	0	-3593	2050	178	0	824	-2100	4.02	4.02	4.02	4.02	3	0.27	0.06	0.34	0.00	0.00	22.3
39	0	-1125	2103	50	0	294	-2308	4.02	4.02	4.02	4.02	3	0.32	0.06	0.36	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	60	-1037	1579	111	0	386	-1661	4.02	4.02	4.02	4.02	3	0.23	0.05	0.27	0.00	0.00	22.3
2	60	-221	1165	95	0	304	-1141	4.02	4.02	4.02	4.02	2	0.17	0.03	0.21	0.00	0.00	22.3
3	60	-637	1233	70	0	237	-1338	4.02	4.02	4.02	4.02	2	0.20	0.04	0.22	0.00	0.00	22.3
4	60	-958	1197	101	0	357	-1218	4.02	4.02	4.02	4.02	2	0.18	0.03	0.21	0.00	0.00	22.3
5	60	-1374	1264	76	0	291	-1414	4.02	4.02	4.02	4.02	2	0.21	0.04	0.22	0.00	0.00	22.3
6	60	6	1098	127	0	400	-940	4.02	4.02	4.02	4.02	2	0.14	0.03	0.20	0.00	0.00	22.3
7	60	-1380	1322	42	0	178	-1594	4.02	4.02	4.02	4.02	2	0.23	0.04	0.23	0.00	0.00	22.3
8	60	-215	1107	129	0	416	-962	4.02	4.02	4.02	4.02	2	0.14	0.03	0.20	0.00	0.00	22.3
9	60	-1602	1331	44	0	194	-1616	4.02	4.02	4.02	4.02	2	0.23	0.04	0.23	0.00	0.00	22.3
10	60	-221	1165	95	0	304	-1141	4.02	4.02	4.02	4.02	2	0.17	0.03	0.21	0.00	0.00	22.3
11	60	-637	1233	70	0	237	-1338	4.02	4.02	4.02	4.02	2	0.20	0.04	0.22	0.00	0.00	22.3
12	60	-958	1197	101	0	357	-1218	4.02	4.02	4.02	4.02	2	0.18	0.03	0.21	0.00	0.00	22.3
13	60	-1374	1264	76	0	291	-1414	4.02	4.02	4.02	4.02	2	0.21	0.04	0.22	0.00	0.00	22.3
14	60	6	1098	127	0	400	-940	4.02	4.02	4.02	4.02	2	0.14	0.03	0.20	0.00	0.00	22.3
15	60	-1380	1322	42	0	178	-1594	4.02	4.02	4.02	4.02	2	0.23	0.04	0.23	0.00	0.00	22.3
16	60	-215	1107	129	0	416	-962	4.02	4.02	4.02	4.02	2	0.14	0.03	0.20	0.00	0.00	22.3
17	60	-1602	1331	44	0	194	-1616	4.02	4.02	4.02	4.02	2	0.23	0.04	0.23	0.00	0.00	22.3
18	60	-100	1524	204	0	665	-1496	4.02	4.02	4.02	4.02	3	0.21	0.04	0.27	0.00	0.00	22.3
19	60	-2820	1620	208	0	787	-1732	4.02	4.02	4.02	4.02	3	0.23	0.05	0.27	0.00	0.00	22.3
20	60	-1339	1652	131	0	515	-1853	4.02	4.02	4.02	4.02	3	0.26	0.05	0.28	0.00	0.00	22.3
37	60	940	1494	172	0	514	-1433	4.02	4.02	4.02	4.02	3	0.21	0.04	0.27	0.00	0.00	22.3
38	60	-3593	1655	178	0	717	-1826	4.02	4.02	4.02	4.02	3	0.24	0.05	0.27	0.00	0.00	22.3
39	60	-1125	1708	50	0	264	-2029	4.02	4.02	4.02	4.02	3	0.28	0.05	0.30	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	120	-1037	1183	111	0	319	-633	4.02	4.02	4.02	4.02	3	0.09	0.03	0.21	0.00	0.00	22.3
2	120	-221	861	95	0	246	492	4.02	4.02	4.02	4.02	2	0.07	0.02	0.15	0.00	0.00	22.3
3	120	-637	929	70	0	195	-536	4.02	4.02	4.02	4.02	2	0.08	0.03	0.16	0.00	0.00	22.3
4	120	-958	893	101	0	297	466	4.02	4.02	4.02	4.02	2	0.08	0.03	0.16	0.00	0.00	22.3
5	120	-1374	960	76	0	245	-593	4.02	4.02	4.02	4.02	2	0.09	0.03	0.17	0.00	0.00	22.3
6	120	6	794	127	0	324	585	4.02	4.02	4.02	4.02	2	0.09	0.02	0.14	0.00	0.00	22.3
7	120	-1380	1018	42	0	153	-738	4.02	4.02	4.02	4.02	2	0.11	0.03	0.18	0.00	0.00	22.3
8	120	-215	803	129	0	339	578	4.02	4.02	4.02	4.02	2	0.09	0.02	0.14	0.00	0.00	22.3
9	120	-1602	1027	44	0	168	-755	4.02	4.02	4.02	4.02	2	0.11	0.03	0.18	0.00	0.00	22.3
10	120	-221	861	95	0	246	492	4.02	4.02	4.02	4.02	2	0.07	0.02	0.15	0.00	0.00	22.3
11	120	-637	929	70	0	195	-536	4.02	4.02	4.02	4.02	2	0.08	0.03	0.16	0.00	0.00	22.3
12	120	-958	893	101	0	297	466	4.02	4.02	4.02	4.02	2	0.08	0.03	0.16	0.00	0.00	22.3
13	120	-1374	960	76	0	245	-593	4.02	4.02	4.02	4.02	2	0.09	0.03	0.17	0.00	0.00	22.3
14	120	6	794	127	0	324	585	4.02	4.02	4.02	4.02	2	0.09	0.02	0.14	0.00	0.00	22.3
15	120	-1380	1018	42	0	153	-738	4.02	4.02	4.02	4.02	2	0.11	0.03	0.18	0.00	0.00	22.3
16	120	-215	803	129	0	339	578	4.02	4.02	4.02	4.02	2	0.09	0.02	0.14	0.00	0.00	22.3
17	120	-1602	1027	44	0	168	-755	4.02	4.02	4.02	4.02	2	0.11	0.03	0.18	0.00	0.00	22.3
18	120	-100	1128	204	0	543	642	4.02	4.02	4.02	4.02	3	0.13	0.03	0.20	0.00	0.00	22.3
19	120	-2820	1225	208	0	662	-678	4.02	4.02	4.02	4.02	3	0.15	0.04	0.20	0.00	0.00	22.3
20	120	-1339	1256	131	0	437	-781	4.02	4.02	4.02	4.02	3	0.11	0.04	0.22	0.00	0.00	22.3
37	120	940	1099	172	0	411	657	4.02	4.02	4.02	4.02	3	0.10	0.03	0.20	0.00	0.00	22.3
38	120	-3593	1259	178	0	609	-752	4.02	4.02	4.02	4.02	3	0.14	0.04	0.21	0.00	0.00	22.3

39	120	-1125	1312	50	0	234	-923	4.02	4.02	4.02	4.02	3	0.13	0.04	0.23	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	180	-1037	788	111	0	253	957	4.02	4.02	4.02	4.02	3	0.13	0.02	0.14	0.00	0.00	22.3
2	180	-221	556	95	0	189	763	4.02	4.02	4.02	4.02	2	0.11	0.02	0.10	0.00	0.00	22.3
3	180	-637	624	70	0	153	716	4.02	4.02	4.02	4.02	2	0.11	0.02	0.11	0.00	0.00	22.3
4	180	-958	588	101	0	236	756	4.02	4.02	4.02	4.02	2	0.11	0.02	0.10	0.00	0.00	22.3
5	180	-1374	655	76	0	200	709	4.02	4.02	4.02	4.02	2	0.10	0.02	0.11	0.00	0.00	22.3
6	180	6	489	127	0	247	791	4.02	4.02	4.02	4.02	2	0.12	0.01	0.09	0.00	0.00	22.3
7	180	-1380	713	42	0	128	657	4.02	4.02	4.02	4.02	2	0.10	0.02	0.12	0.00	0.00	22.3
8	180	-215	498	129	0	261	796	4.02	4.02	4.02	4.02	2	0.12	0.01	0.09	0.00	0.00	22.3
9	180	-1602	722	44	0	142	656	4.02	4.02	4.02	4.02	2	0.09	0.02	0.12	0.00	0.00	22.3
10	180	-221	556	95	0	189	763	4.02	4.02	4.02	4.02	2	0.11	0.02	0.10	0.00	0.00	22.3
11	180	-637	624	70	0	153	716	4.02	4.02	4.02	4.02	2	0.11	0.02	0.11	0.00	0.00	22.3
12	180	-958	588	101	0	236	756	4.02	4.02	4.02	4.02	2	0.11	0.02	0.10	0.00	0.00	22.3
13	180	-1374	655	76	0	200	709	4.02	4.02	4.02	4.02	2	0.10	0.02	0.11	0.00	0.00	22.3
14	180	6	489	127	0	247	791	4.02	4.02	4.02	4.02	2	0.12	0.01	0.09	0.00	0.00	22.3
15	180	-1380	713	42	0	128	657	4.02	4.02	4.02	4.02	2	0.10	0.02	0.12	0.00	0.00	22.3
16	180	-215	498	129	0	261	796	4.02	4.02	4.02	4.02	2	0.12	0.01	0.09	0.00	0.00	22.3
17	180	-1602	722	44	0	142	656	4.02	4.02	4.02	4.02	2	0.09	0.02	0.12	0.00	0.00	22.3
18	180	-100	733	204	0	421	1000	4.02	4.02	4.02	4.02	3	0.14	0.02	0.13	0.00	0.00	22.3
19	180	-2820	830	208	0	537	978	4.02	4.02	4.02	4.02	3	0.13	0.02	0.14	0.00	0.00	22.3
20	180	-1339	861	131	0	358	926	4.02	4.02	4.02	4.02	3	0.13	0.02	0.15	0.00	0.00	22.3
37	180	940	703	172	0	308	998	4.02	4.02	4.02	4.02	3	0.15	0.02	0.13	0.00	0.00	22.3
38	180	-3593	864	178	0	502	960	4.02	4.02	4.02	4.02	3	0.12	0.02	0.14	0.00	0.00	22.3
39	180	-1125	917	50	0	204	873	4.02	4.02	4.02	4.02	3	0.12	0.03	0.16	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	240	-1037	392	111	0	186	1028	4.02	4.02	4.02	4.02	3	0.14	0.01	0.07	0.00	0.00	22.3
2	240	-221	252	95	0	132	785	4.02	4.02	4.02	4.02	2	0.12	0.01	0.04	0.00	0.00	22.3
3	240	-637	320	70	0	111	784	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
4	240	-958	284	101	0	175	799	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
5	240	-1374	351	76	0	154	798	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
6	240	6	185	127	0	171	791	4.02	4.02	4.02	4.02	2	0.12	0.01	0.03	0.00	0.00	22.3
7	240	-1380	409	42	0	103	787	4.02	4.02	4.02	4.02	2	0.11	0.01	0.07	0.00	0.00	22.3
8	240	-215	194	129	0	184	796	4.02	4.02	4.02	4.02	2	0.12	0.01	0.03	0.00	0.00	22.3
9	240	-1602	418	44	0	116	792	4.02	4.02	4.02	4.02	2	0.11	0.01	0.07	0.00	0.00	22.3
10	240	-221	252	95	0	132	785	4.02	4.02	4.02	4.02	2	0.12	0.01	0.04	0.00	0.00	22.3
11	240	-637	320	70	0	111	784	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
12	240	-958	284	101	0	175	799	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
13	240	-1374	351	76	0	154	798	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
14	240	6	185	127	0	171	791	4.02	4.02	4.02	4.02	2	0.12	0.01	0.03	0.00	0.00	22.3
15	240	-1380	409	42	0	103	787	4.02	4.02	4.02	4.02	2	0.11	0.01	0.07	0.00	0.00	22.3
16	240	-215	194	129	0	184	796	4.02	4.02	4.02	4.02	2	0.12	0.01	0.03	0.00	0.00	22.3
17	240	-1602	418	44	0	116	792	4.02	4.02	4.02	4.02	2	0.11	0.01	0.07	0.00	0.00	22.3
18	240	-100	337	204	0	298	1034	4.02	4.02	4.02	4.02	3	0.15	0.01	0.06	0.00	0.00	22.3
19	240	-2820	434	208	0	412	1079	4.02	4.02	4.02	4.02	3	0.14	0.01	0.07	0.00	0.00	22.3
20	240	-1339	465	131	0	280	1048	4.02	4.02	4.02	4.02	3	0.14	0.01	0.08	0.00	0.00	22.3
37	240	940	308	172	0	205	1011	4.02	4.02	4.02	4.02	3	0.15	0.01	0.05	0.00	0.00	22.3
38	240	-3593	468	178	0	395	1085	4.02	4.02	4.02	4.02	3	0.14	0.01	0.08	0.00	0.00	22.3
39	240	-1125	521	50	0	175	1034	4.02	4.02	4.02	4.02	3	0.14	0.02	0.09	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	300	-1037	-3	111	0	119	1028	4.02	4.02	4.02	4.02	3	0.14	0.00	0.00	0.00	0.00	22.3
2	300	-221	-52	95	0	74	785	4.02	4.02	4.02	4.02	2	0.12	0.00	0.01	0.00	0.00	22.3
3	300	-637	16	70	0	69	784	4.02	4.02	4.02	4.02	2	0.12	0.00	0.00	0.00	0.00	22.3
4	300	-958	-20	101	0	114	799	4.02	4.02	4.02	4.02	2	0.12	0.00	0.00	0.00	0.00	22.3
5	300	-1374	47	76	0	109	798	4.02	4.02	4.02	4.02	2	0.12	0.00	0.01	0.00	0.00	22.3
6	300	6	-119	127	0	94	791	4.02	4.02	4.02	4.02	2	0.12	0.00	0.02	0.00	0.00	22.3
7	300	-1380	105	42	0	77	787	4.02	4.02	4.02	4.02	2	0.11	0.00	0.02	0.00	0.00	22.3
8	300	-215	-110	129	0	106	796	4.02	4.02	4.02	4.02	2	0.12	0.00	0.02	0.00	0.00	22.3
9	300	-1602	114	44	0	89	792	4.02	4.02	4.02	4.02	2	0.11	0.00	0.02	0.00	0.00	22.3
10	300	-221	-52	95	0	74	785	4.02	4.02	4.02	4.02	2	0.12	0.00	0.01	0.00	0.00	22.3
11	300	-637	16	70	0	69	784	4.02	4.02	4.02	4.02	2	0.12	0.00	0.00	0.00	0.00	22.3
12	300	-958	-20	101	0	114	799	4.02	4.02	4.02	4.02	2	0.12	0.00	0.00	0.00	0.00	22.3
13	300	-1374	47	76	0	109	798	4.02	4.02	4.02	4.02	2	0.12	0.00	0.01	0.00	0.00	22.3
14	300	6	-119	127	0	94	791	4.02	4.02	4.02	4.02	2	0.12	0.00	0.02	0.00	0.00	22.3
15	300	-1380	105	42	0	77	787	4.02	4.02	4.02	4.02	2	0.11	0.00	0.02	0.00	0.00	22.3
16	300	-215	-110	129	0	106	796	4.02	4.02	4.02	4.02	2	0.12	0.00	0.02	0.00	0.00	22.3
17	300	-1602	114	44	0	89	792	4.02	4.02	4.02	4.02	2	0.11	0.00	0.02	0.00	0.00	22.3
18	300	-100	-58	204	0	176	1034	4.02	4.02	4.02	4.02	3	0.15	0.01	0.03	0.00	0.00	22.3
19	300	-2820	38	208	0	287	1079	4.02	4.02	4.02	4.02	3	0.14	0.01	0.03	0.00	0.00	22.3
20	300	-1339	70	131	0	202	1048	4.02	4.02	4.02	4.02	3	0.14	0.00	0.01	0.00	0.00	22.3
37	300	940	-88	172	0	102	1011	4.02	4.02	4.02	4.02	3	0.15	0.01	0.03	0.00	0.00	22.3
38	300	-3593	73	178	0	288	1085	4.02	4.02	4.02	4.02	3	0.14	0.01	0.03	0.00	0.00	22.3
39	300	-1125	126	50	0	145	1034	4.02	4.02	4.02	4.02	3	0.14	0.00	0.02	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	360	-1037	-398	111	0	53	1028	4.02	4.02	4.02	4.02	3	0.14	0.01	0.07	0.00	0.00	22.3
2	360	-221	-356	95	0	17	785	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
3	360	-637	-288	70	0	28	784	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
4	360	-958	-324	101	0	53	799	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
5	360	-1374	-257	76	0	64	798	4.02	4.02	4.02	4.02	2	0.12	0.01	0.04	0.00	0.00	22.3
6	360	6	-423	127	0	18	791	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
7	360	-1380	-199	42	0	52	787	4.02	4.02	4.02	4.02	2	0.11	0.01	0.03	0.00	0.00	22.3
8	360	-215	-414	129	0	29	796	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
9	360	-1602	-190	44	0	63	792	4.02	4.02	4.02	4.02	2	0.11	0.01	0.03	0.00	0.00	22.3
10	360	-221	-356	95	0	17	785	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
11	360	-637	-288	70	0	28	784	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
12	360	-958	-324	101	0	53	799	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
13	360	-1374	-257	76	0	64	798	4.02	4.02	4.02	4.02	2	0.12	0.01	0.04	0.00	0.00	22.3
14	360	6	-423	127	0	18	791	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
15	360	-1380	-199	42	0	52	787	4.02	4.02	4.02	4.02	2	0.11	0.01	0.03	0.00	0.00	22.3
16	360	-215	-414	129	0	29	796	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
17	360	-1602	-190	44	0	63	792	4.02	4.02	4.02	4.02	2	0.11	0.01	0.03	0.00	0.00	22.3
18	360	-100	-453	204	0	54	1034	4.02	4.02	4.02	4.02	3	0.15	0.01	0.08	0.00	0.00	22.3
19	360	-2820	-357	208	0	163	1079	4.02	4.02	4.02	4.02	3	0.14	0.01	0.06	0.00	0.00	22.3
20	360	-1339	-325	131	0	123	1048	4.02	4.02	4.02	4.02	3	0.14	0.01	0.06	0.00	0.00	22.3
37	360	940	-483	172	0	-1	1011	4.02	4.02	4.02	4.02	3	0.15	0.01	0.09	0.00	0.00	22.3
38	360	-3593	-322	178	0	181	1085	4.02	4.02	4.02	4.02	3	0.14	0.01	0.05	0.00	0.00	22.3
39	360	-1125	-270	50	0	115	1034	4.02	4.02	4.02	4.02	3	0.14	0.01	0.05	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	420	-1037	-794	111	0	-14	952	4.02	4.02	4.02	4.02	3	0.13	0.02	0.14	0.00	0.00	22.3
2	420	-221	-660	95	0	-40	692	4.02	4.02	4.02	4.02	2	0.10	0.02	0.12	0.00	0.00	22.3

3	420	-637	-592	70	0	-14	737	4.02	4.02	4.02	4.02	2	0.11	0.02	0.10	0.00	0.00	22.3
4	420	-958	-628	101	0	-7	727	4.02	4.02	4.02	4.02	2	0.11	0.02	0.11	0.00	0.00	22.3
5	420	-1374	-561	76	0	18	773	4.02	4.02	4.02	4.02	2	0.11	0.02	0.10	0.00	0.00	22.3
6	420	6	-727	127	0	-59	652	4.02	4.02	4.02	4.02	2	0.10	0.02	0.13	0.00	0.00	22.3
7	420	-1380	-503	42	0	27	787	4.02	4.02	4.02	4.02	2	0.11	0.01	0.09	0.00	0.00	22.3
8	420	-215	-718	129	0	-49	663	4.02	4.02	4.02	4.02	2	0.10	0.02	0.13	0.00	0.00	22.3
9	420	-1602	-494	44	0	37	792	4.02	4.02	4.02	4.02	2	0.11	0.01	0.08	0.00	0.00	22.3
10	420	-221	-660	95	0	-40	692	4.02	4.02	4.02	4.02	2	0.10	0.02	0.12	0.00	0.00	22.3
11	420	-637	-592	70	0	-14	737	4.02	4.02	4.02	4.02	2	0.11	0.02	0.10	0.00	0.00	22.3
12	420	-958	-628	101	0	-7	727	4.02	4.02	4.02	4.02	2	0.11	0.02	0.11	0.00	0.00	22.3
13	420	-1374	-561	76	0	18	773	4.02	4.02	4.02	4.02	2	0.11	0.02	0.10	0.00	0.00	22.3
14	420	6	-727	127	0	-59	652	4.02	4.02	4.02	4.02	2	0.10	0.02	0.13	0.00	0.00	22.3
15	420	-1380	-503	42	0	27	787	4.02	4.02	4.02	4.02	2	0.11	0.01	0.09	0.00	0.00	22.3
16	420	-215	-718	129	0	-49	663	4.02	4.02	4.02	4.02	2	0.10	0.02	0.13	0.00	0.00	22.3
17	420	-1602	-494	44	0	37	792	4.02	4.02	4.02	4.02	2	0.11	0.01	0.08	0.00	0.00	22.3
18	420	-100	-849	204	0	-69	920	4.02	4.02	4.02	4.02	3	0.13	0.02	0.15	0.00	0.00	22.3
19	420	-2820	-752	208	0	38	1031	4.02	4.02	4.02	4.02	3	0.14	0.02	0.13	0.00	0.00	22.3
20	420	-1339	-721	131	0	45	1023	4.02	4.02	4.02	4.02	3	0.14	0.02	0.12	0.00	0.00	22.3
37	420	940	-878	172	0	-104	876	4.02	4.02	4.02	4.02	3	0.13	0.03	0.16	0.00	0.00	22.3
38	420	-3593	-718	178	0	74	1061	4.02	4.02	4.02	4.02	3	0.14	0.02	0.12	0.00	0.00	22.3
39	420	-1125	-665	50	0	86	1034	4.02	4.02	4.02	4.02	3	0.14	0.02	0.12	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	480	-1037	-1189	111	0	-81	-647	4.02	4.02	4.02	4.02	3	0.09	0.03	0.21	0.00	0.00	22.3
2	480	-221	-965	95	0	-97	-617	4.02	4.02	4.02	4.02	2	0.09	0.03	0.17	0.00	0.00	22.3
3	480	-637	-897	70	0	-56	-464	4.02	4.02	4.02	4.02	2	0.07	0.03	0.16	0.00	0.00	22.3
4	480	-958	-933	101	0	-68	-531	4.02	4.02	4.02	4.02	2	0.08	0.03	0.16	0.00	0.00	22.3
5	480	-1374	-866	76	0	-27	499	4.02	4.02	4.02	4.02	2	0.07	0.02	0.15	0.00	0.00	22.3
6	480	6	-1032	127	0	-135	-766	4.02	4.02	4.02	4.02	2	0.12	0.03	0.18	0.00	0.00	22.3
7	480	-1380	-808	42	0	2	563	4.02	4.02	4.02	4.02	2	0.08	0.02	0.14	0.00	0.00	22.3
8	480	-215	-1023	129	0	-126	-741	4.02	4.02	4.02	4.02	2	0.11	0.03	0.18	0.00	0.00	22.3
9	480	-1602	-799	44	0	11	580	4.02	4.02	4.02	4.02	2	0.08	0.02	0.14	0.00	0.00	22.3
10	480	-221	-965	95	0	-97	-617	4.02	4.02	4.02	4.02	2	0.09	0.03	0.17	0.00	0.00	22.3
11	480	-637	-897	70	0	-56	-464	4.02	4.02	4.02	4.02	2	0.07	0.03	0.16	0.00	0.00	22.3
12	480	-958	-933	101	0	-68	-531	4.02	4.02	4.02	4.02	2	0.08	0.03	0.16	0.00	0.00	22.3
13	480	-1374	-866	76	0	-27	499	4.02	4.02	4.02	4.02	2	0.07	0.02	0.15	0.00	0.00	22.3
14	480	6	-1032	127	0	-135	-766	4.02	4.02	4.02	4.02	2	0.12	0.03	0.18	0.00	0.00	22.3
15	480	-1380	-808	42	0	2	563	4.02	4.02	4.02	4.02	2	0.08	0.02	0.14	0.00	0.00	22.3
16	480	-215	-1023	129	0	-126	-741	4.02	4.02	4.02	4.02	2	0.11	0.03	0.18	0.00	0.00	22.3
17	480	-1602	-799	44	0	11	580	4.02	4.02	4.02	4.02	2	0.08	0.02	0.14	0.00	0.00	22.3
18	480	-100	-1244	204	0	-191	-767	4.02	4.02	4.02	4.02	3	0.11	0.04	0.22	0.00	0.00	22.3
19	480	-2820	-1148	208	0	-87	661	4.02	4.02	4.02	4.02	3	0.09	0.03	0.19	0.00	0.00	22.3
20	480	-1339	-1116	131	0	-34	671	4.02	4.02	4.02	4.02	3	0.09	0.03	0.19	0.00	0.00	22.3
37	480	940	-1274	172	0	-207	-860	4.02	4.02	4.02	4.02	3	0.13	0.04	0.23	0.00	0.00	22.3
38	480	-3593	-1113	178	0	-33	712	4.02	4.02	4.02	4.02	3	0.09	0.03	0.18	0.00	0.00	22.3
39	480	-1125	-1061	50	0	56	730	4.02	4.02	4.02	4.02	3	0.10	0.03	0.18	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	540	-1037	-1585	111	0	-148	-1680	4.02	4.02	4.02	4.02	3	0.23	0.05	0.28	0.00	0.00	22.3
2	540	-221	-1269	95	0	-155	-1441	4.02	4.02	4.02	4.02	2	0.22	0.04	0.22	0.00	0.00	22.3
3	540	-637	-1201	70	0	-98	-1247	4.02	4.02	4.02	4.02	2	0.19	0.03	0.21	0.00	0.00	22.3
4	540	-958	-1237	101	0	-129	-1336	4.02	4.02	4.02	4.02	2	0.20	0.04	0.22	0.00	0.00	22.3
5	540	-1374	-1170	76	0	-72	-1142	4.02	4.02	4.02	4.02	2	0.17	0.03	0.20	0.00	0.00	22.3
6	540	6	-1336	127	0	-212	-1631	4.02	4.02	4.02	4.02	2	0.25	0.04	0.24	0.00	0.00	22.3
7	540	-1380	-1112	42	0	-23	-984	4.02	4.02	4.02	4.02	2	0.14	0.03	0.19	0.00	0.00	22.3
8	540	-215	-1327	129	0	-204	-1600	4.02	4.02	4.02	4.02	2	0.24	0.04	0.24	0.00	0.00	22.3
9	540	-1602	-1103	44	0	-15	-952	4.02	4.02	4.02	4.02	2	0.14	0.03	0.19	0.00	0.00	22.3
10	540	-221	-1269	95	0	-155	-1441	4.02	4.02	4.02	4.02	2	0.22	0.04	0.22	0.00	0.00	22.3
11	540	-637	-1201	70	0	-98	-1247	4.02	4.02	4.02	4.02	2	0.19	0.03	0.21	0.00	0.00	22.3
12	540	-958	-1237	101	0	-129	-1336	4.02	4.02	4.02	4.02	2	0.20	0.04	0.22	0.00	0.00	22.3
13	540	-1374	-1170	76	0	-72	-1142	4.02	4.02	4.02	4.02	2	0.17	0.03	0.20	0.00	0.00	22.3
14	540	6	-1336	127	0	-212	-1631	4.02	4.02	4.02	4.02	2	0.25	0.04	0.24	0.00	0.00	22.3
15	540	-1380	-1112	42	0	-23	-984	4.02	4.02	4.02	4.02	2	0.14	0.03	0.19	0.00	0.00	22.3
16	540	-215	-1327	129	0	-204	-1600	4.02	4.02	4.02	4.02	2	0.24	0.04	0.24	0.00	0.00	22.3
17	540	-1602	-1103	44	0	-15	-952	4.02	4.02	4.02	4.02	2	0.14	0.03	0.19	0.00	0.00	22.3
18	540	-100	-1640	204	0	-313	-1833	4.02	4.02	4.02	4.02	3	0.26	0.05	0.29	0.00	0.00	22.3
19	540	-2820	-1543	208	0	-212	-1509	4.02	4.02	4.02	4.02	3	0.20	0.04	0.26	0.00	0.00	22.3
20	540	-1339	-1512	131	0	-112	-1447	4.02	4.02	4.02	4.02	3	0.20	0.04	0.26	0.00	0.00	22.3
37	540	940	-1669	172	0	-310	-1943	4.02	4.02	4.02	4.02	3	0.29	0.05	0.30	0.00	0.00	22.3
38	540	-3593	-1509	178	0	-140	-1402	4.02	4.02	4.02	4.02	3	0.18	0.04	0.25	0.00	0.00	22.3
39	540	-1125	-1456	50	0	26	-1300	4.02	4.02	4.02	4.02	3	0.18	0.04	0.25	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	600	-1037	-1980	111	0	-214	-1947	4.02	4.02	4.02	4.02	3	0.27	0.06	0.34	0.00	0.00	22.3
2	600	-221	-1573	95	0	-212	-1651	4.02	4.02	4.02	4.02	2	0.25	0.05	0.28	0.00	0.00	22.3
3	600	-637	-1505	70	0	-140	-1451	4.02	4.02	4.02	4.02	2	0.22	0.04	0.26	0.00	0.00	22.3
4	600	-958	-1541	101	0	-190	-1544	4.02	4.02	4.02	4.02	2	0.23	0.04	0.27	0.00	0.00	22.3
5	600	-1374	-1474	76	0	-118	-1343	4.02	4.02	4.02	4.02	2	0.20	0.04	0.25	0.00	0.00	22.3
6	600	6	-1640	127	0	-288	-1847	4.02	4.02	4.02	4.02	2	0.28	0.05	0.29	0.00	0.00	22.3
7	600	-1380	-1416	42	0	-48	-1180	4.02	4.02	4.02	4.02	2	0.17	0.04	0.24	0.00	0.00	22.3
8	600	-215	-1631	129	0	-281	-1815	4.02	4.02	4.02	4.02	2	0.27	0.05	0.29	0.00	0.00	22.3
9	600	-1602	-1407	44	0	-42	-1147	4.02	4.02	4.02	4.02	2	0.17	0.04	0.24	0.00	0.00	22.3
10	600	-221	-1573	95	0	-212	-1651	4.02	4.02	4.02	4.02	2	0.25	0.05	0.28	0.00	0.00	22.3
11	600	-637	-1505	70	0	-140	-1451	4.02	4.02	4.02	4.02	2	0.22	0.04	0.26	0.00	0.00	22.3
12	600	-958	-1541	101	0	-190	-1544	4.02	4.02	4.02	4.02	2	0.23	0.04	0.27	0.00	0.00	22.3
13	600	-1374	-1474	76	0	-118	-1343	4.02	4.02	4.02	4.02	2	0.20	0.04	0.25	0.00	0.00	22.3
14	600	6	-1640	127	0	-288	-1847	4.02	4.02	4.02	4.02	2	0.28	0.05	0.29	0.00	0.00	22.3
15	600	-1380	-1416	42	0	-48	-1180	4.02	4.02	4.02	4.02	2	0.17	0.04	0.24	0.00	0.00	22.3
16	600	-215	-1631	129	0	-281	-1815	4.02	4.02	4.02	4.02	2	0.27	0.05	0.29	0.00	0.00	22.3
17	600	-1602	-1407	44	0	-42	-1147	4.02	4.02	4.02	4.02	2	0.17	0.04	0.24	0.00	0.00	22.3
18	600	-100	-2035	204	0	-436	-2105	4.02	4.02	4.02	4.02	3	0.30	0.06	0.36	0.00	0.00	22.3
19	600	-2820	-1939	208	0	-337	-1772	4.02	4.02	4.02	4.02	3	0.23	0.06	0.32	0.00	0.00	22.3
20	600	-1339	-1907	131	0	-190	-1708	4.02	4.02	4.02	4.02	3	0.24	0.06	0.33	0.00	0.00	22.3
37	600	940	-2065	172	0	-413	-2218	4.02	4.02	4.02	4.02	3	0.33	0.06	0.37	0.00	0.00	22.3
38	600	-3593	-1904	178	0	-248	-1662	4.02	4.02	4.02	4.02	3	0.22	0.05	0.31	0.00	0.00	22.3
39	600	-1125	-1852	50	0	-4	-1555	4.02	4.02	4.02	4.02	3	0.22	0.05	0.32	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

Nome travata: **Trave_403_IP1** Descrizione: **Trave_4 7-6-5-4-3-2-1**
ASTA NUM. 13 NI 252 NF 253 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y Permanente qy tot.
qy medio: 375.00 132.00 507.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-283	2048	420	0	1404	-2103	4.02	4.02	4.02	4.02	3	0.34	0.06	0.36	0.00	0.00	22.3
2	0	154	1517	282	0	941	-1448	4.02	4.02	4.02	4.02	2	0.26	0.04	0.27	0.00	0.00	22.3
3	0	-163	1590	256	0	867	-1660	4.02	4.02	4.02	4.02	2	0.25	0.05	0.28	0.00	0.00	22.3
4	0	-272	1561	390	0	1293	-1575	4.02	4.02	4.02	4.02	2	0.35	0.05	0.28	0.00	0.00	22.3
5	0	-590	1633	364	0	1219	-1787	4.02	4.02	4.02	4.02	2	0.33	0.05	0.29	0.00	0.00	22.3
6	0	376	1447	350	0	1149	-1246	4.02	4.02	4.02	4.02	2	0.32	0.04	0.26	0.00	0.00	22.3
7	0	-683	1690	264	0	905	-1951	4.02	4.02	4.02	4.02	2	0.29	0.05	0.30	0.00	0.00	22.3
8	0	247	1460	382	0	1255	-1284	4.02	4.02	4.02	4.02	2	0.35	0.04	0.26	0.00	0.00	22.3
9	0	-811	1703	296	0	1010	-1989	4.02	4.02	4.02	4.02	2	0.29	0.05	0.30	0.00	0.00	22.3
10	0	154	1517	282	0	941	-1448	4.02	4.02	4.02	4.02	2	0.26	0.04	0.27	0.00	0.00	22.3
11	0	-163	1590	256	0	867	-1660	4.02	4.02	4.02	4.02	2	0.25	0.05	0.28	0.00	0.00	22.3
12	0	-272	1561	390	0	1293	-1575	4.02	4.02	4.02	4.02	2	0.35	0.05	0.28	0.00	0.00	22.3
13	0	-590	1633	364	0	1219	-1787	4.02	4.02	4.02	4.02	2	0.33	0.05	0.29	0.00	0.00	22.3
14	0	376	1447	350	0	1149	-1246	4.02	4.02	4.02	4.02	2	0.32	0.04	0.26	0.00	0.00	22.3
15	0	-683	1690	264	0	905	-1951	4.02	4.02	4.02	4.02	2	0.29	0.05	0.30	0.00	0.00	22.3
16	0	247	1460	382	0	1255	-1284	4.02	4.02	4.02	4.02	2	0.35	0.04	0.26	0.00	0.00	22.3
17	0	-811	1703	296	0	1010	-1989	4.02	4.02	4.02	4.02	2	0.29	0.05	0.30	0.00	0.00	22.3
18	0	1374	2153	664	0	2270	-2214	4.02	4.02	4.02	4.02	3	0.58	0.06	0.38	0.00	0.00	22.3
19	0	-922	2178	943	0	3166	-2409	4.02	4.02	4.02	4.02	3	0.76	0.06	0.38	0.00	0.00	22.3
20	0	248	2251	677	0	2327	-2562	4.02	4.02	4.02	4.02	3	0.58	0.07	0.40	0.00	0.00	22.3
37	0	1969	2106	446	0	1545	-2080	4.02	4.02	4.02	4.02	3	0.40	0.06	0.38	0.00	0.00	22.3
38	0	-1859	2148	912	0	3038	-2406	4.02	4.02	4.02	4.02	3	0.71	0.06	0.37	0.00	0.00	22.3
39	0	92	2270	468	0	1641	-2661	4.02	4.02	4.02	4.02	3	0.40	0.07	0.40	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	60	-283	1652	420	0	1152	-1830	4.02	4.02	4.02	4.02	3	0.28	0.05	0.29	0.00	0.00	22.3
2	60	154	1213	282	0	772	-1243	4.02	4.02	4.02	4.02	2	0.21	0.04	0.22	0.00	0.00	22.3
3	60	-163	1286	256	0	714	-1448	4.02	4.02	4.02	4.02	2	0.22	0.04	0.23	0.00	0.00	22.3
4	60	-272	1257	390	0	1059	-1366	4.02	4.02	4.02	4.02	2	0.29	0.04	0.22	0.00	0.00	22.3
5	60	-590	1329	364	0	1001	-1571	4.02	4.02	4.02	4.02	2	0.27	0.04	0.23	0.00	0.00	22.3
6	60	376	1143	350	0	939	-1047	4.02	4.02	4.02	4.02	2	0.26	0.03	0.20	0.00	0.00	22.3
7	60	-683	1386	264	0	747	-1730	4.02	4.02	4.02	4.02	2	0.26	0.04	0.24	0.00	0.00	22.3
8	60	247	1156	382	0	1026	-1084	4.02	4.02	4.02	4.02	2	0.29	0.03	0.21	0.00	0.00	22.3
9	60	-811	1399	296	0	832	-1767	4.02	4.02	4.02	4.02	2	0.26	0.04	0.24	0.00	0.00	22.3
10	60	154	1213	282	0	772	-1243	4.02	4.02	4.02	4.02	2	0.21	0.04	0.22	0.00	0.00	22.3
11	60	-163	1286	256	0	714	-1448	4.02	4.02	4.02	4.02	2	0.22	0.04	0.23	0.00	0.00	22.3
12	60	-272	1257	390	0	1059	-1366	4.02	4.02	4.02	4.02	2	0.29	0.04	0.22	0.00	0.00	22.3
13	60	-590	1329	364	0	1001	-1571	4.02	4.02	4.02	4.02	2	0.27	0.04	0.23	0.00	0.00	22.3
14	60	376	1143	350	0	939	-1047	4.02	4.02	4.02	4.02	2	0.26	0.03	0.20	0.00	0.00	22.3
15	60	-683	1386	264	0	747	-1730	4.02	4.02	4.02	4.02	2	0.26	0.04	0.24	0.00	0.00	22.3
16	60	247	1156	382	0	1026	-1084	4.02	4.02	4.02	4.02	2	0.29	0.03	0.21	0.00	0.00	22.3
17	60	-811	1399	296	0	832	-1767	4.02	4.02	4.02	4.02	2	0.26	0.04	0.24	0.00	0.00	22.3
18	60	1374	1758	664	0	1872	-1930	4.02	4.02	4.02	4.02	3	0.48	0.05	0.31	0.00	0.00	22.3
19	60	-922	1783	943	0	2600	-2123	4.02	4.02	4.02	4.02	3	0.62	0.05	0.31	0.00	0.00	22.3
20	60	248	1856	677	0	1921	-2269	4.02	4.02	4.02	4.02	3	0.48	0.05	0.33	0.00	0.00	22.3
37	60	1969	1710	446	0	1277	-1801	4.02	4.02	4.02	4.02	3	0.33	0.05	0.30	0.00	0.00	22.3
38	60	-1859	1753	912	0	2491	-2123	4.02	4.02	4.02	4.02	3	0.58	0.05	0.30	0.00	0.00	22.3
39	60	92	1874	468	0	1360	-2367	4.02	4.02	4.02	4.02	3	0.34	0.05	0.33	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	120	-283	1257	420	0	901	-757	4.02	4.02	4.02	4.02	3	0.22	0.04	0.22	0.00	0.00	22.3
2	120	154	909	282	0	603	467	4.02	4.02	4.02	4.02	2	0.17	0.03	0.16	0.00	0.00	22.3
3	120	-163	982	256	0	560	-615	4.02	4.02	4.02	4.02	2	0.15	0.03	0.17	0.00	0.00	22.3
4	120	-272	953	390	0	825	-549	4.02	4.02	4.02	4.02	2	0.23	0.03	0.17	0.00	0.00	22.3
5	120	-590	1025	364	0	782	-711	4.02	4.02	4.02	4.02	2	0.21	0.03	0.18	0.00	0.00	22.3
6	120	376	839	350	0	730	550	4.02	4.02	4.02	4.02	2	0.20	0.02	0.15	0.00	0.00	22.3
7	120	-683	1082	264	0	589	-836	4.02	4.02	4.02	4.02	2	0.16	0.03	0.19	0.00	0.00	22.3
8	120	247	852	382	0	797	535	4.02	4.02	4.02	4.02	2	0.22	0.02	0.15	0.00	0.00	22.3
9	120	-811	1095	296	0	655	-865	4.02	4.02	4.02	4.02	2	0.18	0.03	0.19	0.00	0.00	22.3
10	120	154	909	282	0	603	467	4.02	4.02	4.02	4.02	2	0.17	0.03	0.16	0.00	0.00	22.3
11	120	-163	982	256	0	560	-615	4.02	4.02	4.02	4.02	2	0.15	0.03	0.17	0.00	0.00	22.3
12	120	-272	953	390	0	825	-549	4.02	4.02	4.02	4.02	2	0.23	0.03	0.17	0.00	0.00	22.3
13	120	-590	1025	364	0	782	-711	4.02	4.02	4.02	4.02	2	0.21	0.03	0.18	0.00	0.00	22.3
14	120	376	839	350	0	730	550	4.02	4.02	4.02	4.02	2	0.20	0.02	0.15	0.00	0.00	22.3
15	120	-683	1082	264	0	589	-836	4.02	4.02	4.02	4.02	2	0.16	0.03	0.19	0.00	0.00	22.3
16	120	247	852	382	0	797	535	4.02	4.02	4.02	4.02	2	0.22	0.02	0.15	0.00	0.00	22.3
17	120	-811	1095	296	0	655	-865	4.02	4.02	4.02	4.02	2	0.18	0.03	0.19	0.00	0.00	22.3
18	120	1374	1362	664	0	1473	-794	4.02	4.02	4.02	4.02	3	0.38	0.04	0.24	0.00	0.00	22.3
19	120	-922	1387	943	0	2034	-972	4.02	4.02	4.02	4.02	3	0.49	0.04	0.24	0.00	0.00	22.3
20	120	248	1460	677	0	1515	-1074	4.02	4.02	4.02	4.02	3	0.37	0.04	0.26	0.00	0.00	22.3
37	120	1969	1315	446	0	1009	-693	4.02	4.02	4.02	4.02	3	0.26	0.04	0.23	0.00	0.00	22.3
38	120	-1859	1357	912	0	1943	-990	4.02	4.02	4.02	4.02	3	0.46	0.04	0.23	0.00	0.00	22.3
39	120	92	1479	468	0	1080	-1160	4.02	4.02	4.02	4.02	3	0.27	0.04	0.26	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	180	-283	862	420	0	649	951	4.02	4.02	4.02	4.02	3	0.16	0.02	0.15	0.00	0.00	22.3
2	180	154	604	282	0	434	767	4.02	4.02	4.02	4.02	2	0.12	0.02	0.11	0.00	0.00	22.3
3	180	-163	677	256	0	407	723	4.02	4.02	4.02	4.02	2	0.11	0.02	0.12	0.00	0.00	22.3
4	180	-272	648	390	0	591	741	4.02	4.02	4.02	4.02	2	0.16	0.02	0.11	0.00	0.00	22.3
5	180	-590	720	364	0	564	697	4.02	4.02	4.02	4.02	2	0.15	0.02	0.13	0.00	0.00	22.3
6	180	376	534	350	0	520	808	4.02	4.02	4.02	4.02	2	0.15	0.02	0.10	0.00	0.00	22.3
7	180	-683	777	264	0	431	663	4.02	4.02	4.02	4.02	2	0.12	0.02	0.14	0.00	0.00	22.3
8	180	247	547	382	0	567	801	4.02	4.02	4.02	4.02	2	0.16	0.02	0.10	0.00	0.00	22.3
9	180	-811	790	296	0	477	655	4.02	4.02	4.02	4.02	2	0.13	0.02	0.14	0.00	0.00	22.3
10	180	154	604	282	0	434	767	4.02	4.02	4.02	4.02	2	0.12	0.02	0.11	0.00	0.00	22.3
11	180	-163	677	256	0	407	723	4.02	4.02	4.02	4.02	2	0.11	0.02	0.12	0.00	0.00	22.3
12	180	-272	648	390	0	591	741	4.02	4.02	4.02	4.02	2	0.16	0.02	0.11	0.00	0.00	22.3
13	180	-590	720	364	0	564	697	4.02	4.02	4.02	4.02	2	0.15	0.02	0.13	0.00	0.00	22.3
14	180	376	534	350	0	520	808	4.02	4.02	4.02	4.02	2	0.15	0.02	0.10	0.00	0.00	22.3
15	180	-683	777	264	0	431	663	4.02	4.02	4.02	4.02	2	0.12	0.02	0.14	0.00	0.00	22.3
16	180	247	547	382	0	567	801	4.02	4.02	4.02	4.02	2	0.16	0.02	0.10	0.00	0.00	22.3
17	180	-811	790	296	0	477	655	4.02	4.02	4.02	4.02	2	0.13	0.02	0.14	0.00	0.00	22.3
18	180	1374	967	664	0	1075	1084	4.02	4.02	4.02	4.02	3	0.27	0.03	0.17	0.00	0.00	22.3
19	180	-922	992	943	0	1468	946	4.02	4.02	4.02	4.02	3	0.35	0.03	0.17	0.00	0.00	22.3
20	180	248	1065	677	0	1109	962	4.02	4.02	4.02	4.02	3	0.27	0.03	0.19	0.00	0.00	22.3
37	180	1969	920	446	0	742	1109	4.02	4.02	4.02	4.02	3	0.19	0.03	0.16	0.00	0.00	22.3
38	180	-1859	962	912	0	1396	880	4.02	4.02	4.02	4.02	3	0.33	0.03	0.16	0.00	0.00	22.3
39	180	92	1084	468	0	799	906	4.02	4.02	4.02	4.02	3	0.20	0.03	0.19	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	240	-283	466	420	0	397	1074	4.02	4.02	4.02	4.02	3	0.15	0.01	0.08	0.00	0.00	22.3
2	240	154	300	282	0	265	821	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
3	240	-163	373	256	0	254	827	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
4	240	-272	344	390	0	357	826	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
5	240	-590	416	364	0	346	832	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
6	240	376	230	350	0	310	815	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
7	240	-683	473	264	0	272	847	4.02	4.02	4.02	4.02	2	0.13	0.01	0.08	0.00	0.00	22.3
8	240	247	243	382	0	338	816	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
9	240	-811	486	296	0	300	856	4.02	4.02	4.02	4.02	2	0.13	0.01	0.08	0.00	0.00	22.3
10	240	154	300	282	0	265	821	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
11	240	-163	373	256	0	254	827	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
12	240	-272	344	390	0	357	826	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
13	240	-590	416	364	0	346	832	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
14	240	376	230	350	0	310	815	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
15	240	-683	473	264	0	272	847	4.02	4.02	4.02	4.02	2	0.13	0.01	0.08	0.00	0.00	22.3
16	240	247	243	382	0	338	816	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
17	240	-811	486	296	0	300	856	4.02	4.02	4.02	4.02	2	0.13	0.01	0.08	0.00	0.00	22.3
18	240	1374	571	664	0	677	1280	4.02	4.02	4.02	4.02	3	0.19	0.02	0.11	0.00	0.00	22.3
19	240	-922	596	943	0	902	1162	4.02	4.02	4.02	4.02	3	0.22	0.03	0.15	0.00	0.00	22.3
20	240	248	669	677	0	703	1272	4.02	4.02	4.02	4.02	3	0.18	0.02	0.12	0.00	0.00	22.3
37	240	1969	524	446	0	474	1272	4.02	4.02	4.02	4.02	3	0.19	0.02	0.09	0.00	0.00	22.3
38	240	-1859	566	912	0	849	1072	4.02	4.02	4.02	4.02	3	0.20	0.03	0.14	0.00	0.00	22.3
39	240	92	688	468	0	518	1237	4.02	4.02	4.02	4.02	3	0.18	0.02	0.12	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	300	-283	70	420	0	146	1074	4.02	4.02	4.02	4.02	3	0.15	0.01	0.07	0.00	0.00	22.3
2	300	154	-4	282	0	96	821	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
3	300	-163	69	256	0	100	827	4.02	4.02	4.02	4.02	2	0.12	0.01	0.04	0.00	0.00	22.3
4	300	-272	40	390	0	123	826	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
5	300	-590	112	364	0	127	832	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
6	300	376	-74	350	0	101	815	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
7	300	-683	169	264	0	114	847	4.02	4.02	4.02	4.02	2	0.13	0.01	0.04	0.00	0.00	22.3
8	300	247	-61	382	0	109	816	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
9	300	-811	182	296	0	122	856	4.02	4.02	4.02	4.02	2	0.13	0.01	0.05	0.00	0.00	22.3
10	300	154	-4	282	0	96	821	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
11	300	-163	69	256	0	100	827	4.02	4.02	4.02	4.02	2	0.12	0.01	0.04	0.00	0.00	22.3
12	300	-272	40	390	0	123	826	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
13	300	-590	112	364	0	127	832	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
14	300	376	-74	350	0	101	815	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
15	300	-683	169	264	0	114	847	4.02	4.02	4.02	4.02	2	0.13	0.01	0.04	0.00	0.00	22.3
16	300	247	-61	382	0	109	816	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
17	300	-811	182	296	0	122	856	4.02	4.02	4.02	4.02	2	0.13	0.01	0.05	0.00	0.00	22.3
18	300	1374	176	664	0	278	1280	4.02	4.02	4.02	4.02	3	0.19	0.02	0.11	0.00	0.00	22.3
19	300	-922	201	943	0	335	1162	4.02	4.02	4.02	4.02	3	0.16	0.03	0.15	0.00	0.00	22.3
20	300	248	274	677	0	297	1272	4.02	4.02	4.02	4.02	3	0.18	0.02	0.11	0.00	0.00	22.3
37	300	1969	128	446	0	206	1272	4.02	4.02	4.02	4.02	3	0.19	0.01	0.07	0.00	0.00	22.3
38	300	-1859	171	912	0	302	1072	4.02	4.02	4.02	4.02	3	0.15	0.03	0.14	0.00	0.00	22.3
39	300	92	292	468	0	237	1240	4.02	4.02	4.02	4.02	3	0.18	0.01	0.08	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	360	-283	-325	420	0	-106	1074	4.02	4.02	4.02	4.02	3	0.15	0.01	0.07	0.00	0.00	22.3
2	360	154	-308	282	0	-73	821	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
3	360	-163	-235	256	0	-53	827	4.02	4.02	4.02	4.02	2	0.12	0.01	0.04	0.00	0.00	22.3
4	360	-272	-264	390	0	-110	826	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
5	360	-590	-192	364	0	-91	832	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
6	360	376	-378	350	0	-109	815	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
7	360	-683	-135	264	0	-44	847	4.02	4.02	4.02	4.02	2	0.13	0.01	0.04	0.00	0.00	22.3
8	360	247	-365	382	0	-120	816	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
9	360	-811	-122	296	0	-55	856	4.02	4.02	4.02	4.02	2	0.13	0.01	0.05	0.00	0.00	22.3
10	360	154	-308	282	0	-73	821	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
11	360	-163	-235	256	0	-53	827	4.02	4.02	4.02	4.02	2	0.12	0.01	0.04	0.00	0.00	22.3
12	360	-272	-264	390	0	-110	826	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
13	360	-590	-192	364	0	-91	832	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
14	360	376	-378	350	0	-109	815	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
15	360	-683	-135	264	0	-44	847	4.02	4.02	4.02	4.02	2	0.13	0.01	0.04	0.00	0.00	22.3
16	360	247	-365	382	0	-120	816	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
17	360	-811	-122	296	0	-55	856	4.02	4.02	4.02	4.02	2	0.13	0.01	0.05	0.00	0.00	22.3
18	360	1374	-219	664	0	-120	1280	4.02	4.02	4.02	4.02	3	0.19	0.02	0.11	0.00	0.00	22.3
19	360	-922	-194	943	0	-231	1162	4.02	4.02	4.02	4.02	3	0.16	0.03	0.15	0.00	0.00	22.3
20	360	248	-121	677	0	-109	1272	4.02	4.02	4.02	4.02	3	0.18	0.02	0.11	0.00	0.00	22.3
37	360	1969	-267	446	0	-62	1272	4.02	4.02	4.02	4.02	3	0.19	0.01	0.07	0.00	0.00	22.3
38	360	-1859	-224	912	0	-246	1072	4.02	4.02	4.02	4.02	3	0.15	0.03	0.14	0.00	0.00	22.3
39	360	92	-103	468	0	-43	1240	4.02	4.02	4.02	4.02	3	0.18	0.01	0.08	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	420	-283	-720	420	0	-358	1049	4.02	4.02	4.02	4.02	3	0.15	0.02	0.13	0.00	0.00	22.3
2	420	154	-612	282	0	-242	760	4.02	4.02	4.02	4.02	2	0.12	0.02	0.11	0.00	0.00	22.3
3	420	-163	-539	256	0	-207	817	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
4	420	-272	-568	390	0	-344	796	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
5	420	-590	-496	364	0	-309	832	4.02	4.02	4.02	4.02	2	0.12	0.01	0.09	0.00	0.00	22.3
6	420	376	-682	350	0	-318	707	4.02	4.02	4.02	4.02	2	0.11	0.02	0.12	0.00	0.00	22.3
7	420	-683	-439	264	0	-202	847	4.02	4.02	4.02	4.02	2	0.13	0.01	0.08	0.00	0.00	22.3
8	420	247	-669	382	0	-349	717	4.02	4.02	4.02	4.02	2	0.11	0.02	0.12	0.00	0.00	22.3
9	420	-811	-426	296	0	-233	856	4.02	4.02	4.02	4.02	2	0.13	0.01	0.07	0.00	0.00	22.3
10	420	154	-612	282	0	-242	760	4.02	4.02	4.02	4.02	2	0.12	0.02	0.11	0.00	0.00	22.3
11	420	-163	-539	256	0	-207	817	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
12	420	-272	-568	390	0	-344	796	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
13	420	-590	-496	364	0	-309	832	4.02	4.02	4.02	4.02	2	0.12	0.01	0.09	0.00	0.00	22.3
14	420	376	-682	350	0	-318	707	4.02	4.02	4.02	4.02	2	0.11	0.02	0.12	0.00	0.00	22.3
15	420	-683	-439	264	0	-202	847	4.02	4.02	4.02	4.02	2	0.13	0.01	0.08	0.00	0.00	22.3
16	420	247	-669	382	0	-349	717	4.02	4.02	4.02	4.02	2	0.11	0.02	0.12	0.00	0.00	22.3
17	420	-811	-426	296	0	-233	856	4.02	4.02	4.02	4.02	2	0.13	0.01	0.07	0.00	0.00	22.3
18	420	1374	-615	664	0	-518	1280	4.02	4.02	4.02	4.02	3	0.19	0.02	0.11	0.00	0.00	22.3
19	420	-922	-590	943	0	-797	1162	4.02	4.02	4.02	4.02	3	0.19	0.03	0.15	0.00	0.00	22.3
20	420	248	-517	677	0	-515	1272	4.02	4.02	4.02	4.02	3	0.18	0.02	0.11	0.00	0.00	22.3
37	420	1969	-662	446	0	-330	1272	4.02	4.02	4.02	4.02	3	0.19	0.02	0.12	0.00	0.00	22.3
38	420	-1859	-620	912	0	-793	1072	4.02	4.02	4.02	4.02	3	0.19	0.03	0.14	0.00	0.00	22.3
39	420	92	-498	468	0	-324	1240	4.02	4.02	4.02	4.02	3	0.18	0.01	0.09	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	480	-283	-1116	420	0	-610	698	4.02	4.02	4.02	4.02	3	0.15	0.03	0.20	0.00	0.00	22.3
2	480	154	-917	282	0	-411	-473	4.02	4.02	4.02	4.02	2	0.11	0.03	0.16	0.00	0.00	22.3
3	480	-163	-844	256	0	-360	556	4.02	4.02	4.02	4.02	2	0.10	0.02	0.15	0.00	0.00	22.3
4	480	-272	-873	390	0	-578	517	4.02	4.02	4.02	4.02	2	0.16	0.03	0.15	0.00	0.00	22.3
5	480	-590	-801	364	0	-528	618	4.02	4.02	4.02	4.02	2	0.14	0.02	0.14	0.00	0.00	22.3
6	480	376	-987	350	0	-528	-639	4.02	4.02	4.02	4.02	2	0.15	0.03	0.18	0.00	0.00	22.3

7	480	-683	-744	264	0	-360	696	4.02	4.02	4.02	4.02	2	0.10	0.02	0.13	0.00	0.00	22.3
8	480	247	-974	382	0	-579	-607	4.02	4.02	4.02	4.02	2	0.16	0.03	0.17	0.00	0.00	22.3
9	480	-811	-731	296	0	-410	714	4.02	4.02	4.02	4.02	2	0.11	0.02	0.13	0.00	0.00	22.3
10	480	154	-917	282	0	-411	-473	4.02	4.02	4.02	4.02	2	0.11	0.03	0.16	0.00	0.00	22.3
11	480	-163	-844	256	0	-360	556	4.02	4.02	4.02	4.02	2	0.10	0.02	0.15	0.00	0.00	22.3
12	480	-272	-873	390	0	-578	517	4.02	4.02	4.02	4.02	2	0.16	0.03	0.15	0.00	0.00	22.3
13	480	-590	-801	364	0	-528	618	4.02	4.02	4.02	4.02	2	0.14	0.02	0.14	0.00	0.00	22.3
14	480	376	-987	350	0	-528	-639	4.02	4.02	4.02	4.02	2	0.15	0.03	0.18	0.00	0.00	22.3
15	480	-683	-744	264	0	-360	696	4.02	4.02	4.02	4.02	2	0.10	0.02	0.13	0.00	0.00	22.3
16	480	247	-974	382	0	-579	-607	4.02	4.02	4.02	4.02	2	0.16	0.03	0.17	0.00	0.00	22.3
17	480	-811	-731	296	0	-410	714	4.02	4.02	4.02	4.02	2	0.11	0.02	0.13	0.00	0.00	22.3
18	480	1374	-1010	664	0	-916	1040	4.02	4.02	4.02	4.02	3	0.23	0.03	0.18	0.00	0.00	22.3
19	480	-922	-985	943	0	-1363	953	4.02	4.02	4.02	4.02	3	0.33	0.03	0.17	0.00	0.00	22.3
20	480	248	-912	677	0	-921	1114	4.02	4.02	4.02	4.02	3	0.23	0.03	0.16	0.00	0.00	22.3
37	480	1969	-1058	446	0	-597	972	4.02	4.02	4.02	4.02	3	0.15	0.03	0.19	0.00	0.00	22.3
38	480	-1859	-1015	912	0	-1340	826	4.02	4.02	4.02	4.02	3	0.31	0.03	0.17	0.00	0.00	22.3
39	480	92	-894	468	0	-605	1094	4.02	4.02	4.02	4.02	3	0.16	0.03	0.16	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	540	-283	-1511	420	0	-861	-1421	4.02	4.02	4.02	4.02	3	0.21	0.04	0.27	0.00	0.00	22.3
2	540	154	-1221	282	0	-579	-1268	4.02	4.02	4.02	4.02	2	0.19	0.04	0.22	0.00	0.00	22.3
3	540	-163	-1148	256	0	-513	-1050	4.02	4.02	4.02	4.02	2	0.16	0.03	0.20	0.00	0.00	22.3
4	540	-272	-1177	390	0	-812	-1135	4.02	4.02	4.02	4.02	2	0.22	0.03	0.21	0.00	0.00	22.3
5	540	-590	-1105	364	0	-746	-917	4.02	4.02	4.02	4.02	2	0.20	0.03	0.19	0.00	0.00	22.3
6	540	376	-1291	350	0	-738	-1476	4.02	4.02	4.02	4.02	2	0.23	0.04	0.23	0.00	0.00	22.3
7	540	-683	-1048	264	0	-518	-749	4.02	4.02	4.02	4.02	2	0.14	0.03	0.18	0.00	0.00	22.3
8	540	247	-1278	382	0	-808	-1436	4.02	4.02	4.02	4.02	2	0.22	0.04	0.23	0.00	0.00	22.3
9	540	-811	-1035	296	0	-588	-709	4.02	4.02	4.02	4.02	2	0.16	0.03	0.18	0.00	0.00	22.3
10	540	154	-1221	282	0	-579	-1268	4.02	4.02	4.02	4.02	2	0.19	0.04	0.22	0.00	0.00	22.3
11	540	-163	-1148	256	0	-513	-1050	4.02	4.02	4.02	4.02	2	0.16	0.03	0.20	0.00	0.00	22.3
12	540	-272	-1177	390	0	-812	-1135	4.02	4.02	4.02	4.02	2	0.22	0.03	0.21	0.00	0.00	22.3
13	540	-590	-1105	364	0	-746	-917	4.02	4.02	4.02	4.02	2	0.20	0.03	0.19	0.00	0.00	22.3
14	540	376	-1291	350	0	-738	-1476	4.02	4.02	4.02	4.02	2	0.23	0.04	0.23	0.00	0.00	22.3
15	540	-683	-1048	264	0	-518	-749	4.02	4.02	4.02	4.02	2	0.14	0.03	0.18	0.00	0.00	22.3
16	540	247	-1278	382	0	-808	-1436	4.02	4.02	4.02	4.02	2	0.22	0.04	0.23	0.00	0.00	22.3
17	540	-811	-1035	296	0	-588	-709	4.02	4.02	4.02	4.02	2	0.16	0.03	0.18	0.00	0.00	22.3
18	540	1374	-1406	664	0	-1315	-907	4.02	4.02	4.02	4.02	3	0.34	0.04	0.25	0.00	0.00	22.3
19	540	-922	-1381	943	0	-1929	-955	4.02	4.02	4.02	4.02	3	0.46	0.04	0.24	0.00	0.00	22.3
20	540	248	-1308	677	0	-1327	-676	4.02	4.02	4.02	4.02	3	0.33	0.04	0.23	0.00	0.00	22.3
37	540	1969	-1453	446	0	-865	-1052	4.02	4.02	4.02	4.02	3	0.22	0.04	0.26	0.00	0.00	22.3
38	540	-1859	-1411	912	0	-1888	-1130	4.02	4.02	4.02	4.02	3	0.44	0.04	0.24	0.00	0.00	22.3
39	540	92	-1289	468	0	-885	-666	4.02	4.02	4.02	4.02	3	0.22	0.04	0.23	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	600	-283	-1907	420	0	-1113	-1681	4.02	4.02	4.02	4.02	3	0.27	0.06	0.34	0.00	0.00	22.3
2	600	154	-1525	282	0	-748	-1474	4.02	4.02	4.02	4.02	2	0.22	0.04	0.27	0.00	0.00	22.3
3	600	-163	-1452	256	0	-667	-1249	4.02	4.02	4.02	4.02	2	0.19	0.04	0.26	0.00	0.00	22.3
4	600	-272	-1481	390	0	-1046	-1337	4.02	4.02	4.02	4.02	2	0.29	0.04	0.26	0.00	0.00	22.3
5	600	-590	-1409	364	0	-964	-1112	4.02	4.02	4.02	4.02	2	0.26	0.04	0.25	0.00	0.00	22.3
6	600	376	-1595	350	0	-947	-1688	4.02	4.02	4.02	4.02	2	0.26	0.05	0.28	0.00	0.00	22.3
7	600	-683	-1352	264	0	-676	-938	4.02	4.02	4.02	4.02	2	0.18	0.04	0.24	0.00	0.00	22.3
8	600	247	-1582	382	0	-1037	-1647	4.02	4.02	4.02	4.02	2	0.29	0.05	0.28	0.00	0.00	22.3
9	600	-811	-1339	296	0	-765	-897	4.02	4.02	4.02	4.02	2	0.21	0.04	0.23	0.00	0.00	22.3
10	600	154	-1525	282	0	-748	-1474	4.02	4.02	4.02	4.02	2	0.22	0.04	0.27	0.00	0.00	22.3
11	600	-163	-1452	256	0	-667	-1249	4.02	4.02	4.02	4.02	2	0.19	0.04	0.26	0.00	0.00	22.3
12	600	-272	-1481	390	0	-1046	-1337	4.02	4.02	4.02	4.02	2	0.29	0.04	0.26	0.00	0.00	22.3
13	600	-590	-1409	364	0	-964	-1112	4.02	4.02	4.02	4.02	2	0.26	0.04	0.25	0.00	0.00	22.3
14	600	376	-1595	350	0	-947	-1688	4.02	4.02	4.02	4.02	2	0.26	0.05	0.28	0.00	0.00	22.3
15	600	-683	-1352	264	0	-676	-938	4.02	4.02	4.02	4.02	2	0.18	0.04	0.24	0.00	0.00	22.3
16	600	247	-1582	382	0	-1037	-1647	4.02	4.02	4.02	4.02	2	0.29	0.05	0.28	0.00	0.00	22.3
17	600	-811	-1339	296	0	-765	-897	4.02	4.02	4.02	4.02	2	0.21	0.04	0.23	0.00	0.00	22.3
18	600	1374	-1801	664	0	-1713	-1158	4.02	4.02	4.02	4.02	3	0.44	0.05	0.32	0.00	0.00	22.3
19	600	-922	-1776	943	0	-2495	-1203	4.02	4.02	4.02	4.02	3	0.60	0.05	0.31	0.00	0.00	22.3
20	600	248	-1703	677	0	-1733	-917	4.02	4.02	4.02	4.02	3	0.43	0.05	0.30	0.00	0.00	22.3
37	600	1969	-1849	446	0	-1133	-1307	4.02	4.02	4.02	4.02	3	0.29	0.05	0.33	0.00	0.00	22.3
38	600	-1859	-1806	912	0	-2435	-1381	4.02	4.02	4.02	4.02	3	0.57	0.05	0.31	0.00	0.00	22.3
39	600	92	-1685	468	0	-1166	-905	4.02	4.02	4.02	4.02	3	0.29	0.05	0.30	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

Nome travata: **Trave_403_IP1** Descrizione: **Trave_4 7-6-5-4-3-2-1**
ASTA NUM. 14 NI 253 NF 291 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y Permanente qy tot.
qy medio: 375.00 132.00 507.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	1321	1923	808	0	2283	-2002	4.02	4.02	4.02	4.02	3	0.58	0.06	0.34	0.00	0.00	22.3
2	0	1134	1416	575	0	1625	-1352	4.02	4.02	4.02	4.02	2	0.47	0.04	0.25	0.00	0.00	22.3
3	0	992	1498	570	0	1617	-1588	4.02	4.02	4.02	4.02	2	0.46	0.04	0.27	0.00	0.00	22.3
4	0	1040	1459	673	0	1895	-1493	4.02	4.02	4.02	4.02	2	0.54	0.04	0.26	0.00	0.00	22.3
5	0	898	1541	668	0	1887	-1729	4.02	4.02	4.02	4.02	2	0.54	0.04	0.27	0.00	0.00	22.3
6	0	1267	1336	615	0	1729	-1126	4.02	4.02	4.02	4.02	2	0.50	0.04	0.24	0.00	0.00	22.3
7	0	793	1609	599	0	1702	-1912	4.02	4.02	4.02	4.02	2	0.48	0.05	0.29	0.00	0.00	22.3
8	0	1239	1349	645	0	1810	-1168	4.02	4.02	4.02	4.02	2	0.52	0.04	0.24	0.00	0.00	22.3
9	0	765	1622	628	0	1783	-1955	4.02	4.02	4.02	4.02	2	0.50	0.05	0.29	0.00	0.00	22.3
10	0	1134	1416	575	0	1625	-1352	4.02	4.02	4.02	4.02	2	0.47	0.04	0.25	0.00	0.00	22.3
11	0	992	1498	570	0	1617	-1588	4.02	4.02	4.02	4.02	2	0.46	0.04	0.27	0.00	0.00	22.3
12	0	1040	1459	673	0	1895	-1493	4.02	4.02	4.02	4.02	2	0.54	0.04	0.26	0.00	0.00	22.3
13	0	898	1541	668	0	1887	-1729	4.02	4.02	4.02	4.02	2	0.54	0.04	0.27	0.00	0.00	22.3
14	0	1267	1336	615	0	1729	-1126	4.02	4.02	4.02	4.02	2	0.50	0.04	0.24	0.00	0.00	22.3
15	0	793	1609	599	0	1702	-1912	4.02	4.02	4.02	4.02	2	0.48	0.05	0.29	0.00	0.00	22.3
16	0	1239	1349	645	0	1810	-1168	4.02	4.02	4.02	4.02	2	0.52	0.04	0.24	0.00	0.00	22.3
17	0	765	1622	628	0	1783	-1955	4.02	4.02	4.02	4.02	2	0.50	0.05	0.29	0.00	0.00	22.3
18	0	6001	1523	1567	0	4356	-1403	6.03	4.02	4.02	4.02	3	0.86	0.05	0.27	0.00	0.00	22.3
19	0	2755	1894	1682	0	4731	-2173	6.03	4.02	4.02	4.02	3	0.87	0.05	0.34	0.00	0.00	22.3
20	0	4382	1834	1507	0	4213	-2123	6.03	4.02	4.02	4.02	3	0.80	0.05	0.33	0.00	0.00	22.3
37	0	6077	1469	1263	0	3496	-1216	6.03	4.02	4.02	4.02	3	0.69	0.04	0.26	0.00	0.00	22.3
38	0	666	2088	1454	0	4120	-2499	6.03	4.02	4.02	4.02	3	0.73	0.06	0.37	0.00	0.00	22.3
39	0	3378	1987	1163	0	3256	-2414	4.02	4.02	4.02	4.02	3	0.88	0.06	0.35	0.00	0.00	22.3

apost= 2.01 aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	60	1321	1528	808	0	1798	-1740	4.02	4.02	4.02	4.02	3	0.46	0.04	0.27	0.00	0.00	22.3
2	60	1134	1112	575	0	1280	-1156	4.02	4.02	4.02	4.02	2	0.37	0.03	0.20	0.00	0.00	22.3
3	60	992	1194	570	0	1275	-1385	4.02	4.02	4.02	4.02	2	0.36	0.03	0.21	0.00	0.00	22.3
4	60	1040	1155	673	0	1491	-1293	4.02	4.02	4.02	4.02	2	0.43	0.03	0.21	0.00	0.00	22.3
5	60	898	1237	668	0	1486	-1522	4.02	4.02	4.02	4.02	2	0.42	0.04	0.22	0.00	0.00	22.3
6	60	1267	1032	615	0	1360	-938	4.02	4.02	4.02	4.02	2	0.39	0.03	0.18	0.00	0.00	22.3
7	60	793	1305	599	0	1343	-1698	4.02	4.02	4.02	4.02	2	0.38	0.04	0.23	0.00	0.00	22.3
8	60	1239	1045	645	0	1423	-979	4.02	4.02	4.02	4.02	2	0.41	0.03	0.19	0.00	0.00	22.3
9	60	765	1318	628	0	1406	-1740	4.02	4.02	4.02	4.02	2	0.40	0.04	0.23	0.00	0.00	22.3
10	60	1134	1112	575	0	1280	-1156	4.02	4.02	4.02	4.02	2	0.37	0.03	0.20	0.00	0.00	22.3
11	60	992	1194	570	0	1275	-1385	4.02	4.02	4.02	4.02	2	0.36	0.03	0.21	0.00	0.00	22.3
12	60	1040	1155	673	0	1491	-1293	4.02	4.02	4.02	4.02	2	0.43	0.03	0.21	0.00	0.00	22.3
13	60	898	1237	668	0	1486	-1522	4.02	4.02	4.02	4.02	2	0.42	0.04	0.22	0.00	0.00	22.3
14	60	1267	1032	615	0	1360	-938	4.02	4.02	4.02	4.02	2	0.39	0.03	0.18	0.00	0.00	22.3
15	60	793	1305	599	0	1343	-1698	4.02	4.02	4.02	4.02	2	0.38	0.04	0.23	0.00	0.00	22.3
16	60	1239	1045	645	0	1423	-979	4.02	4.02	4.02	4.02	2	0.41	0.03	0.19	0.00	0.00	22.3
17	60	765	1318	628	0	1406	-1740	4.02	4.02	4.02	4.02	2	0.40	0.04	0.23	0.00	0.00	22.3
18	60	6001	1128	1567	0	3416	-1179	4.02	4.02	4.02	4.02	3	1.00	0.05	0.25	0.00	0.00	22.3
19	60	2755	1499	1682	0	3722	-1914	4.02	4.02	4.02	4.02	3	0.99	0.05	0.27	0.00	0.00	22.3
20	60	4382	1438	1507	0	3309	-1870	4.02	4.02	4.02	4.02	3	0.92	0.05	0.26	0.00	0.00	22.3
37	60	6077	1074	1263	0	2738	-997	4.02	4.02	4.02	4.02	3	0.80	0.04	0.20	0.00	0.00	22.3
38	60	666	1692	1454	0	3247	-2222	4.02	4.02	4.02	4.02	3	0.81	0.05	0.30	0.00	0.00	22.3
39	60	3378	1592	1163	0	2558	-2146	4.02	4.02	4.02	4.02	3	0.69	0.05	0.28	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	120	1321	1132	808	0	1313	-743	4.02	4.02	4.02	4.02	3	0.33	0.03	0.20	0.00	0.00	22.3
2	120	1134	808	575	0	935	-426	4.02	4.02	4.02	4.02	2	0.27	0.02	0.14	0.00	0.00	22.3
3	120	992	890	570	0	933	-605	4.02	4.02	4.02	4.02	2	0.27	0.03	0.16	0.00	0.00	22.3
4	120	1040	851	673	0	1087	-537	4.02	4.02	4.02	4.02	2	0.31	0.02	0.15	0.00	0.00	22.3
5	120	898	933	668	0	1085	-717	4.02	4.02	4.02	4.02	2	0.31	0.03	0.17	0.00	0.00	22.3
6	120	1267	728	615	0	991	480	4.02	4.02	4.02	4.02	2	0.28	0.02	0.13	0.00	0.00	22.3
7	120	793	1001	599	0	983	-853	4.02	4.02	4.02	4.02	2	0.28	0.03	0.18	0.00	0.00	22.3
8	120	1239	741	645	0	1036	460	4.02	4.02	4.02	4.02	2	0.30	0.02	0.13	0.00	0.00	22.3
9	120	765	1014	628	0	1029	-887	4.02	4.02	4.02	4.02	2	0.29	0.03	0.18	0.00	0.00	22.3
10	120	1134	808	575	0	935	-426	4.02	4.02	4.02	4.02	2	0.27	0.02	0.14	0.00	0.00	22.3
11	120	992	890	570	0	933	-605	4.02	4.02	4.02	4.02	2	0.27	0.03	0.16	0.00	0.00	22.3
12	120	1040	851	673	0	1087	-537	4.02	4.02	4.02	4.02	2	0.31	0.02	0.15	0.00	0.00	22.3
13	120	898	933	668	0	1085	-717	4.02	4.02	4.02	4.02	2	0.31	0.03	0.17	0.00	0.00	22.3
14	120	1267	728	615	0	991	480	4.02	4.02	4.02	4.02	2	0.28	0.02	0.13	0.00	0.00	22.3
15	120	793	1001	599	0	983	-853	4.02	4.02	4.02	4.02	2	0.28	0.03	0.18	0.00	0.00	22.3
16	120	1239	741	645	0	1036	460	4.02	4.02	4.02	4.02	2	0.30	0.02	0.13	0.00	0.00	22.3
17	120	765	1014	628	0	1029	-887	4.02	4.02	4.02	4.02	2	0.29	0.03	0.18	0.00	0.00	22.3
18	120	6001	732	1567	0	2475	-421	4.02	4.02	4.02	4.02	3	0.72	0.05	0.25	0.00	0.00	22.3
19	120	2755	1103	1682	0	2713	-933	4.02	4.02	4.02	4.02	3	0.72	0.05	0.27	0.00	0.00	22.3
20	120	4382	1043	1507	0	2405	-925	4.02	4.02	4.02	4.02	3	0.67	0.05	0.24	0.00	0.00	22.3
37	120	6077	678	1263	0	1980	412	4.02	4.02	4.02	4.02	3	0.58	0.04	0.20	0.00	0.00	22.3
38	120	666	1297	1454	0	2375	-1125	4.02	4.02	4.02	4.02	3	0.59	0.05	0.23	0.00	0.00	22.3
39	120	3378	1196	1163	0	1861	-1110	4.02	4.02	4.02	4.02	3	0.50	0.04	0.21	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	180	1321	737	808	0	828	764	4.02	4.02	4.02	4.02	3	0.21	0.03	0.13	0.00	0.00	22.3
2	180	1134	503	575	0	590	616	4.02	4.02	4.02	4.02	2	0.17	0.02	0.09	0.00	0.00	22.3
3	180	992	585	570	0	591	584	4.02	4.02	4.02	4.02	2	0.17	0.02	0.10	0.00	0.00	22.3
4	180	1040	546	673	0	683	589	4.02	4.02	4.02	4.02	2	0.19	0.02	0.11	0.00	0.00	22.3
5	180	898	628	668	0	683	542	4.02	4.02	4.02	4.02	2	0.19	0.02	0.11	0.00	0.00	22.3
6	180	1267	423	615	0	622	620	4.02	4.02	4.02	4.02	2	0.18	0.02	0.10	0.00	0.00	22.3
7	180	793	696	599	0	624	515	4.02	4.02	4.02	4.02	2	0.18	0.02	0.12	0.00	0.00	22.3
8	180	1239	436	645	0	650	609	4.02	4.02	4.02	4.02	2	0.19	0.02	0.10	0.00	0.00	22.3
9	180	765	709	628	0	652	502	4.02	4.02	4.02	4.02	2	0.18	0.02	0.13	0.00	0.00	22.3
10	180	1134	503	575	0	590	616	4.02	4.02	4.02	4.02	2	0.17	0.02	0.09	0.00	0.00	22.3
11	180	992	585	570	0	591	584	4.02	4.02	4.02	4.02	2	0.17	0.02	0.10	0.00	0.00	22.3
12	180	1040	546	673	0	683	589	4.02	4.02	4.02	4.02	2	0.19	0.02	0.11	0.00	0.00	22.3
13	180	898	628	668	0	683	542	4.02	4.02	4.02	4.02	2	0.19	0.02	0.11	0.00	0.00	22.3
14	180	1267	423	615	0	622	620	4.02	4.02	4.02	4.02	2	0.18	0.02	0.10	0.00	0.00	22.3
15	180	793	696	599	0	624	515	4.02	4.02	4.02	4.02	2	0.18	0.02	0.12	0.00	0.00	22.3
16	180	1239	436	645	0	650	609	4.02	4.02	4.02	4.02	2	0.19	0.02	0.10	0.00	0.00	22.3
17	180	765	709	628	0	652	502	4.02	4.02	4.02	4.02	2	0.18	0.02	0.13	0.00	0.00	22.3
18	180	6001	336	1567	0	1535	354	4.02	4.02	4.02	4.02	3	0.45	0.05	0.25	0.00	0.00	22.3
19	180	2755	708	1682	0	1704	527	4.02	4.02	4.02	4.02	3	0.45	0.05	0.27	0.00	0.00	22.3
20	180	4382	647	1507	0	1501	412	4.02	4.02	4.02	4.02	3	0.42	0.05	0.24	0.00	0.00	22.3
37	180	6077	282	1263	0	1222	412	4.02	4.02	4.02	4.02	3	0.36	0.04	0.20	0.00	0.00	22.3
38	180	666	902	1454	0	1502	648	4.02	4.02	4.02	4.02	3	0.38	0.05	0.23	0.00	0.00	22.3
39	180	3378	801	1163	0	1163	500	4.02	4.02	4.02	4.02	3	0.31	0.04	0.19	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	240	1321	341	808	0	343	799	4.02	4.02	4.02	4.02	3	0.12	0.03	0.13	0.00	0.00	22.3
2	240	1134	199	575	0	245	616	4.02	4.02	4.02	4.02	2	0.10	0.02	0.09	0.00	0.00	22.3
3	240	992	281	570	0	249	626	4.02	4.02	4.02	4.02	2	0.10	0.02	0.09	0.00	0.00	22.3
4	240	1040	242	673	0	279	604	4.02	4.02	4.02	4.02	2	0.09	0.02	0.11	0.00	0.00	22.3
5	240	898	324	668	0	282	614	4.02	4.02	4.02	4.02	2	0.10	0.02	0.11	0.00	0.00	22.3
6	240	1267	119	615	0	253	620	4.02	4.02	4.02	4.02	2	0.10	0.02	0.10	0.00	0.00	22.3
7	240	793	392	599	0	265	634	4.02	4.02	4.02	4.02	2	0.10	0.02	0.10	0.00	0.00	22.3
8	240	1239	132	645	0	263	609	4.02	4.02	4.02	4.02	2	0.10	0.02	0.10	0.00	0.00	22.3
9	240	765	405	628	0	275	630	4.02	4.02	4.02	4.02	2	0.10	0.02	0.10	0.00	0.00	22.3
10	240	1134	199	575	0	245	616	4.02	4.02	4.02	4.02	2	0.10	0.02	0.09	0.00	0.00	22.3
11	240	992	281	570	0	249	626	4.02	4.02	4.02	4.02	2	0.10	0.02	0.09	0.00	0.00	22.3
12	240	1040	242	673	0	279	604	4.02	4.02	4.02	4.02	2	0.09	0.02	0.11	0.00	0.00	22.3
13	240	898	324	668	0	282	614	4.02	4.02	4.02	4.02	2	0.10	0.02	0.11	0.00	0.00	22.3
14	240	1267	119	615	0	253	620	4.02	4.02	4.02	4.02	2	0.10	0.02	0.10	0.00	0.00	22.3
15	240	793	392	599	0	265	634	4.02	4.02	4.02	4.02	2	0.10	0.02	0.10	0.00	0.00	22.3
16	240	1239	132	645	0	263	609	4.02	4.02	4.02	4.02	2	0.10	0.02	0.10	0.00	0.00	22.3
17	240	765	405	628	0	275	630	4.02	4.02	4.02	4.02	2	0.10	0.02	0.10	0.00	0.00	22.3
18	240	6001	-59	1567	0	595	354	4.02	4.02	4.02	4.02	3	0.17	0.05	0.25	0.00	0.00	22.3
19	240	2755	312	1682	0	695	544	4.02	4.02	4.02	4.02	3	0.18	0.05	0.27	0.00	0.00	22.3
20	240	4382	252	1507	0	597	412	4.02	4.02	4.02	4.02	3	0.17	0.05	0.24	0.00	0.00	22.3
37	240	6077	-113	1263	0	464	412	4.02	4.02	4.02	4.02	3	0.14	0.04	0.20	0.00	0.00	22.3
38	240	666	506	1454	0	630	799	4.02	4.02	4.02	4.02	3	0.16	0.05	0.23	0.00	0.00	22.3
39	240	3378	405	1163	0	466	581	4.02	4.02	4.02	4.02	3	0.13	0.04	0.19	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	300	1321	-54	808	0	-141	799	4.02	4.02	4.02	4.02	3	0.12	0.03	0.13	0.00	0.00	22.3
2	300	1134	-105	575	0	-100	616	4.02	4.02	4.02	4.02	2	0.10	0.02	0.09	0.00	0.00	22.3
3	300	992	-23	570	0	-93	626	4.02	4.02	4.02	4.02	2	0.10	0.02	0.09	0.00	0.00	22.3
4	300	1040	-62	673	0	-126	604	4.02	4.02	4.02	4.02	2	0.09	0.02	0.11	0.00	0.00	22.3

5	300	898	20	668	0	-119	614	4.02	4.02	4.02	4.02	2	0.10	0.02	0.11	0.00	0.00	22.3
6	300	1267	-185	615	0	-116	620	4.02	4.02	4.02	4.02	2	0.10	0.02	0.10	0.00	0.00	22.3
7	300	793	88	599	0	-94	634	4.02	4.02	4.02	4.02	2	0.10	0.02	0.10	0.00	0.00	22.3
8	300	1239	-172	645	0	-124	609	4.02	4.02	4.02	4.02	2	0.10	0.02	0.10	0.00	0.00	22.3
9	300	765	101	628	0	-102	630	4.02	4.02	4.02	4.02	2	0.10	0.02	0.10	0.00	0.00	22.3
10	300	1134	-105	575	0	-100	616	4.02	4.02	4.02	4.02	2	0.10	0.02	0.09	0.00	0.00	22.3
11	300	992	-23	570	0	-93	626	4.02	4.02	4.02	4.02	2	0.10	0.02	0.09	0.00	0.00	22.3
12	300	1040	-62	673	0	-126	604	4.02	4.02	4.02	4.02	2	0.09	0.02	0.11	0.00	0.00	22.3
13	300	898	20	668	0	-119	614	4.02	4.02	4.02	4.02	2	0.10	0.02	0.11	0.00	0.00	22.3
14	300	1267	-185	615	0	-116	620	4.02	4.02	4.02	4.02	2	0.10	0.02	0.10	0.00	0.00	22.3
15	300	793	88	599	0	-94	634	4.02	4.02	4.02	4.02	2	0.10	0.02	0.10	0.00	0.00	22.3
16	300	1239	-172	645	0	-124	609	4.02	4.02	4.02	4.02	2	0.10	0.02	0.10	0.00	0.00	22.3
17	300	765	101	628	0	-102	630	4.02	4.02	4.02	4.02	2	0.10	0.02	0.10	0.00	0.00	22.3
18	300	6001	-455	1567	0	-346	354	4.02	4.02	4.02	4.02	3	0.10	0.05	0.25	0.00	0.00	22.3
19	300	2755	-83	1682	0	-314	544	4.02	4.02	4.02	4.02	3	0.08	0.05	0.27	0.00	0.00	22.3
20	300	4382	-144	1507	0	-308	412	4.02	4.02	4.02	4.02	3	0.09	0.05	0.24	0.00	0.00	22.3
37	300	6077	-509	1263	0	-295	412	4.02	4.02	4.02	4.02	3	0.09	0.04	0.20	0.00	0.00	22.3
38	300	666	110	1454	0	-243	799	4.02	4.02	4.02	4.02	3	0.12	0.05	0.23	0.00	0.00	22.3
39	300	3378	10	1163	0	-232	581	4.02	4.02	4.02	4.02	3	0.09	0.04	0.19	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	360	1321	-450	808	0	-626	799	4.02	4.02	4.02	4.02	3	0.16	0.03	0.13	0.00	0.00	22.3
2	360	1134	-409	575	0	-444	616	4.02	4.02	4.02	4.02	2	0.13	0.02	0.09	0.00	0.00	22.3
3	360	992	-327	570	0	-435	626	4.02	4.02	4.02	4.02	2	0.12	0.02	0.09	0.00	0.00	22.3
4	360	1040	-366	673	0	-530	604	4.02	4.02	4.02	4.02	2	0.15	0.02	0.11	0.00	0.00	22.3
5	360	898	-284	668	0	-520	614	4.02	4.02	4.02	4.02	2	0.15	0.02	0.11	0.00	0.00	22.3
6	360	1267	-489	615	0	-485	620	4.02	4.02	4.02	4.02	2	0.14	0.02	0.10	0.00	0.00	22.3
7	360	793	-216	599	0	-454	634	4.02	4.02	4.02	4.02	2	0.13	0.02	0.10	0.00	0.00	22.3
8	360	1239	-476	645	0	-511	609	4.02	4.02	4.02	4.02	2	0.15	0.02	0.10	0.00	0.00	22.3
9	360	765	-203	628	0	-479	630	4.02	4.02	4.02	4.02	2	0.14	0.02	0.10	0.00	0.00	22.3
10	360	1134	-409	575	0	-444	616	4.02	4.02	4.02	4.02	2	0.13	0.02	0.09	0.00	0.00	22.3
11	360	992	-327	570	0	-435	626	4.02	4.02	4.02	4.02	2	0.12	0.02	0.09	0.00	0.00	22.3
12	360	1040	-366	673	0	-530	604	4.02	4.02	4.02	4.02	2	0.15	0.02	0.11	0.00	0.00	22.3
13	360	898	-284	668	0	-520	614	4.02	4.02	4.02	4.02	2	0.15	0.02	0.11	0.00	0.00	22.3
14	360	1267	-489	615	0	-485	620	4.02	4.02	4.02	4.02	2	0.14	0.02	0.10	0.00	0.00	22.3
15	360	793	-216	599	0	-454	634	4.02	4.02	4.02	4.02	2	0.13	0.02	0.10	0.00	0.00	22.3
16	360	1239	-476	645	0	-511	609	4.02	4.02	4.02	4.02	2	0.15	0.02	0.10	0.00	0.00	22.3
17	360	765	-203	628	0	-479	630	4.02	4.02	4.02	4.02	2	0.14	0.02	0.10	0.00	0.00	22.3
18	360	6001	-850	1567	0	-1286	-622	4.02	4.02	4.02	4.02	3	0.38	0.05	0.25	0.00	0.00	22.3
19	360	2755	-478	1682	0	-1324	544	4.02	4.02	4.02	4.02	3	0.35	0.05	0.27	0.00	0.00	22.3
20	360	4382	-539	1507	0	-1212	412	4.02	4.02	4.02	4.02	3	0.34	0.05	0.24	0.00	0.00	22.3
37	360	6077	-904	1263	0	-1053	-656	4.02	4.02	4.02	4.02	3	0.31	0.04	0.20	0.00	0.00	22.3
38	360	666	-285	1454	0	-1116	799	4.02	4.02	4.02	4.02	3	0.28	0.05	0.23	0.00	0.00	22.3
39	360	3378	-385	1163	0	-930	581	4.02	4.02	4.02	4.02	3	0.25	0.04	0.19	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	420	1321	-845	808	0	-1111	687	4.02	4.02	4.02	4.02	3	0.28	0.03	0.15	0.00	0.00	22.3
2	420	1134	-713	575	0	-789	487	4.02	4.02	4.02	4.02	2	0.23	0.02	0.13	0.00	0.00	22.3
3	420	992	-631	570	0	-777	553	4.02	4.02	4.02	4.02	2	0.22	0.02	0.11	0.00	0.00	22.3
4	420	1040	-670	673	0	-934	505	4.02	4.02	4.02	4.02	2	0.27	0.02	0.12	0.00	0.00	22.3
5	420	898	-588	668	0	-921	571	4.02	4.02	4.02	4.02	2	0.26	0.02	0.11	0.00	0.00	22.3
6	420	1267	-793	615	0	-854	414	4.02	4.02	4.02	4.02	2	0.25	0.02	0.14	0.00	0.00	22.3
7	420	793	-520	599	0	-813	634	4.02	4.02	4.02	4.02	2	0.23	0.02	0.10	0.00	0.00	22.3
8	420	1239	-780	645	0	-898	420	4.02	4.02	4.02	4.02	2	0.26	0.02	0.14	0.00	0.00	22.3
9	420	765	-507	628	0	-856	630	4.02	4.02	4.02	4.02	2	0.24	0.02	0.10	0.00	0.00	22.3
10	420	1134	-713	575	0	-789	487	4.02	4.02	4.02	4.02	2	0.23	0.02	0.13	0.00	0.00	22.3
11	420	992	-631	570	0	-777	553	4.02	4.02	4.02	4.02	2	0.22	0.02	0.11	0.00	0.00	22.3
12	420	1040	-670	673	0	-934	505	4.02	4.02	4.02	4.02	2	0.27	0.02	0.12	0.00	0.00	22.3
13	420	898	-588	668	0	-921	571	4.02	4.02	4.02	4.02	2	0.26	0.02	0.11	0.00	0.00	22.3
14	420	1267	-793	615	0	-854	414	4.02	4.02	4.02	4.02	2	0.25	0.02	0.14	0.00	0.00	22.3
15	420	793	-520	599	0	-813	634	4.02	4.02	4.02	4.02	2	0.23	0.02	0.10	0.00	0.00	22.3
16	420	1239	-780	645	0	-898	420	4.02	4.02	4.02	4.02	2	0.26	0.02	0.14	0.00	0.00	22.3
17	420	765	-507	628	0	-856	630	4.02	4.02	4.02	4.02	2	0.24	0.02	0.10	0.00	0.00	22.3
18	420	6001	-1246	1567	0	-2226	-1450	4.02	4.02	4.02	4.02	3	0.65	0.05	0.25	0.00	0.00	22.3
19	420	2755	-874	1682	0	-2333	-473	4.02	4.02	4.02	4.02	3	0.62	0.05	0.27	0.00	0.00	22.3
20	420	4382	-934	1507	0	-2116	-707	4.02	4.02	4.02	4.02	3	0.59	0.05	0.24	0.00	0.00	22.3
37	420	6077	-1300	1263	0	-1811	-1517	4.02	4.02	4.02	4.02	3	0.53	0.04	0.23	0.00	0.00	22.3
38	420	666	-680	1454	0	-1988	799	4.02	4.02	4.02	4.02	3	0.50	0.05	0.23	0.00	0.00	22.3
39	420	3378	-781	1163	0	-1627	513	4.02	4.02	4.02	4.02	3	0.44	0.04	0.19	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	480	1321	-1241	808	0	-1596	-995	4.02	4.02	4.02	4.02	3	0.41	0.04	0.22	0.00	0.00	22.3
2	480	1134	-1018	575	0	-1134	-909	4.02	4.02	4.02	4.02	2	0.32	0.03	0.18	0.00	0.00	22.3
3	480	992	-936	570	0	-1119	-710	4.02	4.02	4.02	4.02	2	0.32	0.03	0.17	0.00	0.00	22.3
4	480	1040	-975	673	0	-1338	-821	4.02	4.02	4.02	4.02	2	0.38	0.03	0.17	0.00	0.00	22.3
5	480	898	-893	668	0	-1323	-623	4.02	4.02	4.02	4.02	2	0.38	0.03	0.16	0.00	0.00	22.3
6	480	1267	-1098	615	0	-1223	-1110	4.02	4.02	4.02	4.02	2	0.35	0.03	0.20	0.00	0.00	22.3
7	480	793	-825	599	0	-1172	-447	4.02	4.02	4.02	4.02	2	0.33	0.02	0.15	0.00	0.00	22.3
8	480	1239	-1085	645	0	-1284	-1084	4.02	4.02	4.02	4.02	2	0.37	0.03	0.19	0.00	0.00	22.3
9	480	765	-812	628	0	-1233	-421	4.02	4.02	4.02	4.02	2	0.35	0.02	0.14	0.00	0.00	22.3
10	480	1134	-1018	575	0	-1134	-909	4.02	4.02	4.02	4.02	2	0.32	0.03	0.18	0.00	0.00	22.3
11	480	992	-936	570	0	-1119	-710	4.02	4.02	4.02	4.02	2	0.32	0.03	0.17	0.00	0.00	22.3
12	480	1040	-975	673	0	-1338	-821	4.02	4.02	4.02	4.02	2	0.38	0.03	0.17	0.00	0.00	22.3
13	480	898	-893	668	0	-1323	-623	4.02	4.02	4.02	4.02	2	0.38	0.03	0.16	0.00	0.00	22.3
14	480	1267	-1098	615	0	-1223	-1110	4.02	4.02	4.02	4.02	2	0.35	0.03	0.20	0.00	0.00	22.3
15	480	793	-825	599	0	-1172	-447	4.02	4.02	4.02	4.02	2	0.33	0.02	0.15	0.00	0.00	22.3
16	480	1239	-1085	645	0	-1284	-1084	4.02	4.02	4.02	4.02	2	0.37	0.03	0.19	0.00	0.00	22.3
17	480	765	-812	628	0	-1233	-421	4.02	4.02	4.02	4.02	2	0.35	0.02	0.14	0.00	0.00	22.3
18	480	6001	-1641	1567	0	-3166	-2516	4.02	4.02	4.02	4.02	3	0.92	0.05	0.29	0.00	0.00	22.3
19	480	2755	-1269	1682	0	-3342	-1316	4.02	4.02	4.02	4.02	3	0.89	0.05	0.27	0.00	0.00	22.3
20	480	4382	-1330	1507	0	-3020	-1587	4.02	4.02	4.02	4.02	3	0.84	0.05	0.24	0.00	0.00	22.3
37	480	6077	-1695	1263	0	-2569	-2615	4.02	4.02	4.02	4.02	3	0.75	0.05	0.30	0.00	0.00	22.3
38	480	666	-1076	1454	0	-2861	-614	4.02	4.02	4.02	4.02	3	0.72	0.05	0.23	0.00	0.00	22.3
39	480	3378	-1176	1163	0	-2325	-1065	4.02	4.02	4.02	4.02	3	0.63	0.04	0.21	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	540	1321	-1636	808	0	-2081	-2059	4.02	4.02	4.02	4.02	3	0.53	0.05	0.29	0.00	0.00	22.3
2	540	1134	-1322	575	0	-1479	-1764	4.02	4.02	4.02	4.02	2	0.42	0.04	0.24	0.00	0.00	22.3
3	540	992	-1240	570	0	-1461	-1517	4.02	4.02	4.02	4.02	2	0.42	0.04	0.22	0.00	0.00	22.3
4	540	1040	-1279	673	0	-1742	-1651	4.02	4.02	4.02	4.02	2	0.50	0.04	0.23	0.00	0.00	22.3
5	540	898	-1197	668	0	-1724	-1404	4.02	4.02	4.02	4.02	2	0.49	0.03	0.21	0.00	0.00	22.3
6	540	1267	-1402	615	0	-1592	-2014	4.02	4.02	4.02	4.02	2	0.46	0.04	0.25	0.00	0.00	22.3
7	540	793	-1129	599	0	-1532	-1187	4.02	4.02	4.02	4.02	2	0.43	0.03	0.20	0.00	0.00	22.3
8	540	1239	-1389	645	0	-1671	-1980	4.02	4.02	4.02	4.02	2	0.48	0.04	0.25	0.00	0.00	22.3
9	540	765	-1116	628	0	-1610	-1153	4.02	4.02	4.02	4.02	2	0.46	0.03	0.20	0.00	0.00	22.3
10	540	1134	-1322	575	0	-1479	-1764	4.02	4.02	4.02	4.02	2	0.42	0.04	0.24	0.00	0.00	22.3

11	540	992	-1240	570	0	-1461	-1517	4.02	4.02	4.02	4.02	2	0.42	0.04	0.22	0.00	0.00	22.3
12	540	1040	-1279	673	0	-1742	-1651	4.02	4.02	4.02	4.02	2	0.50	0.04	0.23	0.00	0.00	22.3
13	540	898	-1197	668	0	-1724	-1404	4.02	4.02	4.02	4.02	2	0.49	0.03	0.21	0.00	0.00	22.3
14	540	1267	-1402	615	0	-1592	-2014	4.02	4.02	4.02	4.02	2	0.46	0.04	0.25	0.00	0.00	22.3
15	540	793	-1129	599	0	-1532	-1187	4.02	4.02	4.02	4.02	2	0.43	0.03	0.20	0.00	0.00	22.3
16	540	1239	-1389	645	0	-1671	-1980	4.02	4.02	4.02	4.02	2	0.48	0.04	0.25	0.00	0.00	22.3
17	540	765	-1116	628	0	-1610	-1153	4.02	4.02	4.02	4.02	2	0.46	0.03	0.20	0.00	0.00	22.3
18	540	6001	-2036	1567	0	-4107	-3820	4.02	6.03	4.02	4.02	3	0.81	0.06	0.36	0.00	0.00	22.3
19	540	2755	-1665	1682	0	-4351	-2396	4.02	6.03	4.02	4.02	3	0.80	0.05	0.30	0.00	0.00	22.3
20	540	4382	-1725	1507	0	-3924	-2704	4.02	6.03	4.02	4.02	3	0.75	0.05	0.31	0.00	0.00	22.3
37	540	6077	-2090	1263	0	-3327	-3951	4.02	4.02	4.02	4.02	3	0.97	0.06	0.37	0.00	0.00	22.3
38	540	666	-1471	1454	0	-3733	-1579	4.02	4.02	4.02	4.02	3	0.93	0.05	0.26	0.00	0.00	22.3
39	540	3378	-1572	1163	0	-3022	-2090	4.02	4.02	4.02	4.02	3	0.82	0.05	0.28	0.00	0.00	22.3

apost= -- aant= 2.01 ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	600	1321	-2032	808	0	-2566	-2331	4.02	4.02	4.02	4.02	3	0.65	0.06	0.36	0.00	0.00	22.3
2	600	1134	-1626	575	0	-1824	-1979	4.02	4.02	4.02	4.02	2	0.52	0.05	0.29	0.00	0.00	22.3
3	600	992	-1544	570	0	-1803	-1724	4.02	4.02	4.02	4.02	2	0.51	0.04	0.28	0.00	0.00	22.3
4	600	1040	-1583	673	0	-2146	-1862	4.02	4.02	4.02	4.02	2	0.61	0.05	0.28	0.00	0.00	22.3
5	600	898	-1501	668	0	-2125	-1607	4.02	4.02	4.02	4.02	2	0.60	0.04	0.27	0.00	0.00	22.3
6	600	1267	-1706	615	0	-1961	-2237	4.02	4.02	4.02	4.02	2	0.56	0.05	0.30	0.00	0.00	22.3
7	600	793	-1433	599	0	-1891	-1384	4.02	4.02	4.02	4.02	2	0.54	0.04	0.26	0.00	0.00	22.3
8	600	1239	-1693	645	0	-2058	-2202	4.02	4.02	4.02	4.02	2	0.59	0.05	0.30	0.00	0.00	22.3
9	600	765	-1420	628	0	-1987	-1349	4.02	4.02	4.02	4.02	2	0.56	0.04	0.25	0.00	0.00	22.3
10	600	1134	-1626	575	0	-1824	-1979	4.02	4.02	4.02	4.02	2	0.52	0.05	0.29	0.00	0.00	22.3
11	600	992	-1544	570	0	-1803	-1724	4.02	4.02	4.02	4.02	2	0.51	0.04	0.28	0.00	0.00	22.3
12	600	1040	-1583	673	0	-2146	-1862	4.02	4.02	4.02	4.02	2	0.61	0.05	0.28	0.00	0.00	22.3
13	600	898	-1501	668	0	-2125	-1607	4.02	4.02	4.02	4.02	2	0.60	0.04	0.27	0.00	0.00	22.3
14	600	1267	-1706	615	0	-1961	-2237	4.02	4.02	4.02	4.02	2	0.56	0.05	0.30	0.00	0.00	22.3
15	600	793	-1433	599	0	-1891	-1384	4.02	4.02	4.02	4.02	2	0.54	0.04	0.26	0.00	0.00	22.3
16	600	1239	-1693	645	0	-2058	-2202	4.02	4.02	4.02	4.02	2	0.59	0.05	0.30	0.00	0.00	22.3
17	600	765	-1420	628	0	-1987	-1349	4.02	4.02	4.02	4.02	2	0.56	0.04	0.25	0.00	0.00	22.3
18	600	6001	-2432	1567	0	-5047	-4129	4.02	6.03	4.02	4.02	3	0.99	0.07	0.43	0.00	0.00	22.3
19	600	2755	-2060	1682	0	-5360	-2671	4.02	6.03	4.02	4.02	3	0.99	0.06	0.37	0.00	0.00	22.3
20	600	4382	-2121	1507	0	-4828	-2984	4.02	6.03	4.02	4.02	3	0.92	0.06	0.38	0.00	0.00	22.3
37	600	6077	-2486	1263	0	-4085	-4265	4.02	6.03	4.02	4.02	3	0.80	0.07	0.44	0.00	0.00	22.3
38	600	666	-1867	1454	0	-4606	-1835	4.02	6.03	4.02	4.02	3	0.81	0.05	0.33	0.00	0.00	22.3
39	600	3378	-1967	1163	0	-3720	-2356	4.02	6.03	4.02	4.02	3	0.69	0.06	0.35	0.00	0.00	22.3

apost= -- aant= 2.01 ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

Nome travata: **Trave_404_IP1** Descrizione: **Trave_4 32-25**
ASTA NUM. 15 NI 26 NF 254 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y Permanente qy tot.
qy medio: 375.00 132.00 507.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	1274	2019	984	0	3130	-2106	4.02	4.02	4.02	4.02	3	0.80	0.06	0.36	0.00	0.00	22.3
2	0	1200	1535	818	0	2609	-1575	4.02	4.02	4.02	4.02	2	0.75	0.04	0.27	0.00	0.00	22.3
3	0	930	1599	859	0	2770	-1791	4.02	4.02	4.02	4.02	2	0.79	0.05	0.28	0.00	0.00	22.3
4	0	1030	1507	655	0	2045	-1449	4.02	4.02	4.02	4.02	2	0.58	0.04	0.27	0.00	0.00	22.3
5	0	760	1572	696	0	2207	-1664	4.02	4.02	4.02	4.02	2	0.62	0.05	0.28	0.00	0.00	22.3
6	0	1455	1450	713	0	2223	-1279	4.02	4.02	4.02	4.02	2	0.64	0.04	0.26	0.00	0.00	22.3
7	0	556	1665	850	0	2761	-1998	4.02	4.02	4.02	4.02	2	0.78	0.05	0.30	0.00	0.00	22.3
8	0	1404	1442	664	0	2054	-1241	4.02	4.02	4.02	4.02	2	0.59	0.04	0.26	0.00	0.00	22.3
9	0	504	1657	801	0	2592	-1960	4.02	4.02	4.02	4.02	2	0.73	0.05	0.30	0.00	0.00	22.3
10	0	1200	1535	818	0	2609	-1575	4.02	4.02	4.02	4.02	2	0.75	0.04	0.27	0.00	0.00	22.3
11	0	930	1599	859	0	2770	-1791	4.02	4.02	4.02	4.02	2	0.79	0.05	0.28	0.00	0.00	22.3
12	0	1030	1507	655	0	2045	-1449	4.02	4.02	4.02	4.02	2	0.58	0.04	0.27	0.00	0.00	22.3
13	0	760	1572	696	0	2207	-1664	4.02	4.02	4.02	4.02	2	0.62	0.05	0.28	0.00	0.00	22.3
14	0	1455	1450	713	0	2223	-1279	4.02	4.02	4.02	4.02	2	0.64	0.04	0.26	0.00	0.00	22.3
15	0	556	1665	850	0	2761	-1998	4.02	4.02	4.02	4.02	2	0.78	0.05	0.30	0.00	0.00	22.3
16	0	1404	1442	664	0	2054	-1241	4.02	4.02	4.02	4.02	2	0.59	0.04	0.26	0.00	0.00	22.3
17	0	504	1657	801	0	2592	-1960	4.02	4.02	4.02	4.02	2	0.73	0.05	0.30	0.00	0.00	22.3
18	0	3300	2140	2274	0	7303	-2626	10.05	4.02	4.02	4.02	3	0.84	0.07	0.38	0.00	0.00	22.3
19	0	2815	2023	1572	0	4945	-2061	6.03	4.02	4.02	4.02	3	0.91	0.06	0.36	0.00	0.00	22.3
20	0	3493	2101	1961	0	6379	-2399	8.04	4.02	4.02	4.02	3	0.91	0.06	0.37	0.00	0.00	22.3
37	0	2876	2159	2201	0	7110	-2738	10.05	4.02	4.02	4.02	3	0.82	0.07	0.38	0.00	0.00	22.3
38	0	2068	1964	1031	0	3181	-1797	4.02	4.02	4.02	4.02	3	0.83	0.06	0.35	0.00	0.00	22.3
39	0	3198	2094	1679	0	5570	-2360	8.04	4.02	4.02	4.02	3	0.79	0.06	0.37	0.00	0.00	22.3

apost= 6.03 aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	60	1274	1624	984	0	2540	-1835	4.02	4.02	4.02	4.02	3	0.65	0.05	0.29	0.00	0.00	22.3
2	60	1200	1231	818	0	2118	-1369	4.02	4.02	4.02	4.02	2	0.61	0.04	0.22	0.00	0.00	22.3
3	60	930	1295	859	0	2254	-1578	4.02	4.02	4.02	4.02	2	0.64	0.04	0.23	0.00	0.00	22.3
4	60	1030	1203	655	0	1652	-1245	4.02	4.02	4.02	4.02	2	0.47	0.03	0.21	0.00	0.00	22.3
5	60	760	1268	696	0	1790	-1454	4.02	4.02	4.02	4.02	2	0.51	0.04	0.23	0.00	0.00	22.3
6	60	1455	1146	713	0	1795	-1081	4.02	4.02	4.02	4.02	2	0.52	0.03	0.20	0.00	0.00	22.3
7	60	556	1361	850	0	2251	-1779	4.02	4.02	4.02	4.02	2	0.63	0.04	0.24	0.00	0.00	22.3
8	60	1404	1138	664	0	1655	-1043	4.02	4.02	4.02	4.02	2	0.48	0.03	0.20	0.00	0.00	22.3
9	60	504	1353	801	0	2112	-1742	4.02	4.02	4.02	4.02	2	0.59	0.04	0.24	0.00	0.00	22.3
10	60	1200	1231	818	0	2118	-1369	4.02	4.02	4.02	4.02	2	0.61	0.04	0.22	0.00	0.00	22.3
11	60	930	1295	859	0	2254	-1578	4.02	4.02	4.02	4.02	2	0.64	0.04	0.23	0.00	0.00	22.3
12	60	1030	1203	655	0	1652	-1245	4.02	4.02	4.02	4.02	2	0.47	0.03	0.21	0.00	0.00	22.3
13	60	760	1268	696	0	1790	-1454	4.02	4.02	4.02	4.02	2	0.51	0.04	0.23	0.00	0.00	22.3
14	60	1455	1146	713	0	1795	-1081	4.02	4.02	4.02	4.02	2	0.52	0.03	0.20	0.00	0.00	22.3
15	60	556	1361	850	0	2251	-1779	4.02	4.02	4.02	4.02	2	0.63	0.04	0.24	0.00	0.00	22.3
16	60	1404	1138	664	0	1655	-1043	4.02	4.02	4.02	4.02	2	0.48	0.03	0.20	0.00	0.00	22.3
17	60	504	1353	801	0	2112	-1742	4.02	4.02	4.02	4.02	2	0.59	0.04	0.24	0.00	0.00	22.3
18	60	3300	1744	2274	0	5938	-2344	8.04	4.02	4.02	4.02	3	0.85	0.07	0.37	0.00	0.00	22.3
19	60	2815	1628	1572	0	4002	-1790	6.03	4.02	4.02	4.02	3	0.74	0.05	0.29	0.00	0.00	22.3
20	60	3493	1706	1961	0	5203	-2121	6.03	4.02	4.02	4.02	3	0.97	0.06	0.32	0.00	0.00	22.3
37	60	2876	1764	2201	0	5789	-2454	8.04	4.02	4.02	4.02	3	0.82	0.07	0.35	0.00	0.00	22.3
38	60	2068	1569	1031	0	2562	-1531	4.02	4.02	4.02	4.02	3	0.67	0.05	0.28	0.00	0.00	22.3
39	60	3198	1698	1679	0	4563	-2082	6.03	4.02	4.02	4.02	3	0.85	0.05	0.30	0.00	0.00	22.3

apost= 4.02 aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	120	1274	1228	984	0	1949	-779	4.02	4.02	4.02	4.02	3	0.50	0.04	0.22	0.00	0.00	22.3
2	120	1200	927	818	0	1627	-568	4.02	4.02	4.02	4.02	2	0.47	0.03	0.17	0.00	0.00	22.3

3	120	930	991	859	0	1739	-738	4.02	4.02	4.02	4.02	2	0.49	0.03	0.18	0.00	0.00	22.3
4	120	1030	899	655	0	1259	-460	4.02	4.02	4.02	4.02	2	0.36	0.03	0.16	0.00	0.00	22.3
5	120	760	964	696	0	1372	-630	4.02	4.02	4.02	4.02	2	0.39	0.03	0.17	0.00	0.00	22.3
6	120	1455	842	713	0	1367	522	4.02	4.02	4.02	4.02	2	0.40	0.02	0.15	0.00	0.00	22.3
7	120	556	1057	850	0	1741	-900	4.02	4.02	4.02	4.02	2	0.49	0.03	0.19	0.00	0.00	22.3
8	120	1404	834	664	0	1257	546	4.02	4.02	4.02	4.02	2	0.36	0.02	0.15	0.00	0.00	22.3
9	120	504	1049	801	0	1631	-867	4.02	4.02	4.02	4.02	2	0.46	0.03	0.19	0.00	0.00	22.3
10	120	1200	927	818	0	1627	-568	4.02	4.02	4.02	4.02	2	0.47	0.03	0.17	0.00	0.00	22.3
11	120	930	991	859	0	1739	-738	4.02	4.02	4.02	4.02	2	0.49	0.03	0.18	0.00	0.00	22.3
12	120	1030	899	655	0	1259	-460	4.02	4.02	4.02	4.02	2	0.36	0.03	0.16	0.00	0.00	22.3
13	120	760	964	696	0	1372	-630	4.02	4.02	4.02	4.02	2	0.39	0.03	0.17	0.00	0.00	22.3
14	120	1455	842	713	0	1367	522	4.02	4.02	4.02	4.02	2	0.40	0.02	0.15	0.00	0.00	22.3
15	120	556	1057	850	0	1741	-900	4.02	4.02	4.02	4.02	2	0.49	0.03	0.19	0.00	0.00	22.3
16	120	1404	834	664	0	1257	546	4.02	4.02	4.02	4.02	2	0.36	0.02	0.15	0.00	0.00	22.3
17	120	504	1049	801	0	1631	-867	4.02	4.02	4.02	4.02	2	0.46	0.03	0.19	0.00	0.00	22.3
18	120	3300	1349	2274	0	4574	-1216	6.03	4.02	4.02	4.02	3	0.85	0.07	0.37	0.00	0.00	22.3
19	120	2815	1232	1572	0	3058	-732	4.02	4.02	4.02	4.02	3	0.81	0.05	0.25	0.00	0.00	22.3
20	120	3493	1310	1961	0	4026	-1016	6.03	4.02	4.02	4.02	3	0.75	0.06	0.32	0.00	0.00	22.3
37	120	2876	1368	2201	0	4468	-1314	6.03	4.02	4.02	4.02	3	0.82	0.07	0.35	0.00	0.00	22.3
38	120	2068	1173	1031	0	1943	679	4.02	4.02	4.02	4.02	3	0.51	0.03	0.21	0.00	0.00	22.3
39	120	3198	1303	1679	0	3556	-981	4.02	4.02	4.02	4.02	3	0.95	0.05	0.27	0.00	0.00	22.3

apost= 2.01 aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	180	1274	833	984	0	1359	883	4.02	4.02	4.02	4.02	3	0.35	0.03	0.16	0.00	0.00	22.3
2	180	1200	622	818	0	1136	681	4.02	4.02	4.02	4.02	2	0.33	0.03	0.13	0.00	0.00	22.3
3	180	930	686	859	0	1224	614	4.02	4.02	4.02	4.02	2	0.35	0.03	0.14	0.00	0.00	22.3
4	180	1030	594	655	0	867	744	4.02	4.02	4.02	4.02	2	0.25	0.02	0.11	0.00	0.00	22.3
5	180	760	659	696	0	955	678	4.02	4.02	4.02	4.02	2	0.27	0.02	0.12	0.00	0.00	22.3
6	180	1455	537	713	0	939	781	4.02	4.02	4.02	4.02	2	0.27	0.02	0.11	0.00	0.00	22.3
7	180	556	752	850	0	1232	559	4.02	4.02	4.02	4.02	2	0.35	0.03	0.14	0.00	0.00	22.3
8	180	1404	529	664	0	859	800	4.02	4.02	4.02	4.02	2	0.25	0.02	0.11	0.00	0.00	22.3
9	180	504	744	801	0	1151	578	4.02	4.02	4.02	4.02	2	0.32	0.03	0.13	0.00	0.00	22.3
10	180	1200	622	818	0	1136	681	4.02	4.02	4.02	4.02	2	0.33	0.03	0.13	0.00	0.00	22.3
11	180	930	686	859	0	1224	614	4.02	4.02	4.02	4.02	2	0.35	0.03	0.14	0.00	0.00	22.3
12	180	1030	594	655	0	867	744	4.02	4.02	4.02	4.02	2	0.25	0.02	0.11	0.00	0.00	22.3
13	180	760	659	696	0	955	678	4.02	4.02	4.02	4.02	2	0.27	0.02	0.12	0.00	0.00	22.3
14	180	1455	537	713	0	939	781	4.02	4.02	4.02	4.02	2	0.27	0.02	0.11	0.00	0.00	22.3
15	180	556	752	850	0	1232	559	4.02	4.02	4.02	4.02	2	0.35	0.03	0.14	0.00	0.00	22.3
16	180	1404	529	664	0	859	800	4.02	4.02	4.02	4.02	2	0.25	0.02	0.11	0.00	0.00	22.3
17	180	504	744	801	0	1151	578	4.02	4.02	4.02	4.02	2	0.32	0.03	0.13	0.00	0.00	22.3
18	180	3300	954	2274	0	3209	640	4.02	4.02	4.02	4.02	3	0.86	0.07	0.37	0.00	0.00	22.3
19	180	2815	837	1572	0	2115	936	4.02	4.02	4.02	4.02	3	0.56	0.05	0.25	0.00	0.00	22.3
20	180	3493	915	1961	0	2850	777	4.02	4.02	4.02	4.02	3	0.77	0.06	0.32	0.00	0.00	22.3
37	180	2876	973	2201	0	3148	573	4.02	4.02	4.02	4.02	3	0.84	0.07	0.35	0.00	0.00	22.3
38	180	2068	778	1031	0	1325	1064	4.02	4.02	4.02	4.02	3	0.34	0.03	0.17	0.00	0.00	22.3
39	180	3198	908	1679	0	2548	801	4.02	4.02	4.02	4.02	3	0.68	0.05	0.27	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	240	1274	437	984	0	768	986	4.02	4.02	4.02	4.02	3	0.20	0.03	0.16	0.00	0.00	22.3
2	240	1200	318	818	0	645	748	4.02	4.02	4.02	4.02	2	0.19	0.03	0.13	0.00	0.00	22.3
3	240	930	382	859	0	708	726	4.02	4.02	4.02	4.02	2	0.20	0.03	0.14	0.00	0.00	22.3
4	240	1030	290	655	0	474	792	4.02	4.02	4.02	4.02	2	0.14	0.02	0.11	0.00	0.00	22.3
5	240	760	355	696	0	537	771	4.02	4.02	4.02	4.02	2	0.15	0.02	0.11	0.00	0.00	22.3
6	240	1455	233	713	0	511	789	4.02	4.02	4.02	4.02	2	0.15	0.02	0.11	0.00	0.00	22.3
7	240	556	448	850	0	722	716	4.02	4.02	4.02	4.02	2	0.20	0.03	0.14	0.00	0.00	22.3
8	240	1404	225	664	0	460	802	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
9	240	504	440	801	0	670	730	4.02	4.02	4.02	4.02	2	0.19	0.03	0.13	0.00	0.00	22.3
10	240	1200	318	818	0	645	748	4.02	4.02	4.02	4.02	2	0.19	0.03	0.13	0.00	0.00	22.3
11	240	930	382	859	0	708	726	4.02	4.02	4.02	4.02	2	0.20	0.03	0.14	0.00	0.00	22.3
12	240	1030	290	655	0	474	792	4.02	4.02	4.02	4.02	2	0.14	0.02	0.11	0.00	0.00	22.3
13	240	760	355	696	0	537	771	4.02	4.02	4.02	4.02	2	0.15	0.02	0.11	0.00	0.00	22.3
14	240	1455	233	713	0	511	789	4.02	4.02	4.02	4.02	2	0.15	0.02	0.11	0.00	0.00	22.3
15	240	556	448	850	0	722	716	4.02	4.02	4.02	4.02	2	0.20	0.03	0.14	0.00	0.00	22.3
16	240	1404	225	664	0	460	802	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
17	240	504	440	801	0	670	730	4.02	4.02	4.02	4.02	2	0.19	0.03	0.13	0.00	0.00	22.3
18	240	3300	558	2274	0	1844	827	4.02	4.02	4.02	4.02	3	0.50	0.07	0.37	0.00	0.00	22.3
19	240	2815	441	1572	0	1171	1041	4.02	4.02	4.02	4.02	3	0.31	0.05	0.25	0.00	0.00	22.3
20	240	3493	519	1961	0	1673	937	4.02	4.02	4.02	4.02	3	0.45	0.06	0.32	0.00	0.00	22.3
37	240	2876	577	2201	0	1827	773	4.02	4.02	4.02	4.02	3	0.49	0.07	0.35	0.00	0.00	22.3
38	240	2068	382	1031	0	706	1129	4.02	4.02	4.02	4.02	3	0.18	0.03	0.17	0.00	0.00	22.3
39	240	3198	512	1679	0	1541	956	4.02	4.02	4.02	4.02	3	0.41	0.05	0.27	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	300	1274	42	984	0	178	986	4.02	4.02	4.02	4.02	3	0.15	0.03	0.16	0.00	0.00	22.3
2	300	1200	14	818	0	155	748	4.02	4.02	4.02	4.02	2	0.12	0.03	0.13	0.00	0.00	22.3
3	300	930	78	859	0	193	726	4.02	4.02	4.02	4.02	2	0.11	0.03	0.14	0.00	0.00	22.3
4	300	1030	-14	655	0	81	792	4.02	4.02	4.02	4.02	2	0.12	0.02	0.11	0.00	0.00	22.3
5	300	760	51	696	0	120	771	4.02	4.02	4.02	4.02	2	0.12	0.02	0.11	0.00	0.00	22.3
6	300	1455	-71	713	0	84	789	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
7	300	556	144	850	0	212	716	4.02	4.02	4.02	4.02	2	0.11	0.03	0.14	0.00	0.00	22.3
8	300	1404	-79	664	0	62	802	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
9	300	504	136	801	0	190	730	4.02	4.02	4.02	4.02	2	0.11	0.03	0.13	0.00	0.00	22.3
10	300	1200	14	818	0	155	748	4.02	4.02	4.02	4.02	2	0.12	0.03	0.13	0.00	0.00	22.3
11	300	930	78	859	0	193	726	4.02	4.02	4.02	4.02	2	0.11	0.03	0.14	0.00	0.00	22.3
12	300	1030	-14	655	0	81	792	4.02	4.02	4.02	4.02	2	0.12	0.02	0.11	0.00	0.00	22.3
13	300	760	51	696	0	120	771	4.02	4.02	4.02	4.02	2	0.12	0.02	0.11	0.00	0.00	22.3
14	300	1455	-71	713	0	84	789	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
15	300	556	144	850	0	212	716	4.02	4.02	4.02	4.02	2	0.11	0.03	0.14	0.00	0.00	22.3
16	300	1404	-79	664	0	62	802	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
17	300	504	136	801	0	190	730	4.02	4.02	4.02	4.02	2	0.11	0.03	0.13	0.00	0.00	22.3
18	300	3300	162	2274	0	479	827	4.02	4.02	4.02	4.02	3	0.13	0.07	0.37	0.00	0.00	22.3
19	300	2815	46	1572	0	228	1041	4.02	4.02	4.02	4.02	3	0.16	0.05	0.25	0.00	0.00	22.3
20	300	3493	124	1961	0	496	937	4.02	4.02	4.02	4.02	3	0.15	0.06	0.32	0.00	0.00	22.3
37	300	2876	182	2201	0	506	773	4.02	4.02	4.02	4.02	3	0.13	0.07	0.35	0.00	0.00	22.3
38	300	2068	-13	1031	0	87	1129	4.02	4.02	4.02	4.02	3	0.17	0.03	0.17	0.00	0.00	22.3
39	300	3198	116	1679	0	534	956	4.02	4.02	4.02	4.02	3	0.15	0.05	0.27	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	360	1274	-353	984	0	-412	986	4.02	4.02	4.02	4.02	3	0.15	0.03	0.16	0.00	0.00	22.3
2	360	1200	-290	818	0	-336	748	4.02	4.02	4.02	4.02	2	0.12	0.03	0.13	0.00	0.00	22.3
3	360	930	-226	859	0	-323	726	4.02	4.02	4.02	4.02	2	0.11	0.03	0.14	0.00	0.00	22.3
4	360	1030	-318	655	0	-312	792	4.02	4.02	4.02	4.02	2	0.12	0.02	0.11	0.00	0.00	22.3
5	360	760	-253	696	0	-298	771	4.02	4.02	4.02	4.02	2	0.12	0.02	0.11	0.00	0.00	22.3
6	360	1455	-375	713	0	-344	789	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
7	360	556	-160	850	0	-298	716	4.02	4.02	4.02	4.02	2	0.11	0.03	0.14	0.00	0.00	22.3
8	360	1404	-383	664	0	-337	802	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3

9	360	504	-168	801	0	-290	730	4.02	4.02	4.02	4.02	2	0.11	0.03	0.13	0.00	0.00	22.3
10	360	1200	-290	818	0	-336	748	4.02	4.02	4.02	4.02	2	0.12	0.03	0.13	0.00	0.00	22.3
11	360	930	-226	859	0	-323	726	4.02	4.02	4.02	4.02	2	0.11	0.03	0.14	0.00	0.00	22.3
12	360	1030	-318	655	0	-312	792	4.02	4.02	4.02	4.02	2	0.12	0.02	0.11	0.00	0.00	22.3
13	360	760	-253	696	0	-298	771	4.02	4.02	4.02	4.02	2	0.12	0.02	0.11	0.00	0.00	22.3
14	360	1455	-375	713	0	-344	789	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
15	360	556	-160	850	0	-298	716	4.02	4.02	4.02	4.02	2	0.11	0.03	0.14	0.00	0.00	22.3
16	360	1404	-383	664	0	-337	802	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
17	360	504	-168	801	0	-290	730	4.02	4.02	4.02	4.02	2	0.11	0.03	0.13	0.00	0.00	22.3
18	360	3300	-233	2274	0	-885	827	4.02	4.02	4.02	4.02	3	0.24	0.07	0.37	0.00	0.00	22.3
19	360	2815	-350	1572	0	-715	1041	4.02	4.02	4.02	4.02	3	0.19	0.05	0.25	0.00	0.00	22.3
20	360	3493	-272	1961	0	-680	937	4.02	4.02	4.02	4.02	3	0.18	0.06	0.32	0.00	0.00	22.3
37	360	2876	-214	2201	0	-815	773	4.02	4.02	4.02	4.02	3	0.22	0.07	0.35	0.00	0.00	22.3
38	360	2068	-408	1031	0	-532	1129	4.02	4.02	4.02	4.02	3	0.17	0.03	0.17	0.00	0.00	22.3
39	360	3198	-279	1679	0	-473	956	4.02	4.02	4.02	4.02	3	0.15	0.05	0.27	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	420	1274	-749	984	0	-1003	942	4.02	4.02	4.02	4.02	3	0.26	0.03	0.16	0.00	0.00	22.3
2	420	1200	-594	818	0	-827	700	4.02	4.02	4.02	4.02	2	0.24	0.03	0.13	0.00	0.00	22.3
3	420	930	-530	859	0	-838	723	4.02	4.02	4.02	4.02	2	0.24	0.03	0.14	0.00	0.00	22.3
4	420	1030	-622	655	0	-705	726	4.02	4.02	4.02	4.02	2	0.20	0.02	0.11	0.00	0.00	22.3
5	420	760	-557	696	0	-716	749	4.02	4.02	4.02	4.02	2	0.20	0.02	0.11	0.00	0.00	22.3
6	420	1455	-679	713	0	-772	682	4.02	4.02	4.02	4.02	2	0.22	0.02	0.12	0.00	0.00	22.3
7	420	556	-464	850	0	-808	716	4.02	4.02	4.02	4.02	2	0.23	0.03	0.14	0.00	0.00	22.3
8	420	1404	-687	664	0	-735	690	4.02	4.02	4.02	4.02	2	0.21	0.02	0.12	0.00	0.00	22.3
9	420	504	-472	801	0	-771	730	4.02	4.02	4.02	4.02	2	0.22	0.03	0.13	0.00	0.00	22.3
10	420	1200	-594	818	0	-827	700	4.02	4.02	4.02	4.02	2	0.24	0.03	0.13	0.00	0.00	22.3
11	420	930	-530	859	0	-838	723	4.02	4.02	4.02	4.02	2	0.24	0.03	0.14	0.00	0.00	22.3
12	420	1030	-622	655	0	-705	726	4.02	4.02	4.02	4.02	2	0.20	0.02	0.11	0.00	0.00	22.3
13	420	760	-557	696	0	-716	749	4.02	4.02	4.02	4.02	2	0.20	0.02	0.11	0.00	0.00	22.3
14	420	1455	-679	713	0	-772	682	4.02	4.02	4.02	4.02	2	0.22	0.02	0.12	0.00	0.00	22.3
15	420	556	-464	850	0	-808	716	4.02	4.02	4.02	4.02	2	0.23	0.03	0.14	0.00	0.00	22.3
16	420	1404	-687	664	0	-735	690	4.02	4.02	4.02	4.02	2	0.21	0.02	0.12	0.00	0.00	22.3
17	420	504	-472	801	0	-771	730	4.02	4.02	4.02	4.02	2	0.22	0.03	0.13	0.00	0.00	22.3
18	420	3300	-628	2274	0	-2250	827	4.02	4.02	4.02	4.02	3	0.61	0.07	0.37	0.00	0.00	22.3
19	420	2815	-745	1572	0	-1659	999	4.02	4.02	4.02	4.02	3	0.44	0.05	0.25	0.00	0.00	22.3
20	420	3493	-667	1961	0	-1857	937	4.02	4.02	4.02	4.02	3	0.50	0.06	0.32	0.00	0.00	22.3
37	420	2876	-609	2201	0	-2136	773	4.02	4.02	4.02	4.02	3	0.57	0.07	0.35	0.00	0.00	22.3
38	420	2068	-804	1031	0	-1151	1046	4.02	4.02	4.02	4.02	3	0.30	0.03	0.17	0.00	0.00	22.3
39	420	3198	-674	1679	0	-1480	956	4.02	4.02	4.02	4.02	3	0.40	0.05	0.27	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	480	1274	-1144	984	0	-1593	-585	4.02	4.02	4.02	4.02	3	0.41	0.03	0.20	0.00	0.00	22.3
2	480	1200	-899	818	0	-1318	-504	4.02	4.02	4.02	4.02	2	0.38	0.03	0.16	0.00	0.00	22.3
3	480	930	-835	859	0	-1354	468	4.02	4.02	4.02	4.02	2	0.38	0.03	0.15	0.00	0.00	22.3
4	480	1030	-927	655	0	-1097	-523	4.02	4.02	4.02	4.02	2	0.31	0.03	0.17	0.00	0.00	22.3
5	480	760	-862	696	0	-1133	477	4.02	4.02	4.02	4.02	2	0.32	0.02	0.15	0.00	0.00	22.3
6	480	1455	-984	713	0	-1200	-659	4.02	4.02	4.02	4.02	2	0.35	0.03	0.18	0.00	0.00	22.3
7	480	556	-769	850	0	-1317	543	4.02	4.02	4.02	4.02	2	0.37	0.03	0.14	0.00	0.00	22.3
8	480	1404	-992	664	0	-1134	-664	4.02	4.02	4.02	4.02	2	0.33	0.03	0.18	0.00	0.00	22.3
9	480	504	-777	801	0	-1251	546	4.02	4.02	4.02	4.02	2	0.35	0.03	0.14	0.00	0.00	22.3
10	480	1200	-899	818	0	-1318	-504	4.02	4.02	4.02	4.02	2	0.38	0.03	0.16	0.00	0.00	22.3
11	480	930	-835	859	0	-1354	468	4.02	4.02	4.02	4.02	2	0.38	0.03	0.15	0.00	0.00	22.3
12	480	1030	-927	655	0	-1097	-523	4.02	4.02	4.02	4.02	2	0.31	0.03	0.17	0.00	0.00	22.3
13	480	760	-862	696	0	-1133	477	4.02	4.02	4.02	4.02	2	0.32	0.02	0.15	0.00	0.00	22.3
14	480	1455	-984	713	0	-1200	-659	4.02	4.02	4.02	4.02	2	0.35	0.03	0.18	0.00	0.00	22.3
15	480	556	-769	850	0	-1317	543	4.02	4.02	4.02	4.02	2	0.37	0.03	0.14	0.00	0.00	22.3
16	480	1404	-992	664	0	-1134	-664	4.02	4.02	4.02	4.02	2	0.33	0.03	0.18	0.00	0.00	22.3
17	480	504	-777	801	0	-1251	546	4.02	4.02	4.02	4.02	2	0.35	0.03	0.14	0.00	0.00	22.3
18	480	3300	-1024	2274	0	-3615	570	4.02	4.02	4.02	4.02	3	0.97	0.07	0.37	0.00	0.00	22.3
19	480	2815	-1141	1572	0	-2602	633	4.02	4.02	4.02	4.02	3	0.69	0.05	0.25	0.00	0.00	22.3
20	480	3493	-1063	1961	0	-3033	629	4.02	4.02	4.02	4.02	3	0.82	0.06	0.32	0.00	0.00	22.3
37	480	2876	-1005	2201	0	-3456	541	4.02	4.02	4.02	4.02	3	0.92	0.07	0.35	0.00	0.00	22.3
38	480	2068	-1199	1031	0	-1769	645	4.02	4.02	4.02	4.02	3	0.46	0.03	0.21	0.00	0.00	22.3
39	480	3198	-1070	1679	0	-2488	640	4.02	4.02	4.02	4.02	3	0.67	0.05	0.27	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	540	1274	-1540	984	0	-2184	-1590	4.02	4.02	4.02	4.02	3	0.56	0.04	0.27	0.00	0.00	22.3
2	540	1200	-1203	818	0	-1809	-1289	4.02	4.02	4.02	4.02	2	0.52	0.03	0.21	0.00	0.00	22.3
3	540	930	-1139	859	0	-1870	-1123	4.02	4.02	4.02	4.02	2	0.53	0.03	0.20	0.00	0.00	22.3
4	540	1030	-1231	655	0	-1490	-1324	4.02	4.02	4.02	4.02	2	0.43	0.04	0.22	0.00	0.00	22.3
5	540	760	-1166	696	0	-1550	-1157	4.02	4.02	4.02	4.02	2	0.44	0.03	0.21	0.00	0.00	22.3
6	540	1455	-1288	713	0	-1628	-1495	4.02	4.02	4.02	4.02	2	0.47	0.04	0.23	0.00	0.00	22.3
7	540	556	-1073	850	0	-1827	-941	4.02	4.02	4.02	4.02	2	0.51	0.03	0.19	0.00	0.00	22.3
8	540	1404	-1296	664	0	-1532	-1505	4.02	4.02	4.02	4.02	2	0.44	0.04	0.23	0.00	0.00	22.3
9	540	504	-1081	801	0	-1732	-951	4.02	4.02	4.02	4.02	2	0.49	0.03	0.19	0.00	0.00	22.3
10	540	1200	-1203	818	0	-1809	-1289	4.02	4.02	4.02	4.02	2	0.52	0.03	0.21	0.00	0.00	22.3
11	540	930	-1139	859	0	-1870	-1123	4.02	4.02	4.02	4.02	2	0.53	0.03	0.20	0.00	0.00	22.3
12	540	1030	-1231	655	0	-1490	-1324	4.02	4.02	4.02	4.02	2	0.43	0.04	0.22	0.00	0.00	22.3
13	540	760	-1166	696	0	-1550	-1157	4.02	4.02	4.02	4.02	2	0.44	0.03	0.21	0.00	0.00	22.3
14	540	1455	-1288	713	0	-1628	-1495	4.02	4.02	4.02	4.02	2	0.47	0.04	0.23	0.00	0.00	22.3
15	540	556	-1073	850	0	-1827	-941	4.02	4.02	4.02	4.02	2	0.51	0.03	0.19	0.00	0.00	22.3
16	540	1404	-1296	664	0	-1532	-1505	4.02	4.02	4.02	4.02	2	0.44	0.04	0.23	0.00	0.00	22.3
17	540	504	-1081	801	0	-1732	-951	4.02	4.02	4.02	4.02	2	0.49	0.03	0.19	0.00	0.00	22.3
18	540	3300	-1419	2274	0	-4979	-1400	4.02	6.03	4.02	4.02	3	0.93	0.07	0.37	0.00	0.00	22.3
19	540	2815	-1536	1572	0	-3546	-1525	4.02	4.02	4.02	4.02	3	0.94	0.05	0.27	0.00	0.00	22.3
20	540	3493	-1458	1961	0	-4210	-1404	4.02	6.03	4.02	4.02	3	0.79	0.06	0.32	0.00	0.00	22.3
37	540	2876	-1400	2201	0	-4777	-1398	4.02	6.03	4.02	4.02	3	0.88	0.07	0.35	0.00	0.00	22.3
38	540	2068	-1595	1031	0	-2388	-1608	4.02	4.02	4.02	4.02	3	0.62	0.05	0.28	0.00	0.00	22.3
39	540	3198	-1465	1679	0	-3495	-1404	4.02	4.02	4.02	4.02	3	0.94	0.05	0.27	0.00	0.00	22.3

apost= -- aant= 2.01 ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	600	1274	-1935	984	0	-2774	-1853	4.02	4.02	4.02	4.02	3	0.71	0.06	0.34	0.00	0.00	22.3
2	600	1200	-1507	818	0	-2300	-1493	4.02	4.02	4.02	4.02	2	0.66	0.04	0.27	0.00	0.00	22.3
3	600	930	-1443	859	0	-2385	-1321	4.02	4.02	4.02	4.02	2	0.68	0.04	0.26	0.00	0.00	22.3
4	600	1030	-1535	655	0	-1883	-1530	4.02	4.02	4.02	4.02	2	0.54	0.04	0.27	0.00	0.00	22.3
5	600	760	-1470	696	0	-1968	-1358	4.02	4.02	4.02	4.02	2	0.56	0.04	0.26	0.00	0.00	22.3
6	600	1455	-1592	713	0	-2056	-1707	4.02	4.02	4.02	4.02	2	0.59	0.05	0.28	0.00	0.00	22.3
7	600	556	-1377	850	0	-2337	-1133	4.02	4.02	4.02	4.02	2	0.66	0.04	0.25	0.00	0.00	22.3
8	600	1404	-1600	664	0	-1931	-1718	4.02	4.02	4.02	4.02	2	0.56	0.05	0.28	0.00	0.00	22.3
9	600	504	-1385	801	0	-2212	-1144	4.02	4.02	4.02	4.02	2	0.62	0.04	0.25	0.00	0.00	22.3
10	600	1200	-1507	818	0	-2300	-1493	4.02	4.02	4.02	4.02	2	0.66	0.04	0.27	0.00	0.00	22.3
11	600	930	-1443	859	0	-2385	-1321	4.02	4.02	4.02	4.02	2	0.68	0.04	0.26	0.00	0.00	22.3
12	600	1030	-1535	655	0	-1883	-1530	4.02	4.02	4.02	4.02	2	0.54	0.04	0.27	0.00	0.00	22.3
13	600	760	-1470	696	0	-1968	-1358	4.02	4.02	4.02	4.02	2	0.56	0.04	0.26	0.00	0.00	22.3
14	600	1455	-1592	713	0	-2056	-1707	4.02	4.02	4.02	4.02	2	0.59	0.05	0.28	0.00	0.00	22.3

15	600	556	-1377	850	0	-2337	-1133	4.02	4.02	4.02	4.02	2	0.66	0.04	0.25	0.00	0.00	22.3
16	600	1404	-1600	664	0	-1931	-1718	4.02	4.02	4.02	4.02	2	0.56	0.05	0.28	0.00	0.00	22.3
17	600	504	-1385	801	0	-2212	-1144	4.02	4.02	4.02	4.02	2	0.62	0.04	0.25	0.00	0.00	22.3
18	600	3300	-1815	2274	0	-6344	-1652	4.02	8.04	4.02	4.02	3	0.90	0.07	0.37	0.00	0.00	22.3
19	600	2815	-1932	1572	0	-4489	-1788	4.02	6.03	4.02	4.02	3	0.83	0.06	0.34	0.00	0.00	22.3
20	600	3493	-1854	1961	0	-5386	-1659	4.02	8.04	4.02	4.02	3	0.77	0.06	0.33	0.00	0.00	22.3
37	600	2876	-1796	2201	0	-6098	-1648	4.02	8.04	4.02	4.02	3	0.86	0.07	0.35	0.00	0.00	22.3
38	600	2068	-1990	1031	0	-3007	-1876	4.02	4.02	4.02	4.02	3	0.78	0.06	0.35	0.00	0.00	22.3
39	600	3198	-1861	1679	0	-4502	-1660	4.02	6.03	4.02	4.02	3	0.84	0.05	0.33	0.00	0.00	22.3

apost= -- aant= 4.02 ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

Nome travata: **Trave_404_IP1** Descrizione: **Trave_4 32-25**
ASTA NUM. 16 NI 254 NF 255 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y Permanente qy tot.
qy medio: 375.00 132.00 507.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	1757	1974	744	0	2026	-1953	4.02	4.02	4.02	4.02	3	0.52	0.06	0.35	0.00	0.00	22.3
2	0	1523	1498	661	0	1801	-1438	4.02	4.02	4.02	4.02	2	0.52	0.04	0.27	0.00	0.00	22.3
3	0	1247	1553	698	0	1914	-1599	4.02	4.02	4.02	4.02	2	0.55	0.05	0.28	0.00	0.00	22.3
4	0	1456	1484	448	0	1202	-1405	4.02	4.02	4.02	4.02	2	0.35	0.04	0.26	0.00	0.00	22.3
5	0	1180	1539	485	0	1316	-1566	4.02	4.02	4.02	4.02	2	0.38	0.04	0.27	0.00	0.00	22.3
6	0	1820	1429	542	0	1458	-1239	4.02	4.02	4.02	4.02	2	0.43	0.04	0.25	0.00	0.00	22.3
7	0	903	1612	667	0	1838	-1775	4.02	4.02	4.02	4.02	2	0.52	0.05	0.29	0.00	0.00	22.3
8	0	1800	1425	478	0	1279	-1229	4.02	4.02	4.02	4.02	2	0.37	0.04	0.25	0.00	0.00	22.3
9	0	882	1608	603	0	1658	-1765	4.02	4.02	4.02	4.02	2	0.47	0.05	0.29	0.00	0.00	22.3
10	0	1523	1498	661	0	1801	-1438	4.02	4.02	4.02	4.02	2	0.52	0.04	0.27	0.00	0.00	22.3
11	0	1247	1553	698	0	1914	-1599	4.02	4.02	4.02	4.02	2	0.55	0.05	0.28	0.00	0.00	22.3
12	0	1456	1484	448	0	1202	-1405	4.02	4.02	4.02	4.02	2	0.35	0.04	0.26	0.00	0.00	22.3
13	0	1180	1539	485	0	1316	-1566	4.02	4.02	4.02	4.02	2	0.38	0.04	0.27	0.00	0.00	22.3
14	0	1820	1429	542	0	1458	-1239	4.02	4.02	4.02	4.02	2	0.43	0.04	0.25	0.00	0.00	22.3
15	0	903	1612	667	0	1838	-1775	4.02	4.02	4.02	4.02	2	0.52	0.05	0.29	0.00	0.00	22.3
16	0	1800	1425	478	0	1279	-1229	4.02	4.02	4.02	4.02	2	0.37	0.04	0.25	0.00	0.00	22.3
17	0	882	1608	603	0	1658	-1765	4.02	4.02	4.02	4.02	2	0.47	0.05	0.29	0.00	0.00	22.3
18	0	4056	2002	1831	0	5001	-2015	6.03	4.02	4.02	4.02	3	0.94	0.06	0.36	0.00	0.00	22.3
19	0	3576	1944	1026	0	2775	-1860	4.02	4.02	4.02	4.02	3	0.75	0.06	0.35	0.00	0.00	22.3
20	0	3774	2052	1395	0	3806	-2164	6.03	4.02	4.02	4.02	3	0.71	0.06	0.37	0.00	0.00	22.3
37	0	3542	2022	1877	0	5137	-2072	6.03	4.02	4.02	4.02	3	0.96	0.06	0.36	0.00	0.00	22.3
38	0	2740	1926	535	0	1428	-1815	4.02	4.02	4.02	4.02	3	0.38	0.06	0.34	0.00	0.00	22.3
39	0	3070	2106	1151	0	3147	-2322	4.02	4.02	4.02	4.02	3	0.84	0.06	0.38	0.00	0.00	22.3

apost= 2.01 aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	60	1757	1578	744	0	1579	-1686	4.02	4.02	4.02	4.02	3	0.41	0.05	0.28	0.00	0.00	22.3
2	60	1523	1194	661	0	1405	-1235	4.02	4.02	4.02	4.02	2	0.41	0.03	0.21	0.00	0.00	22.3
3	60	1247	1249	698	0	1495	-1391	4.02	4.02	4.02	4.02	2	0.43	0.04	0.22	0.00	0.00	22.3
4	60	1456	1180	448	0	934	-1203	4.02	4.02	4.02	4.02	2	0.27	0.03	0.21	0.00	0.00	22.3
5	60	1180	1235	485	0	1025	-1359	4.02	4.02	4.02	4.02	2	0.29	0.04	0.22	0.00	0.00	22.3
6	60	1820	1125	542	0	1133	-1042	4.02	4.02	4.02	4.02	2	0.33	0.03	0.20	0.00	0.00	22.3
7	60	903	1308	667	0	1438	-1561	4.02	4.02	4.02	4.02	2	0.41	0.04	0.23	0.00	0.00	22.3
8	60	1800	1121	478	0	992	-1033	4.02	4.02	4.02	4.02	2	0.29	0.03	0.20	0.00	0.00	22.3
9	60	882	1304	603	0	1296	-1552	4.02	4.02	4.02	4.02	2	0.37	0.04	0.23	0.00	0.00	22.3
10	60	1523	1194	661	0	1405	-1235	4.02	4.02	4.02	4.02	2	0.41	0.03	0.21	0.00	0.00	22.3
11	60	1247	1249	698	0	1495	-1391	4.02	4.02	4.02	4.02	2	0.43	0.04	0.22	0.00	0.00	22.3
12	60	1456	1180	448	0	934	-1203	4.02	4.02	4.02	4.02	2	0.27	0.03	0.21	0.00	0.00	22.3
13	60	1180	1235	485	0	1025	-1359	4.02	4.02	4.02	4.02	2	0.29	0.04	0.22	0.00	0.00	22.3
14	60	1820	1125	542	0	1133	-1042	4.02	4.02	4.02	4.02	2	0.33	0.03	0.20	0.00	0.00	22.3
15	60	903	1308	667	0	1438	-1561	4.02	4.02	4.02	4.02	2	0.41	0.04	0.23	0.00	0.00	22.3
16	60	1800	1121	478	0	992	-1033	4.02	4.02	4.02	4.02	2	0.29	0.03	0.20	0.00	0.00	22.3
17	60	882	1304	603	0	1296	-1552	4.02	4.02	4.02	4.02	2	0.37	0.04	0.23	0.00	0.00	22.3
18	60	4056	1606	1831	0	3902	-1746	6.03	4.02	4.02	4.02	3	0.74	0.06	0.29	0.00	0.00	22.3
19	60	3576	1549	1026	0	2159	-1596	4.02	4.02	4.02	4.02	3	0.59	0.04	0.28	0.00	0.00	22.3
20	60	3774	1657	1395	0	2969	-1890	4.02	4.02	4.02	4.02	3	0.81	0.05	0.30	0.00	0.00	22.3
37	60	3542	1626	1877	0	4011	-1801	6.03	4.02	4.02	4.02	3	0.75	0.06	0.30	0.00	0.00	22.3
38	60	2740	1530	535	0	1107	-1553	4.02	4.02	4.02	4.02	3	0.29	0.04	0.27	0.00	0.00	22.3
39	60	3070	1710	1151	0	2457	-2043	4.02	4.02	4.02	4.02	3	0.66	0.05	0.30	0.00	0.00	22.3

apost= 2.01 aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	120	1757	1183	744	0	1133	-657	4.02	4.02	4.02	4.02	3	0.29	0.03	0.21	0.00	0.00	22.3
2	120	1523	890	661	0	1008	-456	4.02	4.02	4.02	4.02	2	0.29	0.03	0.16	0.00	0.00	22.3
3	120	1247	945	698	0	1077	-579	4.02	4.02	4.02	4.02	2	0.31	0.03	0.17	0.00	0.00	22.3
4	120	1456	876	448	0	665	454	4.02	4.02	4.02	4.02	2	0.19	0.03	0.16	0.00	0.00	22.3
5	120	1180	931	485	0	734	-555	4.02	4.02	4.02	4.02	2	0.21	0.03	0.17	0.00	0.00	22.3
6	120	1820	821	542	0	807	526	4.02	4.02	4.02	4.02	2	0.24	0.02	0.15	0.00	0.00	22.3
7	120	903	1004	667	0	1038	-714	4.02	4.02	4.02	4.02	2	0.29	0.03	0.18	0.00	0.00	22.3
8	120	1800	817	478	0	705	529	4.02	4.02	4.02	4.02	2	0.21	0.02	0.15	0.00	0.00	22.3
9	120	882	1000	603	0	935	-707	4.02	4.02	4.02	4.02	2	0.27	0.03	0.18	0.00	0.00	22.3
10	120	1523	890	661	0	1008	-456	4.02	4.02	4.02	4.02	2	0.29	0.03	0.16	0.00	0.00	22.3
11	120	1247	945	698	0	1077	-579	4.02	4.02	4.02	4.02	2	0.31	0.03	0.17	0.00	0.00	22.3
12	120	1456	876	448	0	665	454	4.02	4.02	4.02	4.02	2	0.19	0.03	0.16	0.00	0.00	22.3
13	120	1180	931	485	0	734	-555	4.02	4.02	4.02	4.02	2	0.21	0.03	0.17	0.00	0.00	22.3
14	120	1820	821	542	0	807	526	4.02	4.02	4.02	4.02	2	0.24	0.02	0.15	0.00	0.00	22.3
15	120	903	1004	667	0	1038	-714	4.02	4.02	4.02	4.02	2	0.29	0.03	0.18	0.00	0.00	22.3
16	120	1800	817	478	0	705	529	4.02	4.02	4.02	4.02	2	0.21	0.02	0.15	0.00	0.00	22.3
17	120	882	1000	603	0	935	-707	4.02	4.02	4.02	4.02	2	0.27	0.03	0.18	0.00	0.00	22.3
18	120	4056	1211	1831	0	2803	-700	4.02	4.02	4.02	4.02	3	0.77	0.06	0.29	0.00	0.00	22.3
19	120	3576	1153	1026	0	1544	-585	4.02	4.02	4.02	4.02	3	0.42	0.03	0.21	0.00	0.00	22.3
20	120	3774	1261	1395	0	2132	-814	4.02	4.02	4.02	4.02	3	0.58	0.04	0.22	0.00	0.00	22.3
37	120	3542	1231	1877	0	2885	-744	4.02	4.02	4.02	4.02	3	0.78	0.06	0.30	0.00	0.00	22.3
38	120	2740	1135	535	0	786	596	4.02	4.02	4.02	4.02	3	0.21	0.03	0.20	0.00	0.00	22.3
39	120	3070	1315	1151	0	1766	-935	4.02	4.02	4.02	4.02	3	0.47	0.04	0.23	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	180	1757	788	744	0	686	931	4.02	4.02	4.02	4.02	3	0.18	0.02	0.14	0.00	0.00	22.3
2	180	1523	585	661	0	612	733	4.02	4.02	4.02	4.02	2	0.18	0.02	0.11	0.00	0.00	22.3
3	180	1247	640	698	0	658	699	4.02	4.02	4.02	4.02	2	0.19	0.02	0.11	0.00	0.00	22.3
4	180	1456	571	448	0	397	734	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
5	180	1180	626	485	0	443	700	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
6	180	1820	516	542	0	482	767	4.02	4.02	4.02	4.02	2	0.14	0.02	0.09	0.00	0.00	22.3

7	180	903	699	667	0	638	659	4.02	4.02	4.02	4.02	2	0.18	0.02	0.12	0.00	0.00	22.3
8	180	1800	512	478	0	418	765	4.02	4.02	4.02	4.02	2	0.12	0.01	0.09	0.00	0.00	22.3
9	180	882	695	603	0	573	660	4.02	4.02	4.02	4.02	2	0.16	0.02	0.12	0.00	0.00	22.3
10	180	1523	585	661	0	612	733	4.02	4.02	4.02	4.02	2	0.18	0.02	0.11	0.00	0.00	22.3
11	180	1247	640	698	0	658	699	4.02	4.02	4.02	4.02	2	0.19	0.02	0.11	0.00	0.00	22.3
12	180	1456	571	448	0	397	734	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
13	180	1180	626	485	0	443	700	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
14	180	1820	516	542	0	482	767	4.02	4.02	4.02	4.02	2	0.14	0.02	0.09	0.00	0.00	22.3
15	180	903	699	667	0	638	659	4.02	4.02	4.02	4.02	2	0.18	0.02	0.12	0.00	0.00	22.3
16	180	1800	512	478	0	418	765	4.02	4.02	4.02	4.02	2	0.12	0.01	0.09	0.00	0.00	22.3
17	180	882	695	603	0	573	660	4.02	4.02	4.02	4.02	2	0.16	0.02	0.12	0.00	0.00	22.3
18	180	4056	816	1831	0	1705	933	4.02	4.02	4.02	4.02	3	0.47	0.06	0.29	0.00	0.00	22.3
19	180	3576	758	1026	0	928	956	4.02	4.02	4.02	4.02	3	0.25	0.03	0.17	0.00	0.00	22.3
20	180	3774	866	1395	0	1294	900	4.02	4.02	4.02	4.02	3	0.35	0.04	0.22	0.00	0.00	22.3
37	180	3542	836	1877	0	1758	922	4.02	4.02	4.02	4.02	3	0.48	0.06	0.30	0.00	0.00	22.3
38	180	2740	740	535	0	464	958	4.02	4.02	4.02	4.02	3	0.15	0.02	0.13	0.00	0.00	22.3
39	180	3070	920	1151	0	1076	866	4.02	4.02	4.02	4.02	3	0.29	0.04	0.19	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	240	1757	392	744	0	239	1003	4.02	4.02	4.02	4.02	3	0.15	0.02	0.12	0.00	0.00	22.3
2	240	1523	281	661	0	215	774	4.02	4.02	4.02	4.02	2	0.12	0.02	0.11	0.00	0.00	22.3
3	240	1247	336	698	0	239	778	4.02	4.02	4.02	4.02	2	0.12	0.02	0.11	0.00	0.00	22.3
4	240	1456	267	448	0	128	766	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
5	240	1180	322	485	0	152	770	4.02	4.02	4.02	4.02	2	0.12	0.02	0.08	0.00	0.00	22.3
6	240	1820	212	542	0	156	767	4.02	4.02	4.02	4.02	2	0.12	0.02	0.09	0.00	0.00	22.3
7	240	903	395	667	0	238	779	4.02	4.02	4.02	4.02	2	0.12	0.02	0.11	0.00	0.00	22.3
8	240	1800	208	478	0	131	765	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
9	240	882	391	603	0	211	777	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
10	240	1523	281	661	0	215	774	4.02	4.02	4.02	4.02	2	0.12	0.02	0.11	0.00	0.00	22.3
11	240	1247	336	698	0	239	778	4.02	4.02	4.02	4.02	2	0.12	0.02	0.11	0.00	0.00	22.3
12	240	1456	267	448	0	128	766	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
13	240	1180	322	485	0	152	770	4.02	4.02	4.02	4.02	2	0.12	0.02	0.08	0.00	0.00	22.3
14	240	1820	212	542	0	156	767	4.02	4.02	4.02	4.02	2	0.12	0.02	0.09	0.00	0.00	22.3
15	240	903	395	667	0	238	779	4.02	4.02	4.02	4.02	2	0.12	0.02	0.11	0.00	0.00	22.3
16	240	1800	208	478	0	131	765	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
17	240	882	391	603	0	211	777	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
18	240	4056	420	1831	0	606	1024	4.02	4.02	4.02	4.02	3	0.17	0.06	0.29	0.00	0.00	22.3
19	240	3576	362	1026	0	312	1007	4.02	4.02	4.02	4.02	3	0.16	0.03	0.17	0.00	0.00	22.3
20	240	3774	470	1395	0	457	1026	4.02	4.02	4.02	4.02	3	0.17	0.04	0.22	0.00	0.00	22.3
37	240	3542	440	1877	0	632	1026	4.02	4.02	4.02	4.02	3	0.17	0.06	0.30	0.00	0.00	22.3
38	240	2740	344	535	0	143	997	4.02	4.02	4.02	4.02	3	0.16	0.02	0.09	0.00	0.00	22.3
39	240	3070	524	1151	0	385	1029	4.02	4.02	4.02	4.02	3	0.16	0.04	0.19	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	300	1757	-4	744	0	-207	1003	4.02	4.02	4.02	4.02	3	0.15	0.02	0.12	0.00	0.00	22.3
2	300	1523	-23	661	0	-181	774	4.02	4.02	4.02	4.02	2	0.12	0.02	0.11	0.00	0.00	22.3
3	300	1247	32	698	0	-179	778	4.02	4.02	4.02	4.02	2	0.12	0.02	0.11	0.00	0.00	22.3
4	300	1456	-37	448	0	-140	766	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
5	300	1180	18	485	0	-138	770	4.02	4.02	4.02	4.02	2	0.12	0.02	0.08	0.00	0.00	22.3
6	300	1820	-92	542	0	-169	767	4.02	4.02	4.02	4.02	2	0.12	0.02	0.09	0.00	0.00	22.3
7	300	903	91	667	0	-162	779	4.02	4.02	4.02	4.02	2	0.12	0.02	0.11	0.00	0.00	22.3
8	300	1800	-96	478	0	-156	765	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
9	300	882	87	603	0	-150	777	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
10	300	1523	-23	661	0	-181	774	4.02	4.02	4.02	4.02	2	0.12	0.02	0.11	0.00	0.00	22.3
11	300	1247	32	698	0	-179	778	4.02	4.02	4.02	4.02	2	0.12	0.02	0.11	0.00	0.00	22.3
12	300	1456	-37	448	0	-140	766	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
13	300	1180	18	485	0	-138	770	4.02	4.02	4.02	4.02	2	0.12	0.02	0.08	0.00	0.00	22.3
14	300	1820	-92	542	0	-169	767	4.02	4.02	4.02	4.02	2	0.12	0.02	0.09	0.00	0.00	22.3
15	300	903	91	667	0	-162	779	4.02	4.02	4.02	4.02	2	0.12	0.02	0.11	0.00	0.00	22.3
16	300	1800	-96	478	0	-156	765	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
17	300	882	87	603	0	-150	777	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
18	300	4056	24	1831	0	-493	1024	4.02	4.02	4.02	4.02	3	0.17	0.06	0.29	0.00	0.00	22.3
19	300	3576	-33	1026	0	-303	1007	4.02	4.02	4.02	4.02	3	0.16	0.03	0.17	0.00	0.00	22.3
20	300	3774	75	1395	0	-380	1026	4.02	4.02	4.02	4.02	3	0.17	0.04	0.22	0.00	0.00	22.3
37	300	3542	44	1877	0	-494	1026	4.02	4.02	4.02	4.02	3	0.16	0.06	0.30	0.00	0.00	22.3
38	300	2740	-52	535	0	-178	997	4.02	4.02	4.02	4.02	3	0.16	0.02	0.09	0.00	0.00	22.3
39	300	3070	128	1151	0	-305	1029	4.02	4.02	4.02	4.02	3	0.16	0.04	0.19	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	360	1757	-399	744	0	-654	1003	4.02	4.02	4.02	4.02	3	0.17	0.02	0.12	0.00	0.00	22.3
2	360	1523	-327	661	0	-577	774	4.02	4.02	4.02	4.02	2	0.17	0.02	0.11	0.00	0.00	22.3
3	360	1247	-272	698	0	-598	778	4.02	4.02	4.02	4.02	2	0.17	0.02	0.11	0.00	0.00	22.3
4	360	1456	-341	448	0	-408	766	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
5	360	1180	-286	485	0	-429	770	4.02	4.02	4.02	4.02	2	0.12	0.02	0.08	0.00	0.00	22.3
6	360	1820	-396	542	0	-494	767	4.02	4.02	4.02	4.02	2	0.14	0.02	0.09	0.00	0.00	22.3
7	360	903	-213	667	0	-563	779	4.02	4.02	4.02	4.02	2	0.16	0.02	0.11	0.00	0.00	22.3
8	360	1800	-400	478	0	-444	765	4.02	4.02	4.02	4.02	2	0.13	0.01	0.08	0.00	0.00	22.3
9	360	882	-217	603	0	-512	777	4.02	4.02	4.02	4.02	2	0.15	0.02	0.10	0.00	0.00	22.3
10	360	1523	-327	661	0	-577	774	4.02	4.02	4.02	4.02	2	0.17	0.02	0.11	0.00	0.00	22.3
11	360	1247	-272	698	0	-598	778	4.02	4.02	4.02	4.02	2	0.17	0.02	0.11	0.00	0.00	22.3
12	360	1456	-341	448	0	-408	766	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
13	360	1180	-286	485	0	-429	770	4.02	4.02	4.02	4.02	2	0.12	0.02	0.08	0.00	0.00	22.3
14	360	1820	-396	542	0	-494	767	4.02	4.02	4.02	4.02	2	0.14	0.02	0.09	0.00	0.00	22.3
15	360	903	-213	667	0	-563	779	4.02	4.02	4.02	4.02	2	0.16	0.02	0.11	0.00	0.00	22.3
16	360	1800	-400	478	0	-444	765	4.02	4.02	4.02	4.02	2	0.13	0.01	0.08	0.00	0.00	22.3
17	360	882	-217	603	0	-512	777	4.02	4.02	4.02	4.02	2	0.15	0.02	0.10	0.00	0.00	22.3
18	360	4056	-371	1831	0	-1592	1024	4.02	4.02	4.02	4.02	3	0.44	0.06	0.29	0.00	0.00	22.3
19	360	3576	-428	1026	0	-919	1007	4.02	4.02	4.02	4.02	3	0.25	0.03	0.17	0.00	0.00	22.3
20	360	3774	-320	1395	0	-1217	1026	4.02	4.02	4.02	4.02	3	0.33	0.04	0.22	0.00	0.00	22.3
37	360	3542	-351	1877	0	-1620	1026	4.02	4.02	4.02	4.02	3	0.44	0.06	0.30	0.00	0.00	22.3
38	360	2740	-447	535	0	-499	997	4.02	4.02	4.02	4.02	3	0.16	0.02	0.09	0.00	0.00	22.3
39	360	3070	-267	1151	0	-995	1029	4.02	4.02	4.02	4.02	3	0.27	0.04	0.19	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	420	1757	-794	744	0	-1101	927	4.02	4.02	4.02	4.02	3	0.28	0.02	0.14	0.00	0.00	22.3
2	420	1523	-631	661	0	-974	701	4.02	4.02	4.02	4.02	2	0.28	0.02	0.11	0.00	0.00	22.3
3	420	1247	-576	698	0	-1017	742	4.02	4.02	4.02	4.02	2	0.29	0.02	0.11	0.00	0.00	22.3
4	420	1456	-645	448	0	-677	683	4.02	4.02	4.02	4.02	2	0.20	0.02	0.11	0.00	0.00	22.3
5	420	1180	-590	485	0	-720	725	4.02	4.02	4.02	4.02	2	0.21	0.02	0.11	0.00	0.00	22.3
6	420	1820	-700	542	0	-820	646	4.02	4.02	4.02	4.02	2	0.24	0.02	0.12	0.00	0.00	22.3
7	420	903	-517	667	0	-963	779	4.02	4.02	4.02	4.02	2	0.27	0.02	0.11	0.00	0.00	22.3
8	420	1800	-704	478	0	-731	641	4.02	4.02	4.02	4.02	2	0.21	0.02	0.13	0.00	0.00	22.3
9	420	882	-521	603	0	-874	777	4.02	4.02	4.02	4.02	2	0.25	0.02	0.10	0.00	0.00	22.3
10	420	1523	-631	661	0	-974	701	4.02	4.02	4.02	4.02	2	0.28	0.02	0.11	0.00	0.00	22.3
11	420	1247	-576	698	0	-1017	742	4.02	4.02	4.02	4.02	2	0.29	0.02	0.11	0.00	0.00	22.3
12	420	1456	-645	448	0	-677	683	4.02	4.02	4.02	4.02	2	0.20	0.02	0.11	0.00	0.00	22.3

13	420	1180	-590	485	0	-720	725	4.02	4.02	4.02	4.02	2	0.21	0.02	0.11	0.00	0.00	22.3
14	420	1820	-700	542	0	-820	646	4.02	4.02	4.02	4.02	2	0.24	0.02	0.12	0.00	0.00	22.3
15	420	903	-517	667	0	-963	779	4.02	4.02	4.02	4.02	2	0.27	0.02	0.11	0.00	0.00	22.3
16	420	1800	-704	478	0	-731	641	4.02	4.02	4.02	4.02	2	0.21	0.02	0.13	0.00	0.00	22.3
17	420	882	-521	603	0	-874	777	4.02	4.02	4.02	4.02	2	0.25	0.02	0.10	0.00	0.00	22.3
18	420	4056	-766	1831	0	-2691	967	4.02	4.02	4.02	4.02	3	0.74	0.06	0.29	0.00	0.00	22.3
19	420	3576	-824	1026	0	-1535	910	4.02	4.02	4.02	4.02	3	0.42	0.03	0.17	0.00	0.00	22.3
20	420	3774	-716	1395	0	-2054	1004	4.02	4.02	4.02	4.02	3	0.56	0.04	0.22	0.00	0.00	22.3
37	420	3542	-746	1877	0	-2746	983	4.02	4.02	4.02	4.02	3	0.74	0.06	0.30	0.00	0.00	22.3
38	420	2740	-842	535	0	-820	887	4.02	4.02	4.02	4.02	3	0.22	0.02	0.15	0.00	0.00	22.3
39	420	3070	-662	1151	0	-1686	1029	4.02	4.02	4.02	4.02	3	0.45	0.04	0.19	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	480	1757	-1190	744	0	-1548	-672	4.02	4.02	4.02	4.02	3	0.40	0.03	0.21	0.00	0.00	22.3
2	480	1523	-936	661	0	-1370	-563	4.02	4.02	4.02	4.02	2	0.40	0.03	0.17	0.00	0.00	22.3
3	480	1247	-881	698	0	-1436	459	4.02	4.02	4.02	4.02	2	0.41	0.03	0.16	0.00	0.00	22.3
4	480	1456	-950	448	0	-945	-602	4.02	4.02	4.02	4.02	2	0.27	0.03	0.17	0.00	0.00	22.3
5	480	1180	-895	485	0	-1011	-472	4.02	4.02	4.02	4.02	2	0.29	0.03	0.16	0.00	0.00	22.3
6	480	1820	-1005	542	0	-1145	-728	4.02	4.02	4.02	4.02	2	0.34	0.03	0.18	0.00	0.00	22.3
7	480	903	-822	667	0	-1363	537	4.02	4.02	4.02	4.02	2	0.39	0.02	0.15	0.00	0.00	22.3
8	480	1800	-1009	479	0	-1018	-740	4.02	4.02	4.02	4.02	2	0.30	0.03	0.18	0.00	0.00	22.3
9	480	882	-826	603	0	-1236	529	4.02	4.02	4.02	4.02	2	0.35	0.02	0.15	0.00	0.00	22.3
10	480	1523	-936	661	0	-1370	-563	4.02	4.02	4.02	4.02	2	0.40	0.03	0.17	0.00	0.00	22.3
11	480	1247	-881	698	0	-1436	459	4.02	4.02	4.02	4.02	2	0.41	0.03	0.16	0.00	0.00	22.3
12	480	1456	-950	448	0	-945	-602	4.02	4.02	4.02	4.02	2	0.27	0.03	0.17	0.00	0.00	22.3
13	480	1180	-895	485	0	-1011	-472	4.02	4.02	4.02	4.02	2	0.29	0.03	0.16	0.00	0.00	22.3
14	480	1820	-1005	542	0	-1145	-728	4.02	4.02	4.02	4.02	2	0.34	0.03	0.18	0.00	0.00	22.3
15	480	903	-822	667	0	-1363	537	4.02	4.02	4.02	4.02	2	0.39	0.02	0.15	0.00	0.00	22.3
16	480	1800	-1009	479	0	-1018	-740	4.02	4.02	4.02	4.02	2	0.30	0.03	0.18	0.00	0.00	22.3
17	480	882	-826	603	0	-1236	529	4.02	4.02	4.02	4.02	2	0.35	0.02	0.15	0.00	0.00	22.3
18	480	4056	-1162	1831	0	-3789	589	4.02	6.03	4.02	4.02	3	0.72	0.06	0.29	0.00	0.00	22.3
19	480	3576	-1219	1026	0	-2151	-737	4.02	4.02	4.02	4.02	3	0.58	0.04	0.22	0.00	0.00	22.3
20	480	3774	-1111	1395	0	-2892	656	4.02	4.02	4.02	4.02	3	0.79	0.04	0.22	0.00	0.00	22.3
37	480	3542	-1142	1877	0	-3873	616	4.02	6.03	4.02	4.02	3	0.72	0.06	0.30	0.00	0.00	22.3
38	480	2740	-1238	535	0	-1142	-790	4.02	4.02	4.02	4.02	3	0.30	0.04	0.22	0.00	0.00	22.3
39	480	3070	-1058	1151	0	-2376	729	4.02	4.02	4.02	4.02	3	0.64	0.04	0.19	0.00	0.00	22.3

apost= -- aant= 2.01 ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	540	1757	-1585	744	0	-1994	-1705	4.02	4.02	4.02	4.02	3	0.51	0.05	0.28	0.00	0.00	22.3
2	540	1523	-1240	661	0	-1767	-1369	4.02	4.02	4.02	4.02	2	0.51	0.04	0.22	0.00	0.00	22.3
3	540	1247	-1185	698	0	-1854	-1206	4.02	4.02	4.02	4.02	2	0.53	0.03	0.21	0.00	0.00	22.3
4	540	1456	-1254	448	0	-1214	-1417	4.02	4.02	4.02	4.02	2	0.35	0.04	0.22	0.00	0.00	22.3
5	540	1180	-1199	485	0	-1302	-1254	4.02	4.02	4.02	4.02	2	0.37	0.03	0.21	0.00	0.00	22.3
6	540	1820	-1309	542	0	-1471	-1576	4.02	4.02	4.02	4.02	2	0.43	0.04	0.23	0.00	0.00	22.3
7	540	903	-1126	667	0	-1763	-1033	4.02	4.02	4.02	4.02	2	0.50	0.03	0.20	0.00	0.00	22.3
8	540	1800	-1313	478	0	-1305	-1591	4.02	4.02	4.02	4.02	2	0.38	0.04	0.23	0.00	0.00	22.3
9	540	882	-1130	603	0	-1597	-1048	4.02	4.02	4.02	4.02	2	0.45	0.03	0.20	0.00	0.00	22.3
10	540	1523	-1240	661	0	-1767	-1369	4.02	4.02	4.02	4.02	2	0.51	0.04	0.22	0.00	0.00	22.3
11	540	1247	-1185	698	0	-1854	-1206	4.02	4.02	4.02	4.02	2	0.53	0.03	0.21	0.00	0.00	22.3
12	540	1456	-1254	448	0	-1214	-1417	4.02	4.02	4.02	4.02	2	0.35	0.04	0.22	0.00	0.00	22.3
13	540	1180	-1199	485	0	-1302	-1254	4.02	4.02	4.02	4.02	2	0.37	0.03	0.21	0.00	0.00	22.3
14	540	1820	-1309	542	0	-1471	-1576	4.02	4.02	4.02	4.02	2	0.43	0.04	0.23	0.00	0.00	22.3
15	540	903	-1126	667	0	-1763	-1033	4.02	4.02	4.02	4.02	2	0.50	0.03	0.20	0.00	0.00	22.3
16	540	1800	-1313	478	0	-1305	-1591	4.02	4.02	4.02	4.02	2	0.38	0.04	0.23	0.00	0.00	22.3
17	540	882	-1130	603	0	-1597	-1048	4.02	4.02	4.02	4.02	2	0.45	0.03	0.20	0.00	0.00	22.3
18	540	4056	-1557	1831	0	-4888	-1603	4.02	6.03	4.02	4.02	3	0.92	0.06	0.29	0.00	0.00	22.3
19	540	3576	-1615	1026	0	-2766	-1788	4.02	4.02	4.02	4.02	3	0.75	0.05	0.29	0.00	0.00	22.3
20	540	3774	-1507	1395	0	-3729	-1455	4.02	6.03	4.02	4.02	3	0.70	0.04	0.27	0.00	0.00	22.3
37	540	3542	-1537	1877	0	-4999	-1544	4.02	6.03	4.02	4.02	3	0.93	0.06	0.30	0.00	0.00	22.3
38	540	2740	-1633	535	0	-1463	-1851	4.02	4.02	4.02	4.02	3	0.39	0.05	0.29	0.00	0.00	22.3
39	540	3070	-1453	1151	0	-3067	-1296	4.02	4.02	4.02	4.02	3	0.82	0.04	0.26	0.00	0.00	22.3

apost= -- aant= 2.01 ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	600	1757	-1981	744	0	-2441	-1972	4.02	4.02	4.02	4.02	3	0.63	0.06	0.35	0.00	0.00	22.3
2	600	1523	-1544	661	0	-2163	-1577	4.02	4.02	4.02	4.02	2	0.63	0.04	0.28	0.00	0.00	22.3
3	600	1247	-1489	698	0	-2273	-1409	4.02	4.02	4.02	4.02	2	0.65	0.04	0.27	0.00	0.00	22.3
4	600	1456	-1558	448	0	-1482	-1626	4.02	4.02	4.02	4.02	2	0.43	0.05	0.28	0.00	0.00	22.3
5	600	1180	-1503	485	0	-1593	-1458	4.02	4.02	4.02	4.02	2	0.46	0.04	0.27	0.00	0.00	22.3
6	600	1820	-1613	542	0	-1796	-1790	4.02	4.02	4.02	4.02	2	0.53	0.05	0.29	0.00	0.00	22.3
7	600	903	-1430	667	0	-2163	-1230	4.02	4.02	4.02	4.02	2	0.61	0.04	0.25	0.00	0.00	22.3
8	600	1800	-1617	478	0	-1592	-1805	4.02	4.02	4.02	4.02	2	0.47	0.05	0.29	0.00	0.00	22.3
9	600	882	-1434	603	0	-1959	-1245	4.02	4.02	4.02	4.02	2	0.56	0.04	0.26	0.00	0.00	22.3
10	600	1523	-1544	661	0	-2163	-1577	4.02	4.02	4.02	4.02	2	0.63	0.04	0.28	0.00	0.00	22.3
11	600	1247	-1489	698	0	-2273	-1409	4.02	4.02	4.02	4.02	2	0.65	0.04	0.27	0.00	0.00	22.3
12	600	1456	-1558	448	0	-1482	-1626	4.02	4.02	4.02	4.02	2	0.43	0.05	0.28	0.00	0.00	22.3
13	600	1180	-1503	485	0	-1593	-1458	4.02	4.02	4.02	4.02	2	0.46	0.04	0.27	0.00	0.00	22.3
14	600	1820	-1613	542	0	-1796	-1790	4.02	4.02	4.02	4.02	2	0.53	0.05	0.29	0.00	0.00	22.3
15	600	903	-1430	667	0	-2163	-1230	4.02	4.02	4.02	4.02	2	0.61	0.04	0.25	0.00	0.00	22.3
16	600	1800	-1617	478	0	-1592	-1805	4.02	4.02	4.02	4.02	2	0.47	0.05	0.29	0.00	0.00	22.3
17	600	882	-1434	603	0	-1959	-1245	4.02	4.02	4.02	4.02	2	0.56	0.04	0.26	0.00	0.00	22.3
18	600	4056	-1953	1831	0	-5987	-1868	4.02	8.04	4.02	4.02	3	0.86	0.06	0.35	0.00	0.00	22.3
19	600	3576	-2010	1026	0	-3382	-2058	4.02	4.02	4.02	4.02	3	0.92	0.06	0.36	0.00	0.00	22.3
20	600	3774	-1902	1395	0	-4566	-1715	4.02	6.03	4.02	4.02	3	0.86	0.06	0.34	0.00	0.00	22.3
37	600	3542	-1933	1877	0	-6125	-1807	4.02	8.04	4.02	4.02	3	0.87	0.06	0.34	0.00	0.00	22.3
38	600	2740	-2029	535	0	-1784	-2123	4.02	4.02	4.02	4.02	3	0.47	0.06	0.36	0.00	0.00	22.3
39	600	3070	-1849	1151	0	-3757	-1551	4.02	6.03	4.02	4.02	3	0.70	0.05	0.33	0.00	0.00	22.3

apost= -- aant= 4.02 ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

Nome travata: **Trave_404_IP1** Descrizione: **Trave_4 32-25**
ASTA NUM. 17 NI 255 NF 256 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y Permanente qy tot.
qy medio: 375.00 132.00 507.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	1995	1891	88	0	-19	-1703	4.02	4.02	4.02	4.02	3	0.26	0.05	0.34	0.00	0.00	22.3
2	0	1699	1428	72	0	-39	-1227	4.02	4.02	4.02	4.02	2	0.20	0.04	0.25	0.00	0.00	22.3
3	0	1454	1484	72	0	-38	-1394	4.02	4.02	4.02	4.02	2	0.22	0.04	0.26	0.00	0.00	22.3
4	0	1615	1426	64	0	9	-1227	4.02	4.02	4.02	4.02	2	0.20	0.04	0.25	0.00	0.00	22.3

5	0	1370	1482	64	0	11	-1394	4.02	4.02	4.02	4.02	2	0.22	0.04	0.26	0.00	0.00	22.3
6	0	1956	1361	70	0	-24	-1032	4.02	4.02	4.02	4.02	2	0.17	0.04	0.24	0.00	0.00	22.3
7	0	1139	1549	69	0	-19	-1589	4.02	4.02	4.02	4.02	2	0.25	0.04	0.28	0.00	0.00	22.3
8	0	1931	1361	67	0	-10	-1032	4.02	4.02	4.02	4.02	2	0.17	0.04	0.24	0.00	0.00	22.3
9	0	1114	1548	66	0	-4	-1589	4.02	4.02	4.02	4.02	2	0.25	0.04	0.28	0.00	0.00	22.3
10	0	1699	1428	72	0	-39	-1227	4.02	4.02	4.02	4.02	2	0.20	0.04	0.25	0.00	0.00	22.3
11	0	1454	1484	72	0	-38	-1394	4.02	4.02	4.02	4.02	2	0.22	0.04	0.26	0.00	0.00	22.3
12	0	1615	1426	64	0	9	-1227	4.02	4.02	4.02	4.02	2	0.20	0.04	0.25	0.00	0.00	22.3
13	0	1370	1482	64	0	11	-1394	4.02	4.02	4.02	4.02	2	0.22	0.04	0.26	0.00	0.00	22.3
14	0	1956	1361	70	0	-24	-1032	4.02	4.02	4.02	4.02	2	0.17	0.04	0.24	0.00	0.00	22.3
15	0	1139	1549	69	0	-19	-1589	4.02	4.02	4.02	4.02	2	0.25	0.04	0.28	0.00	0.00	22.3
16	0	1931	1361	67	0	-10	-1032	4.02	4.02	4.02	4.02	2	0.17	0.04	0.24	0.00	0.00	22.3
17	0	1114	1548	66	0	-4	-1589	4.02	4.02	4.02	4.02	2	0.25	0.04	0.28	0.00	0.00	22.3
18	0	4644	1820	195	0	-106	-1471	4.02	4.02	4.02	4.02	3	0.24	0.05	0.32	0.00	0.00	22.3
19	0	4015	1820	150	0	57	-1483	4.02	4.02	4.02	4.02	3	0.24	0.05	0.32	0.00	0.00	22.3
20	0	4272	1917	162	0	-7	-1767	4.02	4.02	4.02	4.02	3	0.29	0.06	0.34	0.00	0.00	22.3
37	0	4087	1844	183	0	-159	-1541	4.02	4.02	4.02	4.02	3	0.25	0.05	0.33	0.00	0.00	22.3
38	0	3039	1843	108	0	113	-1563	4.02	4.02	4.02	4.02	3	0.25	0.05	0.33	0.00	0.00	22.3
39	0	3467	2006	128	0	7	-2036	4.02	4.02	4.02	4.02	3	0.32	0.06	0.36	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	60	1995	1496	88	0	-72	-1444	4.02	4.02	4.02	4.02	3	0.22	0.04	0.27	0.00	0.00	22.3
2	60	1699	1124	72	0	-83	-1031	4.02	4.02	4.02	4.02	2	0.16	0.03	0.20	0.00	0.00	22.3
3	60	1454	1180	72	0	-81	-1192	4.02	4.02	4.02	4.02	2	0.19	0.03	0.21	0.00	0.00	22.3
4	60	1615	1122	64	0	-29	-1031	4.02	4.02	4.02	4.02	2	0.16	0.03	0.20	0.00	0.00	22.3
5	60	1370	1178	64	0	-27	-1192	4.02	4.02	4.02	4.02	2	0.19	0.03	0.21	0.00	0.00	22.3
6	60	1956	1057	70	0	-66	-841	4.02	4.02	4.02	4.02	2	0.14	0.03	0.19	0.00	0.00	22.3
7	60	1139	1245	69	0	-60	-1381	4.02	4.02	4.02	4.02	2	0.22	0.04	0.22	0.00	0.00	22.3
8	60	1931	1057	67	0	-50	-842	4.02	4.02	4.02	4.02	2	0.14	0.03	0.19	0.00	0.00	22.3
9	60	1114	1244	66	0	-44	-1381	4.02	4.02	4.02	4.02	2	0.22	0.04	0.22	0.00	0.00	22.3
10	60	1699	1124	72	0	-83	-1031	4.02	4.02	4.02	4.02	2	0.16	0.03	0.20	0.00	0.00	22.3
11	60	1454	1180	72	0	-81	-1192	4.02	4.02	4.02	4.02	2	0.19	0.03	0.21	0.00	0.00	22.3
12	60	1615	1122	64	0	-29	-1031	4.02	4.02	4.02	4.02	2	0.16	0.03	0.20	0.00	0.00	22.3
13	60	1370	1178	64	0	-27	-1192	4.02	4.02	4.02	4.02	2	0.19	0.03	0.21	0.00	0.00	22.3
14	60	1956	1057	70	0	-66	-841	4.02	4.02	4.02	4.02	2	0.14	0.03	0.19	0.00	0.00	22.3
15	60	1139	1245	69	0	-60	-1381	4.02	4.02	4.02	4.02	2	0.22	0.04	0.22	0.00	0.00	22.3
16	60	1931	1057	67	0	-50	-842	4.02	4.02	4.02	4.02	2	0.14	0.03	0.19	0.00	0.00	22.3
17	60	1114	1244	66	0	-44	-1381	4.02	4.02	4.02	4.02	2	0.22	0.04	0.22	0.00	0.00	22.3
18	60	4644	1425	195	0	-223	-1219	4.02	4.02	4.02	4.02	3	0.20	0.04	0.25	0.00	0.00	22.3
19	60	4015	1424	150	0	-33	-1231	4.02	4.02	4.02	4.02	3	0.20	0.04	0.25	0.00	0.00	22.3
20	60	4272	1522	162	0	-104	-1506	4.02	4.02	4.02	4.02	3	0.25	0.04	0.27	0.00	0.00	22.3
37	60	4087	1448	183	0	-268	-1287	4.02	4.02	4.02	4.02	3	0.21	0.04	0.26	0.00	0.00	22.3
38	60	3039	1448	108	0	49	-1308	4.02	4.02	4.02	4.02	3	0.21	0.04	0.26	0.00	0.00	22.3
39	60	3467	1610	128	0	-70	-1766	4.02	4.02	4.02	4.02	3	0.28	0.05	0.29	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	120	1995	1100	88	0	-125	649	4.02	4.02	4.02	4.02	3	0.10	0.03	0.20	0.00	0.00	22.3
2	120	1699	820	72	0	-126	536	4.02	4.02	4.02	4.02	2	0.09	0.02	0.15	0.00	0.00	22.3
3	120	1454	876	72	0	-124	465	4.02	4.02	4.02	4.02	2	0.07	0.03	0.16	0.00	0.00	22.3
4	120	1615	818	64	0	-68	533	4.02	4.02	4.02	4.02	2	0.08	0.02	0.15	0.00	0.00	22.3
5	120	1370	874	64	0	-66	462	4.02	4.02	4.02	4.02	2	0.07	0.03	0.16	0.00	0.00	22.3
6	120	1956	753	70	0	-108	618	4.02	4.02	4.02	4.02	2	0.10	0.02	0.13	0.00	0.00	22.3
7	120	1139	941	69	0	-101	-571	4.02	4.02	4.02	4.02	2	0.09	0.03	0.17	0.00	0.00	22.3
8	120	1931	753	67	0	-91	617	4.02	4.02	4.02	4.02	2	0.10	0.02	0.13	0.00	0.00	22.3
9	120	1114	940	66	0	-84	-572	4.02	4.02	4.02	4.02	2	0.09	0.03	0.17	0.00	0.00	22.3
10	120	1699	820	72	0	-126	536	4.02	4.02	4.02	4.02	2	0.09	0.02	0.15	0.00	0.00	22.3
11	120	1454	876	72	0	-124	465	4.02	4.02	4.02	4.02	2	0.07	0.03	0.16	0.00	0.00	22.3
12	120	1615	818	64	0	-68	533	4.02	4.02	4.02	4.02	2	0.08	0.02	0.15	0.00	0.00	22.3
13	120	1370	874	64	0	-66	462	4.02	4.02	4.02	4.02	2	0.07	0.03	0.16	0.00	0.00	22.3
14	120	1956	753	70	0	-108	618	4.02	4.02	4.02	4.02	2	0.10	0.02	0.13	0.00	0.00	22.3
15	120	1139	941	69	0	-101	-571	4.02	4.02	4.02	4.02	2	0.09	0.03	0.17	0.00	0.00	22.3
16	120	1931	753	67	0	-91	617	4.02	4.02	4.02	4.02	2	0.10	0.02	0.13	0.00	0.00	22.3
17	120	1114	940	66	0	-84	-572	4.02	4.02	4.02	4.02	2	0.09	0.03	0.17	0.00	0.00	22.3
18	120	4644	1029	195	0	-340	760	4.02	4.02	4.02	4.02	3	0.13	0.03	0.18	0.00	0.00	22.3
19	120	4015	1029	150	0	-123	747	4.02	4.02	4.02	4.02	3	0.12	0.03	0.18	0.00	0.00	22.3
20	120	4272	1126	162	0	-201	629	4.02	4.02	4.02	4.02	3	0.10	0.03	0.20	0.00	0.00	22.3
37	120	4087	1053	183	0	-378	730	4.02	4.02	4.02	4.02	3	0.12	0.03	0.19	0.00	0.00	22.3
38	120	3039	1052	108	0	-16	707	4.02	4.02	4.02	4.02	3	0.11	0.03	0.19	0.00	0.00	22.3
39	120	3467	1215	128	0	-147	-718	4.02	4.02	4.02	4.02	3	0.11	0.04	0.22	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	180	1995	705	88	0	-178	990	4.02	4.02	4.02	4.02	3	0.15	0.02	0.13	0.00	0.00	22.3
2	180	1699	515	72	0	-170	775	4.02	4.02	4.02	4.02	2	0.12	0.01	0.09	0.00	0.00	22.3
3	180	1454	571	72	0	-167	745	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
4	180	1615	513	64	0	-106	769	4.02	4.02	4.02	4.02	2	0.12	0.01	0.09	0.00	0.00	22.3
5	180	1370	569	64	0	-104	741	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
6	180	1956	448	70	0	-150	775	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
7	180	1139	636	69	0	-142	700	4.02	4.02	4.02	4.02	2	0.11	0.02	0.11	0.00	0.00	22.3
8	180	1931	448	67	0	-131	774	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
9	180	1114	635	66	0	-123	699	4.02	4.02	4.02	4.02	2	0.11	0.02	0.11	0.00	0.00	22.3
10	180	1699	515	72	0	-170	775	4.02	4.02	4.02	4.02	2	0.12	0.01	0.09	0.00	0.00	22.3
11	180	1454	571	72	0	-167	745	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
12	180	1615	513	64	0	-106	769	4.02	4.02	4.02	4.02	2	0.12	0.01	0.09	0.00	0.00	22.3
13	180	1370	569	64	0	-104	741	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
14	180	1956	448	70	0	-150	775	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
15	180	1139	636	69	0	-142	700	4.02	4.02	4.02	4.02	2	0.11	0.02	0.11	0.00	0.00	22.3
16	180	1931	448	67	0	-131	774	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
17	180	1114	635	66	0	-123	699	4.02	4.02	4.02	4.02	2	0.11	0.02	0.11	0.00	0.00	22.3
18	180	4644	634	195	0	-457	1024	4.02	4.02	4.02	4.02	3	0.17	0.02	0.11	0.00	0.00	22.3
19	180	4015	633	150	0	-213	1010	4.02	4.02	4.02	4.02	3	0.16	0.02	0.11	0.00	0.00	22.3
20	180	4272	731	162	0	-299	986	4.02	4.02	4.02	4.02	3	0.16	0.02	0.13	0.00	0.00	22.3
37	180	4087	657	183	0	-487	1025	4.02	4.02	4.02	4.02	3	0.17	0.02	0.12	0.00	0.00	22.3
38	180	3039	657	108	0	-80	1001	4.02	4.02	4.02	4.02	3	0.16	0.02	0.12	0.00	0.00	22.3
39	180	3467	820	128	0	-223	922	4.02	4.02	4.02	4.02	3	0.15	0.02	0.15	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	240	1995	309	88	0	-231	1005	4.02	4.02	4.02	4.02	3	0.15	0.01	0.06	0.00	0.00	22.3
2	240	1699	211	72	0	-213	775	4.02	4.02	4.02	4.02	2	0.12	0.01	0.04	0.00	0.00	22.3
3	240	1454	267	72	0	-211	777	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
4	240	1615	209	64	0	-145	769	4.02	4.02	4.02	4.02	2	0.12	0.01	0.04	0.00	0.00	22.3
5	240	1370	265	64	0	-142	771	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
6	240	1956	144	70	0	-192	775	4.02	4.02	4.02	4.02	2	0.12	0.00	0.03	0.00	0.00	22.3
7	240	1139	332	69	0	-183	777	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
8	240	1931	144	67	0	-172	774	4.02	4.02	4.02	4.02	2	0.12	0.00	0.03	0.00	0.00	22.3
9	240	1114	331	66	0	-163	775	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
10	240	1699	211	72	0	-213	775	4.02	4.02	4.02	4.02	2	0.12	0.01	0.04	0.00	0.00	22.3

11	240	1454	267	72	0	-211	777	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
12	240	1615	209	64	0	-145	769	4.02	4.02	4.02	4.02	2	0.12	0.01	0.04	0.00	0.00	22.3
13	240	1370	265	64	0	-142	771	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
14	240	1956	144	70	0	-192	775	4.02	4.02	4.02	4.02	2	0.12	0.00	0.03	0.00	0.00	22.3
15	240	1139	332	69	0	-183	777	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
16	240	1931	144	67	0	-172	774	4.02	4.02	4.02	4.02	2	0.12	0.00	0.03	0.00	0.00	22.3
17	240	1114	331	66	0	-163	775	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
18	240	4644	238	195	0	-574	1024	4.02	4.02	4.02	4.02	3	0.17	0.01	0.04	0.00	0.00	22.3
19	240	4015	238	150	0	-303	1010	4.02	4.02	4.02	4.02	3	0.16	0.01	0.04	0.00	0.00	22.3
20	240	4272	335	162	0	-396	1019	4.02	4.02	4.02	4.02	3	0.17	0.01	0.06	0.00	0.00	22.3
37	240	4087	262	183	0	-597	1025	4.02	4.02	4.02	4.02	3	0.17	0.01	0.05	0.00	0.00	22.3
38	240	3039	261	108	0	-145	1001	4.02	4.02	4.02	4.02	3	0.16	0.01	0.05	0.00	0.00	22.3
39	240	3467	424	128	0	-300	1016	4.02	4.02	4.02	4.02	3	0.16	0.01	0.08	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	300	1995	-86	88	0	-284	1005	4.02	4.02	4.02	4.02	3	0.15	0.00	0.02	0.00	0.00	22.3
2	300	1699	-93	72	0	-257	775	4.02	4.02	4.02	4.02	2	0.12	0.00	0.02	0.00	0.00	22.3
3	300	1454	-37	72	0	-254	777	4.02	4.02	4.02	4.02	2	0.12	0.00	0.01	0.00	0.00	22.3
4	300	1615	-95	64	0	-183	769	4.02	4.02	4.02	4.02	2	0.12	0.00	0.02	0.00	0.00	22.3
5	300	1370	-39	64	0	-180	771	4.02	4.02	4.02	4.02	2	0.12	0.00	0.01	0.00	0.00	22.3
6	300	1956	-160	70	0	-234	775	4.02	4.02	4.02	4.02	2	0.12	0.00	0.03	0.00	0.00	22.3
7	300	1139	28	69	0	-225	777	4.02	4.02	4.02	4.02	2	0.12	0.00	0.00	0.00	0.00	22.3
8	300	1931	-160	67	0	-212	774	4.02	4.02	4.02	4.02	2	0.12	0.00	0.03	0.00	0.00	22.3
9	300	1114	27	66	0	-202	775	4.02	4.02	4.02	4.02	2	0.12	0.00	0.00	0.00	0.00	22.3
10	300	1699	-93	72	0	-257	775	4.02	4.02	4.02	4.02	2	0.12	0.00	0.02	0.00	0.00	22.3
11	300	1454	-37	72	0	-254	777	4.02	4.02	4.02	4.02	2	0.12	0.00	0.01	0.00	0.00	22.3
12	300	1615	-95	64	0	-183	769	4.02	4.02	4.02	4.02	2	0.12	0.00	0.02	0.00	0.00	22.3
13	300	1370	-39	64	0	-180	771	4.02	4.02	4.02	4.02	2	0.12	0.00	0.01	0.00	0.00	22.3
14	300	1956	-160	70	0	-234	775	4.02	4.02	4.02	4.02	2	0.12	0.00	0.03	0.00	0.00	22.3
15	300	1139	28	69	0	-225	777	4.02	4.02	4.02	4.02	2	0.12	0.00	0.00	0.00	0.00	22.3
16	300	1931	-160	67	0	-212	774	4.02	4.02	4.02	4.02	2	0.12	0.00	0.03	0.00	0.00	22.3
17	300	1114	27	66	0	-202	775	4.02	4.02	4.02	4.02	2	0.12	0.00	0.00	0.00	0.00	22.3
18	300	4644	-157	195	0	-691	1024	4.02	4.02	4.02	4.02	3	0.19	0.01	0.03	0.00	0.00	22.3
19	300	4015	-158	150	0	-393	1010	4.02	4.02	4.02	4.02	3	0.16	0.00	0.03	0.00	0.00	22.3
20	300	4272	-60	162	0	-493	1019	4.02	4.02	4.02	4.02	3	0.17	0.01	0.03	0.00	0.00	22.3
37	300	4087	-134	183	0	-706	1025	4.02	4.02	4.02	4.02	3	0.19	0.01	0.03	0.00	0.00	22.3
38	300	3039	-134	108	0	-209	1001	4.02	4.02	4.02	4.02	3	0.16	0.00	0.02	0.00	0.00	22.3
39	300	3467	28	128	0	-377	1016	4.02	4.02	4.02	4.02	3	0.16	0.00	0.01	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	360	1995	-481	88	0	-337	1005	4.02	4.02	4.02	4.02	3	0.15	0.01	0.09	0.00	0.00	22.3
2	360	1699	-397	72	0	-300	775	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
3	360	1454	-341	72	0	-297	777	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
4	360	1615	-399	64	0	-221	769	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
5	360	1370	-343	64	0	-218	771	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
6	360	1956	-464	70	0	-276	775	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
7	360	1139	-276	69	0	-266	777	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
8	360	1931	-464	67	0	-253	774	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
9	360	1114	-277	66	0	-242	775	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
10	360	1699	-397	72	0	-300	775	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
11	360	1454	-341	72	0	-297	777	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
12	360	1615	-399	64	0	-221	769	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
13	360	1370	-343	64	0	-218	771	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
14	360	1956	-464	70	0	-276	775	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
15	360	1139	-276	69	0	-266	777	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
16	360	1931	-464	67	0	-253	774	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
17	360	1114	-277	66	0	-242	775	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
18	360	4644	-552	195	0	-808	1024	4.02	4.02	4.02	4.02	3	0.23	0.02	0.10	0.00	0.00	22.3
19	360	4015	-553	150	0	-483	1010	4.02	4.02	4.02	4.02	3	0.16	0.02	0.10	0.00	0.00	22.3
20	360	4272	-455	162	0	-590	1019	4.02	4.02	4.02	4.02	3	0.17	0.01	0.08	0.00	0.00	22.3
37	360	4087	-529	183	0	-816	1025	4.02	4.02	4.02	4.02	3	0.22	0.02	0.09	0.00	0.00	22.3
38	360	3039	-529	108	0	-274	1001	4.02	4.02	4.02	4.02	3	0.16	0.02	0.09	0.00	0.00	22.3
39	360	3467	-367	128	0	-453	1016	4.02	4.02	4.02	4.02	3	0.16	0.01	0.07	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	420	1995	-877	88	0	-390	871	4.02	4.02	4.02	4.02	3	0.13	0.03	0.16	0.00	0.00	22.3
2	420	1699	-701	72	0	-344	653	4.02	4.02	4.02	4.02	2	0.10	0.02	0.12	0.00	0.00	22.3
3	420	1454	-645	72	0	-340	694	4.02	4.02	4.02	4.02	2	0.11	0.02	0.11	0.00	0.00	22.3
4	420	1615	-703	64	0	-260	646	4.02	4.02	4.02	4.02	2	0.10	0.02	0.13	0.00	0.00	22.3
5	420	1370	-647	64	0	-256	687	4.02	4.02	4.02	4.02	2	0.11	0.02	0.12	0.00	0.00	22.3
6	420	1956	-768	70	0	-318	603	4.02	4.02	4.02	4.02	2	0.10	0.02	0.14	0.00	0.00	22.3
7	420	1139	-580	69	0	-307	739	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
8	420	1931	-768	67	0	-293	601	4.02	4.02	4.02	4.02	2	0.10	0.02	0.14	0.00	0.00	22.3
9	420	1114	-581	66	0	-282	737	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
10	420	1699	-701	72	0	-344	653	4.02	4.02	4.02	4.02	2	0.10	0.02	0.12	0.00	0.00	22.3
11	420	1454	-645	72	0	-340	694	4.02	4.02	4.02	4.02	2	0.11	0.02	0.11	0.00	0.00	22.3
12	420	1615	-703	64	0	-260	646	4.02	4.02	4.02	4.02	2	0.10	0.02	0.13	0.00	0.00	22.3
13	420	1370	-647	64	0	-256	687	4.02	4.02	4.02	4.02	2	0.11	0.02	0.12	0.00	0.00	22.3
14	420	1956	-768	70	0	-318	603	4.02	4.02	4.02	4.02	2	0.10	0.02	0.14	0.00	0.00	22.3
15	420	1139	-580	69	0	-307	739	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
16	420	1931	-768	67	0	-293	601	4.02	4.02	4.02	4.02	2	0.10	0.02	0.14	0.00	0.00	22.3
17	420	1114	-581	66	0	-282	737	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
18	420	4644	-948	195	0	-925	841	4.02	4.02	4.02	4.02	3	0.26	0.03	0.17	0.00	0.00	22.3
19	420	4015	-948	150	0	-573	827	4.02	4.02	4.02	4.02	3	0.16	0.03	0.17	0.00	0.00	22.3
20	420	4272	-851	162	0	-688	903	4.02	4.02	4.02	4.02	3	0.19	0.02	0.15	0.00	0.00	22.3
37	420	4087	-924	183	0	-925	858	4.02	4.02	4.02	4.02	3	0.25	0.03	0.16	0.00	0.00	22.3
38	420	3039	-925	108	0	-338	834	4.02	4.02	4.02	4.02	3	0.13	0.03	0.16	0.00	0.00	22.3
39	420	3467	-762	128	0	-530	963	4.02	4.02	4.02	4.02	3	0.15	0.02	0.14	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	480	1995	-1272	88	0	-443	-862	4.02	4.02	4.02	4.02	3	0.13	0.04	0.23	0.00	0.00	22.3
2	480	1699	-1006	72	0	-387	-724	4.02	4.02	4.02	4.02	2	0.12	0.03	0.18	0.00	0.00	22.3
3	480	1454	-950	72	0	-383	-592	4.02	4.02	4.02	4.02	2	0.11	0.03	0.17	0.00	0.00	22.3
4	480	1615	-1008	64	0	-298	-734	4.02	4.02	4.02	4.02	2	0.12	0.03	0.18	0.00	0.00	22.3
5	480	1370	-952	64	0	-295	-602	4.02	4.02	4.02	4.02	2	0.10	0.03	0.17	0.00	0.00	22.3
6	480	1956	-1073	70	0	-360	-881	4.02	4.02	4.02	4.02	2	0.14	0.03	0.19	0.00	0.00	22.3
7	480	1139	-885	69	0	-348	453	4.02	4.02	4.02	4.02	2	0.10	0.03	0.16	0.00	0.00	22.3
8	480	1931	-1073	67	0	-334	-884	4.02	4.02	4.02	4.02	2	0.14	0.03	0.19	0.00	0.00	22.3
9	480	1114	-886	66	0	-321	451	4.02	4.02	4.02	4.02	2	0.09	0.03	0.16	0.00	0.00	22.3
10	480	1699	-1006	72	0	-387	-724	4.02	4.02	4.02	4.02	2	0.12	0.03	0.18	0.00	0.00	22.3
11	480	1454	-950	72	0	-383	-592	4.02	4.02	4.02	4.02	2	0.11	0.03	0.17	0.00	0.00	22.3
12	480	1615	-1008	64	0	-298	-734	4.02	4.02	4.02	4.02	2	0.12	0.03	0.18	0.00	0.00	22.3
13	480	1370	-952	64	0	-295	-602	4.02	4.02	4.02	4.02	2	0.10	0.03	0.17	0.00	0.00	22.3
14	480	1956	-1073	70	0	-360	-881	4.02	4.02	4.02	4.02	2	0.14	0.03	0.19	0.00	0.00	22.3
15	480	1139	-885	69	0	-348	453	4.02	4.02	4.02	4.02	2	0.10	0.03	0.16	0.00	0.00	22.3
16	480	1931	-1073	67	0	-334	-884	4.02	4.02	4.02	4.02	2	0.14	0.03	0.19	0.00	0.00	22.3

17	480	1114	-886	66	0	-321	451	4.02	4.02	4.02	4.02	2	0.09	0.03	0.16	0.00	0.00	22.3
18	480	4644	-1343	195	0	-1042	-1006	4.02	4.02	4.02	4.02	3	0.29	0.04	0.24	0.00	0.00	22.3
19	480	4015	-1344	150	0	-663	-1021	4.02	4.02	4.02	4.02	3	0.18	0.04	0.24	0.00	0.00	22.3
20	480	4272	-1246	162	0	-785	-788	4.02	4.02	4.02	4.02	3	0.22	0.04	0.22	0.00	0.00	22.3
37	480	4087	-1320	183	0	-1035	-951	4.02	4.02	4.02	4.02	3	0.29	0.04	0.24	0.00	0.00	22.3
38	480	3039	-1320	108	0	-403	-976	4.02	4.02	4.02	4.02	3	0.15	0.04	0.24	0.00	0.00	22.3
39	480	3467	-1158	128	0	-607	587	4.02	4.02	4.02	4.02	3	0.16	0.03	0.21	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	540	1995	-1668	88	0	-496	-1944	4.02	4.02	4.02	4.02	3	0.30	0.05	0.30	0.00	0.00	22.3
2	540	1699	-1310	72	0	-431	-1573	4.02	4.02	4.02	4.02	2	0.25	0.04	0.23	0.00	0.00	22.3
3	540	1454	-1254	72	0	-427	-1407	4.02	4.02	4.02	4.02	2	0.22	0.04	0.22	0.00	0.00	22.3
4	540	1615	-1312	64	0	-337	-1584	4.02	4.02	4.02	4.02	2	0.25	0.04	0.23	0.00	0.00	22.3
5	540	1370	-1256	64	0	-333	-1418	4.02	4.02	4.02	4.02	2	0.22	0.04	0.22	0.00	0.00	22.3
6	540	1956	-1377	70	0	-402	-1770	4.02	4.02	4.02	4.02	2	0.29	0.04	0.25	0.00	0.00	22.3
7	540	1139	-1189	69	0	-389	-1218	4.02	4.02	4.02	4.02	2	0.19	0.03	0.21	0.00	0.00	22.3
8	540	1931	-1377	67	0	-374	-1773	4.02	4.02	4.02	4.02	2	0.29	0.04	0.25	0.00	0.00	22.3
9	540	1114	-1190	66	0	-361	-1221	4.02	4.02	4.02	4.02	2	0.19	0.03	0.21	0.00	0.00	22.3
10	540	1699	-1310	72	0	-431	-1573	4.02	4.02	4.02	4.02	2	0.25	0.04	0.23	0.00	0.00	22.3
11	540	1454	-1254	72	0	-427	-1407	4.02	4.02	4.02	4.02	2	0.22	0.04	0.22	0.00	0.00	22.3
12	540	1615	-1312	64	0	-337	-1584	4.02	4.02	4.02	4.02	2	0.25	0.04	0.23	0.00	0.00	22.3
13	540	1370	-1256	64	0	-333	-1418	4.02	4.02	4.02	4.02	2	0.22	0.04	0.22	0.00	0.00	22.3
14	540	1956	-1377	70	0	-402	-1770	4.02	4.02	4.02	4.02	2	0.29	0.04	0.25	0.00	0.00	22.3
15	540	1139	-1189	69	0	-389	-1218	4.02	4.02	4.02	4.02	2	0.19	0.03	0.21	0.00	0.00	22.3
16	540	1931	-1377	67	0	-374	-1773	4.02	4.02	4.02	4.02	2	0.29	0.04	0.25	0.00	0.00	22.3
17	540	1114	-1190	66	0	-361	-1221	4.02	4.02	4.02	4.02	2	0.19	0.03	0.21	0.00	0.00	22.3
18	540	4644	-1739	195	0	-1159	-2131	4.02	4.02	4.02	4.02	3	0.35	0.05	0.31	0.00	0.00	22.3
19	540	4015	-1740	150	0	-753	-2146	4.02	4.02	4.02	4.02	3	0.35	0.05	0.31	0.00	0.00	22.3
20	540	4272	-1642	162	0	-882	-1854	4.02	4.02	4.02	4.02	3	0.30	0.05	0.29	0.00	0.00	22.3
37	540	4087	-1716	183	0	-1144	-2062	4.02	4.02	4.02	4.02	3	0.34	0.05	0.31	0.00	0.00	22.3
38	540	3039	-1716	108	0	-467	-2086	4.02	4.02	4.02	4.02	3	0.33	0.05	0.31	0.00	0.00	22.3
39	540	3467	-1553	128	0	-683	-1599	4.02	4.02	4.02	4.02	3	0.26	0.05	0.28	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	600	1995	-2063	88	0	-549	-2219	4.02	4.02	4.02	4.02	3	0.34	0.06	0.37	0.00	0.00	22.3
2	600	1699	-1614	72	0	-474	-1787	4.02	4.02	4.02	4.02	2	0.29	0.05	0.29	0.00	0.00	22.3
3	600	1454	-1558	72	0	-470	-1616	4.02	4.02	4.02	4.02	2	0.26	0.05	0.28	0.00	0.00	22.3
4	600	1615	-1616	64	0	-375	-1798	4.02	4.02	4.02	4.02	2	0.29	0.05	0.29	0.00	0.00	22.3
5	600	1370	-1560	64	0	-371	-1627	4.02	4.02	4.02	4.02	2	0.26	0.05	0.28	0.00	0.00	22.3
6	600	1956	-1681	70	0	-444	-1990	4.02	4.02	4.02	4.02	2	0.32	0.05	0.30	0.00	0.00	22.3
7	600	1139	-1493	69	0	-430	-1421	4.02	4.02	4.02	4.02	2	0.22	0.04	0.27	0.00	0.00	22.3
8	600	1931	-1681	67	0	-415	-1993	4.02	4.02	4.02	4.02	2	0.32	0.05	0.30	0.00	0.00	22.3
9	600	1114	-1494	66	0	-400	-1424	4.02	4.02	4.02	4.02	2	0.22	0.04	0.27	0.00	0.00	22.3
10	600	1699	-1614	72	0	-474	-1787	4.02	4.02	4.02	4.02	2	0.29	0.05	0.29	0.00	0.00	22.3
11	600	1454	-1558	72	0	-470	-1616	4.02	4.02	4.02	4.02	2	0.26	0.05	0.28	0.00	0.00	22.3
12	600	1615	-1616	64	0	-375	-1798	4.02	4.02	4.02	4.02	2	0.29	0.05	0.29	0.00	0.00	22.3
13	600	1370	-1560	64	0	-371	-1627	4.02	4.02	4.02	4.02	2	0.26	0.05	0.28	0.00	0.00	22.3
14	600	1956	-1681	70	0	-444	-1990	4.02	4.02	4.02	4.02	2	0.32	0.05	0.30	0.00	0.00	22.3
15	600	1139	-1493	69	0	-430	-1421	4.02	4.02	4.02	4.02	2	0.22	0.04	0.27	0.00	0.00	22.3
16	600	1931	-1681	67	0	-415	-1993	4.02	4.02	4.02	4.02	2	0.32	0.05	0.30	0.00	0.00	22.3
17	600	1114	-1494	66	0	-400	-1424	4.02	4.02	4.02	4.02	2	0.22	0.04	0.27	0.00	0.00	22.3
18	600	4644	-2134	195	0	-1276	-2413	4.02	4.02	4.02	4.02	3	0.40	0.06	0.38	0.00	0.00	22.3
19	600	4015	-2135	150	0	-843	-2428	4.02	4.02	4.02	4.02	3	0.39	0.06	0.38	0.00	0.00	22.3
20	600	4272	-2037	162	0	-980	-2127	4.02	4.02	4.02	4.02	3	0.35	0.06	0.36	0.00	0.00	22.3
37	600	4087	-2111	183	0	-1254	-2341	4.02	4.02	4.02	4.02	3	0.38	0.06	0.38	0.00	0.00	22.3
38	600	3039	-2111	108	0	-532	-2366	4.02	4.02	4.02	4.02	3	0.37	0.06	0.38	0.00	0.00	22.3
39	600	3467	-1949	128	0	-760	-1863	4.02	4.02	4.02	4.02	3	0.30	0.06	0.35	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

Nome travata: **Trave_404_IP1** Descrizione: **Trave_4 32-25**
ASTA NUM. 18 NI 256 NF 257 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y Permanente qy tot.
qy medio: 375.00 132.00 507.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	2151	1858	-121	0	-619	-1616	4.02	4.02	4.02	4.02	3	0.25	0.05	0.33	0.00	0.00	22.3
2	0	1821	1399	-106	0	-544	-1152	4.02	4.02	4.02	4.02	2	0.18	0.04	0.25	0.00	0.00	22.3
3	0	1634	1461	-82	0	-466	-1339	4.02	4.02	4.02	4.02	2	0.21	0.04	0.26	0.00	0.00	22.3
4	0	1676	1398	-104	0	-485	-1147	4.02	4.02	4.02	4.02	2	0.18	0.04	0.25	0.00	0.00	22.3
5	0	1489	1460	-81	0	-408	-1333	4.02	4.02	4.02	4.02	2	0.21	0.04	0.26	0.00	0.00	22.3
6	0	1989	1326	-132	0	-614	-933	4.02	4.02	4.02	4.02	2	0.18	0.04	0.24	0.00	0.00	22.3
7	0	1364	1534	-54	0	-355	-1555	4.02	4.02	4.02	4.02	2	0.25	0.04	0.27	0.00	0.00	22.3
8	0	1946	1325	-132	0	-597	-931	4.02	4.02	4.02	4.02	2	0.18	0.04	0.24	0.00	0.00	22.3
9	0	1321	1533	-54	0	-338	-1553	4.02	4.02	4.02	4.02	2	0.25	0.04	0.27	0.00	0.00	22.3
10	0	1821	1399	-106	0	-544	-1152	4.02	4.02	4.02	4.02	2	0.18	0.04	0.25	0.00	0.00	22.3
11	0	1634	1461	-82	0	-466	-1339	4.02	4.02	4.02	4.02	2	0.21	0.04	0.26	0.00	0.00	22.3
12	0	1676	1398	-104	0	-485	-1147	4.02	4.02	4.02	4.02	2	0.18	0.04	0.25	0.00	0.00	22.3
13	0	1489	1460	-81	0	-408	-1333	4.02	4.02	4.02	4.02	2	0.21	0.04	0.26	0.00	0.00	22.3
14	0	1989	1326	-132	0	-614	-933	4.02	4.02	4.02	4.02	2	0.18	0.04	0.24	0.00	0.00	22.3
15	0	1364	1534	-54	0	-355	-1555	4.02	4.02	4.02	4.02	2	0.25	0.04	0.27	0.00	0.00	22.3
16	0	1946	1325	-132	0	-597	-931	4.02	4.02	4.02	4.02	2	0.18	0.04	0.24	0.00	0.00	22.3
17	0	1321	1533	-54	0	-338	-1553	4.02	4.02	4.02	4.02	2	0.25	0.04	0.27	0.00	0.00	22.3
18	0	5081	1735	-244	0	-1340	-1258	4.02	4.02	4.02	4.02	3	0.38	0.05	0.31	0.00	0.00	22.3
19	0	4387	1752	-211	0	-1001	-1302	4.02	4.02	4.02	4.02	3	0.28	0.05	0.31	0.00	0.00	22.3
20	0	4665	1859	-155	0	-901	-1622	4.02	4.02	4.02	4.02	3	0.27	0.05	0.33	0.00	0.00	22.3
37	0	4463	1768	-221	0	-1273	-1354	4.02	4.02	4.02	4.02	3	0.35	0.05	0.31	0.00	0.00	22.3
38	0	3308	1796	-165	0	-708	-1428	4.02	4.02	4.02	4.02	3	0.23	0.05	0.32	0.00	0.00	22.3
39	0	3771	1973	-73	0	-541	-1961	4.02	4.02	4.02	4.02	3	0.32	0.06	0.35	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	60	2151	1463	-121	0	-546	-1360	4.02	4.02	4.02	4.02	3	0.21	0.04	0.26	0.00	0.00	22.3
2	60	1821	1095	-106	0	-481	-958	4.02	4.02	4.02	4.02	2	0.15	0.03	0.19	0.00	0.00	22.3
3	60	1634	1157	-82	0	-417	-1139	4.02	4.02	4.02	4.02	2	0.18	0.03	0.21	0.00	0.00	22.3
4	60	1676	1094	-104	0	-423	-953	4.02	4.02	4.02	4.02	2	0.15	0.03	0.19	0.00	0.00	22.3
5	60	1489	1156	-81	0	-359	-1133	4.02	4.02	4.02	4.02	2	0.18	0.03	0.21	0.00	0.00	22.3
6	60	1989	1022	-132	0	-535	-746	4.02	4.02	4.02	4.02	2	0.16	0.03	0.18	0.00	0.00	22.3
7	60	1364	1230	-54	0	-323	-1349	4.02	4.02	4.02	4.02	2	0.21	0.04	0.22	0.00	0.00	22.3
8	60	1946	1021	-132	0	-517	-744	4.02	4.02	4.02	4.02	2	0.15	0.03	0.18	0.00	0.00	22.3

9	60	1321	1229	-54	0	-305	-1346	4.02	4.02	4.02	4.02	2	0.21	0.04	0.22	0.00	0.00	22.3
10	60	1821	1095	-106	0	-481	-958	4.02	4.02	4.02	4.02	2	0.15	0.03	0.19	0.00	0.00	22.3
11	60	1634	1157	-82	0	-417	-1139	4.02	4.02	4.02	4.02	2	0.18	0.03	0.21	0.00	0.00	22.3
12	60	1676	1094	-104	0	-423	-953	4.02	4.02	4.02	4.02	2	0.15	0.03	0.19	0.00	0.00	22.3
13	60	1489	1156	-81	0	-359	-1133	4.02	4.02	4.02	4.02	2	0.18	0.03	0.21	0.00	0.00	22.3
14	60	1989	1022	-132	0	-535	-746	4.02	4.02	4.02	4.02	2	0.16	0.03	0.18	0.00	0.00	22.3
15	60	1364	1230	-54	0	-323	-1349	4.02	4.02	4.02	4.02	2	0.21	0.04	0.22	0.00	0.00	22.3
16	60	1946	1021	-132	0	-517	-744	4.02	4.02	4.02	4.02	2	0.15	0.03	0.18	0.00	0.00	22.3
17	60	1321	1229	-54	0	-305	-1346	4.02	4.02	4.02	4.02	2	0.21	0.04	0.22	0.00	0.00	22.3
18	60	5081	1340	-244	0	-1193	-1014	4.02	4.02	4.02	4.02	3	0.34	0.04	0.24	0.00	0.00	22.3
19	60	4387	1357	-211	0	-875	-1056	4.02	4.02	4.02	4.02	3	0.24	0.04	0.24	0.00	0.00	22.3
20	60	4665	1464	-155	0	-807	-1366	4.02	4.02	4.02	4.02	3	0.23	0.04	0.26	0.00	0.00	22.3
37	60	4463	1372	-221	0	-1140	-1107	4.02	4.02	4.02	4.02	3	0.32	0.04	0.24	0.00	0.00	22.3
38	60	3308	1400	-165	0	-609	-1178	4.02	4.02	4.02	4.02	3	0.19	0.04	0.25	0.00	0.00	22.3
39	60	3771	1578	-73	0	-498	-1694	4.02	4.02	4.02	4.02	3	0.27	0.05	0.28	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	120	2151	1067	-121	0	-473	680	4.02	4.02	4.02	4.02	3	0.12	0.03	0.19	0.00	0.00	22.3
2	120	1821	791	-106	0	-417	562	4.02	4.02	4.02	4.02	2	0.12	0.02	0.14	0.00	0.00	22.3
3	120	1634	853	-82	0	-368	481	4.02	4.02	4.02	4.02	2	0.11	0.02	0.15	0.00	0.00	22.3
4	120	1676	790	-104	0	-360	565	4.02	4.02	4.02	4.02	2	0.11	0.02	0.14	0.00	0.00	22.3
5	120	1489	852	-81	0	-311	485	4.02	4.02	4.02	4.02	2	0.09	0.02	0.15	0.00	0.00	22.3
6	120	1989	718	-132	0	-455	657	4.02	4.02	4.02	4.02	2	0.13	0.02	0.13	0.00	0.00	22.3
7	120	1364	926	-54	0	-290	-548	4.02	4.02	4.02	4.02	2	0.09	0.03	0.16	0.00	0.00	22.3
8	120	1946	717	-132	0	-438	657	4.02	4.02	4.02	4.02	2	0.13	0.02	0.13	0.00	0.00	22.3
9	120	1321	925	-54	0	-273	-546	4.02	4.02	4.02	4.02	2	0.09	0.03	0.16	0.00	0.00	22.3
10	120	1821	791	-106	0	-417	562	4.02	4.02	4.02	4.02	2	0.12	0.02	0.14	0.00	0.00	22.3
11	120	1634	853	-82	0	-368	481	4.02	4.02	4.02	4.02	2	0.11	0.02	0.15	0.00	0.00	22.3
12	120	1676	790	-104	0	-360	565	4.02	4.02	4.02	4.02	2	0.11	0.02	0.14	0.00	0.00	22.3
13	120	1489	852	-81	0	-311	485	4.02	4.02	4.02	4.02	2	0.09	0.02	0.15	0.00	0.00	22.3
14	120	1989	718	-132	0	-455	657	4.02	4.02	4.02	4.02	2	0.13	0.02	0.13	0.00	0.00	22.3
15	120	1364	926	-54	0	-290	-548	4.02	4.02	4.02	4.02	2	0.09	0.03	0.16	0.00	0.00	22.3
16	120	1946	717	-132	0	-438	657	4.02	4.02	4.02	4.02	2	0.13	0.02	0.13	0.00	0.00	22.3
17	120	1321	925	-54	0	-273	-546	4.02	4.02	4.02	4.02	2	0.09	0.03	0.16	0.00	0.00	22.3
18	120	5081	944	-244	0	-1046	828	4.02	4.02	4.02	4.02	3	0.30	0.03	0.17	0.00	0.00	22.3
19	120	4387	961	-211	0	-748	813	4.02	4.02	4.02	4.02	3	0.21	0.03	0.17	0.00	0.00	22.3
20	120	4665	1068	-155	0	-714	675	4.02	4.02	4.02	4.02	3	0.20	0.03	0.19	0.00	0.00	22.3
37	120	4463	977	-221	0	-1008	787	4.02	4.02	4.02	4.02	3	0.28	0.03	0.17	0.00	0.00	22.3
38	120	3308	1005	-165	0	-511	761	4.02	4.02	4.02	4.02	3	0.14	0.03	0.18	0.00	0.00	22.3
39	120	3771	1182	-73	0	-454	-666	4.02	4.02	4.02	4.02	3	0.12	0.03	0.21	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	180	2151	672	-121	0	-401	993	4.02	4.02	4.02	4.02	3	0.15	0.02	0.12	0.00	0.00	22.3
2	180	1821	486	-106	0	-354	764	4.02	4.02	4.02	4.02	2	0.12	0.01	0.09	0.00	0.00	22.3
3	180	1634	548	-82	0	-319	748	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
4	180	1676	485	-104	0	-298	765	4.02	4.02	4.02	4.02	2	0.12	0.01	0.09	0.00	0.00	22.3
5	180	1489	547	-81	0	-262	751	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
6	180	1989	413	-132	0	-376	789	4.02	4.02	4.02	4.02	2	0.13	0.01	0.07	0.00	0.00	22.3
7	180	1364	621	-54	0	-258	699	4.02	4.02	4.02	4.02	2	0.11	0.02	0.11	0.00	0.00	22.3
8	180	1946	412	-132	0	-359	790	4.02	4.02	4.02	4.02	2	0.13	0.01	0.07	0.00	0.00	22.3
9	180	1321	620	-54	0	-241	700	4.02	4.02	4.02	4.02	2	0.11	0.02	0.11	0.00	0.00	22.3
10	180	1821	486	-106	0	-354	764	4.02	4.02	4.02	4.02	2	0.12	0.01	0.09	0.00	0.00	22.3
11	180	1634	548	-82	0	-319	748	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
12	180	1676	485	-104	0	-298	765	4.02	4.02	4.02	4.02	2	0.12	0.01	0.09	0.00	0.00	22.3
13	180	1489	547	-81	0	-262	751	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
14	180	1989	413	-132	0	-376	789	4.02	4.02	4.02	4.02	2	0.13	0.01	0.07	0.00	0.00	22.3
15	180	1364	621	-54	0	-258	699	4.02	4.02	4.02	4.02	2	0.11	0.02	0.11	0.00	0.00	22.3
16	180	1946	412	-132	0	-359	790	4.02	4.02	4.02	4.02	2	0.13	0.01	0.07	0.00	0.00	22.3
17	180	1321	620	-54	0	-241	700	4.02	4.02	4.02	4.02	2	0.11	0.02	0.11	0.00	0.00	22.3
18	180	5081	549	-244	0	-900	1009	4.02	4.02	4.02	4.02	3	0.26	0.02	0.10	0.00	0.00	22.3
19	180	4387	566	-211	0	-622	1006	4.02	4.02	4.02	4.02	3	0.17	0.02	0.10	0.00	0.00	22.3
20	180	4665	672	-155	0	-621	988	4.02	4.02	4.02	4.02	3	0.17	0.02	0.12	0.00	0.00	22.3
37	180	4463	581	-221	0	-875	990	4.02	4.02	4.02	4.02	3	0.24	0.02	0.10	0.00	0.00	22.3
38	180	3308	609	-165	0	-412	994	4.02	4.02	4.02	4.02	3	0.16	0.02	0.11	0.00	0.00	22.3
39	180	3771	787	-73	0	-411	921	4.02	4.02	4.02	4.02	3	0.15	0.02	0.14	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	240	2151	276	-121	0	-328	993	4.02	4.02	4.02	4.02	3	0.15	0.01	0.05	0.00	0.00	22.3
2	240	1821	182	-106	0	-291	764	4.02	4.02	4.02	4.02	2	0.12	0.01	0.03	0.00	0.00	22.3
3	240	1634	244	-82	0	-270	764	4.02	4.02	4.02	4.02	2	0.12	0.01	0.04	0.00	0.00	22.3
4	240	1676	181	-104	0	-235	765	4.02	4.02	4.02	4.02	2	0.12	0.01	0.03	0.00	0.00	22.3
5	240	1489	243	-81	0	-214	766	4.02	4.02	4.02	4.02	2	0.12	0.01	0.04	0.00	0.00	22.3
6	240	1989	109	-132	0	-296	789	4.02	4.02	4.02	4.02	2	0.13	0.00	0.02	0.00	0.00	22.3
7	240	1364	317	-54	0	-225	765	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
8	240	1946	108	-132	0	-279	790	4.02	4.02	4.02	4.02	2	0.13	0.00	0.02	0.00	0.00	22.3
9	240	1321	316	-54	0	-209	766	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
10	240	1821	182	-106	0	-291	764	4.02	4.02	4.02	4.02	2	0.12	0.01	0.03	0.00	0.00	22.3
11	240	1634	244	-82	0	-270	764	4.02	4.02	4.02	4.02	2	0.12	0.01	0.04	0.00	0.00	22.3
12	240	1676	181	-104	0	-235	765	4.02	4.02	4.02	4.02	2	0.12	0.01	0.03	0.00	0.00	22.3
13	240	1489	243	-81	0	-214	766	4.02	4.02	4.02	4.02	2	0.12	0.01	0.04	0.00	0.00	22.3
14	240	1989	109	-132	0	-296	789	4.02	4.02	4.02	4.02	2	0.13	0.00	0.02	0.00	0.00	22.3
15	240	1364	317	-54	0	-225	765	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
16	240	1946	108	-132	0	-279	790	4.02	4.02	4.02	4.02	2	0.13	0.00	0.02	0.00	0.00	22.3
17	240	1321	316	-54	0	-209	766	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
18	240	5081	153	-244	0	-753	1009	4.02	4.02	4.02	4.02	3	0.21	0.01	0.04	0.00	0.00	22.3
19	240	4387	170	-211	0	-495	1006	4.02	4.02	4.02	4.02	3	0.17	0.01	0.03	0.00	0.00	22.3
20	240	4665	277	-155	0	-528	988	4.02	4.02	4.02	4.02	3	0.16	0.01	0.05	0.00	0.00	22.3
37	240	4463	186	-221	0	-742	990	4.02	4.02	4.02	4.02	3	0.21	0.01	0.04	0.00	0.00	22.3
38	240	3308	214	-165	0	-313	994	4.02	4.02	4.02	4.02	3	0.16	0.01	0.04	0.00	0.00	22.3
39	240	3771	391	-73	0	-367	992	4.02	4.02	4.02	4.02	3	0.16	0.01	0.07	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	300	2151	-119	-121	0	-255	993	4.02	4.02	4.02	4.02	3	0.15	0.00	0.02	0.00	0.00	22.3
2	300	1821	-122	-106	0	-227	764	4.02	4.02	4.02	4.02	2	0.12	0.00	0.02	0.00	0.00	22.3
3	300	1634	-60	-82	0	-220	764	4.02	4.02	4.02	4.02	2	0.12	0.00	0.01	0.00	0.00	22.3
4	300	1676	-123	-104	0	-173	765	4.02	4.02	4.02	4.02	2	0.12	0.00	0.02	0.00	0.00	22.3
5	300	1489	-61	-81	0	-165	766	4.02	4.02	4.02	4.02	2	0.12	0.00	0.01	0.00	0.00	22.3
6	300	1989	-195	-132	0	-217	789	4.02	4.02	4.02	4.02	2	0.13	0.01	0.03	0.00	0.00	22.3
7	300	1364	13	-54	0	-193	765	4.02	4.02	4.02	4.02	2	0.12	0.00	0.00	0.00	0.00	22.3
8	300	1946	-196	-132	0	-200	790	4.02	4.02	4.02	4.02	2	0.13	0.01	0.03	0.00	0.00	22.3
9	300	1321	12	-54	0	-176	766	4.02	4.02	4.02	4.02	2	0.12	0.00	0.00	0.00	0.00	22.3
10	300	1821	-122	-106	0	-227	764	4.02	4.02	4.02	4.02	2	0.12	0.00	0.02	0.00	0.00	22.3
11	300	1634	-60	-82	0	-220	764	4.02	4.02	4.02	4.02	2	0.12	0.00	0.01	0.00	0.00	22.3
12	300	1676	-123	-104	0	-173	765	4.02	4.02	4.02	4.02	2	0.12	0.00	0.02	0.00	0.00	22.3
13	300	1489	-61	-81	0	-165	766	4.02	4.02	4.02	4.02	2	0.12	0.00	0.01	0.00	0.00	22.3
14	300	1989	-195	-132	0	-217	789	4.02	4.02	4.02	4.02	2	0.13	0.01	0.03	0.00	0.00	22.3

15	300	1364	13	-54	0	-193	765	4.02	4.02	4.02	4.02	2	0.12	0.00	0.00	0.00	0.00	22.3
16	300	1946	-196	-132	0	-200	790	4.02	4.02	4.02	4.02	2	0.13	0.01	0.03	0.00	0.00	22.3
17	300	1321	12	-54	0	-176	766	4.02	4.02	4.02	4.02	2	0.12	0.00	0.00	0.00	0.00	22.3
18	300	5081	-242	-244	0	-606	1009	4.02	4.02	4.02	4.02	3	0.17	0.01	0.04	0.00	0.00	22.3
19	300	4387	-225	-211	0	-369	1006	4.02	4.02	4.02	4.02	3	0.17	0.01	0.04	0.00	0.00	22.3
20	300	4665	-119	-155	0	-434	988	4.02	4.02	4.02	4.02	3	0.16	0.00	0.03	0.00	0.00	22.3
37	300	4463	-210	-221	0	-610	990	4.02	4.02	4.02	4.02	3	0.17	0.01	0.04	0.00	0.00	22.3
38	300	3308	-182	-165	0	-214	994	4.02	4.02	4.02	4.02	3	0.16	0.01	0.03	0.00	0.00	22.3
39	300	3771	-4	-73	0	-323	992	4.02	4.02	4.02	4.02	3	0.16	0.00	0.00	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	360	2151	-514	-121	0	-183	993	4.02	4.02	4.02	4.02	3	0.15	0.01	0.09	0.00	0.00	22.3
2	360	1821	-426	-106	0	-164	764	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
3	360	1634	-364	-82	0	-171	764	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
4	360	1676	-427	-104	0	-110	765	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
5	360	1489	-365	-81	0	-117	766	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
6	360	1989	-499	-132	0	-137	789	4.02	4.02	4.02	4.02	2	0.13	0.01	0.09	0.00	0.00	22.3
7	360	1364	-291	-54	0	-160	765	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
8	360	1946	-500	-132	0	-121	790	4.02	4.02	4.02	4.02	2	0.13	0.01	0.09	0.00	0.00	22.3
9	360	1321	-292	-54	0	-144	766	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
10	360	1821	-426	-106	0	-164	764	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
11	360	1634	-364	-82	0	-171	764	4.02	4.02	4.02	4.02	2	0.12	0.01	0.06	0.00	0.00	22.3
12	360	1676	-427	-104	0	-110	765	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
13	360	1489	-365	-81	0	-117	766	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
14	360	1989	-499	-132	0	-137	789	4.02	4.02	4.02	4.02	2	0.13	0.01	0.09	0.00	0.00	22.3
15	360	1364	-291	-54	0	-160	765	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
16	360	1946	-500	-132	0	-121	790	4.02	4.02	4.02	4.02	2	0.13	0.01	0.09	0.00	0.00	22.3
17	360	1321	-292	-54	0	-144	766	4.02	4.02	4.02	4.02	2	0.12	0.01	0.05	0.00	0.00	22.3
18	360	5081	-637	-244	0	-459	1009	4.02	4.02	4.02	4.02	3	0.17	0.02	0.11	0.00	0.00	22.3
19	360	4387	-620	-211	0	-242	1006	4.02	4.02	4.02	4.02	3	0.17	0.02	0.11	0.00	0.00	22.3
20	360	4665	-514	-155	0	-341	988	4.02	4.02	4.02	4.02	3	0.16	0.01	0.09	0.00	0.00	22.3
37	360	4463	-605	-221	0	-477	990	4.02	4.02	4.02	4.02	3	0.16	0.02	0.11	0.00	0.00	22.3
38	360	3308	-577	-165	0	-115	994	4.02	4.02	4.02	4.02	3	0.16	0.02	0.10	0.00	0.00	22.3
39	360	3771	-399	-73	0	-280	992	4.02	4.02	4.02	4.02	3	0.16	0.01	0.07	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	420	2151	-910	-121	0	-110	837	4.02	4.02	4.02	4.02	3	0.13	0.03	0.16	0.00	0.00	22.3
2	420	1821	-730	-106	0	-101	622	4.02	4.02	4.02	4.02	2	0.10	0.02	0.13	0.00	0.00	22.3
3	420	1634	-668	-82	0	-122	665	4.02	4.02	4.02	4.02	2	0.11	0.02	0.12	0.00	0.00	22.3
4	420	1676	-731	-104	0	-47	622	4.02	4.02	4.02	4.02	2	0.10	0.02	0.13	0.00	0.00	22.3
5	420	1489	-669	-81	0	-68	666	4.02	4.02	4.02	4.02	2	0.11	0.02	0.12	0.00	0.00	22.3
6	420	1989	-803	-132	0	-58	571	4.02	4.02	4.02	4.02	2	0.09	0.02	0.14	0.00	0.00	22.3
7	420	1364	-595	-54	0	-128	716	4.02	4.02	4.02	4.02	2	0.11	0.02	0.11	0.00	0.00	22.3
8	420	1946	-804	-132	0	-42	571	4.02	4.02	4.02	4.02	2	0.09	0.02	0.14	0.00	0.00	22.3
9	420	1321	-596	-54	0	-112	717	4.02	4.02	4.02	4.02	2	0.11	0.02	0.11	0.00	0.00	22.3
10	420	1821	-730	-106	0	-101	622	4.02	4.02	4.02	4.02	2	0.10	0.02	0.13	0.00	0.00	22.3
11	420	1634	-668	-82	0	-122	665	4.02	4.02	4.02	4.02	2	0.11	0.02	0.12	0.00	0.00	22.3
12	420	1676	-731	-104	0	-47	622	4.02	4.02	4.02	4.02	2	0.10	0.02	0.13	0.00	0.00	22.3
13	420	1489	-669	-81	0	-68	666	4.02	4.02	4.02	4.02	2	0.11	0.02	0.12	0.00	0.00	22.3
14	420	1989	-803	-132	0	-58	571	4.02	4.02	4.02	4.02	2	0.09	0.02	0.14	0.00	0.00	22.3
15	420	1364	-595	-54	0	-128	716	4.02	4.02	4.02	4.02	2	0.11	0.02	0.11	0.00	0.00	22.3
16	420	1946	-804	-132	0	-42	571	4.02	4.02	4.02	4.02	2	0.09	0.02	0.14	0.00	0.00	22.3
17	420	1321	-596	-54	0	-112	717	4.02	4.02	4.02	4.02	2	0.11	0.02	0.11	0.00	0.00	22.3
18	420	5081	-1033	-244	0	-313	741	4.02	4.02	4.02	4.02	3	0.12	0.03	0.18	0.00	0.00	22.3
19	420	4387	-1016	-211	0	-116	759	4.02	4.02	4.02	4.02	3	0.12	0.03	0.18	0.00	0.00	22.3
20	420	4665	-910	-155	0	-248	832	4.02	4.02	4.02	4.02	3	0.14	0.03	0.16	0.00	0.00	22.3
37	420	4463	-1000	-221	0	-344	763	4.02	4.02	4.02	4.02	3	0.13	0.03	0.18	0.00	0.00	22.3
38	420	3308	-972	-165	0	-16	794	4.02	4.02	4.02	4.02	3	0.13	0.03	0.17	0.00	0.00	22.3
39	420	3771	-795	-73	0	-236	915	4.02	4.02	4.02	4.02	3	0.15	0.02	0.14	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	480	2151	-1305	-121	0	-37	-949	4.02	4.02	4.02	4.02	3	0.15	0.04	0.23	0.00	0.00	22.3
2	480	1821	-1035	-106	0	-38	-801	4.02	4.02	4.02	4.02	2	0.13	0.03	0.18	0.00	0.00	22.3
3	480	1634	-973	-82	0	-73	-658	4.02	4.02	4.02	4.02	2	0.10	0.03	0.17	0.00	0.00	22.3
4	480	1676	-1036	-104	0	15	-803	4.02	4.02	4.02	4.02	2	0.13	0.03	0.18	0.00	0.00	22.3
5	480	1489	-974	-81	0	-20	-659	4.02	4.02	4.02	4.02	2	0.10	0.03	0.17	0.00	0.00	22.3
6	480	1989	-1108	-133	0	22	-970	4.02	4.02	4.02	4.02	2	0.16	0.03	0.20	0.00	0.00	22.3
7	480	1364	-900	-54	0	-95	-489	4.02	4.02	4.02	4.02	2	0.08	0.03	0.16	0.00	0.00	22.3
8	480	1946	-1109	-132	0	38	-971	4.02	4.02	4.02	4.02	2	0.16	0.03	0.20	0.00	0.00	22.3
9	480	1321	-901	-54	0	-79	-490	4.02	4.02	4.02	4.02	2	0.08	0.03	0.16	0.00	0.00	22.3
10	480	1821	-1035	-106	0	-38	-801	4.02	4.02	4.02	4.02	2	0.13	0.03	0.18	0.00	0.00	22.3
11	480	1634	-973	-82	0	-73	-658	4.02	4.02	4.02	4.02	2	0.10	0.03	0.17	0.00	0.00	22.3
12	480	1676	-1036	-104	0	15	-803	4.02	4.02	4.02	4.02	2	0.13	0.03	0.18	0.00	0.00	22.3
13	480	1489	-974	-81	0	-20	-659	4.02	4.02	4.02	4.02	2	0.10	0.03	0.17	0.00	0.00	22.3
14	480	1989	-1108	-133	0	22	-970	4.02	4.02	4.02	4.02	2	0.16	0.03	0.20	0.00	0.00	22.3
15	480	1364	-900	-54	0	-95	-489	4.02	4.02	4.02	4.02	2	0.08	0.03	0.16	0.00	0.00	22.3
16	480	1946	-1109	-132	0	38	-971	4.02	4.02	4.02	4.02	2	0.16	0.03	0.20	0.00	0.00	22.3
17	480	1321	-901	-54	0	-79	-490	4.02	4.02	4.02	4.02	2	0.08	0.03	0.16	0.00	0.00	22.3
18	480	5081	-1428	-244	0	-166	-1244	4.02	4.02	4.02	4.02	3	0.21	0.04	0.25	0.00	0.00	22.3
19	480	4387	-1411	-211	0	10	-1197	4.02	4.02	4.02	4.02	3	0.20	0.04	0.25	0.00	0.00	22.3
20	480	4665	-1305	-155	0	-155	-953	4.02	4.02	4.02	4.02	3	0.16	0.04	0.23	0.00	0.00	22.3
37	480	4463	-1396	-221	0	-212	-1170	4.02	4.02	4.02	4.02	3	0.19	0.04	0.25	0.00	0.00	22.3
38	480	3308	-1368	-165	0	83	-1093	4.02	4.02	4.02	4.02	3	0.17	0.04	0.24	0.00	0.00	22.3
39	480	3771	-1190	-73	0	-193	-685	4.02	4.02	4.02	4.02	3	0.11	0.03	0.21	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	540	2151	-1701	-121	0	35	-2051	4.02	4.02	4.02	4.02	3	0.31	0.05	0.30	0.00	0.00	22.3
2	540	1821	-1339	-106	0	26	-1667	4.02	4.02	4.02	4.02	2	0.27	0.04	0.24	0.00	0.00	22.3
3	540	1634	-1277	-82	0	-23	-1486	4.02	4.02	4.02	4.02	2	0.24	0.04	0.23	0.00	0.00	22.3
4	540	1676	-1340	-104	0	78	-1670	4.02	4.02	4.02	4.02	2	0.27	0.04	0.24	0.00	0.00	22.3
5	540	1489	-1278	-81	0	28	-1488	4.02	4.02	4.02	4.02	2	0.24	0.04	0.23	0.00	0.00	22.3
6	540	1989	-1412	-132	0	101	-1880	4.02	4.02	4.02	4.02	2	0.30	0.04	0.25	0.00	0.00	22.3
7	540	1364	-1204	-54	0	-63	-1275	4.02	4.02	4.02	4.02	2	0.20	0.03	0.21	0.00	0.00	22.3
8	540	1946	-1413	-132	0	117	-1881	4.02	4.02	4.02	4.02	2	0.30	0.04	0.25	0.00	0.00	22.3
9	540	1321	-1205	-54	0	-47	-1275	4.02	4.02	4.02	4.02	2	0.20	0.03	0.21	0.00	0.00	22.3
10	540	1821	-1339	-106	0	26	-1667	4.02	4.02	4.02	4.02	2	0.27	0.04	0.24	0.00	0.00	22.3
11	540	1634	-1277	-82	0	-23	-1486	4.02	4.02	4.02	4.02	2	0.24	0.04	0.23	0.00	0.00	22.3
12	540	1676	-1340	-104	0	78	-1670	4.02	4.02	4.02	4.02	2	0.27	0.04	0.24	0.00	0.00	22.3
13	540	1489	-1278	-81	0	28	-1488	4.02	4.02	4.02	4.02	2	0.24	0.04	0.23	0.00	0.00	22.3
14	540	1989	-1412	-132	0	101	-1880	4.02	4.02	4.02	4.02	2	0.30	0.04	0.25	0.00	0.00	22.3
15	540	1364	-1204	-54	0	-63	-1275	4.02	4.02	4.02	4.02	2	0.20	0.03	0.21	0.00	0.00	22.3
16	540	1946	-1413	-132	0	117	-1881	4.02	4.02	4.02	4.02	2	0.30	0.04	0.25	0.00	0.00	22.3
17	540	1321	-1205	-54	0	-47	-1275	4.02	4.02	4.02	4.02	2	0.20	0.03	0.21	0.00	0.00	22.3
18	540	5081	-1824	-244	0	-19	-2419	4.02	4.02	4.02	4.02	3	0.41	0.05	0.32	0.00	0.00	22.3
19	540	4387	-1807	-211	0	137	-2363	4.02	4.02	4.02	4.02	3	0.39	0.05	0.32	0.00	0.00	22.3
20	540	4665	-1700	-155	0	-61	-2055	4.02	4.02	4.02	4.02	3	0.34	0.05	0.30	0.00	0.00	22.3

37	540	4463	-1791	-221	0	-79	-2326	4.02	4.02	4.02	4.02	3	0.38	0.05	0.32	0.00	0.00	22.3
38	540	3308	-1764	-165	0	181	-2232	4.02	4.02	4.02	4.02	3	0.35	0.05	0.31	0.00	0.00	22.3
39	540	3771	-1586	-73	0	-149	-1718	4.02	4.02	4.02	4.02	3	0.28	0.05	0.28	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	600	2151	-2096	-121	0	108	-2329	4.02	4.02	4.02	4.02	3	0.36	0.06	0.37	0.00	0.00	22.3
2	600	1821	-1643	-106	0	89	-1884	4.02	4.02	4.02	4.02	2	0.30	0.05	0.29	0.00	0.00	22.3
3	600	1634	-1581	-82	0	26	-1697	4.02	4.02	4.02	4.02	2	0.27	0.05	0.28	0.00	0.00	22.3
4	600	1676	-1644	-104	0	140	-1887	4.02	4.02	4.02	4.02	2	0.30	0.05	0.29	0.00	0.00	22.3
5	600	1489	-1582	-81	0	77	-1699	4.02	4.02	4.02	4.02	2	0.27	0.05	0.28	0.00	0.00	22.3
6	600	1989	-1716	-132	0	181	-2104	4.02	4.02	4.02	4.02	2	0.34	0.05	0.31	0.00	0.00	22.3
7	600	1364	-1508	-54	0	-30	-1479	4.02	4.02	4.02	4.02	2	0.23	0.04	0.27	0.00	0.00	22.3
8	600	1946	-1717	-132	0	196	-2105	4.02	4.02	4.02	4.02	2	0.34	0.05	0.31	0.00	0.00	22.3
9	600	1321	-1509	-54	0	-15	-1479	4.02	4.02	4.02	4.02	2	0.23	0.04	0.27	0.00	0.00	22.3
10	600	1821	-1643	-106	0	89	-1884	4.02	4.02	4.02	4.02	2	0.30	0.05	0.29	0.00	0.00	22.3
11	600	1634	-1581	-82	0	26	-1697	4.02	4.02	4.02	4.02	2	0.27	0.05	0.28	0.00	0.00	22.3
12	600	1676	-1644	-104	0	140	-1887	4.02	4.02	4.02	4.02	2	0.30	0.05	0.29	0.00	0.00	22.3
13	600	1489	-1582	-81	0	77	-1699	4.02	4.02	4.02	4.02	2	0.27	0.05	0.28	0.00	0.00	22.3
14	600	1989	-1716	-132	0	181	-2104	4.02	4.02	4.02	4.02	2	0.34	0.05	0.31	0.00	0.00	22.3
15	600	1364	-1508	-54	0	-30	-1479	4.02	4.02	4.02	4.02	2	0.23	0.04	0.27	0.00	0.00	22.3
16	600	1946	-1717	-132	0	196	-2105	4.02	4.02	4.02	4.02	2	0.34	0.05	0.31	0.00	0.00	22.3
17	600	1321	-1509	-54	0	-15	-1479	4.02	4.02	4.02	4.02	2	0.23	0.04	0.27	0.00	0.00	22.3
18	600	5081	-2219	-244	0	128	-2709	4.02	4.02	4.02	4.02	3	0.46	0.06	0.40	0.00	0.00	22.3
19	600	4387	-2202	-211	0	263	-2651	4.02	4.02	4.02	4.02	3	0.44	0.06	0.39	0.00	0.00	22.3
20	600	4665	-2096	-155	0	32	-2333	4.02	4.02	4.02	4.02	3	0.39	0.06	0.37	0.00	0.00	22.3
37	600	4463	-2187	-221	0	54	-2613	4.02	4.02	4.02	4.02	3	0.43	0.06	0.39	0.00	0.00	22.3
38	600	3308	-2159	-165	0	280	-2516	4.02	4.02	4.02	4.02	3	0.40	0.06	0.38	0.00	0.00	22.3
39	600	3771	-1981	-73	0	-106	-1986	4.02	4.02	4.02	4.02	3	0.32	0.06	0.35	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

Nome travata: **Trave_404_IP1** Descrizione: **Trave_4 32-25**
ASTA NUM. 19 NI 257 NF 258 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y Permanente qy tot.
qy medio: 375.00 132.00 507.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	1944	1790	-623	0	-2093	-1443	4.02	4.02	4.02	4.02	3	0.54	0.05	0.32	0.00	0.00	22.3
2	0	1620	1343	-546	0	-1831	-1012	4.02	4.02	4.02	4.02	2	0.53	0.04	0.24	0.00	0.00	22.3
3	0	1489	1410	-523	0	-1768	-1209	4.02	4.02	4.02	4.02	2	0.51	0.04	0.25	0.00	0.00	22.3
4	0	1502	1344	-435	0	-1452	-1011	4.02	4.02	4.02	4.02	2	0.42	0.04	0.24	0.00	0.00	22.3
5	0	1372	1411	-412	0	-1389	-1209	4.02	4.02	4.02	4.02	2	0.40	0.04	0.25	0.00	0.00	22.3
6	0	1730	1265	-534	0	-1772	-781	4.02	4.02	4.02	4.02	2	0.52	0.04	0.23	0.00	0.00	22.3
7	0	1296	1488	-458	0	-1562	-1440	4.02	4.02	4.02	4.02	2	0.45	0.04	0.27	0.00	0.00	22.3
8	0	1695	1265	-501	0	-1659	-781	4.02	4.02	4.02	4.02	2	0.48	0.04	0.23	0.00	0.00	22.3
9	0	1261	1488	-425	0	-1448	-1439	4.02	4.02	4.02	4.02	2	0.42	0.04	0.27	0.00	0.00	22.3
10	0	1620	1343	-546	0	-1831	-1012	4.02	4.02	4.02	4.02	2	0.53	0.04	0.24	0.00	0.00	22.3
11	0	1489	1410	-523	0	-1768	-1209	4.02	4.02	4.02	4.02	2	0.51	0.04	0.25	0.00	0.00	22.3
12	0	1502	1344	-435	0	-1452	-1011	4.02	4.02	4.02	4.02	2	0.42	0.04	0.24	0.00	0.00	22.3
13	0	1372	1411	-412	0	-1389	-1209	4.02	4.02	4.02	4.02	2	0.40	0.04	0.25	0.00	0.00	22.3
14	0	1730	1265	-534	0	-1772	-781	4.02	4.02	4.02	4.02	2	0.52	0.04	0.23	0.00	0.00	22.3
15	0	1296	1488	-458	0	-1562	-1440	4.02	4.02	4.02	4.02	2	0.45	0.04	0.27	0.00	0.00	22.3
16	0	1695	1265	-501	0	-1659	-781	4.02	4.02	4.02	4.02	2	0.48	0.04	0.23	0.00	0.00	22.3
17	0	1261	1488	-425	0	-1448	-1439	4.02	4.02	4.02	4.02	2	0.42	0.04	0.27	0.00	0.00	22.3
18	0	4626	1632	-1430	0	-4834	-945	4.02	6.03	4.02	4.02	3	0.92	0.05	0.29	0.00	0.00	22.3
19	0	4431	1699	-951	0	-3179	-1096	4.02	4.02	4.02	4.02	3	0.88	0.05	0.30	0.00	0.00	22.3
20	0	4474	1799	-1046	0	-3555	-1416	4.02	4.02	4.02	4.02	3	0.99	0.05	0.32	0.00	0.00	22.3
37	0	3843	1650	-1406	0	-4763	-1034	4.02	6.03	4.02	4.02	3	0.90	0.05	0.29	0.00	0.00	22.3
38	0	3518	1762	-606	0	-2004	-1285	4.02	4.02	4.02	4.02	3	0.54	0.05	0.31	0.00	0.00	22.3
39	0	3590	1929	-765	0	-2632	-1817	4.02	4.02	4.02	4.02	3	0.71	0.06	0.34	0.00	0.00	22.3

apost= -- aant= 2.01 ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	60	1944	1394	-623	0	-1719	-1194	4.02	4.02	4.02	4.02	3	0.45	0.04	0.25	0.00	0.00	22.3
2	60	1620	1039	-546	0	-1503	-823	4.02	4.02	4.02	4.02	2	0.44	0.03	0.19	0.00	0.00	22.3
3	60	1489	1106	-523	0	-1454	-1014	4.02	4.02	4.02	4.02	2	0.42	0.03	0.20	0.00	0.00	22.3
4	60	1502	1040	-435	0	-1191	-822	4.02	4.02	4.02	4.02	2	0.35	0.03	0.19	0.00	0.00	22.3
5	60	1372	1107	-412	0	-1142	-1014	4.02	4.02	4.02	4.02	2	0.33	0.03	0.20	0.00	0.00	22.3
6	60	1730	961	-534	0	-1452	-600	4.02	4.02	4.02	4.02	2	0.42	0.03	0.17	0.00	0.00	22.3
7	60	1296	1184	-458	0	-1287	-1238	4.02	4.02	4.02	4.02	2	0.37	0.03	0.21	0.00	0.00	22.3
8	60	1695	961	-501	0	-1358	-600	4.02	4.02	4.02	4.02	2	0.40	0.03	0.17	0.00	0.00	22.3
9	60	1261	1184	-425	0	-1193	-1237	4.02	4.02	4.02	4.02	2	0.34	0.03	0.21	0.00	0.00	22.3
10	60	1620	1039	-546	0	-1503	-823	4.02	4.02	4.02	4.02	2	0.44	0.03	0.19	0.00	0.00	22.3
11	60	1489	1106	-523	0	-1454	-1014	4.02	4.02	4.02	4.02	2	0.42	0.03	0.20	0.00	0.00	22.3
12	60	1502	1040	-435	0	-1191	-822	4.02	4.02	4.02	4.02	2	0.35	0.03	0.19	0.00	0.00	22.3
13	60	1372	1107	-412	0	-1142	-1014	4.02	4.02	4.02	4.02	2	0.33	0.03	0.20	0.00	0.00	22.3
14	60	1730	961	-534	0	-1452	-600	4.02	4.02	4.02	4.02	2	0.42	0.03	0.17	0.00	0.00	22.3
15	60	1296	1184	-458	0	-1287	-1238	4.02	4.02	4.02	4.02	2	0.37	0.03	0.21	0.00	0.00	22.3
16	60	1695	961	-501	0	-1358	-600	4.02	4.02	4.02	4.02	2	0.40	0.03	0.17	0.00	0.00	22.3
17	60	1261	1184	-425	0	-1193	-1237	4.02	4.02	4.02	4.02	2	0.34	0.03	0.21	0.00	0.00	22.3
18	60	4626	1236	-1430	0	-3976	-711	4.02	6.03	4.02	4.02	3	0.76	0.04	0.23	0.00	0.00	22.3
19	60	4431	1304	-951	0	-2609	-855	4.02	4.02	4.02	4.02	3	0.73	0.04	0.23	0.00	0.00	22.3
20	60	4474	1404	-1046	0	-2928	-1166	4.02	4.02	4.02	4.02	3	0.82	0.04	0.25	0.00	0.00	22.3
37	60	3843	1255	-1406	0	-3920	-798	4.02	6.03	4.02	4.02	3	0.74	0.04	0.23	0.00	0.00	22.3
38	60	3518	1367	-606	0	-1640	-1038	4.02	4.02	4.02	4.02	3	0.44	0.04	0.24	0.00	0.00	22.3
39	60	3590	1534	-765	0	-2173	-1555	4.02	4.02	4.02	4.02	3	0.59	0.04	0.27	0.00	0.00	22.3

apost= -- aant= 2.01 ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	120	1944	999	-623	0	-1345	736	4.02	4.02	4.02	4.02	3	0.35	0.03	0.18	0.00	0.00	22.3
2	120	1620	735	-546	0	-1176	607	4.02	4.02	4.02	4.02	2	0.34	0.02	0.13	0.00	0.00	22.3
3	120	1489	802	-523	0	-1140	524	4.02	4.02	4.02	4.02	2	0.33	0.02	0.14	0.00	0.00	22.3
4	120	1502	736	-435	0	-930	609	4.02	4.02	4.02	4.02	2	0.27	0.02	0.13	0.00	0.00	22.3
5	120	1372	803	-412	0	-894	525	4.02	4.02	4.02	4.02	2	0.26	0.02	0.14	0.00	0.00	22.3
6	120	1730	657	-534	0	-1131	704	4.02	4.02	4.02	4.02	2	0.33	0.02	0.12	0.00	0.00	22.3
7	120	1296	880	-458	0	-1013	-464	4.02	4.02	4.02	4.02	2	0.29	0.03	0.16	0.00	0.00	22.3
8	120	1695	657	-501	0	-1058	705	4.02	4.02	4.02	4.02	2	0.31	0.02	0.12	0.00	0.00	22.3
9	120	1261	880	-425	0	-939	-463	4.02	4.02	4.02	4.02	2	0.27	0.03	0.16	0.00	0.00	22.3
10	120	1620	735	-546	0	-1176	607	4.02	4.02	4.02	4.02	2	0.34	0.02	0.13	0.00	0.00	22.3
11	120	1489	802	-523	0	-1140	524	4.02	4.02	4.02	4.02	2	0.33	0.02	0.14	0.00	0.00	22.3
12	120	1502	736	-435	0	-930	609	4.02	4.02	4.02	4.02	2	0.27	0.02	0.13	0.00	0.00	22.3

13	120	1372	803	-412	0	-894	525	4.02	4.02	4.02	4.02	2	0.26	0.02	0.14	0.00	0.00	22.3
14	120	1730	657	-534	0	-1131	704	4.02	4.02	4.02	4.02	2	0.33	0.02	0.12	0.00	0.00	22.3
15	120	1296	880	-458	0	-1013	-464	4.02	4.02	4.02	4.02	2	0.29	0.03	0.16	0.00	0.00	22.3
16	120	1695	657	-501	0	-1058	705	4.02	4.02	4.02	4.02	2	0.31	0.02	0.12	0.00	0.00	22.3
17	120	1261	880	-425	0	-939	-463	4.02	4.02	4.02	4.02	2	0.27	0.03	0.16	0.00	0.00	22.3
18	120	4626	841	-1430	0	-3118	964	4.02	4.02	4.02	4.02	3	0.87	0.04	0.23	0.00	0.00	22.3
19	120	4431	908	-951	0	-2038	928	4.02	4.02	4.02	4.02	3	0.57	0.03	0.16	0.00	0.00	22.3
20	120	4474	1008	-1046	0	-2300	779	4.02	4.02	4.02	4.02	3	0.64	0.03	0.18	0.00	0.00	22.3
37	120	3843	859	-1406	0	-3076	907	4.02	4.02	4.02	4.02	3	0.84	0.04	0.23	0.00	0.00	22.3
38	120	3518	971	-606	0	-1276	847	4.02	4.02	4.02	4.02	3	0.35	0.03	0.17	0.00	0.00	22.3
39	120	3590	1138	-765	0	-1714	599	4.02	4.02	4.02	4.02	3	0.47	0.03	0.20	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	180	1944	603	-623	0	-972	960	4.02	4.02	4.02	4.02	3	0.25	0.02	0.11	0.00	0.00	22.3
2	180	1620	430	-546	0	-848	751	4.02	4.02	4.02	4.02	2	0.25	0.02	0.09	0.00	0.00	22.3
3	180	1489	497	-523	0	-826	740	4.02	4.02	4.02	4.02	2	0.24	0.02	0.09	0.00	0.00	22.3
4	180	1502	431	-435	0	-668	754	4.02	4.02	4.02	4.02	2	0.19	0.01	0.08	0.00	0.00	22.3
5	180	1372	498	-412	0	-646	742	4.02	4.02	4.02	4.02	2	0.19	0.01	0.09	0.00	0.00	22.3
6	180	1730	352	-534	0	-811	795	4.02	4.02	4.02	4.02	2	0.24	0.02	0.09	0.00	0.00	22.3
7	180	1296	575	-458	0	-738	709	4.02	4.02	4.02	4.02	2	0.21	0.02	0.10	0.00	0.00	22.3
8	180	1695	352	-501	0	-757	796	4.02	4.02	4.02	4.02	2	0.22	0.02	0.08	0.00	0.00	22.3
9	180	1261	575	-425	0	-684	710	4.02	4.02	4.02	4.02	2	0.20	0.02	0.10	0.00	0.00	22.3
10	180	1620	430	-546	0	-848	751	4.02	4.02	4.02	4.02	2	0.25	0.02	0.09	0.00	0.00	22.3
11	180	1489	497	-523	0	-826	740	4.02	4.02	4.02	4.02	2	0.24	0.02	0.09	0.00	0.00	22.3
12	180	1502	431	-435	0	-668	754	4.02	4.02	4.02	4.02	2	0.19	0.01	0.08	0.00	0.00	22.3
13	180	1372	498	-412	0	-646	742	4.02	4.02	4.02	4.02	2	0.19	0.01	0.09	0.00	0.00	22.3
14	180	1730	352	-534	0	-811	795	4.02	4.02	4.02	4.02	2	0.24	0.02	0.09	0.00	0.00	22.3
15	180	1296	575	-458	0	-738	709	4.02	4.02	4.02	4.02	2	0.21	0.02	0.10	0.00	0.00	22.3
16	180	1695	352	-501	0	-757	796	4.02	4.02	4.02	4.02	2	0.22	0.02	0.08	0.00	0.00	22.3
17	180	1261	575	-425	0	-684	710	4.02	4.02	4.02	4.02	2	0.20	0.02	0.10	0.00	0.00	22.3
18	180	4626	445	-1430	0	-2260	1073	4.02	4.02	4.02	4.02	3	0.63	0.04	0.23	0.00	0.00	22.3
19	180	4431	513	-951	0	-1468	1084	4.02	4.02	4.02	4.02	3	0.41	0.03	0.15	0.00	0.00	22.3
20	180	4474	612	-1046	0	-1672	1015	4.02	4.02	4.02	4.02	3	0.47	0.03	0.17	0.00	0.00	22.3
37	180	3843	464	-1406	0	-2233	1029	4.02	4.02	4.02	4.02	3	0.61	0.04	0.23	0.00	0.00	22.3
38	180	3518	576	-606	0	-913	1047	4.02	4.02	4.02	4.02	3	0.25	0.02	0.10	0.00	0.00	22.3
39	180	3590	743	-765	0	-1255	963	4.02	4.02	4.02	4.02	3	0.34	0.02	0.13	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	240	1944	208	-623	0	-598	960	4.02	4.02	4.02	4.02	3	0.15	0.02	0.10	0.00	0.00	22.3
2	240	1620	126	-546	0	-521	751	4.02	4.02	4.02	4.02	2	0.15	0.02	0.09	0.00	0.00	22.3
3	240	1489	193	-523	0	-512	740	4.02	4.02	4.02	4.02	2	0.15	0.02	0.08	0.00	0.00	22.3
4	240	1502	127	-435	0	-407	754	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
5	240	1372	194	-412	0	-399	742	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
6	240	1730	48	-534	0	-490	795	4.02	4.02	4.02	4.02	2	0.14	0.02	0.09	0.00	0.00	22.3
7	240	1296	271	-458	0	-463	744	4.02	4.02	4.02	4.02	2	0.13	0.01	0.07	0.00	0.00	22.3
8	240	1695	48	-501	0	-457	796	4.02	4.02	4.02	4.02	2	0.13	0.02	0.08	0.00	0.00	22.3
9	240	1261	271	-425	0	-429	745	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
10	240	1620	126	-546	0	-521	751	4.02	4.02	4.02	4.02	2	0.15	0.02	0.09	0.00	0.00	22.3
11	240	1489	193	-523	0	-512	740	4.02	4.02	4.02	4.02	2	0.15	0.02	0.08	0.00	0.00	22.3
12	240	1502	127	-435	0	-407	754	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
13	240	1372	194	-412	0	-399	742	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
14	240	1730	48	-534	0	-490	795	4.02	4.02	4.02	4.02	2	0.14	0.02	0.09	0.00	0.00	22.3
15	240	1296	271	-458	0	-463	744	4.02	4.02	4.02	4.02	2	0.13	0.01	0.07	0.00	0.00	22.3
16	240	1695	48	-501	0	-457	796	4.02	4.02	4.02	4.02	2	0.13	0.02	0.08	0.00	0.00	22.3
17	240	1261	271	-425	0	-429	745	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
18	240	4626	50	-1430	0	-1402	1073	4.02	4.02	4.02	4.02	3	0.39	0.04	0.23	0.00	0.00	22.3
19	240	4431	117	-951	0	-897	1084	4.02	4.02	4.02	4.02	3	0.25	0.03	0.15	0.00	0.00	22.3
20	240	4474	217	-1046	0	-1045	1015	4.02	4.02	4.02	4.02	3	0.29	0.03	0.17	0.00	0.00	22.3
37	240	3843	68	-1406	0	-1390	1029	4.02	4.02	4.02	4.02	3	0.38	0.04	0.23	0.00	0.00	22.3
38	240	3518	180	-606	0	-549	1047	4.02	4.02	4.02	4.02	3	0.17	0.02	0.10	0.00	0.00	22.3
39	240	3590	347	-765	0	-796	1003	4.02	4.02	4.02	4.02	3	0.22	0.02	0.12	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	300	1944	-188	-623	0	-224	960	4.02	4.02	4.02	4.02	3	0.15	0.02	0.10	0.00	0.00	22.3
2	300	1620	-178	-546	0	-193	751	4.02	4.02	4.02	4.02	2	0.12	0.02	0.09	0.00	0.00	22.3
3	300	1489	-111	-523	0	-198	740	4.02	4.02	4.02	4.02	2	0.12	0.02	0.08	0.00	0.00	22.3
4	300	1502	-177	-435	0	-146	754	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
5	300	1372	-110	-412	0	-151	742	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
6	300	1730	-256	-534	0	-170	795	4.02	4.02	4.02	4.02	2	0.13	0.02	0.09	0.00	0.00	22.3
7	300	1296	-33	-458	0	-188	744	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
8	300	1695	-256	-501	0	-156	796	4.02	4.02	4.02	4.02	2	0.13	0.02	0.08	0.00	0.00	22.3
9	300	1261	-33	-425	0	-174	745	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
10	300	1620	-178	-546	0	-193	751	4.02	4.02	4.02	4.02	2	0.12	0.02	0.09	0.00	0.00	22.3
11	300	1489	-111	-523	0	-198	740	4.02	4.02	4.02	4.02	2	0.12	0.02	0.08	0.00	0.00	22.3
12	300	1502	-177	-435	0	-146	754	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
13	300	1372	-110	-412	0	-151	742	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
14	300	1730	-256	-534	0	-170	795	4.02	4.02	4.02	4.02	2	0.13	0.02	0.09	0.00	0.00	22.3
15	300	1296	-33	-458	0	-188	744	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
16	300	1695	-256	-501	0	-156	796	4.02	4.02	4.02	4.02	2	0.13	0.02	0.08	0.00	0.00	22.3
17	300	1261	-33	-425	0	-174	745	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
18	300	4626	-346	-1430	0	-543	1073	4.02	4.02	4.02	4.02	3	0.18	0.04	0.23	0.00	0.00	22.3
19	300	4431	-278	-951	0	-327	1084	4.02	4.02	4.02	4.02	3	0.18	0.03	0.15	0.00	0.00	22.3
20	300	4474	-179	-1046	0	-417	1015	4.02	4.02	4.02	4.02	3	0.17	0.03	0.17	0.00	0.00	22.3
37	300	3843	-327	-1406	0	-546	1029	4.02	4.02	4.02	4.02	3	0.17	0.04	0.23	0.00	0.00	22.3
38	300	3518	-215	-606	0	-185	1047	4.02	4.02	4.02	4.02	3	0.17	0.02	0.10	0.00	0.00	22.3
39	300	3590	-48	-765	0	-337	1003	4.02	4.02	4.02	4.02	3	0.16	0.02	0.12	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	360	1944	-583	-623	0	150	960	4.02	4.02	4.02	4.02	3	0.15	0.02	0.10	0.00	0.00	22.3
2	360	1620	-482	-546	0	135	751	4.02	4.02	4.02	4.02	2	0.12	0.02	0.09	0.00	0.00	22.3
3	360	1489	-415	-523	0	115	740	4.02	4.02	4.02	4.02	2	0.12	0.02	0.08	0.00	0.00	22.3
4	360	1502	-481	-435	0	115	754	4.02	4.02	4.02	4.02	2	0.12	0.01	0.09	0.00	0.00	22.3
5	360	1372	-414	-412	0	96	742	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
6	360	1730	-560	-534	0	150	772	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
7	360	1296	-337	-458	0	86	744	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
8	360	1695	-560	-501	0	144	773	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
9	360	1261	-337	-425	0	80	745	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
10	360	1620	-482	-546	0	135	751	4.02	4.02	4.02	4.02	2	0.12	0.02	0.09	0.00	0.00	22.3
11	360	1489	-415	-523	0	115	740	4.02	4.02	4.02	4.02	2	0.12	0.02	0.08	0.00	0.00	22.3
12	360	1502	-481	-435	0	115	754	4.02	4.02	4.02	4.02	2	0.12	0.01	0.09	0.00	0.00	22.3
13	360	1372	-414	-412	0	96	742	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
14	360	1730	-560	-534	0	150	772	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
15	360	1296	-337	-458	0	86	744	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
16	360	1695	-560	-501	0	144	773	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
17	360	1261	-337	-425	0	80	745	4.02	4.02	4.02	4.02	2	0.12	0.01	0.07	0.00	0.00	22.3
18	360	4626	-741	-1430	0	315	1033	4.02	4.02	4.02	4.02	3	0.17	0.04	0.23	0.00	0.00	22.3

19	360	4431	-673	-951	0	243	1084	4.02	4.02	4.02	4.02	3	0.18	0.03	0.15	0.00	0.00	22.3
20	360	4474	-574	-1046	0	210	1015	4.02	4.02	4.02	4.02	3	0.17	0.03	0.17	0.00	0.00	22.3
37	360	3843	-722	-1406	0	297	1002	4.02	4.02	4.02	4.02	3	0.16	0.04	0.23	0.00	0.00	22.3
38	360	3518	-610	-606	0	179	1047	4.02	4.02	4.02	4.02	3	0.17	0.02	0.11	0.00	0.00	22.3
39	360	3590	-444	-765	0	122	1003	4.02	4.02	4.02	4.02	3	0.16	0.02	0.12	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	420	1944	-978	-623	0	524	756	4.02	4.02	4.02	4.02	3	0.14	0.03	0.17	0.00	0.00	22.3
2	420	1620	-786	-546	0	462	556	4.02	4.02	4.02	4.02	2	0.13	0.02	0.14	0.00	0.00	22.3
3	420	1489	-719	-523	0	429	605	4.02	4.02	4.02	4.02	2	0.12	0.02	0.13	0.00	0.00	22.3
4	420	1502	-785	-435	0	376	558	4.02	4.02	4.02	4.02	2	0.11	0.02	0.14	0.00	0.00	22.3
5	420	1372	-718	-412	0	344	608	4.02	4.02	4.02	4.02	2	0.10	0.02	0.13	0.00	0.00	22.3
6	420	1730	-864	-534	0	471	498	4.02	4.02	4.02	4.02	2	0.14	0.03	0.15	0.00	0.00	22.3
7	420	1296	-641	-458	0	361	664	4.02	4.02	4.02	4.02	2	0.10	0.02	0.11	0.00	0.00	22.3
8	420	1695	-864	-501	0	445	500	4.02	4.02	4.02	4.02	2	0.13	0.03	0.15	0.00	0.00	22.3
9	420	1261	-641	-425	0	335	665	4.02	4.02	4.02	4.02	2	0.10	0.02	0.11	0.00	0.00	22.3
10	420	1620	-786	-546	0	462	556	4.02	4.02	4.02	4.02	2	0.13	0.02	0.14	0.00	0.00	22.3
11	420	1489	-719	-523	0	429	605	4.02	4.02	4.02	4.02	2	0.12	0.02	0.13	0.00	0.00	22.3
12	420	1502	-785	-435	0	376	558	4.02	4.02	4.02	4.02	2	0.11	0.02	0.14	0.00	0.00	22.3
13	420	1372	-718	-412	0	344	608	4.02	4.02	4.02	4.02	2	0.10	0.02	0.13	0.00	0.00	22.3
14	420	1730	-864	-534	0	471	498	4.02	4.02	4.02	4.02	2	0.14	0.03	0.15	0.00	0.00	22.3
15	420	1296	-641	-458	0	361	664	4.02	4.02	4.02	4.02	2	0.10	0.02	0.11	0.00	0.00	22.3
16	420	1695	-864	-501	0	445	500	4.02	4.02	4.02	4.02	2	0.13	0.03	0.15	0.00	0.00	22.3
17	420	1261	-641	-425	0	335	665	4.02	4.02	4.02	4.02	2	0.10	0.02	0.11	0.00	0.00	22.3
18	420	4626	-1136	-1430	0	1173	671	4.02	4.02	4.02	4.02	3	0.33	0.04	0.23	0.00	0.00	22.3
19	420	4431	-1069	-951	0	814	768	4.02	4.02	4.02	4.02	3	0.23	0.03	0.19	0.00	0.00	22.3
20	420	4474	-970	-1046	0	838	817	4.02	4.02	4.02	4.02	3	0.23	0.03	0.17	0.00	0.00	22.3
37	420	3843	-1118	-1406	0	1140	650	4.02	4.02	4.02	4.02	3	0.31	0.04	0.23	0.00	0.00	22.3
38	420	3518	-1006	-606	0	543	813	4.02	4.02	4.02	4.02	3	0.15	0.03	0.18	0.00	0.00	22.3
39	420	3590	-839	-765	0	581	895	4.02	4.02	4.02	4.02	3	0.16	0.02	0.15	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	480	1944	-1374	-623	0	897	-1140	4.02	4.02	4.02	4.02	3	0.23	0.04	0.24	0.00	0.00	22.3
2	480	1620	-1091	-546	0	790	-958	4.02	4.02	4.02	4.02	2	0.23	0.03	0.19	0.00	0.00	22.3
3	480	1489	-1024	-523	0	743	-800	4.02	4.02	4.02	4.02	2	0.22	0.03	0.18	0.00	0.00	22.3
4	480	1502	-1090	-435	0	638	-954	4.02	4.02	4.02	4.02	2	0.18	0.03	0.19	0.00	0.00	22.3
5	480	1372	-1023	-412	0	591	-796	4.02	4.02	4.02	4.02	2	0.17	0.03	0.18	0.00	0.00	22.3
6	480	1730	-1169	-534	0	791	-1141	4.02	4.02	4.02	4.02	2	0.23	0.03	0.21	0.00	0.00	22.3
7	480	1296	-946	-458	0	636	-615	4.02	4.02	4.02	4.02	2	0.18	0.03	0.17	0.00	0.00	22.3
8	480	1695	-1169	-501	0	745	-1139	4.02	4.02	4.02	4.02	2	0.22	0.03	0.21	0.00	0.00	22.3
9	480	1261	-946	-425	0	590	-614	4.02	4.02	4.02	4.02	2	0.17	0.03	0.17	0.00	0.00	22.3
10	480	1620	-1091	-546	0	790	-958	4.02	4.02	4.02	4.02	2	0.23	0.03	0.19	0.00	0.00	22.3
11	480	1489	-1024	-523	0	743	-800	4.02	4.02	4.02	4.02	2	0.22	0.03	0.18	0.00	0.00	22.3
12	480	1502	-1090	-435	0	638	-954	4.02	4.02	4.02	4.02	2	0.18	0.03	0.19	0.00	0.00	22.3
13	480	1372	-1023	-412	0	591	-796	4.02	4.02	4.02	4.02	2	0.17	0.03	0.18	0.00	0.00	22.3
14	480	1730	-1169	-534	0	791	-1141	4.02	4.02	4.02	4.02	2	0.23	0.03	0.21	0.00	0.00	22.3
15	480	1296	-946	-458	0	636	-615	4.02	4.02	4.02	4.02	2	0.18	0.03	0.17	0.00	0.00	22.3
16	480	1695	-1169	-501	0	745	-1139	4.02	4.02	4.02	4.02	2	0.22	0.03	0.21	0.00	0.00	22.3
17	480	1261	-946	-425	0	590	-614	4.02	4.02	4.02	4.02	2	0.17	0.03	0.17	0.00	0.00	22.3
18	480	4626	-1532	-1430	0	2031	-1481	4.02	4.02	4.02	4.02	3	0.57	0.04	0.27	0.00	0.00	22.3
19	480	4431	-1464	-951	0	1384	-1274	4.02	4.02	4.02	4.02	3	0.39	0.04	0.26	0.00	0.00	22.3
20	480	4474	-1365	-1046	0	1465	-1065	4.02	4.02	4.02	4.02	3	0.41	0.04	0.24	0.00	0.00	22.3
37	480	3843	-1513	-1406	0	1983	-1471	4.02	4.02	4.02	4.02	3	0.54	0.04	0.27	0.00	0.00	22.3
38	480	3518	-1401	-606	0	906	-1127	4.02	4.02	4.02	4.02	3	0.25	0.04	0.25	0.00	0.00	22.3
39	480	3590	-1235	-765	0	1040	-778	4.02	4.02	4.02	4.02	3	0.28	0.04	0.22	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	540	1944	-1770	-623	0	1271	-2284	4.02	4.02	4.02	4.02	3	0.35	0.05	0.32	0.00	0.00	22.3
2	540	1620	-1395	-546	0	1117	-1857	4.02	4.02	4.02	4.02	2	0.33	0.04	0.25	0.00	0.00	22.3
3	540	1489	-1328	-523	0	1057	-1659	4.02	4.02	4.02	4.02	2	0.31	0.04	0.24	0.00	0.00	22.3
4	540	1502	-1394	-435	0	899	-1853	4.02	4.02	4.02	4.02	2	0.29	0.04	0.25	0.00	0.00	22.3
5	540	1372	-1327	-412	0	838	-1655	4.02	4.02	4.02	4.02	2	0.26	0.04	0.24	0.00	0.00	22.3
6	540	1730	-1473	-534	0	1112	-2087	4.02	4.02	4.02	4.02	2	0.33	0.04	0.26	0.00	0.00	22.3
7	540	1296	-1250	-458	0	910	-1428	4.02	4.02	4.02	4.02	2	0.26	0.04	0.22	0.00	0.00	22.3
8	540	1695	-1473	-501	0	1046	-2085	4.02	4.02	4.02	4.02	2	0.33	0.04	0.26	0.00	0.00	22.3
9	540	1261	-1250	-425	0	844	-1427	4.02	4.02	4.02	4.02	2	0.24	0.04	0.22	0.00	0.00	22.3
10	540	1620	-1395	-546	0	1117	-1857	4.02	4.02	4.02	4.02	2	0.33	0.04	0.25	0.00	0.00	22.3
11	540	1489	-1328	-523	0	1057	-1659	4.02	4.02	4.02	4.02	2	0.31	0.04	0.24	0.00	0.00	22.3
12	540	1502	-1394	-435	0	899	-1853	4.02	4.02	4.02	4.02	2	0.29	0.04	0.25	0.00	0.00	22.3
13	540	1372	-1327	-412	0	838	-1655	4.02	4.02	4.02	4.02	2	0.26	0.04	0.24	0.00	0.00	22.3
14	540	1730	-1473	-534	0	1112	-2087	4.02	4.02	4.02	4.02	2	0.33	0.04	0.26	0.00	0.00	22.3
15	540	1296	-1250	-458	0	910	-1428	4.02	4.02	4.02	4.02	2	0.26	0.04	0.22	0.00	0.00	22.3
16	540	1695	-1473	-501	0	1046	-2085	4.02	4.02	4.02	4.02	2	0.33	0.04	0.26	0.00	0.00	22.3
17	540	1261	-1250	-425	0	844	-1427	4.02	4.02	4.02	4.02	2	0.24	0.04	0.22	0.00	0.00	22.3
18	540	4626	-1927	-1430	0	2889	-2719	4.02	4.02	4.02	4.02	3	0.81	0.06	0.34	0.00	0.00	22.3
19	540	4431	-1860	-951	0	1955	-2472	4.02	4.02	4.02	4.02	3	0.54	0.05	0.33	0.00	0.00	22.3
20	540	4474	-1760	-1046	0	2093	-2203	4.02	4.02	4.02	4.02	3	0.58	0.05	0.31	0.00	0.00	22.3
37	540	3843	-1909	-1406	0	2827	-2698	4.02	4.02	4.02	4.02	3	0.77	0.06	0.34	0.00	0.00	22.3
38	540	3518	-1797	-606	0	1270	-2287	4.02	4.02	4.02	4.02	3	0.37	0.05	0.32	0.00	0.00	22.3
39	540	3590	-1630	-765	0	1499	-1837	4.02	4.02	4.02	4.02	3	0.41	0.05	0.29	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	600	1944	-2165	-623	0	1645	-2568	4.02	4.02	4.02	4.02	3	0.43	0.06	0.39	0.00	0.00	22.3
2	600	1620	-1699	-546	0	1445	-2079	4.02	4.02	4.02	4.02	2	0.42	0.05	0.30	0.00	0.00	22.3
3	600	1489	-1632	-523	0	1371	-1875	4.02	4.02	4.02	4.02	2	0.40	0.05	0.29	0.00	0.00	22.3
4	600	1502	-1698	-435	0	1160	-2075	4.02	4.02	4.02	4.02	2	0.34	0.05	0.30	0.00	0.00	22.3
5	600	1372	-1631	-412	0	1086	-1871	4.02	4.02	4.02	4.02	2	0.31	0.05	0.29	0.00	0.00	22.3
6	600	1730	-1777	-534	0	1432	-2316	4.02	4.02	4.02	4.02	2	0.42	0.05	0.32	0.00	0.00	22.3
7	600	1296	-1554	-458	0	1185	-1636	4.02	4.02	4.02	4.02	2	0.34	0.05	0.28	0.00	0.00	22.3
8	600	1695	-1777	-501	0	1346	-2314	4.02	4.02	4.02	4.02	2	0.39	0.05	0.32	0.00	0.00	22.3
9	600	1261	-1554	-425	0	1099	-1635	4.02	4.02	4.02	4.02	2	0.32	0.05	0.28	0.00	0.00	22.3
10	600	1620	-1699	-546	0	1445	-2079	4.02	4.02	4.02	4.02	2	0.42	0.05	0.30	0.00	0.00	22.3
11	600	1489	-1632	-523	0	1371	-1875	4.02	4.02	4.02	4.02	2	0.40	0.05	0.29	0.00	0.00	22.3
12	600	1502	-1698	-435	0	1160	-2075	4.02	4.02	4.02	4.02	2	0.34	0.05	0.30	0.00	0.00	22.3
13	600	1372	-1631	-412	0	1086	-1871	4.02	4.02	4.02	4.02	2	0.31	0.05	0.29	0.00	0.00	22.3
14	600	1730	-1777	-534	0	1432	-2316	4.02	4.02	4.02	4.02	2	0.42	0.05	0.32	0.00	0.00	22.3
15	600	1296	-1554	-458	0	1185	-1636	4.02	4.02	4.02	4.02	2	0.34	0.05	0.28	0.00	0.00	22.3
16	600	1695	-1777	-501	0	1346	-2314	4.02	4.02	4.02	4.02	2	0.39	0.05	0.32	0.00	0.00	22.3
17	600	1261	-1554	-425	0	1099	-1635	4.02	4.02	4.02	4.02	2	0.32	0.05	0.28	0.00	0.00	22.3
18	600	4626	-2323	-1430	0	3747	-3018	6.03	4.02	4.02	4.02	3	0.72	0.07	0.41	0.00	0.00	22.3
19	600	4431	-2255	-951	0	2525	-2765	4.02	4.02	4.02	4.02	3	0.70	0.07	0.40	0.00	0.00	22.3
20	600	4474	-2156	-1046	0	2720	-2486	4.02	4.02	4.02	4.02	3	0.76	0.06	0.38	0.00	0.00	22.3
37	600	3843	-2304	-1406	0	3670	-2996	6.03	4.02	4.02	4.02	3	0.69	0.07	0.41	0.00	0.00	22.3
38	600	3518	-2192	-606	0	1634	-2574	4.02	4.02	4.02	4.02	3	0.44	0.06	0.39	0.00	0.00	22.3
39	600	3590	-2026	-765	0	1958	-2109	4.02	4.02	4.02	4.02	3	0.53	0.06	0.36	0.00	0.00	22.3

apost= 2.01 aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

Nome travata: **Trave_404_IP1** Descrizione: **Trave_4 32-25**
ASTA NUM. 20 NI 258 NF 266 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y Permanente qy tot.
qy medio: 375.00 132.00 507.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	3063	1753	-846	0	-2302	-1308	4.02	4.02	4.02	4.02	3	0.62	0.05	0.31	0.00	0.00	22.3
2	0	2499	1299	-677	0	-1817	-866	4.02	4.02	4.02	4.02	2	0.54	0.04	0.23	0.00	0.00	22.3
3	0	2453	1376	-676	0	-1825	-1082	4.02	4.02	4.02	4.02	2	0.55	0.04	0.25	0.00	0.00	22.3
4	0	2259	1322	-625	0	-1716	-931	4.02	4.02	4.02	4.02	2	0.51	0.04	0.24	0.00	0.00	22.3
5	0	2213	1399	-625	0	-1724	-1147	4.02	4.02	4.02	4.02	2	0.51	0.04	0.25	0.00	0.00	22.3
6	0	2469	1217	-660	0	-1773	-637	4.02	4.02	4.02	4.02	2	0.53	0.04	0.22	0.00	0.00	22.3
7	0	2316	1474	-658	0	-1798	-1356	4.02	4.02	4.02	4.02	2	0.54	0.04	0.26	0.00	0.00	22.3
8	0	2397	1224	-644	0	-1743	-656	4.02	4.02	4.02	4.02	2	0.52	0.04	0.22	0.00	0.00	22.3
9	0	2244	1481	-642	0	-1768	-1376	4.02	4.02	4.02	4.02	2	0.53	0.04	0.26	0.00	0.00	22.3
10	0	2499	1299	-677	0	-1817	-866	4.02	4.02	4.02	4.02	2	0.54	0.04	0.23	0.00	0.00	22.3
11	0	2453	1376	-676	0	-1825	-1082	4.02	4.02	4.02	4.02	2	0.55	0.04	0.25	0.00	0.00	22.3
12	0	2259	1322	-625	0	-1716	-931	4.02	4.02	4.02	4.02	2	0.51	0.04	0.24	0.00	0.00	22.3
13	0	2213	1399	-625	0	-1724	-1147	4.02	4.02	4.02	4.02	2	0.51	0.04	0.25	0.00	0.00	22.3
14	0	2469	1217	-660	0	-1773	-637	4.02	4.02	4.02	4.02	2	0.53	0.04	0.22	0.00	0.00	22.3
15	0	2316	1474	-658	0	-1798	-1356	4.02	4.02	4.02	4.02	2	0.54	0.04	0.26	0.00	0.00	22.3
16	0	2397	1224	-644	0	-1743	-656	4.02	4.02	4.02	4.02	2	0.52	0.04	0.22	0.00	0.00	22.3
17	0	2244	1481	-642	0	-1768	-1376	4.02	4.02	4.02	4.02	2	0.53	0.04	0.26	0.00	0.00	22.3
18	0	6918	1344	-1824	0	-4897	-276	4.02	6.03	4.02	4.02	3	0.98	0.06	0.29	0.00	0.00	22.3
19	0	7739	1389	-1515	0	-4180	-510	4.02	6.03	4.02	4.02	3	0.85	0.05	0.25	0.00	0.00	22.3
20	0	7226	1559	-1559	0	-4250	-906	4.02	6.03	4.02	4.02	3	0.86	0.05	0.28	0.00	0.00	22.3
37	0	5246	1455	-1659	0	-4406	-495	4.02	6.03	4.02	4.02	3	0.85	0.05	0.27	0.00	0.00	22.3
38	0	6613	1530	-1143	0	-3211	-885	4.02	4.02	4.02	4.02	3	0.96	0.04	0.27	0.00	0.00	22.3
39	0	5759	1813	-1216	0	-3328	-1545	4.02	4.02	4.02	4.02	3	0.96	0.05	0.32	0.00	0.00	22.3

apost= -- aant= 2.01 ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	60	3063	1358	-846	0	-1794	-1062	4.02	4.02	4.02	4.02	3	0.48	0.04	0.24	0.00	0.00	22.3
2	60	2499	995	-677	0	-1411	-682	4.02	4.02	4.02	4.02	2	0.42	0.03	0.18	0.00	0.00	22.3
3	60	2453	1072	-676	0	-1419	-890	4.02	4.02	4.02	4.02	2	0.42	0.03	0.19	0.00	0.00	22.3
4	60	2259	1018	-625	0	-1341	-745	4.02	4.02	4.02	4.02	2	0.40	0.03	0.18	0.00	0.00	22.3
5	60	2213	1095	-625	0	-1349	-953	4.02	4.02	4.02	4.02	2	0.40	0.03	0.19	0.00	0.00	22.3
6	60	2469	913	-660	0	-1377	464	4.02	4.02	4.02	4.02	2	0.41	0.03	0.16	0.00	0.00	22.3
7	60	2316	1170	-658	0	-1403	-1155	4.02	4.02	4.02	4.02	2	0.42	0.03	0.21	0.00	0.00	22.3
8	60	2397	920	-644	0	-1357	-479	4.02	4.02	4.02	4.02	2	0.41	0.03	0.16	0.00	0.00	22.3
9	60	2244	1177	-642	0	-1383	-1175	4.02	4.02	4.02	4.02	2	0.41	0.03	0.21	0.00	0.00	22.3
10	60	2499	995	-677	0	-1411	-682	4.02	4.02	4.02	4.02	2	0.42	0.03	0.18	0.00	0.00	22.3
11	60	2453	1072	-676	0	-1419	-890	4.02	4.02	4.02	4.02	2	0.42	0.03	0.19	0.00	0.00	22.3
12	60	2259	1018	-625	0	-1341	-745	4.02	4.02	4.02	4.02	2	0.40	0.03	0.18	0.00	0.00	22.3
13	60	2213	1095	-625	0	-1349	-953	4.02	4.02	4.02	4.02	2	0.40	0.03	0.19	0.00	0.00	22.3
14	60	2469	913	-660	0	-1377	464	4.02	4.02	4.02	4.02	2	0.41	0.03	0.16	0.00	0.00	22.3
15	60	2316	1170	-658	0	-1403	-1155	4.02	4.02	4.02	4.02	2	0.42	0.03	0.21	0.00	0.00	22.3
16	60	2397	920	-644	0	-1357	-479	4.02	4.02	4.02	4.02	2	0.41	0.03	0.16	0.00	0.00	22.3
17	60	2244	1177	-642	0	-1383	-1175	4.02	4.02	4.02	4.02	2	0.41	0.03	0.21	0.00	0.00	22.3
18	60	6918	949	-1824	0	-3802	892	4.02	6.03	4.02	4.02	3	0.76	0.06	0.29	0.00	0.00	22.3
19	60	7739	994	-1515	0	-3271	708	4.02	6.03	4.02	4.02	3	0.67	0.05	0.24	0.00	0.00	22.3
20	60	7226	1164	-1559	0	-3315	-679	4.02	6.03	4.02	4.02	3	0.67	0.05	0.25	0.00	0.00	22.3
37	60	5246	1060	-1659	0	-3411	795	4.02	4.02	4.02	4.02	3	0.97	0.05	0.27	0.00	0.00	22.3
38	60	6613	1135	-1143	0	-2525	-660	4.02	4.02	4.02	4.02	3	0.75	0.04	0.20	0.00	0.00	22.3
39	60	5759	1418	-1216	0	-2598	-1294	4.02	4.02	4.02	4.02	3	0.75	0.04	0.25	0.00	0.00	22.3

apost= -- aant= 2.01 ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	120	3063	962	-846	0	-1287	808	4.02	4.02	4.02	4.02	3	0.34	0.03	0.17	0.00	0.00	22.3
2	120	2499	691	-677	0	-1005	677	4.02	4.02	4.02	4.02	2	0.30	0.02	0.12	0.00	0.00	22.3
3	120	2453	768	-676	0	-1013	593	4.02	4.02	4.02	4.02	2	0.30	0.02	0.14	0.00	0.00	22.3
4	120	2259	714	-625	0	-966	651	4.02	4.02	4.02	4.02	2	0.29	0.02	0.13	0.00	0.00	22.3
5	120	2213	791	-625	0	-974	567	4.02	4.02	4.02	4.02	2	0.29	0.02	0.14	0.00	0.00	22.3
6	120	2469	609	-660	0	-982	766	4.02	4.02	4.02	4.02	2	0.29	0.02	0.11	0.00	0.00	22.3
7	120	2316	866	-658	0	-1009	486	4.02	4.02	4.02	4.02	2	0.30	0.03	0.15	0.00	0.00	22.3
8	120	2397	616	-644	0	-970	758	4.02	4.02	4.02	4.02	2	0.29	0.02	0.11	0.00	0.00	22.3
9	120	2244	873	-642	0	-997	478	4.02	4.02	4.02	4.02	2	0.30	0.03	0.16	0.00	0.00	22.3
10	120	2499	691	-677	0	-1005	677	4.02	4.02	4.02	4.02	2	0.30	0.02	0.12	0.00	0.00	22.3
11	120	2453	768	-676	0	-1013	593	4.02	4.02	4.02	4.02	2	0.30	0.02	0.14	0.00	0.00	22.3
12	120	2259	714	-625	0	-966	651	4.02	4.02	4.02	4.02	2	0.29	0.02	0.13	0.00	0.00	22.3
13	120	2213	791	-625	0	-974	567	4.02	4.02	4.02	4.02	2	0.29	0.02	0.14	0.00	0.00	22.3
14	120	2469	609	-660	0	-982	766	4.02	4.02	4.02	4.02	2	0.29	0.02	0.11	0.00	0.00	22.3
15	120	2316	866	-658	0	-1009	486	4.02	4.02	4.02	4.02	2	0.30	0.03	0.15	0.00	0.00	22.3
16	120	2397	616	-644	0	-970	758	4.02	4.02	4.02	4.02	2	0.29	0.02	0.11	0.00	0.00	22.3
17	120	2244	873	-642	0	-997	478	4.02	4.02	4.02	4.02	2	0.30	0.03	0.16	0.00	0.00	22.3
18	120	6918	553	-1824	0	-2708	1076	4.02	4.02	4.02	4.02	3	0.81	0.06	0.29	0.00	0.00	22.3
19	120	7739	598	-1515	0	-2362	926	4.02	4.02	4.02	4.02	3	0.73	0.05	0.24	0.00	0.00	22.3
20	120	7226	768	-1559	0	-2380	879	4.02	4.02	4.02	4.02	3	0.72	0.05	0.25	0.00	0.00	22.3
37	120	5246	664	-1659	0	-2416	1099	4.02	4.02	4.02	4.02	3	0.69	0.05	0.27	0.00	0.00	22.3
38	120	6613	739	-1143	0	-1839	851	4.02	4.02	4.02	4.02	3	0.55	0.04	0.18	0.00	0.00	22.3
39	120	5759	1022	-1216	0	-1869	673	4.02	4.02	4.02	4.02	3	0.54	0.04	0.20	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	180	3063	567	-846	0	-779	1001	4.02	4.02	4.02	4.02	3	0.21	0.03	0.14	0.00	0.00	22.3
2	180	2499	386	-677	0	-599	791	4.02	4.02	4.02	4.02	2	0.18	0.02	0.11	0.00	0.00	22.3
3	180	2453	463	-676	0	-608	764	4.02	4.02	4.02	4.02	2	0.18	0.02	0.11	0.00	0.00	22.3
4	180	2259	409	-625	0	-591	781	4.02	4.02	4.02	4.02	2	0.18	0.02	0.10	0.00	0.00	22.3
5	180	2213	486	-625	0	-600	768	4.02	4.02	4.02	4.02	2	0.18	0.02	0.10	0.00	0.00	22.3
6	180	2469	304	-660	0	-586	823	4.02	4.02	4.02	4.02	2	0.18	0.02	0.11	0.00	0.00	22.3
7	180	2316	561	-658	0	-615	759	4.02	4.02	4.02	4.02	2	0.18	0.02	0.11	0.00	0.00	22.3
8	180	2397	311	-644	0	-584	820	4.02	4.02	4.02	4.02	2	0.17	0.02	0.10	0.00	0.00	22.3
9	180	2244	568	-642	0	-612	756	4.02	4.02	4.02	4.02	2	0.18	0.02	0.10	0.00	0.00	22.3
10	180	2499	386	-677	0	-599	791	4.02	4.02	4.02	4.02	2	0.18	0.02	0.11	0.00	0.00	22.3
11	180	2453	463	-676	0	-608	764	4.02	4.02	4.02	4.02	2	0.18	0.02	0.11	0.00	0.00	22.3
12	180	2259	409	-625	0	-591	781	4.02	4.02	4.02	4.02	2	0.18	0.02	0.10	0.00	0.00	22.3
13	180	2213	486	-625	0	-600	768	4.02	4.02	4.02	4.02	2	0.18	0.02	0.10	0.00	0.00	22.3
14	180	2469	304	-660	0	-586	823	4.02	4.02	4.02	4.02	2	0.18	0.02	0.11	0.00	0.00	22.3
15	180	2316	561	-658	0	-615	759	4.02	4.02	4.02	4.02	2	0.18	0.02	0.11	0.00	0.00	22.3
16	180	2397	311	-644	0	-584	820	4.02	4.02	4.02	4.02	2	0.17	0.02	0.10	0.00	0.00	22.3

17	180	2244	568	-642	0	-612	756	4.02	4.02	4.02	4.02	2	0.18	0.02	0.10	0.00	0.00	22.3
18	180	6918	158	-1824	0	-1613	1076	4.02	4.02	4.02	4.02	3	0.49	0.06	0.29	0.00	0.00	22.3
19	180	7739	203	-1515	0	-1453	926	4.02	4.02	4.02	4.02	3	0.45	0.05	0.24	0.00	0.00	22.3
20	180	7226	372	-1559	0	-1445	937	4.02	4.02	4.02	4.02	3	0.44	0.05	0.25	0.00	0.00	22.3
37	180	5246	268	-1659	0	-1421	1099	4.02	4.02	4.02	4.02	3	0.41	0.05	0.27	0.00	0.00	22.3
38	180	6613	344	-1143	0	-1153	889	4.02	4.02	4.02	4.02	3	0.34	0.04	0.18	0.00	0.00	22.3
39	180	5759	626	-1216	0	-1139	927	4.02	4.02	4.02	4.02	3	0.33	0.04	0.20	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	240	3063	171	-846	0	-272	1001	4.02	4.02	4.02	4.02	3	0.16	0.03	0.14	0.00	0.00	22.3
2	240	2499	82	-677	0	-193	791	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
3	240	2453	159	-676	0	-202	764	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
4	240	2259	105	-625	0	-216	781	4.02	4.02	4.02	4.02	2	0.13	0.02	0.10	0.00	0.00	22.3
5	240	2213	182	-625	0	-225	768	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
6	240	2469	0	-660	0	-190	823	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
7	240	2316	257	-658	0	-220	784	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
8	240	2397	7	-644	0	-197	820	4.02	4.02	4.02	4.02	2	0.13	0.02	0.10	0.00	0.00	22.3
9	240	2244	264	-642	0	-227	785	4.02	4.02	4.02	4.02	2	0.13	0.02	0.10	0.00	0.00	22.3
10	240	2499	82	-677	0	-193	791	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
11	240	2453	159	-676	0	-202	764	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
12	240	2259	105	-625	0	-216	781	4.02	4.02	4.02	4.02	2	0.13	0.02	0.10	0.00	0.00	22.3
13	240	2213	182	-625	0	-225	768	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
14	240	2469	0	-660	0	-190	823	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
15	240	2316	257	-658	0	-220	784	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
16	240	2397	7	-644	0	-197	820	4.02	4.02	4.02	4.02	2	0.13	0.02	0.10	0.00	0.00	22.3
17	240	2244	264	-642	0	-227	785	4.02	4.02	4.02	4.02	2	0.13	0.02	0.10	0.00	0.00	22.3
18	240	6918	-238	-1824	0	-519	1076	4.02	4.02	4.02	4.02	3	0.19	0.06	0.29	0.00	0.00	22.3
19	240	7739	-193	-1515	0	-544	926	4.02	4.02	4.02	4.02	3	0.17	0.05	0.24	0.00	0.00	22.3
20	240	7226	-23	-1559	0	-510	937	4.02	4.02	4.02	4.02	3	0.17	0.05	0.25	0.00	0.00	22.3
37	240	5246	-127	-1659	0	-426	1099	4.02	4.02	4.02	4.02	3	0.19	0.05	0.27	0.00	0.00	22.3
38	240	6613	-52	-1143	0	-467	889	4.02	4.02	4.02	4.02	3	0.16	0.04	0.18	0.00	0.00	22.3
39	240	5759	231	-1216	0	-410	927	4.02	4.02	4.02	4.02	3	0.16	0.04	0.20	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	300	3063	-224	-846	0	236	1001	4.02	4.02	4.02	4.02	3	0.16	0.03	0.14	0.00	0.00	22.3
2	300	2499	-222	-677	0	214	791	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
3	300	2453	-145	-676	0	204	764	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
4	300	2259	-199	-625	0	160	781	4.02	4.02	4.02	4.02	2	0.13	0.02	0.10	0.00	0.00	22.3
5	300	2213	-122	-625	0	150	768	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
6	300	2469	-304	-660	0	206	823	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
7	300	2316	-47	-658	0	175	784	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
8	300	2397	-297	-644	0	189	820	4.02	4.02	4.02	4.02	2	0.13	0.02	0.10	0.00	0.00	22.3
9	300	2244	-40	-642	0	159	785	4.02	4.02	4.02	4.02	2	0.13	0.02	0.10	0.00	0.00	22.3
10	300	2499	-222	-677	0	214	791	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
11	300	2453	-145	-676	0	204	764	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
12	300	2259	-199	-625	0	160	781	4.02	4.02	4.02	4.02	2	0.13	0.02	0.10	0.00	0.00	22.3
13	300	2213	-122	-625	0	150	768	4.02	4.02	4.02	4.02	2	0.12	0.02	0.10	0.00	0.00	22.3
14	300	2469	-304	-660	0	206	823	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
15	300	2316	-47	-658	0	175	784	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
16	300	2397	-297	-644	0	189	820	4.02	4.02	4.02	4.02	2	0.13	0.02	0.10	0.00	0.00	22.3
17	300	2244	-40	-642	0	159	785	4.02	4.02	4.02	4.02	2	0.13	0.02	0.10	0.00	0.00	22.3
18	300	6918	-633	-1824	0	575	1076	4.02	4.02	4.02	4.02	3	0.19	0.06	0.29	0.00	0.00	22.3
19	300	7739	-588	-1515	0	365	926	4.02	4.02	4.02	4.02	3	0.17	0.05	0.24	0.00	0.00	22.3
20	300	7226	-419	-1559	0	426	937	4.02	4.02	4.02	4.02	3	0.17	0.05	0.25	0.00	0.00	22.3
37	300	5246	-523	-1659	0	569	1099	4.02	4.02	4.02	4.02	3	0.19	0.05	0.27	0.00	0.00	22.3
38	300	6613	-447	-1143	0	219	889	4.02	4.02	4.02	4.02	3	0.16	0.04	0.18	0.00	0.00	22.3
39	300	5759	-165	-1216	0	320	927	4.02	4.02	4.02	4.02	3	0.16	0.04	0.20	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	360	3063	-619	-846	0	744	1001	4.02	4.02	4.02	4.02	3	0.20	0.03	0.14	0.00	0.00	22.3
2	360	2499	-526	-677	0	620	790	4.02	4.02	4.02	4.02	2	0.19	0.02	0.11	0.00	0.00	22.3
3	360	2453	-449	-676	0	610	764	4.02	4.02	4.02	4.02	2	0.18	0.02	0.11	0.00	0.00	22.3
4	360	2259	-503	-625	0	535	781	4.02	4.02	4.02	4.02	2	0.16	0.02	0.10	0.00	0.00	22.3
5	360	2213	-426	-625	0	525	768	4.02	4.02	4.02	4.02	2	0.16	0.02	0.10	0.00	0.00	22.3
6	360	2469	-608	-660	0	601	766	4.02	4.02	4.02	4.02	2	0.18	0.02	0.11	0.00	0.00	22.3
7	360	2316	-351	-658	0	569	784	4.02	4.02	4.02	4.02	2	0.17	0.02	0.11	0.00	0.00	22.3
8	360	2397	-601	-644	0	575	767	4.02	4.02	4.02	4.02	2	0.17	0.02	0.11	0.00	0.00	22.3
9	360	2244	-344	-642	0	544	785	4.02	4.02	4.02	4.02	2	0.16	0.02	0.10	0.00	0.00	22.3
10	360	2499	-526	-677	0	620	790	4.02	4.02	4.02	4.02	2	0.19	0.02	0.11	0.00	0.00	22.3
11	360	2453	-449	-676	0	610	764	4.02	4.02	4.02	4.02	2	0.18	0.02	0.11	0.00	0.00	22.3
12	360	2259	-503	-625	0	535	781	4.02	4.02	4.02	4.02	2	0.16	0.02	0.10	0.00	0.00	22.3
13	360	2213	-426	-625	0	525	768	4.02	4.02	4.02	4.02	2	0.16	0.02	0.10	0.00	0.00	22.3
14	360	2469	-608	-660	0	601	766	4.02	4.02	4.02	4.02	2	0.18	0.02	0.11	0.00	0.00	22.3
15	360	2316	-351	-658	0	569	784	4.02	4.02	4.02	4.02	2	0.17	0.02	0.11	0.00	0.00	22.3
16	360	2397	-601	-644	0	575	767	4.02	4.02	4.02	4.02	2	0.17	0.02	0.11	0.00	0.00	22.3
17	360	2244	-344	-642	0	544	785	4.02	4.02	4.02	4.02	2	0.16	0.02	0.10	0.00	0.00	22.3
18	360	6918	-1028	-1824	0	1670	813	4.02	4.02	4.02	4.02	3	0.50	0.06	0.29	0.00	0.00	22.3
19	360	7739	-983	-1515	0	1274	718	4.02	4.02	4.02	4.02	3	0.39	0.05	0.24	0.00	0.00	22.3
20	360	7226	-814	-1559	0	1361	847	4.02	4.02	4.02	4.02	3	0.41	0.05	0.25	0.00	0.00	22.3
37	360	5246	-918	-1659	0	1565	937	4.02	4.02	4.02	4.02	3	0.45	0.05	0.27	0.00	0.00	22.3
38	360	6613	-842	-1143	0	904	779	4.02	4.02	4.02	4.02	3	0.27	0.04	0.18	0.00	0.00	22.3
39	360	5759	-560	-1216	0	1049	927	4.02	4.02	4.02	4.02	3	0.30	0.04	0.20	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	420	3063	-1015	-846	0	1251	756	4.02	4.02	4.02	4.02	3	0.33	0.03	0.18	0.00	0.00	22.3
2	420	2499	-830	-677	0	1026	537	4.02	4.02	4.02	4.02	2	0.31	0.02	0.15	0.00	0.00	22.3
3	420	2453	-753	-676	0	1016	606	4.02	4.02	4.02	4.02	2	0.30	0.02	0.13	0.00	0.00	22.3
4	420	2259	-807	-625	0	910	556	4.02	4.02	4.02	4.02	2	0.27	0.02	0.14	0.00	0.00	22.3
5	420	2213	-730	-625	0	900	625	4.02	4.02	4.02	4.02	2	0.27	0.02	0.13	0.00	0.00	22.3
6	420	2469	-912	-660	0	997	463	4.02	4.02	4.02	4.02	2	0.30	0.03	0.16	0.00	0.00	22.3
7	420	2316	-655	-658	0	963	693	4.02	4.02	4.02	4.02	2	0.29	0.02	0.12	0.00	0.00	22.3
8	420	2397	-905	-644	0	962	469	4.02	4.02	4.02	4.02	2	0.29	0.03	0.16	0.00	0.00	22.3
9	420	2244	-648	-642	0	929	699	4.02	4.02	4.02	4.02	2	0.28	0.02	0.12	0.00	0.00	22.3
10	420	2499	-830	-677	0	1026	537	4.02	4.02	4.02	4.02	2	0.31	0.02	0.15	0.00	0.00	22.3
11	420	2453	-753	-676	0	1016	606	4.02	4.02	4.02	4.02	2	0.30	0.02	0.13	0.00	0.00	22.3
12	420	2259	-807	-625	0	910	556	4.02	4.02	4.02	4.02	2	0.27	0.02	0.14	0.00	0.00	22.3
13	420	2213	-730	-625	0	900	625	4.02	4.02	4.02	4.02	2	0.27	0.02	0.13	0.00	0.00	22.3
14	420	2469	-912	-660	0	997	463	4.02	4.02	4.02	4.02	2	0.30	0.03	0.16	0.00	0.00	22.3
15	420	2316	-655	-658	0	963	693	4.02	4.02	4.02	4.02	2	0.29	0.02	0.12	0.00	0.00	22.3
16	420	2397	-905	-644	0	962	469	4.02	4.02	4.02	4.02	2	0.29	0.03	0.16	0.00	0.00	22.3
17	420	2244	-648	-642	0	929	699	4.02	4.02	4.02	4.02	2	0.28	0.02	0.12	0.00	0.00	22.3
18	420	6918	-1424	-1824	0	2764	-1164	4.02	4.02	4.02	4.02	3	0.83	0.06	0.29	0.00	0.00	22.3
19	420	7739	-1379	-1515	0	2183	-1186	4.02	4.02	4.02	4.02	3	0.67	0.05	0.25	0.00	0.00	22.3
20	420	7226	-1210	-1559	0	2296	-785	4.02	4.02	4.02	4.02	3	0.70	0.05	0.25	0.00	0.00	22.3
37	420	5246	-1314	-1659	0	2560	-862	4.02	4.02	4.02	4.02	3	0.73	0.05	0.27	0.00	0.00	22.3
38	420	6613	-1238	-1143	0	1590	-898	4.02	4.02	4.02	4.02	3	0.47	0.04	0.22	0.00	0.00	22.3

39	420	5759	-956	-1216	0	1778	739	4.02	4.02	4.02	4.02	3	0.52	0.04	0.20	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	480	3063	-1410	-846	0	1759	-1200	4.02	4.02	4.02	4.02	3	0.47	0.04	0.25	0.00	0.00	22.3
2	480	2499	-1135	-677	0	1432	-1047	4.02	4.02	4.02	4.02	2	0.43	0.03	0.20	0.00	0.00	22.3
3	480	2453	-1058	-676	0	1421	-854	4.02	4.02	4.02	4.02	2	0.43	0.03	0.19	0.00	0.00	22.3
4	480	2259	-1112	-625	0	1285	-991	4.02	4.02	4.02	4.02	2	0.38	0.03	0.20	0.00	0.00	22.3
5	480	2213	-1035	-625	0	1274	-798	4.02	4.02	4.02	4.02	2	0.38	0.03	0.18	0.00	0.00	22.3
6	480	2469	-1217	-660	0	1393	-1254	4.02	4.02	4.02	4.02	2	0.42	0.04	0.22	0.00	0.00	22.3
7	480	2316	-960	-658	0	1358	-609	4.02	4.02	4.02	4.02	2	0.40	0.03	0.17	0.00	0.00	22.3
8	480	2397	-1210	-644	0	1348	-1236	4.02	4.02	4.02	4.02	2	0.40	0.04	0.22	0.00	0.00	22.3
9	480	2244	-953	-642	0	1314	-592	4.02	4.02	4.02	4.02	2	0.39	0.03	0.17	0.00	0.00	22.3
10	480	2499	-1135	-677	0	1432	-1047	4.02	4.02	4.02	4.02	2	0.43	0.03	0.20	0.00	0.00	22.3
11	480	2453	-1058	-676	0	1421	-854	4.02	4.02	4.02	4.02	2	0.43	0.03	0.19	0.00	0.00	22.3
12	480	2259	-1112	-625	0	1285	-991	4.02	4.02	4.02	4.02	2	0.38	0.03	0.20	0.00	0.00	22.3
13	480	2213	-1035	-625	0	1274	-798	4.02	4.02	4.02	4.02	2	0.38	0.03	0.18	0.00	0.00	22.3
14	480	2469	-1217	-660	0	1393	-1254	4.02	4.02	4.02	4.02	2	0.42	0.04	0.22	0.00	0.00	22.3
15	480	2316	-960	-658	0	1358	-609	4.02	4.02	4.02	4.02	2	0.40	0.03	0.17	0.00	0.00	22.3
16	480	2397	-1210	-644	0	1348	-1236	4.02	4.02	4.02	4.02	2	0.40	0.04	0.22	0.00	0.00	22.3
17	480	2244	-953	-642	0	1314	-592	4.02	4.02	4.02	4.02	2	0.39	0.03	0.17	0.00	0.00	22.3
18	480	6918	-1819	-1824	0	3859	-2337	6.03	4.02	4.02	4.02	3	0.77	0.06	0.32	0.00	0.00	22.3
19	480	7739	-1774	-1515	0	3092	-2332	4.02	4.02	4.02	4.02	3	0.95	0.05	0.32	0.00	0.00	22.3
20	480	7226	-1605	-1559	0	3231	-1829	4.02	4.02	4.02	4.02	3	0.98	0.05	0.29	0.00	0.00	22.3
37	480	5246	-1709	-1659	0	3555	-1969	6.03	4.02	4.02	4.02	3	0.69	0.05	0.30	0.00	0.00	22.3
38	480	6613	-1633	-1143	0	2276	-1960	4.02	4.02	4.02	4.02	3	0.68	0.05	0.29	0.00	0.00	22.3
39	480	5759	-1351	-1216	0	2508	-1121	4.02	4.02	4.02	4.02	3	0.73	0.04	0.24	0.00	0.00	22.3

apost= 2.01 aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	540	3063	-1806	-846	0	2266	-2365	4.02	4.02	4.02	4.02	3	0.61	0.05	0.32	0.00	0.00	22.3
2	540	2499	-1439	-677	0	1838	-1974	4.02	4.02	4.02	4.02	2	0.55	0.04	0.26	0.00	0.00	22.3
3	540	2453	-1362	-676	0	1827	-1734	4.02	4.02	4.02	4.02	2	0.55	0.04	0.24	0.00	0.00	22.3
4	540	2259	-1416	-625	0	1660	-1904	4.02	4.02	4.02	4.02	2	0.49	0.04	0.25	0.00	0.00	22.3
5	540	2213	-1339	-625	0	1649	-1664	4.02	4.02	4.02	4.02	2	0.49	0.04	0.24	0.00	0.00	22.3
6	540	2469	-1521	-660	0	1788	-2229	4.02	4.02	4.02	4.02	2	0.54	0.04	0.27	0.00	0.00	22.3
7	540	2316	-1264	-658	0	1753	-1430	4.02	4.02	4.02	4.02	2	0.52	0.04	0.23	0.00	0.00	22.3
8	540	2397	-1514	-644	0	1735	-2208	4.02	4.02	4.02	4.02	2	0.52	0.04	0.27	0.00	0.00	22.3
9	540	2244	-1257	-642	0	1700	-1409	4.02	4.02	4.02	4.02	2	0.51	0.04	0.22	0.00	0.00	22.3
10	540	2499	-1439	-677	0	1838	-1974	4.02	4.02	4.02	4.02	2	0.55	0.04	0.26	0.00	0.00	22.3
11	540	2453	-1362	-676	0	1827	-1734	4.02	4.02	4.02	4.02	2	0.55	0.04	0.24	0.00	0.00	22.3
12	540	2259	-1416	-625	0	1660	-1904	4.02	4.02	4.02	4.02	2	0.49	0.04	0.25	0.00	0.00	22.3
13	540	2213	-1339	-625	0	1649	-1664	4.02	4.02	4.02	4.02	2	0.49	0.04	0.24	0.00	0.00	22.3
14	540	2469	-1521	-660	0	1788	-2229	4.02	4.02	4.02	4.02	2	0.54	0.04	0.27	0.00	0.00	22.3
15	540	2316	-1264	-658	0	1753	-1430	4.02	4.02	4.02	4.02	2	0.52	0.04	0.23	0.00	0.00	22.3
16	540	2397	-1514	-644	0	1735	-2208	4.02	4.02	4.02	4.02	2	0.52	0.04	0.27	0.00	0.00	22.3
17	540	2244	-1257	-642	0	1700	-1409	4.02	4.02	4.02	4.02	2	0.51	0.04	0.22	0.00	0.00	22.3
18	540	6918	-2215	-1824	0	4953	-3748	6.03	4.02	4.02	4.02	3	0.99	0.06	0.39	0.00	0.00	22.3
19	540	7739	-2170	-1515	0	4001	-3716	6.03	4.02	4.02	4.02	3	0.82	0.06	0.39	0.00	0.00	22.3
20	540	7226	-2000	-1559	0	4166	-3111	6.03	4.02	4.02	4.02	3	0.84	0.06	0.36	0.00	0.00	22.3
37	540	5246	-2104	-1659	0	4550	-3313	6.03	4.02	4.02	4.02	3	0.88	0.06	0.37	0.00	0.00	22.3
38	540	6613	-2029	-1143	0	2962	-3259	4.02	4.02	4.02	4.02	3	0.88	0.06	0.36	0.00	0.00	22.3
39	540	5759	-1746	-1216	0	3237	-2251	4.02	4.02	4.02	4.02	3	0.94	0.05	0.31	0.00	0.00	22.3

apost= 2.01 aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	600	3063	-2201	-846	0	2774	-2653	4.02	4.02	4.02	4.02	3	0.74	0.06	0.39	0.00	0.00	22.3
2	600	2499	-1743	-677	0	2244	-2200	4.02	4.02	4.02	4.02	2	0.67	0.05	0.31	0.00	0.00	22.3
3	600	2453	-1666	-676	0	2233	-1953	4.02	4.02	4.02	4.02	2	0.67	0.05	0.30	0.00	0.00	22.3
4	600	2259	-1720	-625	0	2035	-2128	4.02	4.02	4.02	4.02	2	0.61	0.05	0.31	0.00	0.00	22.3
5	600	2213	-1643	-625	0	2024	-1881	4.02	4.02	4.02	4.02	2	0.60	0.05	0.29	0.00	0.00	22.3
6	600	2469	-1825	-660	0	2184	-2463	4.02	4.02	4.02	4.02	2	0.65	0.05	0.33	0.00	0.00	22.3
7	600	2316	-1568	-658	0	2147	-1640	4.02	4.02	4.02	4.02	2	0.64	0.05	0.28	0.00	0.00	22.3
8	600	2397	-1818	-644	0	2121	-2441	4.02	4.02	4.02	4.02	2	0.63	0.05	0.32	0.00	0.00	22.3
9	600	2244	-1561	-642	0	2085	-1618	4.02	4.02	4.02	4.02	2	0.62	0.05	0.28	0.00	0.00	22.3
10	600	2499	-1743	-677	0	2244	-2200	4.02	4.02	4.02	4.02	2	0.67	0.05	0.31	0.00	0.00	22.3
11	600	2453	-1666	-676	0	2233	-1953	4.02	4.02	4.02	4.02	2	0.67	0.05	0.30	0.00	0.00	22.3
12	600	2259	-1720	-625	0	2035	-2128	4.02	4.02	4.02	4.02	2	0.61	0.05	0.31	0.00	0.00	22.3
13	600	2213	-1643	-625	0	2024	-1881	4.02	4.02	4.02	4.02	2	0.60	0.05	0.29	0.00	0.00	22.3
14	600	2469	-1825	-660	0	2184	-2463	4.02	4.02	4.02	4.02	2	0.65	0.05	0.33	0.00	0.00	22.3
15	600	2316	-1568	-658	0	2147	-1640	4.02	4.02	4.02	4.02	2	0.64	0.05	0.28	0.00	0.00	22.3
16	600	2397	-1818	-644	0	2121	-2441	4.02	4.02	4.02	4.02	2	0.63	0.05	0.32	0.00	0.00	22.3
17	600	2244	-1561	-642	0	2085	-1618	4.02	4.02	4.02	4.02	2	0.62	0.05	0.28	0.00	0.00	22.3
18	600	6918	-2610	-1824	0	6048	-4074	8.04	4.02	4.02	4.02	3	0.91	0.08	0.46	0.00	0.00	22.3
19	600	7739	-2565	-1515	0	4910	-4038	8.04	4.02	4.02	4.02	3	0.75	0.07	0.46	0.00	0.00	22.3
20	600	7226	-2396	-1559	0	5101	-3417	8.04	4.02	4.02	4.02	3	0.77	0.07	0.43	0.00	0.00	22.3
37	600	5246	-2500	-1659	0	5545	-3629	8.04	4.02	4.02	4.02	3	0.81	0.07	0.45	0.00	0.00	22.3
38	600	6613	-2424	-1143	0	3648	-3568	6.03	4.02	4.02	4.02	3	0.73	0.07	0.43	0.00	0.00	22.3
39	600	5759	-2142	-1216	0	3967	-2533	6.03	4.02	4.02	4.02	3	0.78	0.06	0.38	0.00	0.00	22.3

apost= 4.02 aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

L E G E N D A

Prima asta	Ultima asta	Nome disegno	Descrizione disegno
1	4	Trave_401_IP1.ARM	Trave_4 7-12-17-22-32
5	8	Trave_402_IP1.ARM	Trave_4 1-10-15-20-25
9	14	Trave_403_IP1.ARM	Trave_4 7-6-5-4-3-2-1
15	20	Trave_404_IP1.ARM	Trave_4 32-25

STAMPA SINTETICA (stampa degli elementi con massimo IR a presso-tenso-flessione (Fx, M), IR bielle (taglio))

TRAVI

Gruppo	El.	NC	x	Fx, M	Bielle	Note
			--	-----	------	
			cm	IR	IR	
4	14	18	60	1.00	--	
4	5	38	0	--	0.11	

Delta Ingegneria srl
via Artemide 3 92100 Agrigento - tel 0922 402212
email - g.ferraro@deltaingegneria.it

Lavoro: **D2403a** Intestazione lavoro: **Palestra Campobello**
Elemento: **TRAVE** Gruppo: **3** Tabella: **Tabella travi**
Descrizione: **Travi interpiano paletra**
Rck: **350.00** daN/cm^2 fyk: **4580.0** daN/cm^2 Condizioni ambientali: **Ordinaria**
Copriferro superiore: **5.0** cm Copriferro inferiore: **5.0** cm Copriferro laterale: **5.0** cm
Diametro staffe: **8** mm Numero braccia: **2**

Nome travata: **trave_301_IP1** Descrizione: **Trave_3 7-12-17-22-32**
ASTA NUM. 1 NI 27 NF 34 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y Permanente qy tot.
qy medio: 375.00 308.00 683.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	[Fx]	[Fy]	[Fz]	[Mx]	[My]	Mz	[APOST]	[AANT]	AINF	ASUP	Sc	Sf	w
	cm	daN			daN*m			cm^2				daN/cm^2		mm
40	0	402	2084	170	0	695	-2170	4.02	4.02	4.02	4.02	-14.56	91.2	0.00
41	0	866	2066	174	0	738	-2121	4.02	4.02	4.02	4.02	-14.23	89.1	0.00
42	0	1008	2058	403	0	1438	-2104	4.02	4.02	4.02	4.02	-14.12	88.4	0.00
43	0	35	2076	126	0	498	-2125	4.02	4.02	4.02	4.02	-14.26	89.3	0.00
44	0	1654	2041	189	0	837	-2060	4.02	4.02	4.02	4.02	-13.82	86.6	0.00
45	0	1043	2032	515	0	1737	-2015	4.02	4.02	4.02	4.02	-13.52	84.7	0.00
46	0	771	2032	110	0	468	-1997	4.02	4.02	4.02	4.02	-13.40	83.9	0.00
47	0	747	2024	94	0	400	-1965	4.02	4.02	4.02	4.02	-13.19	82.6	0.00
49	0	593	2030	92	0	386	-1982	4.02	4.02	4.02	4.02	-13.30	83.3	0.00
50	0	917	2023	105	0	454	-1969	4.02	4.02	4.02	4.02	-13.21	82.8	0.00
51	0	795	2021	170	0	634	-1960	4.02	4.02	4.02	4.02	-13.15	82.4	0.00
apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)														
40	56	402	1698	170	0	599	-1101	4.02	4.02	4.02	4.02	-7.39	46.3	0.00
41	56	866	1680	174	0	639	-1063	4.02	4.02	4.02	4.02	-7.13	44.7	0.00
42	56	1008	1672	403	0	1210	-1050	4.02	4.02	4.02	4.02	-7.05	44.1	0.00
43	56	35	1690	126	0	427	-1061	4.02	4.02	4.02	4.02	-7.12	44.6	0.00
44	56	1654	1655	189	0	730	-1016	4.02	4.02	4.02	4.02	-6.82	42.7	0.00
45	56	1043	1646	515	0	1446	-976	4.02	4.02	4.02	4.02	-6.55	41.0	0.00
46	56	771	1646	110	0	406	-958	4.02	4.02	4.02	4.02	-6.43	40.3	0.00
47	56	747	1638	94	0	347	-931	4.02	4.02	4.02	4.02	-6.25	39.1	0.00
49	56	593	1644	92	0	334	-944	4.02	4.02	4.02	4.02	-6.34	39.7	0.00
50	56	917	1637	105	0	395	-935	4.02	4.02	4.02	4.02	-6.27	39.3	0.00
51	56	795	1635	170	0	538	-927	4.02	4.02	4.02	4.02	-6.22	39.0	0.00
apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)														
40	113	402	1312	170	0	504	-251	4.02	4.02	4.02	4.02	-1.68	10.5	0.00
41	113	866	1294	174	0	540	-223	4.02	4.02	4.02	4.02	-1.49	9.4	0.00
42	113	1008	1286	403	0	982	-214	4.02	4.02	4.02	4.02	-1.44	9.0	0.00
43	113	35	1304	126	0	356	-216	4.02	4.02	4.02	4.02	-1.45	9.1	0.00
44	113	1654	1269	189	0	623	-190	4.02	4.02	4.02	4.02	-1.27	8.0	0.00
45	113	1043	1260	515	0	1155	-155	4.02	4.02	4.02	4.02	-1.04	6.5	0.00
46	113	771	1260	110	0	344	-137	4.02	4.02	4.02	4.02	-0.92	5.7	0.00
47	113	747	1252	94	0	294	-115	4.02	4.02	4.02	4.02	-0.77	4.8	0.00
49	113	593	1258	92	0	282	-124	4.02	4.02	4.02	4.02	-0.83	5.2	0.00
50	113	917	1251	105	0	336	-119	4.02	4.02	4.02	4.02	-0.80	5.0	0.00
51	113	795	1249	170	0	442	-112	4.02	4.02	4.02	4.02	-0.75	4.7	0.00
apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)														
40	170	402	926	170	0	408	382	4.02	4.02	4.02	4.02	-2.56	16.0	0.00
41	170	866	908	174	0	442	399	4.02	4.02	4.02	4.02	-2.68	16.8	0.00
42	170	1008	900	403	0	755	403	4.02	4.02	4.02	4.02	-2.71	17.0	0.00
43	170	35	918	126	0	285	412	4.02	4.02	4.02	4.02	-2.77	17.3	0.00
44	170	1654	883	189	0	516	418	4.02	4.02	4.02	4.02	-2.80	17.6	0.00
45	170	1043	874	515	0	864	448	4.02	4.02	4.02	4.02	-3.01	18.8	0.00
46	170	771	874	110	0	282	466	4.02	4.02	4.02	4.02	-3.13	19.6	0.00
47	170	747	866	94	0	242	484	4.02	4.02	4.02	4.02	-3.25	20.3	0.00
49	170	593	872	92	0	230	477	4.02	4.02	4.02	4.02	-3.20	20.1	0.00
50	170	917	865	105	0	276	478	4.02	4.02	4.02	4.02	-3.21	20.1	0.00
51	170	795	863	170	0	346	484	4.02	4.02	4.02	4.02	-3.25	20.4	0.00
apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)														
40	226	402	540	170	0	312	796	4.02	4.02	4.02	4.02	-5.34	33.5	0.00
41	226	866	522	174	0	343	803	4.02	4.02	4.02	4.02	-5.39	33.8	0.00
42	226	1008	514	403	0	527	803	4.02	4.02	4.02	4.02	-5.39	33.8	0.00
43	226	35	532	126	0	213	822	4.02	4.02	4.02	4.02	-5.51	34.5	0.00
44	226	1654	497	189	0	409	808	4.02	4.02	4.02	4.02	-5.42	34.0	0.00
45	226	1043	488	515	0	573	833	4.02	4.02	4.02	4.02	-5.59	35.0	0.00
46	226	771	488	110	0	220	851	4.02	4.02	4.02	4.02	-5.71	35.8	0.00
47	226	747	480	94	0	189	864	4.02	4.02	4.02	4.02	-5.80	36.3	0.00
49	226	593	486	92	0	178	861	4.02	4.02	4.02	4.02	-5.78	36.2	0.00
50	226	917	479	105	0	217	858	4.02	4.02	4.02	4.02	-5.76	36.1	0.00
51	226	795	477	170	0	250	863	4.02	4.02	4.02	4.02	-5.79	36.3	0.00
apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)														
40	282	402	154	170	0	216	993	4.02	4.02	4.02	4.02	-6.66	41.7	0.00
41	282	866	136	174	0	245	989	4.02	4.02	4.02	4.02	-6.64	41.6	0.00
42	282	1008	128	403	0	299	985	4.02	4.02	4.02	4.02	-6.61	41.4	0.00
43	282	35	146	126	0	142	1013	4.02	4.02	4.02	4.02	-6.80	42.6	0.00
44	282	1654	112	189	0	302	980	4.02	4.02	4.02	4.02	-6.58	41.2	0.00
45	282	1043	102	515	0	282	1000	4.02	4.02	4.02	4.02	-6.71	42.0	0.00
46	282	771	102	110	0	158	1018	4.02	4.02	4.02	4.02	-6.83	42.8	0.00
47	282	747	94	94	0	136	1026	4.02	4.02	4.02	4.02	-6.88	43.1	0.00

49	282	593	100	92	0	126	1027	4.02	4.02	4.02	4.02	-6.89	43.2	0.00
50	282	917	94	105	0	158	1020	4.02	4.02	4.02	4.02	-6.84	42.9	0.00
51	282	795	92	170	0	154	1024	4.02	4.02	4.02	4.02	-6.87	43.0	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	339	402	-231	170	0	120	971	4.02	4.02	4.02	4.02	-6.52	40.8	0.00
41	339	866	-249	174	0	146	957	4.02	4.02	4.02	4.02	-6.42	40.2	0.00
42	339	1008	-257	403	0	71	949	4.02	4.02	4.02	4.02	-6.36	39.9	0.00
43	339	35	-239	126	0	71	987	4.02	4.02	4.02	4.02	-6.62	41.5	0.00
44	339	1654	-274	189	0	195	934	4.02	4.02	4.02	4.02	-6.27	39.2	0.00
45	339	1043	-283	515	0	-10	949	4.02	4.02	4.02	4.02	-6.37	39.9	0.00
46	339	771	-283	110	0	96	967	4.02	4.02	4.02	4.02	-6.49	40.7	0.00
47	339	747	-291	94	0	83	970	4.02	4.02	4.02	4.02	-6.51	40.8	0.00
49	339	593	-285	92	0	74	975	4.02	4.02	4.02	4.02	-6.54	41.0	0.00
50	339	917	-292	105	0	99	964	4.02	4.02	4.02	4.02	-6.47	40.5	0.00
51	339	795	-294	170	0	58	967	4.02	4.02	4.02	4.02	-6.49	40.6	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	396	402	-617	170	0	24	732	4.02	4.02	4.02	4.02	-4.91	30.8	0.00
41	396	866	-635	174	0	48	707	4.02	4.02	4.02	4.02	-4.75	29.7	0.00
42	396	1008	-643	403	0	-156	694	4.02	4.02	4.02	4.02	-4.66	29.2	0.00
43	396	35	-625	126	0	-0	743	4.02	4.02	4.02	4.02	-4.98	31.2	0.00
44	396	1654	-660	189	0	88	670	4.02	4.02	4.02	4.02	-4.49	28.1	0.00
45	396	1043	-669	515	0	-301	680	4.02	4.02	4.02	4.02	-4.56	28.6	0.00
46	396	771	-669	110	0	34	698	4.02	4.02	4.02	4.02	-4.69	29.4	0.00
47	396	747	-677	94	0	30	696	4.02	4.02	4.02	4.02	-4.67	29.3	0.00
49	396	593	-671	92	0	22	704	4.02	4.02	4.02	4.02	-4.73	29.6	0.00
50	396	917	-678	105	0	40	689	4.02	4.02	4.02	4.02	-4.62	29.0	0.00
51	396	795	-680	170	0	-38	691	4.02	4.02	4.02	4.02	-4.64	29.1	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	452	402	-1003	170	0	-72	274	4.02	4.02	4.02	4.02	-1.84	11.5	0.00
41	452	866	-1021	174	0	-51	239	4.02	4.02	4.02	4.02	-1.61	10.1	0.00
42	452	1008	-1029	403	0	-384	222	4.02	4.02	4.02	4.02	-1.49	9.3	0.00
43	452	35	-1011	126	0	-72	280	4.02	4.02	4.02	4.02	-1.88	11.8	0.00
44	452	1654	-1046	189	0	-19	187	4.02	4.02	4.02	4.02	-1.26	7.9	0.00
45	452	1043	-1055	515	0	-592	193	4.02	4.02	4.02	4.02	-1.30	8.1	0.00
46	452	771	-1055	110	0	-28	211	4.02	4.02	4.02	4.02	-1.42	8.9	0.00
47	452	747	-1063	94	0	-23	204	4.02	4.02	4.02	4.02	-1.37	8.6	0.00
49	452	593	-1057	92	0	-30	216	4.02	4.02	4.02	4.02	-1.45	9.1	0.00
50	452	917	-1064	105	0	-19	197	4.02	4.02	4.02	4.02	-1.32	8.3	0.00
51	452	795	-1066	170	0	-134	198	4.02	4.02	4.02	4.02	-1.33	8.3	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	508	402	-1389	170	0	-168	-401	4.02	4.02	4.02	4.02	-2.69	16.9	0.00
41	508	866	-1407	174	0	-149	-447	4.02	4.02	4.02	4.02	-3.00	18.8	0.00
42	508	1008	-1415	403	0	-612	-469	4.02	4.02	4.02	4.02	-3.14	19.7	0.00
43	508	35	-1397	126	0	-143	-400	4.02	4.02	4.02	4.02	-2.69	16.8	0.00
44	508	1654	-1432	189	0	-126	-513	4.02	4.02	4.02	4.02	-3.44	21.6	0.00
45	508	1043	-1441	515	0	-883	-512	4.02	4.02	4.02	4.02	-3.43	21.5	0.00
46	508	771	-1441	110	0	-90	-494	4.02	4.02	4.02	4.02	-3.31	20.8	0.00
47	508	747	-1449	94	0	-76	-506	4.02	4.02	4.02	4.02	-3.39	21.3	0.00
49	508	593	-1443	92	0	-82	-491	4.02	4.02	4.02	4.02	-3.29	20.6	0.00
50	508	917	-1450	105	0	-78	-514	4.02	4.02	4.02	4.02	-3.45	21.6	0.00
51	508	795	-1452	170	0	-230	-514	4.02	4.02	4.02	4.02	-3.45	21.6	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	565	402	-1775	170	0	-264	-1295	4.02	4.02	4.02	4.02	-8.69	54.4	0.00
41	565	866	-1793	174	0	-248	-1351	4.02	4.02	4.02	4.02	-9.07	56.8	0.00
42	565	1008	-1801	403	0	-840	-1377	4.02	4.02	4.02	4.02	-9.24	57.9	0.00
43	565	35	-1783	126	0	-214	-1299	4.02	4.02	4.02	4.02	-8.72	54.6	0.00
44	565	1654	-1818	189	0	-233	-1431	4.02	4.02	4.02	4.02	-9.60	60.1	0.00
45	565	1043	-1827	515	0	-1174	-1435	4.02	4.02	4.02	4.02	-9.63	60.3	0.00
46	565	771	-1827	110	0	-152	-1417	4.02	4.02	4.02	4.02	-9.51	59.6	0.00
47	565	747	-1835	94	0	-128	-1434	4.02	4.02	4.02	4.02	-9.62	60.3	0.00
49	565	593	-1829	92	0	-134	-1415	4.02	4.02	4.02	4.02	-9.49	59.5	0.00
50	565	917	-1836	105	0	-137	-1442	4.02	4.02	4.02	4.02	-9.68	60.6	0.00
51	565	795	-1838	170	0	-326	-1443	4.02	4.02	4.02	4.02	-9.68	60.7	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

Nome travata: **trave_301_IP1** Descrizione: **Trave_3 7-12-17-22-32**
ASTA NUM. 2 NI 34 NF 36 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y Permanente qy tot.
qy medio: 375.00 308.00 683.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	[Fx]	[Fy]	[Fz]	[Mx]	[My]	Mz	[APOST]	[AANT]	AINF	ASUP	Sc	Sf	w
	cm	daN			daN*m			cm^2				daN/cm^2		mm
40	0	819	2002	1	0	-113	-2010	4.02	4.02	4.02	4.02	-13.49	84.5	0.00
41	0	1030	2003	7	0	-72	-2016	4.02	4.02	4.02	4.02	-13.53	84.7	0.00
42	0	1174	2001	47	0	-168	-2012	4.02	4.02	4.02	4.02	-13.50	84.6	0.00
43	0	606	2000	-5	0	-122	-2005	4.02	4.02	4.02	4.02	-13.45	84.3	0.00
44	0	1401	2005	17	0	-8	-2026	4.02	4.02	4.02	4.02	-13.59	85.2	0.00
45	0	1198	1999	74	0	-214	-2009	4.02	4.02	4.02	4.02	-13.48	84.4	0.00
46	0	915	2002	5	0	-42	-2016	4.02	4.02	4.02	4.02	-13.53	84.7	0.00
47	0	886	2002	5	0	-35	-2015	4.02	4.02	4.02	4.02	-13.52	84.7	0.00
49	0	816	2001	2	0	-49	-2013	4.02	4.02	4.02	4.02	-13.51	84.6	0.00
50	0	975	2002	7	0	-26	-2017	4.02	4.02	4.02	4.02	-13.53	84.8	0.00
51	0	934	2001	18	0	-67	-2014	4.02	4.02	4.02	4.02	-13.51	84.7	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	56	819	1616	1	0	-113	-988	4.02	4.02	4.02	4.02	-6.63	41.5	0.00
41	56	1030	1617	7	0	-75	-993	4.02	4.02	4.02	4.02	-6.66	41.7	0.00
42	56	1174	1615	47	0	-195	-990	4.02	4.02	4.02	4.02	-6.64	41.6	0.00
43	56	606	1614	-5	0	-119	-984	4.02	4.02	4.02	4.02	-6.60	41.3	0.00
44	56	1401	1619	17	0	-17	-1002	4.02	4.02	4.02	4.02	-6.73	42.1	0.00
45	56	1198	1613	74	0	-256	-988	4.02	4.02	4.02	4.02	-6.63	41.5	0.00

46	56	915	1616	5	0	-45	-994	4.02	4.02	4.02	4.02	-6.67	41.8	0.00
47	56	886	1616	5	0	-38	-993	4.02	4.02	4.02	4.02	-6.66	41.7	0.00
49	56	816	1615	2	0	-50	-991	4.02	4.02	4.02	4.02	-6.65	41.7	0.00
50	56	975	1616	7	0	-30	-995	4.02	4.02	4.02	4.02	-6.68	41.8	0.00
51	56	934	1615	18	0	-77	-993	4.02	4.02	4.02	4.02	-6.66	41.7	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	113	819	1230	1	0	-114	-184	4.02	4.02	4.02	4.02	-1.23	7.7	0.00
41	113	1030	1231	7	0	-79	-188	4.02	4.02	4.02	4.02	-1.26	7.9	0.00
42	113	1174	1229	47	0	-222	-187	4.02	4.02	4.02	4.02	-1.25	7.8	0.00
43	113	606	1228	-5	0	-117	-180	4.02	4.02	4.02	4.02	-1.21	7.6	0.00
44	113	1401	1233	17	0	-27	-197	4.02	4.02	4.02	4.02	-1.32	8.3	0.00
45	113	1198	1227	74	0	-297	-186	4.02	4.02	4.02	4.02	-1.25	7.8	0.00
46	113	915	1230	5	0	-48	-190	4.02	4.02	4.02	4.02	-1.27	8.0	0.00
47	113	886	1230	5	0	-40	-189	4.02	4.02	4.02	4.02	-1.27	8.0	0.00
49	113	816	1229	2	0	-52	-188	4.02	4.02	4.02	4.02	-1.26	7.9	0.00
50	113	975	1230	7	0	-34	-191	4.02	4.02	4.02	4.02	-1.28	8.0	0.00
51	113	934	1229	18	0	-88	-189	4.02	4.02	4.02	4.02	-1.27	8.0	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	170	819	844	1	0	-114	403	4.02	4.02	4.02	4.02	-2.70	16.9	0.00
41	170	1030	845	7	0	-83	398	4.02	4.02	4.02	4.02	-2.67	16.7	0.00
42	170	1174	843	47	0	-248	399	4.02	4.02	4.02	4.02	-2.68	16.8	0.00
43	170	606	843	-5	0	-114	405	4.02	4.02	4.02	4.02	-2.72	17.0	0.00
44	170	1401	847	17	0	-36	391	4.02	4.02	4.02	4.02	-2.62	16.4	0.00
45	170	1198	841	74	0	-339	399	4.02	4.02	4.02	4.02	-2.67	16.8	0.00
46	170	915	844	5	0	-51	396	4.02	4.02	4.02	4.02	-2.66	16.6	0.00
47	170	886	844	5	0	-43	396	4.02	4.02	4.02	4.02	-2.66	16.7	0.00
49	170	816	843	2	0	-53	398	4.02	4.02	4.02	4.02	-2.67	16.7	0.00
50	170	975	844	7	0	-37	395	4.02	4.02	4.02	4.02	-2.65	16.6	0.00
51	170	934	843	18	0	-98	396	4.02	4.02	4.02	4.02	-2.66	16.7	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	226	819	458	1	0	-114	771	4.02	4.02	4.02	4.02	-5.17	32.4	0.00
41	226	1030	459	7	0	-87	767	4.02	4.02	4.02	4.02	-5.15	32.2	0.00
42	226	1174	457	47	0	-275	767	4.02	4.02	4.02	4.02	-5.15	32.2	0.00
43	226	606	457	-5	0	-112	772	4.02	4.02	4.02	4.02	-5.18	32.5	0.00
44	226	1401	461	17	0	-45	761	4.02	4.02	4.02	4.02	-5.10	32.0	0.00
45	226	1198	455	74	0	-380	765	4.02	4.02	4.02	4.02	-5.13	32.2	0.00
46	226	915	458	5	0	-54	764	4.02	4.02	4.02	4.02	-5.13	32.1	0.00
47	226	886	458	5	0	-45	764	4.02	4.02	4.02	4.02	-5.13	32.1	0.00
49	226	816	457	2	0	-54	765	4.02	4.02	4.02	4.02	-5.14	32.2	0.00
50	226	975	458	7	0	-41	763	4.02	4.02	4.02	4.02	-5.12	32.1	0.00
51	226	934	457	18	0	-108	764	4.02	4.02	4.02	4.02	-5.12	32.1	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	282	819	72	1	0	-114	921	4.02	4.02	4.02	4.02	-6.18	38.7	0.00
41	282	1030	74	7	0	-91	918	4.02	4.02	4.02	4.02	-6.16	38.6	0.00
42	282	1174	72	47	0	-302	916	4.02	4.02	4.02	4.02	-6.15	38.5	0.00
43	282	606	71	-5	0	-109	921	4.02	4.02	4.02	4.02	-6.18	38.7	0.00
44	282	1401	76	17	0	-55	912	4.02	4.02	4.02	4.02	-6.12	38.3	0.00
45	282	1198	70	74	0	-422	913	4.02	4.02	4.02	4.02	-6.13	38.4	0.00
46	282	915	72	5	0	-56	914	4.02	4.02	4.02	4.02	-6.13	38.4	0.00
47	282	886	72	5	0	-48	914	4.02	4.02	4.02	4.02	-6.13	38.4	0.00
49	282	816	72	2	0	-56	915	4.02	4.02	4.02	4.02	-6.14	38.5	0.00
50	282	975	72	7	0	-45	913	4.02	4.02	4.02	4.02	-6.13	38.4	0.00
51	282	934	72	18	0	-118	913	4.02	4.02	4.02	4.02	-6.13	38.4	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	339	819	-313	1	0	-115	853	4.02	4.02	4.02	4.02	-5.72	35.9	0.00
41	339	1030	-312	7	0	-94	851	4.02	4.02	4.02	4.02	-5.71	35.8	0.00
42	339	1174	-314	47	0	-329	848	4.02	4.02	4.02	4.02	-5.69	35.6	0.00
43	339	606	-315	-5	0	-107	853	4.02	4.02	4.02	4.02	-5.72	35.8	0.00
44	339	1401	-310	17	0	-64	846	4.02	4.02	4.02	4.02	-5.68	35.6	0.00
45	339	1198	-316	74	0	-463	844	4.02	4.02	4.02	4.02	-5.66	35.5	0.00
46	339	915	-313	5	0	-59	846	4.02	4.02	4.02	4.02	-5.68	35.5	0.00
47	339	886	-313	5	0	-50	846	4.02	4.02	4.02	4.02	-5.67	35.5	0.00
49	339	816	-314	2	0	-57	846	4.02	4.02	4.02	4.02	-5.68	35.6	0.00
50	339	975	-313	7	0	-49	845	4.02	4.02	4.02	4.02	-5.67	35.5	0.00
51	339	934	-314	18	0	-129	844	4.02	4.02	4.02	4.02	-5.66	35.5	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	396	819	-699	1	0	-115	567	4.02	4.02	4.02	4.02	-3.80	23.8	0.00
41	396	1030	-698	7	0	-98	565	4.02	4.02	4.02	4.02	-3.79	23.8	0.00
42	396	1174	-700	47	0	-356	562	4.02	4.02	4.02	4.02	-3.77	23.6	0.00
43	396	606	-701	-5	0	-104	566	4.02	4.02	4.02	4.02	-3.80	23.8	0.00
44	396	1401	-696	17	0	-74	562	4.02	4.02	4.02	4.02	-3.77	23.6	0.00
45	396	1198	-702	74	0	-505	556	4.02	4.02	4.02	4.02	-3.73	23.4	0.00
46	396	915	-699	5	0	-62	560	4.02	4.02	4.02	4.02	-3.76	23.5	0.00
47	396	886	-699	5	0	-53	559	4.02	4.02	4.02	4.02	-3.75	23.5	0.00
49	396	816	-700	2	0	-59	560	4.02	4.02	4.02	4.02	-3.76	23.5	0.00
50	396	975	-699	7	0	-53	559	4.02	4.02	4.02	4.02	-3.75	23.5	0.00
51	396	934	-700	18	0	-139	557	4.02	4.02	4.02	4.02	-3.74	23.4	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	452	819	-1085	1	0	-115	63	4.02	4.02	4.02	4.02	-0.42	2.6	0.00
41	452	1030	-1084	7	0	-102	62	4.02	4.02	4.02	4.02	-0.41	2.6	0.00
42	452	1174	-1086	47	0	-382	57	4.02	4.02	4.02	4.02	-0.38	2.4	0.00
43	452	606	-1086	-5	0	-102	61	4.02	4.02	4.02	4.02	-0.41	2.6	0.00
44	452	1401	-1082	17	0	-83	59	4.02	4.02	4.02	4.02	-0.40	2.5	0.00
45	452	1198	-1088	74	0	-546	50	4.02	4.02	4.02	4.02	-0.34	2.1	0.00
46	452	915	-1085	5	0	-65	55	4.02	4.02	4.02	4.02	-0.37	2.3	0.00
47	452	886	-1085	5	0	-56	55	4.02	4.02	4.02	4.02	-0.37	2.3	0.00
49	452	816	-1086	2	0	-60	55	4.02	4.02	4.02	4.02	-0.37	2.3	0.00
50	452	975	-1085	7	0	-56	54	4.02	4.02	4.02	4.02	-0.37	2.3	0.00
51	452	934	-1086	18	0	-149	53	4.02	4.02	4.02	4.02	-0.35	2.2	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	508	819	-1471	1	0	-116	-659	4.02	4.02	4.02	4.02	-4.42	27.7	0.00
41	508	1030	-1470	7	0	-106	-660	4.02	4.02	4.02	4.02	-4.43	27.7	0.00
42	508	1174	-1472	47	0	-409	-665	4.02	4.02	4.02	4.02	-4.47	28.0	0.00
43	508	606	-1472	-5	0	-99	-662	4.02	4.02	4.02	4.02	-4.44	27.8	0.00

44	508	1401	-1468	17	0	-92	-661	4.02	4.02	4.02	4.02	-4.44	27.8	0.00
45	508	1198	-1474	74	0	-588	-673	4.02	4.02	4.02	4.02	-4.52	28.3	0.00
46	508	915	-1471	5	0	-68	-667	4.02	4.02	4.02	4.02	-4.47	28.0	0.00
47	508	886	-1471	5	0	-58	-668	4.02	4.02	4.02	4.02	-4.48	28.1	0.00
49	508	816	-1472	2	0	-62	-667	4.02	4.02	4.02	4.02	-4.48	28.0	0.00
50	508	975	-1471	7	0	-60	-668	4.02	4.02	4.02	4.02	-4.48	28.1	0.00
51	508	934	-1472	18	0	-159	-670	4.02	4.02	4.02	4.02	-4.50	28.2	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	565	819	-1857	1	0	-116	-1599	4.02	4.02	4.02	4.02	-10.73	67.2	0.00
41	565	1030	-1856	7	0	-109	-1599	4.02	4.02	4.02	4.02	-10.73	67.2	0.00
42	565	1174	-1858	47	0	-436	-1606	4.02	4.02	4.02	4.02	-10.78	67.5	0.00
43	565	606	-1858	-5	0	-96	-1603	4.02	4.02	4.02	4.02	-10.76	67.4	0.00
44	565	1401	-1854	17	0	-102	-1600	4.02	4.02	4.02	4.02	-10.74	67.2	0.00
45	565	1198	-1860	74	0	-629	-1615	4.02	4.02	4.02	4.02	-10.84	67.9	0.00
46	565	915	-1857	5	0	-70	-1607	4.02	4.02	4.02	4.02	-10.78	67.5	0.00
47	565	886	-1857	5	0	-61	-1608	4.02	4.02	4.02	4.02	-10.79	67.6	0.00
49	565	816	-1858	2	0	-63	-1608	4.02	4.02	4.02	4.02	-10.79	67.6	0.00
50	565	975	-1857	7	0	-64	-1608	4.02	4.02	4.02	4.02	-10.79	67.6	0.00
51	565	934	-1858	18	0	-170	-1611	4.02	4.02	4.02	4.02	-10.81	67.7	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

Nome travata: **trave_301_IP1** Descrizione: **Trave_3 7-12-17-22-32**
ASTA NUM. 3 NI 36 NF 38 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y Permanente qy tot.
qy medio: 375.00 308.00 683.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	[Fx]	[Fy]	[Fz]	[Mx]	[My]	Mz	[APOST]	[AANT]	AINF	ASUP	Sc	Sf	w
	--													--
	cm		daN			daN*m				cm^2			daN/cm^2	mm
40	0	1351	1919	-8	0	-134	-1795	4.02	4.02	4.02	4.02	-12.04	75.4	0.00
41	0	1293	1923	5	0	-93	-1807	4.02	4.02	4.02	4.02	-12.12	75.9	0.00
42	0	1434	1928	-38	0	-426	-1821	4.02	4.02	4.02	4.02	-12.22	76.5	0.00
43	0	1301	1916	-18	0	-142	-1788	4.02	4.02	4.02	4.02	-12.00	75.2	0.00
44	0	1218	1930	27	0	-26	-1828	4.02	4.02	4.02	4.02	-12.27	76.8	0.00
45	0	1439	1931	-68	0	-628	-1833	4.02	4.02	4.02	4.02	-12.30	77.0	0.00
46	0	1149	1923	2	0	-59	-1810	4.02	4.02	4.02	4.02	-12.15	76.1	0.00
47	0	1114	1923	2	0	-51	-1811	4.02	4.02	4.02	4.02	-12.15	76.1	0.00
49	0	1133	1921	-2	0	-65	-1807	4.02	4.02	4.02	4.02	-12.12	75.9	0.00
50	0	1117	1924	7	0	-42	-1815	4.02	4.02	4.02	4.02	-12.18	76.3	0.00
51	0	1161	1924	-12	0	-162	-1816	4.02	4.02	4.02	4.02	-12.19	76.3	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	57	1351	1533	-8	0	-130	-820	4.02	4.02	4.02	4.02	-5.50	34.5	0.00
41	57	1293	1537	5	0	-95	-829	4.02	4.02	4.02	4.02	-5.57	34.9	0.00
42	57	1434	1542	-38	0	-404	-841	4.02	4.02	4.02	4.02	-5.64	35.3	0.00
43	57	1301	1530	-18	0	-131	-815	4.02	4.02	4.02	4.02	-5.47	34.2	0.00
44	57	1218	1544	27	0	-41	-847	4.02	4.02	4.02	4.02	-5.68	35.6	0.00
45	57	1439	1545	-68	0	-589	-851	4.02	4.02	4.02	4.02	-5.71	35.8	0.00
46	57	1149	1537	2	0	-61	-833	4.02	4.02	4.02	4.02	-5.59	35.0	0.00
47	57	1114	1537	2	0	-52	-834	4.02	4.02	4.02	4.02	-5.60	35.0	0.00
49	57	1133	1535	-2	0	-64	-831	4.02	4.02	4.02	4.02	-5.57	34.9	0.00
50	57	1117	1538	7	0	-46	-837	4.02	4.02	4.02	4.02	-5.62	35.2	0.00
51	57	1161	1538	-12	0	-155	-838	4.02	4.02	4.02	4.02	-5.62	35.2	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	113	1351	1147	-8	0	-125	-63	4.02	4.02	4.02	4.02	-0.42	2.6	0.00
41	113	1293	1151	5	0	-98	-70	4.02	4.02	4.02	4.02	-0.47	2.9	0.00
42	113	1434	1156	-38	0	-383	-79	4.02	4.02	4.02	4.02	-0.53	3.3	0.00
43	113	1301	1144	-18	0	-121	-59	4.02	4.02	4.02	4.02	-0.40	2.5	0.00
44	113	1218	1158	27	0	-56	-83	4.02	4.02	4.02	4.02	-0.56	3.5	0.00
45	113	1439	1159	-68	0	-551	-87	4.02	4.02	4.02	4.02	-0.59	3.7	0.00
46	113	1149	1151	2	0	-62	-74	4.02	4.02	4.02	4.02	-0.49	3.1	0.00
47	113	1114	1151	2	0	-53	-75	4.02	4.02	4.02	4.02	-0.50	3.1	0.00
49	113	1133	1149	-2	0	-62	-72	4.02	4.02	4.02	4.02	-0.48	3.0	0.00
50	113	1117	1152	7	0	-49	-77	4.02	4.02	4.02	4.02	-0.52	3.2	0.00
51	113	1161	1152	-12	0	-148	-78	4.02	4.02	4.02	4.02	-0.52	3.3	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	170	1351	761	-8	0	-120	477	4.02	4.02	4.02	4.02	-3.20	20.0	0.00
41	170	1293	765	5	0	-100	472	4.02	4.02	4.02	4.02	-3.16	19.8	0.00
42	170	1434	770	-38	0	-362	465	4.02	4.02	4.02	4.02	-3.12	19.6	0.00
43	170	1301	758	-18	0	-110	478	4.02	4.02	4.02	4.02	-3.21	20.1	0.00
44	170	1218	772	27	0	-72	462	4.02	4.02	4.02	4.02	-3.10	19.4	0.00
45	170	1439	773	-68	0	-513	458	4.02	4.02	4.02	4.02	-3.08	19.3	0.00
46	170	1149	765	2	0	-63	468	4.02	4.02	4.02	4.02	-3.14	19.7	0.00
47	170	1114	765	2	0	-54	466	4.02	4.02	4.02	4.02	-3.13	19.6	0.00
49	170	1133	763	-2	0	-61	468	4.02	4.02	4.02	4.02	-3.14	19.7	0.00
50	170	1117	766	7	0	-53	465	4.02	4.02	4.02	4.02	-3.12	19.5	0.00
51	170	1161	766	-12	0	-141	464	4.02	4.02	4.02	4.02	-3.12	19.5	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	226	1351	375	-8	0	-115	798	4.02	4.02	4.02	4.02	-5.35	33.5	0.00
41	226	1293	379	5	0	-103	795	4.02	4.02	4.02	4.02	-5.33	33.4	0.00
42	226	1434	384	-38	0	-340	791	4.02	4.02	4.02	4.02	-5.31	33.3	0.00
43	226	1301	372	-18	0	-100	798	4.02	4.02	4.02	4.02	-5.35	33.5	0.00
44	226	1218	386	27	0	-87	790	4.02	4.02	4.02	4.02	-5.30	33.2	0.00
45	226	1439	387	-68	0	-475	786	4.02	4.02	4.02	4.02	-5.28	33.0	0.00
46	226	1149	379	2	0	-65	791	4.02	4.02	4.02	4.02	-5.31	33.2	0.00
47	226	1114	379	2	0	-55	789	4.02	4.02	4.02	4.02	-5.30	33.2	0.00
49	226	1133	377	-2	0	-60	791	4.02	4.02	4.02	4.02	-5.30	33.2	0.00
50	226	1117	380	7	0	-57	789	4.02	4.02	4.02	4.02	-5.29	33.2	0.00
51	226	1161	380	-12	0	-135	788	4.02	4.02	4.02	4.02	-5.29	33.1	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	283	1351	-10	-8	0	-111	901	4.02	4.02	4.02	4.02	-6.04	37.9	0.00
41	283	1293	-6	5	0	-105	900	4.02	4.02	4.02	4.02	-6.04	37.8	0.00

42	283	1434	-2	-38	0	-319	899	4.02	4.02	4.02	4.02	-6.03	37.8	0.00
43	283	1301	-14	-18	0	-89	899	4.02	4.02	4.02	4.02	-6.03	37.8	0.00
44	283	1218	0	27	0	-102	899	4.02	4.02	4.02	4.02	-6.03	37.8	0.00
45	283	1439	2	-68	0	-437	896	4.02	4.02	4.02	4.02	-6.01	37.7	0.00
46	283	1149	-6	2	0	-66	896	4.02	4.02	4.02	4.02	-6.01	37.7	0.00
47	283	1114	-6	2	0	-57	894	4.02	4.02	4.02	4.02	-6.00	37.6	0.00
49	283	1133	-8	-2	0	-58	895	4.02	4.02	4.02	4.02	-6.00	37.6	0.00
50	283	1117	-6	7	0	-61	895	4.02	4.02	4.02	4.02	-6.00	37.6	0.00
51	283	1161	-6	-12	0	-128	894	4.02	4.02	4.02	4.02	-6.00	37.6	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	339	1351	-396	-8	0	-106	786	4.02	4.02	4.02	4.02	-5.27	33.0	0.00
41	339	1293	-392	5	0	-108	788	4.02	4.02	4.02	4.02	-5.29	33.1	0.00
42	339	1434	-387	-38	0	-297	789	4.02	4.02	4.02	4.02	-5.30	33.2	0.00
43	339	1301	-399	-18	0	-79	782	4.02	4.02	4.02	4.02	-5.25	32.9	0.00
44	339	1218	-385	27	0	-117	790	4.02	4.02	4.02	4.02	-5.30	33.2	0.00
45	339	1439	-384	-68	0	-398	788	4.02	4.02	4.02	4.02	-5.28	33.1	0.00
46	339	1149	-392	2	0	-68	783	4.02	4.02	4.02	4.02	-5.25	32.9	0.00
47	339	1114	-392	2	0	-58	781	4.02	4.02	4.02	4.02	-5.24	32.8	0.00
49	339	1133	-394	-2	0	-57	781	4.02	4.02	4.02	4.02	-5.24	32.8	0.00
50	339	1117	-391	7	0	-64	783	4.02	4.02	4.02	4.02	-5.25	32.9	0.00
51	339	1161	-391	-12	0	-121	782	4.02	4.02	4.02	4.02	-5.25	32.9	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	396	1351	-782	-8	0	-101	453	4.02	4.02	4.02	4.02	-3.04	19.0	0.00
41	396	1293	-778	5	0	-111	457	4.02	4.02	4.02	4.02	-3.07	19.2	0.00
42	396	1434	-773	-38	0	-276	461	4.02	4.02	4.02	4.02	-3.10	19.4	0.00
43	396	1301	-785	-18	0	-69	447	4.02	4.02	4.02	4.02	-3.00	18.8	0.00
44	396	1218	-771	27	0	-132	463	4.02	4.02	4.02	4.02	-3.11	19.5	0.00
45	396	1439	-770	-68	0	-360	461	4.02	4.02	4.02	4.02	-3.09	19.4	0.00
46	396	1149	-778	2	0	-69	452	4.02	4.02	4.02	4.02	-3.03	19.0	0.00
47	396	1114	-778	2	0	-59	450	4.02	4.02	4.02	4.02	-3.02	18.9	0.00
49	396	1133	-780	-2	0	-56	449	4.02	4.02	4.02	4.02	-3.02	18.9	0.00
50	396	1117	-777	7	0	-68	453	4.02	4.02	4.02	4.02	-3.04	19.0	0.00
51	396	1161	-777	-12	0	-114	452	4.02	4.02	4.02	4.02	-3.04	19.0	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	452	1351	-1168	-8	0	-96	-98	4.02	4.02	4.02	4.02	-0.66	4.1	0.00
41	452	1293	-1164	5	0	-113	-92	4.02	4.02	4.02	4.02	-0.61	3.8	0.00
42	452	1434	-1159	-38	0	-255	-85	4.02	4.02	4.02	4.02	-0.57	3.6	0.00
43	452	1301	-1171	-18	0	-58	-105	4.02	4.02	4.02	4.02	-0.71	4.4	0.00
44	452	1218	-1157	27	0	-147	-81	4.02	4.02	4.02	4.02	-0.55	3.4	0.00
45	452	1439	-1156	-68	0	-322	-83	4.02	4.02	4.02	4.02	-0.56	3.5	0.00
46	452	1149	-1164	2	0	-71	-97	4.02	4.02	4.02	4.02	-0.65	4.1	0.00
47	452	1114	-1164	2	0	-60	-99	4.02	4.02	4.02	4.02	-0.66	4.2	0.00
49	452	1133	-1166	-2	0	-54	-100	4.02	4.02	4.02	4.02	-0.67	4.2	0.00
50	452	1117	-1163	7	0	-72	-96	4.02	4.02	4.02	4.02	-0.64	4.0	0.00
51	452	1161	-1163	-12	0	-107	-96	4.02	4.02	4.02	4.02	-0.64	4.0	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	509	1351	-1554	-8	0	-91	-867	4.02	4.02	4.02	4.02	-5.82	36.4	0.00
41	509	1293	-1550	5	0	-116	-858	4.02	4.02	4.02	4.02	-5.76	36.1	0.00
42	509	1434	-1545	-38	0	-233	-849	4.02	4.02	4.02	4.02	-5.70	35.7	0.00
43	509	1301	-1557	-18	0	-48	-876	4.02	4.02	4.02	4.02	-5.88	36.8	0.00
44	509	1218	-1543	27	0	-162	-844	4.02	4.02	4.02	4.02	-5.66	35.5	0.00
45	509	1439	-1542	-68	0	-284	-846	4.02	4.02	4.02	4.02	-5.67	35.5	0.00
46	509	1149	-1550	2	0	-72	-864	4.02	4.02	4.02	4.02	-5.80	36.3	0.00
47	509	1114	-1550	2	0	-61	-866	4.02	4.02	4.02	4.02	-5.81	36.4	0.00
49	509	1133	-1552	-2	0	-53	-868	4.02	4.02	4.02	4.02	-5.83	36.5	0.00
50	509	1117	-1549	7	0	-76	-862	4.02	4.02	4.02	4.02	-5.78	36.2	0.00
51	509	1161	-1549	-12	0	-100	-862	4.02	4.02	4.02	4.02	-5.78	36.2	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	565	1351	-1940	-8	0	-87	-1854	4.02	4.02	4.02	4.02	-12.44	77.9	0.00
41	565	1293	-1936	5	0	-118	-1843	4.02	4.02	4.02	4.02	-12.37	77.5	0.00
42	565	1434	-1931	-38	0	-212	-1831	4.02	4.02	4.02	4.02	-12.29	77.0	0.00
43	565	1301	-1943	-18	0	-37	-1865	4.02	4.02	4.02	4.02	-12.51	78.4	0.00
44	565	1218	-1929	27	0	-178	-1825	4.02	4.02	4.02	4.02	-12.25	76.7	0.00
45	565	1439	-1928	-68	0	-246	-1826	4.02	4.02	4.02	4.02	-12.25	76.7	0.00
46	565	1149	-1936	2	0	-73	-1849	4.02	4.02	4.02	4.02	-12.41	77.7	0.00
47	565	1114	-1936	2	0	-62	-1851	4.02	4.02	4.02	4.02	-12.42	77.8	0.00
49	565	1133	-1938	-2	0	-52	-1854	4.02	4.02	4.02	4.02	-12.44	77.9	0.00
50	565	1117	-1935	7	0	-80	-1846	4.02	4.02	4.02	4.02	-12.39	77.6	0.00
51	565	1161	-1935	-12	0	-93	-1846	4.02	4.02	4.02	4.02	-12.39	77.6	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

Nome travata: **trave_301_IP1** Descrizione: **Trave_3 7-12-17-22-32**
ASTA NUM. 4 NI 38 NF 32 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y Permanente qy tot.
qy medio: 375.00 308.00 683.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	[Fx]	[Fy]	[Fz]	[Mx]	[My]	Mz	[APOST]	[AANT]	AINF	ASUP	Sc	Sf	w
	--													--
	cm		daN			daN*m				cm^2			daN/cm^2	mm
40	0	1711	1840	-358	0	-467	-1599	4.02	4.02	4.02	4.02	-10.73	67.2	0.00
41	0	1381	1844	-289	0	-394	-1578	4.02	4.02	4.02	4.02	-10.59	66.3	0.00
42	0	1526	1855	-504	0	-924	-1613	4.02	4.02	4.02	4.02	-10.82	67.8	0.00
43	0	1811	1857	-344	0	-430	-1640	4.02	4.02	4.02	4.02	-11.00	68.9	0.00
44	0	856	1848	-182	0	-284	-1536	4.02	4.02	4.02	4.02	-10.31	64.6	0.00
45	0	1501	1881	-586	0	-1191	-1663	4.02	4.02	4.02	4.02	-11.16	69.9	0.00
46	0	1189	1876	-191	0	-257	-1622	4.02	4.02	4.02	4.02	-10.88	68.2	0.00
47	0	1141	1884	-167	0	-223	-1632	4.02	4.02	4.02	4.02	-10.95	68.6	0.00
49	0	1251	1882	-190	0	-247	-1639	4.02	4.02	4.02	4.02	-11.00	68.9	0.00
50	0	1059	1881	-158	0	-218	-1619	4.02	4.02	4.02	4.02	-10.86	68.0	0.00
51	0	1189	1887	-239	0	-399	-1644	4.02	4.02	4.02	4.02	-11.03	69.1	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	56	1711	1454	-358	0	-264	-669	4.02	4.02	4.02	4.02	-4.49	28.1	0.00
41	56	1381	1458	-289	0	-230	-645	4.02	4.02	4.02	4.02	-4.33	27.1	0.00
42	56	1526	1469	-504	0	-639	-674	4.02	4.02	4.02	4.02	-4.52	28.3	0.00
43	56	1811	1471	-344	0	-236	-700	4.02	4.02	4.02	4.02	-4.70	29.4	0.00
44	56	856	1462	-182	0	-181	-601	4.02	4.02	4.02	4.02	-4.03	25.3	0.00
45	56	1501	1495	-586	0	-860	-709	4.02	4.02	4.02	4.02	-4.76	29.8	0.00
46	56	1189	1490	-191	0	-149	-671	4.02	4.02	4.02	4.02	-4.50	28.2	0.00
47	56	1141	1498	-167	0	-129	-677	4.02	4.02	4.02	4.02	-4.54	28.4	0.00
49	56	1251	1496	-190	0	-140	-685	4.02	4.02	4.02	4.02	-4.59	28.8	0.00
50	56	1059	1495	-158	0	-129	-665	4.02	4.02	4.02	4.02	-4.47	28.0	0.00
51	56	1189	1501	-239	0	-265	-687	4.02	4.02	4.02	4.02	-4.61	28.9	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	113	1711	1068	-358	0	-62	44	4.02	4.02	4.02	4.02	-0.29	1.8	0.00
41	113	1381	1072	-289	0	-67	70	4.02	4.02	4.02	4.02	-0.47	2.9	0.00
42	113	1526	1083	-504	0	-354	47	4.02	4.02	4.02	4.02	-0.31	2.0	0.00
43	113	1811	1085	-344	0	-41	22	4.02	4.02	4.02	4.02	-0.15	0.9	0.00
44	113	856	1076	-182	0	-78	116	4.02	4.02	4.02	4.02	-0.78	4.9	0.00
45	113	1501	1109	-586	0	-528	27	4.02	4.02	4.02	4.02	-0.18	1.1	0.00
46	113	1189	1104	-191	0	-41	62	4.02	4.02	4.02	4.02	-0.41	2.6	0.00
47	113	1141	1112	-167	0	-34	61	4.02	4.02	4.02	4.02	-0.41	2.5	0.00
49	113	1251	1110	-190	0	-32	52	4.02	4.02	4.02	4.02	-0.35	2.2	0.00
50	113	1059	1109	-158	0	-40	70	4.02	4.02	4.02	4.02	-0.47	2.9	0.00
51	113	1189	1115	-239	0	-130	53	4.02	4.02	4.02	4.02	-0.35	2.2	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	169	1711	682	-358	0	141	538	4.02	4.02	4.02	4.02	-3.61	22.6	0.00
41	169	1381	686	-289	0	96	567	4.02	4.02	4.02	4.02	-3.80	23.8	0.00
42	169	1526	697	-504	0	-69	550	4.02	4.02	4.02	4.02	-3.69	23.1	0.00
43	169	1811	699	-344	0	153	525	4.02	4.02	4.02	4.02	-3.53	22.1	0.00
44	169	856	690	-182	0	25	615	4.02	4.02	4.02	4.02	-4.13	25.8	0.00
45	169	1501	723	-586	0	-197	545	4.02	4.02	4.02	4.02	-3.66	22.9	0.00
46	169	1189	718	-191	0	67	577	4.02	4.02	4.02	4.02	-3.87	24.2	0.00
47	169	1141	726	-167	0	60	580	4.02	4.02	4.02	4.02	-3.89	24.4	0.00
49	169	1251	724	-190	0	75	570	4.02	4.02	4.02	4.02	-3.83	24.0	0.00
50	169	1059	723	-158	0	49	588	4.02	4.02	4.02	4.02	-3.94	24.7	0.00
51	169	1189	729	-239	0	5	574	4.02	4.02	4.02	4.02	-3.85	24.1	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	226	1711	296	-358	0	343	815	4.02	4.02	4.02	4.02	-5.47	34.2	0.00
41	226	1381	300	-289	0	259	846	4.02	4.02	4.02	4.02	-5.68	35.6	0.00
42	226	1526	311	-504	0	215	835	4.02	4.02	4.02	4.02	-5.60	35.1	0.00
43	226	1811	313	-344	0	347	811	4.02	4.02	4.02	4.02	-5.44	34.1	0.00
44	226	856	304	-182	0	128	896	4.02	4.02	4.02	4.02	-6.01	37.7	0.00
45	226	1501	337	-586	0	135	845	4.02	4.02	4.02	4.02	-5.67	35.5	0.00
46	226	1189	332	-191	0	175	874	4.02	4.02	4.02	4.02	-5.86	36.7	0.00
47	226	1141	340	-167	0	154	881	4.02	4.02	4.02	4.02	-5.91	37.0	0.00
49	226	1251	338	-190	0	182	871	4.02	4.02	4.02	4.02	-5.84	36.6	0.00
50	226	1059	337	-158	0	138	887	4.02	4.02	4.02	4.02	-5.95	37.3	0.00
51	226	1189	343	-239	0	140	877	4.02	4.02	4.02	4.02	-5.89	36.9	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	282	1711	-90	-358	0	546	873	4.02	4.02	4.02	4.02	-5.86	36.7	0.00
41	282	1381	-86	-289	0	422	907	4.02	4.02	4.02	4.02	-6.09	38.1	0.00
42	282	1526	-74	-504	0	500	901	4.02	4.02	4.02	4.02	-6.05	37.9	0.00
43	282	1811	-72	-344	0	541	879	4.02	4.02	4.02	4.02	-5.90	36.9	0.00
44	282	856	-82	-182	0	231	959	4.02	4.02	4.02	4.02	-6.43	40.3	0.00
45	282	1501	-48	-586	0	466	926	4.02	4.02	4.02	4.02	-6.22	38.9	0.00
46	282	1189	-54	-191	0	283	952	4.02	4.02	4.02	4.02	-6.39	40.0	0.00
47	282	1141	-46	-167	0	248	964	4.02	4.02	4.02	4.02	-6.47	40.5	0.00
49	282	1251	-48	-190	0	290	953	4.02	4.02	4.02	4.02	-6.39	40.1	0.00
50	282	1059	-48	-158	0	228	968	4.02	4.02	4.02	4.02	-6.50	40.7	0.00
51	282	1189	-42	-239	0	275	962	4.02	4.02	4.02	4.02	-6.46	40.4	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	339	1711	-475	-358	0	748	713	4.02	4.02	4.02	4.02	-4.79	30.0	0.00
41	339	1381	-471	-289	0	585	750	4.02	4.02	4.02	4.02	-5.03	31.5	0.00
42	339	1526	-460	-504	0	785	750	4.02	4.02	4.02	4.02	-5.03	31.5	0.00
43	339	1811	-458	-344	0	736	729	4.02	4.02	4.02	4.02	-4.89	30.6	0.00
44	339	856	-467	-182	0	334	804	4.02	4.02	4.02	4.02	-5.39	33.8	0.00
45	339	1501	-434	-586	0	797	790	4.02	4.02	4.02	4.02	-5.30	33.2	0.00
46	339	1189	-439	-191	0	391	813	4.02	4.02	4.02	4.02	-5.46	34.2	0.00
47	339	1141	-431	-167	0	343	830	4.02	4.02	4.02	4.02	-5.57	34.9	0.00
49	339	1251	-433	-190	0	397	817	4.02	4.02	4.02	4.02	-5.48	34.3	0.00
50	339	1059	-434	-158	0	317	832	4.02	4.02	4.02	4.02	-5.58	35.0	0.00
51	339	1189	-428	-239	0	409	830	4.02	4.02	4.02	4.02	-5.57	34.9	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	395	1711	-861	-358	0	951	335	4.02	4.02	4.02	4.02	-2.25	14.1	0.00
41	395	1381	-857	-289	0	749	375	4.02	4.02	4.02	4.02	-2.51	15.7	0.00
42	395	1526	-846	-504	0	1070	381	4.02	4.02	4.02	4.02	-2.56	16.0	0.00
43	395	1811	-844	-344	0	930	360	4.02	4.02	4.02	4.02	-2.42	15.1	0.00
44	395	856	-853	-182	0	437	431	4.02	4.02	4.02	4.02	-2.89	18.1	0.00
45	395	1501	-820	-586	0	1129	436	4.02	4.02	4.02	4.02	-2.93	18.3	0.00
46	395	1189	-825	-191	0	499	456	4.02	4.02	4.02	4.02	-3.06	19.2	0.00
47	395	1141	-817	-167	0	437	477	4.02	4.02	4.02	4.02	-3.20	20.0	0.00
49	395	1251	-819	-190	0	504	463	4.02	4.02	4.02	4.02	-3.11	19.5	0.00
50	395	1059	-820	-158	0	406	477	4.02	4.02	4.02	4.02	-3.20	20.1	0.00
51	395	1189	-814	-239	0	544	479	4.02	4.02	4.02	4.02	-3.21	20.1	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	452	1711	-1247	-358	0	1153	-260	4.02	4.02	4.02	4.02	-1.75	10.9	0.00
41	452	1381	-1243	-289	0	912	-219	4.02	4.02	4.02	4.02	-1.47	9.2	0.00
42	452	1526	-1232	-504	0	1355	-206	4.02	4.02	4.02	4.02	-1.38	8.7	0.00
43	452	1811	-1230	-344	0	1124	-226	4.02	4.02	4.02	4.02	-1.52	9.5	0.00
44	452	856	-1239	-182	0	540	-161	4.02	4.02	4.02	4.02	-1.08	6.7	0.00
45	452	1501	-1206	-586	0	1460	-136	4.02	4.02	4.02	4.02	-0.91	5.7	0.00
46	452	1189	-1211	-191	0	607	-119	4.02	4.02	4.02	4.02	-0.80	5.0	0.00
47	452	1141	-1203	-167	0	531	-94	4.02	4.02	4.02	4.02	-0.63	4.0	0.00
49	452	1251	-1205	-190	0	612	-108	4.02	4.02	4.02	4.02	-0.73	4.6	0.00
50	452	1059	-1206	-158	0	495	-96	4.02	4.02	4.02	4.02	-0.64	4.0	0.00
51	452	1189	-1200	-239	0	679	-90	4.02	4.02	4.02	4.02	-0.60	3.8	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	508	1711	-1633	-358	0	1356	-1074	4.02	4.02	4.02	4.02	-7.21	45.1	0.00
41	508	1381	-1629	-289	0	1075	-1030	4.02	4.02	4.02	4.02	-6.91	43.3	0.00
42	508	1526	-1618	-504	0	1639	-1012	4.02	4.02	4.02	4.02	-6.79	42.5	0.00
43	508	1811	-1616	-344	0	1319	-1031	4.02	4.02	4.02	4.02	-6.92	43.3	0.00
44	508	856	-1625	-182	0	643	-970	4.02	4.02	4.02	4.02	-6.51	40.8	0.00
45	508	1501	-1592	-586	0	1792	-927	4.02	4.02	4.02	4.02	-6.22	38.9	0.00
46	508	1189	-1597	-191	0	715	-913	4.02	4.02	4.02	4.02	-6.12	38.4	0.00
47	508	1141	-1589	-167	0	626	-883	4.02	4.02	4.02	4.02	-5.93	37.1	0.00
49	508	1251	-1591	-190	0	719	-898	4.02	4.02	4.02	4.02	-6.03	37.8	0.00
50	508	1059	-1592	-158	0	584	-886	4.02	4.02	4.02	4.02	-5.95	37.3	0.00
51	508	1189	-1586	-239	0	814	-877	4.02	4.02	4.02	4.02	-5.89	36.9	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	565	1711	-2019	-358	0	1558	-2106	4.02	4.02	4.02	4.02	-14.13	88.5	0.00
41	565	1381	-2015	-289	0	1238	-2059	4.02	4.02	4.02	4.02	-13.82	86.5	0.00
42	565	1526	-2004	-504	0	1924	-2035	4.02	4.02	4.02	4.02	-13.65	85.5	0.00
43	565	1811	-2002	-344	0	1513	-2053	4.02	4.02	4.02	4.02	-13.78	86.3	0.00
44	565	856	-2011	-182	0	746	-1997	4.02	4.02	4.02	4.02	-13.40	83.9	0.00
45	565	1501	-1978	-586	0	2123	-1935	4.02	4.02	4.02	4.02	-12.98	81.3	0.00
46	565	1189	-1983	-191	0	823	-1924	4.02	4.02	4.02	4.02	-12.91	80.9	0.00
47	565	1141	-1975	-167	0	720	-1890	4.02	4.02	4.02	4.02	-12.68	79.4	0.00
49	565	1251	-1977	-190	0	827	-1906	4.02	4.02	4.02	4.02	-12.79	80.1	0.00
50	565	1059	-1978	-158	0	673	-1895	4.02	4.02	4.02	4.02	-12.72	79.6	0.00
51	565	1189	-1972	-239	0	948	-1882	4.02	4.02	4.02	4.02	-12.63	79.1	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

Nome travata: **trave_304_IP1** Descrizione: **Trave_3 1-10**
ASTA NUM. 5 NI 302 NF 325 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y Permanente qy tot.
qy medio: 375.00 308.00 683.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	[Fx]	[Fy]	[Fz]	[Mx]	[My]	Mz	[APOST]	[AANT]	AINF	ASUP	Sc	Sf	w
	cm	daN			daN*m			cm^2				daN/cm^2		mm
40	0	-454	1316	-46	0	-418	84	4.02	4.02	4.02	4.02	-0.56	3.5	0.00
41	0	170	1891	-74	0	-504	-1414	4.02	4.02	4.02	4.02	-9.49	59.4	0.00
42	0	192	1895	-105	0	-597	-1427	4.02	4.02	4.02	4.02	-9.58	60.0	0.00
43	0	-869	915	-12	0	-252	1131	4.02	4.02	4.02	4.02	-7.59	47.5	0.00
44	0	1227	2853	-122	0	-664	-3924	4.02	4.02	4.02	4.02	-49.38	2369.1	0.19
45	0	208	1880	-110	0	-549	-1387	4.02	4.02	4.02	4.02	-9.31	58.3	0.00
46	0	173	1863	-48	0	-330	-1337	4.02	4.02	4.02	4.02	-8.97	56.2	0.00
47	0	174	1857	-41	0	-286	-1318	4.02	4.02	4.02	4.02	-8.84	55.4	0.00
49	0	-34	1665	-32	0	-257	-818	4.02	4.02	4.02	4.02	-5.49	34.4	0.00
50	0	385	2052	-54	0	-340	-1829	4.02	4.02	4.02	4.02	-12.27	76.9	0.00
51	0	181	1858	-52	0	-317	-1322	4.02	4.02	4.02	4.02	-8.87	55.6	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	56	-454	930	-46	0	-392	718	4.02	4.02	4.02	4.02	-4.82	30.2	0.00
41	56	170	1505	-74	0	-463	-455	4.02	4.02	4.02	4.02	-3.05	19.1	0.00
42	56	192	1509	-105	0	-537	-466	4.02	4.02	4.02	4.02	-3.12	19.6	0.00
43	56	-869	529	-12	0	-245	1539	4.02	4.02	4.02	4.02	-10.33	64.7	0.00
44	56	1227	2467	-122	0	-596	-2421	4.02	4.02	4.02	4.02	-16.24	101.8	0.00
45	56	208	1494	-110	0	-487	-434	4.02	4.02	4.02	4.02	-2.91	18.2	0.00
46	56	173	1477	-48	0	-303	-393	4.02	4.02	4.02	4.02	-2.64	16.5	0.00
47	56	174	1471	-41	0	-263	-378	4.02	4.02	4.02	4.02	-2.54	15.9	0.00
49	56	-34	1279	-32	0	-239	13	4.02	4.02	4.02	4.02	-0.09	0.6	0.00
50	56	385	1666	-54	0	-309	-778	4.02	4.02	4.02	4.02	-5.22	32.7	0.00
51	56	181	1472	-52	0	-287	-381	4.02	4.02	4.02	4.02	-2.56	16.0	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	113	-454	544	-46	0	-366	1135	4.02	4.02	4.02	4.02	-7.61	47.7	0.00
41	113	170	1119	-74	0	-421	287	4.02	4.02	4.02	4.02	-1.92	12.0	0.00
42	113	192	1123	-105	0	-478	278	4.02	4.02	4.02	4.02	-1.86	11.7	0.00
43	113	-869	143	-12	0	-238	1729	4.02	4.02	4.02	4.02	-11.60	72.7	0.00
44	113	1227	2081	-122	0	-527	-1136	4.02	4.02	4.02	4.02	-7.62	47.7	0.00
45	113	208	1108	-110	0	-425	301	4.02	4.02	4.02	4.02	-2.02	12.7	0.00
46	113	173	1091	-48	0	-275	333	4.02	4.02	4.02	4.02	-2.23	14.0	0.00
47	113	174	1085	-41	0	-239	344	4.02	4.02	4.02	4.02	-2.31	14.5	0.00
49	113	-34	893	-32	0	-221	627	4.02	4.02	4.02	4.02	-4.21	26.4	0.00
50	113	385	1280	-54	0	-278	54	4.02	4.02	4.02	4.02	-0.36	2.3	0.00
51	113	181	1086	-52	0	-258	341	4.02	4.02	4.02	4.02	-2.29	14.3	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	170	-454	158	-46	0	-339	1333	4.02	4.02	4.02	4.02	-8.94	56.0	0.00
41	170	170	733	-74	0	-379	810	4.02	4.02	4.02	4.02	-5.43	34.0	0.00
42	170	192	737	-105	0	-419	803	4.02	4.02	4.02	4.02	-5.39	33.8	0.00
43	170	-869	-242	-12	0	-231	1701	4.02	4.02	4.02	4.02	-11.41	71.5	0.00
44	170	1227	1695	-122	0	-458	-69	4.02	4.02	4.02	4.02	-0.46	2.9	0.00
45	170	208	722	-110	0	-363	818	4.02	4.02	4.02	4.02	-5.49	34.4	0.00
46	170	173	706	-48	0	-248	840	4.02	4.02	4.02	4.02	-5.64	35.3	0.00
47	170	174	699	-41	0	-216	848	4.02	4.02	4.02	4.02	-5.69	35.6	0.00
49	170	-34	507	-32	0	-202	1023	4.02	4.02	4.02	4.02	-6.86	43.0	0.00
50	170	385	895	-54	0	-248	669	4.02	4.02	4.02	4.02	-4.49	28.1	0.00
51	170	181	700	-52	0	-229	846	4.02	4.02	4.02	4.02	-5.68	35.6	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	226	-454	-228	-46	0	-313	1313	4.02	4.02	4.02	4.02	-8.81	55.2	0.00
41	226	170	347	-74	0	-337	1115	4.02	4.02	4.02	4.02	-7.48	46.9	0.00
42	226	192	351	-105	0	-359	1111	4.02	4.02	4.02	4.02	-7.45	46.7	0.00
43	226	-869	-628	-12	0	-224	1455	4.02	4.02	4.02	4.02	-9.76	61.2	0.00
44	226	1227	1309	-122	0	-390	780	4.02	4.02	4.02	4.02	-5.23	32.8	0.00
45	226	208	336	-110	0	-301	1117	4.02	4.02	4.02	4.02	-7.49	46.9	0.00
46	226	173	320	-48	0	-221	1130	4.02	4.02	4.02	4.02	-7.58	47.5	0.00
47	226	174	313	-41	0	-192	1134	4.02	4.02	4.02	4.02	-7.61	47.7	0.00
49	226	-34	121	-32	0	-184	1200	4.02	4.02	4.02	4.02	-8.05	50.4	0.00
50	226	385	509	-54	0	-217	1065	4.02	4.02	4.02	4.02	-7.15	44.8	0.00

51	226	181	314	-52	0	-199	1132	4.02	4.02	4.02	4.02	-7.60	47.6	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	282	-454	-614	-46	0	-287	1076	4.02	4.02	4.02	4.02	-7.22	45.2	0.00
41	282	170	-38	-74	0	-296	1202	4.02	4.02	4.02	4.02	-8.07	50.5	0.00
42	282	192	-34	-105	0	-300	1200	4.02	4.02	4.02	4.02	-8.05	50.4	0.00
43	282	-869	-1014	-12	0	-218	991	4.02	4.02	4.02	4.02	-6.65	41.6	0.00
44	282	1227	924	-122	0	-321	1411	4.02	4.02	4.02	4.02	-9.47	59.3	0.00
45	282	208	-50	-110	0	-239	1198	4.02	4.02	4.02	4.02	-8.04	50.3	0.00
46	282	173	-66	-48	0	-194	1202	4.02	4.02	4.02	4.02	-8.06	50.5	0.00
47	282	174	-72	-41	0	-169	1202	4.02	4.02	4.02	4.02	-8.06	50.5	0.00
49	282	-34	-264	-32	0	-166	1160	4.02	4.02	4.02	4.02	-7.78	48.7	0.00
50	282	385	123	-54	0	-187	1244	4.02	4.02	4.02	4.02	-8.35	52.3	0.00
51	282	181	-72	-52	0	-170	1201	4.02	4.02	4.02	4.02	-8.06	50.5	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	339	-454	-999	-46	0	-261	620	4.02	4.02	4.02	4.02	-4.16	26.1	0.00
41	339	170	-424	-74	0	-254	1072	4.02	4.02	4.02	4.02	-7.19	45.0	0.00
42	339	192	-420	-105	0	-240	1071	4.02	4.02	4.02	4.02	-7.19	45.0	0.00
43	339	-869	-1400	-12	0	-211	309	4.02	4.02	4.02	4.02	-2.07	13.0	0.00
44	339	1227	538	-122	0	-252	1824	4.02	4.02	4.02	4.02	-12.24	76.7	0.00
45	339	208	-435	-110	0	-177	1061	4.02	4.02	4.02	4.02	-7.12	44.6	0.00
46	339	173	-452	-48	0	-167	1056	4.02	4.02	4.02	4.02	-7.08	44.4	0.00
47	339	174	-458	-41	0	-145	1052	4.02	4.02	4.02	4.02	-7.06	44.2	0.00
49	339	-34	-650	-32	0	-148	901	4.02	4.02	4.02	4.02	-6.05	37.9	0.00
50	339	385	-263	-54	0	-156	1204	4.02	4.02	4.02	4.02	-8.08	50.6	0.00
51	339	181	-457	-52	0	-141	1051	4.02	4.02	4.02	4.02	-7.05	44.2	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	396	-454	-1385	-46	0	-234	-54	4.02	4.02	4.02	4.02	-0.36	2.3	0.00
41	396	170	-810	-74	0	-212	723	4.02	4.02	4.02	4.02	-4.85	30.4	0.00
42	396	192	-806	-105	0	-181	724	4.02	4.02	4.02	4.02	-4.86	30.4	0.00
43	396	-869	-1786	-12	0	-204	-591	4.02	4.02	4.02	4.02	-3.97	24.9	0.00
44	396	1227	152	-122	0	-184	2019	4.02	4.02	4.02	4.02	-13.54	84.8	0.00
45	396	208	-821	-110	0	-115	706	4.02	4.02	4.02	4.02	-4.73	29.7	0.00
46	396	173	-838	-48	0	-140	691	4.02	4.02	4.02	4.02	-4.64	29.1	0.00
47	396	174	-844	-41	0	-122	684	4.02	4.02	4.02	4.02	-4.59	28.7	0.00
49	396	-34	-1036	-32	0	-129	425	4.02	4.02	4.02	4.02	-2.85	17.9	0.00
50	396	385	-649	-54	0	-125	947	4.02	4.02	4.02	4.02	-6.35	39.8	0.00
51	396	181	-843	-52	0	-111	684	4.02	4.02	4.02	4.02	-4.59	28.7	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	452	-454	-1771	-46	0	-208	-945	4.02	4.02	4.02	4.02	-6.34	39.7	0.00
41	452	170	-1196	-74	0	-171	156	4.02	4.02	4.02	4.02	-1.05	6.6	0.00
42	452	192	-1192	-105	0	-121	160	4.02	4.02	4.02	4.02	-1.07	6.7	0.00
43	452	-869	-2172	-12	0	-197	-1710	4.02	4.02	4.02	4.02	-11.47	71.9	0.00
44	452	1227	-234	-122	0	-115	1995	4.02	4.02	4.02	4.02	-13.39	83.9	0.00
45	452	208	-1207	-110	0	-53	132	4.02	4.02	4.02	4.02	-0.89	5.6	0.00
46	452	173	-1223	-48	0	-113	109	4.02	4.02	4.02	4.02	-0.73	4.6	0.00
47	452	174	-1230	-41	0	-98	97	4.02	4.02	4.02	4.02	-0.65	4.1	0.00
49	452	-34	-1422	-32	0	-111	-270	4.02	4.02	4.02	4.02	-1.81	11.3	0.00
50	452	385	-1034	-54	0	-95	471	4.02	4.02	4.02	4.02	-3.16	19.8	0.00
51	452	181	-1229	-52	0	-82	98	4.02	4.02	4.02	4.02	-0.66	4.1	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	508	-454	-2157	-46	0	-182	-2055	4.02	4.02	4.02	4.02	-13.79	86.4	0.00
41	508	170	-1582	-74	0	-129	-629	4.02	4.02	4.02	4.02	-4.22	26.4	0.00
42	508	192	-1578	-105	0	-62	-623	4.02	4.02	4.02	4.02	-4.18	26.2	0.00
43	508	-869	-2558	-12	0	-190	-3046	4.02	4.02	4.02	4.02	-20.44	128.0	0.00
44	508	1227	-620	-122	0	-46	1754	4.02	4.02	4.02	4.02	-11.77	73.7	0.00
45	508	208	-1593	-110	0	9	-659	4.02	4.02	4.02	4.02	-4.42	27.7	0.00
46	508	173	-1609	-48	0	-86	-692	4.02	4.02	4.02	4.02	-4.64	29.1	0.00
47	508	174	-1616	-41	0	-75	-707	4.02	4.02	4.02	4.02	-4.74	29.7	0.00
49	508	-34	-1808	-32	0	-93	-1182	4.02	4.02	4.02	4.02	-7.93	49.7	0.00
50	508	385	-1420	-54	0	-64	-222	4.02	4.02	4.02	4.02	-1.49	9.3	0.00
51	508	181	-1615	-52	0	-53	-705	4.02	4.02	4.02	4.02	-4.73	29.6	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	565	-454	-2543	-46	0	-156	-3383	4.02	4.02	4.02	4.02	-42.57	2042.5	0.14
41	565	170	-1968	-74	0	-87	-1632	4.02	4.02	4.02	4.02	-10.95	68.6	0.00
42	565	192	-1964	-105	0	-3	-1624	4.02	4.02	4.02	4.02	-10.90	68.3	0.00
43	565	-869	-2944	-12	0	-184	-4600	4.02	4.02	4.02	4.02	-57.88	2777.2	0.25
44	565	1227	-1006	-122	0	22	1295	4.02	4.02	4.02	4.02	-8.69	54.4	0.00
45	565	208	-1979	-110	0	72	-1668	4.02	4.02	4.02	4.02	-11.19	70.1	0.00
46	565	173	-1995	-48	0	-59	-1710	4.02	4.02	4.02	4.02	-11.47	71.9	0.00
47	565	174	-2002	-41	0	-52	-1729	4.02	4.02	4.02	4.02	-11.60	72.7	0.00
49	565	-34	-2194	-32	0	-74	-2313	4.02	4.02	4.02	4.02	-15.52	97.2	0.00
50	565	385	-1806	-54	0	-33	-1134	4.02	4.02	4.02	4.02	-7.61	47.7	0.00
51	565	181	-2001	-52	0	-23	-1727	4.02	4.02	4.02	4.02	-11.59	72.6	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

Nome travata: **trave_302_IP1** Descrizione: **Trave_3 7-6-5-4-3-2-1**
ASTA NUM. 6 NI 27 NF 56 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y Permanente qy tot.
qy medio: 375.00 308.00 683.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	[Fx]	[Fy]	[Fz]	[Mx]	[My]	Mz	[APOST]	[AANT]	AINF	ASUP	Sc	Sf	w
	--													--
	cm		daN			daN*m				cm^2			daN/cm^2	mm
40	0	619	2133	-206	0	-710	-2243	4.02	4.02	4.02	4.02	-15.05	94.3	0.00
41	0	558	2087	-240	0	-836	-2096	4.02	4.02	4.02	4.02	-14.06	88.1	0.00
42	0	1504	2146	-357	0	-1345	-2281	4.02	4.02	4.02	4.02	-15.31	95.9	0.00
43	0	599	2155	-126	0	-430	-2310	4.02	4.02	4.02	4.02	-15.50	97.1	0.00
44	0	466	2012	-307	0	-1080	-1857	4.02	4.02	4.02	4.02	-12.46	78.1	0.00
45	0	2075	2177	-378	0	-1488	-2374	4.02	4.02	4.02	4.02	-15.93	99.8	0.00
46	0	462	2073	-149	0	-522	-2047	4.02	4.02	4.02	4.02	-13.74	86.0	0.00
47	0	438	2069	-127	0	-444	-2035	4.02	4.02	4.02	4.02	-13.65	85.5	0.00

49	0	458	2084	-115	0	-402	-2084	4.02	4.02	4.02	4.02	-13.98	87.6	0.00
50	0	432	2056	-151	0	-532	-1993	4.02	4.02	4.02	4.02	-13.37	83.8	0.00
51	0	753	2089	-166	0	-613	-2097	4.02	4.02	4.02	4.02	-14.07	88.1	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	60	619	1723	-206	0	-586	-1086	4.02	4.02	4.02	4.02	-7.29	45.6	0.00
41	60	558	1677	-240	0	-692	-967	4.02	4.02	4.02	4.02	-6.49	40.6	0.00
42	60	1504	1736	-357	0	-1131	-1116	4.02	4.02	4.02	4.02	-7.49	46.9	0.00
43	60	599	1745	-126	0	-354	-1140	4.02	4.02	4.02	4.02	-7.65	47.9	0.00
44	60	466	1602	-307	0	-896	-773	4.02	4.02	4.02	4.02	-5.19	32.5	0.00
45	60	2075	1767	-378	0	-1261	-1191	4.02	4.02	4.02	4.02	-7.99	50.0	0.00
46	60	462	1663	-149	0	-433	-926	4.02	4.02	4.02	4.02	-6.22	38.9	0.00
47	60	438	1659	-127	0	-368	-917	4.02	4.02	4.02	4.02	-6.15	38.5	0.00
49	60	458	1674	-115	0	-333	-956	4.02	4.02	4.02	4.02	-6.42	40.2	0.00
50	60	432	1646	-151	0	-441	-883	4.02	4.02	4.02	4.02	-5.92	37.1	0.00
51	60	753	1679	-166	0	-514	-967	4.02	4.02	4.02	4.02	-6.49	40.6	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	120	619	1313	-206	0	-463	-175	4.02	4.02	4.02	4.02	-1.17	7.3	0.00
41	120	558	1267	-240	0	-548	-83	4.02	4.02	4.02	4.02	-0.56	3.5	0.00
42	120	1504	1326	-357	0	-917	-197	4.02	4.02	4.02	4.02	-1.32	8.3	0.00
43	120	599	1335	-126	0	-278	-216	4.02	4.02	4.02	4.02	-1.45	9.1	0.00
44	120	466	1192	-307	0	-712	65	4.02	4.02	4.02	4.02	-0.44	2.7	0.00
45	120	2075	1357	-378	0	-1035	-253	4.02	4.02	4.02	4.02	-1.70	10.6	0.00
46	120	462	1253	-149	0	-343	-52	4.02	4.02	4.02	4.02	-0.35	2.2	0.00
47	120	438	1249	-127	0	-292	-44	4.02	4.02	4.02	4.02	-0.29	1.8	0.00
49	120	458	1264	-115	0	-264	-74	4.02	4.02	4.02	4.02	-0.50	3.1	0.00
50	120	432	1236	-151	0	-350	-18	4.02	4.02	4.02	4.02	-0.12	0.8	0.00
51	120	753	1269	-166	0	-415	-82	4.02	4.02	4.02	4.02	-0.55	3.5	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	180	619	904	-206	0	-339	491	4.02	4.02	4.02	4.02	-3.29	20.6	0.00
41	180	558	858	-240	0	-404	554	4.02	4.02	4.02	4.02	-3.72	23.3	0.00
42	180	1504	917	-357	0	-703	476	4.02	4.02	4.02	4.02	-3.20	20.0	0.00
43	180	599	926	-126	0	-203	463	4.02	4.02	4.02	4.02	-3.10	19.4	0.00
44	180	466	783	-307	0	-528	658	4.02	4.02	4.02	4.02	-4.41	27.6	0.00
45	180	2075	948	-378	0	-808	438	4.02	4.02	4.02	4.02	-2.94	18.4	0.00
46	180	462	844	-149	0	-253	577	4.02	4.02	4.02	4.02	-3.87	24.3	0.00
47	180	438	840	-127	0	-216	583	4.02	4.02	4.02	4.02	-3.91	24.5	0.00
49	180	458	855	-115	0	-194	562	4.02	4.02	4.02	4.02	-3.77	23.6	0.00
50	180	432	827	-151	0	-259	601	4.02	4.02	4.02	4.02	-4.03	25.2	0.00
51	180	753	860	-166	0	-315	556	4.02	4.02	4.02	4.02	-3.73	23.4	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	240	619	494	-206	0	-216	910	4.02	4.02	4.02	4.02	-6.11	38.2	0.00
41	240	558	448	-240	0	-260	946	4.02	4.02	4.02	4.02	-6.35	39.8	0.00
42	240	1504	507	-357	0	-489	904	4.02	4.02	4.02	4.02	-6.06	38.0	0.00
43	240	599	516	-126	0	-127	895	4.02	4.02	4.02	4.02	-6.01	37.6	0.00
44	240	466	373	-307	0	-344	1004	4.02	4.02	4.02	4.02	-6.74	42.2	0.00
45	240	2075	538	-378	0	-581	884	4.02	4.02	4.02	4.02	-5.93	37.1	0.00
46	240	462	434	-149	0	-164	960	4.02	4.02	4.02	4.02	-6.44	40.4	0.00
47	240	438	430	-127	0	-140	964	4.02	4.02	4.02	4.02	-6.47	40.5	0.00
49	240	458	445	-115	0	-125	952	4.02	4.02	4.02	4.02	-6.39	40.0	0.00
50	240	432	417	-151	0	-169	974	4.02	4.02	4.02	4.02	-6.53	40.9	0.00
51	240	753	450	-166	0	-216	949	4.02	4.02	4.02	4.02	-6.37	39.9	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	300	619	84	-206	0	-92	1084	4.02	4.02	4.02	4.02	-7.27	45.5	0.00
41	300	558	38	-240	0	-116	1092	4.02	4.02	4.02	4.02	-7.33	45.9	0.00
42	300	1504	97	-357	0	-275	1085	4.02	4.02	4.02	4.02	-7.28	45.6	0.00
43	300	599	106	-126	0	-51	1082	4.02	4.02	4.02	4.02	-7.26	45.5	0.00
44	300	466	-37	-307	0	-159	1105	4.02	4.02	4.02	4.02	-7.41	46.4	0.00
45	300	2075	128	-378	0	-354	1084	4.02	4.02	4.02	4.02	-7.27	45.5	0.00
46	300	462	24	-149	0	-74	1098	4.02	4.02	4.02	4.02	-7.36	46.1	0.00
47	300	438	20	-127	0	-64	1099	4.02	4.02	4.02	4.02	-7.37	46.2	0.00
49	300	458	35	-115	0	-56	1096	4.02	4.02	4.02	4.02	-7.35	46.1	0.00
50	300	432	7	-151	0	-78	1101	4.02	4.02	4.02	4.02	-7.38	46.3	0.00
51	300	753	40	-166	0	-117	1096	4.02	4.02	4.02	4.02	-7.35	46.1	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	360	619	-326	-206	0	31	1011	4.02	4.02	4.02	4.02	-6.78	42.5	0.00
41	360	558	-372	-240	0	28	992	4.02	4.02	4.02	4.02	-6.66	41.7	0.00
42	360	1504	-313	-357	0	-60	1021	4.02	4.02	4.02	4.02	-6.85	42.9	0.00
43	360	599	-304	-126	0	25	1022	4.02	4.02	4.02	4.02	-6.86	43.0	0.00
44	360	466	-447	-307	0	25	959	4.02	4.02	4.02	4.02	-6.44	40.3	0.00
45	360	2075	-282	-378	0	-128	1037	4.02	4.02	4.02	4.02	-6.96	43.6	0.00
46	360	462	-386	-149	0	15	989	4.02	4.02	4.02	4.02	-6.63	41.6	0.00
47	360	438	-390	-127	0	12	988	4.02	4.02	4.02	4.02	-6.63	41.5	0.00
49	360	458	-375	-115	0	13	994	4.02	4.02	4.02	4.02	-6.67	41.8	0.00
50	360	432	-403	-151	0	13	982	4.02	4.02	4.02	4.02	-6.59	41.3	0.00
51	360	753	-370	-166	0	-18	997	4.02	4.02	4.02	4.02	-6.69	41.9	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	420	619	-736	-206	0	155	693	4.02	4.02	4.02	4.02	-4.65	29.1	0.00
41	420	558	-782	-240	0	172	646	4.02	4.02	4.02	4.02	-4.33	27.2	0.00
42	420	1504	-723	-357	0	154	710	4.02	4.02	4.02	4.02	-4.77	29.9	0.00
43	420	599	-714	-126	0	100	717	4.02	4.02	4.02	4.02	-4.81	30.1	0.00
44	420	466	-857	-307	0	209	568	4.02	4.02	4.02	4.02	-3.81	23.9	0.00
45	420	2075	-692	-378	0	99	745	4.02	4.02	4.02	4.02	-5.00	31.3	0.00
46	420	462	-796	-149	0	105	634	4.02	4.02	4.02	4.02	-4.26	26.7	0.00
47	420	438	-800	-127	0	88	631	4.02	4.02	4.02	4.02	-4.23	26.5	0.00
49	420	458	-785	-115	0	82	647	4.02	4.02	4.02	4.02	-4.34	27.2	0.00
50	420	432	-813	-151	0	104	617	4.02	4.02	4.02	4.02	-4.14	25.9	0.00
51	420	753	-780	-166	0	82	652	4.02	4.02	4.02	4.02	-4.38	27.4	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	480	619	-1145	-206	0	278	129	4.02	4.02	4.02	4.02	-0.86	5.4	0.00
41	480	558	-1191	-240	0	316	54	4.02	4.02	4.02	4.02	-0.36	2.3	0.00
42	480	1504	-1132	-357	0	368	154	4.02	4.02	4.02	4.02	-1.03	6.5	0.00
43	480	599	-1123	-126	0	176	166	4.02	4.02	4.02	4.02	-1.11	7.0	0.00
44	480	466	-1266	-307	0	393	-69	4.02	4.02	4.02	4.02	-0.46	2.9	0.00
45	480	2075	-1101	-378	0	326	207	4.02	4.02	4.02	4.02	-1.39	8.7	0.00

46	480	462	-1205	-149	0	194	34	4.02	4.02	4.02	4.02	-0.23	1.4	0.00
47	480	438	-1209	-127	0	164	28	4.02	4.02	4.02	4.02	-0.19	1.2	0.00
49	480	458	-1194	-115	0	151	53	4.02	4.02	4.02	4.02	-0.36	2.2	0.00
50	480	432	-1222	-151	0	194	6	4.02	4.02	4.02	4.02	-0.04	0.3	0.00
51	480	753	-1189	-166	0	181	61	4.02	4.02	4.02	4.02	-0.41	2.6	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	540	619	-1555	-206	0	402	-681	4.02	4.02	4.02	4.02	-4.57	28.6	0.00
41	540	558	-1601	-240	0	461	-783	4.02	4.02	4.02	4.02	-5.26	32.9	0.00
42	540	1504	-1542	-357	0	582	-648	4.02	4.02	4.02	4.02	-4.35	27.2	0.00
43	540	599	-1533	-126	0	252	-631	4.02	4.02	4.02	4.02	-4.23	26.5	0.00
44	540	466	-1676	-307	0	577	-952	4.02	4.02	4.02	4.02	-6.39	40.0	0.00
45	540	2075	-1511	-378	0	552	-576	4.02	4.02	4.02	4.02	-3.87	24.2	0.00
46	540	462	-1615	-149	0	284	-813	4.02	4.02	4.02	4.02	-5.45	34.2	0.00
47	540	438	-1619	-127	0	240	-821	4.02	4.02	4.02	4.02	-5.51	34.5	0.00
49	540	458	-1604	-115	0	220	-786	4.02	4.02	4.02	4.02	-5.27	33.0	0.00
50	540	432	-1632	-151	0	285	-851	4.02	4.02	4.02	4.02	-5.71	35.7	0.00
51	540	753	-1599	-166	0	280	-775	4.02	4.02	4.02	4.02	-5.20	32.6	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	600	619	-1965	-206	0	525	-1737	4.02	4.02	4.02	4.02	-11.66	73.0	0.00
41	600	558	-2011	-240	0	605	-1867	4.02	4.02	4.02	4.02	-12.53	78.5	0.00
42	600	1504	-1952	-357	0	796	-1696	4.02	4.02	4.02	4.02	-11.38	71.3	0.00
43	600	599	-1943	-126	0	328	-1674	4.02	4.02	4.02	4.02	-11.23	70.4	0.00
44	600	466	-2086	-307	0	761	-2081	4.02	4.02	4.02	4.02	-13.96	87.5	0.00
45	600	2075	-1921	-378	0	779	-1606	4.02	4.02	4.02	4.02	-10.78	67.5	0.00
46	600	462	-2025	-149	0	374	-1905	4.02	4.02	4.02	4.02	-12.78	80.1	0.00
47	600	438	-2029	-127	0	316	-1915	4.02	4.02	4.02	4.02	-12.85	80.5	0.00
49	600	458	-2014	-115	0	289	-1871	4.02	4.02	4.02	4.02	-12.55	78.6	0.00
50	600	432	-2042	-151	0	376	-1953	4.02	4.02	4.02	4.02	-13.10	82.1	0.00
51	600	753	-2009	-166	0	380	-1858	4.02	4.02	4.02	4.02	-12.47	78.1	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

Nome travata: **trave_302_IP1** Descrizione: **Trave_3 7-6-5-4-3-2-1**
ASTA NUM. 7 NI 56 NF 79 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y Permanente qy tot.
qy medio: 375.00 308.00 683.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	[Fx]	[Fy]	[Fz]	[Mx]	[My]	Mz	[APOST]	[AANT]	AINF	ASUP	Sc	Sf	w
	cm	daN			daN*m			cm^2				daN/cm^2		mm
40	0	742	2030	-110	0	-226	-1974	4.02	4.02	4.02	4.02	-13.25	83.0	0.00
41	0	731	2037	-138	0	-288	-1995	4.02	4.02	4.02	4.02	-13.39	83.9	0.00
42	0	1540	2113	-143	0	-281	-2228	4.02	4.02	4.02	4.02	-14.95	93.6	0.00
43	0	648	2032	-62	0	-128	-1983	4.02	4.02	4.02	4.02	-13.31	83.3	0.00
44	0	727	2047	-191	0	-402	-2027	4.02	4.02	4.02	4.02	-13.60	85.2	0.00
45	0	1977	2171	-118	0	-220	-2405	4.02	4.02	4.02	4.02	-16.14	101.1	0.00
46	0	566	2047	-92	0	-196	-2030	4.02	4.02	4.02	4.02	-13.62	85.3	0.00
47	0	525	2049	-81	0	-174	-2039	4.02	4.02	4.02	4.02	-13.68	85.7	0.00
49	0	529	2047	-71	0	-153	-2032	4.02	4.02	4.02	4.02	-13.63	85.4	0.00
50	0	545	2050	-97	0	-208	-2041	4.02	4.02	4.02	4.02	-13.70	85.8	0.00
51	0	795	2075	-83	0	-171	-2117	4.02	4.02	4.02	4.02	-14.21	89.0	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	60	742	1620	-110	0	-160	-879	4.02	4.02	4.02	4.02	-5.90	36.9	0.00
41	60	731	1627	-138	0	-205	-896	4.02	4.02	4.02	4.02	-6.01	37.7	0.00
42	60	1540	1703	-143	0	-195	-1083	4.02	4.02	4.02	4.02	-7.27	45.5	0.00
43	60	648	1622	-62	0	-91	-887	4.02	4.02	4.02	4.02	-5.95	37.3	0.00
44	60	727	1637	-191	0	-287	-922	4.02	4.02	4.02	4.02	-6.19	38.7	0.00
45	60	1977	1761	-118	0	-149	-1225	4.02	4.02	4.02	4.02	-8.22	51.5	0.00
46	60	566	1637	-92	0	-141	-925	4.02	4.02	4.02	4.02	-6.21	38.9	0.00
47	60	525	1639	-81	0	-125	-933	4.02	4.02	4.02	4.02	-6.26	39.2	0.00
49	60	529	1637	-71	0	-110	-927	4.02	4.02	4.02	4.02	-6.22	39.0	0.00
50	60	545	1640	-97	0	-149	-934	4.02	4.02	4.02	4.02	-6.27	39.3	0.00
51	60	795	1665	-83	0	-122	-995	4.02	4.02	4.02	4.02	-6.68	41.8	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	120	742	1210	-110	0	-95	-30	4.02	4.02	4.02	4.02	-0.20	1.2	0.00
41	120	731	1217	-138	0	-122	-43	4.02	4.02	4.02	4.02	-0.29	1.8	0.00
42	120	1540	1293	-143	0	-109	-184	4.02	4.02	4.02	4.02	-1.23	7.7	0.00
43	120	648	1212	-62	0	-53	-36	4.02	4.02	4.02	4.02	-0.24	1.5	0.00
44	120	727	1227	-191	0	-173	-63	4.02	4.02	4.02	4.02	-0.42	2.6	0.00
45	120	1977	1351	-118	0	-78	-292	4.02	4.02	4.02	4.02	-1.96	12.3	0.00
46	120	566	1227	-92	0	-85	-66	4.02	4.02	4.02	4.02	-0.44	2.8	0.00
47	120	525	1229	-81	0	-76	-72	4.02	4.02	4.02	4.02	-0.48	3.0	0.00
49	120	529	1227	-71	0	-67	-68	4.02	4.02	4.02	4.02	-0.45	2.8	0.00
50	120	545	1230	-97	0	-91	-73	4.02	4.02	4.02	4.02	-0.49	3.1	0.00
51	120	795	1255	-83	0	-72	-119	4.02	4.02	4.02	4.02	-0.80	5.0	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	180	742	801	-110	0	-29	574	4.02	4.02	4.02	4.02	-3.85	24.1	0.00
41	180	731	808	-138	0	-39	565	4.02	4.02	4.02	4.02	-3.79	23.7	0.00
42	180	1540	884	-143	0	-24	470	4.02	4.02	4.02	4.02	-3.15	19.7	0.00
43	180	648	803	-62	0	-16	568	4.02	4.02	4.02	4.02	-3.81	23.9	0.00
44	180	727	818	-191	0	-58	551	4.02	4.02	4.02	4.02	-3.70	23.2	0.00
45	180	1977	942	-118	0	-8	396	4.02	4.02	4.02	4.02	-2.66	16.7	0.00
46	180	566	818	-92	0	-30	547	4.02	4.02	4.02	4.02	-3.67	23.0	0.00
47	180	525	820	-81	0	-28	543	4.02	4.02	4.02	4.02	-3.64	22.8	0.00
49	180	529	818	-71	0	-24	546	4.02	4.02	4.02	4.02	-3.66	22.9	0.00
50	180	545	821	-97	0	-33	542	4.02	4.02	4.02	4.02	-3.64	22.8	0.00
51	180	795	846	-83	0	-23	511	4.02	4.02	4.02	4.02	-3.43	21.5	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	240	742	391	-110	0	37	931	4.02	4.02	4.02	4.02	-6.25	39.1	0.00
41	240	731	398	-138	0	44	926	4.02	4.02	4.02	4.02	-6.21	38.9	0.00
42	240	1540	474	-143	0	62	877	4.02	4.02	4.02	4.02	-5.89	36.9	0.00
43	240	648	393	-62	0	21	927	4.02	4.02	4.02	4.02	-6.22	39.0	0.00

44	240	727	408	-191	0	56	918	4.02	4.02	4.02	4.02	-6.16	38.6	0.00
45	240	1977	532	-118	0	63	838	4.02	4.02	4.02	4.02	-5.63	35.2	0.00
46	240	566	408	-92	0	25	915	4.02	4.02	4.02	4.02	-6.14	38.4	0.00
47	240	525	410	-81	0	21	912	4.02	4.02	4.02	4.02	-6.12	38.3	0.00
49	240	529	408	-71	0	19	913	4.02	4.02	4.02	4.02	-6.13	38.4	0.00
50	240	545	411	-97	0	25	912	4.02	4.02	4.02	4.02	-6.12	38.3	0.00
51	240	795	436	-83	0	27	896	4.02	4.02	4.02	4.02	-6.01	37.6	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	300	742	-19	-110	0	103	1043	4.02	4.02	4.02	4.02	-7.00	43.8	0.00
41	300	731	-12	-138	0	127	1042	4.02	4.02	4.02	4.02	-6.99	43.8	0.00
42	300	1540	64	-143	0	148	1039	4.02	4.02	4.02	4.02	-6.97	43.7	0.00
43	300	648	-17	-62	0	59	1040	4.02	4.02	4.02	4.02	-6.98	43.7	0.00
44	300	727	-2	-191	0	171	1040	4.02	4.02	4.02	4.02	-6.98	43.7	0.00
45	300	1977	122	-118	0	134	1035	4.02	4.02	4.02	4.02	-6.94	43.5	0.00
46	300	566	-2	-92	0	81	1036	4.02	4.02	4.02	4.02	-6.95	43.5	0.00
47	300	525	0	-81	0	69	1035	4.02	4.02	4.02	4.02	-6.94	43.5	0.00
49	300	529	-2	-71	0	61	1035	4.02	4.02	4.02	4.02	-6.94	43.5	0.00
50	300	545	1	-97	0	84	1035	4.02	4.02	4.02	4.02	-6.94	43.5	0.00
51	300	795	26	-83	0	76	1034	4.02	4.02	4.02	4.02	-6.94	43.5	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	360	742	-429	-110	0	169	909	4.02	4.02	4.02	4.02	-6.10	38.2	0.00
41	360	731	-422	-138	0	210	911	4.02	4.02	4.02	4.02	-6.11	38.3	0.00
42	360	1540	-346	-143	0	234	955	4.02	4.02	4.02	4.02	-6.41	40.1	0.00
43	360	648	-427	-62	0	96	907	4.02	4.02	4.02	4.02	-6.09	38.1	0.00
44	360	727	-412	-191	0	285	916	4.02	4.02	4.02	4.02	-6.14	38.5	0.00
45	360	1977	-288	-118	0	204	985	4.02	4.02	4.02	4.02	-6.61	41.4	0.00
46	360	566	-412	-92	0	136	912	4.02	4.02	4.02	4.02	-6.12	38.3	0.00
47	360	525	-410	-81	0	118	912	4.02	4.02	4.02	4.02	-6.12	38.3	0.00
49	360	529	-412	-71	0	104	911	4.02	4.02	4.02	4.02	-6.11	38.3	0.00
50	360	545	-409	-97	0	142	913	4.02	4.02	4.02	4.02	-6.12	38.4	0.00
51	360	795	-384	-83	0	126	927	4.02	4.02	4.02	4.02	-6.22	38.9	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	420	742	-839	-110	0	235	529	4.02	4.02	4.02	4.02	-3.55	22.2	0.00
41	420	731	-832	-138	0	292	535	4.02	4.02	4.02	4.02	-3.59	22.5	0.00
42	420	1540	-756	-143	0	320	625	4.02	4.02	4.02	4.02	-4.19	26.3	0.00
43	420	648	-837	-62	0	133	528	4.02	4.02	4.02	4.02	-3.54	22.2	0.00
44	420	727	-822	-191	0	400	546	4.02	4.02	4.02	4.02	-3.66	22.9	0.00
45	420	1977	-698	-118	0	275	689	4.02	4.02	4.02	4.02	-4.62	29.0	0.00
46	420	566	-822	-92	0	192	541	4.02	4.02	4.02	4.02	-3.63	22.7	0.00
47	420	525	-820	-81	0	166	543	4.02	4.02	4.02	4.02	-3.64	22.8	0.00
49	420	529	-822	-71	0	147	541	4.02	4.02	4.02	4.02	-3.63	22.7	0.00
50	420	545	-819	-97	0	200	544	4.02	4.02	4.02	4.02	-3.65	22.9	0.00
51	420	795	-794	-83	0	176	573	4.02	4.02	4.02	4.02	-3.85	24.1	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	480	742	-1248	-110	0	300	-97	4.02	4.02	4.02	4.02	-0.65	4.1	0.00
41	480	731	-1241	-138	0	375	-87	4.02	4.02	4.02	4.02	-0.58	3.7	0.00
42	480	1540	-1165	-143	0	406	49	4.02	4.02	4.02	4.02	-0.33	2.0	0.00
43	480	648	-1246	-62	0	171	-97	4.02	4.02	4.02	4.02	-0.65	4.1	0.00
44	480	727	-1231	-191	0	514	-70	4.02	4.02	4.02	4.02	-0.47	3.0	0.00
45	480	1977	-1107	-118	0	346	148	4.02	4.02	4.02	4.02	-0.99	6.2	0.00
46	480	566	-1231	-92	0	247	-75	4.02	4.02	4.02	4.02	-0.50	3.2	0.00
47	480	525	-1229	-81	0	215	-72	4.02	4.02	4.02	4.02	-0.48	3.0	0.00
49	480	529	-1231	-71	0	190	-75	4.02	4.02	4.02	4.02	-0.51	3.2	0.00
50	480	545	-1228	-97	0	259	-70	4.02	4.02	4.02	4.02	-0.47	2.9	0.00
51	480	795	-1203	-83	0	225	-26	4.02	4.02	4.02	4.02	-0.17	1.1	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	540	742	-1658	-110	0	366	-969	4.02	4.02	4.02	4.02	-6.50	40.7	0.00
41	540	731	-1651	-138	0	458	-955	4.02	4.02	4.02	4.02	-6.41	40.1	0.00
42	540	1540	-1575	-143	0	491	-773	4.02	4.02	4.02	4.02	-5.19	32.5	0.00
43	540	648	-1656	-62	0	208	-967	4.02	4.02	4.02	4.02	-6.49	40.7	0.00
44	540	727	-1641	-191	0	629	-932	4.02	4.02	4.02	4.02	-6.26	39.2	0.00
45	540	1977	-1517	-118	0	416	-640	4.02	4.02	4.02	4.02	-4.29	26.9	0.00
46	540	566	-1641	-92	0	302	-937	4.02	4.02	4.02	4.02	-6.29	39.4	0.00
47	540	525	-1639	-81	0	264	-933	4.02	4.02	4.02	4.02	-6.26	39.2	0.00
49	540	529	-1641	-71	0	233	-937	4.02	4.02	4.02	4.02	-6.29	39.4	0.00
50	540	545	-1638	-97	0	317	-930	4.02	4.02	4.02	4.02	-6.24	39.1	0.00
51	540	795	-1613	-83	0	275	-871	4.02	4.02	4.02	4.02	-5.84	36.6	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	600	742	-2068	-110	0	432	-2087	4.02	4.02	4.02	4.02	-14.00	87.7	0.00
41	600	731	-2061	-138	0	541	-2069	4.02	4.02	4.02	4.02	-13.88	87.0	0.00
42	600	1540	-1985	-143	0	577	-1841	4.02	4.02	4.02	4.02	-12.35	77.4	0.00
43	600	648	-2066	-62	0	245	-2084	4.02	4.02	4.02	4.02	-13.98	87.6	0.00
44	600	727	-2051	-191	0	743	-2040	4.02	4.02	4.02	4.02	-13.69	85.7	0.00
45	600	1977	-1927	-118	0	487	-1673	4.02	4.02	4.02	4.02	-11.23	70.3	0.00
46	600	566	-2051	-92	0	358	-2045	4.02	4.02	4.02	4.02	-13.72	86.0	0.00
47	600	525	-2049	-81	0	312	-2039	4.02	4.02	4.02	4.02	-13.68	85.7	0.00
49	600	529	-2051	-71	0	276	-2045	4.02	4.02	4.02	4.02	-13.72	86.0	0.00
50	600	545	-2048	-97	0	375	-2036	4.02	4.02	4.02	4.02	-13.66	85.6	0.00
51	600	795	-2023	-83	0	324	-1962	4.02	4.02	4.02	4.02	-13.17	82.5	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

Nome travata: **trave_302_IP1** Descrizione: **Trave_3 7-6-5-4-3-2-1**
ASTA NUM. 8 NI 79 NF 80 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y Permanente qy tot.
qy medio: 375.00 308.00 683.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	[Fx]	[Fy]	[Fz]	[Mx]	[My]	Mz	[APOST]	[AANT]	AINF	ASUP	Sc	Sf	w
	--													--
	cm		daN			daN*m				cm^2			daN/cm^2	mm
40	0	801	1974	-9	0	86	-1819	4.02	4.02	4.02	4.02	-12.21	76.5	0.00
41	0	841	1981	-1	0	137	-1837	4.02	4.02	4.02	4.02	-12.33	77.2	0.00

42	0	1500	2051	-2	0	131	-2047	4.02	4.02	4.02	4.02	-13.74	86.0	0.00
43	0	656	1985	-14	0	24	-1854	4.02	4.02	4.02	4.02	-12.44	77.9	0.00
44	0	926	1991	12	0	227	-1862	4.02	4.02	4.02	4.02	-12.49	78.3	0.00
45	0	1821	2114	-3	0	98	-2236	4.02	4.02	4.02	4.02	-15.00	94.0	0.00
46	0	650	2006	-1	0	91	-1914	4.02	4.02	4.02	4.02	-12.84	80.4	0.00
47	0	603	2012	-1	0	80	-1934	4.02	4.02	4.02	4.02	-12.98	81.3	0.00
49	0	590	2010	-3	0	63	-1928	4.02	4.02	4.02	4.02	-12.94	81.0	0.00
50	0	644	2011	2	0	103	-1929	4.02	4.02	4.02	4.02	-12.94	81.1	0.00
51	0	823	2036	-1	0	77	-2004	4.02	4.02	4.02	4.02	-13.45	84.2	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	60	801	1564	-9	0	92	-758	4.02	4.02	4.02	4.02	-5.08	31.8	0.00
41	60	841	1571	-1	0	138	-771	4.02	4.02	4.02	4.02	-5.18	32.4	0.00
42	60	1500	1641	-2	0	132	-939	4.02	4.02	4.02	4.02	-6.30	39.5	0.00
43	60	656	1575	-14	0	32	-786	4.02	4.02	4.02	4.02	-5.28	33.0	0.00
44	60	926	1581	12	0	220	-790	4.02	4.02	4.02	4.02	-5.30	33.2	0.00
45	60	1821	1704	-3	0	99	-1091	4.02	4.02	4.02	4.02	-7.32	45.8	0.00
46	60	650	1596	-1	0	91	-833	4.02	4.02	4.02	4.02	-5.59	35.0	0.00
47	60	603	1602	-1	0	80	-849	4.02	4.02	4.02	4.02	-5.70	35.7	0.00
49	60	590	1600	-3	0	65	-845	4.02	4.02	4.02	4.02	-5.67	35.5	0.00
50	60	644	1601	2	0	102	-845	4.02	4.02	4.02	4.02	-5.67	35.5	0.00
51	60	823	1626	-1	0	78	-905	4.02	4.02	4.02	4.02	-6.08	38.1	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	120	801	1154	-9	0	97	58	4.02	4.02	4.02	4.02	-0.39	2.4	0.00
41	120	841	1161	-1	0	138	48	4.02	4.02	4.02	4.02	-0.33	2.0	0.00
42	120	1500	1231	-2	0	133	-77	4.02	4.02	4.02	4.02	-0.52	3.2	0.00
43	120	656	1165	-14	0	40	36	4.02	4.02	4.02	4.02	-0.24	1.5	0.00
44	120	926	1171	12	0	213	36	4.02	4.02	4.02	4.02	-0.24	1.5	0.00
45	120	1821	1294	-3	0	101	-191	4.02	4.02	4.02	4.02	-1.28	8.0	0.00
46	120	650	1186	-1	0	92	1	4.02	4.02	4.02	4.02	-0.01	0.1	0.00
47	120	603	1192	-1	0	80	-11	4.02	4.02	4.02	4.02	-0.07	0.5	0.00
49	120	590	1190	-3	0	66	-8	4.02	4.02	4.02	4.02	-0.05	0.3	0.00
50	120	644	1191	2	0	101	-7	4.02	4.02	4.02	4.02	-0.05	0.3	0.00
51	120	823	1216	-1	0	79	-53	4.02	4.02	4.02	4.02	-0.35	2.2	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	180	801	745	-9	0	102	627	4.02	4.02	4.02	4.02	-4.21	26.4	0.00
41	180	841	752	-1	0	139	622	4.02	4.02	4.02	4.02	-4.18	26.2	0.00
42	180	1500	822	-2	0	135	539	4.02	4.02	4.02	4.02	-3.62	22.7	0.00
43	180	656	756	-14	0	48	612	4.02	4.02	4.02	4.02	-4.10	25.7	0.00
44	180	926	762	12	0	205	616	4.02	4.02	4.02	4.02	-4.13	25.9	0.00
45	180	1821	885	-3	0	103	463	4.02	4.02	4.02	4.02	-3.10	19.4	0.00
46	180	650	777	-1	0	92	590	4.02	4.02	4.02	4.02	-3.96	24.8	0.00
47	180	603	783	-1	0	81	582	4.02	4.02	4.02	4.02	-3.91	24.5	0.00
49	180	590	781	-3	0	68	584	4.02	4.02	4.02	4.02	-3.92	24.5	0.00
50	180	644	782	2	0	100	585	4.02	4.02	4.02	4.02	-3.92	24.6	0.00
51	180	823	807	-1	0	79	554	4.02	4.02	4.02	4.02	-3.72	23.3	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	240	801	335	-9	0	107	951	4.02	4.02	4.02	4.02	-6.38	40.0	0.00
41	240	841	342	-1	0	139	950	4.02	4.02	4.02	4.02	-6.38	39.9	0.00
42	240	1500	412	-2	0	136	909	4.02	4.02	4.02	4.02	-6.10	38.2	0.00
43	240	656	346	-14	0	56	942	4.02	4.02	4.02	4.02	-6.32	39.6	0.00
44	240	926	352	12	0	198	950	4.02	4.02	4.02	4.02	-6.37	39.9	0.00
45	240	1821	475	-3	0	105	871	4.02	4.02	4.02	4.02	-5.84	36.6	0.00
46	240	650	367	-1	0	93	933	4.02	4.02	4.02	4.02	-6.26	39.2	0.00
47	240	603	373	-1	0	81	929	4.02	4.02	4.02	4.02	-6.23	39.0	0.00
49	240	590	371	-3	0	70	929	4.02	4.02	4.02	4.02	-6.23	39.0	0.00
50	240	644	372	2	0	99	931	4.02	4.02	4.02	4.02	-6.25	39.1	0.00
51	240	823	397	-1	0	80	915	4.02	4.02	4.02	4.02	-6.14	38.5	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	300	801	-75	-9	0	112	1029	4.02	4.02	4.02	4.02	-6.90	43.2	0.00
41	300	841	-68	-1	0	140	1033	4.02	4.02	4.02	4.02	-6.93	43.4	0.00
42	300	1500	2	-2	0	137	1034	4.02	4.02	4.02	4.02	-6.93	43.4	0.00
43	300	656	-64	-14	0	65	1026	4.02	4.02	4.02	4.02	-6.88	43.1	0.00
44	300	926	-58	12	0	191	1038	4.02	4.02	4.02	4.02	-6.96	43.6	0.00
45	300	1821	65	-3	0	106	1033	4.02	4.02	4.02	4.02	-6.93	43.4	0.00
46	300	650	-43	-1	0	93	1031	4.02	4.02	4.02	4.02	-6.91	43.3	0.00
47	300	603	-37	-1	0	81	1030	4.02	4.02	4.02	4.02	-6.91	43.3	0.00
49	300	590	-39	-3	0	72	1029	4.02	4.02	4.02	4.02	-6.90	43.2	0.00
50	300	644	-38	2	0	97	1032	4.02	4.02	4.02	4.02	-6.92	43.4	0.00
51	300	823	-13	-1	0	81	1030	4.02	4.02	4.02	4.02	-6.91	43.3	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	360	801	-485	-9	0	117	861	4.02	4.02	4.02	4.02	-5.78	36.2	0.00
41	360	841	-478	-1	0	140	869	4.02	4.02	4.02	4.02	-5.83	36.5	0.00
42	360	1500	-408	-2	0	138	912	4.02	4.02	4.02	4.02	-6.12	38.3	0.00
43	360	656	-474	-14	0	73	864	4.02	4.02	4.02	4.02	-5.80	36.3	0.00
44	360	926	-468	12	0	183	880	4.02	4.02	4.02	4.02	-5.91	37.0	0.00
45	360	1821	-345	-3	0	108	949	4.02	4.02	4.02	4.02	-6.36	39.9	0.00
46	360	650	-453	-1	0	93	882	4.02	4.02	4.02	4.02	-5.92	37.1	0.00
47	360	603	-447	-1	0	82	885	4.02	4.02	4.02	4.02	-5.94	37.2	0.00
49	360	590	-449	-3	0	74	882	4.02	4.02	4.02	4.02	-5.92	37.1	0.00
50	360	644	-448	2	0	96	886	4.02	4.02	4.02	4.02	-5.94	37.2	0.00
51	360	823	-423	-1	0	81	899	4.02	4.02	4.02	4.02	-6.03	37.8	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	420	801	-895	-9	0	122	447	4.02	4.02	4.02	4.02	-3.00	18.8	0.00
41	420	841	-888	-1	0	141	459	4.02	4.02	4.02	4.02	-3.08	19.3	0.00
42	420	1500	-818	-2	0	140	545	4.02	4.02	4.02	4.02	-3.65	22.9	0.00
43	420	656	-884	-14	0	81	457	4.02	4.02	4.02	4.02	-3.07	19.2	0.00
44	420	926	-878	12	0	176	477	4.02	4.02	4.02	4.02	-3.20	20.0	0.00
45	420	1821	-755	-3	0	110	619	4.02	4.02	4.02	4.02	-4.15	26.0	0.00
46	420	650	-863	-1	0	94	487	4.02	4.02	4.02	4.02	-3.27	20.5	0.00
47	420	603	-857	-1	0	82	494	4.02	4.02	4.02	4.02	-3.32	20.8	0.00
49	420	590	-859	-3	0	76	490	4.02	4.02	4.02	4.02	-3.29	20.6	0.00
50	420	644	-858	2	0	95	495	4.02	4.02	4.02	4.02	-3.32	20.8	0.00
51	420	823	-833	-1	0	82	522	4.02	4.02	4.02	4.02	-3.51	22.0	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	480	801	-1304	-9	0	128	-213	4.02	4.02	4.02	4.02	-1.43	8.9	0.00
41	480	841	-1297	-1	0	141	-196	4.02	4.02	4.02	4.02	-1.32	8.3	0.00
42	480	1500	-1227	-2	0	141	-69	4.02	4.02	4.02	4.02	-0.46	2.9	0.00
43	480	656	-1293	-14	0	89	-197	4.02	4.02	4.02	4.02	-1.32	8.3	0.00
44	480	926	-1287	12	0	169	-173	4.02	4.02	4.02	4.02	-1.16	7.3	0.00
45	480	1821	-1164	-3	0	112	43	4.02	4.02	4.02	4.02	-0.29	1.8	0.00
46	480	650	-1272	-1	0	94	-153	4.02	4.02	4.02	4.02	-1.03	6.4	0.00
47	480	603	-1266	-1	0	83	-142	4.02	4.02	4.02	4.02	-0.95	6.0	0.00
49	480	590	-1268	-3	0	78	-148	4.02	4.02	4.02	4.02	-0.99	6.2	0.00
50	480	644	-1267	2	0	94	-143	4.02	4.02	4.02	4.02	-0.96	6.0	0.00
51	480	823	-1242	-1	0	83	-100	4.02	4.02	4.02	4.02	-0.67	4.2	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	540	801	-1714	-9	0	133	-1118	4.02	4.02	4.02	4.02	-7.50	47.0	0.00
41	540	841	-1707	-1	0	142	-1098	4.02	4.02	4.02	4.02	-7.37	46.1	0.00
42	540	1500	-1637	-2	0	142	-928	4.02	4.02	4.02	4.02	-6.23	39.0	0.00
43	540	656	-1703	-14	0	97	-1096	4.02	4.02	4.02	4.02	-7.35	46.1	0.00
44	540	926	-1697	12	0	162	-1068	4.02	4.02	4.02	4.02	-7.17	44.9	0.00
45	540	1821	-1574	-3	0	114	-779	4.02	4.02	4.02	4.02	-5.22	32.7	0.00
46	540	650	-1682	-1	0	95	-1040	4.02	4.02	4.02	4.02	-6.98	43.7	0.00
47	540	603	-1676	-1	0	83	-1025	4.02	4.02	4.02	4.02	-6.88	43.1	0.00
49	540	590	-1678	-3	0	80	-1032	4.02	4.02	4.02	4.02	-6.93	43.4	0.00
50	540	644	-1677	2	0	93	-1026	4.02	4.02	4.02	4.02	-6.88	43.1	0.00
51	540	823	-1652	-1	0	83	-969	4.02	4.02	4.02	4.02	-6.50	40.7	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	600	801	-2124	-9	0	138	-2270	4.02	4.02	4.02	4.02	-15.23	95.4	0.00
41	600	841	-2117	-1	0	142	-2245	4.02	4.02	4.02	4.02	-15.06	94.4	0.00
42	600	1500	-2047	-2	0	144	-2033	4.02	4.02	4.02	4.02	-13.64	85.4	0.00
43	600	656	-2113	-14	0	106	-2241	4.02	4.02	4.02	4.02	-15.04	94.2	0.00
44	600	926	-2107	12	0	154	-2209	4.02	4.02	4.02	4.02	-14.82	92.8	0.00
45	600	1821	-1984	-3	0	115	-1846	4.02	4.02	4.02	4.02	-12.39	77.6	0.00
46	600	650	-2092	-1	0	95	-2172	4.02	4.02	4.02	4.02	-14.57	91.3	0.00
47	600	603	-2086	-1	0	83	-2153	4.02	4.02	4.02	4.02	-14.45	90.5	0.00
49	600	590	-2088	-3	0	82	-2162	4.02	4.02	4.02	4.02	-14.51	90.9	0.00
50	600	644	-2087	2	0	92	-2155	4.02	4.02	4.02	4.02	-14.46	90.6	0.00
51	600	823	-2062	-1	0	84	-2083	4.02	4.02	4.02	4.02	-13.98	87.6	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

Nome travata: **trave_302_IP1** Descrizione: **Trave_3 7-6-5-4-3-2-1**
ASTA NUM. 9 NI 80 NF 81 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y Permanente qy tot.
qy medio: 375.00 308.00 683.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	[Fx]	[Fy]	[Fz]	[Mx]	[My]	Mz	[APOST]	[AANT]	AINF	ASUP	Sc	Sf	w
	cm	daN			daN*m			cm^2				daN/cm^2		mm
40	0	627	1962	29	0	191	-1775	4.02	4.02	4.02	4.02	-11.91	74.6	0.00
41	0	707	1974	24	0	195	-1809	4.02	4.02	4.02	4.02	-12.14	76.0	0.00
42	0	1260	2047	12	0	152	-2029	4.02	4.02	4.02	4.02	-13.61	85.3	0.00
43	0	493	1971	27	0	148	-1806	4.02	4.02	4.02	4.02	-12.12	75.9	0.00
44	0	854	1991	18	0	210	-1859	4.02	4.02	4.02	4.02	-12.47	78.1	0.00
45	0	1548	2114	-1	0	83	-2231	4.02	4.02	4.02	4.02	-14.97	93.8	0.00
46	0	579	2001	17	0	132	-1896	4.02	4.02	4.02	4.02	-12.72	79.7	0.00
47	0	547	2008	15	0	117	-1918	4.02	4.02	4.02	4.02	-12.87	80.6	0.00
49	0	520	2004	16	0	115	-1906	4.02	4.02	4.02	4.02	-12.79	80.1	0.00
50	0	592	2008	14	0	128	-1917	4.02	4.02	4.02	4.02	-12.86	80.6	0.00
51	0	731	2033	11	0	102	-1991	4.02	4.02	4.02	4.02	-13.36	83.7	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	60	627	1552	29	0	173	-721	4.02	4.02	4.02	4.02	-4.84	30.3	0.00
41	60	707	1564	24	0	181	-748	4.02	4.02	4.02	4.02	-5.02	31.4	0.00
42	60	1260	1637	12	0	144	-924	4.02	4.02	4.02	4.02	-6.20	38.8	0.00
43	60	493	1561	27	0	132	-746	4.02	4.02	4.02	4.02	-5.01	31.4	0.00
44	60	854	1581	18	0	199	-787	4.02	4.02	4.02	4.02	-5.28	33.1	0.00
45	60	1548	1704	-1	0	84	-1086	4.02	4.02	4.02	4.02	-7.28	45.6	0.00
46	60	579	1591	17	0	122	-818	4.02	4.02	4.02	4.02	-5.49	34.4	0.00
47	60	547	1598	15	0	108	-836	4.02	4.02	4.02	4.02	-5.61	35.1	0.00
49	60	520	1594	16	0	105	-826	4.02	4.02	4.02	4.02	-5.55	34.7	0.00
50	60	592	1598	14	0	119	-835	4.02	4.02	4.02	4.02	-5.60	35.1	0.00
51	60	731	1623	11	0	96	-894	4.02	4.02	4.02	4.02	-6.00	37.6	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	120	627	1142	29	0	156	88	4.02	4.02	4.02	4.02	-0.59	3.7	0.00
41	120	707	1154	24	0	166	68	4.02	4.02	4.02	4.02	-0.45	2.8	0.00
42	120	1260	1227	12	0	137	-64	4.02	4.02	4.02	4.02	-0.43	2.7	0.00
43	120	493	1151	27	0	116	68	4.02	4.02	4.02	4.02	-0.46	2.9	0.00
44	120	854	1171	18	0	189	38	4.02	4.02	4.02	4.02	-0.26	1.6	0.00
45	120	1548	1294	-1	0	84	-186	4.02	4.02	4.02	4.02	-1.25	7.8	0.00
46	120	579	1181	17	0	112	14	4.02	4.02	4.02	4.02	-0.09	0.6	0.00
47	120	547	1188	15	0	99	0	4.02	4.02	4.02	4.02	-0.00	0.0	0.00
49	120	520	1184	16	0	96	7	4.02	4.02	4.02	4.02	-0.05	0.3	0.00
50	120	592	1188	14	0	110	1	4.02	4.02	4.02	4.02	-0.01	0.0	0.00
51	120	731	1213	11	0	89	-44	4.02	4.02	4.02	4.02	-0.29	1.8	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	180	627	733	29	0	139	650	4.02	4.02	4.02	4.02	-4.36	27.3	0.00
41	180	707	745	24	0	152	637	4.02	4.02	4.02	4.02	-4.28	26.8	0.00
42	180	1260	818	12	0	130	550	4.02	4.02	4.02	4.02	-3.69	23.1	0.00
43	180	493	742	27	0	100	636	4.02	4.02	4.02	4.02	-4.27	26.7	0.00
44	180	854	762	18	0	178	618	4.02	4.02	4.02	4.02	-4.15	26.0	0.00
45	180	1548	885	-1	0	85	467	4.02	4.02	4.02	4.02	-3.14	19.6	0.00
46	180	579	772	17	0	102	600	4.02	4.02	4.02	4.02	-4.02	25.2	0.00
47	180	547	779	15	0	90	590	4.02	4.02	4.02	4.02	-3.96	24.8	0.00
49	180	520	775	16	0	86	595	4.02	4.02	4.02	4.02	-3.99	25.0	0.00
50	180	592	779	14	0	101	591	4.02	4.02	4.02	4.02	-3.97	24.9	0.00
51	180	731	804	11	0	83	561	4.02	4.02	4.02	4.02	-3.77	23.6	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	240	627	323	29	0	122	967	4.02	4.02	4.02	4.02	-6.49	40.7	0.00
41	240	707	335	24	0	137	961	4.02	4.02	4.02	4.02	-6.45	40.4	0.00
42	240	1260	408	12	0	123	918	4.02	4.02	4.02	4.02	-6.16	38.6	0.00
43	240	493	332	27	0	84	959	4.02	4.02	4.02	4.02	-6.43	40.3	0.00
44	240	854	352	18	0	167	952	4.02	4.02	4.02	4.02	-6.39	40.0	0.00
45	240	1548	475	-1	0	86	875	4.02	4.02	4.02	4.02	-5.87	36.8	0.00
46	240	579	362	17	0	92	940	4.02	4.02	4.02	4.02	-6.31	39.5	0.00
47	240	547	369	15	0	81	935	4.02	4.02	4.02	4.02	-6.27	39.3	0.00
49	240	520	365	16	0	76	937	4.02	4.02	4.02	4.02	-6.29	39.4	0.00
50	240	592	369	14	0	93	936	4.02	4.02	4.02	4.02	-6.28	39.3	0.00
51	240	731	394	11	0	76	920	4.02	4.02	4.02	4.02	-6.18	38.7	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	300	627	-87	29	0	105	1038	4.02	4.02	4.02	4.02	-6.96	43.6	0.00
41	300	707	-75	24	0	122	1039	4.02	4.02	4.02	4.02	-6.97	43.6	0.00
42	300	1260	-2	12	0	116	1040	4.02	4.02	4.02	4.02	-6.98	43.7	0.00
43	300	493	-78	27	0	67	1035	4.02	4.02	4.02	4.02	-6.94	43.5	0.00
44	300	854	-58	18	0	157	1040	4.02	4.02	4.02	4.02	-6.98	43.7	0.00
45	300	1548	65	-1	0	87	1037	4.02	4.02	4.02	4.02	-6.96	43.6	0.00
46	300	579	-48	17	0	82	1034	4.02	4.02	4.02	4.02	-6.94	43.5	0.00
47	300	547	-41	15	0	72	1033	4.02	4.02	4.02	4.02	-6.93	43.4	0.00
49	300	520	-45	16	0	66	1033	4.02	4.02	4.02	4.02	-6.93	43.4	0.00
50	300	592	-41	14	0	84	1034	4.02	4.02	4.02	4.02	-6.94	43.5	0.00
51	300	731	-16	11	0	70	1034	4.02	4.02	4.02	4.02	-6.93	43.4	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	360	627	-497	29	0	87	863	4.02	4.02	4.02	4.02	-5.79	36.3	0.00
41	360	707	-485	24	0	108	870	4.02	4.02	4.02	4.02	-5.84	36.6	0.00
42	360	1260	-412	12	0	109	916	4.02	4.02	4.02	4.02	-6.14	38.5	0.00
43	360	493	-488	27	0	51	866	4.02	4.02	4.02	4.02	-5.81	36.4	0.00
44	360	854	-468	18	0	146	882	4.02	4.02	4.02	4.02	-5.92	37.1	0.00
45	360	1548	-345	-1	0	87	953	4.02	4.02	4.02	4.02	-6.39	40.1	0.00
46	360	579	-458	17	0	72	882	4.02	4.02	4.02	4.02	-5.92	37.1	0.00
47	360	547	-451	15	0	63	886	4.02	4.02	4.02	4.02	-5.94	37.2	0.00
49	360	520	-455	16	0	56	883	4.02	4.02	4.02	4.02	-5.93	37.1	0.00
50	360	592	-451	14	0	75	887	4.02	4.02	4.02	4.02	-5.95	37.3	0.00
51	360	731	-426	11	0	64	901	4.02	4.02	4.02	4.02	-6.04	37.9	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	420	627	-907	29	0	70	442	4.02	4.02	4.02	4.02	-2.97	18.6	0.00
41	420	707	-895	24	0	93	456	4.02	4.02	4.02	4.02	-3.06	19.2	0.00
42	420	1260	-822	12	0	102	546	4.02	4.02	4.02	4.02	-3.66	22.9	0.00
43	420	493	-898	27	0	35	450	4.02	4.02	4.02	4.02	-3.02	18.9	0.00
44	420	854	-878	18	0	136	478	4.02	4.02	4.02	4.02	-3.21	20.1	0.00
45	420	1548	-755	-1	0	88	623	4.02	4.02	4.02	4.02	-4.18	26.2	0.00
46	420	579	-868	17	0	62	485	4.02	4.02	4.02	4.02	-3.25	20.4	0.00
47	420	547	-861	15	0	54	492	4.02	4.02	4.02	4.02	-3.30	20.7	0.00
49	420	520	-865	16	0	46	487	4.02	4.02	4.02	4.02	-3.27	20.5	0.00
50	420	592	-861	14	0	67	493	4.02	4.02	4.02	4.02	-3.31	20.7	0.00
51	420	731	-836	11	0	57	522	4.02	4.02	4.02	4.02	-3.50	21.9	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	480	627	-1316	29	0	53	-225	4.02	4.02	4.02	4.02	-1.51	9.4	0.00
41	480	707	-1304	24	0	79	-204	4.02	4.02	4.02	4.02	-1.37	8.6	0.00
42	480	1260	-1231	12	0	95	-70	4.02	4.02	4.02	4.02	-0.47	2.9	0.00
43	480	493	-1307	27	0	19	-211	4.02	4.02	4.02	4.02	-1.42	8.9	0.00
44	480	854	-1287	18	0	125	-171	4.02	4.02	4.02	4.02	-1.15	7.2	0.00
45	480	1548	-1164	-1	0	89	47	4.02	4.02	4.02	4.02	-0.32	2.0	0.00
46	480	579	-1277	17	0	52	-159	4.02	4.02	4.02	4.02	-1.06	6.7	0.00
47	480	547	-1270	15	0	45	-147	4.02	4.02	4.02	4.02	-0.99	6.2	0.00
49	480	520	-1274	16	0	37	-154	4.02	4.02	4.02	4.02	-1.03	6.5	0.00
50	480	592	-1270	14	0	58	-146	4.02	4.02	4.02	4.02	-0.98	6.1	0.00
51	480	731	-1245	11	0	51	-102	4.02	4.02	4.02	4.02	-0.69	4.3	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	540	627	-1726	29	0	36	-1137	4.02	4.02	4.02	4.02	-7.63	47.8	0.00
41	540	707	-1714	24	0	64	-1109	4.02	4.02	4.02	4.02	-7.44	46.6	0.00
42	540	1260	-1641	12	0	88	-932	4.02	4.02	4.02	4.02	-6.25	39.2	0.00
43	540	493	-1717	27	0	3	-1118	4.02	4.02	4.02	4.02	-7.50	47.0	0.00
44	540	854	-1697	18	0	115	-1067	4.02	4.02	4.02	4.02	-7.16	44.8	0.00
45	540	1548	-1574	-1	0	90	-774	4.02	4.02	4.02	4.02	-5.20	32.6	0.00
46	540	579	-1687	17	0	42	-1048	4.02	4.02	4.02	4.02	-7.03	44.0	0.00
47	540	547	-1680	15	0	36	-1032	4.02	4.02	4.02	4.02	-6.92	43.4	0.00
49	540	520	-1684	16	0	27	-1042	4.02	4.02	4.02	4.02	-6.99	43.8	0.00
50	540	592	-1680	14	0	49	-1031	4.02	4.02	4.02	4.02	-6.92	43.3	0.00
51	540	731	-1655	11	0	44	-973	4.02	4.02	4.02	4.02	-6.53	40.9	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	600	627	-2136	29	0	18	-2296	4.02	4.02	4.02	4.02	-15.41	96.5	0.00
41	600	707	-2124	24	0	50	-2261	4.02	4.02	4.02	4.02	-15.17	95.0	0.00
42	600	1260	-2051	12	0	81	-2039	4.02	4.02	4.02	4.02	-13.68	85.7	0.00
43	600	493	-2127	27	0	-13	-2271	4.02	4.02	4.02	4.02	-15.24	95.5	0.00
44	600	854	-2107	18	0	104	-2208	4.02	4.02	4.02	4.02	-14.82	92.8	0.00
45	600	1548	-1984	-1	0	90	-1842	4.02	4.02	4.02	4.02	-12.36	77.4	0.00
46	600	579	-2097	17	0	32	-2183	4.02	4.02	4.02	4.02	-14.65	91.8	0.00
47	600	547	-2090	15	0	27	-2163	4.02	4.02	4.02	4.02	-14.51	90.9	0.00
49	600	520	-2094	16	0	17	-2175	4.02	4.02	4.02	4.02	-14.59	91.4	0.00
50	600	592	-2090	14	0	40	-2162	4.02	4.02	4.02	4.02	-14.51	90.9	0.00
51	600	731	-2065	11	0	38	-2089	4.02	4.02	4.02	4.02	-14.02	87.8	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

Nome travata: **trave_302_IP1** Descrizione: **Trave_3 7-6-5-4-3-2-1**
ASTA NUM. 10 NI 81 NF 82 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y Permanente qy tot.
qy medio: 375.00 308.00 683.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	[Fx]	[Fy]	[Fz]	[Mx]	[My]	Mz	[APOST]	[AANT]	AINF	ASUP	Sc	Sf	w

--														--
	cm		daN			daN*m			cm^2				daN/cm^2	mm
40	0	341	1886	102	0	446	-1593	4.02	4.02	4.02	4.02	-10.69	67.0	0.00
41	0	464	1918	117	0	502	-1676	4.02	4.02	4.02	4.02	-11.25	70.4	0.00
42	0	956	1989	102	0	464	-1894	4.02	4.02	4.02	4.02	-12.71	79.6	0.00
43	0	242	1895	68	0	304	-1622	4.02	4.02	4.02	4.02	-10.88	68.2	0.00
44	0	673	1966	147	0	613	-1801	4.02	4.02	4.02	4.02	-12.08	75.7	0.00
45	0	1269	2067	68	0	335	-2122	4.02	4.02	4.02	4.02	-14.24	89.2	0.00
46	0	439	1965	79	0	334	-1809	4.02	4.02	4.02	4.02	-12.14	76.0	0.00
47	0	433	1977	70	0	292	-1843	4.02	4.02	4.02	4.02	-12.37	77.5	0.00
49	0	392	1966	65	0	274	-1815	4.02	4.02	4.02	4.02	-12.18	76.3	0.00
50	0	478	1981	80	0	336	-1851	4.02	4.02	4.02	4.02	-12.42	77.8	0.00
51	0	597	2001	65	0	280	-1915	4.02	4.02	4.02	4.02	-12.85	80.5	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	60	341	1476	102	0	385	-584	4.02	4.02	4.02	4.02	-3.92	24.6	0.00
41	60	464	1508	117	0	432	-648	4.02	4.02	4.02	4.02	-4.35	27.2	0.00
42	60	956	1579	102	0	403	-823	4.02	4.02	4.02	4.02	-5.52	34.6	0.00
43	60	242	1485	68	0	263	-608	4.02	4.02	4.02	4.02	-4.08	25.6	0.00
44	60	673	1556	147	0	525	-744	4.02	4.02	4.02	4.02	-4.99	31.3	0.00
45	60	1269	1657	68	0	294	-1005	4.02	4.02	4.02	4.02	-6.74	42.2	0.00
46	60	439	1555	79	0	287	-753	4.02	4.02	4.02	4.02	-5.05	31.6	0.00
47	60	433	1567	70	0	251	-780	4.02	4.02	4.02	4.02	-5.23	32.8	0.00
49	60	392	1556	65	0	235	-758	4.02	4.02	4.02	4.02	-5.09	31.9	0.00
50	60	478	1571	80	0	287	-786	4.02	4.02	4.02	4.02	-5.27	33.0	0.00
51	60	597	1591	65	0	241	-838	4.02	4.02	4.02	4.02	-5.62	35.2	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	120	341	1066	102	0	324	179	4.02	4.02	4.02	4.02	-1.20	7.5	0.00
41	120	464	1098	117	0	361	134	4.02	4.02	4.02	4.02	-0.90	5.6	0.00
42	120	956	1169	102	0	342	1	4.02	4.02	4.02	4.02	-0.01	0.1	0.00
43	120	242	1075	68	0	222	160	4.02	4.02	4.02	4.02	-1.07	6.7	0.00
44	120	673	1146	147	0	437	67	4.02	4.02	4.02	4.02	-0.45	2.8	0.00
45	120	1269	1247	68	0	253	-134	4.02	4.02	4.02	4.02	-0.90	5.6	0.00
46	120	439	1145	79	0	239	57	4.02	4.02	4.02	4.02	-0.38	2.4	0.00
47	120	433	1157	70	0	209	38	4.02	4.02	4.02	4.02	-0.25	1.6	0.00
49	120	392	1146	65	0	196	53	4.02	4.02	4.02	4.02	-0.35	2.2	0.00
50	120	478	1161	80	0	239	34	4.02	4.02	4.02	4.02	-0.23	1.4	0.00
51	120	597	1181	65	0	202	-6	4.02	4.02	4.02	4.02	-0.04	0.3	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	180	341	657	102	0	263	696	4.02	4.02	4.02	4.02	-4.67	29.2	0.00
41	180	464	689	117	0	291	670	4.02	4.02	4.02	4.02	-4.49	28.1	0.00
42	180	956	760	102	0	281	580	4.02	4.02	4.02	4.02	-3.89	24.4	0.00
43	180	242	666	68	0	181	682	4.02	4.02	4.02	4.02	-4.58	28.7	0.00
44	180	673	737	147	0	349	632	4.02	4.02	4.02	4.02	-4.24	26.5	0.00
45	180	1269	838	68	0	212	491	4.02	4.02	4.02	4.02	-3.30	20.6	0.00
46	180	439	736	79	0	192	622	4.02	4.02	4.02	4.02	-4.17	26.1	0.00
47	180	433	748	70	0	167	609	4.02	4.02	4.02	4.02	-4.09	25.6	0.00
49	180	392	737	65	0	157	618	4.02	4.02	4.02	4.02	-4.15	26.0	0.00
50	180	478	752	80	0	191	608	4.02	4.02	4.02	4.02	-4.08	25.5	0.00
51	180	597	772	65	0	163	580	4.02	4.02	4.02	4.02	-3.89	24.4	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	240	341	247	102	0	201	967	4.02	4.02	4.02	4.02	-6.49	40.6	0.00
41	240	464	279	117	0	221	960	4.02	4.02	4.02	4.02	-6.44	40.3	0.00
42	240	956	350	102	0	220	913	4.02	4.02	4.02	4.02	-6.13	38.4	0.00
43	240	242	256	68	0	140	958	4.02	4.02	4.02	4.02	-6.43	40.3	0.00
44	240	673	327	147	0	261	951	4.02	4.02	4.02	4.02	-6.38	40.0	0.00
45	240	1269	428	68	0	171	871	4.02	4.02	4.02	4.02	-5.84	36.6	0.00
46	240	439	326	79	0	144	940	4.02	4.02	4.02	4.02	-6.31	39.5	0.00
47	240	433	338	70	0	125	935	4.02	4.02	4.02	4.02	-6.27	39.3	0.00
49	240	392	327	65	0	119	937	4.02	4.02	4.02	4.02	-6.29	39.4	0.00
50	240	478	342	80	0	143	936	4.02	4.02	4.02	4.02	-6.28	39.3	0.00
51	240	597	362	65	0	125	920	4.02	4.02	4.02	4.02	-6.17	38.7	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	300	341	-163	102	0	140	992	4.02	4.02	4.02	4.02	-6.66	41.7	0.00
41	300	464	-131	117	0	151	1004	4.02	4.02	4.02	4.02	-6.74	42.2	0.00
42	300	956	-60	102	0	158	1001	4.02	4.02	4.02	4.02	-6.71	42.1	0.00
43	300	242	-154	68	0	99	989	4.02	4.02	4.02	4.02	-6.63	41.5	0.00
44	300	673	-83	147	0	173	1024	4.02	4.02	4.02	4.02	-6.87	43.0	0.00
45	300	1269	18	68	0	130	1004	4.02	4.02	4.02	4.02	-6.74	42.2	0.00
46	300	439	-84	79	0	97	1013	4.02	4.02	4.02	4.02	-6.79	42.6	0.00
47	300	433	-72	70	0	83	1015	4.02	4.02	4.02	4.02	-6.81	42.6	0.00
49	300	392	-83	65	0	80	1011	4.02	4.02	4.02	4.02	-6.78	42.5	0.00
50	300	478	-68	80	0	95	1018	4.02	4.02	4.02	4.02	-6.83	42.8	0.00
51	300	597	-48	65	0	86	1014	4.02	4.02	4.02	4.02	-6.80	42.6	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	360	341	-573	102	0	79	771	4.02	4.02	4.02	4.02	-5.18	32.4	0.00
41	360	464	-541	117	0	80	802	4.02	4.02	4.02	4.02	-5.38	33.7	0.00
42	360	956	-470	102	0	97	842	4.02	4.02	4.02	4.02	-5.65	35.4	0.00
43	360	242	-564	68	0	58	773	4.02	4.02	4.02	4.02	-5.19	32.5	0.00
44	360	673	-493	147	0	85	851	4.02	4.02	4.02	4.02	-5.71	35.8	0.00
45	360	1269	-392	68	0	89	892	4.02	4.02	4.02	4.02	-5.98	37.5	0.00
46	360	439	-494	79	0	49	839	4.02	4.02	4.02	4.02	-5.63	35.3	0.00
47	360	433	-482	70	0	41	848	4.02	4.02	4.02	4.02	-5.69	35.7	0.00
49	360	392	-493	65	0	41	838	4.02	4.02	4.02	4.02	-5.62	35.2	0.00
50	360	478	-478	80	0	46	854	4.02	4.02	4.02	4.02	-5.73	35.9	0.00
51	360	597	-458	65	0	47	862	4.02	4.02	4.02	4.02	-5.78	36.2	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	420	341	-983	102	0	18	305	4.02	4.02	4.02	4.02	-2.05	12.8	0.00
41	420	464	-951	117	0	10	355	4.02	4.02	4.02	4.02	-2.38	14.9	0.00
42	420	956	-880	102	0	36	437	4.02	4.02	4.02	4.02	-2.93	18.4	0.00
43	420	242	-974	68	0	17	312	4.02	4.02	4.02	4.02	-2.09	13.1	0.00
44	420	673	-903	147	0	-2	433	4.02	4.02	4.02	4.02	-2.90	18.2	0.00
45	420	1269	-802	68	0	48	533	4.02	4.02	4.02	4.02	-3.58	22.4	0.00
46	420	439	-904	79	0	2	420	4.02	4.02	4.02	4.02	-2.82	17.7	0.00
47	420	433	-892	70	0	-0	436	4.02	4.02	4.02	4.02	-2.93	18.3	0.00

49	420	392	-903	65	0	2	420	4.02	4.02	4.02	4.02	-2.82	17.6	0.00
50	420	478	-888	80	0	-2	444	4.02	4.02	4.02	4.02	-2.98	18.7	0.00
51	420	597	-868	65	0	8	464	4.02	4.02	4.02	4.02	-3.11	19.5	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	480	341	-1392	102	0	-44	-408	4.02	4.02	4.02	4.02	-2.73	17.1	0.00
41	480	464	-1360	117	0	-60	-339	4.02	4.02	4.02	4.02	-2.27	14.2	0.00
42	480	956	-1289	102	0	-25	-213	4.02	4.02	4.02	4.02	-1.43	9.0	0.00
43	480	242	-1383	68	0	-24	-396	4.02	4.02	4.02	4.02	-2.66	16.6	0.00
44	480	673	-1312	147	0	-90	-232	4.02	4.02	4.02	4.02	-1.55	9.7	0.00
45	480	1269	-1211	68	0	7	-71	4.02	4.02	4.02	4.02	-0.48	3.0	0.00
46	480	439	-1313	79	0	-46	-245	4.02	4.02	4.02	4.02	-1.65	10.3	0.00
47	480	433	-1301	70	0	-42	-222	4.02	4.02	4.02	4.02	-1.49	9.3	0.00
49	480	392	-1312	65	0	-37	-245	4.02	4.02	4.02	4.02	-1.64	10.3	0.00
50	480	478	-1297	80	0	-50	-212	4.02	4.02	4.02	4.02	-1.42	8.9	0.00
51	480	597	-1277	65	0	-31	-180	4.02	4.02	4.02	4.02	-1.21	7.6	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	540	341	-1802	102	0	-105	-1366	4.02	4.02	4.02	4.02	-9.16	57.4	0.00
41	540	464	-1770	117	0	-130	-1278	4.02	4.02	4.02	4.02	-8.57	53.7	0.00
42	540	956	-1699	102	0	-87	-1110	4.02	4.02	4.02	4.02	-7.45	46.6	0.00
43	540	242	-1793	68	0	-65	-1349	4.02	4.02	4.02	4.02	-9.05	56.7	0.00
44	540	673	-1722	147	0	-178	-1142	4.02	4.02	4.02	4.02	-7.66	48.0	0.00
45	540	1269	-1621	68	0	-34	-921	4.02	4.02	4.02	4.02	-6.18	38.7	0.00
46	540	439	-1723	79	0	-93	-1156	4.02	4.02	4.02	4.02	-7.76	48.6	0.00
47	540	433	-1711	70	0	-84	-1125	4.02	4.02	4.02	4.02	-7.55	47.3	0.00
49	540	392	-1722	65	0	-76	-1155	4.02	4.02	4.02	4.02	-7.75	48.5	0.00
50	540	478	-1707	80	0	-98	-1114	4.02	4.02	4.02	4.02	-7.47	46.8	0.00
51	540	597	-1687	65	0	-69	-1070	4.02	4.02	4.02	4.02	-7.18	45.0	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	600	341	-2212	102	0	-166	-2570	4.02	4.02	4.02	4.02	-17.24	108.0	0.00
41	600	464	-2180	117	0	-201	-2463	4.02	4.02	4.02	4.02	-16.53	103.5	0.00
42	600	956	-2109	102	0	-148	-2252	4.02	4.02	4.02	4.02	-15.11	94.7	0.00
43	600	242	-2203	68	0	-106	-2548	4.02	4.02	4.02	4.02	-17.10	107.1	0.00
44	600	673	-2132	147	0	-266	-2298	4.02	4.02	4.02	4.02	-15.42	96.6	0.00
45	600	1269	-2031	68	0	-75	-2017	4.02	4.02	4.02	4.02	-13.53	84.8	0.00
46	600	439	-2133	79	0	-141	-2313	4.02	4.02	4.02	4.02	-15.52	97.2	0.00
47	600	433	-2121	70	0	-126	-2275	4.02	4.02	4.02	4.02	-15.27	95.6	0.00
49	600	392	-2132	65	0	-114	-2311	4.02	4.02	4.02	4.02	-15.51	97.1	0.00
50	600	478	-2117	80	0	-146	-2261	4.02	4.02	4.02	4.02	-15.17	95.0	0.00
51	600	597	-2097	65	0	-108	-2205	4.02	4.02	4.02	4.02	-14.80	92.7	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

Nome travata: **trave_302_IP1** Descrizione: **Trave_3 7-6-5-4-3-2-1**
ASTA NUM. 11 NI 82 NF 302 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y Permanente qy tot.
qy medio: 375.00 308.00 683.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	[Fx]	[Fy]	[Fz]	[Mx]	[My]	Mz	[APOST]	[AANT]	AINF	ASUP	Sc	Sf	w
	cm	daN			daN*m			cm^2				daN/cm^2		mm
40	0	-691	1943	265	0	701	-1579	4.02	4.02	4.02	4.02	-10.60	66.4	0.00
41	0	-307	2000	279	0	744	-1769	4.02	4.02	4.02	4.02	-11.87	74.4	0.00
42	0	87	2077	290	0	765	-1984	4.02	4.02	4.02	4.02	-13.31	83.4	0.00
43	0	-735	1936	192	0	502	-1559	4.02	4.02	4.02	4.02	-10.46	65.5	0.00
44	0	301	2089	314	0	842	-2067	4.02	4.02	4.02	4.02	-13.87	86.9	0.00
45	0	562	2159	233	0	609	-2233	4.02	4.02	4.02	4.02	-14.98	93.9	0.00
46	0	34	2049	178	0	472	-1939	4.02	4.02	4.02	4.02	-13.01	81.5	0.00
47	0	119	2061	152	0	404	-1982	4.02	4.02	4.02	4.02	-13.30	83.3	0.00
49	0	-9	2042	147	0	390	-1918	4.02	4.02	4.02	4.02	-12.87	80.6	0.00
50	0	198	2073	172	0	458	-2020	4.02	4.02	4.02	4.02	-13.55	84.9	0.00
51	0	250	2087	156	0	411	-2053	4.02	4.02	4.02	4.02	-13.78	86.3	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	60	-691	1533	265	0	542	-536	4.02	4.02	4.02	4.02	-3.60	22.5	0.00
41	60	-307	1590	279	0	576	-692	4.02	4.02	4.02	4.02	-4.64	29.1	0.00
42	60	87	1667	290	0	591	-861	4.02	4.02	4.02	4.02	-5.78	36.2	0.00
43	60	-735	1526	192	0	387	-520	4.02	4.02	4.02	4.02	-3.49	21.9	0.00
44	60	301	1679	314	0	654	-937	4.02	4.02	4.02	4.02	-6.29	39.4	0.00
45	60	562	1749	233	0	469	-1061	4.02	4.02	4.02	4.02	-7.12	44.6	0.00
46	60	34	1639	178	0	365	-833	4.02	4.02	4.02	4.02	-5.59	35.0	0.00
47	60	119	1651	152	0	313	-868	4.02	4.02	4.02	4.02	-5.83	36.5	0.00
49	60	-9	1632	147	0	301	-816	4.02	4.02	4.02	4.02	-5.47	34.3	0.00
50	60	198	1663	172	0	355	-899	4.02	4.02	4.02	4.02	-6.03	37.8	0.00
51	60	250	1677	156	0	318	-924	4.02	4.02	4.02	4.02	-6.20	38.8	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	120	-691	1123	265	0	383	261	4.02	4.02	4.02	4.02	-1.75	11.0	0.00
41	120	-307	1180	279	0	408	139	4.02	4.02	4.02	4.02	-0.93	5.8	0.00
42	120	87	1257	290	0	417	17	4.02	4.02	4.02	4.02	-0.11	0.7	0.00
43	120	-735	1116	192	0	272	272	4.02	4.02	4.02	4.02	-1.83	11.4	0.00
44	120	301	1269	314	0	466	-52	4.02	4.02	4.02	4.02	-0.35	2.2	0.00
45	120	562	1339	233	0	329	-134	4.02	4.02	4.02	4.02	-0.90	5.6	0.00
46	120	34	1229	178	0	259	28	4.02	4.02	4.02	4.02	-0.19	1.2	0.00
47	120	119	1241	152	0	222	-0	4.02	4.02	4.02	4.02	-0.00	0.0	0.00
49	120	-9	1222	147	0	213	41	4.02	4.02	4.02	4.02	-0.27	1.7	0.00
50	120	198	1253	172	0	252	-25	4.02	4.02	4.02	4.02	-0.16	1.0	0.00
51	120	250	1267	156	0	224	-41	4.02	4.02	4.02	4.02	-0.27	1.7	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	180	-691	714	265	0	224	812	4.02	4.02	4.02	4.02	-5.45	34.1	0.00
41	180	-307	771	279	0	241	724	4.02	4.02	4.02	4.02	-4.86	30.4	0.00
42	180	87	848	290	0	243	648	4.02	4.02	4.02	4.02	-4.35	27.2	0.00
43	180	-735	707	192	0	157	819	4.02	4.02	4.02	4.02	-5.50	34.4	0.00
44	180	301	860	314	0	278	586	4.02	4.02	4.02	4.02	-3.93	24.6	0.00
45	180	562	930	233	0	189	547	4.02	4.02	4.02	4.02	-3.67	23.0	0.00

46	180	34	820	178	0	152	642	4.02	4.02	4.02	4.02	-4.31	27.0	0.00
47	180	119	832	152	0	130	622	4.02	4.02	4.02	4.02	-4.17	26.1	0.00
49	180	-9	813	147	0	125	651	4.02	4.02	4.02	4.02	-4.37	27.4	0.00
50	180	198	844	172	0	149	604	4.02	4.02	4.02	4.02	-4.06	25.4	0.00
51	180	250	858	156	0	131	597	4.02	4.02	4.02	4.02	-4.00	25.1	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	240	-691	304	265	0	65	1117	4.02	4.02	4.02	4.02	-7.50	47.0	0.00
41	240	-307	361	279	0	73	1063	4.02	4.02	4.02	4.02	-7.13	44.7	0.00
42	240	87	438	290	0	69	1034	4.02	4.02	4.02	4.02	-6.94	43.4	0.00
43	240	-735	297	192	0	42	1120	4.02	4.02	4.02	4.02	-7.51	47.1	0.00
44	240	301	450	314	0	90	979	4.02	4.02	4.02	4.02	-6.57	41.1	0.00
45	240	562	520	233	0	49	982	4.02	4.02	4.02	4.02	-6.59	41.3	0.00
46	240	34	410	178	0	46	1011	4.02	4.02	4.02	4.02	-6.78	42.5	0.00
47	240	119	422	152	0	39	998	4.02	4.02	4.02	4.02	-6.69	41.9	0.00
49	240	-9	403	147	0	36	1016	4.02	4.02	4.02	4.02	-6.82	42.7	0.00
50	240	198	434	172	0	46	987	4.02	4.02	4.02	4.02	-6.63	41.5	0.00
51	240	250	448	156	0	38	988	4.02	4.02	4.02	4.02	-6.63	41.5	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	300	-691	-106	265	0	-94	1177	4.02	4.02	4.02	4.02	-7.89	49.4	0.00
41	300	-307	-49	279	0	-94	1157	4.02	4.02	4.02	4.02	-7.76	48.6	0.00
42	300	87	28	290	0	-105	1174	4.02	4.02	4.02	4.02	-7.87	49.3	0.00
43	300	-735	-113	192	0	-73	1175	4.02	4.02	4.02	4.02	-7.88	49.4	0.00
44	300	301	40	314	0	-99	1126	4.02	4.02	4.02	4.02	-7.55	47.3	0.00
45	300	562	110	233	0	-91	1171	4.02	4.02	4.02	4.02	-7.85	49.2	0.00
46	300	34	0	178	0	-61	1134	4.02	4.02	4.02	4.02	-7.61	47.7	0.00
47	300	119	12	152	0	-52	1128	4.02	4.02	4.02	4.02	-7.57	47.4	0.00
49	300	-9	-7	147	0	-52	1135	4.02	4.02	4.02	4.02	-7.61	47.7	0.00
50	300	198	24	172	0	-57	1125	4.02	4.02	4.02	4.02	-7.55	47.3	0.00
51	300	250	38	156	0	-56	1134	4.02	4.02	4.02	4.02	-7.61	47.6	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	360	-691	-516	265	0	-253	990	4.02	4.02	4.02	4.02	-6.64	41.6	0.00
41	360	-307	-459	279	0	-262	1004	4.02	4.02	4.02	4.02	-6.74	42.2	0.00
42	360	87	-382	290	0	-279	1067	4.02	4.02	4.02	4.02	-7.16	44.9	0.00
43	360	-735	-523	192	0	-188	984	4.02	4.02	4.02	4.02	-6.60	41.4	0.00
44	360	301	-370	314	0	-287	1026	4.02	4.02	4.02	4.02	-6.89	43.1	0.00
45	360	562	-300	233	0	-231	1114	4.02	4.02	4.02	4.02	-7.47	46.8	0.00
46	360	34	-410	178	0	-167	1011	4.02	4.02	4.02	4.02	-6.78	42.5	0.00
47	360	119	-398	152	0	-143	1012	4.02	4.02	4.02	4.02	-6.79	42.6	0.00
49	360	-9	-417	147	0	-141	1007	4.02	4.02	4.02	4.02	-6.76	42.3	0.00
50	360	198	-386	172	0	-160	1016	4.02	4.02	4.02	4.02	-6.82	42.7	0.00
51	360	250	-372	156	0	-149	1033	4.02	4.02	4.02	4.02	-6.93	43.4	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	420	-691	-926	265	0	-412	558	4.02	4.02	4.02	4.02	-3.74	23.4	0.00
41	420	-307	-869	279	0	-430	606	4.02	4.02	4.02	4.02	-4.06	25.5	0.00
42	420	87	-792	290	0	-453	715	4.02	4.02	4.02	4.02	-4.80	30.1	0.00
43	420	-735	-933	192	0	-303	547	4.02	4.02	4.02	4.02	-3.67	23.0	0.00
44	420	301	-780	314	0	-475	681	4.02	4.02	4.02	4.02	-4.57	28.6	0.00
45	420	562	-710	233	0	-371	811	4.02	4.02	4.02	4.02	-5.44	34.1	0.00
46	420	34	-820	178	0	-274	642	4.02	4.02	4.02	4.02	-4.31	27.0	0.00
47	420	119	-808	152	0	-235	651	4.02	4.02	4.02	4.02	-4.37	27.4	0.00
49	420	-9	-827	147	0	-229	634	4.02	4.02	4.02	4.02	-4.26	26.7	0.00
50	420	198	-796	172	0	-263	661	4.02	4.02	4.02	4.02	-4.44	27.8	0.00
51	420	250	-782	156	0	-242	687	4.02	4.02	4.02	4.02	-4.61	28.9	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	480	-691	-1335	265	0	-571	-121	4.02	4.02	4.02	4.02	-0.81	5.1	0.00
41	480	-307	-1278	279	0	-597	-39	4.02	4.02	4.02	4.02	-0.26	1.6	0.00
42	480	87	-1201	290	0	-627	117	4.02	4.02	4.02	4.02	-0.79	4.9	0.00
43	480	-735	-1342	192	0	-418	-135	4.02	4.02	4.02	4.02	-0.91	5.7	0.00
44	480	301	-1189	314	0	-663	90	4.02	4.02	4.02	4.02	-0.61	3.8	0.00
45	480	562	-1119	233	0	-511	262	4.02	4.02	4.02	4.02	-1.76	11.0	0.00
46	480	34	-1229	178	0	-380	27	4.02	4.02	4.02	4.02	-0.18	1.1	0.00
47	480	119	-1217	152	0	-326	43	4.02	4.02	4.02	4.02	-0.29	1.8	0.00
49	480	-9	-1236	147	0	-317	15	4.02	4.02	4.02	4.02	-0.10	0.6	0.00
50	480	198	-1205	172	0	-366	61	4.02	4.02	4.02	4.02	-0.41	2.5	0.00
51	480	250	-1191	156	0	-336	95	4.02	4.02	4.02	4.02	-0.64	4.0	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	540	-691	-1745	265	0	-730	-1045	4.02	4.02	4.02	4.02	-7.01	43.9	0.00
41	540	-307	-1688	279	0	-765	-929	4.02	4.02	4.02	4.02	-6.23	39.0	0.00
42	540	87	-1611	290	0	-801	-726	4.02	4.02	4.02	4.02	-4.87	30.5	0.00
43	540	-735	-1752	192	0	-533	-1064	4.02	4.02	4.02	4.02	-7.14	44.7	0.00
44	540	301	-1599	314	0	-851	-746	4.02	4.02	4.02	4.02	-5.01	31.4	0.00
45	540	562	-1529	233	0	-651	-533	4.02	4.02	4.02	4.02	-3.57	22.4	0.00
46	540	34	-1639	178	0	-487	-833	4.02	4.02	4.02	4.02	-5.59	35.0	0.00
47	540	119	-1627	152	0	-417	-810	4.02	4.02	4.02	4.02	-5.43	34.0	0.00
49	540	-9	-1646	147	0	-406	-849	4.02	4.02	4.02	4.02	-5.70	35.7	0.00
50	540	198	-1615	172	0	-469	-786	4.02	4.02	4.02	4.02	-5.27	33.0	0.00
51	540	250	-1601	156	0	-429	-743	4.02	4.02	4.02	4.02	-4.99	31.2	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	600	-691	-2155	265	0	-889	-2215	4.02	4.02	4.02	4.02	-14.86	93.1	0.00
41	600	-307	-2098	279	0	-932	-2065	4.02	4.02	4.02	4.02	-13.86	86.8	0.00
42	600	87	-2021	290	0	-975	-1816	4.02	4.02	4.02	4.02	-12.19	76.3	0.00
43	600	-735	-2162	192	0	-648	-2238	4.02	4.02	4.02	4.02	-15.02	94.1	0.00
44	600	301	-2009	314	0	-1039	-1829	4.02	4.02	4.02	4.02	-12.27	76.9	0.00
45	600	562	-1939	233	0	-791	-1573	4.02	4.02	4.02	4.02	-10.55	66.1	0.00
46	600	34	-2049	178	0	-593	-1940	4.02	4.02	4.02	4.02	-13.02	81.5	0.00
47	600	119	-2037	152	0	-508	-1909	4.02	4.02	4.02	4.02	-12.81	80.2	0.00
49	600	-9	-2056	147	0	-494	-1960	4.02	4.02	4.02	4.02	-13.15	82.4	0.00
50	600	198	-2025	172	0	-572	-1878	4.02	4.02	4.02	4.02	-12.60	78.9	0.00
51	600	250	-2011	156	0	-522	-1827	4.02	4.02	4.02	4.02	-12.26	76.8	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

Nome travata: **trave_303_IP1** Descrizione: **Trave_3 32-26**
ASTA NUM. 12 NI 32 NF 83 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y Permanente qy tot.

qy medio: 375.00   308.00   683.00 daN/m

armatura base = 4 X 2.01   per le armature aggiuntive consultare il tabulato

NC	x	[Fx]	[Fy]	[Fz]	[Mx]	[My]	Mz	[APOST]	[AANT]	AINF	ASUP	Sc	Sf	w
	cm	daN			daN*m			cm^2				daN/cm^2		mm
40	0	376	1953	575	0	2006	-1685	4.02	4.02	4.02	4.02	-11.31	70.8	0.00
41	0	520	1977	450	0	1557	-1763	4.02	4.02	4.02	4.02	-11.83	74.1	0.00
42	0	1433	2045	559	0	2020	-1969	4.02	4.02	4.02	4.02	-13.21	82.8	0.00
43	0	241	1940	565	0	1979	-1638	4.02	4.02	4.02	4.02	-10.99	68.8	0.00
44	0	765	2018	257	0	863	-1897	4.02	4.02	4.02	4.02	-12.73	79.7	0.00
45	0	2004	2093	537	0	2004	-2112	4.02	4.02	4.02	4.02	-14.17	88.8	0.00
46	0	460	1982	300	0	1037	-1772	4.02	4.02	4.02	4.02	-11.89	74.5	0.00
47	0	444	1983	262	0	907	-1774	4.02	4.02	4.02	4.02	-11.90	74.6	0.00
49	0	396	1975	304	0	1057	-1748	4.02	4.02	4.02	4.02	-11.73	73.5	0.00
50	0	501	1991	242	0	833	-1800	4.02	4.02	4.02	4.02	-12.08	75.7	0.00
51	0	749	2006	298	0	1062	-1843	4.02	4.02	4.02	4.02	-12.37	77.5	0.00
apost= --		aant= --		ainf= --		asup= --		(e arm. base= 4 X 2.01)						
40	60	376	1543	575	0	1661	-636	4.02	4.02	4.02	4.02	-4.27	26.7	0.00
41	60	520	1567	450	0	1287	-700	4.02	4.02	4.02	4.02	-4.69	29.4	0.00
42	60	1433	1635	559	0	1685	-865	4.02	4.02	4.02	4.02	-5.80	36.3	0.00
43	60	241	1530	565	0	1640	-597	4.02	4.02	4.02	4.02	-4.00	25.1	0.00
44	60	765	1608	257	0	709	-809	4.02	4.02	4.02	4.02	-5.43	34.0	0.00
45	60	2004	1683	537	0	1682	-979	4.02	4.02	4.02	4.02	-6.57	41.1	0.00
46	60	460	1572	300	0	857	-706	4.02	4.02	4.02	4.02	-4.73	29.7	0.00
47	60	444	1573	262	0	750	-707	4.02	4.02	4.02	4.02	-4.74	29.7	0.00
49	60	396	1565	304	0	875	-686	4.02	4.02	4.02	4.02	-4.60	28.8	0.00
50	60	501	1581	242	0	688	-728	4.02	4.02	4.02	4.02	-4.89	30.6	0.00
51	60	749	1596	298	0	883	-762	4.02	4.02	4.02	4.02	-5.12	32.0	0.00
apost= --		aant= --		ainf= --		asup= --		(e arm. base= 4 X 2.01)						
40	120	376	1133	575	0	1315	167	4.02	4.02	4.02	4.02	-1.12	7.0	0.00
41	120	520	1157	450	0	1017	118	4.02	4.02	4.02	4.02	-0.79	5.0	0.00
42	120	1433	1225	559	0	1350	-6	4.02	4.02	4.02	4.02	-0.04	0.3	0.00
43	120	241	1120	565	0	1301	199	4.02	4.02	4.02	4.02	-1.33	8.3	0.00
44	120	765	1198	257	0	554	33	4.02	4.02	4.02	4.02	-0.22	1.4	0.00
45	120	2004	1273	537	0	1360	-92	4.02	4.02	4.02	4.02	-0.61	3.8	0.00
46	120	460	1162	300	0	677	115	4.02	4.02	4.02	4.02	-0.77	4.8	0.00
47	120	444	1163	262	0	592	114	4.02	4.02	4.02	4.02	-0.77	4.8	0.00
49	120	396	1155	304	0	692	130	4.02	4.02	4.02	4.02	-0.88	5.5	0.00
50	120	501	1171	242	0	542	97	4.02	4.02	4.02	4.02	-0.65	4.1	0.00
51	120	749	1186	298	0	704	72	4.02	4.02	4.02	4.02	-0.48	3.0	0.00
apost= --		aant= --		ainf= --		asup= --		(e arm. base= 4 X 2.01)						
40	180	376	724	575	0	970	725	4.02	4.02	4.02	4.02	-4.86	30.5	0.00
41	180	520	748	450	0	746	690	4.02	4.02	4.02	4.02	-4.63	29.0	0.00
42	180	1433	816	559	0	1014	606	4.02	4.02	4.02	4.02	-4.07	25.5	0.00
43	180	241	711	565	0	963	748	4.02	4.02	4.02	4.02	-5.02	31.4	0.00
44	180	765	789	257	0	400	630	4.02	4.02	4.02	4.02	-4.22	26.5	0.00
45	180	2004	864	537	0	1037	550	4.02	4.02	4.02	4.02	-3.69	23.1	0.00
46	180	460	753	300	0	497	689	4.02	4.02	4.02	4.02	-4.63	29.0	0.00
47	180	444	754	262	0	435	689	4.02	4.02	4.02	4.02	-4.62	29.0	0.00
49	180	396	746	304	0	510	701	4.02	4.02	4.02	4.02	-4.70	29.5	0.00
50	180	501	762	242	0	397	677	4.02	4.02	4.02	4.02	-4.54	28.5	0.00
51	180	749	777	298	0	525	661	4.02	4.02	4.02	4.02	-4.44	27.8	0.00
apost= --		aant= --		ainf= --		asup= --		(e arm. base= 4 X 2.01)						
40	240	376	314	575	0	625	1036	4.02	4.02	4.02	4.02	-6.95	43.6	0.00
41	240	520	338	450	0	476	1016	4.02	4.02	4.02	4.02	-6.81	42.7	0.00
42	240	1433	406	559	0	679	973	4.02	4.02	4.02	4.02	-6.53	40.9	0.00
43	240	241	301	565	0	624	1052	4.02	4.02	4.02	4.02	-7.06	44.2	0.00
44	240	765	379	257	0	246	980	4.02	4.02	4.02	4.02	-6.58	41.2	0.00
45	240	2004	454	537	0	715	945	4.02	4.02	4.02	4.02	-6.34	39.7	0.00
46	240	460	343	300	0	317	1018	4.02	4.02	4.02	4.02	-6.83	42.8	0.00
47	240	444	344	262	0	278	1019	4.02	4.02	4.02	4.02	-6.83	42.8	0.00
49	240	396	336	304	0	327	1025	4.02	4.02	4.02	4.02	-6.88	43.1	0.00
50	240	501	352	242	0	251	1011	4.02	4.02	4.02	4.02	-6.78	42.5	0.00
51	240	749	367	298	0	346	1004	4.02	4.02	4.02	4.02	-6.74	42.2	0.00
apost= --		aant= --		ainf= --		asup= --		(e arm. base= 4 X 2.01)						
40	300	376	-96	575	0	280	1102	4.02	4.02	4.02	4.02	-7.39	46.3	0.00
41	300	520	-72	450	0	206	1096	4.02	4.02	4.02	4.02	-7.35	46.0	0.00
42	300	1433	-4	559	0	344	1094	4.02	4.02	4.02	4.02	-7.34	46.0	0.00
43	300	241	-109	565	0	285	1110	4.02	4.02	4.02	4.02	-7.44	46.6	0.00
44	300	765	-31	257	0	91	1085	4.02	4.02	4.02	4.02	-7.28	45.6	0.00
45	300	2004	44	537	0	393	1095	4.02	4.02	4.02	4.02	-7.35	46.0	0.00
46	300	460	-67	300	0	137	1101	4.02	4.02	4.02	4.02	-7.39	46.3	0.00
47	300	444	-66	262	0	120	1102	4.02	4.02	4.02	4.02	-7.39	46.3	0.00
49	300	396	-74	304	0	145	1104	4.02	4.02	4.02	4.02	-7.41	46.4	0.00
50	300	501	-58	242	0	106	1099	4.02	4.02	4.02	4.02	-7.37	46.2	0.00
51	300	749	-43	298	0	167	1101	4.02	4.02	4.02	4.02	-7.39	46.3	0.00
apost= --		aant= --		ainf= --		asup= --		(e arm. base= 4 X 2.01)						
40	360	376	-506	575	0	-66	922	4.02	4.02	4.02	4.02	-6.19	38.7	0.00
41	360	520	-482	450	0	-64	930	4.02	4.02	4.02	4.02	-6.24	39.1	0.00
42	360	1433	-414	559	0	9	968	4.02	4.02	4.02	4.02	-6.50	40.7	0.00
43	360	241	-519	565	0	-54	921	4.02	4.02	4.02	4.02	-6.18	38.7	0.00
44	360	765	-441	257	0	-63	943	4.02	4.02	4.02	4.02	-6.33	39.6	0.00
45	360	2004	-366	537	0	71	999	4.02	4.02	4.02	4.02	-6.70	42.0	0.00
46	360	460	-477	300	0	-43	938	4.02	4.02	4.02	4.02	-6.29	39.4	0.00
47	360	444	-476	262	0	-37	940	4.02	4.02	4.02	4.02	-6.30	39.5	0.00
49	360	396	-484	304	0	-38	937	4.02	4.02	4.02	4.02	-6.29	39.4	0.00
50	360	501	-468	242	0	-40	941	4.02	4.02	4.02	4.02	-6.32	39.6	0.00
51	360	749	-453	298	0	-13	952	4.02	4.02	4.02	4.02	-6.39	40.0	0.00
apost= --		aant= --		ainf= --		asup= --		(e arm. base= 4 X 2.01)						
40	420	376	-916	575	0	-411	496	4.02	4.02	4.02	4.02	-3.33	20.8	0.00
41	420	520	-892	450	0	-334	518	4.02	4.02	4.02	4.02	-3.47	21.8	0.00

42	420	1433	-824	559	0	-326	597	4.02	4.02	4.02	4.02	-4.01	25.1	0.00
43	420	241	-929	565	0	-393	487	4.02	4.02	4.02	4.02	-3.27	20.5	0.00
44	420	765	-851	257	0	-217	556	4.02	4.02	4.02	4.02	-3.73	23.4	0.00
45	420	2004	-776	537	0	-251	657	4.02	4.02	4.02	4.02	-4.41	27.6	0.00
46	420	460	-887	300	0	-223	529	4.02	4.02	4.02	4.02	-3.55	22.2	0.00
47	420	444	-886	262	0	-194	531	4.02	4.02	4.02	4.02	-3.56	22.3	0.00
49	420	396	-894	304	0	-220	524	4.02	4.02	4.02	4.02	-3.51	22.0	0.00
50	420	501	-878	242	0	-185	537	4.02	4.02	4.02	4.02	-3.61	22.6	0.00
51	420	749	-863	298	0	-192	557	4.02	4.02	4.02	4.02	-3.74	23.4	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	480	376	-1325	575	0	-756	-176	4.02	4.02	4.02	4.02	-1.18	7.4	0.00
41	480	520	-1301	450	0	-605	-140	4.02	4.02	4.02	4.02	-0.94	5.9	0.00
42	480	1433	-1233	559	0	-662	-20	4.02	4.02	4.02	4.02	-0.13	0.8	0.00
43	480	241	-1338	565	0	-731	-193	4.02	4.02	4.02	4.02	-1.29	8.1	0.00
44	480	765	-1260	257	0	-372	-77	4.02	4.02	4.02	4.02	-0.52	3.2	0.00
45	480	2004	-1185	537	0	-574	69	4.02	4.02	4.02	4.02	-0.46	2.9	0.00
46	480	460	-1296	300	0	-402	-126	4.02	4.02	4.02	4.02	-0.84	5.3	0.00
47	480	444	-1295	262	0	-352	-123	4.02	4.02	4.02	4.02	-0.83	5.2	0.00
49	480	396	-1303	304	0	-402	-135	4.02	4.02	4.02	4.02	-0.91	5.7	0.00
50	480	501	-1287	242	0	-331	-112	4.02	4.02	4.02	4.02	-0.75	4.7	0.00
51	480	749	-1272	298	0	-371	-83	4.02	4.02	4.02	4.02	-0.56	3.5	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	540	376	-1735	575	0	-1102	-1094	4.02	4.02	4.02	4.02	-7.34	46.0	0.00
41	540	520	-1711	450	0	-875	-1044	4.02	4.02	4.02	4.02	-7.00	43.9	0.00
42	540	1433	-1643	559	0	-997	-882	4.02	4.02	4.02	4.02	-5.92	37.1	0.00
43	540	241	-1748	565	0	-1070	-1118	4.02	4.02	4.02	4.02	-7.50	47.0	0.00
44	540	765	-1670	257	0	-526	-956	4.02	4.02	4.02	4.02	-6.42	40.2	0.00
45	540	2004	-1595	537	0	-896	-765	4.02	4.02	4.02	4.02	-5.13	32.2	0.00
46	540	460	-1706	300	0	-582	-1026	4.02	4.02	4.02	4.02	-6.89	43.1	0.00
47	540	444	-1705	262	0	-509	-1023	4.02	4.02	4.02	4.02	-6.86	43.0	0.00
49	540	396	-1713	304	0	-585	-1040	4.02	4.02	4.02	4.02	-6.98	43.7	0.00
50	540	501	-1697	242	0	-476	-1008	4.02	4.02	4.02	4.02	-6.76	42.4	0.00
51	540	749	-1682	298	0	-550	-970	4.02	4.02	4.02	4.02	-6.51	40.8	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	600	376	-2145	575	0	-1447	-2258	4.02	4.02	4.02	4.02	-15.15	94.9	0.00
41	600	520	-2121	450	0	-1145	-2193	4.02	4.02	4.02	4.02	-14.72	92.2	0.00
42	600	1433	-2053	559	0	-1332	-1991	4.02	4.02	4.02	4.02	-13.36	83.7	0.00
43	600	241	-2158	565	0	-1409	-2290	4.02	4.02	4.02	4.02	-15.37	96.3	0.00
44	600	765	-2080	257	0	-680	-2081	4.02	4.02	4.02	4.02	-13.96	87.5	0.00
45	600	2004	-2005	537	0	-1218	-1845	4.02	4.02	4.02	4.02	-12.38	77.5	0.00
46	600	460	-2116	300	0	-762	-2173	4.02	4.02	4.02	4.02	-14.58	91.3	0.00
47	600	444	-2115	262	0	-667	-2169	4.02	4.02	4.02	4.02	-14.55	91.2	0.00
49	600	396	-2123	304	0	-767	-2191	4.02	4.02	4.02	4.02	-14.70	92.1	0.00
50	600	501	-2107	242	0	-622	-2149	4.02	4.02	4.02	4.02	-14.42	90.3	0.00
51	600	749	-2092	298	0	-729	-2102	4.02	4.02	4.02	4.02	-14.10	88.3	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

Nome travata: **trave_303_IP1** Descrizione: **Trave_3 32-26**
ASTA NUM. 13 NI 83 NF 84 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y Permanente qy tot.
qy medio: 375.00 308.00 683.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	[Fx]	[Fy]	[Fz]	[Mx]	[My]	Mz	[APOST]	[AANT]	AINF	ASUP	Sc	Sf	w
	--													--
	cm		daN			daN*m				cm^2			daN/cm^2	mm
40	0	444	2027	379	0	834	-1979	4.02	4.02	4.02	4.02	-13.28	83.2	0.00
41	0	516	2016	276	0	593	-1944	4.02	4.02	4.02	4.02	-13.04	81.7	0.00
42	0	1389	2110	287	0	613	-2229	4.02	4.02	4.02	4.02	-14.96	93.7	0.00
43	0	342	2044	393	0	875	-2031	4.02	4.02	4.02	4.02	-13.63	85.4	0.00
44	0	644	1997	113	0	214	-1886	4.02	4.02	4.02	4.02	-12.66	79.3	0.00
45	0	1917	2181	239	0	507	-2447	4.02	4.02	4.02	4.02	-16.42	102.8	0.00
46	0	430	2030	187	0	402	-1989	4.02	4.02	4.02	4.02	-13.35	83.6	0.00
47	0	408	2033	164	0	354	-2001	4.02	4.02	4.02	4.02	-13.43	84.1	0.00
49	0	384	2037	199	0	435	-2012	4.02	4.02	4.02	4.02	-13.50	84.6	0.00
50	0	444	2028	143	0	302	-1983	4.02	4.02	4.02	4.02	-13.31	83.3	0.00
51	0	699	2065	168	0	361	-2096	4.02	4.02	4.02	4.02	-14.06	88.1	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	60	444	1617	379	0	606	-886	4.02	4.02	4.02	4.02	-5.94	37.2	0.00
41	60	516	1606	276	0	428	-858	4.02	4.02	4.02	4.02	-5.75	36.0	0.00
42	60	1389	1700	287	0	441	-1086	4.02	4.02	4.02	4.02	-7.29	45.7	0.00
43	60	342	1634	393	0	639	-928	4.02	4.02	4.02	4.02	-6.22	39.0	0.00
44	60	644	1587	113	0	147	-811	4.02	4.02	4.02	4.02	-5.44	34.1	0.00
45	60	1917	1771	239	0	364	-1261	4.02	4.02	4.02	4.02	-8.46	53.0	0.00
46	60	430	1620	187	0	290	-894	4.02	4.02	4.02	4.02	-6.00	37.6	0.00
47	60	408	1623	164	0	256	-904	4.02	4.02	4.02	4.02	-6.07	38.0	0.00
49	60	384	1627	199	0	315	-913	4.02	4.02	4.02	4.02	-6.12	38.4	0.00
50	60	444	1618	143	0	217	-889	4.02	4.02	4.02	4.02	-5.97	37.4	0.00
51	60	699	1655	168	0	260	-980	4.02	4.02	4.02	4.02	-6.58	41.2	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	120	444	1207	379	0	378	-38	4.02	4.02	4.02	4.02	-0.26	1.6	0.00
41	120	516	1196	276	0	262	-17	4.02	4.02	4.02	4.02	-0.11	0.7	0.00
42	120	1389	1290	287	0	268	-189	4.02	4.02	4.02	4.02	-1.27	8.0	0.00
43	120	342	1224	393	0	403	-70	4.02	4.02	4.02	4.02	-0.47	2.9	0.00
44	120	644	1177	113	0	79	18	4.02	4.02	4.02	4.02	-0.12	0.8	0.00
45	120	1917	1361	239	0	220	-322	4.02	4.02	4.02	4.02	-2.16	13.5	0.00
46	120	430	1210	187	0	178	-45	4.02	4.02	4.02	4.02	-0.30	1.9	0.00
47	120	408	1213	164	0	157	-53	4.02	4.02	4.02	4.02	-0.35	2.2	0.00
49	120	384	1217	199	0	196	-59	4.02	4.02	4.02	4.02	-0.40	2.5	0.00
50	120	444	1208	143	0	131	-42	4.02	4.02	4.02	4.02	-0.28	1.7	0.00
51	120	699	1245	168	0	159	-110	4.02	4.02	4.02	4.02	-0.74	4.6	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	180	444	798	379	0	151	563	4.02	4.02	4.02	4.02	-3.78	23.7	0.00
41	180	516	787	276	0	97	578	4.02	4.02	4.02	4.02	-3.88	24.3	0.00
42	180	1389	881	287	0	96	462	4.02	4.02	4.02	4.02	-3.10	19.4	0.00
43	180	342	815	393	0	167	541	4.02	4.02	4.02	4.02	-3.63	22.8	0.00
44	180	644	768	113	0	12	602	4.02	4.02	4.02	4.02	-4.04	25.3	0.00
45	180	1917	952	239	0	76	372	4.02	4.02	4.02	4.02	-2.50	15.6	0.00
46	180	430	801	187	0	66	558	4.02	4.02	4.02	4.02	-3.75	23.5	0.00
47	180	408	804	164	0	59	553	4.02	4.02	4.02	4.02	-3.71	23.2	0.00
49	180	384	808	199	0	76	548	4.02	4.02	4.02	4.02	-3.68	23.1	0.00
50	180	444	799	143	0	45	560	4.02	4.02	4.02	4.02	-3.76	23.6	0.00
51	180	699	836	168	0	58	514	4.02	4.02	4.02	4.02	-3.45	21.6	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	240	444	388	379	0	-77	919	4.02	4.02	4.02	4.02	-6.17	38.6	0.00
41	240	516	377	276	0	-69	927	4.02	4.02	4.02	4.02	-6.22	38.9	0.00
42	240	1389	471	287	0	-76	867	4.02	4.02	4.02	4.02	-5.82	36.4	0.00
43	240	342	405	393	0	-68	907	4.02	4.02	4.02	4.02	-6.09	38.1	0.00
44	240	644	358	113	0	-56	939	4.02	4.02	4.02	4.02	-6.30	39.5	0.00
45	240	1917	542	239	0	-67	820	4.02	4.02	4.02	4.02	-5.50	34.5	0.00
46	240	430	391	187	0	-46	916	4.02	4.02	4.02	4.02	-6.14	38.5	0.00
47	240	408	394	164	0	-40	912	4.02	4.02	4.02	4.02	-6.12	38.3	0.00
49	240	384	398	199	0	-43	910	4.02	4.02	4.02	4.02	-6.11	38.3	0.00
50	240	444	389	143	0	-40	916	4.02	4.02	4.02	4.02	-6.15	38.5	0.00
51	240	699	426	168	0	-43	892	4.02	4.02	4.02	4.02	-5.99	37.5	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	300	444	-22	379	0	-305	1029	4.02	4.02	4.02	4.02	-6.90	43.2	0.00
41	300	516	-33	276	0	-234	1030	4.02	4.02	4.02	4.02	-6.91	43.3	0.00
42	300	1389	61	287	0	-249	1027	4.02	4.02	4.02	4.02	-6.89	43.1	0.00
43	300	342	-5	393	0	-304	1027	4.02	4.02	4.02	4.02	-6.89	43.2	0.00
44	300	644	-52	113	0	-124	1031	4.02	4.02	4.02	4.02	-6.91	43.3	0.00
45	300	1917	132	239	0	-211	1023	4.02	4.02	4.02	4.02	-6.86	43.0	0.00
46	300	430	-19	187	0	-158	1027	4.02	4.02	4.02	4.02	-6.89	43.2	0.00
47	300	408	-16	164	0	-139	1026	4.02	4.02	4.02	4.02	-6.88	43.1	0.00
49	300	384	-12	199	0	-162	1026	4.02	4.02	4.02	4.02	-6.88	43.1	0.00
50	300	444	-21	143	0	-126	1027	4.02	4.02	4.02	4.02	-6.89	43.1	0.00
51	300	699	16	168	0	-144	1025	4.02	4.02	4.02	4.02	-6.87	43.1	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	360	444	-432	379	0	-532	893	4.02	4.02	4.02	4.02	-5.99	37.5	0.00
41	360	516	-443	276	0	-399	887	4.02	4.02	4.02	4.02	-5.95	37.3	0.00
42	360	1389	-349	287	0	-421	940	4.02	4.02	4.02	4.02	-6.31	39.5	0.00
43	360	342	-415	393	0	-540	901	4.02	4.02	4.02	4.02	-6.05	37.9	0.00
44	360	644	-462	113	0	-191	876	4.02	4.02	4.02	4.02	-5.88	36.8	0.00
45	360	1917	-278	239	0	-355	979	4.02	4.02	4.02	4.02	-6.57	41.1	0.00
46	360	430	-429	187	0	-270	893	4.02	4.02	4.02	4.02	-5.99	37.5	0.00
47	360	408	-426	164	0	-237	893	4.02	4.02	4.02	4.02	-5.99	37.5	0.00
49	360	384	-422	199	0	-282	896	4.02	4.02	4.02	4.02	-6.01	37.7	0.00
50	360	444	-431	143	0	-212	891	4.02	4.02	4.02	4.02	-5.98	37.4	0.00
51	360	699	-394	168	0	-245	911	4.02	4.02	4.02	4.02	-6.11	38.3	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	420	444	-842	379	0	-760	511	4.02	4.02	4.02	4.02	-3.43	21.5	0.00
41	420	516	-853	276	0	-565	498	4.02	4.02	4.02	4.02	-3.34	20.9	0.00
42	420	1389	-759	287	0	-594	608	4.02	4.02	4.02	4.02	-4.08	25.5	0.00
43	420	342	-825	393	0	-776	529	4.02	4.02	4.02	4.02	-3.55	22.2	0.00
44	420	644	-872	113	0	-259	476	4.02	4.02	4.02	4.02	-3.19	20.0	0.00
45	420	1917	-688	239	0	-498	689	4.02	4.02	4.02	4.02	-4.62	29.0	0.00
46	420	430	-839	187	0	-382	512	4.02	4.02	4.02	4.02	-3.44	21.5	0.00
47	420	408	-836	164	0	-336	515	4.02	4.02	4.02	4.02	-3.46	21.6	0.00
49	420	384	-832	199	0	-401	520	4.02	4.02	4.02	4.02	-3.49	21.9	0.00
50	420	444	-841	143	0	-298	509	4.02	4.02	4.02	4.02	-3.42	21.4	0.00
51	420	699	-804	168	0	-346	552	4.02	4.02	4.02	4.02	-3.70	23.2	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	480	444	-1251	379	0	-988	-117	4.02	4.02	4.02	4.02	-0.78	4.9	0.00
41	480	516	-1262	276	0	-730	-137	4.02	4.02	4.02	4.02	-0.92	5.8	0.00
42	480	1389	-1168	287	0	-766	29	4.02	4.02	4.02	4.02	-0.20	1.2	0.00
43	480	342	-1234	393	0	-1011	-89	4.02	4.02	4.02	4.02	-0.60	3.7	0.00
44	480	644	-1281	113	0	-327	-170	4.02	4.02	4.02	4.02	-1.14	7.2	0.00
45	480	1917	-1097	239	0	-642	154	4.02	4.02	4.02	4.02	-1.03	6.5	0.00
46	480	430	-1248	187	0	-494	-114	4.02	4.02	4.02	4.02	-0.76	4.8	0.00
47	480	408	-1245	164	0	-435	-109	4.02	4.02	4.02	4.02	-0.73	4.6	0.00
49	480	384	-1241	199	0	-520	-102	4.02	4.02	4.02	4.02	-0.68	4.3	0.00
50	480	444	-1250	143	0	-383	-118	4.02	4.02	4.02	4.02	-0.79	5.0	0.00
51	480	699	-1213	168	0	-447	-54	4.02	4.02	4.02	4.02	-0.36	2.3	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	540	444	-1661	379	0	-1215	-990	4.02	4.02	4.02	4.02	-6.65	41.6	0.00
41	540	516	-1672	276	0	-896	-1018	4.02	4.02	4.02	4.02	-6.83	42.8	0.00
42	540	1389	-1578	287	0	-939	-795	4.02	4.02	4.02	4.02	-5.33	33.4	0.00
43	540	342	-1644	393	0	-1247	-952	4.02	4.02	4.02	4.02	-6.39	40.0	0.00
44	540	644	-1691	113	0	-394	-1062	4.02	4.02	4.02	4.02	-7.13	44.6	0.00
45	540	1917	-1507	239	0	-786	-628	4.02	4.02	4.02	4.02	-4.21	26.4	0.00
46	540	430	-1658	187	0	-606	-986	4.02	4.02	4.02	4.02	-6.62	41.4	0.00
47	540	408	-1655	164	0	-533	-979	4.02	4.02	4.02	4.02	-6.57	41.2	0.00
49	540	384	-1651	199	0	-640	-969	4.02	4.02	4.02	4.02	-6.50	40.7	0.00
50	540	444	-1660	143	0	-469	-992	4.02	4.02	4.02	4.02	-6.65	41.7	0.00
51	540	699	-1623	168	0	-547	-905	4.02	4.02	4.02	4.02	-6.07	38.0	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	600	444	-2071	379	0	-1443	-2110	4.02	4.02	4.02	4.02	-14.16	88.7	0.00
41	600	516	-2082	276	0	-1061	-2144	4.02	4.02	4.02	4.02	-14.39	90.1	0.00
42	600	1389	-1988	287	0	-1111	-1865	4.02	4.02	4.02	4.02	-12.51	78.4	0.00
43	600	342	-2054	393	0	-1483	-2062	4.02	4.02	4.02	4.02	-13.84	86.7	0.00
44	600	644	-2101	113	0	-462	-2200	4.02	4.02	4.02	4.02	-14.76	92.5	0.00
45	600	1917	-1917	239	0	-929	-1655	4.02	4.02	4.02	4.02	-11.11	69.6	0.00
46	600	430	-2068	187	0	-718	-2104	4.02	4.02	4.02	4.02	-14.12	88.4	0.00
47	600	408	-2065	164	0	-632	-2095	4.02	4.02	4.02	4.02	-14.06	88.1	0.00
49	600	384	-2061	199	0	-759	-2083	4.02	4.02	4.02	4.02	-13.98	87.6	0.00
50	600	444	-2070	143	0	-555	-2111	4.02	4.02	4.02	4.02	-14.16	88.7	0.00
51	600	699	-2033	168	0	-648	-2002	4.02	4.02	4.02	4.02	-13.43	84.1	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

Nome travata: **trave_303_IP1** Descrizione: **Trave_3 32-26**
ASTA NUM. 14 NI 84 NF 85 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y Permanente qy tot.
qy medio: 375.00 308.00 683.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	[Fx]	[Fy]	[Fz]	[Mx]	[My]	Mz	[APOST]	[AANT]	AINF	ASUP	Sc	Sf	w
	cm	daN			daN*m			cm^2				daN/cm^2		mm
40	0	334	1906	2	0	-382	-1595	4.02	4.02	4.02	4.02	-10.70	67.0	0.00
41	0	389	1920	6	0	-270	-1643	4.02	4.02	4.02	4.02	-11.02	69.1	0.00
42	0	1220	2005	6	0	-267	-1900	4.02	4.02	4.02	4.02	-12.75	79.9	0.00
43	0	264	1923	-3	0	-402	-1646	4.02	4.02	4.02	4.02	-11.04	69.2	0.00
44	0	484	1940	14	0	-93	-1714	4.02	4.02	4.02	4.02	-11.50	72.0	0.00
45	0	1741	2089	5	0	-211	-2154	4.02	4.02	4.02	4.02	-14.45	90.5	0.00
46	0	336	1962	4	0	-184	-1776	4.02	4.02	4.02	4.02	-11.92	74.6	0.00
47	0	322	1973	3	0	-162	-1809	4.02	4.02	4.02	4.02	-12.14	76.0	0.00
49	0	304	1968	2	0	-200	-1793	4.02	4.02	4.02	4.02	-12.03	75.4	0.00
50	0	348	1971	5	0	-138	-1806	4.02	4.02	4.02	4.02	-12.12	75.9	0.00
51	0	599	2001	3	0	-161	-1894	4.02	4.02	4.02	4.02	-12.71	79.6	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	60	334	1496	2	0	-383	-575	4.02	4.02	4.02	4.02	-3.86	24.1	0.00
41	60	389	1510	6	0	-273	-614	4.02	4.02	4.02	4.02	-4.12	25.8	0.00
42	60	1220	1595	6	0	-271	-820	4.02	4.02	4.02	4.02	-5.50	34.5	0.00
43	60	264	1513	-3	0	-401	-615	4.02	4.02	4.02	4.02	-4.13	25.9	0.00
44	60	484	1530	14	0	-101	-673	4.02	4.02	4.02	4.02	-4.52	28.3	0.00
45	60	1741	1679	5	0	-214	-1024	4.02	4.02	4.02	4.02	-6.87	43.0	0.00
46	60	336	1552	4	0	-186	-722	4.02	4.02	4.02	4.02	-4.84	30.3	0.00
47	60	322	1563	3	0	-164	-748	4.02	4.02	4.02	4.02	-5.02	31.4	0.00
49	60	304	1558	2	0	-201	-735	4.02	4.02	4.02	4.02	-4.93	30.9	0.00
50	60	348	1561	5	0	-141	-746	4.02	4.02	4.02	4.02	-5.01	31.4	0.00
51	60	599	1591	3	0	-163	-816	4.02	4.02	4.02	4.02	-5.48	34.3	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	120	334	1086	2	0	-383	200	4.02	4.02	4.02	4.02	-1.34	8.4	0.00
41	120	389	1100	6	0	-277	169	4.02	4.02	4.02	4.02	-1.13	7.1	0.00
42	120	1220	1185	6	0	-274	14	4.02	4.02	4.02	4.02	-0.10	0.6	0.00
43	120	264	1103	-3	0	-399	170	4.02	4.02	4.02	4.02	-1.14	7.1	0.00
44	120	484	1120	14	0	-109	122	4.02	4.02	4.02	4.02	-0.82	5.1	0.00
45	120	1741	1269	5	0	-217	-139	4.02	4.02	4.02	4.02	-0.93	5.8	0.00
46	120	336	1142	4	0	-188	87	4.02	4.02	4.02	4.02	-0.58	3.6	0.00
47	120	322	1153	3	0	-166	67	4.02	4.02	4.02	4.02	-0.45	2.8	0.00
49	120	304	1148	2	0	-202	77	4.02	4.02	4.02	4.02	-0.52	3.2	0.00
50	120	348	1151	5	0	-144	68	4.02	4.02	4.02	4.02	-0.46	2.9	0.00
51	120	599	1181	3	0	-165	16	4.02	4.02	4.02	4.02	-0.10	0.7	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	180	334	677	2	0	-384	729	4.02	4.02	4.02	4.02	-4.89	30.6	0.00
41	180	389	691	6	0	-281	706	4.02	4.02	4.02	4.02	-4.73	29.7	0.00
42	180	1220	776	6	0	-278	603	4.02	4.02	4.02	4.02	-4.05	25.3	0.00
43	180	264	694	-3	0	-397	709	4.02	4.02	4.02	4.02	-4.76	29.8	0.00
44	180	484	711	14	0	-118	671	4.02	4.02	4.02	4.02	-4.50	28.2	0.00
45	180	1741	860	5	0	-220	499	4.02	4.02	4.02	4.02	-3.35	21.0	0.00
46	180	336	733	4	0	-191	649	4.02	4.02	4.02	4.02	-4.36	27.3	0.00
47	180	322	744	3	0	-168	636	4.02	4.02	4.02	4.02	-4.27	26.7	0.00
49	180	304	739	2	0	-203	643	4.02	4.02	4.02	4.02	-4.32	27.0	0.00
50	180	348	742	5	0	-147	636	4.02	4.02	4.02	4.02	-4.27	26.7	0.00
51	180	599	772	3	0	-167	602	4.02	4.02	4.02	4.02	-4.04	25.3	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	240	334	267	2	0	-385	1012	4.02	4.02	4.02	4.02	-6.79	42.5	0.00
41	240	389	281	6	0	-285	997	4.02	4.02	4.02	4.02	-6.69	41.9	0.00
42	240	1220	366	6	0	-282	945	4.02	4.02	4.02	4.02	-6.34	39.7	0.00
43	240	264	284	-3	0	-395	1002	4.02	4.02	4.02	4.02	-6.72	42.1	0.00
44	240	484	301	14	0	-126	975	4.02	4.02	4.02	4.02	-6.54	41.0	0.00
45	240	1741	450	5	0	-222	892	4.02	4.02	4.02	4.02	-5.99	37.5	0.00
46	240	336	323	4	0	-193	966	4.02	4.02	4.02	4.02	-6.48	40.6	0.00
47	240	322	334	3	0	-170	959	4.02	4.02	4.02	4.02	-6.43	40.3	0.00
49	240	304	329	2	0	-204	964	4.02	4.02	4.02	4.02	-6.47	40.5	0.00
50	240	348	332	5	0	-150	959	4.02	4.02	4.02	4.02	-6.43	40.3	0.00
51	240	599	362	3	0	-169	942	4.02	4.02	4.02	4.02	-6.32	39.6	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	300	334	-143	2	0	-386	1049	4.02	4.02	4.02	4.02	-7.04	44.1	0.00
41	300	389	-129	6	0	-288	1042	4.02	4.02	4.02	4.02	-6.99	43.8	0.00
42	300	1220	-44	6	0	-285	1042	4.02	4.02	4.02	4.02	-6.99	43.8	0.00
43	300	264	-126	-3	0	-394	1050	4.02	4.02	4.02	4.02	-7.04	44.1	0.00
44	300	484	-109	14	0	-135	1032	4.02	4.02	4.02	4.02	-6.92	43.4	0.00
45	300	1741	40	5	0	-225	1039	4.02	4.02	4.02	4.02	-6.97	43.7	0.00
46	300	336	-87	4	0	-196	1037	4.02	4.02	4.02	4.02	-6.96	43.6	0.00
47	300	322	-76	3	0	-172	1036	4.02	4.02	4.02	4.02	-6.95	43.5	0.00
49	300	304	-81	2	0	-205	1038	4.02	4.02	4.02	4.02	-6.96	43.6	0.00
50	300	348	-78	5	0	-153	1035	4.02	4.02	4.02	4.02	-6.94	43.5	0.00
51	300	599	-48	3	0	-171	1036	4.02	4.02	4.02	4.02	-6.95	43.5	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	360	334	-553	2	0	-387	840	4.02	4.02	4.02	4.02	-5.63	35.3	0.00
41	360	389	-539	6	0	-292	841	4.02	4.02	4.02	4.02	-5.65	35.4	0.00
42	360	1220	-454	6	0	-289	893	4.02	4.02	4.02	4.02	-5.99	37.5	0.00
43	360	264	-536	-3	0	-392	851	4.02	4.02	4.02	4.02	-5.71	35.8	0.00
44	360	484	-519	14	0	-143	844	4.02	4.02	4.02	4.02	-5.66	35.5	0.00
45	360	1741	-370	5	0	-228	940	4.02	4.02	4.02	4.02	-6.31	39.5	0.00
46	360	336	-497	4	0	-198	862	4.02	4.02	4.02	4.02	-5.78	36.2	0.00
47	360	322	-486	3	0	-175	867	4.02	4.02	4.02	4.02	-5.82	36.5	0.00
49	360	304	-491	2	0	-206	867	4.02	4.02	4.02	4.02	-5.81	36.4	0.00
50	360	348	-488	5	0	-157	866	4.02	4.02	4.02	4.02	-5.81	36.4	0.00

51	360	599	-458	3	0	-173	884	4.02	4.02	4.02	4.02	-5.93	37.2	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	420	334	-963	2	0	-388	385	4.02	4.02	4.02	4.02	-2.58	16.2	0.00
41	420	389	-949	6	0	-296	395	4.02	4.02	4.02	4.02	-2.65	16.6	0.00
42	420	1220	-864	6	0	-292	498	4.02	4.02	4.02	4.02	-3.34	20.9	0.00
43	420	264	-946	-3	0	-390	407	4.02	4.02	4.02	4.02	-2.73	17.1	0.00
44	420	484	-929	14	0	-152	409	4.02	4.02	4.02	4.02	-2.75	17.2	0.00
45	420	1741	-780	5	0	-231	595	4.02	4.02	4.02	4.02	-3.99	25.0	0.00
46	420	336	-907	4	0	-200	441	4.02	4.02	4.02	4.02	-2.96	18.5	0.00
47	420	322	-896	3	0	-177	453	4.02	4.02	4.02	4.02	-3.04	19.0	0.00
49	420	304	-901	2	0	-207	449	4.02	4.02	4.02	4.02	-3.01	18.9	0.00
50	420	348	-898	5	0	-160	450	4.02	4.02	4.02	4.02	-3.02	18.9	0.00
51	420	599	-868	3	0	-176	487	4.02	4.02	4.02	4.02	-3.27	20.5	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	480	334	-1372	2	0	-389	-316	4.02	4.02	4.02	4.02	-2.12	13.3	0.00
41	480	389	-1358	6	0	-299	-298	4.02	4.02	4.02	4.02	-2.00	12.5	0.00
42	480	1220	-1273	6	0	-296	-143	4.02	4.02	4.02	4.02	-0.96	6.0	0.00
43	480	264	-1355	-3	0	-388	-284	4.02	4.02	4.02	4.02	-1.90	11.9	0.00
44	480	484	-1338	14	0	-160	-271	4.02	4.02	4.02	4.02	-1.82	11.4	0.00
45	480	1741	-1189	5	0	-233	4	4.02	4.02	4.02	4.02	-0.03	0.2	0.00
46	480	336	-1316	4	0	-203	-226	4.02	4.02	4.02	4.02	-1.51	9.5	0.00
47	480	322	-1305	3	0	-179	-208	4.02	4.02	4.02	4.02	-1.39	8.7	0.00
49	480	304	-1310	2	0	-209	-214	4.02	4.02	4.02	4.02	-1.44	9.0	0.00
50	480	348	-1307	5	0	-163	-211	4.02	4.02	4.02	4.02	-1.42	8.9	0.00
51	480	599	-1277	3	0	-178	-157	4.02	4.02	4.02	4.02	-1.05	6.6	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	540	334	-1782	2	0	-390	-1263	4.02	4.02	4.02	4.02	-8.47	53.1	0.00
41	540	389	-1768	6	0	-303	-1236	4.02	4.02	4.02	4.02	-8.29	51.9	0.00
42	540	1220	-1683	6	0	-300	-1030	4.02	4.02	4.02	4.02	-6.91	43.3	0.00
43	540	264	-1765	-3	0	-387	-1220	4.02	4.02	4.02	4.02	-8.19	51.3	0.00
44	540	484	-1748	14	0	-169	-1197	4.02	4.02	4.02	4.02	-8.03	50.3	0.00
45	540	1741	-1599	5	0	-236	-832	4.02	4.02	4.02	4.02	-5.59	35.0	0.00
46	540	336	-1726	4	0	-205	-1138	4.02	4.02	4.02	4.02	-7.64	47.8	0.00
47	540	322	-1715	3	0	-181	-1114	4.02	4.02	4.02	4.02	-7.47	46.8	0.00
49	540	304	-1720	2	0	-210	-1123	4.02	4.02	4.02	4.02	-7.54	47.2	0.00
50	540	348	-1717	5	0	-166	-1118	4.02	4.02	4.02	4.02	-7.50	47.0	0.00
51	540	599	-1687	3	0	-180	-1046	4.02	4.02	4.02	4.02	-7.02	44.0	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	600	334	-2192	2	0	-391	-2455	4.02	4.02	4.02	4.02	-16.47	103.2	0.00
41	600	389	-2178	6	0	-307	-2420	4.02	4.02	4.02	4.02	-16.24	101.7	0.00
42	600	1220	-2093	6	0	-303	-2163	4.02	4.02	4.02	4.02	-14.51	90.9	0.00
43	600	264	-2175	-3	0	-385	-2402	4.02	4.02	4.02	4.02	-16.12	101.0	0.00
44	600	484	-2158	14	0	-177	-2369	4.02	4.02	4.02	4.02	-15.90	99.6	0.00
45	600	1741	-2009	5	0	-239	-1915	4.02	4.02	4.02	4.02	-12.85	80.5	0.00
46	600	336	-2136	4	0	-208	-2297	4.02	4.02	4.02	4.02	-15.41	96.5	0.00
47	600	322	-2125	3	0	-183	-2266	4.02	4.02	4.02	4.02	-15.20	95.2	0.00
49	600	304	-2130	2	0	-211	-2278	4.02	4.02	4.02	4.02	-15.29	95.7	0.00
50	600	348	-2127	5	0	-169	-2271	4.02	4.02	4.02	4.02	-15.24	95.5	0.00
51	600	599	-2097	3	0	-182	-2181	4.02	4.02	4.02	4.02	-14.63	91.7	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

Nome travata: **trave_303_IP1** Descrizione: **Trave_3 32-26**
ASTA NUM. 15 NI 85 NF 86 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y Permanente qy tot.
qy medio: 375.00 308.00 683.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	[Fx]	[Fy]	[Fz]	[Mx]	[My]	Mz	[APOST]	[AANT]	AINF	ASUP	Sc	Sf	w
	--													--
	cm		daN			daN*m				cm^2			daN/cm^2	mm
40	0	88	1854	-38	0	-451	-1458	4.02	4.02	4.02	4.02	-9.78	61.3	0.00
41	0	152	1873	-35	0	-362	-1519	4.02	4.02	4.02	4.02	-10.19	63.8	0.00
42	0	982	1962	-22	0	-312	-1783	4.02	4.02	4.02	4.02	-11.96	74.9	0.00
43	0	62	1877	-34	0	-437	-1525	4.02	4.02	4.02	4.02	-10.23	64.1	0.00
44	0	253	1901	-31	0	-226	-1606	4.02	4.02	4.02	4.02	-10.78	67.5	0.00
45	0	1551	2055	-5	0	-206	-2066	4.02	4.02	4.02	4.02	-13.86	86.8	0.00
46	0	177	1930	-24	0	-246	-1690	4.02	4.02	4.02	4.02	-11.34	71.0	0.00
47	0	183	1944	-21	0	-216	-1733	4.02	4.02	4.02	4.02	-11.63	72.8	0.00
49	0	162	1937	-22	0	-246	-1713	4.02	4.02	4.02	4.02	-11.49	72.0	0.00
50	0	200	1942	-22	0	-204	-1729	4.02	4.02	4.02	4.02	-11.60	72.7	0.00
51	0	460	1973	-17	0	-200	-1821	4.02	4.02	4.02	4.02	-12.22	76.5	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	60	88	1444	-38	0	-428	-468	4.02	4.02	4.02	4.02	-3.14	19.7	0.00
41	60	152	1463	-35	0	-341	-518	4.02	4.02	4.02	4.02	-3.47	21.8	0.00
42	60	982	1552	-22	0	-299	-729	4.02	4.02	4.02	4.02	-4.89	30.6	0.00
43	60	62	1467	-34	0	-417	-522	4.02	4.02	4.02	4.02	-3.50	21.9	0.00
44	60	253	1491	-31	0	-208	-588	4.02	4.02	4.02	4.02	-3.95	24.7	0.00
45	60	1551	1645	-5	0	-203	-956	4.02	4.02	4.02	4.02	-6.41	40.2	0.00
46	60	177	1520	-24	0	-231	-655	4.02	4.02	4.02	4.02	-4.40	27.5	0.00
47	60	183	1534	-21	0	-204	-690	4.02	4.02	4.02	4.02	-4.63	29.0	0.00
49	60	162	1527	-22	0	-233	-674	4.02	4.02	4.02	4.02	-4.52	28.3	0.00
50	60	200	1532	-22	0	-191	-687	4.02	4.02	4.02	4.02	-4.61	28.9	0.00
51	60	460	1563	-17	0	-190	-760	4.02	4.02	4.02	4.02	-5.10	31.9	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	120	88	1034	-38	0	-405	275	4.02	4.02	4.02	4.02	-1.85	11.6	0.00
41	120	152	1053	-35	0	-320	237	4.02	4.02	4.02	4.02	-1.59	10.0	0.00
42	120	982	1142	-22	0	-286	79	4.02	4.02	4.02	4.02	-0.53	3.3	0.00
43	120	62	1057	-34	0	-397	235	4.02	4.02	4.02	4.02	-1.58	9.9	0.00
44	120	253	1081	-31	0	-189	183	4.02	4.02	4.02	4.02	-1.23	7.7	0.00
45	120	1551	1235	-5	0	-200	-91	4.02	4.02	4.02	4.02	-0.61	3.8	0.00
46	120	177	1110	-24	0	-217	134	4.02	4.02	4.02	4.02	-0.90	5.6	0.00
47	120	183	1124	-21	0	-191	108	4.02	4.02	4.02	4.02	-0.72	4.5	0.00

49	120	162	1117	-22	0	-219	120	4.02	4.02	4.02	4.02	-0.80	5.0	0.00
50	120	200	1122	-22	0	-178	110	4.02	4.02	4.02	4.02	-0.74	4.6	0.00
51	120	460	1153	-17	0	-180	55	4.02	4.02	4.02	4.02	-0.37	2.3	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	180	88	625	-38	0	-381	773	4.02	4.02	4.02	4.02	-5.19	32.5	0.00
41	180	152	644	-35	0	-299	747	4.02	4.02	4.02	4.02	-5.01	31.4	0.00
42	180	982	733	-22	0	-274	642	4.02	4.02	4.02	4.02	-4.30	27.0	0.00
43	180	62	648	-34	0	-377	747	4.02	4.02	4.02	4.02	-5.01	31.4	0.00
44	180	253	672	-31	0	-170	709	4.02	4.02	4.02	4.02	-4.76	29.8	0.00
45	180	1551	826	-5	0	-197	527	4.02	4.02	4.02	4.02	-3.54	22.2	0.00
46	180	177	701	-24	0	-202	677	4.02	4.02	4.02	4.02	-4.54	28.4	0.00
47	180	183	715	-21	0	-178	659	4.02	4.02	4.02	4.02	-4.42	27.7	0.00
49	180	162	708	-22	0	-206	667	4.02	4.02	4.02	4.02	-4.48	28.1	0.00
50	180	200	713	-22	0	-165	660	4.02	4.02	4.02	4.02	-4.43	27.7	0.00
51	180	460	744	-17	0	-170	624	4.02	4.02	4.02	4.02	-4.19	26.2	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	240	88	215	-38	0	-358	1025	4.02	4.02	4.02	4.02	-6.88	43.1	0.00
41	240	152	234	-35	0	-277	1010	4.02	4.02	4.02	4.02	-6.78	42.5	0.00
42	240	982	323	-22	0	-261	958	4.02	4.02	4.02	4.02	-6.43	40.3	0.00
43	240	62	238	-34	0	-356	1012	4.02	4.02	4.02	4.02	-6.79	42.5	0.00
44	240	253	262	-31	0	-152	989	4.02	4.02	4.02	4.02	-6.64	41.6	0.00
45	240	1551	416	-5	0	-193	900	4.02	4.02	4.02	4.02	-6.04	37.8	0.00
46	240	177	291	-24	0	-188	974	4.02	4.02	4.02	4.02	-6.53	40.9	0.00
47	240	183	305	-21	0	-165	965	4.02	4.02	4.02	4.02	-6.47	40.5	0.00
49	240	162	298	-22	0	-193	969	4.02	4.02	4.02	4.02	-6.50	40.7	0.00
50	240	200	303	-22	0	-152	965	4.02	4.02	4.02	4.02	-6.47	40.5	0.00
51	240	460	334	-17	0	-160	947	4.02	4.02	4.02	4.02	-6.36	39.8	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	300	88	-195	-38	0	-335	1032	4.02	4.02	4.02	4.02	-6.92	43.4	0.00
41	300	152	-176	-35	0	-256	1028	4.02	4.02	4.02	4.02	-6.90	43.2	0.00
42	300	982	-87	-22	0	-248	1029	4.02	4.02	4.02	4.02	-6.90	43.2	0.00
43	300	62	-172	-34	0	-336	1032	4.02	4.02	4.02	4.02	-6.92	43.4	0.00
44	300	253	-148	-31	0	-133	1024	4.02	4.02	4.02	4.02	-6.87	43.0	0.00
45	300	1551	6	-5	0	-190	1027	4.02	4.02	4.02	4.02	-6.89	43.1	0.00
46	300	177	-119	-24	0	-173	1025	4.02	4.02	4.02	4.02	-6.88	43.1	0.00
47	300	183	-105	-21	0	-153	1025	4.02	4.02	4.02	4.02	-6.87	43.1	0.00
49	300	162	-112	-22	0	-179	1025	4.02	4.02	4.02	4.02	-6.88	43.1	0.00
50	300	200	-107	-22	0	-139	1024	4.02	4.02	4.02	4.02	-6.87	43.0	0.00
51	300	460	-76	-17	0	-150	1025	4.02	4.02	4.02	4.02	-6.87	43.1	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	360	88	-605	-38	0	-312	792	4.02	4.02	4.02	4.02	-5.31	33.3	0.00
41	360	152	-586	-35	0	-235	800	4.02	4.02	4.02	4.02	-5.37	33.6	0.00
42	360	982	-497	-22	0	-235	853	4.02	4.02	4.02	4.02	-5.72	35.9	0.00
43	360	62	-582	-34	0	-316	805	4.02	4.02	4.02	4.02	-5.40	33.8	0.00
44	360	253	-558	-31	0	-115	812	4.02	4.02	4.02	4.02	-5.45	34.1	0.00
45	360	1551	-404	-5	0	-187	907	4.02	4.02	4.02	4.02	-6.09	38.1	0.00
46	360	177	-529	-24	0	-159	830	4.02	4.02	4.02	4.02	-5.57	34.9	0.00
47	360	183	-515	-21	0	-140	838	4.02	4.02	4.02	4.02	-5.63	35.2	0.00
49	360	162	-522	-22	0	-166	835	4.02	4.02	4.02	4.02	-5.60	35.1	0.00
50	360	200	-517	-22	0	-125	836	4.02	4.02	4.02	4.02	-5.61	35.2	0.00
51	360	460	-486	-17	0	-140	856	4.02	4.02	4.02	4.02	-5.74	36.0	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	420	88	-1015	-38	0	-289	306	4.02	4.02	4.02	4.02	-2.05	12.9	0.00
41	420	152	-996	-35	0	-214	326	4.02	4.02	4.02	4.02	-2.19	13.7	0.00
42	420	982	-907	-22	0	-222	432	4.02	4.02	4.02	4.02	-2.90	18.2	0.00
43	420	62	-992	-34	0	-296	333	4.02	4.02	4.02	4.02	-2.23	14.0	0.00
44	420	253	-968	-31	0	-96	354	4.02	4.02	4.02	4.02	-2.38	14.9	0.00
45	420	1551	-814	-5	0	-184	542	4.02	4.02	4.02	4.02	-3.64	22.8	0.00
46	420	177	-939	-24	0	-145	390	4.02	4.02	4.02	4.02	-2.62	16.4	0.00
47	420	183	-925	-21	0	-127	406	4.02	4.02	4.02	4.02	-2.73	17.1	0.00
49	420	162	-932	-22	0	-152	399	4.02	4.02	4.02	4.02	-2.68	16.8	0.00
50	420	200	-927	-22	0	-112	403	4.02	4.02	4.02	4.02	-2.71	17.0	0.00
51	420	460	-896	-17	0	-130	442	4.02	4.02	4.02	4.02	-2.96	18.6	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	480	88	-1424	-38	0	-266	-425	4.02	4.02	4.02	4.02	-2.85	17.9	0.00
41	480	152	-1405	-35	0	-193	-394	4.02	4.02	4.02	4.02	-2.65	16.6	0.00
42	480	982	-1316	-22	0	-209	-235	4.02	4.02	4.02	4.02	-1.58	9.9	0.00
43	480	62	-1401	-34	0	-276	-385	4.02	4.02	4.02	4.02	-2.58	16.2	0.00
44	480	253	-1377	-31	0	-77	-349	4.02	4.02	4.02	4.02	-2.34	14.7	0.00
45	480	1551	-1223	-5	0	-180	-69	4.02	4.02	4.02	4.02	-0.46	2.9	0.00
46	480	177	-1348	-24	0	-130	-297	4.02	4.02	4.02	4.02	-1.99	12.5	0.00
47	480	183	-1334	-21	0	-115	-272	4.02	4.02	4.02	4.02	-1.82	11.4	0.00
49	480	162	-1341	-22	0	-139	-283	4.02	4.02	4.02	4.02	-1.90	11.9	0.00
50	480	200	-1336	-22	0	-99	-276	4.02	4.02	4.02	4.02	-1.85	11.6	0.00
51	480	460	-1305	-17	0	-120	-219	4.02	4.02	4.02	4.02	-1.47	9.2	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	540	88	-1834	-38	0	-243	-1403	4.02	4.02	4.02	4.02	-9.41	59.0	0.00
41	540	152	-1815	-35	0	-172	-1360	4.02	4.02	4.02	4.02	-9.13	57.2	0.00
42	540	982	-1726	-22	0	-196	-1148	4.02	4.02	4.02	4.02	-7.70	48.3	0.00
43	540	62	-1811	-34	0	-255	-1349	4.02	4.02	4.02	4.02	-9.05	56.7	0.00
44	540	253	-1787	-31	0	-59	-1299	4.02	4.02	4.02	4.02	-8.71	54.6	0.00
45	540	1551	-1633	-5	0	-177	-925	4.02	4.02	4.02	4.02	-6.21	38.9	0.00
46	540	177	-1758	-24	0	-116	-1229	4.02	4.02	4.02	4.02	-8.25	51.6	0.00
47	540	183	-1744	-21	0	-102	-1195	4.02	4.02	4.02	4.02	-8.02	50.2	0.00
49	540	162	-1751	-22	0	-126	-1210	4.02	4.02	4.02	4.02	-8.12	50.9	0.00
50	540	200	-1746	-22	0	-86	-1200	4.02	4.02	4.02	4.02	-8.05	50.5	0.00
51	540	460	-1715	-17	0	-110	-1125	4.02	4.02	4.02	4.02	-7.55	47.3	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	600	88	-2244	-38	0	-220	-2626	4.02	4.02	4.02	4.02	-17.62	110.4	0.00
41	600	152	-2225	-35	0	-150	-2572	4.02	4.02	4.02	4.02	-17.26	108.1	0.00
42	600	982	-2136	-22	0	-183	-2307	4.02	4.02	4.02	4.02	-15.48	97.0	0.00
43	600	62	-2221	-34	0	-235	-2559	4.02	4.02	4.02	4.02	-17.17	107.6	0.00
44	600	253	-2197	-31	0	-40	-2494	4.02	4.02	4.02	4.02	-16.73	104.8	0.00
45	600	1551	-2043	-5	0	-174	-2028	4.02	4.02	4.02	4.02	-13.61	85.2	0.00

46	600	177	-2168	-24	0	-101	-2407	4.02	4.02	4.02	4.02	-16.15	101.2	0.00
47	600	183	-2154	-21	0	-89	-2365	4.02	4.02	4.02	4.02	-15.87	99.4	0.00
49	600	162	-2161	-22	0	-112	-2384	4.02	4.02	4.02	4.02	-16.00	100.2	0.00
50	600	200	-2156	-22	0	-73	-2371	4.02	4.02	4.02	4.02	-15.91	99.7	0.00
51	600	460	-2125	-17	0	-100	-2277	4.02	4.02	4.02	4.02	-15.28	95.7	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

Nome travata: **trave_303_IP1** Descrizione: **Trave_3 32-26**
ASTA NUM. 16 NI 86 NF 99 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y Permanente qy tot.
qy medio: 375.00 308.00 683.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	[Fx]	[Fy]	[Fz]	[Mx]	[My]	Mz	[APOST]	[AANT]	AINF	ASUP	Sc	Sf	w
	cm	daN			daN*m			cm^2				daN/cm^2		mm
40	0	-186	1905	-199	0	-1143	-1497	4.02	4.02	4.02	4.02	-10.04	62.9	0.00
41	0	-125	1918	-161	0	-883	-1547	4.02	4.02	4.02	4.02	-10.38	65.0	0.00
42	0	746	2002	-144	0	-844	-1803	4.02	4.02	4.02	4.02	-12.10	75.8	0.00
43	0	-152	1938	-191	0	-1136	-1596	4.02	4.02	4.02	4.02	-10.71	67.1	0.00
44	0	-36	1934	-103	0	-480	-1609	4.02	4.02	4.02	4.02	-10.80	67.6	0.00
45	0	1402	2100	-100	0	-638	-2107	4.02	4.02	4.02	4.02	-14.14	88.6	0.00
46	0	-5	1986	-107	0	-592	-1759	4.02	4.02	4.02	4.02	-11.80	73.9	0.00
47	0	25	2003	-94	0	-520	-1812	4.02	4.02	4.02	4.02	-12.16	76.2	0.00
49	0	5	1998	-107	0	-607	-1795	4.02	4.02	4.02	4.02	-12.04	75.4	0.00
50	0	28	1997	-89	0	-476	-1798	4.02	4.02	4.02	4.02	-12.06	75.6	0.00
51	0	315	2031	-88	0	-507	-1897	4.02	4.02	4.02	4.02	-12.73	79.7	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	60	-186	1495	-199	0	-1024	-477	4.02	4.02	4.02	4.02	-3.20	20.0	0.00
41	60	-125	1508	-161	0	-786	-519	4.02	4.02	4.02	4.02	-3.48	21.8	0.00
42	60	746	1592	-144	0	-758	-725	4.02	4.02	4.02	4.02	-4.86	30.5	0.00
43	60	-152	1528	-191	0	-1022	-556	4.02	4.02	4.02	4.02	-3.73	23.4	0.00
44	60	-36	1524	-103	0	-418	-571	4.02	4.02	4.02	4.02	-3.83	24.0	0.00
45	60	1402	1690	-100	0	-578	-970	4.02	4.02	4.02	4.02	-6.51	40.8	0.00
46	60	-5	1576	-107	0	-528	-690	4.02	4.02	4.02	4.02	-4.63	29.0	0.00
47	60	25	1593	-94	0	-463	-733	4.02	4.02	4.02	4.02	-4.92	30.8	0.00
49	60	5	1588	-107	0	-543	-719	4.02	4.02	4.02	4.02	-4.82	30.2	0.00
50	60	28	1587	-89	0	-422	-722	4.02	4.02	4.02	4.02	-4.85	30.4	0.00
51	60	315	1621	-88	0	-454	-802	4.02	4.02	4.02	4.02	-5.38	33.7	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	120	-186	1085	-199	0	-905	297	4.02	4.02	4.02	4.02	-2.00	12.5	0.00
41	120	-125	1098	-161	0	-690	263	4.02	4.02	4.02	4.02	-1.77	11.1	0.00
42	120	746	1182	-144	0	-672	108	4.02	4.02	4.02	4.02	-0.72	4.5	0.00
43	120	-152	1118	-191	0	-907	238	4.02	4.02	4.02	4.02	-1.60	10.0	0.00
44	120	-36	1114	-103	0	-356	220	4.02	4.02	4.02	4.02	-1.48	9.3	0.00
45	120	1402	1280	-100	0	-518	-79	4.02	4.02	4.02	4.02	-0.53	3.3	0.00
46	120	-5	1166	-107	0	-464	132	4.02	4.02	4.02	4.02	-0.89	5.6	0.00
47	120	25	1183	-94	0	-407	100	4.02	4.02	4.02	4.02	-0.67	4.2	0.00
49	120	5	1178	-107	0	-479	111	4.02	4.02	4.02	4.02	-0.75	4.7	0.00
50	120	28	1177	-89	0	-368	107	4.02	4.02	4.02	4.02	-0.72	4.5	0.00
51	120	315	1211	-88	0	-401	48	4.02	4.02	4.02	4.02	-0.32	2.0	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	180	-186	676	-199	0	-785	826	4.02	4.02	4.02	4.02	-5.54	34.7	0.00
41	180	-125	689	-161	0	-594	800	4.02	4.02	4.02	4.02	-5.37	33.6	0.00
42	180	746	773	-144	0	-585	694	4.02	4.02	4.02	4.02	-4.66	29.2	0.00
43	180	-152	709	-191	0	-793	787	4.02	4.02	4.02	4.02	-5.28	33.1	0.00
44	180	-36	705	-103	0	-294	766	4.02	4.02	4.02	4.02	-5.14	32.2	0.00
45	180	1402	871	-100	0	-458	566	4.02	4.02	4.02	4.02	-3.80	23.8	0.00
46	180	-5	757	-107	0	-399	709	4.02	4.02	4.02	4.02	-4.76	29.8	0.00
47	180	25	774	-94	0	-351	687	4.02	4.02	4.02	4.02	-4.61	28.9	0.00
49	180	5	769	-107	0	-415	696	4.02	4.02	4.02	4.02	-4.67	29.2	0.00
50	180	28	768	-89	0	-315	691	4.02	4.02	4.02	4.02	-4.64	29.0	0.00
51	180	315	802	-88	0	-348	651	4.02	4.02	4.02	4.02	-4.37	27.4	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	240	-186	266	-199	0	-666	1108	4.02	4.02	4.02	4.02	-7.44	46.6	0.00
41	240	-125	279	-161	0	-497	1090	4.02	4.02	4.02	4.02	-7.32	45.8	0.00
42	240	746	363	-144	0	-499	1035	4.02	4.02	4.02	4.02	-6.94	43.5	0.00
43	240	-152	299	-191	0	-678	1089	4.02	4.02	4.02	4.02	-7.31	45.8	0.00
44	240	-36	295	-103	0	-232	1066	4.02	4.02	4.02	4.02	-7.15	44.8	0.00
45	240	1402	461	-100	0	-399	966	4.02	4.02	4.02	4.02	-6.48	40.6	0.00
46	240	-5	347	-107	0	-335	1040	4.02	4.02	4.02	4.02	-6.98	43.7	0.00
47	240	25	364	-94	0	-294	1028	4.02	4.02	4.02	4.02	-6.90	43.2	0.00
49	240	5	359	-107	0	-351	1034	4.02	4.02	4.02	4.02	-6.94	43.5	0.00
50	240	28	358	-89	0	-261	1029	4.02	4.02	4.02	4.02	-6.90	43.2	0.00
51	240	315	392	-88	0	-295	1009	4.02	4.02	4.02	4.02	-6.77	42.4	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	300	-186	-144	-199	0	-547	1145	4.02	4.02	4.02	4.02	-7.68	48.1	0.00
41	300	-125	-131	-161	0	-401	1135	4.02	4.02	4.02	4.02	-7.62	47.7	0.00
42	300	746	-47	-144	0	-412	1130	4.02	4.02	4.02	4.02	-7.58	47.5	0.00
43	300	-152	-111	-191	0	-564	1146	4.02	4.02	4.02	4.02	-7.69	48.1	0.00
44	300	-36	-115	-103	0	-169	1120	4.02	4.02	4.02	4.02	-7.52	47.1	0.00
45	300	1402	51	-100	0	-339	1119	4.02	4.02	4.02	4.02	-7.51	47.0	0.00
46	300	-5	-63	-107	0	-270	1126	4.02	4.02	4.02	4.02	-7.55	47.3	0.00
47	300	25	-46	-94	0	-238	1123	4.02	4.02	4.02	4.02	-7.54	47.2	0.00
49	300	5	-51	-107	0	-287	1127	4.02	4.02	4.02	4.02	-7.56	47.3	0.00
50	300	28	-52	-89	0	-208	1121	4.02	4.02	4.02	4.02	-7.52	47.1	0.00
51	300	315	-18	-88	0	-242	1121	4.02	4.02	4.02	4.02	-7.52	47.1	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	360	-186	-554	-199	0	-428	936	4.02	4.02	4.02	4.02	-6.28	39.3	0.00
41	360	-125	-541	-161	0	-304	934	4.02	4.02	4.02	4.02	-6.27	39.2	0.00
42	360	746	-457	-144	0	-326	978	4.02	4.02	4.02	4.02	-6.56	41.1	0.00
43	360	-152	-521	-191	0	-449	956	4.02	4.02	4.02	4.02	-6.42	40.2	0.00

44	360	-36	-525	-103	0	-107	928	4.02	4.02	4.02	4.02	-6.23	39.0	0.00
45	360	1402	-359	-100	0	-279	1027	4.02	4.02	4.02	4.02	-6.89	43.1	0.00
46	360	-5	-473	-107	0	-206	965	4.02	4.02	4.02	4.02	-6.47	40.5	0.00
47	360	25	-456	-94	0	-181	972	4.02	4.02	4.02	4.02	-6.52	40.9	0.00
49	360	5	-461	-107	0	-223	973	4.02	4.02	4.02	4.02	-6.53	40.9	0.00
50	360	28	-462	-89	0	-154	967	4.02	4.02	4.02	4.02	-6.49	40.7	0.00
51	360	315	-428	-88	0	-189	987	4.02	4.02	4.02	4.02	-6.62	41.5	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	420	-186	-964	-199	0	-309	481	4.02	4.02	4.02	4.02	-3.23	20.2	0.00
41	420	-125	-951	-161	0	-208	487	4.02	4.02	4.02	4.02	-3.27	20.5	0.00
42	420	746	-867	-144	0	-240	581	4.02	4.02	4.02	4.02	-3.90	24.4	0.00
43	420	-152	-931	-191	0	-335	521	4.02	4.02	4.02	4.02	-3.50	21.9	0.00
44	420	-36	-935	-103	0	-45	490	4.02	4.02	4.02	4.02	-3.29	20.6	0.00
45	420	1402	-769	-100	0	-219	688	4.02	4.02	4.02	4.02	-4.62	28.9	0.00
46	420	-5	-883	-107	0	-142	558	4.02	4.02	4.02	4.02	-3.75	23.5	0.00
47	420	25	-866	-94	0	-125	576	4.02	4.02	4.02	4.02	-3.86	24.2	0.00
49	420	5	-871	-107	0	-159	574	4.02	4.02	4.02	4.02	-3.85	24.1	0.00
50	420	28	-872	-89	0	-101	567	4.02	4.02	4.02	4.02	-3.81	23.9	0.00
51	420	315	-838	-88	0	-136	607	4.02	4.02	4.02	4.02	-4.07	25.5	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	480	-186	-1373	-199	0	-190	-220	4.02	4.02	4.02	4.02	-1.48	9.3	0.00
41	480	-125	-1360	-161	0	-112	-206	4.02	4.02	4.02	4.02	-1.38	8.7	0.00
42	480	746	-1276	-144	0	-153	-62	4.02	4.02	4.02	4.02	-0.41	2.6	0.00
43	480	-152	-1340	-191	0	-220	-160	4.02	4.02	4.02	4.02	-1.07	6.7	0.00
44	480	-36	-1344	-103	0	17	-193	4.02	4.02	4.02	4.02	-1.30	8.1	0.00
45	480	1402	-1178	-100	0	-160	104	4.02	4.02	4.02	4.02	-0.70	4.4	0.00
46	480	-5	-1292	-107	0	-77	-94	4.02	4.02	4.02	4.02	-0.63	4.0	0.00
47	480	25	-1275	-94	0	-69	-67	4.02	4.02	4.02	4.02	-0.45	2.8	0.00
49	480	5	-1280	-107	0	-95	-71	4.02	4.02	4.02	4.02	-0.48	3.0	0.00
50	480	28	-1281	-89	0	-47	-78	4.02	4.02	4.02	4.02	-0.52	3.3	0.00
51	480	315	-1247	-88	0	-83	-19	4.02	4.02	4.02	4.02	-0.13	0.8	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	540	-186	-1783	-199	0	-70	-1167	4.02	4.02	4.02	4.02	-7.83	49.1	0.00
41	540	-125	-1770	-161	0	-15	-1145	4.02	4.02	4.02	4.02	-7.68	48.1	0.00
42	540	746	-1686	-144	0	-67	-950	4.02	4.02	4.02	4.02	-6.38	39.9	0.00
43	540	-152	-1750	-191	0	-106	-1087	4.02	4.02	4.02	4.02	-7.29	45.7	0.00
44	540	-36	-1754	-103	0	79	-1123	4.02	4.02	4.02	4.02	-7.53	47.2	0.00
45	540	1402	-1588	-100	0	-100	-726	4.02	4.02	4.02	4.02	-4.87	30.5	0.00
46	540	-5	-1702	-107	0	-13	-993	4.02	4.02	4.02	4.02	-6.66	41.7	0.00
47	540	25	-1685	-94	0	-12	-955	4.02	4.02	4.02	4.02	-6.41	40.1	0.00
49	540	5	-1690	-107	0	-31	-962	4.02	4.02	4.02	4.02	-6.46	40.4	0.00
50	540	28	-1691	-89	0	6	-970	4.02	4.02	4.02	4.02	-6.51	40.8	0.00
51	540	315	-1657	-88	0	-30	-890	4.02	4.02	4.02	4.02	-5.97	37.4	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	600	-186	-2193	-199	0	49	-2360	4.02	10.05	4.02	4.02	-15.84	99.2	0.00
41	600	-125	-2180	-161	0	81	-2330	4.02	10.05	4.02	4.02	-15.63	97.9	0.00
42	600	746	-2096	-144	0	19	-2085	4.02	10.05	4.02	4.02	-13.99	87.6	0.00
43	600	-152	-2160	-191	0	9	-2260	4.02	10.05	4.02	4.02	-15.16	95.0	0.00
44	600	-36	-2164	-103	0	141	-2298	4.02	10.05	4.02	4.02	-15.42	96.6	0.00
45	600	1402	-1998	-100	0	-40	-1802	4.02	10.05	4.02	4.02	-12.09	75.7	0.00
46	600	-5	-2112	-107	0	51	-2137	4.02	10.05	4.02	4.02	-14.34	89.8	0.00
47	600	25	-2095	-94	0	44	-2089	4.02	10.05	4.02	4.02	-14.02	87.8	0.00
49	600	5	-2100	-107	0	33	-2099	4.02	10.05	4.02	4.02	-14.08	88.2	0.00
50	600	28	-2101	-89	0	60	-2107	4.02	10.05	4.02	4.02	-14.14	88.6	0.00
51	600	315	-2067	-88	0	24	-2008	4.02	10.05	4.02	4.02	-13.47	84.4	0.00

apost= -- aant= 6.03 ainf= -- asup= -- (e arm. base= 4 X 2.01)

Nome travata: **trave_303_IP1** Descrizione: **Trave_3 32-26**
ASTA NUM. 17 NI 99 NF 208 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y Permanente qy tot.
qy medio: 375.00 308.00 683.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	[Fx]	[Fy]	[Fz]	[Mx]	[My]	Mz	[APOST]	[AANT]	AINF	ASUP	Sc	Sf	w
	cm	daN			daN*m			cm^2				daN/cm^2		mm
40	0	-1298	-18	-4043	0	-5327	949	4.02	10.05	4.02	4.02	-6.37	39.9	0.00
41	0	-1120	113	-2929	0	-3867	746	4.02	10.05	4.02	4.02	-5.01	31.4	0.00
42	0	-182	341	-2986	0	-3940	397	4.02	10.05	4.02	4.02	-2.66	16.7	0.00
43	0	-1115	106	-4193	0	-5517	738	4.02	10.05	4.02	4.02	-4.95	31.0	0.00
44	0	-871	300	-1168	0	-1559	467	4.02	10.05	4.02	4.02	-3.13	19.6	0.00
45	0	744	705	-2432	0	-3206	-183	4.02	10.05	4.02	4.02	-1.23	7.7	0.00
46	0	-637	452	-1982	0	-2615	191	4.02	10.05	4.02	4.02	-1.28	8.0	0.00
47	0	-516	536	-1745	0	-2302	52	4.02	10.05	4.02	4.02	-0.35	2.2	0.00
49	0	-576	492	-2116	0	-2789	120	4.02	10.05	4.02	4.02	-0.80	5.0	0.00
50	0	-527	531	-1511	0	-1997	66	4.02	10.05	4.02	4.02	-0.44	2.8	0.00
51	0	-204	612	-1764	0	-2326	-64	4.02	10.05	4.02	4.02	-0.43	2.7	0.00

apost= -- aant= 6.03 ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	29	-1298	-216	-4043	0	-4155	915	4.02	8.04	4.02	4.02	-6.14	38.5	0.00
41	29	-1120	-85	-2929	0	-3018	750	4.02	8.04	4.02	4.02	-5.03	31.5	0.00
42	29	-182	143	-2986	0	-3074	467	4.02	8.04	4.02	4.02	-3.13	19.6	0.00
43	29	-1115	-92	-4193	0	-4301	740	4.02	8.04	4.02	4.02	-4.96	31.1	0.00
44	29	-871	101	-1168	0	-1220	525	4.02	8.04	4.02	4.02	-3.53	22.1	0.00
45	29	744	507	-2432	0	-2501	-7	4.02	8.04	4.02	4.02	-0.05	0.3	0.00
46	29	-637	253	-1982	0	-2040	293	4.02	8.04	4.02	4.02	-1.97	12.3	0.00
47	29	-516	338	-1745	0	-1796	179	4.02	8.04	4.02	4.02	-1.20	7.5	0.00
49	29	-576	294	-2116	0	-2175	234	4.02	8.04	4.02	4.02	-1.57	9.8	0.00
50	29	-527	333	-1511	0	-1559	191	4.02	8.04	4.02	4.02	-1.28	8.0	0.00
51	29	-204	414	-1764	0	-1815	85	4.02	8.04	4.02	4.02	-0.57	3.6	0.00

apost= -- aant= 4.02 ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	58	-1298	-414	-4043	0	-2982	824	4.02	6.03	4.02	4.02	-5.53	34.6	0.00
41	58	-1120	-283	-2929	0	-2168	697	4.02	6.03	4.02	4.02	-4.67	29.3	0.00

42	58	-182	-55	-2986	0	-2208	480	4.02	6.03	4.02	4.02	-3.22	20.2	0.00
43	58	-1115	-290	-4193	0	-3085	684	4.02	6.03	4.02	4.02	-4.59	28.8	0.00
44	58	-871	-97	-1168	0	-882	526	4.02	6.03	4.02	4.02	-3.53	22.1	0.00
45	58	744	309	-2432	0	-1795	111	4.02	6.03	4.02	4.02	-0.74	4.7	0.00
46	58	-637	55	-1982	0	-1466	338	4.02	6.03	4.02	4.02	-2.27	14.2	0.00
47	58	-516	140	-1745	0	-1290	248	4.02	6.03	4.02	4.02	-1.67	10.4	0.00
49	58	-576	96	-2116	0	-1562	291	4.02	6.03	4.02	4.02	-1.95	12.2	0.00
50	58	-527	135	-1511	0	-1121	259	4.02	6.03	4.02	4.02	-1.74	10.9	0.00
51	58	-204	216	-1764	0	-1303	176	4.02	6.03	4.02	4.02	-1.18	7.4	0.00

apost= -- aant= 2.01 ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	87	-1298	-612	-4043	0	-1810	675	4.02	4.02	4.02	4.02	-4.53	28.4	0.00
41	87	-1120	-481	-2929	0	-1319	586	4.02	4.02	4.02	4.02	-3.93	24.6	0.00
42	87	-182	-253	-2986	0	-1342	435	4.02	4.02	4.02	4.02	-2.92	18.3	0.00
43	87	-1115	-488	-4193	0	-1869	572	4.02	4.02	4.02	4.02	-3.84	24.0	0.00
44	87	-871	-295	-1168	0	-543	469	4.02	4.02	4.02	4.02	-3.15	19.7	0.00
45	87	744	111	-2432	0	-1090	172	4.02	4.02	4.02	4.02	-1.15	7.2	0.00
46	87	-637	-143	-1982	0	-891	325	4.02	4.02	4.02	4.02	-2.18	13.7	0.00
47	87	-516	-58	-1745	0	-784	260	4.02	4.02	4.02	4.02	-1.75	10.9	0.00
49	87	-576	-102	-2116	0	-948	290	4.02	4.02	4.02	4.02	-1.94	12.2	0.00
50	87	-527	-63	-1511	0	-683	269	4.02	4.02	4.02	4.02	-1.81	11.3	0.00
51	87	-204	18	-1764	0	-792	210	4.02	4.02	4.02	4.02	-1.41	8.8	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	116	-1298	-810	-4043	0	-637	469	4.02	4.02	4.02	4.02	-3.15	19.7	0.00
41	116	-1120	-679	-2929	0	-469	417	4.02	4.02	4.02	4.02	-2.80	17.5	0.00
42	116	-182	-451	-2986	0	-476	333	4.02	4.02	4.02	4.02	-2.23	14.0	0.00
43	116	-1115	-686	-4193	0	-653	401	4.02	4.02	4.02	4.02	-2.69	16.9	0.00
44	116	-871	-493	-1168	0	-205	355	4.02	4.02	4.02	4.02	-2.38	14.9	0.00
45	116	744	-87	-2432	0	-385	175	4.02	4.02	4.02	4.02	-1.18	7.4	0.00
46	116	-637	-341	-1982	0	-317	255	4.02	4.02	4.02	4.02	-1.71	10.7	0.00
47	116	-516	-256	-1745	0	-278	215	4.02	4.02	4.02	4.02	-1.44	9.0	0.00
49	116	-576	-300	-2116	0	-334	232	4.02	4.02	4.02	4.02	-1.55	9.7	0.00
50	116	-527	-261	-1511	0	-245	222	4.02	4.02	4.02	4.02	-1.49	9.3	0.00
51	116	-204	-180	-1764	0	-280	186	4.02	4.02	4.02	4.02	-1.25	7.8	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	145	-1298	-1008	-4043	0	535	205	4.02	4.02	4.02	4.02	-1.38	8.6	0.00
41	145	-1120	-878	-2929	0	380	192	4.02	4.02	4.02	4.02	-1.28	8.0	0.00
42	145	-182	-649	-2986	0	390	173	4.02	4.02	4.02	4.02	-1.16	7.3	0.00
43	145	-1115	-884	-4193	0	563	174	4.02	4.02	4.02	4.02	-1.17	7.3	0.00
44	145	-871	-691	-1168	0	134	184	4.02	4.02	4.02	4.02	-1.23	7.7	0.00
45	145	744	-285	-2432	0	320	121	4.02	4.02	4.02	4.02	-0.81	5.1	0.00
46	145	-637	-539	-1982	0	258	128	4.02	4.02	4.02	4.02	-0.86	5.4	0.00
47	145	-516	-454	-1745	0	228	112	4.02	4.02	4.02	4.02	-0.75	4.7	0.00
49	145	-576	-498	-2116	0	280	116	4.02	4.02	4.02	4.02	-0.78	4.9	0.00
50	145	-527	-459	-1511	0	194	118	4.02	4.02	4.02	4.02	-0.79	5.0	0.00
51	145	-204	-378	-1764	0	231	105	4.02	4.02	4.02	4.02	-0.71	4.4	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	174	-1298	-1207	-4043	0	1707	-116	4.02	4.02	4.02	4.02	-0.78	4.9	0.00
41	174	-1120	-1076	-2929	0	1229	-92	4.02	4.02	4.02	4.02	-0.62	3.9	0.00
42	174	-182	-847	-2986	0	1256	-44	4.02	4.02	4.02	4.02	-0.29	1.8	0.00
43	174	-1115	-1082	-4193	0	1779	-111	4.02	4.02	4.02	4.02	-0.75	4.7	0.00
44	174	-871	-889	-1168	0	473	-45	4.02	4.02	4.02	4.02	-0.30	1.9	0.00
45	174	744	-483	-2432	0	1026	10	4.02	4.02	4.02	4.02	-0.07	0.4	0.00
46	174	-637	-737	-1982	0	833	-58	4.02	4.02	4.02	4.02	-0.39	2.4	0.00
47	174	-516	-653	-1745	0	734	-49	4.02	4.02	4.02	4.02	-0.33	2.1	0.00
49	174	-576	-696	-2116	0	893	-57	4.02	4.02	4.02	4.02	-0.38	2.4	0.00
50	174	-527	-658	-1511	0	632	-44	4.02	4.02	4.02	4.02	-0.30	1.8	0.00
51	174	-204	-576	-1764	0	742	-33	4.02	4.02	4.02	4.02	-0.22	1.4	0.00

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	203	-1298	-1405	-4043	0	2880	-495	6.03	4.02	4.02	4.02	-3.32	20.8	0.00
41	203	-1120	-1274	-2929	0	2079	-432	6.03	4.02	4.02	4.02	-2.90	18.2	0.00
42	203	-182	-1045	-2986	0	2122	-318	6.03	4.02	4.02	4.02	-2.13	13.4	0.00
43	203	-1115	-1280	-4193	0	2995	-454	6.03	4.02	4.02	4.02	-3.04	19.1	0.00
44	203	-871	-1087	-1168	0	811	-332	6.03	4.02	4.02	4.02	-2.23	14.0	0.00
45	203	744	-681	-2432	0	1731	-159	6.03	4.02	4.02	4.02	-1.07	6.7	0.00
46	203	-637	-935	-1982	0	1407	-300	6.03	4.02	4.02	4.02	-2.01	12.6	0.00
47	203	-516	-851	-1745	0	1240	-267	6.03	4.02	4.02	4.02	-1.79	11.2	0.00
49	203	-576	-894	-2116	0	1507	-288	6.03	4.02	4.02	4.02	-1.93	12.1	0.00
50	203	-527	-856	-1511	0	1070	-263	6.03	4.02	4.02	4.02	-1.77	11.1	0.00
51	203	-204	-774	-1764	0	1254	-229	6.03	4.02	4.02	4.02	-1.54	9.6	0.00

apost= 2.01 aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	232	-1298	-1603	-4043	0	4052	-931	8.04	4.02	4.02	4.02	-6.24	39.1	0.00
41	232	-1120	-1472	-2929	0	2928	-830	8.04	4.02	4.02	4.02	-5.57	34.9	0.00
42	232	-182	-1243	-2986	0	2988	-650	8.04	4.02	4.02	4.02	-4.36	27.3	0.00
43	232	-1115	-1478	-4193	0	4211	-854	8.04	4.02	4.02	4.02	-5.73	35.9	0.00
44	232	-871	-1285	-1168	0	1150	-676	8.04	4.02	4.02	4.02	-4.53	28.4	0.00
45	232	744	-879	-2432	0	2436	-385	8.04	4.02	4.02	4.02	-2.58	16.2	0.00
46	232	-637	-1133	-1982	0	1982	-600	8.04	4.02	4.02	4.02	-4.03	25.2	0.00
47	232	-516	-1049	-1745	0	1746	-542	8.04	4.02	4.02	4.02	-3.64	22.8	0.00
49	232	-576	-1092	-2116	0	2121	-576	8.04	4.02	4.02	4.02	-3.86	24.2	0.00
50	232	-527	-1054	-1511	0	1508	-540	8.04	4.02	4.02	4.02	-3.62	22.7	0.00
51	232	-204	-972	-1764	0	1765	-482	8.04	4.02	4.02	4.02	-3.24	20.3	0.00

apost= 4.02 aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	261	-1298	-1801	-4043	0	5225	-1424	10.05	4.02	4.02	4.02	-9.56	59.9	0.00
41	261	-1120	-1670	-2929	0	3778	-1286	10.05	4.02	4.02	4.02	-8.63	54.1	0.00
42	261	-182	-1441	-2986	0	3854	-1039	10.05	4.02	4.02	4.02	-6.97	43.7	0.00
43	261	-1115	-1676	-4193	0	5427	-1311	10.05	4.02	4.02	4.02	-8.80	55.1	0.00
44	261	-871	-1483	-1168	0	1488	-1077	10.05	4.02	4.02	4.02	-7.23	45.3	0.00
45	261	744	-1077	-2432	0	3142	-669	10.05	4.02	4.02	4.02	-4.49	28.1	0.00
46	261	-637	-1331	-1982	0	2556	-957	10.05	4.02	4.02	4.02	-6.42	40.2	0.00
47	261	-516	-1247	-1745	0	2252	-875	10.05	4.02	4.02	4.02	-5.87	36.8	0.00
49	261	-576	-1290	-2116	0	2734	-921	10.05	4.02	4.02	4.02	-6.18	38.7	0.00
50	261	-527	-1252	-1511	0	1946	-874	10.05	4.02	4.02	4.02	-5.87	36.7	0.00
51	261	-204	-1170	-1764	0	2277	-793	10.05	4.02	4.02	4.02	-5.32	33.3	0.00

apost= 6.03 aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

40	290	-1298	-1999	-4043	0	6397	-1975	12.06	4.02	4.02	4.02	-13.25	83.0	0.00
41	290	-1120	-1868	-2929	0	4627	-1799	12.06	4.02	4.02	4.02	-12.07	75.6	0.00
42	290	-182	-1639	-2986	0	4720	-1486	12.06	4.02	4.02	4.02	-9.97	62.5	0.00
43	290	-1115	-1874	-4193	0	6643	-1826	12.06	4.02	4.02	4.02	-12.25	76.7	0.00
44	290	-871	-1681	-1168	0	1827	-1536	12.06	4.02	4.02	4.02	-10.31	64.6	0.00
45	290	744	-1275	-2432	0	3847	-1010	12.06	4.02	4.02	4.02	-6.78	42.5	0.00
46	290	-637	-1529	-1982	0	3131	-1372	12.06	4.02	4.02	4.02	-9.21	57.7	0.00
47	290	-516	-1445	-1745	0	2758	-1265	12.06	4.02	4.02	4.02	-8.49	53.2	0.00
49	290	-576	-1488	-2116	0	3348	-1324	12.06	4.02	4.02	4.02	-8.88	55.6	0.00
50	290	-527	-1450	-1511	0	2384	-1266	12.06	4.02	4.02	4.02	-8.49	53.2	0.00
51	290	-204	-1368	-1764	0	2788	-1161	12.06	4.02	4.02	4.02	-7.79	48.8	0.00

apost= 8.04 aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01)

L E G E N D A

Prima asta	Ultima asta	Nome disegno	Descrizione disegno
1	4	trave_301_IP1.ARM	Trave_3 7-12-17-22-32
5	5	trave_304_IP1.ARM	Trave_3 1-10
6	11	trave_302_IP1.ARM	Trave_3 7-6-5-4-3-2-1
12	17	trave_303_IP1.ARM	Trave_3 32-26

Delta Ingegneria srl
via Artemide 3 92100 Agrigento - tel 0922 402212
email - g.ferraro@deltaingegneria.it

Lavoro: **D2403a** Intestazione lavoro: **Palestra Campobello**
Elemento: **TRAVE** Gruppo: **5** Tabella: **Tabella travi**
Descrizione: **Travi copertura spogliatoi**
Rck: **350.00** daN/cm^2 fyk: **4580.0** daN/cm^2
Copriferro superiore: **5.0** cm Copriferro inferiore: **5.0** cm Copriferro laterale: **5.0** cm
Verifica in ottemperanza alle NTC2018
Per le combinazioni sismiche la capacità è valutata in campo elastico o sostanzialmente elastico(§7.4.1 NTC2018)

Diametro staffe: **8** mm Numero braccia: **2**

Nome travata: **trave_501_IP1** Descrizione: **Trave_5 11-16-21-26**
ASTA NUM. 1 NI 169 NF 171 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y qy tot.
qy medio: 375.00 375.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	634	955	65	0	171	577	4.02	4.02	4.02	4.02	3	0.08	0.03	0.17	0.00	0.00	22.3
2	0	613	571	8	0	13	850	4.02	4.02	4.02	4.02	2	0.13	0.02	0.10	0.00	0.00	22.3
3	0	620	569	8	0	16	854	4.02	4.02	4.02	4.02	2	0.13	0.02	0.10	0.00	0.00	22.3
4	0	355	900	92	0	247	-421	4.02	4.02	4.02	4.02	2	0.07	0.03	0.16	0.00	0.00	22.3
5	0	362	898	93	0	249	-417	4.02	4.02	4.02	4.02	2	0.07	0.03	0.16	0.00	0.00	22.3
6	0	515	687	36	0	93	561	4.02	4.02	4.02	4.02	2	0.09	0.02	0.12	0.00	0.00	22.3
7	0	538	683	39	0	100	572	4.02	4.02	4.02	4.02	2	0.09	0.02	0.12	0.00	0.00	22.3
8	0	437	786	62	0	163	-82	4.02	4.02	4.02	4.02	2	0.05	0.02	0.14	0.00	0.00	22.3
9	0	461	782	64	0	170	-69	4.02	4.02	4.02	4.02	2	0.05	0.02	0.14	0.00	0.00	22.3
10	0	613	571	8	0	13	850	4.02	4.02	4.02	4.02	2	0.13	0.02	0.10	0.00	0.00	22.3
11	0	620	569	8	0	16	854	4.02	4.02	4.02	4.02	2	0.13	0.02	0.10	0.00	0.00	22.3
12	0	355	900	92	0	247	-421	4.02	4.02	4.02	4.02	2	0.07	0.03	0.16	0.00	0.00	22.3
13	0	362	898	93	0	249	-417	4.02	4.02	4.02	4.02	2	0.07	0.03	0.16	0.00	0.00	22.3
14	0	515	687	36	0	93	561	4.02	4.02	4.02	4.02	2	0.09	0.02	0.12	0.00	0.00	22.3
15	0	538	683	39	0	100	572	4.02	4.02	4.02	4.02	2	0.09	0.02	0.12	0.00	0.00	22.3
16	0	437	786	62	0	163	-82	4.02	4.02	4.02	4.02	2	0.05	0.02	0.14	0.00	0.00	22.3
17	0	461	782	64	0	170	-69	4.02	4.02	4.02	4.02	2	0.05	0.02	0.14	0.00	0.00	22.3
18	0	1659	225	20	0	31	2334	4.02	4.02	4.02	4.02	3	0.35	0.01	0.04	0.00	0.00	22.3
19	0	695	1290	250	0	673	-903	4.02	4.02	4.02	4.02	3	0.17	0.04	0.23	0.00	0.00	22.3
20	0	1071	783	113	0	291	1009	4.02	4.02	4.02	4.02	3	0.15	0.02	0.14	0.00	0.00	22.3
37	0	1803	-66	-79	0	-242	3153	4.02	4.02	4.02	4.02	3	0.48	0.00	0.01	0.00	0.00	22.3
38	0	196	1709	304	0	827	-2159	4.02	4.02	4.02	4.02	3	0.31	0.05	0.30	0.00	0.00	22.3
39	0	822	864	75	0	190	804	4.02	4.02	4.02	4.02	3	0.12	0.03	0.15	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	56	634	680	65	0	134	899	4.02	4.02	4.02	4.02	3	0.13	0.02	0.12	0.00	0.00	22.3
2	56	613	359	8	0	9	990	4.02	4.02	4.02	4.02	2	0.15	0.01	0.06	0.00	0.00	22.3
3	56	620	358	8	0	11	992	4.02	4.02	4.02	4.02	2	0.15	0.01	0.06	0.00	0.00	22.3
4	56	355	688	92	0	195	376	4.02	4.02	4.02	4.02	2	0.06	0.02	0.12	0.00	0.00	22.3
5	56	362	687	93	0	197	378	4.02	4.02	4.02	4.02	2	0.06	0.02	0.12	0.00	0.00	22.3
6	56	515	475	36	0	72	782	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
7	56	538	471	39	0	78	791	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
8	56	437	574	62	0	128	593	4.02	4.02	4.02	4.02	2	0.09	0.02	0.10	0.00	0.00	22.3
9	56	461	570	64	0	134	602	4.02	4.02	4.02	4.02	2	0.09	0.02	0.10	0.00	0.00	22.3
10	56	613	359	8	0	9	990	4.02	4.02	4.02	4.02	2	0.15	0.01	0.06	0.00	0.00	22.3
11	56	620	358	8	0	11	992	4.02	4.02	4.02	4.02	2	0.15	0.01	0.06	0.00	0.00	22.3
12	56	355	688	92	0	195	376	4.02	4.02	4.02	4.02	2	0.06	0.02	0.12	0.00	0.00	22.3
13	56	362	687	93	0	197	378	4.02	4.02	4.02	4.02	2	0.06	0.02	0.12	0.00	0.00	22.3
14	56	515	475	36	0	72	782	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
15	56	538	471	39	0	78	791	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
16	56	437	574	62	0	128	593	4.02	4.02	4.02	4.02	2	0.09	0.02	0.10	0.00	0.00	22.3
17	56	461	570	64	0	134	602	4.02	4.02	4.02	4.02	2	0.09	0.02	0.10	0.00	0.00	22.3
18	56	1659	-51	20	0	20	2334	4.02	4.02	4.02	4.02	3	0.35	0.00	0.01	0.00	0.00	22.3
19	56	695	1014	250	0	531	-766	4.02	4.02	4.02	4.02	3	0.13	0.03	0.18	0.00	0.00	22.3
20	56	1071	507	113	0	227	1234	4.02	4.02	4.02	4.02	3	0.18	0.01	0.09	0.00	0.00	22.3
37	56	1803	-341	-79	0	-197	3153	4.02	4.02	4.02	4.02	3	0.48	0.01	0.06	0.00	0.00	22.3
38	56	196	1434	304	0	655	-1997	4.02	4.02	4.02	4.02	3	0.29	0.04	0.26	0.00	0.00	22.3
39	56	822	589	75	0	148	1075	4.02	4.02	4.02	4.02	3	0.16	0.02	0.10	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	113	634	404	65	0	97	1012	4.02	4.02	4.02	4.02	3	0.15	0.01	0.07	0.00	0.00	22.3
2	113	613	147	8	0	5	990	4.02	4.02	4.02	4.02	2	0.15	0.00	0.03	0.00	0.00	22.3
3	113	620	146	8	0	6	992	4.02	4.02	4.02	4.02	2	0.15	0.00	0.03	0.00	0.00	22.3
4	113	355	476	92	0	143	597	4.02	4.02	4.02	4.02	2	0.09	0.01	0.08	0.00	0.00	22.3
5	113	362	475	93	0	144	599	4.02	4.02	4.02	4.02	2	0.09	0.01	0.08	0.00	0.00	22.3
6	113	515	264	36	0	51	839	4.02	4.02	4.02	4.02	2	0.13	0.01	0.05	0.00	0.00	22.3
7	113	538	259	39	0	56	845	4.02	4.02	4.02	4.02	2	0.13	0.01	0.05	0.00	0.00	22.3
8	113	437	362	62	0	93	737	4.02	4.02	4.02	4.02	2	0.11	0.01	0.06	0.00	0.00	22.3
9	113	461	358	64	0	97	741	4.02	4.02	4.02	4.02	2	0.11	0.01	0.06	0.00	0.00	22.3
10	113	613	147	8	0	5	990	4.02	4.02	4.02	4.02	2	0.15	0.00	0.03	0.00	0.00	22.3
11	113	620	146	8	0	6	992	4.02	4.02	4.02	4.02	2	0.15	0.00	0.03	0.00	0.00	22.3
12	113	355	476	92	0	143	597	4.02	4.02	4.02	4.02	2	0.09	0.01	0.08	0.00	0.00	22.3
13	113	362	475	93	0	144	599	4.02	4.02	4.02	4.02	2	0.09	0.01	0.08	0.00	0.00	22.3
14	113	515	264	36	0	51	839	4.02	4.02	4.02	4.02	2	0.13	0.01	0.05	0.00	0.00	22.3
15	113	538	259	39	0	56	845	4.02	4.02	4.02	4.02	2	0.13	0.01	0.05	0.00	0.00	22.3
16	113	437	362	62	0	93	737	4.02	4.02	4.02	4.02	2	0.11	0.01	0.06	0.00	0.00	22.3
17	113	461	358	64	0	97	741	4.02	4.02	4.02	4.02	2	0.11	0.01	0.06	0.00	0.00	22.3
18	113	1659	-326	20	0	8	2334	4.02	4.02	4.02	4.02	3	0.35	0.01	0.06	0.00	0.00	22.3
19	113	695	739	250	0	390	617	4.02	4.02	4.02	4.02	3	0.10	0.02	0.13	0.00	0.00	22.3
20	113	1071	232	113	0	163	1239	4.02	4.02	4.02	4.02	3	0.18	0.01	0.04	0.00	0.00	22.3
37	113	1803	-617	-79	0	-153	3079	4.02	4.02	4.02	4.02	3	0.47	0.02	0.11	0.00	0.00	22.3
38	113	196	1158	304	0	483	-1126	4.02	4.02	4.02	4.02	3	0.16	0.03	0.21	0.00	0.00	22.3
39	113	822	313	75	0	106	1131	4.02	4.02	4.02	4.02	3	0.17	0.01	0.06	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	170	634	129	65	0	60	1012	4.02	4.02	4.02	4.02	3	0.15	0.00	0.02	0.00	0.00	22.3
2	170	613	-65	8	0	1	990	4.02	4.02	4.02	4.02	2	0.15	0.00	0.01	0.00	0.00	22.3
3	170	620	-66	8	0	2	992	4.02	4.02	4.02	4.02	2	0.15	0.00	0.01	0.00	0.00	22.3
4	170	355	264	92	0	90	655	4.02	4.02	4.02	4.02	2	0.10	0.01	0.05	0.00	0.00	22.3
5	170	362	263	93	0	91	656	4.02	4.02	4.02	4.02	2	0.10	0.01	0.05	0.00	0.00	22.3
6	170	515	52	36	0	31	839	4.02	4.02	4.02	4.02	2	0.13	0.00	0.01	0.00	0.00	22.3
7	170	538	47	39	0	34	845	4.02	4.02	4.02	4.02	2	0.13	0.00	0.01	0.00	0.00	22.3
8	170	437	150	62	0	58	737	4.02	4.02	4.02	4.02	2	0.11	0.00	0.03	0.00	0.00	22.3
9	170	461	146	64	0	61	741	4.02	4.02	4.02	4.02	2	0.11	0.00	0.03	0.00	0.00	22.3
10	170	613	-65	8	0	1	990	4.02	4.02	4.02	4.02	2	0.15	0.00	0.01	0.00	0.00	22.3
11	170	620	-66	8	0	2	992	4.02	4.02	4.02	4.02	2	0.15	0.00	0.01	0.00	0.00	22.3
12	170	355	264	92	0	90	655	4.02	4.02	4.02	4.02	2	0.10	0.01	0.05	0.00	0.00	22.3
13	170	362	263	93	0	91	656	4.02	4.02	4.02	4.02	2	0.10	0.01	0.05	0.00	0.00	22.3
14	170	515	52	36	0	31	839	4.02	4.02	4.02	4.02	2	0.13	0.00	0.01	0.00	0.00	22.3
15	170	538	47	39	0	34	845	4.02	4.02	4.02	4.02	2	0.13	0.00	0.01	0.00	0.00	22.3
16	170	437	150	62	0	58	737	4.02	4.02	4.02	4.02	2	0.11	0.00	0.03	0.00	0.00	22.3
17	170	461	146	64	0	61	741	4.02	4.02	4.02	4.02	2	0.11	0.00	0.03	0.00	0.00	22.3
18	170	1659	-602	20	0	-3	2270	4.02	4.02	4.02	4.02	3	0.34	0.02	0.11	0.00	0.00	22.3
19	170	695	464	250	0	248	795	4.02	4.02	4.02	4.02	3	0.12	0.01	0.08	0.00	0.00	22.3
20	170	1071	-44	113	0	100	1239	4.02	4.02	4.02	4.02	3	0.18	0.00	0.01	0.00	0.00	22.3
37	170	1803	-892	-79	0	-108	2792	4.02	4.02	4.02	4.02	3	0.42	0.03	0.16	0.00	0.00	22.3
38	170	196	882	304	0	312	484	4.02	4.02	4.02	4.02	3	0.08	0.03	0.16	0.00	0.00	22.3
39	170	822	38	75	0	64	1131	4.02	4.02	4.02	4.02	3	0.17	0.00	0.01	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	226	634	-147	65	0	23	1012	4.02	4.02	4.02	4.02	3	0.15	0.00	0.03	0.00	0.00	22.3
2	226	613	-277	8	0	-4	990	4.02	4.02	4.02	4.02	2	0.15	0.01	0.05	0.00	0.00	22.3
3	226	620	-278	8	0	-3	992	4.02	4.02	4.02	4.02	2	0.15	0.01	0.05	0.00	0.00	22.3
4	226	355	52	92	0	38	655	4.02	4.02	4.02	4.02	2	0.10	0.00	0.01	0.00	0.00	22.3
5	226	362	51	93	0	39	656	4.02	4.02	4.02	4.02	2	0.10	0.00	0.01	0.00	0.00	22.3
6	226	515	-160	36	0	10	839	4.02	4.02	4.02	4.02	2	0.13	0.00	0.03	0.00	0.00	22.3
7	226	538	-165	39	0	12	845	4.02	4.02	4.02	4.02	2	0.13	0.00	0.03	0.00	0.00	22.3
8	226	437	-62	62	0	23	737	4.02	4.02	4.02	4.02	2	0.11	0.00	0.01	0.00	0.00	22.3
9	226	461	-66	64	0	25	741	4.02	4.02	4.02	4.02	2	0.11	0.00	0.01	0.00	0.00	22.3
10	226	613	-277	8	0	-4	990	4.02	4.02	4.02	4.02	2	0.15	0.01	0.05	0.00	0.00	22.3
11	226	620	-278	8	0	-3	992	4.02	4.02	4.02	4.02	2	0.15	0.01	0.05	0.00	0.00	22.3
12	226	355	52	92	0	38	655	4.02	4.02	4.02	4.02	2	0.10	0.00	0.01	0.00	0.00	22.3
13	226	362	51	93	0	39	656	4.02	4.02	4.02	4.02	2	0.10	0.00	0.01	0.00	0.00	22.3
14	226	515	-160	36	0	10	839	4.02	4.02	4.02	4.02	2	0.13	0.00	0.03	0.00	0.00	22.3
15	226	538	-165	39	0	12	845	4.02	4.02	4.02	4.02	2	0.13	0.00	0.03	0.00	0.00	22.3
16	226	437	-62	62	0	23	737	4.02	4.02	4.02	4.02	2	0.11	0.00	0.01	0.00	0.00	22.3
17	226	461	-66	64	0	25	741	4.02	4.02	4.02	4.02	2	0.11	0.00	0.01	0.00	0.00	22.3
18	226	1659	-877	20	0	-15	1992	4.02	4.02	4.02	4.02	3	0.30	0.03	0.16	0.00	0.00	22.3
19	226	695	188	250	0	107	795	4.02	4.02	4.02	4.02	3	0.12	0.01	0.04	0.00	0.00	22.3
20	226	1071	-319	113	0	36	1239	4.02	4.02	4.02	4.02	3	0.18	0.01	0.06	0.00	0.00	22.3
37	226	1803	-1168	-79	0	-63	2350	4.02	4.02	4.02	4.02	3	0.36	0.03	0.21	0.00	0.00	22.3
38	226	196	607	304	0	140	765	4.02	4.02	4.02	4.02	3	0.11	0.02	0.11	0.00	0.00	22.3
39	226	822	-238	75	0	22	1131	4.02	4.02	4.02	4.02	3	0.17	0.01	0.04	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	282	634	-422	65	0	-14	1012	4.02	4.02	4.02	4.02	3	0.15	0.01	0.08	0.00	0.00	22.3
2	282	613	-489	8	0	-8	924	4.02	4.02	4.02	4.02	2	0.14	0.01	0.09	0.00	0.00	22.3
3	282	620	-490	8	0	-8	925	4.02	4.02	4.02	4.02	2	0.14	0.01	0.09	0.00	0.00	22.3
4	282	355	-160	92	0	-14	655	4.02	4.02	4.02	4.02	2	0.10	0.00	0.03	0.00	0.00	22.3
5	282	362	-161	93	0	-14	656	4.02	4.02	4.02	4.02	2	0.10	0.00	0.03	0.00	0.00	22.3
6	282	515	-372	36	0	-10	839	4.02	4.02	4.02	4.02	2	0.13	0.01	0.07	0.00	0.00	22.3
7	282	538	-376	39	0	-10	845	4.02	4.02	4.02	4.02	2	0.13	0.01	0.07	0.00	0.00	22.3
8	282	437	-274	62	0	-12	737	4.02	4.02	4.02	4.02	2	0.11	0.01	0.05	0.00	0.00	22.3
9	282	461	-278	64	0	-12	741	4.02	4.02	4.02	4.02	2	0.11	0.01	0.05	0.00	0.00	22.3
10	282	613	-489	8	0	-8	924	4.02	4.02	4.02	4.02	2	0.14	0.01	0.09	0.00	0.00	22.3
11	282	620	-490	8	0	-8	925	4.02	4.02	4.02	4.02	2	0.14	0.01	0.09	0.00	0.00	22.3
12	282	355	-160	92	0	-14	655	4.02	4.02	4.02	4.02	2	0.10	0.00	0.03	0.00	0.00	22.3
13	282	362	-161	93	0	-14	656	4.02	4.02	4.02	4.02	2	0.10	0.00	0.03	0.00	0.00	22.3
14	282	515	-372	36	0	-10	839	4.02	4.02	4.02	4.02	2	0.13	0.01	0.07	0.00	0.00	22.3
15	282	538	-376	39	0	-10	845	4.02	4.02	4.02	4.02	2	0.13	0.01	0.07	0.00	0.00	22.3
16	282	437	-274	62	0	-12	737	4.02	4.02	4.02	4.02	2	0.11	0.01	0.05	0.00	0.00	22.3
17	282	461	-278	64	0	-12	741	4.02	4.02	4.02	4.02	2	0.11	0.01	0.05	0.00	0.00	22.3
18	282	1659	-1153	20	0	-26	1558	4.02	4.02	4.02	4.02	3	0.23	0.03	0.21	0.00	0.00	22.3
19	282	695	-88	250	0	-34	795	4.02	4.02	4.02	4.02	3	0.12	0.01	0.04	0.00	0.00	22.3
20	282	1071	-595	113	0	-28	1180	4.02	4.02	4.02	4.02	3	0.17	0.02	0.11	0.00	0.00	22.3
37	282	1803	-1443	-79	0	-18	1752	4.02	4.02	4.02	4.02	3	0.27	0.04	0.26	0.00	0.00	22.3
38	282	196	332	304	0	-32	832	4.02	4.02	4.02	4.02	3	0.12	0.01	0.06	0.00	0.00	22.3
39	282	822	-513	75	0	-21	1122	4.02	4.02	4.02	4.02	3	0.16	0.01	0.09	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	339	634	-697	65	0	-51	883	4.02	4.02	4.02	4.02	3	0.13	0.02	0.12	0.00	0.00	22.3
2	339	613	-701	8	0	-12	696	4.02	4.02	4.02	4.02	2	0.11	0.02	0.12	0.00	0.00	22.3
3	339	620	-702	8	0	-13	696	4.02	4.02	4.02	4.02	2	0.11	0.02	0.12	0.00	0.00	22.3
4	339	355	-372	92	0	-66	655	4.02	4.02	4.02	4.02	2	0.10	0.01	0.07	0.00	0.00	22.3
5	339	362	-373	93	0	-66	656	4.02	4.02	4.02	4.02	2	0.10	0.01	0.07	0.00	0.00	22.3
6	339	515	-584	36	0	-31	684	4.02	4.02	4.02	4.02	2	0.11	0.02	0.10	0.00	0.00	22.3
7	339	538	-588	39	0	-32	685	4.02	4.02	4.02	4.02	2	0.11	0.02	0.10	0.00	0.00	22.3
8	339	437	-485	62	0	-47	674	4.02	4.02	4.02	4.02	2	0.10	0.01	0.09	0.00	0.00	22.3
9	339	461	-489	64	0	-48	675	4.02	4.02	4.02	4.02	2	0.10	0.01	0.09	0.00	0.00	22.3
10	339	613	-701	8	0	-12	696	4.02	4.02	4.02	4.02	2	0.11	0.02	0.12	0.00	0.00	22.3
11	339	620	-702	8	0	-13	696	4.02	4.02	4.02	4.02	2	0.11	0.02	0.12	0.00	0.00	22.3
12	339	355	-372	92	0	-66	655	4.02	4.02	4.02	4.02	2	0.10	0.01	0.07	0.00	0.00	22.3
13	339	362	-373	93	0	-66	656	4.02	4.02	4.02	4.02	2	0.10	0.01	0.07	0.00	0.00	22.3
14	339	515	-584	36	0	-31	684	4.02	4.02	4.02	4.02	2	0.11	0.02	0.10	0.00	0.00	22.3
15	339	538	-588	39	0	-32	685	4.02	4.02	4.02	4.02	2	0.11	0.02	0.10	0.00	0.00	22.3
16	339	437	-485	62	0	-47	674	4.02	4.02	4.02	4.02	2	0.10	0.01	0.09	0.00	0.00	22.3
17	339	461	-489	64	0	-48	675	4.02	4.02	4.02	4.02	2	0.10	0.01	0.09	0.00	0.00	22.3
18	339	1659	-1428	20	0	-38	968	4.02	4.02	4.02	4.02	3	0.15	0.04	0.25	0.00	0.00	22.3
19	339	695	-363	250	0	-176	795	4.02	4.02	4.02	4.02	3	0.12	0.01	0.06	0.00	0.00	22.3
20	339	1071	-870	113	0	-91	905	4.02	4.02	4.02	4.02	3	0.13	0.03	0.15	0.00	0.00	22.3
37	339	1803	-1718	-79	0	27	998	4.02	4.02	4.02	4.02	3	0.15	0.05	0.31	0.00	0.00	22.3
38	339	196	56	304	0	-203	832	4.02	4.02	4.02	4.02	3	0.12	0.01	0.05	0.00	0.00	22.3
39	339	822	-788	75	0	-63	894	4.02	4.02	4.02	4.02	3	0.13	0.02	0.14	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	396	634	-973	65	0	-88	550	4.02	4.02	4.02	4.02	3	0.08	0.03	0.17	0.00	0.00	22.3
2	396	613	-912	8	0	-17	-577	4.02	4.02	4.02	4.02	2	0.09	0.03	0.16	0.00	0.00	22.3
3	396	620	-913	8	0	-17	-578	4.02	4.02	4.02	4.02	2	0.09	0.03	0.16	0.00	0.00	22.3

4	396	355	-583	92	0	-118	500	4.02	4.02	4.02	4.02	2	0.08	0.02	0.10	0.00	0.00	22.3
5	396	362	-584	93	0	-119	499	4.02	4.02	4.02	4.02	2	0.08	0.02	0.10	0.00	0.00	22.3
6	396	515	-796	36	0	-51	-404	4.02	4.02	4.02	4.02	2	0.06	0.02	0.14	0.00	0.00	22.3
7	396	538	-800	39	0	-54	-410	4.02	4.02	4.02	4.02	2	0.06	0.02	0.14	0.00	0.00	22.3
8	396	437	-697	62	0	-82	447	4.02	4.02	4.02	4.02	2	0.07	0.02	0.12	0.00	0.00	22.3
9	396	461	-701	64	0	-84	446	4.02	4.02	4.02	4.02	2	0.07	0.02	0.12	0.00	0.00	22.3
10	396	613	-912	8	0	-17	-577	4.02	4.02	4.02	4.02	2	0.09	0.03	0.16	0.00	0.00	22.3
11	396	620	-913	8	0	-17	-578	4.02	4.02	4.02	4.02	2	0.09	0.03	0.16	0.00	0.00	22.3
12	396	355	-583	92	0	-118	500	4.02	4.02	4.02	4.02	2	0.08	0.02	0.10	0.00	0.00	22.3
13	396	362	-584	93	0	-119	499	4.02	4.02	4.02	4.02	2	0.08	0.02	0.10	0.00	0.00	22.3
14	396	515	-796	36	0	-51	-404	4.02	4.02	4.02	4.02	2	0.06	0.02	0.14	0.00	0.00	22.3
15	396	538	-800	39	0	-54	-410	4.02	4.02	4.02	4.02	2	0.06	0.02	0.14	0.00	0.00	22.3
16	396	437	-697	62	0	-82	447	4.02	4.02	4.02	4.02	2	0.07	0.02	0.12	0.00	0.00	22.3
17	396	461	-701	64	0	-84	446	4.02	4.02	4.02	4.02	2	0.07	0.02	0.12	0.00	0.00	22.3
18	396	1659	-1704	20	0	-49	-1502	4.02	4.02	4.02	4.02	3	0.23	0.05	0.30	0.00	0.00	22.3
19	396	695	-638	250	0	-317	708	4.02	4.02	4.02	4.02	3	0.10	0.02	0.11	0.00	0.00	22.3
20	396	1071	-1146	113	0	-155	-684	4.02	4.02	4.02	4.02	3	0.10	0.03	0.20	0.00	0.00	22.3
37	396	1803	-1994	-79	0	71	-1930	4.02	4.02	4.02	4.02	3	0.29	0.06	0.36	0.00	0.00	22.3
38	396	196	-219	304	0	-375	832	4.02	4.02	4.02	4.02	3	0.12	0.01	0.05	0.00	0.00	22.3
39	396	822	-1064	75	0	-105	-567	4.02	4.02	4.02	4.02	3	0.08	0.03	0.19	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	452	634	-1248	65	0	-125	-1202	4.02	4.02	4.02	4.02	3	0.18	0.04	0.22	0.00	0.00	22.3
2	452	613	-1124	8	0	-21	-1259	4.02	4.02	4.02	4.02	2	0.19	0.03	0.20	0.00	0.00	22.3
3	452	620	-1125	8	0	-22	-1261	4.02	4.02	4.02	4.02	2	0.19	0.03	0.20	0.00	0.00	22.3
4	452	355	-795	92	0	-170	-588	4.02	4.02	4.02	4.02	2	0.09	0.02	0.14	0.00	0.00	22.3
5	452	362	-796	93	0	-172	-590	4.02	4.02	4.02	4.02	2	0.09	0.02	0.14	0.00	0.00	22.3
6	452	515	-1007	36	0	-72	-1021	4.02	4.02	4.02	4.02	2	0.16	0.03	0.18	0.00	0.00	22.3
7	452	538	-1012	39	0	-76	-1030	4.02	4.02	4.02	4.02	2	0.16	0.03	0.18	0.00	0.00	22.3
8	452	437	-909	62	0	-117	-820	4.02	4.02	4.02	4.02	2	0.13	0.03	0.16	0.00	0.00	22.3
9	452	461	-913	64	0	-121	-828	4.02	4.02	4.02	4.02	2	0.13	0.03	0.16	0.00	0.00	22.3
10	452	613	-1124	8	0	-21	-1259	4.02	4.02	4.02	4.02	2	0.19	0.03	0.20	0.00	0.00	22.3
11	452	620	-1125	8	0	-22	-1261	4.02	4.02	4.02	4.02	2	0.19	0.03	0.20	0.00	0.00	22.3
12	452	355	-795	92	0	-170	-588	4.02	4.02	4.02	4.02	2	0.09	0.02	0.14	0.00	0.00	22.3
13	452	362	-796	93	0	-172	-590	4.02	4.02	4.02	4.02	2	0.09	0.02	0.14	0.00	0.00	22.3
14	452	515	-1007	36	0	-72	-1021	4.02	4.02	4.02	4.02	2	0.16	0.03	0.18	0.00	0.00	22.3
15	452	538	-1012	39	0	-76	-1030	4.02	4.02	4.02	4.02	2	0.16	0.03	0.18	0.00	0.00	22.3
16	452	437	-909	62	0	-117	-820	4.02	4.02	4.02	4.02	2	0.13	0.03	0.16	0.00	0.00	22.3
17	452	461	-913	64	0	-121	-828	4.02	4.02	4.02	4.02	2	0.13	0.03	0.16	0.00	0.00	22.3
18	452	1659	-1979	20	0	-61	-2682	4.02	4.02	4.02	4.02	3	0.40	0.06	0.35	0.00	0.00	22.3
19	452	695	-914	250	0	-459	-517	4.02	4.02	4.02	4.02	3	0.11	0.03	0.16	0.00	0.00	22.3
20	452	1071	-1421	113	0	-219	-1549	4.02	4.02	4.02	4.02	3	0.23	0.04	0.25	0.00	0.00	22.3
37	452	1803	-2269	-79	0	116	-3274	4.02	4.02	4.02	4.02	3	0.50	0.07	0.40	0.00	0.00	22.3
38	452	196	-495	304	0	-547	832	4.02	4.02	4.02	4.02	3	0.14	0.01	0.09	0.00	0.00	22.3
39	452	822	-1339	75	0	-147	-1385	4.02	4.02	4.02	4.02	3	0.20	0.04	0.24	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	508	634	-1524	65	0	-162	-2124	4.02	4.02	4.02	4.02	3	0.31	0.04	0.27	0.00	0.00	22.3
2	508	613	-1336	8	0	-25	-2062	4.02	4.02	4.02	4.02	2	0.32	0.04	0.24	0.00	0.00	22.3
3	508	620	-1337	8	0	-27	-2064	4.02	4.02	4.02	4.02	2	0.32	0.04	0.24	0.00	0.00	22.3
4	508	355	-1007	92	0	-222	-1204	4.02	4.02	4.02	4.02	2	0.18	0.03	0.18	0.00	0.00	22.3
5	508	362	-1008	93	0	-224	-1207	4.02	4.02	4.02	4.02	2	0.18	0.03	0.18	0.00	0.00	22.3
6	508	515	-1219	36	0	-92	-1757	4.02	4.02	4.02	4.02	2	0.27	0.04	0.22	0.00	0.00	22.3
7	508	538	-1224	39	0	-98	-1768	4.02	4.02	4.02	4.02	2	0.27	0.04	0.22	0.00	0.00	22.3
8	508	437	-1121	62	0	-151	-1500	4.02	4.02	4.02	4.02	2	0.23	0.03	0.20	0.00	0.00	22.3
9	508	461	-1125	64	0	-157	-1511	4.02	4.02	4.02	4.02	2	0.23	0.03	0.20	0.00	0.00	22.3
10	508	613	-1336	8	0	-25	-2062	4.02	4.02	4.02	4.02	2	0.32	0.04	0.24	0.00	0.00	22.3
11	508	620	-1337	8	0	-27	-2064	4.02	4.02	4.02	4.02	2	0.32	0.04	0.24	0.00	0.00	22.3
12	508	355	-1007	92	0	-222	-1204	4.02	4.02	4.02	4.02	2	0.18	0.03	0.18	0.00	0.00	22.3
13	508	362	-1008	93	0	-224	-1207	4.02	4.02	4.02	4.02	2	0.18	0.03	0.18	0.00	0.00	22.3
14	508	515	-1219	36	0	-92	-1757	4.02	4.02	4.02	4.02	2	0.27	0.04	0.22	0.00	0.00	22.3
15	508	538	-1224	39	0	-98	-1768	4.02	4.02	4.02	4.02	2	0.27	0.04	0.22	0.00	0.00	22.3
16	508	437	-1121	62	0	-151	-1500	4.02	4.02	4.02	4.02	2	0.23	0.03	0.20	0.00	0.00	22.3
17	508	461	-1125	64	0	-157	-1511	4.02	4.02	4.02	4.02	2	0.23	0.03	0.20	0.00	0.00	22.3
18	508	1659	-2255	20	0	-72	-4017	4.02	4.02	4.02	4.02	3	0.61	0.07	0.40	0.00	0.00	22.3
19	508	695	-1189	250	0	-600	-1250	4.02	4.02	4.02	4.02	3	0.18	0.03	0.21	0.00	0.00	22.3
20	508	1071	-1697	113	0	-283	-2569	4.02	4.02	4.02	4.02	3	0.38	0.05	0.30	0.00	0.00	22.3
37	508	1803	-2545	-79	0	161	-4774	4.02	4.02	4.02	4.02	3	0.72	0.07	0.45	0.00	0.00	22.3
38	508	196	-770	304	0	-719	617	4.02	4.02	4.02	4.02	3	0.18	0.02	0.14	0.00	0.00	22.3
39	508	822	-1615	75	0	-190	-2359	4.02	4.02	4.02	4.02	3	0.35	0.05	0.29	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	565	634	-1799	65	0	-199	-2292	4.02	4.02	4.02	4.02	3	0.33	0.05	0.32	0.00	0.00	22.3
2	565	613	-1548	8	0	-29	-2200	4.02	4.02	4.02	4.02	2	0.34	0.04	0.28	0.00	0.00	22.3
3	565	620	-1549	8	0	-32	-2203	4.02	4.02	4.02	4.02	2	0.34	0.04	0.28	0.00	0.00	22.3
4	565	355	-1219	92	0	-275	-1323	4.02	4.02	4.02	4.02	2	0.20	0.04	0.22	0.00	0.00	22.3
5	565	362	-1220	93	0	-277	-1326	4.02	4.02	4.02	4.02	2	0.20	0.04	0.22	0.00	0.00	22.3
6	565	515	-1431	36	0	-113	-1889	4.02	4.02	4.02	4.02	2	0.29	0.04	0.25	0.00	0.00	22.3
7	565	538	-1436	39	0	-120	-1900	4.02	4.02	4.02	4.02	2	0.29	0.04	0.26	0.00	0.00	22.3
8	565	437	-1333	62	0	-186	-1626	4.02	4.02	4.02	4.02	2	0.25	0.04	0.24	0.00	0.00	22.3
9	565	461	-1337	64	0	-193	-1637	4.02	4.02	4.02	4.02	2	0.25	0.04	0.24	0.00	0.00	22.3
10	565	613	-1548	8	0	-29	-2200	4.02	4.02	4.02	4.02	2	0.34	0.04	0.28	0.00	0.00	22.3
11	565	620	-1549	8	0	-32	-2203	4.02	4.02	4.02	4.02	2	0.34	0.04	0.28	0.00	0.00	22.3
12	565	355	-1219	92	0	-275	-1323	4.02	4.02	4.02	4.02	2	0.20	0.04	0.22	0.00	0.00	22.3
13	565	362	-1220	93	0	-277	-1326	4.02	4.02	4.02	4.02	2	0.20	0.04	0.22	0.00	0.00	22.3
14	565	515	-1431	36	0	-113	-1889	4.02	4.02	4.02	4.02	2	0.29	0.04	0.25	0.00	0.00	22.3
15	565	538	-1436	39	0	-120	-1900	4.02	4.02	4.02	4.02	2	0.29	0.04	0.26	0.00	0.00	22.3
16	565	437	-1333	62	0	-186	-1626	4.02	4.02	4.02	4.02	2	0.25	0.04	0.24	0.00	0.00	22.3
17	565	461	-1337	64	0	-193	-1637	4.02	4.02	4.02	4.02	2	0.25	0.04	0.24	0.00	0.00	22.3
18	565	1659	-2530	20	0	-84	-4227	4.02	4.02	4.02	4.02	3	0.64	0.07	0.45	0.00	0.00	22.3
19	565	695	-1465	250	0	-741	-1398	4.02	4.02	4.02	4.02	3	0.20	0.04	0.26	0.00	0.00	22.3
20	565	1071	-1972	113	0	-346	-2746	4.02	4.02	4.02	4.02	3	0.41	0.06	0.35	0.00	0.00	22.3
37	565	1803	-2820	-79	0	206	-5001	4.02	4.02	4.02	4.02	3	0.76	0.08	0.50	0.00	0.00	22.3
38	565	196	-1046	304	0	-890	-286	4.02	4.02	4.02	4.02	3	0.22	0.03	0.19	0.00	0.00	22.3
39	565	822	-1890	75	0	-232	-2532	4.02	4.02	4.02	4.02	3	0.37	0.05	0.34	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

Nome travata: **trave_501_IP1** Descrizione: **Trave_5 11-16-21-26**
ASTA NUM. 2 NI 171 NF 185 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y qy tot.
qy medio: 375.00 375.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

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NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	1917	1111	108	0	313	-611	4.02	4.02	4.02	4.02	3	0.09	0.03	0.20	0.00	0.00	22.3
2	0	1722	703	34	0	104	-45	4.02	4.02	4.02	4.02	2	0.03	0.02	0.13	0.00	0.00	22.3
3	0	1736	704	35	0	109	-46	4.02	4.02	4.02	4.02	2	0.03	0.02	0.13	0.00	0.00	22.3
4	0	1213	1006	131	0	373	-895	4.02	4.02	4.02	4.02	2	0.14	0.03	0.18	0.00	0.00	22.3
5	0	1227	1006	132	0	378	-896	4.02	4.02	4.02	4.02	2	0.14	0.03	0.18	0.00	0.00	22.3
6	0	1526	809	66	0	193	-341	4.02	4.02	4.02	4.02	2	0.06	0.02	0.14	0.00	0.00	22.3
7	0	1575	810	71	0	209	-344	4.02	4.02	4.02	4.02	2	0.06	0.02	0.14	0.00	0.00	22.3
8	0	1374	900	95	0	274	-596	4.02	4.02	4.02	4.02	2	0.09	0.03	0.16	0.00	0.00	22.3
9	0	1423	901	100	0	289	-599	4.02	4.02	4.02	4.02	2	0.09	0.03	0.16	0.00	0.00	22.3
10	0	1722	703	34	0	104	-45	4.02	4.02	4.02	4.02	2	0.03	0.02	0.13	0.00	0.00	22.3
11	0	1736	704	35	0	109	-46	4.02	4.02	4.02	4.02	2	0.03	0.02	0.13	0.00	0.00	22.3
12	0	1213	1006	131	0	373	-895	4.02	4.02	4.02	4.02	2	0.14	0.03	0.18	0.00	0.00	22.3
13	0	1227	1006	132	0	378	-896	4.02	4.02	4.02	4.02	2	0.14	0.03	0.18	0.00	0.00	22.3
14	0	1526	809	66	0	193	-341	4.02	4.02	4.02	4.02	2	0.06	0.02	0.14	0.00	0.00	22.3
15	0	1575	810	71	0	209	-344	4.02	4.02	4.02	4.02	2	0.06	0.02	0.14	0.00	0.00	22.3
16	0	1374	900	95	0	274	-596	4.02	4.02	4.02	4.02	2	0.09	0.03	0.16	0.00	0.00	22.3
17	0	1423	901	100	0	289	-599	4.02	4.02	4.02	4.02	2	0.09	0.03	0.16	0.00	0.00	22.3
18	0	4601	421	90	0	280	1486	4.02	4.02	4.02	4.02	3	0.25	0.01	0.07	0.00	0.00	22.3
19	0	2462	1405	349	0	991	-1442	4.02	4.02	4.02	4.02	3	0.26	0.04	0.25	0.00	0.00	22.3
20	0	3277	942	214	0	624	-139	4.02	4.02	4.02	4.02	3	0.17	0.03	0.17	0.00	0.00	22.3
37	0	4786	158	-33	0	-62	2072	4.02	4.02	4.02	4.02	3	0.35	0.00	0.03	0.00	0.00	22.3
38	0	1221	1799	399	0	1122	-2544	4.02	4.02	4.02	4.02	3	0.38	0.05	0.32	0.00	0.00	22.3
39	0	2579	1026	173	0	511	-373	4.02	4.02	4.02	4.02	3	0.13	0.03	0.18	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	57	1917	836	108	0	252	-484	4.02	4.02	4.02	4.02	3	0.07	0.02	0.15	0.00	0.00	22.3
2	57	1722	491	34	0	85	541	4.02	4.02	4.02	4.02	2	0.09	0.01	0.09	0.00	0.00	22.3
3	57	1736	492	35	0	89	541	4.02	4.02	4.02	4.02	2	0.09	0.01	0.09	0.00	0.00	22.3
4	57	1213	794	131	0	299	-788	4.02	4.02	4.02	4.02	2	0.12	0.02	0.14	0.00	0.00	22.3
5	57	1227	794	132	0	303	-789	4.02	4.02	4.02	4.02	2	0.12	0.02	0.14	0.00	0.00	22.3
6	57	1526	597	66	0	155	358	4.02	4.02	4.02	4.02	2	0.06	0.02	0.11	0.00	0.00	22.3
7	57	1575	598	71	0	169	356	4.02	4.02	4.02	4.02	2	0.06	0.02	0.11	0.00	0.00	22.3
8	57	1374	688	95	0	220	-496	4.02	4.02	4.02	4.02	2	0.08	0.02	0.12	0.00	0.00	22.3
9	57	1423	689	100	0	233	-499	4.02	4.02	4.02	4.02	2	0.08	0.02	0.12	0.00	0.00	22.3
10	57	1722	491	34	0	85	541	4.02	4.02	4.02	4.02	2	0.09	0.01	0.09	0.00	0.00	22.3
11	57	1736	492	35	0	89	541	4.02	4.02	4.02	4.02	2	0.09	0.01	0.09	0.00	0.00	22.3
12	57	1213	794	131	0	299	-788	4.02	4.02	4.02	4.02	2	0.12	0.02	0.14	0.00	0.00	22.3
13	57	1227	794	132	0	303	-789	4.02	4.02	4.02	4.02	2	0.12	0.02	0.14	0.00	0.00	22.3
14	57	1526	597	66	0	155	358	4.02	4.02	4.02	4.02	2	0.06	0.02	0.11	0.00	0.00	22.3
15	57	1575	598	71	0	169	356	4.02	4.02	4.02	4.02	2	0.06	0.02	0.11	0.00	0.00	22.3
16	57	1374	688	95	0	220	-496	4.02	4.02	4.02	4.02	2	0.08	0.02	0.12	0.00	0.00	22.3
17	57	1423	689	100	0	233	-499	4.02	4.02	4.02	4.02	2	0.08	0.02	0.12	0.00	0.00	22.3
18	57	4601	145	90	0	230	1486	4.02	4.02	4.02	4.02	3	0.25	0.00	0.03	0.00	0.00	22.3
19	57	2462	1130	349	0	794	-1298	4.02	4.02	4.02	4.02	3	0.21	0.03	0.20	0.00	0.00	22.3
20	57	3277	666	214	0	503	652	4.02	4.02	4.02	4.02	3	0.14	0.02	0.12	0.00	0.00	22.3
37	57	4786	-118	-33	0	-43	2072	4.02	4.02	4.02	4.02	3	0.35	0.00	0.02	0.00	0.00	22.3
38	57	1221	1524	399	0	897	-2377	4.02	4.02	4.02	4.02	3	0.35	0.04	0.27	0.00	0.00	22.3
39	57	2579	750	173	0	413	509	4.02	4.02	4.02	4.02	3	0.11	0.02	0.13	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	113	1917	560	108	0	191	617	4.02	4.02	4.02	4.02	3	0.09	0.02	0.10	0.00	0.00	22.3
2	113	1722	279	34	0	66	608	4.02	4.02	4.02	4.02	2	0.10	0.01	0.05	0.00	0.00	22.3
3	113	1736	280	35	0	69	608	4.02	4.02	4.02	4.02	2	0.10	0.01	0.05	0.00	0.00	22.3
4	113	1213	582	131	0	225	297	4.02	4.02	4.02	4.02	2	0.06	0.02	0.10	0.00	0.00	22.3
5	113	1227	582	132	0	229	297	4.02	4.02	4.02	4.02	2	0.07	0.02	0.10	0.00	0.00	22.3
6	113	1526	385	66	0	118	528	4.02	4.02	4.02	4.02	2	0.08	0.01	0.07	0.00	0.00	22.3
7	113	1575	386	71	0	129	527	4.02	4.02	4.02	4.02	2	0.08	0.01	0.07	0.00	0.00	22.3
8	113	1374	476	95	0	166	422	4.02	4.02	4.02	4.02	2	0.07	0.01	0.08	0.00	0.00	22.3
9	113	1423	477	100	0	177	421	4.02	4.02	4.02	4.02	2	0.07	0.01	0.08	0.00	0.00	22.3
10	113	1722	279	34	0	66	608	4.02	4.02	4.02	4.02	2	0.10	0.01	0.05	0.00	0.00	22.3
11	113	1736	280	35	0	69	608	4.02	4.02	4.02	4.02	2	0.10	0.01	0.05	0.00	0.00	22.3
12	113	1213	582	131	0	225	297	4.02	4.02	4.02	4.02	2	0.06	0.02	0.10	0.00	0.00	22.3
13	113	1227	582	132	0	229	297	4.02	4.02	4.02	4.02	2	0.07	0.02	0.10	0.00	0.00	22.3
14	113	1526	385	66	0	118	528	4.02	4.02	4.02	4.02	2	0.08	0.01	0.07	0.00	0.00	22.3
15	113	1575	386	71	0	129	527	4.02	4.02	4.02	4.02	2	0.08	0.01	0.07	0.00	0.00	22.3
16	113	1374	476	95	0	166	422	4.02	4.02	4.02	4.02	2	0.07	0.01	0.08	0.00	0.00	22.3
17	113	1423	477	100	0	177	421	4.02	4.02	4.02	4.02	2	0.07	0.01	0.08	0.00	0.00	22.3
18	113	4601	-130	90	0	179	1486	4.02	4.02	4.02	4.02	3	0.25	0.00	0.02	0.00	0.00	22.3
19	113	2462	854	349	0	596	-598	4.02	4.02	4.02	4.02	3	0.16	0.02	0.15	0.00	0.00	22.3
20	113	3277	391	214	0	382	757	4.02	4.02	4.02	4.02	3	0.12	0.01	0.07	0.00	0.00	22.3
37	113	4786	-393	-33	0	-24	2072	4.02	4.02	4.02	4.02	3	0.35	0.01	0.07	0.00	0.00	22.3
38	113	1221	1248	399	0	671	-1455	4.02	4.02	4.02	4.02	3	0.22	0.04	0.22	0.00	0.00	22.3
39	113	2579	475	173	0	315	701	4.02	4.02	4.02	4.02	3	0.11	0.01	0.08	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	170	1917	285	108	0	131	655	4.02	4.02	4.02	4.02	3	0.10	0.01	0.05	0.00	0.00	22.3
2	170	1722	67	34	0	47	608	4.02	4.02	4.02	4.02	2	0.10	0.00	0.01	0.00	0.00	22.3
3	170	1736	68	35	0	49	608	4.02	4.02	4.02	4.02	2	0.10	0.00	0.01	0.00	0.00	22.3
4	170	1213	370	131	0	151	451	4.02	4.02	4.02	4.02	2	0.07	0.01	0.07	0.00	0.00	22.3
5	170	1227	370	132	0	154	451	4.02	4.02	4.02	4.02	2	0.07	0.01	0.07	0.00	0.00	22.3
6	170	1526	173	66	0	80	529	4.02	4.02	4.02	4.02	2	0.08	0.01	0.03	0.00	0.00	22.3
7	170	1575	174	71	0	89	529	4.02	4.02	4.02	4.02	2	0.08	0.01	0.03	0.00	0.00	22.3
8	170	1374	264	95	0	112	479	4.02	4.02	4.02	4.02	2	0.08	0.01	0.05	0.00	0.00	22.3
9	170	1423	265	100	0	120	479	4.02	4.02	4.02	4.02	2	0.08	0.01	0.05	0.00	0.00	22.3
10	170	1722	67	34	0	47	608	4.02	4.02	4.02	4.02	2	0.10	0.00	0.01	0.00	0.00	22.3
11	170	1736	68	35	0	49	608	4.02	4.02	4.02	4.02	2	0.10	0.00	0.01	0.00	0.00	22.3
12	170	1213	370	131	0	151	451	4.02	4.02	4.02	4.02	2	0.07	0.01	0.07	0.00	0.00	22.3
13	170	1227	370	132	0	154	451	4.02	4.02	4.02	4.02	2	0.07	0.01	0.07	0.00	0.00	22.3
14	170	1526	173	66	0	80	529	4.02	4.02	4.02	4.02	2	0.08	0.01	0.03	0.00	0.00	22.3
15	170	1575	174	71	0	89	529	4.02	4.02	4.02	4.02	2	0.08	0.01	0.03	0.00	0.00	22.3
16	170	1374	264	95	0	112	479	4.02	4.02	4.02	4.02	2	0.08	0.01	0.05	0.00	0.00	22.3
17	170	1423	265	100	0	120	479	4.02	4.02	4.02	4.02	2	0.08	0.01	0.05	0.00	0.00	22.3
18	170	4601	-406	90	0	128	1486	4.02	4.02	4.02	4.02	3	0.25	0.01	0.07	0.00	0.00	22.3
19	170	2462	579	349	0	399	533	4.02	4.02	4.02	4.02	3	0.10	0.02	0.10	0.00	0.00	22.3
20	170	3277	115	214	0	262	757	4.02	4.02	4.02	4.02	3	0.12	0.01	0.03	0.00	0.00	22.3
37	170	4786	-669	-33	0	-6	1966	4.02	4.02	4.02	4.02	3	0.33	0.02	0.12	0.00	0.00	22.3
38	170	1221	973	399	0	446	-688	4.02	4.02	4.02	4.02	3	0.11	0.03	0.17	0.00	0.00	22.3
39	170	2579	199	173	0	217	701	4.02	4.02	4.02	4.02	3	0.11	0.01	0.04	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	226	1917	9	108	0	70	655	4.02	4.02	4.02	4.02	3	0.10	0.00	0.00	0.00	0.00	22.3

2	226	1722	-144	34	0	28	608	4.02	4.02	4.02	4.02	2	0.10	0.00	0.03	0.00	0.00	22.3
3	226	1736	-144	35	0	30	608	4.02	4.02	4.02	4.02	2	0.10	0.00	0.03	0.00	0.00	22.3
4	226	1213	158	131	0	78	451	4.02	4.02	4.02	4.02	2	0.07	0.00	0.03	0.00	0.00	22.3
5	226	1227	158	132	0	79	451	4.02	4.02	4.02	4.02	2	0.07	0.00	0.03	0.00	0.00	22.3
6	226	1526	-39	66	0	43	529	4.02	4.02	4.02	4.02	2	0.08	0.00	0.01	0.00	0.00	22.3
7	226	1575	-38	71	0	49	529	4.02	4.02	4.02	4.02	2	0.08	0.00	0.01	0.00	0.00	22.3
8	226	1374	52	95	0	58	479	4.02	4.02	4.02	4.02	2	0.08	0.00	0.01	0.00	0.00	22.3
9	226	1423	53	100	0	64	479	4.02	4.02	4.02	4.02	2	0.08	0.00	0.01	0.00	0.00	22.3
10	226	1722	-144	34	0	28	608	4.02	4.02	4.02	4.02	2	0.10	0.00	0.03	0.00	0.00	22.3
11	226	1736	-144	35	0	30	608	4.02	4.02	4.02	4.02	2	0.10	0.00	0.03	0.00	0.00	22.3
12	226	1213	158	131	0	78	451	4.02	4.02	4.02	4.02	2	0.07	0.00	0.03	0.00	0.00	22.3
13	226	1227	158	132	0	79	451	4.02	4.02	4.02	4.02	2	0.07	0.00	0.03	0.00	0.00	22.3
14	226	1526	-39	66	0	43	529	4.02	4.02	4.02	4.02	2	0.08	0.00	0.01	0.00	0.00	22.3
15	226	1575	-38	71	0	49	529	4.02	4.02	4.02	4.02	2	0.08	0.00	0.01	0.00	0.00	22.3
16	226	1374	52	95	0	58	479	4.02	4.02	4.02	4.02	2	0.08	0.00	0.01	0.00	0.00	22.3
17	226	1423	53	100	0	64	479	4.02	4.02	4.02	4.02	2	0.08	0.00	0.01	0.00	0.00	22.3
18	226	4601	-681	90	0	77	1372	4.02	4.02	4.02	4.02	3	0.23	0.02	0.12	0.00	0.00	22.3
19	226	2462	303	349	0	202	583	4.02	4.02	4.02	4.02	3	0.09	0.01	0.06	0.00	0.00	22.3
20	226	3277	-160	214	0	141	757	4.02	4.02	4.02	4.02	3	0.12	0.01	0.03	0.00	0.00	22.3
37	226	4786	-944	-33	0	13	1650	4.02	4.02	4.02	4.02	3	0.28	0.03	0.17	0.00	0.00	22.3
38	226	1221	697	399	0	220	629	4.02	4.02	4.02	4.02	3	0.09	0.02	0.12	0.00	0.00	22.3
39	226	2579	-76	173	0	120	701	4.02	4.02	4.02	4.02	3	0.11	0.01	0.03	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	283	1917	-266	108	0	9	655	4.02	4.02	4.02	4.02	3	0.10	0.01	0.05	0.00	0.00	22.3
2	283	1722	-356	34	0	8	608	4.02	4.02	4.02	4.02	2	0.10	0.01	0.06	0.00	0.00	22.3
3	283	1736	-356	35	0	10	608	4.02	4.02	4.02	4.02	2	0.10	0.01	0.06	0.00	0.00	22.3
4	283	1213	-54	131	0	4	451	4.02	4.02	4.02	4.02	2	0.07	0.00	0.01	0.00	0.00	22.3
5	283	1227	-54	132	0	5	451	4.02	4.02	4.02	4.02	2	0.07	0.00	0.01	0.00	0.00	22.3
6	283	1526	-251	66	0	5	529	4.02	4.02	4.02	4.02	2	0.08	0.01	0.04	0.00	0.00	22.3
7	283	1575	-250	71	0	9	529	4.02	4.02	4.02	4.02	2	0.08	0.01	0.04	0.00	0.00	22.3
8	283	1374	-160	95	0	4	479	4.02	4.02	4.02	4.02	2	0.08	0.00	0.03	0.00	0.00	22.3
9	283	1423	-159	100	0	8	479	4.02	4.02	4.02	4.02	2	0.08	0.00	0.03	0.00	0.00	22.3
10	283	1722	-356	34	0	8	608	4.02	4.02	4.02	4.02	2	0.10	0.01	0.06	0.00	0.00	22.3
11	283	1736	-356	35	0	10	608	4.02	4.02	4.02	4.02	2	0.10	0.01	0.06	0.00	0.00	22.3
12	283	1213	-54	131	0	4	451	4.02	4.02	4.02	4.02	2	0.07	0.00	0.01	0.00	0.00	22.3
13	283	1227	-54	132	0	5	451	4.02	4.02	4.02	4.02	2	0.07	0.00	0.01	0.00	0.00	22.3
14	283	1526	-251	66	0	5	529	4.02	4.02	4.02	4.02	2	0.08	0.01	0.04	0.00	0.00	22.3
15	283	1575	-250	71	0	9	529	4.02	4.02	4.02	4.02	2	0.08	0.01	0.04	0.00	0.00	22.3
16	283	1374	-160	95	0	4	479	4.02	4.02	4.02	4.02	2	0.08	0.00	0.03	0.00	0.00	22.3
17	283	1423	-159	100	0	8	479	4.02	4.02	4.02	4.02	2	0.08	0.00	0.03	0.00	0.00	22.3
18	283	4601	-957	90	0	26	1049	4.02	4.02	4.02	4.02	3	0.17	0.03	0.17	0.00	0.00	22.3
19	283	2462	28	349	0	4	583	4.02	4.02	4.02	4.02	3	0.09	0.01	0.06	0.00	0.00	22.3
20	283	3277	-436	214	0	21	757	4.02	4.02	4.02	4.02	3	0.12	0.01	0.08	0.00	0.00	22.3
37	283	4786	-1220	-33	0	31	1178	4.02	4.02	4.02	4.02	3	0.20	0.04	0.22	0.00	0.00	22.3
38	283	1221	422	399	0	-5	757	4.02	4.02	4.02	4.02	3	0.11	0.01	0.08	0.00	0.00	22.3
39	283	2579	-352	173	0	22	701	4.02	4.02	4.02	4.02	3	0.11	0.01	0.06	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	339	1917	-541	108	0	-52	629	4.02	4.02	4.02	4.02	3	0.10	0.02	0.10	0.00	0.00	22.3
2	339	1722	-568	34	0	-11	472	4.02	4.02	4.02	4.02	2	0.08	0.02	0.10	0.00	0.00	22.3
3	339	1736	-568	35	0	-10	472	4.02	4.02	4.02	4.02	2	0.08	0.02	0.10	0.00	0.00	22.3
4	339	1213	-265	131	0	-70	451	4.02	4.02	4.02	4.02	2	0.07	0.01	0.05	0.00	0.00	22.3
5	339	1227	-265	132	0	-70	451	4.02	4.02	4.02	4.02	2	0.07	0.01	0.05	0.00	0.00	22.3
6	339	1526	-463	66	0	-32	480	4.02	4.02	4.02	4.02	2	0.08	0.01	0.08	0.00	0.00	22.3
7	339	1575	-461	71	0	-30	481	4.02	4.02	4.02	4.02	2	0.08	0.01	0.08	0.00	0.00	22.3
8	339	1374	-372	95	0	-50	479	4.02	4.02	4.02	4.02	2	0.08	0.01	0.07	0.00	0.00	22.3
9	339	1423	-370	100	0	-48	479	4.02	4.02	4.02	4.02	2	0.08	0.01	0.07	0.00	0.00	22.3
10	339	1722	-568	34	0	-11	472	4.02	4.02	4.02	4.02	2	0.08	0.02	0.10	0.00	0.00	22.3
11	339	1736	-568	35	0	-10	472	4.02	4.02	4.02	4.02	2	0.08	0.02	0.10	0.00	0.00	22.3
12	339	1213	-265	131	0	-70	451	4.02	4.02	4.02	4.02	2	0.07	0.01	0.05	0.00	0.00	22.3
13	339	1227	-265	132	0	-70	451	4.02	4.02	4.02	4.02	2	0.07	0.01	0.05	0.00	0.00	22.3
14	339	1526	-463	66	0	-32	480	4.02	4.02	4.02	4.02	2	0.08	0.01	0.08	0.00	0.00	22.3
15	339	1575	-461	71	0	-30	481	4.02	4.02	4.02	4.02	2	0.08	0.01	0.08	0.00	0.00	22.3
16	339	1374	-372	95	0	-50	479	4.02	4.02	4.02	4.02	2	0.08	0.01	0.07	0.00	0.00	22.3
17	339	1423	-370	100	0	-48	479	4.02	4.02	4.02	4.02	2	0.08	0.01	0.07	0.00	0.00	22.3
18	339	4601	-1232	90	0	-25	-677	4.02	4.02	4.02	4.02	3	0.11	0.04	0.22	0.00	0.00	22.3
19	339	2462	-247	349	0	-193	583	4.02	4.02	4.02	4.02	3	0.09	0.01	0.06	0.00	0.00	22.3
20	339	3277	-711	214	0	-100	612	4.02	4.02	4.02	4.02	3	0.10	0.02	0.13	0.00	0.00	22.3
37	339	4786	-1495	-33	0	50	-963	4.02	4.02	4.02	4.02	3	0.16	0.04	0.27	0.00	0.00	22.3
38	339	1221	146	399	0	-230	757	4.02	4.02	4.02	4.02	3	0.11	0.01	0.06	0.00	0.00	22.3
39	339	2579	-627	173	0	-76	621	4.02	4.02	4.02	4.02	3	0.10	0.02	0.11	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	396	1917	-817	108	0	-113	-443	4.02	4.02	4.02	4.02	3	0.07	0.02	0.15	0.00	0.00	22.3
2	396	1722	-780	34	0	-30	-591	4.02	4.02	4.02	4.02	2	0.09	0.02	0.14	0.00	0.00	22.3
3	396	1736	-779	35	0	-30	-591	4.02	4.02	4.02	4.02	2	0.09	0.02	0.14	0.00	0.00	22.3
4	396	1213	-477	131	0	-144	392	4.02	4.02	4.02	4.02	2	0.06	0.01	0.09	0.00	0.00	22.3
5	396	1227	-477	132	0	-144	393	4.02	4.02	4.02	4.02	2	0.06	0.01	0.09	0.00	0.00	22.3
6	396	1526	-674	66	0	-70	-417	4.02	4.02	4.02	4.02	2	0.07	0.02	0.12	0.00	0.00	22.3
7	396	1575	-673	71	0	-70	-414	4.02	4.02	4.02	4.02	2	0.07	0.02	0.12	0.00	0.00	22.3
8	396	1374	-583	95	0	-104	324	4.02	4.02	4.02	4.02	2	0.05	0.02	0.10	0.00	0.00	22.3
9	396	1423	-582	100	0	-105	326	4.02	4.02	4.02	4.02	2	0.05	0.02	0.10	0.00	0.00	22.3
10	396	1722	-780	34	0	-30	-591	4.02	4.02	4.02	4.02	2	0.09	0.02	0.14	0.00	0.00	22.3
11	396	1736	-779	35	0	-30	-591	4.02	4.02	4.02	4.02	2	0.09	0.02	0.14	0.00	0.00	22.3
12	396	1213	-477	131	0	-144	392	4.02	4.02	4.02	4.02	2	0.06	0.01	0.09	0.00	0.00	22.3
13	396	1227	-477	132	0	-144	393	4.02	4.02	4.02	4.02	2	0.06	0.01	0.09	0.00	0.00	22.3
14	396	1526	-674	66	0	-70	-417	4.02	4.02	4.02	4.02	2	0.07	0.02	0.12	0.00	0.00	22.3
15	396	1575	-673	71	0	-70	-414	4.02	4.02	4.02	4.02	2	0.07	0.02	0.12	0.00	0.00	22.3
16	396	1374	-583	95	0	-104	324	4.02	4.02	4.02	4.02	2	0.05	0.02	0.10	0.00	0.00	22.3
17	396	1423	-582	100	0	-105	326	4.02	4.02	4.02	4.02	2	0.05	0.02	0.10	0.00	0.00	22.3
18	396	4601	-1508	90	0	-75	-1591	4.02	4.02	4.02	4.02	3	0.26	0.04	0.27	0.00	0.00	22.3
19	396	2462	-523	349	0	-390	568	4.02	4.02	4.02	4.02	3	0.10	0.02	0.09	0.00	0.00	22.3
20	396	3277	-987	214	0	-221	-727	4.02	4.02	4.02	4.02	3	0.12	0.03	0.18	0.00	0.00	22.3
37	396	4786	-1771	-33	0	68	-2025	4.02	4.02	4.02	4.02	3	0.34	0.05	0.32	0.00	0.00	22.3
38	396	1221	-129	399	0	-456	757	4.02	4.02	4.02	4.02	3	0.12	0.01	0.06	0.00	0.00	22.3
39	396	2579	-902	173	0	-174	-585	4.02	4.02	4.02	4.02	3	0.09	0.03	0.16	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	452	1917	-1092	108	0	-174	-1121	4.02	4.02	4.02	4.02	3	0.17	0.03	0.19	0.00	0.00	22.3
2	452	1722	-992	34	0	-49	-1199	4.02	4.02	4.02	4.02	2	0.19	0.03	0.18	0.00	0.00	22.3
3	452	1736	-991	35	0	-50	-1198	4.02	4.02	4.02	4.02	2	0.19	0.03	0.18	0.00	0.00	22.3
4	452	1213	-689	131	0	-218	-528	4.02	4.02	4.02	4.02	2	0.08	0.02	0.12	0.00	0.00	22.3
5	452	1227	-689	132	0	-219	-527	4.02	4.02	4.02	4.02	2	0.08	0.02	0.12	0.00	0.00	22.3
6	452	1526	-886	66	0	-107	-965	4.02	4.02	4.02	4.02	2	0.15	0.03	0.16	0.00	0.00	22.3
7	452	1575	-885	71	0	-110	-962	4.02	4.02	4.02	4.02	2	0.15	0.03	0.16	0.00	0.00	22.3

8	452	1374	-795	95	0	-158	-763	4.02	4.02	4.02	4.02	2	0.12	0.02	0.14	0.00	0.00	22.3
9	452	1423	-794	100	0	-161	-760	4.02	4.02	4.02	4.02	2	0.12	0.02	0.14	0.00	0.00	22.3
10	452	1722	-992	34	0	-49	-1199	4.02	4.02	4.02	4.02	2	0.19	0.03	0.18	0.00	0.00	22.3
11	452	1736	-991	35	0	-50	-1198	4.02	4.02	4.02	4.02	2	0.19	0.03	0.18	0.00	0.00	22.3
12	452	1213	-689	131	0	-218	-528	4.02	4.02	4.02	4.02	2	0.08	0.02	0.12	0.00	0.00	22.3
13	452	1227	-689	132	0	-219	-527	4.02	4.02	4.02	4.02	2	0.08	0.02	0.12	0.00	0.00	22.3
14	452	1526	-886	66	0	-107	-965	4.02	4.02	4.02	4.02	2	0.15	0.03	0.16	0.00	0.00	22.3
15	452	1575	-885	71	0	-110	-962	4.02	4.02	4.02	4.02	2	0.15	0.03	0.16	0.00	0.00	22.3
16	452	1374	-795	95	0	-158	-763	4.02	4.02	4.02	4.02	2	0.12	0.02	0.14	0.00	0.00	22.3
17	452	1423	-794	100	0	-161	-760	4.02	4.02	4.02	4.02	2	0.12	0.02	0.14	0.00	0.00	22.3
18	452	4601	-1783	90	0	-126	-2660	4.02	4.02	4.02	4.02	3	0.44	0.05	0.32	0.00	0.00	22.3
19	452	2462	-798	349	0	-587	-474	4.02	4.02	4.02	4.02	3	0.15	0.02	0.14	0.00	0.00	22.3
20	452	3277	-1262	214	0	-341	-1502	4.02	4.02	4.02	4.02	3	0.24	0.04	0.22	0.00	0.00	22.3
37	452	4786	-2046	-33	0	87	-3243	4.02	4.02	4.02	4.02	3	0.54	0.06	0.36	0.00	0.00	22.3
38	452	1221	-405	399	0	-681	757	4.02	4.02	4.02	4.02	3	0.17	0.01	0.07	0.00	0.00	22.3
39	452	2579	-1178	173	0	-271	-1312	4.02	4.02	4.02	4.02	3	0.20	0.03	0.21	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	509	1917	-1368	108	0	-235	-1956	4.02	4.02	4.02	4.02	3	0.30	0.04	0.24	0.00	0.00	22.3
2	509	1722	-1204	34	0	-68	-1927	4.02	4.02	4.02	4.02	2	0.31	0.03	0.21	0.00	0.00	22.3
3	509	1736	-1203	35	0	-70	-1925	4.02	4.02	4.02	4.02	2	0.31	0.03	0.21	0.00	0.00	22.3
4	509	1213	-901	131	0	-292	-1084	4.02	4.02	4.02	4.02	2	0.17	0.03	0.16	0.00	0.00	22.3
5	509	1227	-901	132	0	-293	-1083	4.02	4.02	4.02	4.02	2	0.17	0.03	0.16	0.00	0.00	22.3
6	509	1526	-1098	66	0	-145	-1633	4.02	4.02	4.02	4.02	2	0.26	0.03	0.20	0.00	0.00	22.3
7	509	1575	-1097	71	0	-150	-1629	4.02	4.02	4.02	4.02	2	0.26	0.03	0.20	0.00	0.00	22.3
8	509	1374	-1007	95	0	-212	-1380	4.02	4.02	4.02	4.02	2	0.22	0.03	0.18	0.00	0.00	22.3
9	509	1423	-1006	100	0	-217	-1376	4.02	4.02	4.02	4.02	2	0.22	0.03	0.18	0.00	0.00	22.3
10	509	1722	-1204	34	0	-68	-1927	4.02	4.02	4.02	4.02	2	0.31	0.03	0.21	0.00	0.00	22.3
11	509	1736	-1203	35	0	-70	-1925	4.02	4.02	4.02	4.02	2	0.31	0.03	0.21	0.00	0.00	22.3
12	509	1213	-901	131	0	-292	-1084	4.02	4.02	4.02	4.02	2	0.17	0.03	0.16	0.00	0.00	22.3
13	509	1227	-901	132	0	-293	-1083	4.02	4.02	4.02	4.02	2	0.17	0.03	0.16	0.00	0.00	22.3
14	509	1526	-1098	66	0	-145	-1633	4.02	4.02	4.02	4.02	2	0.26	0.03	0.20	0.00	0.00	22.3
15	509	1575	-1097	71	0	-150	-1629	4.02	4.02	4.02	4.02	2	0.26	0.03	0.20	0.00	0.00	22.3
16	509	1374	-1007	95	0	-212	-1380	4.02	4.02	4.02	4.02	2	0.22	0.03	0.18	0.00	0.00	22.3
17	509	1423	-1006	100	0	-217	-1376	4.02	4.02	4.02	4.02	2	0.22	0.03	0.18	0.00	0.00	22.3
18	509	4601	-2059	90	0	-177	-3884	4.02	4.02	4.02	4.02	3	0.64	0.06	0.37	0.00	0.00	22.3
19	509	2462	-1074	349	0	-785	-1142	4.02	4.02	4.02	4.02	3	0.21	0.03	0.19	0.00	0.00	22.3
20	509	3277	-1538	214	0	-462	-2432	4.02	4.02	4.02	4.02	3	0.39	0.04	0.27	0.00	0.00	22.3
37	509	4786	-2322	-33	0	106	-4616	4.02	4.02	4.02	4.02	3	0.77	0.07	0.41	0.00	0.00	22.3
38	509	1221	-680	399	0	-907	644	4.02	4.02	4.02	4.02	3	0.23	0.02	0.12	0.00	0.00	22.3
39	509	2579	-1454	173	0	-369	-2195	4.02	4.02	4.02	4.02	3	0.34	0.04	0.26	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	565	1917	-1643	108	0	-296	-2114	4.02	4.02	4.02	4.02	3	0.32	0.05	0.29	0.00	0.00	22.3
2	565	1722	-1416	34	0	-88	-2057	4.02	4.02	4.02	4.02	2	0.33	0.04	0.25	0.00	0.00	22.3
3	565	1736	-1415	35	0	-90	-2056	4.02	4.02	4.02	4.02	2	0.33	0.04	0.25	0.00	0.00	22.3
4	565	1213	-1113	131	0	-365	-1197	4.02	4.02	4.02	4.02	2	0.19	0.03	0.20	0.00	0.00	22.3
5	565	1227	-1113	132	0	-368	-1196	4.02	4.02	4.02	4.02	2	0.19	0.03	0.20	0.00	0.00	22.3
6	565	1526	-1310	66	0	-182	-1757	4.02	4.02	4.02	4.02	2	0.28	0.04	0.23	0.00	0.00	22.3
7	565	1575	-1309	71	0	-190	-1753	4.02	4.02	4.02	4.02	2	0.28	0.04	0.23	0.00	0.00	22.3
8	565	1374	-1219	95	0	-266	-1499	4.02	4.02	4.02	4.02	2	0.24	0.04	0.22	0.00	0.00	22.3
9	565	1423	-1218	100	0	-273	-1495	4.02	4.02	4.02	4.02	2	0.24	0.04	0.22	0.00	0.00	22.3
10	565	1722	-1416	34	0	-88	-2057	4.02	4.02	4.02	4.02	2	0.33	0.04	0.25	0.00	0.00	22.3
11	565	1736	-1415	35	0	-90	-2056	4.02	4.02	4.02	4.02	2	0.33	0.04	0.25	0.00	0.00	22.3
12	565	1213	-1113	131	0	-365	-1197	4.02	4.02	4.02	4.02	2	0.19	0.03	0.20	0.00	0.00	22.3
13	565	1227	-1113	132	0	-368	-1196	4.02	4.02	4.02	4.02	2	0.19	0.03	0.20	0.00	0.00	22.3
14	565	1526	-1310	66	0	-182	-1757	4.02	4.02	4.02	4.02	2	0.28	0.04	0.23	0.00	0.00	22.3
15	565	1575	-1309	71	0	-190	-1753	4.02	4.02	4.02	4.02	2	0.28	0.04	0.23	0.00	0.00	22.3
16	565	1374	-1219	95	0	-266	-1499	4.02	4.02	4.02	4.02	2	0.24	0.04	0.22	0.00	0.00	22.3
17	565	1423	-1218	100	0	-273	-1495	4.02	4.02	4.02	4.02	2	0.24	0.04	0.22	0.00	0.00	22.3
18	565	4601	-2334	90	0	-228	-4083	4.02	4.02	4.02	4.02	3	0.68	0.07	0.42	0.00	0.00	22.3
19	565	2462	-1349	349	0	-982	-1283	4.02	4.02	4.02	4.02	3	0.26	0.04	0.24	0.00	0.00	22.3
20	565	3277	-1813	214	0	-583	-2600	4.02	4.02	4.02	4.02	3	0.41	0.05	0.32	0.00	0.00	22.3
37	565	4786	-2597	-33	0	124	-4830	4.02	4.02	4.02	4.02	3	0.81	0.08	0.46	0.00	0.00	22.3
38	565	1221	-956	399	0	-1132	-162	4.02	4.02	4.02	4.02	3	0.29	0.03	0.17	0.00	0.00	22.3
39	565	2579	-1729	173	0	-467	-2358	4.02	4.02	4.02	4.02	3	0.37	0.05	0.31	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

Nome travata: **trave_501_IP1** Descrizione: **Trave_5 11-16-21-26**
ASTA NUM. 3 NI 185 NF 167 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y qy tot.
qy medio: 375.00 375.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	3340	1281	326	0	657	-1011	4.02	4.02	4.02	4.02	3	0.18	0.04	0.23	0.00	0.00	22.3
2	0	2958	815	242	0	434	-337	4.02	4.02	4.02	4.02	2	0.13	0.02	0.15	0.00	0.00	22.3
3	0	2989	812	252	0	460	-329	4.02	4.02	4.02	4.02	2	0.14	0.02	0.14	0.00	0.00	22.3
4	0	2148	1159	249	0	550	-1227	4.02	4.02	4.02	4.02	2	0.20	0.03	0.21	0.00	0.00	22.3
5	0	2180	1155	259	0	576	-1219	4.02	4.02	4.02	4.02	2	0.20	0.03	0.21	0.00	0.00	22.3
6	0	2638	940	233	0	444	-658	4.02	4.02	4.02	4.02	2	0.13	0.03	0.17	0.00	0.00	22.3
7	0	2743	928	266	0	531	-631	4.02	4.02	4.02	4.02	2	0.16	0.03	0.17	0.00	0.00	22.3
8	0	2395	1043	235	0	479	-924	4.02	4.02	4.02	4.02	2	0.15	0.03	0.19	0.00	0.00	22.3
9	0	2500	1031	268	0	566	-898	4.02	4.02	4.02	4.02	2	0.17	0.03	0.18	0.00	0.00	22.3
10	0	2958	815	242	0	434	-337	4.02	4.02	4.02	4.02	2	0.13	0.02	0.15	0.00	0.00	22.3
11	0	2989	812	252	0	460	-329	4.02	4.02	4.02	4.02	2	0.14	0.02	0.14	0.00	0.00	22.3
12	0	2148	1159	249	0	550	-1227	4.02	4.02	4.02	4.02	2	0.20	0.03	0.21	0.00	0.00	22.3
13	0	2180	1155	259	0	576	-1219	4.02	4.02	4.02	4.02	2	0.20	0.03	0.21	0.00	0.00	22.3
14	0	2638	940	233	0	444	-658	4.02	4.02	4.02	4.02	2	0.13	0.03	0.17	0.00	0.00	22.3
15	0	2743	928	266	0	531	-631	4.02	4.02	4.02	4.02	2	0.16	0.03	0.17	0.00	0.00	22.3
16	0	2395	1043	235	0	479	-924	4.02	4.02	4.02	4.02	2	0.15	0.03	0.19	0.00	0.00	22.3
17	0	2500	1031	268	0	566	-898	4.02	4.02	4.02	4.02	2	0.17	0.03	0.18	0.00	0.00	22.3
18	0	8113	470	678	0	1225	1226	4.02	4.02	4.02	4.02	3	0.38	0.02	0.11	0.00	0.00	22.3
19	0	4623	1601	603	0	1387	-1914	4.02	4.02	4.02	4.02	3	0.39	0.05	0.29	0.00	0.00	22.3
20	0	6006	1065	647	0	1353	-522	4.02	4.02	4.02	4.02	3	0.40	0.03	0.19	0.00	0.00	22.3
37	0	8286	174	601	0	960	1815	4.02	4.02	4.02	4.02	3	0.34	0.02	0.10	0.00	0.00	22.3
38	0	2470	2059	475	0	1230	-3071	4.02	4.02	4.02	4.02	3	0.47	0.06	0.37	0.00	0.00	22.3
39	0	4775	1165	548	0	1172	-752	4.02	4.02	4.02	4.02	3	0.33	0.03	0.21	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	56	3340	1006	326	0	473	-874	4.02	4.02	4.02	4.02	3	0.14	0.03	0.18	0.00	0.00	22.3
2	56	2958	603	242	0	297	369	4.02	4.02	4.02	4.02	2	0.09	0.02	0.11	0.00	0.00	22.3
3	56	2989	600	252	0	318	373	4.02	4.02	4.02	4.02	2	0.10	0.02	0.11	0.00	0.00	22.3
4	56	2148	947	249	0	409	-1112	4.02	4.02	4.02	4.02	2	0.18	0.03	0.17	0.00	0.00	22.3
5	56	2180	943	259	0	430	-1104	4.02	4.02	4.02	4.02	2	0.18	0.03	0.17	0.00	0.00	22.3
6	56	2638	728	233	0	312	-555	4.02	4.02	4.02	4.02	2	0.09	0.02	0.13	0.00	0.00	22.3
7	56	2743	716	266	0	381	-529	4.02	4.02	4.02	4.02	2	0.12	0.02	0.13	0.00	0.00	22.3
8	56	2395	831	235	0	346	-816	4.02	4.02	4.02	4.02	2	0.13	0.02	0.15	0.00	0.00	22.3
9	56	2500	819	268	0	415	-790	4.02	4.02	4.02	4.02	2	0.13	0.02	0.15	0.00	0.00	22.3
10	56	2958	603	242	0	297	369	4.02	4.02	4.02	4.02	2	0.09	0.02	0.11	0.00	0.00	22.3
11	56	2989	600	252	0	318	373	4.02	4.02	4.02	4.02	2	0.10	0.02	0.11	0.00	0.00	22.3
12	56	2148	947	249	0	409	-1112	4.02	4.02	4.02	4.02	2	0.18	0.03	0.17	0.00	0.00	22.3
13	56	2180	943	259	0	430	-1104	4.02	4.02	4.02	4.02	2	0.18	0.03	0.17	0.00	0.00	22.3
14	56	2638	728	233	0	312	-555	4.02	4.02	4.02	4.02	2	0.09	0.02	0.13	0.00	0.00	22.3
15	56	2743	716	266	0	381	-529	4.02	4.02	4.02	4.02	2	0.12	0.02	0.13	0.00	0.00	22.3
16	56	2395	831	235	0	346	-816	4.02	4.02	4.02	4.02	2	0.13	0.02	0.15	0.00	0.00	22.3
17	56	2500	819	268	0	415	-790	4.02	4.02	4.02	4.02	2	0.13	0.02	0.15	0.00	0.00	22.3
18	56	8113	195	678	0	842	1226	4.02	4.02	4.02	4.02	3	0.26	0.02	0.11	0.00	0.00	22.3
19	56	4623	1326	603	0	1046	-1758	4.02	4.02	4.02	4.02	3	0.29	0.04	0.24	0.00	0.00	22.3
20	56	6006	790	647	0	988	401	4.02	4.02	4.02	4.02	3	0.29	0.02	0.14	0.00	0.00	22.3
37	56	8286	-101	601	0	620	1815	4.02	4.02	4.02	4.02	3	0.34	0.02	0.10	0.00	0.00	22.3
38	56	2470	1784	475	0	962	-2889	4.02	4.02	4.02	4.02	3	0.45	0.05	0.32	0.00	0.00	22.3
39	56	4775	890	548	0	862	-622	4.02	4.02	4.02	4.02	3	0.24	0.03	0.16	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	113	3340	730	326	0	288	494	4.02	4.02	4.02	4.02	3	0.08	0.02	0.13	0.00	0.00	22.3
2	113	2958	391	242	0	161	543	4.02	4.02	4.02	4.02	2	0.09	0.01	0.07	0.00	0.00	22.3
3	113	2989	388	252	0	176	545	4.02	4.02	4.02	4.02	2	0.09	0.01	0.07	0.00	0.00	22.3
4	113	2148	735	249	0	268	-529	4.02	4.02	4.02	4.02	2	0.09	0.02	0.13	0.00	0.00	22.3
5	113	2180	731	259	0	283	-523	4.02	4.02	4.02	4.02	2	0.08	0.02	0.13	0.00	0.00	22.3
6	113	2638	516	233	0	181	426	4.02	4.02	4.02	4.02	2	0.07	0.01	0.09	0.00	0.00	22.3
7	113	2743	504	266	0	231	433	4.02	4.02	4.02	4.02	2	0.07	0.01	0.09	0.00	0.00	22.3
8	113	2395	619	235	0	213	328	4.02	4.02	4.02	4.02	2	0.06	0.02	0.11	0.00	0.00	22.3
9	113	2500	607	268	0	263	335	4.02	4.02	4.02	4.02	2	0.08	0.02	0.11	0.00	0.00	22.3
10	113	2958	391	242	0	161	543	4.02	4.02	4.02	4.02	2	0.09	0.01	0.07	0.00	0.00	22.3
11	113	2989	388	252	0	176	545	4.02	4.02	4.02	4.02	2	0.09	0.01	0.07	0.00	0.00	22.3
12	113	2148	735	249	0	268	-529	4.02	4.02	4.02	4.02	2	0.09	0.02	0.13	0.00	0.00	22.3
13	113	2180	731	259	0	283	-523	4.02	4.02	4.02	4.02	2	0.08	0.02	0.13	0.00	0.00	22.3
14	113	2638	516	233	0	181	426	4.02	4.02	4.02	4.02	2	0.07	0.01	0.09	0.00	0.00	22.3
15	113	2743	504	266	0	231	433	4.02	4.02	4.02	4.02	2	0.07	0.01	0.09	0.00	0.00	22.3
16	113	2395	619	235	0	213	328	4.02	4.02	4.02	4.02	2	0.06	0.02	0.11	0.00	0.00	22.3
17	113	2500	607	268	0	263	335	4.02	4.02	4.02	4.02	2	0.08	0.02	0.11	0.00	0.00	22.3
18	113	8113	-81	678	0	458	1226	4.02	4.02	4.02	4.02	3	0.23	0.02	0.11	0.00	0.00	22.3
19	113	4623	1050	603	0	706	-948	4.02	4.02	4.02	4.02	3	0.20	0.03	0.19	0.00	0.00	22.3
20	113	6006	514	647	0	622	630	4.02	4.02	4.02	4.02	3	0.18	0.02	0.10	0.00	0.00	22.3
37	113	8286	-377	601	0	281	1815	4.02	4.02	4.02	4.02	3	0.34	0.02	0.10	0.00	0.00	22.3
38	113	2470	1508	475	0	693	-1819	4.02	4.02	4.02	4.02	3	0.28	0.04	0.27	0.00	0.00	22.3
39	113	4775	614	548	0	553	564	4.02	4.02	4.02	4.02	3	0.16	0.02	0.11	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	169	3340	455	326	0	104	661	4.02	4.02	4.02	4.02	3	0.11	0.01	0.08	0.00	0.00	22.3
2	169	2958	179	242	0	24	548	4.02	4.02	4.02	4.02	2	0.09	0.01	0.04	0.00	0.00	22.3
3	169	2989	176	252	0	33	547	4.02	4.02	4.02	4.02	2	0.09	0.01	0.04	0.00	0.00	22.3
4	169	2148	523	249	0	127	463	4.02	4.02	4.02	4.02	2	0.08	0.02	0.09	0.00	0.00	22.3
5	169	2180	519	259	0	137	463	4.02	4.02	4.02	4.02	2	0.08	0.02	0.09	0.00	0.00	22.3
6	169	2638	304	233	0	50	508	4.02	4.02	4.02	4.02	2	0.08	0.01	0.05	0.00	0.00	22.3
7	169	2743	292	266	0	80	508	4.02	4.02	4.02	4.02	2	0.08	0.01	0.05	0.00	0.00	22.3
8	169	2395	407	235	0	81	510	4.02	4.02	4.02	4.02	2	0.08	0.01	0.07	0.00	0.00	22.3
9	169	2500	395	268	0	111	510	4.02	4.02	4.02	4.02	2	0.08	0.01	0.07	0.00	0.00	22.3
10	169	2958	179	242	0	24	548	4.02	4.02	4.02	4.02	2	0.09	0.01	0.04	0.00	0.00	22.3
11	169	2989	176	252	0	33	547	4.02	4.02	4.02	4.02	2	0.09	0.01	0.04	0.00	0.00	22.3
12	169	2148	523	249	0	127	463	4.02	4.02	4.02	4.02	2	0.08	0.02	0.09	0.00	0.00	22.3
13	169	2180	519	259	0	137	463	4.02	4.02	4.02	4.02	2	0.08	0.02	0.09	0.00	0.00	22.3
14	169	2638	304	233	0	50	508	4.02	4.02	4.02	4.02	2	0.08	0.01	0.05	0.00	0.00	22.3
15	169	2743	292	266	0	80	508	4.02	4.02	4.02	4.02	2	0.08	0.01	0.05	0.00	0.00	22.3
16	169	2395	407	235	0	81	510	4.02	4.02	4.02	4.02	2	0.08	0.01	0.07	0.00	0.00	22.3
17	169	2500	395	268	0	111	510	4.02	4.02	4.02	4.02	2	0.08	0.01	0.07	0.00	0.00	22.3
18	169	8113	-356	678	0	75	1226	4.02	4.02	4.02	4.02	3	0.23	0.02	0.11	0.00	0.00	22.3
19	169	4623	775	603	0	365	492	4.02	4.02	4.02	4.02	3	0.10	0.02	0.14	0.00	0.00	22.3
20	169	6006	239	647	0	257	639	4.02	4.02	4.02	4.02	3	0.11	0.02	0.10	0.00	0.00	22.3
37	169	8286	-652	601	0	-59	1720	4.02	4.02	4.02	4.02	3	0.33	0.02	0.12	0.00	0.00	22.3
38	169	2470	1233	475	0	425	-906	4.02	4.02	4.02	4.02	3	0.14	0.04	0.22	0.00	0.00	22.3
39	169	4775	339	548	0	243	636	4.02	4.02	4.02	4.02	3	0.11	0.02	0.09	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	226	3340	179	326	0	-80	661	4.02	4.02	4.02	4.02	3	0.11	0.01	0.05	0.00	0.00	22.3
2	226	2958	-33	242	0	-112	548	4.02	4.02	4.02	4.02	2	0.09	0.01	0.04	0.00	0.00	22.3
3	226	2989	-36	252	0	-109	547	4.02	4.02	4.02	4.02	2	0.09	0.01	0.04	0.00	0.00	22.3
4	226	2148	311	249	0	-14	550	4.02	4.02	4.02	4.02	2	0.09	0.01	0.06	0.00	0.00	22.3
5	226	2180	308	259	0	-10	548	4.02	4.02	4.02	4.02	2	0.09	0.01	0.05	0.00	0.00	22.3
6	226	2638	92	233	0	-82	508	4.02	4.02	4.02	4.02	2	0.08	0.01	0.04	0.00	0.00	22.3
7	226	2743	80	266	0	-70	508	4.02	4.02	4.02	4.02	2	0.08	0.01	0.04	0.00	0.00	22.3
8	226	2395	195	235	0	-52	525	4.02	4.02	4.02	4.02	2	0.09	0.01	0.04	0.00	0.00	22.3
9	226	2500	183	268	0	-41	517	4.02	4.02	4.02	4.02	2	0.08	0.01	0.04	0.00	0.00	22.3
10	226	2958	-33	242	0	-112	548	4.02	4.02	4.02	4.02	2	0.09	0.01	0.04	0.00	0.00	22.3
11	226	2989	-36	252	0	-109	547	4.02	4.02	4.02	4.02	2	0.09	0.01	0.04	0.00	0.00	22.3
12	226	2148	311	249	0	-14	550	4.02	4.02	4.02	4.02	2	0.09	0.01	0.06	0.00	0.00	22.3
13	226	2180	308	259	0	-10	548	4.02	4.02	4.02	4.02	2	0.09	0.01	0.05	0.00	0.00	22.3
14	226	2638	92	233	0	-82	508	4.02	4.02	4.02	4.02	2	0.08	0.01	0.04	0.00	0.00	22.3
15	226	2743	80	266	0	-70	508	4.02	4.02	4.02	4.02	2	0.08	0.01	0.04	0.00	0.00	22.3
16	226	2395	195	235	0	-52	525	4.02	4.02	4.02	4.02	2	0.09	0.01	0.04	0.00	0.00	22.3
17	226	2500	183	268	0	-41	517	4.02	4.02	4.02	4.02	2	0.08	0.01	0.04	0.00	0.00	22.3
18	226	8113	-632	678	0	-308	1143	4.02	4.02	4.02	4.02	3	0.22	0.02	0.11	0.00	0.00	22.3
19	226	4623	499	603	0	25	712	4.02	4.02	4.02	4.02	3	0.12	0.02	0.10	0.00	0.00	22.3
20	226	6006	-37	647	0	-109	639	4.02	4.02	4.02	4.02	3	0.11	0.02	0.10	0.00	0.00	22.3
37	226	8286	-928	601	0	-399	1413	4.02	4.02	4.02	4.02	3	0.27	0.03	0.17	0.00	0.00	22.3
38	226	2470	957	475	0	156	821	4.02	4.02	4.02	4.02	3	0.13	0.03	0.17	0.00	0.00	22.3
39	226	4775	63	548	0	-66	636	4.02	4.02	4.02	4.02	3	0.11	0.02	0.09	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	282	3340	-96	326	0	-264	661	4.02	4.02	4.02	4.02	3	0.11	0.01	0.05	0.00	0.00	22.3
2	282	2958	-244	242	0	-249	548	4.02	4.02	4.02	4.02	2	0.09	0.01	0.04	0.00	0.00	22.3
3	282	2989	-248	252	0	-251	547	4.02	4.02	4.02	4.02	2	0.09	0.01	0.04	0.00	0.00	22.3
4	282	2148	100	249	0	-154	550	4.02	4.02	4.02	4.02	2	0.09	0.01	0.04	0.00	0.00	22.3
5	282	2180	96	259	0	-157	548	4.02	4.02	4.02	4.02	2	0.09	0.01	0.04	0.00	0.00	22.3

6	282	2638	-120	233	0	-213	508	4.02	4.02	4.02	4.02	2	0.08	0.01	0.04	0.00	0.00	22.3
7	282	2743	-132	266	0	-221	508	4.02	4.02	4.02	4.02	2	0.08	0.01	0.04	0.00	0.00	22.3
8	282	2395	-16	235	0	-185	525	4.02	4.02	4.02	4.02	2	0.09	0.01	0.04	0.00	0.00	22.3
9	282	2500	-28	268	0	-192	517	4.02	4.02	4.02	4.02	2	0.08	0.01	0.04	0.00	0.00	22.3
10	282	2958	-244	242	0	-249	548	4.02	4.02	4.02	4.02	2	0.09	0.01	0.04	0.00	0.00	22.3
11	282	2989	-248	252	0	-251	547	4.02	4.02	4.02	4.02	2	0.09	0.01	0.04	0.00	0.00	22.3
12	282	2148	100	249	0	-154	550	4.02	4.02	4.02	4.02	2	0.09	0.01	0.04	0.00	0.00	22.3
13	282	2180	96	259	0	-157	548	4.02	4.02	4.02	4.02	2	0.09	0.01	0.04	0.00	0.00	22.3
14	282	2638	-120	233	0	-213	508	4.02	4.02	4.02	4.02	2	0.08	0.01	0.04	0.00	0.00	22.3
15	282	2743	-132	266	0	-221	508	4.02	4.02	4.02	4.02	2	0.08	0.01	0.04	0.00	0.00	22.3
16	282	2395	-16	235	0	-185	525	4.02	4.02	4.02	4.02	2	0.09	0.01	0.04	0.00	0.00	22.3
17	282	2500	-28	268	0	-192	517	4.02	4.02	4.02	4.02	2	0.08	0.01	0.04	0.00	0.00	22.3
18	282	8113	-907	678	0	-692	848	4.02	4.02	4.02	4.02	3	0.22	0.03	0.16	0.00	0.00	22.3
19	282	4623	224	603	0	-316	712	4.02	4.02	4.02	4.02	3	0.12	0.02	0.10	0.00	0.00	22.3
20	282	6006	-312	647	0	-474	639	4.02	4.02	4.02	4.02	3	0.14	0.02	0.10	0.00	0.00	22.3
37	282	8286	-1203	601	0	-738	950	4.02	4.02	4.02	4.02	3	0.23	0.03	0.21	0.00	0.00	22.3
38	282	2470	682	475	0	-112	1145	4.02	4.02	4.02	4.02	3	0.18	0.02	0.12	0.00	0.00	22.3
39	282	4775	-212	548	0	-376	636	4.02	4.02	4.02	4.02	3	0.11	0.02	0.09	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	339	3340	-372	326	0	-448	661	4.02	4.02	4.02	4.02	3	0.12	0.01	0.07	0.00	0.00	22.3
2	339	2958	-456	242	0	-385	503	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
3	339	2989	-460	252	0	-393	500	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
4	339	2148	-112	249	0	-295	550	4.02	4.02	4.02	4.02	2	0.09	0.01	0.04	0.00	0.00	22.3
5	339	2180	-116	259	0	-303	548	4.02	4.02	4.02	4.02	2	0.09	0.01	0.04	0.00	0.00	22.3
6	339	2638	-332	233	0	-345	508	4.02	4.02	4.02	4.02	2	0.10	0.01	0.06	0.00	0.00	22.3
7	339	2743	-344	266	0	-371	508	4.02	4.02	4.02	4.02	2	0.11	0.01	0.06	0.00	0.00	22.3
8	339	2395	-228	235	0	-318	525	4.02	4.02	4.02	4.02	2	0.09	0.01	0.04	0.00	0.00	22.3
9	339	2500	-240	268	0	-344	517	4.02	4.02	4.02	4.02	2	0.10	0.01	0.04	0.00	0.00	22.3
10	339	2958	-456	242	0	-385	503	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
11	339	2989	-460	252	0	-393	500	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
12	339	2148	-112	249	0	-295	550	4.02	4.02	4.02	4.02	2	0.09	0.01	0.04	0.00	0.00	22.3
13	339	2180	-116	259	0	-303	548	4.02	4.02	4.02	4.02	2	0.09	0.01	0.04	0.00	0.00	22.3
14	339	2638	-332	233	0	-345	508	4.02	4.02	4.02	4.02	2	0.10	0.01	0.06	0.00	0.00	22.3
15	339	2743	-344	266	0	-371	508	4.02	4.02	4.02	4.02	2	0.11	0.01	0.06	0.00	0.00	22.3
16	339	2395	-228	235	0	-318	525	4.02	4.02	4.02	4.02	2	0.09	0.01	0.04	0.00	0.00	22.3
17	339	2500	-240	268	0	-344	517	4.02	4.02	4.02	4.02	2	0.10	0.01	0.04	0.00	0.00	22.3
18	339	8113	-1182	678	0	-1075	-800	4.02	4.02	4.02	4.02	3	0.34	0.03	0.21	0.00	0.00	22.3
19	339	4623	-51	603	0	-657	712	4.02	4.02	4.02	4.02	3	0.18	0.02	0.10	0.00	0.00	22.3
20	339	6006	-588	647	0	-839	583	4.02	4.02	4.02	4.02	3	0.25	0.02	0.10	0.00	0.00	22.3
37	339	8286	-1478	601	0	-1078	-1165	4.02	4.02	4.02	4.02	3	0.34	0.04	0.26	0.00	0.00	22.3
38	339	2470	406	475	0	-380	1258	4.02	4.02	4.02	4.02	3	0.19	0.01	0.08	0.00	0.00	22.3
39	339	4775	-487	548	0	-686	636	4.02	4.02	4.02	4.02	3	0.19	0.02	0.09	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	395	3340	-647	326	0	-632	569	4.02	4.02	4.02	4.02	3	0.17	0.02	0.12	0.00	0.00	22.3
2	395	2958	-668	242	0	-522	-384	4.02	4.02	4.02	4.02	2	0.16	0.02	0.12	0.00	0.00	22.3
3	395	2989	-671	252	0	-536	-392	4.02	4.02	4.02	4.02	2	0.16	0.02	0.12	0.00	0.00	22.3
4	395	2148	-324	249	0	-436	550	4.02	4.02	4.02	4.02	2	0.13	0.01	0.06	0.00	0.00	22.3
5	395	2180	-328	259	0	-450	548	4.02	4.02	4.02	4.02	2	0.13	0.01	0.06	0.00	0.00	22.3
6	395	2638	-543	233	0	-476	400	4.02	4.02	4.02	4.02	2	0.14	0.02	0.10	0.00	0.00	22.3
7	395	2743	-555	266	0	-522	386	4.02	4.02	4.02	4.02	2	0.16	0.02	0.10	0.00	0.00	22.3
8	395	2395	-440	235	0	-450	489	4.02	4.02	4.02	4.02	2	0.13	0.01	0.08	0.00	0.00	22.3
9	395	2500	-452	269	0	-496	474	4.02	4.02	4.02	4.02	2	0.15	0.01	0.08	0.00	0.00	22.3
10	395	2958	-668	242	0	-522	-384	4.02	4.02	4.02	4.02	2	0.16	0.02	0.12	0.00	0.00	22.3
11	395	2989	-671	252	0	-536	-392	4.02	4.02	4.02	4.02	2	0.16	0.02	0.12	0.00	0.00	22.3
12	395	2148	-324	249	0	-436	550	4.02	4.02	4.02	4.02	2	0.13	0.01	0.06	0.00	0.00	22.3
13	395	2180	-328	259	0	-450	548	4.02	4.02	4.02	4.02	2	0.13	0.01	0.06	0.00	0.00	22.3
14	395	2638	-543	233	0	-476	400	4.02	4.02	4.02	4.02	2	0.14	0.02	0.10	0.00	0.00	22.3
15	395	2743	-555	266	0	-522	386	4.02	4.02	4.02	4.02	2	0.16	0.02	0.10	0.00	0.00	22.3
16	395	2395	-440	235	0	-450	489	4.02	4.02	4.02	4.02	2	0.13	0.01	0.08	0.00	0.00	22.3
17	395	2500	-452	269	0	-496	474	4.02	4.02	4.02	4.02	2	0.15	0.01	0.08	0.00	0.00	22.3
18	395	8113	-1458	678	0	-1458	-1685	4.02	4.02	4.02	4.02	3	0.46	0.04	0.26	0.00	0.00	22.3
19	395	4623	-327	603	0	-997	712	4.02	4.02	4.02	4.02	3	0.28	0.02	0.10	0.00	0.00	22.3
20	395	6006	-863	647	0	-1205	-561	4.02	4.02	4.02	4.02	3	0.35	0.03	0.15	0.00	0.00	22.3
37	395	8286	-1754	601	0	-1417	-2217	4.02	4.02	4.02	4.02	3	0.45	0.05	0.31	0.00	0.00	22.3
38	395	2470	131	475	0	-649	1258	4.02	4.02	4.02	4.02	3	0.19	0.01	0.08	0.00	0.00	22.3
39	395	4775	-763	548	0	-995	429	4.02	4.02	4.02	4.02	3	0.28	0.02	0.14	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	452	3340	-923	326	0	-816	-670	4.02	4.02	4.02	4.02	3	0.22	0.03	0.16	0.00	0.00	22.3
2	452	2958	-880	242	0	-658	-929	4.02	4.02	4.02	4.02	2	0.20	0.03	0.16	0.00	0.00	22.3
3	452	2989	-883	252	0	-678	-939	4.02	4.02	4.02	4.02	2	0.21	0.03	0.16	0.00	0.00	22.3
4	452	2148	-536	249	0	-577	452	4.02	4.02	4.02	4.02	2	0.17	0.02	0.10	0.00	0.00	22.3
5	452	2180	-540	259	0	-596	445	4.02	4.02	4.02	4.02	2	0.18	0.02	0.10	0.00	0.00	22.3
6	452	2638	-755	233	0	-607	-624	4.02	4.02	4.02	4.02	2	0.18	0.02	0.13	0.00	0.00	22.3
7	452	2743	-767	266	0	-672	-657	4.02	4.02	4.02	4.02	2	0.20	0.02	0.14	0.00	0.00	22.3
8	452	2395	-652	235	0	-583	-373	4.02	4.02	4.02	4.02	2	0.17	0.02	0.12	0.00	0.00	22.3
9	452	2500	-664	268	0	-648	-406	4.02	4.02	4.02	4.02	2	0.19	0.02	0.12	0.00	0.00	22.3
10	452	2958	-880	242	0	-658	-929	4.02	4.02	4.02	4.02	2	0.20	0.03	0.16	0.00	0.00	22.3
11	452	2989	-883	252	0	-678	-939	4.02	4.02	4.02	4.02	2	0.21	0.03	0.16	0.00	0.00	22.3
12	452	2148	-536	249	0	-577	452	4.02	4.02	4.02	4.02	2	0.17	0.02	0.10	0.00	0.00	22.3
13	452	2180	-540	259	0	-596	445	4.02	4.02	4.02	4.02	2	0.18	0.02	0.10	0.00	0.00	22.3
14	452	2638	-755	233	0	-607	-624	4.02	4.02	4.02	4.02	2	0.18	0.02	0.13	0.00	0.00	22.3
15	452	2743	-767	266	0	-672	-657	4.02	4.02	4.02	4.02	2	0.20	0.02	0.14	0.00	0.00	22.3
16	452	2395	-652	235	0	-583	-373	4.02	4.02	4.02	4.02	2	0.17	0.02	0.12	0.00	0.00	22.3
17	452	2500	-664	268	0	-648	-406	4.02	4.02	4.02	4.02	2	0.19	0.02	0.12	0.00	0.00	22.3
18	452	8113	-1733	678	0	-1841	-2726	4.02	4.02	4.02	4.02	3	0.58	0.05	0.31	0.00	0.00	22.3
19	452	4623	-602	603	0	-1338	647	4.02	4.02	4.02	4.02	3	0.37	0.02	0.11	0.00	0.00	22.3
20	452	6006	-1139	647	0	-1570	-1267	4.02	4.02	4.02	4.02	3	0.46	0.03	0.20	0.00	0.00	22.3
37	452	8286	-2029	601	0	-1757	-3426	4.02	4.02	4.02	4.02	3	0.65	0.06	0.36	0.00	0.00	22.3
38	452	2470	-145	475	0	-917	1258	4.02	4.02	4.02	4.02	3	0.24	0.01	0.08	0.00	0.00	22.3
39	452	4775	-1038	548	0	-1305	-992	4.02	4.02	4.02	4.02	3	0.37	0.03	0.18	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	508	3340	-1198	326	0	-1000	-1409	4.02	4.02	4.02	4.02	3	0.27	0.03	0.21	0.00	0.00	22.3
2	508	2958	-1092	242	0	-795	-1593	4.02	4.02	4.02	4.02	2	0.27	0.03	0.19	0.00	0.00	22.3
3	508	2989	-1095	252	0	-820	-1605	4.02	4.02	4.02	4.02	2	0.27	0.03	0.20	0.00	0.00	22.3
4	508	2148	-748	249	0	-718	-561	4.02	4.02	4.02	4.02	2	0.21	0.02	0.13	0.00	0.00	22.3
5	508	2180	-752	259	0	-743	-573	4.02	4.02	4.02	4.02	2	0.22	0.02	0.13	0.00	0.00	22.3
6	508	2638	-967	233	0	-739	-1218	4.02	4.02	4.02	4.02	2	0.22	0.03	0.17	0.00	0.00	22.3
7	508	2743	-979	266	0	-822	-1258	4.02	4.02	4.02	4.02	2	0.25	0.03	0.17	0.00	0.00	22.3
8	508	2395	-864	235	0	-716	-908	4.02	4.02	4.02	4.02	2	0.21	0.03	0.15	0.00	0.00	22.3
9	508	2500	-876	268	0	-799	-949	4.02	4.02	4.02	4.02	2	0.24	0.03	0.16	0.00	0.00	22.3
10	508	2958	-1092	242	0	-795	-1593	4.02	4.02	4.02	4.02	2	0.27	0.03	0.19	0.00	0.00	22.3
11	508	2989	-1095	252	0	-820	-1605	4.02	4.02	4.02	4.02	2	0.27	0.03	0.20	0.00	0.00	22.3

12	508	2148	-748	249	0	-718	-561	4.02	4.02	4.02	4.02	2	0.21	0.02	0.13	0.00	0.00	22.3
13	508	2180	-752	259	0	-743	-573	4.02	4.02	4.02	4.02	2	0.22	0.02	0.13	0.00	0.00	22.3
14	508	2638	-967	233	0	-739	-1218	4.02	4.02	4.02	4.02	2	0.22	0.03	0.17	0.00	0.00	22.3
15	508	2743	-979	266	0	-822	-1258	4.02	4.02	4.02	4.02	2	0.25	0.03	0.17	0.00	0.00	22.3
16	508	2395	-864	235	0	-716	-908	4.02	4.02	4.02	4.02	2	0.21	0.03	0.15	0.00	0.00	22.3
17	508	2500	-876	268	0	-799	-949	4.02	4.02	4.02	4.02	2	0.24	0.03	0.16	0.00	0.00	22.3
18	508	8113	-2009	678	0	-2225	-3923	4.02	4.02	4.02	4.02	3	0.74	0.06	0.36	0.00	0.00	22.3
19	508	4623	-878	603	0	-1678	-520	4.02	4.02	4.02	4.02	3	0.47	0.03	0.16	0.00	0.00	22.3
20	508	6006	-1414	647	0	-1936	-2127	4.02	4.02	4.02	4.02	3	0.57	0.04	0.25	0.00	0.00	22.3
37	508	8286	-2305	601	0	-2096	-4790	4.02	4.02	4.02	4.02	3	0.91	0.07	0.41	0.00	0.00	22.3
38	508	2470	-420	475	0	-1186	1258	4.02	4.02	4.02	4.02	3	0.31	0.01	0.08	0.00	0.00	22.3
39	508	4775	-1314	548	0	-1614	-1796	4.02	4.02	4.02	4.02	3	0.45	0.04	0.23	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	565	3340	-1474	326	0	-1184	-1557	4.02	4.02	4.02	4.02	3	0.32	0.04	0.26	0.00	0.00	22.3
2	565	2958	-1304	242	0	-932	-1717	4.02	4.02	4.02	4.02	2	0.29	0.04	0.23	0.00	0.00	22.3
3	565	2989	-1307	252	0	-962	-1729	4.02	4.02	4.02	4.02	2	0.29	0.04	0.23	0.00	0.00	22.3
4	565	2148	-960	249	0	-859	-665	4.02	4.02	4.02	4.02	2	0.25	0.03	0.17	0.00	0.00	22.3
5	565	2180	-964	259	0	-890	-677	4.02	4.02	4.02	4.02	2	0.26	0.03	0.17	0.00	0.00	22.3
6	565	2638	-1179	233	0	-870	-1335	4.02	4.02	4.02	4.02	2	0.26	0.03	0.21	0.00	0.00	22.3
7	565	2743	-1191	266	0	-973	-1375	4.02	4.02	4.02	4.02	2	0.29	0.03	0.21	0.00	0.00	22.3
8	565	2395	-1076	235	0	-848	-1019	4.02	4.02	4.02	4.02	2	0.25	0.03	0.19	0.00	0.00	22.3
9	565	2500	-1088	268	0	-951	-1060	4.02	4.02	4.02	4.02	2	0.29	0.03	0.19	0.00	0.00	22.3
10	565	2958	-1304	242	0	-932	-1717	4.02	4.02	4.02	4.02	2	0.29	0.04	0.23	0.00	0.00	22.3
11	565	2989	-1307	252	0	-962	-1729	4.02	4.02	4.02	4.02	2	0.29	0.04	0.23	0.00	0.00	22.3
12	565	2148	-960	249	0	-859	-665	4.02	4.02	4.02	4.02	2	0.25	0.03	0.17	0.00	0.00	22.3
13	565	2180	-964	259	0	-890	-677	4.02	4.02	4.02	4.02	2	0.26	0.03	0.17	0.00	0.00	22.3
14	565	2638	-1179	233	0	-870	-1335	4.02	4.02	4.02	4.02	2	0.26	0.03	0.21	0.00	0.00	22.3
15	565	2743	-1191	266	0	-973	-1375	4.02	4.02	4.02	4.02	2	0.29	0.03	0.21	0.00	0.00	22.3
16	565	2395	-1076	235	0	-848	-1019	4.02	4.02	4.02	4.02	2	0.25	0.03	0.19	0.00	0.00	22.3
17	565	2500	-1088	268	0	-951	-1060	4.02	4.02	4.02	4.02	2	0.29	0.03	0.19	0.00	0.00	22.3
18	565	8113	-2284	678	0	-2608	-4119	4.02	4.02	4.02	4.02	3	0.82	0.07	0.41	0.00	0.00	22.3
19	565	4623	-1153	603	0	-2019	-650	4.02	4.02	4.02	4.02	3	0.57	0.03	0.21	0.00	0.00	22.3
20	565	6006	-1690	647	0	-2301	-2288	4.02	4.02	4.02	4.02	3	0.67	0.05	0.30	0.00	0.00	22.3
37	565	8286	-2580	601	0	-2436	-5003	4.02	4.02	4.02	4.02	3	0.95	0.07	0.46	0.00	0.00	22.3
38	565	2470	-696	475	0	-1454	1132	4.02	4.02	4.02	4.02	3	0.38	0.02	0.12	0.00	0.00	22.3
39	565	4775	-1589	548	0	-1924	-1951	4.02	4.02	4.02	4.02	3	0.54	0.05	0.28	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

Nome travata: **trave_502_IP1** Descrizione: **Trave_5 10-15-20-25**
ASTA NUM. 4 NI 294 NF 296 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y Permanente qy tot.
qy medio: 375.00 308.00 683.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	--												Fx,M	Bielle	V,Mx			
	cm	daN			daN*m			cmq								cmq/m		cm
1	0	113	2511	87	0	273	-2294	4.02	4.02	4.02	4.02	3	0.33	0.07	0.45	0.00	0.00	22.3
2	0	-117	1621	61	0	197	-847	4.02	4.02	4.02	4.02	2	0.13	0.05	0.29	0.00	0.00	22.3
3	0	-109	1622	61	0	196	-852	4.02	4.02	4.02	4.02	2	0.13	0.05	0.29	0.00	0.00	22.3
4	0	283	2240	73	0	224	-2677	4.02	4.02	4.02	4.02	2	0.41	0.06	0.40	0.00	0.00	22.3
5	0	291	2242	73	0	224	-2683	4.02	4.02	4.02	4.02	2	0.41	0.07	0.40	0.00	0.00	22.3
6	0	13	1835	66	0	207	-1481	4.02	4.02	4.02	4.02	2	0.22	0.05	0.33	0.00	0.00	22.3
7	0	40	1841	65	0	205	-1499	4.02	4.02	4.02	4.02	2	0.23	0.05	0.33	0.00	0.00	22.3
8	0	133	2021	69	0	216	-2030	4.02	4.02	4.02	4.02	2	0.31	0.06	0.36	0.00	0.00	22.3
9	0	160	2027	68	0	213	-2048	4.02	4.02	4.02	4.02	2	0.31	0.06	0.36	0.00	0.00	22.3
10	0	-117	1621	61	0	197	-847	4.02	4.02	4.02	4.02	2	0.13	0.05	0.29	0.00	0.00	22.3
11	0	-109	1622	61	0	196	-852	4.02	4.02	4.02	4.02	2	0.13	0.05	0.29	0.00	0.00	22.3
12	0	283	2240	73	0	224	-2677	4.02	4.02	4.02	4.02	2	0.41	0.06	0.40	0.00	0.00	22.3
13	0	291	2242	73	0	224	-2683	4.02	4.02	4.02	4.02	2	0.41	0.07	0.40	0.00	0.00	22.3
14	0	13	1835	66	0	207	-1481	4.02	4.02	4.02	4.02	2	0.22	0.05	0.33	0.00	0.00	22.3
15	0	40	1841	65	0	205	-1499	4.02	4.02	4.02	4.02	2	0.23	0.05	0.33	0.00	0.00	22.3
16	0	133	2021	69	0	216	-2030	4.02	4.02	4.02	4.02	2	0.31	0.06	0.36	0.00	0.00	22.3
17	0	160	2027	68	0	213	-2048	4.02	4.02	4.02	4.02	2	0.31	0.06	0.36	0.00	0.00	22.3
18	0	-638	1688	176	0	576	1029	4.02	4.02	4.02	4.02	3	0.14	0.05	0.30	0.00	0.00	22.3
19	0	1201	3466	179	0	548	-5135	4.02	4.02	4.02	4.02	3	0.76	0.10	0.62	0.00	0.00	22.3
20	0	311	2567	160	0	518	-2452	4.02	4.02	4.02	4.02	3	0.35	0.07	0.46	0.00	0.00	22.3
37	0	-1302	1071	145	0	490	2554	4.02	4.02	4.02	4.02	3	0.35	0.03	0.18	0.00	0.00	22.3
38	0	1764	4035	151	0	445	-6838	4.02	4.02	4.02	6.03	3	0.69	0.12	0.63	0.00	0.00	22.3
39	0	281	2536	119	0	394	-2367	4.02	4.02	4.02	4.02	3	0.34	0.07	0.45	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= 2.01 (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	56	113	2009	87	0	224	-2034	4.02	4.02	4.02	4.02	3	0.29	0.06	0.36	0.00	0.00	22.3
2	56	-117	1235	61	0	162	-665	4.02	4.02	4.02	4.02	2	0.10	0.04	0.22	0.00	0.00	22.3
3	56	-109	1236	61	0	161	-670	4.02	4.02	4.02	4.02	2	0.10	0.04	0.22	0.00	0.00	22.3
4	56	283	1854	73	0	183	-2459	4.02	4.02	4.02	4.02	2	0.38	0.05	0.33	0.00	0.00	22.3
5	56	291	1856	73	0	182	-2465	4.02	4.02	4.02	4.02	2	0.38	0.05	0.33	0.00	0.00	22.3
6	56	13	1449	66	0	170	-1287	4.02	4.02	4.02	4.02	2	0.20	0.04	0.26	0.00	0.00	22.3
7	56	40	1455	65	0	168	-1304	4.02	4.02	4.02	4.02	2	0.20	0.04	0.26	0.00	0.00	22.3
8	56	133	1635	69	0	177	-1825	4.02	4.02	4.02	4.02	2	0.28	0.05	0.29	0.00	0.00	22.3
9	56	160	1641	68	0	174	-1843	4.02	4.02	4.02	4.02	2	0.28	0.05	0.29	0.00	0.00	22.3
10	56	-117	1235	61	0	162	-665	4.02	4.02	4.02	4.02	2	0.10	0.04	0.22	0.00	0.00	22.3
11	56	-109	1236	61	0	161	-670	4.02	4.02	4.02	4.02	2	0.10	0.04	0.22	0.00	0.00	22.3
12	56	283	1854	73	0	183	-2459	4.02	4.02	4.02	4.02	2	0.38	0.05	0.33	0.00	0.00	22.3
13	56	291	1856	73	0	182	-2465	4.02	4.02	4.02	4.02	2	0.38	0.05	0.33	0.00	0.00	22.3
14	56	13	1449	66	0	170	-1287	4.02	4.02	4.02	4.02	2	0.20	0.04	0.26	0.00	0.00	22.3
15	56	40	1455	65	0	168	-1304	4.02	4.02	4.02	4.02	2	0.20	0.04	0.26	0.00	0.00	22.3
16	56	133	1635	69	0	177	-1825	4.02	4.02	4.02	4.02	2	0.28	0.05	0.29	0.00	0.00	22.3
17	56	160	1641	68	0	174	-1843	4.02	4.02	4.02	4.02	2	0.28	0.05	0.29	0.00	0.00	22.3
18	56	-638	1186	176	0	476	1587	4.02	4.02	4.02	4.02	3	0.22	0.03	0.21	0.00	0.00	22.3
19	56	1201	2964	179	0	447	-4819	4.02	4.02	4.02	4.02	3	0.72	0.09	0.53	0.00	0.00	22.3
20	56	311	2065	160	0	427	-2189	4.02	4.02	4.02	4.02	3	0.32	0.06	0.37	0.00	0.00	22.3
37	56	-1302	569	145	0	408	2655	4.02	4.02	4.02	4.02	3	0.37	0.02	0.10	0.00	0.00	22.3
38	56	1764	3533	151	0	360	-6489	4.02	4.02	4.02	4.02	3	0.98	0.10	0.63	0.00	0.00	22.3
39	56	281	2034	119	0	327	-2106	4.02	4.02	4.02	4.02	3	0.30	0.06	0.36	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	113	113	1508	87	0	175	-787	4.02	4.02	4.02	4.02	3	0.11	0.04	0.27	0.00	0.00	22.3
2	113	-117	849	61	0	127	979	4.02	4.02	4.02	4.02	2	0.15	0.02	0.15	0.00	0.00	22.3
3	113	-109	850	61	0	127	976	4.02	4.02	4.02	4.02	2	0.15	0.02	0.15	0.00	0.00	22.3

4	113	283	1468	73	0	142	-1325	4.02	4.02	4.02	4.02	2	0.20	0.04	0.26	0.00	0.00	22.3
5	113	291	1470	73	0	141	-1330	4.02	4.02	4.02	4.02	2	0.20	0.04	0.26	0.00	0.00	22.3
6	113	13	1063	66	0	133	695	4.02	4.02	4.02	4.02	2	0.11	0.03	0.19	0.00	0.00	22.3
7	113	40	1069	65	0	131	687	4.02	4.02	4.02	4.02	2	0.10	0.03	0.19	0.00	0.00	22.3
8	113	133	1249	69	0	138	-815	4.02	4.02	4.02	4.02	2	0.12	0.04	0.22	0.00	0.00	22.3
9	113	160	1255	68	0	136	-829	4.02	4.02	4.02	4.02	2	0.13	0.04	0.22	0.00	0.00	22.3
10	113	-117	849	61	0	127	979	4.02	4.02	4.02	4.02	2	0.15	0.02	0.15	0.00	0.00	22.3
11	113	-109	850	61	0	127	976	4.02	4.02	4.02	4.02	2	0.15	0.02	0.15	0.00	0.00	22.3
12	113	283	1468	73	0	142	-1325	4.02	4.02	4.02	4.02	2	0.20	0.04	0.26	0.00	0.00	22.3
13	113	291	1470	73	0	141	-1330	4.02	4.02	4.02	4.02	2	0.20	0.04	0.26	0.00	0.00	22.3
14	113	13	1063	66	0	133	695	4.02	4.02	4.02	4.02	2	0.11	0.03	0.19	0.00	0.00	22.3
15	113	40	1069	65	0	131	687	4.02	4.02	4.02	4.02	2	0.10	0.03	0.19	0.00	0.00	22.3
16	113	133	1249	69	0	138	-815	4.02	4.02	4.02	4.02	2	0.12	0.04	0.22	0.00	0.00	22.3
17	113	160	1255	68	0	136	-829	4.02	4.02	4.02	4.02	2	0.13	0.04	0.22	0.00	0.00	22.3
18	113	-638	685	176	0	377	1760	4.02	4.02	4.02	4.02	3	0.25	0.02	0.12	0.00	0.00	22.3
19	113	1201	2463	179	0	346	-3032	4.02	4.02	4.02	4.02	3	0.45	0.07	0.44	0.00	0.00	22.3
20	113	311	1564	160	0	337	-910	4.02	4.02	4.02	4.02	3	0.13	0.05	0.28	0.00	0.00	22.3
37	113	-1302	68	145	0	326	2655	4.02	4.02	4.02	4.02	3	0.37	0.00	0.01	0.00	0.00	22.3
38	113	1764	3032	151	0	275	-4380	4.02	4.02	4.02	4.02	3	0.66	0.09	0.54	0.00	0.00	22.3
39	113	281	1533	119	0	259	-844	4.02	4.02	4.02	4.02	3	0.12	0.04	0.27	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	170	113	1006	87	0	126	1195	4.02	4.02	4.02	4.02	3	0.17	0.03	0.18	0.00	0.00	22.3
2	170	-117	463	61	0	93	1072	4.02	4.02	4.02	4.02	2	0.16	0.01	0.08	0.00	0.00	22.3
3	170	-109	464	61	0	92	1070	4.02	4.02	4.02	4.02	2	0.16	0.01	0.08	0.00	0.00	22.3
4	170	283	1082	73	0	101	686	4.02	4.02	4.02	4.02	2	0.10	0.03	0.19	0.00	0.00	22.3
5	170	291	1084	73	0	100	684	4.02	4.02	4.02	4.02	2	0.10	0.03	0.19	0.00	0.00	22.3
6	170	13	677	66	0	96	979	4.02	4.02	4.02	4.02	2	0.15	0.02	0.12	0.00	0.00	22.3
7	170	40	683	65	0	95	977	4.02	4.02	4.02	4.02	2	0.15	0.02	0.12	0.00	0.00	22.3
8	170	133	863	69	0	98	852	4.02	4.02	4.02	4.02	2	0.13	0.03	0.15	0.00	0.00	22.3
9	170	160	869	68	0	97	846	4.02	4.02	4.02	4.02	2	0.13	0.03	0.15	0.00	0.00	22.3
10	170	-117	463	61	0	93	1072	4.02	4.02	4.02	4.02	2	0.16	0.01	0.08	0.00	0.00	22.3
11	170	-109	464	61	0	92	1070	4.02	4.02	4.02	4.02	2	0.16	0.01	0.08	0.00	0.00	22.3
12	170	283	1082	73	0	101	686	4.02	4.02	4.02	4.02	2	0.10	0.03	0.19	0.00	0.00	22.3
13	170	291	1084	73	0	100	684	4.02	4.02	4.02	4.02	2	0.10	0.03	0.19	0.00	0.00	22.3
14	170	13	677	66	0	96	979	4.02	4.02	4.02	4.02	2	0.15	0.02	0.12	0.00	0.00	22.3
15	170	40	683	65	0	95	977	4.02	4.02	4.02	4.02	2	0.15	0.02	0.12	0.00	0.00	22.3
16	170	133	863	69	0	98	852	4.02	4.02	4.02	4.02	2	0.13	0.03	0.15	0.00	0.00	22.3
17	170	160	869	68	0	97	846	4.02	4.02	4.02	4.02	2	0.13	0.03	0.15	0.00	0.00	22.3
18	170	-638	183	176	0	277	1760	4.02	4.02	4.02	4.02	3	0.25	0.01	0.03	0.00	0.00	22.3
19	170	1201	1961	179	0	245	-1528	4.02	4.02	4.02	4.02	3	0.23	0.06	0.35	0.00	0.00	22.3
20	170	311	1062	160	0	246	1161	4.02	4.02	4.02	4.02	3	0.17	0.03	0.19	0.00	0.00	22.3
37	170	-1302	-434	145	0	244	2655	4.02	4.02	4.02	4.02	3	0.37	0.01	0.07	0.00	0.00	22.3
38	170	1764	2530	151	0	189	-2555	4.02	4.02	4.02	4.02	3	0.39	0.07	0.45	0.00	0.00	22.3
39	170	281	1031	119	0	192	1179	4.02	4.02	4.02	4.02	3	0.17	0.03	0.18	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	226	113	504	87	0	76	1255	4.02	4.02	4.02	4.02	3	0.18	0.01	0.09	0.00	0.00	22.3
2	226	-117	77	61	0	58	1072	4.02	4.02	4.02	4.02	2	0.16	0.00	0.01	0.00	0.00	22.3
3	226	-109	78	61	0	58	1070	4.02	4.02	4.02	4.02	2	0.16	0.00	0.01	0.00	0.00	22.3
4	226	283	696	73	0	59	992	4.02	4.02	4.02	4.02	2	0.15	0.02	0.12	0.00	0.00	22.3
5	226	291	698	73	0	59	992	4.02	4.02	4.02	4.02	2	0.15	0.02	0.12	0.00	0.00	22.3
6	226	13	291	66	0	59	979	4.02	4.02	4.02	4.02	2	0.15	0.01	0.05	0.00	0.00	22.3
7	226	40	297	65	0	58	977	4.02	4.02	4.02	4.02	2	0.15	0.01	0.05	0.00	0.00	22.3
8	226	133	477	69	0	59	954	4.02	4.02	4.02	4.02	2	0.15	0.01	0.09	0.00	0.00	22.3
9	226	160	483	68	0	58	952	4.02	4.02	4.02	4.02	2	0.15	0.01	0.09	0.00	0.00	22.3
10	226	-117	77	61	0	58	1072	4.02	4.02	4.02	4.02	2	0.16	0.00	0.01	0.00	0.00	22.3
11	226	-109	78	61	0	58	1070	4.02	4.02	4.02	4.02	2	0.16	0.00	0.01	0.00	0.00	22.3
12	226	283	696	73	0	59	992	4.02	4.02	4.02	4.02	2	0.15	0.02	0.12	0.00	0.00	22.3
13	226	291	698	73	0	59	992	4.02	4.02	4.02	4.02	2	0.15	0.02	0.12	0.00	0.00	22.3
14	226	13	291	66	0	59	979	4.02	4.02	4.02	4.02	2	0.15	0.01	0.05	0.00	0.00	22.3
15	226	40	297	65	0	58	977	4.02	4.02	4.02	4.02	2	0.15	0.01	0.05	0.00	0.00	22.3
16	226	133	477	69	0	59	954	4.02	4.02	4.02	4.02	2	0.15	0.01	0.09	0.00	0.00	22.3
17	226	160	483	68	0	58	952	4.02	4.02	4.02	4.02	2	0.15	0.01	0.09	0.00	0.00	22.3
18	226	-638	-319	176	0	178	1760	4.02	4.02	4.02	4.02	3	0.25	0.01	0.06	0.00	0.00	22.3
19	226	1201	1460	179	0	143	1170	4.02	4.02	4.02	4.02	3	0.17	0.04	0.26	0.00	0.00	22.3
20	226	311	560	160	0	155	1257	4.02	4.02	4.02	4.02	3	0.18	0.02	0.10	0.00	0.00	22.3
37	226	-1302	-936	145	0	162	2639	4.02	4.02	4.02	4.02	3	0.36	0.03	0.16	0.00	0.00	22.3
38	226	1764	2028	151	0	104	1041	4.02	4.02	4.02	4.02	3	0.16	0.06	0.36	0.00	0.00	22.3
39	226	281	530	119	0	125	1255	4.02	4.02	4.02	4.02	3	0.18	0.02	0.09	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	282	113	2	87	0	27	1255	4.02	4.02	4.02	4.02	3	0.18	0.00	0.00	0.00	0.00	22.3
2	282	-117	-308	61	0	24	1072	4.02	4.02	4.02	4.02	2	0.16	0.01	0.05	0.00	0.00	22.3
3	282	-109	-308	61	0	24	1070	4.02	4.02	4.02	4.02	2	0.16	0.01	0.05	0.00	0.00	22.3
4	282	283	310	73	0	18	992	4.02	4.02	4.02	4.02	2	0.15	0.01	0.06	0.00	0.00	22.3
5	282	291	312	73	0	18	992	4.02	4.02	4.02	4.02	2	0.15	0.01	0.06	0.00	0.00	22.3
6	282	13	-94	66	0	22	979	4.02	4.02	4.02	4.02	2	0.15	0.00	0.02	0.00	0.00	22.3
7	282	40	-88	65	0	21	977	4.02	4.02	4.02	4.02	2	0.15	0.00	0.02	0.00	0.00	22.3
8	282	133	92	69	0	20	954	4.02	4.02	4.02	4.02	2	0.15	0.00	0.02	0.00	0.00	22.3
9	282	160	98	68	0	20	952	4.02	4.02	4.02	4.02	2	0.15	0.00	0.02	0.00	0.00	22.3
10	282	-117	-308	61	0	24	1072	4.02	4.02	4.02	4.02	2	0.16	0.01	0.05	0.00	0.00	22.3
11	282	-109	-308	61	0	24	1070	4.02	4.02	4.02	4.02	2	0.16	0.01	0.05	0.00	0.00	22.3
12	282	283	310	73	0	18	992	4.02	4.02	4.02	4.02	2	0.15	0.01	0.06	0.00	0.00	22.3
13	282	291	312	73	0	18	992	4.02	4.02	4.02	4.02	2	0.15	0.01	0.06	0.00	0.00	22.3
14	282	13	-94	66	0	22	979	4.02	4.02	4.02	4.02	2	0.15	0.00	0.02	0.00	0.00	22.3
15	282	40	-88	65	0	21	977	4.02	4.02	4.02	4.02	2	0.15	0.00	0.02	0.00	0.00	22.3
16	282	133	92	69	0	20	954	4.02	4.02	4.02	4.02	2	0.15	0.00	0.02	0.00	0.00	22.3
17	282	160	98	68	0	20	952	4.02	4.02	4.02	4.02	2	0.15	0.00	0.02	0.00	0.00	22.3
18	282	-638	-820	176	0	78	1760	4.02	4.02	4.02	4.02	3	0.25	0.02	0.14	0.00	0.00	22.3
19	282	1201	958	179	0	42	1600	4.02	4.02	4.02	4.02	3	0.24	0.03	0.17	0.00	0.00	22.3
20	282	311	58	160	0	65	1257	4.02	4.02	4.02	4.02	3	0.18	0.01	0.03	0.00	0.00	22.3
37	282	-1302	-1438	145	0	80	2222	4.02	4.02	4.02	4.02	3	0.31	0.04	0.25	0.00	0.00	22.3
38	282	1764	1527	151	0	19	1791	4.02	4.02	4.02	4.02	3	0.27	0.04	0.27	0.00	0.00	22.3
39	282	281	28	119	0	57	1255	4.02	4.02	4.02	4.02	3	0.18	0.00	0.00	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	339	113	-499	87	0	-22	1255	4.02	4.02	4.02	4.02	3	0.18	0.01	0.09	0.00	0.00	22.3
2	339	-117	-694	61	0	-11	1072	4.02	4.02	4.02	4.02	2	0.16	0.02	0.12	0.00	0.00	22.3
3	339	-109	-693	61	0	-11	1070	4.02	4.02	4.02	4.02	2	0.16	0.02	0.12	0.00	0.00	22.3
4	339	283	-75	73	0	-23	992	4.02	4.02	4.02	4.02	2	0.15	0.00	0.01	0.00	0.00	22.3
5	339	291	-73	73	0	-23	992	4.02	4.02	4.02	4.02	2	0.15	0.00	0.01	0.00	0.00	22.3
6	339	13	-480	66	0	-15	979	4.02	4.02	4.02	4.02	2	0.15	0.01	0.09	0.00	0.00	22.3
7	339	40	-474	65	0	-15	977	4.02	4.02	4.02	4.02	2	0.15	0.01	0.08	0.00	0.00	22.3
8	339	133	-294	69	0	-19	954	4.02	4.02	4.02	4.02	2	0.15	0.01	0.05	0.00	0.00	22.3
9	339	160	-288	68	0	-19	952	4.02	4.02	4.02	4.02	2	0.15	0.01	0.05	0.00	0.00	22.3

10	339	-117	-694	61	0	-11	1072	4.02	4.02	4.02	4.02	2	0.16	0.02	0.12	0.00	0.00	22.3
11	339	-109	-693	61	0	-11	1070	4.02	4.02	4.02	4.02	2	0.16	0.02	0.12	0.00	0.00	22.3
12	339	283	-75	73	0	-23	992	4.02	4.02	4.02	4.02	2	0.15	0.00	0.01	0.00	0.00	22.3
13	339	291	-73	73	0	-23	992	4.02	4.02	4.02	4.02	2	0.15	0.00	0.01	0.00	0.00	22.3
14	339	13	-480	66	0	-15	979	4.02	4.02	4.02	4.02	2	0.15	0.01	0.09	0.00	0.00	22.3
15	339	40	-474	65	0	-15	977	4.02	4.02	4.02	4.02	2	0.15	0.01	0.08	0.00	0.00	22.3
16	339	133	-294	69	0	-19	954	4.02	4.02	4.02	4.02	2	0.15	0.01	0.05	0.00	0.00	22.3
17	339	160	-288	68	0	-19	952	4.02	4.02	4.02	4.02	2	0.15	0.01	0.05	0.00	0.00	22.3
18	339	-638	-1322	176	0	-21	1464	4.02	4.02	4.02	4.02	3	0.21	0.04	0.23	0.00	0.00	22.3
19	339	1201	456	179	0	-59	1630	4.02	4.02	4.02	4.02	3	0.24	0.01	0.08	0.00	0.00	22.3
20	339	311	-443	160	0	-26	1257	4.02	4.02	4.02	4.02	3	0.18	0.01	0.08	0.00	0.00	22.3
37	339	-1302	-1939	145	0	-3	1522	4.02	4.02	4.02	4.02	3	0.21	0.06	0.33	0.00	0.00	22.3
38	339	1764	1025	151	0	-66	2258	4.02	4.02	4.02	4.02	3	0.34	0.03	0.18	0.00	0.00	22.3
39	339	281	-474	119	0	-10	1255	4.02	4.02	4.02	4.02	3	0.18	0.01	0.08	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	396	113	-1001	87	0	-71	1198	4.02	4.02	4.02	4.02	3	0.17	0.03	0.18	0.00	0.00	22.3
2	396	-117	-1080	61	0	-45	769	4.02	4.02	4.02	4.02	2	0.12	0.03	0.19	0.00	0.00	22.3
3	396	-109	-1079	61	0	-45	769	4.02	4.02	4.02	4.02	2	0.12	0.03	0.19	0.00	0.00	22.3
4	396	283	-461	73	0	-64	992	4.02	4.02	4.02	4.02	2	0.15	0.01	0.08	0.00	0.00	22.3
5	396	291	-459	73	0	-64	992	4.02	4.02	4.02	4.02	2	0.15	0.01	0.08	0.00	0.00	22.3
6	396	13	-866	66	0	-52	875	4.02	4.02	4.02	4.02	2	0.13	0.03	0.15	0.00	0.00	22.3
7	396	40	-860	65	0	-52	877	4.02	4.02	4.02	4.02	2	0.13	0.02	0.15	0.00	0.00	22.3
8	396	133	-680	69	0	-58	954	4.02	4.02	4.02	4.02	2	0.15	0.02	0.12	0.00	0.00	22.3
9	396	160	-674	68	0	-58	952	4.02	4.02	4.02	4.02	2	0.15	0.02	0.12	0.00	0.00	22.3
10	396	-117	-1080	61	0	-45	769	4.02	4.02	4.02	4.02	2	0.12	0.03	0.19	0.00	0.00	22.3
11	396	-109	-1079	61	0	-45	769	4.02	4.02	4.02	4.02	2	0.12	0.03	0.19	0.00	0.00	22.3
12	396	283	-461	73	0	-64	992	4.02	4.02	4.02	4.02	2	0.15	0.01	0.08	0.00	0.00	22.3
13	396	291	-459	73	0	-64	992	4.02	4.02	4.02	4.02	2	0.15	0.01	0.08	0.00	0.00	22.3
14	396	13	-866	66	0	-52	875	4.02	4.02	4.02	4.02	2	0.13	0.03	0.15	0.00	0.00	22.3
15	396	40	-860	65	0	-52	877	4.02	4.02	4.02	4.02	2	0.13	0.02	0.15	0.00	0.00	22.3
16	396	133	-680	69	0	-58	954	4.02	4.02	4.02	4.02	2	0.15	0.02	0.12	0.00	0.00	22.3
17	396	160	-674	68	0	-58	952	4.02	4.02	4.02	4.02	2	0.15	0.02	0.12	0.00	0.00	22.3
18	396	-638	-1824	176	0	-121	-1018	4.02	4.02	4.02	4.02	3	0.14	0.05	0.32	0.00	0.00	22.3
19	396	1201	-45	179	0	-161	1630	4.02	4.02	4.02	4.02	3	0.24	0.01	0.03	0.00	0.00	22.3
20	396	311	-945	160	0	-116	1235	4.02	4.02	4.02	4.02	3	0.18	0.03	0.17	0.00	0.00	22.3
37	396	-1302	-2441	145	0	-85	-1932	4.02	4.02	4.02	4.02	3	0.27	0.07	0.42	0.00	0.00	22.3
38	396	1764	524	151	0	-151	2331	4.02	4.02	4.02	4.02	3	0.35	0.02	0.09	0.00	0.00	22.3
39	396	281	-975	119	0	-77	1214	4.02	4.02	4.02	4.02	3	0.18	0.03	0.17	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	452	113	-1503	87	0	-120	-777	4.02	4.02	4.02	4.02	3	0.11	0.04	0.27	0.00	0.00	22.3
2	452	-117	-1466	61	0	-80	-1240	4.02	4.02	4.02	4.02	2	0.19	0.04	0.26	0.00	0.00	22.3
3	452	-109	-1465	61	0	-80	-1238	4.02	4.02	4.02	4.02	2	0.19	0.04	0.26	0.00	0.00	22.3
4	452	283	-847	73	0	-105	899	4.02	4.02	4.02	4.02	2	0.14	0.02	0.15	0.00	0.00	22.3
5	452	291	-845	73	0	-105	900	4.02	4.02	4.02	4.02	2	0.14	0.02	0.15	0.00	0.00	22.3
6	452	13	-1252	66	0	-89	-795	4.02	4.02	4.02	4.02	2	0.12	0.04	0.22	0.00	0.00	22.3
7	452	40	-1246	65	0	-89	-785	4.02	4.02	4.02	4.02	2	0.12	0.04	0.22	0.00	0.00	22.3
8	452	133	-1066	69	0	-97	668	4.02	4.02	4.02	4.02	2	0.10	0.03	0.19	0.00	0.00	22.3
9	452	160	-1060	68	0	-96	673	4.02	4.02	4.02	4.02	2	0.10	0.03	0.19	0.00	0.00	22.3
10	452	-117	-1466	61	0	-80	-1240	4.02	4.02	4.02	4.02	2	0.19	0.04	0.26	0.00	0.00	22.3
11	452	-109	-1465	61	0	-80	-1238	4.02	4.02	4.02	4.02	2	0.19	0.04	0.26	0.00	0.00	22.3
12	452	283	-847	73	0	-105	899	4.02	4.02	4.02	4.02	2	0.14	0.02	0.15	0.00	0.00	22.3
13	452	291	-845	73	0	-105	900	4.02	4.02	4.02	4.02	2	0.14	0.02	0.15	0.00	0.00	22.3
14	452	13	-1252	66	0	-89	-795	4.02	4.02	4.02	4.02	2	0.12	0.04	0.22	0.00	0.00	22.3
15	452	40	-1246	65	0	-89	-785	4.02	4.02	4.02	4.02	2	0.12	0.04	0.22	0.00	0.00	22.3
16	452	133	-1066	69	0	-97	668	4.02	4.02	4.02	4.02	2	0.10	0.03	0.19	0.00	0.00	22.3
17	452	160	-1060	68	0	-96	673	4.02	4.02	4.02	4.02	2	0.10	0.03	0.19	0.00	0.00	22.3
18	452	-638	-2326	176	0	-220	-2444	4.02	4.02	4.02	4.02	3	0.34	0.07	0.41	0.00	0.00	22.3
19	452	1201	-547	179	0	-262	1630	4.02	4.02	4.02	4.02	3	0.24	0.02	0.10	0.00	0.00	22.3
20	452	311	-1447	160	0	-207	813	4.02	4.02	4.02	4.02	3	0.12	0.04	0.26	0.00	0.00	22.3
37	452	-1302	-2943	145	0	-167	-3707	4.02	4.02	4.02	4.02	3	0.51	0.08	0.51	0.00	0.00	22.3
38	452	1764	22	151	0	-236	2331	4.02	4.02	4.02	4.02	3	0.35	0.00	0.02	0.00	0.00	22.3
39	452	281	-1477	119	0	-144	775	4.02	4.02	4.02	4.02	3	0.11	0.04	0.26	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	508	113	-2004	87	0	-170	-2021	4.02	4.02	4.02	4.02	3	0.29	0.06	0.36	0.00	0.00	22.3
2	508	-117	-1852	61	0	-115	-2373	4.02	4.02	4.02	4.02	2	0.36	0.05	0.33	0.00	0.00	22.3
3	508	-109	-1851	61	0	-114	-2369	4.02	4.02	4.02	4.02	2	0.36	0.05	0.33	0.00	0.00	22.3
4	508	283	-1233	73	0	-147	-742	4.02	4.02	4.02	4.02	2	0.11	0.04	0.22	0.00	0.00	22.3
5	508	291	-1231	73	0	-146	-738	4.02	4.02	4.02	4.02	2	0.11	0.04	0.22	0.00	0.00	22.3
6	508	13	-1638	66	0	-126	-1807	4.02	4.02	4.02	4.02	2	0.27	0.05	0.29	0.00	0.00	22.3
7	508	40	-1632	65	0	-125	-1793	4.02	4.02	4.02	4.02	2	0.27	0.05	0.29	0.00	0.00	22.3
8	508	133	-1452	69	0	-136	-1318	4.02	4.02	4.02	4.02	2	0.20	0.04	0.26	0.00	0.00	22.3
9	508	160	-1446	68	0	-135	-1304	4.02	4.02	4.02	4.02	2	0.20	0.04	0.26	0.00	0.00	22.3
10	508	-117	-1852	61	0	-115	-2373	4.02	4.02	4.02	4.02	2	0.36	0.05	0.33	0.00	0.00	22.3
11	508	-109	-1851	61	0	-114	-2369	4.02	4.02	4.02	4.02	2	0.36	0.05	0.33	0.00	0.00	22.3
12	508	283	-1233	73	0	-147	-742	4.02	4.02	4.02	4.02	2	0.11	0.04	0.22	0.00	0.00	22.3
13	508	291	-1231	73	0	-146	-738	4.02	4.02	4.02	4.02	2	0.11	0.04	0.22	0.00	0.00	22.3
14	508	13	-1638	66	0	-126	-1807	4.02	4.02	4.02	4.02	2	0.27	0.05	0.29	0.00	0.00	22.3
15	508	40	-1632	65	0	-125	-1793	4.02	4.02	4.02	4.02	2	0.27	0.05	0.29	0.00	0.00	22.3
16	508	133	-1452	69	0	-136	-1318	4.02	4.02	4.02	4.02	2	0.20	0.04	0.26	0.00	0.00	22.3
17	508	160	-1446	68	0	-135	-1304	4.02	4.02	4.02	4.02	2	0.20	0.04	0.26	0.00	0.00	22.3
18	508	-638	-2827	176	0	-320	-4153	4.02	4.02	4.02	4.02	3	0.58	0.08	0.50	0.00	0.00	22.3
19	508	1201	-1048	179	0	-363	1543	4.02	4.02	4.02	4.02	3	0.23	0.03	0.19	0.00	0.00	22.3
20	508	311	-1948	160	0	-298	-1864	4.02	4.02	4.02	4.02	3	0.27	0.06	0.35	0.00	0.00	22.3
37	508	-1302	-3444	145	0	-249	-5765	4.02	4.02	4.02	4.02	3	0.80	0.10	0.59	0.00	0.00	22.3
38	508	1764	-480	151	0	-321	2331	4.02	4.02	4.02	4.02	3	0.35	0.01	0.09	0.00	0.00	22.3
39	508	281	-1978	119	0	-212	-1950	4.02	4.02	4.02	4.02	3	0.28	0.06	0.35	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	565	113	-2506	87	0	-219	-2281	4.02	4.02	4.02	4.02	3	0.33	0.07	0.45	0.00	0.00	22.3
2	565	-117	-2238	61	0	-149	-2591	4.02	4.02	4.02	4.02	2	0.39	0.06	0.40	0.00	0.00	22.3
3	565	-109	-2237	61	0	-149	-2587	4.02	4.02	4.02	4.02	2	0.39	0.06	0.40	0.00	0.00	22.3
4	565	283	-1619	73	0	-188	-923	4.02	4.02	4.02	4.02	2	0.14	0.05	0.29	0.00	0.00	22.3
5	565	291	-1617	73	0	-188	-919	4.02	4.02	4.02	4.02	2	0.14	0.05	0.29	0.00	0.00	22.3
6	565	13	-2024	66	0	-163	-2012	4.02	4.02	4.02	4.02	2	0.31	0.06	0.36	0.00	0.00	22.3
7	565	40	-2018	65	0	-162	-1998	4.02	4.02	4.02	4.02	2	0.30	0.06	0.36	0.00	0.00	22.3
8	565	133	-1838	69	0	-175	-1512	4.02	4.02	4.02	4.02	2	0.23	0.05	0.33	0.00	0.00	22.3
9	565	160	-1832	68	0	-173	-1498	4.02	4.02	4.02	4.02	2	0.23	0.05	0.33	0.00	0.00	22.3
10	565	-117	-2238	61	0	-149	-2591	4.02	4.02	4.02	4.02	2	0.39	0.06	0.40	0.00	0.00	22.3
11	565	-109	-2237	61	0	-149	-2587	4.02	4.02	4.02	4.02	2	0.39	0.06	0.40	0.00	0.00	22.3
12	565	283	-1619	73	0	-188	-923	4.02	4.02	4.02	4.02	2	0.14	0.05	0.29	0.00	0.00	22.3
13	565	291	-1617	73	0	-188	-919	4.02	4.02	4.02	4.02	2	0.14	0.05	0.29	0.00	0.00	22.3
14	565	13	-2024	66	0	-163	-2012	4.02	4.02	4.02	4.02	2	0.31	0.06	0.36	0.00	0.00	22.3
15	565	40	-2018	65	0	-162	-1998	4.02	4.02	4.02	4.02	2	0.30	0.06	0.36	0.00	0.00	22.3

16	565	133	-1838	69	0	-175	-1512	4.02	4.02	4.02	4.02	2	0.23	0.05	0.33	0.00	0.00	22.3
17	565	160	-1832	68	0	-173	-1498	4.02	4.02	4.02	4.02	2	0.23	0.05	0.33	0.00	0.00	22.3
18	565	-638	-3329	176	0	-419	-4461	4.02	4.02	4.02	4.02	3	0.63	0.10	0.58	0.00	0.00	22.3
19	565	1201	-1550	179	0	-464	1063	4.02	4.02	4.02	4.02	3	0.16	0.04	0.28	0.00	0.00	22.3
20	565	311	-2450	160	0	-388	-2120	4.02	4.02	4.02	4.02	3	0.31	0.07	0.44	0.00	0.00	22.3
37	565	-1302	-3946	145	0	-331	-6109	4.02	4.02	4.02	4.02	3	0.84	0.11	0.68	0.00	0.00	22.3
38	565	1764	-981	151	0	-406	2286	4.02	4.02	4.02	4.02	3	0.35	0.03	0.17	0.00	0.00	22.3
39	565	281	-2480	119	0	-279	-2208	4.02	4.02	4.02	4.02	3	0.32	0.07	0.44	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

Nome travata: **trave_502_IP1** Descrizione: **Trave_5 10-15-20-25**
ASTA NUM. 5 NI 296 NF 298 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y Permanente qy tot.
qy medio: 375.00 308.00 683.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-43	2419	75	0	231	-2155	4.02	4.02	4.02	4.02	3	0.31	0.07	0.43	0.00	0.00	22.3
2	0	-253	1584	50	0	153	-888	4.02	4.02	4.02	4.02	2	0.13	0.05	0.28	0.00	0.00	22.3
3	0	-247	1587	52	0	159	-896	4.02	4.02	4.02	4.02	2	0.13	0.05	0.28	0.00	0.00	22.3
4	0	180	2135	64	0	197	-2419	4.02	4.02	4.02	4.02	2	0.37	0.06	0.38	0.00	0.00	22.3
5	0	186	2137	66	0	203	-2427	4.02	4.02	4.02	4.02	2	0.37	0.06	0.38	0.00	0.00	22.3
6	0	-108	1773	52	0	162	-1415	4.02	4.02	4.02	4.02	2	0.21	0.05	0.31	0.00	0.00	22.3
7	0	-88	1783	60	0	181	-1441	4.02	4.02	4.02	4.02	2	0.22	0.05	0.32	0.00	0.00	22.3
8	0	22	1939	57	0	175	-1875	4.02	4.02	4.02	4.02	2	0.28	0.06	0.35	0.00	0.00	22.3
9	0	42	1948	64	0	194	-1900	4.02	4.02	4.02	4.02	2	0.29	0.06	0.35	0.00	0.00	22.3
10	0	-253	1584	50	0	153	-888	4.02	4.02	4.02	4.02	2	0.13	0.05	0.28	0.00	0.00	22.3
11	0	-247	1587	52	0	159	-896	4.02	4.02	4.02	4.02	2	0.13	0.05	0.28	0.00	0.00	22.3
12	0	180	2135	64	0	197	-2419	4.02	4.02	4.02	4.02	2	0.37	0.06	0.38	0.00	0.00	22.3
13	0	186	2137	66	0	203	-2427	4.02	4.02	4.02	4.02	2	0.37	0.06	0.38	0.00	0.00	22.3
14	0	-108	1773	52	0	162	-1415	4.02	4.02	4.02	4.02	2	0.21	0.05	0.31	0.00	0.00	22.3
15	0	-88	1783	60	0	181	-1441	4.02	4.02	4.02	4.02	2	0.22	0.05	0.32	0.00	0.00	22.3
16	0	22	1939	57	0	175	-1875	4.02	4.02	4.02	4.02	2	0.28	0.06	0.35	0.00	0.00	22.3
17	0	42	1948	64	0	194	-1900	4.02	4.02	4.02	4.02	2	0.29	0.06	0.35	0.00	0.00	22.3
18	0	-840	1638	132	0	403	838	4.02	4.02	4.02	4.02	3	0.12	0.05	0.29	0.00	0.00	22.3
19	0	546	3196	146	0	465	-4321	4.02	4.02	4.02	4.02	3	0.63	0.09	0.57	0.00	0.00	22.3
20	0	-71	2416	139	0	437	-2152	4.02	4.02	4.02	4.02	3	0.31	0.07	0.43	0.00	0.00	22.3
37	0	-1264	1120	107	0	316	2017	4.02	4.02	4.02	4.02	3	0.28	0.03	0.19	0.00	0.00	22.3
38	0	1045	3716	129	0	419	-5767	4.02	4.02	4.02	4.02	3	0.85	0.11	0.66	0.00	0.00	22.3
39	0	18	2417	118	0	372	-2152	4.02	4.02	4.02	4.02	3	0.31	0.07	0.43	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	57	-43	1917	75	0	189	-1901	4.02	4.02	4.02	4.02	3	0.27	0.06	0.34	0.00	0.00	22.3
2	57	-253	1198	50	0	125	-709	4.02	4.02	4.02	4.02	2	0.11	0.03	0.21	0.00	0.00	22.3
3	57	-247	1201	52	0	129	-716	4.02	4.02	4.02	4.02	2	0.11	0.03	0.21	0.00	0.00	22.3
4	57	180	1749	64	0	161	-2208	4.02	4.02	4.02	4.02	2	0.34	0.05	0.31	0.00	0.00	22.3
5	57	186	1751	66	0	166	-2215	4.02	4.02	4.02	4.02	2	0.34	0.05	0.31	0.00	0.00	22.3
6	57	-108	1387	52	0	132	-1224	4.02	4.02	4.02	4.02	2	0.18	0.04	0.25	0.00	0.00	22.3
7	57	-88	1397	60	0	147	-1250	4.02	4.02	4.02	4.02	2	0.19	0.04	0.25	0.00	0.00	22.3
8	57	22	1553	57	0	143	-1675	4.02	4.02	4.02	4.02	2	0.25	0.05	0.28	0.00	0.00	22.3
9	57	42	1562	64	0	158	-1699	4.02	4.02	4.02	4.02	2	0.26	0.05	0.28	0.00	0.00	22.3
10	57	-253	1198	50	0	125	-709	4.02	4.02	4.02	4.02	2	0.11	0.03	0.21	0.00	0.00	22.3
11	57	-247	1201	52	0	129	-716	4.02	4.02	4.02	4.02	2	0.11	0.03	0.21	0.00	0.00	22.3
12	57	180	1749	64	0	161	-2208	4.02	4.02	4.02	4.02	2	0.34	0.05	0.31	0.00	0.00	22.3
13	57	186	1751	66	0	166	-2215	4.02	4.02	4.02	4.02	2	0.34	0.05	0.31	0.00	0.00	22.3
14	57	-108	1387	52	0	132	-1224	4.02	4.02	4.02	4.02	2	0.18	0.04	0.25	0.00	0.00	22.3
15	57	-88	1397	60	0	147	-1250	4.02	4.02	4.02	4.02	2	0.19	0.04	0.25	0.00	0.00	22.3
16	57	22	1553	57	0	143	-1675	4.02	4.02	4.02	4.02	2	0.25	0.05	0.28	0.00	0.00	22.3
17	57	42	1562	64	0	158	-1699	4.02	4.02	4.02	4.02	2	0.26	0.05	0.28	0.00	0.00	22.3
18	57	-840	1136	132	0	328	1368	4.02	4.02	4.02	4.02	3	0.19	0.03	0.20	0.00	0.00	22.3
19	57	546	2694	146	0	382	-4021	4.02	4.02	4.02	4.02	3	0.59	0.08	0.48	0.00	0.00	22.3
20	57	-71	1914	139	0	358	-1898	4.02	4.02	4.02	4.02	3	0.27	0.06	0.34	0.00	0.00	22.3
37	57	-1264	618	107	0	256	2149	4.02	4.02	4.02	4.02	3	0.30	0.02	0.11	0.00	0.00	22.3
38	57	1045	3214	129	0	346	-5436	4.02	4.02	4.02	4.02	3	0.80	0.09	0.57	0.00	0.00	22.3
39	57	18	1915	118	0	305	-1898	4.02	4.02	4.02	4.02	3	0.27	0.06	0.34	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	113	-43	1416	75	0	146	728	4.02	4.02	4.02	4.02	3	0.10	0.04	0.25	0.00	0.00	22.3
2	113	-253	812	50	0	97	877	4.02	4.02	4.02	4.02	2	0.13	0.02	0.14	0.00	0.00	22.3
3	113	-247	815	52	0	100	874	4.02	4.02	4.02	4.02	2	0.13	0.02	0.14	0.00	0.00	22.3
4	113	180	1363	64	0	125	-1133	4.02	4.02	4.02	4.02	2	0.17	0.04	0.24	0.00	0.00	22.3
5	113	186	1365	66	0	128	-1139	4.02	4.02	4.02	4.02	2	0.17	0.04	0.24	0.00	0.00	22.3
6	113	-108	1001	52	0	103	660	4.02	4.02	4.02	4.02	2	0.10	0.03	0.18	0.00	0.00	22.3
7	113	-88	1011	60	0	114	649	4.02	4.02	4.02	4.02	2	0.10	0.03	0.18	0.00	0.00	22.3
8	113	22	1167	57	0	111	-711	4.02	4.02	4.02	4.02	2	0.11	0.03	0.21	0.00	0.00	22.3
9	113	42	1176	64	0	122	-730	4.02	4.02	4.02	4.02	2	0.11	0.03	0.21	0.00	0.00	22.3
10	113	-253	812	50	0	97	877	4.02	4.02	4.02	4.02	2	0.13	0.02	0.14	0.00	0.00	22.3
11	113	-247	815	52	0	100	874	4.02	4.02	4.02	4.02	2	0.13	0.02	0.14	0.00	0.00	22.3
12	113	180	1363	64	0	125	-1133	4.02	4.02	4.02	4.02	2	0.17	0.04	0.24	0.00	0.00	22.3
13	113	186	1365	66	0	128	-1139	4.02	4.02	4.02	4.02	2	0.17	0.04	0.24	0.00	0.00	22.3
14	113	-108	1001	52	0	103	660	4.02	4.02	4.02	4.02	2	0.10	0.03	0.18	0.00	0.00	22.3
15	113	-88	1011	60	0	114	649	4.02	4.02	4.02	4.02	2	0.10	0.03	0.18	0.00	0.00	22.3
16	113	22	1167	57	0	111	-711	4.02	4.02	4.02	4.02	2	0.11	0.03	0.21	0.00	0.00	22.3
17	113	42	1176	64	0	122	-730	4.02	4.02	4.02	4.02	2	0.11	0.03	0.21	0.00	0.00	22.3
18	113	-840	635	132	0	254	1510	4.02	4.02	4.02	4.02	3	0.21	0.02	0.11	0.00	0.00	22.3
19	113	546	2193	146	0	300	-2387	4.02	4.02	4.02	4.02	3	0.35	0.06	0.39	0.00	0.00	22.3
20	113	-71	1413	139	0	279	727	4.02	4.02	4.02	4.02	3	0.10	0.04	0.25	0.00	0.00	22.3
37	113	-1264	117	107	0	195	2149	4.02	4.02	4.02	4.02	3	0.30	0.00	0.02	0.00	0.00	22.3
38	113	1045	2713	129	0	273	-3508	4.02	4.02	4.02	4.02	3	0.52	0.08	0.48	0.00	0.00	22.3
39	113	18	1414	118	0	238	728	4.02	4.02	4.02	4.02	3	0.10	0.04	0.25	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	170	-43	914	75	0	104	1132	4.02	4.02	4.02	4.02	3	0.16	0.03	0.16	0.00	0.00	22.3
2	170	-253	426	50	0	69	947	4.02	4.02	4.02	4.02	2	0.14	0.01	0.08	0.00	0.00	22.3
3	170	-247	429	52	0	71	946	4.02	4.02	4.02	4.02	2	0.14	0.01	0.08	0.00	0.00	22.3
4	170	180	977	64	0	89	712	4.02	4.02	4.02	4.02	2	0.11	0.03	0.17	0.00	0.00	22.3
5	170	186	979	66	0	91	710	4.02	4.02	4.02	4.02	2	0.11	0.03	0.17	0.00	0.00	22.3
6	170	-108	615	52	0	73	869	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
7	170	-88	625	60	0	80	870	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3

8	170	22	781	57	0	79	825	4.02	4.02	4.02	4.02	2	0.13	0.02	0.14	0.00	0.00	22.3
9	170	42	790	64	0	86	821	4.02	4.02	4.02	4.02	2	0.12	0.02	0.14	0.00	0.00	22.3
10	170	-253	426	50	0	69	947	4.02	4.02	4.02	4.02	2	0.14	0.01	0.08	0.00	0.00	22.3
11	170	-247	429	52	0	71	946	4.02	4.02	4.02	4.02	2	0.14	0.01	0.08	0.00	0.00	22.3
12	170	180	977	64	0	89	712	4.02	4.02	4.02	4.02	2	0.11	0.03	0.17	0.00	0.00	22.3
13	170	186	979	66	0	91	710	4.02	4.02	4.02	4.02	2	0.11	0.03	0.17	0.00	0.00	22.3
14	170	-108	615	52	0	73	869	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
15	170	-88	625	60	0	80	870	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
16	170	22	781	57	0	79	825	4.02	4.02	4.02	4.02	2	0.13	0.02	0.14	0.00	0.00	22.3
17	170	42	790	64	0	86	821	4.02	4.02	4.02	4.02	2	0.12	0.02	0.14	0.00	0.00	22.3
18	170	-840	133	132	0	179	1510	4.02	4.02	4.02	4.02	3	0.21	0.00	0.02	0.00	0.00	22.3
19	170	546	1691	146	0	218	-1036	4.02	4.02	4.02	4.02	3	0.15	0.05	0.30	0.00	0.00	22.3
20	170	-71	911	139	0	201	1129	4.02	4.02	4.02	4.02	3	0.16	0.03	0.16	0.00	0.00	22.3
37	170	-1264	-385	107	0	135	2149	4.02	4.02	4.02	4.02	3	0.30	0.01	0.07	0.00	0.00	22.3
38	170	1045	2211	129	0	200	-1863	4.02	4.02	4.02	4.02	3	0.28	0.06	0.39	0.00	0.00	22.3
39	170	18	912	118	0	171	1131	4.02	4.02	4.02	4.02	3	0.16	0.03	0.16	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	226	-43	412	75	0	61	1135	4.02	4.02	4.02	4.02	3	0.16	0.01	0.07	0.00	0.00	22.3
2	226	-253	40	50	0	40	947	4.02	4.02	4.02	4.02	2	0.14	0.00	0.01	0.00	0.00	22.3
3	226	-247	43	52	0	41	946	4.02	4.02	4.02	4.02	2	0.14	0.00	0.01	0.00	0.00	22.3
4	226	180	591	64	0	52	892	4.02	4.02	4.02	4.02	2	0.14	0.02	0.11	0.00	0.00	22.3
5	226	186	593	66	0	53	894	4.02	4.02	4.02	4.02	2	0.14	0.02	0.11	0.00	0.00	22.3
6	226	-108	229	52	0	44	869	4.02	4.02	4.02	4.02	2	0.13	0.01	0.04	0.00	0.00	22.3
7	226	-88	239	60	0	47	870	4.02	4.02	4.02	4.02	2	0.13	0.01	0.04	0.00	0.00	22.3
8	226	22	395	57	0	47	876	4.02	4.02	4.02	4.02	2	0.13	0.01	0.07	0.00	0.00	22.3
9	226	42	404	64	0	50	877	4.02	4.02	4.02	4.02	2	0.13	0.01	0.07	0.00	0.00	22.3
10	226	-253	40	50	0	40	947	4.02	4.02	4.02	4.02	2	0.14	0.00	0.01	0.00	0.00	22.3
11	226	-247	43	52	0	41	946	4.02	4.02	4.02	4.02	2	0.14	0.00	0.01	0.00	0.00	22.3
12	226	180	591	64	0	52	892	4.02	4.02	4.02	4.02	2	0.14	0.02	0.11	0.00	0.00	22.3
13	226	186	593	66	0	53	894	4.02	4.02	4.02	4.02	2	0.14	0.02	0.11	0.00	0.00	22.3
14	226	-108	229	52	0	44	869	4.02	4.02	4.02	4.02	2	0.13	0.01	0.04	0.00	0.00	22.3
15	226	-88	239	60	0	47	870	4.02	4.02	4.02	4.02	2	0.13	0.01	0.04	0.00	0.00	22.3
16	226	22	395	57	0	47	876	4.02	4.02	4.02	4.02	2	0.13	0.01	0.07	0.00	0.00	22.3
17	226	42	404	64	0	50	877	4.02	4.02	4.02	4.02	2	0.13	0.01	0.07	0.00	0.00	22.3
18	226	-840	-368	133	0	104	1510	4.02	4.02	4.02	4.02	3	0.21	0.01	0.06	0.00	0.00	22.3
19	226	546	1189	146	0	136	1236	4.02	4.02	4.02	4.02	3	0.18	0.03	0.21	0.00	0.00	22.3
20	226	-71	410	139	0	122	1130	4.02	4.02	4.02	4.02	3	0.16	0.01	0.07	0.00	0.00	22.3
37	226	-1264	-886	107	0	74	2149	4.02	4.02	4.02	4.02	3	0.30	0.03	0.15	0.00	0.00	22.3
38	226	1045	1710	129	0	127	1230	4.02	4.02	4.02	4.02	3	0.18	0.05	0.30	0.00	0.00	22.3
39	226	18	410	118	0	104	1133	4.02	4.02	4.02	4.02	3	0.16	0.01	0.07	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	283	-43	-90	75	0	18	1135	4.02	4.02	4.02	4.02	3	0.16	0.00	0.02	0.00	0.00	22.3
2	283	-253	-346	50	0	12	947	4.02	4.02	4.02	4.02	2	0.14	0.01	0.06	0.00	0.00	22.3
3	283	-247	-342	52	0	12	946	4.02	4.02	4.02	4.02	2	0.14	0.01	0.06	0.00	0.00	22.3
4	283	180	206	64	0	16	892	4.02	4.02	4.02	4.02	2	0.14	0.01	0.04	0.00	0.00	22.3
5	283	186	208	66	0	16	894	4.02	4.02	4.02	4.02	2	0.14	0.01	0.04	0.00	0.00	22.3
6	283	-108	-156	52	0	14	869	4.02	4.02	4.02	4.02	2	0.13	0.00	0.03	0.00	0.00	22.3
7	283	-88	-146	60	0	13	870	4.02	4.02	4.02	4.02	2	0.13	0.00	0.03	0.00	0.00	22.3
8	283	22	10	57	0	15	876	4.02	4.02	4.02	4.02	2	0.13	0.00	0.00	0.00	0.00	22.3
9	283	42	18	64	0	14	877	4.02	4.02	4.02	4.02	2	0.13	0.00	0.00	0.00	0.00	22.3
10	283	-253	-346	50	0	12	947	4.02	4.02	4.02	4.02	2	0.14	0.01	0.06	0.00	0.00	22.3
11	283	-247	-342	52	0	12	946	4.02	4.02	4.02	4.02	2	0.14	0.01	0.06	0.00	0.00	22.3
12	283	180	206	64	0	16	892	4.02	4.02	4.02	4.02	2	0.14	0.01	0.04	0.00	0.00	22.3
13	283	186	208	66	0	16	894	4.02	4.02	4.02	4.02	2	0.14	0.01	0.04	0.00	0.00	22.3
14	283	-108	-156	52	0	14	869	4.02	4.02	4.02	4.02	2	0.13	0.00	0.03	0.00	0.00	22.3
15	283	-88	-146	60	0	13	870	4.02	4.02	4.02	4.02	2	0.13	0.00	0.03	0.00	0.00	22.3
16	283	22	10	57	0	15	876	4.02	4.02	4.02	4.02	2	0.13	0.00	0.00	0.00	0.00	22.3
17	283	42	18	64	0	14	877	4.02	4.02	4.02	4.02	2	0.13	0.00	0.00	0.00	0.00	22.3
18	283	-840	-870	132	0	29	1510	4.02	4.02	4.02	4.02	3	0.21	0.03	0.15	0.00	0.00	22.3
19	283	546	688	146	0	53	1410	4.02	4.02	4.02	4.02	3	0.21	0.02	0.12	0.00	0.00	22.3
20	283	-71	-92	139	0	43	1130	4.02	4.02	4.02	4.02	3	0.16	0.00	0.02	0.00	0.00	22.3
37	283	-1264	-1388	107	0	14	1775	4.02	4.02	4.02	4.02	3	0.25	0.04	0.24	0.00	0.00	22.3
38	283	1045	1208	129	0	54	1800	4.02	4.02	4.02	4.02	3	0.27	0.04	0.22	0.00	0.00	22.3
39	283	18	-92	118	0	37	1133	4.02	4.02	4.02	4.02	3	0.16	0.00	0.02	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	339	-43	-591	75	0	-24	1135	4.02	4.02	4.02	4.02	3	0.16	0.02	0.11	0.00	0.00	22.3
2	339	-253	-731	50	0	-16	927	4.02	4.02	4.02	4.02	2	0.14	0.02	0.13	0.00	0.00	22.3
3	339	-247	-728	52	0	-17	928	4.02	4.02	4.02	4.02	2	0.14	0.02	0.13	0.00	0.00	22.3
4	339	180	-180	64	0	-20	892	4.02	4.02	4.02	4.02	2	0.14	0.01	0.03	0.00	0.00	22.3
5	339	186	-178	66	0	-22	894	4.02	4.02	4.02	4.02	2	0.14	0.01	0.03	0.00	0.00	22.3
6	339	-108	-542	52	0	-16	869	4.02	4.02	4.02	4.02	2	0.13	0.02	0.10	0.00	0.00	22.3
7	339	-88	-532	60	0	-21	870	4.02	4.02	4.02	4.02	2	0.13	0.02	0.09	0.00	0.00	22.3
8	339	22	-376	57	0	-17	876	4.02	4.02	4.02	4.02	2	0.13	0.01	0.07	0.00	0.00	22.3
9	339	42	-367	64	0	-22	877	4.02	4.02	4.02	4.02	2	0.13	0.01	0.07	0.00	0.00	22.3
10	339	-253	-731	50	0	-16	927	4.02	4.02	4.02	4.02	2	0.14	0.02	0.13	0.00	0.00	22.3
11	339	-247	-728	52	0	-17	928	4.02	4.02	4.02	4.02	2	0.14	0.02	0.13	0.00	0.00	22.3
12	339	180	-180	64	0	-20	892	4.02	4.02	4.02	4.02	2	0.14	0.01	0.03	0.00	0.00	22.3
13	339	186	-178	66	0	-22	894	4.02	4.02	4.02	4.02	2	0.14	0.01	0.03	0.00	0.00	22.3
14	339	-108	-542	52	0	-16	869	4.02	4.02	4.02	4.02	2	0.13	0.02	0.10	0.00	0.00	22.3
15	339	-88	-532	60	0	-21	870	4.02	4.02	4.02	4.02	2	0.13	0.02	0.09	0.00	0.00	22.3
16	339	22	-376	57	0	-17	876	4.02	4.02	4.02	4.02	2	0.13	0.01	0.07	0.00	0.00	22.3
17	339	42	-367	64	0	-22	877	4.02	4.02	4.02	4.02	2	0.13	0.01	0.07	0.00	0.00	22.3
18	339	-840	-1372	132	0	-46	1155	4.02	4.02	4.02	4.02	3	0.16	0.04	0.24	0.00	0.00	22.3
19	339	546	186	146	0	-29	1410	4.02	4.02	4.02	4.02	3	0.21	0.01	0.03	0.00	0.00	22.3
20	339	-71	-594	139	0	-35	1130	4.02	4.02	4.02	4.02	3	0.16	0.02	0.11	0.00	0.00	22.3
37	339	-1264	-1890	107	0	-47	1103	4.02	4.02	4.02	4.02	3	0.15	0.05	0.33	0.00	0.00	22.3
38	339	1045	706	129	0	-19	1987	4.02	4.02	4.02	4.02	3	0.29	0.02	0.13	0.00	0.00	22.3
39	339	18	-593	118	0	-30	1133	4.02	4.02	4.02	4.02	3	0.16	0.02	0.11	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	396	-43	-1093	75	0	-67	1020	4.02	4.02	4.02	4.02	3	0.15	0.03	0.19	0.00	0.00	22.3
2	396	-253	-1117	50	0	-44	600	4.02	4.02	4.02	4.02	2	0.09	0.03	0.20	0.00	0.00	22.3
3	396	-247	-1114	52	0	-47	602	4.02	4.02	4.02	4.02	2	0.09	0.03	0.20	0.00	0.00	22.3
4	396	180	-566	64	0	-56	892	4.02	4.02	4.02	4.02	2	0.14	0.02	0.10	0.00	0.00	22.3
5	396	186	-564	66	0	-59	894	4.02	4.02	4.02	4.02	2	0.14	0.02	0.10	0.00	0.00	22.3
6	396	-108	-928	52	0	-45	727	4.02	4.02	4.02	4.02	2	0.11	0.03	0.16	0.00	0.00	22.3
7	396	-88	-918	60	0	-54	733	4.02	4.02	4.02	4.02	2	0.11	0.03	0.16	0.00	0.00	22.3
8	396	22	-762	57	0	-49	837	4.02	4.02	4.02	4.02	2	0.13	0.02	0.14	0.00	0.00	22.3
9	396	42	-753	64	0	-58	843	4.02	4.02	4.02	4.02	2	0.13	0.02	0.13	0.00	0.00	22.3
10	396	-253	-1117	50	0	-44	600	4.02	4.02	4.02	4.02	2	0.09	0.03	0.20	0.00	0.00	22.3
11	396	-247	-1114	52	0	-47	602	4.02	4.02	4.02	4.02	2	0.09	0.03	0.20	0.00	0.00	22.3
12	396	180	-566	64	0	-56	892	4.02	4.02	4.02	4.02	2	0.14	0.02	0.10	0.00	0.00	22.3
13	396	186	-564	66	0	-59	894	4.02	4.02	4.02	4.02	2	0.14	0.02	0.10	0.00	0.00	22.3

14	396	-108	-928	52	0	-45	727	4.02	4.02	4.02	4.02	2	0.11	0.03	0.16	0.00	0.00	22.3
15	396	-88	-918	60	0	-54	733	4.02	4.02	4.02	4.02	2	0.11	0.03	0.16	0.00	0.00	22.3
16	396	22	-762	57	0	-49	837	4.02	4.02	4.02	4.02	2	0.13	0.02	0.14	0.00	0.00	22.3
17	396	42	-753	64	0	-58	843	4.02	4.02	4.02	4.02	2	0.13	0.02	0.13	0.00	0.00	22.3
18	396	-840	-1873	133	0	-121	-1404	4.02	4.02	4.02	4.02	3	0.20	0.05	0.33	0.00	0.00	22.3
19	396	546	-316	146	0	-111	1410	4.02	4.02	4.02	4.02	3	0.21	0.01	0.06	0.00	0.00	22.3
20	396	-71	-1095	139	0	-114	1014	4.02	4.02	4.02	4.02	3	0.15	0.03	0.19	0.00	0.00	22.3
37	396	-1264	-2391	107	0	-108	-2273	4.02	4.02	4.02	4.02	3	0.31	0.07	0.41	0.00	0.00	22.3
38	396	1045	205	129	0	-92	1987	4.02	4.02	4.02	4.02	3	0.29	0.01	0.04	0.00	0.00	22.3
39	396	18	-1095	118	0	-97	1018	4.02	4.02	4.02	4.02	3	0.15	0.03	0.20	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	452	-43	-1595	75	0	-110	-1100	4.02	4.02	4.02	4.02	3	0.16	0.05	0.28	0.00	0.00	22.3
2	452	-253	-1503	50	0	-72	-1467	4.02	4.02	4.02	4.02	2	0.22	0.04	0.27	0.00	0.00	22.3
3	452	-247	-1500	52	0	-76	-1460	4.02	4.02	4.02	4.02	2	0.22	0.04	0.27	0.00	0.00	22.3
4	452	180	-952	64	0	-93	734	4.02	4.02	4.02	4.02	2	0.11	0.03	0.17	0.00	0.00	22.3
5	452	186	-950	66	0	-97	737	4.02	4.02	4.02	4.02	2	0.11	0.03	0.17	0.00	0.00	22.3
6	452	-108	-1314	52	0	-75	-1042	4.02	4.02	4.02	4.02	2	0.16	0.04	0.23	0.00	0.00	22.3
7	452	-88	-1304	60	0	-88	-1020	4.02	4.02	4.02	4.02	2	0.15	0.04	0.23	0.00	0.00	22.3
8	452	22	-1148	57	0	-81	-670	4.02	4.02	4.02	4.02	2	0.10	0.03	0.20	0.00	0.00	22.3
9	452	42	-1139	64	0	-94	-649	4.02	4.02	4.02	4.02	2	0.10	0.03	0.20	0.00	0.00	22.3
10	452	-253	-1503	50	0	-72	-1467	4.02	4.02	4.02	4.02	2	0.22	0.04	0.27	0.00	0.00	22.3
11	452	-247	-1500	52	0	-76	-1460	4.02	4.02	4.02	4.02	2	0.22	0.04	0.27	0.00	0.00	22.3
12	452	180	-952	64	0	-93	734	4.02	4.02	4.02	4.02	2	0.11	0.03	0.17	0.00	0.00	22.3
13	452	186	-950	66	0	-97	737	4.02	4.02	4.02	4.02	2	0.11	0.03	0.17	0.00	0.00	22.3
14	452	-108	-1314	52	0	-75	-1042	4.02	4.02	4.02	4.02	2	0.16	0.04	0.23	0.00	0.00	22.3
15	452	-88	-1304	60	0	-88	-1020	4.02	4.02	4.02	4.02	2	0.15	0.04	0.23	0.00	0.00	22.3
16	452	22	-1148	57	0	-81	-670	4.02	4.02	4.02	4.02	2	0.10	0.03	0.20	0.00	0.00	22.3
17	452	42	-1139	64	0	-94	-649	4.02	4.02	4.02	4.02	2	0.10	0.03	0.20	0.00	0.00	22.3
18	452	-840	-2375	132	0	-196	-2859	4.02	4.02	4.02	4.02	3	0.40	0.07	0.41	0.00	0.00	22.3
19	452	546	-818	146	0	-193	1410	4.02	4.02	4.02	4.02	3	0.21	0.02	0.15	0.00	0.00	22.3
20	452	-71	-1597	139	0	-193	-1110	4.02	4.02	4.02	4.02	3	0.16	0.05	0.28	0.00	0.00	22.3
37	452	-1264	-2893	107	0	-168	-4020	4.02	4.02	4.02	4.02	3	0.56	0.08	0.50	0.00	0.00	22.3
38	452	1045	-297	129	0	-165	1987	4.02	4.02	4.02	4.02	3	0.29	0.01	0.05	0.00	0.00	22.3
39	452	18	-1597	118	0	-164	-1105	4.02	4.02	4.02	4.02	3	0.16	0.05	0.28	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	509	-43	-2096	75	0	-152	-2396	4.02	4.02	4.02	4.02	3	0.34	0.06	0.37	0.00	0.00	22.3
2	509	-253	-1889	50	0	-100	-2621	4.02	4.02	4.02	4.02	2	0.39	0.05	0.33	0.00	0.00	22.3
3	509	-247	-1886	52	0	-105	-2612	4.02	4.02	4.02	4.02	2	0.39	0.05	0.33	0.00	0.00	22.3
4	509	180	-1338	64	0	-129	-1073	4.02	4.02	4.02	4.02	2	0.16	0.04	0.24	0.00	0.00	22.3
5	509	186	-1336	66	0	-134	-1066	4.02	4.02	4.02	4.02	2	0.16	0.04	0.24	0.00	0.00	22.3
6	509	-108	-1700	52	0	-104	-2088	4.02	4.02	4.02	4.02	2	0.32	0.05	0.30	0.00	0.00	22.3
7	509	-88	-1690	60	0	-122	-2062	4.02	4.02	4.02	4.02	2	0.31	0.05	0.30	0.00	0.00	22.3
8	509	22	-1534	57	0	-113	-1624	4.02	4.02	4.02	4.02	2	0.25	0.04	0.27	0.00	0.00	22.3
9	509	42	-1525	64	0	-130	-1597	4.02	4.02	4.02	4.02	2	0.24	0.04	0.27	0.00	0.00	22.3
10	509	-253	-1889	50	0	-100	-2621	4.02	4.02	4.02	4.02	2	0.39	0.05	0.33	0.00	0.00	22.3
11	509	-247	-1886	52	0	-105	-2612	4.02	4.02	4.02	4.02	2	0.39	0.05	0.33	0.00	0.00	22.3
12	509	180	-1338	64	0	-129	-1073	4.02	4.02	4.02	4.02	2	0.16	0.04	0.24	0.00	0.00	22.3
13	509	186	-1336	66	0	-134	-1066	4.02	4.02	4.02	4.02	2	0.16	0.04	0.24	0.00	0.00	22.3
14	509	-108	-1700	52	0	-104	-2088	4.02	4.02	4.02	4.02	2	0.32	0.05	0.30	0.00	0.00	22.3
15	509	-88	-1690	60	0	-122	-2062	4.02	4.02	4.02	4.02	2	0.31	0.05	0.30	0.00	0.00	22.3
16	509	22	-1534	57	0	-113	-1624	4.02	4.02	4.02	4.02	2	0.25	0.04	0.27	0.00	0.00	22.3
17	509	42	-1525	64	0	-130	-1597	4.02	4.02	4.02	4.02	2	0.24	0.04	0.27	0.00	0.00	22.3
18	509	-840	-2876	133	0	-271	-4596	4.02	4.02	4.02	4.02	3	0.64	0.08	0.50	0.00	0.00	22.3
19	509	546	-1319	146	0	-276	1118	4.02	4.02	4.02	4.02	3	0.16	0.04	0.23	0.00	0.00	22.3
20	509	-71	-2098	139	0	-272	-2408	4.02	4.02	4.02	4.02	3	0.34	0.06	0.37	0.00	0.00	22.3
37	509	-1264	-3394	107	0	-229	-6050	4.02	4.02	4.02	4.02	3	0.84	0.10	0.59	0.00	0.00	22.3
38	509	1045	-798	129	0	-237	1987	4.02	4.02	4.02	4.02	3	0.29	0.02	0.14	0.00	0.00	22.3
39	509	18	-2098	118	0	-230	-2402	4.02	4.02	4.02	4.02	3	0.34	0.06	0.37	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	565	-43	-2598	75	0	-195	-2661	4.02	4.02	4.02	4.02	3	0.38	0.08	0.46	0.00	0.00	22.3
2	565	-253	-2275	50	0	-128	-2841	4.02	4.02	4.02	4.02	2	0.43	0.07	0.40	0.00	0.00	22.3
3	565	-247	-2272	52	0	-135	-2832	4.02	4.02	4.02	4.02	2	0.43	0.07	0.40	0.00	0.00	22.3
4	565	180	-1724	64	0	-165	-1261	4.02	4.02	4.02	4.02	2	0.19	0.05	0.31	0.00	0.00	22.3
5	565	186	-1722	66	0	-172	-1253	4.02	4.02	4.02	4.02	2	0.19	0.05	0.31	0.00	0.00	22.3
6	565	-108	-2086	52	0	-134	-2297	4.02	4.02	4.02	4.02	2	0.35	0.06	0.37	0.00	0.00	22.3
7	565	-88	-2076	60	0	-155	-2270	4.02	4.02	4.02	4.02	2	0.34	0.06	0.37	0.00	0.00	22.3
8	565	22	-1920	57	0	-145	-1823	4.02	4.02	4.02	4.02	2	0.28	0.06	0.34	0.00	0.00	22.3
9	565	42	-1911	64	0	-166	-1796	4.02	4.02	4.02	4.02	2	0.27	0.06	0.34	0.00	0.00	22.3
10	565	-253	-2275	50	0	-128	-2841	4.02	4.02	4.02	4.02	2	0.43	0.07	0.40	0.00	0.00	22.3
11	565	-247	-2272	52	0	-135	-2832	4.02	4.02	4.02	4.02	2	0.43	0.07	0.40	0.00	0.00	22.3
12	565	180	-1724	64	0	-165	-1261	4.02	4.02	4.02	4.02	2	0.19	0.05	0.31	0.00	0.00	22.3
13	565	186	-1722	66	0	-172	-1253	4.02	4.02	4.02	4.02	2	0.19	0.05	0.31	0.00	0.00	22.3
14	565	-108	-2086	52	0	-134	-2297	4.02	4.02	4.02	4.02	2	0.35	0.06	0.37	0.00	0.00	22.3
15	565	-88	-2076	60	0	-155	-2270	4.02	4.02	4.02	4.02	2	0.34	0.06	0.37	0.00	0.00	22.3
16	565	22	-1920	57	0	-145	-1823	4.02	4.02	4.02	4.02	2	0.28	0.06	0.34	0.00	0.00	22.3
17	565	42	-1911	64	0	-166	-1796	4.02	4.02	4.02	4.02	2	0.27	0.06	0.34	0.00	0.00	22.3
18	565	-840	-3378	132	0	-345	-4907	4.02	4.02	4.02	4.02	3	0.69	0.10	0.59	0.00	0.00	22.3
19	565	546	-1821	146	0	-358	-437	4.02	4.02	4.02	4.02	3	0.09	0.05	0.32	0.00	0.00	22.3
20	565	-71	-2600	139	0	-350	-2673	4.02	4.02	4.02	4.02	3	0.38	0.08	0.46	0.00	0.00	22.3
37	565	-1264	-3896	107	0	-289	-6391	4.02	4.02	4.02	4.02	3	0.88	0.11	0.67	0.00	0.00	22.3
38	565	1045	-1300	129	0	-310	1716	4.02	4.02	4.02	4.02	3	0.25	0.04	0.23	0.00	0.00	22.3
39	565	18	-2600	118	0	-297	-2667	4.02	4.02	4.02	4.02	3	0.38	0.08	0.46	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

Nome travata: **trave_502_IP1** Descrizione: **Trave_5 10-15-20-25**
ASTA NUM. 6 NI 298 NF 264 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y Permanente qy tot.
qy medio: 375.00 308.00 683.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-491	2750	22	0	48	-2734	4.02	4.02	4.02	4.02	3	0.39	0.08	0.48	0.00	0.00	22.3
2	0	-672	1871	-0	0	-8	-1393	4.02	4.02	4.02	4.02	2	0.21	0.05	0.33	0.00	0.00	22.3
3	0	-673	1872	10	0	20	-1396	4.02	4.02	4.02	4.02	2	0.21	0.05	0.33	0.00	0.00	22.3
4	0	-82	2359	24	0	53	-2810	4.02	4.02	4.02	4.02	2	0.42	0.07	0.42	0.00	0.00	22.3
5	0	-83	2360	34	0	81	-2813	4.02	4.02	4.02	4.02	2	0.43	0.07	0.42	0.00	0.00	22.3

6	0	-464	2041	-3	0	-19	-1886	4.02	4.02	4.02	4.02	2	0.28	0.06	0.36	0.00	0.00	22.3
7	0	-468	2044	30	0	74	-1896	4.02	4.02	4.02	4.02	2	0.28	0.06	0.36	0.00	0.00	22.3
8	0	-287	2187	4	0	-1	-2311	4.02	4.02	4.02	4.02	2	0.35	0.06	0.39	0.00	0.00	22.3
9	0	-291	2190	37	0	92	-2321	4.02	4.02	4.02	4.02	2	0.35	0.06	0.39	0.00	0.00	22.3
10	0	-672	1871	-0	0	-8	-1393	4.02	4.02	4.02	4.02	2	0.21	0.05	0.33	0.00	0.00	22.3
11	0	-673	1872	10	0	20	-1396	4.02	4.02	4.02	4.02	2	0.21	0.05	0.33	0.00	0.00	22.3
12	0	-82	2359	24	0	53	-2810	4.02	4.02	4.02	4.02	2	0.42	0.07	0.42	0.00	0.00	22.3
13	0	-83	2360	34	0	81	-2813	4.02	4.02	4.02	4.02	2	0.43	0.07	0.42	0.00	0.00	22.3
14	0	-464	2041	-3	0	-19	-1886	4.02	4.02	4.02	4.02	2	0.28	0.06	0.36	0.00	0.00	22.3
15	0	-468	2044	30	0	74	-1896	4.02	4.02	4.02	4.02	2	0.28	0.06	0.36	0.00	0.00	22.3
16	0	-287	2187	4	0	-1	-2311	4.02	4.02	4.02	4.02	2	0.35	0.06	0.39	0.00	0.00	22.3
17	0	-291	2190	37	0	92	-2321	4.02	4.02	4.02	4.02	2	0.35	0.06	0.39	0.00	0.00	22.3
18	0	-1798	2109	10	0	13	-866	4.02	4.02	4.02	4.02	3	0.12	0.06	0.36	0.00	0.00	22.3
19	0	-528	3496	68	0	144	-4862	4.02	4.02	4.02	4.02	3	0.69	0.10	0.61	0.00	0.00	22.3
20	0	-1064	2791	83	0	204	-2834	4.02	4.02	4.02	4.02	3	0.39	0.08	0.48	0.00	0.00	22.3
37	0	-1999	1630	-14	0	-41	1331	4.02	4.02	4.02	4.02	3	0.18	0.05	0.28	0.00	0.00	22.3
38	0	119	3942	82	0	178	-6154	4.02	4.02	4.02	4.02	3	0.89	0.11	0.70	0.00	0.00	22.3
39	0	-775	2766	107	0	278	-2774	4.02	4.02	4.02	4.02	3	0.39	0.08	0.48	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	56	-491	2248	22	0	35	-2460	4.02	4.02	4.02	4.02	3	0.35	0.07	0.40	0.00	0.00	22.3
2	56	-672	1485	-0	0	-8	-1197	4.02	4.02	4.02	4.02	2	0.18	0.04	0.26	0.00	0.00	22.3
3	56	-673	1486	10	0	15	-1200	4.02	4.02	4.02	4.02	2	0.18	0.04	0.26	0.00	0.00	22.3
4	56	-82	1973	24	0	39	-2585	4.02	4.02	4.02	4.02	2	0.39	0.06	0.35	0.00	0.00	22.3
5	56	-83	1974	34	0	62	-2588	4.02	4.02	4.02	4.02	2	0.39	0.06	0.35	0.00	0.00	22.3
6	56	-464	1655	-3	0	-17	-1680	4.02	4.02	4.02	4.02	2	0.25	0.05	0.29	0.00	0.00	22.3
7	56	-468	1658	30	0	57	-1690	4.02	4.02	4.02	4.02	2	0.25	0.05	0.29	0.00	0.00	22.3
8	56	-287	1801	4	0	-3	-2096	4.02	4.02	4.02	4.02	2	0.32	0.05	0.32	0.00	0.00	22.3
9	56	-291	1804	37	0	71	-2106	4.02	4.02	4.02	4.02	2	0.32	0.05	0.32	0.00	0.00	22.3
10	56	-672	1485	-0	0	-8	-1197	4.02	4.02	4.02	4.02	2	0.18	0.04	0.26	0.00	0.00	22.3
11	56	-673	1486	10	0	15	-1200	4.02	4.02	4.02	4.02	2	0.18	0.04	0.26	0.00	0.00	22.3
12	56	-82	1973	24	0	39	-2585	4.02	4.02	4.02	4.02	2	0.39	0.06	0.35	0.00	0.00	22.3
13	56	-83	1974	34	0	62	-2588	4.02	4.02	4.02	4.02	2	0.39	0.06	0.35	0.00	0.00	22.3
14	56	-464	1655	-3	0	-17	-1680	4.02	4.02	4.02	4.02	2	0.25	0.05	0.29	0.00	0.00	22.3
15	56	-468	1658	30	0	57	-1690	4.02	4.02	4.02	4.02	2	0.25	0.05	0.29	0.00	0.00	22.3
16	56	-287	1801	4	0	-3	-2096	4.02	4.02	4.02	4.02	2	0.32	0.05	0.32	0.00	0.00	22.3
17	56	-291	1804	37	0	71	-2106	4.02	4.02	4.02	4.02	2	0.32	0.05	0.32	0.00	0.00	22.3
18	56	-1798	1607	10	0	7	998	4.02	4.02	4.02	4.02	3	0.14	0.05	0.27	0.00	0.00	22.3
19	56	-528	2994	68	0	105	-4544	4.02	4.02	4.02	4.02	3	0.64	0.09	0.53	0.00	0.00	22.3
20	56	-1064	2289	83	0	157	-2558	4.02	4.02	4.02	4.02	3	0.36	0.07	0.40	0.00	0.00	22.3
37	56	-1999	1128	-14	0	-33	1856	4.02	4.02	4.02	4.02	3	0.25	0.03	0.19	0.00	0.00	22.3
38	56	119	3440	82	0	132	-5810	4.02	4.02	4.02	4.02	3	0.84	0.10	0.61	0.00	0.00	22.3
39	56	-775	2264	107	0	217	-2499	4.02	4.02	4.02	4.02	3	0.35	0.07	0.40	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	113	-491	1747	22	0	23	-1077	4.02	4.02	4.02	4.02	3	0.15	0.05	0.31	0.00	0.00	22.3
2	113	-672	1099	-0	0	-7	842	4.02	4.02	4.02	4.02	2	0.13	0.03	0.19	0.00	0.00	22.3
3	113	-673	1100	10	0	9	840	4.02	4.02	4.02	4.02	2	0.12	0.03	0.19	0.00	0.00	22.3
4	113	-82	1587	24	0	26	-1384	4.02	4.02	4.02	4.02	2	0.21	0.05	0.28	0.00	0.00	22.3
5	113	-83	1588	34	0	42	-1386	4.02	4.02	4.02	4.02	2	0.21	0.05	0.28	0.00	0.00	22.3
6	113	-464	1269	-3	0	-15	-658	4.02	4.02	4.02	4.02	2	0.10	0.04	0.22	0.00	0.00	22.3
7	113	-468	1272	30	0	40	-667	4.02	4.02	4.02	4.02	2	0.10	0.04	0.22	0.00	0.00	22.3
8	113	-287	1415	4	0	-6	-992	4.02	4.02	4.02	4.02	2	0.15	0.04	0.25	0.00	0.00	22.3
9	113	-291	1418	37	0	50	-1000	4.02	4.02	4.02	4.02	2	0.15	0.04	0.25	0.00	0.00	22.3
10	113	-672	1099	-0	0	-7	842	4.02	4.02	4.02	4.02	2	0.13	0.03	0.19	0.00	0.00	22.3
11	113	-673	1100	10	0	9	840	4.02	4.02	4.02	4.02	2	0.12	0.03	0.19	0.00	0.00	22.3
12	113	-82	1587	24	0	26	-1384	4.02	4.02	4.02	4.02	2	0.21	0.05	0.28	0.00	0.00	22.3
13	113	-83	1588	34	0	42	-1386	4.02	4.02	4.02	4.02	2	0.21	0.05	0.28	0.00	0.00	22.3
14	113	-464	1269	-3	0	-15	-658	4.02	4.02	4.02	4.02	2	0.10	0.04	0.22	0.00	0.00	22.3
15	113	-468	1272	30	0	40	-667	4.02	4.02	4.02	4.02	2	0.10	0.04	0.22	0.00	0.00	22.3
16	113	-287	1415	4	0	-6	-992	4.02	4.02	4.02	4.02	2	0.15	0.04	0.25	0.00	0.00	22.3
17	113	-291	1418	37	0	50	-1000	4.02	4.02	4.02	4.02	2	0.15	0.04	0.25	0.00	0.00	22.3
18	113	-1798	1106	10	0	1	1510	4.02	4.02	4.02	4.02	3	0.21	0.03	0.19	0.00	0.00	22.3
19	113	-528	2493	68	0	67	-2740	4.02	4.02	4.02	4.02	3	0.39	0.07	0.44	0.00	0.00	22.3
20	113	-1064	1788	83	0	110	-1152	4.02	4.02	4.02	4.02	3	0.16	0.05	0.31	0.00	0.00	22.3
37	113	-1999	627	-14	0	-25	1993	4.02	4.02	4.02	4.02	3	0.27	0.02	0.11	0.00	0.00	22.3
38	113	119	2939	82	0	86	-3754	4.02	4.02	4.02	4.02	3	0.54	0.09	0.52	0.00	0.00	22.3
39	113	-775	1763	107	0	156	-1107	4.02	4.02	4.02	4.02	3	0.16	0.05	0.31	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	169	-491	1245	22	0	10	1283	4.02	4.02	4.02	4.02	3	0.18	0.04	0.22	0.00	0.00	22.3
2	169	-672	713	-0	0	-7	1158	4.02	4.02	4.02	4.02	2	0.17	0.02	0.13	0.00	0.00	22.3
3	169	-673	714	10	0	4	1157	4.02	4.02	4.02	4.02	2	0.17	0.02	0.13	0.00	0.00	22.3
4	169	-82	1201	24	0	12	816	4.02	4.02	4.02	4.02	2	0.12	0.03	0.21	0.00	0.00	22.3
5	169	-83	1202	34	0	23	815	4.02	4.02	4.02	4.02	2	0.12	0.03	0.21	0.00	0.00	22.3
6	169	-464	883	-3	0	-14	1039	4.02	4.02	4.02	4.02	2	0.16	0.03	0.16	0.00	0.00	22.3
7	169	-468	886	30	0	24	1036	4.02	4.02	4.02	4.02	2	0.15	0.03	0.16	0.00	0.00	22.3
8	169	-287	1029	4	0	-8	937	4.02	4.02	4.02	4.02	2	0.14	0.03	0.18	0.00	0.00	22.3
9	169	-291	1032	37	0	29	933	4.02	4.02	4.02	4.02	2	0.14	0.03	0.18	0.00	0.00	22.3
10	169	-672	713	-0	0	-7	1158	4.02	4.02	4.02	4.02	2	0.17	0.02	0.13	0.00	0.00	22.3
11	169	-673	714	10	0	4	1157	4.02	4.02	4.02	4.02	2	0.17	0.02	0.13	0.00	0.00	22.3
12	169	-82	1201	24	0	12	816	4.02	4.02	4.02	4.02	2	0.12	0.03	0.21	0.00	0.00	22.3
13	169	-83	1202	34	0	23	815	4.02	4.02	4.02	4.02	2	0.12	0.03	0.21	0.00	0.00	22.3
14	169	-464	883	-3	0	-14	1039	4.02	4.02	4.02	4.02	2	0.16	0.03	0.16	0.00	0.00	22.3
15	169	-468	886	30	0	24	1036	4.02	4.02	4.02	4.02	2	0.15	0.03	0.16	0.00	0.00	22.3
16	169	-287	1029	4	0	-8	937	4.02	4.02	4.02	4.02	2	0.14	0.03	0.18	0.00	0.00	22.3
17	169	-291	1032	37	0	29	933	4.02	4.02	4.02	4.02	2	0.14	0.03	0.18	0.00	0.00	22.3
18	169	-1798	604	10	0	-5	1632	4.02	4.02	4.02	4.02	3	0.22	0.02	0.10	0.00	0.00	22.3
19	169	-528	1991	68	0	29	-1220	4.02	4.02	4.02	4.02	3	0.17	0.06	0.35	0.00	0.00	22.3
20	169	-1064	1286	83	0	62	1272	4.02	4.02	4.02	4.02	3	0.18	0.04	0.22	0.00	0.00	22.3
37	169	-1999	125	-14	0	-17	1993	4.02	4.02	4.02	4.02	3	0.27	0.00	0.02	0.00	0.00	22.3
38	169	119	2437	82	0	40	-1981	4.02	4.02	4.02	4.02	3	0.29	0.07	0.43	0.00	0.00	22.3
39	169	-775	1261	107	0	96	1278	4.02	4.02	4.02	4.02	3	0.18	0.04	0.22	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	226	-491	744	22	0	-2	1492	4.02	4.02	4.02	4.02	3	0.21	0.02	0.13	0.00	0.00	22.3
2	226	-672	327	-0	0	-7	1167	4.02	4.02	4.02	4.02	2	0.17	0.01	0.06	0.00	0.00	22.3
3	226	-673	328	10	0	-2	1166	4.02	4.02	4.02	4.02	2	0.17	0.01	0.06	0.00	0.00	22.3
4	226	-82	815	24	0	-2	1191	4.02	4.02	4.02	4.02	2	0.18	0.02	0.14	0.00	0.00	22.3
5	226	-83	816	34	0	4	1190	4.02	4.02	4.02	4.02	2	0.18	0.02	0.15	0.00	0.00	22.3
6	226	-464	497	-3	0	-12	1154	4.02	4.02	4.02	4.02	2	0.17	0.01	0.09	0.00	0.00	22.3
7	226	-468	500	30	0	7	1152	4.02	4.02	4.02	4.02	2	0.17	0.01	0.09	0.00	0.00	22.3
8	226	-287	643	4	0	-10	1180	4.02	4.02	4.02	4.02	2	0.18	0.02	0.11	0.00	0.00	22.3
9	226	-291	646	37	0	8	1180	4.02	4.02	4.02	4.02	2	0.18	0.02	0.11	0.00	0.00	22.3
10	226	-672	327	-0	0	-7	1167	4.02	4.02	4.02	4.02	2	0.17	0.01	0.06	0.00	0.00	22.3
11	226	-673	328	10	0	-2	1166	4.02	4.02	4.02	4.02	2	0.17	0.01	0.06	0.00	0.00	22.3

12	226	-82	815	24	0	-2	1191	4.02	4.02	4.02	4.02	2	0.18	0.02	0.14	0.00	0.00	22.3
13	226	-83	816	34	0	4	1190	4.02	4.02	4.02	4.02	2	0.18	0.02	0.15	0.00	0.00	22.3
14	226	-464	497	-3	0	-12	1154	4.02	4.02	4.02	4.02	2	0.17	0.01	0.09	0.00	0.00	22.3
15	226	-468	500	30	0	7	1152	4.02	4.02	4.02	4.02	2	0.17	0.01	0.09	0.00	0.00	22.3
16	226	-287	643	4	0	-10	1180	4.02	4.02	4.02	4.02	2	0.18	0.02	0.11	0.00	0.00	22.3
17	226	-291	646	37	0	8	1180	4.02	4.02	4.02	4.02	2	0.18	0.02	0.11	0.00	0.00	22.3
18	226	-1798	102	10	0	-11	1632	4.02	4.02	4.02	4.02	3	0.22	0.00	0.02	0.00	0.00	22.3
19	226	-528	1489	68	0	-10	1525	4.02	4.02	4.02	4.02	3	0.22	0.04	0.26	0.00	0.00	22.3
20	226	-1064	784	83	0	15	1524	4.02	4.02	4.02	4.02	3	0.21	0.02	0.14	0.00	0.00	22.3
37	226	-1999	-377	-14	0	-9	1993	4.02	4.02	4.02	4.02	3	0.27	0.01	0.06	0.00	0.00	22.3
38	226	119	1935	82	0	-7	1467	4.02	4.02	4.02	4.02	3	0.21	0.06	0.34	0.00	0.00	22.3
39	226	-775	760	107	0	35	1502	4.02	4.02	4.02	4.02	3	0.21	0.02	0.13	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	282	-491	242	22	0	-15	1492	4.02	4.02	4.02	4.02	3	0.21	0.01	0.04	0.00	0.00	22.3
2	282	-672	-58	-0	0	-7	1167	4.02	4.02	4.02	4.02	2	0.17	0.00	0.01	0.00	0.00	22.3
3	282	-673	-58	10	0	-7	1166	4.02	4.02	4.02	4.02	2	0.17	0.00	0.01	0.00	0.00	22.3
4	282	-82	429	24	0	-15	1263	4.02	4.02	4.02	4.02	2	0.19	0.01	0.08	0.00	0.00	22.3
5	282	-83	430	34	0	-15	1263	4.02	4.02	4.02	4.02	2	0.19	0.01	0.08	0.00	0.00	22.3
6	282	-464	112	-3	0	-10	1154	4.02	4.02	4.02	4.02	2	0.17	0.00	0.02	0.00	0.00	22.3
7	282	-468	114	30	0	-10	1152	4.02	4.02	4.02	4.02	2	0.17	0.00	0.02	0.00	0.00	22.3
8	282	-287	257	4	0	-12	1180	4.02	4.02	4.02	4.02	2	0.18	0.01	0.05	0.00	0.00	22.3
9	282	-291	260	37	0	-13	1180	4.02	4.02	4.02	4.02	2	0.18	0.01	0.05	0.00	0.00	22.3
10	282	-672	-58	-0	0	-7	1167	4.02	4.02	4.02	4.02	2	0.17	0.00	0.01	0.00	0.00	22.3
11	282	-673	-58	10	0	-7	1166	4.02	4.02	4.02	4.02	2	0.17	0.00	0.01	0.00	0.00	22.3
12	282	-82	429	24	0	-15	1263	4.02	4.02	4.02	4.02	2	0.19	0.01	0.08	0.00	0.00	22.3
13	282	-83	430	34	0	-15	1263	4.02	4.02	4.02	4.02	2	0.19	0.01	0.08	0.00	0.00	22.3
14	282	-464	112	-3	0	-10	1154	4.02	4.02	4.02	4.02	2	0.17	0.00	0.02	0.00	0.00	22.3
15	282	-468	114	30	0	-10	1152	4.02	4.02	4.02	4.02	2	0.17	0.00	0.02	0.00	0.00	22.3
16	282	-287	257	4	0	-12	1180	4.02	4.02	4.02	4.02	2	0.18	0.01	0.05	0.00	0.00	22.3
17	282	-291	260	37	0	-13	1180	4.02	4.02	4.02	4.02	2	0.18	0.01	0.05	0.00	0.00	22.3
18	282	-1798	-400	10	0	-17	1632	4.02	4.02	4.02	4.02	3	0.22	0.01	0.07	0.00	0.00	22.3
19	282	-528	988	68	0	-48	1971	4.02	4.02	4.02	4.02	3	0.28	0.03	0.17	0.00	0.00	22.3
20	282	-1064	282	83	0	-32	1524	4.02	4.02	4.02	4.02	3	0.21	0.01	0.05	0.00	0.00	22.3
37	282	-1999	-878	-14	0	-1	1993	4.02	4.02	4.02	4.02	3	0.27	0.03	0.15	0.00	0.00	22.3
38	282	119	1434	82	0	-53	2165	4.02	4.02	4.02	4.02	3	0.31	0.04	0.26	0.00	0.00	22.3
39	282	-775	258	107	0	-26	1502	4.02	4.02	4.02	4.02	3	0.21	0.01	0.05	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	339	-491	-260	22	0	-27	1492	4.02	4.02	4.02	4.02	3	0.21	0.01	0.05	0.00	0.00	22.3
2	339	-672	-444	-0	0	-7	1167	4.02	4.02	4.02	4.02	2	0.17	0.01	0.08	0.00	0.00	22.3
3	339	-673	-443	10	0	-13	1166	4.02	4.02	4.02	4.02	2	0.17	0.01	0.08	0.00	0.00	22.3
4	339	-82	44	24	0	-29	1263	4.02	4.02	4.02	4.02	2	0.19	0.00	0.01	0.00	0.00	22.3
5	339	-83	45	34	0	-35	1263	4.02	4.02	4.02	4.02	2	0.19	0.00	0.01	0.00	0.00	22.3
6	339	-464	-274	-3	0	-8	1154	4.02	4.02	4.02	4.02	2	0.17	0.01	0.05	0.00	0.00	22.3
7	339	-468	-271	30	0	-27	1152	4.02	4.02	4.02	4.02	2	0.17	0.01	0.05	0.00	0.00	22.3
8	339	-287	-128	4	0	-14	1180	4.02	4.02	4.02	4.02	2	0.18	0.00	0.02	0.00	0.00	22.3
9	339	-291	-125	37	0	-34	1180	4.02	4.02	4.02	4.02	2	0.18	0.00	0.02	0.00	0.00	22.3
10	339	-672	-444	-0	0	-7	1167	4.02	4.02	4.02	4.02	2	0.17	0.01	0.08	0.00	0.00	22.3
11	339	-673	-443	10	0	-13	1166	4.02	4.02	4.02	4.02	2	0.17	0.01	0.08	0.00	0.00	22.3
12	339	-82	44	24	0	-29	1263	4.02	4.02	4.02	4.02	2	0.19	0.00	0.01	0.00	0.00	22.3
13	339	-83	45	34	0	-35	1263	4.02	4.02	4.02	4.02	2	0.19	0.00	0.01	0.00	0.00	22.3
14	339	-464	-274	-3	0	-8	1154	4.02	4.02	4.02	4.02	2	0.17	0.01	0.05	0.00	0.00	22.3
15	339	-468	-271	30	0	-27	1152	4.02	4.02	4.02	4.02	2	0.17	0.01	0.05	0.00	0.00	22.3
16	339	-287	-128	4	0	-14	1180	4.02	4.02	4.02	4.02	2	0.18	0.00	0.02	0.00	0.00	22.3
17	339	-291	-125	37	0	-34	1180	4.02	4.02	4.02	4.02	2	0.18	0.00	0.02	0.00	0.00	22.3
18	339	-1798	-901	10	0	-23	1632	4.02	4.02	4.02	4.02	3	0.22	0.03	0.15	0.00	0.00	22.3
19	339	-528	486	68	0	-86	2020	4.02	4.02	4.02	4.02	3	0.29	0.01	0.09	0.00	0.00	22.3
20	339	-1064	-219	83	0	-79	1524	4.02	4.02	4.02	4.02	3	0.21	0.01	0.04	0.00	0.00	22.3
37	339	-1999	-1380	-14	0	7	1628	4.02	4.02	4.02	4.02	3	0.22	0.04	0.23	0.00	0.00	22.3
38	339	119	932	82	0	-99	2580	4.02	4.02	4.02	4.02	3	0.37	0.03	0.17	0.00	0.00	22.3
39	339	-775	-244	107	0	-87	1502	4.02	4.02	4.02	4.02	3	0.21	0.01	0.04	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	395	-491	-761	22	0	-39	1492	4.02	4.02	4.02	4.02	3	0.21	0.02	0.13	0.00	0.00	22.3
2	395	-672	-830	-0	0	-7	1085	4.02	4.02	4.02	4.02	2	0.16	0.02	0.15	0.00	0.00	22.3
3	395	-673	-829	10	0	-18	1085	4.02	4.02	4.02	4.02	2	0.16	0.02	0.15	0.00	0.00	22.3
4	395	-82	-342	24	0	-43	1263	4.02	4.02	4.02	4.02	2	0.19	0.01	0.06	0.00	0.00	22.3
5	395	-83	-341	34	0	-54	1263	4.02	4.02	4.02	4.02	2	0.19	0.01	0.06	0.00	0.00	22.3
6	395	-464	-660	-3	0	-6	1154	4.02	4.02	4.02	4.02	2	0.17	0.02	0.12	0.00	0.00	22.3
7	395	-468	-657	30	0	-44	1152	4.02	4.02	4.02	4.02	2	0.17	0.02	0.12	0.00	0.00	22.3
8	395	-287	-514	4	0	-17	1180	4.02	4.02	4.02	4.02	2	0.18	0.01	0.09	0.00	0.00	22.3
9	395	-291	-511	37	0	-55	1180	4.02	4.02	4.02	4.02	2	0.18	0.01	0.09	0.00	0.00	22.3
10	395	-672	-830	-0	0	-7	1085	4.02	4.02	4.02	4.02	2	0.16	0.02	0.15	0.00	0.00	22.3
11	395	-673	-829	10	0	-18	1085	4.02	4.02	4.02	4.02	2	0.16	0.02	0.15	0.00	0.00	22.3
12	395	-82	-342	24	0	-43	1263	4.02	4.02	4.02	4.02	2	0.19	0.01	0.06	0.00	0.00	22.3
13	395	-83	-341	34	0	-54	1263	4.02	4.02	4.02	4.02	2	0.19	0.01	0.06	0.00	0.00	22.3
14	395	-464	-660	-3	0	-6	1154	4.02	4.02	4.02	4.02	2	0.17	0.02	0.12	0.00	0.00	22.3
15	395	-468	-657	30	0	-44	1152	4.02	4.02	4.02	4.02	2	0.17	0.02	0.12	0.00	0.00	22.3
16	395	-287	-514	4	0	-17	1180	4.02	4.02	4.02	4.02	2	0.18	0.01	0.09	0.00	0.00	22.3
17	395	-291	-511	37	0	-55	1180	4.02	4.02	4.02	4.02	2	0.18	0.01	0.09	0.00	0.00	22.3
18	395	-1798	-1403	10	0	-28	1240	4.02	4.02	4.02	4.02	3	0.17	0.04	0.24	0.00	0.00	22.3
19	395	-528	-16	68	0	-125	2020	4.02	4.02	4.02	4.02	3	0.29	0.00	0.00	0.00	0.00	22.3
20	395	-1064	-721	83	0	-126	1524	4.02	4.02	4.02	4.02	3	0.21	0.02	0.13	0.00	0.00	22.3
37	395	-1999	-1882	-14	0	15	961	4.02	4.02	4.02	4.02	3	0.13	0.05	0.32	0.00	0.00	22.3
38	395	119	430	82	0	-145	2594	4.02	4.02	4.02	4.02	3	0.37	0.01	0.08	0.00	0.00	22.3
39	395	-775	-745	107	0	-147	1502	4.02	4.02	4.02	4.02	3	0.21	0.02	0.13	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	452	-491	-1263	22	0	-52	1266	4.02	4.02	4.02	4.02	3	0.18	0.04	0.22	0.00	0.00	22.3
2	452	-672	-1216	-0	0	-7	702	4.02	4.02	4.02	4.02	2	0.10	0.04	0.21	0.00	0.00	22.3
3	452	-673	-1215	10	0	-24	703	4.02	4.02	4.02	4.02	2	0.10	0.04	0.21	0.00	0.00	22.3
4	452	-82	-728	24	0	-56	1246	4.02	4.02	4.02	4.02	2	0.19	0.02	0.13	0.00	0.00	22.3
5	452	-83	-727	34	0	-73	1246	4.02	4.02	4.02	4.02	2	0.19	0.02	0.13	0.00	0.00	22.3
6	452	-464	-1046	-3	0	-4	892	4.02	4.02	4.02	4.02	2	0.13	0.03	0.18	0.00	0.00	22.3
7	452	-468	-1043	30	0	-61	893	4.02	4.02	4.02	4.02	2	0.13	0.03	0.18	0.00	0.00	22.3
8	452	-287	-900	4	0	-19	1055	4.02	4.02	4.02	4.02	2	0.16	0.03	0.16	0.00	0.00	22.3
9	452	-291	-897	37	0	-76	1056	4.02	4.02	4.02	4.02	2	0.16	0.03	0.16	0.00	0.00	22.3
10	452	-672	-1216	-0	0	-7	702	4.02	4.02	4.02	4.02	2	0.10	0.04	0.21	0.00	0.00	22.3
11	452	-673	-1215	10	0	-24	703	4.02	4.02	4.02	4.02	2	0.10	0.04	0.21	0.00	0.00	22.3
12	452	-82	-728	24	0	-56	1246	4.02	4.02	4.02	4.02	2	0.19	0.02	0.13	0.00	0.00	22.3
13	452	-83	-727	34	0	-73	1246	4.02	4.02	4.02	4.02	2	0.19	0.02	0.13	0.00	0.00	22.3
14	452	-464	-1046	-3	0	-4	892	4.02	4.02	4.02	4.02	2	0.13	0.03	0.18	0.00	0.00	22.3
15	452	-468	-1043	30	0	-61	893	4.02	4.02	4.02	4.02	2	0.13	0.03	0.18	0.00	0.00	22.3
16	452	-287	-900	4	0	-19	1055	4.02	4.02	4.02	4.02	2	0.16	0.03	0.16	0.00	0.00	22.3
17	452	-291	-897	37	0	-76	1056	4.02	4.02	4.02	4.02	2	0.16	0.03	0.16	0.00	0.00	22.3

18	452	-1798	-1905	10	0	-34	-1369	4.02	4.02	4.02	4.02	3	0.19	0.05	0.33	0.00	0.00	22.3
19	452	-528	-518	68	0	-163	2020	4.02	4.02	4.02	4.02	3	0.29	0.01	0.09	0.00	0.00	22.3
20	452	-1064	-1223	83	0	-173	1328	4.02	4.02	4.02	4.02	3	0.18	0.04	0.21	0.00	0.00	22.3
37	452	-1999	-2384	-14	0	23	-2404	4.02	4.02	4.02	4.02	3	0.33	0.07	0.41	0.00	0.00	22.3
38	452	119	-72	82	0	-191	2594	4.02	4.02	4.02	4.02	3	0.37	0.00	0.01	0.00	0.00	22.3
39	452	-775	-1247	107	0	-208	1291	4.02	4.02	4.02	4.02	3	0.18	0.04	0.22	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	508	-491	-1764	22	0	-64	-1121	4.02	4.02	4.02	4.02	3	0.16	0.05	0.31	0.00	0.00	22.3
2	508	-672	-1602	-0	0	-6	-1521	4.02	4.02	4.02	4.02	2	0.23	0.05	0.28	0.00	0.00	22.3
3	508	-673	-1601	10	0	-29	-1519	4.02	4.02	4.02	4.02	2	0.23	0.05	0.28	0.00	0.00	22.3
4	508	-82	-1114	24	0	-70	921	4.02	4.02	4.02	4.02	2	0.14	0.03	0.20	0.00	0.00	22.3
5	508	-83	-1113	34	0	-93	922	4.02	4.02	4.02	4.02	2	0.14	0.03	0.20	0.00	0.00	22.3
6	508	-464	-1432	-3	0	-2	-1063	4.02	4.02	4.02	4.02	2	0.16	0.04	0.25	0.00	0.00	22.3
7	508	-468	-1429	30	0	-78	-1057	4.02	4.02	4.02	4.02	2	0.16	0.04	0.25	0.00	0.00	22.3
8	508	-287	-1286	4	0	-21	-669	4.02	4.02	4.02	4.02	2	0.10	0.04	0.23	0.00	0.00	22.3
9	508	-291	-1283	37	0	-97	-663	4.02	4.02	4.02	4.02	2	0.10	0.04	0.23	0.00	0.00	22.3
10	508	-672	-1602	-0	0	-6	-1521	4.02	4.02	4.02	4.02	2	0.23	0.05	0.28	0.00	0.00	22.3
11	508	-673	-1601	10	0	-29	-1519	4.02	4.02	4.02	4.02	2	0.23	0.05	0.28	0.00	0.00	22.3
12	508	-82	-1114	24	0	-70	921	4.02	4.02	4.02	4.02	2	0.14	0.03	0.20	0.00	0.00	22.3
13	508	-83	-1113	34	0	-93	922	4.02	4.02	4.02	4.02	2	0.14	0.03	0.20	0.00	0.00	22.3
14	508	-464	-1432	-3	0	-2	-1063	4.02	4.02	4.02	4.02	2	0.16	0.04	0.25	0.00	0.00	22.3
15	508	-468	-1429	30	0	-78	-1057	4.02	4.02	4.02	4.02	2	0.16	0.04	0.25	0.00	0.00	22.3
16	508	-287	-1286	4	0	-21	-669	4.02	4.02	4.02	4.02	2	0.10	0.04	0.23	0.00	0.00	22.3
17	508	-291	-1283	37	0	-97	-663	4.02	4.02	4.02	4.02	2	0.10	0.04	0.23	0.00	0.00	22.3
18	508	-1798	-2406	10	0	-40	-2841	4.02	4.02	4.02	4.02	3	0.39	0.07	0.41	0.00	0.00	22.3
19	508	-528	-1019	68	0	-201	1952	4.02	4.02	4.02	4.02	3	0.28	0.03	0.18	0.00	0.00	22.3
20	508	-1064	-1724	83	0	-220	-996	4.02	4.02	4.02	4.02	3	0.14	0.05	0.30	0.00	0.00	22.3
37	508	-1999	-2885	-14	0	32	-4146	4.02	4.02	4.02	4.02	3	0.56	0.08	0.49	0.00	0.00	22.3
38	508	119	-573	82	0	-237	2594	4.02	4.02	4.02	4.02	3	0.37	0.02	0.10	0.00	0.00	22.3
39	508	-775	-1748	107	0	-269	-1071	4.02	4.02	4.02	4.02	3	0.15	0.05	0.31	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	565	-491	-2266	22	0	-77	-1367	4.02	4.02	4.02	4.02	3	0.19	0.07	0.40	0.00	0.00	22.3
2	565	-672	-1988	-0	0	-6	-1724	4.02	4.02	4.02	4.02	2	0.26	0.06	0.35	0.00	0.00	22.3
3	565	-673	-1987	10	0	-35	-1722	4.02	4.02	4.02	4.02	2	0.26	0.06	0.35	0.00	0.00	22.3
4	565	-82	-1500	24	0	-83	-382	4.02	4.02	4.02	4.02	2	0.06	0.04	0.27	0.00	0.00	22.3
5	565	-83	-1499	34	0	-112	-380	4.02	4.02	4.02	4.02	2	0.06	0.04	0.27	0.00	0.00	22.3
6	565	-464	-1818	-3	0	-0	-1256	4.02	4.02	4.02	4.02	2	0.19	0.05	0.32	0.00	0.00	22.3
7	565	-468	-1815	30	0	-95	-1250	4.02	4.02	4.02	4.02	2	0.19	0.05	0.32	0.00	0.00	22.3
8	565	-287	-1672	4	0	-23	-853	4.02	4.02	4.02	4.02	2	0.13	0.05	0.30	0.00	0.00	22.3
9	565	-291	-1669	37	0	-118	-847	4.02	4.02	4.02	4.02	2	0.13	0.05	0.30	0.00	0.00	22.3
10	565	-672	-1988	-0	0	-6	-1724	4.02	4.02	4.02	4.02	2	0.26	0.06	0.35	0.00	0.00	22.3
11	565	-673	-1987	10	0	-35	-1722	4.02	4.02	4.02	4.02	2	0.26	0.06	0.35	0.00	0.00	22.3
12	565	-82	-1500	24	0	-83	-382	4.02	4.02	4.02	4.02	2	0.06	0.04	0.27	0.00	0.00	22.3
13	565	-83	-1499	34	0	-112	-380	4.02	4.02	4.02	4.02	2	0.06	0.04	0.27	0.00	0.00	22.3
14	565	-464	-1818	-3	0	-0	-1256	4.02	4.02	4.02	4.02	2	0.19	0.05	0.32	0.00	0.00	22.3
15	565	-468	-1815	30	0	-95	-1250	4.02	4.02	4.02	4.02	2	0.19	0.05	0.32	0.00	0.00	22.3
16	565	-287	-1672	4	0	-23	-853	4.02	4.02	4.02	4.02	2	0.13	0.05	0.30	0.00	0.00	22.3
17	565	-291	-1669	37	0	-118	-847	4.02	4.02	4.02	4.02	2	0.13	0.05	0.30	0.00	0.00	22.3
18	565	-1798	-2908	10	0	-46	-3124	4.02	4.02	4.02	4.02	3	0.43	0.08	0.50	0.00	0.00	22.3
19	565	-528	-1521	68	0	-240	1488	4.02	4.02	4.02	4.02	3	0.21	0.04	0.27	0.00	0.00	22.3
20	565	-1064	-2226	83	0	-267	-1239	4.02	4.02	4.02	4.02	3	0.17	0.06	0.39	0.00	0.00	22.3
37	565	-1999	-3387	-14	0	40	-4457	4.02	4.02	4.02	4.02	3	0.60	0.10	0.58	0.00	0.00	22.3
38	565	119	-1075	82	0	-283	2491	4.02	4.02	4.02	4.02	3	0.36	0.03	0.19	0.00	0.00	22.3
39	565	-775	-2250	107	0	-329	-1316	4.02	4.02	4.02	4.02	3	0.18	0.07	0.39	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

Nome travata: **trave_503_IP1** Descrizione: **Trave_5 8-13-18-23**
ASTA NUM. 7 NI 214 NF 212 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y qy tot.
qy medio: 375.00 375.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-93	1183	-14	0	-35	-484	4.02	4.02	4.02	4.02	3	0.07	0.03	0.21	0.00	0.00	22.3
2	0	-63	874	15	0	39	-264	4.02	4.02	4.02	4.02	2	0.04	0.03	0.16	0.00	0.00	22.3
3	0	-65	875	15	0	39	-267	4.02	4.02	4.02	4.02	2	0.04	0.03	0.16	0.00	0.00	22.3
4	0	-79	944	-36	0	-93	-478	4.02	4.02	4.02	4.02	2	0.07	0.03	0.17	0.00	0.00	22.3
5	0	-81	945	-37	0	-94	-482	4.02	4.02	4.02	4.02	2	0.07	0.03	0.17	0.00	0.00	22.3
6	0	-66	897	-3	0	-7	-335	4.02	4.02	4.02	4.02	2	0.05	0.03	0.16	0.00	0.00	22.3
7	0	-72	901	-4	0	-8	-346	4.02	4.02	4.02	4.02	2	0.05	0.03	0.16	0.00	0.00	22.3
8	0	-71	918	-18	0	-46	-399	4.02	4.02	4.02	4.02	2	0.06	0.03	0.16	0.00	0.00	22.3
9	0	-77	922	-19	0	-48	-411	4.02	4.02	4.02	4.02	2	0.06	0.03	0.16	0.00	0.00	22.3
10	0	-63	874	15	0	39	-264	4.02	4.02	4.02	4.02	2	0.04	0.03	0.16	0.00	0.00	22.3
11	0	-65	875	15	0	39	-267	4.02	4.02	4.02	4.02	2	0.04	0.03	0.16	0.00	0.00	22.3
12	0	-79	944	-36	0	-93	-478	4.02	4.02	4.02	4.02	2	0.07	0.03	0.17	0.00	0.00	22.3
13	0	-81	945	-37	0	-94	-482	4.02	4.02	4.02	4.02	2	0.07	0.03	0.17	0.00	0.00	22.3
14	0	-66	897	-3	0	-7	-335	4.02	4.02	4.02	4.02	2	0.05	0.03	0.16	0.00	0.00	22.3
15	0	-72	901	-4	0	-8	-346	4.02	4.02	4.02	4.02	2	0.05	0.03	0.16	0.00	0.00	22.3
16	0	-71	918	-18	0	-46	-399	4.02	4.02	4.02	4.02	2	0.06	0.03	0.16	0.00	0.00	22.3
17	0	-77	922	-19	0	-48	-411	4.02	4.02	4.02	4.02	2	0.06	0.03	0.16	0.00	0.00	22.3
18	0	-50	1088	44	0	111	-194	4.02	4.02	4.02	4.02	3	0.03	0.03	0.19	0.00	0.00	22.3
19	0	-103	1297	-112	0	-289	-836	4.02	4.02	4.02	4.02	3	0.12	0.04	0.23	0.00	0.00	22.3
20	0	-69	1190	-40	0	-105	-508	4.02	4.02	4.02	4.02	3	0.07	0.03	0.21	0.00	0.00	22.3
37	0	-38	1015	102	0	261	544	4.02	4.02	4.02	4.02	3	0.08	0.03	0.18	0.00	0.00	22.3
38	0	-126	1364	-158	0	-405	-1040	4.02	4.02	4.02	4.02	3	0.15	0.04	0.24	0.00	0.00	22.3
39	0	-70	1186	-39	0	-100	-493	4.02	4.02	4.02	4.02	3	0.07	0.03	0.21	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	57	-93	907	-14	0	-27	565	4.02	4.02	4.02	4.02	3	0.08	0.03	0.16	0.00	0.00	22.3
2	57	-63	662	15	0	31	506	4.02	4.02	4.02	4.02	2	0.08	0.02	0.12	0.00	0.00	22.3
3	57	-65	663	15	0	30	503	4.02	4.02	4.02	4.02	2	0.08	0.02	0.12	0.00	0.00	22.3
4	57	-79	732	-36	0	-73	-375	4.02	4.02	4.02	4.02	2	0.06	0.02	0.13	0.00	0.00	22.3
5	57	-81	733	-37	0	-73	-379	4.02	4.02	4.02	4.02	2	0.06	0.02	0.13	0.00	0.00	22.3
6	57	-66	685	-3	0	-5	459	4.02	4.02	4.02	4.02	2	0.07	0.02	0.12	0.00	0.00	22.3
7	57	-72	689	-4	0	-6	452	4.02	4.02	4.02	4.02	2	0.07	0.02	0.12	0.00	0.00	22.3
8	57	-71	706	-18	0	-36	417	4.02	4.02	4.02	4.02	2	0.06	0.02	0.13	0.00	0.00	22.3
9	57	-77	710	-19	0	-37	410	4.02	4.02	4.02	4.02	2	0.06	0.02	0.13	0.00	0.00	22.3

10	57	-63	662	15	0	31	506	4.02	4.02	4.02	4.02	2	0.08	0.02	0.12	0.00	0.00	22.3
11	57	-65	663	15	0	30	503	4.02	4.02	4.02	4.02	2	0.08	0.02	0.12	0.00	0.00	22.3
12	57	-79	732	-36	0	-73	-375	4.02	4.02	4.02	4.02	2	0.06	0.02	0.13	0.00	0.00	22.3
13	57	-81	733	-37	0	-73	-379	4.02	4.02	4.02	4.02	2	0.06	0.02	0.13	0.00	0.00	22.3
14	57	-66	685	-3	0	-5	459	4.02	4.02	4.02	4.02	2	0.07	0.02	0.12	0.00	0.00	22.3
15	57	-72	689	-4	0	-6	452	4.02	4.02	4.02	4.02	2	0.07	0.02	0.12	0.00	0.00	22.3
16	57	-71	706	-18	0	-36	417	4.02	4.02	4.02	4.02	2	0.06	0.02	0.13	0.00	0.00	22.3
17	57	-77	710	-19	0	-37	410	4.02	4.02	4.02	4.02	2	0.06	0.02	0.13	0.00	0.00	22.3
18	57	-50	812	44	0	86	754	4.02	4.02	4.02	4.02	3	0.11	0.02	0.14	0.00	0.00	22.3
19	57	-103	1022	-112	0	-225	-698	4.02	4.02	4.02	4.02	3	0.10	0.03	0.18	0.00	0.00	22.3
20	57	-69	915	-40	0	-83	550	4.02	4.02	4.02	4.02	3	0.08	0.03	0.16	0.00	0.00	22.3
37	57	-38	739	102	0	203	900	4.02	4.02	4.02	4.02	3	0.13	0.02	0.13	0.00	0.00	22.3
38	57	-126	1089	-158	0	-316	-898	4.02	4.02	4.02	4.02	3	0.13	0.03	0.19	0.00	0.00	22.3
39	57	-70	910	-39	0	-78	560	4.02	4.02	4.02	4.02	3	0.08	0.03	0.16	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	113	-93	632	-14	0	-19	861	4.02	4.02	4.02	4.02	3	0.12	0.02	0.11	0.00	0.00	22.3
2	113	-63	450	15	0	22	713	4.02	4.02	4.02	4.02	2	0.11	0.01	0.08	0.00	0.00	22.3
3	113	-65	452	15	0	22	711	4.02	4.02	4.02	4.02	2	0.11	0.01	0.08	0.00	0.00	22.3
4	113	-79	520	-36	0	-52	612	4.02	4.02	4.02	4.02	2	0.09	0.02	0.09	0.00	0.00	22.3
5	113	-81	522	-37	0	-52	611	4.02	4.02	4.02	4.02	2	0.09	0.02	0.09	0.00	0.00	22.3
6	113	-66	473	-3	0	-4	679	4.02	4.02	4.02	4.02	2	0.10	0.01	0.08	0.00	0.00	22.3
7	113	-72	477	-4	0	-4	674	4.02	4.02	4.02	4.02	2	0.10	0.01	0.08	0.00	0.00	22.3
8	113	-71	494	-18	0	-26	649	4.02	4.02	4.02	4.02	2	0.10	0.01	0.09	0.00	0.00	22.3
9	113	-77	498	-19	0	-26	644	4.02	4.02	4.02	4.02	2	0.10	0.01	0.09	0.00	0.00	22.3
10	113	-63	450	15	0	22	713	4.02	4.02	4.02	4.02	2	0.11	0.01	0.08	0.00	0.00	22.3
11	113	-65	452	15	0	22	711	4.02	4.02	4.02	4.02	2	0.11	0.01	0.08	0.00	0.00	22.3
12	113	-79	520	-36	0	-52	612	4.02	4.02	4.02	4.02	2	0.09	0.02	0.09	0.00	0.00	22.3
13	113	-81	522	-37	0	-52	611	4.02	4.02	4.02	4.02	2	0.09	0.02	0.09	0.00	0.00	22.3
14	113	-66	473	-3	0	-4	679	4.02	4.02	4.02	4.02	2	0.10	0.01	0.08	0.00	0.00	22.3
15	113	-72	477	-4	0	-4	674	4.02	4.02	4.02	4.02	2	0.10	0.01	0.08	0.00	0.00	22.3
16	113	-71	494	-18	0	-26	649	4.02	4.02	4.02	4.02	2	0.10	0.01	0.09	0.00	0.00	22.3
17	113	-77	498	-19	0	-26	644	4.02	4.02	4.02	4.02	2	0.10	0.01	0.09	0.00	0.00	22.3
18	113	-50	537	44	0	61	996	4.02	4.02	4.02	4.02	3	0.14	0.02	0.10	0.00	0.00	22.3
19	113	-103	746	-112	0	-162	696	4.02	4.02	4.02	4.02	3	0.10	0.02	0.13	0.00	0.00	22.3
20	113	-69	639	-40	0	-60	850	4.02	4.02	4.02	4.02	3	0.12	0.02	0.11	0.00	0.00	22.3
37	113	-38	464	102	0	146	1078	4.02	4.02	4.02	4.02	3	0.15	0.01	0.08	0.00	0.00	22.3
38	113	-126	813	-158	0	-227	601	4.02	4.02	4.02	4.02	3	0.09	0.02	0.14	0.00	0.00	22.3
39	113	-70	635	-39	0	-56	857	4.02	4.02	4.02	4.02	3	0.12	0.02	0.11	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	170	-93	356	-14	0	-11	943	4.02	4.02	4.02	4.02	3	0.13	0.01	0.06	0.00	0.00	22.3
2	170	-63	238	15	0	14	754	4.02	4.02	4.02	4.02	2	0.11	0.01	0.04	0.00	0.00	22.3
3	170	-65	240	15	0	14	753	4.02	4.02	4.02	4.02	2	0.11	0.01	0.04	0.00	0.00	22.3
4	170	-79	308	-36	0	-31	698	4.02	4.02	4.02	4.02	2	0.11	0.01	0.05	0.00	0.00	22.3
5	170	-81	310	-37	0	-31	697	4.02	4.02	4.02	4.02	2	0.11	0.01	0.06	0.00	0.00	22.3
6	170	-66	261	-3	0	-2	735	4.02	4.02	4.02	4.02	2	0.11	0.01	0.05	0.00	0.00	22.3
7	170	-72	265	-4	0	-2	733	4.02	4.02	4.02	4.02	2	0.11	0.01	0.05	0.00	0.00	22.3
8	170	-71	282	-18	0	-16	718	4.02	4.02	4.02	4.02	2	0.11	0.01	0.05	0.00	0.00	22.3
9	170	-77	286	-19	0	-16	716	4.02	4.02	4.02	4.02	2	0.11	0.01	0.05	0.00	0.00	22.3
10	170	-63	238	15	0	14	754	4.02	4.02	4.02	4.02	2	0.11	0.01	0.04	0.00	0.00	22.3
11	170	-65	240	15	0	14	753	4.02	4.02	4.02	4.02	2	0.11	0.01	0.04	0.00	0.00	22.3
12	170	-79	308	-36	0	-31	698	4.02	4.02	4.02	4.02	2	0.11	0.01	0.05	0.00	0.00	22.3
13	170	-81	310	-37	0	-31	697	4.02	4.02	4.02	4.02	2	0.11	0.01	0.06	0.00	0.00	22.3
14	170	-66	261	-3	0	-2	735	4.02	4.02	4.02	4.02	2	0.11	0.01	0.05	0.00	0.00	22.3
15	170	-72	265	-4	0	-2	733	4.02	4.02	4.02	4.02	2	0.11	0.01	0.05	0.00	0.00	22.3
16	170	-71	282	-18	0	-16	718	4.02	4.02	4.02	4.02	2	0.11	0.01	0.05	0.00	0.00	22.3
17	170	-77	286	-19	0	-16	716	4.02	4.02	4.02	4.02	2	0.11	0.01	0.05	0.00	0.00	22.3
18	170	-50	261	44	0	36	1019	4.02	4.02	4.02	4.02	3	0.15	0.01	0.05	0.00	0.00	22.3
19	170	-103	471	-112	0	-99	884	4.02	4.02	4.02	4.02	3	0.13	0.01	0.08	0.00	0.00	22.3
20	170	-69	364	-40	0	-37	938	4.02	4.02	4.02	4.02	3	0.13	0.01	0.06	0.00	0.00	22.3
37	170	-38	188	102	0	88	1078	4.02	4.02	4.02	4.02	3	0.15	0.01	0.03	0.00	0.00	22.3
38	170	-126	538	-158	0	-138	843	4.02	4.02	4.02	4.02	3	0.12	0.02	0.10	0.00	0.00	22.3
39	170	-70	359	-39	0	-34	942	4.02	4.02	4.02	4.02	3	0.13	0.01	0.06	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	226	-93	81	-14	0	-3	943	4.02	4.02	4.02	4.02	3	0.13	0.00	0.01	0.00	0.00	22.3
2	226	-63	26	15	0	5	754	4.02	4.02	4.02	4.02	2	0.11	0.00	0.00	0.00	0.00	22.3
3	226	-65	28	15	0	6	753	4.02	4.02	4.02	4.02	2	0.11	0.00	0.00	0.00	0.00	22.3
4	226	-79	96	-36	0	-11	698	4.02	4.02	4.02	4.02	2	0.11	0.00	0.02	0.00	0.00	22.3
5	226	-81	98	-37	0	-11	697	4.02	4.02	4.02	4.02	2	0.11	0.00	0.02	0.00	0.00	22.3
6	226	-66	50	-3	0	-0	735	4.02	4.02	4.02	4.02	2	0.11	0.00	0.01	0.00	0.00	22.3
7	226	-72	53	-4	0	0	733	4.02	4.02	4.02	4.02	2	0.11	0.00	0.01	0.00	0.00	22.3
8	226	-71	71	-18	0	-5	718	4.02	4.02	4.02	4.02	2	0.11	0.00	0.01	0.00	0.00	22.3
9	226	-77	74	-19	0	-5	716	4.02	4.02	4.02	4.02	2	0.11	0.00	0.01	0.00	0.00	22.3
10	226	-63	26	15	0	5	754	4.02	4.02	4.02	4.02	2	0.11	0.00	0.00	0.00	0.00	22.3
11	226	-65	28	15	0	6	753	4.02	4.02	4.02	4.02	2	0.11	0.00	0.00	0.00	0.00	22.3
12	226	-79	96	-36	0	-11	698	4.02	4.02	4.02	4.02	2	0.11	0.00	0.02	0.00	0.00	22.3
13	226	-81	98	-37	0	-11	697	4.02	4.02	4.02	4.02	2	0.11	0.00	0.02	0.00	0.00	22.3
14	226	-66	50	-3	0	-0	735	4.02	4.02	4.02	4.02	2	0.11	0.00	0.01	0.00	0.00	22.3
15	226	-72	53	-4	0	0	733	4.02	4.02	4.02	4.02	2	0.11	0.00	0.01	0.00	0.00	22.3
16	226	-71	71	-18	0	-5	718	4.02	4.02	4.02	4.02	2	0.11	0.00	0.01	0.00	0.00	22.3
17	226	-77	74	-19	0	-5	716	4.02	4.02	4.02	4.02	2	0.11	0.00	0.01	0.00	0.00	22.3
18	226	-50	-14	44	0	11	1019	4.02	4.02	4.02	4.02	3	0.15	0.00	0.00	0.00	0.00	22.3
19	226	-103	195	-112	0	-36	884	4.02	4.02	4.02	4.02	3	0.13	0.01	0.03	0.00	0.00	22.3
20	226	-69	88	-40	0	-14	938	4.02	4.02	4.02	4.02	3	0.13	0.00	0.02	0.00	0.00	22.3
37	226	-38	-87	102	0	30	1078	4.02	4.02	4.02	4.02	3	0.15	0.00	0.02	0.00	0.00	22.3
38	226	-126	262	-158	0	-49	867	4.02	4.02	4.02	4.02	3	0.12	0.01	0.05	0.00	0.00	22.3
39	226	-70	84	-39	0	-12	942	4.02	4.02	4.02	4.02	3	0.13	0.00	0.01	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	283	-93	-194	-14	0	5	943	4.02	4.02	4.02	4.02	3	0.13	0.01	0.03	0.00	0.00	22.3
2	283	-63	-185	15	0	-3	754	4.02	4.02	4.02	4.02	2	0.11	0.01	0.03	0.00	0.00	22.3
3	283	-65	-184	15	0	-3	753	4.02	4.02	4.02	4.02	2	0.11	0.01	0.03	0.00	0.00	22.3
4	283	-79	-115	-36	0	10	698	4.02	4.02	4.02	4.02	2	0.11	0.00	0.02	0.00	0.00	22.3
5	283	-81	-114	-37	0	10	697	4.02	4.02	4.02	4.02	2	0.11	0.00	0.02	0.00	0.00	22.3
6	283	-66	-162	-3	0	1	735	4.02	4.02	4.02	4.02	2	0.11	0.00	0.03	0.00	0.00	22.3
7	283	-72	-158	-4	0	2	733	4.02	4.02	4.02	4.02	2	0.11	0.00	0.03	0.00	0.00	22.3
8	283	-71	-141	-18	0	5	718	4.02	4.02	4.02	4.02	2	0.11	0.00	0.03	0.00	0.00	22.3
9	283	-77	-137	-19	0	6	716	4.02	4.02	4.02	4.02	2	0.11	0.00	0.02	0.00	0.00	22.3
10	283	-63	-185	15	0	-3	754	4.02	4.02	4.02	4.02	2	0.11	0.01	0.03	0.00	0.00	22.3
11	283	-65	-184	15	0	-3	753	4.02	4.02	4.02	4.02	2	0.11	0.01	0.03	0.00	0.00	22.3
12	283	-79	-115	-36	0	10	698	4.02	4.02	4.02	4.02	2	0.11	0.00	0.02	0.00	0.00	22.3
13	283	-81	-114	-37	0	10	697	4.02	4.02	4.02	4.02	2	0.11	0.00	0.02	0.00	0.00	22.3
14	283	-66	-162	-3	0	1	735	4.02	4.02	4.02	4.02	2	0.11	0.00	0.03	0.00	0.00	22.3
15	283	-72	-158	-4	0	2	733	4.02	4.02	4.02	4.02	2	0.11	0.00	0.03	0.00	0.00	22.3

16	283	-71	-141	-18	0	5	718	4.02	4.02	4.02	4.02	2	0.11	0.00	0.03	0.00	0.00	22.3
17	283	-77	-137	-19	0	6	716	4.02	4.02	4.02	4.02	2	0.11	0.00	0.02	0.00	0.00	22.3
18	283	-50	-290	44	0	-13	1019	4.02	4.02	4.02	4.02	3	0.15	0.01	0.05	0.00	0.00	22.3
19	283	-103	-80	-112	0	27	884	4.02	4.02	4.02	4.02	3	0.13	0.00	0.01	0.00	0.00	22.3
20	283	-69	-187	-40	0	9	938	4.02	4.02	4.02	4.02	3	0.13	0.01	0.03	0.00	0.00	22.3
37	283	-38	-362	102	0	-28	1078	4.02	4.02	4.02	4.02	3	0.15	0.01	0.06	0.00	0.00	22.3
38	283	-126	-13	-158	0	40	867	4.02	4.02	4.02	4.02	3	0.12	0.00	0.03	0.00	0.00	22.3
39	283	-70	-192	-39	0	10	942	4.02	4.02	4.02	4.02	3	0.13	0.01	0.03	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	339	-93	-470	-14	0	13	943	4.02	4.02	4.02	4.02	3	0.13	0.01	0.08	0.00	0.00	22.3
2	339	-63	-397	15	0	-11	746	4.02	4.02	4.02	4.02	2	0.11	0.01	0.07	0.00	0.00	22.3
3	339	-65	-396	15	0	-11	746	4.02	4.02	4.02	4.02	2	0.11	0.01	0.07	0.00	0.00	22.3
4	339	-79	-327	-36	0	30	698	4.02	4.02	4.02	4.02	2	0.11	0.01	0.06	0.00	0.00	22.3
5	339	-81	-326	-37	0	31	697	4.02	4.02	4.02	4.02	2	0.11	0.01	0.06	0.00	0.00	22.3
6	339	-66	-374	-3	0	3	735	4.02	4.02	4.02	4.02	2	0.11	0.01	0.07	0.00	0.00	22.3
7	339	-72	-370	-4	0	4	733	4.02	4.02	4.02	4.02	2	0.11	0.01	0.07	0.00	0.00	22.3
8	339	-71	-353	-18	0	15	718	4.02	4.02	4.02	4.02	2	0.11	0.01	0.06	0.00	0.00	22.3
9	339	-77	-349	-19	0	17	716	4.02	4.02	4.02	4.02	2	0.11	0.01	0.06	0.00	0.00	22.3
10	339	-63	-397	15	0	-11	746	4.02	4.02	4.02	4.02	2	0.11	0.01	0.07	0.00	0.00	22.3
11	339	-65	-396	15	0	-11	746	4.02	4.02	4.02	4.02	2	0.11	0.01	0.07	0.00	0.00	22.3
12	339	-79	-327	-36	0	30	698	4.02	4.02	4.02	4.02	2	0.11	0.01	0.06	0.00	0.00	22.3
13	339	-81	-326	-37	0	31	697	4.02	4.02	4.02	4.02	2	0.11	0.01	0.06	0.00	0.00	22.3
14	339	-66	-374	-3	0	3	735	4.02	4.02	4.02	4.02	2	0.11	0.01	0.07	0.00	0.00	22.3
15	339	-72	-370	-4	0	4	733	4.02	4.02	4.02	4.02	2	0.11	0.01	0.07	0.00	0.00	22.3
16	339	-71	-353	-18	0	15	718	4.02	4.02	4.02	4.02	2	0.11	0.01	0.06	0.00	0.00	22.3
17	339	-77	-349	-19	0	17	716	4.02	4.02	4.02	4.02	2	0.11	0.01	0.06	0.00	0.00	22.3
18	339	-50	-565	44	0	-38	978	4.02	4.02	4.02	4.02	3	0.14	0.02	0.10	0.00	0.00	22.3
19	339	-103	-355	-112	0	90	884	4.02	4.02	4.02	4.02	3	0.13	0.01	0.06	0.00	0.00	22.3
20	339	-69	-462	-40	0	32	938	4.02	4.02	4.02	4.02	3	0.13	0.01	0.08	0.00	0.00	22.3
37	339	-38	-638	102	0	-85	992	4.02	4.02	4.02	4.02	3	0.14	0.02	0.11	0.00	0.00	22.3
38	339	-126	-288	-158	0	129	867	4.02	4.02	4.02	4.02	3	0.12	0.01	0.05	0.00	0.00	22.3
39	339	-70	-467	-39	0	32	942	4.02	4.02	4.02	4.02	3	0.13	0.01	0.08	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	396	-93	-746	-14	0	21	757	4.02	4.02	4.02	4.02	3	0.11	0.02	0.13	0.00	0.00	22.3
2	396	-63	-609	15	0	-20	569	4.02	4.02	4.02	4.02	2	0.09	0.02	0.11	0.00	0.00	22.3
3	396	-65	-608	15	0	-19	569	4.02	4.02	4.02	4.02	2	0.09	0.02	0.11	0.00	0.00	22.3
4	396	-79	-539	-36	0	51	595	4.02	4.02	4.02	4.02	2	0.09	0.02	0.10	0.00	0.00	22.3
5	396	-81	-538	-37	0	51	596	4.02	4.02	4.02	4.02	2	0.09	0.02	0.10	0.00	0.00	22.3
6	396	-66	-586	-3	0	4	578	4.02	4.02	4.02	4.02	2	0.09	0.02	0.10	0.00	0.00	22.3
7	396	-72	-582	-4	0	6	580	4.02	4.02	4.02	4.02	2	0.09	0.02	0.10	0.00	0.00	22.3
8	396	-71	-565	-18	0	26	585	4.02	4.02	4.02	4.02	2	0.09	0.02	0.10	0.00	0.00	22.3
9	396	-77	-561	-19	0	27	588	4.02	4.02	4.02	4.02	2	0.09	0.02	0.10	0.00	0.00	22.3
10	396	-63	-609	15	0	-20	569	4.02	4.02	4.02	4.02	2	0.09	0.02	0.11	0.00	0.00	22.3
11	396	-65	-608	15	0	-19	569	4.02	4.02	4.02	4.02	2	0.09	0.02	0.11	0.00	0.00	22.3
12	396	-79	-539	-36	0	51	595	4.02	4.02	4.02	4.02	2	0.09	0.02	0.10	0.00	0.00	22.3
13	396	-81	-538	-37	0	51	596	4.02	4.02	4.02	4.02	2	0.09	0.02	0.10	0.00	0.00	22.3
14	396	-66	-586	-3	0	4	578	4.02	4.02	4.02	4.02	2	0.09	0.02	0.10	0.00	0.00	22.3
15	396	-72	-582	-4	0	6	580	4.02	4.02	4.02	4.02	2	0.09	0.02	0.10	0.00	0.00	22.3
16	396	-71	-565	-18	0	26	585	4.02	4.02	4.02	4.02	2	0.09	0.02	0.10	0.00	0.00	22.3
17	396	-77	-561	-19	0	27	588	4.02	4.02	4.02	4.02	2	0.09	0.02	0.10	0.00	0.00	22.3
18	396	-50	-841	44	0	-63	721	4.02	4.02	4.02	4.02	3	0.10	0.02	0.15	0.00	0.00	22.3
19	396	-103	-631	-112	0	153	802	4.02	4.02	4.02	4.02	3	0.11	0.02	0.11	0.00	0.00	22.3
20	396	-69	-738	-40	0	55	761	4.02	4.02	4.02	4.02	3	0.11	0.02	0.13	0.00	0.00	22.3
37	396	-38	-914	102	0	-143	693	4.02	4.02	4.02	4.02	3	0.10	0.03	0.16	0.00	0.00	22.3
38	396	-126	-564	-158	0	218	826	4.02	4.02	4.02	4.02	3	0.12	0.02	0.10	0.00	0.00	22.3
39	396	-70	-743	-39	0	53	760	4.02	4.02	4.02	4.02	3	0.11	0.02	0.13	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	452	-93	-1021	-14	0	29	-636	4.02	4.02	4.02	4.02	3	0.09	0.03	0.18	0.00	0.00	22.3
2	452	-63	-821	15	0	-28	-559	4.02	4.02	4.02	4.02	2	0.08	0.02	0.15	0.00	0.00	22.3
3	452	-65	-819	15	0	-27	-556	4.02	4.02	4.02	4.02	2	0.08	0.02	0.15	0.00	0.00	22.3
4	452	-79	-751	-36	0	72	-422	4.02	4.02	4.02	4.02	2	0.06	0.02	0.13	0.00	0.00	22.3
5	452	-81	-749	-37	0	72	-419	4.02	4.02	4.02	4.02	2	0.06	0.02	0.13	0.00	0.00	22.3
6	452	-66	-798	-3	0	6	-514	4.02	4.02	4.02	4.02	2	0.08	0.02	0.14	0.00	0.00	22.3
7	452	-72	-794	-4	0	8	-506	4.02	4.02	4.02	4.02	2	0.08	0.02	0.14	0.00	0.00	22.3
8	452	-71	-777	-18	0	36	-473	4.02	4.02	4.02	4.02	2	0.07	0.02	0.14	0.00	0.00	22.3
9	452	-77	-773	-19	0	38	-465	4.02	4.02	4.02	4.02	2	0.07	0.02	0.14	0.00	0.00	22.3
10	452	-63	-821	15	0	-28	-559	4.02	4.02	4.02	4.02	2	0.08	0.02	0.15	0.00	0.00	22.3
11	452	-65	-819	15	0	-27	-556	4.02	4.02	4.02	4.02	2	0.08	0.02	0.15	0.00	0.00	22.3
12	452	-79	-751	-36	0	72	-422	4.02	4.02	4.02	4.02	2	0.06	0.02	0.13	0.00	0.00	22.3
13	452	-81	-749	-37	0	72	-419	4.02	4.02	4.02	4.02	2	0.06	0.02	0.13	0.00	0.00	22.3
14	452	-66	-798	-3	0	6	-514	4.02	4.02	4.02	4.02	2	0.08	0.02	0.14	0.00	0.00	22.3
15	452	-72	-794	-4	0	8	-506	4.02	4.02	4.02	4.02	2	0.08	0.02	0.14	0.00	0.00	22.3
16	452	-71	-777	-18	0	36	-473	4.02	4.02	4.02	4.02	2	0.07	0.02	0.14	0.00	0.00	22.3
17	452	-77	-773	-19	0	38	-465	4.02	4.02	4.02	4.02	2	0.07	0.02	0.14	0.00	0.00	22.3
18	452	-50	-1116	44	0	-88	-822	4.02	4.02	4.02	4.02	3	0.12	0.03	0.20	0.00	0.00	22.3
19	452	-103	-906	-112	0	216	507	4.02	4.02	4.02	4.02	3	0.07	0.03	0.16	0.00	0.00	22.3
20	452	-69	-1013	-40	0	77	-620	4.02	4.02	4.02	4.02	3	0.09	0.03	0.18	0.00	0.00	22.3
37	452	-38	-1189	102	0	-201	-965	4.02	4.02	4.02	4.02	3	0.14	0.03	0.21	0.00	0.00	22.3
38	452	-126	-839	-158	0	307	569	4.02	4.02	4.02	4.02	3	0.08	0.02	0.15	0.00	0.00	22.3
39	452	-70	-1018	-39	0	75	-629	4.02	4.02	4.02	4.02	3	0.09	0.03	0.18	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	509	-93	-1296	-14	0	37	-1430	4.02	4.02	4.02	4.02	3	0.20	0.04	0.23	0.00	0.00	22.3
2	509	-63	-1033	15	0	-37	-1190	4.02	4.02	4.02	4.02	2	0.18	0.03	0.18	0.00	0.00	22.3
3	509	-65	-1031	15	0	-36	-1186	4.02	4.02	4.02	4.02	2	0.18	0.03	0.18	0.00	0.00	22.3
4	509	-79	-963	-36	0	92	-1014	4.02	4.02	4.02	4.02	2	0.15	0.03	0.17	0.00	0.00	22.3
5	509	-81	-961	-37	0	93	-1009	4.02	4.02	4.02	4.02	2	0.15	0.03	0.17	0.00	0.00	22.3
6	509	-66	-1010	-3	0	8	-1132	4.02	4.02	4.02	4.02	2	0.17	0.03	0.18	0.00	0.00	22.3
7	509	-72	-1006	-4	0	10	-1121	4.02	4.02	4.02	4.02	2	0.17	0.03	0.18	0.00	0.00	22.3
8	509	-71	-989	-18	0	46	-1079	4.02	4.02	4.02	4.02	2	0.16	0.03	0.18	0.00	0.00	22.3
9	509	-77	-985	-19	0	49	-1068	4.02	4.02	4.02	4.02	2	0.16	0.03	0.18	0.00	0.00	22.3
10	509	-63	-1033	15	0	-37	-1190	4.02	4.02	4.02	4.02	2	0.18	0.03	0.18	0.00	0.00	22.3
11	509	-65	-1031	15	0	-36	-1186	4.02	4.02	4.02	4.02	2	0.18	0.03	0.18	0.00	0.00	22.3
12	509	-79	-963	-36	0	92	-1014	4.02	4.02	4.02	4.02	2	0.15	0.03	0.17	0.00	0.00	22.3
13	509	-81	-961	-37	0	93	-1009	4.02	4.02	4.02	4.02	2	0.15	0.03	0.17	0.00	0.00	22.3
14	509	-66	-1010	-3	0	8	-1132	4.02	4.02	4.02	4.02	2	0.17	0.03	0.18	0.00	0.00	22.3
15	509	-72	-1006	-4	0	10	-1121	4.02	4.02	4.02	4.02	2	0.17	0.03	0.18	0.00	0.00	22.3
16	509	-71	-989	-18	0	46	-1079	4.02	4.02	4.02	4.02	2	0.16	0.03	0.18	0.00	0.00	22.3
17	509	-77	-985	-19	0	49	-1068	4.02	4.02	4.02	4.02	2	0.16	0.03	0.18	0.00	0.00	22.3
18	509	-50	-1392	44	0	-113	-1670	4.02	4.02	4.02	4.02	3	0.24	0.04	0.25	0.00	0.00	22.3
19	509	-103	-1182	-112	0	280	-1140	4.02	4.02	4.02	4.02	3	0.16	0.03	0.21	0.00	0.00	22.3
20	509	-69	-1289	-40	0	100	-1410	4.02	4.02	4.02	4.02	3	0.20	0.04	0.23	0.00	0.00	22.3
37	509	-38	-1464	102	0	-258	-1854	4.02	4.02	4.02	4.02	3	0.27	0.04	0.26	0.00	0.00	22.3

38	509	-126	-1115	-158	0	396	-972	4.02	4.02	4.02	4.02	3	0.14	0.03	0.20	0.00	0.00	22.3
39	509	-70	-1294	-39	0	97	-1421	4.02	4.02	4.02	4.02	3	0.20	0.04	0.23	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	565	-93	-1572	-14	0	45	-1584	4.02	4.02	4.02	4.02	3	0.23	0.05	0.28	0.00	0.00	22.3
2	565	-63	-1245	15	0	-45	-1310	4.02	4.02	4.02	4.02	2	0.20	0.04	0.22	0.00	0.00	22.3
3	565	-65	-1243	15	0	-44	-1307	4.02	4.02	4.02	4.02	2	0.20	0.04	0.22	0.00	0.00	22.3
4	565	-79	-1175	-36	0	113	-1130	4.02	4.02	4.02	4.02	2	0.17	0.03	0.21	0.00	0.00	22.3
5	565	-81	-1173	-37	0	114	-1126	4.02	4.02	4.02	4.02	2	0.17	0.03	0.21	0.00	0.00	22.3
6	565	-66	-1222	-3	0	9	-1251	4.02	4.02	4.02	4.02	2	0.19	0.04	0.22	0.00	0.00	22.3
7	565	-72	-1218	-4	0	12	-1240	4.02	4.02	4.02	4.02	2	0.19	0.04	0.22	0.00	0.00	22.3
8	565	-71	-1201	-18	0	56	-1197	4.02	4.02	4.02	4.02	2	0.18	0.03	0.21	0.00	0.00	22.3
9	565	-77	-1197	-19	0	60	-1186	4.02	4.02	4.02	4.02	2	0.18	0.03	0.21	0.00	0.00	22.3
10	565	-63	-1245	15	0	-45	-1310	4.02	4.02	4.02	4.02	2	0.20	0.04	0.22	0.00	0.00	22.3
11	565	-65	-1243	15	0	-44	-1307	4.02	4.02	4.02	4.02	2	0.20	0.04	0.22	0.00	0.00	22.3
12	565	-79	-1175	-36	0	113	-1130	4.02	4.02	4.02	4.02	2	0.17	0.03	0.21	0.00	0.00	22.3
13	565	-81	-1173	-37	0	114	-1126	4.02	4.02	4.02	4.02	2	0.17	0.03	0.21	0.00	0.00	22.3
14	565	-66	-1222	-3	0	9	-1251	4.02	4.02	4.02	4.02	2	0.19	0.04	0.22	0.00	0.00	22.3
15	565	-72	-1218	-4	0	12	-1240	4.02	4.02	4.02	4.02	2	0.19	0.04	0.22	0.00	0.00	22.3
16	565	-71	-1201	-18	0	56	-1197	4.02	4.02	4.02	4.02	2	0.18	0.03	0.21	0.00	0.00	22.3
17	565	-77	-1197	-19	0	60	-1186	4.02	4.02	4.02	4.02	2	0.18	0.03	0.21	0.00	0.00	22.3
18	565	-50	-1667	44	0	-138	-1829	4.02	4.02	4.02	4.02	3	0.26	0.05	0.30	0.00	0.00	22.3
19	565	-103	-1457	-112	0	343	-1287	4.02	4.02	4.02	4.02	3	0.18	0.04	0.26	0.00	0.00	22.3
20	565	-69	-1564	-40	0	123	-1563	4.02	4.02	4.02	4.02	3	0.22	0.05	0.28	0.00	0.00	22.3
37	565	-38	-1740	102	0	-316	-2018	4.02	4.02	4.02	4.02	3	0.29	0.05	0.31	0.00	0.00	22.3
38	565	-126	-1390	-158	0	485	-1116	4.02	4.02	4.02	4.02	3	0.16	0.04	0.25	0.00	0.00	22.3
39	565	-70	-1569	-39	0	119	-1575	4.02	4.02	4.02	4.02	3	0.23	0.05	0.28	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

Nome travata: **trave_503_IP1** Descrizione: **Trave_5 8-13-18-23**
ASTA NUM. 8 NI 212 NF 123 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y qy tot.
qy medio: 375.00 375.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-21	1377	22	0	55	-1386	4.02	4.02	4.02	4.02	3	0.20	0.04	0.25	0.00	0.00	22.3
2	0	-28	1024	47	0	130	-975	4.02	4.02	4.02	4.02	2	0.15	0.03	0.18	0.00	0.00	22.3
3	0	-31	1024	47	0	130	-975	4.02	4.02	4.02	4.02	2	0.15	0.03	0.18	0.00	0.00	22.3
4	0	-2	1094	-13	0	-45	-1158	4.02	4.02	4.02	4.02	2	0.18	0.03	0.19	0.00	0.00	22.3
5	0	-4	1094	-14	0	-44	-1157	4.02	4.02	4.02	4.02	2	0.18	0.03	0.19	0.00	0.00	22.3
6	0	-16	1048	26	0	68	-1040	4.02	4.02	4.02	4.02	2	0.16	0.03	0.19	0.00	0.00	22.3
7	0	-24	1049	26	0	70	-1038	4.02	4.02	4.02	4.02	2	0.16	0.03	0.19	0.00	0.00	22.3
8	0	-8	1069	8	0	15	-1094	4.02	4.02	4.02	4.02	2	0.17	0.03	0.19	0.00	0.00	22.3
9	0	-16	1070	8	0	18	-1093	4.02	4.02	4.02	4.02	2	0.17	0.03	0.19	0.00	0.00	22.3
10	0	-28	1024	47	0	130	-975	4.02	4.02	4.02	4.02	2	0.15	0.03	0.18	0.00	0.00	22.3
11	0	-31	1024	47	0	130	-975	4.02	4.02	4.02	4.02	2	0.15	0.03	0.18	0.00	0.00	22.3
12	0	-2	1094	-13	0	-45	-1158	4.02	4.02	4.02	4.02	2	0.18	0.03	0.19	0.00	0.00	22.3
13	0	-4	1094	-14	0	-44	-1157	4.02	4.02	4.02	4.02	2	0.18	0.03	0.19	0.00	0.00	22.3
14	0	-16	1048	26	0	68	-1040	4.02	4.02	4.02	4.02	2	0.16	0.03	0.19	0.00	0.00	22.3
15	0	-24	1049	26	0	70	-1038	4.02	4.02	4.02	4.02	2	0.16	0.03	0.19	0.00	0.00	22.3
16	0	-8	1069	8	0	15	-1094	4.02	4.02	4.02	4.02	2	0.17	0.03	0.19	0.00	0.00	22.3
17	0	-16	1070	8	0	18	-1093	4.02	4.02	4.02	4.02	2	0.17	0.03	0.19	0.00	0.00	22.3
18	0	-36	1278	130	0	363	-1131	4.02	4.02	4.02	4.02	3	0.16	0.04	0.23	0.00	0.00	22.3
19	0	46	1486	-60	0	-185	-1672	4.02	4.02	4.02	4.02	3	0.24	0.04	0.26	0.00	0.00	22.3
20	0	12	1379	42	0	116	-1392	4.02	4.02	4.02	4.02	3	0.20	0.04	0.25	0.00	0.00	22.3
37	0	-71	1207	190	0	535	-946	4.02	4.02	4.02	4.02	3	0.14	0.03	0.21	0.00	0.00	22.3
38	0	65	1554	-128	0	-379	-1847	4.02	4.02	4.02	4.02	3	0.27	0.05	0.28	0.00	0.00	22.3
39	0	9	1376	42	0	123	-1382	4.02	4.02	4.02	4.02	3	0.20	0.04	0.25	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	57	-21	1102	22	0	43	-1244	4.02	4.02	4.02	4.02	3	0.18	0.03	0.20	0.00	0.00	22.3
2	57	-28	812	47	0	103	-868	4.02	4.02	4.02	4.02	2	0.13	0.02	0.14	0.00	0.00	22.3
3	57	-31	812	47	0	104	-867	4.02	4.02	4.02	4.02	2	0.13	0.02	0.14	0.00	0.00	22.3
4	57	-2	882	-13	0	-38	-1046	4.02	4.02	4.02	4.02	2	0.16	0.03	0.16	0.00	0.00	22.3
5	57	-4	882	-14	0	-37	-1045	4.02	4.02	4.02	4.02	2	0.16	0.03	0.16	0.00	0.00	22.3
6	57	-16	836	26	0	53	-931	4.02	4.02	4.02	4.02	2	0.14	0.02	0.15	0.00	0.00	22.3
7	57	-24	837	26	0	56	-929	4.02	4.02	4.02	4.02	2	0.14	0.02	0.15	0.00	0.00	22.3
8	57	-8	857	8	0	11	-984	4.02	4.02	4.02	4.02	2	0.15	0.02	0.15	0.00	0.00	22.3
9	57	-16	858	8	0	14	-983	4.02	4.02	4.02	4.02	2	0.15	0.02	0.15	0.00	0.00	22.3
10	57	-28	812	47	0	103	-868	4.02	4.02	4.02	4.02	2	0.13	0.02	0.14	0.00	0.00	22.3
11	57	-31	812	47	0	104	-867	4.02	4.02	4.02	4.02	2	0.13	0.02	0.14	0.00	0.00	22.3
12	57	-2	882	-13	0	-38	-1046	4.02	4.02	4.02	4.02	2	0.16	0.03	0.16	0.00	0.00	22.3
13	57	-4	882	-14	0	-37	-1045	4.02	4.02	4.02	4.02	2	0.16	0.03	0.16	0.00	0.00	22.3
14	57	-16	836	26	0	53	-931	4.02	4.02	4.02	4.02	2	0.14	0.02	0.15	0.00	0.00	22.3
15	57	-24	837	26	0	56	-929	4.02	4.02	4.02	4.02	2	0.14	0.02	0.15	0.00	0.00	22.3
16	57	-8	857	8	0	11	-984	4.02	4.02	4.02	4.02	2	0.15	0.02	0.15	0.00	0.00	22.3
17	57	-16	858	8	0	14	-983	4.02	4.02	4.02	4.02	2	0.15	0.02	0.15	0.00	0.00	22.3
18	57	-36	1003	130	0	289	-994	4.02	4.02	4.02	4.02	3	0.14	0.03	0.18	0.00	0.00	22.3
19	57	46	1211	-60	0	-151	-1523	4.02	4.02	4.02	4.02	3	0.22	0.04	0.22	0.00	0.00	22.3
20	57	12	1104	42	0	92	-1249	4.02	4.02	4.02	4.02	3	0.18	0.03	0.20	0.00	0.00	22.3
37	57	-71	932	190	0	428	-814	4.02	4.02	4.02	4.02	3	0.12	0.03	0.17	0.00	0.00	22.3
38	57	65	1278	-128	0	-307	-1694	4.02	4.02	4.02	4.02	3	0.24	0.04	0.23	0.00	0.00	22.3
39	57	9	1100	42	0	99	-1240	4.02	4.02	4.02	4.02	3	0.18	0.03	0.20	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	113	-21	826	22	0	31	-560	4.02	4.02	4.02	4.02	3	0.08	0.02	0.15	0.00	0.00	22.3
2	113	-28	600	47	0	76	-362	4.02	4.02	4.02	4.02	2	0.05	0.02	0.11	0.00	0.00	22.3
3	113	-31	600	47	0	77	-361	4.02	4.02	4.02	4.02	2	0.05	0.02	0.11	0.00	0.00	22.3
4	113	-2	670	-13	0	-30	-501	4.02	4.02	4.02	4.02	2	0.08	0.02	0.12	0.00	0.00	22.3
5	113	-4	670	-14	0	-29	-499	4.02	4.02	4.02	4.02	2	0.08	0.02	0.12	0.00	0.00	22.3
6	113	-16	624	26	0	38	-411	4.02	4.02	4.02	4.02	2	0.06	0.02	0.11	0.00	0.00	22.3
7	113	-24	625	26	0	41	-409	4.02	4.02	4.02	4.02	2	0.06	0.02	0.11	0.00	0.00	22.3
8	113	-8	645	8	0	6	-452	4.02	4.02	4.02	4.02	2	0.07	0.02	0.11	0.00	0.00	22.3
9	113	-16	646	8	0	9	-451	4.02	4.02	4.02	4.02	2	0.07	0.02	0.12	0.00	0.00	22.3
10	113	-28	600	47	0	76	-362	4.02	4.02	4.02	4.02	2	0.05	0.02	0.11	0.00	0.00	22.3
11	113	-31	600	47	0	77	-361	4.02	4.02	4.02	4.02	2	0.05	0.02	0.11	0.00	0.00	22.3
12	113	-2	670	-13	0	-30	-501	4.02	4.02	4.02	4.02	2	0.08	0.02	0.12	0.00	0.00	22.3
13	113	-4	670	-14	0	-29	-499	4.02	4.02	4.02	4.02	2	0.08	0.02	0.12	0.00	0.00	22.3

14	113	-16	624	26	0	38	-411	4.02	4.02	4.02	4.02	2	0.06	0.02	0.11	0.00	0.00	22.3
15	113	-24	625	26	0	41	-409	4.02	4.02	4.02	4.02	2	0.06	0.02	0.11	0.00	0.00	22.3
16	113	-8	645	8	0	6	-452	4.02	4.02	4.02	4.02	2	0.07	0.02	0.11	0.00	0.00	22.3
17	113	-16	646	8	0	9	-451	4.02	4.02	4.02	4.02	2	0.07	0.02	0.12	0.00	0.00	22.3
18	113	-36	727	130	0	215	370	4.02	4.02	4.02	4.02	3	0.05	0.02	0.13	0.00	0.00	22.3
19	113	46	935	-60	0	-118	-777	4.02	4.02	4.02	4.02	3	0.11	0.03	0.17	0.00	0.00	22.3
20	113	12	828	42	0	69	-564	4.02	4.02	4.02	4.02	3	0.08	0.02	0.15	0.00	0.00	22.3
37	113	-71	656	190	0	320	439	4.02	4.02	4.02	4.02	3	0.08	0.02	0.12	0.00	0.00	22.3
38	113	65	1003	-128	0	-235	-910	4.02	4.02	4.02	4.02	3	0.13	0.03	0.18	0.00	0.00	22.3
39	113	9	825	42	0	76	-556	4.02	4.02	4.02	4.02	3	0.08	0.02	0.15	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	170	-21	550	22	0	18	526	4.02	4.02	4.02	4.02	3	0.08	0.02	0.10	0.00	0.00	22.3
2	170	-28	388	47	0	50	418	4.02	4.02	4.02	4.02	2	0.06	0.01	0.07	0.00	0.00	22.3
3	170	-31	388	47	0	51	418	4.02	4.02	4.02	4.02	2	0.06	0.01	0.07	0.00	0.00	22.3
4	170	-2	458	-13	0	-22	390	4.02	4.02	4.02	4.02	2	0.06	0.01	0.08	0.00	0.00	22.3
5	170	-4	458	-14	0	-21	391	4.02	4.02	4.02	4.02	2	0.06	0.01	0.08	0.00	0.00	22.3
6	170	-16	412	26	0	23	407	4.02	4.02	4.02	4.02	2	0.06	0.01	0.07	0.00	0.00	22.3
7	170	-24	413	26	0	27	410	4.02	4.02	4.02	4.02	2	0.06	0.01	0.07	0.00	0.00	22.3
8	170	-8	433	8	0	2	399	4.02	4.02	4.02	4.02	2	0.06	0.01	0.08	0.00	0.00	22.3
9	170	-16	434	8	0	5	401	4.02	4.02	4.02	4.02	2	0.06	0.01	0.08	0.00	0.00	22.3
10	170	-28	388	47	0	50	418	4.02	4.02	4.02	4.02	2	0.06	0.01	0.07	0.00	0.00	22.3
11	170	-31	388	47	0	51	418	4.02	4.02	4.02	4.02	2	0.06	0.01	0.07	0.00	0.00	22.3
12	170	-2	458	-13	0	-22	390	4.02	4.02	4.02	4.02	2	0.06	0.01	0.08	0.00	0.00	22.3
13	170	-4	458	-14	0	-21	391	4.02	4.02	4.02	4.02	2	0.06	0.01	0.08	0.00	0.00	22.3
14	170	-16	412	26	0	23	407	4.02	4.02	4.02	4.02	2	0.06	0.01	0.07	0.00	0.00	22.3
15	170	-24	413	26	0	27	410	4.02	4.02	4.02	4.02	2	0.06	0.01	0.07	0.00	0.00	22.3
16	170	-8	433	8	0	2	399	4.02	4.02	4.02	4.02	2	0.06	0.01	0.08	0.00	0.00	22.3
17	170	-16	434	8	0	5	401	4.02	4.02	4.02	4.02	2	0.06	0.01	0.08	0.00	0.00	22.3
18	170	-36	452	130	0	142	535	4.02	4.02	4.02	4.02	3	0.08	0.01	0.08	0.00	0.00	22.3
19	170	46	660	-60	0	-84	481	4.02	4.02	4.02	4.02	3	0.07	0.02	0.12	0.00	0.00	22.3
20	170	12	553	42	0	45	525	4.02	4.02	4.02	4.02	3	0.08	0.02	0.10	0.00	0.00	22.3
37	170	-71	381	190	0	213	537	4.02	4.02	4.02	4.02	3	0.08	0.01	0.07	0.00	0.00	22.3
38	170	65	727	-128	0	-162	455	4.02	4.02	4.02	4.02	3	0.07	0.02	0.13	0.00	0.00	22.3
39	170	9	549	42	0	52	528	4.02	4.02	4.02	4.02	3	0.08	0.02	0.10	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	226	-21	275	22	0	6	557	4.02	4.02	4.02	4.02	3	0.08	0.01	0.05	0.00	0.00	22.3
2	226	-28	176	47	0	23	420	4.02	4.02	4.02	4.02	2	0.06	0.01	0.03	0.00	0.00	22.3
3	226	-31	176	47	0	24	421	4.02	4.02	4.02	4.02	2	0.06	0.01	0.03	0.00	0.00	22.3
4	226	-2	246	-13	0	-15	436	4.02	4.02	4.02	4.02	2	0.07	0.01	0.04	0.00	0.00	22.3
5	226	-4	246	-14	0	-14	437	4.02	4.02	4.02	4.02	2	0.07	0.01	0.04	0.00	0.00	22.3
6	226	-16	200	26	0	8	425	4.02	4.02	4.02	4.02	2	0.06	0.01	0.04	0.00	0.00	22.3
7	226	-24	201	26	0	12	427	4.02	4.02	4.02	4.02	2	0.06	0.01	0.04	0.00	0.00	22.3
8	226	-8	221	8	0	-3	430	4.02	4.02	4.02	4.02	2	0.07	0.01	0.04	0.00	0.00	22.3
9	226	-16	222	8	0	1	432	4.02	4.02	4.02	4.02	2	0.07	0.01	0.04	0.00	0.00	22.3
10	226	-28	176	47	0	23	420	4.02	4.02	4.02	4.02	2	0.06	0.01	0.03	0.00	0.00	22.3
11	226	-31	176	47	0	24	421	4.02	4.02	4.02	4.02	2	0.06	0.01	0.03	0.00	0.00	22.3
12	226	-2	246	-13	0	-15	436	4.02	4.02	4.02	4.02	2	0.07	0.01	0.04	0.00	0.00	22.3
13	226	-4	246	-14	0	-14	437	4.02	4.02	4.02	4.02	2	0.07	0.01	0.04	0.00	0.00	22.3
14	226	-16	200	26	0	8	425	4.02	4.02	4.02	4.02	2	0.06	0.01	0.04	0.00	0.00	22.3
15	226	-24	201	26	0	12	427	4.02	4.02	4.02	4.02	2	0.06	0.01	0.04	0.00	0.00	22.3
16	226	-8	221	8	0	-3	430	4.02	4.02	4.02	4.02	2	0.07	0.01	0.04	0.00	0.00	22.3
17	226	-16	222	8	0	1	432	4.02	4.02	4.02	4.02	2	0.07	0.01	0.04	0.00	0.00	22.3
18	226	-36	176	130	0	68	535	4.02	4.02	4.02	4.02	3	0.08	0.01	0.03	0.00	0.00	22.3
19	226	46	384	-60	0	-50	581	4.02	4.02	4.02	4.02	3	0.08	0.01	0.07	0.00	0.00	22.3
20	226	12	277	42	0	21	559	4.02	4.02	4.02	4.02	3	0.08	0.01	0.05	0.00	0.00	22.3
37	226	-71	105	190	0	106	537	4.02	4.02	4.02	4.02	3	0.08	0.01	0.03	0.00	0.00	22.3
38	226	65	452	-128	0	-90	619	4.02	4.02	4.02	4.02	3	0.09	0.01	0.08	0.00	0.00	22.3
39	226	9	274	42	0	29	559	4.02	4.02	4.02	4.02	3	0.08	0.01	0.05	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	283	-21	-0	22	0	-6	557	4.02	4.02	4.02	4.02	3	0.08	0.00	0.00	0.00	0.00	22.3
2	283	-28	-36	47	0	-4	420	4.02	4.02	4.02	4.02	2	0.06	0.00	0.01	0.00	0.00	22.3
3	283	-31	-36	47	0	-3	421	4.02	4.02	4.02	4.02	2	0.06	0.00	0.01	0.00	0.00	22.3
4	283	-2	34	-13	0	-7	436	4.02	4.02	4.02	4.02	2	0.07	0.00	0.01	0.00	0.00	22.3
5	283	-4	34	-14	0	-6	437	4.02	4.02	4.02	4.02	2	0.07	0.00	0.01	0.00	0.00	22.3
6	283	-16	-12	26	0	-6	425	4.02	4.02	4.02	4.02	2	0.06	0.00	0.00	0.00	0.00	22.3
7	283	-24	-10	26	0	-2	427	4.02	4.02	4.02	4.02	2	0.06	0.00	0.00	0.00	0.00	22.3
8	283	-8	10	8	0	-7	430	4.02	4.02	4.02	4.02	2	0.07	0.00	0.00	0.00	0.00	22.3
9	283	-16	10	8	0	-3	432	4.02	4.02	4.02	4.02	2	0.07	0.00	0.00	0.00	0.00	22.3
10	283	-28	-36	47	0	-4	420	4.02	4.02	4.02	4.02	2	0.06	0.00	0.01	0.00	0.00	22.3
11	283	-31	-36	47	0	-3	421	4.02	4.02	4.02	4.02	2	0.06	0.00	0.01	0.00	0.00	22.3
12	283	-2	34	-13	0	-7	436	4.02	4.02	4.02	4.02	2	0.07	0.00	0.01	0.00	0.00	22.3
13	283	-4	34	-14	0	-6	437	4.02	4.02	4.02	4.02	2	0.07	0.00	0.01	0.00	0.00	22.3
14	283	-16	-12	26	0	-6	425	4.02	4.02	4.02	4.02	2	0.06	0.00	0.00	0.00	0.00	22.3
15	283	-24	-10	26	0	-2	427	4.02	4.02	4.02	4.02	2	0.06	0.00	0.00	0.00	0.00	22.3
16	283	-8	10	8	0	-7	430	4.02	4.02	4.02	4.02	2	0.07	0.00	0.00	0.00	0.00	22.3
17	283	-16	10	8	0	-3	432	4.02	4.02	4.02	4.02	2	0.07	0.00	0.00	0.00	0.00	22.3
18	283	-36	-99	130	0	-6	535	4.02	4.02	4.02	4.02	3	0.08	0.00	0.02	0.00	0.00	22.3
19	283	46	109	-60	0	-17	581	4.02	4.02	4.02	4.02	3	0.08	0.00	0.02	0.00	0.00	22.3
20	283	12	2	42	0	-2	559	4.02	4.02	4.02	4.02	3	0.08	0.00	0.00	0.00	0.00	22.3
37	283	-71	-170	190	0	-1	537	4.02	4.02	4.02	4.02	3	0.08	0.01	0.03	0.00	0.00	22.3
38	283	65	176	-128	0	-18	619	4.02	4.02	4.02	4.02	3	0.09	0.01	0.03	0.00	0.00	22.3
39	283	9	-2	42	0	5	559	4.02	4.02	4.02	4.02	3	0.08	0.00	0.00	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	339	-21	-276	22	0	-19	557	4.02	4.02	4.02	4.02	3	0.08	0.01	0.05	0.00	0.00	22.3
2	339	-28	-247	47	0	-31	420	4.02	4.02	4.02	4.02	2	0.06	0.01	0.04	0.00	0.00	22.3
3	339	-31	-247	47	0	-29	421	4.02	4.02	4.02	4.02	2	0.06	0.01	0.04	0.00	0.00	22.3
4	339	-2	-177	-13	0	1	436	4.02	4.02	4.02	4.02	2	0.07	0.01	0.03	0.00	0.00	22.3
5	339	-4	-177	-14	0	2	437	4.02	4.02	4.02	4.02	2	0.07	0.01	0.03	0.00	0.00	22.3
6	339	-16	-223	26	0	-21	425	4.02	4.02	4.02	4.02	2	0.06	0.01	0.04	0.00	0.00	22.3
7	339	-24	-222	26	0	-17	427	4.02	4.02	4.02	4.02	2	0.06	0.01	0.04	0.00	0.00	22.3
8	339	-8	-202	8	0	-12	430	4.02	4.02	4.02	4.02	2	0.07	0.01	0.04	0.00	0.00	22.3
9	339	-16	-201	8	0	-8	432	4.02	4.02	4.02	4.02	2	0.07	0.01	0.04	0.00	0.00	22.3
10	339	-28	-247	47	0	-31	420	4.02	4.02	4.02	4.02	2	0.06	0.01	0.04	0.00	0.00	22.3
11	339	-31	-247	47	0	-29	421	4.02	4.02	4.02	4.02	2	0.06	0.01	0.04	0.00	0.00	22.3
12	339	-2	-177	-13	0	1	436	4.02	4.02	4.02	4.02	2	0.07	0.01	0.03	0.00	0.00	22.3
13	339	-4	-177	-14	0	2	437	4.02	4.02	4.02	4.02	2	0.07	0.01	0.03	0.00	0.00	22.3
14	339	-16	-223	26	0	-21	425	4.02	4.02	4.02	4.02	2	0.06	0.01	0.04	0.00	0.00	22.3
15	339	-24	-222	26	0	-17	427	4.02	4.02	4.02	4.02	2	0.06	0.01	0.04	0.00	0.00	22.3
16	339	-8	-202	8	0	-12	430	4.02	4.02	4.02	4.02	2	0.07	0.01	0.04	0.00	0.00	22.3
17	339	-16	-201	8	0	-8	432	4.02	4.02	4.02	4.02	2	0.07	0.01	0.04	0.00	0.00	22.3
18	339	-36	-374	130	0	-80	535	4.02	4.02	4.02	4.02	3	0.08	0.01	0.07	0.00	0.00	22.3
19	339	46	-166	-60	0	17	581	4.02	4.02	4.02	4.02	3	0.08	0.00	0.03	0.00	0.00	22.3

20	339	12	-273	42	0	-26	559	4.02	4.02	4.02	4.02	3	0.08	0.01	0.05	0.00	0.00	22.3
37	339	-71	-445	190	0	-108	537	4.02	4.02	4.02	4.02	3	0.08	0.01	0.08	0.00	0.00	22.3
38	339	65	-99	-128	0	54	619	4.02	4.02	4.02	4.02	3	0.09	0.00	0.02	0.00	0.00	22.3
39	339	9	-277	42	0	-18	559	4.02	4.02	4.02	4.02	3	0.08	0.01	0.05	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	396	-21	-552	22	0	-31	524	4.02	4.02	4.02	4.02	3	0.08	0.02	0.10	0.00	0.00	22.3
2	396	-28	-459	47	0	-57	373	4.02	4.02	4.02	4.02	2	0.06	0.01	0.08	0.00	0.00	22.3
3	396	-31	-459	47	0	-56	374	4.02	4.02	4.02	4.02	2	0.06	0.01	0.08	0.00	0.00	22.3
4	396	-2	-389	-13	0	8	433	4.02	4.02	4.02	4.02	2	0.07	0.01	0.07	0.00	0.00	22.3
5	396	-4	-389	-14	0	9	434	4.02	4.02	4.02	4.02	2	0.07	0.01	0.07	0.00	0.00	22.3
6	396	-16	-435	26	0	-36	393	4.02	4.02	4.02	4.02	2	0.06	0.01	0.08	0.00	0.00	22.3
7	396	-24	-434	26	0	-32	395	4.02	4.02	4.02	4.02	2	0.06	0.01	0.08	0.00	0.00	22.3
8	396	-8	-414	8	0	-16	411	4.02	4.02	4.02	4.02	2	0.06	0.01	0.07	0.00	0.00	22.3
9	396	-16	-413	8	0	-12	414	4.02	4.02	4.02	4.02	2	0.06	0.01	0.07	0.00	0.00	22.3
10	396	-28	-459	47	0	-57	373	4.02	4.02	4.02	4.02	2	0.06	0.01	0.08	0.00	0.00	22.3
11	396	-31	-459	47	0	-56	374	4.02	4.02	4.02	4.02	2	0.06	0.01	0.08	0.00	0.00	22.3
12	396	-2	-389	-13	0	8	433	4.02	4.02	4.02	4.02	2	0.07	0.01	0.07	0.00	0.00	22.3
13	396	-4	-389	-14	0	9	434	4.02	4.02	4.02	4.02	2	0.07	0.01	0.07	0.00	0.00	22.3
14	396	-16	-435	26	0	-36	393	4.02	4.02	4.02	4.02	2	0.06	0.01	0.08	0.00	0.00	22.3
15	396	-24	-434	26	0	-32	395	4.02	4.02	4.02	4.02	2	0.06	0.01	0.08	0.00	0.00	22.3
16	396	-8	-414	8	0	-16	411	4.02	4.02	4.02	4.02	2	0.06	0.01	0.07	0.00	0.00	22.3
17	396	-16	-413	8	0	-12	414	4.02	4.02	4.02	4.02	2	0.06	0.01	0.07	0.00	0.00	22.3
18	396	-36	-650	130	0	-153	441	4.02	4.02	4.02	4.02	3	0.06	0.02	0.12	0.00	0.00	22.3
19	396	46	-442	-60	0	51	581	4.02	4.02	4.02	4.02	3	0.08	0.01	0.08	0.00	0.00	22.3
20	396	12	-549	42	0	-50	528	4.02	4.02	4.02	4.02	3	0.08	0.02	0.10	0.00	0.00	22.3
37	396	-71	-721	189	0	-215	380	4.02	4.02	4.02	4.02	3	0.05	0.02	0.13	0.00	0.00	22.3
38	396	65	-375	-128	0	126	619	4.02	4.02	4.02	4.02	3	0.09	0.01	0.07	0.00	0.00	22.3
39	396	9	-553	42	0	-42	525	4.02	4.02	4.02	4.02	3	0.08	0.02	0.10	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	452	-21	-827	22	0	-43	-563	4.02	4.02	4.02	4.02	3	0.08	0.02	0.15	0.00	0.00	22.3
2	452	-28	-671	47	0	-84	-519	4.02	4.02	4.02	4.02	2	0.08	0.02	0.12	0.00	0.00	22.3
3	452	-31	-671	47	0	-83	-518	4.02	4.02	4.02	4.02	2	0.08	0.02	0.12	0.00	0.00	22.3
4	452	-2	-601	-13	0	16	-348	4.02	4.02	4.02	4.02	2	0.05	0.02	0.11	0.00	0.00	22.3
5	452	-4	-601	-14	0	17	-347	4.02	4.02	4.02	4.02	2	0.05	0.02	0.11	0.00	0.00	22.3
6	452	-16	-647	26	0	-51	-460	4.02	4.02	4.02	4.02	2	0.07	0.02	0.12	0.00	0.00	22.3
7	452	-24	-646	26	0	-46	-457	4.02	4.02	4.02	4.02	2	0.07	0.02	0.12	0.00	0.00	22.3
8	452	-8	-626	8	0	-21	-409	4.02	4.02	4.02	4.02	2	0.06	0.02	0.11	0.00	0.00	22.3
9	452	-16	-625	8	0	-16	-405	4.02	4.02	4.02	4.02	2	0.06	0.02	0.11	0.00	0.00	22.3
10	452	-28	-671	47	0	-84	-519	4.02	4.02	4.02	4.02	2	0.08	0.02	0.12	0.00	0.00	22.3
11	452	-31	-671	47	0	-83	-518	4.02	4.02	4.02	4.02	2	0.08	0.02	0.12	0.00	0.00	22.3
12	452	-2	-601	-13	0	16	-348	4.02	4.02	4.02	4.02	2	0.05	0.02	0.11	0.00	0.00	22.3
13	452	-4	-601	-14	0	17	-347	4.02	4.02	4.02	4.02	2	0.05	0.02	0.11	0.00	0.00	22.3
14	452	-16	-647	26	0	-51	-460	4.02	4.02	4.02	4.02	2	0.07	0.02	0.12	0.00	0.00	22.3
15	452	-24	-646	26	0	-46	-457	4.02	4.02	4.02	4.02	2	0.07	0.02	0.12	0.00	0.00	22.3
16	452	-8	-626	8	0	-21	-409	4.02	4.02	4.02	4.02	2	0.06	0.02	0.11	0.00	0.00	22.3
17	452	-16	-625	8	0	-16	-405	4.02	4.02	4.02	4.02	2	0.06	0.02	0.11	0.00	0.00	22.3
18	452	-36	-925	130	0	-227	-802	4.02	4.02	4.02	4.02	3	0.11	0.03	0.16	0.00	0.00	22.3
19	452	46	-717	-60	0	85	429	4.02	4.02	4.02	4.02	3	0.06	0.02	0.13	0.00	0.00	22.3
20	452	12	-824	42	0	-73	-555	4.02	4.02	4.02	4.02	3	0.08	0.02	0.15	0.00	0.00	22.3
37	452	-71	-996	190	0	-322	-974	4.02	4.02	4.02	4.02	3	0.14	0.03	0.18	0.00	0.00	22.3
38	452	65	-650	-128	0	198	525	4.02	4.02	4.02	4.02	3	0.08	0.02	0.12	0.00	0.00	22.3
39	452	9	-828	42	0	-65	-563	4.02	4.02	4.02	4.02	3	0.08	0.02	0.15	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	509	-21	-1102	22	0	-56	-1247	4.02	4.02	4.02	4.02	3	0.18	0.03	0.20	0.00	0.00	22.3
2	509	-28	-883	47	0	-111	-1065	4.02	4.02	4.02	4.02	2	0.16	0.03	0.16	0.00	0.00	22.3
3	509	-31	-883	47	0	-109	-1064	4.02	4.02	4.02	4.02	2	0.16	0.03	0.16	0.00	0.00	22.3
4	509	-2	-813	-13	0	23	-855	4.02	4.02	4.02	4.02	2	0.13	0.02	0.14	0.00	0.00	22.3
5	509	-4	-813	-14	0	25	-854	4.02	4.02	4.02	4.02	2	0.13	0.02	0.14	0.00	0.00	22.3
6	509	-16	-859	26	0	-65	-993	4.02	4.02	4.02	4.02	2	0.15	0.02	0.15	0.00	0.00	22.3
7	509	-24	-858	26	0	-61	-990	4.02	4.02	4.02	4.02	2	0.15	0.02	0.15	0.00	0.00	22.3
8	509	-8	-838	8	0	-25	-930	4.02	4.02	4.02	4.02	2	0.14	0.02	0.15	0.00	0.00	22.3
9	509	-16	-837	8	0	-21	-926	4.02	4.02	4.02	4.02	2	0.14	0.02	0.15	0.00	0.00	22.3
10	509	-28	-883	47	0	-111	-1065	4.02	4.02	4.02	4.02	2	0.16	0.03	0.16	0.00	0.00	22.3
11	509	-31	-883	47	0	-109	-1064	4.02	4.02	4.02	4.02	2	0.16	0.03	0.16	0.00	0.00	22.3
12	509	-2	-813	-13	0	23	-855	4.02	4.02	4.02	4.02	2	0.13	0.02	0.14	0.00	0.00	22.3
13	509	-4	-813	-14	0	25	-854	4.02	4.02	4.02	4.02	2	0.13	0.02	0.14	0.00	0.00	22.3
14	509	-16	-859	26	0	-65	-993	4.02	4.02	4.02	4.02	2	0.15	0.02	0.15	0.00	0.00	22.3
15	509	-24	-858	26	0	-61	-990	4.02	4.02	4.02	4.02	2	0.15	0.02	0.15	0.00	0.00	22.3
16	509	-8	-838	8	0	-25	-930	4.02	4.02	4.02	4.02	2	0.14	0.02	0.15	0.00	0.00	22.3
17	509	-16	-837	8	0	-21	-926	4.02	4.02	4.02	4.02	2	0.14	0.02	0.15	0.00	0.00	22.3
18	509	-36	-1201	130	0	-301	-1542	4.02	4.02	4.02	4.02	3	0.22	0.03	0.21	0.00	0.00	22.3
19	509	46	-993	-60	0	118	-920	4.02	4.02	4.02	4.02	3	0.13	0.03	0.18	0.00	0.00	22.3
20	509	12	-1100	42	0	-97	-1238	4.02	4.02	4.02	4.02	3	0.18	0.03	0.20	0.00	0.00	22.3
37	509	-71	-1272	190	0	-429	-1754	4.02	4.02	4.02	4.02	3	0.25	0.04	0.23	0.00	0.00	22.3
38	509	65	-926	-128	0	270	-717	4.02	4.02	4.02	4.02	3	0.10	0.03	0.16	0.00	0.00	22.3
39	509	9	-1104	42	0	-89	-1248	4.02	4.02	4.02	4.02	3	0.18	0.03	0.20	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	565	-21	-1378	22	0	-68	-1390	4.02	4.02	4.02	4.02	3	0.20	0.04	0.25	0.00	0.00	22.3
2	565	-28	-1095	47	0	-137	-1177	4.02	4.02	4.02	4.02	2	0.18	0.03	0.19	0.00	0.00	22.3
3	565	-31	-1095	47	0	-136	-1176	4.02	4.02	4.02	4.02	2	0.18	0.03	0.19	0.00	0.00	22.3
4	565	-2	-1025	-13	0	31	-963	4.02	4.02	4.02	4.02	2	0.15	0.03	0.18	0.00	0.00	22.3
5	565	-4	-1025	-14	0	32	-961	4.02	4.02	4.02	4.02	2	0.15	0.03	0.18	0.00	0.00	22.3
6	565	-16	-1071	26	0	-80	-1103	4.02	4.02	4.02	4.02	2	0.17	0.03	0.19	0.00	0.00	22.3
7	565	-24	-1070	26	0	-75	-1100	4.02	4.02	4.02	4.02	2	0.17	0.03	0.19	0.00	0.00	22.3
8	565	-8	-1050	8	0	-30	-1039	4.02	4.02	4.02	4.02	2	0.16	0.03	0.19	0.00	0.00	22.3
9	565	-16	-1049	8	0	-25	-1035	4.02	4.02	4.02	4.02	2	0.16	0.03	0.19	0.00	0.00	22.3
10	565	-28	-1095	47	0	-137	-1177	4.02	4.02	4.02	4.02	2	0.18	0.03	0.19	0.00	0.00	22.3
11	565	-31	-1095	47	0	-136	-1176	4.02	4.02	4.02	4.02	2	0.18	0.03	0.19	0.00	0.00	22.3
12	565	-2	-1025	-13	0	31	-963	4.02	4.02	4.02	4.02	2	0.15	0.03	0.18	0.00	0.00	22.3
13	565	-4	-1025	-14	0	32	-961	4.02	4.02	4.02	4.02	2	0.15	0.03	0.18	0.00	0.00	22.3
14	565	-16	-1071	26	0	-80	-1103	4.02	4.02	4.02	4.02	2	0.17	0.03	0.19	0.00	0.00	22.3
15	565	-24	-1070	26	0	-75	-1100	4.02	4.02	4.02	4.02	2	0.17	0.03	0.19	0.00	0.00	22.3
16	565	-8	-1050	8	0	-30	-1039	4.02	4.02	4.02	4.02	2	0.16	0.03	0.19	0.00	0.00	22.3
17	565	-16	-1049	8	0	-25	-1035	4.02	4.02	4.02	4.02	2	0.16	0.03	0.19	0.00	0.00	22.3
18	565	-36	-1476	130	0	-375	-1690	4.02	4.02	4.02	4.02	3	0.24	0.04	0.26	0.00	0.00	22.3
19	565	46	-1268	-60	0	152	-1056	4.02	4.02	4.02	4.02	3	0.15	0.04	0.23	0.00	0.00	22.3
20	565	12	-1375	42	0	-121	-1381	4.02	4.02	4.02	4.02	3	0.20	0.04	0.24	0.00	0.00	22.3
37	565	-71	-1547	190	0	-536	-1907	4.02	4.02	4.02	4.02	3	0.27	0.04	0.28	0.00	0.00	22.3
38	565	65	-1201	-128	0	342	-849	4.02	4.02	4.02	4.02	3	0.12	0.03	0.21	0.00	0.00	22.3
39	565	9	-1379	42	0	-112	-1391	4.02	4.02	4.02	4.02	3	0.20	0.04	0.25	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

Nome travata: **trave_503_IP1** Descrizione: **Trave_5 8-13-18-23**
ASTA NUM. 9 NI 123 NF 210 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y qy tot.
qy medio: 375.00 375.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-124	1590	-15	0	-47	-1644	4.02	4.02	4.02	4.02	3	0.23	0.05	0.28	0.00	0.00	22.3
2	0	-102	1185	10	0	27	-1156	4.02	4.02	4.02	4.02	2	0.17	0.03	0.21	0.00	0.00	22.3
3	0	-104	1183	15	0	41	-1152	4.02	4.02	4.02	4.02	2	0.17	0.03	0.21	0.00	0.00	22.3
4	0	-88	1262	-37	0	-112	-1378	4.02	4.02	4.02	4.02	2	0.21	0.04	0.22	0.00	0.00	22.3
5	0	-90	1261	-33	0	-99	-1374	4.02	4.02	4.02	4.02	2	0.21	0.04	0.22	0.00	0.00	22.3
6	0	-95	1214	-12	0	-38	-1239	4.02	4.02	4.02	4.02	2	0.19	0.04	0.22	0.00	0.00	22.3
7	0	-100	1209	3	0	8	-1224	4.02	4.02	4.02	4.02	2	0.18	0.04	0.21	0.00	0.00	22.3
8	0	-91	1237	-26	0	-80	-1306	4.02	4.02	4.02	4.02	2	0.20	0.04	0.22	0.00	0.00	22.3
9	0	-96	1232	-11	0	-34	-1291	4.02	4.02	4.02	4.02	2	0.20	0.04	0.22	0.00	0.00	22.3
10	0	-102	1185	10	0	27	-1156	4.02	4.02	4.02	4.02	2	0.17	0.03	0.21	0.00	0.00	22.3
11	0	-104	1183	15	0	41	-1152	4.02	4.02	4.02	4.02	2	0.17	0.03	0.21	0.00	0.00	22.3
12	0	-88	1262	-37	0	-112	-1378	4.02	4.02	4.02	4.02	2	0.21	0.04	0.22	0.00	0.00	22.3
13	0	-90	1261	-33	0	-99	-1374	4.02	4.02	4.02	4.02	2	0.21	0.04	0.22	0.00	0.00	22.3
14	0	-95	1214	-12	0	-38	-1239	4.02	4.02	4.02	4.02	2	0.19	0.04	0.22	0.00	0.00	22.3
15	0	-100	1209	3	0	8	-1224	4.02	4.02	4.02	4.02	2	0.18	0.04	0.21	0.00	0.00	22.3
16	0	-91	1237	-26	0	-80	-1306	4.02	4.02	4.02	4.02	2	0.20	0.04	0.22	0.00	0.00	22.3
17	0	-96	1232	-11	0	-34	-1291	4.02	4.02	4.02	4.02	2	0.20	0.04	0.22	0.00	0.00	22.3
18	0	-140	1487	38	0	100	-1348	4.02	4.02	4.02	4.02	3	0.19	0.04	0.26	0.00	0.00	22.3
19	0	-100	1715	-98	0	-291	-2000	4.02	4.02	4.02	4.02	3	0.29	0.05	0.30	0.00	0.00	22.3
20	0	-118	1591	4	0	8	-1646	4.02	4.02	4.02	4.02	3	0.24	0.05	0.28	0.00	0.00	22.3
37	0	-154	1407	88	0	247	-1120	4.02	4.02	4.02	4.02	3	0.16	0.04	0.25	0.00	0.00	22.3
38	0	-89	1787	-138	0	-405	-2208	4.02	4.02	4.02	4.02	3	0.32	0.05	0.32	0.00	0.00	22.3
39	0	-119	1581	32	0	94	-1618	4.02	4.02	4.02	4.02	3	0.23	0.05	0.28	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	56	-124	1314	-15	0	-38	-1489	4.02	4.02	4.02	4.02	3	0.21	0.04	0.23	0.00	0.00	22.3
2	56	-102	973	10	0	21	-1039	4.02	4.02	4.02	4.02	2	0.16	0.03	0.17	0.00	0.00	22.3
3	56	-104	971	15	0	32	-1035	4.02	4.02	4.02	4.02	2	0.16	0.03	0.17	0.00	0.00	22.3
4	56	-88	1050	-37	0	-91	-1256	4.02	4.02	4.02	4.02	2	0.19	0.03	0.19	0.00	0.00	22.3
5	56	-90	1049	-33	0	-80	-1253	4.02	4.02	4.02	4.02	2	0.19	0.03	0.19	0.00	0.00	22.3
6	56	-95	1002	-12	0	-31	-1120	4.02	4.02	4.02	4.02	2	0.17	0.03	0.18	0.00	0.00	22.3
7	56	-100	997	3	0	6	-1106	4.02	4.02	4.02	4.02	2	0.17	0.03	0.18	0.00	0.00	22.3
8	56	-91	1025	-26	0	-65	-1186	4.02	4.02	4.02	4.02	2	0.18	0.03	0.18	0.00	0.00	22.3
9	56	-96	1020	-11	0	-28	-1171	4.02	4.02	4.02	4.02	2	0.18	0.03	0.18	0.00	0.00	22.3
10	56	-102	973	10	0	21	-1039	4.02	4.02	4.02	4.02	2	0.16	0.03	0.17	0.00	0.00	22.3
11	56	-104	971	15	0	32	-1035	4.02	4.02	4.02	4.02	2	0.16	0.03	0.17	0.00	0.00	22.3
12	56	-88	1050	-37	0	-91	-1256	4.02	4.02	4.02	4.02	2	0.19	0.03	0.19	0.00	0.00	22.3
13	56	-90	1049	-33	0	-80	-1253	4.02	4.02	4.02	4.02	2	0.19	0.03	0.19	0.00	0.00	22.3
14	56	-95	1002	-12	0	-31	-1120	4.02	4.02	4.02	4.02	2	0.17	0.03	0.18	0.00	0.00	22.3
15	56	-100	997	3	0	6	-1106	4.02	4.02	4.02	4.02	2	0.17	0.03	0.18	0.00	0.00	22.3
16	56	-91	1025	-26	0	-65	-1186	4.02	4.02	4.02	4.02	2	0.18	0.03	0.18	0.00	0.00	22.3
17	56	-96	1020	-11	0	-28	-1171	4.02	4.02	4.02	4.02	2	0.18	0.03	0.18	0.00	0.00	22.3
18	56	-140	1212	38	0	79	-1199	4.02	4.02	4.02	4.02	3	0.17	0.04	0.22	0.00	0.00	22.3
19	56	-100	1440	-98	0	-236	-1838	4.02	4.02	4.02	4.02	3	0.26	0.04	0.26	0.00	0.00	22.3
20	56	-118	1316	4	0	6	-1491	4.02	4.02	4.02	4.02	3	0.21	0.04	0.23	0.00	0.00	22.3
37	56	-154	1132	88	0	197	-976	4.02	4.02	4.02	4.02	3	0.14	0.03	0.20	0.00	0.00	22.3
38	56	-89	1512	-138	0	-327	-2041	4.02	4.02	4.02	4.02	3	0.29	0.04	0.27	0.00	0.00	22.3
39	56	-119	1306	32	0	76	-1463	4.02	4.02	4.02	4.02	3	0.21	0.04	0.23	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	113	-124	1039	-15	0	-30	-685	4.02	4.02	4.02	4.02	3	0.10	0.03	0.18	0.00	0.00	22.3
2	113	-102	761	10	0	15	-442	4.02	4.02	4.02	4.02	2	0.07	0.02	0.14	0.00	0.00	22.3
3	113	-104	759	15	0	24	-439	4.02	4.02	4.02	4.02	2	0.07	0.02	0.13	0.00	0.00	22.3
4	113	-88	838	-37	0	-70	-615	4.02	4.02	4.02	4.02	2	0.09	0.02	0.15	0.00	0.00	22.3
5	113	-90	837	-33	0	-62	-612	4.02	4.02	4.02	4.02	2	0.09	0.02	0.15	0.00	0.00	22.3
6	113	-95	790	-12	0	-25	-507	4.02	4.02	4.02	4.02	2	0.08	0.02	0.14	0.00	0.00	22.3
7	113	-100	785	3	0	4	-495	4.02	4.02	4.02	4.02	2	0.07	0.02	0.14	0.00	0.00	22.3
8	113	-91	813	-26	0	-50	-559	4.02	4.02	4.02	4.02	2	0.08	0.02	0.14	0.00	0.00	22.3
9	113	-96	808	-11	0	-22	-547	4.02	4.02	4.02	4.02	2	0.08	0.02	0.14	0.00	0.00	22.3
10	113	-102	761	10	0	15	-442	4.02	4.02	4.02	4.02	2	0.07	0.02	0.14	0.00	0.00	22.3
11	113	-104	759	15	0	24	-439	4.02	4.02	4.02	4.02	2	0.07	0.02	0.13	0.00	0.00	22.3
12	113	-88	838	-37	0	-70	-615	4.02	4.02	4.02	4.02	2	0.09	0.02	0.15	0.00	0.00	22.3
13	113	-90	837	-33	0	-62	-612	4.02	4.02	4.02	4.02	2	0.09	0.02	0.15	0.00	0.00	22.3
14	113	-95	790	-12	0	-25	-507	4.02	4.02	4.02	4.02	2	0.08	0.02	0.14	0.00	0.00	22.3
15	113	-100	785	3	0	4	-495	4.02	4.02	4.02	4.02	2	0.07	0.02	0.14	0.00	0.00	22.3
16	113	-91	813	-26	0	-50	-559	4.02	4.02	4.02	4.02	2	0.08	0.02	0.14	0.00	0.00	22.3
17	113	-96	808	-11	0	-22	-547	4.02	4.02	4.02	4.02	2	0.08	0.02	0.14	0.00	0.00	22.3
18	113	-140	936	38	0	58	495	4.02	4.02	4.02	4.02	3	0.07	0.03	0.17	0.00	0.00	22.3
19	113	-100	1164	-98	0	-180	-963	4.02	4.02	4.02	4.02	3	0.14	0.03	0.21	0.00	0.00	22.3
20	113	-118	1040	4	0	4	-686	4.02	4.02	4.02	4.02	3	0.10	0.03	0.18	0.00	0.00	22.3
37	113	-154	856	88	0	147	592	4.02	4.02	4.02	4.02	3	0.08	0.02	0.15	0.00	0.00	22.3
38	113	-89	1236	-138	0	-249	-1125	4.02	4.02	4.02	4.02	3	0.16	0.04	0.22	0.00	0.00	22.3
39	113	-119	1030	32	0	58	-664	4.02	4.02	4.02	4.02	3	0.09	0.03	0.18	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	169	-124	764	-15	0	-22	737	4.02	4.02	4.02	4.02	3	0.11	0.02	0.14	0.00	0.00	22.3
2	169	-102	549	10	0	9	592	4.02	4.02	4.02	4.02	2	0.09	0.02	0.10	0.00	0.00	22.3
3	169	-104	547	15	0	15	592	4.02	4.02	4.02	4.02	2	0.09	0.02	0.10	0.00	0.00	22.3
4	169	-88	627	-37	0	-49	540	4.02	4.02	4.02	4.02	2	0.08	0.02	0.11	0.00	0.00	22.3
5	169	-90	625	-33	0	-43	541	4.02	4.02	4.02	4.02	2	0.08	0.02	0.11	0.00	0.00	22.3
6	169	-95	578	-12	0	-18	573	4.02	4.02	4.02	4.02	2	0.09	0.02	0.10	0.00	0.00	22.3
7	169	-100	573	3	0	2	576	4.02	4.02	4.02	4.02	2	0.09	0.02	0.10	0.00	0.00	22.3
8	169	-91	601	-26	0	-36	557	4.02	4.02	4.02	4.02	2	0.08	0.02	0.11	0.00	0.00	22.3
9	169	-96	596	-11	0	-15	560	4.02	4.02	4.02	4.02	2	0.08	0.02	0.11	0.00	0.00	22.3
10	169	-102	549	10	0	9	592	4.02	4.02	4.02	4.02	2	0.09	0.02	0.10	0.00	0.00	22.3
11	169	-104	547	15	0	15	592	4.02	4.02	4.02	4.02	2	0.09	0.02	0.10	0.00	0.00	22.3
12	169	-88	627	-37	0	-49	540	4.02	4.02	4.02	4.02	2	0.08	0.02	0.11	0.00	0.00	22.3
13	169	-90	625	-33	0	-43	541	4.02	4.02	4.02	4.02	2	0.08	0.02	0.11	0.00	0.00	22.3
14	169	-95	578	-12	0	-18	573	4.02	4.02	4.02	4.02	2	0.09	0.02	0.10	0.00	0.00	22.3
15	169	-100	573	3	0	2	576	4.02	4.02	4.02	4.02	2	0.09	0.02	0.10	0.00	0.00	22.3
16	169	-91	601	-26	0	-36	557	4.02	4.02	4.02	4.02	2	0.08	0.02	0.11	0.00	0.00	22.3
17	169	-96	596	-11	0	-15	560	4.02	4.02	4.02	4.02	2	0.08	0.02	0.11	0.00	0.00	22.3

18	169	-140	661	38	0	36	806	4.02	4.02	4.02	4.02	3	0.12	0.02	0.12	0.00	0.00	22.3
19	169	-100	889	-98	0	-125	657	4.02	4.02	4.02	4.02	3	0.09	0.03	0.16	0.00	0.00	22.3
20	169	-118	765	4	0	2	738	4.02	4.02	4.02	4.02	3	0.11	0.02	0.14	0.00	0.00	22.3
37	169	-154	581	88	0	98	859	4.02	4.02	4.02	4.02	3	0.12	0.02	0.10	0.00	0.00	22.3
38	169	-89	961	-138	0	-171	608	4.02	4.02	4.02	4.02	3	0.09	0.03	0.17	0.00	0.00	22.3
39	169	-119	755	32	0	40	744	4.02	4.02	4.02	4.02	3	0.11	0.02	0.13	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	226	-124	488	-15	0	-13	944	4.02	4.02	4.02	4.02	3	0.13	0.01	0.09	0.00	0.00	22.3
2	226	-102	337	10	0	3	706	4.02	4.02	4.02	4.02	2	0.11	0.01	0.06	0.00	0.00	22.3
3	226	-104	336	15	0	7	705	4.02	4.02	4.02	4.02	2	0.11	0.01	0.06	0.00	0.00	22.3
4	226	-88	415	-37	0	-28	727	4.02	4.02	4.02	4.02	2	0.11	0.01	0.07	0.00	0.00	22.3
5	226	-90	413	-33	0	-24	727	4.02	4.02	4.02	4.02	2	0.11	0.01	0.07	0.00	0.00	22.3
6	226	-95	366	-12	0	-12	721	4.02	4.02	4.02	4.02	2	0.11	0.01	0.07	0.00	0.00	22.3
7	226	-100	361	3	0	0	719	4.02	4.02	4.02	4.02	2	0.11	0.01	0.06	0.00	0.00	22.3
8	226	-91	390	-26	0	-21	730	4.02	4.02	4.02	4.02	2	0.11	0.01	0.07	0.00	0.00	22.3
9	226	-96	384	-11	0	-9	730	4.02	4.02	4.02	4.02	2	0.11	0.01	0.07	0.00	0.00	22.3
10	226	-102	337	10	0	3	706	4.02	4.02	4.02	4.02	2	0.11	0.01	0.06	0.00	0.00	22.3
11	226	-104	336	15	0	7	705	4.02	4.02	4.02	4.02	2	0.11	0.01	0.06	0.00	0.00	22.3
12	226	-88	415	-37	0	-28	727	4.02	4.02	4.02	4.02	2	0.11	0.01	0.07	0.00	0.00	22.3
13	226	-90	413	-33	0	-24	727	4.02	4.02	4.02	4.02	2	0.11	0.01	0.07	0.00	0.00	22.3
14	226	-95	366	-12	0	-12	721	4.02	4.02	4.02	4.02	2	0.11	0.01	0.07	0.00	0.00	22.3
15	226	-100	361	3	0	0	719	4.02	4.02	4.02	4.02	2	0.11	0.01	0.06	0.00	0.00	22.3
16	226	-91	390	-26	0	-21	730	4.02	4.02	4.02	4.02	2	0.11	0.01	0.07	0.00	0.00	22.3
17	226	-96	384	-11	0	-9	730	4.02	4.02	4.02	4.02	2	0.11	0.01	0.07	0.00	0.00	22.3
18	226	-140	385	38	0	15	907	4.02	4.02	4.02	4.02	3	0.13	0.01	0.07	0.00	0.00	22.3
19	226	-100	613	-98	0	-69	941	4.02	4.02	4.02	4.02	3	0.13	0.02	0.11	0.00	0.00	22.3
20	226	-118	489	4	0	-0	948	4.02	4.02	4.02	4.02	3	0.14	0.01	0.09	0.00	0.00	22.3
37	226	-154	305	88	0	48	910	4.02	4.02	4.02	4.02	3	0.13	0.01	0.05	0.00	0.00	22.3
38	226	-89	685	-138	0	-92	933	4.02	4.02	4.02	4.02	3	0.13	0.02	0.12	0.00	0.00	22.3
39	226	-119	479	32	0	22	942	4.02	4.02	4.02	4.02	3	0.13	0.01	0.09	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	282	-124	212	-15	0	-5	944	4.02	4.02	4.02	4.02	3	0.13	0.01	0.04	0.00	0.00	22.3
2	282	-102	126	10	0	-2	706	4.02	4.02	4.02	4.02	2	0.11	0.00	0.02	0.00	0.00	22.3
3	282	-104	124	15	0	-1	705	4.02	4.02	4.02	4.02	2	0.11	0.00	0.02	0.00	0.00	22.3
4	282	-88	203	-37	0	-7	747	4.02	4.02	4.02	4.02	2	0.11	0.01	0.04	0.00	0.00	22.3
5	282	-90	202	-33	0	-6	746	4.02	4.02	4.02	4.02	2	0.11	0.01	0.04	0.00	0.00	22.3
6	282	-95	155	-12	0	-5	721	4.02	4.02	4.02	4.02	2	0.11	0.00	0.03	0.00	0.00	22.3
7	282	-100	149	3	0	-2	719	4.02	4.02	4.02	4.02	2	0.11	0.00	0.03	0.00	0.00	22.3
8	282	-91	178	-26	0	-6	733	4.02	4.02	4.02	4.02	2	0.11	0.01	0.03	0.00	0.00	22.3
9	282	-96	173	-11	0	-3	731	4.02	4.02	4.02	4.02	2	0.11	0.01	0.03	0.00	0.00	22.3
10	282	-102	126	10	0	-2	706	4.02	4.02	4.02	4.02	2	0.11	0.00	0.02	0.00	0.00	22.3
11	282	-104	124	15	0	-1	705	4.02	4.02	4.02	4.02	2	0.11	0.00	0.02	0.00	0.00	22.3
12	282	-88	203	-37	0	-7	747	4.02	4.02	4.02	4.02	2	0.11	0.01	0.04	0.00	0.00	22.3
13	282	-90	202	-33	0	-6	746	4.02	4.02	4.02	4.02	2	0.11	0.01	0.04	0.00	0.00	22.3
14	282	-95	155	-12	0	-5	721	4.02	4.02	4.02	4.02	2	0.11	0.00	0.03	0.00	0.00	22.3
15	282	-100	149	3	0	-2	719	4.02	4.02	4.02	4.02	2	0.11	0.00	0.03	0.00	0.00	22.3
16	282	-91	178	-26	0	-6	733	4.02	4.02	4.02	4.02	2	0.11	0.01	0.03	0.00	0.00	22.3
17	282	-96	173	-11	0	-3	731	4.02	4.02	4.02	4.02	2	0.11	0.01	0.03	0.00	0.00	22.3
18	282	-140	110	38	0	-6	907	4.02	4.02	4.02	4.02	3	0.13	0.00	0.02	0.00	0.00	22.3
19	282	-100	338	-98	0	-13	1013	4.02	4.02	4.02	4.02	3	0.14	0.01	0.06	0.00	0.00	22.3
20	282	-118	214	4	0	-2	948	4.02	4.02	4.02	4.02	3	0.14	0.01	0.04	0.00	0.00	22.3
37	282	-154	30	88	0	-2	910	4.02	4.02	4.02	4.02	3	0.13	0.00	0.01	0.00	0.00	22.3
38	282	-89	410	-138	0	-14	1050	4.02	4.02	4.02	4.02	3	0.15	0.01	0.07	0.00	0.00	22.3
39	282	-119	204	32	0	4	942	4.02	4.02	4.02	4.02	3	0.13	0.01	0.04	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	339	-124	-63	-15	0	3	944	4.02	4.02	4.02	4.02	3	0.13	0.00	0.01	0.00	0.00	22.3
2	339	-102	-86	10	0	-8	706	4.02	4.02	4.02	4.02	2	0.11	0.00	0.02	0.00	0.00	22.3
3	339	-104	-88	15	0	-10	705	4.02	4.02	4.02	4.02	2	0.11	0.00	0.02	0.00	0.00	22.3
4	339	-88	-9	-37	0	14	747	4.02	4.02	4.02	4.02	2	0.11	0.00	0.00	0.00	0.00	22.3
5	339	-90	-10	-33	0	13	746	4.02	4.02	4.02	4.02	2	0.11	0.00	0.00	0.00	0.00	22.3
6	339	-95	-57	-12	0	1	721	4.02	4.02	4.02	4.02	2	0.11	0.00	0.01	0.00	0.00	22.3
7	339	-100	-62	3	0	-3	719	4.02	4.02	4.02	4.02	2	0.11	0.00	0.01	0.00	0.00	22.3
8	339	-91	-34	-26	0	8	733	4.02	4.02	4.02	4.02	2	0.11	0.00	0.01	0.00	0.00	22.3
9	339	-96	-39	-11	0	3	731	4.02	4.02	4.02	4.02	2	0.11	0.00	0.01	0.00	0.00	22.3
10	339	-102	-86	10	0	-8	706	4.02	4.02	4.02	4.02	2	0.11	0.00	0.02	0.00	0.00	22.3
11	339	-104	-88	15	0	-10	705	4.02	4.02	4.02	4.02	2	0.11	0.00	0.02	0.00	0.00	22.3
12	339	-88	-9	-37	0	14	747	4.02	4.02	4.02	4.02	2	0.11	0.00	0.00	0.00	0.00	22.3
13	339	-90	-10	-33	0	13	746	4.02	4.02	4.02	4.02	2	0.11	0.00	0.00	0.00	0.00	22.3
14	339	-95	-57	-12	0	1	721	4.02	4.02	4.02	4.02	2	0.11	0.00	0.01	0.00	0.00	22.3
15	339	-100	-62	3	0	-3	719	4.02	4.02	4.02	4.02	2	0.11	0.00	0.01	0.00	0.00	22.3
16	339	-91	-34	-26	0	8	733	4.02	4.02	4.02	4.02	2	0.11	0.00	0.01	0.00	0.00	22.3
17	339	-96	-39	-11	0	3	731	4.02	4.02	4.02	4.02	2	0.11	0.00	0.01	0.00	0.00	22.3
18	339	-140	-166	38	0	-27	907	4.02	4.02	4.02	4.02	3	0.13	0.00	0.03	0.00	0.00	22.3
19	339	-100	63	-98	0	42	1013	4.02	4.02	4.02	4.02	3	0.14	0.00	0.01	0.00	0.00	22.3
20	339	-118	-61	4	0	-5	948	4.02	4.02	4.02	4.02	3	0.14	0.00	0.01	0.00	0.00	22.3
37	339	-154	-245	88	0	-52	910	4.02	4.02	4.02	4.02	3	0.13	0.01	0.04	0.00	0.00	22.3
38	339	-89	135	-138	0	64	1050	4.02	4.02	4.02	4.02	3	0.15	0.00	0.02	0.00	0.00	22.3
39	339	-119	-71	32	0	-14	942	4.02	4.02	4.02	4.02	3	0.13	0.00	0.01	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	395	-124	-338	-15	0	11	944	4.02	4.02	4.02	4.02	3	0.13	0.01	0.06	0.00	0.00	22.3
2	395	-102	-298	10	0	-14	706	4.02	4.02	4.02	4.02	2	0.11	0.01	0.05	0.00	0.00	22.3
3	395	-104	-300	15	0	-18	705	4.02	4.02	4.02	4.02	2	0.11	0.01	0.05	0.00	0.00	22.3
4	395	-88	-221	-37	0	36	747	4.02	4.02	4.02	4.02	2	0.11	0.01	0.04	0.00	0.00	22.3
5	395	-90	-222	-33	0	32	746	4.02	4.02	4.02	4.02	2	0.11	0.01	0.04	0.00	0.00	22.3
6	395	-95	-269	-12	0	8	721	4.02	4.02	4.02	4.02	2	0.11	0.01	0.05	0.00	0.00	22.3
7	395	-100	-274	3	0	-5	719	4.02	4.02	4.02	4.02	2	0.11	0.01	0.05	0.00	0.00	22.3
8	395	-91	-246	-26	0	23	733	4.02	4.02	4.02	4.02	2	0.11	0.01	0.04	0.00	0.00	22.3
9	395	-96	-251	-11	0	10	731	4.02	4.02	4.02	4.02	2	0.11	0.01	0.04	0.00	0.00	22.3
10	395	-102	-298	10	0	-14	706	4.02	4.02	4.02	4.02	2	0.11	0.01	0.05	0.00	0.00	22.3
11	395	-104	-300	15	0	-18	705	4.02	4.02	4.02	4.02	2	0.11	0.01	0.05	0.00	0.00	22.3
12	395	-88	-221	-37	0	36	747	4.02	4.02	4.02	4.02	2	0.11	0.01	0.04	0.00	0.00	22.3
13	395	-90	-222	-33	0	32	746	4.02	4.02	4.02	4.02	2	0.11	0.01	0.04	0.00	0.00	22.3
14	395	-95	-269	-12	0	8	721	4.02	4.02	4.02	4.02	2	0.11	0.01	0.05	0.00	0.00	22.3
15	395	-100	-274	3	0	-5	719	4.02	4.02	4.02	4.02	2	0.11	0.01	0.05	0.00	0.00	22.3
16	395	-91	-246	-26	0	23	733	4.02	4.02	4.02	4.02	2	0.11	0.01	0.04	0.00	0.00	22.3
17	395	-96	-251	-11	0	10	731	4.02	4.02	4.02	4.02	2	0.11	0.01	0.04	0.00	0.00	22.3
18	395	-140	-441	38	0	-49	907	4.02	4.02	4.02	4.02	3	0.13	0.01	0.08	0.00	0.00	22.3
19	395	-100	-213	-98	0	98	1013	4.02	4.02	4.02	4.02	3	0.14	0.01	0.04	0.00	0.00	22.3
20	395	-118	-337	4	0	-7	948	4.02	4.02	4.02	4.02	3	0.14	0.01	0.06	0.00	0.00	22.3
37	395	-154	-521	88	0	-102	896	4.02	4.02	4.02	4.02	3	0.13	0.02	0.09	0.00	0.00	22.3
38	395	-89	-141	-138	0	142	1050	4.02	4.02	4.02	4.02	3	0.15	0.00	0.03	0.00	0.00	22.3
39	395	-119	-347	32	0	-32	942	4.02	4.02	4.02	4.02	3	0.13	0.01	0.06	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	452	-124	-614	-15	0	20	872	4.02	4.02	4.02	4.02	3	0.12	0.02	0.11	0.00	0.00	22.3
2	452	-102	-510	10	0	-20	627	4.02	4.02	4.02	4.02	2	0.09	0.01	0.09	0.00	0.00	22.3
3	452	-104	-512	15	0	-26	625	4.02	4.02	4.02	4.02	2	0.09	0.01	0.09	0.00	0.00	22.3
4	452	-88	-433	-37	0	57	716	4.02	4.02	4.02	4.02	2	0.11	0.01	0.08	0.00	0.00	22.3
5	452	-90	-434	-33	0	50	714	4.02	4.02	4.02	4.02	2	0.11	0.01	0.08	0.00	0.00	22.3
6	452	-95	-481	-12	0	14	661	4.02	4.02	4.02	4.02	2	0.10	0.01	0.09	0.00	0.00	22.3
7	452	-100	-486	3	0	-7	655	4.02	4.02	4.02	4.02	2	0.10	0.01	0.09	0.00	0.00	22.3
8	452	-91	-458	-26	0	37	687	4.02	4.02	4.02	4.02	2	0.10	0.01	0.08	0.00	0.00	22.3
9	452	-96	-463	-11	0	16	681	4.02	4.02	4.02	4.02	2	0.10	0.01	0.08	0.00	0.00	22.3
10	452	-102	-510	10	0	-20	627	4.02	4.02	4.02	4.02	2	0.09	0.01	0.09	0.00	0.00	22.3
11	452	-104	-512	15	0	-26	625	4.02	4.02	4.02	4.02	2	0.09	0.01	0.09	0.00	0.00	22.3
12	452	-88	-433	-37	0	57	716	4.02	4.02	4.02	4.02	2	0.11	0.01	0.08	0.00	0.00	22.3
13	452	-90	-434	-33	0	50	714	4.02	4.02	4.02	4.02	2	0.11	0.01	0.08	0.00	0.00	22.3
14	452	-95	-481	-12	0	14	661	4.02	4.02	4.02	4.02	2	0.10	0.01	0.09	0.00	0.00	22.3
15	452	-100	-486	3	0	-7	655	4.02	4.02	4.02	4.02	2	0.10	0.01	0.09	0.00	0.00	22.3
16	452	-91	-458	-26	0	37	687	4.02	4.02	4.02	4.02	2	0.10	0.01	0.08	0.00	0.00	22.3
17	452	-96	-463	-11	0	16	681	4.02	4.02	4.02	4.02	2	0.10	0.01	0.08	0.00	0.00	22.3
18	452	-140	-717	38	0	-70	756	4.02	4.02	4.02	4.02	3	0.11	0.02	0.13	0.00	0.00	22.3
19	452	-100	-488	-98	0	153	1013	4.02	4.02	4.02	4.02	3	0.14	0.01	0.09	0.00	0.00	22.3
20	452	-118	-612	4	0	-9	877	4.02	4.02	4.02	4.02	3	0.13	0.02	0.11	0.00	0.00	22.3
37	452	-154	-796	88	0	-152	663	4.02	4.02	4.02	4.02	3	0.09	0.02	0.14	0.00	0.00	22.3
38	452	-89	-416	-138	0	220	1050	4.02	4.02	4.02	4.02	3	0.15	0.01	0.07	0.00	0.00	22.3
39	452	-119	-622	32	0	-50	865	4.02	4.02	4.02	4.02	3	0.12	0.02	0.11	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	508	-124	-890	-15	0	28	587	4.02	4.02	4.02	4.02	3	0.08	0.03	0.16	0.00	0.00	22.3
2	508	-102	-722	10	0	-26	387	4.02	4.02	4.02	4.02	2	0.06	0.02	0.13	0.00	0.00	22.3
3	508	-104	-724	15	0	-35	384	4.02	4.02	4.02	4.02	2	0.06	0.02	0.13	0.00	0.00	22.3
4	508	-88	-644	-37	0	78	519	4.02	4.02	4.02	4.02	2	0.08	0.02	0.11	0.00	0.00	22.3
5	508	-90	-646	-33	0	69	517	4.02	4.02	4.02	4.02	2	0.08	0.02	0.11	0.00	0.00	22.3
6	508	-95	-693	-12	0	21	436	4.02	4.02	4.02	4.02	2	0.07	0.02	0.12	0.00	0.00	22.3
7	508	-100	-698	3	0	-9	427	4.02	4.02	4.02	4.02	2	0.06	0.02	0.12	0.00	0.00	22.3
8	508	-91	-670	-26	0	52	476	4.02	4.02	4.02	4.02	2	0.07	0.02	0.12	0.00	0.00	22.3
9	508	-96	-675	-11	0	22	467	4.02	4.02	4.02	4.02	2	0.07	0.02	0.12	0.00	0.00	22.3
10	508	-102	-722	10	0	-26	387	4.02	4.02	4.02	4.02	2	0.06	0.02	0.13	0.00	0.00	22.3
11	508	-104	-724	15	0	-35	384	4.02	4.02	4.02	4.02	2	0.06	0.02	0.13	0.00	0.00	22.3
12	508	-88	-644	-37	0	78	519	4.02	4.02	4.02	4.02	2	0.08	0.02	0.11	0.00	0.00	22.3
13	508	-90	-646	-33	0	69	517	4.02	4.02	4.02	4.02	2	0.08	0.02	0.11	0.00	0.00	22.3
14	508	-95	-693	-12	0	21	436	4.02	4.02	4.02	4.02	2	0.07	0.02	0.12	0.00	0.00	22.3
15	508	-100	-698	3	0	-9	427	4.02	4.02	4.02	4.02	2	0.06	0.02	0.12	0.00	0.00	22.3
16	508	-91	-670	-26	0	52	476	4.02	4.02	4.02	4.02	2	0.07	0.02	0.12	0.00	0.00	22.3
17	508	-96	-675	-11	0	22	467	4.02	4.02	4.02	4.02	2	0.07	0.02	0.12	0.00	0.00	22.3
18	508	-140	-992	38	0	-91	-592	4.02	4.02	4.02	4.02	3	0.08	0.03	0.18	0.00	0.00	22.3
19	508	-100	-764	-98	0	209	805	4.02	4.02	4.02	4.02	3	0.12	0.02	0.14	0.00	0.00	22.3
20	508	-118	-888	4	0	-11	593	4.02	4.02	4.02	4.02	3	0.08	0.03	0.16	0.00	0.00	22.3
37	508	-154	-1072	88	0	-202	-810	4.02	4.02	4.02	4.02	3	0.12	0.03	0.19	0.00	0.00	22.3
38	508	-89	-692	-138	0	299	928	4.02	4.02	4.02	4.02	3	0.13	0.02	0.12	0.00	0.00	22.3
39	508	-119	-898	32	0	-68	575	4.02	4.02	4.02	4.02	3	0.08	0.03	0.16	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	565	-124	-1165	-15	0	36	-443	4.02	4.02	4.02	4.02	3	0.06	0.03	0.21	0.00	0.00	22.3
2	565	-102	-934	10	0	-32	-447	4.02	4.02	4.02	4.02	2	0.07	0.03	0.17	0.00	0.00	22.3
3	565	-104	-935	15	0	-43	-451	4.02	4.02	4.02	4.02	2	0.07	0.03	0.17	0.00	0.00	22.3
4	565	-88	-856	-37	0	99	-231	4.02	4.02	4.02	4.02	2	0.03	0.02	0.15	0.00	0.00	22.3
5	565	-90	-858	-33	0	88	-235	4.02	4.02	4.02	4.02	2	0.04	0.02	0.15	0.00	0.00	22.3
6	565	-95	-905	-12	0	27	-366	4.02	4.02	4.02	4.02	2	0.06	0.03	0.16	0.00	0.00	22.3
7	565	-100	-910	3	0	-11	-381	4.02	4.02	4.02	4.02	2	0.06	0.03	0.16	0.00	0.00	22.3
8	565	-91	-882	-26	0	67	-301	4.02	4.02	4.02	4.02	2	0.05	0.03	0.16	0.00	0.00	22.3
9	565	-96	-887	-11	0	28	-316	4.02	4.02	4.02	4.02	2	0.05	0.03	0.16	0.00	0.00	22.3
10	565	-102	-934	10	0	-32	-447	4.02	4.02	4.02	4.02	2	0.07	0.03	0.17	0.00	0.00	22.3
11	565	-104	-935	15	0	-43	-451	4.02	4.02	4.02	4.02	2	0.07	0.03	0.17	0.00	0.00	22.3
12	565	-88	-856	-37	0	99	-231	4.02	4.02	4.02	4.02	2	0.03	0.02	0.15	0.00	0.00	22.3
13	565	-90	-858	-33	0	88	-235	4.02	4.02	4.02	4.02	2	0.04	0.02	0.15	0.00	0.00	22.3
14	565	-95	-905	-12	0	27	-366	4.02	4.02	4.02	4.02	2	0.06	0.03	0.16	0.00	0.00	22.3
15	565	-100	-910	3	0	-11	-381	4.02	4.02	4.02	4.02	2	0.06	0.03	0.16	0.00	0.00	22.3
16	565	-91	-882	-26	0	67	-301	4.02	4.02	4.02	4.02	2	0.05	0.03	0.16	0.00	0.00	22.3
17	565	-96	-887	-11	0	28	-316	4.02	4.02	4.02	4.02	2	0.05	0.03	0.16	0.00	0.00	22.3
18	565	-140	-1268	38	0	-112	-728	4.02	4.02	4.02	4.02	3	0.10	0.04	0.23	0.00	0.00	22.3
19	565	-100	-1039	-98	0	265	-91	4.02	4.02	4.02	4.02	3	0.06	0.03	0.18	0.00	0.00	22.3
20	565	-118	-1163	4	0	-13	-436	4.02	4.02	4.02	4.02	3	0.06	0.03	0.21	0.00	0.00	22.3
37	565	-154	-1347	88	0	-251	-951	4.02	4.02	4.02	4.02	3	0.14	0.04	0.24	0.00	0.00	22.3
38	565	-89	-967	-138	0	377	599	4.02	4.02	4.02	4.02	3	0.09	0.03	0.17	0.00	0.00	22.3
39	565	-119	-1173	32	0	-86	-464	4.02	4.02	4.02	4.02	3	0.07	0.03	0.21	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

Nome travata: **trave_504_IP1** Descrizione: **Trave_5 11-10-9-8**
ASTA NUM. 10 NI 169 NF 294 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y Permanente Neve qy tot.
qy medio: 375.00 1589.25 142.50 2106.75 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-375	3655	-146	0	-282	-1265	4.02	4.02	4.02	4.02	3	0.18	0.11	0.65	0.00	0.00	22.3
2	0	-329	2783	28	0	-31	-965	4.02	4.02	4.02	4.02	2	0.14	0.08	0.49	0.00	0.00	22.3
3	0	-362	2889	25	0	-35	-1053	4.02	4.02	4.02	4.02	2	0.16	0.08	0.51	0.00	0.00	22.3
4	0	-215	2734	-249	0	-398	-894	4.02	4.02	4.02	4.02	2	0.13	0.08	0.48	0.00	0.00	22.3
5	0	-247	2840	-252	0	-402	-981	4.02	4.02	4.02	4.02	2	0.15	0.08	0.50	0.00	0.00	22.3
6	0	-252	2642	-65	0	-155	-838	4.02	4.02	4.02	4.02	2	0.13	0.08	0.47	0.00	0.00	22.3
7	0	-359	2995	-76	0	-168	-1130	4.02	4.02	4.02	4.02	2	0.17	0.09	0.53	0.00	0.00	22.3
8	0	-217	2627	-148	0	-265	-817	4.02	4.02	4.02	4.02	2	0.12	0.08	0.47	0.00	0.00	22.3
9	0	-325	2980	-159	0	-278	-1108	4.02	4.02	4.02	4.02	2	0.17	0.09	0.53	0.00	0.00	22.3
10	0	-329	2783	28	0	-31	-965	4.02	4.02	4.02	4.02	2	0.14	0.08	0.49	0.00	0.00	22.3
11	0	-362	2889	25	0	-35	-1053	4.02	4.02	4.02	4.02	2	0.16	0.08	0.51	0.00	0.00	22.3
12	0	-215	2734	-249	0	-398	-894	4.02	4.02	4.02	4.02	2	0.13	0.08	0.48	0.00	0.00	22.3
13	0	-247	2840	-252	0	-402	-981	4.02	4.02	4.02	4.02	2	0.15	0.08	0.50	0.00	0.00	22.3
14	0	-252	2642	-65	0	-155	-838	4.02	4.02	4.02	4.02	2	0.13	0.08	0.47	0.00	0.00	22.3
15	0	-359	2995	-76	0	-168	-1130	4.02	4.02	4.02	4.02	2	0.17	0.09	0.53	0.00	0.00	22.3

16	0	-217	2627	-148	0	-265	-817	4.02	4.02	4.02	4.02	2	0.12	0.08	0.47	0.00	0.00	22.3
17	0	-325	2980	-159	0	-278	-1108	4.02	4.02	4.02	4.02	2	0.17	0.09	0.53	0.00	0.00	22.3
18	0	-482	3842	109	0	-61	-1385	4.02	4.02	4.02	4.02	3	0.20	0.11	0.68	0.00	0.00	22.3
19	0	-176	3791	-697	0	-1088	-1220	4.02	4.02	4.02	4.02	3	0.27	0.11	0.67	0.00	0.00	22.3
20	0	-306	3819	-241	0	-499	-1218	4.02	4.02	4.02	4.02	3	0.17	0.11	0.68	0.00	0.00	22.3
37	0	-595	3759	426	0	377	-1418	4.02	4.02	4.02	4.02	3	0.20	0.11	0.66	0.00	0.00	22.3
38	0	-87	3673	-917	0	-1334	-1143	4.02	4.02	4.02	4.02	3	0.33	0.11	0.65	0.00	0.00	22.3
39	0	-303	3720	-156	0	-352	-1140	4.02	4.02	4.02	4.02	3	0.16	0.11	0.66	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	31	-375	2863	-146	0	-237	-1265	4.02	4.02	4.02	4.02	3	0.18	0.08	0.51	0.00	0.00	22.3
2	31	-329	2174	28	0	-40	-965	4.02	4.02	4.02	4.02	2	0.14	0.06	0.38	0.00	0.00	22.3
3	31	-362	2280	25	0	-43	-1053	4.02	4.02	4.02	4.02	2	0.16	0.07	0.40	0.00	0.00	22.3
4	31	-215	2125	-249	0	-321	-894	4.02	4.02	4.02	4.02	2	0.13	0.06	0.38	0.00	0.00	22.3
5	31	-247	2231	-252	0	-324	-981	4.02	4.02	4.02	4.02	2	0.15	0.06	0.40	0.00	0.00	22.3
6	31	-252	2033	-65	0	-135	-838	4.02	4.02	4.02	4.02	2	0.13	0.06	0.36	0.00	0.00	22.3
7	31	-359	2386	-76	0	-145	-1130	4.02	4.02	4.02	4.02	2	0.17	0.07	0.42	0.00	0.00	22.3
8	31	-217	2018	-148	0	-219	-817	4.02	4.02	4.02	4.02	2	0.12	0.06	0.36	0.00	0.00	22.3
9	31	-325	2371	-159	0	-229	-1108	4.02	4.02	4.02	4.02	2	0.17	0.07	0.42	0.00	0.00	22.3
10	31	-329	2174	28	0	-40	-965	4.02	4.02	4.02	4.02	2	0.14	0.06	0.38	0.00	0.00	22.3
11	31	-362	2280	25	0	-43	-1053	4.02	4.02	4.02	4.02	2	0.16	0.07	0.40	0.00	0.00	22.3
12	31	-215	2125	-249	0	-321	-894	4.02	4.02	4.02	4.02	2	0.13	0.06	0.38	0.00	0.00	22.3
13	31	-247	2231	-252	0	-324	-981	4.02	4.02	4.02	4.02	2	0.15	0.06	0.40	0.00	0.00	22.3
14	31	-252	2033	-65	0	-135	-838	4.02	4.02	4.02	4.02	2	0.13	0.06	0.36	0.00	0.00	22.3
15	31	-359	2386	-76	0	-145	-1130	4.02	4.02	4.02	4.02	2	0.17	0.07	0.42	0.00	0.00	22.3
16	31	-217	2018	-148	0	-219	-817	4.02	4.02	4.02	4.02	2	0.12	0.06	0.36	0.00	0.00	22.3
17	31	-325	2371	-159	0	-229	-1108	4.02	4.02	4.02	4.02	2	0.17	0.07	0.42	0.00	0.00	22.3
18	31	-482	2984	109	0	-95	-1385	4.02	4.02	4.02	4.02	3	0.20	0.09	0.53	0.00	0.00	22.3
19	31	-176	2933	-697	0	-872	-1220	4.02	4.02	4.02	4.02	3	0.21	0.08	0.52	0.00	0.00	22.3
20	31	-306	2961	-241	0	-424	-1218	4.02	4.02	4.02	4.02	3	0.17	0.09	0.52	0.00	0.00	22.3
37	31	-595	2934	426	0	245	-1418	4.02	4.02	4.02	4.02	3	0.20	0.08	0.52	0.00	0.00	22.3
38	31	-87	2848	-917	0	-1050	-1143	4.02	4.02	4.02	4.02	3	0.26	0.08	0.51	0.00	0.00	22.3
39	31	-303	2895	-156	0	-303	-1140	4.02	4.02	4.02	4.02	3	0.16	0.08	0.51	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	62	-375	2072	-146	0	-192	1332	4.02	4.02	4.02	4.02	3	0.19	0.06	0.37	0.00	0.00	22.3
2	62	-329	1565	28	0	-49	989	4.02	4.02	4.02	4.02	2	0.15	0.05	0.28	0.00	0.00	22.3
3	62	-362	1671	25	0	-51	1066	4.02	4.02	4.02	4.02	2	0.16	0.05	0.30	0.00	0.00	22.3
4	62	-215	1516	-249	0	-244	986	4.02	4.02	4.02	4.02	2	0.15	0.04	0.27	0.00	0.00	22.3
5	62	-247	1622	-252	0	-246	1060	4.02	4.02	4.02	4.02	2	0.16	0.05	0.29	0.00	0.00	22.3
6	62	-252	1424	-65	0	-115	928	4.02	4.02	4.02	4.02	2	0.14	0.04	0.25	0.00	0.00	22.3
7	62	-359	1777	-76	0	-121	1153	4.02	4.02	4.02	4.02	2	0.17	0.05	0.31	0.00	0.00	22.3
8	62	-217	1409	-148	0	-173	931	4.02	4.02	4.02	4.02	2	0.14	0.04	0.25	0.00	0.00	22.3
9	62	-325	1762	-159	0	-180	1152	4.02	4.02	4.02	4.02	2	0.17	0.05	0.31	0.00	0.00	22.3
10	62	-329	1565	28	0	-49	989	4.02	4.02	4.02	4.02	2	0.15	0.05	0.28	0.00	0.00	22.3
11	62	-362	1671	25	0	-51	1066	4.02	4.02	4.02	4.02	2	0.16	0.05	0.30	0.00	0.00	22.3
12	62	-215	1516	-249	0	-244	986	4.02	4.02	4.02	4.02	2	0.15	0.04	0.27	0.00	0.00	22.3
13	62	-247	1622	-252	0	-246	1060	4.02	4.02	4.02	4.02	2	0.16	0.05	0.29	0.00	0.00	22.3
14	62	-252	1424	-65	0	-115	928	4.02	4.02	4.02	4.02	2	0.14	0.04	0.25	0.00	0.00	22.3
15	62	-359	1777	-76	0	-121	1153	4.02	4.02	4.02	4.02	2	0.17	0.05	0.31	0.00	0.00	22.3
16	62	-217	1409	-148	0	-173	931	4.02	4.02	4.02	4.02	2	0.14	0.04	0.25	0.00	0.00	22.3
17	62	-325	1762	-159	0	-180	1152	4.02	4.02	4.02	4.02	2	0.17	0.05	0.31	0.00	0.00	22.3
18	62	-482	2126	109	0	-129	1252	4.02	4.02	4.02	4.02	3	0.18	0.06	0.37	0.00	0.00	22.3
19	62	-176	2075	-697	0	-656	1352	4.02	4.02	4.02	4.02	3	0.19	0.06	0.37	0.00	0.00	22.3
20	62	-306	2103	-241	0	-349	1390	4.02	4.02	4.02	4.02	3	0.20	0.06	0.37	0.00	0.00	22.3
37	62	-595	2109	426	0	113	1212	4.02	4.02	4.02	4.02	3	0.17	0.06	0.37	0.00	0.00	22.3
38	62	-87	2023	-917	0	-766	1365	4.02	4.02	4.02	4.02	3	0.20	0.06	0.36	0.00	0.00	22.3
39	62	-303	2071	-156	0	-255	1430	4.02	4.02	4.02	4.02	3	0.20	0.06	0.37	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	93	-375	1280	-146	0	-146	1332	4.02	4.02	4.02	4.02	3	0.19	0.04	0.23	0.00	0.00	22.3
2	93	-329	956	28	0	-58	989	4.02	4.02	4.02	4.02	2	0.15	0.03	0.17	0.00	0.00	22.3
3	93	-362	1062	25	0	-59	1066	4.02	4.02	4.02	4.02	2	0.16	0.03	0.19	0.00	0.00	22.3
4	93	-215	907	-249	0	-167	986	4.02	4.02	4.02	4.02	2	0.15	0.03	0.16	0.00	0.00	22.3
5	93	-247	1013	-252	0	-168	1060	4.02	4.02	4.02	4.02	2	0.16	0.03	0.18	0.00	0.00	22.3
6	93	-252	815	-65	0	-95	928	4.02	4.02	4.02	4.02	2	0.14	0.02	0.14	0.00	0.00	22.3
7	93	-359	1168	-76	0	-98	1153	4.02	4.02	4.02	4.02	2	0.17	0.03	0.21	0.00	0.00	22.3
8	93	-217	800	-148	0	-127	931	4.02	4.02	4.02	4.02	2	0.14	0.02	0.14	0.00	0.00	22.3
9	93	-325	1153	-159	0	-131	1152	4.02	4.02	4.02	4.02	2	0.17	0.03	0.20	0.00	0.00	22.3
10	93	-329	956	28	0	-58	989	4.02	4.02	4.02	4.02	2	0.15	0.03	0.17	0.00	0.00	22.3
11	93	-362	1062	25	0	-59	1066	4.02	4.02	4.02	4.02	2	0.16	0.03	0.19	0.00	0.00	22.3
12	93	-215	907	-249	0	-167	986	4.02	4.02	4.02	4.02	2	0.15	0.03	0.16	0.00	0.00	22.3
13	93	-247	1013	-252	0	-168	1060	4.02	4.02	4.02	4.02	2	0.16	0.03	0.18	0.00	0.00	22.3
14	93	-252	815	-65	0	-95	928	4.02	4.02	4.02	4.02	2	0.14	0.02	0.14	0.00	0.00	22.3
15	93	-359	1168	-76	0	-98	1153	4.02	4.02	4.02	4.02	2	0.17	0.03	0.21	0.00	0.00	22.3
16	93	-217	800	-148	0	-127	931	4.02	4.02	4.02	4.02	2	0.14	0.02	0.14	0.00	0.00	22.3
17	93	-325	1153	-159	0	-131	1152	4.02	4.02	4.02	4.02	2	0.17	0.03	0.20	0.00	0.00	22.3
18	93	-482	1269	109	0	-162	1252	4.02	4.02	4.02	4.02	3	0.18	0.04	0.22	0.00	0.00	22.3
19	93	-176	1217	-697	0	-440	1352	4.02	4.02	4.02	4.02	3	0.19	0.04	0.22	0.00	0.00	22.3
20	93	-306	1245	-241	0	-275	1390	4.02	4.02	4.02	4.02	3	0.20	0.04	0.22	0.00	0.00	22.3
37	93	-595	1285	426	0	-19	1212	4.02	4.02	4.02	4.02	3	0.17	0.04	0.23	0.00	0.00	22.3
38	93	-87	1199	-917	0	-482	1365	4.02	4.02	4.02	4.02	3	0.20	0.03	0.21	0.00	0.00	22.3
39	93	-303	1246	-156	0	-207	1430	4.02	4.02	4.02	4.02	3	0.20	0.04	0.22	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	124	-375	489	-146	0	-101	1332	4.02	4.02	4.02	4.02	3	0.19	0.01	0.09	0.00	0.00	22.3
2	124	-329	347	28	0	-66	989	4.02	4.02	4.02	4.02	2	0.15	0.01	0.06	0.00	0.00	22.3
3	124	-362	453	25	0	-66	1066	4.02	4.02	4.02	4.02	2	0.16	0.01	0.08	0.00	0.00	22.3
4	124	-215	298	-249	0	-90	986	4.02	4.02	4.02	4.02	2	0.15	0.01	0.05	0.00	0.00	22.3
5	124	-247	404	-252	0	-89	1060	4.02	4.02	4.02	4.02	2	0.16	0.01	0.07	0.00	0.00	22.3
6	124	-252	206	-65	0	-75	928	4.02	4.02	4.02	4.02	2	0.14	0.01	0.04	0.00	0.00	22.3
7	124	-359	559	-76	0	-74	1153	4.02	4.02	4.02	4.02	2	0.17	0.02	0.10	0.00	0.00	22.3
8	124	-217	191	-148	0	-82	931	4.02	4.02	4.02	4.02	2	0.14	0.01	0.03	0.00	0.00	22.3
9	124	-325	544	-159	0	-81	1152	4.02	4.02	4.02	4.02	2	0.17	0.02	0.10	0.00	0.00	22.3
10	124	-329	347	28	0	-66	989	4.02	4.02	4.02	4.02	2	0.15	0.01	0.06	0.00	0.00	22.3
11	124	-362	453	25	0	-66	1066	4.02	4.02	4.02	4.02	2	0.16	0.01	0.08	0.00	0.00	22.3
12	124	-215	298	-249	0	-90	986	4.02	4.02	4.02	4.02	2	0.15	0.01	0.05	0.00	0.00	22.3
13	124	-247	404	-252	0	-89	1060	4.02	4.02	4.02	4.02	2	0.16	0.01	0.07	0.00	0.00	22.3
14	124	-252	206	-65	0	-75	928	4.02	4.02	4.02	4.02	2	0.14	0.01	0.04	0.00	0.00	22.3
15	124	-359	559	-76	0	-74	1153	4.02	4.02	4.02	4.02	2	0.17	0.02	0.10	0.00	0.00	22.3
16	124	-217	191	-148	0	-82	931	4.02	4.02	4.02	4.02	2	0.14	0.01	0.03	0.00	0.00	22.3
17	124	-325	544	-159	0	-81	1152	4.02	4.02	4.02	4.02	2	0.17	0.02	0.10	0.00	0.00	22.3
18	124	-482	411	109	0	-196	1252	4.02	4.02	4.02	4.02	3	0.18	0.01	0.07	0.00	0.00	22.3
19	124	-176	359	-697	0	-224	1352	4.02	4.02	4.02	4.02	3	0.19	0.02	0.11	0.00	0.00	22.3
20	124	-306	387	-241	0	-200	1390	4.02	4.02	4.02	4.02	3	0.20	0.01	0.07	0.00	0.00	22.3
37	124	-595	460	426	0	-151	1212	4.02	4.02	4.02	4.02	3	0.17	0.01	0.08	0.00	0.00	22.3

38	124	-87	374	-917	0	-198	1365	4.02	4.02	4.02	4.02	3	0.20	0.03	0.15	0.00	0.00	22.3
39	124	-303	421	-156	0	-158	1430	4.02	4.02	4.02	4.02	3	0.20	0.01	0.07	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	155	-375	-303	-146	0	-56	1332	4.02	4.02	4.02	4.02	3	0.19	0.01	0.05	0.00	0.00	22.3
2	155	-329	-261	28	0	-75	989	4.02	4.02	4.02	4.02	2	0.15	0.01	0.05	0.00	0.00	22.3
3	155	-362	-155	25	0	-74	1066	4.02	4.02	4.02	4.02	2	0.16	0.00	0.03	0.00	0.00	22.3
4	155	-215	-311	-249	0	-12	986	4.02	4.02	4.02	4.02	2	0.15	0.01	0.06	0.00	0.00	22.3
5	155	-247	-205	-252	0	-11	1060	4.02	4.02	4.02	4.02	2	0.16	0.01	0.04	0.00	0.00	22.3
6	155	-252	-402	-65	0	-54	928	4.02	4.02	4.02	4.02	2	0.14	0.01	0.07	0.00	0.00	22.3
7	155	-359	-49	-76	0	-51	1153	4.02	4.02	4.02	4.02	2	0.17	0.00	0.01	0.00	0.00	22.3
8	155	-217	-418	-148	0	-36	931	4.02	4.02	4.02	4.02	2	0.14	0.01	0.07	0.00	0.00	22.3
9	155	-325	-64	-159	0	-32	1152	4.02	4.02	4.02	4.02	2	0.17	0.00	0.03	0.00	0.00	22.3
10	155	-329	-261	28	0	-75	989	4.02	4.02	4.02	4.02	2	0.15	0.01	0.05	0.00	0.00	22.3
11	155	-362	-155	25	0	-74	1066	4.02	4.02	4.02	4.02	2	0.16	0.00	0.03	0.00	0.00	22.3
12	155	-215	-311	-249	0	-12	986	4.02	4.02	4.02	4.02	2	0.15	0.01	0.06	0.00	0.00	22.3
13	155	-247	-205	-252	0	-11	1060	4.02	4.02	4.02	4.02	2	0.16	0.01	0.04	0.00	0.00	22.3
14	155	-252	-402	-65	0	-54	928	4.02	4.02	4.02	4.02	2	0.14	0.01	0.07	0.00	0.00	22.3
15	155	-359	-49	-76	0	-51	1153	4.02	4.02	4.02	4.02	2	0.17	0.00	0.01	0.00	0.00	22.3
16	155	-217	-418	-148	0	-36	931	4.02	4.02	4.02	4.02	2	0.14	0.01	0.07	0.00	0.00	22.3
17	155	-325	-64	-159	0	-32	1152	4.02	4.02	4.02	4.02	2	0.17	0.00	0.03	0.00	0.00	22.3
18	155	-482	-447	109	0	-230	1252	4.02	4.02	4.02	4.02	3	0.18	0.01	0.08	0.00	0.00	22.3
19	155	-176	-499	-697	0	-8	1352	4.02	4.02	4.02	4.02	3	0.19	0.02	0.11	0.00	0.00	22.3
20	155	-306	-471	-241	0	-125	1390	4.02	4.02	4.02	4.02	3	0.20	0.01	0.08	0.00	0.00	22.3
37	155	-595	-365	426	0	-283	1212	4.02	4.02	4.02	4.02	3	0.17	0.01	0.07	0.00	0.00	22.3
38	155	-87	-451	-917	0	86	1365	4.02	4.02	4.02	4.02	3	0.20	0.03	0.15	0.00	0.00	22.3
39	155	-303	-403	-156	0	-110	1430	4.02	4.02	4.02	4.02	3	0.20	0.01	0.07	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	186	-375	-1095	-145	0	-11	1332	4.02	4.02	4.02	4.02	3	0.19	0.03	0.19	0.00	0.00	22.3
2	186	-329	-870	28	0	-84	989	4.02	4.02	4.02	4.02	2	0.15	0.03	0.15	0.00	0.00	22.3
3	186	-362	-764	25	0	-82	1066	4.02	4.02	4.02	4.02	2	0.16	0.02	0.13	0.00	0.00	22.3
4	186	-215	-920	-249	0	65	986	4.02	4.02	4.02	4.02	2	0.15	0.03	0.16	0.00	0.00	22.3
5	186	-247	-814	-252	0	67	1060	4.02	4.02	4.02	4.02	2	0.16	0.02	0.14	0.00	0.00	22.3
6	186	-252	-1011	-65	0	-34	928	4.02	4.02	4.02	4.02	2	0.14	0.03	0.18	0.00	0.00	22.3
7	186	-359	-658	-76	0	-27	1153	4.02	4.02	4.02	4.02	2	0.17	0.02	0.12	0.00	0.00	22.3
8	186	-217	-1026	-148	0	10	931	4.02	4.02	4.02	4.02	2	0.14	0.03	0.18	0.00	0.00	22.3
9	186	-325	-673	-159	0	17	1152	4.02	4.02	4.02	4.02	2	0.17	0.02	0.12	0.00	0.00	22.3
10	186	-329	-870	28	0	-84	989	4.02	4.02	4.02	4.02	2	0.15	0.03	0.15	0.00	0.00	22.3
11	186	-362	-764	25	0	-82	1066	4.02	4.02	4.02	4.02	2	0.16	0.02	0.13	0.00	0.00	22.3
12	186	-215	-920	-249	0	65	986	4.02	4.02	4.02	4.02	2	0.15	0.03	0.16	0.00	0.00	22.3
13	186	-247	-814	-252	0	67	1060	4.02	4.02	4.02	4.02	2	0.16	0.02	0.14	0.00	0.00	22.3
14	186	-252	-1011	-65	0	-34	928	4.02	4.02	4.02	4.02	2	0.14	0.03	0.18	0.00	0.00	22.3
15	186	-359	-658	-76	0	-27	1153	4.02	4.02	4.02	4.02	2	0.17	0.02	0.12	0.00	0.00	22.3
16	186	-217	-1026	-148	0	10	931	4.02	4.02	4.02	4.02	2	0.14	0.03	0.18	0.00	0.00	22.3
17	186	-325	-673	-159	0	17	1152	4.02	4.02	4.02	4.02	2	0.17	0.02	0.12	0.00	0.00	22.3
18	186	-482	-1305	109	0	-263	1252	4.02	4.02	4.02	4.02	3	0.18	0.04	0.23	0.00	0.00	22.3
19	186	-176	-1356	-697	0	209	1352	4.02	4.02	4.02	4.02	3	0.19	0.04	0.24	0.00	0.00	22.3
20	186	-306	-1328	-241	0	-51	1390	4.02	4.02	4.02	4.02	3	0.20	0.04	0.23	0.00	0.00	22.3
37	186	-595	-1190	426	0	-416	1212	4.02	4.02	4.02	4.02	3	0.17	0.03	0.21	0.00	0.00	22.3
38	186	-87	-1276	-917	0	371	1365	4.02	4.02	4.02	4.02	3	0.20	0.04	0.23	0.00	0.00	22.3
39	186	-303	-1228	-156	0	-61	1430	4.02	4.02	4.02	4.02	3	0.20	0.04	0.22	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	217	-375	-1886	-145	0	34	1332	4.02	4.02	4.02	4.02	3	0.19	0.05	0.33	0.00	0.00	22.3
2	217	-329	-1479	28	0	-93	989	4.02	4.02	4.02	4.02	2	0.15	0.04	0.26	0.00	0.00	22.3
3	217	-362	-1373	25	0	-90	1066	4.02	4.02	4.02	4.02	2	0.16	0.04	0.24	0.00	0.00	22.3
4	217	-215	-1529	-249	0	142	986	4.02	4.02	4.02	4.02	2	0.15	0.04	0.27	0.00	0.00	22.3
5	217	-247	-1423	-252	0	145	1060	4.02	4.02	4.02	4.02	2	0.16	0.04	0.25	0.00	0.00	22.3
6	217	-252	-1620	-65	0	-14	928	4.02	4.02	4.02	4.02	2	0.14	0.05	0.29	0.00	0.00	22.3
7	217	-359	-1267	-76	0	-4	1153	4.02	4.02	4.02	4.02	2	0.17	0.04	0.22	0.00	0.00	22.3
8	217	-217	-1635	-148	0	56	931	4.02	4.02	4.02	4.02	2	0.14	0.05	0.29	0.00	0.00	22.3
9	217	-325	-1282	-159	0	67	1152	4.02	4.02	4.02	4.02	2	0.17	0.04	0.23	0.00	0.00	22.3
10	217	-329	-1479	28	0	-93	989	4.02	4.02	4.02	4.02	2	0.15	0.04	0.26	0.00	0.00	22.3
11	217	-362	-1373	25	0	-90	1066	4.02	4.02	4.02	4.02	2	0.16	0.04	0.24	0.00	0.00	22.3
12	217	-215	-1529	-249	0	142	986	4.02	4.02	4.02	4.02	2	0.15	0.04	0.27	0.00	0.00	22.3
13	217	-247	-1423	-252	0	145	1060	4.02	4.02	4.02	4.02	2	0.16	0.04	0.25	0.00	0.00	22.3
14	217	-252	-1620	-65	0	-14	928	4.02	4.02	4.02	4.02	2	0.14	0.05	0.29	0.00	0.00	22.3
15	217	-359	-1267	-76	0	-4	1153	4.02	4.02	4.02	4.02	2	0.17	0.04	0.22	0.00	0.00	22.3
16	217	-217	-1635	-148	0	56	931	4.02	4.02	4.02	4.02	2	0.14	0.05	0.29	0.00	0.00	22.3
17	217	-325	-1282	-159	0	67	1152	4.02	4.02	4.02	4.02	2	0.17	0.04	0.23	0.00	0.00	22.3
18	217	-482	-2163	109	0	-297	1252	4.02	4.02	4.02	4.02	3	0.18	0.06	0.38	0.00	0.00	22.3
19	217	-176	-2214	-697	0	425	1352	4.02	4.02	4.02	4.02	3	0.19	0.06	0.39	0.00	0.00	22.3
20	217	-306	-2186	-241	0	24	1390	4.02	4.02	4.02	4.02	3	0.20	0.06	0.39	0.00	0.00	22.3
37	217	-595	-2015	426	0	-548	1212	4.02	4.02	4.02	4.02	3	0.17	0.06	0.35	0.00	0.00	22.3
38	217	-87	-2101	-917	0	655	1365	4.02	4.02	4.02	4.02	3	0.20	0.06	0.37	0.00	0.00	22.3
39	217	-303	-2053	-156	0	-13	1430	4.02	4.02	4.02	4.02	3	0.20	0.06	0.36	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	248	-375	-2678	-146	0	79	-1410	4.02	4.02	4.02	4.02	3	0.20	0.08	0.47	0.00	0.00	22.3
2	248	-329	-2088	28	0	-102	-1161	4.02	4.02	4.02	4.02	2	0.17	0.06	0.37	0.00	0.00	22.3
3	248	-362	-1982	25	0	-98	1066	4.02	4.02	4.02	4.02	2	0.16	0.06	0.35	0.00	0.00	22.3
4	248	-215	-2138	-249	0	219	-1237	4.02	4.02	4.02	4.02	2	0.19	0.06	0.38	0.00	0.00	22.3
5	248	-247	-2032	-252	0	223	1049	4.02	4.02	4.02	4.02	2	0.16	0.06	0.36	0.00	0.00	22.3
6	248	-252	-2229	-65	0	6	-1455	4.02	4.02	4.02	4.02	2	0.22	0.06	0.39	0.00	0.00	22.3
7	248	-359	-1876	-76	0	20	1153	4.02	4.02	4.02	4.02	2	0.17	0.05	0.33	0.00	0.00	22.3
8	248	-217	-2244	-148	0	102	-1478	4.02	4.02	4.02	4.02	2	0.22	0.07	0.40	0.00	0.00	22.3
9	248	-325	-1891	-159	0	116	1152	4.02	4.02	4.02	4.02	2	0.17	0.05	0.33	0.00	0.00	22.3
10	248	-329	-2088	28	0	-102	-1161	4.02	4.02	4.02	4.02	2	0.17	0.06	0.37	0.00	0.00	22.3
11	248	-362	-1982	25	0	-98	1066	4.02	4.02	4.02	4.02	2	0.16	0.06	0.35	0.00	0.00	22.3
12	248	-215	-2138	-249	0	219	-1237	4.02	4.02	4.02	4.02	2	0.19	0.06	0.38	0.00	0.00	22.3
13	248	-247	-2032	-252	0	223	1049	4.02	4.02	4.02	4.02	2	0.16	0.06	0.36	0.00	0.00	22.3
14	248	-252	-2229	-65	0	6	-1455	4.02	4.02	4.02	4.02	2	0.22	0.06	0.39	0.00	0.00	22.3
15	248	-359	-1876	-76	0	20	1153	4.02	4.02	4.02	4.02	2	0.17	0.05	0.33	0.00	0.00	22.3
16	248	-217	-2244	-148	0	102	-1478	4.02	4.02	4.02	4.02	2	0.22	0.07	0.40	0.00	0.00	22.3
17	248	-325	-1891	-159	0	116	1152	4.02	4.02	4.02	4.02	2	0.17	0.05	0.33	0.00	0.00	22.3
18	248	-482	-3020	109	0	-331	-1895	4.02	4.02	4.02	4.02	3	0.27	0.09	0.53	0.00	0.00	22.3
19	248	-176	-3072	-697	0	641	-1885	4.02	4.02	4.02	4.02	3	0.27	0.09	0.54	0.00	0.00	22.3
20	248	-306	-3044	-241	0	99	-1798	4.02	4.02	4.02	4.02	3	0.26	0.09	0.54	0.00	0.00	22.3
37	248	-595	-2839	426	0	-680	-1715	4.02	4.02	4.02	4.02	3	0.24	0.08	0.50	0.00	0.00	22.3
38	248	-87	-2925	-917	0	939	-1698	4.02	4.02	4.02	4.02	3	0.24	0.08	0.52	0.00	0.00	22.3
39	248	-303	-2878	-156	0	36	-1552	4.02	4.02	4.02	4.02	3	0.22	0.08	0.51	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	279	-375	-3469	-146	0	124	-2206	4.02	4.02	4.02	4.02	3	0.31	0.10	0.61	0.00	0.00	22.3

2	279	-329	-2697	28	0	-111	-1776	4.02	4.02	4.02	4.02	2	0.27	0.08	0.48	0.00	0.00	22.3
3	279	-362	-2591	25	0	-105	-1535	4.02	4.02	4.02	4.02	2	0.23	0.08	0.46	0.00	0.00	22.3
4	279	-215	-2747	-249	0	297	-1858	4.02	4.02	4.02	4.02	2	0.28	0.08	0.49	0.00	0.00	22.3
5	279	-247	-2641	-252	0	302	-1617	4.02	4.02	4.02	4.02	2	0.24	0.08	0.47	0.00	0.00	22.3
6	279	-252	-2838	-65	0	26	-2086	4.02	4.02	4.02	4.02	2	0.31	0.08	0.50	0.00	0.00	22.3
7	279	-359	-2485	-76	0	43	-1283	4.02	4.02	4.02	4.02	2	0.19	0.07	0.44	0.00	0.00	22.3
8	279	-217	-2853	-148	0	148	-2111	4.02	4.02	4.02	4.02	2	0.32	0.08	0.51	0.00	0.00	22.3
9	279	-325	-2500	-159	0	165	-1307	4.02	4.02	4.02	4.02	2	0.20	0.07	0.44	0.00	0.00	22.3
10	279	-329	-2697	28	0	-111	-1776	4.02	4.02	4.02	4.02	2	0.27	0.08	0.48	0.00	0.00	22.3
11	279	-362	-2591	25	0	-105	-1535	4.02	4.02	4.02	4.02	2	0.23	0.08	0.46	0.00	0.00	22.3
12	279	-215	-2747	-249	0	297	-1858	4.02	4.02	4.02	4.02	2	0.28	0.08	0.49	0.00	0.00	22.3
13	279	-247	-2641	-252	0	302	-1617	4.02	4.02	4.02	4.02	2	0.24	0.08	0.47	0.00	0.00	22.3
14	279	-252	-2838	-65	0	26	-2086	4.02	4.02	4.02	4.02	2	0.31	0.08	0.50	0.00	0.00	22.3
15	279	-359	-2485	-76	0	43	-1283	4.02	4.02	4.02	4.02	2	0.19	0.07	0.44	0.00	0.00	22.3
16	279	-217	-2853	-148	0	148	-2111	4.02	4.02	4.02	4.02	2	0.32	0.08	0.51	0.00	0.00	22.3
17	279	-325	-2500	-159	0	165	-1307	4.02	4.02	4.02	4.02	2	0.20	0.07	0.44	0.00	0.00	22.3
18	279	-482	-3878	109	0	-364	-2771	4.02	4.02	4.02	4.02	3	0.39	0.11	0.68	0.00	0.00	22.3
19	279	-176	-3930	-697	0	857	-2767	4.02	4.02	4.02	4.02	3	0.39	0.11	0.70	0.00	0.00	22.3
20	279	-306	-3902	-241	0	173	-2676	4.02	4.02	4.02	4.02	3	0.38	0.11	0.69	0.00	0.00	22.3
37	279	-595	-3664	426	0	-812	-2549	4.02	4.02	4.02	4.02	3	0.36	0.11	0.64	0.00	0.00	22.3
38	279	-87	-3750	-917	0	1223	-2542	4.02	4.02	4.02	4.02	3	0.36	0.11	0.67	0.00	0.00	22.3
39	279	-303	-3702	-156	0	84	-2391	4.02	4.02	4.02	4.02	3	0.34	0.11	0.65	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	310	-375	-4261	-146	0	169	-2206	4.02	4.02	4.02	4.02	3	0.31	0.12	0.75	0.00	0.00	22.3
2	310	-329	-3306	28	0	-119	-1776	4.02	4.02	4.02	4.02	2	0.27	0.10	0.58	0.00	0.00	22.3
3	310	-362	-3200	25	0	-113	-1535	4.02	4.02	4.02	4.02	2	0.23	0.09	0.57	0.00	0.00	22.3
4	310	-215	-3356	-249	0	374	-1858	4.02	4.02	4.02	4.02	2	0.28	0.10	0.59	0.00	0.00	22.3
5	310	-247	-3250	-252	0	380	-1617	4.02	4.02	4.02	4.02	2	0.24	0.09	0.58	0.00	0.00	22.3
6	310	-252	-3447	-65	0	46	-2086	4.02	4.02	4.02	4.02	2	0.31	0.10	0.61	0.00	0.00	22.3
7	310	-359	-3094	-76	0	66	-1283	4.02	4.02	4.02	4.02	2	0.19	0.09	0.55	0.00	0.00	22.3
8	310	-217	-3462	-148	0	194	-2111	4.02	4.02	4.02	4.02	2	0.32	0.10	0.61	0.00	0.00	22.3
9	310	-325	-3109	-159	0	214	-1307	4.02	4.02	4.02	4.02	2	0.20	0.09	0.55	0.00	0.00	22.3
10	310	-329	-3306	28	0	-119	-1776	4.02	4.02	4.02	4.02	2	0.27	0.10	0.58	0.00	0.00	22.3
11	310	-362	-3200	25	0	-113	-1535	4.02	4.02	4.02	4.02	2	0.23	0.09	0.57	0.00	0.00	22.3
12	310	-215	-3356	-249	0	374	-1858	4.02	4.02	4.02	4.02	2	0.28	0.10	0.59	0.00	0.00	22.3
13	310	-247	-3250	-252	0	380	-1617	4.02	4.02	4.02	4.02	2	0.24	0.09	0.58	0.00	0.00	22.3
14	310	-252	-3447	-65	0	46	-2086	4.02	4.02	4.02	4.02	2	0.31	0.10	0.61	0.00	0.00	22.3
15	310	-359	-3094	-76	0	66	-1283	4.02	4.02	4.02	4.02	2	0.19	0.09	0.55	0.00	0.00	22.3
16	310	-217	-3462	-148	0	194	-2111	4.02	4.02	4.02	4.02	2	0.32	0.10	0.61	0.00	0.00	22.3
17	310	-325	-3109	-159	0	214	-1307	4.02	4.02	4.02	4.02	2	0.20	0.09	0.55	0.00	0.00	22.3
18	310	-482	-4736	109	0	-398	-2771	4.02	4.02	4.02	4.02	3	0.39	0.14	0.83	0.00	0.00	22.3
19	310	-176	-4788	-697	0	1073	-2767	4.02	4.02	4.02	4.02	3	0.39	0.14	0.85	0.00	0.00	22.3
20	310	-306	-4760	-241	0	248	-2676	4.02	4.02	4.02	4.02	3	0.38	0.14	0.84	0.00	0.00	22.3
37	310	-595	-4489	426	0	-944	-2549	4.02	4.02	4.02	4.02	3	0.36	0.13	0.79	0.00	0.00	22.3
38	310	-87	-4575	-917	0	1507	-2542	4.02	4.02	4.02	4.02	3	0.37	0.13	0.81	0.00	0.00	22.3
39	310	-303	-4527	-156	0	133	-2391	4.02	4.02	4.02	4.02	3	0.34	0.13	0.80	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

Nome travata: **trave_504_IP1** Descrizione: **Trave_5 11-10-9-8**
ASTA NUM. 11 NI 294 NF 124 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y Permanente Neve qy tot.
qy medio: 375.00 1325.25 142.50 1842.75 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-668	3787	34	0	156	-1779	4.02	4.02	4.02	4.02	3	0.25	0.11	0.66	0.00	0.00	22.3
2	0	-648	2848	-68	0	-111	-1215	4.02	4.02	4.02	4.02	2	0.18	0.08	0.50	0.00	0.00	22.3
3	0	-512	2947	-68	0	-109	-1453	4.02	4.02	4.02	4.02	2	0.22	0.09	0.52	0.00	0.00	22.3
4	0	-516	2879	120	0	349	-1283	4.02	4.02	4.02	4.02	2	0.19	0.08	0.51	0.00	0.00	22.3
5	0	-380	2978	121	0	351	-1522	4.02	4.02	4.02	4.02	2	0.23	0.09	0.53	0.00	0.00	22.3
6	0	-761	2744	-3	0	48	-961	4.02	4.02	4.02	4.02	2	0.14	0.08	0.48	0.00	0.00	22.3
7	0	-307	3073	-0	0	54	-1755	4.02	4.02	4.02	4.02	2	0.26	0.09	0.54	0.00	0.00	22.3
8	0	-721	2753	53	0	186	-981	4.02	4.02	4.02	4.02	2	0.15	0.08	0.48	0.00	0.00	22.3
9	0	-268	3082	56	0	192	-1775	4.02	4.02	4.02	4.02	2	0.27	0.09	0.55	0.00	0.00	22.3
10	0	-648	2848	-68	0	-111	-1215	4.02	4.02	4.02	4.02	2	0.18	0.08	0.50	0.00	0.00	22.3
11	0	-512	2947	-68	0	-109	-1453	4.02	4.02	4.02	4.02	2	0.22	0.09	0.52	0.00	0.00	22.3
12	0	-516	2879	120	0	349	-1283	4.02	4.02	4.02	4.02	2	0.19	0.08	0.51	0.00	0.00	22.3
13	0	-380	2978	121	0	351	-1522	4.02	4.02	4.02	4.02	2	0.23	0.09	0.53	0.00	0.00	22.3
14	0	-761	2744	-3	0	48	-961	4.02	4.02	4.02	4.02	2	0.14	0.08	0.48	0.00	0.00	22.3
15	0	-307	3073	-0	0	54	-1755	4.02	4.02	4.02	4.02	2	0.26	0.09	0.54	0.00	0.00	22.3
16	0	-721	2753	53	0	186	-981	4.02	4.02	4.02	4.02	2	0.15	0.08	0.48	0.00	0.00	22.3
17	0	-268	3082	56	0	192	-1775	4.02	4.02	4.02	4.02	2	0.27	0.09	0.55	0.00	0.00	22.3
18	0	-1191	3850	-194	0	-305	-1206	4.02	4.02	4.02	4.02	3	0.17	0.11	0.67	0.00	0.00	22.3
19	0	-575	4107	372	0	1045	-1802	4.02	4.02	4.02	4.02	3	0.25	0.12	0.72	0.00	0.00	22.3
20	0	-1079	4005	90	0	372	-1632	4.02	4.02	4.02	4.02	3	0.23	0.12	0.70	0.00	0.00	22.3
37	0	-1321	3629	-400	0	-825	-1047	4.02	4.02	4.02	4.02	3	0.20	0.10	0.63	0.00	0.00	22.3
38	0	-296	4057	542	0	1426	-2040	4.02	4.02	4.02	4.02	3	0.35	0.12	0.72	0.00	0.00	22.3
39	0	-1135	3888	73	0	304	-1756	4.02	4.02	4.02	4.02	3	0.24	0.11	0.67	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	38	-668	2958	34	0	143	-1779	4.02	4.02	4.02	4.02	3	0.25	0.09	0.52	0.00	0.00	22.3
2	38	-648	2210	-68	0	-86	-1215	4.02	4.02	4.02	4.02	2	0.18	0.06	0.39	0.00	0.00	22.3
3	38	-512	2309	-68	0	-84	-1453	4.02	4.02	4.02	4.02	2	0.22	0.07	0.41	0.00	0.00	22.3
4	38	-516	2241	120	0	304	-1283	4.02	4.02	4.02	4.02	2	0.19	0.06	0.39	0.00	0.00	22.3
5	38	-380	2340	121	0	306	-1522	4.02	4.02	4.02	4.02	2	0.23	0.07	0.41	0.00	0.00	22.3
6	38	-761	2106	-3	0	49	-961	4.02	4.02	4.02	4.02	2	0.14	0.06	0.37	0.00	0.00	22.3
7	38	-307	2435	-0	0	54	-1755	4.02	4.02	4.02	4.02	2	0.26	0.07	0.43	0.00	0.00	22.3
8	38	-721	2115	53	0	166	-981	4.02	4.02	4.02	4.02	2	0.15	0.06	0.37	0.00	0.00	22.3
9	38	-268	2444	56	0	171	-1775	4.02	4.02	4.02	4.02	2	0.27	0.07	0.43	0.00	0.00	22.3
10	38	-648	2210	-68	0	-86	-1215	4.02	4.02	4.02	4.02	2	0.18	0.06	0.39	0.00	0.00	22.3
11	38	-512	2309	-68	0	-84	-1453	4.02	4.02	4.02	4.02	2	0.22	0.07	0.41	0.00	0.00	22.3
12	38	-516	2241	120	0	304	-1283	4.02	4.02	4.02	4.02	2	0.19	0.06	0.39	0.00	0.00	22.3
13	38	-380	2340	121	0	306	-1522	4.02	4.02	4.02	4.02	2	0.23	0.07	0.41	0.00	0.00	22.3
14	38	-761	2106	-3	0	49	-961	4.02	4.02	4.02	4.02	2	0.14	0.06	0.37	0.00	0.00	22.3
15	38	-307	2435	-0	0	54	-1755	4.02	4.02	4.02	4.02	2	0.26	0.07	0.43	0.00	0.00	22.3
16	38	-721	2115	53	0	166	-981	4.02	4.02	4.02	4.02	2	0.15	0.06	0.37	0.00	0.00	22.3
17	38	-268	2444	56	0	171	-1775	4.02	4.02	4.02	4.02	2	0.27	0.07	0.43	0.00	0.00	22.3
18	38	-1191	2941	-194	0	-233	1556	4.02	4.02	4.02	4.02	3	0.22	0.08	0.51	0.00	0.00	22.3
19	38	-575	3198	372	0	906	-1802	4.02	4.02	4.02	4.02	3	0.25	0.09	0.56	0.00	0.00	22.3

20	38	-1079	3096	90	0	338	-1632	4.02	4.02	4.02	4.02	3	0.23	0.09	0.54	0.00	0.00	22.3
37	38	-1321	2760	-400	0	-675	1548	4.02	4.02	4.02	4.02	3	0.21	0.08	0.48	0.00	0.00	22.3
38	38	-296	3188	542	0	1223	-2040	4.02	4.02	4.02	4.02	3	0.30	0.09	0.56	0.00	0.00	22.3
39	38	-1135	3019	73	0	277	-1756	4.02	4.02	4.02	4.02	3	0.24	0.09	0.52	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	75	-668	2129	34	0	130	1436	4.02	4.02	4.02	4.02	3	0.20	0.06	0.37	0.00	0.00	22.3
2	75	-648	1573	-68	0	-60	1145	4.02	4.02	4.02	4.02	2	0.17	0.05	0.28	0.00	0.00	22.3
3	75	-512	1672	-68	0	-59	1083	4.02	4.02	4.02	4.02	2	0.16	0.05	0.29	0.00	0.00	22.3
4	75	-516	1604	120	0	259	1127	4.02	4.02	4.02	4.02	2	0.17	0.05	0.28	0.00	0.00	22.3
5	75	-380	1703	121	0	260	1073	4.02	4.02	4.02	4.02	2	0.16	0.05	0.30	0.00	0.00	22.3
6	75	-761	1469	-3	0	50	1242	4.02	4.02	4.02	4.02	2	0.18	0.04	0.26	0.00	0.00	22.3
7	75	-307	1798	-0	0	54	982	4.02	4.02	4.02	4.02	2	0.15	0.05	0.32	0.00	0.00	22.3
8	75	-721	1478	53	0	146	1235	4.02	4.02	4.02	4.02	2	0.18	0.04	0.26	0.00	0.00	22.3
9	75	-268	1807	56	0	150	973	4.02	4.02	4.02	4.02	2	0.15	0.05	0.32	0.00	0.00	22.3
10	75	-648	1573	-68	0	-60	1145	4.02	4.02	4.02	4.02	2	0.17	0.05	0.28	0.00	0.00	22.3
11	75	-512	1672	-68	0	-59	1083	4.02	4.02	4.02	4.02	2	0.16	0.05	0.29	0.00	0.00	22.3
12	75	-516	1604	120	0	259	1127	4.02	4.02	4.02	4.02	2	0.17	0.05	0.28	0.00	0.00	22.3
13	75	-380	1703	121	0	260	1073	4.02	4.02	4.02	4.02	2	0.16	0.05	0.30	0.00	0.00	22.3
14	75	-761	1469	-3	0	50	1242	4.02	4.02	4.02	4.02	2	0.18	0.04	0.26	0.00	0.00	22.3
15	75	-307	1798	-0	0	54	982	4.02	4.02	4.02	4.02	2	0.15	0.05	0.32	0.00	0.00	22.3
16	75	-721	1478	53	0	146	1235	4.02	4.02	4.02	4.02	2	0.18	0.04	0.26	0.00	0.00	22.3
17	75	-268	1807	56	0	150	973	4.02	4.02	4.02	4.02	2	0.15	0.05	0.32	0.00	0.00	22.3
18	75	-1191	2032	-194	0	-160	1841	4.02	4.02	4.02	4.02	3	0.26	0.06	0.35	0.00	0.00	22.3
19	75	-575	2289	372	0	766	1637	4.02	4.02	4.02	4.02	3	0.23	0.07	0.40	0.00	0.00	22.3
20	75	-1079	2187	90	0	304	1648	4.02	4.02	4.02	4.02	3	0.23	0.06	0.38	0.00	0.00	22.3
37	75	-1321	1891	-400	0	-525	1790	4.02	4.02	4.02	4.02	3	0.25	0.05	0.33	0.00	0.00	22.3
38	75	-296	2319	542	0	1019	1494	4.02	4.02	4.02	4.02	3	0.25	0.07	0.41	0.00	0.00	22.3
39	75	-1135	2150	73	0	249	1469	4.02	4.02	4.02	4.02	3	0.20	0.06	0.37	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	112	-668	1300	34	0	117	1436	4.02	4.02	4.02	4.02	3	0.20	0.04	0.23	0.00	0.00	22.3
2	112	-648	935	-68	0	-34	1145	4.02	4.02	4.02	4.02	2	0.17	0.03	0.16	0.00	0.00	22.3
3	112	-512	1034	-68	0	-33	1083	4.02	4.02	4.02	4.02	2	0.16	0.03	0.18	0.00	0.00	22.3
4	112	-516	966	120	0	214	1127	4.02	4.02	4.02	4.02	2	0.17	0.03	0.17	0.00	0.00	22.3
5	112	-380	1065	121	0	215	1073	4.02	4.02	4.02	4.02	2	0.16	0.03	0.19	0.00	0.00	22.3
6	112	-761	831	-3	0	52	1242	4.02	4.02	4.02	4.02	2	0.18	0.02	0.15	0.00	0.00	22.3
7	112	-307	1160	-0	0	54	1018	4.02	4.02	4.02	4.02	2	0.15	0.03	0.21	0.00	0.00	22.3
8	112	-721	840	53	0	126	1235	4.02	4.02	4.02	4.02	2	0.18	0.02	0.15	0.00	0.00	22.3
9	112	-268	1169	56	0	129	1015	4.02	4.02	4.02	4.02	2	0.15	0.03	0.21	0.00	0.00	22.3
10	112	-648	935	-68	0	-34	1145	4.02	4.02	4.02	4.02	2	0.17	0.03	0.16	0.00	0.00	22.3
11	112	-512	1034	-68	0	-33	1083	4.02	4.02	4.02	4.02	2	0.16	0.03	0.18	0.00	0.00	22.3
12	112	-516	966	120	0	214	1127	4.02	4.02	4.02	4.02	2	0.17	0.03	0.17	0.00	0.00	22.3
13	112	-380	1065	121	0	215	1073	4.02	4.02	4.02	4.02	2	0.16	0.03	0.19	0.00	0.00	22.3
14	112	-761	831	-3	0	52	1242	4.02	4.02	4.02	4.02	2	0.18	0.02	0.15	0.00	0.00	22.3
15	112	-307	1160	-0	0	54	1018	4.02	4.02	4.02	4.02	2	0.15	0.03	0.21	0.00	0.00	22.3
16	112	-721	840	53	0	126	1235	4.02	4.02	4.02	4.02	2	0.18	0.02	0.15	0.00	0.00	22.3
17	112	-268	1169	56	0	129	1015	4.02	4.02	4.02	4.02	2	0.15	0.03	0.21	0.00	0.00	22.3
18	112	-1191	1123	-194	0	-87	1841	4.02	4.02	4.02	4.02	3	0.26	0.03	0.19	0.00	0.00	22.3
19	112	-575	1380	372	0	627	1637	4.02	4.02	4.02	4.02	3	0.23	0.04	0.24	0.00	0.00	22.3
20	112	-1079	1278	90	0	271	1648	4.02	4.02	4.02	4.02	3	0.23	0.04	0.22	0.00	0.00	22.3
37	112	-1321	1022	-400	0	-375	1790	4.02	4.02	4.02	4.02	3	0.25	0.03	0.18	0.00	0.00	22.3
38	112	-296	1450	542	0	816	1494	4.02	4.02	4.02	4.02	3	0.21	0.04	0.26	0.00	0.00	22.3
39	112	-1135	1281	73	0	222	1469	4.02	4.02	4.02	4.02	3	0.20	0.04	0.22	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	150	-668	471	34	0	105	1436	4.02	4.02	4.02	4.02	3	0.20	0.01	0.08	0.00	0.00	22.3
2	150	-648	298	-68	0	-9	1145	4.02	4.02	4.02	4.02	2	0.17	0.01	0.05	0.00	0.00	22.3
3	150	-512	397	-68	0	-8	1083	4.02	4.02	4.02	4.02	2	0.16	0.01	0.07	0.00	0.00	22.3
4	150	-516	329	120	0	169	1127	4.02	4.02	4.02	4.02	2	0.17	0.01	0.06	0.00	0.00	22.3
5	150	-380	428	121	0	169	1073	4.02	4.02	4.02	4.02	2	0.16	0.01	0.08	0.00	0.00	22.3
6	150	-761	194	-3	0	53	1242	4.02	4.02	4.02	4.02	2	0.18	0.01	0.03	0.00	0.00	22.3
7	150	-307	523	-0	0	55	1018	4.02	4.02	4.02	4.02	2	0.15	0.02	0.09	0.00	0.00	22.3
8	150	-721	203	53	0	106	1235	4.02	4.02	4.02	4.02	2	0.18	0.01	0.04	0.00	0.00	22.3
9	150	-268	532	56	0	108	1015	4.02	4.02	4.02	4.02	2	0.15	0.02	0.09	0.00	0.00	22.3
10	150	-648	298	-68	0	-9	1145	4.02	4.02	4.02	4.02	2	0.17	0.01	0.05	0.00	0.00	22.3
11	150	-512	397	-68	0	-8	1083	4.02	4.02	4.02	4.02	2	0.16	0.01	0.07	0.00	0.00	22.3
12	150	-516	329	120	0	169	1127	4.02	4.02	4.02	4.02	2	0.17	0.01	0.06	0.00	0.00	22.3
13	150	-380	428	121	0	169	1073	4.02	4.02	4.02	4.02	2	0.16	0.01	0.08	0.00	0.00	22.3
14	150	-761	194	-3	0	53	1242	4.02	4.02	4.02	4.02	2	0.18	0.01	0.03	0.00	0.00	22.3
15	150	-307	523	-0	0	55	1018	4.02	4.02	4.02	4.02	2	0.15	0.02	0.09	0.00	0.00	22.3
16	150	-721	203	53	0	106	1235	4.02	4.02	4.02	4.02	2	0.18	0.01	0.04	0.00	0.00	22.3
17	150	-268	532	56	0	108	1015	4.02	4.02	4.02	4.02	2	0.15	0.02	0.09	0.00	0.00	22.3
18	150	-1191	214	-194	0	-15	1841	4.02	4.02	4.02	4.02	3	0.26	0.01	0.04	0.00	0.00	22.3
19	150	-575	471	372	0	488	1637	4.02	4.02	4.02	4.02	3	0.23	0.01	0.08	0.00	0.00	22.3
20	150	-1079	369	90	0	237	1648	4.02	4.02	4.02	4.02	3	0.23	0.01	0.06	0.00	0.00	22.3
37	150	-1321	153	-400	0	-225	1790	4.02	4.02	4.02	4.02	3	0.25	0.01	0.06	0.00	0.00	22.3
38	150	-296	581	542	0	612	1494	4.02	4.02	4.02	4.02	3	0.21	0.02	0.10	0.00	0.00	22.3
39	150	-1135	412	73	0	195	1469	4.02	4.02	4.02	4.02	3	0.20	0.01	0.07	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	188	-668	-358	34	0	92	1436	4.02	4.02	4.02	4.02	3	0.20	0.01	0.06	0.00	0.00	22.3
2	188	-648	-340	-68	0	17	1145	4.02	4.02	4.02	4.02	2	0.17	0.01	0.06	0.00	0.00	22.3
3	188	-512	-241	-68	0	17	1083	4.02	4.02	4.02	4.02	2	0.16	0.01	0.04	0.00	0.00	22.3
4	188	-516	-309	120	0	124	1127	4.02	4.02	4.02	4.02	2	0.17	0.01	0.05	0.00	0.00	22.3
5	188	-380	-210	121	0	124	1073	4.02	4.02	4.02	4.02	2	0.16	0.01	0.04	0.00	0.00	22.3
6	188	-761	-444	-3	0	54	1242	4.02	4.02	4.02	4.02	2	0.18	0.01	0.08	0.00	0.00	22.3
7	188	-307	-115	-0	0	55	1018	4.02	4.02	4.02	4.02	2	0.15	0.00	0.02	0.00	0.00	22.3
8	188	-721	-435	53	0	86	1235	4.02	4.02	4.02	4.02	2	0.18	0.01	0.08	0.00	0.00	22.3
9	188	-268	-106	56	0	87	1015	4.02	4.02	4.02	4.02	2	0.15	0.00	0.02	0.00	0.00	22.3
10	188	-648	-340	-68	0	17	1145	4.02	4.02	4.02	4.02	2	0.17	0.01	0.06	0.00	0.00	22.3
11	188	-512	-241	-68	0	17	1083	4.02	4.02	4.02	4.02	2	0.16	0.01	0.04	0.00	0.00	22.3
12	188	-516	-309	120	0	124	1127	4.02	4.02	4.02	4.02	2	0.17	0.01	0.05	0.00	0.00	22.3
13	188	-380	-210	121	0	124	1073	4.02	4.02	4.02	4.02	2	0.16	0.01	0.04	0.00	0.00	22.3
14	188	-761	-444	-3	0	54	1242	4.02	4.02	4.02	4.02	2	0.18	0.01	0.08	0.00	0.00	22.3
15	188	-307	-115	-0	0	55	1018	4.02	4.02	4.02	4.02	2	0.15	0.00	0.02	0.00	0.00	22.3
16	188	-721	-435	53	0	86	1235	4.02	4.02	4.02	4.02	2	0.18	0.01	0.08	0.00	0.00	22.3
17	188	-268	-106	56	0	87	1015	4.02	4.02	4.02	4.02	2	0.15	0.00	0.02	0.00	0.00	22.3
18	188	-1191	-696	-194	0	58	1841	4.02	4.02	4.02	4.02	3	0.26	0.02	0.12	0.00	0.00	22.3
19	188	-575	-438	372	0	348	1637	4.02	4.02	4.02	4.02	3	0.23	0.01	0.08	0.00	0.00	22.3
20	188	-1079	-540	90	0	203	1648	4.02	4.02	4.02	4.02	3	0.23	0.02	0.09	0.00	0.00	22.3
37	188	-1321	-716	-400	0	-75	1790	4.02	4.02	4.02	4.02	3	0.25	0.02	0.12	0.00	0.00	22.3
38	188	-296	-288	542	0	409	1494	4.02	4.02	4.02	4.02	3	0.21	0.02	0.09	0.00	0.00	22.3
39	188	-1135	-457	73	0	167	1469	4.02	4.02	4.02	4.02	3	0.20	0.01	0.08	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	225	-668	-1186	34	0	79	1436	4.02	4.02	4.02	4.02	3	0.20	0.03	0.21	0.00	0.00	22.3
2	225	-648	-978	-68	0	43	1145	4.02	4.02	4.02	4.02	2	0.17	0.03	0.17	0.00	0.00	22.3
3	225	-512	-879	-68	0	43	1083	4.02	4.02	4.02	4.02	2	0.16	0.03	0.15	0.00	0.00	22.3
4	225	-516	-947	120	0	79	1127	4.02	4.02	4.02	4.02	2	0.17	0.03	0.17	0.00	0.00	22.3
5	225	-380	-848	121	0	79	1073	4.02	4.02	4.02	4.02	2	0.16	0.02	0.15	0.00	0.00	22.3
6	225	-761	-1082	-3	0	56	1242	4.02	4.02	4.02	4.02	2	0.18	0.03	0.19	0.00	0.00	22.3
7	225	-307	-753	-0	0	55	1018	4.02	4.02	4.02	4.02	2	0.15	0.02	0.13	0.00	0.00	22.3
8	225	-721	-1073	53	0	66	1235	4.02	4.02	4.02	4.02	2	0.18	0.03	0.19	0.00	0.00	22.3
9	225	-268	-744	56	0	66	1015	4.02	4.02	4.02	4.02	2	0.15	0.02	0.13	0.00	0.00	22.3
10	225	-648	-978	-68	0	43	1145	4.02	4.02	4.02	4.02	2	0.17	0.03	0.17	0.00	0.00	22.3
11	225	-512	-879	-68	0	43	1083	4.02	4.02	4.02	4.02	2	0.16	0.03	0.15	0.00	0.00	22.3
12	225	-516	-947	120	0	79	1127	4.02	4.02	4.02	4.02	2	0.17	0.03	0.17	0.00	0.00	22.3
13	225	-380	-848	121	0	79	1073	4.02	4.02	4.02	4.02	2	0.16	0.02	0.15	0.00	0.00	22.3
14	225	-761	-1082	-3	0	56	1242	4.02	4.02	4.02	4.02	2	0.18	0.03	0.19	0.00	0.00	22.3
15	225	-307	-753	-0	0	55	1018	4.02	4.02	4.02	4.02	2	0.15	0.02	0.13	0.00	0.00	22.3
16	225	-721	-1073	53	0	66	1235	4.02	4.02	4.02	4.02	2	0.18	0.03	0.19	0.00	0.00	22.3
17	225	-268	-744	56	0	66	1015	4.02	4.02	4.02	4.02	2	0.15	0.02	0.13	0.00	0.00	22.3
18	225	-1191	-1605	-194	0	131	1841	4.02	4.02	4.02	4.02	3	0.26	0.05	0.28	0.00	0.00	22.3
19	225	-575	-1348	372	0	209	1637	4.02	4.02	4.02	4.02	3	0.23	0.04	0.24	0.00	0.00	22.3
20	225	-1079	-1449	90	0	169	1648	4.02	4.02	4.02	4.02	3	0.23	0.04	0.25	0.00	0.00	22.3
37	225	-1321	-1584	-400	0	75	1790	4.02	4.02	4.02	4.02	3	0.25	0.05	0.27	0.00	0.00	22.3
38	225	-296	-1156	542	0	205	1494	4.02	4.02	4.02	4.02	3	0.21	0.03	0.20	0.00	0.00	22.3
39	225	-1135	-1326	73	0	140	1469	4.02	4.02	4.02	4.02	3	0.20	0.04	0.23	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	262	-668	-2015	34	0	66	1436	4.02	4.02	4.02	4.02	3	0.20	0.06	0.35	0.00	0.00	22.3
2	262	-648	-1615	-68	0	68	1145	4.02	4.02	4.02	4.02	2	0.17	0.05	0.28	0.00	0.00	22.3
3	262	-512	-1516	-68	0	68	1083	4.02	4.02	4.02	4.02	2	0.16	0.04	0.27	0.00	0.00	22.3
4	262	-516	-1584	120	0	34	1127	4.02	4.02	4.02	4.02	2	0.17	0.05	0.28	0.00	0.00	22.3
5	262	-380	-1485	121	0	33	1073	4.02	4.02	4.02	4.02	2	0.16	0.04	0.26	0.00	0.00	22.3
6	262	-761	-1719	-3	0	57	1242	4.02	4.02	4.02	4.02	2	0.18	0.05	0.30	0.00	0.00	22.3
7	262	-307	-1390	-0	0	55	1018	4.02	4.02	4.02	4.02	2	0.15	0.04	0.25	0.00	0.00	22.3
8	262	-721	-1710	53	0	46	1235	4.02	4.02	4.02	4.02	2	0.18	0.05	0.30	0.00	0.00	22.3
9	262	-268	-1381	56	0	45	1015	4.02	4.02	4.02	4.02	2	0.15	0.04	0.24	0.00	0.00	22.3
10	262	-648	-1615	-68	0	68	1145	4.02	4.02	4.02	4.02	2	0.17	0.05	0.28	0.00	0.00	22.3
11	262	-512	-1516	-68	0	68	1083	4.02	4.02	4.02	4.02	2	0.16	0.04	0.27	0.00	0.00	22.3
12	262	-516	-1584	120	0	34	1127	4.02	4.02	4.02	4.02	2	0.17	0.05	0.28	0.00	0.00	22.3
13	262	-380	-1485	121	0	33	1073	4.02	4.02	4.02	4.02	2	0.16	0.04	0.26	0.00	0.00	22.3
14	262	-761	-1719	-3	0	57	1242	4.02	4.02	4.02	4.02	2	0.18	0.05	0.30	0.00	0.00	22.3
15	262	-307	-1390	-0	0	55	1018	4.02	4.02	4.02	4.02	2	0.15	0.04	0.25	0.00	0.00	22.3
16	262	-721	-1710	53	0	46	1235	4.02	4.02	4.02	4.02	2	0.18	0.05	0.30	0.00	0.00	22.3
17	262	-268	-1381	56	0	45	1015	4.02	4.02	4.02	4.02	2	0.15	0.04	0.24	0.00	0.00	22.3
18	262	-1191	-2514	-194	0	204	1820	4.02	4.02	4.02	4.02	3	0.25	0.07	0.44	0.00	0.00	22.3
19	262	-575	-2257	372	0	70	1637	4.02	4.02	4.02	4.02	3	0.23	0.07	0.40	0.00	0.00	22.3
20	262	-1079	-2358	90	0	136	1648	4.02	4.02	4.02	4.02	3	0.23	0.07	0.41	0.00	0.00	22.3
37	262	-1321	-2453	-400	0	225	1738	4.02	4.02	4.02	4.02	3	0.24	0.07	0.42	0.00	0.00	22.3
38	262	-296	-2025	542	0	2	1494	4.02	4.02	4.02	4.02	3	0.21	0.06	0.36	0.00	0.00	22.3
39	262	-1135	-2195	73	0	112	1469	4.02	4.02	4.02	4.02	3	0.20	0.06	0.38	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	300	-668	-2844	34	0	53	-1804	4.02	4.02	4.02	4.02	3	0.25	0.08	0.50	0.00	0.00	22.3
2	300	-648	-2253	-68	0	94	-1462	4.02	4.02	4.02	4.02	2	0.22	0.07	0.40	0.00	0.00	22.3
3	300	-512	-2154	-68	0	93	-1355	4.02	4.02	4.02	4.02	2	0.20	0.06	0.38	0.00	0.00	22.3
4	300	-516	-2222	120	0	-11	-1421	4.02	4.02	4.02	4.02	2	0.21	0.06	0.39	0.00	0.00	22.3
5	300	-380	-2123	121	0	-12	-1313	4.02	4.02	4.02	4.02	2	0.20	0.06	0.37	0.00	0.00	22.3
6	300	-761	-2357	-3	0	58	-1573	4.02	4.02	4.02	4.02	2	0.23	0.07	0.41	0.00	0.00	22.3
7	300	-307	-2028	-0	0	55	-1214	4.02	4.02	4.02	4.02	2	0.18	0.06	0.36	0.00	0.00	22.3
8	300	-721	-2348	53	0	26	-1562	4.02	4.02	4.02	4.02	2	0.23	0.07	0.41	0.00	0.00	22.3
9	300	-268	-2019	56	0	24	-1203	4.02	4.02	4.02	4.02	2	0.18	0.06	0.36	0.00	0.00	22.3
10	300	-648	-2253	-68	0	94	-1462	4.02	4.02	4.02	4.02	2	0.22	0.07	0.40	0.00	0.00	22.3
11	300	-512	-2154	-68	0	93	-1355	4.02	4.02	4.02	4.02	2	0.20	0.06	0.38	0.00	0.00	22.3
12	300	-516	-2222	120	0	-11	-1421	4.02	4.02	4.02	4.02	2	0.21	0.06	0.39	0.00	0.00	22.3
13	300	-380	-2123	121	0	-12	-1313	4.02	4.02	4.02	4.02	2	0.20	0.06	0.37	0.00	0.00	22.3
14	300	-761	-2357	-3	0	58	-1573	4.02	4.02	4.02	4.02	2	0.23	0.07	0.41	0.00	0.00	22.3
15	300	-307	-2028	-0	0	55	-1214	4.02	4.02	4.02	4.02	2	0.18	0.06	0.36	0.00	0.00	22.3
16	300	-721	-2348	53	0	26	-1562	4.02	4.02	4.02	4.02	2	0.23	0.07	0.41	0.00	0.00	22.3
17	300	-268	-2019	56	0	24	-1203	4.02	4.02	4.02	4.02	2	0.18	0.06	0.36	0.00	0.00	22.3
18	300	-1191	-3423	-194	0	276	-2298	4.02	4.02	4.02	4.02	3	0.32	0.10	0.59	0.00	0.00	22.3
19	300	-575	-3166	372	0	-70	-1994	4.02	4.02	4.02	4.02	3	0.28	0.09	0.56	0.00	0.00	22.3
20	300	-1079	-3267	90	0	102	-2180	4.02	4.02	4.02	4.02	3	0.30	0.09	0.57	0.00	0.00	22.3
37	300	-1321	-3322	-400	0	375	-2268	4.02	4.02	4.02	4.02	3	0.31	0.10	0.57	0.00	0.00	22.3
38	300	-296	-2894	542	0	-201	-1761	4.02	4.02	4.02	4.02	3	0.25	0.08	0.51	0.00	0.00	22.3
39	300	-1135	-3064	73	0	85	-2071	4.02	4.02	4.02	4.02	3	0.29	0.09	0.53	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	338	-668	-3673	34	0	40	-3119	4.02	4.02	4.02	4.02	3	0.44	0.11	0.64	0.00	0.00	22.3
2	338	-648	-2890	-68	0	120	-2489	4.02	4.02	4.02	4.02	2	0.37	0.08	0.51	0.00	0.00	22.3
3	338	-512	-2791	-68	0	119	-2358	4.02	4.02	4.02	4.02	2	0.35	0.08	0.49	0.00	0.00	22.3
4	338	-516	-2859	120	0	-57	-2441	4.02	4.02	4.02	4.02	2	0.36	0.08	0.50	0.00	0.00	22.3
5	338	-380	-2760	121	0	-58	-2309	4.02	4.02	4.02	4.02	2	0.35	0.08	0.49	0.00	0.00	22.3
6	338	-761	-2994	-3	0	59	-2626	4.02	4.02	4.02	4.02	2	0.39	0.09	0.52	0.00	0.00	22.3
7	338	-307	-2665	-0	0	55	-2187	4.02	4.02	4.02	4.02	2	0.33	0.08	0.47	0.00	0.00	22.3
8	338	-721	-2985	53	0	7	-2612	4.02	4.02	4.02	4.02	2	0.39	0.09	0.52	0.00	0.00	22.3
9	338	-268	-2656	56	0	3	-2173	4.02	4.02	4.02	4.02	2	0.33	0.08	0.47	0.00	0.00	22.3
10	338	-648	-2890	-68	0	120	-2489	4.02	4.02	4.02	4.02	2	0.37	0.08	0.51	0.00	0.00	22.3
11	338	-512	-2791	-68	0	119	-2358	4.02	4.02	4.02	4.02	2	0.35	0.08	0.49	0.00	0.00	22.3
12	338	-516	-2859	120	0	-57	-2441	4.02	4.02	4.02	4.02	2	0.36	0.08	0.50	0.00	0.00	22.3
13	338	-380	-2760	121	0	-58	-2309	4.02	4.02	4.02	4.02	2	0.35	0.08	0.49	0.00	0.00	22.3
14	338	-761	-2994	-3	0	59	-2626	4.02	4.02	4.02	4.02	2	0.39	0.09	0.52	0.00	0.00	22.3
15	338	-307	-2665	-0	0	55	-2187	4.02	4.02	4.02	4.02	2	0.33	0.08	0.47	0.00	0.00	22.3
16	338	-721	-2985	53	0	7	-2612	4.02	4.02	4.02	4.02	2	0.39	0.09	0.52	0.00	0.00	22.3
17	338	-268	-2656	56	0	3	-2173	4.02	4.02	4.02	4.02	2	0.33	0.08	0.47	0.00	0.00	22.3
18	338	-1191	-4332	-194	0	349	-3814	4.02	4.02	4.02	4.02	3	0.53	0.13	0.75	0.00	0.00	22.3
19	338	-575	-4075	372	0	-209	-3447	4.02	4.02	4.02	4.02	3	0.49	0.12	0.72	0.00	0.00	22.3
20	338	-1079	-4176	90	0	68	-3658	4.02	4.02	4.02	4.02	3	0.51	0.12	0.72	0.00	0.00	22.3
37	338	-1321	-4191	-400	0	525	-3730	4.02	4.02	4.02	4.02	3	0.51	0.12	0.72	0.00	0.00	22.3
38	338	-296	-3763	542	0	-405	-3118	4.02	4.02	4.02	4.02	3	0.44	0.11	0.67	0.00	0.00	22.3
39	338	-1135	-3933	73	0	57	-3470	4.02	4.02	4.02	4.02	3	0.48	0.11	0.68	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	375	-668	-4502	34	0	27	-3119	4.02	4.02	4.02	4.02	3	0.44	0.13	0.79	0.00	0.00	22.3
2	375	-648	-3528	-68	0	145	-2489	4.02	4.02	4.02	4.02	2	0.37	0.10	0.62	0.00	0.00	22.3
3	375	-512	-3429	-68	0	144	-2358	4.02	4.02	4.02	4.02	2	0.35	0.10	0.60	0.00	0.00	22.3
4	375	-516	-3497	120	0	-102	-2441	4.02	4.02	4.02	4.02	2	0.36	0.10	0.62	0.00	0.00	22.3
5	375	-380	-3398	121	0	-103	-2309	4.02	4.02	4.02	4.02	2	0.35	0.10	0.60	0.00	0.00	22.3

6	375	-761	-3632	-3	0	61	-2626	4.02	4.02	4.02	4.02	2	0.39	0.11	0.64	0.00	0.00	22.3
7	375	-307	-3303	-0	0	56	-2187	4.02	4.02	4.02	4.02	2	0.33	0.10	0.58	0.00	0.00	22.3
8	375	-721	-3623	53	0	-13	-2612	4.02	4.02	4.02	4.02	2	0.39	0.10	0.63	0.00	0.00	22.3
9	375	-268	-3294	56	0	-18	-2173	4.02	4.02	4.02	4.02	2	0.33	0.10	0.58	0.00	0.00	22.3
10	375	-648	-3528	-68	0	145	-2489	4.02	4.02	4.02	4.02	2	0.37	0.10	0.62	0.00	0.00	22.3
11	375	-512	-3429	-68	0	144	-2358	4.02	4.02	4.02	4.02	2	0.35	0.10	0.60	0.00	0.00	22.3
12	375	-516	-3497	120	0	-102	-2441	4.02	4.02	4.02	4.02	2	0.36	0.10	0.62	0.00	0.00	22.3
13	375	-380	-3398	121	0	-103	-2309	4.02	4.02	4.02	4.02	2	0.35	0.10	0.60	0.00	0.00	22.3
14	375	-761	-3632	-3	0	61	-2626	4.02	4.02	4.02	4.02	2	0.39	0.11	0.64	0.00	0.00	22.3
15	375	-307	-3303	-0	0	56	-2187	4.02	4.02	4.02	4.02	2	0.33	0.10	0.58	0.00	0.00	22.3
16	375	-721	-3623	53	0	-13	-2612	4.02	4.02	4.02	4.02	2	0.39	0.10	0.63	0.00	0.00	22.3
17	375	-268	-3294	56	0	-18	-2173	4.02	4.02	4.02	4.02	2	0.33	0.10	0.58	0.00	0.00	22.3
18	375	-1191	-5241	-194	0	422	-3814	4.02	4.02	4.02	4.02	3	0.53	0.15	0.91	0.00	0.00	22.3
19	375	-575	-4984	372	0	-348	-3447	4.02	4.02	4.02	4.02	3	0.49	0.14	0.88	0.00	0.00	22.3
20	375	-1079	-5085	90	0	34	-3658	4.02	4.02	4.02	4.02	3	0.51	0.15	0.88	0.00	0.00	22.3
37	375	-1321	-5060	-400	0	675	-3730	4.02	4.02	4.02	4.02	3	0.51	0.15	0.87	0.00	0.00	22.3
38	375	-296	-4632	542	0	-608	-3118	4.02	4.02	4.02	4.02	3	0.44	0.13	0.82	0.00	0.00	22.3
39	375	-1135	-4802	73	0	30	-3470	4.02	4.02	4.02	4.02	3	0.48	0.14	0.83	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

Nome travata: **trave_504_IP1** Descrizione: **Trave_5 11-10-9-8**
ASTA NUM. 12 NI 124 NF 214 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y Permanente Neve qy tot.
qy medio: 375.00 1325.25 142.50 1842.75 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-592	4491	15	0	27	-2961	4.02	4.02	4.02	4.02	3	0.42	0.13	0.79	0.00	0.00	22.3
2	0	-520	3425	-11	0	16	-2229	4.02	4.02	4.02	4.02	2	0.33	0.10	0.60	0.00	0.00	22.3
3	0	-475	3458	-11	0	15	-2281	4.02	4.02	4.02	4.02	2	0.34	0.10	0.61	0.00	0.00	22.3
4	0	-437	3451	35	0	27	-2274	4.02	4.02	4.02	4.02	2	0.34	0.10	0.61	0.00	0.00	22.3
5	0	-391	3484	35	0	26	-2326	4.02	4.02	4.02	4.02	2	0.35	0.10	0.61	0.00	0.00	22.3
6	0	-544	3395	5	0	21	-2185	4.02	4.02	4.02	4.02	2	0.33	0.10	0.60	0.00	0.00	22.3
7	0	-392	3506	5	0	18	-2357	4.02	4.02	4.02	4.02	2	0.35	0.10	0.62	0.00	0.00	22.3
8	0	-519	3403	19	0	24	-2198	4.02	4.02	4.02	4.02	2	0.33	0.10	0.60	0.00	0.00	22.3
9	0	-367	3513	18	0	21	-2371	4.02	4.02	4.02	4.02	2	0.36	0.10	0.62	0.00	0.00	22.3
10	0	-520	3425	-11	0	16	-2229	4.02	4.02	4.02	4.02	2	0.33	0.10	0.60	0.00	0.00	22.3
11	0	-475	3458	-11	0	15	-2281	4.02	4.02	4.02	4.02	2	0.34	0.10	0.61	0.00	0.00	22.3
12	0	-437	3451	35	0	27	-2274	4.02	4.02	4.02	4.02	2	0.34	0.10	0.61	0.00	0.00	22.3
13	0	-391	3484	35	0	26	-2326	4.02	4.02	4.02	4.02	2	0.35	0.10	0.61	0.00	0.00	22.3
14	0	-544	3395	5	0	21	-2185	4.02	4.02	4.02	4.02	2	0.33	0.10	0.60	0.00	0.00	22.3
15	0	-392	3506	5	0	18	-2357	4.02	4.02	4.02	4.02	2	0.35	0.10	0.62	0.00	0.00	22.3
16	0	-519	3403	19	0	24	-2198	4.02	4.02	4.02	4.02	2	0.33	0.10	0.60	0.00	0.00	22.3
17	0	-367	3513	18	0	21	-2371	4.02	4.02	4.02	4.02	2	0.36	0.10	0.62	0.00	0.00	22.3
18	0	-844	4827	-27	0	56	-3097	4.02	4.02	4.02	4.02	3	0.43	0.14	0.84	0.00	0.00	22.3
19	0	-521	4956	106	0	72	-3311	4.02	4.02	4.02	4.02	3	0.47	0.14	0.87	0.00	0.00	22.3
20	0	-763	4809	43	0	65	-3045	4.02	4.02	4.02	4.02	3	0.43	0.14	0.84	0.00	0.00	22.3
37	0	-914	4577	-79	0	39	-2897	4.02	4.02	4.02	4.02	3	0.40	0.13	0.80	0.00	0.00	22.3
38	0	-375	4792	143	0	66	-3253	4.02	4.02	4.02	4.02	3	0.46	0.14	0.85	0.00	0.00	22.3
39	0	-779	4546	37	0	54	-2810	4.02	4.02	4.02	4.02	3	0.39	0.13	0.79	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	38	-592	3662	15	0	22	-2961	4.02	4.02	4.02	4.02	3	0.42	0.11	0.64	0.00	0.00	22.3
2	38	-520	2787	-11	0	20	-2229	4.02	4.02	4.02	4.02	2	0.33	0.08	0.49	0.00	0.00	22.3
3	38	-475	2820	-11	0	20	-2281	4.02	4.02	4.02	4.02	2	0.34	0.08	0.50	0.00	0.00	22.3
4	38	-437	2813	35	0	14	-2274	4.02	4.02	4.02	4.02	2	0.34	0.08	0.50	0.00	0.00	22.3
5	38	-391	2846	35	0	13	-2326	4.02	4.02	4.02	4.02	2	0.35	0.08	0.50	0.00	0.00	22.3
6	38	-544	2757	5	0	19	-2185	4.02	4.02	4.02	4.02	2	0.33	0.08	0.48	0.00	0.00	22.3
7	38	-392	2868	5	0	16	-2357	4.02	4.02	4.02	4.02	2	0.35	0.08	0.51	0.00	0.00	22.3
8	38	-519	2765	19	0	17	-2198	4.02	4.02	4.02	4.02	2	0.33	0.08	0.49	0.00	0.00	22.3
9	38	-367	2875	18	0	15	-2371	4.02	4.02	4.02	4.02	2	0.36	0.08	0.51	0.00	0.00	22.3
10	38	-520	2787	-11	0	20	-2229	4.02	4.02	4.02	4.02	2	0.33	0.08	0.49	0.00	0.00	22.3
11	38	-475	2820	-11	0	20	-2281	4.02	4.02	4.02	4.02	2	0.34	0.08	0.50	0.00	0.00	22.3
12	38	-437	2813	35	0	14	-2274	4.02	4.02	4.02	4.02	2	0.34	0.08	0.50	0.00	0.00	22.3
13	38	-391	2846	35	0	13	-2326	4.02	4.02	4.02	4.02	2	0.35	0.08	0.50	0.00	0.00	22.3
14	38	-544	2757	5	0	19	-2185	4.02	4.02	4.02	4.02	2	0.33	0.08	0.48	0.00	0.00	22.3
15	38	-392	2868	5	0	16	-2357	4.02	4.02	4.02	4.02	2	0.35	0.08	0.51	0.00	0.00	22.3
16	38	-519	2765	19	0	17	-2198	4.02	4.02	4.02	4.02	2	0.33	0.08	0.49	0.00	0.00	22.3
17	38	-367	2875	18	0	15	-2371	4.02	4.02	4.02	4.02	2	0.36	0.08	0.51	0.00	0.00	22.3
18	38	-844	3918	-27	0	66	-3097	4.02	4.02	4.02	4.02	3	0.43	0.11	0.68	0.00	0.00	22.3
19	38	-521	4047	106	0	32	-3311	4.02	4.02	4.02	4.02	3	0.47	0.12	0.71	0.00	0.00	22.3
20	38	-763	3900	43	0	49	-3045	4.02	4.02	4.02	4.02	3	0.43	0.11	0.68	0.00	0.00	22.3
37	38	-914	3708	-79	0	69	-2897	4.02	4.02	4.02	4.02	3	0.40	0.11	0.65	0.00	0.00	22.3
38	38	-375	3923	143	0	12	-3253	4.02	4.02	4.02	4.02	3	0.46	0.11	0.69	0.00	0.00	22.3
39	38	-779	3677	37	0	40	-2810	4.02	4.02	4.02	4.02	3	0.39	0.11	0.64	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	75	-592	2833	15	0	16	-1649	4.02	4.02	4.02	4.02	3	0.23	0.08	0.50	0.00	0.00	22.3
2	75	-520	2150	-11	0	24	-1227	4.02	4.02	4.02	4.02	2	0.18	0.06	0.38	0.00	0.00	22.3
3	75	-475	2183	-11	0	24	-1271	4.02	4.02	4.02	4.02	2	0.19	0.06	0.38	0.00	0.00	22.3
4	75	-437	2176	35	0	1	-1266	4.02	4.02	4.02	4.02	2	0.19	0.06	0.38	0.00	0.00	22.3
5	75	-391	2209	35	0	0	-1310	4.02	4.02	4.02	4.02	2	0.20	0.06	0.39	0.00	0.00	22.3
6	75	-544	2120	5	0	17	-1190	4.02	4.02	4.02	4.02	2	0.18	0.06	0.37	0.00	0.00	22.3
7	75	-392	2231	5	0	15	-1335	4.02	4.02	4.02	4.02	2	0.20	0.06	0.39	0.00	0.00	22.3
8	75	-519	2128	19	0	10	-1201	4.02	4.02	4.02	4.02	2	0.18	0.06	0.37	0.00	0.00	22.3
9	75	-367	2238	18	0	8	-1347	4.02	4.02	4.02	4.02	2	0.20	0.06	0.40	0.00	0.00	22.3
10	75	-520	2150	-11	0	24	-1227	4.02	4.02	4.02	4.02	2	0.18	0.06	0.38	0.00	0.00	22.3
11	75	-475	2183	-11	0	24	-1271	4.02	4.02	4.02	4.02	2	0.19	0.06	0.38	0.00	0.00	22.3
12	75	-437	2176	35	0	1	-1266	4.02	4.02	4.02	4.02	2	0.19	0.06	0.38	0.00	0.00	22.3
13	75	-391	2209	35	0	0	-1310	4.02	4.02	4.02	4.02	2	0.20	0.06	0.39	0.00	0.00	22.3
14	75	-544	2120	5	0	17	-1190	4.02	4.02	4.02	4.02	2	0.18	0.06	0.37	0.00	0.00	22.3
15	75	-392	2231	5	0	15	-1335	4.02	4.02	4.02	4.02	2	0.20	0.06	0.39	0.00	0.00	22.3
16	75	-519	2128	19	0	10	-1201	4.02	4.02	4.02	4.02	2	0.18	0.06	0.37	0.00	0.00	22.3
17	75	-367	2238	18	0	8	-1347	4.02	4.02	4.02	4.02	2	0.20	0.06	0.40	0.00	0.00	22.3
18	75	-844	3009	-27	0	76	-1682	4.02	4.02	4.02	4.02	3	0.24	0.09	0.53	0.00	0.00	22.3
19	75	-521	3138	106	0	-7	-1865	4.02	4.02	4.02	4.02	3	0.26	0.09	0.55	0.00	0.00	22.3
20	75	-763	2991	43	0	33	-1634	4.02	4.02	4.02	4.02	3	0.23	0.09	0.52	0.00	0.00	22.3
37	75	-914	2839	-79	0	98	-1553	4.02	4.02	4.02	4.02	3	0.22	0.08	0.49	0.00	0.00	22.3
38	75	-375	3054	143	0	-41	-1857	4.02	4.02	4.02	4.02	3	0.26	0.09	0.54	0.00	0.00	22.3
39	75	-779	2808	37	0	25	-1474	4.02	4.02	4.02	4.02	3	0.21	0.08	0.49	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	112	-592	2004	15	0	10	1573	4.02	4.02	4.02	4.02	3	0.22	0.06	0.35	0.00	0.00	22.3
2	112	-520	1512	-11	0	29	1204	4.02	4.02	4.02	4.02	2	0.18	0.04	0.27	0.00	0.00	22.3
3	112	-475	1545	-11	0	28	1214	4.02	4.02	4.02	4.02	2	0.18	0.04	0.27	0.00	0.00	22.3
4	112	-437	1538	35	0	-12	1207	4.02	4.02	4.02	4.02	2	0.18	0.04	0.27	0.00	0.00	22.3
5	112	-391	1571	35	0	-13	1217	4.02	4.02	4.02	4.02	2	0.18	0.05	0.28	0.00	0.00	22.3
6	112	-544	1482	5	0	15	1192	4.02	4.02	4.02	4.02	2	0.18	0.04	0.26	0.00	0.00	22.3
7	112	-392	1593	5	0	13	1227	4.02	4.02	4.02	4.02	2	0.18	0.05	0.28	0.00	0.00	22.3
8	112	-519	1490	19	0	3	1194	4.02	4.02	4.02	4.02	2	0.18	0.04	0.26	0.00	0.00	22.3
9	112	-367	1600	18	0	1	1231	4.02	4.02	4.02	4.02	2	0.18	0.05	0.28	0.00	0.00	22.3
10	112	-520	1512	-11	0	29	1204	4.02	4.02	4.02	4.02	2	0.18	0.04	0.27	0.00	0.00	22.3
11	112	-475	1545	-11	0	28	1214	4.02	4.02	4.02	4.02	2	0.18	0.04	0.27	0.00	0.00	22.3
12	112	-437	1538	35	0	-12	1207	4.02	4.02	4.02	4.02	2	0.18	0.04	0.27	0.00	0.00	22.3
13	112	-391	1571	35	0	-13	1217	4.02	4.02	4.02	4.02	2	0.18	0.05	0.28	0.00	0.00	22.3
14	112	-544	1482	5	0	15	1192	4.02	4.02	4.02	4.02	2	0.18	0.04	0.26	0.00	0.00	22.3
15	112	-392	1593	5	0	13	1227	4.02	4.02	4.02	4.02	2	0.18	0.05	0.28	0.00	0.00	22.3
16	112	-519	1490	19	0	3	1194	4.02	4.02	4.02	4.02	2	0.18	0.04	0.26	0.00	0.00	22.3
17	112	-367	1600	18	0	1	1231	4.02	4.02	4.02	4.02	2	0.18	0.05	0.28	0.00	0.00	22.3
18	112	-844	2100	-27	0	86	1693	4.02	4.02	4.02	4.02	3	0.24	0.06	0.37	0.00	0.00	22.3
19	112	-521	2229	106	0	-47	1720	4.02	4.02	4.02	4.02	3	0.24	0.06	0.39	0.00	0.00	22.3
20	112	-763	2082	43	0	17	1710	4.02	4.02	4.02	4.02	3	0.24	0.06	0.36	0.00	0.00	22.3
37	112	-914	1970	-79	0	128	1612	4.02	4.02	4.02	4.02	3	0.23	0.06	0.34	0.00	0.00	22.3
38	112	-375	2185	143	0	-95	1663	4.02	4.02	4.02	4.02	3	0.24	0.06	0.39	0.00	0.00	22.3
39	112	-779	1939	37	0	11	1641	4.02	4.02	4.02	4.02	3	0.23	0.06	0.34	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	150	-592	1175	15	0	4	1573	4.02	4.02	4.02	4.02	3	0.22	0.03	0.21	0.00	0.00	22.3
2	150	-520	875	-11	0	33	1204	4.02	4.02	4.02	4.02	2	0.18	0.03	0.15	0.00	0.00	22.3
3	150	-475	908	-11	0	32	1214	4.02	4.02	4.02	4.02	2	0.18	0.03	0.16	0.00	0.00	22.3
4	150	-437	901	35	0	-25	1207	4.02	4.02	4.02	4.02	2	0.18	0.03	0.16	0.00	0.00	22.3
5	150	-391	934	35	0	-26	1217	4.02	4.02	4.02	4.02	2	0.18	0.03	0.16	0.00	0.00	22.3
6	150	-544	845	5	0	13	1192	4.02	4.02	4.02	4.02	2	0.18	0.02	0.15	0.00	0.00	22.3
7	150	-392	956	5	0	11	1227	4.02	4.02	4.02	4.02	2	0.18	0.03	0.17	0.00	0.00	22.3
8	150	-519	853	19	0	-4	1194	4.02	4.02	4.02	4.02	2	0.18	0.02	0.15	0.00	0.00	22.3
9	150	-367	963	18	0	-6	1231	4.02	4.02	4.02	4.02	2	0.18	0.03	0.17	0.00	0.00	22.3
10	150	-520	875	-11	0	33	1204	4.02	4.02	4.02	4.02	2	0.18	0.03	0.15	0.00	0.00	22.3
11	150	-475	908	-11	0	32	1214	4.02	4.02	4.02	4.02	2	0.18	0.03	0.16	0.00	0.00	22.3
12	150	-437	901	35	0	-25	1207	4.02	4.02	4.02	4.02	2	0.18	0.03	0.16	0.00	0.00	22.3
13	150	-391	934	35	0	-26	1217	4.02	4.02	4.02	4.02	2	0.18	0.03	0.16	0.00	0.00	22.3
14	150	-544	845	5	0	13	1192	4.02	4.02	4.02	4.02	2	0.18	0.02	0.15	0.00	0.00	22.3
15	150	-392	956	5	0	11	1227	4.02	4.02	4.02	4.02	2	0.18	0.03	0.17	0.00	0.00	22.3
16	150	-519	853	19	0	-4	1194	4.02	4.02	4.02	4.02	2	0.18	0.02	0.15	0.00	0.00	22.3
17	150	-367	963	18	0	-6	1231	4.02	4.02	4.02	4.02	2	0.18	0.03	0.17	0.00	0.00	22.3
18	150	-844	1191	-27	0	96	1693	4.02	4.02	4.02	4.02	3	0.24	0.03	0.21	0.00	0.00	22.3
19	150	-521	1320	106	0	-87	1720	4.02	4.02	4.02	4.02	3	0.24	0.04	0.23	0.00	0.00	22.3
20	150	-763	1173	43	0	0	1710	4.02	4.02	4.02	4.02	3	0.24	0.03	0.21	0.00	0.00	22.3
37	150	-914	1101	-79	0	157	1612	4.02	4.02	4.02	4.02	3	0.23	0.03	0.19	0.00	0.00	22.3
38	150	-375	1316	143	0	-148	1663	4.02	4.02	4.02	4.02	3	0.24	0.04	0.23	0.00	0.00	22.3
39	150	-779	1070	37	0	-3	1641	4.02	4.02	4.02	4.02	3	0.23	0.03	0.19	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	188	-592	346	15	0	-1	1573	4.02	4.02	4.02	4.02	3	0.22	0.01	0.06	0.00	0.00	22.3
2	188	-520	237	-11	0	37	1204	4.02	4.02	4.02	4.02	2	0.18	0.01	0.04	0.00	0.00	22.3
3	188	-475	270	-11	0	36	1214	4.02	4.02	4.02	4.02	2	0.18	0.01	0.05	0.00	0.00	22.3
4	188	-437	263	35	0	-38	1207	4.02	4.02	4.02	4.02	2	0.18	0.01	0.05	0.00	0.00	22.3
5	188	-391	296	35	0	-39	1217	4.02	4.02	4.02	4.02	2	0.18	0.01	0.05	0.00	0.00	22.3
6	188	-544	207	5	0	11	1192	4.02	4.02	4.02	4.02	2	0.18	0.01	0.04	0.00	0.00	22.3
7	188	-392	318	5	0	10	1227	4.02	4.02	4.02	4.02	2	0.18	0.01	0.06	0.00	0.00	22.3
8	188	-519	215	19	0	-12	1194	4.02	4.02	4.02	4.02	2	0.18	0.01	0.04	0.00	0.00	22.3
9	188	-367	325	18	0	-13	1231	4.02	4.02	4.02	4.02	2	0.18	0.01	0.06	0.00	0.00	22.3
10	188	-520	237	-11	0	37	1204	4.02	4.02	4.02	4.02	2	0.18	0.01	0.04	0.00	0.00	22.3
11	188	-475	270	-11	0	36	1214	4.02	4.02	4.02	4.02	2	0.18	0.01	0.05	0.00	0.00	22.3
12	188	-437	263	35	0	-38	1207	4.02	4.02	4.02	4.02	2	0.18	0.01	0.05	0.00	0.00	22.3
13	188	-391	296	35	0	-39	1217	4.02	4.02	4.02	4.02	2	0.18	0.01	0.05	0.00	0.00	22.3
14	188	-544	207	5	0	11	1192	4.02	4.02	4.02	4.02	2	0.18	0.01	0.04	0.00	0.00	22.3
15	188	-392	318	5	0	10	1227	4.02	4.02	4.02	4.02	2	0.18	0.01	0.06	0.00	0.00	22.3
16	188	-519	215	19	0	-12	1194	4.02	4.02	4.02	4.02	2	0.18	0.01	0.04	0.00	0.00	22.3
17	188	-367	325	18	0	-13	1231	4.02	4.02	4.02	4.02	2	0.18	0.01	0.06	0.00	0.00	22.3
18	188	-844	282	-27	0	106	1693	4.02	4.02	4.02	4.02	3	0.24	0.01	0.05	0.00	0.00	22.3
19	188	-521	411	106	0	-127	1720	4.02	4.02	4.02	4.02	3	0.24	0.01	0.07	0.00	0.00	22.3
20	188	-763	264	43	0	-16	1710	4.02	4.02	4.02	4.02	3	0.24	0.01	0.05	0.00	0.00	22.3
37	188	-914	232	-79	0	187	1612	4.02	4.02	4.02	4.02	3	0.23	0.01	0.04	0.00	0.00	22.3
38	188	-375	447	143	0	-202	1663	4.02	4.02	4.02	4.02	3	0.24	0.01	0.08	0.00	0.00	22.3
39	188	-779	202	37	0	-17	1641	4.02	4.02	4.02	4.02	3	0.23	0.01	0.04	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	225	-592	-482	15	0	-7	1573	4.02	4.02	4.02	4.02	3	0.22	0.01	0.08	0.00	0.00	22.3
2	225	-520	-401	-11	0	41	1204	4.02	4.02	4.02	4.02	2	0.18	0.01	0.07	0.00	0.00	22.3
3	225	-475	-368	-11	0	41	1214	4.02	4.02	4.02	4.02	2	0.18	0.01	0.06	0.00	0.00	22.3
4	225	-437	-375	35	0	-51	1207	4.02	4.02	4.02	4.02	2	0.18	0.01	0.07	0.00	0.00	22.3
5	225	-391	-342	35	0	-52	1217	4.02	4.02	4.02	4.02	2	0.18	0.01	0.06	0.00	0.00	22.3
6	225	-544	-431	5	0	9	1192	4.02	4.02	4.02	4.02	2	0.18	0.01	0.08	0.00	0.00	22.3
7	225	-392	-320	5	0	8	1227	4.02	4.02	4.02	4.02	2	0.18	0.01	0.06	0.00	0.00	22.3
8	225	-519	-423	19	0	-19	1194	4.02	4.02	4.02	4.02	2	0.18	0.01	0.07	0.00	0.00	22.3
9	225	-367	-313	18	0	-20	1231	4.02	4.02	4.02	4.02	2	0.18	0.01	0.06	0.00	0.00	22.3
10	225	-520	-401	-11	0	41	1204	4.02	4.02	4.02	4.02	2	0.18	0.01	0.07	0.00	0.00	22.3
11	225	-475	-368	-11	0	41	1214	4.02	4.02	4.02	4.02	2	0.18	0.01	0.06	0.00	0.00	22.3
12	225	-437	-375	35	0	-51	1207	4.02	4.02	4.02	4.02	2	0.18	0.01	0.07	0.00	0.00	22.3
13	225	-391	-342	35	0	-52	1217	4.02	4.02	4.02	4.02	2	0.18	0.01	0.06	0.00	0.00	22.3
14	225	-544	-431	5	0	9	1192	4.02	4.02	4.02	4.02	2	0.18	0.01	0.08	0.00	0.00	22.3
15	225	-392	-320	5	0	8	1227	4.02	4.02	4.02	4.02	2	0.18	0.01	0.06	0.00	0.00	22.3
16	225	-519	-423	19	0	-19	1194	4.02	4.02	4.02	4.02	2	0.18	0.01	0.07	0.00	0.00	22.3
17	225	-367	-313	18	0	-20	1231	4.02	4.02	4.02	4.02	2	0.18	0.01	0.06	0.00	0.00	22.3
18	225	-844	-627	-27	0	116	1693	4.02	4.02	4.02	4.02	3	0.24	0.02	0.11	0.00	0.00	22.3
19	225	-521	-498	106	0	-167	1720	4.02	4.02	4.02	4.02	3	0.24	0.01	0.09	0.00	0.00	22.3
20	225	-763	-646	43	0	-32	1710	4.02	4.02	4.02	4.02	3	0.24	0.02	0.11	0.00	0.00	22.3
37	225	-914	-636	-79	0	216	1612	4.02	4.02	4.02	4.02	3	0.23	0.02	0.11	0.00	0.00	22.3
38	225	-375	-422	143	0	-255	1663	4.02	4.02	4.02	4.02	3	0.24	0.01	0.07	0.00	0.00	22.3
39	225	-779	-667	37	0	-31	1641	4.02	4.02	4.02	4.02	3	0.23	0.02	0.12	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	262	-592	-1311	15	0	-13	1573	4.02	4.02	4.02	4.02	3	0.22	0.04	0.23	0.00	0.00	22.3
2	262	-520	-1038	-11	0	45	1204	4.02	4.02	4.02	4.02	2	0.18	0.03	0.18	0.00	0.00	22.3
3	262	-475	-1005	-11	0	45	1214	4.02	4.02	4.02	4.02	2	0.18	0.03	0.18	0.00	0.00	22.3

4	262	-437	-1012	35	0	-64	1207	4.02	4.02	4.02	4.02	2	0.18	0.03	0.18	0.00	0.00	22.3
5	262	-391	-979	35	0	-65	1217	4.02	4.02	4.02	4.02	2	0.18	0.03	0.17	0.00	0.00	22.3
6	262	-544	-1068	5	0	7	1192	4.02	4.02	4.02	4.02	2	0.18	0.03	0.19	0.00	0.00	22.3
7	262	-392	-957	5	0	6	1227	4.02	4.02	4.02	4.02	2	0.18	0.03	0.17	0.00	0.00	22.3
8	262	-519	-1060	19	0	-26	1194	4.02	4.02	4.02	4.02	2	0.18	0.03	0.19	0.00	0.00	22.3
9	262	-367	-950	18	0	-27	1231	4.02	4.02	4.02	4.02	2	0.18	0.03	0.17	0.00	0.00	22.3
10	262	-520	-1038	-11	0	45	1204	4.02	4.02	4.02	4.02	2	0.18	0.03	0.18	0.00	0.00	22.3
11	262	-475	-1005	-11	0	45	1214	4.02	4.02	4.02	4.02	2	0.18	0.03	0.18	0.00	0.00	22.3
12	262	-437	-1012	35	0	-64	1207	4.02	4.02	4.02	4.02	2	0.18	0.03	0.18	0.00	0.00	22.3
13	262	-391	-979	35	0	-65	1217	4.02	4.02	4.02	4.02	2	0.18	0.03	0.17	0.00	0.00	22.3
14	262	-544	-1068	5	0	7	1192	4.02	4.02	4.02	4.02	2	0.18	0.03	0.19	0.00	0.00	22.3
15	262	-392	-957	5	0	6	1227	4.02	4.02	4.02	4.02	2	0.18	0.03	0.17	0.00	0.00	22.3
16	262	-519	-1060	19	0	-26	1194	4.02	4.02	4.02	4.02	2	0.18	0.03	0.19	0.00	0.00	22.3
17	262	-367	-950	18	0	-27	1231	4.02	4.02	4.02	4.02	2	0.18	0.03	0.17	0.00	0.00	22.3
18	262	-844	-1536	-27	0	126	1693	4.02	4.02	4.02	4.02	3	0.24	0.04	0.27	0.00	0.00	22.3
19	262	-521	-1407	106	0	-206	1720	4.02	4.02	4.02	4.02	3	0.24	0.04	0.25	0.00	0.00	22.3
20	262	-763	-1555	43	0	-48	1710	4.02	4.02	4.02	4.02	3	0.24	0.04	0.27	0.00	0.00	22.3
37	262	-914	-1505	-79	0	246	1612	4.02	4.02	4.02	4.02	3	0.23	0.04	0.26	0.00	0.00	22.3
38	262	-375	-1291	143	0	-309	1663	4.02	4.02	4.02	4.02	3	0.24	0.04	0.23	0.00	0.00	22.3
39	262	-779	-1536	37	0	-45	1641	4.02	4.02	4.02	4.02	3	0.23	0.04	0.27	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	300	-592	-2140	15	0	-18	1573	4.02	4.02	4.02	4.02	3	0.22	0.06	0.38	0.00	0.00	22.3
2	300	-520	-1676	-11	0	49	1204	4.02	4.02	4.02	4.02	2	0.18	0.05	0.29	0.00	0.00	22.3
3	300	-475	-1643	-11	0	49	1214	4.02	4.02	4.02	4.02	2	0.18	0.05	0.29	0.00	0.00	22.3
4	300	-437	-1650	35	0	-77	1207	4.02	4.02	4.02	4.02	2	0.18	0.05	0.29	0.00	0.00	22.3
5	300	-391	-1617	35	0	-78	1217	4.02	4.02	4.02	4.02	2	0.18	0.05	0.29	0.00	0.00	22.3
6	300	-544	-1706	5	0	5	1192	4.02	4.02	4.02	4.02	2	0.18	0.05	0.30	0.00	0.00	22.3
7	300	-392	-1595	5	0	5	1227	4.02	4.02	4.02	4.02	2	0.18	0.05	0.28	0.00	0.00	22.3
8	300	-519	-1698	19	0	-33	1194	4.02	4.02	4.02	4.02	2	0.18	0.05	0.30	0.00	0.00	22.3
9	300	-367	-1588	18	0	-33	1231	4.02	4.02	4.02	4.02	2	0.18	0.05	0.28	0.00	0.00	22.3
10	300	-520	-1676	-11	0	49	1204	4.02	4.02	4.02	4.02	2	0.18	0.05	0.29	0.00	0.00	22.3
11	300	-475	-1643	-11	0	49	1214	4.02	4.02	4.02	4.02	2	0.18	0.05	0.29	0.00	0.00	22.3
12	300	-437	-1650	35	0	-77	1207	4.02	4.02	4.02	4.02	2	0.18	0.05	0.29	0.00	0.00	22.3
13	300	-391	-1617	35	0	-78	1217	4.02	4.02	4.02	4.02	2	0.18	0.05	0.29	0.00	0.00	22.3
14	300	-544	-1706	5	0	5	1192	4.02	4.02	4.02	4.02	2	0.18	0.05	0.30	0.00	0.00	22.3
15	300	-392	-1595	5	0	5	1227	4.02	4.02	4.02	4.02	2	0.18	0.05	0.28	0.00	0.00	22.3
16	300	-519	-1698	19	0	-33	1194	4.02	4.02	4.02	4.02	2	0.18	0.05	0.30	0.00	0.00	22.3
17	300	-367	-1588	18	0	-33	1231	4.02	4.02	4.02	4.02	2	0.18	0.05	0.28	0.00	0.00	22.3
18	300	-844	-2445	-27	0	136	1693	4.02	4.02	4.02	4.02	3	0.24	0.07	0.43	0.00	0.00	22.3
19	300	-521	-2316	106	0	-246	1720	4.02	4.02	4.02	4.02	3	0.24	0.07	0.41	0.00	0.00	22.3
20	300	-763	-2464	43	0	-64	1710	4.02	4.02	4.02	4.02	3	0.24	0.07	0.43	0.00	0.00	22.3
37	300	-914	-2374	-79	0	275	1609	4.02	4.02	4.02	4.02	3	0.22	0.07	0.41	0.00	0.00	22.3
38	300	-375	-2160	143	0	-362	1663	4.02	4.02	4.02	4.02	3	0.24	0.06	0.38	0.00	0.00	22.3
39	300	-779	-2405	37	0	-59	1619	4.02	4.02	4.02	4.02	3	0.23	0.07	0.42	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	338	-592	-2969	15	0	-24	-1663	4.02	4.02	4.02	4.02	3	0.23	0.09	0.52	0.00	0.00	22.3
2	338	-520	-2313	-11	0	54	-1341	4.02	4.02	4.02	4.02	2	0.20	0.07	0.41	0.00	0.00	22.3
3	338	-475	-2280	-11	0	53	-1269	4.02	4.02	4.02	4.02	2	0.19	0.07	0.40	0.00	0.00	22.3
4	338	-437	-2287	35	0	-90	-1289	4.02	4.02	4.02	4.02	2	0.19	0.07	0.40	0.00	0.00	22.3
5	338	-391	-2254	35	0	-91	-1217	4.02	4.02	4.02	4.02	2	0.18	0.07	0.40	0.00	0.00	22.3
6	338	-544	-2343	5	0	3	-1408	4.02	4.02	4.02	4.02	2	0.21	0.07	0.41	0.00	0.00	22.3
7	338	-392	-2232	5	0	3	-1166	4.02	4.02	4.02	4.02	2	0.17	0.06	0.39	0.00	0.00	22.3
8	338	-519	-2335	19	0	-40	-1392	4.02	4.02	4.02	4.02	2	0.21	0.07	0.41	0.00	0.00	22.3
9	338	-367	-2225	18	0	-40	-1150	4.02	4.02	4.02	4.02	2	0.17	0.06	0.39	0.00	0.00	22.3
10	338	-520	-2313	-11	0	54	-1341	4.02	4.02	4.02	4.02	2	0.20	0.07	0.41	0.00	0.00	22.3
11	338	-475	-2280	-11	0	53	-1269	4.02	4.02	4.02	4.02	2	0.19	0.07	0.40	0.00	0.00	22.3
12	338	-437	-2287	35	0	-90	-1289	4.02	4.02	4.02	4.02	2	0.19	0.07	0.40	0.00	0.00	22.3
13	338	-391	-2254	35	0	-91	-1217	4.02	4.02	4.02	4.02	2	0.18	0.07	0.40	0.00	0.00	22.3
14	338	-544	-2343	5	0	3	-1408	4.02	4.02	4.02	4.02	2	0.21	0.07	0.41	0.00	0.00	22.3
15	338	-392	-2232	5	0	3	-1166	4.02	4.02	4.02	4.02	2	0.17	0.06	0.39	0.00	0.00	22.3
16	338	-519	-2335	19	0	-40	-1392	4.02	4.02	4.02	4.02	2	0.21	0.07	0.41	0.00	0.00	22.3
17	338	-367	-2225	18	0	-40	-1150	4.02	4.02	4.02	4.02	2	0.17	0.06	0.39	0.00	0.00	22.3
18	338	-844	-3354	-27	0	146	-2040	4.02	4.02	4.02	4.02	3	0.29	0.10	0.59	0.00	0.00	22.3
19	338	-521	-3225	106	0	-286	-1771	4.02	4.02	4.02	4.02	3	0.25	0.09	0.57	0.00	0.00	22.3
20	338	-763	-3373	43	0	-80	-2057	4.02	4.02	4.02	4.02	3	0.29	0.10	0.59	0.00	0.00	22.3
37	338	-914	-3243	-79	0	305	-2025	4.02	4.02	4.02	4.02	3	0.28	0.09	0.57	0.00	0.00	22.3
38	338	-375	-3029	143	0	-416	-1576	4.02	4.02	4.02	4.02	3	0.22	0.09	0.53	0.00	0.00	22.3
39	338	-779	-3274	37	0	-73	-2054	4.02	4.02	4.02	4.02	3	0.29	0.09	0.57	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	375	-592	-3798	15	0	-30	-1663	4.02	4.02	4.02	4.02	3	0.23	0.11	0.67	0.00	0.00	22.3
2	375	-520	-2951	-11	0	58	-1341	4.02	4.02	4.02	4.02	2	0.20	0.09	0.52	0.00	0.00	22.3
3	375	-475	-2918	-11	0	58	-1269	4.02	4.02	4.02	4.02	2	0.19	0.08	0.51	0.00	0.00	22.3
4	375	-437	-2925	35	0	-103	-1289	4.02	4.02	4.02	4.02	2	0.19	0.08	0.52	0.00	0.00	22.3
5	375	-391	-2892	35	0	-104	-1217	4.02	4.02	4.02	4.02	2	0.18	0.08	0.51	0.00	0.00	22.3
6	375	-544	-2981	5	0	1	-1408	4.02	4.02	4.02	4.02	2	0.21	0.09	0.52	0.00	0.00	22.3
7	375	-392	-2870	5	0	1	-1166	4.02	4.02	4.02	4.02	2	0.17	0.08	0.51	0.00	0.00	22.3
8	375	-519	-2973	19	0	-47	-1392	4.02	4.02	4.02	4.02	2	0.21	0.09	0.52	0.00	0.00	22.3
9	375	-367	-2863	18	0	-47	-1150	4.02	4.02	4.02	4.02	2	0.17	0.08	0.51	0.00	0.00	22.3
10	375	-520	-2951	-11	0	58	-1341	4.02	4.02	4.02	4.02	2	0.20	0.09	0.52	0.00	0.00	22.3
11	375	-475	-2918	-11	0	58	-1269	4.02	4.02	4.02	4.02	2	0.19	0.08	0.51	0.00	0.00	22.3
12	375	-437	-2925	35	0	-103	-1289	4.02	4.02	4.02	4.02	2	0.19	0.08	0.52	0.00	0.00	22.3
13	375	-391	-2892	35	0	-104	-1217	4.02	4.02	4.02	4.02	2	0.18	0.08	0.51	0.00	0.00	22.3
14	375	-544	-2981	5	0	1	-1408	4.02	4.02	4.02	4.02	2	0.21	0.09	0.52	0.00	0.00	22.3
15	375	-392	-2870	5	0	1	-1166	4.02	4.02	4.02	4.02	2	0.17	0.08	0.51	0.00	0.00	22.3
16	375	-519	-2973	19	0	-47	-1392	4.02	4.02	4.02	4.02	2	0.21	0.09	0.52	0.00	0.00	22.3
17	375	-367	-2863	18	0	-47	-1150	4.02	4.02	4.02	4.02	2	0.17	0.08	0.51	0.00	0.00	22.3
18	375	-844	-4263	-27	0	156	-2040	4.02	4.02	4.02	4.02	3	0.29	0.12	0.74	0.00	0.00	22.3
19	375	-521	-4134	106	0	-326	-1771	4.02	4.02	4.02	4.02	3	0.25	0.12	0.73	0.00	0.00	22.3
20	375	-763	-4282	43	0	-96	-2057	4.02	4.02	4.02	4.02	3	0.29	0.12	0.75	0.00	0.00	22.3
37	375	-914	-4112	-79	0	334	-2025	4.02	4.02	4.02	4.02	3	0.28	0.12	0.72	0.00	0.00	22.3
38	375	-375	-3898	143	0	-469	-1576	4.02	4.02	4.02	4.02	3	0.22	0.11	0.69	0.00	0.00	22.3
39	375	-779	-4143	37	0	-87	-2054	4.02	4.02	4.02	4.02	3	0.29	0.12	0.72	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

Nome travata: **trave_505_IP1** Descrizione: **Trave_5 16-15-14-13**
ASTA NUM. 13 NI 171 NF 296 SEZ. Rp B= 0.400 H= 0.500 (trave)

categoria: p.p. y Permanente Neve qy tot.
qy medio: 500.00 2627.25 282.50 3409.75 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

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NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice resistenza			aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-652	5965	-463	0	-672	-2098	4.02	4.02	4.02	4.02	3	0.29	0.13	0.80	0.00	0.00	16.8
2	0	-486	4514	-89	0	-179	-1551	4.02	4.02	4.02	4.02	2	0.23	0.10	0.61	0.00	0.00	16.8
3	0	-520	4636	-95	0	-187	-1644	4.02	4.02	4.02	4.02	2	0.24	0.10	0.62	0.00	0.00	16.8
4	0	-483	4540	-617	0	-847	-1583	4.02	4.02	4.02	4.02	2	0.23	0.10	0.61	0.00	0.00	16.8
5	0	-517	4662	-623	0	-855	-1676	4.02	4.02	4.02	4.02	2	0.25	0.10	0.63	0.00	0.00	16.8
6	0	-445	4381	-266	0	-403	-1454	4.02	4.02	4.02	4.02	2	0.22	0.10	0.59	0.00	0.00	16.8
7	0	-559	4788	-287	0	-431	-1763	4.02	4.02	4.02	4.02	2	0.26	0.10	0.64	0.00	0.00	16.8
8	0	-445	4389	-425	0	-603	-1464	4.02	4.02	4.02	4.02	2	0.22	0.10	0.59	0.00	0.00	16.8
9	0	-558	4795	-446	0	-631	-1773	4.02	4.02	4.02	4.02	2	0.26	0.10	0.64	0.00	0.00	16.8
10	0	-486	4514	-89	0	-179	-1551	4.02	4.02	4.02	4.02	2	0.23	0.10	0.61	0.00	0.00	16.8
11	0	-520	4636	-95	0	-187	-1644	4.02	4.02	4.02	4.02	2	0.24	0.10	0.62	0.00	0.00	16.8
12	0	-483	4540	-617	0	-847	-1583	4.02	4.02	4.02	4.02	2	0.23	0.10	0.61	0.00	0.00	16.8
13	0	-517	4662	-623	0	-855	-1676	4.02	4.02	4.02	4.02	2	0.25	0.10	0.63	0.00	0.00	16.8
14	0	-445	4381	-266	0	-403	-1454	4.02	4.02	4.02	4.02	2	0.22	0.10	0.59	0.00	0.00	16.8
15	0	-559	4788	-287	0	-431	-1763	4.02	4.02	4.02	4.02	2	0.26	0.10	0.64	0.00	0.00	16.8
16	0	-445	4389	-425	0	-603	-1464	4.02	4.02	4.02	4.02	2	0.22	0.10	0.59	0.00	0.00	16.8
17	0	-558	4795	-446	0	-631	-1773	4.02	4.02	4.02	4.02	2	0.26	0.10	0.64	0.00	0.00	16.8
18	0	-635	6343	-252	0	-484	-2151	4.02	4.02	4.02	4.02	3	0.30	0.14	0.85	0.00	0.00	16.8
19	0	-630	6440	-1663	0	-2266	-2236	4.02	4.02	4.02	4.02	3	0.39	0.14	0.86	0.00	0.00	16.8
20	0	-524	6313	-887	0	-1273	-1995	4.02	4.02	4.02	4.02	3	0.28	0.14	0.85	0.00	0.00	16.8
37	0	-632	6069	380	0	340	-2061	4.02	4.02	4.02	4.02	3	0.28	0.13	0.81	0.00	0.00	16.8
38	0	-625	6230	-1971	0	-2630	-2202	4.02	4.02	4.02	4.02	3	0.46	0.14	0.84	0.00	0.00	16.8
39	0	-449	6018	-679	0	-975	-1801	4.02	4.02	4.02	4.02	3	0.25	0.13	0.81	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	31	-652	4705	-463	0	-529	-2098	4.02	4.02	4.02	4.02	3	0.29	0.10	0.63	0.00	0.00	16.8
2	31	-486	3545	-89	0	-151	-1551	4.02	4.02	4.02	4.02	2	0.23	0.08	0.48	0.00	0.00	16.8
3	31	-520	3667	-95	0	-158	-1644	4.02	4.02	4.02	4.02	2	0.24	0.08	0.49	0.00	0.00	16.8
4	31	-483	3571	-617	0	-655	-1583	4.02	4.02	4.02	4.02	2	0.23	0.08	0.48	0.00	0.00	16.8
5	31	-517	3693	-623	0	-662	-1676	4.02	4.02	4.02	4.02	2	0.25	0.08	0.50	0.00	0.00	16.8
6	31	-445	3412	-266	0	-320	-1454	4.02	4.02	4.02	4.02	2	0.22	0.07	0.46	0.00	0.00	16.8
7	31	-559	3818	-287	0	-342	-1763	4.02	4.02	4.02	4.02	2	0.26	0.08	0.51	0.00	0.00	16.8
8	31	-445	3419	-425	0	-472	-1464	4.02	4.02	4.02	4.02	2	0.22	0.07	0.46	0.00	0.00	16.8
9	31	-558	3826	-446	0	-493	-1773	4.02	4.02	4.02	4.02	2	0.26	0.08	0.51	0.00	0.00	16.8
10	31	-486	3545	-89	0	-151	-1551	4.02	4.02	4.02	4.02	2	0.23	0.08	0.48	0.00	0.00	16.8
11	31	-520	3667	-95	0	-158	-1644	4.02	4.02	4.02	4.02	2	0.24	0.08	0.49	0.00	0.00	16.8
12	31	-483	3571	-617	0	-655	-1583	4.02	4.02	4.02	4.02	2	0.23	0.08	0.48	0.00	0.00	16.8
13	31	-517	3693	-623	0	-662	-1676	4.02	4.02	4.02	4.02	2	0.25	0.08	0.50	0.00	0.00	16.8
14	31	-445	3412	-266	0	-320	-1454	4.02	4.02	4.02	4.02	2	0.22	0.07	0.46	0.00	0.00	16.8
15	31	-559	3818	-287	0	-342	-1763	4.02	4.02	4.02	4.02	2	0.26	0.08	0.51	0.00	0.00	16.8
16	31	-445	3419	-425	0	-472	-1464	4.02	4.02	4.02	4.02	2	0.22	0.07	0.46	0.00	0.00	16.8
17	31	-558	3826	-446	0	-493	-1773	4.02	4.02	4.02	4.02	2	0.26	0.08	0.51	0.00	0.00	16.8
18	31	-635	4951	-252	0	-406	-2151	4.02	4.02	4.02	4.02	3	0.30	0.11	0.66	0.00	0.00	16.8
19	31	-630	5048	-1663	0	-1750	-2236	4.02	4.02	4.02	4.02	3	0.31	0.11	0.68	0.00	0.00	16.8
20	31	-524	4921	-887	0	-998	-1995	4.02	4.02	4.02	4.02	3	0.28	0.11	0.66	0.00	0.00	16.8
37	31	-632	4743	380	0	222	-2061	4.02	4.02	4.02	4.02	3	0.28	0.10	0.64	0.00	0.00	16.8
38	31	-625	4904	-1971	0	-2019	-2202	4.02	4.02	4.02	4.02	3	0.35	0.11	0.66	0.00	0.00	16.8
39	31	-449	4692	-679	0	-764	-1801	4.02	4.02	4.02	4.02	3	0.25	0.10	0.63	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	62	-652	3444	-463	0	-385	2264	4.02	4.02	4.02	4.02	3	0.31	0.07	0.46	0.00	0.00	16.8
2	62	-486	2575	-89	0	-124	1689	4.02	4.02	4.02	4.02	2	0.25	0.06	0.35	0.00	0.00	16.8
3	62	-520	2697	-95	0	-128	1786	4.02	4.02	4.02	4.02	2	0.26	0.06	0.36	0.00	0.00	16.8
4	62	-483	2601	-617	0	-464	1698	4.02	4.02	4.02	4.02	2	0.25	0.06	0.35	0.00	0.00	16.8
5	62	-517	2723	-623	0	-469	1794	4.02	4.02	4.02	4.02	2	0.27	0.06	0.37	0.00	0.00	16.8
6	62	-445	2442	-266	0	-238	1580	4.02	4.02	4.02	4.02	2	0.23	0.05	0.33	0.00	0.00	16.8
7	62	-559	2849	-287	0	-252	1901	4.02	4.02	4.02	4.02	2	0.28	0.06	0.38	0.00	0.00	16.8
8	62	-445	2450	-425	0	-340	1582	4.02	4.02	4.02	4.02	2	0.23	0.05	0.33	0.00	0.00	16.8
9	62	-558	2856	-446	0	-355	1903	4.02	4.02	4.02	4.02	2	0.28	0.06	0.38	0.00	0.00	16.8
10	62	-486	2575	-89	0	-124	1689	4.02	4.02	4.02	4.02	2	0.25	0.06	0.35	0.00	0.00	16.8
11	62	-520	2697	-95	0	-128	1786	4.02	4.02	4.02	4.02	2	0.26	0.06	0.36	0.00	0.00	16.8
12	62	-483	2601	-617	0	-464	1698	4.02	4.02	4.02	4.02	2	0.25	0.06	0.35	0.00	0.00	16.8
13	62	-517	2723	-623	0	-469	1794	4.02	4.02	4.02	4.02	2	0.27	0.06	0.37	0.00	0.00	16.8
14	62	-445	2442	-266	0	-238	1580	4.02	4.02	4.02	4.02	2	0.23	0.05	0.33	0.00	0.00	16.8
15	62	-559	2849	-287	0	-252	1901	4.02	4.02	4.02	4.02	2	0.28	0.06	0.38	0.00	0.00	16.8
16	62	-445	2450	-425	0	-340	1582	4.02	4.02	4.02	4.02	2	0.23	0.05	0.33	0.00	0.00	16.8
17	62	-558	2856	-446	0	-355	1903	4.02	4.02	4.02	4.02	2	0.28	0.06	0.38	0.00	0.00	16.8
18	62	-635	3560	-252	0	-328	2288	4.02	4.02	4.02	4.02	3	0.32	0.08	0.48	0.00	0.00	16.8
19	62	-630	3657	-1663	0	-1235	2353	4.02	4.02	4.02	4.02	3	0.32	0.08	0.49	0.00	0.00	16.8
20	62	-524	3530	-887	0	-723	2397	4.02	4.02	4.02	4.02	3	0.33	0.08	0.47	0.00	0.00	16.8
37	62	-632	3417	380	0	104	2207	4.02	4.02	4.02	4.02	3	0.30	0.07	0.46	0.00	0.00	16.8
38	62	-625	3578	-1971	0	-1408	2316	4.02	4.02	4.02	4.02	3	0.32	0.08	0.48	0.00	0.00	16.8
39	62	-449	3366	-679	0	-554	2389	4.02	4.02	4.02	4.02	3	0.33	0.07	0.45	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	93	-652	2184	-463	0	-242	2264	4.02	4.02	4.02	4.02	3	0.31	0.05	0.29	0.00	0.00	16.8
2	93	-486	1606	-89	0	-96	1689	4.02	4.02	4.02	4.02	2	0.25	0.03	0.22	0.00	0.00	16.8
3	93	-520	1728	-95	0	-99	1786	4.02	4.02	4.02	4.02	2	0.26	0.04	0.23	0.00	0.00	16.8
4	93	-483	1632	-617	0	-273	1698	4.02	4.02	4.02	4.02	2	0.25	0.04	0.22	0.00	0.00	16.8
5	93	-517	1754	-623	0	-275	1794	4.02	4.02	4.02	4.02	2	0.27	0.04	0.24	0.00	0.00	16.8
6	93	-445	1473	-266	0	-155	1580	4.02	4.02	4.02	4.02	2	0.23	0.03	0.20	0.00	0.00	16.8
7	93	-559	1879	-287	0	-163	1901	4.02	4.02	4.02	4.02	2	0.28	0.04	0.25	0.00	0.00	16.8
8	93	-445	1480	-425	0	-208	1582	4.02	4.02	4.02	4.02	2	0.23	0.03	0.20	0.00	0.00	16.8
9	93	-558	1887	-446	0	-217	1903	4.02	4.02	4.02	4.02	2	0.28	0.04	0.25	0.00	0.00	16.8
10	93	-486	1606	-89	0	-96	1689	4.02	4.02	4.02	4.02	2	0.25	0.03	0.22	0.00	0.00	16.8
11	93	-520	1728	-95	0	-99	1786	4.02	4.02	4.02	4.02	2	0.26	0.04	0.23	0.00	0.00	16.8
12	93	-483	1632	-617	0	-273	1698	4.02	4.02	4.02	4.02	2	0.25	0.04	0.22	0.00	0.00	16.8
13	93	-517	1754	-623	0	-275	1794	4.02	4.02	4.02	4.02	2	0.27	0.04	0.24	0.00	0.00	16.8
14	93	-445	1473	-266	0	-155	1580	4.02	4.02	4.02	4.02	2	0.23	0.03	0.20	0.00	0.00	16.8
15	93	-559	1879	-287	0	-163	1901	4.02	4.02	4.02	4.02	2	0.28	0.04	0.25	0.00	0.00	16.8
16	93	-445	1480	-425	0	-208	1582	4.02	4.02	4.02	4.02	2	0.23	0.03	0.20	0.00	0.00	16.8
17	93	-558	1887	-446	0	-217	1903	4.02	4.02	4.02	4.02	2	0.28	0.04	0.25	0.00	0.00	16.8
18	93	-635	2168	-252	0	-250	2288	4.02	4.02	4.02	4.02	3	0.32	0.05	0.29	0.00	0.00	16.8
19	93	-630	2265	-1663	0	-720	2353	4.02	4.02	4.02	4.02	3	0.32	0.05	0.30	0.00	0.00	16.8
20	93	-524	2138	-887	0	-448	2397	4.02	4.02	4.02	4.02	3	0.33	0.05	0.29	0.00	0.00	16.8
37	93	-632	2091	380	0	-14	2207	4.02	4.02	4.02	4.02	3	0.30	0.05	0.28	0.00	0.00	16.8
38	93	-625	2252	-1971	0	-796	2316	4.02	4.02	4.02	4.02	3	0.32	0.05	0.30	0.00	0.00	16.8
39	93	-449	2040	-679	0	-343	2389	4.02	4.02	4.02	4.02	3	0.33	0.04	0.27	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	124	-652	924	-463	0	-98	2264	4.02	4.02	4.02	4.02	3	0.31	0.02	0.12	0.00	0.00	16.8

2	124	-486	636	-89	0	-69	1689	4.02	4.02	4.02	4.02	2	0.25	0.01	0.09	0.00	0.00	16.8
3	124	-520	758	-95	0	-69	1786	4.02	4.02	4.02	4.02	2	0.26	0.02	0.10	0.00	0.00	16.8
4	124	-483	662	-617	0	-82	1698	4.02	4.02	4.02	4.02	2	0.25	0.01	0.09	0.00	0.00	16.8
5	124	-517	784	-623	0	-82	1794	4.02	4.02	4.02	4.02	2	0.27	0.02	0.11	0.00	0.00	16.8
6	124	-445	503	-266	0	-73	1580	4.02	4.02	4.02	4.02	2	0.23	0.01	0.07	0.00	0.00	16.8
7	124	-559	910	-287	0	-74	1901	4.02	4.02	4.02	4.02	2	0.28	0.02	0.12	0.00	0.00	16.8
8	124	-445	511	-425	0	-77	1582	4.02	4.02	4.02	4.02	2	0.23	0.01	0.07	0.00	0.00	16.8
9	124	-558	917	-446	0	-78	1903	4.02	4.02	4.02	4.02	2	0.28	0.02	0.12	0.00	0.00	16.8
10	124	-486	636	-89	0	-69	1689	4.02	4.02	4.02	4.02	2	0.25	0.01	0.09	0.00	0.00	16.8
11	124	-520	758	-95	0	-69	1786	4.02	4.02	4.02	4.02	2	0.26	0.02	0.10	0.00	0.00	16.8
12	124	-483	662	-617	0	-82	1698	4.02	4.02	4.02	4.02	2	0.25	0.01	0.09	0.00	0.00	16.8
13	124	-517	784	-623	0	-82	1794	4.02	4.02	4.02	4.02	2	0.27	0.02	0.11	0.00	0.00	16.8
14	124	-445	503	-266	0	-73	1580	4.02	4.02	4.02	4.02	2	0.23	0.01	0.07	0.00	0.00	16.8
15	124	-559	910	-287	0	-74	1901	4.02	4.02	4.02	4.02	2	0.28	0.02	0.12	0.00	0.00	16.8
16	124	-445	511	-425	0	-77	1582	4.02	4.02	4.02	4.02	2	0.23	0.01	0.07	0.00	0.00	16.8
17	124	-558	917	-446	0	-78	1903	4.02	4.02	4.02	4.02	2	0.28	0.02	0.12	0.00	0.00	16.8
18	124	-635	777	-252	0	-172	2288	4.02	4.02	4.02	4.02	3	0.32	0.02	0.10	0.00	0.00	16.8
19	124	-630	873	-1663	0	-204	2353	4.02	4.02	4.02	4.02	3	0.32	0.04	0.21	0.00	0.00	16.8
20	124	-524	746	-887	0	-173	2397	4.02	4.02	4.02	4.02	3	0.33	0.02	0.11	0.00	0.00	16.8
37	124	-632	765	380	0	-132	2207	4.02	4.02	4.02	4.02	3	0.30	0.02	0.10	0.00	0.00	16.8
38	124	-625	926	-1971	0	-185	2316	4.02	4.02	4.02	4.02	3	0.32	0.04	0.25	0.00	0.00	16.8
39	124	-449	714	-679	0	-133	2389	4.02	4.02	4.02	4.02	3	0.33	0.02	0.10	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	155	-652	-336	-463	0	45	2264	4.02	4.02	4.02	4.02	3	0.31	0.01	0.06	0.00	0.00	16.8
2	155	-486	-333	-89	0	-41	1689	4.02	4.02	4.02	4.02	2	0.25	0.01	0.04	0.00	0.00	16.8
3	155	-520	-211	-95	0	-40	1786	4.02	4.02	4.02	4.02	2	0.26	0.00	0.03	0.00	0.00	16.8
4	155	-483	-307	-617	0	110	1698	4.02	4.02	4.02	4.02	2	0.25	0.01	0.08	0.00	0.00	16.8
5	155	-517	-185	-623	0	111	1794	4.02	4.02	4.02	4.02	2	0.27	0.01	0.08	0.00	0.00	16.8
6	155	-445	-466	-266	0	10	1580	4.02	4.02	4.02	4.02	2	0.23	0.01	0.06	0.00	0.00	16.8
7	155	-559	-60	-287	0	15	1901	4.02	4.02	4.02	4.02	2	0.28	0.01	0.04	0.00	0.00	16.8
8	155	-445	-458	-425	0	55	1582	4.02	4.02	4.02	4.02	2	0.23	0.01	0.06	0.00	0.00	16.8
9	155	-558	-52	-446	0	60	1903	4.02	4.02	4.02	4.02	2	0.28	0.01	0.06	0.00	0.00	16.8
10	155	-486	-333	-89	0	-41	1689	4.02	4.02	4.02	4.02	2	0.25	0.01	0.04	0.00	0.00	16.8
11	155	-520	-211	-95	0	-40	1786	4.02	4.02	4.02	4.02	2	0.26	0.00	0.03	0.00	0.00	16.8
12	155	-483	-307	-617	0	110	1698	4.02	4.02	4.02	4.02	2	0.25	0.01	0.08	0.00	0.00	16.8
13	155	-517	-185	-623	0	111	1794	4.02	4.02	4.02	4.02	2	0.27	0.01	0.08	0.00	0.00	16.8
14	155	-445	-466	-266	0	10	1580	4.02	4.02	4.02	4.02	2	0.23	0.01	0.06	0.00	0.00	16.8
15	155	-559	-60	-287	0	15	1901	4.02	4.02	4.02	4.02	2	0.28	0.01	0.04	0.00	0.00	16.8
16	155	-445	-458	-425	0	55	1582	4.02	4.02	4.02	4.02	2	0.23	0.01	0.06	0.00	0.00	16.8
17	155	-558	-52	-446	0	60	1903	4.02	4.02	4.02	4.02	2	0.28	0.01	0.06	0.00	0.00	16.8
18	155	-635	-615	-252	0	-94	2288	4.02	4.02	4.02	4.02	3	0.32	0.01	0.08	0.00	0.00	16.8
19	155	-630	-519	-1663	0	311	2353	4.02	4.02	4.02	4.02	3	0.32	0.04	0.21	0.00	0.00	16.8
20	155	-524	-646	-887	0	102	2397	4.02	4.02	4.02	4.02	3	0.33	0.02	0.11	0.00	0.00	16.8
37	155	-632	-561	380	0	-250	2207	4.02	4.02	4.02	4.02	3	0.30	0.01	0.08	0.00	0.00	16.8
38	155	-625	-400	-1971	0	426	2316	4.02	4.02	4.02	4.02	3	0.32	0.04	0.25	0.00	0.00	16.8
39	155	-449	-612	-679	0	78	2389	4.02	4.02	4.02	4.02	3	0.33	0.02	0.09	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	186	-652	-1597	-463	0	189	2264	4.02	4.02	4.02	4.02	3	0.31	0.03	0.21	0.00	0.00	16.8
2	186	-486	-1302	-89	0	-14	1689	4.02	4.02	4.02	4.02	2	0.25	0.03	0.18	0.00	0.00	16.8
3	186	-520	-1180	-95	0	-10	1786	4.02	4.02	4.02	4.02	2	0.26	0.03	0.16	0.00	0.00	16.8
4	186	-483	-1276	-617	0	301	1698	4.02	4.02	4.02	4.02	2	0.25	0.03	0.17	0.00	0.00	16.8
5	186	-517	-1154	-623	0	304	1794	4.02	4.02	4.02	4.02	2	0.27	0.03	0.16	0.00	0.00	16.8
6	186	-445	-1435	-266	0	92	1580	4.02	4.02	4.02	4.02	2	0.23	0.03	0.19	0.00	0.00	16.8
7	186	-559	-1029	-287	0	104	1901	4.02	4.02	4.02	4.02	2	0.28	0.02	0.14	0.00	0.00	16.8
8	186	-445	-1428	-425	0	187	1582	4.02	4.02	4.02	4.02	2	0.23	0.03	0.19	0.00	0.00	16.8
9	186	-558	-1021	-446	0	198	1903	4.02	4.02	4.02	4.02	2	0.28	0.02	0.14	0.00	0.00	16.8
10	186	-486	-1302	-89	0	-14	1689	4.02	4.02	4.02	4.02	2	0.25	0.03	0.18	0.00	0.00	16.8
11	186	-520	-1180	-95	0	-10	1786	4.02	4.02	4.02	4.02	2	0.26	0.03	0.16	0.00	0.00	16.8
12	186	-483	-1276	-617	0	301	1698	4.02	4.02	4.02	4.02	2	0.25	0.03	0.17	0.00	0.00	16.8
13	186	-517	-1154	-623	0	304	1794	4.02	4.02	4.02	4.02	2	0.27	0.03	0.16	0.00	0.00	16.8
14	186	-445	-1435	-266	0	92	1580	4.02	4.02	4.02	4.02	2	0.23	0.03	0.19	0.00	0.00	16.8
15	186	-559	-1029	-287	0	104	1901	4.02	4.02	4.02	4.02	2	0.28	0.02	0.14	0.00	0.00	16.8
16	186	-445	-1428	-425	0	187	1582	4.02	4.02	4.02	4.02	2	0.23	0.03	0.19	0.00	0.00	16.8
17	186	-558	-1021	-446	0	198	1903	4.02	4.02	4.02	4.02	2	0.28	0.02	0.14	0.00	0.00	16.8
18	186	-635	-2007	-252	0	-16	2288	4.02	4.02	4.02	4.02	3	0.32	0.04	0.27	0.00	0.00	16.8
19	186	-630	-1910	-1663	0	827	2353	4.02	4.02	4.02	4.02	3	0.32	0.04	0.26	0.00	0.00	16.8
20	186	-524	-2037	-887	0	378	2397	4.02	4.02	4.02	4.02	3	0.33	0.04	0.27	0.00	0.00	16.8
37	186	-632	-1887	380	0	-368	2207	4.02	4.02	4.02	4.02	3	0.30	0.04	0.25	0.00	0.00	16.8
38	186	-625	-1726	-1971	0	1037	2316	4.02	4.02	4.02	4.02	3	0.32	0.04	0.25	0.00	0.00	16.8
39	186	-449	-1937	-679	0	289	2389	4.02	4.02	4.02	4.02	3	0.33	0.04	0.26	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	217	-652	-2857	-463	0	332	2264	4.02	4.02	4.02	4.02	3	0.31	0.06	0.38	0.00	0.00	16.8
2	217	-486	-2272	-89	0	14	1689	4.02	4.02	4.02	4.02	2	0.25	0.05	0.31	0.00	0.00	16.8
3	217	-520	-2150	-95	0	19	1786	4.02	4.02	4.02	4.02	2	0.26	0.05	0.29	0.00	0.00	16.8
4	217	-483	-2246	-617	0	492	1698	4.02	4.02	4.02	4.02	2	0.25	0.05	0.30	0.00	0.00	16.8
5	217	-517	-2124	-623	0	497	1794	4.02	4.02	4.02	4.02	2	0.27	0.05	0.29	0.00	0.00	16.8
6	217	-445	-2405	-266	0	175	1580	4.02	4.02	4.02	4.02	2	0.23	0.05	0.32	0.00	0.00	16.8
7	217	-559	-1998	-287	0	193	1901	4.02	4.02	4.02	4.02	2	0.28	0.04	0.27	0.00	0.00	16.8
8	217	-445	-2398	-425	0	318	1582	4.02	4.02	4.02	4.02	2	0.23	0.05	0.32	0.00	0.00	16.8
9	217	-558	-1991	-446	0	336	1903	4.02	4.02	4.02	4.02	2	0.28	0.04	0.27	0.00	0.00	16.8
10	217	-486	-2272	-89	0	14	1689	4.02	4.02	4.02	4.02	2	0.25	0.05	0.31	0.00	0.00	16.8
11	217	-520	-2150	-95	0	19	1786	4.02	4.02	4.02	4.02	2	0.26	0.05	0.29	0.00	0.00	16.8
12	217	-483	-2246	-617	0	492	1698	4.02	4.02	4.02	4.02	2	0.25	0.05	0.30	0.00	0.00	16.8
13	217	-517	-2124	-623	0	497	1794	4.02	4.02	4.02	4.02	2	0.27	0.05	0.29	0.00	0.00	16.8
14	217	-445	-2405	-266	0	175	1580	4.02	4.02	4.02	4.02	2	0.23	0.05	0.32	0.00	0.00	16.8
15	217	-559	-1998	-287	0	193	1901	4.02	4.02	4.02	4.02	2	0.28	0.04	0.27	0.00	0.00	16.8
16	217	-445	-2398	-425	0	318	1582	4.02	4.02	4.02	4.02	2	0.23	0.05	0.32	0.00	0.00	16.8
17	217	-558	-1991	-446	0	336	1903	4.02	4.02	4.02	4.02	2	0.28	0.04	0.27	0.00	0.00	16.8
18	217	-635	-3398	-252	0	62	2288	4.02	4.02	4.02	4.02	3	0.32	0.07	0.46	0.00	0.00	16.8
19	217	-630	-3302	-1663	0	1342	2353	4.02	4.02	4.02	4.02	3	0.32	0.07	0.44	0.00	0.00	16.8
20	217	-524	-3429	-887	0	653	2397	4.02	4.02	4.02	4.02	3	0.33	0.07	0.46	0.00	0.00	16.8
37	217	-632	-3213	380	0	-486	2207	4.02	4.02	4.02	4.02	3	0.30	0.07	0.43	0.00	0.00	16.8
38	217	-625	-3052	-1971	0	1648	2316	4.02	4.02	4.02	4.02	3	0.32	0.07	0.41	0.00	0.00	16.8
39	217	-449	-3263	-679	0	499	2389	4.02	4.02	4.02	4.02	3	0.33	0.07	0.44	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	248	-652	-4117	-463	0	476	2264	4.02	4.02	4.02	4.02	3	0.31	0.09	0.55	0.00	0.00	16.8
2	248	-486	-3241	-89	0	41	1668	4.02	4.02	4.02	4.02	2	0.25	0.07	0.44	0.00	0.00	16.8
3	248	-520	-3119	-95	0	49	1786	4.02	4.02	4.02	4.02	2	0.26	0.07	0.42	0.00	0.00	16.8
4	248	-483	-3215	-617	0	683	1687	4.02	4.02	4.02	4.02	2	0.25	0.07	0.43	0.00	0.00	16.8
5	248	-517	-3093	-623	0	691	1794	4.02	4.02	4.02	4.02	2	0.27	0.07	0.42	0.00	0.00	16.8
6	248	-445	-3374	-266	0	258	-1915	4.02	4.02	4.02	4.02	2	0.28	0.07	0.45	0.00	0.00	16.8
7	248	-559	-2968	-287	0	282	1901	4.02	4.02	4.02	4.02	2	0.28	0.06	0.40	0.00	0.00	16.8

8	248	-445	-3367	-425	0	450	-1901	4.02	4.02	4.02	4.02	2	0.28	0.07	0.45	0.00	0.00	16.8
9	248	-558	-2960	-446	0	474	1903	4.02	4.02	4.02	4.02	2	0.28	0.06	0.40	0.00	0.00	16.8
10	248	-486	-3241	-89	0	41	1668	4.02	4.02	4.02	4.02	2	0.25	0.07	0.44	0.00	0.00	16.8
11	248	-520	-3119	-95	0	49	1786	4.02	4.02	4.02	4.02	2	0.26	0.07	0.42	0.00	0.00	16.8
12	248	-483	-3215	-617	0	683	1687	4.02	4.02	4.02	4.02	2	0.25	0.07	0.43	0.00	0.00	16.8
13	248	-517	-3093	-623	0	691	1794	4.02	4.02	4.02	4.02	2	0.27	0.07	0.42	0.00	0.00	16.8
14	248	-445	-3374	-266	0	258	-1915	4.02	4.02	4.02	4.02	2	0.28	0.07	0.45	0.00	0.00	16.8
15	248	-559	-2968	-287	0	282	1901	4.02	4.02	4.02	4.02	2	0.28	0.06	0.40	0.00	0.00	16.8
16	248	-445	-3367	-425	0	450	-1901	4.02	4.02	4.02	4.02	2	0.28	0.07	0.45	0.00	0.00	16.8
17	248	-558	-2960	-446	0	474	1903	4.02	4.02	4.02	4.02	2	0.28	0.06	0.40	0.00	0.00	16.8
18	248	-635	-4790	-252	0	140	-2650	4.02	4.02	4.02	4.02	3	0.37	0.10	0.64	0.00	0.00	16.8
19	248	-630	-4694	-1663	0	1858	-2446	4.02	4.02	4.02	4.02	3	0.34	0.10	0.63	0.00	0.00	16.8
20	248	-524	-4821	-887	0	928	-2585	4.02	4.02	4.02	4.02	3	0.36	0.10	0.65	0.00	0.00	16.8
37	248	-632	-4539	380	0	-603	-2462	4.02	4.02	4.02	4.02	3	0.34	0.10	0.61	0.00	0.00	16.8
38	248	-625	-4378	-1971	0	2260	2310	4.02	4.02	4.02	4.02	3	0.39	0.10	0.59	0.00	0.00	16.8
39	248	-449	-4589	-679	0	710	-2353	4.02	4.02	4.02	4.02	3	0.33	0.10	0.62	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	279	-652	-5378	-463	0	619	-3142	4.02	4.02	4.02	4.02	3	0.43	0.12	0.72	0.00	0.00	16.8
2	279	-486	-4211	-89	0	69	-2584	4.02	4.02	4.02	4.02	2	0.38	0.09	0.57	0.00	0.00	16.8
3	279	-520	-4089	-95	0	78	-2298	4.02	4.02	4.02	4.02	2	0.34	0.09	0.55	0.00	0.00	16.8
4	279	-483	-4185	-617	0	875	-2535	4.02	4.02	4.02	4.02	2	0.38	0.09	0.56	0.00	0.00	16.8
5	279	-517	-4063	-623	0	884	-2250	4.02	4.02	4.02	4.02	2	0.33	0.09	0.55	0.00	0.00	16.8
6	279	-445	-4344	-266	0	340	-2900	4.02	4.02	4.02	4.02	2	0.43	0.09	0.58	0.00	0.00	16.8
7	279	-559	-3938	-287	0	371	-1948	4.02	4.02	4.02	4.02	2	0.29	0.09	0.53	0.00	0.00	16.8
8	279	-445	-4337	-425	0	582	-2885	4.02	4.02	4.02	4.02	2	0.43	0.09	0.58	0.00	0.00	16.8
9	279	-558	-3930	-446	0	612	-1934	4.02	4.02	4.02	4.02	2	0.29	0.09	0.53	0.00	0.00	16.8
10	279	-486	-4211	-89	0	69	-2584	4.02	4.02	4.02	4.02	2	0.38	0.09	0.57	0.00	0.00	16.8
11	279	-520	-4089	-95	0	78	-2298	4.02	4.02	4.02	4.02	2	0.34	0.09	0.55	0.00	0.00	16.8
12	279	-483	-4185	-617	0	875	-2535	4.02	4.02	4.02	4.02	2	0.38	0.09	0.56	0.00	0.00	16.8
13	279	-517	-4063	-623	0	884	-2250	4.02	4.02	4.02	4.02	2	0.33	0.09	0.55	0.00	0.00	16.8
14	279	-445	-4344	-266	0	340	-2900	4.02	4.02	4.02	4.02	2	0.43	0.09	0.58	0.00	0.00	16.8
15	279	-559	-3938	-287	0	371	-1948	4.02	4.02	4.02	4.02	2	0.29	0.09	0.53	0.00	0.00	16.8
16	279	-445	-4337	-425	0	582	-2885	4.02	4.02	4.02	4.02	2	0.43	0.09	0.58	0.00	0.00	16.8
17	279	-558	-3930	-446	0	612	-1934	4.02	4.02	4.02	4.02	2	0.29	0.09	0.53	0.00	0.00	16.8
18	279	-635	-6181	-252	0	218	-4058	4.02	4.02	4.02	4.02	3	0.56	0.13	0.83	0.00	0.00	16.8
19	279	-630	-6085	-1663	0	2374	-3843	4.02	4.02	4.02	4.02	3	0.53	0.13	0.82	0.00	0.00	16.8
20	279	-524	-6212	-887	0	1203	-3996	4.02	4.02	4.02	4.02	3	0.55	0.13	0.83	0.00	0.00	16.8
37	279	-632	-5865	380	0	-721	-3801	4.02	4.02	4.02	4.02	3	0.52	0.13	0.79	0.00	0.00	16.8
38	279	-625	-5704	-1971	0	2871	-3443	4.02	4.02	4.02	4.02	3	0.50	0.12	0.76	0.00	0.00	16.8
39	279	-449	-5915	-679	0	920	-3697	4.02	4.02	4.02	4.02	3	0.51	0.13	0.80	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	310	-652	-6638	-463	0	763	-3142	4.02	4.02	4.02	4.02	3	0.43	0.14	0.89	0.00	0.00	16.8
2	310	-486	-5180	-89	0	96	-2584	4.02	4.02	4.02	4.02	2	0.38	0.11	0.70	0.00	0.00	16.8
3	310	-520	-5058	-95	0	108	-2298	4.02	4.02	4.02	4.02	2	0.34	0.11	0.68	0.00	0.00	16.8
4	310	-483	-5154	-617	0	1066	-2535	4.02	4.02	4.02	4.02	2	0.38	0.11	0.69	0.00	0.00	16.8
5	310	-517	-5032	-623	0	1077	-2250	4.02	4.02	4.02	4.02	2	0.33	0.11	0.68	0.00	0.00	16.8
6	310	-445	-5313	-266	0	423	-2900	4.02	4.02	4.02	4.02	2	0.43	0.12	0.71	0.00	0.00	16.8
7	310	-559	-4907	-287	0	460	-1948	4.02	4.02	4.02	4.02	2	0.29	0.11	0.66	0.00	0.00	16.8
8	310	-445	-5306	-425	0	713	-2885	4.02	4.02	4.02	4.02	2	0.43	0.12	0.71	0.00	0.00	16.8
9	310	-558	-4899	-446	0	751	-1934	4.02	4.02	4.02	4.02	2	0.29	0.11	0.66	0.00	0.00	16.8
10	310	-486	-5180	-89	0	96	-2584	4.02	4.02	4.02	4.02	2	0.38	0.11	0.70	0.00	0.00	16.8
11	310	-520	-5058	-95	0	108	-2298	4.02	4.02	4.02	4.02	2	0.34	0.11	0.68	0.00	0.00	16.8
12	310	-483	-5154	-617	0	1066	-2535	4.02	4.02	4.02	4.02	2	0.38	0.11	0.69	0.00	0.00	16.8
13	310	-517	-5032	-623	0	1077	-2250	4.02	4.02	4.02	4.02	2	0.33	0.11	0.68	0.00	0.00	16.8
14	310	-445	-5313	-266	0	423	-2900	4.02	4.02	4.02	4.02	2	0.43	0.12	0.71	0.00	0.00	16.8
15	310	-559	-4907	-287	0	460	-1948	4.02	4.02	4.02	4.02	2	0.29	0.11	0.66	0.00	0.00	16.8
16	310	-445	-5306	-425	0	713	-2885	4.02	4.02	4.02	4.02	2	0.43	0.12	0.71	0.00	0.00	16.8
17	310	-558	-4899	-446	0	751	-1934	4.02	4.02	4.02	4.02	2	0.29	0.11	0.66	0.00	0.00	16.8
18	310	-635	-7573	-252	0	296	-4058	4.02	4.02	4.02	4.02	3	0.56	0.16	1.01	1.88	0.00	16.8
19	310	-630	-7477	-1663	0	2889	-3843	4.02	4.02	4.02	4.02	3	0.53	0.16	1.00	1.85	0.00	16.8
20	310	-524	-7604	-887	0	1478	-3996	4.02	4.02	4.02	4.02	3	0.55	0.17	1.02	1.89	0.00	16.8
37	310	-632	-7191	380	0	-839	-3801	4.02	4.02	4.02	4.02	3	0.52	0.16	0.96	0.00	0.00	16.8
38	310	-625	-7030	-1971	0	3482	-3443	4.02	4.02	4.02	4.02	3	0.60	0.15	0.94	0.00	0.00	16.8
39	310	-449	-7241	-679	0	1131	-3697	4.02	4.02	4.02	4.02	3	0.51	0.16	0.97	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

Nome travata: **trave_505_IP1** Descrizione: **Trave_5 16-15-14-13**
ASTA NUM. 14 NI 296 NF 125 SEZ. Rp B= 0.400 H= 0.500 (trave)

categoria: p.p. y Permanente Neve qy tot.
qy medio: 500.00 2627.25 282.50 3409.75 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-1601	7047	-3	0	90	-3392	4.02	4.02	4.02	4.02	3	0.45	0.15	0.93	0.00	0.00	16.8
2	0	-1287	5373	-139	0	-342	-2484	4.02	4.02	4.02	4.02	2	0.36	0.12	0.71	0.00	0.00	16.8
3	0	-1176	5484	-138	0	-340	-2766	4.02	4.02	4.02	4.02	2	0.40	0.12	0.73	0.00	0.00	16.8
4	0	-1288	5357	134	0	478	-2452	4.02	4.02	4.02	4.02	2	0.35	0.12	0.71	0.00	0.00	16.8
5	0	-1177	5469	135	0	481	-2733	4.02	4.02	4.02	4.02	2	0.40	0.12	0.73	0.00	0.00	16.8
6	0	-1418	5237	-45	0	-58	-2145	4.02	4.02	4.02	4.02	2	0.31	0.11	0.69	0.00	0.00	16.8
7	0	-1046	5609	-42	0	-49	-3083	4.02	4.02	4.02	4.02	2	0.45	0.12	0.75	0.00	0.00	16.8
8	0	-1418	5233	38	0	188	-2135	4.02	4.02	4.02	4.02	2	0.31	0.11	0.69	0.00	0.00	16.8
9	0	-1046	5604	40	0	197	-3073	4.02	4.02	4.02	4.02	2	0.45	0.12	0.75	0.00	0.00	16.8
10	0	-1287	5373	-139	0	-342	-2484	4.02	4.02	4.02	4.02	2	0.36	0.12	0.71	0.00	0.00	16.8
11	0	-1176	5484	-138	0	-340	-2766	4.02	4.02	4.02	4.02	2	0.40	0.12	0.73	0.00	0.00	16.8
12	0	-1288	5357	134	0	478	-2452	4.02	4.02	4.02	4.02	2	0.35	0.12	0.71	0.00	0.00	16.8
13	0	-1177	5469	135	0	481	-2733	4.02	4.02	4.02	4.02	2	0.40	0.12	0.73	0.00	0.00	16.8
14	0	-1418	5237	-45	0	-58	-2145	4.02	4.02	4.02	4.02	2	0.31	0.11	0.69	0.00	0.00	16.8
15	0	-1046	5609	-42	0	-49	-3083	4.02	4.02	4.02	4.02	2	0.45	0.12	0.75	0.00	0.00	16.8
16	0	-1418	5233	38	0	188	-2135	4.02	4.02	4.02	4.02	2	0.31	0.11	0.69	0.00	0.00	16.8
17	0	-1046	5604	40	0	197	-3073	4.02	4.02	4.02	4.02	2	0.45	0.12	0.75	0.00	0.00	16.8
18	0	-2249	7427	-386	0	-972	-2881	4.02	4.02	4.02	4.02	3	0.38	0.16	0.97	0.00	0.00	16.8
19	0	-2124	7501	459	0	1546	-3068	4.02	4.02	4.02	4.02	3	0.41	0.16	0.98	0.00	0.00	16.8
20	0	-2491	7448	28	0	248	-3019	4.02	4.02	4.02	4.02	3	0.40	0.16	0.97	0.00	0.00	16.8
37	0	-2082	7124	-680	0	-1874	-2863	4.02	4.02	4.02	4.02	3	0.38	0.15	0.93	0.00	0.00	16.8
38	0	-1875	7248	728	0	2321	-3173	4.02	4.02	4.02	4.02	3	0.42	0.16	0.95	0.00	0.00	16.8
39	0	-2486	7160	9	0	158	-3093	4.02	4.02	4.02	4.02	3	0.40	0.15	0.93	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	38	-1601	5522	-3	0	91	-3392	4.02	4.02	4.02	4.02	3	0.45	0.12	0.73	0.00	0.00	16.8
2	38	-1287	4200	-139	0	-290	-2484	4.02	4.02	4.02	4.02	2	0.36	0.09	0.56	0.00	0.00	16.8
3	38	-1176	4311	-138	0	-288	-2766	4.02	4.02	4.02	4.02	2	0.40	0.09	0.57	0.00	0.00	16.8
4	38	-1288	4184	134	0	428	-2452	4.02	4.02	4.02	4.02	2	0.35	0.09	0.55	0.00	0.00	16.8
5	38	-1177	4296	135	0	430	-2733	4.02	4.02	4.02	4.02	2	0.40	0.09	0.57	0.00	0.00	16.8
6	38	-1418	4064	-45	0	-42	-2145	4.02	4.02	4.02	4.02	2	0.31	0.09	0.54	0.00	0.00	16.8
7	38	-1046	4436	-42	0	-34	-3083	4.02	4.02	4.02	4.02	2	0.45	0.10	0.59	0.00	0.00	16.8
8	38	-1418	4060	38	0	174	-2135	4.02	4.02	4.02	4.02	2	0.31	0.09	0.54	0.00	0.00	16.8
9	38	-1046	4431	40	0	182	-3073	4.02	4.02	4.02	4.02	2	0.45	0.10	0.59	0.00	0.00	16.8
10	38	-1287	4200	-139	0	-290	-2484	4.02	4.02	4.02	4.02	2	0.36	0.09	0.56	0.00	0.00	16.8
11	38	-1176	4311	-138	0	-288	-2766	4.02	4.02	4.02	4.02	2	0.40	0.09	0.57	0.00	0.00	16.8
12	38	-1288	4184	134	0	428	-2452	4.02	4.02	4.02	4.02	2	0.35	0.09	0.55	0.00	0.00	16.8
13	38	-1177	4296	135	0	430	-2733	4.02	4.02	4.02	4.02	2	0.40	0.09	0.57	0.00	0.00	16.8
14	38	-1418	4064	-45	0	-42	-2145	4.02	4.02	4.02	4.02	2	0.31	0.09	0.54	0.00	0.00	16.8
15	38	-1046	4436	-42	0	-34	-3083	4.02	4.02	4.02	4.02	2	0.45	0.10	0.59	0.00	0.00	16.8
16	38	-1418	4060	38	0	174	-2135	4.02	4.02	4.02	4.02	2	0.31	0.09	0.54	0.00	0.00	16.8
17	38	-1046	4431	40	0	182	-3073	4.02	4.02	4.02	4.02	2	0.45	0.10	0.59	0.00	0.00	16.8
18	38	-2249	5744	-386	0	-827	-2881	4.02	4.02	4.02	4.02	3	0.38	0.12	0.75	0.00	0.00	16.8
19	38	-2124	5818	459	0	1374	-3068	4.02	4.02	4.02	4.02	3	0.41	0.13	0.76	0.00	0.00	16.8
20	38	-2491	5765	28	0	238	-3019	4.02	4.02	4.02	4.02	3	0.40	0.12	0.75	0.00	0.00	16.8
37	38	-2082	5520	-680	0	-1619	-2863	4.02	4.02	4.02	4.02	3	0.38	0.12	0.72	0.00	0.00	16.8
38	38	-1875	5644	728	0	2048	-3173	4.02	4.02	4.02	4.02	3	0.42	0.12	0.74	0.00	0.00	16.8
39	38	-2486	5556	9	0	155	-3093	4.02	4.02	4.02	4.02	3	0.40	0.12	0.72	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	75	-1601	3998	-3	0	92	2675	4.02	4.02	4.02	4.02	3	0.36	0.09	0.53	0.00	0.00	16.8
2	75	-1287	3028	-139	0	-238	2093	4.02	4.02	4.02	4.02	2	0.30	0.07	0.40	0.00	0.00	16.8
3	75	-1176	3139	-138	0	-236	2020	4.02	4.02	4.02	4.02	2	0.29	0.07	0.42	0.00	0.00	16.8
4	75	-1288	3012	134	0	377	2096	4.02	4.02	4.02	4.02	2	0.30	0.07	0.40	0.00	0.00	16.8
5	75	-1177	3124	135	0	379	2024	4.02	4.02	4.02	4.02	2	0.29	0.07	0.41	0.00	0.00	16.8
6	75	-1418	2892	-45	0	-25	2193	4.02	4.02	4.02	4.02	2	0.32	0.06	0.38	0.00	0.00	16.8
7	75	-1046	3264	-42	0	-18	1897	4.02	4.02	4.02	4.02	2	0.28	0.07	0.43	0.00	0.00	16.8
8	75	-1418	2887	38	0	160	2196	4.02	4.02	4.02	4.02	2	0.32	0.06	0.38	0.00	0.00	16.8
9	75	-1046	3259	40	0	167	1901	4.02	4.02	4.02	4.02	2	0.28	0.07	0.43	0.00	0.00	16.8
10	75	-1287	3028	-139	0	-238	2093	4.02	4.02	4.02	4.02	2	0.30	0.07	0.40	0.00	0.00	16.8
11	75	-1176	3139	-138	0	-236	2020	4.02	4.02	4.02	4.02	2	0.29	0.07	0.42	0.00	0.00	16.8
12	75	-1288	3012	134	0	377	2096	4.02	4.02	4.02	4.02	2	0.30	0.07	0.40	0.00	0.00	16.8
13	75	-1177	3124	135	0	379	2024	4.02	4.02	4.02	4.02	2	0.29	0.07	0.41	0.00	0.00	16.8
14	75	-1418	2892	-45	0	-25	2193	4.02	4.02	4.02	4.02	2	0.32	0.06	0.38	0.00	0.00	16.8
15	75	-1046	3264	-42	0	-18	1897	4.02	4.02	4.02	4.02	2	0.28	0.07	0.43	0.00	0.00	16.8
16	75	-1418	2887	38	0	160	2196	4.02	4.02	4.02	4.02	2	0.32	0.06	0.38	0.00	0.00	16.8
17	75	-1046	3259	40	0	167	1901	4.02	4.02	4.02	4.02	2	0.28	0.07	0.43	0.00	0.00	16.8
18	75	-2249	4060	-386	0	-682	3209	4.02	4.02	4.02	4.02	3	0.42	0.09	0.53	0.00	0.00	16.8
19	75	-2124	4134	459	0	1202	3133	4.02	4.02	4.02	4.02	3	0.41	0.09	0.54	0.00	0.00	16.8
20	75	-2491	4081	28	0	227	3103	4.02	4.02	4.02	4.02	3	0.41	0.09	0.53	0.00	0.00	16.8
37	75	-2082	3916	-680	0	-1364	3012	4.02	4.02	4.02	4.02	3	0.40	0.08	0.51	0.00	0.00	16.8
38	75	-1875	4040	728	0	1775	2898	4.02	4.02	4.02	4.02	3	0.39	0.09	0.53	0.00	0.00	16.8
39	75	-2486	3952	9	0	151	2836	4.02	4.02	4.02	4.02	3	0.37	0.09	0.51	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	112	-1601	2474	-3	0	93	2675	4.02	4.02	4.02	4.02	3	0.36	0.05	0.33	0.00	0.00	16.8
2	112	-1287	1855	-139	0	-186	2093	4.02	4.02	4.02	4.02	2	0.30	0.04	0.25	0.00	0.00	16.8
3	112	-1176	1966	-138	0	-184	2020	4.02	4.02	4.02	4.02	2	0.29	0.04	0.26	0.00	0.00	16.8
4	112	-1288	1839	134	0	327	2096	4.02	4.02	4.02	4.02	2	0.30	0.04	0.24	0.00	0.00	16.8
5	112	-1177	1951	135	0	329	2024	4.02	4.02	4.02	4.02	2	0.29	0.04	0.26	0.00	0.00	16.8
6	112	-1418	1719	-45	0	-8	2193	4.02	4.02	4.02	4.02	2	0.32	0.04	0.23	0.00	0.00	16.8
7	112	-1046	2091	-42	0	-2	1937	4.02	4.02	4.02	4.02	2	0.28	0.05	0.28	0.00	0.00	16.8
8	112	-1418	1715	38	0	146	2196	4.02	4.02	4.02	4.02	2	0.32	0.04	0.23	0.00	0.00	16.8
9	112	-1046	2086	40	0	151	1939	4.02	4.02	4.02	4.02	2	0.28	0.05	0.28	0.00	0.00	16.8
10	112	-1287	1855	-139	0	-186	2093	4.02	4.02	4.02	4.02	2	0.30	0.04	0.25	0.00	0.00	16.8
11	112	-1176	1966	-138	0	-184	2020	4.02	4.02	4.02	4.02	2	0.29	0.04	0.26	0.00	0.00	16.8
12	112	-1288	1839	134	0	327	2096	4.02	4.02	4.02	4.02	2	0.30	0.04	0.24	0.00	0.00	16.8
13	112	-1177	1951	135	0	329	2024	4.02	4.02	4.02	4.02	2	0.29	0.04	0.26	0.00	0.00	16.8
14	112	-1418	1719	-45	0	-8	2193	4.02	4.02	4.02	4.02	2	0.32	0.04	0.23	0.00	0.00	16.8
15	112	-1046	2091	-42	0	-2	1937	4.02	4.02	4.02	4.02	2	0.28	0.05	0.28	0.00	0.00	16.8
16	112	-1418	1715	38	0	146	2196	4.02	4.02	4.02	4.02	2	0.32	0.04	0.23	0.00	0.00	16.8
17	112	-1046	2086	40	0	151	1939	4.02	4.02	4.02	4.02	2	0.28	0.05	0.28	0.00	0.00	16.8
18	112	-2249	2377	-386	0	-537	3209	4.02	4.02	4.02	4.02	3	0.42	0.05	0.31	0.00	0.00	16.8
19	112	-2124	2451	459	0	1029	3133	4.02	4.02	4.02	4.02	3	0.41	0.05	0.32	0.00	0.00	16.8
20	112	-2491	2398	28	0	217	3103	4.02	4.02	4.02	4.02	3	0.41	0.05	0.31	0.00	0.00	16.8
37	112	-2082	2312	-680	0	-1109	3012	4.02	4.02	4.02	4.02	3	0.40	0.05	0.30	0.00	0.00	16.8
38	112	-1875	2436	728	0	1502	2898	4.02	4.02	4.02	4.02	3	0.39	0.05	0.32	0.00	0.00	16.8
39	112	-2486	2348	9	0	148	2836	4.02	4.02	4.02	4.02	3	0.37	0.05	0.30	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	150	-1601	949	-3	0	94	2675	4.02	4.02	4.02	4.02	3	0.36	0.02	0.12	0.00	0.00	16.8
2	150	-1287	682	-139	0	-133	2093	4.02	4.02	4.02	4.02	2	0.30	0.01	0.09	0.00	0.00	16.8
3	150	-1176	793	-138	0	-132	2020	4.02	4.02	4.02	4.02	2	0.29	0.02	0.11	0.00	0.00	16.8
4	150	-1288	666	134	0	277	2096	4.02	4.02	4.02	4.02	2	0.30	0.01	0.09	0.00	0.00	16.8
5	150	-1177	778	135	0	278	2024	4.02	4.02	4.02	4.02	2	0.29	0.02	0.10	0.00	0.00	16.8
6	150	-1418	546	-45	0	8	2193	4.02	4.02	4.02	4.02	2	0.32	0.01	0.07	0.00	0.00	16.8
7	150	-1046	918	-42	0	13	1937	4.02	4.02	4.02	4.02	2	0.28	0.02	0.12	0.00	0.00	16.8
8	150	-1418	542	38	0	131	2196	4.02	4.02	4.02	4.02	2	0.32	0.01	0.07	0.00	0.00	16.8
9	150	-1046	913	40	0	136	1939	4.02	4.02	4.02	4.02	2	0.28	0.02	0.12	0.00	0.00	16.8
10	150	-1287	682	-139	0	-133	2093	4.02	4.02	4.02	4.02	2	0.30	0.01	0.09	0.00	0.00	16.8
11	150	-1176	793	-138	0	-132	2020	4.02	4.02	4.02	4.02	2	0.29	0.02	0.11	0.00	0.00	16.8
12	150	-1288	666	134	0	277	2096	4.02	4.02	4.02	4.02	2	0.30	0.01	0.09	0.00	0.00	16.8
13	150	-1177	778	135	0	278	2024	4.02	4.02	4.02	4.02	2	0.29	0.02	0.10	0.00	0.00	16.8
14	150	-1418	546	-45	0	8	2193	4.02	4.02	4.02	4.02	2	0.32	0.01	0.07	0.00	0.00	16.8
15	150	-1046	918	-42	0	13	1937	4.02	4.02	4.02	4.02	2	0.28	0.02	0.12	0.00	0.00	16.8
16	150	-1418	542	38	0	131	2196	4.02	4.02	4.02	4.02	2	0.32	0.01	0.07	0.00	0.00	16.8
17	150	-1046	913	40	0	136	1939	4.02	4.02	4.02	4.02	2	0.28	0.02	0.12	0.00	0.00	16.8
18	150	-2249	693	-386	0	-393	3209	4.02	4.02	4.02	4.02	3	0.42	0.01	0.09	0.00	0.00	16.8
19	150	-2124	767	459	0	857	3133	4.02	4.02	4.02	4.02	3	0.41	0.02	0.10	0.00	0.00	16.8
20	150	-2491	714	28	0	206	3103	4.02	4.02	4.02	4.02	3	0.41	0.02	0.09	0.00	0.00	16.8
37	150	-2082	708	-680	0	-854	3012	4.02	4.02	4.02	4.02	3	0.40	0.02	0.09	0.00	0.00	16.8
38	150	-1875	832	728	0	1229	2898	4.02	4.02	4.02	4.02	3	0.39	0.02	0.11	0.00	0.00	16.8
39	150	-2486	744	9	0	144	2836	4.02	4.02	4.02	4.02	3	0.37	0.02	0.10	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	188	-1601	-576	-3	0	95	2675	4.02	4.02	4.02	4.02	3	0.36	0.01	0.08	0.00	0.00	16.8
2	188	-1287	-490	-139	0	-81	2093	4.02	4.02	4.02	4.02	2	0.30	0.01	0.06	0.00	0.00	16.8
3	188	-1176	-380	-138	0	-80	2020	4.02	4.02	4.02	4.02	2	0.29	0.01	0.05	0.00	0.00	16.8
4	188	-1288	-506	134	0	226	2096	4.02	4.02	4.02	4.02	2	0.30	0.01	0.07	0.00	0.00	16.8
5	188	-1177	-394	135	0	228	2024	4.02	4.02	4.02	4.02	2	0.29	0.01	0.05	0.00	0.00	16.8

6	188	-1418	-626	-45	0	25	2193	4.02	4.02	4.02	4.02	2	0.32	0.01	0.08	0.00	0.00	16.8
7	188	-1046	-254	-42	0	29	1937	4.02	4.02	4.02	4.02	2	0.28	0.01	0.03	0.00	0.00	16.8
8	188	-1418	-631	38	0	117	2196	4.02	4.02	4.02	4.02	2	0.32	0.01	0.08	0.00	0.00	16.8
9	188	-1046	-260	40	0	121	1939	4.02	4.02	4.02	4.02	2	0.28	0.01	0.03	0.00	0.00	16.8
10	188	-1287	-490	-139	0	-81	2093	4.02	4.02	4.02	4.02	2	0.30	0.01	0.06	0.00	0.00	16.8
11	188	-1176	-380	-138	0	-80	2020	4.02	4.02	4.02	4.02	2	0.29	0.01	0.05	0.00	0.00	16.8
12	188	-1288	-506	134	0	226	2096	4.02	4.02	4.02	4.02	2	0.30	0.01	0.07	0.00	0.00	16.8
13	188	-1177	-394	135	0	228	2024	4.02	4.02	4.02	4.02	2	0.29	0.01	0.05	0.00	0.00	16.8
14	188	-1418	-626	-45	0	25	2193	4.02	4.02	4.02	4.02	2	0.32	0.01	0.08	0.00	0.00	16.8
15	188	-1046	-254	-42	0	29	1937	4.02	4.02	4.02	4.02	2	0.28	0.01	0.03	0.00	0.00	16.8
16	188	-1418	-631	38	0	117	2196	4.02	4.02	4.02	4.02	2	0.32	0.01	0.08	0.00	0.00	16.8
17	188	-1046	-260	40	0	121	1939	4.02	4.02	4.02	4.02	2	0.28	0.01	0.03	0.00	0.00	16.8
18	188	-2249	-991	-386	0	-248	3209	4.02	4.02	4.02	4.02	3	0.42	0.02	0.13	0.00	0.00	16.8
19	188	-2124	-916	459	0	685	3133	4.02	4.02	4.02	4.02	3	0.41	0.02	0.12	0.00	0.00	16.8
20	188	-2491	-969	28	0	196	3103	4.02	4.02	4.02	4.02	3	0.41	0.02	0.13	0.00	0.00	16.8
37	188	-2082	-896	-680	0	-599	3012	4.02	4.02	4.02	4.02	3	0.40	0.02	0.12	0.00	0.00	16.8
38	188	-1875	-772	728	0	956	2898	4.02	4.02	4.02	4.02	3	0.39	0.02	0.10	0.00	0.00	16.8
39	188	-2486	-860	9	0	141	2836	4.02	4.02	4.02	4.02	3	0.37	0.02	0.11	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	225	-1601	-2100	-3	0	96	2675	4.02	4.02	4.02	4.02	3	0.36	0.05	0.28	0.00	0.00	16.8
2	225	-1287	-1663	-139	0	-29	2093	4.02	4.02	4.02	4.02	2	0.30	0.04	0.22	0.00	0.00	16.8
3	225	-1176	-1552	-138	0	-28	2020	4.02	4.02	4.02	4.02	2	0.29	0.03	0.21	0.00	0.00	16.8
4	225	-1288	-1679	134	0	176	2096	4.02	4.02	4.02	4.02	2	0.30	0.04	0.22	0.00	0.00	16.8
5	225	-1177	-1567	135	0	177	2024	4.02	4.02	4.02	4.02	2	0.29	0.03	0.21	0.00	0.00	16.8
6	225	-1418	-1799	-45	0	42	2193	4.02	4.02	4.02	4.02	2	0.32	0.04	0.24	0.00	0.00	16.8
7	225	-1046	-1427	-42	0	45	1937	4.02	4.02	4.02	4.02	2	0.28	0.03	0.19	0.00	0.00	16.8
8	225	-1418	-1804	38	0	103	2196	4.02	4.02	4.02	4.02	2	0.32	0.04	0.24	0.00	0.00	16.8
9	225	-1046	-1432	40	0	106	1939	4.02	4.02	4.02	4.02	2	0.28	0.03	0.19	0.00	0.00	16.8
10	225	-1287	-1663	-139	0	-29	2093	4.02	4.02	4.02	4.02	2	0.30	0.04	0.22	0.00	0.00	16.8
11	225	-1176	-1552	-138	0	-28	2020	4.02	4.02	4.02	4.02	2	0.29	0.03	0.21	0.00	0.00	16.8
12	225	-1288	-1679	134	0	176	2096	4.02	4.02	4.02	4.02	2	0.30	0.04	0.22	0.00	0.00	16.8
13	225	-1177	-1567	135	0	177	2024	4.02	4.02	4.02	4.02	2	0.29	0.03	0.21	0.00	0.00	16.8
14	225	-1418	-1799	-45	0	42	2193	4.02	4.02	4.02	4.02	2	0.32	0.04	0.24	0.00	0.00	16.8
15	225	-1046	-1427	-42	0	45	1937	4.02	4.02	4.02	4.02	2	0.28	0.03	0.19	0.00	0.00	16.8
16	225	-1418	-1804	38	0	103	2196	4.02	4.02	4.02	4.02	2	0.32	0.04	0.24	0.00	0.00	16.8
17	225	-1046	-1432	40	0	106	1939	4.02	4.02	4.02	4.02	2	0.28	0.03	0.19	0.00	0.00	16.8
18	225	-2249	-2674	-386	0	-103	3209	4.02	4.02	4.02	4.02	3	0.42	0.06	0.35	0.00	0.00	16.8
19	225	-2124	-2599	459	0	513	3133	4.02	4.02	4.02	4.02	3	0.41	0.06	0.34	0.00	0.00	16.8
20	225	-2491	-2652	28	0	185	3103	4.02	4.02	4.02	4.02	3	0.41	0.06	0.34	0.00	0.00	16.8
37	225	-2082	-2500	-680	0	-344	3012	4.02	4.02	4.02	4.02	3	0.40	0.05	0.33	0.00	0.00	16.8
38	225	-1875	-2376	728	0	683	2898	4.02	4.02	4.02	4.02	3	0.39	0.05	0.31	0.00	0.00	16.8
39	225	-2486	-2464	9	0	137	2836	4.02	4.02	4.02	4.02	3	0.37	0.05	0.32	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	262	-1601	-3625	-3	0	97	2675	4.02	4.02	4.02	4.02	3	0.36	0.08	0.48	0.00	0.00	16.8
2	262	-1287	-2836	-139	0	23	2093	4.02	4.02	4.02	4.02	2	0.30	0.06	0.38	0.00	0.00	16.8
3	262	-1176	-2725	-138	0	24	2020	4.02	4.02	4.02	4.02	2	0.29	0.06	0.36	0.00	0.00	16.8
4	262	-1288	-2852	134	0	126	2096	4.02	4.02	4.02	4.02	2	0.30	0.06	0.38	0.00	0.00	16.8
5	262	-1177	-2740	135	0	126	2024	4.02	4.02	4.02	4.02	2	0.29	0.06	0.36	0.00	0.00	16.8
6	262	-1418	-2972	-45	0	59	2193	4.02	4.02	4.02	4.02	2	0.32	0.06	0.39	0.00	0.00	16.8
7	262	-1046	-2600	-42	0	60	1937	4.02	4.02	4.02	4.02	2	0.28	0.06	0.35	0.00	0.00	16.8
8	262	-1418	-2977	38	0	89	2196	4.02	4.02	4.02	4.02	2	0.32	0.06	0.39	0.00	0.00	16.8
9	262	-1046	-2605	40	0	91	1939	4.02	4.02	4.02	4.02	2	0.28	0.06	0.35	0.00	0.00	16.8
10	262	-1287	-2836	-139	0	23	2093	4.02	4.02	4.02	4.02	2	0.30	0.06	0.38	0.00	0.00	16.8
11	262	-1176	-2725	-138	0	24	2020	4.02	4.02	4.02	4.02	2	0.29	0.06	0.36	0.00	0.00	16.8
12	262	-1288	-2852	134	0	126	2096	4.02	4.02	4.02	4.02	2	0.30	0.06	0.38	0.00	0.00	16.8
13	262	-1177	-2740	135	0	126	2024	4.02	4.02	4.02	4.02	2	0.29	0.06	0.36	0.00	0.00	16.8
14	262	-1418	-2972	-45	0	59	2193	4.02	4.02	4.02	4.02	2	0.32	0.06	0.39	0.00	0.00	16.8
15	262	-1046	-2600	-42	0	60	1937	4.02	4.02	4.02	4.02	2	0.28	0.06	0.35	0.00	0.00	16.8
16	262	-1418	-2977	38	0	89	2196	4.02	4.02	4.02	4.02	2	0.32	0.06	0.39	0.00	0.00	16.8
17	262	-1046	-2605	40	0	91	1939	4.02	4.02	4.02	4.02	2	0.28	0.06	0.35	0.00	0.00	16.8
18	262	-2249	-4358	-386	0	41	3209	4.02	4.02	4.02	4.02	3	0.42	0.09	0.57	0.00	0.00	16.8
19	262	-2124	-4283	459	0	340	3133	4.02	4.02	4.02	4.02	3	0.41	0.09	0.56	0.00	0.00	16.8
20	262	-2491	-4336	28	0	175	3103	4.02	4.02	4.02	4.02	3	0.41	0.09	0.56	0.00	0.00	16.8
37	262	-2082	-4104	-680	0	-89	3012	4.02	4.02	4.02	4.02	3	0.40	0.09	0.54	0.00	0.00	16.8
38	262	-1875	-3980	728	0	409	2898	4.02	4.02	4.02	4.02	3	0.39	0.09	0.52	0.00	0.00	16.8
39	262	-2486	-4068	9	0	134	2836	4.02	4.02	4.02	4.02	3	0.37	0.09	0.53	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	300	-1601	-5149	-3	0	98	-3151	4.02	4.02	4.02	4.02	3	0.42	0.11	0.68	0.00	0.00	16.8
2	300	-1287	-4009	-139	0	76	-2468	4.02	4.02	4.02	4.02	2	0.36	0.09	0.53	0.00	0.00	16.8
3	300	-1176	-3898	-138	0	76	-2359	4.02	4.02	4.02	4.02	2	0.34	0.08	0.52	0.00	0.00	16.8
4	300	-1288	-4025	134	0	75	-2490	4.02	4.02	4.02	4.02	2	0.36	0.09	0.53	0.00	0.00	16.8
5	300	-1177	-3913	135	0	76	-2380	4.02	4.02	4.02	4.02	2	0.34	0.08	0.52	0.00	0.00	16.8
6	300	-1418	-4145	-45	0	75	-2604	4.02	4.02	4.02	4.02	2	0.37	0.09	0.55	0.00	0.00	16.8
7	300	-1046	-3773	-42	0	76	-2238	4.02	4.02	4.02	4.02	2	0.33	0.08	0.50	0.00	0.00	16.8
8	300	-1418	-4149	38	0	75	-2610	4.02	4.02	4.02	4.02	2	0.38	0.09	0.55	0.00	0.00	16.8
9	300	-1046	-3778	40	0	76	-2244	4.02	4.02	4.02	4.02	2	0.33	0.08	0.50	0.00	0.00	16.8
10	300	-1287	-4009	-139	0	76	-2468	4.02	4.02	4.02	4.02	2	0.36	0.09	0.53	0.00	0.00	16.8
11	300	-1176	-3898	-138	0	76	-2359	4.02	4.02	4.02	4.02	2	0.34	0.08	0.52	0.00	0.00	16.8
12	300	-1288	-4025	134	0	75	-2490	4.02	4.02	4.02	4.02	2	0.36	0.09	0.53	0.00	0.00	16.8
13	300	-1177	-3913	135	0	76	-2380	4.02	4.02	4.02	4.02	2	0.34	0.08	0.52	0.00	0.00	16.8
14	300	-1418	-4145	-45	0	75	-2604	4.02	4.02	4.02	4.02	2	0.37	0.09	0.55	0.00	0.00	16.8
15	300	-1046	-3773	-42	0	76	-2238	4.02	4.02	4.02	4.02	2	0.33	0.08	0.50	0.00	0.00	16.8
16	300	-1418	-4149	38	0	75	-2610	4.02	4.02	4.02	4.02	2	0.38	0.09	0.55	0.00	0.00	16.8
17	300	-1046	-3778	40	0	76	-2244	4.02	4.02	4.02	4.02	2	0.33	0.08	0.50	0.00	0.00	16.8
18	300	-2249	-6041	-386	0	186	-3860	4.02	4.02	4.02	4.02	3	0.51	0.13	0.79	0.00	0.00	16.8
19	300	-2124	-5966	459	0	168	-3786	4.02	4.02	4.02	4.02	3	0.50	0.13	0.78	0.00	0.00	16.8
20	300	-2491	-6019	28	0	164	-3922	4.02	4.02	4.02	4.02	3	0.51	0.13	0.78	0.00	0.00	16.8
37	300	-2082	-5708	-680	0	166	-3627	4.02	4.02	4.02	4.02	3	0.48	0.12	0.75	0.00	0.00	16.8
38	300	-1875	-5584	728	0	136	-3504	4.02	4.02	4.02	4.02	3	0.47	0.12	0.73	0.00	0.00	16.8
39	300	-2486	-5672	9	0	131	-3731	4.02	4.02	4.02	4.02	3	0.49	0.12	0.74	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	338	-1601	-6674	-3	0	99	-5550	4.02	4.02	4.02	4.02	3	0.74	0.14	0.88	0.00	0.00	16.8
2	338	-1287	-5181	-139	0	128	-4325	4.02	4.02	4.02	4.02	2	0.62	0.11	0.69	0.00	0.00	16.8
3	338	-1176	-5070	-138	0	128	-4188	4.02	4.02	4.02	4.02	2	0.61	0.11	0.67	0.00	0.00	16.8
4	338	-1288	-5197	134	0	25	-4350	4.02	4.02	4.02	4.02	2	0.63	0.11	0.69	0.00	0.00	16.8
5	338	-1177	-5085	135	0	25	-4213	4.02	4.02	4.02	4.02	2	0.61	0.11	0.67	0.00	0.00	16.8
6	338	-1418	-5317	-45	0	92	-4494	4.02	4.02	4.02	4.02	2	0.65	0.12	0.70	0.00	0.00	16.8
7	338	-1046	-4945	-42	0	92	-4037	4.02	4.02	4.02	4.02	2	0.59	0.11	0.66	0.00	0.00	16.8
8	338	-1418	-5322	38	0	61	-4501	4.02	4.02	4.02	4.02	2	0.65	0.12	0.70	0.00	0.00	16.8
9	338	-1046	-4950	40	0	61	-4044	4.02	4.02	4.02	4.02	2	0.59	0.11	0.66	0.00	0.00	16.8
10	338	-1287	-5181	-139	0	128	-4325	4.02	4.02	4.02	4.02	2	0.62	0.11	0.69	0.00	0.00	16.8
11	338	-1176	-5070	-138	0	128	-4188	4.02	4.02	4.02	4.02	2	0.61	0.11	0.67	0.00	0.00	16.8

12	338	-1288	-5197	134	0	25	-4350	4.02	4.02	4.02	4.02	2	0.63	0.11	0.69	0.00	0.00	16.8
13	338	-1177	-5085	135	0	25	-4213	4.02	4.02	4.02	4.02	2	0.61	0.11	0.67	0.00	0.00	16.8
14	338	-1418	-5317	-45	0	92	-4494	4.02	4.02	4.02	4.02	2	0.65	0.12	0.70	0.00	0.00	16.8
15	338	-1046	-4945	-42	0	92	-4037	4.02	4.02	4.02	4.02	2	0.59	0.11	0.66	0.00	0.00	16.8
16	338	-1418	-5322	38	0	61	-4501	4.02	4.02	4.02	4.02	2	0.65	0.12	0.70	0.00	0.00	16.8
17	338	-1046	-4950	40	0	61	-4044	4.02	4.02	4.02	4.02	2	0.59	0.11	0.66	0.00	0.00	16.8
18	338	-2249	-7724	-386	0	331	-6595	4.02	4.02	4.02	4.02	3	0.87	0.17	1.01	1.92	0.00	16.8
19	338	-2124	-7650	459	0	-4	-6503	4.02	4.02	4.02	4.02	3	0.86	0.17	1.00	0.00	0.00	16.8
20	338	-2491	-7703	28	0	154	-6652	4.02	4.02	4.02	4.02	3	0.87	0.17	1.00	0.00	0.00	16.8
37	338	-2082	-7312	-680	0	421	-6221	4.02	4.02	4.02	4.02	3	0.82	0.16	0.95	0.00	0.00	16.8
38	338	-1875	-7188	728	0	-137	-6068	4.02	4.02	4.02	4.02	3	0.81	0.16	0.94	0.00	0.00	16.8
39	338	-2486	-7276	9	0	127	-6316	4.02	4.02	4.02	4.02	3	0.83	0.16	0.94	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	375	-1601	-8198	-3	0	100	-5550	4.02	4.02	4.02	4.02	3	0.74	0.18	1.08	2.03	0.00	16.8
2	375	-1287	-6354	-139	0	180	-4325	4.02	4.02	4.02	4.02	2	0.62	0.14	0.84	0.00	0.00	16.8
3	375	-1176	-6243	-138	0	180	-4188	4.02	4.02	4.02	4.02	2	0.61	0.14	0.83	0.00	0.00	16.8
4	375	-1288	-6370	134	0	-25	-4350	4.02	4.02	4.02	4.02	2	0.63	0.14	0.84	0.00	0.00	16.8
5	375	-1177	-6258	135	0	-26	-4213	4.02	4.02	4.02	4.02	2	0.61	0.14	0.83	0.00	0.00	16.8
6	375	-1418	-6490	-45	0	109	-4494	4.02	4.02	4.02	4.02	2	0.65	0.14	0.86	0.00	0.00	16.8
7	375	-1046	-6118	-42	0	107	-4037	4.02	4.02	4.02	4.02	2	0.59	0.13	0.81	0.00	0.00	16.8
8	375	-1418	-6495	38	0	47	-4501	4.02	4.02	4.02	4.02	2	0.65	0.14	0.86	0.00	0.00	16.8
9	375	-1046	-6123	40	0	46	-4044	4.02	4.02	4.02	4.02	2	0.59	0.13	0.81	0.00	0.00	16.8
10	375	-1287	-6354	-139	0	180	-4325	4.02	4.02	4.02	4.02	2	0.62	0.14	0.84	0.00	0.00	16.8
11	375	-1176	-6243	-138	0	180	-4188	4.02	4.02	4.02	4.02	2	0.61	0.14	0.83	0.00	0.00	16.8
12	375	-1288	-6370	134	0	-25	-4350	4.02	4.02	4.02	4.02	2	0.63	0.14	0.84	0.00	0.00	16.8
13	375	-1177	-6258	135	0	-26	-4213	4.02	4.02	4.02	4.02	2	0.61	0.14	0.83	0.00	0.00	16.8
14	375	-1418	-6490	-45	0	109	-4494	4.02	4.02	4.02	4.02	2	0.65	0.14	0.86	0.00	0.00	16.8
15	375	-1046	-6118	-42	0	107	-4037	4.02	4.02	4.02	4.02	2	0.59	0.13	0.81	0.00	0.00	16.8
16	375	-1418	-6495	38	0	47	-4501	4.02	4.02	4.02	4.02	2	0.65	0.14	0.86	0.00	0.00	16.8
17	375	-1046	-6123	40	0	46	-4044	4.02	4.02	4.02	4.02	2	0.59	0.13	0.81	0.00	0.00	16.8
18	375	-2249	-9408	-386	0	475	-6595	4.02	4.02	4.02	4.02	3	0.87	0.20	1.22	2.33	0.00	16.8
19	375	-2124	-9333	459	0	-176	-6503	4.02	4.02	4.02	4.02	3	0.86	0.20	1.22	2.31	0.00	16.8
20	375	-2491	-9386	28	0	144	-6652	4.02	4.02	4.02	4.02	3	0.87	0.20	1.22	2.33	0.00	16.8
37	375	-2082	-8916	-680	0	676	-6221	4.02	4.02	4.02	4.02	3	0.82	0.19	1.16	2.21	0.00	16.8
38	375	-1875	-8792	728	0	-410	-6068	4.02	4.02	4.02	4.02	3	0.81	0.19	1.15	2.18	0.00	16.8
39	375	-2486	-8880	9	0	124	-6316	4.02	4.02	4.02	4.02	3	0.83	0.19	1.15	2.20	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

Nome travata: **trave_505_IP1** Descrizione: **Trave_5 16-15-14-13**
ASTA NUM. 15 NI 125 NF 212 SEZ. Rp B= 0.400 H= 0.500 (trave)

categoria: p.p. y Permanente Neve qy tot.
qy medio: 500.00 2627.25 282.50 3409.75 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-1241	7984	16	0	68	-4781	4.02	4.02	4.02	4.02	3	0.65	0.17	1.06	1.98	0.00	16.8
2	0	-979	6126	-48	0	24	-3657	4.02	4.02	4.02	4.02	2	0.53	0.13	0.82	0.00	0.00	16.8
3	0	-939	6157	-47	0	25	-3696	4.02	4.02	4.02	4.02	2	0.54	0.13	0.82	0.00	0.00	16.8
4	0	-970	6126	72	0	80	-3658	4.02	4.02	4.02	4.02	2	0.53	0.13	0.82	0.00	0.00	16.8
5	0	-931	6157	72	0	81	-3698	4.02	4.02	4.02	4.02	2	0.54	0.13	0.82	0.00	0.00	16.8
6	0	-1022	6090	-6	0	44	-3611	4.02	4.02	4.02	4.02	2	0.53	0.13	0.81	0.00	0.00	16.8
7	0	-889	6193	-5	0	45	-3743	4.02	4.02	4.02	4.02	2	0.55	0.13	0.83	0.00	0.00	16.8
8	0	-1020	6090	30	0	60	-3612	4.02	4.02	4.02	4.02	2	0.53	0.13	0.81	0.00	0.00	16.8
9	0	-887	6192	30	0	61	-3744	4.02	4.02	4.02	4.02	2	0.55	0.13	0.83	0.00	0.00	16.8
10	0	-979	6126	-48	0	24	-3657	4.02	4.02	4.02	4.02	2	0.53	0.13	0.82	0.00	0.00	16.8
11	0	-939	6157	-47	0	25	-3696	4.02	4.02	4.02	4.02	2	0.54	0.13	0.82	0.00	0.00	16.8
12	0	-970	6126	72	0	80	-3658	4.02	4.02	4.02	4.02	2	0.53	0.13	0.82	0.00	0.00	16.8
13	0	-931	6157	72	0	81	-3698	4.02	4.02	4.02	4.02	2	0.54	0.13	0.82	0.00	0.00	16.8
14	0	-1022	6090	-6	0	44	-3611	4.02	4.02	4.02	4.02	2	0.53	0.13	0.81	0.00	0.00	16.8
15	0	-889	6193	-5	0	45	-3743	4.02	4.02	4.02	4.02	2	0.55	0.13	0.83	0.00	0.00	16.8
16	0	-1020	6090	30	0	60	-3612	4.02	4.02	4.02	4.02	2	0.53	0.13	0.81	0.00	0.00	16.8
17	0	-887	6192	30	0	61	-3744	4.02	4.02	4.02	4.02	2	0.55	0.13	0.83	0.00	0.00	16.8
18	0	-1583	8687	-144	0	42	-5096	4.02	4.02	4.02	4.02	3	0.68	0.19	1.14	2.15	0.00	16.8
19	0	-1512	8715	218	0	196	-5135	4.02	4.02	4.02	4.02	3	0.69	0.19	1.15	2.16	0.00	16.8
20	0	-1692	8573	33	0	111	-4880	4.02	4.02	4.02	4.02	3	0.65	0.19	1.13	2.13	0.00	16.8
37	0	-1487	8298	-271	0	-26	-4887	4.02	4.02	4.02	4.02	3	0.66	0.18	1.10	2.06	0.00	16.8
38	0	-1369	8345	332	0	232	-4953	4.02	4.02	4.02	4.02	3	0.67	0.18	1.10	2.07	0.00	16.8
39	0	-1668	8108	23	0	89	-4528	4.02	4.02	4.02	4.02	3	0.61	0.18	1.07	2.01	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	38	-1241	6459	16	0	62	-4781	4.02	4.02	4.02	4.02	3	0.65	0.14	0.86	0.00	0.00	16.8
2	38	-979	4953	-48	0	42	-3657	4.02	4.02	4.02	4.02	2	0.53	0.11	0.66	0.00	0.00	16.8
3	38	-939	4984	-47	0	42	-3696	4.02	4.02	4.02	4.02	2	0.54	0.11	0.66	0.00	0.00	16.8
4	38	-970	4953	72	0	54	-3658	4.02	4.02	4.02	4.02	2	0.53	0.11	0.66	0.00	0.00	16.8
5	38	-931	4984	72	0	54	-3698	4.02	4.02	4.02	4.02	2	0.54	0.11	0.66	0.00	0.00	16.8
6	38	-1022	4917	-6	0	46	-3611	4.02	4.02	4.02	4.02	2	0.53	0.11	0.65	0.00	0.00	16.8
7	38	-889	5020	-5	0	47	-3743	4.02	4.02	4.02	4.02	2	0.55	0.11	0.67	0.00	0.00	16.8
8	38	-1020	4917	30	0	49	-3612	4.02	4.02	4.02	4.02	2	0.53	0.11	0.65	0.00	0.00	16.8
9	38	-887	5019	30	0	50	-3744	4.02	4.02	4.02	4.02	2	0.55	0.11	0.67	0.00	0.00	16.8
10	38	-979	4953	-48	0	42	-3657	4.02	4.02	4.02	4.02	2	0.53	0.11	0.66	0.00	0.00	16.8
11	38	-939	4984	-47	0	42	-3696	4.02	4.02	4.02	4.02	2	0.54	0.11	0.66	0.00	0.00	16.8
12	38	-970	4953	72	0	54	-3658	4.02	4.02	4.02	4.02	2	0.53	0.11	0.66	0.00	0.00	16.8
13	38	-931	4984	72	0	54	-3698	4.02	4.02	4.02	4.02	2	0.54	0.11	0.66	0.00	0.00	16.8
14	38	-1022	4917	-6	0	46	-3611	4.02	4.02	4.02	4.02	2	0.53	0.11	0.65	0.00	0.00	16.8
15	38	-889	5020	-5	0	47	-3743	4.02	4.02	4.02	4.02	2	0.55	0.11	0.67	0.00	0.00	16.8
16	38	-1020	4917	30	0	49	-3612	4.02	4.02	4.02	4.02	2	0.53	0.11	0.65	0.00	0.00	16.8
17	38	-887	5019	30	0	50	-3744	4.02	4.02	4.02	4.02	2	0.55	0.11	0.67	0.00	0.00	16.8
18	38	-1583	7004	-144	0	96	-5096	4.02	4.02	4.02	4.02	3	0.68	0.15	0.92	0.00	0.00	16.8
19	38	-1512	7032	218	0	115	-5135	4.02	4.02	4.02	4.02	3	0.69	0.15	0.93	0.00	0.00	16.8
20	38	-1692	6890	33	0	98	-4880	4.02	4.02	4.02	4.02	3	0.65	0.15	0.91	0.00	0.00	16.8
37	38	-1487	6694	-271	0	75	-4887	4.02	4.02	4.02	4.02	3	0.66	0.14	0.88	0.00	0.00	16.8
38	38	-1369	6741	332	0	107	-4953	4.02	4.02	4.02	4.02	3	0.67	0.15	0.89	0.00	0.00	16.8
39	38	-1668	6504	23	0	80	-4528	4.02	4.02	4.02	4.02	3	0.61	0.14	0.86	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	75	-1241	4935	16	0	57	2562	4.02	4.02	4.02	4.02	3	0.35	0.11	0.65	0.00	0.00	16.8
2	75	-979	3781	-48	0	60	1972	4.02	4.02	4.02	4.02	2	0.29	0.08	0.50	0.00	0.00	16.8
3	75	-939	3812	-47	0	60	1972	4.02	4.02	4.02	4.02	2	0.29	0.08	0.51	0.00	0.00	16.8

4	75	-970	3781	72	0	27	1971	4.02	4.02	4.02	4.02	2	0.29	0.08	0.50	0.00	0.00	16.8
5	75	-931	3811	72	0	27	1969	4.02	4.02	4.02	4.02	2	0.29	0.08	0.51	0.00	0.00	16.8
6	75	-1022	3745	-6	0	48	1973	4.02	4.02	4.02	4.02	2	0.29	0.08	0.50	0.00	0.00	16.8
7	75	-889	3847	-5	0	49	1970	4.02	4.02	4.02	4.02	2	0.29	0.08	0.51	0.00	0.00	16.8
8	75	-1020	3745	30	0	38	1972	4.02	4.02	4.02	4.02	2	0.29	0.08	0.50	0.00	0.00	16.8
9	75	-887	3847	30	0	39	1968	4.02	4.02	4.02	4.02	2	0.29	0.08	0.51	0.00	0.00	16.8
10	75	-979	3781	-48	0	60	1972	4.02	4.02	4.02	4.02	2	0.29	0.08	0.50	0.00	0.00	16.8
11	75	-939	3812	-47	0	60	1972	4.02	4.02	4.02	4.02	2	0.29	0.08	0.51	0.00	0.00	16.8
12	75	-970	3781	72	0	27	1971	4.02	4.02	4.02	4.02	2	0.29	0.08	0.50	0.00	0.00	16.8
13	75	-931	3811	72	0	27	1969	4.02	4.02	4.02	4.02	2	0.29	0.08	0.51	0.00	0.00	16.8
14	75	-1022	3745	-6	0	48	1973	4.02	4.02	4.02	4.02	2	0.29	0.08	0.50	0.00	0.00	16.8
15	75	-889	3847	-5	0	49	1970	4.02	4.02	4.02	4.02	2	0.29	0.08	0.51	0.00	0.00	16.8
16	75	-1020	3745	30	0	38	1972	4.02	4.02	4.02	4.02	2	0.29	0.08	0.50	0.00	0.00	16.8
17	75	-887	3847	30	0	39	1968	4.02	4.02	4.02	4.02	2	0.29	0.08	0.51	0.00	0.00	16.8
18	75	-1583	5320	-144	0	150	2850	4.02	4.02	4.02	4.02	3	0.38	0.12	0.70	0.00	0.00	16.8
19	75	-1512	5348	218	0	33	2846	4.02	4.02	4.02	4.02	3	0.38	0.12	0.71	0.00	0.00	16.8
20	75	-1692	5206	33	0	86	2922	4.02	4.02	4.02	4.02	3	0.39	0.11	0.68	0.00	0.00	16.8
37	75	-1487	5090	-271	0	177	2710	4.02	4.02	4.02	4.02	3	0.36	0.11	0.67	0.00	0.00	16.8
38	75	-1369	5137	332	0	-18	2703	4.02	4.02	4.02	4.02	3	0.36	0.11	0.68	0.00	0.00	16.8
39	75	-1668	4900	23	0	71	2830	4.02	4.02	4.02	4.02	3	0.38	0.11	0.64	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	112	-1241	3410	16	0	51	3043	4.02	4.02	4.02	4.02	3	0.41	0.07	0.45	0.00	0.00	16.8
2	112	-979	2608	-48	0	78	2333	4.02	4.02	4.02	4.02	2	0.34	0.06	0.35	0.00	0.00	16.8
3	112	-939	2639	-47	0	78	2351	4.02	4.02	4.02	4.02	2	0.34	0.06	0.35	0.00	0.00	16.8
4	112	-970	2608	72	0	-0	2331	4.02	4.02	4.02	4.02	2	0.34	0.06	0.35	0.00	0.00	16.8
5	112	-931	2639	72	0	0	2349	4.02	4.02	4.02	4.02	2	0.34	0.06	0.35	0.00	0.00	16.8
6	112	-1022	2572	-6	0	50	2311	4.02	4.02	4.02	4.02	2	0.34	0.06	0.34	0.00	0.00	16.8
7	112	-889	2675	-5	0	51	2371	4.02	4.02	4.02	4.02	2	0.35	0.06	0.36	0.00	0.00	16.8
8	112	-1020	2572	30	0	27	2310	4.02	4.02	4.02	4.02	2	0.34	0.06	0.34	0.00	0.00	16.8
9	112	-887	2674	30	0	27	2370	4.02	4.02	4.02	4.02	2	0.35	0.06	0.36	0.00	0.00	16.8
10	112	-979	2608	-48	0	78	2333	4.02	4.02	4.02	4.02	2	0.34	0.06	0.35	0.00	0.00	16.8
11	112	-939	2639	-47	0	78	2351	4.02	4.02	4.02	4.02	2	0.34	0.06	0.35	0.00	0.00	16.8
12	112	-970	2608	72	0	-0	2331	4.02	4.02	4.02	4.02	2	0.34	0.06	0.35	0.00	0.00	16.8
13	112	-931	2639	72	0	0	2349	4.02	4.02	4.02	4.02	2	0.34	0.06	0.35	0.00	0.00	16.8
14	112	-1022	2572	-6	0	50	2311	4.02	4.02	4.02	4.02	2	0.34	0.06	0.34	0.00	0.00	16.8
15	112	-889	2675	-5	0	51	2371	4.02	4.02	4.02	4.02	2	0.35	0.06	0.36	0.00	0.00	16.8
16	112	-1020	2572	30	0	27	2310	4.02	4.02	4.02	4.02	2	0.34	0.06	0.34	0.00	0.00	16.8
17	112	-887	2674	30	0	27	2370	4.02	4.02	4.02	4.02	2	0.35	0.06	0.36	0.00	0.00	16.8
18	112	-1583	3636	-144	0	203	3301	4.02	4.02	4.02	4.02	3	0.44	0.08	0.48	0.00	0.00	16.8
19	112	-1512	3664	218	0	-49	3314	4.02	4.02	4.02	4.02	3	0.45	0.08	0.48	0.00	0.00	16.8
20	112	-1692	3523	33	0	74	3302	4.02	4.02	4.02	4.02	3	0.44	0.08	0.46	0.00	0.00	16.8
37	112	-1487	3486	-271	0	279	3153	4.02	4.02	4.02	4.02	3	0.42	0.08	0.46	0.00	0.00	16.8
38	112	-1369	3533	332	0	-142	3175	4.02	4.02	4.02	4.02	3	0.43	0.08	0.47	0.00	0.00	16.8
39	112	-1668	3296	23	0	62	3155	4.02	4.02	4.02	4.02	3	0.42	0.07	0.43	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	150	-1241	1886	16	0	45	3043	4.02	4.02	4.02	4.02	3	0.41	0.04	0.25	0.00	0.00	16.8
2	150	-979	1435	-48	0	96	2333	4.02	4.02	4.02	4.02	2	0.34	0.03	0.19	0.00	0.00	16.8
3	150	-939	1466	-47	0	96	2351	4.02	4.02	4.02	4.02	2	0.34	0.03	0.20	0.00	0.00	16.8
4	150	-970	1435	72	0	-27	2331	4.02	4.02	4.02	4.02	2	0.34	0.03	0.19	0.00	0.00	16.8
5	150	-931	1466	72	0	-27	2349	4.02	4.02	4.02	4.02	2	0.34	0.03	0.20	0.00	0.00	16.8
6	150	-1022	1399	-6	0	53	2311	4.02	4.02	4.02	4.02	2	0.34	0.03	0.19	0.00	0.00	16.8
7	150	-889	1502	-5	0	53	2371	4.02	4.02	4.02	4.02	2	0.35	0.03	0.20	0.00	0.00	16.8
8	150	-1020	1399	30	0	16	2310	4.02	4.02	4.02	4.02	2	0.34	0.03	0.19	0.00	0.00	16.8
9	150	-887	1501	30	0	16	2370	4.02	4.02	4.02	4.02	2	0.35	0.03	0.20	0.00	0.00	16.8
10	150	-979	1435	-48	0	96	2333	4.02	4.02	4.02	4.02	2	0.34	0.03	0.19	0.00	0.00	16.8
11	150	-939	1466	-47	0	96	2351	4.02	4.02	4.02	4.02	2	0.34	0.03	0.20	0.00	0.00	16.8
12	150	-970	1435	72	0	-27	2331	4.02	4.02	4.02	4.02	2	0.34	0.03	0.19	0.00	0.00	16.8
13	150	-931	1466	72	0	-27	2349	4.02	4.02	4.02	4.02	2	0.34	0.03	0.20	0.00	0.00	16.8
14	150	-1022	1399	-6	0	53	2311	4.02	4.02	4.02	4.02	2	0.34	0.03	0.19	0.00	0.00	16.8
15	150	-889	1502	-5	0	53	2371	4.02	4.02	4.02	4.02	2	0.35	0.03	0.20	0.00	0.00	16.8
16	150	-1020	1399	30	0	16	2310	4.02	4.02	4.02	4.02	2	0.34	0.03	0.19	0.00	0.00	16.8
17	150	-887	1501	30	0	16	2370	4.02	4.02	4.02	4.02	2	0.35	0.03	0.20	0.00	0.00	16.8
18	150	-1583	1953	-144	0	257	3301	4.02	4.02	4.02	4.02	3	0.44	0.04	0.26	0.00	0.00	16.8
19	150	-1512	1981	218	0	-131	3314	4.02	4.02	4.02	4.02	3	0.45	0.04	0.26	0.00	0.00	16.8
20	150	-1692	1839	33	0	61	3302	4.02	4.02	4.02	4.02	3	0.44	0.04	0.24	0.00	0.00	16.8
37	150	-1487	1882	-271	0	381	3153	4.02	4.02	4.02	4.02	3	0.42	0.04	0.25	0.00	0.00	16.8
38	150	-1369	1929	332	0	-267	3175	4.02	4.02	4.02	4.02	3	0.43	0.04	0.26	0.00	0.00	16.8
39	150	-1668	1692	23	0	54	3155	4.02	4.02	4.02	4.02	3	0.42	0.04	0.22	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	188	-1241	361	16	0	39	3043	4.02	4.02	4.02	4.02	3	0.41	0.01	0.05	0.00	0.00	16.8
2	188	-979	262	-48	0	114	2333	4.02	4.02	4.02	4.02	2	0.34	0.01	0.03	0.00	0.00	16.8
3	188	-939	294	-47	0	114	2351	4.02	4.02	4.02	4.02	2	0.34	0.01	0.04	0.00	0.00	16.8
4	188	-970	262	72	0	-54	2331	4.02	4.02	4.02	4.02	2	0.34	0.01	0.03	0.00	0.00	16.8
5	188	-931	293	72	0	-54	2349	4.02	4.02	4.02	4.02	2	0.34	0.01	0.04	0.00	0.00	16.8
6	188	-1022	226	-6	0	55	2311	4.02	4.02	4.02	4.02	2	0.34	0.00	0.03	0.00	0.00	16.8
7	188	-889	329	-5	0	55	2371	4.02	4.02	4.02	4.02	2	0.35	0.01	0.04	0.00	0.00	16.8
8	188	-1020	226	30	0	5	2310	4.02	4.02	4.02	4.02	2	0.34	0.00	0.03	0.00	0.00	16.8
9	188	-887	328	30	0	5	2370	4.02	4.02	4.02	4.02	2	0.35	0.01	0.04	0.00	0.00	16.8
10	188	-979	262	-48	0	114	2333	4.02	4.02	4.02	4.02	2	0.34	0.01	0.03	0.00	0.00	16.8
11	188	-939	294	-47	0	114	2351	4.02	4.02	4.02	4.02	2	0.34	0.01	0.04	0.00	0.00	16.8
12	188	-970	262	72	0	-54	2331	4.02	4.02	4.02	4.02	2	0.34	0.01	0.03	0.00	0.00	16.8
13	188	-931	293	72	0	-54	2349	4.02	4.02	4.02	4.02	2	0.34	0.01	0.04	0.00	0.00	16.8
14	188	-1022	226	-6	0	55	2311	4.02	4.02	4.02	4.02	2	0.34	0.00	0.03	0.00	0.00	16.8
15	188	-889	329	-5	0	55	2371	4.02	4.02	4.02	4.02	2	0.35	0.01	0.04	0.00	0.00	16.8
16	188	-1020	226	30	0	5	2310	4.02	4.02	4.02	4.02	2	0.34	0.00	0.03	0.00	0.00	16.8
17	188	-887	328	30	0	5	2370	4.02	4.02	4.02	4.02	2	0.35	0.01	0.04	0.00	0.00	16.8
18	188	-1583	269	-144	0	311	3301	4.02	4.02	4.02	4.02	3	0.44	0.01	0.04	0.00	0.00	16.8
19	188	-1512	297	218	0	-213	3314	4.02	4.02	4.02	4.02	3	0.45	0.01	0.04	0.00	0.00	16.8
20	188	-1692	155	33	0	49	3302	4.02	4.02	4.02	4.02	3	0.44	0.00	0.02	0.00	0.00	16.8
37	188	-1487	278	-271	0	482	3153	4.02	4.02	4.02	4.02	3	0.42	0.01	0.04	0.00	0.00	16.8
38	188	-1369	325	332	0	-392	3175	4.02	4.02	4.02	4.02	3	0.43	0.01	0.04	0.00	0.00	16.8
39	188	-1668	88	23	0	45	3155	4.02	4.02	4.02	4.02	3	0.42	0.00	0.01	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	225	-1241	-1164	16	0	33	3043	4.02	4.02	4.02	4.02	3	0.41	0.03	0.15	0.00	0.00	16.8
2	225	-979	-910	-48	0	131	2333	4.02	4.02	4.02	4.02	2	0.34	0.02	0.12	0.00	0.00	16.8
3	225	-939	-879	-47	0	131	2351	4.02	4.02	4.02	4.02	2	0.34	0.02	0.12	0.00	0.00	16.8
4	225	-970	-910	72	0	-81	2331	4.02	4.02	4.02	4.02	2	0.34	0.02	0.12	0.00	0.00	16.8
5	225	-931	-880	72	0	-81	2349	4.02	4.02	4.02	4.02	2	0.34	0.02	0.12	0.00	0.00	16.8
6	225	-1022	-946	-6	0	57	2311	4.02	4.02	4.02	4.02	2	0.34	0.02	0.13	0.00	0.00	16.8
7	225	-889	-844	-5	0	57	2371	4.02	4.02	4.02	4.02	2	0.35	0.02	0.11	0.00	0.00	16.8
8	225	-1020	-946	30	0	-6	2310	4.02	4.02	4.02	4.02	2	0.34	0.02	0.13	0.00	0.00	16.8
9	225	-887	-844	30	0	-7	2370	4.02	4.02	4.02	4.02	2	0.35	0.02	0.11	0.00	0.00	16.8

10	225	-979	-910	-48	0	131	2333	4.02	4.02	4.02	4.02	2	0.34	0.02	0.12	0.00	0.00	16.8
11	225	-939	-879	-47	0	131	2351	4.02	4.02	4.02	4.02	2	0.34	0.02	0.12	0.00	0.00	16.8
12	225	-970	-910	72	0	-81	2331	4.02	4.02	4.02	4.02	2	0.34	0.02	0.12	0.00	0.00	16.8
13	225	-931	-880	72	0	-81	2349	4.02	4.02	4.02	4.02	2	0.34	0.02	0.12	0.00	0.00	16.8
14	225	-1022	-946	-6	0	57	2311	4.02	4.02	4.02	4.02	2	0.34	0.02	0.13	0.00	0.00	16.8
15	225	-889	-844	-5	0	57	2371	4.02	4.02	4.02	4.02	2	0.35	0.02	0.11	0.00	0.00	16.8
16	225	-1020	-946	30	0	-6	2310	4.02	4.02	4.02	4.02	2	0.34	0.02	0.13	0.00	0.00	16.8
17	225	-887	-844	30	0	-7	2370	4.02	4.02	4.02	4.02	2	0.35	0.02	0.11	0.00	0.00	16.8
18	225	-1583	-1414	-144	0	365	3301	4.02	4.02	4.02	4.02	3	0.44	0.03	0.19	0.00	0.00	16.8
19	225	-1512	-1386	218	0	-295	3314	4.02	4.02	4.02	4.02	3	0.45	0.03	0.18	0.00	0.00	16.8
20	225	-1692	-1528	33	0	36	3302	4.02	4.02	4.02	4.02	3	0.44	0.03	0.20	0.00	0.00	16.8
37	225	-1487	-1326	-271	0	584	3153	4.02	4.02	4.02	4.02	3	0.42	0.03	0.17	0.00	0.00	16.8
38	225	-1369	-1279	332	0	-516	3175	4.02	4.02	4.02	4.02	3	0.43	0.03	0.17	0.00	0.00	16.8
39	225	-1668	-1516	23	0	36	3155	4.02	4.02	4.02	4.02	3	0.42	0.03	0.20	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	262	-1241	-2688	16	0	27	3043	4.02	4.02	4.02	4.02	3	0.41	0.06	0.36	0.00	0.00	16.8
2	262	-979	-2083	-48	0	149	2333	4.02	4.02	4.02	4.02	2	0.34	0.05	0.28	0.00	0.00	16.8
3	262	-939	-2052	-47	0	149	2351	4.02	4.02	4.02	4.02	2	0.34	0.04	0.27	0.00	0.00	16.8
4	262	-970	-2083	72	0	-107	2331	4.02	4.02	4.02	4.02	2	0.34	0.05	0.28	0.00	0.00	16.8
5	262	-931	-2053	72	0	-108	2349	4.02	4.02	4.02	4.02	2	0.34	0.04	0.27	0.00	0.00	16.8
6	262	-1022	-2119	-6	0	60	2311	4.02	4.02	4.02	4.02	2	0.34	0.05	0.28	0.00	0.00	16.8
7	262	-889	-2017	-5	0	59	2371	4.02	4.02	4.02	4.02	2	0.35	0.04	0.27	0.00	0.00	16.8
8	262	-1020	-2119	30	0	-17	2310	4.02	4.02	4.02	4.02	2	0.34	0.05	0.28	0.00	0.00	16.8
9	262	-887	-2017	30	0	-18	2370	4.02	4.02	4.02	4.02	2	0.35	0.04	0.27	0.00	0.00	16.8
10	262	-979	-2083	-48	0	149	2333	4.02	4.02	4.02	4.02	2	0.34	0.05	0.28	0.00	0.00	16.8
11	262	-939	-2052	-47	0	149	2351	4.02	4.02	4.02	4.02	2	0.34	0.04	0.27	0.00	0.00	16.8
12	262	-970	-2083	72	0	-107	2331	4.02	4.02	4.02	4.02	2	0.34	0.05	0.28	0.00	0.00	16.8
13	262	-931	-2053	72	0	-108	2349	4.02	4.02	4.02	4.02	2	0.34	0.04	0.27	0.00	0.00	16.8
14	262	-1022	-2119	-6	0	60	2311	4.02	4.02	4.02	4.02	2	0.34	0.05	0.28	0.00	0.00	16.8
15	262	-889	-2017	-5	0	59	2371	4.02	4.02	4.02	4.02	2	0.35	0.04	0.27	0.00	0.00	16.8
16	262	-1020	-2119	30	0	-17	2310	4.02	4.02	4.02	4.02	2	0.34	0.05	0.28	0.00	0.00	16.8
17	262	-887	-2017	30	0	-18	2370	4.02	4.02	4.02	4.02	2	0.35	0.04	0.27	0.00	0.00	16.8
18	262	-1583	-3098	-144	0	419	3301	4.02	4.02	4.02	4.02	3	0.44	0.07	0.41	0.00	0.00	16.8
19	262	-1512	-3070	218	0	-377	3314	4.02	4.02	4.02	4.02	3	0.45	0.07	0.40	0.00	0.00	16.8
20	262	-1692	-3212	33	0	24	3302	4.02	4.02	4.02	4.02	3	0.44	0.07	0.42	0.00	0.00	16.8
37	262	-1487	-2930	-271	0	686	3153	4.02	4.02	4.02	4.02	3	0.42	0.06	0.39	0.00	0.00	16.8
38	262	-1369	-2883	332	0	-641	3175	4.02	4.02	4.02	4.02	3	0.43	0.06	0.38	0.00	0.00	16.8
39	262	-1668	-3120	23	0	27	3155	4.02	4.02	4.02	4.02	3	0.42	0.07	0.41	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	300	-1241	-4213	16	0	21	3009	4.02	4.02	4.02	4.02	3	0.41	0.09	0.56	0.00	0.00	16.8
2	300	-979	-3256	-48	0	167	2297	4.02	4.02	4.02	4.02	2	0.33	0.07	0.43	0.00	0.00	16.8
3	300	-939	-3225	-47	0	167	2335	4.02	4.02	4.02	4.02	2	0.34	0.07	0.43	0.00	0.00	16.8
4	300	-970	-3256	72	0	-134	2295	4.02	4.02	4.02	4.02	2	0.33	0.07	0.43	0.00	0.00	16.8
5	300	-931	-3225	72	0	-134	2332	4.02	4.02	4.02	4.02	2	0.34	0.07	0.43	0.00	0.00	16.8
6	300	-1022	-3292	-6	0	62	2254	4.02	4.02	4.02	4.02	2	0.33	0.07	0.44	0.00	0.00	16.8
7	300	-889	-3189	-5	0	61	2371	4.02	4.02	4.02	4.02	2	0.35	0.07	0.43	0.00	0.00	16.8
8	300	-1020	-3292	30	0	-28	2253	4.02	4.02	4.02	4.02	2	0.33	0.07	0.44	0.00	0.00	16.8
9	300	-887	-3190	30	0	-29	2370	4.02	4.02	4.02	4.02	2	0.35	0.07	0.43	0.00	0.00	16.8
10	300	-979	-3256	-48	0	167	2297	4.02	4.02	4.02	4.02	2	0.33	0.07	0.43	0.00	0.00	16.8
11	300	-939	-3225	-47	0	167	2335	4.02	4.02	4.02	4.02	2	0.34	0.07	0.43	0.00	0.00	16.8
12	300	-970	-3256	72	0	-134	2295	4.02	4.02	4.02	4.02	2	0.33	0.07	0.43	0.00	0.00	16.8
13	300	-931	-3225	72	0	-134	2332	4.02	4.02	4.02	4.02	2	0.34	0.07	0.43	0.00	0.00	16.8
14	300	-1022	-3292	-6	0	62	2254	4.02	4.02	4.02	4.02	2	0.33	0.07	0.44	0.00	0.00	16.8
15	300	-889	-3189	-5	0	61	2371	4.02	4.02	4.02	4.02	2	0.35	0.07	0.43	0.00	0.00	16.8
16	300	-1020	-3292	30	0	-28	2253	4.02	4.02	4.02	4.02	2	0.33	0.07	0.44	0.00	0.00	16.8
17	300	-887	-3190	30	0	-29	2370	4.02	4.02	4.02	4.02	2	0.35	0.07	0.43	0.00	0.00	16.8
18	300	-1583	-4781	-144	0	473	3184	4.02	4.02	4.02	4.02	3	0.43	0.10	0.63	0.00	0.00	16.8
19	300	-1512	-4753	218	0	-459	3214	4.02	4.02	4.02	4.02	3	0.43	0.10	0.63	0.00	0.00	16.8
20	300	-1692	-4895	33	0	11	3114	4.02	4.02	4.02	4.02	3	0.42	0.11	0.64	0.00	0.00	16.8
37	300	-1487	-4534	-271	0	788	3055	4.02	4.02	4.02	4.02	3	0.41	0.10	0.60	0.00	0.00	16.8
38	300	-1369	-4487	332	0	-766	3105	4.02	4.02	4.02	4.02	3	0.42	0.10	0.59	0.00	0.00	16.8
39	300	-1668	-4724	23	0	18	2939	4.02	4.02	4.02	4.02	3	0.39	0.10	0.62	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	338	-1241	-5737	16	0	15	-3426	4.02	4.02	4.02	4.02	3	0.46	0.12	0.76	0.00	0.00	16.8
2	338	-979	-4428	-48	0	185	-2672	4.02	4.02	4.02	4.02	2	0.39	0.10	0.59	0.00	0.00	16.8
3	338	-939	-4397	-47	0	185	-2596	4.02	4.02	4.02	4.02	2	0.38	0.10	0.59	0.00	0.00	16.8
4	338	-970	-4428	72	0	-161	-2675	4.02	4.02	4.02	4.02	2	0.39	0.10	0.59	0.00	0.00	16.8
5	338	-931	-4398	72	0	-161	-2599	4.02	4.02	4.02	4.02	2	0.38	0.10	0.59	0.00	0.00	16.8
6	338	-1022	-4464	-6	0	64	-2761	4.02	4.02	4.02	4.02	2	0.40	0.10	0.59	0.00	0.00	16.8
7	338	-889	-4362	-5	0	63	-2509	4.02	4.02	4.02	4.02	2	0.37	0.09	0.58	0.00	0.00	16.8
8	338	-1020	-4464	30	0	-40	-2762	4.02	4.02	4.02	4.02	2	0.40	0.10	0.59	0.00	0.00	16.8
9	338	-887	-4362	30	0	-41	-2510	4.02	4.02	4.02	4.02	2	0.37	0.09	0.58	0.00	0.00	16.8
10	338	-979	-4428	-48	0	185	-2672	4.02	4.02	4.02	4.02	2	0.39	0.10	0.59	0.00	0.00	16.8
11	338	-939	-4397	-47	0	185	-2596	4.02	4.02	4.02	4.02	2	0.38	0.10	0.59	0.00	0.00	16.8
12	338	-970	-4428	72	0	-161	-2675	4.02	4.02	4.02	4.02	2	0.39	0.10	0.59	0.00	0.00	16.8
13	338	-931	-4398	72	0	-161	-2599	4.02	4.02	4.02	4.02	2	0.38	0.10	0.59	0.00	0.00	16.8
14	338	-1022	-4464	-6	0	64	-2761	4.02	4.02	4.02	4.02	2	0.40	0.10	0.59	0.00	0.00	16.8
15	338	-889	-4362	-5	0	63	-2509	4.02	4.02	4.02	4.02	2	0.37	0.09	0.58	0.00	0.00	16.8
16	338	-1020	-4464	30	0	-40	-2762	4.02	4.02	4.02	4.02	2	0.40	0.10	0.59	0.00	0.00	16.8
17	338	-887	-4362	30	0	-41	-2510	4.02	4.02	4.02	4.02	2	0.37	0.09	0.58	0.00	0.00	16.8
18	338	-1583	-6464	-144	0	527	-4085	4.02	4.02	4.02	4.02	3	0.55	0.14	0.85	0.00	0.00	16.8
19	338	-1512	-6436	218	0	-541	-4019	4.02	4.02	4.02	4.02	3	0.54	0.14	0.85	0.00	0.00	16.8
20	338	-1692	-6578	33	0	-1	-4298	4.02	4.02	4.02	4.02	3	0.57	0.14	0.87	0.00	0.00	16.8
37	338	-1487	-6138	-271	0	889	-3844	4.02	4.02	4.02	4.02	3	0.52	0.13	0.81	0.00	0.00	16.8
38	338	-1369	-6091	332	0	-890	-3735	4.02	4.02	4.02	4.02	3	0.50	0.13	0.81	0.00	0.00	16.8
39	338	-1668	-6328	23	0	10	-4199	4.02	4.02	4.02	4.02	3	0.56	0.14	0.83	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	375	-1241	-7262	16	0	9	-3426	4.02	4.02	4.02	4.02	3	0.46	0.16	0.96	0.00	0.00	16.8
2	375	-979	-5601	-48	0	203	-2672	4.02	4.02	4.02	4.02	2	0.39	0.12	0.75	0.00	0.00	16.8
3	375	-939	-5570	-47	0	202	-2596	4.02	4.02	4.02	4.02	2	0.38	0.12	0.74	0.00	0.00	16.8
4	375	-970	-5601	72	0	-188	-2675	4.02	4.02	4.02	4.02	2	0.39	0.12	0.75	0.00	0.00	16.8
5	375	-931	-5571	72	0	-188	-2599	4.02	4.02	4.02	4.02	2	0.38	0.12	0.74	0.00	0.00	16.8
6	375	-1022	-5637	-6	0	67	-2761	4.02	4.02	4.02	4.02	2	0.40	0.12	0.75	0.00	0.00	16.8
7	375	-889	-5535	-5	0	65	-2509	4.02	4.02	4.02	4.02	2	0.37	0.12	0.74	0.00	0.00	16.8
8	375	-1020	-5637	30	0	-51	-2762	4.02	4.02	4.02	4.02	2	0.40	0.12	0.75	0.00	0.00	16.8
9	375	-887	-5535	30	0	-52	-2510	4.02	4.02	4.02	4.02	2	0.37	0.12	0.74	0.00	0.00	16.8
10	375	-979	-5601	-48	0	203	-2672	4.02	4.02	4.02	4.02	2	0.39	0.12	0.75	0.00	0.00	16.8
11	375	-939	-5570	-47	0	202	-2596	4.02	4.02	4.02	4.02	2	0.38	0.12	0.74	0.00	0.00	16.8
12	375	-970	-5601	72	0	-188	-2675	4.02	4.02	4.02	4.02	2	0.39	0.12	0.75	0.00	0.00	16.8
13	375	-931	-5571	72	0	-188	-2599	4.02	4.02	4.02	4.02	2	0.38	0.12	0.74	0.00	0.00	16.8
14	375	-1022	-5637	-6	0	67	-2761	4.02	4.02	4.02	4.02	2	0.40	0.12	0.75	0.00	0.00	16.8
15	375	-889	-5535	-5	0	65	-2509	4.02	4.02	4.02	4.02	2	0.37	0.12	0.74	0.00	0.00	16.8

16	375	-1020	-5637	30	0	-51	-2762	4.02	4.02	4.02	4.02	2	0.40	0.12	0.75	0.00	0.00	16.8
17	375	-887	-5535	30	0	-52	-2510	4.02	4.02	4.02	4.02	2	0.37	0.12	0.74	0.00	0.00	16.8
18	375	-1583	-8148	-144	0	581	-4085	4.02	4.02	4.02	4.02	3	0.55	0.18	1.07	2.02	0.00	16.8
19	375	-1512	-8120	218	0	-623	-4019	4.02	4.02	4.02	4.02	3	0.54	0.18	1.07	2.01	0.00	16.8
20	375	-1692	-8262	33	0	-13	-4298	4.02	4.02	4.02	4.02	3	0.57	0.18	1.09	2.05	0.00	16.8
37	375	-1487	-7742	-271	0	991	-3844	4.02	4.02	4.02	4.02	3	0.52	0.17	1.02	1.92	0.00	16.8
38	375	-1369	-7695	332	0	-1015	-3735	4.02	4.02	4.02	4.02	3	0.50	0.17	1.02	1.91	0.00	16.8
39	375	-1668	-7932	23	0	1	-4199	4.02	4.02	4.02	4.02	3	0.56	0.17	1.04	1.97	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

Nome travata: **trave_506_IP1** Descrizione: **Trave_5 21-20-19-18**
ASTA NUM. 16 NI 185 NF 298 SEZ. Rp B= 0.400 H= 0.500 (trave)

categoria: p.p. y Permanente Neve qy tot.
qy medio: 500.00 2627.25 282.50 3409.75 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-501	5981	-754	0	-1082	-2157	4.02	4.02	4.02	4.02	3	0.30	0.13	0.80	0.00	0.00	16.8
2	0	-332	4542	-331	0	-538	-1618	4.02	4.02	4.02	4.02	2	0.24	0.10	0.61	0.00	0.00	16.8
3	0	-363	4679	-345	0	-564	-1731	4.02	4.02	4.02	4.02	2	0.26	0.10	0.63	0.00	0.00	16.8
4	0	-407	4522	-816	0	-1102	-1588	4.02	4.02	4.02	4.02	2	0.24	0.10	0.61	0.00	0.00	16.8
5	0	-438	4659	-829	0	-1128	-1701	4.02	4.02	4.02	4.02	2	0.25	0.10	0.63	0.00	0.00	16.8
6	0	-321	4375	-485	0	-705	-1476	4.02	4.02	4.02	4.02	2	0.22	0.10	0.59	0.00	0.00	16.8
7	0	-426	4832	-530	0	-791	-1853	4.02	4.02	4.02	4.02	2	0.27	0.10	0.65	0.00	0.00	16.8
8	0	-344	4369	-631	0	-874	-1466	4.02	4.02	4.02	4.02	2	0.22	0.09	0.59	0.00	0.00	16.8
9	0	-449	4826	-675	0	-961	-1843	4.02	4.02	4.02	4.02	2	0.27	0.10	0.65	0.00	0.00	16.8
10	0	-332	4542	-331	0	-538	-1618	4.02	4.02	4.02	4.02	2	0.24	0.10	0.61	0.00	0.00	16.8
11	0	-363	4679	-345	0	-564	-1731	4.02	4.02	4.02	4.02	2	0.26	0.10	0.63	0.00	0.00	16.8
12	0	-407	4522	-816	0	-1102	-1588	4.02	4.02	4.02	4.02	2	0.24	0.10	0.61	0.00	0.00	16.8
13	0	-438	4659	-829	0	-1128	-1701	4.02	4.02	4.02	4.02	2	0.25	0.10	0.63	0.00	0.00	16.8
14	0	-321	4375	-485	0	-705	-1476	4.02	4.02	4.02	4.02	2	0.22	0.10	0.59	0.00	0.00	16.8
15	0	-426	4832	-530	0	-791	-1853	4.02	4.02	4.02	4.02	2	0.27	0.10	0.65	0.00	0.00	16.8
16	0	-344	4369	-631	0	-874	-1466	4.02	4.02	4.02	4.02	2	0.22	0.09	0.59	0.00	0.00	16.8
17	0	-449	4826	-675	0	-961	-1843	4.02	4.02	4.02	4.02	2	0.27	0.10	0.65	0.00	0.00	16.8
18	0	-231	6517	-904	0	-1483	-2413	4.02	4.02	4.02	4.02	3	0.34	0.14	0.88	0.00	0.00	16.8
19	0	-505	6423	-2200	0	-2887	-2283	4.02	4.02	4.02	4.02	3	0.50	0.14	0.86	0.00	0.00	16.8
20	0	-316	6527	-1528	0	-2167	-2300	4.02	4.02	4.02	4.02	3	0.38	0.14	0.88	0.00	0.00	16.8
37	0	-173	6287	-213	0	-656	-2365	4.02	4.02	4.02	4.02	3	0.33	0.14	0.85	0.00	0.00	16.8
38	0	-630	6130	-2372	0	-2996	-2149	4.02	4.02	4.02	4.02	3	0.52	0.13	0.82	0.00	0.00	16.8
39	0	-314	6303	-1253	0	-1797	-2176	4.02	4.02	4.02	4.02	3	0.31	0.14	0.85	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	31	-501	4721	-754	0	-848	-2157	4.02	4.02	4.02	4.02	3	0.30	0.10	0.63	0.00	0.00	16.8
2	31	-332	3573	-331	0	-435	-1618	4.02	4.02	4.02	4.02	2	0.24	0.08	0.48	0.00	0.00	16.8
3	31	-363	3710	-345	0	-457	-1731	4.02	4.02	4.02	4.02	2	0.26	0.08	0.50	0.00	0.00	16.8
4	31	-407	3552	-816	0	-849	-1588	4.02	4.02	4.02	4.02	2	0.24	0.08	0.48	0.00	0.00	16.8
5	31	-438	3689	-829	0	-871	-1701	4.02	4.02	4.02	4.02	2	0.25	0.08	0.50	0.00	0.00	16.8
6	31	-321	3406	-485	0	-554	-1476	4.02	4.02	4.02	4.02	2	0.22	0.07	0.46	0.00	0.00	16.8
7	31	-426	3862	-530	0	-627	-1853	4.02	4.02	4.02	4.02	2	0.27	0.08	0.52	0.00	0.00	16.8
8	31	-344	3400	-631	0	-678	-1466	4.02	4.02	4.02	4.02	2	0.22	0.07	0.46	0.00	0.00	16.8
9	31	-449	3856	-675	0	-751	-1843	4.02	4.02	4.02	4.02	2	0.27	0.08	0.52	0.00	0.00	16.8
10	31	-332	3573	-331	0	-435	-1618	4.02	4.02	4.02	4.02	2	0.24	0.08	0.48	0.00	0.00	16.8
11	31	-363	3710	-345	0	-457	-1731	4.02	4.02	4.02	4.02	2	0.26	0.08	0.50	0.00	0.00	16.8
12	31	-407	3552	-816	0	-849	-1588	4.02	4.02	4.02	4.02	2	0.24	0.08	0.48	0.00	0.00	16.8
13	31	-438	3689	-829	0	-871	-1701	4.02	4.02	4.02	4.02	2	0.25	0.08	0.50	0.00	0.00	16.8
14	31	-321	3406	-485	0	-554	-1476	4.02	4.02	4.02	4.02	2	0.22	0.07	0.46	0.00	0.00	16.8
15	31	-426	3862	-530	0	-627	-1853	4.02	4.02	4.02	4.02	2	0.27	0.08	0.52	0.00	0.00	16.8
16	31	-344	3400	-631	0	-678	-1466	4.02	4.02	4.02	4.02	2	0.22	0.07	0.46	0.00	0.00	16.8
17	31	-449	3856	-675	0	-751	-1843	4.02	4.02	4.02	4.02	2	0.27	0.08	0.52	0.00	0.00	16.8
18	31	-231	5125	-904	0	-1203	-2413	4.02	4.02	4.02	4.02	3	0.34	0.11	0.69	0.00	0.00	16.8
19	31	-505	5031	-2200	0	-2205	-2283	4.02	4.02	4.02	4.02	3	0.38	0.11	0.68	0.00	0.00	16.8
20	31	-316	5135	-1528	0	-1694	-2300	4.02	4.02	4.02	4.02	3	0.32	0.11	0.69	0.00	0.00	16.8
37	31	-173	4961	-213	0	-590	-2365	4.02	4.02	4.02	4.02	3	0.33	0.11	0.67	0.00	0.00	16.8
38	31	-630	4804	-2372	0	-2261	-2149	4.02	4.02	4.02	4.02	3	0.39	0.10	0.64	0.00	0.00	16.8
39	31	-314	4977	-1253	0	-1409	-2176	4.02	4.02	4.02	4.02	3	0.30	0.11	0.67	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	62	-501	3460	-754	0	-614	2229	4.02	4.02	4.02	4.02	3	0.31	0.08	0.46	0.00	0.00	16.8
2	62	-332	2603	-331	0	-332	1666	4.02	4.02	4.02	4.02	2	0.25	0.06	0.35	0.00	0.00	16.8
3	62	-363	2740	-345	0	-350	1765	4.02	4.02	4.02	4.02	2	0.26	0.06	0.37	0.00	0.00	16.8
4	62	-407	2583	-816	0	-596	1664	4.02	4.02	4.02	4.02	2	0.25	0.06	0.35	0.00	0.00	16.8
5	62	-438	2720	-829	0	-614	1764	4.02	4.02	4.02	4.02	2	0.26	0.06	0.37	0.00	0.00	16.8
6	62	-321	2436	-485	0	-404	1549	4.02	4.02	4.02	4.02	2	0.23	0.05	0.33	0.00	0.00	16.8
7	62	-426	2893	-530	0	-463	1880	4.02	4.02	4.02	4.02	2	0.28	0.06	0.39	0.00	0.00	16.8
8	62	-344	2430	-631	0	-483	1549	4.02	4.02	4.02	4.02	2	0.23	0.05	0.33	0.00	0.00	16.8
9	62	-449	2887	-675	0	-542	1880	4.02	4.02	4.02	4.02	2	0.28	0.06	0.39	0.00	0.00	16.8
10	62	-332	2603	-331	0	-332	1666	4.02	4.02	4.02	4.02	2	0.25	0.06	0.35	0.00	0.00	16.8
11	62	-363	2740	-345	0	-350	1765	4.02	4.02	4.02	4.02	2	0.26	0.06	0.37	0.00	0.00	16.8
12	62	-407	2583	-816	0	-596	1664	4.02	4.02	4.02	4.02	2	0.25	0.06	0.35	0.00	0.00	16.8
13	62	-438	2720	-829	0	-614	1764	4.02	4.02	4.02	4.02	2	0.26	0.06	0.37	0.00	0.00	16.8
14	62	-321	2436	-485	0	-404	1549	4.02	4.02	4.02	4.02	2	0.23	0.05	0.33	0.00	0.00	16.8
15	62	-426	2893	-530	0	-463	1880	4.02	4.02	4.02	4.02	2	0.28	0.06	0.39	0.00	0.00	16.8
16	62	-344	2430	-631	0	-483	1549	4.02	4.02	4.02	4.02	2	0.23	0.05	0.33	0.00	0.00	16.8
17	62	-449	2887	-675	0	-542	1880	4.02	4.02	4.02	4.02	2	0.28	0.06	0.39	0.00	0.00	16.8
18	62	-231	3734	-904	0	-923	2296	4.02	4.02	4.02	4.02	3	0.32	0.08	0.50	0.00	0.00	16.8
19	62	-505	3640	-2200	0	-1523	2279	4.02	4.02	4.02	4.02	3	0.32	0.08	0.49	0.00	0.00	16.8
20	62	-316	3744	-1528	0	-1220	2424	4.02	4.02	4.02	4.02	3	0.34	0.08	0.50	0.00	0.00	16.8
37	62	-173	3635	-213	0	-524	2242	4.02	4.02	4.02	4.02	3	0.31	0.08	0.49	0.00	0.00	16.8
38	62	-630	3478	-2372	0	-1525	2215	4.02	4.02	4.02	4.02	3	0.31	0.08	0.47	0.00	0.00	16.8
39	62	-314	3651	-1253	0	-1020	2456	4.02	4.02	4.02	4.02	3	0.34	0.08	0.49	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	93	-501	2200	-754	0	-381	2229	4.02	4.02	4.02	4.02	3	0.31	0.05	0.30	0.00	0.00	16.8
2	93	-332	1634	-331	0	-230	1666	4.02	4.02	4.02	4.02	2	0.25	0.04	0.22	0.00	0.00	16.8
3	93	-363	1771	-345	0	-243	1765	4.02	4.02	4.02	4.02	2	0.26	0.04	0.24	0.00	0.00	16.8
4	93	-407	1613	-816	0	-343	1664	4.02	4.02	4.02	4.02	2	0.25	0.04	0.22	0.00	0.00	16.8
5	93	-438	1750	-829	0	-357	1764	4.02	4.02	4.02	4.02	2	0.26	0.04	0.24	0.00	0.00	16.8
6	93	-321	1466	-485	0	-254	1549	4.02	4.02	4.02	4.02	2	0.23	0.03	0.20	0.00	0.00	16.8
7	93	-426	1923	-530	0	-299	1880	4.02	4.02	4.02	4.02	2	0.28	0.04	0.26	0.00	0.00	16.8

8	93	-344	1460	-631	0	-287	1549	4.02	4.02	4.02	4.02	2	0.23	0.03	0.20	0.00	0.00	16.8
9	93	-449	1917	-675	0	-333	1880	4.02	4.02	4.02	4.02	2	0.28	0.04	0.26	0.00	0.00	16.8
10	93	-332	1634	-331	0	-230	1666	4.02	4.02	4.02	4.02	2	0.25	0.04	0.22	0.00	0.00	16.8
11	93	-363	1771	-345	0	-243	1765	4.02	4.02	4.02	4.02	2	0.26	0.04	0.24	0.00	0.00	16.8
12	93	-407	1613	-816	0	-343	1664	4.02	4.02	4.02	4.02	2	0.25	0.04	0.22	0.00	0.00	16.8
13	93	-438	1750	-829	0	-357	1764	4.02	4.02	4.02	4.02	2	0.26	0.04	0.24	0.00	0.00	16.8
14	93	-321	1466	-485	0	-254	1549	4.02	4.02	4.02	4.02	2	0.23	0.03	0.20	0.00	0.00	16.8
15	93	-426	1923	-530	0	-299	1880	4.02	4.02	4.02	4.02	2	0.28	0.04	0.26	0.00	0.00	16.8
16	93	-344	1460	-631	0	-287	1549	4.02	4.02	4.02	4.02	2	0.23	0.03	0.20	0.00	0.00	16.8
17	93	-449	1917	-675	0	-333	1880	4.02	4.02	4.02	4.02	2	0.28	0.04	0.26	0.00	0.00	16.8
18	93	-231	2342	-904	0	-642	2296	4.02	4.02	4.02	4.02	3	0.32	0.05	0.32	0.00	0.00	16.8
19	93	-505	2248	-2200	0	-841	2279	4.02	4.02	4.02	4.02	3	0.32	0.05	0.30	0.00	0.00	16.8
20	93	-316	2352	-1528	0	-747	2424	4.02	4.02	4.02	4.02	3	0.34	0.05	0.32	0.00	0.00	16.8
37	93	-173	2309	-213	0	-458	2242	4.02	4.02	4.02	4.02	3	0.31	0.05	0.31	0.00	0.00	16.8
38	93	-630	2152	-2372	0	-790	2215	4.02	4.02	4.02	4.02	3	0.31	0.05	0.30	0.00	0.00	16.8
39	93	-314	2325	-1253	0	-632	2456	4.02	4.02	4.02	4.02	3	0.34	0.05	0.31	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	124	-501	940	-754	0	-147	2229	4.02	4.02	4.02	4.02	3	0.31	0.02	0.13	0.00	0.00	16.8
2	124	-332	664	-331	0	-127	1666	4.02	4.02	4.02	4.02	2	0.25	0.01	0.09	0.00	0.00	16.8
3	124	-363	801	-345	0	-136	1765	4.02	4.02	4.02	4.02	2	0.26	0.02	0.11	0.00	0.00	16.8
4	124	-407	644	-816	0	-90	1664	4.02	4.02	4.02	4.02	2	0.25	0.02	0.10	0.00	0.00	16.8
5	124	-438	781	-829	0	-100	1764	4.02	4.02	4.02	4.02	2	0.26	0.02	0.11	0.00	0.00	16.8
6	124	-321	497	-485	0	-103	1549	4.02	4.02	4.02	4.02	2	0.23	0.01	0.07	0.00	0.00	16.8
7	124	-426	954	-530	0	-134	1880	4.02	4.02	4.02	4.02	2	0.28	0.02	0.13	0.00	0.00	16.8
8	124	-344	491	-631	0	-92	1549	4.02	4.02	4.02	4.02	2	0.23	0.01	0.08	0.00	0.00	16.8
9	124	-449	948	-675	0	-123	1880	4.02	4.02	4.02	4.02	2	0.28	0.02	0.13	0.00	0.00	16.8
10	124	-332	664	-331	0	-127	1666	4.02	4.02	4.02	4.02	2	0.25	0.01	0.09	0.00	0.00	16.8
11	124	-363	801	-345	0	-136	1765	4.02	4.02	4.02	4.02	2	0.26	0.02	0.11	0.00	0.00	16.8
12	124	-407	644	-816	0	-90	1664	4.02	4.02	4.02	4.02	2	0.25	0.02	0.10	0.00	0.00	16.8
13	124	-438	781	-829	0	-100	1764	4.02	4.02	4.02	4.02	2	0.26	0.02	0.11	0.00	0.00	16.8
14	124	-321	497	-485	0	-103	1549	4.02	4.02	4.02	4.02	2	0.23	0.01	0.07	0.00	0.00	16.8
15	124	-426	954	-530	0	-134	1880	4.02	4.02	4.02	4.02	2	0.28	0.02	0.13	0.00	0.00	16.8
16	124	-344	491	-631	0	-92	1549	4.02	4.02	4.02	4.02	2	0.23	0.01	0.08	0.00	0.00	16.8
17	124	-449	948	-675	0	-123	1880	4.02	4.02	4.02	4.02	2	0.28	0.02	0.13	0.00	0.00	16.8
18	124	-231	950	-904	0	-362	2296	4.02	4.02	4.02	4.02	3	0.32	0.02	0.13	0.00	0.00	16.8
19	124	-505	856	-2200	0	-159	2279	4.02	4.02	4.02	4.02	3	0.32	0.05	0.28	0.00	0.00	16.8
20	124	-316	960	-1528	0	-273	2424	4.02	4.02	4.02	4.02	3	0.34	0.03	0.20	0.00	0.00	16.8
37	124	-173	983	-213	0	-392	2242	4.02	4.02	4.02	4.02	3	0.31	0.02	0.13	0.00	0.00	16.8
38	124	-630	826	-2372	0	-54	2215	4.02	4.02	4.02	4.02	3	0.31	0.05	0.30	0.00	0.00	16.8
39	124	-314	999	-1253	0	-244	2456	4.02	4.02	4.02	4.02	3	0.34	0.03	0.16	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	155	-501	-320	-754	0	87	2229	4.02	4.02	4.02	4.02	3	0.31	0.02	0.10	0.00	0.00	16.8
2	155	-332	-305	-331	0	-24	1666	4.02	4.02	4.02	4.02	2	0.25	0.01	0.04	0.00	0.00	16.8
3	155	-363	-168	-345	0	-29	1765	4.02	4.02	4.02	4.02	2	0.26	0.01	0.04	0.00	0.00	16.8
4	155	-407	-326	-816	0	162	1664	4.02	4.02	4.02	4.02	2	0.25	0.02	0.10	0.00	0.00	16.8
5	155	-438	-188	-829	0	157	1764	4.02	4.02	4.02	4.02	2	0.26	0.02	0.11	0.00	0.00	16.8
6	155	-321	-472	-485	0	47	1549	4.02	4.02	4.02	4.02	2	0.23	0.01	0.06	0.00	0.00	16.8
7	155	-426	-16	-530	0	30	1880	4.02	4.02	4.02	4.02	2	0.28	0.01	0.07	0.00	0.00	16.8
8	155	-344	-478	-631	0	104	1549	4.02	4.02	4.02	4.02	2	0.23	0.01	0.08	0.00	0.00	16.8
9	155	-449	-22	-675	0	86	1880	4.02	4.02	4.02	4.02	2	0.28	0.02	0.09	0.00	0.00	16.8
10	155	-332	-305	-331	0	-24	1666	4.02	4.02	4.02	4.02	2	0.25	0.01	0.04	0.00	0.00	16.8
11	155	-363	-168	-345	0	-29	1765	4.02	4.02	4.02	4.02	2	0.26	0.01	0.04	0.00	0.00	16.8
12	155	-407	-326	-816	0	162	1664	4.02	4.02	4.02	4.02	2	0.25	0.02	0.10	0.00	0.00	16.8
13	155	-438	-188	-829	0	157	1764	4.02	4.02	4.02	4.02	2	0.26	0.02	0.11	0.00	0.00	16.8
14	155	-321	-472	-485	0	47	1549	4.02	4.02	4.02	4.02	2	0.23	0.01	0.06	0.00	0.00	16.8
15	155	-426	-16	-530	0	30	1880	4.02	4.02	4.02	4.02	2	0.28	0.01	0.07	0.00	0.00	16.8
16	155	-344	-478	-631	0	104	1549	4.02	4.02	4.02	4.02	2	0.23	0.01	0.08	0.00	0.00	16.8
17	155	-449	-22	-675	0	86	1880	4.02	4.02	4.02	4.02	2	0.28	0.02	0.09	0.00	0.00	16.8
18	155	-231	-442	-904	0	-82	2296	4.02	4.02	4.02	4.02	3	0.32	0.02	0.12	0.00	0.00	16.8
19	155	-505	-536	-2200	0	522	2279	4.02	4.02	4.02	4.02	3	0.32	0.05	0.28	0.00	0.00	16.8
20	155	-316	-432	-1528	0	200	2424	4.02	4.02	4.02	4.02	3	0.34	0.03	0.20	0.00	0.00	16.8
37	155	-173	-343	-213	0	-326	2242	4.02	4.02	4.02	4.02	3	0.31	0.01	0.05	0.00	0.00	16.8
38	155	-630	-500	-2372	0	681	2215	4.02	4.02	4.02	4.02	3	0.31	0.05	0.30	0.00	0.00	16.8
39	155	-314	-327	-1253	0	144	2456	4.02	4.02	4.02	4.02	3	0.34	0.03	0.16	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	186	-501	-1581	-754	0	321	2229	4.02	4.02	4.02	4.02	3	0.31	0.03	0.21	0.00	0.00	16.8
2	186	-332	-1274	-331	0	78	1666	4.02	4.02	4.02	4.02	2	0.25	0.03	0.17	0.00	0.00	16.8
3	186	-363	-1137	-345	0	77	1765	4.02	4.02	4.02	4.02	2	0.26	0.02	0.15	0.00	0.00	16.8
4	186	-407	-1295	-816	0	415	1664	4.02	4.02	4.02	4.02	2	0.25	0.03	0.17	0.00	0.00	16.8
5	186	-438	-1158	-829	0	415	1764	4.02	4.02	4.02	4.02	2	0.26	0.03	0.16	0.00	0.00	16.8
6	186	-321	-1442	-485	0	198	1549	4.02	4.02	4.02	4.02	2	0.23	0.03	0.19	0.00	0.00	16.8
7	186	-426	-985	-530	0	194	1880	4.02	4.02	4.02	4.02	2	0.28	0.02	0.13	0.00	0.00	16.8
8	186	-344	-1448	-631	0	299	1549	4.02	4.02	4.02	4.02	2	0.23	0.03	0.20	0.00	0.00	16.8
9	186	-449	-991	-675	0	296	1880	4.02	4.02	4.02	4.02	2	0.28	0.02	0.13	0.00	0.00	16.8
10	186	-332	-1274	-331	0	78	1666	4.02	4.02	4.02	4.02	2	0.25	0.03	0.17	0.00	0.00	16.8
11	186	-363	-1137	-345	0	77	1765	4.02	4.02	4.02	4.02	2	0.26	0.02	0.15	0.00	0.00	16.8
12	186	-407	-1295	-816	0	415	1664	4.02	4.02	4.02	4.02	2	0.25	0.03	0.17	0.00	0.00	16.8
13	186	-438	-1158	-829	0	415	1764	4.02	4.02	4.02	4.02	2	0.26	0.03	0.16	0.00	0.00	16.8
14	186	-321	-1442	-485	0	198	1549	4.02	4.02	4.02	4.02	2	0.23	0.03	0.19	0.00	0.00	16.8
15	186	-426	-985	-530	0	194	1880	4.02	4.02	4.02	4.02	2	0.28	0.02	0.13	0.00	0.00	16.8
16	186	-344	-1448	-631	0	299	1549	4.02	4.02	4.02	4.02	2	0.23	0.03	0.20	0.00	0.00	16.8
17	186	-449	-991	-675	0	296	1880	4.02	4.02	4.02	4.02	2	0.28	0.02	0.13	0.00	0.00	16.8
18	186	-231	-1833	-904	0	198	2296	4.02	4.02	4.02	4.02	3	0.32	0.04	0.25	0.00	0.00	16.8
19	186	-505	-1927	-2200	0	1204	2279	4.02	4.02	4.02	4.02	3	0.32	0.05	0.28	0.00	0.00	16.8
20	186	-316	-1823	-1528	0	674	2424	4.02	4.02	4.02	4.02	3	0.34	0.04	0.25	0.00	0.00	16.8
37	186	-173	-1669	-213	0	-260	2242	4.02	4.02	4.02	4.02	3	0.31	0.04	0.23	0.00	0.00	16.8
38	186	-630	-1826	-2372	0	1416	2215	4.02	4.02	4.02	4.02	3	0.31	0.05	0.30	0.00	0.00	16.8
39	186	-314	-1652	-1253	0	533	2456	4.02	4.02	4.02	4.02	3	0.34	0.04	0.22	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	217	-501	-2841	-754	0	555	2229	4.02	4.02	4.02	4.02	3	0.31	0.06	0.38	0.00	0.00	16.8
2	217	-332	-2244	-331	0	181	1666	4.02	4.02	4.02	4.02	2	0.25	0.05	0.30	0.00	0.00	16.8
3	217	-363	-2107	-345	0	184	1765	4.02	4.02	4.02	4.02	2	0.26	0.05	0.28	0.00	0.00	16.8
4	217	-407	-2264	-816	0	668	1664	4.02	4.02	4.02	4.02	2	0.25	0.05	0.30	0.00	0.00	16.8
5	217	-438	-2128	-829	0	672	1764	4.02	4.02	4.02	4.02	2	0.26	0.05	0.29	0.00	0.00	16.8
6	217	-321	-2412	-485	0	348	1549	4.02	4.02	4.02	4.02	2	0.23	0.05	0.33	0.00	0.00	16.8
7	217	-426	-1954	-530	0	358	1880	4.02	4.02	4.02	4.02	2	0.28	0.04	0.26	0.00	0.00	16.8
8	217	-344	-2418	-631	0	495	1549	4.02	4.02	4.02	4.02	2	0.23	0.05	0.33	0.00	0.00	16.8
9	217	-449	-1960	-675	0	505	1880	4.02	4.02	4.02	4.02	2	0.28	0.04	0.26	0.00	0.00	16.8
10	217	-332	-2244	-331	0	181	1666	4.02	4.02	4.02	4.02	2	0.25	0.05	0.30	0.00	0.00	16.8
11	217	-363	-2107	-345	0	184	1765	4.02	4.02	4.02	4.02	2	0.26	0.05	0.28	0.00	0.00	16.8
12	217	-407	-2264	-816	0	668	1664	4.02	4.02	4.02	4.02	2	0.25	0.05	0.30	0.00	0.00	16.8
13	217	-438	-2128	-829	0	672	1764	4.02	4.02	4.02	4.02	2	0.26	0.05	0.29	0.00	0.00	16.8

14	217	-321	-2412	-485	0	348	1549	4.02	4.02	4.02	4.02	2	0.23	0.05	0.33	0.00	0.00	16.8
15	217	-426	-1954	-530	0	358	1880	4.02	4.02	4.02	4.02	2	0.28	0.04	0.26	0.00	0.00	16.8
16	217	-344	-2418	-631	0	495	1549	4.02	4.02	4.02	4.02	2	0.23	0.05	0.33	0.00	0.00	16.8
17	217	-449	-1960	-675	0	505	1880	4.02	4.02	4.02	4.02	2	0.28	0.04	0.26	0.00	0.00	16.8
18	217	-231	-3225	-904	0	478	2296	4.02	4.02	4.02	4.02	3	0.32	0.07	0.44	0.00	0.00	16.8
19	217	-505	-3319	-2200	0	1886	2279	4.02	4.02	4.02	4.02	3	0.33	0.07	0.45	0.00	0.00	16.8
20	217	-316	-3215	-1528	0	1148	2424	4.02	4.02	4.02	4.02	3	0.34	0.07	0.43	0.00	0.00	16.8
37	217	-173	-2995	-213	0	-194	2242	4.02	4.02	4.02	4.02	3	0.31	0.07	0.40	0.00	0.00	16.8
38	217	-630	-3152	-2372	0	2152	2215	4.02	4.02	4.02	4.02	3	0.37	0.07	0.42	0.00	0.00	16.8
39	217	-314	-2978	-1253	0	921	2456	4.02	4.02	4.02	4.02	3	0.34	0.06	0.40	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	248	-501	-4101	-754	0	788	2229	4.02	4.02	4.02	4.02	3	0.31	0.09	0.55	0.00	0.00	16.8
2	248	-332	-3213	-331	0	284	1656	4.02	4.02	4.02	4.02	2	0.25	0.07	0.43	0.00	0.00	16.8
3	248	-363	-3076	-345	0	291	1765	4.02	4.02	4.02	4.02	2	0.26	0.07	0.41	0.00	0.00	16.8
4	248	-407	-3234	-816	0	921	1646	4.02	4.02	4.02	4.02	2	0.24	0.07	0.44	0.00	0.00	16.8
5	248	-438	-3097	-829	0	929	1764	4.02	4.02	4.02	4.02	2	0.26	0.07	0.42	0.00	0.00	16.8
6	248	-321	-3381	-485	0	499	-1955	4.02	4.02	4.02	4.02	2	0.29	0.07	0.46	0.00	0.00	16.8
7	248	-426	-2924	-530	0	523	1880	4.02	4.02	4.02	4.02	2	0.28	0.06	0.39	0.00	0.00	16.8
8	248	-344	-3387	-631	0	690	-1963	4.02	4.02	4.02	4.02	2	0.29	0.07	0.46	0.00	0.00	16.8
9	248	-449	-2930	-675	0	714	1880	4.02	4.02	4.02	4.02	2	0.28	0.06	0.39	0.00	0.00	16.8
10	248	-332	-3213	-331	0	284	1656	4.02	4.02	4.02	4.02	2	0.25	0.07	0.43	0.00	0.00	16.8
11	248	-363	-3076	-345	0	291	1765	4.02	4.02	4.02	4.02	2	0.26	0.07	0.41	0.00	0.00	16.8
12	248	-407	-3234	-816	0	921	1646	4.02	4.02	4.02	4.02	2	0.24	0.07	0.44	0.00	0.00	16.8
13	248	-438	-3097	-829	0	929	1764	4.02	4.02	4.02	4.02	2	0.26	0.07	0.42	0.00	0.00	16.8
14	248	-321	-3381	-485	0	499	-1955	4.02	4.02	4.02	4.02	2	0.29	0.07	0.46	0.00	0.00	16.8
15	248	-426	-2924	-530	0	523	1880	4.02	4.02	4.02	4.02	2	0.28	0.06	0.39	0.00	0.00	16.8
16	248	-344	-3387	-631	0	690	-1963	4.02	4.02	4.02	4.02	2	0.29	0.07	0.46	0.00	0.00	16.8
17	248	-449	-2930	-675	0	714	1880	4.02	4.02	4.02	4.02	2	0.28	0.06	0.39	0.00	0.00	16.8
18	248	-231	-4617	-904	0	759	-2393	4.02	4.02	4.02	4.02	3	0.33	0.10	0.62	0.00	0.00	16.8
19	248	-505	-4711	-2200	0	2568	-2545	4.02	4.02	4.02	4.02	3	0.45	0.10	0.63	0.00	0.00	16.8
20	248	-316	-4607	-1528	0	1621	2413	4.02	4.02	4.02	4.02	3	0.34	0.10	0.62	0.00	0.00	16.8
37	248	-173	-4321	-213	0	-129	2242	4.02	4.02	4.02	4.02	3	0.31	0.09	0.58	0.00	0.00	16.8
38	248	-630	-4478	-2372	0	2887	-2367	4.02	4.02	4.02	4.02	3	0.50	0.10	0.60	0.00	0.00	16.8
39	248	-314	-4304	-1253	0	1309	2456	4.02	4.02	4.02	4.02	3	0.34	0.09	0.58	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	279	-501	-5362	-754	0	1022	-3152	4.02	4.02	4.02	4.02	3	0.44	0.12	0.72	0.00	0.00	16.8
2	279	-332	-4183	-331	0	387	-2564	4.02	4.02	4.02	4.02	2	0.38	0.09	0.56	0.00	0.00	16.8
3	279	-363	-4046	-345	0	398	-2252	4.02	4.02	4.02	4.02	2	0.33	0.09	0.54	0.00	0.00	16.8
4	279	-407	-4204	-816	0	1174	-2597	4.02	4.02	4.02	4.02	2	0.39	0.09	0.57	0.00	0.00	16.8
5	279	-438	-4067	-829	0	1186	-2285	4.02	4.02	4.02	4.02	2	0.34	0.09	0.55	0.00	0.00	16.8
6	279	-321	-4351	-485	0	649	-2940	4.02	4.02	4.02	4.02	2	0.44	0.09	0.59	0.00	0.00	16.8
7	279	-426	-3894	-530	0	687	-1900	4.02	4.02	4.02	4.02	2	0.28	0.08	0.52	0.00	0.00	16.8
8	279	-344	-4357	-631	0	886	-2949	4.02	4.02	4.02	4.02	2	0.44	0.09	0.59	0.00	0.00	16.8
9	279	-449	-3900	-675	0	924	-1910	4.02	4.02	4.02	4.02	2	0.28	0.08	0.52	0.00	0.00	16.8
10	279	-332	-4183	-331	0	387	-2564	4.02	4.02	4.02	4.02	2	0.38	0.09	0.56	0.00	0.00	16.8
11	279	-363	-4046	-345	0	398	-2252	4.02	4.02	4.02	4.02	2	0.33	0.09	0.54	0.00	0.00	16.8
12	279	-407	-4204	-816	0	1174	-2597	4.02	4.02	4.02	4.02	2	0.39	0.09	0.57	0.00	0.00	16.8
13	279	-438	-4067	-829	0	1186	-2285	4.02	4.02	4.02	4.02	2	0.34	0.09	0.55	0.00	0.00	16.8
14	279	-321	-4351	-485	0	649	-2940	4.02	4.02	4.02	4.02	2	0.44	0.09	0.59	0.00	0.00	16.8
15	279	-426	-3894	-530	0	687	-1900	4.02	4.02	4.02	4.02	2	0.28	0.08	0.52	0.00	0.00	16.8
16	279	-344	-4357	-631	0	886	-2949	4.02	4.02	4.02	4.02	2	0.44	0.09	0.59	0.00	0.00	16.8
17	279	-449	-3900	-675	0	924	-1910	4.02	4.02	4.02	4.02	2	0.28	0.08	0.52	0.00	0.00	16.8
18	279	-231	-6008	-904	0	1039	-3781	4.02	4.02	4.02	4.02	3	0.53	0.13	0.81	0.00	0.00	16.8
19	279	-505	-6102	-2200	0	3250	-3944	4.02	4.02	4.02	4.02	3	0.57	0.13	0.82	0.00	0.00	16.8
20	279	-316	-5998	-1528	0	2095	-3638	4.02	4.02	4.02	4.02	3	0.51	0.13	0.81	0.00	0.00	16.8
37	279	-173	-5647	-213	0	-63	-3427	4.02	4.02	4.02	4.02	3	0.48	0.12	0.76	0.00	0.00	16.8
38	279	-630	-5804	-2372	0	3623	-3698	4.02	4.02	4.02	4.02	3	0.63	0.13	0.78	0.00	0.00	16.8
39	279	-314	-5630	-1253	0	1698	-3188	4.02	4.02	4.02	4.02	3	0.44	0.12	0.76	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	310	-501	-6622	-754	0	1256	-3152	4.02	4.02	4.02	4.02	3	0.44	0.14	0.89	0.00	0.00	16.8
2	310	-332	-5152	-331	0	489	-2564	4.02	4.02	4.02	4.02	2	0.38	0.11	0.69	0.00	0.00	16.8
3	310	-363	-5015	-345	0	505	-2252	4.02	4.02	4.02	4.02	2	0.33	0.11	0.68	0.00	0.00	16.8
4	310	-407	-5173	-816	0	1427	-2597	4.02	4.02	4.02	4.02	2	0.39	0.11	0.70	0.00	0.00	16.8
5	310	-438	-5036	-829	0	1443	-2285	4.02	4.02	4.02	4.02	2	0.34	0.11	0.68	0.00	0.00	16.8
6	310	-321	-5320	-485	0	800	-2940	4.02	4.02	4.02	4.02	2	0.44	0.12	0.72	0.00	0.00	16.8
7	310	-426	-4863	-530	0	851	-1900	4.02	4.02	4.02	4.02	2	0.28	0.11	0.65	0.00	0.00	16.8
8	310	-344	-5326	-631	0	1081	-2949	4.02	4.02	4.02	4.02	2	0.44	0.12	0.72	0.00	0.00	16.8
9	310	-449	-4869	-675	0	1133	-1910	4.02	4.02	4.02	4.02	2	0.28	0.11	0.65	0.00	0.00	16.8
10	310	-332	-5152	-331	0	489	-2564	4.02	4.02	4.02	4.02	2	0.38	0.11	0.69	0.00	0.00	16.8
11	310	-363	-5015	-345	0	505	-2252	4.02	4.02	4.02	4.02	2	0.33	0.11	0.68	0.00	0.00	16.8
12	310	-407	-5173	-816	0	1427	-2597	4.02	4.02	4.02	4.02	2	0.39	0.11	0.70	0.00	0.00	16.8
13	310	-438	-5036	-829	0	1443	-2285	4.02	4.02	4.02	4.02	2	0.34	0.11	0.68	0.00	0.00	16.8
14	310	-321	-5320	-485	0	800	-2940	4.02	4.02	4.02	4.02	2	0.44	0.12	0.72	0.00	0.00	16.8
15	310	-426	-4863	-530	0	851	-1900	4.02	4.02	4.02	4.02	2	0.28	0.11	0.65	0.00	0.00	16.8
16	310	-344	-5326	-631	0	1081	-2949	4.02	4.02	4.02	4.02	2	0.44	0.12	0.72	0.00	0.00	16.8
17	310	-449	-4869	-675	0	1133	-1910	4.02	4.02	4.02	4.02	2	0.28	0.11	0.65	0.00	0.00	16.8
18	310	-231	-7400	-904	0	1319	-3781	4.02	4.02	4.02	4.02	3	0.53	0.16	1.00	0.00	0.00	16.8
19	310	-505	-7494	-2200	0	3932	-3944	4.02	4.02	4.02	4.02	3	0.68	0.16	1.01	1.86	0.00	16.8
20	310	-316	-7390	-1528	0	2568	-3638	4.02	4.02	4.02	4.02	3	0.51	0.16	1.00	0.00	0.00	16.8
37	310	-173	-6973	-213	0	3	-3427	4.02	4.02	4.02	4.02	3	0.48	0.15	0.94	0.00	0.00	16.8
38	310	-630	-7130	-2372	0	4358	-3698	4.02	4.02	4.02	4.02	3	0.76	0.15	0.96	0.00	0.00	16.8
39	310	-314	-6956	-1253	0	2086	-3188	4.02	4.02	4.02	4.02	3	0.44	0.15	0.94	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

Nome travata: **trave_506_IP1** Descrizione: **Trave_5 21-20-19-18**
ASTA NUM. 17 NI 298 NF 126 SEZ. Rp B= 0.400 H= 0.500 (trave)

categoria: p.p. y Permanente Neve qy tot.
qy medio: 500.00 2627.25 282.50 3409.75 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-1362	7227	-17	0	-12	-3726	4.02	4.02	4.02	4.02	3	0.50	0.16	0.96	0.00	0.00	16.8
2	0	-1084	5514	-145	0	-403	-2745	4.02	4.02	4.02	4.02	2	0.40	0.12	0.73	0.00	0.00	16.8
3	0	-953	5633	-146	0	-402	-3043	4.02	4.02	4.02	4.02	2	0.44	0.12	0.75	0.00	0.00	16.8
4	0	-1143	5485	119	0	383	-2688	4.02	4.02	4.02	4.02	2	0.39	0.12	0.73	0.00	0.00	16.8
5	0	-1011	5604	118	0	385	-2986	4.02	4.02	4.02	4.02	2	0.43	0.12	0.75	0.00	0.00	16.8

6	0	-1258	5365	-53	0	-129	-2378	4.02	4.02	4.02	4.02	2	0.34	0.12	0.71	0.00	0.00	16.8
7	0	-820	5762	-53	0	-125	-3371	4.02	4.02	4.02	4.02	2	0.49	0.13	0.77	0.00	0.00	16.8
8	0	-1276	5356	27	0	107	-2361	4.02	4.02	4.02	4.02	2	0.34	0.12	0.71	0.00	0.00	16.8
9	0	-837	5753	26	0	111	-3354	4.02	4.02	4.02	4.02	2	0.49	0.12	0.77	0.00	0.00	16.8
10	0	-1084	5514	-145	0	-403	-2745	4.02	4.02	4.02	4.02	2	0.40	0.12	0.73	0.00	0.00	16.8
11	0	-953	5633	-146	0	-402	-3043	4.02	4.02	4.02	4.02	2	0.44	0.12	0.75	0.00	0.00	16.8
12	0	-1143	5485	119	0	383	-2688	4.02	4.02	4.02	4.02	2	0.39	0.12	0.73	0.00	0.00	16.8
13	0	-1011	5604	118	0	385	-2986	4.02	4.02	4.02	4.02	2	0.43	0.12	0.75	0.00	0.00	16.8
14	0	-1258	5365	-53	0	-129	-2378	4.02	4.02	4.02	4.02	2	0.34	0.12	0.71	0.00	0.00	16.8
15	0	-820	5762	-53	0	-125	-3371	4.02	4.02	4.02	4.02	2	0.49	0.13	0.77	0.00	0.00	16.8
16	0	-1276	5356	27	0	107	-2361	4.02	4.02	4.02	4.02	2	0.34	0.12	0.71	0.00	0.00	16.8
17	0	-837	5753	26	0	111	-3354	4.02	4.02	4.02	4.02	2	0.49	0.12	0.77	0.00	0.00	16.8
18	0	-1544	7836	-412	0	-1138	-3696	4.02	4.02	4.02	4.02	3	0.50	0.17	1.03	1.94	0.00	16.8
19	0	-1799	7704	382	0	1179	-3425	4.02	4.02	4.02	4.02	3	0.46	0.17	1.01	1.91	0.00	16.8
20	0	-1841	7848	-40	0	-65	-3822	4.02	4.02	4.02	4.02	3	0.51	0.17	1.03	1.95	0.00	16.8
37	0	-1340	7560	-677	0	-1921	-3746	4.02	4.02	4.02	4.02	3	0.51	0.16	1.00	1.87	0.00	16.8
38	0	-1764	7340	645	0	1940	-3294	4.02	4.02	4.02	4.02	3	0.44	0.16	0.96	0.00	0.00	16.8
39	0	-1834	7580	-57	0	-133	-3957	4.02	4.02	4.02	4.02	3	0.53	0.16	0.99	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	38	-1362	5702	-17	0	-5	-3726	4.02	4.02	4.02	4.02	3	0.50	0.12	0.75	0.00	0.00	16.8
2	38	-1084	4341	-145	0	-349	-2745	4.02	4.02	4.02	4.02	2	0.40	0.09	0.58	0.00	0.00	16.8
3	38	-953	4460	-146	0	-347	-3043	4.02	4.02	4.02	4.02	2	0.44	0.10	0.59	0.00	0.00	16.8
4	38	-1143	4312	119	0	339	-2688	4.02	4.02	4.02	4.02	2	0.39	0.09	0.57	0.00	0.00	16.8
5	38	-1011	4431	118	0	340	-2986	4.02	4.02	4.02	4.02	2	0.43	0.10	0.59	0.00	0.00	16.8
6	38	-1258	4192	-53	0	-110	-2378	4.02	4.02	4.02	4.02	2	0.34	0.09	0.56	0.00	0.00	16.8
7	38	-820	4589	-53	0	-105	-3371	4.02	4.02	4.02	4.02	2	0.49	0.10	0.61	0.00	0.00	16.8
8	38	-1276	4183	27	0	97	-2361	4.02	4.02	4.02	4.02	2	0.34	0.09	0.55	0.00	0.00	16.8
9	38	-837	4580	26	0	101	-3354	4.02	4.02	4.02	4.02	2	0.49	0.10	0.61	0.00	0.00	16.8
10	38	-1084	4341	-145	0	-349	-2745	4.02	4.02	4.02	4.02	2	0.40	0.09	0.58	0.00	0.00	16.8
11	38	-953	4460	-146	0	-347	-3043	4.02	4.02	4.02	4.02	2	0.44	0.10	0.59	0.00	0.00	16.8
12	38	-1143	4312	119	0	339	-2688	4.02	4.02	4.02	4.02	2	0.39	0.09	0.57	0.00	0.00	16.8
13	38	-1011	4431	118	0	340	-2986	4.02	4.02	4.02	4.02	2	0.43	0.10	0.59	0.00	0.00	16.8
14	38	-1258	4192	-53	0	-110	-2378	4.02	4.02	4.02	4.02	2	0.34	0.09	0.56	0.00	0.00	16.8
15	38	-820	4589	-53	0	-105	-3371	4.02	4.02	4.02	4.02	2	0.49	0.10	0.61	0.00	0.00	16.8
16	38	-1276	4183	27	0	97	-2361	4.02	4.02	4.02	4.02	2	0.34	0.09	0.55	0.00	0.00	16.8
17	38	-837	4580	26	0	101	-3354	4.02	4.02	4.02	4.02	2	0.49	0.10	0.61	0.00	0.00	16.8
18	38	-1544	6153	-412	0	-984	-3696	4.02	4.02	4.02	4.02	3	0.50	0.13	0.81	0.00	0.00	16.8
19	38	-1799	6021	382	0	1036	-3425	4.02	4.02	4.02	4.02	3	0.46	0.13	0.79	0.00	0.00	16.8
20	38	-1841	6165	-40	0	-50	-3822	4.02	4.02	4.02	4.02	3	0.51	0.13	0.81	0.00	0.00	16.8
37	38	-1340	5956	-677	0	-1667	-3746	4.02	4.02	4.02	4.02	3	0.51	0.13	0.79	0.00	0.00	16.8
38	38	-1764	5736	645	0	1698	-3294	4.02	4.02	4.02	4.02	3	0.44	0.12	0.75	0.00	0.00	16.8
39	38	-1834	5976	-57	0	-112	-3957	4.02	4.02	4.02	4.02	3	0.53	0.13	0.78	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	75	-1362	4178	-17	0	1	2666	4.02	4.02	4.02	4.02	3	0.36	0.09	0.55	0.00	0.00	16.8
2	75	-1084	3169	-145	0	-294	2096	4.02	4.02	4.02	4.02	2	0.30	0.07	0.42	0.00	0.00	16.8
3	75	-953	3288	-146	0	-293	1966	4.02	4.02	4.02	4.02	2	0.29	0.07	0.44	0.00	0.00	16.8
4	75	-1143	3140	119	0	294	2099	4.02	4.02	4.02	4.02	2	0.30	0.07	0.42	0.00	0.00	16.8
5	75	-1011	3259	118	0	296	1987	4.02	4.02	4.02	4.02	2	0.29	0.07	0.43	0.00	0.00	16.8
6	75	-1258	3020	-53	0	-90	2184	4.02	4.02	4.02	4.02	2	0.32	0.07	0.40	0.00	0.00	16.8
7	75	-820	3416	-53	0	-85	1800	4.02	4.02	4.02	4.02	2	0.26	0.07	0.46	0.00	0.00	16.8
8	75	-1276	3011	27	0	87	2185	4.02	4.02	4.02	4.02	2	0.32	0.07	0.40	0.00	0.00	16.8
9	75	-837	3408	26	0	92	1806	4.02	4.02	4.02	4.02	2	0.26	0.07	0.45	0.00	0.00	16.8
10	75	-1084	3169	-145	0	-294	2096	4.02	4.02	4.02	4.02	2	0.30	0.07	0.42	0.00	0.00	16.8
11	75	-953	3288	-146	0	-293	1966	4.02	4.02	4.02	4.02	2	0.29	0.07	0.44	0.00	0.00	16.8
12	75	-1143	3140	119	0	294	2099	4.02	4.02	4.02	4.02	2	0.30	0.07	0.42	0.00	0.00	16.8
13	75	-1011	3259	118	0	296	1987	4.02	4.02	4.02	4.02	2	0.29	0.07	0.43	0.00	0.00	16.8
14	75	-1258	3020	-53	0	-90	2184	4.02	4.02	4.02	4.02	2	0.32	0.07	0.40	0.00	0.00	16.8
15	75	-820	3416	-53	0	-85	1800	4.02	4.02	4.02	4.02	2	0.26	0.07	0.46	0.00	0.00	16.8
16	75	-1276	3011	27	0	87	2185	4.02	4.02	4.02	4.02	2	0.32	0.07	0.40	0.00	0.00	16.8
17	75	-837	3408	26	0	92	1806	4.02	4.02	4.02	4.02	2	0.26	0.07	0.45	0.00	0.00	16.8
18	75	-1544	4469	-412	0	-829	3106	4.02	4.02	4.02	4.02	3	0.42	0.10	0.59	0.00	0.00	16.8
19	75	-1799	4337	382	0	893	3129	4.02	4.02	4.02	4.02	3	0.42	0.09	0.57	0.00	0.00	16.8
20	75	-1841	4481	-40	0	-35	3002	4.02	4.02	4.02	4.02	3	0.40	0.10	0.59	0.00	0.00	16.8
37	75	-1340	4352	-677	0	-1413	2911	4.02	4.02	4.02	4.02	3	0.39	0.09	0.58	0.00	0.00	16.8
38	75	-1764	4132	645	0	1456	2949	4.02	4.02	4.02	4.02	3	0.39	0.09	0.54	0.00	0.00	16.8
39	75	-1834	4372	-57	0	-90	2737	4.02	4.02	4.02	4.02	3	0.36	0.09	0.57	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	112	-1362	2653	-17	0	8	2678	4.02	4.02	4.02	4.02	3	0.36	0.06	0.35	0.00	0.00	16.8
2	112	-1084	1996	-145	0	-240	2096	4.02	4.02	4.02	4.02	2	0.30	0.04	0.27	0.00	0.00	16.8
3	112	-953	2115	-146	0	-238	2021	4.02	4.02	4.02	4.02	2	0.29	0.05	0.28	0.00	0.00	16.8
4	112	-1143	1967	119	0	250	2099	4.02	4.02	4.02	4.02	2	0.30	0.04	0.26	0.00	0.00	16.8
5	112	-1011	2086	118	0	251	2025	4.02	4.02	4.02	4.02	2	0.29	0.05	0.28	0.00	0.00	16.8
6	112	-1258	1847	-53	0	-70	2184	4.02	4.02	4.02	4.02	2	0.32	0.04	0.24	0.00	0.00	16.8
7	112	-820	2244	-53	0	-65	1935	4.02	4.02	4.02	4.02	2	0.28	0.05	0.30	0.00	0.00	16.8
8	112	-1276	1838	27	0	77	2185	4.02	4.02	4.02	4.02	2	0.32	0.04	0.24	0.00	0.00	16.8
9	112	-837	2235	26	0	82	1936	4.02	4.02	4.02	4.02	2	0.28	0.05	0.30	0.00	0.00	16.8
10	112	-1084	1996	-145	0	-240	2096	4.02	4.02	4.02	4.02	2	0.30	0.04	0.27	0.00	0.00	16.8
11	112	-953	2115	-146	0	-238	2021	4.02	4.02	4.02	4.02	2	0.29	0.05	0.28	0.00	0.00	16.8
12	112	-1143	1967	119	0	250	2099	4.02	4.02	4.02	4.02	2	0.30	0.04	0.26	0.00	0.00	16.8
13	112	-1011	2086	118	0	251	2025	4.02	4.02	4.02	4.02	2	0.29	0.05	0.28	0.00	0.00	16.8
14	112	-1258	1847	-53	0	-70	2184	4.02	4.02	4.02	4.02	2	0.32	0.04	0.24	0.00	0.00	16.8
15	112	-820	2244	-53	0	-65	1935	4.02	4.02	4.02	4.02	2	0.28	0.05	0.30	0.00	0.00	16.8
16	112	-1276	1838	27	0	77	2185	4.02	4.02	4.02	4.02	2	0.32	0.04	0.24	0.00	0.00	16.8
17	112	-837	2235	26	0	82	1936	4.02	4.02	4.02	4.02	2	0.28	0.05	0.30	0.00	0.00	16.8
18	112	-1544	2786	-412	0	-675	3106	4.02	4.02	4.02	4.02	3	0.42	0.06	0.37	0.00	0.00	16.8
19	112	-1799	2654	382	0	749	3129	4.02	4.02	4.02	4.02	3	0.42	0.06	0.35	0.00	0.00	16.8
20	112	-1841	2798	-40	0	-20	3002	4.02	4.02	4.02	4.02	3	0.40	0.06	0.37	0.00	0.00	16.8
37	112	-1340	2748	-677	0	-1159	2911	4.02	4.02	4.02	4.02	3	0.39	0.06	0.36	0.00	0.00	16.8
38	112	-1764	2528	645	0	1214	2949	4.02	4.02	4.02	4.02	3	0.39	0.05	0.33	0.00	0.00	16.8
39	112	-1834	2768	-57	0	-69	2737	4.02	4.02	4.02	4.02	3	0.36	0.06	0.36	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	150	-1362	1129	-17	0	14	2678	4.02	4.02	4.02	4.02	3	0.36	0.02	0.15	0.00	0.00	16.8
2	150	-1084	823	-145	0	-185	2096	4.02	4.02	4.02	4.02	2	0.30	0.02	0.11	0.00	0.00	16.8
3	150	-953	942	-146	0	-184	2021	4.02	4.02	4.02	4.02	2	0.29	0.02	0.13	0.00	0.00	16.8
4	150	-1143	794	119	0	205	2099	4.02	4.02	4.02	4.02	2	0.30	0.02	0.11	0.00	0.00	16.8
5	150	-1011	913	118	0	207	2025	4.02	4.02	4.02	4.02	2	0.29	0.02	0.12	0.00	0.00	16.8
6	150	-1258	674	-53	0	-50	2184	4.02	4.02	4.02	4.02	2	0.32	0.01	0.09	0.00	0.00	16.8
7	150	-820	1071	-53	0	-45	1935	4.02	4.02	4.02	4.02	2	0.28	0.02	0.14	0.00	0.00	16.8
8	150	-1276	665	27	0	67	2185	4.02	4.02	4.02	4.02	2	0.32	0.01	0.09	0.00	0.00	16.8
9	150	-837	1062	26	0	72	1936	4.02	4.02	4.02	4.02	2	0.28	0.02	0.14	0.00	0.00	16.8
10	150	-1084	823	-145	0	-185	2096	4.02	4.02	4.02	4.02	2	0.30	0.02	0.11	0.00	0.00	16.8
11	150	-953	942	-146	0	-184	2021	4.02	4.02	4.02	4.02	2	0.29	0.02	0.13	0.00	0.00	16.8

12	150	-1143	794	119	0	205	2099	4.02	4.02	4.02	4.02	2	0.30	0.02	0.11	0.00	0.00	16.8
13	150	-1011	913	118	0	207	2025	4.02	4.02	4.02	4.02	2	0.29	0.02	0.12	0.00	0.00	16.8
14	150	-1258	674	-53	0	-50	2184	4.02	4.02	4.02	4.02	2	0.32	0.01	0.09	0.00	0.00	16.8
15	150	-820	1071	-53	0	-45	1935	4.02	4.02	4.02	4.02	2	0.28	0.02	0.14	0.00	0.00	16.8
16	150	-1276	665	27	0	67	2185	4.02	4.02	4.02	4.02	2	0.32	0.01	0.09	0.00	0.00	16.8
17	150	-837	1062	26	0	72	1936	4.02	4.02	4.02	4.02	2	0.28	0.02	0.14	0.00	0.00	16.8
18	150	-1544	1102	-412	0	-520	3106	4.02	4.02	4.02	4.02	3	0.42	0.02	0.15	0.00	0.00	16.8
19	150	-1799	970	382	0	606	3129	4.02	4.02	4.02	4.02	3	0.42	0.02	0.13	0.00	0.00	16.8
20	150	-1841	1114	-40	0	-5	3002	4.02	4.02	4.02	4.02	3	0.40	0.02	0.15	0.00	0.00	16.8
37	150	-1340	1144	-677	0	-905	2911	4.02	4.02	4.02	4.02	3	0.39	0.02	0.15	0.00	0.00	16.8
38	150	-1764	924	645	0	972	2949	4.02	4.02	4.02	4.02	3	0.39	0.02	0.12	0.00	0.00	16.8
39	150	-1834	1164	-57	0	-47	2737	4.02	4.02	4.02	4.02	3	0.36	0.03	0.15	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	188	-1362	-396	-17	0	21	2678	4.02	4.02	4.02	4.02	3	0.36	0.01	0.05	0.00	0.00	16.8
2	188	-1084	-350	-145	0	-131	2096	4.02	4.02	4.02	4.02	2	0.30	0.01	0.05	0.00	0.00	16.8
3	188	-953	-230	-146	0	-129	2021	4.02	4.02	4.02	4.02	2	0.29	0.00	0.03	0.00	0.00	16.8
4	188	-1143	-378	119	0	161	2099	4.02	4.02	4.02	4.02	2	0.30	0.01	0.05	0.00	0.00	16.8
5	188	-1011	-260	118	0	163	2025	4.02	4.02	4.02	4.02	2	0.29	0.01	0.03	0.00	0.00	16.8
6	188	-1258	-498	-53	0	-31	2184	4.02	4.02	4.02	4.02	2	0.32	0.01	0.07	0.00	0.00	16.8
7	188	-820	-102	-53	0	-25	1935	4.02	4.02	4.02	4.02	2	0.28	0.00	0.01	0.00	0.00	16.8
8	188	-1276	-508	27	0	57	2185	4.02	4.02	4.02	4.02	2	0.32	0.01	0.07	0.00	0.00	16.8
9	188	-837	-110	26	0	63	1936	4.02	4.02	4.02	4.02	2	0.28	0.00	0.01	0.00	0.00	16.8
10	188	-1084	-350	-145	0	-131	2096	4.02	4.02	4.02	4.02	2	0.30	0.01	0.05	0.00	0.00	16.8
11	188	-953	-230	-146	0	-129	2021	4.02	4.02	4.02	4.02	2	0.29	0.00	0.03	0.00	0.00	16.8
12	188	-1143	-378	119	0	161	2099	4.02	4.02	4.02	4.02	2	0.30	0.01	0.05	0.00	0.00	16.8
13	188	-1011	-260	118	0	163	2025	4.02	4.02	4.02	4.02	2	0.29	0.01	0.03	0.00	0.00	16.8
14	188	-1258	-498	-53	0	-31	2184	4.02	4.02	4.02	4.02	2	0.32	0.01	0.07	0.00	0.00	16.8
15	188	-820	-102	-53	0	-25	1935	4.02	4.02	4.02	4.02	2	0.28	0.00	0.01	0.00	0.00	16.8
16	188	-1276	-508	27	0	57	2185	4.02	4.02	4.02	4.02	2	0.32	0.01	0.07	0.00	0.00	16.8
17	188	-837	-110	26	0	63	1936	4.02	4.02	4.02	4.02	2	0.28	0.00	0.01	0.00	0.00	16.8
18	188	-1544	-581	-412	0	-366	3106	4.02	4.02	4.02	4.02	3	0.42	0.01	0.08	0.00	0.00	16.8
19	188	-1799	-713	382	0	463	3129	4.02	4.02	4.02	4.02	3	0.42	0.02	0.09	0.00	0.00	16.8
20	188	-1841	-569	-40	0	10	3002	4.02	4.02	4.02	4.02	3	0.40	0.01	0.07	0.00	0.00	16.8
37	188	-1340	-460	-677	0	-651	2911	4.02	4.02	4.02	4.02	3	0.39	0.02	0.09	0.00	0.00	16.8
38	188	-1764	-680	645	0	730	2949	4.02	4.02	4.02	4.02	3	0.39	0.01	0.09	0.00	0.00	16.8
39	188	-1834	-440	-57	0	-26	2737	4.02	4.02	4.02	4.02	3	0.36	0.01	0.06	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	225	-1362	-1921	-17	0	27	2678	4.02	4.02	4.02	4.02	3	0.36	0.04	0.25	0.00	0.00	16.8
2	225	-1084	-1522	-145	0	-76	2096	4.02	4.02	4.02	4.02	2	0.30	0.03	0.20	0.00	0.00	16.8
3	225	-953	-1403	-146	0	-74	2021	4.02	4.02	4.02	4.02	2	0.29	0.03	0.19	0.00	0.00	16.8
4	225	-1143	-1551	119	0	116	2099	4.02	4.02	4.02	4.02	2	0.30	0.03	0.21	0.00	0.00	16.8
5	225	-1011	-1432	118	0	118	2025	4.02	4.02	4.02	4.02	2	0.29	0.03	0.19	0.00	0.00	16.8
6	225	-1258	-1671	-53	0	-11	2184	4.02	4.02	4.02	4.02	2	0.32	0.04	0.22	0.00	0.00	16.8
7	225	-820	-1275	-53	0	-5	1935	4.02	4.02	4.02	4.02	2	0.28	0.03	0.17	0.00	0.00	16.8
8	225	-1276	-1680	27	0	47	2185	4.02	4.02	4.02	4.02	2	0.32	0.04	0.22	0.00	0.00	16.8
9	225	-837	-1283	26	0	53	1936	4.02	4.02	4.02	4.02	2	0.28	0.03	0.17	0.00	0.00	16.8
10	225	-1084	-1522	-145	0	-76	2096	4.02	4.02	4.02	4.02	2	0.30	0.03	0.20	0.00	0.00	16.8
11	225	-953	-1403	-146	0	-74	2021	4.02	4.02	4.02	4.02	2	0.29	0.03	0.19	0.00	0.00	16.8
12	225	-1143	-1551	119	0	116	2099	4.02	4.02	4.02	4.02	2	0.30	0.03	0.21	0.00	0.00	16.8
13	225	-1011	-1432	118	0	118	2025	4.02	4.02	4.02	4.02	2	0.29	0.03	0.19	0.00	0.00	16.8
14	225	-1258	-1671	-53	0	-11	2184	4.02	4.02	4.02	4.02	2	0.32	0.04	0.22	0.00	0.00	16.8
15	225	-820	-1275	-53	0	-5	1935	4.02	4.02	4.02	4.02	2	0.28	0.03	0.17	0.00	0.00	16.8
16	225	-1276	-1680	27	0	47	2185	4.02	4.02	4.02	4.02	2	0.32	0.04	0.22	0.00	0.00	16.8
17	225	-837	-1283	26	0	53	1936	4.02	4.02	4.02	4.02	2	0.28	0.03	0.17	0.00	0.00	16.8
18	225	-1544	-2264	-412	0	-211	3106	4.02	4.02	4.02	4.02	3	0.42	0.05	0.30	0.00	0.00	16.8
19	225	-1799	-2396	382	0	320	3129	4.02	4.02	4.02	4.02	3	0.42	0.05	0.31	0.00	0.00	16.8
20	225	-1841	-2252	-40	0	25	3002	4.02	4.02	4.02	4.02	3	0.40	0.05	0.30	0.00	0.00	16.8
37	225	-1340	-2064	-677	0	-398	2911	4.02	4.02	4.02	4.02	3	0.39	0.04	0.27	0.00	0.00	16.8
38	225	-1764	-2284	645	0	488	2949	4.02	4.02	4.02	4.02	3	0.39	0.05	0.30	0.00	0.00	16.8
39	225	-1834	-2044	-57	0	-4	2737	4.02	4.02	4.02	4.02	3	0.36	0.04	0.27	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	262	-1362	-3445	-17	0	34	2678	4.02	4.02	4.02	4.02	3	0.36	0.07	0.46	0.00	0.00	16.8
2	262	-1084	-2695	-145	0	-22	2096	4.02	4.02	4.02	4.02	2	0.30	0.06	0.36	0.00	0.00	16.8
3	262	-953	-2576	-146	0	-20	2021	4.02	4.02	4.02	4.02	2	0.29	0.06	0.34	0.00	0.00	16.8
4	262	-1143	-2724	119	0	72	2099	4.02	4.02	4.02	4.02	2	0.30	0.06	0.36	0.00	0.00	16.8
5	262	-1011	-2605	118	0	74	2025	4.02	4.02	4.02	4.02	2	0.29	0.06	0.35	0.00	0.00	16.8
6	262	-1258	-2844	-53	0	9	2184	4.02	4.02	4.02	4.02	2	0.32	0.06	0.38	0.00	0.00	16.8
7	262	-820	-2448	-53	0	15	1935	4.02	4.02	4.02	4.02	2	0.28	0.05	0.33	0.00	0.00	16.8
8	262	-1276	-2853	27	0	37	2185	4.02	4.02	4.02	4.02	2	0.32	0.06	0.38	0.00	0.00	16.8
9	262	-837	-2456	26	0	43	1936	4.02	4.02	4.02	4.02	2	0.28	0.05	0.33	0.00	0.00	16.8
10	262	-1084	-2695	-145	0	-22	2096	4.02	4.02	4.02	4.02	2	0.30	0.06	0.36	0.00	0.00	16.8
11	262	-953	-2576	-146	0	-20	2021	4.02	4.02	4.02	4.02	2	0.29	0.06	0.34	0.00	0.00	16.8
12	262	-1143	-2724	119	0	72	2099	4.02	4.02	4.02	4.02	2	0.30	0.06	0.36	0.00	0.00	16.8
13	262	-1011	-2605	118	0	74	2025	4.02	4.02	4.02	4.02	2	0.29	0.06	0.35	0.00	0.00	16.8
14	262	-1258	-2844	-53	0	9	2184	4.02	4.02	4.02	4.02	2	0.32	0.06	0.38	0.00	0.00	16.8
15	262	-820	-2448	-53	0	15	1935	4.02	4.02	4.02	4.02	2	0.28	0.05	0.33	0.00	0.00	16.8
16	262	-1276	-2853	27	0	37	2185	4.02	4.02	4.02	4.02	2	0.32	0.06	0.38	0.00	0.00	16.8
17	262	-837	-2456	26	0	43	1936	4.02	4.02	4.02	4.02	2	0.28	0.05	0.33	0.00	0.00	16.8
18	262	-1544	-3948	-412	0	-57	3106	4.02	4.02	4.02	4.02	3	0.42	0.09	0.52	0.00	0.00	16.8
19	262	-1799	-4080	382	0	177	3129	4.02	4.02	4.02	4.02	3	0.42	0.09	0.54	0.00	0.00	16.8
20	262	-1841	-3936	-40	0	40	3002	4.02	4.02	4.02	4.02	3	0.40	0.09	0.52	0.00	0.00	16.8
37	262	-1340	-3668	-677	0	-144	2911	4.02	4.02	4.02	4.02	3	0.39	0.08	0.49	0.00	0.00	16.8
38	262	-1764	-3888	645	0	246	2949	4.02	4.02	4.02	4.02	3	0.39	0.08	0.51	0.00	0.00	16.8
39	262	-1834	-3648	-57	0	17	2737	4.02	4.02	4.02	4.02	3	0.36	0.08	0.48	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	300	-1362	-4970	-17	0	40	-2856	4.02	4.02	4.02	4.02	3	0.39	0.11	0.66	0.00	0.00	16.8
2	300	-1084	-3868	-145	0	33	-2235	4.02	4.02	4.02	4.02	2	0.32	0.08	0.51	0.00	0.00	16.8
3	300	-953	-3749	-146	0	35	-2115	4.02	4.02	4.02	4.02	2	0.31	0.08	0.50	0.00	0.00	16.8
4	300	-1143	-3897	119	0	28	-2278	4.02	4.02	4.02	4.02	2	0.33	0.08	0.52	0.00	0.00	16.8
5	300	-1011	-3778	118	0	30	-2159	4.02	4.02	4.02	4.02	2	0.31	0.08	0.50	0.00	0.00	16.8
6	300	-1258	-4017	-53	0	28	-2390	4.02	4.02	4.02	4.02	2	0.35	0.09	0.53	0.00	0.00	16.8
7	300	-820	-3620	-53	0	35	-1991	4.02	4.02	4.02	4.02	2	0.29	0.08	0.48	0.00	0.00	16.8
8	300	-1276	-4026	27	0	27	-2403	4.02	4.02	4.02	4.02	2	0.35	0.09	0.53	0.00	0.00	16.8
9	300	-837	-3629	26	0	34	-2004	4.02	4.02	4.02	4.02	2	0.29	0.08	0.48	0.00	0.00	16.8
10	300	-1084	-3868	-145	0	33	-2235	4.02	4.02	4.02	4.02	2	0.32	0.08	0.51	0.00	0.00	16.8
11	300	-953	-3749	-146	0	35	-2115	4.02	4.02	4.02	4.02	2	0.31	0.08	0.50	0.00	0.00	16.8
12	300	-1143	-3897	119	0	28	-2278	4.02	4.02	4.02	4.02	2	0.33	0.08	0.52	0.00	0.00	16.8
13	300	-1011	-3778	118	0	30	-2159	4.02	4.02	4.02	4.02	2	0.31	0.08	0.50	0.00	0.00	16.8
14	300	-1258	-4017	-53	0	28	-2390	4.02	4.02	4.02	4.02	2	0.35	0.09	0.53	0.00	0.00	16.8
15	300	-820	-3620	-53	0	35	-1991	4.02	4.02	4.02	4.02	2	0.29	0.08	0.48	0.00	0.00	16.8
16	300	-1276	-4026	27	0	27	-2403	4.02	4.02	4.02	4.02	2	0.35	0.09	0.53	0.00	0.00	16.8
17	300	-837	-3629	26	0	34	-2004	4.02	4.02	4.02	4.02	2	0.29	0.08	0.48	0.00	0.00	16.8

18	300	-1544	-5631	-412	0	98	-3240	4.02	4.02	4.02	4.02	3	0.43	0.12	0.74	0.00	0.00	16.8
19	300	-1799	-5763	382	0	34	-3431	4.02	4.02	4.02	4.02	3	0.46	0.12	0.76	0.00	0.00	16.8
20	300	-1841	-5619	-40	0	55	-3324	4.02	4.02	4.02	4.02	3	0.44	0.12	0.74	0.00	0.00	16.8
37	300	-1340	-5272	-677	0	110	-2982	4.02	4.02	4.02	4.02	3	0.40	0.11	0.70	0.00	0.00	16.8
38	300	-1764	-5492	645	0	4	-3303	4.02	4.02	4.02	4.02	3	0.44	0.12	0.72	0.00	0.00	16.8
39	300	-1834	-5252	-57	0	39	-3123	4.02	4.02	4.02	4.02	3	0.42	0.11	0.69	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	338	-1362	-6494	-17	0	47	-5211	4.02	4.02	4.02	4.02	3	0.70	0.14	0.86	0.00	0.00	16.8
2	338	-1084	-5040	-145	0	87	-4058	4.02	4.02	4.02	4.02	2	0.59	0.11	0.67	0.00	0.00	16.8
3	338	-953	-4921	-146	0	89	-3909	4.02	4.02	4.02	4.02	2	0.57	0.11	0.66	0.00	0.00	16.8
4	338	-1143	-5069	119	0	-17	-4108	4.02	4.02	4.02	4.02	2	0.60	0.11	0.67	0.00	0.00	16.8
5	338	-1011	-4950	118	0	-15	-3959	4.02	4.02	4.02	4.02	2	0.58	0.11	0.66	0.00	0.00	16.8
6	338	-1258	-5189	-53	0	48	-4249	4.02	4.02	4.02	4.02	2	0.61	0.11	0.69	0.00	0.00	16.8
7	338	-820	-4793	-53	0	55	-3753	4.02	4.02	4.02	4.02	2	0.55	0.10	0.64	0.00	0.00	16.8
8	338	-1276	-5198	27	0	17	-4264	4.02	4.02	4.02	4.02	2	0.62	0.11	0.69	0.00	0.00	16.8
9	338	-837	-4801	26	0	24	-3768	4.02	4.02	4.02	4.02	2	0.55	0.10	0.64	0.00	0.00	16.8
10	338	-1084	-5040	-145	0	87	-4058	4.02	4.02	4.02	4.02	2	0.59	0.11	0.67	0.00	0.00	16.8
11	338	-953	-4921	-146	0	89	-3909	4.02	4.02	4.02	4.02	2	0.57	0.11	0.66	0.00	0.00	16.8
12	338	-1143	-5069	119	0	-17	-4108	4.02	4.02	4.02	4.02	2	0.60	0.11	0.67	0.00	0.00	16.8
13	338	-1011	-4950	118	0	-15	-3959	4.02	4.02	4.02	4.02	2	0.58	0.11	0.66	0.00	0.00	16.8
14	338	-1258	-5189	-53	0	48	-4249	4.02	4.02	4.02	4.02	2	0.61	0.11	0.69	0.00	0.00	16.8
15	338	-820	-4793	-53	0	55	-3753	4.02	4.02	4.02	4.02	2	0.55	0.10	0.64	0.00	0.00	16.8
16	338	-1276	-5198	27	0	17	-4264	4.02	4.02	4.02	4.02	2	0.62	0.11	0.69	0.00	0.00	16.8
17	338	-837	-4801	26	0	24	-3768	4.02	4.02	4.02	4.02	2	0.55	0.10	0.64	0.00	0.00	16.8
18	338	-1544	-7315	-412	0	252	-5875	4.02	4.02	4.02	4.02	3	0.79	0.16	0.96	0.00	0.00	16.8
19	338	-1799	-7447	382	0	-110	-6099	4.02	4.02	4.02	4.02	3	0.81	0.16	0.98	0.00	0.00	16.8
20	338	-1841	-7303	-40	0	70	-5956	4.02	4.02	4.02	4.02	3	0.79	0.16	0.96	0.00	0.00	16.8
37	338	-1340	-6876	-677	0	364	-5470	4.02	4.02	4.02	4.02	3	0.74	0.15	0.91	0.00	0.00	16.8
38	338	-1764	-7096	645	0	-238	-5845	4.02	4.02	4.02	4.02	3	0.78	0.15	0.93	0.00	0.00	16.8
39	338	-1834	-6856	-57	0	60	-5606	4.02	4.02	4.02	4.02	3	0.75	0.15	0.90	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	375	-1362	-8019	-17	0	54	-5211	4.02	4.02	4.02	4.02	3	0.70	0.17	1.06	1.99	0.00	16.8
2	375	-1084	-6213	-145	0	142	-4058	4.02	4.02	4.02	4.02	2	0.59	0.13	0.83	0.00	0.00	16.8
3	375	-953	-6094	-146	0	144	-3909	4.02	4.02	4.02	4.02	2	0.57	0.13	0.81	0.00	0.00	16.8
4	375	-1143	-6242	119	0	-61	-4108	4.02	4.02	4.02	4.02	2	0.60	0.14	0.83	0.00	0.00	16.8
5	375	-1011	-6123	118	0	-59	-3959	4.02	4.02	4.02	4.02	2	0.58	0.13	0.81	0.00	0.00	16.8
6	375	-1258	-6362	-53	0	68	-4249	4.02	4.02	4.02	4.02	2	0.61	0.14	0.84	0.00	0.00	16.8
7	375	-820	-5966	-53	0	75	-3753	4.02	4.02	4.02	4.02	2	0.55	0.13	0.80	0.00	0.00	16.8
8	375	-1276	-6371	27	0	7	-4264	4.02	4.02	4.02	4.02	2	0.62	0.14	0.84	0.00	0.00	16.8
9	375	-837	-5974	26	0	14	-3768	4.02	4.02	4.02	4.02	2	0.55	0.13	0.80	0.00	0.00	16.8
10	375	-1084	-6213	-145	0	142	-4058	4.02	4.02	4.02	4.02	2	0.59	0.13	0.83	0.00	0.00	16.8
11	375	-953	-6094	-146	0	144	-3909	4.02	4.02	4.02	4.02	2	0.57	0.13	0.81	0.00	0.00	16.8
12	375	-1143	-6242	119	0	-61	-4108	4.02	4.02	4.02	4.02	2	0.60	0.14	0.83	0.00	0.00	16.8
13	375	-1011	-6123	118	0	-59	-3959	4.02	4.02	4.02	4.02	2	0.58	0.13	0.81	0.00	0.00	16.8
14	375	-1258	-6362	-53	0	68	-4249	4.02	4.02	4.02	4.02	2	0.61	0.14	0.84	0.00	0.00	16.8
15	375	-820	-5966	-53	0	75	-3753	4.02	4.02	4.02	4.02	2	0.55	0.13	0.80	0.00	0.00	16.8
16	375	-1276	-6371	27	0	7	-4264	4.02	4.02	4.02	4.02	2	0.62	0.14	0.84	0.00	0.00	16.8
17	375	-837	-5974	26	0	14	-3768	4.02	4.02	4.02	4.02	2	0.55	0.13	0.80	0.00	0.00	16.8
18	375	-1544	-8998	-412	0	406	-5875	4.02	4.02	4.02	4.02	3	0.79	0.19	1.19	2.23	0.00	16.8
19	375	-1799	-9130	382	0	-253	-6099	4.02	4.02	4.02	4.02	3	0.81	0.20	1.20	2.26	0.00	16.8
20	375	-1841	-8986	-40	0	85	-5956	4.02	4.02	4.02	4.02	3	0.79	0.19	1.18	2.23	0.00	16.8
37	375	-1340	-8480	-677	0	618	-5470	4.02	4.02	4.02	4.02	3	0.74	0.18	1.12	2.10	0.00	16.8
38	375	-1764	-8700	645	0	-481	-5845	4.02	4.02	4.02	4.02	3	0.78	0.19	1.14	2.16	0.00	16.8
39	375	-1834	-8460	-57	0	82	-5606	4.02	4.02	4.02	4.02	3	0.75	0.18	1.11	2.10	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

Nome travata: **trave_506_IP1** Descrizione: **Trave_5 21-20-19-18**
ASTA NUM. 18 NI 126 NF 123 SEZ. Rp B= 0.400 H= 0.500 (trave)

categoria: p.p. y Permanente Neve qy tot.
qy medio: 500.00 2627.25 282.50 3409.75 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-1178	7951	-7	0	13	-4809	4.02	4.02	4.02	4.02	3	0.65	0.17	1.06	1.97	0.00	16.8
2	0	-916	6102	-67	0	-20	-3682	4.02	4.02	4.02	4.02	2	0.54	0.13	0.81	0.00	0.00	16.8
3	0	-867	6142	-68	0	-17	-3735	4.02	4.02	4.02	4.02	2	0.55	0.13	0.82	0.00	0.00	16.8
4	0	-945	6090	58	0	37	-3663	4.02	4.02	4.02	4.02	2	0.53	0.13	0.81	0.00	0.00	16.8
5	0	-896	6129	56	0	39	-3716	4.02	4.02	4.02	4.02	2	0.54	0.13	0.82	0.00	0.00	16.8
6	0	-984	6051	-22	0	-3	-3614	4.02	4.02	4.02	4.02	2	0.53	0.13	0.81	0.00	0.00	16.8
7	0	-820	6184	-26	0	5	-3789	4.02	4.02	4.02	4.02	2	0.56	0.13	0.83	0.00	0.00	16.8
8	0	-992	6047	16	0	14	-3609	4.02	4.02	4.02	4.02	2	0.53	0.13	0.81	0.00	0.00	16.8
9	0	-828	6181	11	0	22	-3784	4.02	4.02	4.02	4.02	2	0.55	0.13	0.83	0.00	0.00	16.8
10	0	-916	6102	-67	0	-20	-3682	4.02	4.02	4.02	4.02	2	0.54	0.13	0.81	0.00	0.00	16.8
11	0	-867	6142	-68	0	-17	-3735	4.02	4.02	4.02	4.02	2	0.55	0.13	0.82	0.00	0.00	16.8
12	0	-945	6090	58	0	37	-3663	4.02	4.02	4.02	4.02	2	0.53	0.13	0.81	0.00	0.00	16.8
13	0	-896	6129	56	0	39	-3716	4.02	4.02	4.02	4.02	2	0.54	0.13	0.82	0.00	0.00	16.8
14	0	-984	6051	-22	0	-3	-3614	4.02	4.02	4.02	4.02	2	0.53	0.13	0.81	0.00	0.00	16.8
15	0	-820	6184	-26	0	5	-3789	4.02	4.02	4.02	4.02	2	0.56	0.13	0.83	0.00	0.00	16.8
16	0	-992	6047	16	0	14	-3609	4.02	4.02	4.02	4.02	2	0.53	0.13	0.81	0.00	0.00	16.8
17	0	-828	6181	11	0	22	-3784	4.02	4.02	4.02	4.02	2	0.55	0.13	0.83	0.00	0.00	16.8
18	0	-1290	8750	-184	0	-41	-5284	4.02	4.02	4.02	4.02	3	0.71	0.19	1.16	2.17	0.00	16.8
19	0	-1415	8697	177	0	90	-5208	4.02	4.02	4.02	4.02	3	0.70	0.19	1.15	2.16	0.00	16.8
20	0	-1458	8650	-27	0	22	-5100	4.02	4.02	4.02	4.02	3	0.69	0.19	1.14	2.15	0.00	16.8
37	0	-1170	8373	-306	0	-89	-5083	4.02	4.02	4.02	4.02	3	0.69	0.18	1.11	2.08	0.00	16.8
38	0	-1379	8284	296	0	130	-4956	4.02	4.02	4.02	4.02	3	0.67	0.18	1.10	2.05	0.00	16.8
39	0	-1450	8205	-43	0	15	-4776	4.02	4.02	4.02	4.02	3	0.64	0.18	1.08	2.03	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	38	-1178	6426	-7	0	15	-4809	4.02	4.02	4.02	4.02	3	0.65	0.14	0.85	0.00	0.00	16.8
2	38	-916	4929	-67	0	5	-3682	4.02	4.02	4.02	4.02	2	0.54	0.11	0.66	0.00	0.00	16.8
3	38	-867	4969	-68	0	8	-3735	4.02	4.02	4.02	4.02	2	0.55	0.11	0.66	0.00	0.00	16.8
4	38	-945	4917	58	0	15	-3663	4.02	4.02	4.02	4.02	2	0.53	0.11	0.66	0.00	0.00	16.8
5	38	-896	4956	56	0	18	-3716	4.02	4.02	4.02	4.02	2	0.54	0.11	0.66	0.00	0.00	16.8
6	38	-984	4878	-22	0	6	-3614	4.02	4.02	4.02	4.02	2	0.53	0.11	0.65	0.00	0.00	16.8
7	38	-820	5011	-26	0	15	-3789	4.02	4.02	4.02	4.02	2	0.56	0.11	0.67	0.00	0.00	16.8
8	38	-992	4874	16	0	8	-3609	4.02	4.02	4.02	4.02	2	0.53	0.11	0.65	0.00	0.00	16.8
9	38	-828	5008	11	0	18	-3784	4.02	4.02	4.02	4.02	2	0.55	0.11	0.67	0.00	0.00	16.8

10	38	-916	4929	-67	0	5	-3682	4.02	4.02	4.02	4.02	2	0.54	0.11	0.66	0.00	0.00	16.8
11	38	-867	4969	-68	0	8	-3735	4.02	4.02	4.02	4.02	2	0.55	0.11	0.66	0.00	0.00	16.8
12	38	-945	4917	58	0	15	-3663	4.02	4.02	4.02	4.02	2	0.53	0.11	0.66	0.00	0.00	16.8
13	38	-896	4956	56	0	18	-3716	4.02	4.02	4.02	4.02	2	0.54	0.11	0.66	0.00	0.00	16.8
14	38	-984	4878	-22	0	6	-3614	4.02	4.02	4.02	4.02	2	0.53	0.11	0.65	0.00	0.00	16.8
15	38	-820	5011	-26	0	15	-3789	4.02	4.02	4.02	4.02	2	0.56	0.11	0.67	0.00	0.00	16.8
16	38	-992	4874	16	0	8	-3609	4.02	4.02	4.02	4.02	2	0.53	0.11	0.65	0.00	0.00	16.8
17	38	-828	5008	11	0	18	-3784	4.02	4.02	4.02	4.02	2	0.55	0.11	0.67	0.00	0.00	16.8
18	38	-1290	7067	-184	0	28	-5284	4.02	4.02	4.02	4.02	3	0.71	0.15	0.94	0.00	0.00	16.8
19	38	-1415	7014	177	0	24	-5208	4.02	4.02	4.02	4.02	3	0.70	0.15	0.93	0.00	0.00	16.8
20	38	-1458	6967	-27	0	32	-5100	4.02	4.02	4.02	4.02	3	0.69	0.15	0.92	0.00	0.00	16.8
37	38	-1170	6769	-306	0	26	-5083	4.02	4.02	4.02	4.02	3	0.69	0.15	0.90	0.00	0.00	16.8
38	38	-1379	6680	296	0	19	-4956	4.02	4.02	4.02	4.02	3	0.67	0.14	0.88	0.00	0.00	16.8
39	38	-1450	6601	-43	0	31	-4776	4.02	4.02	4.02	4.02	3	0.64	0.14	0.87	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	75	-1178	4902	-7	0	18	2492	4.02	4.02	4.02	4.02	3	0.34	0.11	0.65	0.00	0.00	16.8
2	75	-916	3757	-67	0	31	1917	4.02	4.02	4.02	4.02	2	0.28	0.08	0.50	0.00	0.00	16.8
3	75	-867	3797	-68	0	34	-1930	4.02	4.02	4.02	4.02	2	0.28	0.08	0.51	0.00	0.00	16.8
4	75	-945	3744	58	0	-6	1920	4.02	4.02	4.02	4.02	2	0.28	0.08	0.50	0.00	0.00	16.8
5	75	-896	3784	56	0	-3	1917	4.02	4.02	4.02	4.02	2	0.28	0.08	0.50	0.00	0.00	16.8
6	75	-984	3706	-22	0	14	1921	4.02	4.02	4.02	4.02	2	0.28	0.08	0.49	0.00	0.00	16.8
7	75	-820	3839	-26	0	25	-1974	4.02	4.02	4.02	4.02	2	0.29	0.08	0.51	0.00	0.00	16.8
8	75	-992	3702	16	0	3	1921	4.02	4.02	4.02	4.02	2	0.28	0.08	0.49	0.00	0.00	16.8
9	75	-828	3835	11	0	14	-1970	4.02	4.02	4.02	4.02	2	0.29	0.08	0.51	0.00	0.00	16.8
10	75	-916	3757	-67	0	31	1917	4.02	4.02	4.02	4.02	2	0.28	0.08	0.50	0.00	0.00	16.8
11	75	-867	3797	-68	0	34	-1930	4.02	4.02	4.02	4.02	2	0.28	0.08	0.51	0.00	0.00	16.8
12	75	-945	3744	58	0	-6	1920	4.02	4.02	4.02	4.02	2	0.28	0.08	0.50	0.00	0.00	16.8
13	75	-896	3784	56	0	-3	1917	4.02	4.02	4.02	4.02	2	0.28	0.08	0.50	0.00	0.00	16.8
14	75	-984	3706	-22	0	14	1921	4.02	4.02	4.02	4.02	2	0.28	0.08	0.49	0.00	0.00	16.8
15	75	-820	3839	-26	0	25	-1974	4.02	4.02	4.02	4.02	2	0.29	0.08	0.51	0.00	0.00	16.8
16	75	-992	3702	16	0	3	1921	4.02	4.02	4.02	4.02	2	0.28	0.08	0.49	0.00	0.00	16.8
17	75	-828	3835	11	0	14	-1970	4.02	4.02	4.02	4.02	2	0.29	0.08	0.51	0.00	0.00	16.8
18	75	-1290	5383	-184	0	97	2741	4.02	4.02	4.02	4.02	3	0.37	0.12	0.71	0.00	0.00	16.8
19	75	-1415	5330	177	0	-42	2751	4.02	4.02	4.02	4.02	3	0.37	0.12	0.70	0.00	0.00	16.8
20	75	-1458	5283	-27	0	42	2800	4.02	4.02	4.02	4.02	3	0.38	0.11	0.70	0.00	0.00	16.8
37	75	-1170	5165	-306	0	140	-2621	4.02	4.02	4.02	4.02	3	0.36	0.11	0.69	0.00	0.00	16.8
38	75	-1379	5076	296	0	-92	2624	4.02	4.02	4.02	4.02	3	0.35	0.11	0.67	0.00	0.00	16.8
39	75	-1450	4997	-43	0	48	2705	4.02	4.02	4.02	4.02	3	0.36	0.11	0.66	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	112	-1178	3377	-7	0	20	2952	4.02	4.02	4.02	4.02	3	0.40	0.07	0.45	0.00	0.00	16.8
2	112	-916	2584	-67	0	56	2263	4.02	4.02	4.02	4.02	2	0.33	0.06	0.34	0.00	0.00	16.8
3	112	-867	2624	-68	0	59	2285	4.02	4.02	4.02	4.02	2	0.33	0.06	0.35	0.00	0.00	16.8
4	112	-945	2572	58	0	-28	2258	4.02	4.02	4.02	4.02	2	0.33	0.06	0.34	0.00	0.00	16.8
5	112	-896	2611	56	0	-24	2280	4.02	4.02	4.02	4.02	2	0.33	0.06	0.35	0.00	0.00	16.8
6	112	-984	2533	-22	0	22	2235	4.02	4.02	4.02	4.02	2	0.33	0.05	0.34	0.00	0.00	16.8
7	112	-820	2666	-26	0	34	2310	4.02	4.02	4.02	4.02	2	0.34	0.06	0.36	0.00	0.00	16.8
8	112	-992	2529	16	0	-3	2233	4.02	4.02	4.02	4.02	2	0.33	0.05	0.34	0.00	0.00	16.8
9	112	-828	2663	11	0	9	2308	4.02	4.02	4.02	4.02	2	0.34	0.06	0.36	0.00	0.00	16.8
10	112	-916	2584	-67	0	56	2263	4.02	4.02	4.02	4.02	2	0.33	0.06	0.34	0.00	0.00	16.8
11	112	-867	2624	-68	0	59	2285	4.02	4.02	4.02	4.02	2	0.33	0.06	0.35	0.00	0.00	16.8
12	112	-945	2572	58	0	-28	2258	4.02	4.02	4.02	4.02	2	0.33	0.06	0.34	0.00	0.00	16.8
13	112	-896	2611	56	0	-24	2280	4.02	4.02	4.02	4.02	2	0.33	0.06	0.35	0.00	0.00	16.8
14	112	-984	2533	-22	0	22	2235	4.02	4.02	4.02	4.02	2	0.33	0.05	0.34	0.00	0.00	16.8
15	112	-820	2666	-26	0	34	2310	4.02	4.02	4.02	4.02	2	0.34	0.06	0.36	0.00	0.00	16.8
16	112	-992	2529	16	0	-3	2233	4.02	4.02	4.02	4.02	2	0.33	0.05	0.34	0.00	0.00	16.8
17	112	-828	2663	11	0	9	2308	4.02	4.02	4.02	4.02	2	0.34	0.06	0.36	0.00	0.00	16.8
18	112	-1290	3700	-184	0	166	3232	4.02	4.02	4.02	4.02	3	0.44	0.08	0.49	0.00	0.00	16.8
19	112	-1415	3647	177	0	-108	3208	4.02	4.02	4.02	4.02	3	0.43	0.08	0.48	0.00	0.00	16.8
20	112	-1458	3600	-27	0	52	3228	4.02	4.02	4.02	4.02	3	0.43	0.08	0.48	0.00	0.00	16.8
37	112	-1170	3561	-306	0	255	3097	4.02	4.02	4.02	4.02	3	0.42	0.08	0.47	0.00	0.00	16.8
38	112	-1379	3472	296	0	-203	3058	4.02	4.02	4.02	4.02	3	0.41	0.08	0.46	0.00	0.00	16.8
39	112	-1450	3393	-43	0	64	3090	4.02	4.02	4.02	4.02	3	0.42	0.07	0.45	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	150	-1178	1853	-7	0	23	2952	4.02	4.02	4.02	4.02	3	0.40	0.04	0.25	0.00	0.00	16.8
2	150	-916	1411	-67	0	81	2263	4.02	4.02	4.02	4.02	2	0.33	0.03	0.19	0.00	0.00	16.8
3	150	-867	1451	-68	0	85	2285	4.02	4.02	4.02	4.02	2	0.33	0.03	0.19	0.00	0.00	16.8
4	150	-945	1399	58	0	-50	2258	4.02	4.02	4.02	4.02	2	0.33	0.03	0.19	0.00	0.00	16.8
5	150	-896	1438	56	0	-45	2280	4.02	4.02	4.02	4.02	2	0.33	0.03	0.19	0.00	0.00	16.8
6	150	-984	1360	-22	0	30	2235	4.02	4.02	4.02	4.02	2	0.33	0.03	0.18	0.00	0.00	16.8
7	150	-820	1493	-26	0	44	2310	4.02	4.02	4.02	4.02	2	0.34	0.03	0.20	0.00	0.00	16.8
8	150	-992	1356	16	0	-9	2233	4.02	4.02	4.02	4.02	2	0.33	0.03	0.18	0.00	0.00	16.8
9	150	-828	1490	11	0	5	2308	4.02	4.02	4.02	4.02	2	0.34	0.03	0.20	0.00	0.00	16.8
10	150	-916	1411	-67	0	81	2263	4.02	4.02	4.02	4.02	2	0.33	0.03	0.19	0.00	0.00	16.8
11	150	-867	1451	-68	0	85	2285	4.02	4.02	4.02	4.02	2	0.33	0.03	0.19	0.00	0.00	16.8
12	150	-945	1399	58	0	-50	2258	4.02	4.02	4.02	4.02	2	0.33	0.03	0.19	0.00	0.00	16.8
13	150	-896	1438	56	0	-45	2280	4.02	4.02	4.02	4.02	2	0.33	0.03	0.19	0.00	0.00	16.8
14	150	-984	1360	-22	0	30	2235	4.02	4.02	4.02	4.02	2	0.33	0.03	0.18	0.00	0.00	16.8
15	150	-820	1493	-26	0	44	2310	4.02	4.02	4.02	4.02	2	0.34	0.03	0.20	0.00	0.00	16.8
16	150	-992	1356	16	0	-9	2233	4.02	4.02	4.02	4.02	2	0.33	0.03	0.18	0.00	0.00	16.8
17	150	-828	1490	11	0	5	2308	4.02	4.02	4.02	4.02	2	0.34	0.03	0.20	0.00	0.00	16.8
18	150	-1290	2016	-184	0	235	3232	4.02	4.02	4.02	4.02	3	0.44	0.04	0.27	0.00	0.00	16.8
19	150	-1415	1963	177	0	-175	3208	4.02	4.02	4.02	4.02	3	0.43	0.04	0.26	0.00	0.00	16.8
20	150	-1458	1916	-27	0	62	3228	4.02	4.02	4.02	4.02	3	0.43	0.04	0.25	0.00	0.00	16.8
37	150	-1170	1957	-306	0	370	3097	4.02	4.02	4.02	4.02	3	0.42	0.04	0.26	0.00	0.00	16.8
38	150	-1379	1868	296	0	-314	3058	4.02	4.02	4.02	4.02	3	0.41	0.04	0.25	0.00	0.00	16.8
39	150	-1450	1789	-43	0	80	3090	4.02	4.02	4.02	4.02	3	0.42	0.04	0.24	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	188	-1178	328	-7	0	25	2952	4.02	4.02	4.02	4.02	3	0.40	0.01	0.04	0.00	0.00	16.8
2	188	-916	238	-67	0	106	2263	4.02	4.02	4.02	4.02	2	0.33	0.01	0.03	0.00	0.00	16.8
3	188	-867	278	-68	0	110	2285	4.02	4.02	4.02	4.02	2	0.33	0.01	0.04	0.00	0.00	16.8
4	188	-945	226	58	0	-71	2258	4.02	4.02	4.02	4.02	2	0.33	0.00	0.03	0.00	0.00	16.8
5	188	-896	266	56	0	-67	2280	4.02	4.02	4.02	4.02	2	0.33	0.01	0.04	0.00	0.00	16.8
6	188	-984	188	-22	0	38	2235	4.02	4.02	4.02	4.02	2	0.33	0.00	0.02	0.00	0.00	16.8
7	188	-820	320	-26	0	54	2310	4.02	4.02	4.02	4.02	2	0.34	0.01	0.04	0.00	0.00	16.8
8	188	-992	184	16	0	-15	2233	4.02	4.02	4.02	4.02	2	0.33	0.00	0.02	0.00	0.00	16.8
9	188	-828	317	11	0	1	2308	4.02	4.02	4.02	4.02	2	0.34	0.01	0.04	0.00	0.00	16.8
10	188	-916	238	-67	0	106	2263	4.02	4.02	4.02	4.02	2	0.33	0.01	0.03	0.00	0.00	16.8
11	188	-867	278	-68	0	110	2285	4.02	4.02	4.02	4.02	2	0.33	0.01	0.04	0.00	0.00	16.8
12	188	-945	226	58	0	-71	2258	4.02	4.02	4.02	4.02	2	0.33	0.00	0.03	0.00	0.00	16.8
13	188	-896	266	56	0	-67	2280	4.02	4.02	4.02	4.02	2	0.33	0.01	0.04	0.00	0.00	16.8
14	188	-984	188	-22	0	38	2235	4.02	4.02	4.02	4.02	2	0.33	0.00	0.02	0.00	0.00	16.8
15	188	-820	320	-26	0	54	2310	4.02	4.02	4.02	4.02	2	0.34	0.01	0.04	0.00	0.00	16.8

16	188	-992	184	16	0	-15	2233	4.02	4.02	4.02	4.02	2	0.33	0.00	0.02	0.00	0.00	16.8
17	188	-828	317	11	0	1	2308	4.02	4.02	4.02	4.02	2	0.34	0.01	0.04	0.00	0.00	16.8
18	188	-1290	333	-184	0	304	3232	4.02	4.02	4.02	4.02	3	0.44	0.01	0.04	0.00	0.00	16.8
19	188	-1415	280	177	0	-241	3208	4.02	4.02	4.02	4.02	3	0.43	0.01	0.04	0.00	0.00	16.8
20	188	-1458	233	-27	0	72	3228	4.02	4.02	4.02	4.02	3	0.43	0.01	0.03	0.00	0.00	16.8
37	188	-1170	353	-306	0	484	3097	4.02	4.02	4.02	4.02	3	0.42	0.01	0.05	0.00	0.00	16.8
38	188	-1379	264	296	0	-425	3058	4.02	4.02	4.02	4.02	3	0.41	0.01	0.04	0.00	0.00	16.8
39	188	-1450	185	-43	0	96	3090	4.02	4.02	4.02	4.02	3	0.42	0.00	0.02	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	225	-1178	-1197	-7	0	28	2952	4.02	4.02	4.02	4.02	3	0.40	0.03	0.16	0.00	0.00	16.8
2	225	-916	-934	-67	0	131	2263	4.02	4.02	4.02	4.02	2	0.33	0.02	0.12	0.00	0.00	16.8
3	225	-867	-894	-68	0	136	2285	4.02	4.02	4.02	4.02	2	0.33	0.02	0.12	0.00	0.00	16.8
4	225	-945	-947	58	0	-93	2258	4.02	4.02	4.02	4.02	2	0.33	0.02	0.13	0.00	0.00	16.8
5	225	-896	-907	56	0	-88	2280	4.02	4.02	4.02	4.02	2	0.33	0.02	0.12	0.00	0.00	16.8
6	225	-984	-985	-22	0	46	2235	4.02	4.02	4.02	4.02	2	0.33	0.02	0.13	0.00	0.00	16.8
7	225	-820	-852	-26	0	64	2310	4.02	4.02	4.02	4.02	2	0.34	0.02	0.11	0.00	0.00	16.8
8	225	-992	-989	16	0	-21	2233	4.02	4.02	4.02	4.02	2	0.33	0.02	0.13	0.00	0.00	16.8
9	225	-828	-856	11	0	-3	2308	4.02	4.02	4.02	4.02	2	0.34	0.02	0.11	0.00	0.00	16.8
10	225	-916	-934	-67	0	131	2263	4.02	4.02	4.02	4.02	2	0.33	0.02	0.12	0.00	0.00	16.8
11	225	-867	-894	-68	0	136	2285	4.02	4.02	4.02	4.02	2	0.33	0.02	0.12	0.00	0.00	16.8
12	225	-945	-947	58	0	-93	2258	4.02	4.02	4.02	4.02	2	0.33	0.02	0.13	0.00	0.00	16.8
13	225	-896	-907	56	0	-88	2280	4.02	4.02	4.02	4.02	2	0.33	0.02	0.12	0.00	0.00	16.8
14	225	-984	-985	-22	0	46	2235	4.02	4.02	4.02	4.02	2	0.33	0.02	0.13	0.00	0.00	16.8
15	225	-820	-852	-26	0	64	2310	4.02	4.02	4.02	4.02	2	0.34	0.02	0.11	0.00	0.00	16.8
16	225	-992	-989	16	0	-21	2233	4.02	4.02	4.02	4.02	2	0.33	0.02	0.13	0.00	0.00	16.8
17	225	-828	-856	11	0	-3	2308	4.02	4.02	4.02	4.02	2	0.34	0.02	0.11	0.00	0.00	16.8
18	225	-1290	-1350	-184	0	373	3232	4.02	4.02	4.02	4.02	3	0.44	0.03	0.18	0.00	0.00	16.8
19	225	-1415	-1403	177	0	-307	3208	4.02	4.02	4.02	4.02	3	0.43	0.03	0.19	0.00	0.00	16.8
20	225	-1458	-1450	-27	0	82	3228	4.02	4.02	4.02	4.02	3	0.43	0.03	0.19	0.00	0.00	16.8
37	225	-1170	-1251	-306	0	599	3097	4.02	4.02	4.02	4.02	3	0.42	0.03	0.17	0.00	0.00	16.8
38	225	-1379	-1340	296	0	-536	3058	4.02	4.02	4.02	4.02	3	0.41	0.03	0.18	0.00	0.00	16.8
39	225	-1450	-1419	-43	0	113	3090	4.02	4.02	4.02	4.02	3	0.42	0.03	0.19	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	262	-1178	-2721	-7	0	31	2952	4.02	4.02	4.02	4.02	3	0.40	0.06	0.36	0.00	0.00	16.8
2	262	-916	-2107	-67	0	156	2263	4.02	4.02	4.02	4.02	2	0.33	0.05	0.28	0.00	0.00	16.8
3	262	-867	-2067	-68	0	161	2285	4.02	4.02	4.02	4.02	2	0.33	0.04	0.28	0.00	0.00	16.8
4	262	-945	-2120	58	0	-114	2258	4.02	4.02	4.02	4.02	2	0.33	0.05	0.28	0.00	0.00	16.8
5	262	-896	-2080	56	0	-109	2280	4.02	4.02	4.02	4.02	2	0.33	0.05	0.28	0.00	0.00	16.8
6	262	-984	-2158	-22	0	55	2235	4.02	4.02	4.02	4.02	2	0.33	0.05	0.29	0.00	0.00	16.8
7	262	-820	-2025	-26	0	73	2310	4.02	4.02	4.02	4.02	2	0.34	0.04	0.27	0.00	0.00	16.8
8	262	-992	-2162	16	0	-26	2233	4.02	4.02	4.02	4.02	2	0.33	0.05	0.29	0.00	0.00	16.8
9	262	-828	-2029	11	0	-8	2308	4.02	4.02	4.02	4.02	2	0.34	0.04	0.27	0.00	0.00	16.8
10	262	-916	-2107	-67	0	156	2263	4.02	4.02	4.02	4.02	2	0.33	0.05	0.28	0.00	0.00	16.8
11	262	-867	-2067	-68	0	161	2285	4.02	4.02	4.02	4.02	2	0.33	0.04	0.28	0.00	0.00	16.8
12	262	-945	-2120	58	0	-114	2258	4.02	4.02	4.02	4.02	2	0.33	0.05	0.28	0.00	0.00	16.8
13	262	-896	-2080	56	0	-109	2280	4.02	4.02	4.02	4.02	2	0.33	0.05	0.28	0.00	0.00	16.8
14	262	-984	-2158	-22	0	55	2235	4.02	4.02	4.02	4.02	2	0.33	0.05	0.29	0.00	0.00	16.8
15	262	-820	-2025	-26	0	73	2310	4.02	4.02	4.02	4.02	2	0.34	0.04	0.27	0.00	0.00	16.8
16	262	-992	-2162	16	0	-26	2233	4.02	4.02	4.02	4.02	2	0.33	0.05	0.29	0.00	0.00	16.8
17	262	-828	-2029	11	0	-8	2308	4.02	4.02	4.02	4.02	2	0.34	0.04	0.27	0.00	0.00	16.8
18	262	-1290	-3034	-184	0	442	3232	4.02	4.02	4.02	4.02	3	0.44	0.07	0.40	0.00	0.00	16.8
19	262	-1415	-3087	177	0	-374	3208	4.02	4.02	4.02	4.02	3	0.43	0.07	0.41	0.00	0.00	16.8
20	262	-1458	-3134	-27	0	92	3228	4.02	4.02	4.02	4.02	3	0.43	0.07	0.41	0.00	0.00	16.8
37	262	-1170	-2855	-306	0	713	3097	4.02	4.02	4.02	4.02	3	0.42	0.06	0.38	0.00	0.00	16.8
38	262	-1379	-2944	296	0	-647	3058	4.02	4.02	4.02	4.02	3	0.41	0.06	0.39	0.00	0.00	16.8
39	262	-1450	-3023	-43	0	129	3090	4.02	4.02	4.02	4.02	3	0.42	0.07	0.40	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	300	-1178	-4246	-7	0	33	2898	4.02	4.02	4.02	4.02	3	0.39	0.09	0.56	0.00	0.00	16.8
2	300	-916	-3280	-67	0	181	2212	4.02	4.02	4.02	4.02	2	0.32	0.07	0.44	0.00	0.00	16.8
3	300	-867	-3240	-68	0	187	2259	4.02	4.02	4.02	4.02	2	0.33	0.07	0.43	0.00	0.00	16.8
4	300	-945	-3292	58	0	-136	2200	4.02	4.02	4.02	4.02	2	0.32	0.07	0.44	0.00	0.00	16.8
5	300	-896	-3253	56	0	-130	2246	4.02	4.02	4.02	4.02	2	0.33	0.07	0.43	0.00	0.00	16.8
6	300	-984	-3331	-22	0	63	2153	4.02	4.02	4.02	4.02	2	0.31	0.07	0.44	0.00	0.00	16.8
7	300	-820	-3198	-26	0	83	2310	4.02	4.02	4.02	4.02	2	0.34	0.07	0.43	0.00	0.00	16.8
8	300	-992	-3335	16	0	-32	2148	4.02	4.02	4.02	4.02	2	0.31	0.07	0.44	0.00	0.00	16.8
9	300	-828	-3201	11	0	-12	2306	4.02	4.02	4.02	4.02	2	0.34	0.07	0.43	0.00	0.00	16.8
10	300	-916	-3280	-67	0	181	2212	4.02	4.02	4.02	4.02	2	0.32	0.07	0.44	0.00	0.00	16.8
11	300	-867	-3240	-68	0	187	2259	4.02	4.02	4.02	4.02	2	0.33	0.07	0.43	0.00	0.00	16.8
12	300	-945	-3292	58	0	-136	2200	4.02	4.02	4.02	4.02	2	0.32	0.07	0.44	0.00	0.00	16.8
13	300	-896	-3253	56	0	-130	2246	4.02	4.02	4.02	4.02	2	0.33	0.07	0.43	0.00	0.00	16.8
14	300	-984	-3331	-22	0	63	2153	4.02	4.02	4.02	4.02	2	0.31	0.07	0.44	0.00	0.00	16.8
15	300	-820	-3198	-26	0	83	2310	4.02	4.02	4.02	4.02	2	0.34	0.07	0.43	0.00	0.00	16.8
16	300	-992	-3335	16	0	-32	2148	4.02	4.02	4.02	4.02	2	0.31	0.07	0.44	0.00	0.00	16.8
17	300	-828	-3201	11	0	-12	2306	4.02	4.02	4.02	4.02	2	0.34	0.07	0.43	0.00	0.00	16.8
18	300	-1290	-4717	-184	0	511	3154	4.02	4.02	4.02	4.02	3	0.43	0.10	0.62	0.00	0.00	16.8
19	300	-1415	-4770	177	0	-440	3097	4.02	4.02	4.02	4.02	3	0.42	0.10	0.63	0.00	0.00	16.8
20	300	-1458	-4817	-27	0	102	3087	4.02	4.02	4.02	4.02	3	0.42	0.10	0.64	0.00	0.00	16.8
37	300	-1170	-4459	-306	0	828	3044	4.02	4.02	4.02	4.02	3	0.41	0.10	0.59	0.00	0.00	16.8
38	300	-1379	-4548	296	0	-758	2950	4.02	4.02	4.02	4.02	3	0.40	0.10	0.60	0.00	0.00	16.8
39	300	-1450	-4627	-43	0	145	2934	4.02	4.02	4.02	4.02	3	0.40	0.10	0.61	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	338	-1178	-5770	-7	0	36	-3579	4.02	4.02	4.02	4.02	3	0.49	0.13	0.77	0.00	0.00	16.8
2	338	-916	-4452	-67	0	206	-2787	4.02	4.02	4.02	4.02	2	0.41	0.10	0.59	0.00	0.00	16.8
3	338	-867	-4412	-68	0	212	-2690	4.02	4.02	4.02	4.02	2	0.39	0.10	0.59	0.00	0.00	16.8
4	338	-945	-4465	58	0	-158	-2816	4.02	4.02	4.02	4.02	2	0.41	0.10	0.60	0.00	0.00	16.8
5	338	-896	-4425	56	0	-151	-2719	4.02	4.02	4.02	4.02	2	0.40	0.10	0.59	0.00	0.00	16.8
6	338	-984	-4503	-22	0	71	-2911	4.02	4.02	4.02	4.02	2	0.42	0.10	0.60	0.00	0.00	16.8
7	338	-820	-4370	-26	0	93	-2586	4.02	4.02	4.02	4.02	2	0.38	0.09	0.58	0.00	0.00	16.8
8	338	-992	-4507	16	0	-38	-2920	4.02	4.02	4.02	4.02	2	0.43	0.10	0.60	0.00	0.00	16.8
9	338	-828	-4374	11	0	-16	-2595	4.02	4.02	4.02	4.02	2	0.38	0.09	0.58	0.00	0.00	16.8
10	338	-916	-4452	-67	0	206	-2787	4.02	4.02	4.02	4.02	2	0.41	0.10	0.59	0.00	0.00	16.8
11	338	-867	-4412	-68	0	212	-2690	4.02	4.02	4.02	4.02	2	0.39	0.10	0.59	0.00	0.00	16.8
12	338	-945	-4465	58	0	-158	-2816	4.02	4.02	4.02	4.02	2	0.41	0.10	0.60	0.00	0.00	16.8
13	338	-896	-4425	56	0	-151	-2719	4.02	4.02	4.02	4.02	2	0.40	0.10	0.59	0.00	0.00	16.8
14	338	-984	-4503	-22	0	71	-2911	4.02	4.02	4.02	4.02	2	0.42	0.10	0.60	0.00	0.00	16.8
15	338	-820	-4370	-26	0	93	-2586	4.02	4.02	4.02	4.02	2	0.38	0.09	0.58	0.00	0.00	16.8
16	338	-992	-4507	16	0	-38	-2920	4.02	4.02	4.02	4.02	2	0.43	0.10	0.60	0.00	0.00	16.8
17	338	-828	-4374	11	0	-16	-2595	4.02	4.02	4.02	4.02	2	0.38	0.09	0.58	0.00	0.00	16.8
18	338	-1290	-6401	-184	0	580	-4035	4.02	4.02	4.02	4.02	3	0.55	0.14	0.85	0.00	0.00	16.8
19	338	-1415	-6454	177	0	-506	-4158	4.02	4.02	4.02	4.02	3	0.56	0.14	0.85	0.00	0.00	16.8
20	338	-1458	-6501	-27	0	112	-4227	4.02	4.02	4.02	4.02	3	0.57	0.14	0.86	0.00	0.00	16.8
37	338	-1170	-6063	-306	0	942	-3761	4.02	4.02	4.02	4.02	3	0.51	0.13	0.80	0.00	0.00	16.8

38	338	-1379	-6152	296	0	-869	-3966	4.02	4.02	4.02	4.02	3	0.53	0.13	0.81	0.00	0.00	16.8
39	338	-1450	-6231	-43	0	161	-4081	4.02	4.02	4.02	4.02	3	0.55	0.13	0.82	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	375	-1178	-7295	-7	0	38	-3579	4.02	4.02	4.02	4.02	3	0.49	0.16	0.97	0.00	0.00	16.8
2	375	-916	-5625	-67	0	231	-2787	4.02	4.02	4.02	4.02	2	0.41	0.12	0.75	0.00	0.00	16.8
3	375	-867	-5585	-68	0	238	-2690	4.02	4.02	4.02	4.02	2	0.39	0.12	0.75	0.00	0.00	16.8
4	375	-945	-5638	58	0	-179	-2816	4.02	4.02	4.02	4.02	2	0.41	0.12	0.75	0.00	0.00	16.8
5	375	-896	-5598	56	0	-172	-2719	4.02	4.02	4.02	4.02	2	0.40	0.12	0.75	0.00	0.00	16.8
6	375	-984	-5676	-22	0	79	-2911	4.02	4.02	4.02	4.02	2	0.42	0.12	0.76	0.00	0.00	16.8
7	375	-820	-5543	-26	0	103	-2586	4.02	4.02	4.02	4.02	2	0.38	0.12	0.74	0.00	0.00	16.8
8	375	-992	-5680	16	0	-44	-2920	4.02	4.02	4.02	4.02	2	0.43	0.12	0.76	0.00	0.00	16.8
9	375	-828	-5547	11	0	-20	-2595	4.02	4.02	4.02	4.02	2	0.38	0.12	0.74	0.00	0.00	16.8
10	375	-916	-5625	-67	0	231	-2787	4.02	4.02	4.02	4.02	2	0.41	0.12	0.75	0.00	0.00	16.8
11	375	-867	-5585	-68	0	238	-2690	4.02	4.02	4.02	4.02	2	0.39	0.12	0.75	0.00	0.00	16.8
12	375	-945	-5638	58	0	-179	-2816	4.02	4.02	4.02	4.02	2	0.41	0.12	0.75	0.00	0.00	16.8
13	375	-896	-5598	56	0	-172	-2719	4.02	4.02	4.02	4.02	2	0.40	0.12	0.75	0.00	0.00	16.8
14	375	-984	-5676	-22	0	79	-2911	4.02	4.02	4.02	4.02	2	0.42	0.12	0.76	0.00	0.00	16.8
15	375	-820	-5543	-26	0	103	-2586	4.02	4.02	4.02	4.02	2	0.38	0.12	0.74	0.00	0.00	16.8
16	375	-992	-5680	16	0	-44	-2920	4.02	4.02	4.02	4.02	2	0.43	0.12	0.76	0.00	0.00	16.8
17	375	-828	-5547	11	0	-20	-2595	4.02	4.02	4.02	4.02	2	0.38	0.12	0.74	0.00	0.00	16.8
18	375	-1290	-8084	-184	0	650	-4035	4.02	4.02	4.02	4.02	3	0.55	0.18	1.07	2.00	0.00	16.8
19	375	-1415	-8137	177	0	-573	-4158	4.02	4.02	4.02	4.02	3	0.56	0.18	1.08	2.02	0.00	16.8
20	375	-1458	-8184	-27	0	122	-4227	4.02	4.02	4.02	4.02	3	0.57	0.18	1.08	2.03	0.00	16.8
37	375	-1170	-7667	-306	0	1057	-3761	4.02	4.02	4.02	4.02	3	0.51	0.17	1.02	1.90	0.00	16.8
38	375	-1379	-7756	296	0	-980	-3966	4.02	4.02	4.02	4.02	3	0.53	0.17	1.03	1.92	0.00	16.8
39	375	-1450	-7835	-43	0	177	-4081	4.02	4.02	4.02	4.02	3	0.55	0.17	1.03	1.94	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

Nome travata: **trave_507_IP1** Descrizione: **Trave_5 26-25-24-23**
ASTA NUM. 19 NI 167 NF 264 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y Permanente Neve qy tot.
qy medio: 375.00 1635.75 142.50 2153.25 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-991	3670	569	0	1372	-1404	4.02	4.02	4.02	4.02	3	0.33	0.11	0.64	0.00	0.00	22.3
2	0	-951	2779	677	0	1480	-1021	4.02	4.02	4.02	4.02	2	0.40	0.08	0.48	0.00	0.00	22.3
3	0	-676	2915	679	0	1485	-1213	4.02	4.02	4.02	4.02	2	0.40	0.08	0.51	0.00	0.00	22.3
4	0	-848	2731	196	0	626	-947	4.02	4.02	4.02	4.02	2	0.17	0.08	0.48	0.00	0.00	22.3
5	0	-573	2867	198	0	631	-1138	4.02	4.02	4.02	4.02	2	0.17	0.08	0.50	0.00	0.00	22.3
6	0	-1236	2603	506	0	1175	-771	4.02	4.02	4.02	4.02	2	0.31	0.08	0.45	0.00	0.00	22.3
7	0	-319	3057	514	0	1192	-1411	4.02	4.02	4.02	4.02	2	0.33	0.09	0.54	0.00	0.00	22.3
8	0	-1205	2589	362	0	919	-749	4.02	4.02	4.02	4.02	2	0.24	0.07	0.45	0.00	0.00	22.3
9	0	-288	3042	369	0	936	-1388	4.02	4.02	4.02	4.02	2	0.26	0.09	0.54	0.00	0.00	22.3
10	0	-951	2779	677	0	1480	-1021	4.02	4.02	4.02	4.02	2	0.40	0.08	0.48	0.00	0.00	22.3
11	0	-676	2915	679	0	1485	-1213	4.02	4.02	4.02	4.02	2	0.40	0.08	0.51	0.00	0.00	22.3
12	0	-848	2731	196	0	626	-947	4.02	4.02	4.02	4.02	2	0.17	0.08	0.48	0.00	0.00	22.3
13	0	-573	2867	198	0	631	-1138	4.02	4.02	4.02	4.02	2	0.17	0.08	0.50	0.00	0.00	22.3
14	0	-1236	2603	506	0	1175	-771	4.02	4.02	4.02	4.02	2	0.31	0.08	0.45	0.00	0.00	22.3
15	0	-319	3057	514	0	1192	-1411	4.02	4.02	4.02	4.02	2	0.33	0.09	0.54	0.00	0.00	22.3
16	0	-1205	2589	362	0	919	-749	4.02	4.02	4.02	4.02	2	0.24	0.07	0.45	0.00	0.00	22.3
17	0	-288	3042	369	0	936	-1388	4.02	4.02	4.02	4.02	2	0.26	0.09	0.54	0.00	0.00	22.3
18	0	-2191	3735	1883	0	4114	-1235	4.02	4.02	4.02	4.02	3	0.96	0.11	0.63	0.00	0.00	22.3
19	0	-1940	3715	220	0	1051	-1182	4.02	4.02	4.02	4.02	3	0.25	0.11	0.63	0.00	0.00	22.3
20	0	-747	4101	966	0	2388	-1781	4.02	4.02	4.02	4.02	3	0.58	0.12	0.72	0.00	0.00	22.3
37	0	-1917	3670	2279	0	4739	-1296	6.03	4.02	4.02	4.02	3	0.80	0.11	0.62	0.00	0.00	22.3
38	0	-1499	3637	-492	0	-367	-1208	4.02	4.02	4.02	4.02	3	0.17	0.10	0.63	0.00	0.00	22.3
39	0	490	4280	751	0	1863	-2206	4.02	4.02	4.02	4.02	3	0.46	0.12	0.76	0.00	0.00	22.3

apost= 2.01 aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	31	-991	2860	569	0	1196	-1404	4.02	4.02	4.02	4.02	3	0.29	0.08	0.50	0.00	0.00	22.3
2	31	-951	2156	677	0	1270	-1021	4.02	4.02	4.02	4.02	2	0.34	0.06	0.38	0.00	0.00	22.3
3	31	-676	2292	679	0	1274	-1213	4.02	4.02	4.02	4.02	2	0.34	0.07	0.40	0.00	0.00	22.3
4	31	-848	2108	196	0	565	-947	4.02	4.02	4.02	4.02	2	0.15	0.06	0.37	0.00	0.00	22.3
5	31	-573	2244	198	0	570	-1138	4.02	4.02	4.02	4.02	2	0.17	0.06	0.39	0.00	0.00	22.3
6	31	-1236	1980	506	0	1018	-771	4.02	4.02	4.02	4.02	2	0.27	0.06	0.34	0.00	0.00	22.3
7	31	-319	2434	514	0	1033	-1411	4.02	4.02	4.02	4.02	2	0.28	0.07	0.43	0.00	0.00	22.3
8	31	-1205	1966	362	0	807	-749	4.02	4.02	4.02	4.02	2	0.21	0.06	0.34	0.00	0.00	22.3
9	31	-288	2419	369	0	821	-1388	4.02	4.02	4.02	4.02	2	0.22	0.07	0.43	0.00	0.00	22.3
10	31	-951	2156	677	0	1270	-1021	4.02	4.02	4.02	4.02	2	0.34	0.06	0.38	0.00	0.00	22.3
11	31	-676	2292	679	0	1274	-1213	4.02	4.02	4.02	4.02	2	0.34	0.07	0.40	0.00	0.00	22.3
12	31	-848	2108	196	0	565	-947	4.02	4.02	4.02	4.02	2	0.15	0.06	0.37	0.00	0.00	22.3
13	31	-573	2244	198	0	570	-1138	4.02	4.02	4.02	4.02	2	0.17	0.06	0.39	0.00	0.00	22.3
14	31	-1236	1980	506	0	1018	-771	4.02	4.02	4.02	4.02	2	0.27	0.06	0.34	0.00	0.00	22.3
15	31	-319	2434	514	0	1033	-1411	4.02	4.02	4.02	4.02	2	0.28	0.07	0.43	0.00	0.00	22.3
16	31	-1205	1966	362	0	807	-749	4.02	4.02	4.02	4.02	2	0.21	0.06	0.34	0.00	0.00	22.3
17	31	-288	2419	369	0	821	-1388	4.02	4.02	4.02	4.02	2	0.22	0.07	0.43	0.00	0.00	22.3
18	31	-2191	2858	1883	0	3530	-1235	4.02	4.02	4.02	4.02	3	0.82	0.08	0.48	0.00	0.00	22.3
19	31	-1940	2838	220	0	983	-1182	4.02	4.02	4.02	4.02	3	0.23	0.08	0.48	0.00	0.00	22.3
20	31	-747	3224	966	0	2089	-1781	4.02	4.02	4.02	4.02	3	0.50	0.09	0.56	0.00	0.00	22.3
37	31	-1917	2826	2279	0	4033	-1296	4.02	4.02	4.02	4.02	3	0.94	0.08	0.48	0.00	0.00	22.3
38	31	-1499	2794	-492	0	-214	-1208	4.02	4.02	4.02	4.02	3	0.17	0.08	0.48	0.00	0.00	22.3
39	31	490	3436	751	0	1630	-2206	4.02	4.02	4.02	4.02	3	0.41	0.10	0.61	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	62	-991	2049	569	0	1019	1144	4.02	4.02	4.02	4.02	3	0.24	0.06	0.36	0.00	0.00	22.3
2	62	-951	1532	677	0	1060	879	4.02	4.02	4.02	4.02	2	0.28	0.04	0.27	0.00	0.00	22.3
3	62	-676	1668	679	0	1064	889	4.02	4.02	4.02	4.02	2	0.29	0.05	0.29	0.00	0.00	22.3
4	62	-848	1484	196	0	505	894	4.02	4.02	4.02	4.02	2	0.14	0.04	0.26	0.00	0.00	22.3
5	62	-573	1620	198	0	508	890	4.02	4.02	4.02	4.02	2	0.14	0.05	0.28	0.00	0.00	22.3
6	62	-1236	1356	506	0	861	911	4.02	4.02	4.02	4.02	2	0.23	0.04	0.23	0.00	0.00	22.3
7	62	-319	1810	514	0	874	911	4.02	4.02	4.02	4.02	2	0.24	0.05	0.32	0.00	0.00	22.3
8	62	-1205	1342	362	0	695	916	4.02	4.02	4.02	4.02	2	0.18	0.04	0.23	0.00	0.00	22.3
9	62	-288	1795	369	0	707	912	4.02	4.02	4.02	4.02	2	0.19	0.05	0.32	0.00	0.00	22.3
10	62	-951	1532	677	0	1060	879	4.02	4.02	4.02	4.02	2	0.28	0.04	0.27	0.00	0.00	22.3
11	62	-676	1668	679	0	1064	889	4.02	4.02	4.02	4.02	2	0.29	0.05	0.29	0.00	0.00	22.3
12	62	-848	1484	196	0	505	894	4.02	4.02	4.02	4.02	2	0.14	0.04	0.26	0.00	0.00	22.3
13	62	-573	1620	198	0	508	890	4.02	4.02	4.02	4.02	2	0.14	0.05	0.28	0.00	0.00	22.3

14	62	-1236	1356	506	0	861	911	4.02	4.02	4.02	4.02	2	0.23	0.04	0.23	0.00	0.00	22.3
15	62	-319	1810	514	0	874	911	4.02	4.02	4.02	4.02	2	0.24	0.05	0.32	0.00	0.00	22.3
16	62	-1205	1342	362	0	695	916	4.02	4.02	4.02	4.02	2	0.18	0.04	0.23	0.00	0.00	22.3
17	62	-288	1795	369	0	707	912	4.02	4.02	4.02	4.02	2	0.19	0.05	0.32	0.00	0.00	22.3
18	62	-2191	1982	1883	0	2946	1222	4.02	4.02	4.02	4.02	3	0.68	0.06	0.34	0.00	0.00	22.3
19	62	-1940	1962	220	0	914	1251	4.02	4.02	4.02	4.02	3	0.21	0.06	0.33	0.00	0.00	22.3
20	62	-747	2348	966	0	1789	1178	4.02	4.02	4.02	4.02	3	0.43	0.07	0.41	0.00	0.00	22.3
37	62	-1917	1983	2279	0	3326	1163	4.02	4.02	4.02	4.02	3	0.78	0.07	0.35	0.00	0.00	22.3
38	62	-1499	1950	-492	0	-62	1210	4.02	4.02	4.02	4.02	3	0.17	0.06	0.34	0.00	0.00	22.3
39	62	490	2593	751	0	1397	-1388	4.02	4.02	4.02	4.02	3	0.35	0.08	0.46	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	93	-991	1239	569	0	843	1144	4.02	4.02	4.02	4.02	3	0.20	0.04	0.22	0.00	0.00	22.3
2	93	-951	909	677	0	850	879	4.02	4.02	4.02	4.02	2	0.23	0.03	0.16	0.00	0.00	22.3
3	93	-676	1045	679	0	853	889	4.02	4.02	4.02	4.02	2	0.23	0.03	0.18	0.00	0.00	22.3
4	93	-848	861	196	0	444	894	4.02	4.02	4.02	4.02	2	0.13	0.02	0.15	0.00	0.00	22.3
5	93	-573	997	198	0	447	890	4.02	4.02	4.02	4.02	2	0.13	0.03	0.18	0.00	0.00	22.3
6	93	-1236	733	506	0	704	911	4.02	4.02	4.02	4.02	2	0.19	0.02	0.13	0.00	0.00	22.3
7	93	-319	1187	514	0	714	911	4.02	4.02	4.02	4.02	2	0.20	0.03	0.21	0.00	0.00	22.3
8	93	-1205	719	362	0	583	916	4.02	4.02	4.02	4.02	2	0.15	0.02	0.12	0.00	0.00	22.3
9	93	-288	1172	369	0	592	912	4.02	4.02	4.02	4.02	2	0.16	0.03	0.21	0.00	0.00	22.3
10	93	-951	909	677	0	850	879	4.02	4.02	4.02	4.02	2	0.23	0.03	0.16	0.00	0.00	22.3
11	93	-676	1045	679	0	853	889	4.02	4.02	4.02	4.02	2	0.23	0.03	0.18	0.00	0.00	22.3
12	93	-848	861	196	0	444	894	4.02	4.02	4.02	4.02	2	0.13	0.02	0.15	0.00	0.00	22.3
13	93	-573	997	198	0	447	890	4.02	4.02	4.02	4.02	2	0.13	0.03	0.18	0.00	0.00	22.3
14	93	-1236	733	506	0	704	911	4.02	4.02	4.02	4.02	2	0.19	0.02	0.13	0.00	0.00	22.3
15	93	-319	1187	514	0	714	911	4.02	4.02	4.02	4.02	2	0.20	0.03	0.21	0.00	0.00	22.3
16	93	-1205	719	362	0	583	916	4.02	4.02	4.02	4.02	2	0.15	0.02	0.12	0.00	0.00	22.3
17	93	-288	1172	369	0	592	912	4.02	4.02	4.02	4.02	2	0.16	0.03	0.21	0.00	0.00	22.3
18	93	-2191	1105	1883	0	2363	1222	4.02	4.02	4.02	4.02	3	0.55	0.06	0.29	0.00	0.00	22.3
19	93	-1940	1085	220	0	846	1251	4.02	4.02	4.02	4.02	3	0.20	0.03	0.18	0.00	0.00	22.3
20	93	-747	1471	966	0	1490	1178	4.02	4.02	4.02	4.02	3	0.36	0.04	0.26	0.00	0.00	22.3
37	93	-1917	1140	2279	0	2619	1163	4.02	4.02	4.02	4.02	3	0.61	0.07	0.35	0.00	0.00	22.3
38	93	-1499	1106	-492	0	91	1210	4.02	4.02	4.02	4.02	3	0.17	0.03	0.19	0.00	0.00	22.3
39	93	490	1750	751	0	1165	1159	4.02	4.02	4.02	4.02	3	0.29	0.05	0.31	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	124	-991	428	569	0	667	1144	4.02	4.02	4.02	4.02	3	0.16	0.02	0.09	0.00	0.00	22.3
2	124	-951	285	677	0	640	879	4.02	4.02	4.02	4.02	2	0.17	0.02	0.11	0.00	0.00	22.3
3	124	-676	421	679	0	643	889	4.02	4.02	4.02	4.02	2	0.17	0.02	0.11	0.00	0.00	22.3
4	124	-848	238	196	0	383	894	4.02	4.02	4.02	4.02	2	0.13	0.01	0.04	0.00	0.00	22.3
5	124	-573	374	198	0	385	890	4.02	4.02	4.02	4.02	2	0.13	0.01	0.07	0.00	0.00	22.3
6	124	-1236	110	506	0	547	911	4.02	4.02	4.02	4.02	2	0.15	0.02	0.08	0.00	0.00	22.3
7	124	-319	563	514	0	555	911	4.02	4.02	4.02	4.02	2	0.15	0.02	0.10	0.00	0.00	22.3
8	124	-1205	96	362	0	470	916	4.02	4.02	4.02	4.02	2	0.13	0.01	0.06	0.00	0.00	22.3
9	124	-288	549	369	0	478	912	4.02	4.02	4.02	4.02	2	0.14	0.02	0.10	0.00	0.00	22.3
10	124	-951	285	677	0	640	879	4.02	4.02	4.02	4.02	2	0.17	0.02	0.11	0.00	0.00	22.3
11	124	-676	421	679	0	643	889	4.02	4.02	4.02	4.02	2	0.17	0.02	0.11	0.00	0.00	22.3
12	124	-848	238	196	0	383	894	4.02	4.02	4.02	4.02	2	0.13	0.01	0.04	0.00	0.00	22.3
13	124	-573	374	198	0	385	890	4.02	4.02	4.02	4.02	2	0.13	0.01	0.07	0.00	0.00	22.3
14	124	-1236	110	506	0	547	911	4.02	4.02	4.02	4.02	2	0.15	0.02	0.08	0.00	0.00	22.3
15	124	-319	563	514	0	555	911	4.02	4.02	4.02	4.02	2	0.15	0.02	0.10	0.00	0.00	22.3
16	124	-1205	96	362	0	470	916	4.02	4.02	4.02	4.02	2	0.13	0.01	0.06	0.00	0.00	22.3
17	124	-288	549	369	0	478	912	4.02	4.02	4.02	4.02	2	0.14	0.02	0.10	0.00	0.00	22.3
18	124	-2191	229	1883	0	1779	1222	4.02	4.02	4.02	4.02	3	0.41	0.06	0.29	0.00	0.00	22.3
19	124	-1940	209	220	0	778	1251	4.02	4.02	4.02	4.02	3	0.18	0.01	0.04	0.00	0.00	22.3
20	124	-747	595	966	0	1190	1178	4.02	4.02	4.02	4.02	3	0.29	0.03	0.15	0.00	0.00	22.3
37	124	-1917	296	2279	0	1913	1163	4.02	4.02	4.02	4.02	3	0.45	0.07	0.35	0.00	0.00	22.3
38	124	-1499	263	-492	0	243	1210	4.02	4.02	4.02	4.02	3	0.17	0.02	0.08	0.00	0.00	22.3
39	124	490	906	751	0	932	1159	4.02	4.02	4.02	4.02	3	0.23	0.03	0.16	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	155	-991	-382	569	0	490	1144	4.02	4.02	4.02	4.02	3	0.16	0.02	0.09	0.00	0.00	22.3
2	155	-951	-338	677	0	430	879	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
3	155	-676	-202	679	0	432	889	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
4	155	-848	-386	196	0	322	894	4.02	4.02	4.02	4.02	2	0.13	0.01	0.07	0.00	0.00	22.3
5	155	-573	-250	198	0	324	890	4.02	4.02	4.02	4.02	2	0.13	0.01	0.04	0.00	0.00	22.3
6	155	-1236	-514	506	0	391	911	4.02	4.02	4.02	4.02	2	0.13	0.02	0.09	0.00	0.00	22.3
7	155	-319	-60	514	0	396	911	4.02	4.02	4.02	4.02	2	0.14	0.02	0.08	0.00	0.00	22.3
8	155	-1205	-528	362	0	358	916	4.02	4.02	4.02	4.02	2	0.13	0.02	0.09	0.00	0.00	22.3
9	155	-288	-74	369	0	364	912	4.02	4.02	4.02	4.02	2	0.14	0.01	0.06	0.00	0.00	22.3
10	155	-951	-338	677	0	430	879	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
11	155	-676	-202	679	0	432	889	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
12	155	-848	-386	196	0	322	894	4.02	4.02	4.02	4.02	2	0.13	0.01	0.07	0.00	0.00	22.3
13	155	-573	-250	198	0	324	890	4.02	4.02	4.02	4.02	2	0.13	0.01	0.04	0.00	0.00	22.3
14	155	-1236	-514	506	0	391	911	4.02	4.02	4.02	4.02	2	0.13	0.02	0.09	0.00	0.00	22.3
15	155	-319	-60	514	0	396	911	4.02	4.02	4.02	4.02	2	0.14	0.02	0.08	0.00	0.00	22.3
16	155	-1205	-528	362	0	358	916	4.02	4.02	4.02	4.02	2	0.13	0.02	0.09	0.00	0.00	22.3
17	155	-288	-74	369	0	364	912	4.02	4.02	4.02	4.02	2	0.14	0.01	0.06	0.00	0.00	22.3
18	155	-2191	-648	1883	0	1195	1222	4.02	4.02	4.02	4.02	3	0.28	0.06	0.29	0.00	0.00	22.3
19	155	-1940	-668	220	0	709	1251	4.02	4.02	4.02	4.02	3	0.17	0.02	0.11	0.00	0.00	22.3
20	155	-747	-282	966	0	891	1178	4.02	4.02	4.02	4.02	3	0.21	0.03	0.15	0.00	0.00	22.3
37	155	-1917	-548	2279	0	1207	1163	4.02	4.02	4.02	4.02	3	0.28	0.07	0.35	0.00	0.00	22.3
38	155	-1499	-580	-492	0	396	1210	4.02	4.02	4.02	4.02	3	0.17	0.02	0.10	0.00	0.00	22.3
39	155	490	62	751	0	699	1159	4.02	4.02	4.02	4.02	3	0.17	0.02	0.12	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	186	-991	-1192	569	0	314	1144	4.02	4.02	4.02	4.02	3	0.16	0.03	0.21	0.00	0.00	22.3
2	186	-951	-961	677	0	220	879	4.02	4.02	4.02	4.02	2	0.13	0.03	0.17	0.00	0.00	22.3
3	186	-676	-825	679	0	221	889	4.02	4.02	4.02	4.02	2	0.13	0.02	0.14	0.00	0.00	22.3
4	186	-848	-1009	196	0	262	894	4.02	4.02	4.02	4.02	2	0.13	0.03	0.18	0.00	0.00	22.3
5	186	-573	-873	198	0	262	890	4.02	4.02	4.02	4.02	2	0.13	0.03	0.15	0.00	0.00	22.3
6	186	-1236	-1137	506	0	234	911	4.02	4.02	4.02	4.02	2	0.13	0.03	0.20	0.00	0.00	22.3
7	186	-319	-683	514	0	237	911	4.02	4.02	4.02	4.02	2	0.14	0.02	0.12	0.00	0.00	22.3
8	186	-1205	-1151	362	0	246	916	4.02	4.02	4.02	4.02	2	0.13	0.03	0.20	0.00	0.00	22.3
9	186	-288	-698	369	0	249	912	4.02	4.02	4.02	4.02	2	0.14	0.02	0.12	0.00	0.00	22.3
10	186	-951	-961	677	0	220	879	4.02	4.02	4.02	4.02	2	0.13	0.03	0.17	0.00	0.00	22.3
11	186	-676	-825	679	0	221	889	4.02	4.02	4.02	4.02	2	0.13	0.02	0.14	0.00	0.00	22.3
12	186	-848	-1009	196	0	262	894	4.02	4.02	4.02	4.02	2	0.13	0.03	0.18	0.00	0.00	22.3
13	186	-573	-873	198	0	262	890	4.02	4.02	4.02	4.02	2	0.13	0.03	0.15	0.00	0.00	22.3
14	186	-1236	-1137	506	0	234	911	4.02	4.02	4.02	4.02	2	0.13	0.03	0.20	0.00	0.00	22.3
15	186	-319	-683	514	0	237	911	4.02	4.02	4.02	4.02	2	0.14	0.02	0.12	0.00	0.00	22.3
16	186	-1205	-1151	362	0	246	916	4.02	4.02	4.02	4.02	2	0.13	0.03	0.20	0.00	0.00	22.3
17	186	-288	-698	369	0	249	912	4.02	4.02	4.02	4.02	2	0.14	0.02	0.12	0.00	0.00	22.3
18	186	-2191	-1525	1883	0	611	1222	4.02	4.02	4.02	4.02	3	0.16	0.06	0.29	0.00	0.00	22.3
19	186	-1940	-1545	220	0	641	1251	4.02	4.02	4.02	4.02	3	0.17	0.04	0.26	0.00	0.00	22.3

20	186	-747	-1159	966	0	591	1178	4.02	4.02	4.02	4.02	3	0.17	0.03	0.20	0.00	0.00	22.3
37	186	-1917	-1391	2279	0	500	1163	4.02	4.02	4.02	4.02	3	0.16	0.07	0.35	0.00	0.00	22.3
38	186	-1499	-1424	-492	0	549	1210	4.02	4.02	4.02	4.02	3	0.17	0.04	0.24	0.00	0.00	22.3
39	186	490	-781	751	0	466	1159	4.02	4.02	4.02	4.02	3	0.17	0.02	0.14	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	217	-991	-2003	569	0	137	1144	4.02	4.02	4.02	4.02	3	0.16	0.06	0.35	0.00	0.00	22.3
2	217	-951	-1585	677	0	11	879	4.02	4.02	4.02	4.02	2	0.13	0.05	0.28	0.00	0.00	22.3
3	217	-676	-1449	679	0	11	889	4.02	4.02	4.02	4.02	2	0.13	0.04	0.25	0.00	0.00	22.3
4	217	-848	-1632	196	0	201	894	4.02	4.02	4.02	4.02	2	0.13	0.05	0.28	0.00	0.00	22.3
5	217	-573	-1496	198	0	201	890	4.02	4.02	4.02	4.02	2	0.13	0.04	0.26	0.00	0.00	22.3
6	217	-1236	-1760	506	0	77	911	4.02	4.02	4.02	4.02	2	0.13	0.05	0.30	0.00	0.00	22.3
7	217	-319	-1307	514	0	78	911	4.02	4.02	4.02	4.02	2	0.14	0.04	0.23	0.00	0.00	22.3
8	217	-1205	-1774	362	0	134	916	4.02	4.02	4.02	4.02	2	0.13	0.05	0.31	0.00	0.00	22.3
9	217	-288	-1321	369	0	135	912	4.02	4.02	4.02	4.02	2	0.14	0.04	0.23	0.00	0.00	22.3
10	217	-951	-1585	677	0	11	879	4.02	4.02	4.02	4.02	2	0.13	0.05	0.28	0.00	0.00	22.3
11	217	-676	-1449	679	0	11	889	4.02	4.02	4.02	4.02	2	0.13	0.04	0.25	0.00	0.00	22.3
12	217	-848	-1632	196	0	201	894	4.02	4.02	4.02	4.02	2	0.13	0.05	0.28	0.00	0.00	22.3
13	217	-573	-1496	198	0	201	890	4.02	4.02	4.02	4.02	2	0.13	0.04	0.26	0.00	0.00	22.3
14	217	-1236	-1760	506	0	77	911	4.02	4.02	4.02	4.02	2	0.13	0.05	0.30	0.00	0.00	22.3
15	217	-319	-1307	514	0	78	911	4.02	4.02	4.02	4.02	2	0.14	0.04	0.23	0.00	0.00	22.3
16	217	-1205	-1774	362	0	134	916	4.02	4.02	4.02	4.02	2	0.13	0.05	0.31	0.00	0.00	22.3
17	217	-288	-1321	369	0	135	912	4.02	4.02	4.02	4.02	2	0.14	0.04	0.23	0.00	0.00	22.3
18	217	-2191	-2401	1883	0	27	1222	4.02	4.02	4.02	4.02	3	0.16	0.07	0.41	0.00	0.00	22.3
19	217	-1940	-2421	220	0	572	1251	4.02	4.02	4.02	4.02	3	0.17	0.07	0.41	0.00	0.00	22.3
20	217	-747	-2035	966	0	292	1178	4.02	4.02	4.02	4.02	3	0.17	0.06	0.36	0.00	0.00	22.3
37	217	-1917	-2235	2279	0	-207	1163	4.02	4.02	4.02	4.02	3	0.16	0.07	0.38	0.00	0.00	22.3
38	217	-1499	-2268	-492	0	701	1210	4.02	4.02	4.02	4.02	3	0.17	0.07	0.39	0.00	0.00	22.3
39	217	490	-1625	751	0	233	1159	4.02	4.02	4.02	4.02	3	0.17	0.05	0.29	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	248	-991	-2813	569	0	-39	-1766	4.02	4.02	4.02	4.02	3	0.25	0.08	0.49	0.00	0.00	22.3
2	248	-951	-2208	677	0	-199	-1431	4.02	4.02	4.02	4.02	2	0.21	0.06	0.38	0.00	0.00	22.3
3	248	-676	-2072	679	0	-200	-1217	4.02	4.02	4.02	4.02	2	0.18	0.06	0.36	0.00	0.00	22.3
4	248	-848	-2255	196	0	140	-1499	4.02	4.02	4.02	4.02	2	0.22	0.07	0.39	0.00	0.00	22.3
5	248	-573	-2119	198	0	140	-1284	4.02	4.02	4.02	4.02	2	0.19	0.06	0.37	0.00	0.00	22.3
6	248	-1236	-2383	506	0	-80	-1705	4.02	4.02	4.02	4.02	2	0.25	0.07	0.41	0.00	0.00	22.3
7	248	-319	-1930	514	0	-82	-991	4.02	4.02	4.02	4.02	2	0.15	0.06	0.34	0.00	0.00	22.3
8	248	-1205	-2397	362	0	22	-1725	4.02	4.02	4.02	4.02	2	0.25	0.07	0.41	0.00	0.00	22.3
9	248	-288	-1944	369	0	20	-1011	4.02	4.02	4.02	4.02	2	0.15	0.06	0.34	0.00	0.00	22.3
10	248	-951	-2208	677	0	-199	-1431	4.02	4.02	4.02	4.02	2	0.21	0.06	0.38	0.00	0.00	22.3
11	248	-676	-2072	679	0	-200	-1217	4.02	4.02	4.02	4.02	2	0.18	0.06	0.36	0.00	0.00	22.3
12	248	-848	-2255	196	0	140	-1499	4.02	4.02	4.02	4.02	2	0.22	0.07	0.39	0.00	0.00	22.3
13	248	-573	-2119	198	0	140	-1284	4.02	4.02	4.02	4.02	2	0.19	0.06	0.37	0.00	0.00	22.3
14	248	-1236	-2383	506	0	-80	-1705	4.02	4.02	4.02	4.02	2	0.25	0.07	0.41	0.00	0.00	22.3
15	248	-319	-1930	514	0	-82	-991	4.02	4.02	4.02	4.02	2	0.15	0.06	0.34	0.00	0.00	22.3
16	248	-1205	-2397	362	0	22	-1725	4.02	4.02	4.02	4.02	2	0.25	0.07	0.41	0.00	0.00	22.3
17	248	-288	-1944	369	0	20	-1011	4.02	4.02	4.02	4.02	2	0.15	0.06	0.34	0.00	0.00	22.3
18	248	-2191	-3278	1883	0	-556	-2328	4.02	4.02	4.02	4.02	3	0.31	0.09	0.55	0.00	0.00	22.3
19	248	-1940	-3298	220	0	504	-2334	4.02	4.02	4.02	4.02	3	0.32	0.09	0.56	0.00	0.00	22.3
20	248	-747	-2912	966	0	-8	-1781	4.02	4.02	4.02	4.02	3	0.25	0.08	0.51	0.00	0.00	22.3
37	248	-1917	-3078	2279	0	-913	-2120	4.02	4.02	4.02	4.02	3	0.29	0.09	0.52	0.00	0.00	22.3
38	248	-1499	-3111	-492	0	854	-2131	4.02	4.02	4.02	4.02	3	0.29	0.09	0.53	0.00	0.00	22.3
39	248	490	-2468	751	0	1	1159	4.02	4.02	4.02	4.02	3	0.17	0.07	0.44	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	279	-991	-3624	569	0	-215	-2588	4.02	4.02	4.02	4.02	3	0.36	0.10	0.63	0.00	0.00	22.3
2	279	-951	-2832	677	0	-409	-2069	4.02	4.02	4.02	4.02	2	0.30	0.08	0.49	0.00	0.00	22.3
3	279	-676	-2696	679	0	-410	-1839	4.02	4.02	4.02	4.02	2	0.27	0.08	0.47	0.00	0.00	22.3
4	279	-848	-2879	196	0	79	-2142	4.02	4.02	4.02	4.02	2	0.32	0.08	0.50	0.00	0.00	22.3
5	279	-573	-2743	198	0	78	-1912	4.02	4.02	4.02	4.02	2	0.28	0.08	0.48	0.00	0.00	22.3
6	279	-1236	-3007	506	0	-237	-2362	4.02	4.02	4.02	4.02	2	0.35	0.09	0.52	0.00	0.00	22.3
7	279	-319	-2554	514	0	-241	-1597	4.02	4.02	4.02	4.02	2	0.24	0.07	0.45	0.00	0.00	22.3
8	279	-1205	-3021	362	0	-90	-2384	4.02	4.02	4.02	4.02	2	0.35	0.09	0.52	0.00	0.00	22.3
9	279	-288	-2568	369	0	-94	-1619	4.02	4.02	4.02	4.02	2	0.24	0.07	0.45	0.00	0.00	22.3
10	279	-951	-2832	677	0	-409	-2069	4.02	4.02	4.02	4.02	2	0.30	0.08	0.49	0.00	0.00	22.3
11	279	-676	-2696	679	0	-410	-1839	4.02	4.02	4.02	4.02	2	0.27	0.08	0.47	0.00	0.00	22.3
12	279	-848	-2879	196	0	79	-2142	4.02	4.02	4.02	4.02	2	0.32	0.08	0.50	0.00	0.00	22.3
13	279	-573	-2743	198	0	78	-1912	4.02	4.02	4.02	4.02	2	0.28	0.08	0.48	0.00	0.00	22.3
14	279	-1236	-3007	506	0	-237	-2362	4.02	4.02	4.02	4.02	2	0.35	0.09	0.52	0.00	0.00	22.3
15	279	-319	-2554	514	0	-241	-1597	4.02	4.02	4.02	4.02	2	0.24	0.07	0.45	0.00	0.00	22.3
16	279	-1205	-3021	362	0	-90	-2384	4.02	4.02	4.02	4.02	2	0.35	0.09	0.52	0.00	0.00	22.3
17	279	-288	-2568	369	0	-94	-1619	4.02	4.02	4.02	4.02	2	0.24	0.07	0.45	0.00	0.00	22.3
18	279	-2191	-4154	1883	0	-1140	-3245	4.02	4.02	4.02	4.02	3	0.44	0.12	0.70	0.00	0.00	22.3
19	279	-1940	-4174	220	0	436	-3253	4.02	4.02	4.02	4.02	3	0.44	0.12	0.71	0.00	0.00	22.3
20	279	-747	-3788	966	0	-307	-2656	4.02	4.02	4.02	4.02	3	0.37	0.11	0.66	0.00	0.00	22.3
37	279	-1917	-3922	2279	0	-1620	-2993	4.02	4.02	4.02	4.02	3	0.41	0.11	0.67	0.00	0.00	22.3
38	279	-1499	-3955	-492	0	1006	-3008	4.02	4.02	4.02	4.02	3	0.41	0.11	0.68	0.00	0.00	22.3
39	279	490	-3312	751	0	-232	-2013	4.02	4.02	4.02	4.02	3	0.29	0.10	0.59	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	310	-991	-4434	569	0	-392	-2588	4.02	4.02	4.02	4.02	3	0.36	0.13	0.77	0.00	0.00	22.3
2	310	-951	-3455	677	0	-619	-2069	4.02	4.02	4.02	4.02	2	0.30	0.10	0.60	0.00	0.00	22.3
3	310	-676	-3319	679	0	-621	-1839	4.02	4.02	4.02	4.02	2	0.27	0.10	0.58	0.00	0.00	22.3
4	310	-848	-3502	196	0	19	-2142	4.02	4.02	4.02	4.02	2	0.32	0.10	0.61	0.00	0.00	22.3
5	310	-573	-3366	198	0	17	-1912	4.02	4.02	4.02	4.02	2	0.28	0.10	0.59	0.00	0.00	22.3
6	310	-1236	-3630	506	0	-394	-2362	4.02	4.02	4.02	4.02	2	0.35	0.10	0.63	0.00	0.00	22.3
7	310	-319	-3177	514	0	-400	-1597	4.02	4.02	4.02	4.02	2	0.24	0.09	0.56	0.00	0.00	22.3
8	310	-1205	-3644	362	0	-202	-2384	4.02	4.02	4.02	4.02	2	0.35	0.11	0.63	0.00	0.00	22.3
9	310	-288	-3191	369	0	-209	-1619	4.02	4.02	4.02	4.02	2	0.24	0.09	0.56	0.00	0.00	22.3
10	310	-951	-3455	677	0	-619	-2069	4.02	4.02	4.02	4.02	2	0.30	0.10	0.60	0.00	0.00	22.3
11	310	-676	-3319	679	0	-621	-1839	4.02	4.02	4.02	4.02	2	0.27	0.10	0.58	0.00	0.00	22.3
12	310	-848	-3502	196	0	19	-2142	4.02	4.02	4.02	4.02	2	0.32	0.10	0.61	0.00	0.00	22.3
13	310	-573	-3366	198	0	17	-1912	4.02	4.02	4.02	4.02	2	0.28	0.10	0.59	0.00	0.00	22.3
14	310	-1236	-3630	506	0	-394	-2362	4.02	4.02	4.02	4.02	2	0.35	0.10	0.63	0.00	0.00	22.3
15	310	-319	-3177	514	0	-400	-1597	4.02	4.02	4.02	4.02	2	0.24	0.09	0.56	0.00	0.00	22.3
16	310	-1205	-3644	362	0	-202	-2384	4.02	4.02	4.02	4.02	2	0.35	0.11	0.63	0.00	0.00	22.3
17	310	-288	-3191	369	0	-209	-1619	4.02	4.02	4.02	4.02	2	0.24	0.09	0.56	0.00	0.00	22.3
18	310	-2191	-5031	1883	0	-1724	-3245	4.02	4.02	4.02	4.02	3	0.44	0.14	0.85	0.00	0.00	22.3
19	310	-1940	-5051	220	0	367	-3253	4.02	4.02	4.02	4.02	3	0.44	0.15	0.86	0.00	0.00	22.3
20	310	-747	-4665	966	0	-607	-2656	4.02	4.02	4.02	4.02	3	0.37	0.13	0.82	0.00	0.00	22.3
37	310	-1917	-4765	2279	0	-2326	-2993	4.02	4.02	4.02	4.02	3	0.54	0.14	0.81	0.00	0.00	22.3
38	310	-1499	-4798	-492	0	1159	-3008	4.02	4.02	4.02	4.02	3	0.41	0.14	0.82	0.00	0.00	22.3
39	310	490	-4155	751	0	-465	-2013	4.02	4.02	4.02	4.02	3	0.29	0.12	0.74	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

Nome travata: **trave_507_IP1** Descrizione: **Trave_5 26-25-24-23**
ASTA NUM. 20 NI 264 NF 165 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y Permanente Neve qy tot.
qy medio: 375.00 1371.75 142.50 1889.25 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-1286	3769	10	0	55	-1637	4.02	4.02	4.02	4.02	3	0.23	0.11	0.65	0.00	0.00	22.3
2	0	-1141	2821	-65	0	-160	-1098	4.02	4.02	4.02	4.02	2	0.16	0.08	0.49	0.00	0.00	22.3
3	0	-888	2915	-65	0	-161	-1295	4.02	4.02	4.02	4.02	2	0.19	0.08	0.51	0.00	0.00	22.3
4	0	-1090	2883	80	0	245	-1224	4.02	4.02	4.02	4.02	2	0.18	0.08	0.50	0.00	0.00	22.3
5	0	-837	2976	79	0	245	-1421	4.02	4.02	4.02	4.02	2	0.21	0.09	0.52	0.00	0.00	22.3
6	0	-1419	2734	-13	0	-18	-913	4.02	4.02	4.02	4.02	2	0.13	0.08	0.47	0.00	0.00	22.3
7	0	-575	3046	-15	0	-19	-1568	4.02	4.02	4.02	4.02	2	0.23	0.09	0.54	0.00	0.00	22.3
8	0	-1404	2752	30	0	104	-950	4.02	4.02	4.02	4.02	2	0.14	0.08	0.47	0.00	0.00	22.3
9	0	-560	3064	28	0	103	-1606	4.02	4.02	4.02	4.02	2	0.24	0.09	0.54	0.00	0.00	22.3
10	0	-1141	2821	-65	0	-160	-1098	4.02	4.02	4.02	4.02	2	0.16	0.08	0.49	0.00	0.00	22.3
11	0	-888	2915	-65	0	-161	-1295	4.02	4.02	4.02	4.02	2	0.19	0.08	0.51	0.00	0.00	22.3
12	0	-1090	2883	80	0	245	-1224	4.02	4.02	4.02	4.02	2	0.18	0.08	0.50	0.00	0.00	22.3
13	0	-837	2976	79	0	245	-1421	4.02	4.02	4.02	4.02	2	0.21	0.09	0.52	0.00	0.00	22.3
14	0	-1419	2734	-13	0	-18	-913	4.02	4.02	4.02	4.02	2	0.13	0.08	0.47	0.00	0.00	22.3
15	0	-575	3046	-15	0	-19	-1568	4.02	4.02	4.02	4.02	2	0.23	0.09	0.54	0.00	0.00	22.3
16	0	-1404	2752	30	0	104	-950	4.02	4.02	4.02	4.02	2	0.14	0.08	0.47	0.00	0.00	22.3
17	0	-560	3064	28	0	103	-1606	4.02	4.02	4.02	4.02	2	0.24	0.09	0.54	0.00	0.00	22.3
18	0	-2077	3817	-180	0	-453	-1169	4.02	4.02	4.02	4.02	3	0.16	0.11	0.65	0.00	0.00	22.3
19	0	-1837	4013	254	0	758	-1571	4.02	4.02	4.02	4.02	3	0.21	0.12	0.68	0.00	0.00	22.3
20	0	-1263	4151	20	0	101	-1851	4.02	4.02	4.02	4.02	3	0.26	0.12	0.72	0.00	0.00	22.3
37	0	-1929	3636	-334	0	-889	-1080	4.02	4.02	4.02	4.02	3	0.21	0.10	0.62	0.00	0.00	22.3
38	0	-1529	3961	390	0	1130	-1750	4.02	4.02	4.02	4.02	3	0.27	0.11	0.68	0.00	0.00	22.3
39	0	-572	4191	-0	0	36	-2217	4.02	4.02	4.02	4.02	3	0.31	0.12	0.74	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	38	-1286	2917	10	0	51	-1637	4.02	4.02	4.02	4.02	3	0.23	0.08	0.50	0.00	0.00	22.3
2	38	-1141	2166	-65	0	-136	-1098	4.02	4.02	4.02	4.02	2	0.16	0.06	0.38	0.00	0.00	22.3
3	38	-888	2260	-65	0	-136	-1295	4.02	4.02	4.02	4.02	2	0.19	0.07	0.39	0.00	0.00	22.3
4	38	-1090	2228	80	0	215	-1224	4.02	4.02	4.02	4.02	2	0.18	0.06	0.39	0.00	0.00	22.3
5	38	-837	2321	79	0	215	-1421	4.02	4.02	4.02	4.02	2	0.21	0.07	0.41	0.00	0.00	22.3
6	38	-1419	2079	-13	0	-13	-913	4.02	4.02	4.02	4.02	2	0.13	0.06	0.36	0.00	0.00	22.3
7	38	-575	2391	-15	0	-13	-1568	4.02	4.02	4.02	4.02	2	0.23	0.07	0.42	0.00	0.00	22.3
8	38	-1404	2097	30	0	92	-950	4.02	4.02	4.02	4.02	2	0.14	0.06	0.36	0.00	0.00	22.3
9	38	-560	2409	28	0	92	-1606	4.02	4.02	4.02	4.02	2	0.24	0.07	0.42	0.00	0.00	22.3
10	38	-1141	2166	-65	0	-136	-1098	4.02	4.02	4.02	4.02	2	0.16	0.06	0.38	0.00	0.00	22.3
11	38	-888	2260	-65	0	-136	-1295	4.02	4.02	4.02	4.02	2	0.19	0.07	0.39	0.00	0.00	22.3
12	38	-1090	2228	80	0	215	-1224	4.02	4.02	4.02	4.02	2	0.18	0.06	0.39	0.00	0.00	22.3
13	38	-837	2321	79	0	215	-1421	4.02	4.02	4.02	4.02	2	0.21	0.07	0.41	0.00	0.00	22.3
14	38	-1419	2079	-13	0	-13	-913	4.02	4.02	4.02	4.02	2	0.13	0.06	0.36	0.00	0.00	22.3
15	38	-575	2391	-15	0	-13	-1568	4.02	4.02	4.02	4.02	2	0.23	0.07	0.42	0.00	0.00	22.3
16	38	-1404	2097	30	0	92	-950	4.02	4.02	4.02	4.02	2	0.14	0.06	0.36	0.00	0.00	22.3
17	38	-560	2409	28	0	92	-1606	4.02	4.02	4.02	4.02	2	0.24	0.07	0.42	0.00	0.00	22.3
18	38	-2077	2885	-180	0	-385	1549	4.02	4.02	4.02	4.02	3	0.21	0.08	0.49	0.00	0.00	22.3
19	38	-1837	3081	254	0	663	-1571	4.02	4.02	4.02	4.02	3	0.21	0.09	0.53	0.00	0.00	22.3
20	38	-1263	3219	20	0	94	-1851	4.02	4.02	4.02	4.02	3	0.26	0.09	0.56	0.00	0.00	22.3
37	38	-1929	2744	-334	0	-763	1506	4.02	4.02	4.02	4.02	3	0.20	0.08	0.47	0.00	0.00	22.3
38	38	-1529	3069	390	0	984	-1750	4.02	4.02	4.02	4.02	3	0.24	0.09	0.53	0.00	0.00	22.3
39	38	-572	3299	-0	0	36	-2217	4.02	4.02	4.02	4.02	3	0.31	0.10	0.58	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	75	-1286	2066	10	0	48	1461	4.02	4.02	4.02	4.02	3	0.20	0.06	0.36	0.00	0.00	22.3
2	75	-1141	1511	-65	0	-112	1169	4.02	4.02	4.02	4.02	2	0.17	0.04	0.26	0.00	0.00	22.3
3	75	-888	1605	-65	0	-112	1113	4.02	4.02	4.02	4.02	2	0.16	0.05	0.28	0.00	0.00	22.3
4	75	-1090	1573	80	0	185	1135	4.02	4.02	4.02	4.02	2	0.17	0.05	0.27	0.00	0.00	22.3
5	75	-837	1666	79	0	186	1089	4.02	4.02	4.02	4.02	2	0.16	0.05	0.29	0.00	0.00	22.3
6	75	-1419	1424	-13	0	-8	1223	4.02	4.02	4.02	4.02	2	0.18	0.04	0.25	0.00	0.00	22.3
7	75	-575	1736	-15	0	-8	1072	4.02	4.02	4.02	4.02	2	0.16	0.05	0.30	0.00	0.00	22.3
8	75	-1404	1442	30	0	81	1213	4.02	4.02	4.02	4.02	2	0.18	0.04	0.25	0.00	0.00	22.3
9	75	-560	1754	28	0	82	1068	4.02	4.02	4.02	4.02	2	0.16	0.05	0.31	0.00	0.00	22.3
10	75	-1141	1511	-65	0	-112	1169	4.02	4.02	4.02	4.02	2	0.17	0.04	0.26	0.00	0.00	22.3
11	75	-888	1605	-65	0	-112	1113	4.02	4.02	4.02	4.02	2	0.16	0.05	0.28	0.00	0.00	22.3
12	75	-1090	1573	80	0	185	1135	4.02	4.02	4.02	4.02	2	0.17	0.05	0.27	0.00	0.00	22.3
13	75	-837	1666	79	0	186	1089	4.02	4.02	4.02	4.02	2	0.16	0.05	0.29	0.00	0.00	22.3
14	75	-1419	1424	-13	0	-8	1223	4.02	4.02	4.02	4.02	2	0.18	0.04	0.25	0.00	0.00	22.3
15	75	-575	1736	-15	0	-8	1072	4.02	4.02	4.02	4.02	2	0.16	0.05	0.30	0.00	0.00	22.3
16	75	-1404	1442	30	0	81	1213	4.02	4.02	4.02	4.02	2	0.18	0.04	0.25	0.00	0.00	22.3
17	75	-560	1754	28	0	82	1068	4.02	4.02	4.02	4.02	2	0.16	0.05	0.31	0.00	0.00	22.3
18	75	-2077	1954	-180	0	-318	1762	4.02	4.02	4.02	4.02	3	0.24	0.06	0.33	0.00	0.00	22.3
19	75	-1837	2150	254	0	567	1653	4.02	4.02	4.02	4.02	3	0.22	0.06	0.37	0.00	0.00	22.3
20	75	-1263	2288	20	0	86	1580	4.02	4.02	4.02	4.02	3	0.22	0.07	0.40	0.00	0.00	22.3
37	75	-1929	1853	-334	0	-638	1699	4.02	4.02	4.02	4.02	3	0.23	0.05	0.32	0.00	0.00	22.3
38	75	-1529	2178	390	0	837	1516	4.02	4.02	4.02	4.02	3	0.21	0.06	0.37	0.00	0.00	22.3
39	75	-572	2408	-0	0	36	1461	4.02	4.02	4.02	4.02	3	0.21	0.07	0.42	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	112	-1286	1214	10	0	44	1461	4.02	4.02	4.02	4.02	3	0.20	0.04	0.21	0.00	0.00	22.3
2	112	-1141	856	-65	0	-88	1169	4.02	4.02	4.02	4.02	2	0.17	0.02	0.15	0.00	0.00	22.3
3	112	-888	950	-65	0	-87	1113	4.02	4.02	4.02	4.02	2	0.16	0.03	0.17	0.00	0.00	22.3
4	112	-1090	918	80	0	155	1135	4.02	4.02	4.02	4.02	2	0.17	0.03	0.16	0.00	0.00	22.3
5	112	-837	1011	79	0	156	1089	4.02	4.02	4.02	4.02	2	0.16	0.03	0.18	0.00	0.00	22.3
6	112	-1419	769	-13	0	-3	1223	4.02	4.02	4.02	4.02	2	0.18	0.02	0.13	0.00	0.00	22.3
7	112	-575	1081	-15	0	-2	1072	4.02	4.02	4.02	4.02	2	0.16	0.03	0.19	0.00	0.00	22.3
8	112	-1404	787	30	0	70	1213	4.02	4.02	4.02	4.02	2	0.18	0.02	0.14	0.00	0.00	22.3
9	112	-560	1099	28	0	71	1068	4.02	4.02	4.02	4.02	2	0.16	0.03	0.19	0.00	0.00	22.3
10	112	-1141	856	-65	0	-88	1169	4.02	4.02	4.02	4.02	2	0.17	0.02	0.15	0.00	0.00	22.3
11	112	-888	950	-65	0	-87	1113	4.02	4.02	4.02	4.02	2	0.16	0.03	0.17	0.00	0.00	22.3
12	112	-1090	918	80	0	155	1135	4.02	4.02	4.02	4.02	2	0.17	0.03	0.16	0.00	0.00	22.3
13	112	-837	1011	79	0	156	1089	4.02	4.02	4.02	4.02	2	0.16	0.03	0.18	0.00	0.00	22.3
14	112	-1419	769	-13	0	-3	1223	4.02	4.02	4.02	4.02	2	0.18	0.02	0.13	0.00	0.00	22.3
15	112	-575	1081	-15	0	-2	1072	4.02	4.02	4.02	4.02	2	0.16	0.03	0.19	0.00	0.00	22.3
16	112	-1404	787	30	0	70	1213	4.02	4.02	4.02	4.02	2	0.18	0.02	0.14	0.00	0.00	22.3
17	112	-560	1099	28	0	71	1068	4.02	4.02	4.02	4.02	2	0.16	0.03	0.19	0.00	0.00	22.3

18	112	-2077	1022	-180	0	-250	1762	4.02	4.02	4.02	4.02	3	0.24	0.03	0.17	0.00	0.00	22.3
19	112	-1837	1218	254	0	472	1653	4.02	4.02	4.02	4.02	3	0.22	0.04	0.21	0.00	0.00	22.3
20	112	-1263	1356	20	0	79	1580	4.02	4.02	4.02	4.02	3	0.22	0.04	0.23	0.00	0.00	22.3
37	112	-1929	961	-334	0	-513	1699	4.02	4.02	4.02	4.02	3	0.23	0.03	0.16	0.00	0.00	22.3
38	112	-1529	1286	390	0	691	1516	4.02	4.02	4.02	4.02	3	0.21	0.04	0.22	0.00	0.00	22.3
39	112	-572	1516	-0	0	36	1461	4.02	4.02	4.02	4.02	3	0.21	0.04	0.27	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	150	-1286	363	10	0	41	1461	4.02	4.02	4.02	4.02	3	0.20	0.01	0.06	0.00	0.00	22.3
2	150	-1141	201	-65	0	-64	1169	4.02	4.02	4.02	4.02	2	0.17	0.01	0.03	0.00	0.00	22.3
3	150	-888	295	-65	0	-63	1113	4.02	4.02	4.02	4.02	2	0.16	0.01	0.05	0.00	0.00	22.3
4	150	-1090	263	80	0	126	1135	4.02	4.02	4.02	4.02	2	0.17	0.01	0.05	0.00	0.00	22.3
5	150	-837	356	79	0	126	1089	4.02	4.02	4.02	4.02	2	0.16	0.01	0.06	0.00	0.00	22.3
6	150	-1419	114	-13	0	2	1223	4.02	4.02	4.02	4.02	2	0.18	0.00	0.02	0.00	0.00	22.3
7	150	-575	426	-15	0	4	1072	4.02	4.02	4.02	4.02	2	0.16	0.01	0.07	0.00	0.00	22.3
8	150	-1404	132	30	0	59	1213	4.02	4.02	4.02	4.02	2	0.18	0.00	0.02	0.00	0.00	22.3
9	150	-560	444	28	0	61	1068	4.02	4.02	4.02	4.02	2	0.16	0.01	0.08	0.00	0.00	22.3
10	150	-1141	201	-65	0	-64	1169	4.02	4.02	4.02	4.02	2	0.17	0.01	0.03	0.00	0.00	22.3
11	150	-888	295	-65	0	-63	1113	4.02	4.02	4.02	4.02	2	0.16	0.01	0.05	0.00	0.00	22.3
12	150	-1090	263	80	0	126	1135	4.02	4.02	4.02	4.02	2	0.17	0.01	0.05	0.00	0.00	22.3
13	150	-837	356	79	0	126	1089	4.02	4.02	4.02	4.02	2	0.16	0.01	0.06	0.00	0.00	22.3
14	150	-1419	114	-13	0	2	1223	4.02	4.02	4.02	4.02	2	0.18	0.00	0.02	0.00	0.00	22.3
15	150	-575	426	-15	0	4	1072	4.02	4.02	4.02	4.02	2	0.16	0.01	0.07	0.00	0.00	22.3
16	150	-1404	132	30	0	59	1213	4.02	4.02	4.02	4.02	2	0.18	0.00	0.02	0.00	0.00	22.3
17	150	-560	444	28	0	61	1068	4.02	4.02	4.02	4.02	2	0.16	0.01	0.08	0.00	0.00	22.3
18	150	-2077	90	-180	0	-182	1762	4.02	4.02	4.02	4.02	3	0.24	0.01	0.03	0.00	0.00	22.3
19	150	-1837	286	254	0	377	1653	4.02	4.02	4.02	4.02	3	0.22	0.01	0.05	0.00	0.00	22.3
20	150	-1263	424	20	0	71	1580	4.02	4.02	4.02	4.02	3	0.22	0.01	0.07	0.00	0.00	22.3
37	150	-1929	69	-334	0	-387	1699	4.02	4.02	4.02	4.02	3	0.23	0.01	0.05	0.00	0.00	22.3
38	150	-1529	395	390	0	545	1516	4.02	4.02	4.02	4.02	3	0.21	0.01	0.07	0.00	0.00	22.3
39	150	-572	625	-0	0	36	1461	4.02	4.02	4.02	4.02	3	0.21	0.02	0.11	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	188	-1286	-489	10	0	37	1461	4.02	4.02	4.02	4.02	3	0.20	0.01	0.08	0.00	0.00	22.3
2	188	-1141	-454	-65	0	-39	1169	4.02	4.02	4.02	4.02	2	0.17	0.01	0.08	0.00	0.00	22.3
3	188	-888	-360	-65	0	-39	1113	4.02	4.02	4.02	4.02	2	0.16	0.01	0.06	0.00	0.00	22.3
4	188	-1090	-392	80	0	96	1135	4.02	4.02	4.02	4.02	2	0.17	0.01	0.07	0.00	0.00	22.3
5	188	-837	-299	79	0	96	1089	4.02	4.02	4.02	4.02	2	0.16	0.01	0.05	0.00	0.00	22.3
6	188	-1419	-542	-13	0	7	1223	4.02	4.02	4.02	4.02	2	0.18	0.02	0.09	0.00	0.00	22.3
7	188	-575	-230	-15	0	9	1072	4.02	4.02	4.02	4.02	2	0.16	0.01	0.04	0.00	0.00	22.3
8	188	-1404	-523	30	0	47	1213	4.02	4.02	4.02	4.02	2	0.18	0.02	0.09	0.00	0.00	22.3
9	188	-560	-211	28	0	50	1068	4.02	4.02	4.02	4.02	2	0.16	0.01	0.04	0.00	0.00	22.3
10	188	-1141	-454	-65	0	-39	1169	4.02	4.02	4.02	4.02	2	0.17	0.01	0.08	0.00	0.00	22.3
11	188	-888	-360	-65	0	-39	1113	4.02	4.02	4.02	4.02	2	0.16	0.01	0.06	0.00	0.00	22.3
12	188	-1090	-392	80	0	96	1135	4.02	4.02	4.02	4.02	2	0.17	0.01	0.07	0.00	0.00	22.3
13	188	-837	-299	79	0	96	1089	4.02	4.02	4.02	4.02	2	0.16	0.01	0.05	0.00	0.00	22.3
14	188	-1419	-542	-13	0	7	1223	4.02	4.02	4.02	4.02	2	0.18	0.02	0.09	0.00	0.00	22.3
15	188	-575	-230	-15	0	9	1072	4.02	4.02	4.02	4.02	2	0.16	0.01	0.04	0.00	0.00	22.3
16	188	-1404	-523	30	0	47	1213	4.02	4.02	4.02	4.02	2	0.18	0.02	0.09	0.00	0.00	22.3
17	188	-560	-211	28	0	50	1068	4.02	4.02	4.02	4.02	2	0.16	0.01	0.04	0.00	0.00	22.3
18	188	-2077	-842	-180	0	-115	1762	4.02	4.02	4.02	4.02	3	0.24	0.02	0.14	0.00	0.00	22.3
19	188	-1837	-646	254	0	282	1653	4.02	4.02	4.02	4.02	3	0.22	0.02	0.11	0.00	0.00	22.3
20	188	-1263	-508	20	0	64	1580	4.02	4.02	4.02	4.02	3	0.22	0.01	0.09	0.00	0.00	22.3
37	188	-1929	-822	-334	0	-262	1699	4.02	4.02	4.02	4.02	3	0.23	0.02	0.14	0.00	0.00	22.3
38	188	-1529	-497	390	0	398	1516	4.02	4.02	4.02	4.02	3	0.21	0.01	0.09	0.00	0.00	22.3
39	188	-572	-267	-0	0	36	1461	4.02	4.02	4.02	4.02	3	0.21	0.01	0.05	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	225	-1286	-1341	10	0	33	1461	4.02	4.02	4.02	4.02	3	0.20	0.04	0.23	0.00	0.00	22.3
2	225	-1141	-1109	-65	0	-15	1169	4.02	4.02	4.02	4.02	2	0.17	0.03	0.19	0.00	0.00	22.3
3	225	-888	-1015	-65	0	-14	1113	4.02	4.02	4.02	4.02	2	0.16	0.03	0.18	0.00	0.00	22.3
4	225	-1090	-1047	80	0	66	1135	4.02	4.02	4.02	4.02	2	0.17	0.03	0.18	0.00	0.00	22.3
5	225	-837	-954	79	0	66	1089	4.02	4.02	4.02	4.02	2	0.16	0.03	0.17	0.00	0.00	22.3
6	225	-1419	-1197	-13	0	12	1223	4.02	4.02	4.02	4.02	2	0.18	0.03	0.21	0.00	0.00	22.3
7	225	-575	-885	-15	0	15	1072	4.02	4.02	4.02	4.02	2	0.16	0.03	0.16	0.00	0.00	22.3
8	225	-1404	-1178	30	0	36	1213	4.02	4.02	4.02	4.02	2	0.18	0.03	0.20	0.00	0.00	22.3
9	225	-560	-866	28	0	39	1068	4.02	4.02	4.02	4.02	2	0.16	0.03	0.15	0.00	0.00	22.3
10	225	-1141	-1109	-65	0	-15	1169	4.02	4.02	4.02	4.02	2	0.17	0.03	0.19	0.00	0.00	22.3
11	225	-888	-1015	-65	0	-14	1113	4.02	4.02	4.02	4.02	2	0.16	0.03	0.18	0.00	0.00	22.3
12	225	-1090	-1047	80	0	66	1135	4.02	4.02	4.02	4.02	2	0.17	0.03	0.18	0.00	0.00	22.3
13	225	-837	-954	79	0	66	1089	4.02	4.02	4.02	4.02	2	0.16	0.03	0.17	0.00	0.00	22.3
14	225	-1419	-1197	-13	0	12	1223	4.02	4.02	4.02	4.02	2	0.18	0.03	0.21	0.00	0.00	22.3
15	225	-575	-885	-15	0	15	1072	4.02	4.02	4.02	4.02	2	0.16	0.03	0.16	0.00	0.00	22.3
16	225	-1404	-1178	30	0	36	1213	4.02	4.02	4.02	4.02	2	0.18	0.03	0.20	0.00	0.00	22.3
17	225	-560	-866	28	0	39	1068	4.02	4.02	4.02	4.02	2	0.16	0.03	0.15	0.00	0.00	22.3
18	225	-2077	-1773	-180	0	-47	1762	4.02	4.02	4.02	4.02	3	0.24	0.05	0.30	0.00	0.00	22.3
19	225	-1837	-1577	254	0	186	1653	4.02	4.02	4.02	4.02	3	0.22	0.05	0.27	0.00	0.00	22.3
20	225	-1263	-1439	20	0	56	1580	4.02	4.02	4.02	4.02	3	0.22	0.04	0.25	0.00	0.00	22.3
37	225	-1929	-1714	-334	0	-136	1699	4.02	4.02	4.02	4.02	3	0.23	0.05	0.29	0.00	0.00	22.3
38	225	-1529	-1389	390	0	252	1516	4.02	4.02	4.02	4.02	3	0.21	0.04	0.24	0.00	0.00	22.3
39	225	-572	-1159	-0	0	36	1461	4.02	4.02	4.02	4.02	3	0.21	0.03	0.20	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	262	-1286	-2192	10	0	30	1461	4.02	4.02	4.02	4.02	3	0.20	0.06	0.38	0.00	0.00	22.3
2	262	-1141	-1764	-65	0	9	1169	4.02	4.02	4.02	4.02	2	0.17	0.05	0.31	0.00	0.00	22.3
3	262	-888	-1670	-65	0	10	1113	4.02	4.02	4.02	4.02	2	0.16	0.05	0.29	0.00	0.00	22.3
4	262	-1090	-1702	80	0	36	1135	4.02	4.02	4.02	4.02	2	0.17	0.05	0.30	0.00	0.00	22.3
5	262	-837	-1609	79	0	37	1089	4.02	4.02	4.02	4.02	2	0.16	0.05	0.28	0.00	0.00	22.3
6	262	-1419	-1852	-13	0	17	1183	4.02	4.02	4.02	4.02	2	0.17	0.05	0.32	0.00	0.00	22.3
7	262	-575	-1540	-15	0	21	1072	4.02	4.02	4.02	4.02	2	0.16	0.04	0.27	0.00	0.00	22.3
8	262	-1404	-1833	30	0	25	1184	4.02	4.02	4.02	4.02	2	0.17	0.05	0.32	0.00	0.00	22.3
9	262	-560	-1521	28	0	29	1068	4.02	4.02	4.02	4.02	2	0.16	0.04	0.27	0.00	0.00	22.3
10	262	-1141	-1764	-65	0	9	1169	4.02	4.02	4.02	4.02	2	0.17	0.05	0.31	0.00	0.00	22.3
11	262	-888	-1670	-65	0	10	1113	4.02	4.02	4.02	4.02	2	0.16	0.05	0.29	0.00	0.00	22.3
12	262	-1090	-1702	80	0	36	1135	4.02	4.02	4.02	4.02	2	0.17	0.05	0.30	0.00	0.00	22.3
13	262	-837	-1609	79	0	37	1089	4.02	4.02	4.02	4.02	2	0.16	0.05	0.28	0.00	0.00	22.3
14	262	-1419	-1852	-13	0	17	1183	4.02	4.02	4.02	4.02	2	0.17	0.05	0.32	0.00	0.00	22.3
15	262	-575	-1540	-15	0	21	1072	4.02	4.02	4.02	4.02	2	0.16	0.04	0.27	0.00	0.00	22.3
16	262	-1404	-1833	30	0	25	1184	4.02	4.02	4.02	4.02	2	0.17	0.05	0.32	0.00	0.00	22.3
17	262	-560	-1521	28	0	29	1068	4.02	4.02	4.02	4.02	2	0.16	0.04	0.27	0.00	0.00	22.3
18	262	-2077	-2705	-180	0	21	1662	4.02	4.02	4.02	4.02	3	0.22	0.08	0.46	0.00	0.00	22.3
19	262	-1837	-2509	254	0	91	1653	4.02	4.02	4.02	4.02	3	0.22	0.07	0.43	0.00	0.00	22.3
20	262	-1263	-2371	20	0	49	1580	4.02	4.02	4.02	4.02	3	0.22	0.07	0.41	0.00	0.00	22.3
37	262	-1929	-2606	-334	0	-11	1591	4.02	4.02	4.02	4.02	3	0.22	0.07	0.44	0.00	0.00	22.3
38	262	-1529	-2280	390	0	106	1516	4.02	4.02	4.02	4.02	3	0.21	0.07	0.39	0.00	0.00	22.3
39	262	-572	-2050	-0	0	36	1461	4.02	4.02	4.02	4.02	3	0.21	0.06	0.36	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	300	-1286	-3044	10	0	26	-2091	4.02	4.02	4.02	4.02	3	0.29	0.09	0.53	0.00	0.00	22.3
2	300	-1141	-2419	-65	0	33	-1718	4.02	4.02	4.02	4.02	2	0.25	0.07	0.42	0.00	0.00	22.3
3	300	-888	-2325	-65	0	35	-1587	4.02	4.02	4.02	4.02	2	0.23	0.07	0.41	0.00	0.00	22.3
4	300	-1090	-2357	80	0	6	-1629	4.02	4.02	4.02	4.02	2	0.24	0.07	0.41	0.00	0.00	22.3
5	300	-837	-2264	79	0	7	-1498	4.02	4.02	4.02	4.02	2	0.22	0.07	0.40	0.00	0.00	22.3
6	300	-1419	-2507	-13	0	22	-1841	4.02	4.02	4.02	4.02	2	0.27	0.07	0.43	0.00	0.00	22.3
7	300	-575	-2195	-15	0	26	-1403	4.02	4.02	4.02	4.02	2	0.21	0.06	0.39	0.00	0.00	22.3
8	300	-1404	-2488	30	0	14	-1814	4.02	4.02	4.02	4.02	2	0.26	0.07	0.43	0.00	0.00	22.3
9	300	-560	-2176	28	0	18	-1376	4.02	4.02	4.02	4.02	2	0.21	0.06	0.38	0.00	0.00	22.3
10	300	-1141	-2419	-65	0	33	-1718	4.02	4.02	4.02	4.02	2	0.25	0.07	0.42	0.00	0.00	22.3
11	300	-888	-2325	-65	0	35	-1587	4.02	4.02	4.02	4.02	2	0.23	0.07	0.41	0.00	0.00	22.3
12	300	-1090	-2357	80	0	6	-1629	4.02	4.02	4.02	4.02	2	0.24	0.07	0.41	0.00	0.00	22.3
13	300	-837	-2264	79	0	7	-1498	4.02	4.02	4.02	4.02	2	0.22	0.07	0.40	0.00	0.00	22.3
14	300	-1419	-2507	-13	0	22	-1841	4.02	4.02	4.02	4.02	2	0.27	0.07	0.43	0.00	0.00	22.3
15	300	-575	-2195	-15	0	26	-1403	4.02	4.02	4.02	4.02	2	0.21	0.06	0.39	0.00	0.00	22.3
16	300	-1404	-2488	30	0	14	-1814	4.02	4.02	4.02	4.02	2	0.26	0.07	0.43	0.00	0.00	22.3
17	300	-560	-2176	28	0	18	-1376	4.02	4.02	4.02	4.02	2	0.21	0.06	0.38	0.00	0.00	22.3
18	300	-2077	-3637	-180	0	89	-2737	4.02	4.02	4.02	4.02	3	0.37	0.10	0.62	0.00	0.00	22.3
19	300	-1837	-3441	254	0	-4	-2455	4.02	4.02	4.02	4.02	3	0.33	0.10	0.59	0.00	0.00	22.3
20	300	-1263	-3303	20	0	41	-2251	4.02	4.02	4.02	4.02	3	0.31	0.10	0.57	0.00	0.00	22.3
37	300	-1929	-3498	-334	0	114	-2643	4.02	4.02	4.02	4.02	3	0.36	0.10	0.60	0.00	0.00	22.3
38	300	-1529	-3172	390	0	-41	-2173	4.02	4.02	4.02	4.02	3	0.30	0.09	0.54	0.00	0.00	22.3
39	300	-572	-2942	-0	0	36	-1833	4.02	4.02	4.02	4.02	3	0.26	0.09	0.52	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	338	-1286	-3895	10	0	23	-3471	4.02	4.02	4.02	4.02	3	0.48	0.11	0.67	0.00	0.00	22.3
2	338	-1141	-3074	-65	0	58	-2799	4.02	4.02	4.02	4.02	2	0.41	0.09	0.53	0.00	0.00	22.3
3	338	-888	-2980	-65	0	59	-2645	4.02	4.02	4.02	4.02	2	0.39	0.09	0.52	0.00	0.00	22.3
4	338	-1090	-3012	80	0	-24	-2695	4.02	4.02	4.02	4.02	2	0.40	0.09	0.52	0.00	0.00	22.3
5	338	-837	-2919	79	0	-23	-2541	4.02	4.02	4.02	4.02	2	0.38	0.08	0.51	0.00	0.00	22.3
6	338	-1419	-3162	-13	0	27	-2943	4.02	4.02	4.02	4.02	2	0.43	0.09	0.54	0.00	0.00	22.3
7	338	-575	-2850	-15	0	32	-2429	4.02	4.02	4.02	4.02	2	0.36	0.08	0.50	0.00	0.00	22.3
8	338	-1404	-3143	30	0	3	-2912	4.02	4.02	4.02	4.02	2	0.42	0.09	0.54	0.00	0.00	22.3
9	338	-560	-2831	28	0	8	-2398	4.02	4.02	4.02	4.02	2	0.36	0.08	0.50	0.00	0.00	22.3
10	338	-1141	-3074	-65	0	58	-2799	4.02	4.02	4.02	4.02	2	0.41	0.09	0.53	0.00	0.00	22.3
11	338	-888	-2980	-65	0	59	-2645	4.02	4.02	4.02	4.02	2	0.39	0.09	0.52	0.00	0.00	22.3
12	338	-1090	-3012	80	0	-24	-2695	4.02	4.02	4.02	4.02	2	0.40	0.09	0.52	0.00	0.00	22.3
13	338	-837	-2919	79	0	-23	-2541	4.02	4.02	4.02	4.02	2	0.38	0.08	0.51	0.00	0.00	22.3
14	338	-1419	-3162	-13	0	27	-2943	4.02	4.02	4.02	4.02	2	0.43	0.09	0.54	0.00	0.00	22.3
15	338	-575	-2850	-15	0	32	-2429	4.02	4.02	4.02	4.02	2	0.36	0.08	0.50	0.00	0.00	22.3
16	338	-1404	-3143	30	0	3	-2912	4.02	4.02	4.02	4.02	2	0.42	0.09	0.54	0.00	0.00	22.3
17	338	-560	-2831	28	0	8	-2398	4.02	4.02	4.02	4.02	2	0.36	0.08	0.50	0.00	0.00	22.3
18	338	-2077	-4568	-180	0	156	-4322	4.02	4.02	4.02	4.02	3	0.58	0.13	0.77	0.00	0.00	22.3
19	338	-1837	-4372	254	0	-100	-3992	4.02	4.02	4.02	4.02	3	0.54	0.13	0.75	0.00	0.00	22.3
20	338	-1263	-4234	20	0	34	-3755	4.02	4.02	4.02	4.02	3	0.52	0.12	0.73	0.00	0.00	22.3
37	338	-1929	-4389	-334	0	240	-4164	4.02	4.02	4.02	4.02	3	0.57	0.13	0.75	0.00	0.00	22.3
38	338	-1529	-4063	390	0	-187	-3615	4.02	4.02	4.02	4.02	3	0.50	0.12	0.70	0.00	0.00	22.3
39	338	-572	-3833	-0	0	36	-3219	4.02	4.02	4.02	4.02	3	0.45	0.11	0.67	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	375	-1286	-4747	10	0	19	-3471	4.02	4.02	4.02	4.02	3	0.48	0.14	0.82	0.00	0.00	22.3
2	375	-1141	-3729	-65	0	82	-2799	4.02	4.02	4.02	4.02	2	0.41	0.11	0.65	0.00	0.00	22.3
3	375	-888	-3635	-65	0	83	-2645	4.02	4.02	4.02	4.02	2	0.39	0.11	0.63	0.00	0.00	22.3
4	375	-1090	-3667	80	0	-54	-2695	4.02	4.02	4.02	4.02	2	0.40	0.11	0.64	0.00	0.00	22.3
5	375	-837	-3574	79	0	-53	-2541	4.02	4.02	4.02	4.02	2	0.38	0.10	0.62	0.00	0.00	22.3
6	375	-1419	-3817	-13	0	32	-2943	4.02	4.02	4.02	4.02	2	0.43	0.11	0.66	0.00	0.00	22.3
7	375	-575	-3505	-15	0	38	-2429	4.02	4.02	4.02	4.02	2	0.36	0.10	0.62	0.00	0.00	22.3
8	375	-1404	-3798	30	0	-9	-2912	4.02	4.02	4.02	4.02	2	0.42	0.11	0.65	0.00	0.00	22.3
9	375	-560	-3486	28	0	-3	-2398	4.02	4.02	4.02	4.02	2	0.36	0.10	0.61	0.00	0.00	22.3
10	375	-1141	-3729	-65	0	82	-2799	4.02	4.02	4.02	4.02	2	0.41	0.11	0.65	0.00	0.00	22.3
11	375	-888	-3635	-65	0	83	-2645	4.02	4.02	4.02	4.02	2	0.39	0.11	0.63	0.00	0.00	22.3
12	375	-1090	-3667	80	0	-54	-2695	4.02	4.02	4.02	4.02	2	0.40	0.11	0.64	0.00	0.00	22.3
13	375	-837	-3574	79	0	-53	-2541	4.02	4.02	4.02	4.02	2	0.38	0.10	0.62	0.00	0.00	22.3
14	375	-1419	-3817	-13	0	32	-2943	4.02	4.02	4.02	4.02	2	0.43	0.11	0.66	0.00	0.00	22.3
15	375	-575	-3505	-15	0	38	-2429	4.02	4.02	4.02	4.02	2	0.36	0.10	0.62	0.00	0.00	22.3
16	375	-1404	-3798	30	0	-9	-2912	4.02	4.02	4.02	4.02	2	0.42	0.11	0.65	0.00	0.00	22.3
17	375	-560	-3486	28	0	-3	-2398	4.02	4.02	4.02	4.02	2	0.36	0.10	0.61	0.00	0.00	22.3
18	375	-2077	-5500	-180	0	224	-4322	4.02	4.02	4.02	4.02	3	0.58	0.16	0.93	0.00	0.00	22.3
19	375	-1837	-5304	254	0	-195	-3992	4.02	4.02	4.02	4.02	3	0.54	0.15	0.90	0.00	0.00	22.3
20	375	-1263	-5166	20	0	26	-3755	4.02	4.02	4.02	4.02	3	0.52	0.15	0.89	0.00	0.00	22.3
37	375	-1929	-5281	-334	0	365	-4164	4.02	4.02	4.02	4.02	3	0.57	0.15	0.90	0.00	0.00	22.3
38	375	-1529	-4955	390	0	-333	-3615	4.02	4.02	4.02	4.02	3	0.50	0.14	0.85	0.00	0.00	22.3
39	375	-572	-4725	-0	0	36	-3219	4.02	4.02	4.02	4.02	3	0.45	0.14	0.83	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

Nome travata: **trave_507_IP1** Descrizione: **Trave_5 26-25-24-23**
ASTA NUM. 21 NI 165 NF 210 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y Permanente Neve qy tot.
qy medio: 375.00 1371.75 142.50 1889.25 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm

1	0	-876	4408	11	0	17	-2683	4.02	4.02	4.02	4.02	3	0.38	0.13	0.77	0.00	0.00	22.3
2	0	-721	3340	-15	0	8	-1984	4.02	4.02	4.02	4.02	2	0.29	0.10	0.58	0.00	0.00	22.3
3	0	-613	3419	-16	0	9	-2114	4.02	4.02	4.02	4.02	2	0.31	0.10	0.60	0.00	0.00	22.3
4	0	-735	3362	33	0	17	-2013	4.02	4.02	4.02	4.02	2	0.30	0.10	0.59	0.00	0.00	22.3
5	0	-627	3441	31	0	18	-2144	4.02	4.02	4.02	4.02	2	0.32	0.10	0.60	0.00	0.00	22.3
6	0	-851	3256	3	0	9	-1842	4.02	4.02	4.02	4.02	2	0.27	0.09	0.57	0.00	0.00	22.3
7	0	-493	3518	-1	0	14	-2277	4.02	4.02	4.02	4.02	2	0.34	0.10	0.62	0.00	0.00	22.3
8	0	-855	3263	18	0	12	-1851	4.02	4.02	4.02	4.02	2	0.27	0.09	0.57	0.00	0.00	22.3
9	0	-497	3525	13	0	17	-2285	4.02	4.02	4.02	4.02	2	0.34	0.10	0.62	0.00	0.00	22.3
10	0	-721	3340	-15	0	8	-1984	4.02	4.02	4.02	4.02	2	0.29	0.10	0.58	0.00	0.00	22.3
11	0	-613	3419	-16	0	9	-2114	4.02	4.02	4.02	4.02	2	0.31	0.10	0.60	0.00	0.00	22.3
12	0	-735	3362	33	0	17	-2013	4.02	4.02	4.02	4.02	2	0.30	0.10	0.59	0.00	0.00	22.3
13	0	-627	3441	31	0	18	-2144	4.02	4.02	4.02	4.02	2	0.32	0.10	0.60	0.00	0.00	22.3
14	0	-851	3256	3	0	9	-1842	4.02	4.02	4.02	4.02	2	0.27	0.09	0.57	0.00	0.00	22.3
15	0	-493	3518	-1	0	14	-2277	4.02	4.02	4.02	4.02	2	0.34	0.10	0.62	0.00	0.00	22.3

16	0	-855	3263	18	0	12	-1851	4.02	4.02	4.02	4.02	2	0.27	0.09	0.57	0.00	0.00	22.3
17	0	-497	3525	13	0	17	-2285	4.02	4.02	4.02	4.02	2	0.34	0.10	0.62	0.00	0.00	22.3
18	0	-1190	4611	-50	0	10	-2595	4.02	4.02	4.02	4.02	3	0.36	0.13	0.80	0.00	0.00	22.3
19	0	-1187	4708	90	0	32	-2741	4.02	4.02	4.02	4.02	3	0.38	0.14	0.82	0.00	0.00	22.3
20	0	-879	4866	5	0	23	-3013	4.02	4.02	4.02	4.02	3	0.42	0.14	0.85	0.00	0.00	22.3
37	0	-1078	4422	-100	0	1	-2503	4.02	4.02	4.02	4.02	3	0.35	0.13	0.77	0.00	0.00	22.3
38	0	-1073	4584	134	0	39	-2748	4.02	4.02	4.02	4.02	3	0.38	0.13	0.80	0.00	0.00	22.3
39	0	-560	4847	-8	0	23	-3201	4.02	4.02	4.02	4.02	3	0.45	0.14	0.85	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	38	-876	3556	11	0	13	-2683	4.02	4.02	4.02	4.02	3	0.38	0.10	0.62	0.00	0.00	22.3
2	38	-721	2685	-15	0	14	-1984	4.02	4.02	4.02	4.02	2	0.29	0.08	0.47	0.00	0.00	22.3
3	38	-613	2764	-16	0	15	-2114	4.02	4.02	4.02	4.02	2	0.31	0.08	0.49	0.00	0.00	22.3
4	38	-735	2707	33	0	4	-2013	4.02	4.02	4.02	4.02	2	0.30	0.08	0.47	0.00	0.00	22.3
5	38	-627	2786	31	0	6	-2144	4.02	4.02	4.02	4.02	2	0.32	0.08	0.49	0.00	0.00	22.3
6	38	-851	2601	3	0	8	-1842	4.02	4.02	4.02	4.02	2	0.27	0.08	0.45	0.00	0.00	22.3
7	38	-493	2863	-1	0	15	-2277	4.02	4.02	4.02	4.02	2	0.34	0.08	0.50	0.00	0.00	22.3
8	38	-855	2608	18	0	5	-1851	4.02	4.02	4.02	4.02	2	0.27	0.08	0.46	0.00	0.00	22.3
9	38	-497	2870	13	0	12	-2285	4.02	4.02	4.02	4.02	2	0.34	0.08	0.51	0.00	0.00	22.3
10	38	-721	2685	-15	0	14	-1984	4.02	4.02	4.02	4.02	2	0.29	0.08	0.47	0.00	0.00	22.3
11	38	-613	2764	-16	0	15	-2114	4.02	4.02	4.02	4.02	2	0.31	0.08	0.49	0.00	0.00	22.3
12	38	-735	2707	33	0	4	-2013	4.02	4.02	4.02	4.02	2	0.30	0.08	0.47	0.00	0.00	22.3
13	38	-627	2786	31	0	6	-2144	4.02	4.02	4.02	4.02	2	0.32	0.08	0.49	0.00	0.00	22.3
14	38	-851	2601	3	0	8	-1842	4.02	4.02	4.02	4.02	2	0.27	0.08	0.45	0.00	0.00	22.3
15	38	-493	2863	-1	0	15	-2277	4.02	4.02	4.02	4.02	2	0.34	0.08	0.50	0.00	0.00	22.3
16	38	-855	2608	18	0	5	-1851	4.02	4.02	4.02	4.02	2	0.27	0.08	0.46	0.00	0.00	22.3
17	38	-497	2870	13	0	12	-2285	4.02	4.02	4.02	4.02	2	0.34	0.08	0.51	0.00	0.00	22.3
18	38	-1190	3679	-50	0	29	-2595	4.02	4.02	4.02	4.02	3	0.36	0.11	0.64	0.00	0.00	22.3
19	38	-1187	3776	90	0	-1	-2741	4.02	4.02	4.02	4.02	3	0.38	0.11	0.65	0.00	0.00	22.3
20	38	-879	3934	5	0	22	-3013	4.02	4.02	4.02	4.02	3	0.42	0.11	0.69	0.00	0.00	22.3
37	38	-1078	3530	-100	0	39	-2503	4.02	4.02	4.02	4.02	3	0.35	0.10	0.61	0.00	0.00	22.3
38	38	-1073	3692	134	0	-12	-2748	4.02	4.02	4.02	4.02	3	0.38	0.11	0.64	0.00	0.00	22.3
39	38	-560	3955	-8	0	27	-3201	4.02	4.02	4.02	4.02	3	0.45	0.11	0.70	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	75	-876	2705	11	0	9	-1385	4.02	4.02	4.02	4.02	3	0.19	0.08	0.47	0.00	0.00	22.3
2	75	-721	2030	-15	0	19	1058	4.02	4.02	4.02	4.02	2	0.16	0.06	0.36	0.00	0.00	22.3
3	75	-613	2109	-16	0	21	-1109	4.02	4.02	4.02	4.02	2	0.17	0.06	0.37	0.00	0.00	22.3
4	75	-735	2052	33	0	-8	1056	4.02	4.02	4.02	4.02	2	0.16	0.06	0.36	0.00	0.00	22.3
5	75	-627	2131	31	0	-5	-1133	4.02	4.02	4.02	4.02	2	0.17	0.06	0.37	0.00	0.00	22.3
6	75	-851	1946	3	0	7	1094	4.02	4.02	4.02	4.02	2	0.16	0.06	0.34	0.00	0.00	22.3
7	75	-493	2208	-1	0	15	-1247	4.02	4.02	4.02	4.02	2	0.19	0.06	0.39	0.00	0.00	22.3
8	75	-855	1953	18	0	-1	1093	4.02	4.02	4.02	4.02	2	0.16	0.06	0.34	0.00	0.00	22.3
9	75	-497	2215	13	0	7	-1254	4.02	4.02	4.02	4.02	2	0.19	0.06	0.39	0.00	0.00	22.3
10	75	-721	2030	-15	0	19	1058	4.02	4.02	4.02	4.02	2	0.16	0.06	0.36	0.00	0.00	22.3
11	75	-613	2109	-16	0	21	-1109	4.02	4.02	4.02	4.02	2	0.17	0.06	0.37	0.00	0.00	22.3
12	75	-735	2052	33	0	-8	1056	4.02	4.02	4.02	4.02	2	0.16	0.06	0.36	0.00	0.00	22.3
13	75	-627	2131	31	0	-5	-1133	4.02	4.02	4.02	4.02	2	0.17	0.06	0.37	0.00	0.00	22.3
14	75	-851	1946	3	0	7	1094	4.02	4.02	4.02	4.02	2	0.16	0.06	0.34	0.00	0.00	22.3
15	75	-493	2208	-1	0	15	-1247	4.02	4.02	4.02	4.02	2	0.19	0.06	0.39	0.00	0.00	22.3
16	75	-855	1953	18	0	-1	1093	4.02	4.02	4.02	4.02	2	0.16	0.06	0.34	0.00	0.00	22.3
17	75	-497	2215	13	0	7	-1254	4.02	4.02	4.02	4.02	2	0.19	0.06	0.39	0.00	0.00	22.3
18	75	-1190	2748	-50	0	48	1556	4.02	4.02	4.02	4.02	3	0.22	0.08	0.48	0.00	0.00	22.3
19	75	-1187	2845	90	0	-35	1531	4.02	4.02	4.02	4.02	3	0.21	0.08	0.49	0.00	0.00	22.3
20	75	-879	3003	5	0	20	-1582	4.02	4.02	4.02	4.02	3	0.22	0.09	0.52	0.00	0.00	22.3
37	75	-1078	2639	-100	0	76	1481	4.02	4.02	4.02	4.02	3	0.21	0.08	0.46	0.00	0.00	22.3
38	75	-1073	2801	134	0	-62	1439	4.02	4.02	4.02	4.02	3	0.20	0.08	0.49	0.00	0.00	22.3
39	75	-560	3064	-8	0	30	-1786	4.02	4.02	4.02	4.02	3	0.25	0.09	0.54	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	112	-876	1853	11	0	5	1590	4.02	4.02	4.02	4.02	3	0.22	0.05	0.32	0.00	0.00	22.3
2	112	-721	1375	-15	0	25	1208	4.02	4.02	4.02	4.02	2	0.18	0.04	0.24	0.00	0.00	22.3
3	112	-613	1454	-16	0	28	1226	4.02	4.02	4.02	4.02	2	0.18	0.04	0.26	0.00	0.00	22.3
4	112	-735	1397	33	0	-20	1220	4.02	4.02	4.02	4.02	2	0.18	0.04	0.24	0.00	0.00	22.3
5	112	-627	1476	31	0	-17	1237	4.02	4.02	4.02	4.02	2	0.18	0.04	0.26	0.00	0.00	22.3
6	112	-851	1291	3	0	6	1192	4.02	4.02	4.02	4.02	2	0.18	0.04	0.23	0.00	0.00	22.3
7	112	-493	1553	-1	0	15	1249	4.02	4.02	4.02	4.02	2	0.19	0.04	0.27	0.00	0.00	22.3
8	112	-855	1298	18	0	-8	1196	4.02	4.02	4.02	4.02	2	0.18	0.04	0.23	0.00	0.00	22.3
9	112	-497	1560	13	0	2	1253	4.02	4.02	4.02	4.02	2	0.19	0.05	0.27	0.00	0.00	22.3
10	112	-721	1375	-15	0	25	1208	4.02	4.02	4.02	4.02	2	0.18	0.04	0.24	0.00	0.00	22.3
11	112	-613	1454	-16	0	28	1226	4.02	4.02	4.02	4.02	2	0.18	0.04	0.26	0.00	0.00	22.3
12	112	-735	1397	33	0	-20	1220	4.02	4.02	4.02	4.02	2	0.18	0.04	0.24	0.00	0.00	22.3
13	112	-627	1476	31	0	-17	1237	4.02	4.02	4.02	4.02	2	0.18	0.04	0.26	0.00	0.00	22.3
14	112	-851	1291	3	0	6	1192	4.02	4.02	4.02	4.02	2	0.18	0.04	0.23	0.00	0.00	22.3
15	112	-493	1553	-1	0	15	1249	4.02	4.02	4.02	4.02	2	0.19	0.04	0.27	0.00	0.00	22.3
16	112	-855	1298	18	0	-8	1196	4.02	4.02	4.02	4.02	2	0.18	0.04	0.23	0.00	0.00	22.3
17	112	-497	1560	13	0	2	1253	4.02	4.02	4.02	4.02	2	0.19	0.05	0.27	0.00	0.00	22.3
18	112	-1190	1816	-50	0	67	1684	4.02	4.02	4.02	4.02	3	0.23	0.05	0.31	0.00	0.00	22.3
19	112	-1187	1913	90	0	-69	1719	4.02	4.02	4.02	4.02	3	0.24	0.06	0.33	0.00	0.00	22.3
20	112	-879	2071	5	0	18	1743	4.02	4.02	4.02	4.02	3	0.24	0.06	0.36	0.00	0.00	22.3
37	112	-1078	1747	-100	0	114	1609	4.02	4.02	4.02	4.02	3	0.22	0.05	0.30	0.00	0.00	22.3
38	112	-1073	1909	134	0	-112	1667	4.02	4.02	4.02	4.02	3	0.23	0.06	0.33	0.00	0.00	22.3
39	112	-560	2172	-8	0	33	1707	4.02	4.02	4.02	4.02	3	0.24	0.06	0.38	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	150	-876	1002	11	0	1	1590	4.02	4.02	4.02	4.02	3	0.22	0.03	0.17	0.00	0.00	22.3
2	150	-721	720	-15	0	30	1208	4.02	4.02	4.02	4.02	2	0.18	0.02	0.13	0.00	0.00	22.3
3	150	-613	799	-16	0	34	1226	4.02	4.02	4.02	4.02	2	0.18	0.02	0.14	0.00	0.00	22.3
4	150	-735	742	33	0	-32	1220	4.02	4.02	4.02	4.02	2	0.18	0.02	0.13	0.00	0.00	22.3
5	150	-627	821	31	0	-29	1237	4.02	4.02	4.02	4.02	2	0.18	0.02	0.14	0.00	0.00	22.3
6	150	-851	636	3	0	4	1192	4.02	4.02	4.02	4.02	2	0.18	0.02	0.11	0.00	0.00	22.3
7	150	-493	898	-1	0	16	1249	4.02	4.02	4.02	4.02	2	0.19	0.03	0.16	0.00	0.00	22.3
8	150	-855	643	18	0	-15	1196	4.02	4.02	4.02	4.02	2	0.18	0.02	0.11	0.00	0.00	22.3
9	150	-497	905	13	0	-3	1253	4.02	4.02	4.02	4.02	2	0.19	0.03	0.16	0.00	0.00	22.3
10	150	-721	720	-15	0	30	1208	4.02	4.02	4.02	4.02	2	0.18	0.02	0.13	0.00	0.00	22.3
11	150	-613	799	-16	0	34	1226	4.02	4.02	4.02	4.02	2	0.18	0.02	0.14	0.00	0.00	22.3
12	150	-735	742	33	0	-32	1220	4.02	4.02	4.02	4.02	2	0.18	0.02	0.13	0.00	0.00	22.3
13	150	-627	821	31	0	-29	1237	4.02	4.02	4.02	4.02	2	0.18	0.02	0.14	0.00	0.00	22.3
14	150	-851	636	3	0	4	1192	4.02	4.02	4.02	4.02	2	0.18	0.02	0.11	0.00	0.00	22.3
15	150	-493	898	-1	0	16	1249	4.02	4.02	4.02	4.02	2	0.19	0.03	0.16	0.00	0.00	22.3
16	150	-855	643	18	0	-15	1196	4.02	4.02	4.02	4.02	2	0.18	0.02	0.11	0.00	0.00	22.3
17	150	-497	905	13	0	-3	1253	4.02	4.02	4.02	4.02	2	0.19	0.03	0.16	0.00	0.00	22.3
18	150	-1190	884	-50	0	86	1684	4.02	4.02	4.02	4.02	3	0.23	0.03	0.15	0.00	0.00	22.3
19	150	-1187	981	90	0	-102	1719	4.02	4.02	4.02	4.02	3	0.24	0.03	0.17	0.00	0.00	22.3
20	150	-879	1139	5	0	16	1743	4.02	4.02	4.02	4.02	3	0.24	0.03	0.20	0.00	0.00	22.3
37	150	-1078	856	-100	0	151	1609	4.02	4.02	4.02	4.02	3	0.22	0.02	0.15	0.00	0.00	22.3

38	150	-1073	1017	134	0	-162	1667	4.02	4.02	4.02	4.02	3	0.23	0.03	0.18	0.00	0.00	22.3
39	150	-560	1281	-8	0	36	1707	4.02	4.02	4.02	4.02	3	0.24	0.04	0.23	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	188	-876	150	11	0	-3	1590	4.02	4.02	4.02	4.02	3	0.22	0.00	0.03	0.00	0.00	22.3
2	188	-721	65	-15	0	36	1208	4.02	4.02	4.02	4.02	2	0.18	0.00	0.01	0.00	0.00	22.3
3	188	-613	144	-16	0	40	1226	4.02	4.02	4.02	4.02	2	0.18	0.00	0.03	0.00	0.00	22.3
4	188	-735	87	33	0	-45	1220	4.02	4.02	4.02	4.02	2	0.18	0.00	0.02	0.00	0.00	22.3
5	188	-627	166	31	0	-41	1237	4.02	4.02	4.02	4.02	2	0.18	0.00	0.03	0.00	0.00	22.3
6	188	-851	-19	3	0	3	1192	4.02	4.02	4.02	4.02	2	0.18	0.00	0.00	0.00	0.00	22.3
7	188	-493	243	-1	0	16	1249	4.02	4.02	4.02	4.02	2	0.19	0.01	0.04	0.00	0.00	22.3
8	188	-855	-12	18	0	-21	1196	4.02	4.02	4.02	4.02	2	0.18	0.00	0.00	0.00	0.00	22.3
9	188	-497	250	13	0	-8	1253	4.02	4.02	4.02	4.02	2	0.19	0.01	0.04	0.00	0.00	22.3
10	188	-721	65	-15	0	36	1208	4.02	4.02	4.02	4.02	2	0.18	0.00	0.01	0.00	0.00	22.3
11	188	-613	144	-16	0	40	1226	4.02	4.02	4.02	4.02	2	0.18	0.00	0.03	0.00	0.00	22.3
12	188	-735	87	33	0	-45	1220	4.02	4.02	4.02	4.02	2	0.18	0.00	0.02	0.00	0.00	22.3
13	188	-627	166	31	0	-41	1237	4.02	4.02	4.02	4.02	2	0.18	0.00	0.03	0.00	0.00	22.3
14	188	-851	-19	3	0	3	1192	4.02	4.02	4.02	4.02	2	0.18	0.00	0.00	0.00	0.00	22.3
15	188	-493	243	-1	0	16	1249	4.02	4.02	4.02	4.02	2	0.19	0.01	0.04	0.00	0.00	22.3
16	188	-855	-12	18	0	-21	1196	4.02	4.02	4.02	4.02	2	0.18	0.00	0.00	0.00	0.00	22.3
17	188	-497	250	13	0	-8	1253	4.02	4.02	4.02	4.02	2	0.19	0.01	0.04	0.00	0.00	22.3
18	188	-1190	-48	-50	0	105	1684	4.02	4.02	4.02	4.02	3	0.23	0.00	0.01	0.00	0.00	22.3
19	188	-1187	50	90	0	-136	1719	4.02	4.02	4.02	4.02	3	0.24	0.00	0.01	0.00	0.00	22.3
20	188	-879	208	5	0	15	1743	4.02	4.02	4.02	4.02	3	0.24	0.01	0.04	0.00	0.00	22.3
37	188	-1078	-36	-100	0	189	1609	4.02	4.02	4.02	4.02	3	0.22	0.00	0.01	0.00	0.00	22.3
38	188	-1073	126	134	0	-212	1667	4.02	4.02	4.02	4.02	3	0.23	0.00	0.02	0.00	0.00	22.3
39	188	-560	389	-8	0	39	1707	4.02	4.02	4.02	4.02	3	0.24	0.01	0.07	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	225	-876	-702	11	0	-7	1590	4.02	4.02	4.02	4.02	3	0.22	0.02	0.12	0.00	0.00	22.3
2	225	-721	-590	-15	0	41	1208	4.02	4.02	4.02	4.02	2	0.18	0.02	0.10	0.00	0.00	22.3
3	225	-613	-512	-16	0	46	1226	4.02	4.02	4.02	4.02	2	0.18	0.01	0.09	0.00	0.00	22.3
4	225	-735	-568	33	0	-57	1220	4.02	4.02	4.02	4.02	2	0.18	0.02	0.10	0.00	0.00	22.3
5	225	-627	-490	31	0	-53	1237	4.02	4.02	4.02	4.02	2	0.18	0.01	0.09	0.00	0.00	22.3
6	225	-851	-674	3	0	2	1192	4.02	4.02	4.02	4.02	2	0.18	0.02	0.12	0.00	0.00	22.3
7	225	-493	-412	-1	0	16	1249	4.02	4.02	4.02	4.02	2	0.19	0.01	0.07	0.00	0.00	22.3
8	225	-855	-668	18	0	-28	1196	4.02	4.02	4.02	4.02	2	0.18	0.02	0.12	0.00	0.00	22.3
9	225	-497	-405	13	0	-13	1253	4.02	4.02	4.02	4.02	2	0.19	0.01	0.07	0.00	0.00	22.3
10	225	-721	-590	-15	0	41	1208	4.02	4.02	4.02	4.02	2	0.18	0.02	0.10	0.00	0.00	22.3
11	225	-613	-512	-16	0	46	1226	4.02	4.02	4.02	4.02	2	0.18	0.01	0.09	0.00	0.00	22.3
12	225	-735	-568	33	0	-57	1220	4.02	4.02	4.02	4.02	2	0.18	0.02	0.10	0.00	0.00	22.3
13	225	-627	-490	31	0	-53	1237	4.02	4.02	4.02	4.02	2	0.18	0.01	0.09	0.00	0.00	22.3
14	225	-851	-674	3	0	2	1192	4.02	4.02	4.02	4.02	2	0.18	0.02	0.12	0.00	0.00	22.3
15	225	-493	-412	-1	0	16	1249	4.02	4.02	4.02	4.02	2	0.19	0.01	0.07	0.00	0.00	22.3
16	225	-855	-668	18	0	-28	1196	4.02	4.02	4.02	4.02	2	0.18	0.02	0.12	0.00	0.00	22.3
17	225	-497	-405	13	0	-13	1253	4.02	4.02	4.02	4.02	2	0.19	0.01	0.07	0.00	0.00	22.3
18	225	-1190	-979	-50	0	123	1684	4.02	4.02	4.02	4.02	3	0.23	0.03	0.17	0.00	0.00	22.3
19	225	-1187	-882	90	0	-170	1719	4.02	4.02	4.02	4.02	3	0.24	0.03	0.15	0.00	0.00	22.3
20	225	-879	-724	5	0	13	1743	4.02	4.02	4.02	4.02	3	0.24	0.02	0.13	0.00	0.00	22.3
37	225	-1078	-928	-100	0	226	1609	4.02	4.02	4.02	4.02	3	0.22	0.03	0.16	0.00	0.00	22.3
38	225	-1073	-766	134	0	-262	1667	4.02	4.02	4.02	4.02	3	0.23	0.02	0.13	0.00	0.00	22.3
39	225	-560	-503	-8	0	42	1707	4.02	4.02	4.02	4.02	3	0.24	0.01	0.09	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	262	-876	-1553	11	0	-11	1590	4.02	4.02	4.02	4.02	3	0.22	0.04	0.27	0.00	0.00	22.3
2	262	-721	-1245	-15	0	47	1208	4.02	4.02	4.02	4.02	2	0.18	0.04	0.22	0.00	0.00	22.3
3	262	-613	-1167	-16	0	52	1226	4.02	4.02	4.02	4.02	2	0.18	0.03	0.20	0.00	0.00	22.3
4	262	-735	-1223	33	0	-69	1220	4.02	4.02	4.02	4.02	2	0.18	0.04	0.21	0.00	0.00	22.3
5	262	-627	-1145	31	0	-64	1237	4.02	4.02	4.02	4.02	2	0.18	0.03	0.20	0.00	0.00	22.3
6	262	-851	-1329	3	0	1	1192	4.02	4.02	4.02	4.02	2	0.18	0.04	0.23	0.00	0.00	22.3
7	262	-493	-1067	-1	0	17	1249	4.02	4.02	4.02	4.02	2	0.19	0.03	0.19	0.00	0.00	22.3
8	262	-855	-1323	18	0	-34	1196	4.02	4.02	4.02	4.02	2	0.18	0.04	0.23	0.00	0.00	22.3
9	262	-497	-1060	13	0	-18	1253	4.02	4.02	4.02	4.02	2	0.19	0.03	0.19	0.00	0.00	22.3
10	262	-721	-1245	-15	0	47	1208	4.02	4.02	4.02	4.02	2	0.18	0.04	0.22	0.00	0.00	22.3
11	262	-613	-1167	-16	0	52	1226	4.02	4.02	4.02	4.02	2	0.18	0.03	0.20	0.00	0.00	22.3
12	262	-735	-1223	33	0	-69	1220	4.02	4.02	4.02	4.02	2	0.18	0.04	0.21	0.00	0.00	22.3
13	262	-627	-1145	31	0	-64	1237	4.02	4.02	4.02	4.02	2	0.18	0.03	0.20	0.00	0.00	22.3
14	262	-851	-1329	3	0	1	1192	4.02	4.02	4.02	4.02	2	0.18	0.04	0.23	0.00	0.00	22.3
15	262	-493	-1067	-1	0	17	1249	4.02	4.02	4.02	4.02	2	0.19	0.03	0.19	0.00	0.00	22.3
16	262	-855	-1323	18	0	-34	1196	4.02	4.02	4.02	4.02	2	0.18	0.04	0.23	0.00	0.00	22.3
17	262	-497	-1060	13	0	-18	1253	4.02	4.02	4.02	4.02	2	0.19	0.03	0.19	0.00	0.00	22.3
18	262	-1190	-1911	-50	0	142	1684	4.02	4.02	4.02	4.02	3	0.23	0.06	0.33	0.00	0.00	22.3
19	262	-1187	-1814	90	0	-203	1719	4.02	4.02	4.02	4.02	3	0.24	0.05	0.31	0.00	0.00	22.3
20	262	-879	-1656	5	0	11	1743	4.02	4.02	4.02	4.02	3	0.24	0.05	0.29	0.00	0.00	22.3
37	262	-1078	-1819	-100	0	264	1609	4.02	4.02	4.02	4.02	3	0.22	0.05	0.32	0.00	0.00	22.3
38	262	-1073	-1658	134	0	-312	1667	4.02	4.02	4.02	4.02	3	0.23	0.05	0.29	0.00	0.00	22.3
39	262	-560	-1394	-8	0	46	1707	4.02	4.02	4.02	4.02	3	0.24	0.04	0.25	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	300	-876	-2405	11	0	-15	1539	4.02	4.02	4.02	4.02	3	0.22	0.07	0.42	0.00	0.00	22.3
2	300	-721	-1900	-15	0	52	1138	4.02	4.02	4.02	4.02	2	0.17	0.05	0.33	0.00	0.00	22.3
3	300	-613	-1822	-16	0	58	1205	4.02	4.02	4.02	4.02	2	0.18	0.05	0.32	0.00	0.00	22.3
4	300	-735	-1878	33	0	-82	1164	4.02	4.02	4.02	4.02	2	0.17	0.05	0.33	0.00	0.00	22.3
5	300	-627	-1800	31	0	-76	1229	4.02	4.02	4.02	4.02	2	0.18	0.05	0.32	0.00	0.00	22.3
6	300	-851	-1984	3	0	-1	1070	4.02	4.02	4.02	4.02	2	0.16	0.06	0.35	0.00	0.00	22.3
7	300	-493	-1722	-1	0	17	1249	4.02	4.02	4.02	4.02	2	0.19	0.05	0.30	0.00	0.00	22.3
8	300	-855	-1978	18	0	-41	1078	4.02	4.02	4.02	4.02	2	0.16	0.06	0.35	0.00	0.00	22.3
9	300	-497	-1715	13	0	-23	1253	4.02	4.02	4.02	4.02	2	0.19	0.05	0.30	0.00	0.00	22.3
10	300	-721	-1900	-15	0	52	1138	4.02	4.02	4.02	4.02	2	0.17	0.05	0.33	0.00	0.00	22.3
11	300	-613	-1822	-16	0	58	1205	4.02	4.02	4.02	4.02	2	0.18	0.05	0.32	0.00	0.00	22.3
12	300	-735	-1878	33	0	-82	1164	4.02	4.02	4.02	4.02	2	0.17	0.05	0.33	0.00	0.00	22.3
13	300	-627	-1800	31	0	-76	1229	4.02	4.02	4.02	4.02	2	0.18	0.05	0.32	0.00	0.00	22.3
14	300	-851	-1984	3	0	-1	1070	4.02	4.02	4.02	4.02	2	0.16	0.06	0.35	0.00	0.00	22.3
15	300	-493	-1722	-1	0	17	1249	4.02	4.02	4.02	4.02	2	0.19	0.05	0.30	0.00	0.00	22.3
16	300	-855	-1978	18	0	-41	1078	4.02	4.02	4.02	4.02	2	0.16	0.06	0.35	0.00	0.00	22.3
17	300	-497	-1715	13	0	-23	1253	4.02	4.02	4.02	4.02	2	0.19	0.05	0.30	0.00	0.00	22.3
18	300	-1190	-2843	-50	0	161	1498	4.02	4.02	4.02	4.02	3	0.21	0.08	0.49	0.00	0.00	22.3
19	300	-1187	-2746	90	0	-237	1593	4.02	4.02	4.02	4.02	3	0.22	0.08	0.48	0.00	0.00	22.3
20	300	-879	-2588	5	0	10	1714	4.02	4.02	4.02	4.02	3	0.24	0.07	0.45	0.00	0.00	22.3
37	300	-1078	-2711	-100	0	302	1436	4.02	4.02	4.02	4.02	3	0.20	0.08	0.47	0.00	0.00	22.3
38	300	-1073	-2550	134	0	-362	1594	4.02	4.02	4.02	4.02	3	0.22	0.07	0.44	0.00	0.00	22.3
39	300	-560	-2286	-8	0	49	1707	4.02	4.02	4.02	4.02	3	0.24	0.07	0.40	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	338	-876	-3256	11	0	-19	-2121	4.02	4.02	4.02	4.02	3	0.30	0.09	0.57	0.00	0.00	22.3

2	338	-721	-2555	-15	0	58	-1740	4.02	4.02	4.02	4.02	2	0.26	0.07	0.45	0.00	0.00	22.3
3	338	-613	-2477	-16	0	64	-1575	4.02	4.02	4.02	4.02	2	0.23	0.07	0.43	0.00	0.00	22.3
4	338	-735	-2533	33	0	-94	-1687	4.02	4.02	4.02	4.02	2	0.25	0.07	0.44	0.00	0.00	22.3
5	338	-627	-2455	31	0	-88	-1523	4.02	4.02	4.02	4.02	2	0.23	0.07	0.43	0.00	0.00	22.3
6	338	-851	-2639	3	0	-2	-1914	4.02	4.02	4.02	4.02	2	0.28	0.08	0.46	0.00	0.00	22.3
7	338	-493	-2377	-1	0	18	-1365	4.02	4.02	4.02	4.02	2	0.20	0.07	0.42	0.00	0.00	22.3
8	338	-855	-2633	18	0	-48	-1898	4.02	4.02	4.02	4.02	2	0.28	0.08	0.46	0.00	0.00	22.3
9	338	-497	-2370	13	0	-28	-1349	4.02	4.02	4.02	4.02	2	0.20	0.07	0.42	0.00	0.00	22.3
10	338	-721	-2555	-15	0	58	-1740	4.02	4.02	4.02	4.02	2	0.26	0.07	0.45	0.00	0.00	22.3
11	338	-613	-2477	-16	0	64	-1575	4.02	4.02	4.02	4.02	2	0.23	0.07	0.43	0.00	0.00	22.3
12	338	-735	-2533	33	0	-94	-1687	4.02	4.02	4.02	4.02	2	0.25	0.07	0.44	0.00	0.00	22.3
13	338	-627	-2455	31	0	-88	-1523	4.02	4.02	4.02	4.02	2	0.23	0.07	0.43	0.00	0.00	22.3
14	338	-851	-2639	3	0	-2	-1914	4.02	4.02	4.02	4.02	2	0.28	0.08	0.46	0.00	0.00	22.3
15	338	-493	-2377	-1	0	18	-1365	4.02	4.02	4.02	4.02	2	0.20	0.07	0.42	0.00	0.00	22.3
16	338	-855	-2633	18	0	-48	-1898	4.02	4.02	4.02	4.02	2	0.28	0.08	0.46	0.00	0.00	22.3
17	338	-497	-2370	13	0	-28	-1349	4.02	4.02	4.02	4.02	2	0.20	0.07	0.42	0.00	0.00	22.3
18	338	-1190	-3774	-50	0	180	-2771	4.02	4.02	4.02	4.02	3	0.38	0.11	0.65	0.00	0.00	22.3
19	338	-1187	-3677	90	0	-271	-2555	4.02	4.02	4.02	4.02	3	0.35	0.11	0.64	0.00	0.00	22.3
20	338	-879	-3519	5	0	8	-2235	4.02	4.02	4.02	4.02	3	0.31	0.10	0.61	0.00	0.00	22.3
37	338	-1078	-3602	-100	0	339	-2638	4.02	4.02	4.02	4.02	3	0.37	0.10	0.63	0.00	0.00	22.3
38	338	-1073	-3441	134	0	-412	-2277	4.02	4.02	4.02	4.02	3	0.32	0.10	0.60	0.00	0.00	22.3
39	338	-560	-3177	-8	0	52	-1743	4.02	4.02	4.02	4.02	3	0.25	0.09	0.56	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	375	-876	-4108	11	0	-24	-2121	4.02	4.02	4.02	4.02	3	0.30	0.12	0.72	0.00	0.00	22.3
2	375	-721	-3210	-15	0	64	-1740	4.02	4.02	4.02	4.02	2	0.26	0.09	0.56	0.00	0.00	22.3
3	375	-613	-3132	-16	0	70	-1575	4.02	4.02	4.02	4.02	2	0.23	0.09	0.55	0.00	0.00	22.3
4	375	-735	-3188	33	0	-106	-1687	4.02	4.02	4.02	4.02	2	0.25	0.09	0.56	0.00	0.00	22.3
5	375	-627	-3110	31	0	-100	-1523	4.02	4.02	4.02	4.02	2	0.23	0.09	0.55	0.00	0.00	22.3
6	375	-851	-3294	3	0	-3	-1914	4.02	4.02	4.02	4.02	2	0.28	0.10	0.57	0.00	0.00	22.3
7	375	-493	-3032	-1	0	18	-1365	4.02	4.02	4.02	4.02	2	0.20	0.09	0.53	0.00	0.00	22.3
8	375	-855	-3288	18	0	-54	-1898	4.02	4.02	4.02	4.02	2	0.28	0.10	0.57	0.00	0.00	22.3
9	375	-497	-3025	13	0	-33	-1349	4.02	4.02	4.02	4.02	2	0.20	0.09	0.53	0.00	0.00	22.3
10	375	-721	-3210	-15	0	64	-1740	4.02	4.02	4.02	4.02	2	0.26	0.09	0.56	0.00	0.00	22.3
11	375	-613	-3132	-16	0	70	-1575	4.02	4.02	4.02	4.02	2	0.23	0.09	0.55	0.00	0.00	22.3
12	375	-735	-3188	33	0	-106	-1687	4.02	4.02	4.02	4.02	2	0.25	0.09	0.56	0.00	0.00	22.3
13	375	-627	-3110	31	0	-100	-1523	4.02	4.02	4.02	4.02	2	0.23	0.09	0.55	0.00	0.00	22.3
14	375	-851	-3294	3	0	-3	-1914	4.02	4.02	4.02	4.02	2	0.28	0.10	0.57	0.00	0.00	22.3
15	375	-493	-3032	-1	0	18	-1365	4.02	4.02	4.02	4.02	2	0.20	0.09	0.53	0.00	0.00	22.3
16	375	-855	-3288	18	0	-54	-1898	4.02	4.02	4.02	4.02	2	0.28	0.10	0.57	0.00	0.00	22.3
17	375	-497	-3025	13	0	-33	-1349	4.02	4.02	4.02	4.02	2	0.20	0.09	0.53	0.00	0.00	22.3
18	375	-1190	-4706	-50	0	199	-2771	4.02	4.02	4.02	4.02	3	0.38	0.14	0.81	0.00	0.00	22.3
19	375	-1187	-4609	90	0	-304	-2555	4.02	4.02	4.02	4.02	3	0.35	0.13	0.80	0.00	0.00	22.3
20	375	-879	-4451	5	0	6	-2235	4.02	4.02	4.02	4.02	3	0.31	0.13	0.78	0.00	0.00	22.3
37	375	-1078	-4494	-100	0	377	-2638	4.02	4.02	4.02	4.02	3	0.37	0.13	0.78	0.00	0.00	22.3
38	375	-1073	-4333	134	0	-462	-2277	4.02	4.02	4.02	4.02	3	0.32	0.13	0.75	0.00	0.00	22.3
39	375	-560	-4069	-8	0	55	-1743	4.02	4.02	4.02	4.02	3	0.25	0.12	0.72	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

Delta Ingegneria srl
via Artemide 3 92100 Agrigento - tel 0922 402212
email - g.ferraro@deltaingegneria.it

Lavoro: **D2403a** Intestazione lavoro: **Palestra Campobello**
Elemento: **TRAVE** Gruppo: **5** Tabella: **Tabella travi**
Descrizione: **Travi copertura spogliatoi**
Rck: **350.00** daN/cm^2 fyk: **4580.0** daN/cm^2
Copriferro superiore: **5.0** cm Copriferro inferiore: **5.0** cm Copriferro laterale: **5.0** cm
Verifica in ottemperanza alle NTC2018
Per le combinazioni sismiche la capacità è valutata in campo elastico o sostanzialmente elastico(§7.4.1 NTC2018)

Diametro staffe: **8** mm Numero braccia: **2**

Nome travata: **trave_501_IP1** Descrizione: **Trave_5 11-16-21-26**
ASTA NUM. 1 NI 169 NF 171 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y qy tot.
qy medio: 375.00 375.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	634	955	65	0	171	577	4.02	4.02	4.02	4.02	3	0.08	0.03	0.17	0.00	0.00	22.3
2	0	613	571	8	0	13	850	4.02	4.02	4.02	4.02	2	0.13	0.02	0.10	0.00	0.00	22.3
3	0	620	569	8	0	16	854	4.02	4.02	4.02	4.02	2	0.13	0.02	0.10	0.00	0.00	22.3
4	0	355	900	92	0	247	-421	4.02	4.02	4.02	4.02	2	0.07	0.03	0.16	0.00	0.00	22.3
5	0	362	898	93	0	249	-417	4.02	4.02	4.02	4.02	2	0.07	0.03	0.16	0.00	0.00	22.3
6	0	515	687	36	0	93	561	4.02	4.02	4.02	4.02	2	0.09	0.02	0.12	0.00	0.00	22.3
7	0	538	683	39	0	100	572	4.02	4.02	4.02	4.02	2	0.09	0.02	0.12	0.00	0.00	22.3
8	0	437	786	62	0	163	-82	4.02	4.02	4.02	4.02	2	0.05	0.02	0.14	0.00	0.00	22.3
9	0	461	782	64	0	170	-69	4.02	4.02	4.02	4.02	2	0.05	0.02	0.14	0.00	0.00	22.3
10	0	613	571	8	0	13	850	4.02	4.02	4.02	4.02	2	0.13	0.02	0.10	0.00	0.00	22.3
11	0	620	569	8	0	16	854	4.02	4.02	4.02	4.02	2	0.13	0.02	0.10	0.00	0.00	22.3
12	0	355	900	92	0	247	-421	4.02	4.02	4.02	4.02	2	0.07	0.03	0.16	0.00	0.00	22.3
13	0	362	898	93	0	249	-417	4.02	4.02	4.02	4.02	2	0.07	0.03	0.16	0.00	0.00	22.3
14	0	515	687	36	0	93	561	4.02	4.02	4.02	4.02	2	0.09	0.02	0.12	0.00	0.00	22.3
15	0	538	683	39	0	100	572	4.02	4.02	4.02	4.02	2	0.09	0.02	0.12	0.00	0.00	22.3
16	0	437	786	62	0	163	-82	4.02	4.02	4.02	4.02	2	0.05	0.02	0.14	0.00	0.00	22.3
17	0	461	782	64	0	170	-69	4.02	4.02	4.02	4.02	2	0.05	0.02	0.14	0.00	0.00	22.3
18	0	1659	225	20	0	31	2334	4.02	4.02	4.02	4.02	3	0.35	0.01	0.04	0.00	0.00	22.3
19	0	695	1290	250	0	673	-903	4.02	4.02	4.02	4.02	3	0.17	0.04	0.23	0.00	0.00	22.3
20	0	1071	783	113	0	291	1009	4.02	4.02	4.02	4.02	3	0.15	0.02	0.14	0.00	0.00	22.3
37	0	1803	-66	-79	0	-242	3153	4.02	4.02	4.02	4.02	3	0.48	0.00	0.01	0.00	0.00	22.3
38	0	196	1709	304	0	827	-2159	4.02	4.02	4.02	4.02	3	0.31	0.05	0.30	0.00	0.00	22.3
39	0	822	864	75	0	190	804	4.02	4.02	4.02	4.02	3	0.12	0.03	0.15	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	56	634	680	65	0	134	899	4.02	4.02	4.02	4.02	3	0.13	0.02	0.12	0.00	0.00	22.3
2	56	613	359	8	0	9	990	4.02	4.02	4.02	4.02	2	0.15	0.01	0.06	0.00	0.00	22.3
3	56	620	358	8	0	11	992	4.02	4.02	4.02	4.02	2	0.15	0.01	0.06	0.00	0.00	22.3
4	56	355	688	92	0	195	376	4.02	4.02	4.02	4.02	2	0.06	0.02	0.12	0.00	0.00	22.3
5	56	362	687	93	0	197	378	4.02	4.02	4.02	4.02	2	0.06	0.02	0.12	0.00	0.00	22.3
6	56	515	475	36	0	72	782	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
7	56	538	471	39	0	78	791	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
8	56	437	574	62	0	128	593	4.02	4.02	4.02	4.02	2	0.09	0.02	0.10	0.00	0.00	22.3
9	56	461	570	64	0	134	602	4.02	4.02	4.02	4.02	2	0.09	0.02	0.10	0.00	0.00	22.3
10	56	613	359	8	0	9	990	4.02	4.02	4.02	4.02	2	0.15	0.01	0.06	0.00	0.00	22.3
11	56	620	358	8	0	11	992	4.02	4.02	4.02	4.02	2	0.15	0.01	0.06	0.00	0.00	22.3
12	56	355	688	92	0	195	376	4.02	4.02	4.02	4.02	2	0.06	0.02	0.12	0.00	0.00	22.3
13	56	362	687	93	0	197	378	4.02	4.02	4.02	4.02	2	0.06	0.02	0.12	0.00	0.00	22.3
14	56	515	475	36	0	72	782	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
15	56	538	471	39	0	78	791	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
16	56	437	574	62	0	128	593	4.02	4.02	4.02	4.02	2	0.09	0.02	0.10	0.00	0.00	22.3
17	56	461	570	64	0	134	602	4.02	4.02	4.02	4.02	2	0.09	0.02	0.10	0.00	0.00	22.3
18	56	1659	-51	20	0	20	2334	4.02	4.02	4.02	4.02	3	0.35	0.00	0.01	0.00	0.00	22.3
19	56	695	1014	250	0	531	-766	4.02	4.02	4.02	4.02	3	0.13	0.03	0.18	0.00	0.00	22.3
20	56	1071	507	113	0	227	1234	4.02	4.02	4.02	4.02	3	0.18	0.01	0.09	0.00	0.00	22.3
37	56	1803	-341	-79	0	-197	3153	4.02	4.02	4.02	4.02	3	0.48	0.01	0.06	0.00	0.00	22.3
38	56	196	1434	304	0	655	-1997	4.02	4.02	4.02	4.02	3	0.29	0.04	0.26	0.00	0.00	22.3
39	56	822	589	75	0	148	1075	4.02	4.02	4.02	4.02	3	0.16	0.02	0.10	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	113	634	404	65	0	97	1012	4.02	4.02	4.02	4.02	3	0.15	0.01	0.07	0.00	0.00	22.3
2	113	613	147	8	0	5	990	4.02	4.02	4.02	4.02	2	0.15	0.00	0.03	0.00	0.00	22.3
3	113	620	146	8	0	6	992	4.02	4.02	4.02	4.02	2	0.15	0.00	0.03	0.00	0.00	22.3
4	113	355	476	92	0	143	597	4.02	4.02	4.02	4.02	2	0.09	0.01	0.08	0.00	0.00	22.3
5	113	362	475	93	0	144	599	4.02	4.02	4.02	4.02	2	0.09	0.01	0.08	0.00	0.00	22.3
6	113	515	264	36	0	51	839	4.02	4.02	4.02	4.02	2	0.13	0.01	0.05	0.00	0.00	22.3
7	113	538	259	39	0	56	845	4.02	4.02	4.02	4.02	2	0.13	0.01	0.05	0.00	0.00	22.3
8	113	437	362	62	0	93	737	4.02	4.02	4.02	4.02	2	0.11	0.01	0.06	0.00	0.00	22.3
9	113	461	358	64	0	97	741	4.02	4.02	4.02	4.02	2	0.11	0.01	0.06	0.00	0.00	22.3
10	113	613	147	8	0	5	990	4.02	4.02	4.02	4.02	2	0.15	0.00	0.03	0.00	0.00	22.3
11	113	620	146	8	0	6	992	4.02	4.02	4.02	4.02	2	0.15	0.00	0.03	0.00	0.00	22.3
12	113	355	476	92	0	143	597	4.02	4.02	4.02	4.02	2	0.09	0.01	0.08	0.00	0.00	22.3
13	113	362	475	93	0	144	599	4.02	4.02	4.02	4.02	2	0.09	0.01	0.08	0.00	0.00	22.3
14	113	515	264	36	0	51	839	4.02	4.02	4.02	4.02	2	0.13	0.01	0.05	0.00	0.00	22.3
15	113	538	259	39	0	56	845	4.02	4.02	4.02	4.02	2	0.13	0.01	0.05	0.00	0.00	22.3
16	113	437	362	62	0	93	737	4.02	4.02	4.02	4.02	2	0.11	0.01	0.06	0.00	0.00	22.3
17	113	461	358	64	0	97	741	4.02	4.02	4.02	4.02	2	0.11	0.01	0.06	0.00	0.00	22.3
18	113	1659	-326	20	0	8	2334	4.02	4.02	4.02	4.02	3	0.35	0.01	0.06	0.00	0.00	22.3
19	113	695	739	250	0	390	617	4.02	4.02	4.02	4.02	3	0.10	0.02	0.13	0.00	0.00	22.3
20	113	1071	232	113	0	163	1239	4.02	4.02	4.02	4.02	3	0.18	0.01	0.04	0.00	0.00	22.3
37	113	1803	-617	-79	0	-153	3079	4.02	4.02	4.02	4.02	3	0.47	0.02	0.11	0.00	0.00	22.3
38	113	196	1158	304	0	483	-1126	4.02	4.02	4.02	4.02	3	0.16	0.03	0.21	0.00	0.00	22.3
39	113	822	313	75	0	106	1131	4.02	4.02	4.02	4.02	3	0.17	0.01	0.06	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	170	634	129	65	0	60	1012	4.02	4.02	4.02	4.02	3	0.15	0.00	0.02	0.00	0.00	22.3
2	170	613	-65	8	0	1	990	4.02	4.02	4.02	4.02	2	0.15	0.00	0.01	0.00	0.00	22.3
3	170	620	-66	8	0	2	992	4.02	4.02	4.02	4.02	2	0.15	0.00	0.01	0.00	0.00	22.3
4	170	355	264	92	0	90	655	4.02	4.02	4.02	4.02	2	0.10	0.01	0.05	0.00	0.00	22.3
5	170	362	263	93	0	91	656	4.02	4.02	4.02	4.02	2	0.10	0.01	0.05	0.00	0.00	22.3
6	170	515	52	36	0	31	839	4.02	4.02	4.02	4.02	2	0.13	0.00	0.01	0.00	0.00	22.3
7	170	538	47	39	0	34	845	4.02	4.02	4.02	4.02	2	0.13	0.00	0.01	0.00	0.00	22.3
8	170	437	150	62	0	58	737	4.02	4.02	4.02	4.02	2	0.11	0.00	0.03	0.00	0.00	22.3
9	170	461	146	64	0	61	741	4.02	4.02	4.02	4.02	2	0.11	0.00	0.03	0.00	0.00	22.3
10	170	613	-65	8	0	1	990	4.02	4.02	4.02	4.02	2	0.15	0.00	0.01	0.00	0.00	22.3
11	170	620	-66	8	0	2	992	4.02	4.02	4.02	4.02	2	0.15	0.00	0.01	0.00	0.00	22.3
12	170	355	264	92	0	90	655	4.02	4.02	4.02	4.02	2	0.10	0.01	0.05	0.00	0.00	22.3
13	170	362	263	93	0	91	656	4.02	4.02	4.02	4.02	2	0.10	0.01	0.05	0.00	0.00	22.3
14	170	515	52	36	0	31	839	4.02	4.02	4.02	4.02	2	0.13	0.00	0.01	0.00	0.00	22.3
15	170	538	47	39	0	34	845	4.02	4.02	4.02	4.02	2	0.13	0.00	0.01	0.00	0.00	22.3
16	170	437	150	62	0	58	737	4.02	4.02	4.02	4.02	2	0.11	0.00	0.03	0.00	0.00	22.3
17	170	461	146	64	0	61	741	4.02	4.02	4.02	4.02	2	0.11	0.00	0.03	0.00	0.00	22.3
18	170	1659	-602	20	0	-3	2270	4.02	4.02	4.02	4.02	3	0.34	0.02	0.11	0.00	0.00	22.3
19	170	695	464	250	0	248	795	4.02	4.02	4.02	4.02	3	0.12	0.01	0.08	0.00	0.00	22.3
20	170	1071	-44	113	0	100	1239	4.02	4.02	4.02	4.02	3	0.18	0.00	0.01	0.00	0.00	22.3
37	170	1803	-892	-79	0	-108	2792	4.02	4.02	4.02	4.02	3	0.42	0.03	0.16	0.00	0.00	22.3
38	170	196	882	304	0	312	484	4.02	4.02	4.02	4.02	3	0.08	0.03	0.16	0.00	0.00	22.3
39	170	822	38	75	0	64	1131	4.02	4.02	4.02	4.02	3	0.17	0.00	0.01	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	226	634	-147	65	0	23	1012	4.02	4.02	4.02	4.02	3	0.15	0.00	0.03	0.00	0.00	22.3
2	226	613	-277	8	0	-4	990	4.02	4.02	4.02	4.02	2	0.15	0.01	0.05	0.00	0.00	22.3
3	226	620	-278	8	0	-3	992	4.02	4.02	4.02	4.02	2	0.15	0.01	0.05	0.00	0.00	22.3
4	226	355	52	92	0	38	655	4.02	4.02	4.02	4.02	2	0.10	0.00	0.01	0.00	0.00	22.3
5	226	362	51	93	0	39	656	4.02	4.02	4.02	4.02	2	0.10	0.00	0.01	0.00	0.00	22.3
6	226	515	-160	36	0	10	839	4.02	4.02	4.02	4.02	2	0.13	0.00	0.03	0.00	0.00	22.3
7	226	538	-165	39	0	12	845	4.02	4.02	4.02	4.02	2	0.13	0.00	0.03	0.00	0.00	22.3
8	226	437	-62	62	0	23	737	4.02	4.02	4.02	4.02	2	0.11	0.00	0.01	0.00	0.00	22.3
9	226	461	-66	64	0	25	741	4.02	4.02	4.02	4.02	2	0.11	0.00	0.01	0.00	0.00	22.3
10	226	613	-277	8	0	-4	990	4.02	4.02	4.02	4.02	2	0.15	0.01	0.05	0.00	0.00	22.3
11	226	620	-278	8	0	-3	992	4.02	4.02	4.02	4.02	2	0.15	0.01	0.05	0.00	0.00	22.3
12	226	355	52	92	0	38	655	4.02	4.02	4.02	4.02	2	0.10	0.00	0.01	0.00	0.00	22.3
13	226	362	51	93	0	39	656	4.02	4.02	4.02	4.02	2	0.10	0.00	0.01	0.00	0.00	22.3
14	226	515	-160	36	0	10	839	4.02	4.02	4.02	4.02	2	0.13	0.00	0.03	0.00	0.00	22.3
15	226	538	-165	39	0	12	845	4.02	4.02	4.02	4.02	2	0.13	0.00	0.03	0.00	0.00	22.3
16	226	437	-62	62	0	23	737	4.02	4.02	4.02	4.02	2	0.11	0.00	0.01	0.00	0.00	22.3
17	226	461	-66	64	0	25	741	4.02	4.02	4.02	4.02	2	0.11	0.00	0.01	0.00	0.00	22.3
18	226	1659	-877	20	0	-15	1992	4.02	4.02	4.02	4.02	3	0.30	0.03	0.16	0.00	0.00	22.3
19	226	695	188	250	0	107	795	4.02	4.02	4.02	4.02	3	0.12	0.01	0.04	0.00	0.00	22.3
20	226	1071	-319	113	0	36	1239	4.02	4.02	4.02	4.02	3	0.18	0.01	0.06	0.00	0.00	22.3
37	226	1803	-1168	-79	0	-63	2350	4.02	4.02	4.02	4.02	3	0.36	0.03	0.21	0.00	0.00	22.3
38	226	196	607	304	0	140	765	4.02	4.02	4.02	4.02	3	0.11	0.02	0.11	0.00	0.00	22.3
39	226	822	-238	75	0	22	1131	4.02	4.02	4.02	4.02	3	0.17	0.01	0.04	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	282	634	-422	65	0	-14	1012	4.02	4.02	4.02	4.02	3	0.15	0.01	0.08	0.00	0.00	22.3
2	282	613	-489	8	0	-8	924	4.02	4.02	4.02	4.02	2	0.14	0.01	0.09	0.00	0.00	22.3
3	282	620	-490	8	0	-8	925	4.02	4.02	4.02	4.02	2	0.14	0.01	0.09	0.00	0.00	22.3
4	282	355	-160	92	0	-14	655	4.02	4.02	4.02	4.02	2	0.10	0.00	0.03	0.00	0.00	22.3
5	282	362	-161	93	0	-14	656	4.02	4.02	4.02	4.02	2	0.10	0.00	0.03	0.00	0.00	22.3
6	282	515	-372	36	0	-10	839	4.02	4.02	4.02	4.02	2	0.13	0.01	0.07	0.00	0.00	22.3
7	282	538	-376	39	0	-10	845	4.02	4.02	4.02	4.02	2	0.13	0.01	0.07	0.00	0.00	22.3
8	282	437	-274	62	0	-12	737	4.02	4.02	4.02	4.02	2	0.11	0.01	0.05	0.00	0.00	22.3
9	282	461	-278	64	0	-12	741	4.02	4.02	4.02	4.02	2	0.11	0.01	0.05	0.00	0.00	22.3
10	282	613	-489	8	0	-8	924	4.02	4.02	4.02	4.02	2	0.14	0.01	0.09	0.00	0.00	22.3
11	282	620	-490	8	0	-8	925	4.02	4.02	4.02	4.02	2	0.14	0.01	0.09	0.00	0.00	22.3
12	282	355	-160	92	0	-14	655	4.02	4.02	4.02	4.02	2	0.10	0.00	0.03	0.00	0.00	22.3
13	282	362	-161	93	0	-14	656	4.02	4.02	4.02	4.02	2	0.10	0.00	0.03	0.00	0.00	22.3
14	282	515	-372	36	0	-10	839	4.02	4.02	4.02	4.02	2	0.13	0.01	0.07	0.00	0.00	22.3
15	282	538	-376	39	0	-10	845	4.02	4.02	4.02	4.02	2	0.13	0.01	0.07	0.00	0.00	22.3
16	282	437	-274	62	0	-12	737	4.02	4.02	4.02	4.02	2	0.11	0.01	0.05	0.00	0.00	22.3
17	282	461	-278	64	0	-12	741	4.02	4.02	4.02	4.02	2	0.11	0.01	0.05	0.00	0.00	22.3
18	282	1659	-1153	20	0	-26	1558	4.02	4.02	4.02	4.02	3	0.23	0.03	0.21	0.00	0.00	22.3
19	282	695	-88	250	0	-34	795	4.02	4.02	4.02	4.02	3	0.12	0.01	0.04	0.00	0.00	22.3
20	282	1071	-595	113	0	-28	1180	4.02	4.02	4.02	4.02	3	0.17	0.02	0.11	0.00	0.00	22.3
37	282	1803	-1443	-79	0	-18	1752	4.02	4.02	4.02	4.02	3	0.27	0.04	0.26	0.00	0.00	22.3
38	282	196	332	304	0	-32	832	4.02	4.02	4.02	4.02	3	0.12	0.01	0.06	0.00	0.00	22.3
39	282	822	-513	75	0	-21	1122	4.02	4.02	4.02	4.02	3	0.16	0.01	0.09	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	339	634	-697	65	0	-51	883	4.02	4.02	4.02	4.02	3	0.13	0.02	0.12	0.00	0.00	22.3
2	339	613	-701	8	0	-12	696	4.02	4.02	4.02	4.02	2	0.11	0.02	0.12	0.00	0.00	22.3
3	339	620	-702	8	0	-13	696	4.02	4.02	4.02	4.02	2	0.11	0.02	0.12	0.00	0.00	22.3
4	339	355	-372	92	0	-66	655	4.02	4.02	4.02	4.02	2	0.10	0.01	0.07	0.00	0.00	22.3
5	339	362	-373	93	0	-66	656	4.02	4.02	4.02	4.02	2	0.10	0.01	0.07	0.00	0.00	22.3
6	339	515	-584	36	0	-31	684	4.02	4.02	4.02	4.02	2	0.11	0.02	0.10	0.00	0.00	22.3
7	339	538	-588	39	0	-32	685	4.02	4.02	4.02	4.02	2	0.11	0.02	0.10	0.00	0.00	22.3
8	339	437	-485	62	0	-47	674	4.02	4.02	4.02	4.02	2	0.10	0.01	0.09	0.00	0.00	22.3
9	339	461	-489	64	0	-48	675	4.02	4.02	4.02	4.02	2	0.10	0.01	0.09	0.00	0.00	22.3
10	339	613	-701	8	0	-12	696	4.02	4.02	4.02	4.02	2	0.11	0.02	0.12	0.00	0.00	22.3
11	339	620	-702	8	0	-13	696	4.02	4.02	4.02	4.02	2	0.11	0.02	0.12	0.00	0.00	22.3
12	339	355	-372	92	0	-66	655	4.02	4.02	4.02	4.02	2	0.10	0.01	0.07	0.00	0.00	22.3
13	339	362	-373	93	0	-66	656	4.02	4.02	4.02	4.02	2	0.10	0.01	0.07	0.00	0.00	22.3
14	339	515	-584	36	0	-31	684	4.02	4.02	4.02	4.02	2	0.11	0.02	0.10	0.00	0.00	22.3
15	339	538	-588	39	0	-32	685	4.02	4.02	4.02	4.02	2	0.11	0.02	0.10	0.00	0.00	22.3
16	339	437	-485	62	0	-47	674	4.02	4.02	4.02	4.02	2	0.10	0.01	0.09	0.00	0.00	22.3
17	339	461	-489	64	0	-48	675	4.02	4.02	4.02	4.02	2	0.10	0.01	0.09	0.00	0.00	22.3
18	339	1659	-1428	20	0	-38	968	4.02	4.02	4.02	4.02	3	0.15	0.04	0.25	0.00	0.00	22.3
19	339	695	-363	250	0	-176	795	4.02	4.02	4.02	4.02	3	0.12	0.01	0.06	0.00	0.00	22.3
20	339	1071	-870	113	0	-91	905	4.02	4.02	4.02	4.02	3	0.13	0.03	0.15	0.00	0.00	22.3
37	339	1803	-1718	-79	0	27	998	4.02	4.02	4.02	4.02	3	0.15	0.05	0.31	0.00	0.00	22.3
38	339	196	56	304	0	-203	832	4.02	4.02	4.02	4.02	3	0.12	0.01	0.05	0.00	0.00	22.3
39	339	822	-788	75	0	-63	894	4.02	4.02	4.02	4.02	3	0.13	0.02	0.14	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	396	634	-973	65	0	-88	550	4.02	4.02	4.02	4.02	3	0.08	0.03	0.17	0.00	0.00	22.3
2	396	613	-912	8	0	-17	-577	4.02	4.02	4.02	4.02	2	0.09	0.03	0.16	0.00	0.00	22.3
3	396	620	-913	8	0	-17	-578	4.02	4.02	4.02	4.02	2	0.09	0.03	0.16	0.00	0.00	22.3

4	396	355	-583	92	0	-118	500	4.02	4.02	4.02	4.02	2	0.08	0.02	0.10	0.00	0.00	22.3
5	396	362	-584	93	0	-119	499	4.02	4.02	4.02	4.02	2	0.08	0.02	0.10	0.00	0.00	22.3
6	396	515	-796	36	0	-51	-404	4.02	4.02	4.02	4.02	2	0.06	0.02	0.14	0.00	0.00	22.3
7	396	538	-800	39	0	-54	-410	4.02	4.02	4.02	4.02	2	0.06	0.02	0.14	0.00	0.00	22.3
8	396	437	-697	62	0	-82	447	4.02	4.02	4.02	4.02	2	0.07	0.02	0.12	0.00	0.00	22.3
9	396	461	-701	64	0	-84	446	4.02	4.02	4.02	4.02	2	0.07	0.02	0.12	0.00	0.00	22.3
10	396	613	-912	8	0	-17	-577	4.02	4.02	4.02	4.02	2	0.09	0.03	0.16	0.00	0.00	22.3
11	396	620	-913	8	0	-17	-578	4.02	4.02	4.02	4.02	2	0.09	0.03	0.16	0.00	0.00	22.3
12	396	355	-583	92	0	-118	500	4.02	4.02	4.02	4.02	2	0.08	0.02	0.10	0.00	0.00	22.3
13	396	362	-584	93	0	-119	499	4.02	4.02	4.02	4.02	2	0.08	0.02	0.10	0.00	0.00	22.3
14	396	515	-796	36	0	-51	-404	4.02	4.02	4.02	4.02	2	0.06	0.02	0.14	0.00	0.00	22.3
15	396	538	-800	39	0	-54	-410	4.02	4.02	4.02	4.02	2	0.06	0.02	0.14	0.00	0.00	22.3
16	396	437	-697	62	0	-82	447	4.02	4.02	4.02	4.02	2	0.07	0.02	0.12	0.00	0.00	22.3
17	396	461	-701	64	0	-84	446	4.02	4.02	4.02	4.02	2	0.07	0.02	0.12	0.00	0.00	22.3
18	396	1659	-1704	20	0	-49	-1502	4.02	4.02	4.02	4.02	3	0.23	0.05	0.30	0.00	0.00	22.3
19	396	695	-638	250	0	-317	708	4.02	4.02	4.02	4.02	3	0.10	0.02	0.11	0.00	0.00	22.3
20	396	1071	-1146	113	0	-155	-684	4.02	4.02	4.02	4.02	3	0.10	0.03	0.20	0.00	0.00	22.3
37	396	1803	-1994	-79	0	71	-1930	4.02	4.02	4.02	4.02	3	0.29	0.06	0.36	0.00	0.00	22.3
38	396	196	-219	304	0	-375	832	4.02	4.02	4.02	4.02	3	0.12	0.01	0.05	0.00	0.00	22.3
39	396	822	-1064	75	0	-105	-567	4.02	4.02	4.02	4.02	3	0.08	0.03	0.19	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	452	634	-1248	65	0	-125	-1202	4.02	4.02	4.02	4.02	3	0.18	0.04	0.22	0.00	0.00	22.3
2	452	613	-1124	8	0	-21	-1259	4.02	4.02	4.02	4.02	2	0.19	0.03	0.20	0.00	0.00	22.3
3	452	620	-1125	8	0	-22	-1261	4.02	4.02	4.02	4.02	2	0.19	0.03	0.20	0.00	0.00	22.3
4	452	355	-795	92	0	-170	-588	4.02	4.02	4.02	4.02	2	0.09	0.02	0.14	0.00	0.00	22.3
5	452	362	-796	93	0	-172	-590	4.02	4.02	4.02	4.02	2	0.09	0.02	0.14	0.00	0.00	22.3
6	452	515	-1007	36	0	-72	-1021	4.02	4.02	4.02	4.02	2	0.16	0.03	0.18	0.00	0.00	22.3
7	452	538	-1012	39	0	-76	-1030	4.02	4.02	4.02	4.02	2	0.16	0.03	0.18	0.00	0.00	22.3
8	452	437	-909	62	0	-117	-820	4.02	4.02	4.02	4.02	2	0.13	0.03	0.16	0.00	0.00	22.3
9	452	461	-913	64	0	-121	-828	4.02	4.02	4.02	4.02	2	0.13	0.03	0.16	0.00	0.00	22.3
10	452	613	-1124	8	0	-21	-1259	4.02	4.02	4.02	4.02	2	0.19	0.03	0.20	0.00	0.00	22.3
11	452	620	-1125	8	0	-22	-1261	4.02	4.02	4.02	4.02	2	0.19	0.03	0.20	0.00	0.00	22.3
12	452	355	-795	92	0	-170	-588	4.02	4.02	4.02	4.02	2	0.09	0.02	0.14	0.00	0.00	22.3
13	452	362	-796	93	0	-172	-590	4.02	4.02	4.02	4.02	2	0.09	0.02	0.14	0.00	0.00	22.3
14	452	515	-1007	36	0	-72	-1021	4.02	4.02	4.02	4.02	2	0.16	0.03	0.18	0.00	0.00	22.3
15	452	538	-1012	39	0	-76	-1030	4.02	4.02	4.02	4.02	2	0.16	0.03	0.18	0.00	0.00	22.3
16	452	437	-909	62	0	-117	-820	4.02	4.02	4.02	4.02	2	0.13	0.03	0.16	0.00	0.00	22.3
17	452	461	-913	64	0	-121	-828	4.02	4.02	4.02	4.02	2	0.13	0.03	0.16	0.00	0.00	22.3
18	452	1659	-1979	20	0	-61	-2682	4.02	4.02	4.02	4.02	3	0.40	0.06	0.35	0.00	0.00	22.3
19	452	695	-914	250	0	-459	-517	4.02	4.02	4.02	4.02	3	0.11	0.03	0.16	0.00	0.00	22.3
20	452	1071	-1421	113	0	-219	-1549	4.02	4.02	4.02	4.02	3	0.23	0.04	0.25	0.00	0.00	22.3
37	452	1803	-2269	-79	0	116	-3274	4.02	4.02	4.02	4.02	3	0.50	0.07	0.40	0.00	0.00	22.3
38	452	196	-495	304	0	-547	832	4.02	4.02	4.02	4.02	3	0.14	0.01	0.09	0.00	0.00	22.3
39	452	822	-1339	75	0	-147	-1385	4.02	4.02	4.02	4.02	3	0.20	0.04	0.24	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	508	634	-1524	65	0	-162	-2124	4.02	4.02	4.02	4.02	3	0.31	0.04	0.27	0.00	0.00	22.3
2	508	613	-1336	8	0	-25	-2062	4.02	4.02	4.02	4.02	2	0.32	0.04	0.24	0.00	0.00	22.3
3	508	620	-1337	8	0	-27	-2064	4.02	4.02	4.02	4.02	2	0.32	0.04	0.24	0.00	0.00	22.3
4	508	355	-1007	92	0	-222	-1204	4.02	4.02	4.02	4.02	2	0.18	0.03	0.18	0.00	0.00	22.3
5	508	362	-1008	93	0	-224	-1207	4.02	4.02	4.02	4.02	2	0.18	0.03	0.18	0.00	0.00	22.3
6	508	515	-1219	36	0	-92	-1757	4.02	4.02	4.02	4.02	2	0.27	0.04	0.22	0.00	0.00	22.3
7	508	538	-1224	39	0	-98	-1768	4.02	4.02	4.02	4.02	2	0.27	0.04	0.22	0.00	0.00	22.3
8	508	437	-1121	62	0	-151	-1500	4.02	4.02	4.02	4.02	2	0.23	0.03	0.20	0.00	0.00	22.3
9	508	461	-1125	64	0	-157	-1511	4.02	4.02	4.02	4.02	2	0.23	0.03	0.20	0.00	0.00	22.3
10	508	613	-1336	8	0	-25	-2062	4.02	4.02	4.02	4.02	2	0.32	0.04	0.24	0.00	0.00	22.3
11	508	620	-1337	8	0	-27	-2064	4.02	4.02	4.02	4.02	2	0.32	0.04	0.24	0.00	0.00	22.3
12	508	355	-1007	92	0	-222	-1204	4.02	4.02	4.02	4.02	2	0.18	0.03	0.18	0.00	0.00	22.3
13	508	362	-1008	93	0	-224	-1207	4.02	4.02	4.02	4.02	2	0.18	0.03	0.18	0.00	0.00	22.3
14	508	515	-1219	36	0	-92	-1757	4.02	4.02	4.02	4.02	2	0.27	0.04	0.22	0.00	0.00	22.3
15	508	538	-1224	39	0	-98	-1768	4.02	4.02	4.02	4.02	2	0.27	0.04	0.22	0.00	0.00	22.3
16	508	437	-1121	62	0	-151	-1500	4.02	4.02	4.02	4.02	2	0.23	0.03	0.20	0.00	0.00	22.3
17	508	461	-1125	64	0	-157	-1511	4.02	4.02	4.02	4.02	2	0.23	0.03	0.20	0.00	0.00	22.3
18	508	1659	-2255	20	0	-72	-4017	4.02	4.02	4.02	4.02	3	0.61	0.07	0.40	0.00	0.00	22.3
19	508	695	-1189	250	0	-600	-1250	4.02	4.02	4.02	4.02	3	0.18	0.03	0.21	0.00	0.00	22.3
20	508	1071	-1697	113	0	-283	-2569	4.02	4.02	4.02	4.02	3	0.38	0.05	0.30	0.00	0.00	22.3
37	508	1803	-2545	-79	0	161	-4774	4.02	4.02	4.02	4.02	3	0.72	0.07	0.45	0.00	0.00	22.3
38	508	196	-770	304	0	-719	617	4.02	4.02	4.02	4.02	3	0.18	0.02	0.14	0.00	0.00	22.3
39	508	822	-1615	75	0	-190	-2359	4.02	4.02	4.02	4.02	3	0.35	0.05	0.29	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	565	634	-1799	65	0	-199	-2292	4.02	4.02	4.02	4.02	3	0.33	0.05	0.32	0.00	0.00	22.3
2	565	613	-1548	8	0	-29	-2200	4.02	4.02	4.02	4.02	2	0.34	0.04	0.28	0.00	0.00	22.3
3	565	620	-1549	8	0	-32	-2203	4.02	4.02	4.02	4.02	2	0.34	0.04	0.28	0.00	0.00	22.3
4	565	355	-1219	92	0	-275	-1323	4.02	4.02	4.02	4.02	2	0.20	0.04	0.22	0.00	0.00	22.3
5	565	362	-1220	93	0	-277	-1326	4.02	4.02	4.02	4.02	2	0.20	0.04	0.22	0.00	0.00	22.3
6	565	515	-1431	36	0	-113	-1889	4.02	4.02	4.02	4.02	2	0.29	0.04	0.25	0.00	0.00	22.3
7	565	538	-1436	39	0	-120	-1900	4.02	4.02	4.02	4.02	2	0.29	0.04	0.26	0.00	0.00	22.3
8	565	437	-1333	62	0	-186	-1626	4.02	4.02	4.02	4.02	2	0.25	0.04	0.24	0.00	0.00	22.3
9	565	461	-1337	64	0	-193	-1637	4.02	4.02	4.02	4.02	2	0.25	0.04	0.24	0.00	0.00	22.3
10	565	613	-1548	8	0	-29	-2200	4.02	4.02	4.02	4.02	2	0.34	0.04	0.28	0.00	0.00	22.3
11	565	620	-1549	8	0	-32	-2203	4.02	4.02	4.02	4.02	2	0.34	0.04	0.28	0.00	0.00	22.3
12	565	355	-1219	92	0	-275	-1323	4.02	4.02	4.02	4.02	2	0.20	0.04	0.22	0.00	0.00	22.3
13	565	362	-1220	93	0	-277	-1326	4.02	4.02	4.02	4.02	2	0.20	0.04	0.22	0.00	0.00	22.3
14	565	515	-1431	36	0	-113	-1889	4.02	4.02	4.02	4.02	2	0.29	0.04	0.25	0.00	0.00	22.3
15	565	538	-1436	39	0	-120	-1900	4.02	4.02	4.02	4.02	2	0.29	0.04	0.26	0.00	0.00	22.3
16	565	437	-1333	62	0	-186	-1626	4.02	4.02	4.02	4.02	2	0.25	0.04	0.24	0.00	0.00	22.3
17	565	461	-1337	64	0	-193	-1637	4.02	4.02	4.02	4.02	2	0.25	0.04	0.24	0.00	0.00	22.3
18	565	1659	-2530	20	0	-84	-4227	4.02	4.02	4.02	4.02	3	0.64	0.07	0.45	0.00	0.00	22.3
19	565	695	-1465	250	0	-741	-1398	4.02	4.02	4.02	4.02	3	0.20	0.04	0.26	0.00	0.00	22.3
20	565	1071	-1972	113	0	-346	-2746	4.02	4.02	4.02	4.02	3	0.41	0.06	0.35	0.00	0.00	22.3
37	565	1803	-2820	-79	0	206	-5001	4.02	4.02	4.02	4.02	3	0.76	0.08	0.50	0.00	0.00	22.3
38	565	196	-1046	304	0	-890	-286	4.02	4.02	4.02	4.02	3	0.22	0.03	0.19	0.00	0.00	22.3
39	565	822	-1890	75	0	-232	-2532	4.02	4.02	4.02	4.02	3	0.37	0.05	0.34	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

Nome travata: **trave_501_IP1** Descrizione: **Trave_5 11-16-21-26**
ASTA NUM. 2 NI 171 NF 185 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y qy tot.
qy medio: 375.00 375.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

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NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	1917	1111	108	0	313	-611	4.02	4.02	4.02	4.02	3	0.09	0.03	0.20	0.00	0.00	22.3
2	0	1722	703	34	0	104	-45	4.02	4.02	4.02	4.02	2	0.03	0.02	0.13	0.00	0.00	22.3
3	0	1736	704	35	0	109	-46	4.02	4.02	4.02	4.02	2	0.03	0.02	0.13	0.00	0.00	22.3
4	0	1213	1006	131	0	373	-895	4.02	4.02	4.02	4.02	2	0.14	0.03	0.18	0.00	0.00	22.3
5	0	1227	1006	132	0	378	-896	4.02	4.02	4.02	4.02	2	0.14	0.03	0.18	0.00	0.00	22.3
6	0	1526	809	66	0	193	-341	4.02	4.02	4.02	4.02	2	0.06	0.02	0.14	0.00	0.00	22.3
7	0	1575	810	71	0	209	-344	4.02	4.02	4.02	4.02	2	0.06	0.02	0.14	0.00	0.00	22.3
8	0	1374	900	95	0	274	-596	4.02	4.02	4.02	4.02	2	0.09	0.03	0.16	0.00	0.00	22.3
9	0	1423	901	100	0	289	-599	4.02	4.02	4.02	4.02	2	0.09	0.03	0.16	0.00	0.00	22.3
10	0	1722	703	34	0	104	-45	4.02	4.02	4.02	4.02	2	0.03	0.02	0.13	0.00	0.00	22.3
11	0	1736	704	35	0	109	-46	4.02	4.02	4.02	4.02	2	0.03	0.02	0.13	0.00	0.00	22.3
12	0	1213	1006	131	0	373	-895	4.02	4.02	4.02	4.02	2	0.14	0.03	0.18	0.00	0.00	22.3
13	0	1227	1006	132	0	378	-896	4.02	4.02	4.02	4.02	2	0.14	0.03	0.18	0.00	0.00	22.3
14	0	1526	809	66	0	193	-341	4.02	4.02	4.02	4.02	2	0.06	0.02	0.14	0.00	0.00	22.3
15	0	1575	810	71	0	209	-344	4.02	4.02	4.02	4.02	2	0.06	0.02	0.14	0.00	0.00	22.3
16	0	1374	900	95	0	274	-596	4.02	4.02	4.02	4.02	2	0.09	0.03	0.16	0.00	0.00	22.3
17	0	1423	901	100	0	289	-599	4.02	4.02	4.02	4.02	2	0.09	0.03	0.16	0.00	0.00	22.3
18	0	4601	421	90	0	280	1486	4.02	4.02	4.02	4.02	3	0.25	0.01	0.07	0.00	0.00	22.3
19	0	2462	1405	349	0	991	-1442	4.02	4.02	4.02	4.02	3	0.26	0.04	0.25	0.00	0.00	22.3
20	0	3277	942	214	0	624	-139	4.02	4.02	4.02	4.02	3	0.17	0.03	0.17	0.00	0.00	22.3
37	0	4786	158	-33	0	-62	2072	4.02	4.02	4.02	4.02	3	0.35	0.00	0.03	0.00	0.00	22.3
38	0	1221	1799	399	0	1122	-2544	4.02	4.02	4.02	4.02	3	0.38	0.05	0.32	0.00	0.00	22.3
39	0	2579	1026	173	0	511	-373	4.02	4.02	4.02	4.02	3	0.13	0.03	0.18	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	57	1917	836	108	0	252	-484	4.02	4.02	4.02	4.02	3	0.07	0.02	0.15	0.00	0.00	22.3
2	57	1722	491	34	0	85	541	4.02	4.02	4.02	4.02	2	0.09	0.01	0.09	0.00	0.00	22.3
3	57	1736	492	35	0	89	541	4.02	4.02	4.02	4.02	2	0.09	0.01	0.09	0.00	0.00	22.3
4	57	1213	794	131	0	299	-788	4.02	4.02	4.02	4.02	2	0.12	0.02	0.14	0.00	0.00	22.3
5	57	1227	794	132	0	303	-789	4.02	4.02	4.02	4.02	2	0.12	0.02	0.14	0.00	0.00	22.3
6	57	1526	597	66	0	155	358	4.02	4.02	4.02	4.02	2	0.06	0.02	0.11	0.00	0.00	22.3
7	57	1575	598	71	0	169	356	4.02	4.02	4.02	4.02	2	0.06	0.02	0.11	0.00	0.00	22.3
8	57	1374	688	95	0	220	-496	4.02	4.02	4.02	4.02	2	0.08	0.02	0.12	0.00	0.00	22.3
9	57	1423	689	100	0	233	-499	4.02	4.02	4.02	4.02	2	0.08	0.02	0.12	0.00	0.00	22.3
10	57	1722	491	34	0	85	541	4.02	4.02	4.02	4.02	2	0.09	0.01	0.09	0.00	0.00	22.3
11	57	1736	492	35	0	89	541	4.02	4.02	4.02	4.02	2	0.09	0.01	0.09	0.00	0.00	22.3
12	57	1213	794	131	0	299	-788	4.02	4.02	4.02	4.02	2	0.12	0.02	0.14	0.00	0.00	22.3
13	57	1227	794	132	0	303	-789	4.02	4.02	4.02	4.02	2	0.12	0.02	0.14	0.00	0.00	22.3
14	57	1526	597	66	0	155	358	4.02	4.02	4.02	4.02	2	0.06	0.02	0.11	0.00	0.00	22.3
15	57	1575	598	71	0	169	356	4.02	4.02	4.02	4.02	2	0.06	0.02	0.11	0.00	0.00	22.3
16	57	1374	688	95	0	220	-496	4.02	4.02	4.02	4.02	2	0.08	0.02	0.12	0.00	0.00	22.3
17	57	1423	689	100	0	233	-499	4.02	4.02	4.02	4.02	2	0.08	0.02	0.12	0.00	0.00	22.3
18	57	4601	145	90	0	230	1486	4.02	4.02	4.02	4.02	3	0.25	0.00	0.03	0.00	0.00	22.3
19	57	2462	1130	349	0	794	-1298	4.02	4.02	4.02	4.02	3	0.21	0.03	0.20	0.00	0.00	22.3
20	57	3277	666	214	0	503	652	4.02	4.02	4.02	4.02	3	0.14	0.02	0.12	0.00	0.00	22.3
37	57	4786	-118	-33	0	-43	2072	4.02	4.02	4.02	4.02	3	0.35	0.00	0.02	0.00	0.00	22.3
38	57	1221	1524	399	0	897	-2377	4.02	4.02	4.02	4.02	3	0.35	0.04	0.27	0.00	0.00	22.3
39	57	2579	750	173	0	413	509	4.02	4.02	4.02	4.02	3	0.11	0.02	0.13	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	113	1917	560	108	0	191	617	4.02	4.02	4.02	4.02	3	0.09	0.02	0.10	0.00	0.00	22.3
2	113	1722	279	34	0	66	608	4.02	4.02	4.02	4.02	2	0.10	0.01	0.05	0.00	0.00	22.3
3	113	1736	280	35	0	69	608	4.02	4.02	4.02	4.02	2	0.10	0.01	0.05	0.00	0.00	22.3
4	113	1213	582	131	0	225	297	4.02	4.02	4.02	4.02	2	0.06	0.02	0.10	0.00	0.00	22.3
5	113	1227	582	132	0	229	297	4.02	4.02	4.02	4.02	2	0.07	0.02	0.10	0.00	0.00	22.3
6	113	1526	385	66	0	118	528	4.02	4.02	4.02	4.02	2	0.08	0.01	0.07	0.00	0.00	22.3
7	113	1575	386	71	0	129	527	4.02	4.02	4.02	4.02	2	0.08	0.01	0.07	0.00	0.00	22.3
8	113	1374	476	95	0	166	422	4.02	4.02	4.02	4.02	2	0.07	0.01	0.08	0.00	0.00	22.3
9	113	1423	477	100	0	177	421	4.02	4.02	4.02	4.02	2	0.07	0.01	0.08	0.00	0.00	22.3
10	113	1722	279	34	0	66	608	4.02	4.02	4.02	4.02	2	0.10	0.01	0.05	0.00	0.00	22.3
11	113	1736	280	35	0	69	608	4.02	4.02	4.02	4.02	2	0.10	0.01	0.05	0.00	0.00	22.3
12	113	1213	582	131	0	225	297	4.02	4.02	4.02	4.02	2	0.06	0.02	0.10	0.00	0.00	22.3
13	113	1227	582	132	0	229	297	4.02	4.02	4.02	4.02	2	0.07	0.02	0.10	0.00	0.00	22.3
14	113	1526	385	66	0	118	528	4.02	4.02	4.02	4.02	2	0.08	0.01	0.07	0.00	0.00	22.3
15	113	1575	386	71	0	129	527	4.02	4.02	4.02	4.02	2	0.08	0.01	0.07	0.00	0.00	22.3
16	113	1374	476	95	0	166	422	4.02	4.02	4.02	4.02	2	0.07	0.01	0.08	0.00	0.00	22.3
17	113	1423	477	100	0	177	421	4.02	4.02	4.02	4.02	2	0.07	0.01	0.08	0.00	0.00	22.3
18	113	4601	-130	90	0	179	1486	4.02	4.02	4.02	4.02	3	0.25	0.00	0.02	0.00	0.00	22.3
19	113	2462	854	349	0	596	-598	4.02	4.02	4.02	4.02	3	0.16	0.02	0.15	0.00	0.00	22.3
20	113	3277	391	214	0	382	757	4.02	4.02	4.02	4.02	3	0.12	0.01	0.07	0.00	0.00	22.3
37	113	4786	-393	-33	0	-24	2072	4.02	4.02	4.02	4.02	3	0.35	0.01	0.07	0.00	0.00	22.3
38	113	1221	1248	399	0	671	-1455	4.02	4.02	4.02	4.02	3	0.22	0.04	0.22	0.00	0.00	22.3
39	113	2579	475	173	0	315	701	4.02	4.02	4.02	4.02	3	0.11	0.01	0.08	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	170	1917	285	108	0	131	655	4.02	4.02	4.02	4.02	3	0.10	0.01	0.05	0.00	0.00	22.3
2	170	1722	67	34	0	47	608	4.02	4.02	4.02	4.02	2	0.10	0.00	0.01	0.00	0.00	22.3
3	170	1736	68	35	0	49	608	4.02	4.02	4.02	4.02	2	0.10	0.00	0.01	0.00	0.00	22.3
4	170	1213	370	131	0	151	451	4.02	4.02	4.02	4.02	2	0.07	0.01	0.07	0.00	0.00	22.3
5	170	1227	370	132	0	154	451	4.02	4.02	4.02	4.02	2	0.07	0.01	0.07	0.00	0.00	22.3
6	170	1526	173	66	0	80	529	4.02	4.02	4.02	4.02	2	0.08	0.01	0.03	0.00	0.00	22.3
7	170	1575	174	71	0	89	529	4.02	4.02	4.02	4.02	2	0.08	0.01	0.03	0.00	0.00	22.3
8	170	1374	264	95	0	112	479	4.02	4.02	4.02	4.02	2	0.08	0.01	0.05	0.00	0.00	22.3
9	170	1423	265	100	0	120	479	4.02	4.02	4.02	4.02	2	0.08	0.01	0.05	0.00	0.00	22.3
10	170	1722	67	34	0	47	608	4.02	4.02	4.02	4.02	2	0.10	0.00	0.01	0.00	0.00	22.3
11	170	1736	68	35	0	49	608	4.02	4.02	4.02	4.02	2	0.10	0.00	0.01	0.00	0.00	22.3
12	170	1213	370	131	0	151	451	4.02	4.02	4.02	4.02	2	0.07	0.01	0.07	0.00	0.00	22.3
13	170	1227	370	132	0	154	451	4.02	4.02	4.02	4.02	2	0.07	0.01	0.07	0.00	0.00	22.3
14	170	1526	173	66	0	80	529	4.02	4.02	4.02	4.02	2	0.08	0.01	0.03	0.00	0.00	22.3
15	170	1575	174	71	0	89	529	4.02	4.02	4.02	4.02	2	0.08	0.01	0.03	0.00	0.00	22.3
16	170	1374	264	95	0	112	479	4.02	4.02	4.02	4.02	2	0.08	0.01	0.05	0.00	0.00	22.3
17	170	1423	265	100	0	120	479	4.02	4.02	4.02	4.02	2	0.08	0.01	0.05	0.00	0.00	22.3
18	170	4601	-406	90	0	128	1486	4.02	4.02	4.02	4.02	3	0.25	0.01	0.07	0.00	0.00	22.3
19	170	2462	579	349	0	399	533	4.02	4.02	4.02	4.02	3	0.10	0.02	0.10	0.00	0.00	22.3
20	170	3277	115	214	0	262	757	4.02	4.02	4.02	4.02	3	0.12	0.01	0.03	0.00	0.00	22.3
37	170	4786	-669	-33	0	-6	1966	4.02	4.02	4.02	4.02	3	0.33	0.02	0.12	0.00	0.00	22.3
38	170	1221	973	399	0	446	-688	4.02	4.02	4.02	4.02	3	0.11	0.03	0.17	0.00	0.00	22.3
39	170	2579	199	173	0	217	701	4.02	4.02	4.02	4.02	3	0.11	0.01	0.04	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	226	1917	9	108	0	70	655	4.02	4.02	4.02	4.02	3	0.10	0.00	0.00	0.00	0.00	22.3

2	226	1722	-144	34	0	28	608	4.02	4.02	4.02	4.02	2	0.10	0.00	0.03	0.00	0.00	22.3
3	226	1736	-144	35	0	30	608	4.02	4.02	4.02	4.02	2	0.10	0.00	0.03	0.00	0.00	22.3
4	226	1213	158	131	0	78	451	4.02	4.02	4.02	4.02	2	0.07	0.00	0.03	0.00	0.00	22.3
5	226	1227	158	132	0	79	451	4.02	4.02	4.02	4.02	2	0.07	0.00	0.03	0.00	0.00	22.3
6	226	1526	-39	66	0	43	529	4.02	4.02	4.02	4.02	2	0.08	0.00	0.01	0.00	0.00	22.3
7	226	1575	-38	71	0	49	529	4.02	4.02	4.02	4.02	2	0.08	0.00	0.01	0.00	0.00	22.3
8	226	1374	52	95	0	58	479	4.02	4.02	4.02	4.02	2	0.08	0.00	0.01	0.00	0.00	22.3
9	226	1423	53	100	0	64	479	4.02	4.02	4.02	4.02	2	0.08	0.00	0.01	0.00	0.00	22.3
10	226	1722	-144	34	0	28	608	4.02	4.02	4.02	4.02	2	0.10	0.00	0.03	0.00	0.00	22.3
11	226	1736	-144	35	0	30	608	4.02	4.02	4.02	4.02	2	0.10	0.00	0.03	0.00	0.00	22.3
12	226	1213	158	131	0	78	451	4.02	4.02	4.02	4.02	2	0.07	0.00	0.03	0.00	0.00	22.3
13	226	1227	158	132	0	79	451	4.02	4.02	4.02	4.02	2	0.07	0.00	0.03	0.00	0.00	22.3
14	226	1526	-39	66	0	43	529	4.02	4.02	4.02	4.02	2	0.08	0.00	0.01	0.00	0.00	22.3
15	226	1575	-38	71	0	49	529	4.02	4.02	4.02	4.02	2	0.08	0.00	0.01	0.00	0.00	22.3
16	226	1374	52	95	0	58	479	4.02	4.02	4.02	4.02	2	0.08	0.00	0.01	0.00	0.00	22.3
17	226	1423	53	100	0	64	479	4.02	4.02	4.02	4.02	2	0.08	0.00	0.01	0.00	0.00	22.3
18	226	4601	-681	90	0	77	1372	4.02	4.02	4.02	4.02	3	0.23	0.02	0.12	0.00	0.00	22.3
19	226	2462	303	349	0	202	583	4.02	4.02	4.02	4.02	3	0.09	0.01	0.06	0.00	0.00	22.3
20	226	3277	-160	214	0	141	757	4.02	4.02	4.02	4.02	3	0.12	0.01	0.03	0.00	0.00	22.3
37	226	4786	-944	-33	0	13	1650	4.02	4.02	4.02	4.02	3	0.28	0.03	0.17	0.00	0.00	22.3
38	226	1221	697	399	0	220	629	4.02	4.02	4.02	4.02	3	0.09	0.02	0.12	0.00	0.00	22.3
39	226	2579	-76	173	0	120	701	4.02	4.02	4.02	4.02	3	0.11	0.01	0.03	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	283	1917	-266	108	0	9	655	4.02	4.02	4.02	4.02	3	0.10	0.01	0.05	0.00	0.00	22.3
2	283	1722	-356	34	0	8	608	4.02	4.02	4.02	4.02	2	0.10	0.01	0.06	0.00	0.00	22.3
3	283	1736	-356	35	0	10	608	4.02	4.02	4.02	4.02	2	0.10	0.01	0.06	0.00	0.00	22.3
4	283	1213	-54	131	0	4	451	4.02	4.02	4.02	4.02	2	0.07	0.00	0.01	0.00	0.00	22.3
5	283	1227	-54	132	0	5	451	4.02	4.02	4.02	4.02	2	0.07	0.00	0.01	0.00	0.00	22.3
6	283	1526	-251	66	0	5	529	4.02	4.02	4.02	4.02	2	0.08	0.01	0.04	0.00	0.00	22.3
7	283	1575	-250	71	0	9	529	4.02	4.02	4.02	4.02	2	0.08	0.01	0.04	0.00	0.00	22.3
8	283	1374	-160	95	0	4	479	4.02	4.02	4.02	4.02	2	0.08	0.00	0.03	0.00	0.00	22.3
9	283	1423	-159	100	0	8	479	4.02	4.02	4.02	4.02	2	0.08	0.00	0.03	0.00	0.00	22.3
10	283	1722	-356	34	0	8	608	4.02	4.02	4.02	4.02	2	0.10	0.01	0.06	0.00	0.00	22.3
11	283	1736	-356	35	0	10	608	4.02	4.02	4.02	4.02	2	0.10	0.01	0.06	0.00	0.00	22.3
12	283	1213	-54	131	0	4	451	4.02	4.02	4.02	4.02	2	0.07	0.00	0.01	0.00	0.00	22.3
13	283	1227	-54	132	0	5	451	4.02	4.02	4.02	4.02	2	0.07	0.00	0.01	0.00	0.00	22.3
14	283	1526	-251	66	0	5	529	4.02	4.02	4.02	4.02	2	0.08	0.01	0.04	0.00	0.00	22.3
15	283	1575	-250	71	0	9	529	4.02	4.02	4.02	4.02	2	0.08	0.01	0.04	0.00	0.00	22.3
16	283	1374	-160	95	0	4	479	4.02	4.02	4.02	4.02	2	0.08	0.00	0.03	0.00	0.00	22.3
17	283	1423	-159	100	0	8	479	4.02	4.02	4.02	4.02	2	0.08	0.00	0.03	0.00	0.00	22.3
18	283	4601	-957	90	0	26	1049	4.02	4.02	4.02	4.02	3	0.17	0.03	0.17	0.00	0.00	22.3
19	283	2462	28	349	0	4	583	4.02	4.02	4.02	4.02	3	0.09	0.01	0.06	0.00	0.00	22.3
20	283	3277	-436	214	0	21	757	4.02	4.02	4.02	4.02	3	0.12	0.01	0.08	0.00	0.00	22.3
37	283	4786	-1220	-33	0	31	1178	4.02	4.02	4.02	4.02	3	0.20	0.04	0.22	0.00	0.00	22.3
38	283	1221	422	399	0	-5	757	4.02	4.02	4.02	4.02	3	0.11	0.01	0.08	0.00	0.00	22.3
39	283	2579	-352	173	0	22	701	4.02	4.02	4.02	4.02	3	0.11	0.01	0.06	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	339	1917	-541	108	0	-52	629	4.02	4.02	4.02	4.02	3	0.10	0.02	0.10	0.00	0.00	22.3
2	339	1722	-568	34	0	-11	472	4.02	4.02	4.02	4.02	2	0.08	0.02	0.10	0.00	0.00	22.3
3	339	1736	-568	35	0	-10	472	4.02	4.02	4.02	4.02	2	0.08	0.02	0.10	0.00	0.00	22.3
4	339	1213	-265	131	0	-70	451	4.02	4.02	4.02	4.02	2	0.07	0.01	0.05	0.00	0.00	22.3
5	339	1227	-265	132	0	-70	451	4.02	4.02	4.02	4.02	2	0.07	0.01	0.05	0.00	0.00	22.3
6	339	1526	-463	66	0	-32	480	4.02	4.02	4.02	4.02	2	0.08	0.01	0.08	0.00	0.00	22.3
7	339	1575	-461	71	0	-30	481	4.02	4.02	4.02	4.02	2	0.08	0.01	0.08	0.00	0.00	22.3
8	339	1374	-372	95	0	-50	479	4.02	4.02	4.02	4.02	2	0.08	0.01	0.07	0.00	0.00	22.3
9	339	1423	-370	100	0	-48	479	4.02	4.02	4.02	4.02	2	0.08	0.01	0.07	0.00	0.00	22.3
10	339	1722	-568	34	0	-11	472	4.02	4.02	4.02	4.02	2	0.08	0.02	0.10	0.00	0.00	22.3
11	339	1736	-568	35	0	-10	472	4.02	4.02	4.02	4.02	2	0.08	0.02	0.10	0.00	0.00	22.3
12	339	1213	-265	131	0	-70	451	4.02	4.02	4.02	4.02	2	0.07	0.01	0.05	0.00	0.00	22.3
13	339	1227	-265	132	0	-70	451	4.02	4.02	4.02	4.02	2	0.07	0.01	0.05	0.00	0.00	22.3
14	339	1526	-463	66	0	-32	480	4.02	4.02	4.02	4.02	2	0.08	0.01	0.08	0.00	0.00	22.3
15	339	1575	-461	71	0	-30	481	4.02	4.02	4.02	4.02	2	0.08	0.01	0.08	0.00	0.00	22.3
16	339	1374	-372	95	0	-50	479	4.02	4.02	4.02	4.02	2	0.08	0.01	0.07	0.00	0.00	22.3
17	339	1423	-370	100	0	-48	479	4.02	4.02	4.02	4.02	2	0.08	0.01	0.07	0.00	0.00	22.3
18	339	4601	-1232	90	0	-25	-677	4.02	4.02	4.02	4.02	3	0.11	0.04	0.22	0.00	0.00	22.3
19	339	2462	-247	349	0	-193	583	4.02	4.02	4.02	4.02	3	0.09	0.01	0.06	0.00	0.00	22.3
20	339	3277	-711	214	0	-100	612	4.02	4.02	4.02	4.02	3	0.10	0.02	0.13	0.00	0.00	22.3
37	339	4786	-1495	-33	0	50	-963	4.02	4.02	4.02	4.02	3	0.16	0.04	0.27	0.00	0.00	22.3
38	339	1221	146	399	0	-230	757	4.02	4.02	4.02	4.02	3	0.11	0.01	0.06	0.00	0.00	22.3
39	339	2579	-627	173	0	-76	621	4.02	4.02	4.02	4.02	3	0.10	0.02	0.11	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	396	1917	-817	108	0	-113	-443	4.02	4.02	4.02	4.02	3	0.07	0.02	0.15	0.00	0.00	22.3
2	396	1722	-780	34	0	-30	-591	4.02	4.02	4.02	4.02	2	0.09	0.02	0.14	0.00	0.00	22.3
3	396	1736	-779	35	0	-30	-591	4.02	4.02	4.02	4.02	2	0.09	0.02	0.14	0.00	0.00	22.3
4	396	1213	-477	131	0	-144	392	4.02	4.02	4.02	4.02	2	0.06	0.01	0.09	0.00	0.00	22.3
5	396	1227	-477	132	0	-144	393	4.02	4.02	4.02	4.02	2	0.06	0.01	0.09	0.00	0.00	22.3
6	396	1526	-674	66	0	-70	-417	4.02	4.02	4.02	4.02	2	0.07	0.02	0.12	0.00	0.00	22.3
7	396	1575	-673	71	0	-70	-414	4.02	4.02	4.02	4.02	2	0.07	0.02	0.12	0.00	0.00	22.3
8	396	1374	-583	95	0	-104	324	4.02	4.02	4.02	4.02	2	0.05	0.02	0.10	0.00	0.00	22.3
9	396	1423	-582	100	0	-105	326	4.02	4.02	4.02	4.02	2	0.05	0.02	0.10	0.00	0.00	22.3
10	396	1722	-780	34	0	-30	-591	4.02	4.02	4.02	4.02	2	0.09	0.02	0.14	0.00	0.00	22.3
11	396	1736	-779	35	0	-30	-591	4.02	4.02	4.02	4.02	2	0.09	0.02	0.14	0.00	0.00	22.3
12	396	1213	-477	131	0	-144	392	4.02	4.02	4.02	4.02	2	0.06	0.01	0.09	0.00	0.00	22.3
13	396	1227	-477	132	0	-144	393	4.02	4.02	4.02	4.02	2	0.06	0.01	0.09	0.00	0.00	22.3
14	396	1526	-674	66	0	-70	-417	4.02	4.02	4.02	4.02	2	0.07	0.02	0.12	0.00	0.00	22.3
15	396	1575	-673	71	0	-70	-414	4.02	4.02	4.02	4.02	2	0.07	0.02	0.12	0.00	0.00	22.3
16	396	1374	-583	95	0	-104	324	4.02	4.02	4.02	4.02	2	0.05	0.02	0.10	0.00	0.00	22.3
17	396	1423	-582	100	0	-105	326	4.02	4.02	4.02	4.02	2	0.05	0.02	0.10	0.00	0.00	22.3
18	396	4601	-1508	90	0	-75	-1591	4.02	4.02	4.02	4.02	3	0.26	0.04	0.27	0.00	0.00	22.3
19	396	2462	-523	349	0	-390	568	4.02	4.02	4.02	4.02	3	0.10	0.02	0.09	0.00	0.00	22.3
20	396	3277	-987	214	0	-221	-727	4.02	4.02	4.02	4.02	3	0.12	0.03	0.18	0.00	0.00	22.3
37	396	4786	-1771	-33	0	68	-2025	4.02	4.02	4.02	4.02	3	0.34	0.05	0.32	0.00	0.00	22.3
38	396	1221	-129	399	0	-456	757	4.02	4.02	4.02	4.02	3	0.12	0.01	0.06	0.00	0.00	22.3
39	396	2579	-902	173	0	-174	-585	4.02	4.02	4.02	4.02	3	0.09	0.03	0.16	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	452	1917	-1092	108	0	-174	-1121	4.02	4.02	4.02	4.02	3	0.17	0.03	0.19	0.00	0.00	22.3
2	452	1722	-992	34	0	-49	-1199	4.02	4.02	4.02	4.02	2	0.19	0.03	0.18	0.00	0.00	22.3
3	452	1736	-991	35	0	-50	-1198	4.02	4.02	4.02	4.02	2	0.19	0.03	0.18	0.00	0.00	22.3
4	452	1213	-689	131	0	-218	-528	4.02	4.02	4.02	4.02	2	0.08	0.02	0.12	0.00	0.00	22.3
5	452	1227	-689	132	0	-219	-527	4.02	4.02	4.02	4.02	2	0.08	0.02	0.12	0.00	0.00	22.3
6	452	1526	-886	66	0	-107	-965	4.02	4.02	4.02	4.02	2	0.15	0.03	0.16	0.00	0.00	22.3
7	452	1575	-885	71	0	-110	-962	4.02	4.02	4.02	4.02	2	0.15	0.03	0.16	0.00	0.00	22.3

8	452	1374	-795	95	0	-158	-763	4.02	4.02	4.02	4.02	2	0.12	0.02	0.14	0.00	0.00	22.3
9	452	1423	-794	100	0	-161	-760	4.02	4.02	4.02	4.02	2	0.12	0.02	0.14	0.00	0.00	22.3
10	452	1722	-992	34	0	-49	-1199	4.02	4.02	4.02	4.02	2	0.19	0.03	0.18	0.00	0.00	22.3
11	452	1736	-991	35	0	-50	-1198	4.02	4.02	4.02	4.02	2	0.19	0.03	0.18	0.00	0.00	22.3
12	452	1213	-689	131	0	-218	-528	4.02	4.02	4.02	4.02	2	0.08	0.02	0.12	0.00	0.00	22.3
13	452	1227	-689	132	0	-219	-527	4.02	4.02	4.02	4.02	2	0.08	0.02	0.12	0.00	0.00	22.3
14	452	1526	-886	66	0	-107	-965	4.02	4.02	4.02	4.02	2	0.15	0.03	0.16	0.00	0.00	22.3
15	452	1575	-885	71	0	-110	-962	4.02	4.02	4.02	4.02	2	0.15	0.03	0.16	0.00	0.00	22.3
16	452	1374	-795	95	0	-158	-763	4.02	4.02	4.02	4.02	2	0.12	0.02	0.14	0.00	0.00	22.3
17	452	1423	-794	100	0	-161	-760	4.02	4.02	4.02	4.02	2	0.12	0.02	0.14	0.00	0.00	22.3
18	452	4601	-1783	90	0	-126	-2660	4.02	4.02	4.02	4.02	3	0.44	0.05	0.32	0.00	0.00	22.3
19	452	2462	-798	349	0	-587	-474	4.02	4.02	4.02	4.02	3	0.15	0.02	0.14	0.00	0.00	22.3
20	452	3277	-1262	214	0	-341	-1502	4.02	4.02	4.02	4.02	3	0.24	0.04	0.22	0.00	0.00	22.3
37	452	4786	-2046	-33	0	87	-3243	4.02	4.02	4.02	4.02	3	0.54	0.06	0.36	0.00	0.00	22.3
38	452	1221	-405	399	0	-681	757	4.02	4.02	4.02	4.02	3	0.17	0.01	0.07	0.00	0.00	22.3
39	452	2579	-1178	173	0	-271	-1312	4.02	4.02	4.02	4.02	3	0.20	0.03	0.21	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	509	1917	-1368	108	0	-235	-1956	4.02	4.02	4.02	4.02	3	0.30	0.04	0.24	0.00	0.00	22.3
2	509	1722	-1204	34	0	-68	-1927	4.02	4.02	4.02	4.02	2	0.31	0.03	0.21	0.00	0.00	22.3
3	509	1736	-1203	35	0	-70	-1925	4.02	4.02	4.02	4.02	2	0.31	0.03	0.21	0.00	0.00	22.3
4	509	1213	-901	131	0	-292	-1084	4.02	4.02	4.02	4.02	2	0.17	0.03	0.16	0.00	0.00	22.3
5	509	1227	-901	132	0	-293	-1083	4.02	4.02	4.02	4.02	2	0.17	0.03	0.16	0.00	0.00	22.3
6	509	1526	-1098	66	0	-145	-1633	4.02	4.02	4.02	4.02	2	0.26	0.03	0.20	0.00	0.00	22.3
7	509	1575	-1097	71	0	-150	-1629	4.02	4.02	4.02	4.02	2	0.26	0.03	0.20	0.00	0.00	22.3
8	509	1374	-1007	95	0	-212	-1380	4.02	4.02	4.02	4.02	2	0.22	0.03	0.18	0.00	0.00	22.3
9	509	1423	-1006	100	0	-217	-1376	4.02	4.02	4.02	4.02	2	0.22	0.03	0.18	0.00	0.00	22.3
10	509	1722	-1204	34	0	-68	-1927	4.02	4.02	4.02	4.02	2	0.31	0.03	0.21	0.00	0.00	22.3
11	509	1736	-1203	35	0	-70	-1925	4.02	4.02	4.02	4.02	2	0.31	0.03	0.21	0.00	0.00	22.3
12	509	1213	-901	131	0	-292	-1084	4.02	4.02	4.02	4.02	2	0.17	0.03	0.16	0.00	0.00	22.3
13	509	1227	-901	132	0	-293	-1083	4.02	4.02	4.02	4.02	2	0.17	0.03	0.16	0.00	0.00	22.3
14	509	1526	-1098	66	0	-145	-1633	4.02	4.02	4.02	4.02	2	0.26	0.03	0.20	0.00	0.00	22.3
15	509	1575	-1097	71	0	-150	-1629	4.02	4.02	4.02	4.02	2	0.26	0.03	0.20	0.00	0.00	22.3
16	509	1374	-1007	95	0	-212	-1380	4.02	4.02	4.02	4.02	2	0.22	0.03	0.18	0.00	0.00	22.3
17	509	1423	-1006	100	0	-217	-1376	4.02	4.02	4.02	4.02	2	0.22	0.03	0.18	0.00	0.00	22.3
18	509	4601	-2059	90	0	-177	-3884	4.02	4.02	4.02	4.02	3	0.64	0.06	0.37	0.00	0.00	22.3
19	509	2462	-1074	349	0	-785	-1142	4.02	4.02	4.02	4.02	3	0.21	0.03	0.19	0.00	0.00	22.3
20	509	3277	-1538	214	0	-462	-2432	4.02	4.02	4.02	4.02	3	0.39	0.04	0.27	0.00	0.00	22.3
37	509	4786	-2322	-33	0	106	-4616	4.02	4.02	4.02	4.02	3	0.77	0.07	0.41	0.00	0.00	22.3
38	509	1221	-680	399	0	-907	644	4.02	4.02	4.02	4.02	3	0.23	0.02	0.12	0.00	0.00	22.3
39	509	2579	-1454	173	0	-369	-2195	4.02	4.02	4.02	4.02	3	0.34	0.04	0.26	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	565	1917	-1643	108	0	-296	-2114	4.02	4.02	4.02	4.02	3	0.32	0.05	0.29	0.00	0.00	22.3
2	565	1722	-1416	34	0	-88	-2057	4.02	4.02	4.02	4.02	2	0.33	0.04	0.25	0.00	0.00	22.3
3	565	1736	-1415	35	0	-90	-2056	4.02	4.02	4.02	4.02	2	0.33	0.04	0.25	0.00	0.00	22.3
4	565	1213	-1113	131	0	-365	-1197	4.02	4.02	4.02	4.02	2	0.19	0.03	0.20	0.00	0.00	22.3
5	565	1227	-1113	132	0	-368	-1196	4.02	4.02	4.02	4.02	2	0.19	0.03	0.20	0.00	0.00	22.3
6	565	1526	-1310	66	0	-182	-1757	4.02	4.02	4.02	4.02	2	0.28	0.04	0.23	0.00	0.00	22.3
7	565	1575	-1309	71	0	-190	-1753	4.02	4.02	4.02	4.02	2	0.28	0.04	0.23	0.00	0.00	22.3
8	565	1374	-1219	95	0	-266	-1499	4.02	4.02	4.02	4.02	2	0.24	0.04	0.22	0.00	0.00	22.3
9	565	1423	-1218	100	0	-273	-1495	4.02	4.02	4.02	4.02	2	0.24	0.04	0.22	0.00	0.00	22.3
10	565	1722	-1416	34	0	-88	-2057	4.02	4.02	4.02	4.02	2	0.33	0.04	0.25	0.00	0.00	22.3
11	565	1736	-1415	35	0	-90	-2056	4.02	4.02	4.02	4.02	2	0.33	0.04	0.25	0.00	0.00	22.3
12	565	1213	-1113	131	0	-365	-1197	4.02	4.02	4.02	4.02	2	0.19	0.03	0.20	0.00	0.00	22.3
13	565	1227	-1113	132	0	-368	-1196	4.02	4.02	4.02	4.02	2	0.19	0.03	0.20	0.00	0.00	22.3
14	565	1526	-1310	66	0	-182	-1757	4.02	4.02	4.02	4.02	2	0.28	0.04	0.23	0.00	0.00	22.3
15	565	1575	-1309	71	0	-190	-1753	4.02	4.02	4.02	4.02	2	0.28	0.04	0.23	0.00	0.00	22.3
16	565	1374	-1219	95	0	-266	-1499	4.02	4.02	4.02	4.02	2	0.24	0.04	0.22	0.00	0.00	22.3
17	565	1423	-1218	100	0	-273	-1495	4.02	4.02	4.02	4.02	2	0.24	0.04	0.22	0.00	0.00	22.3
18	565	4601	-2334	90	0	-228	-4083	4.02	4.02	4.02	4.02	3	0.68	0.07	0.42	0.00	0.00	22.3
19	565	2462	-1349	349	0	-982	-1283	4.02	4.02	4.02	4.02	3	0.26	0.04	0.24	0.00	0.00	22.3
20	565	3277	-1813	214	0	-583	-2600	4.02	4.02	4.02	4.02	3	0.41	0.05	0.32	0.00	0.00	22.3
37	565	4786	-2597	-33	0	124	-4830	4.02	4.02	4.02	4.02	3	0.81	0.08	0.46	0.00	0.00	22.3
38	565	1221	-956	399	0	-1132	-162	4.02	4.02	4.02	4.02	3	0.29	0.03	0.17	0.00	0.00	22.3
39	565	2579	-1729	173	0	-467	-2358	4.02	4.02	4.02	4.02	3	0.37	0.05	0.31	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

Nome travata: **trave_501_IP1** Descrizione: **Trave_5 11-16-21-26**
ASTA NUM. 3 NI 185 NF 167 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y qy tot.
qy medio: 375.00 375.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m			cmq				Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	3340	1281	326	0	657	-1011	4.02	4.02	4.02	4.02	3	0.18	0.04	0.23	0.00	0.00	22.3
2	0	2958	815	242	0	434	-337	4.02	4.02	4.02	4.02	2	0.13	0.02	0.15	0.00	0.00	22.3
3	0	2989	812	252	0	460	-329	4.02	4.02	4.02	4.02	2	0.14	0.02	0.14	0.00	0.00	22.3
4	0	2148	1159	249	0	550	-1227	4.02	4.02	4.02	4.02	2	0.20	0.03	0.21	0.00	0.00	22.3
5	0	2180	1155	259	0	576	-1219	4.02	4.02	4.02	4.02	2	0.20	0.03	0.21	0.00	0.00	22.3
6	0	2638	940	233	0	444	-658	4.02	4.02	4.02	4.02	2	0.13	0.03	0.17	0.00	0.00	22.3
7	0	2743	928	266	0	531	-631	4.02	4.02	4.02	4.02	2	0.16	0.03	0.17	0.00	0.00	22.3
8	0	2395	1043	235	0	479	-924	4.02	4.02	4.02	4.02	2	0.15	0.03	0.19	0.00	0.00	22.3
9	0	2500	1031	268	0	566	-898	4.02	4.02	4.02	4.02	2	0.17	0.03	0.18	0.00	0.00	22.3
10	0	2958	815	242	0	434	-337	4.02	4.02	4.02	4.02	2	0.13	0.02	0.15	0.00	0.00	22.3
11	0	2989	812	252	0	460	-329	4.02	4.02	4.02	4.02	2	0.14	0.02	0.14	0.00	0.00	22.3
12	0	2148	1159	249	0	550	-1227	4.02	4.02	4.02	4.02	2	0.20	0.03	0.21	0.00	0.00	22.3
13	0	2180	1155	259	0	576	-1219	4.02	4.02	4.02	4.02	2	0.20	0.03	0.21	0.00	0.00	22.3
14	0	2638	940	233	0	444	-658	4.02	4.02	4.02	4.02	2	0.13	0.03	0.17	0.00	0.00	22.3
15	0	2743	928	266	0	531	-631	4.02	4.02	4.02	4.02	2	0.16	0.03	0.17	0.00	0.00	22.3
16	0	2395	1043	235	0	479	-924	4.02	4.02	4.02	4.02	2	0.15	0.03	0.19	0.00	0.00	22.3
17	0	2500	1031	268	0	566	-898	4.02	4.02	4.02	4.02	2	0.17	0.03	0.18	0.00	0.00	22.3
18	0	8113	470	678	0	1225	1226	4.02	4.02	4.02	4.02	3	0.38	0.02	0.11	0.00	0.00	22.3
19	0	4623	1601	603	0	1387	-1914	4.02	4.02	4.02	4.02	3	0.39	0.05	0.29	0.00	0.00	22.3
20	0	6006	1065	647	0	1353	-522	4.02	4.02	4.02	4.02	3	0.40	0.03	0.19	0.00	0.00	22.3
37	0	8286	174	601	0	960	1815	4.02	4.02	4.02	4.02	3	0.34	0.02	0.10	0.00	0.00	22.3
38	0	2470	2059	475	0	1230	-3071	4.02	4.02	4.02	4.02	3	0.47	0.06	0.37	0.00	0.00	22.3
39	0	4775	1165	548	0	1172	-752	4.02	4.02	4.02	4.02	3	0.33	0.03	0.21	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	56	3340	1006	326	0	473	-874	4.02	4.02	4.02	4.02	3	0.14	0.03	0.18	0.00	0.00	22.3
2	56	2958	603	242	0	297	369	4.02	4.02	4.02	4.02	2	0.09	0.02	0.11	0.00	0.00	22.3
3	56	2989	600	252	0	318	373	4.02	4.02	4.02	4.02	2	0.10	0.02	0.11	0.00	0.00	22.3
4	56	2148	947	249	0	409	-1112	4.02	4.02	4.02	4.02	2	0.18	0.03	0.17	0.00	0.00	22.3
5	56	2180	943	259	0	430	-1104	4.02	4.02	4.02	4.02	2	0.18	0.03	0.17	0.00	0.00	22.3
6	56	2638	728	233	0	312	-555	4.02	4.02	4.02	4.02	2	0.09	0.02	0.13	0.00	0.00	22.3
7	56	2743	716	266	0	381	-529	4.02	4.02	4.02	4.02	2	0.12	0.02	0.13	0.00	0.00	22.3
8	56	2395	831	235	0	346	-816	4.02	4.02	4.02	4.02	2	0.13	0.02	0.15	0.00	0.00	22.3
9	56	2500	819	268	0	415	-790	4.02	4.02	4.02	4.02	2	0.13	0.02	0.15	0.00	0.00	22.3
10	56	2958	603	242	0	297	369	4.02	4.02	4.02	4.02	2	0.09	0.02	0.11	0.00	0.00	22.3
11	56	2989	600	252	0	318	373	4.02	4.02	4.02	4.02	2	0.10	0.02	0.11	0.00	0.00	22.3
12	56	2148	947	249	0	409	-1112	4.02	4.02	4.02	4.02	2	0.18	0.03	0.17	0.00	0.00	22.3
13	56	2180	943	259	0	430	-1104	4.02	4.02	4.02	4.02	2	0.18	0.03	0.17	0.00	0.00	22.3
14	56	2638	728	233	0	312	-555	4.02	4.02	4.02	4.02	2	0.09	0.02	0.13	0.00	0.00	22.3
15	56	2743	716	266	0	381	-529	4.02	4.02	4.02	4.02	2	0.12	0.02	0.13	0.00	0.00	22.3
16	56	2395	831	235	0	346	-816	4.02	4.02	4.02	4.02	2	0.13	0.02	0.15	0.00	0.00	22.3
17	56	2500	819	268	0	415	-790	4.02	4.02	4.02	4.02	2	0.13	0.02	0.15	0.00	0.00	22.3
18	56	8113	195	678	0	842	1226	4.02	4.02	4.02	4.02	3	0.26	0.02	0.11	0.00	0.00	22.3
19	56	4623	1326	603	0	1046	-1758	4.02	4.02	4.02	4.02	3	0.29	0.04	0.24	0.00	0.00	22.3
20	56	6006	790	647	0	988	401	4.02	4.02	4.02	4.02	3	0.29	0.02	0.14	0.00	0.00	22.3
37	56	8286	-101	601	0	620	1815	4.02	4.02	4.02	4.02	3	0.34	0.02	0.10	0.00	0.00	22.3
38	56	2470	1784	475	0	962	-2889	4.02	4.02	4.02	4.02	3	0.45	0.05	0.32	0.00	0.00	22.3
39	56	4775	890	548	0	862	-622	4.02	4.02	4.02	4.02	3	0.24	0.03	0.16	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	113	3340	730	326	0	288	494	4.02	4.02	4.02	4.02	3	0.08	0.02	0.13	0.00	0.00	22.3
2	113	2958	391	242	0	161	543	4.02	4.02	4.02	4.02	2	0.09	0.01	0.07	0.00	0.00	22.3
3	113	2989	388	252	0	176	545	4.02	4.02	4.02	4.02	2	0.09	0.01	0.07	0.00	0.00	22.3
4	113	2148	735	249	0	268	-529	4.02	4.02	4.02	4.02	2	0.09	0.02	0.13	0.00	0.00	22.3
5	113	2180	731	259	0	283	-523	4.02	4.02	4.02	4.02	2	0.08	0.02	0.13	0.00	0.00	22.3
6	113	2638	516	233	0	181	426	4.02	4.02	4.02	4.02	2	0.07	0.01	0.09	0.00	0.00	22.3
7	113	2743	504	266	0	231	433	4.02	4.02	4.02	4.02	2	0.07	0.01	0.09	0.00	0.00	22.3
8	113	2395	619	235	0	213	328	4.02	4.02	4.02	4.02	2	0.06	0.02	0.11	0.00	0.00	22.3
9	113	2500	607	268	0	263	335	4.02	4.02	4.02	4.02	2	0.08	0.02	0.11	0.00	0.00	22.3
10	113	2958	391	242	0	161	543	4.02	4.02	4.02	4.02	2	0.09	0.01	0.07	0.00	0.00	22.3
11	113	2989	388	252	0	176	545	4.02	4.02	4.02	4.02	2	0.09	0.01	0.07	0.00	0.00	22.3
12	113	2148	735	249	0	268	-529	4.02	4.02	4.02	4.02	2	0.09	0.02	0.13	0.00	0.00	22.3
13	113	2180	731	259	0	283	-523	4.02	4.02	4.02	4.02	2	0.08	0.02	0.13	0.00	0.00	22.3
14	113	2638	516	233	0	181	426	4.02	4.02	4.02	4.02	2	0.07	0.01	0.09	0.00	0.00	22.3
15	113	2743	504	266	0	231	433	4.02	4.02	4.02	4.02	2	0.07	0.01	0.09	0.00	0.00	22.3
16	113	2395	619	235	0	213	328	4.02	4.02	4.02	4.02	2	0.06	0.02	0.11	0.00	0.00	22.3
17	113	2500	607	268	0	263	335	4.02	4.02	4.02	4.02	2	0.08	0.02	0.11	0.00	0.00	22.3
18	113	8113	-81	678	0	458	1226	4.02	4.02	4.02	4.02	3	0.23	0.02	0.11	0.00	0.00	22.3
19	113	4623	1050	603	0	706	-948	4.02	4.02	4.02	4.02	3	0.20	0.03	0.19	0.00	0.00	22.3
20	113	6006	514	647	0	622	630	4.02	4.02	4.02	4.02	3	0.18	0.02	0.10	0.00	0.00	22.3
37	113	8286	-377	601	0	281	1815	4.02	4.02	4.02	4.02	3	0.34	0.02	0.10	0.00	0.00	22.3
38	113	2470	1508	475	0	693	-1819	4.02	4.02	4.02	4.02	3	0.28	0.04	0.27	0.00	0.00	22.3
39	113	4775	614	548	0	553	564	4.02	4.02	4.02	4.02	3	0.16	0.02	0.11	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	169	3340	455	326	0	104	661	4.02	4.02	4.02	4.02	3	0.11	0.01	0.08	0.00	0.00	22.3
2	169	2958	179	242	0	24	548	4.02	4.02	4.02	4.02	2	0.09	0.01	0.04	0.00	0.00	22.3
3	169	2989	176	252	0	33	547	4.02	4.02	4.02	4.02	2	0.09	0.01	0.04	0.00	0.00	22.3
4	169	2148	523	249	0	127	463	4.02	4.02	4.02	4.02	2	0.08	0.02	0.09	0.00	0.00	22.3
5	169	2180	519	259	0	137	463	4.02	4.02	4.02	4.02	2	0.08	0.02	0.09	0.00	0.00	22.3
6	169	2638	304	233	0	50	508	4.02	4.02	4.02	4.02	2	0.08	0.01	0.05	0.00	0.00	22.3
7	169	2743	292	266	0	80	508	4.02	4.02	4.02	4.02	2	0.08	0.01	0.05	0.00	0.00	22.3
8	169	2395	407	235	0	81	510	4.02	4.02	4.02	4.02	2	0.08	0.01	0.07	0.00	0.00	22.3
9	169	2500	395	268	0	111	510	4.02	4.02	4.02	4.02	2	0.08	0.01	0.07	0.00	0.00	22.3
10	169	2958	179	242	0	24	548	4.02	4.02	4.02	4.02	2	0.09	0.01	0.04	0.00	0.00	22.3
11	169	2989	176	252	0	33	547	4.02	4.02	4.02	4.02	2	0.09	0.01	0.04	0.00	0.00	22.3
12	169	2148	523	249	0	127	463	4.02	4.02	4.02	4.02	2	0.08	0.02	0.09	0.00	0.00	22.3
13	169	2180	519	259	0	137	463	4.02	4.02	4.02	4.02	2	0.08	0.02	0.09	0.00	0.00	22.3
14	169	2638	304	233	0	50	508	4.02	4.02	4.02	4.02	2	0.08	0.01	0.05	0.00	0.00	22.3
15	169	2743	292	266	0	80	508	4.02	4.02	4.02	4.02	2	0.08	0.01	0.05	0.00	0.00	22.3
16	169	2395	407	235	0	81	510	4.02	4.02	4.02	4.02	2	0.08	0.01	0.07	0.00	0.00	22.3
17	169	2500	395	268	0	111	510	4.02	4.02	4.02	4.02	2	0.08	0.01	0.07	0.00	0.00	22.3
18	169	8113	-356	678	0	75	1226	4.02	4.02	4.02	4.02	3	0.23	0.02	0.11	0.00	0.00	22.3
19	169	4623	775	603	0	365	492	4.02	4.02	4.02	4.02	3	0.10	0.02	0.14	0.00	0.00	22.3
20	169	6006	239	647	0	257	639	4.02	4.02	4.02	4.02	3	0.11	0.02	0.10	0.00	0.00	22.3
37	169	8286	-652	601	0	-59	1720	4.02	4.02	4.02	4.02	3	0.33	0.02	0.12	0.00	0.00	22.3
38	169	2470	1233	475	0	425	-906	4.02	4.02	4.02	4.02	3	0.14	0.04	0.22	0.00	0.00	22.3
39	169	4775	339	548	0	243	636	4.02	4.02	4.02	4.02	3	0.11	0.02	0.09	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	226	3340	179	326	0	-80	661	4.02	4.02	4.02	4.02	3	0.11	0.01	0.05	0.00	0.00	22.3
2	226	2958	-33	242	0	-112	548	4.02	4.02	4.02	4.02	2	0.09	0.01	0.04	0.00	0.00	22.3
3	226	2989	-36	252	0	-109	547	4.02	4.02	4.02	4.02	2	0.09	0.01	0.04	0.00	0.00	22.3
4	226	2148	311	249	0	-14	550	4.02	4.02	4.02	4.02	2	0.09	0.01	0.06	0.00	0.00	22.3
5	226	2180	308	259	0	-10	548	4.02	4.02	4.02	4.02	2	0.09	0.01	0.05	0.00	0.00	22.3
6	226	2638	92	233	0	-82	508	4.02	4.02	4.02	4.02	2	0.08	0.01	0.04	0.00	0.00	22.3
7	226	2743	80	266	0	-70	508	4.02	4.02	4.02	4.02	2	0.08	0.01	0.04	0.00	0.00	22.3
8	226	2395	195	235	0	-52	525	4.02	4.02	4.02	4.02	2	0.09	0.01	0.04	0.00	0.00	22.3
9	226	2500	183	268	0	-41	517	4.02	4.02	4.02	4.02	2	0.08	0.01	0.04	0.00	0.00	22.3
10	226	2958	-33	242	0	-112	548	4.02	4.02	4.02	4.02	2	0.09	0.01	0.04	0.00	0.00	22.3
11	226	2989	-36	252	0	-109	547	4.02	4.02	4.02	4.02	2	0.09	0.01	0.04	0.00	0.00	22.3
12	226	2148	311	249	0	-14	550	4.02	4.02	4.02	4.02	2	0.09	0.01	0.06	0.00	0.00	22.3
13	226	2180	308	259	0	-10	548	4.02	4.02	4.02	4.02	2	0.09	0.01	0.05	0.00	0.00	22.3
14	226	2638	92	233	0	-82	508	4.02	4.02	4.02	4.02	2	0.08	0.01	0.04	0.00	0.00	22.3
15	226	2743	80	266	0	-70	508	4.02	4.02	4.02	4.02	2	0.08	0.01	0.04	0.00	0.00	22.3
16	226	2395	195	235	0	-52	525	4.02	4.02	4.02	4.02	2	0.09	0.01	0.04	0.00	0.00	22.3
17	226	2500	183	268	0	-41	517	4.02	4.02	4.02	4.02	2	0.08	0.01	0.04	0.00	0.00	22.3
18	226	8113	-632	678	0	-308	1143	4.02	4.02	4.02	4.02	3	0.22	0.02	0.11	0.00	0.00	22.3
19	226	4623	499	603	0	25	712	4.02	4.02	4.02	4.02	3	0.12	0.02	0.10	0.00	0.00	22.3
20	226	6006	-37	647	0	-109	639	4.02	4.02	4.02	4.02	3	0.11	0.02	0.10	0.00	0.00	22.3
37	226	8286	-928	601	0	-399	1413	4.02	4.02	4.02	4.02	3	0.27	0.03	0.17	0.00	0.00	22.3
38	226	2470	957	475	0	156	821	4.02	4.02	4.02	4.02	3	0.13	0.03	0.17	0.00	0.00	22.3
39	226	4775	63	548	0	-66	636	4.02	4.02	4.02	4.02	3	0.11	0.02	0.09	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	282	3340	-96	326	0	-264	661	4.02	4.02	4.02	4.02	3	0.11	0.01	0.05	0.00	0.00	22.3
2	282	2958	-244	242	0	-249	548	4.02	4.02	4.02	4.02	2	0.09	0.01	0.04	0.00	0.00	22.3
3	282	2989	-248	252	0	-251	547	4.02	4.02	4.02	4.02	2	0.09	0.01	0.04	0.00	0.00	22.3
4	282	2148	100	249	0	-154	550	4.02	4.02	4.02	4.02	2	0.09	0.01	0.04	0.00	0.00	22.3
5	282	2180	96	259	0	-157	548	4.02	4.02	4.02	4.02	2	0.09	0.01	0.04	0.00	0.00	22.3

6	282	2638	-120	233	0	-213	508	4.02	4.02	4.02	4.02	2	0.08	0.01	0.04	0.00	0.00	22.3
7	282	2743	-132	266	0	-221	508	4.02	4.02	4.02	4.02	2	0.08	0.01	0.04	0.00	0.00	22.3
8	282	2395	-16	235	0	-185	525	4.02	4.02	4.02	4.02	2	0.09	0.01	0.04	0.00	0.00	22.3
9	282	2500	-28	268	0	-192	517	4.02	4.02	4.02	4.02	2	0.08	0.01	0.04	0.00	0.00	22.3
10	282	2958	-244	242	0	-249	548	4.02	4.02	4.02	4.02	2	0.09	0.01	0.04	0.00	0.00	22.3
11	282	2989	-248	252	0	-251	547	4.02	4.02	4.02	4.02	2	0.09	0.01	0.04	0.00	0.00	22.3
12	282	2148	100	249	0	-154	550	4.02	4.02	4.02	4.02	2	0.09	0.01	0.04	0.00	0.00	22.3
13	282	2180	96	259	0	-157	548	4.02	4.02	4.02	4.02	2	0.09	0.01	0.04	0.00	0.00	22.3
14	282	2638	-120	233	0	-213	508	4.02	4.02	4.02	4.02	2	0.08	0.01	0.04	0.00	0.00	22.3
15	282	2743	-132	266	0	-221	508	4.02	4.02	4.02	4.02	2	0.08	0.01	0.04	0.00	0.00	22.3
16	282	2395	-16	235	0	-185	525	4.02	4.02	4.02	4.02	2	0.09	0.01	0.04	0.00	0.00	22.3
17	282	2500	-28	268	0	-192	517	4.02	4.02	4.02	4.02	2	0.08	0.01	0.04	0.00	0.00	22.3
18	282	8113	-907	678	0	-692	848	4.02	4.02	4.02	4.02	3	0.22	0.03	0.16	0.00	0.00	22.3
19	282	4623	224	603	0	-316	712	4.02	4.02	4.02	4.02	3	0.12	0.02	0.10	0.00	0.00	22.3
20	282	6006	-312	647	0	-474	639	4.02	4.02	4.02	4.02	3	0.14	0.02	0.10	0.00	0.00	22.3
37	282	8286	-1203	601	0	-738	950	4.02	4.02	4.02	4.02	3	0.23	0.03	0.21	0.00	0.00	22.3
38	282	2470	682	475	0	-112	1145	4.02	4.02	4.02	4.02	3	0.18	0.02	0.12	0.00	0.00	22.3
39	282	4775	-212	548	0	-376	636	4.02	4.02	4.02	4.02	3	0.11	0.02	0.09	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	339	3340	-372	326	0	-448	661	4.02	4.02	4.02	4.02	3	0.12	0.01	0.07	0.00	0.00	22.3
2	339	2958	-456	242	0	-385	503	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
3	339	2989	-460	252	0	-393	500	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
4	339	2148	-112	249	0	-295	550	4.02	4.02	4.02	4.02	2	0.09	0.01	0.04	0.00	0.00	22.3
5	339	2180	-116	259	0	-303	548	4.02	4.02	4.02	4.02	2	0.09	0.01	0.04	0.00	0.00	22.3
6	339	2638	-332	233	0	-345	508	4.02	4.02	4.02	4.02	2	0.10	0.01	0.06	0.00	0.00	22.3
7	339	2743	-344	266	0	-371	508	4.02	4.02	4.02	4.02	2	0.11	0.01	0.06	0.00	0.00	22.3
8	339	2395	-228	235	0	-318	525	4.02	4.02	4.02	4.02	2	0.09	0.01	0.04	0.00	0.00	22.3
9	339	2500	-240	268	0	-344	517	4.02	4.02	4.02	4.02	2	0.10	0.01	0.04	0.00	0.00	22.3
10	339	2958	-456	242	0	-385	503	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
11	339	2989	-460	252	0	-393	500	4.02	4.02	4.02	4.02	2	0.12	0.01	0.08	0.00	0.00	22.3
12	339	2148	-112	249	0	-295	550	4.02	4.02	4.02	4.02	2	0.09	0.01	0.04	0.00	0.00	22.3
13	339	2180	-116	259	0	-303	548	4.02	4.02	4.02	4.02	2	0.09	0.01	0.04	0.00	0.00	22.3
14	339	2638	-332	233	0	-345	508	4.02	4.02	4.02	4.02	2	0.10	0.01	0.06	0.00	0.00	22.3
15	339	2743	-344	266	0	-371	508	4.02	4.02	4.02	4.02	2	0.11	0.01	0.06	0.00	0.00	22.3
16	339	2395	-228	235	0	-318	525	4.02	4.02	4.02	4.02	2	0.09	0.01	0.04	0.00	0.00	22.3
17	339	2500	-240	268	0	-344	517	4.02	4.02	4.02	4.02	2	0.10	0.01	0.04	0.00	0.00	22.3
18	339	8113	-1182	678	0	-1075	-800	4.02	4.02	4.02	4.02	3	0.34	0.03	0.21	0.00	0.00	22.3
19	339	4623	-51	603	0	-657	712	4.02	4.02	4.02	4.02	3	0.18	0.02	0.10	0.00	0.00	22.3
20	339	6006	-588	647	0	-839	583	4.02	4.02	4.02	4.02	3	0.25	0.02	0.10	0.00	0.00	22.3
37	339	8286	-1478	601	0	-1078	-1165	4.02	4.02	4.02	4.02	3	0.34	0.04	0.26	0.00	0.00	22.3
38	339	2470	406	475	0	-380	1258	4.02	4.02	4.02	4.02	3	0.19	0.01	0.08	0.00	0.00	22.3
39	339	4775	-487	548	0	-686	636	4.02	4.02	4.02	4.02	3	0.19	0.02	0.09	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	395	3340	-647	326	0	-632	569	4.02	4.02	4.02	4.02	3	0.17	0.02	0.12	0.00	0.00	22.3
2	395	2958	-668	242	0	-522	-384	4.02	4.02	4.02	4.02	2	0.16	0.02	0.12	0.00	0.00	22.3
3	395	2989	-671	252	0	-536	-392	4.02	4.02	4.02	4.02	2	0.16	0.02	0.12	0.00	0.00	22.3
4	395	2148	-324	249	0	-436	550	4.02	4.02	4.02	4.02	2	0.13	0.01	0.06	0.00	0.00	22.3
5	395	2180	-328	259	0	-450	548	4.02	4.02	4.02	4.02	2	0.13	0.01	0.06	0.00	0.00	22.3
6	395	2638	-543	233	0	-476	400	4.02	4.02	4.02	4.02	2	0.14	0.02	0.10	0.00	0.00	22.3
7	395	2743	-555	266	0	-522	386	4.02	4.02	4.02	4.02	2	0.16	0.02	0.10	0.00	0.00	22.3
8	395	2395	-440	235	0	-450	489	4.02	4.02	4.02	4.02	2	0.13	0.01	0.08	0.00	0.00	22.3
9	395	2500	-452	269	0	-496	474	4.02	4.02	4.02	4.02	2	0.15	0.01	0.08	0.00	0.00	22.3
10	395	2958	-668	242	0	-522	-384	4.02	4.02	4.02	4.02	2	0.16	0.02	0.12	0.00	0.00	22.3
11	395	2989	-671	252	0	-536	-392	4.02	4.02	4.02	4.02	2	0.16	0.02	0.12	0.00	0.00	22.3
12	395	2148	-324	249	0	-436	550	4.02	4.02	4.02	4.02	2	0.13	0.01	0.06	0.00	0.00	22.3
13	395	2180	-328	259	0	-450	548	4.02	4.02	4.02	4.02	2	0.13	0.01	0.06	0.00	0.00	22.3
14	395	2638	-543	233	0	-476	400	4.02	4.02	4.02	4.02	2	0.14	0.02	0.10	0.00	0.00	22.3
15	395	2743	-555	266	0	-522	386	4.02	4.02	4.02	4.02	2	0.16	0.02	0.10	0.00	0.00	22.3
16	395	2395	-440	235	0	-450	489	4.02	4.02	4.02	4.02	2	0.13	0.01	0.08	0.00	0.00	22.3
17	395	2500	-452	269	0	-496	474	4.02	4.02	4.02	4.02	2	0.15	0.01	0.08	0.00	0.00	22.3
18	395	8113	-1458	678	0	-1458	-1685	4.02	4.02	4.02	4.02	3	0.46	0.04	0.26	0.00	0.00	22.3
19	395	4623	-327	603	0	-997	712	4.02	4.02	4.02	4.02	3	0.28	0.02	0.10	0.00	0.00	22.3
20	395	6006	-863	647	0	-1205	-561	4.02	4.02	4.02	4.02	3	0.35	0.03	0.15	0.00	0.00	22.3
37	395	8286	-1754	601	0	-1417	-2217	4.02	4.02	4.02	4.02	3	0.45	0.05	0.31	0.00	0.00	22.3
38	395	2470	131	475	0	-649	1258	4.02	4.02	4.02	4.02	3	0.19	0.01	0.08	0.00	0.00	22.3
39	395	4775	-763	548	0	-995	429	4.02	4.02	4.02	4.02	3	0.28	0.02	0.14	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	452	3340	-923	326	0	-816	-670	4.02	4.02	4.02	4.02	3	0.22	0.03	0.16	0.00	0.00	22.3
2	452	2958	-880	242	0	-658	-929	4.02	4.02	4.02	4.02	2	0.20	0.03	0.16	0.00	0.00	22.3
3	452	2989	-883	252	0	-678	-939	4.02	4.02	4.02	4.02	2	0.21	0.03	0.16	0.00	0.00	22.3
4	452	2148	-536	249	0	-577	452	4.02	4.02	4.02	4.02	2	0.17	0.02	0.10	0.00	0.00	22.3
5	452	2180	-540	259	0	-596	445	4.02	4.02	4.02	4.02	2	0.18	0.02	0.10	0.00	0.00	22.3
6	452	2638	-755	233	0	-607	-624	4.02	4.02	4.02	4.02	2	0.18	0.02	0.13	0.00	0.00	22.3
7	452	2743	-767	266	0	-672	-657	4.02	4.02	4.02	4.02	2	0.20	0.02	0.14	0.00	0.00	22.3
8	452	2395	-652	235	0	-583	-373	4.02	4.02	4.02	4.02	2	0.17	0.02	0.12	0.00	0.00	22.3
9	452	2500	-664	268	0	-648	-406	4.02	4.02	4.02	4.02	2	0.19	0.02	0.12	0.00	0.00	22.3
10	452	2958	-880	242	0	-658	-929	4.02	4.02	4.02	4.02	2	0.20	0.03	0.16	0.00	0.00	22.3
11	452	2989	-883	252	0	-678	-939	4.02	4.02	4.02	4.02	2	0.21	0.03	0.16	0.00	0.00	22.3
12	452	2148	-536	249	0	-577	452	4.02	4.02	4.02	4.02	2	0.17	0.02	0.10	0.00	0.00	22.3
13	452	2180	-540	259	0	-596	445	4.02	4.02	4.02	4.02	2	0.18	0.02	0.10	0.00	0.00	22.3
14	452	2638	-755	233	0	-607	-624	4.02	4.02	4.02	4.02	2	0.18	0.02	0.13	0.00	0.00	22.3
15	452	2743	-767	266	0	-672	-657	4.02	4.02	4.02	4.02	2	0.20	0.02	0.14	0.00	0.00	22.3
16	452	2395	-652	235	0	-583	-373	4.02	4.02	4.02	4.02	2	0.17	0.02	0.12	0.00	0.00	22.3
17	452	2500	-664	268	0	-648	-406	4.02	4.02	4.02	4.02	2	0.19	0.02	0.12	0.00	0.00	22.3
18	452	8113	-1733	678	0	-1841	-2726	4.02	4.02	4.02	4.02	3	0.58	0.05	0.31	0.00	0.00	22.3
19	452	4623	-602	603	0	-1338	647	4.02	4.02	4.02	4.02	3	0.37	0.02	0.11	0.00	0.00	22.3
20	452	6006	-1139	647	0	-1570	-1267	4.02	4.02	4.02	4.02	3	0.46	0.03	0.20	0.00	0.00	22.3
37	452	8286	-2029	601	0	-1757	-3426	4.02	4.02	4.02	4.02	3	0.65	0.06	0.36	0.00	0.00	22.3
38	452	2470	-145	475	0	-917	1258	4.02	4.02	4.02	4.02	3	0.24	0.01	0.08	0.00	0.00	22.3
39	452	4775	-1038	548	0	-1305	-992	4.02	4.02	4.02	4.02	3	0.37	0.03	0.18	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	508	3340	-1198	326	0	-1000	-1409	4.02	4.02	4.02	4.02	3	0.27	0.03	0.21	0.00	0.00	22.3
2	508	2958	-1092	242	0	-795	-1593	4.02	4.02	4.02	4.02	2	0.27	0.03	0.19	0.00	0.00	22.3
3	508	2989	-1095	252	0	-820	-1605	4.02	4.02	4.02	4.02	2	0.27	0.03	0.20	0.00	0.00	22.3
4	508	2148	-748	249	0	-718	-561	4.02	4.02	4.02	4.02	2	0.21	0.02	0.13	0.00	0.00	22.3
5	508	2180	-752	259	0	-743	-573	4.02	4.02	4.02	4.02	2	0.22	0.02	0.13	0.00	0.00	22.3
6	508	2638	-967	233	0	-739	-1218	4.02	4.02	4.02	4.02	2	0.22	0.03	0.17	0.00	0.00	22.3
7	508	2743	-979	266	0	-822	-1258	4.02	4.02	4.02	4.02	2	0.25	0.03	0.17	0.00	0.00	22.3
8	508	2395	-864	235	0	-716	-908	4.02	4.02	4.02	4.02	2	0.21	0.03	0.15	0.00	0.00	22.3
9	508	2500	-876	268	0	-799	-949	4.02	4.02	4.02	4.02	2	0.24	0.03	0.16	0.00	0.00	22.3
10	508	2958	-1092	242	0	-795	-1593	4.02	4.02	4.02	4.02	2	0.27	0.03	0.19	0.00	0.00	22.3
11	508	2989	-1095	252	0	-820	-1605	4.02	4.02	4.02	4.02	2	0.27	0.03	0.20	0.00	0.00	22.3

12	508	2148	-748	249	0	-718	-561	4.02	4.02	4.02	4.02	2	0.21	0.02	0.13	0.00	0.00	22.3
13	508	2180	-752	259	0	-743	-573	4.02	4.02	4.02	4.02	2	0.22	0.02	0.13	0.00	0.00	22.3
14	508	2638	-967	233	0	-739	-1218	4.02	4.02	4.02	4.02	2	0.22	0.03	0.17	0.00	0.00	22.3
15	508	2743	-979	266	0	-822	-1258	4.02	4.02	4.02	4.02	2	0.25	0.03	0.17	0.00	0.00	22.3
16	508	2395	-864	235	0	-716	-908	4.02	4.02	4.02	4.02	2	0.21	0.03	0.15	0.00	0.00	22.3
17	508	2500	-876	268	0	-799	-949	4.02	4.02	4.02	4.02	2	0.24	0.03	0.16	0.00	0.00	22.3
18	508	8113	-2009	678	0	-2225	-3923	4.02	4.02	4.02	4.02	3	0.74	0.06	0.36	0.00	0.00	22.3
19	508	4623	-878	603	0	-1678	-520	4.02	4.02	4.02	4.02	3	0.47	0.03	0.16	0.00	0.00	22.3
20	508	6006	-1414	647	0	-1936	-2127	4.02	4.02	4.02	4.02	3	0.57	0.04	0.25	0.00	0.00	22.3
37	508	8286	-2305	601	0	-2096	-4790	4.02	4.02	4.02	4.02	3	0.91	0.07	0.41	0.00	0.00	22.3
38	508	2470	-420	475	0	-1186	1258	4.02	4.02	4.02	4.02	3	0.31	0.01	0.08	0.00	0.00	22.3
39	508	4775	-1314	548	0	-1614	-1796	4.02	4.02	4.02	4.02	3	0.45	0.04	0.23	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	565	3340	-1474	326	0	-1184	-1557	4.02	4.02	4.02	4.02	3	0.32	0.04	0.26	0.00	0.00	22.3
2	565	2958	-1304	242	0	-932	-1717	4.02	4.02	4.02	4.02	2	0.29	0.04	0.23	0.00	0.00	22.3
3	565	2989	-1307	252	0	-962	-1729	4.02	4.02	4.02	4.02	2	0.29	0.04	0.23	0.00	0.00	22.3
4	565	2148	-960	249	0	-859	-665	4.02	4.02	4.02	4.02	2	0.25	0.03	0.17	0.00	0.00	22.3
5	565	2180	-964	259	0	-890	-677	4.02	4.02	4.02	4.02	2	0.26	0.03	0.17	0.00	0.00	22.3
6	565	2638	-1179	233	0	-870	-1335	4.02	4.02	4.02	4.02	2	0.26	0.03	0.21	0.00	0.00	22.3
7	565	2743	-1191	266	0	-973	-1375	4.02	4.02	4.02	4.02	2	0.29	0.03	0.21	0.00	0.00	22.3
8	565	2395	-1076	235	0	-848	-1019	4.02	4.02	4.02	4.02	2	0.25	0.03	0.19	0.00	0.00	22.3
9	565	2500	-1088	268	0	-951	-1060	4.02	4.02	4.02	4.02	2	0.29	0.03	0.19	0.00	0.00	22.3
10	565	2958	-1304	242	0	-932	-1717	4.02	4.02	4.02	4.02	2	0.29	0.04	0.23	0.00	0.00	22.3
11	565	2989	-1307	252	0	-962	-1729	4.02	4.02	4.02	4.02	2	0.29	0.04	0.23	0.00	0.00	22.3
12	565	2148	-960	249	0	-859	-665	4.02	4.02	4.02	4.02	2	0.25	0.03	0.17	0.00	0.00	22.3
13	565	2180	-964	259	0	-890	-677	4.02	4.02	4.02	4.02	2	0.26	0.03	0.17	0.00	0.00	22.3
14	565	2638	-1179	233	0	-870	-1335	4.02	4.02	4.02	4.02	2	0.26	0.03	0.21	0.00	0.00	22.3
15	565	2743	-1191	266	0	-973	-1375	4.02	4.02	4.02	4.02	2	0.29	0.03	0.21	0.00	0.00	22.3
16	565	2395	-1076	235	0	-848	-1019	4.02	4.02	4.02	4.02	2	0.25	0.03	0.19	0.00	0.00	22.3
17	565	2500	-1088	268	0	-951	-1060	4.02	4.02	4.02	4.02	2	0.29	0.03	0.19	0.00	0.00	22.3
18	565	8113	-2284	678	0	-2608	-4119	4.02	4.02	4.02	4.02	3	0.82	0.07	0.41	0.00	0.00	22.3
19	565	4623	-1153	603	0	-2019	-650	4.02	4.02	4.02	4.02	3	0.57	0.03	0.21	0.00	0.00	22.3
20	565	6006	-1690	647	0	-2301	-2288	4.02	4.02	4.02	4.02	3	0.67	0.05	0.30	0.00	0.00	22.3
37	565	8286	-2580	601	0	-2436	-5003	4.02	4.02	4.02	4.02	3	0.95	0.07	0.46	0.00	0.00	22.3
38	565	2470	-696	475	0	-1454	1132	4.02	4.02	4.02	4.02	3	0.38	0.02	0.12	0.00	0.00	22.3
39	565	4775	-1589	548	0	-1924	-1951	4.02	4.02	4.02	4.02	3	0.54	0.05	0.28	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

Nome travata: **trave_502_IP1** Descrizione: **Trave_5 10-15-20-25**
ASTA NUM. 4 NI 294 NF 296 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y Permanente qy tot.
qy medio: 375.00 308.00 683.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	--												Fx,M	Bielle	V,Mx			
	cm	daN			daN*m			cmq								cmq/m		cm
1	0	113	2511	87	0	273	-2294	4.02	4.02	4.02	4.02	3	0.33	0.07	0.45	0.00	0.00	22.3
2	0	-117	1621	61	0	197	-847	4.02	4.02	4.02	4.02	2	0.13	0.05	0.29	0.00	0.00	22.3
3	0	-109	1622	61	0	196	-852	4.02	4.02	4.02	4.02	2	0.13	0.05	0.29	0.00	0.00	22.3
4	0	283	2240	73	0	224	-2677	4.02	4.02	4.02	4.02	2	0.41	0.06	0.40	0.00	0.00	22.3
5	0	291	2242	73	0	224	-2683	4.02	4.02	4.02	4.02	2	0.41	0.07	0.40	0.00	0.00	22.3
6	0	13	1835	66	0	207	-1481	4.02	4.02	4.02	4.02	2	0.22	0.05	0.33	0.00	0.00	22.3
7	0	40	1841	65	0	205	-1499	4.02	4.02	4.02	4.02	2	0.23	0.05	0.33	0.00	0.00	22.3
8	0	133	2021	69	0	216	-2030	4.02	4.02	4.02	4.02	2	0.31	0.06	0.36	0.00	0.00	22.3
9	0	160	2027	68	0	213	-2048	4.02	4.02	4.02	4.02	2	0.31	0.06	0.36	0.00	0.00	22.3
10	0	-117	1621	61	0	197	-847	4.02	4.02	4.02	4.02	2	0.13	0.05	0.29	0.00	0.00	22.3
11	0	-109	1622	61	0	196	-852	4.02	4.02	4.02	4.02	2	0.13	0.05	0.29	0.00	0.00	22.3
12	0	283	2240	73	0	224	-2677	4.02	4.02	4.02	4.02	2	0.41	0.06	0.40	0.00	0.00	22.3
13	0	291	2242	73	0	224	-2683	4.02	4.02	4.02	4.02	2	0.41	0.07	0.40	0.00	0.00	22.3
14	0	13	1835	66	0	207	-1481	4.02	4.02	4.02	4.02	2	0.22	0.05	0.33	0.00	0.00	22.3
15	0	40	1841	65	0	205	-1499	4.02	4.02	4.02	4.02	2	0.23	0.05	0.33	0.00	0.00	22.3
16	0	133	2021	69	0	216	-2030	4.02	4.02	4.02	4.02	2	0.31	0.06	0.36	0.00	0.00	22.3
17	0	160	2027	68	0	213	-2048	4.02	4.02	4.02	4.02	2	0.31	0.06	0.36	0.00	0.00	22.3
18	0	-638	1688	176	0	576	1029	4.02	4.02	4.02	4.02	3	0.14	0.05	0.30	0.00	0.00	22.3
19	0	1201	3466	179	0	548	-5135	4.02	4.02	4.02	4.02	3	0.76	0.10	0.62	0.00	0.00	22.3
20	0	311	2567	160	0	518	-2452	4.02	4.02	4.02	4.02	3	0.35	0.07	0.46	0.00	0.00	22.3
37	0	-1302	1071	145	0	490	2554	4.02	4.02	4.02	4.02	3	0.35	0.03	0.18	0.00	0.00	22.3
38	0	1764	4035	151	0	445	-6838	4.02	4.02	4.02	6.03	3	0.69	0.12	0.63	0.00	0.00	22.3
39	0	281	2536	119	0	394	-2367	4.02	4.02	4.02	4.02	3	0.34	0.07	0.45	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= 2.01 (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	56	113	2009	87	0	224	-2034	4.02	4.02	4.02	4.02	3	0.29	0.06	0.36	0.00	0.00	22.3
2	56	-117	1235	61	0	162	-665	4.02	4.02	4.02	4.02	2	0.10	0.04	0.22	0.00	0.00	22.3
3	56	-109	1236	61	0	161	-670	4.02	4.02	4.02	4.02	2	0.10	0.04	0.22	0.00	0.00	22.3
4	56	283	1854	73	0	183	-2459	4.02	4.02	4.02	4.02	2	0.38	0.05	0.33	0.00	0.00	22.3
5	56	291	1856	73	0	182	-2465	4.02	4.02	4.02	4.02	2	0.38	0.05	0.33	0.00	0.00	22.3
6	56	13	1449	66	0	170	-1287	4.02	4.02	4.02	4.02	2	0.20	0.04	0.26	0.00	0.00	22.3
7	56	40	1455	65	0	168	-1304	4.02	4.02	4.02	4.02	2	0.20	0.04	0.26	0.00	0.00	22.3
8	56	133	1635	69	0	177	-1825	4.02	4.02	4.02	4.02	2	0.28	0.05	0.29	0.00	0.00	22.3
9	56	160	1641	68	0	174	-1843	4.02	4.02	4.02	4.02	2	0.28	0.05	0.29	0.00	0.00	22.3
10	56	-117	1235	61	0	162	-665	4.02	4.02	4.02	4.02	2	0.10	0.04	0.22	0.00	0.00	22.3
11	56	-109	1236	61	0	161	-670	4.02	4.02	4.02	4.02	2	0.10	0.04	0.22	0.00	0.00	22.3
12	56	283	1854	73	0	183	-2459	4.02	4.02	4.02	4.02	2	0.38	0.05	0.33	0.00	0.00	22.3
13	56	291	1856	73	0	182	-2465	4.02	4.02	4.02	4.02	2	0.38	0.05	0.33	0.00	0.00	22.3
14	56	13	1449	66	0	170	-1287	4.02	4.02	4.02	4.02	2	0.20	0.04	0.26	0.00	0.00	22.3
15	56	40	1455	65	0	168	-1304	4.02	4.02	4.02	4.02	2	0.20	0.04	0.26	0.00	0.00	22.3
16	56	133	1635	69	0	177	-1825	4.02	4.02	4.02	4.02	2	0.28	0.05	0.29	0.00	0.00	22.3
17	56	160	1641	68	0	174	-1843	4.02	4.02	4.02	4.02	2	0.28	0.05	0.29	0.00	0.00	22.3
18	56	-638	1186	176	0	476	1587	4.02	4.02	4.02	4.02	3	0.22	0.03	0.21	0.00	0.00	22.3
19	56	1201	2964	179	0	447	-4819	4.02	4.02	4.02	4.02	3	0.72	0.09	0.53	0.00	0.00	22.3
20	56	311	2065	160	0	427	-2189	4.02	4.02	4.02	4.02	3	0.32	0.06	0.37	0.00	0.00	22.3
37	56	-1302	569	145	0	408	2655	4.02	4.02	4.02	4.02	3	0.37	0.02	0.10	0.00	0.00	22.3
38	56	1764	3533	151	0	360	-6489	4.02	4.02	4.02	4.02	3	0.98	0.10	0.63	0.00	0.00	22.3
39	56	281	2034	119	0	327	-2106	4.02	4.02	4.02	4.02	3	0.30	0.06	0.36	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	113	113	1508	87	0	175	-787	4.02	4.02	4.02	4.02	3	0.11	0.04	0.27	0.00	0.00	22.3
2	113	-117	849	61	0	127	979	4.02	4.02	4.02	4.02	2	0.15	0.02	0.15	0.00	0.00	22.3
3	113	-109	850	61	0	127	976	4.02	4.02	4.02	4.02	2	0.15	0.02	0.15	0.00	0.00	22.3

4	113	283	1468	73	0	142	-1325	4.02	4.02	4.02	4.02	2	0.20	0.04	0.26	0.00	0.00	22.3
5	113	291	1470	73	0	141	-1330	4.02	4.02	4.02	4.02	2	0.20	0.04	0.26	0.00	0.00	22.3
6	113	13	1063	66	0	133	695	4.02	4.02	4.02	4.02	2	0.11	0.03	0.19	0.00	0.00	22.3
7	113	40	1069	65	0	131	687	4.02	4.02	4.02	4.02	2	0.10	0.03	0.19	0.00	0.00	22.3
8	113	133	1249	69	0	138	-815	4.02	4.02	4.02	4.02	2	0.12	0.04	0.22	0.00	0.00	22.3
9	113	160	1255	68	0	136	-829	4.02	4.02	4.02	4.02	2	0.13	0.04	0.22	0.00	0.00	22.3
10	113	-117	849	61	0	127	979	4.02	4.02	4.02	4.02	2	0.15	0.02	0.15	0.00	0.00	22.3
11	113	-109	850	61	0	127	976	4.02	4.02	4.02	4.02	2	0.15	0.02	0.15	0.00	0.00	22.3
12	113	283	1468	73	0	142	-1325	4.02	4.02	4.02	4.02	2	0.20	0.04	0.26	0.00	0.00	22.3
13	113	291	1470	73	0	141	-1330	4.02	4.02	4.02	4.02	2	0.20	0.04	0.26	0.00	0.00	22.3
14	113	13	1063	66	0	133	695	4.02	4.02	4.02	4.02	2	0.11	0.03	0.19	0.00	0.00	22.3
15	113	40	1069	65	0	131	687	4.02	4.02	4.02	4.02	2	0.10	0.03	0.19	0.00	0.00	22.3
16	113	133	1249	69	0	138	-815	4.02	4.02	4.02	4.02	2	0.12	0.04	0.22	0.00	0.00	22.3
17	113	160	1255	68	0	136	-829	4.02	4.02	4.02	4.02	2	0.13	0.04	0.22	0.00	0.00	22.3
18	113	-638	685	176	0	377	1760	4.02	4.02	4.02	4.02	3	0.25	0.02	0.12	0.00	0.00	22.3
19	113	1201	2463	179	0	346	-3032	4.02	4.02	4.02	4.02	3	0.45	0.07	0.44	0.00	0.00	22.3
20	113	311	1564	160	0	337	-910	4.02	4.02	4.02	4.02	3	0.13	0.05	0.28	0.00	0.00	22.3
37	113	-1302	68	145	0	326	2655	4.02	4.02	4.02	4.02	3	0.37	0.00	0.01	0.00	0.00	22.3
38	113	1764	3032	151	0	275	-4380	4.02	4.02	4.02	4.02	3	0.66	0.09	0.54	0.00	0.00	22.3
39	113	281	1533	119	0	259	-844	4.02	4.02	4.02	4.02	3	0.12	0.04	0.27	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	170	113	1006	87	0	126	1195	4.02	4.02	4.02	4.02	3	0.17	0.03	0.18	0.00	0.00	22.3
2	170	-117	463	61	0	93	1072	4.02	4.02	4.02	4.02	2	0.16	0.01	0.08	0.00	0.00	22.3
3	170	-109	464	61	0	92	1070	4.02	4.02	4.02	4.02	2	0.16	0.01	0.08	0.00	0.00	22.3
4	170	283	1082	73	0	101	686	4.02	4.02	4.02	4.02	2	0.10	0.03	0.19	0.00	0.00	22.3
5	170	291	1084	73	0	100	684	4.02	4.02	4.02	4.02	2	0.10	0.03	0.19	0.00	0.00	22.3
6	170	13	677	66	0	96	979	4.02	4.02	4.02	4.02	2	0.15	0.02	0.12	0.00	0.00	22.3
7	170	40	683	65	0	95	977	4.02	4.02	4.02	4.02	2	0.15	0.02	0.12	0.00	0.00	22.3
8	170	133	863	69	0	98	852	4.02	4.02	4.02	4.02	2	0.13	0.03	0.15	0.00	0.00	22.3
9	170	160	869	68	0	97	846	4.02	4.02	4.02	4.02	2	0.13	0.03	0.15	0.00	0.00	22.3
10	170	-117	463	61	0	93	1072	4.02	4.02	4.02	4.02	2	0.16	0.01	0.08	0.00	0.00	22.3
11	170	-109	464	61	0	92	1070	4.02	4.02	4.02	4.02	2	0.16	0.01	0.08	0.00	0.00	22.3
12	170	283	1082	73	0	101	686	4.02	4.02	4.02	4.02	2	0.10	0.03	0.19	0.00	0.00	22.3
13	170	291	1084	73	0	100	684	4.02	4.02	4.02	4.02	2	0.10	0.03	0.19	0.00	0.00	22.3
14	170	13	677	66	0	96	979	4.02	4.02	4.02	4.02	2	0.15	0.02	0.12	0.00	0.00	22.3
15	170	40	683	65	0	95	977	4.02	4.02	4.02	4.02	2	0.15	0.02	0.12	0.00	0.00	22.3
16	170	133	863	69	0	98	852	4.02	4.02	4.02	4.02	2	0.13	0.03	0.15	0.00	0.00	22.3
17	170	160	869	68	0	97	846	4.02	4.02	4.02	4.02	2	0.13	0.03	0.15	0.00	0.00	22.3
18	170	-638	183	176	0	277	1760	4.02	4.02	4.02	4.02	3	0.25	0.01	0.03	0.00	0.00	22.3
19	170	1201	1961	179	0	245	-1528	4.02	4.02	4.02	4.02	3	0.23	0.06	0.35	0.00	0.00	22.3
20	170	311	1062	160	0	246	1161	4.02	4.02	4.02	4.02	3	0.17	0.03	0.19	0.00	0.00	22.3
37	170	-1302	-434	145	0	244	2655	4.02	4.02	4.02	4.02	3	0.37	0.01	0.07	0.00	0.00	22.3
38	170	1764	2530	151	0	189	-2555	4.02	4.02	4.02	4.02	3	0.39	0.07	0.45	0.00	0.00	22.3
39	170	281	1031	119	0	192	1179	4.02	4.02	4.02	4.02	3	0.17	0.03	0.18	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	226	113	504	87	0	76	1255	4.02	4.02	4.02	4.02	3	0.18	0.01	0.09	0.00	0.00	22.3
2	226	-117	77	61	0	58	1072	4.02	4.02	4.02	4.02	2	0.16	0.00	0.01	0.00	0.00	22.3
3	226	-109	78	61	0	58	1070	4.02	4.02	4.02	4.02	2	0.16	0.00	0.01	0.00	0.00	22.3
4	226	283	696	73	0	59	992	4.02	4.02	4.02	4.02	2	0.15	0.02	0.12	0.00	0.00	22.3
5	226	291	698	73	0	59	992	4.02	4.02	4.02	4.02	2	0.15	0.02	0.12	0.00	0.00	22.3
6	226	13	291	66	0	59	979	4.02	4.02	4.02	4.02	2	0.15	0.01	0.05	0.00	0.00	22.3
7	226	40	297	65	0	58	977	4.02	4.02	4.02	4.02	2	0.15	0.01	0.05	0.00	0.00	22.3
8	226	133	477	69	0	59	954	4.02	4.02	4.02	4.02	2	0.15	0.01	0.09	0.00	0.00	22.3
9	226	160	483	68	0	58	952	4.02	4.02	4.02	4.02	2	0.15	0.01	0.09	0.00	0.00	22.3
10	226	-117	77	61	0	58	1072	4.02	4.02	4.02	4.02	2	0.16	0.00	0.01	0.00	0.00	22.3
11	226	-109	78	61	0	58	1070	4.02	4.02	4.02	4.02	2	0.16	0.00	0.01	0.00	0.00	22.3
12	226	283	696	73	0	59	992	4.02	4.02	4.02	4.02	2	0.15	0.02	0.12	0.00	0.00	22.3
13	226	291	698	73	0	59	992	4.02	4.02	4.02	4.02	2	0.15	0.02	0.12	0.00	0.00	22.3
14	226	13	291	66	0	59	979	4.02	4.02	4.02	4.02	2	0.15	0.01	0.05	0.00	0.00	22.3
15	226	40	297	65	0	58	977	4.02	4.02	4.02	4.02	2	0.15	0.01	0.05	0.00	0.00	22.3
16	226	133	477	69	0	59	954	4.02	4.02	4.02	4.02	2	0.15	0.01	0.09	0.00	0.00	22.3
17	226	160	483	68	0	58	952	4.02	4.02	4.02	4.02	2	0.15	0.01	0.09	0.00	0.00	22.3
18	226	-638	-319	176	0	178	1760	4.02	4.02	4.02	4.02	3	0.25	0.01	0.06	0.00	0.00	22.3
19	226	1201	1460	179	0	143	1170	4.02	4.02	4.02	4.02	3	0.17	0.04	0.26	0.00	0.00	22.3
20	226	311	560	160	0	155	1257	4.02	4.02	4.02	4.02	3	0.18	0.02	0.10	0.00	0.00	22.3
37	226	-1302	-936	145	0	162	2639	4.02	4.02	4.02	4.02	3	0.36	0.03	0.16	0.00	0.00	22.3
38	226	1764	2028	151	0	104	1041	4.02	4.02	4.02	4.02	3	0.16	0.06	0.36	0.00	0.00	22.3
39	226	281	530	119	0	125	1255	4.02	4.02	4.02	4.02	3	0.18	0.02	0.09	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	282	113	2	87	0	27	1255	4.02	4.02	4.02	4.02	3	0.18	0.00	0.00	0.00	0.00	22.3
2	282	-117	-308	61	0	24	1072	4.02	4.02	4.02	4.02	2	0.16	0.01	0.05	0.00	0.00	22.3
3	282	-109	-308	61	0	24	1070	4.02	4.02	4.02	4.02	2	0.16	0.01	0.05	0.00	0.00	22.3
4	282	283	310	73	0	18	992	4.02	4.02	4.02	4.02	2	0.15	0.01	0.06	0.00	0.00	22.3
5	282	291	312	73	0	18	992	4.02	4.02	4.02	4.02	2	0.15	0.01	0.06	0.00	0.00	22.3
6	282	13	-94	66	0	22	979	4.02	4.02	4.02	4.02	2	0.15	0.00	0.02	0.00	0.00	22.3
7	282	40	-88	65	0	21	977	4.02	4.02	4.02	4.02	2	0.15	0.00	0.02	0.00	0.00	22.3
8	282	133	92	69	0	20	954	4.02	4.02	4.02	4.02	2	0.15	0.00	0.02	0.00	0.00	22.3
9	282	160	98	68	0	20	952	4.02	4.02	4.02	4.02	2	0.15	0.00	0.02	0.00	0.00	22.3
10	282	-117	-308	61	0	24	1072	4.02	4.02	4.02	4.02	2	0.16	0.01	0.05	0.00	0.00	22.3
11	282	-109	-308	61	0	24	1070	4.02	4.02	4.02	4.02	2	0.16	0.01	0.05	0.00	0.00	22.3
12	282	283	310	73	0	18	992	4.02	4.02	4.02	4.02	2	0.15	0.01	0.06	0.00	0.00	22.3
13	282	291	312	73	0	18	992	4.02	4.02	4.02	4.02	2	0.15	0.01	0.06	0.00	0.00	22.3
14	282	13	-94	66	0	22	979	4.02	4.02	4.02	4.02	2	0.15	0.00	0.02	0.00	0.00	22.3
15	282	40	-88	65	0	21	977	4.02	4.02	4.02	4.02	2	0.15	0.00	0.02	0.00	0.00	22.3
16	282	133	92	69	0	20	954	4.02	4.02	4.02	4.02	2	0.15	0.00	0.02	0.00	0.00	22.3
17	282	160	98	68	0	20	952	4.02	4.02	4.02	4.02	2	0.15	0.00	0.02	0.00	0.00	22.3
18	282	-638	-820	176	0	78	1760	4.02	4.02	4.02	4.02	3	0.25	0.02	0.14	0.00	0.00	22.3
19	282	1201	958	179	0	42	1600	4.02	4.02	4.02	4.02	3	0.24	0.03	0.17	0.00	0.00	22.3
20	282	311	58	160	0	65	1257	4.02	4.02	4.02	4.02	3	0.18	0.01	0.03	0.00	0.00	22.3
37	282	-1302	-1438	145	0	80	2222	4.02	4.02	4.02	4.02	3	0.31	0.04	0.25	0.00	0.00	22.3
38	282	1764	1527	151	0	19	1791	4.02	4.02	4.02	4.02	3	0.27	0.04	0.27	0.00	0.00	22.3
39	282	281	28	119	0	57	1255	4.02	4.02	4.02	4.02	3	0.18	0.00	0.00	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	339	113	-499	87	0	-22	1255	4.02	4.02	4.02	4.02	3	0.18	0.01	0.09	0.00	0.00	22.3
2	339	-117	-694	61	0	-11	1072	4.02	4.02	4.02	4.02	2	0.16	0.02	0.12	0.00	0.00	22.3
3	339	-109	-693	61	0	-11	1070	4.02	4.02	4.02	4.02	2	0.16	0.02	0.12	0.00	0.00	22.3
4	339	283	-75	73	0	-23	992	4.02	4.02	4.02	4.02	2	0.15	0.00	0.01	0.00	0.00	22.3
5	339	291	-73	73	0	-23	992	4.02	4.02	4.02	4.02	2	0.15	0.00	0.01	0.00	0.00	22.3
6	339	13	-480	66	0	-15	979	4.02	4.02	4.02	4.02	2	0.15	0.01	0.09	0.00	0.00	22.3
7	339	40	-474	65	0	-15	977	4.02	4.02	4.02	4.02	2	0.15	0.01	0.08	0.00	0.00	22.3
8	339	133	-294	69	0	-19	954	4.02	4.02	4.02	4.02	2	0.15	0.01	0.05	0.00	0.00	22.3
9	339	160	-288	68	0	-19	952	4.02	4.02	4.02	4.02	2	0.15	0.01	0.05	0.00	0.00	22.3

10	339	-117	-694	61	0	-11	1072	4.02	4.02	4.02	4.02	2	0.16	0.02	0.12	0.00	0.00	22.3
11	339	-109	-693	61	0	-11	1070	4.02	4.02	4.02	4.02	2	0.16	0.02	0.12	0.00	0.00	22.3
12	339	283	-75	73	0	-23	992	4.02	4.02	4.02	4.02	2	0.15	0.00	0.01	0.00	0.00	22.3
13	339	291	-73	73	0	-23	992	4.02	4.02	4.02	4.02	2	0.15	0.00	0.01	0.00	0.00	22.3
14	339	13	-480	66	0	-15	979	4.02	4.02	4.02	4.02	2	0.15	0.01	0.09	0.00	0.00	22.3
15	339	40	-474	65	0	-15	977	4.02	4.02	4.02	4.02	2	0.15	0.01	0.08	0.00	0.00	22.3
16	339	133	-294	69	0	-19	954	4.02	4.02	4.02	4.02	2	0.15	0.01	0.05	0.00	0.00	22.3
17	339	160	-288	68	0	-19	952	4.02	4.02	4.02	4.02	2	0.15	0.01	0.05	0.00	0.00	22.3
18	339	-638	-1322	176	0	-21	1464	4.02	4.02	4.02	4.02	3	0.21	0.04	0.23	0.00	0.00	22.3
19	339	1201	456	179	0	-59	1630	4.02	4.02	4.02	4.02	3	0.24	0.01	0.08	0.00	0.00	22.3
20	339	311	-443	160	0	-26	1257	4.02	4.02	4.02	4.02	3	0.18	0.01	0.08	0.00	0.00	22.3
37	339	-1302	-1939	145	0	-3	1522	4.02	4.02	4.02	4.02	3	0.21	0.06	0.33	0.00	0.00	22.3
38	339	1764	1025	151	0	-66	2258	4.02	4.02	4.02	4.02	3	0.34	0.03	0.18	0.00	0.00	22.3
39	339	281	-474	119	0	-10	1255	4.02	4.02	4.02	4.02	3	0.18	0.01	0.08	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	396	113	-1001	87	0	-71	1198	4.02	4.02	4.02	4.02	3	0.17	0.03	0.18	0.00	0.00	22.3
2	396	-117	-1080	61	0	-45	769	4.02	4.02	4.02	4.02	2	0.12	0.03	0.19	0.00	0.00	22.3
3	396	-109	-1079	61	0	-45	769	4.02	4.02	4.02	4.02	2	0.12	0.03	0.19	0.00	0.00	22.3
4	396	283	-461	73	0	-64	992	4.02	4.02	4.02	4.02	2	0.15	0.01	0.08	0.00	0.00	22.3
5	396	291	-459	73	0	-64	992	4.02	4.02	4.02	4.02	2	0.15	0.01	0.08	0.00	0.00	22.3
6	396	13	-866	66	0	-52	875	4.02	4.02	4.02	4.02	2	0.13	0.03	0.15	0.00	0.00	22.3
7	396	40	-860	65	0	-52	877	4.02	4.02	4.02	4.02	2	0.13	0.02	0.15	0.00	0.00	22.3
8	396	133	-680	69	0	-58	954	4.02	4.02	4.02	4.02	2	0.15	0.02	0.12	0.00	0.00	22.3
9	396	160	-674	68	0	-58	952	4.02	4.02	4.02	4.02	2	0.15	0.02	0.12	0.00	0.00	22.3
10	396	-117	-1080	61	0	-45	769	4.02	4.02	4.02	4.02	2	0.12	0.03	0.19	0.00	0.00	22.3
11	396	-109	-1079	61	0	-45	769	4.02	4.02	4.02	4.02	2	0.12	0.03	0.19	0.00	0.00	22.3
12	396	283	-461	73	0	-64	992	4.02	4.02	4.02	4.02	2	0.15	0.01	0.08	0.00	0.00	22.3
13	396	291	-459	73	0	-64	992	4.02	4.02	4.02	4.02	2	0.15	0.01	0.08	0.00	0.00	22.3
14	396	13	-866	66	0	-52	875	4.02	4.02	4.02	4.02	2	0.13	0.03	0.15	0.00	0.00	22.3
15	396	40	-860	65	0	-52	877	4.02	4.02	4.02	4.02	2	0.13	0.02	0.15	0.00	0.00	22.3
16	396	133	-680	69	0	-58	954	4.02	4.02	4.02	4.02	2	0.15	0.02	0.12	0.00	0.00	22.3
17	396	160	-674	68	0	-58	952	4.02	4.02	4.02	4.02	2	0.15	0.02	0.12	0.00	0.00	22.3
18	396	-638	-1824	176	0	-121	-1018	4.02	4.02	4.02	4.02	3	0.14	0.05	0.32	0.00	0.00	22.3
19	396	1201	-45	179	0	-161	1630	4.02	4.02	4.02	4.02	3	0.24	0.01	0.03	0.00	0.00	22.3
20	396	311	-945	160	0	-116	1235	4.02	4.02	4.02	4.02	3	0.18	0.03	0.17	0.00	0.00	22.3
37	396	-1302	-2441	145	0	-85	-1932	4.02	4.02	4.02	4.02	3	0.27	0.07	0.42	0.00	0.00	22.3
38	396	1764	524	151	0	-151	2331	4.02	4.02	4.02	4.02	3	0.35	0.02	0.09	0.00	0.00	22.3
39	396	281	-975	119	0	-77	1214	4.02	4.02	4.02	4.02	3	0.18	0.03	0.17	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	452	113	-1503	87	0	-120	-777	4.02	4.02	4.02	4.02	3	0.11	0.04	0.27	0.00	0.00	22.3
2	452	-117	-1466	61	0	-80	-1240	4.02	4.02	4.02	4.02	2	0.19	0.04	0.26	0.00	0.00	22.3
3	452	-109	-1465	61	0	-80	-1238	4.02	4.02	4.02	4.02	2	0.19	0.04	0.26	0.00	0.00	22.3
4	452	283	-847	73	0	-105	899	4.02	4.02	4.02	4.02	2	0.14	0.02	0.15	0.00	0.00	22.3
5	452	291	-845	73	0	-105	900	4.02	4.02	4.02	4.02	2	0.14	0.02	0.15	0.00	0.00	22.3
6	452	13	-1252	66	0	-89	-795	4.02	4.02	4.02	4.02	2	0.12	0.04	0.22	0.00	0.00	22.3
7	452	40	-1246	65	0	-89	-785	4.02	4.02	4.02	4.02	2	0.12	0.04	0.22	0.00	0.00	22.3
8	452	133	-1066	69	0	-97	668	4.02	4.02	4.02	4.02	2	0.10	0.03	0.19	0.00	0.00	22.3
9	452	160	-1060	68	0	-96	673	4.02	4.02	4.02	4.02	2	0.10	0.03	0.19	0.00	0.00	22.3
10	452	-117	-1466	61	0	-80	-1240	4.02	4.02	4.02	4.02	2	0.19	0.04	0.26	0.00	0.00	22.3
11	452	-109	-1465	61	0	-80	-1238	4.02	4.02	4.02	4.02	2	0.19	0.04	0.26	0.00	0.00	22.3
12	452	283	-847	73	0	-105	899	4.02	4.02	4.02	4.02	2	0.14	0.02	0.15	0.00	0.00	22.3
13	452	291	-845	73	0	-105	900	4.02	4.02	4.02	4.02	2	0.14	0.02	0.15	0.00	0.00	22.3
14	452	13	-1252	66	0	-89	-795	4.02	4.02	4.02	4.02	2	0.12	0.04	0.22	0.00	0.00	22.3
15	452	40	-1246	65	0	-89	-785	4.02	4.02	4.02	4.02	2	0.12	0.04	0.22	0.00	0.00	22.3
16	452	133	-1066	69	0	-97	668	4.02	4.02	4.02	4.02	2	0.10	0.03	0.19	0.00	0.00	22.3
17	452	160	-1060	68	0	-96	673	4.02	4.02	4.02	4.02	2	0.10	0.03	0.19	0.00	0.00	22.3
18	452	-638	-2326	176	0	-220	-2444	4.02	4.02	4.02	4.02	3	0.34	0.07	0.41	0.00	0.00	22.3
19	452	1201	-547	179	0	-262	1630	4.02	4.02	4.02	4.02	3	0.24	0.02	0.10	0.00	0.00	22.3
20	452	311	-1447	160	0	-207	813	4.02	4.02	4.02	4.02	3	0.12	0.04	0.26	0.00	0.00	22.3
37	452	-1302	-2943	145	0	-167	-3707	4.02	4.02	4.02	4.02	3	0.51	0.08	0.51	0.00	0.00	22.3
38	452	1764	22	151	0	-236	2331	4.02	4.02	4.02	4.02	3	0.35	0.00	0.02	0.00	0.00	22.3
39	452	281	-1477	119	0	-144	775	4.02	4.02	4.02	4.02	3	0.11	0.04	0.26	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	508	113	-2004	87	0	-170	-2021	4.02	4.02	4.02	4.02	3	0.29	0.06	0.36	0.00	0.00	22.3
2	508	-117	-1852	61	0	-115	-2373	4.02	4.02	4.02	4.02	2	0.36	0.05	0.33	0.00	0.00	22.3
3	508	-109	-1851	61	0	-114	-2369	4.02	4.02	4.02	4.02	2	0.36	0.05	0.33	0.00	0.00	22.3
4	508	283	-1233	73	0	-147	-742	4.02	4.02	4.02	4.02	2	0.11	0.04	0.22	0.00	0.00	22.3
5	508	291	-1231	73	0	-146	-738	4.02	4.02	4.02	4.02	2	0.11	0.04	0.22	0.00	0.00	22.3
6	508	13	-1638	66	0	-126	-1807	4.02	4.02	4.02	4.02	2	0.27	0.05	0.29	0.00	0.00	22.3
7	508	40	-1632	65	0	-125	-1793	4.02	4.02	4.02	4.02	2	0.27	0.05	0.29	0.00	0.00	22.3
8	508	133	-1452	69	0	-136	-1318	4.02	4.02	4.02	4.02	2	0.20	0.04	0.26	0.00	0.00	22.3
9	508	160	-1446	68	0	-135	-1304	4.02	4.02	4.02	4.02	2	0.20	0.04	0.26	0.00	0.00	22.3
10	508	-117	-1852	61	0	-115	-2373	4.02	4.02	4.02	4.02	2	0.36	0.05	0.33	0.00	0.00	22.3
11	508	-109	-1851	61	0	-114	-2369	4.02	4.02	4.02	4.02	2	0.36	0.05	0.33	0.00	0.00	22.3
12	508	283	-1233	73	0	-147	-742	4.02	4.02	4.02	4.02	2	0.11	0.04	0.22	0.00	0.00	22.3
13	508	291	-1231	73	0	-146	-738	4.02	4.02	4.02	4.02	2	0.11	0.04	0.22	0.00	0.00	22.3
14	508	13	-1638	66	0	-126	-1807	4.02	4.02	4.02	4.02	2	0.27	0.05	0.29	0.00	0.00	22.3
15	508	40	-1632	65	0	-125	-1793	4.02	4.02	4.02	4.02	2	0.27	0.05	0.29	0.00	0.00	22.3
16	508	133	-1452	69	0	-136	-1318	4.02	4.02	4.02	4.02	2	0.20	0.04	0.26	0.00	0.00	22.3
17	508	160	-1446	68	0	-135	-1304	4.02	4.02	4.02	4.02	2	0.20	0.04	0.26	0.00	0.00	22.3
18	508	-638	-2827	176	0	-320	-4153	4.02	4.02	4.02	4.02	3	0.58	0.08	0.50	0.00	0.00	22.3
19	508	1201	-1048	179	0	-363	1543	4.02	4.02	4.02	4.02	3	0.23	0.03	0.19	0.00	0.00	22.3
20	508	311	-1948	160	0	-298	-1864	4.02	4.02	4.02	4.02	3	0.27	0.06	0.35	0.00	0.00	22.3
37	508	-1302	-3444	145	0	-249	-5765	4.02	4.02	4.02	4.02	3	0.80	0.10	0.59	0.00	0.00	22.3
38	508	1764	-480	151	0	-321	2331	4.02	4.02	4.02	4.02	3	0.35	0.01	0.09	0.00	0.00	22.3
39	508	281	-1978	119	0	-212	-1950	4.02	4.02	4.02	4.02	3	0.28	0.06	0.35	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	565	113	-2506	87	0	-219	-2281	4.02	4.02	4.02	4.02	3	0.33	0.07	0.45	0.00	0.00	22.3
2	565	-117	-2238	61	0	-149	-2591	4.02	4.02	4.02	4.02	2	0.39	0.06	0.40	0.00	0.00	22.3
3	565	-109	-2237	61	0	-149	-2587	4.02	4.02	4.02	4.02	2	0.39	0.06	0.40	0.00	0.00	22.3
4	565	283	-1619	73	0	-188	-923	4.02	4.02	4.02	4.02	2	0.14	0.05	0.29	0.00	0.00	22.3
5	565	291	-1617	73	0	-188	-919	4.02	4.02	4.02	4.02	2	0.14	0.05	0.29	0.00	0.00	22.3
6	565	13	-2024	66	0	-163	-2012	4.02	4.02	4.02	4.02	2	0.31	0.06	0.36	0.00	0.00	22.3
7	565	40	-2018	65	0	-162	-1998	4.02	4.02	4.02	4.02	2	0.30	0.06	0.36	0.00	0.00	22.3
8	565	133	-1838	69	0	-175	-1512	4.02	4.02	4.02	4.02	2	0.23	0.05	0.33	0.00	0.00	22.3
9	565	160	-1832	68	0	-173	-1498	4.02	4.02	4.02	4.02	2	0.23	0.05	0.33	0.00	0.00	22.3
10	565	-117	-2238	61	0	-149	-2591	4.02	4.02	4.02	4.02	2	0.39	0.06	0.40	0.00	0.00	22.3
11	565	-109	-2237	61	0	-149	-2587	4.02	4.02	4.02	4.02	2	0.39	0.06	0.40	0.00	0.00	22.3
12	565	283	-1619	73	0	-188	-923	4.02	4.02	4.02	4.02	2	0.14	0.05	0.29	0.00	0.00	22.3
13	565	291	-1617	73	0	-188	-919	4.02	4.02	4.02	4.02	2	0.14	0.05	0.29	0.00	0.00	22.3
14	565	13	-2024	66	0	-163	-2012	4.02	4.02	4.02	4.02	2	0.31	0.06	0.36	0.00	0.00	22.3
15	565	40	-2018	65	0	-162	-1998	4.02	4.02	4.02	4.02	2	0.30	0.06	0.36	0.00	0.00	22.3

16	565	133	-1838	69	0	-175	-1512	4.02	4.02	4.02	4.02	2	0.23	0.05	0.33	0.00	0.00	22.3
17	565	160	-1832	68	0	-173	-1498	4.02	4.02	4.02	4.02	2	0.23	0.05	0.33	0.00	0.00	22.3
18	565	-638	-3329	176	0	-419	-4461	4.02	4.02	4.02	4.02	3	0.63	0.10	0.58	0.00	0.00	22.3
19	565	1201	-1550	179	0	-464	1063	4.02	4.02	4.02	4.02	3	0.16	0.04	0.28	0.00	0.00	22.3
20	565	311	-2450	160	0	-388	-2120	4.02	4.02	4.02	4.02	3	0.31	0.07	0.44	0.00	0.00	22.3
37	565	-1302	-3946	145	0	-331	-6109	4.02	4.02	4.02	4.02	3	0.84	0.11	0.68	0.00	0.00	22.3
38	565	1764	-981	151	0	-406	2286	4.02	4.02	4.02	4.02	3	0.35	0.03	0.17	0.00	0.00	22.3
39	565	281	-2480	119	0	-279	-2208	4.02	4.02	4.02	4.02	3	0.32	0.07	0.44	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

Nome travata: **trave_502_IP1** Descrizione: **Trave_5 10-15-20-25**
ASTA NUM. 5 NI 296 NF 298 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y Permanente qy tot.
qy medio: 375.00 308.00 683.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-43	2419	75	0	231	-2155	4.02	4.02	4.02	4.02	3	0.31	0.07	0.43	0.00	0.00	22.3
2	0	-253	1584	50	0	153	-888	4.02	4.02	4.02	4.02	2	0.13	0.05	0.28	0.00	0.00	22.3
3	0	-247	1587	52	0	159	-896	4.02	4.02	4.02	4.02	2	0.13	0.05	0.28	0.00	0.00	22.3
4	0	180	2135	64	0	197	-2419	4.02	4.02	4.02	4.02	2	0.37	0.06	0.38	0.00	0.00	22.3
5	0	186	2137	66	0	203	-2427	4.02	4.02	4.02	4.02	2	0.37	0.06	0.38	0.00	0.00	22.3
6	0	-108	1773	52	0	162	-1415	4.02	4.02	4.02	4.02	2	0.21	0.05	0.31	0.00	0.00	22.3
7	0	-88	1783	60	0	181	-1441	4.02	4.02	4.02	4.02	2	0.22	0.05	0.32	0.00	0.00	22.3
8	0	22	1939	57	0	175	-1875	4.02	4.02	4.02	4.02	2	0.28	0.06	0.35	0.00	0.00	22.3
9	0	42	1948	64	0	194	-1900	4.02	4.02	4.02	4.02	2	0.29	0.06	0.35	0.00	0.00	22.3
10	0	-253	1584	50	0	153	-888	4.02	4.02	4.02	4.02	2	0.13	0.05	0.28	0.00	0.00	22.3
11	0	-247	1587	52	0	159	-896	4.02	4.02	4.02	4.02	2	0.13	0.05	0.28	0.00	0.00	22.3
12	0	180	2135	64	0	197	-2419	4.02	4.02	4.02	4.02	2	0.37	0.06	0.38	0.00	0.00	22.3
13	0	186	2137	66	0	203	-2427	4.02	4.02	4.02	4.02	2	0.37	0.06	0.38	0.00	0.00	22.3
14	0	-108	1773	52	0	162	-1415	4.02	4.02	4.02	4.02	2	0.21	0.05	0.31	0.00	0.00	22.3
15	0	-88	1783	60	0	181	-1441	4.02	4.02	4.02	4.02	2	0.22	0.05	0.32	0.00	0.00	22.3
16	0	22	1939	57	0	175	-1875	4.02	4.02	4.02	4.02	2	0.28	0.06	0.35	0.00	0.00	22.3
17	0	42	1948	64	0	194	-1900	4.02	4.02	4.02	4.02	2	0.29	0.06	0.35	0.00	0.00	22.3
18	0	-840	1638	132	0	403	838	4.02	4.02	4.02	4.02	3	0.12	0.05	0.29	0.00	0.00	22.3
19	0	546	3196	146	0	465	-4321	4.02	4.02	4.02	4.02	3	0.63	0.09	0.57	0.00	0.00	22.3
20	0	-71	2416	139	0	437	-2152	4.02	4.02	4.02	4.02	3	0.31	0.07	0.43	0.00	0.00	22.3
37	0	-1264	1120	107	0	316	2017	4.02	4.02	4.02	4.02	3	0.28	0.03	0.19	0.00	0.00	22.3
38	0	1045	3716	129	0	419	-5767	4.02	4.02	4.02	4.02	3	0.85	0.11	0.66	0.00	0.00	22.3
39	0	18	2417	118	0	372	-2152	4.02	4.02	4.02	4.02	3	0.31	0.07	0.43	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	57	-43	1917	75	0	189	-1901	4.02	4.02	4.02	4.02	3	0.27	0.06	0.34	0.00	0.00	22.3
2	57	-253	1198	50	0	125	-709	4.02	4.02	4.02	4.02	2	0.11	0.03	0.21	0.00	0.00	22.3
3	57	-247	1201	52	0	129	-716	4.02	4.02	4.02	4.02	2	0.11	0.03	0.21	0.00	0.00	22.3
4	57	180	1749	64	0	161	-2208	4.02	4.02	4.02	4.02	2	0.34	0.05	0.31	0.00	0.00	22.3
5	57	186	1751	66	0	166	-2215	4.02	4.02	4.02	4.02	2	0.34	0.05	0.31	0.00	0.00	22.3
6	57	-108	1387	52	0	132	-1224	4.02	4.02	4.02	4.02	2	0.18	0.04	0.25	0.00	0.00	22.3
7	57	-88	1397	60	0	147	-1250	4.02	4.02	4.02	4.02	2	0.19	0.04	0.25	0.00	0.00	22.3
8	57	22	1553	57	0	143	-1675	4.02	4.02	4.02	4.02	2	0.25	0.05	0.28	0.00	0.00	22.3
9	57	42	1562	64	0	158	-1699	4.02	4.02	4.02	4.02	2	0.26	0.05	0.28	0.00	0.00	22.3
10	57	-253	1198	50	0	125	-709	4.02	4.02	4.02	4.02	2	0.11	0.03	0.21	0.00	0.00	22.3
11	57	-247	1201	52	0	129	-716	4.02	4.02	4.02	4.02	2	0.11	0.03	0.21	0.00	0.00	22.3
12	57	180	1749	64	0	161	-2208	4.02	4.02	4.02	4.02	2	0.34	0.05	0.31	0.00	0.00	22.3
13	57	186	1751	66	0	166	-2215	4.02	4.02	4.02	4.02	2	0.34	0.05	0.31	0.00	0.00	22.3
14	57	-108	1387	52	0	132	-1224	4.02	4.02	4.02	4.02	2	0.18	0.04	0.25	0.00	0.00	22.3
15	57	-88	1397	60	0	147	-1250	4.02	4.02	4.02	4.02	2	0.19	0.04	0.25	0.00	0.00	22.3
16	57	22	1553	57	0	143	-1675	4.02	4.02	4.02	4.02	2	0.25	0.05	0.28	0.00	0.00	22.3
17	57	42	1562	64	0	158	-1699	4.02	4.02	4.02	4.02	2	0.26	0.05	0.28	0.00	0.00	22.3
18	57	-840	1136	132	0	328	1368	4.02	4.02	4.02	4.02	3	0.19	0.03	0.20	0.00	0.00	22.3
19	57	546	2694	146	0	382	-4021	4.02	4.02	4.02	4.02	3	0.59	0.08	0.48	0.00	0.00	22.3
20	57	-71	1914	139	0	358	-1898	4.02	4.02	4.02	4.02	3	0.27	0.06	0.34	0.00	0.00	22.3
37	57	-1264	618	107	0	256	2149	4.02	4.02	4.02	4.02	3	0.30	0.02	0.11	0.00	0.00	22.3
38	57	1045	3214	129	0	346	-5436	4.02	4.02	4.02	4.02	3	0.80	0.09	0.57	0.00	0.00	22.3
39	57	18	1915	118	0	305	-1898	4.02	4.02	4.02	4.02	3	0.27	0.06	0.34	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	113	-43	1416	75	0	146	728	4.02	4.02	4.02	4.02	3	0.10	0.04	0.25	0.00	0.00	22.3
2	113	-253	812	50	0	97	877	4.02	4.02	4.02	4.02	2	0.13	0.02	0.14	0.00	0.00	22.3
3	113	-247	815	52	0	100	874	4.02	4.02	4.02	4.02	2	0.13	0.02	0.14	0.00	0.00	22.3
4	113	180	1363	64	0	125	-1133	4.02	4.02	4.02	4.02	2	0.17	0.04	0.24	0.00	0.00	22.3
5	113	186	1365	66	0	128	-1139	4.02	4.02	4.02	4.02	2	0.17	0.04	0.24	0.00	0.00	22.3
6	113	-108	1001	52	0	103	660	4.02	4.02	4.02	4.02	2	0.10	0.03	0.18	0.00	0.00	22.3
7	113	-88	1011	60	0	114	649	4.02	4.02	4.02	4.02	2	0.10	0.03	0.18	0.00	0.00	22.3
8	113	22	1167	57	0	111	-711	4.02	4.02	4.02	4.02	2	0.11	0.03	0.21	0.00	0.00	22.3
9	113	42	1176	64	0	122	-730	4.02	4.02	4.02	4.02	2	0.11	0.03	0.21	0.00	0.00	22.3
10	113	-253	812	50	0	97	877	4.02	4.02	4.02	4.02	2	0.13	0.02	0.14	0.00	0.00	22.3
11	113	-247	815	52	0	100	874	4.02	4.02	4.02	4.02	2	0.13	0.02	0.14	0.00	0.00	22.3
12	113	180	1363	64	0	125	-1133	4.02	4.02	4.02	4.02	2	0.17	0.04	0.24	0.00	0.00	22.3
13	113	186	1365	66	0	128	-1139	4.02	4.02	4.02	4.02	2	0.17	0.04	0.24	0.00	0.00	22.3
14	113	-108	1001	52	0	103	660	4.02	4.02	4.02	4.02	2	0.10	0.03	0.18	0.00	0.00	22.3
15	113	-88	1011	60	0	114	649	4.02	4.02	4.02	4.02	2	0.10	0.03	0.18	0.00	0.00	22.3
16	113	22	1167	57	0	111	-711	4.02	4.02	4.02	4.02	2	0.11	0.03	0.21	0.00	0.00	22.3
17	113	42	1176	64	0	122	-730	4.02	4.02	4.02	4.02	2	0.11	0.03	0.21	0.00	0.00	22.3
18	113	-840	635	132	0	254	1510	4.02	4.02	4.02	4.02	3	0.21	0.02	0.11	0.00	0.00	22.3
19	113	546	2193	146	0	300	-2387	4.02	4.02	4.02	4.02	3	0.35	0.06	0.39	0.00	0.00	22.3
20	113	-71	1413	139	0	279	727	4.02	4.02	4.02	4.02	3	0.10	0.04	0.25	0.00	0.00	22.3
37	113	-1264	117	107	0	195	2149	4.02	4.02	4.02	4.02	3	0.30	0.00	0.02	0.00	0.00	22.3
38	113	1045	2713	129	0	273	-3508	4.02	4.02	4.02	4.02	3	0.52	0.08	0.48	0.00	0.00	22.3
39	113	18	1414	118	0	238	728	4.02	4.02	4.02	4.02	3	0.10	0.04	0.25	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	170	-43	914	75	0	104	1132	4.02	4.02	4.02	4.02	3	0.16	0.03	0.16	0.00	0.00	22.3
2	170	-253	426	50	0	69	947	4.02	4.02	4.02	4.02	2	0.14	0.01	0.08	0.00	0.00	22.3
3	170	-247	429	52	0	71	946	4.02	4.02	4.02	4.02	2	0.14	0.01	0.08	0.00	0.00	22.3
4	170	180	977	64	0	89	712	4.02	4.02	4.02	4.02	2	0.11	0.03	0.17	0.00	0.00	22.3
5	170	186	979	66	0	91	710	4.02	4.02	4.02	4.02	2	0.11	0.03	0.17	0.00	0.00	22.3
6	170	-108	615	52	0	73	869	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
7	170	-88	625	60	0	80	870	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3

8	170	22	781	57	0	79	825	4.02	4.02	4.02	4.02	2	0.13	0.02	0.14	0.00	0.00	22.3
9	170	42	790	64	0	86	821	4.02	4.02	4.02	4.02	2	0.12	0.02	0.14	0.00	0.00	22.3
10	170	-253	426	50	0	69	947	4.02	4.02	4.02	4.02	2	0.14	0.01	0.08	0.00	0.00	22.3
11	170	-247	429	52	0	71	946	4.02	4.02	4.02	4.02	2	0.14	0.01	0.08	0.00	0.00	22.3
12	170	180	977	64	0	89	712	4.02	4.02	4.02	4.02	2	0.11	0.03	0.17	0.00	0.00	22.3
13	170	186	979	66	0	91	710	4.02	4.02	4.02	4.02	2	0.11	0.03	0.17	0.00	0.00	22.3
14	170	-108	615	52	0	73	869	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
15	170	-88	625	60	0	80	870	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
16	170	22	781	57	0	79	825	4.02	4.02	4.02	4.02	2	0.13	0.02	0.14	0.00	0.00	22.3
17	170	42	790	64	0	86	821	4.02	4.02	4.02	4.02	2	0.12	0.02	0.14	0.00	0.00	22.3
18	170	-840	133	132	0	179	1510	4.02	4.02	4.02	4.02	3	0.21	0.00	0.02	0.00	0.00	22.3
19	170	546	1691	146	0	218	-1036	4.02	4.02	4.02	4.02	3	0.15	0.05	0.30	0.00	0.00	22.3
20	170	-71	911	139	0	201	1129	4.02	4.02	4.02	4.02	3	0.16	0.03	0.16	0.00	0.00	22.3
37	170	-1264	-385	107	0	135	2149	4.02	4.02	4.02	4.02	3	0.30	0.01	0.07	0.00	0.00	22.3
38	170	1045	2211	129	0	200	-1863	4.02	4.02	4.02	4.02	3	0.28	0.06	0.39	0.00	0.00	22.3
39	170	18	912	118	0	171	1131	4.02	4.02	4.02	4.02	3	0.16	0.03	0.16	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	226	-43	412	75	0	61	1135	4.02	4.02	4.02	4.02	3	0.16	0.01	0.07	0.00	0.00	22.3
2	226	-253	40	50	0	40	947	4.02	4.02	4.02	4.02	2	0.14	0.00	0.01	0.00	0.00	22.3
3	226	-247	43	52	0	41	946	4.02	4.02	4.02	4.02	2	0.14	0.00	0.01	0.00	0.00	22.3
4	226	180	591	64	0	52	892	4.02	4.02	4.02	4.02	2	0.14	0.02	0.11	0.00	0.00	22.3
5	226	186	593	66	0	53	894	4.02	4.02	4.02	4.02	2	0.14	0.02	0.11	0.00	0.00	22.3
6	226	-108	229	52	0	44	869	4.02	4.02	4.02	4.02	2	0.13	0.01	0.04	0.00	0.00	22.3
7	226	-88	239	60	0	47	870	4.02	4.02	4.02	4.02	2	0.13	0.01	0.04	0.00	0.00	22.3
8	226	22	395	57	0	47	876	4.02	4.02	4.02	4.02	2	0.13	0.01	0.07	0.00	0.00	22.3
9	226	42	404	64	0	50	877	4.02	4.02	4.02	4.02	2	0.13	0.01	0.07	0.00	0.00	22.3
10	226	-253	40	50	0	40	947	4.02	4.02	4.02	4.02	2	0.14	0.00	0.01	0.00	0.00	22.3
11	226	-247	43	52	0	41	946	4.02	4.02	4.02	4.02	2	0.14	0.00	0.01	0.00	0.00	22.3
12	226	180	591	64	0	52	892	4.02	4.02	4.02	4.02	2	0.14	0.02	0.11	0.00	0.00	22.3
13	226	186	593	66	0	53	894	4.02	4.02	4.02	4.02	2	0.14	0.02	0.11	0.00	0.00	22.3
14	226	-108	229	52	0	44	869	4.02	4.02	4.02	4.02	2	0.13	0.01	0.04	0.00	0.00	22.3
15	226	-88	239	60	0	47	870	4.02	4.02	4.02	4.02	2	0.13	0.01	0.04	0.00	0.00	22.3
16	226	22	395	57	0	47	876	4.02	4.02	4.02	4.02	2	0.13	0.01	0.07	0.00	0.00	22.3
17	226	42	404	64	0	50	877	4.02	4.02	4.02	4.02	2	0.13	0.01	0.07	0.00	0.00	22.3
18	226	-840	-368	133	0	104	1510	4.02	4.02	4.02	4.02	3	0.21	0.01	0.06	0.00	0.00	22.3
19	226	546	1189	146	0	136	1236	4.02	4.02	4.02	4.02	3	0.18	0.03	0.21	0.00	0.00	22.3
20	226	-71	410	139	0	122	1130	4.02	4.02	4.02	4.02	3	0.16	0.01	0.07	0.00	0.00	22.3
37	226	-1264	-886	107	0	74	2149	4.02	4.02	4.02	4.02	3	0.30	0.03	0.15	0.00	0.00	22.3
38	226	1045	1710	129	0	127	1230	4.02	4.02	4.02	4.02	3	0.18	0.05	0.30	0.00	0.00	22.3
39	226	18	410	118	0	104	1133	4.02	4.02	4.02	4.02	3	0.16	0.01	0.07	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	283	-43	-90	75	0	18	1135	4.02	4.02	4.02	4.02	3	0.16	0.00	0.02	0.00	0.00	22.3
2	283	-253	-346	50	0	12	947	4.02	4.02	4.02	4.02	2	0.14	0.01	0.06	0.00	0.00	22.3
3	283	-247	-342	52	0	12	946	4.02	4.02	4.02	4.02	2	0.14	0.01	0.06	0.00	0.00	22.3
4	283	180	206	64	0	16	892	4.02	4.02	4.02	4.02	2	0.14	0.01	0.04	0.00	0.00	22.3
5	283	186	208	66	0	16	894	4.02	4.02	4.02	4.02	2	0.14	0.01	0.04	0.00	0.00	22.3
6	283	-108	-156	52	0	14	869	4.02	4.02	4.02	4.02	2	0.13	0.00	0.03	0.00	0.00	22.3
7	283	-88	-146	60	0	13	870	4.02	4.02	4.02	4.02	2	0.13	0.00	0.03	0.00	0.00	22.3
8	283	22	10	57	0	15	876	4.02	4.02	4.02	4.02	2	0.13	0.00	0.00	0.00	0.00	22.3
9	283	42	18	64	0	14	877	4.02	4.02	4.02	4.02	2	0.13	0.00	0.00	0.00	0.00	22.3
10	283	-253	-346	50	0	12	947	4.02	4.02	4.02	4.02	2	0.14	0.01	0.06	0.00	0.00	22.3
11	283	-247	-342	52	0	12	946	4.02	4.02	4.02	4.02	2	0.14	0.01	0.06	0.00	0.00	22.3
12	283	180	206	64	0	16	892	4.02	4.02	4.02	4.02	2	0.14	0.01	0.04	0.00	0.00	22.3
13	283	186	208	66	0	16	894	4.02	4.02	4.02	4.02	2	0.14	0.01	0.04	0.00	0.00	22.3
14	283	-108	-156	52	0	14	869	4.02	4.02	4.02	4.02	2	0.13	0.00	0.03	0.00	0.00	22.3
15	283	-88	-146	60	0	13	870	4.02	4.02	4.02	4.02	2	0.13	0.00	0.03	0.00	0.00	22.3
16	283	22	10	57	0	15	876	4.02	4.02	4.02	4.02	2	0.13	0.00	0.00	0.00	0.00	22.3
17	283	42	18	64	0	14	877	4.02	4.02	4.02	4.02	2	0.13	0.00	0.00	0.00	0.00	22.3
18	283	-840	-870	132	0	29	1510	4.02	4.02	4.02	4.02	3	0.21	0.03	0.15	0.00	0.00	22.3
19	283	546	688	146	0	53	1410	4.02	4.02	4.02	4.02	3	0.21	0.02	0.12	0.00	0.00	22.3
20	283	-71	-92	139	0	43	1130	4.02	4.02	4.02	4.02	3	0.16	0.00	0.02	0.00	0.00	22.3
37	283	-1264	-1388	107	0	14	1775	4.02	4.02	4.02	4.02	3	0.25	0.04	0.24	0.00	0.00	22.3
38	283	1045	1208	129	0	54	1800	4.02	4.02	4.02	4.02	3	0.27	0.04	0.22	0.00	0.00	22.3
39	283	18	-92	118	0	37	1133	4.02	4.02	4.02	4.02	3	0.16	0.00	0.02	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	339	-43	-591	75	0	-24	1135	4.02	4.02	4.02	4.02	3	0.16	0.02	0.11	0.00	0.00	22.3
2	339	-253	-731	50	0	-16	927	4.02	4.02	4.02	4.02	2	0.14	0.02	0.13	0.00	0.00	22.3
3	339	-247	-728	52	0	-17	928	4.02	4.02	4.02	4.02	2	0.14	0.02	0.13	0.00	0.00	22.3
4	339	180	-180	64	0	-20	892	4.02	4.02	4.02	4.02	2	0.14	0.01	0.03	0.00	0.00	22.3
5	339	186	-178	66	0	-22	894	4.02	4.02	4.02	4.02	2	0.14	0.01	0.03	0.00	0.00	22.3
6	339	-108	-542	52	0	-16	869	4.02	4.02	4.02	4.02	2	0.13	0.02	0.10	0.00	0.00	22.3
7	339	-88	-532	60	0	-21	870	4.02	4.02	4.02	4.02	2	0.13	0.02	0.09	0.00	0.00	22.3
8	339	22	-376	57	0	-17	876	4.02	4.02	4.02	4.02	2	0.13	0.01	0.07	0.00	0.00	22.3
9	339	42	-367	64	0	-22	877	4.02	4.02	4.02	4.02	2	0.13	0.01	0.07	0.00	0.00	22.3
10	339	-253	-731	50	0	-16	927	4.02	4.02	4.02	4.02	2	0.14	0.02	0.13	0.00	0.00	22.3
11	339	-247	-728	52	0	-17	928	4.02	4.02	4.02	4.02	2	0.14	0.02	0.13	0.00	0.00	22.3
12	339	180	-180	64	0	-20	892	4.02	4.02	4.02	4.02	2	0.14	0.01	0.03	0.00	0.00	22.3
13	339	186	-178	66	0	-22	894	4.02	4.02	4.02	4.02	2	0.14	0.01	0.03	0.00	0.00	22.3
14	339	-108	-542	52	0	-16	869	4.02	4.02	4.02	4.02	2	0.13	0.02	0.10	0.00	0.00	22.3
15	339	-88	-532	60	0	-21	870	4.02	4.02	4.02	4.02	2	0.13	0.02	0.09	0.00	0.00	22.3
16	339	22	-376	57	0	-17	876	4.02	4.02	4.02	4.02	2	0.13	0.01	0.07	0.00	0.00	22.3
17	339	42	-367	64	0	-22	877	4.02	4.02	4.02	4.02	2	0.13	0.01	0.07	0.00	0.00	22.3
18	339	-840	-1372	132	0	-46	1155	4.02	4.02	4.02	4.02	3	0.16	0.04	0.24	0.00	0.00	22.3
19	339	546	186	146	0	-29	1410	4.02	4.02	4.02	4.02	3	0.21	0.01	0.03	0.00	0.00	22.3
20	339	-71	-594	139	0	-35	1130	4.02	4.02	4.02	4.02	3	0.16	0.02	0.11	0.00	0.00	22.3
37	339	-1264	-1890	107	0	-47	1103	4.02	4.02	4.02	4.02	3	0.15	0.05	0.33	0.00	0.00	22.3
38	339	1045	706	129	0	-19	1987	4.02	4.02	4.02	4.02	3	0.29	0.02	0.13	0.00	0.00	22.3
39	339	18	-593	118	0	-30	1133	4.02	4.02	4.02	4.02	3	0.16	0.02	0.11	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	396	-43	-1093	75	0	-67	1020	4.02	4.02	4.02	4.02	3	0.15	0.03	0.19	0.00	0.00	22.3
2	396	-253	-1117	50	0	-44	600	4.02	4.02	4.02	4.02	2	0.09	0.03	0.20	0.00	0.00	22.3
3	396	-247	-1114	52	0	-47	602	4.02	4.02	4.02	4.02	2	0.09	0.03	0.20	0.00	0.00	22.3
4	396	180	-566	64	0	-56	892	4.02	4.02	4.02	4.02	2	0.14	0.02	0.10	0.00	0.00	22.3
5	396	186	-564	66	0	-59	894	4.02	4.02	4.02	4.02	2	0.14	0.02	0.10	0.00	0.00	22.3
6	396	-108	-928	52	0	-45	727	4.02	4.02	4.02	4.02	2	0.11	0.03	0.16	0.00	0.00	22.3
7	396	-88	-918	60	0	-54	733	4.02	4.02	4.02	4.02	2	0.11	0.03	0.16	0.00	0.00	22.3
8	396	22	-762	57	0	-49	837	4.02	4.02	4.02	4.02	2	0.13	0.02	0.14	0.00	0.00	22.3
9	396	42	-753	64	0	-58	843	4.02	4.02	4.02	4.02	2	0.13	0.02	0.13	0.00	0.00	22.3
10	396	-253	-1117	50	0	-44	600	4.02	4.02	4.02	4.02	2	0.09	0.03	0.20	0.00	0.00	22.3
11	396	-247	-1114	52	0	-47	602	4.02	4.02	4.02	4.02	2	0.09	0.03	0.20	0.00	0.00	22.3
12	396	180	-566	64	0	-56	892	4.02	4.02	4.02	4.02	2	0.14	0.02	0.10	0.00	0.00	22.3
13	396	186	-564	66	0	-59	894	4.02	4.02	4.02	4.02	2	0.14	0.02	0.10	0.00	0.00	22.3

14	396	-108	-928	52	0	-45	727	4.02	4.02	4.02	4.02	2	0.11	0.03	0.16	0.00	0.00	22.3
15	396	-88	-918	60	0	-54	733	4.02	4.02	4.02	4.02	2	0.11	0.03	0.16	0.00	0.00	22.3
16	396	22	-762	57	0	-49	837	4.02	4.02	4.02	4.02	2	0.13	0.02	0.14	0.00	0.00	22.3
17	396	42	-753	64	0	-58	843	4.02	4.02	4.02	4.02	2	0.13	0.02	0.13	0.00	0.00	22.3
18	396	-840	-1873	133	0	-121	-1404	4.02	4.02	4.02	4.02	3	0.20	0.05	0.33	0.00	0.00	22.3
19	396	546	-316	146	0	-111	1410	4.02	4.02	4.02	4.02	3	0.21	0.01	0.06	0.00	0.00	22.3
20	396	-71	-1095	139	0	-114	1014	4.02	4.02	4.02	4.02	3	0.15	0.03	0.19	0.00	0.00	22.3
37	396	-1264	-2391	107	0	-108	-2273	4.02	4.02	4.02	4.02	3	0.31	0.07	0.41	0.00	0.00	22.3
38	396	1045	205	129	0	-92	1987	4.02	4.02	4.02	4.02	3	0.29	0.01	0.04	0.00	0.00	22.3
39	396	18	-1095	118	0	-97	1018	4.02	4.02	4.02	4.02	3	0.15	0.03	0.20	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	452	-43	-1595	75	0	-110	-1100	4.02	4.02	4.02	4.02	3	0.16	0.05	0.28	0.00	0.00	22.3
2	452	-253	-1503	50	0	-72	-1467	4.02	4.02	4.02	4.02	2	0.22	0.04	0.27	0.00	0.00	22.3
3	452	-247	-1500	52	0	-76	-1460	4.02	4.02	4.02	4.02	2	0.22	0.04	0.27	0.00	0.00	22.3
4	452	180	-952	64	0	-93	734	4.02	4.02	4.02	4.02	2	0.11	0.03	0.17	0.00	0.00	22.3
5	452	186	-950	66	0	-97	737	4.02	4.02	4.02	4.02	2	0.11	0.03	0.17	0.00	0.00	22.3
6	452	-108	-1314	52	0	-75	-1042	4.02	4.02	4.02	4.02	2	0.16	0.04	0.23	0.00	0.00	22.3
7	452	-88	-1304	60	0	-88	-1020	4.02	4.02	4.02	4.02	2	0.15	0.04	0.23	0.00	0.00	22.3
8	452	22	-1148	57	0	-81	-670	4.02	4.02	4.02	4.02	2	0.10	0.03	0.20	0.00	0.00	22.3
9	452	42	-1139	64	0	-94	-649	4.02	4.02	4.02	4.02	2	0.10	0.03	0.20	0.00	0.00	22.3
10	452	-253	-1503	50	0	-72	-1467	4.02	4.02	4.02	4.02	2	0.22	0.04	0.27	0.00	0.00	22.3
11	452	-247	-1500	52	0	-76	-1460	4.02	4.02	4.02	4.02	2	0.22	0.04	0.27	0.00	0.00	22.3
12	452	180	-952	64	0	-93	734	4.02	4.02	4.02	4.02	2	0.11	0.03	0.17	0.00	0.00	22.3
13	452	186	-950	66	0	-97	737	4.02	4.02	4.02	4.02	2	0.11	0.03	0.17	0.00	0.00	22.3
14	452	-108	-1314	52	0	-75	-1042	4.02	4.02	4.02	4.02	2	0.16	0.04	0.23	0.00	0.00	22.3
15	452	-88	-1304	60	0	-88	-1020	4.02	4.02	4.02	4.02	2	0.15	0.04	0.23	0.00	0.00	22.3
16	452	22	-1148	57	0	-81	-670	4.02	4.02	4.02	4.02	2	0.10	0.03	0.20	0.00	0.00	22.3
17	452	42	-1139	64	0	-94	-649	4.02	4.02	4.02	4.02	2	0.10	0.03	0.20	0.00	0.00	22.3
18	452	-840	-2375	132	0	-196	-2859	4.02	4.02	4.02	4.02	3	0.40	0.07	0.41	0.00	0.00	22.3
19	452	546	-818	146	0	-193	1410	4.02	4.02	4.02	4.02	3	0.21	0.02	0.15	0.00	0.00	22.3
20	452	-71	-1597	139	0	-193	-1110	4.02	4.02	4.02	4.02	3	0.16	0.05	0.28	0.00	0.00	22.3
37	452	-1264	-2893	107	0	-168	-4020	4.02	4.02	4.02	4.02	3	0.56	0.08	0.50	0.00	0.00	22.3
38	452	1045	-297	129	0	-165	1987	4.02	4.02	4.02	4.02	3	0.29	0.01	0.05	0.00	0.00	22.3
39	452	18	-1597	118	0	-164	-1105	4.02	4.02	4.02	4.02	3	0.16	0.05	0.28	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	509	-43	-2096	75	0	-152	-2396	4.02	4.02	4.02	4.02	3	0.34	0.06	0.37	0.00	0.00	22.3
2	509	-253	-1889	50	0	-100	-2621	4.02	4.02	4.02	4.02	2	0.39	0.05	0.33	0.00	0.00	22.3
3	509	-247	-1886	52	0	-105	-2612	4.02	4.02	4.02	4.02	2	0.39	0.05	0.33	0.00	0.00	22.3
4	509	180	-1338	64	0	-129	-1073	4.02	4.02	4.02	4.02	2	0.16	0.04	0.24	0.00	0.00	22.3
5	509	186	-1336	66	0	-134	-1066	4.02	4.02	4.02	4.02	2	0.16	0.04	0.24	0.00	0.00	22.3
6	509	-108	-1700	52	0	-104	-2088	4.02	4.02	4.02	4.02	2	0.32	0.05	0.30	0.00	0.00	22.3
7	509	-88	-1690	60	0	-122	-2062	4.02	4.02	4.02	4.02	2	0.31	0.05	0.30	0.00	0.00	22.3
8	509	22	-1534	57	0	-113	-1624	4.02	4.02	4.02	4.02	2	0.25	0.04	0.27	0.00	0.00	22.3
9	509	42	-1525	64	0	-130	-1597	4.02	4.02	4.02	4.02	2	0.24	0.04	0.27	0.00	0.00	22.3
10	509	-253	-1889	50	0	-100	-2621	4.02	4.02	4.02	4.02	2	0.39	0.05	0.33	0.00	0.00	22.3
11	509	-247	-1886	52	0	-105	-2612	4.02	4.02	4.02	4.02	2	0.39	0.05	0.33	0.00	0.00	22.3
12	509	180	-1338	64	0	-129	-1073	4.02	4.02	4.02	4.02	2	0.16	0.04	0.24	0.00	0.00	22.3
13	509	186	-1336	66	0	-134	-1066	4.02	4.02	4.02	4.02	2	0.16	0.04	0.24	0.00	0.00	22.3
14	509	-108	-1700	52	0	-104	-2088	4.02	4.02	4.02	4.02	2	0.32	0.05	0.30	0.00	0.00	22.3
15	509	-88	-1690	60	0	-122	-2062	4.02	4.02	4.02	4.02	2	0.31	0.05	0.30	0.00	0.00	22.3
16	509	22	-1534	57	0	-113	-1624	4.02	4.02	4.02	4.02	2	0.25	0.04	0.27	0.00	0.00	22.3
17	509	42	-1525	64	0	-130	-1597	4.02	4.02	4.02	4.02	2	0.24	0.04	0.27	0.00	0.00	22.3
18	509	-840	-2876	133	0	-271	-4596	4.02	4.02	4.02	4.02	3	0.64	0.08	0.50	0.00	0.00	22.3
19	509	546	-1319	146	0	-276	1118	4.02	4.02	4.02	4.02	3	0.16	0.04	0.23	0.00	0.00	22.3
20	509	-71	-2098	139	0	-272	-2408	4.02	4.02	4.02	4.02	3	0.34	0.06	0.37	0.00	0.00	22.3
37	509	-1264	-3394	107	0	-229	-6050	4.02	4.02	4.02	4.02	3	0.84	0.10	0.59	0.00	0.00	22.3
38	509	1045	-798	129	0	-237	1987	4.02	4.02	4.02	4.02	3	0.29	0.02	0.14	0.00	0.00	22.3
39	509	18	-2098	118	0	-230	-2402	4.02	4.02	4.02	4.02	3	0.34	0.06	0.37	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	565	-43	-2598	75	0	-195	-2661	4.02	4.02	4.02	4.02	3	0.38	0.08	0.46	0.00	0.00	22.3
2	565	-253	-2275	50	0	-128	-2841	4.02	4.02	4.02	4.02	2	0.43	0.07	0.40	0.00	0.00	22.3
3	565	-247	-2272	52	0	-135	-2832	4.02	4.02	4.02	4.02	2	0.43	0.07	0.40	0.00	0.00	22.3
4	565	180	-1724	64	0	-165	-1261	4.02	4.02	4.02	4.02	2	0.19	0.05	0.31	0.00	0.00	22.3
5	565	186	-1722	66	0	-172	-1253	4.02	4.02	4.02	4.02	2	0.19	0.05	0.31	0.00	0.00	22.3
6	565	-108	-2086	52	0	-134	-2297	4.02	4.02	4.02	4.02	2	0.35	0.06	0.37	0.00	0.00	22.3
7	565	-88	-2076	60	0	-155	-2270	4.02	4.02	4.02	4.02	2	0.34	0.06	0.37	0.00	0.00	22.3
8	565	22	-1920	57	0	-145	-1823	4.02	4.02	4.02	4.02	2	0.28	0.06	0.34	0.00	0.00	22.3
9	565	42	-1911	64	0	-166	-1796	4.02	4.02	4.02	4.02	2	0.27	0.06	0.34	0.00	0.00	22.3
10	565	-253	-2275	50	0	-128	-2841	4.02	4.02	4.02	4.02	2	0.43	0.07	0.40	0.00	0.00	22.3
11	565	-247	-2272	52	0	-135	-2832	4.02	4.02	4.02	4.02	2	0.43	0.07	0.40	0.00	0.00	22.3
12	565	180	-1724	64	0	-165	-1261	4.02	4.02	4.02	4.02	2	0.19	0.05	0.31	0.00	0.00	22.3
13	565	186	-1722	66	0	-172	-1253	4.02	4.02	4.02	4.02	2	0.19	0.05	0.31	0.00	0.00	22.3
14	565	-108	-2086	52	0	-134	-2297	4.02	4.02	4.02	4.02	2	0.35	0.06	0.37	0.00	0.00	22.3
15	565	-88	-2076	60	0	-155	-2270	4.02	4.02	4.02	4.02	2	0.34	0.06	0.37	0.00	0.00	22.3
16	565	22	-1920	57	0	-145	-1823	4.02	4.02	4.02	4.02	2	0.28	0.06	0.34	0.00	0.00	22.3
17	565	42	-1911	64	0	-166	-1796	4.02	4.02	4.02	4.02	2	0.27	0.06	0.34	0.00	0.00	22.3
18	565	-840	-3378	132	0	-345	-4907	4.02	4.02	4.02	4.02	3	0.69	0.10	0.59	0.00	0.00	22.3
19	565	546	-1821	146	0	-358	-437	4.02	4.02	4.02	4.02	3	0.09	0.05	0.32	0.00	0.00	22.3
20	565	-71	-2600	139	0	-350	-2673	4.02	4.02	4.02	4.02	3	0.38	0.08	0.46	0.00	0.00	22.3
37	565	-1264	-3896	107	0	-289	-6391	4.02	4.02	4.02	4.02	3	0.88	0.11	0.67	0.00	0.00	22.3
38	565	1045	-1300	129	0	-310	1716	4.02	4.02	4.02	4.02	3	0.25	0.04	0.23	0.00	0.00	22.3
39	565	18	-2600	118	0	-297	-2667	4.02	4.02	4.02	4.02	3	0.38	0.08	0.46	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

Nome travata: **trave_502_IP1** Descrizione: **Trave_5 10-15-20-25**
ASTA NUM. 6 NI 298 NF 264 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y Permanente qy tot.
qy medio: 375.00 308.00 683.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-491	2750	22	0	48	-2734	4.02	4.02	4.02	4.02	3	0.39	0.08	0.48	0.00	0.00	22.3
2	0	-672	1871	-0	0	-8	-1393	4.02	4.02	4.02	4.02	2	0.21	0.05	0.33	0.00	0.00	22.3
3	0	-673	1872	10	0	20	-1396	4.02	4.02	4.02	4.02	2	0.21	0.05	0.33	0.00	0.00	22.3
4	0	-82	2359	24	0	53	-2810	4.02	4.02	4.02	4.02	2	0.42	0.07	0.42	0.00	0.00	22.3
5	0	-83	2360	34	0	81	-2813	4.02	4.02	4.02	4.02	2	0.43	0.07	0.42	0.00	0.00	22.3

6	0	-464	2041	-3	0	-19	-1886	4.02	4.02	4.02	4.02	2	0.28	0.06	0.36	0.00	0.00	22.3
7	0	-468	2044	30	0	74	-1896	4.02	4.02	4.02	4.02	2	0.28	0.06	0.36	0.00	0.00	22.3
8	0	-287	2187	4	0	-1	-2311	4.02	4.02	4.02	4.02	2	0.35	0.06	0.39	0.00	0.00	22.3
9	0	-291	2190	37	0	92	-2321	4.02	4.02	4.02	4.02	2	0.35	0.06	0.39	0.00	0.00	22.3
10	0	-672	1871	-0	0	-8	-1393	4.02	4.02	4.02	4.02	2	0.21	0.05	0.33	0.00	0.00	22.3
11	0	-673	1872	10	0	20	-1396	4.02	4.02	4.02	4.02	2	0.21	0.05	0.33	0.00	0.00	22.3
12	0	-82	2359	24	0	53	-2810	4.02	4.02	4.02	4.02	2	0.42	0.07	0.42	0.00	0.00	22.3
13	0	-83	2360	34	0	81	-2813	4.02	4.02	4.02	4.02	2	0.43	0.07	0.42	0.00	0.00	22.3
14	0	-464	2041	-3	0	-19	-1886	4.02	4.02	4.02	4.02	2	0.28	0.06	0.36	0.00	0.00	22.3
15	0	-468	2044	30	0	74	-1896	4.02	4.02	4.02	4.02	2	0.28	0.06	0.36	0.00	0.00	22.3
16	0	-287	2187	4	0	-1	-2311	4.02	4.02	4.02	4.02	2	0.35	0.06	0.39	0.00	0.00	22.3
17	0	-291	2190	37	0	92	-2321	4.02	4.02	4.02	4.02	2	0.35	0.06	0.39	0.00	0.00	22.3
18	0	-1798	2109	10	0	13	-866	4.02	4.02	4.02	4.02	3	0.12	0.06	0.36	0.00	0.00	22.3
19	0	-528	3496	68	0	144	-4862	4.02	4.02	4.02	4.02	3	0.69	0.10	0.61	0.00	0.00	22.3
20	0	-1064	2791	83	0	204	-2834	4.02	4.02	4.02	4.02	3	0.39	0.08	0.48	0.00	0.00	22.3
37	0	-1999	1630	-14	0	-41	1331	4.02	4.02	4.02	4.02	3	0.18	0.05	0.28	0.00	0.00	22.3
38	0	119	3942	82	0	178	-6154	4.02	4.02	4.02	4.02	3	0.89	0.11	0.70	0.00	0.00	22.3
39	0	-775	2766	107	0	278	-2774	4.02	4.02	4.02	4.02	3	0.39	0.08	0.48	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	56	-491	2248	22	0	35	-2460	4.02	4.02	4.02	4.02	3	0.35	0.07	0.40	0.00	0.00	22.3
2	56	-672	1485	-0	0	-8	-1197	4.02	4.02	4.02	4.02	2	0.18	0.04	0.26	0.00	0.00	22.3
3	56	-673	1486	10	0	15	-1200	4.02	4.02	4.02	4.02	2	0.18	0.04	0.26	0.00	0.00	22.3
4	56	-82	1973	24	0	39	-2585	4.02	4.02	4.02	4.02	2	0.39	0.06	0.35	0.00	0.00	22.3
5	56	-83	1974	34	0	62	-2588	4.02	4.02	4.02	4.02	2	0.39	0.06	0.35	0.00	0.00	22.3
6	56	-464	1655	-3	0	-17	-1680	4.02	4.02	4.02	4.02	2	0.25	0.05	0.29	0.00	0.00	22.3
7	56	-468	1658	30	0	57	-1690	4.02	4.02	4.02	4.02	2	0.25	0.05	0.29	0.00	0.00	22.3
8	56	-287	1801	4	0	-3	-2096	4.02	4.02	4.02	4.02	2	0.32	0.05	0.32	0.00	0.00	22.3
9	56	-291	1804	37	0	71	-2106	4.02	4.02	4.02	4.02	2	0.32	0.05	0.32	0.00	0.00	22.3
10	56	-672	1485	-0	0	-8	-1197	4.02	4.02	4.02	4.02	2	0.18	0.04	0.26	0.00	0.00	22.3
11	56	-673	1486	10	0	15	-1200	4.02	4.02	4.02	4.02	2	0.18	0.04	0.26	0.00	0.00	22.3
12	56	-82	1973	24	0	39	-2585	4.02	4.02	4.02	4.02	2	0.39	0.06	0.35	0.00	0.00	22.3
13	56	-83	1974	34	0	62	-2588	4.02	4.02	4.02	4.02	2	0.39	0.06	0.35	0.00	0.00	22.3
14	56	-464	1655	-3	0	-17	-1680	4.02	4.02	4.02	4.02	2	0.25	0.05	0.29	0.00	0.00	22.3
15	56	-468	1658	30	0	57	-1690	4.02	4.02	4.02	4.02	2	0.25	0.05	0.29	0.00	0.00	22.3
16	56	-287	1801	4	0	-3	-2096	4.02	4.02	4.02	4.02	2	0.32	0.05	0.32	0.00	0.00	22.3
17	56	-291	1804	37	0	71	-2106	4.02	4.02	4.02	4.02	2	0.32	0.05	0.32	0.00	0.00	22.3
18	56	-1798	1607	10	0	7	998	4.02	4.02	4.02	4.02	3	0.14	0.05	0.27	0.00	0.00	22.3
19	56	-528	2994	68	0	105	-4544	4.02	4.02	4.02	4.02	3	0.64	0.09	0.53	0.00	0.00	22.3
20	56	-1064	2289	83	0	157	-2558	4.02	4.02	4.02	4.02	3	0.36	0.07	0.40	0.00	0.00	22.3
37	56	-1999	1128	-14	0	-33	1856	4.02	4.02	4.02	4.02	3	0.25	0.03	0.19	0.00	0.00	22.3
38	56	119	3440	82	0	132	-5810	4.02	4.02	4.02	4.02	3	0.84	0.10	0.61	0.00	0.00	22.3
39	56	-775	2264	107	0	217	-2499	4.02	4.02	4.02	4.02	3	0.35	0.07	0.40	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	113	-491	1747	22	0	23	-1077	4.02	4.02	4.02	4.02	3	0.15	0.05	0.31	0.00	0.00	22.3
2	113	-672	1099	-0	0	-7	842	4.02	4.02	4.02	4.02	2	0.13	0.03	0.19	0.00	0.00	22.3
3	113	-673	1100	10	0	9	840	4.02	4.02	4.02	4.02	2	0.12	0.03	0.19	0.00	0.00	22.3
4	113	-82	1587	24	0	26	-1384	4.02	4.02	4.02	4.02	2	0.21	0.05	0.28	0.00	0.00	22.3
5	113	-83	1588	34	0	42	-1386	4.02	4.02	4.02	4.02	2	0.21	0.05	0.28	0.00	0.00	22.3
6	113	-464	1269	-3	0	-15	-658	4.02	4.02	4.02	4.02	2	0.10	0.04	0.22	0.00	0.00	22.3
7	113	-468	1272	30	0	40	-667	4.02	4.02	4.02	4.02	2	0.10	0.04	0.22	0.00	0.00	22.3
8	113	-287	1415	4	0	-6	-992	4.02	4.02	4.02	4.02	2	0.15	0.04	0.25	0.00	0.00	22.3
9	113	-291	1418	37	0	50	-1000	4.02	4.02	4.02	4.02	2	0.15	0.04	0.25	0.00	0.00	22.3
10	113	-672	1099	-0	0	-7	842	4.02	4.02	4.02	4.02	2	0.13	0.03	0.19	0.00	0.00	22.3
11	113	-673	1100	10	0	9	840	4.02	4.02	4.02	4.02	2	0.12	0.03	0.19	0.00	0.00	22.3
12	113	-82	1587	24	0	26	-1384	4.02	4.02	4.02	4.02	2	0.21	0.05	0.28	0.00	0.00	22.3
13	113	-83	1588	34	0	42	-1386	4.02	4.02	4.02	4.02	2	0.21	0.05	0.28	0.00	0.00	22.3
14	113	-464	1269	-3	0	-15	-658	4.02	4.02	4.02	4.02	2	0.10	0.04	0.22	0.00	0.00	22.3
15	113	-468	1272	30	0	40	-667	4.02	4.02	4.02	4.02	2	0.10	0.04	0.22	0.00	0.00	22.3
16	113	-287	1415	4	0	-6	-992	4.02	4.02	4.02	4.02	2	0.15	0.04	0.25	0.00	0.00	22.3
17	113	-291	1418	37	0	50	-1000	4.02	4.02	4.02	4.02	2	0.15	0.04	0.25	0.00	0.00	22.3
18	113	-1798	1106	10	0	1	1510	4.02	4.02	4.02	4.02	3	0.21	0.03	0.19	0.00	0.00	22.3
19	113	-528	2493	68	0	67	-2740	4.02	4.02	4.02	4.02	3	0.39	0.07	0.44	0.00	0.00	22.3
20	113	-1064	1788	83	0	110	-1152	4.02	4.02	4.02	4.02	3	0.16	0.05	0.31	0.00	0.00	22.3
37	113	-1999	627	-14	0	-25	1993	4.02	4.02	4.02	4.02	3	0.27	0.02	0.11	0.00	0.00	22.3
38	113	119	2939	82	0	86	-3754	4.02	4.02	4.02	4.02	3	0.54	0.09	0.52	0.00	0.00	22.3
39	113	-775	1763	107	0	156	-1107	4.02	4.02	4.02	4.02	3	0.16	0.05	0.31	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	169	-491	1245	22	0	10	1283	4.02	4.02	4.02	4.02	3	0.18	0.04	0.22	0.00	0.00	22.3
2	169	-672	713	-0	0	-7	1158	4.02	4.02	4.02	4.02	2	0.17	0.02	0.13	0.00	0.00	22.3
3	169	-673	714	10	0	4	1157	4.02	4.02	4.02	4.02	2	0.17	0.02	0.13	0.00	0.00	22.3
4	169	-82	1201	24	0	12	816	4.02	4.02	4.02	4.02	2	0.12	0.03	0.21	0.00	0.00	22.3
5	169	-83	1202	34	0	23	815	4.02	4.02	4.02	4.02	2	0.12	0.03	0.21	0.00	0.00	22.3
6	169	-464	883	-3	0	-14	1039	4.02	4.02	4.02	4.02	2	0.16	0.03	0.16	0.00	0.00	22.3
7	169	-468	886	30	0	24	1036	4.02	4.02	4.02	4.02	2	0.15	0.03	0.16	0.00	0.00	22.3
8	169	-287	1029	4	0	-8	937	4.02	4.02	4.02	4.02	2	0.14	0.03	0.18	0.00	0.00	22.3
9	169	-291	1032	37	0	29	933	4.02	4.02	4.02	4.02	2	0.14	0.03	0.18	0.00	0.00	22.3
10	169	-672	713	-0	0	-7	1158	4.02	4.02	4.02	4.02	2	0.17	0.02	0.13	0.00	0.00	22.3
11	169	-673	714	10	0	4	1157	4.02	4.02	4.02	4.02	2	0.17	0.02	0.13	0.00	0.00	22.3
12	169	-82	1201	24	0	12	816	4.02	4.02	4.02	4.02	2	0.12	0.03	0.21	0.00	0.00	22.3
13	169	-83	1202	34	0	23	815	4.02	4.02	4.02	4.02	2	0.12	0.03	0.21	0.00	0.00	22.3
14	169	-464	883	-3	0	-14	1039	4.02	4.02	4.02	4.02	2	0.16	0.03	0.16	0.00	0.00	22.3
15	169	-468	886	30	0	24	1036	4.02	4.02	4.02	4.02	2	0.15	0.03	0.16	0.00	0.00	22.3
16	169	-287	1029	4	0	-8	937	4.02	4.02	4.02	4.02	2	0.14	0.03	0.18	0.00	0.00	22.3
17	169	-291	1032	37	0	29	933	4.02	4.02	4.02	4.02	2	0.14	0.03	0.18	0.00	0.00	22.3
18	169	-1798	604	10	0	-5	1632	4.02	4.02	4.02	4.02	3	0.22	0.02	0.10	0.00	0.00	22.3
19	169	-528	1991	68	0	29	-1220	4.02	4.02	4.02	4.02	3	0.17	0.06	0.35	0.00	0.00	22.3
20	169	-1064	1286	83	0	62	1272	4.02	4.02	4.02	4.02	3	0.18	0.04	0.22	0.00	0.00	22.3
37	169	-1999	125	-14	0	-17	1993	4.02	4.02	4.02	4.02	3	0.27	0.00	0.02	0.00	0.00	22.3
38	169	119	2437	82	0	40	-1981	4.02	4.02	4.02	4.02	3	0.29	0.07	0.43	0.00	0.00	22.3
39	169	-775	1261	107	0	96	1278	4.02	4.02	4.02	4.02	3	0.18	0.04	0.22	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	226	-491	744	22	0	-2	1492	4.02	4.02	4.02	4.02	3	0.21	0.02	0.13	0.00	0.00	22.3
2	226	-672	327	-0	0	-7	1167	4.02	4.02	4.02	4.02	2	0.17	0.01	0.06	0.00	0.00	22.3
3	226	-673	328	10	0	-2	1166	4.02	4.02	4.02	4.02	2	0.17	0.01	0.06	0.00	0.00	22.3
4	226	-82	815	24	0	-2	1191	4.02	4.02	4.02	4.02	2	0.18	0.02	0.14	0.00	0.00	22.3
5	226	-83	816	34	0	4	1190	4.02	4.02	4.02	4.02	2	0.18	0.02	0.15	0.00	0.00	22.3
6	226	-464	497	-3	0	-12	1154	4.02	4.02	4.02	4.02	2	0.17	0.01	0.09	0.00	0.00	22.3
7	226	-468	500	30	0	7	1152	4.02	4.02	4.02	4.02	2	0.17	0.01	0.09	0.00	0.00	22.3
8	226	-287	643	4	0	-10	1180	4.02	4.02	4.02	4.02	2	0.18	0.02	0.11	0.00	0.00	22.3
9	226	-291	646	37	0	8	1180	4.02	4.02	4.02	4.02	2	0.18	0.02	0.11	0.00	0.00	22.3
10	226	-672	327	-0	0	-7	1167	4.02	4.02	4.02	4.02	2	0.17	0.01	0.06	0.00	0.00	22.3
11	226	-673	328	10	0	-2	1166	4.02	4.02	4.02	4.02	2	0.17	0.01	0.06	0.00	0.00	22.3

12	226	-82	815	24	0	-2	1191	4.02	4.02	4.02	4.02	2	0.18	0.02	0.14	0.00	0.00	22.3
13	226	-83	816	34	0	4	1190	4.02	4.02	4.02	4.02	2	0.18	0.02	0.15	0.00	0.00	22.3
14	226	-464	497	-3	0	-12	1154	4.02	4.02	4.02	4.02	2	0.17	0.01	0.09	0.00	0.00	22.3
15	226	-468	500	30	0	7	1152	4.02	4.02	4.02	4.02	2	0.17	0.01	0.09	0.00	0.00	22.3
16	226	-287	643	4	0	-10	1180	4.02	4.02	4.02	4.02	2	0.18	0.02	0.11	0.00	0.00	22.3
17	226	-291	646	37	0	8	1180	4.02	4.02	4.02	4.02	2	0.18	0.02	0.11	0.00	0.00	22.3
18	226	-1798	102	10	0	-11	1632	4.02	4.02	4.02	4.02	3	0.22	0.00	0.02	0.00	0.00	22.3
19	226	-528	1489	68	0	-10	1525	4.02	4.02	4.02	4.02	3	0.22	0.04	0.26	0.00	0.00	22.3
20	226	-1064	784	83	0	15	1524	4.02	4.02	4.02	4.02	3	0.21	0.02	0.14	0.00	0.00	22.3
37	226	-1999	-377	-14	0	-9	1993	4.02	4.02	4.02	4.02	3	0.27	0.01	0.06	0.00	0.00	22.3
38	226	119	1935	82	0	-7	1467	4.02	4.02	4.02	4.02	3	0.21	0.06	0.34	0.00	0.00	22.3
39	226	-775	760	107	0	35	1502	4.02	4.02	4.02	4.02	3	0.21	0.02	0.13	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	282	-491	242	22	0	-15	1492	4.02	4.02	4.02	4.02	3	0.21	0.01	0.04	0.00	0.00	22.3
2	282	-672	-58	-0	0	-7	1167	4.02	4.02	4.02	4.02	2	0.17	0.00	0.01	0.00	0.00	22.3
3	282	-673	-58	10	0	-7	1166	4.02	4.02	4.02	4.02	2	0.17	0.00	0.01	0.00	0.00	22.3
4	282	-82	429	24	0	-15	1263	4.02	4.02	4.02	4.02	2	0.19	0.01	0.08	0.00	0.00	22.3
5	282	-83	430	34	0	-15	1263	4.02	4.02	4.02	4.02	2	0.19	0.01	0.08	0.00	0.00	22.3
6	282	-464	112	-3	0	-10	1154	4.02	4.02	4.02	4.02	2	0.17	0.00	0.02	0.00	0.00	22.3
7	282	-468	114	30	0	-10	1152	4.02	4.02	4.02	4.02	2	0.17	0.00	0.02	0.00	0.00	22.3
8	282	-287	257	4	0	-12	1180	4.02	4.02	4.02	4.02	2	0.18	0.01	0.05	0.00	0.00	22.3
9	282	-291	260	37	0	-13	1180	4.02	4.02	4.02	4.02	2	0.18	0.01	0.05	0.00	0.00	22.3
10	282	-672	-58	-0	0	-7	1167	4.02	4.02	4.02	4.02	2	0.17	0.00	0.01	0.00	0.00	22.3
11	282	-673	-58	10	0	-7	1166	4.02	4.02	4.02	4.02	2	0.17	0.00	0.01	0.00	0.00	22.3
12	282	-82	429	24	0	-15	1263	4.02	4.02	4.02	4.02	2	0.19	0.01	0.08	0.00	0.00	22.3
13	282	-83	430	34	0	-15	1263	4.02	4.02	4.02	4.02	2	0.19	0.01	0.08	0.00	0.00	22.3
14	282	-464	112	-3	0	-10	1154	4.02	4.02	4.02	4.02	2	0.17	0.00	0.02	0.00	0.00	22.3
15	282	-468	114	30	0	-10	1152	4.02	4.02	4.02	4.02	2	0.17	0.00	0.02	0.00	0.00	22.3
16	282	-287	257	4	0	-12	1180	4.02	4.02	4.02	4.02	2	0.18	0.01	0.05	0.00	0.00	22.3
17	282	-291	260	37	0	-13	1180	4.02	4.02	4.02	4.02	2	0.18	0.01	0.05	0.00	0.00	22.3
18	282	-1798	-400	10	0	-17	1632	4.02	4.02	4.02	4.02	3	0.22	0.01	0.07	0.00	0.00	22.3
19	282	-528	988	68	0	-48	1971	4.02	4.02	4.02	4.02	3	0.28	0.03	0.17	0.00	0.00	22.3
20	282	-1064	282	83	0	-32	1524	4.02	4.02	4.02	4.02	3	0.21	0.01	0.05	0.00	0.00	22.3
37	282	-1999	-878	-14	0	-1	1993	4.02	4.02	4.02	4.02	3	0.27	0.03	0.15	0.00	0.00	22.3
38	282	119	1434	82	0	-53	2165	4.02	4.02	4.02	4.02	3	0.31	0.04	0.26	0.00	0.00	22.3
39	282	-775	258	107	0	-26	1502	4.02	4.02	4.02	4.02	3	0.21	0.01	0.05	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	339	-491	-260	22	0	-27	1492	4.02	4.02	4.02	4.02	3	0.21	0.01	0.05	0.00	0.00	22.3
2	339	-672	-444	-0	0	-7	1167	4.02	4.02	4.02	4.02	2	0.17	0.01	0.08	0.00	0.00	22.3
3	339	-673	-443	10	0	-13	1166	4.02	4.02	4.02	4.02	2	0.17	0.01	0.08	0.00	0.00	22.3
4	339	-82	44	24	0	-29	1263	4.02	4.02	4.02	4.02	2	0.19	0.00	0.01	0.00	0.00	22.3
5	339	-83	45	34	0	-35	1263	4.02	4.02	4.02	4.02	2	0.19	0.00	0.01	0.00	0.00	22.3
6	339	-464	-274	-3	0	-8	1154	4.02	4.02	4.02	4.02	2	0.17	0.01	0.05	0.00	0.00	22.3
7	339	-468	-271	30	0	-27	1152	4.02	4.02	4.02	4.02	2	0.17	0.01	0.05	0.00	0.00	22.3
8	339	-287	-128	4	0	-14	1180	4.02	4.02	4.02	4.02	2	0.18	0.00	0.02	0.00	0.00	22.3
9	339	-291	-125	37	0	-34	1180	4.02	4.02	4.02	4.02	2	0.18	0.00	0.02	0.00	0.00	22.3
10	339	-672	-444	-0	0	-7	1167	4.02	4.02	4.02	4.02	2	0.17	0.01	0.08	0.00	0.00	22.3
11	339	-673	-443	10	0	-13	1166	4.02	4.02	4.02	4.02	2	0.17	0.01	0.08	0.00	0.00	22.3
12	339	-82	44	24	0	-29	1263	4.02	4.02	4.02	4.02	2	0.19	0.00	0.01	0.00	0.00	22.3
13	339	-83	45	34	0	-35	1263	4.02	4.02	4.02	4.02	2	0.19	0.00	0.01	0.00	0.00	22.3
14	339	-464	-274	-3	0	-8	1154	4.02	4.02	4.02	4.02	2	0.17	0.01	0.05	0.00	0.00	22.3
15	339	-468	-271	30	0	-27	1152	4.02	4.02	4.02	4.02	2	0.17	0.01	0.05	0.00	0.00	22.3
16	339	-287	-128	4	0	-14	1180	4.02	4.02	4.02	4.02	2	0.18	0.00	0.02	0.00	0.00	22.3
17	339	-291	-125	37	0	-34	1180	4.02	4.02	4.02	4.02	2	0.18	0.00	0.02	0.00	0.00	22.3
18	339	-1798	-901	10	0	-23	1632	4.02	4.02	4.02	4.02	3	0.22	0.03	0.15	0.00	0.00	22.3
19	339	-528	486	68	0	-86	2020	4.02	4.02	4.02	4.02	3	0.29	0.01	0.09	0.00	0.00	22.3
20	339	-1064	-219	83	0	-79	1524	4.02	4.02	4.02	4.02	3	0.21	0.01	0.04	0.00	0.00	22.3
37	339	-1999	-1380	-14	0	7	1628	4.02	4.02	4.02	4.02	3	0.22	0.04	0.23	0.00	0.00	22.3
38	339	119	932	82	0	-99	2580	4.02	4.02	4.02	4.02	3	0.37	0.03	0.17	0.00	0.00	22.3
39	339	-775	-244	107	0	-87	1502	4.02	4.02	4.02	4.02	3	0.21	0.01	0.04	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	395	-491	-761	22	0	-39	1492	4.02	4.02	4.02	4.02	3	0.21	0.02	0.13	0.00	0.00	22.3
2	395	-672	-830	-0	0	-7	1085	4.02	4.02	4.02	4.02	2	0.16	0.02	0.15	0.00	0.00	22.3
3	395	-673	-829	10	0	-18	1085	4.02	4.02	4.02	4.02	2	0.16	0.02	0.15	0.00	0.00	22.3
4	395	-82	-342	24	0	-43	1263	4.02	4.02	4.02	4.02	2	0.19	0.01	0.06	0.00	0.00	22.3
5	395	-83	-341	34	0	-54	1263	4.02	4.02	4.02	4.02	2	0.19	0.01	0.06	0.00	0.00	22.3
6	395	-464	-660	-3	0	-6	1154	4.02	4.02	4.02	4.02	2	0.17	0.02	0.12	0.00	0.00	22.3
7	395	-468	-657	30	0	-44	1152	4.02	4.02	4.02	4.02	2	0.17	0.02	0.12	0.00	0.00	22.3
8	395	-287	-514	4	0	-17	1180	4.02	4.02	4.02	4.02	2	0.18	0.01	0.09	0.00	0.00	22.3
9	395	-291	-511	37	0	-55	1180	4.02	4.02	4.02	4.02	2	0.18	0.01	0.09	0.00	0.00	22.3
10	395	-672	-830	-0	0	-7	1085	4.02	4.02	4.02	4.02	2	0.16	0.02	0.15	0.00	0.00	22.3
11	395	-673	-829	10	0	-18	1085	4.02	4.02	4.02	4.02	2	0.16	0.02	0.15	0.00	0.00	22.3
12	395	-82	-342	24	0	-43	1263	4.02	4.02	4.02	4.02	2	0.19	0.01	0.06	0.00	0.00	22.3
13	395	-83	-341	34	0	-54	1263	4.02	4.02	4.02	4.02	2	0.19	0.01	0.06	0.00	0.00	22.3
14	395	-464	-660	-3	0	-6	1154	4.02	4.02	4.02	4.02	2	0.17	0.02	0.12	0.00	0.00	22.3
15	395	-468	-657	30	0	-44	1152	4.02	4.02	4.02	4.02	2	0.17	0.02	0.12	0.00	0.00	22.3
16	395	-287	-514	4	0	-17	1180	4.02	4.02	4.02	4.02	2	0.18	0.01	0.09	0.00	0.00	22.3
17	395	-291	-511	37	0	-55	1180	4.02	4.02	4.02	4.02	2	0.18	0.01	0.09	0.00	0.00	22.3
18	395	-1798	-1403	10	0	-28	1240	4.02	4.02	4.02	4.02	3	0.17	0.04	0.24	0.00	0.00	22.3
19	395	-528	-16	68	0	-125	2020	4.02	4.02	4.02	4.02	3	0.29	0.00	0.00	0.00	0.00	22.3
20	395	-1064	-721	83	0	-126	1524	4.02	4.02	4.02	4.02	3	0.21	0.02	0.13	0.00	0.00	22.3
37	395	-1999	-1882	-14	0	15	961	4.02	4.02	4.02	4.02	3	0.13	0.05	0.32	0.00	0.00	22.3
38	395	119	430	82	0	-145	2594	4.02	4.02	4.02	4.02	3	0.37	0.01	0.08	0.00	0.00	22.3
39	395	-775	-745	107	0	-147	1502	4.02	4.02	4.02	4.02	3	0.21	0.02	0.13	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	452	-491	-1263	22	0	-52	1266	4.02	4.02	4.02	4.02	3	0.18	0.04	0.22	0.00	0.00	22.3
2	452	-672	-1216	-0	0	-7	702	4.02	4.02	4.02	4.02	2	0.10	0.04	0.21	0.00	0.00	22.3
3	452	-673	-1215	10	0	-24	703	4.02	4.02	4.02	4.02	2	0.10	0.04	0.21	0.00	0.00	22.3
4	452	-82	-728	24	0	-56	1246	4.02	4.02	4.02	4.02	2	0.19	0.02	0.13	0.00	0.00	22.3
5	452	-83	-727	34	0	-73	1246	4.02	4.02	4.02	4.02	2	0.19	0.02	0.13	0.00	0.00	22.3
6	452	-464	-1046	-3	0	-4	892	4.02	4.02	4.02	4.02	2	0.13	0.03	0.18	0.00	0.00	22.3
7	452	-468	-1043	30	0	-61	893	4.02	4.02	4.02	4.02	2	0.13	0.03	0.18	0.00	0.00	22.3
8	452	-287	-900	4	0	-19	1055	4.02	4.02	4.02	4.02	2	0.16	0.03	0.16	0.00	0.00	22.3
9	452	-291	-897	37	0	-76	1056	4.02	4.02	4.02	4.02	2	0.16	0.03	0.16	0.00	0.00	22.3
10	452	-672	-1216	-0	0	-7	702	4.02	4.02	4.02	4.02	2	0.10	0.04	0.21	0.00	0.00	22.3
11	452	-673	-1215	10	0	-24	703	4.02	4.02	4.02	4.02	2	0.10	0.04	0.21	0.00	0.00	22.3
12	452	-82	-728	24	0	-56	1246	4.02	4.02	4.02	4.02	2	0.19	0.02	0.13	0.00	0.00	22.3
13	452	-83	-727	34	0	-73	1246	4.02	4.02	4.02	4.02	2	0.19	0.02	0.13	0.00	0.00	22.3
14	452	-464	-1046	-3	0	-4	892	4.02	4.02	4.02	4.02	2	0.13	0.03	0.18	0.00	0.00	22.3
15	452	-468	-1043	30	0	-61	893	4.02	4.02	4.02	4.02	2	0.13	0.03	0.18	0.00	0.00	22.3
16	452	-287	-900	4	0	-19	1055	4.02	4.02	4.02	4.02	2	0.16	0.03	0.16	0.00	0.00	22.3
17	452	-291	-897	37	0	-76	1056	4.02	4.02	4.02	4.02	2	0.16	0.03	0.16	0.00	0.00	22.3

18	452	-1798	-1905	10	0	-34	-1369	4.02	4.02	4.02	4.02	3	0.19	0.05	0.33	0.00	0.00	22.3
19	452	-528	-518	68	0	-163	2020	4.02	4.02	4.02	4.02	3	0.29	0.01	0.09	0.00	0.00	22.3
20	452	-1064	-1223	83	0	-173	1328	4.02	4.02	4.02	4.02	3	0.18	0.04	0.21	0.00	0.00	22.3
37	452	-1999	-2384	-14	0	23	-2404	4.02	4.02	4.02	4.02	3	0.33	0.07	0.41	0.00	0.00	22.3
38	452	119	-72	82	0	-191	2594	4.02	4.02	4.02	4.02	3	0.37	0.00	0.01	0.00	0.00	22.3
39	452	-775	-1247	107	0	-208	1291	4.02	4.02	4.02	4.02	3	0.18	0.04	0.22	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	508	-491	-1764	22	0	-64	-1121	4.02	4.02	4.02	4.02	3	0.16	0.05	0.31	0.00	0.00	22.3
2	508	-672	-1602	-0	0	-6	-1521	4.02	4.02	4.02	4.02	2	0.23	0.05	0.28	0.00	0.00	22.3
3	508	-673	-1601	10	0	-29	-1519	4.02	4.02	4.02	4.02	2	0.23	0.05	0.28	0.00	0.00	22.3
4	508	-82	-1114	24	0	-70	921	4.02	4.02	4.02	4.02	2	0.14	0.03	0.20	0.00	0.00	22.3
5	508	-83	-1113	34	0	-93	922	4.02	4.02	4.02	4.02	2	0.14	0.03	0.20	0.00	0.00	22.3
6	508	-464	-1432	-3	0	-2	-1063	4.02	4.02	4.02	4.02	2	0.16	0.04	0.25	0.00	0.00	22.3
7	508	-468	-1429	30	0	-78	-1057	4.02	4.02	4.02	4.02	2	0.16	0.04	0.25	0.00	0.00	22.3
8	508	-287	-1286	4	0	-21	-669	4.02	4.02	4.02	4.02	2	0.10	0.04	0.23	0.00	0.00	22.3
9	508	-291	-1283	37	0	-97	-663	4.02	4.02	4.02	4.02	2	0.10	0.04	0.23	0.00	0.00	22.3
10	508	-672	-1602	-0	0	-6	-1521	4.02	4.02	4.02	4.02	2	0.23	0.05	0.28	0.00	0.00	22.3
11	508	-673	-1601	10	0	-29	-1519	4.02	4.02	4.02	4.02	2	0.23	0.05	0.28	0.00	0.00	22.3
12	508	-82	-1114	24	0	-70	921	4.02	4.02	4.02	4.02	2	0.14	0.03	0.20	0.00	0.00	22.3
13	508	-83	-1113	34	0	-93	922	4.02	4.02	4.02	4.02	2	0.14	0.03	0.20	0.00	0.00	22.3
14	508	-464	-1432	-3	0	-2	-1063	4.02	4.02	4.02	4.02	2	0.16	0.04	0.25	0.00	0.00	22.3
15	508	-468	-1429	30	0	-78	-1057	4.02	4.02	4.02	4.02	2	0.16	0.04	0.25	0.00	0.00	22.3
16	508	-287	-1286	4	0	-21	-669	4.02	4.02	4.02	4.02	2	0.10	0.04	0.23	0.00	0.00	22.3
17	508	-291	-1283	37	0	-97	-663	4.02	4.02	4.02	4.02	2	0.10	0.04	0.23	0.00	0.00	22.3
18	508	-1798	-2406	10	0	-40	-2841	4.02	4.02	4.02	4.02	3	0.39	0.07	0.41	0.00	0.00	22.3
19	508	-528	-1019	68	0	-201	1952	4.02	4.02	4.02	4.02	3	0.28	0.03	0.18	0.00	0.00	22.3
20	508	-1064	-1724	83	0	-220	-996	4.02	4.02	4.02	4.02	3	0.14	0.05	0.30	0.00	0.00	22.3
37	508	-1999	-2885	-14	0	32	-4146	4.02	4.02	4.02	4.02	3	0.56	0.08	0.49	0.00	0.00	22.3
38	508	119	-573	82	0	-237	2594	4.02	4.02	4.02	4.02	3	0.37	0.02	0.10	0.00	0.00	22.3
39	508	-775	-1748	107	0	-269	-1071	4.02	4.02	4.02	4.02	3	0.15	0.05	0.31	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	565	-491	-2266	22	0	-77	-1367	4.02	4.02	4.02	4.02	3	0.19	0.07	0.40	0.00	0.00	22.3
2	565	-672	-1988	-0	0	-6	-1724	4.02	4.02	4.02	4.02	2	0.26	0.06	0.35	0.00	0.00	22.3
3	565	-673	-1987	10	0	-35	-1722	4.02	4.02	4.02	4.02	2	0.26	0.06	0.35	0.00	0.00	22.3
4	565	-82	-1500	24	0	-83	-382	4.02	4.02	4.02	4.02	2	0.06	0.04	0.27	0.00	0.00	22.3
5	565	-83	-1499	34	0	-112	-380	4.02	4.02	4.02	4.02	2	0.06	0.04	0.27	0.00	0.00	22.3
6	565	-464	-1818	-3	0	-0	-1256	4.02	4.02	4.02	4.02	2	0.19	0.05	0.32	0.00	0.00	22.3
7	565	-468	-1815	30	0	-95	-1250	4.02	4.02	4.02	4.02	2	0.19	0.05	0.32	0.00	0.00	22.3
8	565	-287	-1672	4	0	-23	-853	4.02	4.02	4.02	4.02	2	0.13	0.05	0.30	0.00	0.00	22.3
9	565	-291	-1669	37	0	-118	-847	4.02	4.02	4.02	4.02	2	0.13	0.05	0.30	0.00	0.00	22.3
10	565	-672	-1988	-0	0	-6	-1724	4.02	4.02	4.02	4.02	2	0.26	0.06	0.35	0.00	0.00	22.3
11	565	-673	-1987	10	0	-35	-1722	4.02	4.02	4.02	4.02	2	0.26	0.06	0.35	0.00	0.00	22.3
12	565	-82	-1500	24	0	-83	-382	4.02	4.02	4.02	4.02	2	0.06	0.04	0.27	0.00	0.00	22.3
13	565	-83	-1499	34	0	-112	-380	4.02	4.02	4.02	4.02	2	0.06	0.04	0.27	0.00	0.00	22.3
14	565	-464	-1818	-3	0	-0	-1256	4.02	4.02	4.02	4.02	2	0.19	0.05	0.32	0.00	0.00	22.3
15	565	-468	-1815	30	0	-95	-1250	4.02	4.02	4.02	4.02	2	0.19	0.05	0.32	0.00	0.00	22.3
16	565	-287	-1672	4	0	-23	-853	4.02	4.02	4.02	4.02	2	0.13	0.05	0.30	0.00	0.00	22.3
17	565	-291	-1669	37	0	-118	-847	4.02	4.02	4.02	4.02	2	0.13	0.05	0.30	0.00	0.00	22.3
18	565	-1798	-2908	10	0	-46	-3124	4.02	4.02	4.02	4.02	3	0.43	0.08	0.50	0.00	0.00	22.3
19	565	-528	-1521	68	0	-240	1488	4.02	4.02	4.02	4.02	3	0.21	0.04	0.27	0.00	0.00	22.3
20	565	-1064	-2226	83	0	-267	-1239	4.02	4.02	4.02	4.02	3	0.17	0.06	0.39	0.00	0.00	22.3
37	565	-1999	-3387	-14	0	40	-4457	4.02	4.02	4.02	4.02	3	0.60	0.10	0.58	0.00	0.00	22.3
38	565	119	-1075	82	0	-283	2491	4.02	4.02	4.02	4.02	3	0.36	0.03	0.19	0.00	0.00	22.3
39	565	-775	-2250	107	0	-329	-1316	4.02	4.02	4.02	4.02	3	0.18	0.07	0.39	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

Nome travata: **trave_503_IP1** Descrizione: **Trave_5 8-13-18-23**
ASTA NUM. 7 NI 214 NF 212 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y qy tot.
qy medio: 375.00 375.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-93	1183	-14	0	-35	-484	4.02	4.02	4.02	4.02	3	0.07	0.03	0.21	0.00	0.00	22.3
2	0	-63	874	15	0	39	-264	4.02	4.02	4.02	4.02	2	0.04	0.03	0.16	0.00	0.00	22.3
3	0	-65	875	15	0	39	-267	4.02	4.02	4.02	4.02	2	0.04	0.03	0.16	0.00	0.00	22.3
4	0	-79	944	-36	0	-93	-478	4.02	4.02	4.02	4.02	2	0.07	0.03	0.17	0.00	0.00	22.3
5	0	-81	945	-37	0	-94	-482	4.02	4.02	4.02	4.02	2	0.07	0.03	0.17	0.00	0.00	22.3
6	0	-66	897	-3	0	-7	-335	4.02	4.02	4.02	4.02	2	0.05	0.03	0.16	0.00	0.00	22.3
7	0	-72	901	-4	0	-8	-346	4.02	4.02	4.02	4.02	2	0.05	0.03	0.16	0.00	0.00	22.3
8	0	-71	918	-18	0	-46	-399	4.02	4.02	4.02	4.02	2	0.06	0.03	0.16	0.00	0.00	22.3
9	0	-77	922	-19	0	-48	-411	4.02	4.02	4.02	4.02	2	0.06	0.03	0.16	0.00	0.00	22.3
10	0	-63	874	15	0	39	-264	4.02	4.02	4.02	4.02	2	0.04	0.03	0.16	0.00	0.00	22.3
11	0	-65	875	15	0	39	-267	4.02	4.02	4.02	4.02	2	0.04	0.03	0.16	0.00	0.00	22.3
12	0	-79	944	-36	0	-93	-478	4.02	4.02	4.02	4.02	2	0.07	0.03	0.17	0.00	0.00	22.3
13	0	-81	945	-37	0	-94	-482	4.02	4.02	4.02	4.02	2	0.07	0.03	0.17	0.00	0.00	22.3
14	0	-66	897	-3	0	-7	-335	4.02	4.02	4.02	4.02	2	0.05	0.03	0.16	0.00	0.00	22.3
15	0	-72	901	-4	0	-8	-346	4.02	4.02	4.02	4.02	2	0.05	0.03	0.16	0.00	0.00	22.3
16	0	-71	918	-18	0	-46	-399	4.02	4.02	4.02	4.02	2	0.06	0.03	0.16	0.00	0.00	22.3
17	0	-77	922	-19	0	-48	-411	4.02	4.02	4.02	4.02	2	0.06	0.03	0.16	0.00	0.00	22.3
18	0	-50	1088	44	0	111	-194	4.02	4.02	4.02	4.02	3	0.03	0.03	0.19	0.00	0.00	22.3
19	0	-103	1297	-112	0	-289	-836	4.02	4.02	4.02	4.02	3	0.12	0.04	0.23	0.00	0.00	22.3
20	0	-69	1190	-40	0	-105	-508	4.02	4.02	4.02	4.02	3	0.07	0.03	0.21	0.00	0.00	22.3
37	0	-38	1015	102	0	261	544	4.02	4.02	4.02	4.02	3	0.08	0.03	0.18	0.00	0.00	22.3
38	0	-126	1364	-158	0	-405	-1040	4.02	4.02	4.02	4.02	3	0.15	0.04	0.24	0.00	0.00	22.3
39	0	-70	1186	-39	0	-100	-493	4.02	4.02	4.02	4.02	3	0.07	0.03	0.21	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	57	-93	907	-14	0	-27	565	4.02	4.02	4.02	4.02	3	0.08	0.03	0.16	0.00	0.00	22.3
2	57	-63	662	15	0	31	506	4.02	4.02	4.02	4.02	2	0.08	0.02	0.12	0.00	0.00	22.3
3	57	-65	663	15	0	30	503	4.02	4.02	4.02	4.02	2	0.08	0.02	0.12	0.00	0.00	22.3
4	57	-79	732	-36	0	-73	-375	4.02	4.02	4.02	4.02	2	0.06	0.02	0.13	0.00	0.00	22.3
5	57	-81	733	-37	0	-73	-379	4.02	4.02	4.02	4.02	2	0.06	0.02	0.13	0.00	0.00	22.3
6	57	-66	685	-3	0	-5	459	4.02	4.02	4.02	4.02	2	0.07	0.02	0.12	0.00	0.00	22.3
7	57	-72	689	-4	0	-6	452	4.02	4.02	4.02	4.02	2	0.07	0.02	0.12	0.00	0.00	22.3
8	57	-71	706	-18	0	-36	417	4.02	4.02	4.02	4.02	2	0.06	0.02	0.13	0.00	0.00	22.3
9	57	-77	710	-19	0	-37	410	4.02	4.02	4.02	4.02	2	0.06	0.02	0.13	0.00	0.00	22.3

10	57	-63	662	15	0	31	506	4.02	4.02	4.02	4.02	2	0.08	0.02	0.12	0.00	0.00	22.3
11	57	-65	663	15	0	30	503	4.02	4.02	4.02	4.02	2	0.08	0.02	0.12	0.00	0.00	22.3
12	57	-79	732	-36	0	-73	-375	4.02	4.02	4.02	4.02	2	0.06	0.02	0.13	0.00	0.00	22.3
13	57	-81	733	-37	0	-73	-379	4.02	4.02	4.02	4.02	2	0.06	0.02	0.13	0.00	0.00	22.3
14	57	-66	685	-3	0	-5	459	4.02	4.02	4.02	4.02	2	0.07	0.02	0.12	0.00	0.00	22.3
15	57	-72	689	-4	0	-6	452	4.02	4.02	4.02	4.02	2	0.07	0.02	0.12	0.00	0.00	22.3
16	57	-71	706	-18	0	-36	417	4.02	4.02	4.02	4.02	2	0.06	0.02	0.13	0.00	0.00	22.3
17	57	-77	710	-19	0	-37	410	4.02	4.02	4.02	4.02	2	0.06	0.02	0.13	0.00	0.00	22.3
18	57	-50	812	44	0	86	754	4.02	4.02	4.02	4.02	3	0.11	0.02	0.14	0.00	0.00	22.3
19	57	-103	1022	-112	0	-225	-698	4.02	4.02	4.02	4.02	3	0.10	0.03	0.18	0.00	0.00	22.3
20	57	-69	915	-40	0	-83	550	4.02	4.02	4.02	4.02	3	0.08	0.03	0.16	0.00	0.00	22.3
37	57	-38	739	102	0	203	900	4.02	4.02	4.02	4.02	3	0.13	0.02	0.13	0.00	0.00	22.3
38	57	-126	1089	-158	0	-316	-898	4.02	4.02	4.02	4.02	3	0.13	0.03	0.19	0.00	0.00	22.3
39	57	-70	910	-39	0	-78	560	4.02	4.02	4.02	4.02	3	0.08	0.03	0.16	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	113	-93	632	-14	0	-19	861	4.02	4.02	4.02	4.02	3	0.12	0.02	0.11	0.00	0.00	22.3
2	113	-63	450	15	0	22	713	4.02	4.02	4.02	4.02	2	0.11	0.01	0.08	0.00	0.00	22.3
3	113	-65	452	15	0	22	711	4.02	4.02	4.02	4.02	2	0.11	0.01	0.08	0.00	0.00	22.3
4	113	-79	520	-36	0	-52	612	4.02	4.02	4.02	4.02	2	0.09	0.02	0.09	0.00	0.00	22.3
5	113	-81	522	-37	0	-52	611	4.02	4.02	4.02	4.02	2	0.09	0.02	0.09	0.00	0.00	22.3
6	113	-66	473	-3	0	-4	679	4.02	4.02	4.02	4.02	2	0.10	0.01	0.08	0.00	0.00	22.3
7	113	-72	477	-4	0	-4	674	4.02	4.02	4.02	4.02	2	0.10	0.01	0.08	0.00	0.00	22.3
8	113	-71	494	-18	0	-26	649	4.02	4.02	4.02	4.02	2	0.10	0.01	0.09	0.00	0.00	22.3
9	113	-77	498	-19	0	-26	644	4.02	4.02	4.02	4.02	2	0.10	0.01	0.09	0.00	0.00	22.3
10	113	-63	450	15	0	22	713	4.02	4.02	4.02	4.02	2	0.11	0.01	0.08	0.00	0.00	22.3
11	113	-65	452	15	0	22	711	4.02	4.02	4.02	4.02	2	0.11	0.01	0.08	0.00	0.00	22.3
12	113	-79	520	-36	0	-52	612	4.02	4.02	4.02	4.02	2	0.09	0.02	0.09	0.00	0.00	22.3
13	113	-81	522	-37	0	-52	611	4.02	4.02	4.02	4.02	2	0.09	0.02	0.09	0.00	0.00	22.3
14	113	-66	473	-3	0	-4	679	4.02	4.02	4.02	4.02	2	0.10	0.01	0.08	0.00	0.00	22.3
15	113	-72	477	-4	0	-4	674	4.02	4.02	4.02	4.02	2	0.10	0.01	0.08	0.00	0.00	22.3
16	113	-71	494	-18	0	-26	649	4.02	4.02	4.02	4.02	2	0.10	0.01	0.09	0.00	0.00	22.3
17	113	-77	498	-19	0	-26	644	4.02	4.02	4.02	4.02	2	0.10	0.01	0.09	0.00	0.00	22.3
18	113	-50	537	44	0	61	996	4.02	4.02	4.02	4.02	3	0.14	0.02	0.10	0.00	0.00	22.3
19	113	-103	746	-112	0	-162	696	4.02	4.02	4.02	4.02	3	0.10	0.02	0.13	0.00	0.00	22.3
20	113	-69	639	-40	0	-60	850	4.02	4.02	4.02	4.02	3	0.12	0.02	0.11	0.00	0.00	22.3
37	113	-38	464	102	0	146	1078	4.02	4.02	4.02	4.02	3	0.15	0.01	0.08	0.00	0.00	22.3
38	113	-126	813	-158	0	-227	601	4.02	4.02	4.02	4.02	3	0.09	0.02	0.14	0.00	0.00	22.3
39	113	-70	635	-39	0	-56	857	4.02	4.02	4.02	4.02	3	0.12	0.02	0.11	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	170	-93	356	-14	0	-11	943	4.02	4.02	4.02	4.02	3	0.13	0.01	0.06	0.00	0.00	22.3
2	170	-63	238	15	0	14	754	4.02	4.02	4.02	4.02	2	0.11	0.01	0.04	0.00	0.00	22.3
3	170	-65	240	15	0	14	753	4.02	4.02	4.02	4.02	2	0.11	0.01	0.04	0.00	0.00	22.3
4	170	-79	308	-36	0	-31	698	4.02	4.02	4.02	4.02	2	0.11	0.01	0.05	0.00	0.00	22.3
5	170	-81	310	-37	0	-31	697	4.02	4.02	4.02	4.02	2	0.11	0.01	0.06	0.00	0.00	22.3
6	170	-66	261	-3	0	-2	735	4.02	4.02	4.02	4.02	2	0.11	0.01	0.05	0.00	0.00	22.3
7	170	-72	265	-4	0	-2	733	4.02	4.02	4.02	4.02	2	0.11	0.01	0.05	0.00	0.00	22.3
8	170	-71	282	-18	0	-16	718	4.02	4.02	4.02	4.02	2	0.11	0.01	0.05	0.00	0.00	22.3
9	170	-77	286	-19	0	-16	716	4.02	4.02	4.02	4.02	2	0.11	0.01	0.05	0.00	0.00	22.3
10	170	-63	238	15	0	14	754	4.02	4.02	4.02	4.02	2	0.11	0.01	0.04	0.00	0.00	22.3
11	170	-65	240	15	0	14	753	4.02	4.02	4.02	4.02	2	0.11	0.01	0.04	0.00	0.00	22.3
12	170	-79	308	-36	0	-31	698	4.02	4.02	4.02	4.02	2	0.11	0.01	0.05	0.00	0.00	22.3
13	170	-81	310	-37	0	-31	697	4.02	4.02	4.02	4.02	2	0.11	0.01	0.06	0.00	0.00	22.3
14	170	-66	261	-3	0	-2	735	4.02	4.02	4.02	4.02	2	0.11	0.01	0.05	0.00	0.00	22.3
15	170	-72	265	-4	0	-2	733	4.02	4.02	4.02	4.02	2	0.11	0.01	0.05	0.00	0.00	22.3
16	170	-71	282	-18	0	-16	718	4.02	4.02	4.02	4.02	2	0.11	0.01	0.05	0.00	0.00	22.3
17	170	-77	286	-19	0	-16	716	4.02	4.02	4.02	4.02	2	0.11	0.01	0.05	0.00	0.00	22.3
18	170	-50	261	44	0	36	1019	4.02	4.02	4.02	4.02	3	0.15	0.01	0.05	0.00	0.00	22.3
19	170	-103	471	-112	0	-99	884	4.02	4.02	4.02	4.02	3	0.13	0.01	0.08	0.00	0.00	22.3
20	170	-69	364	-40	0	-37	938	4.02	4.02	4.02	4.02	3	0.13	0.01	0.06	0.00	0.00	22.3
37	170	-38	188	102	0	88	1078	4.02	4.02	4.02	4.02	3	0.15	0.01	0.03	0.00	0.00	22.3
38	170	-126	538	-158	0	-138	843	4.02	4.02	4.02	4.02	3	0.12	0.02	0.10	0.00	0.00	22.3
39	170	-70	359	-39	0	-34	942	4.02	4.02	4.02	4.02	3	0.13	0.01	0.06	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	226	-93	81	-14	0	-3	943	4.02	4.02	4.02	4.02	3	0.13	0.00	0.01	0.00	0.00	22.3
2	226	-63	26	15	0	5	754	4.02	4.02	4.02	4.02	2	0.11	0.00	0.00	0.00	0.00	22.3
3	226	-65	28	15	0	6	753	4.02	4.02	4.02	4.02	2	0.11	0.00	0.00	0.00	0.00	22.3
4	226	-79	96	-36	0	-11	698	4.02	4.02	4.02	4.02	2	0.11	0.00	0.02	0.00	0.00	22.3
5	226	-81	98	-37	0	-11	697	4.02	4.02	4.02	4.02	2	0.11	0.00	0.02	0.00	0.00	22.3
6	226	-66	50	-3	0	-0	735	4.02	4.02	4.02	4.02	2	0.11	0.00	0.01	0.00	0.00	22.3
7	226	-72	53	-4	0	0	733	4.02	4.02	4.02	4.02	2	0.11	0.00	0.01	0.00	0.00	22.3
8	226	-71	71	-18	0	-5	718	4.02	4.02	4.02	4.02	2	0.11	0.00	0.01	0.00	0.00	22.3
9	226	-77	74	-19	0	-5	716	4.02	4.02	4.02	4.02	2	0.11	0.00	0.01	0.00	0.00	22.3
10	226	-63	26	15	0	5	754	4.02	4.02	4.02	4.02	2	0.11	0.00	0.00	0.00	0.00	22.3
11	226	-65	28	15	0	6	753	4.02	4.02	4.02	4.02	2	0.11	0.00	0.00	0.00	0.00	22.3
12	226	-79	96	-36	0	-11	698	4.02	4.02	4.02	4.02	2	0.11	0.00	0.02	0.00	0.00	22.3
13	226	-81	98	-37	0	-11	697	4.02	4.02	4.02	4.02	2	0.11	0.00	0.02	0.00	0.00	22.3
14	226	-66	50	-3	0	-0	735	4.02	4.02	4.02	4.02	2	0.11	0.00	0.01	0.00	0.00	22.3
15	226	-72	53	-4	0	0	733	4.02	4.02	4.02	4.02	2	0.11	0.00	0.01	0.00	0.00	22.3
16	226	-71	71	-18	0	-5	718	4.02	4.02	4.02	4.02	2	0.11	0.00	0.01	0.00	0.00	22.3
17	226	-77	74	-19	0	-5	716	4.02	4.02	4.02	4.02	2	0.11	0.00	0.01	0.00	0.00	22.3
18	226	-50	-14	44	0	11	1019	4.02	4.02	4.02	4.02	3	0.15	0.00	0.00	0.00	0.00	22.3
19	226	-103	195	-112	0	-36	884	4.02	4.02	4.02	4.02	3	0.13	0.01	0.03	0.00	0.00	22.3
20	226	-69	88	-40	0	-14	938	4.02	4.02	4.02	4.02	3	0.13	0.00	0.02	0.00	0.00	22.3
37	226	-38	-87	102	0	30	1078	4.02	4.02	4.02	4.02	3	0.15	0.00	0.02	0.00	0.00	22.3
38	226	-126	262	-158	0	-49	867	4.02	4.02	4.02	4.02	3	0.12	0.01	0.05	0.00	0.00	22.3
39	226	-70	84	-39	0	-12	942	4.02	4.02	4.02	4.02	3	0.13	0.00	0.01	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	283	-93	-194	-14	0	5	943	4.02	4.02	4.02	4.02	3	0.13	0.01	0.03	0.00	0.00	22.3
2	283	-63	-185	15	0	-3	754	4.02	4.02	4.02	4.02	2	0.11	0.01	0.03	0.00	0.00	22.3
3	283	-65	-184	15	0	-3	753	4.02	4.02	4.02	4.02	2	0.11	0.01	0.03	0.00	0.00	22.3
4	283	-79	-115	-36	0	10	698	4.02	4.02	4.02	4.02	2	0.11	0.00	0.02	0.00	0.00	22.3
5	283	-81	-114	-37	0	10	697	4.02	4.02	4.02	4.02	2	0.11	0.00	0.02	0.00	0.00	22.3
6	283	-66	-162	-3	0	1	735	4.02	4.02	4.02	4.02	2	0.11	0.00	0.03	0.00	0.00	22.3
7	283	-72	-158	-4	0	2	733	4.02	4.02	4.02	4.02	2	0.11	0.00	0.03	0.00	0.00	22.3
8	283	-71	-141	-18	0	5	718	4.02	4.02	4.02	4.02	2	0.11	0.00	0.03	0.00	0.00	22.3
9	283	-77	-137	-19	0	6	716	4.02	4.02	4.02	4.02	2	0.11	0.00	0.02	0.00	0.00	22.3
10	283	-63	-185	15	0	-3	754	4.02	4.02	4.02	4.02	2	0.11	0.01	0.03	0.00	0.00	22.3
11	283	-65	-184	15	0	-3	753	4.02	4.02	4.02	4.02	2	0.11	0.01	0.03	0.00	0.00	22.3
12	283	-79	-115	-36	0	10	698	4.02	4.02	4.02	4.02	2	0.11	0.00	0.02	0.00	0.00	22.3
13	283	-81	-114	-37	0	10	697	4.02	4.02	4.02	4.02	2	0.11	0.00	0.02	0.00	0.00	22.3
14	283	-66	-162	-3	0	1	735	4.02	4.02	4.02	4.02	2	0.11	0.00	0.03	0.00	0.00	22.3
15	283	-72	-158	-4	0	2	733	4.02	4.02	4.02	4.02	2	0.11	0.00	0.03	0.00	0.00	22.3

16	283	-71	-141	-18	0	5	718	4.02	4.02	4.02	4.02	2	0.11	0.00	0.03	0.00	0.00	22.3
17	283	-77	-137	-19	0	6	716	4.02	4.02	4.02	4.02	2	0.11	0.00	0.02	0.00	0.00	22.3
18	283	-50	-290	44	0	-13	1019	4.02	4.02	4.02	4.02	3	0.15	0.01	0.05	0.00	0.00	22.3
19	283	-103	-80	-112	0	27	884	4.02	4.02	4.02	4.02	3	0.13	0.00	0.01	0.00	0.00	22.3
20	283	-69	-187	-40	0	9	938	4.02	4.02	4.02	4.02	3	0.13	0.01	0.03	0.00	0.00	22.3
37	283	-38	-362	102	0	-28	1078	4.02	4.02	4.02	4.02	3	0.15	0.01	0.06	0.00	0.00	22.3
38	283	-126	-13	-158	0	40	867	4.02	4.02	4.02	4.02	3	0.12	0.00	0.03	0.00	0.00	22.3
39	283	-70	-192	-39	0	10	942	4.02	4.02	4.02	4.02	3	0.13	0.01	0.03	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	339	-93	-470	-14	0	13	943	4.02	4.02	4.02	4.02	3	0.13	0.01	0.08	0.00	0.00	22.3
2	339	-63	-397	15	0	-11	746	4.02	4.02	4.02	4.02	2	0.11	0.01	0.07	0.00	0.00	22.3
3	339	-65	-396	15	0	-11	746	4.02	4.02	4.02	4.02	2	0.11	0.01	0.07	0.00	0.00	22.3
4	339	-79	-327	-36	0	30	698	4.02	4.02	4.02	4.02	2	0.11	0.01	0.06	0.00	0.00	22.3
5	339	-81	-326	-37	0	31	697	4.02	4.02	4.02	4.02	2	0.11	0.01	0.06	0.00	0.00	22.3
6	339	-66	-374	-3	0	3	735	4.02	4.02	4.02	4.02	2	0.11	0.01	0.07	0.00	0.00	22.3
7	339	-72	-370	-4	0	4	733	4.02	4.02	4.02	4.02	2	0.11	0.01	0.07	0.00	0.00	22.3
8	339	-71	-353	-18	0	15	718	4.02	4.02	4.02	4.02	2	0.11	0.01	0.06	0.00	0.00	22.3
9	339	-77	-349	-19	0	17	716	4.02	4.02	4.02	4.02	2	0.11	0.01	0.06	0.00	0.00	22.3
10	339	-63	-397	15	0	-11	746	4.02	4.02	4.02	4.02	2	0.11	0.01	0.07	0.00	0.00	22.3
11	339	-65	-396	15	0	-11	746	4.02	4.02	4.02	4.02	2	0.11	0.01	0.07	0.00	0.00	22.3
12	339	-79	-327	-36	0	30	698	4.02	4.02	4.02	4.02	2	0.11	0.01	0.06	0.00	0.00	22.3
13	339	-81	-326	-37	0	31	697	4.02	4.02	4.02	4.02	2	0.11	0.01	0.06	0.00	0.00	22.3
14	339	-66	-374	-3	0	3	735	4.02	4.02	4.02	4.02	2	0.11	0.01	0.07	0.00	0.00	22.3
15	339	-72	-370	-4	0	4	733	4.02	4.02	4.02	4.02	2	0.11	0.01	0.07	0.00	0.00	22.3
16	339	-71	-353	-18	0	15	718	4.02	4.02	4.02	4.02	2	0.11	0.01	0.06	0.00	0.00	22.3
17	339	-77	-349	-19	0	17	716	4.02	4.02	4.02	4.02	2	0.11	0.01	0.06	0.00	0.00	22.3
18	339	-50	-565	44	0	-38	978	4.02	4.02	4.02	4.02	3	0.14	0.02	0.10	0.00	0.00	22.3
19	339	-103	-355	-112	0	90	884	4.02	4.02	4.02	4.02	3	0.13	0.01	0.06	0.00	0.00	22.3
20	339	-69	-462	-40	0	32	938	4.02	4.02	4.02	4.02	3	0.13	0.01	0.08	0.00	0.00	22.3
37	339	-38	-638	102	0	-85	992	4.02	4.02	4.02	4.02	3	0.14	0.02	0.11	0.00	0.00	22.3
38	339	-126	-288	-158	0	129	867	4.02	4.02	4.02	4.02	3	0.12	0.01	0.05	0.00	0.00	22.3
39	339	-70	-467	-39	0	32	942	4.02	4.02	4.02	4.02	3	0.13	0.01	0.08	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	396	-93	-746	-14	0	21	757	4.02	4.02	4.02	4.02	3	0.11	0.02	0.13	0.00	0.00	22.3
2	396	-63	-609	15	0	-20	569	4.02	4.02	4.02	4.02	2	0.09	0.02	0.11	0.00	0.00	22.3
3	396	-65	-608	15	0	-19	569	4.02	4.02	4.02	4.02	2	0.09	0.02	0.11	0.00	0.00	22.3
4	396	-79	-539	-36	0	51	595	4.02	4.02	4.02	4.02	2	0.09	0.02	0.10	0.00	0.00	22.3
5	396	-81	-538	-37	0	51	596	4.02	4.02	4.02	4.02	2	0.09	0.02	0.10	0.00	0.00	22.3
6	396	-66	-586	-3	0	4	578	4.02	4.02	4.02	4.02	2	0.09	0.02	0.10	0.00	0.00	22.3
7	396	-72	-582	-4	0	6	580	4.02	4.02	4.02	4.02	2	0.09	0.02	0.10	0.00	0.00	22.3
8	396	-71	-565	-18	0	26	585	4.02	4.02	4.02	4.02	2	0.09	0.02	0.10	0.00	0.00	22.3
9	396	-77	-561	-19	0	27	588	4.02	4.02	4.02	4.02	2	0.09	0.02	0.10	0.00	0.00	22.3
10	396	-63	-609	15	0	-20	569	4.02	4.02	4.02	4.02	2	0.09	0.02	0.11	0.00	0.00	22.3
11	396	-65	-608	15	0	-19	569	4.02	4.02	4.02	4.02	2	0.09	0.02	0.11	0.00	0.00	22.3
12	396	-79	-539	-36	0	51	595	4.02	4.02	4.02	4.02	2	0.09	0.02	0.10	0.00	0.00	22.3
13	396	-81	-538	-37	0	51	596	4.02	4.02	4.02	4.02	2	0.09	0.02	0.10	0.00	0.00	22.3
14	396	-66	-586	-3	0	4	578	4.02	4.02	4.02	4.02	2	0.09	0.02	0.10	0.00	0.00	22.3
15	396	-72	-582	-4	0	6	580	4.02	4.02	4.02	4.02	2	0.09	0.02	0.10	0.00	0.00	22.3
16	396	-71	-565	-18	0	26	585	4.02	4.02	4.02	4.02	2	0.09	0.02	0.10	0.00	0.00	22.3
17	396	-77	-561	-19	0	27	588	4.02	4.02	4.02	4.02	2	0.09	0.02	0.10	0.00	0.00	22.3
18	396	-50	-841	44	0	-63	721	4.02	4.02	4.02	4.02	3	0.10	0.02	0.15	0.00	0.00	22.3
19	396	-103	-631	-112	0	153	802	4.02	4.02	4.02	4.02	3	0.11	0.02	0.11	0.00	0.00	22.3
20	396	-69	-738	-40	0	55	761	4.02	4.02	4.02	4.02	3	0.11	0.02	0.13	0.00	0.00	22.3
37	396	-38	-914	102	0	-143	693	4.02	4.02	4.02	4.02	3	0.10	0.03	0.16	0.00	0.00	22.3
38	396	-126	-564	-158	0	218	826	4.02	4.02	4.02	4.02	3	0.12	0.02	0.10	0.00	0.00	22.3
39	396	-70	-743	-39	0	53	760	4.02	4.02	4.02	4.02	3	0.11	0.02	0.13	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	452	-93	-1021	-14	0	29	-636	4.02	4.02	4.02	4.02	3	0.09	0.03	0.18	0.00	0.00	22.3
2	452	-63	-821	15	0	-28	-559	4.02	4.02	4.02	4.02	2	0.08	0.02	0.15	0.00	0.00	22.3
3	452	-65	-819	15	0	-27	-556	4.02	4.02	4.02	4.02	2	0.08	0.02	0.15	0.00	0.00	22.3
4	452	-79	-751	-36	0	72	-422	4.02	4.02	4.02	4.02	2	0.06	0.02	0.13	0.00	0.00	22.3
5	452	-81	-749	-37	0	72	-419	4.02	4.02	4.02	4.02	2	0.06	0.02	0.13	0.00	0.00	22.3
6	452	-66	-798	-3	0	6	-514	4.02	4.02	4.02	4.02	2	0.08	0.02	0.14	0.00	0.00	22.3
7	452	-72	-794	-4	0	8	-506	4.02	4.02	4.02	4.02	2	0.08	0.02	0.14	0.00	0.00	22.3
8	452	-71	-777	-18	0	36	-473	4.02	4.02	4.02	4.02	2	0.07	0.02	0.14	0.00	0.00	22.3
9	452	-77	-773	-19	0	38	-465	4.02	4.02	4.02	4.02	2	0.07	0.02	0.14	0.00	0.00	22.3
10	452	-63	-821	15	0	-28	-559	4.02	4.02	4.02	4.02	2	0.08	0.02	0.15	0.00	0.00	22.3
11	452	-65	-819	15	0	-27	-556	4.02	4.02	4.02	4.02	2	0.08	0.02	0.15	0.00	0.00	22.3
12	452	-79	-751	-36	0	72	-422	4.02	4.02	4.02	4.02	2	0.06	0.02	0.13	0.00	0.00	22.3
13	452	-81	-749	-37	0	72	-419	4.02	4.02	4.02	4.02	2	0.06	0.02	0.13	0.00	0.00	22.3
14	452	-66	-798	-3	0	6	-514	4.02	4.02	4.02	4.02	2	0.08	0.02	0.14	0.00	0.00	22.3
15	452	-72	-794	-4	0	8	-506	4.02	4.02	4.02	4.02	2	0.08	0.02	0.14	0.00	0.00	22.3
16	452	-71	-777	-18	0	36	-473	4.02	4.02	4.02	4.02	2	0.07	0.02	0.14	0.00	0.00	22.3
17	452	-77	-773	-19	0	38	-465	4.02	4.02	4.02	4.02	2	0.07	0.02	0.14	0.00	0.00	22.3
18	452	-50	-1116	44	0	-88	-822	4.02	4.02	4.02	4.02	3	0.12	0.03	0.20	0.00	0.00	22.3
19	452	-103	-906	-112	0	216	507	4.02	4.02	4.02	4.02	3	0.07	0.03	0.16	0.00	0.00	22.3
20	452	-69	-1013	-40	0	77	-620	4.02	4.02	4.02	4.02	3	0.09	0.03	0.18	0.00	0.00	22.3
37	452	-38	-1189	102	0	-201	-965	4.02	4.02	4.02	4.02	3	0.14	0.03	0.21	0.00	0.00	22.3
38	452	-126	-839	-158	0	307	569	4.02	4.02	4.02	4.02	3	0.08	0.02	0.15	0.00	0.00	22.3
39	452	-70	-1018	-39	0	75	-629	4.02	4.02	4.02	4.02	3	0.09	0.03	0.18	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	509	-93	-1296	-14	0	37	-1430	4.02	4.02	4.02	4.02	3	0.20	0.04	0.23	0.00	0.00	22.3
2	509	-63	-1033	15	0	-37	-1190	4.02	4.02	4.02	4.02	2	0.18	0.03	0.18	0.00	0.00	22.3
3	509	-65	-1031	15	0	-36	-1186	4.02	4.02	4.02	4.02	2	0.18	0.03	0.18	0.00	0.00	22.3
4	509	-79	-963	-36	0	92	-1014	4.02	4.02	4.02	4.02	2	0.15	0.03	0.17	0.00	0.00	22.3
5	509	-81	-961	-37	0	93	-1009	4.02	4.02	4.02	4.02	2	0.15	0.03	0.17	0.00	0.00	22.3
6	509	-66	-1010	-3	0	8	-1132	4.02	4.02	4.02	4.02	2	0.17	0.03	0.18	0.00	0.00	22.3
7	509	-72	-1006	-4	0	10	-1121	4.02	4.02	4.02	4.02	2	0.17	0.03	0.18	0.00	0.00	22.3
8	509	-71	-989	-18	0	46	-1079	4.02	4.02	4.02	4.02	2	0.16	0.03	0.18	0.00	0.00	22.3
9	509	-77	-985	-19	0	49	-1068	4.02	4.02	4.02	4.02	2	0.16	0.03	0.18	0.00	0.00	22.3
10	509	-63	-1033	15	0	-37	-1190	4.02	4.02	4.02	4.02	2	0.18	0.03	0.18	0.00	0.00	22.3
11	509	-65	-1031	15	0	-36	-1186	4.02	4.02	4.02	4.02	2	0.18	0.03	0.18	0.00	0.00	22.3
12	509	-79	-963	-36	0	92	-1014	4.02	4.02	4.02	4.02	2	0.15	0.03	0.17	0.00	0.00	22.3
13	509	-81	-961	-37	0	93	-1009	4.02	4.02	4.02	4.02	2	0.15	0.03	0.17	0.00	0.00	22.3
14	509	-66	-1010	-3	0	8	-1132	4.02	4.02	4.02	4.02	2	0.17	0.03	0.18	0.00	0.00	22.3
15	509	-72	-1006	-4	0	10	-1121	4.02	4.02	4.02	4.02	2	0.17	0.03	0.18	0.00	0.00	22.3
16	509	-71	-989	-18	0	46	-1079	4.02	4.02	4.02	4.02	2	0.16	0.03	0.18	0.00	0.00	22.3
17	509	-77	-985	-19	0	49	-1068	4.02	4.02	4.02	4.02	2	0.16	0.03	0.18	0.00	0.00	22.3
18	509	-50	-1392	44	0	-113	-1670	4.02	4.02	4.02	4.02	3	0.24	0.04	0.25	0.00	0.00	22.3
19	509	-103	-1182	-112	0	280	-1140	4.02	4.02	4.02	4.02	3	0.16	0.03	0.21	0.00	0.00	22.3
20	509	-69	-1289	-40	0	100	-1410	4.02	4.02	4.02	4.02	3	0.20	0.04	0.23	0.00	0.00	22.3
37	509	-38	-1464	102	0	-258	-1854	4.02	4.02	4.02	4.02	3	0.27	0.04	0.26	0.00	0.00	22.3

38	509	-126	-1115	-158	0	396	-972	4.02	4.02	4.02	4.02	3	0.14	0.03	0.20	0.00	0.00	22.3
39	509	-70	-1294	-39	0	97	-1421	4.02	4.02	4.02	4.02	3	0.20	0.04	0.23	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	565	-93	-1572	-14	0	45	-1584	4.02	4.02	4.02	4.02	3	0.23	0.05	0.28	0.00	0.00	22.3
2	565	-63	-1245	15	0	-45	-1310	4.02	4.02	4.02	4.02	2	0.20	0.04	0.22	0.00	0.00	22.3
3	565	-65	-1243	15	0	-44	-1307	4.02	4.02	4.02	4.02	2	0.20	0.04	0.22	0.00	0.00	22.3
4	565	-79	-1175	-36	0	113	-1130	4.02	4.02	4.02	4.02	2	0.17	0.03	0.21	0.00	0.00	22.3
5	565	-81	-1173	-37	0	114	-1126	4.02	4.02	4.02	4.02	2	0.17	0.03	0.21	0.00	0.00	22.3
6	565	-66	-1222	-3	0	9	-1251	4.02	4.02	4.02	4.02	2	0.19	0.04	0.22	0.00	0.00	22.3
7	565	-72	-1218	-4	0	12	-1240	4.02	4.02	4.02	4.02	2	0.19	0.04	0.22	0.00	0.00	22.3
8	565	-71	-1201	-18	0	56	-1197	4.02	4.02	4.02	4.02	2	0.18	0.03	0.21	0.00	0.00	22.3
9	565	-77	-1197	-19	0	60	-1186	4.02	4.02	4.02	4.02	2	0.18	0.03	0.21	0.00	0.00	22.3
10	565	-63	-1245	15	0	-45	-1310	4.02	4.02	4.02	4.02	2	0.20	0.04	0.22	0.00	0.00	22.3
11	565	-65	-1243	15	0	-44	-1307	4.02	4.02	4.02	4.02	2	0.20	0.04	0.22	0.00	0.00	22.3
12	565	-79	-1175	-36	0	113	-1130	4.02	4.02	4.02	4.02	2	0.17	0.03	0.21	0.00	0.00	22.3
13	565	-81	-1173	-37	0	114	-1126	4.02	4.02	4.02	4.02	2	0.17	0.03	0.21	0.00	0.00	22.3
14	565	-66	-1222	-3	0	9	-1251	4.02	4.02	4.02	4.02	2	0.19	0.04	0.22	0.00	0.00	22.3
15	565	-72	-1218	-4	0	12	-1240	4.02	4.02	4.02	4.02	2	0.19	0.04	0.22	0.00	0.00	22.3
16	565	-71	-1201	-18	0	56	-1197	4.02	4.02	4.02	4.02	2	0.18	0.03	0.21	0.00	0.00	22.3
17	565	-77	-1197	-19	0	60	-1186	4.02	4.02	4.02	4.02	2	0.18	0.03	0.21	0.00	0.00	22.3
18	565	-50	-1667	44	0	-138	-1829	4.02	4.02	4.02	4.02	3	0.26	0.05	0.30	0.00	0.00	22.3
19	565	-103	-1457	-112	0	343	-1287	4.02	4.02	4.02	4.02	3	0.18	0.04	0.26	0.00	0.00	22.3
20	565	-69	-1564	-40	0	123	-1563	4.02	4.02	4.02	4.02	3	0.22	0.05	0.28	0.00	0.00	22.3
37	565	-38	-1740	102	0	-316	-2018	4.02	4.02	4.02	4.02	3	0.29	0.05	0.31	0.00	0.00	22.3
38	565	-126	-1390	-158	0	485	-1116	4.02	4.02	4.02	4.02	3	0.16	0.04	0.25	0.00	0.00	22.3
39	565	-70	-1569	-39	0	119	-1575	4.02	4.02	4.02	4.02	3	0.23	0.05	0.28	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

Nome travata: **trave_503_IP1** Descrizione: **Trave_5 8-13-18-23**
ASTA NUM. 8 NI 212 NF 123 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y qy tot.
qy medio: 375.00 375.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-21	1377	22	0	55	-1386	4.02	4.02	4.02	4.02	3	0.20	0.04	0.25	0.00	0.00	22.3
2	0	-28	1024	47	0	130	-975	4.02	4.02	4.02	4.02	2	0.15	0.03	0.18	0.00	0.00	22.3
3	0	-31	1024	47	0	130	-975	4.02	4.02	4.02	4.02	2	0.15	0.03	0.18	0.00	0.00	22.3
4	0	-2	1094	-13	0	-45	-1158	4.02	4.02	4.02	4.02	2	0.18	0.03	0.19	0.00	0.00	22.3
5	0	-4	1094	-14	0	-44	-1157	4.02	4.02	4.02	4.02	2	0.18	0.03	0.19	0.00	0.00	22.3
6	0	-16	1048	26	0	68	-1040	4.02	4.02	4.02	4.02	2	0.16	0.03	0.19	0.00	0.00	22.3
7	0	-24	1049	26	0	70	-1038	4.02	4.02	4.02	4.02	2	0.16	0.03	0.19	0.00	0.00	22.3
8	0	-8	1069	8	0	15	-1094	4.02	4.02	4.02	4.02	2	0.17	0.03	0.19	0.00	0.00	22.3
9	0	-16	1070	8	0	18	-1093	4.02	4.02	4.02	4.02	2	0.17	0.03	0.19	0.00	0.00	22.3
10	0	-28	1024	47	0	130	-975	4.02	4.02	4.02	4.02	2	0.15	0.03	0.18	0.00	0.00	22.3
11	0	-31	1024	47	0	130	-975	4.02	4.02	4.02	4.02	2	0.15	0.03	0.18	0.00	0.00	22.3
12	0	-2	1094	-13	0	-45	-1158	4.02	4.02	4.02	4.02	2	0.18	0.03	0.19	0.00	0.00	22.3
13	0	-4	1094	-14	0	-44	-1157	4.02	4.02	4.02	4.02	2	0.18	0.03	0.19	0.00	0.00	22.3
14	0	-16	1048	26	0	68	-1040	4.02	4.02	4.02	4.02	2	0.16	0.03	0.19	0.00	0.00	22.3
15	0	-24	1049	26	0	70	-1038	4.02	4.02	4.02	4.02	2	0.16	0.03	0.19	0.00	0.00	22.3
16	0	-8	1069	8	0	15	-1094	4.02	4.02	4.02	4.02	2	0.17	0.03	0.19	0.00	0.00	22.3
17	0	-16	1070	8	0	18	-1093	4.02	4.02	4.02	4.02	2	0.17	0.03	0.19	0.00	0.00	22.3
18	0	-36	1278	130	0	363	-1131	4.02	4.02	4.02	4.02	3	0.16	0.04	0.23	0.00	0.00	22.3
19	0	46	1486	-60	0	-185	-1672	4.02	4.02	4.02	4.02	3	0.24	0.04	0.26	0.00	0.00	22.3
20	0	12	1379	42	0	116	-1392	4.02	4.02	4.02	4.02	3	0.20	0.04	0.25	0.00	0.00	22.3
37	0	-71	1207	190	0	535	-946	4.02	4.02	4.02	4.02	3	0.14	0.03	0.21	0.00	0.00	22.3
38	0	65	1554	-128	0	-379	-1847	4.02	4.02	4.02	4.02	3	0.27	0.05	0.28	0.00	0.00	22.3
39	0	9	1376	42	0	123	-1382	4.02	4.02	4.02	4.02	3	0.20	0.04	0.25	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	57	-21	1102	22	0	43	-1244	4.02	4.02	4.02	4.02	3	0.18	0.03	0.20	0.00	0.00	22.3
2	57	-28	812	47	0	103	-868	4.02	4.02	4.02	4.02	2	0.13	0.02	0.14	0.00	0.00	22.3
3	57	-31	812	47	0	104	-867	4.02	4.02	4.02	4.02	2	0.13	0.02	0.14	0.00	0.00	22.3
4	57	-2	882	-13	0	-38	-1046	4.02	4.02	4.02	4.02	2	0.16	0.03	0.16	0.00	0.00	22.3
5	57	-4	882	-14	0	-37	-1045	4.02	4.02	4.02	4.02	2	0.16	0.03	0.16	0.00	0.00	22.3
6	57	-16	836	26	0	53	-931	4.02	4.02	4.02	4.02	2	0.14	0.02	0.15	0.00	0.00	22.3
7	57	-24	837	26	0	56	-929	4.02	4.02	4.02	4.02	2	0.14	0.02	0.15	0.00	0.00	22.3
8	57	-8	857	8	0	11	-984	4.02	4.02	4.02	4.02	2	0.15	0.02	0.15	0.00	0.00	22.3
9	57	-16	858	8	0	14	-983	4.02	4.02	4.02	4.02	2	0.15	0.02	0.15	0.00	0.00	22.3
10	57	-28	812	47	0	103	-868	4.02	4.02	4.02	4.02	2	0.13	0.02	0.14	0.00	0.00	22.3
11	57	-31	812	47	0	104	-867	4.02	4.02	4.02	4.02	2	0.13	0.02	0.14	0.00	0.00	22.3
12	57	-2	882	-13	0	-38	-1046	4.02	4.02	4.02	4.02	2	0.16	0.03	0.16	0.00	0.00	22.3
13	57	-4	882	-14	0	-37	-1045	4.02	4.02	4.02	4.02	2	0.16	0.03	0.16	0.00	0.00	22.3
14	57	-16	836	26	0	53	-931	4.02	4.02	4.02	4.02	2	0.14	0.02	0.15	0.00	0.00	22.3
15	57	-24	837	26	0	56	-929	4.02	4.02	4.02	4.02	2	0.14	0.02	0.15	0.00	0.00	22.3
16	57	-8	857	8	0	11	-984	4.02	4.02	4.02	4.02	2	0.15	0.02	0.15	0.00	0.00	22.3
17	57	-16	858	8	0	14	-983	4.02	4.02	4.02	4.02	2	0.15	0.02	0.15	0.00	0.00	22.3
18	57	-36	1003	130	0	289	-994	4.02	4.02	4.02	4.02	3	0.14	0.03	0.18	0.00	0.00	22.3
19	57	46	1211	-60	0	-151	-1523	4.02	4.02	4.02	4.02	3	0.22	0.04	0.22	0.00	0.00	22.3
20	57	12	1104	42	0	92	-1249	4.02	4.02	4.02	4.02	3	0.18	0.03	0.20	0.00	0.00	22.3
37	57	-71	932	190	0	428	-814	4.02	4.02	4.02	4.02	3	0.12	0.03	0.17	0.00	0.00	22.3
38	57	65	1278	-128	0	-307	-1694	4.02	4.02	4.02	4.02	3	0.24	0.04	0.23	0.00	0.00	22.3
39	57	9	1100	42	0	99	-1240	4.02	4.02	4.02	4.02	3	0.18	0.03	0.20	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	113	-21	826	22	0	31	-560	4.02	4.02	4.02	4.02	3	0.08	0.02	0.15	0.00	0.00	22.3
2	113	-28	600	47	0	76	-362	4.02	4.02	4.02	4.02	2	0.05	0.02	0.11	0.00	0.00	22.3
3	113	-31	600	47	0	77	-361	4.02	4.02	4.02	4.02	2	0.05	0.02	0.11	0.00	0.00	22.3
4	113	-2	670	-13	0	-30	-501	4.02	4.02	4.02	4.02	2	0.08	0.02	0.12	0.00	0.00	22.3
5	113	-4	670	-14	0	-29	-499	4.02	4.02	4.02	4.02	2	0.08	0.02	0.12	0.00	0.00	22.3
6	113	-16	624	26	0	38	-411	4.02	4.02	4.02	4.02	2	0.06	0.02	0.11	0.00	0.00	22.3
7	113	-24	625	26	0	41	-409	4.02	4.02	4.02	4.02	2	0.06	0.02	0.11	0.00	0.00	22.3
8	113	-8	645	8	0	6	-452	4.02	4.02	4.02	4.02	2	0.07	0.02	0.11	0.00	0.00	22.3
9	113	-16	646	8	0	9	-451	4.02	4.02	4.02	4.02	2	0.07	0.02	0.12	0.00	0.00	22.3
10	113	-28	600	47	0	76	-362	4.02	4.02	4.02	4.02	2	0.05	0.02	0.11	0.00	0.00	22.3
11	113	-31	600	47	0	77	-361	4.02	4.02	4.02	4.02	2	0.05	0.02	0.11	0.00	0.00	22.3
12	113	-2	670	-13	0	-30	-501	4.02	4.02	4.02	4.02	2	0.08	0.02	0.12	0.00	0.00	22.3
13	113	-4	670	-14	0	-29	-499	4.02	4.02	4.02	4.02	2	0.08	0.02	0.12	0.00	0.00	22.3

14	113	-16	624	26	0	38	-411	4.02	4.02	4.02	4.02	2	0.06	0.02	0.11	0.00	0.00	22.3
15	113	-24	625	26	0	41	-409	4.02	4.02	4.02	4.02	2	0.06	0.02	0.11	0.00	0.00	22.3
16	113	-8	645	8	0	6	-452	4.02	4.02	4.02	4.02	2	0.07	0.02	0.11	0.00	0.00	22.3
17	113	-16	646	8	0	9	-451	4.02	4.02	4.02	4.02	2	0.07	0.02	0.12	0.00	0.00	22.3
18	113	-36	727	130	0	215	370	4.02	4.02	4.02	4.02	3	0.05	0.02	0.13	0.00	0.00	22.3
19	113	46	935	-60	0	-118	-777	4.02	4.02	4.02	4.02	3	0.11	0.03	0.17	0.00	0.00	22.3
20	113	12	828	42	0	69	-564	4.02	4.02	4.02	4.02	3	0.08	0.02	0.15	0.00	0.00	22.3
37	113	-71	656	190	0	320	439	4.02	4.02	4.02	4.02	3	0.08	0.02	0.12	0.00	0.00	22.3
38	113	65	1003	-128	0	-235	-910	4.02	4.02	4.02	4.02	3	0.13	0.03	0.18	0.00	0.00	22.3
39	113	9	825	42	0	76	-556	4.02	4.02	4.02	4.02	3	0.08	0.02	0.15	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	170	-21	550	22	0	18	526	4.02	4.02	4.02	4.02	3	0.08	0.02	0.10	0.00	0.00	22.3
2	170	-28	388	47	0	50	418	4.02	4.02	4.02	4.02	2	0.06	0.01	0.07	0.00	0.00	22.3
3	170	-31	388	47	0	51	418	4.02	4.02	4.02	4.02	2	0.06	0.01	0.07	0.00	0.00	22.3
4	170	-2	458	-13	0	-22	390	4.02	4.02	4.02	4.02	2	0.06	0.01	0.08	0.00	0.00	22.3
5	170	-4	458	-14	0	-21	391	4.02	4.02	4.02	4.02	2	0.06	0.01	0.08	0.00	0.00	22.3
6	170	-16	412	26	0	23	407	4.02	4.02	4.02	4.02	2	0.06	0.01	0.07	0.00	0.00	22.3
7	170	-24	413	26	0	27	410	4.02	4.02	4.02	4.02	2	0.06	0.01	0.07	0.00	0.00	22.3
8	170	-8	433	8	0	2	399	4.02	4.02	4.02	4.02	2	0.06	0.01	0.08	0.00	0.00	22.3
9	170	-16	434	8	0	5	401	4.02	4.02	4.02	4.02	2	0.06	0.01	0.08	0.00	0.00	22.3
10	170	-28	388	47	0	50	418	4.02	4.02	4.02	4.02	2	0.06	0.01	0.07	0.00	0.00	22.3
11	170	-31	388	47	0	51	418	4.02	4.02	4.02	4.02	2	0.06	0.01	0.07	0.00	0.00	22.3
12	170	-2	458	-13	0	-22	390	4.02	4.02	4.02	4.02	2	0.06	0.01	0.08	0.00	0.00	22.3
13	170	-4	458	-14	0	-21	391	4.02	4.02	4.02	4.02	2	0.06	0.01	0.08	0.00	0.00	22.3
14	170	-16	412	26	0	23	407	4.02	4.02	4.02	4.02	2	0.06	0.01	0.07	0.00	0.00	22.3
15	170	-24	413	26	0	27	410	4.02	4.02	4.02	4.02	2	0.06	0.01	0.07	0.00	0.00	22.3
16	170	-8	433	8	0	2	399	4.02	4.02	4.02	4.02	2	0.06	0.01	0.08	0.00	0.00	22.3
17	170	-16	434	8	0	5	401	4.02	4.02	4.02	4.02	2	0.06	0.01	0.08	0.00	0.00	22.3
18	170	-36	452	130	0	142	535	4.02	4.02	4.02	4.02	3	0.08	0.01	0.08	0.00	0.00	22.3
19	170	46	660	-60	0	-84	481	4.02	4.02	4.02	4.02	3	0.07	0.02	0.12	0.00	0.00	22.3
20	170	12	553	42	0	45	525	4.02	4.02	4.02	4.02	3	0.08	0.02	0.10	0.00	0.00	22.3
37	170	-71	381	190	0	213	537	4.02	4.02	4.02	4.02	3	0.08	0.01	0.07	0.00	0.00	22.3
38	170	65	727	-128	0	-162	455	4.02	4.02	4.02	4.02	3	0.07	0.02	0.13	0.00	0.00	22.3
39	170	9	549	42	0	52	528	4.02	4.02	4.02	4.02	3	0.08	0.02	0.10	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	226	-21	275	22	0	6	557	4.02	4.02	4.02	4.02	3	0.08	0.01	0.05	0.00	0.00	22.3
2	226	-28	176	47	0	23	420	4.02	4.02	4.02	4.02	2	0.06	0.01	0.03	0.00	0.00	22.3
3	226	-31	176	47	0	24	421	4.02	4.02	4.02	4.02	2	0.06	0.01	0.03	0.00	0.00	22.3
4	226	-2	246	-13	0	-15	436	4.02	4.02	4.02	4.02	2	0.07	0.01	0.04	0.00	0.00	22.3
5	226	-4	246	-14	0	-14	437	4.02	4.02	4.02	4.02	2	0.07	0.01	0.04	0.00	0.00	22.3
6	226	-16	200	26	0	8	425	4.02	4.02	4.02	4.02	2	0.06	0.01	0.04	0.00	0.00	22.3
7	226	-24	201	26	0	12	427	4.02	4.02	4.02	4.02	2	0.06	0.01	0.04	0.00	0.00	22.3
8	226	-8	221	8	0	-3	430	4.02	4.02	4.02	4.02	2	0.07	0.01	0.04	0.00	0.00	22.3
9	226	-16	222	8	0	1	432	4.02	4.02	4.02	4.02	2	0.07	0.01	0.04	0.00	0.00	22.3
10	226	-28	176	47	0	23	420	4.02	4.02	4.02	4.02	2	0.06	0.01	0.03	0.00	0.00	22.3
11	226	-31	176	47	0	24	421	4.02	4.02	4.02	4.02	2	0.06	0.01	0.03	0.00	0.00	22.3
12	226	-2	246	-13	0	-15	436	4.02	4.02	4.02	4.02	2	0.07	0.01	0.04	0.00	0.00	22.3
13	226	-4	246	-14	0	-14	437	4.02	4.02	4.02	4.02	2	0.07	0.01	0.04	0.00	0.00	22.3
14	226	-16	200	26	0	8	425	4.02	4.02	4.02	4.02	2	0.06	0.01	0.04	0.00	0.00	22.3
15	226	-24	201	26	0	12	427	4.02	4.02	4.02	4.02	2	0.06	0.01	0.04	0.00	0.00	22.3
16	226	-8	221	8	0	-3	430	4.02	4.02	4.02	4.02	2	0.07	0.01	0.04	0.00	0.00	22.3
17	226	-16	222	8	0	1	432	4.02	4.02	4.02	4.02	2	0.07	0.01	0.04	0.00	0.00	22.3
18	226	-36	176	130	0	68	535	4.02	4.02	4.02	4.02	3	0.08	0.01	0.03	0.00	0.00	22.3
19	226	46	384	-60	0	-50	581	4.02	4.02	4.02	4.02	3	0.08	0.01	0.07	0.00	0.00	22.3
20	226	12	277	42	0	21	559	4.02	4.02	4.02	4.02	3	0.08	0.01	0.05	0.00	0.00	22.3
37	226	-71	105	190	0	106	537	4.02	4.02	4.02	4.02	3	0.08	0.01	0.03	0.00	0.00	22.3
38	226	65	452	-128	0	-90	619	4.02	4.02	4.02	4.02	3	0.09	0.01	0.08	0.00	0.00	22.3
39	226	9	274	42	0	29	559	4.02	4.02	4.02	4.02	3	0.08	0.01	0.05	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	283	-21	-0	22	0	-6	557	4.02	4.02	4.02	4.02	3	0.08	0.00	0.00	0.00	0.00	22.3
2	283	-28	-36	47	0	-4	420	4.02	4.02	4.02	4.02	2	0.06	0.00	0.01	0.00	0.00	22.3
3	283	-31	-36	47	0	-3	421	4.02	4.02	4.02	4.02	2	0.06	0.00	0.01	0.00	0.00	22.3
4	283	-2	34	-13	0	-7	436	4.02	4.02	4.02	4.02	2	0.07	0.00	0.01	0.00	0.00	22.3
5	283	-4	34	-14	0	-6	437	4.02	4.02	4.02	4.02	2	0.07	0.00	0.01	0.00	0.00	22.3
6	283	-16	-12	26	0	-6	425	4.02	4.02	4.02	4.02	2	0.06	0.00	0.00	0.00	0.00	22.3
7	283	-24	-10	26	0	-2	427	4.02	4.02	4.02	4.02	2	0.06	0.00	0.00	0.00	0.00	22.3
8	283	-8	10	8	0	-7	430	4.02	4.02	4.02	4.02	2	0.07	0.00	0.00	0.00	0.00	22.3
9	283	-16	10	8	0	-3	432	4.02	4.02	4.02	4.02	2	0.07	0.00	0.00	0.00	0.00	22.3
10	283	-28	-36	47	0	-4	420	4.02	4.02	4.02	4.02	2	0.06	0.00	0.01	0.00	0.00	22.3
11	283	-31	-36	47	0	-3	421	4.02	4.02	4.02	4.02	2	0.06	0.00	0.01	0.00	0.00	22.3
12	283	-2	34	-13	0	-7	436	4.02	4.02	4.02	4.02	2	0.07	0.00	0.01	0.00	0.00	22.3
13	283	-4	34	-14	0	-6	437	4.02	4.02	4.02	4.02	2	0.07	0.00	0.01	0.00	0.00	22.3
14	283	-16	-12	26	0	-6	425	4.02	4.02	4.02	4.02	2	0.06	0.00	0.00	0.00	0.00	22.3
15	283	-24	-10	26	0	-2	427	4.02	4.02	4.02	4.02	2	0.06	0.00	0.00	0.00	0.00	22.3
16	283	-8	10	8	0	-7	430	4.02	4.02	4.02	4.02	2	0.07	0.00	0.00	0.00	0.00	22.3
17	283	-16	10	8	0	-3	432	4.02	4.02	4.02	4.02	2	0.07	0.00	0.00	0.00	0.00	22.3
18	283	-36	-99	130	0	-6	535	4.02	4.02	4.02	4.02	3	0.08	0.00	0.02	0.00	0.00	22.3
19	283	46	109	-60	0	-17	581	4.02	4.02	4.02	4.02	3	0.08	0.00	0.02	0.00	0.00	22.3
20	283	12	2	42	0	-2	559	4.02	4.02	4.02	4.02	3	0.08	0.00	0.00	0.00	0.00	22.3
37	283	-71	-170	190	0	-1	537	4.02	4.02	4.02	4.02	3	0.08	0.01	0.03	0.00	0.00	22.3
38	283	65	176	-128	0	-18	619	4.02	4.02	4.02	4.02	3	0.09	0.01	0.03	0.00	0.00	22.3
39	283	9	-2	42	0	5	559	4.02	4.02	4.02	4.02	3	0.08	0.00	0.00	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	339	-21	-276	22	0	-19	557	4.02	4.02	4.02	4.02	3	0.08	0.01	0.05	0.00	0.00	22.3
2	339	-28	-247	47	0	-31	420	4.02	4.02	4.02	4.02	2	0.06	0.01	0.04	0.00	0.00	22.3
3	339	-31	-247	47	0	-29	421	4.02	4.02	4.02	4.02	2	0.06	0.01	0.04	0.00	0.00	22.3
4	339	-2	-177	-13	0	1	436	4.02	4.02	4.02	4.02	2	0.07	0.01	0.03	0.00	0.00	22.3
5	339	-4	-177	-14	0	2	437	4.02	4.02	4.02	4.02	2	0.07	0.01	0.03	0.00	0.00	22.3
6	339	-16	-223	26	0	-21	425	4.02	4.02	4.02	4.02	2	0.06	0.01	0.04	0.00	0.00	22.3
7	339	-24	-222	26	0	-17	427	4.02	4.02	4.02	4.02	2	0.06	0.01	0.04	0.00	0.00	22.3
8	339	-8	-202	8	0	-12	430	4.02	4.02	4.02	4.02	2	0.07	0.01	0.04	0.00	0.00	22.3
9	339	-16	-201	8	0	-8	432	4.02	4.02	4.02	4.02	2	0.07	0.01	0.04	0.00	0.00	22.3
10	339	-28	-247	47	0	-31	420	4.02	4.02	4.02	4.02	2	0.06	0.01	0.04	0.00	0.00	22.3
11	339	-31	-247	47	0	-29	421	4.02	4.02	4.02	4.02	2	0.06	0.01	0.04	0.00	0.00	22.3
12	339	-2	-177	-13	0	1	436	4.02	4.02	4.02	4.02	2	0.07	0.01	0.03	0.00	0.00	22.3
13	339	-4	-177	-14	0	2	437	4.02	4.02	4.02	4.02	2	0.07	0.01	0.03	0.00	0.00	22.3
14	339	-16	-223	26	0	-21	425	4.02	4.02	4.02	4.02	2	0.06	0.01	0.04	0.00	0.00	22.3
15	339	-24	-222	26	0	-17	427	4.02	4.02	4.02	4.02	2	0.06	0.01	0.04	0.00	0.00	22.3
16	339	-8	-202	8	0	-12	430	4.02	4.02	4.02	4.02	2	0.07	0.01	0.04	0.00	0.00	22.3
17	339	-16	-201	8	0	-8	432	4.02	4.02	4.02	4.02	2	0.07	0.01	0.04	0.00	0.00	22.3
18	339	-36	-374	130	0	-80	535	4.02	4.02	4.02	4.02	3	0.08	0.01	0.07	0.00	0.00	22.3
19	339	46	-166	-60	0	17	581	4.02	4.02	4.02	4.02	3	0.08	0.00	0.03	0.00	0.00	22.3

20	339	12	-273	42	0	-26	559	4.02	4.02	4.02	4.02	3	0.08	0.01	0.05	0.00	0.00	22.3
37	339	-71	-445	190	0	-108	537	4.02	4.02	4.02	4.02	3	0.08	0.01	0.08	0.00	0.00	22.3
38	339	65	-99	-128	0	54	619	4.02	4.02	4.02	4.02	3	0.09	0.00	0.02	0.00	0.00	22.3
39	339	9	-277	42	0	-18	559	4.02	4.02	4.02	4.02	3	0.08	0.01	0.05	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	396	-21	-552	22	0	-31	524	4.02	4.02	4.02	4.02	3	0.08	0.02	0.10	0.00	0.00	22.3
2	396	-28	-459	47	0	-57	373	4.02	4.02	4.02	4.02	2	0.06	0.01	0.08	0.00	0.00	22.3
3	396	-31	-459	47	0	-56	374	4.02	4.02	4.02	4.02	2	0.06	0.01	0.08	0.00	0.00	22.3
4	396	-2	-389	-13	0	8	433	4.02	4.02	4.02	4.02	2	0.07	0.01	0.07	0.00	0.00	22.3
5	396	-4	-389	-14	0	9	434	4.02	4.02	4.02	4.02	2	0.07	0.01	0.07	0.00	0.00	22.3
6	396	-16	-435	26	0	-36	393	4.02	4.02	4.02	4.02	2	0.06	0.01	0.08	0.00	0.00	22.3
7	396	-24	-434	26	0	-32	395	4.02	4.02	4.02	4.02	2	0.06	0.01	0.08	0.00	0.00	22.3
8	396	-8	-414	8	0	-16	411	4.02	4.02	4.02	4.02	2	0.06	0.01	0.07	0.00	0.00	22.3
9	396	-16	-413	8	0	-12	414	4.02	4.02	4.02	4.02	2	0.06	0.01	0.07	0.00	0.00	22.3
10	396	-28	-459	47	0	-57	373	4.02	4.02	4.02	4.02	2	0.06	0.01	0.08	0.00	0.00	22.3
11	396	-31	-459	47	0	-56	374	4.02	4.02	4.02	4.02	2	0.06	0.01	0.08	0.00	0.00	22.3
12	396	-2	-389	-13	0	8	433	4.02	4.02	4.02	4.02	2	0.07	0.01	0.07	0.00	0.00	22.3
13	396	-4	-389	-14	0	9	434	4.02	4.02	4.02	4.02	2	0.07	0.01	0.07	0.00	0.00	22.3
14	396	-16	-435	26	0	-36	393	4.02	4.02	4.02	4.02	2	0.06	0.01	0.08	0.00	0.00	22.3
15	396	-24	-434	26	0	-32	395	4.02	4.02	4.02	4.02	2	0.06	0.01	0.08	0.00	0.00	22.3
16	396	-8	-414	8	0	-16	411	4.02	4.02	4.02	4.02	2	0.06	0.01	0.07	0.00	0.00	22.3
17	396	-16	-413	8	0	-12	414	4.02	4.02	4.02	4.02	2	0.06	0.01	0.07	0.00	0.00	22.3
18	396	-36	-650	130	0	-153	441	4.02	4.02	4.02	4.02	3	0.06	0.02	0.12	0.00	0.00	22.3
19	396	46	-442	-60	0	51	581	4.02	4.02	4.02	4.02	3	0.08	0.01	0.08	0.00	0.00	22.3
20	396	12	-549	42	0	-50	528	4.02	4.02	4.02	4.02	3	0.08	0.02	0.10	0.00	0.00	22.3
37	396	-71	-721	189	0	-215	380	4.02	4.02	4.02	4.02	3	0.05	0.02	0.13	0.00	0.00	22.3
38	396	65	-375	-128	0	126	619	4.02	4.02	4.02	4.02	3	0.09	0.01	0.07	0.00	0.00	22.3
39	396	9	-553	42	0	-42	525	4.02	4.02	4.02	4.02	3	0.08	0.02	0.10	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	452	-21	-827	22	0	-43	-563	4.02	4.02	4.02	4.02	3	0.08	0.02	0.15	0.00	0.00	22.3
2	452	-28	-671	47	0	-84	-519	4.02	4.02	4.02	4.02	2	0.08	0.02	0.12	0.00	0.00	22.3
3	452	-31	-671	47	0	-83	-518	4.02	4.02	4.02	4.02	2	0.08	0.02	0.12	0.00	0.00	22.3
4	452	-2	-601	-13	0	16	-348	4.02	4.02	4.02	4.02	2	0.05	0.02	0.11	0.00	0.00	22.3
5	452	-4	-601	-14	0	17	-347	4.02	4.02	4.02	4.02	2	0.05	0.02	0.11	0.00	0.00	22.3
6	452	-16	-647	26	0	-51	-460	4.02	4.02	4.02	4.02	2	0.07	0.02	0.12	0.00	0.00	22.3
7	452	-24	-646	26	0	-46	-457	4.02	4.02	4.02	4.02	2	0.07	0.02	0.12	0.00	0.00	22.3
8	452	-8	-626	8	0	-21	-409	4.02	4.02	4.02	4.02	2	0.06	0.02	0.11	0.00	0.00	22.3
9	452	-16	-625	8	0	-16	-405	4.02	4.02	4.02	4.02	2	0.06	0.02	0.11	0.00	0.00	22.3
10	452	-28	-671	47	0	-84	-519	4.02	4.02	4.02	4.02	2	0.08	0.02	0.12	0.00	0.00	22.3
11	452	-31	-671	47	0	-83	-518	4.02	4.02	4.02	4.02	2	0.08	0.02	0.12	0.00	0.00	22.3
12	452	-2	-601	-13	0	16	-348	4.02	4.02	4.02	4.02	2	0.05	0.02	0.11	0.00	0.00	22.3
13	452	-4	-601	-14	0	17	-347	4.02	4.02	4.02	4.02	2	0.05	0.02	0.11	0.00	0.00	22.3
14	452	-16	-647	26	0	-51	-460	4.02	4.02	4.02	4.02	2	0.07	0.02	0.12	0.00	0.00	22.3
15	452	-24	-646	26	0	-46	-457	4.02	4.02	4.02	4.02	2	0.07	0.02	0.12	0.00	0.00	22.3
16	452	-8	-626	8	0	-21	-409	4.02	4.02	4.02	4.02	2	0.06	0.02	0.11	0.00	0.00	22.3
17	452	-16	-625	8	0	-16	-405	4.02	4.02	4.02	4.02	2	0.06	0.02	0.11	0.00	0.00	22.3
18	452	-36	-925	130	0	-227	-802	4.02	4.02	4.02	4.02	3	0.11	0.03	0.16	0.00	0.00	22.3
19	452	46	-717	-60	0	85	429	4.02	4.02	4.02	4.02	3	0.06	0.02	0.13	0.00	0.00	22.3
20	452	12	-824	42	0	-73	-555	4.02	4.02	4.02	4.02	3	0.08	0.02	0.15	0.00	0.00	22.3
37	452	-71	-996	190	0	-322	-974	4.02	4.02	4.02	4.02	3	0.14	0.03	0.18	0.00	0.00	22.3
38	452	65	-650	-128	0	198	525	4.02	4.02	4.02	4.02	3	0.08	0.02	0.12	0.00	0.00	22.3
39	452	9	-828	42	0	-65	-563	4.02	4.02	4.02	4.02	3	0.08	0.02	0.15	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	509	-21	-1102	22	0	-56	-1247	4.02	4.02	4.02	4.02	3	0.18	0.03	0.20	0.00	0.00	22.3
2	509	-28	-883	47	0	-111	-1065	4.02	4.02	4.02	4.02	2	0.16	0.03	0.16	0.00	0.00	22.3
3	509	-31	-883	47	0	-109	-1064	4.02	4.02	4.02	4.02	2	0.16	0.03	0.16	0.00	0.00	22.3
4	509	-2	-813	-13	0	23	-855	4.02	4.02	4.02	4.02	2	0.13	0.02	0.14	0.00	0.00	22.3
5	509	-4	-813	-14	0	25	-854	4.02	4.02	4.02	4.02	2	0.13	0.02	0.14	0.00	0.00	22.3
6	509	-16	-859	26	0	-65	-993	4.02	4.02	4.02	4.02	2	0.15	0.02	0.15	0.00	0.00	22.3
7	509	-24	-858	26	0	-61	-990	4.02	4.02	4.02	4.02	2	0.15	0.02	0.15	0.00	0.00	22.3
8	509	-8	-838	8	0	-25	-930	4.02	4.02	4.02	4.02	2	0.14	0.02	0.15	0.00	0.00	22.3
9	509	-16	-837	8	0	-21	-926	4.02	4.02	4.02	4.02	2	0.14	0.02	0.15	0.00	0.00	22.3
10	509	-28	-883	47	0	-111	-1065	4.02	4.02	4.02	4.02	2	0.16	0.03	0.16	0.00	0.00	22.3
11	509	-31	-883	47	0	-109	-1064	4.02	4.02	4.02	4.02	2	0.16	0.03	0.16	0.00	0.00	22.3
12	509	-2	-813	-13	0	23	-855	4.02	4.02	4.02	4.02	2	0.13	0.02	0.14	0.00	0.00	22.3
13	509	-4	-813	-14	0	25	-854	4.02	4.02	4.02	4.02	2	0.13	0.02	0.14	0.00	0.00	22.3
14	509	-16	-859	26	0	-65	-993	4.02	4.02	4.02	4.02	2	0.15	0.02	0.15	0.00	0.00	22.3
15	509	-24	-858	26	0	-61	-990	4.02	4.02	4.02	4.02	2	0.15	0.02	0.15	0.00	0.00	22.3
16	509	-8	-838	8	0	-25	-930	4.02	4.02	4.02	4.02	2	0.14	0.02	0.15	0.00	0.00	22.3
17	509	-16	-837	8	0	-21	-926	4.02	4.02	4.02	4.02	2	0.14	0.02	0.15	0.00	0.00	22.3
18	509	-36	-1201	130	0	-301	-1542	4.02	4.02	4.02	4.02	3	0.22	0.03	0.21	0.00	0.00	22.3
19	509	46	-993	-60	0	118	-920	4.02	4.02	4.02	4.02	3	0.13	0.03	0.18	0.00	0.00	22.3
20	509	12	-1100	42	0	-97	-1238	4.02	4.02	4.02	4.02	3	0.18	0.03	0.20	0.00	0.00	22.3
37	509	-71	-1272	190	0	-429	-1754	4.02	4.02	4.02	4.02	3	0.25	0.04	0.23	0.00	0.00	22.3
38	509	65	-926	-128	0	270	-717	4.02	4.02	4.02	4.02	3	0.10	0.03	0.16	0.00	0.00	22.3
39	509	9	-1104	42	0	-89	-1248	4.02	4.02	4.02	4.02	3	0.18	0.03	0.20	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	565	-21	-1378	22	0	-68	-1390	4.02	4.02	4.02	4.02	3	0.20	0.04	0.25	0.00	0.00	22.3
2	565	-28	-1095	47	0	-137	-1177	4.02	4.02	4.02	4.02	2	0.18	0.03	0.19	0.00	0.00	22.3
3	565	-31	-1095	47	0	-136	-1176	4.02	4.02	4.02	4.02	2	0.18	0.03	0.19	0.00	0.00	22.3
4	565	-2	-1025	-13	0	31	-963	4.02	4.02	4.02	4.02	2	0.15	0.03	0.18	0.00	0.00	22.3
5	565	-4	-1025	-14	0	32	-961	4.02	4.02	4.02	4.02	2	0.15	0.03	0.18	0.00	0.00	22.3
6	565	-16	-1071	26	0	-80	-1103	4.02	4.02	4.02	4.02	2	0.17	0.03	0.19	0.00	0.00	22.3
7	565	-24	-1070	26	0	-75	-1100	4.02	4.02	4.02	4.02	2	0.17	0.03	0.19	0.00	0.00	22.3
8	565	-8	-1050	8	0	-30	-1039	4.02	4.02	4.02	4.02	2	0.16	0.03	0.19	0.00	0.00	22.3
9	565	-16	-1049	8	0	-25	-1035	4.02	4.02	4.02	4.02	2	0.16	0.03	0.19	0.00	0.00	22.3
10	565	-28	-1095	47	0	-137	-1177	4.02	4.02	4.02	4.02	2	0.18	0.03	0.19	0.00	0.00	22.3
11	565	-31	-1095	47	0	-136	-1176	4.02	4.02	4.02	4.02	2	0.18	0.03	0.19	0.00	0.00	22.3
12	565	-2	-1025	-13	0	31	-963	4.02	4.02	4.02	4.02	2	0.15	0.03	0.18	0.00	0.00	22.3
13	565	-4	-1025	-14	0	32	-961	4.02	4.02	4.02	4.02	2	0.15	0.03	0.18	0.00	0.00	22.3
14	565	-16	-1071	26	0	-80	-1103	4.02	4.02	4.02	4.02	2	0.17	0.03	0.19	0.00	0.00	22.3
15	565	-24	-1070	26	0	-75	-1100	4.02	4.02	4.02	4.02	2	0.17	0.03	0.19	0.00	0.00	22.3
16	565	-8	-1050	8	0	-30	-1039	4.02	4.02	4.02	4.02	2	0.16	0.03	0.19	0.00	0.00	22.3
17	565	-16	-1049	8	0	-25	-1035	4.02	4.02	4.02	4.02	2	0.16	0.03	0.19	0.00	0.00	22.3
18	565	-36	-1476	130	0	-375	-1690	4.02	4.02	4.02	4.02	3	0.24	0.04	0.26	0.00	0.00	22.3
19	565	46	-1268	-60	0	152	-1056	4.02	4.02	4.02	4.02	3	0.15	0.04	0.23	0.00	0.00	22.3
20	565	12	-1375	42	0	-121	-1381	4.02	4.02	4.02	4.02	3	0.20	0.04	0.24	0.00	0.00	22.3
37	565	-71	-1547	190	0	-536	-1907	4.02	4.02	4.02	4.02	3	0.27	0.04	0.28	0.00	0.00	22.3
38	565	65	-1201	-128	0	342	-849	4.02	4.02	4.02	4.02	3	0.12	0.03	0.21	0.00	0.00	22.3
39	565	9	-1379	42	0	-112	-1391	4.02	4.02	4.02	4.02	3	0.20	0.04	0.25	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

Nome travata: **trave_503_IP1** Descrizione: **Trave_5 8-13-18-23**
ASTA NUM. 9 NI 123 NF 210 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y qy tot.
qy medio: 375.00 375.00 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-124	1590	-15	0	-47	-1644	4.02	4.02	4.02	4.02	3	0.23	0.05	0.28	0.00	0.00	22.3
2	0	-102	1185	10	0	27	-1156	4.02	4.02	4.02	4.02	2	0.17	0.03	0.21	0.00	0.00	22.3
3	0	-104	1183	15	0	41	-1152	4.02	4.02	4.02	4.02	2	0.17	0.03	0.21	0.00	0.00	22.3
4	0	-88	1262	-37	0	-112	-1378	4.02	4.02	4.02	4.02	2	0.21	0.04	0.22	0.00	0.00	22.3
5	0	-90	1261	-33	0	-99	-1374	4.02	4.02	4.02	4.02	2	0.21	0.04	0.22	0.00	0.00	22.3
6	0	-95	1214	-12	0	-38	-1239	4.02	4.02	4.02	4.02	2	0.19	0.04	0.22	0.00	0.00	22.3
7	0	-100	1209	3	0	8	-1224	4.02	4.02	4.02	4.02	2	0.18	0.04	0.21	0.00	0.00	22.3
8	0	-91	1237	-26	0	-80	-1306	4.02	4.02	4.02	4.02	2	0.20	0.04	0.22	0.00	0.00	22.3
9	0	-96	1232	-11	0	-34	-1291	4.02	4.02	4.02	4.02	2	0.20	0.04	0.22	0.00	0.00	22.3
10	0	-102	1185	10	0	27	-1156	4.02	4.02	4.02	4.02	2	0.17	0.03	0.21	0.00	0.00	22.3
11	0	-104	1183	15	0	41	-1152	4.02	4.02	4.02	4.02	2	0.17	0.03	0.21	0.00	0.00	22.3
12	0	-88	1262	-37	0	-112	-1378	4.02	4.02	4.02	4.02	2	0.21	0.04	0.22	0.00	0.00	22.3
13	0	-90	1261	-33	0	-99	-1374	4.02	4.02	4.02	4.02	2	0.21	0.04	0.22	0.00	0.00	22.3
14	0	-95	1214	-12	0	-38	-1239	4.02	4.02	4.02	4.02	2	0.19	0.04	0.22	0.00	0.00	22.3
15	0	-100	1209	3	0	8	-1224	4.02	4.02	4.02	4.02	2	0.18	0.04	0.21	0.00	0.00	22.3
16	0	-91	1237	-26	0	-80	-1306	4.02	4.02	4.02	4.02	2	0.20	0.04	0.22	0.00	0.00	22.3
17	0	-96	1232	-11	0	-34	-1291	4.02	4.02	4.02	4.02	2	0.20	0.04	0.22	0.00	0.00	22.3
18	0	-140	1487	38	0	100	-1348	4.02	4.02	4.02	4.02	3	0.19	0.04	0.26	0.00	0.00	22.3
19	0	-100	1715	-98	0	-291	-2000	4.02	4.02	4.02	4.02	3	0.29	0.05	0.30	0.00	0.00	22.3
20	0	-118	1591	4	0	8	-1646	4.02	4.02	4.02	4.02	3	0.24	0.05	0.28	0.00	0.00	22.3
37	0	-154	1407	88	0	247	-1120	4.02	4.02	4.02	4.02	3	0.16	0.04	0.25	0.00	0.00	22.3
38	0	-89	1787	-138	0	-405	-2208	4.02	4.02	4.02	4.02	3	0.32	0.05	0.32	0.00	0.00	22.3
39	0	-119	1581	32	0	94	-1618	4.02	4.02	4.02	4.02	3	0.23	0.05	0.28	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	56	-124	1314	-15	0	-38	-1489	4.02	4.02	4.02	4.02	3	0.21	0.04	0.23	0.00	0.00	22.3
2	56	-102	973	10	0	21	-1039	4.02	4.02	4.02	4.02	2	0.16	0.03	0.17	0.00	0.00	22.3
3	56	-104	971	15	0	32	-1035	4.02	4.02	4.02	4.02	2	0.16	0.03	0.17	0.00	0.00	22.3
4	56	-88	1050	-37	0	-91	-1256	4.02	4.02	4.02	4.02	2	0.19	0.03	0.19	0.00	0.00	22.3
5	56	-90	1049	-33	0	-80	-1253	4.02	4.02	4.02	4.02	2	0.19	0.03	0.19	0.00	0.00	22.3
6	56	-95	1002	-12	0	-31	-1120	4.02	4.02	4.02	4.02	2	0.17	0.03	0.18	0.00	0.00	22.3
7	56	-100	997	3	0	6	-1106	4.02	4.02	4.02	4.02	2	0.17	0.03	0.18	0.00	0.00	22.3
8	56	-91	1025	-26	0	-65	-1186	4.02	4.02	4.02	4.02	2	0.18	0.03	0.18	0.00	0.00	22.3
9	56	-96	1020	-11	0	-28	-1171	4.02	4.02	4.02	4.02	2	0.18	0.03	0.18	0.00	0.00	22.3
10	56	-102	973	10	0	21	-1039	4.02	4.02	4.02	4.02	2	0.16	0.03	0.17	0.00	0.00	22.3
11	56	-104	971	15	0	32	-1035	4.02	4.02	4.02	4.02	2	0.16	0.03	0.17	0.00	0.00	22.3
12	56	-88	1050	-37	0	-91	-1256	4.02	4.02	4.02	4.02	2	0.19	0.03	0.19	0.00	0.00	22.3
13	56	-90	1049	-33	0	-80	-1253	4.02	4.02	4.02	4.02	2	0.19	0.03	0.19	0.00	0.00	22.3
14	56	-95	1002	-12	0	-31	-1120	4.02	4.02	4.02	4.02	2	0.17	0.03	0.18	0.00	0.00	22.3
15	56	-100	997	3	0	6	-1106	4.02	4.02	4.02	4.02	2	0.17	0.03	0.18	0.00	0.00	22.3
16	56	-91	1025	-26	0	-65	-1186	4.02	4.02	4.02	4.02	2	0.18	0.03	0.18	0.00	0.00	22.3
17	56	-96	1020	-11	0	-28	-1171	4.02	4.02	4.02	4.02	2	0.18	0.03	0.18	0.00	0.00	22.3
18	56	-140	1212	38	0	79	-1199	4.02	4.02	4.02	4.02	3	0.17	0.04	0.22	0.00	0.00	22.3
19	56	-100	1440	-98	0	-236	-1838	4.02	4.02	4.02	4.02	3	0.26	0.04	0.26	0.00	0.00	22.3
20	56	-118	1316	4	0	6	-1491	4.02	4.02	4.02	4.02	3	0.21	0.04	0.23	0.00	0.00	22.3
37	56	-154	1132	88	0	197	-976	4.02	4.02	4.02	4.02	3	0.14	0.03	0.20	0.00	0.00	22.3
38	56	-89	1512	-138	0	-327	-2041	4.02	4.02	4.02	4.02	3	0.29	0.04	0.27	0.00	0.00	22.3
39	56	-119	1306	32	0	76	-1463	4.02	4.02	4.02	4.02	3	0.21	0.04	0.23	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	113	-124	1039	-15	0	-30	-685	4.02	4.02	4.02	4.02	3	0.10	0.03	0.18	0.00	0.00	22.3
2	113	-102	761	10	0	15	-442	4.02	4.02	4.02	4.02	2	0.07	0.02	0.14	0.00	0.00	22.3
3	113	-104	759	15	0	24	-439	4.02	4.02	4.02	4.02	2	0.07	0.02	0.13	0.00	0.00	22.3
4	113	-88	838	-37	0	-70	-615	4.02	4.02	4.02	4.02	2	0.09	0.02	0.15	0.00	0.00	22.3
5	113	-90	837	-33	0	-62	-612	4.02	4.02	4.02	4.02	2	0.09	0.02	0.15	0.00	0.00	22.3
6	113	-95	790	-12	0	-25	-507	4.02	4.02	4.02	4.02	2	0.08	0.02	0.14	0.00	0.00	22.3
7	113	-100	785	3	0	4	-495	4.02	4.02	4.02	4.02	2	0.07	0.02	0.14	0.00	0.00	22.3
8	113	-91	813	-26	0	-50	-559	4.02	4.02	4.02	4.02	2	0.08	0.02	0.14	0.00	0.00	22.3
9	113	-96	808	-11	0	-22	-547	4.02	4.02	4.02	4.02	2	0.08	0.02	0.14	0.00	0.00	22.3
10	113	-102	761	10	0	15	-442	4.02	4.02	4.02	4.02	2	0.07	0.02	0.14	0.00	0.00	22.3
11	113	-104	759	15	0	24	-439	4.02	4.02	4.02	4.02	2	0.07	0.02	0.13	0.00	0.00	22.3
12	113	-88	838	-37	0	-70	-615	4.02	4.02	4.02	4.02	2	0.09	0.02	0.15	0.00	0.00	22.3
13	113	-90	837	-33	0	-62	-612	4.02	4.02	4.02	4.02	2	0.09	0.02	0.15	0.00	0.00	22.3
14	113	-95	790	-12	0	-25	-507	4.02	4.02	4.02	4.02	2	0.08	0.02	0.14	0.00	0.00	22.3
15	113	-100	785	3	0	4	-495	4.02	4.02	4.02	4.02	2	0.07	0.02	0.14	0.00	0.00	22.3
16	113	-91	813	-26	0	-50	-559	4.02	4.02	4.02	4.02	2	0.08	0.02	0.14	0.00	0.00	22.3
17	113	-96	808	-11	0	-22	-547	4.02	4.02	4.02	4.02	2	0.08	0.02	0.14	0.00	0.00	22.3
18	113	-140	936	38	0	58	495	4.02	4.02	4.02	4.02	3	0.07	0.03	0.17	0.00	0.00	22.3
19	113	-100	1164	-98	0	-180	-963	4.02	4.02	4.02	4.02	3	0.14	0.03	0.21	0.00	0.00	22.3
20	113	-118	1040	4	0	4	-686	4.02	4.02	4.02	4.02	3	0.10	0.03	0.18	0.00	0.00	22.3
37	113	-154	856	88	0	147	592	4.02	4.02	4.02	4.02	3	0.08	0.02	0.15	0.00	0.00	22.3
38	113	-89	1236	-138	0	-249	-1125	4.02	4.02	4.02	4.02	3	0.16	0.04	0.22	0.00	0.00	22.3
39	113	-119	1030	32	0	58	-664	4.02	4.02	4.02	4.02	3	0.09	0.03	0.18	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	169	-124	764	-15	0	-22	737	4.02	4.02	4.02	4.02	3	0.11	0.02	0.14	0.00	0.00	22.3
2	169	-102	549	10	0	9	592	4.02	4.02	4.02	4.02	2	0.09	0.02	0.10	0.00	0.00	22.3
3	169	-104	547	15	0	15	592	4.02	4.02	4.02	4.02	2	0.09	0.02	0.10	0.00	0.00	22.3
4	169	-88	627	-37	0	-49	540	4.02	4.02	4.02	4.02	2	0.08	0.02	0.11	0.00	0.00	22.3
5	169	-90	625	-33	0	-43	541	4.02	4.02	4.02	4.02	2	0.08	0.02	0.11	0.00	0.00	22.3
6	169	-95	578	-12	0	-18	573	4.02	4.02	4.02	4.02	2	0.09	0.02	0.10	0.00	0.00	22.3
7	169	-100	573	3	0	2	576	4.02	4.02	4.02	4.02	2	0.09	0.02	0.10	0.00	0.00	22.3
8	169	-91	601	-26	0	-36	557	4.02	4.02	4.02	4.02	2	0.08	0.02	0.11	0.00	0.00	22.3
9	169	-96	596	-11	0	-15	560	4.02	4.02	4.02	4.02	2	0.08	0.02	0.11	0.00	0.00	22.3
10	169	-102	549	10	0	9	592	4.02	4.02	4.02	4.02	2	0.09	0.02	0.10	0.00	0.00	22.3
11	169	-104	547	15	0	15	592	4.02	4.02	4.02	4.02	2	0.09	0.02	0.10	0.00	0.00	22.3
12	169	-88	627	-37	0	-49	540	4.02	4.02	4.02	4.02	2	0.08	0.02	0.11	0.00	0.00	22.3
13	169	-90	625	-33	0	-43	541	4.02	4.02	4.02	4.02	2	0.08	0.02	0.11	0.00	0.00	22.3
14	169	-95	578	-12	0	-18	573	4.02	4.02	4.02	4.02	2	0.09	0.02	0.10	0.00	0.00	22.3
15	169	-100	573	3	0	2	576	4.02	4.02	4.02	4.02	2	0.09	0.02	0.10	0.00	0.00	22.3
16	169	-91	601	-26	0	-36	557	4.02	4.02	4.02	4.02	2	0.08	0.02	0.11	0.00	0.00	22.3
17	169	-96	596	-11	0	-15	560	4.02	4.02	4.02	4.02	2	0.08	0.02	0.11	0.00	0.00	22.3

18	169	-140	661	38	0	36	806	4.02	4.02	4.02	4.02	3	0.12	0.02	0.12	0.00	0.00	22.3
19	169	-100	889	-98	0	-125	657	4.02	4.02	4.02	4.02	3	0.09	0.03	0.16	0.00	0.00	22.3
20	169	-118	765	4	0	2	738	4.02	4.02	4.02	4.02	3	0.11	0.02	0.14	0.00	0.00	22.3
37	169	-154	581	88	0	98	859	4.02	4.02	4.02	4.02	3	0.12	0.02	0.10	0.00	0.00	22.3
38	169	-89	961	-138	0	-171	608	4.02	4.02	4.02	4.02	3	0.09	0.03	0.17	0.00	0.00	22.3
39	169	-119	755	32	0	40	744	4.02	4.02	4.02	4.02	3	0.11	0.02	0.13	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	226	-124	488	-15	0	-13	944	4.02	4.02	4.02	4.02	3	0.13	0.01	0.09	0.00	0.00	22.3
2	226	-102	337	10	0	3	706	4.02	4.02	4.02	4.02	2	0.11	0.01	0.06	0.00	0.00	22.3
3	226	-104	336	15	0	7	705	4.02	4.02	4.02	4.02	2	0.11	0.01	0.06	0.00	0.00	22.3
4	226	-88	415	-37	0	-28	727	4.02	4.02	4.02	4.02	2	0.11	0.01	0.07	0.00	0.00	22.3
5	226	-90	413	-33	0	-24	727	4.02	4.02	4.02	4.02	2	0.11	0.01	0.07	0.00	0.00	22.3
6	226	-95	366	-12	0	-12	721	4.02	4.02	4.02	4.02	2	0.11	0.01	0.07	0.00	0.00	22.3
7	226	-100	361	3	0	0	719	4.02	4.02	4.02	4.02	2	0.11	0.01	0.06	0.00	0.00	22.3
8	226	-91	390	-26	0	-21	730	4.02	4.02	4.02	4.02	2	0.11	0.01	0.07	0.00	0.00	22.3
9	226	-96	384	-11	0	-9	730	4.02	4.02	4.02	4.02	2	0.11	0.01	0.07	0.00	0.00	22.3
10	226	-102	337	10	0	3	706	4.02	4.02	4.02	4.02	2	0.11	0.01	0.06	0.00	0.00	22.3
11	226	-104	336	15	0	7	705	4.02	4.02	4.02	4.02	2	0.11	0.01	0.06	0.00	0.00	22.3
12	226	-88	415	-37	0	-28	727	4.02	4.02	4.02	4.02	2	0.11	0.01	0.07	0.00	0.00	22.3
13	226	-90	413	-33	0	-24	727	4.02	4.02	4.02	4.02	2	0.11	0.01	0.07	0.00	0.00	22.3
14	226	-95	366	-12	0	-12	721	4.02	4.02	4.02	4.02	2	0.11	0.01	0.07	0.00	0.00	22.3
15	226	-100	361	3	0	0	719	4.02	4.02	4.02	4.02	2	0.11	0.01	0.06	0.00	0.00	22.3
16	226	-91	390	-26	0	-21	730	4.02	4.02	4.02	4.02	2	0.11	0.01	0.07	0.00	0.00	22.3
17	226	-96	384	-11	0	-9	730	4.02	4.02	4.02	4.02	2	0.11	0.01	0.07	0.00	0.00	22.3
18	226	-140	385	38	0	15	907	4.02	4.02	4.02	4.02	3	0.13	0.01	0.07	0.00	0.00	22.3
19	226	-100	613	-98	0	-69	941	4.02	4.02	4.02	4.02	3	0.13	0.02	0.11	0.00	0.00	22.3
20	226	-118	489	4	0	-0	948	4.02	4.02	4.02	4.02	3	0.14	0.01	0.09	0.00	0.00	22.3
37	226	-154	305	88	0	48	910	4.02	4.02	4.02	4.02	3	0.13	0.01	0.05	0.00	0.00	22.3
38	226	-89	685	-138	0	-92	933	4.02	4.02	4.02	4.02	3	0.13	0.02	0.12	0.00	0.00	22.3
39	226	-119	479	32	0	22	942	4.02	4.02	4.02	4.02	3	0.13	0.01	0.09	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	282	-124	212	-15	0	-5	944	4.02	4.02	4.02	4.02	3	0.13	0.01	0.04	0.00	0.00	22.3
2	282	-102	126	10	0	-2	706	4.02	4.02	4.02	4.02	2	0.11	0.00	0.02	0.00	0.00	22.3
3	282	-104	124	15	0	-1	705	4.02	4.02	4.02	4.02	2	0.11	0.00	0.02	0.00	0.00	22.3
4	282	-88	203	-37	0	-7	747	4.02	4.02	4.02	4.02	2	0.11	0.01	0.04	0.00	0.00	22.3
5	282	-90	202	-33	0	-6	746	4.02	4.02	4.02	4.02	2	0.11	0.01	0.04	0.00	0.00	22.3
6	282	-95	155	-12	0	-5	721	4.02	4.02	4.02	4.02	2	0.11	0.00	0.03	0.00	0.00	22.3
7	282	-100	149	3	0	-2	719	4.02	4.02	4.02	4.02	2	0.11	0.00	0.03	0.00	0.00	22.3
8	282	-91	178	-26	0	-6	733	4.02	4.02	4.02	4.02	2	0.11	0.01	0.03	0.00	0.00	22.3
9	282	-96	173	-11	0	-3	731	4.02	4.02	4.02	4.02	2	0.11	0.01	0.03	0.00	0.00	22.3
10	282	-102	126	10	0	-2	706	4.02	4.02	4.02	4.02	2	0.11	0.00	0.02	0.00	0.00	22.3
11	282	-104	124	15	0	-1	705	4.02	4.02	4.02	4.02	2	0.11	0.00	0.02	0.00	0.00	22.3
12	282	-88	203	-37	0	-7	747	4.02	4.02	4.02	4.02	2	0.11	0.01	0.04	0.00	0.00	22.3
13	282	-90	202	-33	0	-6	746	4.02	4.02	4.02	4.02	2	0.11	0.01	0.04	0.00	0.00	22.3
14	282	-95	155	-12	0	-5	721	4.02	4.02	4.02	4.02	2	0.11	0.00	0.03	0.00	0.00	22.3
15	282	-100	149	3	0	-2	719	4.02	4.02	4.02	4.02	2	0.11	0.00	0.03	0.00	0.00	22.3
16	282	-91	178	-26	0	-6	733	4.02	4.02	4.02	4.02	2	0.11	0.01	0.03	0.00	0.00	22.3
17	282	-96	173	-11	0	-3	731	4.02	4.02	4.02	4.02	2	0.11	0.01	0.03	0.00	0.00	22.3
18	282	-140	110	38	0	-6	907	4.02	4.02	4.02	4.02	3	0.13	0.00	0.02	0.00	0.00	22.3
19	282	-100	338	-98	0	-13	1013	4.02	4.02	4.02	4.02	3	0.14	0.01	0.06	0.00	0.00	22.3
20	282	-118	214	4	0	-2	948	4.02	4.02	4.02	4.02	3	0.14	0.01	0.04	0.00	0.00	22.3
37	282	-154	30	88	0	-2	910	4.02	4.02	4.02	4.02	3	0.13	0.00	0.01	0.00	0.00	22.3
38	282	-89	410	-138	0	-14	1050	4.02	4.02	4.02	4.02	3	0.15	0.01	0.07	0.00	0.00	22.3
39	282	-119	204	32	0	4	942	4.02	4.02	4.02	4.02	3	0.13	0.01	0.04	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	339	-124	-63	-15	0	3	944	4.02	4.02	4.02	4.02	3	0.13	0.00	0.01	0.00	0.00	22.3
2	339	-102	-86	10	0	-8	706	4.02	4.02	4.02	4.02	2	0.11	0.00	0.02	0.00	0.00	22.3
3	339	-104	-88	15	0	-10	705	4.02	4.02	4.02	4.02	2	0.11	0.00	0.02	0.00	0.00	22.3
4	339	-88	-9	-37	0	14	747	4.02	4.02	4.02	4.02	2	0.11	0.00	0.00	0.00	0.00	22.3
5	339	-90	-10	-33	0	13	746	4.02	4.02	4.02	4.02	2	0.11	0.00	0.00	0.00	0.00	22.3
6	339	-95	-57	-12	0	1	721	4.02	4.02	4.02	4.02	2	0.11	0.00	0.01	0.00	0.00	22.3
7	339	-100	-62	3	0	-3	719	4.02	4.02	4.02	4.02	2	0.11	0.00	0.01	0.00	0.00	22.3
8	339	-91	-34	-26	0	8	733	4.02	4.02	4.02	4.02	2	0.11	0.00	0.01	0.00	0.00	22.3
9	339	-96	-39	-11	0	3	731	4.02	4.02	4.02	4.02	2	0.11	0.00	0.01	0.00	0.00	22.3
10	339	-102	-86	10	0	-8	706	4.02	4.02	4.02	4.02	2	0.11	0.00	0.02	0.00	0.00	22.3
11	339	-104	-88	15	0	-10	705	4.02	4.02	4.02	4.02	2	0.11	0.00	0.02	0.00	0.00	22.3
12	339	-88	-9	-37	0	14	747	4.02	4.02	4.02	4.02	2	0.11	0.00	0.00	0.00	0.00	22.3
13	339	-90	-10	-33	0	13	746	4.02	4.02	4.02	4.02	2	0.11	0.00	0.00	0.00	0.00	22.3
14	339	-95	-57	-12	0	1	721	4.02	4.02	4.02	4.02	2	0.11	0.00	0.01	0.00	0.00	22.3
15	339	-100	-62	3	0	-3	719	4.02	4.02	4.02	4.02	2	0.11	0.00	0.01	0.00	0.00	22.3
16	339	-91	-34	-26	0	8	733	4.02	4.02	4.02	4.02	2	0.11	0.00	0.01	0.00	0.00	22.3
17	339	-96	-39	-11	0	3	731	4.02	4.02	4.02	4.02	2	0.11	0.00	0.01	0.00	0.00	22.3
18	339	-140	-166	38	0	-27	907	4.02	4.02	4.02	4.02	3	0.13	0.00	0.03	0.00	0.00	22.3
19	339	-100	63	-98	0	42	1013	4.02	4.02	4.02	4.02	3	0.14	0.00	0.01	0.00	0.00	22.3
20	339	-118	-61	4	0	-5	948	4.02	4.02	4.02	4.02	3	0.14	0.00	0.01	0.00	0.00	22.3
37	339	-154	-245	88	0	-52	910	4.02	4.02	4.02	4.02	3	0.13	0.01	0.04	0.00	0.00	22.3
38	339	-89	135	-138	0	64	1050	4.02	4.02	4.02	4.02	3	0.15	0.00	0.02	0.00	0.00	22.3
39	339	-119	-71	32	0	-14	942	4.02	4.02	4.02	4.02	3	0.13	0.00	0.01	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	395	-124	-338	-15	0	11	944	4.02	4.02	4.02	4.02	3	0.13	0.01	0.06	0.00	0.00	22.3
2	395	-102	-298	10	0	-14	706	4.02	4.02	4.02	4.02	2	0.11	0.01	0.05	0.00	0.00	22.3
3	395	-104	-300	15	0	-18	705	4.02	4.02	4.02	4.02	2	0.11	0.01	0.05	0.00	0.00	22.3
4	395	-88	-221	-37	0	36	747	4.02	4.02	4.02	4.02	2	0.11	0.01	0.04	0.00	0.00	22.3
5	395	-90	-222	-33	0	32	746	4.02	4.02	4.02	4.02	2	0.11	0.01	0.04	0.00	0.00	22.3
6	395	-95	-269	-12	0	8	721	4.02	4.02	4.02	4.02	2	0.11	0.01	0.05	0.00	0.00	22.3
7	395	-100	-274	3	0	-5	719	4.02	4.02	4.02	4.02	2	0.11	0.01	0.05	0.00	0.00	22.3
8	395	-91	-246	-26	0	23	733	4.02	4.02	4.02	4.02	2	0.11	0.01	0.04	0.00	0.00	22.3
9	395	-96	-251	-11	0	10	731	4.02	4.02	4.02	4.02	2	0.11	0.01	0.04	0.00	0.00	22.3
10	395	-102	-298	10	0	-14	706	4.02	4.02	4.02	4.02	2	0.11	0.01	0.05	0.00	0.00	22.3
11	395	-104	-300	15	0	-18	705	4.02	4.02	4.02	4.02	2	0.11	0.01	0.05	0.00	0.00	22.3
12	395	-88	-221	-37	0	36	747	4.02	4.02	4.02	4.02	2	0.11	0.01	0.04	0.00	0.00	22.3
13	395	-90	-222	-33	0	32	746	4.02	4.02	4.02	4.02	2	0.11	0.01	0.04	0.00	0.00	22.3
14	395	-95	-269	-12	0	8	721	4.02	4.02	4.02	4.02	2	0.11	0.01	0.05	0.00	0.00	22.3
15	395	-100	-274	3	0	-5	719	4.02	4.02	4.02	4.02	2	0.11	0.01	0.05	0.00	0.00	22.3
16	395	-91	-246	-26	0	23	733	4.02	4.02	4.02	4.02	2	0.11	0.01	0.04	0.00	0.00	22.3
17	395	-96	-251	-11	0	10	731	4.02	4.02	4.02	4.02	2	0.11	0.01	0.04	0.00	0.00	22.3
18	395	-140	-441	38	0	-49	907	4.02	4.02	4.02	4.02	3	0.13	0.01	0.08	0.00	0.00	22.3
19	395	-100	-213	-98	0	98	1013	4.02	4.02	4.02	4.02	3	0.14	0.01	0.04	0.00	0.00	22.3
20	395	-118	-337	4	0	-7	948	4.02	4.02	4.02	4.02	3	0.14	0.01	0.06	0.00	0.00	22.3
37	395	-154	-521	88	0	-102	896	4.02	4.02	4.02	4.02	3	0.13	0.02	0.09	0.00	0.00	22.3
38	395	-89	-141	-138	0	142	1050	4.02	4.02	4.02	4.02	3	0.15	0.00	0.03	0.00	0.00	22.3
39	395	-119	-347	32	0	-32	942	4.02	4.02	4.02	4.02	3	0.13	0.01	0.06	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	452	-124	-614	-15	0	20	872	4.02	4.02	4.02	4.02	3	0.12	0.02	0.11	0.00	0.00	22.3
2	452	-102	-510	10	0	-20	627	4.02	4.02	4.02	4.02	2	0.09	0.01	0.09	0.00	0.00	22.3
3	452	-104	-512	15	0	-26	625	4.02	4.02	4.02	4.02	2	0.09	0.01	0.09	0.00	0.00	22.3
4	452	-88	-433	-37	0	57	716	4.02	4.02	4.02	4.02	2	0.11	0.01	0.08	0.00	0.00	22.3
5	452	-90	-434	-33	0	50	714	4.02	4.02	4.02	4.02	2	0.11	0.01	0.08	0.00	0.00	22.3
6	452	-95	-481	-12	0	14	661	4.02	4.02	4.02	4.02	2	0.10	0.01	0.09	0.00	0.00	22.3
7	452	-100	-486	3	0	-7	655	4.02	4.02	4.02	4.02	2	0.10	0.01	0.09	0.00	0.00	22.3
8	452	-91	-458	-26	0	37	687	4.02	4.02	4.02	4.02	2	0.10	0.01	0.08	0.00	0.00	22.3
9	452	-96	-463	-11	0	16	681	4.02	4.02	4.02	4.02	2	0.10	0.01	0.08	0.00	0.00	22.3
10	452	-102	-510	10	0	-20	627	4.02	4.02	4.02	4.02	2	0.09	0.01	0.09	0.00	0.00	22.3
11	452	-104	-512	15	0	-26	625	4.02	4.02	4.02	4.02	2	0.09	0.01	0.09	0.00	0.00	22.3
12	452	-88	-433	-37	0	57	716	4.02	4.02	4.02	4.02	2	0.11	0.01	0.08	0.00	0.00	22.3
13	452	-90	-434	-33	0	50	714	4.02	4.02	4.02	4.02	2	0.11	0.01	0.08	0.00	0.00	22.3
14	452	-95	-481	-12	0	14	661	4.02	4.02	4.02	4.02	2	0.10	0.01	0.09	0.00	0.00	22.3
15	452	-100	-486	3	0	-7	655	4.02	4.02	4.02	4.02	2	0.10	0.01	0.09	0.00	0.00	22.3
16	452	-91	-458	-26	0	37	687	4.02	4.02	4.02	4.02	2	0.10	0.01	0.08	0.00	0.00	22.3
17	452	-96	-463	-11	0	16	681	4.02	4.02	4.02	4.02	2	0.10	0.01	0.08	0.00	0.00	22.3
18	452	-140	-717	38	0	-70	756	4.02	4.02	4.02	4.02	3	0.11	0.02	0.13	0.00	0.00	22.3
19	452	-100	-488	-98	0	153	1013	4.02	4.02	4.02	4.02	3	0.14	0.01	0.09	0.00	0.00	22.3
20	452	-118	-612	4	0	-9	877	4.02	4.02	4.02	4.02	3	0.13	0.02	0.11	0.00	0.00	22.3
37	452	-154	-796	88	0	-152	663	4.02	4.02	4.02	4.02	3	0.09	0.02	0.14	0.00	0.00	22.3
38	452	-89	-416	-138	0	220	1050	4.02	4.02	4.02	4.02	3	0.15	0.01	0.07	0.00	0.00	22.3
39	452	-119	-622	32	0	-50	865	4.02	4.02	4.02	4.02	3	0.12	0.02	0.11	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	508	-124	-890	-15	0	28	587	4.02	4.02	4.02	4.02	3	0.08	0.03	0.16	0.00	0.00	22.3
2	508	-102	-722	10	0	-26	387	4.02	4.02	4.02	4.02	2	0.06	0.02	0.13	0.00	0.00	22.3
3	508	-104	-724	15	0	-35	384	4.02	4.02	4.02	4.02	2	0.06	0.02	0.13	0.00	0.00	22.3
4	508	-88	-644	-37	0	78	519	4.02	4.02	4.02	4.02	2	0.08	0.02	0.11	0.00	0.00	22.3
5	508	-90	-646	-33	0	69	517	4.02	4.02	4.02	4.02	2	0.08	0.02	0.11	0.00	0.00	22.3
6	508	-95	-693	-12	0	21	436	4.02	4.02	4.02	4.02	2	0.07	0.02	0.12	0.00	0.00	22.3
7	508	-100	-698	3	0	-9	427	4.02	4.02	4.02	4.02	2	0.06	0.02	0.12	0.00	0.00	22.3
8	508	-91	-670	-26	0	52	476	4.02	4.02	4.02	4.02	2	0.07	0.02	0.12	0.00	0.00	22.3
9	508	-96	-675	-11	0	22	467	4.02	4.02	4.02	4.02	2	0.07	0.02	0.12	0.00	0.00	22.3
10	508	-102	-722	10	0	-26	387	4.02	4.02	4.02	4.02	2	0.06	0.02	0.13	0.00	0.00	22.3
11	508	-104	-724	15	0	-35	384	4.02	4.02	4.02	4.02	2	0.06	0.02	0.13	0.00	0.00	22.3
12	508	-88	-644	-37	0	78	519	4.02	4.02	4.02	4.02	2	0.08	0.02	0.11	0.00	0.00	22.3
13	508	-90	-646	-33	0	69	517	4.02	4.02	4.02	4.02	2	0.08	0.02	0.11	0.00	0.00	22.3
14	508	-95	-693	-12	0	21	436	4.02	4.02	4.02	4.02	2	0.07	0.02	0.12	0.00	0.00	22.3
15	508	-100	-698	3	0	-9	427	4.02	4.02	4.02	4.02	2	0.06	0.02	0.12	0.00	0.00	22.3
16	508	-91	-670	-26	0	52	476	4.02	4.02	4.02	4.02	2	0.07	0.02	0.12	0.00	0.00	22.3
17	508	-96	-675	-11	0	22	467	4.02	4.02	4.02	4.02	2	0.07	0.02	0.12	0.00	0.00	22.3
18	508	-140	-992	38	0	-91	-592	4.02	4.02	4.02	4.02	3	0.08	0.03	0.18	0.00	0.00	22.3
19	508	-100	-764	-98	0	209	805	4.02	4.02	4.02	4.02	3	0.12	0.02	0.14	0.00	0.00	22.3
20	508	-118	-888	4	0	-11	593	4.02	4.02	4.02	4.02	3	0.08	0.03	0.16	0.00	0.00	22.3
37	508	-154	-1072	88	0	-202	-810	4.02	4.02	4.02	4.02	3	0.12	0.03	0.19	0.00	0.00	22.3
38	508	-89	-692	-138	0	299	928	4.02	4.02	4.02	4.02	3	0.13	0.02	0.12	0.00	0.00	22.3
39	508	-119	-898	32	0	-68	575	4.02	4.02	4.02	4.02	3	0.08	0.03	0.16	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	565	-124	-1165	-15	0	36	-443	4.02	4.02	4.02	4.02	3	0.06	0.03	0.21	0.00	0.00	22.3
2	565	-102	-934	10	0	-32	-447	4.02	4.02	4.02	4.02	2	0.07	0.03	0.17	0.00	0.00	22.3
3	565	-104	-935	15	0	-43	-451	4.02	4.02	4.02	4.02	2	0.07	0.03	0.17	0.00	0.00	22.3
4	565	-88	-856	-37	0	99	-231	4.02	4.02	4.02	4.02	2	0.03	0.02	0.15	0.00	0.00	22.3
5	565	-90	-858	-33	0	88	-235	4.02	4.02	4.02	4.02	2	0.04	0.02	0.15	0.00	0.00	22.3
6	565	-95	-905	-12	0	27	-366	4.02	4.02	4.02	4.02	2	0.06	0.03	0.16	0.00	0.00	22.3
7	565	-100	-910	3	0	-11	-381	4.02	4.02	4.02	4.02	2	0.06	0.03	0.16	0.00	0.00	22.3
8	565	-91	-882	-26	0	67	-301	4.02	4.02	4.02	4.02	2	0.05	0.03	0.16	0.00	0.00	22.3
9	565	-96	-887	-11	0	28	-316	4.02	4.02	4.02	4.02	2	0.05	0.03	0.16	0.00	0.00	22.3
10	565	-102	-934	10	0	-32	-447	4.02	4.02	4.02	4.02	2	0.07	0.03	0.17	0.00	0.00	22.3
11	565	-104	-935	15	0	-43	-451	4.02	4.02	4.02	4.02	2	0.07	0.03	0.17	0.00	0.00	22.3
12	565	-88	-856	-37	0	99	-231	4.02	4.02	4.02	4.02	2	0.03	0.02	0.15	0.00	0.00	22.3
13	565	-90	-858	-33	0	88	-235	4.02	4.02	4.02	4.02	2	0.04	0.02	0.15	0.00	0.00	22.3
14	565	-95	-905	-12	0	27	-366	4.02	4.02	4.02	4.02	2	0.06	0.03	0.16	0.00	0.00	22.3
15	565	-100	-910	3	0	-11	-381	4.02	4.02	4.02	4.02	2	0.06	0.03	0.16	0.00	0.00	22.3
16	565	-91	-882	-26	0	67	-301	4.02	4.02	4.02	4.02	2	0.05	0.03	0.16	0.00	0.00	22.3
17	565	-96	-887	-11	0	28	-316	4.02	4.02	4.02	4.02	2	0.05	0.03	0.16	0.00	0.00	22.3
18	565	-140	-1268	38	0	-112	-728	4.02	4.02	4.02	4.02	3	0.10	0.04	0.23	0.00	0.00	22.3
19	565	-100	-1039	-98	0	265	-91	4.02	4.02	4.02	4.02	3	0.06	0.03	0.18	0.00	0.00	22.3
20	565	-118	-1163	4	0	-13	-436	4.02	4.02	4.02	4.02	3	0.06	0.03	0.21	0.00	0.00	22.3
37	565	-154	-1347	88	0	-251	-951	4.02	4.02	4.02	4.02	3	0.14	0.04	0.24	0.00	0.00	22.3
38	565	-89	-967	-138	0	377	599	4.02	4.02	4.02	4.02	3	0.09	0.03	0.17	0.00	0.00	22.3
39	565	-119	-1173	32	0	-86	-464	4.02	4.02	4.02	4.02	3	0.07	0.03	0.21	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

Nome travata: **trave_504_IP1** Descrizione: **Trave_5 11-10-9-8**
ASTA NUM. 10 NI 169 NF 294 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y Permanente Neve qy tot.
qy medio: 375.00 1589.25 142.50 2106.75 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm

1	0	-375	3655	-146	0	-282	-1265	4.02	4.02	4.02	4.02	3	0.18	0.11	0.65	0.00	0.00	22.3
2	0	-329	2783	28	0	-31	-965	4.02	4.02	4.02	4.02	2	0.14	0.08	0.49	0.00	0.00	22.3
3	0	-362	2889	25	0	-35	-1053	4.02	4.02	4.02	4.02	2	0.16	0.08	0.51	0.00	0.00	22.3
4	0	-215	2734	-249	0	-398	-894	4.02	4.02	4.02	4.02	2	0.13	0.08	0.48	0.00	0.00	22.3
5	0	-247	2840	-252	0	-402	-981	4.02	4.02	4.02	4.02	2	0.15	0.08	0.50	0.00	0.00	22.3
6	0	-252	2642	-65	0	-155	-838	4.02	4.02	4.02	4.02	2	0.13	0.08	0.47	0.00	0.00	22.3
7	0	-359	2995	-76	0	-168	-1130	4.02	4.02	4.02	4.02	2	0.17	0.09	0.53	0.00	0.00	22.3
8	0	-217	2627	-148	0	-265	-817	4.02	4.02	4.02	4.02	2	0.12	0.08	0.47	0.00	0.00	22.3
9	0	-325	2980	-159	0	-278	-1108	4.02	4.02	4.02	4.02	2	0.17	0.09	0.53	0.00	0.00	22.3
10	0	-329	2783	28	0	-31	-965	4.02	4.02	4.02	4.02	2	0.14	0.08	0.49	0.00	0.00	22.3
11	0	-362	2889	25	0	-35	-1053	4.02	4.02	4.02	4.02	2	0.16	0.08	0.51	0.00	0.00	22.3
12	0	-215	2734	-249	0	-398	-894	4.02	4.02	4.02	4.02	2	0.13	0.08	0.48	0.00	0.00	22.3
13	0	-247	2840	-252	0	-402	-981	4.02	4.02	4.02	4.02	2	0.15	0.08	0.50	0.00	0.00	22.3
14	0	-252	2642	-65	0	-155	-838	4.02	4.02	4.02	4.02	2	0.13	0.08	0.47	0.00	0.00	22.3
15	0	-359	2995	-76	0	-168	-1130	4.02	4.02	4.02	4.02	2	0.17	0.09	0.53	0.00	0.00	22.3

16	0	-217	2627	-148	0	-265	-817	4.02	4.02	4.02	4.02	2	0.12	0.08	0.47	0.00	0.00	22.3
17	0	-325	2980	-159	0	-278	-1108	4.02	4.02	4.02	4.02	2	0.17	0.09	0.53	0.00	0.00	22.3
18	0	-482	3842	109	0	-61	-1385	4.02	4.02	4.02	4.02	3	0.20	0.11	0.68	0.00	0.00	22.3
19	0	-176	3791	-697	0	-1088	-1220	4.02	4.02	4.02	4.02	3	0.27	0.11	0.67	0.00	0.00	22.3
20	0	-306	3819	-241	0	-499	-1218	4.02	4.02	4.02	4.02	3	0.17	0.11	0.68	0.00	0.00	22.3
37	0	-595	3759	426	0	377	-1418	4.02	4.02	4.02	4.02	3	0.20	0.11	0.66	0.00	0.00	22.3
38	0	-87	3673	-917	0	-1334	-1143	4.02	4.02	4.02	4.02	3	0.33	0.11	0.65	0.00	0.00	22.3
39	0	-303	3720	-156	0	-352	-1140	4.02	4.02	4.02	4.02	3	0.16	0.11	0.66	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	31	-375	2863	-146	0	-237	-1265	4.02	4.02	4.02	4.02	3	0.18	0.08	0.51	0.00	0.00	22.3
2	31	-329	2174	28	0	-40	-965	4.02	4.02	4.02	4.02	2	0.14	0.06	0.38	0.00	0.00	22.3
3	31	-362	2280	25	0	-43	-1053	4.02	4.02	4.02	4.02	2	0.16	0.07	0.40	0.00	0.00	22.3
4	31	-215	2125	-249	0	-321	-894	4.02	4.02	4.02	4.02	2	0.13	0.06	0.38	0.00	0.00	22.3
5	31	-247	2231	-252	0	-324	-981	4.02	4.02	4.02	4.02	2	0.15	0.06	0.40	0.00	0.00	22.3
6	31	-252	2033	-65	0	-135	-838	4.02	4.02	4.02	4.02	2	0.13	0.06	0.36	0.00	0.00	22.3
7	31	-359	2386	-76	0	-145	-1130	4.02	4.02	4.02	4.02	2	0.17	0.07	0.42	0.00	0.00	22.3
8	31	-217	2018	-148	0	-219	-817	4.02	4.02	4.02	4.02	2	0.12	0.06	0.36	0.00	0.00	22.3
9	31	-325	2371	-159	0	-229	-1108	4.02	4.02	4.02	4.02	2	0.17	0.07	0.42	0.00	0.00	22.3
10	31	-329	2174	28	0	-40	-965	4.02	4.02	4.02	4.02	2	0.14	0.06	0.38	0.00	0.00	22.3
11	31	-362	2280	25	0	-43	-1053	4.02	4.02	4.02	4.02	2	0.16	0.07	0.40	0.00	0.00	22.3
12	31	-215	2125	-249	0	-321	-894	4.02	4.02	4.02	4.02	2	0.13	0.06	0.38	0.00	0.00	22.3
13	31	-247	2231	-252	0	-324	-981	4.02	4.02	4.02	4.02	2	0.15	0.06	0.40	0.00	0.00	22.3
14	31	-252	2033	-65	0	-135	-838	4.02	4.02	4.02	4.02	2	0.13	0.06	0.36	0.00	0.00	22.3
15	31	-359	2386	-76	0	-145	-1130	4.02	4.02	4.02	4.02	2	0.17	0.07	0.42	0.00	0.00	22.3
16	31	-217	2018	-148	0	-219	-817	4.02	4.02	4.02	4.02	2	0.12	0.06	0.36	0.00	0.00	22.3
17	31	-325	2371	-159	0	-229	-1108	4.02	4.02	4.02	4.02	2	0.17	0.07	0.42	0.00	0.00	22.3
18	31	-482	2984	109	0	-95	-1385	4.02	4.02	4.02	4.02	3	0.20	0.09	0.53	0.00	0.00	22.3
19	31	-176	2933	-697	0	-872	-1220	4.02	4.02	4.02	4.02	3	0.21	0.08	0.52	0.00	0.00	22.3
20	31	-306	2961	-241	0	-424	-1218	4.02	4.02	4.02	4.02	3	0.17	0.09	0.52	0.00	0.00	22.3
37	31	-595	2934	426	0	245	-1418	4.02	4.02	4.02	4.02	3	0.20	0.08	0.52	0.00	0.00	22.3
38	31	-87	2848	-917	0	-1050	-1143	4.02	4.02	4.02	4.02	3	0.26	0.08	0.51	0.00	0.00	22.3
39	31	-303	2895	-156	0	-303	-1140	4.02	4.02	4.02	4.02	3	0.16	0.08	0.51	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	62	-375	2072	-146	0	-192	1332	4.02	4.02	4.02	4.02	3	0.19	0.06	0.37	0.00	0.00	22.3
2	62	-329	1565	28	0	-49	989	4.02	4.02	4.02	4.02	2	0.15	0.05	0.28	0.00	0.00	22.3
3	62	-362	1671	25	0	-51	1066	4.02	4.02	4.02	4.02	2	0.16	0.05	0.30	0.00	0.00	22.3
4	62	-215	1516	-249	0	-244	986	4.02	4.02	4.02	4.02	2	0.15	0.04	0.27	0.00	0.00	22.3
5	62	-247	1622	-252	0	-246	1060	4.02	4.02	4.02	4.02	2	0.16	0.05	0.29	0.00	0.00	22.3
6	62	-252	1424	-65	0	-115	928	4.02	4.02	4.02	4.02	2	0.14	0.04	0.25	0.00	0.00	22.3
7	62	-359	1777	-76	0	-121	1153	4.02	4.02	4.02	4.02	2	0.17	0.05	0.31	0.00	0.00	22.3
8	62	-217	1409	-148	0	-173	931	4.02	4.02	4.02	4.02	2	0.14	0.04	0.25	0.00	0.00	22.3
9	62	-325	1762	-159	0	-180	1152	4.02	4.02	4.02	4.02	2	0.17	0.05	0.31	0.00	0.00	22.3
10	62	-329	1565	28	0	-49	989	4.02	4.02	4.02	4.02	2	0.15	0.05	0.28	0.00	0.00	22.3
11	62	-362	1671	25	0	-51	1066	4.02	4.02	4.02	4.02	2	0.16	0.05	0.30	0.00	0.00	22.3
12	62	-215	1516	-249	0	-244	986	4.02	4.02	4.02	4.02	2	0.15	0.04	0.27	0.00	0.00	22.3
13	62	-247	1622	-252	0	-246	1060	4.02	4.02	4.02	4.02	2	0.16	0.05	0.29	0.00	0.00	22.3
14	62	-252	1424	-65	0	-115	928	4.02	4.02	4.02	4.02	2	0.14	0.04	0.25	0.00	0.00	22.3
15	62	-359	1777	-76	0	-121	1153	4.02	4.02	4.02	4.02	2	0.17	0.05	0.31	0.00	0.00	22.3
16	62	-217	1409	-148	0	-173	931	4.02	4.02	4.02	4.02	2	0.14	0.04	0.25	0.00	0.00	22.3
17	62	-325	1762	-159	0	-180	1152	4.02	4.02	4.02	4.02	2	0.17	0.05	0.31	0.00	0.00	22.3
18	62	-482	2126	109	0	-129	1252	4.02	4.02	4.02	4.02	3	0.18	0.06	0.37	0.00	0.00	22.3
19	62	-176	2075	-697	0	-656	1352	4.02	4.02	4.02	4.02	3	0.19	0.06	0.37	0.00	0.00	22.3
20	62	-306	2103	-241	0	-349	1390	4.02	4.02	4.02	4.02	3	0.20	0.06	0.37	0.00	0.00	22.3
37	62	-595	2109	426	0	113	1212	4.02	4.02	4.02	4.02	3	0.17	0.06	0.37	0.00	0.00	22.3
38	62	-87	2023	-917	0	-766	1365	4.02	4.02	4.02	4.02	3	0.20	0.06	0.36	0.00	0.00	22.3
39	62	-303	2071	-156	0	-255	1430	4.02	4.02	4.02	4.02	3	0.20	0.06	0.37	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	93	-375	1280	-146	0	-146	1332	4.02	4.02	4.02	4.02	3	0.19	0.04	0.23	0.00	0.00	22.3
2	93	-329	956	28	0	-58	989	4.02	4.02	4.02	4.02	2	0.15	0.03	0.17	0.00	0.00	22.3
3	93	-362	1062	25	0	-59	1066	4.02	4.02	4.02	4.02	2	0.16	0.03	0.19	0.00	0.00	22.3
4	93	-215	907	-249	0	-167	986	4.02	4.02	4.02	4.02	2	0.15	0.03	0.16	0.00	0.00	22.3
5	93	-247	1013	-252	0	-168	1060	4.02	4.02	4.02	4.02	2	0.16	0.03	0.18	0.00	0.00	22.3
6	93	-252	815	-65	0	-95	928	4.02	4.02	4.02	4.02	2	0.14	0.02	0.14	0.00	0.00	22.3
7	93	-359	1168	-76	0	-98	1153	4.02	4.02	4.02	4.02	2	0.17	0.03	0.21	0.00	0.00	22.3
8	93	-217	800	-148	0	-127	931	4.02	4.02	4.02	4.02	2	0.14	0.02	0.14	0.00	0.00	22.3
9	93	-325	1153	-159	0	-131	1152	4.02	4.02	4.02	4.02	2	0.17	0.03	0.20	0.00	0.00	22.3
10	93	-329	956	28	0	-58	989	4.02	4.02	4.02	4.02	2	0.15	0.03	0.17	0.00	0.00	22.3
11	93	-362	1062	25	0	-59	1066	4.02	4.02	4.02	4.02	2	0.16	0.03	0.19	0.00	0.00	22.3
12	93	-215	907	-249	0	-167	986	4.02	4.02	4.02	4.02	2	0.15	0.03	0.16	0.00	0.00	22.3
13	93	-247	1013	-252	0	-168	1060	4.02	4.02	4.02	4.02	2	0.16	0.03	0.18	0.00	0.00	22.3
14	93	-252	815	-65	0	-95	928	4.02	4.02	4.02	4.02	2	0.14	0.02	0.14	0.00	0.00	22.3
15	93	-359	1168	-76	0	-98	1153	4.02	4.02	4.02	4.02	2	0.17	0.03	0.21	0.00	0.00	22.3
16	93	-217	800	-148	0	-127	931	4.02	4.02	4.02	4.02	2	0.14	0.02	0.14	0.00	0.00	22.3
17	93	-325	1153	-159	0	-131	1152	4.02	4.02	4.02	4.02	2	0.17	0.03	0.20	0.00	0.00	22.3
18	93	-482	1269	109	0	-162	1252	4.02	4.02	4.02	4.02	3	0.18	0.04	0.22	0.00	0.00	22.3
19	93	-176	1217	-697	0	-440	1352	4.02	4.02	4.02	4.02	3	0.19	0.04	0.22	0.00	0.00	22.3
20	93	-306	1245	-241	0	-275	1390	4.02	4.02	4.02	4.02	3	0.20	0.04	0.22	0.00	0.00	22.3
37	93	-595	1285	426	0	-19	1212	4.02	4.02	4.02	4.02	3	0.17	0.04	0.23	0.00	0.00	22.3
38	93	-87	1199	-917	0	-482	1365	4.02	4.02	4.02	4.02	3	0.20	0.03	0.21	0.00	0.00	22.3
39	93	-303	1246	-156	0	-207	1430	4.02	4.02	4.02	4.02	3	0.20	0.04	0.22	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	124	-375	489	-146	0	-101	1332	4.02	4.02	4.02	4.02	3	0.19	0.01	0.09	0.00	0.00	22.3
2	124	-329	347	28	0	-66	989	4.02	4.02	4.02	4.02	2	0.15	0.01	0.06	0.00	0.00	22.3
3	124	-362	453	25	0	-66	1066	4.02	4.02	4.02	4.02	2	0.16	0.01	0.08	0.00	0.00	22.3
4	124	-215	298	-249	0	-90	986	4.02	4.02	4.02	4.02	2	0.15	0.01	0.05	0.00	0.00	22.3
5	124	-247	404	-252	0	-89	1060	4.02	4.02	4.02	4.02	2	0.16	0.01	0.07	0.00	0.00	22.3
6	124	-252	206	-65	0	-75	928	4.02	4.02	4.02	4.02	2	0.14	0.01	0.04	0.00	0.00	22.3
7	124	-359	559	-76	0	-74	1153	4.02	4.02	4.02	4.02	2	0.17	0.02	0.10	0.00	0.00	22.3
8	124	-217	191	-148	0	-82	931	4.02	4.02	4.02	4.02	2	0.14	0.01	0.03	0.00	0.00	22.3
9	124	-325	544	-159	0	-81	1152	4.02	4.02	4.02	4.02	2	0.17	0.02	0.10	0.00	0.00	22.3
10	124	-329	347	28	0	-66	989	4.02	4.02	4.02	4.02	2	0.15	0.01	0.06	0.00	0.00	22.3
11	124	-362	453	25	0	-66	1066	4.02	4.02	4.02	4.02	2	0.16	0.01	0.08	0.00	0.00	22.3
12	124	-215	298	-249	0	-90	986	4.02	4.02	4.02	4.02	2	0.15	0.01	0.05	0.00	0.00	22.3
13	124	-247	404	-252	0	-89	1060	4.02	4.02	4.02	4.02	2	0.16	0.01	0.07	0.00	0.00	22.3
14	124	-252	206	-65	0	-75	928	4.02	4.02	4.02	4.02	2	0.14	0.01	0.04	0.00	0.00	22.3
15	124	-359	559	-76	0	-74	1153	4.02	4.02	4.02	4.02	2	0.17	0.02	0.10	0.00	0.00	22.3
16	124	-217	191	-148	0	-82	931	4.02	4.02	4.02	4.02	2	0.14	0.01	0.03	0.00	0.00	22.3
17	124	-325	544	-159	0	-81	1152	4.02	4.02	4.02	4.02	2	0.17	0.02	0.10	0.00	0.00	22.3
18	124	-482	411	109	0	-196	1252	4.02	4.02	4.02	4.02	3	0.18	0.01	0.07	0.00	0.00	22.3
19	124	-176	359	-697	0	-224	1352	4.02	4.02	4.02	4.02	3	0.19	0.02	0.11	0.00	0.00	22.3
20	124	-306	387	-241	0	-200	1390	4.02	4.02	4.02	4.02	3	0.20	0.01	0.07	0.00	0.00	22.3
37	124	-595	460	426	0	-151	1212	4.02	4.02	4.02	4.02	3	0.17	0.01	0.08	0.00	0.00	22.3

38	124	-87	374	-917	0	-198	1365	4.02	4.02	4.02	4.02	3	0.20	0.03	0.15	0.00	0.00	22.3
39	124	-303	421	-156	0	-158	1430	4.02	4.02	4.02	4.02	3	0.20	0.01	0.07	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	155	-375	-303	-146	0	-56	1332	4.02	4.02	4.02	4.02	3	0.19	0.01	0.05	0.00	0.00	22.3
2	155	-329	-261	28	0	-75	989	4.02	4.02	4.02	4.02	2	0.15	0.01	0.05	0.00	0.00	22.3
3	155	-362	-155	25	0	-74	1066	4.02	4.02	4.02	4.02	2	0.16	0.00	0.03	0.00	0.00	22.3
4	155	-215	-311	-249	0	-12	986	4.02	4.02	4.02	4.02	2	0.15	0.01	0.06	0.00	0.00	22.3
5	155	-247	-205	-252	0	-11	1060	4.02	4.02	4.02	4.02	2	0.16	0.01	0.04	0.00	0.00	22.3
6	155	-252	-402	-65	0	-54	928	4.02	4.02	4.02	4.02	2	0.14	0.01	0.07	0.00	0.00	22.3
7	155	-359	-49	-76	0	-51	1153	4.02	4.02	4.02	4.02	2	0.17	0.00	0.01	0.00	0.00	22.3
8	155	-217	-418	-148	0	-36	931	4.02	4.02	4.02	4.02	2	0.14	0.01	0.07	0.00	0.00	22.3
9	155	-325	-64	-159	0	-32	1152	4.02	4.02	4.02	4.02	2	0.17	0.00	0.03	0.00	0.00	22.3
10	155	-329	-261	28	0	-75	989	4.02	4.02	4.02	4.02	2	0.15	0.01	0.05	0.00	0.00	22.3
11	155	-362	-155	25	0	-74	1066	4.02	4.02	4.02	4.02	2	0.16	0.00	0.03	0.00	0.00	22.3
12	155	-215	-311	-249	0	-12	986	4.02	4.02	4.02	4.02	2	0.15	0.01	0.06	0.00	0.00	22.3
13	155	-247	-205	-252	0	-11	1060	4.02	4.02	4.02	4.02	2	0.16	0.01	0.04	0.00	0.00	22.3
14	155	-252	-402	-65	0	-54	928	4.02	4.02	4.02	4.02	2	0.14	0.01	0.07	0.00	0.00	22.3
15	155	-359	-49	-76	0	-51	1153	4.02	4.02	4.02	4.02	2	0.17	0.00	0.01	0.00	0.00	22.3
16	155	-217	-418	-148	0	-36	931	4.02	4.02	4.02	4.02	2	0.14	0.01	0.07	0.00	0.00	22.3
17	155	-325	-64	-159	0	-32	1152	4.02	4.02	4.02	4.02	2	0.17	0.00	0.03	0.00	0.00	22.3
18	155	-482	-447	109	0	-230	1252	4.02	4.02	4.02	4.02	3	0.18	0.01	0.08	0.00	0.00	22.3
19	155	-176	-499	-697	0	-8	1352	4.02	4.02	4.02	4.02	3	0.19	0.02	0.11	0.00	0.00	22.3
20	155	-306	-471	-241	0	-125	1390	4.02	4.02	4.02	4.02	3	0.20	0.01	0.08	0.00	0.00	22.3
37	155	-595	-365	426	0	-283	1212	4.02	4.02	4.02	4.02	3	0.17	0.01	0.07	0.00	0.00	22.3
38	155	-87	-451	-917	0	86	1365	4.02	4.02	4.02	4.02	3	0.20	0.03	0.15	0.00	0.00	22.3
39	155	-303	-403	-156	0	-110	1430	4.02	4.02	4.02	4.02	3	0.20	0.01	0.07	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	186	-375	-1095	-145	0	-11	1332	4.02	4.02	4.02	4.02	3	0.19	0.03	0.19	0.00	0.00	22.3
2	186	-329	-870	28	0	-84	989	4.02	4.02	4.02	4.02	2	0.15	0.03	0.15	0.00	0.00	22.3
3	186	-362	-764	25	0	-82	1066	4.02	4.02	4.02	4.02	2	0.16	0.02	0.13	0.00	0.00	22.3
4	186	-215	-920	-249	0	65	986	4.02	4.02	4.02	4.02	2	0.15	0.03	0.16	0.00	0.00	22.3
5	186	-247	-814	-252	0	67	1060	4.02	4.02	4.02	4.02	2	0.16	0.02	0.14	0.00	0.00	22.3
6	186	-252	-1011	-65	0	-34	928	4.02	4.02	4.02	4.02	2	0.14	0.03	0.18	0.00	0.00	22.3
7	186	-359	-658	-76	0	-27	1153	4.02	4.02	4.02	4.02	2	0.17	0.02	0.12	0.00	0.00	22.3
8	186	-217	-1026	-148	0	10	931	4.02	4.02	4.02	4.02	2	0.14	0.03	0.18	0.00	0.00	22.3
9	186	-325	-673	-159	0	17	1152	4.02	4.02	4.02	4.02	2	0.17	0.02	0.12	0.00	0.00	22.3
10	186	-329	-870	28	0	-84	989	4.02	4.02	4.02	4.02	2	0.15	0.03	0.15	0.00	0.00	22.3
11	186	-362	-764	25	0	-82	1066	4.02	4.02	4.02	4.02	2	0.16	0.02	0.13	0.00	0.00	22.3
12	186	-215	-920	-249	0	65	986	4.02	4.02	4.02	4.02	2	0.15	0.03	0.16	0.00	0.00	22.3
13	186	-247	-814	-252	0	67	1060	4.02	4.02	4.02	4.02	2	0.16	0.02	0.14	0.00	0.00	22.3
14	186	-252	-1011	-65	0	-34	928	4.02	4.02	4.02	4.02	2	0.14	0.03	0.18	0.00	0.00	22.3
15	186	-359	-658	-76	0	-27	1153	4.02	4.02	4.02	4.02	2	0.17	0.02	0.12	0.00	0.00	22.3
16	186	-217	-1026	-148	0	10	931	4.02	4.02	4.02	4.02	2	0.14	0.03	0.18	0.00	0.00	22.3
17	186	-325	-673	-159	0	17	1152	4.02	4.02	4.02	4.02	2	0.17	0.02	0.12	0.00	0.00	22.3
18	186	-482	-1305	109	0	-263	1252	4.02	4.02	4.02	4.02	3	0.18	0.04	0.23	0.00	0.00	22.3
19	186	-176	-1356	-697	0	209	1352	4.02	4.02	4.02	4.02	3	0.19	0.04	0.24	0.00	0.00	22.3
20	186	-306	-1328	-241	0	-51	1390	4.02	4.02	4.02	4.02	3	0.20	0.04	0.23	0.00	0.00	22.3
37	186	-595	-1190	426	0	-416	1212	4.02	4.02	4.02	4.02	3	0.17	0.03	0.21	0.00	0.00	22.3
38	186	-87	-1276	-917	0	371	1365	4.02	4.02	4.02	4.02	3	0.20	0.04	0.23	0.00	0.00	22.3
39	186	-303	-1228	-156	0	-61	1430	4.02	4.02	4.02	4.02	3	0.20	0.04	0.22	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	217	-375	-1886	-145	0	34	1332	4.02	4.02	4.02	4.02	3	0.19	0.05	0.33	0.00	0.00	22.3
2	217	-329	-1479	28	0	-93	989	4.02	4.02	4.02	4.02	2	0.15	0.04	0.26	0.00	0.00	22.3
3	217	-362	-1373	25	0	-90	1066	4.02	4.02	4.02	4.02	2	0.16	0.04	0.24	0.00	0.00	22.3
4	217	-215	-1529	-249	0	142	986	4.02	4.02	4.02	4.02	2	0.15	0.04	0.27	0.00	0.00	22.3
5	217	-247	-1423	-252	0	145	1060	4.02	4.02	4.02	4.02	2	0.16	0.04	0.25	0.00	0.00	22.3
6	217	-252	-1620	-65	0	-14	928	4.02	4.02	4.02	4.02	2	0.14	0.05	0.29	0.00	0.00	22.3
7	217	-359	-1267	-76	0	-4	1153	4.02	4.02	4.02	4.02	2	0.17	0.04	0.22	0.00	0.00	22.3
8	217	-217	-1635	-148	0	56	931	4.02	4.02	4.02	4.02	2	0.14	0.05	0.29	0.00	0.00	22.3
9	217	-325	-1282	-159	0	67	1152	4.02	4.02	4.02	4.02	2	0.17	0.04	0.23	0.00	0.00	22.3
10	217	-329	-1479	28	0	-93	989	4.02	4.02	4.02	4.02	2	0.15	0.04	0.26	0.00	0.00	22.3
11	217	-362	-1373	25	0	-90	1066	4.02	4.02	4.02	4.02	2	0.16	0.04	0.24	0.00	0.00	22.3
12	217	-215	-1529	-249	0	142	986	4.02	4.02	4.02	4.02	2	0.15	0.04	0.27	0.00	0.00	22.3
13	217	-247	-1423	-252	0	145	1060	4.02	4.02	4.02	4.02	2	0.16	0.04	0.25	0.00	0.00	22.3
14	217	-252	-1620	-65	0	-14	928	4.02	4.02	4.02	4.02	2	0.14	0.05	0.29	0.00	0.00	22.3
15	217	-359	-1267	-76	0	-4	1153	4.02	4.02	4.02	4.02	2	0.17	0.04	0.22	0.00	0.00	22.3
16	217	-217	-1635	-148	0	56	931	4.02	4.02	4.02	4.02	2	0.14	0.05	0.29	0.00	0.00	22.3
17	217	-325	-1282	-159	0	67	1152	4.02	4.02	4.02	4.02	2	0.17	0.04	0.23	0.00	0.00	22.3
18	217	-482	-2163	109	0	-297	1252	4.02	4.02	4.02	4.02	3	0.18	0.06	0.38	0.00	0.00	22.3
19	217	-176	-2214	-697	0	425	1352	4.02	4.02	4.02	4.02	3	0.19	0.06	0.39	0.00	0.00	22.3
20	217	-306	-2186	-241	0	24	1390	4.02	4.02	4.02	4.02	3	0.20	0.06	0.39	0.00	0.00	22.3
37	217	-595	-2015	426	0	-548	1212	4.02	4.02	4.02	4.02	3	0.17	0.06	0.35	0.00	0.00	22.3
38	217	-87	-2101	-917	0	655	1365	4.02	4.02	4.02	4.02	3	0.20	0.06	0.37	0.00	0.00	22.3
39	217	-303	-2053	-156	0	-13	1430	4.02	4.02	4.02	4.02	3	0.20	0.06	0.36	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	248	-375	-2678	-146	0	79	-1410	4.02	4.02	4.02	4.02	3	0.20	0.08	0.47	0.00	0.00	22.3
2	248	-329	-2088	28	0	-102	-1161	4.02	4.02	4.02	4.02	2	0.17	0.06	0.37	0.00	0.00	22.3
3	248	-362	-1982	25	0	-98	1066	4.02	4.02	4.02	4.02	2	0.16	0.06	0.35	0.00	0.00	22.3
4	248	-215	-2138	-249	0	219	-1237	4.02	4.02	4.02	4.02	2	0.19	0.06	0.38	0.00	0.00	22.3
5	248	-247	-2032	-252	0	223	1049	4.02	4.02	4.02	4.02	2	0.16	0.06	0.36	0.00	0.00	22.3
6	248	-252	-2229	-65	0	6	-1455	4.02	4.02	4.02	4.02	2	0.22	0.06	0.39	0.00	0.00	22.3
7	248	-359	-1876	-76	0	20	1153	4.02	4.02	4.02	4.02	2	0.17	0.05	0.33	0.00	0.00	22.3
8	248	-217	-2244	-148	0	102	-1478	4.02	4.02	4.02	4.02	2	0.22	0.07	0.40	0.00	0.00	22.3
9	248	-325	-1891	-159	0	116	1152	4.02	4.02	4.02	4.02	2	0.17	0.05	0.33	0.00	0.00	22.3
10	248	-329	-2088	28	0	-102	-1161	4.02	4.02	4.02	4.02	2	0.17	0.06	0.37	0.00	0.00	22.3
11	248	-362	-1982	25	0	-98	1066	4.02	4.02	4.02	4.02	2	0.16	0.06	0.35	0.00	0.00	22.3
12	248	-215	-2138	-249	0	219	-1237	4.02	4.02	4.02	4.02	2	0.19	0.06	0.38	0.00	0.00	22.3
13	248	-247	-2032	-252	0	223	1049	4.02	4.02	4.02	4.02	2	0.16	0.06	0.36	0.00	0.00	22.3
14	248	-252	-2229	-65	0	6	-1455	4.02	4.02	4.02	4.02	2	0.22	0.06	0.39	0.00	0.00	22.3
15	248	-359	-1876	-76	0	20	1153	4.02	4.02	4.02	4.02	2	0.17	0.05	0.33	0.00	0.00	22.3
16	248	-217	-2244	-148	0	102	-1478	4.02	4.02	4.02	4.02	2	0.22	0.07	0.40	0.00	0.00	22.3
17	248	-325	-1891	-159	0	116	1152	4.02	4.02	4.02	4.02	2	0.17	0.05	0.33	0.00	0.00	22.3
18	248	-482	-3020	109	0	-331	-1895	4.02	4.02	4.02	4.02	3	0.27	0.09	0.53	0.00	0.00	22.3
19	248	-176	-3072	-697	0	641	-1885	4.02	4.02	4.02	4.02	3	0.27	0.09	0.54	0.00	0.00	22.3
20	248	-306	-3044	-241	0	99	-1798	4.02	4.02	4.02	4.02	3	0.26	0.09	0.54	0.00	0.00	22.3
37	248	-595	-2839	426	0	-680	-1715	4.02	4.02	4.02	4.02	3	0.24	0.08	0.50	0.00	0.00	22.3
38	248	-87	-2925	-917	0	939	-1698	4.02	4.02	4.02	4.02	3	0.24	0.08	0.52	0.00	0.00	22.3
39	248	-303	-2878	-156	0	36	-1552	4.02	4.02	4.02	4.02	3	0.22	0.08	0.51	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	279	-375	-3469	-146	0	124	-2206	4.02	4.02	4.02	4.02	3	0.31	0.10	0.61	0.00	0.00	22.3

2	279	-329	-2697	28	0	-111	-1776	4.02	4.02	4.02	4.02	2	0.27	0.08	0.48	0.00	0.00	22.3
3	279	-362	-2591	25	0	-105	-1535	4.02	4.02	4.02	4.02	2	0.23	0.08	0.46	0.00	0.00	22.3
4	279	-215	-2747	-249	0	297	-1858	4.02	4.02	4.02	4.02	2	0.28	0.08	0.49	0.00	0.00	22.3
5	279	-247	-2641	-252	0	302	-1617	4.02	4.02	4.02	4.02	2	0.24	0.08	0.47	0.00	0.00	22.3
6	279	-252	-2838	-65	0	26	-2086	4.02	4.02	4.02	4.02	2	0.31	0.08	0.50	0.00	0.00	22.3
7	279	-359	-2485	-76	0	43	-1283	4.02	4.02	4.02	4.02	2	0.19	0.07	0.44	0.00	0.00	22.3
8	279	-217	-2853	-148	0	148	-2111	4.02	4.02	4.02	4.02	2	0.32	0.08	0.51	0.00	0.00	22.3
9	279	-325	-2500	-159	0	165	-1307	4.02	4.02	4.02	4.02	2	0.20	0.07	0.44	0.00	0.00	22.3
10	279	-329	-2697	28	0	-111	-1776	4.02	4.02	4.02	4.02	2	0.27	0.08	0.48	0.00	0.00	22.3
11	279	-362	-2591	25	0	-105	-1535	4.02	4.02	4.02	4.02	2	0.23	0.08	0.46	0.00	0.00	22.3
12	279	-215	-2747	-249	0	297	-1858	4.02	4.02	4.02	4.02	2	0.28	0.08	0.49	0.00	0.00	22.3
13	279	-247	-2641	-252	0	302	-1617	4.02	4.02	4.02	4.02	2	0.24	0.08	0.47	0.00	0.00	22.3
14	279	-252	-2838	-65	0	26	-2086	4.02	4.02	4.02	4.02	2	0.31	0.08	0.50	0.00	0.00	22.3
15	279	-359	-2485	-76	0	43	-1283	4.02	4.02	4.02	4.02	2	0.19	0.07	0.44	0.00	0.00	22.3
16	279	-217	-2853	-148	0	148	-2111	4.02	4.02	4.02	4.02	2	0.32	0.08	0.51	0.00	0.00	22.3
17	279	-325	-2500	-159	0	165	-1307	4.02	4.02	4.02	4.02	2	0.20	0.07	0.44	0.00	0.00	22.3
18	279	-482	-3878	109	0	-364	-2771	4.02	4.02	4.02	4.02	3	0.39	0.11	0.68	0.00	0.00	22.3
19	279	-176	-3930	-697	0	857	-2767	4.02	4.02	4.02	4.02	3	0.39	0.11	0.70	0.00	0.00	22.3
20	279	-306	-3902	-241	0	173	-2676	4.02	4.02	4.02	4.02	3	0.38	0.11	0.69	0.00	0.00	22.3
37	279	-595	-3664	426	0	-812	-2549	4.02	4.02	4.02	4.02	3	0.36	0.11	0.64	0.00	0.00	22.3
38	279	-87	-3750	-917	0	1223	-2542	4.02	4.02	4.02	4.02	3	0.36	0.11	0.67	0.00	0.00	22.3
39	279	-303	-3702	-156	0	84	-2391	4.02	4.02	4.02	4.02	3	0.34	0.11	0.65	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	310	-375	-4261	-146	0	169	-2206	4.02	4.02	4.02	4.02	3	0.31	0.12	0.75	0.00	0.00	22.3
2	310	-329	-3306	28	0	-119	-1776	4.02	4.02	4.02	4.02	2	0.27	0.10	0.58	0.00	0.00	22.3
3	310	-362	-3200	25	0	-113	-1535	4.02	4.02	4.02	4.02	2	0.23	0.09	0.57	0.00	0.00	22.3
4	310	-215	-3356	-249	0	374	-1858	4.02	4.02	4.02	4.02	2	0.28	0.10	0.59	0.00	0.00	22.3
5	310	-247	-3250	-252	0	380	-1617	4.02	4.02	4.02	4.02	2	0.24	0.09	0.58	0.00	0.00	22.3
6	310	-252	-3447	-65	0	46	-2086	4.02	4.02	4.02	4.02	2	0.31	0.10	0.61	0.00	0.00	22.3
7	310	-359	-3094	-76	0	66	-1283	4.02	4.02	4.02	4.02	2	0.19	0.09	0.55	0.00	0.00	22.3
8	310	-217	-3462	-148	0	194	-2111	4.02	4.02	4.02	4.02	2	0.32	0.10	0.61	0.00	0.00	22.3
9	310	-325	-3109	-159	0	214	-1307	4.02	4.02	4.02	4.02	2	0.20	0.09	0.55	0.00	0.00	22.3
10	310	-329	-3306	28	0	-119	-1776	4.02	4.02	4.02	4.02	2	0.27	0.10	0.58	0.00	0.00	22.3
11	310	-362	-3200	25	0	-113	-1535	4.02	4.02	4.02	4.02	2	0.23	0.09	0.57	0.00	0.00	22.3
12	310	-215	-3356	-249	0	374	-1858	4.02	4.02	4.02	4.02	2	0.28	0.10	0.59	0.00	0.00	22.3
13	310	-247	-3250	-252	0	380	-1617	4.02	4.02	4.02	4.02	2	0.24	0.09	0.58	0.00	0.00	22.3
14	310	-252	-3447	-65	0	46	-2086	4.02	4.02	4.02	4.02	2	0.31	0.10	0.61	0.00	0.00	22.3
15	310	-359	-3094	-76	0	66	-1283	4.02	4.02	4.02	4.02	2	0.19	0.09	0.55	0.00	0.00	22.3
16	310	-217	-3462	-148	0	194	-2111	4.02	4.02	4.02	4.02	2	0.32	0.10	0.61	0.00	0.00	22.3
17	310	-325	-3109	-159	0	214	-1307	4.02	4.02	4.02	4.02	2	0.20	0.09	0.55	0.00	0.00	22.3
18	310	-482	-4736	109	0	-398	-2771	4.02	4.02	4.02	4.02	3	0.39	0.14	0.83	0.00	0.00	22.3
19	310	-176	-4788	-697	0	1073	-2767	4.02	4.02	4.02	4.02	3	0.39	0.14	0.85	0.00	0.00	22.3
20	310	-306	-4760	-241	0	248	-2676	4.02	4.02	4.02	4.02	3	0.38	0.14	0.84	0.00	0.00	22.3
37	310	-595	-4489	426	0	-944	-2549	4.02	4.02	4.02	4.02	3	0.36	0.13	0.79	0.00	0.00	22.3
38	310	-87	-4575	-917	0	1507	-2542	4.02	4.02	4.02	4.02	3	0.37	0.13	0.81	0.00	0.00	22.3
39	310	-303	-4527	-156	0	133	-2391	4.02	4.02	4.02	4.02	3	0.34	0.13	0.80	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

Nome travata: **trave_504_IP1** Descrizione: **Trave_5 11-10-9-8**
ASTA NUM. 11 NI 294 NF 124 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y Permanente Neve qy tot.
qy medio: 375.00 1325.25 142.50 1842.75 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-668	3787	34	0	156	-1779	4.02	4.02	4.02	4.02	3	0.25	0.11	0.66	0.00	0.00	22.3
2	0	-648	2848	-68	0	-111	-1215	4.02	4.02	4.02	4.02	2	0.18	0.08	0.50	0.00	0.00	22.3
3	0	-512	2947	-68	0	-109	-1453	4.02	4.02	4.02	4.02	2	0.22	0.09	0.52	0.00	0.00	22.3
4	0	-516	2879	120	0	349	-1283	4.02	4.02	4.02	4.02	2	0.19	0.08	0.51	0.00	0.00	22.3
5	0	-380	2978	121	0	351	-1522	4.02	4.02	4.02	4.02	2	0.23	0.09	0.53	0.00	0.00	22.3
6	0	-761	2744	-3	0	48	-961	4.02	4.02	4.02	4.02	2	0.14	0.08	0.48	0.00	0.00	22.3
7	0	-307	3073	-0	0	54	-1755	4.02	4.02	4.02	4.02	2	0.26	0.09	0.54	0.00	0.00	22.3
8	0	-721	2753	53	0	186	-981	4.02	4.02	4.02	4.02	2	0.15	0.08	0.48	0.00	0.00	22.3
9	0	-268	3082	56	0	192	-1775	4.02	4.02	4.02	4.02	2	0.27	0.09	0.55	0.00	0.00	22.3
10	0	-648	2848	-68	0	-111	-1215	4.02	4.02	4.02	4.02	2	0.18	0.08	0.50	0.00	0.00	22.3
11	0	-512	2947	-68	0	-109	-1453	4.02	4.02	4.02	4.02	2	0.22	0.09	0.52	0.00	0.00	22.3
12	0	-516	2879	120	0	349	-1283	4.02	4.02	4.02	4.02	2	0.19	0.08	0.51	0.00	0.00	22.3
13	0	-380	2978	121	0	351	-1522	4.02	4.02	4.02	4.02	2	0.23	0.09	0.53	0.00	0.00	22.3
14	0	-761	2744	-3	0	48	-961	4.02	4.02	4.02	4.02	2	0.14	0.08	0.48	0.00	0.00	22.3
15	0	-307	3073	-0	0	54	-1755	4.02	4.02	4.02	4.02	2	0.26	0.09	0.54	0.00	0.00	22.3
16	0	-721	2753	53	0	186	-981	4.02	4.02	4.02	4.02	2	0.15	0.08	0.48	0.00	0.00	22.3
17	0	-268	3082	56	0	192	-1775	4.02	4.02	4.02	4.02	2	0.27	0.09	0.55	0.00	0.00	22.3
18	0	-1191	3850	-194	0	-305	-1206	4.02	4.02	4.02	4.02	3	0.17	0.11	0.67	0.00	0.00	22.3
19	0	-575	4107	372	0	1045	-1802	4.02	4.02	4.02	4.02	3	0.25	0.12	0.72	0.00	0.00	22.3
20	0	-1079	4005	90	0	372	-1632	4.02	4.02	4.02	4.02	3	0.23	0.12	0.70	0.00	0.00	22.3
37	0	-1321	3629	-400	0	-825	-1047	4.02	4.02	4.02	4.02	3	0.20	0.10	0.63	0.00	0.00	22.3
38	0	-296	4057	542	0	1426	-2040	4.02	4.02	4.02	4.02	3	0.35	0.12	0.72	0.00	0.00	22.3
39	0	-1135	3888	73	0	304	-1756	4.02	4.02	4.02	4.02	3	0.24	0.11	0.67	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	38	-668	2958	34	0	143	-1779	4.02	4.02	4.02	4.02	3	0.25	0.09	0.52	0.00	0.00	22.3
2	38	-648	2210	-68	0	-86	-1215	4.02	4.02	4.02	4.02	2	0.18	0.06	0.39	0.00	0.00	22.3
3	38	-512	2309	-68	0	-84	-1453	4.02	4.02	4.02	4.02	2	0.22	0.07	0.41	0.00	0.00	22.3
4	38	-516	2241	120	0	304	-1283	4.02	4.02	4.02	4.02	2	0.19	0.06	0.39	0.00	0.00	22.3
5	38	-380	2340	121	0	306	-1522	4.02	4.02	4.02	4.02	2	0.23	0.07	0.41	0.00	0.00	22.3
6	38	-761	2106	-3	0	49	-961	4.02	4.02	4.02	4.02	2	0.14	0.06	0.37	0.00	0.00	22.3
7	38	-307	2435	-0	0	54	-1755	4.02	4.02	4.02	4.02	2	0.26	0.07	0.43	0.00	0.00	22.3
8	38	-721	2115	53	0	166	-981	4.02	4.02	4.02	4.02	2	0.15	0.06	0.37	0.00	0.00	22.3
9	38	-268	2444	56	0	171	-1775	4.02	4.02	4.02	4.02	2	0.27	0.07	0.43	0.00	0.00	22.3
10	38	-648	2210	-68	0	-86	-1215	4.02	4.02	4.02	4.02	2	0.18	0.06	0.39	0.00	0.00	22.3
11	38	-512	2309	-68	0	-84	-1453	4.02	4.02	4.02	4.02	2	0.22	0.07	0.41	0.00	0.00	22.3
12	38	-516	2241	120	0	304	-1283	4.02	4.02	4.02	4.02	2	0.19	0.06	0.39	0.00	0.00	22.3
13	38	-380	2340	121	0	306	-1522	4.02	4.02	4.02	4.02	2	0.23	0.07	0.41	0.00	0.00	22.3
14	38	-761	2106	-3	0	49	-961	4.02	4.02	4.02	4.02	2	0.14	0.06	0.37	0.00	0.00	22.3
15	38	-307	2435	-0	0	54	-1755	4.02	4.02	4.02	4.02	2	0.26	0.07	0.43	0.00	0.00	22.3
16	38	-721	2115	53	0	166	-981	4.02	4.02	4.02	4.02	2	0.15	0.06	0.37	0.00	0.00	22.3
17	38	-268	2444	56	0	171	-1775	4.02	4.02	4.02	4.02	2	0.27	0.07	0.43	0.00	0.00	22.3
18	38	-1191	2941	-194	0	-233	1556	4.02	4.02	4.02	4.02	3	0.22	0.08	0.51	0.00	0.00	22.3
19	38	-575	3198	372	0	906	-1802	4.02	4.02	4.02	4.02	3	0.25	0.09	0.56	0.00	0.00	22.3

20	38	-1079	3096	90	0	338	-1632	4.02	4.02	4.02	4.02	3	0.23	0.09	0.54	0.00	0.00	22.3
37	38	-1321	2760	-400	0	-675	1548	4.02	4.02	4.02	4.02	3	0.21	0.08	0.48	0.00	0.00	22.3
38	38	-296	3188	542	0	1223	-2040	4.02	4.02	4.02	4.02	3	0.30	0.09	0.56	0.00	0.00	22.3
39	38	-1135	3019	73	0	277	-1756	4.02	4.02	4.02	4.02	3	0.24	0.09	0.52	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	75	-668	2129	34	0	130	1436	4.02	4.02	4.02	4.02	3	0.20	0.06	0.37	0.00	0.00	22.3
2	75	-648	1573	-68	0	-60	1145	4.02	4.02	4.02	4.02	2	0.17	0.05	0.28	0.00	0.00	22.3
3	75	-512	1672	-68	0	-59	1083	4.02	4.02	4.02	4.02	2	0.16	0.05	0.29	0.00	0.00	22.3
4	75	-516	1604	120	0	259	1127	4.02	4.02	4.02	4.02	2	0.17	0.05	0.28	0.00	0.00	22.3
5	75	-380	1703	121	0	260	1073	4.02	4.02	4.02	4.02	2	0.16	0.05	0.30	0.00	0.00	22.3
6	75	-761	1469	-3	0	50	1242	4.02	4.02	4.02	4.02	2	0.18	0.04	0.26	0.00	0.00	22.3
7	75	-307	1798	-0	0	54	982	4.02	4.02	4.02	4.02	2	0.15	0.05	0.32	0.00	0.00	22.3
8	75	-721	1478	53	0	146	1235	4.02	4.02	4.02	4.02	2	0.18	0.04	0.26	0.00	0.00	22.3
9	75	-268	1807	56	0	150	973	4.02	4.02	4.02	4.02	2	0.15	0.05	0.32	0.00	0.00	22.3
10	75	-648	1573	-68	0	-60	1145	4.02	4.02	4.02	4.02	2	0.17	0.05	0.28	0.00	0.00	22.3
11	75	-512	1672	-68	0	-59	1083	4.02	4.02	4.02	4.02	2	0.16	0.05	0.29	0.00	0.00	22.3
12	75	-516	1604	120	0	259	1127	4.02	4.02	4.02	4.02	2	0.17	0.05	0.28	0.00	0.00	22.3
13	75	-380	1703	121	0	260	1073	4.02	4.02	4.02	4.02	2	0.16	0.05	0.30	0.00	0.00	22.3
14	75	-761	1469	-3	0	50	1242	4.02	4.02	4.02	4.02	2	0.18	0.04	0.26	0.00	0.00	22.3
15	75	-307	1798	-0	0	54	982	4.02	4.02	4.02	4.02	2	0.15	0.05	0.32	0.00	0.00	22.3
16	75	-721	1478	53	0	146	1235	4.02	4.02	4.02	4.02	2	0.18	0.04	0.26	0.00	0.00	22.3
17	75	-268	1807	56	0	150	973	4.02	4.02	4.02	4.02	2	0.15	0.05	0.32	0.00	0.00	22.3
18	75	-1191	2032	-194	0	-160	1841	4.02	4.02	4.02	4.02	3	0.26	0.06	0.35	0.00	0.00	22.3
19	75	-575	2289	372	0	766	1637	4.02	4.02	4.02	4.02	3	0.23	0.07	0.40	0.00	0.00	22.3
20	75	-1079	2187	90	0	304	1648	4.02	4.02	4.02	4.02	3	0.23	0.06	0.38	0.00	0.00	22.3
37	75	-1321	1891	-400	0	-525	1790	4.02	4.02	4.02	4.02	3	0.25	0.05	0.33	0.00	0.00	22.3
38	75	-296	2319	542	0	1019	1494	4.02	4.02	4.02	4.02	3	0.25	0.07	0.41	0.00	0.00	22.3
39	75	-1135	2150	73	0	249	1469	4.02	4.02	4.02	4.02	3	0.20	0.06	0.37	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	112	-668	1300	34	0	117	1436	4.02	4.02	4.02	4.02	3	0.20	0.04	0.23	0.00	0.00	22.3
2	112	-648	935	-68	0	-34	1145	4.02	4.02	4.02	4.02	2	0.17	0.03	0.16	0.00	0.00	22.3
3	112	-512	1034	-68	0	-33	1083	4.02	4.02	4.02	4.02	2	0.16	0.03	0.18	0.00	0.00	22.3
4	112	-516	966	120	0	214	1127	4.02	4.02	4.02	4.02	2	0.17	0.03	0.17	0.00	0.00	22.3
5	112	-380	1065	121	0	215	1073	4.02	4.02	4.02	4.02	2	0.16	0.03	0.19	0.00	0.00	22.3
6	112	-761	831	-3	0	52	1242	4.02	4.02	4.02	4.02	2	0.18	0.02	0.15	0.00	0.00	22.3
7	112	-307	1160	-0	0	54	1018	4.02	4.02	4.02	4.02	2	0.15	0.03	0.21	0.00	0.00	22.3
8	112	-721	840	53	0	126	1235	4.02	4.02	4.02	4.02	2	0.18	0.02	0.15	0.00	0.00	22.3
9	112	-268	1169	56	0	129	1015	4.02	4.02	4.02	4.02	2	0.15	0.03	0.21	0.00	0.00	22.3
10	112	-648	935	-68	0	-34	1145	4.02	4.02	4.02	4.02	2	0.17	0.03	0.16	0.00	0.00	22.3
11	112	-512	1034	-68	0	-33	1083	4.02	4.02	4.02	4.02	2	0.16	0.03	0.18	0.00	0.00	22.3
12	112	-516	966	120	0	214	1127	4.02	4.02	4.02	4.02	2	0.17	0.03	0.17	0.00	0.00	22.3
13	112	-380	1065	121	0	215	1073	4.02	4.02	4.02	4.02	2	0.16	0.03	0.19	0.00	0.00	22.3
14	112	-761	831	-3	0	52	1242	4.02	4.02	4.02	4.02	2	0.18	0.02	0.15	0.00	0.00	22.3
15	112	-307	1160	-0	0	54	1018	4.02	4.02	4.02	4.02	2	0.15	0.03	0.21	0.00	0.00	22.3
16	112	-721	840	53	0	126	1235	4.02	4.02	4.02	4.02	2	0.18	0.02	0.15	0.00	0.00	22.3
17	112	-268	1169	56	0	129	1015	4.02	4.02	4.02	4.02	2	0.15	0.03	0.21	0.00	0.00	22.3
18	112	-1191	1123	-194	0	-87	1841	4.02	4.02	4.02	4.02	3	0.26	0.03	0.19	0.00	0.00	22.3
19	112	-575	1380	372	0	627	1637	4.02	4.02	4.02	4.02	3	0.23	0.04	0.24	0.00	0.00	22.3
20	112	-1079	1278	90	0	271	1648	4.02	4.02	4.02	4.02	3	0.23	0.04	0.22	0.00	0.00	22.3
37	112	-1321	1022	-400	0	-375	1790	4.02	4.02	4.02	4.02	3	0.25	0.03	0.18	0.00	0.00	22.3
38	112	-296	1450	542	0	816	1494	4.02	4.02	4.02	4.02	3	0.21	0.04	0.26	0.00	0.00	22.3
39	112	-1135	1281	73	0	222	1469	4.02	4.02	4.02	4.02	3	0.20	0.04	0.22	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	150	-668	471	34	0	105	1436	4.02	4.02	4.02	4.02	3	0.20	0.01	0.08	0.00	0.00	22.3
2	150	-648	298	-68	0	-9	1145	4.02	4.02	4.02	4.02	2	0.17	0.01	0.05	0.00	0.00	22.3
3	150	-512	397	-68	0	-8	1083	4.02	4.02	4.02	4.02	2	0.16	0.01	0.07	0.00	0.00	22.3
4	150	-516	329	120	0	169	1127	4.02	4.02	4.02	4.02	2	0.17	0.01	0.06	0.00	0.00	22.3
5	150	-380	428	121	0	169	1073	4.02	4.02	4.02	4.02	2	0.16	0.01	0.08	0.00	0.00	22.3
6	150	-761	194	-3	0	53	1242	4.02	4.02	4.02	4.02	2	0.18	0.01	0.03	0.00	0.00	22.3
7	150	-307	523	-0	0	55	1018	4.02	4.02	4.02	4.02	2	0.15	0.02	0.09	0.00	0.00	22.3
8	150	-721	203	53	0	106	1235	4.02	4.02	4.02	4.02	2	0.18	0.01	0.04	0.00	0.00	22.3
9	150	-268	532	56	0	108	1015	4.02	4.02	4.02	4.02	2	0.15	0.02	0.09	0.00	0.00	22.3
10	150	-648	298	-68	0	-9	1145	4.02	4.02	4.02	4.02	2	0.17	0.01	0.05	0.00	0.00	22.3
11	150	-512	397	-68	0	-8	1083	4.02	4.02	4.02	4.02	2	0.16	0.01	0.07	0.00	0.00	22.3
12	150	-516	329	120	0	169	1127	4.02	4.02	4.02	4.02	2	0.17	0.01	0.06	0.00	0.00	22.3
13	150	-380	428	121	0	169	1073	4.02	4.02	4.02	4.02	2	0.16	0.01	0.08	0.00	0.00	22.3
14	150	-761	194	-3	0	53	1242	4.02	4.02	4.02	4.02	2	0.18	0.01	0.03	0.00	0.00	22.3
15	150	-307	523	-0	0	55	1018	4.02	4.02	4.02	4.02	2	0.15	0.02	0.09	0.00	0.00	22.3
16	150	-721	203	53	0	106	1235	4.02	4.02	4.02	4.02	2	0.18	0.01	0.04	0.00	0.00	22.3
17	150	-268	532	56	0	108	1015	4.02	4.02	4.02	4.02	2	0.15	0.02	0.09	0.00	0.00	22.3
18	150	-1191	214	-194	0	-15	1841	4.02	4.02	4.02	4.02	3	0.26	0.01	0.04	0.00	0.00	22.3
19	150	-575	471	372	0	488	1637	4.02	4.02	4.02	4.02	3	0.23	0.01	0.08	0.00	0.00	22.3
20	150	-1079	369	90	0	237	1648	4.02	4.02	4.02	4.02	3	0.23	0.01	0.06	0.00	0.00	22.3
37	150	-1321	153	-400	0	-225	1790	4.02	4.02	4.02	4.02	3	0.25	0.01	0.06	0.00	0.00	22.3
38	150	-296	581	542	0	612	1494	4.02	4.02	4.02	4.02	3	0.21	0.02	0.10	0.00	0.00	22.3
39	150	-1135	412	73	0	195	1469	4.02	4.02	4.02	4.02	3	0.20	0.01	0.07	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	188	-668	-358	34	0	92	1436	4.02	4.02	4.02	4.02	3	0.20	0.01	0.06	0.00	0.00	22.3
2	188	-648	-340	-68	0	17	1145	4.02	4.02	4.02	4.02	2	0.17	0.01	0.06	0.00	0.00	22.3
3	188	-512	-241	-68	0	17	1083	4.02	4.02	4.02	4.02	2	0.16	0.01	0.04	0.00	0.00	22.3
4	188	-516	-309	120	0	124	1127	4.02	4.02	4.02	4.02	2	0.17	0.01	0.05	0.00	0.00	22.3
5	188	-380	-210	121	0	124	1073	4.02	4.02	4.02	4.02	2	0.16	0.01	0.04	0.00	0.00	22.3
6	188	-761	-444	-3	0	54	1242	4.02	4.02	4.02	4.02	2	0.18	0.01	0.08	0.00	0.00	22.3
7	188	-307	-115	-0	0	55	1018	4.02	4.02	4.02	4.02	2	0.15	0.00	0.02	0.00	0.00	22.3
8	188	-721	-435	53	0	86	1235	4.02	4.02	4.02	4.02	2	0.18	0.01	0.08	0.00	0.00	22.3
9	188	-268	-106	56	0	87	1015	4.02	4.02	4.02	4.02	2	0.15	0.00	0.02	0.00	0.00	22.3
10	188	-648	-340	-68	0	17	1145	4.02	4.02	4.02	4.02	2	0.17	0.01	0.06	0.00	0.00	22.3
11	188	-512	-241	-68	0	17	1083	4.02	4.02	4.02	4.02	2	0.16	0.01	0.04	0.00	0.00	22.3
12	188	-516	-309	120	0	124	1127	4.02	4.02	4.02	4.02	2	0.17	0.01	0.05	0.00	0.00	22.3
13	188	-380	-210	121	0	124	1073	4.02	4.02	4.02	4.02	2	0.16	0.01	0.04	0.00	0.00	22.3
14	188	-761	-444	-3	0	54	1242	4.02	4.02	4.02	4.02	2	0.18	0.01	0.08	0.00	0.00	22.3
15	188	-307	-115	-0	0	55	1018	4.02	4.02	4.02	4.02	2	0.15	0.00	0.02	0.00	0.00	22.3
16	188	-721	-435	53	0	86	1235	4.02	4.02	4.02	4.02	2	0.18	0.01	0.08	0.00	0.00	22.3
17	188	-268	-106	56	0	87	1015	4.02	4.02	4.02	4.02	2	0.15	0.00	0.02	0.00	0.00	22.3
18	188	-1191	-696	-194	0	58	1841	4.02	4.02	4.02	4.02	3	0.26	0.02	0.12	0.00	0.00	22.3
19	188	-575	-438	372	0	348	1637	4.02	4.02	4.02	4.02	3	0.23	0.01	0.08	0.00	0.00	22.3
20	188	-1079	-540	90	0	203	1648	4.02	4.02	4.02	4.02	3	0.23	0.02	0.09	0.00	0.00	22.3
37	188	-1321	-716	-400	0	-75	1790	4.02	4.02	4.02	4.02	3	0.25	0.02	0.12	0.00	0.00	22.3
38	188	-296	-288	542	0	409	1494	4.02	4.02	4.02	4.02	3	0.21	0.02	0.09	0.00	0.00	22.3
39	188	-1135	-457	73	0	167	1469	4.02	4.02	4.02	4.02	3	0.20	0.01	0.08	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	225	-668	-1186	34	0	79	1436	4.02	4.02	4.02	4.02	3	0.20	0.03	0.21	0.00	0.00	22.3
2	225	-648	-978	-68	0	43	1145	4.02	4.02	4.02	4.02	2	0.17	0.03	0.17	0.00	0.00	22.3
3	225	-512	-879	-68	0	43	1083	4.02	4.02	4.02	4.02	2	0.16	0.03	0.15	0.00	0.00	22.3
4	225	-516	-947	120	0	79	1127	4.02	4.02	4.02	4.02	2	0.17	0.03	0.17	0.00	0.00	22.3
5	225	-380	-848	121	0	79	1073	4.02	4.02	4.02	4.02	2	0.16	0.02	0.15	0.00	0.00	22.3
6	225	-761	-1082	-3	0	56	1242	4.02	4.02	4.02	4.02	2	0.18	0.03	0.19	0.00	0.00	22.3
7	225	-307	-753	-0	0	55	1018	4.02	4.02	4.02	4.02	2	0.15	0.02	0.13	0.00	0.00	22.3
8	225	-721	-1073	53	0	66	1235	4.02	4.02	4.02	4.02	2	0.18	0.03	0.19	0.00	0.00	22.3
9	225	-268	-744	56	0	66	1015	4.02	4.02	4.02	4.02	2	0.15	0.02	0.13	0.00	0.00	22.3
10	225	-648	-978	-68	0	43	1145	4.02	4.02	4.02	4.02	2	0.17	0.03	0.17	0.00	0.00	22.3
11	225	-512	-879	-68	0	43	1083	4.02	4.02	4.02	4.02	2	0.16	0.03	0.15	0.00	0.00	22.3
12	225	-516	-947	120	0	79	1127	4.02	4.02	4.02	4.02	2	0.17	0.03	0.17	0.00	0.00	22.3
13	225	-380	-848	121	0	79	1073	4.02	4.02	4.02	4.02	2	0.16	0.02	0.15	0.00	0.00	22.3
14	225	-761	-1082	-3	0	56	1242	4.02	4.02	4.02	4.02	2	0.18	0.03	0.19	0.00	0.00	22.3
15	225	-307	-753	-0	0	55	1018	4.02	4.02	4.02	4.02	2	0.15	0.02	0.13	0.00	0.00	22.3
16	225	-721	-1073	53	0	66	1235	4.02	4.02	4.02	4.02	2	0.18	0.03	0.19	0.00	0.00	22.3
17	225	-268	-744	56	0	66	1015	4.02	4.02	4.02	4.02	2	0.15	0.02	0.13	0.00	0.00	22.3
18	225	-1191	-1605	-194	0	131	1841	4.02	4.02	4.02	4.02	3	0.26	0.05	0.28	0.00	0.00	22.3
19	225	-575	-1348	372	0	209	1637	4.02	4.02	4.02	4.02	3	0.23	0.04	0.24	0.00	0.00	22.3
20	225	-1079	-1449	90	0	169	1648	4.02	4.02	4.02	4.02	3	0.23	0.04	0.25	0.00	0.00	22.3
37	225	-1321	-1584	-400	0	75	1790	4.02	4.02	4.02	4.02	3	0.25	0.05	0.27	0.00	0.00	22.3
38	225	-296	-1156	542	0	205	1494	4.02	4.02	4.02	4.02	3	0.21	0.03	0.20	0.00	0.00	22.3
39	225	-1135	-1326	73	0	140	1469	4.02	4.02	4.02	4.02	3	0.20	0.04	0.23	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	262	-668	-2015	34	0	66	1436	4.02	4.02	4.02	4.02	3	0.20	0.06	0.35	0.00	0.00	22.3
2	262	-648	-1615	-68	0	68	1145	4.02	4.02	4.02	4.02	2	0.17	0.05	0.28	0.00	0.00	22.3
3	262	-512	-1516	-68	0	68	1083	4.02	4.02	4.02	4.02	2	0.16	0.04	0.27	0.00	0.00	22.3
4	262	-516	-1584	120	0	34	1127	4.02	4.02	4.02	4.02	2	0.17	0.05	0.28	0.00	0.00	22.3
5	262	-380	-1485	121	0	33	1073	4.02	4.02	4.02	4.02	2	0.16	0.04	0.26	0.00	0.00	22.3
6	262	-761	-1719	-3	0	57	1242	4.02	4.02	4.02	4.02	2	0.18	0.05	0.30	0.00	0.00	22.3
7	262	-307	-1390	-0	0	55	1018	4.02	4.02	4.02	4.02	2	0.15	0.04	0.25	0.00	0.00	22.3
8	262	-721	-1710	53	0	46	1235	4.02	4.02	4.02	4.02	2	0.18	0.05	0.30	0.00	0.00	22.3
9	262	-268	-1381	56	0	45	1015	4.02	4.02	4.02	4.02	2	0.15	0.04	0.24	0.00	0.00	22.3
10	262	-648	-1615	-68	0	68	1145	4.02	4.02	4.02	4.02	2	0.17	0.05	0.28	0.00	0.00	22.3
11	262	-512	-1516	-68	0	68	1083	4.02	4.02	4.02	4.02	2	0.16	0.04	0.27	0.00	0.00	22.3
12	262	-516	-1584	120	0	34	1127	4.02	4.02	4.02	4.02	2	0.17	0.05	0.28	0.00	0.00	22.3
13	262	-380	-1485	121	0	33	1073	4.02	4.02	4.02	4.02	2	0.16	0.04	0.26	0.00	0.00	22.3
14	262	-761	-1719	-3	0	57	1242	4.02	4.02	4.02	4.02	2	0.18	0.05	0.30	0.00	0.00	22.3
15	262	-307	-1390	-0	0	55	1018	4.02	4.02	4.02	4.02	2	0.15	0.04	0.25	0.00	0.00	22.3
16	262	-721	-1710	53	0	46	1235	4.02	4.02	4.02	4.02	2	0.18	0.05	0.30	0.00	0.00	22.3
17	262	-268	-1381	56	0	45	1015	4.02	4.02	4.02	4.02	2	0.15	0.04	0.24	0.00	0.00	22.3
18	262	-1191	-2514	-194	0	204	1820	4.02	4.02	4.02	4.02	3	0.25	0.07	0.44	0.00	0.00	22.3
19	262	-575	-2257	372	0	70	1637	4.02	4.02	4.02	4.02	3	0.23	0.07	0.40	0.00	0.00	22.3
20	262	-1079	-2358	90	0	136	1648	4.02	4.02	4.02	4.02	3	0.23	0.07	0.41	0.00	0.00	22.3
37	262	-1321	-2453	-400	0	225	1738	4.02	4.02	4.02	4.02	3	0.24	0.07	0.42	0.00	0.00	22.3
38	262	-296	-2025	542	0	2	1494	4.02	4.02	4.02	4.02	3	0.21	0.06	0.36	0.00	0.00	22.3
39	262	-1135	-2195	73	0	112	1469	4.02	4.02	4.02	4.02	3	0.20	0.06	0.38	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	300	-668	-2844	34	0	53	-1804	4.02	4.02	4.02	4.02	3	0.25	0.08	0.50	0.00	0.00	22.3
2	300	-648	-2253	-68	0	94	-1462	4.02	4.02	4.02	4.02	2	0.22	0.07	0.40	0.00	0.00	22.3
3	300	-512	-2154	-68	0	93	-1355	4.02	4.02	4.02	4.02	2	0.20	0.06	0.38	0.00	0.00	22.3
4	300	-516	-2222	120	0	-11	-1421	4.02	4.02	4.02	4.02	2	0.21	0.06	0.39	0.00	0.00	22.3
5	300	-380	-2123	121	0	-12	-1313	4.02	4.02	4.02	4.02	2	0.20	0.06	0.37	0.00	0.00	22.3
6	300	-761	-2357	-3	0	58	-1573	4.02	4.02	4.02	4.02	2	0.23	0.07	0.41	0.00	0.00	22.3
7	300	-307	-2028	-0	0	55	-1214	4.02	4.02	4.02	4.02	2	0.18	0.06	0.36	0.00	0.00	22.3
8	300	-721	-2348	53	0	26	-1562	4.02	4.02	4.02	4.02	2	0.23	0.07	0.41	0.00	0.00	22.3
9	300	-268	-2019	56	0	24	-1203	4.02	4.02	4.02	4.02	2	0.18	0.06	0.36	0.00	0.00	22.3
10	300	-648	-2253	-68	0	94	-1462	4.02	4.02	4.02	4.02	2	0.22	0.07	0.40	0.00	0.00	22.3
11	300	-512	-2154	-68	0	93	-1355	4.02	4.02	4.02	4.02	2	0.20	0.06	0.38	0.00	0.00	22.3
12	300	-516	-2222	120	0	-11	-1421	4.02	4.02	4.02	4.02	2	0.21	0.06	0.39	0.00	0.00	22.3
13	300	-380	-2123	121	0	-12	-1313	4.02	4.02	4.02	4.02	2	0.20	0.06	0.37	0.00	0.00	22.3
14	300	-761	-2357	-3	0	58	-1573	4.02	4.02	4.02	4.02	2	0.23	0.07	0.41	0.00	0.00	22.3
15	300	-307	-2028	-0	0	55	-1214	4.02	4.02	4.02	4.02	2	0.18	0.06	0.36	0.00	0.00	22.3
16	300	-721	-2348	53	0	26	-1562	4.02	4.02	4.02	4.02	2	0.23	0.07	0.41	0.00	0.00	22.3
17	300	-268	-2019	56	0	24	-1203	4.02	4.02	4.02	4.02	2	0.18	0.06	0.36	0.00	0.00	22.3
18	300	-1191	-3423	-194	0	276	-2298	4.02	4.02	4.02	4.02	3	0.32	0.10	0.59	0.00	0.00	22.3
19	300	-575	-3166	372	0	-70	-1994	4.02	4.02	4.02	4.02	3	0.28	0.09	0.56	0.00	0.00	22.3
20	300	-1079	-3267	90	0	102	-2180	4.02	4.02	4.02	4.02	3	0.30	0.09	0.57	0.00	0.00	22.3
37	300	-1321	-3322	-400	0	375	-2268	4.02	4.02	4.02	4.02	3	0.31	0.10	0.57	0.00	0.00	22.3
38	300	-296	-2894	542	0	-201	-1761	4.02	4.02	4.02	4.02	3	0.25	0.08	0.51	0.00	0.00	22.3
39	300	-1135	-3064	73	0	85	-2071	4.02	4.02	4.02	4.02	3	0.29	0.09	0.53	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	338	-668	-3673	34	0	40	-3119	4.02	4.02	4.02	4.02	3	0.44	0.11	0.64	0.00	0.00	22.3
2	338	-648	-2890	-68	0	120	-2489	4.02	4.02	4.02	4.02	2	0.37	0.08	0.51	0.00	0.00	22.3
3	338	-512	-2791	-68	0	119	-2358	4.02	4.02	4.02	4.02	2	0.35	0.08	0.49	0.00	0.00	22.3
4	338	-516	-2859	120	0	-57	-2441	4.02	4.02	4.02	4.02	2	0.36	0.08	0.50	0.00	0.00	22.3
5	338	-380	-2760	121	0	-58	-2309	4.02	4.02	4.02	4.02	2	0.35	0.08	0.49	0.00	0.00	22.3
6	338	-761	-2994	-3	0	59	-2626	4.02	4.02	4.02	4.02	2	0.39	0.09	0.52	0.00	0.00	22.3
7	338	-307	-2665	-0	0	55	-2187	4.02	4.02	4.02	4.02	2	0.33	0.08	0.47	0.00	0.00	22.3
8	338	-721	-2985	53	0	7	-2612	4.02	4.02	4.02	4.02	2	0.39	0.09	0.52	0.00	0.00	22.3
9	338	-268	-2656	56	0	3	-2173	4.02	4.02	4.02	4.02	2	0.33	0.08	0.47	0.00	0.00	22.3
10	338	-648	-2890	-68	0	120	-2489	4.02	4.02	4.02	4.02	2	0.37	0.08	0.51	0.00	0.00	22.3
11	338	-512	-2791	-68	0	119	-2358	4.02	4.02	4.02	4.02	2	0.35	0.08	0.49	0.00	0.00	22.3
12	338	-516	-2859	120	0	-57	-2441	4.02	4.02	4.02	4.02	2	0.36	0.08	0.50	0.00	0.00	22.3
13	338	-380	-2760	121	0	-58	-2309	4.02	4.02	4.02	4.02	2	0.35	0.08	0.49	0.00	0.00	22.3
14	338	-761	-2994	-3	0	59	-2626	4.02	4.02	4.02	4.02	2	0.39	0.09	0.52	0.00	0.00	22.3
15	338	-307	-2665	-0	0	55	-2187	4.02	4.02	4.02	4.02	2	0.33	0.08	0.47	0.00	0.00	22.3
16	338	-721	-2985	53	0	7	-2612	4.02	4.02	4.02	4.02	2	0.39	0.09	0.52	0.00	0.00	22.3
17	338	-268	-2656	56	0	3	-2173	4.02	4.02	4.02	4.02	2	0.33	0.08	0.47	0.00	0.00	22.3
18	338	-1191	-4332	-194	0	349	-3814	4.02	4.02	4.02	4.02	3	0.53	0.13	0.75	0.00	0.00	22.3
19	338	-575	-4075	372	0	-209	-3447	4.02	4.02	4.02	4.02	3	0.49	0.12	0.72	0.00	0.00	22.3
20	338	-1079	-4176	90	0	68	-3658	4.02	4.02	4.02	4.02	3	0.51	0.12	0.72	0.00	0.00	22.3
37	338	-1321	-4191	-400	0	525	-3730	4.02	4.02	4.02	4.02	3	0.51	0.12	0.72	0.00	0.00	22.3
38	338	-296	-3763	542	0	-405	-3118	4.02	4.02	4.02	4.02	3	0.44	0.11	0.67	0.00	0.00	22.3
39	338	-1135	-3933	73	0	57	-3470	4.02	4.02	4.02	4.02	3	0.48	0.11	0.68	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	375	-668	-4502	34	0	27	-3119	4.02	4.02	4.02	4.02	3	0.44	0.13	0.79	0.00	0.00	22.3
2	375	-648	-3528	-68	0	145	-2489	4.02	4.02	4.02	4.02	2	0.37	0.10	0.62	0.00	0.00	22.3
3	375	-512	-3429	-68	0	144	-2358	4.02	4.02	4.02	4.02	2	0.35	0.10	0.60	0.00	0.00	22.3
4	375	-516	-3497	120	0	-102	-2441	4.02	4.02	4.02	4.02	2	0.36	0.10	0.62	0.00	0.00	22.3
5	375	-380	-3398	121	0	-103	-2309	4.02	4.02	4.02	4.02	2	0.35	0.10	0.60	0.00	0.00	22.3

6	375	-761	-3632	-3	0	61	-2626	4.02	4.02	4.02	4.02	2	0.39	0.11	0.64	0.00	0.00	22.3
7	375	-307	-3303	-0	0	56	-2187	4.02	4.02	4.02	4.02	2	0.33	0.10	0.58	0.00	0.00	22.3
8	375	-721	-3623	53	0	-13	-2612	4.02	4.02	4.02	4.02	2	0.39	0.10	0.63	0.00	0.00	22.3
9	375	-268	-3294	56	0	-18	-2173	4.02	4.02	4.02	4.02	2	0.33	0.10	0.58	0.00	0.00	22.3
10	375	-648	-3528	-68	0	145	-2489	4.02	4.02	4.02	4.02	2	0.37	0.10	0.62	0.00	0.00	22.3
11	375	-512	-3429	-68	0	144	-2358	4.02	4.02	4.02	4.02	2	0.35	0.10	0.60	0.00	0.00	22.3
12	375	-516	-3497	120	0	-102	-2441	4.02	4.02	4.02	4.02	2	0.36	0.10	0.62	0.00	0.00	22.3
13	375	-380	-3398	121	0	-103	-2309	4.02	4.02	4.02	4.02	2	0.35	0.10	0.60	0.00	0.00	22.3
14	375	-761	-3632	-3	0	61	-2626	4.02	4.02	4.02	4.02	2	0.39	0.11	0.64	0.00	0.00	22.3
15	375	-307	-3303	-0	0	56	-2187	4.02	4.02	4.02	4.02	2	0.33	0.10	0.58	0.00	0.00	22.3
16	375	-721	-3623	53	0	-13	-2612	4.02	4.02	4.02	4.02	2	0.39	0.10	0.63	0.00	0.00	22.3
17	375	-268	-3294	56	0	-18	-2173	4.02	4.02	4.02	4.02	2	0.33	0.10	0.58	0.00	0.00	22.3
18	375	-1191	-5241	-194	0	422	-3814	4.02	4.02	4.02	4.02	3	0.53	0.15	0.91	0.00	0.00	22.3
19	375	-575	-4984	372	0	-348	-3447	4.02	4.02	4.02	4.02	3	0.49	0.14	0.88	0.00	0.00	22.3
20	375	-1079	-5085	90	0	34	-3658	4.02	4.02	4.02	4.02	3	0.51	0.15	0.88	0.00	0.00	22.3
37	375	-1321	-5060	-400	0	675	-3730	4.02	4.02	4.02	4.02	3	0.51	0.15	0.87	0.00	0.00	22.3
38	375	-296	-4632	542	0	-608	-3118	4.02	4.02	4.02	4.02	3	0.44	0.13	0.82	0.00	0.00	22.3
39	375	-1135	-4802	73	0	30	-3470	4.02	4.02	4.02	4.02	3	0.48	0.14	0.83	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

Nome travata: **trave_504_IP1** Descrizione: **Trave_5 11-10-9-8**
ASTA NUM. 12 NI 124 NF 214 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y Permanente Neve qy tot.
qy medio: 375.00 1325.25 142.50 1842.75 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-592	4491	15	0	27	-2961	4.02	4.02	4.02	4.02	3	0.42	0.13	0.79	0.00	0.00	22.3
2	0	-520	3425	-11	0	16	-2229	4.02	4.02	4.02	4.02	2	0.33	0.10	0.60	0.00	0.00	22.3
3	0	-475	3458	-11	0	15	-2281	4.02	4.02	4.02	4.02	2	0.34	0.10	0.61	0.00	0.00	22.3
4	0	-437	3451	35	0	27	-2274	4.02	4.02	4.02	4.02	2	0.34	0.10	0.61	0.00	0.00	22.3
5	0	-391	3484	35	0	26	-2326	4.02	4.02	4.02	4.02	2	0.35	0.10	0.61	0.00	0.00	22.3
6	0	-544	3395	5	0	21	-2185	4.02	4.02	4.02	4.02	2	0.33	0.10	0.60	0.00	0.00	22.3
7	0	-392	3506	5	0	18	-2357	4.02	4.02	4.02	4.02	2	0.35	0.10	0.62	0.00	0.00	22.3
8	0	-519	3403	19	0	24	-2198	4.02	4.02	4.02	4.02	2	0.33	0.10	0.60	0.00	0.00	22.3
9	0	-367	3513	18	0	21	-2371	4.02	4.02	4.02	4.02	2	0.36	0.10	0.62	0.00	0.00	22.3
10	0	-520	3425	-11	0	16	-2229	4.02	4.02	4.02	4.02	2	0.33	0.10	0.60	0.00	0.00	22.3
11	0	-475	3458	-11	0	15	-2281	4.02	4.02	4.02	4.02	2	0.34	0.10	0.61	0.00	0.00	22.3
12	0	-437	3451	35	0	27	-2274	4.02	4.02	4.02	4.02	2	0.34	0.10	0.61	0.00	0.00	22.3
13	0	-391	3484	35	0	26	-2326	4.02	4.02	4.02	4.02	2	0.35	0.10	0.61	0.00	0.00	22.3
14	0	-544	3395	5	0	21	-2185	4.02	4.02	4.02	4.02	2	0.33	0.10	0.60	0.00	0.00	22.3
15	0	-392	3506	5	0	18	-2357	4.02	4.02	4.02	4.02	2	0.35	0.10	0.62	0.00	0.00	22.3
16	0	-519	3403	19	0	24	-2198	4.02	4.02	4.02	4.02	2	0.33	0.10	0.60	0.00	0.00	22.3
17	0	-367	3513	18	0	21	-2371	4.02	4.02	4.02	4.02	2	0.36	0.10	0.62	0.00	0.00	22.3
18	0	-844	4827	-27	0	56	-3097	4.02	4.02	4.02	4.02	3	0.43	0.14	0.84	0.00	0.00	22.3
19	0	-521	4956	106	0	72	-3311	4.02	4.02	4.02	4.02	3	0.47	0.14	0.87	0.00	0.00	22.3
20	0	-763	4809	43	0	65	-3045	4.02	4.02	4.02	4.02	3	0.43	0.14	0.84	0.00	0.00	22.3
37	0	-914	4577	-79	0	39	-2897	4.02	4.02	4.02	4.02	3	0.40	0.13	0.80	0.00	0.00	22.3
38	0	-375	4792	143	0	66	-3253	4.02	4.02	4.02	4.02	3	0.46	0.14	0.85	0.00	0.00	22.3
39	0	-779	4546	37	0	54	-2810	4.02	4.02	4.02	4.02	3	0.39	0.13	0.79	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	38	-592	3662	15	0	22	-2961	4.02	4.02	4.02	4.02	3	0.42	0.11	0.64	0.00	0.00	22.3
2	38	-520	2787	-11	0	20	-2229	4.02	4.02	4.02	4.02	2	0.33	0.08	0.49	0.00	0.00	22.3
3	38	-475	2820	-11	0	20	-2281	4.02	4.02	4.02	4.02	2	0.34	0.08	0.50	0.00	0.00	22.3
4	38	-437	2813	35	0	14	-2274	4.02	4.02	4.02	4.02	2	0.34	0.08	0.50	0.00	0.00	22.3
5	38	-391	2846	35	0	13	-2326	4.02	4.02	4.02	4.02	2	0.35	0.08	0.50	0.00	0.00	22.3
6	38	-544	2757	5	0	19	-2185	4.02	4.02	4.02	4.02	2	0.33	0.08	0.48	0.00	0.00	22.3
7	38	-392	2868	5	0	16	-2357	4.02	4.02	4.02	4.02	2	0.35	0.08	0.51	0.00	0.00	22.3
8	38	-519	2765	19	0	17	-2198	4.02	4.02	4.02	4.02	2	0.33	0.08	0.49	0.00	0.00	22.3
9	38	-367	2875	18	0	15	-2371	4.02	4.02	4.02	4.02	2	0.36	0.08	0.51	0.00	0.00	22.3
10	38	-520	2787	-11	0	20	-2229	4.02	4.02	4.02	4.02	2	0.33	0.08	0.49	0.00	0.00	22.3
11	38	-475	2820	-11	0	20	-2281	4.02	4.02	4.02	4.02	2	0.34	0.08	0.50	0.00	0.00	22.3
12	38	-437	2813	35	0	14	-2274	4.02	4.02	4.02	4.02	2	0.34	0.08	0.50	0.00	0.00	22.3
13	38	-391	2846	35	0	13	-2326	4.02	4.02	4.02	4.02	2	0.35	0.08	0.50	0.00	0.00	22.3
14	38	-544	2757	5	0	19	-2185	4.02	4.02	4.02	4.02	2	0.33	0.08	0.48	0.00	0.00	22.3
15	38	-392	2868	5	0	16	-2357	4.02	4.02	4.02	4.02	2	0.35	0.08	0.51	0.00	0.00	22.3
16	38	-519	2765	19	0	17	-2198	4.02	4.02	4.02	4.02	2	0.33	0.08	0.49	0.00	0.00	22.3
17	38	-367	2875	18	0	15	-2371	4.02	4.02	4.02	4.02	2	0.36	0.08	0.51	0.00	0.00	22.3
18	38	-844	3918	-27	0	66	-3097	4.02	4.02	4.02	4.02	3	0.43	0.11	0.68	0.00	0.00	22.3
19	38	-521	4047	106	0	32	-3311	4.02	4.02	4.02	4.02	3	0.47	0.12	0.71	0.00	0.00	22.3
20	38	-763	3900	43	0	49	-3045	4.02	4.02	4.02	4.02	3	0.43	0.11	0.68	0.00	0.00	22.3
37	38	-914	3708	-79	0	69	-2897	4.02	4.02	4.02	4.02	3	0.40	0.11	0.65	0.00	0.00	22.3
38	38	-375	3923	143	0	12	-3253	4.02	4.02	4.02	4.02	3	0.46	0.11	0.69	0.00	0.00	22.3
39	38	-779	3677	37	0	40	-2810	4.02	4.02	4.02	4.02	3	0.39	0.11	0.64	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	75	-592	2833	15	0	16	-1649	4.02	4.02	4.02	4.02	3	0.23	0.08	0.50	0.00	0.00	22.3
2	75	-520	2150	-11	0	24	-1227	4.02	4.02	4.02	4.02	2	0.18	0.06	0.38	0.00	0.00	22.3
3	75	-475	2183	-11	0	24	-1271	4.02	4.02	4.02	4.02	2	0.19	0.06	0.38	0.00	0.00	22.3
4	75	-437	2176	35	0	1	-1266	4.02	4.02	4.02	4.02	2	0.19	0.06	0.38	0.00	0.00	22.3
5	75	-391	2209	35	0	0	-1310	4.02	4.02	4.02	4.02	2	0.20	0.06	0.39	0.00	0.00	22.3
6	75	-544	2120	5	0	17	-1190	4.02	4.02	4.02	4.02	2	0.18	0.06	0.37	0.00	0.00	22.3
7	75	-392	2231	5	0	15	-1335	4.02	4.02	4.02	4.02	2	0.20	0.06	0.39	0.00	0.00	22.3
8	75	-519	2128	19	0	10	-1201	4.02	4.02	4.02	4.02	2	0.18	0.06	0.37	0.00	0.00	22.3
9	75	-367	2238	18	0	8	-1347	4.02	4.02	4.02	4.02	2	0.20	0.06	0.40	0.00	0.00	22.3
10	75	-520	2150	-11	0	24	-1227	4.02	4.02	4.02	4.02	2	0.18	0.06	0.38	0.00	0.00	22.3
11	75	-475	2183	-11	0	24	-1271	4.02	4.02	4.02	4.02	2	0.19	0.06	0.38	0.00	0.00	22.3
12	75	-437	2176	35	0	1	-1266	4.02	4.02	4.02	4.02	2	0.19	0.06	0.38	0.00	0.00	22.3
13	75	-391	2209	35	0	0	-1310	4.02	4.02	4.02	4.02	2	0.20	0.06	0.39	0.00	0.00	22.3
14	75	-544	2120	5	0	17	-1190	4.02	4.02	4.02	4.02	2	0.18	0.06	0.37	0.00	0.00	22.3
15	75	-392	2231	5	0	15	-1335	4.02	4.02	4.02	4.02	2	0.20	0.06	0.39	0.00	0.00	22.3
16	75	-519	2128	19	0	10	-1201	4.02	4.02	4.02	4.02	2	0.18	0.06	0.37	0.00	0.00	22.3
17	75	-367	2238	18	0	8	-1347	4.02	4.02	4.02	4.02	2	0.20	0.06	0.40	0.00	0.00	22.3
18	75	-844	3009	-27	0	76	-1682	4.02	4.02	4.02	4.02	3	0.24	0.09	0.53	0.00	0.00	22.3
19	75	-521	3138	106	0	-7	-1865	4.02	4.02	4.02	4.02	3	0.26	0.09	0.55	0.00	0.00	22.3
20	75	-763	2991	43	0	33	-1634	4.02	4.02	4.02	4.02	3	0.23	0.09	0.52	0.00	0.00	22.3
37	75	-914	2839	-79	0	98	-1553	4.02	4.02	4.02	4.02	3	0.22	0.08	0.49	0.00	0.00	22.3
38	75	-375	3054	143	0	-41	-1857	4.02	4.02	4.02	4.02	3	0.26	0.09	0.54	0.00	0.00	22.3
39	75	-779	2808	37	0	25	-1474	4.02	4.02	4.02	4.02	3	0.21	0.08	0.49	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	112	-592	2004	15	0	10	1573	4.02	4.02	4.02	4.02	3	0.22	0.06	0.35	0.00	0.00	22.3
2	112	-520	1512	-11	0	29	1204	4.02	4.02	4.02	4.02	2	0.18	0.04	0.27	0.00	0.00	22.3
3	112	-475	1545	-11	0	28	1214	4.02	4.02	4.02	4.02	2	0.18	0.04	0.27	0.00	0.00	22.3
4	112	-437	1538	35	0	-12	1207	4.02	4.02	4.02	4.02	2	0.18	0.04	0.27	0.00	0.00	22.3
5	112	-391	1571	35	0	-13	1217	4.02	4.02	4.02	4.02	2	0.18	0.05	0.28	0.00	0.00	22.3
6	112	-544	1482	5	0	15	1192	4.02	4.02	4.02	4.02	2	0.18	0.04	0.26	0.00	0.00	22.3
7	112	-392	1593	5	0	13	1227	4.02	4.02	4.02	4.02	2	0.18	0.05	0.28	0.00	0.00	22.3
8	112	-519	1490	19	0	3	1194	4.02	4.02	4.02	4.02	2	0.18	0.04	0.26	0.00	0.00	22.3
9	112	-367	1600	18	0	1	1231	4.02	4.02	4.02	4.02	2	0.18	0.05	0.28	0.00	0.00	22.3
10	112	-520	1512	-11	0	29	1204	4.02	4.02	4.02	4.02	2	0.18	0.04	0.27	0.00	0.00	22.3
11	112	-475	1545	-11	0	28	1214	4.02	4.02	4.02	4.02	2	0.18	0.04	0.27	0.00	0.00	22.3
12	112	-437	1538	35	0	-12	1207	4.02	4.02	4.02	4.02	2	0.18	0.04	0.27	0.00	0.00	22.3
13	112	-391	1571	35	0	-13	1217	4.02	4.02	4.02	4.02	2	0.18	0.05	0.28	0.00	0.00	22.3
14	112	-544	1482	5	0	15	1192	4.02	4.02	4.02	4.02	2	0.18	0.04	0.26	0.00	0.00	22.3
15	112	-392	1593	5	0	13	1227	4.02	4.02	4.02	4.02	2	0.18	0.05	0.28	0.00	0.00	22.3
16	112	-519	1490	19	0	3	1194	4.02	4.02	4.02	4.02	2	0.18	0.04	0.26	0.00	0.00	22.3
17	112	-367	1600	18	0	1	1231	4.02	4.02	4.02	4.02	2	0.18	0.05	0.28	0.00	0.00	22.3
18	112	-844	2100	-27	0	86	1693	4.02	4.02	4.02	4.02	3	0.24	0.06	0.37	0.00	0.00	22.3
19	112	-521	2229	106	0	-47	1720	4.02	4.02	4.02	4.02	3	0.24	0.06	0.39	0.00	0.00	22.3
20	112	-763	2082	43	0	17	1710	4.02	4.02	4.02	4.02	3	0.24	0.06	0.36	0.00	0.00	22.3
37	112	-914	1970	-79	0	128	1612	4.02	4.02	4.02	4.02	3	0.23	0.06	0.34	0.00	0.00	22.3
38	112	-375	2185	143	0	-95	1663	4.02	4.02	4.02	4.02	3	0.24	0.06	0.39	0.00	0.00	22.3
39	112	-779	1939	37	0	11	1641	4.02	4.02	4.02	4.02	3	0.23	0.06	0.34	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	150	-592	1175	15	0	4	1573	4.02	4.02	4.02	4.02	3	0.22	0.03	0.21	0.00	0.00	22.3
2	150	-520	875	-11	0	33	1204	4.02	4.02	4.02	4.02	2	0.18	0.03	0.15	0.00	0.00	22.3
3	150	-475	908	-11	0	32	1214	4.02	4.02	4.02	4.02	2	0.18	0.03	0.16	0.00	0.00	22.3
4	150	-437	901	35	0	-25	1207	4.02	4.02	4.02	4.02	2	0.18	0.03	0.16	0.00	0.00	22.3
5	150	-391	934	35	0	-26	1217	4.02	4.02	4.02	4.02	2	0.18	0.03	0.16	0.00	0.00	22.3
6	150	-544	845	5	0	13	1192	4.02	4.02	4.02	4.02	2	0.18	0.02	0.15	0.00	0.00	22.3
7	150	-392	956	5	0	11	1227	4.02	4.02	4.02	4.02	2	0.18	0.03	0.17	0.00	0.00	22.3
8	150	-519	853	19	0	-4	1194	4.02	4.02	4.02	4.02	2	0.18	0.02	0.15	0.00	0.00	22.3
9	150	-367	963	18	0	-6	1231	4.02	4.02	4.02	4.02	2	0.18	0.03	0.17	0.00	0.00	22.3
10	150	-520	875	-11	0	33	1204	4.02	4.02	4.02	4.02	2	0.18	0.03	0.15	0.00	0.00	22.3
11	150	-475	908	-11	0	32	1214	4.02	4.02	4.02	4.02	2	0.18	0.03	0.16	0.00	0.00	22.3
12	150	-437	901	35	0	-25	1207	4.02	4.02	4.02	4.02	2	0.18	0.03	0.16	0.00	0.00	22.3
13	150	-391	934	35	0	-26	1217	4.02	4.02	4.02	4.02	2	0.18	0.03	0.16	0.00	0.00	22.3
14	150	-544	845	5	0	13	1192	4.02	4.02	4.02	4.02	2	0.18	0.02	0.15	0.00	0.00	22.3
15	150	-392	956	5	0	11	1227	4.02	4.02	4.02	4.02	2	0.18	0.03	0.17	0.00	0.00	22.3
16	150	-519	853	19	0	-4	1194	4.02	4.02	4.02	4.02	2	0.18	0.02	0.15	0.00	0.00	22.3
17	150	-367	963	18	0	-6	1231	4.02	4.02	4.02	4.02	2	0.18	0.03	0.17	0.00	0.00	22.3
18	150	-844	1191	-27	0	96	1693	4.02	4.02	4.02	4.02	3	0.24	0.03	0.21	0.00	0.00	22.3
19	150	-521	1320	106	0	-87	1720	4.02	4.02	4.02	4.02	3	0.24	0.04	0.23	0.00	0.00	22.3
20	150	-763	1173	43	0	0	1710	4.02	4.02	4.02	4.02	3	0.24	0.03	0.21	0.00	0.00	22.3
37	150	-914	1101	-79	0	157	1612	4.02	4.02	4.02	4.02	3	0.23	0.03	0.19	0.00	0.00	22.3
38	150	-375	1316	143	0	-148	1663	4.02	4.02	4.02	4.02	3	0.24	0.04	0.23	0.00	0.00	22.3
39	150	-779	1070	37	0	-3	1641	4.02	4.02	4.02	4.02	3	0.23	0.03	0.19	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	188	-592	346	15	0	-1	1573	4.02	4.02	4.02	4.02	3	0.22	0.01	0.06	0.00	0.00	22.3
2	188	-520	237	-11	0	37	1204	4.02	4.02	4.02	4.02	2	0.18	0.01	0.04	0.00	0.00	22.3
3	188	-475	270	-11	0	36	1214	4.02	4.02	4.02	4.02	2	0.18	0.01	0.05	0.00	0.00	22.3
4	188	-437	263	35	0	-38	1207	4.02	4.02	4.02	4.02	2	0.18	0.01	0.05	0.00	0.00	22.3
5	188	-391	296	35	0	-39	1217	4.02	4.02	4.02	4.02	2	0.18	0.01	0.05	0.00	0.00	22.3
6	188	-544	207	5	0	11	1192	4.02	4.02	4.02	4.02	2	0.18	0.01	0.04	0.00	0.00	22.3
7	188	-392	318	5	0	10	1227	4.02	4.02	4.02	4.02	2	0.18	0.01	0.06	0.00	0.00	22.3
8	188	-519	215	19	0	-12	1194	4.02	4.02	4.02	4.02	2	0.18	0.01	0.04	0.00	0.00	22.3
9	188	-367	325	18	0	-13	1231	4.02	4.02	4.02	4.02	2	0.18	0.01	0.06	0.00	0.00	22.3
10	188	-520	237	-11	0	37	1204	4.02	4.02	4.02	4.02	2	0.18	0.01	0.04	0.00	0.00	22.3
11	188	-475	270	-11	0	36	1214	4.02	4.02	4.02	4.02	2	0.18	0.01	0.05	0.00	0.00	22.3
12	188	-437	263	35	0	-38	1207	4.02	4.02	4.02	4.02	2	0.18	0.01	0.05	0.00	0.00	22.3
13	188	-391	296	35	0	-39	1217	4.02	4.02	4.02	4.02	2	0.18	0.01	0.05	0.00	0.00	22.3
14	188	-544	207	5	0	11	1192	4.02	4.02	4.02	4.02	2	0.18	0.01	0.04	0.00	0.00	22.3
15	188	-392	318	5	0	10	1227	4.02	4.02	4.02	4.02	2	0.18	0.01	0.06	0.00	0.00	22.3
16	188	-519	215	19	0	-12	1194	4.02	4.02	4.02	4.02	2	0.18	0.01	0.04	0.00	0.00	22.3
17	188	-367	325	18	0	-13	1231	4.02	4.02	4.02	4.02	2	0.18	0.01	0.06	0.00	0.00	22.3
18	188	-844	282	-27	0	106	1693	4.02	4.02	4.02	4.02	3	0.24	0.01	0.05	0.00	0.00	22.3
19	188	-521	411	106	0	-127	1720	4.02	4.02	4.02	4.02	3	0.24	0.01	0.07	0.00	0.00	22.3
20	188	-763	264	43	0	-16	1710	4.02	4.02	4.02	4.02	3	0.24	0.01	0.05	0.00	0.00	22.3
37	188	-914	232	-79	0	187	1612	4.02	4.02	4.02	4.02	3	0.23	0.01	0.04	0.00	0.00	22.3
38	188	-375	447	143	0	-202	1663	4.02	4.02	4.02	4.02	3	0.24	0.01	0.08	0.00	0.00	22.3
39	188	-779	202	37	0	-17	1641	4.02	4.02	4.02	4.02	3	0.23	0.01	0.04	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	225	-592	-482	15	0	-7	1573	4.02	4.02	4.02	4.02	3	0.22	0.01	0.08	0.00	0.00	22.3
2	225	-520	-401	-11	0	41	1204	4.02	4.02	4.02	4.02	2	0.18	0.01	0.07	0.00	0.00	22.3
3	225	-475	-368	-11	0	41	1214	4.02	4.02	4.02	4.02	2	0.18	0.01	0.06	0.00	0.00	22.3
4	225	-437	-375	35	0	-51	1207	4.02	4.02	4.02	4.02	2	0.18	0.01	0.07	0.00	0.00	22.3
5	225	-391	-342	35	0	-52	1217	4.02	4.02	4.02	4.02	2	0.18	0.01	0.06	0.00	0.00	22.3
6	225	-544	-431	5	0	9	1192	4.02	4.02	4.02	4.02	2	0.18	0.01	0.08	0.00	0.00	22.3
7	225	-392	-320	5	0	8	1227	4.02	4.02	4.02	4.02	2	0.18	0.01	0.06	0.00	0.00	22.3
8	225	-519	-423	19	0	-19	1194	4.02	4.02	4.02	4.02	2	0.18	0.01	0.07	0.00	0.00	22.3
9	225	-367	-313	18	0	-20	1231	4.02	4.02	4.02	4.02	2	0.18	0.01	0.06	0.00	0.00	22.3
10	225	-520	-401	-11	0	41	1204	4.02	4.02	4.02	4.02	2	0.18	0.01	0.07	0.00	0.00	22.3
11	225	-475	-368	-11	0	41	1214	4.02	4.02	4.02	4.02	2	0.18	0.01	0.06	0.00	0.00	22.3
12	225	-437	-375	35	0	-51	1207	4.02	4.02	4.02	4.02	2	0.18	0.01	0.07	0.00	0.00	22.3
13	225	-391	-342	35	0	-52	1217	4.02	4.02	4.02	4.02	2	0.18	0.01	0.06	0.00	0.00	22.3
14	225	-544	-431	5	0	9	1192	4.02	4.02	4.02	4.02	2	0.18	0.01	0.08	0.00	0.00	22.3
15	225	-392	-320	5	0	8	1227	4.02	4.02	4.02	4.02	2	0.18	0.01	0.06	0.00	0.00	22.3
16	225	-519	-423	19	0	-19	1194	4.02	4.02	4.02	4.02	2	0.18	0.01	0.07	0.00	0.00	22.3
17	225	-367	-313	18	0	-20	1231	4.02	4.02	4.02	4.02	2	0.18	0.01	0.06	0.00	0.00	22.3
18	225	-844	-627	-27	0	116	1693	4.02	4.02	4.02	4.02	3	0.24	0.02	0.11	0.00	0.00	22.3
19	225	-521	-498	106	0	-167	1720	4.02	4.02	4.02	4.02	3	0.24	0.01	0.09	0.00	0.00	22.3
20	225	-763	-646	43	0	-32	1710	4.02	4.02	4.02	4.02	3	0.24	0.02	0.11	0.00	0.00	22.3
37	225	-914	-636	-79	0	216	1612	4.02	4.02	4.02	4.02	3	0.23	0.02	0.11	0.00	0.00	22.3
38	225	-375	-422	143	0	-255	1663	4.02	4.02	4.02	4.02	3	0.24	0.01	0.07	0.00	0.00	22.3
39	225	-779	-667	37	0	-31	1641	4.02	4.02	4.02	4.02	3	0.23	0.02	0.12	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	262	-592	-1311	15	0	-13	1573	4.02	4.02	4.02	4.02	3	0.22	0.04	0.23	0.00	0.00	22.3
2	262	-520	-1038	-11	0	45	1204	4.02	4.02	4.02	4.02	2	0.18	0.03	0.18	0.00	0.00	22.3
3	262	-475	-1005	-11	0	45	1214	4.02	4.02	4.02	4.02	2	0.18	0.03	0.18	0.00	0.00	22.3

4	262	-437	-1012	35	0	-64	1207	4.02	4.02	4.02	4.02	2	0.18	0.03	0.18	0.00	0.00	22.3
5	262	-391	-979	35	0	-65	1217	4.02	4.02	4.02	4.02	2	0.18	0.03	0.17	0.00	0.00	22.3
6	262	-544	-1068	5	0	7	1192	4.02	4.02	4.02	4.02	2	0.18	0.03	0.19	0.00	0.00	22.3
7	262	-392	-957	5	0	6	1227	4.02	4.02	4.02	4.02	2	0.18	0.03	0.17	0.00	0.00	22.3
8	262	-519	-1060	19	0	-26	1194	4.02	4.02	4.02	4.02	2	0.18	0.03	0.19	0.00	0.00	22.3
9	262	-367	-950	18	0	-27	1231	4.02	4.02	4.02	4.02	2	0.18	0.03	0.17	0.00	0.00	22.3
10	262	-520	-1038	-11	0	45	1204	4.02	4.02	4.02	4.02	2	0.18	0.03	0.18	0.00	0.00	22.3
11	262	-475	-1005	-11	0	45	1214	4.02	4.02	4.02	4.02	2	0.18	0.03	0.18	0.00	0.00	22.3
12	262	-437	-1012	35	0	-64	1207	4.02	4.02	4.02	4.02	2	0.18	0.03	0.18	0.00	0.00	22.3
13	262	-391	-979	35	0	-65	1217	4.02	4.02	4.02	4.02	2	0.18	0.03	0.17	0.00	0.00	22.3
14	262	-544	-1068	5	0	7	1192	4.02	4.02	4.02	4.02	2	0.18	0.03	0.19	0.00	0.00	22.3
15	262	-392	-957	5	0	6	1227	4.02	4.02	4.02	4.02	2	0.18	0.03	0.17	0.00	0.00	22.3
16	262	-519	-1060	19	0	-26	1194	4.02	4.02	4.02	4.02	2	0.18	0.03	0.19	0.00	0.00	22.3
17	262	-367	-950	18	0	-27	1231	4.02	4.02	4.02	4.02	2	0.18	0.03	0.17	0.00	0.00	22.3
18	262	-844	-1536	-27	0	126	1693	4.02	4.02	4.02	4.02	3	0.24	0.04	0.27	0.00	0.00	22.3
19	262	-521	-1407	106	0	-206	1720	4.02	4.02	4.02	4.02	3	0.24	0.04	0.25	0.00	0.00	22.3
20	262	-763	-1555	43	0	-48	1710	4.02	4.02	4.02	4.02	3	0.24	0.04	0.27	0.00	0.00	22.3
37	262	-914	-1505	-79	0	246	1612	4.02	4.02	4.02	4.02	3	0.23	0.04	0.26	0.00	0.00	22.3
38	262	-375	-1291	143	0	-309	1663	4.02	4.02	4.02	4.02	3	0.24	0.04	0.23	0.00	0.00	22.3
39	262	-779	-1536	37	0	-45	1641	4.02	4.02	4.02	4.02	3	0.23	0.04	0.27	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	300	-592	-2140	15	0	-18	1573	4.02	4.02	4.02	4.02	3	0.22	0.06	0.38	0.00	0.00	22.3
2	300	-520	-1676	-11	0	49	1204	4.02	4.02	4.02	4.02	2	0.18	0.05	0.29	0.00	0.00	22.3
3	300	-475	-1643	-11	0	49	1214	4.02	4.02	4.02	4.02	2	0.18	0.05	0.29	0.00	0.00	22.3
4	300	-437	-1650	35	0	-77	1207	4.02	4.02	4.02	4.02	2	0.18	0.05	0.29	0.00	0.00	22.3
5	300	-391	-1617	35	0	-78	1217	4.02	4.02	4.02	4.02	2	0.18	0.05	0.29	0.00	0.00	22.3
6	300	-544	-1706	5	0	5	1192	4.02	4.02	4.02	4.02	2	0.18	0.05	0.30	0.00	0.00	22.3
7	300	-392	-1595	5	0	5	1227	4.02	4.02	4.02	4.02	2	0.18	0.05	0.28	0.00	0.00	22.3
8	300	-519	-1698	19	0	-33	1194	4.02	4.02	4.02	4.02	2	0.18	0.05	0.30	0.00	0.00	22.3
9	300	-367	-1588	18	0	-33	1231	4.02	4.02	4.02	4.02	2	0.18	0.05	0.28	0.00	0.00	22.3
10	300	-520	-1676	-11	0	49	1204	4.02	4.02	4.02	4.02	2	0.18	0.05	0.29	0.00	0.00	22.3
11	300	-475	-1643	-11	0	49	1214	4.02	4.02	4.02	4.02	2	0.18	0.05	0.29	0.00	0.00	22.3
12	300	-437	-1650	35	0	-77	1207	4.02	4.02	4.02	4.02	2	0.18	0.05	0.29	0.00	0.00	22.3
13	300	-391	-1617	35	0	-78	1217	4.02	4.02	4.02	4.02	2	0.18	0.05	0.29	0.00	0.00	22.3
14	300	-544	-1706	5	0	5	1192	4.02	4.02	4.02	4.02	2	0.18	0.05	0.30	0.00	0.00	22.3
15	300	-392	-1595	5	0	5	1227	4.02	4.02	4.02	4.02	2	0.18	0.05	0.28	0.00	0.00	22.3
16	300	-519	-1698	19	0	-33	1194	4.02	4.02	4.02	4.02	2	0.18	0.05	0.30	0.00	0.00	22.3
17	300	-367	-1588	18	0	-33	1231	4.02	4.02	4.02	4.02	2	0.18	0.05	0.28	0.00	0.00	22.3
18	300	-844	-2445	-27	0	136	1693	4.02	4.02	4.02	4.02	3	0.24	0.07	0.43	0.00	0.00	22.3
19	300	-521	-2316	106	0	-246	1720	4.02	4.02	4.02	4.02	3	0.24	0.07	0.41	0.00	0.00	22.3
20	300	-763	-2464	43	0	-64	1710	4.02	4.02	4.02	4.02	3	0.24	0.07	0.43	0.00	0.00	22.3
37	300	-914	-2374	-79	0	275	1609	4.02	4.02	4.02	4.02	3	0.22	0.07	0.41	0.00	0.00	22.3
38	300	-375	-2160	143	0	-362	1663	4.02	4.02	4.02	4.02	3	0.24	0.06	0.38	0.00	0.00	22.3
39	300	-779	-2405	37	0	-59	1619	4.02	4.02	4.02	4.02	3	0.23	0.07	0.42	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	338	-592	-2969	15	0	-24	-1663	4.02	4.02	4.02	4.02	3	0.23	0.09	0.52	0.00	0.00	22.3
2	338	-520	-2313	-11	0	54	-1341	4.02	4.02	4.02	4.02	2	0.20	0.07	0.41	0.00	0.00	22.3
3	338	-475	-2280	-11	0	53	-1269	4.02	4.02	4.02	4.02	2	0.19	0.07	0.40	0.00	0.00	22.3
4	338	-437	-2287	35	0	-90	-1289	4.02	4.02	4.02	4.02	2	0.19	0.07	0.40	0.00	0.00	22.3
5	338	-391	-2254	35	0	-91	-1217	4.02	4.02	4.02	4.02	2	0.18	0.07	0.40	0.00	0.00	22.3
6	338	-544	-2343	5	0	3	-1408	4.02	4.02	4.02	4.02	2	0.21	0.07	0.41	0.00	0.00	22.3
7	338	-392	-2232	5	0	3	-1166	4.02	4.02	4.02	4.02	2	0.17	0.06	0.39	0.00	0.00	22.3
8	338	-519	-2335	19	0	-40	-1392	4.02	4.02	4.02	4.02	2	0.21	0.07	0.41	0.00	0.00	22.3
9	338	-367	-2225	18	0	-40	-1150	4.02	4.02	4.02	4.02	2	0.17	0.06	0.39	0.00	0.00	22.3
10	338	-520	-2313	-11	0	54	-1341	4.02	4.02	4.02	4.02	2	0.20	0.07	0.41	0.00	0.00	22.3
11	338	-475	-2280	-11	0	53	-1269	4.02	4.02	4.02	4.02	2	0.19	0.07	0.40	0.00	0.00	22.3
12	338	-437	-2287	35	0	-90	-1289	4.02	4.02	4.02	4.02	2	0.19	0.07	0.40	0.00	0.00	22.3
13	338	-391	-2254	35	0	-91	-1217	4.02	4.02	4.02	4.02	2	0.18	0.07	0.40	0.00	0.00	22.3
14	338	-544	-2343	5	0	3	-1408	4.02	4.02	4.02	4.02	2	0.21	0.07	0.41	0.00	0.00	22.3
15	338	-392	-2232	5	0	3	-1166	4.02	4.02	4.02	4.02	2	0.17	0.06	0.39	0.00	0.00	22.3
16	338	-519	-2335	19	0	-40	-1392	4.02	4.02	4.02	4.02	2	0.21	0.07	0.41	0.00	0.00	22.3
17	338	-367	-2225	18	0	-40	-1150	4.02	4.02	4.02	4.02	2	0.17	0.06	0.39	0.00	0.00	22.3
18	338	-844	-3354	-27	0	146	-2040	4.02	4.02	4.02	4.02	3	0.29	0.10	0.59	0.00	0.00	22.3
19	338	-521	-3225	106	0	-286	-1771	4.02	4.02	4.02	4.02	3	0.25	0.09	0.57	0.00	0.00	22.3
20	338	-763	-3373	43	0	-80	-2057	4.02	4.02	4.02	4.02	3	0.29	0.10	0.59	0.00	0.00	22.3
37	338	-914	-3243	-79	0	305	-2025	4.02	4.02	4.02	4.02	3	0.28	0.09	0.57	0.00	0.00	22.3
38	338	-375	-3029	143	0	-416	-1576	4.02	4.02	4.02	4.02	3	0.22	0.09	0.53	0.00	0.00	22.3
39	338	-779	-3274	37	0	-73	-2054	4.02	4.02	4.02	4.02	3	0.29	0.09	0.57	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	375	-592	-3798	15	0	-30	-1663	4.02	4.02	4.02	4.02	3	0.23	0.11	0.67	0.00	0.00	22.3
2	375	-520	-2951	-11	0	58	-1341	4.02	4.02	4.02	4.02	2	0.20	0.09	0.52	0.00	0.00	22.3
3	375	-475	-2918	-11	0	58	-1269	4.02	4.02	4.02	4.02	2	0.19	0.08	0.51	0.00	0.00	22.3
4	375	-437	-2925	35	0	-103	-1289	4.02	4.02	4.02	4.02	2	0.19	0.08	0.52	0.00	0.00	22.3
5	375	-391	-2892	35	0	-104	-1217	4.02	4.02	4.02	4.02	2	0.18	0.08	0.51	0.00	0.00	22.3
6	375	-544	-2981	5	0	1	-1408	4.02	4.02	4.02	4.02	2	0.21	0.09	0.52	0.00	0.00	22.3
7	375	-392	-2870	5	0	1	-1166	4.02	4.02	4.02	4.02	2	0.17	0.08	0.51	0.00	0.00	22.3
8	375	-519	-2973	19	0	-47	-1392	4.02	4.02	4.02	4.02	2	0.21	0.09	0.52	0.00	0.00	22.3
9	375	-367	-2863	18	0	-47	-1150	4.02	4.02	4.02	4.02	2	0.17	0.08	0.51	0.00	0.00	22.3
10	375	-520	-2951	-11	0	58	-1341	4.02	4.02	4.02	4.02	2	0.20	0.09	0.52	0.00	0.00	22.3
11	375	-475	-2918	-11	0	58	-1269	4.02	4.02	4.02	4.02	2	0.19	0.08	0.51	0.00	0.00	22.3
12	375	-437	-2925	35	0	-103	-1289	4.02	4.02	4.02	4.02	2	0.19	0.08	0.52	0.00	0.00	22.3
13	375	-391	-2892	35	0	-104	-1217	4.02	4.02	4.02	4.02	2	0.18	0.08	0.51	0.00	0.00	22.3
14	375	-544	-2981	5	0	1	-1408	4.02	4.02	4.02	4.02	2	0.21	0.09	0.52	0.00	0.00	22.3
15	375	-392	-2870	5	0	1	-1166	4.02	4.02	4.02	4.02	2	0.17	0.08	0.51	0.00	0.00	22.3
16	375	-519	-2973	19	0	-47	-1392	4.02	4.02	4.02	4.02	2	0.21	0.09	0.52	0.00	0.00	22.3
17	375	-367	-2863	18	0	-47	-1150	4.02	4.02	4.02	4.02	2	0.17	0.08	0.51	0.00	0.00	22.3
18	375	-844	-4263	-27	0	156	-2040	4.02	4.02	4.02	4.02	3	0.29	0.12	0.74	0.00	0.00	22.3
19	375	-521	-4134	106	0	-326	-1771	4.02	4.02	4.02	4.02	3	0.25	0.12	0.73	0.00	0.00	22.3
20	375	-763	-4282	43	0	-96	-2057	4.02	4.02	4.02	4.02	3	0.29	0.12	0.75	0.00	0.00	22.3
37	375	-914	-4112	-79	0	334	-2025	4.02	4.02	4.02	4.02	3	0.28	0.12	0.72	0.00	0.00	22.3
38	375	-375	-3898	143	0	-469	-1576	4.02	4.02	4.02	4.02	3	0.22	0.11	0.69	0.00	0.00	22.3
39	375	-779	-4143	37	0	-87	-2054	4.02	4.02	4.02	4.02	3	0.29	0.12	0.72	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

Nome travata: **trave_505_IP1** Descrizione: **Trave_5 16-15-14-13**
ASTA NUM. 13 NI 171 NF 296 SEZ. Rp B= 0.400 H= 0.500 (trave)

categoria: p.p. y Permanente Neve qy tot.
qy medio: 500.00 2627.25 282.50 3409.75 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

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NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-652	5965	-463	0	-672	-2098	4.02	4.02	4.02	4.02	3	0.29	0.13	0.80	0.00	0.00	16.8
2	0	-486	4514	-89	0	-179	-1551	4.02	4.02	4.02	4.02	2	0.23	0.10	0.61	0.00	0.00	16.8
3	0	-520	4636	-95	0	-187	-1644	4.02	4.02	4.02	4.02	2	0.24	0.10	0.62	0.00	0.00	16.8
4	0	-483	4540	-617	0	-847	-1583	4.02	4.02	4.02	4.02	2	0.23	0.10	0.61	0.00	0.00	16.8
5	0	-517	4662	-623	0	-855	-1676	4.02	4.02	4.02	4.02	2	0.25	0.10	0.63	0.00	0.00	16.8
6	0	-445	4381	-266	0	-403	-1454	4.02	4.02	4.02	4.02	2	0.22	0.10	0.59	0.00	0.00	16.8
7	0	-559	4788	-287	0	-431	-1763	4.02	4.02	4.02	4.02	2	0.26	0.10	0.64	0.00	0.00	16.8
8	0	-445	4389	-425	0	-603	-1464	4.02	4.02	4.02	4.02	2	0.22	0.10	0.59	0.00	0.00	16.8
9	0	-558	4795	-446	0	-631	-1773	4.02	4.02	4.02	4.02	2	0.26	0.10	0.64	0.00	0.00	16.8
10	0	-486	4514	-89	0	-179	-1551	4.02	4.02	4.02	4.02	2	0.23	0.10	0.61	0.00	0.00	16.8
11	0	-520	4636	-95	0	-187	-1644	4.02	4.02	4.02	4.02	2	0.24	0.10	0.62	0.00	0.00	16.8
12	0	-483	4540	-617	0	-847	-1583	4.02	4.02	4.02	4.02	2	0.23	0.10	0.61	0.00	0.00	16.8
13	0	-517	4662	-623	0	-855	-1676	4.02	4.02	4.02	4.02	2	0.25	0.10	0.63	0.00	0.00	16.8
14	0	-445	4381	-266	0	-403	-1454	4.02	4.02	4.02	4.02	2	0.22	0.10	0.59	0.00	0.00	16.8
15	0	-559	4788	-287	0	-431	-1763	4.02	4.02	4.02	4.02	2	0.26	0.10	0.64	0.00	0.00	16.8
16	0	-445	4389	-425	0	-603	-1464	4.02	4.02	4.02	4.02	2	0.22	0.10	0.59	0.00	0.00	16.8
17	0	-558	4795	-446	0	-631	-1773	4.02	4.02	4.02	4.02	2	0.26	0.10	0.64	0.00	0.00	16.8
18	0	-635	6343	-252	0	-484	-2151	4.02	4.02	4.02	4.02	3	0.30	0.14	0.85	0.00	0.00	16.8
19	0	-630	6440	-1663	0	-2266	-2236	4.02	4.02	4.02	4.02	3	0.39	0.14	0.86	0.00	0.00	16.8
20	0	-524	6313	-887	0	-1273	-1995	4.02	4.02	4.02	4.02	3	0.28	0.14	0.85	0.00	0.00	16.8
37	0	-632	6069	380	0	340	-2061	4.02	4.02	4.02	4.02	3	0.28	0.13	0.81	0.00	0.00	16.8
38	0	-625	6230	-1971	0	-2630	-2202	4.02	4.02	4.02	4.02	3	0.46	0.14	0.84	0.00	0.00	16.8
39	0	-449	6018	-679	0	-975	-1801	4.02	4.02	4.02	4.02	3	0.25	0.13	0.81	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	31	-652	4705	-463	0	-529	-2098	4.02	4.02	4.02	4.02	3	0.29	0.10	0.63	0.00	0.00	16.8
2	31	-486	3545	-89	0	-151	-1551	4.02	4.02	4.02	4.02	2	0.23	0.08	0.48	0.00	0.00	16.8
3	31	-520	3667	-95	0	-158	-1644	4.02	4.02	4.02	4.02	2	0.24	0.08	0.49	0.00	0.00	16.8
4	31	-483	3571	-617	0	-655	-1583	4.02	4.02	4.02	4.02	2	0.23	0.08	0.48	0.00	0.00	16.8
5	31	-517	3693	-623	0	-662	-1676	4.02	4.02	4.02	4.02	2	0.25	0.08	0.50	0.00	0.00	16.8
6	31	-445	3412	-266	0	-320	-1454	4.02	4.02	4.02	4.02	2	0.22	0.07	0.46	0.00	0.00	16.8
7	31	-559	3818	-287	0	-342	-1763	4.02	4.02	4.02	4.02	2	0.26	0.08	0.51	0.00	0.00	16.8
8	31	-445	3419	-425	0	-472	-1464	4.02	4.02	4.02	4.02	2	0.22	0.07	0.46	0.00	0.00	16.8
9	31	-558	3826	-446	0	-493	-1773	4.02	4.02	4.02	4.02	2	0.26	0.08	0.51	0.00	0.00	16.8
10	31	-486	3545	-89	0	-151	-1551	4.02	4.02	4.02	4.02	2	0.23	0.08	0.48	0.00	0.00	16.8
11	31	-520	3667	-95	0	-158	-1644	4.02	4.02	4.02	4.02	2	0.24	0.08	0.49	0.00	0.00	16.8
12	31	-483	3571	-617	0	-655	-1583	4.02	4.02	4.02	4.02	2	0.23	0.08	0.48	0.00	0.00	16.8
13	31	-517	3693	-623	0	-662	-1676	4.02	4.02	4.02	4.02	2	0.25	0.08	0.50	0.00	0.00	16.8
14	31	-445	3412	-266	0	-320	-1454	4.02	4.02	4.02	4.02	2	0.22	0.07	0.46	0.00	0.00	16.8
15	31	-559	3818	-287	0	-342	-1763	4.02	4.02	4.02	4.02	2	0.26	0.08	0.51	0.00	0.00	16.8
16	31	-445	3419	-425	0	-472	-1464	4.02	4.02	4.02	4.02	2	0.22	0.07	0.46	0.00	0.00	16.8
17	31	-558	3826	-446	0	-493	-1773	4.02	4.02	4.02	4.02	2	0.26	0.08	0.51	0.00	0.00	16.8
18	31	-635	4951	-252	0	-406	-2151	4.02	4.02	4.02	4.02	3	0.30	0.11	0.66	0.00	0.00	16.8
19	31	-630	5048	-1663	0	-1750	-2236	4.02	4.02	4.02	4.02	3	0.31	0.11	0.68	0.00	0.00	16.8
20	31	-524	4921	-887	0	-998	-1995	4.02	4.02	4.02	4.02	3	0.28	0.11	0.66	0.00	0.00	16.8
37	31	-632	4743	380	0	222	-2061	4.02	4.02	4.02	4.02	3	0.28	0.10	0.64	0.00	0.00	16.8
38	31	-625	4904	-1971	0	-2019	-2202	4.02	4.02	4.02	4.02	3	0.35	0.11	0.66	0.00	0.00	16.8
39	31	-449	4692	-679	0	-764	-1801	4.02	4.02	4.02	4.02	3	0.25	0.10	0.63	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	62	-652	3444	-463	0	-385	2264	4.02	4.02	4.02	4.02	3	0.31	0.07	0.46	0.00	0.00	16.8
2	62	-486	2575	-89	0	-124	1689	4.02	4.02	4.02	4.02	2	0.25	0.06	0.35	0.00	0.00	16.8
3	62	-520	2697	-95	0	-128	1786	4.02	4.02	4.02	4.02	2	0.26	0.06	0.36	0.00	0.00	16.8
4	62	-483	2601	-617	0	-464	1698	4.02	4.02	4.02	4.02	2	0.25	0.06	0.35	0.00	0.00	16.8
5	62	-517	2723	-623	0	-469	1794	4.02	4.02	4.02	4.02	2	0.27	0.06	0.37	0.00	0.00	16.8
6	62	-445	2442	-266	0	-238	1580	4.02	4.02	4.02	4.02	2	0.23	0.05	0.33	0.00	0.00	16.8
7	62	-559	2849	-287	0	-252	1901	4.02	4.02	4.02	4.02	2	0.28	0.06	0.38	0.00	0.00	16.8
8	62	-445	2450	-425	0	-340	1582	4.02	4.02	4.02	4.02	2	0.23	0.05	0.33	0.00	0.00	16.8
9	62	-558	2856	-446	0	-355	1903	4.02	4.02	4.02	4.02	2	0.28	0.06	0.38	0.00	0.00	16.8
10	62	-486	2575	-89	0	-124	1689	4.02	4.02	4.02	4.02	2	0.25	0.06	0.35	0.00	0.00	16.8
11	62	-520	2697	-95	0	-128	1786	4.02	4.02	4.02	4.02	2	0.26	0.06	0.36	0.00	0.00	16.8
12	62	-483	2601	-617	0	-464	1698	4.02	4.02	4.02	4.02	2	0.25	0.06	0.35	0.00	0.00	16.8
13	62	-517	2723	-623	0	-469	1794	4.02	4.02	4.02	4.02	2	0.27	0.06	0.37	0.00	0.00	16.8
14	62	-445	2442	-266	0	-238	1580	4.02	4.02	4.02	4.02	2	0.23	0.05	0.33	0.00	0.00	16.8
15	62	-559	2849	-287	0	-252	1901	4.02	4.02	4.02	4.02	2	0.28	0.06	0.38	0.00	0.00	16.8
16	62	-445	2450	-425	0	-340	1582	4.02	4.02	4.02	4.02	2	0.23	0.05	0.33	0.00	0.00	16.8
17	62	-558	2856	-446	0	-355	1903	4.02	4.02	4.02	4.02	2	0.28	0.06	0.38	0.00	0.00	16.8
18	62	-635	3560	-252	0	-328	2288	4.02	4.02	4.02	4.02	3	0.32	0.08	0.48	0.00	0.00	16.8
19	62	-630	3657	-1663	0	-1235	2353	4.02	4.02	4.02	4.02	3	0.32	0.08	0.49	0.00	0.00	16.8
20	62	-524	3530	-887	0	-723	2397	4.02	4.02	4.02	4.02	3	0.33	0.08	0.47	0.00	0.00	16.8
37	62	-632	3417	380	0	104	2207	4.02	4.02	4.02	4.02	3	0.30	0.07	0.46	0.00	0.00	16.8
38	62	-625	3578	-1971	0	-1408	2316	4.02	4.02	4.02	4.02	3	0.32	0.08	0.48	0.00	0.00	16.8
39	62	-449	3366	-679	0	-554	2389	4.02	4.02	4.02	4.02	3	0.33	0.07	0.45	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	93	-652	2184	-463	0	-242	2264	4.02	4.02	4.02	4.02	3	0.31	0.05	0.29	0.00	0.00	16.8
2	93	-486	1606	-89	0	-96	1689	4.02	4.02	4.02	4.02	2	0.25	0.03	0.22	0.00	0.00	16.8
3	93	-520	1728	-95	0	-99	1786	4.02	4.02	4.02	4.02	2	0.26	0.04	0.23	0.00	0.00	16.8
4	93	-483	1632	-617	0	-273	1698	4.02	4.02	4.02	4.02	2	0.25	0.04	0.22	0.00	0.00	16.8
5	93	-517	1754	-623	0	-275	1794	4.02	4.02	4.02	4.02	2	0.27	0.04	0.24	0.00	0.00	16.8
6	93	-445	1473	-266	0	-155	1580	4.02	4.02	4.02	4.02	2	0.23	0.03	0.20	0.00	0.00	16.8
7	93	-559	1879	-287	0	-163	1901	4.02	4.02	4.02	4.02	2	0.28	0.04	0.25	0.00	0.00	16.8
8	93	-445	1480	-425	0	-208	1582	4.02	4.02	4.02	4.02	2	0.23	0.03	0.20	0.00	0.00	16.8
9	93	-558	1887	-446	0	-217	1903	4.02	4.02	4.02	4.02	2	0.28	0.04	0.25	0.00	0.00	16.8
10	93	-486	1606	-89	0	-96	1689	4.02	4.02	4.02	4.02	2	0.25	0.03	0.22	0.00	0.00	16.8
11	93	-520	1728	-95	0	-99	1786	4.02	4.02	4.02	4.02	2	0.26	0.04	0.23	0.00	0.00	16.8
12	93	-483	1632	-617	0	-273	1698	4.02	4.02	4.02	4.02	2	0.25	0.04	0.22	0.00	0.00	16.8
13	93	-517	1754	-623	0	-275	1794	4.02	4.02	4.02	4.02	2	0.27	0.04	0.24	0.00	0.00	16.8
14	93	-445	1473	-266	0	-155	1580	4.02	4.02	4.02	4.02	2	0.23	0.03	0.20	0.00	0.00	16.8
15	93	-559	1879	-287	0	-163	1901	4.02	4.02	4.02	4.02	2	0.28	0.04	0.25	0.00	0.00	16.8
16	93	-445	1480	-425	0	-208	1582	4.02	4.02	4.02	4.02	2	0.23	0.03	0.20	0.00	0.00	16.8
17	93	-558	1887	-446	0	-217	1903	4.02	4.02	4.02	4.02	2	0.28	0.04	0.25	0.00	0.00	16.8
18	93	-635	2168	-252	0	-250	2288	4.02	4.02	4.02	4.02	3	0.32	0.05	0.29	0.00	0.00	16.8
19	93	-630	2265	-1663	0	-720	2353	4.02	4.02	4.02	4.02	3	0.32	0.05	0.30	0.00	0.00	16.8
20	93	-524	2138	-887	0	-448	2397	4.02	4.02	4.02	4.02	3	0.33	0.05	0.29	0.00	0.00	16.8
37	93	-632	2091	380	0	-14	2207	4.02	4.02	4.02	4.02	3	0.30	0.05	0.28	0.00	0.00	16.8
38	93	-625	2252	-1971	0	-796	2316	4.02	4.02	4.02	4.02	3	0.32	0.05	0.30	0.00	0.00	16.8
39	93	-449	2040	-679	0	-343	2389	4.02	4.02	4.02	4.02	3	0.33	0.04	0.27	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	124	-652	924	-463	0	-98	2264	4.02	4.02	4.02	4.02	3	0.31	0.02	0.12	0.00	0.00	16.8

2	124	-486	636	-89	0	-69	1689	4.02	4.02	4.02	4.02	2	0.25	0.01	0.09	0.00	0.00	16.8
3	124	-520	758	-95	0	-69	1786	4.02	4.02	4.02	4.02	2	0.26	0.02	0.10	0.00	0.00	16.8
4	124	-483	662	-617	0	-82	1698	4.02	4.02	4.02	4.02	2	0.25	0.01	0.09	0.00	0.00	16.8
5	124	-517	784	-623	0	-82	1794	4.02	4.02	4.02	4.02	2	0.27	0.02	0.11	0.00	0.00	16.8
6	124	-445	503	-266	0	-73	1580	4.02	4.02	4.02	4.02	2	0.23	0.01	0.07	0.00	0.00	16.8
7	124	-559	910	-287	0	-74	1901	4.02	4.02	4.02	4.02	2	0.28	0.02	0.12	0.00	0.00	16.8
8	124	-445	511	-425	0	-77	1582	4.02	4.02	4.02	4.02	2	0.23	0.01	0.07	0.00	0.00	16.8
9	124	-558	917	-446	0	-78	1903	4.02	4.02	4.02	4.02	2	0.28	0.02	0.12	0.00	0.00	16.8
10	124	-486	636	-89	0	-69	1689	4.02	4.02	4.02	4.02	2	0.25	0.01	0.09	0.00	0.00	16.8
11	124	-520	758	-95	0	-69	1786	4.02	4.02	4.02	4.02	2	0.26	0.02	0.10	0.00	0.00	16.8
12	124	-483	662	-617	0	-82	1698	4.02	4.02	4.02	4.02	2	0.25	0.01	0.09	0.00	0.00	16.8
13	124	-517	784	-623	0	-82	1794	4.02	4.02	4.02	4.02	2	0.27	0.02	0.11	0.00	0.00	16.8
14	124	-445	503	-266	0	-73	1580	4.02	4.02	4.02	4.02	2	0.23	0.01	0.07	0.00	0.00	16.8
15	124	-559	910	-287	0	-74	1901	4.02	4.02	4.02	4.02	2	0.28	0.02	0.12	0.00	0.00	16.8
16	124	-445	511	-425	0	-77	1582	4.02	4.02	4.02	4.02	2	0.23	0.01	0.07	0.00	0.00	16.8
17	124	-558	917	-446	0	-78	1903	4.02	4.02	4.02	4.02	2	0.28	0.02	0.12	0.00	0.00	16.8
18	124	-635	777	-252	0	-172	2288	4.02	4.02	4.02	4.02	3	0.32	0.02	0.10	0.00	0.00	16.8
19	124	-630	873	-1663	0	-204	2353	4.02	4.02	4.02	4.02	3	0.32	0.04	0.21	0.00	0.00	16.8
20	124	-524	746	-887	0	-173	2397	4.02	4.02	4.02	4.02	3	0.33	0.02	0.11	0.00	0.00	16.8
37	124	-632	765	380	0	-132	2207	4.02	4.02	4.02	4.02	3	0.30	0.02	0.10	0.00	0.00	16.8
38	124	-625	926	-1971	0	-185	2316	4.02	4.02	4.02	4.02	3	0.32	0.04	0.25	0.00	0.00	16.8
39	124	-449	714	-679	0	-133	2389	4.02	4.02	4.02	4.02	3	0.33	0.02	0.10	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	155	-652	-336	-463	0	45	2264	4.02	4.02	4.02	4.02	3	0.31	0.01	0.06	0.00	0.00	16.8
2	155	-486	-333	-89	0	-41	1689	4.02	4.02	4.02	4.02	2	0.25	0.01	0.04	0.00	0.00	16.8
3	155	-520	-211	-95	0	-40	1786	4.02	4.02	4.02	4.02	2	0.26	0.00	0.03	0.00	0.00	16.8
4	155	-483	-307	-617	0	110	1698	4.02	4.02	4.02	4.02	2	0.25	0.01	0.08	0.00	0.00	16.8
5	155	-517	-185	-623	0	111	1794	4.02	4.02	4.02	4.02	2	0.27	0.01	0.08	0.00	0.00	16.8
6	155	-445	-466	-266	0	10	1580	4.02	4.02	4.02	4.02	2	0.23	0.01	0.06	0.00	0.00	16.8
7	155	-559	-60	-287	0	15	1901	4.02	4.02	4.02	4.02	2	0.28	0.01	0.04	0.00	0.00	16.8
8	155	-445	-458	-425	0	55	1582	4.02	4.02	4.02	4.02	2	0.23	0.01	0.06	0.00	0.00	16.8
9	155	-558	-52	-446	0	60	1903	4.02	4.02	4.02	4.02	2	0.28	0.01	0.06	0.00	0.00	16.8
10	155	-486	-333	-89	0	-41	1689	4.02	4.02	4.02	4.02	2	0.25	0.01	0.04	0.00	0.00	16.8
11	155	-520	-211	-95	0	-40	1786	4.02	4.02	4.02	4.02	2	0.26	0.00	0.03	0.00	0.00	16.8
12	155	-483	-307	-617	0	110	1698	4.02	4.02	4.02	4.02	2	0.25	0.01	0.08	0.00	0.00	16.8
13	155	-517	-185	-623	0	111	1794	4.02	4.02	4.02	4.02	2	0.27	0.01	0.08	0.00	0.00	16.8
14	155	-445	-466	-266	0	10	1580	4.02	4.02	4.02	4.02	2	0.23	0.01	0.06	0.00	0.00	16.8
15	155	-559	-60	-287	0	15	1901	4.02	4.02	4.02	4.02	2	0.28	0.01	0.04	0.00	0.00	16.8
16	155	-445	-458	-425	0	55	1582	4.02	4.02	4.02	4.02	2	0.23	0.01	0.06	0.00	0.00	16.8
17	155	-558	-52	-446	0	60	1903	4.02	4.02	4.02	4.02	2	0.28	0.01	0.06	0.00	0.00	16.8
18	155	-635	-615	-252	0	-94	2288	4.02	4.02	4.02	4.02	3	0.32	0.01	0.08	0.00	0.00	16.8
19	155	-630	-519	-1663	0	311	2353	4.02	4.02	4.02	4.02	3	0.32	0.04	0.21	0.00	0.00	16.8
20	155	-524	-646	-887	0	102	2397	4.02	4.02	4.02	4.02	3	0.33	0.02	0.11	0.00	0.00	16.8
37	155	-632	-561	380	0	-250	2207	4.02	4.02	4.02	4.02	3	0.30	0.01	0.08	0.00	0.00	16.8
38	155	-625	-400	-1971	0	426	2316	4.02	4.02	4.02	4.02	3	0.32	0.04	0.25	0.00	0.00	16.8
39	155	-449	-612	-679	0	78	2389	4.02	4.02	4.02	4.02	3	0.33	0.02	0.09	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	186	-652	-1597	-463	0	189	2264	4.02	4.02	4.02	4.02	3	0.31	0.03	0.21	0.00	0.00	16.8
2	186	-486	-1302	-89	0	-14	1689	4.02	4.02	4.02	4.02	2	0.25	0.03	0.18	0.00	0.00	16.8
3	186	-520	-1180	-95	0	-10	1786	4.02	4.02	4.02	4.02	2	0.26	0.03	0.16	0.00	0.00	16.8
4	186	-483	-1276	-617	0	301	1698	4.02	4.02	4.02	4.02	2	0.25	0.03	0.17	0.00	0.00	16.8
5	186	-517	-1154	-623	0	304	1794	4.02	4.02	4.02	4.02	2	0.27	0.03	0.16	0.00	0.00	16.8
6	186	-445	-1435	-266	0	92	1580	4.02	4.02	4.02	4.02	2	0.23	0.03	0.19	0.00	0.00	16.8
7	186	-559	-1029	-287	0	104	1901	4.02	4.02	4.02	4.02	2	0.28	0.02	0.14	0.00	0.00	16.8
8	186	-445	-1428	-425	0	187	1582	4.02	4.02	4.02	4.02	2	0.23	0.03	0.19	0.00	0.00	16.8
9	186	-558	-1021	-446	0	198	1903	4.02	4.02	4.02	4.02	2	0.28	0.02	0.14	0.00	0.00	16.8
10	186	-486	-1302	-89	0	-14	1689	4.02	4.02	4.02	4.02	2	0.25	0.03	0.18	0.00	0.00	16.8
11	186	-520	-1180	-95	0	-10	1786	4.02	4.02	4.02	4.02	2	0.26	0.03	0.16	0.00	0.00	16.8
12	186	-483	-1276	-617	0	301	1698	4.02	4.02	4.02	4.02	2	0.25	0.03	0.17	0.00	0.00	16.8
13	186	-517	-1154	-623	0	304	1794	4.02	4.02	4.02	4.02	2	0.27	0.03	0.16	0.00	0.00	16.8
14	186	-445	-1435	-266	0	92	1580	4.02	4.02	4.02	4.02	2	0.23	0.03	0.19	0.00	0.00	16.8
15	186	-559	-1029	-287	0	104	1901	4.02	4.02	4.02	4.02	2	0.28	0.02	0.14	0.00	0.00	16.8
16	186	-445	-1428	-425	0	187	1582	4.02	4.02	4.02	4.02	2	0.23	0.03	0.19	0.00	0.00	16.8
17	186	-558	-1021	-446	0	198	1903	4.02	4.02	4.02	4.02	2	0.28	0.02	0.14	0.00	0.00	16.8
18	186	-635	-2007	-252	0	-16	2288	4.02	4.02	4.02	4.02	3	0.32	0.04	0.27	0.00	0.00	16.8
19	186	-630	-1910	-1663	0	827	2353	4.02	4.02	4.02	4.02	3	0.32	0.04	0.26	0.00	0.00	16.8
20	186	-524	-2037	-887	0	378	2397	4.02	4.02	4.02	4.02	3	0.33	0.04	0.27	0.00	0.00	16.8
37	186	-632	-1887	380	0	-368	2207	4.02	4.02	4.02	4.02	3	0.30	0.04	0.25	0.00	0.00	16.8
38	186	-625	-1726	-1971	0	1037	2316	4.02	4.02	4.02	4.02	3	0.32	0.04	0.25	0.00	0.00	16.8
39	186	-449	-1937	-679	0	289	2389	4.02	4.02	4.02	4.02	3	0.33	0.04	0.26	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	217	-652	-2857	-463	0	332	2264	4.02	4.02	4.02	4.02	3	0.31	0.06	0.38	0.00	0.00	16.8
2	217	-486	-2272	-89	0	14	1689	4.02	4.02	4.02	4.02	2	0.25	0.05	0.31	0.00	0.00	16.8
3	217	-520	-2150	-95	0	19	1786	4.02	4.02	4.02	4.02	2	0.26	0.05	0.29	0.00	0.00	16.8
4	217	-483	-2246	-617	0	492	1698	4.02	4.02	4.02	4.02	2	0.25	0.05	0.30	0.00	0.00	16.8
5	217	-517	-2124	-623	0	497	1794	4.02	4.02	4.02	4.02	2	0.27	0.05	0.29	0.00	0.00	16.8
6	217	-445	-2405	-266	0	175	1580	4.02	4.02	4.02	4.02	2	0.23	0.05	0.32	0.00	0.00	16.8
7	217	-559	-1998	-287	0	193	1901	4.02	4.02	4.02	4.02	2	0.28	0.04	0.27	0.00	0.00	16.8
8	217	-445	-2398	-425	0	318	1582	4.02	4.02	4.02	4.02	2	0.23	0.05	0.32	0.00	0.00	16.8
9	217	-558	-1991	-446	0	336	1903	4.02	4.02	4.02	4.02	2	0.28	0.04	0.27	0.00	0.00	16.8
10	217	-486	-2272	-89	0	14	1689	4.02	4.02	4.02	4.02	2	0.25	0.05	0.31	0.00	0.00	16.8
11	217	-520	-2150	-95	0	19	1786	4.02	4.02	4.02	4.02	2	0.26	0.05	0.29	0.00	0.00	16.8
12	217	-483	-2246	-617	0	492	1698	4.02	4.02	4.02	4.02	2	0.25	0.05	0.30	0.00	0.00	16.8
13	217	-517	-2124	-623	0	497	1794	4.02	4.02	4.02	4.02	2	0.27	0.05	0.29	0.00	0.00	16.8
14	217	-445	-2405	-266	0	175	1580	4.02	4.02	4.02	4.02	2	0.23	0.05	0.32	0.00	0.00	16.8
15	217	-559	-1998	-287	0	193	1901	4.02	4.02	4.02	4.02	2	0.28	0.04	0.27	0.00	0.00	16.8
16	217	-445	-2398	-425	0	318	1582	4.02	4.02	4.02	4.02	2	0.23	0.05	0.32	0.00	0.00	16.8
17	217	-558	-1991	-446	0	336	1903	4.02	4.02	4.02	4.02	2	0.28	0.04	0.27	0.00	0.00	16.8
18	217	-635	-3398	-252	0	62	2288	4.02	4.02	4.02	4.02	3	0.32	0.07	0.46	0.00	0.00	16.8
19	217	-630	-3302	-1663	0	1342	2353	4.02	4.02	4.02	4.02	3	0.32	0.07	0.44	0.00	0.00	16.8
20	217	-524	-3429	-887	0	653	2397	4.02	4.02	4.02	4.02	3	0.33	0.07	0.46	0.00	0.00	16.8
37	217	-632	-3213	380	0	-486	2207	4.02	4.02	4.02	4.02	3	0.30	0.07	0.43	0.00	0.00	16.8
38	217	-625	-3052	-1971	0	1648	2316	4.02	4.02	4.02	4.02	3	0.32	0.07	0.41	0.00	0.00	16.8
39	217	-449	-3263	-679	0	499	2389	4.02	4.02	4.02	4.02	3	0.33	0.07	0.44	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	248	-652	-4117	-463	0	476	2264	4.02	4.02	4.02	4.02	3	0.31	0.09	0.55	0.00	0.00	16.8
2	248	-486	-3241	-89	0	41	1668	4.02	4.02	4.02	4.02	2	0.25	0.07	0.44	0.00	0.00	16.8
3	248	-520	-3119	-95	0	49	1786	4.02	4.02	4.02	4.02	2	0.26	0.07	0.42	0.00	0.00	16.8
4	248	-483	-3215	-617	0	683	1687	4.02	4.02	4.02	4.02	2	0.25	0.07	0.43	0.00	0.00	16.8
5	248	-517	-3093	-623	0	691	1794	4.02	4.02	4.02	4.02	2	0.27	0.07	0.42	0.00	0.00	16.8
6	248	-445	-3374	-266	0	258	-1915	4.02	4.02	4.02	4.02	2	0.28	0.07	0.45	0.00	0.00	16.8
7	248	-559	-2968	-287	0	282	1901	4.02	4.02	4.02	4.02	2	0.28	0.06	0.40	0.00	0.00	16.8

8	248	-445	-3367	-425	0	450	-1901	4.02	4.02	4.02	4.02	2	0.28	0.07	0.45	0.00	0.00	16.8
9	248	-558	-2960	-446	0	474	1903	4.02	4.02	4.02	4.02	2	0.28	0.06	0.40	0.00	0.00	16.8
10	248	-486	-3241	-89	0	41	1668	4.02	4.02	4.02	4.02	2	0.25	0.07	0.44	0.00	0.00	16.8
11	248	-520	-3119	-95	0	49	1786	4.02	4.02	4.02	4.02	2	0.26	0.07	0.42	0.00	0.00	16.8
12	248	-483	-3215	-617	0	683	1687	4.02	4.02	4.02	4.02	2	0.25	0.07	0.43	0.00	0.00	16.8
13	248	-517	-3093	-623	0	691	1794	4.02	4.02	4.02	4.02	2	0.27	0.07	0.42	0.00	0.00	16.8
14	248	-445	-3374	-266	0	258	-1915	4.02	4.02	4.02	4.02	2	0.28	0.07	0.45	0.00	0.00	16.8
15	248	-559	-2968	-287	0	282	1901	4.02	4.02	4.02	4.02	2	0.28	0.06	0.40	0.00	0.00	16.8
16	248	-445	-3367	-425	0	450	-1901	4.02	4.02	4.02	4.02	2	0.28	0.07	0.45	0.00	0.00	16.8
17	248	-558	-2960	-446	0	474	1903	4.02	4.02	4.02	4.02	2	0.28	0.06	0.40	0.00	0.00	16.8
18	248	-635	-4790	-252	0	140	-2650	4.02	4.02	4.02	4.02	3	0.37	0.10	0.64	0.00	0.00	16.8
19	248	-630	-4694	-1663	0	1858	-2446	4.02	4.02	4.02	4.02	3	0.34	0.10	0.63	0.00	0.00	16.8
20	248	-524	-4821	-887	0	928	-2585	4.02	4.02	4.02	4.02	3	0.36	0.10	0.65	0.00	0.00	16.8
37	248	-632	-4539	380	0	-603	-2462	4.02	4.02	4.02	4.02	3	0.34	0.10	0.61	0.00	0.00	16.8
38	248	-625	-4378	-1971	0	2260	2310	4.02	4.02	4.02	4.02	3	0.39	0.10	0.59	0.00	0.00	16.8
39	248	-449	-4589	-679	0	710	-2353	4.02	4.02	4.02	4.02	3	0.33	0.10	0.62	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	279	-652	-5378	-463	0	619	-3142	4.02	4.02	4.02	4.02	3	0.43	0.12	0.72	0.00	0.00	16.8
2	279	-486	-4211	-89	0	69	-2584	4.02	4.02	4.02	4.02	2	0.38	0.09	0.57	0.00	0.00	16.8
3	279	-520	-4089	-95	0	78	-2298	4.02	4.02	4.02	4.02	2	0.34	0.09	0.55	0.00	0.00	16.8
4	279	-483	-4185	-617	0	875	-2535	4.02	4.02	4.02	4.02	2	0.38	0.09	0.56	0.00	0.00	16.8
5	279	-517	-4063	-623	0	884	-2250	4.02	4.02	4.02	4.02	2	0.33	0.09	0.55	0.00	0.00	16.8
6	279	-445	-4344	-266	0	340	-2900	4.02	4.02	4.02	4.02	2	0.43	0.09	0.58	0.00	0.00	16.8
7	279	-559	-3938	-287	0	371	-1948	4.02	4.02	4.02	4.02	2	0.29	0.09	0.53	0.00	0.00	16.8
8	279	-445	-4337	-425	0	582	-2885	4.02	4.02	4.02	4.02	2	0.43	0.09	0.58	0.00	0.00	16.8
9	279	-558	-3930	-446	0	612	-1934	4.02	4.02	4.02	4.02	2	0.29	0.09	0.53	0.00	0.00	16.8
10	279	-486	-4211	-89	0	69	-2584	4.02	4.02	4.02	4.02	2	0.38	0.09	0.57	0.00	0.00	16.8
11	279	-520	-4089	-95	0	78	-2298	4.02	4.02	4.02	4.02	2	0.34	0.09	0.55	0.00	0.00	16.8
12	279	-483	-4185	-617	0	875	-2535	4.02	4.02	4.02	4.02	2	0.38	0.09	0.56	0.00	0.00	16.8
13	279	-517	-4063	-623	0	884	-2250	4.02	4.02	4.02	4.02	2	0.33	0.09	0.55	0.00	0.00	16.8
14	279	-445	-4344	-266	0	340	-2900	4.02	4.02	4.02	4.02	2	0.43	0.09	0.58	0.00	0.00	16.8
15	279	-559	-3938	-287	0	371	-1948	4.02	4.02	4.02	4.02	2	0.29	0.09	0.53	0.00	0.00	16.8
16	279	-445	-4337	-425	0	582	-2885	4.02	4.02	4.02	4.02	2	0.43	0.09	0.58	0.00	0.00	16.8
17	279	-558	-3930	-446	0	612	-1934	4.02	4.02	4.02	4.02	2	0.29	0.09	0.53	0.00	0.00	16.8
18	279	-635	-6181	-252	0	218	-4058	4.02	4.02	4.02	4.02	3	0.56	0.13	0.83	0.00	0.00	16.8
19	279	-630	-6085	-1663	0	2374	-3843	4.02	4.02	4.02	4.02	3	0.53	0.13	0.82	0.00	0.00	16.8
20	279	-524	-6212	-887	0	1203	-3996	4.02	4.02	4.02	4.02	3	0.55	0.13	0.83	0.00	0.00	16.8
37	279	-632	-5865	380	0	-721	-3801	4.02	4.02	4.02	4.02	3	0.52	0.13	0.79	0.00	0.00	16.8
38	279	-625	-5704	-1971	0	2871	-3443	4.02	4.02	4.02	4.02	3	0.50	0.12	0.76	0.00	0.00	16.8
39	279	-449	-5915	-679	0	920	-3697	4.02	4.02	4.02	4.02	3	0.51	0.13	0.80	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	310	-652	-6638	-463	0	763	-3142	4.02	4.02	4.02	4.02	3	0.43	0.14	0.89	0.00	0.00	16.8
2	310	-486	-5180	-89	0	96	-2584	4.02	4.02	4.02	4.02	2	0.38	0.11	0.70	0.00	0.00	16.8
3	310	-520	-5058	-95	0	108	-2298	4.02	4.02	4.02	4.02	2	0.34	0.11	0.68	0.00	0.00	16.8
4	310	-483	-5154	-617	0	1066	-2535	4.02	4.02	4.02	4.02	2	0.38	0.11	0.69	0.00	0.00	16.8
5	310	-517	-5032	-623	0	1077	-2250	4.02	4.02	4.02	4.02	2	0.33	0.11	0.68	0.00	0.00	16.8
6	310	-445	-5313	-266	0	423	-2900	4.02	4.02	4.02	4.02	2	0.43	0.12	0.71	0.00	0.00	16.8
7	310	-559	-4907	-287	0	460	-1948	4.02	4.02	4.02	4.02	2	0.29	0.11	0.66	0.00	0.00	16.8
8	310	-445	-5306	-425	0	713	-2885	4.02	4.02	4.02	4.02	2	0.43	0.12	0.71	0.00	0.00	16.8
9	310	-558	-4899	-446	0	751	-1934	4.02	4.02	4.02	4.02	2	0.29	0.11	0.66	0.00	0.00	16.8
10	310	-486	-5180	-89	0	96	-2584	4.02	4.02	4.02	4.02	2	0.38	0.11	0.70	0.00	0.00	16.8
11	310	-520	-5058	-95	0	108	-2298	4.02	4.02	4.02	4.02	2	0.34	0.11	0.68	0.00	0.00	16.8
12	310	-483	-5154	-617	0	1066	-2535	4.02	4.02	4.02	4.02	2	0.38	0.11	0.69	0.00	0.00	16.8
13	310	-517	-5032	-623	0	1077	-2250	4.02	4.02	4.02	4.02	2	0.33	0.11	0.68	0.00	0.00	16.8
14	310	-445	-5313	-266	0	423	-2900	4.02	4.02	4.02	4.02	2	0.43	0.12	0.71	0.00	0.00	16.8
15	310	-559	-4907	-287	0	460	-1948	4.02	4.02	4.02	4.02	2	0.29	0.11	0.66	0.00	0.00	16.8
16	310	-445	-5306	-425	0	713	-2885	4.02	4.02	4.02	4.02	2	0.43	0.12	0.71	0.00	0.00	16.8
17	310	-558	-4899	-446	0	751	-1934	4.02	4.02	4.02	4.02	2	0.29	0.11	0.66	0.00	0.00	16.8
18	310	-635	-7573	-252	0	296	-4058	4.02	4.02	4.02	4.02	3	0.56	0.16	1.01	1.88	0.00	16.8
19	310	-630	-7477	-1663	0	2889	-3843	4.02	4.02	4.02	4.02	3	0.53	0.16	1.00	1.85	0.00	16.8
20	310	-524	-7604	-887	0	1478	-3996	4.02	4.02	4.02	4.02	3	0.55	0.17	1.02	1.89	0.00	16.8
37	310	-632	-7191	380	0	-839	-3801	4.02	4.02	4.02	4.02	3	0.52	0.16	0.96	0.00	0.00	16.8
38	310	-625	-7030	-1971	0	3482	-3443	4.02	4.02	4.02	4.02	3	0.60	0.15	0.94	0.00	0.00	16.8
39	310	-449	-7241	-679	0	1131	-3697	4.02	4.02	4.02	4.02	3	0.51	0.16	0.97	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

Nome travata: **trave_505_IP1** Descrizione: **Trave_5 16-15-14-13**
ASTA NUM. 14 NI 296 NF 125 SEZ. Rp B= 0.400 H= 0.500 (trave)

categoria: p.p. y Permanente Neve qy tot.
qy medio: 500.00 2627.25 282.50 3409.75 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-1601	7047	-3	0	90	-3392	4.02	4.02	4.02	4.02	3	0.45	0.15	0.93	0.00	0.00	16.8
2	0	-1287	5373	-139	0	-342	-2484	4.02	4.02	4.02	4.02	2	0.36	0.12	0.71	0.00	0.00	16.8
3	0	-1176	5484	-138	0	-340	-2766	4.02	4.02	4.02	4.02	2	0.40	0.12	0.73	0.00	0.00	16.8
4	0	-1288	5357	134	0	478	-2452	4.02	4.02	4.02	4.02	2	0.35	0.12	0.71	0.00	0.00	16.8
5	0	-1177	5469	135	0	481	-2733	4.02	4.02	4.02	4.02	2	0.40	0.12	0.73	0.00	0.00	16.8
6	0	-1418	5237	-45	0	-58	-2145	4.02	4.02	4.02	4.02	2	0.31	0.11	0.69	0.00	0.00	16.8
7	0	-1046	5609	-42	0	-49	-3083	4.02	4.02	4.02	4.02	2	0.45	0.12	0.75	0.00	0.00	16.8
8	0	-1418	5233	38	0	188	-2135	4.02	4.02	4.02	4.02	2	0.31	0.11	0.69	0.00	0.00	16.8
9	0	-1046	5604	40	0	197	-3073	4.02	4.02	4.02	4.02	2	0.45	0.12	0.75	0.00	0.00	16.8
10	0	-1287	5373	-139	0	-342	-2484	4.02	4.02	4.02	4.02	2	0.36	0.12	0.71	0.00	0.00	16.8
11	0	-1176	5484	-138	0	-340	-2766	4.02	4.02	4.02	4.02	2	0.40	0.12	0.73	0.00	0.00	16.8
12	0	-1288	5357	134	0	478	-2452	4.02	4.02	4.02	4.02	2	0.35	0.12	0.71	0.00	0.00	16.8
13	0	-1177	5469	135	0	481	-2733	4.02	4.02	4.02	4.02	2	0.40	0.12	0.73	0.00	0.00	16.8
14	0	-1418	5237	-45	0	-58	-2145	4.02	4.02	4.02	4.02	2	0.31	0.11	0.69	0.00	0.00	16.8
15	0	-1046	5609	-42	0	-49	-3083	4.02	4.02	4.02	4.02	2	0.45	0.12	0.75	0.00	0.00	16.8
16	0	-1418	5233	38	0	188	-2135	4.02	4.02	4.02	4.02	2	0.31	0.11	0.69	0.00	0.00	16.8
17	0	-1046	5604	40	0	197	-3073	4.02	4.02	4.02	4.02	2	0.45	0.12	0.75	0.00	0.00	16.8
18	0	-2249	7427	-386	0	-972	-2881	4.02	4.02	4.02	4.02	3	0.38	0.16	0.97	0.00	0.00	16.8
19	0	-2124	7501	459	0	1546	-3068	4.02	4.02	4.02	4.02	3	0.41	0.16	0.98	0.00	0.00	16.8
20	0	-2491	7448	28	0	248	-3019	4.02	4.02	4.02	4.02	3	0.40	0.16	0.97	0.00	0.00	16.8
37	0	-2082	7124	-680	0	-1874	-2863	4.02	4.02	4.02	4.02	3	0.38	0.15	0.93	0.00	0.00	16.8
38	0	-1875	7248	728	0	2321	-3173	4.02	4.02	4.02	4.02	3	0.42	0.16	0.95	0.00	0.00	16.8
39	0	-2486	7160	9	0	158	-3093	4.02	4.02	4.02	4.02	3	0.40	0.15	0.93	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	38	-1601	5522	-3	0	91	-3392	4.02	4.02	4.02	4.02	3	0.45	0.12	0.73	0.00	0.00	16.8
2	38	-1287	4200	-139	0	-290	-2484	4.02	4.02	4.02	4.02	2	0.36	0.09	0.56	0.00	0.00	16.8
3	38	-1176	4311	-138	0	-288	-2766	4.02	4.02	4.02	4.02	2	0.40	0.09	0.57	0.00	0.00	16.8
4	38	-1288	4184	134	0	428	-2452	4.02	4.02	4.02	4.02	2	0.35	0.09	0.55	0.00	0.00	16.8
5	38	-1177	4296	135	0	430	-2733	4.02	4.02	4.02	4.02	2	0.40	0.09	0.57	0.00	0.00	16.8
6	38	-1418	4064	-45	0	-42	-2145	4.02	4.02	4.02	4.02	2	0.31	0.09	0.54	0.00	0.00	16.8
7	38	-1046	4436	-42	0	-34	-3083	4.02	4.02	4.02	4.02	2	0.45	0.10	0.59	0.00	0.00	16.8
8	38	-1418	4060	38	0	174	-2135	4.02	4.02	4.02	4.02	2	0.31	0.09	0.54	0.00	0.00	16.8
9	38	-1046	4431	40	0	182	-3073	4.02	4.02	4.02	4.02	2	0.45	0.10	0.59	0.00	0.00	16.8
10	38	-1287	4200	-139	0	-290	-2484	4.02	4.02	4.02	4.02	2	0.36	0.09	0.56	0.00	0.00	16.8
11	38	-1176	4311	-138	0	-288	-2766	4.02	4.02	4.02	4.02	2	0.40	0.09	0.57	0.00	0.00	16.8
12	38	-1288	4184	134	0	428	-2452	4.02	4.02	4.02	4.02	2	0.35	0.09	0.55	0.00	0.00	16.8
13	38	-1177	4296	135	0	430	-2733	4.02	4.02	4.02	4.02	2	0.40	0.09	0.57	0.00	0.00	16.8
14	38	-1418	4064	-45	0	-42	-2145	4.02	4.02	4.02	4.02	2	0.31	0.09	0.54	0.00	0.00	16.8
15	38	-1046	4436	-42	0	-34	-3083	4.02	4.02	4.02	4.02	2	0.45	0.10	0.59	0.00	0.00	16.8
16	38	-1418	4060	38	0	174	-2135	4.02	4.02	4.02	4.02	2	0.31	0.09	0.54	0.00	0.00	16.8
17	38	-1046	4431	40	0	182	-3073	4.02	4.02	4.02	4.02	2	0.45	0.10	0.59	0.00	0.00	16.8
18	38	-2249	5744	-386	0	-827	-2881	4.02	4.02	4.02	4.02	3	0.38	0.12	0.75	0.00	0.00	16.8
19	38	-2124	5818	459	0	1374	-3068	4.02	4.02	4.02	4.02	3	0.41	0.13	0.76	0.00	0.00	16.8
20	38	-2491	5765	28	0	238	-3019	4.02	4.02	4.02	4.02	3	0.40	0.12	0.75	0.00	0.00	16.8
37	38	-2082	5520	-680	0	-1619	-2863	4.02	4.02	4.02	4.02	3	0.38	0.12	0.72	0.00	0.00	16.8
38	38	-1875	5644	728	0	2048	-3173	4.02	4.02	4.02	4.02	3	0.42	0.12	0.74	0.00	0.00	16.8
39	38	-2486	5556	9	0	155	-3093	4.02	4.02	4.02	4.02	3	0.40	0.12	0.72	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	75	-1601	3998	-3	0	92	2675	4.02	4.02	4.02	4.02	3	0.36	0.09	0.53	0.00	0.00	16.8
2	75	-1287	3028	-139	0	-238	2093	4.02	4.02	4.02	4.02	2	0.30	0.07	0.40	0.00	0.00	16.8
3	75	-1176	3139	-138	0	-236	2020	4.02	4.02	4.02	4.02	2	0.29	0.07	0.42	0.00	0.00	16.8
4	75	-1288	3012	134	0	377	2096	4.02	4.02	4.02	4.02	2	0.30	0.07	0.40	0.00	0.00	16.8
5	75	-1177	3124	135	0	379	2024	4.02	4.02	4.02	4.02	2	0.29	0.07	0.41	0.00	0.00	16.8
6	75	-1418	2892	-45	0	-25	2193	4.02	4.02	4.02	4.02	2	0.32	0.06	0.38	0.00	0.00	16.8
7	75	-1046	3264	-42	0	-18	1897	4.02	4.02	4.02	4.02	2	0.28	0.07	0.43	0.00	0.00	16.8
8	75	-1418	2887	38	0	160	2196	4.02	4.02	4.02	4.02	2	0.32	0.06	0.38	0.00	0.00	16.8
9	75	-1046	3259	40	0	167	1901	4.02	4.02	4.02	4.02	2	0.28	0.07	0.43	0.00	0.00	16.8
10	75	-1287	3028	-139	0	-238	2093	4.02	4.02	4.02	4.02	2	0.30	0.07	0.40	0.00	0.00	16.8
11	75	-1176	3139	-138	0	-236	2020	4.02	4.02	4.02	4.02	2	0.29	0.07	0.42	0.00	0.00	16.8
12	75	-1288	3012	134	0	377	2096	4.02	4.02	4.02	4.02	2	0.30	0.07	0.40	0.00	0.00	16.8
13	75	-1177	3124	135	0	379	2024	4.02	4.02	4.02	4.02	2	0.29	0.07	0.41	0.00	0.00	16.8
14	75	-1418	2892	-45	0	-25	2193	4.02	4.02	4.02	4.02	2	0.32	0.06	0.38	0.00	0.00	16.8
15	75	-1046	3264	-42	0	-18	1897	4.02	4.02	4.02	4.02	2	0.28	0.07	0.43	0.00	0.00	16.8
16	75	-1418	2887	38	0	160	2196	4.02	4.02	4.02	4.02	2	0.32	0.06	0.38	0.00	0.00	16.8
17	75	-1046	3259	40	0	167	1901	4.02	4.02	4.02	4.02	2	0.28	0.07	0.43	0.00	0.00	16.8
18	75	-2249	4060	-386	0	-682	3209	4.02	4.02	4.02	4.02	3	0.42	0.09	0.53	0.00	0.00	16.8
19	75	-2124	4134	459	0	1202	3133	4.02	4.02	4.02	4.02	3	0.41	0.09	0.54	0.00	0.00	16.8
20	75	-2491	4081	28	0	227	3103	4.02	4.02	4.02	4.02	3	0.41	0.09	0.53	0.00	0.00	16.8
37	75	-2082	3916	-680	0	-1364	3012	4.02	4.02	4.02	4.02	3	0.40	0.08	0.51	0.00	0.00	16.8
38	75	-1875	4040	728	0	1775	2898	4.02	4.02	4.02	4.02	3	0.39	0.09	0.53	0.00	0.00	16.8
39	75	-2486	3952	9	0	151	2836	4.02	4.02	4.02	4.02	3	0.37	0.09	0.51	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	112	-1601	2474	-3	0	93	2675	4.02	4.02	4.02	4.02	3	0.36	0.05	0.33	0.00	0.00	16.8
2	112	-1287	1855	-139	0	-186	2093	4.02	4.02	4.02	4.02	2	0.30	0.04	0.25	0.00	0.00	16.8
3	112	-1176	1966	-138	0	-184	2020	4.02	4.02	4.02	4.02	2	0.29	0.04	0.26	0.00	0.00	16.8
4	112	-1288	1839	134	0	327	2096	4.02	4.02	4.02	4.02	2	0.30	0.04	0.24	0.00	0.00	16.8
5	112	-1177	1951	135	0	329	2024	4.02	4.02	4.02	4.02	2	0.29	0.04	0.26	0.00	0.00	16.8
6	112	-1418	1719	-45	0	-8	2193	4.02	4.02	4.02	4.02	2	0.32	0.04	0.23	0.00	0.00	16.8
7	112	-1046	2091	-42	0	-2	1937	4.02	4.02	4.02	4.02	2	0.28	0.05	0.28	0.00	0.00	16.8
8	112	-1418	1715	38	0	146	2196	4.02	4.02	4.02	4.02	2	0.32	0.04	0.23	0.00	0.00	16.8
9	112	-1046	2086	40	0	151	1939	4.02	4.02	4.02	4.02	2	0.28	0.05	0.28	0.00	0.00	16.8
10	112	-1287	1855	-139	0	-186	2093	4.02	4.02	4.02	4.02	2	0.30	0.04	0.25	0.00	0.00	16.8
11	112	-1176	1966	-138	0	-184	2020	4.02	4.02	4.02	4.02	2	0.29	0.04	0.26	0.00	0.00	16.8
12	112	-1288	1839	134	0	327	2096	4.02	4.02	4.02	4.02	2	0.30	0.04	0.24	0.00	0.00	16.8
13	112	-1177	1951	135	0	329	2024	4.02	4.02	4.02	4.02	2	0.29	0.04	0.26	0.00	0.00	16.8
14	112	-1418	1719	-45	0	-8	2193	4.02	4.02	4.02	4.02	2	0.32	0.04	0.23	0.00	0.00	16.8
15	112	-1046	2091	-42	0	-2	1937	4.02	4.02	4.02	4.02	2	0.28	0.05	0.28	0.00	0.00	16.8
16	112	-1418	1715	38	0	146	2196	4.02	4.02	4.02	4.02	2	0.32	0.04	0.23	0.00	0.00	16.8
17	112	-1046	2086	40	0	151	1939	4.02	4.02	4.02	4.02	2	0.28	0.05	0.28	0.00	0.00	16.8
18	112	-2249	2377	-386	0	-537	3209	4.02	4.02	4.02	4.02	3	0.42	0.05	0.31	0.00	0.00	16.8
19	112	-2124	2451	459	0	1029	3133	4.02	4.02	4.02	4.02	3	0.41	0.05	0.32	0.00	0.00	16.8
20	112	-2491	2398	28	0	217	3103	4.02	4.02	4.02	4.02	3	0.41	0.05	0.31	0.00	0.00	16.8
37	112	-2082	2312	-680	0	-1109	3012	4.02	4.02	4.02	4.02	3	0.40	0.05	0.30	0.00	0.00	16.8
38	112	-1875	2436	728	0	1502	2898	4.02	4.02	4.02	4.02	3	0.39	0.05	0.32	0.00	0.00	16.8
39	112	-2486	2348	9	0	148	2836	4.02	4.02	4.02	4.02	3	0.37	0.05	0.30	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	150	-1601	949	-3	0	94	2675	4.02	4.02	4.02	4.02	3	0.36	0.02	0.12	0.00	0.00	16.8
2	150	-1287	682	-139	0	-133	2093	4.02	4.02	4.02	4.02	2	0.30	0.01	0.09	0.00	0.00	16.8
3	150	-1176	793	-138	0	-132	2020	4.02	4.02	4.02	4.02	2	0.29	0.02	0.11	0.00	0.00	16.8
4	150	-1288	666	134	0	277	2096	4.02	4.02	4.02	4.02	2	0.30	0.01	0.09	0.00	0.00	16.8
5	150	-1177	778	135	0	278	2024	4.02	4.02	4.02	4.02	2	0.29	0.02	0.10	0.00	0.00	16.8
6	150	-1418	546	-45	0	8	2193	4.02	4.02	4.02	4.02	2	0.32	0.01	0.07	0.00	0.00	16.8
7	150	-1046	918	-42	0	13	1937	4.02	4.02	4.02	4.02	2	0.28	0.02	0.12	0.00	0.00	16.8
8	150	-1418	542	38	0	131	2196	4.02	4.02	4.02	4.02	2	0.32	0.01	0.07	0.00	0.00	16.8
9	150	-1046	913	40	0	136	1939	4.02	4.02	4.02	4.02	2	0.28	0.02	0.12	0.00	0.00	16.8
10	150	-1287	682	-139	0	-133	2093	4.02	4.02	4.02	4.02	2	0.30	0.01	0.09	0.00	0.00	16.8
11	150	-1176	793	-138	0	-132	2020	4.02	4.02	4.02	4.02	2	0.29	0.02	0.11	0.00	0.00	16.8
12	150	-1288	666	134	0	277	2096	4.02	4.02	4.02	4.02	2	0.30	0.01	0.09	0.00	0.00	16.8
13	150	-1177	778	135	0	278	2024	4.02	4.02	4.02	4.02	2	0.29	0.02	0.10	0.00	0.00	16.8
14	150	-1418	546	-45	0	8	2193	4.02	4.02	4.02	4.02	2	0.32	0.01	0.07	0.00	0.00	16.8
15	150	-1046	918	-42	0	13	1937	4.02	4.02	4.02	4.02	2	0.28	0.02	0.12	0.00	0.00	16.8
16	150	-1418	542	38	0	131	2196	4.02	4.02	4.02	4.02	2	0.32	0.01	0.07	0.00	0.00	16.8
17	150	-1046	913	40	0	136	1939	4.02	4.02	4.02	4.02	2	0.28	0.02	0.12	0.00	0.00	16.8
18	150	-2249	693	-386	0	-393	3209	4.02	4.02	4.02	4.02	3	0.42	0.01	0.09	0.00	0.00	16.8
19	150	-2124	767	459	0	857	3133	4.02	4.02	4.02	4.02	3	0.41	0.02	0.10	0.00	0.00	16.8
20	150	-2491	714	28	0	206	3103	4.02	4.02	4.02	4.02	3	0.41	0.02	0.09	0.00	0.00	16.8
37	150	-2082	708	-680	0	-854	3012	4.02	4.02	4.02	4.02	3	0.40	0.02	0.09	0.00	0.00	16.8
38	150	-1875	832	728	0	1229	2898	4.02	4.02	4.02	4.02	3	0.39	0.02	0.11	0.00	0.00	16.8
39	150	-2486	744	9	0	144	2836	4.02	4.02	4.02	4.02	3	0.37	0.02	0.10	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	188	-1601	-576	-3	0	95	2675	4.02	4.02	4.02	4.02	3	0.36	0.01	0.08	0.00	0.00	16.8
2	188	-1287	-490	-139	0	-81	2093	4.02	4.02	4.02	4.02	2	0.30	0.01	0.06	0.00	0.00	16.8
3	188	-1176	-380	-138	0	-80	2020	4.02	4.02	4.02	4.02	2	0.29	0.01	0.05	0.00	0.00	16.8
4	188	-1288	-506	134	0	226	2096	4.02	4.02	4.02	4.02	2	0.30	0.01	0.07	0.00	0.00	16.8
5	188	-1177	-394	135	0	228	2024	4.02	4.02	4.02	4.02	2	0.29	0.01	0.05	0.00	0.00	16.8

6	188	-1418	-626	-45	0	25	2193	4.02	4.02	4.02	4.02	2	0.32	0.01	0.08	0.00	0.00	16.8
7	188	-1046	-254	-42	0	29	1937	4.02	4.02	4.02	4.02	2	0.28	0.01	0.03	0.00	0.00	16.8
8	188	-1418	-631	38	0	117	2196	4.02	4.02	4.02	4.02	2	0.32	0.01	0.08	0.00	0.00	16.8
9	188	-1046	-260	40	0	121	1939	4.02	4.02	4.02	4.02	2	0.28	0.01	0.03	0.00	0.00	16.8
10	188	-1287	-490	-139	0	-81	2093	4.02	4.02	4.02	4.02	2	0.30	0.01	0.06	0.00	0.00	16.8
11	188	-1176	-380	-138	0	-80	2020	4.02	4.02	4.02	4.02	2	0.29	0.01	0.05	0.00	0.00	16.8
12	188	-1288	-506	134	0	226	2096	4.02	4.02	4.02	4.02	2	0.30	0.01	0.07	0.00	0.00	16.8
13	188	-1177	-394	135	0	228	2024	4.02	4.02	4.02	4.02	2	0.29	0.01	0.05	0.00	0.00	16.8
14	188	-1418	-626	-45	0	25	2193	4.02	4.02	4.02	4.02	2	0.32	0.01	0.08	0.00	0.00	16.8
15	188	-1046	-254	-42	0	29	1937	4.02	4.02	4.02	4.02	2	0.28	0.01	0.03	0.00	0.00	16.8
16	188	-1418	-631	38	0	117	2196	4.02	4.02	4.02	4.02	2	0.32	0.01	0.08	0.00	0.00	16.8
17	188	-1046	-260	40	0	121	1939	4.02	4.02	4.02	4.02	2	0.28	0.01	0.03	0.00	0.00	16.8
18	188	-2249	-991	-386	0	-248	3209	4.02	4.02	4.02	4.02	3	0.42	0.02	0.13	0.00	0.00	16.8
19	188	-2124	-916	459	0	685	3133	4.02	4.02	4.02	4.02	3	0.41	0.02	0.12	0.00	0.00	16.8
20	188	-2491	-969	28	0	196	3103	4.02	4.02	4.02	4.02	3	0.41	0.02	0.13	0.00	0.00	16.8
37	188	-2082	-896	-680	0	-599	3012	4.02	4.02	4.02	4.02	3	0.40	0.02	0.12	0.00	0.00	16.8
38	188	-1875	-772	728	0	956	2898	4.02	4.02	4.02	4.02	3	0.39	0.02	0.10	0.00	0.00	16.8
39	188	-2486	-860	9	0	141	2836	4.02	4.02	4.02	4.02	3	0.37	0.02	0.11	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	225	-1601	-2100	-3	0	96	2675	4.02	4.02	4.02	4.02	3	0.36	0.05	0.28	0.00	0.00	16.8
2	225	-1287	-1663	-139	0	-29	2093	4.02	4.02	4.02	4.02	2	0.30	0.04	0.22	0.00	0.00	16.8
3	225	-1176	-1552	-138	0	-28	2020	4.02	4.02	4.02	4.02	2	0.29	0.03	0.21	0.00	0.00	16.8
4	225	-1288	-1679	134	0	176	2096	4.02	4.02	4.02	4.02	2	0.30	0.04	0.22	0.00	0.00	16.8
5	225	-1177	-1567	135	0	177	2024	4.02	4.02	4.02	4.02	2	0.29	0.03	0.21	0.00	0.00	16.8
6	225	-1418	-1799	-45	0	42	2193	4.02	4.02	4.02	4.02	2	0.32	0.04	0.24	0.00	0.00	16.8
7	225	-1046	-1427	-42	0	45	1937	4.02	4.02	4.02	4.02	2	0.28	0.03	0.19	0.00	0.00	16.8
8	225	-1418	-1804	38	0	103	2196	4.02	4.02	4.02	4.02	2	0.32	0.04	0.24	0.00	0.00	16.8
9	225	-1046	-1432	40	0	106	1939	4.02	4.02	4.02	4.02	2	0.28	0.03	0.19	0.00	0.00	16.8
10	225	-1287	-1663	-139	0	-29	2093	4.02	4.02	4.02	4.02	2	0.30	0.04	0.22	0.00	0.00	16.8
11	225	-1176	-1552	-138	0	-28	2020	4.02	4.02	4.02	4.02	2	0.29	0.03	0.21	0.00	0.00	16.8
12	225	-1288	-1679	134	0	176	2096	4.02	4.02	4.02	4.02	2	0.30	0.04	0.22	0.00	0.00	16.8
13	225	-1177	-1567	135	0	177	2024	4.02	4.02	4.02	4.02	2	0.29	0.03	0.21	0.00	0.00	16.8
14	225	-1418	-1799	-45	0	42	2193	4.02	4.02	4.02	4.02	2	0.32	0.04	0.24	0.00	0.00	16.8
15	225	-1046	-1427	-42	0	45	1937	4.02	4.02	4.02	4.02	2	0.28	0.03	0.19	0.00	0.00	16.8
16	225	-1418	-1804	38	0	103	2196	4.02	4.02	4.02	4.02	2	0.32	0.04	0.24	0.00	0.00	16.8
17	225	-1046	-1432	40	0	106	1939	4.02	4.02	4.02	4.02	2	0.28	0.03	0.19	0.00	0.00	16.8
18	225	-2249	-2674	-386	0	-103	3209	4.02	4.02	4.02	4.02	3	0.42	0.06	0.35	0.00	0.00	16.8
19	225	-2124	-2599	459	0	513	3133	4.02	4.02	4.02	4.02	3	0.41	0.06	0.34	0.00	0.00	16.8
20	225	-2491	-2652	28	0	185	3103	4.02	4.02	4.02	4.02	3	0.41	0.06	0.34	0.00	0.00	16.8
37	225	-2082	-2500	-680	0	-344	3012	4.02	4.02	4.02	4.02	3	0.40	0.05	0.33	0.00	0.00	16.8
38	225	-1875	-2376	728	0	683	2898	4.02	4.02	4.02	4.02	3	0.39	0.05	0.31	0.00	0.00	16.8
39	225	-2486	-2464	9	0	137	2836	4.02	4.02	4.02	4.02	3	0.37	0.05	0.32	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	262	-1601	-3625	-3	0	97	2675	4.02	4.02	4.02	4.02	3	0.36	0.08	0.48	0.00	0.00	16.8
2	262	-1287	-2836	-139	0	23	2093	4.02	4.02	4.02	4.02	2	0.30	0.06	0.38	0.00	0.00	16.8
3	262	-1176	-2725	-138	0	24	2020	4.02	4.02	4.02	4.02	2	0.29	0.06	0.36	0.00	0.00	16.8
4	262	-1288	-2852	134	0	126	2096	4.02	4.02	4.02	4.02	2	0.30	0.06	0.38	0.00	0.00	16.8
5	262	-1177	-2740	135	0	126	2024	4.02	4.02	4.02	4.02	2	0.29	0.06	0.36	0.00	0.00	16.8
6	262	-1418	-2972	-45	0	59	2193	4.02	4.02	4.02	4.02	2	0.32	0.06	0.39	0.00	0.00	16.8
7	262	-1046	-2600	-42	0	60	1937	4.02	4.02	4.02	4.02	2	0.28	0.06	0.35	0.00	0.00	16.8
8	262	-1418	-2977	38	0	89	2196	4.02	4.02	4.02	4.02	2	0.32	0.06	0.39	0.00	0.00	16.8
9	262	-1046	-2605	40	0	91	1939	4.02	4.02	4.02	4.02	2	0.28	0.06	0.35	0.00	0.00	16.8
10	262	-1287	-2836	-139	0	23	2093	4.02	4.02	4.02	4.02	2	0.30	0.06	0.38	0.00	0.00	16.8
11	262	-1176	-2725	-138	0	24	2020	4.02	4.02	4.02	4.02	2	0.29	0.06	0.36	0.00	0.00	16.8
12	262	-1288	-2852	134	0	126	2096	4.02	4.02	4.02	4.02	2	0.30	0.06	0.38	0.00	0.00	16.8
13	262	-1177	-2740	135	0	126	2024	4.02	4.02	4.02	4.02	2	0.29	0.06	0.36	0.00	0.00	16.8
14	262	-1418	-2972	-45	0	59	2193	4.02	4.02	4.02	4.02	2	0.32	0.06	0.39	0.00	0.00	16.8
15	262	-1046	-2600	-42	0	60	1937	4.02	4.02	4.02	4.02	2	0.28	0.06	0.35	0.00	0.00	16.8
16	262	-1418	-2977	38	0	89	2196	4.02	4.02	4.02	4.02	2	0.32	0.06	0.39	0.00	0.00	16.8
17	262	-1046	-2605	40	0	91	1939	4.02	4.02	4.02	4.02	2	0.28	0.06	0.35	0.00	0.00	16.8
18	262	-2249	-4358	-386	0	41	3209	4.02	4.02	4.02	4.02	3	0.42	0.09	0.57	0.00	0.00	16.8
19	262	-2124	-4283	459	0	340	3133	4.02	4.02	4.02	4.02	3	0.41	0.09	0.56	0.00	0.00	16.8
20	262	-2491	-4336	28	0	175	3103	4.02	4.02	4.02	4.02	3	0.41	0.09	0.56	0.00	0.00	16.8
37	262	-2082	-4104	-680	0	-89	3012	4.02	4.02	4.02	4.02	3	0.40	0.09	0.54	0.00	0.00	16.8
38	262	-1875	-3980	728	0	409	2898	4.02	4.02	4.02	4.02	3	0.39	0.09	0.52	0.00	0.00	16.8
39	262	-2486	-4068	9	0	134	2836	4.02	4.02	4.02	4.02	3	0.37	0.09	0.53	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	300	-1601	-5149	-3	0	98	-3151	4.02	4.02	4.02	4.02	3	0.42	0.11	0.68	0.00	0.00	16.8
2	300	-1287	-4009	-139	0	76	-2468	4.02	4.02	4.02	4.02	2	0.36	0.09	0.53	0.00	0.00	16.8
3	300	-1176	-3898	-138	0	76	-2359	4.02	4.02	4.02	4.02	2	0.34	0.08	0.52	0.00	0.00	16.8
4	300	-1288	-4025	134	0	75	-2490	4.02	4.02	4.02	4.02	2	0.36	0.09	0.53	0.00	0.00	16.8
5	300	-1177	-3913	135	0	76	-2380	4.02	4.02	4.02	4.02	2	0.34	0.08	0.52	0.00	0.00	16.8
6	300	-1418	-4145	-45	0	75	-2604	4.02	4.02	4.02	4.02	2	0.37	0.09	0.55	0.00	0.00	16.8
7	300	-1046	-3773	-42	0	76	-2238	4.02	4.02	4.02	4.02	2	0.33	0.08	0.50	0.00	0.00	16.8
8	300	-1418	-4149	38	0	75	-2610	4.02	4.02	4.02	4.02	2	0.38	0.09	0.55	0.00	0.00	16.8
9	300	-1046	-3778	40	0	76	-2244	4.02	4.02	4.02	4.02	2	0.33	0.08	0.50	0.00	0.00	16.8
10	300	-1287	-4009	-139	0	76	-2468	4.02	4.02	4.02	4.02	2	0.36	0.09	0.53	0.00	0.00	16.8
11	300	-1176	-3898	-138	0	76	-2359	4.02	4.02	4.02	4.02	2	0.34	0.08	0.52	0.00	0.00	16.8
12	300	-1288	-4025	134	0	75	-2490	4.02	4.02	4.02	4.02	2	0.36	0.09	0.53	0.00	0.00	16.8
13	300	-1177	-3913	135	0	76	-2380	4.02	4.02	4.02	4.02	2	0.34	0.08	0.52	0.00	0.00	16.8
14	300	-1418	-4145	-45	0	75	-2604	4.02	4.02	4.02	4.02	2	0.37	0.09	0.55	0.00	0.00	16.8
15	300	-1046	-3773	-42	0	76	-2238	4.02	4.02	4.02	4.02	2	0.33	0.08	0.50	0.00	0.00	16.8
16	300	-1418	-4149	38	0	75	-2610	4.02	4.02	4.02	4.02	2	0.38	0.09	0.55	0.00	0.00	16.8
17	300	-1046	-3778	40	0	76	-2244	4.02	4.02	4.02	4.02	2	0.33	0.08	0.50	0.00	0.00	16.8
18	300	-2249	-6041	-386	0	186	-3860	4.02	4.02	4.02	4.02	3	0.51	0.13	0.79	0.00	0.00	16.8
19	300	-2124	-5966	459	0	168	-3786	4.02	4.02	4.02	4.02	3	0.50	0.13	0.78	0.00	0.00	16.8
20	300	-2491	-6019	28	0	164	-3922	4.02	4.02	4.02	4.02	3	0.51	0.13	0.78	0.00	0.00	16.8
37	300	-2082	-5708	-680	0	166	-3627	4.02	4.02	4.02	4.02	3	0.48	0.12	0.75	0.00	0.00	16.8
38	300	-1875	-5584	728	0	136	-3504	4.02	4.02	4.02	4.02	3	0.47	0.12	0.73	0.00	0.00	16.8
39	300	-2486	-5672	9	0	131	-3731	4.02	4.02	4.02	4.02	3	0.49	0.12	0.74	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	338	-1601	-6674	-3	0	99	-5550	4.02	4.02	4.02	4.02	3	0.74	0.14	0.88	0.00	0.00	16.8
2	338	-1287	-5181	-139	0	128	-4325	4.02	4.02	4.02	4.02	2	0.62	0.11	0.69	0.00	0.00	16.8
3	338	-1176	-5070	-138	0	128	-4188	4.02	4.02	4.02	4.02	2	0.61	0.11	0.67	0.00	0.00	16.8
4	338	-1288	-5197	134	0	25	-4350	4.02	4.02	4.02	4.02	2	0.63	0.11	0.69	0.00	0.00	16.8
5	338	-1177	-5085	135	0	25	-4213	4.02	4.02	4.02	4.02	2	0.61	0.11	0.67	0.00	0.00	16.8
6	338	-1418	-5317	-45	0	92	-4494	4.02	4.02	4.02	4.02	2	0.65	0.12	0.70	0.00	0.00	16.8
7	338	-1046	-4945	-42	0	92	-4037	4.02	4.02	4.02	4.02	2	0.59	0.11	0.66	0.00	0.00	16.8
8	338	-1418	-5322	38	0	61	-4501	4.02	4.02	4.02	4.02	2	0.65	0.12	0.70	0.00	0.00	16.8
9	338	-1046	-4950	40	0	61	-4044	4.02	4.02	4.02	4.02	2	0.59	0.11	0.66	0.00	0.00	16.8
10	338	-1287	-5181	-139	0	128	-4325	4.02	4.02	4.02	4.02	2	0.62	0.11	0.69	0.00	0.00	16.8
11	338	-1176	-5070	-138	0	128	-4188	4.02	4.02	4.02	4.02	2	0.61	0.11	0.67	0.00	0.00	16.8

12	338	-1288	-5197	134	0	25	-4350	4.02	4.02	4.02	4.02	2	0.63	0.11	0.69	0.00	0.00	16.8
13	338	-1177	-5085	135	0	25	-4213	4.02	4.02	4.02	4.02	2	0.61	0.11	0.67	0.00	0.00	16.8
14	338	-1418	-5317	-45	0	92	-4494	4.02	4.02	4.02	4.02	2	0.65	0.12	0.70	0.00	0.00	16.8
15	338	-1046	-4945	-42	0	92	-4037	4.02	4.02	4.02	4.02	2	0.59	0.11	0.66	0.00	0.00	16.8
16	338	-1418	-5322	38	0	61	-4501	4.02	4.02	4.02	4.02	2	0.65	0.12	0.70	0.00	0.00	16.8
17	338	-1046	-4950	40	0	61	-4044	4.02	4.02	4.02	4.02	2	0.59	0.11	0.66	0.00	0.00	16.8
18	338	-2249	-7724	-386	0	331	-6595	4.02	4.02	4.02	4.02	3	0.87	0.17	1.01	1.92	0.00	16.8
19	338	-2124	-7650	459	0	-4	-6503	4.02	4.02	4.02	4.02	3	0.86	0.17	1.00	0.00	0.00	16.8
20	338	-2491	-7703	28	0	154	-6652	4.02	4.02	4.02	4.02	3	0.87	0.17	1.00	0.00	0.00	16.8
37	338	-2082	-7312	-680	0	421	-6221	4.02	4.02	4.02	4.02	3	0.82	0.16	0.95	0.00	0.00	16.8
38	338	-1875	-7188	728	0	-137	-6068	4.02	4.02	4.02	4.02	3	0.81	0.16	0.94	0.00	0.00	16.8
39	338	-2486	-7276	9	0	127	-6316	4.02	4.02	4.02	4.02	3	0.83	0.16	0.94	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	375	-1601	-8198	-3	0	100	-5550	4.02	4.02	4.02	4.02	3	0.74	0.18	1.08	2.03	0.00	16.8
2	375	-1287	-6354	-139	0	180	-4325	4.02	4.02	4.02	4.02	2	0.62	0.14	0.84	0.00	0.00	16.8
3	375	-1176	-6243	-138	0	180	-4188	4.02	4.02	4.02	4.02	2	0.61	0.14	0.83	0.00	0.00	16.8
4	375	-1288	-6370	134	0	-25	-4350	4.02	4.02	4.02	4.02	2	0.63	0.14	0.84	0.00	0.00	16.8
5	375	-1177	-6258	135	0	-26	-4213	4.02	4.02	4.02	4.02	2	0.61	0.14	0.83	0.00	0.00	16.8
6	375	-1418	-6490	-45	0	109	-4494	4.02	4.02	4.02	4.02	2	0.65	0.14	0.86	0.00	0.00	16.8
7	375	-1046	-6118	-42	0	107	-4037	4.02	4.02	4.02	4.02	2	0.59	0.13	0.81	0.00	0.00	16.8
8	375	-1418	-6495	38	0	47	-4501	4.02	4.02	4.02	4.02	2	0.65	0.14	0.86	0.00	0.00	16.8
9	375	-1046	-6123	40	0	46	-4044	4.02	4.02	4.02	4.02	2	0.59	0.13	0.81	0.00	0.00	16.8
10	375	-1287	-6354	-139	0	180	-4325	4.02	4.02	4.02	4.02	2	0.62	0.14	0.84	0.00	0.00	16.8
11	375	-1176	-6243	-138	0	180	-4188	4.02	4.02	4.02	4.02	2	0.61	0.14	0.83	0.00	0.00	16.8
12	375	-1288	-6370	134	0	-25	-4350	4.02	4.02	4.02	4.02	2	0.63	0.14	0.84	0.00	0.00	16.8
13	375	-1177	-6258	135	0	-26	-4213	4.02	4.02	4.02	4.02	2	0.61	0.14	0.83	0.00	0.00	16.8
14	375	-1418	-6490	-45	0	109	-4494	4.02	4.02	4.02	4.02	2	0.65	0.14	0.86	0.00	0.00	16.8
15	375	-1046	-6118	-42	0	107	-4037	4.02	4.02	4.02	4.02	2	0.59	0.13	0.81	0.00	0.00	16.8
16	375	-1418	-6495	38	0	47	-4501	4.02	4.02	4.02	4.02	2	0.65	0.14	0.86	0.00	0.00	16.8
17	375	-1046	-6123	40	0	46	-4044	4.02	4.02	4.02	4.02	2	0.59	0.13	0.81	0.00	0.00	16.8
18	375	-2249	-9408	-386	0	475	-6595	4.02	4.02	4.02	4.02	3	0.87	0.20	1.22	2.33	0.00	16.8
19	375	-2124	-9333	459	0	-176	-6503	4.02	4.02	4.02	4.02	3	0.86	0.20	1.22	2.31	0.00	16.8
20	375	-2491	-9386	28	0	144	-6652	4.02	4.02	4.02	4.02	3	0.87	0.20	1.22	2.33	0.00	16.8
37	375	-2082	-8916	-680	0	676	-6221	4.02	4.02	4.02	4.02	3	0.82	0.19	1.16	2.21	0.00	16.8
38	375	-1875	-8792	728	0	-410	-6068	4.02	4.02	4.02	4.02	3	0.81	0.19	1.15	2.18	0.00	16.8
39	375	-2486	-8880	9	0	124	-6316	4.02	4.02	4.02	4.02	3	0.83	0.19	1.15	2.20	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

Nome travata: **trave_505_IP1** Descrizione: **Trave_5 16-15-14-13**
ASTA NUM. 15 NI 125 NF 212 SEZ. Rp B= 0.400 H= 0.500 (trave)

categoria: p.p. y Permanente Neve qy tot.
qy medio: 500.00 2627.25 282.50 3409.75 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-1241	7984	16	0	68	-4781	4.02	4.02	4.02	4.02	3	0.65	0.17	1.06	1.98	0.00	16.8
2	0	-979	6126	-48	0	24	-3657	4.02	4.02	4.02	4.02	2	0.53	0.13	0.82	0.00	0.00	16.8
3	0	-939	6157	-47	0	25	-3696	4.02	4.02	4.02	4.02	2	0.54	0.13	0.82	0.00	0.00	16.8
4	0	-970	6126	72	0	80	-3658	4.02	4.02	4.02	4.02	2	0.53	0.13	0.82	0.00	0.00	16.8
5	0	-931	6157	72	0	81	-3698	4.02	4.02	4.02	4.02	2	0.54	0.13	0.82	0.00	0.00	16.8
6	0	-1022	6090	-6	0	44	-3611	4.02	4.02	4.02	4.02	2	0.53	0.13	0.81	0.00	0.00	16.8
7	0	-889	6193	-5	0	45	-3743	4.02	4.02	4.02	4.02	2	0.55	0.13	0.83	0.00	0.00	16.8
8	0	-1020	6090	30	0	60	-3612	4.02	4.02	4.02	4.02	2	0.53	0.13	0.81	0.00	0.00	16.8
9	0	-887	6192	30	0	61	-3744	4.02	4.02	4.02	4.02	2	0.55	0.13	0.83	0.00	0.00	16.8
10	0	-979	6126	-48	0	24	-3657	4.02	4.02	4.02	4.02	2	0.53	0.13	0.82	0.00	0.00	16.8
11	0	-939	6157	-47	0	25	-3696	4.02	4.02	4.02	4.02	2	0.54	0.13	0.82	0.00	0.00	16.8
12	0	-970	6126	72	0	80	-3658	4.02	4.02	4.02	4.02	2	0.53	0.13	0.82	0.00	0.00	16.8
13	0	-931	6157	72	0	81	-3698	4.02	4.02	4.02	4.02	2	0.54	0.13	0.82	0.00	0.00	16.8
14	0	-1022	6090	-6	0	44	-3611	4.02	4.02	4.02	4.02	2	0.53	0.13	0.81	0.00	0.00	16.8
15	0	-889	6193	-5	0	45	-3743	4.02	4.02	4.02	4.02	2	0.55	0.13	0.83	0.00	0.00	16.8
16	0	-1020	6090	30	0	60	-3612	4.02	4.02	4.02	4.02	2	0.53	0.13	0.81	0.00	0.00	16.8
17	0	-887	6192	30	0	61	-3744	4.02	4.02	4.02	4.02	2	0.55	0.13	0.83	0.00	0.00	16.8
18	0	-1583	8687	-144	0	42	-5096	4.02	4.02	4.02	4.02	3	0.68	0.19	1.14	2.15	0.00	16.8
19	0	-1512	8715	218	0	196	-5135	4.02	4.02	4.02	4.02	3	0.69	0.19	1.15	2.16	0.00	16.8
20	0	-1692	8573	33	0	111	-4880	4.02	4.02	4.02	4.02	3	0.65	0.19	1.13	2.13	0.00	16.8
37	0	-1487	8298	-271	0	-26	-4887	4.02	4.02	4.02	4.02	3	0.66	0.18	1.10	2.06	0.00	16.8
38	0	-1369	8345	332	0	232	-4953	4.02	4.02	4.02	4.02	3	0.67	0.18	1.10	2.07	0.00	16.8
39	0	-1668	8108	23	0	89	-4528	4.02	4.02	4.02	4.02	3	0.61	0.18	1.07	2.01	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	38	-1241	6459	16	0	62	-4781	4.02	4.02	4.02	4.02	3	0.65	0.14	0.86	0.00	0.00	16.8
2	38	-979	4953	-48	0	42	-3657	4.02	4.02	4.02	4.02	2	0.53	0.11	0.66	0.00	0.00	16.8
3	38	-939	4984	-47	0	42	-3696	4.02	4.02	4.02	4.02	2	0.54	0.11	0.66	0.00	0.00	16.8
4	38	-970	4953	72	0	54	-3658	4.02	4.02	4.02	4.02	2	0.53	0.11	0.66	0.00	0.00	16.8
5	38	-931	4984	72	0	54	-3698	4.02	4.02	4.02	4.02	2	0.54	0.11	0.66	0.00	0.00	16.8
6	38	-1022	4917	-6	0	46	-3611	4.02	4.02	4.02	4.02	2	0.53	0.11	0.65	0.00	0.00	16.8
7	38	-889	5020	-5	0	47	-3743	4.02	4.02	4.02	4.02	2	0.55	0.11	0.67	0.00	0.00	16.8
8	38	-1020	4917	30	0	49	-3612	4.02	4.02	4.02	4.02	2	0.53	0.11	0.65	0.00	0.00	16.8
9	38	-887	5019	30	0	50	-3744	4.02	4.02	4.02	4.02	2	0.55	0.11	0.67	0.00	0.00	16.8
10	38	-979	4953	-48	0	42	-3657	4.02	4.02	4.02	4.02	2	0.53	0.11	0.66	0.00	0.00	16.8
11	38	-939	4984	-47	0	42	-3696	4.02	4.02	4.02	4.02	2	0.54	0.11	0.66	0.00	0.00	16.8
12	38	-970	4953	72	0	54	-3658	4.02	4.02	4.02	4.02	2	0.53	0.11	0.66	0.00	0.00	16.8
13	38	-931	4984	72	0	54	-3698	4.02	4.02	4.02	4.02	2	0.54	0.11	0.66	0.00	0.00	16.8
14	38	-1022	4917	-6	0	46	-3611	4.02	4.02	4.02	4.02	2	0.53	0.11	0.65	0.00	0.00	16.8
15	38	-889	5020	-5	0	47	-3743	4.02	4.02	4.02	4.02	2	0.55	0.11	0.67	0.00	0.00	16.8
16	38	-1020	4917	30	0	49	-3612	4.02	4.02	4.02	4.02	2	0.53	0.11	0.65	0.00	0.00	16.8
17	38	-887	5019	30	0	50	-3744	4.02	4.02	4.02	4.02	2	0.55	0.11	0.67	0.00	0.00	16.8
18	38	-1583	7004	-144	0	96	-5096	4.02	4.02	4.02	4.02	3	0.68	0.15	0.92	0.00	0.00	16.8
19	38	-1512	7032	218	0	115	-5135	4.02	4.02	4.02	4.02	3	0.69	0.15	0.93	0.00	0.00	16.8
20	38	-1692	6890	33	0	98	-4880	4.02	4.02	4.02	4.02	3	0.65	0.15	0.91	0.00	0.00	16.8
37	38	-1487	6694	-271	0	75	-4887	4.02	4.02	4.02	4.02	3	0.66	0.14	0.88	0.00	0.00	16.8
38	38	-1369	6741	332	0	107	-4953	4.02	4.02	4.02	4.02	3	0.67	0.15	0.89	0.00	0.00	16.8
39	38	-1668	6504	23	0	80	-4528	4.02	4.02	4.02	4.02	3	0.61	0.14	0.86	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	75	-1241	4935	16	0	57	2562	4.02	4.02	4.02	4.02	3	0.35	0.11	0.65	0.00	0.00	16.8
2	75	-979	3781	-48	0	60	1972	4.02	4.02	4.02	4.02	2	0.29	0.08	0.50	0.00	0.00	16.8
3	75	-939	3812	-47	0	60	1972	4.02	4.02	4.02	4.02	2	0.29	0.08	0.51	0.00	0.00	16.8

4	75	-970	3781	72	0	27	1971	4.02	4.02	4.02	4.02	2	0.29	0.08	0.50	0.00	0.00	16.8
5	75	-931	3811	72	0	27	1969	4.02	4.02	4.02	4.02	2	0.29	0.08	0.51	0.00	0.00	16.8
6	75	-1022	3745	-6	0	48	1973	4.02	4.02	4.02	4.02	2	0.29	0.08	0.50	0.00	0.00	16.8
7	75	-889	3847	-5	0	49	1970	4.02	4.02	4.02	4.02	2	0.29	0.08	0.51	0.00	0.00	16.8
8	75	-1020	3745	30	0	38	1972	4.02	4.02	4.02	4.02	2	0.29	0.08	0.50	0.00	0.00	16.8
9	75	-887	3847	30	0	39	1968	4.02	4.02	4.02	4.02	2	0.29	0.08	0.51	0.00	0.00	16.8
10	75	-979	3781	-48	0	60	1972	4.02	4.02	4.02	4.02	2	0.29	0.08	0.50	0.00	0.00	16.8
11	75	-939	3812	-47	0	60	1972	4.02	4.02	4.02	4.02	2	0.29	0.08	0.51	0.00	0.00	16.8
12	75	-970	3781	72	0	27	1971	4.02	4.02	4.02	4.02	2	0.29	0.08	0.50	0.00	0.00	16.8
13	75	-931	3811	72	0	27	1969	4.02	4.02	4.02	4.02	2	0.29	0.08	0.51	0.00	0.00	16.8
14	75	-1022	3745	-6	0	48	1973	4.02	4.02	4.02	4.02	2	0.29	0.08	0.50	0.00	0.00	16.8
15	75	-889	3847	-5	0	49	1970	4.02	4.02	4.02	4.02	2	0.29	0.08	0.51	0.00	0.00	16.8
16	75	-1020	3745	30	0	38	1972	4.02	4.02	4.02	4.02	2	0.29	0.08	0.50	0.00	0.00	16.8
17	75	-887	3847	30	0	39	1968	4.02	4.02	4.02	4.02	2	0.29	0.08	0.51	0.00	0.00	16.8
18	75	-1583	5320	-144	0	150	2850	4.02	4.02	4.02	4.02	3	0.38	0.12	0.70	0.00	0.00	16.8
19	75	-1512	5348	218	0	33	2846	4.02	4.02	4.02	4.02	3	0.38	0.12	0.71	0.00	0.00	16.8
20	75	-1692	5206	33	0	86	2922	4.02	4.02	4.02	4.02	3	0.39	0.11	0.68	0.00	0.00	16.8
37	75	-1487	5090	-271	0	177	2710	4.02	4.02	4.02	4.02	3	0.36	0.11	0.67	0.00	0.00	16.8
38	75	-1369	5137	332	0	-18	2703	4.02	4.02	4.02	4.02	3	0.36	0.11	0.68	0.00	0.00	16.8
39	75	-1668	4900	23	0	71	2830	4.02	4.02	4.02	4.02	3	0.38	0.11	0.64	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	112	-1241	3410	16	0	51	3043	4.02	4.02	4.02	4.02	3	0.41	0.07	0.45	0.00	0.00	16.8
2	112	-979	2608	-48	0	78	2333	4.02	4.02	4.02	4.02	2	0.34	0.06	0.35	0.00	0.00	16.8
3	112	-939	2639	-47	0	78	2351	4.02	4.02	4.02	4.02	2	0.34	0.06	0.35	0.00	0.00	16.8
4	112	-970	2608	72	0	-0	2331	4.02	4.02	4.02	4.02	2	0.34	0.06	0.35	0.00	0.00	16.8
5	112	-931	2639	72	0	0	2349	4.02	4.02	4.02	4.02	2	0.34	0.06	0.35	0.00	0.00	16.8
6	112	-1022	2572	-6	0	50	2311	4.02	4.02	4.02	4.02	2	0.34	0.06	0.34	0.00	0.00	16.8
7	112	-889	2675	-5	0	51	2371	4.02	4.02	4.02	4.02	2	0.35	0.06	0.36	0.00	0.00	16.8
8	112	-1020	2572	30	0	27	2310	4.02	4.02	4.02	4.02	2	0.34	0.06	0.34	0.00	0.00	16.8
9	112	-887	2674	30	0	27	2370	4.02	4.02	4.02	4.02	2	0.35	0.06	0.36	0.00	0.00	16.8
10	112	-979	2608	-48	0	78	2333	4.02	4.02	4.02	4.02	2	0.34	0.06	0.35	0.00	0.00	16.8
11	112	-939	2639	-47	0	78	2351	4.02	4.02	4.02	4.02	2	0.34	0.06	0.35	0.00	0.00	16.8
12	112	-970	2608	72	0	-0	2331	4.02	4.02	4.02	4.02	2	0.34	0.06	0.35	0.00	0.00	16.8
13	112	-931	2639	72	0	0	2349	4.02	4.02	4.02	4.02	2	0.34	0.06	0.35	0.00	0.00	16.8
14	112	-1022	2572	-6	0	50	2311	4.02	4.02	4.02	4.02	2	0.34	0.06	0.34	0.00	0.00	16.8
15	112	-889	2675	-5	0	51	2371	4.02	4.02	4.02	4.02	2	0.35	0.06	0.36	0.00	0.00	16.8
16	112	-1020	2572	30	0	27	2310	4.02	4.02	4.02	4.02	2	0.34	0.06	0.34	0.00	0.00	16.8
17	112	-887	2674	30	0	27	2370	4.02	4.02	4.02	4.02	2	0.35	0.06	0.36	0.00	0.00	16.8
18	112	-1583	3636	-144	0	203	3301	4.02	4.02	4.02	4.02	3	0.44	0.08	0.48	0.00	0.00	16.8
19	112	-1512	3664	218	0	-49	3314	4.02	4.02	4.02	4.02	3	0.45	0.08	0.48	0.00	0.00	16.8
20	112	-1692	3523	33	0	74	3302	4.02	4.02	4.02	4.02	3	0.44	0.08	0.46	0.00	0.00	16.8
37	112	-1487	3486	-271	0	279	3153	4.02	4.02	4.02	4.02	3	0.42	0.08	0.46	0.00	0.00	16.8
38	112	-1369	3533	332	0	-142	3175	4.02	4.02	4.02	4.02	3	0.43	0.08	0.47	0.00	0.00	16.8
39	112	-1668	3296	23	0	62	3155	4.02	4.02	4.02	4.02	3	0.42	0.07	0.43	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	150	-1241	1886	16	0	45	3043	4.02	4.02	4.02	4.02	3	0.41	0.04	0.25	0.00	0.00	16.8
2	150	-979	1435	-48	0	96	2333	4.02	4.02	4.02	4.02	2	0.34	0.03	0.19	0.00	0.00	16.8
3	150	-939	1466	-47	0	96	2351	4.02	4.02	4.02	4.02	2	0.34	0.03	0.20	0.00	0.00	16.8
4	150	-970	1435	72	0	-27	2331	4.02	4.02	4.02	4.02	2	0.34	0.03	0.19	0.00	0.00	16.8
5	150	-931	1466	72	0	-27	2349	4.02	4.02	4.02	4.02	2	0.34	0.03	0.20	0.00	0.00	16.8
6	150	-1022	1399	-6	0	53	2311	4.02	4.02	4.02	4.02	2	0.34	0.03	0.19	0.00	0.00	16.8
7	150	-889	1502	-5	0	53	2371	4.02	4.02	4.02	4.02	2	0.35	0.03	0.20	0.00	0.00	16.8
8	150	-1020	1399	30	0	16	2310	4.02	4.02	4.02	4.02	2	0.34	0.03	0.19	0.00	0.00	16.8
9	150	-887	1501	30	0	16	2370	4.02	4.02	4.02	4.02	2	0.35	0.03	0.20	0.00	0.00	16.8
10	150	-979	1435	-48	0	96	2333	4.02	4.02	4.02	4.02	2	0.34	0.03	0.19	0.00	0.00	16.8
11	150	-939	1466	-47	0	96	2351	4.02	4.02	4.02	4.02	2	0.34	0.03	0.20	0.00	0.00	16.8
12	150	-970	1435	72	0	-27	2331	4.02	4.02	4.02	4.02	2	0.34	0.03	0.19	0.00	0.00	16.8
13	150	-931	1466	72	0	-27	2349	4.02	4.02	4.02	4.02	2	0.34	0.03	0.20	0.00	0.00	16.8
14	150	-1022	1399	-6	0	53	2311	4.02	4.02	4.02	4.02	2	0.34	0.03	0.19	0.00	0.00	16.8
15	150	-889	1502	-5	0	53	2371	4.02	4.02	4.02	4.02	2	0.35	0.03	0.20	0.00	0.00	16.8
16	150	-1020	1399	30	0	16	2310	4.02	4.02	4.02	4.02	2	0.34	0.03	0.19	0.00	0.00	16.8
17	150	-887	1501	30	0	16	2370	4.02	4.02	4.02	4.02	2	0.35	0.03	0.20	0.00	0.00	16.8
18	150	-1583	1953	-144	0	257	3301	4.02	4.02	4.02	4.02	3	0.44	0.04	0.26	0.00	0.00	16.8
19	150	-1512	1981	218	0	-131	3314	4.02	4.02	4.02	4.02	3	0.45	0.04	0.26	0.00	0.00	16.8
20	150	-1692	1839	33	0	61	3302	4.02	4.02	4.02	4.02	3	0.44	0.04	0.24	0.00	0.00	16.8
37	150	-1487	1882	-271	0	381	3153	4.02	4.02	4.02	4.02	3	0.42	0.04	0.25	0.00	0.00	16.8
38	150	-1369	1929	332	0	-267	3175	4.02	4.02	4.02	4.02	3	0.43	0.04	0.26	0.00	0.00	16.8
39	150	-1668	1692	23	0	54	3155	4.02	4.02	4.02	4.02	3	0.42	0.04	0.22	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	188	-1241	361	16	0	39	3043	4.02	4.02	4.02	4.02	3	0.41	0.01	0.05	0.00	0.00	16.8
2	188	-979	262	-48	0	114	2333	4.02	4.02	4.02	4.02	2	0.34	0.01	0.03	0.00	0.00	16.8
3	188	-939	294	-47	0	114	2351	4.02	4.02	4.02	4.02	2	0.34	0.01	0.04	0.00	0.00	16.8
4	188	-970	262	72	0	-54	2331	4.02	4.02	4.02	4.02	2	0.34	0.01	0.03	0.00	0.00	16.8
5	188	-931	293	72	0	-54	2349	4.02	4.02	4.02	4.02	2	0.34	0.01	0.04	0.00	0.00	16.8
6	188	-1022	226	-6	0	55	2311	4.02	4.02	4.02	4.02	2	0.34	0.00	0.03	0.00	0.00	16.8
7	188	-889	329	-5	0	55	2371	4.02	4.02	4.02	4.02	2	0.35	0.01	0.04	0.00	0.00	16.8
8	188	-1020	226	30	0	5	2310	4.02	4.02	4.02	4.02	2	0.34	0.00	0.03	0.00	0.00	16.8
9	188	-887	328	30	0	5	2370	4.02	4.02	4.02	4.02	2	0.35	0.01	0.04	0.00	0.00	16.8
10	188	-979	262	-48	0	114	2333	4.02	4.02	4.02	4.02	2	0.34	0.01	0.03	0.00	0.00	16.8
11	188	-939	294	-47	0	114	2351	4.02	4.02	4.02	4.02	2	0.34	0.01	0.04	0.00	0.00	16.8
12	188	-970	262	72	0	-54	2331	4.02	4.02	4.02	4.02	2	0.34	0.01	0.03	0.00	0.00	16.8
13	188	-931	293	72	0	-54	2349	4.02	4.02	4.02	4.02	2	0.34	0.01	0.04	0.00	0.00	16.8
14	188	-1022	226	-6	0	55	2311	4.02	4.02	4.02	4.02	2	0.34	0.00	0.03	0.00	0.00	16.8
15	188	-889	329	-5	0	55	2371	4.02	4.02	4.02	4.02	2	0.35	0.01	0.04	0.00	0.00	16.8
16	188	-1020	226	30	0	5	2310	4.02	4.02	4.02	4.02	2	0.34	0.00	0.03	0.00	0.00	16.8
17	188	-887	328	30	0	5	2370	4.02	4.02	4.02	4.02	2	0.35	0.01	0.04	0.00	0.00	16.8
18	188	-1583	269	-144	0	311	3301	4.02	4.02	4.02	4.02	3	0.44	0.01	0.04	0.00	0.00	16.8
19	188	-1512	297	218	0	-213	3314	4.02	4.02	4.02	4.02	3	0.45	0.01	0.04	0.00	0.00	16.8
20	188	-1692	155	33	0	49	3302	4.02	4.02	4.02	4.02	3	0.44	0.00	0.02	0.00	0.00	16.8
37	188	-1487	278	-271	0	482	3153	4.02	4.02	4.02	4.02	3	0.42	0.01	0.04	0.00	0.00	16.8
38	188	-1369	325	332	0	-392	3175	4.02	4.02	4.02	4.02	3	0.43	0.01	0.04	0.00	0.00	16.8
39	188	-1668	88	23	0	45	3155	4.02	4.02	4.02	4.02	3	0.42	0.00	0.01	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	225	-1241	-1164	16	0	33	3043	4.02	4.02	4.02	4.02	3	0.41	0.03	0.15	0.00	0.00	16.8
2	225	-979	-910	-48	0	131	2333	4.02	4.02	4.02	4.02	2	0.34	0.02	0.12	0.00	0.00	16.8
3	225	-939	-879	-47	0	131	2351	4.02	4.02	4.02	4.02	2	0.34	0.02	0.12	0.00	0.00	16.8
4	225	-970	-910	72	0	-81	2331	4.02	4.02	4.02	4.02	2	0.34	0.02	0.12	0.00	0.00	16.8
5	225	-931	-880	72	0	-81	2349	4.02	4.02	4.02	4.02	2	0.34	0.02	0.12	0.00	0.00	16.8
6	225	-1022	-946	-6	0	57	2311	4.02	4.02	4.02	4.02	2	0.34	0.02	0.13	0.00	0.00	16.8
7	225	-889	-844	-5	0	57	2371	4.02	4.02	4.02	4.02	2	0.35	0.02	0.11	0.00	0.00	16.8
8	225	-1020	-946	30	0	-6	2310	4.02	4.02	4.02	4.02	2	0.34	0.02	0.13	0.00	0.00	16.8
9	225	-887	-844	30	0	-7	2370	4.02	4.02	4.02	4.02	2	0.35	0.02	0.11	0.00	0.00	16.8

10	225	-979	-910	-48	0	131	2333	4.02	4.02	4.02	4.02	2	0.34	0.02	0.12	0.00	0.00	16.8
11	225	-939	-879	-47	0	131	2351	4.02	4.02	4.02	4.02	2	0.34	0.02	0.12	0.00	0.00	16.8
12	225	-970	-910	72	0	-81	2331	4.02	4.02	4.02	4.02	2	0.34	0.02	0.12	0.00	0.00	16.8
13	225	-931	-880	72	0	-81	2349	4.02	4.02	4.02	4.02	2	0.34	0.02	0.12	0.00	0.00	16.8
14	225	-1022	-946	-6	0	57	2311	4.02	4.02	4.02	4.02	2	0.34	0.02	0.13	0.00	0.00	16.8
15	225	-889	-844	-5	0	57	2371	4.02	4.02	4.02	4.02	2	0.35	0.02	0.11	0.00	0.00	16.8
16	225	-1020	-946	30	0	-6	2310	4.02	4.02	4.02	4.02	2	0.34	0.02	0.13	0.00	0.00	16.8
17	225	-887	-844	30	0	-7	2370	4.02	4.02	4.02	4.02	2	0.35	0.02	0.11	0.00	0.00	16.8
18	225	-1583	-1414	-144	0	365	3301	4.02	4.02	4.02	4.02	3	0.44	0.03	0.19	0.00	0.00	16.8
19	225	-1512	-1386	218	0	-295	3314	4.02	4.02	4.02	4.02	3	0.45	0.03	0.18	0.00	0.00	16.8
20	225	-1692	-1528	33	0	36	3302	4.02	4.02	4.02	4.02	3	0.44	0.03	0.20	0.00	0.00	16.8
37	225	-1487	-1326	-271	0	584	3153	4.02	4.02	4.02	4.02	3	0.42	0.03	0.17	0.00	0.00	16.8
38	225	-1369	-1279	332	0	-516	3175	4.02	4.02	4.02	4.02	3	0.43	0.03	0.17	0.00	0.00	16.8
39	225	-1668	-1516	23	0	36	3155	4.02	4.02	4.02	4.02	3	0.42	0.03	0.20	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	262	-1241	-2688	16	0	27	3043	4.02	4.02	4.02	4.02	3	0.41	0.06	0.36	0.00	0.00	16.8
2	262	-979	-2083	-48	0	149	2333	4.02	4.02	4.02	4.02	2	0.34	0.05	0.28	0.00	0.00	16.8
3	262	-939	-2052	-47	0	149	2351	4.02	4.02	4.02	4.02	2	0.34	0.04	0.27	0.00	0.00	16.8
4	262	-970	-2083	72	0	-107	2331	4.02	4.02	4.02	4.02	2	0.34	0.05	0.28	0.00	0.00	16.8
5	262	-931	-2053	72	0	-108	2349	4.02	4.02	4.02	4.02	2	0.34	0.04	0.27	0.00	0.00	16.8
6	262	-1022	-2119	-6	0	60	2311	4.02	4.02	4.02	4.02	2	0.34	0.05	0.28	0.00	0.00	16.8
7	262	-889	-2017	-5	0	59	2371	4.02	4.02	4.02	4.02	2	0.35	0.04	0.27	0.00	0.00	16.8
8	262	-1020	-2119	30	0	-17	2310	4.02	4.02	4.02	4.02	2	0.34	0.05	0.28	0.00	0.00	16.8
9	262	-887	-2017	30	0	-18	2370	4.02	4.02	4.02	4.02	2	0.35	0.04	0.27	0.00	0.00	16.8
10	262	-979	-2083	-48	0	149	2333	4.02	4.02	4.02	4.02	2	0.34	0.05	0.28	0.00	0.00	16.8
11	262	-939	-2052	-47	0	149	2351	4.02	4.02	4.02	4.02	2	0.34	0.04	0.27	0.00	0.00	16.8
12	262	-970	-2083	72	0	-107	2331	4.02	4.02	4.02	4.02	2	0.34	0.05	0.28	0.00	0.00	16.8
13	262	-931	-2053	72	0	-108	2349	4.02	4.02	4.02	4.02	2	0.34	0.04	0.27	0.00	0.00	16.8
14	262	-1022	-2119	-6	0	60	2311	4.02	4.02	4.02	4.02	2	0.34	0.05	0.28	0.00	0.00	16.8
15	262	-889	-2017	-5	0	59	2371	4.02	4.02	4.02	4.02	2	0.35	0.04	0.27	0.00	0.00	16.8
16	262	-1020	-2119	30	0	-17	2310	4.02	4.02	4.02	4.02	2	0.34	0.05	0.28	0.00	0.00	16.8
17	262	-887	-2017	30	0	-18	2370	4.02	4.02	4.02	4.02	2	0.35	0.04	0.27	0.00	0.00	16.8
18	262	-1583	-3098	-144	0	419	3301	4.02	4.02	4.02	4.02	3	0.44	0.07	0.41	0.00	0.00	16.8
19	262	-1512	-3070	218	0	-377	3314	4.02	4.02	4.02	4.02	3	0.45	0.07	0.40	0.00	0.00	16.8
20	262	-1692	-3212	33	0	24	3302	4.02	4.02	4.02	4.02	3	0.44	0.07	0.42	0.00	0.00	16.8
37	262	-1487	-2930	-271	0	686	3153	4.02	4.02	4.02	4.02	3	0.42	0.06	0.39	0.00	0.00	16.8
38	262	-1369	-2883	332	0	-641	3175	4.02	4.02	4.02	4.02	3	0.43	0.06	0.38	0.00	0.00	16.8
39	262	-1668	-3120	23	0	27	3155	4.02	4.02	4.02	4.02	3	0.42	0.07	0.41	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	300	-1241	-4213	16	0	21	3009	4.02	4.02	4.02	4.02	3	0.41	0.09	0.56	0.00	0.00	16.8
2	300	-979	-3256	-48	0	167	2297	4.02	4.02	4.02	4.02	2	0.33	0.07	0.43	0.00	0.00	16.8
3	300	-939	-3225	-47	0	167	2335	4.02	4.02	4.02	4.02	2	0.34	0.07	0.43	0.00	0.00	16.8
4	300	-970	-3256	72	0	-134	2295	4.02	4.02	4.02	4.02	2	0.33	0.07	0.43	0.00	0.00	16.8
5	300	-931	-3225	72	0	-134	2332	4.02	4.02	4.02	4.02	2	0.34	0.07	0.43	0.00	0.00	16.8
6	300	-1022	-3292	-6	0	62	2254	4.02	4.02	4.02	4.02	2	0.33	0.07	0.44	0.00	0.00	16.8
7	300	-889	-3189	-5	0	61	2371	4.02	4.02	4.02	4.02	2	0.35	0.07	0.43	0.00	0.00	16.8
8	300	-1020	-3292	30	0	-28	2253	4.02	4.02	4.02	4.02	2	0.33	0.07	0.44	0.00	0.00	16.8
9	300	-887	-3190	30	0	-29	2370	4.02	4.02	4.02	4.02	2	0.35	0.07	0.43	0.00	0.00	16.8
10	300	-979	-3256	-48	0	167	2297	4.02	4.02	4.02	4.02	2	0.33	0.07	0.43	0.00	0.00	16.8
11	300	-939	-3225	-47	0	167	2335	4.02	4.02	4.02	4.02	2	0.34	0.07	0.43	0.00	0.00	16.8
12	300	-970	-3256	72	0	-134	2295	4.02	4.02	4.02	4.02	2	0.33	0.07	0.43	0.00	0.00	16.8
13	300	-931	-3225	72	0	-134	2332	4.02	4.02	4.02	4.02	2	0.34	0.07	0.43	0.00	0.00	16.8
14	300	-1022	-3292	-6	0	62	2254	4.02	4.02	4.02	4.02	2	0.33	0.07	0.44	0.00	0.00	16.8
15	300	-889	-3189	-5	0	61	2371	4.02	4.02	4.02	4.02	2	0.35	0.07	0.43	0.00	0.00	16.8
16	300	-1020	-3292	30	0	-28	2253	4.02	4.02	4.02	4.02	2	0.33	0.07	0.44	0.00	0.00	16.8
17	300	-887	-3190	30	0	-29	2370	4.02	4.02	4.02	4.02	2	0.35	0.07	0.43	0.00	0.00	16.8
18	300	-1583	-4781	-144	0	473	3184	4.02	4.02	4.02	4.02	3	0.43	0.10	0.63	0.00	0.00	16.8
19	300	-1512	-4753	218	0	-459	3214	4.02	4.02	4.02	4.02	3	0.43	0.10	0.63	0.00	0.00	16.8
20	300	-1692	-4895	33	0	11	3114	4.02	4.02	4.02	4.02	3	0.42	0.11	0.64	0.00	0.00	16.8
37	300	-1487	-4534	-271	0	788	3055	4.02	4.02	4.02	4.02	3	0.41	0.10	0.60	0.00	0.00	16.8
38	300	-1369	-4487	332	0	-766	3105	4.02	4.02	4.02	4.02	3	0.42	0.10	0.59	0.00	0.00	16.8
39	300	-1668	-4724	23	0	18	2939	4.02	4.02	4.02	4.02	3	0.39	0.10	0.62	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	338	-1241	-5737	16	0	15	-3426	4.02	4.02	4.02	4.02	3	0.46	0.12	0.76	0.00	0.00	16.8
2	338	-979	-4428	-48	0	185	-2672	4.02	4.02	4.02	4.02	2	0.39	0.10	0.59	0.00	0.00	16.8
3	338	-939	-4397	-47	0	185	-2596	4.02	4.02	4.02	4.02	2	0.38	0.10	0.59	0.00	0.00	16.8
4	338	-970	-4428	72	0	-161	-2675	4.02	4.02	4.02	4.02	2	0.39	0.10	0.59	0.00	0.00	16.8
5	338	-931	-4398	72	0	-161	-2599	4.02	4.02	4.02	4.02	2	0.38	0.10	0.59	0.00	0.00	16.8
6	338	-1022	-4464	-6	0	64	-2761	4.02	4.02	4.02	4.02	2	0.40	0.10	0.59	0.00	0.00	16.8
7	338	-889	-4362	-5	0	63	-2509	4.02	4.02	4.02	4.02	2	0.37	0.09	0.58	0.00	0.00	16.8
8	338	-1020	-4464	30	0	-40	-2762	4.02	4.02	4.02	4.02	2	0.40	0.10	0.59	0.00	0.00	16.8
9	338	-887	-4362	30	0	-41	-2510	4.02	4.02	4.02	4.02	2	0.37	0.09	0.58	0.00	0.00	16.8
10	338	-979	-4428	-48	0	185	-2672	4.02	4.02	4.02	4.02	2	0.39	0.10	0.59	0.00	0.00	16.8
11	338	-939	-4397	-47	0	185	-2596	4.02	4.02	4.02	4.02	2	0.38	0.10	0.59	0.00	0.00	16.8
12	338	-970	-4428	72	0	-161	-2675	4.02	4.02	4.02	4.02	2	0.39	0.10	0.59	0.00	0.00	16.8
13	338	-931	-4398	72	0	-161	-2599	4.02	4.02	4.02	4.02	2	0.38	0.10	0.59	0.00	0.00	16.8
14	338	-1022	-4464	-6	0	64	-2761	4.02	4.02	4.02	4.02	2	0.40	0.10	0.59	0.00	0.00	16.8
15	338	-889	-4362	-5	0	63	-2509	4.02	4.02	4.02	4.02	2	0.37	0.09	0.58	0.00	0.00	16.8
16	338	-1020	-4464	30	0	-40	-2762	4.02	4.02	4.02	4.02	2	0.40	0.10	0.59	0.00	0.00	16.8
17	338	-887	-4362	30	0	-41	-2510	4.02	4.02	4.02	4.02	2	0.37	0.09	0.58	0.00	0.00	16.8
18	338	-1583	-6464	-144	0	527	-4085	4.02	4.02	4.02	4.02	3	0.55	0.14	0.85	0.00	0.00	16.8
19	338	-1512	-6436	218	0	-541	-4019	4.02	4.02	4.02	4.02	3	0.54	0.14	0.85	0.00	0.00	16.8
20	338	-1692	-6578	33	0	-1	-4298	4.02	4.02	4.02	4.02	3	0.57	0.14	0.87	0.00	0.00	16.8
37	338	-1487	-6138	-271	0	889	-3844	4.02	4.02	4.02	4.02	3	0.52	0.13	0.81	0.00	0.00	16.8
38	338	-1369	-6091	332	0	-890	-3735	4.02	4.02	4.02	4.02	3	0.50	0.13	0.81	0.00	0.00	16.8
39	338	-1668	-6328	23	0	10	-4199	4.02	4.02	4.02	4.02	3	0.56	0.14	0.83	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	375	-1241	-7262	16	0	9	-3426	4.02	4.02	4.02	4.02	3	0.46	0.16	0.96	0.00	0.00	16.8
2	375	-979	-5601	-48	0	203	-2672	4.02	4.02	4.02	4.02	2	0.39	0.12	0.75	0.00	0.00	16.8
3	375	-939	-5570	-47	0	202	-2596	4.02	4.02	4.02	4.02	2	0.38	0.12	0.74	0.00	0.00	16.8
4	375	-970	-5601	72	0	-188	-2675	4.02	4.02	4.02	4.02	2	0.39	0.12	0.75	0.00	0.00	16.8
5	375	-931	-5571	72	0	-188	-2599	4.02	4.02	4.02	4.02	2	0.38	0.12	0.74	0.00	0.00	16.8
6	375	-1022	-5637	-6	0	67	-2761	4.02	4.02	4.02	4.02	2	0.40	0.12	0.75	0.00	0.00	16.8
7	375	-889	-5535	-5	0	65	-2509	4.02	4.02	4.02	4.02	2	0.37	0.12	0.74	0.00	0.00	16.8
8	375	-1020	-5637	30	0	-51	-2762	4.02	4.02	4.02	4.02	2	0.40	0.12	0.75	0.00	0.00	16.8
9	375	-887	-5535	30	0	-52	-2510	4.02	4.02	4.02	4.02	2	0.37	0.12	0.74	0.00	0.00	16.8
10	375	-979	-5601	-48	0	203	-2672	4.02	4.02	4.02	4.02	2	0.39	0.12	0.75	0.00	0.00	16.8
11	375	-939	-5570	-47	0	202	-2596	4.02	4.02	4.02	4.02	2	0.38	0.12	0.74	0.00	0.00	16.8
12	375	-970	-5601	72	0	-188	-2675	4.02	4.02	4.02	4.02	2	0.39	0.12	0.75	0.00	0.00	16.8
13	375	-931	-5571	72	0	-188	-2599	4.02	4.02	4.02	4.02	2	0.38	0.12	0.74	0.00	0.00	16.8
14	375	-1022	-5637	-6	0	67	-2761	4.02	4.02	4.02	4.02	2	0.40	0.12	0.75	0.00	0.00	16.8
15	375	-889	-5535	-5	0	65	-2509	4.02	4.02	4.02	4.02	2	0.37	0.12	0.74	0.00	0.00	16.8

16	375	-1020	-5637	30	0	-51	-2762	4.02	4.02	4.02	4.02	2	0.40	0.12	0.75	0.00	0.00	16.8
17	375	-887	-5535	30	0	-52	-2510	4.02	4.02	4.02	4.02	2	0.37	0.12	0.74	0.00	0.00	16.8
18	375	-1583	-8148	-144	0	581	-4085	4.02	4.02	4.02	4.02	3	0.55	0.18	1.07	2.02	0.00	16.8
19	375	-1512	-8120	218	0	-623	-4019	4.02	4.02	4.02	4.02	3	0.54	0.18	1.07	2.01	0.00	16.8
20	375	-1692	-8262	33	0	-13	-4298	4.02	4.02	4.02	4.02	3	0.57	0.18	1.09	2.05	0.00	16.8
37	375	-1487	-7742	-271	0	991	-3844	4.02	4.02	4.02	4.02	3	0.52	0.17	1.02	1.92	0.00	16.8
38	375	-1369	-7695	332	0	-1015	-3735	4.02	4.02	4.02	4.02	3	0.50	0.17	1.02	1.91	0.00	16.8
39	375	-1668	-7932	23	0	1	-4199	4.02	4.02	4.02	4.02	3	0.56	0.17	1.04	1.97	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

Nome travata: **trave_506_IP1** Descrizione: **Trave_5 21-20-19-18**
ASTA NUM. 16 NI 185 NF 298 SEZ. Rp B= 0.400 H= 0.500 (trave)

categoria: p.p. y Permanente Neve qy tot.
qy medio: 500.00 2627.25 282.50 3409.75 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
													Fx,M	Bielle	V,Mx			
	cm		daN			daN*m				cmq						cmq/m		cm
1	0	-501	5981	-754	0	-1082	-2157	4.02	4.02	4.02	4.02	3	0.30	0.13	0.80	0.00	0.00	16.8
2	0	-332	4542	-331	0	-538	-1618	4.02	4.02	4.02	4.02	2	0.24	0.10	0.61	0.00	0.00	16.8
3	0	-363	4679	-345	0	-564	-1731	4.02	4.02	4.02	4.02	2	0.26	0.10	0.63	0.00	0.00	16.8
4	0	-407	4522	-816	0	-1102	-1588	4.02	4.02	4.02	4.02	2	0.24	0.10	0.61	0.00	0.00	16.8
5	0	-438	4659	-829	0	-1128	-1701	4.02	4.02	4.02	4.02	2	0.25	0.10	0.63	0.00	0.00	16.8
6	0	-321	4375	-485	0	-705	-1476	4.02	4.02	4.02	4.02	2	0.22	0.10	0.59	0.00	0.00	16.8
7	0	-426	4832	-530	0	-791	-1853	4.02	4.02	4.02	4.02	2	0.27	0.10	0.65	0.00	0.00	16.8
8	0	-344	4369	-631	0	-874	-1466	4.02	4.02	4.02	4.02	2	0.22	0.09	0.59	0.00	0.00	16.8
9	0	-449	4826	-675	0	-961	-1843	4.02	4.02	4.02	4.02	2	0.27	0.10	0.65	0.00	0.00	16.8
10	0	-332	4542	-331	0	-538	-1618	4.02	4.02	4.02	4.02	2	0.24	0.10	0.61	0.00	0.00	16.8
11	0	-363	4679	-345	0	-564	-1731	4.02	4.02	4.02	4.02	2	0.26	0.10	0.63	0.00	0.00	16.8
12	0	-407	4522	-816	0	-1102	-1588	4.02	4.02	4.02	4.02	2	0.24	0.10	0.61	0.00	0.00	16.8
13	0	-438	4659	-829	0	-1128	-1701	4.02	4.02	4.02	4.02	2	0.25	0.10	0.63	0.00	0.00	16.8
14	0	-321	4375	-485	0	-705	-1476	4.02	4.02	4.02	4.02	2	0.22	0.10	0.59	0.00	0.00	16.8
15	0	-426	4832	-530	0	-791	-1853	4.02	4.02	4.02	4.02	2	0.27	0.10	0.65	0.00	0.00	16.8
16	0	-344	4369	-631	0	-874	-1466	4.02	4.02	4.02	4.02	2	0.22	0.09	0.59	0.00	0.00	16.8
17	0	-449	4826	-675	0	-961	-1843	4.02	4.02	4.02	4.02	2	0.27	0.10	0.65	0.00	0.00	16.8
18	0	-231	6517	-904	0	-1483	-2413	4.02	4.02	4.02	4.02	3	0.34	0.14	0.88	0.00	0.00	16.8
19	0	-505	6423	-2200	0	-2887	-2283	4.02	4.02	4.02	4.02	3	0.50	0.14	0.86	0.00	0.00	16.8
20	0	-316	6527	-1528	0	-2167	-2300	4.02	4.02	4.02	4.02	3	0.38	0.14	0.88	0.00	0.00	16.8
37	0	-173	6287	-213	0	-656	-2365	4.02	4.02	4.02	4.02	3	0.33	0.14	0.85	0.00	0.00	16.8
38	0	-630	6130	-2372	0	-2996	-2149	4.02	4.02	4.02	4.02	3	0.52	0.13	0.82	0.00	0.00	16.8
39	0	-314	6303	-1253	0	-1797	-2176	4.02	4.02	4.02	4.02	3	0.31	0.14	0.85	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	31	-501	4721	-754	0	-848	-2157	4.02	4.02	4.02	4.02	3	0.30	0.10	0.63	0.00	0.00	16.8
2	31	-332	3573	-331	0	-435	-1618	4.02	4.02	4.02	4.02	2	0.24	0.08	0.48	0.00	0.00	16.8
3	31	-363	3710	-345	0	-457	-1731	4.02	4.02	4.02	4.02	2	0.26	0.08	0.50	0.00	0.00	16.8
4	31	-407	3552	-816	0	-849	-1588	4.02	4.02	4.02	4.02	2	0.24	0.08	0.48	0.00	0.00	16.8
5	31	-438	3689	-829	0	-871	-1701	4.02	4.02	4.02	4.02	2	0.25	0.08	0.50	0.00	0.00	16.8
6	31	-321	3406	-485	0	-554	-1476	4.02	4.02	4.02	4.02	2	0.22	0.07	0.46	0.00	0.00	16.8
7	31	-426	3862	-530	0	-627	-1853	4.02	4.02	4.02	4.02	2	0.27	0.08	0.52	0.00	0.00	16.8
8	31	-344	3400	-631	0	-678	-1466	4.02	4.02	4.02	4.02	2	0.22	0.07	0.46	0.00	0.00	16.8
9	31	-449	3856	-675	0	-751	-1843	4.02	4.02	4.02	4.02	2	0.27	0.08	0.52	0.00	0.00	16.8
10	31	-332	3573	-331	0	-435	-1618	4.02	4.02	4.02	4.02	2	0.24	0.08	0.48	0.00	0.00	16.8
11	31	-363	3710	-345	0	-457	-1731	4.02	4.02	4.02	4.02	2	0.26	0.08	0.50	0.00	0.00	16.8
12	31	-407	3552	-816	0	-849	-1588	4.02	4.02	4.02	4.02	2	0.24	0.08	0.48	0.00	0.00	16.8
13	31	-438	3689	-829	0	-871	-1701	4.02	4.02	4.02	4.02	2	0.25	0.08	0.50	0.00	0.00	16.8
14	31	-321	3406	-485	0	-554	-1476	4.02	4.02	4.02	4.02	2	0.22	0.07	0.46	0.00	0.00	16.8
15	31	-426	3862	-530	0	-627	-1853	4.02	4.02	4.02	4.02	2	0.27	0.08	0.52	0.00	0.00	16.8
16	31	-344	3400	-631	0	-678	-1466	4.02	4.02	4.02	4.02	2	0.22	0.07	0.46	0.00	0.00	16.8
17	31	-449	3856	-675	0	-751	-1843	4.02	4.02	4.02	4.02	2	0.27	0.08	0.52	0.00	0.00	16.8
18	31	-231	5125	-904	0	-1203	-2413	4.02	4.02	4.02	4.02	3	0.34	0.11	0.69	0.00	0.00	16.8
19	31	-505	5031	-2200	0	-2205	-2283	4.02	4.02	4.02	4.02	3	0.38	0.11	0.68	0.00	0.00	16.8
20	31	-316	5135	-1528	0	-1694	-2300	4.02	4.02	4.02	4.02	3	0.32	0.11	0.69	0.00	0.00	16.8
37	31	-173	4961	-213	0	-590	-2365	4.02	4.02	4.02	4.02	3	0.33	0.11	0.67	0.00	0.00	16.8
38	31	-630	4804	-2372	0	-2261	-2149	4.02	4.02	4.02	4.02	3	0.39	0.10	0.64	0.00	0.00	16.8
39	31	-314	4977	-1253	0	-1409	-2176	4.02	4.02	4.02	4.02	3	0.30	0.11	0.67	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	62	-501	3460	-754	0	-614	2229	4.02	4.02	4.02	4.02	3	0.31	0.08	0.46	0.00	0.00	16.8
2	62	-332	2603	-331	0	-332	1666	4.02	4.02	4.02	4.02	2	0.25	0.06	0.35	0.00	0.00	16.8
3	62	-363	2740	-345	0	-350	1765	4.02	4.02	4.02	4.02	2	0.26	0.06	0.37	0.00	0.00	16.8
4	62	-407	2583	-816	0	-596	1664	4.02	4.02	4.02	4.02	2	0.25	0.06	0.35	0.00	0.00	16.8
5	62	-438	2720	-829	0	-614	1764	4.02	4.02	4.02	4.02	2	0.26	0.06	0.37	0.00	0.00	16.8
6	62	-321	2436	-485	0	-404	1549	4.02	4.02	4.02	4.02	2	0.23	0.05	0.33	0.00	0.00	16.8
7	62	-426	2893	-530	0	-463	1880	4.02	4.02	4.02	4.02	2	0.28	0.06	0.39	0.00	0.00	16.8
8	62	-344	2430	-631	0	-483	1549	4.02	4.02	4.02	4.02	2	0.23	0.05	0.33	0.00	0.00	16.8
9	62	-449	2887	-675	0	-542	1880	4.02	4.02	4.02	4.02	2	0.28	0.06	0.39	0.00	0.00	16.8
10	62	-332	2603	-331	0	-332	1666	4.02	4.02	4.02	4.02	2	0.25	0.06	0.35	0.00	0.00	16.8
11	62	-363	2740	-345	0	-350	1765	4.02	4.02	4.02	4.02	2	0.26	0.06	0.37	0.00	0.00	16.8
12	62	-407	2583	-816	0	-596	1664	4.02	4.02	4.02	4.02	2	0.25	0.06	0.35	0.00	0.00	16.8
13	62	-438	2720	-829	0	-614	1764	4.02	4.02	4.02	4.02	2	0.26	0.06	0.37	0.00	0.00	16.8
14	62	-321	2436	-485	0	-404	1549	4.02	4.02	4.02	4.02	2	0.23	0.05	0.33	0.00	0.00	16.8
15	62	-426	2893	-530	0	-463	1880	4.02	4.02	4.02	4.02	2	0.28	0.06	0.39	0.00	0.00	16.8
16	62	-344	2430	-631	0	-483	1549	4.02	4.02	4.02	4.02	2	0.23	0.05	0.33	0.00	0.00	16.8
17	62	-449	2887	-675	0	-542	1880	4.02	4.02	4.02	4.02	2	0.28	0.06	0.39	0.00	0.00	16.8
18	62	-231	3734	-904	0	-923	2296	4.02	4.02	4.02	4.02	3	0.32	0.08	0.50	0.00	0.00	16.8
19	62	-505	3640	-2200	0	-1523	2279	4.02	4.02	4.02	4.02	3	0.32	0.08	0.49	0.00	0.00	16.8
20	62	-316	3744	-1528	0	-1220	2424	4.02	4.02	4.02	4.02	3	0.34	0.08	0.50	0.00	0.00	16.8
37	62	-173	3635	-213	0	-524	2242	4.02	4.02	4.02	4.02	3	0.31	0.08	0.49	0.00	0.00	16.8
38	62	-630	3478	-2372	0	-1525	2215	4.02	4.02	4.02	4.02	3	0.31	0.08	0.47	0.00	0.00	16.8
39	62	-314	3651	-1253	0	-1020	2456	4.02	4.02	4.02	4.02	3	0.34	0.08	0.49	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	93	-501	2200	-754	0	-381	2229	4.02	4.02	4.02	4.02	3	0.31	0.05	0.30	0.00	0.00	16.8
2	93	-332	1634	-331	0	-230	1666	4.02	4.02	4.02	4.02	2	0.25	0.04	0.22	0.00	0.00	16.8
3	93	-363	1771	-345	0	-243	1765	4.02	4.02	4.02	4.02	2	0.26	0.04	0.24	0.00	0.00	16.8
4	93	-407	1613	-816	0	-343	1664	4.02	4.02	4.02	4.02	2	0.25	0.04	0.22	0.00	0.00	16.8
5	93	-438	1750	-829	0	-357	1764	4.02	4.02	4.02	4.02	2	0.26	0.04	0.24	0.00	0.00	16.8
6	93	-321	1466	-485	0	-254	1549	4.02	4.02	4.02	4.02	2	0.23	0.03	0.20	0.00	0.00	16.8
7	93	-426	1923	-530	0	-299	1880	4.02	4.02	4.02	4.02	2	0.28	0.04	0.26	0.00	0.00	16.8

8	93	-344	1460	-631	0	-287	1549	4.02	4.02	4.02	4.02	2	0.23	0.03	0.20	0.00	0.00	16.8
9	93	-449	1917	-675	0	-333	1880	4.02	4.02	4.02	4.02	2	0.28	0.04	0.26	0.00	0.00	16.8
10	93	-332	1634	-331	0	-230	1666	4.02	4.02	4.02	4.02	2	0.25	0.04	0.22	0.00	0.00	16.8
11	93	-363	1771	-345	0	-243	1765	4.02	4.02	4.02	4.02	2	0.26	0.04	0.24	0.00	0.00	16.8
12	93	-407	1613	-816	0	-343	1664	4.02	4.02	4.02	4.02	2	0.25	0.04	0.22	0.00	0.00	16.8
13	93	-438	1750	-829	0	-357	1764	4.02	4.02	4.02	4.02	2	0.26	0.04	0.24	0.00	0.00	16.8
14	93	-321	1466	-485	0	-254	1549	4.02	4.02	4.02	4.02	2	0.23	0.03	0.20	0.00	0.00	16.8
15	93	-426	1923	-530	0	-299	1880	4.02	4.02	4.02	4.02	2	0.28	0.04	0.26	0.00	0.00	16.8
16	93	-344	1460	-631	0	-287	1549	4.02	4.02	4.02	4.02	2	0.23	0.03	0.20	0.00	0.00	16.8
17	93	-449	1917	-675	0	-333	1880	4.02	4.02	4.02	4.02	2	0.28	0.04	0.26	0.00	0.00	16.8
18	93	-231	2342	-904	0	-642	2296	4.02	4.02	4.02	4.02	3	0.32	0.05	0.32	0.00	0.00	16.8
19	93	-505	2248	-2200	0	-841	2279	4.02	4.02	4.02	4.02	3	0.32	0.05	0.30	0.00	0.00	16.8
20	93	-316	2352	-1528	0	-747	2424	4.02	4.02	4.02	4.02	3	0.34	0.05	0.32	0.00	0.00	16.8
37	93	-173	2309	-213	0	-458	2242	4.02	4.02	4.02	4.02	3	0.31	0.05	0.31	0.00	0.00	16.8
38	93	-630	2152	-2372	0	-790	2215	4.02	4.02	4.02	4.02	3	0.31	0.05	0.30	0.00	0.00	16.8
39	93	-314	2325	-1253	0	-632	2456	4.02	4.02	4.02	4.02	3	0.34	0.05	0.31	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	124	-501	940	-754	0	-147	2229	4.02	4.02	4.02	4.02	3	0.31	0.02	0.13	0.00	0.00	16.8
2	124	-332	664	-331	0	-127	1666	4.02	4.02	4.02	4.02	2	0.25	0.01	0.09	0.00	0.00	16.8
3	124	-363	801	-345	0	-136	1765	4.02	4.02	4.02	4.02	2	0.26	0.02	0.11	0.00	0.00	16.8
4	124	-407	644	-816	0	-90	1664	4.02	4.02	4.02	4.02	2	0.25	0.02	0.10	0.00	0.00	16.8
5	124	-438	781	-829	0	-100	1764	4.02	4.02	4.02	4.02	2	0.26	0.02	0.11	0.00	0.00	16.8
6	124	-321	497	-485	0	-103	1549	4.02	4.02	4.02	4.02	2	0.23	0.01	0.07	0.00	0.00	16.8
7	124	-426	954	-530	0	-134	1880	4.02	4.02	4.02	4.02	2	0.28	0.02	0.13	0.00	0.00	16.8
8	124	-344	491	-631	0	-92	1549	4.02	4.02	4.02	4.02	2	0.23	0.01	0.08	0.00	0.00	16.8
9	124	-449	948	-675	0	-123	1880	4.02	4.02	4.02	4.02	2	0.28	0.02	0.13	0.00	0.00	16.8
10	124	-332	664	-331	0	-127	1666	4.02	4.02	4.02	4.02	2	0.25	0.01	0.09	0.00	0.00	16.8
11	124	-363	801	-345	0	-136	1765	4.02	4.02	4.02	4.02	2	0.26	0.02	0.11	0.00	0.00	16.8
12	124	-407	644	-816	0	-90	1664	4.02	4.02	4.02	4.02	2	0.25	0.02	0.10	0.00	0.00	16.8
13	124	-438	781	-829	0	-100	1764	4.02	4.02	4.02	4.02	2	0.26	0.02	0.11	0.00	0.00	16.8
14	124	-321	497	-485	0	-103	1549	4.02	4.02	4.02	4.02	2	0.23	0.01	0.07	0.00	0.00	16.8
15	124	-426	954	-530	0	-134	1880	4.02	4.02	4.02	4.02	2	0.28	0.02	0.13	0.00	0.00	16.8
16	124	-344	491	-631	0	-92	1549	4.02	4.02	4.02	4.02	2	0.23	0.01	0.08	0.00	0.00	16.8
17	124	-449	948	-675	0	-123	1880	4.02	4.02	4.02	4.02	2	0.28	0.02	0.13	0.00	0.00	16.8
18	124	-231	950	-904	0	-362	2296	4.02	4.02	4.02	4.02	3	0.32	0.02	0.13	0.00	0.00	16.8
19	124	-505	856	-2200	0	-159	2279	4.02	4.02	4.02	4.02	3	0.32	0.05	0.28	0.00	0.00	16.8
20	124	-316	960	-1528	0	-273	2424	4.02	4.02	4.02	4.02	3	0.34	0.03	0.20	0.00	0.00	16.8
37	124	-173	983	-213	0	-392	2242	4.02	4.02	4.02	4.02	3	0.31	0.02	0.13	0.00	0.00	16.8
38	124	-630	826	-2372	0	-54	2215	4.02	4.02	4.02	4.02	3	0.31	0.05	0.30	0.00	0.00	16.8
39	124	-314	999	-1253	0	-244	2456	4.02	4.02	4.02	4.02	3	0.34	0.03	0.16	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	155	-501	-320	-754	0	87	2229	4.02	4.02	4.02	4.02	3	0.31	0.02	0.10	0.00	0.00	16.8
2	155	-332	-305	-331	0	-24	1666	4.02	4.02	4.02	4.02	2	0.25	0.01	0.04	0.00	0.00	16.8
3	155	-363	-168	-345	0	-29	1765	4.02	4.02	4.02	4.02	2	0.26	0.01	0.04	0.00	0.00	16.8
4	155	-407	-326	-816	0	162	1664	4.02	4.02	4.02	4.02	2	0.25	0.02	0.10	0.00	0.00	16.8
5	155	-438	-188	-829	0	157	1764	4.02	4.02	4.02	4.02	2	0.26	0.02	0.11	0.00	0.00	16.8
6	155	-321	-472	-485	0	47	1549	4.02	4.02	4.02	4.02	2	0.23	0.01	0.06	0.00	0.00	16.8
7	155	-426	-16	-530	0	30	1880	4.02	4.02	4.02	4.02	2	0.28	0.01	0.07	0.00	0.00	16.8
8	155	-344	-478	-631	0	104	1549	4.02	4.02	4.02	4.02	2	0.23	0.01	0.08	0.00	0.00	16.8
9	155	-449	-22	-675	0	86	1880	4.02	4.02	4.02	4.02	2	0.28	0.02	0.09	0.00	0.00	16.8
10	155	-332	-305	-331	0	-24	1666	4.02	4.02	4.02	4.02	2	0.25	0.01	0.04	0.00	0.00	16.8
11	155	-363	-168	-345	0	-29	1765	4.02	4.02	4.02	4.02	2	0.26	0.01	0.04	0.00	0.00	16.8
12	155	-407	-326	-816	0	162	1664	4.02	4.02	4.02	4.02	2	0.25	0.02	0.10	0.00	0.00	16.8
13	155	-438	-188	-829	0	157	1764	4.02	4.02	4.02	4.02	2	0.26	0.02	0.11	0.00	0.00	16.8
14	155	-321	-472	-485	0	47	1549	4.02	4.02	4.02	4.02	2	0.23	0.01	0.06	0.00	0.00	16.8
15	155	-426	-16	-530	0	30	1880	4.02	4.02	4.02	4.02	2	0.28	0.01	0.07	0.00	0.00	16.8
16	155	-344	-478	-631	0	104	1549	4.02	4.02	4.02	4.02	2	0.23	0.01	0.08	0.00	0.00	16.8
17	155	-449	-22	-675	0	86	1880	4.02	4.02	4.02	4.02	2	0.28	0.02	0.09	0.00	0.00	16.8
18	155	-231	-442	-904	0	-82	2296	4.02	4.02	4.02	4.02	3	0.32	0.02	0.12	0.00	0.00	16.8
19	155	-505	-536	-2200	0	522	2279	4.02	4.02	4.02	4.02	3	0.32	0.05	0.28	0.00	0.00	16.8
20	155	-316	-432	-1528	0	200	2424	4.02	4.02	4.02	4.02	3	0.34	0.03	0.20	0.00	0.00	16.8
37	155	-173	-343	-213	0	-326	2242	4.02	4.02	4.02	4.02	3	0.31	0.01	0.05	0.00	0.00	16.8
38	155	-630	-500	-2372	0	681	2215	4.02	4.02	4.02	4.02	3	0.31	0.05	0.30	0.00	0.00	16.8
39	155	-314	-327	-1253	0	144	2456	4.02	4.02	4.02	4.02	3	0.34	0.03	0.16	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	186	-501	-1581	-754	0	321	2229	4.02	4.02	4.02	4.02	3	0.31	0.03	0.21	0.00	0.00	16.8
2	186	-332	-1274	-331	0	78	1666	4.02	4.02	4.02	4.02	2	0.25	0.03	0.17	0.00	0.00	16.8
3	186	-363	-1137	-345	0	77	1765	4.02	4.02	4.02	4.02	2	0.26	0.02	0.15	0.00	0.00	16.8
4	186	-407	-1295	-816	0	415	1664	4.02	4.02	4.02	4.02	2	0.25	0.03	0.17	0.00	0.00	16.8
5	186	-438	-1158	-829	0	415	1764	4.02	4.02	4.02	4.02	2	0.26	0.03	0.16	0.00	0.00	16.8
6	186	-321	-1442	-485	0	198	1549	4.02	4.02	4.02	4.02	2	0.23	0.03	0.19	0.00	0.00	16.8
7	186	-426	-985	-530	0	194	1880	4.02	4.02	4.02	4.02	2	0.28	0.02	0.13	0.00	0.00	16.8
8	186	-344	-1448	-631	0	299	1549	4.02	4.02	4.02	4.02	2	0.23	0.03	0.20	0.00	0.00	16.8
9	186	-449	-991	-675	0	296	1880	4.02	4.02	4.02	4.02	2	0.28	0.02	0.13	0.00	0.00	16.8
10	186	-332	-1274	-331	0	78	1666	4.02	4.02	4.02	4.02	2	0.25	0.03	0.17	0.00	0.00	16.8
11	186	-363	-1137	-345	0	77	1765	4.02	4.02	4.02	4.02	2	0.26	0.02	0.15	0.00	0.00	16.8
12	186	-407	-1295	-816	0	415	1664	4.02	4.02	4.02	4.02	2	0.25	0.03	0.17	0.00	0.00	16.8
13	186	-438	-1158	-829	0	415	1764	4.02	4.02	4.02	4.02	2	0.26	0.03	0.16	0.00	0.00	16.8
14	186	-321	-1442	-485	0	198	1549	4.02	4.02	4.02	4.02	2	0.23	0.03	0.19	0.00	0.00	16.8
15	186	-426	-985	-530	0	194	1880	4.02	4.02	4.02	4.02	2	0.28	0.02	0.13	0.00	0.00	16.8
16	186	-344	-1448	-631	0	299	1549	4.02	4.02	4.02	4.02	2	0.23	0.03	0.20	0.00	0.00	16.8
17	186	-449	-991	-675	0	296	1880	4.02	4.02	4.02	4.02	2	0.28	0.02	0.13	0.00	0.00	16.8
18	186	-231	-1833	-904	0	198	2296	4.02	4.02	4.02	4.02	3	0.32	0.04	0.25	0.00	0.00	16.8
19	186	-505	-1927	-2200	0	1204	2279	4.02	4.02	4.02	4.02	3	0.32	0.05	0.28	0.00	0.00	16.8
20	186	-316	-1823	-1528	0	674	2424	4.02	4.02	4.02	4.02	3	0.34	0.04	0.25	0.00	0.00	16.8
37	186	-173	-1669	-213	0	-260	2242	4.02	4.02	4.02	4.02	3	0.31	0.04	0.23	0.00	0.00	16.8
38	186	-630	-1826	-2372	0	1416	2215	4.02	4.02	4.02	4.02	3	0.31	0.05	0.30	0.00	0.00	16.8
39	186	-314	-1652	-1253	0	533	2456	4.02	4.02	4.02	4.02	3	0.34	0.04	0.22	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	217	-501	-2841	-754	0	555	2229	4.02	4.02	4.02	4.02	3	0.31	0.06	0.38	0.00	0.00	16.8
2	217	-332	-2244	-331	0	181	1666	4.02	4.02	4.02	4.02	2	0.25	0.05	0.30	0.00	0.00	16.8
3	217	-363	-2107	-345	0	184	1765	4.02	4.02	4.02	4.02	2	0.26	0.05	0.28	0.00	0.00	16.8
4	217	-407	-2264	-816	0	668	1664	4.02	4.02	4.02	4.02	2	0.25	0.05	0.30	0.00	0.00	16.8
5	217	-438	-2128	-829	0	672	1764	4.02	4.02	4.02	4.02	2	0.26	0.05	0.29	0.00	0.00	16.8
6	217	-321	-2412	-485	0	348	1549	4.02	4.02	4.02	4.02	2	0.23	0.05	0.33	0.00	0.00	16.8
7	217	-426	-1954	-530	0	358	1880	4.02	4.02	4.02	4.02	2	0.28	0.04	0.26	0.00	0.00	16.8
8	217	-344	-2418	-631	0	495	1549	4.02	4.02	4.02	4.02	2	0.23	0.05	0.33	0.00	0.00	16.8
9	217	-449	-1960	-675	0	505	1880	4.02	4.02	4.02	4.02	2	0.28	0.04	0.26	0.00	0.00	16.8
10	217	-332	-2244	-331	0	181	1666	4.02	4.02	4.02	4.02	2	0.25	0.05	0.30	0.00	0.00	16.8
11	217	-363	-2107	-345	0	184	1765	4.02	4.02	4.02	4.02	2	0.26	0.05	0.28	0.00	0.00	16.8
12	217	-407	-2264	-816	0	668	1664	4.02	4.02	4.02	4.02	2	0.25	0.05	0.30	0.00	0.00	16.8
13	217	-438	-2128	-829	0	672	1764	4.02	4.02	4.02	4.02	2	0.26	0.05	0.29	0.00	0.00	16.8

14	217	-321	-2412	-485	0	348	1549	4.02	4.02	4.02	4.02	2	0.23	0.05	0.33	0.00	0.00	16.8
15	217	-426	-1954	-530	0	358	1880	4.02	4.02	4.02	4.02	2	0.28	0.04	0.26	0.00	0.00	16.8
16	217	-344	-2418	-631	0	495	1549	4.02	4.02	4.02	4.02	2	0.23	0.05	0.33	0.00	0.00	16.8
17	217	-449	-1960	-675	0	505	1880	4.02	4.02	4.02	4.02	2	0.28	0.04	0.26	0.00	0.00	16.8
18	217	-231	-3225	-904	0	478	2296	4.02	4.02	4.02	4.02	3	0.32	0.07	0.44	0.00	0.00	16.8
19	217	-505	-3319	-2200	0	1886	2279	4.02	4.02	4.02	4.02	3	0.33	0.07	0.45	0.00	0.00	16.8
20	217	-316	-3215	-1528	0	1148	2424	4.02	4.02	4.02	4.02	3	0.34	0.07	0.43	0.00	0.00	16.8
37	217	-173	-2995	-213	0	-194	2242	4.02	4.02	4.02	4.02	3	0.31	0.07	0.40	0.00	0.00	16.8
38	217	-630	-3152	-2372	0	2152	2215	4.02	4.02	4.02	4.02	3	0.37	0.07	0.42	0.00	0.00	16.8
39	217	-314	-2978	-1253	0	921	2456	4.02	4.02	4.02	4.02	3	0.34	0.06	0.40	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	248	-501	-4101	-754	0	788	2229	4.02	4.02	4.02	4.02	3	0.31	0.09	0.55	0.00	0.00	16.8
2	248	-332	-3213	-331	0	284	1656	4.02	4.02	4.02	4.02	2	0.25	0.07	0.43	0.00	0.00	16.8
3	248	-363	-3076	-345	0	291	1765	4.02	4.02	4.02	4.02	2	0.26	0.07	0.41	0.00	0.00	16.8
4	248	-407	-3234	-816	0	921	1646	4.02	4.02	4.02	4.02	2	0.24	0.07	0.44	0.00	0.00	16.8
5	248	-438	-3097	-829	0	929	1764	4.02	4.02	4.02	4.02	2	0.26	0.07	0.42	0.00	0.00	16.8
6	248	-321	-3381	-485	0	499	-1955	4.02	4.02	4.02	4.02	2	0.29	0.07	0.46	0.00	0.00	16.8
7	248	-426	-2924	-530	0	523	1880	4.02	4.02	4.02	4.02	2	0.28	0.06	0.39	0.00	0.00	16.8
8	248	-344	-3387	-631	0	690	-1963	4.02	4.02	4.02	4.02	2	0.29	0.07	0.46	0.00	0.00	16.8
9	248	-449	-2930	-675	0	714	1880	4.02	4.02	4.02	4.02	2	0.28	0.06	0.39	0.00	0.00	16.8
10	248	-332	-3213	-331	0	284	1656	4.02	4.02	4.02	4.02	2	0.25	0.07	0.43	0.00	0.00	16.8
11	248	-363	-3076	-345	0	291	1765	4.02	4.02	4.02	4.02	2	0.26	0.07	0.41	0.00	0.00	16.8
12	248	-407	-3234	-816	0	921	1646	4.02	4.02	4.02	4.02	2	0.24	0.07	0.44	0.00	0.00	16.8
13	248	-438	-3097	-829	0	929	1764	4.02	4.02	4.02	4.02	2	0.26	0.07	0.42	0.00	0.00	16.8
14	248	-321	-3381	-485	0	499	-1955	4.02	4.02	4.02	4.02	2	0.29	0.07	0.46	0.00	0.00	16.8
15	248	-426	-2924	-530	0	523	1880	4.02	4.02	4.02	4.02	2	0.28	0.06	0.39	0.00	0.00	16.8
16	248	-344	-3387	-631	0	690	-1963	4.02	4.02	4.02	4.02	2	0.29	0.07	0.46	0.00	0.00	16.8
17	248	-449	-2930	-675	0	714	1880	4.02	4.02	4.02	4.02	2	0.28	0.06	0.39	0.00	0.00	16.8
18	248	-231	-4617	-904	0	759	-2393	4.02	4.02	4.02	4.02	3	0.33	0.10	0.62	0.00	0.00	16.8
19	248	-505	-4711	-2200	0	2568	-2545	4.02	4.02	4.02	4.02	3	0.45	0.10	0.63	0.00	0.00	16.8
20	248	-316	-4607	-1528	0	1621	2413	4.02	4.02	4.02	4.02	3	0.34	0.10	0.62	0.00	0.00	16.8
37	248	-173	-4321	-213	0	-129	2242	4.02	4.02	4.02	4.02	3	0.31	0.09	0.58	0.00	0.00	16.8
38	248	-630	-4478	-2372	0	2887	-2367	4.02	4.02	4.02	4.02	3	0.50	0.10	0.60	0.00	0.00	16.8
39	248	-314	-4304	-1253	0	1309	2456	4.02	4.02	4.02	4.02	3	0.34	0.09	0.58	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	279	-501	-5362	-754	0	1022	-3152	4.02	4.02	4.02	4.02	3	0.44	0.12	0.72	0.00	0.00	16.8
2	279	-332	-4183	-331	0	387	-2564	4.02	4.02	4.02	4.02	2	0.38	0.09	0.56	0.00	0.00	16.8
3	279	-363	-4046	-345	0	398	-2252	4.02	4.02	4.02	4.02	2	0.33	0.09	0.54	0.00	0.00	16.8
4	279	-407	-4204	-816	0	1174	-2597	4.02	4.02	4.02	4.02	2	0.39	0.09	0.57	0.00	0.00	16.8
5	279	-438	-4067	-829	0	1186	-2285	4.02	4.02	4.02	4.02	2	0.34	0.09	0.55	0.00	0.00	16.8
6	279	-321	-4351	-485	0	649	-2940	4.02	4.02	4.02	4.02	2	0.44	0.09	0.59	0.00	0.00	16.8
7	279	-426	-3894	-530	0	687	-1900	4.02	4.02	4.02	4.02	2	0.28	0.08	0.52	0.00	0.00	16.8
8	279	-344	-4357	-631	0	886	-2949	4.02	4.02	4.02	4.02	2	0.44	0.09	0.59	0.00	0.00	16.8
9	279	-449	-3900	-675	0	924	-1910	4.02	4.02	4.02	4.02	2	0.28	0.08	0.52	0.00	0.00	16.8
10	279	-332	-4183	-331	0	387	-2564	4.02	4.02	4.02	4.02	2	0.38	0.09	0.56	0.00	0.00	16.8
11	279	-363	-4046	-345	0	398	-2252	4.02	4.02	4.02	4.02	2	0.33	0.09	0.54	0.00	0.00	16.8
12	279	-407	-4204	-816	0	1174	-2597	4.02	4.02	4.02	4.02	2	0.39	0.09	0.57	0.00	0.00	16.8
13	279	-438	-4067	-829	0	1186	-2285	4.02	4.02	4.02	4.02	2	0.34	0.09	0.55	0.00	0.00	16.8
14	279	-321	-4351	-485	0	649	-2940	4.02	4.02	4.02	4.02	2	0.44	0.09	0.59	0.00	0.00	16.8
15	279	-426	-3894	-530	0	687	-1900	4.02	4.02	4.02	4.02	2	0.28	0.08	0.52	0.00	0.00	16.8
16	279	-344	-4357	-631	0	886	-2949	4.02	4.02	4.02	4.02	2	0.44	0.09	0.59	0.00	0.00	16.8
17	279	-449	-3900	-675	0	924	-1910	4.02	4.02	4.02	4.02	2	0.28	0.08	0.52	0.00	0.00	16.8
18	279	-231	-6008	-904	0	1039	-3781	4.02	4.02	4.02	4.02	3	0.53	0.13	0.81	0.00	0.00	16.8
19	279	-505	-6102	-2200	0	3250	-3944	4.02	4.02	4.02	4.02	3	0.57	0.13	0.82	0.00	0.00	16.8
20	279	-316	-5998	-1528	0	2095	-3638	4.02	4.02	4.02	4.02	3	0.51	0.13	0.81	0.00	0.00	16.8
37	279	-173	-5647	-213	0	-63	-3427	4.02	4.02	4.02	4.02	3	0.48	0.12	0.76	0.00	0.00	16.8
38	279	-630	-5804	-2372	0	3623	-3698	4.02	4.02	4.02	4.02	3	0.63	0.13	0.78	0.00	0.00	16.8
39	279	-314	-5630	-1253	0	1698	-3188	4.02	4.02	4.02	4.02	3	0.44	0.12	0.76	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	310	-501	-6622	-754	0	1256	-3152	4.02	4.02	4.02	4.02	3	0.44	0.14	0.89	0.00	0.00	16.8
2	310	-332	-5152	-331	0	489	-2564	4.02	4.02	4.02	4.02	2	0.38	0.11	0.69	0.00	0.00	16.8
3	310	-363	-5015	-345	0	505	-2252	4.02	4.02	4.02	4.02	2	0.33	0.11	0.68	0.00	0.00	16.8
4	310	-407	-5173	-816	0	1427	-2597	4.02	4.02	4.02	4.02	2	0.39	0.11	0.70	0.00	0.00	16.8
5	310	-438	-5036	-829	0	1443	-2285	4.02	4.02	4.02	4.02	2	0.34	0.11	0.68	0.00	0.00	16.8
6	310	-321	-5320	-485	0	800	-2940	4.02	4.02	4.02	4.02	2	0.44	0.12	0.72	0.00	0.00	16.8
7	310	-426	-4863	-530	0	851	-1900	4.02	4.02	4.02	4.02	2	0.28	0.11	0.65	0.00	0.00	16.8
8	310	-344	-5326	-631	0	1081	-2949	4.02	4.02	4.02	4.02	2	0.44	0.12	0.72	0.00	0.00	16.8
9	310	-449	-4869	-675	0	1133	-1910	4.02	4.02	4.02	4.02	2	0.28	0.11	0.65	0.00	0.00	16.8
10	310	-332	-5152	-331	0	489	-2564	4.02	4.02	4.02	4.02	2	0.38	0.11	0.69	0.00	0.00	16.8
11	310	-363	-5015	-345	0	505	-2252	4.02	4.02	4.02	4.02	2	0.33	0.11	0.68	0.00	0.00	16.8
12	310	-407	-5173	-816	0	1427	-2597	4.02	4.02	4.02	4.02	2	0.39	0.11	0.70	0.00	0.00	16.8
13	310	-438	-5036	-829	0	1443	-2285	4.02	4.02	4.02	4.02	2	0.34	0.11	0.68	0.00	0.00	16.8
14	310	-321	-5320	-485	0	800	-2940	4.02	4.02	4.02	4.02	2	0.44	0.12	0.72	0.00	0.00	16.8
15	310	-426	-4863	-530	0	851	-1900	4.02	4.02	4.02	4.02	2	0.28	0.11	0.65	0.00	0.00	16.8
16	310	-344	-5326	-631	0	1081	-2949	4.02	4.02	4.02	4.02	2	0.44	0.12	0.72	0.00	0.00	16.8
17	310	-449	-4869	-675	0	1133	-1910	4.02	4.02	4.02	4.02	2	0.28	0.11	0.65	0.00	0.00	16.8
18	310	-231	-7400	-904	0	1319	-3781	4.02	4.02	4.02	4.02	3	0.53	0.16	1.00	0.00	0.00	16.8
19	310	-505	-7494	-2200	0	3932	-3944	4.02	4.02	4.02	4.02	3	0.68	0.16	1.01	1.86	0.00	16.8
20	310	-316	-7390	-1528	0	2568	-3638	4.02	4.02	4.02	4.02	3	0.51	0.16	1.00	0.00	0.00	16.8
37	310	-173	-6973	-213	0	3	-3427	4.02	4.02	4.02	4.02	3	0.48	0.15	0.94	0.00	0.00	16.8
38	310	-630	-7130	-2372	0	4358	-3698	4.02	4.02	4.02	4.02	3	0.76	0.15	0.96	0.00	0.00	16.8
39	310	-314	-6956	-1253	0	2086	-3188	4.02	4.02	4.02	4.02	3	0.44	0.15	0.94	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

Nome travata: **trave_506_IP1** Descrizione: **Trave_5 21-20-19-18**
ASTA NUM. 17 NI 298 NF 126 SEZ. Rp B= 0.400 H= 0.500 (trave)

categoria: p.p. y Permanente Neve qy tot.
qy medio: 500.00 2627.25 282.50 3409.75 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-1362	7227	-17	0	-12	-3726	4.02	4.02	4.02	4.02	3	0.50	0.16	0.96	0.00	0.00	16.8
2	0	-1084	5514	-145	0	-403	-2745	4.02	4.02	4.02	4.02	2	0.40	0.12	0.73	0.00	0.00	16.8
3	0	-953	5633	-146	0	-402	-3043	4.02	4.02	4.02	4.02	2	0.44	0.12	0.75	0.00	0.00	16.8
4	0	-1143	5485	119	0	383	-2688	4.02	4.02	4.02	4.02	2	0.39	0.12	0.73	0.00	0.00	16.8
5	0	-1011	5604	118	0	385	-2986	4.02	4.02	4.02	4.02	2	0.43	0.12	0.75	0.00	0.00	16.8

6	0	-1258	5365	-53	0	-129	-2378	4.02	4.02	4.02	4.02	2	0.34	0.12	0.71	0.00	0.00	16.8
7	0	-820	5762	-53	0	-125	-3371	4.02	4.02	4.02	4.02	2	0.49	0.13	0.77	0.00	0.00	16.8
8	0	-1276	5356	27	0	107	-2361	4.02	4.02	4.02	4.02	2	0.34	0.12	0.71	0.00	0.00	16.8
9	0	-837	5753	26	0	111	-3354	4.02	4.02	4.02	4.02	2	0.49	0.12	0.77	0.00	0.00	16.8
10	0	-1084	5514	-145	0	-403	-2745	4.02	4.02	4.02	4.02	2	0.40	0.12	0.73	0.00	0.00	16.8
11	0	-953	5633	-146	0	-402	-3043	4.02	4.02	4.02	4.02	2	0.44	0.12	0.75	0.00	0.00	16.8
12	0	-1143	5485	119	0	383	-2688	4.02	4.02	4.02	4.02	2	0.39	0.12	0.73	0.00	0.00	16.8
13	0	-1011	5604	118	0	385	-2986	4.02	4.02	4.02	4.02	2	0.43	0.12	0.75	0.00	0.00	16.8
14	0	-1258	5365	-53	0	-129	-2378	4.02	4.02	4.02	4.02	2	0.34	0.12	0.71	0.00	0.00	16.8
15	0	-820	5762	-53	0	-125	-3371	4.02	4.02	4.02	4.02	2	0.49	0.13	0.77	0.00	0.00	16.8
16	0	-1276	5356	27	0	107	-2361	4.02	4.02	4.02	4.02	2	0.34	0.12	0.71	0.00	0.00	16.8
17	0	-837	5753	26	0	111	-3354	4.02	4.02	4.02	4.02	2	0.49	0.12	0.77	0.00	0.00	16.8
18	0	-1544	7836	-412	0	-1138	-3696	4.02	4.02	4.02	4.02	3	0.50	0.17	1.03	1.94	0.00	16.8
19	0	-1799	7704	382	0	1179	-3425	4.02	4.02	4.02	4.02	3	0.46	0.17	1.01	1.91	0.00	16.8
20	0	-1841	7848	-40	0	-65	-3822	4.02	4.02	4.02	4.02	3	0.51	0.17	1.03	1.95	0.00	16.8
37	0	-1340	7560	-677	0	-1921	-3746	4.02	4.02	4.02	4.02	3	0.51	0.16	1.00	1.87	0.00	16.8
38	0	-1764	7340	645	0	1940	-3294	4.02	4.02	4.02	4.02	3	0.44	0.16	0.96	0.00	0.00	16.8
39	0	-1834	7580	-57	0	-133	-3957	4.02	4.02	4.02	4.02	3	0.53	0.16	0.99	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	38	-1362	5702	-17	0	-5	-3726	4.02	4.02	4.02	4.02	3	0.50	0.12	0.75	0.00	0.00	16.8
2	38	-1084	4341	-145	0	-349	-2745	4.02	4.02	4.02	4.02	2	0.40	0.09	0.58	0.00	0.00	16.8
3	38	-953	4460	-146	0	-347	-3043	4.02	4.02	4.02	4.02	2	0.44	0.10	0.59	0.00	0.00	16.8
4	38	-1143	4312	119	0	339	-2688	4.02	4.02	4.02	4.02	2	0.39	0.09	0.57	0.00	0.00	16.8
5	38	-1011	4431	118	0	340	-2986	4.02	4.02	4.02	4.02	2	0.43	0.10	0.59	0.00	0.00	16.8
6	38	-1258	4192	-53	0	-110	-2378	4.02	4.02	4.02	4.02	2	0.34	0.09	0.56	0.00	0.00	16.8
7	38	-820	4589	-53	0	-105	-3371	4.02	4.02	4.02	4.02	2	0.49	0.10	0.61	0.00	0.00	16.8
8	38	-1276	4183	27	0	97	-2361	4.02	4.02	4.02	4.02	2	0.34	0.09	0.55	0.00	0.00	16.8
9	38	-837	4580	26	0	101	-3354	4.02	4.02	4.02	4.02	2	0.49	0.10	0.61	0.00	0.00	16.8
10	38	-1084	4341	-145	0	-349	-2745	4.02	4.02	4.02	4.02	2	0.40	0.09	0.58	0.00	0.00	16.8
11	38	-953	4460	-146	0	-347	-3043	4.02	4.02	4.02	4.02	2	0.44	0.10	0.59	0.00	0.00	16.8
12	38	-1143	4312	119	0	339	-2688	4.02	4.02	4.02	4.02	2	0.39	0.09	0.57	0.00	0.00	16.8
13	38	-1011	4431	118	0	340	-2986	4.02	4.02	4.02	4.02	2	0.43	0.10	0.59	0.00	0.00	16.8
14	38	-1258	4192	-53	0	-110	-2378	4.02	4.02	4.02	4.02	2	0.34	0.09	0.56	0.00	0.00	16.8
15	38	-820	4589	-53	0	-105	-3371	4.02	4.02	4.02	4.02	2	0.49	0.10	0.61	0.00	0.00	16.8
16	38	-1276	4183	27	0	97	-2361	4.02	4.02	4.02	4.02	2	0.34	0.09	0.55	0.00	0.00	16.8
17	38	-837	4580	26	0	101	-3354	4.02	4.02	4.02	4.02	2	0.49	0.10	0.61	0.00	0.00	16.8
18	38	-1544	6153	-412	0	-984	-3696	4.02	4.02	4.02	4.02	3	0.50	0.13	0.81	0.00	0.00	16.8
19	38	-1799	6021	382	0	1036	-3425	4.02	4.02	4.02	4.02	3	0.46	0.13	0.79	0.00	0.00	16.8
20	38	-1841	6165	-40	0	-50	-3822	4.02	4.02	4.02	4.02	3	0.51	0.13	0.81	0.00	0.00	16.8
37	38	-1340	5956	-677	0	-1667	-3746	4.02	4.02	4.02	4.02	3	0.51	0.13	0.79	0.00	0.00	16.8
38	38	-1764	5736	645	0	1698	-3294	4.02	4.02	4.02	4.02	3	0.44	0.12	0.75	0.00	0.00	16.8
39	38	-1834	5976	-57	0	-112	-3957	4.02	4.02	4.02	4.02	3	0.53	0.13	0.78	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	75	-1362	4178	-17	0	1	2666	4.02	4.02	4.02	4.02	3	0.36	0.09	0.55	0.00	0.00	16.8
2	75	-1084	3169	-145	0	-294	2096	4.02	4.02	4.02	4.02	2	0.30	0.07	0.42	0.00	0.00	16.8
3	75	-953	3288	-146	0	-293	1966	4.02	4.02	4.02	4.02	2	0.29	0.07	0.44	0.00	0.00	16.8
4	75	-1143	3140	119	0	294	2099	4.02	4.02	4.02	4.02	2	0.30	0.07	0.42	0.00	0.00	16.8
5	75	-1011	3259	118	0	296	1987	4.02	4.02	4.02	4.02	2	0.29	0.07	0.43	0.00	0.00	16.8
6	75	-1258	3020	-53	0	-90	2184	4.02	4.02	4.02	4.02	2	0.32	0.07	0.40	0.00	0.00	16.8
7	75	-820	3416	-53	0	-85	1800	4.02	4.02	4.02	4.02	2	0.26	0.07	0.46	0.00	0.00	16.8
8	75	-1276	3011	27	0	87	2185	4.02	4.02	4.02	4.02	2	0.32	0.07	0.40	0.00	0.00	16.8
9	75	-837	3408	26	0	92	1806	4.02	4.02	4.02	4.02	2	0.26	0.07	0.45	0.00	0.00	16.8
10	75	-1084	3169	-145	0	-294	2096	4.02	4.02	4.02	4.02	2	0.30	0.07	0.42	0.00	0.00	16.8
11	75	-953	3288	-146	0	-293	1966	4.02	4.02	4.02	4.02	2	0.29	0.07	0.44	0.00	0.00	16.8
12	75	-1143	3140	119	0	294	2099	4.02	4.02	4.02	4.02	2	0.30	0.07	0.42	0.00	0.00	16.8
13	75	-1011	3259	118	0	296	1987	4.02	4.02	4.02	4.02	2	0.29	0.07	0.43	0.00	0.00	16.8
14	75	-1258	3020	-53	0	-90	2184	4.02	4.02	4.02	4.02	2	0.32	0.07	0.40	0.00	0.00	16.8
15	75	-820	3416	-53	0	-85	1800	4.02	4.02	4.02	4.02	2	0.26	0.07	0.46	0.00	0.00	16.8
16	75	-1276	3011	27	0	87	2185	4.02	4.02	4.02	4.02	2	0.32	0.07	0.40	0.00	0.00	16.8
17	75	-837	3408	26	0	92	1806	4.02	4.02	4.02	4.02	2	0.26	0.07	0.45	0.00	0.00	16.8
18	75	-1544	4469	-412	0	-829	3106	4.02	4.02	4.02	4.02	3	0.42	0.10	0.59	0.00	0.00	16.8
19	75	-1799	4337	382	0	893	3129	4.02	4.02	4.02	4.02	3	0.42	0.09	0.57	0.00	0.00	16.8
20	75	-1841	4481	-40	0	-35	3002	4.02	4.02	4.02	4.02	3	0.40	0.10	0.59	0.00	0.00	16.8
37	75	-1340	4352	-677	0	-1413	2911	4.02	4.02	4.02	4.02	3	0.39	0.09	0.58	0.00	0.00	16.8
38	75	-1764	4132	645	0	1456	2949	4.02	4.02	4.02	4.02	3	0.39	0.09	0.54	0.00	0.00	16.8
39	75	-1834	4372	-57	0	-90	2737	4.02	4.02	4.02	4.02	3	0.36	0.09	0.57	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	112	-1362	2653	-17	0	8	2678	4.02	4.02	4.02	4.02	3	0.36	0.06	0.35	0.00	0.00	16.8
2	112	-1084	1996	-145	0	-240	2096	4.02	4.02	4.02	4.02	2	0.30	0.04	0.27	0.00	0.00	16.8
3	112	-953	2115	-146	0	-238	2021	4.02	4.02	4.02	4.02	2	0.29	0.05	0.28	0.00	0.00	16.8
4	112	-1143	1967	119	0	250	2099	4.02	4.02	4.02	4.02	2	0.30	0.04	0.26	0.00	0.00	16.8
5	112	-1011	2086	118	0	251	2025	4.02	4.02	4.02	4.02	2	0.29	0.05	0.28	0.00	0.00	16.8
6	112	-1258	1847	-53	0	-70	2184	4.02	4.02	4.02	4.02	2	0.32	0.04	0.24	0.00	0.00	16.8
7	112	-820	2244	-53	0	-65	1935	4.02	4.02	4.02	4.02	2	0.28	0.05	0.30	0.00	0.00	16.8
8	112	-1276	1838	27	0	77	2185	4.02	4.02	4.02	4.02	2	0.32	0.04	0.24	0.00	0.00	16.8
9	112	-837	2235	26	0	82	1936	4.02	4.02	4.02	4.02	2	0.28	0.05	0.30	0.00	0.00	16.8
10	112	-1084	1996	-145	0	-240	2096	4.02	4.02	4.02	4.02	2	0.30	0.04	0.27	0.00	0.00	16.8
11	112	-953	2115	-146	0	-238	2021	4.02	4.02	4.02	4.02	2	0.29	0.05	0.28	0.00	0.00	16.8
12	112	-1143	1967	119	0	250	2099	4.02	4.02	4.02	4.02	2	0.30	0.04	0.26	0.00	0.00	16.8
13	112	-1011	2086	118	0	251	2025	4.02	4.02	4.02	4.02	2	0.29	0.05	0.28	0.00	0.00	16.8
14	112	-1258	1847	-53	0	-70	2184	4.02	4.02	4.02	4.02	2	0.32	0.04	0.24	0.00	0.00	16.8
15	112	-820	2244	-53	0	-65	1935	4.02	4.02	4.02	4.02	2	0.28	0.05	0.30	0.00	0.00	16.8
16	112	-1276	1838	27	0	77	2185	4.02	4.02	4.02	4.02	2	0.32	0.04	0.24	0.00	0.00	16.8
17	112	-837	2235	26	0	82	1936	4.02	4.02	4.02	4.02	2	0.28	0.05	0.30	0.00	0.00	16.8
18	112	-1544	2786	-412	0	-675	3106	4.02	4.02	4.02	4.02	3	0.42	0.06	0.37	0.00	0.00	16.8
19	112	-1799	2654	382	0	749	3129	4.02	4.02	4.02	4.02	3	0.42	0.06	0.35	0.00	0.00	16.8
20	112	-1841	2798	-40	0	-20	3002	4.02	4.02	4.02	4.02	3	0.40	0.06	0.37	0.00	0.00	16.8
37	112	-1340	2748	-677	0	-1159	2911	4.02	4.02	4.02	4.02	3	0.39	0.06	0.36	0.00	0.00	16.8
38	112	-1764	2528	645	0	1214	2949	4.02	4.02	4.02	4.02	3	0.39	0.05	0.33	0.00	0.00	16.8
39	112	-1834	2768	-57	0	-69	2737	4.02	4.02	4.02	4.02	3	0.36	0.06	0.36	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	150	-1362	1129	-17	0	14	2678	4.02	4.02	4.02	4.02	3	0.36	0.02	0.15	0.00	0.00	16.8
2	150	-1084	823	-145	0	-185	2096	4.02	4.02	4.02	4.02	2	0.30	0.02	0.11	0.00	0.00	16.8
3	150	-953	942	-146	0	-184	2021	4.02	4.02	4.02	4.02	2	0.29	0.02	0.13	0.00	0.00	16.8
4	150	-1143	794	119	0	205	2099	4.02	4.02	4.02	4.02	2	0.30	0.02	0.11	0.00	0.00	16.8
5	150	-1011	913	118	0	207	2025	4.02	4.02	4.02	4.02	2	0.29	0.02	0.12	0.00	0.00	16.8
6	150	-1258	674	-53	0	-50	2184	4.02	4.02	4.02	4.02	2	0.32	0.01	0.09	0.00	0.00	16.8
7	150	-820	1071	-53	0	-45	1935	4.02	4.02	4.02	4.02	2	0.28	0.02	0.14	0.00	0.00	16.8
8	150	-1276	665	27	0	67	2185	4.02	4.02	4.02	4.02	2	0.32	0.01	0.09	0.00	0.00	16.8
9	150	-837	1062	26	0	72	1936	4.02	4.02	4.02	4.02	2	0.28	0.02	0.14	0.00	0.00	16.8
10	150	-1084	823	-145	0	-185	2096	4.02	4.02	4.02	4.02	2	0.30	0.02	0.11	0.00	0.00	16.8
11	150	-953	942	-146	0	-184	2021	4.02	4.02	4.02	4.02	2	0.29	0.02	0.13	0.00	0.00	16.8

12	150	-1143	794	119	0	205	2099	4.02	4.02	4.02	4.02	2	0.30	0.02	0.11	0.00	0.00	16.8
13	150	-1011	913	118	0	207	2025	4.02	4.02	4.02	4.02	2	0.29	0.02	0.12	0.00	0.00	16.8
14	150	-1258	674	-53	0	-50	2184	4.02	4.02	4.02	4.02	2	0.32	0.01	0.09	0.00	0.00	16.8
15	150	-820	1071	-53	0	-45	1935	4.02	4.02	4.02	4.02	2	0.28	0.02	0.14	0.00	0.00	16.8
16	150	-1276	665	27	0	67	2185	4.02	4.02	4.02	4.02	2	0.32	0.01	0.09	0.00	0.00	16.8
17	150	-837	1062	26	0	72	1936	4.02	4.02	4.02	4.02	2	0.28	0.02	0.14	0.00	0.00	16.8
18	150	-1544	1102	-412	0	-520	3106	4.02	4.02	4.02	4.02	3	0.42	0.02	0.15	0.00	0.00	16.8
19	150	-1799	970	382	0	606	3129	4.02	4.02	4.02	4.02	3	0.42	0.02	0.13	0.00	0.00	16.8
20	150	-1841	1114	-40	0	-5	3002	4.02	4.02	4.02	4.02	3	0.40	0.02	0.15	0.00	0.00	16.8
37	150	-1340	1144	-677	0	-905	2911	4.02	4.02	4.02	4.02	3	0.39	0.02	0.15	0.00	0.00	16.8
38	150	-1764	924	645	0	972	2949	4.02	4.02	4.02	4.02	3	0.39	0.02	0.12	0.00	0.00	16.8
39	150	-1834	1164	-57	0	-47	2737	4.02	4.02	4.02	4.02	3	0.36	0.03	0.15	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	188	-1362	-396	-17	0	21	2678	4.02	4.02	4.02	4.02	3	0.36	0.01	0.05	0.00	0.00	16.8
2	188	-1084	-350	-145	0	-131	2096	4.02	4.02	4.02	4.02	2	0.30	0.01	0.05	0.00	0.00	16.8
3	188	-953	-230	-146	0	-129	2021	4.02	4.02	4.02	4.02	2	0.29	0.00	0.03	0.00	0.00	16.8
4	188	-1143	-378	119	0	161	2099	4.02	4.02	4.02	4.02	2	0.30	0.01	0.05	0.00	0.00	16.8
5	188	-1011	-260	118	0	163	2025	4.02	4.02	4.02	4.02	2	0.29	0.01	0.03	0.00	0.00	16.8
6	188	-1258	-498	-53	0	-31	2184	4.02	4.02	4.02	4.02	2	0.32	0.01	0.07	0.00	0.00	16.8
7	188	-820	-102	-53	0	-25	1935	4.02	4.02	4.02	4.02	2	0.28	0.00	0.01	0.00	0.00	16.8
8	188	-1276	-508	27	0	57	2185	4.02	4.02	4.02	4.02	2	0.32	0.01	0.07	0.00	0.00	16.8
9	188	-837	-110	26	0	63	1936	4.02	4.02	4.02	4.02	2	0.28	0.00	0.01	0.00	0.00	16.8
10	188	-1084	-350	-145	0	-131	2096	4.02	4.02	4.02	4.02	2	0.30	0.01	0.05	0.00	0.00	16.8
11	188	-953	-230	-146	0	-129	2021	4.02	4.02	4.02	4.02	2	0.29	0.00	0.03	0.00	0.00	16.8
12	188	-1143	-378	119	0	161	2099	4.02	4.02	4.02	4.02	2	0.30	0.01	0.05	0.00	0.00	16.8
13	188	-1011	-260	118	0	163	2025	4.02	4.02	4.02	4.02	2	0.29	0.01	0.03	0.00	0.00	16.8
14	188	-1258	-498	-53	0	-31	2184	4.02	4.02	4.02	4.02	2	0.32	0.01	0.07	0.00	0.00	16.8
15	188	-820	-102	-53	0	-25	1935	4.02	4.02	4.02	4.02	2	0.28	0.00	0.01	0.00	0.00	16.8
16	188	-1276	-508	27	0	57	2185	4.02	4.02	4.02	4.02	2	0.32	0.01	0.07	0.00	0.00	16.8
17	188	-837	-110	26	0	63	1936	4.02	4.02	4.02	4.02	2	0.28	0.00	0.01	0.00	0.00	16.8
18	188	-1544	-581	-412	0	-366	3106	4.02	4.02	4.02	4.02	3	0.42	0.01	0.08	0.00	0.00	16.8
19	188	-1799	-713	382	0	463	3129	4.02	4.02	4.02	4.02	3	0.42	0.02	0.09	0.00	0.00	16.8
20	188	-1841	-569	-40	0	10	3002	4.02	4.02	4.02	4.02	3	0.40	0.01	0.07	0.00	0.00	16.8
37	188	-1340	-460	-677	0	-651	2911	4.02	4.02	4.02	4.02	3	0.39	0.02	0.09	0.00	0.00	16.8
38	188	-1764	-680	645	0	730	2949	4.02	4.02	4.02	4.02	3	0.39	0.01	0.09	0.00	0.00	16.8
39	188	-1834	-440	-57	0	-26	2737	4.02	4.02	4.02	4.02	3	0.36	0.01	0.06	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	225	-1362	-1921	-17	0	27	2678	4.02	4.02	4.02	4.02	3	0.36	0.04	0.25	0.00	0.00	16.8
2	225	-1084	-1522	-145	0	-76	2096	4.02	4.02	4.02	4.02	2	0.30	0.03	0.20	0.00	0.00	16.8
3	225	-953	-1403	-146	0	-74	2021	4.02	4.02	4.02	4.02	2	0.29	0.03	0.19	0.00	0.00	16.8
4	225	-1143	-1551	119	0	116	2099	4.02	4.02	4.02	4.02	2	0.30	0.03	0.21	0.00	0.00	16.8
5	225	-1011	-1432	118	0	118	2025	4.02	4.02	4.02	4.02	2	0.29	0.03	0.19	0.00	0.00	16.8
6	225	-1258	-1671	-53	0	-11	2184	4.02	4.02	4.02	4.02	2	0.32	0.04	0.22	0.00	0.00	16.8
7	225	-820	-1275	-53	0	-5	1935	4.02	4.02	4.02	4.02	2	0.28	0.03	0.17	0.00	0.00	16.8
8	225	-1276	-1680	27	0	47	2185	4.02	4.02	4.02	4.02	2	0.32	0.04	0.22	0.00	0.00	16.8
9	225	-837	-1283	26	0	53	1936	4.02	4.02	4.02	4.02	2	0.28	0.03	0.17	0.00	0.00	16.8
10	225	-1084	-1522	-145	0	-76	2096	4.02	4.02	4.02	4.02	2	0.30	0.03	0.20	0.00	0.00	16.8
11	225	-953	-1403	-146	0	-74	2021	4.02	4.02	4.02	4.02	2	0.29	0.03	0.19	0.00	0.00	16.8
12	225	-1143	-1551	119	0	116	2099	4.02	4.02	4.02	4.02	2	0.30	0.03	0.21	0.00	0.00	16.8
13	225	-1011	-1432	118	0	118	2025	4.02	4.02	4.02	4.02	2	0.29	0.03	0.19	0.00	0.00	16.8
14	225	-1258	-1671	-53	0	-11	2184	4.02	4.02	4.02	4.02	2	0.32	0.04	0.22	0.00	0.00	16.8
15	225	-820	-1275	-53	0	-5	1935	4.02	4.02	4.02	4.02	2	0.28	0.03	0.17	0.00	0.00	16.8
16	225	-1276	-1680	27	0	47	2185	4.02	4.02	4.02	4.02	2	0.32	0.04	0.22	0.00	0.00	16.8
17	225	-837	-1283	26	0	53	1936	4.02	4.02	4.02	4.02	2	0.28	0.03	0.17	0.00	0.00	16.8
18	225	-1544	-2264	-412	0	-211	3106	4.02	4.02	4.02	4.02	3	0.42	0.05	0.30	0.00	0.00	16.8
19	225	-1799	-2396	382	0	320	3129	4.02	4.02	4.02	4.02	3	0.42	0.05	0.31	0.00	0.00	16.8
20	225	-1841	-2252	-40	0	25	3002	4.02	4.02	4.02	4.02	3	0.40	0.05	0.30	0.00	0.00	16.8
37	225	-1340	-2064	-677	0	-398	2911	4.02	4.02	4.02	4.02	3	0.39	0.04	0.27	0.00	0.00	16.8
38	225	-1764	-2284	645	0	488	2949	4.02	4.02	4.02	4.02	3	0.39	0.05	0.30	0.00	0.00	16.8
39	225	-1834	-2044	-57	0	-4	2737	4.02	4.02	4.02	4.02	3	0.36	0.04	0.27	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	262	-1362	-3445	-17	0	34	2678	4.02	4.02	4.02	4.02	3	0.36	0.07	0.46	0.00	0.00	16.8
2	262	-1084	-2695	-145	0	-22	2096	4.02	4.02	4.02	4.02	2	0.30	0.06	0.36	0.00	0.00	16.8
3	262	-953	-2576	-146	0	-20	2021	4.02	4.02	4.02	4.02	2	0.29	0.06	0.34	0.00	0.00	16.8
4	262	-1143	-2724	119	0	72	2099	4.02	4.02	4.02	4.02	2	0.30	0.06	0.36	0.00	0.00	16.8
5	262	-1011	-2605	118	0	74	2025	4.02	4.02	4.02	4.02	2	0.29	0.06	0.35	0.00	0.00	16.8
6	262	-1258	-2844	-53	0	9	2184	4.02	4.02	4.02	4.02	2	0.32	0.06	0.38	0.00	0.00	16.8
7	262	-820	-2448	-53	0	15	1935	4.02	4.02	4.02	4.02	2	0.28	0.05	0.33	0.00	0.00	16.8
8	262	-1276	-2853	27	0	37	2185	4.02	4.02	4.02	4.02	2	0.32	0.06	0.38	0.00	0.00	16.8
9	262	-837	-2456	26	0	43	1936	4.02	4.02	4.02	4.02	2	0.28	0.05	0.33	0.00	0.00	16.8
10	262	-1084	-2695	-145	0	-22	2096	4.02	4.02	4.02	4.02	2	0.30	0.06	0.36	0.00	0.00	16.8
11	262	-953	-2576	-146	0	-20	2021	4.02	4.02	4.02	4.02	2	0.29	0.06	0.34	0.00	0.00	16.8
12	262	-1143	-2724	119	0	72	2099	4.02	4.02	4.02	4.02	2	0.30	0.06	0.36	0.00	0.00	16.8
13	262	-1011	-2605	118	0	74	2025	4.02	4.02	4.02	4.02	2	0.29	0.06	0.35	0.00	0.00	16.8
14	262	-1258	-2844	-53	0	9	2184	4.02	4.02	4.02	4.02	2	0.32	0.06	0.38	0.00	0.00	16.8
15	262	-820	-2448	-53	0	15	1935	4.02	4.02	4.02	4.02	2	0.28	0.05	0.33	0.00	0.00	16.8
16	262	-1276	-2853	27	0	37	2185	4.02	4.02	4.02	4.02	2	0.32	0.06	0.38	0.00	0.00	16.8
17	262	-837	-2456	26	0	43	1936	4.02	4.02	4.02	4.02	2	0.28	0.05	0.33	0.00	0.00	16.8
18	262	-1544	-3948	-412	0	-57	3106	4.02	4.02	4.02	4.02	3	0.42	0.09	0.52	0.00	0.00	16.8
19	262	-1799	-4080	382	0	177	3129	4.02	4.02	4.02	4.02	3	0.42	0.09	0.54	0.00	0.00	16.8
20	262	-1841	-3936	-40	0	40	3002	4.02	4.02	4.02	4.02	3	0.40	0.09	0.52	0.00	0.00	16.8
37	262	-1340	-3668	-677	0	-144	2911	4.02	4.02	4.02	4.02	3	0.39	0.08	0.49	0.00	0.00	16.8
38	262	-1764	-3888	645	0	246	2949	4.02	4.02	4.02	4.02	3	0.39	0.08	0.51	0.00	0.00	16.8
39	262	-1834	-3648	-57	0	17	2737	4.02	4.02	4.02	4.02	3	0.36	0.08	0.48	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	300	-1362	-4970	-17	0	40	-2856	4.02	4.02	4.02	4.02	3	0.39	0.11	0.66	0.00	0.00	16.8
2	300	-1084	-3868	-145	0	33	-2235	4.02	4.02	4.02	4.02	2	0.32	0.08	0.51	0.00	0.00	16.8
3	300	-953	-3749	-146	0	35	-2115	4.02	4.02	4.02	4.02	2	0.31	0.08	0.50	0.00	0.00	16.8
4	300	-1143	-3897	119	0	28	-2278	4.02	4.02	4.02	4.02	2	0.33	0.08	0.52	0.00	0.00	16.8
5	300	-1011	-3778	118	0	30	-2159	4.02	4.02	4.02	4.02	2	0.31	0.08	0.50	0.00	0.00	16.8
6	300	-1258	-4017	-53	0	28	-2390	4.02	4.02	4.02	4.02	2	0.35	0.09	0.53	0.00	0.00	16.8
7	300	-820	-3620	-53	0	35	-1991	4.02	4.02	4.02	4.02	2	0.29	0.08	0.48	0.00	0.00	16.8
8	300	-1276	-4026	27	0	27	-2403	4.02	4.02	4.02	4.02	2	0.35	0.09	0.53	0.00	0.00	16.8
9	300	-837	-3629	26	0	34	-2004	4.02	4.02	4.02	4.02	2	0.29	0.08	0.48	0.00	0.00	16.8
10	300	-1084	-3868	-145	0	33	-2235	4.02	4.02	4.02	4.02	2	0.32	0.08	0.51	0.00	0.00	16.8
11	300	-953	-3749	-146	0	35	-2115	4.02	4.02	4.02	4.02	2	0.31	0.08	0.50	0.00	0.00	16.8
12	300	-1143	-3897	119	0	28	-2278	4.02	4.02	4.02	4.02	2	0.33	0.08	0.52	0.00	0.00	16.8
13	300	-1011	-3778	118	0	30	-2159	4.02	4.02	4.02	4.02	2	0.31	0.08	0.50	0.00	0.00	16.8
14	300	-1258	-4017	-53	0	28	-2390	4.02	4.02	4.02	4.02	2	0.35	0.09	0.53	0.00	0.00	16.8
15	300	-820	-3620	-53	0	35	-1991	4.02	4.02	4.02	4.02	2	0.29	0.08	0.48	0.00	0.00	16.8
16	300	-1276	-4026	27	0	27	-2403	4.02	4.02	4.02	4.02	2	0.35	0.09	0.53	0.00	0.00	16.8
17	300	-837	-3629	26	0	34	-2004	4.02	4.02	4.02	4.02	2	0.29	0.08	0.48	0.00	0.00	16.8

18	300	-1544	-5631	-412	0	98	-3240	4.02	4.02	4.02	4.02	3	0.43	0.12	0.74	0.00	0.00	16.8
19	300	-1799	-5763	382	0	34	-3431	4.02	4.02	4.02	4.02	3	0.46	0.12	0.76	0.00	0.00	16.8
20	300	-1841	-5619	-40	0	55	-3324	4.02	4.02	4.02	4.02	3	0.44	0.12	0.74	0.00	0.00	16.8
37	300	-1340	-5272	-677	0	110	-2982	4.02	4.02	4.02	4.02	3	0.40	0.11	0.70	0.00	0.00	16.8
38	300	-1764	-5492	645	0	4	-3303	4.02	4.02	4.02	4.02	3	0.44	0.12	0.72	0.00	0.00	16.8
39	300	-1834	-5252	-57	0	39	-3123	4.02	4.02	4.02	4.02	3	0.42	0.11	0.69	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	338	-1362	-6494	-17	0	47	-5211	4.02	4.02	4.02	4.02	3	0.70	0.14	0.86	0.00	0.00	16.8
2	338	-1084	-5040	-145	0	87	-4058	4.02	4.02	4.02	4.02	2	0.59	0.11	0.67	0.00	0.00	16.8
3	338	-953	-4921	-146	0	89	-3909	4.02	4.02	4.02	4.02	2	0.57	0.11	0.66	0.00	0.00	16.8
4	338	-1143	-5069	119	0	-17	-4108	4.02	4.02	4.02	4.02	2	0.60	0.11	0.67	0.00	0.00	16.8
5	338	-1011	-4950	118	0	-15	-3959	4.02	4.02	4.02	4.02	2	0.58	0.11	0.66	0.00	0.00	16.8
6	338	-1258	-5189	-53	0	48	-4249	4.02	4.02	4.02	4.02	2	0.61	0.11	0.69	0.00	0.00	16.8
7	338	-820	-4793	-53	0	55	-3753	4.02	4.02	4.02	4.02	2	0.55	0.10	0.64	0.00	0.00	16.8
8	338	-1276	-5198	27	0	17	-4264	4.02	4.02	4.02	4.02	2	0.62	0.11	0.69	0.00	0.00	16.8
9	338	-837	-4801	26	0	24	-3768	4.02	4.02	4.02	4.02	2	0.55	0.10	0.64	0.00	0.00	16.8
10	338	-1084	-5040	-145	0	87	-4058	4.02	4.02	4.02	4.02	2	0.59	0.11	0.67	0.00	0.00	16.8
11	338	-953	-4921	-146	0	89	-3909	4.02	4.02	4.02	4.02	2	0.57	0.11	0.66	0.00	0.00	16.8
12	338	-1143	-5069	119	0	-17	-4108	4.02	4.02	4.02	4.02	2	0.60	0.11	0.67	0.00	0.00	16.8
13	338	-1011	-4950	118	0	-15	-3959	4.02	4.02	4.02	4.02	2	0.58	0.11	0.66	0.00	0.00	16.8
14	338	-1258	-5189	-53	0	48	-4249	4.02	4.02	4.02	4.02	2	0.61	0.11	0.69	0.00	0.00	16.8
15	338	-820	-4793	-53	0	55	-3753	4.02	4.02	4.02	4.02	2	0.55	0.10	0.64	0.00	0.00	16.8
16	338	-1276	-5198	27	0	17	-4264	4.02	4.02	4.02	4.02	2	0.62	0.11	0.69	0.00	0.00	16.8
17	338	-837	-4801	26	0	24	-3768	4.02	4.02	4.02	4.02	2	0.55	0.10	0.64	0.00	0.00	16.8
18	338	-1544	-7315	-412	0	252	-5875	4.02	4.02	4.02	4.02	3	0.79	0.16	0.96	0.00	0.00	16.8
19	338	-1799	-7447	382	0	-110	-6099	4.02	4.02	4.02	4.02	3	0.81	0.16	0.98	0.00	0.00	16.8
20	338	-1841	-7303	-40	0	70	-5956	4.02	4.02	4.02	4.02	3	0.79	0.16	0.96	0.00	0.00	16.8
37	338	-1340	-6876	-677	0	364	-5470	4.02	4.02	4.02	4.02	3	0.74	0.15	0.91	0.00	0.00	16.8
38	338	-1764	-7096	645	0	-238	-5845	4.02	4.02	4.02	4.02	3	0.78	0.15	0.93	0.00	0.00	16.8
39	338	-1834	-6856	-57	0	60	-5606	4.02	4.02	4.02	4.02	3	0.75	0.15	0.90	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	375	-1362	-8019	-17	0	54	-5211	4.02	4.02	4.02	4.02	3	0.70	0.17	1.06	1.99	0.00	16.8
2	375	-1084	-6213	-145	0	142	-4058	4.02	4.02	4.02	4.02	2	0.59	0.13	0.83	0.00	0.00	16.8
3	375	-953	-6094	-146	0	144	-3909	4.02	4.02	4.02	4.02	2	0.57	0.13	0.81	0.00	0.00	16.8
4	375	-1143	-6242	119	0	-61	-4108	4.02	4.02	4.02	4.02	2	0.60	0.14	0.83	0.00	0.00	16.8
5	375	-1011	-6123	118	0	-59	-3959	4.02	4.02	4.02	4.02	2	0.58	0.13	0.81	0.00	0.00	16.8
6	375	-1258	-6362	-53	0	68	-4249	4.02	4.02	4.02	4.02	2	0.61	0.14	0.84	0.00	0.00	16.8
7	375	-820	-5966	-53	0	75	-3753	4.02	4.02	4.02	4.02	2	0.55	0.13	0.80	0.00	0.00	16.8
8	375	-1276	-6371	27	0	7	-4264	4.02	4.02	4.02	4.02	2	0.62	0.14	0.84	0.00	0.00	16.8
9	375	-837	-5974	26	0	14	-3768	4.02	4.02	4.02	4.02	2	0.55	0.13	0.80	0.00	0.00	16.8
10	375	-1084	-6213	-145	0	142	-4058	4.02	4.02	4.02	4.02	2	0.59	0.13	0.83	0.00	0.00	16.8
11	375	-953	-6094	-146	0	144	-3909	4.02	4.02	4.02	4.02	2	0.57	0.13	0.81	0.00	0.00	16.8
12	375	-1143	-6242	119	0	-61	-4108	4.02	4.02	4.02	4.02	2	0.60	0.14	0.83	0.00	0.00	16.8
13	375	-1011	-6123	118	0	-59	-3959	4.02	4.02	4.02	4.02	2	0.58	0.13	0.81	0.00	0.00	16.8
14	375	-1258	-6362	-53	0	68	-4249	4.02	4.02	4.02	4.02	2	0.61	0.14	0.84	0.00	0.00	16.8
15	375	-820	-5966	-53	0	75	-3753	4.02	4.02	4.02	4.02	2	0.55	0.13	0.80	0.00	0.00	16.8
16	375	-1276	-6371	27	0	7	-4264	4.02	4.02	4.02	4.02	2	0.62	0.14	0.84	0.00	0.00	16.8
17	375	-837	-5974	26	0	14	-3768	4.02	4.02	4.02	4.02	2	0.55	0.13	0.80	0.00	0.00	16.8
18	375	-1544	-8998	-412	0	406	-5875	4.02	4.02	4.02	4.02	3	0.79	0.19	1.19	2.23	0.00	16.8
19	375	-1799	-9130	382	0	-253	-6099	4.02	4.02	4.02	4.02	3	0.81	0.20	1.20	2.26	0.00	16.8
20	375	-1841	-8986	-40	0	85	-5956	4.02	4.02	4.02	4.02	3	0.79	0.19	1.18	2.23	0.00	16.8
37	375	-1340	-8480	-677	0	618	-5470	4.02	4.02	4.02	4.02	3	0.74	0.18	1.12	2.10	0.00	16.8
38	375	-1764	-8700	645	0	-481	-5845	4.02	4.02	4.02	4.02	3	0.78	0.19	1.14	2.16	0.00	16.8
39	375	-1834	-8460	-57	0	82	-5606	4.02	4.02	4.02	4.02	3	0.75	0.18	1.11	2.10	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

Nome travata: **trave_506_IP1** Descrizione: **Trave_5 21-20-19-18**
ASTA NUM. 18 NI 126 NF 123 SEZ. Rp B= 0.400 H= 0.500 (trave)

categoria: p.p. y Permanente Neve qy tot.
qy medio: 500.00 2627.25 282.50 3409.75 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-1178	7951	-7	0	13	-4809	4.02	4.02	4.02	4.02	3	0.65	0.17	1.06	1.97	0.00	16.8
2	0	-916	6102	-67	0	-20	-3682	4.02	4.02	4.02	4.02	2	0.54	0.13	0.81	0.00	0.00	16.8
3	0	-867	6142	-68	0	-17	-3735	4.02	4.02	4.02	4.02	2	0.55	0.13	0.82	0.00	0.00	16.8
4	0	-945	6090	58	0	37	-3663	4.02	4.02	4.02	4.02	2	0.53	0.13	0.81	0.00	0.00	16.8
5	0	-896	6129	56	0	39	-3716	4.02	4.02	4.02	4.02	2	0.54	0.13	0.82	0.00	0.00	16.8
6	0	-984	6051	-22	0	-3	-3614	4.02	4.02	4.02	4.02	2	0.53	0.13	0.81	0.00	0.00	16.8
7	0	-820	6184	-26	0	5	-3789	4.02	4.02	4.02	4.02	2	0.56	0.13	0.83	0.00	0.00	16.8
8	0	-992	6047	16	0	14	-3609	4.02	4.02	4.02	4.02	2	0.53	0.13	0.81	0.00	0.00	16.8
9	0	-828	6181	11	0	22	-3784	4.02	4.02	4.02	4.02	2	0.55	0.13	0.83	0.00	0.00	16.8
10	0	-916	6102	-67	0	-20	-3682	4.02	4.02	4.02	4.02	2	0.54	0.13	0.81	0.00	0.00	16.8
11	0	-867	6142	-68	0	-17	-3735	4.02	4.02	4.02	4.02	2	0.55	0.13	0.82	0.00	0.00	16.8
12	0	-945	6090	58	0	37	-3663	4.02	4.02	4.02	4.02	2	0.53	0.13	0.81	0.00	0.00	16.8
13	0	-896	6129	56	0	39	-3716	4.02	4.02	4.02	4.02	2	0.54	0.13	0.82	0.00	0.00	16.8
14	0	-984	6051	-22	0	-3	-3614	4.02	4.02	4.02	4.02	2	0.53	0.13	0.81	0.00	0.00	16.8
15	0	-820	6184	-26	0	5	-3789	4.02	4.02	4.02	4.02	2	0.56	0.13	0.83	0.00	0.00	16.8
16	0	-992	6047	16	0	14	-3609	4.02	4.02	4.02	4.02	2	0.53	0.13	0.81	0.00	0.00	16.8
17	0	-828	6181	11	0	22	-3784	4.02	4.02	4.02	4.02	2	0.55	0.13	0.83	0.00	0.00	16.8
18	0	-1290	8750	-184	0	-41	-5284	4.02	4.02	4.02	4.02	3	0.71	0.19	1.16	2.17	0.00	16.8
19	0	-1415	8697	177	0	90	-5208	4.02	4.02	4.02	4.02	3	0.70	0.19	1.15	2.16	0.00	16.8
20	0	-1458	8650	-27	0	22	-5100	4.02	4.02	4.02	4.02	3	0.69	0.19	1.14	2.15	0.00	16.8
37	0	-1170	8373	-306	0	-89	-5083	4.02	4.02	4.02	4.02	3	0.69	0.18	1.11	2.08	0.00	16.8
38	0	-1379	8284	296	0	130	-4956	4.02	4.02	4.02	4.02	3	0.67	0.18	1.10	2.05	0.00	16.8
39	0	-1450	8205	-43	0	15	-4776	4.02	4.02	4.02	4.02	3	0.64	0.18	1.08	2.03	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	38	-1178	6426	-7	0	15	-4809	4.02	4.02	4.02	4.02	3	0.65	0.14	0.85	0.00	0.00	16.8
2	38	-916	4929	-67	0	5	-3682	4.02	4.02	4.02	4.02	2	0.54	0.11	0.66	0.00	0.00	16.8
3	38	-867	4969	-68	0	8	-3735	4.02	4.02	4.02	4.02	2	0.55	0.11	0.66	0.00	0.00	16.8
4	38	-945	4917	58	0	15	-3663	4.02	4.02	4.02	4.02	2	0.53	0.11	0.66	0.00	0.00	16.8
5	38	-896	4956	56	0	18	-3716	4.02	4.02	4.02	4.02	2	0.54	0.11	0.66	0.00	0.00	16.8
6	38	-984	4878	-22	0	6	-3614	4.02	4.02	4.02	4.02	2	0.53	0.11	0.65	0.00	0.00	16.8
7	38	-820	5011	-26	0	15	-3789	4.02	4.02	4.02	4.02	2	0.56	0.11	0.67	0.00	0.00	16.8
8	38	-992	4874	16	0	8	-3609	4.02	4.02	4.02	4.02	2	0.53	0.11	0.65	0.00	0.00	16.8
9	38	-828	5008	11	0	18	-3784	4.02	4.02	4.02	4.02	2	0.55	0.11	0.67	0.00	0.00	16.8

10	38	-916	4929	-67	0	5	-3682	4.02	4.02	4.02	4.02	2	0.54	0.11	0.66	0.00	0.00	16.8
11	38	-867	4969	-68	0	8	-3735	4.02	4.02	4.02	4.02	2	0.55	0.11	0.66	0.00	0.00	16.8
12	38	-945	4917	58	0	15	-3663	4.02	4.02	4.02	4.02	2	0.53	0.11	0.66	0.00	0.00	16.8
13	38	-896	4956	56	0	18	-3716	4.02	4.02	4.02	4.02	2	0.54	0.11	0.66	0.00	0.00	16.8
14	38	-984	4878	-22	0	6	-3614	4.02	4.02	4.02	4.02	2	0.53	0.11	0.65	0.00	0.00	16.8
15	38	-820	5011	-26	0	15	-3789	4.02	4.02	4.02	4.02	2	0.56	0.11	0.67	0.00	0.00	16.8
16	38	-992	4874	16	0	8	-3609	4.02	4.02	4.02	4.02	2	0.53	0.11	0.65	0.00	0.00	16.8
17	38	-828	5008	11	0	18	-3784	4.02	4.02	4.02	4.02	2	0.55	0.11	0.67	0.00	0.00	16.8
18	38	-1290	7067	-184	0	28	-5284	4.02	4.02	4.02	4.02	3	0.71	0.15	0.94	0.00	0.00	16.8
19	38	-1415	7014	177	0	24	-5208	4.02	4.02	4.02	4.02	3	0.70	0.15	0.93	0.00	0.00	16.8
20	38	-1458	6967	-27	0	32	-5100	4.02	4.02	4.02	4.02	3	0.69	0.15	0.92	0.00	0.00	16.8
37	38	-1170	6769	-306	0	26	-5083	4.02	4.02	4.02	4.02	3	0.69	0.15	0.90	0.00	0.00	16.8
38	38	-1379	6680	296	0	19	-4956	4.02	4.02	4.02	4.02	3	0.67	0.14	0.88	0.00	0.00	16.8
39	38	-1450	6601	-43	0	31	-4776	4.02	4.02	4.02	4.02	3	0.64	0.14	0.87	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	75	-1178	4902	-7	0	18	2492	4.02	4.02	4.02	4.02	3	0.34	0.11	0.65	0.00	0.00	16.8
2	75	-916	3757	-67	0	31	1917	4.02	4.02	4.02	4.02	2	0.28	0.08	0.50	0.00	0.00	16.8
3	75	-867	3797	-68	0	34	-1930	4.02	4.02	4.02	4.02	2	0.28	0.08	0.51	0.00	0.00	16.8
4	75	-945	3744	58	0	-6	1920	4.02	4.02	4.02	4.02	2	0.28	0.08	0.50	0.00	0.00	16.8
5	75	-896	3784	56	0	-3	1917	4.02	4.02	4.02	4.02	2	0.28	0.08	0.50	0.00	0.00	16.8
6	75	-984	3706	-22	0	14	1921	4.02	4.02	4.02	4.02	2	0.28	0.08	0.49	0.00	0.00	16.8
7	75	-820	3839	-26	0	25	-1974	4.02	4.02	4.02	4.02	2	0.29	0.08	0.51	0.00	0.00	16.8
8	75	-992	3702	16	0	3	1921	4.02	4.02	4.02	4.02	2	0.28	0.08	0.49	0.00	0.00	16.8
9	75	-828	3835	11	0	14	-1970	4.02	4.02	4.02	4.02	2	0.29	0.08	0.51	0.00	0.00	16.8
10	75	-916	3757	-67	0	31	1917	4.02	4.02	4.02	4.02	2	0.28	0.08	0.50	0.00	0.00	16.8
11	75	-867	3797	-68	0	34	-1930	4.02	4.02	4.02	4.02	2	0.28	0.08	0.51	0.00	0.00	16.8
12	75	-945	3744	58	0	-6	1920	4.02	4.02	4.02	4.02	2	0.28	0.08	0.50	0.00	0.00	16.8
13	75	-896	3784	56	0	-3	1917	4.02	4.02	4.02	4.02	2	0.28	0.08	0.50	0.00	0.00	16.8
14	75	-984	3706	-22	0	14	1921	4.02	4.02	4.02	4.02	2	0.28	0.08	0.49	0.00	0.00	16.8
15	75	-820	3839	-26	0	25	-1974	4.02	4.02	4.02	4.02	2	0.29	0.08	0.51	0.00	0.00	16.8
16	75	-992	3702	16	0	3	1921	4.02	4.02	4.02	4.02	2	0.28	0.08	0.49	0.00	0.00	16.8
17	75	-828	3835	11	0	14	-1970	4.02	4.02	4.02	4.02	2	0.29	0.08	0.51	0.00	0.00	16.8
18	75	-1290	5383	-184	0	97	2741	4.02	4.02	4.02	4.02	3	0.37	0.12	0.71	0.00	0.00	16.8
19	75	-1415	5330	177	0	-42	2751	4.02	4.02	4.02	4.02	3	0.37	0.12	0.70	0.00	0.00	16.8
20	75	-1458	5283	-27	0	42	2800	4.02	4.02	4.02	4.02	3	0.38	0.11	0.70	0.00	0.00	16.8
37	75	-1170	5165	-306	0	140	-2621	4.02	4.02	4.02	4.02	3	0.36	0.11	0.69	0.00	0.00	16.8
38	75	-1379	5076	296	0	-92	2624	4.02	4.02	4.02	4.02	3	0.35	0.11	0.67	0.00	0.00	16.8
39	75	-1450	4997	-43	0	48	2705	4.02	4.02	4.02	4.02	3	0.36	0.11	0.66	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	112	-1178	3377	-7	0	20	2952	4.02	4.02	4.02	4.02	3	0.40	0.07	0.45	0.00	0.00	16.8
2	112	-916	2584	-67	0	56	2263	4.02	4.02	4.02	4.02	2	0.33	0.06	0.34	0.00	0.00	16.8
3	112	-867	2624	-68	0	59	2285	4.02	4.02	4.02	4.02	2	0.33	0.06	0.35	0.00	0.00	16.8
4	112	-945	2572	58	0	-28	2258	4.02	4.02	4.02	4.02	2	0.33	0.06	0.34	0.00	0.00	16.8
5	112	-896	2611	56	0	-24	2280	4.02	4.02	4.02	4.02	2	0.33	0.06	0.35	0.00	0.00	16.8
6	112	-984	2533	-22	0	22	2235	4.02	4.02	4.02	4.02	2	0.33	0.05	0.34	0.00	0.00	16.8
7	112	-820	2666	-26	0	34	2310	4.02	4.02	4.02	4.02	2	0.34	0.06	0.36	0.00	0.00	16.8
8	112	-992	2529	16	0	-3	2233	4.02	4.02	4.02	4.02	2	0.33	0.05	0.34	0.00	0.00	16.8
9	112	-828	2663	11	0	9	2308	4.02	4.02	4.02	4.02	2	0.34	0.06	0.36	0.00	0.00	16.8
10	112	-916	2584	-67	0	56	2263	4.02	4.02	4.02	4.02	2	0.33	0.06	0.34	0.00	0.00	16.8
11	112	-867	2624	-68	0	59	2285	4.02	4.02	4.02	4.02	2	0.33	0.06	0.35	0.00	0.00	16.8
12	112	-945	2572	58	0	-28	2258	4.02	4.02	4.02	4.02	2	0.33	0.06	0.34	0.00	0.00	16.8
13	112	-896	2611	56	0	-24	2280	4.02	4.02	4.02	4.02	2	0.33	0.06	0.35	0.00	0.00	16.8
14	112	-984	2533	-22	0	22	2235	4.02	4.02	4.02	4.02	2	0.33	0.05	0.34	0.00	0.00	16.8
15	112	-820	2666	-26	0	34	2310	4.02	4.02	4.02	4.02	2	0.34	0.06	0.36	0.00	0.00	16.8
16	112	-992	2529	16	0	-3	2233	4.02	4.02	4.02	4.02	2	0.33	0.05	0.34	0.00	0.00	16.8
17	112	-828	2663	11	0	9	2308	4.02	4.02	4.02	4.02	2	0.34	0.06	0.36	0.00	0.00	16.8
18	112	-1290	3700	-184	0	166	3232	4.02	4.02	4.02	4.02	3	0.44	0.08	0.49	0.00	0.00	16.8
19	112	-1415	3647	177	0	-108	3208	4.02	4.02	4.02	4.02	3	0.43	0.08	0.48	0.00	0.00	16.8
20	112	-1458	3600	-27	0	52	3228	4.02	4.02	4.02	4.02	3	0.43	0.08	0.48	0.00	0.00	16.8
37	112	-1170	3561	-306	0	255	3097	4.02	4.02	4.02	4.02	3	0.42	0.08	0.47	0.00	0.00	16.8
38	112	-1379	3472	296	0	-203	3058	4.02	4.02	4.02	4.02	3	0.41	0.08	0.46	0.00	0.00	16.8
39	112	-1450	3393	-43	0	64	3090	4.02	4.02	4.02	4.02	3	0.42	0.07	0.45	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	150	-1178	1853	-7	0	23	2952	4.02	4.02	4.02	4.02	3	0.40	0.04	0.25	0.00	0.00	16.8
2	150	-916	1411	-67	0	81	2263	4.02	4.02	4.02	4.02	2	0.33	0.03	0.19	0.00	0.00	16.8
3	150	-867	1451	-68	0	85	2285	4.02	4.02	4.02	4.02	2	0.33	0.03	0.19	0.00	0.00	16.8
4	150	-945	1399	58	0	-50	2258	4.02	4.02	4.02	4.02	2	0.33	0.03	0.19	0.00	0.00	16.8
5	150	-896	1438	56	0	-45	2280	4.02	4.02	4.02	4.02	2	0.33	0.03	0.19	0.00	0.00	16.8
6	150	-984	1360	-22	0	30	2235	4.02	4.02	4.02	4.02	2	0.33	0.03	0.18	0.00	0.00	16.8
7	150	-820	1493	-26	0	44	2310	4.02	4.02	4.02	4.02	2	0.34	0.03	0.20	0.00	0.00	16.8
8	150	-992	1356	16	0	-9	2233	4.02	4.02	4.02	4.02	2	0.33	0.03	0.18	0.00	0.00	16.8
9	150	-828	1490	11	0	5	2308	4.02	4.02	4.02	4.02	2	0.34	0.03	0.20	0.00	0.00	16.8
10	150	-916	1411	-67	0	81	2263	4.02	4.02	4.02	4.02	2	0.33	0.03	0.19	0.00	0.00	16.8
11	150	-867	1451	-68	0	85	2285	4.02	4.02	4.02	4.02	2	0.33	0.03	0.19	0.00	0.00	16.8
12	150	-945	1399	58	0	-50	2258	4.02	4.02	4.02	4.02	2	0.33	0.03	0.19	0.00	0.00	16.8
13	150	-896	1438	56	0	-45	2280	4.02	4.02	4.02	4.02	2	0.33	0.03	0.19	0.00	0.00	16.8
14	150	-984	1360	-22	0	30	2235	4.02	4.02	4.02	4.02	2	0.33	0.03	0.18	0.00	0.00	16.8
15	150	-820	1493	-26	0	44	2310	4.02	4.02	4.02	4.02	2	0.34	0.03	0.20	0.00	0.00	16.8
16	150	-992	1356	16	0	-9	2233	4.02	4.02	4.02	4.02	2	0.33	0.03	0.18	0.00	0.00	16.8
17	150	-828	1490	11	0	5	2308	4.02	4.02	4.02	4.02	2	0.34	0.03	0.20	0.00	0.00	16.8
18	150	-1290	2016	-184	0	235	3232	4.02	4.02	4.02	4.02	3	0.44	0.04	0.27	0.00	0.00	16.8
19	150	-1415	1963	177	0	-175	3208	4.02	4.02	4.02	4.02	3	0.43	0.04	0.26	0.00	0.00	16.8
20	150	-1458	1916	-27	0	62	3228	4.02	4.02	4.02	4.02	3	0.43	0.04	0.25	0.00	0.00	16.8
37	150	-1170	1957	-306	0	370	3097	4.02	4.02	4.02	4.02	3	0.42	0.04	0.26	0.00	0.00	16.8
38	150	-1379	1868	296	0	-314	3058	4.02	4.02	4.02	4.02	3	0.41	0.04	0.25	0.00	0.00	16.8
39	150	-1450	1789	-43	0	80	3090	4.02	4.02	4.02	4.02	3	0.42	0.04	0.24	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	188	-1178	328	-7	0	25	2952	4.02	4.02	4.02	4.02	3	0.40	0.01	0.04	0.00	0.00	16.8
2	188	-916	238	-67	0	106	2263	4.02	4.02	4.02	4.02	2	0.33	0.01	0.03	0.00	0.00	16.8
3	188	-867	278	-68	0	110	2285	4.02	4.02	4.02	4.02	2	0.33	0.01	0.04	0.00	0.00	16.8
4	188	-945	226	58	0	-71	2258	4.02	4.02	4.02	4.02	2	0.33	0.00	0.03	0.00	0.00	16.8
5	188	-896	266	56	0	-67	2280	4.02	4.02	4.02	4.02	2	0.33	0.01	0.04	0.00	0.00	16.8
6	188	-984	188	-22	0	38	2235	4.02	4.02	4.02	4.02	2	0.33	0.00	0.02	0.00	0.00	16.8
7	188	-820	320	-26	0	54	2310	4.02	4.02	4.02	4.02	2	0.34	0.01	0.04	0.00	0.00	16.8
8	188	-992	184	16	0	-15	2233	4.02	4.02	4.02	4.02	2	0.33	0.00	0.02	0.00	0.00	16.8
9	188	-828	317	11	0	1	2308	4.02	4.02	4.02	4.02	2	0.34	0.01	0.04	0.00	0.00	16.8
10	188	-916	238	-67	0	106	2263	4.02	4.02	4.02	4.02	2	0.33	0.01	0.03	0.00	0.00	16.8
11	188	-867	278	-68	0	110	2285	4.02	4.02	4.02	4.02	2	0.33	0.01	0.04	0.00	0.00	16.8
12	188	-945	226	58	0	-71	2258	4.02	4.02	4.02	4.02	2	0.33	0.00	0.03	0.00	0.00	16.8
13	188	-896	266	56	0	-67	2280	4.02	4.02	4.02	4.02	2	0.33	0.01	0.04	0.00	0.00	16.8
14	188	-984	188	-22	0	38	2235	4.02	4.02	4.02	4.02	2	0.33	0.00	0.02	0.00	0.00	16.8
15	188	-820	320	-26	0	54	2310	4.02	4.02	4.02	4.02	2	0.34	0.01	0.04	0.00	0.00	16.8

16	188	-992	184	16	0	-15	2233	4.02	4.02	4.02	4.02	2	0.33	0.00	0.02	0.00	0.00	16.8
17	188	-828	317	11	0	1	2308	4.02	4.02	4.02	4.02	2	0.34	0.01	0.04	0.00	0.00	16.8
18	188	-1290	333	-184	0	304	3232	4.02	4.02	4.02	4.02	3	0.44	0.01	0.04	0.00	0.00	16.8
19	188	-1415	280	177	0	-241	3208	4.02	4.02	4.02	4.02	3	0.43	0.01	0.04	0.00	0.00	16.8
20	188	-1458	233	-27	0	72	3228	4.02	4.02	4.02	4.02	3	0.43	0.01	0.03	0.00	0.00	16.8
37	188	-1170	353	-306	0	484	3097	4.02	4.02	4.02	4.02	3	0.42	0.01	0.05	0.00	0.00	16.8
38	188	-1379	264	296	0	-425	3058	4.02	4.02	4.02	4.02	3	0.41	0.01	0.04	0.00	0.00	16.8
39	188	-1450	185	-43	0	96	3090	4.02	4.02	4.02	4.02	3	0.42	0.00	0.02	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	225	-1178	-1197	-7	0	28	2952	4.02	4.02	4.02	4.02	3	0.40	0.03	0.16	0.00	0.00	16.8
2	225	-916	-934	-67	0	131	2263	4.02	4.02	4.02	4.02	2	0.33	0.02	0.12	0.00	0.00	16.8
3	225	-867	-894	-68	0	136	2285	4.02	4.02	4.02	4.02	2	0.33	0.02	0.12	0.00	0.00	16.8
4	225	-945	-947	58	0	-93	2258	4.02	4.02	4.02	4.02	2	0.33	0.02	0.13	0.00	0.00	16.8
5	225	-896	-907	56	0	-88	2280	4.02	4.02	4.02	4.02	2	0.33	0.02	0.12	0.00	0.00	16.8
6	225	-984	-985	-22	0	46	2235	4.02	4.02	4.02	4.02	2	0.33	0.02	0.13	0.00	0.00	16.8
7	225	-820	-852	-26	0	64	2310	4.02	4.02	4.02	4.02	2	0.34	0.02	0.11	0.00	0.00	16.8
8	225	-992	-989	16	0	-21	2233	4.02	4.02	4.02	4.02	2	0.33	0.02	0.13	0.00	0.00	16.8
9	225	-828	-856	11	0	-3	2308	4.02	4.02	4.02	4.02	2	0.34	0.02	0.11	0.00	0.00	16.8
10	225	-916	-934	-67	0	131	2263	4.02	4.02	4.02	4.02	2	0.33	0.02	0.12	0.00	0.00	16.8
11	225	-867	-894	-68	0	136	2285	4.02	4.02	4.02	4.02	2	0.33	0.02	0.12	0.00	0.00	16.8
12	225	-945	-947	58	0	-93	2258	4.02	4.02	4.02	4.02	2	0.33	0.02	0.13	0.00	0.00	16.8
13	225	-896	-907	56	0	-88	2280	4.02	4.02	4.02	4.02	2	0.33	0.02	0.12	0.00	0.00	16.8
14	225	-984	-985	-22	0	46	2235	4.02	4.02	4.02	4.02	2	0.33	0.02	0.13	0.00	0.00	16.8
15	225	-820	-852	-26	0	64	2310	4.02	4.02	4.02	4.02	2	0.34	0.02	0.11	0.00	0.00	16.8
16	225	-992	-989	16	0	-21	2233	4.02	4.02	4.02	4.02	2	0.33	0.02	0.13	0.00	0.00	16.8
17	225	-828	-856	11	0	-3	2308	4.02	4.02	4.02	4.02	2	0.34	0.02	0.11	0.00	0.00	16.8
18	225	-1290	-1350	-184	0	373	3232	4.02	4.02	4.02	4.02	3	0.44	0.03	0.18	0.00	0.00	16.8
19	225	-1415	-1403	177	0	-307	3208	4.02	4.02	4.02	4.02	3	0.43	0.03	0.19	0.00	0.00	16.8
20	225	-1458	-1450	-27	0	82	3228	4.02	4.02	4.02	4.02	3	0.43	0.03	0.19	0.00	0.00	16.8
37	225	-1170	-1251	-306	0	599	3097	4.02	4.02	4.02	4.02	3	0.42	0.03	0.17	0.00	0.00	16.8
38	225	-1379	-1340	296	0	-536	3058	4.02	4.02	4.02	4.02	3	0.41	0.03	0.18	0.00	0.00	16.8
39	225	-1450	-1419	-43	0	113	3090	4.02	4.02	4.02	4.02	3	0.42	0.03	0.19	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	262	-1178	-2721	-7	0	31	2952	4.02	4.02	4.02	4.02	3	0.40	0.06	0.36	0.00	0.00	16.8
2	262	-916	-2107	-67	0	156	2263	4.02	4.02	4.02	4.02	2	0.33	0.05	0.28	0.00	0.00	16.8
3	262	-867	-2067	-68	0	161	2285	4.02	4.02	4.02	4.02	2	0.33	0.04	0.28	0.00	0.00	16.8
4	262	-945	-2120	58	0	-114	2258	4.02	4.02	4.02	4.02	2	0.33	0.05	0.28	0.00	0.00	16.8
5	262	-896	-2080	56	0	-109	2280	4.02	4.02	4.02	4.02	2	0.33	0.05	0.28	0.00	0.00	16.8
6	262	-984	-2158	-22	0	55	2235	4.02	4.02	4.02	4.02	2	0.33	0.05	0.29	0.00	0.00	16.8
7	262	-820	-2025	-26	0	73	2310	4.02	4.02	4.02	4.02	2	0.34	0.04	0.27	0.00	0.00	16.8
8	262	-992	-2162	16	0	-26	2233	4.02	4.02	4.02	4.02	2	0.33	0.05	0.29	0.00	0.00	16.8
9	262	-828	-2029	11	0	-8	2308	4.02	4.02	4.02	4.02	2	0.34	0.04	0.27	0.00	0.00	16.8
10	262	-916	-2107	-67	0	156	2263	4.02	4.02	4.02	4.02	2	0.33	0.05	0.28	0.00	0.00	16.8
11	262	-867	-2067	-68	0	161	2285	4.02	4.02	4.02	4.02	2	0.33	0.04	0.28	0.00	0.00	16.8
12	262	-945	-2120	58	0	-114	2258	4.02	4.02	4.02	4.02	2	0.33	0.05	0.28	0.00	0.00	16.8
13	262	-896	-2080	56	0	-109	2280	4.02	4.02	4.02	4.02	2	0.33	0.05	0.28	0.00	0.00	16.8
14	262	-984	-2158	-22	0	55	2235	4.02	4.02	4.02	4.02	2	0.33	0.05	0.29	0.00	0.00	16.8
15	262	-820	-2025	-26	0	73	2310	4.02	4.02	4.02	4.02	2	0.34	0.04	0.27	0.00	0.00	16.8
16	262	-992	-2162	16	0	-26	2233	4.02	4.02	4.02	4.02	2	0.33	0.05	0.29	0.00	0.00	16.8
17	262	-828	-2029	11	0	-8	2308	4.02	4.02	4.02	4.02	2	0.34	0.04	0.27	0.00	0.00	16.8
18	262	-1290	-3034	-184	0	442	3232	4.02	4.02	4.02	4.02	3	0.44	0.07	0.40	0.00	0.00	16.8
19	262	-1415	-3087	177	0	-374	3208	4.02	4.02	4.02	4.02	3	0.43	0.07	0.41	0.00	0.00	16.8
20	262	-1458	-3134	-27	0	92	3228	4.02	4.02	4.02	4.02	3	0.43	0.07	0.41	0.00	0.00	16.8
37	262	-1170	-2855	-306	0	713	3097	4.02	4.02	4.02	4.02	3	0.42	0.06	0.38	0.00	0.00	16.8
38	262	-1379	-2944	296	0	-647	3058	4.02	4.02	4.02	4.02	3	0.41	0.06	0.39	0.00	0.00	16.8
39	262	-1450	-3023	-43	0	129	3090	4.02	4.02	4.02	4.02	3	0.42	0.07	0.40	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	300	-1178	-4246	-7	0	33	2898	4.02	4.02	4.02	4.02	3	0.39	0.09	0.56	0.00	0.00	16.8
2	300	-916	-3280	-67	0	181	2212	4.02	4.02	4.02	4.02	2	0.32	0.07	0.44	0.00	0.00	16.8
3	300	-867	-3240	-68	0	187	2259	4.02	4.02	4.02	4.02	2	0.33	0.07	0.43	0.00	0.00	16.8
4	300	-945	-3292	58	0	-136	2200	4.02	4.02	4.02	4.02	2	0.32	0.07	0.44	0.00	0.00	16.8
5	300	-896	-3253	56	0	-130	2246	4.02	4.02	4.02	4.02	2	0.33	0.07	0.43	0.00	0.00	16.8
6	300	-984	-3331	-22	0	63	2153	4.02	4.02	4.02	4.02	2	0.31	0.07	0.44	0.00	0.00	16.8
7	300	-820	-3198	-26	0	83	2310	4.02	4.02	4.02	4.02	2	0.34	0.07	0.43	0.00	0.00	16.8
8	300	-992	-3335	16	0	-32	2148	4.02	4.02	4.02	4.02	2	0.31	0.07	0.44	0.00	0.00	16.8
9	300	-828	-3201	11	0	-12	2306	4.02	4.02	4.02	4.02	2	0.34	0.07	0.43	0.00	0.00	16.8
10	300	-916	-3280	-67	0	181	2212	4.02	4.02	4.02	4.02	2	0.32	0.07	0.44	0.00	0.00	16.8
11	300	-867	-3240	-68	0	187	2259	4.02	4.02	4.02	4.02	2	0.33	0.07	0.43	0.00	0.00	16.8
12	300	-945	-3292	58	0	-136	2200	4.02	4.02	4.02	4.02	2	0.32	0.07	0.44	0.00	0.00	16.8
13	300	-896	-3253	56	0	-130	2246	4.02	4.02	4.02	4.02	2	0.33	0.07	0.43	0.00	0.00	16.8
14	300	-984	-3331	-22	0	63	2153	4.02	4.02	4.02	4.02	2	0.31	0.07	0.44	0.00	0.00	16.8
15	300	-820	-3198	-26	0	83	2310	4.02	4.02	4.02	4.02	2	0.34	0.07	0.43	0.00	0.00	16.8
16	300	-992	-3335	16	0	-32	2148	4.02	4.02	4.02	4.02	2	0.31	0.07	0.44	0.00	0.00	16.8
17	300	-828	-3201	11	0	-12	2306	4.02	4.02	4.02	4.02	2	0.34	0.07	0.43	0.00	0.00	16.8
18	300	-1290	-4717	-184	0	511	3154	4.02	4.02	4.02	4.02	3	0.43	0.10	0.62	0.00	0.00	16.8
19	300	-1415	-4770	177	0	-440	3097	4.02	4.02	4.02	4.02	3	0.42	0.10	0.63	0.00	0.00	16.8
20	300	-1458	-4817	-27	0	102	3087	4.02	4.02	4.02	4.02	3	0.42	0.10	0.64	0.00	0.00	16.8
37	300	-1170	-4459	-306	0	828	3044	4.02	4.02	4.02	4.02	3	0.41	0.10	0.59	0.00	0.00	16.8
38	300	-1379	-4548	296	0	-758	2950	4.02	4.02	4.02	4.02	3	0.40	0.10	0.60	0.00	0.00	16.8
39	300	-1450	-4627	-43	0	145	2934	4.02	4.02	4.02	4.02	3	0.40	0.10	0.61	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	338	-1178	-5770	-7	0	36	-3579	4.02	4.02	4.02	4.02	3	0.49	0.13	0.77	0.00	0.00	16.8
2	338	-916	-4452	-67	0	206	-2787	4.02	4.02	4.02	4.02	2	0.41	0.10	0.59	0.00	0.00	16.8
3	338	-867	-4412	-68	0	212	-2690	4.02	4.02	4.02	4.02	2	0.39	0.10	0.59	0.00	0.00	16.8
4	338	-945	-4465	58	0	-158	-2816	4.02	4.02	4.02	4.02	2	0.41	0.10	0.60	0.00	0.00	16.8
5	338	-896	-4425	56	0	-151	-2719	4.02	4.02	4.02	4.02	2	0.40	0.10	0.59	0.00	0.00	16.8
6	338	-984	-4503	-22	0	71	-2911	4.02	4.02	4.02	4.02	2	0.42	0.10	0.60	0.00	0.00	16.8
7	338	-820	-4370	-26	0	93	-2586	4.02	4.02	4.02	4.02	2	0.38	0.09	0.58	0.00	0.00	16.8
8	338	-992	-4507	16	0	-38	-2920	4.02	4.02	4.02	4.02	2	0.43	0.10	0.60	0.00	0.00	16.8
9	338	-828	-4374	11	0	-16	-2595	4.02	4.02	4.02	4.02	2	0.38	0.09	0.58	0.00	0.00	16.8
10	338	-916	-4452	-67	0	206	-2787	4.02	4.02	4.02	4.02	2	0.41	0.10	0.59	0.00	0.00	16.8
11	338	-867	-4412	-68	0	212	-2690	4.02	4.02	4.02	4.02	2	0.39	0.10	0.59	0.00	0.00	16.8
12	338	-945	-4465	58	0	-158	-2816	4.02	4.02	4.02	4.02	2	0.41	0.10	0.60	0.00	0.00	16.8
13	338	-896	-4425	56	0	-151	-2719	4.02	4.02	4.02	4.02	2	0.40	0.10	0.59	0.00	0.00	16.8
14	338	-984	-4503	-22	0	71	-2911	4.02	4.02	4.02	4.02	2	0.42	0.10	0.60	0.00	0.00	16.8
15	338	-820	-4370	-26	0	93	-2586	4.02	4.02	4.02	4.02	2	0.38	0.09	0.58	0.00	0.00	16.8
16	338	-992	-4507	16	0	-38	-2920	4.02	4.02	4.02	4.02	2	0.43	0.10	0.60	0.00	0.00	16.8
17	338	-828	-4374	11	0	-16	-2595	4.02	4.02	4.02	4.02	2	0.38	0.09	0.58	0.00	0.00	16.8
18	338	-1290	-6401	-184	0	580	-4035	4.02	4.02	4.02	4.02	3	0.55	0.14	0.85	0.00	0.00	16.8
19	338	-1415	-6454	177	0	-506	-4158	4.02	4.02	4.02	4.02	3	0.56	0.14	0.85	0.00	0.00	16.8
20	338	-1458	-6501	-27	0	112	-4227	4.02	4.02	4.02	4.02	3	0.57	0.14	0.86	0.00	0.00	16.8
37	338	-1170	-6063	-306	0	942	-3761	4.02	4.02	4.02	4.02	3	0.51	0.13	0.80	0.00	0.00	16.8

38	338	-1379	-6152	296	0	-869	-3966	4.02	4.02	4.02	4.02	3	0.53	0.13	0.81	0.00	0.00	16.8
39	338	-1450	-6231	-43	0	161	-4081	4.02	4.02	4.02	4.02	3	0.55	0.13	0.82	0.00	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

1	375	-1178	-7295	-7	0	38	-3579	4.02	4.02	4.02	4.02	3	0.49	0.16	0.97	0.00	0.00	16.8
2	375	-916	-5625	-67	0	231	-2787	4.02	4.02	4.02	4.02	2	0.41	0.12	0.75	0.00	0.00	16.8
3	375	-867	-5585	-68	0	238	-2690	4.02	4.02	4.02	4.02	2	0.39	0.12	0.75	0.00	0.00	16.8
4	375	-945	-5638	58	0	-179	-2816	4.02	4.02	4.02	4.02	2	0.41	0.12	0.75	0.00	0.00	16.8
5	375	-896	-5598	56	0	-172	-2719	4.02	4.02	4.02	4.02	2	0.40	0.12	0.75	0.00	0.00	16.8
6	375	-984	-5676	-22	0	79	-2911	4.02	4.02	4.02	4.02	2	0.42	0.12	0.76	0.00	0.00	16.8
7	375	-820	-5543	-26	0	103	-2586	4.02	4.02	4.02	4.02	2	0.38	0.12	0.74	0.00	0.00	16.8
8	375	-992	-5680	16	0	-44	-2920	4.02	4.02	4.02	4.02	2	0.43	0.12	0.76	0.00	0.00	16.8
9	375	-828	-5547	11	0	-20	-2595	4.02	4.02	4.02	4.02	2	0.38	0.12	0.74	0.00	0.00	16.8
10	375	-916	-5625	-67	0	231	-2787	4.02	4.02	4.02	4.02	2	0.41	0.12	0.75	0.00	0.00	16.8
11	375	-867	-5585	-68	0	238	-2690	4.02	4.02	4.02	4.02	2	0.39	0.12	0.75	0.00	0.00	16.8
12	375	-945	-5638	58	0	-179	-2816	4.02	4.02	4.02	4.02	2	0.41	0.12	0.75	0.00	0.00	16.8
13	375	-896	-5598	56	0	-172	-2719	4.02	4.02	4.02	4.02	2	0.40	0.12	0.75	0.00	0.00	16.8
14	375	-984	-5676	-22	0	79	-2911	4.02	4.02	4.02	4.02	2	0.42	0.12	0.76	0.00	0.00	16.8
15	375	-820	-5543	-26	0	103	-2586	4.02	4.02	4.02	4.02	2	0.38	0.12	0.74	0.00	0.00	16.8
16	375	-992	-5680	16	0	-44	-2920	4.02	4.02	4.02	4.02	2	0.43	0.12	0.76	0.00	0.00	16.8
17	375	-828	-5547	11	0	-20	-2595	4.02	4.02	4.02	4.02	2	0.38	0.12	0.74	0.00	0.00	16.8
18	375	-1290	-8084	-184	0	650	-4035	4.02	4.02	4.02	4.02	3	0.55	0.18	1.07	2.00	0.00	16.8
19	375	-1415	-8137	177	0	-573	-4158	4.02	4.02	4.02	4.02	3	0.56	0.18	1.08	2.02	0.00	16.8
20	375	-1458	-8184	-27	0	122	-4227	4.02	4.02	4.02	4.02	3	0.57	0.18	1.08	2.03	0.00	16.8
37	375	-1170	-7667	-306	0	1057	-3761	4.02	4.02	4.02	4.02	3	0.51	0.17	1.02	1.90	0.00	16.8
38	375	-1379	-7756	296	0	-980	-3966	4.02	4.02	4.02	4.02	3	0.53	0.17	1.03	1.92	0.00	16.8
39	375	-1450	-7835	-43	0	177	-4081	4.02	4.02	4.02	4.02	3	0.55	0.17	1.03	1.94	0.00	16.8

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 16.8

Nome travata: **trave_507_IP1** Descrizione: **Trave_5 26-25-24-23**
ASTA NUM. 19 NI 167 NF 264 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y Permanente Neve qy tot.
qy medio: 375.00 1635.75 142.50 2153.25 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-991	3670	569	0	1372	-1404	4.02	4.02	4.02	4.02	3	0.33	0.11	0.64	0.00	0.00	22.3
2	0	-951	2779	677	0	1480	-1021	4.02	4.02	4.02	4.02	2	0.40	0.08	0.48	0.00	0.00	22.3
3	0	-676	2915	679	0	1485	-1213	4.02	4.02	4.02	4.02	2	0.40	0.08	0.51	0.00	0.00	22.3
4	0	-848	2731	196	0	626	-947	4.02	4.02	4.02	4.02	2	0.17	0.08	0.48	0.00	0.00	22.3
5	0	-573	2867	198	0	631	-1138	4.02	4.02	4.02	4.02	2	0.17	0.08	0.50	0.00	0.00	22.3
6	0	-1236	2603	506	0	1175	-771	4.02	4.02	4.02	4.02	2	0.31	0.08	0.45	0.00	0.00	22.3
7	0	-319	3057	514	0	1192	-1411	4.02	4.02	4.02	4.02	2	0.33	0.09	0.54	0.00	0.00	22.3
8	0	-1205	2589	362	0	919	-749	4.02	4.02	4.02	4.02	2	0.24	0.07	0.45	0.00	0.00	22.3
9	0	-288	3042	369	0	936	-1388	4.02	4.02	4.02	4.02	2	0.26	0.09	0.54	0.00	0.00	22.3
10	0	-951	2779	677	0	1480	-1021	4.02	4.02	4.02	4.02	2	0.40	0.08	0.48	0.00	0.00	22.3
11	0	-676	2915	679	0	1485	-1213	4.02	4.02	4.02	4.02	2	0.40	0.08	0.51	0.00	0.00	22.3
12	0	-848	2731	196	0	626	-947	4.02	4.02	4.02	4.02	2	0.17	0.08	0.48	0.00	0.00	22.3
13	0	-573	2867	198	0	631	-1138	4.02	4.02	4.02	4.02	2	0.17	0.08	0.50	0.00	0.00	22.3
14	0	-1236	2603	506	0	1175	-771	4.02	4.02	4.02	4.02	2	0.31	0.08	0.45	0.00	0.00	22.3
15	0	-319	3057	514	0	1192	-1411	4.02	4.02	4.02	4.02	2	0.33	0.09	0.54	0.00	0.00	22.3
16	0	-1205	2589	362	0	919	-749	4.02	4.02	4.02	4.02	2	0.24	0.07	0.45	0.00	0.00	22.3
17	0	-288	3042	369	0	936	-1388	4.02	4.02	4.02	4.02	2	0.26	0.09	0.54	0.00	0.00	22.3
18	0	-2191	3735	1883	0	4114	-1235	4.02	4.02	4.02	4.02	3	0.96	0.11	0.63	0.00	0.00	22.3
19	0	-1940	3715	220	0	1051	-1182	4.02	4.02	4.02	4.02	3	0.25	0.11	0.63	0.00	0.00	22.3
20	0	-747	4101	966	0	2388	-1781	4.02	4.02	4.02	4.02	3	0.58	0.12	0.72	0.00	0.00	22.3
37	0	-1917	3670	2279	0	4739	-1296	6.03	4.02	4.02	4.02	3	0.80	0.11	0.62	0.00	0.00	22.3
38	0	-1499	3637	-492	0	-367	-1208	4.02	4.02	4.02	4.02	3	0.17	0.10	0.63	0.00	0.00	22.3
39	0	490	4280	751	0	1863	-2206	4.02	4.02	4.02	4.02	3	0.46	0.12	0.76	0.00	0.00	22.3

apost= 2.01 aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	31	-991	2860	569	0	1196	-1404	4.02	4.02	4.02	4.02	3	0.29	0.08	0.50	0.00	0.00	22.3
2	31	-951	2156	677	0	1270	-1021	4.02	4.02	4.02	4.02	2	0.34	0.06	0.38	0.00	0.00	22.3
3	31	-676	2292	679	0	1274	-1213	4.02	4.02	4.02	4.02	2	0.34	0.07	0.40	0.00	0.00	22.3
4	31	-848	2108	196	0	565	-947	4.02	4.02	4.02	4.02	2	0.15	0.06	0.37	0.00	0.00	22.3
5	31	-573	2244	198	0	570	-1138	4.02	4.02	4.02	4.02	2	0.17	0.06	0.39	0.00	0.00	22.3
6	31	-1236	1980	506	0	1018	-771	4.02	4.02	4.02	4.02	2	0.27	0.06	0.34	0.00	0.00	22.3
7	31	-319	2434	514	0	1033	-1411	4.02	4.02	4.02	4.02	2	0.28	0.07	0.43	0.00	0.00	22.3
8	31	-1205	1966	362	0	807	-749	4.02	4.02	4.02	4.02	2	0.21	0.06	0.34	0.00	0.00	22.3
9	31	-288	2419	369	0	821	-1388	4.02	4.02	4.02	4.02	2	0.22	0.07	0.43	0.00	0.00	22.3
10	31	-951	2156	677	0	1270	-1021	4.02	4.02	4.02	4.02	2	0.34	0.06	0.38	0.00	0.00	22.3
11	31	-676	2292	679	0	1274	-1213	4.02	4.02	4.02	4.02	2	0.34	0.07	0.40	0.00	0.00	22.3
12	31	-848	2108	196	0	565	-947	4.02	4.02	4.02	4.02	2	0.15	0.06	0.37	0.00	0.00	22.3
13	31	-573	2244	198	0	570	-1138	4.02	4.02	4.02	4.02	2	0.17	0.06	0.39	0.00	0.00	22.3
14	31	-1236	1980	506	0	1018	-771	4.02	4.02	4.02	4.02	2	0.27	0.06	0.34	0.00	0.00	22.3
15	31	-319	2434	514	0	1033	-1411	4.02	4.02	4.02	4.02	2	0.28	0.07	0.43	0.00	0.00	22.3
16	31	-1205	1966	362	0	807	-749	4.02	4.02	4.02	4.02	2	0.21	0.06	0.34	0.00	0.00	22.3
17	31	-288	2419	369	0	821	-1388	4.02	4.02	4.02	4.02	2	0.22	0.07	0.43	0.00	0.00	22.3
18	31	-2191	2858	1883	0	3530	-1235	4.02	4.02	4.02	4.02	3	0.82	0.08	0.48	0.00	0.00	22.3
19	31	-1940	2838	220	0	983	-1182	4.02	4.02	4.02	4.02	3	0.23	0.08	0.48	0.00	0.00	22.3
20	31	-747	3224	966	0	2089	-1781	4.02	4.02	4.02	4.02	3	0.50	0.09	0.56	0.00	0.00	22.3
37	31	-1917	2826	2279	0	4033	-1296	4.02	4.02	4.02	4.02	3	0.94	0.08	0.48	0.00	0.00	22.3
38	31	-1499	2794	-492	0	-214	-1208	4.02	4.02	4.02	4.02	3	0.17	0.08	0.48	0.00	0.00	22.3
39	31	490	3436	751	0	1630	-2206	4.02	4.02	4.02	4.02	3	0.41	0.10	0.61	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	62	-991	2049	569	0	1019	1144	4.02	4.02	4.02	4.02	3	0.24	0.06	0.36	0.00	0.00	22.3
2	62	-951	1532	677	0	1060	879	4.02	4.02	4.02	4.02	2	0.28	0.04	0.27	0.00	0.00	22.3
3	62	-676	1668	679	0	1064	889	4.02	4.02	4.02	4.02	2	0.29	0.05	0.29	0.00	0.00	22.3
4	62	-848	1484	196	0	505	894	4.02	4.02	4.02	4.02	2	0.14	0.04	0.26	0.00	0.00	22.3
5	62	-573	1620	198	0	508	890	4.02	4.02	4.02	4.02	2	0.14	0.05	0.28	0.00	0.00	22.3
6	62	-1236	1356	506	0	861	911	4.02	4.02	4.02	4.02	2	0.23	0.04	0.23	0.00	0.00	22.3
7	62	-319	1810	514	0	874	911	4.02	4.02	4.02	4.02	2	0.24	0.05	0.32	0.00	0.00	22.3
8	62	-1205	1342	362	0	695	916	4.02	4.02	4.02	4.02	2	0.18	0.04	0.23	0.00	0.00	22.3
9	62	-288	1795	369	0	707	912	4.02	4.02	4.02	4.02	2	0.19	0.05	0.32	0.00	0.00	22.3
10	62	-951	1532	677	0	1060	879	4.02	4.02	4.02	4.02	2	0.28	0.04	0.27	0.00	0.00	22.3
11	62	-676	1668	679	0	1064	889	4.02	4.02	4.02	4.02	2	0.29	0.05	0.29	0.00	0.00	22.3
12	62	-848	1484	196	0	505	894	4.02	4.02	4.02	4.02	2	0.14	0.04	0.26	0.00	0.00	22.3
13	62	-573	1620	198	0	508	890	4.02	4.02	4.02	4.02	2	0.14	0.05	0.28	0.00	0.00	22.3

14	62	-1236	1356	506	0	861	911	4.02	4.02	4.02	4.02	2	0.23	0.04	0.23	0.00	0.00	22.3
15	62	-319	1810	514	0	874	911	4.02	4.02	4.02	4.02	2	0.24	0.05	0.32	0.00	0.00	22.3
16	62	-1205	1342	362	0	695	916	4.02	4.02	4.02	4.02	2	0.18	0.04	0.23	0.00	0.00	22.3
17	62	-288	1795	369	0	707	912	4.02	4.02	4.02	4.02	2	0.19	0.05	0.32	0.00	0.00	22.3
18	62	-2191	1982	1883	0	2946	1222	4.02	4.02	4.02	4.02	3	0.68	0.06	0.34	0.00	0.00	22.3
19	62	-1940	1962	220	0	914	1251	4.02	4.02	4.02	4.02	3	0.21	0.06	0.33	0.00	0.00	22.3
20	62	-747	2348	966	0	1789	1178	4.02	4.02	4.02	4.02	3	0.43	0.07	0.41	0.00	0.00	22.3
37	62	-1917	1983	2279	0	3326	1163	4.02	4.02	4.02	4.02	3	0.78	0.07	0.35	0.00	0.00	22.3
38	62	-1499	1950	-492	0	-62	1210	4.02	4.02	4.02	4.02	3	0.17	0.06	0.34	0.00	0.00	22.3
39	62	490	2593	751	0	1397	-1388	4.02	4.02	4.02	4.02	3	0.35	0.08	0.46	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	93	-991	1239	569	0	843	1144	4.02	4.02	4.02	4.02	3	0.20	0.04	0.22	0.00	0.00	22.3
2	93	-951	909	677	0	850	879	4.02	4.02	4.02	4.02	2	0.23	0.03	0.16	0.00	0.00	22.3
3	93	-676	1045	679	0	853	889	4.02	4.02	4.02	4.02	2	0.23	0.03	0.18	0.00	0.00	22.3
4	93	-848	861	196	0	444	894	4.02	4.02	4.02	4.02	2	0.13	0.02	0.15	0.00	0.00	22.3
5	93	-573	997	198	0	447	890	4.02	4.02	4.02	4.02	2	0.13	0.03	0.18	0.00	0.00	22.3
6	93	-1236	733	506	0	704	911	4.02	4.02	4.02	4.02	2	0.19	0.02	0.13	0.00	0.00	22.3
7	93	-319	1187	514	0	714	911	4.02	4.02	4.02	4.02	2	0.20	0.03	0.21	0.00	0.00	22.3
8	93	-1205	719	362	0	583	916	4.02	4.02	4.02	4.02	2	0.15	0.02	0.12	0.00	0.00	22.3
9	93	-288	1172	369	0	592	912	4.02	4.02	4.02	4.02	2	0.16	0.03	0.21	0.00	0.00	22.3
10	93	-951	909	677	0	850	879	4.02	4.02	4.02	4.02	2	0.23	0.03	0.16	0.00	0.00	22.3
11	93	-676	1045	679	0	853	889	4.02	4.02	4.02	4.02	2	0.23	0.03	0.18	0.00	0.00	22.3
12	93	-848	861	196	0	444	894	4.02	4.02	4.02	4.02	2	0.13	0.02	0.15	0.00	0.00	22.3
13	93	-573	997	198	0	447	890	4.02	4.02	4.02	4.02	2	0.13	0.03	0.18	0.00	0.00	22.3
14	93	-1236	733	506	0	704	911	4.02	4.02	4.02	4.02	2	0.19	0.02	0.13	0.00	0.00	22.3
15	93	-319	1187	514	0	714	911	4.02	4.02	4.02	4.02	2	0.20	0.03	0.21	0.00	0.00	22.3
16	93	-1205	719	362	0	583	916	4.02	4.02	4.02	4.02	2	0.15	0.02	0.12	0.00	0.00	22.3
17	93	-288	1172	369	0	592	912	4.02	4.02	4.02	4.02	2	0.16	0.03	0.21	0.00	0.00	22.3
18	93	-2191	1105	1883	0	2363	1222	4.02	4.02	4.02	4.02	3	0.55	0.06	0.29	0.00	0.00	22.3
19	93	-1940	1085	220	0	846	1251	4.02	4.02	4.02	4.02	3	0.20	0.03	0.18	0.00	0.00	22.3
20	93	-747	1471	966	0	1490	1178	4.02	4.02	4.02	4.02	3	0.36	0.04	0.26	0.00	0.00	22.3
37	93	-1917	1140	2279	0	2619	1163	4.02	4.02	4.02	4.02	3	0.61	0.07	0.35	0.00	0.00	22.3
38	93	-1499	1106	-492	0	91	1210	4.02	4.02	4.02	4.02	3	0.17	0.03	0.19	0.00	0.00	22.3
39	93	490	1750	751	0	1165	1159	4.02	4.02	4.02	4.02	3	0.29	0.05	0.31	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	124	-991	428	569	0	667	1144	4.02	4.02	4.02	4.02	3	0.16	0.02	0.09	0.00	0.00	22.3
2	124	-951	285	677	0	640	879	4.02	4.02	4.02	4.02	2	0.17	0.02	0.11	0.00	0.00	22.3
3	124	-676	421	679	0	643	889	4.02	4.02	4.02	4.02	2	0.17	0.02	0.11	0.00	0.00	22.3
4	124	-848	238	196	0	383	894	4.02	4.02	4.02	4.02	2	0.13	0.01	0.04	0.00	0.00	22.3
5	124	-573	374	198	0	385	890	4.02	4.02	4.02	4.02	2	0.13	0.01	0.07	0.00	0.00	22.3
6	124	-1236	110	506	0	547	911	4.02	4.02	4.02	4.02	2	0.15	0.02	0.08	0.00	0.00	22.3
7	124	-319	563	514	0	555	911	4.02	4.02	4.02	4.02	2	0.15	0.02	0.10	0.00	0.00	22.3
8	124	-1205	96	362	0	470	916	4.02	4.02	4.02	4.02	2	0.13	0.01	0.06	0.00	0.00	22.3
9	124	-288	549	369	0	478	912	4.02	4.02	4.02	4.02	2	0.14	0.02	0.10	0.00	0.00	22.3
10	124	-951	285	677	0	640	879	4.02	4.02	4.02	4.02	2	0.17	0.02	0.11	0.00	0.00	22.3
11	124	-676	421	679	0	643	889	4.02	4.02	4.02	4.02	2	0.17	0.02	0.11	0.00	0.00	22.3
12	124	-848	238	196	0	383	894	4.02	4.02	4.02	4.02	2	0.13	0.01	0.04	0.00	0.00	22.3
13	124	-573	374	198	0	385	890	4.02	4.02	4.02	4.02	2	0.13	0.01	0.07	0.00	0.00	22.3
14	124	-1236	110	506	0	547	911	4.02	4.02	4.02	4.02	2	0.15	0.02	0.08	0.00	0.00	22.3
15	124	-319	563	514	0	555	911	4.02	4.02	4.02	4.02	2	0.15	0.02	0.10	0.00	0.00	22.3
16	124	-1205	96	362	0	470	916	4.02	4.02	4.02	4.02	2	0.13	0.01	0.06	0.00	0.00	22.3
17	124	-288	549	369	0	478	912	4.02	4.02	4.02	4.02	2	0.14	0.02	0.10	0.00	0.00	22.3
18	124	-2191	229	1883	0	1779	1222	4.02	4.02	4.02	4.02	3	0.41	0.06	0.29	0.00	0.00	22.3
19	124	-1940	209	220	0	778	1251	4.02	4.02	4.02	4.02	3	0.18	0.01	0.04	0.00	0.00	22.3
20	124	-747	595	966	0	1190	1178	4.02	4.02	4.02	4.02	3	0.29	0.03	0.15	0.00	0.00	22.3
37	124	-1917	296	2279	0	1913	1163	4.02	4.02	4.02	4.02	3	0.45	0.07	0.35	0.00	0.00	22.3
38	124	-1499	263	-492	0	243	1210	4.02	4.02	4.02	4.02	3	0.17	0.02	0.08	0.00	0.00	22.3
39	124	490	906	751	0	932	1159	4.02	4.02	4.02	4.02	3	0.23	0.03	0.16	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	155	-991	-382	569	0	490	1144	4.02	4.02	4.02	4.02	3	0.16	0.02	0.09	0.00	0.00	22.3
2	155	-951	-338	677	0	430	879	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
3	155	-676	-202	679	0	432	889	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
4	155	-848	-386	196	0	322	894	4.02	4.02	4.02	4.02	2	0.13	0.01	0.07	0.00	0.00	22.3
5	155	-573	-250	198	0	324	890	4.02	4.02	4.02	4.02	2	0.13	0.01	0.04	0.00	0.00	22.3
6	155	-1236	-514	506	0	391	911	4.02	4.02	4.02	4.02	2	0.13	0.02	0.09	0.00	0.00	22.3
7	155	-319	-60	514	0	396	911	4.02	4.02	4.02	4.02	2	0.14	0.02	0.08	0.00	0.00	22.3
8	155	-1205	-528	362	0	358	916	4.02	4.02	4.02	4.02	2	0.13	0.02	0.09	0.00	0.00	22.3
9	155	-288	-74	369	0	364	912	4.02	4.02	4.02	4.02	2	0.14	0.01	0.06	0.00	0.00	22.3
10	155	-951	-338	677	0	430	879	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
11	155	-676	-202	679	0	432	889	4.02	4.02	4.02	4.02	2	0.13	0.02	0.11	0.00	0.00	22.3
12	155	-848	-386	196	0	322	894	4.02	4.02	4.02	4.02	2	0.13	0.01	0.07	0.00	0.00	22.3
13	155	-573	-250	198	0	324	890	4.02	4.02	4.02	4.02	2	0.13	0.01	0.04	0.00	0.00	22.3
14	155	-1236	-514	506	0	391	911	4.02	4.02	4.02	4.02	2	0.13	0.02	0.09	0.00	0.00	22.3
15	155	-319	-60	514	0	396	911	4.02	4.02	4.02	4.02	2	0.14	0.02	0.08	0.00	0.00	22.3
16	155	-1205	-528	362	0	358	916	4.02	4.02	4.02	4.02	2	0.13	0.02	0.09	0.00	0.00	22.3
17	155	-288	-74	369	0	364	912	4.02	4.02	4.02	4.02	2	0.14	0.01	0.06	0.00	0.00	22.3
18	155	-2191	-648	1883	0	1195	1222	4.02	4.02	4.02	4.02	3	0.28	0.06	0.29	0.00	0.00	22.3
19	155	-1940	-668	220	0	709	1251	4.02	4.02	4.02	4.02	3	0.17	0.02	0.11	0.00	0.00	22.3
20	155	-747	-282	966	0	891	1178	4.02	4.02	4.02	4.02	3	0.21	0.03	0.15	0.00	0.00	22.3
37	155	-1917	-548	2279	0	1207	1163	4.02	4.02	4.02	4.02	3	0.28	0.07	0.35	0.00	0.00	22.3
38	155	-1499	-580	-492	0	396	1210	4.02	4.02	4.02	4.02	3	0.17	0.02	0.10	0.00	0.00	22.3
39	155	490	62	751	0	699	1159	4.02	4.02	4.02	4.02	3	0.17	0.02	0.12	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	186	-991	-1192	569	0	314	1144	4.02	4.02	4.02	4.02	3	0.16	0.03	0.21	0.00	0.00	22.3
2	186	-951	-961	677	0	220	879	4.02	4.02	4.02	4.02	2	0.13	0.03	0.17	0.00	0.00	22.3
3	186	-676	-825	679	0	221	889	4.02	4.02	4.02	4.02	2	0.13	0.02	0.14	0.00	0.00	22.3
4	186	-848	-1009	196	0	262	894	4.02	4.02	4.02	4.02	2	0.13	0.03	0.18	0.00	0.00	22.3
5	186	-573	-873	198	0	262	890	4.02	4.02	4.02	4.02	2	0.13	0.03	0.15	0.00	0.00	22.3
6	186	-1236	-1137	506	0	234	911	4.02	4.02	4.02	4.02	2	0.13	0.03	0.20	0.00	0.00	22.3
7	186	-319	-683	514	0	237	911	4.02	4.02	4.02	4.02	2	0.14	0.02	0.12	0.00	0.00	22.3
8	186	-1205	-1151	362	0	246	916	4.02	4.02	4.02	4.02	2	0.13	0.03	0.20	0.00	0.00	22.3
9	186	-288	-698	369	0	249	912	4.02	4.02	4.02	4.02	2	0.14	0.02	0.12	0.00	0.00	22.3
10	186	-951	-961	677	0	220	879	4.02	4.02	4.02	4.02	2	0.13	0.03	0.17	0.00	0.00	22.3
11	186	-676	-825	679	0	221	889	4.02	4.02	4.02	4.02	2	0.13	0.02	0.14	0.00	0.00	22.3
12	186	-848	-1009	196	0	262	894	4.02	4.02	4.02	4.02	2	0.13	0.03	0.18	0.00	0.00	22.3
13	186	-573	-873	198	0	262	890	4.02	4.02	4.02	4.02	2	0.13	0.03	0.15	0.00	0.00	22.3
14	186	-1236	-1137	506	0	234	911	4.02	4.02	4.02	4.02	2	0.13	0.03	0.20	0.00	0.00	22.3
15	186	-319	-683	514	0	237	911	4.02	4.02	4.02	4.02	2	0.14	0.02	0.12	0.00	0.00	22.3
16	186	-1205	-1151	362	0	246	916	4.02	4.02	4.02	4.02	2	0.13	0.03	0.20	0.00	0.00	22.3
17	186	-288	-698	369	0	249	912	4.02	4.02	4.02	4.02	2	0.14	0.02	0.12	0.00	0.00	22.3
18	186	-2191	-1525	1883	0	611	1222	4.02	4.02	4.02	4.02	3	0.16	0.06	0.29	0.00	0.00	22.3
19	186	-1940	-1545	220	0	641	1251	4.02	4.02	4.02	4.02	3	0.17	0.04	0.26	0.00	0.00	22.3

20	186	-747	-1159	966	0	591	1178	4.02	4.02	4.02	4.02	3	0.17	0.03	0.20	0.00	0.00	22.3
37	186	-1917	-1391	2279	0	500	1163	4.02	4.02	4.02	4.02	3	0.16	0.07	0.35	0.00	0.00	22.3
38	186	-1499	-1424	-492	0	549	1210	4.02	4.02	4.02	4.02	3	0.17	0.04	0.24	0.00	0.00	22.3
39	186	490	-781	751	0	466	1159	4.02	4.02	4.02	4.02	3	0.17	0.02	0.14	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	217	-991	-2003	569	0	137	1144	4.02	4.02	4.02	4.02	3	0.16	0.06	0.35	0.00	0.00	22.3
2	217	-951	-1585	677	0	11	879	4.02	4.02	4.02	4.02	2	0.13	0.05	0.28	0.00	0.00	22.3
3	217	-676	-1449	679	0	11	889	4.02	4.02	4.02	4.02	2	0.13	0.04	0.25	0.00	0.00	22.3
4	217	-848	-1632	196	0	201	894	4.02	4.02	4.02	4.02	2	0.13	0.05	0.28	0.00	0.00	22.3
5	217	-573	-1496	198	0	201	890	4.02	4.02	4.02	4.02	2	0.13	0.04	0.26	0.00	0.00	22.3
6	217	-1236	-1760	506	0	77	911	4.02	4.02	4.02	4.02	2	0.13	0.05	0.30	0.00	0.00	22.3
7	217	-319	-1307	514	0	78	911	4.02	4.02	4.02	4.02	2	0.14	0.04	0.23	0.00	0.00	22.3
8	217	-1205	-1774	362	0	134	916	4.02	4.02	4.02	4.02	2	0.13	0.05	0.31	0.00	0.00	22.3
9	217	-288	-1321	369	0	135	912	4.02	4.02	4.02	4.02	2	0.14	0.04	0.23	0.00	0.00	22.3
10	217	-951	-1585	677	0	11	879	4.02	4.02	4.02	4.02	2	0.13	0.05	0.28	0.00	0.00	22.3
11	217	-676	-1449	679	0	11	889	4.02	4.02	4.02	4.02	2	0.13	0.04	0.25	0.00	0.00	22.3
12	217	-848	-1632	196	0	201	894	4.02	4.02	4.02	4.02	2	0.13	0.05	0.28	0.00	0.00	22.3
13	217	-573	-1496	198	0	201	890	4.02	4.02	4.02	4.02	2	0.13	0.04	0.26	0.00	0.00	22.3
14	217	-1236	-1760	506	0	77	911	4.02	4.02	4.02	4.02	2	0.13	0.05	0.30	0.00	0.00	22.3
15	217	-319	-1307	514	0	78	911	4.02	4.02	4.02	4.02	2	0.14	0.04	0.23	0.00	0.00	22.3
16	217	-1205	-1774	362	0	134	916	4.02	4.02	4.02	4.02	2	0.13	0.05	0.31	0.00	0.00	22.3
17	217	-288	-1321	369	0	135	912	4.02	4.02	4.02	4.02	2	0.14	0.04	0.23	0.00	0.00	22.3
18	217	-2191	-2401	1883	0	27	1222	4.02	4.02	4.02	4.02	3	0.16	0.07	0.41	0.00	0.00	22.3
19	217	-1940	-2421	220	0	572	1251	4.02	4.02	4.02	4.02	3	0.17	0.07	0.41	0.00	0.00	22.3
20	217	-747	-2035	966	0	292	1178	4.02	4.02	4.02	4.02	3	0.17	0.06	0.36	0.00	0.00	22.3
37	217	-1917	-2235	2279	0	-207	1163	4.02	4.02	4.02	4.02	3	0.16	0.07	0.38	0.00	0.00	22.3
38	217	-1499	-2268	-492	0	701	1210	4.02	4.02	4.02	4.02	3	0.17	0.07	0.39	0.00	0.00	22.3
39	217	490	-1625	751	0	233	1159	4.02	4.02	4.02	4.02	3	0.17	0.05	0.29	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	248	-991	-2813	569	0	-39	-1766	4.02	4.02	4.02	4.02	3	0.25	0.08	0.49	0.00	0.00	22.3
2	248	-951	-2208	677	0	-199	-1431	4.02	4.02	4.02	4.02	2	0.21	0.06	0.38	0.00	0.00	22.3
3	248	-676	-2072	679	0	-200	-1217	4.02	4.02	4.02	4.02	2	0.18	0.06	0.36	0.00	0.00	22.3
4	248	-848	-2255	196	0	140	-1499	4.02	4.02	4.02	4.02	2	0.22	0.07	0.39	0.00	0.00	22.3
5	248	-573	-2119	198	0	140	-1284	4.02	4.02	4.02	4.02	2	0.19	0.06	0.37	0.00	0.00	22.3
6	248	-1236	-2383	506	0	-80	-1705	4.02	4.02	4.02	4.02	2	0.25	0.07	0.41	0.00	0.00	22.3
7	248	-319	-1930	514	0	-82	-991	4.02	4.02	4.02	4.02	2	0.15	0.06	0.34	0.00	0.00	22.3
8	248	-1205	-2397	362	0	22	-1725	4.02	4.02	4.02	4.02	2	0.25	0.07	0.41	0.00	0.00	22.3
9	248	-288	-1944	369	0	20	-1011	4.02	4.02	4.02	4.02	2	0.15	0.06	0.34	0.00	0.00	22.3
10	248	-951	-2208	677	0	-199	-1431	4.02	4.02	4.02	4.02	2	0.21	0.06	0.38	0.00	0.00	22.3
11	248	-676	-2072	679	0	-200	-1217	4.02	4.02	4.02	4.02	2	0.18	0.06	0.36	0.00	0.00	22.3
12	248	-848	-2255	196	0	140	-1499	4.02	4.02	4.02	4.02	2	0.22	0.07	0.39	0.00	0.00	22.3
13	248	-573	-2119	198	0	140	-1284	4.02	4.02	4.02	4.02	2	0.19	0.06	0.37	0.00	0.00	22.3
14	248	-1236	-2383	506	0	-80	-1705	4.02	4.02	4.02	4.02	2	0.25	0.07	0.41	0.00	0.00	22.3
15	248	-319	-1930	514	0	-82	-991	4.02	4.02	4.02	4.02	2	0.15	0.06	0.34	0.00	0.00	22.3
16	248	-1205	-2397	362	0	22	-1725	4.02	4.02	4.02	4.02	2	0.25	0.07	0.41	0.00	0.00	22.3
17	248	-288	-1944	369	0	20	-1011	4.02	4.02	4.02	4.02	2	0.15	0.06	0.34	0.00	0.00	22.3
18	248	-2191	-3278	1883	0	-556	-2328	4.02	4.02	4.02	4.02	3	0.31	0.09	0.55	0.00	0.00	22.3
19	248	-1940	-3298	220	0	504	-2334	4.02	4.02	4.02	4.02	3	0.32	0.09	0.56	0.00	0.00	22.3
20	248	-747	-2912	966	0	-8	-1781	4.02	4.02	4.02	4.02	3	0.25	0.08	0.51	0.00	0.00	22.3
37	248	-1917	-3078	2279	0	-913	-2120	4.02	4.02	4.02	4.02	3	0.29	0.09	0.52	0.00	0.00	22.3
38	248	-1499	-3111	-492	0	854	-2131	4.02	4.02	4.02	4.02	3	0.29	0.09	0.53	0.00	0.00	22.3
39	248	490	-2468	751	0	1	1159	4.02	4.02	4.02	4.02	3	0.17	0.07	0.44	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	279	-991	-3624	569	0	-215	-2588	4.02	4.02	4.02	4.02	3	0.36	0.10	0.63	0.00	0.00	22.3
2	279	-951	-2832	677	0	-409	-2069	4.02	4.02	4.02	4.02	2	0.30	0.08	0.49	0.00	0.00	22.3
3	279	-676	-2696	679	0	-410	-1839	4.02	4.02	4.02	4.02	2	0.27	0.08	0.47	0.00	0.00	22.3
4	279	-848	-2879	196	0	79	-2142	4.02	4.02	4.02	4.02	2	0.32	0.08	0.50	0.00	0.00	22.3
5	279	-573	-2743	198	0	78	-1912	4.02	4.02	4.02	4.02	2	0.28	0.08	0.48	0.00	0.00	22.3
6	279	-1236	-3007	506	0	-237	-2362	4.02	4.02	4.02	4.02	2	0.35	0.09	0.52	0.00	0.00	22.3
7	279	-319	-2554	514	0	-241	-1597	4.02	4.02	4.02	4.02	2	0.24	0.07	0.45	0.00	0.00	22.3
8	279	-1205	-3021	362	0	-90	-2384	4.02	4.02	4.02	4.02	2	0.35	0.09	0.52	0.00	0.00	22.3
9	279	-288	-2568	369	0	-94	-1619	4.02	4.02	4.02	4.02	2	0.24	0.07	0.45	0.00	0.00	22.3
10	279	-951	-2832	677	0	-409	-2069	4.02	4.02	4.02	4.02	2	0.30	0.08	0.49	0.00	0.00	22.3
11	279	-676	-2696	679	0	-410	-1839	4.02	4.02	4.02	4.02	2	0.27	0.08	0.47	0.00	0.00	22.3
12	279	-848	-2879	196	0	79	-2142	4.02	4.02	4.02	4.02	2	0.32	0.08	0.50	0.00	0.00	22.3
13	279	-573	-2743	198	0	78	-1912	4.02	4.02	4.02	4.02	2	0.28	0.08	0.48	0.00	0.00	22.3
14	279	-1236	-3007	506	0	-237	-2362	4.02	4.02	4.02	4.02	2	0.35	0.09	0.52	0.00	0.00	22.3
15	279	-319	-2554	514	0	-241	-1597	4.02	4.02	4.02	4.02	2	0.24	0.07	0.45	0.00	0.00	22.3
16	279	-1205	-3021	362	0	-90	-2384	4.02	4.02	4.02	4.02	2	0.35	0.09	0.52	0.00	0.00	22.3
17	279	-288	-2568	369	0	-94	-1619	4.02	4.02	4.02	4.02	2	0.24	0.07	0.45	0.00	0.00	22.3
18	279	-2191	-4154	1883	0	-1140	-3245	4.02	4.02	4.02	4.02	3	0.44	0.12	0.70	0.00	0.00	22.3
19	279	-1940	-4174	220	0	436	-3253	4.02	4.02	4.02	4.02	3	0.44	0.12	0.71	0.00	0.00	22.3
20	279	-747	-3788	966	0	-307	-2656	4.02	4.02	4.02	4.02	3	0.37	0.11	0.66	0.00	0.00	22.3
37	279	-1917	-3922	2279	0	-1620	-2993	4.02	4.02	4.02	4.02	3	0.41	0.11	0.67	0.00	0.00	22.3
38	279	-1499	-3955	-492	0	1006	-3008	4.02	4.02	4.02	4.02	3	0.41	0.11	0.68	0.00	0.00	22.3
39	279	490	-3312	751	0	-232	-2013	4.02	4.02	4.02	4.02	3	0.29	0.10	0.59	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	310	-991	-4434	569	0	-392	-2588	4.02	4.02	4.02	4.02	3	0.36	0.13	0.77	0.00	0.00	22.3
2	310	-951	-3455	677	0	-619	-2069	4.02	4.02	4.02	4.02	2	0.30	0.10	0.60	0.00	0.00	22.3
3	310	-676	-3319	679	0	-621	-1839	4.02	4.02	4.02	4.02	2	0.27	0.10	0.58	0.00	0.00	22.3
4	310	-848	-3502	196	0	19	-2142	4.02	4.02	4.02	4.02	2	0.32	0.10	0.61	0.00	0.00	22.3
5	310	-573	-3366	198	0	17	-1912	4.02	4.02	4.02	4.02	2	0.28	0.10	0.59	0.00	0.00	22.3
6	310	-1236	-3630	506	0	-394	-2362	4.02	4.02	4.02	4.02	2	0.35	0.10	0.63	0.00	0.00	22.3
7	310	-319	-3177	514	0	-400	-1597	4.02	4.02	4.02	4.02	2	0.24	0.09	0.56	0.00	0.00	22.3
8	310	-1205	-3644	362	0	-202	-2384	4.02	4.02	4.02	4.02	2	0.35	0.11	0.63	0.00	0.00	22.3
9	310	-288	-3191	369	0	-209	-1619	4.02	4.02	4.02	4.02	2	0.24	0.09	0.56	0.00	0.00	22.3
10	310	-951	-3455	677	0	-619	-2069	4.02	4.02	4.02	4.02	2	0.30	0.10	0.60	0.00	0.00	22.3
11	310	-676	-3319	679	0	-621	-1839	4.02	4.02	4.02	4.02	2	0.27	0.10	0.58	0.00	0.00	22.3
12	310	-848	-3502	196	0	19	-2142	4.02	4.02	4.02	4.02	2	0.32	0.10	0.61	0.00	0.00	22.3
13	310	-573	-3366	198	0	17	-1912	4.02	4.02	4.02	4.02	2	0.28	0.10	0.59	0.00	0.00	22.3
14	310	-1236	-3630	506	0	-394	-2362	4.02	4.02	4.02	4.02	2	0.35	0.10	0.63	0.00	0.00	22.3
15	310	-319	-3177	514	0	-400	-1597	4.02	4.02	4.02	4.02	2	0.24	0.09	0.56	0.00	0.00	22.3
16	310	-1205	-3644	362	0	-202	-2384	4.02	4.02	4.02	4.02	2	0.35	0.11	0.63	0.00	0.00	22.3
17	310	-288	-3191	369	0	-209	-1619	4.02	4.02	4.02	4.02	2	0.24	0.09	0.56	0.00	0.00	22.3
18	310	-2191	-5031	1883	0	-1724	-3245	4.02	4.02	4.02	4.02	3	0.44	0.14	0.85	0.00	0.00	22.3
19	310	-1940	-5051	220	0	367	-3253	4.02	4.02	4.02	4.02	3	0.44	0.15	0.86	0.00	0.00	22.3
20	310	-747	-4665	966	0	-607	-2656	4.02	4.02	4.02	4.02	3	0.37	0.13	0.82	0.00	0.00	22.3
37	310	-1917	-4765	2279	0	-2326	-2993	4.02	4.02	4.02	4.02	3	0.54	0.14	0.81	0.00	0.00	22.3
38	310	-1499	-4798	-492	0	1159	-3008	4.02	4.02	4.02	4.02	3	0.41	0.14	0.82	0.00	0.00	22.3
39	310	490	-4155	751	0	-465	-2013	4.02	4.02	4.02	4.02	3	0.29	0.12	0.74	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

Nome travata: **trave_507_IP1** Descrizione: **Trave_5 26-25-24-23**
ASTA NUM. 20 NI 264 NF 165 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y Permanente Neve qy tot.
qy medio: 375.00 1371.75 142.50 1889.25 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-1286	3769	10	0	55	-1637	4.02	4.02	4.02	4.02	3	0.23	0.11	0.65	0.00	0.00	22.3
2	0	-1141	2821	-65	0	-160	-1098	4.02	4.02	4.02	4.02	2	0.16	0.08	0.49	0.00	0.00	22.3
3	0	-888	2915	-65	0	-161	-1295	4.02	4.02	4.02	4.02	2	0.19	0.08	0.51	0.00	0.00	22.3
4	0	-1090	2883	80	0	245	-1224	4.02	4.02	4.02	4.02	2	0.18	0.08	0.50	0.00	0.00	22.3
5	0	-837	2976	79	0	245	-1421	4.02	4.02	4.02	4.02	2	0.21	0.09	0.52	0.00	0.00	22.3
6	0	-1419	2734	-13	0	-18	-913	4.02	4.02	4.02	4.02	2	0.13	0.08	0.47	0.00	0.00	22.3
7	0	-575	3046	-15	0	-19	-1568	4.02	4.02	4.02	4.02	2	0.23	0.09	0.54	0.00	0.00	22.3
8	0	-1404	2752	30	0	104	-950	4.02	4.02	4.02	4.02	2	0.14	0.08	0.47	0.00	0.00	22.3
9	0	-560	3064	28	0	103	-1606	4.02	4.02	4.02	4.02	2	0.24	0.09	0.54	0.00	0.00	22.3
10	0	-1141	2821	-65	0	-160	-1098	4.02	4.02	4.02	4.02	2	0.16	0.08	0.49	0.00	0.00	22.3
11	0	-888	2915	-65	0	-161	-1295	4.02	4.02	4.02	4.02	2	0.19	0.08	0.51	0.00	0.00	22.3
12	0	-1090	2883	80	0	245	-1224	4.02	4.02	4.02	4.02	2	0.18	0.08	0.50	0.00	0.00	22.3
13	0	-837	2976	79	0	245	-1421	4.02	4.02	4.02	4.02	2	0.21	0.09	0.52	0.00	0.00	22.3
14	0	-1419	2734	-13	0	-18	-913	4.02	4.02	4.02	4.02	2	0.13	0.08	0.47	0.00	0.00	22.3
15	0	-575	3046	-15	0	-19	-1568	4.02	4.02	4.02	4.02	2	0.23	0.09	0.54	0.00	0.00	22.3
16	0	-1404	2752	30	0	104	-950	4.02	4.02	4.02	4.02	2	0.14	0.08	0.47	0.00	0.00	22.3
17	0	-560	3064	28	0	103	-1606	4.02	4.02	4.02	4.02	2	0.24	0.09	0.54	0.00	0.00	22.3
18	0	-2077	3817	-180	0	-453	-1169	4.02	4.02	4.02	4.02	3	0.16	0.11	0.65	0.00	0.00	22.3
19	0	-1837	4013	254	0	758	-1571	4.02	4.02	4.02	4.02	3	0.21	0.12	0.68	0.00	0.00	22.3
20	0	-1263	4151	20	0	101	-1851	4.02	4.02	4.02	4.02	3	0.26	0.12	0.72	0.00	0.00	22.3
37	0	-1929	3636	-334	0	-889	-1080	4.02	4.02	4.02	4.02	3	0.21	0.10	0.62	0.00	0.00	22.3
38	0	-1529	3961	390	0	1130	-1750	4.02	4.02	4.02	4.02	3	0.27	0.11	0.68	0.00	0.00	22.3
39	0	-572	4191	-0	0	36	-2217	4.02	4.02	4.02	4.02	3	0.31	0.12	0.74	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	38	-1286	2917	10	0	51	-1637	4.02	4.02	4.02	4.02	3	0.23	0.08	0.50	0.00	0.00	22.3
2	38	-1141	2166	-65	0	-136	-1098	4.02	4.02	4.02	4.02	2	0.16	0.06	0.38	0.00	0.00	22.3
3	38	-888	2260	-65	0	-136	-1295	4.02	4.02	4.02	4.02	2	0.19	0.07	0.39	0.00	0.00	22.3
4	38	-1090	2228	80	0	215	-1224	4.02	4.02	4.02	4.02	2	0.18	0.06	0.39	0.00	0.00	22.3
5	38	-837	2321	79	0	215	-1421	4.02	4.02	4.02	4.02	2	0.21	0.07	0.41	0.00	0.00	22.3
6	38	-1419	2079	-13	0	-13	-913	4.02	4.02	4.02	4.02	2	0.13	0.06	0.36	0.00	0.00	22.3
7	38	-575	2391	-15	0	-13	-1568	4.02	4.02	4.02	4.02	2	0.23	0.07	0.42	0.00	0.00	22.3
8	38	-1404	2097	30	0	92	-950	4.02	4.02	4.02	4.02	2	0.14	0.06	0.36	0.00	0.00	22.3
9	38	-560	2409	28	0	92	-1606	4.02	4.02	4.02	4.02	2	0.24	0.07	0.42	0.00	0.00	22.3
10	38	-1141	2166	-65	0	-136	-1098	4.02	4.02	4.02	4.02	2	0.16	0.06	0.38	0.00	0.00	22.3
11	38	-888	2260	-65	0	-136	-1295	4.02	4.02	4.02	4.02	2	0.19	0.07	0.39	0.00	0.00	22.3
12	38	-1090	2228	80	0	215	-1224	4.02	4.02	4.02	4.02	2	0.18	0.06	0.39	0.00	0.00	22.3
13	38	-837	2321	79	0	215	-1421	4.02	4.02	4.02	4.02	2	0.21	0.07	0.41	0.00	0.00	22.3
14	38	-1419	2079	-13	0	-13	-913	4.02	4.02	4.02	4.02	2	0.13	0.06	0.36	0.00	0.00	22.3
15	38	-575	2391	-15	0	-13	-1568	4.02	4.02	4.02	4.02	2	0.23	0.07	0.42	0.00	0.00	22.3
16	38	-1404	2097	30	0	92	-950	4.02	4.02	4.02	4.02	2	0.14	0.06	0.36	0.00	0.00	22.3
17	38	-560	2409	28	0	92	-1606	4.02	4.02	4.02	4.02	2	0.24	0.07	0.42	0.00	0.00	22.3
18	38	-2077	2885	-180	0	-385	1549	4.02	4.02	4.02	4.02	3	0.21	0.08	0.49	0.00	0.00	22.3
19	38	-1837	3081	254	0	663	-1571	4.02	4.02	4.02	4.02	3	0.21	0.09	0.53	0.00	0.00	22.3
20	38	-1263	3219	20	0	94	-1851	4.02	4.02	4.02	4.02	3	0.26	0.09	0.56	0.00	0.00	22.3
37	38	-1929	2744	-334	0	-763	1506	4.02	4.02	4.02	4.02	3	0.20	0.08	0.47	0.00	0.00	22.3
38	38	-1529	3069	390	0	984	-1750	4.02	4.02	4.02	4.02	3	0.24	0.09	0.53	0.00	0.00	22.3
39	38	-572	3299	-0	0	36	-2217	4.02	4.02	4.02	4.02	3	0.31	0.10	0.58	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	75	-1286	2066	10	0	48	1461	4.02	4.02	4.02	4.02	3	0.20	0.06	0.36	0.00	0.00	22.3
2	75	-1141	1511	-65	0	-112	1169	4.02	4.02	4.02	4.02	2	0.17	0.04	0.26	0.00	0.00	22.3
3	75	-888	1605	-65	0	-112	1113	4.02	4.02	4.02	4.02	2	0.16	0.05	0.28	0.00	0.00	22.3
4	75	-1090	1573	80	0	185	1135	4.02	4.02	4.02	4.02	2	0.17	0.05	0.27	0.00	0.00	22.3
5	75	-837	1666	79	0	186	1089	4.02	4.02	4.02	4.02	2	0.16	0.05	0.29	0.00	0.00	22.3
6	75	-1419	1424	-13	0	-8	1223	4.02	4.02	4.02	4.02	2	0.18	0.04	0.25	0.00	0.00	22.3
7	75	-575	1736	-15	0	-8	1072	4.02	4.02	4.02	4.02	2	0.16	0.05	0.30	0.00	0.00	22.3
8	75	-1404	1442	30	0	81	1213	4.02	4.02	4.02	4.02	2	0.18	0.04	0.25	0.00	0.00	22.3
9	75	-560	1754	28	0	82	1068	4.02	4.02	4.02	4.02	2	0.16	0.05	0.31	0.00	0.00	22.3
10	75	-1141	1511	-65	0	-112	1169	4.02	4.02	4.02	4.02	2	0.17	0.04	0.26	0.00	0.00	22.3
11	75	-888	1605	-65	0	-112	1113	4.02	4.02	4.02	4.02	2	0.16	0.05	0.28	0.00	0.00	22.3
12	75	-1090	1573	80	0	185	1135	4.02	4.02	4.02	4.02	2	0.17	0.05	0.27	0.00	0.00	22.3
13	75	-837	1666	79	0	186	1089	4.02	4.02	4.02	4.02	2	0.16	0.05	0.29	0.00	0.00	22.3
14	75	-1419	1424	-13	0	-8	1223	4.02	4.02	4.02	4.02	2	0.18	0.04	0.25	0.00	0.00	22.3
15	75	-575	1736	-15	0	-8	1072	4.02	4.02	4.02	4.02	2	0.16	0.05	0.30	0.00	0.00	22.3
16	75	-1404	1442	30	0	81	1213	4.02	4.02	4.02	4.02	2	0.18	0.04	0.25	0.00	0.00	22.3
17	75	-560	1754	28	0	82	1068	4.02	4.02	4.02	4.02	2	0.16	0.05	0.31	0.00	0.00	22.3
18	75	-2077	1954	-180	0	-318	1762	4.02	4.02	4.02	4.02	3	0.24	0.06	0.33	0.00	0.00	22.3
19	75	-1837	2150	254	0	567	1653	4.02	4.02	4.02	4.02	3	0.22	0.06	0.37	0.00	0.00	22.3
20	75	-1263	2288	20	0	86	1580	4.02	4.02	4.02	4.02	3	0.22	0.07	0.40	0.00	0.00	22.3
37	75	-1929	1853	-334	0	-638	1699	4.02	4.02	4.02	4.02	3	0.23	0.05	0.32	0.00	0.00	22.3
38	75	-1529	2178	390	0	837	1516	4.02	4.02	4.02	4.02	3	0.21	0.06	0.37	0.00	0.00	22.3
39	75	-572	2408	-0	0	36	1461	4.02	4.02	4.02	4.02	3	0.21	0.07	0.42	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	112	-1286	1214	10	0	44	1461	4.02	4.02	4.02	4.02	3	0.20	0.04	0.21	0.00	0.00	22.3
2	112	-1141	856	-65	0	-88	1169	4.02	4.02	4.02	4.02	2	0.17	0.02	0.15	0.00	0.00	22.3
3	112	-888	950	-65	0	-87	1113	4.02	4.02	4.02	4.02	2	0.16	0.03	0.17	0.00	0.00	22.3
4	112	-1090	918	80	0	155	1135	4.02	4.02	4.02	4.02	2	0.17	0.03	0.16	0.00	0.00	22.3
5	112	-837	1011	79	0	156	1089	4.02	4.02	4.02	4.02	2	0.16	0.03	0.18	0.00	0.00	22.3
6	112	-1419	769	-13	0	-3	1223	4.02	4.02	4.02	4.02	2	0.18	0.02	0.13	0.00	0.00	22.3
7	112	-575	1081	-15	0	-2	1072	4.02	4.02	4.02	4.02	2	0.16	0.03	0.19	0.00	0.00	22.3
8	112	-1404	787	30	0	70	1213	4.02	4.02	4.02	4.02	2	0.18	0.02	0.14	0.00	0.00	22.3
9	112	-560	1099	28	0	71	1068	4.02	4.02	4.02	4.02	2	0.16	0.03	0.19	0.00	0.00	22.3
10	112	-1141	856	-65	0	-88	1169	4.02	4.02	4.02	4.02	2	0.17	0.02	0.15	0.00	0.00	22.3
11	112	-888	950	-65	0	-87	1113	4.02	4.02	4.02	4.02	2	0.16	0.03	0.17	0.00	0.00	22.3
12	112	-1090	918	80	0	155	1135	4.02	4.02	4.02	4.02	2	0.17	0.03	0.16	0.00	0.00	22.3
13	112	-837	1011	79	0	156	1089	4.02	4.02	4.02	4.02	2	0.16	0.03	0.18	0.00	0.00	22.3
14	112	-1419	769	-13	0	-3	1223	4.02	4.02	4.02	4.02	2	0.18	0.02	0.13	0.00	0.00	22.3
15	112	-575	1081	-15	0	-2	1072	4.02	4.02	4.02	4.02	2	0.16	0.03	0.19	0.00	0.00	22.3
16	112	-1404	787	30	0	70	1213	4.02	4.02	4.02	4.02	2	0.18	0.02	0.14	0.00	0.00	22.3
17	112	-560	1099	28	0	71	1068	4.02	4.02	4.02	4.02	2	0.16	0.03	0.19	0.00	0.00	22.3

18	112	-2077	1022	-180	0	-250	1762	4.02	4.02	4.02	4.02	3	0.24	0.03	0.17	0.00	0.00	22.3
19	112	-1837	1218	254	0	472	1653	4.02	4.02	4.02	4.02	3	0.22	0.04	0.21	0.00	0.00	22.3
20	112	-1263	1356	20	0	79	1580	4.02	4.02	4.02	4.02	3	0.22	0.04	0.23	0.00	0.00	22.3
37	112	-1929	961	-334	0	-513	1699	4.02	4.02	4.02	4.02	3	0.23	0.03	0.16	0.00	0.00	22.3
38	112	-1529	1286	390	0	691	1516	4.02	4.02	4.02	4.02	3	0.21	0.04	0.22	0.00	0.00	22.3
39	112	-572	1516	-0	0	36	1461	4.02	4.02	4.02	4.02	3	0.21	0.04	0.27	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	150	-1286	363	10	0	41	1461	4.02	4.02	4.02	4.02	3	0.20	0.01	0.06	0.00	0.00	22.3
2	150	-1141	201	-65	0	-64	1169	4.02	4.02	4.02	4.02	2	0.17	0.01	0.03	0.00	0.00	22.3
3	150	-888	295	-65	0	-63	1113	4.02	4.02	4.02	4.02	2	0.16	0.01	0.05	0.00	0.00	22.3
4	150	-1090	263	80	0	126	1135	4.02	4.02	4.02	4.02	2	0.17	0.01	0.05	0.00	0.00	22.3
5	150	-837	356	79	0	126	1089	4.02	4.02	4.02	4.02	2	0.16	0.01	0.06	0.00	0.00	22.3
6	150	-1419	114	-13	0	2	1223	4.02	4.02	4.02	4.02	2	0.18	0.00	0.02	0.00	0.00	22.3
7	150	-575	426	-15	0	4	1072	4.02	4.02	4.02	4.02	2	0.16	0.01	0.07	0.00	0.00	22.3
8	150	-1404	132	30	0	59	1213	4.02	4.02	4.02	4.02	2	0.18	0.00	0.02	0.00	0.00	22.3
9	150	-560	444	28	0	61	1068	4.02	4.02	4.02	4.02	2	0.16	0.01	0.08	0.00	0.00	22.3
10	150	-1141	201	-65	0	-64	1169	4.02	4.02	4.02	4.02	2	0.17	0.01	0.03	0.00	0.00	22.3
11	150	-888	295	-65	0	-63	1113	4.02	4.02	4.02	4.02	2	0.16	0.01	0.05	0.00	0.00	22.3
12	150	-1090	263	80	0	126	1135	4.02	4.02	4.02	4.02	2	0.17	0.01	0.05	0.00	0.00	22.3
13	150	-837	356	79	0	126	1089	4.02	4.02	4.02	4.02	2	0.16	0.01	0.06	0.00	0.00	22.3
14	150	-1419	114	-13	0	2	1223	4.02	4.02	4.02	4.02	2	0.18	0.00	0.02	0.00	0.00	22.3
15	150	-575	426	-15	0	4	1072	4.02	4.02	4.02	4.02	2	0.16	0.01	0.07	0.00	0.00	22.3
16	150	-1404	132	30	0	59	1213	4.02	4.02	4.02	4.02	2	0.18	0.00	0.02	0.00	0.00	22.3
17	150	-560	444	28	0	61	1068	4.02	4.02	4.02	4.02	2	0.16	0.01	0.08	0.00	0.00	22.3
18	150	-2077	90	-180	0	-182	1762	4.02	4.02	4.02	4.02	3	0.24	0.01	0.03	0.00	0.00	22.3
19	150	-1837	286	254	0	377	1653	4.02	4.02	4.02	4.02	3	0.22	0.01	0.05	0.00	0.00	22.3
20	150	-1263	424	20	0	71	1580	4.02	4.02	4.02	4.02	3	0.22	0.01	0.07	0.00	0.00	22.3
37	150	-1929	69	-334	0	-387	1699	4.02	4.02	4.02	4.02	3	0.23	0.01	0.05	0.00	0.00	22.3
38	150	-1529	395	390	0	545	1516	4.02	4.02	4.02	4.02	3	0.21	0.01	0.07	0.00	0.00	22.3
39	150	-572	625	-0	0	36	1461	4.02	4.02	4.02	4.02	3	0.21	0.02	0.11	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	188	-1286	-489	10	0	37	1461	4.02	4.02	4.02	4.02	3	0.20	0.01	0.08	0.00	0.00	22.3
2	188	-1141	-454	-65	0	-39	1169	4.02	4.02	4.02	4.02	2	0.17	0.01	0.08	0.00	0.00	22.3
3	188	-888	-360	-65	0	-39	1113	4.02	4.02	4.02	4.02	2	0.16	0.01	0.06	0.00	0.00	22.3
4	188	-1090	-392	80	0	96	1135	4.02	4.02	4.02	4.02	2	0.17	0.01	0.07	0.00	0.00	22.3
5	188	-837	-299	79	0	96	1089	4.02	4.02	4.02	4.02	2	0.16	0.01	0.05	0.00	0.00	22.3
6	188	-1419	-542	-13	0	7	1223	4.02	4.02	4.02	4.02	2	0.18	0.02	0.09	0.00	0.00	22.3
7	188	-575	-230	-15	0	9	1072	4.02	4.02	4.02	4.02	2	0.16	0.01	0.04	0.00	0.00	22.3
8	188	-1404	-523	30	0	47	1213	4.02	4.02	4.02	4.02	2	0.18	0.02	0.09	0.00	0.00	22.3
9	188	-560	-211	28	0	50	1068	4.02	4.02	4.02	4.02	2	0.16	0.01	0.04	0.00	0.00	22.3
10	188	-1141	-454	-65	0	-39	1169	4.02	4.02	4.02	4.02	2	0.17	0.01	0.08	0.00	0.00	22.3
11	188	-888	-360	-65	0	-39	1113	4.02	4.02	4.02	4.02	2	0.16	0.01	0.06	0.00	0.00	22.3
12	188	-1090	-392	80	0	96	1135	4.02	4.02	4.02	4.02	2	0.17	0.01	0.07	0.00	0.00	22.3
13	188	-837	-299	79	0	96	1089	4.02	4.02	4.02	4.02	2	0.16	0.01	0.05	0.00	0.00	22.3
14	188	-1419	-542	-13	0	7	1223	4.02	4.02	4.02	4.02	2	0.18	0.02	0.09	0.00	0.00	22.3
15	188	-575	-230	-15	0	9	1072	4.02	4.02	4.02	4.02	2	0.16	0.01	0.04	0.00	0.00	22.3
16	188	-1404	-523	30	0	47	1213	4.02	4.02	4.02	4.02	2	0.18	0.02	0.09	0.00	0.00	22.3
17	188	-560	-211	28	0	50	1068	4.02	4.02	4.02	4.02	2	0.16	0.01	0.04	0.00	0.00	22.3
18	188	-2077	-842	-180	0	-115	1762	4.02	4.02	4.02	4.02	3	0.24	0.02	0.14	0.00	0.00	22.3
19	188	-1837	-646	254	0	282	1653	4.02	4.02	4.02	4.02	3	0.22	0.02	0.11	0.00	0.00	22.3
20	188	-1263	-508	20	0	64	1580	4.02	4.02	4.02	4.02	3	0.22	0.01	0.09	0.00	0.00	22.3
37	188	-1929	-822	-334	0	-262	1699	4.02	4.02	4.02	4.02	3	0.23	0.02	0.14	0.00	0.00	22.3
38	188	-1529	-497	390	0	398	1516	4.02	4.02	4.02	4.02	3	0.21	0.01	0.09	0.00	0.00	22.3
39	188	-572	-267	-0	0	36	1461	4.02	4.02	4.02	4.02	3	0.21	0.01	0.05	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	225	-1286	-1341	10	0	33	1461	4.02	4.02	4.02	4.02	3	0.20	0.04	0.23	0.00	0.00	22.3
2	225	-1141	-1109	-65	0	-15	1169	4.02	4.02	4.02	4.02	2	0.17	0.03	0.19	0.00	0.00	22.3
3	225	-888	-1015	-65	0	-14	1113	4.02	4.02	4.02	4.02	2	0.16	0.03	0.18	0.00	0.00	22.3
4	225	-1090	-1047	80	0	66	1135	4.02	4.02	4.02	4.02	2	0.17	0.03	0.18	0.00	0.00	22.3
5	225	-837	-954	79	0	66	1089	4.02	4.02	4.02	4.02	2	0.16	0.03	0.17	0.00	0.00	22.3
6	225	-1419	-1197	-13	0	12	1223	4.02	4.02	4.02	4.02	2	0.18	0.03	0.21	0.00	0.00	22.3
7	225	-575	-885	-15	0	15	1072	4.02	4.02	4.02	4.02	2	0.16	0.03	0.16	0.00	0.00	22.3
8	225	-1404	-1178	30	0	36	1213	4.02	4.02	4.02	4.02	2	0.18	0.03	0.20	0.00	0.00	22.3
9	225	-560	-866	28	0	39	1068	4.02	4.02	4.02	4.02	2	0.16	0.03	0.15	0.00	0.00	22.3
10	225	-1141	-1109	-65	0	-15	1169	4.02	4.02	4.02	4.02	2	0.17	0.03	0.19	0.00	0.00	22.3
11	225	-888	-1015	-65	0	-14	1113	4.02	4.02	4.02	4.02	2	0.16	0.03	0.18	0.00	0.00	22.3
12	225	-1090	-1047	80	0	66	1135	4.02	4.02	4.02	4.02	2	0.17	0.03	0.18	0.00	0.00	22.3
13	225	-837	-954	79	0	66	1089	4.02	4.02	4.02	4.02	2	0.16	0.03	0.17	0.00	0.00	22.3
14	225	-1419	-1197	-13	0	12	1223	4.02	4.02	4.02	4.02	2	0.18	0.03	0.21	0.00	0.00	22.3
15	225	-575	-885	-15	0	15	1072	4.02	4.02	4.02	4.02	2	0.16	0.03	0.16	0.00	0.00	22.3
16	225	-1404	-1178	30	0	36	1213	4.02	4.02	4.02	4.02	2	0.18	0.03	0.20	0.00	0.00	22.3
17	225	-560	-866	28	0	39	1068	4.02	4.02	4.02	4.02	2	0.16	0.03	0.15	0.00	0.00	22.3
18	225	-2077	-1773	-180	0	-47	1762	4.02	4.02	4.02	4.02	3	0.24	0.05	0.30	0.00	0.00	22.3
19	225	-1837	-1577	254	0	186	1653	4.02	4.02	4.02	4.02	3	0.22	0.05	0.27	0.00	0.00	22.3
20	225	-1263	-1439	20	0	56	1580	4.02	4.02	4.02	4.02	3	0.22	0.04	0.25	0.00	0.00	22.3
37	225	-1929	-1714	-334	0	-136	1699	4.02	4.02	4.02	4.02	3	0.23	0.05	0.29	0.00	0.00	22.3
38	225	-1529	-1389	390	0	252	1516	4.02	4.02	4.02	4.02	3	0.21	0.04	0.24	0.00	0.00	22.3
39	225	-572	-1159	-0	0	36	1461	4.02	4.02	4.02	4.02	3	0.21	0.03	0.20	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	262	-1286	-2192	10	0	30	1461	4.02	4.02	4.02	4.02	3	0.20	0.06	0.38	0.00	0.00	22.3
2	262	-1141	-1764	-65	0	9	1169	4.02	4.02	4.02	4.02	2	0.17	0.05	0.31	0.00	0.00	22.3
3	262	-888	-1670	-65	0	10	1113	4.02	4.02	4.02	4.02	2	0.16	0.05	0.29	0.00	0.00	22.3
4	262	-1090	-1702	80	0	36	1135	4.02	4.02	4.02	4.02	2	0.17	0.05	0.30	0.00	0.00	22.3
5	262	-837	-1609	79	0	37	1089	4.02	4.02	4.02	4.02	2	0.16	0.05	0.28	0.00	0.00	22.3
6	262	-1419	-1852	-13	0	17	1183	4.02	4.02	4.02	4.02	2	0.17	0.05	0.32	0.00	0.00	22.3
7	262	-575	-1540	-15	0	21	1072	4.02	4.02	4.02	4.02	2	0.16	0.04	0.27	0.00	0.00	22.3
8	262	-1404	-1833	30	0	25	1184	4.02	4.02	4.02	4.02	2	0.17	0.05	0.32	0.00	0.00	22.3
9	262	-560	-1521	28	0	29	1068	4.02	4.02	4.02	4.02	2	0.16	0.04	0.27	0.00	0.00	22.3
10	262	-1141	-1764	-65	0	9	1169	4.02	4.02	4.02	4.02	2	0.17	0.05	0.31	0.00	0.00	22.3
11	262	-888	-1670	-65	0	10	1113	4.02	4.02	4.02	4.02	2	0.16	0.05	0.29	0.00	0.00	22.3
12	262	-1090	-1702	80	0	36	1135	4.02	4.02	4.02	4.02	2	0.17	0.05	0.30	0.00	0.00	22.3
13	262	-837	-1609	79	0	37	1089	4.02	4.02	4.02	4.02	2	0.16	0.05	0.28	0.00	0.00	22.3
14	262	-1419	-1852	-13	0	17	1183	4.02	4.02	4.02	4.02	2	0.17	0.05	0.32	0.00	0.00	22.3
15	262	-575	-1540	-15	0	21	1072	4.02	4.02	4.02	4.02	2	0.16	0.04	0.27	0.00	0.00	22.3
16	262	-1404	-1833	30	0	25	1184	4.02	4.02	4.02	4.02	2	0.17	0.05	0.32	0.00	0.00	22.3
17	262	-560	-1521	28	0	29	1068	4.02	4.02	4.02	4.02	2	0.16	0.04	0.27	0.00	0.00	22.3
18	262	-2077	-2705	-180	0	21	1662	4.02	4.02	4.02	4.02	3	0.22	0.08	0.46	0.00	0.00	22.3
19	262	-1837	-2509	254	0	91	1653	4.02	4.02	4.02	4.02	3	0.22	0.07	0.43	0.00	0.00	22.3
20	262	-1263	-2371	20	0	49	1580	4.02	4.02	4.02	4.02	3	0.22	0.07	0.41	0.00	0.00	22.3
37	262	-1929	-2606	-334	0	-11	1591	4.02	4.02	4.02	4.02	3	0.22	0.07	0.44	0.00	0.00	22.3
38	262	-1529	-2280	390	0	106	1516	4.02	4.02	4.02	4.02	3	0.21	0.07	0.39	0.00	0.00	22.3
39	262	-572	-2050	-0	0	36	1461	4.02	4.02	4.02	4.02	3	0.21	0.06	0.36	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	300	-1286	-3044	10	0	26	-2091	4.02	4.02	4.02	4.02	3	0.29	0.09	0.53	0.00	0.00	22.3
2	300	-1141	-2419	-65	0	33	-1718	4.02	4.02	4.02	4.02	2	0.25	0.07	0.42	0.00	0.00	22.3
3	300	-888	-2325	-65	0	35	-1587	4.02	4.02	4.02	4.02	2	0.23	0.07	0.41	0.00	0.00	22.3
4	300	-1090	-2357	80	0	6	-1629	4.02	4.02	4.02	4.02	2	0.24	0.07	0.41	0.00	0.00	22.3
5	300	-837	-2264	79	0	7	-1498	4.02	4.02	4.02	4.02	2	0.22	0.07	0.40	0.00	0.00	22.3
6	300	-1419	-2507	-13	0	22	-1841	4.02	4.02	4.02	4.02	2	0.27	0.07	0.43	0.00	0.00	22.3
7	300	-575	-2195	-15	0	26	-1403	4.02	4.02	4.02	4.02	2	0.21	0.06	0.39	0.00	0.00	22.3
8	300	-1404	-2488	30	0	14	-1814	4.02	4.02	4.02	4.02	2	0.26	0.07	0.43	0.00	0.00	22.3
9	300	-560	-2176	28	0	18	-1376	4.02	4.02	4.02	4.02	2	0.21	0.06	0.38	0.00	0.00	22.3
10	300	-1141	-2419	-65	0	33	-1718	4.02	4.02	4.02	4.02	2	0.25	0.07	0.42	0.00	0.00	22.3
11	300	-888	-2325	-65	0	35	-1587	4.02	4.02	4.02	4.02	2	0.23	0.07	0.41	0.00	0.00	22.3
12	300	-1090	-2357	80	0	6	-1629	4.02	4.02	4.02	4.02	2	0.24	0.07	0.41	0.00	0.00	22.3
13	300	-837	-2264	79	0	7	-1498	4.02	4.02	4.02	4.02	2	0.22	0.07	0.40	0.00	0.00	22.3
14	300	-1419	-2507	-13	0	22	-1841	4.02	4.02	4.02	4.02	2	0.27	0.07	0.43	0.00	0.00	22.3
15	300	-575	-2195	-15	0	26	-1403	4.02	4.02	4.02	4.02	2	0.21	0.06	0.39	0.00	0.00	22.3
16	300	-1404	-2488	30	0	14	-1814	4.02	4.02	4.02	4.02	2	0.26	0.07	0.43	0.00	0.00	22.3
17	300	-560	-2176	28	0	18	-1376	4.02	4.02	4.02	4.02	2	0.21	0.06	0.38	0.00	0.00	22.3
18	300	-2077	-3637	-180	0	89	-2737	4.02	4.02	4.02	4.02	3	0.37	0.10	0.62	0.00	0.00	22.3
19	300	-1837	-3441	254	0	-4	-2455	4.02	4.02	4.02	4.02	3	0.33	0.10	0.59	0.00	0.00	22.3
20	300	-1263	-3303	20	0	41	-2251	4.02	4.02	4.02	4.02	3	0.31	0.10	0.57	0.00	0.00	22.3
37	300	-1929	-3498	-334	0	114	-2643	4.02	4.02	4.02	4.02	3	0.36	0.10	0.60	0.00	0.00	22.3
38	300	-1529	-3172	390	0	-41	-2173	4.02	4.02	4.02	4.02	3	0.30	0.09	0.54	0.00	0.00	22.3
39	300	-572	-2942	-0	0	36	-1833	4.02	4.02	4.02	4.02	3	0.26	0.09	0.52	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	338	-1286	-3895	10	0	23	-3471	4.02	4.02	4.02	4.02	3	0.48	0.11	0.67	0.00	0.00	22.3
2	338	-1141	-3074	-65	0	58	-2799	4.02	4.02	4.02	4.02	2	0.41	0.09	0.53	0.00	0.00	22.3
3	338	-888	-2980	-65	0	59	-2645	4.02	4.02	4.02	4.02	2	0.39	0.09	0.52	0.00	0.00	22.3
4	338	-1090	-3012	80	0	-24	-2695	4.02	4.02	4.02	4.02	2	0.40	0.09	0.52	0.00	0.00	22.3
5	338	-837	-2919	79	0	-23	-2541	4.02	4.02	4.02	4.02	2	0.38	0.08	0.51	0.00	0.00	22.3
6	338	-1419	-3162	-13	0	27	-2943	4.02	4.02	4.02	4.02	2	0.43	0.09	0.54	0.00	0.00	22.3
7	338	-575	-2850	-15	0	32	-2429	4.02	4.02	4.02	4.02	2	0.36	0.08	0.50	0.00	0.00	22.3
8	338	-1404	-3143	30	0	3	-2912	4.02	4.02	4.02	4.02	2	0.42	0.09	0.54	0.00	0.00	22.3
9	338	-560	-2831	28	0	8	-2398	4.02	4.02	4.02	4.02	2	0.36	0.08	0.50	0.00	0.00	22.3
10	338	-1141	-3074	-65	0	58	-2799	4.02	4.02	4.02	4.02	2	0.41	0.09	0.53	0.00	0.00	22.3
11	338	-888	-2980	-65	0	59	-2645	4.02	4.02	4.02	4.02	2	0.39	0.09	0.52	0.00	0.00	22.3
12	338	-1090	-3012	80	0	-24	-2695	4.02	4.02	4.02	4.02	2	0.40	0.09	0.52	0.00	0.00	22.3
13	338	-837	-2919	79	0	-23	-2541	4.02	4.02	4.02	4.02	2	0.38	0.08	0.51	0.00	0.00	22.3
14	338	-1419	-3162	-13	0	27	-2943	4.02	4.02	4.02	4.02	2	0.43	0.09	0.54	0.00	0.00	22.3
15	338	-575	-2850	-15	0	32	-2429	4.02	4.02	4.02	4.02	2	0.36	0.08	0.50	0.00	0.00	22.3
16	338	-1404	-3143	30	0	3	-2912	4.02	4.02	4.02	4.02	2	0.42	0.09	0.54	0.00	0.00	22.3
17	338	-560	-2831	28	0	8	-2398	4.02	4.02	4.02	4.02	2	0.36	0.08	0.50	0.00	0.00	22.3
18	338	-2077	-4568	-180	0	156	-4322	4.02	4.02	4.02	4.02	3	0.58	0.13	0.77	0.00	0.00	22.3
19	338	-1837	-4372	254	0	-100	-3992	4.02	4.02	4.02	4.02	3	0.54	0.13	0.75	0.00	0.00	22.3
20	338	-1263	-4234	20	0	34	-3755	4.02	4.02	4.02	4.02	3	0.52	0.12	0.73	0.00	0.00	22.3
37	338	-1929	-4389	-334	0	240	-4164	4.02	4.02	4.02	4.02	3	0.57	0.13	0.75	0.00	0.00	22.3
38	338	-1529	-4063	390	0	-187	-3615	4.02	4.02	4.02	4.02	3	0.50	0.12	0.70	0.00	0.00	22.3
39	338	-572	-3833	-0	0	36	-3219	4.02	4.02	4.02	4.02	3	0.45	0.11	0.67	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	375	-1286	-4747	10	0	19	-3471	4.02	4.02	4.02	4.02	3	0.48	0.14	0.82	0.00	0.00	22.3
2	375	-1141	-3729	-65	0	82	-2799	4.02	4.02	4.02	4.02	2	0.41	0.11	0.65	0.00	0.00	22.3
3	375	-888	-3635	-65	0	83	-2645	4.02	4.02	4.02	4.02	2	0.39	0.11	0.63	0.00	0.00	22.3
4	375	-1090	-3667	80	0	-54	-2695	4.02	4.02	4.02	4.02	2	0.40	0.11	0.64	0.00	0.00	22.3
5	375	-837	-3574	79	0	-53	-2541	4.02	4.02	4.02	4.02	2	0.38	0.10	0.62	0.00	0.00	22.3
6	375	-1419	-3817	-13	0	32	-2943	4.02	4.02	4.02	4.02	2	0.43	0.11	0.66	0.00	0.00	22.3
7	375	-575	-3505	-15	0	38	-2429	4.02	4.02	4.02	4.02	2	0.36	0.10	0.62	0.00	0.00	22.3
8	375	-1404	-3798	30	0	-9	-2912	4.02	4.02	4.02	4.02	2	0.42	0.11	0.65	0.00	0.00	22.3
9	375	-560	-3486	28	0	-3	-2398	4.02	4.02	4.02	4.02	2	0.36	0.10	0.61	0.00	0.00	22.3
10	375	-1141	-3729	-65	0	82	-2799	4.02	4.02	4.02	4.02	2	0.41	0.11	0.65	0.00	0.00	22.3
11	375	-888	-3635	-65	0	83	-2645	4.02	4.02	4.02	4.02	2	0.39	0.11	0.63	0.00	0.00	22.3
12	375	-1090	-3667	80	0	-54	-2695	4.02	4.02	4.02	4.02	2	0.40	0.11	0.64	0.00	0.00	22.3
13	375	-837	-3574	79	0	-53	-2541	4.02	4.02	4.02	4.02	2	0.38	0.10	0.62	0.00	0.00	22.3
14	375	-1419	-3817	-13	0	32	-2943	4.02	4.02	4.02	4.02	2	0.43	0.11	0.66	0.00	0.00	22.3
15	375	-575	-3505	-15	0	38	-2429	4.02	4.02	4.02	4.02	2	0.36	0.10	0.62	0.00	0.00	22.3
16	375	-1404	-3798	30	0	-9	-2912	4.02	4.02	4.02	4.02	2	0.42	0.11	0.65	0.00	0.00	22.3
17	375	-560	-3486	28	0	-3	-2398	4.02	4.02	4.02	4.02	2	0.36	0.10	0.61	0.00	0.00	22.3
18	375	-2077	-5500	-180	0	224	-4322	4.02	4.02	4.02	4.02	3	0.58	0.16	0.93	0.00	0.00	22.3
19	375	-1837	-5304	254	0	-195	-3992	4.02	4.02	4.02	4.02	3	0.54	0.15	0.90	0.00	0.00	22.3
20	375	-1263	-5166	20	0	26	-3755	4.02	4.02	4.02	4.02	3	0.52	0.15	0.89	0.00	0.00	22.3
37	375	-1929	-5281	-334	0	365	-4164	4.02	4.02	4.02	4.02	3	0.57	0.15	0.90	0.00	0.00	22.3
38	375	-1529	-4955	390	0	-333	-3615	4.02	4.02	4.02	4.02	3	0.50	0.14	0.85	0.00	0.00	22.3
39	375	-572	-4725	-0	0	36	-3219	4.02	4.02	4.02	4.02	3	0.45	0.14	0.83	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

Nome travata: **trave_507_IP1** Descrizione: **Trave_5 26-25-24-23**
ASTA NUM. 21 NI 165 NF 210 SEZ. Rp B= 0.300 H= 0.500 (trave)

categoria: p.p. y Permanente Neve qy tot.
qy medio: 375.00 1371.75 142.50 1889.25 daN/m

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	campo	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm

1	0	-876	4408	11	0	17	-2683	4.02	4.02	4.02	4.02	3	0.38	0.13	0.77	0.00	0.00	22.3
2	0	-721	3340	-15	0	8	-1984	4.02	4.02	4.02	4.02	2	0.29	0.10	0.58	0.00	0.00	22.3
3	0	-613	3419	-16	0	9	-2114	4.02	4.02	4.02	4.02	2	0.31	0.10	0.60	0.00	0.00	22.3
4	0	-735	3362	33	0	17	-2013	4.02	4.02	4.02	4.02	2	0.30	0.10	0.59	0.00	0.00	22.3
5	0	-627	3441	31	0	18	-2144	4.02	4.02	4.02	4.02	2	0.32	0.10	0.60	0.00	0.00	22.3
6	0	-851	3256	3	0	9	-1842	4.02	4.02	4.02	4.02	2	0.27	0.09	0.57	0.00	0.00	22.3
7	0	-493	3518	-1	0	14	-2277	4.02	4.02	4.02	4.02	2	0.34	0.10	0.62	0.00	0.00	22.3
8	0	-855	3263	18	0	12	-1851	4.02	4.02	4.02	4.02	2	0.27	0.09	0.57	0.00	0.00	22.3
9	0	-497	3525	13	0	17	-2285	4.02	4.02	4.02	4.02	2	0.34	0.10	0.62	0.00	0.00	22.3
10	0	-721	3340	-15	0	8	-1984	4.02	4.02	4.02	4.02	2	0.29	0.10	0.58	0.00	0.00	22.3
11	0	-613	3419	-16	0	9	-2114	4.02	4.02	4.02	4.02	2	0.31	0.10	0.60	0.00	0.00	22.3
12	0	-735	3362	33	0	17	-2013	4.02	4.02	4.02	4.02	2	0.30	0.10	0.59	0.00	0.00	22.3
13	0	-627	3441	31	0	18	-2144	4.02	4.02	4.02	4.02	2	0.32	0.10	0.60	0.00	0.00	22.3
14	0	-851	3256	3	0	9	-1842	4.02	4.02	4.02	4.02	2	0.27	0.09	0.57	0.00	0.00	22.3
15	0	-493	3518	-1	0	14	-2277	4.02	4.02	4.02	4.02	2	0.34	0.10	0.62	0.00	0.00	22.3

16	0	-855	3263	18	0	12	-1851	4.02	4.02	4.02	4.02	2	0.27	0.09	0.57	0.00	0.00	22.3
17	0	-497	3525	13	0	17	-2285	4.02	4.02	4.02	4.02	2	0.34	0.10	0.62	0.00	0.00	22.3
18	0	-1190	4611	-50	0	10	-2595	4.02	4.02	4.02	4.02	3	0.36	0.13	0.80	0.00	0.00	22.3
19	0	-1187	4708	90	0	32	-2741	4.02	4.02	4.02	4.02	3	0.38	0.14	0.82	0.00	0.00	22.3
20	0	-879	4866	5	0	23	-3013	4.02	4.02	4.02	4.02	3	0.42	0.14	0.85	0.00	0.00	22.3
37	0	-1078	4422	-100	0	1	-2503	4.02	4.02	4.02	4.02	3	0.35	0.13	0.77	0.00	0.00	22.3
38	0	-1073	4584	134	0	39	-2748	4.02	4.02	4.02	4.02	3	0.38	0.13	0.80	0.00	0.00	22.3
39	0	-560	4847	-8	0	23	-3201	4.02	4.02	4.02	4.02	3	0.45	0.14	0.85	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	38	-876	3556	11	0	13	-2683	4.02	4.02	4.02	4.02	3	0.38	0.10	0.62	0.00	0.00	22.3
2	38	-721	2685	-15	0	14	-1984	4.02	4.02	4.02	4.02	2	0.29	0.08	0.47	0.00	0.00	22.3
3	38	-613	2764	-16	0	15	-2114	4.02	4.02	4.02	4.02	2	0.31	0.08	0.49	0.00	0.00	22.3
4	38	-735	2707	33	0	4	-2013	4.02	4.02	4.02	4.02	2	0.30	0.08	0.47	0.00	0.00	22.3
5	38	-627	2786	31	0	6	-2144	4.02	4.02	4.02	4.02	2	0.32	0.08	0.49	0.00	0.00	22.3
6	38	-851	2601	3	0	8	-1842	4.02	4.02	4.02	4.02	2	0.27	0.08	0.45	0.00	0.00	22.3
7	38	-493	2863	-1	0	15	-2277	4.02	4.02	4.02	4.02	2	0.34	0.08	0.50	0.00	0.00	22.3
8	38	-855	2608	18	0	5	-1851	4.02	4.02	4.02	4.02	2	0.27	0.08	0.46	0.00	0.00	22.3
9	38	-497	2870	13	0	12	-2285	4.02	4.02	4.02	4.02	2	0.34	0.08	0.51	0.00	0.00	22.3
10	38	-721	2685	-15	0	14	-1984	4.02	4.02	4.02	4.02	2	0.29	0.08	0.47	0.00	0.00	22.3
11	38	-613	2764	-16	0	15	-2114	4.02	4.02	4.02	4.02	2	0.31	0.08	0.49	0.00	0.00	22.3
12	38	-735	2707	33	0	4	-2013	4.02	4.02	4.02	4.02	2	0.30	0.08	0.47	0.00	0.00	22.3
13	38	-627	2786	31	0	6	-2144	4.02	4.02	4.02	4.02	2	0.32	0.08	0.49	0.00	0.00	22.3
14	38	-851	2601	3	0	8	-1842	4.02	4.02	4.02	4.02	2	0.27	0.08	0.45	0.00	0.00	22.3
15	38	-493	2863	-1	0	15	-2277	4.02	4.02	4.02	4.02	2	0.34	0.08	0.50	0.00	0.00	22.3
16	38	-855	2608	18	0	5	-1851	4.02	4.02	4.02	4.02	2	0.27	0.08	0.46	0.00	0.00	22.3
17	38	-497	2870	13	0	12	-2285	4.02	4.02	4.02	4.02	2	0.34	0.08	0.51	0.00	0.00	22.3
18	38	-1190	3679	-50	0	29	-2595	4.02	4.02	4.02	4.02	3	0.36	0.11	0.64	0.00	0.00	22.3
19	38	-1187	3776	90	0	-1	-2741	4.02	4.02	4.02	4.02	3	0.38	0.11	0.65	0.00	0.00	22.3
20	38	-879	3934	5	0	22	-3013	4.02	4.02	4.02	4.02	3	0.42	0.11	0.69	0.00	0.00	22.3
37	38	-1078	3530	-100	0	39	-2503	4.02	4.02	4.02	4.02	3	0.35	0.10	0.61	0.00	0.00	22.3
38	38	-1073	3692	134	0	-12	-2748	4.02	4.02	4.02	4.02	3	0.38	0.11	0.64	0.00	0.00	22.3
39	38	-560	3955	-8	0	27	-3201	4.02	4.02	4.02	4.02	3	0.45	0.11	0.70	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	75	-876	2705	11	0	9	-1385	4.02	4.02	4.02	4.02	3	0.19	0.08	0.47	0.00	0.00	22.3
2	75	-721	2030	-15	0	19	1058	4.02	4.02	4.02	4.02	2	0.16	0.06	0.36	0.00	0.00	22.3
3	75	-613	2109	-16	0	21	-1109	4.02	4.02	4.02	4.02	2	0.17	0.06	0.37	0.00	0.00	22.3
4	75	-735	2052	33	0	-8	1056	4.02	4.02	4.02	4.02	2	0.16	0.06	0.36	0.00	0.00	22.3
5	75	-627	2131	31	0	-5	-1133	4.02	4.02	4.02	4.02	2	0.17	0.06	0.37	0.00	0.00	22.3
6	75	-851	1946	3	0	7	1094	4.02	4.02	4.02	4.02	2	0.16	0.06	0.34	0.00	0.00	22.3
7	75	-493	2208	-1	0	15	-1247	4.02	4.02	4.02	4.02	2	0.19	0.06	0.39	0.00	0.00	22.3
8	75	-855	1953	18	0	-1	1093	4.02	4.02	4.02	4.02	2	0.16	0.06	0.34	0.00	0.00	22.3
9	75	-497	2215	13	0	7	-1254	4.02	4.02	4.02	4.02	2	0.19	0.06	0.39	0.00	0.00	22.3
10	75	-721	2030	-15	0	19	1058	4.02	4.02	4.02	4.02	2	0.16	0.06	0.36	0.00	0.00	22.3
11	75	-613	2109	-16	0	21	-1109	4.02	4.02	4.02	4.02	2	0.17	0.06	0.37	0.00	0.00	22.3
12	75	-735	2052	33	0	-8	1056	4.02	4.02	4.02	4.02	2	0.16	0.06	0.36	0.00	0.00	22.3
13	75	-627	2131	31	0	-5	-1133	4.02	4.02	4.02	4.02	2	0.17	0.06	0.37	0.00	0.00	22.3
14	75	-851	1946	3	0	7	1094	4.02	4.02	4.02	4.02	2	0.16	0.06	0.34	0.00	0.00	22.3
15	75	-493	2208	-1	0	15	-1247	4.02	4.02	4.02	4.02	2	0.19	0.06	0.39	0.00	0.00	22.3
16	75	-855	1953	18	0	-1	1093	4.02	4.02	4.02	4.02	2	0.16	0.06	0.34	0.00	0.00	22.3
17	75	-497	2215	13	0	7	-1254	4.02	4.02	4.02	4.02	2	0.19	0.06	0.39	0.00	0.00	22.3
18	75	-1190	2748	-50	0	48	1556	4.02	4.02	4.02	4.02	3	0.22	0.08	0.48	0.00	0.00	22.3
19	75	-1187	2845	90	0	-35	1531	4.02	4.02	4.02	4.02	3	0.21	0.08	0.49	0.00	0.00	22.3
20	75	-879	3003	5	0	20	-1582	4.02	4.02	4.02	4.02	3	0.22	0.09	0.52	0.00	0.00	22.3
37	75	-1078	2639	-100	0	76	1481	4.02	4.02	4.02	4.02	3	0.21	0.08	0.46	0.00	0.00	22.3
38	75	-1073	2801	134	0	-62	1439	4.02	4.02	4.02	4.02	3	0.20	0.08	0.49	0.00	0.00	22.3
39	75	-560	3064	-8	0	30	-1786	4.02	4.02	4.02	4.02	3	0.25	0.09	0.54	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	112	-876	1853	11	0	5	1590	4.02	4.02	4.02	4.02	3	0.22	0.05	0.32	0.00	0.00	22.3
2	112	-721	1375	-15	0	25	1208	4.02	4.02	4.02	4.02	2	0.18	0.04	0.24	0.00	0.00	22.3
3	112	-613	1454	-16	0	28	1226	4.02	4.02	4.02	4.02	2	0.18	0.04	0.26	0.00	0.00	22.3
4	112	-735	1397	33	0	-20	1220	4.02	4.02	4.02	4.02	2	0.18	0.04	0.24	0.00	0.00	22.3
5	112	-627	1476	31	0	-17	1237	4.02	4.02	4.02	4.02	2	0.18	0.04	0.26	0.00	0.00	22.3
6	112	-851	1291	3	0	6	1192	4.02	4.02	4.02	4.02	2	0.18	0.04	0.23	0.00	0.00	22.3
7	112	-493	1553	-1	0	15	1249	4.02	4.02	4.02	4.02	2	0.19	0.04	0.27	0.00	0.00	22.3
8	112	-855	1298	18	0	-8	1196	4.02	4.02	4.02	4.02	2	0.18	0.04	0.23	0.00	0.00	22.3
9	112	-497	1560	13	0	2	1253	4.02	4.02	4.02	4.02	2	0.19	0.05	0.27	0.00	0.00	22.3
10	112	-721	1375	-15	0	25	1208	4.02	4.02	4.02	4.02	2	0.18	0.04	0.24	0.00	0.00	22.3
11	112	-613	1454	-16	0	28	1226	4.02	4.02	4.02	4.02	2	0.18	0.04	0.26	0.00	0.00	22.3
12	112	-735	1397	33	0	-20	1220	4.02	4.02	4.02	4.02	2	0.18	0.04	0.24	0.00	0.00	22.3
13	112	-627	1476	31	0	-17	1237	4.02	4.02	4.02	4.02	2	0.18	0.04	0.26	0.00	0.00	22.3
14	112	-851	1291	3	0	6	1192	4.02	4.02	4.02	4.02	2	0.18	0.04	0.23	0.00	0.00	22.3
15	112	-493	1553	-1	0	15	1249	4.02	4.02	4.02	4.02	2	0.19	0.04	0.27	0.00	0.00	22.3
16	112	-855	1298	18	0	-8	1196	4.02	4.02	4.02	4.02	2	0.18	0.04	0.23	0.00	0.00	22.3
17	112	-497	1560	13	0	2	1253	4.02	4.02	4.02	4.02	2	0.19	0.05	0.27	0.00	0.00	22.3
18	112	-1190	1816	-50	0	67	1684	4.02	4.02	4.02	4.02	3	0.23	0.05	0.31	0.00	0.00	22.3
19	112	-1187	1913	90	0	-69	1719	4.02	4.02	4.02	4.02	3	0.24	0.06	0.33	0.00	0.00	22.3
20	112	-879	2071	5	0	18	1743	4.02	4.02	4.02	4.02	3	0.24	0.06	0.36	0.00	0.00	22.3
37	112	-1078	1747	-100	0	114	1609	4.02	4.02	4.02	4.02	3	0.22	0.05	0.30	0.00	0.00	22.3
38	112	-1073	1909	134	0	-112	1667	4.02	4.02	4.02	4.02	3	0.23	0.06	0.33	0.00	0.00	22.3
39	112	-560	2172	-8	0	33	1707	4.02	4.02	4.02	4.02	3	0.24	0.06	0.38	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	150	-876	1002	11	0	1	1590	4.02	4.02	4.02	4.02	3	0.22	0.03	0.17	0.00	0.00	22.3
2	150	-721	720	-15	0	30	1208	4.02	4.02	4.02	4.02	2	0.18	0.02	0.13	0.00	0.00	22.3
3	150	-613	799	-16	0	34	1226	4.02	4.02	4.02	4.02	2	0.18	0.02	0.14	0.00	0.00	22.3
4	150	-735	742	33	0	-32	1220	4.02	4.02	4.02	4.02	2	0.18	0.02	0.13	0.00	0.00	22.3
5	150	-627	821	31	0	-29	1237	4.02	4.02	4.02	4.02	2	0.18	0.02	0.14	0.00	0.00	22.3
6	150	-851	636	3	0	4	1192	4.02	4.02	4.02	4.02	2	0.18	0.02	0.11	0.00	0.00	22.3
7	150	-493	898	-1	0	16	1249	4.02	4.02	4.02	4.02	2	0.19	0.03	0.16	0.00	0.00	22.3
8	150	-855	643	18	0	-15	1196	4.02	4.02	4.02	4.02	2	0.18	0.02	0.11	0.00	0.00	22.3
9	150	-497	905	13	0	-3	1253	4.02	4.02	4.02	4.02	2	0.19	0.03	0.16	0.00	0.00	22.3
10	150	-721	720	-15	0	30	1208	4.02	4.02	4.02	4.02	2	0.18	0.02	0.13	0.00	0.00	22.3
11	150	-613	799	-16	0	34	1226	4.02	4.02	4.02	4.02	2	0.18	0.02	0.14	0.00	0.00	22.3
12	150	-735	742	33	0	-32	1220	4.02	4.02	4.02	4.02	2	0.18	0.02	0.13	0.00	0.00	22.3
13	150	-627	821	31	0	-29	1237	4.02	4.02	4.02	4.02	2	0.18	0.02	0.14	0.00	0.00	22.3
14	150	-851	636	3	0	4	1192	4.02	4.02	4.02	4.02	2	0.18	0.02	0.11	0.00	0.00	22.3
15	150	-493	898	-1	0	16	1249	4.02	4.02	4.02	4.02	2	0.19	0.03	0.16	0.00	0.00	22.3
16	150	-855	643	18	0	-15	1196	4.02	4.02	4.02	4.02	2	0.18	0.02	0.11	0.00	0.00	22.3
17	150	-497	905	13	0	-3	1253	4.02	4.02	4.02	4.02	2	0.19	0.03	0.16	0.00	0.00	22.3
18	150	-1190	884	-50	0	86	1684	4.02	4.02	4.02	4.02	3	0.23	0.03	0.15	0.00	0.00	22.3
19	150	-1187	981	90	0	-102	1719	4.02	4.02	4.02	4.02	3	0.24	0.03	0.17	0.00	0.00	22.3
20	150	-879	1139	5	0	16	1743	4.02	4.02	4.02	4.02	3	0.24	0.03	0.20	0.00	0.00	22.3
37	150	-1078	856	-100	0	151	1609	4.02	4.02	4.02	4.02	3	0.22	0.02	0.15	0.00	0.00	22.3

38	150	-1073	1017	134	0	-162	1667	4.02	4.02	4.02	4.02	3	0.23	0.03	0.18	0.00	0.00	22.3
39	150	-560	1281	-8	0	36	1707	4.02	4.02	4.02	4.02	3	0.24	0.04	0.23	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	188	-876	150	11	0	-3	1590	4.02	4.02	4.02	4.02	3	0.22	0.00	0.03	0.00	0.00	22.3
2	188	-721	65	-15	0	36	1208	4.02	4.02	4.02	4.02	2	0.18	0.00	0.01	0.00	0.00	22.3
3	188	-613	144	-16	0	40	1226	4.02	4.02	4.02	4.02	2	0.18	0.00	0.03	0.00	0.00	22.3
4	188	-735	87	33	0	-45	1220	4.02	4.02	4.02	4.02	2	0.18	0.00	0.02	0.00	0.00	22.3
5	188	-627	166	31	0	-41	1237	4.02	4.02	4.02	4.02	2	0.18	0.00	0.03	0.00	0.00	22.3
6	188	-851	-19	3	0	3	1192	4.02	4.02	4.02	4.02	2	0.18	0.00	0.00	0.00	0.00	22.3
7	188	-493	243	-1	0	16	1249	4.02	4.02	4.02	4.02	2	0.19	0.01	0.04	0.00	0.00	22.3
8	188	-855	-12	18	0	-21	1196	4.02	4.02	4.02	4.02	2	0.18	0.00	0.00	0.00	0.00	22.3
9	188	-497	250	13	0	-8	1253	4.02	4.02	4.02	4.02	2	0.19	0.01	0.04	0.00	0.00	22.3
10	188	-721	65	-15	0	36	1208	4.02	4.02	4.02	4.02	2	0.18	0.00	0.01	0.00	0.00	22.3
11	188	-613	144	-16	0	40	1226	4.02	4.02	4.02	4.02	2	0.18	0.00	0.03	0.00	0.00	22.3
12	188	-735	87	33	0	-45	1220	4.02	4.02	4.02	4.02	2	0.18	0.00	0.02	0.00	0.00	22.3
13	188	-627	166	31	0	-41	1237	4.02	4.02	4.02	4.02	2	0.18	0.00	0.03	0.00	0.00	22.3
14	188	-851	-19	3	0	3	1192	4.02	4.02	4.02	4.02	2	0.18	0.00	0.00	0.00	0.00	22.3
15	188	-493	243	-1	0	16	1249	4.02	4.02	4.02	4.02	2	0.19	0.01	0.04	0.00	0.00	22.3
16	188	-855	-12	18	0	-21	1196	4.02	4.02	4.02	4.02	2	0.18	0.00	0.00	0.00	0.00	22.3
17	188	-497	250	13	0	-8	1253	4.02	4.02	4.02	4.02	2	0.19	0.01	0.04	0.00	0.00	22.3
18	188	-1190	-48	-50	0	105	1684	4.02	4.02	4.02	4.02	3	0.23	0.00	0.01	0.00	0.00	22.3
19	188	-1187	50	90	0	-136	1719	4.02	4.02	4.02	4.02	3	0.24	0.00	0.01	0.00	0.00	22.3
20	188	-879	208	5	0	15	1743	4.02	4.02	4.02	4.02	3	0.24	0.01	0.04	0.00	0.00	22.3
37	188	-1078	-36	-100	0	189	1609	4.02	4.02	4.02	4.02	3	0.22	0.00	0.01	0.00	0.00	22.3
38	188	-1073	126	134	0	-212	1667	4.02	4.02	4.02	4.02	3	0.23	0.00	0.02	0.00	0.00	22.3
39	188	-560	389	-8	0	39	1707	4.02	4.02	4.02	4.02	3	0.24	0.01	0.07	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	225	-876	-702	11	0	-7	1590	4.02	4.02	4.02	4.02	3	0.22	0.02	0.12	0.00	0.00	22.3
2	225	-721	-590	-15	0	41	1208	4.02	4.02	4.02	4.02	2	0.18	0.02	0.10	0.00	0.00	22.3
3	225	-613	-512	-16	0	46	1226	4.02	4.02	4.02	4.02	2	0.18	0.01	0.09	0.00	0.00	22.3
4	225	-735	-568	33	0	-57	1220	4.02	4.02	4.02	4.02	2	0.18	0.02	0.10	0.00	0.00	22.3
5	225	-627	-490	31	0	-53	1237	4.02	4.02	4.02	4.02	2	0.18	0.01	0.09	0.00	0.00	22.3
6	225	-851	-674	3	0	2	1192	4.02	4.02	4.02	4.02	2	0.18	0.02	0.12	0.00	0.00	22.3
7	225	-493	-412	-1	0	16	1249	4.02	4.02	4.02	4.02	2	0.19	0.01	0.07	0.00	0.00	22.3
8	225	-855	-668	18	0	-28	1196	4.02	4.02	4.02	4.02	2	0.18	0.02	0.12	0.00	0.00	22.3
9	225	-497	-405	13	0	-13	1253	4.02	4.02	4.02	4.02	2	0.19	0.01	0.07	0.00	0.00	22.3
10	225	-721	-590	-15	0	41	1208	4.02	4.02	4.02	4.02	2	0.18	0.02	0.10	0.00	0.00	22.3
11	225	-613	-512	-16	0	46	1226	4.02	4.02	4.02	4.02	2	0.18	0.01	0.09	0.00	0.00	22.3
12	225	-735	-568	33	0	-57	1220	4.02	4.02	4.02	4.02	2	0.18	0.02	0.10	0.00	0.00	22.3
13	225	-627	-490	31	0	-53	1237	4.02	4.02	4.02	4.02	2	0.18	0.01	0.09	0.00	0.00	22.3
14	225	-851	-674	3	0	2	1192	4.02	4.02	4.02	4.02	2	0.18	0.02	0.12	0.00	0.00	22.3
15	225	-493	-412	-1	0	16	1249	4.02	4.02	4.02	4.02	2	0.19	0.01	0.07	0.00	0.00	22.3
16	225	-855	-668	18	0	-28	1196	4.02	4.02	4.02	4.02	2	0.18	0.02	0.12	0.00	0.00	22.3
17	225	-497	-405	13	0	-13	1253	4.02	4.02	4.02	4.02	2	0.19	0.01	0.07	0.00	0.00	22.3
18	225	-1190	-979	-50	0	123	1684	4.02	4.02	4.02	4.02	3	0.23	0.03	0.17	0.00	0.00	22.3
19	225	-1187	-882	90	0	-170	1719	4.02	4.02	4.02	4.02	3	0.24	0.03	0.15	0.00	0.00	22.3
20	225	-879	-724	5	0	13	1743	4.02	4.02	4.02	4.02	3	0.24	0.02	0.13	0.00	0.00	22.3
37	225	-1078	-928	-100	0	226	1609	4.02	4.02	4.02	4.02	3	0.22	0.03	0.16	0.00	0.00	22.3
38	225	-1073	-766	134	0	-262	1667	4.02	4.02	4.02	4.02	3	0.23	0.02	0.13	0.00	0.00	22.3
39	225	-560	-503	-8	0	42	1707	4.02	4.02	4.02	4.02	3	0.24	0.01	0.09	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	262	-876	-1553	11	0	-11	1590	4.02	4.02	4.02	4.02	3	0.22	0.04	0.27	0.00	0.00	22.3
2	262	-721	-1245	-15	0	47	1208	4.02	4.02	4.02	4.02	2	0.18	0.04	0.22	0.00	0.00	22.3
3	262	-613	-1167	-16	0	52	1226	4.02	4.02	4.02	4.02	2	0.18	0.03	0.20	0.00	0.00	22.3
4	262	-735	-1223	33	0	-69	1220	4.02	4.02	4.02	4.02	2	0.18	0.04	0.21	0.00	0.00	22.3
5	262	-627	-1145	31	0	-64	1237	4.02	4.02	4.02	4.02	2	0.18	0.03	0.20	0.00	0.00	22.3
6	262	-851	-1329	3	0	1	1192	4.02	4.02	4.02	4.02	2	0.18	0.04	0.23	0.00	0.00	22.3
7	262	-493	-1067	-1	0	17	1249	4.02	4.02	4.02	4.02	2	0.19	0.03	0.19	0.00	0.00	22.3
8	262	-855	-1323	18	0	-34	1196	4.02	4.02	4.02	4.02	2	0.18	0.04	0.23	0.00	0.00	22.3
9	262	-497	-1060	13	0	-18	1253	4.02	4.02	4.02	4.02	2	0.19	0.03	0.19	0.00	0.00	22.3
10	262	-721	-1245	-15	0	47	1208	4.02	4.02	4.02	4.02	2	0.18	0.04	0.22	0.00	0.00	22.3
11	262	-613	-1167	-16	0	52	1226	4.02	4.02	4.02	4.02	2	0.18	0.03	0.20	0.00	0.00	22.3
12	262	-735	-1223	33	0	-69	1220	4.02	4.02	4.02	4.02	2	0.18	0.04	0.21	0.00	0.00	22.3
13	262	-627	-1145	31	0	-64	1237	4.02	4.02	4.02	4.02	2	0.18	0.03	0.20	0.00	0.00	22.3
14	262	-851	-1329	3	0	1	1192	4.02	4.02	4.02	4.02	2	0.18	0.04	0.23	0.00	0.00	22.3
15	262	-493	-1067	-1	0	17	1249	4.02	4.02	4.02	4.02	2	0.19	0.03	0.19	0.00	0.00	22.3
16	262	-855	-1323	18	0	-34	1196	4.02	4.02	4.02	4.02	2	0.18	0.04	0.23	0.00	0.00	22.3
17	262	-497	-1060	13	0	-18	1253	4.02	4.02	4.02	4.02	2	0.19	0.03	0.19	0.00	0.00	22.3
18	262	-1190	-1911	-50	0	142	1684	4.02	4.02	4.02	4.02	3	0.23	0.06	0.33	0.00	0.00	22.3
19	262	-1187	-1814	90	0	-203	1719	4.02	4.02	4.02	4.02	3	0.24	0.05	0.31	0.00	0.00	22.3
20	262	-879	-1656	5	0	11	1743	4.02	4.02	4.02	4.02	3	0.24	0.05	0.29	0.00	0.00	22.3
37	262	-1078	-1819	-100	0	264	1609	4.02	4.02	4.02	4.02	3	0.22	0.05	0.32	0.00	0.00	22.3
38	262	-1073	-1658	134	0	-312	1667	4.02	4.02	4.02	4.02	3	0.23	0.05	0.29	0.00	0.00	22.3
39	262	-560	-1394	-8	0	46	1707	4.02	4.02	4.02	4.02	3	0.24	0.04	0.25	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	300	-876	-2405	11	0	-15	1539	4.02	4.02	4.02	4.02	3	0.22	0.07	0.42	0.00	0.00	22.3
2	300	-721	-1900	-15	0	52	1138	4.02	4.02	4.02	4.02	2	0.17	0.05	0.33	0.00	0.00	22.3
3	300	-613	-1822	-16	0	58	1205	4.02	4.02	4.02	4.02	2	0.18	0.05	0.32	0.00	0.00	22.3
4	300	-735	-1878	33	0	-82	1164	4.02	4.02	4.02	4.02	2	0.17	0.05	0.33	0.00	0.00	22.3
5	300	-627	-1800	31	0	-76	1229	4.02	4.02	4.02	4.02	2	0.18	0.05	0.32	0.00	0.00	22.3
6	300	-851	-1984	3	0	-1	1070	4.02	4.02	4.02	4.02	2	0.16	0.06	0.35	0.00	0.00	22.3
7	300	-493	-1722	-1	0	17	1249	4.02	4.02	4.02	4.02	2	0.19	0.05	0.30	0.00	0.00	22.3
8	300	-855	-1978	18	0	-41	1078	4.02	4.02	4.02	4.02	2	0.16	0.06	0.35	0.00	0.00	22.3
9	300	-497	-1715	13	0	-23	1253	4.02	4.02	4.02	4.02	2	0.19	0.05	0.30	0.00	0.00	22.3
10	300	-721	-1900	-15	0	52	1138	4.02	4.02	4.02	4.02	2	0.17	0.05	0.33	0.00	0.00	22.3
11	300	-613	-1822	-16	0	58	1205	4.02	4.02	4.02	4.02	2	0.18	0.05	0.32	0.00	0.00	22.3
12	300	-735	-1878	33	0	-82	1164	4.02	4.02	4.02	4.02	2	0.17	0.05	0.33	0.00	0.00	22.3
13	300	-627	-1800	31	0	-76	1229	4.02	4.02	4.02	4.02	2	0.18	0.05	0.32	0.00	0.00	22.3
14	300	-851	-1984	3	0	-1	1070	4.02	4.02	4.02	4.02	2	0.16	0.06	0.35	0.00	0.00	22.3
15	300	-493	-1722	-1	0	17	1249	4.02	4.02	4.02	4.02	2	0.19	0.05	0.30	0.00	0.00	22.3
16	300	-855	-1978	18	0	-41	1078	4.02	4.02	4.02	4.02	2	0.16	0.06	0.35	0.00	0.00	22.3
17	300	-497	-1715	13	0	-23	1253	4.02	4.02	4.02	4.02	2	0.19	0.05	0.30	0.00	0.00	22.3
18	300	-1190	-2843	-50	0	161	1498	4.02	4.02	4.02	4.02	3	0.21	0.08	0.49	0.00	0.00	22.3
19	300	-1187	-2746	90	0	-237	1593	4.02	4.02	4.02	4.02	3	0.22	0.08	0.48	0.00	0.00	22.3
20	300	-879	-2588	5	0	10	1714	4.02	4.02	4.02	4.02	3	0.24	0.07	0.45	0.00	0.00	22.3
37	300	-1078	-2711	-100	0	302	1436	4.02	4.02	4.02	4.02	3	0.20	0.08	0.47	0.00	0.00	22.3
38	300	-1073	-2550	134	0	-362	1594	4.02	4.02	4.02	4.02	3	0.22	0.07	0.44	0.00	0.00	22.3
39	300	-560	-2286	-8	0	49	1707	4.02	4.02	4.02	4.02	3	0.24	0.07	0.40	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	338	-876	-3256	11	0	-19	-2121	4.02	4.02	4.02	4.02	3	0.30	0.09	0.57	0.00	0.00	22.3

2	338	-721	-2555	-15	0	58	-1740	4.02	4.02	4.02	4.02	2	0.26	0.07	0.45	0.00	0.00	22.3
3	338	-613	-2477	-16	0	64	-1575	4.02	4.02	4.02	4.02	2	0.23	0.07	0.43	0.00	0.00	22.3
4	338	-735	-2533	33	0	-94	-1687	4.02	4.02	4.02	4.02	2	0.25	0.07	0.44	0.00	0.00	22.3
5	338	-627	-2455	31	0	-88	-1523	4.02	4.02	4.02	4.02	2	0.23	0.07	0.43	0.00	0.00	22.3
6	338	-851	-2639	3	0	-2	-1914	4.02	4.02	4.02	4.02	2	0.28	0.08	0.46	0.00	0.00	22.3
7	338	-493	-2377	-1	0	18	-1365	4.02	4.02	4.02	4.02	2	0.20	0.07	0.42	0.00	0.00	22.3
8	338	-855	-2633	18	0	-48	-1898	4.02	4.02	4.02	4.02	2	0.28	0.08	0.46	0.00	0.00	22.3
9	338	-497	-2370	13	0	-28	-1349	4.02	4.02	4.02	4.02	2	0.20	0.07	0.42	0.00	0.00	22.3
10	338	-721	-2555	-15	0	58	-1740	4.02	4.02	4.02	4.02	2	0.26	0.07	0.45	0.00	0.00	22.3
11	338	-613	-2477	-16	0	64	-1575	4.02	4.02	4.02	4.02	2	0.23	0.07	0.43	0.00	0.00	22.3
12	338	-735	-2533	33	0	-94	-1687	4.02	4.02	4.02	4.02	2	0.25	0.07	0.44	0.00	0.00	22.3
13	338	-627	-2455	31	0	-88	-1523	4.02	4.02	4.02	4.02	2	0.23	0.07	0.43	0.00	0.00	22.3
14	338	-851	-2639	3	0	-2	-1914	4.02	4.02	4.02	4.02	2	0.28	0.08	0.46	0.00	0.00	22.3
15	338	-493	-2377	-1	0	18	-1365	4.02	4.02	4.02	4.02	2	0.20	0.07	0.42	0.00	0.00	22.3
16	338	-855	-2633	18	0	-48	-1898	4.02	4.02	4.02	4.02	2	0.28	0.08	0.46	0.00	0.00	22.3
17	338	-497	-2370	13	0	-28	-1349	4.02	4.02	4.02	4.02	2	0.20	0.07	0.42	0.00	0.00	22.3
18	338	-1190	-3774	-50	0	180	-2771	4.02	4.02	4.02	4.02	3	0.38	0.11	0.65	0.00	0.00	22.3
19	338	-1187	-3677	90	0	-271	-2555	4.02	4.02	4.02	4.02	3	0.35	0.11	0.64	0.00	0.00	22.3
20	338	-879	-3519	5	0	8	-2235	4.02	4.02	4.02	4.02	3	0.31	0.10	0.61	0.00	0.00	22.3
37	338	-1078	-3602	-100	0	339	-2638	4.02	4.02	4.02	4.02	3	0.37	0.10	0.63	0.00	0.00	22.3
38	338	-1073	-3441	134	0	-412	-2277	4.02	4.02	4.02	4.02	3	0.32	0.10	0.60	0.00	0.00	22.3
39	338	-560	-3177	-8	0	52	-1743	4.02	4.02	4.02	4.02	3	0.25	0.09	0.56	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

1	375	-876	-4108	11	0	-24	-2121	4.02	4.02	4.02	4.02	3	0.30	0.12	0.72	0.00	0.00	22.3
2	375	-721	-3210	-15	0	64	-1740	4.02	4.02	4.02	4.02	2	0.26	0.09	0.56	0.00	0.00	22.3
3	375	-613	-3132	-16	0	70	-1575	4.02	4.02	4.02	4.02	2	0.23	0.09	0.55	0.00	0.00	22.3
4	375	-735	-3188	33	0	-106	-1687	4.02	4.02	4.02	4.02	2	0.25	0.09	0.56	0.00	0.00	22.3
5	375	-627	-3110	31	0	-100	-1523	4.02	4.02	4.02	4.02	2	0.23	0.09	0.55	0.00	0.00	22.3
6	375	-851	-3294	3	0	-3	-1914	4.02	4.02	4.02	4.02	2	0.28	0.10	0.57	0.00	0.00	22.3
7	375	-493	-3032	-1	0	18	-1365	4.02	4.02	4.02	4.02	2	0.20	0.09	0.53	0.00	0.00	22.3
8	375	-855	-3288	18	0	-54	-1898	4.02	4.02	4.02	4.02	2	0.28	0.10	0.57	0.00	0.00	22.3
9	375	-497	-3025	13	0	-33	-1349	4.02	4.02	4.02	4.02	2	0.20	0.09	0.53	0.00	0.00	22.3
10	375	-721	-3210	-15	0	64	-1740	4.02	4.02	4.02	4.02	2	0.26	0.09	0.56	0.00	0.00	22.3
11	375	-613	-3132	-16	0	70	-1575	4.02	4.02	4.02	4.02	2	0.23	0.09	0.55	0.00	0.00	22.3
12	375	-735	-3188	33	0	-106	-1687	4.02	4.02	4.02	4.02	2	0.25	0.09	0.56	0.00	0.00	22.3
13	375	-627	-3110	31	0	-100	-1523	4.02	4.02	4.02	4.02	2	0.23	0.09	0.55	0.00	0.00	22.3
14	375	-851	-3294	3	0	-3	-1914	4.02	4.02	4.02	4.02	2	0.28	0.10	0.57	0.00	0.00	22.3
15	375	-493	-3032	-1	0	18	-1365	4.02	4.02	4.02	4.02	2	0.20	0.09	0.53	0.00	0.00	22.3
16	375	-855	-3288	18	0	-54	-1898	4.02	4.02	4.02	4.02	2	0.28	0.10	0.57	0.00	0.00	22.3
17	375	-497	-3025	13	0	-33	-1349	4.02	4.02	4.02	4.02	2	0.20	0.09	0.53	0.00	0.00	22.3
18	375	-1190	-4706	-50	0	199	-2771	4.02	4.02	4.02	4.02	3	0.38	0.14	0.81	0.00	0.00	22.3
19	375	-1187	-4609	90	0	-304	-2555	4.02	4.02	4.02	4.02	3	0.35	0.13	0.80	0.00	0.00	22.3
20	375	-879	-4451	5	0	6	-2235	4.02	4.02	4.02	4.02	3	0.31	0.13	0.78	0.00	0.00	22.3
37	375	-1078	-4494	-100	0	377	-2638	4.02	4.02	4.02	4.02	3	0.37	0.13	0.78	0.00	0.00	22.3
38	375	-1073	-4333	134	0	-462	-2277	4.02	4.02	4.02	4.02	3	0.32	0.13	0.75	0.00	0.00	22.3
39	375	-560	-4069	-8	0	55	-1743	4.02	4.02	4.02	4.02	3	0.25	0.12	0.72	0.00	0.00	22.3

apost= -- aant= -- ainf= -- asup= -- (e arm. base= 4 X 2.01) staffe= 2 d 8 / 22.3

Delta Ingegneria srl
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Lavoro: **D2403a** Intestazione lavoro: **Palestra Campobello**
Elemento: **TRAVE DI FONDAZIONE** Gruppo: **1** Tabella: **Tabella fondazioni**
Descrizione: **Fondazione dir X**
Rck: **350.00** daN/cm^2 fyk: **4580.0** daN/cm^2 Copriferro: **5.0** cm
Verifica in ottemperanza alle NTC2018
Per le combinazioni sismiche la capacità è valutata in campo elastico o sostanzialmente elastico (§7.2.5,7.4.1 NTC2018)
Diametro staffe: **10** mm Numero braccia: **2**

ASTA NUM. 1 NI 1541 NF 1503 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice resistenza Fx,M	Bielle	V,Mx	aswta cmq/m	aswto	PASSO cm
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-351	0	0	0	-601	--	--	16.08	16.08	0.18	0.01	0.00	0.02	0.00	0.00	20.9
2	0	-0	-339	0	0	0	-347	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
3	0	-0	-401	0	0	0	-328	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
4	0	-0	-139	0	0	0	-596	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
5	0	-0	-201	0	0	0	-578	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
6	0	-0	-196	0	0	0	-456	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
7	0	-0	-404	0	0	0	-394	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
8	0	-0	-136	0	0	0	-531	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
9	0	-0	-344	0	0	0	-469	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
10	0	-0	-339	0	0	0	-347	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
11	0	-0	-401	0	0	0	-328	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
12	0	-0	-139	0	0	0	-596	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
13	0	-0	-201	0	0	0	-578	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
14	0	-0	-196	0	0	0	-456	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
15	0	-0	-404	0	0	0	-394	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
16	0	-0	-136	0	0	0	-531	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
17	0	-0	-344	0	0	0	-469	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
18	0	-0	-123	0	0	0	-519	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9
19	0	-0	545	0	0	0	-2273	--	--	16.08	16.08	0.18	0.04	0.00	0.03	0.00	0.00	20.9
20	0	-0	-858	0	0	0	-962	--	--	16.08	16.08	0.18	0.02	0.01	0.05	0.00	0.00	20.9
37	0	-0	-534	0	0	0	460	--	--	16.08	16.08	0.00	0.01	0.00	0.03	0.00	0.00	20.9
38	0	-0	579	0	0	0	-2569	--	--	16.08	16.08	0.18	0.04	0.00	0.04	0.00	0.00	20.9
39	0	-0	-1758	0	0	0	350	--	--	16.08	16.08	0.00	0.01	0.01	0.11	0.00	0.00	20.9
apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9																		
1	26	-0	-351	0	0	0	-601	--	--	16.08	16.08	0.18	0.01	0.00	0.02	0.00	0.00	20.9
2	26	-0	-339	0	0	0	-347	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
3	26	-0	-401	0	0	0	-328	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
4	26	-0	-139	0	0	0	-596	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
5	26	-0	-201	0	0	0	-578	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
6	26	-0	-196	0	0	0	-456	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
7	26	-0	-404	0	0	0	-394	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
8	26	-0	-136	0	0	0	-531	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
9	26	-0	-344	0	0	0	-469	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
10	26	-0	-339	0	0	0	-347	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
11	26	-0	-401	0	0	0	-328	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
12	26	-0	-139	0	0	0	-596	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
13	26	-0	-201	0	0	0	-578	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
14	26	-0	-196	0	0	0	-456	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
15	26	-0	-404	0	0	0	-394	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
16	26	-0	-136	0	0	0	-531	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
17	26	-0	-344	0	0	0	-469	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
18	26	-0	-123	0	0	0	-519	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9
19	26	-0	545	0	0	0	-2273	--	--	16.08	16.08	0.18	0.04	0.00	0.03	0.00	0.00	20.9
20	26	-0	-858	0	0	0	-962	--	--	16.08	16.08	0.18	0.02	0.01	0.05	0.00	0.00	20.9
37	26	-0	-534	0	0	0	460	--	--	16.08	16.08	0.00	0.01	0.00	0.03	0.00	0.00	20.9
38	26	-0	579	0	0	0	-2569	--	--	16.08	16.08	0.18	0.04	0.00	0.04	0.00	0.00	20.9
39	26	-0	-1758	0	0	0	-554	--	--	16.08	16.08	0.18	0.01	0.01	0.11	0.00	0.00	20.9
apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9																		
1	51	-0	-351	0	0	0	-601	--	--	16.08	16.08	0.18	0.01	0.00	0.02	0.00	0.00	20.9
2	51	-0	-339	0	0	0	-347	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
3	51	-0	-401	0	0	0	-328	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
4	51	-0	-139	0	0	0	-596	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
5	51	-0	-201	0	0	0	-578	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
6	51	-0	-196	0	0	0	-456	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
7	51	-0	-404	0	0	0	-394	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
8	51	-0	-136	0	0	0	-531	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
9	51	-0	-344	0	0	0	-469	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
10	51	-0	-339	0	0	0	-347	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
11	51	-0	-401	0	0	0	-328	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
12	51	-0	-139	0	0	0	-596	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
13	51	-0	-201	0	0	0	-578	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
14	51	-0	-196	0	0	0	-456	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
15	51	-0	-404	0	0	0	-394	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
16	51	-0	-136	0	0	0	-531	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
17	51	-0	-344	0	0	0	-469	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
18	51	-0	-123	0	0	0	-519	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9
19	51	-0	545	0	0	0	-2273	--	--	16.08	16.08	0.18	0.04	0.00	0.03	0.00	0.00	20.9
20	51	-0	-858	0	0	0	-962	--	--	16.08	16.08	0.18	0.02	0.01	0.05	0.00	0.00	20.9
37	51	-0	-534	0	0	0	186	--	--	16.08	16.08	0.00	0.00	0.00	0.03	0.00	0.00	20.9
38	51	-0	579	0	0	0	-2569	--	--	16.08	16.08	0.18	0.04	0.00	0.04	0.00	0.00	20.9
39	51	-0	-1758	0	0	0	-554	--	--	16.08	16.08	0.18	0.01	0.01	0.11	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 2 NI 1503 NF 1522 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-262	0	0	0	-546	--	--	16.08	16.08	0.18	0.01	0.00	0.02	0.00	0.00	20.9
2	0	-0	-241	0	0	0	-333	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
3	0	-0	-290	0	0	0	-337	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
4	0	-0	-113	0	0	0	-504	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
5	0	-0	-163	0	0	0	-507	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
6	0	-0	-138	0	0	0	-388	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
7	0	-0	-303	0	0	0	-401	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
8	0	-0	-100	0	0	0	-439	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
9	0	-0	-265	0	0	0	-452	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
10	0	-0	-241	0	0	0	-333	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
11	0	-0	-290	0	0	0	-337	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
12	0	-0	-113	0	0	0	-504	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
13	0	-0	-163	0	0	0	-507	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
14	0	-0	-138	0	0	0	-388	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
15	0	-0	-303	0	0	0	-401	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
16	0	-0	-100	0	0	0	-439	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
17	0	-0	-265	0	0	0	-452	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
18	0	-0	-45	0	0	0	-443	--	--	16.08	16.08	0.18	0.01	0.00	0.00	0.00	0.00	20.9
19	0	-0	383	0	0	0	-1716	--	--	16.08	16.08	0.18	0.03	0.00	0.02	0.00	0.00	20.9
20	0	-0	-387	0	0	0	-1019	--	--	16.08	16.08	0.18	0.02	0.00	0.02	0.00	0.00	20.9
37	0	-0	-332	0	0	0	227	--	--	16.08	16.08	0.00	0.00	0.00	0.02	0.00	0.00	20.9
38	0	-0	381	0	0	0	-1933	--	--	16.08	16.08	0.18	0.03	0.00	0.02	0.00	0.00	20.9
39	0	-0	-903	0	0	0	-904	--	--	16.08	16.08	0.18	0.01	0.01	0.06	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	26	-0	-262	0	0	0	-546	--	--	16.08	16.08	0.18	0.01	0.00	0.02	0.00	0.00	20.9
2	26	-0	-241	0	0	0	-333	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
3	26	-0	-290	0	0	0	-337	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
4	26	-0	-113	0	0	0	-504	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
5	26	-0	-163	0	0	0	-507	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
6	26	-0	-138	0	0	0	-388	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
7	26	-0	-303	0	0	0	-401	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
8	26	-0	-100	0	0	0	-439	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
9	26	-0	-265	0	0	0	-452	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
10	26	-0	-241	0	0	0	-333	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
11	26	-0	-290	0	0	0	-337	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
12	26	-0	-113	0	0	0	-504	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
13	26	-0	-163	0	0	0	-507	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
14	26	-0	-138	0	0	0	-388	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
15	26	-0	-303	0	0	0	-401	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
16	26	-0	-100	0	0	0	-439	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
17	26	-0	-265	0	0	0	-452	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
18	26	-0	-45	0	0	0	-443	--	--	16.08	16.08	0.18	0.01	0.00	0.00	0.00	0.00	20.9
19	26	-0	383	0	0	0	-1716	--	--	16.08	16.08	0.18	0.03	0.00	0.02	0.00	0.00	20.9
20	26	-0	-387	0	0	0	-1019	--	--	16.08	16.08	0.18	0.02	0.00	0.02	0.00	0.00	20.9
37	26	-0	-332	0	0	0	227	--	--	16.08	16.08	0.00	0.00	0.00	0.02	0.00	0.00	20.9
38	26	-0	381	0	0	0	-1933	--	--	16.08	16.08	0.18	0.03	0.00	0.02	0.00	0.00	20.9
39	26	-0	-903	0	0	0	-904	--	--	16.08	16.08	0.18	0.01	0.01	0.06	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	51	-0	-262	0	0	0	-546	--	--	16.08	16.08	0.18	0.01	0.00	0.02	0.00	0.00	20.9
2	51	-0	-241	0	0	0	-333	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
3	51	-0	-290	0	0	0	-337	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
4	51	-0	-113	0	0	0	-504	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
5	51	-0	-163	0	0	0	-507	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
6	51	-0	-138	0	0	0	-388	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
7	51	-0	-303	0	0	0	-401	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
8	51	-0	-100	0	0	0	-439	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
9	51	-0	-265	0	0	0	-452	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
10	51	-0	-241	0	0	0	-333	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
11	51	-0	-290	0	0	0	-337	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
12	51	-0	-113	0	0	0	-504	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
13	51	-0	-163	0	0	0	-507	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
14	51	-0	-138	0	0	0	-388	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
15	51	-0	-303	0	0	0	-401	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
16	51	-0	-100	0	0	0	-439	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
17	51	-0	-265	0	0	0	-452	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
18	51	-0	-45	0	0	0	-443	--	--	16.08	16.08	0.18	0.01	0.00	0.00	0.00	0.00	20.9
19	51	-0	383	0	0	0	-1716	--	--	16.08	16.08	0.18	0.03	0.00	0.02	0.00	0.00	20.9
20	51	-0	-387	0	0	0	-1019	--	--	16.08	16.08	0.18	0.02	0.00	0.02	0.00	0.00	20.9
37	51	-0	-332	0	0	0	56	--	--	16.08	16.08	0.00	0.00	0.00	0.02	0.00	0.00	20.9
38	51	-0	381	0	0	0	-1933	--	--	16.08	16.08	0.18	0.03	0.00	0.02	0.00	0.00	20.9
39	51	-0	-903	0	0	0	-904	--	--	16.08	16.08	0.18	0.01	0.01	0.06	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 3 NI 1522 NF 1521 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	154	0	0	0	-553	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9
2	0	-0	101	0	0	0	-343	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
3	0	-0	66	0	0	0	-339	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
4	0	-0	170	0	0	0	-513	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
5	0	-0	135	0	0	0	-508	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
6	0	-0	165	0	0	0	-408	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
7	0	-0	50	0	0	0	-393	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
8	0	-0	186	0	0	0	-459	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
9	0	-0	71	0	0	0	-444	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
10	0	-0	101	0	0	0	-343	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9

11	0	-0	66	0	0	0	-339	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
12	0	-0	170	0	0	0	-513	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
13	0	-0	135	0	0	0	-508	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
14	0	-0	165	0	0	0	-408	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
15	0	-0	50	0	0	0	-393	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
16	0	-0	186	0	0	0	-459	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
17	0	-0	71	0	0	0	-444	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
18	0	-0	228	0	0	0	-436	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9
19	0	-0	655	0	0	0	-1598	--	--	16.08	16.08	0.18	0.03	0.01	0.04	0.00	0.00	20.9
20	0	-0	86	0	0	0	-987	--	--	16.08	16.08	0.18	0.02	0.00	0.01	0.00	0.00	20.9
37	0	-0	-10	0	0	0	101	--	--	16.08	16.08	0.00	0.00	0.00	0.00	0.00	0.00	20.9
38	0	-0	703	0	0	0	-1835	--	--	16.08	16.08	0.18	0.03	0.01	0.04	0.00	0.00	20.9
39	0	-0	-246	0	0	0	-943	--	--	16.08	16.08	0.18	0.02	0.00	0.02	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	154	0	0	0	-553	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9
2	26	-0	101	0	0	0	-343	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
3	26	-0	66	0	0	0	-339	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
4	26	-0	170	0	0	0	-513	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
5	26	-0	135	0	0	0	-508	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
6	26	-0	165	0	0	0	-408	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
7	26	-0	50	0	0	0	-393	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
8	26	-0	186	0	0	0	-459	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
9	26	-0	71	0	0	0	-444	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
10	26	-0	101	0	0	0	-343	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
11	26	-0	66	0	0	0	-339	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
12	26	-0	170	0	0	0	-513	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
13	26	-0	135	0	0	0	-508	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
14	26	-0	165	0	0	0	-408	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
15	26	-0	50	0	0	0	-393	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
16	26	-0	186	0	0	0	-459	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
17	26	-0	71	0	0	0	-444	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
18	26	-0	228	0	0	0	-436	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9
19	26	-0	655	0	0	0	-1598	--	--	16.08	16.08	0.18	0.03	0.01	0.04	0.00	0.00	20.9
20	26	-0	86	0	0	0	-987	--	--	16.08	16.08	0.18	0.02	0.00	0.01	0.00	0.00	20.9
37	26	-0	-10	0	0	0	101	--	--	16.08	16.08	0.00	0.00	0.00	0.00	0.00	0.00	20.9
38	26	-0	703	0	0	0	-1835	--	--	16.08	16.08	0.18	0.03	0.01	0.04	0.00	0.00	20.9
39	26	-0	-246	0	0	0	-943	--	--	16.08	16.08	0.18	0.02	0.00	0.02	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	154	0	0	0	-553	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9
2	51	-0	101	0	0	0	-343	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
3	51	-0	66	0	0	0	-339	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
4	51	-0	170	0	0	0	-513	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
5	51	-0	135	0	0	0	-508	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
6	51	-0	165	0	0	0	-408	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
7	51	-0	50	0	0	0	-393	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
8	51	-0	186	0	0	0	-459	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
9	51	-0	71	0	0	0	-444	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
10	51	-0	101	0	0	0	-343	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
11	51	-0	66	0	0	0	-339	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
12	51	-0	170	0	0	0	-513	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
13	51	-0	135	0	0	0	-508	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
14	51	-0	165	0	0	0	-408	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
15	51	-0	50	0	0	0	-393	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
16	51	-0	186	0	0	0	-459	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
17	51	-0	71	0	0	0	-444	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
18	51	-0	228	0	0	0	-436	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9
19	51	-0	655	0	0	0	-1598	--	--	16.08	16.08	0.18	0.03	0.01	0.04	0.00	0.00	20.9
20	51	-0	86	0	0	0	-987	--	--	16.08	16.08	0.18	0.02	0.00	0.01	0.00	0.00	20.9
37	51	-0	-10	0	0	0	96	--	--	16.08	16.08	0.00	0.00	0.00	0.00	0.00	0.00	20.9
38	51	-0	703	0	0	0	-1835	--	--	16.08	16.08	0.18	0.03	0.01	0.04	0.00	0.00	20.9
39	51	-0	-246	0	0	0	-943	--	--	16.08	16.08	0.18	0.02	0.00	0.02	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 4 NI 1521 NF 1520 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	609	0	0	0	-630	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
2	0	-0	456	0	0	0	-411	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
3	0	-0	433	0	0	0	-418	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
4	0	-0	504	0	0	0	-552	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
5	0	-0	481	0	0	0	-558	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
6	0	-0	499	0	0	0	-453	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
7	0	-0	423	0	0	0	-474	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
8	0	-0	514	0	0	0	-496	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
9	0	-0	438	0	0	0	-516	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
10	0	-0	456	0	0	0	-411	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
11	0	-0	433	0	0	0	-418	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
12	0	-0	504	0	0	0	-552	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
13	0	-0	481	0	0	0	-558	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
14	0	-0	499	0	0	0	-453	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
15	0	-0	423	0	0	0	-474	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
16	0	-0	514	0	0	0	-496	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
17	0	-0	438	0	0	0	-516	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
18	0	-0	664	0	0	0	-472	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
19	0	-0	1053	0	0	0	-1528	--	--	16.08	16.08	0.18	0.03	0.01	0.07	0.00	0.00	20.9
20	0	-0	606	0	0	0	-1074	--	--	16.08	16.08	0.18	0.02	0.00	0.04	0.00	0.00	20.9
37	0	-0	455	0	0	0	-1	--	--	16.08	16.08	0.18	0.00	0.00	0.03	0.00	0.00	20.9
38	0	-0	1104	0	0	0	-1762	--	--	16.08	16.08	0.18	0.03	0.01	0.07	0.00	0.00	20.9
39	0	-0	360	0	0	0	-1006	--	--	16.08	16.08	0.18	0.02	0.00	0.02	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	609	0	0	0	-630	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
2	26	-0	456	0	0	0	-411	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
3	26	-0	433	0	0	0	-418	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
4	26	-0	504	0	0	0	-552	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
5	26	-0	481	0	0	0	-558	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
6	26	-0	499	0	0	0	-453	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9

7	26	-0	423	0	0	0	-474	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
8	26	-0	514	0	0	0	-496	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
9	26	-0	438	0	0	0	-516	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
10	26	-0	456	0	0	0	-411	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
11	26	-0	433	0	0	0	-418	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
12	26	-0	504	0	0	0	-552	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
13	26	-0	481	0	0	0	-558	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
14	26	-0	499	0	0	0	-453	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
15	26	-0	423	0	0	0	-474	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
16	26	-0	514	0	0	0	-496	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
17	26	-0	438	0	0	0	-516	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
18	26	-0	664	0	0	0	-472	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
19	26	-0	1053	0	0	0	-1528	--	--	16.08	16.08	0.18	0.03	0.01	0.07	0.00	0.00	20.9
20	26	-0	606	0	0	0	-1074	--	--	16.08	16.08	0.18	0.02	0.00	0.04	0.00	0.00	20.9
37	26	-0	455	0	0	0	602	--	--	16.08	16.08	0.00	0.01	0.00	0.03	0.00	0.00	20.9
38	26	-0	1104	0	0	0	-1762	--	--	16.08	16.08	0.18	0.03	0.01	0.07	0.00	0.00	20.9
39	26	-0	360	0	0	0	-1006	--	--	16.08	16.08	0.18	0.02	0.00	0.02	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	609	0	0	0	-630	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
2	51	-0	456	0	0	0	-411	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
3	51	-0	433	0	0	0	-418	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
4	51	-0	504	0	0	0	-552	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
5	51	-0	481	0	0	0	-558	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
6	51	-0	499	0	0	0	-453	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
7	51	-0	423	0	0	0	-474	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
8	51	-0	514	0	0	0	-496	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
9	51	-0	438	0	0	0	-516	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
10	51	-0	456	0	0	0	-411	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
11	51	-0	433	0	0	0	-418	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
12	51	-0	504	0	0	0	-552	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
13	51	-0	481	0	0	0	-558	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
14	51	-0	499	0	0	0	-453	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
15	51	-0	423	0	0	0	-474	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
16	51	-0	514	0	0	0	-496	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
17	51	-0	438	0	0	0	-516	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
18	51	-0	664	0	0	0	-472	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
19	51	-0	1053	0	0	0	-1528	--	--	16.08	16.08	0.18	0.03	0.01	0.07	0.00	0.00	20.9
20	51	-0	606	0	0	0	-1074	--	--	16.08	16.08	0.18	0.02	0.00	0.04	0.00	0.00	20.9
37	51	-0	455	0	0	0	233	--	--	16.08	16.08	0.00	0.00	0.00	0.03	0.00	0.00	20.9
38	51	-0	1104	0	0	0	-1762	--	--	16.08	16.08	0.18	0.03	0.01	0.07	0.00	0.00	20.9
39	51	-0	360	0	0	0	-1006	--	--	16.08	16.08	0.18	0.02	0.00	0.02	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 5 NI 1520 NF 1535 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm

1	0	-0	1081	0	0	0	-615	--	--	16.08	16.08	0.18	0.01	0.01	0.07	0.00	0.00	20.9
2	0	-0	818	0	0	0	-403	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
3	0	-0	802	0	0	0	-415	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
4	0	-0	861	0	0	0	-531	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
5	0	-0	845	0	0	0	-543	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
6	0	-0	851	0	0	0	-433	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
7	0	-0	800	0	0	0	-475	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
8	0	-0	864	0	0	0	-471	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
9	0	-0	812	0	0	0	-513	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
10	0	-0	818	0	0	0	-403	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
11	0	-0	802	0	0	0	-415	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
12	0	-0	861	0	0	0	-531	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
13	0	-0	845	0	0	0	-543	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
14	0	-0	851	0	0	0	-433	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
15	0	-0	800	0	0	0	-475	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
16	0	-0	864	0	0	0	-471	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
17	0	-0	812	0	0	0	-513	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
18	0	-0	1181	0	0	0	-451	--	--	16.08	16.08	0.18	0.01	0.01	0.07	0.00	0.00	20.9
19	0	-0	1522	0	0	0	-1416	--	--	16.08	16.08	0.18	0.02	0.01	0.10	0.00	0.00	20.9
20	0	-0	1166	0	0	0	-1071	--	--	16.08	16.08	0.18	0.02	0.01	0.07	0.00	0.00	20.9
37	0	-0	985	0	0	0	-27	--	--	16.08	16.08	0.18	0.00	0.01	0.06	0.00	0.00	20.9
38	0	-0	1553	0	0	0	-1636	--	--	16.08	16.08	0.18	0.03	0.01	0.10	0.00	0.00	20.9
39	0	-0	959	0	0	0	-1062	--	--	16.08	16.08	0.18	0.02	0.01	0.06	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	1081	0	0	0	-615	--	--	16.08	16.08	0.18	0.01	0.01	0.07	0.00	0.00	20.9
2	26	-0	818	0	0	0	-403	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
3	26	-0	802	0	0	0	-415	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
4	26	-0	861	0	0	0	-531	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
5	26	-0	845	0	0	0	-543	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
6	26	-0	851	0	0	0	-433	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
7	26	-0	800	0	0	0	-475	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
8	26	-0	864	0	0	0	-471	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
9	26	-0	812	0	0	0	-513	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
10	26	-0	818	0	0	0	-403	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
11	26	-0	802	0	0	0	-415	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
12	26	-0	861	0	0	0	-531	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
13	26	-0	845	0	0	0	-543	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
14	26	-0	851	0	0	0	-433	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
15	26	-0	800	0	0	0	-475	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
16	26	-0	864	0	0	0	-471	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
17	26	-0	812	0	0	0	-513	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
18	26	-0	1181	0	0	0	-451	--	--	16.08	16.08	0.18	0.01	0.01	0.07	0.00	0.00	20.9
19	26	-0	1522	0	0	0	-1416	--	--	16.08	16.08	0.18	0.02	0.01	0.10	0.00	0.00	20.9
20	26	-0	1166	0	0	0	-1071	--	--	16.08	16.08	0.18	0.02	0.01	0.07	0.00	0.00	20.9
37	26	-0	985	0	0	0	1279	--	--	16.08	16.08	0.00	0.02	0.01	0.06	0.00	0.00	20.9
38	26	-0	1553	0	0	0	-1636	--	--	16.08	16.08	0.18	0.03	0.01	0.10	0.00	0.00	20.9
39	26	-0	959	0	0	0	-1062	--	--	16.08	16.08	0.18	0.02	0.01	0.06	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	1081	0	0	0	-615	--	--	16.08	16.08	0.18	0.01	0.01	0.07	0.00	0.00	20.9
2	51	-0	818	0	0	0	17	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9

3	51	-0	802	0	0	0	-415	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
4	51	-0	861	0	0	0	-531	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
5	51	-0	845	0	0	0	-543	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
6	51	-0	851	0	0	0	4	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
7	51	-0	800	0	0	0	-475	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
8	51	-0	864	0	0	0	-471	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
9	51	-0	812	0	0	0	-513	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
10	51	-0	818	0	0	0	17	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
11	51	-0	802	0	0	0	-415	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
12	51	-0	861	0	0	0	-531	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
13	51	-0	845	0	0	0	-543	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
14	51	-0	851	0	0	0	4	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
15	51	-0	800	0	0	0	-475	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
16	51	-0	864	0	0	0	-471	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
17	51	-0	812	0	0	0	-513	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
18	51	-0	1181	0	0	0	156	--	--	16.08	16.08	0.00	0.00	0.01	0.07	0.00	0.00	20.9
19	51	-0	1522	0	0	0	-1416	--	--	16.08	16.08	0.18	0.02	0.01	0.10	0.00	0.00	20.9
20	51	-0	1166	0	0	0	-1071	--	--	16.08	16.08	0.18	0.02	0.01	0.07	0.00	0.00	20.9
37	51	-0	985	0	0	0	479	--	--	16.08	16.08	0.00	0.01	0.01	0.06	0.00	0.00	20.9
38	51	-0	1553	0	0	0	-1636	--	--	16.08	16.08	0.18	0.03	0.01	0.10	0.00	0.00	20.9
39	51	-0	959	0	0	0	-1062	--	--	16.08	16.08	0.18	0.02	0.01	0.06	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 6 NI 1535 NF 1534 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	1605	0	0	0	-519	--	--	16.08	16.08	0.18	0.01	0.01	0.10	0.00	0.00	20.9
2	0	-0	1219	0	0	0	-332	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
3	0	-0	1209	0	0	0	-348	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
4	0	-0	1261	0	0	0	-451	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
5	0	-0	1251	0	0	0	-467	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
6	0	-0	1245	0	0	0	-355	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
7	0	-0	1212	0	0	0	-409	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
8	0	-0	1258	0	0	0	-390	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
9	0	-0	1224	0	0	0	-444	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
10	0	-0	1219	0	0	0	-332	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
11	0	-0	1209	0	0	0	-348	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
12	0	-0	1261	0	0	0	-451	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
13	0	-0	1251	0	0	0	-467	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
14	0	-0	1245	0	0	0	-355	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
15	0	-0	1212	0	0	0	-409	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
16	0	-0	1258	0	0	0	-390	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
17	0	-0	1224	0	0	0	-444	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
18	0	-0	1772	0	0	0	-350	--	--	16.08	16.08	0.18	0.01	0.01	0.11	0.00	0.00	20.9
19	0	-0	2065	0	0	0	-1241	--	--	16.08	16.08	0.18	0.02	0.02	0.13	0.00	0.00	20.9
20	0	-0	1777	0	0	0	-975	--	--	16.08	16.08	0.18	0.02	0.01	0.11	0.00	0.00	20.9
37	0	-0	1581	0	0	0	36	--	--	16.08	16.08	0.00	0.00	0.01	0.10	0.00	0.00	20.9
38	0	-0	2070	0	0	0	-1450	--	--	16.08	16.08	0.18	0.02	0.02	0.13	0.00	0.00	20.9
39	0	-0	1589	0	0	0	-1006	--	--	16.08	16.08	0.18	0.02	0.01	0.10	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	1605	0	0	0	-519	--	--	16.08	16.08	0.18	0.01	0.01	0.10	0.00	0.00	20.9
2	26	-0	1219	0	0	0	-332	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
3	26	-0	1209	0	0	0	-348	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
4	26	-0	1261	0	0	0	-451	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
5	26	-0	1251	0	0	0	-467	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
6	26	-0	1245	0	0	0	-355	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
7	26	-0	1212	0	0	0	-409	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
8	26	-0	1258	0	0	0	-390	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
9	26	-0	1224	0	0	0	-444	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
10	26	-0	1219	0	0	0	-332	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
11	26	-0	1209	0	0	0	-348	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
12	26	-0	1261	0	0	0	-451	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
13	26	-0	1251	0	0	0	-467	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
14	26	-0	1245	0	0	0	-355	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
15	26	-0	1212	0	0	0	-409	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
16	26	-0	1258	0	0	0	-390	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
17	26	-0	1224	0	0	0	-444	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
18	26	-0	1772	0	0	0	1999	--	--	16.08	16.08	0.00	0.03	0.01	0.11	0.00	0.00	20.9
19	26	-0	2065	0	0	0	-1241	--	--	16.08	16.08	0.18	0.02	0.02	0.13	0.00	0.00	20.9
20	26	-0	1777	0	0	0	-975	--	--	16.08	16.08	0.18	0.02	0.01	0.11	0.00	0.00	20.9
37	26	-0	1581	0	0	0	2132	--	--	16.08	16.08	0.00	0.04	0.01	0.10	0.00	0.00	20.9
38	26	-0	2070	0	0	0	-1450	--	--	16.08	16.08	0.18	0.02	0.02	0.13	0.00	0.00	20.9
39	26	-0	1589	0	0	0	-1006	--	--	16.08	16.08	0.18	0.02	0.01	0.10	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	1605	0	0	0	305	--	--	16.08	16.08	0.00	0.01	0.01	0.10	0.00	0.00	20.9
2	51	-0	1219	0	0	0	294	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
3	51	-0	1209	0	0	0	273	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
4	51	-0	1261	0	0	0	197	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
5	51	-0	1251	0	0	0	175	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
6	51	-0	1245	0	0	0	285	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
7	51	-0	1212	0	0	0	214	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
8	51	-0	1258	0	0	0	256	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
9	51	-0	1224	0	0	0	184	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
10	51	-0	1219	0	0	0	294	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
11	51	-0	1209	0	0	0	273	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
12	51	-0	1261	0	0	0	197	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
13	51	-0	1251	0	0	0	175	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
14	51	-0	1245	0	0	0	285	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
15	51	-0	1212	0	0	0	214	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
16	51	-0	1258	0	0	0	256	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
17	51	-0	1224	0	0	0	184	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
18	51	-0	1772	0	0	0	561	--	--	16.08	16.08	0.00	0.01	0.01	0.11	0.00	0.00	20.9
19	51	-0	2065	0	0	0	-1241	--	--	16.08	16.08	0.18	0.02	0.02	0.13	0.00	0.00	20.9
20	51	-0	1777	0	0	0	-975	--	--	16.08	16.08	0.18	0.02	0.01	0.11	0.00	0.00	20.9
37	51	-0	1581	0	0	0	848	--	--	16.08	16.08	0.00	0.01	0.01	0.10	0.00	0.00	20.9
38	51	-0	2070	0	0	0	-1450	--	--	16.08	16.08	0.18	0.02	0.02	0.13	0.00	0.00	20.9
39	51	-0	1589	0	0	0	-1006	--	--	16.08	16.08	0.18	0.02	0.01	0.10	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 7 NI 1534 NF 1504 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	2208	0	0	0	-333	--	--	16.08	16.08	0.18	0.01	0.02	0.14	0.00	0.00	20.9
2	0	-0	1681	0	0	0	-192	--	--	16.08	16.08	0.29	0.00	0.01	0.11	0.00	0.00	20.9
3	0	-0	1675	0	0	0	-210	--	--	16.08	16.08	0.29	0.00	0.01	0.11	0.00	0.00	20.9
4	0	-0	1721	0	0	0	-303	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
5	0	-0	1716	0	0	0	-321	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
6	0	-0	1702	0	0	0	-209	--	--	16.08	16.08	0.29	0.00	0.01	0.11	0.00	0.00	20.9
7	0	-0	1682	0	0	0	-271	--	--	16.08	16.08	0.29	0.00	0.01	0.11	0.00	0.00	20.9
8	0	-0	1714	0	0	0	-242	--	--	16.08	16.08	0.29	0.00	0.01	0.11	0.00	0.00	20.9
9	0	-0	1694	0	0	0	-304	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
10	0	-0	1681	0	0	0	-192	--	--	16.08	16.08	0.29	0.00	0.01	0.11	0.00	0.00	20.9
11	0	-0	1675	0	0	0	-210	--	--	16.08	16.08	0.29	0.00	0.01	0.11	0.00	0.00	20.9
12	0	-0	1721	0	0	0	-303	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
13	0	-0	1716	0	0	0	-321	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
14	0	-0	1702	0	0	0	-209	--	--	16.08	16.08	0.29	0.00	0.01	0.11	0.00	0.00	20.9
15	0	-0	1682	0	0	0	-271	--	--	16.08	16.08	0.29	0.00	0.01	0.11	0.00	0.00	20.9
16	0	-0	1714	0	0	0	-242	--	--	16.08	16.08	0.29	0.00	0.01	0.11	0.00	0.00	20.9
17	0	-0	1694	0	0	0	-304	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
18	0	-0	2458	0	0	0	-148	--	--	16.08	16.08	0.18	0.00	0.02	0.15	0.00	0.00	20.9
19	0	-0	2696	0	0	0	-977	--	--	16.08	16.08	0.18	0.02	0.02	0.17	0.00	0.00	20.9
20	0	-0	2466	0	0	0	-772	--	--	16.08	16.08	0.18	0.01	0.02	0.15	0.00	0.00	20.9
37	0	-0	2271	0	0	0	202	--	--	16.08	16.08	0.00	0.00	0.02	0.14	0.00	0.00	20.9
38	0	-0	2666	0	0	0	-1179	--	--	16.08	16.08	0.18	0.02	0.02	0.17	0.00	0.00	20.9
39	0	-0	2283	0	0	0	-838	--	--	16.08	16.08	0.18	0.01	0.02	0.14	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	26	-0	2208	0	0	0	2593	--	--	16.08	16.08	0.00	0.04	0.02	0.14	0.00	0.00	20.9
2	26	-0	1681	0	0	0	2037	--	--	16.08	16.08	0.10	0.04	0.01	0.11	0.00	0.00	20.9
3	26	-0	1675	0	0	0	2010	--	--	16.08	16.08	0.10	0.04	0.01	0.11	0.00	0.00	20.9
4	26	-0	1721	0	0	0	1979	--	--	16.08	16.08	0.10	0.04	0.01	0.11	0.00	0.00	20.9
5	26	-0	1716	0	0	0	1953	--	--	16.08	16.08	0.10	0.03	0.01	0.11	0.00	0.00	20.9
6	26	-0	1702	0	0	0	2047	--	--	16.08	16.08	0.10	0.04	0.01	0.11	0.00	0.00	20.9
7	26	-0	1682	0	0	0	1959	--	--	16.08	16.08	0.10	0.03	0.01	0.11	0.00	0.00	20.9
8	26	-0	1714	0	0	0	2030	--	--	16.08	16.08	0.10	0.04	0.01	0.11	0.00	0.00	20.9
9	26	-0	1694	0	0	0	1941	--	--	16.08	16.08	0.10	0.03	0.01	0.11	0.00	0.00	20.9
10	26	-0	1681	0	0	0	2037	--	--	16.08	16.08	0.10	0.04	0.01	0.11	0.00	0.00	20.9
11	26	-0	1675	0	0	0	2010	--	--	16.08	16.08	0.10	0.04	0.01	0.11	0.00	0.00	20.9
12	26	-0	1721	0	0	0	1979	--	--	16.08	16.08	0.10	0.04	0.01	0.11	0.00	0.00	20.9
13	26	-0	1716	0	0	0	1953	--	--	16.08	16.08	0.10	0.03	0.01	0.11	0.00	0.00	20.9
14	26	-0	1702	0	0	0	2047	--	--	16.08	16.08	0.10	0.04	0.01	0.11	0.00	0.00	20.9
15	26	-0	1682	0	0	0	1959	--	--	16.08	16.08	0.10	0.03	0.01	0.11	0.00	0.00	20.9
16	26	-0	1714	0	0	0	2030	--	--	16.08	16.08	0.10	0.04	0.01	0.11	0.00	0.00	20.9
17	26	-0	1694	0	0	0	1941	--	--	16.08	16.08	0.10	0.03	0.01	0.11	0.00	0.00	20.9
18	26	-0	2458	0	0	0	3110	--	--	16.08	16.08	0.00	0.05	0.02	0.15	0.00	0.00	20.9
19	26	-0	2696	0	0	0	-977	--	--	16.08	16.08	0.18	0.02	0.02	0.17	0.00	0.00	20.9
20	26	-0	2466	0	0	0	-772	--	--	16.08	16.08	0.18	0.01	0.02	0.15	0.00	0.00	20.9
37	26	-0	2271	0	0	0	3213	--	--	16.08	16.08	0.00	0.05	0.02	0.14	0.00	0.00	20.9
38	26	-0	2666	0	0	0	-1179	--	--	16.08	16.08	0.18	0.02	0.02	0.17	0.00	0.00	20.9
39	26	-0	2283	0	0	0	-838	--	--	16.08	16.08	0.18	0.01	0.02	0.14	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	51	-0	2208	0	0	0	801	--	--	16.08	16.08	0.00	0.01	0.02	0.14	0.00	0.00	20.9
2	51	-0	1681	0	0	0	672	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
3	51	-0	1675	0	0	0	650	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
4	51	-0	1721	0	0	0	582	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
5	51	-0	1716	0	0	0	560	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
6	51	-0	1702	0	0	0	666	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
7	51	-0	1682	0	0	0	593	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
8	51	-0	1714	0	0	0	639	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
9	51	-0	1694	0	0	0	566	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
10	51	-0	1681	0	0	0	672	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
11	51	-0	1675	0	0	0	650	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
12	51	-0	1721	0	0	0	582	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
13	51	-0	1716	0	0	0	560	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
14	51	-0	1702	0	0	0	666	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
15	51	-0	1682	0	0	0	593	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
16	51	-0	1714	0	0	0	639	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
17	51	-0	1694	0	0	0	566	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
18	51	-0	2458	0	0	0	1115	--	--	16.08	16.08	0.00	0.02	0.02	0.15	0.00	0.00	20.9
19	51	-0	2696	0	0	0	408	--	--	16.08	16.08	0.00	0.01	0.02	0.17	0.00	0.00	20.9
20	51	-0	2466	0	0	0	495	--	--	16.08	16.08	0.00	0.01	0.02	0.15	0.00	0.00	20.9
37	51	-0	2271	0	0	0	1369	--	--	16.08	16.08	0.00	0.02	0.02	0.14	0.00	0.00	20.9
38	51	-0	2666	0	0	0	190	--	--	16.08	16.08	0.00	0.00	0.02	0.17	0.00	0.00	20.9
39	51	-0	2283	0	0	0	335	--	--	16.08	16.08	0.00	0.01	0.02	0.14	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 8 NI 1504 NF 1524 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	2928	0	0	0	-34	--	--	16.08	16.08	0.18	0.00	0.02	0.18	0.00	0.00	20.9
2	0	-0	2235	0	0	0	35	--	--	16.08	16.08	0.10	0.00	0.02	0.14	0.00	0.00	20.9
3	0	-0	2232	0	0	0	15	--	--	16.08	16.08	0.10	0.00	0.02	0.14	0.00	0.00	20.9
4	0	-0	2273	0	0	0	-68	--	--	16.08	16.08	0.29	0.00	0.02	0.14	0.00	0.00	20.9
5	0	-0	2271	0	0	0	-88	--	--	16.08	16.08	0.29	0.00	0.02	0.14	0.00	0.00	20.9
6	0	-0	2251	0	0	0	23	--	--	16.08	16.08	0.10	0.00	0.02	0.14	0.00	0.00	20.9
7	0	-0	2243	0	0	0	-45	--	--	16.08	16.08	0.29	0.00	0.02	0.14	0.00	0.00	20.9
8	0	-0	2262	0	0	0	-8	--	--	16.08	16.08	0.29	0.00	0.02	0.14	0.00	0.00	20.9
9	0	-0	2255	0	0	0	-76	--	--	16.08	16.08	0.29	0.00	0.02	0.14	0.00	0.00	20.9
10	0	-0	2235	0	0	0	35	--	--	16.08	16.08	0.10	0.00	0.02	0.14	0.00	0.00	20.9

11	0	-0	2232	0	0	0	15	--	--	16.08	16.08	0.10	0.00	0.02	0.14	0.00	0.00	20.9
12	0	-0	2273	0	0	0	-68	--	--	16.08	16.08	0.29	0.00	0.02	0.14	0.00	0.00	20.9
13	0	-0	2271	0	0	0	-88	--	--	16.08	16.08	0.29	0.00	0.02	0.14	0.00	0.00	20.9
14	0	-0	2251	0	0	0	23	--	--	16.08	16.08	0.10	0.00	0.02	0.14	0.00	0.00	20.9
15	0	-0	2243	0	0	0	-45	--	--	16.08	16.08	0.29	0.00	0.02	0.14	0.00	0.00	20.9
16	0	-0	2262	0	0	0	-8	--	--	16.08	16.08	0.29	0.00	0.02	0.14	0.00	0.00	20.9
17	0	-0	2255	0	0	0	-76	--	--	16.08	16.08	0.29	0.00	0.02	0.14	0.00	0.00	20.9
18	0	-0	3285	0	0	0	183	--	--	16.08	16.08	0.00	0.00	0.03	0.21	0.00	0.00	20.9
19	0	-0	3448	0	0	0	-595	--	--	16.08	16.08	0.18	0.01	0.03	0.22	0.00	0.00	20.9
20	0	-0	3276	0	0	0	-439	--	--	16.08	16.08	0.18	0.01	0.03	0.21	0.00	0.00	20.9
37	0	-0	3104	0	0	0	500	--	--	16.08	16.08	0.00	0.01	0.03	0.19	0.00	0.00	20.9
38	0	-0	3376	0	0	0	-798	--	--	16.08	16.08	0.18	0.01	0.03	0.21	0.00	0.00	20.9
39	0	-0	3088	0	0	0	-536	--	--	16.08	16.08	0.18	0.01	0.03	0.19	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	2928	0	0	0	3847	--	--	16.08	16.08	0.00	0.07	0.02	0.18	0.00	0.00	20.9
2	26	-0	2235	0	0	0	2998	--	--	16.08	16.08	0.10	0.05	0.02	0.14	0.00	0.00	20.9
3	26	-0	2232	0	0	0	2974	--	--	16.08	16.08	0.10	0.05	0.02	0.14	0.00	0.00	20.9
4	26	-0	2273	0	0	0	2945	--	--	16.08	16.08	0.10	0.05	0.02	0.14	0.00	0.00	20.9
5	26	-0	2271	0	0	0	2922	--	--	16.08	16.08	0.10	0.05	0.02	0.14	0.00	0.00	20.9
6	26	-0	2251	0	0	0	3007	--	--	16.08	16.08	0.10	0.05	0.02	0.14	0.00	0.00	20.9
7	26	-0	2243	0	0	0	2928	--	--	16.08	16.08	0.10	0.05	0.02	0.14	0.00	0.00	20.9
8	26	-0	2262	0	0	0	2990	--	--	16.08	16.08	0.10	0.05	0.02	0.14	0.00	0.00	20.9
9	26	-0	2255	0	0	0	2913	--	--	16.08	16.08	0.10	0.05	0.02	0.14	0.00	0.00	20.9
10	26	-0	2235	0	0	0	2998	--	--	16.08	16.08	0.10	0.05	0.02	0.14	0.00	0.00	20.9
11	26	-0	2232	0	0	0	2974	--	--	16.08	16.08	0.10	0.05	0.02	0.14	0.00	0.00	20.9
12	26	-0	2273	0	0	0	2945	--	--	16.08	16.08	0.10	0.05	0.02	0.14	0.00	0.00	20.9
13	26	-0	2271	0	0	0	2922	--	--	16.08	16.08	0.10	0.05	0.02	0.14	0.00	0.00	20.9
14	26	-0	2251	0	0	0	3007	--	--	16.08	16.08	0.10	0.05	0.02	0.14	0.00	0.00	20.9
15	26	-0	2243	0	0	0	2928	--	--	16.08	16.08	0.10	0.05	0.02	0.14	0.00	0.00	20.9
16	26	-0	2262	0	0	0	2990	--	--	16.08	16.08	0.10	0.05	0.02	0.14	0.00	0.00	20.9
17	26	-0	2255	0	0	0	2913	--	--	16.08	16.08	0.10	0.05	0.02	0.14	0.00	0.00	20.9
18	26	-0	3285	0	0	0	4538	--	--	16.08	16.08	0.00	0.08	0.03	0.21	0.00	0.00	20.9
19	26	-0	3448	0	0	0	3975	--	--	16.08	16.08	0.00	0.07	0.03	0.22	0.00	0.00	20.9
20	26	-0	3276	0	0	0	3904	--	--	16.08	16.08	0.00	0.07	0.03	0.21	0.00	0.00	20.9
37	26	-0	3104	0	0	0	4614	--	--	16.08	16.08	0.00	0.08	0.03	0.19	0.00	0.00	20.9
38	26	-0	3376	0	0	0	3677	--	--	16.08	16.08	0.00	0.06	0.03	0.21	0.00	0.00	20.9
39	26	-0	3088	0	0	0	3557	--	--	16.08	16.08	0.00	0.06	0.03	0.19	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	2928	0	0	0	1470	--	--	16.08	16.08	0.00	0.03	0.02	0.18	0.00	0.00	20.9
2	51	-0	2235	0	0	0	1183	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
3	51	-0	2232	0	0	0	1162	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
4	51	-0	2273	0	0	0	1100	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
5	51	-0	2271	0	0	0	1078	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
6	51	-0	2251	0	0	0	1179	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
7	51	-0	2243	0	0	0	1107	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
8	51	-0	2262	0	0	0	1154	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
9	51	-0	2255	0	0	0	1082	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
10	51	-0	2235	0	0	0	1183	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
11	51	-0	2232	0	0	0	1162	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
12	51	-0	2273	0	0	0	1100	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
13	51	-0	2271	0	0	0	1078	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
14	51	-0	2251	0	0	0	1179	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
15	51	-0	2243	0	0	0	1107	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
16	51	-0	2262	0	0	0	1154	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
17	51	-0	2255	0	0	0	1082	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
18	51	-0	3285	0	0	0	1871	--	--	16.08	16.08	0.00	0.03	0.03	0.21	0.00	0.00	20.9
19	51	-0	3448	0	0	0	1176	--	--	16.08	16.08	0.00	0.02	0.03	0.22	0.00	0.00	20.9
20	51	-0	3276	0	0	0	1244	--	--	16.08	16.08	0.00	0.02	0.03	0.21	0.00	0.00	20.9
37	51	-0	3104	0	0	0	2094	--	--	16.08	16.08	0.00	0.04	0.03	0.19	0.00	0.00	20.9
38	51	-0	3376	0	0	0	936	--	--	16.08	16.08	0.00	0.02	0.03	0.21	0.00	0.00	20.9
39	51	-0	3088	0	0	0	1050	--	--	16.08	16.08	0.00	0.02	0.03	0.19	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 9 NI 1524 NF 1523 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm

1	0	-0	3797	0	0	0	414	--	--	16.08	16.08	0.00	0.01	0.03	0.24	0.00	0.00	20.9
2	0	-0	2904	0	0	0	377	--	--	16.08	16.08	0.10	0.01	0.02	0.18	0.00	0.00	20.9
3	0	-0	2905	0	0	0	356	--	--	16.08	16.08	0.10	0.01	0.02	0.18	0.00	0.00	20.9
4	0	-0	2937	0	0	0	281	--	--	16.08	16.08	0.10	0.00	0.02	0.18	0.00	0.00	20.9
5	0	-0	2938	0	0	0	260	--	--	16.08	16.08	0.10	0.00	0.02	0.18	0.00	0.00	20.9
6	0	-0	2914	0	0	0	368	--	--	16.08	16.08	0.10	0.01	0.02	0.18	0.00	0.00	20.9
7	0	-0	2917	0	0	0	298	--	--	16.08	16.08	0.10	0.01	0.02	0.18	0.00	0.00	20.9
8	0	-0	2924	0	0	0	339	--	--	16.08	16.08	0.10	0.01	0.02	0.18	0.00	0.00	20.9
9	0	-0	2927	0	0	0	269	--	--	16.08	16.08	0.10	0.00	0.02	0.18	0.00	0.00	20.9
10	0	-0	2904	0	0	0	377	--	--	16.08	16.08	0.10	0.01	0.02	0.18	0.00	0.00	20.9
11	0	-0	2905	0	0	0	356	--	--	16.08	16.08	0.10	0.01	0.02	0.18	0.00	0.00	20.9
12	0	-0	2937	0	0	0	281	--	--	16.08	16.08	0.10	0.00	0.02	0.18	0.00	0.00	20.9
13	0	-0	2938	0	0	0	260	--	--	16.08	16.08	0.10	0.00	0.02	0.18	0.00	0.00	20.9
14	0	-0	2914	0	0	0	368	--	--	16.08	16.08	0.10	0.01	0.02	0.18	0.00	0.00	20.9
15	0	-0	2917	0	0	0	298	--	--	16.08	16.08	0.10	0.01	0.02	0.18	0.00	0.00	20.9
16	0	-0	2924	0	0	0	339	--	--	16.08	16.08	0.10	0.01	0.02	0.18	0.00	0.00	20.9
17	0	-0	2927	0	0	0	269	--	--	16.08	16.08	0.10	0.00	0.02	0.18	0.00	0.00	20.9
18	0	-0	4302	0	0	0	689	--	--	16.08	16.08	0.00	0.01	0.04	0.27	0.00	0.00	20.9
19	0	-0	4342	0	0	0	-61	--	--	16.08	16.08	0.18	0.00	0.04	0.27	0.00	0.00	20.9
20	0	-0	4242	0	0	0	63	--	--	16.08	16.08	0.00	0.00	0.03	0.27	0.00	0.00	20.9
37	0	-0	4138	0	0	0	976	--	--	16.08	16.08	0.00	0.02	0.03	0.26	0.00	0.00	20.9
38	0	-0	4205	0	0	0	-275	--	--	16.08	16.08	0.18	0.00	0.03	0.26	0.00	0.00	20.9
39	0	-0	4039	0	0	0	-68	--	--	16.08	16.08	0.18	0.00	0.03	0.25	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	3797	0	0	0	5447	--	--	16.08	16.08	0.00	0.09	0.03	0.24	0.00	0.00	20.9
2	26	-0	2904	0	0	0	4227	--	--	16.08	16.08	0.10	0.08	0.02	0.18	0.00	0.00	20.9
3	26	-0	2905	0	0	0	4207	--	--	16.08	16.08	0.10	0.07	0.02	0.18	0.00	0.00	20.9
4	26	-0	2937	0	0	0	4174	--	--	16.08	16.08	0.10	0.07	0.02	0.18	0.00	0.00	20.9
5	26	-0	2938	0	0	0	4154	--	--	16.08	16.08	0.10	0.07	0.02	0.18	0.00	0.00	20.9
6	26	-0	2914	0	0	0	4231	--	--	16.08	16.08	0.10	0.08	0.02	0.18	0.00	0.00	20.9

7	26	-0	2917	0	0	0	4164	--	--	16.08	16.08	0.10	0.07	0.02	0.18	0.00	0.00	20.9
8	26	-0	2924	0	0	0	4215	--	--	16.08	16.08	0.10	0.07	0.02	0.18	0.00	0.00	20.9
9	26	-0	2927	0	0	0	4149	--	--	16.08	16.08	0.10	0.07	0.02	0.18	0.00	0.00	20.9
10	26	-0	2904	0	0	0	4227	--	--	16.08	16.08	0.10	0.08	0.02	0.18	0.00	0.00	20.9
11	26	-0	2905	0	0	0	4207	--	--	16.08	16.08	0.10	0.07	0.02	0.18	0.00	0.00	20.9
12	26	-0	2937	0	0	0	4174	--	--	16.08	16.08	0.10	0.07	0.02	0.18	0.00	0.00	20.9
13	26	-0	2938	0	0	0	4154	--	--	16.08	16.08	0.10	0.07	0.02	0.18	0.00	0.00	20.9
14	26	-0	2914	0	0	0	4231	--	--	16.08	16.08	0.10	0.08	0.02	0.18	0.00	0.00	20.9
15	26	-0	2917	0	0	0	4164	--	--	16.08	16.08	0.10	0.07	0.02	0.18	0.00	0.00	20.9
16	26	-0	2924	0	0	0	4215	--	--	16.08	16.08	0.10	0.07	0.02	0.18	0.00	0.00	20.9
17	26	-0	2927	0	0	0	4149	--	--	16.08	16.08	0.10	0.07	0.02	0.18	0.00	0.00	20.9
18	26	-0	4302	0	0	0	6392	--	--	16.08	16.08	0.00	0.11	0.04	0.27	0.00	0.00	20.9
19	26	-0	4342	0	0	0	5694	--	--	16.08	16.08	0.00	0.10	0.04	0.27	0.00	0.00	20.9
20	26	-0	4242	0	0	0	5686	--	--	16.08	16.08	0.00	0.10	0.03	0.27	0.00	0.00	20.9
37	26	-0	4138	0	0	0	6461	--	--	16.08	16.08	0.00	0.11	0.03	0.26	0.00	0.00	20.9
38	26	-0	4205	0	0	0	5298	--	--	16.08	16.08	0.00	0.09	0.03	0.26	0.00	0.00	20.9
39	26	-0	4039	0	0	0	5286	--	--	16.08	16.08	0.00	0.09	0.03	0.25	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	3797	0	0	0	2364	--	--	16.08	16.08	0.00	0.04	0.03	0.24	0.00	0.00	20.9
2	51	-0	2904	0	0	0	1869	--	--	16.08	16.08	0.10	0.03	0.02	0.18	0.00	0.00	20.9
3	51	-0	2905	0	0	0	1849	--	--	16.08	16.08	0.10	0.03	0.02	0.18	0.00	0.00	20.9
4	51	-0	2937	0	0	0	1789	--	--	16.08	16.08	0.10	0.03	0.02	0.18	0.00	0.00	20.9
5	51	-0	2938	0	0	0	1769	--	--	16.08	16.08	0.10	0.03	0.02	0.18	0.00	0.00	20.9
6	51	-0	2914	0	0	0	1865	--	--	16.08	16.08	0.10	0.03	0.02	0.18	0.00	0.00	20.9
7	51	-0	2917	0	0	0	1796	--	--	16.08	16.08	0.10	0.03	0.02	0.18	0.00	0.00	20.9
8	51	-0	2924	0	0	0	1841	--	--	16.08	16.08	0.10	0.03	0.02	0.18	0.00	0.00	20.9
9	51	-0	2927	0	0	0	1772	--	--	16.08	16.08	0.10	0.03	0.02	0.18	0.00	0.00	20.9
10	51	-0	2904	0	0	0	1869	--	--	16.08	16.08	0.10	0.03	0.02	0.18	0.00	0.00	20.9
11	51	-0	2905	0	0	0	1849	--	--	16.08	16.08	0.10	0.03	0.02	0.18	0.00	0.00	20.9
12	51	-0	2937	0	0	0	1789	--	--	16.08	16.08	0.10	0.03	0.02	0.18	0.00	0.00	20.9
13	51	-0	2938	0	0	0	1769	--	--	16.08	16.08	0.10	0.03	0.02	0.18	0.00	0.00	20.9
14	51	-0	2914	0	0	0	1865	--	--	16.08	16.08	0.10	0.03	0.02	0.18	0.00	0.00	20.9
15	51	-0	2917	0	0	0	1796	--	--	16.08	16.08	0.10	0.03	0.02	0.18	0.00	0.00	20.9
16	51	-0	2924	0	0	0	1841	--	--	16.08	16.08	0.10	0.03	0.02	0.18	0.00	0.00	20.9
17	51	-0	2927	0	0	0	1772	--	--	16.08	16.08	0.10	0.03	0.02	0.18	0.00	0.00	20.9
18	51	-0	4302	0	0	0	2899	--	--	16.08	16.08	0.00	0.05	0.04	0.27	0.00	0.00	20.9
19	51	-0	4342	0	0	0	2169	--	--	16.08	16.08	0.00	0.04	0.04	0.27	0.00	0.00	20.9
20	51	-0	4242	0	0	0	2242	--	--	16.08	16.08	0.00	0.04	0.03	0.27	0.00	0.00	20.9
37	51	-0	4138	0	0	0	3101	--	--	16.08	16.08	0.00	0.05	0.03	0.26	0.00	0.00	20.9
38	51	-0	4205	0	0	0	1884	--	--	16.08	16.08	0.00	0.03	0.03	0.26	0.00	0.00	20.9
39	51	-0	4039	0	0	0	2007	--	--	16.08	16.08	0.00	0.03	0.03	0.25	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 10 NI 1523 NF 1536 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	4240	0	0	0	966	--	--	16.08	16.08	0.00	0.02	0.03	0.27	0.00	0.00	20.9
2	0	-0	3248	0	0	0	799	--	--	16.08	16.08	0.10	0.01	0.03	0.20	0.00	0.00	20.9
3	0	-0	3252	0	0	0	778	--	--	16.08	16.08	0.10	0.01	0.03	0.20	0.00	0.00	20.9
4	0	-0	3271	0	0	0	708	--	--	16.08	16.08	0.10	0.01	0.03	0.21	0.00	0.00	20.9
5	0	-0	3276	0	0	0	687	--	--	16.08	16.08	0.10	0.01	0.03	0.21	0.00	0.00	20.9
6	0	-0	3251	0	0	0	792	--	--	16.08	16.08	0.10	0.01	0.03	0.20	0.00	0.00	20.9
7	0	-0	3265	0	0	0	721	--	--	16.08	16.08	0.10	0.01	0.03	0.20	0.00	0.00	20.9
8	0	-0	3258	0	0	0	765	--	--	16.08	16.08	0.10	0.01	0.03	0.20	0.00	0.00	20.9
9	0	-0	3272	0	0	0	694	--	--	16.08	16.08	0.10	0.01	0.03	0.21	0.00	0.00	20.9
10	0	-0	3248	0	0	0	799	--	--	16.08	16.08	0.10	0.01	0.03	0.20	0.00	0.00	20.9
11	0	-0	3252	0	0	0	778	--	--	16.08	16.08	0.10	0.01	0.03	0.20	0.00	0.00	20.9
12	0	-0	3271	0	0	0	708	--	--	16.08	16.08	0.10	0.01	0.03	0.21	0.00	0.00	20.9
13	0	-0	3276	0	0	0	687	--	--	16.08	16.08	0.10	0.01	0.03	0.21	0.00	0.00	20.9
14	0	-0	3251	0	0	0	792	--	--	16.08	16.08	0.10	0.01	0.03	0.20	0.00	0.00	20.9
15	0	-0	3265	0	0	0	721	--	--	16.08	16.08	0.10	0.01	0.03	0.20	0.00	0.00	20.9
16	0	-0	3258	0	0	0	765	--	--	16.08	16.08	0.10	0.01	0.03	0.20	0.00	0.00	20.9
17	0	-0	3272	0	0	0	694	--	--	16.08	16.08	0.10	0.01	0.03	0.21	0.00	0.00	20.9
18	0	-0	4874	0	0	0	1324	--	--	16.08	16.08	0.00	0.02	0.04	0.31	0.00	0.00	20.9
19	0	-0	4743	0	0	0	572	--	--	16.08	16.08	0.00	0.01	0.04	0.30	0.00	0.00	20.9
20	0	-0	4751	0	0	0	684	--	--	16.08	16.08	0.00	0.01	0.04	0.30	0.00	0.00	20.9
37	0	-0	4755	0	0	0	1587	--	--	16.08	16.08	0.00	0.03	0.04	0.30	0.00	0.00	20.9
38	0	-0	4537	0	0	0	334	--	--	16.08	16.08	0.00	0.01	0.04	0.28	0.00	0.00	20.9
39	0	-0	4549	0	0	0	521	--	--	16.08	16.08	0.00	0.01	0.04	0.29	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	4240	0	0	0	6586	--	--	16.08	16.08	0.00	0.11	0.03	0.27	0.00	0.00	20.9
2	26	-0	3248	0	0	0	5104	--	--	16.08	16.08	0.10	0.09	0.03	0.20	0.00	0.00	20.9
3	26	-0	3252	0	0	0	5089	--	--	16.08	16.08	0.10	0.09	0.03	0.20	0.00	0.00	20.9
4	26	-0	3271	0	0	0	5044	--	--	16.08	16.08	0.10	0.09	0.03	0.21	0.00	0.00	20.9
5	26	-0	3276	0	0	0	5029	--	--	16.08	16.08	0.10	0.09	0.03	0.21	0.00	0.00	20.9
6	26	-0	3251	0	0	0	5101	--	--	16.08	16.08	0.10	0.09	0.03	0.20	0.00	0.00	20.9
7	26	-0	3265	0	0	0	5049	--	--	16.08	16.08	0.10	0.09	0.03	0.20	0.00	0.00	20.9
8	26	-0	3258	0	0	0	5083	--	--	16.08	16.08	0.10	0.09	0.03	0.20	0.00	0.00	20.9
9	26	-0	3272	0	0	0	5031	--	--	16.08	16.08	0.10	0.09	0.03	0.21	0.00	0.00	20.9
10	26	-0	3248	0	0	0	5104	--	--	16.08	16.08	0.10	0.09	0.03	0.20	0.00	0.00	20.9
11	26	-0	3252	0	0	0	5089	--	--	16.08	16.08	0.10	0.09	0.03	0.20	0.00	0.00	20.9
12	26	-0	3271	0	0	0	5044	--	--	16.08	16.08	0.10	0.09	0.03	0.21	0.00	0.00	20.9
13	26	-0	3276	0	0	0	5029	--	--	16.08	16.08	0.10	0.09	0.03	0.21	0.00	0.00	20.9
14	26	-0	3251	0	0	0	5101	--	--	16.08	16.08	0.10	0.09	0.03	0.20	0.00	0.00	20.9
15	26	-0	3265	0	0	0	5049	--	--	16.08	16.08	0.10	0.09	0.03	0.20	0.00	0.00	20.9
16	26	-0	3258	0	0	0	5083	--	--	16.08	16.08	0.10	0.09	0.03	0.20	0.00	0.00	20.9
17	26	-0	3272	0	0	0	5031	--	--	16.08	16.08	0.10	0.09	0.03	0.21	0.00	0.00	20.9
18	26	-0	4874	0	0	0	7785	--	--	16.08	16.08	0.00	0.13	0.04	0.31	0.00	0.00	20.9
19	26	-0	4743	0	0	0	6859	--	--	16.08	16.08	0.00	0.12	0.04	0.30	0.00	0.00	20.9
20	26	-0	4751	0	0	0	6982	--	--	16.08	16.08	0.00	0.12	0.04	0.30	0.00	0.00	20.9
37	26	-0	4755	0	0	0	7890	--	--	16.08	16.08	0.00	0.13	0.04	0.30	0.00	0.00	20.9
38	26	-0	4537	0	0	0	6348	--	--	16.08	16.08	0.00	0.11	0.04	0.28	0.00	0.00	20.9
39	26	-0	4549	0	0	0	6551	--	--	16.08	16.08	0.00	0.11	0.04	0.29	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	4240	0	0	0	3144	--	--	16.08	16.08	0.00	0.05	0.03	0.27	0.00	0.00	20.9
2	51	-0	3248	0	0	0	2467	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9

3	51	-0	3252	0	0	0	2448	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
4	51	-0	3271	0	0	0	2388	--	--	16.08	16.08	0.10	0.04	0.03	0.21	0.00	0.00	20.9
5	51	-0	3276	0	0	0	2369	--	--	16.08	16.08	0.10	0.04	0.03	0.21	0.00	0.00	20.9
6	51	-0	3251	0	0	0	2462	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
7	51	-0	3265	0	0	0	2398	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
8	51	-0	3258	0	0	0	2438	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
9	51	-0	3272	0	0	0	2375	--	--	16.08	16.08	0.10	0.04	0.03	0.21	0.00	0.00	20.9
10	51	-0	3248	0	0	0	2467	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
11	51	-0	3252	0	0	0	2448	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
12	51	-0	3271	0	0	0	2388	--	--	16.08	16.08	0.10	0.04	0.03	0.21	0.00	0.00	20.9
13	51	-0	3276	0	0	0	2369	--	--	16.08	16.08	0.10	0.04	0.03	0.21	0.00	0.00	20.9
14	51	-0	3251	0	0	0	2462	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
15	51	-0	3265	0	0	0	2398	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
16	51	-0	3258	0	0	0	2438	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
17	51	-0	3272	0	0	0	2375	--	--	16.08	16.08	0.10	0.04	0.03	0.21	0.00	0.00	20.9
18	51	-0	4874	0	0	0	3827	--	--	16.08	16.08	0.00	0.07	0.04	0.31	0.00	0.00	20.9
19	51	-0	4743	0	0	0	3008	--	--	16.08	16.08	0.00	0.05	0.04	0.30	0.00	0.00	20.9
20	51	-0	4751	0	0	0	3124	--	--	16.08	16.08	0.00	0.05	0.04	0.30	0.00	0.00	20.9
37	51	-0	4755	0	0	0	4029	--	--	16.08	16.08	0.00	0.07	0.04	0.30	0.00	0.00	20.9
38	51	-0	4537	0	0	0	2664	--	--	16.08	16.08	0.00	0.05	0.04	0.28	0.00	0.00	20.9
39	51	-0	4549	0	0	0	2857	--	--	16.08	16.08	0.00	0.05	0.04	0.29	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 11 NI 1536 NF 1539 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--												Fx,M	Bielle	V,Mx			
	cm		daN			daN*m				cmq						cmq/m		cm
1	0	-0	3679	0	0	0	1914	--	--	16.08	16.08	0.00	0.03	0.03	0.23	0.00	0.00	20.9
2	0	-0	2815	0	0	0	1525	--	--	16.08	16.08	0.10	0.03	0.02	0.18	0.00	0.00	20.9
3	0	-0	2821	0	0	0	1505	--	--	16.08	16.08	0.10	0.03	0.02	0.18	0.00	0.00	20.9
4	0	-0	2838	0	0	0	1440	--	--	16.08	16.08	0.10	0.03	0.02	0.18	0.00	0.00	20.9
5	0	-0	2845	0	0	0	1419	--	--	16.08	16.08	0.10	0.03	0.02	0.18	0.00	0.00	20.9
6	0	-0	2815	0	0	0	1519	--	--	16.08	16.08	0.10	0.03	0.02	0.18	0.00	0.00	20.9
7	0	-0	2837	0	0	0	1451	--	--	16.08	16.08	0.10	0.03	0.02	0.18	0.00	0.00	20.9
8	0	-0	2822	0	0	0	1494	--	--	16.08	16.08	0.10	0.03	0.02	0.18	0.00	0.00	20.9
9	0	-0	2844	0	0	0	1425	--	--	16.08	16.08	0.10	0.03	0.02	0.18	0.00	0.00	20.9
10	0	-0	2815	0	0	0	1525	--	--	16.08	16.08	0.10	0.03	0.02	0.18	0.00	0.00	20.9
11	0	-0	2821	0	0	0	1505	--	--	16.08	16.08	0.10	0.03	0.02	0.18	0.00	0.00	20.9
12	0	-0	2838	0	0	0	1440	--	--	16.08	16.08	0.10	0.03	0.02	0.18	0.00	0.00	20.9
13	0	-0	2845	0	0	0	1419	--	--	16.08	16.08	0.10	0.03	0.02	0.18	0.00	0.00	20.9
14	0	-0	2815	0	0	0	1519	--	--	16.08	16.08	0.10	0.03	0.02	0.18	0.00	0.00	20.9
15	0	-0	2837	0	0	0	1451	--	--	16.08	16.08	0.10	0.03	0.02	0.18	0.00	0.00	20.9
16	0	-0	2822	0	0	0	1494	--	--	16.08	16.08	0.10	0.03	0.02	0.18	0.00	0.00	20.9
17	0	-0	2844	0	0	0	1425	--	--	16.08	16.08	0.10	0.03	0.02	0.18	0.00	0.00	20.9
18	0	-0	4250	0	0	0	2399	--	--	16.08	16.08	0.00	0.04	0.04	0.27	0.00	0.00	20.9
19	0	-0	4109	0	0	0	1640	--	--	16.08	16.08	0.00	0.03	0.03	0.26	0.00	0.00	20.9
20	0	-0	4165	0	0	0	1738	--	--	16.08	16.08	0.00	0.03	0.03	0.26	0.00	0.00	20.9
37	0	-0	4153	0	0	0	2629	--	--	16.08	16.08	0.00	0.04	0.03	0.26	0.00	0.00	20.9
38	0	-0	3917	0	0	0	1364	--	--	16.08	16.08	0.00	0.02	0.03	0.25	0.00	0.00	20.9
39	0	-0	4011	0	0	0	1529	--	--	16.08	16.08	0.00	0.03	0.03	0.25	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	3679	0	0	0	6790	--	--	16.08	16.08	0.00	0.12	0.03	0.23	0.00	0.00	20.9
2	26	-0	2815	0	0	0	5257	--	--	16.08	16.08	0.10	0.09	0.02	0.18	0.00	0.00	20.9
3	26	-0	2821	0	0	0	5244	--	--	16.08	16.08	0.10	0.09	0.02	0.18	0.00	0.00	20.9
4	26	-0	2838	0	0	0	5202	--	--	16.08	16.08	0.10	0.09	0.02	0.18	0.00	0.00	20.9
5	26	-0	2845	0	0	0	5191	--	--	16.08	16.08	0.10	0.09	0.02	0.18	0.00	0.00	20.9
6	26	-0	2815	0	0	0	5251	--	--	16.08	16.08	0.10	0.09	0.02	0.18	0.00	0.00	20.9
7	26	-0	2837	0	0	0	5212	--	--	16.08	16.08	0.10	0.09	0.02	0.18	0.00	0.00	20.9
8	26	-0	2822	0	0	0	5235	--	--	16.08	16.08	0.10	0.09	0.02	0.18	0.00	0.00	20.9
9	26	-0	2844	0	0	0	5195	--	--	16.08	16.08	0.10	0.09	0.02	0.18	0.00	0.00	20.9
10	26	-0	2815	0	0	0	5257	--	--	16.08	16.08	0.10	0.09	0.02	0.18	0.00	0.00	20.9
11	26	-0	2821	0	0	0	5244	--	--	16.08	16.08	0.10	0.09	0.02	0.18	0.00	0.00	20.9
12	26	-0	2838	0	0	0	5202	--	--	16.08	16.08	0.10	0.09	0.02	0.18	0.00	0.00	20.9
13	26	-0	2845	0	0	0	5191	--	--	16.08	16.08	0.10	0.09	0.02	0.18	0.00	0.00	20.9
14	26	-0	2815	0	0	0	5251	--	--	16.08	16.08	0.10	0.09	0.02	0.18	0.00	0.00	20.9
15	26	-0	2837	0	0	0	5212	--	--	16.08	16.08	0.10	0.09	0.02	0.18	0.00	0.00	20.9
16	26	-0	2822	0	0	0	5235	--	--	16.08	16.08	0.10	0.09	0.02	0.18	0.00	0.00	20.9
17	26	-0	2844	0	0	0	5195	--	--	16.08	16.08	0.10	0.09	0.02	0.18	0.00	0.00	20.9
18	26	-0	4250	0	0	0	8033	--	--	16.08	16.08	0.00	0.14	0.04	0.27	0.00	0.00	20.9
19	26	-0	4109	0	0	0	7086	--	--	16.08	16.08	0.00	0.12	0.03	0.26	0.00	0.00	20.9
20	26	-0	4165	0	0	0	7259	--	--	16.08	16.08	0.00	0.12	0.03	0.26	0.00	0.00	20.9
37	26	-0	4153	0	0	0	8135	--	--	16.08	16.08	0.00	0.14	0.03	0.26	0.00	0.00	20.9
38	26	-0	3917	0	0	0	6556	--	--	16.08	16.08	0.00	0.11	0.03	0.25	0.00	0.00	20.9
39	26	-0	4011	0	0	0	6846	--	--	16.08	16.08	0.00	0.12	0.03	0.25	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	3679	0	0	0	3803	--	--	16.08	16.08	0.00	0.06	0.03	0.23	0.00	0.00	20.9
2	51	-0	2815	0	0	0	2971	--	--	16.08	16.08	0.10	0.05	0.02	0.18	0.00	0.00	20.9
3	51	-0	2821	0	0	0	2954	--	--	16.08	16.08	0.10	0.05	0.02	0.18	0.00	0.00	20.9
4	51	-0	2838	0	0	0	2898	--	--	16.08	16.08	0.10	0.05	0.02	0.18	0.00	0.00	20.9
5	51	-0	2845	0	0	0	2881	--	--	16.08	16.08	0.10	0.05	0.02	0.18	0.00	0.00	20.9
6	51	-0	2815	0	0	0	2965	--	--	16.08	16.08	0.10	0.05	0.02	0.18	0.00	0.00	20.9
7	51	-0	2837	0	0	0	2908	--	--	16.08	16.08	0.10	0.05	0.02	0.18	0.00	0.00	20.9
8	51	-0	2822	0	0	0	2943	--	--	16.08	16.08	0.10	0.05	0.02	0.18	0.00	0.00	20.9
9	51	-0	2844	0	0	0	2886	--	--	16.08	16.08	0.10	0.05	0.02	0.18	0.00	0.00	20.9
10	51	-0	2815	0	0	0	2971	--	--	16.08	16.08	0.10	0.05	0.02	0.18	0.00	0.00	20.9
11	51	-0	2821	0	0	0	2954	--	--	16.08	16.08	0.10	0.05	0.02	0.18	0.00	0.00	20.9
12	51	-0	2838	0	0	0	2898	--	--	16.08	16.08	0.10	0.05	0.02	0.18	0.00	0.00	20.9
13	51	-0	2845	0	0	0	2881	--	--	16.08	16.08	0.10	0.05	0.02	0.18	0.00	0.00	20.9
14	51	-0	2815	0	0	0	2965	--	--	16.08	16.08	0.10	0.05	0.02	0.18	0.00	0.00	20.9
15	51	-0	2837	0	0	0	2908	--	--	16.08	16.08	0.10	0.05	0.02	0.18	0.00	0.00	20.9
16	51	-0	2822	0	0	0	2943	--	--	16.08	16.08	0.10	0.05	0.02	0.18	0.00	0.00	20.9
17	51	-0	2844	0	0	0	2886	--	--	16.08	16.08	0.10	0.05	0.02	0.18	0.00	0.00	20.9
18	51	-0	4250	0	0	0	4582	--	--	16.08	16.08	0.00	0.08	0.04	0.27	0.00	0.00	20.9
19	51	-0	4109	0	0	0	3750	--	--	16.08	16.08	0.00	0.06	0.03	0.26	0.00	0.00	20.9
20	51	-0	4165	0	0	0	3878	--	--	16.08	16.08	0.00	0.07	0.03	0.26	0.00	0.00	20.9
37	51	-0	4153	0	0	0	4763	--	--	16.08	16.08	0.00	0.08	0.03	0.26	0.00	0.00	20.9
38	51	-0	3917	0	0	0	3376	--	--	16.08	16.08	0.00	0.06	0.03	0.25	0.00	0.00	20.9
39	51	-0	4011	0	0	0	3589	--	--	16.08	16.08	0.00	0.06	0.03	0.25	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 12 NI 1539 NF 1501 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-3792	0	0	0	3854	--	--	16.08	16.08	0.00	0.07	0.03	0.24	0.00	0.00	20.9
2	0	-0	-2939	0	0	0	3016	--	--	16.08	16.08	0.10	0.05	0.02	0.18	0.00	0.00	20.9
3	0	-0	-2937	0	0	0	2997	--	--	16.08	16.08	0.10	0.05	0.02	0.18	0.00	0.00	20.9
4	0	-0	-2896	0	0	0	2932	--	--	16.08	16.08	0.10	0.05	0.02	0.18	0.00	0.00	20.9
5	0	-0	-2895	0	0	0	2913	--	--	16.08	16.08	0.10	0.05	0.02	0.18	0.00	0.00	20.9
6	0	-0	-2926	0	0	0	3009	--	--	16.08	16.08	0.10	0.05	0.02	0.18	0.00	0.00	20.9
7	0	-0	-2920	0	0	0	2945	--	--	16.08	16.08	0.10	0.05	0.02	0.18	0.00	0.00	20.9
8	0	-0	-2913	0	0	0	2983	--	--	16.08	16.08	0.10	0.05	0.02	0.18	0.00	0.00	20.9
9	0	-0	-2908	0	0	0	2920	--	--	16.08	16.08	0.10	0.05	0.02	0.18	0.00	0.00	20.9
10	0	-0	-2939	0	0	0	3016	--	--	16.08	16.08	0.10	0.05	0.02	0.18	0.00	0.00	20.9
11	0	-0	-2937	0	0	0	2997	--	--	16.08	16.08	0.10	0.05	0.02	0.18	0.00	0.00	20.9
12	0	-0	-2896	0	0	0	2932	--	--	16.08	16.08	0.10	0.05	0.02	0.18	0.00	0.00	20.9
13	0	-0	-2895	0	0	0	2913	--	--	16.08	16.08	0.10	0.05	0.02	0.18	0.00	0.00	20.9
14	0	-0	-2926	0	0	0	3009	--	--	16.08	16.08	0.10	0.05	0.02	0.18	0.00	0.00	20.9
15	0	-0	-2920	0	0	0	2945	--	--	16.08	16.08	0.10	0.05	0.02	0.18	0.00	0.00	20.9
16	0	-0	-2913	0	0	0	2983	--	--	16.08	16.08	0.10	0.05	0.02	0.18	0.00	0.00	20.9
17	0	-0	-2908	0	0	0	2920	--	--	16.08	16.08	0.10	0.05	0.02	0.18	0.00	0.00	20.9
18	0	-0	-4277	0	0	0	4592	--	--	16.08	16.08	0.00	0.08	0.04	0.27	0.00	0.00	20.9
19	0	-0	-3854	0	0	0	3749	--	--	16.08	16.08	0.00	0.06	0.03	0.24	0.00	0.00	20.9
20	0	-0	-3946	0	0	0	3859	--	--	16.08	16.08	0.00	0.07	0.03	0.25	0.00	0.00	20.9
37	0	-0	-4348	0	0	0	4792	--	--	16.08	16.08	0.00	0.08	0.04	0.27	0.00	0.00	20.9
38	0	-0	-3643	0	0	0	3386	--	--	16.08	16.08	0.00	0.06	0.03	0.23	0.00	0.00	20.9
39	0	-0	-3797	0	0	0	3570	--	--	16.08	16.08	0.00	0.06	0.03	0.24	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	-3792	0	0	0	3854	--	--	16.08	16.08	0.00	0.07	0.03	0.24	0.00	0.00	20.9
2	26	-0	-2939	0	0	0	3016	--	--	16.08	16.08	0.10	0.05	0.02	0.18	0.00	0.00	20.9
3	26	-0	-2937	0	0	0	2997	--	--	16.08	16.08	0.10	0.05	0.02	0.18	0.00	0.00	20.9
4	26	-0	-2896	0	0	0	2932	--	--	16.08	16.08	0.10	0.05	0.02	0.18	0.00	0.00	20.9
5	26	-0	-2895	0	0	0	2913	--	--	16.08	16.08	0.10	0.05	0.02	0.18	0.00	0.00	20.9
6	26	-0	-2926	0	0	0	3009	--	--	16.08	16.08	0.10	0.05	0.02	0.18	0.00	0.00	20.9
7	26	-0	-2920	0	0	0	2945	--	--	16.08	16.08	0.10	0.05	0.02	0.18	0.00	0.00	20.9
8	26	-0	-2913	0	0	0	2983	--	--	16.08	16.08	0.10	0.05	0.02	0.18	0.00	0.00	20.9
9	26	-0	-2908	0	0	0	2920	--	--	16.08	16.08	0.10	0.05	0.02	0.18	0.00	0.00	20.9
10	26	-0	-2939	0	0	0	3016	--	--	16.08	16.08	0.10	0.05	0.02	0.18	0.00	0.00	20.9
11	26	-0	-2937	0	0	0	2997	--	--	16.08	16.08	0.10	0.05	0.02	0.18	0.00	0.00	20.9
12	26	-0	-2896	0	0	0	2932	--	--	16.08	16.08	0.10	0.05	0.02	0.18	0.00	0.00	20.9
13	26	-0	-2895	0	0	0	2913	--	--	16.08	16.08	0.10	0.05	0.02	0.18	0.00	0.00	20.9
14	26	-0	-2926	0	0	0	3009	--	--	16.08	16.08	0.10	0.05	0.02	0.18	0.00	0.00	20.9
15	26	-0	-2920	0	0	0	2945	--	--	16.08	16.08	0.10	0.05	0.02	0.18	0.00	0.00	20.9
16	26	-0	-2913	0	0	0	2983	--	--	16.08	16.08	0.10	0.05	0.02	0.18	0.00	0.00	20.9
17	26	-0	-2908	0	0	0	2920	--	--	16.08	16.08	0.10	0.05	0.02	0.18	0.00	0.00	20.9
18	26	-0	-4277	0	0	0	4592	--	--	16.08	16.08	0.00	0.08	0.04	0.27	0.00	0.00	20.9
19	26	-0	-3854	0	0	0	3749	--	--	16.08	16.08	0.00	0.06	0.03	0.24	0.00	0.00	20.9
20	26	-0	-3946	0	0	0	3859	--	--	16.08	16.08	0.00	0.07	0.03	0.25	0.00	0.00	20.9
37	26	-0	-4348	0	0	0	4792	--	--	16.08	16.08	0.00	0.08	0.04	0.27	0.00	0.00	20.9
38	26	-0	-3643	0	0	0	3386	--	--	16.08	16.08	0.00	0.06	0.03	0.23	0.00	0.00	20.9
39	26	-0	-3797	0	0	0	3570	--	--	16.08	16.08	0.00	0.06	0.03	0.24	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	-3792	0	0	0	1906	--	--	16.08	16.08	0.00	0.03	0.03	0.24	0.00	0.00	20.9
2	51	-0	-2939	0	0	0	1507	--	--	16.08	16.08	0.10	0.03	0.02	0.18	0.00	0.00	20.9
3	51	-0	-2937	0	0	0	1488	--	--	16.08	16.08	0.10	0.03	0.02	0.18	0.00	0.00	20.9
4	51	-0	-2896	0	0	0	1444	--	--	16.08	16.08	0.10	0.03	0.02	0.18	0.00	0.00	20.9
5	51	-0	-2895	0	0	0	1426	--	--	16.08	16.08	0.10	0.03	0.02	0.18	0.00	0.00	20.9
6	51	-0	-2926	0	0	0	1506	--	--	16.08	16.08	0.10	0.03	0.02	0.18	0.00	0.00	20.9
7	51	-0	-2920	0	0	0	1445	--	--	16.08	16.08	0.10	0.03	0.02	0.18	0.00	0.00	20.9
8	51	-0	-2913	0	0	0	1487	--	--	16.08	16.08	0.10	0.03	0.02	0.18	0.00	0.00	20.9
9	51	-0	-2908	0	0	0	1427	--	--	16.08	16.08	0.10	0.03	0.02	0.18	0.00	0.00	20.9
10	51	-0	-2939	0	0	0	1507	--	--	16.08	16.08	0.10	0.03	0.02	0.18	0.00	0.00	20.9
11	51	-0	-2937	0	0	0	1488	--	--	16.08	16.08	0.10	0.03	0.02	0.18	0.00	0.00	20.9
12	51	-0	-2896	0	0	0	1444	--	--	16.08	16.08	0.10	0.03	0.02	0.18	0.00	0.00	20.9
13	51	-0	-2895	0	0	0	1426	--	--	16.08	16.08	0.10	0.03	0.02	0.18	0.00	0.00	20.9
14	51	-0	-2926	0	0	0	1506	--	--	16.08	16.08	0.10	0.03	0.02	0.18	0.00	0.00	20.9
15	51	-0	-2920	0	0	0	1445	--	--	16.08	16.08	0.10	0.03	0.02	0.18	0.00	0.00	20.9
16	51	-0	-2913	0	0	0	1487	--	--	16.08	16.08	0.10	0.03	0.02	0.18	0.00	0.00	20.9
17	51	-0	-2908	0	0	0	1427	--	--	16.08	16.08	0.10	0.03	0.02	0.18	0.00	0.00	20.9
18	51	-0	-4277	0	0	0	2396	--	--	16.08	16.08	0.00	0.04	0.04	0.27	0.00	0.00	20.9
19	51	-0	-3854	0	0	0	1770	--	--	16.08	16.08	0.00	0.03	0.03	0.24	0.00	0.00	20.9
20	51	-0	-3946	0	0	0	1832	--	--	16.08	16.08	0.00	0.03	0.03	0.25	0.00	0.00	20.9
37	51	-0	-4348	0	0	0	2558	--	--	16.08	16.08	0.00	0.04	0.04	0.27	0.00	0.00	20.9
38	51	-0	-3643	0	0	0	1515	--	--	16.08	16.08	0.00	0.03	0.03	0.23	0.00	0.00	20.9
39	51	-0	-3797	0	0	0	1619	--	--	16.08	16.08	0.00	0.03	0.03	0.24	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 13 NI 1501 NF 1517 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-4189	0	0	0	3157	--	--	16.08	16.08	0.00	0.05	0.03	0.26	0.00	0.00	20.9
2	0	-0	-3248	0	0	0	2476	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
3	0	-0	-3245	0	0	0	2457	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
4	0	-0	-3200	0	0	0	2400	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
5	0	-0	-3197	0	0	0	2381	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
6	0	-0	-3234	0	0	0	2472	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
7	0	-0	-3225	0	0	0	2408	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
8	0	-0	-3220	0	0	0	2449	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
9	0	-0	-3210	0	0	0	2385	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
10	0	-0	-3248	0	0	0	2476	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9

11	0	-0	-3245	0	0	0	2457	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
12	0	-0	-3200	0	0	0	2400	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
13	0	-0	-3197	0	0	0	2381	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
14	0	-0	-3234	0	0	0	2472	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
15	0	-0	-3225	0	0	0	2408	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
16	0	-0	-3220	0	0	0	2449	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
17	0	-0	-3210	0	0	0	2385	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
18	0	-0	-4789	0	0	0	3811	--	--	16.08	16.08	0.00	0.06	0.04	0.30	0.00	0.00	20.9
19	0	-0	-4250	0	0	0	3045	--	--	16.08	16.08	0.00	0.05	0.04	0.27	0.00	0.00	20.9
20	0	-0	-4377	0	0	0	3134	--	--	16.08	16.08	0.00	0.05	0.04	0.27	0.00	0.00	20.9
37	0	-0	-4884	0	0	0	3996	--	--	16.08	16.08	0.00	0.07	0.04	0.31	0.00	0.00	20.9
38	0	-0	-3986	0	0	0	2720	--	--	16.08	16.08	0.00	0.05	0.03	0.25	0.00	0.00	20.9
39	0	-0	-4198	0	0	0	2868	--	--	16.08	16.08	0.00	0.05	0.03	0.26	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	-4189	0	0	0	3157	--	--	16.08	16.08	0.00	0.05	0.03	0.26	0.00	0.00	20.9
2	26	-0	-3248	0	0	0	2476	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
3	26	-0	-3245	0	0	0	2457	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
4	26	-0	-3200	0	0	0	2400	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
5	26	-0	-3197	0	0	0	2381	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
6	26	-0	-3234	0	0	0	2472	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
7	26	-0	-3225	0	0	0	2408	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
8	26	-0	-3220	0	0	0	2449	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
9	26	-0	-3210	0	0	0	2385	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
10	26	-0	-3248	0	0	0	2476	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
11	26	-0	-3245	0	0	0	2457	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
12	26	-0	-3200	0	0	0	2400	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
13	26	-0	-3197	0	0	0	2381	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
14	26	-0	-3234	0	0	0	2472	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
15	26	-0	-3225	0	0	0	2408	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
16	26	-0	-3220	0	0	0	2449	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
17	26	-0	-3210	0	0	0	2385	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
18	26	-0	-4789	0	0	0	3811	--	--	16.08	16.08	0.00	0.06	0.04	0.30	0.00	0.00	20.9
19	26	-0	-4250	0	0	0	3045	--	--	16.08	16.08	0.00	0.05	0.04	0.27	0.00	0.00	20.9
20	26	-0	-4377	0	0	0	3134	--	--	16.08	16.08	0.00	0.05	0.04	0.27	0.00	0.00	20.9
37	26	-0	-4884	0	0	0	3996	--	--	16.08	16.08	0.00	0.07	0.04	0.31	0.00	0.00	20.9
38	26	-0	-3986	0	0	0	2720	--	--	16.08	16.08	0.00	0.05	0.03	0.25	0.00	0.00	20.9
39	26	-0	-4198	0	0	0	2868	--	--	16.08	16.08	0.00	0.05	0.03	0.26	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	-4189	0	0	0	1005	--	--	16.08	16.08	0.00	0.02	0.03	0.26	0.00	0.00	20.9
2	51	-0	-3248	0	0	0	808	--	--	16.08	16.08	0.10	0.01	0.03	0.20	0.00	0.00	20.9
3	51	-0	-3245	0	0	0	790	--	--	16.08	16.08	0.10	0.01	0.03	0.20	0.00	0.00	20.9
4	51	-0	-3200	0	0	0	756	--	--	16.08	16.08	0.10	0.01	0.03	0.20	0.00	0.00	20.9
5	51	-0	-3197	0	0	0	739	--	--	16.08	16.08	0.10	0.01	0.03	0.20	0.00	0.00	20.9
6	51	-0	-3234	0	0	0	810	--	--	16.08	16.08	0.10	0.01	0.03	0.20	0.00	0.00	20.9
7	51	-0	-3225	0	0	0	752	--	--	16.08	16.08	0.10	0.01	0.03	0.20	0.00	0.00	20.9
8	51	-0	-3220	0	0	0	795	--	--	16.08	16.08	0.10	0.01	0.03	0.20	0.00	0.00	20.9
9	51	-0	-3210	0	0	0	736	--	--	16.08	16.08	0.10	0.01	0.03	0.20	0.00	0.00	20.9
10	51	-0	-3248	0	0	0	808	--	--	16.08	16.08	0.10	0.01	0.03	0.20	0.00	0.00	20.9
11	51	-0	-3245	0	0	0	790	--	--	16.08	16.08	0.10	0.01	0.03	0.20	0.00	0.00	20.9
12	51	-0	-3200	0	0	0	756	--	--	16.08	16.08	0.10	0.01	0.03	0.20	0.00	0.00	20.9
13	51	-0	-3197	0	0	0	739	--	--	16.08	16.08	0.10	0.01	0.03	0.20	0.00	0.00	20.9
14	51	-0	-3234	0	0	0	810	--	--	16.08	16.08	0.10	0.01	0.03	0.20	0.00	0.00	20.9
15	51	-0	-3225	0	0	0	752	--	--	16.08	16.08	0.10	0.01	0.03	0.20	0.00	0.00	20.9
16	51	-0	-3220	0	0	0	795	--	--	16.08	16.08	0.10	0.01	0.03	0.20	0.00	0.00	20.9
17	51	-0	-3210	0	0	0	736	--	--	16.08	16.08	0.10	0.01	0.03	0.20	0.00	0.00	20.9
18	51	-0	-4789	0	0	0	1351	--	--	16.08	16.08	0.00	0.02	0.04	0.30	0.00	0.00	20.9
19	51	-0	-4250	0	0	0	862	--	--	16.08	16.08	0.00	0.01	0.04	0.27	0.00	0.00	20.9
20	51	-0	-4377	0	0	0	886	--	--	16.08	16.08	0.00	0.02	0.04	0.27	0.00	0.00	20.9
37	51	-0	-4884	0	0	0	1488	--	--	16.08	16.08	0.00	0.03	0.04	0.31	0.00	0.00	20.9
38	51	-0	-3986	0	0	0	673	--	--	16.08	16.08	0.00	0.01	0.03	0.25	0.00	0.00	20.9
39	51	-0	-4198	0	0	0	712	--	--	16.08	16.08	0.00	0.01	0.03	0.26	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 14 NI 1517 NF 1516 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-3439	0	0	0	2269	--	--	16.08	16.08	0.00	0.04	0.03	0.22	0.00	0.00	20.9
2	0	-0	-2673	0	0	0	1790	--	--	16.08	16.08	0.10	0.03	0.02	0.17	0.00	0.00	20.9
3	0	-0	-2670	0	0	0	1771	--	--	16.08	16.08	0.10	0.03	0.02	0.17	0.00	0.00	20.9
4	0	-0	-2622	0	0	0	1719	--	--	16.08	16.08	0.10	0.03	0.02	0.16	0.00	0.00	20.9
5	0	-0	-2618	0	0	0	1701	--	--	16.08	16.08	0.10	0.03	0.02	0.16	0.00	0.00	20.9
6	0	-0	-2660	0	0	0	1787	--	--	16.08	16.08	0.10	0.03	0.02	0.17	0.00	0.00	20.9
7	0	-0	-2647	0	0	0	1725	--	--	16.08	16.08	0.10	0.03	0.02	0.17	0.00	0.00	20.9
8	0	-0	-2644	0	0	0	1766	--	--	16.08	16.08	0.10	0.03	0.02	0.17	0.00	0.00	20.9
9	0	-0	-2632	0	0	0	1704	--	--	16.08	16.08	0.10	0.03	0.02	0.17	0.00	0.00	20.9
10	0	-0	-2673	0	0	0	1790	--	--	16.08	16.08	0.10	0.03	0.02	0.17	0.00	0.00	20.9
11	0	-0	-2670	0	0	0	1771	--	--	16.08	16.08	0.10	0.03	0.02	0.17	0.00	0.00	20.9
12	0	-0	-2622	0	0	0	1719	--	--	16.08	16.08	0.10	0.03	0.02	0.16	0.00	0.00	20.9
13	0	-0	-2618	0	0	0	1701	--	--	16.08	16.08	0.10	0.03	0.02	0.16	0.00	0.00	20.9
14	0	-0	-2660	0	0	0	1787	--	--	16.08	16.08	0.10	0.03	0.02	0.17	0.00	0.00	20.9
15	0	-0	-2647	0	0	0	1725	--	--	16.08	16.08	0.10	0.03	0.02	0.17	0.00	0.00	20.9
16	0	-0	-2644	0	0	0	1766	--	--	16.08	16.08	0.10	0.03	0.02	0.17	0.00	0.00	20.9
17	0	-0	-2632	0	0	0	1704	--	--	16.08	16.08	0.10	0.03	0.02	0.17	0.00	0.00	20.9
18	0	-0	-3996	0	0	0	2831	--	--	16.08	16.08	0.00	0.05	0.03	0.25	0.00	0.00	20.9
19	0	-0	-3401	0	0	0	2108	--	--	16.08	16.08	0.00	0.04	0.03	0.21	0.00	0.00	20.9
20	0	-0	-3570	0	0	0	2205	--	--	16.08	16.08	0.00	0.04	0.03	0.22	0.00	0.00	20.9
37	0	-0	-4130	0	0	0	3021	--	--	16.08	16.08	0.00	0.05	0.03	0.26	0.00	0.00	20.9
38	0	-0	-3139	0	0	0	1815	--	--	16.08	16.08	0.00	0.03	0.03	0.20	0.00	0.00	20.9
39	0	-0	-3421	0	0	0	1978	--	--	16.08	16.08	0.00	0.03	0.03	0.21	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	-3439	0	0	0	2269	--	--	16.08	16.08	0.00	0.04	0.03	0.22	0.00	0.00	20.9
2	26	-0	-2673	0	0	0	1790	--	--	16.08	16.08	0.10	0.03	0.02	0.17	0.00	0.00	20.9
3	26	-0	-2670	0	0	0	1771	--	--	16.08	16.08	0.10	0.03	0.02	0.17	0.00	0.00	20.9
4	26	-0	-2622	0	0	0	1719	--	--	16.08	16.08	0.10	0.03	0.02	0.16	0.00	0.00	20.9
5	26	-0	-2618	0	0	0	1701	--	--	16.08	16.08	0.10	0.03	0.02	0.16	0.00	0.00	20.9
6	26	-0	-2660	0	0	0	1787	--	--	16.08	16.08	0.10	0.03	0.02	0.17	0.00	0.00	20.9

7	26	-0	-2647	0	0	0	1725	--	--	16.08	16.08	0.10	0.03	0.02	0.17	0.00	0.00	20.9
8	26	-0	-2644	0	0	0	1766	--	--	16.08	16.08	0.10	0.03	0.02	0.17	0.00	0.00	20.9
9	26	-0	-2632	0	0	0	1704	--	--	16.08	16.08	0.10	0.03	0.02	0.17	0.00	0.00	20.9
10	26	-0	-2673	0	0	0	1790	--	--	16.08	16.08	0.10	0.03	0.02	0.17	0.00	0.00	20.9
11	26	-0	-2670	0	0	0	1771	--	--	16.08	16.08	0.10	0.03	0.02	0.17	0.00	0.00	20.9
12	26	-0	-2622	0	0	0	1719	--	--	16.08	16.08	0.10	0.03	0.02	0.16	0.00	0.00	20.9
13	26	-0	-2618	0	0	0	1701	--	--	16.08	16.08	0.10	0.03	0.02	0.16	0.00	0.00	20.9
14	26	-0	-2660	0	0	0	1787	--	--	16.08	16.08	0.10	0.03	0.02	0.17	0.00	0.00	20.9
15	26	-0	-2647	0	0	0	1725	--	--	16.08	16.08	0.10	0.03	0.02	0.17	0.00	0.00	20.9
16	26	-0	-2644	0	0	0	1766	--	--	16.08	16.08	0.10	0.03	0.02	0.17	0.00	0.00	20.9
17	26	-0	-2632	0	0	0	1704	--	--	16.08	16.08	0.10	0.03	0.02	0.17	0.00	0.00	20.9
18	26	-0	-3996	0	0	0	2831	--	--	16.08	16.08	0.00	0.05	0.03	0.25	0.00	0.00	20.9
19	26	-0	-3401	0	0	0	2108	--	--	16.08	16.08	0.00	0.04	0.03	0.21	0.00	0.00	20.9
20	26	-0	-3570	0	0	0	2205	--	--	16.08	16.08	0.00	0.04	0.03	0.22	0.00	0.00	20.9
37	26	-0	-4130	0	0	0	3021	--	--	16.08	16.08	0.00	0.05	0.03	0.26	0.00	0.00	20.9
38	26	-0	-3139	0	0	0	1815	--	--	16.08	16.08	0.00	0.03	0.03	0.20	0.00	0.00	20.9
39	26	-0	-3421	0	0	0	1978	--	--	16.08	16.08	0.00	0.03	0.03	0.21	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	-3439	0	0	0	502	--	--	16.08	16.08	0.00	0.01	0.03	0.22	0.00	0.00	20.9
2	51	-0	-2673	0	0	0	417	--	--	16.08	16.08	0.10	0.01	0.02	0.17	0.00	0.00	20.9
3	51	-0	-2670	0	0	0	400	--	--	16.08	16.08	0.10	0.01	0.02	0.17	0.00	0.00	20.9
4	51	-0	-2622	0	0	0	373	--	--	16.08	16.08	0.10	0.01	0.02	0.16	0.00	0.00	20.9
5	51	-0	-2618	0	0	0	356	--	--	16.08	16.08	0.10	0.01	0.02	0.16	0.00	0.00	20.9
6	51	-0	-2660	0	0	0	421	--	--	16.08	16.08	0.10	0.01	0.02	0.17	0.00	0.00	20.9
7	51	-0	-2647	0	0	0	365	--	--	16.08	16.08	0.10	0.01	0.02	0.17	0.00	0.00	20.9
8	51	-0	-2644	0	0	0	407	--	--	16.08	16.08	0.10	0.01	0.02	0.17	0.00	0.00	20.9
9	51	-0	-2632	0	0	0	352	--	--	16.08	16.08	0.10	0.01	0.02	0.17	0.00	0.00	20.9
10	51	-0	-2673	0	0	0	417	--	--	16.08	16.08	0.10	0.01	0.02	0.17	0.00	0.00	20.9
11	51	-0	-2670	0	0	0	400	--	--	16.08	16.08	0.10	0.01	0.02	0.17	0.00	0.00	20.9
12	51	-0	-2622	0	0	0	373	--	--	16.08	16.08	0.10	0.01	0.02	0.16	0.00	0.00	20.9
13	51	-0	-2618	0	0	0	356	--	--	16.08	16.08	0.10	0.01	0.02	0.16	0.00	0.00	20.9
14	51	-0	-2660	0	0	0	421	--	--	16.08	16.08	0.10	0.01	0.02	0.17	0.00	0.00	20.9
15	51	-0	-2647	0	0	0	365	--	--	16.08	16.08	0.10	0.01	0.02	0.17	0.00	0.00	20.9
16	51	-0	-2644	0	0	0	407	--	--	16.08	16.08	0.10	0.01	0.02	0.17	0.00	0.00	20.9
17	51	-0	-2632	0	0	0	352	--	--	16.08	16.08	0.10	0.01	0.02	0.17	0.00	0.00	20.9
18	51	-0	-3996	0	0	0	778	--	--	16.08	16.08	0.00	0.01	0.03	0.25	0.00	0.00	20.9
19	51	-0	-3401	0	0	0	361	--	--	16.08	16.08	0.00	0.01	0.03	0.21	0.00	0.00	20.9
20	51	-0	-3570	0	0	0	371	--	--	16.08	16.08	0.00	0.01	0.03	0.22	0.00	0.00	20.9
37	51	-0	-4130	0	0	0	899	--	--	16.08	16.08	0.00	0.02	0.03	0.26	0.00	0.00	20.9
38	51	-0	-3139	0	0	0	203	--	--	16.08	16.08	0.00	0.00	0.03	0.20	0.00	0.00	20.9
39	51	-0	-3421	0	0	0	221	--	--	16.08	16.08	0.00	0.00	0.03	0.21	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 15 NI 1516 NF 1515 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-2305	0	0	0	1363	--	--	16.08	16.08	0.00	0.02	0.02	0.14	0.00	0.00	20.9
2	0	-0	-1800	0	0	0	1088	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
3	0	-0	-1795	0	0	0	1070	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
4	0	-0	-1752	0	0	0	1027	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
5	0	-0	-1747	0	0	0	1009	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
6	0	-0	-1789	0	0	0	1088	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
7	0	-0	-1773	0	0	0	1028	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
8	0	-0	-1774	0	0	0	1070	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
9	0	-0	-1758	0	0	0	1009	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
10	0	-0	-1800	0	0	0	1088	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
11	0	-0	-1795	0	0	0	1070	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
12	0	-0	-1752	0	0	0	1027	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
13	0	-0	-1747	0	0	0	1009	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
14	0	-0	-1789	0	0	0	1088	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
15	0	-0	-1773	0	0	0	1028	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
16	0	-0	-1774	0	0	0	1070	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
17	0	-0	-1758	0	0	0	1009	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
18	0	-0	-2709	0	0	0	1793	--	--	16.08	16.08	0.00	0.03	0.02	0.17	0.00	0.00	20.9
19	0	-0	-2185	0	0	0	1182	--	--	16.08	16.08	0.00	0.02	0.02	0.14	0.00	0.00	20.9
20	0	-0	-2342	0	0	0	1254	--	--	16.08	16.08	0.00	0.02	0.02	0.15	0.00	0.00	20.9
37	0	-0	-2853	0	0	0	1965	--	--	16.08	16.08	0.00	0.03	0.02	0.18	0.00	0.00	20.9
38	0	-0	-1979	0	0	0	946	--	--	16.08	16.08	0.00	0.02	0.02	0.12	0.00	0.00	20.9
39	0	-0	-2241	0	0	0	1066	--	--	16.08	16.08	0.00	0.02	0.02	0.14	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	-2305	0	0	0	1363	--	--	16.08	16.08	0.00	0.02	0.02	0.14	0.00	0.00	20.9
2	26	-0	-1800	0	0	0	1088	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
3	26	-0	-1795	0	0	0	1070	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
4	26	-0	-1752	0	0	0	1027	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
5	26	-0	-1747	0	0	0	1009	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
6	26	-0	-1789	0	0	0	1088	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
7	26	-0	-1773	0	0	0	1028	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
8	26	-0	-1774	0	0	0	1070	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
9	26	-0	-1758	0	0	0	1009	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
10	26	-0	-1800	0	0	0	1088	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
11	26	-0	-1795	0	0	0	1070	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
12	26	-0	-1752	0	0	0	1027	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
13	26	-0	-1747	0	0	0	1009	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
14	26	-0	-1789	0	0	0	1088	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
15	26	-0	-1773	0	0	0	1028	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
16	26	-0	-1774	0	0	0	1070	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
17	26	-0	-1758	0	0	0	1009	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
18	26	-0	-2709	0	0	0	1793	--	--	16.08	16.08	0.00	0.03	0.02	0.17	0.00	0.00	20.9
19	26	-0	-2185	0	0	0	1182	--	--	16.08	16.08	0.00	0.02	0.02	0.14	0.00	0.00	20.9
20	26	-0	-2342	0	0	0	1254	--	--	16.08	16.08	0.00	0.02	0.02	0.15	0.00	0.00	20.9
37	26	-0	-2853	0	0	0	1965	--	--	16.08	16.08	0.00	0.03	0.02	0.18	0.00	0.00	20.9
38	26	-0	-1979	0	0	0	946	--	--	16.08	16.08	0.00	0.02	0.02	0.12	0.00	0.00	20.9
39	26	-0	-2241	0	0	0	1066	--	--	16.08	16.08	0.00	0.02	0.02	0.14	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	-2305	0	0	0	179	--	--	16.08	16.08	0.00	0.00	0.02	0.14	0.00	0.00	20.9
2	51	-0	-1800	0	0	0	164	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9

3	51	-0	-1795	0	0	0	148	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
4	51	-0	-1752	0	0	0	128	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
5	51	-0	-1747	0	0	0	112	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
6	51	-0	-1789	0	0	0	169	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
7	51	-0	-1773	0	0	0	117	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
8	51	-0	-1774	0	0	0	158	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
9	51	-0	-1758	0	0	0	106	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
10	51	-0	-1800	0	0	0	164	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
11	51	-0	-1795	0	0	0	148	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
12	51	-0	-1752	0	0	0	128	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
13	51	-0	-1747	0	0	0	112	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
14	51	-0	-1789	0	0	0	169	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
15	51	-0	-1773	0	0	0	117	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
16	51	-0	-1774	0	0	0	158	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
17	51	-0	-1758	0	0	0	106	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
18	51	-0	-2709	0	0	0	401	--	--	16.08	16.08	0.00	0.01	0.02	0.17	0.00	0.00	20.9
19	51	-0	-2185	0	0	0	59	--	--	16.08	16.08	0.00	0.00	0.02	0.14	0.00	0.00	20.9
20	51	-0	-2342	0	0	0	51	--	--	16.08	16.08	0.00	0.00	0.02	0.15	0.00	0.00	20.9
37	51	-0	-2853	0	0	0	500	--	--	16.08	16.08	0.00	0.01	0.02	0.18	0.00	0.00	20.9
38	51	-0	-1979	0	0	0	-70	--	--	16.08	16.08	0.18	0.00	0.02	0.12	0.00	0.00	20.9
39	51	-0	-2241	0	0	0	-85	--	--	16.08	16.08	0.18	0.00	0.02	0.14	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 16 NI 1515 NF 1532 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-1285	0	0	0	741	--	--	16.08	16.08	0.00	0.01	0.01	0.08	0.00	0.00	20.9
2	0	-0	-1013	0	0	0	604	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
3	0	-0	-1007	0	0	0	587	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
4	0	-0	-969	0	0	0	552	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
5	0	-0	-963	0	0	0	535	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
6	0	-0	-1005	0	0	0	606	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
7	0	-0	-985	0	0	0	549	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
8	0	-0	-991	0	0	0	591	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
9	0	-0	-972	0	0	0	533	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
10	0	-0	-1013	0	0	0	604	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
11	0	-0	-1007	0	0	0	587	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
12	0	-0	-969	0	0	0	552	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
13	0	-0	-963	0	0	0	535	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
14	0	-0	-1005	0	0	0	606	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
15	0	-0	-985	0	0	0	549	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
16	0	-0	-991	0	0	0	591	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
17	0	-0	-972	0	0	0	533	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
18	0	-0	-1538	0	0	0	1068	--	--	16.08	16.08	0.00	0.02	0.01	0.10	0.00	0.00	20.9
19	0	-0	-1099	0	0	0	565	--	--	16.08	16.08	0.00	0.01	0.01	0.07	0.00	0.00	20.9
20	0	-0	-1234	0	0	0	606	--	--	16.08	16.08	0.00	0.01	0.01	0.08	0.00	0.00	20.9
37	0	-0	-1684	0	0	0	1216	--	--	16.08	16.08	0.00	0.02	0.01	0.11	0.00	0.00	20.9
38	0	-0	-954	0	0	0	378	--	--	16.08	16.08	0.00	0.01	0.01	0.06	0.00	0.00	20.9
39	0	-0	-1179	0	0	0	447	--	--	16.08	16.08	0.00	0.01	0.01	0.07	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	-1285	0	0	0	741	--	--	16.08	16.08	0.00	0.01	0.01	0.08	0.00	0.00	20.9
2	26	-0	-1013	0	0	0	604	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
3	26	-0	-1007	0	0	0	587	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
4	26	-0	-969	0	0	0	552	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
5	26	-0	-963	0	0	0	535	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
6	26	-0	-1005	0	0	0	606	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
7	26	-0	-985	0	0	0	549	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
8	26	-0	-991	0	0	0	591	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
9	26	-0	-972	0	0	0	533	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
10	26	-0	-1013	0	0	0	604	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
11	26	-0	-1007	0	0	0	587	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
12	26	-0	-969	0	0	0	552	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
13	26	-0	-963	0	0	0	535	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
14	26	-0	-1005	0	0	0	606	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
15	26	-0	-985	0	0	0	549	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
16	26	-0	-991	0	0	0	591	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
17	26	-0	-972	0	0	0	533	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
18	26	-0	-1538	0	0	0	1068	--	--	16.08	16.08	0.00	0.02	0.01	0.10	0.00	0.00	20.9
19	26	-0	-1099	0	0	0	565	--	--	16.08	16.08	0.00	0.01	0.01	0.07	0.00	0.00	20.9
20	26	-0	-1234	0	0	0	606	--	--	16.08	16.08	0.00	0.01	0.01	0.08	0.00	0.00	20.9
37	26	-0	-1684	0	0	0	1216	--	--	16.08	16.08	0.00	0.02	0.01	0.11	0.00	0.00	20.9
38	26	-0	-954	0	0	0	378	--	--	16.08	16.08	0.00	0.01	0.01	0.06	0.00	0.00	20.9
39	26	-0	-1179	0	0	0	447	--	--	16.08	16.08	0.00	0.01	0.01	0.07	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	-1285	0	0	0	81	--	--	16.08	16.08	0.00	0.00	0.01	0.08	0.00	0.00	20.9
2	51	-0	-1013	0	0	0	84	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
3	51	-0	-1007	0	0	0	70	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
4	51	-0	-969	0	0	0	55	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
5	51	-0	-963	0	0	0	40	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
6	51	-0	-1005	0	0	0	90	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
7	51	-0	-985	0	0	0	43	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
8	51	-0	-991	0	0	0	82	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
9	51	-0	-972	0	0	0	34	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
10	51	-0	-1013	0	0	0	84	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
11	51	-0	-1007	0	0	0	70	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
12	51	-0	-969	0	0	0	55	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
13	51	-0	-963	0	0	0	40	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
14	51	-0	-1005	0	0	0	90	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
15	51	-0	-985	0	0	0	43	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
16	51	-0	-991	0	0	0	82	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
17	51	-0	-972	0	0	0	34	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
18	51	-0	-1538	0	0	0	278	--	--	16.08	16.08	0.00	0.00	0.01	0.10	0.00	0.00	20.9
19	51	-0	-1099	0	0	0	0	--	--	16.08	16.08	0.00	0.00	0.01	0.07	0.00	0.00	20.9
20	51	-0	-1234	0	0	0	-28	--	--	16.08	16.08	0.18	0.00	0.01	0.08	0.00	0.00	20.9
37	51	-0	-1684	0	0	0	351	--	--	16.08	16.08	0.00	0.01	0.01	0.11	0.00	0.00	20.9
38	51	-0	-954	0	0	0	-112	--	--	16.08	16.08	0.18	0.00	0.01	0.06	0.00	0.00	20.9
39	51	-0	-1179	0	0	0	-159	--	--	16.08	16.08	0.18	0.00	0.01	0.07	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 17 NI 1532 NF 1531 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-308	0	0	0	337	--	--	16.08	16.08	0.00	0.01	0.00	0.02	0.00	0.00	20.9
2	0	-0	-261	0	0	0	289	--	--	16.08	16.08	0.10	0.01	0.00	0.02	0.00	0.00	20.9
3	0	-0	-254	0	0	0	272	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
4	0	-0	-220	0	0	0	245	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
5	0	-0	-213	0	0	0	229	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
6	0	-0	-255	0	0	0	293	--	--	16.08	16.08	0.10	0.01	0.00	0.02	0.00	0.00	20.9
7	0	-0	-232	0	0	0	238	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
8	0	-0	-242	0	0	0	280	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
9	0	-0	-220	0	0	0	225	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
10	0	-0	-261	0	0	0	289	--	--	16.08	16.08	0.10	0.01	0.00	0.02	0.00	0.00	20.9
11	0	-0	-254	0	0	0	272	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
12	0	-0	-220	0	0	0	245	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
13	0	-0	-213	0	0	0	229	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
14	0	-0	-255	0	0	0	293	--	--	16.08	16.08	0.10	0.01	0.00	0.02	0.00	0.00	20.9
15	0	-0	-232	0	0	0	238	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
16	0	-0	-242	0	0	0	280	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
17	0	-0	-220	0	0	0	225	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
18	0	-0	-417	0	0	0	593	--	--	16.08	16.08	0.00	0.01	0.00	0.03	0.00	0.00	20.9
19	0	-0	-58	0	0	0	182	--	--	16.08	16.08	0.00	0.00	0.00	0.00	0.00	0.00	20.9
20	0	-0	-175	0	0	0	196	--	--	16.08	16.08	0.00	0.00	0.00	0.01	0.00	0.00	20.9
37	0	-0	-568	0	0	0	717	--	--	16.08	16.08	0.00	0.01	0.00	0.04	0.00	0.00	20.9
38	0	-0	31	0	0	0	30	--	--	16.08	16.08	0.00	0.00	0.00	0.00	0.00	0.00	20.9
39	0	-0	-165	0	0	0	55	--	--	16.08	16.08	0.00	0.00	0.00	0.01	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	26	-0	-308	0	0	0	337	--	--	16.08	16.08	0.00	0.01	0.00	0.02	0.00	0.00	20.9
2	26	-0	-261	0	0	0	289	--	--	16.08	16.08	0.10	0.01	0.00	0.02	0.00	0.00	20.9
3	26	-0	-254	0	0	0	272	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
4	26	-0	-220	0	0	0	245	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
5	26	-0	-213	0	0	0	229	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
6	26	-0	-255	0	0	0	293	--	--	16.08	16.08	0.10	0.01	0.00	0.02	0.00	0.00	20.9
7	26	-0	-232	0	0	0	238	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
8	26	-0	-242	0	0	0	280	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
9	26	-0	-220	0	0	0	225	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
10	26	-0	-261	0	0	0	289	--	--	16.08	16.08	0.10	0.01	0.00	0.02	0.00	0.00	20.9
11	26	-0	-254	0	0	0	272	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
12	26	-0	-220	0	0	0	245	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
13	26	-0	-213	0	0	0	229	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
14	26	-0	-255	0	0	0	293	--	--	16.08	16.08	0.10	0.01	0.00	0.02	0.00	0.00	20.9
15	26	-0	-232	0	0	0	238	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
16	26	-0	-242	0	0	0	280	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
17	26	-0	-220	0	0	0	225	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
18	26	-0	-417	0	0	0	593	--	--	16.08	16.08	0.00	0.01	0.00	0.03	0.00	0.00	20.9
19	26	-0	-58	0	0	0	182	--	--	16.08	16.08	0.00	0.00	0.00	0.00	0.00	0.00	20.9
20	26	-0	-175	0	0	0	196	--	--	16.08	16.08	0.00	0.00	0.00	0.01	0.00	0.00	20.9
37	26	-0	-568	0	0	0	717	--	--	16.08	16.08	0.00	0.01	0.00	0.04	0.00	0.00	20.9
38	26	-0	31	0	0	0	71	--	--	16.08	16.08	0.00	0.00	0.00	0.00	0.00	0.00	20.9
39	26	-0	-165	0	0	0	55	--	--	16.08	16.08	0.00	0.00	0.00	0.01	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	51	-0	-308	0	0	0	178	--	--	16.08	16.08	0.00	0.00	0.00	0.02	0.00	0.00	20.9
2	51	-0	-261	0	0	0	155	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
3	51	-0	-254	0	0	0	142	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
4	51	-0	-220	0	0	0	132	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
5	51	-0	-213	0	0	0	119	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
6	51	-0	-255	0	0	0	162	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
7	51	-0	-232	0	0	0	119	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
8	51	-0	-242	0	0	0	155	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
9	51	-0	-220	0	0	0	112	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
10	51	-0	-261	0	0	0	155	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
11	51	-0	-254	0	0	0	142	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
12	51	-0	-220	0	0	0	132	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
13	51	-0	-213	0	0	0	119	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
14	51	-0	-255	0	0	0	162	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
15	51	-0	-232	0	0	0	119	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
16	51	-0	-242	0	0	0	155	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
17	51	-0	-220	0	0	0	112	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
18	51	-0	-417	0	0	0	379	--	--	16.08	16.08	0.00	0.01	0.00	0.03	0.00	0.00	20.9
19	51	-0	-58	0	0	0	152	--	--	16.08	16.08	0.00	0.00	0.00	0.00	0.00	0.00	20.9
20	51	-0	-175	0	0	0	106	--	--	16.08	16.08	0.00	0.00	0.00	0.01	0.00	0.00	20.9
37	51	-0	-568	0	0	0	424	--	--	16.08	16.08	0.00	0.01	0.00	0.04	0.00	0.00	20.9
38	51	-0	31	0	0	0	46	--	--	16.08	16.08	0.00	0.00	0.00	0.00	0.00	0.00	20.9
39	51	-0	-165	0	0	0	-30	--	--	16.08	16.08	0.18	0.00	0.00	0.01	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 18 NI 1531 NF 1502 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	685	0	0	0	122	--	--	16.08	16.08	0.00	0.00	0.01	0.04	0.00	0.00	20.9
2	0	-0	504	0	0	0	120	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
3	0	-0	512	0	0	0	104	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
4	0	-0	542	0	0	0	84	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
5	0	-0	550	0	0	0	68	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
6	0	-0	508	0	0	0	125	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
7	0	-0	534	0	0	0	74	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
8	0	-0	520	0	0	0	114	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
9	0	-0	546	0	0	0	63	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
10	0	-0	504	0	0	0	120	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9

11	0	-0	512	0	0	0	104	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
12	0	-0	542	0	0	0	84	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
13	0	-0	550	0	0	0	68	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
14	0	-0	508	0	0	0	125	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
15	0	-0	534	0	0	0	74	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
16	0	-0	520	0	0	0	114	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
17	0	-0	546	0	0	0	63	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
18	0	-0	720	0	0	0	337	--	--	16.08	16.08	0.00	0.01	0.01	0.05	0.00	0.00	20.9
19	0	-0	1008	0	0	0	-0	--	--	16.08	16.08	0.18	0.00	0.01	0.06	0.00	0.00	20.9
20	0	-0	903	0	0	0	-8	--	--	16.08	16.08	0.18	0.00	0.01	0.06	0.00	0.00	20.9
37	0	-0	561	0	0	0	435	--	--	16.08	16.08	0.00	0.01	0.00	0.04	0.00	0.00	20.9
38	0	-0	1041	0	0	0	-127	--	--	16.08	16.08	0.18	0.00	0.01	0.07	0.00	0.00	20.9
39	0	-0	866	0	0	0	-139	--	--	16.08	16.08	0.18	0.00	0.01	0.05	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	685	0	0	0	1031	--	--	16.08	16.08	0.00	0.02	0.01	0.04	0.00	0.00	20.9
2	26	-0	504	0	0	0	788	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
3	26	-0	512	0	0	0	783	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
4	26	-0	542	0	0	0	802	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
5	26	-0	550	0	0	0	797	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
6	26	-0	508	0	0	0	799	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
7	26	-0	534	0	0	0	782	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
8	26	-0	520	0	0	0	803	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
9	26	-0	546	0	0	0	786	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
10	26	-0	504	0	0	0	788	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
11	26	-0	512	0	0	0	783	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
12	26	-0	542	0	0	0	802	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
13	26	-0	550	0	0	0	797	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
14	26	-0	508	0	0	0	799	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
15	26	-0	534	0	0	0	782	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
16	26	-0	520	0	0	0	803	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
17	26	-0	546	0	0	0	786	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
18	26	-0	720	0	0	0	1292	--	--	16.08	16.08	0.00	0.02	0.01	0.05	0.00	0.00	20.9
19	26	-0	1008	0	0	0	1336	--	--	16.08	16.08	0.00	0.02	0.01	0.06	0.00	0.00	20.9
20	26	-0	903	0	0	0	1190	--	--	16.08	16.08	0.00	0.02	0.01	0.06	0.00	0.00	20.9
37	26	-0	561	0	0	0	1179	--	--	16.08	16.08	0.00	0.02	0.00	0.04	0.00	0.00	20.9
38	26	-0	1041	0	0	0	1253	--	--	16.08	16.08	0.00	0.02	0.01	0.07	0.00	0.00	20.9
39	26	-0	866	0	0	0	1008	--	--	16.08	16.08	0.00	0.02	0.01	0.05	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	685	0	0	0	474	--	--	16.08	16.08	0.00	0.01	0.01	0.04	0.00	0.00	20.9
2	51	-0	504	0	0	0	379	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
3	51	-0	512	0	0	0	367	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
4	51	-0	542	0	0	0	362	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
5	51	-0	550	0	0	0	351	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
6	51	-0	508	0	0	0	386	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
7	51	-0	534	0	0	0	348	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
8	51	-0	520	0	0	0	381	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
9	51	-0	546	0	0	0	343	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
10	51	-0	504	0	0	0	379	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
11	51	-0	512	0	0	0	367	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
12	51	-0	542	0	0	0	362	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
13	51	-0	550	0	0	0	351	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
14	51	-0	508	0	0	0	386	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
15	51	-0	534	0	0	0	348	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
16	51	-0	520	0	0	0	381	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
17	51	-0	546	0	0	0	343	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
18	51	-0	720	0	0	0	707	--	--	16.08	16.08	0.00	0.01	0.01	0.05	0.00	0.00	20.9
19	51	-0	1008	0	0	0	518	--	--	16.08	16.08	0.00	0.01	0.01	0.06	0.00	0.00	20.9
20	51	-0	903	0	0	0	456	--	--	16.08	16.08	0.00	0.01	0.01	0.06	0.00	0.00	20.9
37	51	-0	561	0	0	0	724	--	--	16.08	16.08	0.00	0.01	0.00	0.04	0.00	0.00	20.9
38	51	-0	1041	0	0	0	408	--	--	16.08	16.08	0.00	0.01	0.01	0.07	0.00	0.00	20.9
39	51	-0	866	0	0	0	305	--	--	16.08	16.08	0.00	0.01	0.01	0.05	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 19 NI 1502 NF 1519 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	1754	0	0	0	100	--	--	16.08	16.08	0.00	0.00	0.01	0.11	0.00	0.00	20.9
2	0	-0	1327	0	0	0	99	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
3	0	-0	1336	0	0	0	85	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
4	0	-0	1363	0	0	0	70	--	--	16.08	16.08	0.10	0.00	0.01	0.09	0.00	0.00	20.9
5	0	-0	1372	0	0	0	56	--	--	16.08	16.08	0.10	0.00	0.01	0.09	0.00	0.00	20.9
6	0	-0	1330	0	0	0	105	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
7	0	-0	1359	0	0	0	58	--	--	16.08	16.08	0.10	0.00	0.01	0.09	0.00	0.00	20.9
8	0	-0	1340	0	0	0	96	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
9	0	-0	1369	0	0	0	49	--	--	16.08	16.08	0.10	0.00	0.01	0.09	0.00	0.00	20.9
10	0	-0	1327	0	0	0	99	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
11	0	-0	1336	0	0	0	85	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
12	0	-0	1363	0	0	0	70	--	--	16.08	16.08	0.10	0.00	0.01	0.09	0.00	0.00	20.9
13	0	-0	1372	0	0	0	56	--	--	16.08	16.08	0.10	0.00	0.01	0.09	0.00	0.00	20.9
14	0	-0	1330	0	0	0	105	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
15	0	-0	1359	0	0	0	58	--	--	16.08	16.08	0.10	0.00	0.01	0.09	0.00	0.00	20.9
16	0	-0	1340	0	0	0	96	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
17	0	-0	1369	0	0	0	49	--	--	16.08	16.08	0.10	0.00	0.01	0.09	0.00	0.00	20.9
18	0	-0	1946	0	0	0	303	--	--	16.08	16.08	0.00	0.01	0.02	0.12	0.00	0.00	20.9
19	0	-0	2161	0	0	0	24	--	--	16.08	16.08	0.00	0.00	0.02	0.14	0.00	0.00	20.9
20	0	-0	2067	0	0	0	-2	--	--	16.08	16.08	0.18	0.00	0.02	0.13	0.00	0.00	20.9
37	0	-0	1775	0	0	0	375	--	--	16.08	16.08	0.00	0.01	0.01	0.11	0.00	0.00	20.9
38	0	-0	2134	0	0	0	-91	--	--	16.08	16.08	0.18	0.00	0.02	0.13	0.00	0.00	20.9
39	0	-0	1976	0	0	0	-134	--	--	16.08	16.08	0.18	0.00	0.02	0.12	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	1754	0	0	0	2425	--	--	16.08	16.08	0.00	0.04	0.01	0.11	0.00	0.00	20.9
2	26	-0	1327	0	0	0	1858	--	--	16.08	16.08	0.10	0.03	0.01	0.08	0.00	0.00	20.9
3	26	-0	1336	0	0	0	1856	--	--	16.08	16.08	0.10	0.03	0.01	0.08	0.00	0.00	20.9
4	26	-0	1363	0	0	0	1876	--	--	16.08	16.08	0.10	0.03	0.01	0.09	0.00	0.00	20.9
5	26	-0	1372	0	0	0	1874	--	--	16.08	16.08	0.10	0.03	0.01	0.09	0.00	0.00	20.9
6	26	-0	1330	0	0	0	1868	--	--	16.08	16.08	0.10	0.03	0.01	0.08	0.00	0.00	20.9

7	26	-0	1359	0	0	0	1859	--	--	16.08	16.08	0.10	0.03	0.01	0.09	0.00	0.00	20.9
8	26	-0	1340	0	0	0	1873	--	--	16.08	16.08	0.10	0.03	0.01	0.08	0.00	0.00	20.9
9	26	-0	1369	0	0	0	1864	--	--	16.08	16.08	0.10	0.03	0.01	0.09	0.00	0.00	20.9
10	26	-0	1327	0	0	0	1858	--	--	16.08	16.08	0.10	0.03	0.01	0.08	0.00	0.00	20.9
11	26	-0	1336	0	0	0	1856	--	--	16.08	16.08	0.10	0.03	0.01	0.08	0.00	0.00	20.9
12	26	-0	1363	0	0	0	1876	--	--	16.08	16.08	0.10	0.03	0.01	0.09	0.00	0.00	20.9
13	26	-0	1372	0	0	0	1874	--	--	16.08	16.08	0.10	0.03	0.01	0.09	0.00	0.00	20.9
14	26	-0	1330	0	0	0	1868	--	--	16.08	16.08	0.10	0.03	0.01	0.08	0.00	0.00	20.9
15	26	-0	1359	0	0	0	1859	--	--	16.08	16.08	0.10	0.03	0.01	0.09	0.00	0.00	20.9
16	26	-0	1340	0	0	0	1873	--	--	16.08	16.08	0.10	0.03	0.01	0.08	0.00	0.00	20.9
17	26	-0	1369	0	0	0	1864	--	--	16.08	16.08	0.10	0.03	0.01	0.09	0.00	0.00	20.9
18	26	-0	1946	0	0	0	2883	--	--	16.08	16.08	0.00	0.05	0.02	0.12	0.00	0.00	20.9
19	26	-0	2161	0	0	0	2888	--	--	16.08	16.08	0.00	0.05	0.02	0.14	0.00	0.00	20.9
20	26	-0	2067	0	0	0	2738	--	--	16.08	16.08	0.00	0.05	0.02	0.13	0.00	0.00	20.9
37	26	-0	1775	0	0	0	2728	--	--	16.08	16.08	0.00	0.05	0.01	0.11	0.00	0.00	20.9
38	26	-0	2134	0	0	0	2738	--	--	16.08	16.08	0.00	0.05	0.02	0.13	0.00	0.00	20.9
39	26	-0	1976	0	0	0	2486	--	--	16.08	16.08	0.00	0.04	0.02	0.12	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	1754	0	0	0	1001	--	--	16.08	16.08	0.00	0.02	0.01	0.11	0.00	0.00	20.9
2	51	-0	1327	0	0	0	781	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
3	51	-0	1336	0	0	0	771	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
4	51	-0	1363	0	0	0	770	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
5	51	-0	1372	0	0	0	760	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
6	51	-0	1330	0	0	0	788	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
7	51	-0	1359	0	0	0	756	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
8	51	-0	1340	0	0	0	785	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
9	51	-0	1369	0	0	0	753	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
10	51	-0	1327	0	0	0	781	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
11	51	-0	1336	0	0	0	771	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
12	51	-0	1363	0	0	0	770	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
13	51	-0	1372	0	0	0	760	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
14	51	-0	1330	0	0	0	788	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
15	51	-0	1359	0	0	0	756	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
16	51	-0	1340	0	0	0	785	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
17	51	-0	1369	0	0	0	753	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
18	51	-0	1946	0	0	0	1303	--	--	16.08	16.08	0.00	0.02	0.02	0.12	0.00	0.00	20.9
19	51	-0	2161	0	0	0	1134	--	--	16.08	16.08	0.00	0.02	0.02	0.14	0.00	0.00	20.9
20	51	-0	2067	0	0	0	1059	--	--	16.08	16.08	0.00	0.02	0.02	0.13	0.00	0.00	20.9
37	51	-0	1775	0	0	0	1287	--	--	16.08	16.08	0.00	0.02	0.01	0.11	0.00	0.00	20.9
38	51	-0	2134	0	0	0	1005	--	--	16.08	16.08	0.00	0.02	0.02	0.13	0.00	0.00	20.9
39	51	-0	1976	0	0	0	881	--	--	16.08	16.08	0.00	0.02	0.02	0.12	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 20 NI 1519 NF 1518 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm

1	0	-0	2950	0	0	0	300	--	--	16.08	16.08	0.00	0.01	0.02	0.19	0.00	0.00	20.9
2	0	-0	2249	0	0	0	249	--	--	16.08	16.08	0.10	0.00	0.02	0.14	0.00	0.00	20.9
3	0	-0	2259	0	0	0	236	--	--	16.08	16.08	0.10	0.00	0.02	0.14	0.00	0.00	20.9
4	0	-0	2280	0	0	0	225	--	--	16.08	16.08	0.10	0.00	0.02	0.14	0.00	0.00	20.9
5	0	-0	2290	0	0	0	213	--	--	16.08	16.08	0.10	0.00	0.02	0.14	0.00	0.00	20.9
6	0	-0	2248	0	0	0	255	--	--	16.08	16.08	0.10	0.00	0.02	0.14	0.00	0.00	20.9
7	0	-0	2281	0	0	0	213	--	--	16.08	16.08	0.10	0.00	0.02	0.14	0.00	0.00	20.9
8	0	-0	2258	0	0	0	248	--	--	16.08	16.08	0.10	0.00	0.02	0.14	0.00	0.00	20.9
9	0	-0	2291	0	0	0	206	--	--	16.08	16.08	0.10	0.00	0.02	0.14	0.00	0.00	20.9
10	0	-0	2249	0	0	0	249	--	--	16.08	16.08	0.10	0.00	0.02	0.14	0.00	0.00	20.9
11	0	-0	2259	0	0	0	236	--	--	16.08	16.08	0.10	0.00	0.02	0.14	0.00	0.00	20.9
12	0	-0	2280	0	0	0	225	--	--	16.08	16.08	0.10	0.00	0.02	0.14	0.00	0.00	20.9
13	0	-0	2290	0	0	0	213	--	--	16.08	16.08	0.10	0.00	0.02	0.14	0.00	0.00	20.9
14	0	-0	2248	0	0	0	255	--	--	16.08	16.08	0.10	0.00	0.02	0.14	0.00	0.00	20.9
15	0	-0	2281	0	0	0	213	--	--	16.08	16.08	0.10	0.00	0.02	0.14	0.00	0.00	20.9
16	0	-0	2258	0	0	0	248	--	--	16.08	16.08	0.10	0.00	0.02	0.14	0.00	0.00	20.9
17	0	-0	2291	0	0	0	206	--	--	16.08	16.08	0.10	0.00	0.02	0.14	0.00	0.00	20.9
18	0	-0	3338	0	0	0	530	--	--	16.08	16.08	0.00	0.01	0.03	0.21	0.00	0.00	20.9
19	0	-0	3445	0	0	0	283	--	--	16.08	16.08	0.00	0.00	0.03	0.22	0.00	0.00	20.9
20	0	-0	3374	0	0	0	246	--	--	16.08	16.08	0.00	0.00	0.03	0.21	0.00	0.00	20.9
37	0	-0	3161	0	0	0	576	--	--	16.08	16.08	0.00	0.01	0.03	0.20	0.00	0.00	20.9
38	0	-0	3338	0	0	0	165	--	--	16.08	16.08	0.00	0.00	0.03	0.21	0.00	0.00	20.9
39	0	-0	3221	0	0	0	103	--	--	16.08	16.08	0.00	0.00	0.03	0.20	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	2950	0	0	0	4210	--	--	16.08	16.08	0.00	0.07	0.02	0.19	0.00	0.00	20.9
2	26	-0	2249	0	0	0	3230	--	--	16.08	16.08	0.10	0.06	0.02	0.14	0.00	0.00	20.9
3	26	-0	2259	0	0	0	3230	--	--	16.08	16.08	0.10	0.06	0.02	0.14	0.00	0.00	20.9
4	26	-0	2280	0	0	0	3247	--	--	16.08	16.08	0.10	0.06	0.02	0.14	0.00	0.00	20.9
5	26	-0	2290	0	0	0	3248	--	--	16.08	16.08	0.10	0.06	0.02	0.14	0.00	0.00	20.9
6	26	-0	2248	0	0	0	3235	--	--	16.08	16.08	0.10	0.06	0.02	0.14	0.00	0.00	20.9
7	26	-0	2281	0	0	0	3237	--	--	16.08	16.08	0.10	0.06	0.02	0.14	0.00	0.00	20.9
8	26	-0	2258	0	0	0	3241	--	--	16.08	16.08	0.10	0.06	0.02	0.14	0.00	0.00	20.9
9	26	-0	2291	0	0	0	3243	--	--	16.08	16.08	0.10	0.06	0.02	0.14	0.00	0.00	20.9
10	26	-0	2249	0	0	0	3230	--	--	16.08	16.08	0.10	0.06	0.02	0.14	0.00	0.00	20.9
11	26	-0	2259	0	0	0	3230	--	--	16.08	16.08	0.10	0.06	0.02	0.14	0.00	0.00	20.9
12	26	-0	2280	0	0	0	3247	--	--	16.08	16.08	0.10	0.06	0.02	0.14	0.00	0.00	20.9
13	26	-0	2290	0	0	0	3248	--	--	16.08	16.08	0.10	0.06	0.02	0.14	0.00	0.00	20.9
14	26	-0	2248	0	0	0	3235	--	--	16.08	16.08	0.10	0.06	0.02	0.14	0.00	0.00	20.9
15	26	-0	2281	0	0	0	3237	--	--	16.08	16.08	0.10	0.06	0.02	0.14	0.00	0.00	20.9
16	26	-0	2258	0	0	0	3241	--	--	16.08	16.08	0.10	0.06	0.02	0.14	0.00	0.00	20.9
17	26	-0	2291	0	0	0	3243	--	--	16.08	16.08	0.10	0.06	0.02	0.14	0.00	0.00	20.9
18	26	-0	3338	0	0	0	4954	--	--	16.08	16.08	0.00	0.08	0.03	0.21	0.00	0.00	20.9
19	26	-0	3445	0	0	0	4849	--	--	16.08	16.08	0.00	0.08	0.03	0.22	0.00	0.00	20.9
20	26	-0	3374	0	0	0	4719	--	--	16.08	16.08	0.00	0.08	0.03	0.21	0.00	0.00	20.9
37	26	-0	3161	0	0	0	4766	--	--	16.08	16.08	0.00	0.08	0.03	0.20	0.00	0.00	20.9
38	26	-0	3338	0	0	0	4589	--	--	16.08	16.08	0.00	0.08	0.03	0.21	0.00	0.00	20.9
39	26	-0	3221	0	0	0	4373	--	--	16.08	16.08	0.00	0.07	0.03	0.20	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	2950	0	0	0	1815	--	--	16.08	16.08	0.00	0.03	0.02	0.19	0.00	0.00	20.9
2	51	-0	2249	0	0	0	1404	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9

3	51	-0	2259	0	0	0	1396	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
4	51	-0	2280	0	0	0	1396	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
5	51	-0	2290	0	0	0	1389	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
6	51	-0	2248	0	0	0	1410	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
7	51	-0	2281	0	0	0	1385	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
8	51	-0	2258	0	0	0	1408	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
9	51	-0	2291	0	0	0	1383	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
10	51	-0	2249	0	0	0	1404	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
11	51	-0	2259	0	0	0	1396	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
12	51	-0	2280	0	0	0	1396	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
13	51	-0	2290	0	0	0	1389	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
14	51	-0	2248	0	0	0	1410	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
15	51	-0	2281	0	0	0	1385	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
16	51	-0	2258	0	0	0	1408	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
17	51	-0	2291	0	0	0	1383	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
18	51	-0	3338	0	0	0	2244	--	--	16.08	16.08	0.00	0.04	0.03	0.21	0.00	0.00	20.9
19	51	-0	3445	0	0	0	2052	--	--	16.08	16.08	0.00	0.03	0.03	0.22	0.00	0.00	20.9
20	51	-0	3374	0	0	0	1979	--	--	16.08	16.08	0.00	0.03	0.03	0.21	0.00	0.00	20.9
37	51	-0	3161	0	0	0	2199	--	--	16.08	16.08	0.00	0.04	0.03	0.20	0.00	0.00	20.9
38	51	-0	3338	0	0	0	1879	--	--	16.08	16.08	0.00	0.03	0.03	0.21	0.00	0.00	20.9
39	51	-0	3221	0	0	0	1758	--	--	16.08	16.08	0.00	0.03	0.03	0.20	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 21 NI 1518 NF 1533 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	3745	0	0	0	676	--	--	16.08	16.08	0.00	0.01	0.03	0.23	0.00	0.00	20.9
2	0	-0	2864	0	0	0	535	--	--	16.08	16.08	0.10	0.01	0.02	0.18	0.00	0.00	20.9
3	0	-0	2875	0	0	0	524	--	--	16.08	16.08	0.10	0.01	0.02	0.18	0.00	0.00	20.9
4	0	-0	2888	0	0	0	516	--	--	16.08	16.08	0.10	0.01	0.02	0.18	0.00	0.00	20.9
5	0	-0	2898	0	0	0	505	--	--	16.08	16.08	0.10	0.01	0.02	0.18	0.00	0.00	20.9
6	0	-0	2861	0	0	0	541	--	--	16.08	16.08	0.10	0.01	0.02	0.18	0.00	0.00	20.9
7	0	-0	2894	0	0	0	505	--	--	16.08	16.08	0.10	0.01	0.02	0.18	0.00	0.00	20.9
8	0	-0	2868	0	0	0	536	--	--	16.08	16.08	0.10	0.01	0.02	0.18	0.00	0.00	20.9
9	0	-0	2901	0	0	0	499	--	--	16.08	16.08	0.10	0.01	0.02	0.18	0.00	0.00	20.9
10	0	-0	2864	0	0	0	535	--	--	16.08	16.08	0.10	0.01	0.02	0.18	0.00	0.00	20.9
11	0	-0	2875	0	0	0	524	--	--	16.08	16.08	0.10	0.01	0.02	0.18	0.00	0.00	20.9
12	0	-0	2888	0	0	0	516	--	--	16.08	16.08	0.10	0.01	0.02	0.18	0.00	0.00	20.9
13	0	-0	2898	0	0	0	505	--	--	16.08	16.08	0.10	0.01	0.02	0.18	0.00	0.00	20.9
14	0	-0	2861	0	0	0	541	--	--	16.08	16.08	0.10	0.01	0.02	0.18	0.00	0.00	20.9
15	0	-0	2894	0	0	0	505	--	--	16.08	16.08	0.10	0.01	0.02	0.18	0.00	0.00	20.9
16	0	-0	2868	0	0	0	536	--	--	16.08	16.08	0.10	0.01	0.02	0.18	0.00	0.00	20.9
17	0	-0	2901	0	0	0	499	--	--	16.08	16.08	0.10	0.01	0.02	0.18	0.00	0.00	20.9
18	0	-0	4309	0	0	0	970	--	--	16.08	16.08	0.00	0.02	0.04	0.27	0.00	0.00	20.9
19	0	-0	4241	0	0	0	724	--	--	16.08	16.08	0.00	0.01	0.03	0.27	0.00	0.00	20.9
20	0	-0	4234	0	0	0	687	--	--	16.08	16.08	0.00	0.01	0.03	0.27	0.00	0.00	20.9
37	0	-0	4163	0	0	0	995	--	--	16.08	16.08	0.00	0.02	0.03	0.26	0.00	0.00	20.9
38	0	-0	4050	0	0	0	585	--	--	16.08	16.08	0.00	0.01	0.03	0.25	0.00	0.00	20.9
39	0	-0	4037	0	0	0	524	--	--	16.08	16.08	0.00	0.01	0.03	0.25	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	3745	0	0	0	5641	--	--	16.08	16.08	0.00	0.10	0.03	0.23	0.00	0.00	20.9
2	26	-0	2864	0	0	0	4332	--	--	16.08	16.08	0.10	0.08	0.02	0.18	0.00	0.00	20.9
3	26	-0	2875	0	0	0	4335	--	--	16.08	16.08	0.10	0.08	0.02	0.18	0.00	0.00	20.9
4	26	-0	2888	0	0	0	4344	--	--	16.08	16.08	0.10	0.08	0.02	0.18	0.00	0.00	20.9
5	26	-0	2898	0	0	0	4347	--	--	16.08	16.08	0.10	0.08	0.02	0.18	0.00	0.00	20.9
6	26	-0	2861	0	0	0	4334	--	--	16.08	16.08	0.10	0.08	0.02	0.18	0.00	0.00	20.9
7	26	-0	2894	0	0	0	4341	--	--	16.08	16.08	0.10	0.08	0.02	0.18	0.00	0.00	20.9
8	26	-0	2868	0	0	0	4337	--	--	16.08	16.08	0.10	0.08	0.02	0.18	0.00	0.00	20.9
9	26	-0	2901	0	0	0	4344	--	--	16.08	16.08	0.10	0.08	0.02	0.18	0.00	0.00	20.9
10	26	-0	2864	0	0	0	4332	--	--	16.08	16.08	0.10	0.08	0.02	0.18	0.00	0.00	20.9
11	26	-0	2875	0	0	0	4335	--	--	16.08	16.08	0.10	0.08	0.02	0.18	0.00	0.00	20.9
12	26	-0	2888	0	0	0	4344	--	--	16.08	16.08	0.10	0.08	0.02	0.18	0.00	0.00	20.9
13	26	-0	2898	0	0	0	4347	--	--	16.08	16.08	0.10	0.08	0.02	0.18	0.00	0.00	20.9
14	26	-0	2861	0	0	0	4334	--	--	16.08	16.08	0.10	0.08	0.02	0.18	0.00	0.00	20.9
15	26	-0	2894	0	0	0	4341	--	--	16.08	16.08	0.10	0.08	0.02	0.18	0.00	0.00	20.9
16	26	-0	2868	0	0	0	4337	--	--	16.08	16.08	0.10	0.08	0.02	0.18	0.00	0.00	20.9
17	26	-0	2901	0	0	0	4344	--	--	16.08	16.08	0.10	0.08	0.02	0.18	0.00	0.00	20.9
18	26	-0	4309	0	0	0	6682	--	--	16.08	16.08	0.00	0.11	0.04	0.27	0.00	0.00	20.9
19	26	-0	4241	0	0	0	6346	--	--	16.08	16.08	0.00	0.11	0.03	0.27	0.00	0.00	20.9
20	26	-0	4234	0	0	0	6300	--	--	16.08	16.08	0.00	0.11	0.03	0.27	0.00	0.00	20.9
37	26	-0	4163	0	0	0	6514	--	--	16.08	16.08	0.00	0.11	0.03	0.26	0.00	0.00	20.9
38	26	-0	4050	0	0	0	5953	--	--	16.08	16.08	0.00	0.10	0.03	0.25	0.00	0.00	20.9
39	26	-0	4037	0	0	0	5875	--	--	16.08	16.08	0.00	0.10	0.03	0.25	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	3745	0	0	0	2600	--	--	16.08	16.08	0.00	0.04	0.03	0.23	0.00	0.00	20.9
2	51	-0	2864	0	0	0	2007	--	--	16.08	16.08	0.10	0.04	0.02	0.18	0.00	0.00	20.9
3	51	-0	2875	0	0	0	2001	--	--	16.08	16.08	0.10	0.04	0.02	0.18	0.00	0.00	20.9
4	51	-0	2888	0	0	0	1999	--	--	16.08	16.08	0.10	0.04	0.02	0.18	0.00	0.00	20.9
5	51	-0	2898	0	0	0	1994	--	--	16.08	16.08	0.10	0.04	0.02	0.18	0.00	0.00	20.9
6	51	-0	2861	0	0	0	2011	--	--	16.08	16.08	0.10	0.04	0.02	0.18	0.00	0.00	20.9
7	51	-0	2894	0	0	0	1992	--	--	16.08	16.08	0.10	0.04	0.02	0.18	0.00	0.00	20.9
8	51	-0	2868	0	0	0	2009	--	--	16.08	16.08	0.10	0.04	0.02	0.18	0.00	0.00	20.9
9	51	-0	2901	0	0	0	1989	--	--	16.08	16.08	0.10	0.04	0.02	0.18	0.00	0.00	20.9
10	51	-0	2864	0	0	0	2007	--	--	16.08	16.08	0.10	0.04	0.02	0.18	0.00	0.00	20.9
11	51	-0	2875	0	0	0	2001	--	--	16.08	16.08	0.10	0.04	0.02	0.18	0.00	0.00	20.9
12	51	-0	2888	0	0	0	1999	--	--	16.08	16.08	0.10	0.04	0.02	0.18	0.00	0.00	20.9
13	51	-0	2898	0	0	0	1994	--	--	16.08	16.08	0.10	0.04	0.02	0.18	0.00	0.00	20.9
14	51	-0	2861	0	0	0	2011	--	--	16.08	16.08	0.10	0.04	0.02	0.18	0.00	0.00	20.9
15	51	-0	2894	0	0	0	1992	--	--	16.08	16.08	0.10	0.04	0.02	0.18	0.00	0.00	20.9
16	51	-0	2868	0	0	0	2009	--	--	16.08	16.08	0.10	0.04	0.02	0.18	0.00	0.00	20.9
17	51	-0	2901	0	0	0	1989	--	--	16.08	16.08	0.10	0.04	0.02	0.18	0.00	0.00	20.9
18	51	-0	4309	0	0	0	3184	--	--	16.08	16.08	0.00	0.05	0.04	0.27	0.00	0.00	20.9
19	51	-0	4241	0	0	0	2903	--	--	16.08	16.08	0.00	0.05	0.03	0.27	0.00	0.00	20.9
20	51	-0	4234	0	0	0	2862	--	--	16.08	16.08	0.00	0.05	0.03	0.27	0.00	0.00	20.9
37	51	-0	4163	0	0	0	3134	--	--	16.08	16.08	0.00	0.05	0.03	0.26	0.00	0.00	20.9
38	51	-0	4050	0	0	0	2665	--	--	16.08	16.08	0.00	0.05	0.03	0.25	0.00	0.00	20.9
39	51	-0	4037	0	0	0	2598	--	--	16.08	16.08	0.00	0.04	0.03	0.25	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 22 NI 1533 NF 1537 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	3489	0	0	0	1484	--	--	16.08	16.08	0.00	0.03	0.03	0.22	0.00	0.00	20.9
2	0	-0	2668	0	0	0	1153	--	--	16.08	16.08	0.10	0.02	0.02	0.17	0.00	0.00	20.9
3	0	-0	2676	0	0	0	1144	--	--	16.08	16.08	0.10	0.02	0.02	0.17	0.00	0.00	20.9
4	0	-0	2691	0	0	0	1139	--	--	16.08	16.08	0.10	0.02	0.02	0.17	0.00	0.00	20.9
5	0	-0	2699	0	0	0	1130	--	--	16.08	16.08	0.10	0.02	0.02	0.17	0.00	0.00	20.9
6	0	-0	2667	0	0	0	1158	--	--	16.08	16.08	0.10	0.02	0.02	0.17	0.00	0.00	20.9
7	0	-0	2693	0	0	0	1129	--	--	16.08	16.08	0.10	0.02	0.02	0.17	0.00	0.00	20.9
8	0	-0	2674	0	0	0	1154	--	--	16.08	16.08	0.10	0.02	0.02	0.17	0.00	0.00	20.9
9	0	-0	2700	0	0	0	1125	--	--	16.08	16.08	0.10	0.02	0.02	0.17	0.00	0.00	20.9
10	0	-0	2668	0	0	0	1153	--	--	16.08	16.08	0.10	0.02	0.02	0.17	0.00	0.00	20.9
11	0	-0	2676	0	0	0	1144	--	--	16.08	16.08	0.10	0.02	0.02	0.17	0.00	0.00	20.9
12	0	-0	2691	0	0	0	1139	--	--	16.08	16.08	0.10	0.02	0.02	0.17	0.00	0.00	20.9
13	0	-0	2699	0	0	0	1130	--	--	16.08	16.08	0.10	0.02	0.02	0.17	0.00	0.00	20.9
14	0	-0	2667	0	0	0	1158	--	--	16.08	16.08	0.10	0.02	0.02	0.17	0.00	0.00	20.9
15	0	-0	2693	0	0	0	1129	--	--	16.08	16.08	0.10	0.02	0.02	0.17	0.00	0.00	20.9
16	0	-0	2674	0	0	0	1154	--	--	16.08	16.08	0.10	0.02	0.02	0.17	0.00	0.00	20.9
17	0	-0	2700	0	0	0	1125	--	--	16.08	16.08	0.10	0.02	0.02	0.17	0.00	0.00	20.9
18	0	-0	3992	0	0	0	1889	--	--	16.08	16.08	0.00	0.03	0.03	0.25	0.00	0.00	20.9
19	0	-0	3890	0	0	0	1651	--	--	16.08	16.08	0.00	0.03	0.03	0.24	0.00	0.00	20.9
20	0	-0	3897	0	0	0	1603	--	--	16.08	16.08	0.00	0.03	0.03	0.24	0.00	0.00	20.9
37	0	-0	3884	0	0	0	1875	--	--	16.08	16.08	0.00	0.03	0.03	0.24	0.00	0.00	20.9
38	0	-0	3713	0	0	0	1478	--	--	16.08	16.08	0.00	0.03	0.03	0.23	0.00	0.00	20.9
39	0	-0	3726	0	0	0	1398	--	--	16.08	16.08	0.00	0.02	0.03	0.23	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	26	-0	3489	0	0	0	6109	--	--	16.08	16.08	0.00	0.10	0.03	0.22	0.00	0.00	20.9
2	26	-0	2668	0	0	0	4689	--	--	16.08	16.08	0.10	0.08	0.02	0.17	0.00	0.00	20.9
3	26	-0	2676	0	0	0	4691	--	--	16.08	16.08	0.10	0.08	0.02	0.17	0.00	0.00	20.9
4	26	-0	2691	0	0	0	4706	--	--	16.08	16.08	0.10	0.08	0.02	0.17	0.00	0.00	20.9
5	26	-0	2699	0	0	0	4708	--	--	16.08	16.08	0.10	0.08	0.02	0.17	0.00	0.00	20.9
6	26	-0	2667	0	0	0	4693	--	--	16.08	16.08	0.10	0.08	0.02	0.17	0.00	0.00	20.9
7	26	-0	2693	0	0	0	4699	--	--	16.08	16.08	0.10	0.08	0.02	0.17	0.00	0.00	20.9
8	26	-0	2674	0	0	0	4698	--	--	16.08	16.08	0.10	0.08	0.02	0.17	0.00	0.00	20.9
9	26	-0	2700	0	0	0	4704	--	--	16.08	16.08	0.10	0.08	0.02	0.17	0.00	0.00	20.9
10	26	-0	2668	0	0	0	4689	--	--	16.08	16.08	0.10	0.08	0.02	0.17	0.00	0.00	20.9
11	26	-0	2676	0	0	0	4691	--	--	16.08	16.08	0.10	0.08	0.02	0.17	0.00	0.00	20.9
12	26	-0	2691	0	0	0	4706	--	--	16.08	16.08	0.10	0.08	0.02	0.17	0.00	0.00	20.9
13	26	-0	2699	0	0	0	4708	--	--	16.08	16.08	0.10	0.08	0.02	0.17	0.00	0.00	20.9
14	26	-0	2667	0	0	0	4693	--	--	16.08	16.08	0.10	0.08	0.02	0.17	0.00	0.00	20.9
15	26	-0	2693	0	0	0	4699	--	--	16.08	16.08	0.10	0.08	0.02	0.17	0.00	0.00	20.9
16	26	-0	2674	0	0	0	4698	--	--	16.08	16.08	0.10	0.08	0.02	0.17	0.00	0.00	20.9
17	26	-0	2700	0	0	0	4704	--	--	16.08	16.08	0.10	0.08	0.02	0.17	0.00	0.00	20.9
18	26	-0	3992	0	0	0	7181	--	--	16.08	16.08	0.00	0.12	0.03	0.25	0.00	0.00	20.9
19	26	-0	3890	0	0	0	6807	--	--	16.08	16.08	0.00	0.12	0.03	0.24	0.00	0.00	20.9
20	26	-0	3897	0	0	0	6769	--	--	16.08	16.08	0.00	0.12	0.03	0.24	0.00	0.00	20.9
37	26	-0	3884	0	0	0	7023	--	--	16.08	16.08	0.00	0.12	0.03	0.24	0.00	0.00	20.9
38	26	-0	3713	0	0	0	6400	--	--	16.08	16.08	0.00	0.11	0.03	0.23	0.00	0.00	20.9
39	26	-0	3726	0	0	0	6337	--	--	16.08	16.08	0.00	0.11	0.03	0.23	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	51	-0	3489	0	0	0	3276	--	--	16.08	16.08	0.00	0.06	0.03	0.22	0.00	0.00	20.9
2	51	-0	2668	0	0	0	2523	--	--	16.08	16.08	0.10	0.04	0.02	0.17	0.00	0.00	20.9
3	51	-0	2676	0	0	0	2518	--	--	16.08	16.08	0.10	0.04	0.02	0.17	0.00	0.00	20.9
4	51	-0	2691	0	0	0	2521	--	--	16.08	16.08	0.10	0.04	0.02	0.17	0.00	0.00	20.9
5	51	-0	2699	0	0	0	2516	--	--	16.08	16.08	0.10	0.04	0.02	0.17	0.00	0.00	20.9
6	51	-0	2667	0	0	0	2527	--	--	16.08	16.08	0.10	0.04	0.02	0.17	0.00	0.00	20.9
7	51	-0	2693	0	0	0	2512	--	--	16.08	16.08	0.10	0.04	0.02	0.17	0.00	0.00	20.9
8	51	-0	2674	0	0	0	2527	--	--	16.08	16.08	0.10	0.04	0.02	0.17	0.00	0.00	20.9
9	51	-0	2700	0	0	0	2512	--	--	16.08	16.08	0.10	0.04	0.02	0.17	0.00	0.00	20.9
10	51	-0	2668	0	0	0	2523	--	--	16.08	16.08	0.10	0.04	0.02	0.17	0.00	0.00	20.9
11	51	-0	2676	0	0	0	2518	--	--	16.08	16.08	0.10	0.04	0.02	0.17	0.00	0.00	20.9
12	51	-0	2691	0	0	0	2521	--	--	16.08	16.08	0.10	0.04	0.02	0.17	0.00	0.00	20.9
13	51	-0	2699	0	0	0	2516	--	--	16.08	16.08	0.10	0.04	0.02	0.17	0.00	0.00	20.9
14	51	-0	2667	0	0	0	2527	--	--	16.08	16.08	0.10	0.04	0.02	0.17	0.00	0.00	20.9
15	51	-0	2693	0	0	0	2512	--	--	16.08	16.08	0.10	0.04	0.02	0.17	0.00	0.00	20.9
16	51	-0	2674	0	0	0	2527	--	--	16.08	16.08	0.10	0.04	0.02	0.17	0.00	0.00	20.9
17	51	-0	2700	0	0	0	2512	--	--	16.08	16.08	0.10	0.04	0.02	0.17	0.00	0.00	20.9
18	51	-0	3992	0	0	0	3940	--	--	16.08	16.08	0.00	0.07	0.03	0.25	0.00	0.00	20.9
19	51	-0	3890	0	0	0	3649	--	--	16.08	16.08	0.00	0.06	0.03	0.24	0.00	0.00	20.9
20	51	-0	3897	0	0	0	3605	--	--	16.08	16.08	0.00	0.06	0.03	0.24	0.00	0.00	20.9
37	51	-0	3884	0	0	0	3869	--	--	16.08	16.08	0.00	0.07	0.03	0.24	0.00	0.00	20.9
38	51	-0	3713	0	0	0	3385	--	--	16.08	16.08	0.00	0.06	0.03	0.23	0.00	0.00	20.9
39	51	-0	3726	0	0	0	3312	--	--	16.08	16.08	0.00	0.06	0.03	0.23	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 23 NI 1537 NF 1499 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-3888	0	0	0	3358	--	--	16.08	16.08	0.00	0.06	0.03	0.24	0.00	0.00	20.9
2	0	-0	-3007	0	0	0	2591	--	--	16.08	16.08	0.10	0.05	0.02	0.19	0.00	0.00	20.9
3	0	-0	-3018	0	0	0	2587	--	--	16.08	16.08	0.10	0.05	0.02	0.19	0.00	0.00	20.9
4	0	-0	-2963	0	0	0	2579	--	--	16.08	16.08	0.10	0.05	0.02	0.19	0.00	0.00	20.9
5	0	-0	-2974	0	0	0	2575	--	--	16.08	16.08	0.10	0.05	0.02	0.19	0.00	0.00	20.9
6	0	-0	-2980	0	0	0	2591	--	--	16.08	16.08	0.10	0.05	0.02	0.19	0.00	0.00	20.9
7	0	-0	-3015	0	0	0	2578	--	--	16.08	16.08	0.10	0.05	0.02	0.19	0.00	0.00	20.9
8	0	-0	-2966	0	0	0	2587	--	--	16.08	16.08	0.10	0.05	0.02	0.19	0.00	0.00	20.9
9	0	-0	-3001	0	0	0	2575	--	--	16.08	16.08	0.10	0.05	0.02	0.19	0.00	0.00	20.9
10	0	-0	-3007	0	0	0	2591	--	--	16.08	16.08	0.10	0.05	0.02	0.19	0.00	0.00	20.9

11	0	-0	-3018	0	0	0	2587	--	--	16.08	16.08	0.10	0.05	0.02	0.19	0.00	0.00	20.9
12	0	-0	-2963	0	0	0	2579	--	--	16.08	16.08	0.10	0.05	0.02	0.19	0.00	0.00	20.9
13	0	-0	-2974	0	0	0	2575	--	--	16.08	16.08	0.10	0.05	0.02	0.19	0.00	0.00	20.9
14	0	-0	-2980	0	0	0	2591	--	--	16.08	16.08	0.10	0.05	0.02	0.19	0.00	0.00	20.9
15	0	-0	-3015	0	0	0	2578	--	--	16.08	16.08	0.10	0.05	0.02	0.19	0.00	0.00	20.9
16	0	-0	-2966	0	0	0	2587	--	--	16.08	16.08	0.10	0.05	0.02	0.19	0.00	0.00	20.9
17	0	-0	-3001	0	0	0	2575	--	--	16.08	16.08	0.10	0.05	0.02	0.19	0.00	0.00	20.9
18	0	-0	-4624	0	0	0	4039	--	--	16.08	16.08	0.00	0.07	0.04	0.29	0.00	0.00	20.9
19	0	-0	-4292	0	0	0	3754	--	--	16.08	16.08	0.00	0.06	0.04	0.27	0.00	0.00	20.9
20	0	-0	-4404	0	0	0	3707	--	--	16.08	16.08	0.00	0.06	0.04	0.28	0.00	0.00	20.9
37	0	-0	-4556	0	0	0	3961	--	--	16.08	16.08	0.00	0.07	0.04	0.29	0.00	0.00	20.9
38	0	-0	-4004	0	0	0	3486	--	--	16.08	16.08	0.00	0.06	0.03	0.25	0.00	0.00	20.9
39	0	-0	-4190	0	0	0	3407	--	--	16.08	16.08	0.00	0.06	0.03	0.26	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	-3888	0	0	0	3358	--	--	16.08	16.08	0.00	0.06	0.03	0.24	0.00	0.00	20.9
2	26	-0	-3007	0	0	0	2591	--	--	16.08	16.08	0.10	0.05	0.02	0.19	0.00	0.00	20.9
3	26	-0	-3018	0	0	0	2587	--	--	16.08	16.08	0.10	0.05	0.02	0.19	0.00	0.00	20.9
4	26	-0	-2963	0	0	0	2579	--	--	16.08	16.08	0.10	0.05	0.02	0.19	0.00	0.00	20.9
5	26	-0	-2974	0	0	0	2575	--	--	16.08	16.08	0.10	0.05	0.02	0.19	0.00	0.00	20.9
6	26	-0	-2980	0	0	0	2591	--	--	16.08	16.08	0.10	0.05	0.02	0.19	0.00	0.00	20.9
7	26	-0	-3015	0	0	0	2578	--	--	16.08	16.08	0.10	0.05	0.02	0.19	0.00	0.00	20.9
8	26	-0	-2966	0	0	0	2587	--	--	16.08	16.08	0.10	0.05	0.02	0.19	0.00	0.00	20.9
9	26	-0	-3001	0	0	0	2575	--	--	16.08	16.08	0.10	0.05	0.02	0.19	0.00	0.00	20.9
10	26	-0	-3007	0	0	0	2591	--	--	16.08	16.08	0.10	0.05	0.02	0.19	0.00	0.00	20.9
11	26	-0	-3018	0	0	0	2587	--	--	16.08	16.08	0.10	0.05	0.02	0.19	0.00	0.00	20.9
12	26	-0	-2963	0	0	0	2579	--	--	16.08	16.08	0.10	0.05	0.02	0.19	0.00	0.00	20.9
13	26	-0	-2974	0	0	0	2575	--	--	16.08	16.08	0.10	0.05	0.02	0.19	0.00	0.00	20.9
14	26	-0	-2980	0	0	0	2591	--	--	16.08	16.08	0.10	0.05	0.02	0.19	0.00	0.00	20.9
15	26	-0	-3015	0	0	0	2578	--	--	16.08	16.08	0.10	0.05	0.02	0.19	0.00	0.00	20.9
16	26	-0	-2966	0	0	0	2587	--	--	16.08	16.08	0.10	0.05	0.02	0.19	0.00	0.00	20.9
17	26	-0	-3001	0	0	0	2575	--	--	16.08	16.08	0.10	0.05	0.02	0.19	0.00	0.00	20.9
18	26	-0	-4624	0	0	0	4039	--	--	16.08	16.08	0.00	0.07	0.04	0.29	0.00	0.00	20.9
19	26	-0	-4292	0	0	0	3754	--	--	16.08	16.08	0.00	0.06	0.04	0.27	0.00	0.00	20.9
20	26	-0	-4404	0	0	0	3707	--	--	16.08	16.08	0.00	0.06	0.04	0.28	0.00	0.00	20.9
37	26	-0	-4556	0	0	0	3961	--	--	16.08	16.08	0.00	0.07	0.04	0.29	0.00	0.00	20.9
38	26	-0	-4004	0	0	0	3486	--	--	16.08	16.08	0.00	0.06	0.03	0.25	0.00	0.00	20.9
39	26	-0	-4190	0	0	0	3407	--	--	16.08	16.08	0.00	0.06	0.03	0.26	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	-3888	0	0	0	1361	--	--	16.08	16.08	0.00	0.02	0.03	0.24	0.00	0.00	20.9
2	51	-0	-3007	0	0	0	1047	--	--	16.08	16.08	0.10	0.02	0.02	0.19	0.00	0.00	20.9
3	51	-0	-3018	0	0	0	1037	--	--	16.08	16.08	0.10	0.02	0.02	0.19	0.00	0.00	20.9
4	51	-0	-2963	0	0	0	1057	--	--	16.08	16.08	0.10	0.02	0.02	0.19	0.00	0.00	20.9
5	51	-0	-2974	0	0	0	1047	--	--	16.08	16.08	0.10	0.02	0.02	0.19	0.00	0.00	20.9
6	51	-0	-2980	0	0	0	1061	--	--	16.08	16.08	0.10	0.02	0.02	0.19	0.00	0.00	20.9
7	51	-0	-3015	0	0	0	1030	--	--	16.08	16.08	0.10	0.02	0.02	0.19	0.00	0.00	20.9
8	51	-0	-2966	0	0	0	1064	--	--	16.08	16.08	0.10	0.02	0.02	0.19	0.00	0.00	20.9
9	51	-0	-3001	0	0	0	1033	--	--	16.08	16.08	0.10	0.02	0.02	0.19	0.00	0.00	20.9
10	51	-0	-3007	0	0	0	1047	--	--	16.08	16.08	0.10	0.02	0.02	0.19	0.00	0.00	20.9
11	51	-0	-3018	0	0	0	1037	--	--	16.08	16.08	0.10	0.02	0.02	0.19	0.00	0.00	20.9
12	51	-0	-2963	0	0	0	1057	--	--	16.08	16.08	0.10	0.02	0.02	0.19	0.00	0.00	20.9
13	51	-0	-2974	0	0	0	1047	--	--	16.08	16.08	0.10	0.02	0.02	0.19	0.00	0.00	20.9
14	51	-0	-2980	0	0	0	1061	--	--	16.08	16.08	0.10	0.02	0.02	0.19	0.00	0.00	20.9
15	51	-0	-3015	0	0	0	1030	--	--	16.08	16.08	0.10	0.02	0.02	0.19	0.00	0.00	20.9
16	51	-0	-2966	0	0	0	1064	--	--	16.08	16.08	0.10	0.02	0.02	0.19	0.00	0.00	20.9
17	51	-0	-3001	0	0	0	1033	--	--	16.08	16.08	0.10	0.02	0.02	0.19	0.00	0.00	20.9
18	51	-0	-4624	0	0	0	1664	--	--	16.08	16.08	0.00	0.03	0.04	0.29	0.00	0.00	20.9
19	51	-0	-4292	0	0	0	1550	--	--	16.08	16.08	0.00	0.03	0.04	0.27	0.00	0.00	20.9
20	51	-0	-4404	0	0	0	1445	--	--	16.08	16.08	0.00	0.02	0.04	0.28	0.00	0.00	20.9
37	51	-0	-4556	0	0	0	1620	--	--	16.08	16.08	0.00	0.03	0.04	0.29	0.00	0.00	20.9
38	51	-0	-4004	0	0	0	1430	--	--	16.08	16.08	0.00	0.02	0.03	0.25	0.00	0.00	20.9
39	51	-0	-4190	0	0	0	1255	--	--	16.08	16.08	0.00	0.02	0.03	0.26	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 24 NI 1499 NF 1512 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm

1	0	-0	-4131	0	0	0	2602	--	--	16.08	16.08	0.00	0.04	0.03	0.26	0.00	0.00	20.9
2	0	-0	-3198	0	0	0	2007	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
3	0	-0	-3210	0	0	0	2001	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
4	0	-0	-3145	0	0	0	2002	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
5	0	-0	-3157	0	0	0	1996	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
6	0	-0	-3166	0	0	0	2012	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
7	0	-0	-3206	0	0	0	1993	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
8	0	-0	-3150	0	0	0	2010	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
9	0	-0	-3190	0	0	0	1991	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
10	0	-0	-3198	0	0	0	2007	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
11	0	-0	-3210	0	0	0	2001	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
12	0	-0	-3145	0	0	0	2002	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
13	0	-0	-3157	0	0	0	1996	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
14	0	-0	-3166	0	0	0	2012	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
15	0	-0	-3206	0	0	0	1993	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
16	0	-0	-3150	0	0	0	2010	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
17	0	-0	-3190	0	0	0	1991	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
18	0	-0	-5024	0	0	0	3154	--	--	16.08	16.08	0.00	0.05	0.04	0.32	0.00	0.00	20.9
19	0	-0	-4554	0	0	0	2928	--	--	16.08	16.08	0.00	0.05	0.04	0.29	0.00	0.00	20.9
20	0	-0	-4732	0	0	0	2861	--	--	16.08	16.08	0.00	0.05	0.04	0.30	0.00	0.00	20.9
37	0	-0	-4974	0	0	0	3087	--	--	16.08	16.08	0.00	0.05	0.04	0.31	0.00	0.00	20.9
38	0	-0	-4190	0	0	0	2710	--	--	16.08	16.08	0.00	0.05	0.03	0.26	0.00	0.00	20.9
39	0	-0	-4487	0	0	0	2599	--	--	16.08	16.08	0.00	0.04	0.04	0.28	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	-4131	0	0	0	2602	--	--	16.08	16.08	0.00	0.04	0.03	0.26	0.00	0.00	20.9
2	26	-0	-3198	0	0	0	2007	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
3	26	-0	-3210	0	0	0	2001	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
4	26	-0	-3145	0	0	0	2002	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
5	26	-0	-3157	0	0	0	1996	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
6	26	-0	-3166	0	0	0	2012	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9

7	26	-0	-3206	0	0	0	1993	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
8	26	-0	-3150	0	0	0	2010	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
9	26	-0	-3190	0	0	0	1991	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
10	26	-0	-3198	0	0	0	2007	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
11	26	-0	-3210	0	0	0	2001	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
12	26	-0	-3145	0	0	0	2002	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
13	26	-0	-3157	0	0	0	1996	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
14	26	-0	-3166	0	0	0	2012	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
15	26	-0	-3206	0	0	0	1993	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
16	26	-0	-3150	0	0	0	2010	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
17	26	-0	-3190	0	0	0	1991	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
18	26	-0	-5024	0	0	0	3154	--	--	16.08	16.08	0.00	0.05	0.04	0.32	0.00	0.00	20.9
19	26	-0	-4554	0	0	0	2928	--	--	16.08	16.08	0.00	0.05	0.04	0.29	0.00	0.00	20.9
20	26	-0	-4732	0	0	0	2861	--	--	16.08	16.08	0.00	0.05	0.04	0.30	0.00	0.00	20.9
37	26	-0	-4974	0	0	0	3087	--	--	16.08	16.08	0.00	0.05	0.04	0.31	0.00	0.00	20.9
38	26	-0	-4190	0	0	0	2710	--	--	16.08	16.08	0.00	0.05	0.03	0.26	0.00	0.00	20.9
39	26	-0	-4487	0	0	0	2599	--	--	16.08	16.08	0.00	0.04	0.04	0.28	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	-4131	0	0	0	480	--	--	16.08	16.08	0.00	0.01	0.03	0.26	0.00	0.00	20.9
2	51	-0	-3198	0	0	0	364	--	--	16.08	16.08	0.10	0.01	0.03	0.20	0.00	0.00	20.9
3	51	-0	-3210	0	0	0	352	--	--	16.08	16.08	0.10	0.01	0.03	0.20	0.00	0.00	20.9
4	51	-0	-3145	0	0	0	387	--	--	16.08	16.08	0.10	0.01	0.03	0.20	0.00	0.00	20.9
5	51	-0	-3157	0	0	0	375	--	--	16.08	16.08	0.10	0.01	0.03	0.20	0.00	0.00	20.9
6	51	-0	-3166	0	0	0	386	--	--	16.08	16.08	0.10	0.01	0.03	0.20	0.00	0.00	20.9
7	51	-0	-3206	0	0	0	346	--	--	16.08	16.08	0.10	0.01	0.03	0.20	0.00	0.00	20.9
8	51	-0	-3150	0	0	0	392	--	--	16.08	16.08	0.10	0.01	0.03	0.20	0.00	0.00	20.9
9	51	-0	-3190	0	0	0	353	--	--	16.08	16.08	0.10	0.01	0.03	0.20	0.00	0.00	20.9
10	51	-0	-3198	0	0	0	364	--	--	16.08	16.08	0.10	0.01	0.03	0.20	0.00	0.00	20.9
11	51	-0	-3210	0	0	0	352	--	--	16.08	16.08	0.10	0.01	0.03	0.20	0.00	0.00	20.9
12	51	-0	-3145	0	0	0	387	--	--	16.08	16.08	0.10	0.01	0.03	0.20	0.00	0.00	20.9
13	51	-0	-3157	0	0	0	375	--	--	16.08	16.08	0.10	0.01	0.03	0.20	0.00	0.00	20.9
14	51	-0	-3166	0	0	0	386	--	--	16.08	16.08	0.10	0.01	0.03	0.20	0.00	0.00	20.9
15	51	-0	-3206	0	0	0	346	--	--	16.08	16.08	0.10	0.01	0.03	0.20	0.00	0.00	20.9
16	51	-0	-3150	0	0	0	392	--	--	16.08	16.08	0.10	0.01	0.03	0.20	0.00	0.00	20.9
17	51	-0	-3190	0	0	0	353	--	--	16.08	16.08	0.10	0.01	0.03	0.20	0.00	0.00	20.9
18	51	-0	-5024	0	0	0	573	--	--	16.08	16.08	0.00	0.01	0.04	0.32	0.00	0.00	20.9
19	51	-0	-4554	0	0	0	588	--	--	16.08	16.08	0.00	0.01	0.04	0.29	0.00	0.00	20.9
20	51	-0	-4732	0	0	0	430	--	--	16.08	16.08	0.00	0.01	0.04	0.30	0.00	0.00	20.9
37	51	-0	-4974	0	0	0	532	--	--	16.08	16.08	0.00	0.01	0.04	0.31	0.00	0.00	20.9
38	51	-0	-4190	0	0	0	557	--	--	16.08	16.08	0.00	0.01	0.03	0.26	0.00	0.00	20.9
39	51	-0	-4487	0	0	0	294	--	--	16.08	16.08	0.00	0.01	0.04	0.28	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 25 NI 1512 NF 1511 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm

1	0	-0	-3322	0	0	0	1743	--	--	16.08	16.08	0.00	0.03	0.03	0.21	0.00	0.00	20.9
2	0	-0	-2582	0	0	0	1345	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
3	0	-0	-2593	0	0	0	1337	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
4	0	-0	-2517	0	0	0	1345	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
5	0	-0	-2528	0	0	0	1337	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
6	0	-0	-2546	0	0	0	1355	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
7	0	-0	-2583	0	0	0	1327	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
8	0	-0	-2527	0	0	0	1355	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
9	0	-0	-2564	0	0	0	1327	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
10	0	-0	-2582	0	0	0	1345	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
11	0	-0	-2593	0	0	0	1337	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
12	0	-0	-2517	0	0	0	1345	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
13	0	-0	-2528	0	0	0	1337	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
14	0	-0	-2546	0	0	0	1355	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
15	0	-0	-2583	0	0	0	1327	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
16	0	-0	-2527	0	0	0	1355	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
17	0	-0	-2564	0	0	0	1327	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
18	0	-0	-4216	0	0	0	2168	--	--	16.08	16.08	0.00	0.04	0.03	0.26	0.00	0.00	20.9
19	0	-0	-3607	0	0	0	1951	--	--	16.08	16.08	0.00	0.03	0.03	0.23	0.00	0.00	20.9
20	0	-0	-3870	0	0	0	1891	--	--	16.08	16.08	0.00	0.03	0.03	0.24	0.00	0.00	20.9
37	0	-0	-4232	0	0	0	2136	--	--	16.08	16.08	0.00	0.04	0.03	0.27	0.00	0.00	20.9
38	0	-0	-3218	0	0	0	1775	--	--	16.08	16.08	0.00	0.03	0.03	0.20	0.00	0.00	20.9
39	0	-0	-3656	0	0	0	1674	--	--	16.08	16.08	0.00	0.03	0.03	0.23	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	-3322	0	0	0	1743	--	--	16.08	16.08	0.00	0.03	0.03	0.21	0.00	0.00	20.9
2	26	-0	-2582	0	0	0	1345	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
3	26	-0	-2593	0	0	0	1337	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
4	26	-0	-2517	0	0	0	1345	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
5	26	-0	-2528	0	0	0	1337	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
6	26	-0	-2546	0	0	0	1355	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
7	26	-0	-2583	0	0	0	1327	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
8	26	-0	-2527	0	0	0	1355	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
9	26	-0	-2564	0	0	0	1327	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
10	26	-0	-2582	0	0	0	1345	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
11	26	-0	-2593	0	0	0	1337	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
12	26	-0	-2517	0	0	0	1345	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
13	26	-0	-2528	0	0	0	1337	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
14	26	-0	-2546	0	0	0	1355	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
15	26	-0	-2583	0	0	0	1327	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
16	26	-0	-2527	0	0	0	1355	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
17	26	-0	-2564	0	0	0	1327	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
18	26	-0	-4216	0	0	0	2168	--	--	16.08	16.08	0.00	0.04	0.03	0.26	0.00	0.00	20.9
19	26	-0	-3607	0	0	0	1951	--	--	16.08	16.08	0.00	0.03	0.03	0.23	0.00	0.00	20.9
20	26	-0	-3870	0	0	0	1891	--	--	16.08	16.08	0.00	0.03	0.03	0.24	0.00	0.00	20.9
37	26	-0	-4232	0	0	0	2136	--	--	16.08	16.08	0.00	0.04	0.03	0.27	0.00	0.00	20.9
38	26	-0	-3218	0	0	0	1775	--	--	16.08	16.08	0.00	0.03	0.03	0.20	0.00	0.00	20.9
39	26	-0	-3656	0	0	0	1674	--	--	16.08	16.08	0.00	0.03	0.03	0.23	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	-3322	0	0	0	37	--	--	16.08	16.08	0.00	0.00	0.03	0.21	0.00	0.00	20.9
2	51	-0	-2582	0	0	0	19	--	--	16.08	16.08	0.10	0.00	0.02	0.16	0.00	0.00	20.9

3	51	-0	-2593	0	0	0	5	--	--	16.08	16.08	0.10	0.00	0.02	0.16	0.00	0.00	20.9
4	51	-0	-2517	0	0	0	52	--	--	16.08	16.08	0.10	0.00	0.02	0.16	0.00	0.00	20.9
5	51	-0	-2528	0	0	0	38	--	--	16.08	16.08	0.10	0.00	0.02	0.16	0.00	0.00	20.9
6	51	-0	-2546	0	0	0	47	--	--	16.08	16.08	0.10	0.00	0.02	0.16	0.00	0.00	20.9
7	51	-0	-2583	0	0	0	1	--	--	16.08	16.08	0.10	0.00	0.02	0.16	0.00	0.00	20.9
8	51	-0	-2527	0	0	0	57	--	--	16.08	16.08	0.10	0.00	0.02	0.16	0.00	0.00	20.9
9	51	-0	-2564	0	0	0	11	--	--	16.08	16.08	0.10	0.00	0.02	0.16	0.00	0.00	20.9
10	51	-0	-2582	0	0	0	19	--	--	16.08	16.08	0.10	0.00	0.02	0.16	0.00	0.00	20.9
11	51	-0	-2593	0	0	0	5	--	--	16.08	16.08	0.10	0.00	0.02	0.16	0.00	0.00	20.9
12	51	-0	-2517	0	0	0	52	--	--	16.08	16.08	0.10	0.00	0.02	0.16	0.00	0.00	20.9
13	51	-0	-2528	0	0	0	38	--	--	16.08	16.08	0.10	0.00	0.02	0.16	0.00	0.00	20.9
14	51	-0	-2546	0	0	0	47	--	--	16.08	16.08	0.10	0.00	0.02	0.16	0.00	0.00	20.9
15	51	-0	-2583	0	0	0	1	--	--	16.08	16.08	0.10	0.00	0.02	0.16	0.00	0.00	20.9
16	51	-0	-2527	0	0	0	57	--	--	16.08	16.08	0.10	0.00	0.02	0.16	0.00	0.00	20.9
17	51	-0	-2564	0	0	0	11	--	--	16.08	16.08	0.10	0.00	0.02	0.16	0.00	0.00	20.9
18	51	-0	-4216	0	0	0	3	--	--	16.08	16.08	0.00	0.00	0.03	0.26	0.00	0.00	20.9
19	51	-0	-3607	0	0	0	99	--	--	16.08	16.08	0.00	0.00	0.03	0.23	0.00	0.00	20.9
20	51	-0	-3870	0	0	0	-97	--	--	16.08	16.08	0.18	0.00	0.03	0.24	0.00	0.00	20.9
37	51	-0	-4232	0	0	0	-37	--	--	16.08	16.08	0.18	0.00	0.03	0.27	0.00	0.00	20.9
38	51	-0	-3218	0	0	0	123	--	--	16.08	16.08	0.00	0.00	0.03	0.20	0.00	0.00	20.9
39	51	-0	-3656	0	0	0	-204	--	--	16.08	16.08	0.18	0.00	0.03	0.23	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 26 NI 1511 NF 1510 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-2108	0	0	0	859	--	--	16.08	16.08	0.00	0.01	0.02	0.13	0.00	0.00	20.9
2	0	-0	-1652	0	0	0	661	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
3	0	-0	-1661	0	0	0	651	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
4	0	-0	-1583	0	0	0	671	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
5	0	-0	-1592	0	0	0	661	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
6	0	-0	-1617	0	0	0	677	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
7	0	-0	-1648	0	0	0	642	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
8	0	-0	-1596	0	0	0	680	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
9	0	-0	-1627	0	0	0	645	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
10	0	-0	-1652	0	0	0	661	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
11	0	-0	-1661	0	0	0	651	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
12	0	-0	-1583	0	0	0	671	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
13	0	-0	-1592	0	0	0	661	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
14	0	-0	-1617	0	0	0	677	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
15	0	-0	-1648	0	0	0	642	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
16	0	-0	-1596	0	0	0	680	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
17	0	-0	-1627	0	0	0	645	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
18	0	-0	-2878	0	0	0	1099	--	--	16.08	16.08	0.00	0.02	0.02	0.18	0.00	0.00	20.9
19	0	-0	-2249	0	0	0	974	--	--	16.08	16.08	0.00	0.02	0.02	0.14	0.00	0.00	20.9
20	0	-0	-2548	0	0	0	880	--	--	16.08	16.08	0.00	0.02	0.02	0.16	0.00	0.00	20.9
37	0	-0	-2942	0	0	0	1080	--	--	16.08	16.08	0.00	0.02	0.02	0.18	0.00	0.00	20.9
38	0	-0	-1893	0	0	0	873	--	--	16.08	16.08	0.00	0.01	0.02	0.12	0.00	0.00	20.9
39	0	-0	-2392	0	0	0	716	--	--	16.08	16.08	0.00	0.01	0.02	0.15	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	-2108	0	0	0	859	--	--	16.08	16.08	0.00	0.01	0.02	0.13	0.00	0.00	20.9
2	26	-0	-1652	0	0	0	661	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
3	26	-0	-1661	0	0	0	651	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
4	26	-0	-1583	0	0	0	671	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
5	26	-0	-1592	0	0	0	661	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
6	26	-0	-1617	0	0	0	677	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
7	26	-0	-1648	0	0	0	642	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
8	26	-0	-1596	0	0	0	680	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
9	26	-0	-1627	0	0	0	645	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
10	26	-0	-1652	0	0	0	661	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
11	26	-0	-1661	0	0	0	651	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
12	26	-0	-1583	0	0	0	671	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
13	26	-0	-1592	0	0	0	661	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
14	26	-0	-1617	0	0	0	677	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
15	26	-0	-1648	0	0	0	642	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
16	26	-0	-1596	0	0	0	680	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
17	26	-0	-1627	0	0	0	645	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
18	26	-0	-2878	0	0	0	1099	--	--	16.08	16.08	0.00	0.02	0.02	0.18	0.00	0.00	20.9
19	26	-0	-2249	0	0	0	974	--	--	16.08	16.08	0.00	0.02	0.02	0.14	0.00	0.00	20.9
20	26	-0	-2548	0	0	0	880	--	--	16.08	16.08	0.00	0.02	0.02	0.16	0.00	0.00	20.9
37	26	-0	-2942	0	0	0	1080	--	--	16.08	16.08	0.00	0.02	0.02	0.18	0.00	0.00	20.9
38	26	-0	-1893	0	0	0	873	--	--	16.08	16.08	0.00	0.01	0.02	0.12	0.00	0.00	20.9
39	26	-0	-2392	0	0	0	716	--	--	16.08	16.08	0.00	0.01	0.02	0.15	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	-2108	0	0	0	-224	--	--	16.08	16.08	0.18	0.00	0.02	0.13	0.00	0.00	20.9
2	51	-0	-1652	0	0	0	-187	--	--	16.08	16.08	0.29	0.00	0.01	0.10	0.00	0.00	20.9
3	51	-0	-1661	0	0	0	-202	--	--	16.08	16.08	0.29	0.00	0.01	0.10	0.00	0.00	20.9
4	51	-0	-1583	0	0	0	-141	--	--	16.08	16.08	0.29	0.00	0.01	0.10	0.00	0.00	20.9
5	51	-0	-1592	0	0	0	-157	--	--	16.08	16.08	0.29	0.00	0.01	0.10	0.00	0.00	20.9
6	51	-0	-1617	0	0	0	-153	--	--	16.08	16.08	0.29	0.00	0.01	0.10	0.00	0.00	20.9
7	51	-0	-1648	0	0	0	-204	--	--	16.08	16.08	0.29	0.00	0.01	0.10	0.00	0.00	20.9
8	51	-0	-1596	0	0	0	-139	--	--	16.08	16.08	0.29	0.00	0.01	0.10	0.00	0.00	20.9
9	51	-0	-1627	0	0	0	-191	--	--	16.08	16.08	0.29	0.00	0.01	0.10	0.00	0.00	20.9
10	51	-0	-1652	0	0	0	-187	--	--	16.08	16.08	0.29	0.00	0.01	0.10	0.00	0.00	20.9
11	51	-0	-1661	0	0	0	-202	--	--	16.08	16.08	0.29	0.00	0.01	0.10	0.00	0.00	20.9
12	51	-0	-1583	0	0	0	-141	--	--	16.08	16.08	0.29	0.00	0.01	0.10	0.00	0.00	20.9
13	51	-0	-1592	0	0	0	-157	--	--	16.08	16.08	0.29	0.00	0.01	0.10	0.00	0.00	20.9
14	51	-0	-1617	0	0	0	-153	--	--	16.08	16.08	0.29	0.00	0.01	0.10	0.00	0.00	20.9
15	51	-0	-1648	0	0	0	-204	--	--	16.08	16.08	0.29	0.00	0.01	0.10	0.00	0.00	20.9
16	51	-0	-1596	0	0	0	-139	--	--	16.08	16.08	0.29	0.00	0.01	0.10	0.00	0.00	20.9
17	51	-0	-1627	0	0	0	-191	--	--	16.08	16.08	0.29	0.00	0.01	0.10	0.00	0.00	20.9
18	51	-0	-2878	0	0	0	-379	--	--	16.08	16.08	0.18	0.01	0.02	0.18	0.00	0.00	20.9
19	51	-0	-2249	0	0	0	-180	--	--	16.08	16.08	0.18	0.00	0.02	0.14	0.00	0.00	20.9
20	51	-0	-2548	0	0	0	-428	--	--	16.08	16.08	0.18	0.01	0.02	0.16	0.00	0.00	20.9
37	51	-0	-2942	0	0	0	-431	--	--	16.08	16.08	0.18	0.01	0.02	0.18	0.00	0.00	20.9
38	51	-0	-1893	0	0	0	-100	--	--	16.08	16.08	0.18	0.00	0.02	0.12	0.00	0.00	20.9
39	51	-0	-2392	0	0	0	-513	--	--	16.08	16.08	0.18	0.01	0.02	0.15	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 27 NI 1510 NF 1529 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-1017	0	0	0	265	--	--	16.08	16.08	0.00	0.00	0.01	0.06	0.00	0.00	20.9
2	0	-0	-815	0	0	0	200	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
3	0	-0	-823	0	0	0	187	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
4	0	-0	-742	0	0	0	221	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
5	0	-0	-750	0	0	0	208	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
6	0	-0	-780	0	0	0	222	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
7	0	-0	-806	0	0	0	180	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
8	0	-0	-759	0	0	0	228	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
9	0	-0	-784	0	0	0	186	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
10	0	-0	-815	0	0	0	200	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
11	0	-0	-823	0	0	0	187	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
12	0	-0	-742	0	0	0	221	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
13	0	-0	-750	0	0	0	208	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
14	0	-0	-780	0	0	0	222	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
15	0	-0	-806	0	0	0	180	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
16	0	-0	-759	0	0	0	228	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
17	0	-0	-784	0	0	0	186	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
18	0	-0	-1669	0	0	0	345	--	--	16.08	16.08	0.00	0.01	0.01	0.10	0.00	0.00	20.9
19	0	-0	-1037	0	0	0	329	--	--	16.08	16.08	0.00	0.01	0.01	0.07	0.00	0.00	20.9
20	0	-0	-1361	0	0	0	188	--	--	16.08	16.08	0.00	0.00	0.01	0.09	0.00	0.00	20.9
37	0	-0	-1771	0	0	0	323	--	--	16.08	16.08	0.00	0.01	0.01	0.11	0.00	0.00	20.9
38	0	-0	-717	0	0	0	298	--	--	16.08	16.08	0.00	0.01	0.01	0.04	0.00	0.00	20.9
39	0	-0	-1257	0	0	0	61	--	--	16.08	16.08	0.00	0.00	0.01	0.08	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	26	-0	-1017	0	0	0	265	--	--	16.08	16.08	0.00	0.00	0.01	0.06	0.00	0.00	20.9
2	26	-0	-815	0	0	0	-219	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
3	26	-0	-823	0	0	0	-236	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
4	26	-0	-742	0	0	0	221	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
5	26	-0	-750	0	0	0	208	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
6	26	-0	-780	0	0	0	222	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
7	26	-0	-806	0	0	0	-235	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
8	26	-0	-759	0	0	0	228	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
9	26	-0	-784	0	0	0	-217	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
10	26	-0	-815	0	0	0	-219	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
11	26	-0	-823	0	0	0	-236	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
12	26	-0	-742	0	0	0	221	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
13	26	-0	-750	0	0	0	208	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
14	26	-0	-780	0	0	0	222	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
15	26	-0	-806	0	0	0	-235	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
16	26	-0	-759	0	0	0	228	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
17	26	-0	-784	0	0	0	-217	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
18	26	-0	-1669	0	0	0	-513	--	--	16.08	16.08	0.18	0.01	0.01	0.10	0.00	0.00	20.9
19	26	-0	-1037	0	0	0	329	--	--	16.08	16.08	0.00	0.01	0.01	0.07	0.00	0.00	20.9
20	26	-0	-1361	0	0	0	-511	--	--	16.08	16.08	0.18	0.01	0.01	0.09	0.00	0.00	20.9
37	26	-0	-1771	0	0	0	-587	--	--	16.08	16.08	0.18	0.01	0.01	0.11	0.00	0.00	20.9
38	26	-0	-717	0	0	0	298	--	--	16.08	16.08	0.00	0.01	0.01	0.04	0.00	0.00	20.9
39	26	-0	-1257	0	0	0	-584	--	--	16.08	16.08	0.18	0.01	0.01	0.08	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	51	-0	-1017	0	0	0	-257	--	--	16.08	16.08	0.18	0.00	0.01	0.06	0.00	0.00	20.9
2	51	-0	-815	0	0	0	-219	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
3	51	-0	-823	0	0	0	-236	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
4	51	-0	-742	0	0	0	-160	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
5	51	-0	-750	0	0	0	-177	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
6	51	-0	-780	0	0	0	-179	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
7	51	-0	-806	0	0	0	-235	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
8	51	-0	-759	0	0	0	-161	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
9	51	-0	-784	0	0	0	-217	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
10	51	-0	-815	0	0	0	-219	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
11	51	-0	-823	0	0	0	-236	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
12	51	-0	-742	0	0	0	-160	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
13	51	-0	-750	0	0	0	-177	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
14	51	-0	-780	0	0	0	-179	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
15	51	-0	-806	0	0	0	-235	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
16	51	-0	-759	0	0	0	-161	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
17	51	-0	-784	0	0	0	-217	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
18	51	-0	-1669	0	0	0	-513	--	--	16.08	16.08	0.18	0.01	0.01	0.10	0.00	0.00	20.9
19	51	-0	-1037	0	0	0	-203	--	--	16.08	16.08	0.18	0.00	0.01	0.07	0.00	0.00	20.9
20	51	-0	-1361	0	0	0	-511	--	--	16.08	16.08	0.18	0.01	0.01	0.09	0.00	0.00	20.9
37	51	-0	-1771	0	0	0	-587	--	--	16.08	16.08	0.18	0.01	0.01	0.11	0.00	0.00	20.9
38	51	-0	-717	0	0	0	-71	--	--	16.08	16.08	0.18	0.00	0.01	0.04	0.00	0.00	20.9
39	51	-0	-1257	0	0	0	-584	--	--	16.08	16.08	0.18	0.01	0.01	0.08	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 28 NI 1529 NF 1528 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	5	0	0	0	-95	--	--	16.08	16.08	0.18	0.00	0.00	0.00	0.00	0.00	20.9
2	0	-0	-32	0	0	0	-99	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
3	0	-0	-38	0	0	0	-117	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
4	0	-0	46	0	0	0	-49	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
5	0	-0	39	0	0	0	-64	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
6	0	-0	2	0	0	0	-54	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
7	0	-0	-18	0	0	0	-112	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
8	0	-0	26	0	0	0	-44	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
9	0	-0	5	0	0	0	-92	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
10	0	-0	-32	0	0	0	-99	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9

11	0	-0	-38	0	0	0	-117	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
12	0	-0	46	0	0	0	-49	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
13	0	-0	39	0	0	0	-64	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
14	0	-0	2	0	0	0	-54	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
15	0	-0	-18	0	0	0	-112	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
16	0	-0	26	0	0	0	-44	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
17	0	-0	5	0	0	0	-92	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
18	0	-0	-546	0	0	0	-429	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9
19	0	-0	99	0	0	0	-55	--	--	16.08	16.08	0.18	0.00	0.00	0.01	0.00	0.00	20.9
20	0	-0	-251	0	0	0	-378	--	--	16.08	16.08	0.18	0.01	0.00	0.02	0.00	0.00	20.9
37	0	-0	-684	0	0	0	-533	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
38	0	-0	390	0	0	0	-25	--	--	16.08	16.08	0.18	0.00	0.00	0.02	0.00	0.00	20.9
39	0	-0	-193	0	0	0	-449	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	5	0	0	0	-95	--	--	16.08	16.08	0.18	0.00	0.00	0.00	0.00	0.00	20.9
2	26	-0	-32	0	0	0	-99	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
3	26	-0	-38	0	0	0	-117	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
4	26	-0	46	0	0	0	-49	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
5	26	-0	39	0	0	0	-64	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
6	26	-0	2	0	0	0	-54	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
7	26	-0	-18	0	0	0	-112	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
8	26	-0	26	0	0	0	-44	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
9	26	-0	5	0	0	0	-92	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
10	26	-0	-32	0	0	0	-99	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
11	26	-0	-38	0	0	0	-117	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
12	26	-0	46	0	0	0	-49	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
13	26	-0	39	0	0	0	-64	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
14	26	-0	2	0	0	0	-54	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
15	26	-0	-18	0	0	0	-112	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
16	26	-0	26	0	0	0	-44	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
17	26	-0	5	0	0	0	-92	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
18	26	-0	-546	0	0	0	-429	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9
19	26	-0	99	0	0	0	-55	--	--	16.08	16.08	0.18	0.00	0.00	0.01	0.00	0.00	20.9
20	26	-0	-251	0	0	0	-378	--	--	16.08	16.08	0.18	0.01	0.00	0.02	0.00	0.00	20.9
37	26	-0	-684	0	0	0	-533	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
38	26	-0	390	0	0	0	492	--	--	16.08	16.08	0.00	0.01	0.00	0.02	0.00	0.00	20.9
39	26	-0	-193	0	0	0	-449	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	5	0	0	0	-95	--	--	16.08	16.08	0.18	0.00	0.00	0.00	0.00	0.00	20.9
2	51	-0	-32	0	0	0	-99	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
3	51	-0	-38	0	0	0	-117	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
4	51	-0	46	0	0	0	-49	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
5	51	-0	39	0	0	0	-64	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
6	51	-0	2	0	0	0	-54	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
7	51	-0	-18	0	0	0	-112	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
8	51	-0	26	0	0	0	-44	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
9	51	-0	5	0	0	0	-92	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
10	51	-0	-32	0	0	0	-99	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
11	51	-0	-38	0	0	0	-117	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
12	51	-0	46	0	0	0	-49	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
13	51	-0	39	0	0	0	-64	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
14	51	-0	2	0	0	0	-54	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
15	51	-0	-18	0	0	0	-112	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
16	51	-0	26	0	0	0	-44	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
17	51	-0	5	0	0	0	-92	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
18	51	-0	-546	0	0	0	-429	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9
19	51	-0	99	0	0	0	-55	--	--	16.08	16.08	0.18	0.00	0.00	0.01	0.00	0.00	20.9
20	51	-0	-251	0	0	0	-378	--	--	16.08	16.08	0.18	0.01	0.00	0.02	0.00	0.00	20.9
37	51	-0	-684	0	0	0	-533	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
38	51	-0	390	0	0	0	175	--	--	16.08	16.08	0.00	0.00	0.00	0.02	0.00	0.00	20.9
39	51	-0	-193	0	0	0	-449	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 29 NI 1528 NF 1500 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	1019	0	0	0	-252	--	--	16.08	16.08	0.18	0.00	0.01	0.06	0.00	0.00	20.9
2	0	-0	745	0	0	0	-209	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
3	0	-0	740	0	0	0	-225	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
4	0	-0	828	0	0	0	-163	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
5	0	-0	823	0	0	0	-179	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
6	0	-0	779	0	0	0	-175	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
7	0	-0	764	0	0	0	-227	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
8	0	-0	804	0	0	0	-161	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
9	0	-0	789	0	0	0	-213	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
10	0	-0	745	0	0	0	-209	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
11	0	-0	740	0	0	0	-225	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
12	0	-0	828	0	0	0	-163	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
13	0	-0	823	0	0	0	-179	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
14	0	-0	779	0	0	0	-175	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
15	0	-0	764	0	0	0	-227	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
16	0	-0	804	0	0	0	-161	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
17	0	-0	789	0	0	0	-213	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
18	0	-0	560	0	0	0	-417	--	--	16.08	16.08	0.18	0.01	0.00	0.04	0.00	0.00	20.9
19	0	-0	1231	0	0	0	-214	--	--	16.08	16.08	0.18	0.00	0.01	0.08	0.00	0.00	20.9
20	0	-0	851	0	0	0	-465	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9
37	0	-0	381	0	0	0	-468	--	--	16.08	16.08	0.18	0.01	0.00	0.02	0.00	0.00	20.9
38	0	-0	1500	0	0	0	-130	--	--	16.08	16.08	0.18	0.00	0.01	0.09	0.00	0.00	20.9
39	0	-0	866	0	0	0	-549	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	1019	0	0	0	1098	--	--	16.08	16.08	0.00	0.02	0.01	0.06	0.00	0.00	20.9
2	26	-0	745	0	0	0	-209	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
3	26	-0	740	0	0	0	-225	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
4	26	-0	828	0	0	0	934	--	--	16.08	16.08	0.10	0.02	0.01	0.05	0.00	0.00	20.9
5	26	-0	823	0	0	0	912	--	--	16.08	16.08	0.10	0.02	0.01	0.05	0.00	0.00	20.9
6	26	-0	779	0	0	0	858	--	--	16.08	16.08	0.10	0.02	0.01	0.05	0.00	0.00	20.9

7	26	-0	764	0	0	0	-227	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
8	26	-0	804	0	0	0	905	--	--	16.08	16.08	0.10	0.02	0.01	0.05	0.00	0.00	20.9
9	26	-0	789	0	0	0	-213	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
10	26	-0	745	0	0	0	-209	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
11	26	-0	740	0	0	0	-225	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
12	26	-0	828	0	0	0	934	--	--	16.08	16.08	0.10	0.02	0.01	0.05	0.00	0.00	20.9
13	26	-0	823	0	0	0	912	--	--	16.08	16.08	0.10	0.02	0.01	0.05	0.00	0.00	20.9
14	26	-0	779	0	0	0	858	--	--	16.08	16.08	0.10	0.02	0.01	0.05	0.00	0.00	20.9
15	26	-0	764	0	0	0	-227	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
16	26	-0	804	0	0	0	905	--	--	16.08	16.08	0.10	0.02	0.01	0.05	0.00	0.00	20.9
17	26	-0	789	0	0	0	-213	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
18	26	-0	560	0	0	0	-417	--	--	16.08	16.08	0.18	0.01	0.00	0.04	0.00	0.00	20.9
19	26	-0	1231	0	0	0	1418	--	--	16.08	16.08	0.00	0.02	0.01	0.08	0.00	0.00	20.9
20	26	-0	851	0	0	0	-465	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9
37	26	-0	381	0	0	0	-468	--	--	16.08	16.08	0.18	0.01	0.00	0.02	0.00	0.00	20.9
38	26	-0	1500	0	0	0	1859	--	--	16.08	16.08	0.00	0.03	0.01	0.09	0.00	0.00	20.9
39	26	-0	866	0	0	0	-549	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	1019	0	0	0	271	--	--	16.08	16.08	0.00	0.00	0.01	0.06	0.00	0.00	20.9
2	51	-0	745	0	0	0	173	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
3	51	-0	740	0	0	0	155	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
4	51	-0	828	0	0	0	262	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
5	51	-0	823	0	0	0	244	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
6	51	-0	779	0	0	0	225	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
7	51	-0	764	0	0	0	165	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
8	51	-0	804	0	0	0	252	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
9	51	-0	789	0	0	0	192	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
10	51	-0	745	0	0	0	173	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
11	51	-0	740	0	0	0	155	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
12	51	-0	828	0	0	0	262	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
13	51	-0	823	0	0	0	244	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
14	51	-0	779	0	0	0	225	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
15	51	-0	764	0	0	0	165	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
16	51	-0	804	0	0	0	252	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
17	51	-0	789	0	0	0	192	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
18	51	-0	560	0	0	0	-417	--	--	16.08	16.08	0.18	0.01	0.00	0.04	0.00	0.00	20.9
19	51	-0	1231	0	0	0	419	--	--	16.08	16.08	0.00	0.01	0.01	0.08	0.00	0.00	20.9
20	51	-0	851	0	0	0	-465	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9
37	51	-0	381	0	0	0	-468	--	--	16.08	16.08	0.18	0.01	0.00	0.02	0.00	0.00	20.9
38	51	-0	1500	0	0	0	641	--	--	16.08	16.08	0.00	0.01	0.01	0.09	0.00	0.00	20.9
39	51	-0	866	0	0	0	-549	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 30 NI 1500 NF 1514 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	2092	0	0	0	-207	--	--	16.08	16.08	0.18	0.00	0.02	0.13	0.00	0.00	20.9
2	0	-0	1566	0	0	0	-181	--	--	16.08	16.08	0.29	0.00	0.01	0.10	0.00	0.00	20.9
3	0	-0	1564	0	0	0	-198	--	--	16.08	16.08	0.29	0.00	0.01	0.10	0.00	0.00	20.9
4	0	-0	1654	0	0	0	-121	--	--	16.08	16.08	0.29	0.00	0.01	0.10	0.00	0.00	20.9
5	0	-0	1652	0	0	0	-138	--	--	16.08	16.08	0.29	0.00	0.01	0.10	0.00	0.00	20.9
6	0	-0	1600	0	0	0	-140	--	--	16.08	16.08	0.29	0.00	0.01	0.10	0.00	0.00	20.9
7	0	-0	1592	0	0	0	-196	--	--	16.08	16.08	0.29	0.00	0.01	0.10	0.00	0.00	20.9
8	0	-0	1626	0	0	0	-122	--	--	16.08	16.08	0.29	0.00	0.01	0.10	0.00	0.00	20.9
9	0	-0	1618	0	0	0	-178	--	--	16.08	16.08	0.29	0.00	0.01	0.10	0.00	0.00	20.9
10	0	-0	1566	0	0	0	-181	--	--	16.08	16.08	0.29	0.00	0.01	0.10	0.00	0.00	20.9
11	0	-0	1564	0	0	0	-198	--	--	16.08	16.08	0.29	0.00	0.01	0.10	0.00	0.00	20.9
12	0	-0	1654	0	0	0	-121	--	--	16.08	16.08	0.29	0.00	0.01	0.10	0.00	0.00	20.9
13	0	-0	1652	0	0	0	-138	--	--	16.08	16.08	0.29	0.00	0.01	0.10	0.00	0.00	20.9
14	0	-0	1600	0	0	0	-140	--	--	16.08	16.08	0.29	0.00	0.01	0.10	0.00	0.00	20.9
15	0	-0	1592	0	0	0	-196	--	--	16.08	16.08	0.29	0.00	0.01	0.10	0.00	0.00	20.9
16	0	-0	1626	0	0	0	-122	--	--	16.08	16.08	0.29	0.00	0.01	0.10	0.00	0.00	20.9
17	0	-0	1618	0	0	0	-178	--	--	16.08	16.08	0.29	0.00	0.01	0.10	0.00	0.00	20.9
18	0	-0	1726	0	0	0	-461	--	--	16.08	16.08	0.18	0.01	0.01	0.11	0.00	0.00	20.9
19	0	-0	2433	0	0	0	-147	--	--	16.08	16.08	0.18	0.00	0.02	0.15	0.00	0.00	20.9
20	0	-0	2018	0	0	0	-461	--	--	16.08	16.08	0.18	0.01	0.02	0.13	0.00	0.00	20.9
37	0	-0	1502	0	0	0	-538	--	--	16.08	16.08	0.18	0.01	0.01	0.09	0.00	0.00	20.9
38	0	-0	2679	0	0	0	-14	--	--	16.08	16.08	0.18	0.00	0.02	0.17	0.00	0.00	20.9
39	0	-0	1988	0	0	0	-537	--	--	16.08	16.08	0.18	0.01	0.02	0.12	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	2092	0	0	0	2566	--	--	16.08	16.08	0.00	0.04	0.02	0.13	0.00	0.00	20.9
2	26	-0	1566	0	0	0	1895	--	--	16.08	16.08	0.10	0.03	0.01	0.10	0.00	0.00	20.9
3	26	-0	1564	0	0	0	1875	--	--	16.08	16.08	0.10	0.03	0.01	0.10	0.00	0.00	20.9
4	26	-0	1654	0	0	0	2072	--	--	16.08	16.08	0.10	0.04	0.01	0.10	0.00	0.00	20.9
5	26	-0	1652	0	0	0	2052	--	--	16.08	16.08	0.10	0.04	0.01	0.10	0.00	0.00	20.9
6	26	-0	1600	0	0	0	1981	--	--	16.08	16.08	0.10	0.04	0.01	0.10	0.00	0.00	20.9
7	26	-0	1592	0	0	0	1914	--	--	16.08	16.08	0.10	0.03	0.01	0.10	0.00	0.00	20.9
8	26	-0	1626	0	0	0	2033	--	--	16.08	16.08	0.10	0.04	0.01	0.10	0.00	0.00	20.9
9	26	-0	1618	0	0	0	1966	--	--	16.08	16.08	0.10	0.03	0.01	0.10	0.00	0.00	20.9
10	26	-0	1566	0	0	0	1895	--	--	16.08	16.08	0.10	0.03	0.01	0.10	0.00	0.00	20.9
11	26	-0	1564	0	0	0	1875	--	--	16.08	16.08	0.10	0.03	0.01	0.10	0.00	0.00	20.9
12	26	-0	1654	0	0	0	2072	--	--	16.08	16.08	0.10	0.04	0.01	0.10	0.00	0.00	20.9
13	26	-0	1652	0	0	0	2052	--	--	16.08	16.08	0.10	0.04	0.01	0.10	0.00	0.00	20.9
14	26	-0	1600	0	0	0	1981	--	--	16.08	16.08	0.10	0.04	0.01	0.10	0.00	0.00	20.9
15	26	-0	1592	0	0	0	1914	--	--	16.08	16.08	0.10	0.03	0.01	0.10	0.00	0.00	20.9
16	26	-0	1626	0	0	0	2033	--	--	16.08	16.08	0.10	0.04	0.01	0.10	0.00	0.00	20.9
17	26	-0	1618	0	0	0	1966	--	--	16.08	16.08	0.10	0.03	0.01	0.10	0.00	0.00	20.9
18	26	-0	1726	0	0	0	-461	--	--	16.08	16.08	0.18	0.01	0.01	0.11	0.00	0.00	20.9
19	26	-0	2433	0	0	0	3078	--	--	16.08	16.08	0.00	0.05	0.02	0.15	0.00	0.00	20.9
20	26	-0	2018	0	0	0	2214	--	--	16.08	16.08	0.00	0.04	0.02	0.13	0.00	0.00	20.9
37	26	-0	1502	0	0	0	-538	--	--	16.08	16.08	0.18	0.01	0.01	0.09	0.00	0.00	20.9
38	26	-0	2679	0	0	0	3537	--	--	16.08	16.08	0.00	0.06	0.02	0.17	0.00	0.00	20.9
39	26	-0	1988	0	0	0	-537	--	--	16.08	16.08	0.18	0.01	0.02	0.12	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	2092	0	0	0	867	--	--	16.08	16.08	0.00	0.01	0.02	0.13	0.00	0.00	20.9
2	51	-0	1566	0	0	0	624	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9

3	51	-0	1564	0	0	0	605	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
4	51	-0	1654	0	0	0	729	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
5	51	-0	1652	0	0	0	711	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
6	51	-0	1600	0	0	0	681	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
7	51	-0	1592	0	0	0	621	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
8	51	-0	1626	0	0	0	713	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
9	51	-0	1618	0	0	0	653	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
10	51	-0	1566	0	0	0	624	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
11	51	-0	1564	0	0	0	605	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
12	51	-0	1654	0	0	0	729	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
13	51	-0	1652	0	0	0	711	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
14	51	-0	1600	0	0	0	681	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
15	51	-0	1592	0	0	0	621	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
16	51	-0	1626	0	0	0	713	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
17	51	-0	1618	0	0	0	653	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
18	51	-0	1726	0	0	0	425	--	--	16.08	16.08	0.00	0.01	0.01	0.11	0.00	0.00	20.9
19	51	-0	2433	0	0	0	1102	--	--	16.08	16.08	0.00	0.02	0.02	0.15	0.00	0.00	20.9
20	51	-0	2018	0	0	0	576	--	--	16.08	16.08	0.00	0.01	0.02	0.13	0.00	0.00	20.9
37	51	-0	1502	0	0	0	233	--	--	16.08	16.08	0.00	0.00	0.01	0.09	0.00	0.00	20.9
38	51	-0	2679	0	0	0	1362	--	--	16.08	16.08	0.00	0.02	0.02	0.17	0.00	0.00	20.9
39	51	-0	1988	0	0	0	484	--	--	16.08	16.08	0.00	0.01	0.02	0.12	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 31 NI 1514 NF 1513 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	3291	0	0	0	72	--	--	16.08	16.08	0.00	0.00	0.03	0.21	0.00	0.00	20.9
2	0	-0	2485	0	0	0	27	--	--	16.08	16.08	0.10	0.00	0.02	0.16	0.00	0.00	20.9
3	0	-0	2485	0	0	0	9	--	--	16.08	16.08	0.10	0.00	0.02	0.16	0.00	0.00	20.9
4	0	-0	2578	0	0	0	101	--	--	16.08	16.08	0.10	0.00	0.02	0.16	0.00	0.00	20.9
5	0	-0	2578	0	0	0	84	--	--	16.08	16.08	0.10	0.00	0.02	0.16	0.00	0.00	20.9
6	0	-0	2517	0	0	0	74	--	--	16.08	16.08	0.10	0.00	0.02	0.16	0.00	0.00	20.9
7	0	-0	2517	0	0	0	15	--	--	16.08	16.08	0.10	0.00	0.02	0.16	0.00	0.00	20.9
8	0	-0	2545	0	0	0	96	--	--	16.08	16.08	0.10	0.00	0.02	0.16	0.00	0.00	20.9
9	0	-0	2545	0	0	0	37	--	--	16.08	16.08	0.10	0.00	0.02	0.16	0.00	0.00	20.9
10	0	-0	2485	0	0	0	27	--	--	16.08	16.08	0.10	0.00	0.02	0.16	0.00	0.00	20.9
11	0	-0	2485	0	0	0	9	--	--	16.08	16.08	0.10	0.00	0.02	0.16	0.00	0.00	20.9
12	0	-0	2578	0	0	0	101	--	--	16.08	16.08	0.10	0.00	0.02	0.16	0.00	0.00	20.9
13	0	-0	2578	0	0	0	84	--	--	16.08	16.08	0.10	0.00	0.02	0.16	0.00	0.00	20.9
14	0	-0	2517	0	0	0	74	--	--	16.08	16.08	0.10	0.00	0.02	0.16	0.00	0.00	20.9
15	0	-0	2517	0	0	0	15	--	--	16.08	16.08	0.10	0.00	0.02	0.16	0.00	0.00	20.9
16	0	-0	2545	0	0	0	96	--	--	16.08	16.08	0.10	0.00	0.02	0.16	0.00	0.00	20.9
17	0	-0	2545	0	0	0	37	--	--	16.08	16.08	0.10	0.00	0.02	0.16	0.00	0.00	20.9
18	0	-0	3046	0	0	0	-247	--	--	16.08	16.08	0.18	0.00	0.03	0.19	0.00	0.00	20.9
19	0	-0	3770	0	0	0	179	--	--	16.08	16.08	0.00	0.00	0.03	0.24	0.00	0.00	20.9
20	0	-0	3328	0	0	0	-202	--	--	16.08	16.08	0.18	0.00	0.03	0.21	0.00	0.00	20.9
37	0	-0	2775	0	0	0	-357	--	--	16.08	16.08	0.18	0.01	0.02	0.17	0.00	0.00	20.9
38	0	-0	3982	0	0	0	353	--	--	16.08	16.08	0.00	0.01	0.03	0.25	0.00	0.00	20.9
39	0	-0	3246	0	0	0	-283	--	--	16.08	16.08	0.18	0.00	0.03	0.20	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	3291	0	0	0	4434	--	--	16.08	16.08	0.00	0.08	0.03	0.21	0.00	0.00	20.9
2	26	-0	2485	0	0	0	3321	--	--	16.08	16.08	0.10	0.06	0.02	0.16	0.00	0.00	20.9
3	26	-0	2485	0	0	0	3303	--	--	16.08	16.08	0.10	0.06	0.02	0.16	0.00	0.00	20.9
4	26	-0	2578	0	0	0	3518	--	--	16.08	16.08	0.10	0.06	0.02	0.16	0.00	0.00	20.9
5	26	-0	2578	0	0	0	3501	--	--	16.08	16.08	0.10	0.06	0.02	0.16	0.00	0.00	20.9
6	26	-0	2517	0	0	0	3410	--	--	16.08	16.08	0.10	0.06	0.02	0.16	0.00	0.00	20.9
7	26	-0	2517	0	0	0	3351	--	--	16.08	16.08	0.10	0.06	0.02	0.16	0.00	0.00	20.9
8	26	-0	2545	0	0	0	3469	--	--	16.08	16.08	0.10	0.06	0.02	0.16	0.00	0.00	20.9
9	26	-0	2545	0	0	0	3410	--	--	16.08	16.08	0.10	0.06	0.02	0.16	0.00	0.00	20.9
10	26	-0	2485	0	0	0	3321	--	--	16.08	16.08	0.10	0.06	0.02	0.16	0.00	0.00	20.9
11	26	-0	2485	0	0	0	3303	--	--	16.08	16.08	0.10	0.06	0.02	0.16	0.00	0.00	20.9
12	26	-0	2578	0	0	0	3518	--	--	16.08	16.08	0.10	0.06	0.02	0.16	0.00	0.00	20.9
13	26	-0	2578	0	0	0	3501	--	--	16.08	16.08	0.10	0.06	0.02	0.16	0.00	0.00	20.9
14	26	-0	2517	0	0	0	3410	--	--	16.08	16.08	0.10	0.06	0.02	0.16	0.00	0.00	20.9
15	26	-0	2517	0	0	0	3351	--	--	16.08	16.08	0.10	0.06	0.02	0.16	0.00	0.00	20.9
16	26	-0	2545	0	0	0	3469	--	--	16.08	16.08	0.10	0.06	0.02	0.16	0.00	0.00	20.9
17	26	-0	2545	0	0	0	3410	--	--	16.08	16.08	0.10	0.06	0.02	0.16	0.00	0.00	20.9
18	26	-0	3046	0	0	0	3791	--	--	16.08	16.08	0.00	0.06	0.03	0.19	0.00	0.00	20.9
19	26	-0	3770	0	0	0	5176	--	--	16.08	16.08	0.00	0.09	0.03	0.24	0.00	0.00	20.9
20	26	-0	3328	0	0	0	4209	--	--	16.08	16.08	0.00	0.07	0.03	0.21	0.00	0.00	20.9
37	26	-0	2775	0	0	0	3322	--	--	16.08	16.08	0.00	0.06	0.02	0.17	0.00	0.00	20.9
38	26	-0	3982	0	0	0	5631	--	--	16.08	16.08	0.00	0.10	0.03	0.25	0.00	0.00	20.9
39	26	-0	3246	0	0	0	4020	--	--	16.08	16.08	0.00	0.07	0.03	0.20	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	3291	0	0	0	1762	--	--	16.08	16.08	0.00	0.03	0.03	0.21	0.00	0.00	20.9
2	51	-0	2485	0	0	0	1303	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
3	51	-0	2485	0	0	0	1285	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
4	51	-0	2578	0	0	0	1425	--	--	16.08	16.08	0.10	0.03	0.02	0.16	0.00	0.00	20.9
5	51	-0	2578	0	0	0	1408	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
6	51	-0	2517	0	0	0	1367	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
7	51	-0	2517	0	0	0	1307	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
8	51	-0	2545	0	0	0	1403	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
9	51	-0	2545	0	0	0	1344	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
10	51	-0	2485	0	0	0	1303	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
11	51	-0	2485	0	0	0	1285	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
12	51	-0	2578	0	0	0	1425	--	--	16.08	16.08	0.10	0.03	0.02	0.16	0.00	0.00	20.9
13	51	-0	2578	0	0	0	1408	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
14	51	-0	2517	0	0	0	1367	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
15	51	-0	2517	0	0	0	1307	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
16	51	-0	2545	0	0	0	1403	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
17	51	-0	2545	0	0	0	1344	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
18	51	-0	3046	0	0	0	1318	--	--	16.08	16.08	0.00	0.02	0.03	0.19	0.00	0.00	20.9
19	51	-0	3770	0	0	0	2115	--	--	16.08	16.08	0.00	0.04	0.03	0.24	0.00	0.00	20.9
20	51	-0	3328	0	0	0	1507	--	--	16.08	16.08	0.00	0.03	0.03	0.21	0.00	0.00	20.9
37	51	-0	2775	0	0	0	1069	--	--	16.08	16.08	0.00	0.02	0.02	0.17	0.00	0.00	20.9
38	51	-0	3982	0	0	0	2398	--	--	16.08	16.08	0.00	0.04	0.03	0.25	0.00	0.00	20.9
39	51	-0	3246	0	0	0	1384	--	--	16.08	16.08	0.00	0.02	0.03	0.20	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 32 NI 1513 NF 1530 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	4052	0	0	0	533	--	--	16.08	16.08	0.00	0.01	0.03	0.25	0.00	0.00	20.9
2	0	-0	3070	0	0	0	375	--	--	16.08	16.08	0.10	0.01	0.03	0.19	0.00	0.00	20.9
3	0	-0	3071	0	0	0	356	--	--	16.08	16.08	0.10	0.01	0.03	0.19	0.00	0.00	20.9
4	0	-0	3163	0	0	0	464	--	--	16.08	16.08	0.10	0.01	0.03	0.20	0.00	0.00	20.9
5	0	-0	3164	0	0	0	445	--	--	16.08	16.08	0.10	0.01	0.03	0.20	0.00	0.00	20.9
6	0	-0	3101	0	0	0	427	--	--	16.08	16.08	0.10	0.01	0.03	0.19	0.00	0.00	20.9
7	0	-0	3105	0	0	0	366	--	--	16.08	16.08	0.10	0.01	0.03	0.19	0.00	0.00	20.9
8	0	-0	3129	0	0	0	454	--	--	16.08	16.08	0.10	0.01	0.03	0.20	0.00	0.00	20.9
9	0	-0	3133	0	0	0	393	--	--	16.08	16.08	0.10	0.01	0.03	0.20	0.00	0.00	20.9
10	0	-0	3070	0	0	0	375	--	--	16.08	16.08	0.10	0.01	0.03	0.19	0.00	0.00	20.9
11	0	-0	3071	0	0	0	356	--	--	16.08	16.08	0.10	0.01	0.03	0.19	0.00	0.00	20.9
12	0	-0	3163	0	0	0	464	--	--	16.08	16.08	0.10	0.01	0.03	0.20	0.00	0.00	20.9
13	0	-0	3164	0	0	0	445	--	--	16.08	16.08	0.10	0.01	0.03	0.20	0.00	0.00	20.9
14	0	-0	3101	0	0	0	427	--	--	16.08	16.08	0.10	0.01	0.03	0.19	0.00	0.00	20.9
15	0	-0	3105	0	0	0	366	--	--	16.08	16.08	0.10	0.01	0.03	0.19	0.00	0.00	20.9
16	0	-0	3129	0	0	0	454	--	--	16.08	16.08	0.10	0.01	0.03	0.20	0.00	0.00	20.9
17	0	-0	3133	0	0	0	393	--	--	16.08	16.08	0.10	0.01	0.03	0.20	0.00	0.00	20.9
18	0	-0	3935	0	0	0	177	--	--	16.08	16.08	0.00	0.00	0.03	0.25	0.00	0.00	20.9
19	0	-0	4567	0	0	0	701	--	--	16.08	16.08	0.00	0.01	0.04	0.29	0.00	0.00	20.9
20	0	-0	4156	0	0	0	254	--	--	16.08	16.08	0.00	0.00	0.03	0.26	0.00	0.00	20.9
37	0	-0	3670	0	0	0	32	--	--	16.08	16.08	0.00	0.00	0.03	0.23	0.00	0.00	20.9
38	0	-0	4723	0	0	0	905	--	--	16.08	16.08	0.00	0.02	0.04	0.30	0.00	0.00	20.9
39	0	-0	4039	0	0	0	161	--	--	16.08	16.08	0.00	0.00	0.03	0.25	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	26	-0	4052	0	0	0	5905	--	--	16.08	16.08	0.00	0.10	0.03	0.25	0.00	0.00	20.9
2	26	-0	3070	0	0	0	4444	--	--	16.08	16.08	0.10	0.08	0.03	0.19	0.00	0.00	20.9
3	26	-0	3071	0	0	0	4427	--	--	16.08	16.08	0.10	0.08	0.03	0.19	0.00	0.00	20.9
4	26	-0	3163	0	0	0	4656	--	--	16.08	16.08	0.10	0.08	0.03	0.20	0.00	0.00	20.9
5	26	-0	3164	0	0	0	4640	--	--	16.08	16.08	0.10	0.08	0.03	0.20	0.00	0.00	20.9
6	26	-0	3101	0	0	0	4538	--	--	16.08	16.08	0.10	0.08	0.03	0.19	0.00	0.00	20.9
7	26	-0	3105	0	0	0	4482	--	--	16.08	16.08	0.10	0.08	0.03	0.19	0.00	0.00	20.9
8	26	-0	3129	0	0	0	4602	--	--	16.08	16.08	0.10	0.08	0.03	0.20	0.00	0.00	20.9
9	26	-0	3133	0	0	0	4546	--	--	16.08	16.08	0.10	0.08	0.03	0.20	0.00	0.00	20.9
10	26	-0	3070	0	0	0	4444	--	--	16.08	16.08	0.10	0.08	0.03	0.19	0.00	0.00	20.9
11	26	-0	3071	0	0	0	4427	--	--	16.08	16.08	0.10	0.08	0.03	0.19	0.00	0.00	20.9
12	26	-0	3163	0	0	0	4656	--	--	16.08	16.08	0.10	0.08	0.03	0.20	0.00	0.00	20.9
13	26	-0	3164	0	0	0	4640	--	--	16.08	16.08	0.10	0.08	0.03	0.20	0.00	0.00	20.9
14	26	-0	3101	0	0	0	4538	--	--	16.08	16.08	0.10	0.08	0.03	0.19	0.00	0.00	20.9
15	26	-0	3105	0	0	0	4482	--	--	16.08	16.08	0.10	0.08	0.03	0.19	0.00	0.00	20.9
16	26	-0	3129	0	0	0	4602	--	--	16.08	16.08	0.10	0.08	0.03	0.20	0.00	0.00	20.9
17	26	-0	3133	0	0	0	4546	--	--	16.08	16.08	0.10	0.08	0.03	0.20	0.00	0.00	20.9
18	26	-0	3935	0	0	0	5393	--	--	16.08	16.08	0.00	0.09	0.03	0.25	0.00	0.00	20.9
19	26	-0	4567	0	0	0	6755	--	--	16.08	16.08	0.00	0.12	0.04	0.29	0.00	0.00	20.9
20	26	-0	4156	0	0	0	5763	--	--	16.08	16.08	0.00	0.10	0.03	0.26	0.00	0.00	20.9
37	26	-0	3670	0	0	0	4897	--	--	16.08	16.08	0.00	0.08	0.03	0.23	0.00	0.00	20.9
38	26	-0	4723	0	0	0	7166	--	--	16.08	16.08	0.00	0.12	0.04	0.30	0.00	0.00	20.9
39	26	-0	4039	0	0	0	5515	--	--	16.08	16.08	0.00	0.09	0.03	0.25	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	51	-0	4052	0	0	0	2615	--	--	16.08	16.08	0.00	0.04	0.03	0.25	0.00	0.00	20.9
2	51	-0	3070	0	0	0	1952	--	--	16.08	16.08	0.10	0.03	0.03	0.19	0.00	0.00	20.9
3	51	-0	3071	0	0	0	1934	--	--	16.08	16.08	0.10	0.03	0.03	0.19	0.00	0.00	20.9
4	51	-0	3163	0	0	0	2088	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
5	51	-0	3164	0	0	0	2071	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
6	51	-0	3101	0	0	0	2020	--	--	16.08	16.08	0.10	0.04	0.03	0.19	0.00	0.00	20.9
7	51	-0	3105	0	0	0	1961	--	--	16.08	16.08	0.10	0.03	0.03	0.19	0.00	0.00	20.9
8	51	-0	3129	0	0	0	2061	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
9	51	-0	3133	0	0	0	2002	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
10	51	-0	3070	0	0	0	1952	--	--	16.08	16.08	0.10	0.03	0.03	0.19	0.00	0.00	20.9
11	51	-0	3071	0	0	0	1934	--	--	16.08	16.08	0.10	0.03	0.03	0.19	0.00	0.00	20.9
12	51	-0	3163	0	0	0	2088	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
13	51	-0	3164	0	0	0	2071	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
14	51	-0	3101	0	0	0	2020	--	--	16.08	16.08	0.10	0.04	0.03	0.19	0.00	0.00	20.9
15	51	-0	3105	0	0	0	1961	--	--	16.08	16.08	0.10	0.03	0.03	0.19	0.00	0.00	20.9
16	51	-0	3129	0	0	0	2061	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
17	51	-0	3133	0	0	0	2002	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
18	51	-0	3935	0	0	0	2198	--	--	16.08	16.08	0.00	0.04	0.03	0.25	0.00	0.00	20.9
19	51	-0	4567	0	0	0	3047	--	--	16.08	16.08	0.00	0.05	0.04	0.29	0.00	0.00	20.9
20	51	-0	4156	0	0	0	2389	--	--	16.08	16.08	0.00	0.04	0.03	0.26	0.00	0.00	20.9
37	51	-0	3670	0	0	0	1917	--	--	16.08	16.08	0.00	0.03	0.03	0.23	0.00	0.00	20.9
38	51	-0	4723	0	0	0	3332	--	--	16.08	16.08	0.00	0.06	0.04	0.30	0.00	0.00	20.9
39	51	-0	4039	0	0	0	2236	--	--	16.08	16.08	0.00	0.04	0.03	0.25	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 33 NI 1530 NF 1540 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	3568	0	0	0	1428	--	--	16.08	16.08	0.00	0.02	0.03	0.22	0.00	0.00	20.9
2	0	-0	2697	0	0	0	1054	--	--	16.08	16.08	0.10	0.02	0.02	0.17	0.00	0.00	20.9
3	0	-0	2699	0	0	0	1036	--	--	16.08	16.08	0.10	0.02	0.02	0.17	0.00	0.00	20.9
4	0	-0	2791	0	0	0	1161	--	--	16.08	16.08	0.10	0.02	0.02	0.18	0.00	0.00	20.9
5	0	-0	2793	0	0	0	1143	--	--	16.08	16.08	0.10	0.02	0.02	0.18	0.00	0.00	20.9
6	0	-0	2728	0	0	0	1112	--	--	16.08	16.08	0.10	0.02	0.02	0.17	0.00	0.00	20.9
7	0	-0	2734	0	0	0	1053	--	--	16.08	16.08	0.10	0.02	0.02	0.17	0.00	0.00	20.9
8	0	-0	2756	0	0	0	1145	--	--	16.08	16.08	0.10	0.02	0.02	0.17	0.00	0.00	20.9
9	0	-0	2762	0	0	0	1085	--	--	16.08	16.08	0.10	0.02	0.02	0.17	0.00	0.00	20.9
10	0	-0	2697	0	0	0	1054	--	--	16.08	16.08	0.10	0.02	0.02	0.17	0.00	0.00	20.9

11	0	-0	2699	0	0	0	1036	--	--	16.08	16.08	0.10	0.02	0.02	0.17	0.00	0.00	20.9
12	0	-0	2791	0	0	0	1161	--	--	16.08	16.08	0.10	0.02	0.02	0.18	0.00	0.00	20.9
13	0	-0	2793	0	0	0	1143	--	--	16.08	16.08	0.10	0.02	0.02	0.18	0.00	0.00	20.9
14	0	-0	2728	0	0	0	1112	--	--	16.08	16.08	0.10	0.02	0.02	0.17	0.00	0.00	20.9
15	0	-0	2734	0	0	0	1053	--	--	16.08	16.08	0.10	0.02	0.02	0.17	0.00	0.00	20.9
16	0	-0	2756	0	0	0	1145	--	--	16.08	16.08	0.10	0.02	0.02	0.17	0.00	0.00	20.9
17	0	-0	2762	0	0	0	1085	--	--	16.08	16.08	0.10	0.02	0.02	0.17	0.00	0.00	20.9
18	0	-0	3407	0	0	0	1050	--	--	16.08	16.08	0.00	0.02	0.03	0.21	0.00	0.00	20.9
19	0	-0	3945	0	0	0	1725	--	--	16.08	16.08	0.00	0.03	0.03	0.25	0.00	0.00	20.9
20	0	-0	3604	0	0	0	1183	--	--	16.08	16.08	0.00	0.02	0.03	0.23	0.00	0.00	20.9
37	0	-0	3202	0	0	0	840	--	--	16.08	16.08	0.00	0.01	0.03	0.20	0.00	0.00	20.9
38	0	-0	4098	0	0	0	1965	--	--	16.08	16.08	0.00	0.03	0.03	0.26	0.00	0.00	20.9
39	0	-0	3531	0	0	0	1062	--	--	16.08	16.08	0.00	0.02	0.03	0.22	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	3568	0	0	0	6158	--	--	16.08	16.08	0.00	0.10	0.03	0.22	0.00	0.00	20.9
2	26	-0	2697	0	0	0	4629	--	--	16.08	16.08	0.10	0.08	0.02	0.17	0.00	0.00	20.9
3	26	-0	2699	0	0	0	4614	--	--	16.08	16.08	0.10	0.08	0.02	0.17	0.00	0.00	20.9
4	26	-0	2791	0	0	0	4861	--	--	16.08	16.08	0.10	0.09	0.02	0.18	0.00	0.00	20.9
5	26	-0	2793	0	0	0	4846	--	--	16.08	16.08	0.10	0.09	0.02	0.18	0.00	0.00	20.9
6	26	-0	2728	0	0	0	4728	--	--	16.08	16.08	0.10	0.08	0.02	0.17	0.00	0.00	20.9
7	26	-0	2734	0	0	0	4677	--	--	16.08	16.08	0.10	0.08	0.02	0.17	0.00	0.00	20.9
8	26	-0	2756	0	0	0	4798	--	--	16.08	16.08	0.10	0.09	0.02	0.17	0.00	0.00	20.9
9	26	-0	2762	0	0	0	4746	--	--	16.08	16.08	0.10	0.08	0.02	0.17	0.00	0.00	20.9
10	26	-0	2697	0	0	0	4629	--	--	16.08	16.08	0.10	0.08	0.02	0.17	0.00	0.00	20.9
11	26	-0	2699	0	0	0	4614	--	--	16.08	16.08	0.10	0.08	0.02	0.17	0.00	0.00	20.9
12	26	-0	2791	0	0	0	4861	--	--	16.08	16.08	0.10	0.09	0.02	0.18	0.00	0.00	20.9
13	26	-0	2793	0	0	0	4846	--	--	16.08	16.08	0.10	0.09	0.02	0.18	0.00	0.00	20.9
14	26	-0	2728	0	0	0	4728	--	--	16.08	16.08	0.10	0.08	0.02	0.17	0.00	0.00	20.9
15	26	-0	2734	0	0	0	4677	--	--	16.08	16.08	0.10	0.08	0.02	0.17	0.00	0.00	20.9
16	26	-0	2756	0	0	0	4798	--	--	16.08	16.08	0.10	0.09	0.02	0.17	0.00	0.00	20.9
17	26	-0	2762	0	0	0	4746	--	--	16.08	16.08	0.10	0.08	0.02	0.17	0.00	0.00	20.9
18	26	-0	3407	0	0	0	5566	--	--	16.08	16.08	0.00	0.09	0.03	0.21	0.00	0.00	20.9
19	26	-0	3945	0	0	0	6954	--	--	16.08	16.08	0.00	0.12	0.03	0.25	0.00	0.00	20.9
20	26	-0	3604	0	0	0	5961	--	--	16.08	16.08	0.00	0.10	0.03	0.23	0.00	0.00	20.9
37	26	-0	3202	0	0	0	5084	--	--	16.08	16.08	0.00	0.09	0.03	0.20	0.00	0.00	20.9
38	26	-0	4098	0	0	0	7397	--	--	16.08	16.08	0.00	0.13	0.03	0.26	0.00	0.00	20.9
39	26	-0	3531	0	0	0	5742	--	--	16.08	16.08	0.00	0.10	0.03	0.22	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	3568	0	0	0	3261	--	--	16.08	16.08	0.00	0.06	0.03	0.22	0.00	0.00	20.9
2	51	-0	2697	0	0	0	2439	--	--	16.08	16.08	0.10	0.04	0.02	0.17	0.00	0.00	20.9
3	51	-0	2699	0	0	0	2422	--	--	16.08	16.08	0.10	0.04	0.02	0.17	0.00	0.00	20.9
4	51	-0	2791	0	0	0	2595	--	--	16.08	16.08	0.10	0.05	0.02	0.18	0.00	0.00	20.9
5	51	-0	2793	0	0	0	2578	--	--	16.08	16.08	0.10	0.05	0.02	0.18	0.00	0.00	20.9
6	51	-0	2728	0	0	0	2513	--	--	16.08	16.08	0.10	0.04	0.02	0.17	0.00	0.00	20.9
7	51	-0	2734	0	0	0	2457	--	--	16.08	16.08	0.10	0.04	0.02	0.17	0.00	0.00	20.9
8	51	-0	2756	0	0	0	2560	--	--	16.08	16.08	0.10	0.05	0.02	0.17	0.00	0.00	20.9
9	51	-0	2762	0	0	0	2504	--	--	16.08	16.08	0.10	0.04	0.02	0.17	0.00	0.00	20.9
10	51	-0	2697	0	0	0	2439	--	--	16.08	16.08	0.10	0.04	0.02	0.17	0.00	0.00	20.9
11	51	-0	2699	0	0	0	2422	--	--	16.08	16.08	0.10	0.04	0.02	0.17	0.00	0.00	20.9
12	51	-0	2791	0	0	0	2595	--	--	16.08	16.08	0.10	0.05	0.02	0.18	0.00	0.00	20.9
13	51	-0	2793	0	0	0	2578	--	--	16.08	16.08	0.10	0.05	0.02	0.18	0.00	0.00	20.9
14	51	-0	2728	0	0	0	2513	--	--	16.08	16.08	0.10	0.04	0.02	0.17	0.00	0.00	20.9
15	51	-0	2734	0	0	0	2457	--	--	16.08	16.08	0.10	0.04	0.02	0.17	0.00	0.00	20.9
16	51	-0	2756	0	0	0	2560	--	--	16.08	16.08	0.10	0.05	0.02	0.17	0.00	0.00	20.9
17	51	-0	2762	0	0	0	2504	--	--	16.08	16.08	0.10	0.04	0.02	0.17	0.00	0.00	20.9
18	51	-0	3407	0	0	0	2800	--	--	16.08	16.08	0.00	0.05	0.03	0.21	0.00	0.00	20.9
19	51	-0	3945	0	0	0	3751	--	--	16.08	16.08	0.00	0.06	0.03	0.25	0.00	0.00	20.9
20	51	-0	3604	0	0	0	3035	--	--	16.08	16.08	0.00	0.05	0.03	0.23	0.00	0.00	20.9
37	51	-0	3202	0	0	0	2484	--	--	16.08	16.08	0.00	0.04	0.03	0.20	0.00	0.00	20.9
38	51	-0	4098	0	0	0	4070	--	--	16.08	16.08	0.00	0.07	0.03	0.26	0.00	0.00	20.9
39	51	-0	3531	0	0	0	2875	--	--	16.08	16.08	0.00	0.05	0.03	0.22	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 34 NI 1540 NF 1497 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm

1	0	-0	-4847	0	0	0	3505	--	--	16.08	16.08	0.00	0.06	0.04	0.30	0.00	0.00	20.9
2	0	-0	-3779	0	0	0	2645	--	--	16.08	16.08	0.10	0.05	0.03	0.24	0.00	0.00	20.9
3	0	-0	-3792	0	0	0	2631	--	--	16.08	16.08	0.10	0.05	0.03	0.24	0.00	0.00	20.9
4	0	-0	-3665	0	0	0	2761	--	--	16.08	16.08	0.10	0.05	0.03	0.23	0.00	0.00	20.9
5	0	-0	-3678	0	0	0	2746	--	--	16.08	16.08	0.10	0.05	0.03	0.23	0.00	0.00	20.9
6	0	-0	-3724	0	0	0	2703	--	--	16.08	16.08	0.10	0.05	0.03	0.23	0.00	0.00	20.9
7	0	-0	-3767	0	0	0	2655	--	--	16.08	16.08	0.10	0.05	0.03	0.24	0.00	0.00	20.9
8	0	-0	-3690	0	0	0	2737	--	--	16.08	16.08	0.10	0.05	0.03	0.23	0.00	0.00	20.9
9	0	-0	-3733	0	0	0	2689	--	--	16.08	16.08	0.10	0.05	0.03	0.23	0.00	0.00	20.9
10	0	-0	-3779	0	0	0	2645	--	--	16.08	16.08	0.10	0.05	0.03	0.24	0.00	0.00	20.9
11	0	-0	-3792	0	0	0	2631	--	--	16.08	16.08	0.10	0.05	0.03	0.24	0.00	0.00	20.9
12	0	-0	-3665	0	0	0	2761	--	--	16.08	16.08	0.10	0.05	0.03	0.23	0.00	0.00	20.9
13	0	-0	-3678	0	0	0	2746	--	--	16.08	16.08	0.10	0.05	0.03	0.23	0.00	0.00	20.9
14	0	-0	-3724	0	0	0	2703	--	--	16.08	16.08	0.10	0.05	0.03	0.23	0.00	0.00	20.9
15	0	-0	-3767	0	0	0	2655	--	--	16.08	16.08	0.10	0.05	0.03	0.24	0.00	0.00	20.9
16	0	-0	-3690	0	0	0	2737	--	--	16.08	16.08	0.10	0.05	0.03	0.23	0.00	0.00	20.9
17	0	-0	-3733	0	0	0	2689	--	--	16.08	16.08	0.10	0.05	0.03	0.23	0.00	0.00	20.9
18	0	-0	-6015	0	0	0	3283	--	--	16.08	16.08	0.00	0.06	0.05	0.38	0.00	0.00	20.9
19	0	-0	-5686	0	0	0	4106	--	--	16.08	16.08	0.00	0.07	0.05	0.36	0.00	0.00	20.9
20	0	-0	-5792	0	0	0	3461	--	--	16.08	16.08	0.00	0.06	0.05	0.36	0.00	0.00	20.9
37	0	-0	-5804	0	0	0	2953	--	--	16.08	16.08	0.00	0.05	0.05	0.36	0.00	0.00	20.9
38	0	-0	-5256	0	0	0	4324	--	--	16.08	16.08	0.00	0.07	0.04	0.33	0.00	0.00	20.9
39	0	-0	-5433	0	0	0	3249	--	--	16.08	16.08	0.00	0.06	0.04	0.34	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	-4847	0	0	0	3505	--	--	16.08	16.08	0.00	0.06	0.04	0.30	0.00	0.00	20.9
2	26	-0	-3779	0	0	0	2645	--	--	16.08	16.08	0.10	0.05	0.03	0.24	0.00	0.00	20.9
3	26	-0	-3792	0	0	0	2631	--	--	16.08	16.08	0.10	0.05	0.03	0.24	0.00	0.00	20.9
4	26	-0	-3665	0	0	0	2761	--	--	16.08	16.08	0.10	0.05	0.03	0.23	0.00	0.00	20.9
5	26	-0	-3678	0	0	0	2746	--	--	16.08	16.08	0.10	0.05	0.03	0.23	0.00	0.00	20.9
6	26	-0	-3724	0	0	0	2703	--	--	16.08	16.08	0.10	0.05	0.03	0.23	0.00	0.00	20.9

7	26	-0	-3767	0	0	0	2655	--	--	16.08	16.08	0.10	0.05	0.03	0.24	0.00	0.00	20.9
8	26	-0	-3690	0	0	0	2737	--	--	16.08	16.08	0.10	0.05	0.03	0.23	0.00	0.00	20.9
9	26	-0	-3733	0	0	0	2689	--	--	16.08	16.08	0.10	0.05	0.03	0.23	0.00	0.00	20.9
10	26	-0	-3779	0	0	0	2645	--	--	16.08	16.08	0.10	0.05	0.03	0.24	0.00	0.00	20.9
11	26	-0	-3792	0	0	0	2631	--	--	16.08	16.08	0.10	0.05	0.03	0.24	0.00	0.00	20.9
12	26	-0	-3665	0	0	0	2761	--	--	16.08	16.08	0.10	0.05	0.03	0.23	0.00	0.00	20.9
13	26	-0	-3678	0	0	0	2746	--	--	16.08	16.08	0.10	0.05	0.03	0.23	0.00	0.00	20.9
14	26	-0	-3724	0	0	0	2703	--	--	16.08	16.08	0.10	0.05	0.03	0.23	0.00	0.00	20.9
15	26	-0	-3767	0	0	0	2655	--	--	16.08	16.08	0.10	0.05	0.03	0.24	0.00	0.00	20.9
16	26	-0	-3690	0	0	0	2737	--	--	16.08	16.08	0.10	0.05	0.03	0.23	0.00	0.00	20.9
17	26	-0	-3733	0	0	0	2689	--	--	16.08	16.08	0.10	0.05	0.03	0.23	0.00	0.00	20.9
18	26	-0	-6015	0	0	0	3283	--	--	16.08	16.08	0.00	0.06	0.05	0.38	0.00	0.00	20.9
19	26	-0	-5686	0	0	0	4106	--	--	16.08	16.08	0.00	0.07	0.05	0.36	0.00	0.00	20.9
20	26	-0	-5792	0	0	0	3461	--	--	16.08	16.08	0.00	0.06	0.05	0.36	0.00	0.00	20.9
37	26	-0	-5804	0	0	0	2953	--	--	16.08	16.08	0.00	0.05	0.05	0.36	0.00	0.00	20.9
38	26	-0	-5256	0	0	0	4324	--	--	16.08	16.08	0.00	0.07	0.04	0.33	0.00	0.00	20.9
39	26	-0	-5433	0	0	0	3249	--	--	16.08	16.08	0.00	0.06	0.04	0.34	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	-4847	0	0	0	1015	--	--	16.08	16.08	0.00	0.02	0.04	0.30	0.00	0.00	20.9
2	51	-0	-3779	0	0	0	705	--	--	16.08	16.08	0.10	0.01	0.03	0.24	0.00	0.00	20.9
3	51	-0	-3792	0	0	0	684	--	--	16.08	16.08	0.10	0.01	0.03	0.24	0.00	0.00	20.9
4	51	-0	-3665	0	0	0	879	--	--	16.08	16.08	0.10	0.02	0.03	0.23	0.00	0.00	20.9
5	51	-0	-3678	0	0	0	858	--	--	16.08	16.08	0.10	0.02	0.03	0.23	0.00	0.00	20.9
6	51	-0	-3724	0	0	0	790	--	--	16.08	16.08	0.10	0.01	0.03	0.23	0.00	0.00	20.9
7	51	-0	-3767	0	0	0	720	--	--	16.08	16.08	0.10	0.01	0.03	0.24	0.00	0.00	20.9
8	51	-0	-3690	0	0	0	842	--	--	16.08	16.08	0.10	0.01	0.03	0.23	0.00	0.00	20.9
9	51	-0	-3733	0	0	0	772	--	--	16.08	16.08	0.10	0.01	0.03	0.23	0.00	0.00	20.9
10	51	-0	-3779	0	0	0	705	--	--	16.08	16.08	0.10	0.01	0.03	0.24	0.00	0.00	20.9
11	51	-0	-3792	0	0	0	684	--	--	16.08	16.08	0.10	0.01	0.03	0.24	0.00	0.00	20.9
12	51	-0	-3665	0	0	0	879	--	--	16.08	16.08	0.10	0.02	0.03	0.23	0.00	0.00	20.9
13	51	-0	-3678	0	0	0	858	--	--	16.08	16.08	0.10	0.02	0.03	0.23	0.00	0.00	20.9
14	51	-0	-3724	0	0	0	790	--	--	16.08	16.08	0.10	0.01	0.03	0.23	0.00	0.00	20.9
15	51	-0	-3767	0	0	0	720	--	--	16.08	16.08	0.10	0.01	0.03	0.24	0.00	0.00	20.9
16	51	-0	-3690	0	0	0	842	--	--	16.08	16.08	0.10	0.01	0.03	0.23	0.00	0.00	20.9
17	51	-0	-3733	0	0	0	772	--	--	16.08	16.08	0.10	0.01	0.03	0.23	0.00	0.00	20.9
18	51	-0	-6015	0	0	0	194	--	--	16.08	16.08	0.00	0.00	0.05	0.38	0.00	0.00	20.9
19	51	-0	-5686	0	0	0	1186	--	--	16.08	16.08	0.00	0.02	0.05	0.36	0.00	0.00	20.9
20	51	-0	-5792	0	0	0	486	--	--	16.08	16.08	0.00	0.01	0.05	0.36	0.00	0.00	20.9
37	51	-0	-5804	0	0	0	-28	--	--	16.08	16.08	0.18	0.00	0.05	0.36	0.00	0.00	20.9
38	51	-0	-5256	0	0	0	1625	--	--	16.08	16.08	0.00	0.03	0.04	0.33	0.00	0.00	20.9
39	51	-0	-5433	0	0	0	458	--	--	16.08	16.08	0.00	0.01	0.04	0.34	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 35 NI 1497 NF 1507 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-5409	0	0	0	2612	--	--	16.08	16.08	0.00	0.04	0.04	0.34	0.00	0.00	20.9
2	0	-0	-4214	0	0	0	1948	--	--	16.08	16.08	0.10	0.03	0.03	0.26	0.00	0.00	20.9
3	0	-0	-4224	0	0	0	1931	--	--	16.08	16.08	0.10	0.03	0.03	0.26	0.00	0.00	20.9
4	0	-0	-4098	0	0	0	2087	--	--	16.08	16.08	0.10	0.04	0.03	0.26	0.00	0.00	20.9
5	0	-0	-4108	0	0	0	2070	--	--	16.08	16.08	0.10	0.04	0.03	0.26	0.00	0.00	20.9
6	0	-0	-4161	0	0	0	2017	--	--	16.08	16.08	0.10	0.04	0.03	0.26	0.00	0.00	20.9
7	0	-0	-4195	0	0	0	1959	--	--	16.08	16.08	0.10	0.03	0.03	0.26	0.00	0.00	20.9
8	0	-0	-4127	0	0	0	2059	--	--	16.08	16.08	0.10	0.04	0.03	0.26	0.00	0.00	20.9
9	0	-0	-4160	0	0	0	2001	--	--	16.08	16.08	0.10	0.04	0.03	0.26	0.00	0.00	20.9
10	0	-0	-4214	0	0	0	1948	--	--	16.08	16.08	0.10	0.03	0.03	0.26	0.00	0.00	20.9
11	0	-0	-4224	0	0	0	1931	--	--	16.08	16.08	0.10	0.03	0.03	0.26	0.00	0.00	20.9
12	0	-0	-4098	0	0	0	2087	--	--	16.08	16.08	0.10	0.04	0.03	0.26	0.00	0.00	20.9
13	0	-0	-4108	0	0	0	2070	--	--	16.08	16.08	0.10	0.04	0.03	0.26	0.00	0.00	20.9
14	0	-0	-4161	0	0	0	2017	--	--	16.08	16.08	0.10	0.04	0.03	0.26	0.00	0.00	20.9
15	0	-0	-4195	0	0	0	1959	--	--	16.08	16.08	0.10	0.03	0.03	0.26	0.00	0.00	20.9
16	0	-0	-4127	0	0	0	2059	--	--	16.08	16.08	0.10	0.04	0.03	0.26	0.00	0.00	20.9
17	0	-0	-4160	0	0	0	2001	--	--	16.08	16.08	0.10	0.04	0.03	0.26	0.00	0.00	20.9
18	0	-0	-6696	0	0	0	2166	--	--	16.08	16.08	0.00	0.04	0.06	0.42	0.00	0.00	20.9
19	0	-0	-6330	0	0	0	3066	--	--	16.08	16.08	0.00	0.05	0.05	0.40	0.00	0.00	20.9
20	0	-0	-6407	0	0	0	2385	--	--	16.08	16.08	0.00	0.04	0.05	0.40	0.00	0.00	20.9
37	0	-0	-6466	0	0	0	1869	--	--	16.08	16.08	0.00	0.03	0.05	0.41	0.00	0.00	20.9
38	0	-0	-5856	0	0	0	3369	--	--	16.08	16.08	0.00	0.06	0.05	0.37	0.00	0.00	20.9
39	0	-0	-5984	0	0	0	2235	--	--	16.08	16.08	0.00	0.04	0.05	0.38	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	-5409	0	0	0	2612	--	--	16.08	16.08	0.00	0.04	0.04	0.34	0.00	0.00	20.9
2	26	-0	-4214	0	0	0	1948	--	--	16.08	16.08	0.10	0.03	0.03	0.26	0.00	0.00	20.9
3	26	-0	-4224	0	0	0	1931	--	--	16.08	16.08	0.10	0.03	0.03	0.26	0.00	0.00	20.9
4	26	-0	-4098	0	0	0	2087	--	--	16.08	16.08	0.10	0.04	0.03	0.26	0.00	0.00	20.9
5	26	-0	-4108	0	0	0	2070	--	--	16.08	16.08	0.10	0.04	0.03	0.26	0.00	0.00	20.9
6	26	-0	-4161	0	0	0	2017	--	--	16.08	16.08	0.10	0.04	0.03	0.26	0.00	0.00	20.9
7	26	-0	-4195	0	0	0	1959	--	--	16.08	16.08	0.10	0.03	0.03	0.26	0.00	0.00	20.9
8	26	-0	-4127	0	0	0	2059	--	--	16.08	16.08	0.10	0.04	0.03	0.26	0.00	0.00	20.9
9	26	-0	-4160	0	0	0	2001	--	--	16.08	16.08	0.10	0.04	0.03	0.26	0.00	0.00	20.9
10	26	-0	-4214	0	0	0	1948	--	--	16.08	16.08	0.10	0.03	0.03	0.26	0.00	0.00	20.9
11	26	-0	-4224	0	0	0	1931	--	--	16.08	16.08	0.10	0.03	0.03	0.26	0.00	0.00	20.9
12	26	-0	-4098	0	0	0	2087	--	--	16.08	16.08	0.10	0.04	0.03	0.26	0.00	0.00	20.9
13	26	-0	-4108	0	0	0	2070	--	--	16.08	16.08	0.10	0.04	0.03	0.26	0.00	0.00	20.9
14	26	-0	-4161	0	0	0	2017	--	--	16.08	16.08	0.10	0.04	0.03	0.26	0.00	0.00	20.9
15	26	-0	-4195	0	0	0	1959	--	--	16.08	16.08	0.10	0.03	0.03	0.26	0.00	0.00	20.9
16	26	-0	-4127	0	0	0	2059	--	--	16.08	16.08	0.10	0.04	0.03	0.26	0.00	0.00	20.9
17	26	-0	-4160	0	0	0	2001	--	--	16.08	16.08	0.10	0.04	0.03	0.26	0.00	0.00	20.9
18	26	-0	-6696	0	0	0	2166	--	--	16.08	16.08	0.00	0.04	0.06	0.42	0.00	0.00	20.9
19	26	-0	-6330	0	0	0	3066	--	--	16.08	16.08	0.00	0.05	0.05	0.40	0.00	0.00	20.9
20	26	-0	-6407	0	0	0	2385	--	--	16.08	16.08	0.00	0.04	0.05	0.40	0.00	0.00	20.9
37	26	-0	-6466	0	0	0	1869	--	--	16.08	16.08	0.00	0.03	0.05	0.41	0.00	0.00	20.9
38	26	-0	-5856	0	0	0	3369	--	--	16.08	16.08	0.00	0.06	0.05	0.37	0.00	0.00	20.9
39	26	-0	-5984	0	0	0	2235	--	--	16.08	16.08	0.00	0.04	0.05	0.38	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	-5409	0	0	0	-167	--	--	16.08	16.08	0.18	0.00	0.04	0.34	0.00	0.00	20.9
2	51	-0	-4214	0	0	0	-216	--	--	16.08	16.08	0.29	0.00	0.03	0.26	0.00	0.00	20.9

3	51	-0	-4224	0	0	0	-239	--	--	16.08	16.08	0.29	0.00	0.03	0.26	0.00	0.00	20.9
4	51	-0	-4098	0	0	0	-18	--	--	16.08	16.08	0.29	0.00	0.03	0.26	0.00	0.00	20.9
5	51	-0	-4108	0	0	0	-40	--	--	16.08	16.08	0.29	0.00	0.03	0.26	0.00	0.00	20.9
6	51	-0	-4161	0	0	0	-121	--	--	16.08	16.08	0.29	0.00	0.03	0.26	0.00	0.00	20.9
7	51	-0	-4195	0	0	0	-196	--	--	16.08	16.08	0.29	0.00	0.03	0.26	0.00	0.00	20.9
8	51	-0	-4127	0	0	0	-61	--	--	16.08	16.08	0.29	0.00	0.03	0.26	0.00	0.00	20.9
9	51	-0	-4160	0	0	0	-136	--	--	16.08	16.08	0.29	0.00	0.03	0.26	0.00	0.00	20.9
10	51	-0	-4214	0	0	0	-216	--	--	16.08	16.08	0.29	0.00	0.03	0.26	0.00	0.00	20.9
11	51	-0	-4224	0	0	0	-239	--	--	16.08	16.08	0.29	0.00	0.03	0.26	0.00	0.00	20.9
12	51	-0	-4098	0	0	0	-18	--	--	16.08	16.08	0.29	0.00	0.03	0.26	0.00	0.00	20.9
13	51	-0	-4108	0	0	0	-40	--	--	16.08	16.08	0.29	0.00	0.03	0.26	0.00	0.00	20.9
14	51	-0	-4161	0	0	0	-121	--	--	16.08	16.08	0.29	0.00	0.03	0.26	0.00	0.00	20.9
15	51	-0	-4195	0	0	0	-196	--	--	16.08	16.08	0.29	0.00	0.03	0.26	0.00	0.00	20.9
16	51	-0	-4127	0	0	0	-61	--	--	16.08	16.08	0.29	0.00	0.03	0.26	0.00	0.00	20.9
17	51	-0	-4160	0	0	0	-136	--	--	16.08	16.08	0.29	0.00	0.03	0.26	0.00	0.00	20.9
18	51	-0	-6696	0	0	0	-1274	--	--	16.08	16.08	0.18	0.02	0.06	0.42	0.00	0.00	20.9
19	51	-0	-6330	0	0	0	-186	--	--	16.08	16.08	0.18	0.00	0.05	0.40	0.00	0.00	20.9
20	51	-0	-6407	0	0	0	-906	--	--	16.08	16.08	0.18	0.02	0.05	0.40	0.00	0.00	20.9
37	51	-0	-6466	0	0	0	-1452	--	--	16.08	16.08	0.18	0.02	0.05	0.41	0.00	0.00	20.9
38	51	-0	-5856	0	0	0	361	--	--	16.08	16.08	0.00	0.01	0.05	0.37	0.00	0.00	20.9
39	51	-0	-5984	0	0	0	-839	--	--	16.08	16.08	0.18	0.01	0.05	0.38	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 36 NI 1507 NF 1506 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-4837	0	0	0	1588	--	--	16.08	16.08	0.00	0.03	0.04	0.30	0.00	0.00	20.9
2	0	-0	-3780	0	0	0	1153	--	--	16.08	16.08	0.10	0.02	0.03	0.24	0.00	0.00	20.9
3	0	-0	-3785	0	0	0	1132	--	--	16.08	16.08	0.10	0.02	0.03	0.24	0.00	0.00	20.9
4	0	-0	-3657	0	0	0	1310	--	--	16.08	16.08	0.10	0.02	0.03	0.23	0.00	0.00	20.9
5	0	-0	-3662	0	0	0	1290	--	--	16.08	16.08	0.10	0.02	0.03	0.23	0.00	0.00	20.9
6	0	-0	-3731	0	0	0	1232	--	--	16.08	16.08	0.10	0.02	0.03	0.23	0.00	0.00	20.9
7	0	-0	-3747	0	0	0	1163	--	--	16.08	16.08	0.10	0.02	0.03	0.24	0.00	0.00	20.9
8	0	-0	-3694	0	0	0	1279	--	--	16.08	16.08	0.10	0.02	0.03	0.23	0.00	0.00	20.9
9	0	-0	-3710	0	0	0	1210	--	--	16.08	16.08	0.10	0.02	0.03	0.23	0.00	0.00	20.9
10	0	-0	-3780	0	0	0	1153	--	--	16.08	16.08	0.10	0.02	0.03	0.24	0.00	0.00	20.9
11	0	-0	-3785	0	0	0	1132	--	--	16.08	16.08	0.10	0.02	0.03	0.24	0.00	0.00	20.9
12	0	-0	-3657	0	0	0	1310	--	--	16.08	16.08	0.10	0.02	0.03	0.23	0.00	0.00	20.9
13	0	-0	-3662	0	0	0	1290	--	--	16.08	16.08	0.10	0.02	0.03	0.23	0.00	0.00	20.9
14	0	-0	-3731	0	0	0	1232	--	--	16.08	16.08	0.10	0.02	0.03	0.23	0.00	0.00	20.9
15	0	-0	-3747	0	0	0	1163	--	--	16.08	16.08	0.10	0.02	0.03	0.24	0.00	0.00	20.9
16	0	-0	-3694	0	0	0	1279	--	--	16.08	16.08	0.10	0.02	0.03	0.23	0.00	0.00	20.9
17	0	-0	-3710	0	0	0	1210	--	--	16.08	16.08	0.10	0.02	0.03	0.23	0.00	0.00	20.9
18	0	-0	-6165	0	0	0	947	--	--	16.08	16.08	0.00	0.02	0.05	0.39	0.00	0.00	20.9
19	0	-0	-5639	0	0	0	1846	--	--	16.08	16.08	0.00	0.03	0.05	0.35	0.00	0.00	20.9
20	0	-0	-5763	0	0	0	1172	--	--	16.08	16.08	0.00	0.02	0.05	0.36	0.00	0.00	20.9
37	0	-0	-6000	0	0	0	712	--	--	16.08	16.08	0.00	0.01	0.05	0.38	0.00	0.00	20.9
38	0	-0	-5123	0	0	0	2210	--	--	16.08	16.08	0.00	0.04	0.04	0.32	0.00	0.00	20.9
39	0	-0	-5330	0	0	0	1089	--	--	16.08	16.08	0.00	0.02	0.04	0.33	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	-4837	0	0	0	1588	--	--	16.08	16.08	0.00	0.03	0.04	0.30	0.00	0.00	20.9
2	26	-0	-3780	0	0	0	1153	--	--	16.08	16.08	0.10	0.02	0.03	0.24	0.00	0.00	20.9
3	26	-0	-3785	0	0	0	1132	--	--	16.08	16.08	0.10	0.02	0.03	0.24	0.00	0.00	20.9
4	26	-0	-3657	0	0	0	1310	--	--	16.08	16.08	0.10	0.02	0.03	0.23	0.00	0.00	20.9
5	26	-0	-3662	0	0	0	1290	--	--	16.08	16.08	0.10	0.02	0.03	0.23	0.00	0.00	20.9
6	26	-0	-3731	0	0	0	1232	--	--	16.08	16.08	0.10	0.02	0.03	0.23	0.00	0.00	20.9
7	26	-0	-3747	0	0	0	1163	--	--	16.08	16.08	0.10	0.02	0.03	0.24	0.00	0.00	20.9
8	26	-0	-3694	0	0	0	1279	--	--	16.08	16.08	0.10	0.02	0.03	0.23	0.00	0.00	20.9
9	26	-0	-3710	0	0	0	1210	--	--	16.08	16.08	0.10	0.02	0.03	0.23	0.00	0.00	20.9
10	26	-0	-3780	0	0	0	1153	--	--	16.08	16.08	0.10	0.02	0.03	0.24	0.00	0.00	20.9
11	26	-0	-3785	0	0	0	1132	--	--	16.08	16.08	0.10	0.02	0.03	0.24	0.00	0.00	20.9
12	26	-0	-3657	0	0	0	1310	--	--	16.08	16.08	0.10	0.02	0.03	0.23	0.00	0.00	20.9
13	26	-0	-3662	0	0	0	1290	--	--	16.08	16.08	0.10	0.02	0.03	0.23	0.00	0.00	20.9
14	26	-0	-3731	0	0	0	1232	--	--	16.08	16.08	0.10	0.02	0.03	0.23	0.00	0.00	20.9
15	26	-0	-3747	0	0	0	1163	--	--	16.08	16.08	0.10	0.02	0.03	0.24	0.00	0.00	20.9
16	26	-0	-3694	0	0	0	1279	--	--	16.08	16.08	0.10	0.02	0.03	0.23	0.00	0.00	20.9
17	26	-0	-3710	0	0	0	1210	--	--	16.08	16.08	0.10	0.02	0.03	0.23	0.00	0.00	20.9
18	26	-0	-6165	0	0	0	-2220	--	--	16.08	16.08	0.18	0.04	0.05	0.39	0.00	0.00	20.9
19	26	-0	-5639	0	0	0	1846	--	--	16.08	16.08	0.00	0.03	0.05	0.35	0.00	0.00	20.9
20	26	-0	-5763	0	0	0	-1787	--	--	16.08	16.08	0.18	0.03	0.05	0.36	0.00	0.00	20.9
37	26	-0	-6000	0	0	0	-2370	--	--	16.08	16.08	0.18	0.04	0.05	0.38	0.00	0.00	20.9
38	26	-0	-5123	0	0	0	2210	--	--	16.08	16.08	0.00	0.04	0.04	0.32	0.00	0.00	20.9
39	26	-0	-5330	0	0	0	-1649	--	--	16.08	16.08	0.18	0.03	0.04	0.33	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	-4837	0	0	0	-897	--	--	16.08	16.08	0.18	0.01	0.04	0.30	0.00	0.00	20.9
2	51	-0	-3780	0	0	0	-789	--	--	16.08	16.08	0.29	0.01	0.03	0.24	0.00	0.00	20.9
3	51	-0	-3785	0	0	0	-812	--	--	16.08	16.08	0.29	0.01	0.03	0.24	0.00	0.00	20.9
4	51	-0	-3657	0	0	0	-568	--	--	16.08	16.08	0.29	0.01	0.03	0.23	0.00	0.00	20.9
5	51	-0	-3662	0	0	0	-591	--	--	16.08	16.08	0.29	0.01	0.03	0.23	0.00	0.00	20.9
6	51	-0	-3731	0	0	0	-684	--	--	16.08	16.08	0.29	0.01	0.03	0.23	0.00	0.00	20.9
7	51	-0	-3747	0	0	0	-761	--	--	16.08	16.08	0.29	0.01	0.03	0.24	0.00	0.00	20.9
8	51	-0	-3694	0	0	0	-618	--	--	16.08	16.08	0.29	0.01	0.03	0.23	0.00	0.00	20.9
9	51	-0	-3710	0	0	0	-695	--	--	16.08	16.08	0.29	0.01	0.03	0.23	0.00	0.00	20.9
10	51	-0	-3780	0	0	0	-789	--	--	16.08	16.08	0.29	0.01	0.03	0.24	0.00	0.00	20.9
11	51	-0	-3785	0	0	0	-812	--	--	16.08	16.08	0.29	0.01	0.03	0.24	0.00	0.00	20.9
12	51	-0	-3657	0	0	0	-568	--	--	16.08	16.08	0.29	0.01	0.03	0.23	0.00	0.00	20.9
13	51	-0	-3662	0	0	0	-591	--	--	16.08	16.08	0.29	0.01	0.03	0.23	0.00	0.00	20.9
14	51	-0	-3731	0	0	0	-684	--	--	16.08	16.08	0.29	0.01	0.03	0.23	0.00	0.00	20.9
15	51	-0	-3747	0	0	0	-761	--	--	16.08	16.08	0.29	0.01	0.03	0.24	0.00	0.00	20.9
16	51	-0	-3694	0	0	0	-618	--	--	16.08	16.08	0.29	0.01	0.03	0.23	0.00	0.00	20.9
17	51	-0	-3710	0	0	0	-695	--	--	16.08	16.08	0.29	0.01	0.03	0.23	0.00	0.00	20.9
18	51	-0	-6165	0	0	0	-2220	--	--	16.08	16.08	0.18	0.04	0.05	0.39	0.00	0.00	20.9
19	51	-0	-5639	0	0	0	-1050	--	--	16.08	16.08	0.18	0.02	0.05	0.35	0.00	0.00	20.9
20	51	-0	-5763	0	0	0	-1787	--	--	16.08	16.08	0.18	0.03	0.05	0.36	0.00	0.00	20.9
37	51	-0	-6000	0	0	0	-2370	--	--	16.08	16.08	0.18	0.04	0.05	0.38	0.00	0.00	20.9
38	51	-0	-5123	0	0	0	-421	--	--	16.08	16.08	0.18	0.01	0.04	0.32	0.00	0.00	20.9
39	51	-0	-5330	0	0	0	-1649	--	--	16.08	16.08	0.18	0.03	0.04	0.33	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 37 NI 1506 NF 1505 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-3803	0	0	0	465	--	--	16.08	16.08	0.00	0.01	0.03	0.24	0.00	0.00	20.9
2	0	-0	-2989	0	0	0	280	--	--	16.08	16.08	0.10	0.00	0.02	0.19	0.00	0.00	20.9
3	0	-0	-2988	0	0	0	257	--	--	16.08	16.08	0.10	0.00	0.02	0.19	0.00	0.00	20.9
4	0	-0	-2862	0	0	0	458	--	--	16.08	16.08	0.10	0.01	0.02	0.18	0.00	0.00	20.9
5	0	-0	-2861	0	0	0	435	--	--	16.08	16.08	0.10	0.01	0.02	0.18	0.00	0.00	20.9
6	0	-0	-2945	0	0	0	369	--	--	16.08	16.08	0.10	0.01	0.02	0.18	0.00	0.00	20.9
7	0	-0	-2943	0	0	0	293	--	--	16.08	16.08	0.10	0.01	0.02	0.18	0.00	0.00	20.9
8	0	-0	-2907	0	0	0	422	--	--	16.08	16.08	0.10	0.01	0.02	0.18	0.00	0.00	20.9
9	0	-0	-2905	0	0	0	346	--	--	16.08	16.08	0.10	0.01	0.02	0.18	0.00	0.00	20.9
10	0	-0	-2989	0	0	0	280	--	--	16.08	16.08	0.10	0.00	0.02	0.19	0.00	0.00	20.9
11	0	-0	-2988	0	0	0	257	--	--	16.08	16.08	0.10	0.00	0.02	0.19	0.00	0.00	20.9
12	0	-0	-2862	0	0	0	458	--	--	16.08	16.08	0.10	0.01	0.02	0.18	0.00	0.00	20.9
13	0	-0	-2861	0	0	0	435	--	--	16.08	16.08	0.10	0.01	0.02	0.18	0.00	0.00	20.9
14	0	-0	-2945	0	0	0	369	--	--	16.08	16.08	0.10	0.01	0.02	0.18	0.00	0.00	20.9
15	0	-0	-2943	0	0	0	293	--	--	16.08	16.08	0.10	0.01	0.02	0.18	0.00	0.00	20.9
16	0	-0	-2907	0	0	0	422	--	--	16.08	16.08	0.10	0.01	0.02	0.18	0.00	0.00	20.9
17	0	-0	-2905	0	0	0	346	--	--	16.08	16.08	0.10	0.01	0.02	0.18	0.00	0.00	20.9
18	0	-0	-5068	0	0	0	-3027	--	--	16.08	16.08	0.18	0.05	0.04	0.32	0.00	0.00	20.9
19	0	-0	-4447	0	0	0	534	--	--	16.08	16.08	0.00	0.01	0.04	0.28	0.00	0.00	20.9
20	0	-0	-4599	0	0	0	-2510	--	--	16.08	16.08	0.18	0.04	0.04	0.29	0.00	0.00	20.9
37	0	-0	-4968	0	0	0	-3160	--	--	16.08	16.08	0.18	0.05	0.04	0.31	0.00	0.00	20.9
38	0	-0	-3934	0	0	0	988	--	--	16.08	16.08	0.00	0.02	0.03	0.25	0.00	0.00	20.9
39	0	-0	-4187	0	0	0	-2299	--	--	16.08	16.08	0.18	0.04	0.03	0.26	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	-3803	0	0	0	-1488	--	--	16.08	16.08	0.18	0.02	0.03	0.24	0.00	0.00	20.9
2	26	-0	-2989	0	0	0	-1255	--	--	16.08	16.08	0.29	0.02	0.02	0.19	0.00	0.00	20.9
3	26	-0	-2988	0	0	0	-1278	--	--	16.08	16.08	0.29	0.02	0.02	0.19	0.00	0.00	20.9
4	26	-0	-2862	0	0	0	-1012	--	--	16.08	16.08	0.29	0.02	0.02	0.18	0.00	0.00	20.9
5	26	-0	-2861	0	0	0	-1034	--	--	16.08	16.08	0.29	0.02	0.02	0.18	0.00	0.00	20.9
6	26	-0	-2945	0	0	0	-1144	--	--	16.08	16.08	0.29	0.02	0.02	0.18	0.00	0.00	20.9
7	26	-0	-2943	0	0	0	-1219	--	--	16.08	16.08	0.29	0.02	0.02	0.18	0.00	0.00	20.9
8	26	-0	-2907	0	0	0	-1071	--	--	16.08	16.08	0.29	0.02	0.02	0.18	0.00	0.00	20.9
9	26	-0	-2905	0	0	0	-1146	--	--	16.08	16.08	0.29	0.02	0.02	0.18	0.00	0.00	20.9
10	26	-0	-2989	0	0	0	-1255	--	--	16.08	16.08	0.29	0.02	0.02	0.19	0.00	0.00	20.9
11	26	-0	-2988	0	0	0	-1278	--	--	16.08	16.08	0.29	0.02	0.02	0.19	0.00	0.00	20.9
12	26	-0	-2862	0	0	0	-1012	--	--	16.08	16.08	0.29	0.02	0.02	0.18	0.00	0.00	20.9
13	26	-0	-2861	0	0	0	-1034	--	--	16.08	16.08	0.29	0.02	0.02	0.18	0.00	0.00	20.9
14	26	-0	-2945	0	0	0	-1144	--	--	16.08	16.08	0.29	0.02	0.02	0.18	0.00	0.00	20.9
15	26	-0	-2943	0	0	0	-1219	--	--	16.08	16.08	0.29	0.02	0.02	0.18	0.00	0.00	20.9
16	26	-0	-2907	0	0	0	-1071	--	--	16.08	16.08	0.29	0.02	0.02	0.18	0.00	0.00	20.9
17	26	-0	-2905	0	0	0	-1146	--	--	16.08	16.08	0.29	0.02	0.02	0.18	0.00	0.00	20.9
18	26	-0	-5068	0	0	0	-3027	--	--	16.08	16.08	0.18	0.05	0.04	0.32	0.00	0.00	20.9
19	26	-0	-4447	0	0	0	-1750	--	--	16.08	16.08	0.18	0.03	0.04	0.28	0.00	0.00	20.9
20	26	-0	-4599	0	0	0	-2510	--	--	16.08	16.08	0.18	0.04	0.04	0.29	0.00	0.00	20.9
37	26	-0	-4968	0	0	0	-3160	--	--	16.08	16.08	0.18	0.05	0.04	0.31	0.00	0.00	20.9
38	26	-0	-3934	0	0	0	-1033	--	--	16.08	16.08	0.18	0.02	0.03	0.25	0.00	0.00	20.9
39	26	-0	-4187	0	0	0	-2299	--	--	16.08	16.08	0.18	0.04	0.03	0.26	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	-3803	0	0	0	-1488	--	--	16.08	16.08	0.18	0.02	0.03	0.24	0.00	0.00	20.9
2	51	-0	-2989	0	0	0	-1255	--	--	16.08	16.08	0.29	0.02	0.02	0.19	0.00	0.00	20.9
3	51	-0	-2988	0	0	0	-1278	--	--	16.08	16.08	0.29	0.02	0.02	0.19	0.00	0.00	20.9
4	51	-0	-2862	0	0	0	-1012	--	--	16.08	16.08	0.29	0.02	0.02	0.18	0.00	0.00	20.9
5	51	-0	-2861	0	0	0	-1034	--	--	16.08	16.08	0.29	0.02	0.02	0.18	0.00	0.00	20.9
6	51	-0	-2945	0	0	0	-1144	--	--	16.08	16.08	0.29	0.02	0.02	0.18	0.00	0.00	20.9
7	51	-0	-2943	0	0	0	-1219	--	--	16.08	16.08	0.29	0.02	0.02	0.18	0.00	0.00	20.9
8	51	-0	-2907	0	0	0	-1071	--	--	16.08	16.08	0.29	0.02	0.02	0.18	0.00	0.00	20.9
9	51	-0	-2905	0	0	0	-1146	--	--	16.08	16.08	0.29	0.02	0.02	0.18	0.00	0.00	20.9
10	51	-0	-2989	0	0	0	-1255	--	--	16.08	16.08	0.29	0.02	0.02	0.19	0.00	0.00	20.9
11	51	-0	-2988	0	0	0	-1278	--	--	16.08	16.08	0.29	0.02	0.02	0.19	0.00	0.00	20.9
12	51	-0	-2862	0	0	0	-1012	--	--	16.08	16.08	0.29	0.02	0.02	0.18	0.00	0.00	20.9
13	51	-0	-2861	0	0	0	-1034	--	--	16.08	16.08	0.29	0.02	0.02	0.18	0.00	0.00	20.9
14	51	-0	-2945	0	0	0	-1144	--	--	16.08	16.08	0.29	0.02	0.02	0.18	0.00	0.00	20.9
15	51	-0	-2943	0	0	0	-1219	--	--	16.08	16.08	0.29	0.02	0.02	0.18	0.00	0.00	20.9
16	51	-0	-2907	0	0	0	-1071	--	--	16.08	16.08	0.29	0.02	0.02	0.18	0.00	0.00	20.9
17	51	-0	-2905	0	0	0	-1146	--	--	16.08	16.08	0.29	0.02	0.02	0.18	0.00	0.00	20.9
18	51	-0	-5068	0	0	0	-3027	--	--	16.08	16.08	0.18	0.05	0.04	0.32	0.00	0.00	20.9
19	51	-0	-4447	0	0	0	-1750	--	--	16.08	16.08	0.18	0.03	0.04	0.28	0.00	0.00	20.9
20	51	-0	-4599	0	0	0	-2510	--	--	16.08	16.08	0.18	0.04	0.04	0.29	0.00	0.00	20.9
37	51	-0	-4968	0	0	0	-3160	--	--	16.08	16.08	0.18	0.05	0.04	0.31	0.00	0.00	20.9
38	51	-0	-3934	0	0	0	-1033	--	--	16.08	16.08	0.18	0.02	0.03	0.25	0.00	0.00	20.9
39	51	-0	-4187	0	0	0	-2299	--	--	16.08	16.08	0.18	0.04	0.03	0.26	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 38 NI 1505 NF 1526 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-2915	0	0	0	-1893	--	--	16.08	16.08	0.18	0.03	0.02	0.18	0.00	0.00	20.9
2	0	-0	-2309	0	0	0	-1579	--	--	16.08	16.08	0.29	0.03	0.02	0.14	0.00	0.00	20.9
3	0	-0	-2302	0	0	0	-1599	--	--	16.08	16.08	0.29	0.03	0.02	0.14	0.00	0.00	20.9
4	0	-0	-2183	0	0	0	-1313	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
5	0	-0	-2176	0	0	0	-1333	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
6	0	-0	-2273	0	0	0	-1462	--	--	16.08	16.08	0.29	0.03	0.02	0.14	0.00	0.00	20.9
7	0	-0	-2251	0	0	0	-1530	--	--	16.08	16.08	0.29	0.03	0.02	0.14	0.00	0.00	20.9
8	0	-0	-2235	0	0	0	-1382	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
9	0	-0	-2213	0	0	0	-1450	--	--	16.08	16.08	0.29	0.03	0.02	0.14	0.00	0.00	20.9
10	0	-0	-2309	0	0	0	-1579	--	--	16.08	16.08	0.29	0.03	0.02	0.14	0.00	0.00	20.9

11	0	-0	-2302	0	0	0	-1599	--	--	16.08	16.08	0.29	0.03	0.02	0.14	0.00	0.00	20.9
12	0	-0	-2183	0	0	0	-1313	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
13	0	-0	-2176	0	0	0	-1333	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
14	0	-0	-2273	0	0	0	-1462	--	--	16.08	16.08	0.29	0.03	0.02	0.14	0.00	0.00	20.9
15	0	-0	-2251	0	0	0	-1530	--	--	16.08	16.08	0.29	0.03	0.02	0.14	0.00	0.00	20.9
16	0	-0	-2235	0	0	0	-1382	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
17	0	-0	-2213	0	0	0	-1450	--	--	16.08	16.08	0.29	0.03	0.02	0.14	0.00	0.00	20.9
18	0	-0	-4107	0	0	0	-3634	--	--	16.08	16.08	0.18	0.06	0.03	0.26	0.00	0.00	20.9
19	0	-0	-3437	0	0	0	-2233	--	--	16.08	16.08	0.18	0.04	0.03	0.22	0.00	0.00	20.9
20	0	-0	-3588	0	0	0	-3019	--	--	16.08	16.08	0.18	0.05	0.03	0.23	0.00	0.00	20.9
37	0	-0	-4054	0	0	0	-3763	--	--	16.08	16.08	0.18	0.06	0.03	0.25	0.00	0.00	20.9
38	0	-0	-2937	0	0	0	80	--	--	16.08	16.08	0.00	0.00	0.02	0.18	0.00	0.00	20.9
39	0	-0	-3189	0	0	0	-2738	--	--	16.08	16.08	0.18	0.05	0.03	0.20	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	-2915	0	0	0	-1893	--	--	16.08	16.08	0.18	0.03	0.02	0.18	0.00	0.00	20.9
2	26	-0	-2309	0	0	0	-1579	--	--	16.08	16.08	0.29	0.03	0.02	0.14	0.00	0.00	20.9
3	26	-0	-2302	0	0	0	-1599	--	--	16.08	16.08	0.29	0.03	0.02	0.14	0.00	0.00	20.9
4	26	-0	-2183	0	0	0	-1313	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
5	26	-0	-2176	0	0	0	-1333	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
6	26	-0	-2273	0	0	0	-1462	--	--	16.08	16.08	0.29	0.03	0.02	0.14	0.00	0.00	20.9
7	26	-0	-2251	0	0	0	-1530	--	--	16.08	16.08	0.29	0.03	0.02	0.14	0.00	0.00	20.9
8	26	-0	-2235	0	0	0	-1382	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
9	26	-0	-2213	0	0	0	-1450	--	--	16.08	16.08	0.29	0.03	0.02	0.14	0.00	0.00	20.9
10	26	-0	-2309	0	0	0	-1579	--	--	16.08	16.08	0.29	0.03	0.02	0.14	0.00	0.00	20.9
11	26	-0	-2302	0	0	0	-1599	--	--	16.08	16.08	0.29	0.03	0.02	0.14	0.00	0.00	20.9
12	26	-0	-2183	0	0	0	-1313	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
13	26	-0	-2176	0	0	0	-1333	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
14	26	-0	-2273	0	0	0	-1462	--	--	16.08	16.08	0.29	0.03	0.02	0.14	0.00	0.00	20.9
15	26	-0	-2251	0	0	0	-1530	--	--	16.08	16.08	0.29	0.03	0.02	0.14	0.00	0.00	20.9
16	26	-0	-2235	0	0	0	-1382	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
17	26	-0	-2213	0	0	0	-1450	--	--	16.08	16.08	0.29	0.03	0.02	0.14	0.00	0.00	20.9
18	26	-0	-4107	0	0	0	-3634	--	--	16.08	16.08	0.18	0.06	0.03	0.26	0.00	0.00	20.9
19	26	-0	-3437	0	0	0	-2233	--	--	16.08	16.08	0.18	0.04	0.03	0.22	0.00	0.00	20.9
20	26	-0	-3588	0	0	0	-3019	--	--	16.08	16.08	0.18	0.05	0.03	0.23	0.00	0.00	20.9
37	26	-0	-4054	0	0	0	-3763	--	--	16.08	16.08	0.18	0.06	0.03	0.25	0.00	0.00	20.9
38	26	-0	-2937	0	0	0	-1428	--	--	16.08	16.08	0.18	0.02	0.02	0.18	0.00	0.00	20.9
39	26	-0	-3189	0	0	0	-2738	--	--	16.08	16.08	0.18	0.05	0.03	0.20	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	-2915	0	0	0	-1893	--	--	16.08	16.08	0.18	0.03	0.02	0.18	0.00	0.00	20.9
2	51	-0	-2309	0	0	0	-1579	--	--	16.08	16.08	0.29	0.03	0.02	0.14	0.00	0.00	20.9
3	51	-0	-2302	0	0	0	-1599	--	--	16.08	16.08	0.29	0.03	0.02	0.14	0.00	0.00	20.9
4	51	-0	-2183	0	0	0	-1313	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
5	51	-0	-2176	0	0	0	-1333	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
6	51	-0	-2273	0	0	0	-1462	--	--	16.08	16.08	0.29	0.03	0.02	0.14	0.00	0.00	20.9
7	51	-0	-2251	0	0	0	-1530	--	--	16.08	16.08	0.29	0.03	0.02	0.14	0.00	0.00	20.9
8	51	-0	-2235	0	0	0	-1382	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
9	51	-0	-2213	0	0	0	-1450	--	--	16.08	16.08	0.29	0.03	0.02	0.14	0.00	0.00	20.9
10	51	-0	-2309	0	0	0	-1579	--	--	16.08	16.08	0.29	0.03	0.02	0.14	0.00	0.00	20.9
11	51	-0	-2302	0	0	0	-1599	--	--	16.08	16.08	0.29	0.03	0.02	0.14	0.00	0.00	20.9
12	51	-0	-2183	0	0	0	-1313	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
13	51	-0	-2176	0	0	0	-1333	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
14	51	-0	-2273	0	0	0	-1462	--	--	16.08	16.08	0.29	0.03	0.02	0.14	0.00	0.00	20.9
15	51	-0	-2251	0	0	0	-1530	--	--	16.08	16.08	0.29	0.03	0.02	0.14	0.00	0.00	20.9
16	51	-0	-2235	0	0	0	-1382	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
17	51	-0	-2213	0	0	0	-1450	--	--	16.08	16.08	0.29	0.03	0.02	0.14	0.00	0.00	20.9
18	51	-0	-4107	0	0	0	-3634	--	--	16.08	16.08	0.18	0.06	0.03	0.26	0.00	0.00	20.9
19	51	-0	-3437	0	0	0	-2233	--	--	16.08	16.08	0.18	0.04	0.03	0.22	0.00	0.00	20.9
20	51	-0	-3588	0	0	0	-3019	--	--	16.08	16.08	0.18	0.05	0.03	0.23	0.00	0.00	20.9
37	51	-0	-4054	0	0	0	-3763	--	--	16.08	16.08	0.18	0.06	0.03	0.25	0.00	0.00	20.9
38	51	-0	-2937	0	0	0	-1428	--	--	16.08	16.08	0.18	0.02	0.02	0.18	0.00	0.00	20.9
39	51	-0	-3189	0	0	0	-2738	--	--	16.08	16.08	0.18	0.05	0.03	0.20	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 39 NI 1526 NF 1525 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm

1	0	-0	-2132	0	0	0	-2147	--	--	16.08	16.08	0.18	0.04	0.02	0.13	0.00	0.00	20.9
2	0	-0	-1708	0	0	0	-1787	--	--	16.08	16.08	0.29	0.03	0.01	0.11	0.00	0.00	20.9
3	0	-0	-1695	0	0	0	-1804	--	--	16.08	16.08	0.29	0.03	0.01	0.11	0.00	0.00	20.9
4	0	-0	-1585	0	0	0	-1499	--	--	16.08	16.08	0.29	0.03	0.01	0.10	0.00	0.00	20.9
5	0	-0	-1572	0	0	0	-1516	--	--	16.08	16.08	0.29	0.03	0.01	0.10	0.00	0.00	20.9
6	0	-0	-1680	0	0	0	-1666	--	--	16.08	16.08	0.29	0.03	0.01	0.11	0.00	0.00	20.9
7	0	-0	-1637	0	0	0	-1723	--	--	16.08	16.08	0.29	0.03	0.01	0.10	0.00	0.00	20.9
8	0	-0	-1643	0	0	0	-1580	--	--	16.08	16.08	0.29	0.03	0.01	0.10	0.00	0.00	20.9
9	0	-0	-1600	0	0	0	-1637	--	--	16.08	16.08	0.29	0.03	0.01	0.10	0.00	0.00	20.9
10	0	-0	-1708	0	0	0	-1787	--	--	16.08	16.08	0.29	0.03	0.01	0.11	0.00	0.00	20.9
11	0	-0	-1695	0	0	0	-1804	--	--	16.08	16.08	0.29	0.03	0.01	0.11	0.00	0.00	20.9
12	0	-0	-1585	0	0	0	-1499	--	--	16.08	16.08	0.29	0.03	0.01	0.10	0.00	0.00	20.9
13	0	-0	-1572	0	0	0	-1516	--	--	16.08	16.08	0.29	0.03	0.01	0.10	0.00	0.00	20.9
14	0	-0	-1680	0	0	0	-1666	--	--	16.08	16.08	0.29	0.03	0.01	0.11	0.00	0.00	20.9
15	0	-0	-1637	0	0	0	-1723	--	--	16.08	16.08	0.29	0.03	0.01	0.10	0.00	0.00	20.9
16	0	-0	-1643	0	0	0	-1580	--	--	16.08	16.08	0.29	0.03	0.01	0.10	0.00	0.00	20.9
17	0	-0	-1600	0	0	0	-1637	--	--	16.08	16.08	0.29	0.03	0.01	0.10	0.00	0.00	20.9
18	0	-0	-3252	0	0	0	-4079	--	--	16.08	16.08	0.18	0.07	0.03	0.20	0.00	0.00	20.9
19	0	-0	-2545	0	0	0	-2544	--	--	16.08	16.08	0.18	0.04	0.02	0.16	0.00	0.00	20.9
20	0	-0	-2680	0	0	0	-3352	--	--	16.08	16.08	0.18	0.06	0.02	0.17	0.00	0.00	20.9
37	0	-0	-3239	0	0	0	-4212	--	--	16.08	16.08	0.18	0.07	0.03	0.20	0.00	0.00	20.9
38	0	-0	-2060	0	0	0	-1654	--	--	16.08	16.08	0.18	0.03	0.02	0.13	0.00	0.00	20.9
39	0	-0	-2285	0	0	0	-3001	--	--	16.08	16.08	0.18	0.05	0.02	0.14	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	-2132	0	0	0	-2147	--	--	16.08	16.08	0.18	0.04	0.02	0.13	0.00	0.00	20.9
2	26	-0	-1708	0	0	0	-1787	--	--	16.08	16.08	0.29	0.03	0.01	0.11	0.00	0.00	20.9
3	26	-0	-1695	0	0	0	-1804	--	--	16.08	16.08	0.29	0.03	0.01	0.11	0.00	0.00	20.9
4	26	-0	-1585	0	0	0	-1499	--	--	16.08	16.08	0.29	0.03	0.01	0.10	0.00	0.00	20.9
5	26	-0	-1572	0	0	0	-1516	--	--	16.08	16.08	0.29	0.03	0.01	0.10	0.00	0.00	20.9
6	26	-0	-1680	0	0	0	-1666	--	--	16.08	16.08	0.29	0.03	0.01	0.11	0.00	0.00	20.9

7	26	-0	-1637	0	0	0	-1723	--	--	16.08	16.08	0.29	0.03	0.01	0.10	0.00	0.00	20.9
8	26	-0	-1643	0	0	0	-1580	--	--	16.08	16.08	0.29	0.03	0.01	0.10	0.00	0.00	20.9
9	26	-0	-1600	0	0	0	-1637	--	--	16.08	16.08	0.29	0.03	0.01	0.10	0.00	0.00	20.9
10	26	-0	-1708	0	0	0	-1787	--	--	16.08	16.08	0.29	0.03	0.01	0.11	0.00	0.00	20.9
11	26	-0	-1695	0	0	0	-1804	--	--	16.08	16.08	0.29	0.03	0.01	0.11	0.00	0.00	20.9
12	26	-0	-1585	0	0	0	-1499	--	--	16.08	16.08	0.29	0.03	0.01	0.10	0.00	0.00	20.9
13	26	-0	-1572	0	0	0	-1516	--	--	16.08	16.08	0.29	0.03	0.01	0.10	0.00	0.00	20.9
14	26	-0	-1680	0	0	0	-1666	--	--	16.08	16.08	0.29	0.03	0.01	0.11	0.00	0.00	20.9
15	26	-0	-1637	0	0	0	-1723	--	--	16.08	16.08	0.29	0.03	0.01	0.10	0.00	0.00	20.9
16	26	-0	-1643	0	0	0	-1580	--	--	16.08	16.08	0.29	0.03	0.01	0.10	0.00	0.00	20.9
17	26	-0	-1600	0	0	0	-1637	--	--	16.08	16.08	0.29	0.03	0.01	0.10	0.00	0.00	20.9
18	26	-0	-3252	0	0	0	-4079	--	--	16.08	16.08	0.18	0.07	0.03	0.20	0.00	0.00	20.9
19	26	-0	-2545	0	0	0	-2544	--	--	16.08	16.08	0.18	0.04	0.02	0.16	0.00	0.00	20.9
20	26	-0	-2680	0	0	0	-3352	--	--	16.08	16.08	0.18	0.06	0.02	0.17	0.00	0.00	20.9
37	26	-0	-3239	0	0	0	-4212	--	--	16.08	16.08	0.18	0.07	0.03	0.20	0.00	0.00	20.9
38	26	-0	-2060	0	0	0	-1654	--	--	16.08	16.08	0.18	0.03	0.02	0.13	0.00	0.00	20.9
39	26	-0	-2285	0	0	0	-3001	--	--	16.08	16.08	0.18	0.05	0.02	0.14	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	-2132	0	0	0	-2147	--	--	16.08	16.08	0.18	0.04	0.02	0.13	0.00	0.00	20.9
2	51	-0	-1708	0	0	0	-1787	--	--	16.08	16.08	0.29	0.03	0.01	0.11	0.00	0.00	20.9
3	51	-0	-1695	0	0	0	-1804	--	--	16.08	16.08	0.29	0.03	0.01	0.11	0.00	0.00	20.9
4	51	-0	-1585	0	0	0	-1499	--	--	16.08	16.08	0.29	0.03	0.01	0.10	0.00	0.00	20.9
5	51	-0	-1572	0	0	0	-1516	--	--	16.08	16.08	0.29	0.03	0.01	0.10	0.00	0.00	20.9
6	51	-0	-1680	0	0	0	-1666	--	--	16.08	16.08	0.29	0.03	0.01	0.11	0.00	0.00	20.9
7	51	-0	-1637	0	0	0	-1723	--	--	16.08	16.08	0.29	0.03	0.01	0.10	0.00	0.00	20.9
8	51	-0	-1643	0	0	0	-1580	--	--	16.08	16.08	0.29	0.03	0.01	0.10	0.00	0.00	20.9
9	51	-0	-1600	0	0	0	-1637	--	--	16.08	16.08	0.29	0.03	0.01	0.10	0.00	0.00	20.9
10	51	-0	-1708	0	0	0	-1787	--	--	16.08	16.08	0.29	0.03	0.01	0.11	0.00	0.00	20.9
11	51	-0	-1695	0	0	0	-1804	--	--	16.08	16.08	0.29	0.03	0.01	0.11	0.00	0.00	20.9
12	51	-0	-1585	0	0	0	-1499	--	--	16.08	16.08	0.29	0.03	0.01	0.10	0.00	0.00	20.9
13	51	-0	-1572	0	0	0	-1516	--	--	16.08	16.08	0.29	0.03	0.01	0.10	0.00	0.00	20.9
14	51	-0	-1680	0	0	0	-1666	--	--	16.08	16.08	0.29	0.03	0.01	0.11	0.00	0.00	20.9
15	51	-0	-1637	0	0	0	-1723	--	--	16.08	16.08	0.29	0.03	0.01	0.10	0.00	0.00	20.9
16	51	-0	-1643	0	0	0	-1580	--	--	16.08	16.08	0.29	0.03	0.01	0.10	0.00	0.00	20.9
17	51	-0	-1600	0	0	0	-1637	--	--	16.08	16.08	0.29	0.03	0.01	0.10	0.00	0.00	20.9
18	51	-0	-3252	0	0	0	-4079	--	--	16.08	16.08	0.18	0.07	0.03	0.20	0.00	0.00	20.9
19	51	-0	-2545	0	0	0	-2544	--	--	16.08	16.08	0.18	0.04	0.02	0.16	0.00	0.00	20.9
20	51	-0	-2680	0	0	0	-3352	--	--	16.08	16.08	0.18	0.06	0.02	0.17	0.00	0.00	20.9
37	51	-0	-3239	0	0	0	-4212	--	--	16.08	16.08	0.18	0.07	0.03	0.20	0.00	0.00	20.9
38	51	-0	-2060	0	0	0	-1654	--	--	16.08	16.08	0.18	0.03	0.02	0.13	0.00	0.00	20.9
39	51	-0	-2285	0	0	0	-3001	--	--	16.08	16.08	0.18	0.05	0.02	0.14	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 40 NI 1525 NF 1498 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-1406	0	0	0	-2274	--	--	16.08	16.08	0.18	0.04	0.01	0.09	0.00	0.00	20.9
2	0	-0	-1151	0	0	0	-1898	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
3	0	-0	-1131	0	0	0	-1910	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
4	0	-0	-1032	0	0	0	-1588	--	--	16.08	16.08	0.29	0.03	0.01	0.06	0.00	0.00	20.9
5	0	-0	-1011	0	0	0	-1600	--	--	16.08	16.08	0.29	0.03	0.01	0.06	0.00	0.00	20.9
6	0	-0	-1134	0	0	0	-1776	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
7	0	-0	-1065	0	0	0	-1816	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
8	0	-0	-1098	0	0	0	-1683	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
9	0	-0	-1029	0	0	0	-1722	--	--	16.08	16.08	0.29	0.03	0.01	0.06	0.00	0.00	20.9
10	0	-0	-1151	0	0	0	-1898	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
11	0	-0	-1131	0	0	0	-1910	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
12	0	-0	-1032	0	0	0	-1588	--	--	16.08	16.08	0.29	0.03	0.01	0.06	0.00	0.00	20.9
13	0	-0	-1011	0	0	0	-1600	--	--	16.08	16.08	0.29	0.03	0.01	0.06	0.00	0.00	20.9
14	0	-0	-1134	0	0	0	-1776	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
15	0	-0	-1065	0	0	0	-1816	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
16	0	-0	-1098	0	0	0	-1683	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
17	0	-0	-1029	0	0	0	-1722	--	--	16.08	16.08	0.29	0.03	0.01	0.06	0.00	0.00	20.9
18	0	-0	-2464	0	0	0	-4395	--	--	16.08	16.08	0.18	0.07	0.02	0.15	0.00	0.00	20.9
19	0	-0	-1720	0	0	0	-2713	--	--	16.08	16.08	0.18	0.04	0.01	0.11	0.00	0.00	20.9
20	0	-0	-1825	0	0	0	-3538	--	--	16.08	16.08	0.18	0.06	0.02	0.11	0.00	0.00	20.9
37	0	-0	-2487	0	0	0	-4540	--	--	16.08	16.08	0.18	0.08	0.02	0.16	0.00	0.00	20.9
38	0	-0	-1249	0	0	0	-1736	--	--	16.08	16.08	0.18	0.03	0.01	0.08	0.00	0.00	20.9
39	0	-0	-1423	0	0	0	-3111	--	--	16.08	16.08	0.18	0.05	0.01	0.09	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	-1406	0	0	0	-2274	--	--	16.08	16.08	0.18	0.04	0.01	0.09	0.00	0.00	20.9
2	26	-0	-1151	0	0	0	-1898	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
3	26	-0	-1131	0	0	0	-1910	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
4	26	-0	-1032	0	0	0	-1588	--	--	16.08	16.08	0.29	0.03	0.01	0.06	0.00	0.00	20.9
5	26	-0	-1011	0	0	0	-1600	--	--	16.08	16.08	0.29	0.03	0.01	0.06	0.00	0.00	20.9
6	26	-0	-1134	0	0	0	-1776	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
7	26	-0	-1065	0	0	0	-1816	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
8	26	-0	-1098	0	0	0	-1683	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
9	26	-0	-1029	0	0	0	-1722	--	--	16.08	16.08	0.29	0.03	0.01	0.06	0.00	0.00	20.9
10	26	-0	-1151	0	0	0	-1898	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
11	26	-0	-1131	0	0	0	-1910	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
12	26	-0	-1032	0	0	0	-1588	--	--	16.08	16.08	0.29	0.03	0.01	0.06	0.00	0.00	20.9
13	26	-0	-1011	0	0	0	-1600	--	--	16.08	16.08	0.29	0.03	0.01	0.06	0.00	0.00	20.9
14	26	-0	-1134	0	0	0	-1776	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
15	26	-0	-1065	0	0	0	-1816	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
16	26	-0	-1098	0	0	0	-1683	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
17	26	-0	-1029	0	0	0	-1722	--	--	16.08	16.08	0.29	0.03	0.01	0.06	0.00	0.00	20.9
18	26	-0	-2464	0	0	0	-4395	--	--	16.08	16.08	0.18	0.07	0.02	0.15	0.00	0.00	20.9
19	26	-0	-1720	0	0	0	-2713	--	--	16.08	16.08	0.18	0.04	0.01	0.11	0.00	0.00	20.9
20	26	-0	-1825	0	0	0	-3538	--	--	16.08	16.08	0.18	0.06	0.02	0.11	0.00	0.00	20.9
37	26	-0	-2487	0	0	0	-4540	--	--	16.08	16.08	0.18	0.08	0.02	0.16	0.00	0.00	20.9
38	26	-0	-1249	0	0	0	-1736	--	--	16.08	16.08	0.18	0.03	0.01	0.08	0.00	0.00	20.9
39	26	-0	-1423	0	0	0	-3111	--	--	16.08	16.08	0.18	0.05	0.01	0.09	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	-1406	0	0	0	-2274	--	--	16.08	16.08	0.18	0.04	0.01	0.09	0.00	0.00	20.9
2	51	-0	-1151	0	0	0	-1898	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9

3	51	-0	-1131	0	0	0	-1910	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
4	51	-0	-1032	0	0	0	-1588	--	--	16.08	16.08	0.29	0.03	0.01	0.06	0.00	0.00	20.9
5	51	-0	-1011	0	0	0	-1600	--	--	16.08	16.08	0.29	0.03	0.01	0.06	0.00	0.00	20.9
6	51	-0	-1134	0	0	0	-1776	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
7	51	-0	-1065	0	0	0	-1816	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
8	51	-0	-1098	0	0	0	-1683	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
9	51	-0	-1029	0	0	0	-1722	--	--	16.08	16.08	0.29	0.03	0.01	0.06	0.00	0.00	20.9
10	51	-0	-1151	0	0	0	-1898	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
11	51	-0	-1131	0	0	0	-1910	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
12	51	-0	-1032	0	0	0	-1588	--	--	16.08	16.08	0.29	0.03	0.01	0.06	0.00	0.00	20.9
13	51	-0	-1011	0	0	0	-1600	--	--	16.08	16.08	0.29	0.03	0.01	0.06	0.00	0.00	20.9
14	51	-0	-1134	0	0	0	-1776	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
15	51	-0	-1065	0	0	0	-1816	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
16	51	-0	-1098	0	0	0	-1683	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
17	51	-0	-1029	0	0	0	-1722	--	--	16.08	16.08	0.29	0.03	0.01	0.06	0.00	0.00	20.9
18	51	-0	-2464	0	0	0	-4395	--	--	16.08	16.08	0.18	0.07	0.02	0.15	0.00	0.00	20.9
19	51	-0	-1720	0	0	0	-2713	--	--	16.08	16.08	0.18	0.04	0.01	0.11	0.00	0.00	20.9
20	51	-0	-1825	0	0	0	-3538	--	--	16.08	16.08	0.18	0.06	0.02	0.11	0.00	0.00	20.9
37	51	-0	-2487	0	0	0	-4540	--	--	16.08	16.08	0.18	0.08	0.02	0.16	0.00	0.00	20.9
38	51	-0	-1249	0	0	0	-1736	--	--	16.08	16.08	0.18	0.03	0.01	0.08	0.00	0.00	20.9
39	51	-0	-1423	0	0	0	-3111	--	--	16.08	16.08	0.18	0.05	0.01	0.09	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 41 NI 1498 NF 1509 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-730	0	0	0	-2300	--	--	16.08	16.08	0.18	0.04	0.01	0.05	0.00	0.00	20.9
2	0	-0	-638	0	0	0	-1937	--	--	16.08	16.08	0.29	0.03	0.01	0.04	0.00	0.00	20.9
3	0	-0	-607	0	0	0	-1941	--	--	16.08	16.08	0.29	0.03	0.01	0.04	0.00	0.00	20.9
4	0	-0	-516	0	0	0	-1597	--	--	16.08	16.08	0.29	0.03	0.00	0.03	0.00	0.00	20.9
5	0	-0	-485	0	0	0	-1601	--	--	16.08	16.08	0.29	0.03	0.00	0.03	0.00	0.00	20.9
6	0	-0	-631	0	0	0	-1814	--	--	16.08	16.08	0.29	0.03	0.01	0.04	0.00	0.00	20.9
7	0	-0	-528	0	0	0	-1827	--	--	16.08	16.08	0.29	0.03	0.00	0.03	0.00	0.00	20.9
8	0	-0	-594	0	0	0	-1712	--	--	16.08	16.08	0.29	0.03	0.00	0.04	0.00	0.00	20.9
9	0	-0	-492	0	0	0	-1725	--	--	16.08	16.08	0.29	0.03	0.00	0.03	0.00	0.00	20.9
10	0	-0	-638	0	0	0	-1937	--	--	16.08	16.08	0.29	0.03	0.01	0.04	0.00	0.00	20.9
11	0	-0	-607	0	0	0	-1941	--	--	16.08	16.08	0.29	0.03	0.01	0.04	0.00	0.00	20.9
12	0	-0	-516	0	0	0	-1597	--	--	16.08	16.08	0.29	0.03	0.00	0.03	0.00	0.00	20.9
13	0	-0	-485	0	0	0	-1601	--	--	16.08	16.08	0.29	0.03	0.00	0.03	0.00	0.00	20.9
14	0	-0	-631	0	0	0	-1814	--	--	16.08	16.08	0.29	0.03	0.01	0.04	0.00	0.00	20.9
15	0	-0	-528	0	0	0	-1827	--	--	16.08	16.08	0.29	0.03	0.00	0.03	0.00	0.00	20.9
16	0	-0	-594	0	0	0	-1712	--	--	16.08	16.08	0.29	0.03	0.00	0.04	0.00	0.00	20.9
17	0	-0	-492	0	0	0	-1725	--	--	16.08	16.08	0.29	0.03	0.00	0.03	0.00	0.00	20.9
18	0	-0	-1781	0	0	0	-4654	--	--	16.08	16.08	0.18	0.08	0.01	0.11	0.00	0.00	20.9
19	0	-0	-968	0	0	0	-2781	--	--	16.08	16.08	0.18	0.05	0.01	0.06	0.00	0.00	20.9
20	0	-0	-1037	0	0	0	-3620	--	--	16.08	16.08	0.18	0.06	0.01	0.07	0.00	0.00	20.9
37	0	-0	-1840	0	0	0	-4817	--	--	16.08	16.08	0.18	0.08	0.02	0.12	0.00	0.00	20.9
38	0	-0	-485	0	0	0	-1695	--	--	16.08	16.08	0.18	0.03	0.00	0.03	0.00	0.00	20.9
39	0	-0	-599	0	0	0	-3094	--	--	16.08	16.08	0.18	0.05	0.00	0.04	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	-730	0	0	0	-2300	--	--	16.08	16.08	0.18	0.04	0.01	0.05	0.00	0.00	20.9
2	26	-0	-638	0	0	0	-1937	--	--	16.08	16.08	0.29	0.03	0.01	0.04	0.00	0.00	20.9
3	26	-0	-607	0	0	0	-1941	--	--	16.08	16.08	0.29	0.03	0.01	0.04	0.00	0.00	20.9
4	26	-0	-516	0	0	0	-1597	--	--	16.08	16.08	0.29	0.03	0.00	0.03	0.00	0.00	20.9
5	26	-0	-485	0	0	0	-1601	--	--	16.08	16.08	0.29	0.03	0.00	0.03	0.00	0.00	20.9
6	26	-0	-631	0	0	0	-1814	--	--	16.08	16.08	0.29	0.03	0.01	0.04	0.00	0.00	20.9
7	26	-0	-528	0	0	0	-1827	--	--	16.08	16.08	0.29	0.03	0.00	0.03	0.00	0.00	20.9
8	26	-0	-594	0	0	0	-1712	--	--	16.08	16.08	0.29	0.03	0.00	0.04	0.00	0.00	20.9
9	26	-0	-492	0	0	0	-1725	--	--	16.08	16.08	0.29	0.03	0.00	0.03	0.00	0.00	20.9
10	26	-0	-638	0	0	0	-1937	--	--	16.08	16.08	0.29	0.03	0.01	0.04	0.00	0.00	20.9
11	26	-0	-607	0	0	0	-1941	--	--	16.08	16.08	0.29	0.03	0.01	0.04	0.00	0.00	20.9
12	26	-0	-516	0	0	0	-1597	--	--	16.08	16.08	0.29	0.03	0.00	0.03	0.00	0.00	20.9
13	26	-0	-485	0	0	0	-1601	--	--	16.08	16.08	0.29	0.03	0.00	0.03	0.00	0.00	20.9
14	26	-0	-631	0	0	0	-1814	--	--	16.08	16.08	0.29	0.03	0.01	0.04	0.00	0.00	20.9
15	26	-0	-528	0	0	0	-1827	--	--	16.08	16.08	0.29	0.03	0.00	0.03	0.00	0.00	20.9
16	26	-0	-594	0	0	0	-1712	--	--	16.08	16.08	0.29	0.03	0.00	0.04	0.00	0.00	20.9
17	26	-0	-492	0	0	0	-1725	--	--	16.08	16.08	0.29	0.03	0.00	0.03	0.00	0.00	20.9
18	26	-0	-1781	0	0	0	-4654	--	--	16.08	16.08	0.18	0.08	0.01	0.11	0.00	0.00	20.9
19	26	-0	-968	0	0	0	-2781	--	--	16.08	16.08	0.18	0.05	0.01	0.06	0.00	0.00	20.9
20	26	-0	-1037	0	0	0	-3620	--	--	16.08	16.08	0.18	0.06	0.01	0.07	0.00	0.00	20.9
37	26	-0	-1840	0	0	0	-4817	--	--	16.08	16.08	0.18	0.08	0.02	0.12	0.00	0.00	20.9
38	26	-0	-485	0	0	0	-1695	--	--	16.08	16.08	0.18	0.03	0.00	0.03	0.00	0.00	20.9
39	26	-0	-599	0	0	0	-3094	--	--	16.08	16.08	0.18	0.05	0.00	0.04	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	-730	0	0	0	-2300	--	--	16.08	16.08	0.18	0.04	0.01	0.05	0.00	0.00	20.9
2	51	-0	-638	0	0	0	-1937	--	--	16.08	16.08	0.29	0.03	0.01	0.04	0.00	0.00	20.9
3	51	-0	-607	0	0	0	-1941	--	--	16.08	16.08	0.29	0.03	0.01	0.04	0.00	0.00	20.9
4	51	-0	-516	0	0	0	-1597	--	--	16.08	16.08	0.29	0.03	0.00	0.03	0.00	0.00	20.9
5	51	-0	-485	0	0	0	-1601	--	--	16.08	16.08	0.29	0.03	0.00	0.03	0.00	0.00	20.9
6	51	-0	-631	0	0	0	-1814	--	--	16.08	16.08	0.29	0.03	0.01	0.04	0.00	0.00	20.9
7	51	-0	-528	0	0	0	-1827	--	--	16.08	16.08	0.29	0.03	0.00	0.03	0.00	0.00	20.9
8	51	-0	-594	0	0	0	-1712	--	--	16.08	16.08	0.29	0.03	0.00	0.04	0.00	0.00	20.9
9	51	-0	-492	0	0	0	-1725	--	--	16.08	16.08	0.29	0.03	0.00	0.03	0.00	0.00	20.9
10	51	-0	-638	0	0	0	-1937	--	--	16.08	16.08	0.29	0.03	0.01	0.04	0.00	0.00	20.9
11	51	-0	-607	0	0	0	-1941	--	--	16.08	16.08	0.29	0.03	0.01	0.04	0.00	0.00	20.9
12	51	-0	-516	0	0	0	-1597	--	--	16.08	16.08	0.29	0.03	0.00	0.03	0.00	0.00	20.9
13	51	-0	-485	0	0	0	-1601	--	--	16.08	16.08	0.29	0.03	0.00	0.03	0.00	0.00	20.9
14	51	-0	-631	0	0	0	-1814	--	--	16.08	16.08	0.29	0.03	0.01	0.04	0.00	0.00	20.9
15	51	-0	-528	0	0	0	-1827	--	--	16.08	16.08	0.29	0.03	0.00	0.03	0.00	0.00	20.9
16	51	-0	-594	0	0	0	-1712	--	--	16.08	16.08	0.29	0.03	0.00	0.04	0.00	0.00	20.9
17	51	-0	-492	0	0	0	-1725	--	--	16.08	16.08	0.29	0.03	0.00	0.03	0.00	0.00	20.9
18	51	-0	-1781	0	0	0	-4654	--	--	16.08	16.08	0.18	0.08	0.01	0.11	0.00	0.00	20.9
19	51	-0	-968	0	0	0	-2781	--	--	16.08	16.08	0.18	0.05	0.01	0.06	0.00	0.00	20.9
20	51	-0	-1037	0	0	0	-3620	--	--	16.08	16.08	0.18	0.06	0.01	0.07	0.00	0.00	20.9
37	51	-0	-1840	0	0	0	-4817	--	--	16.08	16.08	0.18	0.08	0.02	0.12	0.00	0.00	20.9
38	51	-0	-485	0	0	0	-1695	--	--	16.08	16.08	0.18	0.03	0.00	0.03	0.00	0.00	20.9
39	51	-0	-599	0	0	0	-3094	--	--	16.08	16.08	0.18	0.05	0.00	0.04	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 42 NI 1509 NF 1508 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-155	0	0	0	-2284	--	--	16.08	16.08	0.18	0.04	0.00	0.01	0.00	0.00	20.9
2	0	-0	-220	0	0	0	-1961	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
3	0	-0	-175	0	0	0	-1951	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
4	0	-0	-64	0	0	0	-1563	--	--	16.08	16.08	0.29	0.03	0.00	0.00	0.00	0.00	20.9
5	0	-0	-18	0	0	0	-1553	--	--	16.08	16.08	0.29	0.03	0.00	0.00	0.00	0.00	20.9
6	0	-0	-218	0	0	0	-1832	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
7	0	-0	-67	0	0	0	-1801	--	--	16.08	16.08	0.29	0.03	0.00	0.00	0.00	0.00	20.9
8	0	-0	-171	0	0	0	-1713	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
9	0	-0	-20	0	0	0	-1682	--	--	16.08	16.08	0.29	0.03	0.00	0.00	0.00	0.00	20.9
10	0	-0	-220	0	0	0	-1961	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
11	0	-0	-175	0	0	0	-1951	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
12	0	-0	-64	0	0	0	-1563	--	--	16.08	16.08	0.29	0.03	0.00	0.00	0.00	0.00	20.9
13	0	-0	-18	0	0	0	-1553	--	--	16.08	16.08	0.29	0.03	0.00	0.00	0.00	0.00	20.9
14	0	-0	-218	0	0	0	-1832	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
15	0	-0	-67	0	0	0	-1801	--	--	16.08	16.08	0.29	0.03	0.00	0.00	0.00	0.00	20.9
16	0	-0	-171	0	0	0	-1713	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
17	0	-0	-20	0	0	0	-1682	--	--	16.08	16.08	0.29	0.03	0.00	0.00	0.00	0.00	20.9
18	0	-0	-1396	0	0	0	-5044	--	--	16.08	16.08	0.18	0.08	0.01	0.09	0.00	0.00	20.9
19	0	-0	-397	0	0	0	-2858	--	--	16.08	16.08	0.18	0.05	0.00	0.02	0.00	0.00	20.9
20	0	-0	-439	0	0	0	-3722	--	--	16.08	16.08	0.18	0.06	0.00	0.03	0.00	0.00	20.9
37	0	-0	-1484	0	0	0	-5229	--	--	16.08	16.08	0.18	0.09	0.01	0.09	0.00	0.00	20.9
38	0	-0	182	0	0	0	-1678	--	--	16.08	16.08	0.18	0.03	0.00	0.01	0.00	0.00	20.9
39	0	-0	111	0	0	0	-3082	--	--	16.08	16.08	0.18	0.05	0.00	0.01	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	26	-0	-155	0	0	0	-2284	--	--	16.08	16.08	0.18	0.04	0.00	0.01	0.00	0.00	20.9
2	26	-0	-220	0	0	0	-1961	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
3	26	-0	-175	0	0	0	-1951	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
4	26	-0	-64	0	0	0	-1563	--	--	16.08	16.08	0.29	0.03	0.00	0.00	0.00	0.00	20.9
5	26	-0	-18	0	0	0	-1553	--	--	16.08	16.08	0.29	0.03	0.00	0.00	0.00	0.00	20.9
6	26	-0	-218	0	0	0	-1832	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
7	26	-0	-67	0	0	0	-1801	--	--	16.08	16.08	0.29	0.03	0.00	0.00	0.00	0.00	20.9
8	26	-0	-171	0	0	0	-1713	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
9	26	-0	-20	0	0	0	-1682	--	--	16.08	16.08	0.29	0.03	0.00	0.00	0.00	0.00	20.9
10	26	-0	-220	0	0	0	-1961	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
11	26	-0	-175	0	0	0	-1951	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
12	26	-0	-64	0	0	0	-1563	--	--	16.08	16.08	0.29	0.03	0.00	0.00	0.00	0.00	20.9
13	26	-0	-18	0	0	0	-1553	--	--	16.08	16.08	0.29	0.03	0.00	0.00	0.00	0.00	20.9
14	26	-0	-218	0	0	0	-1832	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
15	26	-0	-67	0	0	0	-1801	--	--	16.08	16.08	0.29	0.03	0.00	0.00	0.00	0.00	20.9
16	26	-0	-171	0	0	0	-1713	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
17	26	-0	-20	0	0	0	-1682	--	--	16.08	16.08	0.29	0.03	0.00	0.00	0.00	0.00	20.9
18	26	-0	-1396	0	0	0	-5044	--	--	16.08	16.08	0.18	0.08	0.01	0.09	0.00	0.00	20.9
19	26	-0	-397	0	0	0	-2858	--	--	16.08	16.08	0.18	0.05	0.00	0.02	0.00	0.00	20.9
20	26	-0	-439	0	0	0	-3722	--	--	16.08	16.08	0.18	0.06	0.00	0.03	0.00	0.00	20.9
37	26	-0	-1484	0	0	0	-5229	--	--	16.08	16.08	0.18	0.09	0.01	0.09	0.00	0.00	20.9
38	26	-0	182	0	0	0	-1678	--	--	16.08	16.08	0.18	0.03	0.00	0.01	0.00	0.00	20.9
39	26	-0	111	0	0	0	-3082	--	--	16.08	16.08	0.18	0.05	0.00	0.01	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	51	-0	-155	0	0	0	-2284	--	--	16.08	16.08	0.18	0.04	0.00	0.01	0.00	0.00	20.9
2	51	-0	-220	0	0	0	-1961	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
3	51	-0	-175	0	0	0	-1951	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
4	51	-0	-64	0	0	0	-1563	--	--	16.08	16.08	0.29	0.03	0.00	0.00	0.00	0.00	20.9
5	51	-0	-18	0	0	0	-1553	--	--	16.08	16.08	0.29	0.03	0.00	0.00	0.00	0.00	20.9
6	51	-0	-218	0	0	0	-1832	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
7	51	-0	-67	0	0	0	-1801	--	--	16.08	16.08	0.29	0.03	0.00	0.00	0.00	0.00	20.9
8	51	-0	-171	0	0	0	-1713	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
9	51	-0	-20	0	0	0	-1682	--	--	16.08	16.08	0.29	0.03	0.00	0.00	0.00	0.00	20.9
10	51	-0	-220	0	0	0	-1961	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
11	51	-0	-175	0	0	0	-1951	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
12	51	-0	-64	0	0	0	-1563	--	--	16.08	16.08	0.29	0.03	0.00	0.00	0.00	0.00	20.9
13	51	-0	-18	0	0	0	-1553	--	--	16.08	16.08	0.29	0.03	0.00	0.00	0.00	0.00	20.9
14	51	-0	-218	0	0	0	-1832	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
15	51	-0	-67	0	0	0	-1801	--	--	16.08	16.08	0.29	0.03	0.00	0.00	0.00	0.00	20.9
16	51	-0	-171	0	0	0	-1713	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
17	51	-0	-20	0	0	0	-1682	--	--	16.08	16.08	0.29	0.03	0.00	0.00	0.00	0.00	20.9
18	51	-0	-1396	0	0	0	-5044	--	--	16.08	16.08	0.18	0.08	0.01	0.09	0.00	0.00	20.9
19	51	-0	-397	0	0	0	-2858	--	--	16.08	16.08	0.18	0.05	0.00	0.02	0.00	0.00	20.9
20	51	-0	-439	0	0	0	-3722	--	--	16.08	16.08	0.18	0.06	0.00	0.03	0.00	0.00	20.9
37	51	-0	-1484	0	0	0	-5229	--	--	16.08	16.08	0.18	0.09	0.01	0.09	0.00	0.00	20.9
38	51	-0	182	0	0	0	-1678	--	--	16.08	16.08	0.18	0.03	0.00	0.01	0.00	0.00	20.9
39	51	-0	111	0	0	0	-3082	--	--	16.08	16.08	0.18	0.05	0.00	0.01	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 43 NI 1508 NF 1527 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	16	0	0	0	-2501	--	--	16.08	16.08	0.18	0.04	0.00	0.00	0.00	0.00	20.9
2	0	-0	-153	0	0	0	-2198	--	--	16.08	16.08	0.29	0.04	0.00	0.01	0.00	0.00	20.9
3	0	-0	-90	0	0	0	-2169	--	--	16.08	16.08	0.29	0.04	0.00	0.01	0.00	0.00	20.9
4	0	-0	114	0	0	0	-1724	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
5	0	-0	177	0	0	0	-1728	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
6	0	-0	-132	0	0	0	-2045	--	--	16.08	16.08	0.29	0.04	0.00	0.01	0.00	0.00	20.9
7	0	-0	76	0	0	0	-1989	--	--	16.08	16.08	0.29	0.03	0.00	0.00	0.00	0.00	20.9
8	0	-0	-52	0	0	0	-1885	--	--	16.08	16.08	0.29	0.03	0.00	0.00	0.00	0.00	20.9
9	0	-0	156	0	0	0	-1870	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
10	0	-0	-153	0	0	0	-2198	--	--	16.08	16.08	0.29	0.04	0.00	0.01	0.00	0.00	20.9

11	0	-0	-90	0	0	0	-2169	--	--	16.08	16.08	0.29	0.04	0.00	0.01	0.00	0.00	20.9
12	0	-0	114	0	0	0	-1724	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
13	0	-0	177	0	0	0	-1728	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
14	0	-0	-132	0	0	0	-2045	--	--	16.08	16.08	0.29	0.04	0.00	0.01	0.00	0.00	20.9
15	0	-0	76	0	0	0	-1989	--	--	16.08	16.08	0.29	0.03	0.00	0.00	0.00	0.00	20.9
16	0	-0	-52	0	0	0	-1885	--	--	16.08	16.08	0.29	0.03	0.00	0.00	0.00	0.00	20.9
17	0	-0	156	0	0	0	-1870	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
18	0	-0	-1850	0	0	0	-6100	--	--	16.08	16.08	0.18	0.10	0.02	0.12	0.00	0.00	20.9
19	0	-0	-429	0	0	0	-3320	--	--	16.08	16.08	0.18	0.06	0.00	0.03	0.00	0.00	20.9
20	0	-0	-453	0	0	0	-4224	--	--	16.08	16.08	0.18	0.07	0.00	0.03	0.00	0.00	20.9
37	0	-0	-1942	0	0	0	-6301	--	--	16.08	16.08	0.18	0.10	0.02	0.12	0.00	0.00	20.9
38	0	-0	426	0	0	0	-1888	--	--	16.08	16.08	0.18	0.03	0.00	0.03	0.00	0.00	20.9
39	0	-0	387	0	0	0	-3374	--	--	16.08	16.08	0.18	0.06	0.00	0.02	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	16	0	0	0	-2501	--	--	16.08	16.08	0.18	0.04	0.00	0.00	0.00	0.00	20.9
2	26	-0	-153	0	0	0	-2198	--	--	16.08	16.08	0.29	0.04	0.00	0.01	0.00	0.00	20.9
3	26	-0	-90	0	0	0	-2169	--	--	16.08	16.08	0.29	0.04	0.00	0.01	0.00	0.00	20.9
4	26	-0	114	0	0	0	-1724	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
5	26	-0	177	0	0	0	-1728	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
6	26	-0	-132	0	0	0	-2045	--	--	16.08	16.08	0.29	0.04	0.00	0.01	0.00	0.00	20.9
7	26	-0	76	0	0	0	-1989	--	--	16.08	16.08	0.29	0.03	0.00	0.00	0.00	0.00	20.9
8	26	-0	-52	0	0	0	-1885	--	--	16.08	16.08	0.29	0.03	0.00	0.00	0.00	0.00	20.9
9	26	-0	156	0	0	0	-1870	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
10	26	-0	-153	0	0	0	-2198	--	--	16.08	16.08	0.29	0.04	0.00	0.01	0.00	0.00	20.9
11	26	-0	-90	0	0	0	-2169	--	--	16.08	16.08	0.29	0.04	0.00	0.01	0.00	0.00	20.9
12	26	-0	114	0	0	0	-1724	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
13	26	-0	177	0	0	0	-1728	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
14	26	-0	-132	0	0	0	-2045	--	--	16.08	16.08	0.29	0.04	0.00	0.01	0.00	0.00	20.9
15	26	-0	76	0	0	0	-1989	--	--	16.08	16.08	0.29	0.03	0.00	0.00	0.00	0.00	20.9
16	26	-0	-52	0	0	0	-1885	--	--	16.08	16.08	0.29	0.03	0.00	0.00	0.00	0.00	20.9
17	26	-0	156	0	0	0	-1870	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
18	26	-0	-1850	0	0	0	-6100	--	--	16.08	16.08	0.18	0.10	0.02	0.12	0.00	0.00	20.9
19	26	-0	-429	0	0	0	-3320	--	--	16.08	16.08	0.18	0.06	0.00	0.03	0.00	0.00	20.9
20	26	-0	-453	0	0	0	-4224	--	--	16.08	16.08	0.18	0.07	0.00	0.03	0.00	0.00	20.9
37	26	-0	-1942	0	0	0	-6301	--	--	16.08	16.08	0.18	0.10	0.02	0.12	0.00	0.00	20.9
38	26	-0	426	0	0	0	-1888	--	--	16.08	16.08	0.18	0.03	0.00	0.03	0.00	0.00	20.9
39	26	-0	387	0	0	0	-3374	--	--	16.08	16.08	0.18	0.06	0.00	0.02	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	16	0	0	0	-2501	--	--	16.08	16.08	0.18	0.04	0.00	0.00	0.00	0.00	20.9
2	51	-0	-153	0	0	0	-2198	--	--	16.08	16.08	0.29	0.04	0.00	0.01	0.00	0.00	20.9
3	51	-0	-90	0	0	0	-2169	--	--	16.08	16.08	0.29	0.04	0.00	0.01	0.00	0.00	20.9
4	51	-0	114	0	0	0	-1724	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
5	51	-0	177	0	0	0	-1728	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
6	51	-0	-132	0	0	0	-2045	--	--	16.08	16.08	0.29	0.04	0.00	0.01	0.00	0.00	20.9
7	51	-0	76	0	0	0	-1989	--	--	16.08	16.08	0.29	0.03	0.00	0.00	0.00	0.00	20.9
8	51	-0	-52	0	0	0	-1885	--	--	16.08	16.08	0.29	0.03	0.00	0.00	0.00	0.00	20.9
9	51	-0	156	0	0	0	-1870	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
10	51	-0	-153	0	0	0	-2198	--	--	16.08	16.08	0.29	0.04	0.00	0.01	0.00	0.00	20.9
11	51	-0	-90	0	0	0	-2169	--	--	16.08	16.08	0.29	0.04	0.00	0.01	0.00	0.00	20.9
12	51	-0	114	0	0	0	-1724	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
13	51	-0	177	0	0	0	-1728	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
14	51	-0	-132	0	0	0	-2045	--	--	16.08	16.08	0.29	0.04	0.00	0.01	0.00	0.00	20.9
15	51	-0	76	0	0	0	-1989	--	--	16.08	16.08	0.29	0.03	0.00	0.00	0.00	0.00	20.9
16	51	-0	-52	0	0	0	-1885	--	--	16.08	16.08	0.29	0.03	0.00	0.00	0.00	0.00	20.9
17	51	-0	156	0	0	0	-1870	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
18	51	-0	-1850	0	0	0	-6100	--	--	16.08	16.08	0.18	0.10	0.02	0.12	0.00	0.00	20.9
19	51	-0	-429	0	0	0	-3320	--	--	16.08	16.08	0.18	0.06	0.00	0.03	0.00	0.00	20.9
20	51	-0	-453	0	0	0	-4224	--	--	16.08	16.08	0.18	0.07	0.00	0.03	0.00	0.00	20.9
37	51	-0	-1942	0	0	0	-6301	--	--	16.08	16.08	0.18	0.10	0.02	0.12	0.00	0.00	20.9
38	51	-0	426	0	0	0	-1888	--	--	16.08	16.08	0.18	0.03	0.00	0.03	0.00	0.00	20.9
39	51	-0	387	0	0	0	-3374	--	--	16.08	16.08	0.18	0.06	0.00	0.02	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 44 NI 1527 NF 1538 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm

1	0	-0	-389	0	0	0	-3159	--	--	16.08	16.08	0.18	0.05	0.00	0.02	0.00	0.00	20.9
2	0	-0	-542	0	0	0	-2839	--	--	16.08	16.08	0.29	0.05	0.00	0.03	0.00	0.00	20.9
3	0	-0	-468	0	0	0	-2782	--	--	16.08	16.08	0.29	0.05	0.00	0.03	0.00	0.00	20.9
4	0	-0	-131	0	0	0	-2079	--	--	16.08	16.08	0.29	0.04	0.00	0.01	0.00	0.00	20.9
5	0	-0	-57	0	0	0	-2022	--	--	16.08	16.08	0.29	0.04	0.00	0.00	0.00	0.00	20.9
6	0	-0	-484	0	0	0	-2640	--	--	16.08	16.08	0.29	0.05	0.00	0.03	0.00	0.00	20.9
7	0	-0	-239	0	0	0	-2449	--	--	16.08	16.08	0.29	0.04	0.00	0.01	0.00	0.00	20.9
8	0	-0	-360	0	0	0	-2412	--	--	16.08	16.08	0.29	0.04	0.00	0.02	0.00	0.00	20.9
9	0	-0	-115	0	0	0	-2221	--	--	16.08	16.08	0.29	0.04	0.00	0.01	0.00	0.00	20.9
10	0	-0	-542	0	0	0	-2839	--	--	16.08	16.08	0.29	0.05	0.00	0.03	0.00	0.00	20.9
11	0	-0	-468	0	0	0	-2782	--	--	16.08	16.08	0.29	0.05	0.00	0.03	0.00	0.00	20.9
12	0	-0	-131	0	0	0	-2079	--	--	16.08	16.08	0.29	0.04	0.00	0.01	0.00	0.00	20.9
13	0	-0	-57	0	0	0	-2022	--	--	16.08	16.08	0.29	0.04	0.00	0.00	0.00	0.00	20.9
14	0	-0	-484	0	0	0	-2640	--	--	16.08	16.08	0.29	0.05	0.00	0.03	0.00	0.00	20.9
15	0	-0	-239	0	0	0	-2449	--	--	16.08	16.08	0.29	0.04	0.00	0.01	0.00	0.00	20.9
16	0	-0	-360	0	0	0	-2412	--	--	16.08	16.08	0.29	0.04	0.00	0.02	0.00	0.00	20.9
17	0	-0	-115	0	0	0	-2221	--	--	16.08	16.08	0.29	0.04	0.00	0.01	0.00	0.00	20.9
18	0	-0	-3067	0	0	0	-8228	--	--	16.08	16.08	0.18	0.14	0.03	0.19	0.00	0.00	20.9
19	0	-0	-1054	0	0	0	-4341	--	--	16.08	16.08	0.18	0.07	0.01	0.07	0.00	0.00	20.9
20	0	-0	-908	0	0	0	-5219	--	--	16.08	16.08	0.18	0.09	0.01	0.06	0.00	0.00	20.9
37	0	-0	-3187	0	0	0	-8501	--	--	16.08	16.08	0.18	0.14	0.03	0.20	0.00	0.00	20.9
38	0	-0	168	0	0	0	-2109	--	--	16.08	16.08	0.18	0.03	0.00	0.01	0.00	0.00	20.9
39	0	-0	411	0	0	0	-3697	--	--	16.08	16.08	0.18	0.06	0.00	0.03	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	-389	0	0	0	-3159	--	--	16.08	16.08	0.18	0.05	0.00	0.02	0.00	0.00	20.9
2	26	-0	-542	0	0	0	-2839	--	--	16.08	16.08	0.29	0.05	0.00	0.03	0.00	0.00	20.9
3	26	-0	-468	0	0	0	-2782	--	--	16.08	16.08	0.29	0.05	0.00	0.03	0.00	0.00	20.9
4	26	-0	-131	0	0	0	-2079	--	--	16.08	16.08	0.29	0.04	0.00	0.01	0.00	0.00	20.9
5	26	-0	-57	0	0	0	-2022	--	--	16.08	16.08	0.29	0.04	0.00	0.00	0.00	0.00	20.9
6	26	-0	-484	0	0	0	-2640	--	--	16.08	16.08	0.29	0.05	0.00	0.03	0.00	0.00	20.9

7	26	-0	-239	0	0	0	-2449	--	--	16.08	16.08	0.29	0.04	0.00	0.01	0.00	0.00	20.9
8	26	-0	-360	0	0	0	-2412	--	--	16.08	16.08	0.29	0.04	0.00	0.02	0.00	0.00	20.9
9	26	-0	-115	0	0	0	-2221	--	--	16.08	16.08	0.29	0.04	0.00	0.01	0.00	0.00	20.9
10	26	-0	-542	0	0	0	-2839	--	--	16.08	16.08	0.29	0.05	0.00	0.03	0.00	0.00	20.9
11	26	-0	-468	0	0	0	-2782	--	--	16.08	16.08	0.29	0.05	0.00	0.03	0.00	0.00	20.9
12	26	-0	-131	0	0	0	-2079	--	--	16.08	16.08	0.29	0.04	0.00	0.01	0.00	0.00	20.9
13	26	-0	-57	0	0	0	-2022	--	--	16.08	16.08	0.29	0.04	0.00	0.00	0.00	0.00	20.9
14	26	-0	-484	0	0	0	-2640	--	--	16.08	16.08	0.29	0.05	0.00	0.03	0.00	0.00	20.9
15	26	-0	-239	0	0	0	-2449	--	--	16.08	16.08	0.29	0.04	0.00	0.01	0.00	0.00	20.9
16	26	-0	-360	0	0	0	-2412	--	--	16.08	16.08	0.29	0.04	0.00	0.02	0.00	0.00	20.9
17	26	-0	-115	0	0	0	-2221	--	--	16.08	16.08	0.29	0.04	0.00	0.01	0.00	0.00	20.9
18	26	-0	-3067	0	0	0	-8228	--	--	16.08	16.08	0.18	0.14	0.03	0.19	0.00	0.00	20.9
19	26	-0	-1054	0	0	0	-4341	--	--	16.08	16.08	0.18	0.07	0.01	0.07	0.00	0.00	20.9
20	26	-0	-908	0	0	0	-5219	--	--	16.08	16.08	0.18	0.09	0.01	0.06	0.00	0.00	20.9
37	26	-0	-3187	0	0	0	-8501	--	--	16.08	16.08	0.18	0.14	0.03	0.20	0.00	0.00	20.9
38	26	-0	168	0	0	0	-2109	--	--	16.08	16.08	0.18	0.03	0.00	0.01	0.00	0.00	20.9
39	26	-0	411	0	0	0	-3697	--	--	16.08	16.08	0.18	0.06	0.00	0.03	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	-389	0	0	0	-3159	--	--	16.08	16.08	0.18	0.05	0.00	0.02	0.00	0.00	20.9
2	51	-0	-542	0	0	0	-2839	--	--	16.08	16.08	0.29	0.05	0.00	0.03	0.00	0.00	20.9
3	51	-0	-468	0	0	0	-2782	--	--	16.08	16.08	0.29	0.05	0.00	0.03	0.00	0.00	20.9
4	51	-0	-131	0	0	0	-2079	--	--	16.08	16.08	0.29	0.04	0.00	0.01	0.00	0.00	20.9
5	51	-0	-57	0	0	0	-2022	--	--	16.08	16.08	0.29	0.04	0.00	0.00	0.00	0.00	20.9
6	51	-0	-484	0	0	0	-2640	--	--	16.08	16.08	0.29	0.05	0.00	0.03	0.00	0.00	20.9
7	51	-0	-239	0	0	0	-2449	--	--	16.08	16.08	0.29	0.04	0.00	0.01	0.00	0.00	20.9
8	51	-0	-360	0	0	0	-2412	--	--	16.08	16.08	0.29	0.04	0.00	0.02	0.00	0.00	20.9
9	51	-0	-115	0	0	0	-2221	--	--	16.08	16.08	0.29	0.04	0.00	0.01	0.00	0.00	20.9
10	51	-0	-542	0	0	0	-2839	--	--	16.08	16.08	0.29	0.05	0.00	0.03	0.00	0.00	20.9
11	51	-0	-468	0	0	0	-2782	--	--	16.08	16.08	0.29	0.05	0.00	0.03	0.00	0.00	20.9
12	51	-0	-131	0	0	0	-2079	--	--	16.08	16.08	0.29	0.04	0.00	0.01	0.00	0.00	20.9
13	51	-0	-57	0	0	0	-2022	--	--	16.08	16.08	0.29	0.04	0.00	0.00	0.00	0.00	20.9
14	51	-0	-484	0	0	0	-2640	--	--	16.08	16.08	0.29	0.05	0.00	0.03	0.00	0.00	20.9
15	51	-0	-239	0	0	0	-2449	--	--	16.08	16.08	0.29	0.04	0.00	0.01	0.00	0.00	20.9
16	51	-0	-360	0	0	0	-2412	--	--	16.08	16.08	0.29	0.04	0.00	0.02	0.00	0.00	20.9
17	51	-0	-115	0	0	0	-2221	--	--	16.08	16.08	0.29	0.04	0.00	0.01	0.00	0.00	20.9
18	51	-0	-3067	0	0	0	-8228	--	--	16.08	16.08	0.18	0.14	0.03	0.19	0.00	0.00	20.9
19	51	-0	-1054	0	0	0	-4341	--	--	16.08	16.08	0.18	0.07	0.01	0.07	0.00	0.00	20.9
20	51	-0	-908	0	0	0	-5219	--	--	16.08	16.08	0.18	0.09	0.01	0.06	0.00	0.00	20.9
37	51	-0	-3187	0	0	0	-8501	--	--	16.08	16.08	0.18	0.14	0.03	0.20	0.00	0.00	20.9
38	51	-0	168	0	0	0	-2109	--	--	16.08	16.08	0.18	0.03	0.00	0.01	0.00	0.00	20.9
39	51	-0	411	0	0	0	-3697	--	--	16.08	16.08	0.18	0.06	0.00	0.03	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 45 NI 1642 NF 1643 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-4147	0	0	0	4796	--	--	16.08	16.08	0.00	0.08	0.03	0.26	0.00	0.00	20.9
2	0	-0	-3030	0	0	0	3600	--	--	16.08	16.08	0.10	0.06	0.02	0.19	0.00	0.00	20.9
3	0	-0	-2977	0	0	0	3521	--	--	16.08	16.08	0.10	0.06	0.02	0.19	0.00	0.00	20.9
4	0	-0	-3403	0	0	0	3858	--	--	16.08	16.08	0.10	0.07	0.03	0.21	0.00	0.00	20.9
5	0	-0	-3350	0	0	0	3778	--	--	16.08	16.08	0.10	0.07	0.03	0.21	0.00	0.00	20.9
6	0	-0	-3222	0	0	0	3783	--	--	16.08	16.08	0.10	0.07	0.03	0.20	0.00	0.00	20.9
7	0	-0	-3046	0	0	0	3519	--	--	16.08	16.08	0.10	0.06	0.03	0.19	0.00	0.00	20.9
8	0	-0	-3334	0	0	0	3860	--	--	16.08	16.08	0.10	0.07	0.03	0.21	0.00	0.00	20.9
9	0	-0	-3158	0	0	0	3596	--	--	16.08	16.08	0.10	0.06	0.03	0.20	0.00	0.00	20.9
10	0	-0	-3030	0	0	0	3600	--	--	16.08	16.08	0.10	0.06	0.02	0.19	0.00	0.00	20.9
11	0	-0	-2977	0	0	0	3521	--	--	16.08	16.08	0.10	0.06	0.02	0.19	0.00	0.00	20.9
12	0	-0	-3403	0	0	0	3858	--	--	16.08	16.08	0.10	0.07	0.03	0.21	0.00	0.00	20.9
13	0	-0	-3350	0	0	0	3778	--	--	16.08	16.08	0.10	0.07	0.03	0.21	0.00	0.00	20.9
14	0	-0	-3222	0	0	0	3783	--	--	16.08	16.08	0.10	0.07	0.03	0.20	0.00	0.00	20.9
15	0	-0	-3046	0	0	0	3519	--	--	16.08	16.08	0.10	0.06	0.03	0.19	0.00	0.00	20.9
16	0	-0	-3334	0	0	0	3860	--	--	16.08	16.08	0.10	0.07	0.03	0.21	0.00	0.00	20.9
17	0	-0	-3158	0	0	0	3596	--	--	16.08	16.08	0.10	0.06	0.03	0.20	0.00	0.00	20.9
18	0	-0	-4208	0	0	0	5140	--	--	16.08	16.08	0.00	0.09	0.03	0.26	0.00	0.00	20.9
19	0	-0	-4468	0	0	0	4497	--	--	16.08	16.08	0.00	0.08	0.04	0.28	0.00	0.00	20.9
20	0	-0	-4221	0	0	0	4677	--	--	16.08	16.08	0.00	0.08	0.03	0.26	0.00	0.00	20.9
37	0	-0	-4058	0	0	0	5352	--	--	16.08	16.08	0.00	0.09	0.03	0.25	0.00	0.00	20.9
38	0	-0	-4491	0	0	0	4280	--	--	16.08	16.08	0.00	0.07	0.04	0.28	0.00	0.00	20.9
39	0	-0	-4079	0	0	0	4580	--	--	16.08	16.08	0.00	0.08	0.03	0.26	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	10	-0	-4147	0	0	0	4796	--	--	16.08	16.08	0.00	0.08	0.03	0.26	0.00	0.00	20.9
2	10	-0	-3030	0	0	0	3600	--	--	16.08	16.08	0.10	0.06	0.02	0.19	0.00	0.00	20.9
3	10	-0	-2977	0	0	0	3521	--	--	16.08	16.08	0.10	0.06	0.02	0.19	0.00	0.00	20.9
4	10	-0	-3403	0	0	0	3858	--	--	16.08	16.08	0.10	0.07	0.03	0.21	0.00	0.00	20.9
5	10	-0	-3350	0	0	0	3778	--	--	16.08	16.08	0.10	0.07	0.03	0.21	0.00	0.00	20.9
6	10	-0	-3222	0	0	0	3783	--	--	16.08	16.08	0.10	0.07	0.03	0.20	0.00	0.00	20.9
7	10	-0	-3046	0	0	0	3519	--	--	16.08	16.08	0.10	0.06	0.03	0.19	0.00	0.00	20.9
8	10	-0	-3334	0	0	0	3860	--	--	16.08	16.08	0.10	0.07	0.03	0.21	0.00	0.00	20.9
9	10	-0	-3158	0	0	0	3596	--	--	16.08	16.08	0.10	0.06	0.03	0.20	0.00	0.00	20.9
10	10	-0	-3030	0	0	0	3600	--	--	16.08	16.08	0.10	0.06	0.02	0.19	0.00	0.00	20.9
11	10	-0	-2977	0	0	0	3521	--	--	16.08	16.08	0.10	0.06	0.02	0.19	0.00	0.00	20.9
12	10	-0	-3403	0	0	0	3858	--	--	16.08	16.08	0.10	0.07	0.03	0.21	0.00	0.00	20.9
13	10	-0	-3350	0	0	0	3778	--	--	16.08	16.08	0.10	0.07	0.03	0.21	0.00	0.00	20.9
14	10	-0	-3222	0	0	0	3783	--	--	16.08	16.08	0.10	0.07	0.03	0.20	0.00	0.00	20.9
15	10	-0	-3046	0	0	0	3519	--	--	16.08	16.08	0.10	0.06	0.03	0.19	0.00	0.00	20.9
16	10	-0	-3334	0	0	0	3860	--	--	16.08	16.08	0.10	0.07	0.03	0.21	0.00	0.00	20.9
17	10	-0	-3158	0	0	0	3596	--	--	16.08	16.08	0.10	0.06	0.03	0.20	0.00	0.00	20.9
18	10	-0	-4208	0	0	0	5140	--	--	16.08	16.08	0.00	0.09	0.03	0.26	0.00	0.00	20.9
19	10	-0	-4468	0	0	0	4497	--	--	16.08	16.08	0.00	0.08	0.04	0.28	0.00	0.00	20.9
20	10	-0	-4221	0	0	0	4677	--	--	16.08	16.08	0.00	0.08	0.03	0.26	0.00	0.00	20.9
37	10	-0	-4058	0	0	0	5352	--	--	16.08	16.08	0.00	0.09	0.03	0.25	0.00	0.00	20.9
38	10	-0	-4491	0	0	0	4280	--	--	16.08	16.08	0.00	0.07	0.04	0.28	0.00	0.00	20.9
39	10	-0	-4079	0	0	0	4580	--	--	16.08	16.08	0.00	0.08	0.03	0.26	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	20	-0	-4147	0	0	0	3967	--	--	16.08	16.08	0.00	0.07	0.03	0.26	0.00	0.00	20.9
2	20	-0	-3030	0	0	0	2995	--	--	16.08	16.08	0.10	0.05	0.02	0.19	0.00	0.00	20.9

3	20	-0	-2977	0	0	0	2926	--	--	16.08	16.08	0.10	0.05	0.02	0.19	0.00	0.00	20.9
4	20	-0	-3403	0	0	0	3177	--	--	16.08	16.08	0.10	0.06	0.03	0.21	0.00	0.00	20.9
5	20	-0	-3350	0	0	0	3108	--	--	16.08	16.08	0.10	0.06	0.03	0.21	0.00	0.00	20.9
6	20	-0	-3222	0	0	0	3139	--	--	16.08	16.08	0.10	0.06	0.03	0.20	0.00	0.00	20.9
7	20	-0	-3046	0	0	0	2909	--	--	16.08	16.08	0.10	0.05	0.03	0.19	0.00	0.00	20.9
8	20	-0	-3334	0	0	0	3194	--	--	16.08	16.08	0.10	0.06	0.03	0.21	0.00	0.00	20.9
9	20	-0	-3158	0	0	0	2964	--	--	16.08	16.08	0.10	0.05	0.03	0.20	0.00	0.00	20.9
10	20	-0	-3030	0	0	0	2995	--	--	16.08	16.08	0.10	0.05	0.02	0.19	0.00	0.00	20.9
11	20	-0	-2977	0	0	0	2926	--	--	16.08	16.08	0.10	0.05	0.02	0.19	0.00	0.00	20.9
12	20	-0	-3403	0	0	0	3177	--	--	16.08	16.08	0.10	0.06	0.03	0.21	0.00	0.00	20.9
13	20	-0	-3350	0	0	0	3108	--	--	16.08	16.08	0.10	0.06	0.03	0.21	0.00	0.00	20.9
14	20	-0	-3222	0	0	0	3139	--	--	16.08	16.08	0.10	0.06	0.03	0.20	0.00	0.00	20.9
15	20	-0	-3046	0	0	0	2909	--	--	16.08	16.08	0.10	0.05	0.03	0.19	0.00	0.00	20.9
16	20	-0	-3334	0	0	0	3194	--	--	16.08	16.08	0.10	0.06	0.03	0.21	0.00	0.00	20.9
17	20	-0	-3158	0	0	0	2964	--	--	16.08	16.08	0.10	0.05	0.03	0.20	0.00	0.00	20.9
18	20	-0	-4208	0	0	0	4299	--	--	16.08	16.08	0.00	0.07	0.03	0.26	0.00	0.00	20.9
19	20	-0	-4468	0	0	0	3603	--	--	16.08	16.08	0.00	0.06	0.04	0.28	0.00	0.00	20.9
20	20	-0	-4221	0	0	0	3833	--	--	16.08	16.08	0.00	0.07	0.03	0.26	0.00	0.00	20.9
37	20	-0	-4058	0	0	0	4541	--	--	16.08	16.08	0.00	0.08	0.03	0.25	0.00	0.00	20.9
38	20	-0	-4491	0	0	0	3382	--	--	16.08	16.08	0.00	0.06	0.04	0.28	0.00	0.00	20.9
39	20	-0	-4079	0	0	0	3765	--	--	16.08	16.08	0.00	0.06	0.03	0.26	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 46 NI 1649 NF 1642 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	5896	0	0	0	4703	--	--	16.08	16.08	0.00	0.08	0.05	0.37	0.00	0.00	20.9
2	0	-0	4192	0	0	0	3309	--	--	16.08	16.08	0.10	0.06	0.03	0.26	0.00	0.00	20.9
3	0	-0	4122	0	0	0	3247	--	--	16.08	16.08	0.10	0.06	0.03	0.26	0.00	0.00	20.9
4	0	-0	4949	0	0	0	3988	--	--	16.08	16.08	0.10	0.07	0.04	0.31	0.00	0.00	20.9
5	0	-0	4879	0	0	0	3926	--	--	16.08	16.08	0.10	0.07	0.04	0.31	0.00	0.00	20.9
6	0	-0	4539	0	0	0	3618	--	--	16.08	16.08	0.10	0.06	0.04	0.28	0.00	0.00	20.9
7	0	-0	4305	0	0	0	3413	--	--	16.08	16.08	0.10	0.06	0.04	0.27	0.00	0.00	20.9
8	0	-0	4766	0	0	0	3822	--	--	16.08	16.08	0.10	0.07	0.04	0.30	0.00	0.00	20.9
9	0	-0	4532	0	0	0	3617	--	--	16.08	16.08	0.10	0.06	0.04	0.28	0.00	0.00	20.9
10	0	-0	4192	0	0	0	3309	--	--	16.08	16.08	0.10	0.06	0.03	0.26	0.00	0.00	20.9
11	0	-0	4122	0	0	0	3247	--	--	16.08	16.08	0.10	0.06	0.03	0.26	0.00	0.00	20.9
12	0	-0	4949	0	0	0	3988	--	--	16.08	16.08	0.10	0.07	0.04	0.31	0.00	0.00	20.9
13	0	-0	4879	0	0	0	3926	--	--	16.08	16.08	0.10	0.07	0.04	0.31	0.00	0.00	20.9
14	0	-0	4539	0	0	0	3618	--	--	16.08	16.08	0.10	0.06	0.04	0.28	0.00	0.00	20.9
15	0	-0	4305	0	0	0	3413	--	--	16.08	16.08	0.10	0.06	0.04	0.27	0.00	0.00	20.9
16	0	-0	4766	0	0	0	3822	--	--	16.08	16.08	0.10	0.07	0.04	0.30	0.00	0.00	20.9
17	0	-0	4532	0	0	0	3617	--	--	16.08	16.08	0.10	0.06	0.04	0.28	0.00	0.00	20.9
18	0	-0	6142	0	0	0	4877	--	--	16.08	16.08	0.00	0.08	0.05	0.39	0.00	0.00	20.9
19	0	-0	7811	0	0	0	6435	--	--	16.08	16.08	0.00	0.11	0.06	0.49	0.00	0.00	20.9
20	0	-0	6688	0	0	0	5405	--	--	16.08	16.08	0.00	0.09	0.06	0.42	0.00	0.00	20.9
37	0	-0	5236	0	0	0	4050	--	--	16.08	16.08	0.00	0.07	0.04	0.33	0.00	0.00	20.9
38	0	-0	8017	0	0	0	6647	--	--	16.08	16.08	0.00	0.11	0.07	0.50	0.00	0.00	20.9
39	0	-0	6146	0	0	0	4931	--	--	16.08	16.08	0.00	0.08	0.05	0.39	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	30	-0	5896	0	0	0	12773	--	--	16.08	16.08	0.00	0.22	0.05	0.37	0.00	0.00	20.9
2	30	-0	4192	0	0	0	9047	--	--	16.08	16.08	0.10	0.16	0.03	0.26	0.00	0.00	20.9
3	30	-0	4122	0	0	0	8889	--	--	16.08	16.08	0.10	0.16	0.03	0.26	0.00	0.00	20.9
4	30	-0	4949	0	0	0	10762	--	--	16.08	16.08	0.10	0.19	0.04	0.31	0.00	0.00	20.9
5	30	-0	4879	0	0	0	10604	--	--	16.08	16.08	0.10	0.19	0.04	0.31	0.00	0.00	20.9
6	30	-0	4539	0	0	0	9831	--	--	16.08	16.08	0.10	0.17	0.04	0.28	0.00	0.00	20.9
7	30	-0	4305	0	0	0	9305	--	--	16.08	16.08	0.10	0.17	0.04	0.27	0.00	0.00	20.9
8	30	-0	4766	0	0	0	10345	--	--	16.08	16.08	0.10	0.18	0.04	0.30	0.00	0.00	20.9
9	30	-0	4532	0	0	0	9820	--	--	16.08	16.08	0.10	0.17	0.04	0.28	0.00	0.00	20.9
10	30	-0	4192	0	0	0	9047	--	--	16.08	16.08	0.10	0.16	0.03	0.26	0.00	0.00	20.9
11	30	-0	4122	0	0	0	8889	--	--	16.08	16.08	0.10	0.16	0.03	0.26	0.00	0.00	20.9
12	30	-0	4949	0	0	0	10762	--	--	16.08	16.08	0.10	0.19	0.04	0.31	0.00	0.00	20.9
13	30	-0	4879	0	0	0	10604	--	--	16.08	16.08	0.10	0.19	0.04	0.31	0.00	0.00	20.9
14	30	-0	4539	0	0	0	9831	--	--	16.08	16.08	0.10	0.17	0.04	0.28	0.00	0.00	20.9
15	30	-0	4305	0	0	0	9305	--	--	16.08	16.08	0.10	0.17	0.04	0.27	0.00	0.00	20.9
16	30	-0	4766	0	0	0	10345	--	--	16.08	16.08	0.10	0.18	0.04	0.30	0.00	0.00	20.9
17	30	-0	4532	0	0	0	9820	--	--	16.08	16.08	0.10	0.17	0.04	0.28	0.00	0.00	20.9
18	30	-0	6142	0	0	0	13284	--	--	16.08	16.08	0.00	0.23	0.05	0.39	0.00	0.00	20.9
19	30	-0	7811	0	0	0	17126	--	--	16.08	16.08	0.00	0.29	0.06	0.49	0.00	0.00	20.9
20	30	-0	6688	0	0	0	14559	--	--	16.08	16.08	0.00	0.25	0.06	0.42	0.00	0.00	20.9
37	30	-0	5236	0	0	0	11216	--	--	16.08	16.08	0.00	0.19	0.04	0.33	0.00	0.00	20.9
38	30	-0	8017	0	0	0	17622	--	--	16.08	16.08	0.00	0.30	0.07	0.50	0.00	0.00	20.9
39	30	-0	6146	0	0	0	13343	--	--	16.08	16.08	0.00	0.23	0.05	0.39	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	60	-0	5896	0	0	0	8240	--	--	16.08	16.08	0.00	0.14	0.05	0.37	0.00	0.00	20.9
2	60	-0	4192	0	0	0	5824	--	--	16.08	16.08	0.10	0.10	0.03	0.26	0.00	0.00	20.9
3	60	-0	4122	0	0	0	5721	--	--	16.08	16.08	0.10	0.10	0.03	0.26	0.00	0.00	20.9
4	60	-0	4949	0	0	0	6957	--	--	16.08	16.08	0.10	0.12	0.04	0.31	0.00	0.00	20.9
5	60	-0	4879	0	0	0	6853	--	--	16.08	16.08	0.10	0.12	0.04	0.31	0.00	0.00	20.9
6	60	-0	4539	0	0	0	6342	--	--	16.08	16.08	0.10	0.11	0.04	0.28	0.00	0.00	20.9
7	60	-0	4305	0	0	0	5996	--	--	16.08	16.08	0.10	0.11	0.04	0.27	0.00	0.00	20.9
8	60	-0	4766	0	0	0	6681	--	--	16.08	16.08	0.10	0.12	0.04	0.30	0.00	0.00	20.9
9	60	-0	4532	0	0	0	6336	--	--	16.08	16.08	0.10	0.11	0.04	0.28	0.00	0.00	20.9
10	60	-0	4192	0	0	0	5824	--	--	16.08	16.08	0.10	0.10	0.03	0.26	0.00	0.00	20.9
11	60	-0	4122	0	0	0	5721	--	--	16.08	16.08	0.10	0.10	0.03	0.26	0.00	0.00	20.9
12	60	-0	4949	0	0	0	6957	--	--	16.08	16.08	0.10	0.12	0.04	0.31	0.00	0.00	20.9
13	60	-0	4879	0	0	0	6853	--	--	16.08	16.08	0.10	0.12	0.04	0.31	0.00	0.00	20.9
14	60	-0	4539	0	0	0	6342	--	--	16.08	16.08	0.10	0.11	0.04	0.28	0.00	0.00	20.9
15	60	-0	4305	0	0	0	5996	--	--	16.08	16.08	0.10	0.11	0.04	0.27	0.00	0.00	20.9
16	60	-0	4766	0	0	0	6681	--	--	16.08	16.08	0.10	0.12	0.04	0.30	0.00	0.00	20.9
17	60	-0	4532	0	0	0	6336	--	--	16.08	16.08	0.10	0.11	0.04	0.28	0.00	0.00	20.9
18	60	-0	6142	0	0	0	8562	--	--	16.08	16.08	0.00	0.15	0.05	0.39	0.00	0.00	20.9
19	60	-0	7811	0	0	0	11120	--	--	16.08	16.08	0.00	0.19	0.06	0.49	0.00	0.00	20.9
20	60	-0	6688	0	0	0	9418	--	--	16.08	16.08	0.00	0.16	0.06	0.42	0.00	0.00	20.9
37	60	-0	5236	0	0	0	7191	--	--	16.08	16.08	0.00	0.12	0.04	0.33	0.00	0.00	20.9
38	60	-0	8017	0	0	0	11460	--	--	16.08	16.08	0.00	0.20	0.07	0.50	0.00	0.00	20.9
39	60	-0	6146	0	0	0	8618	--	--	16.08	16.08	0.00	0.15	0.05	0.39	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 47 NI 1648 NF 1649 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	4289	0	0	0	2558	--	--	16.08	16.08	0.00	0.04	0.04	0.27	0.00	0.00	20.9
2	0	-0	3033	0	0	0	1792	--	--	16.08	16.08	0.10	0.03	0.02	0.19	0.00	0.00	20.9
3	0	-0	2979	0	0	0	1758	--	--	16.08	16.08	0.10	0.03	0.02	0.19	0.00	0.00	20.9
4	0	-0	3619	0	0	0	2178	--	--	16.08	16.08	0.10	0.04	0.03	0.23	0.00	0.00	20.9
5	0	-0	3565	0	0	0	2143	--	--	16.08	16.08	0.10	0.04	0.03	0.22	0.00	0.00	20.9
6	0	-0	3301	0	0	0	1968	--	--	16.08	16.08	0.10	0.03	0.03	0.21	0.00	0.00	20.9
7	0	-0	3122	0	0	0	1852	--	--	16.08	16.08	0.10	0.03	0.03	0.20	0.00	0.00	20.9
8	0	-0	3477	0	0	0	2083	--	--	16.08	16.08	0.10	0.04	0.03	0.22	0.00	0.00	20.9
9	0	-0	3298	0	0	0	1968	--	--	16.08	16.08	0.10	0.03	0.03	0.21	0.00	0.00	20.9
10	0	-0	3033	0	0	0	1792	--	--	16.08	16.08	0.10	0.03	0.02	0.19	0.00	0.00	20.9
11	0	-0	2979	0	0	0	1758	--	--	16.08	16.08	0.10	0.03	0.02	0.19	0.00	0.00	20.9
12	0	-0	3619	0	0	0	2178	--	--	16.08	16.08	0.10	0.04	0.03	0.23	0.00	0.00	20.9
13	0	-0	3565	0	0	0	2143	--	--	16.08	16.08	0.10	0.04	0.03	0.22	0.00	0.00	20.9
14	0	-0	3301	0	0	0	1968	--	--	16.08	16.08	0.10	0.03	0.03	0.21	0.00	0.00	20.9
15	0	-0	3122	0	0	0	1852	--	--	16.08	16.08	0.10	0.03	0.03	0.20	0.00	0.00	20.9
16	0	-0	3477	0	0	0	2083	--	--	16.08	16.08	0.10	0.04	0.03	0.22	0.00	0.00	20.9
17	0	-0	3298	0	0	0	1968	--	--	16.08	16.08	0.10	0.03	0.03	0.21	0.00	0.00	20.9
18	0	-0	4457	0	0	0	2648	--	--	16.08	16.08	0.00	0.05	0.04	0.28	0.00	0.00	20.9
19	0	-0	5779	0	0	0	3546	--	--	16.08	16.08	0.00	0.06	0.05	0.36	0.00	0.00	20.9
20	0	-0	4899	0	0	0	2956	--	--	16.08	16.08	0.00	0.05	0.04	0.31	0.00	0.00	20.9
37	0	-0	3748	0	0	0	2175	--	--	16.08	16.08	0.00	0.04	0.03	0.24	0.00	0.00	20.9
38	0	-0	5952	0	0	0	3671	--	--	16.08	16.08	0.00	0.06	0.05	0.37	0.00	0.00	20.9
39	0	-0	4484	0	0	0	2689	--	--	16.08	16.08	0.00	0.05	0.04	0.28	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	25	-0	4289	0	0	0	8214	--	--	16.08	16.08	0.00	0.14	0.04	0.27	0.00	0.00	20.9
2	25	-0	3033	0	0	0	5792	--	--	16.08	16.08	0.10	0.10	0.02	0.19	0.00	0.00	20.9
3	25	-0	2979	0	0	0	5686	--	--	16.08	16.08	0.10	0.10	0.02	0.19	0.00	0.00	20.9
4	25	-0	3619	0	0	0	6951	--	--	16.08	16.08	0.10	0.12	0.03	0.23	0.00	0.00	20.9
5	25	-0	3565	0	0	0	6845	--	--	16.08	16.08	0.10	0.12	0.03	0.22	0.00	0.00	20.9
6	25	-0	3301	0	0	0	6321	--	--	16.08	16.08	0.10	0.11	0.03	0.21	0.00	0.00	20.9
7	25	-0	3122	0	0	0	5969	--	--	16.08	16.08	0.10	0.11	0.03	0.20	0.00	0.00	20.9
8	25	-0	3477	0	0	0	6669	--	--	16.08	16.08	0.10	0.12	0.03	0.22	0.00	0.00	20.9
9	25	-0	3298	0	0	0	6317	--	--	16.08	16.08	0.10	0.11	0.03	0.21	0.00	0.00	20.9
10	25	-0	3033	0	0	0	5792	--	--	16.08	16.08	0.10	0.10	0.02	0.19	0.00	0.00	20.9
11	25	-0	2979	0	0	0	5686	--	--	16.08	16.08	0.10	0.10	0.02	0.19	0.00	0.00	20.9
12	25	-0	3619	0	0	0	6951	--	--	16.08	16.08	0.10	0.12	0.03	0.23	0.00	0.00	20.9
13	25	-0	3565	0	0	0	6845	--	--	16.08	16.08	0.10	0.12	0.03	0.22	0.00	0.00	20.9
14	25	-0	3301	0	0	0	6321	--	--	16.08	16.08	0.10	0.11	0.03	0.21	0.00	0.00	20.9
15	25	-0	3122	0	0	0	5969	--	--	16.08	16.08	0.10	0.11	0.03	0.20	0.00	0.00	20.9
16	25	-0	3477	0	0	0	6669	--	--	16.08	16.08	0.10	0.12	0.03	0.22	0.00	0.00	20.9
17	25	-0	3298	0	0	0	6317	--	--	16.08	16.08	0.10	0.11	0.03	0.21	0.00	0.00	20.9
18	25	-0	4457	0	0	0	8526	--	--	16.08	16.08	0.00	0.15	0.04	0.28	0.00	0.00	20.9
19	25	-0	5779	0	0	0	11167	--	--	16.08	16.08	0.00	0.19	0.05	0.36	0.00	0.00	20.9
20	25	-0	4899	0	0	0	9416	--	--	16.08	16.08	0.00	0.16	0.04	0.31	0.00	0.00	20.9
37	25	-0	3748	0	0	0	7118	--	--	16.08	16.08	0.00	0.12	0.03	0.24	0.00	0.00	20.9
38	25	-0	5952	0	0	0	11520	--	--	16.08	16.08	0.00	0.20	0.05	0.37	0.00	0.00	20.9
39	25	-0	4484	0	0	0	8602	--	--	16.08	16.08	0.00	0.15	0.04	0.28	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	50	-0	4289	0	0	0	4703	--	--	16.08	16.08	0.00	0.08	0.04	0.27	0.00	0.00	20.9
2	50	-0	3033	0	0	0	3309	--	--	16.08	16.08	0.10	0.06	0.02	0.19	0.00	0.00	20.9
3	50	-0	2979	0	0	0	3247	--	--	16.08	16.08	0.10	0.06	0.02	0.19	0.00	0.00	20.9
4	50	-0	3619	0	0	0	3988	--	--	16.08	16.08	0.10	0.07	0.03	0.23	0.00	0.00	20.9
5	50	-0	3565	0	0	0	3926	--	--	16.08	16.08	0.10	0.07	0.03	0.22	0.00	0.00	20.9
6	50	-0	3301	0	0	0	3618	--	--	16.08	16.08	0.10	0.06	0.03	0.21	0.00	0.00	20.9
7	50	-0	3122	0	0	0	3413	--	--	16.08	16.08	0.10	0.06	0.03	0.20	0.00	0.00	20.9
8	50	-0	3477	0	0	0	3822	--	--	16.08	16.08	0.10	0.07	0.03	0.22	0.00	0.00	20.9
9	50	-0	3298	0	0	0	3617	--	--	16.08	16.08	0.10	0.06	0.03	0.21	0.00	0.00	20.9
10	50	-0	3033	0	0	0	3309	--	--	16.08	16.08	0.10	0.06	0.02	0.19	0.00	0.00	20.9
11	50	-0	2979	0	0	0	3247	--	--	16.08	16.08	0.10	0.06	0.02	0.19	0.00	0.00	20.9
12	50	-0	3619	0	0	0	3988	--	--	16.08	16.08	0.10	0.07	0.03	0.23	0.00	0.00	20.9
13	50	-0	3565	0	0	0	3926	--	--	16.08	16.08	0.10	0.07	0.03	0.22	0.00	0.00	20.9
14	50	-0	3301	0	0	0	3618	--	--	16.08	16.08	0.10	0.06	0.03	0.21	0.00	0.00	20.9
15	50	-0	3122	0	0	0	3413	--	--	16.08	16.08	0.10	0.06	0.03	0.20	0.00	0.00	20.9
16	50	-0	3477	0	0	0	3822	--	--	16.08	16.08	0.10	0.07	0.03	0.22	0.00	0.00	20.9
17	50	-0	3298	0	0	0	3617	--	--	16.08	16.08	0.10	0.06	0.03	0.21	0.00	0.00	20.9
18	50	-0	4457	0	0	0	4877	--	--	16.08	16.08	0.00	0.08	0.04	0.28	0.00	0.00	20.9
19	50	-0	5779	0	0	0	6435	--	--	16.08	16.08	0.00	0.11	0.05	0.36	0.00	0.00	20.9
20	50	-0	4899	0	0	0	5405	--	--	16.08	16.08	0.00	0.09	0.04	0.31	0.00	0.00	20.9
37	50	-0	3748	0	0	0	4050	--	--	16.08	16.08	0.00	0.07	0.03	0.24	0.00	0.00	20.9
38	50	-0	5952	0	0	0	6647	--	--	16.08	16.08	0.00	0.11	0.05	0.37	0.00	0.00	20.9
39	50	-0	4484	0	0	0	4931	--	--	16.08	16.08	0.00	0.08	0.04	0.28	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 48 NI 1647 NF 1648 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	2926	0	0	0	1095	--	--	16.08	16.08	0.00	0.02	0.02	0.18	0.00	0.00	20.9
2	0	-0	2058	0	0	0	764	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
3	0	-0	2019	0	0	0	748	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
4	0	-0	2482	0	0	0	937	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
5	0	-0	2444	0	0	0	921	--	--	16.08	16.08	0.10	0.02	0.02	0.15	0.00	0.00	20.9
6	0	-0	2251	0	0	0	842	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
7	0	-0	2123	0	0	0	791	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
8	0	-0	2379	0	0	0	894	--	--	16.08	16.08	0.10	0.02	0.02	0.15	0.00	0.00	20.9
9	0	-0	2251	0	0	0	843	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
10	0	-0	2058	0	0	0	764	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9

11	0	-0	2019	0	0	0	748	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
12	0	-0	2482	0	0	0	937	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
13	0	-0	2444	0	0	0	921	--	--	16.08	16.08	0.10	0.02	0.02	0.15	0.00	0.00	20.9
14	0	-0	2251	0	0	0	842	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
15	0	-0	2123	0	0	0	791	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
16	0	-0	2379	0	0	0	894	--	--	16.08	16.08	0.10	0.02	0.02	0.15	0.00	0.00	20.9
17	0	-0	2251	0	0	0	843	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
18	0	-0	3034	0	0	0	1131	--	--	16.08	16.08	0.00	0.02	0.03	0.19	0.00	0.00	20.9
19	0	-0	4011	0	0	0	1540	--	--	16.08	16.08	0.00	0.03	0.03	0.25	0.00	0.00	20.9
20	0	-0	3366	0	0	0	1273	--	--	16.08	16.08	0.00	0.02	0.03	0.21	0.00	0.00	20.9
37	0	-0	2515	0	0	0	918	--	--	16.08	16.08	0.00	0.02	0.02	0.16	0.00	0.00	20.9
38	0	-0	4145	0	0	0	1599	--	--	16.08	16.08	0.00	0.03	0.03	0.26	0.00	0.00	20.9
39	0	-0	3069	0	0	0	1154	--	--	16.08	16.08	0.00	0.02	0.03	0.19	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	25	-0	2926	0	0	0	4954	--	--	16.08	16.08	0.00	0.08	0.02	0.18	0.00	0.00	20.9
2	25	-0	2058	0	0	0	3477	--	--	16.08	16.08	0.10	0.06	0.02	0.13	0.00	0.00	20.9
3	25	-0	2019	0	0	0	3411	--	--	16.08	16.08	0.10	0.06	0.02	0.13	0.00	0.00	20.9
4	25	-0	2482	0	0	0	4210	--	--	16.08	16.08	0.10	0.07	0.02	0.16	0.00	0.00	20.9
5	25	-0	2444	0	0	0	4144	--	--	16.08	16.08	0.10	0.07	0.02	0.15	0.00	0.00	20.9
6	25	-0	2251	0	0	0	3811	--	--	16.08	16.08	0.10	0.07	0.02	0.14	0.00	0.00	20.9
7	25	-0	2123	0	0	0	3590	--	--	16.08	16.08	0.10	0.06	0.02	0.13	0.00	0.00	20.9
8	25	-0	2379	0	0	0	4031	--	--	16.08	16.08	0.10	0.07	0.02	0.15	0.00	0.00	20.9
9	25	-0	2251	0	0	0	3811	--	--	16.08	16.08	0.10	0.07	0.02	0.14	0.00	0.00	20.9
10	25	-0	2058	0	0	0	3477	--	--	16.08	16.08	0.10	0.06	0.02	0.13	0.00	0.00	20.9
11	25	-0	2019	0	0	0	3411	--	--	16.08	16.08	0.10	0.06	0.02	0.13	0.00	0.00	20.9
12	25	-0	2482	0	0	0	4210	--	--	16.08	16.08	0.10	0.07	0.02	0.16	0.00	0.00	20.9
13	25	-0	2444	0	0	0	4144	--	--	16.08	16.08	0.10	0.07	0.02	0.15	0.00	0.00	20.9
14	25	-0	2251	0	0	0	3811	--	--	16.08	16.08	0.10	0.07	0.02	0.14	0.00	0.00	20.9
15	25	-0	2123	0	0	0	3590	--	--	16.08	16.08	0.10	0.06	0.02	0.13	0.00	0.00	20.9
16	25	-0	2379	0	0	0	4031	--	--	16.08	16.08	0.10	0.07	0.02	0.15	0.00	0.00	20.9
17	25	-0	2251	0	0	0	3811	--	--	16.08	16.08	0.10	0.07	0.02	0.14	0.00	0.00	20.9
18	25	-0	3034	0	0	0	5132	--	--	16.08	16.08	0.00	0.09	0.03	0.19	0.00	0.00	20.9
19	25	-0	4011	0	0	0	6830	--	--	16.08	16.08	0.00	0.12	0.03	0.25	0.00	0.00	20.9
20	25	-0	3366	0	0	0	5712	--	--	16.08	16.08	0.00	0.10	0.03	0.21	0.00	0.00	20.9
37	25	-0	2515	0	0	0	4234	--	--	16.08	16.08	0.00	0.07	0.02	0.16	0.00	0.00	20.9
38	25	-0	4145	0	0	0	7065	--	--	16.08	16.08	0.00	0.12	0.03	0.26	0.00	0.00	20.9
39	25	-0	3069	0	0	0	5201	--	--	16.08	16.08	0.00	0.09	0.03	0.19	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	50	-0	2926	0	0	0	2558	--	--	16.08	16.08	0.00	0.04	0.02	0.18	0.00	0.00	20.9
2	50	-0	2058	0	0	0	1792	--	--	16.08	16.08	0.10	0.03	0.02	0.13	0.00	0.00	20.9
3	50	-0	2019	0	0	0	1758	--	--	16.08	16.08	0.10	0.03	0.02	0.13	0.00	0.00	20.9
4	50	-0	2482	0	0	0	2178	--	--	16.08	16.08	0.10	0.04	0.02	0.16	0.00	0.00	20.9
5	50	-0	2444	0	0	0	2143	--	--	16.08	16.08	0.10	0.04	0.02	0.15	0.00	0.00	20.9
6	50	-0	2251	0	0	0	1968	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
7	50	-0	2123	0	0	0	1852	--	--	16.08	16.08	0.10	0.03	0.02	0.13	0.00	0.00	20.9
8	50	-0	2379	0	0	0	2083	--	--	16.08	16.08	0.10	0.04	0.02	0.15	0.00	0.00	20.9
9	50	-0	2251	0	0	0	1968	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
10	50	-0	2058	0	0	0	1792	--	--	16.08	16.08	0.10	0.03	0.02	0.13	0.00	0.00	20.9
11	50	-0	2019	0	0	0	1758	--	--	16.08	16.08	0.10	0.03	0.02	0.13	0.00	0.00	20.9
12	50	-0	2482	0	0	0	2178	--	--	16.08	16.08	0.10	0.04	0.02	0.16	0.00	0.00	20.9
13	50	-0	2444	0	0	0	2143	--	--	16.08	16.08	0.10	0.04	0.02	0.15	0.00	0.00	20.9
14	50	-0	2251	0	0	0	1968	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
15	50	-0	2123	0	0	0	1852	--	--	16.08	16.08	0.10	0.03	0.02	0.13	0.00	0.00	20.9
16	50	-0	2379	0	0	0	2083	--	--	16.08	16.08	0.10	0.04	0.02	0.15	0.00	0.00	20.9
17	50	-0	2251	0	0	0	1968	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
18	50	-0	3034	0	0	0	2648	--	--	16.08	16.08	0.00	0.05	0.03	0.19	0.00	0.00	20.9
19	50	-0	4011	0	0	0	3546	--	--	16.08	16.08	0.00	0.06	0.03	0.25	0.00	0.00	20.9
20	50	-0	3366	0	0	0	2956	--	--	16.08	16.08	0.00	0.05	0.03	0.21	0.00	0.00	20.9
37	50	-0	2515	0	0	0	2175	--	--	16.08	16.08	0.00	0.04	0.02	0.16	0.00	0.00	20.9
38	50	-0	4145	0	0	0	3671	--	--	16.08	16.08	0.00	0.06	0.03	0.26	0.00	0.00	20.9
39	50	-0	3069	0	0	0	2689	--	--	16.08	16.08	0.00	0.05	0.03	0.19	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 49 NI 1646 NF 1647 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm

1	0	-0	1670	0	0	0	260	--	--	16.08	16.08	0.00	0.00	0.01	0.10	0.00	0.00	20.9
2	0	-0	1167	0	0	0	180	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
3	0	-0	1143	0	0	0	177	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
4	0	-0	1425	0	0	0	224	--	--	16.08	16.08	0.10	0.00	0.01	0.09	0.00	0.00	20.9
5	0	-0	1402	0	0	0	220	--	--	16.08	16.08	0.10	0.00	0.01	0.09	0.00	0.00	20.9
6	0	-0	1284	0	0	0	200	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
7	0	-0	1207	0	0	0	187	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
8	0	-0	1361	0	0	0	213	--	--	16.08	16.08	0.10	0.00	0.01	0.09	0.00	0.00	20.9
9	0	-0	1285	0	0	0	201	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
10	0	-0	1167	0	0	0	180	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
11	0	-0	1143	0	0	0	177	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
12	0	-0	1425	0	0	0	224	--	--	16.08	16.08	0.10	0.00	0.01	0.09	0.00	0.00	20.9
13	0	-0	1402	0	0	0	220	--	--	16.08	16.08	0.10	0.00	0.01	0.09	0.00	0.00	20.9
14	0	-0	1284	0	0	0	200	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
15	0	-0	1207	0	0	0	187	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
16	0	-0	1361	0	0	0	213	--	--	16.08	16.08	0.10	0.00	0.01	0.09	0.00	0.00	20.9
17	0	-0	1285	0	0	0	201	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
18	0	-0	1726	0	0	0	268	--	--	16.08	16.08	0.00	0.00	0.01	0.11	0.00	0.00	20.9
19	0	-0	2333	0	0	0	374	--	--	16.08	16.08	0.00	0.01	0.02	0.15	0.00	0.00	20.9
20	0	-0	1936	0	0	0	305	--	--	16.08	16.08	0.00	0.01	0.02	0.12	0.00	0.00	20.9
37	0	-0	1408	0	0	0	214	--	--	16.08	16.08	0.00	0.00	0.01	0.09	0.00	0.00	20.9
38	0	-0	2419	0	0	0	389	--	--	16.08	16.08	0.00	0.01	0.02	0.15	0.00	0.00	20.9
39	0	-0	1757	0	0	0	275	--	--	16.08	16.08	0.00	0.00	0.01	0.11	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	25	-0	1670	0	0	0	2463	--	--	16.08	16.08	0.00	0.04	0.01	0.10	0.00	0.00	20.9
2	25	-0	1167	0	0	0	1719	--	--	16.08	16.08	0.10	0.03	0.01	0.07	0.00	0.00	20.9
3	25	-0	1143	0	0	0	1684	--	--	16.08	16.08	0.10	0.03	0.01	0.07	0.00	0.00	20.9
4	25	-0	1425	0	0	0	2103	--	--	16.08	16.08	0.10	0.04	0.01	0.09	0.00	0.00	20.9
5	25	-0	1402	0	0	0	2069	--	--	16.08	16.08	0.10	0.04	0.01	0.09	0.00	0.00	20.9
6	25	-0	1284	0	0	0	1893	--	--	16.08	16.08	0.10	0.03	0.01	0.08	0.00	0.00	20.9

7	25	-0	1207	0	0	0	1779	--	--	16.08	16.08	0.10	0.03	0.01	0.08	0.00	0.00	20.9
8	25	-0	1361	0	0	0	2008	--	--	16.08	16.08	0.10	0.04	0.01	0.09	0.00	0.00	20.9
9	25	-0	1285	0	0	0	1895	--	--	16.08	16.08	0.10	0.03	0.01	0.08	0.00	0.00	20.9
10	25	-0	1167	0	0	0	1719	--	--	16.08	16.08	0.10	0.03	0.01	0.07	0.00	0.00	20.9
11	25	-0	1143	0	0	0	1684	--	--	16.08	16.08	0.10	0.03	0.01	0.07	0.00	0.00	20.9
12	25	-0	1425	0	0	0	2103	--	--	16.08	16.08	0.10	0.04	0.01	0.09	0.00	0.00	20.9
13	25	-0	1402	0	0	0	2069	--	--	16.08	16.08	0.10	0.04	0.01	0.09	0.00	0.00	20.9
14	25	-0	1284	0	0	0	1893	--	--	16.08	16.08	0.10	0.03	0.01	0.08	0.00	0.00	20.9
15	25	-0	1207	0	0	0	1779	--	--	16.08	16.08	0.10	0.03	0.01	0.08	0.00	0.00	20.9
16	25	-0	1361	0	0	0	2008	--	--	16.08	16.08	0.10	0.04	0.01	0.09	0.00	0.00	20.9
17	25	-0	1285	0	0	0	1895	--	--	16.08	16.08	0.10	0.03	0.01	0.08	0.00	0.00	20.9
18	25	-0	1726	0	0	0	2544	--	--	16.08	16.08	0.00	0.04	0.01	0.11	0.00	0.00	20.9
19	25	-0	2333	0	0	0	3450	--	--	16.08	16.08	0.00	0.06	0.02	0.15	0.00	0.00	20.9
20	25	-0	1936	0	0	0	2858	--	--	16.08	16.08	0.00	0.05	0.02	0.12	0.00	0.00	20.9
37	25	-0	1408	0	0	0	2070	--	--	16.08	16.08	0.00	0.04	0.01	0.09	0.00	0.00	20.9
38	25	-0	2419	0	0	0	3580	--	--	16.08	16.08	0.00	0.06	0.02	0.15	0.00	0.00	20.9
39	25	-0	1757	0	0	0	2593	--	--	16.08	16.08	0.00	0.04	0.01	0.11	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	50	-0	1670	0	0	0	1095	--	--	16.08	16.08	0.00	0.02	0.01	0.10	0.00	0.00	20.9
2	50	-0	1167	0	0	0	764	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
3	50	-0	1143	0	0	0	748	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
4	50	-0	1425	0	0	0	937	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
5	50	-0	1402	0	0	0	921	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
6	50	-0	1284	0	0	0	842	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
7	50	-0	1207	0	0	0	791	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
8	50	-0	1361	0	0	0	894	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
9	50	-0	1285	0	0	0	843	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
10	50	-0	1167	0	0	0	764	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
11	50	-0	1143	0	0	0	748	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
12	50	-0	1425	0	0	0	937	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
13	50	-0	1402	0	0	0	921	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
14	50	-0	1284	0	0	0	842	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
15	50	-0	1207	0	0	0	791	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
16	50	-0	1361	0	0	0	894	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
17	50	-0	1285	0	0	0	843	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
18	50	-0	1726	0	0	0	1131	--	--	16.08	16.08	0.00	0.02	0.01	0.11	0.00	0.00	20.9
19	50	-0	2333	0	0	0	1540	--	--	16.08	16.08	0.00	0.03	0.02	0.15	0.00	0.00	20.9
20	50	-0	1936	0	0	0	1273	--	--	16.08	16.08	0.00	0.02	0.02	0.12	0.00	0.00	20.9
37	50	-0	1408	0	0	0	918	--	--	16.08	16.08	0.00	0.02	0.01	0.09	0.00	0.00	20.9
38	50	-0	2419	0	0	0	1599	--	--	16.08	16.08	0.00	0.03	0.02	0.15	0.00	0.00	20.9
39	50	-0	1757	0	0	0	1154	--	--	16.08	16.08	0.00	0.02	0.01	0.11	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 50 NI 1645 NF 1646 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	521	0	0	0	-557	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9
2	0	-0	361	0	0	0	-385	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
3	0	-0	353	0	0	0	-377	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
4	0	-0	448	0	0	0	-479	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
5	0	-0	441	0	0	0	-471	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
6	0	-0	400	0	0	0	-428	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
7	0	-0	375	0	0	0	-400	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
8	0	-0	427	0	0	0	-456	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
9	0	-0	401	0	0	0	-429	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
10	0	-0	361	0	0	0	-385	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
11	0	-0	353	0	0	0	-377	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
12	0	-0	448	0	0	0	-479	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
13	0	-0	441	0	0	0	-471	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
14	0	-0	400	0	0	0	-428	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
15	0	-0	375	0	0	0	-400	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
16	0	-0	427	0	0	0	-456	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
17	0	-0	401	0	0	0	-429	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
18	0	-0	536	0	0	0	-573	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9
19	0	-0	747	0	0	0	-799	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9
20	0	-0	611	0	0	0	-653	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
37	0	-0	427	0	0	0	-457	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9
38	0	-0	779	0	0	0	-832	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9
39	0	-0	551	0	0	0	-589	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	25	-0	521	0	0	0	687	--	--	16.08	16.08	0.00	0.01	0.00	0.03	0.00	0.00	20.9
2	25	-0	361	0	0	0	476	--	--	16.08	16.08	0.10	0.01	0.00	0.02	0.00	0.00	20.9
3	25	-0	353	0	0	0	466	--	--	16.08	16.08	0.10	0.01	0.00	0.02	0.00	0.00	20.9
4	25	-0	448	0	0	0	591	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
5	25	-0	441	0	0	0	581	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
6	25	-0	400	0	0	0	528	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
7	25	-0	375	0	0	0	494	--	--	16.08	16.08	0.10	0.01	0.00	0.02	0.00	0.00	20.9
8	25	-0	427	0	0	0	563	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
9	25	-0	401	0	0	0	529	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
10	25	-0	361	0	0	0	476	--	--	16.08	16.08	0.10	0.01	0.00	0.02	0.00	0.00	20.9
11	25	-0	353	0	0	0	466	--	--	16.08	16.08	0.10	0.01	0.00	0.02	0.00	0.00	20.9
12	25	-0	448	0	0	0	591	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
13	25	-0	441	0	0	0	581	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
14	25	-0	400	0	0	0	528	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
15	25	-0	375	0	0	0	494	--	--	16.08	16.08	0.10	0.01	0.00	0.02	0.00	0.00	20.9
16	25	-0	427	0	0	0	563	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
17	25	-0	401	0	0	0	529	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
18	25	-0	536	0	0	0	708	--	--	16.08	16.08	0.00	0.01	0.00	0.03	0.00	0.00	20.9
19	25	-0	747	0	0	0	986	--	--	16.08	16.08	0.00	0.02	0.01	0.05	0.00	0.00	20.9
20	25	-0	611	0	0	0	805	--	--	16.08	16.08	0.00	0.01	0.01	0.04	0.00	0.00	20.9
37	25	-0	427	0	0	0	564	--	--	16.08	16.08	0.00	0.01	0.00	0.03	0.00	0.00	20.9
38	25	-0	779	0	0	0	1027	--	--	16.08	16.08	0.00	0.02	0.01	0.05	0.00	0.00	20.9
39	25	-0	551	0	0	0	727	--	--	16.08	16.08	0.00	0.01	0.00	0.03	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	50	-0	521	0	0	0	260	--	--	16.08	16.08	0.00	0.00	0.00	0.03	0.00	0.00	20.9
2	50	-0	361	0	0	0	180	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9

3	50	-0	353	0	0	0	177	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
4	50	-0	448	0	0	0	224	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
5	50	-0	441	0	0	0	220	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
6	50	-0	400	0	0	0	200	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
7	50	-0	375	0	0	0	187	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
8	50	-0	427	0	0	0	213	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
9	50	-0	401	0	0	0	201	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
10	50	-0	361	0	0	0	180	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
11	50	-0	353	0	0	0	177	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
12	50	-0	448	0	0	0	224	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
13	50	-0	441	0	0	0	220	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
14	50	-0	400	0	0	0	200	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
15	50	-0	375	0	0	0	187	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
16	50	-0	427	0	0	0	213	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
17	50	-0	401	0	0	0	201	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
18	50	-0	536	0	0	0	268	--	--	16.08	16.08	0.00	0.00	0.00	0.03	0.00	0.00	20.9
19	50	-0	747	0	0	0	374	--	--	16.08	16.08	0.00	0.01	0.01	0.05	0.00	0.00	20.9
20	50	-0	611	0	0	0	305	--	--	16.08	16.08	0.00	0.01	0.01	0.04	0.00	0.00	20.9
37	50	-0	427	0	0	0	214	--	--	16.08	16.08	0.00	0.00	0.00	0.03	0.00	0.00	20.9
38	50	-0	779	0	0	0	389	--	--	16.08	16.08	0.00	0.01	0.01	0.05	0.00	0.00	20.9
39	50	-0	551	0	0	0	275	--	--	16.08	16.08	0.00	0.00	0.00	0.03	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 51 NI 1643 NF 1651 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
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	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-4934	0	0	0	4114	--	--	16.08	16.08	0.00	0.07	0.04	0.31	0.00	0.00	20.9
2	0	-0	-3540	0	0	0	3045	--	--	16.08	16.08	0.10	0.05	0.03	0.22	0.00	0.00	20.9
3	0	-0	-3467	0	0	0	2976	--	--	16.08	16.08	0.10	0.05	0.03	0.22	0.00	0.00	20.9
4	0	-0	-4124	0	0	0	3354	--	--	16.08	16.08	0.10	0.06	0.03	0.26	0.00	0.00	20.9
5	0	-0	-4051	0	0	0	3284	--	--	16.08	16.08	0.10	0.06	0.03	0.25	0.00	0.00	20.9
6	0	-0	-3830	0	0	0	3235	--	--	16.08	16.08	0.10	0.06	0.03	0.24	0.00	0.00	20.9
7	0	-0	-3586	0	0	0	3002	--	--	16.08	16.08	0.10	0.05	0.03	0.22	0.00	0.00	20.9
8	0	-0	-4005	0	0	0	3327	--	--	16.08	16.08	0.10	0.06	0.03	0.25	0.00	0.00	20.9
9	0	-0	-3761	0	0	0	3095	--	--	16.08	16.08	0.10	0.05	0.03	0.24	0.00	0.00	20.9
10	0	-0	-3540	0	0	0	3045	--	--	16.08	16.08	0.10	0.05	0.03	0.22	0.00	0.00	20.9
11	0	-0	-3467	0	0	0	2976	--	--	16.08	16.08	0.10	0.05	0.03	0.22	0.00	0.00	20.9
12	0	-0	-4124	0	0	0	3354	--	--	16.08	16.08	0.10	0.06	0.03	0.26	0.00	0.00	20.9
13	0	-0	-4051	0	0	0	3284	--	--	16.08	16.08	0.10	0.06	0.03	0.25	0.00	0.00	20.9
14	0	-0	-3830	0	0	0	3235	--	--	16.08	16.08	0.10	0.06	0.03	0.24	0.00	0.00	20.9
15	0	-0	-3586	0	0	0	3002	--	--	16.08	16.08	0.10	0.05	0.03	0.22	0.00	0.00	20.9
16	0	-0	-4005	0	0	0	3327	--	--	16.08	16.08	0.10	0.06	0.03	0.25	0.00	0.00	20.9
17	0	-0	-3761	0	0	0	3095	--	--	16.08	16.08	0.10	0.05	0.03	0.24	0.00	0.00	20.9
18	0	-0	-4864	0	0	0	4246	--	--	16.08	16.08	0.00	0.07	0.04	0.31	0.00	0.00	20.9
19	0	-0	-5767	0	0	0	4012	--	--	16.08	16.08	0.00	0.07	0.05	0.36	0.00	0.00	20.9
20	0	-0	-5129	0	0	0	4003	--	--	16.08	16.08	0.00	0.07	0.04	0.32	0.00	0.00	20.9
37	0	-0	-4437	0	0	0	4324	--	--	16.08	16.08	0.00	0.07	0.04	0.28	0.00	0.00	20.9
38	0	-0	-5943	0	0	0	3933	--	--	16.08	16.08	0.00	0.07	0.05	0.37	0.00	0.00	20.9
39	0	-0	-4879	0	0	0	3917	--	--	16.08	16.08	0.00	0.07	0.04	0.31	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	16	-0	-4934	0	0	0	4114	--	--	16.08	16.08	0.00	0.07	0.04	0.31	0.00	0.00	20.9
2	16	-0	-3540	0	0	0	3045	--	--	16.08	16.08	0.10	0.05	0.03	0.22	0.00	0.00	20.9
3	16	-0	-3467	0	0	0	2976	--	--	16.08	16.08	0.10	0.05	0.03	0.22	0.00	0.00	20.9
4	16	-0	-4124	0	0	0	3354	--	--	16.08	16.08	0.10	0.06	0.03	0.26	0.00	0.00	20.9
5	16	-0	-4051	0	0	0	3284	--	--	16.08	16.08	0.10	0.06	0.03	0.25	0.00	0.00	20.9
6	16	-0	-3830	0	0	0	3235	--	--	16.08	16.08	0.10	0.06	0.03	0.24	0.00	0.00	20.9
7	16	-0	-3586	0	0	0	3002	--	--	16.08	16.08	0.10	0.05	0.03	0.22	0.00	0.00	20.9
8	16	-0	-4005	0	0	0	3327	--	--	16.08	16.08	0.10	0.06	0.03	0.25	0.00	0.00	20.9
9	16	-0	-3761	0	0	0	3095	--	--	16.08	16.08	0.10	0.05	0.03	0.24	0.00	0.00	20.9
10	16	-0	-3540	0	0	0	3045	--	--	16.08	16.08	0.10	0.05	0.03	0.22	0.00	0.00	20.9
11	16	-0	-3467	0	0	0	2976	--	--	16.08	16.08	0.10	0.05	0.03	0.22	0.00	0.00	20.9
12	16	-0	-4124	0	0	0	3354	--	--	16.08	16.08	0.10	0.06	0.03	0.26	0.00	0.00	20.9
13	16	-0	-4051	0	0	0	3284	--	--	16.08	16.08	0.10	0.06	0.03	0.25	0.00	0.00	20.9
14	16	-0	-3830	0	0	0	3235	--	--	16.08	16.08	0.10	0.06	0.03	0.24	0.00	0.00	20.9
15	16	-0	-3586	0	0	0	3002	--	--	16.08	16.08	0.10	0.05	0.03	0.22	0.00	0.00	20.9
16	16	-0	-4005	0	0	0	3327	--	--	16.08	16.08	0.10	0.06	0.03	0.25	0.00	0.00	20.9
17	16	-0	-3761	0	0	0	3095	--	--	16.08	16.08	0.10	0.05	0.03	0.24	0.00	0.00	20.9
18	16	-0	-4864	0	0	0	4246	--	--	16.08	16.08	0.00	0.07	0.04	0.31	0.00	0.00	20.9
19	16	-0	-5767	0	0	0	4012	--	--	16.08	16.08	0.00	0.07	0.05	0.36	0.00	0.00	20.9
20	16	-0	-5129	0	0	0	4003	--	--	16.08	16.08	0.00	0.07	0.04	0.32	0.00	0.00	20.9
37	16	-0	-4437	0	0	0	4324	--	--	16.08	16.08	0.00	0.07	0.04	0.28	0.00	0.00	20.9
38	16	-0	-5943	0	0	0	3933	--	--	16.08	16.08	0.00	0.07	0.05	0.37	0.00	0.00	20.9
39	16	-0	-4879	0	0	0	3917	--	--	16.08	16.08	0.00	0.07	0.04	0.31	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	31	-0	-4934	0	0	0	2567	--	--	16.08	16.08	0.00	0.04	0.04	0.31	0.00	0.00	20.9
2	31	-0	-3540	0	0	0	1935	--	--	16.08	16.08	0.10	0.03	0.03	0.22	0.00	0.00	20.9
3	31	-0	-3467	0	0	0	1888	--	--	16.08	16.08	0.10	0.03	0.03	0.22	0.00	0.00	20.9
4	31	-0	-4124	0	0	0	2060	--	--	16.08	16.08	0.10	0.04	0.03	0.26	0.00	0.00	20.9
5	31	-0	-4051	0	0	0	2013	--	--	16.08	16.08	0.10	0.04	0.03	0.25	0.00	0.00	20.9
6	31	-0	-3830	0	0	0	2034	--	--	16.08	16.08	0.10	0.04	0.03	0.24	0.00	0.00	20.9
7	31	-0	-3586	0	0	0	1877	--	--	16.08	16.08	0.10	0.03	0.03	0.22	0.00	0.00	20.9
8	31	-0	-4005	0	0	0	2071	--	--	16.08	16.08	0.10	0.04	0.03	0.25	0.00	0.00	20.9
9	31	-0	-3761	0	0	0	1915	--	--	16.08	16.08	0.10	0.03	0.03	0.24	0.00	0.00	20.9
10	31	-0	-3540	0	0	0	1935	--	--	16.08	16.08	0.10	0.03	0.03	0.22	0.00	0.00	20.9
11	31	-0	-3467	0	0	0	1888	--	--	16.08	16.08	0.10	0.03	0.03	0.22	0.00	0.00	20.9
12	31	-0	-4124	0	0	0	2060	--	--	16.08	16.08	0.10	0.04	0.03	0.26	0.00	0.00	20.9
13	31	-0	-4051	0	0	0	2013	--	--	16.08	16.08	0.10	0.04	0.03	0.25	0.00	0.00	20.9
14	31	-0	-3830	0	0	0	2034	--	--	16.08	16.08	0.10	0.04	0.03	0.24	0.00	0.00	20.9
15	31	-0	-3586	0	0	0	1877	--	--	16.08	16.08	0.10	0.03	0.03	0.22	0.00	0.00	20.9
16	31	-0	-4005	0	0	0	2071	--	--	16.08	16.08	0.10	0.04	0.03	0.25	0.00	0.00	20.9
17	31	-0	-3761	0	0	0	1915	--	--	16.08	16.08	0.10	0.03	0.03	0.24	0.00	0.00	20.9
18	31	-0	-4864	0	0	0	2721	--	--	16.08	16.08	0.00	0.05	0.04	0.31	0.00	0.00	20.9
19	31	-0	-5767	0	0	0	2203	--	--	16.08	16.08	0.00	0.04	0.05	0.36	0.00	0.00	20.9
20	31	-0	-5129	0	0	0	2394	--	--	16.08	16.08	0.00	0.04	0.04	0.32	0.00	0.00	20.9
37	31	-0	-4437	0	0	0	2932	--	--	16.08	16.08	0.00	0.05	0.04	0.28	0.00	0.00	20.9
38	31	-0	-5943	0	0	0	2069	--	--	16.08	16.08	0.00	0.04	0.05	0.37	0.00	0.00	20.9
39	31	-0	-4879	0	0	0	2387	--	--	16.08	16.08	0.00	0.04	0.04	0.31	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 52 NI 1651 NF 1813 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-4436	0	0	0	3111	--	--	16.08	16.08	0.00	0.05	0.04	0.28	0.00	0.00	20.9
2	0	-0	-3274	0	0	0	2344	--	--	16.08	16.08	0.10	0.04	0.03	0.21	0.00	0.00	20.9
3	0	-0	-3202	0	0	0	2288	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
4	0	-0	-3622	0	0	0	2498	--	--	16.08	16.08	0.10	0.04	0.03	0.23	0.00	0.00	20.9
5	0	-0	-3550	0	0	0	2443	--	--	16.08	16.08	0.10	0.04	0.03	0.22	0.00	0.00	20.9
6	0	-0	-3480	0	0	0	2463	--	--	16.08	16.08	0.10	0.04	0.03	0.22	0.00	0.00	20.9
7	0	-0	-3240	0	0	0	2278	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
8	0	-0	-3584	0	0	0	2509	--	--	16.08	16.08	0.10	0.04	0.03	0.22	0.00	0.00	20.9
9	0	-0	-3344	0	0	0	2324	--	--	16.08	16.08	0.10	0.04	0.03	0.21	0.00	0.00	20.9
10	0	-0	-3274	0	0	0	2344	--	--	16.08	16.08	0.10	0.04	0.03	0.21	0.00	0.00	20.9
11	0	-0	-3202	0	0	0	2288	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
12	0	-0	-3622	0	0	0	2498	--	--	16.08	16.08	0.10	0.04	0.03	0.23	0.00	0.00	20.9
13	0	-0	-3550	0	0	0	2443	--	--	16.08	16.08	0.10	0.04	0.03	0.22	0.00	0.00	20.9
14	0	-0	-3480	0	0	0	2463	--	--	16.08	16.08	0.10	0.04	0.03	0.22	0.00	0.00	20.9
15	0	-0	-3240	0	0	0	2278	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
16	0	-0	-3584	0	0	0	2509	--	--	16.08	16.08	0.10	0.04	0.03	0.22	0.00	0.00	20.9
17	0	-0	-3344	0	0	0	2324	--	--	16.08	16.08	0.10	0.04	0.03	0.21	0.00	0.00	20.9
18	0	-0	-4861	0	0	0	3395	--	--	16.08	16.08	0.00	0.06	0.04	0.30	0.00	0.00	20.9
19	0	-0	-4982	0	0	0	2845	--	--	16.08	16.08	0.00	0.05	0.04	0.31	0.00	0.00	20.9
20	0	-0	-4723	0	0	0	3020	--	--	16.08	16.08	0.00	0.05	0.04	0.30	0.00	0.00	20.9
37	0	-0	-4660	0	0	0	3579	--	--	16.08	16.08	0.00	0.06	0.04	0.29	0.00	0.00	20.9
38	0	-0	-4861	0	0	0	2662	--	--	16.08	16.08	0.00	0.05	0.04	0.30	0.00	0.00	20.9
39	0	-0	-4431	0	0	0	2954	--	--	16.08	16.08	0.00	0.05	0.04	0.28	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	26	-0	-4436	0	0	0	3111	--	--	16.08	16.08	0.00	0.05	0.04	0.28	0.00	0.00	20.9
2	26	-0	-3274	0	0	0	2344	--	--	16.08	16.08	0.10	0.04	0.03	0.21	0.00	0.00	20.9
3	26	-0	-3202	0	0	0	2288	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
4	26	-0	-3622	0	0	0	2498	--	--	16.08	16.08	0.10	0.04	0.03	0.23	0.00	0.00	20.9
5	26	-0	-3550	0	0	0	2443	--	--	16.08	16.08	0.10	0.04	0.03	0.22	0.00	0.00	20.9
6	26	-0	-3480	0	0	0	2463	--	--	16.08	16.08	0.10	0.04	0.03	0.22	0.00	0.00	20.9
7	26	-0	-3240	0	0	0	2278	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
8	26	-0	-3584	0	0	0	2509	--	--	16.08	16.08	0.10	0.04	0.03	0.22	0.00	0.00	20.9
9	26	-0	-3344	0	0	0	2324	--	--	16.08	16.08	0.10	0.04	0.03	0.21	0.00	0.00	20.9
10	26	-0	-3274	0	0	0	2344	--	--	16.08	16.08	0.10	0.04	0.03	0.21	0.00	0.00	20.9
11	26	-0	-3202	0	0	0	2288	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
12	26	-0	-3622	0	0	0	2498	--	--	16.08	16.08	0.10	0.04	0.03	0.23	0.00	0.00	20.9
13	26	-0	-3550	0	0	0	2443	--	--	16.08	16.08	0.10	0.04	0.03	0.22	0.00	0.00	20.9
14	26	-0	-3480	0	0	0	2463	--	--	16.08	16.08	0.10	0.04	0.03	0.22	0.00	0.00	20.9
15	26	-0	-3240	0	0	0	2278	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
16	26	-0	-3584	0	0	0	2509	--	--	16.08	16.08	0.10	0.04	0.03	0.22	0.00	0.00	20.9
17	26	-0	-3344	0	0	0	2324	--	--	16.08	16.08	0.10	0.04	0.03	0.21	0.00	0.00	20.9
18	26	-0	-4861	0	0	0	3395	--	--	16.08	16.08	0.00	0.06	0.04	0.30	0.00	0.00	20.9
19	26	-0	-4982	0	0	0	2845	--	--	16.08	16.08	0.00	0.05	0.04	0.31	0.00	0.00	20.9
20	26	-0	-4723	0	0	0	3020	--	--	16.08	16.08	0.00	0.05	0.04	0.30	0.00	0.00	20.9
37	26	-0	-4660	0	0	0	3579	--	--	16.08	16.08	0.00	0.06	0.04	0.29	0.00	0.00	20.9
38	26	-0	-4861	0	0	0	2662	--	--	16.08	16.08	0.00	0.05	0.04	0.30	0.00	0.00	20.9
39	26	-0	-4431	0	0	0	2954	--	--	16.08	16.08	0.00	0.05	0.04	0.28	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	51	-0	-4436	0	0	0	833	--	--	16.08	16.08	0.00	0.01	0.04	0.28	0.00	0.00	20.9
2	51	-0	-3274	0	0	0	662	--	--	16.08	16.08	0.10	0.01	0.03	0.21	0.00	0.00	20.9
3	51	-0	-3202	0	0	0	644	--	--	16.08	16.08	0.10	0.01	0.03	0.20	0.00	0.00	20.9
4	51	-0	-3622	0	0	0	638	--	--	16.08	16.08	0.10	0.01	0.03	0.23	0.00	0.00	20.9
5	51	-0	-3550	0	0	0	619	--	--	16.08	16.08	0.10	0.01	0.03	0.22	0.00	0.00	20.9
6	51	-0	-3480	0	0	0	675	--	--	16.08	16.08	0.10	0.01	0.03	0.22	0.00	0.00	20.9
7	51	-0	-3240	0	0	0	613	--	--	16.08	16.08	0.10	0.01	0.03	0.20	0.00	0.00	20.9
8	51	-0	-3584	0	0	0	668	--	--	16.08	16.08	0.10	0.01	0.03	0.22	0.00	0.00	20.9
9	51	-0	-3344	0	0	0	606	--	--	16.08	16.08	0.10	0.01	0.03	0.21	0.00	0.00	20.9
10	51	-0	-3274	0	0	0	662	--	--	16.08	16.08	0.10	0.01	0.03	0.21	0.00	0.00	20.9
11	51	-0	-3202	0	0	0	644	--	--	16.08	16.08	0.10	0.01	0.03	0.20	0.00	0.00	20.9
12	51	-0	-3622	0	0	0	638	--	--	16.08	16.08	0.10	0.01	0.03	0.23	0.00	0.00	20.9
13	51	-0	-3550	0	0	0	619	--	--	16.08	16.08	0.10	0.01	0.03	0.22	0.00	0.00	20.9
14	51	-0	-3480	0	0	0	675	--	--	16.08	16.08	0.10	0.01	0.03	0.22	0.00	0.00	20.9
15	51	-0	-3240	0	0	0	613	--	--	16.08	16.08	0.10	0.01	0.03	0.20	0.00	0.00	20.9
16	51	-0	-3584	0	0	0	668	--	--	16.08	16.08	0.10	0.01	0.03	0.22	0.00	0.00	20.9
17	51	-0	-3344	0	0	0	606	--	--	16.08	16.08	0.10	0.01	0.03	0.21	0.00	0.00	20.9
18	51	-0	-4861	0	0	0	899	--	--	16.08	16.08	0.00	0.02	0.04	0.30	0.00	0.00	20.9
19	51	-0	-4982	0	0	0	286	--	--	16.08	16.08	0.00	0.00	0.04	0.31	0.00	0.00	20.9
20	51	-0	-4723	0	0	0	594	--	--	16.08	16.08	0.00	0.01	0.04	0.30	0.00	0.00	20.9
37	51	-0	-4660	0	0	0	1186	--	--	16.08	16.08	0.00	0.02	0.04	0.29	0.00	0.00	20.9
38	51	-0	-4861	0	0	0	165	--	--	16.08	16.08	0.00	0.00	0.04	0.30	0.00	0.00	20.9
39	51	-0	-4431	0	0	0	678	--	--	16.08	16.08	0.00	0.01	0.04	0.28	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 53 NI 1813 NF 1812 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-2827	0	0	0	1400	--	--	16.08	16.08	0.00	0.02	0.02	0.18	0.00	0.00	20.9
2	0	-0	-2215	0	0	0	1142	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
3	0	-0	-2163	0	0	0	1113	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
4	0	-0	-2186	0	0	0	1042	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
5	0	-0	-2134	0	0	0	1012	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
6	0	-0	-2265	0	0	0	1141	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
7	0	-0	-2092	0	0	0	1043	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
8	0	-0	-2256	0	0	0	1111	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
9	0	-0	-2084	0	0	0	1013	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
10	0	-0	-2215	0	0	0	1142	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9

11	0	-0	-2163	0	0	0	1113	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
12	0	-0	-2186	0	0	0	1042	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
13	0	-0	-2134	0	0	0	1012	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
14	0	-0	-2265	0	0	0	1141	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
15	0	-0	-2092	0	0	0	1043	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
16	0	-0	-2256	0	0	0	1111	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
17	0	-0	-2084	0	0	0	1013	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
18	0	-0	-3674	0	0	0	1817	--	--	16.08	16.08	0.00	0.03	0.03	0.23	0.00	0.00	20.9
19	0	-0	-2738	0	0	0	739	--	--	16.08	16.08	0.00	0.01	0.02	0.17	0.00	0.00	20.9
20	0	-0	-3066	0	0	0	1245	--	--	16.08	16.08	0.00	0.02	0.03	0.19	0.00	0.00	20.9
37	0	-0	-3860	0	0	0	2220	--	--	16.08	16.08	0.00	0.04	0.03	0.24	0.00	0.00	20.9
38	0	-0	-2300	0	0	0	423	--	--	16.08	16.08	0.00	0.01	0.02	0.14	0.00	0.00	20.9
39	0	-0	-2846	0	0	0	1267	--	--	16.08	16.08	0.00	0.02	0.02	0.18	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	-2827	0	0	0	1400	--	--	16.08	16.08	0.00	0.02	0.02	0.18	0.00	0.00	20.9
2	26	-0	-2215	0	0	0	1142	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
3	26	-0	-2163	0	0	0	1113	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
4	26	-0	-2186	0	0	0	1042	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
5	26	-0	-2134	0	0	0	1012	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
6	26	-0	-2265	0	0	0	1141	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
7	26	-0	-2092	0	0	0	1043	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
8	26	-0	-2256	0	0	0	1111	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
9	26	-0	-2084	0	0	0	1013	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
10	26	-0	-2215	0	0	0	1142	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
11	26	-0	-2163	0	0	0	1113	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
12	26	-0	-2186	0	0	0	1042	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
13	26	-0	-2134	0	0	0	1012	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
14	26	-0	-2265	0	0	0	1141	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
15	26	-0	-2092	0	0	0	1043	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
16	26	-0	-2256	0	0	0	1111	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
17	26	-0	-2084	0	0	0	1013	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
18	26	-0	-3674	0	0	0	1817	--	--	16.08	16.08	0.00	0.03	0.03	0.23	0.00	0.00	20.9
19	26	-0	-2738	0	0	0	739	--	--	16.08	16.08	0.00	0.01	0.02	0.17	0.00	0.00	20.9
20	26	-0	-3066	0	0	0	1245	--	--	16.08	16.08	0.00	0.02	0.03	0.19	0.00	0.00	20.9
37	26	-0	-3860	0	0	0	2220	--	--	16.08	16.08	0.00	0.04	0.03	0.24	0.00	0.00	20.9
38	26	-0	-2300	0	0	0	-759	--	--	16.08	16.08	0.18	0.01	0.02	0.14	0.00	0.00	20.9
39	26	-0	-2846	0	0	0	1267	--	--	16.08	16.08	0.00	0.02	0.02	0.18	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	-2827	0	0	0	-52	--	--	16.08	16.08	0.18	0.00	0.02	0.18	0.00	0.00	20.9
2	51	-0	-2215	0	0	0	5	--	--	16.08	16.08	0.10	0.00	0.02	0.14	0.00	0.00	20.9
3	51	-0	-2163	0	0	0	2	--	--	16.08	16.08	0.10	0.00	0.02	0.14	0.00	0.00	20.9
4	51	-0	-2186	0	0	0	-81	--	--	16.08	16.08	0.29	0.00	0.02	0.14	0.00	0.00	20.9
5	51	-0	-2134	0	0	0	-84	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
6	51	-0	-2265	0	0	0	-22	--	--	16.08	16.08	0.29	0.00	0.02	0.14	0.00	0.00	20.9
7	51	-0	-2092	0	0	0	-32	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
8	51	-0	-2256	0	0	0	-48	--	--	16.08	16.08	0.29	0.00	0.02	0.14	0.00	0.00	20.9
9	51	-0	-2084	0	0	0	-57	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
10	51	-0	-2215	0	0	0	5	--	--	16.08	16.08	0.10	0.00	0.02	0.14	0.00	0.00	20.9
11	51	-0	-2163	0	0	0	2	--	--	16.08	16.08	0.10	0.00	0.02	0.14	0.00	0.00	20.9
12	51	-0	-2186	0	0	0	-81	--	--	16.08	16.08	0.29	0.00	0.02	0.14	0.00	0.00	20.9
13	51	-0	-2134	0	0	0	-84	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
14	51	-0	-2265	0	0	0	-22	--	--	16.08	16.08	0.29	0.00	0.02	0.14	0.00	0.00	20.9
15	51	-0	-2092	0	0	0	-32	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
16	51	-0	-2256	0	0	0	-48	--	--	16.08	16.08	0.29	0.00	0.02	0.14	0.00	0.00	20.9
17	51	-0	-2084	0	0	0	-57	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
18	51	-0	-3674	0	0	0	-70	--	--	16.08	16.08	0.18	0.00	0.03	0.23	0.00	0.00	20.9
19	51	-0	-2738	0	0	0	-668	--	--	16.08	16.08	0.18	0.01	0.02	0.17	0.00	0.00	20.9
20	51	-0	-3066	0	0	0	-329	--	--	16.08	16.08	0.18	0.01	0.03	0.19	0.00	0.00	20.9
37	51	-0	-3860	0	0	0	237	--	--	16.08	16.08	0.00	0.00	0.03	0.24	0.00	0.00	20.9
38	51	-0	-2300	0	0	0	-759	--	--	16.08	16.08	0.18	0.01	0.02	0.14	0.00	0.00	20.9
39	51	-0	-2846	0	0	0	-195	--	--	16.08	16.08	0.18	0.00	0.02	0.18	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 54 NI 1812 NF 1811 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-1547	0	0	0	359	--	--	16.08	16.08	0.00	0.01	0.01	0.10	0.00	0.00	20.9
2	0	-0	-1322	0	0	0	378	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
3	0	-0	-1287	0	0	0	366	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
4	0	-0	-1093	0	0	0	186	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
5	0	-0	-1058	0	0	0	173	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
6	0	-0	-1284	0	0	0	326	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
7	0	-0	-1165	0	0	0	284	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
8	0	-0	-1215	0	0	0	268	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
9	0	-0	-1096	0	0	0	226	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
10	0	-0	-1322	0	0	0	378	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
11	0	-0	-1287	0	0	0	366	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
12	0	-0	-1093	0	0	0	186	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
13	0	-0	-1058	0	0	0	173	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
14	0	-0	-1284	0	0	0	326	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
15	0	-0	-1165	0	0	0	284	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
16	0	-0	-1215	0	0	0	268	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
17	0	-0	-1096	0	0	0	226	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
18	0	-0	-2491	0	0	0	699	--	--	16.08	16.08	0.00	0.01	0.02	0.16	0.00	0.00	20.9
19	0	-0	-1084	0	0	0	-1009	--	--	16.08	16.08	0.18	0.02	0.01	0.07	0.00	0.00	20.9
20	0	-0	-1701	0	0	0	138	--	--	16.08	16.08	0.00	0.00	0.01	0.11	0.00	0.00	20.9
37	0	-0	-2879	0	0	0	1164	--	--	16.08	16.08	0.00	0.02	0.02	0.18	0.00	0.00	20.9
38	0	-0	-535	0	0	0	-1031	--	--	16.08	16.08	0.18	0.02	0.00	0.03	0.00	0.00	20.9
39	0	-0	-1563	0	0	0	228	--	--	16.08	16.08	0.00	0.00	0.01	0.10	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	-1547	0	0	0	-436	--	--	16.08	16.08	0.18	0.01	0.01	0.10	0.00	0.00	20.9
2	26	-0	-1322	0	0	0	378	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
3	26	-0	-1287	0	0	0	366	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
4	26	-0	-1093	0	0	0	-376	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
5	26	-0	-1058	0	0	0	-370	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
6	26	-0	-1284	0	0	0	-334	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9

7	26	-0	-1165	0	0	0	-314	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
8	26	-0	-1215	0	0	0	-356	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
9	26	-0	-1096	0	0	0	-337	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
10	26	-0	-1322	0	0	0	378	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
11	26	-0	-1287	0	0	0	366	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
12	26	-0	-1093	0	0	0	-376	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
13	26	-0	-1058	0	0	0	-370	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
14	26	-0	-1284	0	0	0	-334	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
15	26	-0	-1165	0	0	0	-314	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
16	26	-0	-1215	0	0	0	-356	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
17	26	-0	-1096	0	0	0	-337	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
18	26	-0	-2491	0	0	0	699	--	--	16.08	16.08	0.00	0.01	0.02	0.16	0.00	0.00	20.9
19	26	-0	-1084	0	0	0	-1009	--	--	16.08	16.08	0.18	0.02	0.01	0.07	0.00	0.00	20.9
20	26	-0	-1701	0	0	0	-736	--	--	16.08	16.08	0.18	0.01	0.01	0.11	0.00	0.00	20.9
37	26	-0	-2879	0	0	0	1164	--	--	16.08	16.08	0.00	0.02	0.02	0.18	0.00	0.00	20.9
38	26	-0	-535	0	0	0	-1031	--	--	16.08	16.08	0.18	0.02	0.00	0.03	0.00	0.00	20.9
39	26	-0	-1563	0	0	0	-575	--	--	16.08	16.08	0.18	0.01	0.01	0.10	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	-1547	0	0	0	-436	--	--	16.08	16.08	0.18	0.01	0.01	0.10	0.00	0.00	20.9
2	51	-0	-1322	0	0	0	-301	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
3	51	-0	-1287	0	0	0	-295	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
4	51	-0	-1093	0	0	0	-376	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
5	51	-0	-1058	0	0	0	-370	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
6	51	-0	-1284	0	0	0	-334	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
7	51	-0	-1165	0	0	0	-314	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
8	51	-0	-1215	0	0	0	-356	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
9	51	-0	-1096	0	0	0	-337	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
10	51	-0	-1322	0	0	0	-301	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
11	51	-0	-1287	0	0	0	-295	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
12	51	-0	-1093	0	0	0	-376	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
13	51	-0	-1058	0	0	0	-370	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
14	51	-0	-1284	0	0	0	-334	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
15	51	-0	-1165	0	0	0	-314	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
16	51	-0	-1215	0	0	0	-356	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
17	51	-0	-1096	0	0	0	-337	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
18	51	-0	-2491	0	0	0	-580	--	--	16.08	16.08	0.18	0.01	0.02	0.16	0.00	0.00	20.9
19	51	-0	-1084	0	0	0	-1009	--	--	16.08	16.08	0.18	0.02	0.01	0.07	0.00	0.00	20.9
20	51	-0	-1701	0	0	0	-736	--	--	16.08	16.08	0.18	0.01	0.01	0.11	0.00	0.00	20.9
37	51	-0	-2879	0	0	0	-315	--	--	16.08	16.08	0.18	0.01	0.02	0.18	0.00	0.00	20.9
38	51	-0	-535	0	0	0	-1031	--	--	16.08	16.08	0.18	0.02	0.00	0.03	0.00	0.00	20.9
39	51	-0	-1563	0	0	0	-575	--	--	16.08	16.08	0.18	0.01	0.01	0.10	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 55 NI 1811 NF 1832 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm

1	0	-0	-680	0	0	0	-525	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
2	0	-0	-692	0	0	0	-398	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
3	0	-0	-665	0	0	0	-387	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
4	0	-0	-380	0	0	0	-421	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
5	0	-0	-354	0	0	0	-410	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
6	0	-0	-614	0	0	0	-419	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
7	0	-0	-525	0	0	0	-383	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
8	0	-0	-521	0	0	0	-426	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
9	0	-0	-432	0	0	0	-389	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
10	0	-0	-692	0	0	0	-398	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
11	0	-0	-665	0	0	0	-387	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
12	0	-0	-380	0	0	0	-421	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
13	0	-0	-354	0	0	0	-410	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
14	0	-0	-614	0	0	0	-419	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
15	0	-0	-525	0	0	0	-383	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
16	0	-0	-521	0	0	0	-426	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
17	0	-0	-432	0	0	0	-389	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
18	0	-0	-1584	0	0	0	-814	--	--	16.08	16.08	0.18	0.01	0.01	0.10	0.00	0.00	20.9
19	0	-0	-41	0	0	0	-983	--	--	16.08	16.08	0.18	0.02	0.00	0.00	0.00	0.00	20.9
20	0	-0	-762	0	0	0	-832	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9
37	0	-0	-2054	0	0	0	424	--	--	16.08	16.08	0.00	0.01	0.02	0.13	0.00	0.00	20.9
38	0	-0	518	0	0	0	-1179	--	--	16.08	16.08	0.18	0.02	0.00	0.03	0.00	0.00	20.9
39	0	-0	-683	0	0	0	-661	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	-680	0	0	0	-525	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
2	26	-0	-692	0	0	0	-398	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
3	26	-0	-665	0	0	0	-387	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
4	26	-0	-380	0	0	0	-421	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
5	26	-0	-354	0	0	0	-410	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
6	26	-0	-614	0	0	0	-419	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
7	26	-0	-525	0	0	0	-383	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
8	26	-0	-521	0	0	0	-426	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
9	26	-0	-432	0	0	0	-389	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
10	26	-0	-692	0	0	0	-398	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
11	26	-0	-665	0	0	0	-387	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
12	26	-0	-380	0	0	0	-421	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
13	26	-0	-354	0	0	0	-410	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
14	26	-0	-614	0	0	0	-419	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
15	26	-0	-525	0	0	0	-383	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
16	26	-0	-521	0	0	0	-426	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
17	26	-0	-432	0	0	0	-389	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
18	26	-0	-1584	0	0	0	-814	--	--	16.08	16.08	0.18	0.01	0.01	0.10	0.00	0.00	20.9
19	26	-0	-41	0	0	0	-983	--	--	16.08	16.08	0.18	0.02	0.00	0.00	0.00	0.00	20.9
20	26	-0	-762	0	0	0	-832	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9
37	26	-0	-2054	0	0	0	-632	--	--	16.08	16.08	0.18	0.01	0.02	0.13	0.00	0.00	20.9
38	26	-0	518	0	0	0	-1179	--	--	16.08	16.08	0.18	0.02	0.00	0.03	0.00	0.00	20.9
39	26	-0	-683	0	0	0	-661	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	-680	0	0	0	-525	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
2	51	-0	-692	0	0	0	-398	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9

3	51	-0	-665	0	0	0	-387	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
4	51	-0	-380	0	0	0	-421	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
5	51	-0	-354	0	0	0	-410	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
6	51	-0	-614	0	0	0	-419	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
7	51	-0	-525	0	0	0	-383	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
8	51	-0	-521	0	0	0	-426	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
9	51	-0	-432	0	0	0	-389	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
10	51	-0	-692	0	0	0	-398	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
11	51	-0	-665	0	0	0	-387	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
12	51	-0	-380	0	0	0	-421	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
13	51	-0	-354	0	0	0	-410	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
14	51	-0	-614	0	0	0	-419	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
15	51	-0	-525	0	0	0	-383	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
16	51	-0	-521	0	0	0	-426	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
17	51	-0	-432	0	0	0	-389	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
18	51	-0	-1584	0	0	0	-814	--	--	16.08	16.08	0.18	0.01	0.01	0.10	0.00	0.00	20.9
19	51	-0	-41	0	0	0	-983	--	--	16.08	16.08	0.18	0.02	0.00	0.00	0.00	0.00	20.9
20	51	-0	-762	0	0	0	-832	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9
37	51	-0	-2054	0	0	0	-632	--	--	16.08	16.08	0.18	0.01	0.02	0.13	0.00	0.00	20.9
38	51	-0	518	0	0	0	-1179	--	--	16.08	16.08	0.18	0.02	0.00	0.03	0.00	0.00	20.9
39	51	-0	-683	0	0	0	-661	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 56 NI 1832 NF 1831 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	30	0	0	0	-442	--	--	16.08	16.08	0.18	0.01	0.00	0.00	0.00	0.00	20.9
2	0	-0	-166	0	0	0	-357	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
3	0	-0	-144	0	0	0	-343	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
4	0	-0	190	0	0	0	-410	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
5	0	-0	212	0	0	0	-407	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
6	0	-0	-66	0	0	0	-358	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
7	0	-0	6	0	0	0	-314	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
8	0	-0	40	0	0	0	-366	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
9	0	-0	113	0	0	0	-355	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
10	0	-0	-166	0	0	0	-357	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
11	0	-0	-144	0	0	0	-343	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
12	0	-0	190	0	0	0	-410	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
13	0	-0	212	0	0	0	-407	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
14	0	-0	-66	0	0	0	-358	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
15	0	-0	6	0	0	0	-314	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
16	0	-0	40	0	0	0	-366	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
17	0	-0	113	0	0	0	-355	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
18	0	-0	-814	0	0	0	-854	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9
19	0	-0	778	0	0	0	-1138	--	--	16.08	16.08	0.18	0.02	0.01	0.05	0.00	0.00	20.9
20	0	-0	7	0	0	0	-732	--	--	16.08	16.08	0.18	0.01	0.00	0.00	0.00	0.00	20.9
37	0	-0	-1329	0	0	0	-767	--	--	16.08	16.08	0.18	0.01	0.01	0.08	0.00	0.00	20.9
38	0	-0	1324	0	0	0	-1254	--	--	16.08	16.08	0.18	0.02	0.01	0.08	0.00	0.00	20.9
39	0	-0	40	0	0	0	-578	--	--	16.08	16.08	0.18	0.01	0.00	0.00	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	30	0	0	0	-442	--	--	16.08	16.08	0.18	0.01	0.00	0.00	0.00	0.00	20.9
2	26	-0	-166	0	0	0	-357	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
3	26	-0	-144	0	0	0	-343	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
4	26	-0	190	0	0	0	-410	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
5	26	-0	212	0	0	0	-407	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
6	26	-0	-66	0	0	0	-358	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
7	26	-0	6	0	0	0	-314	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
8	26	-0	40	0	0	0	-366	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
9	26	-0	113	0	0	0	-355	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
10	26	-0	-166	0	0	0	-357	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
11	26	-0	-144	0	0	0	-343	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
12	26	-0	190	0	0	0	-410	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
13	26	-0	212	0	0	0	-407	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
14	26	-0	-66	0	0	0	-358	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
15	26	-0	6	0	0	0	-314	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
16	26	-0	40	0	0	0	-366	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
17	26	-0	113	0	0	0	-355	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
18	26	-0	-814	0	0	0	-854	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9
19	26	-0	778	0	0	0	-1138	--	--	16.08	16.08	0.18	0.02	0.01	0.05	0.00	0.00	20.9
20	26	-0	7	0	0	0	-732	--	--	16.08	16.08	0.18	0.01	0.00	0.00	0.00	0.00	20.9
37	26	-0	-1329	0	0	0	-767	--	--	16.08	16.08	0.18	0.01	0.01	0.08	0.00	0.00	20.9
38	26	-0	1324	0	0	0	-1254	--	--	16.08	16.08	0.18	0.02	0.01	0.08	0.00	0.00	20.9
39	26	-0	40	0	0	0	-578	--	--	16.08	16.08	0.18	0.01	0.00	0.00	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	30	0	0	0	-442	--	--	16.08	16.08	0.18	0.01	0.00	0.00	0.00	0.00	20.9
2	51	-0	-166	0	0	0	-357	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
3	51	-0	-144	0	0	0	-343	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
4	51	-0	190	0	0	0	-410	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
5	51	-0	212	0	0	0	-407	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
6	51	-0	-66	0	0	0	-358	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
7	51	-0	6	0	0	0	-314	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
8	51	-0	40	0	0	0	-366	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
9	51	-0	113	0	0	0	-355	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
10	51	-0	-166	0	0	0	-357	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
11	51	-0	-144	0	0	0	-343	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
12	51	-0	190	0	0	0	-410	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
13	51	-0	212	0	0	0	-407	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
14	51	-0	-66	0	0	0	-358	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
15	51	-0	6	0	0	0	-314	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
16	51	-0	40	0	0	0	-366	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
17	51	-0	113	0	0	0	-355	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
18	51	-0	-814	0	0	0	-854	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9
19	51	-0	778	0	0	0	-1138	--	--	16.08	16.08	0.18	0.02	0.01	0.05	0.00	0.00	20.9
20	51	-0	7	0	0	0	-732	--	--	16.08	16.08	0.18	0.01	0.00	0.00	0.00	0.00	20.9
37	51	-0	-1329	0	0	0	-767	--	--	16.08	16.08	0.18	0.01	0.01	0.08	0.00	0.00	20.9
38	51	-0	1324	0	0	0	-1254	--	--	16.08	16.08	0.18	0.02	0.01	0.08	0.00	0.00	20.9
39	51	-0	40	0	0	0	-578	--	--	16.08	16.08	0.18	0.01	0.00	0.00	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 57 NI 1831 NF 1644 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	759	0	0	0	-533	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9
2	0	-0	383	0	0	0	-372	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
3	0	-0	402	0	0	0	-365	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
4	0	-0	766	0	0	0	-456	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
5	0	-0	784	0	0	0	-448	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
6	0	-0	495	0	0	0	-410	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
7	0	-0	557	0	0	0	-385	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
8	0	-0	610	0	0	0	-436	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
9	0	-0	672	0	0	0	-410	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
10	0	-0	383	0	0	0	-372	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
11	0	-0	402	0	0	0	-365	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
12	0	-0	766	0	0	0	-456	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
13	0	-0	784	0	0	0	-448	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
14	0	-0	495	0	0	0	-410	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
15	0	-0	557	0	0	0	-385	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
16	0	-0	610	0	0	0	-436	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
17	0	-0	672	0	0	0	-410	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
18	0	-0	-15	0	0	0	-690	--	--	16.08	16.08	0.18	0.01	0.00	0.00	0.00	0.00	20.9
19	0	-0	1586	0	0	0	-1115	--	--	16.08	16.08	0.18	0.02	0.01	0.10	0.00	0.00	20.9
20	0	-0	789	0	0	0	-836	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9
37	0	-0	-558	0	0	0	-701	--	--	16.08	16.08	0.18	0.01	0.00	0.04	0.00	0.00	20.9
38	0	-0	2110	0	0	0	-1135	--	--	16.08	16.08	0.18	0.02	0.02	0.13	0.00	0.00	20.9
39	0	-0	781	0	0	0	-670	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	26	-0	759	0	0	0	-533	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9
2	26	-0	383	0	0	0	-372	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
3	26	-0	402	0	0	0	-365	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
4	26	-0	766	0	0	0	-456	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
5	26	-0	784	0	0	0	-448	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
6	26	-0	495	0	0	0	-410	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
7	26	-0	557	0	0	0	-385	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
8	26	-0	610	0	0	0	-436	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
9	26	-0	672	0	0	0	-410	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
10	26	-0	383	0	0	0	-372	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
11	26	-0	402	0	0	0	-365	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
12	26	-0	766	0	0	0	-456	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
13	26	-0	784	0	0	0	-448	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
14	26	-0	495	0	0	0	-410	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
15	26	-0	557	0	0	0	-385	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
16	26	-0	610	0	0	0	-436	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
17	26	-0	672	0	0	0	-410	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
18	26	-0	-15	0	0	0	-690	--	--	16.08	16.08	0.18	0.01	0.00	0.00	0.00	0.00	20.9
19	26	-0	1586	0	0	0	-1115	--	--	16.08	16.08	0.18	0.02	0.01	0.10	0.00	0.00	20.9
20	26	-0	789	0	0	0	-836	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9
37	26	-0	-558	0	0	0	-701	--	--	16.08	16.08	0.18	0.01	0.00	0.04	0.00	0.00	20.9
38	26	-0	2110	0	0	0	-1135	--	--	16.08	16.08	0.18	0.02	0.02	0.13	0.00	0.00	20.9
39	26	-0	781	0	0	0	-670	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	51	-0	759	0	0	0	-533	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9
2	51	-0	383	0	0	0	-372	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
3	51	-0	402	0	0	0	-365	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
4	51	-0	766	0	0	0	-456	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
5	51	-0	784	0	0	0	-448	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
6	51	-0	495	0	0	0	-410	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
7	51	-0	557	0	0	0	-385	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
8	51	-0	610	0	0	0	-436	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
9	51	-0	672	0	0	0	-410	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
10	51	-0	383	0	0	0	-372	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
11	51	-0	402	0	0	0	-365	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
12	51	-0	766	0	0	0	-456	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
13	51	-0	784	0	0	0	-448	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
14	51	-0	495	0	0	0	-410	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
15	51	-0	557	0	0	0	-385	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
16	51	-0	610	0	0	0	-436	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
17	51	-0	672	0	0	0	-410	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
18	51	-0	-15	0	0	0	-690	--	--	16.08	16.08	0.18	0.01	0.00	0.00	0.00	0.00	20.9
19	51	-0	1586	0	0	0	-1115	--	--	16.08	16.08	0.18	0.02	0.01	0.10	0.00	0.00	20.9
20	51	-0	789	0	0	0	-836	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9
37	51	-0	-558	0	0	0	-701	--	--	16.08	16.08	0.18	0.01	0.00	0.04	0.00	0.00	20.9
38	51	-0	2110	0	0	0	-1135	--	--	16.08	16.08	0.18	0.02	0.02	0.13	0.00	0.00	20.9
39	51	-0	781	0	0	0	-670	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 58 NI 1644 NF 1815 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	1692	0	0	0	-432	--	--	16.08	16.08	0.18	0.01	0.01	0.11	0.00	0.00	20.9
2	0	-0	1113	0	0	0	-320	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
3	0	-0	1130	0	0	0	-309	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
4	0	-0	1473	0	0	0	-356	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
5	0	-0	1490	0	0	0	-344	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
6	0	-0	1219	0	0	0	-346	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
7	0	-0	1276	0	0	0	-308	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
8	0	-0	1327	0	0	0	-357	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
9	0	-0	1384	0	0	0	-318	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
10	0	-0	1113	0	0	0	-320	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9

11	0	-0	1130	0	0	0	-309	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
12	0	-0	1473	0	0	0	-356	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
13	0	-0	1490	0	0	0	-344	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
14	0	-0	1219	0	0	0	-346	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
15	0	-0	1276	0	0	0	-308	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
16	0	-0	1327	0	0	0	-357	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
17	0	-0	1384	0	0	0	-318	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
18	0	-0	1058	0	0	0	-702	--	--	16.08	16.08	0.18	0.01	0.01	0.07	0.00	0.00	20.9
19	0	-0	2526	0	0	0	-903	--	--	16.08	16.08	0.18	0.01	0.02	0.16	0.00	0.00	20.9
20	0	-0	1773	0	0	0	-737	--	--	16.08	16.08	0.18	0.01	0.01	0.11	0.00	0.00	20.9
37	0	-0	534	0	0	0	-509	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9
38	0	-0	2980	0	0	0	-844	--	--	16.08	16.08	0.18	0.01	0.02	0.19	0.00	0.00	20.9
39	0	-0	1725	0	0	0	-567	--	--	16.08	16.08	0.18	0.01	0.01	0.11	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	1692	0	0	0	1811	--	--	16.08	16.08	0.00	0.03	0.01	0.11	0.00	0.00	20.9
2	26	-0	1113	0	0	0	-320	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
3	26	-0	1130	0	0	0	-309	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
4	26	-0	1473	0	0	0	1597	--	--	16.08	16.08	0.10	0.03	0.01	0.09	0.00	0.00	20.9
5	26	-0	1490	0	0	0	1631	--	--	16.08	16.08	0.10	0.03	0.01	0.09	0.00	0.00	20.9
6	26	-0	1219	0	0	0	-346	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
7	26	-0	1276	0	0	0	1384	--	--	16.08	16.08	0.10	0.02	0.01	0.08	0.00	0.00	20.9
8	26	-0	1327	0	0	0	-357	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
9	26	-0	1384	0	0	0	1516	--	--	16.08	16.08	0.10	0.03	0.01	0.09	0.00	0.00	20.9
10	26	-0	1113	0	0	0	-320	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
11	26	-0	1130	0	0	0	-309	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
12	26	-0	1473	0	0	0	1597	--	--	16.08	16.08	0.10	0.03	0.01	0.09	0.00	0.00	20.9
13	26	-0	1490	0	0	0	1631	--	--	16.08	16.08	0.10	0.03	0.01	0.09	0.00	0.00	20.9
14	26	-0	1219	0	0	0	-346	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
15	26	-0	1276	0	0	0	1384	--	--	16.08	16.08	0.10	0.02	0.01	0.08	0.00	0.00	20.9
16	26	-0	1327	0	0	0	-357	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
17	26	-0	1384	0	0	0	1516	--	--	16.08	16.08	0.10	0.03	0.01	0.09	0.00	0.00	20.9
18	26	-0	1058	0	0	0	-702	--	--	16.08	16.08	0.18	0.01	0.01	0.07	0.00	0.00	20.9
19	26	-0	2526	0	0	0	-903	--	--	16.08	16.08	0.18	0.01	0.02	0.16	0.00	0.00	20.9
20	26	-0	1773	0	0	0	-737	--	--	16.08	16.08	0.18	0.01	0.01	0.11	0.00	0.00	20.9
37	26	-0	534	0	0	0	-509	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9
38	26	-0	2980	0	0	0	-844	--	--	16.08	16.08	0.18	0.01	0.02	0.19	0.00	0.00	20.9
39	26	-0	1725	0	0	0	-567	--	--	16.08	16.08	0.18	0.01	0.01	0.11	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	1692	0	0	0	437	--	--	16.08	16.08	0.00	0.01	0.01	0.11	0.00	0.00	20.9
2	51	-0	1113	0	0	0	251	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
3	51	-0	1130	0	0	0	272	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
4	51	-0	1473	0	0	0	401	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
5	51	-0	1490	0	0	0	421	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
6	51	-0	1219	0	0	0	280	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
7	51	-0	1276	0	0	0	348	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
8	51	-0	1327	0	0	0	325	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
9	51	-0	1384	0	0	0	393	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
10	51	-0	1113	0	0	0	251	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
11	51	-0	1130	0	0	0	272	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
12	51	-0	1473	0	0	0	401	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
13	51	-0	1490	0	0	0	421	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
14	51	-0	1219	0	0	0	280	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
15	51	-0	1276	0	0	0	348	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
16	51	-0	1327	0	0	0	325	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
17	51	-0	1384	0	0	0	393	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
18	51	-0	1058	0	0	0	-702	--	--	16.08	16.08	0.18	0.01	0.01	0.07	0.00	0.00	20.9
19	51	-0	2526	0	0	0	394	--	--	16.08	16.08	0.00	0.01	0.02	0.16	0.00	0.00	20.9
20	51	-0	1773	0	0	0	174	--	--	16.08	16.08	0.00	0.00	0.01	0.11	0.00	0.00	20.9
37	51	-0	534	0	0	0	-509	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9
38	51	-0	2980	0	0	0	686	--	--	16.08	16.08	0.00	0.01	0.02	0.19	0.00	0.00	20.9
39	51	-0	1725	0	0	0	319	--	--	16.08	16.08	0.00	0.01	0.01	0.11	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 59 NI 1815 NF 1814 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	3151	0	0	0	-10	--	--	16.08	16.08	0.18	0.00	0.03	0.20	0.00	0.00	20.9
2	0	-0	2345	0	0	0	5	--	--	16.08	16.08	0.10	0.00	0.02	0.15	0.00	0.00	20.9
3	0	-0	2363	0	0	0	21	--	--	16.08	16.08	0.10	0.00	0.02	0.15	0.00	0.00	20.9
4	0	-0	2486	0	0	0	-36	--	--	16.08	16.08	0.29	0.00	0.02	0.16	0.00	0.00	20.9
5	0	-0	2504	0	0	0	-20	--	--	16.08	16.08	0.29	0.00	0.02	0.16	0.00	0.00	20.9
6	0	-0	2372	0	0	0	-28	--	--	16.08	16.08	0.29	0.00	0.02	0.15	0.00	0.00	20.9
7	0	-0	2434	0	0	0	25	--	--	16.08	16.08	0.10	0.00	0.02	0.15	0.00	0.00	20.9
8	0	-0	2415	0	0	0	-41	--	--	16.08	16.08	0.29	0.00	0.02	0.15	0.00	0.00	20.9
9	0	-0	2476	0	0	0	13	--	--	16.08	16.08	0.10	0.00	0.02	0.16	0.00	0.00	20.9
10	0	-0	2345	0	0	0	5	--	--	16.08	16.08	0.10	0.00	0.02	0.15	0.00	0.00	20.9
11	0	-0	2363	0	0	0	21	--	--	16.08	16.08	0.10	0.00	0.02	0.15	0.00	0.00	20.9
12	0	-0	2486	0	0	0	-36	--	--	16.08	16.08	0.29	0.00	0.02	0.16	0.00	0.00	20.9
13	0	-0	2504	0	0	0	-20	--	--	16.08	16.08	0.29	0.00	0.02	0.16	0.00	0.00	20.9
14	0	-0	2372	0	0	0	-28	--	--	16.08	16.08	0.29	0.00	0.02	0.15	0.00	0.00	20.9
15	0	-0	2434	0	0	0	25	--	--	16.08	16.08	0.10	0.00	0.02	0.15	0.00	0.00	20.9
16	0	-0	2415	0	0	0	-41	--	--	16.08	16.08	0.29	0.00	0.02	0.15	0.00	0.00	20.9
17	0	-0	2476	0	0	0	13	--	--	16.08	16.08	0.10	0.00	0.02	0.16	0.00	0.00	20.9
18	0	-0	2968	0	0	0	-296	--	--	16.08	16.08	0.18	0.00	0.02	0.19	0.00	0.00	20.9
19	0	-0	3691	0	0	0	-445	--	--	16.08	16.08	0.18	0.01	0.03	0.23	0.00	0.00	20.9
20	0	-0	3286	0	0	0	-307	--	--	16.08	16.08	0.18	0.01	0.03	0.21	0.00	0.00	20.9
37	0	-0	2664	0	0	0	-124	--	--	16.08	16.08	0.18	0.00	0.02	0.17	0.00	0.00	20.9
38	0	-0	3870	0	0	0	-372	--	--	16.08	16.08	0.18	0.01	0.03	0.24	0.00	0.00	20.9
39	0	-0	3196	0	0	0	-143	--	--	16.08	16.08	0.18	0.00	0.03	0.20	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	3151	0	0	0	4167	--	--	16.08	16.08	0.00	0.07	0.03	0.20	0.00	0.00	20.9
2	26	-0	2345	0	0	0	3113	--	--	16.08	16.08	0.10	0.06	0.02	0.15	0.00	0.00	20.9
3	26	-0	2363	0	0	0	3153	--	--	16.08	16.08	0.10	0.06	0.02	0.15	0.00	0.00	20.9
4	26	-0	2486	0	0	0	3259	--	--	16.08	16.08	0.10	0.06	0.02	0.16	0.00	0.00	20.9
5	26	-0	2504	0	0	0	3299	--	--	16.08	16.08	0.10	0.06	0.02	0.16	0.00	0.00	20.9
6	26	-0	2372	0	0	0	3116	--	--	16.08	16.08	0.10	0.06	0.02	0.15	0.00	0.00	20.9

7	26	-0	2434	0	0	0	3251	--	--	16.08	16.08	0.10	0.06	0.02	0.15	0.00	0.00	20.9
8	26	-0	2415	0	0	0	3161	--	--	16.08	16.08	0.10	0.06	0.02	0.15	0.00	0.00	20.9
9	26	-0	2476	0	0	0	3295	--	--	16.08	16.08	0.10	0.06	0.02	0.16	0.00	0.00	20.9
10	26	-0	2345	0	0	0	3113	--	--	16.08	16.08	0.10	0.06	0.02	0.15	0.00	0.00	20.9
11	26	-0	2363	0	0	0	3153	--	--	16.08	16.08	0.10	0.06	0.02	0.15	0.00	0.00	20.9
12	26	-0	2486	0	0	0	3259	--	--	16.08	16.08	0.10	0.06	0.02	0.16	0.00	0.00	20.9
13	26	-0	2504	0	0	0	3299	--	--	16.08	16.08	0.10	0.06	0.02	0.16	0.00	0.00	20.9
14	26	-0	2372	0	0	0	3116	--	--	16.08	16.08	0.10	0.06	0.02	0.15	0.00	0.00	20.9
15	26	-0	2434	0	0	0	3251	--	--	16.08	16.08	0.10	0.06	0.02	0.15	0.00	0.00	20.9
16	26	-0	2415	0	0	0	3161	--	--	16.08	16.08	0.10	0.06	0.02	0.15	0.00	0.00	20.9
17	26	-0	2476	0	0	0	3295	--	--	16.08	16.08	0.10	0.06	0.02	0.16	0.00	0.00	20.9
18	26	-0	2968	0	0	0	3638	--	--	16.08	16.08	0.00	0.06	0.02	0.19	0.00	0.00	20.9
19	26	-0	3691	0	0	0	4448	--	--	16.08	16.08	0.00	0.08	0.03	0.23	0.00	0.00	20.9
20	26	-0	3286	0	0	0	4049	--	--	16.08	16.08	0.00	0.07	0.03	0.21	0.00	0.00	20.9
37	26	-0	2664	0	0	0	3407	--	--	16.08	16.08	0.00	0.06	0.02	0.17	0.00	0.00	20.9
38	26	-0	3870	0	0	0	4758	--	--	16.08	16.08	0.00	0.08	0.03	0.24	0.00	0.00	20.9
39	26	-0	3196	0	0	0	4094	--	--	16.08	16.08	0.00	0.07	0.03	0.20	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	3151	0	0	0	1608	--	--	16.08	16.08	0.00	0.03	0.03	0.20	0.00	0.00	20.9
2	51	-0	2345	0	0	0	1209	--	--	16.08	16.08	0.10	0.02	0.02	0.15	0.00	0.00	20.9
3	51	-0	2363	0	0	0	1234	--	--	16.08	16.08	0.10	0.02	0.02	0.15	0.00	0.00	20.9
4	51	-0	2486	0	0	0	1240	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
5	51	-0	2504	0	0	0	1266	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
6	51	-0	2372	0	0	0	1190	--	--	16.08	16.08	0.10	0.02	0.02	0.15	0.00	0.00	20.9
7	51	-0	2434	0	0	0	1275	--	--	16.08	16.08	0.10	0.02	0.02	0.15	0.00	0.00	20.9
8	51	-0	2415	0	0	0	1200	--	--	16.08	16.08	0.10	0.02	0.02	0.15	0.00	0.00	20.9
9	51	-0	2476	0	0	0	1284	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
10	51	-0	2345	0	0	0	1209	--	--	16.08	16.08	0.10	0.02	0.02	0.15	0.00	0.00	20.9
11	51	-0	2363	0	0	0	1234	--	--	16.08	16.08	0.10	0.02	0.02	0.15	0.00	0.00	20.9
12	51	-0	2486	0	0	0	1240	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
13	51	-0	2504	0	0	0	1266	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
14	51	-0	2372	0	0	0	1190	--	--	16.08	16.08	0.10	0.02	0.02	0.15	0.00	0.00	20.9
15	51	-0	2434	0	0	0	1275	--	--	16.08	16.08	0.10	0.02	0.02	0.15	0.00	0.00	20.9
16	51	-0	2415	0	0	0	1200	--	--	16.08	16.08	0.10	0.02	0.02	0.15	0.00	0.00	20.9
17	51	-0	2476	0	0	0	1284	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
18	51	-0	2968	0	0	0	1228	--	--	16.08	16.08	0.00	0.02	0.02	0.19	0.00	0.00	20.9
19	51	-0	3691	0	0	0	1451	--	--	16.08	16.08	0.00	0.02	0.03	0.23	0.00	0.00	20.9
20	51	-0	3286	0	0	0	1381	--	--	16.08	16.08	0.00	0.02	0.03	0.21	0.00	0.00	20.9
37	51	-0	2664	0	0	0	1244	--	--	16.08	16.08	0.00	0.02	0.02	0.17	0.00	0.00	20.9
38	51	-0	3870	0	0	0	1616	--	--	16.08	16.08	0.00	0.03	0.03	0.24	0.00	0.00	20.9
39	51	-0	3196	0	0	0	1499	--	--	16.08	16.08	0.00	0.03	0.03	0.20	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 60 NI 1814 NF 1833 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	4701	0	0	0	854	--	--	16.08	16.08	0.00	0.01	0.04	0.29	0.00	0.00	20.9
2	0	-0	3863	0	0	0	736	--	--	16.08	16.08	0.10	0.01	0.03	0.24	0.00	0.00	20.9
3	0	-0	3888	0	0	0	759	--	--	16.08	16.08	0.10	0.01	0.03	0.24	0.00	0.00	20.9
4	0	-0	3345	0	0	0	554	--	--	16.08	16.08	0.10	0.01	0.03	0.21	0.00	0.00	20.9
5	0	-0	3369	0	0	0	577	--	--	16.08	16.08	0.10	0.01	0.03	0.21	0.00	0.00	20.9
6	0	-0	3653	0	0	0	646	--	--	16.08	16.08	0.10	0.01	0.03	0.23	0.00	0.00	20.9
7	0	-0	3735	0	0	0	722	--	--	16.08	16.08	0.10	0.01	0.03	0.23	0.00	0.00	20.9
8	0	-0	3497	0	0	0	592	--	--	16.08	16.08	0.10	0.01	0.03	0.22	0.00	0.00	20.9
9	0	-0	3580	0	0	0	667	--	--	16.08	16.08	0.10	0.01	0.03	0.22	0.00	0.00	20.9
10	0	-0	3863	0	0	0	736	--	--	16.08	16.08	0.10	0.01	0.03	0.24	0.00	0.00	20.9
11	0	-0	3888	0	0	0	759	--	--	16.08	16.08	0.10	0.01	0.03	0.24	0.00	0.00	20.9
12	0	-0	3345	0	0	0	554	--	--	16.08	16.08	0.10	0.01	0.03	0.21	0.00	0.00	20.9
13	0	-0	3369	0	0	0	577	--	--	16.08	16.08	0.10	0.01	0.03	0.21	0.00	0.00	20.9
14	0	-0	3653	0	0	0	646	--	--	16.08	16.08	0.10	0.01	0.03	0.23	0.00	0.00	20.9
15	0	-0	3735	0	0	0	722	--	--	16.08	16.08	0.10	0.01	0.03	0.23	0.00	0.00	20.9
16	0	-0	3497	0	0	0	592	--	--	16.08	16.08	0.10	0.01	0.03	0.22	0.00	0.00	20.9
17	0	-0	3580	0	0	0	667	--	--	16.08	16.08	0.10	0.01	0.03	0.22	0.00	0.00	20.9
18	0	-0	5575	0	0	0	762	--	--	16.08	16.08	0.00	0.01	0.05	0.35	0.00	0.00	20.9
19	0	-0	4220	0	0	0	243	--	--	16.08	16.08	0.00	0.00	0.03	0.26	0.00	0.00	20.9
20	0	-0	4849	0	0	0	562	--	--	16.08	16.08	0.00	0.01	0.04	0.30	0.00	0.00	20.9
37	0	-0	5958	0	0	0	1055	--	--	16.08	16.08	0.00	0.02	0.05	0.37	0.00	0.00	20.9
38	0	-0	3699	0	0	0	189	--	--	16.08	16.08	0.00	0.00	0.03	0.23	0.00	0.00	20.9
39	0	-0	4747	0	0	0	721	--	--	16.08	16.08	0.00	0.01	0.04	0.30	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	4701	0	0	0	7085	--	--	16.08	16.08	0.00	0.12	0.04	0.29	0.00	0.00	20.9
2	26	-0	3863	0	0	0	5857	--	--	16.08	16.08	0.10	0.10	0.03	0.24	0.00	0.00	20.9
3	26	-0	3888	0	0	0	5913	--	--	16.08	16.08	0.10	0.10	0.03	0.24	0.00	0.00	20.9
4	26	-0	3345	0	0	0	4988	--	--	16.08	16.08	0.10	0.09	0.03	0.21	0.00	0.00	20.9
5	26	-0	3369	0	0	0	5043	--	--	16.08	16.08	0.10	0.09	0.03	0.21	0.00	0.00	20.9
6	26	-0	3653	0	0	0	5488	--	--	16.08	16.08	0.10	0.10	0.03	0.23	0.00	0.00	20.9
7	26	-0	3735	0	0	0	5673	--	--	16.08	16.08	0.10	0.10	0.03	0.23	0.00	0.00	20.9
8	26	-0	3497	0	0	0	5227	--	--	16.08	16.08	0.10	0.09	0.03	0.22	0.00	0.00	20.9
9	26	-0	3580	0	0	0	5413	--	--	16.08	16.08	0.10	0.10	0.03	0.22	0.00	0.00	20.9
10	26	-0	3863	0	0	0	5857	--	--	16.08	16.08	0.10	0.10	0.03	0.24	0.00	0.00	20.9
11	26	-0	3888	0	0	0	5913	--	--	16.08	16.08	0.10	0.10	0.03	0.24	0.00	0.00	20.9
12	26	-0	3345	0	0	0	4988	--	--	16.08	16.08	0.10	0.09	0.03	0.21	0.00	0.00	20.9
13	26	-0	3369	0	0	0	5043	--	--	16.08	16.08	0.10	0.09	0.03	0.21	0.00	0.00	20.9
14	26	-0	3653	0	0	0	5488	--	--	16.08	16.08	0.10	0.10	0.03	0.23	0.00	0.00	20.9
15	26	-0	3735	0	0	0	5673	--	--	16.08	16.08	0.10	0.10	0.03	0.23	0.00	0.00	20.9
16	26	-0	3497	0	0	0	5227	--	--	16.08	16.08	0.10	0.09	0.03	0.22	0.00	0.00	20.9
17	26	-0	3580	0	0	0	5413	--	--	16.08	16.08	0.10	0.10	0.03	0.22	0.00	0.00	20.9
18	26	-0	5575	0	0	0	8153	--	--	16.08	16.08	0.00	0.14	0.05	0.35	0.00	0.00	20.9
19	26	-0	4220	0	0	0	5837	--	--	16.08	16.08	0.00	0.10	0.03	0.26	0.00	0.00	20.9
20	26	-0	4849	0	0	0	6990	--	--	16.08	16.08	0.00	0.12	0.04	0.30	0.00	0.00	20.9
37	26	-0	5958	0	0	0	8953	--	--	16.08	16.08	0.00	0.15	0.05	0.37	0.00	0.00	20.9
38	26	-0	3699	0	0	0	5093	--	--	16.08	16.08	0.00	0.09	0.03	0.23	0.00	0.00	20.9
39	26	-0	4747	0	0	0	7014	--	--	16.08	16.08	0.00	0.12	0.04	0.30	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	4701	0	0	0	3268	--	--	16.08	16.08	0.00	0.06	0.04	0.29	0.00	0.00	20.9
2	51	-0	3863	0	0	0	2720	--	--	16.08	16.08	0.10	0.05	0.03	0.24	0.00	0.00	20.9

3	51	-0	3888	0	0	0	2756	--	--	16.08	16.08	0.10	0.05	0.03	0.24	0.00	0.00	20.9
4	51	-0	3345	0	0	0	2272	--	--	16.08	16.08	0.10	0.04	0.03	0.21	0.00	0.00	20.9
5	51	-0	3369	0	0	0	2308	--	--	16.08	16.08	0.10	0.04	0.03	0.21	0.00	0.00	20.9
6	51	-0	3653	0	0	0	2522	--	--	16.08	16.08	0.10	0.04	0.03	0.23	0.00	0.00	20.9
7	51	-0	3735	0	0	0	2640	--	--	16.08	16.08	0.10	0.05	0.03	0.23	0.00	0.00	20.9
8	51	-0	3497	0	0	0	2388	--	--	16.08	16.08	0.10	0.04	0.03	0.22	0.00	0.00	20.9
9	51	-0	3580	0	0	0	2506	--	--	16.08	16.08	0.10	0.04	0.03	0.22	0.00	0.00	20.9
10	51	-0	3863	0	0	0	2720	--	--	16.08	16.08	0.10	0.05	0.03	0.24	0.00	0.00	20.9
11	51	-0	3888	0	0	0	2756	--	--	16.08	16.08	0.10	0.05	0.03	0.24	0.00	0.00	20.9
12	51	-0	3345	0	0	0	2272	--	--	16.08	16.08	0.10	0.04	0.03	0.21	0.00	0.00	20.9
13	51	-0	3369	0	0	0	2308	--	--	16.08	16.08	0.10	0.04	0.03	0.21	0.00	0.00	20.9
14	51	-0	3653	0	0	0	2522	--	--	16.08	16.08	0.10	0.04	0.03	0.23	0.00	0.00	20.9
15	51	-0	3735	0	0	0	2640	--	--	16.08	16.08	0.10	0.05	0.03	0.23	0.00	0.00	20.9
16	51	-0	3497	0	0	0	2388	--	--	16.08	16.08	0.10	0.04	0.03	0.22	0.00	0.00	20.9
17	51	-0	3580	0	0	0	2506	--	--	16.08	16.08	0.10	0.04	0.03	0.22	0.00	0.00	20.9
18	51	-0	5575	0	0	0	3626	--	--	16.08	16.08	0.00	0.06	0.05	0.35	0.00	0.00	20.9
19	51	-0	4220	0	0	0	2411	--	--	16.08	16.08	0.00	0.04	0.03	0.26	0.00	0.00	20.9
20	51	-0	4849	0	0	0	3053	--	--	16.08	16.08	0.00	0.05	0.04	0.30	0.00	0.00	20.9
37	51	-0	5958	0	0	0	4115	--	--	16.08	16.08	0.00	0.07	0.05	0.37	0.00	0.00	20.9
38	51	-0	3699	0	0	0	2089	--	--	16.08	16.08	0.00	0.04	0.03	0.23	0.00	0.00	20.9
39	51	-0	4747	0	0	0	3160	--	--	16.08	16.08	0.00	0.05	0.04	0.30	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 61 NI 1833 NF 1845 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	3996	0	0	0	2655	--	--	16.08	16.08	0.00	0.05	0.03	0.25	0.00	0.00	20.9
2	0	-0	3489	0	0	0	2210	--	--	16.08	16.08	0.10	0.04	0.03	0.22	0.00	0.00	20.9
3	0	-0	3528	0	0	0	2248	--	--	16.08	16.08	0.10	0.04	0.03	0.22	0.00	0.00	20.9
4	0	-0	2620	0	0	0	1837	--	--	16.08	16.08	0.10	0.03	0.02	0.16	0.00	0.00	20.9
5	0	-0	2659	0	0	0	1875	--	--	16.08	16.08	0.10	0.03	0.02	0.17	0.00	0.00	20.9
6	0	-0	3140	0	0	0	2036	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
7	0	-0	3269	0	0	0	2161	--	--	16.08	16.08	0.10	0.04	0.03	0.21	0.00	0.00	20.9
8	0	-0	2879	0	0	0	1924	--	--	16.08	16.08	0.10	0.03	0.02	0.18	0.00	0.00	20.9
9	0	-0	3008	0	0	0	2049	--	--	16.08	16.08	0.10	0.04	0.02	0.19	0.00	0.00	20.9
10	0	-0	3489	0	0	0	2210	--	--	16.08	16.08	0.10	0.04	0.03	0.22	0.00	0.00	20.9
11	0	-0	3528	0	0	0	2248	--	--	16.08	16.08	0.10	0.04	0.03	0.22	0.00	0.00	20.9
12	0	-0	2620	0	0	0	1837	--	--	16.08	16.08	0.10	0.03	0.02	0.16	0.00	0.00	20.9
13	0	-0	2659	0	0	0	1875	--	--	16.08	16.08	0.10	0.03	0.02	0.17	0.00	0.00	20.9
14	0	-0	3140	0	0	0	2036	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
15	0	-0	3269	0	0	0	2161	--	--	16.08	16.08	0.10	0.04	0.03	0.21	0.00	0.00	20.9
16	0	-0	2879	0	0	0	1924	--	--	16.08	16.08	0.10	0.03	0.02	0.18	0.00	0.00	20.9
17	0	-0	3008	0	0	0	2049	--	--	16.08	16.08	0.10	0.04	0.02	0.19	0.00	0.00	20.9
18	0	-0	5131	0	0	0	2789	--	--	16.08	16.08	0.00	0.05	0.04	0.32	0.00	0.00	20.9
19	0	-0	2796	0	0	0	1773	--	--	16.08	16.08	0.00	0.03	0.02	0.18	0.00	0.00	20.9
20	0	-0	3992	0	0	0	2341	--	--	16.08	16.08	0.00	0.04	0.03	0.25	0.00	0.00	20.9
37	0	-0	5914	0	0	0	3254	--	--	16.08	16.08	0.00	0.06	0.05	0.37	0.00	0.00	20.9
38	0	-0	2023	0	0	0	1561	--	--	16.08	16.08	0.00	0.03	0.02	0.13	0.00	0.00	20.9
39	0	-0	4016	0	0	0	2507	--	--	16.08	16.08	0.00	0.04	0.03	0.25	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	3996	0	0	0	7952	--	--	16.08	16.08	0.00	0.14	0.03	0.25	0.00	0.00	20.9
2	26	-0	3489	0	0	0	6835	--	--	16.08	16.08	0.10	0.12	0.03	0.22	0.00	0.00	20.9
3	26	-0	3528	0	0	0	6925	--	--	16.08	16.08	0.10	0.12	0.03	0.22	0.00	0.00	20.9
4	26	-0	2620	0	0	0	5310	--	--	16.08	16.08	0.10	0.09	0.02	0.16	0.00	0.00	20.9
5	26	-0	2659	0	0	0	5399	--	--	16.08	16.08	0.10	0.10	0.02	0.17	0.00	0.00	20.9
6	26	-0	3140	0	0	0	6198	--	--	16.08	16.08	0.10	0.11	0.03	0.20	0.00	0.00	20.9
7	26	-0	3269	0	0	0	6494	--	--	16.08	16.08	0.10	0.12	0.03	0.21	0.00	0.00	20.9
8	26	-0	2879	0	0	0	5740	--	--	16.08	16.08	0.10	0.10	0.02	0.18	0.00	0.00	20.9
9	26	-0	3008	0	0	0	6036	--	--	16.08	16.08	0.10	0.11	0.02	0.19	0.00	0.00	20.9
10	26	-0	3489	0	0	0	6835	--	--	16.08	16.08	0.10	0.12	0.03	0.22	0.00	0.00	20.9
11	26	-0	3528	0	0	0	6925	--	--	16.08	16.08	0.10	0.12	0.03	0.22	0.00	0.00	20.9
12	26	-0	2620	0	0	0	5310	--	--	16.08	16.08	0.10	0.09	0.02	0.16	0.00	0.00	20.9
13	26	-0	2659	0	0	0	5399	--	--	16.08	16.08	0.10	0.10	0.02	0.17	0.00	0.00	20.9
14	26	-0	3140	0	0	0	6198	--	--	16.08	16.08	0.10	0.11	0.03	0.20	0.00	0.00	20.9
15	26	-0	3269	0	0	0	6494	--	--	16.08	16.08	0.10	0.12	0.03	0.21	0.00	0.00	20.9
16	26	-0	2879	0	0	0	5740	--	--	16.08	16.08	0.10	0.10	0.02	0.18	0.00	0.00	20.9
17	26	-0	3008	0	0	0	6036	--	--	16.08	16.08	0.10	0.11	0.02	0.19	0.00	0.00	20.9
18	26	-0	5131	0	0	0	9591	--	--	16.08	16.08	0.00	0.16	0.04	0.32	0.00	0.00	20.9
19	26	-0	2796	0	0	0	5480	--	--	16.08	16.08	0.00	0.09	0.02	0.18	0.00	0.00	20.9
20	26	-0	3992	0	0	0	7632	--	--	16.08	16.08	0.00	0.13	0.03	0.25	0.00	0.00	20.9
37	26	-0	5914	0	0	0	11094	--	--	16.08	16.08	0.00	0.19	0.05	0.37	0.00	0.00	20.9
38	26	-0	2023	0	0	0	4243	--	--	16.08	16.08	0.00	0.07	0.02	0.13	0.00	0.00	20.9
39	26	-0	4016	0	0	0	7831	--	--	16.08	16.08	0.00	0.13	0.03	0.25	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	3996	0	0	0	4708	--	--	16.08	16.08	0.00	0.08	0.03	0.25	0.00	0.00	20.9
2	51	-0	3489	0	0	0	4002	--	--	16.08	16.08	0.10	0.07	0.03	0.22	0.00	0.00	20.9
3	51	-0	3528	0	0	0	4060	--	--	16.08	16.08	0.10	0.07	0.03	0.22	0.00	0.00	20.9
4	51	-0	2620	0	0	0	3183	--	--	16.08	16.08	0.10	0.06	0.02	0.16	0.00	0.00	20.9
5	51	-0	2659	0	0	0	3240	--	--	16.08	16.08	0.10	0.06	0.02	0.17	0.00	0.00	20.9
6	51	-0	3140	0	0	0	3649	--	--	16.08	16.08	0.10	0.06	0.03	0.20	0.00	0.00	20.9
7	51	-0	3269	0	0	0	3840	--	--	16.08	16.08	0.10	0.07	0.03	0.21	0.00	0.00	20.9
8	51	-0	2879	0	0	0	3403	--	--	16.08	16.08	0.10	0.06	0.02	0.18	0.00	0.00	20.9
9	51	-0	3008	0	0	0	3594	--	--	16.08	16.08	0.10	0.06	0.02	0.19	0.00	0.00	20.9
10	51	-0	3489	0	0	0	4002	--	--	16.08	16.08	0.10	0.07	0.03	0.22	0.00	0.00	20.9
11	51	-0	3528	0	0	0	4060	--	--	16.08	16.08	0.10	0.07	0.03	0.22	0.00	0.00	20.9
12	51	-0	2620	0	0	0	3183	--	--	16.08	16.08	0.10	0.06	0.02	0.16	0.00	0.00	20.9
13	51	-0	2659	0	0	0	3240	--	--	16.08	16.08	0.10	0.06	0.02	0.17	0.00	0.00	20.9
14	51	-0	3140	0	0	0	3649	--	--	16.08	16.08	0.10	0.06	0.03	0.20	0.00	0.00	20.9
15	51	-0	3269	0	0	0	3840	--	--	16.08	16.08	0.10	0.07	0.03	0.21	0.00	0.00	20.9
16	51	-0	2879	0	0	0	3403	--	--	16.08	16.08	0.10	0.06	0.02	0.18	0.00	0.00	20.9
17	51	-0	3008	0	0	0	3594	--	--	16.08	16.08	0.10	0.06	0.02	0.19	0.00	0.00	20.9
18	51	-0	5131	0	0	0	5425	--	--	16.08	16.08	0.00	0.09	0.04	0.32	0.00	0.00	20.9
19	51	-0	2796	0	0	0	3210	--	--	16.08	16.08	0.00	0.05	0.02	0.18	0.00	0.00	20.9
20	51	-0	3992	0	0	0	4391	--	--	16.08	16.08	0.00	0.07	0.03	0.25	0.00	0.00	20.9
37	51	-0	5914	0	0	0	6292	--	--	16.08	16.08	0.00	0.11	0.05	0.37	0.00	0.00	20.9
38	51	-0	2023	0	0	0	2601	--	--	16.08	16.08	0.00	0.04	0.02	0.13	0.00	0.00	20.9
39	51	-0	4016	0	0	0	4570	--	--	16.08	16.08	0.00	0.08	0.03	0.25	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 62 NI 1845 NF 1809 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-8062	0	0	0	6829	--	--	16.08	16.08	0.00	0.12	0.07	0.51	0.00	0.00	20.9
2	0	-0	-6421	0	0	0	5851	--	--	16.08	16.08	0.10	0.10	0.05	0.40	0.00	0.00	20.9
3	0	-0	-6444	0	0	0	5933	--	--	16.08	16.08	0.10	0.11	0.05	0.40	0.00	0.00	20.9
4	0	-0	-5959	0	0	0	4573	--	--	16.08	16.08	0.10	0.08	0.05	0.37	0.00	0.00	20.9
5	0	-0	-5983	0	0	0	4655	--	--	16.08	16.08	0.10	0.08	0.05	0.38	0.00	0.00	20.9
6	0	-0	-6231	0	0	0	5309	--	--	16.08	16.08	0.10	0.09	0.05	0.39	0.00	0.00	20.9
7	0	-0	-6310	0	0	0	5581	--	--	16.08	16.08	0.10	0.10	0.05	0.40	0.00	0.00	20.9
8	0	-0	-6093	0	0	0	4925	--	--	16.08	16.08	0.10	0.09	0.05	0.38	0.00	0.00	20.9
9	0	-0	-6172	0	0	0	5197	--	--	16.08	16.08	0.10	0.09	0.05	0.39	0.00	0.00	20.9
10	0	-0	-6421	0	0	0	5851	--	--	16.08	16.08	0.10	0.10	0.05	0.40	0.00	0.00	20.9
11	0	-0	-6444	0	0	0	5933	--	--	16.08	16.08	0.10	0.11	0.05	0.40	0.00	0.00	20.9
12	0	-0	-5959	0	0	0	4573	--	--	16.08	16.08	0.10	0.08	0.05	0.37	0.00	0.00	20.9
13	0	-0	-5983	0	0	0	4655	--	--	16.08	16.08	0.10	0.08	0.05	0.38	0.00	0.00	20.9
14	0	-0	-6231	0	0	0	5309	--	--	16.08	16.08	0.10	0.09	0.05	0.39	0.00	0.00	20.9
15	0	-0	-6310	0	0	0	5581	--	--	16.08	16.08	0.10	0.10	0.05	0.40	0.00	0.00	20.9
16	0	-0	-6093	0	0	0	4925	--	--	16.08	16.08	0.10	0.09	0.05	0.38	0.00	0.00	20.9
17	0	-0	-6172	0	0	0	5197	--	--	16.08	16.08	0.10	0.09	0.05	0.39	0.00	0.00	20.9
18	0	-0	-9019	0	0	0	7887	--	--	16.08	16.08	0.00	0.13	0.07	0.57	0.00	0.00	20.9
19	0	-0	-7495	0	0	0	4335	--	--	16.08	16.08	0.00	0.07	0.06	0.47	0.00	0.00	20.9
20	0	-0	-8201	0	0	0	6213	--	--	16.08	16.08	0.00	0.11	0.07	0.51	0.00	0.00	20.9
37	0	-0	-9446	0	0	0	9318	--	--	16.08	16.08	0.00	0.16	0.08	0.59	0.00	0.00	20.9
38	0	-0	-6906	0	0	0	3398	--	--	16.08	16.08	0.00	0.06	0.06	0.43	0.00	0.00	20.9
39	0	-0	-8083	0	0	0	6529	--	--	16.08	16.08	0.00	0.11	0.07	0.51	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	26	-0	-8062	0	0	0	6829	--	--	16.08	16.08	0.00	0.12	0.07	0.51	0.00	0.00	20.9
2	26	-0	-6421	0	0	0	5851	--	--	16.08	16.08	0.10	0.10	0.05	0.40	0.00	0.00	20.9
3	26	-0	-6444	0	0	0	5933	--	--	16.08	16.08	0.10	0.11	0.05	0.40	0.00	0.00	20.9
4	26	-0	-5959	0	0	0	4573	--	--	16.08	16.08	0.10	0.08	0.05	0.37	0.00	0.00	20.9
5	26	-0	-5983	0	0	0	4655	--	--	16.08	16.08	0.10	0.08	0.05	0.38	0.00	0.00	20.9
6	26	-0	-6231	0	0	0	5309	--	--	16.08	16.08	0.10	0.09	0.05	0.39	0.00	0.00	20.9
7	26	-0	-6310	0	0	0	5581	--	--	16.08	16.08	0.10	0.10	0.05	0.40	0.00	0.00	20.9
8	26	-0	-6093	0	0	0	4925	--	--	16.08	16.08	0.10	0.09	0.05	0.38	0.00	0.00	20.9
9	26	-0	-6172	0	0	0	5197	--	--	16.08	16.08	0.10	0.09	0.05	0.39	0.00	0.00	20.9
10	26	-0	-6421	0	0	0	5851	--	--	16.08	16.08	0.10	0.10	0.05	0.40	0.00	0.00	20.9
11	26	-0	-6444	0	0	0	5933	--	--	16.08	16.08	0.10	0.11	0.05	0.40	0.00	0.00	20.9
12	26	-0	-5959	0	0	0	4573	--	--	16.08	16.08	0.10	0.08	0.05	0.37	0.00	0.00	20.9
13	26	-0	-5983	0	0	0	4655	--	--	16.08	16.08	0.10	0.08	0.05	0.38	0.00	0.00	20.9
14	26	-0	-6231	0	0	0	5309	--	--	16.08	16.08	0.10	0.09	0.05	0.39	0.00	0.00	20.9
15	26	-0	-6310	0	0	0	5581	--	--	16.08	16.08	0.10	0.10	0.05	0.40	0.00	0.00	20.9
16	26	-0	-6093	0	0	0	4925	--	--	16.08	16.08	0.10	0.09	0.05	0.38	0.00	0.00	20.9
17	26	-0	-6172	0	0	0	5197	--	--	16.08	16.08	0.10	0.09	0.05	0.39	0.00	0.00	20.9
18	26	-0	-9019	0	0	0	7887	--	--	16.08	16.08	0.00	0.13	0.07	0.57	0.00	0.00	20.9
19	26	-0	-7495	0	0	0	4335	--	--	16.08	16.08	0.00	0.07	0.06	0.47	0.00	0.00	20.9
20	26	-0	-8201	0	0	0	6213	--	--	16.08	16.08	0.00	0.11	0.07	0.51	0.00	0.00	20.9
37	26	-0	-9446	0	0	0	9318	--	--	16.08	16.08	0.00	0.16	0.08	0.59	0.00	0.00	20.9
38	26	-0	-6906	0	0	0	3398	--	--	16.08	16.08	0.00	0.06	0.06	0.43	0.00	0.00	20.9
39	26	-0	-8083	0	0	0	6529	--	--	16.08	16.08	0.00	0.11	0.07	0.51	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	51	-0	-8062	0	0	0	2688	--	--	16.08	16.08	0.00	0.05	0.07	0.51	0.00	0.00	20.9
2	51	-0	-6421	0	0	0	2554	--	--	16.08	16.08	0.10	0.05	0.05	0.40	0.00	0.00	20.9
3	51	-0	-6444	0	0	0	2623	--	--	16.08	16.08	0.10	0.05	0.05	0.40	0.00	0.00	20.9
4	51	-0	-5959	0	0	0	1512	--	--	16.08	16.08	0.10	0.03	0.05	0.37	0.00	0.00	20.9
5	51	-0	-5983	0	0	0	1582	--	--	16.08	16.08	0.10	0.03	0.05	0.38	0.00	0.00	20.9
6	51	-0	-6231	0	0	0	2108	--	--	16.08	16.08	0.10	0.04	0.05	0.39	0.00	0.00	20.9
7	51	-0	-6310	0	0	0	2340	--	--	16.08	16.08	0.10	0.04	0.05	0.40	0.00	0.00	20.9
8	51	-0	-6093	0	0	0	1796	--	--	16.08	16.08	0.10	0.03	0.05	0.38	0.00	0.00	20.9
9	51	-0	-6172	0	0	0	2027	--	--	16.08	16.08	0.10	0.04	0.05	0.39	0.00	0.00	20.9
10	51	-0	-6421	0	0	0	2554	--	--	16.08	16.08	0.10	0.05	0.05	0.40	0.00	0.00	20.9
11	51	-0	-6444	0	0	0	2623	--	--	16.08	16.08	0.10	0.05	0.05	0.40	0.00	0.00	20.9
12	51	-0	-5959	0	0	0	1512	--	--	16.08	16.08	0.10	0.03	0.05	0.37	0.00	0.00	20.9
13	51	-0	-5983	0	0	0	1582	--	--	16.08	16.08	0.10	0.03	0.05	0.38	0.00	0.00	20.9
14	51	-0	-6231	0	0	0	2108	--	--	16.08	16.08	0.10	0.04	0.05	0.39	0.00	0.00	20.9
15	51	-0	-6310	0	0	0	2340	--	--	16.08	16.08	0.10	0.04	0.05	0.40	0.00	0.00	20.9
16	51	-0	-6093	0	0	0	1796	--	--	16.08	16.08	0.10	0.03	0.05	0.38	0.00	0.00	20.9
17	51	-0	-6172	0	0	0	2027	--	--	16.08	16.08	0.10	0.04	0.05	0.39	0.00	0.00	20.9
18	51	-0	-9019	0	0	0	3254	--	--	16.08	16.08	0.00	0.06	0.07	0.57	0.00	0.00	20.9
19	51	-0	-7495	0	0	0	485	--	--	16.08	16.08	0.00	0.01	0.06	0.47	0.00	0.00	20.9
20	51	-0	-8201	0	0	0	2000	--	--	16.08	16.08	0.00	0.03	0.07	0.51	0.00	0.00	20.9
37	51	-0	-9446	0	0	0	4466	--	--	16.08	16.08	0.00	0.08	0.08	0.59	0.00	0.00	20.9
38	51	-0	-6906	0	0	0	-149	--	--	16.08	16.08	0.18	0.00	0.06	0.43	0.00	0.00	20.9
39	51	-0	-8083	0	0	0	2377	--	--	16.08	16.08	0.00	0.04	0.07	0.51	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 63 NI 1809 NF 1828 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-6266	0	0	0	2688	--	--	16.08	16.08	0.00	0.05	0.05	0.39	0.00	0.00	20.9
2	0	-0	-5032	0	0	0	2554	--	--	16.08	16.08	0.10	0.05	0.04	0.32	0.00	0.00	20.9
3	0	-0	-5055	0	0	0	2623	--	--	16.08	16.08	0.10	0.05	0.04	0.32	0.00	0.00	20.9
4	0	-0	-4585	0	0	0	1512	--	--	16.08	16.08	0.10	0.03	0.04	0.29	0.00	0.00	20.9
5	0	-0	-4608	0	0	0	1582	--	--	16.08	16.08	0.10	0.03	0.04	0.29	0.00	0.00	20.9
6	0	-0	-4849	0	0	0	2108	--	--	16.08	16.08	0.10	0.04	0.04	0.30	0.00	0.00	20.9
7	0	-0	-4925	0	0	0	2340	--	--	16.08	16.08	0.10	0.04	0.04	0.31	0.00	0.00	20.9
8	0	-0	-4715	0	0	0	1796	--	--	16.08	16.08	0.10	0.03	0.04	0.30	0.00	0.00	20.9
9	0	-0	-4791	0	0	0	2027	--	--	16.08	16.08	0.10	0.04	0.04	0.30	0.00	0.00	20.9
10	0	-0	-5032	0	0	0	2554	--	--	16.08	16.08	0.10	0.05	0.04	0.32	0.00	0.00	20.9

11	0	-0	-5055	0	0	0	2623	--	--	16.08	16.08	0.10	0.05	0.04	0.32	0.00	0.00	20.9
12	0	-0	-4585	0	0	0	1512	--	--	16.08	16.08	0.10	0.03	0.04	0.29	0.00	0.00	20.9
13	0	-0	-4608	0	0	0	1582	--	--	16.08	16.08	0.10	0.03	0.04	0.29	0.00	0.00	20.9
14	0	-0	-4849	0	0	0	2108	--	--	16.08	16.08	0.10	0.04	0.04	0.30	0.00	0.00	20.9
15	0	-0	-4925	0	0	0	2340	--	--	16.08	16.08	0.10	0.04	0.04	0.31	0.00	0.00	20.9
16	0	-0	-4715	0	0	0	1796	--	--	16.08	16.08	0.10	0.03	0.04	0.30	0.00	0.00	20.9
17	0	-0	-4791	0	0	0	2027	--	--	16.08	16.08	0.10	0.04	0.04	0.30	0.00	0.00	20.9
18	0	-0	-7064	0	0	0	3254	--	--	16.08	16.08	0.00	0.06	0.06	0.44	0.00	0.00	20.9
19	0	-0	-5648	0	0	0	485	--	--	16.08	16.08	0.00	0.01	0.05	0.35	0.00	0.00	20.9
20	0	-0	-6324	0	0	0	2000	--	--	16.08	16.08	0.00	0.03	0.05	0.40	0.00	0.00	20.9
37	0	-0	-7494	0	0	0	4466	--	--	16.08	16.08	0.00	0.08	0.06	0.47	0.00	0.00	20.9
38	0	-0	-5135	0	0	0	-2786	--	--	16.08	16.08	0.18	0.05	0.04	0.32	0.00	0.00	20.9
39	0	-0	-6262	0	0	0	2377	--	--	16.08	16.08	0.00	0.04	0.05	0.39	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	-6266	0	0	0	2688	--	--	16.08	16.08	0.00	0.05	0.05	0.39	0.00	0.00	20.9
2	26	-0	-5032	0	0	0	2554	--	--	16.08	16.08	0.10	0.05	0.04	0.32	0.00	0.00	20.9
3	26	-0	-5055	0	0	0	2623	--	--	16.08	16.08	0.10	0.05	0.04	0.32	0.00	0.00	20.9
4	26	-0	-4585	0	0	0	1512	--	--	16.08	16.08	0.10	0.03	0.04	0.29	0.00	0.00	20.9
5	26	-0	-4608	0	0	0	1582	--	--	16.08	16.08	0.10	0.03	0.04	0.29	0.00	0.00	20.9
6	26	-0	-4849	0	0	0	2108	--	--	16.08	16.08	0.10	0.04	0.04	0.30	0.00	0.00	20.9
7	26	-0	-4925	0	0	0	2340	--	--	16.08	16.08	0.10	0.04	0.04	0.31	0.00	0.00	20.9
8	26	-0	-4715	0	0	0	1796	--	--	16.08	16.08	0.10	0.03	0.04	0.30	0.00	0.00	20.9
9	26	-0	-4791	0	0	0	2027	--	--	16.08	16.08	0.10	0.04	0.04	0.30	0.00	0.00	20.9
10	26	-0	-5032	0	0	0	2554	--	--	16.08	16.08	0.10	0.05	0.04	0.32	0.00	0.00	20.9
11	26	-0	-5055	0	0	0	2623	--	--	16.08	16.08	0.10	0.05	0.04	0.32	0.00	0.00	20.9
12	26	-0	-4585	0	0	0	1512	--	--	16.08	16.08	0.10	0.03	0.04	0.29	0.00	0.00	20.9
13	26	-0	-4608	0	0	0	1582	--	--	16.08	16.08	0.10	0.03	0.04	0.29	0.00	0.00	20.9
14	26	-0	-4849	0	0	0	2108	--	--	16.08	16.08	0.10	0.04	0.04	0.30	0.00	0.00	20.9
15	26	-0	-4925	0	0	0	2340	--	--	16.08	16.08	0.10	0.04	0.04	0.31	0.00	0.00	20.9
16	26	-0	-4715	0	0	0	1796	--	--	16.08	16.08	0.10	0.03	0.04	0.30	0.00	0.00	20.9
17	26	-0	-4791	0	0	0	2027	--	--	16.08	16.08	0.10	0.04	0.04	0.30	0.00	0.00	20.9
18	26	-0	-7064	0	0	0	3254	--	--	16.08	16.08	0.00	0.06	0.06	0.44	0.00	0.00	20.9
19	26	-0	-5648	0	0	0	-2416	--	--	16.08	16.08	0.18	0.04	0.05	0.35	0.00	0.00	20.9
20	26	-0	-6324	0	0	0	2000	--	--	16.08	16.08	0.00	0.03	0.05	0.40	0.00	0.00	20.9
37	26	-0	-7494	0	0	0	4466	--	--	16.08	16.08	0.00	0.08	0.06	0.47	0.00	0.00	20.9
38	26	-0	-5135	0	0	0	-2786	--	--	16.08	16.08	0.18	0.05	0.04	0.32	0.00	0.00	20.9
39	26	-0	-6262	0	0	0	2377	--	--	16.08	16.08	0.00	0.04	0.05	0.39	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	-6266	0	0	0	-531	--	--	16.08	16.08	0.18	0.01	0.05	0.39	0.00	0.00	20.9
2	51	-0	-5032	0	0	0	-31	--	--	16.08	16.08	0.29	0.00	0.04	0.32	0.00	0.00	20.9
3	51	-0	-5055	0	0	0	27	--	--	16.08	16.08	0.10	0.00	0.04	0.32	0.00	0.00	20.9
4	51	-0	-4585	0	0	0	-843	--	--	16.08	16.08	0.29	0.01	0.04	0.29	0.00	0.00	20.9
5	51	-0	-4608	0	0	0	-785	--	--	16.08	16.08	0.29	0.01	0.04	0.29	0.00	0.00	20.9
6	51	-0	-4849	0	0	0	-382	--	--	16.08	16.08	0.29	0.01	0.04	0.30	0.00	0.00	20.9
7	51	-0	-4925	0	0	0	-190	--	--	16.08	16.08	0.29	0.00	0.04	0.31	0.00	0.00	20.9
8	51	-0	-4715	0	0	0	-626	--	--	16.08	16.08	0.29	0.01	0.04	0.30	0.00	0.00	20.9
9	51	-0	-4791	0	0	0	-434	--	--	16.08	16.08	0.29	0.01	0.04	0.30	0.00	0.00	20.9
10	51	-0	-5032	0	0	0	-31	--	--	16.08	16.08	0.29	0.00	0.04	0.32	0.00	0.00	20.9
11	51	-0	-5055	0	0	0	27	--	--	16.08	16.08	0.10	0.00	0.04	0.32	0.00	0.00	20.9
12	51	-0	-4585	0	0	0	-843	--	--	16.08	16.08	0.29	0.01	0.04	0.29	0.00	0.00	20.9
13	51	-0	-4608	0	0	0	-785	--	--	16.08	16.08	0.29	0.01	0.04	0.29	0.00	0.00	20.9
14	51	-0	-4849	0	0	0	-382	--	--	16.08	16.08	0.29	0.01	0.04	0.30	0.00	0.00	20.9
15	51	-0	-4925	0	0	0	-190	--	--	16.08	16.08	0.29	0.00	0.04	0.31	0.00	0.00	20.9
16	51	-0	-4715	0	0	0	-626	--	--	16.08	16.08	0.29	0.01	0.04	0.30	0.00	0.00	20.9
17	51	-0	-4791	0	0	0	-434	--	--	16.08	16.08	0.29	0.01	0.04	0.30	0.00	0.00	20.9
18	51	-0	-7064	0	0	0	-374	--	--	16.08	16.08	0.18	0.01	0.06	0.44	0.00	0.00	20.9
19	51	-0	-5648	0	0	0	-2416	--	--	16.08	16.08	0.18	0.04	0.05	0.35	0.00	0.00	20.9
20	51	-0	-6324	0	0	0	-1248	--	--	16.08	16.08	0.18	0.02	0.05	0.40	0.00	0.00	20.9
37	51	-0	-7494	0	0	0	617	--	--	16.08	16.08	0.00	0.01	0.06	0.47	0.00	0.00	20.9
38	51	-0	-5135	0	0	0	-2786	--	--	16.08	16.08	0.18	0.05	0.04	0.32	0.00	0.00	20.9
39	51	-0	-6262	0	0	0	-840	--	--	16.08	16.08	0.18	0.01	0.05	0.39	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 64 NI 1828 NF 1827 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm

1	0	-0	-4518	0	0	0	-2851	--	--	16.08	16.08	0.18	0.05	0.04	0.28	0.00	0.00	20.9
2	0	-0	-3680	0	0	0	-1921	--	--	16.08	16.08	0.29	0.03	0.03	0.23	0.00	0.00	20.9
3	0	-0	-3702	0	0	0	27	--	--	16.08	16.08	0.10	0.00	0.03	0.23	0.00	0.00	20.9
4	0	-0	-3249	0	0	0	-2511	--	--	16.08	16.08	0.29	0.04	0.03	0.20	0.00	0.00	20.9
5	0	-0	-3271	0	0	0	-2465	--	--	16.08	16.08	0.29	0.04	0.03	0.21	0.00	0.00	20.9
6	0	-0	-3503	0	0	0	-2182	--	--	16.08	16.08	0.29	0.04	0.03	0.22	0.00	0.00	20.9
7	0	-0	-3576	0	0	0	-2027	--	--	16.08	16.08	0.29	0.04	0.03	0.22	0.00	0.00	20.9
8	0	-0	-3374	0	0	0	-2359	--	--	16.08	16.08	0.29	0.04	0.03	0.21	0.00	0.00	20.9
9	0	-0	-3447	0	0	0	-2204	--	--	16.08	16.08	0.29	0.04	0.03	0.22	0.00	0.00	20.9
10	0	-0	-3680	0	0	0	-1921	--	--	16.08	16.08	0.29	0.03	0.03	0.23	0.00	0.00	20.9
11	0	-0	-3702	0	0	0	27	--	--	16.08	16.08	0.10	0.00	0.03	0.23	0.00	0.00	20.9
12	0	-0	-3249	0	0	0	-2511	--	--	16.08	16.08	0.29	0.04	0.03	0.20	0.00	0.00	20.9
13	0	-0	-3271	0	0	0	-2465	--	--	16.08	16.08	0.29	0.04	0.03	0.21	0.00	0.00	20.9
14	0	-0	-3503	0	0	0	-2182	--	--	16.08	16.08	0.29	0.04	0.03	0.22	0.00	0.00	20.9
15	0	-0	-3576	0	0	0	-2027	--	--	16.08	16.08	0.29	0.04	0.03	0.22	0.00	0.00	20.9
16	0	-0	-3374	0	0	0	-2359	--	--	16.08	16.08	0.29	0.04	0.03	0.21	0.00	0.00	20.9
17	0	-0	-3447	0	0	0	-2204	--	--	16.08	16.08	0.29	0.04	0.03	0.22	0.00	0.00	20.9
18	0	-0	-5154	0	0	0	-3021	--	--	16.08	16.08	0.18	0.05	0.04	0.32	0.00	0.00	20.9
19	0	-0	-3845	0	0	0	-4391	--	--	16.08	16.08	0.18	0.07	0.03	0.24	0.00	0.00	20.9
20	0	-0	-4492	0	0	0	-3555	--	--	16.08	16.08	0.18	0.06	0.04	0.28	0.00	0.00	20.9
37	0	-0	-5590	0	0	0	617	--	--	16.08	16.08	0.00	0.01	0.05	0.35	0.00	0.00	20.9
38	0	-0	-3409	0	0	0	-4537	--	--	16.08	16.08	0.18	0.08	0.03	0.21	0.00	0.00	20.9
39	0	-0	-4486	0	0	0	-3144	--	--	16.08	16.08	0.18	0.05	0.04	0.28	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	-4518	0	0	0	-2851	--	--	16.08	16.08	0.18	0.05	0.04	0.28	0.00	0.00	20.9
2	26	-0	-3680	0	0	0	-1921	--	--	16.08	16.08	0.29	0.03	0.03	0.23	0.00	0.00	20.9
3	26	-0	-3702	0	0	0	-1875	--	--	16.08	16.08	0.29	0.03	0.03	0.23	0.00	0.00	20.9
4	26	-0	-3249	0	0	0	-2511	--	--	16.08	16.08	0.29	0.04	0.03	0.20	0.00	0.00	20.9
5	26	-0	-3271	0	0	0	-2465	--	--	16.08	16.08	0.29	0.04	0.03	0.21	0.00	0.00	20.9
6	26	-0	-3503	0	0	0	-2182	--	--	16.08	16.08	0.29	0.04	0.03	0.22	0.00	0.00	20.9

7	26	-0	-3576	0	0	0	-2027	--	--	16.08	16.08	0.29	0.04	0.03	0.22	0.00	0.00	20.9
8	26	-0	-3374	0	0	0	-2359	--	--	16.08	16.08	0.29	0.04	0.03	0.21	0.00	0.00	20.9
9	26	-0	-3447	0	0	0	-2204	--	--	16.08	16.08	0.29	0.04	0.03	0.22	0.00	0.00	20.9
10	26	-0	-3680	0	0	0	-1921	--	--	16.08	16.08	0.29	0.03	0.03	0.23	0.00	0.00	20.9
11	26	-0	-3702	0	0	0	-1875	--	--	16.08	16.08	0.29	0.03	0.03	0.23	0.00	0.00	20.9
12	26	-0	-3249	0	0	0	-2511	--	--	16.08	16.08	0.29	0.04	0.03	0.20	0.00	0.00	20.9
13	26	-0	-3271	0	0	0	-2465	--	--	16.08	16.08	0.29	0.04	0.03	0.21	0.00	0.00	20.9
14	26	-0	-3503	0	0	0	-2182	--	--	16.08	16.08	0.29	0.04	0.03	0.22	0.00	0.00	20.9
15	26	-0	-3576	0	0	0	-2027	--	--	16.08	16.08	0.29	0.04	0.03	0.22	0.00	0.00	20.9
16	26	-0	-3374	0	0	0	-2359	--	--	16.08	16.08	0.29	0.04	0.03	0.21	0.00	0.00	20.9
17	26	-0	-3447	0	0	0	-2204	--	--	16.08	16.08	0.29	0.04	0.03	0.22	0.00	0.00	20.9
18	26	-0	-5154	0	0	0	-3021	--	--	16.08	16.08	0.18	0.05	0.04	0.32	0.00	0.00	20.9
19	26	-0	-3845	0	0	0	-4391	--	--	16.08	16.08	0.18	0.07	0.03	0.24	0.00	0.00	20.9
20	26	-0	-4492	0	0	0	-3555	--	--	16.08	16.08	0.18	0.06	0.04	0.28	0.00	0.00	20.9
37	26	-0	-5590	0	0	0	-2254	--	--	16.08	16.08	0.18	0.04	0.05	0.35	0.00	0.00	20.9
38	26	-0	-3409	0	0	0	-4537	--	--	16.08	16.08	0.18	0.08	0.03	0.21	0.00	0.00	20.9
39	26	-0	-4486	0	0	0	-3144	--	--	16.08	16.08	0.18	0.05	0.04	0.28	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	-4518	0	0	0	-2851	--	--	16.08	16.08	0.18	0.05	0.04	0.28	0.00	0.00	20.9
2	51	-0	-3680	0	0	0	-1921	--	--	16.08	16.08	0.29	0.03	0.03	0.23	0.00	0.00	20.9
3	51	-0	-3702	0	0	0	-1875	--	--	16.08	16.08	0.29	0.03	0.03	0.23	0.00	0.00	20.9
4	51	-0	-3249	0	0	0	-2511	--	--	16.08	16.08	0.29	0.04	0.03	0.20	0.00	0.00	20.9
5	51	-0	-3271	0	0	0	-2465	--	--	16.08	16.08	0.29	0.04	0.03	0.21	0.00	0.00	20.9
6	51	-0	-3503	0	0	0	-2182	--	--	16.08	16.08	0.29	0.04	0.03	0.22	0.00	0.00	20.9
7	51	-0	-3576	0	0	0	-2027	--	--	16.08	16.08	0.29	0.04	0.03	0.22	0.00	0.00	20.9
8	51	-0	-3374	0	0	0	-2359	--	--	16.08	16.08	0.29	0.04	0.03	0.21	0.00	0.00	20.9
9	51	-0	-3447	0	0	0	-2204	--	--	16.08	16.08	0.29	0.04	0.03	0.22	0.00	0.00	20.9
10	51	-0	-3680	0	0	0	-1921	--	--	16.08	16.08	0.29	0.03	0.03	0.23	0.00	0.00	20.9
11	51	-0	-3702	0	0	0	-1875	--	--	16.08	16.08	0.29	0.03	0.03	0.23	0.00	0.00	20.9
12	51	-0	-3249	0	0	0	-2511	--	--	16.08	16.08	0.29	0.04	0.03	0.20	0.00	0.00	20.9
13	51	-0	-3271	0	0	0	-2465	--	--	16.08	16.08	0.29	0.04	0.03	0.21	0.00	0.00	20.9
14	51	-0	-3503	0	0	0	-2182	--	--	16.08	16.08	0.29	0.04	0.03	0.22	0.00	0.00	20.9
15	51	-0	-3576	0	0	0	-2027	--	--	16.08	16.08	0.29	0.04	0.03	0.22	0.00	0.00	20.9
16	51	-0	-3374	0	0	0	-2359	--	--	16.08	16.08	0.29	0.04	0.03	0.21	0.00	0.00	20.9
17	51	-0	-3447	0	0	0	-2204	--	--	16.08	16.08	0.29	0.04	0.03	0.22	0.00	0.00	20.9
18	51	-0	-5154	0	0	0	-3021	--	--	16.08	16.08	0.18	0.05	0.04	0.32	0.00	0.00	20.9
19	51	-0	-3845	0	0	0	-4391	--	--	16.08	16.08	0.18	0.07	0.03	0.24	0.00	0.00	20.9
20	51	-0	-4492	0	0	0	-3555	--	--	16.08	16.08	0.18	0.06	0.04	0.28	0.00	0.00	20.9
37	51	-0	-5590	0	0	0	-2254	--	--	16.08	16.08	0.18	0.04	0.05	0.35	0.00	0.00	20.9
38	51	-0	-3409	0	0	0	-4537	--	--	16.08	16.08	0.18	0.08	0.03	0.21	0.00	0.00	20.9
39	51	-0	-4486	0	0	0	-3144	--	--	16.08	16.08	0.18	0.05	0.04	0.28	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 65 NI 1827 NF 1826 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm

1	0	-0	-2811	0	0	0	-4295	--	--	16.08	16.08	0.18	0.07	0.02	0.18	0.00	0.00	20.9
2	0	-0	-2361	0	0	0	-3134	--	--	16.08	16.08	0.29	0.05	0.02	0.15	0.00	0.00	20.9
3	0	-0	-2382	0	0	0	-3098	--	--	16.08	16.08	0.29	0.05	0.02	0.15	0.00	0.00	20.9
4	0	-0	-1943	0	0	0	-3510	--	--	16.08	16.08	0.29	0.06	0.02	0.12	0.00	0.00	20.9
5	0	-0	-1964	0	0	0	-3474	--	--	16.08	16.08	0.29	0.06	0.02	0.12	0.00	0.00	20.9
6	0	-0	-2191	0	0	0	-3307	--	--	16.08	16.08	0.29	0.06	0.02	0.14	0.00	0.00	20.9
7	0	-0	-2260	0	0	0	-3188	--	--	16.08	16.08	0.29	0.06	0.02	0.14	0.00	0.00	20.9
8	0	-0	-2065	0	0	0	-3420	--	--	16.08	16.08	0.29	0.06	0.02	0.13	0.00	0.00	20.9
9	0	-0	-2135	0	0	0	-3301	--	--	16.08	16.08	0.29	0.06	0.02	0.13	0.00	0.00	20.9
10	0	-0	-2361	0	0	0	-3134	--	--	16.08	16.08	0.29	0.05	0.02	0.15	0.00	0.00	20.9
11	0	-0	-2382	0	0	0	-3098	--	--	16.08	16.08	0.29	0.05	0.02	0.15	0.00	0.00	20.9
12	0	-0	-1943	0	0	0	-3510	--	--	16.08	16.08	0.29	0.06	0.02	0.12	0.00	0.00	20.9
13	0	-0	-1964	0	0	0	-3474	--	--	16.08	16.08	0.29	0.06	0.02	0.12	0.00	0.00	20.9
14	0	-0	-2191	0	0	0	-3307	--	--	16.08	16.08	0.29	0.06	0.02	0.14	0.00	0.00	20.9
15	0	-0	-2260	0	0	0	-3188	--	--	16.08	16.08	0.29	0.06	0.02	0.14	0.00	0.00	20.9
16	0	-0	-2065	0	0	0	-3420	--	--	16.08	16.08	0.29	0.06	0.02	0.13	0.00	0.00	20.9
17	0	-0	-2135	0	0	0	-3301	--	--	16.08	16.08	0.29	0.06	0.02	0.13	0.00	0.00	20.9
18	0	-0	-3286	0	0	0	-4709	--	--	16.08	16.08	0.18	0.08	0.03	0.21	0.00	0.00	20.9
19	0	-0	-2071	0	0	0	-5455	--	--	16.08	16.08	0.18	0.09	0.02	0.13	0.00	0.00	20.9
20	0	-0	-2693	0	0	0	-4938	--	--	16.08	16.08	0.18	0.08	0.02	0.17	0.00	0.00	20.9
37	0	-0	-3734	0	0	0	-4172	--	--	16.08	16.08	0.18	0.07	0.03	0.23	0.00	0.00	20.9
38	0	-0	-1710	0	0	0	-5415	--	--	16.08	16.08	0.18	0.09	0.01	0.11	0.00	0.00	20.9
39	0	-0	-2746	0	0	0	-4554	--	--	16.08	16.08	0.18	0.08	0.02	0.17	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	-2811	0	0	0	-4295	--	--	16.08	16.08	0.18	0.07	0.02	0.18	0.00	0.00	20.9
2	26	-0	-2361	0	0	0	-3134	--	--	16.08	16.08	0.29	0.05	0.02	0.15	0.00	0.00	20.9
3	26	-0	-2382	0	0	0	-3098	--	--	16.08	16.08	0.29	0.05	0.02	0.15	0.00	0.00	20.9
4	26	-0	-1943	0	0	0	-3510	--	--	16.08	16.08	0.29	0.06	0.02	0.12	0.00	0.00	20.9
5	26	-0	-1964	0	0	0	-3474	--	--	16.08	16.08	0.29	0.06	0.02	0.12	0.00	0.00	20.9
6	26	-0	-2191	0	0	0	-3307	--	--	16.08	16.08	0.29	0.06	0.02	0.14	0.00	0.00	20.9
7	26	-0	-2260	0	0	0	-3188	--	--	16.08	16.08	0.29	0.06	0.02	0.14	0.00	0.00	20.9
8	26	-0	-2065	0	0	0	-3420	--	--	16.08	16.08	0.29	0.06	0.02	0.13	0.00	0.00	20.9
9	26	-0	-2135	0	0	0	-3301	--	--	16.08	16.08	0.29	0.06	0.02	0.13	0.00	0.00	20.9
10	26	-0	-2361	0	0	0	-3134	--	--	16.08	16.08	0.29	0.05	0.02	0.15	0.00	0.00	20.9
11	26	-0	-2382	0	0	0	-3098	--	--	16.08	16.08	0.29	0.05	0.02	0.15	0.00	0.00	20.9
12	26	-0	-1943	0	0	0	-3510	--	--	16.08	16.08	0.29	0.06	0.02	0.12	0.00	0.00	20.9
13	26	-0	-1964	0	0	0	-3474	--	--	16.08	16.08	0.29	0.06	0.02	0.12	0.00	0.00	20.9
14	26	-0	-2191	0	0	0	-3307	--	--	16.08	16.08	0.29	0.06	0.02	0.14	0.00	0.00	20.9
15	26	-0	-2260	0	0	0	-3188	--	--	16.08	16.08	0.29	0.06	0.02	0.14	0.00	0.00	20.9
16	26	-0	-2065	0	0	0	-3420	--	--	16.08	16.08	0.29	0.06	0.02	0.13	0.00	0.00	20.9
17	26	-0	-2135	0	0	0	-3301	--	--	16.08	16.08	0.29	0.06	0.02	0.13	0.00	0.00	20.9
18	26	-0	-3286	0	0	0	-4709	--	--	16.08	16.08	0.18	0.08	0.03	0.21	0.00	0.00	20.9
19	26	-0	-2071	0	0	0	-5455	--	--	16.08	16.08	0.18	0.09	0.02	0.13	0.00	0.00	20.9
20	26	-0	-2693	0	0	0	-4938	--	--	16.08	16.08	0.18	0.08	0.02	0.17	0.00	0.00	20.9
37	26	-0	-3734	0	0	0	-4172	--	--	16.08	16.08	0.18	0.07	0.03	0.23	0.00	0.00	20.9
38	26	-0	-1710	0	0	0	-5415	--	--	16.08	16.08	0.18	0.09	0.01	0.11	0.00	0.00	20.9
39	26	-0	-2746	0	0	0	-4554	--	--	16.08	16.08	0.18	0.08	0.02	0.17	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	-2811	0	0	0	-4295	--	--	16.08	16.08	0.18	0.07	0.02	0.18	0.00	0.00	20.9
2	51	-0	-2361	0	0	0	-3134	--	--	16.08	16.08	0.29	0.05	0.02	0.15	0.00	0.00	20.9

3	51	-0	-2382	0	0	0	-3098	--	--	16.08	16.08	0.29	0.05	0.02	0.15	0.00	0.00	20.9
4	51	-0	-1943	0	0	0	-3510	--	--	16.08	16.08	0.29	0.06	0.02	0.12	0.00	0.00	20.9
5	51	-0	-1964	0	0	0	-3474	--	--	16.08	16.08	0.29	0.06	0.02	0.12	0.00	0.00	20.9
6	51	-0	-2191	0	0	0	-3307	--	--	16.08	16.08	0.29	0.06	0.02	0.14	0.00	0.00	20.9
7	51	-0	-2260	0	0	0	-3188	--	--	16.08	16.08	0.29	0.06	0.02	0.14	0.00	0.00	20.9
8	51	-0	-2065	0	0	0	-3420	--	--	16.08	16.08	0.29	0.06	0.02	0.13	0.00	0.00	20.9
9	51	-0	-2135	0	0	0	-3301	--	--	16.08	16.08	0.29	0.06	0.02	0.13	0.00	0.00	20.9
10	51	-0	-2361	0	0	0	-3134	--	--	16.08	16.08	0.29	0.05	0.02	0.15	0.00	0.00	20.9
11	51	-0	-2382	0	0	0	-3098	--	--	16.08	16.08	0.29	0.05	0.02	0.15	0.00	0.00	20.9
12	51	-0	-1943	0	0	0	-3510	--	--	16.08	16.08	0.29	0.06	0.02	0.12	0.00	0.00	20.9
13	51	-0	-1964	0	0	0	-3474	--	--	16.08	16.08	0.29	0.06	0.02	0.12	0.00	0.00	20.9
14	51	-0	-2191	0	0	0	-3307	--	--	16.08	16.08	0.29	0.06	0.02	0.14	0.00	0.00	20.9
15	51	-0	-2260	0	0	0	-3188	--	--	16.08	16.08	0.29	0.06	0.02	0.14	0.00	0.00	20.9
16	51	-0	-2065	0	0	0	-3420	--	--	16.08	16.08	0.29	0.06	0.02	0.13	0.00	0.00	20.9
17	51	-0	-2135	0	0	0	-3301	--	--	16.08	16.08	0.29	0.06	0.02	0.13	0.00	0.00	20.9
18	51	-0	-3286	0	0	0	-4709	--	--	16.08	16.08	0.18	0.08	0.03	0.21	0.00	0.00	20.9
19	51	-0	-2071	0	0	0	-5455	--	--	16.08	16.08	0.18	0.09	0.02	0.13	0.00	0.00	20.9
20	51	-0	-2693	0	0	0	-4938	--	--	16.08	16.08	0.18	0.08	0.02	0.17	0.00	0.00	20.9
37	51	-0	-3734	0	0	0	-4172	--	--	16.08	16.08	0.18	0.07	0.03	0.23	0.00	0.00	20.9
38	51	-0	-1710	0	0	0	-5415	--	--	16.08	16.08	0.18	0.09	0.01	0.11	0.00	0.00	20.9
39	51	-0	-2746	0	0	0	-4554	--	--	16.08	16.08	0.18	0.08	0.02	0.17	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 66 NI 1826 NF 1841 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice resistenza			aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-1130	0	0	0	-4875	--	--	16.08	16.08	0.18	0.08	0.01	0.07	0.00	0.00	20.9
2	0	-0	-1064	0	0	0	-3680	--	--	16.08	16.08	0.29	0.06	0.01	0.07	0.00	0.00	20.9
3	0	-0	-1084	0	0	0	-3655	--	--	16.08	16.08	0.29	0.06	0.01	0.07	0.00	0.00	20.9
4	0	-0	-654	0	0	0	-3846	--	--	16.08	16.08	0.29	0.07	0.01	0.04	0.00	0.00	20.9
5	0	-0	-674	0	0	0	-3820	--	--	16.08	16.08	0.29	0.07	0.01	0.04	0.00	0.00	20.9
6	0	-0	-897	0	0	0	-3768	--	--	16.08	16.08	0.29	0.07	0.01	0.06	0.00	0.00	20.9
7	0	-0	-964	0	0	0	-3683	--	--	16.08	16.08	0.29	0.06	0.01	0.06	0.00	0.00	20.9
8	0	-0	-774	0	0	0	-3818	--	--	16.08	16.08	0.29	0.07	0.01	0.05	0.00	0.00	20.9
9	0	-0	-841	0	0	0	-3732	--	--	16.08	16.08	0.29	0.06	0.01	0.05	0.00	0.00	20.9
10	0	-0	-1064	0	0	0	-3680	--	--	16.08	16.08	0.29	0.06	0.01	0.07	0.00	0.00	20.9
11	0	-0	-1084	0	0	0	-3655	--	--	16.08	16.08	0.29	0.06	0.01	0.07	0.00	0.00	20.9
12	0	-0	-654	0	0	0	-3846	--	--	16.08	16.08	0.29	0.07	0.01	0.04	0.00	0.00	20.9
13	0	-0	-674	0	0	0	-3820	--	--	16.08	16.08	0.29	0.07	0.01	0.04	0.00	0.00	20.9
14	0	-0	-897	0	0	0	-3768	--	--	16.08	16.08	0.29	0.07	0.01	0.06	0.00	0.00	20.9
15	0	-0	-964	0	0	0	-3683	--	--	16.08	16.08	0.29	0.06	0.01	0.06	0.00	0.00	20.9
16	0	-0	-774	0	0	0	-3818	--	--	16.08	16.08	0.29	0.07	0.01	0.05	0.00	0.00	20.9
17	0	-0	-841	0	0	0	-3732	--	--	16.08	16.08	0.29	0.06	0.01	0.05	0.00	0.00	20.9
18	0	-0	-1439	0	0	0	-5448	--	--	16.08	16.08	0.18	0.09	0.01	0.09	0.00	0.00	20.9
19	0	-0	-301	0	0	0	-5610	--	--	16.08	16.08	0.18	0.09	0.00	0.02	0.00	0.00	20.9
20	0	-0	-908	0	0	0	-5404	--	--	16.08	16.08	0.18	0.09	0.01	0.06	0.00	0.00	20.9
37	0	-0	-1911	0	0	0	-5154	--	--	16.08	16.08	0.18	0.09	0.02	0.12	0.00	0.00	20.9
38	0	-0	-15	0	0	0	-5423	--	--	16.08	16.08	0.18	0.09	0.00	0.00	0.00	0.00	20.9
39	0	-0	-1025	0	0	0	-5081	--	--	16.08	16.08	0.18	0.08	0.01	0.06	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	-1130	0	0	0	-4875	--	--	16.08	16.08	0.18	0.08	0.01	0.07	0.00	0.00	20.9
2	26	-0	-1064	0	0	0	-3680	--	--	16.08	16.08	0.29	0.06	0.01	0.07	0.00	0.00	20.9
3	26	-0	-1084	0	0	0	-3655	--	--	16.08	16.08	0.29	0.06	0.01	0.07	0.00	0.00	20.9
4	26	-0	-654	0	0	0	-3846	--	--	16.08	16.08	0.29	0.07	0.01	0.04	0.00	0.00	20.9
5	26	-0	-674	0	0	0	-3820	--	--	16.08	16.08	0.29	0.07	0.01	0.04	0.00	0.00	20.9
6	26	-0	-897	0	0	0	-3768	--	--	16.08	16.08	0.29	0.07	0.01	0.06	0.00	0.00	20.9
7	26	-0	-964	0	0	0	-3683	--	--	16.08	16.08	0.29	0.06	0.01	0.06	0.00	0.00	20.9
8	26	-0	-774	0	0	0	-3818	--	--	16.08	16.08	0.29	0.07	0.01	0.05	0.00	0.00	20.9
9	26	-0	-841	0	0	0	-3732	--	--	16.08	16.08	0.29	0.06	0.01	0.05	0.00	0.00	20.9
10	26	-0	-1064	0	0	0	-3680	--	--	16.08	16.08	0.29	0.06	0.01	0.07	0.00	0.00	20.9
11	26	-0	-1084	0	0	0	-3655	--	--	16.08	16.08	0.29	0.06	0.01	0.07	0.00	0.00	20.9
12	26	-0	-654	0	0	0	-3846	--	--	16.08	16.08	0.29	0.07	0.01	0.04	0.00	0.00	20.9
13	26	-0	-674	0	0	0	-3820	--	--	16.08	16.08	0.29	0.07	0.01	0.04	0.00	0.00	20.9
14	26	-0	-897	0	0	0	-3768	--	--	16.08	16.08	0.29	0.07	0.01	0.06	0.00	0.00	20.9
15	26	-0	-964	0	0	0	-3683	--	--	16.08	16.08	0.29	0.06	0.01	0.06	0.00	0.00	20.9
16	26	-0	-774	0	0	0	-3818	--	--	16.08	16.08	0.29	0.07	0.01	0.05	0.00	0.00	20.9
17	26	-0	-841	0	0	0	-3732	--	--	16.08	16.08	0.29	0.06	0.01	0.05	0.00	0.00	20.9
18	26	-0	-1439	0	0	0	-5448	--	--	16.08	16.08	0.18	0.09	0.01	0.09	0.00	0.00	20.9
19	26	-0	-301	0	0	0	-5610	--	--	16.08	16.08	0.18	0.09	0.00	0.02	0.00	0.00	20.9
20	26	-0	-908	0	0	0	-5404	--	--	16.08	16.08	0.18	0.09	0.01	0.06	0.00	0.00	20.9
37	26	-0	-1911	0	0	0	-5154	--	--	16.08	16.08	0.18	0.09	0.02	0.12	0.00	0.00	20.9
38	26	-0	-15	0	0	0	-5423	--	--	16.08	16.08	0.18	0.09	0.00	0.00	0.00	0.00	20.9
39	26	-0	-1025	0	0	0	-5081	--	--	16.08	16.08	0.18	0.08	0.01	0.06	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	-1130	0	0	0	-4875	--	--	16.08	16.08	0.18	0.08	0.01	0.07	0.00	0.00	20.9
2	51	-0	-1064	0	0	0	-3680	--	--	16.08	16.08	0.29	0.06	0.01	0.07	0.00	0.00	20.9
3	51	-0	-1084	0	0	0	-3655	--	--	16.08	16.08	0.29	0.06	0.01	0.07	0.00	0.00	20.9
4	51	-0	-654	0	0	0	-3846	--	--	16.08	16.08	0.29	0.07	0.01	0.04	0.00	0.00	20.9
5	51	-0	-674	0	0	0	-3820	--	--	16.08	16.08	0.29	0.07	0.01	0.04	0.00	0.00	20.9
6	51	-0	-897	0	0	0	-3768	--	--	16.08	16.08	0.29	0.07	0.01	0.06	0.00	0.00	20.9
7	51	-0	-964	0	0	0	-3683	--	--	16.08	16.08	0.29	0.06	0.01	0.06	0.00	0.00	20.9
8	51	-0	-774	0	0	0	-3818	--	--	16.08	16.08	0.29	0.07	0.01	0.05	0.00	0.00	20.9
9	51	-0	-841	0	0	0	-3732	--	--	16.08	16.08	0.29	0.06	0.01	0.05	0.00	0.00	20.9
10	51	-0	-1064	0	0	0	-3680	--	--	16.08	16.08	0.29	0.06	0.01	0.07	0.00	0.00	20.9
11	51	-0	-1084	0	0	0	-3655	--	--	16.08	16.08	0.29	0.06	0.01	0.07	0.00	0.00	20.9
12	51	-0	-654	0	0	0	-3846	--	--	16.08	16.08	0.29	0.07	0.01	0.04	0.00	0.00	20.9
13	51	-0	-674	0	0	0	-3820	--	--	16.08	16.08	0.29	0.07	0.01	0.04	0.00	0.00	20.9
14	51	-0	-897	0	0	0	-3768	--	--	16.08	16.08	0.29	0.07	0.01	0.06	0.00	0.00	20.9
15	51	-0	-964	0	0	0	-3683	--	--	16.08	16.08	0.29	0.06	0.01	0.06	0.00	0.00	20.9
16	51	-0	-774	0	0	0	-3818	--	--	16.08	16.08	0.29	0.07	0.01	0.05	0.00	0.00	20.9
17	51	-0	-841	0	0	0	-3732	--	--	16.08	16.08	0.29	0.06	0.01	0.05	0.00	0.00	20.9
18	51	-0	-1439	0	0	0	-5448	--	--	16.08	16.08	0.18	0.09	0.01	0.09	0.00	0.00	20.9
19	51	-0	-301	0	0	0	-5610	--	--	16.08	16.08	0.18	0.09	0.00	0.02	0.00	0.00	20.9
20	51	-0	-908	0	0	0	-5404	--	--	16.08	16.08	0.18	0.09	0.01	0.06	0.00	0.00	20.9
37	51	-0	-1911	0	0	0	-5154	--	--	16.08	16.08	0.18	0.09	0.02	0.12	0.00	0.00	20.9
38	51	-0	-15	0	0	0	-5423	--	--	16.08	16.08	0.18	0.09	0.00	0.00	0.00	0.00	20.9
39	51	-0	-1025	0	0	0	-5081	--	--	16.08	16.08	0.18	0.08	0.01	0.06	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 67 NI 1841 NF 1840 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	551	0	0	0	-4875	--	--	16.08	16.08	0.18	0.08	0.00	0.03	0.00	0.00	20.9
2	0	-0	229	0	0	0	-3680	--	--	16.08	16.08	0.29	0.06	0.00	0.01	0.00	0.00	20.9
3	0	-0	210	0	0	0	-3655	--	--	16.08	16.08	0.29	0.06	0.00	0.01	0.00	0.00	20.9
4	0	-0	638	0	0	0	-3846	--	--	16.08	16.08	0.29	0.07	0.01	0.04	0.00	0.00	20.9
5	0	-0	618	0	0	0	-3820	--	--	16.08	16.08	0.29	0.07	0.01	0.04	0.00	0.00	20.9
6	0	-0	395	0	0	0	-3768	--	--	16.08	16.08	0.29	0.07	0.00	0.02	0.00	0.00	20.9
7	0	-0	330	0	0	0	-3683	--	--	16.08	16.08	0.29	0.06	0.00	0.02	0.00	0.00	20.9
8	0	-0	517	0	0	0	-3818	--	--	16.08	16.08	0.29	0.07	0.00	0.03	0.00	0.00	20.9
9	0	-0	452	0	0	0	-3732	--	--	16.08	16.08	0.29	0.06	0.00	0.03	0.00	0.00	20.9
10	0	-0	229	0	0	0	-3680	--	--	16.08	16.08	0.29	0.06	0.00	0.01	0.00	0.00	20.9
11	0	-0	210	0	0	0	-3655	--	--	16.08	16.08	0.29	0.06	0.00	0.01	0.00	0.00	20.9
12	0	-0	638	0	0	0	-3846	--	--	16.08	16.08	0.29	0.07	0.01	0.04	0.00	0.00	20.9
13	0	-0	618	0	0	0	-3820	--	--	16.08	16.08	0.29	0.07	0.01	0.04	0.00	0.00	20.9
14	0	-0	395	0	0	0	-3768	--	--	16.08	16.08	0.29	0.07	0.00	0.02	0.00	0.00	20.9
15	0	-0	330	0	0	0	-3683	--	--	16.08	16.08	0.29	0.06	0.00	0.02	0.00	0.00	20.9
16	0	-0	517	0	0	0	-3818	--	--	16.08	16.08	0.29	0.07	0.00	0.03	0.00	0.00	20.9
17	0	-0	452	0	0	0	-3732	--	--	16.08	16.08	0.29	0.06	0.00	0.03	0.00	0.00	20.9
18	0	-0	411	0	0	0	-5448	--	--	16.08	16.08	0.18	0.09	0.00	0.03	0.00	0.00	20.9
19	0	-0	1494	0	0	0	-5610	--	--	16.08	16.08	0.18	0.09	0.01	0.09	0.00	0.00	20.9
20	0	-0	891	0	0	0	-5404	--	--	16.08	16.08	0.18	0.09	0.01	0.06	0.00	0.00	20.9
37	0	-0	-97	0	0	0	-5204	--	--	16.08	16.08	0.18	0.09	0.00	0.01	0.00	0.00	20.9
38	0	-0	1707	0	0	0	-5423	--	--	16.08	16.08	0.18	0.09	0.01	0.11	0.00	0.00	20.9
39	0	-0	702	0	0	0	-5081	--	--	16.08	16.08	0.18	0.08	0.01	0.04	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	26	-0	551	0	0	0	-4875	--	--	16.08	16.08	0.18	0.08	0.00	0.03	0.00	0.00	20.9
2	26	-0	229	0	0	0	-3680	--	--	16.08	16.08	0.29	0.06	0.00	0.01	0.00	0.00	20.9
3	26	-0	210	0	0	0	-3655	--	--	16.08	16.08	0.29	0.06	0.00	0.01	0.00	0.00	20.9
4	26	-0	638	0	0	0	-3846	--	--	16.08	16.08	0.29	0.07	0.01	0.04	0.00	0.00	20.9
5	26	-0	618	0	0	0	-3820	--	--	16.08	16.08	0.29	0.07	0.01	0.04	0.00	0.00	20.9
6	26	-0	395	0	0	0	-3768	--	--	16.08	16.08	0.29	0.07	0.00	0.02	0.00	0.00	20.9
7	26	-0	330	0	0	0	-3683	--	--	16.08	16.08	0.29	0.06	0.00	0.02	0.00	0.00	20.9
8	26	-0	517	0	0	0	-3818	--	--	16.08	16.08	0.29	0.07	0.00	0.03	0.00	0.00	20.9
9	26	-0	452	0	0	0	-3732	--	--	16.08	16.08	0.29	0.06	0.00	0.03	0.00	0.00	20.9
10	26	-0	229	0	0	0	-3680	--	--	16.08	16.08	0.29	0.06	0.00	0.01	0.00	0.00	20.9
11	26	-0	210	0	0	0	-3655	--	--	16.08	16.08	0.29	0.06	0.00	0.01	0.00	0.00	20.9
12	26	-0	638	0	0	0	-3846	--	--	16.08	16.08	0.29	0.07	0.01	0.04	0.00	0.00	20.9
13	26	-0	618	0	0	0	-3820	--	--	16.08	16.08	0.29	0.07	0.01	0.04	0.00	0.00	20.9
14	26	-0	395	0	0	0	-3768	--	--	16.08	16.08	0.29	0.07	0.00	0.02	0.00	0.00	20.9
15	26	-0	330	0	0	0	-3683	--	--	16.08	16.08	0.29	0.06	0.00	0.02	0.00	0.00	20.9
16	26	-0	517	0	0	0	-3818	--	--	16.08	16.08	0.29	0.07	0.00	0.03	0.00	0.00	20.9
17	26	-0	452	0	0	0	-3732	--	--	16.08	16.08	0.29	0.06	0.00	0.03	0.00	0.00	20.9
18	26	-0	411	0	0	0	-5448	--	--	16.08	16.08	0.18	0.09	0.00	0.03	0.00	0.00	20.9
19	26	-0	1494	0	0	0	-5610	--	--	16.08	16.08	0.18	0.09	0.01	0.09	0.00	0.00	20.9
20	26	-0	891	0	0	0	-5404	--	--	16.08	16.08	0.18	0.09	0.01	0.06	0.00	0.00	20.9
37	26	-0	-97	0	0	0	-5204	--	--	16.08	16.08	0.18	0.09	0.00	0.01	0.00	0.00	20.9
38	26	-0	1707	0	0	0	-5423	--	--	16.08	16.08	0.18	0.09	0.01	0.11	0.00	0.00	20.9
39	26	-0	702	0	0	0	-5081	--	--	16.08	16.08	0.18	0.08	0.01	0.04	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	51	-0	551	0	0	0	-4875	--	--	16.08	16.08	0.18	0.08	0.00	0.03	0.00	0.00	20.9
2	51	-0	229	0	0	0	-3680	--	--	16.08	16.08	0.29	0.06	0.00	0.01	0.00	0.00	20.9
3	51	-0	210	0	0	0	-3655	--	--	16.08	16.08	0.29	0.06	0.00	0.01	0.00	0.00	20.9
4	51	-0	638	0	0	0	-3846	--	--	16.08	16.08	0.29	0.07	0.01	0.04	0.00	0.00	20.9
5	51	-0	618	0	0	0	-3820	--	--	16.08	16.08	0.29	0.07	0.01	0.04	0.00	0.00	20.9
6	51	-0	395	0	0	0	-3768	--	--	16.08	16.08	0.29	0.07	0.00	0.02	0.00	0.00	20.9
7	51	-0	330	0	0	0	-3683	--	--	16.08	16.08	0.29	0.06	0.00	0.02	0.00	0.00	20.9
8	51	-0	517	0	0	0	-3818	--	--	16.08	16.08	0.29	0.07	0.00	0.03	0.00	0.00	20.9
9	51	-0	452	0	0	0	-3732	--	--	16.08	16.08	0.29	0.06	0.00	0.03	0.00	0.00	20.9
10	51	-0	229	0	0	0	-3680	--	--	16.08	16.08	0.29	0.06	0.00	0.01	0.00	0.00	20.9
11	51	-0	210	0	0	0	-3655	--	--	16.08	16.08	0.29	0.06	0.00	0.01	0.00	0.00	20.9
12	51	-0	638	0	0	0	-3846	--	--	16.08	16.08	0.29	0.07	0.01	0.04	0.00	0.00	20.9
13	51	-0	618	0	0	0	-3820	--	--	16.08	16.08	0.29	0.07	0.01	0.04	0.00	0.00	20.9
14	51	-0	395	0	0	0	-3768	--	--	16.08	16.08	0.29	0.07	0.00	0.02	0.00	0.00	20.9
15	51	-0	330	0	0	0	-3683	--	--	16.08	16.08	0.29	0.06	0.00	0.02	0.00	0.00	20.9
16	51	-0	517	0	0	0	-3818	--	--	16.08	16.08	0.29	0.07	0.00	0.03	0.00	0.00	20.9
17	51	-0	452	0	0	0	-3732	--	--	16.08	16.08	0.29	0.06	0.00	0.03	0.00	0.00	20.9
18	51	-0	411	0	0	0	-5448	--	--	16.08	16.08	0.18	0.09	0.00	0.03	0.00	0.00	20.9
19	51	-0	1494	0	0	0	-5610	--	--	16.08	16.08	0.18	0.09	0.01	0.09	0.00	0.00	20.9
20	51	-0	891	0	0	0	-5404	--	--	16.08	16.08	0.18	0.09	0.01	0.06	0.00	0.00	20.9
37	51	-0	-97	0	0	0	-5204	--	--	16.08	16.08	0.18	0.09	0.00	0.01	0.00	0.00	20.9
38	51	-0	1707	0	0	0	-5423	--	--	16.08	16.08	0.18	0.09	0.01	0.11	0.00	0.00	20.9
39	51	-0	702	0	0	0	-5081	--	--	16.08	16.08	0.18	0.08	0.01	0.04	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 68 NI 1840 NF 1810 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	2256	0	0	0	-4593	--	--	16.08	16.08	0.18	0.08	0.02	0.14	0.00	0.00	20.9
2	0	-0	1538	0	0	0	-3563	--	--	16.08	16.08	0.29	0.06	0.01	0.10	0.00	0.00	20.9
3	0	-0	1519	0	0	0	-3547	--	--	16.08	16.08	0.29	0.06	0.01	0.10	0.00	0.00	20.9
4	0	-0	1953	0	0	0	-3518	--	--	16.08	16.08	0.29	0.06	0.02	0.12	0.00	0.00	20.9
5	0	-0	1933	0	0	0	-3503	--	--	16.08	16.08	0.29	0.06	0.02	0.12	0.00	0.00	20.9
6	0	-0	1706	0	0	0	-3565	--	--	16.08	16.08	0.29	0.06	0.01	0.11	0.00	0.00	20.9
7	0	-0	1641	0	0	0	-3513	--	--	16.08	16.08	0.29	0.06	0.01	0.10	0.00	0.00	20.9
8	0	-0	1830	0	0	0	-3552	--	--	16.08	16.08	0.29	0.06	0.02	0.11	0.00	0.00	20.9
9	0	-0	1765	0	0	0	-3500	--	--	16.08	16.08	0.29	0.06	0.01	0.11	0.00	0.00	20.9
10	0	-0	1538	0	0	0	-3563	--	--	16.08	16.08	0.29	0.06	0.01	0.10	0.00	0.00	20.9

11	0	-0	1519	0	0	0	-3547	--	--	16.08	16.08	0.29	0.06	0.01	0.10	0.00	0.00	20.9
12	0	-0	1953	0	0	0	-3518	--	--	16.08	16.08	0.29	0.06	0.02	0.12	0.00	0.00	20.9
13	0	-0	1933	0	0	0	-3503	--	--	16.08	16.08	0.29	0.06	0.02	0.12	0.00	0.00	20.9
14	0	-0	1706	0	0	0	-3565	--	--	16.08	16.08	0.29	0.06	0.01	0.11	0.00	0.00	20.9
15	0	-0	1641	0	0	0	-3513	--	--	16.08	16.08	0.29	0.06	0.01	0.10	0.00	0.00	20.9
16	0	-0	1830	0	0	0	-3552	--	--	16.08	16.08	0.29	0.06	0.02	0.11	0.00	0.00	20.9
17	0	-0	1765	0	0	0	-3500	--	--	16.08	16.08	0.29	0.06	0.01	0.11	0.00	0.00	20.9
18	0	-0	2295	0	0	0	-5237	--	--	16.08	16.08	0.18	0.09	0.02	0.14	0.00	0.00	20.9
19	0	-0	3344	0	0	0	-4842	--	--	16.08	16.08	0.18	0.08	0.03	0.21	0.00	0.00	20.9
20	0	-0	2732	0	0	0	-4947	--	--	16.08	16.08	0.18	0.08	0.02	0.17	0.00	0.00	20.9
37	0	-0	1735	0	0	0	-5204	--	--	16.08	16.08	0.18	0.09	0.01	0.11	0.00	0.00	20.9
38	0	-0	3483	0	0	0	-4546	--	--	16.08	16.08	0.18	0.08	0.03	0.22	0.00	0.00	20.9
39	0	-0	2463	0	0	0	-4720	--	--	16.08	16.08	0.18	0.08	0.02	0.15	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	2256	0	0	0	-4593	--	--	16.08	16.08	0.18	0.08	0.02	0.14	0.00	0.00	20.9
2	26	-0	1538	0	0	0	-3563	--	--	16.08	16.08	0.29	0.06	0.01	0.10	0.00	0.00	20.9
3	26	-0	1519	0	0	0	-3547	--	--	16.08	16.08	0.29	0.06	0.01	0.10	0.00	0.00	20.9
4	26	-0	1953	0	0	0	-3518	--	--	16.08	16.08	0.29	0.06	0.02	0.12	0.00	0.00	20.9
5	26	-0	1933	0	0	0	-3503	--	--	16.08	16.08	0.29	0.06	0.02	0.12	0.00	0.00	20.9
6	26	-0	1706	0	0	0	-3565	--	--	16.08	16.08	0.29	0.06	0.01	0.11	0.00	0.00	20.9
7	26	-0	1641	0	0	0	-3513	--	--	16.08	16.08	0.29	0.06	0.01	0.10	0.00	0.00	20.9
8	26	-0	1830	0	0	0	-3552	--	--	16.08	16.08	0.29	0.06	0.02	0.11	0.00	0.00	20.9
9	26	-0	1765	0	0	0	-3500	--	--	16.08	16.08	0.29	0.06	0.01	0.11	0.00	0.00	20.9
10	26	-0	1538	0	0	0	-3563	--	--	16.08	16.08	0.29	0.06	0.01	0.10	0.00	0.00	20.9
11	26	-0	1519	0	0	0	-3547	--	--	16.08	16.08	0.29	0.06	0.01	0.10	0.00	0.00	20.9
12	26	-0	1953	0	0	0	-3518	--	--	16.08	16.08	0.29	0.06	0.02	0.12	0.00	0.00	20.9
13	26	-0	1933	0	0	0	-3503	--	--	16.08	16.08	0.29	0.06	0.02	0.12	0.00	0.00	20.9
14	26	-0	1706	0	0	0	-3565	--	--	16.08	16.08	0.29	0.06	0.01	0.11	0.00	0.00	20.9
15	26	-0	1641	0	0	0	-3513	--	--	16.08	16.08	0.29	0.06	0.01	0.10	0.00	0.00	20.9
16	26	-0	1830	0	0	0	-3552	--	--	16.08	16.08	0.29	0.06	0.02	0.11	0.00	0.00	20.9
17	26	-0	1765	0	0	0	-3500	--	--	16.08	16.08	0.29	0.06	0.01	0.11	0.00	0.00	20.9
18	26	-0	2295	0	0	0	-5237	--	--	16.08	16.08	0.18	0.09	0.02	0.14	0.00	0.00	20.9
19	26	-0	3344	0	0	0	-4842	--	--	16.08	16.08	0.18	0.08	0.03	0.21	0.00	0.00	20.9
20	26	-0	2732	0	0	0	-4947	--	--	16.08	16.08	0.18	0.08	0.02	0.17	0.00	0.00	20.9
37	26	-0	1735	0	0	0	-5204	--	--	16.08	16.08	0.18	0.09	0.01	0.11	0.00	0.00	20.9
38	26	-0	3483	0	0	0	-4546	--	--	16.08	16.08	0.18	0.08	0.03	0.22	0.00	0.00	20.9
39	26	-0	2463	0	0	0	-4720	--	--	16.08	16.08	0.18	0.08	0.02	0.15	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	2256	0	0	0	-4593	--	--	16.08	16.08	0.18	0.08	0.02	0.14	0.00	0.00	20.9
2	51	-0	1538	0	0	0	-3563	--	--	16.08	16.08	0.29	0.06	0.01	0.10	0.00	0.00	20.9
3	51	-0	1519	0	0	0	-3547	--	--	16.08	16.08	0.29	0.06	0.01	0.10	0.00	0.00	20.9
4	51	-0	1953	0	0	0	-3518	--	--	16.08	16.08	0.29	0.06	0.02	0.12	0.00	0.00	20.9
5	51	-0	1933	0	0	0	-3503	--	--	16.08	16.08	0.29	0.06	0.02	0.12	0.00	0.00	20.9
6	51	-0	1706	0	0	0	-3565	--	--	16.08	16.08	0.29	0.06	0.01	0.11	0.00	0.00	20.9
7	51	-0	1641	0	0	0	-3513	--	--	16.08	16.08	0.29	0.06	0.01	0.10	0.00	0.00	20.9
8	51	-0	1830	0	0	0	-3552	--	--	16.08	16.08	0.29	0.06	0.02	0.11	0.00	0.00	20.9
9	51	-0	1765	0	0	0	-3500	--	--	16.08	16.08	0.29	0.06	0.01	0.11	0.00	0.00	20.9
10	51	-0	1538	0	0	0	-3563	--	--	16.08	16.08	0.29	0.06	0.01	0.10	0.00	0.00	20.9
11	51	-0	1519	0	0	0	-3547	--	--	16.08	16.08	0.29	0.06	0.01	0.10	0.00	0.00	20.9
12	51	-0	1953	0	0	0	-3518	--	--	16.08	16.08	0.29	0.06	0.02	0.12	0.00	0.00	20.9
13	51	-0	1933	0	0	0	-3503	--	--	16.08	16.08	0.29	0.06	0.02	0.12	0.00	0.00	20.9
14	51	-0	1706	0	0	0	-3565	--	--	16.08	16.08	0.29	0.06	0.01	0.11	0.00	0.00	20.9
15	51	-0	1641	0	0	0	-3513	--	--	16.08	16.08	0.29	0.06	0.01	0.10	0.00	0.00	20.9
16	51	-0	1830	0	0	0	-3552	--	--	16.08	16.08	0.29	0.06	0.02	0.11	0.00	0.00	20.9
17	51	-0	1765	0	0	0	-3500	--	--	16.08	16.08	0.29	0.06	0.01	0.11	0.00	0.00	20.9
18	51	-0	2295	0	0	0	-5237	--	--	16.08	16.08	0.18	0.09	0.02	0.14	0.00	0.00	20.9
19	51	-0	3344	0	0	0	-4842	--	--	16.08	16.08	0.18	0.08	0.03	0.21	0.00	0.00	20.9
20	51	-0	2732	0	0	0	-4947	--	--	16.08	16.08	0.18	0.08	0.02	0.17	0.00	0.00	20.9
37	51	-0	1735	0	0	0	-5204	--	--	16.08	16.08	0.18	0.09	0.01	0.11	0.00	0.00	20.9
38	51	-0	3483	0	0	0	-4546	--	--	16.08	16.08	0.18	0.08	0.03	0.22	0.00	0.00	20.9
39	51	-0	2463	0	0	0	-4720	--	--	16.08	16.08	0.18	0.08	0.02	0.15	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 69 NI 1810 NF 1830 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm

1	0	-0	4012	0	0	0	-3434	--	--	16.08	16.08	0.18	0.06	0.03	0.25	0.00	0.00	20.9
2	0	-0	2882	0	0	0	-2773	--	--	16.08	16.08	0.29	0.05	0.02	0.18	0.00	0.00	20.9
3	0	-0	2862	0	0	0	-2767	--	--	16.08	16.08	0.29	0.05	0.02	0.18	0.00	0.00	20.9
4	0	-0	3311	0	0	0	-2515	--	--	16.08	16.08	0.29	0.04	0.03	0.21	0.00	0.00	20.9
5	0	-0	3291	0	0	0	-2510	--	--	16.08	16.08	0.29	0.04	0.03	0.21	0.00	0.00	20.9
6	0	-0	3055	0	0	0	-2689	--	--	16.08	16.08	0.29	0.05	0.03	0.19	0.00	0.00	20.9
7	0	-0	2989	0	0	0	-2670	--	--	16.08	16.08	0.29	0.05	0.02	0.19	0.00	0.00	20.9
8	0	-0	3184	0	0	0	-2612	--	--	16.08	16.08	0.29	0.05	0.03	0.20	0.00	0.00	20.9
9	0	-0	3117	0	0	0	-2593	--	--	16.08	16.08	0.29	0.04	0.03	0.20	0.00	0.00	20.9
10	0	-0	2882	0	0	0	-2773	--	--	16.08	16.08	0.29	0.05	0.02	0.18	0.00	0.00	20.9
11	0	-0	2862	0	0	0	-2767	--	--	16.08	16.08	0.29	0.05	0.02	0.18	0.00	0.00	20.9
12	0	-0	3311	0	0	0	-2515	--	--	16.08	16.08	0.29	0.04	0.03	0.21	0.00	0.00	20.9
13	0	-0	3291	0	0	0	-2510	--	--	16.08	16.08	0.29	0.04	0.03	0.21	0.00	0.00	20.9
14	0	-0	3055	0	0	0	-2689	--	--	16.08	16.08	0.29	0.05	0.03	0.19	0.00	0.00	20.9
15	0	-0	2989	0	0	0	-2670	--	--	16.08	16.08	0.29	0.05	0.02	0.19	0.00	0.00	20.9
16	0	-0	3184	0	0	0	-2612	--	--	16.08	16.08	0.29	0.05	0.03	0.20	0.00	0.00	20.9
17	0	-0	3117	0	0	0	-2593	--	--	16.08	16.08	0.29	0.04	0.03	0.20	0.00	0.00	20.9
18	0	-0	4240	0	0	0	-4058	--	--	16.08	16.08	0.18	0.07	0.03	0.27	0.00	0.00	20.9
19	0	-0	5275	0	0	0	-3125	--	--	16.08	16.08	0.18	0.05	0.04	0.33	0.00	0.00	20.9
20	0	-0	4642	0	0	0	-3543	--	--	16.08	16.08	0.18	0.06	0.04	0.29	0.00	0.00	20.9
37	0	-0	3614	0	0	0	-4313	--	--	16.08	16.08	0.18	0.07	0.03	0.23	0.00	0.00	20.9
38	0	-0	5339	0	0	0	-2757	--	--	16.08	16.08	0.18	0.05	0.04	0.33	0.00	0.00	20.9
39	0	-0	4284	0	0	0	-3455	--	--	16.08	16.08	0.18	0.06	0.04	0.27	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	4012	0	0	0	-3434	--	--	16.08	16.08	0.18	0.06	0.03	0.25	0.00	0.00	20.9
2	26	-0	2882	0	0	0	-2773	--	--	16.08	16.08	0.29	0.05	0.02	0.18	0.00	0.00	20.9
3	26	-0	2862	0	0	0	-2767	--	--	16.08	16.08	0.29	0.05	0.02	0.18	0.00	0.00	20.9
4	26	-0	3311	0	0	0	-2515	--	--	16.08	16.08	0.29	0.04	0.03	0.21	0.00	0.00	20.9
5	26	-0	3291	0	0	0	-2510	--	--	16.08	16.08	0.29	0.04	0.03	0.21	0.00	0.00	20.9
6	26	-0	3055	0	0	0	-2689	--	--	16.08	16.08	0.29	0.05	0.03	0.19	0.00	0.00	20.9

7	26	-0	2989	0	0	0	-2670	--	--	16.08	16.08	0.29	0.05	0.02	0.19	0.00	0.00	20.9
8	26	-0	3184	0	0	0	-2612	--	--	16.08	16.08	0.29	0.05	0.03	0.20	0.00	0.00	20.9
9	26	-0	3117	0	0	0	-2593	--	--	16.08	16.08	0.29	0.04	0.03	0.20	0.00	0.00	20.9
10	26	-0	2882	0	0	0	-2773	--	--	16.08	16.08	0.29	0.05	0.02	0.18	0.00	0.00	20.9
11	26	-0	2862	0	0	0	-2767	--	--	16.08	16.08	0.29	0.05	0.02	0.18	0.00	0.00	20.9
12	26	-0	3311	0	0	0	-2515	--	--	16.08	16.08	0.29	0.04	0.03	0.21	0.00	0.00	20.9
13	26	-0	3291	0	0	0	-2510	--	--	16.08	16.08	0.29	0.04	0.03	0.21	0.00	0.00	20.9
14	26	-0	3055	0	0	0	-2689	--	--	16.08	16.08	0.29	0.05	0.03	0.19	0.00	0.00	20.9
15	26	-0	2989	0	0	0	-2670	--	--	16.08	16.08	0.29	0.05	0.02	0.19	0.00	0.00	20.9
16	26	-0	3184	0	0	0	-2612	--	--	16.08	16.08	0.29	0.05	0.03	0.20	0.00	0.00	20.9
17	26	-0	3117	0	0	0	-2593	--	--	16.08	16.08	0.29	0.04	0.03	0.20	0.00	0.00	20.9
18	26	-0	4240	0	0	0	-4058	--	--	16.08	16.08	0.18	0.07	0.03	0.27	0.00	0.00	20.9
19	26	-0	5275	0	0	0	-3125	--	--	16.08	16.08	0.18	0.05	0.04	0.33	0.00	0.00	20.9
20	26	-0	4642	0	0	0	-3543	--	--	16.08	16.08	0.18	0.06	0.04	0.29	0.00	0.00	20.9
37	26	-0	3614	0	0	0	-4313	--	--	16.08	16.08	0.18	0.07	0.03	0.23	0.00	0.00	20.9
38	26	-0	5339	0	0	0	-2757	--	--	16.08	16.08	0.18	0.05	0.04	0.33	0.00	0.00	20.9
39	26	-0	4284	0	0	0	-3455	--	--	16.08	16.08	0.18	0.06	0.04	0.27	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	4012	0	0	0	-3434	--	--	16.08	16.08	0.18	0.06	0.03	0.25	0.00	0.00	20.9
2	51	-0	2882	0	0	0	-2773	--	--	16.08	16.08	0.29	0.05	0.02	0.18	0.00	0.00	20.9
3	51	-0	2862	0	0	0	-2767	--	--	16.08	16.08	0.29	0.05	0.02	0.18	0.00	0.00	20.9
4	51	-0	3311	0	0	0	-2515	--	--	16.08	16.08	0.29	0.04	0.03	0.21	0.00	0.00	20.9
5	51	-0	3291	0	0	0	-2510	--	--	16.08	16.08	0.29	0.04	0.03	0.21	0.00	0.00	20.9
6	51	-0	3055	0	0	0	-2689	--	--	16.08	16.08	0.29	0.05	0.03	0.19	0.00	0.00	20.9
7	51	-0	2989	0	0	0	-2670	--	--	16.08	16.08	0.29	0.05	0.02	0.19	0.00	0.00	20.9
8	51	-0	3184	0	0	0	-2612	--	--	16.08	16.08	0.29	0.05	0.03	0.20	0.00	0.00	20.9
9	51	-0	3117	0	0	0	-2593	--	--	16.08	16.08	0.29	0.04	0.03	0.20	0.00	0.00	20.9
10	51	-0	2882	0	0	0	-2773	--	--	16.08	16.08	0.29	0.05	0.02	0.18	0.00	0.00	20.9
11	51	-0	2862	0	0	0	-2767	--	--	16.08	16.08	0.29	0.05	0.02	0.18	0.00	0.00	20.9
12	51	-0	3311	0	0	0	-2515	--	--	16.08	16.08	0.29	0.04	0.03	0.21	0.00	0.00	20.9
13	51	-0	3291	0	0	0	-2510	--	--	16.08	16.08	0.29	0.04	0.03	0.21	0.00	0.00	20.9
14	51	-0	3055	0	0	0	-2689	--	--	16.08	16.08	0.29	0.05	0.03	0.19	0.00	0.00	20.9
15	51	-0	2989	0	0	0	-2670	--	--	16.08	16.08	0.29	0.05	0.02	0.19	0.00	0.00	20.9
16	51	-0	3184	0	0	0	-2612	--	--	16.08	16.08	0.29	0.05	0.03	0.20	0.00	0.00	20.9
17	51	-0	3117	0	0	0	-2593	--	--	16.08	16.08	0.29	0.04	0.03	0.20	0.00	0.00	20.9
18	51	-0	4240	0	0	0	-4058	--	--	16.08	16.08	0.18	0.07	0.03	0.27	0.00	0.00	20.9
19	51	-0	5275	0	0	0	-3125	--	--	16.08	16.08	0.18	0.05	0.04	0.33	0.00	0.00	20.9
20	51	-0	4642	0	0	0	-3543	--	--	16.08	16.08	0.18	0.06	0.04	0.29	0.00	0.00	20.9
37	51	-0	3614	0	0	0	-4313	--	--	16.08	16.08	0.18	0.07	0.03	0.23	0.00	0.00	20.9
38	51	-0	5339	0	0	0	-2757	--	--	16.08	16.08	0.18	0.05	0.04	0.33	0.00	0.00	20.9
39	51	-0	4284	0	0	0	-3455	--	--	16.08	16.08	0.18	0.06	0.04	0.27	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 70 NI 1830 NF 1829 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	5838	0	0	0	-1373	--	--	16.08	16.08	0.18	0.02	0.05	0.37	0.00	0.00	20.9
2	0	-0	4277	0	0	0	-1292	--	--	16.08	16.08	0.29	0.02	0.04	0.27	0.00	0.00	20.9
3	0	-0	4256	0	0	0	-1297	--	--	16.08	16.08	0.29	0.02	0.04	0.27	0.00	0.00	20.9
4	0	-0	4726	0	0	0	-815	--	--	16.08	16.08	0.29	0.01	0.04	0.30	0.00	0.00	20.9
5	0	-0	4705	0	0	0	-820	--	--	16.08	16.08	0.29	0.01	0.04	0.30	0.00	0.00	20.9
6	0	-0	4459	0	0	0	-1120	--	--	16.08	16.08	0.29	0.02	0.04	0.28	0.00	0.00	20.9
7	0	-0	4388	0	0	0	-1136	--	--	16.08	16.08	0.29	0.02	0.04	0.28	0.00	0.00	20.9
8	0	-0	4594	0	0	0	-976	--	--	16.08	16.08	0.29	0.02	0.04	0.29	0.00	0.00	20.9
9	0	-0	4523	0	0	0	-992	--	--	16.08	16.08	0.29	0.02	0.04	0.28	0.00	0.00	20.9
10	0	-0	4277	0	0	0	-1292	--	--	16.08	16.08	0.29	0.02	0.04	0.27	0.00	0.00	20.9
11	0	-0	4256	0	0	0	-1297	--	--	16.08	16.08	0.29	0.02	0.04	0.27	0.00	0.00	20.9
12	0	-0	4726	0	0	0	-815	--	--	16.08	16.08	0.29	0.01	0.04	0.30	0.00	0.00	20.9
13	0	-0	4705	0	0	0	-820	--	--	16.08	16.08	0.29	0.01	0.04	0.30	0.00	0.00	20.9
14	0	-0	4459	0	0	0	-1120	--	--	16.08	16.08	0.29	0.02	0.04	0.28	0.00	0.00	20.9
15	0	-0	4388	0	0	0	-1136	--	--	16.08	16.08	0.29	0.02	0.04	0.28	0.00	0.00	20.9
16	0	-0	4594	0	0	0	-976	--	--	16.08	16.08	0.29	0.02	0.04	0.29	0.00	0.00	20.9
17	0	-0	4523	0	0	0	-992	--	--	16.08	16.08	0.29	0.02	0.04	0.28	0.00	0.00	20.9
18	0	-0	6270	0	0	0	-1880	--	--	16.08	16.08	0.18	0.03	0.05	0.39	0.00	0.00	20.9
19	0	-0	7306	0	0	0	-416	--	--	16.08	16.08	0.18	0.01	0.06	0.46	0.00	0.00	20.9
20	0	-0	6642	0	0	0	-1159	--	--	16.08	16.08	0.18	0.02	0.05	0.42	0.00	0.00	20.9
37	0	-0	5564	0	0	0	-2456	--	--	16.08	16.08	0.18	0.04	0.05	0.35	0.00	0.00	20.9
38	0	-0	7291	0	0	0	-15	--	--	16.08	16.08	0.18	0.00	0.06	0.46	0.00	0.00	20.9
39	0	-0	6184	0	0	0	-1255	--	--	16.08	16.08	0.18	0.02	0.05	0.39	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	5838	0	0	0	6366	--	--	16.08	16.08	0.00	0.11	0.05	0.37	0.00	0.00	20.9
2	26	-0	4277	0	0	0	-1292	--	--	16.08	16.08	0.29	0.02	0.04	0.27	0.00	0.00	20.9
3	26	-0	4256	0	0	0	-1297	--	--	16.08	16.08	0.29	0.02	0.04	0.27	0.00	0.00	20.9
4	26	-0	4726	0	0	0	5450	--	--	16.08	16.08	0.10	0.10	0.04	0.30	0.00	0.00	20.9
5	26	-0	4705	0	0	0	5417	--	--	16.08	16.08	0.10	0.10	0.04	0.30	0.00	0.00	20.9
6	26	-0	4459	0	0	0	4791	--	--	16.08	16.08	0.10	0.09	0.04	0.28	0.00	0.00	20.9
7	26	-0	4388	0	0	0	-1136	--	--	16.08	16.08	0.29	0.02	0.04	0.28	0.00	0.00	20.9
8	26	-0	4594	0	0	0	5113	--	--	16.08	16.08	0.10	0.09	0.04	0.29	0.00	0.00	20.9
9	26	-0	4523	0	0	0	5003	--	--	16.08	16.08	0.10	0.09	0.04	0.28	0.00	0.00	20.9
10	26	-0	4277	0	0	0	-1292	--	--	16.08	16.08	0.29	0.02	0.04	0.27	0.00	0.00	20.9
11	26	-0	4256	0	0	0	-1297	--	--	16.08	16.08	0.29	0.02	0.04	0.27	0.00	0.00	20.9
12	26	-0	4726	0	0	0	5450	--	--	16.08	16.08	0.10	0.10	0.04	0.30	0.00	0.00	20.9
13	26	-0	4705	0	0	0	5417	--	--	16.08	16.08	0.10	0.10	0.04	0.30	0.00	0.00	20.9
14	26	-0	4459	0	0	0	4791	--	--	16.08	16.08	0.10	0.09	0.04	0.28	0.00	0.00	20.9
15	26	-0	4388	0	0	0	-1136	--	--	16.08	16.08	0.29	0.02	0.04	0.28	0.00	0.00	20.9
16	26	-0	4594	0	0	0	5113	--	--	16.08	16.08	0.10	0.09	0.04	0.29	0.00	0.00	20.9
17	26	-0	4523	0	0	0	5003	--	--	16.08	16.08	0.10	0.09	0.04	0.28	0.00	0.00	20.9
18	26	-0	6270	0	0	0	-1880	--	--	16.08	16.08	0.18	0.03	0.05	0.39	0.00	0.00	20.9
19	26	-0	7306	0	0	0	9269	--	--	16.08	16.08	0.00	0.16	0.06	0.46	0.00	0.00	20.9
20	26	-0	6642	0	0	0	7645	--	--	16.08	16.08	0.00	0.13	0.05	0.42	0.00	0.00	20.9
37	26	-0	5564	0	0	0	-2456	--	--	16.08	16.08	0.18	0.04	0.05	0.35	0.00	0.00	20.9
38	26	-0	7291	0	0	0	9650	--	--	16.08	16.08	0.00	0.16	0.06	0.46	0.00	0.00	20.9
39	26	-0	6184	0	0	0	6942	--	--	16.08	16.08	0.00	0.12	0.05	0.39	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	5838	0	0	0	1626	--	--	16.08	16.08	0.00	0.03	0.05	0.37	0.00	0.00	20.9
2	51	-0	4277	0	0	0	904	--	--	16.08	16.08	0.10	0.02	0.04	0.27	0.00	0.00	20.9

3	51	-0	4256	0	0	0	889	--	--	16.08	16.08	0.10	0.02	0.04	0.27	0.00	0.00	20.9
4	51	-0	4726	0	0	0	1612	--	--	16.08	16.08	0.10	0.03	0.04	0.30	0.00	0.00	20.9
5	51	-0	4705	0	0	0	1597	--	--	16.08	16.08	0.10	0.03	0.04	0.30	0.00	0.00	20.9
6	51	-0	4459	0	0	0	1170	--	--	16.08	16.08	0.10	0.02	0.04	0.28	0.00	0.00	20.9
7	51	-0	4388	0	0	0	1118	--	--	16.08	16.08	0.10	0.02	0.04	0.28	0.00	0.00	20.9
8	51	-0	4594	0	0	0	1383	--	--	16.08	16.08	0.10	0.02	0.04	0.29	0.00	0.00	20.9
9	51	-0	4523	0	0	0	1331	--	--	16.08	16.08	0.10	0.02	0.04	0.28	0.00	0.00	20.9
10	51	-0	4277	0	0	0	904	--	--	16.08	16.08	0.10	0.02	0.04	0.27	0.00	0.00	20.9
11	51	-0	4256	0	0	0	889	--	--	16.08	16.08	0.10	0.02	0.04	0.27	0.00	0.00	20.9
12	51	-0	4726	0	0	0	1612	--	--	16.08	16.08	0.10	0.03	0.04	0.30	0.00	0.00	20.9
13	51	-0	4705	0	0	0	1597	--	--	16.08	16.08	0.10	0.03	0.04	0.30	0.00	0.00	20.9
14	51	-0	4459	0	0	0	1170	--	--	16.08	16.08	0.10	0.02	0.04	0.28	0.00	0.00	20.9
15	51	-0	4388	0	0	0	1118	--	--	16.08	16.08	0.10	0.02	0.04	0.28	0.00	0.00	20.9
16	51	-0	4594	0	0	0	1383	--	--	16.08	16.08	0.10	0.02	0.04	0.29	0.00	0.00	20.9
17	51	-0	4523	0	0	0	1331	--	--	16.08	16.08	0.10	0.02	0.04	0.28	0.00	0.00	20.9
18	51	-0	6270	0	0	0	1340	--	--	16.08	16.08	0.00	0.02	0.05	0.39	0.00	0.00	20.9
19	51	-0	7306	0	0	0	3337	--	--	16.08	16.08	0.00	0.06	0.06	0.46	0.00	0.00	20.9
20	51	-0	6642	0	0	0	2252	--	--	16.08	16.08	0.00	0.04	0.05	0.42	0.00	0.00	20.9
37	51	-0	5564	0	0	0	401	--	--	16.08	16.08	0.00	0.01	0.05	0.35	0.00	0.00	20.9
38	51	-0	7291	0	0	0	3730	--	--	16.08	16.08	0.00	0.06	0.06	0.46	0.00	0.00	20.9
39	51	-0	6184	0	0	0	1921	--	--	16.08	16.08	0.00	0.03	0.05	0.39	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 71 NI 1829 NF 1842 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	7745	0	0	0	1626	--	--	16.08	16.08	0.00	0.03	0.06	0.49	0.00	0.00	20.9
2	0	-0	5733	0	0	0	904	--	--	16.08	16.08	0.10	0.02	0.05	0.36	0.00	0.00	20.9
3	0	-0	5710	0	0	0	889	--	--	16.08	16.08	0.10	0.02	0.05	0.36	0.00	0.00	20.9
4	0	-0	6206	0	0	0	1612	--	--	16.08	16.08	0.10	0.03	0.05	0.39	0.00	0.00	20.9
5	0	-0	6183	0	0	0	1597	--	--	16.08	16.08	0.10	0.03	0.05	0.39	0.00	0.00	20.9
6	0	-0	5925	0	0	0	1170	--	--	16.08	16.08	0.10	0.02	0.05	0.37	0.00	0.00	20.9
7	0	-0	5849	0	0	0	1118	--	--	16.08	16.08	0.10	0.02	0.05	0.37	0.00	0.00	20.9
8	0	-0	6067	0	0	0	1383	--	--	16.08	16.08	0.10	0.02	0.05	0.38	0.00	0.00	20.9
9	0	-0	5991	0	0	0	1331	--	--	16.08	16.08	0.10	0.02	0.05	0.38	0.00	0.00	20.9
10	0	-0	5733	0	0	0	904	--	--	16.08	16.08	0.10	0.02	0.05	0.36	0.00	0.00	20.9
11	0	-0	5710	0	0	0	889	--	--	16.08	16.08	0.10	0.02	0.05	0.36	0.00	0.00	20.9
12	0	-0	6206	0	0	0	1612	--	--	16.08	16.08	0.10	0.03	0.05	0.39	0.00	0.00	20.9
13	0	-0	6183	0	0	0	1597	--	--	16.08	16.08	0.10	0.03	0.05	0.39	0.00	0.00	20.9
14	0	-0	5925	0	0	0	1170	--	--	16.08	16.08	0.10	0.02	0.05	0.37	0.00	0.00	20.9
15	0	-0	5849	0	0	0	1118	--	--	16.08	16.08	0.10	0.02	0.05	0.37	0.00	0.00	20.9
16	0	-0	6067	0	0	0	1383	--	--	16.08	16.08	0.10	0.02	0.05	0.38	0.00	0.00	20.9
17	0	-0	5991	0	0	0	1331	--	--	16.08	16.08	0.10	0.02	0.05	0.38	0.00	0.00	20.9
18	0	-0	8397	0	0	0	1340	--	--	16.08	16.08	0.00	0.02	0.07	0.53	0.00	0.00	20.9
19	0	-0	9444	0	0	0	3337	--	--	16.08	16.08	0.00	0.06	0.08	0.59	0.00	0.00	20.9
20	0	-0	8742	0	0	0	2252	--	--	16.08	16.08	0.00	0.04	0.07	0.55	0.00	0.00	20.9
37	0	-0	7600	0	0	0	401	--	--	16.08	16.08	0.00	0.01	0.06	0.48	0.00	0.00	20.9
38	0	-0	9345	0	0	0	3730	--	--	16.08	16.08	0.00	0.06	0.08	0.59	0.00	0.00	20.9
39	0	-0	8175	0	0	0	1921	--	--	16.08	16.08	0.00	0.03	0.07	0.51	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	7745	0	0	0	11892	--	--	16.08	16.08	0.00	0.20	0.06	0.49	0.00	0.00	20.9
2	26	-0	5733	0	0	0	8504	--	--	16.08	16.08	0.10	0.15	0.05	0.36	0.00	0.00	20.9
3	26	-0	5710	0	0	0	8458	--	--	16.08	16.08	0.10	0.15	0.05	0.36	0.00	0.00	20.9
4	26	-0	6206	0	0	0	9839	--	--	16.08	16.08	0.10	0.17	0.05	0.39	0.00	0.00	20.9
5	26	-0	6183	0	0	0	9793	--	--	16.08	16.08	0.10	0.17	0.05	0.39	0.00	0.00	20.9
6	26	-0	5925	0	0	0	9024	--	--	16.08	16.08	0.10	0.16	0.05	0.37	0.00	0.00	20.9
7	26	-0	5849	0	0	0	8872	--	--	16.08	16.08	0.10	0.16	0.05	0.37	0.00	0.00	20.9
8	26	-0	6067	0	0	0	9425	--	--	16.08	16.08	0.10	0.17	0.05	0.38	0.00	0.00	20.9
9	26	-0	5991	0	0	0	9272	--	--	16.08	16.08	0.10	0.16	0.05	0.38	0.00	0.00	20.9
10	26	-0	5733	0	0	0	8504	--	--	16.08	16.08	0.10	0.15	0.05	0.36	0.00	0.00	20.9
11	26	-0	5710	0	0	0	8458	--	--	16.08	16.08	0.10	0.15	0.05	0.36	0.00	0.00	20.9
12	26	-0	6206	0	0	0	9839	--	--	16.08	16.08	0.10	0.17	0.05	0.39	0.00	0.00	20.9
13	26	-0	6183	0	0	0	9793	--	--	16.08	16.08	0.10	0.17	0.05	0.39	0.00	0.00	20.9
14	26	-0	5925	0	0	0	9024	--	--	16.08	16.08	0.10	0.16	0.05	0.37	0.00	0.00	20.9
15	26	-0	5849	0	0	0	8872	--	--	16.08	16.08	0.10	0.16	0.05	0.37	0.00	0.00	20.9
16	26	-0	6067	0	0	0	9425	--	--	16.08	16.08	0.10	0.17	0.05	0.38	0.00	0.00	20.9
17	26	-0	5991	0	0	0	9272	--	--	16.08	16.08	0.10	0.16	0.05	0.38	0.00	0.00	20.9
18	26	-0	8397	0	0	0	12471	--	--	16.08	16.08	0.00	0.21	0.07	0.53	0.00	0.00	20.9
19	26	-0	9444	0	0	0	15856	--	--	16.08	16.08	0.00	0.27	0.08	0.59	0.00	0.00	20.9
20	26	-0	8742	0	0	0	13841	--	--	16.08	16.08	0.00	0.24	0.07	0.55	0.00	0.00	20.9
37	26	-0	7600	0	0	0	10476	--	--	16.08	16.08	0.00	0.18	0.06	0.48	0.00	0.00	20.9
38	26	-0	9345	0	0	0	16117	--	--	16.08	16.08	0.00	0.27	0.08	0.59	0.00	0.00	20.9
39	26	-0	8175	0	0	0	12758	--	--	16.08	16.08	0.00	0.22	0.07	0.51	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	7745	0	0	0	5604	--	--	16.08	16.08	0.00	0.10	0.06	0.49	0.00	0.00	20.9
2	51	-0	5733	0	0	0	3849	--	--	16.08	16.08	0.10	0.07	0.05	0.36	0.00	0.00	20.9
3	51	-0	5710	0	0	0	3822	--	--	16.08	16.08	0.10	0.07	0.05	0.36	0.00	0.00	20.9
4	51	-0	6206	0	0	0	4800	--	--	16.08	16.08	0.10	0.09	0.05	0.39	0.00	0.00	20.9
5	51	-0	6183	0	0	0	4773	--	--	16.08	16.08	0.10	0.08	0.05	0.39	0.00	0.00	20.9
6	51	-0	5925	0	0	0	4214	--	--	16.08	16.08	0.10	0.07	0.05	0.37	0.00	0.00	20.9
7	51	-0	5849	0	0	0	4123	--	--	16.08	16.08	0.10	0.07	0.05	0.37	0.00	0.00	20.9
8	51	-0	6067	0	0	0	4499	--	--	16.08	16.08	0.10	0.08	0.05	0.38	0.00	0.00	20.9
9	51	-0	5991	0	0	0	4408	--	--	16.08	16.08	0.10	0.08	0.05	0.38	0.00	0.00	20.9
10	51	-0	5733	0	0	0	3849	--	--	16.08	16.08	0.10	0.07	0.05	0.36	0.00	0.00	20.9
11	51	-0	5710	0	0	0	3822	--	--	16.08	16.08	0.10	0.07	0.05	0.36	0.00	0.00	20.9
12	51	-0	6206	0	0	0	4800	--	--	16.08	16.08	0.10	0.09	0.05	0.39	0.00	0.00	20.9
13	51	-0	6183	0	0	0	4773	--	--	16.08	16.08	0.10	0.08	0.05	0.39	0.00	0.00	20.9
14	51	-0	5925	0	0	0	4214	--	--	16.08	16.08	0.10	0.07	0.05	0.37	0.00	0.00	20.9
15	51	-0	5849	0	0	0	4123	--	--	16.08	16.08	0.10	0.07	0.05	0.37	0.00	0.00	20.9
16	51	-0	6067	0	0	0	4499	--	--	16.08	16.08	0.10	0.08	0.05	0.38	0.00	0.00	20.9
17	51	-0	5991	0	0	0	4408	--	--	16.08	16.08	0.10	0.08	0.05	0.38	0.00	0.00	20.9
18	51	-0	8397	0	0	0	5654	--	--	16.08	16.08	0.00	0.10	0.07	0.53	0.00	0.00	20.9
19	51	-0	9444	0	0	0	8189	--	--	16.08	16.08	0.00	0.14	0.08	0.59	0.00	0.00	20.9
20	51	-0	8742	0	0	0	6743	--	--	16.08	16.08	0.00	0.11	0.07	0.55	0.00	0.00	20.9
37	51	-0	7600	0	0	0	4305	--	--	16.08	16.08	0.00	0.07	0.06	0.48	0.00	0.00	20.9
38	51	-0	9345	0	0	0	8530	--	--	16.08	16.08	0.00	0.15	0.08	0.59	0.00	0.00	20.9
39	51	-0	8175	0	0	0	6121	--	--	16.08	16.08	0.00	0.10	0.07	0.51	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 72 NI 1842 NF 1844 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	9729	0	0	0	5604	--	--	16.08	16.08	0.00	0.10	0.08	0.61	0.00	0.00	20.9
2	0	-0	7247	0	0	0	3849	--	--	16.08	16.08	0.10	0.07	0.06	0.45	0.00	0.00	20.9
3	0	-0	7222	0	0	0	3822	--	--	16.08	16.08	0.10	0.07	0.06	0.45	0.00	0.00	20.9
4	0	-0	7746	0	0	0	4800	--	--	16.08	16.08	0.10	0.09	0.06	0.49	0.00	0.00	20.9
5	0	-0	7721	0	0	0	4773	--	--	16.08	16.08	0.10	0.08	0.06	0.48	0.00	0.00	20.9
6	0	-0	7451	0	0	0	4214	--	--	16.08	16.08	0.10	0.07	0.06	0.47	0.00	0.00	20.9
7	0	-0	7367	0	0	0	4123	--	--	16.08	16.08	0.10	0.07	0.06	0.46	0.00	0.00	20.9
8	0	-0	7601	0	0	0	4499	--	--	16.08	16.08	0.10	0.08	0.06	0.48	0.00	0.00	20.9
9	0	-0	7517	0	0	0	4408	--	--	16.08	16.08	0.10	0.08	0.06	0.47	0.00	0.00	20.9
10	0	-0	7247	0	0	0	3849	--	--	16.08	16.08	0.10	0.07	0.06	0.45	0.00	0.00	20.9
11	0	-0	7222	0	0	0	3822	--	--	16.08	16.08	0.10	0.07	0.06	0.45	0.00	0.00	20.9
12	0	-0	7746	0	0	0	4800	--	--	16.08	16.08	0.10	0.09	0.06	0.49	0.00	0.00	20.9
13	0	-0	7721	0	0	0	4773	--	--	16.08	16.08	0.10	0.08	0.06	0.48	0.00	0.00	20.9
14	0	-0	7451	0	0	0	4214	--	--	16.08	16.08	0.10	0.07	0.06	0.47	0.00	0.00	20.9
15	0	-0	7367	0	0	0	4123	--	--	16.08	16.08	0.10	0.07	0.06	0.46	0.00	0.00	20.9
16	0	-0	7601	0	0	0	4499	--	--	16.08	16.08	0.10	0.08	0.06	0.48	0.00	0.00	20.9
17	0	-0	7517	0	0	0	4408	--	--	16.08	16.08	0.10	0.08	0.06	0.47	0.00	0.00	20.9
18	0	-0	10620	0	0	0	5654	--	--	16.08	16.08	0.00	0.10	0.09	0.67	0.00	0.00	20.9
19	0	-0	11680	0	0	0	8189	--	--	16.08	16.08	0.00	0.14	0.10	0.73	0.00	0.00	20.9
20	0	-0	10940	0	0	0	6743	--	--	16.08	16.08	0.00	0.11	0.09	0.69	0.00	0.00	20.9
37	0	-0	9726	0	0	0	4305	--	--	16.08	16.08	0.00	0.07	0.08	0.61	0.00	0.00	20.9
38	0	-0	11490	0	0	0	8530	--	--	16.08	16.08	0.00	0.15	0.09	0.72	0.00	0.00	20.9
39	0	-0	10250	0	0	0	6121	--	--	16.08	16.08	0.00	0.10	0.08	0.64	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	9729	0	0	0	18500	--	--	16.08	16.08	0.00	0.32	0.08	0.61	0.00	0.00	20.9
2	26	-0	7247	0	0	0	13456	--	--	16.08	16.08	0.10	0.24	0.06	0.45	0.00	0.00	20.9
3	26	-0	7222	0	0	0	13395	--	--	16.08	16.08	0.10	0.24	0.06	0.45	0.00	0.00	20.9
4	26	-0	7746	0	0	0	15068	--	--	16.08	16.08	0.10	0.27	0.06	0.49	0.00	0.00	20.9
5	26	-0	7721	0	0	0	15007	--	--	16.08	16.08	0.10	0.27	0.06	0.48	0.00	0.00	20.9
6	26	-0	7451	0	0	0	14091	--	--	16.08	16.08	0.10	0.25	0.06	0.47	0.00	0.00	20.9
7	26	-0	7367	0	0	0	13888	--	--	16.08	16.08	0.10	0.25	0.06	0.46	0.00	0.00	20.9
8	26	-0	7601	0	0	0	14575	--	--	16.08	16.08	0.10	0.26	0.06	0.48	0.00	0.00	20.9
9	26	-0	7517	0	0	0	14372	--	--	16.08	16.08	0.10	0.26	0.06	0.47	0.00	0.00	20.9
10	26	-0	7247	0	0	0	13456	--	--	16.08	16.08	0.10	0.24	0.06	0.45	0.00	0.00	20.9
11	26	-0	7222	0	0	0	13395	--	--	16.08	16.08	0.10	0.24	0.06	0.45	0.00	0.00	20.9
12	26	-0	7746	0	0	0	15068	--	--	16.08	16.08	0.10	0.27	0.06	0.49	0.00	0.00	20.9
13	26	-0	7721	0	0	0	15007	--	--	16.08	16.08	0.10	0.27	0.06	0.48	0.00	0.00	20.9
14	26	-0	7451	0	0	0	14091	--	--	16.08	16.08	0.10	0.25	0.06	0.47	0.00	0.00	20.9
15	26	-0	7367	0	0	0	13888	--	--	16.08	16.08	0.10	0.25	0.06	0.46	0.00	0.00	20.9
16	26	-0	7601	0	0	0	14575	--	--	16.08	16.08	0.10	0.26	0.06	0.48	0.00	0.00	20.9
17	26	-0	7517	0	0	0	14372	--	--	16.08	16.08	0.10	0.26	0.06	0.47	0.00	0.00	20.9
18	26	-0	10620	0	0	0	19732	--	--	16.08	16.08	0.00	0.34	0.09	0.67	0.00	0.00	20.9
19	26	-0	11680	0	0	0	23672	--	--	16.08	16.08	0.00	0.40	0.10	0.73	0.00	0.00	20.9
20	26	-0	10940	0	0	0	21244	--	--	16.08	16.08	0.00	0.36	0.09	0.69	0.00	0.00	20.9
37	26	-0	9726	0	0	0	17198	--	--	16.08	16.08	0.00	0.29	0.08	0.61	0.00	0.00	20.9
38	26	-0	11490	0	0	0	23760	--	--	16.08	16.08	0.00	0.41	0.09	0.72	0.00	0.00	20.9
39	26	-0	10250	0	0	0	19710	--	--	16.08	16.08	0.00	0.34	0.08	0.64	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	9729	0	0	0	10600	--	--	16.08	16.08	0.00	0.18	0.08	0.61	0.00	0.00	20.9
2	51	-0	7247	0	0	0	7572	--	--	16.08	16.08	0.10	0.13	0.06	0.45	0.00	0.00	20.9
3	51	-0	7222	0	0	0	7531	--	--	16.08	16.08	0.10	0.13	0.06	0.45	0.00	0.00	20.9
4	51	-0	7746	0	0	0	8779	--	--	16.08	16.08	0.10	0.16	0.06	0.49	0.00	0.00	20.9
5	51	-0	7721	0	0	0	8738	--	--	16.08	16.08	0.10	0.16	0.06	0.48	0.00	0.00	20.9
6	51	-0	7451	0	0	0	8041	--	--	16.08	16.08	0.10	0.14	0.06	0.47	0.00	0.00	20.9
7	51	-0	7367	0	0	0	7907	--	--	16.08	16.08	0.10	0.14	0.06	0.46	0.00	0.00	20.9
8	51	-0	7601	0	0	0	8403	--	--	16.08	16.08	0.10	0.15	0.06	0.48	0.00	0.00	20.9
9	51	-0	7517	0	0	0	8269	--	--	16.08	16.08	0.10	0.15	0.06	0.47	0.00	0.00	20.9
10	51	-0	7247	0	0	0	7572	--	--	16.08	16.08	0.10	0.13	0.06	0.45	0.00	0.00	20.9
11	51	-0	7222	0	0	0	7531	--	--	16.08	16.08	0.10	0.13	0.06	0.45	0.00	0.00	20.9
12	51	-0	7746	0	0	0	8779	--	--	16.08	16.08	0.10	0.16	0.06	0.49	0.00	0.00	20.9
13	51	-0	7721	0	0	0	8738	--	--	16.08	16.08	0.10	0.16	0.06	0.48	0.00	0.00	20.9
14	51	-0	7451	0	0	0	8041	--	--	16.08	16.08	0.10	0.14	0.06	0.47	0.00	0.00	20.9
15	51	-0	7367	0	0	0	7907	--	--	16.08	16.08	0.10	0.14	0.06	0.46	0.00	0.00	20.9
16	51	-0	7601	0	0	0	8403	--	--	16.08	16.08	0.10	0.15	0.06	0.48	0.00	0.00	20.9
17	51	-0	7517	0	0	0	8269	--	--	16.08	16.08	0.10	0.15	0.06	0.47	0.00	0.00	20.9
18	51	-0	10620	0	0	0	11110	--	--	16.08	16.08	0.00	0.19	0.09	0.67	0.00	0.00	20.9
19	51	-0	11680	0	0	0	14190	--	--	16.08	16.08	0.00	0.24	0.10	0.73	0.00	0.00	20.9
20	51	-0	10940	0	0	0	12360	--	--	16.08	16.08	0.00	0.21	0.09	0.69	0.00	0.00	20.9
37	51	-0	9726	0	0	0	9301	--	--	16.08	16.08	0.00	0.16	0.08	0.61	0.00	0.00	20.9
38	51	-0	11490	0	0	0	14430	--	--	16.08	16.08	0.00	0.25	0.09	0.72	0.00	0.00	20.9
39	51	-0	10250	0	0	0	11390	--	--	16.08	16.08	0.00	0.19	0.08	0.64	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 73 NI 1844 NF 1659 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-9679	0	0	0	10950	--	--	16.08	16.08	0.00	0.19	0.08	0.61	0.00	0.00	20.9
2	0	-0	-7594	0	0	0	8883	--	--	16.08	16.08	0.10	0.16	0.06	0.48	0.00	0.00	20.9
3	0	-0	-7573	0	0	0	8841	--	--	16.08	16.08	0.10	0.16	0.06	0.48	0.00	0.00	20.9
4	0	-0	-7318	0	0	0	8008	--	--	16.08	16.08	0.10	0.14	0.06	0.46	0.00	0.00	20.9
5	0	-0	-7297	0	0	0	7966	--	--	16.08	16.08	0.10	0.14	0.06	0.46	0.00	0.00	20.9
6	0	-0	-7522	0	0	0	8625	--	--	16.08	16.08	0.10	0.15	0.06	0.47	0.00	0.00	20.9
7	0	-0	-7452	0	0	0	8486	--	--	16.08	16.08	0.10	0.15	0.06	0.47	0.00	0.00	20.9
8	0	-0	-7439	0	0	0	8363	--	--	16.08	16.08	0.10	0.15	0.06	0.47	0.00	0.00	20.9
9	0	-0	-7370	0	0	0	8224	--	--	16.08	16.08	0.10	0.15	0.06	0.46	0.00	0.00	20.9
10	0	-0	-7594	0	0	0	8883	--	--	16.08	16.08	0.10	0.16	0.06	0.48	0.00	0.00	20.9

11	0	-0	-7573	0	0	0	8841	--	--	16.08	16.08	0.10	0.16	0.06	0.48	0.00	0.00	20.9
12	0	-0	-7318	0	0	0	8008	--	--	16.08	16.08	0.10	0.14	0.06	0.46	0.00	0.00	20.9
13	0	-0	-7297	0	0	0	7966	--	--	16.08	16.08	0.10	0.14	0.06	0.46	0.00	0.00	20.9
14	0	-0	-7522	0	0	0	8625	--	--	16.08	16.08	0.10	0.15	0.06	0.47	0.00	0.00	20.9
15	0	-0	-7452	0	0	0	8486	--	--	16.08	16.08	0.10	0.15	0.06	0.47	0.00	0.00	20.9
16	0	-0	-7439	0	0	0	8363	--	--	16.08	16.08	0.10	0.15	0.06	0.47	0.00	0.00	20.9
17	0	-0	-7370	0	0	0	8224	--	--	16.08	16.08	0.10	0.15	0.06	0.46	0.00	0.00	20.9
18	0	-0	-11730	0	0	0	14840	--	--	16.08	16.08	0.00	0.25	0.10	0.74	0.00	0.00	20.9
19	0	-0	-10460	0	0	0	11280	--	--	16.08	16.08	0.00	0.19	0.09	0.66	0.00	0.00	20.9
20	0	-0	-10900	0	0	0	12780	--	--	16.08	16.08	0.00	0.22	0.09	0.68	0.00	0.00	20.9
37	0	-0	-11600	0	0	0	15230	--	--	16.08	16.08	0.00	0.26	0.10	0.73	0.00	0.00	20.9
38	0	-0	-9500	0	0	0	9299	--	--	16.08	16.08	0.00	0.16	0.08	0.60	0.00	0.00	20.9
39	0	-0	-10230	0	0	0	11790	--	--	16.08	16.08	0.00	0.20	0.08	0.64	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	-9679	0	0	0	10950	--	--	16.08	16.08	0.00	0.19	0.08	0.61	0.00	0.00	20.9
2	26	-0	-7594	0	0	0	8883	--	--	16.08	16.08	0.10	0.16	0.06	0.48	0.00	0.00	20.9
3	26	-0	-7573	0	0	0	8841	--	--	16.08	16.08	0.10	0.16	0.06	0.48	0.00	0.00	20.9
4	26	-0	-7318	0	0	0	8008	--	--	16.08	16.08	0.10	0.14	0.06	0.46	0.00	0.00	20.9
5	26	-0	-7297	0	0	0	7966	--	--	16.08	16.08	0.10	0.14	0.06	0.46	0.00	0.00	20.9
6	26	-0	-7522	0	0	0	8625	--	--	16.08	16.08	0.10	0.15	0.06	0.47	0.00	0.00	20.9
7	26	-0	-7452	0	0	0	8486	--	--	16.08	16.08	0.10	0.15	0.06	0.47	0.00	0.00	20.9
8	26	-0	-7439	0	0	0	8363	--	--	16.08	16.08	0.10	0.15	0.06	0.47	0.00	0.00	20.9
9	26	-0	-7370	0	0	0	8224	--	--	16.08	16.08	0.10	0.15	0.06	0.46	0.00	0.00	20.9
10	26	-0	-7594	0	0	0	8883	--	--	16.08	16.08	0.10	0.16	0.06	0.48	0.00	0.00	20.9
11	26	-0	-7573	0	0	0	8841	--	--	16.08	16.08	0.10	0.16	0.06	0.48	0.00	0.00	20.9
12	26	-0	-7318	0	0	0	8008	--	--	16.08	16.08	0.10	0.14	0.06	0.46	0.00	0.00	20.9
13	26	-0	-7297	0	0	0	7966	--	--	16.08	16.08	0.10	0.14	0.06	0.46	0.00	0.00	20.9
14	26	-0	-7522	0	0	0	8625	--	--	16.08	16.08	0.10	0.15	0.06	0.47	0.00	0.00	20.9
15	26	-0	-7452	0	0	0	8486	--	--	16.08	16.08	0.10	0.15	0.06	0.47	0.00	0.00	20.9
16	26	-0	-7439	0	0	0	8363	--	--	16.08	16.08	0.10	0.15	0.06	0.47	0.00	0.00	20.9
17	26	-0	-7370	0	0	0	8224	--	--	16.08	16.08	0.10	0.15	0.06	0.46	0.00	0.00	20.9
18	26	-0	-11730	0	0	0	14840	--	--	16.08	16.08	0.00	0.25	0.10	0.74	0.00	0.00	20.9
19	26	-0	-10460	0	0	0	11280	--	--	16.08	16.08	0.00	0.19	0.09	0.66	0.00	0.00	20.9
20	26	-0	-10900	0	0	0	12780	--	--	16.08	16.08	0.00	0.22	0.09	0.68	0.00	0.00	20.9
37	26	-0	-11600	0	0	0	15230	--	--	16.08	16.08	0.00	0.26	0.10	0.73	0.00	0.00	20.9
38	26	-0	-9500	0	0	0	9299	--	--	16.08	16.08	0.00	0.16	0.08	0.60	0.00	0.00	20.9
39	26	-0	-10230	0	0	0	11790	--	--	16.08	16.08	0.00	0.20	0.08	0.64	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	-9679	0	0	0	5981	--	--	16.08	16.08	0.00	0.10	0.08	0.61	0.00	0.00	20.9
2	51	-0	-7594	0	0	0	4982	--	--	16.08	16.08	0.10	0.09	0.06	0.48	0.00	0.00	20.9
3	51	-0	-7573	0	0	0	4951	--	--	16.08	16.08	0.10	0.09	0.06	0.48	0.00	0.00	20.9
4	51	-0	-7318	0	0	0	4249	--	--	16.08	16.08	0.10	0.08	0.06	0.46	0.00	0.00	20.9
5	51	-0	-7297	0	0	0	4218	--	--	16.08	16.08	0.10	0.07	0.06	0.46	0.00	0.00	20.9
6	51	-0	-7522	0	0	0	4762	--	--	16.08	16.08	0.10	0.08	0.06	0.47	0.00	0.00	20.9
7	51	-0	-7452	0	0	0	4659	--	--	16.08	16.08	0.10	0.08	0.06	0.47	0.00	0.00	20.9
8	51	-0	-7439	0	0	0	4542	--	--	16.08	16.08	0.10	0.08	0.06	0.47	0.00	0.00	20.9
9	51	-0	-7370	0	0	0	4439	--	--	16.08	16.08	0.10	0.08	0.06	0.46	0.00	0.00	20.9
10	51	-0	-7594	0	0	0	4982	--	--	16.08	16.08	0.10	0.09	0.06	0.48	0.00	0.00	20.9
11	51	-0	-7573	0	0	0	4951	--	--	16.08	16.08	0.10	0.09	0.06	0.48	0.00	0.00	20.9
12	51	-0	-7318	0	0	0	4249	--	--	16.08	16.08	0.10	0.08	0.06	0.46	0.00	0.00	20.9
13	51	-0	-7297	0	0	0	4218	--	--	16.08	16.08	0.10	0.07	0.06	0.46	0.00	0.00	20.9
14	51	-0	-7522	0	0	0	4762	--	--	16.08	16.08	0.10	0.08	0.06	0.47	0.00	0.00	20.9
15	51	-0	-7452	0	0	0	4659	--	--	16.08	16.08	0.10	0.08	0.06	0.47	0.00	0.00	20.9
16	51	-0	-7439	0	0	0	4542	--	--	16.08	16.08	0.10	0.08	0.06	0.47	0.00	0.00	20.9
17	51	-0	-7370	0	0	0	4439	--	--	16.08	16.08	0.10	0.08	0.06	0.46	0.00	0.00	20.9
18	51	-0	-11730	0	0	0	8821	--	--	16.08	16.08	0.00	0.15	0.10	0.74	0.00	0.00	20.9
19	51	-0	-10460	0	0	0	5909	--	--	16.08	16.08	0.00	0.10	0.09	0.66	0.00	0.00	20.9
20	51	-0	-10900	0	0	0	7177	--	--	16.08	16.08	0.00	0.12	0.09	0.68	0.00	0.00	20.9
37	51	-0	-11600	0	0	0	9273	--	--	16.08	16.08	0.00	0.16	0.10	0.73	0.00	0.00	20.9
38	51	-0	-9500	0	0	0	4420	--	--	16.08	16.08	0.00	0.08	0.08	0.60	0.00	0.00	20.9
39	51	-0	-10230	0	0	0	6534	--	--	16.08	16.08	0.00	0.11	0.08	0.64	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 74 NI 1659 NF 1823 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm

1	0	-0	-7677	0	0	0	5981	--	--	16.08	16.08	0.00	0.10	0.06	0.48	0.00	0.00	20.9
2	0	-0	-6061	0	0	0	4982	--	--	16.08	16.08	0.10	0.09	0.05	0.38	0.00	0.00	20.9
3	0	-0	-6043	0	0	0	4951	--	--	16.08	16.08	0.10	0.09	0.05	0.38	0.00	0.00	20.9
4	0	-0	-5768	0	0	0	4249	--	--	16.08	16.08	0.10	0.08	0.05	0.36	0.00	0.00	20.9
5	0	-0	-5750	0	0	0	4218	--	--	16.08	16.08	0.10	0.07	0.05	0.36	0.00	0.00	20.9
6	0	-0	-5979	0	0	0	4762	--	--	16.08	16.08	0.10	0.08	0.05	0.38	0.00	0.00	20.9
7	0	-0	-5919	0	0	0	4659	--	--	16.08	16.08	0.10	0.08	0.05	0.37	0.00	0.00	20.9
8	0	-0	-5891	0	0	0	4542	--	--	16.08	16.08	0.10	0.08	0.05	0.37	0.00	0.00	20.9
9	0	-0	-5831	0	0	0	4439	--	--	16.08	16.08	0.10	0.08	0.05	0.37	0.00	0.00	20.9
10	0	-0	-6061	0	0	0	4982	--	--	16.08	16.08	0.10	0.09	0.05	0.38	0.00	0.00	20.9
11	0	-0	-6043	0	0	0	4951	--	--	16.08	16.08	0.10	0.09	0.05	0.38	0.00	0.00	20.9
12	0	-0	-5768	0	0	0	4249	--	--	16.08	16.08	0.10	0.08	0.05	0.36	0.00	0.00	20.9
13	0	-0	-5750	0	0	0	4218	--	--	16.08	16.08	0.10	0.07	0.05	0.36	0.00	0.00	20.9
14	0	-0	-5979	0	0	0	4762	--	--	16.08	16.08	0.10	0.08	0.05	0.38	0.00	0.00	20.9
15	0	-0	-5919	0	0	0	4659	--	--	16.08	16.08	0.10	0.08	0.05	0.37	0.00	0.00	20.9
16	0	-0	-5891	0	0	0	4542	--	--	16.08	16.08	0.10	0.08	0.05	0.37	0.00	0.00	20.9
17	0	-0	-5831	0	0	0	4439	--	--	16.08	16.08	0.10	0.08	0.05	0.37	0.00	0.00	20.9
18	0	-0	-9461	0	0	0	8821	--	--	16.08	16.08	0.00	0.15	0.08	0.59	0.00	0.00	20.9
19	0	-0	-8212	0	0	0	5909	--	--	16.08	16.08	0.00	0.10	0.07	0.52	0.00	0.00	20.9
20	0	-0	-8677	0	0	0	7177	--	--	16.08	16.08	0.00	0.12	0.07	0.54	0.00	0.00	20.9
37	0	-0	-9433	0	0	0	9273	--	--	16.08	16.08	0.00	0.16	0.08	0.59	0.00	0.00	20.9
38	0	-0	-7352	0	0	0	4420	--	--	16.08	16.08	0.00	0.08	0.06	0.46	0.00	0.00	20.9
39	0	-0	-8127	0	0	0	6534	--	--	16.08	16.08	0.00	0.11	0.07	0.51	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	-7677	0	0	0	5981	--	--	16.08	16.08	0.00	0.10	0.06	0.48	0.00	0.00	20.9
2	26	-0	-6061	0	0	0	4982	--	--	16.08	16.08	0.10	0.09	0.05	0.38	0.00	0.00	20.9
3	26	-0	-6043	0	0	0	4951	--	--	16.08	16.08	0.10	0.09	0.05	0.38	0.00	0.00	20.9
4	26	-0	-5768	0	0	0	4249	--	--	16.08	16.08	0.10	0.08	0.05	0.36	0.00	0.00	20.9
5	26	-0	-5750	0	0	0	4218	--	--	16.08	16.08	0.10	0.07	0.05	0.36	0.00	0.00	20.9
6	26	-0	-5979	0	0	0	4762	--	--	16.08	16.08	0.10	0.08	0.05	0.38	0.00	0.00	20.9

7	26	-0	-5919	0	0	0	4659	--	--	16.08	16.08	0.10	0.08	0.05	0.37	0.00	0.00	20.9
8	26	-0	-5891	0	0	0	4542	--	--	16.08	16.08	0.10	0.08	0.05	0.37	0.00	0.00	20.9
9	26	-0	-5831	0	0	0	4439	--	--	16.08	16.08	0.10	0.08	0.05	0.37	0.00	0.00	20.9
10	26	-0	-6061	0	0	0	4982	--	--	16.08	16.08	0.10	0.09	0.05	0.38	0.00	0.00	20.9
11	26	-0	-6043	0	0	0	4951	--	--	16.08	16.08	0.10	0.09	0.05	0.38	0.00	0.00	20.9
12	26	-0	-5768	0	0	0	4249	--	--	16.08	16.08	0.10	0.08	0.05	0.36	0.00	0.00	20.9
13	26	-0	-5750	0	0	0	4218	--	--	16.08	16.08	0.10	0.07	0.05	0.36	0.00	0.00	20.9
14	26	-0	-5979	0	0	0	4762	--	--	16.08	16.08	0.10	0.08	0.05	0.38	0.00	0.00	20.9
15	26	-0	-5919	0	0	0	4659	--	--	16.08	16.08	0.10	0.08	0.05	0.37	0.00	0.00	20.9
16	26	-0	-5891	0	0	0	4542	--	--	16.08	16.08	0.10	0.08	0.05	0.37	0.00	0.00	20.9
17	26	-0	-5831	0	0	0	4439	--	--	16.08	16.08	0.10	0.08	0.05	0.37	0.00	0.00	20.9
18	26	-0	-9461	0	0	0	8821	--	--	16.08	16.08	0.00	0.15	0.08	0.59	0.00	0.00	20.9
19	26	-0	-8212	0	0	0	5909	--	--	16.08	16.08	0.00	0.10	0.07	0.52	0.00	0.00	20.9
20	26	-0	-8677	0	0	0	7177	--	--	16.08	16.08	0.00	0.12	0.07	0.54	0.00	0.00	20.9
37	26	-0	-9433	0	0	0	9273	--	--	16.08	16.08	0.00	0.16	0.08	0.59	0.00	0.00	20.9
38	26	-0	-7352	0	0	0	4420	--	--	16.08	16.08	0.00	0.08	0.06	0.46	0.00	0.00	20.9
39	26	-0	-8127	0	0	0	6534	--	--	16.08	16.08	0.00	0.11	0.07	0.51	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	-7677	0	0	0	2037	--	--	16.08	16.08	0.00	0.03	0.06	0.48	0.00	0.00	20.9
2	51	-0	-6061	0	0	0	1869	--	--	16.08	16.08	0.10	0.03	0.05	0.38	0.00	0.00	20.9
3	51	-0	-6043	0	0	0	1847	--	--	16.08	16.08	0.10	0.03	0.05	0.38	0.00	0.00	20.9
4	51	-0	-5768	0	0	0	1286	--	--	16.08	16.08	0.10	0.02	0.05	0.36	0.00	0.00	20.9
5	51	-0	-5750	0	0	0	1265	--	--	16.08	16.08	0.10	0.02	0.05	0.36	0.00	0.00	20.9
6	51	-0	-5979	0	0	0	1690	--	--	16.08	16.08	0.10	0.03	0.05	0.38	0.00	0.00	20.9
7	51	-0	-5919	0	0	0	1618	--	--	16.08	16.08	0.10	0.03	0.05	0.37	0.00	0.00	20.9
8	51	-0	-5891	0	0	0	1516	--	--	16.08	16.08	0.10	0.03	0.05	0.37	0.00	0.00	20.9
9	51	-0	-5831	0	0	0	1443	--	--	16.08	16.08	0.10	0.03	0.05	0.37	0.00	0.00	20.9
10	51	-0	-6061	0	0	0	1869	--	--	16.08	16.08	0.10	0.03	0.05	0.38	0.00	0.00	20.9
11	51	-0	-6043	0	0	0	1847	--	--	16.08	16.08	0.10	0.03	0.05	0.38	0.00	0.00	20.9
12	51	-0	-5768	0	0	0	1286	--	--	16.08	16.08	0.10	0.02	0.05	0.36	0.00	0.00	20.9
13	51	-0	-5750	0	0	0	1265	--	--	16.08	16.08	0.10	0.02	0.05	0.36	0.00	0.00	20.9
14	51	-0	-5979	0	0	0	1690	--	--	16.08	16.08	0.10	0.03	0.05	0.38	0.00	0.00	20.9
15	51	-0	-5919	0	0	0	1618	--	--	16.08	16.08	0.10	0.03	0.05	0.37	0.00	0.00	20.9
16	51	-0	-5891	0	0	0	1516	--	--	16.08	16.08	0.10	0.03	0.05	0.37	0.00	0.00	20.9
17	51	-0	-5831	0	0	0	1443	--	--	16.08	16.08	0.10	0.03	0.05	0.37	0.00	0.00	20.9
18	51	-0	-9461	0	0	0	3961	--	--	16.08	16.08	0.00	0.07	0.08	0.59	0.00	0.00	20.9
19	51	-0	-8212	0	0	0	1691	--	--	16.08	16.08	0.00	0.03	0.07	0.52	0.00	0.00	20.9
20	51	-0	-8677	0	0	0	2720	--	--	16.08	16.08	0.00	0.05	0.07	0.54	0.00	0.00	20.9
37	51	-0	-9433	0	0	0	4427	--	--	16.08	16.08	0.00	0.08	0.08	0.59	0.00	0.00	20.9
38	51	-0	-7352	0	0	0	644	--	--	16.08	16.08	0.00	0.01	0.06	0.46	0.00	0.00	20.9
39	51	-0	-8127	0	0	0	2359	--	--	16.08	16.08	0.00	0.04	0.07	0.51	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 75 NI 1823 NF 1822 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-5735	0	0	0	2037	--	--	16.08	16.08	0.00	0.03	0.05	0.36	0.00	0.00	20.9
2	0	-0	-4574	0	0	0	1869	--	--	16.08	16.08	0.10	0.03	0.04	0.29	0.00	0.00	20.9
3	0	-0	-4558	0	0	0	1847	--	--	16.08	16.08	0.10	0.03	0.04	0.29	0.00	0.00	20.9
4	0	-0	-4265	0	0	0	1286	--	--	16.08	16.08	0.10	0.02	0.04	0.27	0.00	0.00	20.9
5	0	-0	-4249	0	0	0	1265	--	--	16.08	16.08	0.10	0.02	0.04	0.27	0.00	0.00	20.9
6	0	-0	-4484	0	0	0	1690	--	--	16.08	16.08	0.10	0.03	0.04	0.28	0.00	0.00	20.9
7	0	-0	-4432	0	0	0	1618	--	--	16.08	16.08	0.10	0.03	0.04	0.28	0.00	0.00	20.9
8	0	-0	-4391	0	0	0	1516	--	--	16.08	16.08	0.10	0.03	0.04	0.28	0.00	0.00	20.9
9	0	-0	-4340	0	0	0	1443	--	--	16.08	16.08	0.10	0.03	0.04	0.27	0.00	0.00	20.9
10	0	-0	-4574	0	0	0	1869	--	--	16.08	16.08	0.10	0.03	0.04	0.29	0.00	0.00	20.9
11	0	-0	-4558	0	0	0	1847	--	--	16.08	16.08	0.10	0.03	0.04	0.29	0.00	0.00	20.9
12	0	-0	-4265	0	0	0	1286	--	--	16.08	16.08	0.10	0.02	0.04	0.27	0.00	0.00	20.9
13	0	-0	-4249	0	0	0	1265	--	--	16.08	16.08	0.10	0.02	0.04	0.27	0.00	0.00	20.9
14	0	-0	-4484	0	0	0	1690	--	--	16.08	16.08	0.10	0.03	0.04	0.28	0.00	0.00	20.9
15	0	-0	-4432	0	0	0	1618	--	--	16.08	16.08	0.10	0.03	0.04	0.28	0.00	0.00	20.9
16	0	-0	-4391	0	0	0	1516	--	--	16.08	16.08	0.10	0.03	0.04	0.28	0.00	0.00	20.9
17	0	-0	-4340	0	0	0	1443	--	--	16.08	16.08	0.10	0.03	0.04	0.27	0.00	0.00	20.9
18	0	-0	-7266	0	0	0	3961	--	--	16.08	16.08	0.00	0.07	0.06	0.46	0.00	0.00	20.9
19	0	-0	-6027	0	0	0	1691	--	--	16.08	16.08	0.00	0.03	0.05	0.38	0.00	0.00	20.9
20	0	-0	-6522	0	0	0	2720	--	--	16.08	16.08	0.00	0.05	0.05	0.41	0.00	0.00	20.9
37	0	-0	-7332	0	0	0	4427	--	--	16.08	16.08	0.00	0.08	0.06	0.46	0.00	0.00	20.9
38	0	-0	-5267	0	0	0	644	--	--	16.08	16.08	0.00	0.01	0.04	0.33	0.00	0.00	20.9
39	0	-0	-6091	0	0	0	2359	--	--	16.08	16.08	0.00	0.04	0.05	0.38	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	-5735	0	0	0	2037	--	--	16.08	16.08	0.00	0.03	0.05	0.36	0.00	0.00	20.9
2	26	-0	-4574	0	0	0	1869	--	--	16.08	16.08	0.10	0.03	0.04	0.29	0.00	0.00	20.9
3	26	-0	-4558	0	0	0	1847	--	--	16.08	16.08	0.10	0.03	0.04	0.29	0.00	0.00	20.9
4	26	-0	-4265	0	0	0	1286	--	--	16.08	16.08	0.10	0.02	0.04	0.27	0.00	0.00	20.9
5	26	-0	-4249	0	0	0	1265	--	--	16.08	16.08	0.10	0.02	0.04	0.27	0.00	0.00	20.9
6	26	-0	-4484	0	0	0	1690	--	--	16.08	16.08	0.10	0.03	0.04	0.28	0.00	0.00	20.9
7	26	-0	-4432	0	0	0	1618	--	--	16.08	16.08	0.10	0.03	0.04	0.28	0.00	0.00	20.9
8	26	-0	-4391	0	0	0	1516	--	--	16.08	16.08	0.10	0.03	0.04	0.28	0.00	0.00	20.9
9	26	-0	-4340	0	0	0	1443	--	--	16.08	16.08	0.10	0.03	0.04	0.27	0.00	0.00	20.9
10	26	-0	-4574	0	0	0	1869	--	--	16.08	16.08	0.10	0.03	0.04	0.29	0.00	0.00	20.9
11	26	-0	-4558	0	0	0	1847	--	--	16.08	16.08	0.10	0.03	0.04	0.29	0.00	0.00	20.9
12	26	-0	-4265	0	0	0	1286	--	--	16.08	16.08	0.10	0.02	0.04	0.27	0.00	0.00	20.9
13	26	-0	-4249	0	0	0	1265	--	--	16.08	16.08	0.10	0.02	0.04	0.27	0.00	0.00	20.9
14	26	-0	-4484	0	0	0	1690	--	--	16.08	16.08	0.10	0.03	0.04	0.28	0.00	0.00	20.9
15	26	-0	-4432	0	0	0	1618	--	--	16.08	16.08	0.10	0.03	0.04	0.28	0.00	0.00	20.9
16	26	-0	-4391	0	0	0	1516	--	--	16.08	16.08	0.10	0.03	0.04	0.28	0.00	0.00	20.9
17	26	-0	-4340	0	0	0	1443	--	--	16.08	16.08	0.10	0.03	0.04	0.27	0.00	0.00	20.9
18	26	-0	-7266	0	0	0	3961	--	--	16.08	16.08	0.00	0.07	0.06	0.46	0.00	0.00	20.9
19	26	-0	-6027	0	0	0	1691	--	--	16.08	16.08	0.00	0.03	0.05	0.38	0.00	0.00	20.9
20	26	-0	-6522	0	0	0	2720	--	--	16.08	16.08	0.00	0.05	0.05	0.41	0.00	0.00	20.9
37	26	-0	-7332	0	0	0	4427	--	--	16.08	16.08	0.00	0.08	0.06	0.46	0.00	0.00	20.9
38	26	-0	-5267	0	0	0	-2061	--	--	16.08	16.08	0.18	0.03	0.04	0.33	0.00	0.00	20.9
39	26	-0	-6091	0	0	0	2359	--	--	16.08	16.08	0.00	0.04	0.05	0.38	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	-5735	0	0	0	-909	--	--	16.08	16.08	0.18	0.02	0.05	0.36	0.00	0.00	20.9
2	51	-0	-4574	0	0	0	-480	--	--	16.08	16.08	0.29	0.01	0.04	0.29	0.00	0.00	20.9

3	51	-0	-4558	0	0	0	-494	--	--	16.08	16.08	0.29	0.01	0.04	0.29	0.00	0.00	20.9
4	51	-0	-4265	0	0	0	-904	--	--	16.08	16.08	0.29	0.02	0.04	0.27	0.00	0.00	20.9
5	51	-0	-4249	0	0	0	-918	--	--	16.08	16.08	0.29	0.02	0.04	0.27	0.00	0.00	20.9
6	51	-0	-4484	0	0	0	-612	--	--	16.08	16.08	0.29	0.01	0.04	0.28	0.00	0.00	20.9
7	51	-0	-4432	0	0	0	-658	--	--	16.08	16.08	0.29	0.01	0.04	0.28	0.00	0.00	20.9
8	51	-0	-4391	0	0	0	-740	--	--	16.08	16.08	0.29	0.01	0.04	0.28	0.00	0.00	20.9
9	51	-0	-4340	0	0	0	-785	--	--	16.08	16.08	0.29	0.01	0.04	0.27	0.00	0.00	20.9
10	51	-0	-4574	0	0	0	-480	--	--	16.08	16.08	0.29	0.01	0.04	0.29	0.00	0.00	20.9
11	51	-0	-4558	0	0	0	-494	--	--	16.08	16.08	0.29	0.01	0.04	0.29	0.00	0.00	20.9
12	51	-0	-4265	0	0	0	-904	--	--	16.08	16.08	0.29	0.02	0.04	0.27	0.00	0.00	20.9
13	51	-0	-4249	0	0	0	-918	--	--	16.08	16.08	0.29	0.02	0.04	0.27	0.00	0.00	20.9
14	51	-0	-4484	0	0	0	-612	--	--	16.08	16.08	0.29	0.01	0.04	0.28	0.00	0.00	20.9
15	51	-0	-4432	0	0	0	-658	--	--	16.08	16.08	0.29	0.01	0.04	0.28	0.00	0.00	20.9
16	51	-0	-4391	0	0	0	-740	--	--	16.08	16.08	0.29	0.01	0.04	0.28	0.00	0.00	20.9
17	51	-0	-4340	0	0	0	-785	--	--	16.08	16.08	0.29	0.01	0.04	0.27	0.00	0.00	20.9
18	51	-0	-7266	0	0	0	229	--	--	16.08	16.08	0.00	0.00	0.06	0.46	0.00	0.00	20.9
19	51	-0	-6027	0	0	0	-1405	--	--	16.08	16.08	0.18	0.02	0.05	0.38	0.00	0.00	20.9
20	51	-0	-6522	0	0	0	-630	--	--	16.08	16.08	0.18	0.01	0.05	0.41	0.00	0.00	20.9
37	51	-0	-7332	0	0	0	661	--	--	16.08	16.08	0.00	0.01	0.06	0.46	0.00	0.00	20.9
38	51	-0	-5267	0	0	0	-2061	--	--	16.08	16.08	0.18	0.03	0.04	0.33	0.00	0.00	20.9
39	51	-0	-6091	0	0	0	-769	--	--	16.08	16.08	0.18	0.01	0.05	0.38	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 76 NI 1822 NF 1821 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-3859	0	0	0	-2891	--	--	16.08	16.08	0.18	0.05	0.03	0.24	0.00	0.00	20.9
2	0	-0	-3138	0	0	0	-2092	--	--	16.08	16.08	0.29	0.04	0.03	0.20	0.00	0.00	20.9
3	0	-0	-3125	0	0	0	-2099	--	--	16.08	16.08	0.29	0.04	0.03	0.20	0.00	0.00	20.9
4	0	-0	-2812	0	0	0	-2348	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
5	0	-0	-2799	0	0	0	-2355	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
6	0	-0	-3039	0	0	0	-2173	--	--	16.08	16.08	0.29	0.04	0.03	0.19	0.00	0.00	20.9
7	0	-0	-2996	0	0	0	-2197	--	--	16.08	16.08	0.29	0.04	0.02	0.19	0.00	0.00	20.9
8	0	-0	-2941	0	0	0	-2250	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
9	0	-0	-2898	0	0	0	-2274	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
10	0	-0	-3138	0	0	0	-2092	--	--	16.08	16.08	0.29	0.04	0.03	0.20	0.00	0.00	20.9
11	0	-0	-3125	0	0	0	-2099	--	--	16.08	16.08	0.29	0.04	0.03	0.20	0.00	0.00	20.9
12	0	-0	-2812	0	0	0	-2348	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
13	0	-0	-2799	0	0	0	-2355	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
14	0	-0	-3039	0	0	0	-2173	--	--	16.08	16.08	0.29	0.04	0.03	0.19	0.00	0.00	20.9
15	0	-0	-2996	0	0	0	-2197	--	--	16.08	16.08	0.29	0.04	0.02	0.19	0.00	0.00	20.9
16	0	-0	-2941	0	0	0	-2250	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
17	0	-0	-2898	0	0	0	-2274	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
18	0	-0	-5156	0	0	0	229	--	--	16.08	16.08	0.00	0.00	0.04	0.32	0.00	0.00	20.9
19	0	-0	-3913	0	0	0	-3415	--	--	16.08	16.08	0.18	0.06	0.03	0.25	0.00	0.00	20.9
20	0	-0	-4441	0	0	0	-2911	--	--	16.08	16.08	0.18	0.05	0.04	0.28	0.00	0.00	20.9
37	0	-0	-5315	0	0	0	661	--	--	16.08	16.08	0.00	0.01	0.04	0.33	0.00	0.00	20.9
38	0	-0	-3243	0	0	0	-3727	--	--	16.08	16.08	0.18	0.06	0.03	0.20	0.00	0.00	20.9
39	0	-0	-4124	0	0	0	-2887	--	--	16.08	16.08	0.18	0.05	0.03	0.26	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	-3859	0	0	0	-2891	--	--	16.08	16.08	0.18	0.05	0.03	0.24	0.00	0.00	20.9
2	26	-0	-3138	0	0	0	-2092	--	--	16.08	16.08	0.29	0.04	0.03	0.20	0.00	0.00	20.9
3	26	-0	-3125	0	0	0	-2099	--	--	16.08	16.08	0.29	0.04	0.03	0.20	0.00	0.00	20.9
4	26	-0	-2812	0	0	0	-2348	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
5	26	-0	-2799	0	0	0	-2355	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
6	26	-0	-3039	0	0	0	-2173	--	--	16.08	16.08	0.29	0.04	0.03	0.19	0.00	0.00	20.9
7	26	-0	-2996	0	0	0	-2197	--	--	16.08	16.08	0.29	0.04	0.02	0.19	0.00	0.00	20.9
8	26	-0	-2941	0	0	0	-2250	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
9	26	-0	-2898	0	0	0	-2274	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
10	26	-0	-3138	0	0	0	-2092	--	--	16.08	16.08	0.29	0.04	0.03	0.20	0.00	0.00	20.9
11	26	-0	-3125	0	0	0	-2099	--	--	16.08	16.08	0.29	0.04	0.03	0.20	0.00	0.00	20.9
12	26	-0	-2812	0	0	0	-2348	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
13	26	-0	-2799	0	0	0	-2355	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
14	26	-0	-3039	0	0	0	-2173	--	--	16.08	16.08	0.29	0.04	0.03	0.19	0.00	0.00	20.9
15	26	-0	-2996	0	0	0	-2197	--	--	16.08	16.08	0.29	0.04	0.02	0.19	0.00	0.00	20.9
16	26	-0	-2941	0	0	0	-2250	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
17	26	-0	-2898	0	0	0	-2274	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
18	26	-0	-5156	0	0	0	-2419	--	--	16.08	16.08	0.18	0.04	0.04	0.32	0.00	0.00	20.9
19	26	-0	-3913	0	0	0	-3415	--	--	16.08	16.08	0.18	0.06	0.03	0.25	0.00	0.00	20.9
20	26	-0	-4441	0	0	0	-2911	--	--	16.08	16.08	0.18	0.05	0.04	0.28	0.00	0.00	20.9
37	26	-0	-5315	0	0	0	-2069	--	--	16.08	16.08	0.18	0.03	0.04	0.33	0.00	0.00	20.9
38	26	-0	-3243	0	0	0	-3727	--	--	16.08	16.08	0.18	0.06	0.03	0.20	0.00	0.00	20.9
39	26	-0	-4124	0	0	0	-2887	--	--	16.08	16.08	0.18	0.05	0.03	0.26	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	-3859	0	0	0	-2891	--	--	16.08	16.08	0.18	0.05	0.03	0.24	0.00	0.00	20.9
2	51	-0	-3138	0	0	0	-2092	--	--	16.08	16.08	0.29	0.04	0.03	0.20	0.00	0.00	20.9
3	51	-0	-3125	0	0	0	-2099	--	--	16.08	16.08	0.29	0.04	0.03	0.20	0.00	0.00	20.9
4	51	-0	-2812	0	0	0	-2348	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
5	51	-0	-2799	0	0	0	-2355	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
6	51	-0	-3039	0	0	0	-2173	--	--	16.08	16.08	0.29	0.04	0.03	0.19	0.00	0.00	20.9
7	51	-0	-2996	0	0	0	-2197	--	--	16.08	16.08	0.29	0.04	0.02	0.19	0.00	0.00	20.9
8	51	-0	-2941	0	0	0	-2250	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
9	51	-0	-2898	0	0	0	-2274	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
10	51	-0	-3138	0	0	0	-2092	--	--	16.08	16.08	0.29	0.04	0.03	0.20	0.00	0.00	20.9
11	51	-0	-3125	0	0	0	-2099	--	--	16.08	16.08	0.29	0.04	0.03	0.20	0.00	0.00	20.9
12	51	-0	-2812	0	0	0	-2348	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
13	51	-0	-2799	0	0	0	-2355	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
14	51	-0	-3039	0	0	0	-2173	--	--	16.08	16.08	0.29	0.04	0.03	0.19	0.00	0.00	20.9
15	51	-0	-2996	0	0	0	-2197	--	--	16.08	16.08	0.29	0.04	0.02	0.19	0.00	0.00	20.9
16	51	-0	-2941	0	0	0	-2250	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
17	51	-0	-2898	0	0	0	-2274	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
18	51	-0	-5156	0	0	0	-2419	--	--	16.08	16.08	0.18	0.04	0.04	0.32	0.00	0.00	20.9
19	51	-0	-3913	0	0	0	-3415	--	--	16.08	16.08	0.18	0.06	0.03	0.25	0.00	0.00	20.9
20	51	-0	-4441	0	0	0	-2911	--	--	16.08	16.08	0.18	0.05	0.04	0.28	0.00	0.00	20.9
37	51	-0	-5315	0	0	0	-2069	--	--	16.08	16.08	0.18	0.03	0.04	0.33	0.00	0.00	20.9
38	51	-0	-3243	0	0	0	-3727	--	--	16.08	16.08	0.18	0.06	0.03	0.20	0.00	0.00	20.9
39	51	-0	-4124	0	0	0	-2887	--	--	16.08	16.08	0.18	0.05	0.03	0.26	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 77 NI 1821 NF 1838 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-2040	0	0	0	-3939	--	--	16.08	16.08	0.18	0.07	0.02	0.13	0.00	0.00	20.9
2	0	-0	-1749	0	0	0	-2990	--	--	16.08	16.08	0.29	0.05	0.01	0.11	0.00	0.00	20.9
3	0	-0	-1738	0	0	0	-2992	--	--	16.08	16.08	0.29	0.05	0.01	0.11	0.00	0.00	20.9
4	0	-0	-1401	0	0	0	-3068	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
5	0	-0	-1391	0	0	0	-3069	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
6	0	-0	-1639	0	0	0	-3016	--	--	16.08	16.08	0.29	0.05	0.01	0.10	0.00	0.00	20.9
7	0	-0	-1604	0	0	0	-3021	--	--	16.08	16.08	0.29	0.05	0.01	0.10	0.00	0.00	20.9
8	0	-0	-1535	0	0	0	-3039	--	--	16.08	16.08	0.29	0.05	0.01	0.10	0.00	0.00	20.9
9	0	-0	-1500	0	0	0	-3044	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
10	0	-0	-1749	0	0	0	-2990	--	--	16.08	16.08	0.29	0.05	0.01	0.11	0.00	0.00	20.9
11	0	-0	-1738	0	0	0	-2992	--	--	16.08	16.08	0.29	0.05	0.01	0.11	0.00	0.00	20.9
12	0	-0	-1401	0	0	0	-3068	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
13	0	-0	-1391	0	0	0	-3069	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
14	0	-0	-1639	0	0	0	-3016	--	--	16.08	16.08	0.29	0.05	0.01	0.10	0.00	0.00	20.9
15	0	-0	-1604	0	0	0	-3021	--	--	16.08	16.08	0.29	0.05	0.01	0.10	0.00	0.00	20.9
16	0	-0	-1535	0	0	0	-3039	--	--	16.08	16.08	0.29	0.05	0.01	0.10	0.00	0.00	20.9
17	0	-0	-1500	0	0	0	-3044	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
18	0	-0	-3125	0	0	0	-4025	--	--	16.08	16.08	0.18	0.07	0.03	0.20	0.00	0.00	20.9
19	0	-0	-1857	0	0	0	-4369	--	--	16.08	16.08	0.18	0.07	0.02	0.12	0.00	0.00	20.9
20	0	-0	-2428	0	0	0	-4158	--	--	16.08	16.08	0.18	0.07	0.02	0.15	0.00	0.00	20.9
37	0	-0	-3382	0	0	0	-3806	--	--	16.08	16.08	0.18	0.06	0.03	0.21	0.00	0.00	20.9
38	0	-0	-1268	0	0	0	-4379	--	--	16.08	16.08	0.18	0.07	0.01	0.08	0.00	0.00	20.9
39	0	-0	-2219	0	0	0	-4027	--	--	16.08	16.08	0.18	0.07	0.02	0.14	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	26	-0	-2040	0	0	0	-3939	--	--	16.08	16.08	0.18	0.07	0.02	0.13	0.00	0.00	20.9
2	26	-0	-1749	0	0	0	-2990	--	--	16.08	16.08	0.29	0.05	0.01	0.11	0.00	0.00	20.9
3	26	-0	-1738	0	0	0	-2992	--	--	16.08	16.08	0.29	0.05	0.01	0.11	0.00	0.00	20.9
4	26	-0	-1401	0	0	0	-3068	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
5	26	-0	-1391	0	0	0	-3069	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
6	26	-0	-1639	0	0	0	-3016	--	--	16.08	16.08	0.29	0.05	0.01	0.10	0.00	0.00	20.9
7	26	-0	-1604	0	0	0	-3021	--	--	16.08	16.08	0.29	0.05	0.01	0.10	0.00	0.00	20.9
8	26	-0	-1535	0	0	0	-3039	--	--	16.08	16.08	0.29	0.05	0.01	0.10	0.00	0.00	20.9
9	26	-0	-1500	0	0	0	-3044	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
10	26	-0	-1749	0	0	0	-2990	--	--	16.08	16.08	0.29	0.05	0.01	0.11	0.00	0.00	20.9
11	26	-0	-1738	0	0	0	-2992	--	--	16.08	16.08	0.29	0.05	0.01	0.11	0.00	0.00	20.9
12	26	-0	-1401	0	0	0	-3068	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
13	26	-0	-1391	0	0	0	-3069	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
14	26	-0	-1639	0	0	0	-3016	--	--	16.08	16.08	0.29	0.05	0.01	0.10	0.00	0.00	20.9
15	26	-0	-1604	0	0	0	-3021	--	--	16.08	16.08	0.29	0.05	0.01	0.10	0.00	0.00	20.9
16	26	-0	-1535	0	0	0	-3039	--	--	16.08	16.08	0.29	0.05	0.01	0.10	0.00	0.00	20.9
17	26	-0	-1500	0	0	0	-3044	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
18	26	-0	-3125	0	0	0	-4025	--	--	16.08	16.08	0.18	0.07	0.03	0.20	0.00	0.00	20.9
19	26	-0	-1857	0	0	0	-4369	--	--	16.08	16.08	0.18	0.07	0.02	0.12	0.00	0.00	20.9
20	26	-0	-2428	0	0	0	-4158	--	--	16.08	16.08	0.18	0.07	0.02	0.15	0.00	0.00	20.9
37	26	-0	-3382	0	0	0	-3806	--	--	16.08	16.08	0.18	0.06	0.03	0.21	0.00	0.00	20.9
38	26	-0	-1268	0	0	0	-4379	--	--	16.08	16.08	0.18	0.07	0.01	0.08	0.00	0.00	20.9
39	26	-0	-2219	0	0	0	-4027	--	--	16.08	16.08	0.18	0.07	0.02	0.14	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	51	-0	-2040	0	0	0	-3939	--	--	16.08	16.08	0.18	0.07	0.02	0.13	0.00	0.00	20.9
2	51	-0	-1749	0	0	0	-2990	--	--	16.08	16.08	0.29	0.05	0.01	0.11	0.00	0.00	20.9
3	51	-0	-1738	0	0	0	-2992	--	--	16.08	16.08	0.29	0.05	0.01	0.11	0.00	0.00	20.9
4	51	-0	-1401	0	0	0	-3068	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
5	51	-0	-1391	0	0	0	-3069	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
6	51	-0	-1639	0	0	0	-3016	--	--	16.08	16.08	0.29	0.05	0.01	0.10	0.00	0.00	20.9
7	51	-0	-1604	0	0	0	-3021	--	--	16.08	16.08	0.29	0.05	0.01	0.10	0.00	0.00	20.9
8	51	-0	-1535	0	0	0	-3039	--	--	16.08	16.08	0.29	0.05	0.01	0.10	0.00	0.00	20.9
9	51	-0	-1500	0	0	0	-3044	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
10	51	-0	-1749	0	0	0	-2990	--	--	16.08	16.08	0.29	0.05	0.01	0.11	0.00	0.00	20.9
11	51	-0	-1738	0	0	0	-2992	--	--	16.08	16.08	0.29	0.05	0.01	0.11	0.00	0.00	20.9
12	51	-0	-1401	0	0	0	-3068	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
13	51	-0	-1391	0	0	0	-3069	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
14	51	-0	-1639	0	0	0	-3016	--	--	16.08	16.08	0.29	0.05	0.01	0.10	0.00	0.00	20.9
15	51	-0	-1604	0	0	0	-3021	--	--	16.08	16.08	0.29	0.05	0.01	0.10	0.00	0.00	20.9
16	51	-0	-1535	0	0	0	-3039	--	--	16.08	16.08	0.29	0.05	0.01	0.10	0.00	0.00	20.9
17	51	-0	-1500	0	0	0	-3044	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
18	51	-0	-3125	0	0	0	-4025	--	--	16.08	16.08	0.18	0.07	0.03	0.20	0.00	0.00	20.9
19	51	-0	-1857	0	0	0	-4369	--	--	16.08	16.08	0.18	0.07	0.02	0.12	0.00	0.00	20.9
20	51	-0	-2428	0	0	0	-4158	--	--	16.08	16.08	0.18	0.07	0.02	0.15	0.00	0.00	20.9
37	51	-0	-3382	0	0	0	-3806	--	--	16.08	16.08	0.18	0.06	0.03	0.21	0.00	0.00	20.9
38	51	-0	-1268	0	0	0	-4379	--	--	16.08	16.08	0.18	0.07	0.01	0.08	0.00	0.00	20.9
39	51	-0	-2219	0	0	0	-4027	--	--	16.08	16.08	0.18	0.07	0.02	0.14	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 78 NI 1838 NF 1837 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-262	0	0	0	-4073	--	--	16.08	16.08	0.18	0.07	0.00	0.02	0.00	0.00	20.9
2	0	-0	-392	0	0	0	-3192	--	--	16.08	16.08	0.29	0.06	0.00	0.02	0.00	0.00	20.9
3	0	-0	-384	0	0	0	-3189	--	--	16.08	16.08	0.29	0.06	0.00	0.02	0.00	0.00	20.9
4	0	-0	-19	0	0	0	-3078	--	--	16.08	16.08	0.29	0.05	0.00	0.00	0.00	0.00	20.9
5	0	-0	-10	0	0	0	-3075	--	--	16.08	16.08	0.29	0.05	0.00	0.00	0.00	0.00	20.9
6	0	-0	-271	0	0	0	-3155	--	--	16.08	16.08	0.29	0.05	0.00	0.02	0.00	0.00	20.9
7	0	-0	-243	0	0	0	-3146	--	--	16.08	16.08	0.29	0.05	0.00	0.02	0.00	0.00	20.9
8	0	-0	-160	0	0	0	-3121	--	--	16.08	16.08	0.29	0.05	0.00	0.01	0.00	0.00	20.9
9	0	-0	-131	0	0	0	-3111	--	--	16.08	16.08	0.29	0.05	0.00	0.01	0.00	0.00	20.9
10	0	-0	-392	0	0	0	-3192	--	--	16.08	16.08	0.29	0.06	0.00	0.02	0.00	0.00	20.9

11	0	-0	-384	0	0	0	-3189	--	--	16.08	16.08	0.29	0.06	0.00	0.02	0.00	0.00	20.9
12	0	-0	-19	0	0	0	-3078	--	--	16.08	16.08	0.29	0.05	0.00	0.00	0.00	0.00	20.9
13	0	-0	-10	0	0	0	-3075	--	--	16.08	16.08	0.29	0.05	0.00	0.00	0.00	0.00	20.9
14	0	-0	-271	0	0	0	-3155	--	--	16.08	16.08	0.29	0.05	0.00	0.02	0.00	0.00	20.9
15	0	-0	-243	0	0	0	-3146	--	--	16.08	16.08	0.29	0.05	0.00	0.02	0.00	0.00	20.9
16	0	-0	-160	0	0	0	-3121	--	--	16.08	16.08	0.29	0.05	0.00	0.01	0.00	0.00	20.9
17	0	-0	-131	0	0	0	-3111	--	--	16.08	16.08	0.29	0.05	0.00	0.01	0.00	0.00	20.9
18	0	-0	-1159	0	0	0	-4620	--	--	16.08	16.08	0.18	0.08	0.01	0.07	0.00	0.00	20.9
19	0	-0	159	0	0	0	-4369	--	--	16.08	16.08	0.18	0.07	0.00	0.01	0.00	0.00	20.9
20	0	-0	-464	0	0	0	-4397	--	--	16.08	16.08	0.18	0.07	0.00	0.03	0.00	0.00	20.9
37	0	-0	-1516	0	0	0	-4584	--	--	16.08	16.08	0.18	0.08	0.01	0.10	0.00	0.00	20.9
38	0	-0	681	0	0	0	-4379	--	--	16.08	16.08	0.18	0.07	0.01	0.04	0.00	0.00	20.9
39	0	-0	-358	0	0	0	-4211	--	--	16.08	16.08	0.18	0.07	0.00	0.02	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	-262	0	0	0	-4073	--	--	16.08	16.08	0.18	0.07	0.00	0.02	0.00	0.00	20.9
2	26	-0	-392	0	0	0	-3192	--	--	16.08	16.08	0.29	0.06	0.00	0.02	0.00	0.00	20.9
3	26	-0	-384	0	0	0	-3189	--	--	16.08	16.08	0.29	0.06	0.00	0.02	0.00	0.00	20.9
4	26	-0	-19	0	0	0	-3078	--	--	16.08	16.08	0.29	0.05	0.00	0.00	0.00	0.00	20.9
5	26	-0	-10	0	0	0	-3075	--	--	16.08	16.08	0.29	0.05	0.00	0.00	0.00	0.00	20.9
6	26	-0	-271	0	0	0	-3155	--	--	16.08	16.08	0.29	0.05	0.00	0.02	0.00	0.00	20.9
7	26	-0	-243	0	0	0	-3146	--	--	16.08	16.08	0.29	0.05	0.00	0.02	0.00	0.00	20.9
8	26	-0	-160	0	0	0	-3121	--	--	16.08	16.08	0.29	0.05	0.00	0.01	0.00	0.00	20.9
9	26	-0	-131	0	0	0	-3111	--	--	16.08	16.08	0.29	0.05	0.00	0.01	0.00	0.00	20.9
10	26	-0	-392	0	0	0	-3192	--	--	16.08	16.08	0.29	0.06	0.00	0.02	0.00	0.00	20.9
11	26	-0	-384	0	0	0	-3189	--	--	16.08	16.08	0.29	0.06	0.00	0.02	0.00	0.00	20.9
12	26	-0	-19	0	0	0	-3078	--	--	16.08	16.08	0.29	0.05	0.00	0.00	0.00	0.00	20.9
13	26	-0	-10	0	0	0	-3075	--	--	16.08	16.08	0.29	0.05	0.00	0.00	0.00	0.00	20.9
14	26	-0	-271	0	0	0	-3155	--	--	16.08	16.08	0.29	0.05	0.00	0.02	0.00	0.00	20.9
15	26	-0	-243	0	0	0	-3146	--	--	16.08	16.08	0.29	0.05	0.00	0.02	0.00	0.00	20.9
16	26	-0	-160	0	0	0	-3121	--	--	16.08	16.08	0.29	0.05	0.00	0.01	0.00	0.00	20.9
17	26	-0	-131	0	0	0	-3111	--	--	16.08	16.08	0.29	0.05	0.00	0.01	0.00	0.00	20.9
18	26	-0	-1159	0	0	0	-4620	--	--	16.08	16.08	0.18	0.08	0.01	0.07	0.00	0.00	20.9
19	26	-0	159	0	0	0	-4369	--	--	16.08	16.08	0.18	0.07	0.00	0.01	0.00	0.00	20.9
20	26	-0	-464	0	0	0	-4397	--	--	16.08	16.08	0.18	0.07	0.00	0.03	0.00	0.00	20.9
37	26	-0	-1516	0	0	0	-4584	--	--	16.08	16.08	0.18	0.08	0.01	0.10	0.00	0.00	20.9
38	26	-0	681	0	0	0	-4379	--	--	16.08	16.08	0.18	0.07	0.01	0.04	0.00	0.00	20.9
39	26	-0	-358	0	0	0	-4211	--	--	16.08	16.08	0.18	0.07	0.00	0.02	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	-262	0	0	0	-4073	--	--	16.08	16.08	0.18	0.07	0.00	0.02	0.00	0.00	20.9
2	51	-0	-392	0	0	0	-3192	--	--	16.08	16.08	0.29	0.06	0.00	0.02	0.00	0.00	20.9
3	51	-0	-384	0	0	0	-3189	--	--	16.08	16.08	0.29	0.06	0.00	0.02	0.00	0.00	20.9
4	51	-0	-19	0	0	0	-3078	--	--	16.08	16.08	0.29	0.05	0.00	0.00	0.00	0.00	20.9
5	51	-0	-10	0	0	0	-3075	--	--	16.08	16.08	0.29	0.05	0.00	0.00	0.00	0.00	20.9
6	51	-0	-271	0	0	0	-3155	--	--	16.08	16.08	0.29	0.05	0.00	0.02	0.00	0.00	20.9
7	51	-0	-243	0	0	0	-3146	--	--	16.08	16.08	0.29	0.05	0.00	0.02	0.00	0.00	20.9
8	51	-0	-160	0	0	0	-3121	--	--	16.08	16.08	0.29	0.05	0.00	0.01	0.00	0.00	20.9
9	51	-0	-131	0	0	0	-3111	--	--	16.08	16.08	0.29	0.05	0.00	0.01	0.00	0.00	20.9
10	51	-0	-392	0	0	0	-3192	--	--	16.08	16.08	0.29	0.06	0.00	0.02	0.00	0.00	20.9
11	51	-0	-384	0	0	0	-3189	--	--	16.08	16.08	0.29	0.06	0.00	0.02	0.00	0.00	20.9
12	51	-0	-19	0	0	0	-3078	--	--	16.08	16.08	0.29	0.05	0.00	0.00	0.00	0.00	20.9
13	51	-0	-10	0	0	0	-3075	--	--	16.08	16.08	0.29	0.05	0.00	0.00	0.00	0.00	20.9
14	51	-0	-271	0	0	0	-3155	--	--	16.08	16.08	0.29	0.05	0.00	0.02	0.00	0.00	20.9
15	51	-0	-243	0	0	0	-3146	--	--	16.08	16.08	0.29	0.05	0.00	0.02	0.00	0.00	20.9
16	51	-0	-160	0	0	0	-3121	--	--	16.08	16.08	0.29	0.05	0.00	0.01	0.00	0.00	20.9
17	51	-0	-131	0	0	0	-3111	--	--	16.08	16.08	0.29	0.05	0.00	0.01	0.00	0.00	20.9
18	51	-0	-1159	0	0	0	-4620	--	--	16.08	16.08	0.18	0.08	0.01	0.07	0.00	0.00	20.9
19	51	-0	159	0	0	0	-4369	--	--	16.08	16.08	0.18	0.07	0.00	0.01	0.00	0.00	20.9
20	51	-0	-464	0	0	0	-4397	--	--	16.08	16.08	0.18	0.07	0.00	0.03	0.00	0.00	20.9
37	51	-0	-1516	0	0	0	-4584	--	--	16.08	16.08	0.18	0.08	0.01	0.10	0.00	0.00	20.9
38	51	-0	681	0	0	0	-4379	--	--	16.08	16.08	0.18	0.07	0.01	0.04	0.00	0.00	20.9
39	51	-0	-358	0	0	0	-4211	--	--	16.08	16.08	0.18	0.07	0.00	0.02	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 79 NI 1837 NF 1650 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	1500	0	0	0	-4073	--	--	16.08	16.08	0.18	0.07	0.01	0.09	0.00	0.00	20.9
2	0	-0	948	0	0	0	-3192	--	--	16.08	16.08	0.29	0.06	0.01	0.06	0.00	0.00	20.9
3	0	-0	955	0	0	0	-3189	--	--	16.08	16.08	0.29	0.06	0.01	0.06	0.00	0.00	20.9
4	0	-0	1352	0	0	0	-3078	--	--	16.08	16.08	0.29	0.05	0.01	0.08	0.00	0.00	20.9
5	0	-0	1359	0	0	0	-3075	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
6	0	-0	1082	0	0	0	-3155	--	--	16.08	16.08	0.29	0.05	0.01	0.07	0.00	0.00	20.9
7	0	-0	1104	0	0	0	-3146	--	--	16.08	16.08	0.29	0.05	0.01	0.07	0.00	0.00	20.9
8	0	-0	1203	0	0	0	-3121	--	--	16.08	16.08	0.29	0.05	0.01	0.08	0.00	0.00	20.9
9	0	-0	1225	0	0	0	-3111	--	--	16.08	16.08	0.29	0.05	0.01	0.08	0.00	0.00	20.9
10	0	-0	948	0	0	0	-3192	--	--	16.08	16.08	0.29	0.06	0.01	0.06	0.00	0.00	20.9
11	0	-0	955	0	0	0	-3189	--	--	16.08	16.08	0.29	0.06	0.01	0.06	0.00	0.00	20.9
12	0	-0	1352	0	0	0	-3078	--	--	16.08	16.08	0.29	0.05	0.01	0.08	0.00	0.00	20.9
13	0	-0	1359	0	0	0	-3075	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
14	0	-0	1082	0	0	0	-3155	--	--	16.08	16.08	0.29	0.05	0.01	0.07	0.00	0.00	20.9
15	0	-0	1104	0	0	0	-3146	--	--	16.08	16.08	0.29	0.05	0.01	0.07	0.00	0.00	20.9
16	0	-0	1203	0	0	0	-3121	--	--	16.08	16.08	0.29	0.05	0.01	0.08	0.00	0.00	20.9
17	0	-0	1225	0	0	0	-3111	--	--	16.08	16.08	0.29	0.05	0.01	0.08	0.00	0.00	20.9
18	0	-0	766	0	0	0	-4620	--	--	16.08	16.08	0.18	0.08	0.01	0.05	0.00	0.00	20.9
19	0	-0	2162	0	0	0	-4287	--	--	16.08	16.08	0.18	0.07	0.02	0.14	0.00	0.00	20.9
20	0	-0	1473	0	0	0	-4397	--	--	16.08	16.08	0.18	0.07	0.01	0.09	0.00	0.00	20.9
37	0	-0	302	0	0	0	-4584	--	--	16.08	16.08	0.18	0.08	0.00	0.02	0.00	0.00	20.9
38	0	-0	2629	0	0	0	-4029	--	--	16.08	16.08	0.18	0.07	0.02	0.16	0.00	0.00	20.9
39	0	-0	1481	0	0	0	-4211	--	--	16.08	16.08	0.18	0.07	0.01	0.09	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	1500	0	0	0	-4073	--	--	16.08	16.08	0.18	0.07	0.01	0.09	0.00	0.00	20.9
2	26	-0	948	0	0	0	-3192	--	--	16.08	16.08	0.29	0.06	0.01	0.06	0.00	0.00	20.9
3	26	-0	955	0	0	0	-3189	--	--	16.08	16.08	0.29	0.06	0.01	0.06	0.00	0.00	20.9
4	26	-0	1352	0	0	0	-3078	--	--	16.08	16.08	0.29	0.05	0.01	0.08	0.00	0.00	20.9
5	26	-0	1359	0	0	0	-3075	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
6	26	-0	1082	0	0	0	-3155	--	--	16.08	16.08	0.29	0.05	0.01	0.07	0.00	0.00	20.9

7	26	-0	1104	0	0	0	-3146	--	--	16.08	16.08	0.29	0.05	0.01	0.07	0.00	0.00	20.9
8	26	-0	1203	0	0	0	-3121	--	--	16.08	16.08	0.29	0.05	0.01	0.08	0.00	0.00	20.9
9	26	-0	1225	0	0	0	-3111	--	--	16.08	16.08	0.29	0.05	0.01	0.08	0.00	0.00	20.9
10	26	-0	948	0	0	0	-3192	--	--	16.08	16.08	0.29	0.06	0.01	0.06	0.00	0.00	20.9
11	26	-0	955	0	0	0	-3189	--	--	16.08	16.08	0.29	0.06	0.01	0.06	0.00	0.00	20.9
12	26	-0	1352	0	0	0	-3078	--	--	16.08	16.08	0.29	0.05	0.01	0.08	0.00	0.00	20.9
13	26	-0	1359	0	0	0	-3075	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
14	26	-0	1082	0	0	0	-3155	--	--	16.08	16.08	0.29	0.05	0.01	0.07	0.00	0.00	20.9
15	26	-0	1104	0	0	0	-3146	--	--	16.08	16.08	0.29	0.05	0.01	0.07	0.00	0.00	20.9
16	26	-0	1203	0	0	0	-3121	--	--	16.08	16.08	0.29	0.05	0.01	0.08	0.00	0.00	20.9
17	26	-0	1225	0	0	0	-3111	--	--	16.08	16.08	0.29	0.05	0.01	0.08	0.00	0.00	20.9
18	26	-0	766	0	0	0	-4620	--	--	16.08	16.08	0.18	0.08	0.01	0.05	0.00	0.00	20.9
19	26	-0	2162	0	0	0	-4287	--	--	16.08	16.08	0.18	0.07	0.02	0.14	0.00	0.00	20.9
20	26	-0	1473	0	0	0	-4397	--	--	16.08	16.08	0.18	0.07	0.01	0.09	0.00	0.00	20.9
37	26	-0	302	0	0	0	-4584	--	--	16.08	16.08	0.18	0.08	0.00	0.02	0.00	0.00	20.9
38	26	-0	2629	0	0	0	-4029	--	--	16.08	16.08	0.18	0.07	0.02	0.16	0.00	0.00	20.9
39	26	-0	1481	0	0	0	-4211	--	--	16.08	16.08	0.18	0.07	0.01	0.09	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	1500	0	0	0	-4073	--	--	16.08	16.08	0.18	0.07	0.01	0.09	0.00	0.00	20.9
2	51	-0	948	0	0	0	-3192	--	--	16.08	16.08	0.29	0.06	0.01	0.06	0.00	0.00	20.9
3	51	-0	955	0	0	0	-3189	--	--	16.08	16.08	0.29	0.06	0.01	0.06	0.00	0.00	20.9
4	51	-0	1352	0	0	0	-3078	--	--	16.08	16.08	0.29	0.05	0.01	0.08	0.00	0.00	20.9
5	51	-0	1359	0	0	0	-3075	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
6	51	-0	1082	0	0	0	-3155	--	--	16.08	16.08	0.29	0.05	0.01	0.07	0.00	0.00	20.9
7	51	-0	1104	0	0	0	-3146	--	--	16.08	16.08	0.29	0.05	0.01	0.07	0.00	0.00	20.9
8	51	-0	1203	0	0	0	-3121	--	--	16.08	16.08	0.29	0.05	0.01	0.08	0.00	0.00	20.9
9	51	-0	1225	0	0	0	-3111	--	--	16.08	16.08	0.29	0.05	0.01	0.08	0.00	0.00	20.9
10	51	-0	948	0	0	0	-3192	--	--	16.08	16.08	0.29	0.06	0.01	0.06	0.00	0.00	20.9
11	51	-0	955	0	0	0	-3189	--	--	16.08	16.08	0.29	0.06	0.01	0.06	0.00	0.00	20.9
12	51	-0	1352	0	0	0	-3078	--	--	16.08	16.08	0.29	0.05	0.01	0.08	0.00	0.00	20.9
13	51	-0	1359	0	0	0	-3075	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
14	51	-0	1082	0	0	0	-3155	--	--	16.08	16.08	0.29	0.05	0.01	0.07	0.00	0.00	20.9
15	51	-0	1104	0	0	0	-3146	--	--	16.08	16.08	0.29	0.05	0.01	0.07	0.00	0.00	20.9
16	51	-0	1203	0	0	0	-3121	--	--	16.08	16.08	0.29	0.05	0.01	0.08	0.00	0.00	20.9
17	51	-0	1225	0	0	0	-3111	--	--	16.08	16.08	0.29	0.05	0.01	0.08	0.00	0.00	20.9
18	51	-0	766	0	0	0	-4620	--	--	16.08	16.08	0.18	0.08	0.01	0.05	0.00	0.00	20.9
19	51	-0	2162	0	0	0	-4287	--	--	16.08	16.08	0.18	0.07	0.02	0.14	0.00	0.00	20.9
20	51	-0	1473	0	0	0	-4397	--	--	16.08	16.08	0.18	0.07	0.01	0.09	0.00	0.00	20.9
37	51	-0	302	0	0	0	-4584	--	--	16.08	16.08	0.18	0.08	0.00	0.02	0.00	0.00	20.9
38	51	-0	2629	0	0	0	-4029	--	--	16.08	16.08	0.18	0.07	0.02	0.16	0.00	0.00	20.9
39	51	-0	1481	0	0	0	-4211	--	--	16.08	16.08	0.18	0.07	0.01	0.09	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 80 NI 1650 NF 1825 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm

1	0	-0	3266	0	0	0	-3303	--	--	16.08	16.08	0.18	0.05	0.03	0.20	0.00	0.00	20.9
2	0	-0	2290	0	0	0	-2705	--	--	16.08	16.08	0.29	0.05	0.02	0.14	0.00	0.00	20.9
3	0	-0	2295	0	0	0	-2698	--	--	16.08	16.08	0.29	0.05	0.02	0.14	0.00	0.00	20.9
4	0	-0	2730	0	0	0	-2383	--	--	16.08	16.08	0.29	0.04	0.02	0.17	0.00	0.00	20.9
5	0	-0	2735	0	0	0	-2377	--	--	16.08	16.08	0.29	0.04	0.02	0.17	0.00	0.00	20.9
6	0	-0	2438	0	0	0	-2599	--	--	16.08	16.08	0.29	0.05	0.02	0.15	0.00	0.00	20.9
7	0	-0	2455	0	0	0	-2578	--	--	16.08	16.08	0.29	0.04	0.02	0.15	0.00	0.00	20.9
8	0	-0	2570	0	0	0	-2503	--	--	16.08	16.08	0.29	0.04	0.02	0.16	0.00	0.00	20.9
9	0	-0	2587	0	0	0	-2482	--	--	16.08	16.08	0.29	0.04	0.02	0.16	0.00	0.00	20.9
10	0	-0	2290	0	0	0	-2705	--	--	16.08	16.08	0.29	0.05	0.02	0.14	0.00	0.00	20.9
11	0	-0	2295	0	0	0	-2698	--	--	16.08	16.08	0.29	0.05	0.02	0.14	0.00	0.00	20.9
12	0	-0	2730	0	0	0	-2383	--	--	16.08	16.08	0.29	0.04	0.02	0.17	0.00	0.00	20.9
13	0	-0	2735	0	0	0	-2377	--	--	16.08	16.08	0.29	0.04	0.02	0.17	0.00	0.00	20.9
14	0	-0	2438	0	0	0	-2599	--	--	16.08	16.08	0.29	0.05	0.02	0.15	0.00	0.00	20.9
15	0	-0	2455	0	0	0	-2578	--	--	16.08	16.08	0.29	0.04	0.02	0.15	0.00	0.00	20.9
16	0	-0	2570	0	0	0	-2503	--	--	16.08	16.08	0.29	0.04	0.02	0.16	0.00	0.00	20.9
17	0	-0	2587	0	0	0	-2482	--	--	16.08	16.08	0.29	0.04	0.02	0.16	0.00	0.00	20.9
18	0	-0	2675	0	0	0	-4227	--	--	16.08	16.08	0.18	0.07	0.02	0.17	0.00	0.00	20.9
19	0	-0	4175	0	0	0	-3176	--	--	16.08	16.08	0.18	0.05	0.03	0.26	0.00	0.00	20.9
20	0	-0	3410	0	0	0	-3640	--	--	16.08	16.08	0.18	0.06	0.03	0.21	0.00	0.00	20.9
37	0	-0	2099	0	0	0	-4429	--	--	16.08	16.08	0.18	0.07	0.02	0.13	0.00	0.00	20.9
38	0	-0	4598	0	0	0	-2678	--	--	16.08	16.08	0.18	0.04	0.04	0.29	0.00	0.00	20.9
39	0	-0	3324	0	0	0	-3450	--	--	16.08	16.08	0.18	0.06	0.03	0.21	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	3266	0	0	0	-3303	--	--	16.08	16.08	0.18	0.05	0.03	0.20	0.00	0.00	20.9
2	26	-0	2290	0	0	0	-2705	--	--	16.08	16.08	0.29	0.05	0.02	0.14	0.00	0.00	20.9
3	26	-0	2295	0	0	0	-2698	--	--	16.08	16.08	0.29	0.05	0.02	0.14	0.00	0.00	20.9
4	26	-0	2730	0	0	0	-2383	--	--	16.08	16.08	0.29	0.04	0.02	0.17	0.00	0.00	20.9
5	26	-0	2735	0	0	0	-2377	--	--	16.08	16.08	0.29	0.04	0.02	0.17	0.00	0.00	20.9
6	26	-0	2438	0	0	0	-2599	--	--	16.08	16.08	0.29	0.05	0.02	0.15	0.00	0.00	20.9
7	26	-0	2455	0	0	0	-2578	--	--	16.08	16.08	0.29	0.04	0.02	0.15	0.00	0.00	20.9
8	26	-0	2570	0	0	0	-2503	--	--	16.08	16.08	0.29	0.04	0.02	0.16	0.00	0.00	20.9
9	26	-0	2587	0	0	0	-2482	--	--	16.08	16.08	0.29	0.04	0.02	0.16	0.00	0.00	20.9
10	26	-0	2290	0	0	0	-2705	--	--	16.08	16.08	0.29	0.05	0.02	0.14	0.00	0.00	20.9
11	26	-0	2295	0	0	0	-2698	--	--	16.08	16.08	0.29	0.05	0.02	0.14	0.00	0.00	20.9
12	26	-0	2730	0	0	0	-2383	--	--	16.08	16.08	0.29	0.04	0.02	0.17	0.00	0.00	20.9
13	26	-0	2735	0	0	0	-2377	--	--	16.08	16.08	0.29	0.04	0.02	0.17	0.00	0.00	20.9
14	26	-0	2438	0	0	0	-2599	--	--	16.08	16.08	0.29	0.05	0.02	0.15	0.00	0.00	20.9
15	26	-0	2455	0	0	0	-2578	--	--	16.08	16.08	0.29	0.04	0.02	0.15	0.00	0.00	20.9
16	26	-0	2570	0	0	0	-2503	--	--	16.08	16.08	0.29	0.04	0.02	0.16	0.00	0.00	20.9
17	26	-0	2587	0	0	0	-2482	--	--	16.08	16.08	0.29	0.04	0.02	0.16	0.00	0.00	20.9
18	26	-0	2675	0	0	0	-4227	--	--	16.08	16.08	0.18	0.07	0.02	0.17	0.00	0.00	20.9
19	26	-0	4175	0	0	0	-3176	--	--	16.08	16.08	0.18	0.05	0.03	0.26	0.00	0.00	20.9
20	26	-0	3410	0	0	0	-3640	--	--	16.08	16.08	0.18	0.06	0.03	0.21	0.00	0.00	20.9
37	26	-0	2099	0	0	0	-4429	--	--	16.08	16.08	0.18	0.07	0.02	0.13	0.00	0.00	20.9
38	26	-0	4598	0	0	0	-2678	--	--	16.08	16.08	0.18	0.04	0.04	0.29	0.00	0.00	20.9
39	26	-0	3324	0	0	0	-3450	--	--	16.08	16.08	0.18	0.06	0.03	0.21	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	3266	0	0	0	-3303	--	--	16.08	16.08	0.18	0.05	0.03	0.20	0.00	0.00	20.9
2	51	-0	2290	0	0	0	-2705	--	--	16.08	16.08	0.29	0.05	0.02	0.14	0.00	0.00	20.9

3	51	-0	2295	0	0	0	-2698	--	--	16.08	16.08	0.29	0.05	0.02	0.14	0.00	0.00	20.9
4	51	-0	2730	0	0	0	-2383	--	--	16.08	16.08	0.29	0.04	0.02	0.17	0.00	0.00	20.9
5	51	-0	2735	0	0	0	-2377	--	--	16.08	16.08	0.29	0.04	0.02	0.17	0.00	0.00	20.9
6	51	-0	2438	0	0	0	-2599	--	--	16.08	16.08	0.29	0.05	0.02	0.15	0.00	0.00	20.9
7	51	-0	2455	0	0	0	-2578	--	--	16.08	16.08	0.29	0.04	0.02	0.15	0.00	0.00	20.9
8	51	-0	2570	0	0	0	-2503	--	--	16.08	16.08	0.29	0.04	0.02	0.16	0.00	0.00	20.9
9	51	-0	2587	0	0	0	-2482	--	--	16.08	16.08	0.29	0.04	0.02	0.16	0.00	0.00	20.9
10	51	-0	2290	0	0	0	-2705	--	--	16.08	16.08	0.29	0.05	0.02	0.14	0.00	0.00	20.9
11	51	-0	2295	0	0	0	-2698	--	--	16.08	16.08	0.29	0.05	0.02	0.14	0.00	0.00	20.9
12	51	-0	2730	0	0	0	-2383	--	--	16.08	16.08	0.29	0.04	0.02	0.17	0.00	0.00	20.9
13	51	-0	2735	0	0	0	-2377	--	--	16.08	16.08	0.29	0.04	0.02	0.17	0.00	0.00	20.9
14	51	-0	2438	0	0	0	-2599	--	--	16.08	16.08	0.29	0.05	0.02	0.15	0.00	0.00	20.9
15	51	-0	2455	0	0	0	-2578	--	--	16.08	16.08	0.29	0.04	0.02	0.15	0.00	0.00	20.9
16	51	-0	2570	0	0	0	-2503	--	--	16.08	16.08	0.29	0.04	0.02	0.16	0.00	0.00	20.9
17	51	-0	2587	0	0	0	-2482	--	--	16.08	16.08	0.29	0.04	0.02	0.16	0.00	0.00	20.9
18	51	-0	2675	0	0	0	-4227	--	--	16.08	16.08	0.18	0.07	0.02	0.17	0.00	0.00	20.9
19	51	-0	4175	0	0	0	-3176	--	--	16.08	16.08	0.18	0.05	0.03	0.26	0.00	0.00	20.9
20	51	-0	3410	0	0	0	-3640	--	--	16.08	16.08	0.18	0.06	0.03	0.21	0.00	0.00	20.9
37	51	-0	2099	0	0	0	-4429	--	--	16.08	16.08	0.18	0.07	0.02	0.13	0.00	0.00	20.9
38	51	-0	4598	0	0	0	-2678	--	--	16.08	16.08	0.18	0.04	0.04	0.29	0.00	0.00	20.9
39	51	-0	3324	0	0	0	-3450	--	--	16.08	16.08	0.18	0.06	0.03	0.21	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 81 NI 1825 NF 1824 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	5057	0	0	0	-1625	--	--	16.08	16.08	0.18	0.03	0.04	0.32	0.00	0.00	20.9
2	0	-0	3649	0	0	0	-1528	--	--	16.08	16.08	0.29	0.03	0.03	0.23	0.00	0.00	20.9
3	0	-0	3653	0	0	0	-1519	--	--	16.08	16.08	0.29	0.03	0.03	0.23	0.00	0.00	20.9
4	0	-0	4128	0	0	0	-981	--	--	16.08	16.08	0.29	0.02	0.03	0.26	0.00	0.00	20.9
5	0	-0	4131	0	0	0	-972	--	--	16.08	16.08	0.29	0.02	0.03	0.26	0.00	0.00	20.9
6	0	-0	3813	0	0	0	-1347	--	--	16.08	16.08	0.29	0.02	0.03	0.24	0.00	0.00	20.9
7	0	-0	3825	0	0	0	-1318	--	--	16.08	16.08	0.29	0.02	0.03	0.24	0.00	0.00	20.9
8	0	-0	3956	0	0	0	-1183	--	--	16.08	16.08	0.29	0.02	0.03	0.25	0.00	0.00	20.9
9	0	-0	3968	0	0	0	-1153	--	--	16.08	16.08	0.29	0.02	0.03	0.25	0.00	0.00	20.9
10	0	-0	3649	0	0	0	-1528	--	--	16.08	16.08	0.29	0.03	0.03	0.23	0.00	0.00	20.9
11	0	-0	3653	0	0	0	-1519	--	--	16.08	16.08	0.29	0.03	0.03	0.23	0.00	0.00	20.9
12	0	-0	4128	0	0	0	-981	--	--	16.08	16.08	0.29	0.02	0.03	0.26	0.00	0.00	20.9
13	0	-0	4131	0	0	0	-972	--	--	16.08	16.08	0.29	0.02	0.03	0.26	0.00	0.00	20.9
14	0	-0	3813	0	0	0	-1347	--	--	16.08	16.08	0.29	0.02	0.03	0.24	0.00	0.00	20.9
15	0	-0	3825	0	0	0	-1318	--	--	16.08	16.08	0.29	0.02	0.03	0.24	0.00	0.00	20.9
16	0	-0	3956	0	0	0	-1183	--	--	16.08	16.08	0.29	0.02	0.03	0.25	0.00	0.00	20.9
17	0	-0	3968	0	0	0	-1153	--	--	16.08	16.08	0.29	0.02	0.03	0.25	0.00	0.00	20.9
18	0	-0	4593	0	0	0	-2853	--	--	16.08	16.08	0.18	0.05	0.04	0.29	0.00	0.00	20.9
19	0	-0	6217	0	0	0	-1032	--	--	16.08	16.08	0.18	0.02	0.05	0.39	0.00	0.00	20.9
20	0	-0	5367	0	0	0	-1888	--	--	16.08	16.08	0.18	0.03	0.04	0.34	0.00	0.00	20.9
37	0	-0	3899	0	0	0	-3351	--	--	16.08	16.08	0.18	0.06	0.03	0.24	0.00	0.00	20.9
38	0	-0	6606	0	0	0	-317	--	--	16.08	16.08	0.18	0.01	0.05	0.41	0.00	0.00	20.9
39	0	-0	5189	0	0	0	-1743	--	--	16.08	16.08	0.18	0.03	0.04	0.33	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	5057	0	0	0	-1625	--	--	16.08	16.08	0.18	0.03	0.04	0.32	0.00	0.00	20.9
2	26	-0	3649	0	0	0	-1528	--	--	16.08	16.08	0.29	0.03	0.03	0.23	0.00	0.00	20.9
3	26	-0	3653	0	0	0	-1519	--	--	16.08	16.08	0.29	0.03	0.03	0.23	0.00	0.00	20.9
4	26	-0	4128	0	0	0	4491	--	--	16.08	16.08	0.10	0.08	0.03	0.26	0.00	0.00	20.9
5	26	-0	4131	0	0	0	4504	--	--	16.08	16.08	0.10	0.08	0.03	0.26	0.00	0.00	20.9
6	26	-0	3813	0	0	0	-1347	--	--	16.08	16.08	0.29	0.02	0.03	0.24	0.00	0.00	20.9
7	26	-0	3825	0	0	0	-1318	--	--	16.08	16.08	0.29	0.02	0.03	0.24	0.00	0.00	20.9
8	26	-0	3956	0	0	0	-1183	--	--	16.08	16.08	0.29	0.02	0.03	0.25	0.00	0.00	20.9
9	26	-0	3968	0	0	0	-1153	--	--	16.08	16.08	0.29	0.02	0.03	0.25	0.00	0.00	20.9
10	26	-0	3649	0	0	0	-1528	--	--	16.08	16.08	0.29	0.03	0.03	0.23	0.00	0.00	20.9
11	26	-0	3653	0	0	0	-1519	--	--	16.08	16.08	0.29	0.03	0.03	0.23	0.00	0.00	20.9
12	26	-0	4128	0	0	0	4491	--	--	16.08	16.08	0.10	0.08	0.03	0.26	0.00	0.00	20.9
13	26	-0	4131	0	0	0	4504	--	--	16.08	16.08	0.10	0.08	0.03	0.26	0.00	0.00	20.9
14	26	-0	3813	0	0	0	-1347	--	--	16.08	16.08	0.29	0.02	0.03	0.24	0.00	0.00	20.9
15	26	-0	3825	0	0	0	-1318	--	--	16.08	16.08	0.29	0.02	0.03	0.24	0.00	0.00	20.9
16	26	-0	3956	0	0	0	-1183	--	--	16.08	16.08	0.29	0.02	0.03	0.25	0.00	0.00	20.9
17	26	-0	3968	0	0	0	-1153	--	--	16.08	16.08	0.29	0.02	0.03	0.25	0.00	0.00	20.9
18	26	-0	4593	0	0	0	-2853	--	--	16.08	16.08	0.18	0.05	0.04	0.29	0.00	0.00	20.9
19	26	-0	6217	0	0	0	7209	--	--	16.08	16.08	0.00	0.12	0.05	0.39	0.00	0.00	20.9
20	26	-0	5367	0	0	0	-1888	--	--	16.08	16.08	0.18	0.03	0.04	0.34	0.00	0.00	20.9
37	26	-0	3899	0	0	0	-3351	--	--	16.08	16.08	0.18	0.06	0.03	0.24	0.00	0.00	20.9
38	26	-0	6606	0	0	0	8440	--	--	16.08	16.08	0.00	0.14	0.05	0.41	0.00	0.00	20.9
39	26	-0	5189	0	0	0	-1743	--	--	16.08	16.08	0.18	0.03	0.04	0.33	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	5057	0	0	0	972	--	--	16.08	16.08	0.00	0.02	0.04	0.32	0.00	0.00	20.9
2	51	-0	3649	0	0	0	346	--	--	16.08	16.08	0.10	0.01	0.03	0.23	0.00	0.00	20.9
3	51	-0	3653	0	0	0	357	--	--	16.08	16.08	0.10	0.01	0.03	0.23	0.00	0.00	20.9
4	51	-0	4128	0	0	0	1139	--	--	16.08	16.08	0.10	0.02	0.03	0.26	0.00	0.00	20.9
5	51	-0	4131	0	0	0	1150	--	--	16.08	16.08	0.10	0.02	0.03	0.26	0.00	0.00	20.9
6	51	-0	3813	0	0	0	611	--	--	16.08	16.08	0.10	0.01	0.03	0.24	0.00	0.00	20.9
7	51	-0	3825	0	0	0	647	--	--	16.08	16.08	0.10	0.01	0.03	0.24	0.00	0.00	20.9
8	51	-0	3956	0	0	0	849	--	--	16.08	16.08	0.10	0.02	0.03	0.25	0.00	0.00	20.9
9	51	-0	3968	0	0	0	885	--	--	16.08	16.08	0.10	0.02	0.03	0.25	0.00	0.00	20.9
10	51	-0	3649	0	0	0	346	--	--	16.08	16.08	0.10	0.01	0.03	0.23	0.00	0.00	20.9
11	51	-0	3653	0	0	0	357	--	--	16.08	16.08	0.10	0.01	0.03	0.23	0.00	0.00	20.9
12	51	-0	4128	0	0	0	1139	--	--	16.08	16.08	0.10	0.02	0.03	0.26	0.00	0.00	20.9
13	51	-0	4131	0	0	0	1150	--	--	16.08	16.08	0.10	0.02	0.03	0.26	0.00	0.00	20.9
14	51	-0	3813	0	0	0	611	--	--	16.08	16.08	0.10	0.01	0.03	0.24	0.00	0.00	20.9
15	51	-0	3825	0	0	0	647	--	--	16.08	16.08	0.10	0.01	0.03	0.24	0.00	0.00	20.9
16	51	-0	3956	0	0	0	849	--	--	16.08	16.08	0.10	0.02	0.03	0.25	0.00	0.00	20.9
17	51	-0	3968	0	0	0	885	--	--	16.08	16.08	0.10	0.02	0.03	0.25	0.00	0.00	20.9
18	51	-0	4593	0	0	0	-2853	--	--	16.08	16.08	0.18	0.05	0.04	0.29	0.00	0.00	20.9
19	51	-0	6217	0	0	0	2161	--	--	16.08	16.08	0.00	0.04	0.05	0.39	0.00	0.00	20.9
20	51	-0	5367	0	0	0	868	--	--	16.08	16.08	0.00	0.01	0.04	0.34	0.00	0.00	20.9
37	51	-0	3899	0	0	0	-3351	--	--	16.08	16.08	0.18	0.06	0.03	0.24	0.00	0.00	20.9
38	51	-0	6606	0	0	0	3076	--	--	16.08	16.08	0.00	0.05	0.05	0.41	0.00	0.00	20.9
39	51	-0	5189	0	0	0	922	--	--	16.08	16.08	0.00	0.02	0.04	0.33	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 82 NI 1824 NF 1839 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	6885	0	0	0	972	--	--	16.08	16.08	0.00	0.02	0.06	0.43	0.00	0.00	20.9
2	0	-0	5036	0	0	0	346	--	--	16.08	16.08	0.10	0.01	0.04	0.32	0.00	0.00	20.9
3	0	-0	5038	0	0	0	357	--	--	16.08	16.08	0.10	0.01	0.04	0.32	0.00	0.00	20.9
4	0	-0	5554	0	0	0	1139	--	--	16.08	16.08	0.10	0.02	0.05	0.35	0.00	0.00	20.9
5	0	-0	5556	0	0	0	1150	--	--	16.08	16.08	0.10	0.02	0.05	0.35	0.00	0.00	20.9
6	0	-0	5214	0	0	0	611	--	--	16.08	16.08	0.10	0.01	0.04	0.33	0.00	0.00	20.9
7	0	-0	5222	0	0	0	647	--	--	16.08	16.08	0.10	0.01	0.04	0.33	0.00	0.00	20.9
8	0	-0	5370	0	0	0	849	--	--	16.08	16.08	0.10	0.02	0.04	0.34	0.00	0.00	20.9
9	0	-0	5377	0	0	0	885	--	--	16.08	16.08	0.10	0.02	0.04	0.34	0.00	0.00	20.9
10	0	-0	5036	0	0	0	346	--	--	16.08	16.08	0.10	0.01	0.04	0.32	0.00	0.00	20.9
11	0	-0	5038	0	0	0	357	--	--	16.08	16.08	0.10	0.01	0.04	0.32	0.00	0.00	20.9
12	0	-0	5554	0	0	0	1139	--	--	16.08	16.08	0.10	0.02	0.05	0.35	0.00	0.00	20.9
13	0	-0	5556	0	0	0	1150	--	--	16.08	16.08	0.10	0.02	0.05	0.35	0.00	0.00	20.9
14	0	-0	5214	0	0	0	611	--	--	16.08	16.08	0.10	0.01	0.04	0.33	0.00	0.00	20.9
15	0	-0	5222	0	0	0	647	--	--	16.08	16.08	0.10	0.01	0.04	0.33	0.00	0.00	20.9
16	0	-0	5370	0	0	0	849	--	--	16.08	16.08	0.10	0.02	0.04	0.34	0.00	0.00	20.9
17	0	-0	5377	0	0	0	885	--	--	16.08	16.08	0.10	0.02	0.04	0.34	0.00	0.00	20.9
18	0	-0	6536	0	0	0	-494	--	--	16.08	16.08	0.18	0.01	0.05	0.41	0.00	0.00	20.9
19	0	-0	8299	0	0	0	2161	--	--	16.08	16.08	0.00	0.04	0.07	0.52	0.00	0.00	20.9
20	0	-0	7357	0	0	0	868	--	--	16.08	16.08	0.00	0.01	0.06	0.46	0.00	0.00	20.9
37	0	-0	5721	0	0	0	-1349	--	--	16.08	16.08	0.18	0.02	0.05	0.36	0.00	0.00	20.9
38	0	-0	8658	0	0	0	3076	--	--	16.08	16.08	0.00	0.05	0.07	0.54	0.00	0.00	20.9
39	0	-0	7088	0	0	0	922	--	--	16.08	16.08	0.00	0.02	0.06	0.44	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	26	-0	6885	0	0	0	10099	--	--	16.08	16.08	0.00	0.17	0.06	0.43	0.00	0.00	20.9
2	26	-0	5036	0	0	0	7022	--	--	16.08	16.08	0.10	0.12	0.04	0.32	0.00	0.00	20.9
3	26	-0	5038	0	0	0	7035	--	--	16.08	16.08	0.10	0.12	0.04	0.32	0.00	0.00	20.9
4	26	-0	5554	0	0	0	8501	--	--	16.08	16.08	0.10	0.15	0.05	0.35	0.00	0.00	20.9
5	26	-0	5556	0	0	0	8515	--	--	16.08	16.08	0.10	0.15	0.05	0.35	0.00	0.00	20.9
6	26	-0	5214	0	0	0	7523	--	--	16.08	16.08	0.10	0.13	0.04	0.33	0.00	0.00	20.9
7	26	-0	5222	0	0	0	7569	--	--	16.08	16.08	0.10	0.13	0.04	0.33	0.00	0.00	20.9
8	26	-0	5370	0	0	0	7968	--	--	16.08	16.08	0.10	0.14	0.04	0.34	0.00	0.00	20.9
9	26	-0	5377	0	0	0	8012	--	--	16.08	16.08	0.10	0.14	0.04	0.34	0.00	0.00	20.9
10	26	-0	5036	0	0	0	7022	--	--	16.08	16.08	0.10	0.12	0.04	0.32	0.00	0.00	20.9
11	26	-0	5038	0	0	0	7035	--	--	16.08	16.08	0.10	0.12	0.04	0.32	0.00	0.00	20.9
12	26	-0	5554	0	0	0	8501	--	--	16.08	16.08	0.10	0.15	0.05	0.35	0.00	0.00	20.9
13	26	-0	5556	0	0	0	8515	--	--	16.08	16.08	0.10	0.15	0.05	0.35	0.00	0.00	20.9
14	26	-0	5214	0	0	0	7523	--	--	16.08	16.08	0.10	0.13	0.04	0.33	0.00	0.00	20.9
15	26	-0	5222	0	0	0	7569	--	--	16.08	16.08	0.10	0.13	0.04	0.33	0.00	0.00	20.9
16	26	-0	5370	0	0	0	7968	--	--	16.08	16.08	0.10	0.14	0.04	0.34	0.00	0.00	20.9
17	26	-0	5377	0	0	0	8012	--	--	16.08	16.08	0.10	0.14	0.04	0.34	0.00	0.00	20.9
18	26	-0	6536	0	0	0	8170	--	--	16.08	16.08	0.00	0.14	0.05	0.41	0.00	0.00	20.9
19	26	-0	8299	0	0	0	13162	--	--	16.08	16.08	0.00	0.22	0.07	0.52	0.00	0.00	20.9
20	26	-0	7357	0	0	0	10620	--	--	16.08	16.08	0.00	0.18	0.06	0.46	0.00	0.00	20.9
37	26	-0	5721	0	0	0	6235	--	--	16.08	16.08	0.00	0.11	0.05	0.36	0.00	0.00	20.9
38	26	-0	8658	0	0	0	14553	--	--	16.08	16.08	0.00	0.25	0.07	0.54	0.00	0.00	20.9
39	26	-0	7088	0	0	0	10318	--	--	16.08	16.08	0.00	0.18	0.06	0.44	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	51	-0	6885	0	0	0	4509	--	--	16.08	16.08	0.00	0.08	0.06	0.43	0.00	0.00	20.9
2	51	-0	5036	0	0	0	2933	--	--	16.08	16.08	0.10	0.05	0.04	0.32	0.00	0.00	20.9
3	51	-0	5038	0	0	0	2945	--	--	16.08	16.08	0.10	0.05	0.04	0.32	0.00	0.00	20.9
4	51	-0	5554	0	0	0	3992	--	--	16.08	16.08	0.10	0.07	0.05	0.35	0.00	0.00	20.9
5	51	-0	5556	0	0	0	4004	--	--	16.08	16.08	0.10	0.07	0.05	0.35	0.00	0.00	20.9
6	51	-0	5214	0	0	0	3290	--	--	16.08	16.08	0.10	0.06	0.04	0.33	0.00	0.00	20.9
7	51	-0	5222	0	0	0	3329	--	--	16.08	16.08	0.10	0.06	0.04	0.33	0.00	0.00	20.9
8	51	-0	5370	0	0	0	3608	--	--	16.08	16.08	0.10	0.06	0.04	0.34	0.00	0.00	20.9
9	51	-0	5377	0	0	0	3647	--	--	16.08	16.08	0.10	0.06	0.04	0.34	0.00	0.00	20.9
10	51	-0	5036	0	0	0	2933	--	--	16.08	16.08	0.10	0.05	0.04	0.32	0.00	0.00	20.9
11	51	-0	5038	0	0	0	2945	--	--	16.08	16.08	0.10	0.05	0.04	0.32	0.00	0.00	20.9
12	51	-0	5554	0	0	0	3992	--	--	16.08	16.08	0.10	0.07	0.05	0.35	0.00	0.00	20.9
13	51	-0	5556	0	0	0	4004	--	--	16.08	16.08	0.10	0.07	0.05	0.35	0.00	0.00	20.9
14	51	-0	5214	0	0	0	3290	--	--	16.08	16.08	0.10	0.06	0.04	0.33	0.00	0.00	20.9
15	51	-0	5222	0	0	0	3329	--	--	16.08	16.08	0.10	0.06	0.04	0.33	0.00	0.00	20.9
16	51	-0	5370	0	0	0	3608	--	--	16.08	16.08	0.10	0.06	0.04	0.34	0.00	0.00	20.9
17	51	-0	5377	0	0	0	3647	--	--	16.08	16.08	0.10	0.06	0.04	0.34	0.00	0.00	20.9
18	51	-0	6536	0	0	0	2864	--	--	16.08	16.08	0.00	0.05	0.05	0.41	0.00	0.00	20.9
19	51	-0	8299	0	0	0	6424	--	--	16.08	16.08	0.00	0.11	0.07	0.52	0.00	0.00	20.9
20	51	-0	7357	0	0	0	4647	--	--	16.08	16.08	0.00	0.08	0.06	0.46	0.00	0.00	20.9
37	51	-0	5721	0	0	0	1590	--	--	16.08	16.08	0.00	0.03	0.05	0.36	0.00	0.00	20.9
38	51	-0	8658	0	0	0	7524	--	--	16.08	16.08	0.00	0.13	0.07	0.54	0.00	0.00	20.9
39	51	-0	7088	0	0	0	4563	--	--	16.08	16.08	0.00	0.08	0.06	0.44	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 83 NI 1839 NF 1843 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	8747	0	0	0	4509	--	--	16.08	16.08	0.00	0.08	0.07	0.55	0.00	0.00	20.9
2	0	-0	6451	0	0	0	2933	--	--	16.08	16.08	0.10	0.05	0.05	0.40	0.00	0.00	20.9
3	0	-0	6452	0	0	0	2945	--	--	16.08	16.08	0.10	0.05	0.05	0.40	0.00	0.00	20.9
4	0	-0	7006	0	0	0	3992	--	--	16.08	16.08	0.10	0.07	0.06	0.44	0.00	0.00	20.9
5	0	-0	7007	0	0	0	4004	--	--	16.08	16.08	0.10	0.07	0.06	0.44	0.00	0.00	20.9
6	0	-0	6644	0	0	0	3290	--	--	16.08	16.08	0.10	0.06	0.05	0.42	0.00	0.00	20.9
7	0	-0	6647	0	0	0	3329	--	--	16.08	16.08	0.10	0.06	0.05	0.42	0.00	0.00	20.9
8	0	-0	6810	0	0	0	3608	--	--	16.08	16.08	0.10	0.06	0.06	0.43	0.00	0.00	20.9
9	0	-0	6814	0	0	0	3647	--	--	16.08	16.08	0.10	0.06	0.06	0.43	0.00	0.00	20.9
10	0	-0	6451	0	0	0	2933	--	--	16.08	16.08	0.10	0.05	0.05	0.40	0.00	0.00	20.9

11	0	-0	6452	0	0	0	2945	--	--	16.08	16.08	0.10	0.05	0.05	0.40	0.00	0.00	20.9
12	0	-0	7006	0	0	0	3992	--	--	16.08	16.08	0.10	0.07	0.06	0.44	0.00	0.00	20.9
13	0	-0	7007	0	0	0	4004	--	--	16.08	16.08	0.10	0.07	0.06	0.44	0.00	0.00	20.9
14	0	-0	6644	0	0	0	3290	--	--	16.08	16.08	0.10	0.06	0.05	0.42	0.00	0.00	20.9
15	0	-0	6647	0	0	0	3329	--	--	16.08	16.08	0.10	0.06	0.05	0.42	0.00	0.00	20.9
16	0	-0	6810	0	0	0	3608	--	--	16.08	16.08	0.10	0.06	0.06	0.43	0.00	0.00	20.9
17	0	-0	6814	0	0	0	3647	--	--	16.08	16.08	0.10	0.06	0.06	0.43	0.00	0.00	20.9
18	0	-0	8513	0	0	0	2864	--	--	16.08	16.08	0.00	0.05	0.07	0.53	0.00	0.00	20.9
19	0	-0	10410	0	0	0	6424	--	--	16.08	16.08	0.00	0.11	0.09	0.65	0.00	0.00	20.9
20	0	-0	9381	0	0	0	4647	--	--	16.08	16.08	0.00	0.08	0.08	0.59	0.00	0.00	20.9
37	0	-0	7576	0	0	0	1590	--	--	16.08	16.08	0.00	0.03	0.06	0.48	0.00	0.00	20.9
38	0	-0	10750	0	0	0	7524	--	--	16.08	16.08	0.00	0.13	0.09	0.67	0.00	0.00	20.9
39	0	-0	9023	0	0	0	4563	--	--	16.08	16.08	0.00	0.08	0.07	0.57	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	8747	0	0	0	16104	--	--	16.08	16.08	0.00	0.27	0.07	0.55	0.00	0.00	20.9
2	26	-0	6451	0	0	0	11484	--	--	16.08	16.08	0.10	0.20	0.05	0.40	0.00	0.00	20.9
3	26	-0	6452	0	0	0	11498	--	--	16.08	16.08	0.10	0.20	0.05	0.40	0.00	0.00	20.9
4	26	-0	7006	0	0	0	13279	--	--	16.08	16.08	0.10	0.24	0.06	0.44	0.00	0.00	20.9
5	26	-0	7007	0	0	0	13292	--	--	16.08	16.08	0.10	0.24	0.06	0.44	0.00	0.00	20.9
6	26	-0	6644	0	0	0	12097	--	--	16.08	16.08	0.10	0.21	0.05	0.42	0.00	0.00	20.9
7	26	-0	6647	0	0	0	12140	--	--	16.08	16.08	0.10	0.22	0.05	0.42	0.00	0.00	20.9
8	26	-0	6810	0	0	0	12635	--	--	16.08	16.08	0.10	0.22	0.06	0.43	0.00	0.00	20.9
9	26	-0	6814	0	0	0	12679	--	--	16.08	16.08	0.10	0.22	0.06	0.43	0.00	0.00	20.9
10	26	-0	6451	0	0	0	11484	--	--	16.08	16.08	0.10	0.20	0.05	0.40	0.00	0.00	20.9
11	26	-0	6452	0	0	0	11498	--	--	16.08	16.08	0.10	0.20	0.05	0.40	0.00	0.00	20.9
12	26	-0	7006	0	0	0	13279	--	--	16.08	16.08	0.10	0.24	0.06	0.44	0.00	0.00	20.9
13	26	-0	7007	0	0	0	13292	--	--	16.08	16.08	0.10	0.24	0.06	0.44	0.00	0.00	20.9
14	26	-0	6644	0	0	0	12097	--	--	16.08	16.08	0.10	0.21	0.05	0.42	0.00	0.00	20.9
15	26	-0	6647	0	0	0	12140	--	--	16.08	16.08	0.10	0.22	0.05	0.42	0.00	0.00	20.9
16	26	-0	6810	0	0	0	12635	--	--	16.08	16.08	0.10	0.22	0.06	0.43	0.00	0.00	20.9
17	26	-0	6814	0	0	0	12679	--	--	16.08	16.08	0.10	0.22	0.06	0.43	0.00	0.00	20.9
18	26	-0	8513	0	0	0	14148	--	--	16.08	16.08	0.00	0.24	0.07	0.53	0.00	0.00	20.9
19	26	-0	10410	0	0	0	20223	--	--	16.08	16.08	0.00	0.34	0.09	0.65	0.00	0.00	20.9
20	26	-0	9381	0	0	0	17082	--	--	16.08	16.08	0.00	0.29	0.08	0.59	0.00	0.00	20.9
37	26	-0	7576	0	0	0	11632	--	--	16.08	16.08	0.00	0.20	0.06	0.48	0.00	0.00	20.9
38	26	-0	10750	0	0	0	21771	--	--	16.08	16.08	0.00	0.37	0.09	0.67	0.00	0.00	20.9
39	26	-0	9023	0	0	0	16523	--	--	16.08	16.08	0.00	0.28	0.07	0.57	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	8747	0	0	0	9002	--	--	16.08	16.08	0.00	0.15	0.07	0.55	0.00	0.00	20.9
2	51	-0	6451	0	0	0	6246	--	--	16.08	16.08	0.10	0.11	0.05	0.40	0.00	0.00	20.9
3	51	-0	6452	0	0	0	6259	--	--	16.08	16.08	0.10	0.11	0.05	0.40	0.00	0.00	20.9
4	51	-0	7006	0	0	0	7590	--	--	16.08	16.08	0.10	0.13	0.06	0.44	0.00	0.00	20.9
5	51	-0	7007	0	0	0	7602	--	--	16.08	16.08	0.10	0.13	0.06	0.44	0.00	0.00	20.9
6	51	-0	6644	0	0	0	6702	--	--	16.08	16.08	0.10	0.12	0.05	0.42	0.00	0.00	20.9
7	51	-0	6647	0	0	0	6743	--	--	16.08	16.08	0.10	0.12	0.05	0.42	0.00	0.00	20.9
8	51	-0	6810	0	0	0	7105	--	--	16.08	16.08	0.10	0.13	0.06	0.43	0.00	0.00	20.9
9	51	-0	6814	0	0	0	7146	--	--	16.08	16.08	0.10	0.13	0.06	0.43	0.00	0.00	20.9
10	51	-0	6451	0	0	0	6246	--	--	16.08	16.08	0.10	0.11	0.05	0.40	0.00	0.00	20.9
11	51	-0	6452	0	0	0	6259	--	--	16.08	16.08	0.10	0.11	0.05	0.40	0.00	0.00	20.9
12	51	-0	7006	0	0	0	7590	--	--	16.08	16.08	0.10	0.13	0.06	0.44	0.00	0.00	20.9
13	51	-0	7007	0	0	0	7602	--	--	16.08	16.08	0.10	0.13	0.06	0.44	0.00	0.00	20.9
14	51	-0	6644	0	0	0	6702	--	--	16.08	16.08	0.10	0.12	0.05	0.42	0.00	0.00	20.9
15	51	-0	6647	0	0	0	6743	--	--	16.08	16.08	0.10	0.12	0.05	0.42	0.00	0.00	20.9
16	51	-0	6810	0	0	0	7105	--	--	16.08	16.08	0.10	0.13	0.06	0.43	0.00	0.00	20.9
17	51	-0	6814	0	0	0	7146	--	--	16.08	16.08	0.10	0.13	0.06	0.43	0.00	0.00	20.9
18	51	-0	8513	0	0	0	7236	--	--	16.08	16.08	0.00	0.12	0.07	0.53	0.00	0.00	20.9
19	51	-0	10410	0	0	0	11770	--	--	16.08	16.08	0.00	0.20	0.09	0.65	0.00	0.00	20.9
20	51	-0	9381	0	0	0	9465	--	--	16.08	16.08	0.00	0.16	0.08	0.59	0.00	0.00	20.9
37	51	-0	7576	0	0	0	5481	--	--	16.08	16.08	0.00	0.09	0.06	0.48	0.00	0.00	20.9
38	51	-0	10750	0	0	0	13040	--	--	16.08	16.08	0.00	0.22	0.09	0.67	0.00	0.00	20.9
39	51	-0	9023	0	0	0	9197	--	--	16.08	16.08	0.00	0.16	0.07	0.57	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 84 NI 1843 NF 1653 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm

1	0	-0	-10320	0	0	0	9915	--	--	16.08	16.08	0.00	0.17	0.09	0.65	0.00	0.00	20.9
2	0	-0	-8159	0	0	0	7886	--	--	16.08	16.08	0.10	0.14	0.07	0.51	0.00	0.00	20.9
3	0	-0	-8151	0	0	0	7886	--	--	16.08	16.08	0.10	0.14	0.07	0.51	0.00	0.00	20.9
4	0	-0	-7731	0	0	0	7367	--	--	16.08	16.08	0.10	0.13	0.06	0.48	0.00	0.00	20.9
5	0	-0	-7722	0	0	0	7367	--	--	16.08	16.08	0.10	0.13	0.06	0.48	0.00	0.00	20.9
6	0	-0	-8019	0	0	0	7704	--	--	16.08	16.08	0.10	0.14	0.07	0.50	0.00	0.00	20.9
7	0	-0	-7991	0	0	0	7705	--	--	16.08	16.08	0.10	0.14	0.07	0.50	0.00	0.00	20.9
8	0	-0	-7891	0	0	0	7548	--	--	16.08	16.08	0.10	0.13	0.07	0.50	0.00	0.00	20.9
9	0	-0	-7862	0	0	0	7549	--	--	16.08	16.08	0.10	0.13	0.06	0.49	0.00	0.00	20.9
10	0	-0	-8159	0	0	0	7886	--	--	16.08	16.08	0.10	0.14	0.07	0.51	0.00	0.00	20.9
11	0	-0	-8151	0	0	0	7886	--	--	16.08	16.08	0.10	0.14	0.07	0.51	0.00	0.00	20.9
12	0	-0	-7731	0	0	0	7367	--	--	16.08	16.08	0.10	0.13	0.06	0.48	0.00	0.00	20.9
13	0	-0	-7722	0	0	0	7367	--	--	16.08	16.08	0.10	0.13	0.06	0.48	0.00	0.00	20.9
14	0	-0	-8019	0	0	0	7704	--	--	16.08	16.08	0.10	0.14	0.07	0.50	0.00	0.00	20.9
15	0	-0	-7991	0	0	0	7705	--	--	16.08	16.08	0.10	0.14	0.07	0.50	0.00	0.00	20.9
16	0	-0	-7891	0	0	0	7548	--	--	16.08	16.08	0.10	0.13	0.07	0.50	0.00	0.00	20.9
17	0	-0	-7862	0	0	0	7549	--	--	16.08	16.08	0.10	0.13	0.06	0.49	0.00	0.00	20.9
18	0	-0	-12070	0	0	0	11370	--	--	16.08	16.08	0.00	0.19	0.10	0.76	0.00	0.00	20.9
19	0	-0	-10870	0	0	0	9922	--	--	16.08	16.08	0.00	0.17	0.09	0.68	0.00	0.00	20.9
20	0	-0	-11330	0	0	0	10590	--	--	16.08	16.08	0.00	0.18	0.09	0.71	0.00	0.00	20.9
37	0	-0	-12030	0	0	0	11520	--	--	16.08	16.08	0.00	0.20	0.10	0.75	0.00	0.00	20.9
38	0	-0	-10020	0	0	0	9118	--	--	16.08	16.08	0.00	0.16	0.08	0.63	0.00	0.00	20.9
39	0	-0	-10790	0	0	0	10230	--	--	16.08	16.08	0.00	0.17	0.09	0.68	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	-10320	0	0	0	9915	--	--	16.08	16.08	0.00	0.17	0.09	0.65	0.00	0.00	20.9
2	26	-0	-8159	0	0	0	7886	--	--	16.08	16.08	0.10	0.14	0.07	0.51	0.00	0.00	20.9
3	26	-0	-8151	0	0	0	7886	--	--	16.08	16.08	0.10	0.14	0.07	0.51	0.00	0.00	20.9
4	26	-0	-7731	0	0	0	7367	--	--	16.08	16.08	0.10	0.13	0.06	0.48	0.00	0.00	20.9
5	26	-0	-7722	0	0	0	7367	--	--	16.08	16.08	0.10	0.13	0.06	0.48	0.00	0.00	20.9
6	26	-0	-8019	0	0	0	7704	--	--	16.08	16.08	0.10	0.14	0.07	0.50	0.00	0.00	20.9

7	26	-0	-7991	0	0	0	7705	--	--	16.08	16.08	0.10	0.14	0.07	0.50	0.00	0.00	20.9
8	26	-0	-7891	0	0	0	7548	--	--	16.08	16.08	0.10	0.13	0.07	0.50	0.00	0.00	20.9
9	26	-0	-7862	0	0	0	7549	--	--	16.08	16.08	0.10	0.13	0.06	0.49	0.00	0.00	20.9
10	26	-0	-8159	0	0	0	7886	--	--	16.08	16.08	0.10	0.14	0.07	0.51	0.00	0.00	20.9
11	26	-0	-8151	0	0	0	7886	--	--	16.08	16.08	0.10	0.14	0.07	0.51	0.00	0.00	20.9
12	26	-0	-7731	0	0	0	7367	--	--	16.08	16.08	0.10	0.13	0.06	0.48	0.00	0.00	20.9
13	26	-0	-7722	0	0	0	7367	--	--	16.08	16.08	0.10	0.13	0.06	0.48	0.00	0.00	20.9
14	26	-0	-8019	0	0	0	7704	--	--	16.08	16.08	0.10	0.14	0.07	0.50	0.00	0.00	20.9
15	26	-0	-7991	0	0	0	7705	--	--	16.08	16.08	0.10	0.14	0.07	0.50	0.00	0.00	20.9
16	26	-0	-7891	0	0	0	7548	--	--	16.08	16.08	0.10	0.13	0.07	0.50	0.00	0.00	20.9
17	26	-0	-7862	0	0	0	7549	--	--	16.08	16.08	0.10	0.13	0.06	0.49	0.00	0.00	20.9
18	26	-0	-12070	0	0	0	11370	--	--	16.08	16.08	0.00	0.19	0.10	0.76	0.00	0.00	20.9
19	26	-0	-10870	0	0	0	9922	--	--	16.08	16.08	0.00	0.17	0.09	0.68	0.00	0.00	20.9
20	26	-0	-11330	0	0	0	10590	--	--	16.08	16.08	0.00	0.18	0.09	0.71	0.00	0.00	20.9
37	26	-0	-12030	0	0	0	11520	--	--	16.08	16.08	0.00	0.20	0.10	0.75	0.00	0.00	20.9
38	26	-0	-10020	0	0	0	9118	--	--	16.08	16.08	0.00	0.16	0.08	0.63	0.00	0.00	20.9
39	26	-0	-10790	0	0	0	10230	--	--	16.08	16.08	0.00	0.17	0.09	0.68	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	-10320	0	0	0	4613	--	--	16.08	16.08	0.00	0.08	0.09	0.65	0.00	0.00	20.9
2	51	-0	-8159	0	0	0	3695	--	--	16.08	16.08	0.10	0.07	0.07	0.51	0.00	0.00	20.9
3	51	-0	-8151	0	0	0	3700	--	--	16.08	16.08	0.10	0.07	0.07	0.51	0.00	0.00	20.9
4	51	-0	-7731	0	0	0	3396	--	--	16.08	16.08	0.10	0.06	0.06	0.48	0.00	0.00	20.9
5	51	-0	-7722	0	0	0	3401	--	--	16.08	16.08	0.10	0.06	0.06	0.48	0.00	0.00	20.9
6	51	-0	-8019	0	0	0	3585	--	--	16.08	16.08	0.10	0.06	0.07	0.50	0.00	0.00	20.9
7	51	-0	-7991	0	0	0	3601	--	--	16.08	16.08	0.10	0.06	0.07	0.50	0.00	0.00	20.9
8	51	-0	-7891	0	0	0	3495	--	--	16.08	16.08	0.10	0.06	0.07	0.50	0.00	0.00	20.9
9	51	-0	-7862	0	0	0	3511	--	--	16.08	16.08	0.10	0.06	0.06	0.49	0.00	0.00	20.9
10	51	-0	-8159	0	0	0	3695	--	--	16.08	16.08	0.10	0.07	0.07	0.51	0.00	0.00	20.9
11	51	-0	-8151	0	0	0	3700	--	--	16.08	16.08	0.10	0.07	0.07	0.51	0.00	0.00	20.9
12	51	-0	-7731	0	0	0	3396	--	--	16.08	16.08	0.10	0.06	0.06	0.48	0.00	0.00	20.9
13	51	-0	-7722	0	0	0	3401	--	--	16.08	16.08	0.10	0.06	0.06	0.48	0.00	0.00	20.9
14	51	-0	-8019	0	0	0	3585	--	--	16.08	16.08	0.10	0.06	0.07	0.50	0.00	0.00	20.9
15	51	-0	-7991	0	0	0	3601	--	--	16.08	16.08	0.10	0.06	0.07	0.50	0.00	0.00	20.9
16	51	-0	-7891	0	0	0	3495	--	--	16.08	16.08	0.10	0.06	0.07	0.50	0.00	0.00	20.9
17	51	-0	-7862	0	0	0	3511	--	--	16.08	16.08	0.10	0.06	0.06	0.49	0.00	0.00	20.9
18	51	-0	-12070	0	0	0	5164	--	--	16.08	16.08	0.00	0.09	0.10	0.76	0.00	0.00	20.9
19	51	-0	-10870	0	0	0	4339	--	--	16.08	16.08	0.00	0.07	0.09	0.68	0.00	0.00	20.9
20	51	-0	-11330	0	0	0	4770	--	--	16.08	16.08	0.00	0.08	0.09	0.71	0.00	0.00	20.9
37	51	-0	-12030	0	0	0	5346	--	--	16.08	16.08	0.00	0.09	0.10	0.75	0.00	0.00	20.9
38	51	-0	-10020	0	0	0	3971	--	--	16.08	16.08	0.00	0.07	0.08	0.63	0.00	0.00	20.9
39	51	-0	-10790	0	0	0	4689	--	--	16.08	16.08	0.00	0.08	0.09	0.68	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 85 NI 1653 NF 1818 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-8509	0	0	0	4613	--	--	16.08	16.08	0.00	0.08	0.07	0.53	0.00	0.00	20.9
2	0	-0	-6773	0	0	0	3695	--	--	16.08	16.08	0.10	0.07	0.06	0.42	0.00	0.00	20.9
3	0	-0	-6766	0	0	0	3700	--	--	16.08	16.08	0.10	0.07	0.06	0.42	0.00	0.00	20.9
4	0	-0	-6325	0	0	0	3396	--	--	16.08	16.08	0.10	0.06	0.05	0.40	0.00	0.00	20.9
5	0	-0	-6317	0	0	0	3401	--	--	16.08	16.08	0.10	0.06	0.05	0.40	0.00	0.00	20.9
6	0	-0	-6625	0	0	0	3585	--	--	16.08	16.08	0.10	0.06	0.05	0.42	0.00	0.00	20.9
7	0	-0	-6600	0	0	0	3601	--	--	16.08	16.08	0.10	0.06	0.05	0.41	0.00	0.00	20.9
8	0	-0	-6490	0	0	0	3495	--	--	16.08	16.08	0.10	0.06	0.05	0.41	0.00	0.00	20.9
9	0	-0	-6466	0	0	0	3511	--	--	16.08	16.08	0.10	0.06	0.05	0.41	0.00	0.00	20.9
10	0	-0	-6773	0	0	0	3695	--	--	16.08	16.08	0.10	0.07	0.06	0.42	0.00	0.00	20.9
11	0	-0	-6766	0	0	0	3700	--	--	16.08	16.08	0.10	0.07	0.06	0.42	0.00	0.00	20.9
12	0	-0	-6325	0	0	0	3396	--	--	16.08	16.08	0.10	0.06	0.05	0.40	0.00	0.00	20.9
13	0	-0	-6317	0	0	0	3401	--	--	16.08	16.08	0.10	0.06	0.05	0.40	0.00	0.00	20.9
14	0	-0	-6625	0	0	0	3585	--	--	16.08	16.08	0.10	0.06	0.05	0.42	0.00	0.00	20.9
15	0	-0	-6600	0	0	0	3601	--	--	16.08	16.08	0.10	0.06	0.05	0.41	0.00	0.00	20.9
16	0	-0	-6490	0	0	0	3495	--	--	16.08	16.08	0.10	0.06	0.05	0.41	0.00	0.00	20.9
17	0	-0	-6466	0	0	0	3511	--	--	16.08	16.08	0.10	0.06	0.05	0.41	0.00	0.00	20.9
18	0	-0	-10140	0	0	0	5164	--	--	16.08	16.08	0.00	0.09	0.08	0.64	0.00	0.00	20.9
19	0	-0	-8836	0	0	0	4339	--	--	16.08	16.08	0.00	0.07	0.07	0.55	0.00	0.00	20.9
20	0	-0	-9369	0	0	0	4770	--	--	16.08	16.08	0.00	0.08	0.08	0.59	0.00	0.00	20.9
37	0	-0	-10200	0	0	0	5346	--	--	16.08	16.08	0.00	0.09	0.08	0.64	0.00	0.00	20.9
38	0	-0	-8021	0	0	0	3971	--	--	16.08	16.08	0.00	0.07	0.07	0.50	0.00	0.00	20.9
39	0	-0	-8910	0	0	0	4689	--	--	16.08	16.08	0.00	0.08	0.07	0.56	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	-8509	0	0	0	4613	--	--	16.08	16.08	0.00	0.08	0.07	0.53	0.00	0.00	20.9
2	26	-0	-6773	0	0	0	3695	--	--	16.08	16.08	0.10	0.07	0.06	0.42	0.00	0.00	20.9
3	26	-0	-6766	0	0	0	3700	--	--	16.08	16.08	0.10	0.07	0.06	0.42	0.00	0.00	20.9
4	26	-0	-6325	0	0	0	3396	--	--	16.08	16.08	0.10	0.06	0.05	0.40	0.00	0.00	20.9
5	26	-0	-6317	0	0	0	3401	--	--	16.08	16.08	0.10	0.06	0.05	0.40	0.00	0.00	20.9
6	26	-0	-6625	0	0	0	3585	--	--	16.08	16.08	0.10	0.06	0.05	0.42	0.00	0.00	20.9
7	26	-0	-6600	0	0	0	3601	--	--	16.08	16.08	0.10	0.06	0.05	0.41	0.00	0.00	20.9
8	26	-0	-6490	0	0	0	3495	--	--	16.08	16.08	0.10	0.06	0.05	0.41	0.00	0.00	20.9
9	26	-0	-6466	0	0	0	3511	--	--	16.08	16.08	0.10	0.06	0.05	0.41	0.00	0.00	20.9
10	26	-0	-6773	0	0	0	3695	--	--	16.08	16.08	0.10	0.07	0.06	0.42	0.00	0.00	20.9
11	26	-0	-6766	0	0	0	3700	--	--	16.08	16.08	0.10	0.07	0.06	0.42	0.00	0.00	20.9
12	26	-0	-6325	0	0	0	3396	--	--	16.08	16.08	0.10	0.06	0.05	0.40	0.00	0.00	20.9
13	26	-0	-6317	0	0	0	3401	--	--	16.08	16.08	0.10	0.06	0.05	0.40	0.00	0.00	20.9
14	26	-0	-6625	0	0	0	3585	--	--	16.08	16.08	0.10	0.06	0.05	0.42	0.00	0.00	20.9
15	26	-0	-6600	0	0	0	3601	--	--	16.08	16.08	0.10	0.06	0.05	0.41	0.00	0.00	20.9
16	26	-0	-6490	0	0	0	3495	--	--	16.08	16.08	0.10	0.06	0.05	0.41	0.00	0.00	20.9
17	26	-0	-6466	0	0	0	3511	--	--	16.08	16.08	0.10	0.06	0.05	0.41	0.00	0.00	20.9
18	26	-0	-10140	0	0	0	5164	--	--	16.08	16.08	0.00	0.09	0.08	0.64	0.00	0.00	20.9
19	26	-0	-8836	0	0	0	4339	--	--	16.08	16.08	0.00	0.07	0.07	0.55	0.00	0.00	20.9
20	26	-0	-9369	0	0	0	4770	--	--	16.08	16.08	0.00	0.08	0.08	0.59	0.00	0.00	20.9
37	26	-0	-10200	0	0	0	5346	--	--	16.08	16.08	0.00	0.09	0.08	0.64	0.00	0.00	20.9
38	26	-0	-8021	0	0	0	3971	--	--	16.08	16.08	0.00	0.07	0.07	0.50	0.00	0.00	20.9
39	26	-0	-8910	0	0	0	4689	--	--	16.08	16.08	0.00	0.08	0.07	0.56	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	-8509	0	0	0	242	--	--	16.08	16.08	0.00	0.00	0.07	0.53	0.00	0.00	20.9
2	51	-0	-6773	0	0	0	216	--	--	16.08	16.08	0.10	0.00	0.06	0.42	0.00	0.00	20.9

3	51	-0	-6766	0	0	0	225	--	--	16.08	16.08	0.10	0.00	0.06	0.42	0.00	0.00	20.9
4	51	-0	-6325	0	0	0	147	--	--	16.08	16.08	0.10	0.00	0.05	0.40	0.00	0.00	20.9
5	51	-0	-6317	0	0	0	156	--	--	16.08	16.08	0.10	0.00	0.05	0.40	0.00	0.00	20.9
6	51	-0	-6625	0	0	0	182	--	--	16.08	16.08	0.10	0.00	0.05	0.42	0.00	0.00	20.9
7	51	-0	-6600	0	0	0	211	--	--	16.08	16.08	0.10	0.00	0.05	0.41	0.00	0.00	20.9
8	51	-0	-6490	0	0	0	161	--	--	16.08	16.08	0.10	0.00	0.05	0.41	0.00	0.00	20.9
9	51	-0	-6466	0	0	0	190	--	--	16.08	16.08	0.10	0.00	0.05	0.41	0.00	0.00	20.9
10	51	-0	-6773	0	0	0	216	--	--	16.08	16.08	0.10	0.00	0.06	0.42	0.00	0.00	20.9
11	51	-0	-6766	0	0	0	225	--	--	16.08	16.08	0.10	0.00	0.06	0.42	0.00	0.00	20.9
12	51	-0	-6325	0	0	0	147	--	--	16.08	16.08	0.10	0.00	0.05	0.40	0.00	0.00	20.9
13	51	-0	-6317	0	0	0	156	--	--	16.08	16.08	0.10	0.00	0.05	0.40	0.00	0.00	20.9
14	51	-0	-6625	0	0	0	182	--	--	16.08	16.08	0.10	0.00	0.05	0.42	0.00	0.00	20.9
15	51	-0	-6600	0	0	0	211	--	--	16.08	16.08	0.10	0.00	0.05	0.41	0.00	0.00	20.9
16	51	-0	-6490	0	0	0	161	--	--	16.08	16.08	0.10	0.00	0.05	0.41	0.00	0.00	20.9
17	51	-0	-6466	0	0	0	190	--	--	16.08	16.08	0.10	0.00	0.05	0.41	0.00	0.00	20.9
18	51	-0	-10140	0	0	0	-45	--	--	16.08	16.08	0.18	0.00	0.08	0.64	0.00	0.00	20.9
19	51	-0	-8836	0	0	0	-199	--	--	16.08	16.08	0.18	0.00	0.07	0.55	0.00	0.00	20.9
20	51	-0	-9369	0	0	0	-43	--	--	16.08	16.08	0.18	0.00	0.08	0.59	0.00	0.00	20.9
37	51	-0	-10200	0	0	0	108	--	--	16.08	16.08	0.00	0.00	0.08	0.64	0.00	0.00	20.9
38	51	-0	-8021	0	0	0	-149	--	--	16.08	16.08	0.18	0.00	0.07	0.50	0.00	0.00	20.9
39	51	-0	-8910	0	0	0	112	--	--	16.08	16.08	0.00	0.00	0.07	0.56	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 86 NI 1818 NF 1817 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-6780	0	0	0	242	--	--	16.08	16.08	0.00	0.00	0.06	0.43	0.00	0.00	20.9
2	0	-0	-5448	0	0	0	216	--	--	16.08	16.08	0.10	0.00	0.04	0.34	0.00	0.00	20.9
3	0	-0	-5442	0	0	0	225	--	--	16.08	16.08	0.10	0.00	0.04	0.34	0.00	0.00	20.9
4	0	-0	-4988	0	0	0	147	--	--	16.08	16.08	0.10	0.00	0.04	0.31	0.00	0.00	20.9
5	0	-0	-4982	0	0	0	156	--	--	16.08	16.08	0.10	0.00	0.04	0.31	0.00	0.00	20.9
6	0	-0	-5294	0	0	0	182	--	--	16.08	16.08	0.10	0.00	0.04	0.33	0.00	0.00	20.9
7	0	-0	-5274	0	0	0	211	--	--	16.08	16.08	0.10	0.00	0.04	0.33	0.00	0.00	20.9
8	0	-0	-5156	0	0	0	161	--	--	16.08	16.08	0.10	0.00	0.04	0.32	0.00	0.00	20.9
9	0	-0	-5136	0	0	0	190	--	--	16.08	16.08	0.10	0.00	0.04	0.32	0.00	0.00	20.9
10	0	-0	-5448	0	0	0	216	--	--	16.08	16.08	0.10	0.00	0.04	0.34	0.00	0.00	20.9
11	0	-0	-5442	0	0	0	225	--	--	16.08	16.08	0.10	0.00	0.04	0.34	0.00	0.00	20.9
12	0	-0	-4988	0	0	0	147	--	--	16.08	16.08	0.10	0.00	0.04	0.31	0.00	0.00	20.9
13	0	-0	-4982	0	0	0	156	--	--	16.08	16.08	0.10	0.00	0.04	0.31	0.00	0.00	20.9
14	0	-0	-5294	0	0	0	182	--	--	16.08	16.08	0.10	0.00	0.04	0.33	0.00	0.00	20.9
15	0	-0	-5274	0	0	0	211	--	--	16.08	16.08	0.10	0.00	0.04	0.33	0.00	0.00	20.9
16	0	-0	-5156	0	0	0	161	--	--	16.08	16.08	0.10	0.00	0.04	0.32	0.00	0.00	20.9
17	0	-0	-5136	0	0	0	190	--	--	16.08	16.08	0.10	0.00	0.04	0.32	0.00	0.00	20.9
18	0	-0	-8292	0	0	0	-4303	--	--	16.08	16.08	0.18	0.07	0.07	0.52	0.00	0.00	20.9
19	0	-0	-6906	0	0	0	-3746	--	--	16.08	16.08	0.18	0.06	0.06	0.43	0.00	0.00	20.9
20	0	-0	-7498	0	0	0	-3894	--	--	16.08	16.08	0.18	0.06	0.06	0.47	0.00	0.00	20.9
37	0	-0	-8440	0	0	0	108	--	--	16.08	16.08	0.00	0.00	0.07	0.53	0.00	0.00	20.9
38	0	-0	-6130	0	0	0	-3298	--	--	16.08	16.08	0.18	0.05	0.05	0.38	0.00	0.00	20.9
39	0	-0	-7118	0	0	0	112	--	--	16.08	16.08	0.00	0.00	0.06	0.45	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	-6780	0	0	0	-3240	--	--	16.08	16.08	0.18	0.05	0.06	0.43	0.00	0.00	20.9
2	26	-0	-5448	0	0	0	-2582	--	--	16.08	16.08	0.29	0.04	0.04	0.34	0.00	0.00	20.9
3	26	-0	-5442	0	0	0	-2570	--	--	16.08	16.08	0.29	0.04	0.04	0.34	0.00	0.00	20.9
4	26	-0	-4988	0	0	0	-2415	--	--	16.08	16.08	0.29	0.04	0.04	0.31	0.00	0.00	20.9
5	26	-0	-4982	0	0	0	-2403	--	--	16.08	16.08	0.29	0.04	0.04	0.31	0.00	0.00	20.9
6	26	-0	-5294	0	0	0	-2537	--	--	16.08	16.08	0.29	0.04	0.04	0.33	0.00	0.00	20.9
7	26	-0	-5274	0	0	0	-2498	--	--	16.08	16.08	0.29	0.04	0.04	0.33	0.00	0.00	20.9
8	26	-0	-5156	0	0	0	-2487	--	--	16.08	16.08	0.29	0.04	0.04	0.32	0.00	0.00	20.9
9	26	-0	-5136	0	0	0	-2448	--	--	16.08	16.08	0.29	0.04	0.04	0.32	0.00	0.00	20.9
10	26	-0	-5448	0	0	0	-2582	--	--	16.08	16.08	0.29	0.04	0.04	0.34	0.00	0.00	20.9
11	26	-0	-5442	0	0	0	-2570	--	--	16.08	16.08	0.29	0.04	0.04	0.34	0.00	0.00	20.9
12	26	-0	-4988	0	0	0	-2415	--	--	16.08	16.08	0.29	0.04	0.04	0.31	0.00	0.00	20.9
13	26	-0	-4982	0	0	0	-2403	--	--	16.08	16.08	0.29	0.04	0.04	0.31	0.00	0.00	20.9
14	26	-0	-5294	0	0	0	-2537	--	--	16.08	16.08	0.29	0.04	0.04	0.33	0.00	0.00	20.9
15	26	-0	-5274	0	0	0	-2498	--	--	16.08	16.08	0.29	0.04	0.04	0.33	0.00	0.00	20.9
16	26	-0	-5156	0	0	0	-2487	--	--	16.08	16.08	0.29	0.04	0.04	0.32	0.00	0.00	20.9
17	26	-0	-5136	0	0	0	-2448	--	--	16.08	16.08	0.29	0.04	0.04	0.32	0.00	0.00	20.9
18	26	-0	-8292	0	0	0	-4303	--	--	16.08	16.08	0.18	0.07	0.07	0.52	0.00	0.00	20.9
19	26	-0	-6906	0	0	0	-3746	--	--	16.08	16.08	0.18	0.06	0.06	0.43	0.00	0.00	20.9
20	26	-0	-7498	0	0	0	-3894	--	--	16.08	16.08	0.18	0.06	0.06	0.47	0.00	0.00	20.9
37	26	-0	-8440	0	0	0	-4226	--	--	16.08	16.08	0.18	0.07	0.07	0.53	0.00	0.00	20.9
38	26	-0	-6130	0	0	0	-3298	--	--	16.08	16.08	0.18	0.05	0.05	0.38	0.00	0.00	20.9
39	26	-0	-7118	0	0	0	-3543	--	--	16.08	16.08	0.18	0.06	0.06	0.45	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	-6780	0	0	0	-3240	--	--	16.08	16.08	0.18	0.05	0.06	0.43	0.00	0.00	20.9
2	51	-0	-5448	0	0	0	-2582	--	--	16.08	16.08	0.29	0.04	0.04	0.34	0.00	0.00	20.9
3	51	-0	-5442	0	0	0	-2570	--	--	16.08	16.08	0.29	0.04	0.04	0.34	0.00	0.00	20.9
4	51	-0	-4988	0	0	0	-2415	--	--	16.08	16.08	0.29	0.04	0.04	0.31	0.00	0.00	20.9
5	51	-0	-4982	0	0	0	-2403	--	--	16.08	16.08	0.29	0.04	0.04	0.31	0.00	0.00	20.9
6	51	-0	-5294	0	0	0	-2537	--	--	16.08	16.08	0.29	0.04	0.04	0.33	0.00	0.00	20.9
7	51	-0	-5274	0	0	0	-2498	--	--	16.08	16.08	0.29	0.04	0.04	0.33	0.00	0.00	20.9
8	51	-0	-5156	0	0	0	-2487	--	--	16.08	16.08	0.29	0.04	0.04	0.32	0.00	0.00	20.9
9	51	-0	-5136	0	0	0	-2448	--	--	16.08	16.08	0.29	0.04	0.04	0.32	0.00	0.00	20.9
10	51	-0	-5448	0	0	0	-2582	--	--	16.08	16.08	0.29	0.04	0.04	0.34	0.00	0.00	20.9
11	51	-0	-5442	0	0	0	-2570	--	--	16.08	16.08	0.29	0.04	0.04	0.34	0.00	0.00	20.9
12	51	-0	-4988	0	0	0	-2415	--	--	16.08	16.08	0.29	0.04	0.04	0.31	0.00	0.00	20.9
13	51	-0	-4982	0	0	0	-2403	--	--	16.08	16.08	0.29	0.04	0.04	0.31	0.00	0.00	20.9
14	51	-0	-5294	0	0	0	-2537	--	--	16.08	16.08	0.29	0.04	0.04	0.33	0.00	0.00	20.9
15	51	-0	-5274	0	0	0	-2498	--	--	16.08	16.08	0.29	0.04	0.04	0.33	0.00	0.00	20.9
16	51	-0	-5156	0	0	0	-2487	--	--	16.08	16.08	0.29	0.04	0.04	0.32	0.00	0.00	20.9
17	51	-0	-5136	0	0	0	-2448	--	--	16.08	16.08	0.29	0.04	0.04	0.32	0.00	0.00	20.9
18	51	-0	-8292	0	0	0	-4303	--	--	16.08	16.08	0.18	0.07	0.07	0.52	0.00	0.00	20.9
19	51	-0	-6906	0	0	0	-3746	--	--	16.08	16.08	0.18	0.06	0.06	0.43	0.00	0.00	20.9
20	51	-0	-7498	0	0	0	-3894	--	--	16.08	16.08	0.18	0.06	0.06	0.47	0.00	0.00	20.9
37	51	-0	-8440	0	0	0	-4226	--	--	16.08	16.08	0.18	0.07	0.07	0.53	0.00	0.00	20.9
38	51	-0	-6130	0	0	0	-3298	--	--	16.08	16.08	0.18	0.05	0.05	0.38	0.00	0.00	20.9
39	51	-0	-7118	0	0	0	-3543	--	--	16.08	16.08	0.18	0.06	0.06	0.45	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 87 NI 1817 NF 1816 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-5133	0	0	0	-5876	--	--	16.08	16.08	0.18	0.10	0.04	0.32	0.00	0.00	20.9
2	0	-0	-4182	0	0	0	-4730	--	--	16.08	16.08	0.29	0.08	0.03	0.26	0.00	0.00	20.9
3	0	-0	-4177	0	0	0	-4716	--	--	16.08	16.08	0.29	0.08	0.03	0.26	0.00	0.00	20.9
4	0	-0	-3719	0	0	0	-4325	--	--	16.08	16.08	0.29	0.07	0.03	0.23	0.00	0.00	20.9
5	0	-0	-3714	0	0	0	-4310	--	--	16.08	16.08	0.29	0.07	0.03	0.23	0.00	0.00	20.9
6	0	-0	-4026	0	0	0	-4605	--	--	16.08	16.08	0.29	0.08	0.03	0.25	0.00	0.00	20.9
7	0	-0	-4009	0	0	0	-4557	--	--	16.08	16.08	0.29	0.08	0.03	0.25	0.00	0.00	20.9
8	0	-0	-3887	0	0	0	-4483	--	--	16.08	16.08	0.29	0.08	0.03	0.24	0.00	0.00	20.9
9	0	-0	-3870	0	0	0	-4436	--	--	16.08	16.08	0.29	0.08	0.03	0.24	0.00	0.00	20.9
10	0	-0	-4182	0	0	0	-4730	--	--	16.08	16.08	0.29	0.08	0.03	0.26	0.00	0.00	20.9
11	0	-0	-4177	0	0	0	-4716	--	--	16.08	16.08	0.29	0.08	0.03	0.26	0.00	0.00	20.9
12	0	-0	-3719	0	0	0	-4325	--	--	16.08	16.08	0.29	0.07	0.03	0.23	0.00	0.00	20.9
13	0	-0	-3714	0	0	0	-4310	--	--	16.08	16.08	0.29	0.07	0.03	0.23	0.00	0.00	20.9
14	0	-0	-4026	0	0	0	-4605	--	--	16.08	16.08	0.29	0.08	0.03	0.25	0.00	0.00	20.9
15	0	-0	-4009	0	0	0	-4557	--	--	16.08	16.08	0.29	0.08	0.03	0.25	0.00	0.00	20.9
16	0	-0	-3887	0	0	0	-4483	--	--	16.08	16.08	0.29	0.08	0.03	0.24	0.00	0.00	20.9
17	0	-0	-3870	0	0	0	-4436	--	--	16.08	16.08	0.29	0.08	0.03	0.24	0.00	0.00	20.9
18	0	-0	-6524	0	0	0	-7654	--	--	16.08	16.08	0.18	0.13	0.05	0.41	0.00	0.00	20.9
19	0	-0	-5075	0	0	0	-6353	--	--	16.08	16.08	0.18	0.11	0.04	0.32	0.00	0.00	20.9
20	0	-0	-5717	0	0	0	-6830	--	--	16.08	16.08	0.18	0.11	0.05	0.36	0.00	0.00	20.9
37	0	-0	-6755	0	0	0	-7695	--	--	16.08	16.08	0.18	0.13	0.06	0.42	0.00	0.00	20.9
38	0	-0	-4340	0	0	0	-5527	--	--	16.08	16.08	0.18	0.09	0.04	0.27	0.00	0.00	20.9
39	0	-0	-5410	0	0	0	-6322	--	--	16.08	16.08	0.18	0.10	0.04	0.34	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	26	-0	-5133	0	0	0	-5876	--	--	16.08	16.08	0.18	0.10	0.04	0.32	0.00	0.00	20.9
2	26	-0	-4182	0	0	0	-4730	--	--	16.08	16.08	0.29	0.08	0.03	0.26	0.00	0.00	20.9
3	26	-0	-4177	0	0	0	-4716	--	--	16.08	16.08	0.29	0.08	0.03	0.26	0.00	0.00	20.9
4	26	-0	-3719	0	0	0	-4325	--	--	16.08	16.08	0.29	0.07	0.03	0.23	0.00	0.00	20.9
5	26	-0	-3714	0	0	0	-4310	--	--	16.08	16.08	0.29	0.07	0.03	0.23	0.00	0.00	20.9
6	26	-0	-4026	0	0	0	-4605	--	--	16.08	16.08	0.29	0.08	0.03	0.25	0.00	0.00	20.9
7	26	-0	-4009	0	0	0	-4557	--	--	16.08	16.08	0.29	0.08	0.03	0.25	0.00	0.00	20.9
8	26	-0	-3887	0	0	0	-4483	--	--	16.08	16.08	0.29	0.08	0.03	0.24	0.00	0.00	20.9
9	26	-0	-3870	0	0	0	-4436	--	--	16.08	16.08	0.29	0.08	0.03	0.24	0.00	0.00	20.9
10	26	-0	-4182	0	0	0	-4730	--	--	16.08	16.08	0.29	0.08	0.03	0.26	0.00	0.00	20.9
11	26	-0	-4177	0	0	0	-4716	--	--	16.08	16.08	0.29	0.08	0.03	0.26	0.00	0.00	20.9
12	26	-0	-3719	0	0	0	-4325	--	--	16.08	16.08	0.29	0.07	0.03	0.23	0.00	0.00	20.9
13	26	-0	-3714	0	0	0	-4310	--	--	16.08	16.08	0.29	0.07	0.03	0.23	0.00	0.00	20.9
14	26	-0	-4026	0	0	0	-4605	--	--	16.08	16.08	0.29	0.08	0.03	0.25	0.00	0.00	20.9
15	26	-0	-4009	0	0	0	-4557	--	--	16.08	16.08	0.29	0.08	0.03	0.25	0.00	0.00	20.9
16	26	-0	-3887	0	0	0	-4483	--	--	16.08	16.08	0.29	0.08	0.03	0.24	0.00	0.00	20.9
17	26	-0	-3870	0	0	0	-4436	--	--	16.08	16.08	0.29	0.08	0.03	0.24	0.00	0.00	20.9
18	26	-0	-6524	0	0	0	-7654	--	--	16.08	16.08	0.18	0.13	0.05	0.41	0.00	0.00	20.9
19	26	-0	-5075	0	0	0	-6353	--	--	16.08	16.08	0.18	0.11	0.04	0.32	0.00	0.00	20.9
20	26	-0	-5717	0	0	0	-6830	--	--	16.08	16.08	0.18	0.11	0.05	0.36	0.00	0.00	20.9
37	26	-0	-6755	0	0	0	-7695	--	--	16.08	16.08	0.18	0.13	0.06	0.42	0.00	0.00	20.9
38	26	-0	-4340	0	0	0	-5527	--	--	16.08	16.08	0.18	0.09	0.04	0.27	0.00	0.00	20.9
39	26	-0	-5410	0	0	0	-6322	--	--	16.08	16.08	0.18	0.10	0.04	0.34	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	51	-0	-5133	0	0	0	-5876	--	--	16.08	16.08	0.18	0.10	0.04	0.32	0.00	0.00	20.9
2	51	-0	-4182	0	0	0	-4730	--	--	16.08	16.08	0.29	0.08	0.03	0.26	0.00	0.00	20.9
3	51	-0	-4177	0	0	0	-4716	--	--	16.08	16.08	0.29	0.08	0.03	0.26	0.00	0.00	20.9
4	51	-0	-3719	0	0	0	-4325	--	--	16.08	16.08	0.29	0.07	0.03	0.23	0.00	0.00	20.9
5	51	-0	-3714	0	0	0	-4310	--	--	16.08	16.08	0.29	0.07	0.03	0.23	0.00	0.00	20.9
6	51	-0	-4026	0	0	0	-4605	--	--	16.08	16.08	0.29	0.08	0.03	0.25	0.00	0.00	20.9
7	51	-0	-4009	0	0	0	-4557	--	--	16.08	16.08	0.29	0.08	0.03	0.25	0.00	0.00	20.9
8	51	-0	-3887	0	0	0	-4483	--	--	16.08	16.08	0.29	0.08	0.03	0.24	0.00	0.00	20.9
9	51	-0	-3870	0	0	0	-4436	--	--	16.08	16.08	0.29	0.08	0.03	0.24	0.00	0.00	20.9
10	51	-0	-4182	0	0	0	-4730	--	--	16.08	16.08	0.29	0.08	0.03	0.26	0.00	0.00	20.9
11	51	-0	-4177	0	0	0	-4716	--	--	16.08	16.08	0.29	0.08	0.03	0.26	0.00	0.00	20.9
12	51	-0	-3719	0	0	0	-4325	--	--	16.08	16.08	0.29	0.07	0.03	0.23	0.00	0.00	20.9
13	51	-0	-3714	0	0	0	-4310	--	--	16.08	16.08	0.29	0.07	0.03	0.23	0.00	0.00	20.9
14	51	-0	-4026	0	0	0	-4605	--	--	16.08	16.08	0.29	0.08	0.03	0.25	0.00	0.00	20.9
15	51	-0	-4009	0	0	0	-4557	--	--	16.08	16.08	0.29	0.08	0.03	0.25	0.00	0.00	20.9
16	51	-0	-3887	0	0	0	-4483	--	--	16.08	16.08	0.29	0.08	0.03	0.24	0.00	0.00	20.9
17	51	-0	-3870	0	0	0	-4436	--	--	16.08	16.08	0.29	0.08	0.03	0.24	0.00	0.00	20.9
18	51	-0	-6524	0	0	0	-7654	--	--	16.08	16.08	0.18	0.13	0.05	0.41	0.00	0.00	20.9
19	51	-0	-5075	0	0	0	-6353	--	--	16.08	16.08	0.18	0.11	0.04	0.32	0.00	0.00	20.9
20	51	-0	-5717	0	0	0	-6830	--	--	16.08	16.08	0.18	0.11	0.05	0.36	0.00	0.00	20.9
37	51	-0	-6755	0	0	0	-7695	--	--	16.08	16.08	0.18	0.13	0.06	0.42	0.00	0.00	20.9
38	51	-0	-4340	0	0	0	-5527	--	--	16.08	16.08	0.18	0.09	0.04	0.27	0.00	0.00	20.9
39	51	-0	-5410	0	0	0	-6322	--	--	16.08	16.08	0.18	0.10	0.04	0.34	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 88 NI 1816 NF 1835 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-3549	0	0	0	-7700	--	--	16.08	16.08	0.18	0.13	0.03	0.22	0.00	0.00	20.9
2	0	-0	-2961	0	0	0	-6251	--	--	16.08	16.08	0.29	0.11	0.02	0.19	0.00	0.00	20.9
3	0	-0	-2957	0	0	0	-6235	--	--	16.08	16.08	0.29	0.11	0.02	0.19	0.00	0.00	20.9
4	0	-0	-2503	0	0	0	-5610	--	--	16.08	16.08	0.29	0.10	0.02	0.16	0.00	0.00	20.9
5	0	-0	-2499	0	0	0	-5594	--	--	16.08	16.08	0.29	0.10	0.02	0.16	0.00	0.00	20.9
6	0	-0	-2805	0	0	0	-6046	--	--	16.08	16.08	0.29	0.10	0.02	0.18	0.00	0.00	20.9
7	0	-0	-2793	0	0	0	-5992	--	--	16.08	16.08	0.29	0.10	0.02	0.18	0.00	0.00	20.9
8	0	-0	-2667	0	0	0	-5853	--	--	16.08	16.08	0.29	0.10	0.02	0.17	0.00	0.00	20.9
9	0	-0	-2656	0	0	0	-5800	--	--	16.08	16.08	0.29	0.10	0.02	0.17	0.00	0.00	20.9
10	0	-0	-2961	0	0	0	-6251	--	--	16.08	16.08	0.29	0.11	0.02	0.19	0.00	0.00	20.9

11	0	-0	-2957	0	0	0	-6235	--	--	16.08	16.08	0.29	0.11	0.02	0.19	0.00	0.00	20.9
12	0	-0	-2503	0	0	0	-5610	--	--	16.08	16.08	0.29	0.10	0.02	0.16	0.00	0.00	20.9
13	0	-0	-2499	0	0	0	-5594	--	--	16.08	16.08	0.29	0.10	0.02	0.16	0.00	0.00	20.9
14	0	-0	-2805	0	0	0	-6046	--	--	16.08	16.08	0.29	0.10	0.02	0.18	0.00	0.00	20.9
15	0	-0	-2793	0	0	0	-5992	--	--	16.08	16.08	0.29	0.10	0.02	0.18	0.00	0.00	20.9
16	0	-0	-2667	0	0	0	-5853	--	--	16.08	16.08	0.29	0.10	0.02	0.17	0.00	0.00	20.9
17	0	-0	-2656	0	0	0	-5800	--	--	16.08	16.08	0.29	0.10	0.02	0.17	0.00	0.00	20.9
18	0	-0	-4813	0	0	0	-10130	--	--	16.08	16.08	0.18	0.17	0.04	0.30	0.00	0.00	20.9
19	0	-0	-3323	0	0	0	-8060	--	--	16.08	16.08	0.18	0.13	0.03	0.21	0.00	0.00	20.9
20	0	-0	-4004	0	0	0	-8887	--	--	16.08	16.08	0.18	0.15	0.03	0.25	0.00	0.00	20.9
37	0	-0	-5118	0	0	0	-10320	--	--	16.08	16.08	0.18	0.17	0.04	0.32	0.00	0.00	20.9
38	0	-0	-2634	0	0	0	-6880	--	--	16.08	16.08	0.18	0.11	0.02	0.17	0.00	0.00	20.9
39	0	-0	-3769	0	0	0	-8258	--	--	16.08	16.08	0.18	0.14	0.03	0.24	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	-3549	0	0	0	-7700	--	--	16.08	16.08	0.18	0.13	0.03	0.22	0.00	0.00	20.9
2	26	-0	-2961	0	0	0	-6251	--	--	16.08	16.08	0.29	0.11	0.02	0.19	0.00	0.00	20.9
3	26	-0	-2957	0	0	0	-6235	--	--	16.08	16.08	0.29	0.11	0.02	0.19	0.00	0.00	20.9
4	26	-0	-2503	0	0	0	-5610	--	--	16.08	16.08	0.29	0.10	0.02	0.16	0.00	0.00	20.9
5	26	-0	-2499	0	0	0	-5594	--	--	16.08	16.08	0.29	0.10	0.02	0.16	0.00	0.00	20.9
6	26	-0	-2805	0	0	0	-6046	--	--	16.08	16.08	0.29	0.10	0.02	0.18	0.00	0.00	20.9
7	26	-0	-2793	0	0	0	-5992	--	--	16.08	16.08	0.29	0.10	0.02	0.18	0.00	0.00	20.9
8	26	-0	-2667	0	0	0	-5853	--	--	16.08	16.08	0.29	0.10	0.02	0.17	0.00	0.00	20.9
9	26	-0	-2656	0	0	0	-5800	--	--	16.08	16.08	0.29	0.10	0.02	0.17	0.00	0.00	20.9
10	26	-0	-2961	0	0	0	-6251	--	--	16.08	16.08	0.29	0.11	0.02	0.19	0.00	0.00	20.9
11	26	-0	-2957	0	0	0	-6235	--	--	16.08	16.08	0.29	0.11	0.02	0.19	0.00	0.00	20.9
12	26	-0	-2503	0	0	0	-5610	--	--	16.08	16.08	0.29	0.10	0.02	0.16	0.00	0.00	20.9
13	26	-0	-2499	0	0	0	-5594	--	--	16.08	16.08	0.29	0.10	0.02	0.16	0.00	0.00	20.9
14	26	-0	-2805	0	0	0	-6046	--	--	16.08	16.08	0.29	0.10	0.02	0.18	0.00	0.00	20.9
15	26	-0	-2793	0	0	0	-5992	--	--	16.08	16.08	0.29	0.10	0.02	0.18	0.00	0.00	20.9
16	26	-0	-2667	0	0	0	-5853	--	--	16.08	16.08	0.29	0.10	0.02	0.17	0.00	0.00	20.9
17	26	-0	-2656	0	0	0	-5800	--	--	16.08	16.08	0.29	0.10	0.02	0.17	0.00	0.00	20.9
18	26	-0	-4813	0	0	0	-10130	--	--	16.08	16.08	0.18	0.17	0.04	0.30	0.00	0.00	20.9
19	26	-0	-3323	0	0	0	-8060	--	--	16.08	16.08	0.18	0.13	0.03	0.21	0.00	0.00	20.9
20	26	-0	-4004	0	0	0	-8887	--	--	16.08	16.08	0.18	0.15	0.03	0.25	0.00	0.00	20.9
37	26	-0	-5118	0	0	0	-10320	--	--	16.08	16.08	0.18	0.17	0.04	0.32	0.00	0.00	20.9
38	26	-0	-2634	0	0	0	-6880	--	--	16.08	16.08	0.18	0.11	0.02	0.17	0.00	0.00	20.9
39	26	-0	-3769	0	0	0	-8258	--	--	16.08	16.08	0.18	0.14	0.03	0.24	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	-3549	0	0	0	-7700	--	--	16.08	16.08	0.18	0.13	0.03	0.22	0.00	0.00	20.9
2	51	-0	-2961	0	0	0	-6251	--	--	16.08	16.08	0.29	0.11	0.02	0.19	0.00	0.00	20.9
3	51	-0	-2957	0	0	0	-6235	--	--	16.08	16.08	0.29	0.11	0.02	0.19	0.00	0.00	20.9
4	51	-0	-2503	0	0	0	-5610	--	--	16.08	16.08	0.29	0.10	0.02	0.16	0.00	0.00	20.9
5	51	-0	-2499	0	0	0	-5594	--	--	16.08	16.08	0.29	0.10	0.02	0.16	0.00	0.00	20.9
6	51	-0	-2805	0	0	0	-6046	--	--	16.08	16.08	0.29	0.10	0.02	0.18	0.00	0.00	20.9
7	51	-0	-2793	0	0	0	-5992	--	--	16.08	16.08	0.29	0.10	0.02	0.18	0.00	0.00	20.9
8	51	-0	-2667	0	0	0	-5853	--	--	16.08	16.08	0.29	0.10	0.02	0.17	0.00	0.00	20.9
9	51	-0	-2656	0	0	0	-5800	--	--	16.08	16.08	0.29	0.10	0.02	0.17	0.00	0.00	20.9
10	51	-0	-2961	0	0	0	-6251	--	--	16.08	16.08	0.29	0.11	0.02	0.19	0.00	0.00	20.9
11	51	-0	-2957	0	0	0	-6235	--	--	16.08	16.08	0.29	0.11	0.02	0.19	0.00	0.00	20.9
12	51	-0	-2503	0	0	0	-5610	--	--	16.08	16.08	0.29	0.10	0.02	0.16	0.00	0.00	20.9
13	51	-0	-2499	0	0	0	-5594	--	--	16.08	16.08	0.29	0.10	0.02	0.16	0.00	0.00	20.9
14	51	-0	-2805	0	0	0	-6046	--	--	16.08	16.08	0.29	0.10	0.02	0.18	0.00	0.00	20.9
15	51	-0	-2793	0	0	0	-5992	--	--	16.08	16.08	0.29	0.10	0.02	0.18	0.00	0.00	20.9
16	51	-0	-2667	0	0	0	-5853	--	--	16.08	16.08	0.29	0.10	0.02	0.17	0.00	0.00	20.9
17	51	-0	-2656	0	0	0	-5800	--	--	16.08	16.08	0.29	0.10	0.02	0.17	0.00	0.00	20.9
18	51	-0	-4813	0	0	0	-10130	--	--	16.08	16.08	0.18	0.17	0.04	0.30	0.00	0.00	20.9
19	51	-0	-3323	0	0	0	-8060	--	--	16.08	16.08	0.18	0.13	0.03	0.21	0.00	0.00	20.9
20	51	-0	-4004	0	0	0	-8887	--	--	16.08	16.08	0.18	0.15	0.03	0.25	0.00	0.00	20.9
37	51	-0	-5118	0	0	0	-10320	--	--	16.08	16.08	0.18	0.17	0.04	0.32	0.00	0.00	20.9
38	51	-0	-2634	0	0	0	-6880	--	--	16.08	16.08	0.18	0.11	0.02	0.17	0.00	0.00	20.9
39	51	-0	-3769	0	0	0	-8258	--	--	16.08	16.08	0.18	0.14	0.03	0.24	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 89 NI 1835 NF 1834 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-1999	0	0	0	-8726	--	--	16.08	16.08	0.18	0.14	0.02	0.13	0.00	0.00	20.9
2	0	-0	-1759	0	0	0	-7155	--	--	16.08	16.08	0.29	0.12	0.01	0.11	0.00	0.00	20.9
3	0	-0	-1757	0	0	0	-7138	--	--	16.08	16.08	0.29	0.12	0.01	0.11	0.00	0.00	20.9
4	0	-0	-1317	0	0	0	-6287	--	--	16.08	16.08	0.29	0.11	0.01	0.08	0.00	0.00	20.9
5	0	-0	-1315	0	0	0	-6270	--	--	16.08	16.08	0.29	0.11	0.01	0.08	0.00	0.00	20.9
6	0	-0	-1607	0	0	0	-6871	--	--	16.08	16.08	0.29	0.12	0.01	0.10	0.00	0.00	20.9
7	0	-0	-1600	0	0	0	-6814	--	--	16.08	16.08	0.29	0.12	0.01	0.10	0.00	0.00	20.9
8	0	-0	-1474	0	0	0	-6611	--	--	16.08	16.08	0.29	0.11	0.01	0.09	0.00	0.00	20.9
9	0	-0	-1468	0	0	0	-6554	--	--	16.08	16.08	0.29	0.11	0.01	0.09	0.00	0.00	20.9
10	0	-0	-1759	0	0	0	-7155	--	--	16.08	16.08	0.29	0.12	0.01	0.11	0.00	0.00	20.9
11	0	-0	-1757	0	0	0	-7138	--	--	16.08	16.08	0.29	0.12	0.01	0.11	0.00	0.00	20.9
12	0	-0	-1317	0	0	0	-6287	--	--	16.08	16.08	0.29	0.11	0.01	0.08	0.00	0.00	20.9
13	0	-0	-1315	0	0	0	-6270	--	--	16.08	16.08	0.29	0.11	0.01	0.08	0.00	0.00	20.9
14	0	-0	-1607	0	0	0	-6871	--	--	16.08	16.08	0.29	0.12	0.01	0.10	0.00	0.00	20.9
15	0	-0	-1600	0	0	0	-6814	--	--	16.08	16.08	0.29	0.12	0.01	0.10	0.00	0.00	20.9
16	0	-0	-1474	0	0	0	-6611	--	--	16.08	16.08	0.29	0.11	0.01	0.09	0.00	0.00	20.9
17	0	-0	-1468	0	0	0	-6554	--	--	16.08	16.08	0.29	0.11	0.01	0.09	0.00	0.00	20.9
18	0	-0	-3121	0	0	0	-11730	--	--	16.08	16.08	0.18	0.19	0.03	0.20	0.00	0.00	20.9
19	0	-0	-1616	0	0	0	-8890	--	--	16.08	16.08	0.18	0.15	0.01	0.10	0.00	0.00	20.9
20	0	-0	-2323	0	0	0	-10080	--	--	16.08	16.08	0.18	0.17	0.02	0.15	0.00	0.00	20.9
37	0	-0	-3489	0	0	0	-12120	--	--	16.08	16.08	0.18	0.20	0.03	0.22	0.00	0.00	20.9
38	0	-0	-981	0	0	0	-7384	--	--	16.08	16.08	0.18	0.12	0.01	0.06	0.00	0.00	20.9
39	0	-0	-2159	0	0	0	-9367	--	--	16.08	16.08	0.18	0.16	0.02	0.14	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	-1999	0	0	0	-8726	--	--	16.08	16.08	0.18	0.14	0.02	0.13	0.00	0.00	20.9
2	26	-0	-1759	0	0	0	-7155	--	--	16.08	16.08	0.29	0.12	0.01	0.11	0.00	0.00	20.9
3	26	-0	-1757	0	0	0	-7138	--	--	16.08	16.08	0.29	0.12	0.01	0.11	0.00	0.00	20.9
4	26	-0	-1317	0	0	0	-6287	--	--	16.08	16.08	0.29	0.11	0.01	0.08	0.00	0.00	20.9
5	26	-0	-1315	0	0	0	-6270	--	--	16.08	16.08	0.29	0.11	0.01	0.08	0.00	0.00	20.9
6	26	-0	-1607	0	0	0	-6871	--	--	16.08	16.08	0.29	0.12	0.01	0.10	0.00	0.00	20.9

7	26	-0	-1600	0	0	0	-6814	--	--	16.08	16.08	0.29	0.12	0.01	0.10	0.00	0.00	20.9
8	26	-0	-1474	0	0	0	-6611	--	--	16.08	16.08	0.29	0.11	0.01	0.09	0.00	0.00	20.9
9	26	-0	-1468	0	0	0	-6554	--	--	16.08	16.08	0.29	0.11	0.01	0.09	0.00	0.00	20.9
10	26	-0	-1759	0	0	0	-7155	--	--	16.08	16.08	0.29	0.12	0.01	0.11	0.00	0.00	20.9
11	26	-0	-1757	0	0	0	-7138	--	--	16.08	16.08	0.29	0.12	0.01	0.11	0.00	0.00	20.9
12	26	-0	-1317	0	0	0	-6287	--	--	16.08	16.08	0.29	0.11	0.01	0.08	0.00	0.00	20.9
13	26	-0	-1315	0	0	0	-6270	--	--	16.08	16.08	0.29	0.11	0.01	0.08	0.00	0.00	20.9
14	26	-0	-1607	0	0	0	-6871	--	--	16.08	16.08	0.29	0.12	0.01	0.10	0.00	0.00	20.9
15	26	-0	-1600	0	0	0	-6814	--	--	16.08	16.08	0.29	0.12	0.01	0.10	0.00	0.00	20.9
16	26	-0	-1474	0	0	0	-6611	--	--	16.08	16.08	0.29	0.11	0.01	0.09	0.00	0.00	20.9
17	26	-0	-1468	0	0	0	-6554	--	--	16.08	16.08	0.29	0.11	0.01	0.09	0.00	0.00	20.9
18	26	-0	-3121	0	0	0	-11730	--	--	16.08	16.08	0.18	0.19	0.03	0.20	0.00	0.00	20.9
19	26	-0	-1616	0	0	0	-8890	--	--	16.08	16.08	0.18	0.15	0.01	0.10	0.00	0.00	20.9
20	26	-0	-2323	0	0	0	-10080	--	--	16.08	16.08	0.18	0.17	0.02	0.15	0.00	0.00	20.9
37	26	-0	-3489	0	0	0	-12120	--	--	16.08	16.08	0.18	0.20	0.03	0.22	0.00	0.00	20.9
38	26	-0	-981	0	0	0	-7384	--	--	16.08	16.08	0.18	0.12	0.01	0.06	0.00	0.00	20.9
39	26	-0	-2159	0	0	0	-9367	--	--	16.08	16.08	0.18	0.16	0.02	0.14	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	-1999	0	0	0	-8726	--	--	16.08	16.08	0.18	0.14	0.02	0.13	0.00	0.00	20.9
2	51	-0	-1759	0	0	0	-7155	--	--	16.08	16.08	0.29	0.12	0.01	0.11	0.00	0.00	20.9
3	51	-0	-1757	0	0	0	-7138	--	--	16.08	16.08	0.29	0.12	0.01	0.11	0.00	0.00	20.9
4	51	-0	-1317	0	0	0	-6287	--	--	16.08	16.08	0.29	0.11	0.01	0.08	0.00	0.00	20.9
5	51	-0	-1315	0	0	0	-6270	--	--	16.08	16.08	0.29	0.11	0.01	0.08	0.00	0.00	20.9
6	51	-0	-1607	0	0	0	-6871	--	--	16.08	16.08	0.29	0.12	0.01	0.10	0.00	0.00	20.9
7	51	-0	-1600	0	0	0	-6814	--	--	16.08	16.08	0.29	0.12	0.01	0.10	0.00	0.00	20.9
8	51	-0	-1474	0	0	0	-6611	--	--	16.08	16.08	0.29	0.11	0.01	0.09	0.00	0.00	20.9
9	51	-0	-1468	0	0	0	-6554	--	--	16.08	16.08	0.29	0.11	0.01	0.09	0.00	0.00	20.9
10	51	-0	-1759	0	0	0	-7155	--	--	16.08	16.08	0.29	0.12	0.01	0.11	0.00	0.00	20.9
11	51	-0	-1757	0	0	0	-7138	--	--	16.08	16.08	0.29	0.12	0.01	0.11	0.00	0.00	20.9
12	51	-0	-1317	0	0	0	-6287	--	--	16.08	16.08	0.29	0.11	0.01	0.08	0.00	0.00	20.9
13	51	-0	-1315	0	0	0	-6270	--	--	16.08	16.08	0.29	0.11	0.01	0.08	0.00	0.00	20.9
14	51	-0	-1607	0	0	0	-6871	--	--	16.08	16.08	0.29	0.12	0.01	0.10	0.00	0.00	20.9
15	51	-0	-1600	0	0	0	-6814	--	--	16.08	16.08	0.29	0.12	0.01	0.10	0.00	0.00	20.9
16	51	-0	-1474	0	0	0	-6611	--	--	16.08	16.08	0.29	0.11	0.01	0.09	0.00	0.00	20.9
17	51	-0	-1468	0	0	0	-6554	--	--	16.08	16.08	0.29	0.11	0.01	0.09	0.00	0.00	20.9
18	51	-0	-3121	0	0	0	-11730	--	--	16.08	16.08	0.18	0.19	0.03	0.20	0.00	0.00	20.9
19	51	-0	-1616	0	0	0	-8890	--	--	16.08	16.08	0.18	0.15	0.01	0.10	0.00	0.00	20.9
20	51	-0	-2323	0	0	0	-10080	--	--	16.08	16.08	0.18	0.17	0.02	0.15	0.00	0.00	20.9
37	51	-0	-3489	0	0	0	-12120	--	--	16.08	16.08	0.18	0.20	0.03	0.22	0.00	0.00	20.9
38	51	-0	-981	0	0	0	-7384	--	--	16.08	16.08	0.18	0.12	0.01	0.06	0.00	0.00	20.9
39	51	-0	-2159	0	0	0	-9367	--	--	16.08	16.08	0.18	0.16	0.02	0.14	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 90 NI 1834 NF 1652 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-442	0	0	0	-8953	--	--	16.08	16.08	0.18	0.15	0.00	0.03	0.00	0.00	20.9
2	0	-0	-546	0	0	0	-7435	--	--	16.08	16.08	0.29	0.13	0.00	0.03	0.00	0.00	20.9
3	0	-0	-546	0	0	0	-7418	--	--	16.08	16.08	0.29	0.13	0.00	0.03	0.00	0.00	20.9
4	0	-0	-134	0	0	0	-6356	--	--	16.08	16.08	0.29	0.11	0.00	0.01	0.00	0.00	20.9
5	0	-0	-134	0	0	0	-6339	--	--	16.08	16.08	0.29	0.11	0.00	0.01	0.00	0.00	20.9
6	0	-0	-402	0	0	0	-7078	--	--	16.08	16.08	0.29	0.12	0.00	0.03	0.00	0.00	20.9
7	0	-0	-401	0	0	0	-7020	--	--	16.08	16.08	0.29	0.12	0.00	0.03	0.00	0.00	20.9
8	0	-0	-278	0	0	0	-6754	--	--	16.08	16.08	0.29	0.12	0.00	0.02	0.00	0.00	20.9
9	0	-0	-278	0	0	0	-6696	--	--	16.08	16.08	0.29	0.12	0.00	0.02	0.00	0.00	20.9
10	0	-0	-546	0	0	0	-7435	--	--	16.08	16.08	0.29	0.13	0.00	0.03	0.00	0.00	20.9
11	0	-0	-546	0	0	0	-7418	--	--	16.08	16.08	0.29	0.13	0.00	0.03	0.00	0.00	20.9
12	0	-0	-134	0	0	0	-6356	--	--	16.08	16.08	0.29	0.11	0.00	0.01	0.00	0.00	20.9
13	0	-0	-134	0	0	0	-6339	--	--	16.08	16.08	0.29	0.11	0.00	0.01	0.00	0.00	20.9
14	0	-0	-402	0	0	0	-7078	--	--	16.08	16.08	0.29	0.12	0.00	0.03	0.00	0.00	20.9
15	0	-0	-401	0	0	0	-7020	--	--	16.08	16.08	0.29	0.12	0.00	0.03	0.00	0.00	20.9
16	0	-0	-278	0	0	0	-6754	--	--	16.08	16.08	0.29	0.12	0.00	0.02	0.00	0.00	20.9
17	0	-0	-278	0	0	0	-6696	--	--	16.08	16.08	0.29	0.12	0.00	0.02	0.00	0.00	20.9
18	0	-0	-1396	0	0	0	-12450	--	--	16.08	16.08	0.18	0.21	0.01	0.09	0.00	0.00	20.9
19	0	-0	87	0	0	0	-8890	--	--	16.08	16.08	0.18	0.15	0.00	0.01	0.00	0.00	20.9
20	0	-0	-629	0	0	0	-10400	--	--	16.08	16.08	0.18	0.17	0.01	0.04	0.00	0.00	20.9
37	0	-0	-1819	0	0	0	-13050	--	--	16.08	16.08	0.18	0.22	0.01	0.11	0.00	0.00	20.9
38	0	-0	654	0	0	0	-7384	--	--	16.08	16.08	0.18	0.12	0.01	0.04	0.00	0.00	20.9
39	0	-0	-540	0	0	0	-9645	--	--	16.08	16.08	0.18	0.16	0.00	0.03	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	-442	0	0	0	-8953	--	--	16.08	16.08	0.18	0.15	0.00	0.03	0.00	0.00	20.9
2	26	-0	-546	0	0	0	-7435	--	--	16.08	16.08	0.29	0.13	0.00	0.03	0.00	0.00	20.9
3	26	-0	-546	0	0	0	-7418	--	--	16.08	16.08	0.29	0.13	0.00	0.03	0.00	0.00	20.9
4	26	-0	-134	0	0	0	-6356	--	--	16.08	16.08	0.29	0.11	0.00	0.01	0.00	0.00	20.9
5	26	-0	-134	0	0	0	-6339	--	--	16.08	16.08	0.29	0.11	0.00	0.01	0.00	0.00	20.9
6	26	-0	-402	0	0	0	-7078	--	--	16.08	16.08	0.29	0.12	0.00	0.03	0.00	0.00	20.9
7	26	-0	-401	0	0	0	-7020	--	--	16.08	16.08	0.29	0.12	0.00	0.03	0.00	0.00	20.9
8	26	-0	-278	0	0	0	-6754	--	--	16.08	16.08	0.29	0.12	0.00	0.02	0.00	0.00	20.9
9	26	-0	-278	0	0	0	-6696	--	--	16.08	16.08	0.29	0.12	0.00	0.02	0.00	0.00	20.9
10	26	-0	-546	0	0	0	-7435	--	--	16.08	16.08	0.29	0.13	0.00	0.03	0.00	0.00	20.9
11	26	-0	-546	0	0	0	-7418	--	--	16.08	16.08	0.29	0.13	0.00	0.03	0.00	0.00	20.9
12	26	-0	-134	0	0	0	-6356	--	--	16.08	16.08	0.29	0.11	0.00	0.01	0.00	0.00	20.9
13	26	-0	-134	0	0	0	-6339	--	--	16.08	16.08	0.29	0.11	0.00	0.01	0.00	0.00	20.9
14	26	-0	-402	0	0	0	-7078	--	--	16.08	16.08	0.29	0.12	0.00	0.03	0.00	0.00	20.9
15	26	-0	-401	0	0	0	-7020	--	--	16.08	16.08	0.29	0.12	0.00	0.03	0.00	0.00	20.9
16	26	-0	-278	0	0	0	-6754	--	--	16.08	16.08	0.29	0.12	0.00	0.02	0.00	0.00	20.9
17	26	-0	-278	0	0	0	-6696	--	--	16.08	16.08	0.29	0.12	0.00	0.02	0.00	0.00	20.9
18	26	-0	-1396	0	0	0	-12450	--	--	16.08	16.08	0.18	0.21	0.01	0.09	0.00	0.00	20.9
19	26	-0	87	0	0	0	-8890	--	--	16.08	16.08	0.18	0.15	0.00	0.01	0.00	0.00	20.9
20	26	-0	-629	0	0	0	-10400	--	--	16.08	16.08	0.18	0.17	0.01	0.04	0.00	0.00	20.9
37	26	-0	-1819	0	0	0	-13050	--	--	16.08	16.08	0.18	0.22	0.01	0.11	0.00	0.00	20.9
38	26	-0	654	0	0	0	-7384	--	--	16.08	16.08	0.18	0.12	0.01	0.04	0.00	0.00	20.9
39	26	-0	-540	0	0	0	-9645	--	--	16.08	16.08	0.18	0.16	0.00	0.03	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	-442	0	0	0	-8953	--	--	16.08	16.08	0.18	0.15	0.00	0.03	0.00	0.00	20.9
2	51	-0	-546	0	0	0	-7435	--	--	16.08	16.08	0.29	0.13	0.00	0.03	0.00	0.00	20.9

3	51	-0	-546	0	0	0	-7418	--	--	16.08	16.08	0.29	0.13	0.00	0.03	0.00	0.00	20.9
4	51	-0	-134	0	0	0	-6356	--	--	16.08	16.08	0.29	0.11	0.00	0.01	0.00	0.00	20.9
5	51	-0	-134	0	0	0	-6339	--	--	16.08	16.08	0.29	0.11	0.00	0.01	0.00	0.00	20.9
6	51	-0	-402	0	0	0	-7078	--	--	16.08	16.08	0.29	0.12	0.00	0.03	0.00	0.00	20.9
7	51	-0	-401	0	0	0	-7020	--	--	16.08	16.08	0.29	0.12	0.00	0.03	0.00	0.00	20.9
8	51	-0	-278	0	0	0	-6754	--	--	16.08	16.08	0.29	0.12	0.00	0.02	0.00	0.00	20.9
9	51	-0	-278	0	0	0	-6696	--	--	16.08	16.08	0.29	0.12	0.00	0.02	0.00	0.00	20.9
10	51	-0	-546	0	0	0	-7435	--	--	16.08	16.08	0.29	0.13	0.00	0.03	0.00	0.00	20.9
11	51	-0	-546	0	0	0	-7418	--	--	16.08	16.08	0.29	0.13	0.00	0.03	0.00	0.00	20.9
12	51	-0	-134	0	0	0	-6356	--	--	16.08	16.08	0.29	0.11	0.00	0.01	0.00	0.00	20.9
13	51	-0	-134	0	0	0	-6339	--	--	16.08	16.08	0.29	0.11	0.00	0.01	0.00	0.00	20.9
14	51	-0	-402	0	0	0	-7078	--	--	16.08	16.08	0.29	0.12	0.00	0.03	0.00	0.00	20.9
15	51	-0	-401	0	0	0	-7020	--	--	16.08	16.08	0.29	0.12	0.00	0.03	0.00	0.00	20.9
16	51	-0	-278	0	0	0	-6754	--	--	16.08	16.08	0.29	0.12	0.00	0.02	0.00	0.00	20.9
17	51	-0	-278	0	0	0	-6696	--	--	16.08	16.08	0.29	0.12	0.00	0.02	0.00	0.00	20.9
18	51	-0	-1396	0	0	0	-12450	--	--	16.08	16.08	0.18	0.21	0.01	0.09	0.00	0.00	20.9
19	51	-0	87	0	0	0	-8890	--	--	16.08	16.08	0.18	0.15	0.00	0.01	0.00	0.00	20.9
20	51	-0	-629	0	0	0	-10400	--	--	16.08	16.08	0.18	0.17	0.01	0.04	0.00	0.00	20.9
37	51	-0	-1819	0	0	0	-13050	--	--	16.08	16.08	0.18	0.22	0.01	0.11	0.00	0.00	20.9
38	51	-0	654	0	0	0	-7384	--	--	16.08	16.08	0.18	0.12	0.01	0.04	0.00	0.00	20.9
39	51	-0	-540	0	0	0	-9645	--	--	16.08	16.08	0.18	0.16	0.00	0.03	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 91 NI 1652 NF 1820 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	1165	0	0	0	-8953	--	--	16.08	16.08	0.18	0.15	0.01	0.07	0.00	0.00	20.9
2	0	-0	714	0	0	0	-7435	--	--	16.08	16.08	0.29	0.13	0.01	0.04	0.00	0.00	20.9
3	0	-0	712	0	0	0	-7418	--	--	16.08	16.08	0.29	0.13	0.01	0.04	0.00	0.00	20.9
4	0	-0	1080	0	0	0	-6356	--	--	16.08	16.08	0.29	0.11	0.01	0.07	0.00	0.00	20.9
5	0	-0	1078	0	0	0	-6339	--	--	16.08	16.08	0.29	0.11	0.01	0.07	0.00	0.00	20.9
6	0	-0	844	0	0	0	-7078	--	--	16.08	16.08	0.29	0.12	0.01	0.05	0.00	0.00	20.9
7	0	-0	838	0	0	0	-7020	--	--	16.08	16.08	0.29	0.12	0.01	0.05	0.00	0.00	20.9
8	0	-0	954	0	0	0	-6754	--	--	16.08	16.08	0.29	0.12	0.01	0.06	0.00	0.00	20.9
9	0	-0	948	0	0	0	-6696	--	--	16.08	16.08	0.29	0.12	0.01	0.06	0.00	0.00	20.9
10	0	-0	714	0	0	0	-7435	--	--	16.08	16.08	0.29	0.13	0.01	0.04	0.00	0.00	20.9
11	0	-0	712	0	0	0	-7418	--	--	16.08	16.08	0.29	0.13	0.01	0.04	0.00	0.00	20.9
12	0	-0	1080	0	0	0	-6356	--	--	16.08	16.08	0.29	0.11	0.01	0.07	0.00	0.00	20.9
13	0	-0	1078	0	0	0	-6339	--	--	16.08	16.08	0.29	0.11	0.01	0.07	0.00	0.00	20.9
14	0	-0	844	0	0	0	-7078	--	--	16.08	16.08	0.29	0.12	0.01	0.05	0.00	0.00	20.9
15	0	-0	838	0	0	0	-7020	--	--	16.08	16.08	0.29	0.12	0.01	0.05	0.00	0.00	20.9
16	0	-0	954	0	0	0	-6754	--	--	16.08	16.08	0.29	0.12	0.01	0.06	0.00	0.00	20.9
17	0	-0	948	0	0	0	-6696	--	--	16.08	16.08	0.29	0.12	0.01	0.06	0.00	0.00	20.9
18	0	-0	419	0	0	0	-12450	--	--	16.08	16.08	0.18	0.21	0.00	0.03	0.00	0.00	20.9
19	0	-0	1832	0	0	0	-8845	--	--	16.08	16.08	0.18	0.15	0.02	0.11	0.00	0.00	20.9
20	0	-0	1128	0	0	0	-10400	--	--	16.08	16.08	0.18	0.17	0.01	0.07	0.00	0.00	20.9
37	0	-0	-45	0	0	0	-13070	--	--	16.08	16.08	0.18	0.22	0.00	0.00	0.00	0.00	20.9
38	0	-0	2309	0	0	0	-7048	--	--	16.08	16.08	0.18	0.12	0.02	0.14	0.00	0.00	20.9
39	0	-0	1135	0	0	0	-9645	--	--	16.08	16.08	0.18	0.16	0.01	0.07	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	1165	0	0	0	-8953	--	--	16.08	16.08	0.18	0.15	0.01	0.07	0.00	0.00	20.9
2	26	-0	714	0	0	0	-7435	--	--	16.08	16.08	0.29	0.13	0.01	0.04	0.00	0.00	20.9
3	26	-0	712	0	0	0	-7418	--	--	16.08	16.08	0.29	0.13	0.01	0.04	0.00	0.00	20.9
4	26	-0	1080	0	0	0	-6356	--	--	16.08	16.08	0.29	0.11	0.01	0.07	0.00	0.00	20.9
5	26	-0	1078	0	0	0	-6339	--	--	16.08	16.08	0.29	0.11	0.01	0.07	0.00	0.00	20.9
6	26	-0	844	0	0	0	-7078	--	--	16.08	16.08	0.29	0.12	0.01	0.05	0.00	0.00	20.9
7	26	-0	838	0	0	0	-7020	--	--	16.08	16.08	0.29	0.12	0.01	0.05	0.00	0.00	20.9
8	26	-0	954	0	0	0	-6754	--	--	16.08	16.08	0.29	0.12	0.01	0.06	0.00	0.00	20.9
9	26	-0	948	0	0	0	-6696	--	--	16.08	16.08	0.29	0.12	0.01	0.06	0.00	0.00	20.9
10	26	-0	714	0	0	0	-7435	--	--	16.08	16.08	0.29	0.13	0.01	0.04	0.00	0.00	20.9
11	26	-0	712	0	0	0	-7418	--	--	16.08	16.08	0.29	0.13	0.01	0.04	0.00	0.00	20.9
12	26	-0	1080	0	0	0	-6356	--	--	16.08	16.08	0.29	0.11	0.01	0.07	0.00	0.00	20.9
13	26	-0	1078	0	0	0	-6339	--	--	16.08	16.08	0.29	0.11	0.01	0.07	0.00	0.00	20.9
14	26	-0	844	0	0	0	-7078	--	--	16.08	16.08	0.29	0.12	0.01	0.05	0.00	0.00	20.9
15	26	-0	838	0	0	0	-7020	--	--	16.08	16.08	0.29	0.12	0.01	0.05	0.00	0.00	20.9
16	26	-0	954	0	0	0	-6754	--	--	16.08	16.08	0.29	0.12	0.01	0.06	0.00	0.00	20.9
17	26	-0	948	0	0	0	-6696	--	--	16.08	16.08	0.29	0.12	0.01	0.06	0.00	0.00	20.9
18	26	-0	419	0	0	0	-12450	--	--	16.08	16.08	0.18	0.21	0.00	0.03	0.00	0.00	20.9
19	26	-0	1832	0	0	0	-8845	--	--	16.08	16.08	0.18	0.15	0.02	0.11	0.00	0.00	20.9
20	26	-0	1128	0	0	0	-10400	--	--	16.08	16.08	0.18	0.17	0.01	0.07	0.00	0.00	20.9
37	26	-0	-45	0	0	0	-13070	--	--	16.08	16.08	0.18	0.22	0.00	0.00	0.00	0.00	20.9
38	26	-0	2309	0	0	0	-7048	--	--	16.08	16.08	0.18	0.12	0.02	0.14	0.00	0.00	20.9
39	26	-0	1135	0	0	0	-9645	--	--	16.08	16.08	0.18	0.16	0.01	0.07	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	1165	0	0	0	-8953	--	--	16.08	16.08	0.18	0.15	0.01	0.07	0.00	0.00	20.9
2	51	-0	714	0	0	0	-7435	--	--	16.08	16.08	0.29	0.13	0.01	0.04	0.00	0.00	20.9
3	51	-0	712	0	0	0	-7418	--	--	16.08	16.08	0.29	0.13	0.01	0.04	0.00	0.00	20.9
4	51	-0	1080	0	0	0	-6356	--	--	16.08	16.08	0.29	0.11	0.01	0.07	0.00	0.00	20.9
5	51	-0	1078	0	0	0	-6339	--	--	16.08	16.08	0.29	0.11	0.01	0.07	0.00	0.00	20.9
6	51	-0	844	0	0	0	-7078	--	--	16.08	16.08	0.29	0.12	0.01	0.05	0.00	0.00	20.9
7	51	-0	838	0	0	0	-7020	--	--	16.08	16.08	0.29	0.12	0.01	0.05	0.00	0.00	20.9
8	51	-0	954	0	0	0	-6754	--	--	16.08	16.08	0.29	0.12	0.01	0.06	0.00	0.00	20.9
9	51	-0	948	0	0	0	-6696	--	--	16.08	16.08	0.29	0.12	0.01	0.06	0.00	0.00	20.9
10	51	-0	714	0	0	0	-7435	--	--	16.08	16.08	0.29	0.13	0.01	0.04	0.00	0.00	20.9
11	51	-0	712	0	0	0	-7418	--	--	16.08	16.08	0.29	0.13	0.01	0.04	0.00	0.00	20.9
12	51	-0	1080	0	0	0	-6356	--	--	16.08	16.08	0.29	0.11	0.01	0.07	0.00	0.00	20.9
13	51	-0	1078	0	0	0	-6339	--	--	16.08	16.08	0.29	0.11	0.01	0.07	0.00	0.00	20.9
14	51	-0	844	0	0	0	-7078	--	--	16.08	16.08	0.29	0.12	0.01	0.05	0.00	0.00	20.9
15	51	-0	838	0	0	0	-7020	--	--	16.08	16.08	0.29	0.12	0.01	0.05	0.00	0.00	20.9
16	51	-0	954	0	0	0	-6754	--	--	16.08	16.08	0.29	0.12	0.01	0.06	0.00	0.00	20.9
17	51	-0	948	0	0	0	-6696	--	--	16.08	16.08	0.29	0.12	0.01	0.06	0.00	0.00	20.9
18	51	-0	419	0	0	0	-12450	--	--	16.08	16.08	0.18	0.21	0.00	0.03	0.00	0.00	20.9
19	51	-0	1832	0	0	0	-8845	--	--	16.08	16.08	0.18	0.15	0.02	0.11	0.00	0.00	20.9
20	51	-0	1128	0	0	0	-10400	--	--	16.08	16.08	0.18	0.17	0.01	0.07	0.00	0.00	20.9
37	51	-0	-45	0	0	0	-13070	--	--	16.08	16.08	0.18	0.22	0.00	0.00	0.00	0.00	20.9
38	51	-0	2309	0	0	0	-7048	--	--	16.08	16.08	0.18	0.12	0.02	0.14	0.00	0.00	20.9
39	51	-0	1135	0	0	0	-9645	--	--	16.08	16.08	0.18	0.16	0.01	0.07	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 92 NI 1820 NF 1819 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	2867	0	0	0	-8355	--	--	16.08	16.08	0.18	0.14	0.02	0.18	0.00	0.00	20.9
2	0	-0	2060	0	0	0	-7068	--	--	16.08	16.08	0.29	0.12	0.02	0.13	0.00	0.00	20.9
3	0	-0	2055	0	0	0	-7052	--	--	16.08	16.08	0.29	0.12	0.02	0.13	0.00	0.00	20.9
4	0	-0	2355	0	0	0	-5801	--	--	16.08	16.08	0.29	0.10	0.02	0.15	0.00	0.00	20.9
5	0	-0	2351	0	0	0	-5785	--	--	16.08	16.08	0.29	0.10	0.02	0.15	0.00	0.00	20.9
6	0	-0	2168	0	0	0	-6644	--	--	16.08	16.08	0.29	0.12	0.02	0.14	0.00	0.00	20.9
7	0	-0	2153	0	0	0	-6590	--	--	16.08	16.08	0.29	0.11	0.02	0.14	0.00	0.00	20.9
8	0	-0	2257	0	0	0	-6264	--	--	16.08	16.08	0.29	0.11	0.02	0.14	0.00	0.00	20.9
9	0	-0	2242	0	0	0	-6210	--	--	16.08	16.08	0.29	0.11	0.02	0.14	0.00	0.00	20.9
10	0	-0	2060	0	0	0	-7068	--	--	16.08	16.08	0.29	0.12	0.02	0.13	0.00	0.00	20.9
11	0	-0	2055	0	0	0	-7052	--	--	16.08	16.08	0.29	0.12	0.02	0.13	0.00	0.00	20.9
12	0	-0	2355	0	0	0	-5801	--	--	16.08	16.08	0.29	0.10	0.02	0.15	0.00	0.00	20.9
13	0	-0	2351	0	0	0	-5785	--	--	16.08	16.08	0.29	0.10	0.02	0.15	0.00	0.00	20.9
14	0	-0	2168	0	0	0	-6644	--	--	16.08	16.08	0.29	0.12	0.02	0.14	0.00	0.00	20.9
15	0	-0	2153	0	0	0	-6590	--	--	16.08	16.08	0.29	0.11	0.02	0.14	0.00	0.00	20.9
16	0	-0	2257	0	0	0	-6264	--	--	16.08	16.08	0.29	0.11	0.02	0.14	0.00	0.00	20.9
17	0	-0	2242	0	0	0	-6210	--	--	16.08	16.08	0.29	0.11	0.02	0.14	0.00	0.00	20.9
18	0	-0	2387	0	0	0	-12230	--	--	16.08	16.08	0.18	0.20	0.02	0.15	0.00	0.00	20.9
19	0	-0	3662	0	0	0	-7904	--	--	16.08	16.08	0.18	0.13	0.03	0.23	0.00	0.00	20.9
20	0	-0	2999	0	0	0	-9824	--	--	16.08	16.08	0.18	0.16	0.02	0.19	0.00	0.00	20.9
37	0	-0	1894	0	0	0	-13070	--	--	16.08	16.08	0.18	0.22	0.02	0.12	0.00	0.00	20.9
38	0	-0	4019	0	0	0	-5862	--	--	16.08	16.08	0.18	0.10	0.03	0.25	0.00	0.00	20.9
39	0	-0	2915	0	0	0	-9062	--	--	16.08	16.08	0.18	0.15	0.02	0.18	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	26	-0	2867	0	0	0	-8355	--	--	16.08	16.08	0.18	0.14	0.02	0.18	0.00	0.00	20.9
2	26	-0	2060	0	0	0	-7068	--	--	16.08	16.08	0.29	0.12	0.02	0.13	0.00	0.00	20.9
3	26	-0	2055	0	0	0	-7052	--	--	16.08	16.08	0.29	0.12	0.02	0.13	0.00	0.00	20.9
4	26	-0	2355	0	0	0	-5801	--	--	16.08	16.08	0.29	0.10	0.02	0.15	0.00	0.00	20.9
5	26	-0	2351	0	0	0	-5785	--	--	16.08	16.08	0.29	0.10	0.02	0.15	0.00	0.00	20.9
6	26	-0	2168	0	0	0	-6644	--	--	16.08	16.08	0.29	0.12	0.02	0.14	0.00	0.00	20.9
7	26	-0	2153	0	0	0	-6590	--	--	16.08	16.08	0.29	0.11	0.02	0.14	0.00	0.00	20.9
8	26	-0	2257	0	0	0	-6264	--	--	16.08	16.08	0.29	0.11	0.02	0.14	0.00	0.00	20.9
9	26	-0	2242	0	0	0	-6210	--	--	16.08	16.08	0.29	0.11	0.02	0.14	0.00	0.00	20.9
10	26	-0	2060	0	0	0	-7068	--	--	16.08	16.08	0.29	0.12	0.02	0.13	0.00	0.00	20.9
11	26	-0	2055	0	0	0	-7052	--	--	16.08	16.08	0.29	0.12	0.02	0.13	0.00	0.00	20.9
12	26	-0	2355	0	0	0	-5801	--	--	16.08	16.08	0.29	0.10	0.02	0.15	0.00	0.00	20.9
13	26	-0	2351	0	0	0	-5785	--	--	16.08	16.08	0.29	0.10	0.02	0.15	0.00	0.00	20.9
14	26	-0	2168	0	0	0	-6644	--	--	16.08	16.08	0.29	0.12	0.02	0.14	0.00	0.00	20.9
15	26	-0	2153	0	0	0	-6590	--	--	16.08	16.08	0.29	0.11	0.02	0.14	0.00	0.00	20.9
16	26	-0	2257	0	0	0	-6264	--	--	16.08	16.08	0.29	0.11	0.02	0.14	0.00	0.00	20.9
17	26	-0	2242	0	0	0	-6210	--	--	16.08	16.08	0.29	0.11	0.02	0.14	0.00	0.00	20.9
18	26	-0	2387	0	0	0	-12230	--	--	16.08	16.08	0.18	0.20	0.02	0.15	0.00	0.00	20.9
19	26	-0	3662	0	0	0	-7904	--	--	16.08	16.08	0.18	0.13	0.03	0.23	0.00	0.00	20.9
20	26	-0	2999	0	0	0	-9824	--	--	16.08	16.08	0.18	0.16	0.02	0.19	0.00	0.00	20.9
37	26	-0	1894	0	0	0	-13070	--	--	16.08	16.08	0.18	0.22	0.02	0.12	0.00	0.00	20.9
38	26	-0	4019	0	0	0	-5862	--	--	16.08	16.08	0.18	0.10	0.03	0.25	0.00	0.00	20.9
39	26	-0	2915	0	0	0	-9062	--	--	16.08	16.08	0.18	0.15	0.02	0.18	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	51	-0	2867	0	0	0	-8355	--	--	16.08	16.08	0.18	0.14	0.02	0.18	0.00	0.00	20.9
2	51	-0	2060	0	0	0	-7068	--	--	16.08	16.08	0.29	0.12	0.02	0.13	0.00	0.00	20.9
3	51	-0	2055	0	0	0	-7052	--	--	16.08	16.08	0.29	0.12	0.02	0.13	0.00	0.00	20.9
4	51	-0	2355	0	0	0	-5801	--	--	16.08	16.08	0.29	0.10	0.02	0.15	0.00	0.00	20.9
5	51	-0	2351	0	0	0	-5785	--	--	16.08	16.08	0.29	0.10	0.02	0.15	0.00	0.00	20.9
6	51	-0	2168	0	0	0	-6644	--	--	16.08	16.08	0.29	0.12	0.02	0.14	0.00	0.00	20.9
7	51	-0	2153	0	0	0	-6590	--	--	16.08	16.08	0.29	0.11	0.02	0.14	0.00	0.00	20.9
8	51	-0	2257	0	0	0	-6264	--	--	16.08	16.08	0.29	0.11	0.02	0.14	0.00	0.00	20.9
9	51	-0	2242	0	0	0	-6210	--	--	16.08	16.08	0.29	0.11	0.02	0.14	0.00	0.00	20.9
10	51	-0	2060	0	0	0	-7068	--	--	16.08	16.08	0.29	0.12	0.02	0.13	0.00	0.00	20.9
11	51	-0	2055	0	0	0	-7052	--	--	16.08	16.08	0.29	0.12	0.02	0.13	0.00	0.00	20.9
12	51	-0	2355	0	0	0	-5801	--	--	16.08	16.08	0.29	0.10	0.02	0.15	0.00	0.00	20.9
13	51	-0	2351	0	0	0	-5785	--	--	16.08	16.08	0.29	0.10	0.02	0.15	0.00	0.00	20.9
14	51	-0	2168	0	0	0	-6644	--	--	16.08	16.08	0.29	0.12	0.02	0.14	0.00	0.00	20.9
15	51	-0	2153	0	0	0	-6590	--	--	16.08	16.08	0.29	0.11	0.02	0.14	0.00	0.00	20.9
16	51	-0	2257	0	0	0	-6264	--	--	16.08	16.08	0.29	0.11	0.02	0.14	0.00	0.00	20.9
17	51	-0	2242	0	0	0	-6210	--	--	16.08	16.08	0.29	0.11	0.02	0.14	0.00	0.00	20.9
18	51	-0	2387	0	0	0	-12230	--	--	16.08	16.08	0.18	0.20	0.02	0.15	0.00	0.00	20.9
19	51	-0	3662	0	0	0	-7904	--	--	16.08	16.08	0.18	0.13	0.03	0.23	0.00	0.00	20.9
20	51	-0	2999	0	0	0	-9824	--	--	16.08	16.08	0.18	0.16	0.02	0.19	0.00	0.00	20.9
37	51	-0	1894	0	0	0	-13070	--	--	16.08	16.08	0.18	0.22	0.02	0.12	0.00	0.00	20.9
38	51	-0	4019	0	0	0	-5862	--	--	16.08	16.08	0.18	0.10	0.03	0.25	0.00	0.00	20.9
39	51	-0	2915	0	0	0	-9062	--	--	16.08	16.08	0.18	0.15	0.02	0.18	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 93 NI 1819 NF 1836 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	4705	0	0	0	-6882	--	--	16.08	16.08	0.18	0.11	0.04	0.30	0.00	0.00	20.9
2	0	-0	3525	0	0	0	-6011	--	--	16.08	16.08	0.29	0.10	0.03	0.22	0.00	0.00	20.9
3	0	-0	3517	0	0	0	-5997	--	--	16.08	16.08	0.29	0.10	0.03	0.22	0.00	0.00	20.9
4	0	-0	3722	0	0	0	-4592	--	--	16.08	16.08	0.29	0.08	0.03	0.23	0.00	0.00	20.9
5	0	-0	3714	0	0	0	-4578	--	--	16.08	16.08	0.29	0.08	0.03	0.23	0.00	0.00	20.9
6	0	-0	3602	0	0	0	-5530	--	--	16.08	16.08	0.29	0.10	0.03	0.23	0.00	0.00	20.9
7	0	-0	3577	0	0	0	-5484	--	--	16.08	16.08	0.29	0.09	0.03	0.22	0.00	0.00	20.9
8	0	-0	3662	0	0	0	-5105	--	--	16.08	16.08	0.29	0.09	0.03	0.23	0.00	0.00	20.9
9	0	-0	3636	0	0	0	-5058	--	--	16.08	16.08	0.29	0.09	0.03	0.23	0.00	0.00	20.9
10	0	-0	3525	0	0	0	-6011	--	--	16.08	16.08	0.29	0.10	0.03	0.22	0.00	0.00	20.9

11	0	-0	3517	0	0	0	-5997	--	--	16.08	16.08	0.29	0.10	0.03	0.22	0.00	0.00	20.9
12	0	-0	3722	0	0	0	-4592	--	--	16.08	16.08	0.29	0.08	0.03	0.23	0.00	0.00	20.9
13	0	-0	3714	0	0	0	-4578	--	--	16.08	16.08	0.29	0.08	0.03	0.23	0.00	0.00	20.9
14	0	-0	3602	0	0	0	-5530	--	--	16.08	16.08	0.29	0.10	0.03	0.23	0.00	0.00	20.9
15	0	-0	3577	0	0	0	-5484	--	--	16.08	16.08	0.29	0.09	0.03	0.22	0.00	0.00	20.9
16	0	-0	3662	0	0	0	-5105	--	--	16.08	16.08	0.29	0.09	0.03	0.23	0.00	0.00	20.9
17	0	-0	3636	0	0	0	-5058	--	--	16.08	16.08	0.29	0.09	0.03	0.23	0.00	0.00	20.9
18	0	-0	4567	0	0	0	-11010	--	--	16.08	16.08	0.18	0.18	0.04	0.29	0.00	0.00	20.9
19	0	-0	5618	0	0	0	-6024	--	--	16.08	16.08	0.18	0.10	0.05	0.35	0.00	0.00	20.9
20	0	-0	5035	0	0	0	-8284	--	--	16.08	16.08	0.18	0.14	0.04	0.32	0.00	0.00	20.9
37	0	-0	4065	0	0	0	-12100	--	--	16.08	16.08	0.18	0.20	0.03	0.26	0.00	0.00	20.9
38	0	-0	5817	0	0	0	-3798	--	--	16.08	16.08	0.18	0.06	0.05	0.36	0.00	0.00	20.9
39	0	-0	4845	0	0	0	-7565	--	--	16.08	16.08	0.18	0.13	0.04	0.30	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	4705	0	0	0	-6882	--	--	16.08	16.08	0.18	0.11	0.04	0.30	0.00	0.00	20.9
2	26	-0	3525	0	0	0	-6011	--	--	16.08	16.08	0.29	0.10	0.03	0.22	0.00	0.00	20.9
3	26	-0	3517	0	0	0	-5997	--	--	16.08	16.08	0.29	0.10	0.03	0.22	0.00	0.00	20.9
4	26	-0	3722	0	0	0	-4592	--	--	16.08	16.08	0.29	0.08	0.03	0.23	0.00	0.00	20.9
5	26	-0	3714	0	0	0	-4578	--	--	16.08	16.08	0.29	0.08	0.03	0.23	0.00	0.00	20.9
6	26	-0	3602	0	0	0	-5530	--	--	16.08	16.08	0.29	0.10	0.03	0.23	0.00	0.00	20.9
7	26	-0	3577	0	0	0	-5484	--	--	16.08	16.08	0.29	0.09	0.03	0.22	0.00	0.00	20.9
8	26	-0	3662	0	0	0	-5105	--	--	16.08	16.08	0.29	0.09	0.03	0.23	0.00	0.00	20.9
9	26	-0	3636	0	0	0	-5058	--	--	16.08	16.08	0.29	0.09	0.03	0.23	0.00	0.00	20.9
10	26	-0	3525	0	0	0	-6011	--	--	16.08	16.08	0.29	0.10	0.03	0.22	0.00	0.00	20.9
11	26	-0	3517	0	0	0	-5997	--	--	16.08	16.08	0.29	0.10	0.03	0.22	0.00	0.00	20.9
12	26	-0	3722	0	0	0	-4592	--	--	16.08	16.08	0.29	0.08	0.03	0.23	0.00	0.00	20.9
13	26	-0	3714	0	0	0	-4578	--	--	16.08	16.08	0.29	0.08	0.03	0.23	0.00	0.00	20.9
14	26	-0	3602	0	0	0	-5530	--	--	16.08	16.08	0.29	0.10	0.03	0.23	0.00	0.00	20.9
15	26	-0	3577	0	0	0	-5484	--	--	16.08	16.08	0.29	0.09	0.03	0.22	0.00	0.00	20.9
16	26	-0	3662	0	0	0	-5105	--	--	16.08	16.08	0.29	0.09	0.03	0.23	0.00	0.00	20.9
17	26	-0	3636	0	0	0	-5058	--	--	16.08	16.08	0.29	0.09	0.03	0.23	0.00	0.00	20.9
18	26	-0	4567	0	0	0	-11010	--	--	16.08	16.08	0.18	0.18	0.04	0.29	0.00	0.00	20.9
19	26	-0	5618	0	0	0	-6024	--	--	16.08	16.08	0.18	0.10	0.05	0.35	0.00	0.00	20.9
20	26	-0	5035	0	0	0	-8284	--	--	16.08	16.08	0.18	0.14	0.04	0.32	0.00	0.00	20.9
37	26	-0	4065	0	0	0	-12100	--	--	16.08	16.08	0.18	0.20	0.03	0.26	0.00	0.00	20.9
38	26	-0	5817	0	0	0	-3798	--	--	16.08	16.08	0.18	0.06	0.05	0.36	0.00	0.00	20.9
39	26	-0	4845	0	0	0	-7565	--	--	16.08	16.08	0.18	0.13	0.04	0.30	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	4705	0	0	0	-6882	--	--	16.08	16.08	0.18	0.11	0.04	0.30	0.00	0.00	20.9
2	51	-0	3525	0	0	0	-6011	--	--	16.08	16.08	0.29	0.10	0.03	0.22	0.00	0.00	20.9
3	51	-0	3517	0	0	0	-5997	--	--	16.08	16.08	0.29	0.10	0.03	0.22	0.00	0.00	20.9
4	51	-0	3722	0	0	0	-4592	--	--	16.08	16.08	0.29	0.08	0.03	0.23	0.00	0.00	20.9
5	51	-0	3714	0	0	0	-4578	--	--	16.08	16.08	0.29	0.08	0.03	0.23	0.00	0.00	20.9
6	51	-0	3602	0	0	0	-5530	--	--	16.08	16.08	0.29	0.10	0.03	0.23	0.00	0.00	20.9
7	51	-0	3577	0	0	0	-5484	--	--	16.08	16.08	0.29	0.09	0.03	0.22	0.00	0.00	20.9
8	51	-0	3662	0	0	0	-5105	--	--	16.08	16.08	0.29	0.09	0.03	0.23	0.00	0.00	20.9
9	51	-0	3636	0	0	0	-5058	--	--	16.08	16.08	0.29	0.09	0.03	0.23	0.00	0.00	20.9
10	51	-0	3525	0	0	0	-6011	--	--	16.08	16.08	0.29	0.10	0.03	0.22	0.00	0.00	20.9
11	51	-0	3517	0	0	0	-5997	--	--	16.08	16.08	0.29	0.10	0.03	0.22	0.00	0.00	20.9
12	51	-0	3722	0	0	0	-4592	--	--	16.08	16.08	0.29	0.08	0.03	0.23	0.00	0.00	20.9
13	51	-0	3714	0	0	0	-4578	--	--	16.08	16.08	0.29	0.08	0.03	0.23	0.00	0.00	20.9
14	51	-0	3602	0	0	0	-5530	--	--	16.08	16.08	0.29	0.10	0.03	0.23	0.00	0.00	20.9
15	51	-0	3577	0	0	0	-5484	--	--	16.08	16.08	0.29	0.09	0.03	0.22	0.00	0.00	20.9
16	51	-0	3662	0	0	0	-5105	--	--	16.08	16.08	0.29	0.09	0.03	0.23	0.00	0.00	20.9
17	51	-0	3636	0	0	0	-5058	--	--	16.08	16.08	0.29	0.09	0.03	0.23	0.00	0.00	20.9
18	51	-0	4567	0	0	0	-11010	--	--	16.08	16.08	0.18	0.18	0.04	0.29	0.00	0.00	20.9
19	51	-0	5618	0	0	0	-6024	--	--	16.08	16.08	0.18	0.10	0.05	0.35	0.00	0.00	20.9
20	51	-0	5035	0	0	0	-8284	--	--	16.08	16.08	0.18	0.14	0.04	0.32	0.00	0.00	20.9
37	51	-0	4065	0	0	0	-12100	--	--	16.08	16.08	0.18	0.20	0.03	0.26	0.00	0.00	20.9
38	51	-0	5817	0	0	0	-3798	--	--	16.08	16.08	0.18	0.06	0.05	0.36	0.00	0.00	20.9
39	51	-0	4845	0	0	0	-7565	--	--	16.08	16.08	0.18	0.13	0.04	0.30	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 94 NI 1836 NF 1799 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	6717	0	0	0	-4465	--	--	16.08	16.08	0.18	0.07	0.06	0.42	0.00	0.00	20.9
2	0	-0	5141	0	0	0	-4200	--	--	16.08	16.08	0.29	0.07	0.04	0.32	0.00	0.00	20.9
3	0	-0	5130	0	0	0	-4190	--	--	16.08	16.08	0.29	0.07	0.04	0.32	0.00	0.00	20.9
4	0	-0	5204	0	0	0	-2680	--	--	16.08	16.08	0.29	0.05	0.04	0.33	0.00	0.00	20.9
5	0	-0	5193	0	0	0	-2670	--	--	16.08	16.08	0.29	0.05	0.04	0.33	0.00	0.00	20.9
6	0	-0	5176	0	0	0	-3680	--	--	16.08	16.08	0.29	0.06	0.04	0.32	0.00	0.00	20.9
7	0	-0	5139	0	0	0	-3646	--	--	16.08	16.08	0.29	0.06	0.04	0.32	0.00	0.00	20.9
8	0	-0	5195	0	0	0	-3224	--	--	16.08	16.08	0.29	0.06	0.04	0.33	0.00	0.00	20.9
9	0	-0	5158	0	0	0	-3190	--	--	16.08	16.08	0.29	0.06	0.04	0.32	0.00	0.00	20.9
10	0	-0	5141	0	0	0	-4200	--	--	16.08	16.08	0.29	0.07	0.04	0.32	0.00	0.00	20.9
11	0	-0	5130	0	0	0	-4190	--	--	16.08	16.08	0.29	0.07	0.04	0.32	0.00	0.00	20.9
12	0	-0	5204	0	0	0	-2680	--	--	16.08	16.08	0.29	0.05	0.04	0.33	0.00	0.00	20.9
13	0	-0	5193	0	0	0	-2670	--	--	16.08	16.08	0.29	0.05	0.04	0.33	0.00	0.00	20.9
14	0	-0	5176	0	0	0	-3680	--	--	16.08	16.08	0.29	0.06	0.04	0.32	0.00	0.00	20.9
15	0	-0	5139	0	0	0	-3646	--	--	16.08	16.08	0.29	0.06	0.04	0.32	0.00	0.00	20.9
16	0	-0	5195	0	0	0	-3224	--	--	16.08	16.08	0.29	0.06	0.04	0.33	0.00	0.00	20.9
17	0	-0	5158	0	0	0	-3190	--	--	16.08	16.08	0.29	0.06	0.04	0.32	0.00	0.00	20.9
18	0	-0	7016	0	0	0	-8659	--	--	16.08	16.08	0.18	0.14	0.06	0.44	0.00	0.00	20.9
19	0	-0	7733	0	0	0	-3137	--	--	16.08	16.08	0.18	0.05	0.06	0.49	0.00	0.00	20.9
20	0	-0	7278	0	0	0	-5697	--	--	16.08	16.08	0.18	0.09	0.06	0.46	0.00	0.00	20.9
37	0	-0	6527	0	0	0	-10010	--	--	16.08	16.08	0.18	0.17	0.05	0.41	0.00	0.00	20.9
38	0	-0	7722	0	0	0	-810	--	--	16.08	16.08	0.18	0.01	0.06	0.48	0.00	0.00	20.9
39	0	-0	6964	0	0	0	-5076	--	--	16.08	16.08	0.18	0.08	0.06	0.44	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	6717	0	0	0	-4465	--	--	16.08	16.08	0.18	0.07	0.06	0.42	0.00	0.00	20.9
2	26	-0	5141	0	0	0	-4200	--	--	16.08	16.08	0.29	0.07	0.04	0.32	0.00	0.00	20.9
3	26	-0	5130	0	0	0	-4190	--	--	16.08	16.08	0.29	0.07	0.04	0.32	0.00	0.00	20.9
4	26	-0	5204	0	0	0	-2680	--	--	16.08	16.08	0.29	0.05	0.04	0.33	0.00	0.00	20.9
5	26	-0	5193	0	0	0	-2670	--	--	16.08	16.08	0.29	0.05	0.04	0.33	0.00	0.00	20.9
6	26	-0	5176	0	0	0	-3680	--	--	16.08	16.08	0.29	0.06	0.04	0.32	0.00	0.00	20.9

7	26	-0	5139	0	0	0	-3646	--	--	16.08	16.08	0.29	0.06	0.04	0.32	0.00	0.00	20.9
8	26	-0	5195	0	0	0	-3224	--	--	16.08	16.08	0.29	0.06	0.04	0.33	0.00	0.00	20.9
9	26	-0	5158	0	0	0	-3190	--	--	16.08	16.08	0.29	0.06	0.04	0.32	0.00	0.00	20.9
10	26	-0	5141	0	0	0	-4200	--	--	16.08	16.08	0.29	0.07	0.04	0.32	0.00	0.00	20.9
11	26	-0	5130	0	0	0	-4190	--	--	16.08	16.08	0.29	0.07	0.04	0.32	0.00	0.00	20.9
12	26	-0	5204	0	0	0	-2680	--	--	16.08	16.08	0.29	0.05	0.04	0.33	0.00	0.00	20.9
13	26	-0	5193	0	0	0	-2670	--	--	16.08	16.08	0.29	0.05	0.04	0.33	0.00	0.00	20.9
14	26	-0	5176	0	0	0	-3680	--	--	16.08	16.08	0.29	0.06	0.04	0.32	0.00	0.00	20.9
15	26	-0	5139	0	0	0	-3646	--	--	16.08	16.08	0.29	0.06	0.04	0.32	0.00	0.00	20.9
16	26	-0	5195	0	0	0	-3224	--	--	16.08	16.08	0.29	0.06	0.04	0.33	0.00	0.00	20.9
17	26	-0	5158	0	0	0	-3190	--	--	16.08	16.08	0.29	0.06	0.04	0.32	0.00	0.00	20.9
18	26	-0	7016	0	0	0	-8659	--	--	16.08	16.08	0.18	0.14	0.06	0.44	0.00	0.00	20.9
19	26	-0	7733	0	0	0	-3137	--	--	16.08	16.08	0.18	0.05	0.06	0.49	0.00	0.00	20.9
20	26	-0	7278	0	0	0	-5697	--	--	16.08	16.08	0.18	0.09	0.06	0.46	0.00	0.00	20.9
37	26	-0	6527	0	0	0	-10010	--	--	16.08	16.08	0.18	0.17	0.05	0.41	0.00	0.00	20.9
38	26	-0	7722	0	0	0	9426	--	--	16.08	16.08	0.00	0.16	0.06	0.48	0.00	0.00	20.9
39	26	-0	6964	0	0	0	-5076	--	--	16.08	16.08	0.18	0.08	0.06	0.44	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	6717	0	0	0	-4465	--	--	16.08	16.08	0.18	0.07	0.06	0.42	0.00	0.00	20.9
2	51	-0	5141	0	0	0	-4200	--	--	16.08	16.08	0.29	0.07	0.04	0.32	0.00	0.00	20.9
3	51	-0	5130	0	0	0	-4190	--	--	16.08	16.08	0.29	0.07	0.04	0.32	0.00	0.00	20.9
4	51	-0	5204	0	0	0	-2680	--	--	16.08	16.08	0.29	0.05	0.04	0.33	0.00	0.00	20.9
5	51	-0	5193	0	0	0	-2670	--	--	16.08	16.08	0.29	0.05	0.04	0.33	0.00	0.00	20.9
6	51	-0	5176	0	0	0	-3680	--	--	16.08	16.08	0.29	0.06	0.04	0.32	0.00	0.00	20.9
7	51	-0	5139	0	0	0	-3646	--	--	16.08	16.08	0.29	0.06	0.04	0.32	0.00	0.00	20.9
8	51	-0	5195	0	0	0	-3224	--	--	16.08	16.08	0.29	0.06	0.04	0.33	0.00	0.00	20.9
9	51	-0	5158	0	0	0	-3190	--	--	16.08	16.08	0.29	0.06	0.04	0.32	0.00	0.00	20.9
10	51	-0	5141	0	0	0	-4200	--	--	16.08	16.08	0.29	0.07	0.04	0.32	0.00	0.00	20.9
11	51	-0	5130	0	0	0	-4190	--	--	16.08	16.08	0.29	0.07	0.04	0.32	0.00	0.00	20.9
12	51	-0	5204	0	0	0	-2680	--	--	16.08	16.08	0.29	0.05	0.04	0.33	0.00	0.00	20.9
13	51	-0	5193	0	0	0	-2670	--	--	16.08	16.08	0.29	0.05	0.04	0.33	0.00	0.00	20.9
14	51	-0	5176	0	0	0	-3680	--	--	16.08	16.08	0.29	0.06	0.04	0.32	0.00	0.00	20.9
15	51	-0	5139	0	0	0	-3646	--	--	16.08	16.08	0.29	0.06	0.04	0.32	0.00	0.00	20.9
16	51	-0	5195	0	0	0	-3224	--	--	16.08	16.08	0.29	0.06	0.04	0.33	0.00	0.00	20.9
17	51	-0	5158	0	0	0	-3190	--	--	16.08	16.08	0.29	0.06	0.04	0.32	0.00	0.00	20.9
18	51	-0	7016	0	0	0	-8659	--	--	16.08	16.08	0.18	0.14	0.06	0.44	0.00	0.00	20.9
19	51	-0	7733	0	0	0	834	--	--	16.08	16.08	0.00	0.01	0.06	0.49	0.00	0.00	20.9
20	51	-0	7278	0	0	0	-5697	--	--	16.08	16.08	0.18	0.09	0.06	0.46	0.00	0.00	20.9
37	51	-0	6527	0	0	0	-10010	--	--	16.08	16.08	0.18	0.17	0.05	0.41	0.00	0.00	20.9
38	51	-0	7722	0	0	0	3156	--	--	16.08	16.08	0.00	0.05	0.06	0.48	0.00	0.00	20.9
39	51	-0	6964	0	0	0	-5076	--	--	16.08	16.08	0.18	0.08	0.06	0.44	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 95 NI 1265 NF 1263 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-5450	0	0	0	3123	--	--	16.08	16.08	0.00	0.05	0.04	0.34	0.00	0.00	20.9
2	0	-0	-4342	0	0	0	3264	--	--	16.08	16.08	0.10	0.06	0.04	0.27	0.00	0.00	20.9
3	0	-0	-4403	0	0	0	3298	--	--	16.08	16.08	0.10	0.06	0.04	0.28	0.00	0.00	20.9
4	0	-0	-3982	0	0	0	1507	--	--	16.08	16.08	0.10	0.03	0.03	0.25	0.00	0.00	20.9
5	0	-0	-4043	0	0	0	1541	--	--	16.08	16.08	0.10	0.03	0.03	0.25	0.00	0.00	20.9
6	0	-0	-4145	0	0	0	2609	--	--	16.08	16.08	0.10	0.05	0.03	0.26	0.00	0.00	20.9
7	0	-0	-4348	0	0	0	2723	--	--	16.08	16.08	0.10	0.05	0.04	0.27	0.00	0.00	20.9
8	0	-0	-4037	0	0	0	2082	--	--	16.08	16.08	0.10	0.04	0.03	0.25	0.00	0.00	20.9
9	0	-0	-4240	0	0	0	2196	--	--	16.08	16.08	0.10	0.04	0.03	0.27	0.00	0.00	20.9
10	0	-0	-4342	0	0	0	3264	--	--	16.08	16.08	0.10	0.06	0.04	0.27	0.00	0.00	20.9
11	0	-0	-4403	0	0	0	3298	--	--	16.08	16.08	0.10	0.06	0.04	0.28	0.00	0.00	20.9
12	0	-0	-3982	0	0	0	1507	--	--	16.08	16.08	0.10	0.03	0.03	0.25	0.00	0.00	20.9
13	0	-0	-4043	0	0	0	1541	--	--	16.08	16.08	0.10	0.03	0.03	0.25	0.00	0.00	20.9
14	0	-0	-4145	0	0	0	2609	--	--	16.08	16.08	0.10	0.05	0.03	0.26	0.00	0.00	20.9
15	0	-0	-4348	0	0	0	2723	--	--	16.08	16.08	0.10	0.05	0.04	0.27	0.00	0.00	20.9
16	0	-0	-4037	0	0	0	2082	--	--	16.08	16.08	0.10	0.04	0.03	0.25	0.00	0.00	20.9
17	0	-0	-4240	0	0	0	2196	--	--	16.08	16.08	0.10	0.04	0.03	0.27	0.00	0.00	20.9
18	0	-0	-6450	0	0	0	7151	--	--	16.08	16.08	0.00	0.12	0.05	0.40	0.00	0.00	20.9
19	0	-0	-5218	0	0	0	1441	--	--	16.08	16.08	0.00	0.02	0.04	0.33	0.00	0.00	20.9
20	0	-0	-5729	0	0	0	4139	--	--	16.08	16.08	0.00	0.07	0.05	0.36	0.00	0.00	20.9
37	0	-0	-6717	0	0	0	8666	--	--	16.08	16.08	0.00	0.15	0.06	0.42	0.00	0.00	20.9
38	0	-0	-4663	0	0	0	-3246	--	--	16.08	16.08	0.18	0.05	0.04	0.29	0.00	0.00	20.9
39	0	-0	-5514	0	0	0	3647	--	--	16.08	16.08	0.00	0.06	0.05	0.35	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	-5450	0	0	0	3123	--	--	16.08	16.08	0.00	0.05	0.04	0.34	0.00	0.00	20.9
2	26	-0	-4342	0	0	0	3264	--	--	16.08	16.08	0.10	0.06	0.04	0.27	0.00	0.00	20.9
3	26	-0	-4403	0	0	0	3298	--	--	16.08	16.08	0.10	0.06	0.04	0.28	0.00	0.00	20.9
4	26	-0	-3982	0	0	0	1507	--	--	16.08	16.08	0.10	0.03	0.03	0.25	0.00	0.00	20.9
5	26	-0	-4043	0	0	0	1541	--	--	16.08	16.08	0.10	0.03	0.03	0.25	0.00	0.00	20.9
6	26	-0	-4145	0	0	0	2609	--	--	16.08	16.08	0.10	0.05	0.03	0.26	0.00	0.00	20.9
7	26	-0	-4348	0	0	0	2723	--	--	16.08	16.08	0.10	0.05	0.04	0.27	0.00	0.00	20.9
8	26	-0	-4037	0	0	0	2082	--	--	16.08	16.08	0.10	0.04	0.03	0.25	0.00	0.00	20.9
9	26	-0	-4240	0	0	0	2196	--	--	16.08	16.08	0.10	0.04	0.03	0.27	0.00	0.00	20.9
10	26	-0	-4342	0	0	0	3264	--	--	16.08	16.08	0.10	0.06	0.04	0.27	0.00	0.00	20.9
11	26	-0	-4403	0	0	0	3298	--	--	16.08	16.08	0.10	0.06	0.04	0.28	0.00	0.00	20.9
12	26	-0	-3982	0	0	0	1507	--	--	16.08	16.08	0.10	0.03	0.03	0.25	0.00	0.00	20.9
13	26	-0	-4043	0	0	0	1541	--	--	16.08	16.08	0.10	0.03	0.03	0.25	0.00	0.00	20.9
14	26	-0	-4145	0	0	0	2609	--	--	16.08	16.08	0.10	0.05	0.03	0.26	0.00	0.00	20.9
15	26	-0	-4348	0	0	0	2723	--	--	16.08	16.08	0.10	0.05	0.04	0.27	0.00	0.00	20.9
16	26	-0	-4037	0	0	0	2082	--	--	16.08	16.08	0.10	0.04	0.03	0.25	0.00	0.00	20.9
17	26	-0	-4240	0	0	0	2196	--	--	16.08	16.08	0.10	0.04	0.03	0.27	0.00	0.00	20.9
18	26	-0	-6450	0	0	0	7151	--	--	16.08	16.08	0.00	0.12	0.05	0.40	0.00	0.00	20.9
19	26	-0	-5218	0	0	0	1441	--	--	16.08	16.08	0.00	0.02	0.04	0.33	0.00	0.00	20.9
20	26	-0	-5729	0	0	0	4139	--	--	16.08	16.08	0.00	0.07	0.05	0.36	0.00	0.00	20.9
37	26	-0	-6717	0	0	0	8666	--	--	16.08	16.08	0.00	0.15	0.06	0.42	0.00	0.00	20.9
38	26	-0	-4663	0	0	0	-3246	--	--	16.08	16.08	0.18	0.05	0.04	0.29	0.00	0.00	20.9
39	26	-0	-5514	0	0	0	3647	--	--	16.08	16.08	0.00	0.06	0.05	0.35	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	-5450	0	0	0	324	--	--	16.08	16.08	0.00	0.01	0.04	0.34	0.00	0.00	20.9
2	51	-0	-4342	0	0	0	1034	--	--	16.08	16.08	0.10	0.02	0.04	0.27	0.00	0.00	20.9

3	51	-0	-4403	0	0	0	1037	--	--	16.08	16.08	0.10	0.02	0.04	0.28	0.00	0.00	20.9
4	51	-0	-3982	0	0	0	-539	--	--	16.08	16.08	0.29	0.01	0.03	0.25	0.00	0.00	20.9
5	51	-0	-4043	0	0	0	-536	--	--	16.08	16.08	0.29	0.01	0.03	0.25	0.00	0.00	20.9
6	51	-0	-4145	0	0	0	480	--	--	16.08	16.08	0.10	0.01	0.03	0.26	0.00	0.00	20.9
7	51	-0	-4348	0	0	0	490	--	--	16.08	16.08	0.10	0.01	0.04	0.27	0.00	0.00	20.9
8	51	-0	-4037	0	0	0	8	--	--	16.08	16.08	0.10	0.00	0.03	0.25	0.00	0.00	20.9
9	51	-0	-4240	0	0	0	18	--	--	16.08	16.08	0.10	0.00	0.03	0.27	0.00	0.00	20.9
10	51	-0	-4342	0	0	0	1034	--	--	16.08	16.08	0.10	0.02	0.04	0.27	0.00	0.00	20.9
11	51	-0	-4403	0	0	0	1037	--	--	16.08	16.08	0.10	0.02	0.04	0.28	0.00	0.00	20.9
12	51	-0	-3982	0	0	0	-539	--	--	16.08	16.08	0.29	0.01	0.03	0.25	0.00	0.00	20.9
13	51	-0	-4043	0	0	0	-536	--	--	16.08	16.08	0.29	0.01	0.03	0.25	0.00	0.00	20.9
14	51	-0	-4145	0	0	0	480	--	--	16.08	16.08	0.10	0.01	0.03	0.26	0.00	0.00	20.9
15	51	-0	-4348	0	0	0	490	--	--	16.08	16.08	0.10	0.01	0.04	0.27	0.00	0.00	20.9
16	51	-0	-4037	0	0	0	8	--	--	16.08	16.08	0.10	0.00	0.03	0.25	0.00	0.00	20.9
17	51	-0	-4240	0	0	0	18	--	--	16.08	16.08	0.10	0.00	0.03	0.27	0.00	0.00	20.9
18	51	-0	-6450	0	0	0	3838	--	--	16.08	16.08	0.00	0.07	0.05	0.40	0.00	0.00	20.9
19	51	-0	-5218	0	0	0	-1240	--	--	16.08	16.08	0.18	0.02	0.04	0.33	0.00	0.00	20.9
20	51	-0	-5729	0	0	0	1197	--	--	16.08	16.08	0.00	0.02	0.05	0.36	0.00	0.00	20.9
37	51	-0	-6717	0	0	0	5216	--	--	16.08	16.08	0.00	0.09	0.06	0.42	0.00	0.00	20.9
38	51	-0	-4663	0	0	0	-3246	--	--	16.08	16.08	0.18	0.05	0.04	0.29	0.00	0.00	20.9
39	51	-0	-5514	0	0	0	815	--	--	16.08	16.08	0.00	0.01	0.05	0.35	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 96 NI 1263 NF 1293 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-4123	0	0	0	324	--	--	16.08	16.08	0.00	0.01	0.03	0.26	0.00	0.00	20.9
2	0	-0	-3360	0	0	0	1034	--	--	16.08	16.08	0.10	0.02	0.03	0.21	0.00	0.00	20.9
3	0	-0	-3406	0	0	0	1037	--	--	16.08	16.08	0.10	0.02	0.03	0.21	0.00	0.00	20.9
4	0	-0	-2937	0	0	0	-2047	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
5	0	-0	-2983	0	0	0	-2068	--	--	16.08	16.08	0.29	0.04	0.02	0.19	0.00	0.00	20.9
6	0	-0	-3159	0	0	0	480	--	--	16.08	16.08	0.10	0.01	0.03	0.20	0.00	0.00	20.9
7	0	-0	-3311	0	0	0	490	--	--	16.08	16.08	0.10	0.01	0.03	0.21	0.00	0.00	20.9
8	0	-0	-3032	0	0	0	8	--	--	16.08	16.08	0.10	0.00	0.02	0.19	0.00	0.00	20.9
9	0	-0	-3184	0	0	0	18	--	--	16.08	16.08	0.10	0.00	0.03	0.20	0.00	0.00	20.9
10	0	-0	-3360	0	0	0	1034	--	--	16.08	16.08	0.10	0.02	0.03	0.21	0.00	0.00	20.9
11	0	-0	-3406	0	0	0	1037	--	--	16.08	16.08	0.10	0.02	0.03	0.21	0.00	0.00	20.9
12	0	-0	-2937	0	0	0	-2047	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
13	0	-0	-2983	0	0	0	-2068	--	--	16.08	16.08	0.29	0.04	0.02	0.19	0.00	0.00	20.9
14	0	-0	-3159	0	0	0	480	--	--	16.08	16.08	0.10	0.01	0.03	0.20	0.00	0.00	20.9
15	0	-0	-3311	0	0	0	490	--	--	16.08	16.08	0.10	0.01	0.03	0.21	0.00	0.00	20.9
16	0	-0	-3032	0	0	0	8	--	--	16.08	16.08	0.10	0.00	0.02	0.19	0.00	0.00	20.9
17	0	-0	-3184	0	0	0	18	--	--	16.08	16.08	0.10	0.00	0.03	0.20	0.00	0.00	20.9
18	0	-0	-5215	0	0	0	3838	--	--	16.08	16.08	0.00	0.07	0.04	0.33	0.00	0.00	20.9
19	0	-0	-3799	0	0	0	-3191	--	--	16.08	16.08	0.18	0.05	0.03	0.24	0.00	0.00	20.9
20	0	-0	-4418	0	0	0	1197	--	--	16.08	16.08	0.00	0.02	0.04	0.28	0.00	0.00	20.9
37	0	-0	-5547	0	0	0	5216	--	--	16.08	16.08	0.00	0.09	0.05	0.35	0.00	0.00	20.9
38	0	-0	-3188	0	0	0	-4883	--	--	16.08	16.08	0.18	0.08	0.03	0.20	0.00	0.00	20.9
39	0	-0	-4220	0	0	0	815	--	--	16.08	16.08	0.00	0.01	0.03	0.26	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	-4123	0	0	0	-1794	--	--	16.08	16.08	0.18	0.03	0.03	0.26	0.00	0.00	20.9
2	26	-0	-3360	0	0	0	1034	--	--	16.08	16.08	0.10	0.02	0.03	0.21	0.00	0.00	20.9
3	26	-0	-3406	0	0	0	1037	--	--	16.08	16.08	0.10	0.02	0.03	0.21	0.00	0.00	20.9
4	26	-0	-2937	0	0	0	-2047	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
5	26	-0	-2983	0	0	0	-2068	--	--	16.08	16.08	0.29	0.04	0.02	0.19	0.00	0.00	20.9
6	26	-0	-3159	0	0	0	-1143	--	--	16.08	16.08	0.29	0.02	0.03	0.20	0.00	0.00	20.9
7	26	-0	-3311	0	0	0	-1211	--	--	16.08	16.08	0.29	0.02	0.03	0.21	0.00	0.00	20.9
8	26	-0	-3032	0	0	0	-1549	--	--	16.08	16.08	0.29	0.03	0.02	0.19	0.00	0.00	20.9
9	26	-0	-3184	0	0	0	-1617	--	--	16.08	16.08	0.29	0.03	0.03	0.20	0.00	0.00	20.9
10	26	-0	-3360	0	0	0	1034	--	--	16.08	16.08	0.10	0.02	0.03	0.21	0.00	0.00	20.9
11	26	-0	-3406	0	0	0	1037	--	--	16.08	16.08	0.10	0.02	0.03	0.21	0.00	0.00	20.9
12	26	-0	-2937	0	0	0	-2047	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
13	26	-0	-2983	0	0	0	-2068	--	--	16.08	16.08	0.29	0.04	0.02	0.19	0.00	0.00	20.9
14	26	-0	-3159	0	0	0	-1143	--	--	16.08	16.08	0.29	0.02	0.03	0.20	0.00	0.00	20.9
15	26	-0	-3311	0	0	0	-1211	--	--	16.08	16.08	0.29	0.02	0.03	0.21	0.00	0.00	20.9
16	26	-0	-3032	0	0	0	-1549	--	--	16.08	16.08	0.29	0.03	0.02	0.19	0.00	0.00	20.9
17	26	-0	-3184	0	0	0	-1617	--	--	16.08	16.08	0.29	0.03	0.03	0.20	0.00	0.00	20.9
18	26	-0	-5215	0	0	0	3838	--	--	16.08	16.08	0.00	0.07	0.04	0.33	0.00	0.00	20.9
19	26	-0	-3799	0	0	0	-3191	--	--	16.08	16.08	0.18	0.05	0.03	0.24	0.00	0.00	20.9
20	26	-0	-4418	0	0	0	1197	--	--	16.08	16.08	0.00	0.02	0.04	0.28	0.00	0.00	20.9
37	26	-0	-5547	0	0	0	5216	--	--	16.08	16.08	0.00	0.09	0.05	0.35	0.00	0.00	20.9
38	26	-0	-3188	0	0	0	-4883	--	--	16.08	16.08	0.18	0.08	0.03	0.20	0.00	0.00	20.9
39	26	-0	-4220	0	0	0	-1353	--	--	16.08	16.08	0.18	0.02	0.03	0.26	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	-4123	0	0	0	-1794	--	--	16.08	16.08	0.18	0.03	0.03	0.26	0.00	0.00	20.9
2	51	-0	-3360	0	0	0	-692	--	--	16.08	16.08	0.29	0.01	0.03	0.21	0.00	0.00	20.9
3	51	-0	-3406	0	0	0	-713	--	--	16.08	16.08	0.29	0.01	0.03	0.21	0.00	0.00	20.9
4	51	-0	-2937	0	0	0	-2047	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
5	51	-0	-2983	0	0	0	-2068	--	--	16.08	16.08	0.29	0.04	0.02	0.19	0.00	0.00	20.9
6	51	-0	-3159	0	0	0	-1143	--	--	16.08	16.08	0.29	0.02	0.03	0.20	0.00	0.00	20.9
7	51	-0	-3311	0	0	0	-1211	--	--	16.08	16.08	0.29	0.02	0.03	0.21	0.00	0.00	20.9
8	51	-0	-3032	0	0	0	-1549	--	--	16.08	16.08	0.29	0.03	0.02	0.19	0.00	0.00	20.9
9	51	-0	-3184	0	0	0	-1617	--	--	16.08	16.08	0.29	0.03	0.03	0.20	0.00	0.00	20.9
10	51	-0	-3360	0	0	0	-692	--	--	16.08	16.08	0.29	0.01	0.03	0.21	0.00	0.00	20.9
11	51	-0	-3406	0	0	0	-713	--	--	16.08	16.08	0.29	0.01	0.03	0.21	0.00	0.00	20.9
12	51	-0	-2937	0	0	0	-2047	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
13	51	-0	-2983	0	0	0	-2068	--	--	16.08	16.08	0.29	0.04	0.02	0.19	0.00	0.00	20.9
14	51	-0	-3159	0	0	0	-1143	--	--	16.08	16.08	0.29	0.02	0.03	0.20	0.00	0.00	20.9
15	51	-0	-3311	0	0	0	-1211	--	--	16.08	16.08	0.29	0.02	0.03	0.21	0.00	0.00	20.9
16	51	-0	-3032	0	0	0	-1549	--	--	16.08	16.08	0.29	0.03	0.02	0.19	0.00	0.00	20.9
17	51	-0	-3184	0	0	0	-1617	--	--	16.08	16.08	0.29	0.03	0.03	0.20	0.00	0.00	20.9
18	51	-0	-5215	0	0	0	1159	--	--	16.08	16.08	0.00	0.02	0.04	0.33	0.00	0.00	20.9
19	51	-0	-3799	0	0	0	-3191	--	--	16.08	16.08	0.18	0.05	0.03	0.24	0.00	0.00	20.9
20	51	-0	-4418	0	0	0	-1073	--	--	16.08	16.08	0.18	0.02	0.04	0.28	0.00	0.00	20.9
37	51	-0	-5547	0	0	0	2367	--	--	16.08	16.08	0.00	0.04	0.05	0.35	0.00	0.00	20.9
38	51	-0	-3188	0	0	0	-4883	--	--	16.08	16.08	0.18	0.08	0.03	0.20	0.00	0.00	20.9
39	51	-0	-4220	0	0	0	-1353	--	--	16.08	16.08	0.18	0.02	0.03	0.26	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 97 NI 1293 NF 1292 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-2893	0	0	0	-3280	--	--	16.08	16.08	0.18	0.05	0.02	0.18	0.00	0.00	20.9
2	0	-0	-2442	0	0	0	-1947	--	--	16.08	16.08	0.29	0.03	0.02	0.15	0.00	0.00	20.9
3	0	-0	-2474	0	0	0	-1983	--	--	16.08	16.08	0.29	0.03	0.02	0.16	0.00	0.00	20.9
4	0	-0	-1977	0	0	0	-3063	--	--	16.08	16.08	0.29	0.05	0.02	0.12	0.00	0.00	20.9
5	0	-0	-2009	0	0	0	-3100	--	--	16.08	16.08	0.29	0.05	0.02	0.13	0.00	0.00	20.9
6	0	-0	-2242	0	0	0	-2294	--	--	16.08	16.08	0.29	0.04	0.02	0.14	0.00	0.00	20.9
7	0	-0	-2349	0	0	0	-2417	--	--	16.08	16.08	0.29	0.04	0.02	0.15	0.00	0.00	20.9
8	0	-0	-2103	0	0	0	-2629	--	--	16.08	16.08	0.29	0.05	0.02	0.13	0.00	0.00	20.9
9	0	-0	-2209	0	0	0	-2752	--	--	16.08	16.08	0.29	0.05	0.02	0.14	0.00	0.00	20.9
10	0	-0	-2442	0	0	0	-1947	--	--	16.08	16.08	0.29	0.03	0.02	0.15	0.00	0.00	20.9
11	0	-0	-2474	0	0	0	-1983	--	--	16.08	16.08	0.29	0.03	0.02	0.16	0.00	0.00	20.9
12	0	-0	-1977	0	0	0	-3063	--	--	16.08	16.08	0.29	0.05	0.02	0.12	0.00	0.00	20.9
13	0	-0	-2009	0	0	0	-3100	--	--	16.08	16.08	0.29	0.05	0.02	0.13	0.00	0.00	20.9
14	0	-0	-2242	0	0	0	-2294	--	--	16.08	16.08	0.29	0.04	0.02	0.14	0.00	0.00	20.9
15	0	-0	-2349	0	0	0	-2417	--	--	16.08	16.08	0.29	0.04	0.02	0.15	0.00	0.00	20.9
16	0	-0	-2103	0	0	0	-2629	--	--	16.08	16.08	0.29	0.05	0.02	0.13	0.00	0.00	20.9
17	0	-0	-2209	0	0	0	-2752	--	--	16.08	16.08	0.29	0.05	0.02	0.14	0.00	0.00	20.9
18	0	-0	-4031	0	0	0	1159	--	--	16.08	16.08	0.00	0.02	0.03	0.25	0.00	0.00	20.9
19	0	-0	-2496	0	0	0	-4473	--	--	16.08	16.08	0.18	0.07	0.02	0.16	0.00	0.00	20.9
20	0	-0	-3193	0	0	0	-2713	--	--	16.08	16.08	0.18	0.04	0.03	0.20	0.00	0.00	20.9
37	0	-0	-4413	0	0	0	2367	--	--	16.08	16.08	0.00	0.04	0.04	0.28	0.00	0.00	20.9
38	0	-0	-1854	0	0	0	-5835	--	--	16.08	16.08	0.18	0.10	0.02	0.12	0.00	0.00	20.9
39	0	-0	-3015	0	0	0	-2902	--	--	16.08	16.08	0.18	0.05	0.02	0.19	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	26	-0	-2893	0	0	0	-3280	--	--	16.08	16.08	0.18	0.05	0.02	0.18	0.00	0.00	20.9
2	26	-0	-2442	0	0	0	-1947	--	--	16.08	16.08	0.29	0.03	0.02	0.15	0.00	0.00	20.9
3	26	-0	-2474	0	0	0	-1983	--	--	16.08	16.08	0.29	0.03	0.02	0.16	0.00	0.00	20.9
4	26	-0	-1977	0	0	0	-3063	--	--	16.08	16.08	0.29	0.05	0.02	0.12	0.00	0.00	20.9
5	26	-0	-2009	0	0	0	-3100	--	--	16.08	16.08	0.29	0.05	0.02	0.13	0.00	0.00	20.9
6	26	-0	-2242	0	0	0	-2294	--	--	16.08	16.08	0.29	0.04	0.02	0.14	0.00	0.00	20.9
7	26	-0	-2349	0	0	0	-2417	--	--	16.08	16.08	0.29	0.04	0.02	0.15	0.00	0.00	20.9
8	26	-0	-2103	0	0	0	-2629	--	--	16.08	16.08	0.29	0.05	0.02	0.13	0.00	0.00	20.9
9	26	-0	-2209	0	0	0	-2752	--	--	16.08	16.08	0.29	0.05	0.02	0.14	0.00	0.00	20.9
10	26	-0	-2442	0	0	0	-1947	--	--	16.08	16.08	0.29	0.03	0.02	0.15	0.00	0.00	20.9
11	26	-0	-2474	0	0	0	-1983	--	--	16.08	16.08	0.29	0.03	0.02	0.16	0.00	0.00	20.9
12	26	-0	-1977	0	0	0	-3063	--	--	16.08	16.08	0.29	0.05	0.02	0.12	0.00	0.00	20.9
13	26	-0	-2009	0	0	0	-3100	--	--	16.08	16.08	0.29	0.05	0.02	0.13	0.00	0.00	20.9
14	26	-0	-2242	0	0	0	-2294	--	--	16.08	16.08	0.29	0.04	0.02	0.14	0.00	0.00	20.9
15	26	-0	-2349	0	0	0	-2417	--	--	16.08	16.08	0.29	0.04	0.02	0.15	0.00	0.00	20.9
16	26	-0	-2103	0	0	0	-2629	--	--	16.08	16.08	0.29	0.05	0.02	0.13	0.00	0.00	20.9
17	26	-0	-2209	0	0	0	-2752	--	--	16.08	16.08	0.29	0.05	0.02	0.14	0.00	0.00	20.9
18	26	-0	-4031	0	0	0	1159	--	--	16.08	16.08	0.00	0.02	0.03	0.25	0.00	0.00	20.9
19	26	-0	-2496	0	0	0	-4473	--	--	16.08	16.08	0.18	0.07	0.02	0.16	0.00	0.00	20.9
20	26	-0	-3193	0	0	0	-2713	--	--	16.08	16.08	0.18	0.04	0.03	0.20	0.00	0.00	20.9
37	26	-0	-4413	0	0	0	2367	--	--	16.08	16.08	0.00	0.04	0.04	0.28	0.00	0.00	20.9
38	26	-0	-1854	0	0	0	-5835	--	--	16.08	16.08	0.18	0.10	0.02	0.12	0.00	0.00	20.9
39	26	-0	-3015	0	0	0	-2902	--	--	16.08	16.08	0.18	0.05	0.02	0.19	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	51	-0	-2893	0	0	0	-3280	--	--	16.08	16.08	0.18	0.05	0.02	0.18	0.00	0.00	20.9
2	51	-0	-2442	0	0	0	-1947	--	--	16.08	16.08	0.29	0.03	0.02	0.15	0.00	0.00	20.9
3	51	-0	-2474	0	0	0	-1983	--	--	16.08	16.08	0.29	0.03	0.02	0.16	0.00	0.00	20.9
4	51	-0	-1977	0	0	0	-3063	--	--	16.08	16.08	0.29	0.05	0.02	0.12	0.00	0.00	20.9
5	51	-0	-2009	0	0	0	-3100	--	--	16.08	16.08	0.29	0.05	0.02	0.13	0.00	0.00	20.9
6	51	-0	-2242	0	0	0	-2294	--	--	16.08	16.08	0.29	0.04	0.02	0.14	0.00	0.00	20.9
7	51	-0	-2349	0	0	0	-2417	--	--	16.08	16.08	0.29	0.04	0.02	0.15	0.00	0.00	20.9
8	51	-0	-2103	0	0	0	-2629	--	--	16.08	16.08	0.29	0.05	0.02	0.13	0.00	0.00	20.9
9	51	-0	-2209	0	0	0	-2752	--	--	16.08	16.08	0.29	0.05	0.02	0.14	0.00	0.00	20.9
10	51	-0	-2442	0	0	0	-1947	--	--	16.08	16.08	0.29	0.03	0.02	0.15	0.00	0.00	20.9
11	51	-0	-2474	0	0	0	-1983	--	--	16.08	16.08	0.29	0.03	0.02	0.16	0.00	0.00	20.9
12	51	-0	-1977	0	0	0	-3063	--	--	16.08	16.08	0.29	0.05	0.02	0.12	0.00	0.00	20.9
13	51	-0	-2009	0	0	0	-3100	--	--	16.08	16.08	0.29	0.05	0.02	0.13	0.00	0.00	20.9
14	51	-0	-2242	0	0	0	-2294	--	--	16.08	16.08	0.29	0.04	0.02	0.14	0.00	0.00	20.9
15	51	-0	-2349	0	0	0	-2417	--	--	16.08	16.08	0.29	0.04	0.02	0.15	0.00	0.00	20.9
16	51	-0	-2103	0	0	0	-2629	--	--	16.08	16.08	0.29	0.05	0.02	0.13	0.00	0.00	20.9
17	51	-0	-2209	0	0	0	-2752	--	--	16.08	16.08	0.29	0.05	0.02	0.14	0.00	0.00	20.9
18	51	-0	-4031	0	0	0	-912	--	--	16.08	16.08	0.18	0.02	0.03	0.25	0.00	0.00	20.9
19	51	-0	-2496	0	0	0	-4473	--	--	16.08	16.08	0.18	0.07	0.02	0.16	0.00	0.00	20.9
20	51	-0	-3193	0	0	0	-2713	--	--	16.08	16.08	0.18	0.04	0.03	0.20	0.00	0.00	20.9
37	51	-0	-4413	0	0	0	100	--	--	16.08	16.08	0.00	0.00	0.04	0.28	0.00	0.00	20.9
38	51	-0	-1854	0	0	0	-5835	--	--	16.08	16.08	0.18	0.10	0.02	0.12	0.00	0.00	20.9
39	51	-0	-3015	0	0	0	-2902	--	--	16.08	16.08	0.18	0.05	0.02	0.19	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 98 NI 1292 NF 1291 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-1751	0	0	0	-4179	--	--	16.08	16.08	0.18	0.07	0.01	0.11	0.00	0.00	20.9
2	0	-0	-1584	0	0	0	-2760	--	--	16.08	16.08	0.29	0.05	0.01	0.10	0.00	0.00	20.9
3	0	-0	-1603	0	0	0	-2807	--	--	16.08	16.08	0.29	0.05	0.01	0.10	0.00	0.00	20.9
4	0	-0	-1090	0	0	0	-3623	--	--	16.08	16.08	0.29	0.06	0.01	0.07	0.00	0.00	20.9
5	0	-0	-1110	0	0	0	-3670	--	--	16.08	16.08	0.29	0.06	0.01	0.07	0.00	0.00	20.9
6	0	-0	-1388	0	0	0	-3007	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
7	0	-0	-1453	0	0	0	-3163	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
8	0	-0	-1240	0	0	0	-3266	--	--	16.08	16.08	0.29	0.06	0.01	0.08	0.00	0.00	20.9
9	0	-0	-1305	0	0	0	-3422	--	--	16.08	16.08	0.29	0.06	0.01	0.08	0.00	0.00	20.9
10	0	-0	-1584	0	0	0	-2760	--	--	16.08	16.08	0.29	0.05	0.01	0.10	0.00	0.00	20.9

11	0	-0	-1603	0	0	0	-2807	--	--	16.08	16.08	0.29	0.05	0.01	0.10	0.00	0.00	20.9
12	0	-0	-1090	0	0	0	-3623	--	--	16.08	16.08	0.29	0.06	0.01	0.07	0.00	0.00	20.9
13	0	-0	-1110	0	0	0	-3670	--	--	16.08	16.08	0.29	0.06	0.01	0.07	0.00	0.00	20.9
14	0	-0	-1388	0	0	0	-3007	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
15	0	-0	-1453	0	0	0	-3163	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
16	0	-0	-1240	0	0	0	-3266	--	--	16.08	16.08	0.29	0.06	0.01	0.08	0.00	0.00	20.9
17	0	-0	-1305	0	0	0	-3422	--	--	16.08	16.08	0.29	0.06	0.01	0.08	0.00	0.00	20.9
18	0	-0	-2903	0	0	0	-2403	--	--	16.08	16.08	0.18	0.04	0.02	0.18	0.00	0.00	20.9
19	0	-0	-1291	0	0	0	-5136	--	--	16.08	16.08	0.18	0.09	0.01	0.08	0.00	0.00	20.9
20	0	-0	-2044	0	0	0	-3763	--	--	16.08	16.08	0.18	0.06	0.02	0.13	0.00	0.00	20.9
37	0	-0	-3323	0	0	0	100	--	--	16.08	16.08	0.00	0.00	0.03	0.21	0.00	0.00	20.9
38	0	-0	-636	0	0	0	-6162	--	--	16.08	16.08	0.18	0.10	0.01	0.04	0.00	0.00	20.9
39	0	-0	-1892	0	0	0	-3873	--	--	16.08	16.08	0.18	0.06	0.02	0.12	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	-1751	0	0	0	-4179	--	--	16.08	16.08	0.18	0.07	0.01	0.11	0.00	0.00	20.9
2	26	-0	-1584	0	0	0	-2760	--	--	16.08	16.08	0.29	0.05	0.01	0.10	0.00	0.00	20.9
3	26	-0	-1603	0	0	0	-2807	--	--	16.08	16.08	0.29	0.05	0.01	0.10	0.00	0.00	20.9
4	26	-0	-1090	0	0	0	-3623	--	--	16.08	16.08	0.29	0.06	0.01	0.07	0.00	0.00	20.9
5	26	-0	-1110	0	0	0	-3670	--	--	16.08	16.08	0.29	0.06	0.01	0.07	0.00	0.00	20.9
6	26	-0	-1388	0	0	0	-3007	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
7	26	-0	-1453	0	0	0	-3163	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
8	26	-0	-1240	0	0	0	-3266	--	--	16.08	16.08	0.29	0.06	0.01	0.08	0.00	0.00	20.9
9	26	-0	-1305	0	0	0	-3422	--	--	16.08	16.08	0.29	0.06	0.01	0.08	0.00	0.00	20.9
10	26	-0	-1584	0	0	0	-2760	--	--	16.08	16.08	0.29	0.05	0.01	0.10	0.00	0.00	20.9
11	26	-0	-1603	0	0	0	-2807	--	--	16.08	16.08	0.29	0.05	0.01	0.10	0.00	0.00	20.9
12	26	-0	-1090	0	0	0	-3623	--	--	16.08	16.08	0.29	0.06	0.01	0.07	0.00	0.00	20.9
13	26	-0	-1110	0	0	0	-3670	--	--	16.08	16.08	0.29	0.06	0.01	0.07	0.00	0.00	20.9
14	26	-0	-1388	0	0	0	-3007	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
15	26	-0	-1453	0	0	0	-3163	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
16	26	-0	-1240	0	0	0	-3266	--	--	16.08	16.08	0.29	0.06	0.01	0.08	0.00	0.00	20.9
17	26	-0	-1305	0	0	0	-3422	--	--	16.08	16.08	0.29	0.06	0.01	0.08	0.00	0.00	20.9
18	26	-0	-2903	0	0	0	-2403	--	--	16.08	16.08	0.18	0.04	0.02	0.18	0.00	0.00	20.9
19	26	-0	-1291	0	0	0	-5136	--	--	16.08	16.08	0.18	0.09	0.01	0.08	0.00	0.00	20.9
20	26	-0	-2044	0	0	0	-3763	--	--	16.08	16.08	0.18	0.06	0.02	0.13	0.00	0.00	20.9
37	26	-0	-3323	0	0	0	-1606	--	--	16.08	16.08	0.18	0.03	0.03	0.21	0.00	0.00	20.9
38	26	-0	-636	0	0	0	-6162	--	--	16.08	16.08	0.18	0.10	0.01	0.04	0.00	0.00	20.9
39	26	-0	-1892	0	0	0	-3873	--	--	16.08	16.08	0.18	0.06	0.02	0.12	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	-1751	0	0	0	-4179	--	--	16.08	16.08	0.18	0.07	0.01	0.11	0.00	0.00	20.9
2	51	-0	-1584	0	0	0	-2760	--	--	16.08	16.08	0.29	0.05	0.01	0.10	0.00	0.00	20.9
3	51	-0	-1603	0	0	0	-2807	--	--	16.08	16.08	0.29	0.05	0.01	0.10	0.00	0.00	20.9
4	51	-0	-1090	0	0	0	-3623	--	--	16.08	16.08	0.29	0.06	0.01	0.07	0.00	0.00	20.9
5	51	-0	-1110	0	0	0	-3670	--	--	16.08	16.08	0.29	0.06	0.01	0.07	0.00	0.00	20.9
6	51	-0	-1388	0	0	0	-3007	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
7	51	-0	-1453	0	0	0	-3163	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
8	51	-0	-1240	0	0	0	-3266	--	--	16.08	16.08	0.29	0.06	0.01	0.08	0.00	0.00	20.9
9	51	-0	-1305	0	0	0	-3422	--	--	16.08	16.08	0.29	0.06	0.01	0.08	0.00	0.00	20.9
10	51	-0	-1584	0	0	0	-2760	--	--	16.08	16.08	0.29	0.05	0.01	0.10	0.00	0.00	20.9
11	51	-0	-1603	0	0	0	-2807	--	--	16.08	16.08	0.29	0.05	0.01	0.10	0.00	0.00	20.9
12	51	-0	-1090	0	0	0	-3623	--	--	16.08	16.08	0.29	0.06	0.01	0.07	0.00	0.00	20.9
13	51	-0	-1110	0	0	0	-3670	--	--	16.08	16.08	0.29	0.06	0.01	0.07	0.00	0.00	20.9
14	51	-0	-1388	0	0	0	-3007	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
15	51	-0	-1453	0	0	0	-3163	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
16	51	-0	-1240	0	0	0	-3266	--	--	16.08	16.08	0.29	0.06	0.01	0.08	0.00	0.00	20.9
17	51	-0	-1305	0	0	0	-3422	--	--	16.08	16.08	0.29	0.06	0.01	0.08	0.00	0.00	20.9
18	51	-0	-2903	0	0	0	-2403	--	--	16.08	16.08	0.18	0.04	0.02	0.18	0.00	0.00	20.9
19	51	-0	-1291	0	0	0	-5136	--	--	16.08	16.08	0.18	0.09	0.01	0.08	0.00	0.00	20.9
20	51	-0	-2044	0	0	0	-3763	--	--	16.08	16.08	0.18	0.06	0.02	0.13	0.00	0.00	20.9
37	51	-0	-3323	0	0	0	-1606	--	--	16.08	16.08	0.18	0.03	0.03	0.21	0.00	0.00	20.9
38	51	-0	-636	0	0	0	-6162	--	--	16.08	16.08	0.18	0.10	0.01	0.04	0.00	0.00	20.9
39	51	-0	-1892	0	0	0	-3873	--	--	16.08	16.08	0.18	0.06	0.02	0.12	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 99 NI 1291 NF 1333 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-677	0	0	0	-4527	--	--	16.08	16.08	0.18	0.08	0.01	0.04	0.00	0.00	20.9
2	0	-0	-773	0	0	0	-3157	--	--	16.08	16.08	0.29	0.05	0.01	0.05	0.00	0.00	20.9
3	0	-0	-781	0	0	0	-3208	--	--	16.08	16.08	0.29	0.06	0.01	0.05	0.00	0.00	20.9
4	0	-0	-260	0	0	0	-3756	--	--	16.08	16.08	0.29	0.07	0.00	0.02	0.00	0.00	20.9
5	0	-0	-268	0	0	0	-3807	--	--	16.08	16.08	0.29	0.07	0.00	0.02	0.00	0.00	20.9
6	0	-0	-585	0	0	0	-3308	--	--	16.08	16.08	0.29	0.06	0.00	0.04	0.00	0.00	20.9
7	0	-0	-610	0	0	0	-3477	--	--	16.08	16.08	0.29	0.06	0.01	0.04	0.00	0.00	20.9
8	0	-0	-430	0	0	0	-3487	--	--	16.08	16.08	0.29	0.06	0.00	0.03	0.00	0.00	20.9
9	0	-0	-456	0	0	0	-3657	--	--	16.08	16.08	0.29	0.06	0.00	0.03	0.00	0.00	20.9
10	0	-0	-773	0	0	0	-3157	--	--	16.08	16.08	0.29	0.05	0.01	0.05	0.00	0.00	20.9
11	0	-0	-781	0	0	0	-3208	--	--	16.08	16.08	0.29	0.06	0.01	0.05	0.00	0.00	20.9
12	0	-0	-260	0	0	0	-3756	--	--	16.08	16.08	0.29	0.07	0.00	0.02	0.00	0.00	20.9
13	0	-0	-268	0	0	0	-3807	--	--	16.08	16.08	0.29	0.07	0.00	0.02	0.00	0.00	20.9
14	0	-0	-585	0	0	0	-3308	--	--	16.08	16.08	0.29	0.06	0.00	0.04	0.00	0.00	20.9
15	0	-0	-610	0	0	0	-3477	--	--	16.08	16.08	0.29	0.06	0.01	0.04	0.00	0.00	20.9
16	0	-0	-430	0	0	0	-3487	--	--	16.08	16.08	0.29	0.06	0.00	0.03	0.00	0.00	20.9
17	0	-0	-456	0	0	0	-3657	--	--	16.08	16.08	0.29	0.06	0.00	0.03	0.00	0.00	20.9
18	0	-0	-1823	0	0	0	-3339	--	--	16.08	16.08	0.18	0.06	0.02	0.11	0.00	0.00	20.9
19	0	-0	-161	0	0	0	-5219	--	--	16.08	16.08	0.18	0.09	0.00	0.01	0.00	0.00	20.9
20	0	-0	-958	0	0	0	-4255	--	--	16.08	16.08	0.18	0.07	0.01	0.06	0.00	0.00	20.9
37	0	-0	-2275	0	0	0	-2775	--	--	16.08	16.08	0.18	0.05	0.02	0.14	0.00	0.00	20.9
38	0	-0	496	0	0	0	-6162	--	--	16.08	16.08	0.18	0.10	0.00	0.03	0.00	0.00	20.9
39	0	-0	-833	0	0	0	-4301	--	--	16.08	16.08	0.18	0.07	0.01	0.05	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	-677	0	0	0	-4527	--	--	16.08	16.08	0.18	0.08	0.01	0.04	0.00	0.00	20.9
2	26	-0	-773	0	0	0	-3157	--	--	16.08	16.08	0.29	0.05	0.01	0.05	0.00	0.00	20.9
3	26	-0	-781	0	0	0	-3208	--	--	16.08	16.08	0.29	0.06	0.01	0.05	0.00	0.00	20.9
4	26	-0	-260	0	0	0	-3756	--	--	16.08	16.08	0.29	0.07	0.00	0.02	0.00	0.00	20.9
5	26	-0	-268	0	0	0	-3807	--	--	16.08	16.08	0.29	0.07	0.00	0.02	0.00	0.00	20.9
6	26	-0	-585	0	0	0	-3308	--	--	16.08	16.08	0.29	0.06	0.00	0.04	0.00	0.00	20.9

7	26	-0	-610	0	0	0	-3477	--	--	16.08	16.08	0.29	0.06	0.01	0.04	0.00	0.00	20.9
8	26	-0	-430	0	0	0	-3487	--	--	16.08	16.08	0.29	0.06	0.00	0.03	0.00	0.00	20.9
9	26	-0	-456	0	0	0	-3657	--	--	16.08	16.08	0.29	0.06	0.00	0.03	0.00	0.00	20.9
10	26	-0	-773	0	0	0	-3157	--	--	16.08	16.08	0.29	0.05	0.01	0.05	0.00	0.00	20.9
11	26	-0	-781	0	0	0	-3208	--	--	16.08	16.08	0.29	0.06	0.01	0.05	0.00	0.00	20.9
12	26	-0	-260	0	0	0	-3756	--	--	16.08	16.08	0.29	0.07	0.00	0.02	0.00	0.00	20.9
13	26	-0	-268	0	0	0	-3807	--	--	16.08	16.08	0.29	0.07	0.00	0.02	0.00	0.00	20.9
14	26	-0	-585	0	0	0	-3308	--	--	16.08	16.08	0.29	0.06	0.00	0.04	0.00	0.00	20.9
15	26	-0	-610	0	0	0	-3477	--	--	16.08	16.08	0.29	0.06	0.01	0.04	0.00	0.00	20.9
16	26	-0	-430	0	0	0	-3487	--	--	16.08	16.08	0.29	0.06	0.00	0.03	0.00	0.00	20.9
17	26	-0	-456	0	0	0	-3657	--	--	16.08	16.08	0.29	0.06	0.00	0.03	0.00	0.00	20.9
18	26	-0	-1823	0	0	0	-3339	--	--	16.08	16.08	0.18	0.06	0.02	0.11	0.00	0.00	20.9
19	26	-0	-161	0	0	0	-5219	--	--	16.08	16.08	0.18	0.09	0.00	0.01	0.00	0.00	20.9
20	26	-0	-958	0	0	0	-4255	--	--	16.08	16.08	0.18	0.07	0.01	0.06	0.00	0.00	20.9
37	26	-0	-2275	0	0	0	-2775	--	--	16.08	16.08	0.18	0.05	0.02	0.14	0.00	0.00	20.9
38	26	-0	496	0	0	0	-6162	--	--	16.08	16.08	0.18	0.10	0.00	0.03	0.00	0.00	20.9
39	26	-0	-833	0	0	0	-4301	--	--	16.08	16.08	0.18	0.07	0.01	0.05	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	-677	0	0	0	-4527	--	--	16.08	16.08	0.18	0.08	0.01	0.04	0.00	0.00	20.9
2	51	-0	-773	0	0	0	-3157	--	--	16.08	16.08	0.29	0.05	0.01	0.05	0.00	0.00	20.9
3	51	-0	-781	0	0	0	-3208	--	--	16.08	16.08	0.29	0.06	0.01	0.05	0.00	0.00	20.9
4	51	-0	-260	0	0	0	-3756	--	--	16.08	16.08	0.29	0.07	0.00	0.02	0.00	0.00	20.9
5	51	-0	-268	0	0	0	-3807	--	--	16.08	16.08	0.29	0.07	0.00	0.02	0.00	0.00	20.9
6	51	-0	-585	0	0	0	-3308	--	--	16.08	16.08	0.29	0.06	0.00	0.04	0.00	0.00	20.9
7	51	-0	-610	0	0	0	-3477	--	--	16.08	16.08	0.29	0.06	0.01	0.04	0.00	0.00	20.9
8	51	-0	-430	0	0	0	-3487	--	--	16.08	16.08	0.29	0.06	0.00	0.03	0.00	0.00	20.9
9	51	-0	-456	0	0	0	-3657	--	--	16.08	16.08	0.29	0.06	0.00	0.03	0.00	0.00	20.9
10	51	-0	-773	0	0	0	-3157	--	--	16.08	16.08	0.29	0.05	0.01	0.05	0.00	0.00	20.9
11	51	-0	-781	0	0	0	-3208	--	--	16.08	16.08	0.29	0.06	0.01	0.05	0.00	0.00	20.9
12	51	-0	-260	0	0	0	-3756	--	--	16.08	16.08	0.29	0.07	0.00	0.02	0.00	0.00	20.9
13	51	-0	-268	0	0	0	-3807	--	--	16.08	16.08	0.29	0.07	0.00	0.02	0.00	0.00	20.9
14	51	-0	-585	0	0	0	-3308	--	--	16.08	16.08	0.29	0.06	0.00	0.04	0.00	0.00	20.9
15	51	-0	-610	0	0	0	-3477	--	--	16.08	16.08	0.29	0.06	0.01	0.04	0.00	0.00	20.9
16	51	-0	-430	0	0	0	-3487	--	--	16.08	16.08	0.29	0.06	0.00	0.03	0.00	0.00	20.9
17	51	-0	-456	0	0	0	-3657	--	--	16.08	16.08	0.29	0.06	0.00	0.03	0.00	0.00	20.9
18	51	-0	-1823	0	0	0	-3339	--	--	16.08	16.08	0.18	0.06	0.02	0.11	0.00	0.00	20.9
19	51	-0	-161	0	0	0	-5219	--	--	16.08	16.08	0.18	0.09	0.00	0.01	0.00	0.00	20.9
20	51	-0	-958	0	0	0	-4255	--	--	16.08	16.08	0.18	0.07	0.01	0.06	0.00	0.00	20.9
37	51	-0	-2275	0	0	0	-2775	--	--	16.08	16.08	0.18	0.05	0.02	0.14	0.00	0.00	20.9
38	51	-0	496	0	0	0	-6162	--	--	16.08	16.08	0.18	0.10	0.00	0.03	0.00	0.00	20.9
39	51	-0	-833	0	0	0	-4301	--	--	16.08	16.08	0.18	0.07	0.01	0.05	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 100 NI 1333 NF 1332 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	350	0	0	0	-4527	--	--	16.08	16.08	0.18	0.08	0.00	0.02	0.00	0.00	20.9
2	0	-0	3	0	0	0	-3157	--	--	16.08	16.08	0.29	0.05	0.00	0.00	0.00	0.00	20.9
3	0	-0	6	0	0	0	-3208	--	--	16.08	16.08	0.29	0.06	0.00	0.00	0.00	0.00	20.9
4	0	-0	532	0	0	0	-3756	--	--	16.08	16.08	0.29	0.07	0.00	0.03	0.00	0.00	20.9
5	0	-0	536	0	0	0	-3807	--	--	16.08	16.08	0.29	0.07	0.00	0.03	0.00	0.00	20.9
6	0	-0	185	0	0	0	-3308	--	--	16.08	16.08	0.29	0.06	0.00	0.01	0.00	0.00	20.9
7	0	-0	195	0	0	0	-3477	--	--	16.08	16.08	0.29	0.06	0.00	0.01	0.00	0.00	20.9
8	0	-0	344	0	0	0	-3487	--	--	16.08	16.08	0.29	0.06	0.00	0.02	0.00	0.00	20.9
9	0	-0	354	0	0	0	-3657	--	--	16.08	16.08	0.29	0.06	0.00	0.02	0.00	0.00	20.9
10	0	-0	3	0	0	0	-3157	--	--	16.08	16.08	0.29	0.05	0.00	0.00	0.00	0.00	20.9
11	0	-0	6	0	0	0	-3208	--	--	16.08	16.08	0.29	0.06	0.00	0.00	0.00	0.00	20.9
12	0	-0	532	0	0	0	-3756	--	--	16.08	16.08	0.29	0.07	0.00	0.03	0.00	0.00	20.9
13	0	-0	536	0	0	0	-3807	--	--	16.08	16.08	0.29	0.07	0.00	0.03	0.00	0.00	20.9
14	0	-0	185	0	0	0	-3308	--	--	16.08	16.08	0.29	0.06	0.00	0.01	0.00	0.00	20.9
15	0	-0	195	0	0	0	-3477	--	--	16.08	16.08	0.29	0.06	0.00	0.01	0.00	0.00	20.9
16	0	-0	344	0	0	0	-3487	--	--	16.08	16.08	0.29	0.06	0.00	0.02	0.00	0.00	20.9
17	0	-0	354	0	0	0	-3657	--	--	16.08	16.08	0.29	0.06	0.00	0.02	0.00	0.00	20.9
18	0	-0	-778	0	0	0	-3738	--	--	16.08	16.08	0.18	0.06	0.01	0.05	0.00	0.00	20.9
19	0	-0	921	0	0	0	-5219	--	--	16.08	16.08	0.18	0.09	0.01	0.06	0.00	0.00	20.9
20	0	-0	87	0	0	0	-4255	--	--	16.08	16.08	0.18	0.07	0.00	0.01	0.00	0.00	20.9
37	0	-0	-1259	0	0	0	-3422	--	--	16.08	16.08	0.18	0.06	0.01	0.08	0.00	0.00	20.9
38	0	-0	1573	0	0	0	-5907	--	--	16.08	16.08	0.18	0.10	0.01	0.10	0.00	0.00	20.9
39	0	-0	182	0	0	0	-4301	--	--	16.08	16.08	0.18	0.07	0.00	0.01	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	350	0	0	0	-4527	--	--	16.08	16.08	0.18	0.08	0.00	0.02	0.00	0.00	20.9
2	26	-0	3	0	0	0	-3157	--	--	16.08	16.08	0.29	0.05	0.00	0.00	0.00	0.00	20.9
3	26	-0	6	0	0	0	-3208	--	--	16.08	16.08	0.29	0.06	0.00	0.00	0.00	0.00	20.9
4	26	-0	532	0	0	0	-3756	--	--	16.08	16.08	0.29	0.07	0.00	0.03	0.00	0.00	20.9
5	26	-0	536	0	0	0	-3807	--	--	16.08	16.08	0.29	0.07	0.00	0.03	0.00	0.00	20.9
6	26	-0	185	0	0	0	-3308	--	--	16.08	16.08	0.29	0.06	0.00	0.01	0.00	0.00	20.9
7	26	-0	195	0	0	0	-3477	--	--	16.08	16.08	0.29	0.06	0.00	0.01	0.00	0.00	20.9
8	26	-0	344	0	0	0	-3487	--	--	16.08	16.08	0.29	0.06	0.00	0.02	0.00	0.00	20.9
9	26	-0	354	0	0	0	-3657	--	--	16.08	16.08	0.29	0.06	0.00	0.02	0.00	0.00	20.9
10	26	-0	3	0	0	0	-3157	--	--	16.08	16.08	0.29	0.05	0.00	0.00	0.00	0.00	20.9
11	26	-0	6	0	0	0	-3208	--	--	16.08	16.08	0.29	0.06	0.00	0.00	0.00	0.00	20.9
12	26	-0	532	0	0	0	-3756	--	--	16.08	16.08	0.29	0.07	0.00	0.03	0.00	0.00	20.9
13	26	-0	536	0	0	0	-3807	--	--	16.08	16.08	0.29	0.07	0.00	0.03	0.00	0.00	20.9
14	26	-0	185	0	0	0	-3308	--	--	16.08	16.08	0.29	0.06	0.00	0.01	0.00	0.00	20.9
15	26	-0	195	0	0	0	-3477	--	--	16.08	16.08	0.29	0.06	0.00	0.01	0.00	0.00	20.9
16	26	-0	344	0	0	0	-3487	--	--	16.08	16.08	0.29	0.06	0.00	0.02	0.00	0.00	20.9
17	26	-0	354	0	0	0	-3657	--	--	16.08	16.08	0.29	0.06	0.00	0.02	0.00	0.00	20.9
18	26	-0	-778	0	0	0	-3738	--	--	16.08	16.08	0.18	0.06	0.01	0.05	0.00	0.00	20.9
19	26	-0	921	0	0	0	-5219	--	--	16.08	16.08	0.18	0.09	0.01	0.06	0.00	0.00	20.9
20	26	-0	87	0	0	0	-4255	--	--	16.08	16.08	0.18	0.07	0.00	0.01	0.00	0.00	20.9
37	26	-0	-1259	0	0	0	-3422	--	--	16.08	16.08	0.18	0.06	0.01	0.08	0.00	0.00	20.9
38	26	-0	1573	0	0	0	-5907	--	--	16.08	16.08	0.18	0.10	0.01	0.10	0.00	0.00	20.9
39	26	-0	182	0	0	0	-4301	--	--	16.08	16.08	0.18	0.07	0.00	0.01	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	350	0	0	0	-4527	--	--	16.08	16.08	0.18	0.08	0.00	0.02	0.00	0.00	20.9
2	51	-0	3	0	0	0	-3157	--	--	16.08	16.08	0.29	0.05	0.00	0.00	0.00	0.00	20.9

3	51	-0	6	0	0	0	-3208	--	--	16.08	16.08	0.29	0.06	0.00	0.00	0.00	0.00	20.9
4	51	-0	532	0	0	0	-3756	--	--	16.08	16.08	0.29	0.07	0.00	0.03	0.00	0.00	20.9
5	51	-0	536	0	0	0	-3807	--	--	16.08	16.08	0.29	0.07	0.00	0.03	0.00	0.00	20.9
6	51	-0	185	0	0	0	-3308	--	--	16.08	16.08	0.29	0.06	0.00	0.01	0.00	0.00	20.9
7	51	-0	195	0	0	0	-3477	--	--	16.08	16.08	0.29	0.06	0.00	0.01	0.00	0.00	20.9
8	51	-0	344	0	0	0	-3487	--	--	16.08	16.08	0.29	0.06	0.00	0.02	0.00	0.00	20.9
9	51	-0	354	0	0	0	-3657	--	--	16.08	16.08	0.29	0.06	0.00	0.02	0.00	0.00	20.9
10	51	-0	3	0	0	0	-3157	--	--	16.08	16.08	0.29	0.05	0.00	0.00	0.00	0.00	20.9
11	51	-0	6	0	0	0	-3208	--	--	16.08	16.08	0.29	0.06	0.00	0.00	0.00	0.00	20.9
12	51	-0	532	0	0	0	-3756	--	--	16.08	16.08	0.29	0.07	0.00	0.03	0.00	0.00	20.9
13	51	-0	536	0	0	0	-3807	--	--	16.08	16.08	0.29	0.07	0.00	0.03	0.00	0.00	20.9
14	51	-0	185	0	0	0	-3308	--	--	16.08	16.08	0.29	0.06	0.00	0.01	0.00	0.00	20.9
15	51	-0	195	0	0	0	-3477	--	--	16.08	16.08	0.29	0.06	0.00	0.01	0.00	0.00	20.9
16	51	-0	344	0	0	0	-3487	--	--	16.08	16.08	0.29	0.06	0.00	0.02	0.00	0.00	20.9
17	51	-0	354	0	0	0	-3657	--	--	16.08	16.08	0.29	0.06	0.00	0.02	0.00	0.00	20.9
18	51	-0	-778	0	0	0	-3738	--	--	16.08	16.08	0.18	0.06	0.01	0.05	0.00	0.00	20.9
19	51	-0	921	0	0	0	-5219	--	--	16.08	16.08	0.18	0.09	0.01	0.06	0.00	0.00	20.9
20	51	-0	87	0	0	0	-4255	--	--	16.08	16.08	0.18	0.07	0.00	0.01	0.00	0.00	20.9
37	51	-0	-1259	0	0	0	-3422	--	--	16.08	16.08	0.18	0.06	0.01	0.08	0.00	0.00	20.9
38	51	-0	1573	0	0	0	-5907	--	--	16.08	16.08	0.18	0.10	0.01	0.10	0.00	0.00	20.9
39	51	-0	182	0	0	0	-4301	--	--	16.08	16.08	0.18	0.07	0.00	0.01	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 101 NI 1332 NF 1264 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	1353	0	0	0	-4347	--	--	16.08	16.08	0.18	0.07	0.01	0.08	0.00	0.00	20.9
2	0	-0	762	0	0	0	-3156	--	--	16.08	16.08	0.29	0.05	0.01	0.05	0.00	0.00	20.9
3	0	-0	775	0	0	0	-3205	--	--	16.08	16.08	0.29	0.06	0.01	0.05	0.00	0.00	20.9
4	0	-0	1306	0	0	0	-3483	--	--	16.08	16.08	0.29	0.06	0.01	0.08	0.00	0.00	20.9
5	0	-0	1319	0	0	0	-3532	--	--	16.08	16.08	0.29	0.06	0.01	0.08	0.00	0.00	20.9
6	0	-0	936	0	0	0	-3213	--	--	16.08	16.08	0.29	0.06	0.01	0.06	0.00	0.00	20.9
7	0	-0	982	0	0	0	-3377	--	--	16.08	16.08	0.29	0.06	0.01	0.06	0.00	0.00	20.9
8	0	-0	1100	0	0	0	-3311	--	--	16.08	16.08	0.29	0.06	0.01	0.07	0.00	0.00	20.9
9	0	-0	1145	0	0	0	-3475	--	--	16.08	16.08	0.29	0.06	0.01	0.07	0.00	0.00	20.9
10	0	-0	762	0	0	0	-3156	--	--	16.08	16.08	0.29	0.05	0.01	0.05	0.00	0.00	20.9
11	0	-0	775	0	0	0	-3205	--	--	16.08	16.08	0.29	0.06	0.01	0.05	0.00	0.00	20.9
12	0	-0	1306	0	0	0	-3483	--	--	16.08	16.08	0.29	0.06	0.01	0.08	0.00	0.00	20.9
13	0	-0	1319	0	0	0	-3532	--	--	16.08	16.08	0.29	0.06	0.01	0.08	0.00	0.00	20.9
14	0	-0	936	0	0	0	-3213	--	--	16.08	16.08	0.29	0.06	0.01	0.06	0.00	0.00	20.9
15	0	-0	982	0	0	0	-3377	--	--	16.08	16.08	0.29	0.06	0.01	0.06	0.00	0.00	20.9
16	0	-0	1100	0	0	0	-3311	--	--	16.08	16.08	0.29	0.06	0.01	0.07	0.00	0.00	20.9
17	0	-0	1145	0	0	0	-3475	--	--	16.08	16.08	0.29	0.06	0.01	0.07	0.00	0.00	20.9
18	0	-0	251	0	0	0	-3738	--	--	16.08	16.08	0.18	0.06	0.00	0.02	0.00	0.00	20.9
19	0	-0	1981	0	0	0	-4745	--	--	16.08	16.08	0.18	0.08	0.02	0.12	0.00	0.00	20.9
20	0	-0	1111	0	0	0	-4210	--	--	16.08	16.08	0.18	0.07	0.01	0.07	0.00	0.00	20.9
37	0	-0	-261	0	0	0	-3555	--	--	16.08	16.08	0.18	0.06	0.00	0.02	0.00	0.00	20.9
38	0	-0	2624	0	0	0	-5100	--	--	16.08	16.08	0.18	0.08	0.02	0.16	0.00	0.00	20.9
39	0	-0	1174	0	0	0	-4207	--	--	16.08	16.08	0.18	0.07	0.01	0.07	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	1353	0	0	0	-4347	--	--	16.08	16.08	0.18	0.07	0.01	0.08	0.00	0.00	20.9
2	26	-0	762	0	0	0	-3156	--	--	16.08	16.08	0.29	0.05	0.01	0.05	0.00	0.00	20.9
3	26	-0	775	0	0	0	-3205	--	--	16.08	16.08	0.29	0.06	0.01	0.05	0.00	0.00	20.9
4	26	-0	1306	0	0	0	-3483	--	--	16.08	16.08	0.29	0.06	0.01	0.08	0.00	0.00	20.9
5	26	-0	1319	0	0	0	-3532	--	--	16.08	16.08	0.29	0.06	0.01	0.08	0.00	0.00	20.9
6	26	-0	936	0	0	0	-3213	--	--	16.08	16.08	0.29	0.06	0.01	0.06	0.00	0.00	20.9
7	26	-0	982	0	0	0	-3377	--	--	16.08	16.08	0.29	0.06	0.01	0.06	0.00	0.00	20.9
8	26	-0	1100	0	0	0	-3311	--	--	16.08	16.08	0.29	0.06	0.01	0.07	0.00	0.00	20.9
9	26	-0	1145	0	0	0	-3475	--	--	16.08	16.08	0.29	0.06	0.01	0.07	0.00	0.00	20.9
10	26	-0	762	0	0	0	-3156	--	--	16.08	16.08	0.29	0.05	0.01	0.05	0.00	0.00	20.9
11	26	-0	775	0	0	0	-3205	--	--	16.08	16.08	0.29	0.06	0.01	0.05	0.00	0.00	20.9
12	26	-0	1306	0	0	0	-3483	--	--	16.08	16.08	0.29	0.06	0.01	0.08	0.00	0.00	20.9
13	26	-0	1319	0	0	0	-3532	--	--	16.08	16.08	0.29	0.06	0.01	0.08	0.00	0.00	20.9
14	26	-0	936	0	0	0	-3213	--	--	16.08	16.08	0.29	0.06	0.01	0.06	0.00	0.00	20.9
15	26	-0	982	0	0	0	-3377	--	--	16.08	16.08	0.29	0.06	0.01	0.06	0.00	0.00	20.9
16	26	-0	1100	0	0	0	-3311	--	--	16.08	16.08	0.29	0.06	0.01	0.07	0.00	0.00	20.9
17	26	-0	1145	0	0	0	-3475	--	--	16.08	16.08	0.29	0.06	0.01	0.07	0.00	0.00	20.9
18	26	-0	251	0	0	0	-3738	--	--	16.08	16.08	0.18	0.06	0.00	0.02	0.00	0.00	20.9
19	26	-0	1981	0	0	0	-4745	--	--	16.08	16.08	0.18	0.08	0.02	0.12	0.00	0.00	20.9
20	26	-0	1111	0	0	0	-4210	--	--	16.08	16.08	0.18	0.07	0.01	0.07	0.00	0.00	20.9
37	26	-0	-261	0	0	0	-3555	--	--	16.08	16.08	0.18	0.06	0.00	0.02	0.00	0.00	20.9
38	26	-0	2624	0	0	0	-5100	--	--	16.08	16.08	0.18	0.08	0.02	0.16	0.00	0.00	20.9
39	26	-0	1174	0	0	0	-4207	--	--	16.08	16.08	0.18	0.07	0.01	0.07	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	1353	0	0	0	-4347	--	--	16.08	16.08	0.18	0.07	0.01	0.08	0.00	0.00	20.9
2	51	-0	762	0	0	0	-3156	--	--	16.08	16.08	0.29	0.05	0.01	0.05	0.00	0.00	20.9
3	51	-0	775	0	0	0	-3205	--	--	16.08	16.08	0.29	0.06	0.01	0.05	0.00	0.00	20.9
4	51	-0	1306	0	0	0	-3483	--	--	16.08	16.08	0.29	0.06	0.01	0.08	0.00	0.00	20.9
5	51	-0	1319	0	0	0	-3532	--	--	16.08	16.08	0.29	0.06	0.01	0.08	0.00	0.00	20.9
6	51	-0	936	0	0	0	-3213	--	--	16.08	16.08	0.29	0.06	0.01	0.06	0.00	0.00	20.9
7	51	-0	982	0	0	0	-3377	--	--	16.08	16.08	0.29	0.06	0.01	0.06	0.00	0.00	20.9
8	51	-0	1100	0	0	0	-3311	--	--	16.08	16.08	0.29	0.06	0.01	0.07	0.00	0.00	20.9
9	51	-0	1145	0	0	0	-3475	--	--	16.08	16.08	0.29	0.06	0.01	0.07	0.00	0.00	20.9
10	51	-0	762	0	0	0	-3156	--	--	16.08	16.08	0.29	0.05	0.01	0.05	0.00	0.00	20.9
11	51	-0	775	0	0	0	-3205	--	--	16.08	16.08	0.29	0.06	0.01	0.05	0.00	0.00	20.9
12	51	-0	1306	0	0	0	-3483	--	--	16.08	16.08	0.29	0.06	0.01	0.08	0.00	0.00	20.9
13	51	-0	1319	0	0	0	-3532	--	--	16.08	16.08	0.29	0.06	0.01	0.08	0.00	0.00	20.9
14	51	-0	936	0	0	0	-3213	--	--	16.08	16.08	0.29	0.06	0.01	0.06	0.00	0.00	20.9
15	51	-0	982	0	0	0	-3377	--	--	16.08	16.08	0.29	0.06	0.01	0.06	0.00	0.00	20.9
16	51	-0	1100	0	0	0	-3311	--	--	16.08	16.08	0.29	0.06	0.01	0.07	0.00	0.00	20.9
17	51	-0	1145	0	0	0	-3475	--	--	16.08	16.08	0.29	0.06	0.01	0.07	0.00	0.00	20.9
18	51	-0	251	0	0	0	-3738	--	--	16.08	16.08	0.18	0.06	0.00	0.02	0.00	0.00	20.9
19	51	-0	1981	0	0	0	-4745	--	--	16.08	16.08	0.18	0.08	0.02	0.12	0.00	0.00	20.9
20	51	-0	1111	0	0	0	-4210	--	--	16.08	16.08	0.18	0.07	0.01	0.07	0.00	0.00	20.9
37	51	-0	-261	0	0	0	-3555	--	--	16.08	16.08	0.18	0.06	0.00	0.02	0.00	0.00	20.9
38	51	-0	2624	0	0	0	-5100	--	--	16.08	16.08	0.18	0.08	0.02	0.16	0.00	0.00	20.9
39	51	-0	1174	0	0	0	-4207	--	--	16.08	16.08	0.18	0.07	0.01	0.07	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 102 NI 1264 NF 1295 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	2354	0	0	0	-3652	--	--	16.08	16.08	0.18	0.06	0.02	0.15	0.00	0.00	20.9
2	0	-0	1520	0	0	0	-2764	--	--	16.08	16.08	0.29	0.05	0.01	0.10	0.00	0.00	20.9
3	0	-0	1543	0	0	0	-2806	--	--	16.08	16.08	0.29	0.05	0.01	0.10	0.00	0.00	20.9
4	0	-0	2078	0	0	0	-2812	--	--	16.08	16.08	0.29	0.05	0.02	0.13	0.00	0.00	20.9
5	0	-0	2102	0	0	0	-2854	--	--	16.08	16.08	0.29	0.05	0.02	0.13	0.00	0.00	20.9
6	0	-0	1687	0	0	0	-2732	--	--	16.08	16.08	0.29	0.05	0.01	0.11	0.00	0.00	20.9
7	0	-0	1766	0	0	0	-2872	--	--	16.08	16.08	0.29	0.05	0.01	0.11	0.00	0.00	20.9
8	0	-0	1855	0	0	0	-2746	--	--	16.08	16.08	0.29	0.05	0.02	0.12	0.00	0.00	20.9
9	0	-0	1934	0	0	0	-2887	--	--	16.08	16.08	0.29	0.05	0.02	0.12	0.00	0.00	20.9
10	0	-0	1520	0	0	0	-2764	--	--	16.08	16.08	0.29	0.05	0.01	0.10	0.00	0.00	20.9
11	0	-0	1543	0	0	0	-2806	--	--	16.08	16.08	0.29	0.05	0.01	0.10	0.00	0.00	20.9
12	0	-0	2078	0	0	0	-2812	--	--	16.08	16.08	0.29	0.05	0.02	0.13	0.00	0.00	20.9
13	0	-0	2102	0	0	0	-2854	--	--	16.08	16.08	0.29	0.05	0.02	0.13	0.00	0.00	20.9
14	0	-0	1687	0	0	0	-2732	--	--	16.08	16.08	0.29	0.05	0.01	0.11	0.00	0.00	20.9
15	0	-0	1766	0	0	0	-2872	--	--	16.08	16.08	0.29	0.05	0.01	0.11	0.00	0.00	20.9
16	0	-0	1855	0	0	0	-2746	--	--	16.08	16.08	0.29	0.05	0.02	0.12	0.00	0.00	20.9
17	0	-0	1934	0	0	0	-2887	--	--	16.08	16.08	0.29	0.05	0.02	0.12	0.00	0.00	20.9
18	0	-0	1282	0	0	0	-3610	--	--	16.08	16.08	0.18	0.06	0.01	0.08	0.00	0.00	20.9
19	0	-0	3044	0	0	0	-3727	--	--	16.08	16.08	0.18	0.06	0.03	0.19	0.00	0.00	20.9
20	0	-0	2138	0	0	0	-3639	--	--	16.08	16.08	0.18	0.06	0.02	0.13	0.00	0.00	20.9
37	0	-0	739	0	0	0	-3555	--	--	16.08	16.08	0.18	0.06	0.01	0.05	0.00	0.00	20.9
38	0	-0	3676	0	0	0	-3752	--	--	16.08	16.08	0.18	0.06	0.03	0.23	0.00	0.00	20.9
39	0	-0	2165	0	0	0	-3604	--	--	16.08	16.08	0.18	0.06	0.02	0.14	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	26	-0	2354	0	0	0	-3652	--	--	16.08	16.08	0.18	0.06	0.02	0.15	0.00	0.00	20.9
2	26	-0	1520	0	0	0	-2764	--	--	16.08	16.08	0.29	0.05	0.01	0.10	0.00	0.00	20.9
3	26	-0	1543	0	0	0	-2806	--	--	16.08	16.08	0.29	0.05	0.01	0.10	0.00	0.00	20.9
4	26	-0	2078	0	0	0	-2812	--	--	16.08	16.08	0.29	0.05	0.02	0.13	0.00	0.00	20.9
5	26	-0	2102	0	0	0	-2854	--	--	16.08	16.08	0.29	0.05	0.02	0.13	0.00	0.00	20.9
6	26	-0	1687	0	0	0	-2732	--	--	16.08	16.08	0.29	0.05	0.01	0.11	0.00	0.00	20.9
7	26	-0	1766	0	0	0	-2872	--	--	16.08	16.08	0.29	0.05	0.01	0.11	0.00	0.00	20.9
8	26	-0	1855	0	0	0	-2746	--	--	16.08	16.08	0.29	0.05	0.02	0.12	0.00	0.00	20.9
9	26	-0	1934	0	0	0	-2887	--	--	16.08	16.08	0.29	0.05	0.02	0.12	0.00	0.00	20.9
10	26	-0	1520	0	0	0	-2764	--	--	16.08	16.08	0.29	0.05	0.01	0.10	0.00	0.00	20.9
11	26	-0	1543	0	0	0	-2806	--	--	16.08	16.08	0.29	0.05	0.01	0.10	0.00	0.00	20.9
12	26	-0	2078	0	0	0	-2812	--	--	16.08	16.08	0.29	0.05	0.02	0.13	0.00	0.00	20.9
13	26	-0	2102	0	0	0	-2854	--	--	16.08	16.08	0.29	0.05	0.02	0.13	0.00	0.00	20.9
14	26	-0	1687	0	0	0	-2732	--	--	16.08	16.08	0.29	0.05	0.01	0.11	0.00	0.00	20.9
15	26	-0	1766	0	0	0	-2872	--	--	16.08	16.08	0.29	0.05	0.01	0.11	0.00	0.00	20.9
16	26	-0	1855	0	0	0	-2746	--	--	16.08	16.08	0.29	0.05	0.02	0.12	0.00	0.00	20.9
17	26	-0	1934	0	0	0	-2887	--	--	16.08	16.08	0.29	0.05	0.02	0.12	0.00	0.00	20.9
18	26	-0	1282	0	0	0	-3610	--	--	16.08	16.08	0.18	0.06	0.01	0.08	0.00	0.00	20.9
19	26	-0	3044	0	0	0	-3727	--	--	16.08	16.08	0.18	0.06	0.03	0.19	0.00	0.00	20.9
20	26	-0	2138	0	0	0	-3639	--	--	16.08	16.08	0.18	0.06	0.02	0.13	0.00	0.00	20.9
37	26	-0	739	0	0	0	-3555	--	--	16.08	16.08	0.18	0.06	0.01	0.05	0.00	0.00	20.9
38	26	-0	3676	0	0	0	-3752	--	--	16.08	16.08	0.18	0.06	0.03	0.23	0.00	0.00	20.9
39	26	-0	2165	0	0	0	-3604	--	--	16.08	16.08	0.18	0.06	0.02	0.14	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	51	-0	2354	0	0	0	-3652	--	--	16.08	16.08	0.18	0.06	0.02	0.15	0.00	0.00	20.9
2	51	-0	1520	0	0	0	-2764	--	--	16.08	16.08	0.29	0.05	0.01	0.10	0.00	0.00	20.9
3	51	-0	1543	0	0	0	-2806	--	--	16.08	16.08	0.29	0.05	0.01	0.10	0.00	0.00	20.9
4	51	-0	2078	0	0	0	-2812	--	--	16.08	16.08	0.29	0.05	0.02	0.13	0.00	0.00	20.9
5	51	-0	2102	0	0	0	-2854	--	--	16.08	16.08	0.29	0.05	0.02	0.13	0.00	0.00	20.9
6	51	-0	1687	0	0	0	-2732	--	--	16.08	16.08	0.29	0.05	0.01	0.11	0.00	0.00	20.9
7	51	-0	1766	0	0	0	-2872	--	--	16.08	16.08	0.29	0.05	0.01	0.11	0.00	0.00	20.9
8	51	-0	1855	0	0	0	-2746	--	--	16.08	16.08	0.29	0.05	0.02	0.12	0.00	0.00	20.9
9	51	-0	1934	0	0	0	-2887	--	--	16.08	16.08	0.29	0.05	0.02	0.12	0.00	0.00	20.9
10	51	-0	1520	0	0	0	-2764	--	--	16.08	16.08	0.29	0.05	0.01	0.10	0.00	0.00	20.9
11	51	-0	1543	0	0	0	-2806	--	--	16.08	16.08	0.29	0.05	0.01	0.10	0.00	0.00	20.9
12	51	-0	2078	0	0	0	-2812	--	--	16.08	16.08	0.29	0.05	0.02	0.13	0.00	0.00	20.9
13	51	-0	2102	0	0	0	-2854	--	--	16.08	16.08	0.29	0.05	0.02	0.13	0.00	0.00	20.9
14	51	-0	1687	0	0	0	-2732	--	--	16.08	16.08	0.29	0.05	0.01	0.11	0.00	0.00	20.9
15	51	-0	1766	0	0	0	-2872	--	--	16.08	16.08	0.29	0.05	0.01	0.11	0.00	0.00	20.9
16	51	-0	1855	0	0	0	-2746	--	--	16.08	16.08	0.29	0.05	0.02	0.12	0.00	0.00	20.9
17	51	-0	1934	0	0	0	-2887	--	--	16.08	16.08	0.29	0.05	0.02	0.12	0.00	0.00	20.9
18	51	-0	1282	0	0	0	-3610	--	--	16.08	16.08	0.18	0.06	0.01	0.08	0.00	0.00	20.9
19	51	-0	3044	0	0	0	-3727	--	--	16.08	16.08	0.18	0.06	0.03	0.19	0.00	0.00	20.9
20	51	-0	2138	0	0	0	-3639	--	--	16.08	16.08	0.18	0.06	0.02	0.13	0.00	0.00	20.9
37	51	-0	739	0	0	0	-3555	--	--	16.08	16.08	0.18	0.06	0.01	0.05	0.00	0.00	20.9
38	51	-0	3676	0	0	0	-3752	--	--	16.08	16.08	0.18	0.06	0.03	0.23	0.00	0.00	20.9
39	51	-0	2165	0	0	0	-3604	--	--	16.08	16.08	0.18	0.06	0.02	0.14	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 103 NI 1295 NF 1294 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	3372	0	0	0	-2443	--	--	16.08	16.08	0.18	0.04	0.03	0.21	0.00	0.00	20.9
2	0	-0	2291	0	0	0	-1984	--	--	16.08	16.08	0.29	0.03	0.02	0.14	0.00	0.00	20.9
3	0	-0	2324	0	0	0	-2014	--	--	16.08	16.08	0.29	0.03	0.02	0.15	0.00	0.00	20.9
4	0	-0	2864	0	0	0	-1745	--	--	16.08	16.08	0.29	0.03	0.02	0.18	0.00	0.00	20.9
5	0	-0	2897	0	0	0	-1775	--	--	16.08	16.08	0.29	0.03	0.02	0.18	0.00	0.00	20.9
6	0	-0	2452	0	0	0	-1865	--	--	16.08	16.08	0.29	0.03	0.02	0.15	0.00	0.00	20.9
7	0	-0	2564	0	0	0	-1965	--	--	16.08	16.08	0.29	0.03	0.02	0.16	0.00	0.00	20.9
8	0	-0	2624	0	0	0	-1793	--	--	16.08	16.08	0.29	0.03	0.02	0.16	0.00	0.00	20.9
9	0	-0	2736	0	0	0	-1894	--	--	16.08	16.08	0.29	0.03	0.02	0.17	0.00	0.00	20.9
10	0	-0	2291	0	0	0	-1984	--	--	16.08	16.08	0.29	0.03	0.02	0.14	0.00	0.00	20.9

11	0	-0	2324	0	0	0	-2014	--	--	16.08	16.08	0.29	0.03	0.02	0.15	0.00	0.00	20.9
12	0	-0	2864	0	0	0	-1745	--	--	16.08	16.08	0.29	0.03	0.02	0.18	0.00	0.00	20.9
13	0	-0	2897	0	0	0	-1775	--	--	16.08	16.08	0.29	0.03	0.02	0.18	0.00	0.00	20.9
14	0	-0	2452	0	0	0	-1865	--	--	16.08	16.08	0.29	0.03	0.02	0.15	0.00	0.00	20.9
15	0	-0	2564	0	0	0	-1965	--	--	16.08	16.08	0.29	0.03	0.02	0.16	0.00	0.00	20.9
16	0	-0	2624	0	0	0	-1793	--	--	16.08	16.08	0.29	0.03	0.02	0.16	0.00	0.00	20.9
17	0	-0	2736	0	0	0	-1894	--	--	16.08	16.08	0.29	0.03	0.02	0.17	0.00	0.00	20.9
18	0	-0	2335	0	0	0	-2951	--	--	16.08	16.08	0.18	0.05	0.02	0.15	0.00	0.00	20.9
19	0	-0	4129	0	0	0	-2164	--	--	16.08	16.08	0.18	0.04	0.03	0.26	0.00	0.00	20.9
20	0	-0	3185	0	0	0	-2541	--	--	16.08	16.08	0.18	0.04	0.03	0.20	0.00	0.00	20.9
37	0	-0	1758	0	0	0	-3176	--	--	16.08	16.08	0.18	0.05	0.01	0.11	0.00	0.00	20.9
38	0	-0	4748	0	0	0	-1864	--	--	16.08	16.08	0.18	0.03	0.04	0.30	0.00	0.00	20.9
39	0	-0	3175	0	0	0	-2492	--	--	16.08	16.08	0.18	0.04	0.03	0.20	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	3372	0	0	0	-2443	--	--	16.08	16.08	0.18	0.04	0.03	0.21	0.00	0.00	20.9
2	26	-0	2291	0	0	0	-1984	--	--	16.08	16.08	0.29	0.03	0.02	0.14	0.00	0.00	20.9
3	26	-0	2324	0	0	0	-2014	--	--	16.08	16.08	0.29	0.03	0.02	0.15	0.00	0.00	20.9
4	26	-0	2864	0	0	0	-1745	--	--	16.08	16.08	0.29	0.03	0.02	0.18	0.00	0.00	20.9
5	26	-0	2897	0	0	0	-1775	--	--	16.08	16.08	0.29	0.03	0.02	0.18	0.00	0.00	20.9
6	26	-0	2452	0	0	0	-1865	--	--	16.08	16.08	0.29	0.03	0.02	0.15	0.00	0.00	20.9
7	26	-0	2564	0	0	0	-1965	--	--	16.08	16.08	0.29	0.03	0.02	0.16	0.00	0.00	20.9
8	26	-0	2624	0	0	0	-1793	--	--	16.08	16.08	0.29	0.03	0.02	0.16	0.00	0.00	20.9
9	26	-0	2736	0	0	0	-1894	--	--	16.08	16.08	0.29	0.03	0.02	0.17	0.00	0.00	20.9
10	26	-0	2291	0	0	0	-1984	--	--	16.08	16.08	0.29	0.03	0.02	0.14	0.00	0.00	20.9
11	26	-0	2324	0	0	0	-2014	--	--	16.08	16.08	0.29	0.03	0.02	0.15	0.00	0.00	20.9
12	26	-0	2864	0	0	0	-1745	--	--	16.08	16.08	0.29	0.03	0.02	0.18	0.00	0.00	20.9
13	26	-0	2897	0	0	0	-1775	--	--	16.08	16.08	0.29	0.03	0.02	0.18	0.00	0.00	20.9
14	26	-0	2452	0	0	0	-1865	--	--	16.08	16.08	0.29	0.03	0.02	0.15	0.00	0.00	20.9
15	26	-0	2564	0	0	0	-1965	--	--	16.08	16.08	0.29	0.03	0.02	0.16	0.00	0.00	20.9
16	26	-0	2624	0	0	0	-1793	--	--	16.08	16.08	0.29	0.03	0.02	0.16	0.00	0.00	20.9
17	26	-0	2736	0	0	0	-1894	--	--	16.08	16.08	0.29	0.03	0.02	0.17	0.00	0.00	20.9
18	26	-0	2335	0	0	0	-2951	--	--	16.08	16.08	0.18	0.05	0.02	0.15	0.00	0.00	20.9
19	26	-0	4129	0	0	0	-2164	--	--	16.08	16.08	0.18	0.04	0.03	0.26	0.00	0.00	20.9
20	26	-0	3185	0	0	0	-2541	--	--	16.08	16.08	0.18	0.04	0.03	0.20	0.00	0.00	20.9
37	26	-0	1758	0	0	0	-3176	--	--	16.08	16.08	0.18	0.05	0.01	0.11	0.00	0.00	20.9
38	26	-0	4748	0	0	0	-1864	--	--	16.08	16.08	0.18	0.03	0.04	0.30	0.00	0.00	20.9
39	26	-0	3175	0	0	0	-2492	--	--	16.08	16.08	0.18	0.04	0.03	0.20	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	3372	0	0	0	-2443	--	--	16.08	16.08	0.18	0.04	0.03	0.21	0.00	0.00	20.9
2	51	-0	2291	0	0	0	-1984	--	--	16.08	16.08	0.29	0.03	0.02	0.14	0.00	0.00	20.9
3	51	-0	2324	0	0	0	-2014	--	--	16.08	16.08	0.29	0.03	0.02	0.15	0.00	0.00	20.9
4	51	-0	2864	0	0	0	-1745	--	--	16.08	16.08	0.29	0.03	0.02	0.18	0.00	0.00	20.9
5	51	-0	2897	0	0	0	-1775	--	--	16.08	16.08	0.29	0.03	0.02	0.18	0.00	0.00	20.9
6	51	-0	2452	0	0	0	-1865	--	--	16.08	16.08	0.29	0.03	0.02	0.15	0.00	0.00	20.9
7	51	-0	2564	0	0	0	-1965	--	--	16.08	16.08	0.29	0.03	0.02	0.16	0.00	0.00	20.9
8	51	-0	2624	0	0	0	-1793	--	--	16.08	16.08	0.29	0.03	0.02	0.16	0.00	0.00	20.9
9	51	-0	2736	0	0	0	-1894	--	--	16.08	16.08	0.29	0.03	0.02	0.17	0.00	0.00	20.9
10	51	-0	2291	0	0	0	-1984	--	--	16.08	16.08	0.29	0.03	0.02	0.14	0.00	0.00	20.9
11	51	-0	2324	0	0	0	-2014	--	--	16.08	16.08	0.29	0.03	0.02	0.15	0.00	0.00	20.9
12	51	-0	2864	0	0	0	-1745	--	--	16.08	16.08	0.29	0.03	0.02	0.18	0.00	0.00	20.9
13	51	-0	2897	0	0	0	-1775	--	--	16.08	16.08	0.29	0.03	0.02	0.18	0.00	0.00	20.9
14	51	-0	2452	0	0	0	-1865	--	--	16.08	16.08	0.29	0.03	0.02	0.15	0.00	0.00	20.9
15	51	-0	2564	0	0	0	-1965	--	--	16.08	16.08	0.29	0.03	0.02	0.16	0.00	0.00	20.9
16	51	-0	2624	0	0	0	-1793	--	--	16.08	16.08	0.29	0.03	0.02	0.16	0.00	0.00	20.9
17	51	-0	2736	0	0	0	-1894	--	--	16.08	16.08	0.29	0.03	0.02	0.17	0.00	0.00	20.9
18	51	-0	2335	0	0	0	-2951	--	--	16.08	16.08	0.18	0.05	0.02	0.15	0.00	0.00	20.9
19	51	-0	4129	0	0	0	-2164	--	--	16.08	16.08	0.18	0.04	0.03	0.26	0.00	0.00	20.9
20	51	-0	3185	0	0	0	-2541	--	--	16.08	16.08	0.18	0.04	0.03	0.20	0.00	0.00	20.9
37	51	-0	1758	0	0	0	-3176	--	--	16.08	16.08	0.18	0.05	0.01	0.11	0.00	0.00	20.9
38	51	-0	4748	0	0	0	574	--	--	16.08	16.08	0.00	0.01	0.04	0.30	0.00	0.00	20.9
39	51	-0	3175	0	0	0	-2492	--	--	16.08	16.08	0.18	0.04	0.03	0.20	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 104 NI 1294 NF 1334 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	4422	0	0	0	-711	--	--	16.08	16.08	0.18	0.01	0.04	0.28	0.00	0.00	20.9
2	0	-0	3086	0	0	0	-807	--	--	16.08	16.08	0.29	0.01	0.03	0.19	0.00	0.00	20.9
3	0	-0	3130	0	0	0	-820	--	--	16.08	16.08	0.29	0.01	0.03	0.20	0.00	0.00	20.9
4	0	-0	3673	0	0	0	-274	--	--	16.08	16.08	0.29	0.00	0.03	0.23	0.00	0.00	20.9
5	0	-0	3717	0	0	0	-287	--	--	16.08	16.08	0.29	0.00	0.03	0.23	0.00	0.00	20.9
6	0	-0	3240	0	0	0	-606	--	--	16.08	16.08	0.29	0.01	0.03	0.20	0.00	0.00	20.9
7	0	-0	3387	0	0	0	-648	--	--	16.08	16.08	0.29	0.01	0.03	0.21	0.00	0.00	20.9
8	0	-0	3416	0	0	0	-446	--	--	16.08	16.08	0.29	0.01	0.03	0.21	0.00	0.00	20.9
9	0	-0	3563	0	0	0	-488	--	--	16.08	16.08	0.29	0.01	0.03	0.22	0.00	0.00	20.9
10	0	-0	3086	0	0	0	-807	--	--	16.08	16.08	0.29	0.01	0.03	0.19	0.00	0.00	20.9
11	0	-0	3130	0	0	0	-820	--	--	16.08	16.08	0.29	0.01	0.03	0.20	0.00	0.00	20.9
12	0	-0	3673	0	0	0	-274	--	--	16.08	16.08	0.29	0.00	0.03	0.23	0.00	0.00	20.9
13	0	-0	3717	0	0	0	-287	--	--	16.08	16.08	0.29	0.00	0.03	0.23	0.00	0.00	20.9
14	0	-0	3240	0	0	0	-606	--	--	16.08	16.08	0.29	0.01	0.03	0.20	0.00	0.00	20.9
15	0	-0	3387	0	0	0	-648	--	--	16.08	16.08	0.29	0.01	0.03	0.21	0.00	0.00	20.9
16	0	-0	3416	0	0	0	-446	--	--	16.08	16.08	0.29	0.01	0.03	0.21	0.00	0.00	20.9
17	0	-0	3563	0	0	0	-488	--	--	16.08	16.08	0.29	0.01	0.03	0.22	0.00	0.00	20.9
18	0	-0	3425	0	0	0	-1752	--	--	16.08	16.08	0.18	0.03	0.03	0.21	0.00	0.00	20.9
19	0	-0	5247	0	0	0	-44	--	--	16.08	16.08	0.18	0.00	0.04	0.33	0.00	0.00	20.9
20	0	-0	4267	0	0	0	-905	--	--	16.08	16.08	0.18	0.01	0.04	0.27	0.00	0.00	20.9
37	0	-0	2813	0	0	0	-2273	--	--	16.08	16.08	0.18	0.04	0.02	0.18	0.00	0.00	20.9
38	0	-0	5850	0	0	0	574	--	--	16.08	16.08	0.00	0.01	0.05	0.37	0.00	0.00	20.9
39	0	-0	4216	0	0	0	-862	--	--	16.08	16.08	0.18	0.01	0.03	0.26	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	4422	0	0	0	5150	--	--	16.08	16.08	0.00	0.09	0.04	0.28	0.00	0.00	20.9
2	26	-0	3086	0	0	0	-807	--	--	16.08	16.08	0.29	0.01	0.03	0.19	0.00	0.00	20.9
3	26	-0	3130	0	0	0	-820	--	--	16.08	16.08	0.29	0.01	0.03	0.20	0.00	0.00	20.9
4	26	-0	3673	0	0	0	4595	--	--	16.08	16.08	0.10	0.08	0.03	0.23	0.00	0.00	20.9
5	26	-0	3717	0	0	0	4641	--	--	16.08	16.08	0.10	0.08	0.03	0.23	0.00	0.00	20.9
6	26	-0	3240	0	0	0	3689	--	--	16.08	16.08	0.10	0.07	0.03	0.20	0.00	0.00	20.9

7	26	-0	3387	0	0	0	3841	--	--	16.08	16.08	0.10	0.07	0.03	0.21	0.00	0.00	20.9
8	26	-0	3416	0	0	0	4082	--	--	16.08	16.08	0.10	0.07	0.03	0.21	0.00	0.00	20.9
9	26	-0	3563	0	0	0	4235	--	--	16.08	16.08	0.10	0.08	0.03	0.22	0.00	0.00	20.9
10	26	-0	3086	0	0	0	-807	--	--	16.08	16.08	0.29	0.01	0.03	0.19	0.00	0.00	20.9
11	26	-0	3130	0	0	0	-820	--	--	16.08	16.08	0.29	0.01	0.03	0.20	0.00	0.00	20.9
12	26	-0	3673	0	0	0	4595	--	--	16.08	16.08	0.10	0.08	0.03	0.23	0.00	0.00	20.9
13	26	-0	3717	0	0	0	4641	--	--	16.08	16.08	0.10	0.08	0.03	0.23	0.00	0.00	20.9
14	26	-0	3240	0	0	0	3689	--	--	16.08	16.08	0.10	0.07	0.03	0.20	0.00	0.00	20.9
15	26	-0	3387	0	0	0	3841	--	--	16.08	16.08	0.10	0.07	0.03	0.21	0.00	0.00	20.9
16	26	-0	3416	0	0	0	4082	--	--	16.08	16.08	0.10	0.07	0.03	0.21	0.00	0.00	20.9
17	26	-0	3563	0	0	0	4235	--	--	16.08	16.08	0.10	0.08	0.03	0.22	0.00	0.00	20.9
18	26	-0	3425	0	0	0	-1752	--	--	16.08	16.08	0.18	0.03	0.03	0.21	0.00	0.00	20.9
19	26	-0	5247	0	0	0	6912	--	--	16.08	16.08	0.00	0.12	0.04	0.33	0.00	0.00	20.9
20	26	-0	4267	0	0	0	4751	--	--	16.08	16.08	0.00	0.08	0.04	0.27	0.00	0.00	20.9
37	26	-0	2813	0	0	0	-2273	--	--	16.08	16.08	0.18	0.04	0.02	0.18	0.00	0.00	20.9
38	26	-0	5850	0	0	0	8329	--	--	16.08	16.08	0.00	0.14	0.05	0.37	0.00	0.00	20.9
39	26	-0	4216	0	0	0	4727	--	--	16.08	16.08	0.00	0.08	0.03	0.26	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	4422	0	0	0	1560	--	--	16.08	16.08	0.00	0.03	0.04	0.28	0.00	0.00	20.9
2	51	-0	3086	0	0	0	778	--	--	16.08	16.08	0.10	0.01	0.03	0.19	0.00	0.00	20.9
3	51	-0	3130	0	0	0	788	--	--	16.08	16.08	0.10	0.01	0.03	0.20	0.00	0.00	20.9
4	51	-0	3673	0	0	0	1613	--	--	16.08	16.08	0.10	0.03	0.03	0.23	0.00	0.00	20.9
5	51	-0	3717	0	0	0	1623	--	--	16.08	16.08	0.10	0.03	0.03	0.23	0.00	0.00	20.9
6	51	-0	3240	0	0	0	1058	--	--	16.08	16.08	0.10	0.02	0.03	0.20	0.00	0.00	20.9
7	51	-0	3387	0	0	0	1091	--	--	16.08	16.08	0.10	0.02	0.03	0.21	0.00	0.00	20.9
8	51	-0	3416	0	0	0	1309	--	--	16.08	16.08	0.10	0.02	0.03	0.21	0.00	0.00	20.9
9	51	-0	3563	0	0	0	1342	--	--	16.08	16.08	0.10	0.02	0.03	0.22	0.00	0.00	20.9
10	51	-0	3086	0	0	0	778	--	--	16.08	16.08	0.10	0.01	0.03	0.19	0.00	0.00	20.9
11	51	-0	3130	0	0	0	788	--	--	16.08	16.08	0.10	0.01	0.03	0.20	0.00	0.00	20.9
12	51	-0	3673	0	0	0	1613	--	--	16.08	16.08	0.10	0.03	0.03	0.23	0.00	0.00	20.9
13	51	-0	3717	0	0	0	1623	--	--	16.08	16.08	0.10	0.03	0.03	0.23	0.00	0.00	20.9
14	51	-0	3240	0	0	0	1058	--	--	16.08	16.08	0.10	0.02	0.03	0.20	0.00	0.00	20.9
15	51	-0	3387	0	0	0	1091	--	--	16.08	16.08	0.10	0.02	0.03	0.21	0.00	0.00	20.9
16	51	-0	3416	0	0	0	1309	--	--	16.08	16.08	0.10	0.02	0.03	0.21	0.00	0.00	20.9
17	51	-0	3563	0	0	0	1342	--	--	16.08	16.08	0.10	0.02	0.03	0.22	0.00	0.00	20.9
18	51	-0	3425	0	0	0	7	--	--	16.08	16.08	0.00	0.00	0.03	0.21	0.00	0.00	20.9
19	51	-0	5247	0	0	0	2652	--	--	16.08	16.08	0.00	0.05	0.04	0.33	0.00	0.00	20.9
20	51	-0	4267	0	0	0	1287	--	--	16.08	16.08	0.00	0.02	0.04	0.27	0.00	0.00	20.9
37	51	-0	2813	0	0	0	-2273	--	--	16.08	16.08	0.18	0.04	0.02	0.18	0.00	0.00	20.9
38	51	-0	5850	0	0	0	3580	--	--	16.08	16.08	0.00	0.06	0.05	0.37	0.00	0.00	20.9
39	51	-0	4216	0	0	0	1304	--	--	16.08	16.08	0.00	0.02	0.03	0.26	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 105 NI 1334 NF 1258 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	5508	0	0	0	1560	--	--	16.08	16.08	0.00	0.03	0.05	0.35	0.00	0.00	20.9
2	0	-0	3911	0	0	0	778	--	--	16.08	16.08	0.10	0.01	0.03	0.25	0.00	0.00	20.9
3	0	-0	3965	0	0	0	788	--	--	16.08	16.08	0.10	0.01	0.03	0.25	0.00	0.00	20.9
4	0	-0	4508	0	0	0	1613	--	--	16.08	16.08	0.10	0.03	0.04	0.28	0.00	0.00	20.9
5	0	-0	4563	0	0	0	1623	--	--	16.08	16.08	0.10	0.03	0.04	0.29	0.00	0.00	20.9
6	0	-0	4056	0	0	0	1058	--	--	16.08	16.08	0.10	0.02	0.03	0.25	0.00	0.00	20.9
7	0	-0	4238	0	0	0	1091	--	--	16.08	16.08	0.10	0.02	0.03	0.27	0.00	0.00	20.9
8	0	-0	4235	0	0	0	1309	--	--	16.08	16.08	0.10	0.02	0.03	0.27	0.00	0.00	20.9
9	0	-0	4417	0	0	0	1342	--	--	16.08	16.08	0.10	0.02	0.04	0.28	0.00	0.00	20.9
10	0	-0	3911	0	0	0	778	--	--	16.08	16.08	0.10	0.01	0.03	0.25	0.00	0.00	20.9
11	0	-0	3965	0	0	0	788	--	--	16.08	16.08	0.10	0.01	0.03	0.25	0.00	0.00	20.9
12	0	-0	4508	0	0	0	1613	--	--	16.08	16.08	0.10	0.03	0.04	0.28	0.00	0.00	20.9
13	0	-0	4563	0	0	0	1623	--	--	16.08	16.08	0.10	0.03	0.04	0.29	0.00	0.00	20.9
14	0	-0	4056	0	0	0	1058	--	--	16.08	16.08	0.10	0.02	0.03	0.25	0.00	0.00	20.9
15	0	-0	4238	0	0	0	1091	--	--	16.08	16.08	0.10	0.02	0.03	0.27	0.00	0.00	20.9
16	0	-0	4235	0	0	0	1309	--	--	16.08	16.08	0.10	0.02	0.03	0.27	0.00	0.00	20.9
17	0	-0	4417	0	0	0	1342	--	--	16.08	16.08	0.10	0.02	0.04	0.28	0.00	0.00	20.9
18	0	-0	4563	0	0	0	7	--	--	16.08	16.08	0.00	0.00	0.04	0.29	0.00	0.00	20.9
19	0	-0	6404	0	0	0	2652	--	--	16.08	16.08	0.00	0.05	0.05	0.40	0.00	0.00	20.9
20	0	-0	5390	0	0	0	1287	--	--	16.08	16.08	0.00	0.02	0.04	0.34	0.00	0.00	20.9
37	0	-0	3918	0	0	0	-828	--	--	16.08	16.08	0.18	0.01	0.03	0.25	0.00	0.00	20.9
38	0	-0	6984	0	0	0	3580	--	--	16.08	16.08	0.00	0.06	0.06	0.44	0.00	0.00	20.9
39	0	-0	5296	0	0	0	1304	--	--	16.08	16.08	0.00	0.02	0.04	0.33	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	5508	0	0	0	8861	--	--	16.08	16.08	0.00	0.15	0.05	0.35	0.00	0.00	20.9
2	26	-0	3911	0	0	0	5962	--	--	16.08	16.08	0.10	0.11	0.03	0.25	0.00	0.00	20.9
3	26	-0	3965	0	0	0	6043	--	--	16.08	16.08	0.10	0.11	0.03	0.25	0.00	0.00	20.9
4	26	-0	4508	0	0	0	7588	--	--	16.08	16.08	0.10	0.13	0.04	0.28	0.00	0.00	20.9
5	26	-0	4563	0	0	0	7671	--	--	16.08	16.08	0.10	0.14	0.04	0.29	0.00	0.00	20.9
6	26	-0	4056	0	0	0	6435	--	--	16.08	16.08	0.10	0.11	0.03	0.25	0.00	0.00	20.9
7	26	-0	4238	0	0	0	6709	--	--	16.08	16.08	0.10	0.12	0.03	0.27	0.00	0.00	20.9
8	26	-0	4235	0	0	0	6923	--	--	16.08	16.08	0.10	0.12	0.03	0.27	0.00	0.00	20.9
9	26	-0	4417	0	0	0	7197	--	--	16.08	16.08	0.10	0.13	0.04	0.28	0.00	0.00	20.9
10	26	-0	3911	0	0	0	5962	--	--	16.08	16.08	0.10	0.11	0.03	0.25	0.00	0.00	20.9
11	26	-0	3965	0	0	0	6043	--	--	16.08	16.08	0.10	0.11	0.03	0.25	0.00	0.00	20.9
12	26	-0	4508	0	0	0	7588	--	--	16.08	16.08	0.10	0.13	0.04	0.28	0.00	0.00	20.9
13	26	-0	4563	0	0	0	7671	--	--	16.08	16.08	0.10	0.14	0.04	0.29	0.00	0.00	20.9
14	26	-0	4056	0	0	0	6435	--	--	16.08	16.08	0.10	0.11	0.03	0.25	0.00	0.00	20.9
15	26	-0	4238	0	0	0	6709	--	--	16.08	16.08	0.10	0.12	0.03	0.27	0.00	0.00	20.9
16	26	-0	4235	0	0	0	6923	--	--	16.08	16.08	0.10	0.12	0.03	0.27	0.00	0.00	20.9
17	26	-0	4417	0	0	0	7197	--	--	16.08	16.08	0.10	0.13	0.04	0.28	0.00	0.00	20.9
18	26	-0	4563	0	0	0	6056	--	--	16.08	16.08	0.00	0.10	0.04	0.29	0.00	0.00	20.9
19	26	-0	6404	0	0	0	11141	--	--	16.08	16.08	0.00	0.19	0.05	0.40	0.00	0.00	20.9
20	26	-0	5390	0	0	0	8432	--	--	16.08	16.08	0.00	0.14	0.04	0.34	0.00	0.00	20.9
37	26	-0	3918	0	0	0	4365	--	--	16.08	16.08	0.00	0.07	0.03	0.25	0.00	0.00	20.9
38	26	-0	6984	0	0	0	12838	--	--	16.08	16.08	0.00	0.22	0.06	0.44	0.00	0.00	20.9
39	26	-0	5296	0	0	0	8324	--	--	16.08	16.08	0.00	0.14	0.04	0.33	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	5508	0	0	0	4389	--	--	16.08	16.08	0.00	0.07	0.05	0.35	0.00	0.00	20.9
2	51	-0	3911	0	0	0	2786	--	--	16.08	16.08	0.10	0.05	0.03	0.25	0.00	0.00	20.9

3	51	-0	3965	0	0	0	2824	--	--	16.08	16.08	0.10	0.05	0.03	0.25	0.00	0.00	20.9
4	51	-0	4508	0	0	0	3928	--	--	16.08	16.08	0.10	0.07	0.04	0.28	0.00	0.00	20.9
5	51	-0	4563	0	0	0	3966	--	--	16.08	16.08	0.10	0.07	0.04	0.29	0.00	0.00	20.9
6	51	-0	4056	0	0	0	3142	--	--	16.08	16.08	0.10	0.06	0.03	0.25	0.00	0.00	20.9
7	51	-0	4238	0	0	0	3268	--	--	16.08	16.08	0.10	0.06	0.03	0.27	0.00	0.00	20.9
8	51	-0	4235	0	0	0	3484	--	--	16.08	16.08	0.10	0.06	0.03	0.27	0.00	0.00	20.9
9	51	-0	4417	0	0	0	3611	--	--	16.08	16.08	0.10	0.06	0.04	0.28	0.00	0.00	20.9
10	51	-0	3911	0	0	0	2786	--	--	16.08	16.08	0.10	0.05	0.03	0.25	0.00	0.00	20.9
11	51	-0	3965	0	0	0	2824	--	--	16.08	16.08	0.10	0.05	0.03	0.25	0.00	0.00	20.9
12	51	-0	4508	0	0	0	3928	--	--	16.08	16.08	0.10	0.07	0.04	0.28	0.00	0.00	20.9
13	51	-0	4563	0	0	0	3966	--	--	16.08	16.08	0.10	0.07	0.04	0.29	0.00	0.00	20.9
14	51	-0	4056	0	0	0	3142	--	--	16.08	16.08	0.10	0.06	0.03	0.25	0.00	0.00	20.9
15	51	-0	4238	0	0	0	3268	--	--	16.08	16.08	0.10	0.06	0.03	0.27	0.00	0.00	20.9
16	51	-0	4235	0	0	0	3484	--	--	16.08	16.08	0.10	0.06	0.03	0.27	0.00	0.00	20.9
17	51	-0	4417	0	0	0	3611	--	--	16.08	16.08	0.10	0.06	0.04	0.28	0.00	0.00	20.9
18	51	-0	4563	0	0	0	2351	--	--	16.08	16.08	0.00	0.04	0.04	0.29	0.00	0.00	20.9
19	51	-0	6404	0	0	0	5941	--	--	16.08	16.08	0.00	0.10	0.05	0.40	0.00	0.00	20.9
20	51	-0	5390	0	0	0	4055	--	--	16.08	16.08	0.00	0.07	0.04	0.34	0.00	0.00	20.9
37	51	-0	3918	0	0	0	1184	--	--	16.08	16.08	0.00	0.02	0.03	0.25	0.00	0.00	20.9
38	51	-0	6984	0	0	0	7167	--	--	16.08	16.08	0.00	0.12	0.06	0.44	0.00	0.00	20.9
39	51	-0	5296	0	0	0	4024	--	--	16.08	16.08	0.00	0.07	0.04	0.33	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 106 NI 1258 NF 1289 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-5731	0	0	0	6978	--	--	16.08	16.08	0.00	0.12	0.05	0.36	0.00	0.00	20.9
2	0	-0	-4623	0	0	0	6060	--	--	16.08	16.08	0.10	0.11	0.04	0.29	0.00	0.00	20.9
3	0	-0	-4667	0	0	0	6099	--	--	16.08	16.08	0.10	0.11	0.04	0.29	0.00	0.00	20.9
4	0	-0	-4150	0	0	0	4636	--	--	16.08	16.08	0.10	0.08	0.03	0.26	0.00	0.00	20.9
5	0	-0	-4194	0	0	0	4676	--	--	16.08	16.08	0.10	0.08	0.03	0.26	0.00	0.00	20.9
6	0	-0	-4405	0	0	0	5515	--	--	16.08	16.08	0.10	0.10	0.04	0.28	0.00	0.00	20.9
7	0	-0	-4554	0	0	0	5647	--	--	16.08	16.08	0.10	0.10	0.04	0.29	0.00	0.00	20.9
8	0	-0	-4263	0	0	0	5088	--	--	16.08	16.08	0.10	0.09	0.04	0.27	0.00	0.00	20.9
9	0	-0	-4412	0	0	0	5220	--	--	16.08	16.08	0.10	0.09	0.04	0.28	0.00	0.00	20.9
10	0	-0	-4623	0	0	0	6060	--	--	16.08	16.08	0.10	0.11	0.04	0.29	0.00	0.00	20.9
11	0	-0	-4667	0	0	0	6099	--	--	16.08	16.08	0.10	0.11	0.04	0.29	0.00	0.00	20.9
12	0	-0	-4150	0	0	0	4636	--	--	16.08	16.08	0.10	0.08	0.03	0.26	0.00	0.00	20.9
13	0	-0	-4194	0	0	0	4676	--	--	16.08	16.08	0.10	0.08	0.03	0.26	0.00	0.00	20.9
14	0	-0	-4405	0	0	0	5515	--	--	16.08	16.08	0.10	0.10	0.04	0.28	0.00	0.00	20.9
15	0	-0	-4554	0	0	0	5647	--	--	16.08	16.08	0.10	0.10	0.04	0.29	0.00	0.00	20.9
16	0	-0	-4263	0	0	0	5088	--	--	16.08	16.08	0.10	0.09	0.04	0.27	0.00	0.00	20.9
17	0	-0	-4412	0	0	0	5220	--	--	16.08	16.08	0.10	0.09	0.04	0.28	0.00	0.00	20.9
18	0	-0	-7216	0	0	0	11020	--	--	16.08	16.08	0.00	0.19	0.06	0.45	0.00	0.00	20.9
19	0	-0	-5639	0	0	0	6156	--	--	16.08	16.08	0.00	0.10	0.05	0.35	0.00	0.00	20.9
20	0	-0	-6256	0	0	0	8249	--	--	16.08	16.08	0.00	0.14	0.05	0.39	0.00	0.00	20.9
37	0	-0	-7472	0	0	0	12060	--	--	16.08	16.08	0.00	0.21	0.06	0.47	0.00	0.00	20.9
38	0	-0	-4845	0	0	0	3955	--	--	16.08	16.08	0.00	0.07	0.04	0.30	0.00	0.00	20.9
39	0	-0	-5873	0	0	0	7443	--	--	16.08	16.08	0.00	0.13	0.05	0.37	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	-5731	0	0	0	6978	--	--	16.08	16.08	0.00	0.12	0.05	0.36	0.00	0.00	20.9
2	26	-0	-4623	0	0	0	6060	--	--	16.08	16.08	0.10	0.11	0.04	0.29	0.00	0.00	20.9
3	26	-0	-4667	0	0	0	6099	--	--	16.08	16.08	0.10	0.11	0.04	0.29	0.00	0.00	20.9
4	26	-0	-4150	0	0	0	4636	--	--	16.08	16.08	0.10	0.08	0.03	0.26	0.00	0.00	20.9
5	26	-0	-4194	0	0	0	4676	--	--	16.08	16.08	0.10	0.08	0.03	0.26	0.00	0.00	20.9
6	26	-0	-4405	0	0	0	5515	--	--	16.08	16.08	0.10	0.10	0.04	0.28	0.00	0.00	20.9
7	26	-0	-4554	0	0	0	5647	--	--	16.08	16.08	0.10	0.10	0.04	0.29	0.00	0.00	20.9
8	26	-0	-4263	0	0	0	5088	--	--	16.08	16.08	0.10	0.09	0.04	0.27	0.00	0.00	20.9
9	26	-0	-4412	0	0	0	5220	--	--	16.08	16.08	0.10	0.09	0.04	0.28	0.00	0.00	20.9
10	26	-0	-4623	0	0	0	6060	--	--	16.08	16.08	0.10	0.11	0.04	0.29	0.00	0.00	20.9
11	26	-0	-4667	0	0	0	6099	--	--	16.08	16.08	0.10	0.11	0.04	0.29	0.00	0.00	20.9
12	26	-0	-4150	0	0	0	4636	--	--	16.08	16.08	0.10	0.08	0.03	0.26	0.00	0.00	20.9
13	26	-0	-4194	0	0	0	4676	--	--	16.08	16.08	0.10	0.08	0.03	0.26	0.00	0.00	20.9
14	26	-0	-4405	0	0	0	5515	--	--	16.08	16.08	0.10	0.10	0.04	0.28	0.00	0.00	20.9
15	26	-0	-4554	0	0	0	5647	--	--	16.08	16.08	0.10	0.10	0.04	0.29	0.00	0.00	20.9
16	26	-0	-4263	0	0	0	5088	--	--	16.08	16.08	0.10	0.09	0.04	0.27	0.00	0.00	20.9
17	26	-0	-4412	0	0	0	5220	--	--	16.08	16.08	0.10	0.09	0.04	0.28	0.00	0.00	20.9
18	26	-0	-7216	0	0	0	11020	--	--	16.08	16.08	0.00	0.19	0.06	0.45	0.00	0.00	20.9
19	26	-0	-5639	0	0	0	6156	--	--	16.08	16.08	0.00	0.10	0.05	0.35	0.00	0.00	20.9
20	26	-0	-6256	0	0	0	8249	--	--	16.08	16.08	0.00	0.14	0.05	0.39	0.00	0.00	20.9
37	26	-0	-7472	0	0	0	12060	--	--	16.08	16.08	0.00	0.21	0.06	0.47	0.00	0.00	20.9
38	26	-0	-4845	0	0	0	3955	--	--	16.08	16.08	0.00	0.07	0.04	0.30	0.00	0.00	20.9
39	26	-0	-5873	0	0	0	7443	--	--	16.08	16.08	0.00	0.13	0.05	0.37	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	-5731	0	0	0	4035	--	--	16.08	16.08	0.00	0.07	0.05	0.36	0.00	0.00	20.9
2	51	-0	-4623	0	0	0	3685	--	--	16.08	16.08	0.10	0.07	0.04	0.29	0.00	0.00	20.9
3	51	-0	-4667	0	0	0	3702	--	--	16.08	16.08	0.10	0.07	0.04	0.29	0.00	0.00	20.9
4	51	-0	-4150	0	0	0	2505	--	--	16.08	16.08	0.10	0.04	0.03	0.26	0.00	0.00	20.9
5	51	-0	-4194	0	0	0	2522	--	--	16.08	16.08	0.10	0.04	0.03	0.26	0.00	0.00	20.9
6	51	-0	-4405	0	0	0	3253	--	--	16.08	16.08	0.10	0.06	0.04	0.28	0.00	0.00	20.9
7	51	-0	-4554	0	0	0	3309	--	--	16.08	16.08	0.10	0.06	0.04	0.29	0.00	0.00	20.9
8	51	-0	-4263	0	0	0	2898	--	--	16.08	16.08	0.10	0.05	0.04	0.27	0.00	0.00	20.9
9	51	-0	-4412	0	0	0	2954	--	--	16.08	16.08	0.10	0.05	0.04	0.28	0.00	0.00	20.9
10	51	-0	-4623	0	0	0	3685	--	--	16.08	16.08	0.10	0.07	0.04	0.29	0.00	0.00	20.9
11	51	-0	-4667	0	0	0	3702	--	--	16.08	16.08	0.10	0.07	0.04	0.29	0.00	0.00	20.9
12	51	-0	-4150	0	0	0	2505	--	--	16.08	16.08	0.10	0.04	0.03	0.26	0.00	0.00	20.9
13	51	-0	-4194	0	0	0	2522	--	--	16.08	16.08	0.10	0.04	0.03	0.26	0.00	0.00	20.9
14	51	-0	-4405	0	0	0	3253	--	--	16.08	16.08	0.10	0.06	0.04	0.28	0.00	0.00	20.9
15	51	-0	-4554	0	0	0	3309	--	--	16.08	16.08	0.10	0.06	0.04	0.29	0.00	0.00	20.9
16	51	-0	-4263	0	0	0	2898	--	--	16.08	16.08	0.10	0.05	0.04	0.27	0.00	0.00	20.9
17	51	-0	-4412	0	0	0	2954	--	--	16.08	16.08	0.10	0.05	0.04	0.28	0.00	0.00	20.9
18	51	-0	-7216	0	0	0	7315	--	--	16.08	16.08	0.00	0.12	0.06	0.45	0.00	0.00	20.9
19	51	-0	-5639	0	0	0	3259	--	--	16.08	16.08	0.00	0.06	0.05	0.35	0.00	0.00	20.9
20	51	-0	-6256	0	0	0	5035	--	--	16.08	16.08	0.00	0.09	0.05	0.39	0.00	0.00	20.9
37	51	-0	-7472	0	0	0	8227	--	--	16.08	16.08	0.00	0.14	0.06	0.47	0.00	0.00	20.9
38	51	-0	-4845	0	0	0	1467	--	--	16.08	16.08	0.00	0.03	0.04	0.30	0.00	0.00	20.9
39	51	-0	-5873	0	0	0	4427	--	--	16.08	16.08	0.00	0.08	0.05	0.37	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 107 NI 1289 NF 1329 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-4633	0	0	0	4035	--	--	16.08	16.08	0.00	0.07	0.04	0.29	0.00	0.00	20.9
2	0	-0	-3782	0	0	0	3685	--	--	16.08	16.08	0.10	0.07	0.03	0.24	0.00	0.00	20.9
3	0	-0	-3816	0	0	0	3702	--	--	16.08	16.08	0.10	0.07	0.03	0.24	0.00	0.00	20.9
4	0	-0	-3312	0	0	0	2505	--	--	16.08	16.08	0.10	0.04	0.03	0.21	0.00	0.00	20.9
5	0	-0	-3346	0	0	0	2522	--	--	16.08	16.08	0.10	0.04	0.03	0.21	0.00	0.00	20.9
6	0	-0	-3578	0	0	0	3253	--	--	16.08	16.08	0.10	0.06	0.03	0.22	0.00	0.00	20.9
7	0	-0	-3691	0	0	0	3309	--	--	16.08	16.08	0.10	0.06	0.03	0.23	0.00	0.00	20.9
8	0	-0	-3436	0	0	0	2898	--	--	16.08	16.08	0.10	0.05	0.03	0.22	0.00	0.00	20.9
9	0	-0	-3550	0	0	0	2954	--	--	16.08	16.08	0.10	0.05	0.03	0.22	0.00	0.00	20.9
10	0	-0	-3782	0	0	0	3685	--	--	16.08	16.08	0.10	0.07	0.03	0.24	0.00	0.00	20.9
11	0	-0	-3816	0	0	0	3702	--	--	16.08	16.08	0.10	0.07	0.03	0.24	0.00	0.00	20.9
12	0	-0	-3312	0	0	0	2505	--	--	16.08	16.08	0.10	0.04	0.03	0.21	0.00	0.00	20.9
13	0	-0	-3346	0	0	0	2522	--	--	16.08	16.08	0.10	0.04	0.03	0.21	0.00	0.00	20.9
14	0	-0	-3578	0	0	0	3253	--	--	16.08	16.08	0.10	0.06	0.03	0.22	0.00	0.00	20.9
15	0	-0	-3691	0	0	0	3309	--	--	16.08	16.08	0.10	0.06	0.03	0.23	0.00	0.00	20.9
16	0	-0	-3436	0	0	0	2898	--	--	16.08	16.08	0.10	0.05	0.03	0.22	0.00	0.00	20.9
17	0	-0	-3550	0	0	0	2954	--	--	16.08	16.08	0.10	0.05	0.03	0.22	0.00	0.00	20.9
18	0	-0	-6033	0	0	0	7315	--	--	16.08	16.08	0.00	0.12	0.05	0.38	0.00	0.00	20.9
19	0	-0	-4483	0	0	0	3259	--	--	16.08	16.08	0.00	0.06	0.04	0.28	0.00	0.00	20.9
20	0	-0	-5111	0	0	0	5035	--	--	16.08	16.08	0.00	0.09	0.04	0.32	0.00	0.00	20.9
37	0	-0	-6313	0	0	0	8227	--	--	16.08	16.08	0.00	0.14	0.05	0.40	0.00	0.00	20.9
38	0	-0	-3729	0	0	0	1467	--	--	16.08	16.08	0.00	0.03	0.03	0.23	0.00	0.00	20.9
39	0	-0	-4776	0	0	0	4427	--	--	16.08	16.08	0.00	0.08	0.04	0.30	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	26	-0	-4633	0	0	0	4035	--	--	16.08	16.08	0.00	0.07	0.04	0.29	0.00	0.00	20.9
2	26	-0	-3782	0	0	0	3685	--	--	16.08	16.08	0.10	0.07	0.03	0.24	0.00	0.00	20.9
3	26	-0	-3816	0	0	0	3702	--	--	16.08	16.08	0.10	0.07	0.03	0.24	0.00	0.00	20.9
4	26	-0	-3312	0	0	0	2505	--	--	16.08	16.08	0.10	0.04	0.03	0.21	0.00	0.00	20.9
5	26	-0	-3346	0	0	0	2522	--	--	16.08	16.08	0.10	0.04	0.03	0.21	0.00	0.00	20.9
6	26	-0	-3578	0	0	0	3253	--	--	16.08	16.08	0.10	0.06	0.03	0.22	0.00	0.00	20.9
7	26	-0	-3691	0	0	0	3309	--	--	16.08	16.08	0.10	0.06	0.03	0.23	0.00	0.00	20.9
8	26	-0	-3436	0	0	0	2898	--	--	16.08	16.08	0.10	0.05	0.03	0.22	0.00	0.00	20.9
9	26	-0	-3550	0	0	0	2954	--	--	16.08	16.08	0.10	0.05	0.03	0.22	0.00	0.00	20.9
10	26	-0	-3782	0	0	0	3685	--	--	16.08	16.08	0.10	0.07	0.03	0.24	0.00	0.00	20.9
11	26	-0	-3816	0	0	0	3702	--	--	16.08	16.08	0.10	0.07	0.03	0.24	0.00	0.00	20.9
12	26	-0	-3312	0	0	0	2505	--	--	16.08	16.08	0.10	0.04	0.03	0.21	0.00	0.00	20.9
13	26	-0	-3346	0	0	0	2522	--	--	16.08	16.08	0.10	0.04	0.03	0.21	0.00	0.00	20.9
14	26	-0	-3578	0	0	0	3253	--	--	16.08	16.08	0.10	0.06	0.03	0.22	0.00	0.00	20.9
15	26	-0	-3691	0	0	0	3309	--	--	16.08	16.08	0.10	0.06	0.03	0.23	0.00	0.00	20.9
16	26	-0	-3436	0	0	0	2898	--	--	16.08	16.08	0.10	0.05	0.03	0.22	0.00	0.00	20.9
17	26	-0	-3550	0	0	0	2954	--	--	16.08	16.08	0.10	0.05	0.03	0.22	0.00	0.00	20.9
18	26	-0	-6033	0	0	0	7315	--	--	16.08	16.08	0.00	0.12	0.05	0.38	0.00	0.00	20.9
19	26	-0	-4483	0	0	0	3259	--	--	16.08	16.08	0.00	0.06	0.04	0.28	0.00	0.00	20.9
20	26	-0	-5111	0	0	0	5035	--	--	16.08	16.08	0.00	0.09	0.04	0.32	0.00	0.00	20.9
37	26	-0	-6313	0	0	0	8227	--	--	16.08	16.08	0.00	0.14	0.05	0.40	0.00	0.00	20.9
38	26	-0	-3729	0	0	0	1467	--	--	16.08	16.08	0.00	0.03	0.03	0.23	0.00	0.00	20.9
39	26	-0	-4776	0	0	0	4427	--	--	16.08	16.08	0.00	0.08	0.04	0.30	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	51	-0	-4633	0	0	0	1655	--	--	16.08	16.08	0.00	0.03	0.04	0.29	0.00	0.00	20.9
2	51	-0	-3782	0	0	0	1743	--	--	16.08	16.08	0.10	0.03	0.03	0.24	0.00	0.00	20.9
3	51	-0	-3816	0	0	0	1742	--	--	16.08	16.08	0.10	0.03	0.03	0.24	0.00	0.00	20.9
4	51	-0	-3312	0	0	0	804	--	--	16.08	16.08	0.10	0.01	0.03	0.21	0.00	0.00	20.9
5	51	-0	-3346	0	0	0	803	--	--	16.08	16.08	0.10	0.01	0.03	0.21	0.00	0.00	20.9
6	51	-0	-3578	0	0	0	1415	--	--	16.08	16.08	0.10	0.03	0.03	0.22	0.00	0.00	20.9
7	51	-0	-3691	0	0	0	1413	--	--	16.08	16.08	0.10	0.03	0.03	0.23	0.00	0.00	20.9
8	51	-0	-3436	0	0	0	1133	--	--	16.08	16.08	0.10	0.02	0.03	0.22	0.00	0.00	20.9
9	51	-0	-3550	0	0	0	1131	--	--	16.08	16.08	0.10	0.02	0.03	0.22	0.00	0.00	20.9
10	51	-0	-3782	0	0	0	1743	--	--	16.08	16.08	0.10	0.03	0.03	0.24	0.00	0.00	20.9
11	51	-0	-3816	0	0	0	1742	--	--	16.08	16.08	0.10	0.03	0.03	0.24	0.00	0.00	20.9
12	51	-0	-3312	0	0	0	804	--	--	16.08	16.08	0.10	0.01	0.03	0.21	0.00	0.00	20.9
13	51	-0	-3346	0	0	0	803	--	--	16.08	16.08	0.10	0.01	0.03	0.21	0.00	0.00	20.9
14	51	-0	-3578	0	0	0	1415	--	--	16.08	16.08	0.10	0.03	0.03	0.22	0.00	0.00	20.9
15	51	-0	-3691	0	0	0	1413	--	--	16.08	16.08	0.10	0.03	0.03	0.23	0.00	0.00	20.9
16	51	-0	-3436	0	0	0	1133	--	--	16.08	16.08	0.10	0.02	0.03	0.22	0.00	0.00	20.9
17	51	-0	-3550	0	0	0	1131	--	--	16.08	16.08	0.10	0.02	0.03	0.22	0.00	0.00	20.9
18	51	-0	-6033	0	0	0	4216	--	--	16.08	16.08	0.00	0.07	0.05	0.38	0.00	0.00	20.9
19	51	-0	-4483	0	0	0	956	--	--	16.08	16.08	0.00	0.02	0.04	0.28	0.00	0.00	20.9
20	51	-0	-5111	0	0	0	2410	--	--	16.08	16.08	0.00	0.04	0.04	0.32	0.00	0.00	20.9
37	51	-0	-6313	0	0	0	4984	--	--	16.08	16.08	0.00	0.08	0.05	0.40	0.00	0.00	20.9
38	51	-0	-3729	0	0	0	-449	--	--	16.08	16.08	0.18	0.01	0.03	0.23	0.00	0.00	20.9
39	51	-0	-4776	0	0	0	1973	--	--	16.08	16.08	0.00	0.03	0.04	0.30	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 108 NI 1329 NF 1328 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-3571	0	0	0	1655	--	--	16.08	16.08	0.00	0.03	0.03	0.22	0.00	0.00	20.9
2	0	-0	-2968	0	0	0	1743	--	--	16.08	16.08	0.10	0.03	0.02	0.19	0.00	0.00	20.9
3	0	-0	-2992	0	0	0	1742	--	--	16.08	16.08	0.10	0.03	0.02	0.19	0.00	0.00	20.9
4	0	-0	-2502	0	0	0	804	--	--	16.08	16.08	0.10	0.01	0.02	0.16	0.00	0.00	20.9
5	0	-0	-2526	0	0	0	803	--	--	16.08	16.08	0.10	0.01	0.02	0.16	0.00	0.00	20.9
6	0	-0	-2777	0	0	0	1415	--	--	16.08	16.08	0.10	0.03	0.02	0.17	0.00	0.00	20.9
7	0	-0	-2856	0	0	0	1413	--	--	16.08	16.08	0.10	0.03	0.02	0.18	0.00	0.00	20.9
8	0	-0	-2637	0	0	0	1133	--	--	16.08	16.08	0.10	0.02	0.02	0.17	0.00	0.00	20.9
9	0	-0	-2717	0	0	0	1131	--	--	16.08	16.08	0.10	0.02	0.02	0.17	0.00	0.00	20.9
10	0	-0	-2968	0	0	0	1743	--	--	16.08	16.08	0.10	0.03	0.02	0.19	0.00	0.00	20.9

11	0	-0	-2992	0	0	0	1742	--	--	16.08	16.08	0.10	0.03	0.02	0.19	0.00	0.00	20.9
12	0	-0	-2502	0	0	0	804	--	--	16.08	16.08	0.10	0.01	0.02	0.16	0.00	0.00	20.9
13	0	-0	-2526	0	0	0	803	--	--	16.08	16.08	0.10	0.01	0.02	0.16	0.00	0.00	20.9
14	0	-0	-2777	0	0	0	1415	--	--	16.08	16.08	0.10	0.03	0.02	0.17	0.00	0.00	20.9
15	0	-0	-2856	0	0	0	1413	--	--	16.08	16.08	0.10	0.03	0.02	0.18	0.00	0.00	20.9
16	0	-0	-2637	0	0	0	1133	--	--	16.08	16.08	0.10	0.02	0.02	0.17	0.00	0.00	20.9
17	0	-0	-2717	0	0	0	1131	--	--	16.08	16.08	0.10	0.02	0.02	0.17	0.00	0.00	20.9
18	0	-0	-4889	0	0	0	4216	--	--	16.08	16.08	0.00	0.07	0.04	0.31	0.00	0.00	20.9
19	0	-0	-3368	0	0	0	956	--	--	16.08	16.08	0.00	0.02	0.03	0.21	0.00	0.00	20.9
20	0	-0	-4004	0	0	0	2410	--	--	16.08	16.08	0.00	0.04	0.03	0.25	0.00	0.00	20.9
37	0	-0	-5189	0	0	0	4984	--	--	16.08	16.08	0.00	0.08	0.04	0.33	0.00	0.00	20.9
38	0	-0	-2654	0	0	0	-1812	--	--	16.08	16.08	0.18	0.03	0.02	0.17	0.00	0.00	20.9
39	0	-0	-3714	0	0	0	1973	--	--	16.08	16.08	0.00	0.03	0.03	0.23	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	-3571	0	0	0	1655	--	--	16.08	16.08	0.00	0.03	0.03	0.22	0.00	0.00	20.9
2	26	-0	-2968	0	0	0	1743	--	--	16.08	16.08	0.10	0.03	0.02	0.19	0.00	0.00	20.9
3	26	-0	-2992	0	0	0	1742	--	--	16.08	16.08	0.10	0.03	0.02	0.19	0.00	0.00	20.9
4	26	-0	-2502	0	0	0	804	--	--	16.08	16.08	0.10	0.01	0.02	0.16	0.00	0.00	20.9
5	26	-0	-2526	0	0	0	803	--	--	16.08	16.08	0.10	0.01	0.02	0.16	0.00	0.00	20.9
6	26	-0	-2777	0	0	0	1415	--	--	16.08	16.08	0.10	0.03	0.02	0.17	0.00	0.00	20.9
7	26	-0	-2856	0	0	0	1413	--	--	16.08	16.08	0.10	0.03	0.02	0.18	0.00	0.00	20.9
8	26	-0	-2637	0	0	0	1133	--	--	16.08	16.08	0.10	0.02	0.02	0.17	0.00	0.00	20.9
9	26	-0	-2717	0	0	0	1131	--	--	16.08	16.08	0.10	0.02	0.02	0.17	0.00	0.00	20.9
10	26	-0	-2968	0	0	0	1743	--	--	16.08	16.08	0.10	0.03	0.02	0.19	0.00	0.00	20.9
11	26	-0	-2992	0	0	0	1742	--	--	16.08	16.08	0.10	0.03	0.02	0.19	0.00	0.00	20.9
12	26	-0	-2502	0	0	0	804	--	--	16.08	16.08	0.10	0.01	0.02	0.16	0.00	0.00	20.9
13	26	-0	-2526	0	0	0	803	--	--	16.08	16.08	0.10	0.01	0.02	0.16	0.00	0.00	20.9
14	26	-0	-2777	0	0	0	1415	--	--	16.08	16.08	0.10	0.03	0.02	0.17	0.00	0.00	20.9
15	26	-0	-2856	0	0	0	1413	--	--	16.08	16.08	0.10	0.03	0.02	0.18	0.00	0.00	20.9
16	26	-0	-2637	0	0	0	1133	--	--	16.08	16.08	0.10	0.02	0.02	0.17	0.00	0.00	20.9
17	26	-0	-2717	0	0	0	1131	--	--	16.08	16.08	0.10	0.02	0.02	0.17	0.00	0.00	20.9
18	26	-0	-4889	0	0	0	4216	--	--	16.08	16.08	0.00	0.07	0.04	0.31	0.00	0.00	20.9
19	26	-0	-3368	0	0	0	956	--	--	16.08	16.08	0.00	0.02	0.03	0.21	0.00	0.00	20.9
20	26	-0	-4004	0	0	0	2410	--	--	16.08	16.08	0.00	0.04	0.03	0.25	0.00	0.00	20.9
37	26	-0	-5189	0	0	0	4984	--	--	16.08	16.08	0.00	0.08	0.04	0.33	0.00	0.00	20.9
38	26	-0	-2654	0	0	0	-1812	--	--	16.08	16.08	0.18	0.03	0.02	0.17	0.00	0.00	20.9
39	26	-0	-3714	0	0	0	1973	--	--	16.08	16.08	0.00	0.03	0.03	0.23	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	-3571	0	0	0	-179	--	--	16.08	16.08	0.18	0.00	0.03	0.22	0.00	0.00	20.9
2	51	-0	-2968	0	0	0	219	--	--	16.08	16.08	0.10	0.00	0.02	0.19	0.00	0.00	20.9
3	51	-0	-2992	0	0	0	206	--	--	16.08	16.08	0.10	0.00	0.02	0.19	0.00	0.00	20.9
4	51	-0	-2502	0	0	0	-482	--	--	16.08	16.08	0.29	0.01	0.02	0.16	0.00	0.00	20.9
5	51	-0	-2526	0	0	0	-495	--	--	16.08	16.08	0.29	0.01	0.02	0.16	0.00	0.00	20.9
6	51	-0	-2777	0	0	0	-11	--	--	16.08	16.08	0.29	0.00	0.02	0.17	0.00	0.00	20.9
7	51	-0	-2856	0	0	0	-54	--	--	16.08	16.08	0.29	0.00	0.02	0.18	0.00	0.00	20.9
8	51	-0	-2637	0	0	0	-222	--	--	16.08	16.08	0.29	0.00	0.02	0.17	0.00	0.00	20.9
9	51	-0	-2717	0	0	0	-265	--	--	16.08	16.08	0.29	0.00	0.02	0.17	0.00	0.00	20.9
10	51	-0	-2968	0	0	0	219	--	--	16.08	16.08	0.10	0.00	0.02	0.19	0.00	0.00	20.9
11	51	-0	-2992	0	0	0	206	--	--	16.08	16.08	0.10	0.00	0.02	0.19	0.00	0.00	20.9
12	51	-0	-2502	0	0	0	-482	--	--	16.08	16.08	0.29	0.01	0.02	0.16	0.00	0.00	20.9
13	51	-0	-2526	0	0	0	-495	--	--	16.08	16.08	0.29	0.01	0.02	0.16	0.00	0.00	20.9
14	51	-0	-2777	0	0	0	-11	--	--	16.08	16.08	0.29	0.00	0.02	0.17	0.00	0.00	20.9
15	51	-0	-2856	0	0	0	-54	--	--	16.08	16.08	0.29	0.00	0.02	0.18	0.00	0.00	20.9
16	51	-0	-2637	0	0	0	-222	--	--	16.08	16.08	0.29	0.00	0.02	0.17	0.00	0.00	20.9
17	51	-0	-2717	0	0	0	-265	--	--	16.08	16.08	0.29	0.00	0.02	0.17	0.00	0.00	20.9
18	51	-0	-4889	0	0	0	1705	--	--	16.08	16.08	0.00	0.03	0.04	0.31	0.00	0.00	20.9
19	51	-0	-3368	0	0	0	-773	--	--	16.08	16.08	0.18	0.01	0.03	0.21	0.00	0.00	20.9
20	51	-0	-4004	0	0	0	353	--	--	16.08	16.08	0.00	0.01	0.03	0.25	0.00	0.00	20.9
37	51	-0	-5189	0	0	0	2318	--	--	16.08	16.08	0.00	0.04	0.04	0.33	0.00	0.00	20.9
38	51	-0	-2654	0	0	0	-1812	--	--	16.08	16.08	0.18	0.03	0.02	0.17	0.00	0.00	20.9
39	51	-0	-3714	0	0	0	66	--	--	16.08	16.08	0.00	0.00	0.03	0.23	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 109 NI 1328 NF 1327 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-2550	0	0	0	-1489	--	--	16.08	16.08	0.18	0.02	0.02	0.16	0.00	0.00	20.9
2	0	-0	-2187	0	0	0	219	--	--	16.08	16.08	0.10	0.00	0.02	0.14	0.00	0.00	20.9
3	0	-0	-2201	0	0	0	206	--	--	16.08	16.08	0.10	0.00	0.02	0.14	0.00	0.00	20.9
4	0	-0	-1722	0	0	0	-1366	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
5	0	-0	-1736	0	0	0	-1386	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
6	0	-0	-2008	0	0	0	-1043	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
7	0	-0	-2054	0	0	0	-1110	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
8	0	-0	-1869	0	0	0	-1181	--	--	16.08	16.08	0.29	0.02	0.02	0.12	0.00	0.00	20.9
9	0	-0	-1915	0	0	0	-1248	--	--	16.08	16.08	0.29	0.02	0.02	0.12	0.00	0.00	20.9
10	0	-0	-2187	0	0	0	219	--	--	16.08	16.08	0.10	0.00	0.02	0.14	0.00	0.00	20.9
11	0	-0	-2201	0	0	0	206	--	--	16.08	16.08	0.10	0.00	0.02	0.14	0.00	0.00	20.9
12	0	-0	-1722	0	0	0	-1366	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
13	0	-0	-1736	0	0	0	-1386	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
14	0	-0	-2008	0	0	0	-1043	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
15	0	-0	-2054	0	0	0	-1110	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
16	0	-0	-1869	0	0	0	-1181	--	--	16.08	16.08	0.29	0.02	0.02	0.12	0.00	0.00	20.9
17	0	-0	-1915	0	0	0	-1248	--	--	16.08	16.08	0.29	0.02	0.02	0.12	0.00	0.00	20.9
18	0	-0	-3799	0	0	0	1705	--	--	16.08	16.08	0.00	0.03	0.03	0.24	0.00	0.00	20.9
19	0	-0	-2294	0	0	0	-1951	--	--	16.08	16.08	0.18	0.03	0.02	0.14	0.00	0.00	20.9
20	0	-0	-2943	0	0	0	353	--	--	16.08	16.08	0.00	0.01	0.02	0.18	0.00	0.00	20.9
37	0	-0	-4122	0	0	0	2318	--	--	16.08	16.08	0.00	0.04	0.03	0.26	0.00	0.00	20.9
38	0	-0	-1613	0	0	0	-2640	--	--	16.08	16.08	0.18	0.04	0.01	0.10	0.00	0.00	20.9
39	0	-0	-2694	0	0	0	66	--	--	16.08	16.08	0.00	0.00	0.02	0.17	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	-2550	0	0	0	-1489	--	--	16.08	16.08	0.18	0.02	0.02	0.16	0.00	0.00	20.9
2	26	-0	-2187	0	0	0	-905	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
3	26	-0	-2201	0	0	0	-925	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
4	26	-0	-1722	0	0	0	-1366	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
5	26	-0	-1736	0	0	0	-1386	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
6	26	-0	-2008	0	0	0	-1043	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9

7	26	-0	-2054	0	0	0	-1110	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
8	26	-0	-1869	0	0	0	-1181	--	--	16.08	16.08	0.29	0.02	0.02	0.12	0.00	0.00	20.9
9	26	-0	-1915	0	0	0	-1248	--	--	16.08	16.08	0.29	0.02	0.02	0.12	0.00	0.00	20.9
10	26	-0	-2187	0	0	0	-905	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
11	26	-0	-2201	0	0	0	-925	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
12	26	-0	-1722	0	0	0	-1366	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
13	26	-0	-1736	0	0	0	-1386	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
14	26	-0	-2008	0	0	0	-1043	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
15	26	-0	-2054	0	0	0	-1110	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
16	26	-0	-1869	0	0	0	-1181	--	--	16.08	16.08	0.29	0.02	0.02	0.12	0.00	0.00	20.9
17	26	-0	-1915	0	0	0	-1248	--	--	16.08	16.08	0.29	0.02	0.02	0.12	0.00	0.00	20.9
18	26	-0	-3799	0	0	0	1705	--	--	16.08	16.08	0.00	0.03	0.03	0.24	0.00	0.00	20.9
19	26	-0	-2294	0	0	0	-1951	--	--	16.08	16.08	0.18	0.03	0.02	0.14	0.00	0.00	20.9
20	26	-0	-2943	0	0	0	-1158	--	--	16.08	16.08	0.18	0.02	0.02	0.18	0.00	0.00	20.9
37	26	-0	-4122	0	0	0	2318	--	--	16.08	16.08	0.00	0.04	0.03	0.26	0.00	0.00	20.9
38	26	-0	-1613	0	0	0	-2640	--	--	16.08	16.08	0.18	0.04	0.01	0.10	0.00	0.00	20.9
39	26	-0	-2694	0	0	0	-1318	--	--	16.08	16.08	0.18	0.02	0.02	0.17	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	-2550	0	0	0	-1489	--	--	16.08	16.08	0.18	0.02	0.02	0.16	0.00	0.00	20.9
2	51	-0	-2187	0	0	0	-905	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
3	51	-0	-2201	0	0	0	-925	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
4	51	-0	-1722	0	0	0	-1366	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
5	51	-0	-1736	0	0	0	-1386	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
6	51	-0	-2008	0	0	0	-1043	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
7	51	-0	-2054	0	0	0	-1110	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
8	51	-0	-1869	0	0	0	-1181	--	--	16.08	16.08	0.29	0.02	0.02	0.12	0.00	0.00	20.9
9	51	-0	-1915	0	0	0	-1248	--	--	16.08	16.08	0.29	0.02	0.02	0.12	0.00	0.00	20.9
10	51	-0	-2187	0	0	0	-905	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
11	51	-0	-2201	0	0	0	-925	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
12	51	-0	-1722	0	0	0	-1366	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
13	51	-0	-1736	0	0	0	-1386	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
14	51	-0	-2008	0	0	0	-1043	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
15	51	-0	-2054	0	0	0	-1110	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
16	51	-0	-1869	0	0	0	-1181	--	--	16.08	16.08	0.29	0.02	0.02	0.12	0.00	0.00	20.9
17	51	-0	-1915	0	0	0	-1248	--	--	16.08	16.08	0.29	0.02	0.02	0.12	0.00	0.00	20.9
18	51	-0	-3799	0	0	0	-247	--	--	16.08	16.08	0.18	0.00	0.03	0.24	0.00	0.00	20.9
19	51	-0	-2294	0	0	0	-1951	--	--	16.08	16.08	0.18	0.03	0.02	0.14	0.00	0.00	20.9
20	51	-0	-2943	0	0	0	-1158	--	--	16.08	16.08	0.18	0.02	0.02	0.18	0.00	0.00	20.9
37	51	-0	-4122	0	0	0	201	--	--	16.08	16.08	0.00	0.00	0.03	0.26	0.00	0.00	20.9
38	51	-0	-1613	0	0	0	-2640	--	--	16.08	16.08	0.18	0.04	0.01	0.10	0.00	0.00	20.9
39	51	-0	-2694	0	0	0	-1318	--	--	16.08	16.08	0.18	0.02	0.02	0.17	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 110 NI 1327 NF 1347 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-1567	0	0	0	-2294	--	--	16.08	16.08	0.18	0.04	0.01	0.10	0.00	0.00	20.9
2	0	-0	-1438	0	0	0	-1643	--	--	16.08	16.08	0.29	0.03	0.01	0.09	0.00	0.00	20.9
3	0	-0	-1442	0	0	0	-1666	--	--	16.08	16.08	0.29	0.03	0.01	0.09	0.00	0.00	20.9
4	0	-0	-969	0	0	0	-1864	--	--	16.08	16.08	0.29	0.03	0.01	0.06	0.00	0.00	20.9
5	0	-0	-973	0	0	0	-1886	--	--	16.08	16.08	0.29	0.03	0.01	0.06	0.00	0.00	20.9
6	0	-0	-1269	0	0	0	-1695	--	--	16.08	16.08	0.29	0.03	0.01	0.08	0.00	0.00	20.9
7	0	-0	-1283	0	0	0	-1768	--	--	16.08	16.08	0.29	0.03	0.01	0.08	0.00	0.00	20.9
8	0	-0	-1129	0	0	0	-1761	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
9	0	-0	-1142	0	0	0	-1835	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
10	0	-0	-1438	0	0	0	-1643	--	--	16.08	16.08	0.29	0.03	0.01	0.09	0.00	0.00	20.9
11	0	-0	-1442	0	0	0	-1666	--	--	16.08	16.08	0.29	0.03	0.01	0.09	0.00	0.00	20.9
12	0	-0	-969	0	0	0	-1864	--	--	16.08	16.08	0.29	0.03	0.01	0.06	0.00	0.00	20.9
13	0	-0	-973	0	0	0	-1886	--	--	16.08	16.08	0.29	0.03	0.01	0.06	0.00	0.00	20.9
14	0	-0	-1269	0	0	0	-1695	--	--	16.08	16.08	0.29	0.03	0.01	0.08	0.00	0.00	20.9
15	0	-0	-1283	0	0	0	-1768	--	--	16.08	16.08	0.29	0.03	0.01	0.08	0.00	0.00	20.9
16	0	-0	-1129	0	0	0	-1761	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
17	0	-0	-1142	0	0	0	-1835	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
18	0	-0	-2770	0	0	0	-1669	--	--	16.08	16.08	0.18	0.03	0.02	0.17	0.00	0.00	20.9
19	0	-0	-1256	0	0	0	-2597	--	--	16.08	16.08	0.18	0.04	0.01	0.08	0.00	0.00	20.9
20	0	-0	-1926	0	0	0	-2148	--	--	16.08	16.08	0.18	0.04	0.02	0.12	0.00	0.00	20.9
37	0	-0	-3120	0	0	0	201	--	--	16.08	16.08	0.00	0.00	0.03	0.20	0.00	0.00	20.9
38	0	-0	-597	0	0	0	-2947	--	--	16.08	16.08	0.18	0.05	0.00	0.04	0.00	0.00	20.9
39	0	-0	-1714	0	0	0	-2199	--	--	16.08	16.08	0.18	0.04	0.01	0.11	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	-1567	0	0	0	-2294	--	--	16.08	16.08	0.18	0.04	0.01	0.10	0.00	0.00	20.9
2	26	-0	-1438	0	0	0	-1643	--	--	16.08	16.08	0.29	0.03	0.01	0.09	0.00	0.00	20.9
3	26	-0	-1442	0	0	0	-1666	--	--	16.08	16.08	0.29	0.03	0.01	0.09	0.00	0.00	20.9
4	26	-0	-969	0	0	0	-1864	--	--	16.08	16.08	0.29	0.03	0.01	0.06	0.00	0.00	20.9
5	26	-0	-973	0	0	0	-1886	--	--	16.08	16.08	0.29	0.03	0.01	0.06	0.00	0.00	20.9
6	26	-0	-1269	0	0	0	-1695	--	--	16.08	16.08	0.29	0.03	0.01	0.08	0.00	0.00	20.9
7	26	-0	-1283	0	0	0	-1768	--	--	16.08	16.08	0.29	0.03	0.01	0.08	0.00	0.00	20.9
8	26	-0	-1129	0	0	0	-1761	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
9	26	-0	-1142	0	0	0	-1835	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
10	26	-0	-1438	0	0	0	-1643	--	--	16.08	16.08	0.29	0.03	0.01	0.09	0.00	0.00	20.9
11	26	-0	-1442	0	0	0	-1666	--	--	16.08	16.08	0.29	0.03	0.01	0.09	0.00	0.00	20.9
12	26	-0	-969	0	0	0	-1864	--	--	16.08	16.08	0.29	0.03	0.01	0.06	0.00	0.00	20.9
13	26	-0	-973	0	0	0	-1886	--	--	16.08	16.08	0.29	0.03	0.01	0.06	0.00	0.00	20.9
14	26	-0	-1269	0	0	0	-1695	--	--	16.08	16.08	0.29	0.03	0.01	0.08	0.00	0.00	20.9
15	26	-0	-1283	0	0	0	-1768	--	--	16.08	16.08	0.29	0.03	0.01	0.08	0.00	0.00	20.9
16	26	-0	-1129	0	0	0	-1761	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
17	26	-0	-1142	0	0	0	-1835	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
18	26	-0	-2770	0	0	0	-1669	--	--	16.08	16.08	0.18	0.03	0.02	0.17	0.00	0.00	20.9
19	26	-0	-1256	0	0	0	-2597	--	--	16.08	16.08	0.18	0.04	0.01	0.08	0.00	0.00	20.9
20	26	-0	-1926	0	0	0	-2148	--	--	16.08	16.08	0.18	0.04	0.02	0.12	0.00	0.00	20.9
37	26	-0	-3120	0	0	0	-1401	--	--	16.08	16.08	0.18	0.02	0.03	0.20	0.00	0.00	20.9
38	26	-0	-597	0	0	0	-2947	--	--	16.08	16.08	0.18	0.05	0.00	0.04	0.00	0.00	20.9
39	26	-0	-1714	0	0	0	-2199	--	--	16.08	16.08	0.18	0.04	0.01	0.11	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	-1567	0	0	0	-2294	--	--	16.08	16.08	0.18	0.04	0.01	0.10	0.00	0.00	20.9
2	51	-0	-1438	0	0	0	-1643	--	--	16.08	16.08	0.29	0.03	0.01	0.09	0.00	0.00	20.9

3	51	-0	-1442	0	0	0	-1666	--	--	16.08	16.08	0.29	0.03	0.01	0.09	0.00	0.00	20.9
4	51	-0	-969	0	0	0	-1864	--	--	16.08	16.08	0.29	0.03	0.01	0.06	0.00	0.00	20.9
5	51	-0	-973	0	0	0	-1886	--	--	16.08	16.08	0.29	0.03	0.01	0.06	0.00	0.00	20.9
6	51	-0	-1269	0	0	0	-1695	--	--	16.08	16.08	0.29	0.03	0.01	0.08	0.00	0.00	20.9
7	51	-0	-1283	0	0	0	-1768	--	--	16.08	16.08	0.29	0.03	0.01	0.08	0.00	0.00	20.9
8	51	-0	-1129	0	0	0	-1761	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
9	51	-0	-1142	0	0	0	-1835	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
10	51	-0	-1438	0	0	0	-1643	--	--	16.08	16.08	0.29	0.03	0.01	0.09	0.00	0.00	20.9
11	51	-0	-1442	0	0	0	-1666	--	--	16.08	16.08	0.29	0.03	0.01	0.09	0.00	0.00	20.9
12	51	-0	-969	0	0	0	-1864	--	--	16.08	16.08	0.29	0.03	0.01	0.06	0.00	0.00	20.9
13	51	-0	-973	0	0	0	-1886	--	--	16.08	16.08	0.29	0.03	0.01	0.06	0.00	0.00	20.9
14	51	-0	-1269	0	0	0	-1695	--	--	16.08	16.08	0.29	0.03	0.01	0.08	0.00	0.00	20.9
15	51	-0	-1283	0	0	0	-1768	--	--	16.08	16.08	0.29	0.03	0.01	0.08	0.00	0.00	20.9
16	51	-0	-1129	0	0	0	-1761	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
17	51	-0	-1142	0	0	0	-1835	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
18	51	-0	-2770	0	0	0	-1669	--	--	16.08	16.08	0.18	0.03	0.02	0.17	0.00	0.00	20.9
19	51	-0	-1256	0	0	0	-2597	--	--	16.08	16.08	0.18	0.04	0.01	0.08	0.00	0.00	20.9
20	51	-0	-1926	0	0	0	-2148	--	--	16.08	16.08	0.18	0.04	0.02	0.12	0.00	0.00	20.9
37	51	-0	-3120	0	0	0	-1401	--	--	16.08	16.08	0.18	0.02	0.03	0.20	0.00	0.00	20.9
38	51	-0	-597	0	0	0	-2947	--	--	16.08	16.08	0.18	0.05	0.00	0.04	0.00	0.00	20.9
39	51	-0	-1714	0	0	0	-2199	--	--	16.08	16.08	0.18	0.04	0.01	0.11	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 111 NI 1347 NF 1346 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-614	0	0	0	-2609	--	--	16.08	16.08	0.18	0.04	0.01	0.04	0.00	0.00	20.9
2	0	-0	-716	0	0	0	-2011	--	--	16.08	16.08	0.29	0.03	0.01	0.04	0.00	0.00	20.9
3	0	-0	-710	0	0	0	-2030	--	--	16.08	16.08	0.29	0.04	0.01	0.04	0.00	0.00	20.9
4	0	-0	-233	0	0	0	-1984	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
5	0	-0	-228	0	0	0	-2003	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
6	0	-0	-554	0	0	0	-1979	--	--	16.08	16.08	0.29	0.03	0.00	0.03	0.00	0.00	20.9
7	0	-0	-535	0	0	0	-2043	--	--	16.08	16.08	0.29	0.04	0.00	0.03	0.00	0.00	20.9
8	0	-0	-409	0	0	0	-1971	--	--	16.08	16.08	0.29	0.03	0.00	0.03	0.00	0.00	20.9
9	0	-0	-390	0	0	0	-2035	--	--	16.08	16.08	0.29	0.04	0.00	0.02	0.00	0.00	20.9
10	0	-0	-716	0	0	0	-2011	--	--	16.08	16.08	0.29	0.03	0.01	0.04	0.00	0.00	20.9
11	0	-0	-710	0	0	0	-2030	--	--	16.08	16.08	0.29	0.04	0.01	0.04	0.00	0.00	20.9
12	0	-0	-233	0	0	0	-1984	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
13	0	-0	-228	0	0	0	-2003	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
14	0	-0	-554	0	0	0	-1979	--	--	16.08	16.08	0.29	0.03	0.00	0.03	0.00	0.00	20.9
15	0	-0	-535	0	0	0	-2043	--	--	16.08	16.08	0.29	0.04	0.00	0.03	0.00	0.00	20.9
16	0	-0	-409	0	0	0	-1971	--	--	16.08	16.08	0.29	0.03	0.00	0.03	0.00	0.00	20.9
17	0	-0	-390	0	0	0	-2035	--	--	16.08	16.08	0.29	0.04	0.00	0.02	0.00	0.00	20.9
18	0	-0	-1797	0	0	0	-2592	--	--	16.08	16.08	0.18	0.04	0.01	0.11	0.00	0.00	20.9
19	0	-0	-243	0	0	0	-2721	--	--	16.08	16.08	0.18	0.05	0.00	0.02	0.00	0.00	20.9
20	0	-0	-948	0	0	0	-2634	--	--	16.08	16.08	0.18	0.04	0.01	0.06	0.00	0.00	20.9
37	0	-0	-2181	0	0	0	-2522	--	--	16.08	16.08	0.18	0.04	0.02	0.14	0.00	0.00	20.9
38	0	-0	409	0	0	0	-2947	--	--	16.08	16.08	0.18	0.05	0.00	0.03	0.00	0.00	20.9
39	0	-0	-765	0	0	0	-2591	--	--	16.08	16.08	0.18	0.04	0.01	0.05	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	-614	0	0	0	-2609	--	--	16.08	16.08	0.18	0.04	0.01	0.04	0.00	0.00	20.9
2	26	-0	-716	0	0	0	-2011	--	--	16.08	16.08	0.29	0.03	0.01	0.04	0.00	0.00	20.9
3	26	-0	-710	0	0	0	-2030	--	--	16.08	16.08	0.29	0.04	0.01	0.04	0.00	0.00	20.9
4	26	-0	-233	0	0	0	-1984	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
5	26	-0	-228	0	0	0	-2003	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
6	26	-0	-554	0	0	0	-1979	--	--	16.08	16.08	0.29	0.03	0.00	0.03	0.00	0.00	20.9
7	26	-0	-535	0	0	0	-2043	--	--	16.08	16.08	0.29	0.04	0.00	0.03	0.00	0.00	20.9
8	26	-0	-409	0	0	0	-1971	--	--	16.08	16.08	0.29	0.03	0.00	0.03	0.00	0.00	20.9
9	26	-0	-390	0	0	0	-2035	--	--	16.08	16.08	0.29	0.04	0.00	0.02	0.00	0.00	20.9
10	26	-0	-716	0	0	0	-2011	--	--	16.08	16.08	0.29	0.03	0.01	0.04	0.00	0.00	20.9
11	26	-0	-710	0	0	0	-2030	--	--	16.08	16.08	0.29	0.04	0.01	0.04	0.00	0.00	20.9
12	26	-0	-233	0	0	0	-1984	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
13	26	-0	-228	0	0	0	-2003	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
14	26	-0	-554	0	0	0	-1979	--	--	16.08	16.08	0.29	0.03	0.00	0.03	0.00	0.00	20.9
15	26	-0	-535	0	0	0	-2043	--	--	16.08	16.08	0.29	0.04	0.00	0.03	0.00	0.00	20.9
16	26	-0	-409	0	0	0	-1971	--	--	16.08	16.08	0.29	0.03	0.00	0.03	0.00	0.00	20.9
17	26	-0	-390	0	0	0	-2035	--	--	16.08	16.08	0.29	0.04	0.00	0.02	0.00	0.00	20.9
18	26	-0	-1797	0	0	0	-2592	--	--	16.08	16.08	0.18	0.04	0.01	0.11	0.00	0.00	20.9
19	26	-0	-243	0	0	0	-2721	--	--	16.08	16.08	0.18	0.05	0.00	0.02	0.00	0.00	20.9
20	26	-0	-948	0	0	0	-2634	--	--	16.08	16.08	0.18	0.04	0.01	0.06	0.00	0.00	20.9
37	26	-0	-2181	0	0	0	-2522	--	--	16.08	16.08	0.18	0.04	0.02	0.14	0.00	0.00	20.9
38	26	-0	409	0	0	0	-2947	--	--	16.08	16.08	0.18	0.05	0.00	0.03	0.00	0.00	20.9
39	26	-0	-765	0	0	0	-2591	--	--	16.08	16.08	0.18	0.04	0.01	0.05	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	-614	0	0	0	-2609	--	--	16.08	16.08	0.18	0.04	0.01	0.04	0.00	0.00	20.9
2	51	-0	-716	0	0	0	-2011	--	--	16.08	16.08	0.29	0.03	0.01	0.04	0.00	0.00	20.9
3	51	-0	-710	0	0	0	-2030	--	--	16.08	16.08	0.29	0.04	0.01	0.04	0.00	0.00	20.9
4	51	-0	-233	0	0	0	-1984	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
5	51	-0	-228	0	0	0	-2003	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
6	51	-0	-554	0	0	0	-1979	--	--	16.08	16.08	0.29	0.03	0.00	0.03	0.00	0.00	20.9
7	51	-0	-535	0	0	0	-2043	--	--	16.08	16.08	0.29	0.04	0.00	0.03	0.00	0.00	20.9
8	51	-0	-409	0	0	0	-1971	--	--	16.08	16.08	0.29	0.03	0.00	0.03	0.00	0.00	20.9
9	51	-0	-390	0	0	0	-2035	--	--	16.08	16.08	0.29	0.04	0.00	0.02	0.00	0.00	20.9
10	51	-0	-716	0	0	0	-2011	--	--	16.08	16.08	0.29	0.03	0.01	0.04	0.00	0.00	20.9
11	51	-0	-710	0	0	0	-2030	--	--	16.08	16.08	0.29	0.04	0.01	0.04	0.00	0.00	20.9
12	51	-0	-233	0	0	0	-1984	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
13	51	-0	-228	0	0	0	-2003	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
14	51	-0	-554	0	0	0	-1979	--	--	16.08	16.08	0.29	0.03	0.00	0.03	0.00	0.00	20.9
15	51	-0	-535	0	0	0	-2043	--	--	16.08	16.08	0.29	0.04	0.00	0.03	0.00	0.00	20.9
16	51	-0	-409	0	0	0	-1971	--	--	16.08	16.08	0.29	0.03	0.00	0.03	0.00	0.00	20.9
17	51	-0	-390	0	0	0	-2035	--	--	16.08	16.08	0.29	0.04	0.00	0.02	0.00	0.00	20.9
18	51	-0	-1797	0	0	0	-2592	--	--	16.08	16.08	0.18	0.04	0.01	0.11	0.00	0.00	20.9
19	51	-0	-243	0	0	0	-2721	--	--	16.08	16.08	0.18	0.05	0.00	0.02	0.00	0.00	20.9
20	51	-0	-948	0	0	0	-2634	--	--	16.08	16.08	0.18	0.04	0.01	0.06	0.00	0.00	20.9
37	51	-0	-2181	0	0	0	-2522	--	--	16.08	16.08	0.18	0.04	0.02	0.14	0.00	0.00	20.9
38	51	-0	409	0	0	0	-2947	--	--	16.08	16.08	0.18	0.05	0.00	0.03	0.00	0.00	20.9
39	51	-0	-765	0	0	0	-2591	--	--	16.08	16.08	0.18	0.04	0.01	0.05	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 112 NI 1346 NF 1290 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	324	0	0	0	-2609	--	--	16.08	16.08	0.18	0.04	0.00	0.02	0.00	0.00	20.9
2	0	-0	-11	0	0	0	-2017	--	--	16.08	16.08	0.29	0.03	0.00	0.00	0.00	0.00	20.9
3	0	-0	4	0	0	0	-2030	--	--	16.08	16.08	0.29	0.04	0.00	0.00	0.00	0.00	20.9
4	0	-0	494	0	0	0	-1984	--	--	16.08	16.08	0.29	0.03	0.00	0.03	0.00	0.00	20.9
5	0	-0	510	0	0	0	-2003	--	--	16.08	16.08	0.29	0.03	0.00	0.03	0.00	0.00	20.9
6	0	-0	147	0	0	0	-1979	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
7	0	-0	200	0	0	0	-2043	--	--	16.08	16.08	0.29	0.04	0.00	0.01	0.00	0.00	20.9
8	0	-0	299	0	0	0	-1971	--	--	16.08	16.08	0.29	0.03	0.00	0.02	0.00	0.00	20.9
9	0	-0	351	0	0	0	-2035	--	--	16.08	16.08	0.29	0.04	0.00	0.02	0.00	0.00	20.9
10	0	-0	-11	0	0	0	-2017	--	--	16.08	16.08	0.29	0.03	0.00	0.00	0.00	0.00	20.9
11	0	-0	4	0	0	0	-2030	--	--	16.08	16.08	0.29	0.04	0.00	0.00	0.00	0.00	20.9
12	0	-0	494	0	0	0	-1984	--	--	16.08	16.08	0.29	0.03	0.00	0.03	0.00	0.00	20.9
13	0	-0	510	0	0	0	-2003	--	--	16.08	16.08	0.29	0.03	0.00	0.03	0.00	0.00	20.9
14	0	-0	147	0	0	0	-1979	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
15	0	-0	200	0	0	0	-2043	--	--	16.08	16.08	0.29	0.04	0.00	0.01	0.00	0.00	20.9
16	0	-0	299	0	0	0	-1971	--	--	16.08	16.08	0.29	0.03	0.00	0.02	0.00	0.00	20.9
17	0	-0	351	0	0	0	-2035	--	--	16.08	16.08	0.29	0.04	0.00	0.02	0.00	0.00	20.9
18	0	-0	-871	0	0	0	-3040	--	--	16.08	16.08	0.18	0.05	0.01	0.05	0.00	0.00	20.9
19	0	-0	760	0	0	0	-2721	--	--	16.08	16.08	0.18	0.05	0.01	0.05	0.00	0.00	20.9
20	0	-0	6	0	0	0	-2634	--	--	16.08	16.08	0.18	0.04	0.00	0.00	0.00	0.00	20.9
37	0	-0	-1297	0	0	0	-3188	--	--	16.08	16.08	0.18	0.05	0.01	0.08	0.00	0.00	20.9
38	0	-0	1421	0	0	0	-2737	--	--	16.08	16.08	0.18	0.05	0.01	0.09	0.00	0.00	20.9
39	0	-0	165	0	0	0	-2591	--	--	16.08	16.08	0.18	0.04	0.00	0.01	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	26	-0	324	0	0	0	-2609	--	--	16.08	16.08	0.18	0.04	0.00	0.02	0.00	0.00	20.9
2	26	-0	-11	0	0	0	-2017	--	--	16.08	16.08	0.29	0.03	0.00	0.00	0.00	0.00	20.9
3	26	-0	4	0	0	0	-2030	--	--	16.08	16.08	0.29	0.04	0.00	0.00	0.00	0.00	20.9
4	26	-0	494	0	0	0	-1984	--	--	16.08	16.08	0.29	0.03	0.00	0.03	0.00	0.00	20.9
5	26	-0	510	0	0	0	-2003	--	--	16.08	16.08	0.29	0.03	0.00	0.03	0.00	0.00	20.9
6	26	-0	147	0	0	0	-1979	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
7	26	-0	200	0	0	0	-2043	--	--	16.08	16.08	0.29	0.04	0.00	0.01	0.00	0.00	20.9
8	26	-0	299	0	0	0	-1971	--	--	16.08	16.08	0.29	0.03	0.00	0.02	0.00	0.00	20.9
9	26	-0	351	0	0	0	-2035	--	--	16.08	16.08	0.29	0.04	0.00	0.02	0.00	0.00	20.9
10	26	-0	-11	0	0	0	-2017	--	--	16.08	16.08	0.29	0.03	0.00	0.00	0.00	0.00	20.9
11	26	-0	4	0	0	0	-2030	--	--	16.08	16.08	0.29	0.04	0.00	0.00	0.00	0.00	20.9
12	26	-0	494	0	0	0	-1984	--	--	16.08	16.08	0.29	0.03	0.00	0.03	0.00	0.00	20.9
13	26	-0	510	0	0	0	-2003	--	--	16.08	16.08	0.29	0.03	0.00	0.03	0.00	0.00	20.9
14	26	-0	147	0	0	0	-1979	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
15	26	-0	200	0	0	0	-2043	--	--	16.08	16.08	0.29	0.04	0.00	0.01	0.00	0.00	20.9
16	26	-0	299	0	0	0	-1971	--	--	16.08	16.08	0.29	0.03	0.00	0.02	0.00	0.00	20.9
17	26	-0	351	0	0	0	-2035	--	--	16.08	16.08	0.29	0.04	0.00	0.02	0.00	0.00	20.9
18	26	-0	-871	0	0	0	-3040	--	--	16.08	16.08	0.18	0.05	0.01	0.05	0.00	0.00	20.9
19	26	-0	760	0	0	0	-2721	--	--	16.08	16.08	0.18	0.05	0.01	0.05	0.00	0.00	20.9
20	26	-0	6	0	0	0	-2634	--	--	16.08	16.08	0.18	0.04	0.00	0.00	0.00	0.00	20.9
37	26	-0	-1297	0	0	0	-3188	--	--	16.08	16.08	0.18	0.05	0.01	0.08	0.00	0.00	20.9
38	26	-0	1421	0	0	0	-2737	--	--	16.08	16.08	0.18	0.05	0.01	0.09	0.00	0.00	20.9
39	26	-0	165	0	0	0	-2591	--	--	16.08	16.08	0.18	0.04	0.00	0.01	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	51	-0	324	0	0	0	-2609	--	--	16.08	16.08	0.18	0.04	0.00	0.02	0.00	0.00	20.9
2	51	-0	-11	0	0	0	-2017	--	--	16.08	16.08	0.29	0.03	0.00	0.00	0.00	0.00	20.9
3	51	-0	4	0	0	0	-2030	--	--	16.08	16.08	0.29	0.04	0.00	0.00	0.00	0.00	20.9
4	51	-0	494	0	0	0	-1984	--	--	16.08	16.08	0.29	0.03	0.00	0.03	0.00	0.00	20.9
5	51	-0	510	0	0	0	-2003	--	--	16.08	16.08	0.29	0.03	0.00	0.03	0.00	0.00	20.9
6	51	-0	147	0	0	0	-1979	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
7	51	-0	200	0	0	0	-2043	--	--	16.08	16.08	0.29	0.04	0.00	0.01	0.00	0.00	20.9
8	51	-0	299	0	0	0	-1971	--	--	16.08	16.08	0.29	0.03	0.00	0.02	0.00	0.00	20.9
9	51	-0	351	0	0	0	-2035	--	--	16.08	16.08	0.29	0.04	0.00	0.02	0.00	0.00	20.9
10	51	-0	-11	0	0	0	-2017	--	--	16.08	16.08	0.29	0.03	0.00	0.00	0.00	0.00	20.9
11	51	-0	4	0	0	0	-2030	--	--	16.08	16.08	0.29	0.04	0.00	0.00	0.00	0.00	20.9
12	51	-0	494	0	0	0	-1984	--	--	16.08	16.08	0.29	0.03	0.00	0.03	0.00	0.00	20.9
13	51	-0	510	0	0	0	-2003	--	--	16.08	16.08	0.29	0.03	0.00	0.03	0.00	0.00	20.9
14	51	-0	147	0	0	0	-1979	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
15	51	-0	200	0	0	0	-2043	--	--	16.08	16.08	0.29	0.04	0.00	0.01	0.00	0.00	20.9
16	51	-0	299	0	0	0	-1971	--	--	16.08	16.08	0.29	0.03	0.00	0.02	0.00	0.00	20.9
17	51	-0	351	0	0	0	-2035	--	--	16.08	16.08	0.29	0.04	0.00	0.02	0.00	0.00	20.9
18	51	-0	-871	0	0	0	-3040	--	--	16.08	16.08	0.18	0.05	0.01	0.05	0.00	0.00	20.9
19	51	-0	760	0	0	0	-2721	--	--	16.08	16.08	0.18	0.05	0.01	0.05	0.00	0.00	20.9
20	51	-0	6	0	0	0	-2634	--	--	16.08	16.08	0.18	0.04	0.00	0.00	0.00	0.00	20.9
37	51	-0	-1297	0	0	0	-3188	--	--	16.08	16.08	0.18	0.05	0.01	0.08	0.00	0.00	20.9
38	51	-0	1421	0	0	0	-2737	--	--	16.08	16.08	0.18	0.05	0.01	0.09	0.00	0.00	20.9
39	51	-0	165	0	0	0	-2591	--	--	16.08	16.08	0.18	0.04	0.00	0.01	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 113 NI 1290 NF 1331 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	1260	0	0	0	-2443	--	--	16.08	16.08	0.18	0.04	0.01	0.08	0.00	0.00	20.9
2	0	-0	687	0	0	0	-2017	--	--	16.08	16.08	0.29	0.03	0.01	0.04	0.00	0.00	20.9
3	0	-0	713	0	0	0	-2028	--	--	16.08	16.08	0.29	0.04	0.01	0.04	0.00	0.00	20.9
4	0	-0	1225	0	0	0	-1730	--	--	16.08	16.08	0.29	0.03	0.01	0.08	0.00	0.00	20.9
5	0	-0	1251	0	0	0	-1741	--	--	16.08	16.08	0.29	0.03	0.01	0.08	0.00	0.00	20.9
6	0	-0	845	0	0	0	-1904	--	--	16.08	16.08	0.29	0.03	0.01	0.05	0.00	0.00	20.9
7	0	-0	931	0	0	0	-1940	--	--	16.08	16.08	0.29	0.03	0.01	0.06	0.00	0.00	20.9
8	0	-0	1007	0	0	0	-1818	--	--	16.08	16.08	0.29	0.03	0.01	0.06	0.00	0.00	20.9
9	0	-0	1093	0	0	0	-1854	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
10	0	-0	687	0	0	0	-2017	--	--	16.08	16.08	0.29	0.03	0.01	0.04	0.00	0.00	20.9

11	0	-0	713	0	0	0	-2028	--	--	16.08	16.08	0.29	0.04	0.01	0.04	0.00	0.00	20.9
12	0	-0	1225	0	0	0	-1730	--	--	16.08	16.08	0.29	0.03	0.01	0.08	0.00	0.00	20.9
13	0	-0	1251	0	0	0	-1741	--	--	16.08	16.08	0.29	0.03	0.01	0.08	0.00	0.00	20.9
14	0	-0	845	0	0	0	-1904	--	--	16.08	16.08	0.29	0.03	0.01	0.05	0.00	0.00	20.9
15	0	-0	931	0	0	0	-1940	--	--	16.08	16.08	0.29	0.03	0.01	0.06	0.00	0.00	20.9
16	0	-0	1007	0	0	0	-1818	--	--	16.08	16.08	0.29	0.03	0.01	0.06	0.00	0.00	20.9
17	0	-0	1093	0	0	0	-1854	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
18	0	-0	22	0	0	0	-3040	--	--	16.08	16.08	0.18	0.05	0.00	0.00	0.00	0.00	20.9
19	0	-0	1767	0	0	0	-2331	--	--	16.08	16.08	0.18	0.04	0.01	0.11	0.00	0.00	20.9
20	0	-0	948	0	0	0	-2631	--	--	16.08	16.08	0.18	0.04	0.01	0.06	0.00	0.00	20.9
37	0	-0	-454	0	0	0	-3421	--	--	16.08	16.08	0.18	0.06	0.00	0.03	0.00	0.00	20.9
38	0	-0	2454	0	0	0	-2007	--	--	16.08	16.08	0.18	0.03	0.02	0.15	0.00	0.00	20.9
39	0	-0	1090	0	0	0	-2507	--	--	16.08	16.08	0.18	0.04	0.01	0.07	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	1260	0	0	0	-2443	--	--	16.08	16.08	0.18	0.04	0.01	0.08	0.00	0.00	20.9
2	26	-0	687	0	0	0	-2017	--	--	16.08	16.08	0.29	0.03	0.01	0.04	0.00	0.00	20.9
3	26	-0	713	0	0	0	-2028	--	--	16.08	16.08	0.29	0.04	0.01	0.04	0.00	0.00	20.9
4	26	-0	1225	0	0	0	-1730	--	--	16.08	16.08	0.29	0.03	0.01	0.08	0.00	0.00	20.9
5	26	-0	1251	0	0	0	-1741	--	--	16.08	16.08	0.29	0.03	0.01	0.08	0.00	0.00	20.9
6	26	-0	845	0	0	0	-1904	--	--	16.08	16.08	0.29	0.03	0.01	0.05	0.00	0.00	20.9
7	26	-0	931	0	0	0	-1940	--	--	16.08	16.08	0.29	0.03	0.01	0.06	0.00	0.00	20.9
8	26	-0	1007	0	0	0	-1818	--	--	16.08	16.08	0.29	0.03	0.01	0.06	0.00	0.00	20.9
9	26	-0	1093	0	0	0	-1854	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
10	26	-0	687	0	0	0	-2017	--	--	16.08	16.08	0.29	0.03	0.01	0.04	0.00	0.00	20.9
11	26	-0	713	0	0	0	-2028	--	--	16.08	16.08	0.29	0.04	0.01	0.04	0.00	0.00	20.9
12	26	-0	1225	0	0	0	-1730	--	--	16.08	16.08	0.29	0.03	0.01	0.08	0.00	0.00	20.9
13	26	-0	1251	0	0	0	-1741	--	--	16.08	16.08	0.29	0.03	0.01	0.08	0.00	0.00	20.9
14	26	-0	845	0	0	0	-1904	--	--	16.08	16.08	0.29	0.03	0.01	0.05	0.00	0.00	20.9
15	26	-0	931	0	0	0	-1940	--	--	16.08	16.08	0.29	0.03	0.01	0.06	0.00	0.00	20.9
16	26	-0	1007	0	0	0	-1818	--	--	16.08	16.08	0.29	0.03	0.01	0.06	0.00	0.00	20.9
17	26	-0	1093	0	0	0	-1854	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
18	26	-0	22	0	0	0	-3040	--	--	16.08	16.08	0.18	0.05	0.00	0.00	0.00	0.00	20.9
19	26	-0	1767	0	0	0	-2331	--	--	16.08	16.08	0.18	0.04	0.01	0.11	0.00	0.00	20.9
20	26	-0	948	0	0	0	-2631	--	--	16.08	16.08	0.18	0.04	0.01	0.06	0.00	0.00	20.9
37	26	-0	-454	0	0	0	-3421	--	--	16.08	16.08	0.18	0.06	0.00	0.03	0.00	0.00	20.9
38	26	-0	2454	0	0	0	-2007	--	--	16.08	16.08	0.18	0.03	0.02	0.15	0.00	0.00	20.9
39	26	-0	1090	0	0	0	-2507	--	--	16.08	16.08	0.18	0.04	0.01	0.07	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	1260	0	0	0	-2443	--	--	16.08	16.08	0.18	0.04	0.01	0.08	0.00	0.00	20.9
2	51	-0	687	0	0	0	-2017	--	--	16.08	16.08	0.29	0.03	0.01	0.04	0.00	0.00	20.9
3	51	-0	713	0	0	0	-2028	--	--	16.08	16.08	0.29	0.04	0.01	0.04	0.00	0.00	20.9
4	51	-0	1225	0	0	0	-1730	--	--	16.08	16.08	0.29	0.03	0.01	0.08	0.00	0.00	20.9
5	51	-0	1251	0	0	0	-1741	--	--	16.08	16.08	0.29	0.03	0.01	0.08	0.00	0.00	20.9
6	51	-0	845	0	0	0	-1904	--	--	16.08	16.08	0.29	0.03	0.01	0.05	0.00	0.00	20.9
7	51	-0	931	0	0	0	-1940	--	--	16.08	16.08	0.29	0.03	0.01	0.06	0.00	0.00	20.9
8	51	-0	1007	0	0	0	-1818	--	--	16.08	16.08	0.29	0.03	0.01	0.06	0.00	0.00	20.9
9	51	-0	1093	0	0	0	-1854	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
10	51	-0	687	0	0	0	-2017	--	--	16.08	16.08	0.29	0.03	0.01	0.04	0.00	0.00	20.9
11	51	-0	713	0	0	0	-2028	--	--	16.08	16.08	0.29	0.04	0.01	0.04	0.00	0.00	20.9
12	51	-0	1225	0	0	0	-1730	--	--	16.08	16.08	0.29	0.03	0.01	0.08	0.00	0.00	20.9
13	51	-0	1251	0	0	0	-1741	--	--	16.08	16.08	0.29	0.03	0.01	0.08	0.00	0.00	20.9
14	51	-0	845	0	0	0	-1904	--	--	16.08	16.08	0.29	0.03	0.01	0.05	0.00	0.00	20.9
15	51	-0	931	0	0	0	-1940	--	--	16.08	16.08	0.29	0.03	0.01	0.06	0.00	0.00	20.9
16	51	-0	1007	0	0	0	-1818	--	--	16.08	16.08	0.29	0.03	0.01	0.06	0.00	0.00	20.9
17	51	-0	1093	0	0	0	-1854	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
18	51	-0	22	0	0	0	-3040	--	--	16.08	16.08	0.18	0.05	0.00	0.00	0.00	0.00	20.9
19	51	-0	1767	0	0	0	-2331	--	--	16.08	16.08	0.18	0.04	0.01	0.11	0.00	0.00	20.9
20	51	-0	948	0	0	0	-2631	--	--	16.08	16.08	0.18	0.04	0.01	0.06	0.00	0.00	20.9
37	51	-0	-454	0	0	0	-3421	--	--	16.08	16.08	0.18	0.06	0.00	0.03	0.00	0.00	20.9
38	51	-0	2454	0	0	0	-2007	--	--	16.08	16.08	0.18	0.03	0.02	0.15	0.00	0.00	20.9
39	51	-0	1090	0	0	0	-2507	--	--	16.08	16.08	0.18	0.04	0.01	0.07	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 114 NI 1331 NF 1330 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	2207	0	0	0	-1796	--	--	16.08	16.08	0.18	0.03	0.02	0.14	0.00	0.00	20.9
2	0	-0	1390	0	0	0	-1664	--	--	16.08	16.08	0.29	0.03	0.01	0.09	0.00	0.00	20.9
3	0	-0	1426	0	0	0	-1662	--	--	16.08	16.08	0.29	0.03	0.01	0.09	0.00	0.00	20.9
4	0	-0	1969	0	0	0	-1100	--	--	16.08	16.08	0.29	0.02	0.02	0.12	0.00	0.00	20.9
5	0	-0	2005	0	0	0	-1098	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
6	0	-0	1550	0	0	0	-1470	--	--	16.08	16.08	0.29	0.03	0.01	0.10	0.00	0.00	20.9
7	0	-0	1671	0	0	0	-1462	--	--	16.08	16.08	0.29	0.03	0.01	0.10	0.00	0.00	20.9
8	0	-0	1724	0	0	0	-1300	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
9	0	-0	1845	0	0	0	-1293	--	--	16.08	16.08	0.29	0.02	0.02	0.12	0.00	0.00	20.9
10	0	-0	1390	0	0	0	-1664	--	--	16.08	16.08	0.29	0.03	0.01	0.09	0.00	0.00	20.9
11	0	-0	1426	0	0	0	-1662	--	--	16.08	16.08	0.29	0.03	0.01	0.09	0.00	0.00	20.9
12	0	-0	1969	0	0	0	-1100	--	--	16.08	16.08	0.29	0.02	0.02	0.12	0.00	0.00	20.9
13	0	-0	2005	0	0	0	-1098	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
14	0	-0	1550	0	0	0	-1470	--	--	16.08	16.08	0.29	0.03	0.01	0.10	0.00	0.00	20.9
15	0	-0	1671	0	0	0	-1462	--	--	16.08	16.08	0.29	0.03	0.01	0.10	0.00	0.00	20.9
16	0	-0	1724	0	0	0	-1300	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
17	0	-0	1845	0	0	0	-1293	--	--	16.08	16.08	0.29	0.02	0.02	0.12	0.00	0.00	20.9
18	0	-0	899	0	0	0	-3028	--	--	16.08	16.08	0.18	0.05	0.01	0.06	0.00	0.00	20.9
19	0	-0	2792	0	0	0	-1424	--	--	16.08	16.08	0.18	0.02	0.02	0.18	0.00	0.00	20.9
20	0	-0	1894	0	0	0	-2144	--	--	16.08	16.08	0.18	0.04	0.02	0.12	0.00	0.00	20.9
37	0	-0	365	0	0	0	-3421	--	--	16.08	16.08	0.18	0.06	0.00	0.02	0.00	0.00	20.9
38	0	-0	3519	0	0	0	-747	--	--	16.08	16.08	0.18	0.01	0.03	0.22	0.00	0.00	20.9
39	0	-0	2023	0	0	0	-1947	--	--	16.08	16.08	0.18	0.03	0.02	0.13	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	2207	0	0	0	-1796	--	--	16.08	16.08	0.18	0.03	0.02	0.14	0.00	0.00	20.9
2	26	-0	1390	0	0	0	-1664	--	--	16.08	16.08	0.29	0.03	0.01	0.09	0.00	0.00	20.9
3	26	-0	1426	0	0	0	-1662	--	--	16.08	16.08	0.29	0.03	0.01	0.09	0.00	0.00	20.9
4	26	-0	1969	0	0	0	-1100	--	--	16.08	16.08	0.29	0.02	0.02	0.12	0.00	0.00	20.9
5	26	-0	2005	0	0	0	-1098	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
6	26	-0	1550	0	0	0	-1470	--	--	16.08	16.08	0.29	0.03	0.01	0.10	0.00	0.00	20.9

7	26	-0	1671	0	0	0	-1462	--	--	16.08	16.08	0.29	0.03	0.01	0.10	0.00	0.00	20.9
8	26	-0	1724	0	0	0	-1300	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
9	26	-0	1845	0	0	0	-1293	--	--	16.08	16.08	0.29	0.02	0.02	0.12	0.00	0.00	20.9
10	26	-0	1390	0	0	0	-1664	--	--	16.08	16.08	0.29	0.03	0.01	0.09	0.00	0.00	20.9
11	26	-0	1426	0	0	0	-1662	--	--	16.08	16.08	0.29	0.03	0.01	0.09	0.00	0.00	20.9
12	26	-0	1969	0	0	0	-1100	--	--	16.08	16.08	0.29	0.02	0.02	0.12	0.00	0.00	20.9
13	26	-0	2005	0	0	0	-1098	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
14	26	-0	1550	0	0	0	-1470	--	--	16.08	16.08	0.29	0.03	0.01	0.10	0.00	0.00	20.9
15	26	-0	1671	0	0	0	-1462	--	--	16.08	16.08	0.29	0.03	0.01	0.10	0.00	0.00	20.9
16	26	-0	1724	0	0	0	-1300	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
17	26	-0	1845	0	0	0	-1293	--	--	16.08	16.08	0.29	0.02	0.02	0.12	0.00	0.00	20.9
18	26	-0	899	0	0	0	-3028	--	--	16.08	16.08	0.18	0.05	0.01	0.06	0.00	0.00	20.9
19	26	-0	2792	0	0	0	-1424	--	--	16.08	16.08	0.18	0.02	0.02	0.18	0.00	0.00	20.9
20	26	-0	1894	0	0	0	-2144	--	--	16.08	16.08	0.18	0.04	0.02	0.12	0.00	0.00	20.9
37	26	-0	365	0	0	0	-3421	--	--	16.08	16.08	0.18	0.06	0.00	0.02	0.00	0.00	20.9
38	26	-0	3519	0	0	0	3918	--	--	16.08	16.08	0.00	0.07	0.03	0.22	0.00	0.00	20.9
39	26	-0	2023	0	0	0	-1947	--	--	16.08	16.08	0.18	0.03	0.02	0.13	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	2207	0	0	0	-1796	--	--	16.08	16.08	0.18	0.03	0.02	0.14	0.00	0.00	20.9
2	51	-0	1390	0	0	0	-1664	--	--	16.08	16.08	0.29	0.03	0.01	0.09	0.00	0.00	20.9
3	51	-0	1426	0	0	0	-1662	--	--	16.08	16.08	0.29	0.03	0.01	0.09	0.00	0.00	20.9
4	51	-0	1969	0	0	0	-1100	--	--	16.08	16.08	0.29	0.02	0.02	0.12	0.00	0.00	20.9
5	51	-0	2005	0	0	0	-1098	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
6	51	-0	1550	0	0	0	-1470	--	--	16.08	16.08	0.29	0.03	0.01	0.10	0.00	0.00	20.9
7	51	-0	1671	0	0	0	-1462	--	--	16.08	16.08	0.29	0.03	0.01	0.10	0.00	0.00	20.9
8	51	-0	1724	0	0	0	-1300	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
9	51	-0	1845	0	0	0	-1293	--	--	16.08	16.08	0.29	0.02	0.02	0.12	0.00	0.00	20.9
10	51	-0	1390	0	0	0	-1664	--	--	16.08	16.08	0.29	0.03	0.01	0.09	0.00	0.00	20.9
11	51	-0	1426	0	0	0	-1662	--	--	16.08	16.08	0.29	0.03	0.01	0.09	0.00	0.00	20.9
12	51	-0	1969	0	0	0	-1100	--	--	16.08	16.08	0.29	0.02	0.02	0.12	0.00	0.00	20.9
13	51	-0	2005	0	0	0	-1098	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
14	51	-0	1550	0	0	0	-1470	--	--	16.08	16.08	0.29	0.03	0.01	0.10	0.00	0.00	20.9
15	51	-0	1671	0	0	0	-1462	--	--	16.08	16.08	0.29	0.03	0.01	0.10	0.00	0.00	20.9
16	51	-0	1724	0	0	0	-1300	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
17	51	-0	1845	0	0	0	-1293	--	--	16.08	16.08	0.29	0.02	0.02	0.12	0.00	0.00	20.9
18	51	-0	899	0	0	0	-3028	--	--	16.08	16.08	0.18	0.05	0.01	0.06	0.00	0.00	20.9
19	51	-0	2792	0	0	0	10	--	--	16.08	16.08	0.00	0.00	0.02	0.18	0.00	0.00	20.9
20	51	-0	1894	0	0	0	-2144	--	--	16.08	16.08	0.18	0.04	0.02	0.12	0.00	0.00	20.9
37	51	-0	365	0	0	0	-3421	--	--	16.08	16.08	0.18	0.06	0.00	0.02	0.00	0.00	20.9
38	51	-0	3519	0	0	0	1061	--	--	16.08	16.08	0.00	0.02	0.03	0.22	0.00	0.00	20.9
39	51	-0	2023	0	0	0	-1947	--	--	16.08	16.08	0.18	0.03	0.02	0.13	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 115 NI 1330 NF 1348 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm

1	0	-0	3176	0	0	0	-662	--	--	16.08	16.08	0.18	0.01	0.03	0.20	0.00	0.00	20.9
2	0	-0	2107	0	0	0	-950	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
3	0	-0	2154	0	0	0	-930	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
4	0	-0	2732	0	0	0	-89	--	--	16.08	16.08	0.29	0.00	0.02	0.17	0.00	0.00	20.9
5	0	-0	2779	0	0	0	-68	--	--	16.08	16.08	0.29	0.00	0.02	0.17	0.00	0.00	20.9
6	0	-0	2271	0	0	0	-673	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
7	0	-0	2427	0	0	0	-604	--	--	16.08	16.08	0.29	0.01	0.02	0.15	0.00	0.00	20.9
8	0	-0	2458	0	0	0	-415	--	--	16.08	16.08	0.29	0.01	0.02	0.15	0.00	0.00	20.9
9	0	-0	2615	0	0	0	-346	--	--	16.08	16.08	0.29	0.01	0.02	0.16	0.00	0.00	20.9
10	0	-0	2107	0	0	0	-950	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
11	0	-0	2154	0	0	0	-930	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
12	0	-0	2732	0	0	0	-89	--	--	16.08	16.08	0.29	0.00	0.02	0.17	0.00	0.00	20.9
13	0	-0	2779	0	0	0	-68	--	--	16.08	16.08	0.29	0.00	0.02	0.17	0.00	0.00	20.9
14	0	-0	2271	0	0	0	-673	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
15	0	-0	2427	0	0	0	-604	--	--	16.08	16.08	0.29	0.01	0.02	0.15	0.00	0.00	20.9
16	0	-0	2458	0	0	0	-415	--	--	16.08	16.08	0.29	0.01	0.02	0.15	0.00	0.00	20.9
17	0	-0	2615	0	0	0	-346	--	--	16.08	16.08	0.29	0.01	0.02	0.16	0.00	0.00	20.9
18	0	-0	1776	0	0	0	-2566	--	--	16.08	16.08	0.18	0.04	0.01	0.11	0.00	0.00	20.9
19	0	-0	3843	0	0	0	10	--	--	16.08	16.08	0.00	0.00	0.03	0.24	0.00	0.00	20.9
20	0	-0	2855	0	0	0	-1171	--	--	16.08	16.08	0.18	0.02	0.02	0.18	0.00	0.00	20.9
37	0	-0	1177	0	0	0	-3233	--	--	16.08	16.08	0.18	0.05	0.01	0.07	0.00	0.00	20.9
38	0	-0	4622	0	0	0	1061	--	--	16.08	16.08	0.00	0.02	0.04	0.29	0.00	0.00	20.9
39	0	-0	2976	0	0	0	-908	--	--	16.08	16.08	0.18	0.02	0.02	0.19	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	3176	0	0	0	3548	--	--	16.08	16.08	0.00	0.06	0.03	0.20	0.00	0.00	20.9
2	26	-0	2107	0	0	0	-950	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
3	26	-0	2154	0	0	0	-930	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
4	26	-0	2732	0	0	0	3532	--	--	16.08	16.08	0.10	0.06	0.02	0.17	0.00	0.00	20.9
5	26	-0	2779	0	0	0	3615	--	--	16.08	16.08	0.10	0.06	0.02	0.17	0.00	0.00	20.9
6	26	-0	2271	0	0	0	-673	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
7	26	-0	2427	0	0	0	2614	--	--	16.08	16.08	0.10	0.05	0.02	0.15	0.00	0.00	20.9
8	26	-0	2458	0	0	0	2843	--	--	16.08	16.08	0.10	0.05	0.02	0.15	0.00	0.00	20.9
9	26	-0	2615	0	0	0	3121	--	--	16.08	16.08	0.10	0.06	0.02	0.16	0.00	0.00	20.9
10	26	-0	2107	0	0	0	-950	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
11	26	-0	2154	0	0	0	-930	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
12	26	-0	2732	0	0	0	3532	--	--	16.08	16.08	0.10	0.06	0.02	0.17	0.00	0.00	20.9
13	26	-0	2779	0	0	0	3615	--	--	16.08	16.08	0.10	0.06	0.02	0.17	0.00	0.00	20.9
14	26	-0	2271	0	0	0	-673	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
15	26	-0	2427	0	0	0	2614	--	--	16.08	16.08	0.10	0.05	0.02	0.15	0.00	0.00	20.9
16	26	-0	2458	0	0	0	2843	--	--	16.08	16.08	0.10	0.05	0.02	0.15	0.00	0.00	20.9
17	26	-0	2615	0	0	0	3121	--	--	16.08	16.08	0.10	0.06	0.02	0.16	0.00	0.00	20.9
18	26	-0	1776	0	0	0	-2566	--	--	16.08	16.08	0.18	0.04	0.01	0.11	0.00	0.00	20.9
19	26	-0	3843	0	0	0	5104	--	--	16.08	16.08	0.00	0.09	0.03	0.24	0.00	0.00	20.9
20	26	-0	2855	0	0	0	-1171	--	--	16.08	16.08	0.18	0.02	0.02	0.18	0.00	0.00	20.9
37	26	-0	1177	0	0	0	-3233	--	--	16.08	16.08	0.18	0.05	0.01	0.07	0.00	0.00	20.9
38	26	-0	4622	0	0	0	7188	--	--	16.08	16.08	0.00	0.12	0.04	0.29	0.00	0.00	20.9
39	26	-0	2976	0	0	0	-908	--	--	16.08	16.08	0.18	0.02	0.02	0.19	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	3176	0	0	0	969	--	--	16.08	16.08	0.00	0.02	0.03	0.20	0.00	0.00	20.9
2	51	-0	2107	0	0	0	132	--	--	16.08	16.08	0.10	0.00	0.02	0.13	0.00	0.00	20.9

3	51	-0	2154	0	0	0	177	--	--	16.08	16.08	0.10	0.00	0.02	0.14	0.00	0.00	20.9
4	51	-0	2732	0	0	0	1314	--	--	16.08	16.08	0.10	0.02	0.02	0.17	0.00	0.00	20.9
5	51	-0	2779	0	0	0	1359	--	--	16.08	16.08	0.10	0.02	0.02	0.17	0.00	0.00	20.9
6	51	-0	2271	0	0	0	493	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
7	51	-0	2427	0	0	0	643	--	--	16.08	16.08	0.10	0.01	0.02	0.15	0.00	0.00	20.9
8	51	-0	2458	0	0	0	848	--	--	16.08	16.08	0.10	0.02	0.02	0.15	0.00	0.00	20.9
9	51	-0	2615	0	0	0	998	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
10	51	-0	2107	0	0	0	132	--	--	16.08	16.08	0.10	0.00	0.02	0.13	0.00	0.00	20.9
11	51	-0	2154	0	0	0	177	--	--	16.08	16.08	0.10	0.00	0.02	0.14	0.00	0.00	20.9
12	51	-0	2732	0	0	0	1314	--	--	16.08	16.08	0.10	0.02	0.02	0.17	0.00	0.00	20.9
13	51	-0	2779	0	0	0	1359	--	--	16.08	16.08	0.10	0.02	0.02	0.17	0.00	0.00	20.9
14	51	-0	2271	0	0	0	493	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
15	51	-0	2427	0	0	0	643	--	--	16.08	16.08	0.10	0.01	0.02	0.15	0.00	0.00	20.9
16	51	-0	2458	0	0	0	848	--	--	16.08	16.08	0.10	0.02	0.02	0.15	0.00	0.00	20.9
17	51	-0	2615	0	0	0	998	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
18	51	-0	1776	0	0	0	-2566	--	--	16.08	16.08	0.18	0.04	0.01	0.11	0.00	0.00	20.9
19	51	-0	3843	0	0	0	1984	--	--	16.08	16.08	0.00	0.03	0.03	0.24	0.00	0.00	20.9
20	51	-0	2855	0	0	0	295	--	--	16.08	16.08	0.00	0.01	0.02	0.18	0.00	0.00	20.9
37	51	-0	1177	0	0	0	-3233	--	--	16.08	16.08	0.18	0.05	0.01	0.07	0.00	0.00	20.9
38	51	-0	4622	0	0	0	3435	--	--	16.08	16.08	0.00	0.06	0.04	0.29	0.00	0.00	20.9
39	51	-0	2976	0	0	0	621	--	--	16.08	16.08	0.00	0.01	0.02	0.19	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 116 NI 1348 NF 1257 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	4172	0	0	0	969	--	--	16.08	16.08	0.00	0.02	0.03	0.26	0.00	0.00	20.9
2	0	-0	2844	0	0	0	132	--	--	16.08	16.08	0.10	0.00	0.02	0.18	0.00	0.00	20.9
3	0	-0	2901	0	0	0	177	--	--	16.08	16.08	0.10	0.00	0.02	0.18	0.00	0.00	20.9
4	0	-0	3516	0	0	0	1314	--	--	16.08	16.08	0.10	0.02	0.03	0.22	0.00	0.00	20.9
5	0	-0	3574	0	0	0	1359	--	--	16.08	16.08	0.10	0.02	0.03	0.22	0.00	0.00	20.9
6	0	-0	3012	0	0	0	493	--	--	16.08	16.08	0.10	0.01	0.02	0.19	0.00	0.00	20.9
7	0	-0	3204	0	0	0	643	--	--	16.08	16.08	0.10	0.01	0.03	0.20	0.00	0.00	20.9
8	0	-0	3214	0	0	0	848	--	--	16.08	16.08	0.10	0.02	0.03	0.20	0.00	0.00	20.9
9	0	-0	3406	0	0	0	998	--	--	16.08	16.08	0.10	0.02	0.03	0.21	0.00	0.00	20.9
10	0	-0	2844	0	0	0	132	--	--	16.08	16.08	0.10	0.00	0.02	0.18	0.00	0.00	20.9
11	0	-0	2901	0	0	0	177	--	--	16.08	16.08	0.10	0.00	0.02	0.18	0.00	0.00	20.9
12	0	-0	3516	0	0	0	1314	--	--	16.08	16.08	0.10	0.02	0.03	0.22	0.00	0.00	20.9
13	0	-0	3574	0	0	0	1359	--	--	16.08	16.08	0.10	0.02	0.03	0.22	0.00	0.00	20.9
14	0	-0	3012	0	0	0	493	--	--	16.08	16.08	0.10	0.01	0.02	0.19	0.00	0.00	20.9
15	0	-0	3204	0	0	0	643	--	--	16.08	16.08	0.10	0.01	0.03	0.20	0.00	0.00	20.9
16	0	-0	3214	0	0	0	848	--	--	16.08	16.08	0.10	0.02	0.03	0.20	0.00	0.00	20.9
17	0	-0	3406	0	0	0	998	--	--	16.08	16.08	0.10	0.02	0.03	0.21	0.00	0.00	20.9
18	0	-0	2665	0	0	0	-1654	--	--	16.08	16.08	0.18	0.03	0.02	0.17	0.00	0.00	20.9
19	0	-0	4923	0	0	0	1984	--	--	16.08	16.08	0.00	0.03	0.04	0.31	0.00	0.00	20.9
20	0	-0	3839	0	0	0	295	--	--	16.08	16.08	0.00	0.01	0.03	0.24	0.00	0.00	20.9
37	0	-0	1999	0	0	0	-2629	--	--	16.08	16.08	0.18	0.04	0.02	0.13	0.00	0.00	20.9
38	0	-0	5762	0	0	0	3435	--	--	16.08	16.08	0.00	0.06	0.05	0.36	0.00	0.00	20.9
39	0	-0	3955	0	0	0	621	--	--	16.08	16.08	0.00	0.01	0.03	0.25	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	4172	0	0	0	6499	--	--	16.08	16.08	0.00	0.11	0.03	0.26	0.00	0.00	20.9
2	26	-0	2844	0	0	0	3902	--	--	16.08	16.08	0.10	0.07	0.02	0.18	0.00	0.00	20.9
3	26	-0	2901	0	0	0	4022	--	--	16.08	16.08	0.10	0.07	0.02	0.18	0.00	0.00	20.9
4	26	-0	3516	0	0	0	5975	--	--	16.08	16.08	0.10	0.11	0.03	0.22	0.00	0.00	20.9
5	26	-0	3574	0	0	0	6097	--	--	16.08	16.08	0.10	0.11	0.03	0.22	0.00	0.00	20.9
6	26	-0	3012	0	0	0	4486	--	--	16.08	16.08	0.10	0.08	0.02	0.19	0.00	0.00	20.9
7	26	-0	3204	0	0	0	4890	--	--	16.08	16.08	0.10	0.09	0.03	0.20	0.00	0.00	20.9
8	26	-0	3214	0	0	0	5108	--	--	16.08	16.08	0.10	0.09	0.03	0.20	0.00	0.00	20.9
9	26	-0	3406	0	0	0	5513	--	--	16.08	16.08	0.10	0.10	0.03	0.21	0.00	0.00	20.9
10	26	-0	2844	0	0	0	3902	--	--	16.08	16.08	0.10	0.07	0.02	0.18	0.00	0.00	20.9
11	26	-0	2901	0	0	0	4022	--	--	16.08	16.08	0.10	0.07	0.02	0.18	0.00	0.00	20.9
12	26	-0	3516	0	0	0	5975	--	--	16.08	16.08	0.10	0.11	0.03	0.22	0.00	0.00	20.9
13	26	-0	3574	0	0	0	6097	--	--	16.08	16.08	0.10	0.11	0.03	0.22	0.00	0.00	20.9
14	26	-0	3012	0	0	0	4486	--	--	16.08	16.08	0.10	0.08	0.02	0.19	0.00	0.00	20.9
15	26	-0	3204	0	0	0	4890	--	--	16.08	16.08	0.10	0.09	0.03	0.20	0.00	0.00	20.9
16	26	-0	3214	0	0	0	5108	--	--	16.08	16.08	0.10	0.09	0.03	0.20	0.00	0.00	20.9
17	26	-0	3406	0	0	0	5513	--	--	16.08	16.08	0.10	0.10	0.03	0.21	0.00	0.00	20.9
18	26	-0	2665	0	0	0	-1654	--	--	16.08	16.08	0.18	0.03	0.02	0.17	0.00	0.00	20.9
19	26	-0	4923	0	0	0	8509	--	--	16.08	16.08	0.00	0.15	0.04	0.31	0.00	0.00	20.9
20	26	-0	3839	0	0	0	5384	--	--	16.08	16.08	0.00	0.09	0.03	0.24	0.00	0.00	20.9
37	26	-0	1999	0	0	0	-2629	--	--	16.08	16.08	0.18	0.04	0.02	0.13	0.00	0.00	20.9
38	26	-0	5762	0	0	0	11073	--	--	16.08	16.08	0.00	0.19	0.05	0.36	0.00	0.00	20.9
39	26	-0	3955	0	0	0	5863	--	--	16.08	16.08	0.00	0.10	0.03	0.25	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	4172	0	0	0	3112	--	--	16.08	16.08	0.00	0.05	0.03	0.26	0.00	0.00	20.9
2	51	-0	2844	0	0	0	1593	--	--	16.08	16.08	0.10	0.03	0.02	0.18	0.00	0.00	20.9
3	51	-0	2901	0	0	0	1667	--	--	16.08	16.08	0.10	0.03	0.02	0.18	0.00	0.00	20.9
4	51	-0	3516	0	0	0	3120	--	--	16.08	16.08	0.10	0.06	0.03	0.22	0.00	0.00	20.9
5	51	-0	3574	0	0	0	3195	--	--	16.08	16.08	0.10	0.06	0.03	0.22	0.00	0.00	20.9
6	51	-0	3012	0	0	0	2040	--	--	16.08	16.08	0.10	0.04	0.02	0.19	0.00	0.00	20.9
7	51	-0	3204	0	0	0	2289	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
8	51	-0	3214	0	0	0	2498	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
9	51	-0	3406	0	0	0	2747	--	--	16.08	16.08	0.10	0.05	0.03	0.21	0.00	0.00	20.9
10	51	-0	2844	0	0	0	1593	--	--	16.08	16.08	0.10	0.03	0.02	0.18	0.00	0.00	20.9
11	51	-0	2901	0	0	0	1667	--	--	16.08	16.08	0.10	0.03	0.02	0.18	0.00	0.00	20.9
12	51	-0	3516	0	0	0	3120	--	--	16.08	16.08	0.10	0.06	0.03	0.22	0.00	0.00	20.9
13	51	-0	3574	0	0	0	3195	--	--	16.08	16.08	0.10	0.06	0.03	0.22	0.00	0.00	20.9
14	51	-0	3012	0	0	0	2040	--	--	16.08	16.08	0.10	0.04	0.02	0.19	0.00	0.00	20.9
15	51	-0	3204	0	0	0	2289	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
16	51	-0	3214	0	0	0	2498	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
17	51	-0	3406	0	0	0	2747	--	--	16.08	16.08	0.10	0.05	0.03	0.21	0.00	0.00	20.9
18	51	-0	2665	0	0	0	-1654	--	--	16.08	16.08	0.18	0.03	0.02	0.17	0.00	0.00	20.9
19	51	-0	4923	0	0	0	4512	--	--	16.08	16.08	0.00	0.08	0.04	0.31	0.00	0.00	20.9
20	51	-0	3839	0	0	0	2267	--	--	16.08	16.08	0.00	0.04	0.03	0.24	0.00	0.00	20.9
37	51	-0	1999	0	0	0	-2629	--	--	16.08	16.08	0.18	0.04	0.02	0.13	0.00	0.00	20.9
38	51	-0	5762	0	0	0	6394	--	--	16.08	16.08	0.00	0.11	0.05	0.36	0.00	0.00	20.9
39	51	-0	3955	0	0	0	2652	--	--	16.08	16.08	0.00	0.05	0.03	0.25	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 117 NI 1257 NF 1287 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-7318	0	0	0	5132	--	--	16.08	16.08	0.00	0.09	0.06	0.46	0.00	0.00	20.9
2	0	-0	-6015	0	0	0	4478	--	--	16.08	16.08	0.10	0.08	0.05	0.38	0.00	0.00	20.9
3	0	-0	-6074	0	0	0	4565	--	--	16.08	16.08	0.10	0.08	0.05	0.38	0.00	0.00	20.9
4	0	-0	-5184	0	0	0	3331	--	--	16.08	16.08	0.10	0.06	0.04	0.33	0.00	0.00	20.9
5	0	-0	-5243	0	0	0	3418	--	--	16.08	16.08	0.10	0.06	0.04	0.33	0.00	0.00	20.9
6	0	-0	-5656	0	0	0	3975	--	--	16.08	16.08	0.10	0.07	0.05	0.35	0.00	0.00	20.9
7	0	-0	-5852	0	0	0	4265	--	--	16.08	16.08	0.10	0.08	0.05	0.37	0.00	0.00	20.9
8	0	-0	-5407	0	0	0	3631	--	--	16.08	16.08	0.10	0.06	0.04	0.34	0.00	0.00	20.9
9	0	-0	-5602	0	0	0	3921	--	--	16.08	16.08	0.10	0.07	0.05	0.35	0.00	0.00	20.9
10	0	-0	-6015	0	0	0	4478	--	--	16.08	16.08	0.10	0.08	0.05	0.38	0.00	0.00	20.9
11	0	-0	-6074	0	0	0	4565	--	--	16.08	16.08	0.10	0.08	0.05	0.38	0.00	0.00	20.9
12	0	-0	-5184	0	0	0	3331	--	--	16.08	16.08	0.10	0.06	0.04	0.33	0.00	0.00	20.9
13	0	-0	-5243	0	0	0	3418	--	--	16.08	16.08	0.10	0.06	0.04	0.33	0.00	0.00	20.9
14	0	-0	-5656	0	0	0	3975	--	--	16.08	16.08	0.10	0.07	0.05	0.35	0.00	0.00	20.9
15	0	-0	-5852	0	0	0	4265	--	--	16.08	16.08	0.10	0.08	0.05	0.37	0.00	0.00	20.9
16	0	-0	-5407	0	0	0	3631	--	--	16.08	16.08	0.10	0.06	0.04	0.34	0.00	0.00	20.9
17	0	-0	-5602	0	0	0	3921	--	--	16.08	16.08	0.10	0.07	0.05	0.35	0.00	0.00	20.9
18	0	-0	-10280	0	0	0	8206	--	--	16.08	16.08	0.00	0.14	0.08	0.64	0.00	0.00	20.9
19	0	-0	-7333	0	0	0	3999	--	--	16.08	16.08	0.00	0.07	0.06	0.46	0.00	0.00	20.9
20	0	-0	-8606	0	0	0	5979	--	--	16.08	16.08	0.00	0.10	0.07	0.54	0.00	0.00	20.9
37	0	-0	-10740	0	0	0	9244	--	--	16.08	16.08	0.00	0.16	0.09	0.67	0.00	0.00	20.9
38	0	-0	-5825	0	0	0	2233	--	--	16.08	16.08	0.00	0.04	0.05	0.37	0.00	0.00	20.9
39	0	-0	-7945	0	0	0	5532	--	--	16.08	16.08	0.00	0.09	0.07	0.50	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	26	-0	-7318	0	0	0	5132	--	--	16.08	16.08	0.00	0.09	0.06	0.46	0.00	0.00	20.9
2	26	-0	-6015	0	0	0	4478	--	--	16.08	16.08	0.10	0.08	0.05	0.38	0.00	0.00	20.9
3	26	-0	-6074	0	0	0	4565	--	--	16.08	16.08	0.10	0.08	0.05	0.38	0.00	0.00	20.9
4	26	-0	-5184	0	0	0	3331	--	--	16.08	16.08	0.10	0.06	0.04	0.33	0.00	0.00	20.9
5	26	-0	-5243	0	0	0	3418	--	--	16.08	16.08	0.10	0.06	0.04	0.33	0.00	0.00	20.9
6	26	-0	-5656	0	0	0	3975	--	--	16.08	16.08	0.10	0.07	0.05	0.35	0.00	0.00	20.9
7	26	-0	-5852	0	0	0	4265	--	--	16.08	16.08	0.10	0.08	0.05	0.37	0.00	0.00	20.9
8	26	-0	-5407	0	0	0	3631	--	--	16.08	16.08	0.10	0.06	0.04	0.34	0.00	0.00	20.9
9	26	-0	-5602	0	0	0	3921	--	--	16.08	16.08	0.10	0.07	0.05	0.35	0.00	0.00	20.9
10	26	-0	-6015	0	0	0	4478	--	--	16.08	16.08	0.10	0.08	0.05	0.38	0.00	0.00	20.9
11	26	-0	-6074	0	0	0	4565	--	--	16.08	16.08	0.10	0.08	0.05	0.38	0.00	0.00	20.9
12	26	-0	-5184	0	0	0	3331	--	--	16.08	16.08	0.10	0.06	0.04	0.33	0.00	0.00	20.9
13	26	-0	-5243	0	0	0	3418	--	--	16.08	16.08	0.10	0.06	0.04	0.33	0.00	0.00	20.9
14	26	-0	-5656	0	0	0	3975	--	--	16.08	16.08	0.10	0.07	0.05	0.35	0.00	0.00	20.9
15	26	-0	-5852	0	0	0	4265	--	--	16.08	16.08	0.10	0.08	0.05	0.37	0.00	0.00	20.9
16	26	-0	-5407	0	0	0	3631	--	--	16.08	16.08	0.10	0.06	0.04	0.34	0.00	0.00	20.9
17	26	-0	-5602	0	0	0	3921	--	--	16.08	16.08	0.10	0.07	0.05	0.35	0.00	0.00	20.9
18	26	-0	-10280	0	0	0	8206	--	--	16.08	16.08	0.00	0.14	0.08	0.64	0.00	0.00	20.9
19	26	-0	-7333	0	0	0	3999	--	--	16.08	16.08	0.00	0.07	0.06	0.46	0.00	0.00	20.9
20	26	-0	-8606	0	0	0	5979	--	--	16.08	16.08	0.00	0.10	0.07	0.54	0.00	0.00	20.9
37	26	-0	-10740	0	0	0	9244	--	--	16.08	16.08	0.00	0.16	0.09	0.67	0.00	0.00	20.9
38	26	-0	-5825	0	0	0	2233	--	--	16.08	16.08	0.00	0.04	0.05	0.37	0.00	0.00	20.9
39	26	-0	-7945	0	0	0	5532	--	--	16.08	16.08	0.00	0.09	0.07	0.50	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	51	-0	-7318	0	0	0	1374	--	--	16.08	16.08	0.00	0.02	0.06	0.46	0.00	0.00	20.9
2	51	-0	-6015	0	0	0	1388	--	--	16.08	16.08	0.10	0.02	0.05	0.38	0.00	0.00	20.9
3	51	-0	-6074	0	0	0	1445	--	--	16.08	16.08	0.10	0.03	0.05	0.38	0.00	0.00	20.9
4	51	-0	-5184	0	0	0	668	--	--	16.08	16.08	0.10	0.01	0.04	0.33	0.00	0.00	20.9
5	51	-0	-5243	0	0	0	725	--	--	16.08	16.08	0.10	0.01	0.04	0.33	0.00	0.00	20.9
6	51	-0	-5656	0	0	0	1070	--	--	16.08	16.08	0.10	0.02	0.05	0.35	0.00	0.00	20.9
7	51	-0	-5852	0	0	0	1259	--	--	16.08	16.08	0.10	0.02	0.05	0.37	0.00	0.00	20.9
8	51	-0	-5407	0	0	0	854	--	--	16.08	16.08	0.10	0.02	0.04	0.34	0.00	0.00	20.9
9	51	-0	-5602	0	0	0	1043	--	--	16.08	16.08	0.10	0.02	0.05	0.35	0.00	0.00	20.9
10	51	-0	-6015	0	0	0	1388	--	--	16.08	16.08	0.10	0.02	0.05	0.38	0.00	0.00	20.9
11	51	-0	-6074	0	0	0	1445	--	--	16.08	16.08	0.10	0.03	0.05	0.38	0.00	0.00	20.9
12	51	-0	-5184	0	0	0	668	--	--	16.08	16.08	0.10	0.01	0.04	0.33	0.00	0.00	20.9
13	51	-0	-5243	0	0	0	725	--	--	16.08	16.08	0.10	0.01	0.04	0.33	0.00	0.00	20.9
14	51	-0	-5656	0	0	0	1070	--	--	16.08	16.08	0.10	0.02	0.05	0.35	0.00	0.00	20.9
15	51	-0	-5852	0	0	0	1259	--	--	16.08	16.08	0.10	0.02	0.05	0.37	0.00	0.00	20.9
16	51	-0	-5407	0	0	0	854	--	--	16.08	16.08	0.10	0.02	0.04	0.34	0.00	0.00	20.9
17	51	-0	-5602	0	0	0	1043	--	--	16.08	16.08	0.10	0.02	0.05	0.35	0.00	0.00	20.9
18	51	-0	-10280	0	0	0	2926	--	--	16.08	16.08	0.00	0.05	0.08	0.64	0.00	0.00	20.9
19	51	-0	-7333	0	0	0	233	--	--	16.08	16.08	0.00	0.00	0.06	0.46	0.00	0.00	20.9
20	51	-0	-8606	0	0	0	1559	--	--	16.08	16.08	0.00	0.03	0.07	0.54	0.00	0.00	20.9
37	51	-0	-10740	0	0	0	3729	--	--	16.08	16.08	0.00	0.06	0.09	0.67	0.00	0.00	20.9
38	51	-0	-5825	0	0	0	-759	--	--	16.08	16.08	0.18	0.01	0.05	0.37	0.00	0.00	20.9
39	51	-0	-7945	0	0	0	1451	--	--	16.08	16.08	0.00	0.02	0.07	0.50	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 118 NI 1287 NF 1324 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-6317	0	0	0	1374	--	--	16.08	16.08	0.00	0.02	0.05	0.40	0.00	0.00	20.9
2	0	-0	-5271	0	0	0	1388	--	--	16.08	16.08	0.10	0.02	0.04	0.33	0.00	0.00	20.9
3	0	-0	-5319	0	0	0	1445	--	--	16.08	16.08	0.10	0.03	0.04	0.33	0.00	0.00	20.9
4	0	-0	-4400	0	0	0	668	--	--	16.08	16.08	0.10	0.01	0.04	0.28	0.00	0.00	20.9
5	0	-0	-4448	0	0	0	725	--	--	16.08	16.08	0.10	0.01	0.04	0.28	0.00	0.00	20.9
6	0	-0	-4910	0	0	0	1070	--	--	16.08	16.08	0.10	0.02	0.04	0.31	0.00	0.00	20.9
7	0	-0	-5071	0	0	0	1259	--	--	16.08	16.08	0.10	0.02	0.04	0.32	0.00	0.00	20.9
8	0	-0	-4648	0	0	0	854	--	--	16.08	16.08	0.10	0.02	0.04	0.29	0.00	0.00	20.9
9	0	-0	-4809	0	0	0	1043	--	--	16.08	16.08	0.10	0.02	0.04	0.30	0.00	0.00	20.9
10	0	-0	-5271	0	0	0	1388	--	--	16.08	16.08	0.10	0.02	0.04	0.33	0.00	0.00	20.9

11	0	-0	-5319	0	0	0	1445	--	--	16.08	16.08	0.10	0.03	0.04	0.33	0.00	0.00	20.9
12	0	-0	-4400	0	0	0	668	--	--	16.08	16.08	0.10	0.01	0.04	0.28	0.00	0.00	20.9
13	0	-0	-4448	0	0	0	725	--	--	16.08	16.08	0.10	0.01	0.04	0.28	0.00	0.00	20.9
14	0	-0	-4910	0	0	0	1070	--	--	16.08	16.08	0.10	0.02	0.04	0.31	0.00	0.00	20.9
15	0	-0	-5071	0	0	0	1259	--	--	16.08	16.08	0.10	0.02	0.04	0.32	0.00	0.00	20.9
16	0	-0	-4648	0	0	0	854	--	--	16.08	16.08	0.10	0.02	0.04	0.29	0.00	0.00	20.9
17	0	-0	-4809	0	0	0	1043	--	--	16.08	16.08	0.10	0.02	0.04	0.30	0.00	0.00	20.9
18	0	-0	-9394	0	0	0	2926	--	--	16.08	16.08	0.00	0.05	0.08	0.59	0.00	0.00	20.9
19	0	-0	-6257	0	0	0	233	--	--	16.08	16.08	0.00	0.00	0.05	0.39	0.00	0.00	20.9
20	0	-0	-7622	0	0	0	1559	--	--	16.08	16.08	0.00	0.03	0.06	0.48	0.00	0.00	20.9
37	0	-0	-9914	0	0	0	3729	--	--	16.08	16.08	0.00	0.06	0.08	0.62	0.00	0.00	20.9
38	0	-0	-4686	0	0	0	-3166	--	--	16.08	16.08	0.18	0.05	0.04	0.29	0.00	0.00	20.9
39	0	-0	-6962	0	0	0	1451	--	--	16.08	16.08	0.00	0.02	0.06	0.44	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	-6317	0	0	0	-1872	--	--	16.08	16.08	0.18	0.03	0.05	0.40	0.00	0.00	20.9
2	26	-0	-5271	0	0	0	1388	--	--	16.08	16.08	0.10	0.02	0.04	0.33	0.00	0.00	20.9
3	26	-0	-5319	0	0	0	1445	--	--	16.08	16.08	0.10	0.03	0.04	0.33	0.00	0.00	20.9
4	26	-0	-4400	0	0	0	-1592	--	--	16.08	16.08	0.29	0.03	0.04	0.28	0.00	0.00	20.9
5	26	-0	-4448	0	0	0	-1560	--	--	16.08	16.08	0.29	0.03	0.04	0.28	0.00	0.00	20.9
6	26	-0	-4910	0	0	0	-1452	--	--	16.08	16.08	0.29	0.03	0.04	0.31	0.00	0.00	20.9
7	26	-0	-5071	0	0	0	-1345	--	--	16.08	16.08	0.29	0.02	0.04	0.32	0.00	0.00	20.9
8	26	-0	-4648	0	0	0	-1534	--	--	16.08	16.08	0.29	0.03	0.04	0.29	0.00	0.00	20.9
9	26	-0	-4809	0	0	0	-1427	--	--	16.08	16.08	0.29	0.02	0.04	0.30	0.00	0.00	20.9
10	26	-0	-5271	0	0	0	1388	--	--	16.08	16.08	0.10	0.02	0.04	0.33	0.00	0.00	20.9
11	26	-0	-5319	0	0	0	1445	--	--	16.08	16.08	0.10	0.03	0.04	0.33	0.00	0.00	20.9
12	26	-0	-4400	0	0	0	-1592	--	--	16.08	16.08	0.29	0.03	0.04	0.28	0.00	0.00	20.9
13	26	-0	-4448	0	0	0	-1560	--	--	16.08	16.08	0.29	0.03	0.04	0.28	0.00	0.00	20.9
14	26	-0	-4910	0	0	0	-1452	--	--	16.08	16.08	0.29	0.03	0.04	0.31	0.00	0.00	20.9
15	26	-0	-5071	0	0	0	-1345	--	--	16.08	16.08	0.29	0.02	0.04	0.32	0.00	0.00	20.9
16	26	-0	-4648	0	0	0	-1534	--	--	16.08	16.08	0.29	0.03	0.04	0.29	0.00	0.00	20.9
17	26	-0	-4809	0	0	0	-1427	--	--	16.08	16.08	0.29	0.02	0.04	0.30	0.00	0.00	20.9
18	26	-0	-9394	0	0	0	2926	--	--	16.08	16.08	0.00	0.05	0.08	0.59	0.00	0.00	20.9
19	26	-0	-6257	0	0	0	-2981	--	--	16.08	16.08	0.18	0.05	0.05	0.39	0.00	0.00	20.9
20	26	-0	-7622	0	0	0	-2357	--	--	16.08	16.08	0.18	0.04	0.06	0.48	0.00	0.00	20.9
37	26	-0	-9914	0	0	0	3729	--	--	16.08	16.08	0.00	0.06	0.08	0.62	0.00	0.00	20.9
38	26	-0	-4686	0	0	0	-3166	--	--	16.08	16.08	0.18	0.05	0.04	0.29	0.00	0.00	20.9
39	26	-0	-6962	0	0	0	-2125	--	--	16.08	16.08	0.18	0.04	0.06	0.44	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	-6317	0	0	0	-1872	--	--	16.08	16.08	0.18	0.03	0.05	0.40	0.00	0.00	20.9
2	51	-0	-5271	0	0	0	-1320	--	--	16.08	16.08	0.29	0.02	0.04	0.33	0.00	0.00	20.9
3	51	-0	-5319	0	0	0	-1288	--	--	16.08	16.08	0.29	0.02	0.04	0.33	0.00	0.00	20.9
4	51	-0	-4400	0	0	0	-1592	--	--	16.08	16.08	0.29	0.03	0.04	0.28	0.00	0.00	20.9
5	51	-0	-4448	0	0	0	-1560	--	--	16.08	16.08	0.29	0.03	0.04	0.28	0.00	0.00	20.9
6	51	-0	-4910	0	0	0	-1452	--	--	16.08	16.08	0.29	0.03	0.04	0.31	0.00	0.00	20.9
7	51	-0	-5071	0	0	0	-1345	--	--	16.08	16.08	0.29	0.02	0.04	0.32	0.00	0.00	20.9
8	51	-0	-4648	0	0	0	-1534	--	--	16.08	16.08	0.29	0.03	0.04	0.29	0.00	0.00	20.9
9	51	-0	-4809	0	0	0	-1427	--	--	16.08	16.08	0.29	0.02	0.04	0.30	0.00	0.00	20.9
10	51	-0	-5271	0	0	0	-1320	--	--	16.08	16.08	0.29	0.02	0.04	0.33	0.00	0.00	20.9
11	51	-0	-5319	0	0	0	-1288	--	--	16.08	16.08	0.29	0.02	0.04	0.33	0.00	0.00	20.9
12	51	-0	-4400	0	0	0	-1592	--	--	16.08	16.08	0.29	0.03	0.04	0.28	0.00	0.00	20.9
13	51	-0	-4448	0	0	0	-1560	--	--	16.08	16.08	0.29	0.03	0.04	0.28	0.00	0.00	20.9
14	51	-0	-4910	0	0	0	-1452	--	--	16.08	16.08	0.29	0.03	0.04	0.31	0.00	0.00	20.9
15	51	-0	-5071	0	0	0	-1345	--	--	16.08	16.08	0.29	0.02	0.04	0.32	0.00	0.00	20.9
16	51	-0	-4648	0	0	0	-1534	--	--	16.08	16.08	0.29	0.03	0.04	0.29	0.00	0.00	20.9
17	51	-0	-4809	0	0	0	-1427	--	--	16.08	16.08	0.29	0.02	0.04	0.30	0.00	0.00	20.9
18	51	-0	-9394	0	0	0	-1900	--	--	16.08	16.08	0.18	0.03	0.08	0.59	0.00	0.00	20.9
19	51	-0	-6257	0	0	0	-2981	--	--	16.08	16.08	0.18	0.05	0.05	0.39	0.00	0.00	20.9
20	51	-0	-7622	0	0	0	-2357	--	--	16.08	16.08	0.18	0.04	0.06	0.48	0.00	0.00	20.9
37	51	-0	-9914	0	0	0	-1364	--	--	16.08	16.08	0.18	0.02	0.08	0.62	0.00	0.00	20.9
38	51	-0	-4686	0	0	0	-3166	--	--	16.08	16.08	0.18	0.05	0.04	0.29	0.00	0.00	20.9
39	51	-0	-6962	0	0	0	-2125	--	--	16.08	16.08	0.18	0.04	0.06	0.44	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 119 NI 1324 NF 1297 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm

1	0	-0	-5341	0	0	0	-4615	--	--	16.08	16.08	0.18	0.08	0.04	0.34	0.00	0.00	20.9
2	0	-0	-4545	0	0	0	-3654	--	--	16.08	16.08	0.29	0.06	0.04	0.29	0.00	0.00	20.9
3	0	-0	-4584	0	0	0	-3642	--	--	16.08	16.08	0.29	0.06	0.04	0.29	0.00	0.00	20.9
4	0	-0	-3634	0	0	0	-3458	--	--	16.08	16.08	0.29	0.06	0.03	0.23	0.00	0.00	20.9
5	0	-0	-3673	0	0	0	-3446	--	--	16.08	16.08	0.29	0.06	0.03	0.23	0.00	0.00	20.9
6	0	-0	-4181	0	0	0	-3599	--	--	16.08	16.08	0.29	0.06	0.03	0.26	0.00	0.00	20.9
7	0	-0	-4310	0	0	0	-3559	--	--	16.08	16.08	0.29	0.06	0.04	0.27	0.00	0.00	20.9
8	0	-0	-3907	0	0	0	-3541	--	--	16.08	16.08	0.29	0.06	0.03	0.25	0.00	0.00	20.9
9	0	-0	-4037	0	0	0	-3501	--	--	16.08	16.08	0.29	0.06	0.03	0.25	0.00	0.00	20.9
10	0	-0	-4545	0	0	0	-3654	--	--	16.08	16.08	0.29	0.06	0.04	0.29	0.00	0.00	20.9
11	0	-0	-4584	0	0	0	-3642	--	--	16.08	16.08	0.29	0.06	0.04	0.29	0.00	0.00	20.9
12	0	-0	-3634	0	0	0	-3458	--	--	16.08	16.08	0.29	0.06	0.03	0.23	0.00	0.00	20.9
13	0	-0	-3673	0	0	0	-3446	--	--	16.08	16.08	0.29	0.06	0.03	0.23	0.00	0.00	20.9
14	0	-0	-4181	0	0	0	-3599	--	--	16.08	16.08	0.29	0.06	0.03	0.26	0.00	0.00	20.9
15	0	-0	-4310	0	0	0	-3559	--	--	16.08	16.08	0.29	0.06	0.04	0.27	0.00	0.00	20.9
16	0	-0	-3907	0	0	0	-3541	--	--	16.08	16.08	0.29	0.06	0.03	0.25	0.00	0.00	20.9
17	0	-0	-4037	0	0	0	-3501	--	--	16.08	16.08	0.29	0.06	0.03	0.25	0.00	0.00	20.9
18	0	-0	-8543	0	0	0	-6288	--	--	16.08	16.08	0.18	0.10	0.07	0.54	0.00	0.00	20.9
19	0	-0	-5205	0	0	0	-5654	--	--	16.08	16.08	0.18	0.09	0.04	0.33	0.00	0.00	20.9
20	0	-0	-6667	0	0	0	-5781	--	--	16.08	16.08	0.18	0.10	0.05	0.42	0.00	0.00	20.9
37	0	-0	-9130	0	0	0	-6053	--	--	16.08	16.08	0.18	0.10	0.08	0.57	0.00	0.00	20.9
38	0	-0	-3566	0	0	0	-4997	--	--	16.08	16.08	0.18	0.08	0.03	0.22	0.00	0.00	20.9
39	0	-0	-6003	0	0	0	-5208	--	--	16.08	16.08	0.18	0.09	0.05	0.38	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	-5341	0	0	0	-4615	--	--	16.08	16.08	0.18	0.08	0.04	0.34	0.00	0.00	20.9
2	26	-0	-4545	0	0	0	-3654	--	--	16.08	16.08	0.29	0.06	0.04	0.29	0.00	0.00	20.9
3	26	-0	-4584	0	0	0	-3642	--	--	16.08	16.08	0.29	0.06	0.04	0.29	0.00	0.00	20.9
4	26	-0	-3634	0	0	0	-3458	--	--	16.08	16.08	0.29	0.06	0.03	0.23	0.00	0.00	20.9
5	26	-0	-3673	0	0	0	-3446	--	--	16.08	16.08	0.29	0.06	0.03	0.23	0.00	0.00	20.9
6	26	-0	-4181	0	0	0	-3599	--	--	16.08	16.08	0.29	0.06	0.03	0.26	0.00	0.00	20.9

7	26	-0	-4310	0	0	0	-3559	--	--	16.08	16.08	0.29	0.06	0.04	0.27	0.00	0.00	20.9
8	26	-0	-3907	0	0	0	-3541	--	--	16.08	16.08	0.29	0.06	0.03	0.25	0.00	0.00	20.9
9	26	-0	-4037	0	0	0	-3501	--	--	16.08	16.08	0.29	0.06	0.03	0.25	0.00	0.00	20.9
10	26	-0	-4545	0	0	0	-3654	--	--	16.08	16.08	0.29	0.06	0.04	0.29	0.00	0.00	20.9
11	26	-0	-4584	0	0	0	-3642	--	--	16.08	16.08	0.29	0.06	0.04	0.29	0.00	0.00	20.9
12	26	-0	-3634	0	0	0	-3458	--	--	16.08	16.08	0.29	0.06	0.03	0.23	0.00	0.00	20.9
13	26	-0	-3673	0	0	0	-3446	--	--	16.08	16.08	0.29	0.06	0.03	0.23	0.00	0.00	20.9
14	26	-0	-4181	0	0	0	-3599	--	--	16.08	16.08	0.29	0.06	0.03	0.26	0.00	0.00	20.9
15	26	-0	-4310	0	0	0	-3559	--	--	16.08	16.08	0.29	0.06	0.04	0.27	0.00	0.00	20.9
16	26	-0	-3907	0	0	0	-3541	--	--	16.08	16.08	0.29	0.06	0.03	0.25	0.00	0.00	20.9
17	26	-0	-4037	0	0	0	-3501	--	--	16.08	16.08	0.29	0.06	0.03	0.25	0.00	0.00	20.9
18	26	-0	-8543	0	0	0	-6288	--	--	16.08	16.08	0.18	0.10	0.07	0.54	0.00	0.00	20.9
19	26	-0	-5205	0	0	0	-5654	--	--	16.08	16.08	0.18	0.09	0.04	0.33	0.00	0.00	20.9
20	26	-0	-6667	0	0	0	-5781	--	--	16.08	16.08	0.18	0.10	0.05	0.42	0.00	0.00	20.9
37	26	-0	-9130	0	0	0	-6053	--	--	16.08	16.08	0.18	0.10	0.08	0.57	0.00	0.00	20.9
38	26	-0	-3566	0	0	0	-4997	--	--	16.08	16.08	0.18	0.08	0.03	0.22	0.00	0.00	20.9
39	26	-0	-6003	0	0	0	-5208	--	--	16.08	16.08	0.18	0.09	0.05	0.38	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	-5341	0	0	0	-4615	--	--	16.08	16.08	0.18	0.08	0.04	0.34	0.00	0.00	20.9
2	51	-0	-4545	0	0	0	-3654	--	--	16.08	16.08	0.29	0.06	0.04	0.29	0.00	0.00	20.9
3	51	-0	-4584	0	0	0	-3642	--	--	16.08	16.08	0.29	0.06	0.04	0.29	0.00	0.00	20.9
4	51	-0	-3634	0	0	0	-3458	--	--	16.08	16.08	0.29	0.06	0.03	0.23	0.00	0.00	20.9
5	51	-0	-3673	0	0	0	-3446	--	--	16.08	16.08	0.29	0.06	0.03	0.23	0.00	0.00	20.9
6	51	-0	-4181	0	0	0	-3599	--	--	16.08	16.08	0.29	0.06	0.03	0.26	0.00	0.00	20.9
7	51	-0	-4310	0	0	0	-3559	--	--	16.08	16.08	0.29	0.06	0.04	0.27	0.00	0.00	20.9
8	51	-0	-3907	0	0	0	-3541	--	--	16.08	16.08	0.29	0.06	0.03	0.25	0.00	0.00	20.9
9	51	-0	-4037	0	0	0	-3501	--	--	16.08	16.08	0.29	0.06	0.03	0.25	0.00	0.00	20.9
10	51	-0	-4545	0	0	0	-3654	--	--	16.08	16.08	0.29	0.06	0.04	0.29	0.00	0.00	20.9
11	51	-0	-4584	0	0	0	-3642	--	--	16.08	16.08	0.29	0.06	0.04	0.29	0.00	0.00	20.9
12	51	-0	-3634	0	0	0	-3458	--	--	16.08	16.08	0.29	0.06	0.03	0.23	0.00	0.00	20.9
13	51	-0	-3673	0	0	0	-3446	--	--	16.08	16.08	0.29	0.06	0.03	0.23	0.00	0.00	20.9
14	51	-0	-4181	0	0	0	-3599	--	--	16.08	16.08	0.29	0.06	0.03	0.26	0.00	0.00	20.9
15	51	-0	-4310	0	0	0	-3559	--	--	16.08	16.08	0.29	0.06	0.04	0.27	0.00	0.00	20.9
16	51	-0	-3907	0	0	0	-3541	--	--	16.08	16.08	0.29	0.06	0.03	0.25	0.00	0.00	20.9
17	51	-0	-4037	0	0	0	-3501	--	--	16.08	16.08	0.29	0.06	0.03	0.25	0.00	0.00	20.9
18	51	-0	-8543	0	0	0	-6288	--	--	16.08	16.08	0.18	0.10	0.07	0.54	0.00	0.00	20.9
19	51	-0	-5205	0	0	0	-5654	--	--	16.08	16.08	0.18	0.09	0.04	0.33	0.00	0.00	20.9
20	51	-0	-6667	0	0	0	-5781	--	--	16.08	16.08	0.18	0.10	0.05	0.42	0.00	0.00	20.9
37	51	-0	-9130	0	0	0	-6053	--	--	16.08	16.08	0.18	0.10	0.08	0.57	0.00	0.00	20.9
38	51	-0	-3566	0	0	0	-4997	--	--	16.08	16.08	0.18	0.08	0.03	0.22	0.00	0.00	20.9
39	51	-0	-6003	0	0	0	-5208	--	--	16.08	16.08	0.18	0.09	0.05	0.38	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 120 NI 1297 NF 1296 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-4379	0	0	0	-6864	--	--	16.08	16.08	0.18	0.11	0.04	0.27	0.00	0.00	20.9
2	0	-0	-3829	0	0	0	-5620	--	--	16.08	16.08	0.29	0.10	0.03	0.24	0.00	0.00	20.9
3	0	-0	-3859	0	0	0	-5624	--	--	16.08	16.08	0.29	0.10	0.03	0.24	0.00	0.00	20.9
4	0	-0	-2878	0	0	0	-4936	--	--	16.08	16.08	0.29	0.09	0.02	0.18	0.00	0.00	20.9
5	0	-0	-2908	0	0	0	-4940	--	--	16.08	16.08	0.29	0.09	0.02	0.18	0.00	0.00	20.9
6	0	-0	-3460	0	0	0	-5377	--	--	16.08	16.08	0.29	0.09	0.03	0.22	0.00	0.00	20.9
7	0	-0	-3562	0	0	0	-5389	--	--	16.08	16.08	0.29	0.09	0.03	0.22	0.00	0.00	20.9
8	0	-0	-3175	0	0	0	-5171	--	--	16.08	16.08	0.29	0.09	0.03	0.20	0.00	0.00	20.9
9	0	-0	-3276	0	0	0	-5183	--	--	16.08	16.08	0.29	0.09	0.03	0.21	0.00	0.00	20.9
10	0	-0	-3829	0	0	0	-5620	--	--	16.08	16.08	0.29	0.10	0.03	0.24	0.00	0.00	20.9
11	0	-0	-3859	0	0	0	-5624	--	--	16.08	16.08	0.29	0.10	0.03	0.24	0.00	0.00	20.9
12	0	-0	-2878	0	0	0	-4936	--	--	16.08	16.08	0.29	0.09	0.02	0.18	0.00	0.00	20.9
13	0	-0	-2908	0	0	0	-4940	--	--	16.08	16.08	0.29	0.09	0.02	0.18	0.00	0.00	20.9
14	0	-0	-3460	0	0	0	-5377	--	--	16.08	16.08	0.29	0.09	0.03	0.22	0.00	0.00	20.9
15	0	-0	-3562	0	0	0	-5389	--	--	16.08	16.08	0.29	0.09	0.03	0.22	0.00	0.00	20.9
16	0	-0	-3175	0	0	0	-5171	--	--	16.08	16.08	0.29	0.09	0.03	0.20	0.00	0.00	20.9
17	0	-0	-3276	0	0	0	-5183	--	--	16.08	16.08	0.29	0.09	0.03	0.21	0.00	0.00	20.9
18	0	-0	-7718	0	0	0	-10250	--	--	16.08	16.08	0.18	0.17	0.06	0.48	0.00	0.00	20.9
19	0	-0	-4160	0	0	0	-7791	--	--	16.08	16.08	0.18	0.13	0.03	0.26	0.00	0.00	20.9
20	0	-0	-5727	0	0	0	-8723	--	--	16.08	16.08	0.18	0.14	0.05	0.36	0.00	0.00	20.9
37	0	-0	-8375	0	0	0	-10350	--	--	16.08	16.08	0.18	0.17	0.07	0.53	0.00	0.00	20.9
38	0	-0	-2446	0	0	0	-6253	--	--	16.08	16.08	0.18	0.10	0.02	0.15	0.00	0.00	20.9
39	0	-0	-5057	0	0	0	-7806	--	--	16.08	16.08	0.18	0.13	0.04	0.32	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	-4379	0	0	0	-6864	--	--	16.08	16.08	0.18	0.11	0.04	0.27	0.00	0.00	20.9
2	26	-0	-3829	0	0	0	-5620	--	--	16.08	16.08	0.29	0.10	0.03	0.24	0.00	0.00	20.9
3	26	-0	-3859	0	0	0	-5624	--	--	16.08	16.08	0.29	0.10	0.03	0.24	0.00	0.00	20.9
4	26	-0	-2878	0	0	0	-4936	--	--	16.08	16.08	0.29	0.09	0.02	0.18	0.00	0.00	20.9
5	26	-0	-2908	0	0	0	-4940	--	--	16.08	16.08	0.29	0.09	0.02	0.18	0.00	0.00	20.9
6	26	-0	-3460	0	0	0	-5377	--	--	16.08	16.08	0.29	0.09	0.03	0.22	0.00	0.00	20.9
7	26	-0	-3562	0	0	0	-5389	--	--	16.08	16.08	0.29	0.09	0.03	0.22	0.00	0.00	20.9
8	26	-0	-3175	0	0	0	-5171	--	--	16.08	16.08	0.29	0.09	0.03	0.20	0.00	0.00	20.9
9	26	-0	-3276	0	0	0	-5183	--	--	16.08	16.08	0.29	0.09	0.03	0.21	0.00	0.00	20.9
10	26	-0	-3829	0	0	0	-5620	--	--	16.08	16.08	0.29	0.10	0.03	0.24	0.00	0.00	20.9
11	26	-0	-3859	0	0	0	-5624	--	--	16.08	16.08	0.29	0.10	0.03	0.24	0.00	0.00	20.9
12	26	-0	-2878	0	0	0	-4936	--	--	16.08	16.08	0.29	0.09	0.02	0.18	0.00	0.00	20.9
13	26	-0	-2908	0	0	0	-4940	--	--	16.08	16.08	0.29	0.09	0.02	0.18	0.00	0.00	20.9
14	26	-0	-3460	0	0	0	-5377	--	--	16.08	16.08	0.29	0.09	0.03	0.22	0.00	0.00	20.9
15	26	-0	-3562	0	0	0	-5389	--	--	16.08	16.08	0.29	0.09	0.03	0.22	0.00	0.00	20.9
16	26	-0	-3175	0	0	0	-5171	--	--	16.08	16.08	0.29	0.09	0.03	0.20	0.00	0.00	20.9
17	26	-0	-3276	0	0	0	-5183	--	--	16.08	16.08	0.29	0.09	0.03	0.21	0.00	0.00	20.9
18	26	-0	-7718	0	0	0	-10250	--	--	16.08	16.08	0.18	0.17	0.06	0.48	0.00	0.00	20.9
19	26	-0	-4160	0	0	0	-7791	--	--	16.08	16.08	0.18	0.13	0.03	0.26	0.00	0.00	20.9
20	26	-0	-5727	0	0	0	-8723	--	--	16.08	16.08	0.18	0.14	0.05	0.36	0.00	0.00	20.9
37	26	-0	-8375	0	0	0	-10350	--	--	16.08	16.08	0.18	0.17	0.07	0.53	0.00	0.00	20.9
38	26	-0	-2446	0	0	0	-6253	--	--	16.08	16.08	0.18	0.10	0.02	0.15	0.00	0.00	20.9
39	26	-0	-5057	0	0	0	-7806	--	--	16.08	16.08	0.18	0.13	0.04	0.32	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	-4379	0	0	0	-6864	--	--	16.08	16.08	0.18	0.11	0.04	0.27	0.00	0.00	20.9
2	51	-0	-3829	0	0	0	-5620	--	--	16.08	16.08	0.29	0.10	0.03	0.24	0.00	0.00	20.9

3	51	-0	-3859	0	0	0	-5624	--	--	16.08	16.08	0.29	0.10	0.03	0.24	0.00	0.00	20.9
4	51	-0	-2878	0	0	0	-4936	--	--	16.08	16.08	0.29	0.09	0.02	0.18	0.00	0.00	20.9
5	51	-0	-2908	0	0	0	-4940	--	--	16.08	16.08	0.29	0.09	0.02	0.18	0.00	0.00	20.9
6	51	-0	-3460	0	0	0	-5377	--	--	16.08	16.08	0.29	0.09	0.03	0.22	0.00	0.00	20.9
7	51	-0	-3562	0	0	0	-5389	--	--	16.08	16.08	0.29	0.09	0.03	0.22	0.00	0.00	20.9
8	51	-0	-3175	0	0	0	-5171	--	--	16.08	16.08	0.29	0.09	0.03	0.20	0.00	0.00	20.9
9	51	-0	-3276	0	0	0	-5183	--	--	16.08	16.08	0.29	0.09	0.03	0.21	0.00	0.00	20.9
10	51	-0	-3829	0	0	0	-5620	--	--	16.08	16.08	0.29	0.10	0.03	0.24	0.00	0.00	20.9
11	51	-0	-3859	0	0	0	-5624	--	--	16.08	16.08	0.29	0.10	0.03	0.24	0.00	0.00	20.9
12	51	-0	-2878	0	0	0	-4936	--	--	16.08	16.08	0.29	0.09	0.02	0.18	0.00	0.00	20.9
13	51	-0	-2908	0	0	0	-4940	--	--	16.08	16.08	0.29	0.09	0.02	0.18	0.00	0.00	20.9
14	51	-0	-3460	0	0	0	-5377	--	--	16.08	16.08	0.29	0.09	0.03	0.22	0.00	0.00	20.9
15	51	-0	-3562	0	0	0	-5389	--	--	16.08	16.08	0.29	0.09	0.03	0.22	0.00	0.00	20.9
16	51	-0	-3175	0	0	0	-5171	--	--	16.08	16.08	0.29	0.09	0.03	0.20	0.00	0.00	20.9
17	51	-0	-3276	0	0	0	-5183	--	--	16.08	16.08	0.29	0.09	0.03	0.21	0.00	0.00	20.9
18	51	-0	-7718	0	0	0	-10250	--	--	16.08	16.08	0.18	0.17	0.06	0.48	0.00	0.00	20.9
19	51	-0	-4160	0	0	0	-7791	--	--	16.08	16.08	0.18	0.13	0.03	0.26	0.00	0.00	20.9
20	51	-0	-5727	0	0	0	-8723	--	--	16.08	16.08	0.18	0.14	0.05	0.36	0.00	0.00	20.9
37	51	-0	-8375	0	0	0	-10350	--	--	16.08	16.08	0.18	0.17	0.07	0.53	0.00	0.00	20.9
38	51	-0	-2446	0	0	0	-6253	--	--	16.08	16.08	0.18	0.10	0.02	0.15	0.00	0.00	20.9
39	51	-0	-5057	0	0	0	-7806	--	--	16.08	16.08	0.18	0.13	0.04	0.32	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 121 NI 1296 NF 1336 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice resistenza			aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-3407	0	0	0	-8614	--	--	16.08	16.08	0.18	0.14	0.03	0.21	0.00	0.00	20.9
2	0	-0	-3105	0	0	0	-7216	--	--	16.08	16.08	0.29	0.12	0.03	0.19	0.00	0.00	20.9
3	0	-0	-3128	0	0	0	-7231	--	--	16.08	16.08	0.29	0.13	0.03	0.20	0.00	0.00	20.9
4	0	-0	-2113	0	0	0	-6022	--	--	16.08	16.08	0.29	0.10	0.02	0.13	0.00	0.00	20.9
5	0	-0	-2136	0	0	0	-6037	--	--	16.08	16.08	0.29	0.10	0.02	0.13	0.00	0.00	20.9
6	0	-0	-2731	0	0	0	-6780	--	--	16.08	16.08	0.29	0.12	0.02	0.17	0.00	0.00	20.9
7	0	-0	-2808	0	0	0	-6831	--	--	16.08	16.08	0.29	0.12	0.02	0.18	0.00	0.00	20.9
8	0	-0	-2434	0	0	0	-6422	--	--	16.08	16.08	0.29	0.11	0.02	0.15	0.00	0.00	20.9
9	0	-0	-2510	0	0	0	-6473	--	--	16.08	16.08	0.29	0.11	0.02	0.16	0.00	0.00	20.9
10	0	-0	-3105	0	0	0	-7216	--	--	16.08	16.08	0.29	0.12	0.03	0.19	0.00	0.00	20.9
11	0	-0	-3128	0	0	0	-7231	--	--	16.08	16.08	0.29	0.13	0.03	0.20	0.00	0.00	20.9
12	0	-0	-2113	0	0	0	-6022	--	--	16.08	16.08	0.29	0.10	0.02	0.13	0.00	0.00	20.9
13	0	-0	-2136	0	0	0	-6037	--	--	16.08	16.08	0.29	0.10	0.02	0.13	0.00	0.00	20.9
14	0	-0	-2731	0	0	0	-6780	--	--	16.08	16.08	0.29	0.12	0.02	0.17	0.00	0.00	20.9
15	0	-0	-2808	0	0	0	-6831	--	--	16.08	16.08	0.29	0.12	0.02	0.18	0.00	0.00	20.9
16	0	-0	-2434	0	0	0	-6422	--	--	16.08	16.08	0.29	0.11	0.02	0.15	0.00	0.00	20.9
17	0	-0	-2510	0	0	0	-6473	--	--	16.08	16.08	0.29	0.11	0.02	0.16	0.00	0.00	20.9
18	0	-0	-6888	0	0	0	-13790	--	--	16.08	16.08	0.18	0.23	0.06	0.43	0.00	0.00	20.9
19	0	-0	-3096	0	0	0	-9381	--	--	16.08	16.08	0.18	0.16	0.03	0.19	0.00	0.00	20.9
20	0	-0	-4775	0	0	0	-11180	--	--	16.08	16.08	0.18	0.19	0.04	0.30	0.00	0.00	20.9
37	0	-0	-7621	0	0	0	-14270	--	--	16.08	16.08	0.18	0.24	0.06	0.48	0.00	0.00	20.9
38	0	-0	-1300	0	0	0	-6921	--	--	16.08	16.08	0.18	0.11	0.01	0.08	0.00	0.00	20.9
39	0	-0	-4099	0	0	0	-9911	--	--	16.08	16.08	0.18	0.16	0.03	0.26	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	-3407	0	0	0	-8614	--	--	16.08	16.08	0.18	0.14	0.03	0.21	0.00	0.00	20.9
2	26	-0	-3105	0	0	0	-7216	--	--	16.08	16.08	0.29	0.12	0.03	0.19	0.00	0.00	20.9
3	26	-0	-3128	0	0	0	-7231	--	--	16.08	16.08	0.29	0.13	0.03	0.20	0.00	0.00	20.9
4	26	-0	-2113	0	0	0	-6022	--	--	16.08	16.08	0.29	0.10	0.02	0.13	0.00	0.00	20.9
5	26	-0	-2136	0	0	0	-6037	--	--	16.08	16.08	0.29	0.10	0.02	0.13	0.00	0.00	20.9
6	26	-0	-2731	0	0	0	-6780	--	--	16.08	16.08	0.29	0.12	0.02	0.17	0.00	0.00	20.9
7	26	-0	-2808	0	0	0	-6831	--	--	16.08	16.08	0.29	0.12	0.02	0.18	0.00	0.00	20.9
8	26	-0	-2434	0	0	0	-6422	--	--	16.08	16.08	0.29	0.11	0.02	0.15	0.00	0.00	20.9
9	26	-0	-2510	0	0	0	-6473	--	--	16.08	16.08	0.29	0.11	0.02	0.16	0.00	0.00	20.9
10	26	-0	-3105	0	0	0	-7216	--	--	16.08	16.08	0.29	0.12	0.03	0.19	0.00	0.00	20.9
11	26	-0	-3128	0	0	0	-7231	--	--	16.08	16.08	0.29	0.13	0.03	0.20	0.00	0.00	20.9
12	26	-0	-2113	0	0	0	-6022	--	--	16.08	16.08	0.29	0.10	0.02	0.13	0.00	0.00	20.9
13	26	-0	-2136	0	0	0	-6037	--	--	16.08	16.08	0.29	0.10	0.02	0.13	0.00	0.00	20.9
14	26	-0	-2731	0	0	0	-6780	--	--	16.08	16.08	0.29	0.12	0.02	0.17	0.00	0.00	20.9
15	26	-0	-2808	0	0	0	-6831	--	--	16.08	16.08	0.29	0.12	0.02	0.18	0.00	0.00	20.9
16	26	-0	-2434	0	0	0	-6422	--	--	16.08	16.08	0.29	0.11	0.02	0.15	0.00	0.00	20.9
17	26	-0	-2510	0	0	0	-6473	--	--	16.08	16.08	0.29	0.11	0.02	0.16	0.00	0.00	20.9
18	26	-0	-6888	0	0	0	-13790	--	--	16.08	16.08	0.18	0.23	0.06	0.43	0.00	0.00	20.9
19	26	-0	-3096	0	0	0	-9381	--	--	16.08	16.08	0.18	0.16	0.03	0.19	0.00	0.00	20.9
20	26	-0	-4775	0	0	0	-11180	--	--	16.08	16.08	0.18	0.19	0.04	0.30	0.00	0.00	20.9
37	26	-0	-7621	0	0	0	-14270	--	--	16.08	16.08	0.18	0.24	0.06	0.48	0.00	0.00	20.9
38	26	-0	-1300	0	0	0	-6921	--	--	16.08	16.08	0.18	0.11	0.01	0.08	0.00	0.00	20.9
39	26	-0	-4099	0	0	0	-9911	--	--	16.08	16.08	0.18	0.16	0.03	0.26	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	-3407	0	0	0	-8614	--	--	16.08	16.08	0.18	0.14	0.03	0.21	0.00	0.00	20.9
2	51	-0	-3105	0	0	0	-7216	--	--	16.08	16.08	0.29	0.12	0.03	0.19	0.00	0.00	20.9
3	51	-0	-3128	0	0	0	-7231	--	--	16.08	16.08	0.29	0.13	0.03	0.20	0.00	0.00	20.9
4	51	-0	-2113	0	0	0	-6022	--	--	16.08	16.08	0.29	0.10	0.02	0.13	0.00	0.00	20.9
5	51	-0	-2136	0	0	0	-6037	--	--	16.08	16.08	0.29	0.10	0.02	0.13	0.00	0.00	20.9
6	51	-0	-2731	0	0	0	-6780	--	--	16.08	16.08	0.29	0.12	0.02	0.17	0.00	0.00	20.9
7	51	-0	-2808	0	0	0	-6831	--	--	16.08	16.08	0.29	0.12	0.02	0.18	0.00	0.00	20.9
8	51	-0	-2434	0	0	0	-6422	--	--	16.08	16.08	0.29	0.11	0.02	0.15	0.00	0.00	20.9
9	51	-0	-2510	0	0	0	-6473	--	--	16.08	16.08	0.29	0.11	0.02	0.16	0.00	0.00	20.9
10	51	-0	-3105	0	0	0	-7216	--	--	16.08	16.08	0.29	0.12	0.03	0.19	0.00	0.00	20.9
11	51	-0	-3128	0	0	0	-7231	--	--	16.08	16.08	0.29	0.13	0.03	0.20	0.00	0.00	20.9
12	51	-0	-2113	0	0	0	-6022	--	--	16.08	16.08	0.29	0.10	0.02	0.13	0.00	0.00	20.9
13	51	-0	-2136	0	0	0	-6037	--	--	16.08	16.08	0.29	0.10	0.02	0.13	0.00	0.00	20.9
14	51	-0	-2731	0	0	0	-6780	--	--	16.08	16.08	0.29	0.12	0.02	0.17	0.00	0.00	20.9
15	51	-0	-2808	0	0	0	-6831	--	--	16.08	16.08	0.29	0.12	0.02	0.18	0.00	0.00	20.9
16	51	-0	-2434	0	0	0	-6422	--	--	16.08	16.08	0.29	0.11	0.02	0.15	0.00	0.00	20.9
17	51	-0	-2510	0	0	0	-6473	--	--	16.08	16.08	0.29	0.11	0.02	0.16	0.00	0.00	20.9
18	51	-0	-6888	0	0	0	-13790	--	--	16.08	16.08	0.18	0.23	0.06	0.43	0.00	0.00	20.9
19	51	-0	-3096	0	0	0	-9381	--	--	16.08	16.08	0.18	0.16	0.03	0.19	0.00	0.00	20.9
20	51	-0	-4775	0	0	0	-11180	--	--	16.08	16.08	0.18	0.19	0.04	0.30	0.00	0.00	20.9
37	51	-0	-7621	0	0	0	-14270	--	--	16.08	16.08	0.18	0.24	0.06	0.48	0.00	0.00	20.9
38	51	-0	-1300	0	0	0	-6921	--	--	16.08	16.08	0.18	0.11	0.01	0.08	0.00	0.00	20.9
39	51	-0	-4099	0	0	0	-9911	--	--	16.08	16.08	0.18	0.16	0.03	0.26	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 122 NI 1336 NF 1335 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-2391	0	0	0	-9842	--	--	16.08	16.08	0.18	0.16	0.02	0.15	0.00	0.00	20.9
2	0	-0	-2345	0	0	0	-8420	--	--	16.08	16.08	0.29	0.15	0.02	0.15	0.00	0.00	20.9
3	0	-0	-2362	0	0	0	-8444	--	--	16.08	16.08	0.29	0.15	0.02	0.15	0.00	0.00	20.9
4	0	-0	-1317	0	0	0	-6698	--	--	16.08	16.08	0.29	0.12	0.01	0.08	0.00	0.00	20.9
5	0	-0	-1333	0	0	0	-6722	--	--	16.08	16.08	0.29	0.12	0.01	0.08	0.00	0.00	20.9
6	0	-0	-1966	0	0	0	-7790	--	--	16.08	16.08	0.29	0.13	0.02	0.12	0.00	0.00	20.9
7	0	-0	-2021	0	0	0	-7869	--	--	16.08	16.08	0.29	0.14	0.02	0.13	0.00	0.00	20.9
8	0	-0	-1657	0	0	0	-7273	--	--	16.08	16.08	0.29	0.13	0.01	0.10	0.00	0.00	20.9
9	0	-0	-1712	0	0	0	-7352	--	--	16.08	16.08	0.29	0.13	0.01	0.11	0.00	0.00	20.9
10	0	-0	-2345	0	0	0	-8420	--	--	16.08	16.08	0.29	0.15	0.02	0.15	0.00	0.00	20.9
11	0	-0	-2362	0	0	0	-8444	--	--	16.08	16.08	0.29	0.15	0.02	0.15	0.00	0.00	20.9
12	0	-0	-1317	0	0	0	-6698	--	--	16.08	16.08	0.29	0.12	0.01	0.08	0.00	0.00	20.9
13	0	-0	-1333	0	0	0	-6722	--	--	16.08	16.08	0.29	0.12	0.01	0.08	0.00	0.00	20.9
14	0	-0	-1966	0	0	0	-7790	--	--	16.08	16.08	0.29	0.13	0.02	0.12	0.00	0.00	20.9
15	0	-0	-2021	0	0	0	-7869	--	--	16.08	16.08	0.29	0.14	0.02	0.13	0.00	0.00	20.9
16	0	-0	-1657	0	0	0	-7273	--	--	16.08	16.08	0.29	0.13	0.01	0.10	0.00	0.00	20.9
17	0	-0	-1712	0	0	0	-7352	--	--	16.08	16.08	0.29	0.13	0.01	0.11	0.00	0.00	20.9
18	0	-0	-6004	0	0	0	-16870	--	--	16.08	16.08	0.18	0.28	0.05	0.38	0.00	0.00	20.9
19	0	-0	-1972	0	0	0	-10390	--	--	16.08	16.08	0.18	0.17	0.02	0.12	0.00	0.00	20.9
20	0	-0	-3766	0	0	0	-13110	--	--	16.08	16.08	0.18	0.22	0.03	0.24	0.00	0.00	20.9
37	0	-0	-6819	0	0	0	-17770	--	--	16.08	16.08	0.18	0.29	0.06	0.43	0.00	0.00	20.9
38	0	-0	-98	0	0	0	-6972	--	--	16.08	16.08	0.18	0.12	0.00	0.01	0.00	0.00	20.9
39	0	-0	-3089	0	0	0	-11500	--	--	16.08	16.08	0.18	0.19	0.03	0.19	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	26	-0	-2391	0	0	0	-9842	--	--	16.08	16.08	0.18	0.16	0.02	0.15	0.00	0.00	20.9
2	26	-0	-2345	0	0	0	-8420	--	--	16.08	16.08	0.29	0.15	0.02	0.15	0.00	0.00	20.9
3	26	-0	-2362	0	0	0	-8444	--	--	16.08	16.08	0.29	0.15	0.02	0.15	0.00	0.00	20.9
4	26	-0	-1317	0	0	0	-6698	--	--	16.08	16.08	0.29	0.12	0.01	0.08	0.00	0.00	20.9
5	26	-0	-1333	0	0	0	-6722	--	--	16.08	16.08	0.29	0.12	0.01	0.08	0.00	0.00	20.9
6	26	-0	-1966	0	0	0	-7790	--	--	16.08	16.08	0.29	0.13	0.02	0.12	0.00	0.00	20.9
7	26	-0	-2021	0	0	0	-7869	--	--	16.08	16.08	0.29	0.14	0.02	0.13	0.00	0.00	20.9
8	26	-0	-1657	0	0	0	-7273	--	--	16.08	16.08	0.29	0.13	0.01	0.10	0.00	0.00	20.9
9	26	-0	-1712	0	0	0	-7352	--	--	16.08	16.08	0.29	0.13	0.01	0.11	0.00	0.00	20.9
10	26	-0	-2345	0	0	0	-8420	--	--	16.08	16.08	0.29	0.15	0.02	0.15	0.00	0.00	20.9
11	26	-0	-2362	0	0	0	-8444	--	--	16.08	16.08	0.29	0.15	0.02	0.15	0.00	0.00	20.9
12	26	-0	-1317	0	0	0	-6698	--	--	16.08	16.08	0.29	0.12	0.01	0.08	0.00	0.00	20.9
13	26	-0	-1333	0	0	0	-6722	--	--	16.08	16.08	0.29	0.12	0.01	0.08	0.00	0.00	20.9
14	26	-0	-1966	0	0	0	-7790	--	--	16.08	16.08	0.29	0.13	0.02	0.12	0.00	0.00	20.9
15	26	-0	-2021	0	0	0	-7869	--	--	16.08	16.08	0.29	0.14	0.02	0.13	0.00	0.00	20.9
16	26	-0	-1657	0	0	0	-7273	--	--	16.08	16.08	0.29	0.13	0.01	0.10	0.00	0.00	20.9
17	26	-0	-1712	0	0	0	-7352	--	--	16.08	16.08	0.29	0.13	0.01	0.11	0.00	0.00	20.9
18	26	-0	-6004	0	0	0	-16870	--	--	16.08	16.08	0.18	0.28	0.05	0.38	0.00	0.00	20.9
19	26	-0	-1972	0	0	0	-10390	--	--	16.08	16.08	0.18	0.17	0.02	0.12	0.00	0.00	20.9
20	26	-0	-3766	0	0	0	-13110	--	--	16.08	16.08	0.18	0.22	0.03	0.24	0.00	0.00	20.9
37	26	-0	-6819	0	0	0	-17770	--	--	16.08	16.08	0.18	0.29	0.06	0.43	0.00	0.00	20.9
38	26	-0	-98	0	0	0	-6972	--	--	16.08	16.08	0.18	0.12	0.00	0.01	0.00	0.00	20.9
39	26	-0	-3089	0	0	0	-11500	--	--	16.08	16.08	0.18	0.19	0.03	0.19	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	51	-0	-2391	0	0	0	-9842	--	--	16.08	16.08	0.18	0.16	0.02	0.15	0.00	0.00	20.9
2	51	-0	-2345	0	0	0	-8420	--	--	16.08	16.08	0.29	0.15	0.02	0.15	0.00	0.00	20.9
3	51	-0	-2362	0	0	0	-8444	--	--	16.08	16.08	0.29	0.15	0.02	0.15	0.00	0.00	20.9
4	51	-0	-1317	0	0	0	-6698	--	--	16.08	16.08	0.29	0.12	0.01	0.08	0.00	0.00	20.9
5	51	-0	-1333	0	0	0	-6722	--	--	16.08	16.08	0.29	0.12	0.01	0.08	0.00	0.00	20.9
6	51	-0	-1966	0	0	0	-7790	--	--	16.08	16.08	0.29	0.13	0.02	0.12	0.00	0.00	20.9
7	51	-0	-2021	0	0	0	-7869	--	--	16.08	16.08	0.29	0.14	0.02	0.13	0.00	0.00	20.9
8	51	-0	-1657	0	0	0	-7273	--	--	16.08	16.08	0.29	0.13	0.01	0.10	0.00	0.00	20.9
9	51	-0	-1712	0	0	0	-7352	--	--	16.08	16.08	0.29	0.13	0.01	0.11	0.00	0.00	20.9
10	51	-0	-2345	0	0	0	-8420	--	--	16.08	16.08	0.29	0.15	0.02	0.15	0.00	0.00	20.9
11	51	-0	-2362	0	0	0	-8444	--	--	16.08	16.08	0.29	0.15	0.02	0.15	0.00	0.00	20.9
12	51	-0	-1317	0	0	0	-6698	--	--	16.08	16.08	0.29	0.12	0.01	0.08	0.00	0.00	20.9
13	51	-0	-1333	0	0	0	-6722	--	--	16.08	16.08	0.29	0.12	0.01	0.08	0.00	0.00	20.9
14	51	-0	-1966	0	0	0	-7790	--	--	16.08	16.08	0.29	0.13	0.02	0.12	0.00	0.00	20.9
15	51	-0	-2021	0	0	0	-7869	--	--	16.08	16.08	0.29	0.14	0.02	0.13	0.00	0.00	20.9
16	51	-0	-1657	0	0	0	-7273	--	--	16.08	16.08	0.29	0.13	0.01	0.10	0.00	0.00	20.9
17	51	-0	-1712	0	0	0	-7352	--	--	16.08	16.08	0.29	0.13	0.01	0.11	0.00	0.00	20.9
18	51	-0	-6004	0	0	0	-16870	--	--	16.08	16.08	0.18	0.28	0.05	0.38	0.00	0.00	20.9
19	51	-0	-1972	0	0	0	-10390	--	--	16.08	16.08	0.18	0.17	0.02	0.12	0.00	0.00	20.9
20	51	-0	-3766	0	0	0	-13110	--	--	16.08	16.08	0.18	0.22	0.03	0.24	0.00	0.00	20.9
37	51	-0	-6819	0	0	0	-17770	--	--	16.08	16.08	0.18	0.29	0.06	0.43	0.00	0.00	20.9
38	51	-0	-98	0	0	0	-6972	--	--	16.08	16.08	0.18	0.12	0.00	0.01	0.00	0.00	20.9
39	51	-0	-3089	0	0	0	-11500	--	--	16.08	16.08	0.18	0.19	0.03	0.19	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 123 NI 1335 NF 1288 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-1289	0	0	0	-10500	--	--	16.08	16.08	0.18	0.17	0.01	0.08	0.00	0.00	20.9
2	0	-0	-1515	0	0	0	-9198	--	--	16.08	16.08	0.29	0.16	0.01	0.10	0.00	0.00	20.9
3	0	-0	-1526	0	0	0	-9228	--	--	16.08	16.08	0.29	0.16	0.01	0.10	0.00	0.00	20.9
4	0	-0	-458	0	0	0	-6933	--	--	16.08	16.08	0.29	0.12	0.00	0.03	0.00	0.00	20.9
5	0	-0	-469	0	0	0	-6962	--	--	16.08	16.08	0.29	0.12	0.00	0.03	0.00	0.00	20.9
6	0	-0	-1132	0	0	0	-8371	--	--	16.08	16.08	0.29	0.14	0.01	0.07	0.00	0.00	20.9
7	0	-0	-1168	0	0	0	-8469	--	--	16.08	16.08	0.29	0.15	0.01	0.07	0.00	0.00	20.9
8	0	-0	-815	0	0	0	-7692	--	--	16.08	16.08	0.29	0.13	0.01	0.05	0.00	0.00	20.9
9	0	-0	-851	0	0	0	-7789	--	--	16.08	16.08	0.29	0.13	0.01	0.05	0.00	0.00	20.9
10	0	-0	-1515	0	0	0	-9198	--	--	16.08	16.08	0.29	0.16	0.01	0.10	0.00	0.00	20.9

11	0	-0	-1526	0	0	0	-9228	--	--	16.08	16.08	0.29	0.16	0.01	0.10	0.00	0.00	20.9
12	0	-0	-458	0	0	0	-6933	--	--	16.08	16.08	0.29	0.12	0.00	0.03	0.00	0.00	20.9
13	0	-0	-469	0	0	0	-6962	--	--	16.08	16.08	0.29	0.12	0.00	0.03	0.00	0.00	20.9
14	0	-0	-1132	0	0	0	-8371	--	--	16.08	16.08	0.29	0.14	0.01	0.07	0.00	0.00	20.9
15	0	-0	-1168	0	0	0	-8469	--	--	16.08	16.08	0.29	0.15	0.01	0.07	0.00	0.00	20.9
16	0	-0	-815	0	0	0	-7692	--	--	16.08	16.08	0.29	0.13	0.01	0.05	0.00	0.00	20.9
17	0	-0	-851	0	0	0	-7789	--	--	16.08	16.08	0.29	0.13	0.01	0.05	0.00	0.00	20.9
18	0	-0	-5001	0	0	0	-19440	--	--	16.08	16.08	0.18	0.32	0.04	0.31	0.00	0.00	20.9
19	0	-0	-744	0	0	0	-10780	--	--	16.08	16.08	0.18	0.18	0.01	0.05	0.00	0.00	20.9
20	0	-0	-2649	0	0	0	-14470	--	--	16.08	16.08	0.18	0.24	0.02	0.17	0.00	0.00	20.9
37	0	-0	-5900	0	0	0	-20800	--	--	16.08	16.08	0.18	0.34	0.05	0.37	0.00	0.00	20.9
38	0	-0	1194	0	0	0	-6972	--	--	16.08	16.08	0.18	0.12	0.01	0.07	0.00	0.00	20.9
39	0	-0	-1980	0	0	0	-12510	--	--	16.08	16.08	0.18	0.21	0.02	0.12	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	-1289	0	0	0	-10500	--	--	16.08	16.08	0.18	0.17	0.01	0.08	0.00	0.00	20.9
2	26	-0	-1515	0	0	0	-9198	--	--	16.08	16.08	0.29	0.16	0.01	0.10	0.00	0.00	20.9
3	26	-0	-1526	0	0	0	-9228	--	--	16.08	16.08	0.29	0.16	0.01	0.10	0.00	0.00	20.9
4	26	-0	-458	0	0	0	-6933	--	--	16.08	16.08	0.29	0.12	0.00	0.03	0.00	0.00	20.9
5	26	-0	-469	0	0	0	-6962	--	--	16.08	16.08	0.29	0.12	0.00	0.03	0.00	0.00	20.9
6	26	-0	-1132	0	0	0	-8371	--	--	16.08	16.08	0.29	0.14	0.01	0.07	0.00	0.00	20.9
7	26	-0	-1168	0	0	0	-8469	--	--	16.08	16.08	0.29	0.15	0.01	0.07	0.00	0.00	20.9
8	26	-0	-815	0	0	0	-7692	--	--	16.08	16.08	0.29	0.13	0.01	0.05	0.00	0.00	20.9
9	26	-0	-851	0	0	0	-7789	--	--	16.08	16.08	0.29	0.13	0.01	0.05	0.00	0.00	20.9
10	26	-0	-1515	0	0	0	-9198	--	--	16.08	16.08	0.29	0.16	0.01	0.10	0.00	0.00	20.9
11	26	-0	-1526	0	0	0	-9228	--	--	16.08	16.08	0.29	0.16	0.01	0.10	0.00	0.00	20.9
12	26	-0	-458	0	0	0	-6933	--	--	16.08	16.08	0.29	0.12	0.00	0.03	0.00	0.00	20.9
13	26	-0	-469	0	0	0	-6962	--	--	16.08	16.08	0.29	0.12	0.00	0.03	0.00	0.00	20.9
14	26	-0	-1132	0	0	0	-8371	--	--	16.08	16.08	0.29	0.14	0.01	0.07	0.00	0.00	20.9
15	26	-0	-1168	0	0	0	-8469	--	--	16.08	16.08	0.29	0.15	0.01	0.07	0.00	0.00	20.9
16	26	-0	-815	0	0	0	-7692	--	--	16.08	16.08	0.29	0.13	0.01	0.05	0.00	0.00	20.9
17	26	-0	-851	0	0	0	-7789	--	--	16.08	16.08	0.29	0.13	0.01	0.05	0.00	0.00	20.9
18	26	-0	-5001	0	0	0	-19440	--	--	16.08	16.08	0.18	0.32	0.04	0.31	0.00	0.00	20.9
19	26	-0	-744	0	0	0	-10780	--	--	16.08	16.08	0.18	0.18	0.01	0.05	0.00	0.00	20.9
20	26	-0	-2649	0	0	0	-14470	--	--	16.08	16.08	0.18	0.24	0.02	0.17	0.00	0.00	20.9
37	26	-0	-5900	0	0	0	-20800	--	--	16.08	16.08	0.18	0.34	0.05	0.37	0.00	0.00	20.9
38	26	-0	1194	0	0	0	-6972	--	--	16.08	16.08	0.18	0.12	0.01	0.07	0.00	0.00	20.9
39	26	-0	-1980	0	0	0	-12510	--	--	16.08	16.08	0.18	0.21	0.02	0.12	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	-1289	0	0	0	-10500	--	--	16.08	16.08	0.18	0.17	0.01	0.08	0.00	0.00	20.9
2	51	-0	-1515	0	0	0	-9198	--	--	16.08	16.08	0.29	0.16	0.01	0.10	0.00	0.00	20.9
3	51	-0	-1526	0	0	0	-9228	--	--	16.08	16.08	0.29	0.16	0.01	0.10	0.00	0.00	20.9
4	51	-0	-458	0	0	0	-6933	--	--	16.08	16.08	0.29	0.12	0.00	0.03	0.00	0.00	20.9
5	51	-0	-469	0	0	0	-6962	--	--	16.08	16.08	0.29	0.12	0.00	0.03	0.00	0.00	20.9
6	51	-0	-1132	0	0	0	-8371	--	--	16.08	16.08	0.29	0.14	0.01	0.07	0.00	0.00	20.9
7	51	-0	-1168	0	0	0	-8469	--	--	16.08	16.08	0.29	0.15	0.01	0.07	0.00	0.00	20.9
8	51	-0	-815	0	0	0	-7692	--	--	16.08	16.08	0.29	0.13	0.01	0.05	0.00	0.00	20.9
9	51	-0	-851	0	0	0	-7789	--	--	16.08	16.08	0.29	0.13	0.01	0.05	0.00	0.00	20.9
10	51	-0	-1515	0	0	0	-9198	--	--	16.08	16.08	0.29	0.16	0.01	0.10	0.00	0.00	20.9
11	51	-0	-1526	0	0	0	-9228	--	--	16.08	16.08	0.29	0.16	0.01	0.10	0.00	0.00	20.9
12	51	-0	-458	0	0	0	-6933	--	--	16.08	16.08	0.29	0.12	0.00	0.03	0.00	0.00	20.9
13	51	-0	-469	0	0	0	-6962	--	--	16.08	16.08	0.29	0.12	0.00	0.03	0.00	0.00	20.9
14	51	-0	-1132	0	0	0	-8371	--	--	16.08	16.08	0.29	0.14	0.01	0.07	0.00	0.00	20.9
15	51	-0	-1168	0	0	0	-8469	--	--	16.08	16.08	0.29	0.15	0.01	0.07	0.00	0.00	20.9
16	51	-0	-815	0	0	0	-7692	--	--	16.08	16.08	0.29	0.13	0.01	0.05	0.00	0.00	20.9
17	51	-0	-851	0	0	0	-7789	--	--	16.08	16.08	0.29	0.13	0.01	0.05	0.00	0.00	20.9
18	51	-0	-5001	0	0	0	-19440	--	--	16.08	16.08	0.18	0.32	0.04	0.31	0.00	0.00	20.9
19	51	-0	-744	0	0	0	-10780	--	--	16.08	16.08	0.18	0.18	0.01	0.05	0.00	0.00	20.9
20	51	-0	-2649	0	0	0	-14470	--	--	16.08	16.08	0.18	0.24	0.02	0.17	0.00	0.00	20.9
37	51	-0	-5900	0	0	0	-20800	--	--	16.08	16.08	0.18	0.34	0.05	0.37	0.00	0.00	20.9
38	51	-0	1194	0	0	0	-6972	--	--	16.08	16.08	0.18	0.12	0.01	0.07	0.00	0.00	20.9
39	51	-0	-1980	0	0	0	-12510	--	--	16.08	16.08	0.18	0.21	0.02	0.12	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 124 NI 1288 NF 1326 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-54	0	0	0	-10530	--	--	16.08	16.08	0.18	0.17	0.00	0.00	0.00	0.00	20.9
2	0	-0	-573	0	0	0	-9493	--	--	16.08	16.08	0.29	0.16	0.00	0.04	0.00	0.00	20.9
3	0	-0	-579	0	0	0	-9525	--	--	16.08	16.08	0.29	0.16	0.00	0.04	0.00	0.00	20.9
4	0	-0	496	0	0	0	-6933	--	--	16.08	16.08	0.29	0.12	0.00	0.03	0.00	0.00	20.9
5	0	-0	490	0	0	0	-6962	--	--	16.08	16.08	0.29	0.12	0.00	0.03	0.00	0.00	20.9
6	0	-0	-192	0	0	0	-8470	--	--	16.08	16.08	0.29	0.15	0.00	0.01	0.00	0.00	20.9
7	0	-0	-212	0	0	0	-8578	--	--	16.08	16.08	0.29	0.15	0.00	0.01	0.00	0.00	20.9
8	0	-0	129	0	0	0	-7692	--	--	16.08	16.08	0.29	0.13	0.00	0.01	0.00	0.00	20.9
9	0	-0	109	0	0	0	-7789	--	--	16.08	16.08	0.29	0.13	0.00	0.01	0.00	0.00	20.9
10	0	-0	-573	0	0	0	-9493	--	--	16.08	16.08	0.29	0.16	0.00	0.04	0.00	0.00	20.9
11	0	-0	-579	0	0	0	-9525	--	--	16.08	16.08	0.29	0.16	0.00	0.04	0.00	0.00	20.9
12	0	-0	496	0	0	0	-6933	--	--	16.08	16.08	0.29	0.12	0.00	0.03	0.00	0.00	20.9
13	0	-0	490	0	0	0	-6962	--	--	16.08	16.08	0.29	0.12	0.00	0.03	0.00	0.00	20.9
14	0	-0	-192	0	0	0	-8470	--	--	16.08	16.08	0.29	0.15	0.00	0.01	0.00	0.00	20.9
15	0	-0	-212	0	0	0	-8578	--	--	16.08	16.08	0.29	0.15	0.00	0.01	0.00	0.00	20.9
16	0	-0	129	0	0	0	-7692	--	--	16.08	16.08	0.29	0.13	0.00	0.01	0.00	0.00	20.9
17	0	-0	109	0	0	0	-7789	--	--	16.08	16.08	0.29	0.13	0.00	0.01	0.00	0.00	20.9
18	0	-0	-3798	0	0	0	-21390	--	--	16.08	16.08	0.18	0.35	0.03	0.24	0.00	0.00	20.9
19	0	-0	639	0	0	0	-10780	--	--	16.08	16.08	0.18	0.18	0.01	0.04	0.00	0.00	20.9
20	0	-0	-1359	0	0	0	-15170	--	--	16.08	16.08	0.18	0.25	0.01	0.09	0.00	0.00	20.9
37	0	-0	-4780	0	0	0	-23260	--	--	16.08	16.08	0.18	0.39	0.04	0.30	0.00	0.00	20.9
38	0	-0	2614	0	0	0	-6358	--	--	16.08	16.08	0.18	0.11	0.02	0.16	0.00	0.00	20.9
39	0	-0	-716	0	0	0	-12880	--	--	16.08	16.08	0.18	0.21	0.01	0.04	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	-54	0	0	0	-10530	--	--	16.08	16.08	0.18	0.17	0.00	0.00	0.00	0.00	20.9
2	26	-0	-573	0	0	0	-9493	--	--	16.08	16.08	0.29	0.16	0.00	0.04	0.00	0.00	20.9
3	26	-0	-579	0	0	0	-9525	--	--	16.08	16.08	0.29	0.16	0.00	0.04	0.00	0.00	20.9
4	26	-0	496	0	0	0	-6933	--	--	16.08	16.08	0.29	0.12	0.00	0.03	0.00	0.00	20.9
5	26	-0	490	0	0	0	-6962	--	--	16.08	16.08	0.29	0.12	0.00	0.03	0.00	0.00	20.9
6	26	-0	-192	0	0	0	-8470	--	--	16.08	16.08	0.29	0.15	0.00	0.01	0.00	0.00	20.9

7	26	-0	-212	0	0	0	-8578	--	--	16.08	16.08	0.29	0.15	0.00	0.01	0.00	0.00	20.9
8	26	-0	129	0	0	0	-7692	--	--	16.08	16.08	0.29	0.13	0.00	0.01	0.00	0.00	20.9
9	26	-0	109	0	0	0	-7789	--	--	16.08	16.08	0.29	0.13	0.00	0.01	0.00	0.00	20.9
10	26	-0	-573	0	0	0	-9493	--	--	16.08	16.08	0.29	0.16	0.00	0.04	0.00	0.00	20.9
11	26	-0	-579	0	0	0	-9525	--	--	16.08	16.08	0.29	0.16	0.00	0.04	0.00	0.00	20.9
12	26	-0	496	0	0	0	-6933	--	--	16.08	16.08	0.29	0.12	0.00	0.03	0.00	0.00	20.9
13	26	-0	490	0	0	0	-6962	--	--	16.08	16.08	0.29	0.12	0.00	0.03	0.00	0.00	20.9
14	26	-0	-192	0	0	0	-8470	--	--	16.08	16.08	0.29	0.15	0.00	0.01	0.00	0.00	20.9
15	26	-0	-212	0	0	0	-8578	--	--	16.08	16.08	0.29	0.15	0.00	0.01	0.00	0.00	20.9
16	26	-0	129	0	0	0	-7692	--	--	16.08	16.08	0.29	0.13	0.00	0.01	0.00	0.00	20.9
17	26	-0	109	0	0	0	-7789	--	--	16.08	16.08	0.29	0.13	0.00	0.01	0.00	0.00	20.9
18	26	-0	-3798	0	0	0	-21390	--	--	16.08	16.08	0.18	0.35	0.03	0.24	0.00	0.00	20.9
19	26	-0	639	0	0	0	-10780	--	--	16.08	16.08	0.18	0.18	0.01	0.04	0.00	0.00	20.9
20	26	-0	-1359	0	0	0	-15170	--	--	16.08	16.08	0.18	0.25	0.01	0.09	0.00	0.00	20.9
37	26	-0	-4780	0	0	0	-23260	--	--	16.08	16.08	0.18	0.39	0.04	0.30	0.00	0.00	20.9
38	26	-0	2614	0	0	0	-6358	--	--	16.08	16.08	0.18	0.11	0.02	0.16	0.00	0.00	20.9
39	26	-0	-716	0	0	0	-12880	--	--	16.08	16.08	0.18	0.21	0.01	0.04	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	-54	0	0	0	-10530	--	--	16.08	16.08	0.18	0.17	0.00	0.00	0.00	0.00	20.9
2	51	-0	-573	0	0	0	-9493	--	--	16.08	16.08	0.29	0.16	0.00	0.04	0.00	0.00	20.9
3	51	-0	-579	0	0	0	-9525	--	--	16.08	16.08	0.29	0.16	0.00	0.04	0.00	0.00	20.9
4	51	-0	496	0	0	0	-6933	--	--	16.08	16.08	0.29	0.12	0.00	0.03	0.00	0.00	20.9
5	51	-0	490	0	0	0	-6962	--	--	16.08	16.08	0.29	0.12	0.00	0.03	0.00	0.00	20.9
6	51	-0	-192	0	0	0	-8470	--	--	16.08	16.08	0.29	0.15	0.00	0.01	0.00	0.00	20.9
7	51	-0	-212	0	0	0	-8578	--	--	16.08	16.08	0.29	0.15	0.00	0.01	0.00	0.00	20.9
8	51	-0	129	0	0	0	-7692	--	--	16.08	16.08	0.29	0.13	0.00	0.01	0.00	0.00	20.9
9	51	-0	109	0	0	0	-7789	--	--	16.08	16.08	0.29	0.13	0.00	0.01	0.00	0.00	20.9
10	51	-0	-573	0	0	0	-9493	--	--	16.08	16.08	0.29	0.16	0.00	0.04	0.00	0.00	20.9
11	51	-0	-579	0	0	0	-9525	--	--	16.08	16.08	0.29	0.16	0.00	0.04	0.00	0.00	20.9
12	51	-0	496	0	0	0	-6933	--	--	16.08	16.08	0.29	0.12	0.00	0.03	0.00	0.00	20.9
13	51	-0	490	0	0	0	-6962	--	--	16.08	16.08	0.29	0.12	0.00	0.03	0.00	0.00	20.9
14	51	-0	-192	0	0	0	-8470	--	--	16.08	16.08	0.29	0.15	0.00	0.01	0.00	0.00	20.9
15	51	-0	-212	0	0	0	-8578	--	--	16.08	16.08	0.29	0.15	0.00	0.01	0.00	0.00	20.9
16	51	-0	129	0	0	0	-7692	--	--	16.08	16.08	0.29	0.13	0.00	0.01	0.00	0.00	20.9
17	51	-0	109	0	0	0	-7789	--	--	16.08	16.08	0.29	0.13	0.00	0.01	0.00	0.00	20.9
18	51	-0	-3798	0	0	0	-21390	--	--	16.08	16.08	0.18	0.35	0.03	0.24	0.00	0.00	20.9
19	51	-0	639	0	0	0	-10780	--	--	16.08	16.08	0.18	0.18	0.01	0.04	0.00	0.00	20.9
20	51	-0	-1359	0	0	0	-15170	--	--	16.08	16.08	0.18	0.25	0.01	0.09	0.00	0.00	20.9
37	51	-0	-4780	0	0	0	-23260	--	--	16.08	16.08	0.18	0.39	0.04	0.30	0.00	0.00	20.9
38	51	-0	2614	0	0	0	-6358	--	--	16.08	16.08	0.18	0.11	0.02	0.16	0.00	0.00	20.9
39	51	-0	-716	0	0	0	-12880	--	--	16.08	16.08	0.18	0.21	0.01	0.04	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 125 NI 1326 NF 1325 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	1366	0	0	0	-10530	--	--	16.08	16.08	0.18	0.17	0.01	0.09	0.00	0.00	20.9
2	0	-0	524	0	0	0	-9493	--	--	16.08	16.08	0.29	0.16	0.00	0.03	0.00	0.00	20.9
3	0	-0	523	0	0	0	-9525	--	--	16.08	16.08	0.29	0.16	0.00	0.03	0.00	0.00	20.9
4	0	-0	1579	0	0	0	-6678	--	--	16.08	16.08	0.29	0.12	0.01	0.10	0.00	0.00	20.9
5	0	-0	1577	0	0	0	-6711	--	--	16.08	16.08	0.29	0.12	0.01	0.10	0.00	0.00	20.9
6	0	-0	895	0	0	0	-8470	--	--	16.08	16.08	0.29	0.15	0.01	0.06	0.00	0.00	20.9
7	0	-0	890	0	0	0	-8578	--	--	16.08	16.08	0.29	0.15	0.01	0.06	0.00	0.00	20.9
8	0	-0	1212	0	0	0	-7626	--	--	16.08	16.08	0.29	0.13	0.01	0.08	0.00	0.00	20.9
9	0	-0	1206	0	0	0	-7733	--	--	16.08	16.08	0.29	0.13	0.01	0.08	0.00	0.00	20.9
10	0	-0	524	0	0	0	-9493	--	--	16.08	16.08	0.29	0.16	0.00	0.03	0.00	0.00	20.9
11	0	-0	523	0	0	0	-9525	--	--	16.08	16.08	0.29	0.16	0.00	0.03	0.00	0.00	20.9
12	0	-0	1579	0	0	0	-6678	--	--	16.08	16.08	0.29	0.12	0.01	0.10	0.00	0.00	20.9
13	0	-0	1577	0	0	0	-6711	--	--	16.08	16.08	0.29	0.12	0.01	0.10	0.00	0.00	20.9
14	0	-0	895	0	0	0	-8470	--	--	16.08	16.08	0.29	0.15	0.01	0.06	0.00	0.00	20.9
15	0	-0	890	0	0	0	-8578	--	--	16.08	16.08	0.29	0.15	0.01	0.06	0.00	0.00	20.9
16	0	-0	1212	0	0	0	-7626	--	--	16.08	16.08	0.29	0.13	0.01	0.08	0.00	0.00	20.9
17	0	-0	1206	0	0	0	-7733	--	--	16.08	16.08	0.29	0.13	0.01	0.08	0.00	0.00	20.9
18	0	-0	-2302	0	0	0	-22580	--	--	16.08	16.08	0.18	0.37	0.02	0.14	0.00	0.00	20.9
19	0	-0	2230	0	0	0	-10450	--	--	16.08	16.08	0.18	0.17	0.02	0.14	0.00	0.00	20.9
20	0	-0	172	0	0	0	-15170	--	--	16.08	16.08	0.18	0.25	0.00	0.01	0.00	0.00	20.9
37	0	-0	-3362	0	0	0	-24980	--	--	16.08	16.08	0.18	0.41	0.03	0.21	0.00	0.00	20.9
38	0	-0	4192	0	0	0	-5016	--	--	16.08	16.08	0.18	0.08	0.03	0.26	0.00	0.00	20.9
39	0	-0	763	0	0	0	-12880	--	--	16.08	16.08	0.18	0.21	0.01	0.05	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	1366	0	0	0	-10530	--	--	16.08	16.08	0.18	0.17	0.01	0.09	0.00	0.00	20.9
2	26	-0	524	0	0	0	-9493	--	--	16.08	16.08	0.29	0.16	0.00	0.03	0.00	0.00	20.9
3	26	-0	523	0	0	0	-9525	--	--	16.08	16.08	0.29	0.16	0.00	0.03	0.00	0.00	20.9
4	26	-0	1579	0	0	0	-6678	--	--	16.08	16.08	0.29	0.12	0.01	0.10	0.00	0.00	20.9
5	26	-0	1577	0	0	0	-6711	--	--	16.08	16.08	0.29	0.12	0.01	0.10	0.00	0.00	20.9
6	26	-0	895	0	0	0	-8470	--	--	16.08	16.08	0.29	0.15	0.01	0.06	0.00	0.00	20.9
7	26	-0	890	0	0	0	-8578	--	--	16.08	16.08	0.29	0.15	0.01	0.06	0.00	0.00	20.9
8	26	-0	1212	0	0	0	-7626	--	--	16.08	16.08	0.29	0.13	0.01	0.08	0.00	0.00	20.9
9	26	-0	1206	0	0	0	-7733	--	--	16.08	16.08	0.29	0.13	0.01	0.08	0.00	0.00	20.9
10	26	-0	524	0	0	0	-9493	--	--	16.08	16.08	0.29	0.16	0.00	0.03	0.00	0.00	20.9
11	26	-0	523	0	0	0	-9525	--	--	16.08	16.08	0.29	0.16	0.00	0.03	0.00	0.00	20.9
12	26	-0	1579	0	0	0	-6678	--	--	16.08	16.08	0.29	0.12	0.01	0.10	0.00	0.00	20.9
13	26	-0	1577	0	0	0	-6711	--	--	16.08	16.08	0.29	0.12	0.01	0.10	0.00	0.00	20.9
14	26	-0	895	0	0	0	-8470	--	--	16.08	16.08	0.29	0.15	0.01	0.06	0.00	0.00	20.9
15	26	-0	890	0	0	0	-8578	--	--	16.08	16.08	0.29	0.15	0.01	0.06	0.00	0.00	20.9
16	26	-0	1212	0	0	0	-7626	--	--	16.08	16.08	0.29	0.13	0.01	0.08	0.00	0.00	20.9
17	26	-0	1206	0	0	0	-7733	--	--	16.08	16.08	0.29	0.13	0.01	0.08	0.00	0.00	20.9
18	26	-0	-2302	0	0	0	-22580	--	--	16.08	16.08	0.18	0.37	0.02	0.14	0.00	0.00	20.9
19	26	-0	2230	0	0	0	-10450	--	--	16.08	16.08	0.18	0.17	0.02	0.14	0.00	0.00	20.9
20	26	-0	172	0	0	0	-15170	--	--	16.08	16.08	0.18	0.25	0.00	0.01	0.00	0.00	20.9
37	26	-0	-3362	0	0	0	-24980	--	--	16.08	16.08	0.18	0.41	0.03	0.21	0.00	0.00	20.9
38	26	-0	4192	0	0	0	-5016	--	--	16.08	16.08	0.18	0.08	0.03	0.26	0.00	0.00	20.9
39	26	-0	763	0	0	0	-12880	--	--	16.08	16.08	0.18	0.21	0.01	0.05	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	1366	0	0	0	-10530	--	--	16.08	16.08	0.18	0.17	0.01	0.09	0.00	0.00	20.9
2	51	-0	524	0	0	0	-9493	--	--	16.08	16.08	0.29	0.16	0.00	0.03	0.00	0.00	20.9

3	51	-0	523	0	0	0	-9525	--	--	16.08	16.08	0.29	0.16	0.00	0.03	0.00	0.00	20.9
4	51	-0	1579	0	0	0	-6678	--	--	16.08	16.08	0.29	0.12	0.01	0.10	0.00	0.00	20.9
5	51	-0	1577	0	0	0	-6711	--	--	16.08	16.08	0.29	0.12	0.01	0.10	0.00	0.00	20.9
6	51	-0	895	0	0	0	-8470	--	--	16.08	16.08	0.29	0.15	0.01	0.06	0.00	0.00	20.9
7	51	-0	890	0	0	0	-8578	--	--	16.08	16.08	0.29	0.15	0.01	0.06	0.00	0.00	20.9
8	51	-0	1212	0	0	0	-7626	--	--	16.08	16.08	0.29	0.13	0.01	0.08	0.00	0.00	20.9
9	51	-0	1206	0	0	0	-7733	--	--	16.08	16.08	0.29	0.13	0.01	0.08	0.00	0.00	20.9
10	51	-0	524	0	0	0	-9493	--	--	16.08	16.08	0.29	0.16	0.00	0.03	0.00	0.00	20.9
11	51	-0	523	0	0	0	-9525	--	--	16.08	16.08	0.29	0.16	0.00	0.03	0.00	0.00	20.9
12	51	-0	1579	0	0	0	-6678	--	--	16.08	16.08	0.29	0.12	0.01	0.10	0.00	0.00	20.9
13	51	-0	1577	0	0	0	-6711	--	--	16.08	16.08	0.29	0.12	0.01	0.10	0.00	0.00	20.9
14	51	-0	895	0	0	0	-8470	--	--	16.08	16.08	0.29	0.15	0.01	0.06	0.00	0.00	20.9
15	51	-0	890	0	0	0	-8578	--	--	16.08	16.08	0.29	0.15	0.01	0.06	0.00	0.00	20.9
16	51	-0	1212	0	0	0	-7626	--	--	16.08	16.08	0.29	0.13	0.01	0.08	0.00	0.00	20.9
17	51	-0	1206	0	0	0	-7733	--	--	16.08	16.08	0.29	0.13	0.01	0.08	0.00	0.00	20.9
18	51	-0	-2302	0	0	0	-22580	--	--	16.08	16.08	0.18	0.37	0.02	0.14	0.00	0.00	20.9
19	51	-0	2230	0	0	0	-10450	--	--	16.08	16.08	0.18	0.17	0.02	0.14	0.00	0.00	20.9
20	51	-0	172	0	0	0	-15170	--	--	16.08	16.08	0.18	0.25	0.00	0.01	0.00	0.00	20.9
37	51	-0	-3362	0	0	0	-24980	--	--	16.08	16.08	0.18	0.41	0.03	0.21	0.00	0.00	20.9
38	51	-0	4192	0	0	0	-5016	--	--	16.08	16.08	0.18	0.08	0.03	0.26	0.00	0.00	20.9
39	51	-0	763	0	0	0	-12880	--	--	16.08	16.08	0.18	0.21	0.01	0.05	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 126 NI 1325 NF 1345 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	3022	0	0	0	-9831	--	--	16.08	16.08	0.18	0.16	0.02	0.19	0.00	0.00	20.9
2	0	-0	1824	0	0	0	-9223	--	--	16.08	16.08	0.29	0.16	0.02	0.11	0.00	0.00	20.9
3	0	-0	1826	0	0	0	-9257	--	--	16.08	16.08	0.29	0.16	0.02	0.11	0.00	0.00	20.9
4	0	-0	2823	0	0	0	-5868	--	--	16.08	16.08	0.29	0.10	0.02	0.18	0.00	0.00	20.9
5	0	-0	2826	0	0	0	-5901	--	--	16.08	16.08	0.29	0.10	0.02	0.18	0.00	0.00	20.9
6	0	-0	2171	0	0	0	-8010	--	--	16.08	16.08	0.29	0.14	0.02	0.14	0.00	0.00	20.9
7	0	-0	2178	0	0	0	-8121	--	--	16.08	16.08	0.29	0.14	0.02	0.14	0.00	0.00	20.9
8	0	-0	2471	0	0	0	-7003	--	--	16.08	16.08	0.29	0.12	0.02	0.16	0.00	0.00	20.9
9	0	-0	2478	0	0	0	-7114	--	--	16.08	16.08	0.29	0.12	0.02	0.16	0.00	0.00	20.9
10	0	-0	1824	0	0	0	-9223	--	--	16.08	16.08	0.29	0.16	0.02	0.11	0.00	0.00	20.9
11	0	-0	1826	0	0	0	-9257	--	--	16.08	16.08	0.29	0.16	0.02	0.11	0.00	0.00	20.9
12	0	-0	2823	0	0	0	-5868	--	--	16.08	16.08	0.29	0.10	0.02	0.18	0.00	0.00	20.9
13	0	-0	2826	0	0	0	-5901	--	--	16.08	16.08	0.29	0.10	0.02	0.18	0.00	0.00	20.9
14	0	-0	2171	0	0	0	-8010	--	--	16.08	16.08	0.29	0.14	0.02	0.14	0.00	0.00	20.9
15	0	-0	2178	0	0	0	-8121	--	--	16.08	16.08	0.29	0.14	0.02	0.14	0.00	0.00	20.9
16	0	-0	2471	0	0	0	-7003	--	--	16.08	16.08	0.29	0.12	0.02	0.16	0.00	0.00	20.9
17	0	-0	2478	0	0	0	-7114	--	--	16.08	16.08	0.29	0.12	0.02	0.16	0.00	0.00	20.9
18	0	-0	-413	0	0	0	-22790	--	--	16.08	16.08	0.18	0.38	0.00	0.03	0.00	0.00	20.9
19	0	-0	4080	0	0	0	-9304	--	--	16.08	16.08	0.18	0.15	0.03	0.26	0.00	0.00	20.9
20	0	-0	2019	0	0	0	-15080	--	--	16.08	16.08	0.18	0.25	0.02	0.13	0.00	0.00	20.9
37	0	-0	-1534	0	0	0	-25770	--	--	16.08	16.08	0.18	0.43	0.01	0.10	0.00	0.00	20.9
38	0	-0	5955	0	0	0	-2863	--	--	16.08	16.08	0.18	0.05	0.05	0.37	0.00	0.00	20.9
39	0	-0	2519	0	0	0	-12490	--	--	16.08	16.08	0.18	0.21	0.02	0.16	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	3022	0	0	0	-9831	--	--	16.08	16.08	0.18	0.16	0.02	0.19	0.00	0.00	20.9
2	26	-0	1824	0	0	0	-9223	--	--	16.08	16.08	0.29	0.16	0.02	0.11	0.00	0.00	20.9
3	26	-0	1826	0	0	0	-9257	--	--	16.08	16.08	0.29	0.16	0.02	0.11	0.00	0.00	20.9
4	26	-0	2823	0	0	0	-5868	--	--	16.08	16.08	0.29	0.10	0.02	0.18	0.00	0.00	20.9
5	26	-0	2826	0	0	0	-5901	--	--	16.08	16.08	0.29	0.10	0.02	0.18	0.00	0.00	20.9
6	26	-0	2171	0	0	0	-8010	--	--	16.08	16.08	0.29	0.14	0.02	0.14	0.00	0.00	20.9
7	26	-0	2178	0	0	0	-8121	--	--	16.08	16.08	0.29	0.14	0.02	0.14	0.00	0.00	20.9
8	26	-0	2471	0	0	0	-7003	--	--	16.08	16.08	0.29	0.12	0.02	0.16	0.00	0.00	20.9
9	26	-0	2478	0	0	0	-7114	--	--	16.08	16.08	0.29	0.12	0.02	0.16	0.00	0.00	20.9
10	26	-0	1824	0	0	0	-9223	--	--	16.08	16.08	0.29	0.16	0.02	0.11	0.00	0.00	20.9
11	26	-0	1826	0	0	0	-9257	--	--	16.08	16.08	0.29	0.16	0.02	0.11	0.00	0.00	20.9
12	26	-0	2823	0	0	0	-5868	--	--	16.08	16.08	0.29	0.10	0.02	0.18	0.00	0.00	20.9
13	26	-0	2826	0	0	0	-5901	--	--	16.08	16.08	0.29	0.10	0.02	0.18	0.00	0.00	20.9
14	26	-0	2171	0	0	0	-8010	--	--	16.08	16.08	0.29	0.14	0.02	0.14	0.00	0.00	20.9
15	26	-0	2178	0	0	0	-8121	--	--	16.08	16.08	0.29	0.14	0.02	0.14	0.00	0.00	20.9
16	26	-0	2471	0	0	0	-7003	--	--	16.08	16.08	0.29	0.12	0.02	0.16	0.00	0.00	20.9
17	26	-0	2478	0	0	0	-7114	--	--	16.08	16.08	0.29	0.12	0.02	0.16	0.00	0.00	20.9
18	26	-0	-413	0	0	0	-22790	--	--	16.08	16.08	0.18	0.38	0.00	0.03	0.00	0.00	20.9
19	26	-0	4080	0	0	0	-9304	--	--	16.08	16.08	0.18	0.15	0.03	0.26	0.00	0.00	20.9
20	26	-0	2019	0	0	0	-15080	--	--	16.08	16.08	0.18	0.25	0.02	0.13	0.00	0.00	20.9
37	26	-0	-1534	0	0	0	-25770	--	--	16.08	16.08	0.18	0.43	0.01	0.10	0.00	0.00	20.9
38	26	-0	5955	0	0	0	-2863	--	--	16.08	16.08	0.18	0.05	0.05	0.37	0.00	0.00	20.9
39	26	-0	2519	0	0	0	-12490	--	--	16.08	16.08	0.18	0.21	0.02	0.16	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	3022	0	0	0	-9831	--	--	16.08	16.08	0.18	0.16	0.02	0.19	0.00	0.00	20.9
2	51	-0	1824	0	0	0	-9223	--	--	16.08	16.08	0.29	0.16	0.02	0.11	0.00	0.00	20.9
3	51	-0	1826	0	0	0	-9257	--	--	16.08	16.08	0.29	0.16	0.02	0.11	0.00	0.00	20.9
4	51	-0	2823	0	0	0	-5868	--	--	16.08	16.08	0.29	0.10	0.02	0.18	0.00	0.00	20.9
5	51	-0	2826	0	0	0	-5901	--	--	16.08	16.08	0.29	0.10	0.02	0.18	0.00	0.00	20.9
6	51	-0	2171	0	0	0	-8010	--	--	16.08	16.08	0.29	0.14	0.02	0.14	0.00	0.00	20.9
7	51	-0	2178	0	0	0	-8121	--	--	16.08	16.08	0.29	0.14	0.02	0.14	0.00	0.00	20.9
8	51	-0	2471	0	0	0	-7003	--	--	16.08	16.08	0.29	0.12	0.02	0.16	0.00	0.00	20.9
9	51	-0	2478	0	0	0	-7114	--	--	16.08	16.08	0.29	0.12	0.02	0.16	0.00	0.00	20.9
10	51	-0	1824	0	0	0	-9223	--	--	16.08	16.08	0.29	0.16	0.02	0.11	0.00	0.00	20.9
11	51	-0	1826	0	0	0	-9257	--	--	16.08	16.08	0.29	0.16	0.02	0.11	0.00	0.00	20.9
12	51	-0	2823	0	0	0	-5868	--	--	16.08	16.08	0.29	0.10	0.02	0.18	0.00	0.00	20.9
13	51	-0	2826	0	0	0	-5901	--	--	16.08	16.08	0.29	0.10	0.02	0.18	0.00	0.00	20.9
14	51	-0	2171	0	0	0	-8010	--	--	16.08	16.08	0.29	0.14	0.02	0.14	0.00	0.00	20.9
15	51	-0	2178	0	0	0	-8121	--	--	16.08	16.08	0.29	0.14	0.02	0.14	0.00	0.00	20.9
16	51	-0	2471	0	0	0	-7003	--	--	16.08	16.08	0.29	0.12	0.02	0.16	0.00	0.00	20.9
17	51	-0	2478	0	0	0	-7114	--	--	16.08	16.08	0.29	0.12	0.02	0.16	0.00	0.00	20.9
18	51	-0	-413	0	0	0	-22790	--	--	16.08	16.08	0.18	0.38	0.00	0.03	0.00	0.00	20.9
19	51	-0	4080	0	0	0	-9304	--	--	16.08	16.08	0.18	0.15	0.03	0.26	0.00	0.00	20.9
20	51	-0	2019	0	0	0	-15080	--	--	16.08	16.08	0.18	0.25	0.02	0.13	0.00	0.00	20.9
37	51	-0	-1534	0	0	0	-25770	--	--	16.08	16.08	0.18	0.43	0.01	0.10	0.00	0.00	20.9
38	51	-0	5955	0	0	0	196	--	--	16.08	16.08	0.00	0.00	0.05	0.37	0.00	0.00	20.9
39	51	-0	2519	0	0	0	-12490	--	--	16.08	16.08	0.18	0.21	0.02	0.16	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 127 NI 1345 NF 1800 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	4964	0	0	0	-8278	--	--	16.08	16.08	0.18	0.14	0.04	0.31	0.00	0.00	20.9
2	0	-0	3371	0	0	0	-8286	--	--	16.08	16.08	0.29	0.14	0.03	0.21	0.00	0.00	20.9
3	0	-0	3377	0	0	0	-8318	--	--	16.08	16.08	0.29	0.14	0.03	0.21	0.00	0.00	20.9
4	0	-0	4260	0	0	0	-4417	--	--	16.08	16.08	0.29	0.08	0.04	0.27	0.00	0.00	20.9
5	0	-0	4266	0	0	0	-4449	--	--	16.08	16.08	0.29	0.08	0.04	0.27	0.00	0.00	20.9
6	0	-0	3676	0	0	0	-6895	--	--	16.08	16.08	0.29	0.12	0.03	0.23	0.00	0.00	20.9
7	0	-0	3695	0	0	0	-7002	--	--	16.08	16.08	0.29	0.12	0.03	0.23	0.00	0.00	20.9
8	0	-0	3943	0	0	0	-5734	--	--	16.08	16.08	0.29	0.10	0.03	0.25	0.00	0.00	20.9
9	0	-0	3961	0	0	0	-5841	--	--	16.08	16.08	0.29	0.10	0.03	0.25	0.00	0.00	20.9
10	0	-0	3371	0	0	0	-8286	--	--	16.08	16.08	0.29	0.14	0.03	0.21	0.00	0.00	20.9
11	0	-0	3377	0	0	0	-8318	--	--	16.08	16.08	0.29	0.14	0.03	0.21	0.00	0.00	20.9
12	0	-0	4260	0	0	0	-4417	--	--	16.08	16.08	0.29	0.08	0.04	0.27	0.00	0.00	20.9
13	0	-0	4266	0	0	0	-4449	--	--	16.08	16.08	0.29	0.08	0.04	0.27	0.00	0.00	20.9
14	0	-0	3676	0	0	0	-6895	--	--	16.08	16.08	0.29	0.12	0.03	0.23	0.00	0.00	20.9
15	0	-0	3695	0	0	0	-7002	--	--	16.08	16.08	0.29	0.12	0.03	0.23	0.00	0.00	20.9
16	0	-0	3943	0	0	0	-5734	--	--	16.08	16.08	0.29	0.10	0.03	0.25	0.00	0.00	20.9
17	0	-0	3961	0	0	0	-5841	--	--	16.08	16.08	0.29	0.10	0.03	0.25	0.00	0.00	20.9
18	0	-0	1978	0	0	0	-22790	--	--	16.08	16.08	0.18	0.38	0.02	0.12	0.00	0.00	20.9
19	0	-0	6238	0	0	0	-7208	--	--	16.08	16.08	0.18	0.12	0.05	0.39	0.00	0.00	20.9
20	0	-0	4254	0	0	0	-14040	--	--	16.08	16.08	0.18	0.23	0.04	0.27	0.00	0.00	20.9
37	0	-0	821	0	0	0	-25770	--	--	16.08	16.08	0.18	0.43	0.01	0.05	0.00	0.00	20.9
38	0	-0	7921	0	0	0	196	--	--	16.08	16.08	0.00	0.00	0.07	0.50	0.00	0.00	20.9
39	0	-0	4615	0	0	0	-11200	--	--	16.08	16.08	0.18	0.19	0.04	0.29	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	26	-0	4964	0	0	0	-8278	--	--	16.08	16.08	0.18	0.14	0.04	0.31	0.00	0.00	20.9
2	26	-0	3371	0	0	0	-8286	--	--	16.08	16.08	0.29	0.14	0.03	0.21	0.00	0.00	20.9
3	26	-0	3377	0	0	0	-8318	--	--	16.08	16.08	0.29	0.14	0.03	0.21	0.00	0.00	20.9
4	26	-0	4260	0	0	0	-4417	--	--	16.08	16.08	0.29	0.08	0.04	0.27	0.00	0.00	20.9
5	26	-0	4266	0	0	0	-4449	--	--	16.08	16.08	0.29	0.08	0.04	0.27	0.00	0.00	20.9
6	26	-0	3676	0	0	0	-6895	--	--	16.08	16.08	0.29	0.12	0.03	0.23	0.00	0.00	20.9
7	26	-0	3695	0	0	0	-7002	--	--	16.08	16.08	0.29	0.12	0.03	0.23	0.00	0.00	20.9
8	26	-0	3943	0	0	0	-5734	--	--	16.08	16.08	0.29	0.10	0.03	0.25	0.00	0.00	20.9
9	26	-0	3961	0	0	0	-5841	--	--	16.08	16.08	0.29	0.10	0.03	0.25	0.00	0.00	20.9
10	26	-0	3371	0	0	0	-8286	--	--	16.08	16.08	0.29	0.14	0.03	0.21	0.00	0.00	20.9
11	26	-0	3377	0	0	0	-8318	--	--	16.08	16.08	0.29	0.14	0.03	0.21	0.00	0.00	20.9
12	26	-0	4260	0	0	0	-4417	--	--	16.08	16.08	0.29	0.08	0.04	0.27	0.00	0.00	20.9
13	26	-0	4266	0	0	0	-4449	--	--	16.08	16.08	0.29	0.08	0.04	0.27	0.00	0.00	20.9
14	26	-0	3676	0	0	0	-6895	--	--	16.08	16.08	0.29	0.12	0.03	0.23	0.00	0.00	20.9
15	26	-0	3695	0	0	0	-7002	--	--	16.08	16.08	0.29	0.12	0.03	0.23	0.00	0.00	20.9
16	26	-0	3943	0	0	0	-5734	--	--	16.08	16.08	0.29	0.10	0.03	0.25	0.00	0.00	20.9
17	26	-0	3961	0	0	0	-5841	--	--	16.08	16.08	0.29	0.10	0.03	0.25	0.00	0.00	20.9
18	26	-0	1978	0	0	0	-22790	--	--	16.08	16.08	0.18	0.38	0.02	0.12	0.00	0.00	20.9
19	26	-0	6238	0	0	0	-7208	--	--	16.08	16.08	0.18	0.12	0.05	0.39	0.00	0.00	20.9
20	26	-0	4254	0	0	0	-14040	--	--	16.08	16.08	0.18	0.23	0.04	0.27	0.00	0.00	20.9
37	26	-0	821	0	0	0	-25770	--	--	16.08	16.08	0.18	0.43	0.01	0.05	0.00	0.00	20.9
38	26	-0	7921	0	0	0	10696	--	--	16.08	16.08	0.00	0.18	0.07	0.50	0.00	0.00	20.9
39	26	-0	4615	0	0	0	-11200	--	--	16.08	16.08	0.18	0.19	0.04	0.29	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	51	-0	4964	0	0	0	-8278	--	--	16.08	16.08	0.18	0.14	0.04	0.31	0.00	0.00	20.9
2	51	-0	3371	0	0	0	-8286	--	--	16.08	16.08	0.29	0.14	0.03	0.21	0.00	0.00	20.9
3	51	-0	3377	0	0	0	-8318	--	--	16.08	16.08	0.29	0.14	0.03	0.21	0.00	0.00	20.9
4	51	-0	4260	0	0	0	-4417	--	--	16.08	16.08	0.29	0.08	0.04	0.27	0.00	0.00	20.9
5	51	-0	4266	0	0	0	-4449	--	--	16.08	16.08	0.29	0.08	0.04	0.27	0.00	0.00	20.9
6	51	-0	3676	0	0	0	-6895	--	--	16.08	16.08	0.29	0.12	0.03	0.23	0.00	0.00	20.9
7	51	-0	3695	0	0	0	-7002	--	--	16.08	16.08	0.29	0.12	0.03	0.23	0.00	0.00	20.9
8	51	-0	3943	0	0	0	-5734	--	--	16.08	16.08	0.29	0.10	0.03	0.25	0.00	0.00	20.9
9	51	-0	3961	0	0	0	-5841	--	--	16.08	16.08	0.29	0.10	0.03	0.25	0.00	0.00	20.9
10	51	-0	3371	0	0	0	-8286	--	--	16.08	16.08	0.29	0.14	0.03	0.21	0.00	0.00	20.9
11	51	-0	3377	0	0	0	-8318	--	--	16.08	16.08	0.29	0.14	0.03	0.21	0.00	0.00	20.9
12	51	-0	4260	0	0	0	-4417	--	--	16.08	16.08	0.29	0.08	0.04	0.27	0.00	0.00	20.9
13	51	-0	4266	0	0	0	-4449	--	--	16.08	16.08	0.29	0.08	0.04	0.27	0.00	0.00	20.9
14	51	-0	3676	0	0	0	-6895	--	--	16.08	16.08	0.29	0.12	0.03	0.23	0.00	0.00	20.9
15	51	-0	3695	0	0	0	-7002	--	--	16.08	16.08	0.29	0.12	0.03	0.23	0.00	0.00	20.9
16	51	-0	3943	0	0	0	-5734	--	--	16.08	16.08	0.29	0.10	0.03	0.25	0.00	0.00	20.9
17	51	-0	3961	0	0	0	-5841	--	--	16.08	16.08	0.29	0.10	0.03	0.25	0.00	0.00	20.9
18	51	-0	1978	0	0	0	-22790	--	--	16.08	16.08	0.18	0.38	0.02	0.12	0.00	0.00	20.9
19	51	-0	6238	0	0	0	-7208	--	--	16.08	16.08	0.18	0.12	0.05	0.39	0.00	0.00	20.9
20	51	-0	4254	0	0	0	-14040	--	--	16.08	16.08	0.18	0.23	0.04	0.27	0.00	0.00	20.9
37	51	-0	821	0	0	0	-25770	--	--	16.08	16.08	0.18	0.43	0.01	0.05	0.00	0.00	20.9
38	51	-0	7921	0	0	0	4264	--	--	16.08	16.08	0.00	0.07	0.07	0.50	0.00	0.00	20.9
39	51	-0	4615	0	0	0	-11200	--	--	16.08	16.08	0.18	0.19	0.04	0.29	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 128 NI 1279 NF 1266 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-2500	0	0	0	662	--	--	16.08	16.08	0.00	0.01	0.02	0.16	0.00	0.00	20.9
2	0	-0	-1963	0	0	0	585	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
3	0	-0	-1935	0	0	0	577	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
4	0	-0	-1912	0	0	0	441	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
5	0	-0	-1884	0	0	0	434	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
6	0	-0	-1977	0	0	0	543	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
7	0	-0	-1885	0	0	0	518	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
8	0	-0	-1962	0	0	0	500	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
9	0	-0	-1870	0	0	0	475	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
10	0	-0	-1963	0	0	0	585	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9

11	0	-0	-1935	0	0	0	577	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
12	0	-0	-1912	0	0	0	441	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
13	0	-0	-1884	0	0	0	434	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
14	0	-0	-1977	0	0	0	543	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
15	0	-0	-1885	0	0	0	518	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
16	0	-0	-1962	0	0	0	500	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
17	0	-0	-1870	0	0	0	475	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
18	0	-0	-2735	0	0	0	878	--	--	16.08	16.08	0.00	0.01	0.02	0.17	0.00	0.00	20.9
19	0	-0	-2560	0	0	0	456	--	--	16.08	16.08	0.00	0.01	0.02	0.16	0.00	0.00	20.9
20	0	-0	-2693	0	0	0	688	--	--	16.08	16.08	0.00	0.01	0.02	0.17	0.00	0.00	20.9
37	0	-0	-2724	0	0	0	1011	--	--	16.08	16.08	0.00	0.02	0.02	0.17	0.00	0.00	20.9
38	0	-0	-2432	0	0	0	308	--	--	16.08	16.08	0.00	0.01	0.02	0.15	0.00	0.00	20.9
39	0	-0	-2653	0	0	0	695	--	--	16.08	16.08	0.00	0.01	0.02	0.17	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	-2500	0	0	0	662	--	--	16.08	16.08	0.00	0.01	0.02	0.16	0.00	0.00	20.9
2	26	-0	-1963	0	0	0	585	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
3	26	-0	-1935	0	0	0	577	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
4	26	-0	-1912	0	0	0	-541	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
5	26	-0	-1884	0	0	0	-534	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
6	26	-0	-1977	0	0	0	543	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
7	26	-0	-1885	0	0	0	518	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
8	26	-0	-1962	0	0	0	-507	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
9	26	-0	-1870	0	0	0	-485	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
10	26	-0	-1963	0	0	0	585	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
11	26	-0	-1935	0	0	0	577	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
12	26	-0	-1912	0	0	0	-541	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
13	26	-0	-1884	0	0	0	-534	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
14	26	-0	-1977	0	0	0	543	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
15	26	-0	-1885	0	0	0	518	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
16	26	-0	-1962	0	0	0	-507	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
17	26	-0	-1870	0	0	0	-485	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
18	26	-0	-2735	0	0	0	878	--	--	16.08	16.08	0.00	0.01	0.02	0.17	0.00	0.00	20.9
19	26	-0	-2560	0	0	0	-858	--	--	16.08	16.08	0.18	0.01	0.02	0.16	0.00	0.00	20.9
20	26	-0	-2693	0	0	0	-695	--	--	16.08	16.08	0.18	0.01	0.02	0.17	0.00	0.00	20.9
37	26	-0	-2724	0	0	0	1011	--	--	16.08	16.08	0.00	0.02	0.02	0.17	0.00	0.00	20.9
38	26	-0	-2432	0	0	0	-941	--	--	16.08	16.08	0.18	0.02	0.02	0.15	0.00	0.00	20.9
39	26	-0	-2653	0	0	0	695	--	--	16.08	16.08	0.00	0.01	0.02	0.17	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	-2500	0	0	0	-622	--	--	16.08	16.08	0.18	0.01	0.02	0.16	0.00	0.00	20.9
2	51	-0	-1963	0	0	0	-423	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
3	51	-0	-1935	0	0	0	-417	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
4	51	-0	-1912	0	0	0	-541	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
5	51	-0	-1884	0	0	0	-534	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
6	51	-0	-1977	0	0	0	-472	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
7	51	-0	-1885	0	0	0	-450	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
8	51	-0	-1962	0	0	0	-507	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
9	51	-0	-1870	0	0	0	-485	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
10	51	-0	-1963	0	0	0	-423	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
11	51	-0	-1935	0	0	0	-417	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
12	51	-0	-1912	0	0	0	-541	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
13	51	-0	-1884	0	0	0	-534	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
14	51	-0	-1977	0	0	0	-472	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
15	51	-0	-1885	0	0	0	-450	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
16	51	-0	-1962	0	0	0	-507	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
17	51	-0	-1870	0	0	0	-485	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
18	51	-0	-2735	0	0	0	-527	--	--	16.08	16.08	0.18	0.01	0.02	0.17	0.00	0.00	20.9
19	51	-0	-2560	0	0	0	-858	--	--	16.08	16.08	0.18	0.01	0.02	0.16	0.00	0.00	20.9
20	51	-0	-2693	0	0	0	-695	--	--	16.08	16.08	0.18	0.01	0.02	0.17	0.00	0.00	20.9
37	51	-0	-2724	0	0	0	-388	--	--	16.08	16.08	0.18	0.01	0.02	0.17	0.00	0.00	20.9
38	51	-0	-2432	0	0	0	-941	--	--	16.08	16.08	0.18	0.02	0.02	0.15	0.00	0.00	20.9
39	51	-0	-2653	0	0	0	-668	--	--	16.08	16.08	0.18	0.01	0.02	0.17	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 129 NI 1266 NF 1274 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-2344	0	0	0	96	--	--	16.08	16.08	0.00	0.00	0.02	0.15	0.00	0.00	20.9
2	0	-0	-1839	0	0	0	124	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
3	0	-0	-1809	0	0	0	122	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
4	0	-0	-1797	0	0	0	26	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
5	0	-0	-1767	0	0	0	24	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
6	0	-0	-1860	0	0	0	92	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
7	0	-0	-1759	0	0	0	85	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
8	0	-0	-1847	0	0	0	62	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
9	0	-0	-1746	0	0	0	56	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
10	0	-0	-1839	0	0	0	124	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
11	0	-0	-1809	0	0	0	122	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
12	0	-0	-1797	0	0	0	26	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
13	0	-0	-1767	0	0	0	24	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
14	0	-0	-1860	0	0	0	92	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
15	0	-0	-1759	0	0	0	85	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
16	0	-0	-1847	0	0	0	62	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
17	0	-0	-1746	0	0	0	56	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
18	0	-0	-2566	0	0	0	220	--	--	16.08	16.08	0.00	0.00	0.02	0.16	0.00	0.00	20.9
19	0	-0	-2408	0	0	0	-1304	--	--	16.08	16.08	0.18	0.02	0.02	0.15	0.00	0.00	20.9
20	0	-0	-2534	0	0	0	86	--	--	16.08	16.08	0.00	0.00	0.02	0.16	0.00	0.00	20.9
37	0	-0	-2552	0	0	0	321	--	--	16.08	16.08	0.00	0.01	0.02	0.16	0.00	0.00	20.9
38	0	-0	-2288	0	0	0	-1332	--	--	16.08	16.08	0.18	0.02	0.02	0.14	0.00	0.00	20.9
39	0	-0	-2498	0	0	0	97	--	--	16.08	16.08	0.00	0.00	0.02	0.16	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	-2344	0	0	0	-1108	--	--	16.08	16.08	0.18	0.02	0.02	0.15	0.00	0.00	20.9
2	26	-0	-1839	0	0	0	-820	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
3	26	-0	-1809	0	0	0	-807	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
4	26	-0	-1797	0	0	0	-897	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
5	26	-0	-1767	0	0	0	-884	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
6	26	-0	-1860	0	0	0	-863	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9

7	26	-0	-1759	0	0	0	-818	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
8	26	-0	-1847	0	0	0	-886	--	--	16.08	16.08	0.29	0.02	0.02	0.12	0.00	0.00	20.9
9	26	-0	-1746	0	0	0	-841	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
10	26	-0	-1839	0	0	0	-820	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
11	26	-0	-1809	0	0	0	-807	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
12	26	-0	-1797	0	0	0	-897	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
13	26	-0	-1767	0	0	0	-884	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
14	26	-0	-1860	0	0	0	-863	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
15	26	-0	-1759	0	0	0	-818	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
16	26	-0	-1847	0	0	0	-886	--	--	16.08	16.08	0.29	0.02	0.02	0.12	0.00	0.00	20.9
17	26	-0	-1746	0	0	0	-841	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
18	26	-0	-2566	0	0	0	-1098	--	--	16.08	16.08	0.18	0.02	0.02	0.16	0.00	0.00	20.9
19	26	-0	-2408	0	0	0	-1304	--	--	16.08	16.08	0.18	0.02	0.02	0.15	0.00	0.00	20.9
20	26	-0	-2534	0	0	0	-1216	--	--	16.08	16.08	0.18	0.02	0.02	0.16	0.00	0.00	20.9
37	26	-0	-2552	0	0	0	-990	--	--	16.08	16.08	0.18	0.02	0.02	0.16	0.00	0.00	20.9
38	26	-0	-2288	0	0	0	-1332	--	--	16.08	16.08	0.18	0.02	0.02	0.14	0.00	0.00	20.9
39	26	-0	-2498	0	0	0	-1186	--	--	16.08	16.08	0.18	0.02	0.02	0.16	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	-2344	0	0	0	-1108	--	--	16.08	16.08	0.18	0.02	0.02	0.15	0.00	0.00	20.9
2	51	-0	-1839	0	0	0	-820	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
3	51	-0	-1809	0	0	0	-807	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
4	51	-0	-1797	0	0	0	-897	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
5	51	-0	-1767	0	0	0	-884	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
6	51	-0	-1860	0	0	0	-863	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
7	51	-0	-1759	0	0	0	-818	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
8	51	-0	-1847	0	0	0	-886	--	--	16.08	16.08	0.29	0.02	0.02	0.12	0.00	0.00	20.9
9	51	-0	-1746	0	0	0	-841	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
10	51	-0	-1839	0	0	0	-820	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
11	51	-0	-1809	0	0	0	-807	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
12	51	-0	-1797	0	0	0	-897	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
13	51	-0	-1767	0	0	0	-884	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
14	51	-0	-1860	0	0	0	-863	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
15	51	-0	-1759	0	0	0	-818	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
16	51	-0	-1847	0	0	0	-886	--	--	16.08	16.08	0.29	0.02	0.02	0.12	0.00	0.00	20.9
17	51	-0	-1746	0	0	0	-841	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
18	51	-0	-2566	0	0	0	-1098	--	--	16.08	16.08	0.18	0.02	0.02	0.16	0.00	0.00	20.9
19	51	-0	-2408	0	0	0	-1304	--	--	16.08	16.08	0.18	0.02	0.02	0.15	0.00	0.00	20.9
20	51	-0	-2534	0	0	0	-1216	--	--	16.08	16.08	0.18	0.02	0.02	0.16	0.00	0.00	20.9
37	51	-0	-2552	0	0	0	-990	--	--	16.08	16.08	0.18	0.02	0.02	0.16	0.00	0.00	20.9
38	51	-0	-2288	0	0	0	-1332	--	--	16.08	16.08	0.18	0.02	0.02	0.14	0.00	0.00	20.9
39	51	-0	-2498	0	0	0	-1186	--	--	16.08	16.08	0.18	0.02	0.02	0.16	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 130 NI 1274 NF 1273 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-1657	0	0	0	-1350	--	--	16.08	16.08	0.18	0.02	0.01	0.10	0.00	0.00	20.9
2	0	-0	-1323	0	0	0	-1015	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
3	0	-0	-1299	0	0	0	-998	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
4	0	-0	-1251	0	0	0	-1079	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
5	0	-0	-1227	0	0	0	-1062	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
6	0	-0	-1326	0	0	0	-1057	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
7	0	-0	-1245	0	0	0	-1000	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
8	0	-0	-1305	0	0	0	-1077	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
9	0	-0	-1224	0	0	0	-1019	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
10	0	-0	-1323	0	0	0	-1015	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
11	0	-0	-1299	0	0	0	-998	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
12	0	-0	-1251	0	0	0	-1079	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
13	0	-0	-1227	0	0	0	-1062	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
14	0	-0	-1326	0	0	0	-1057	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
15	0	-0	-1245	0	0	0	-1000	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
16	0	-0	-1305	0	0	0	-1077	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
17	0	-0	-1224	0	0	0	-1019	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
18	0	-0	-1870	0	0	0	-1371	--	--	16.08	16.08	0.18	0.02	0.02	0.12	0.00	0.00	20.9
19	0	-0	-1629	0	0	0	-1535	--	--	16.08	16.08	0.18	0.03	0.01	0.10	0.00	0.00	20.9
20	0	-0	-1781	0	0	0	-1472	--	--	16.08	16.08	0.18	0.02	0.01	0.11	0.00	0.00	20.9
37	0	-0	-1906	0	0	0	-1272	--	--	16.08	16.08	0.18	0.02	0.02	0.12	0.00	0.00	20.9
38	0	-0	-1505	0	0	0	-1545	--	--	16.08	16.08	0.18	0.03	0.01	0.09	0.00	0.00	20.9
39	0	-0	-1757	0	0	0	-1440	--	--	16.08	16.08	0.18	0.02	0.01	0.11	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	-1657	0	0	0	-1350	--	--	16.08	16.08	0.18	0.02	0.01	0.10	0.00	0.00	20.9
2	26	-0	-1323	0	0	0	-1015	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
3	26	-0	-1299	0	0	0	-998	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
4	26	-0	-1251	0	0	0	-1079	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
5	26	-0	-1227	0	0	0	-1062	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
6	26	-0	-1326	0	0	0	-1057	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
7	26	-0	-1245	0	0	0	-1000	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
8	26	-0	-1305	0	0	0	-1077	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
9	26	-0	-1224	0	0	0	-1019	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
10	26	-0	-1323	0	0	0	-1015	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
11	26	-0	-1299	0	0	0	-998	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
12	26	-0	-1251	0	0	0	-1079	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
13	26	-0	-1227	0	0	0	-1062	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
14	26	-0	-1326	0	0	0	-1057	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
15	26	-0	-1245	0	0	0	-1000	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
16	26	-0	-1305	0	0	0	-1077	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
17	26	-0	-1224	0	0	0	-1019	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
18	26	-0	-1870	0	0	0	-1371	--	--	16.08	16.08	0.18	0.02	0.02	0.12	0.00	0.00	20.9
19	26	-0	-1629	0	0	0	-1535	--	--	16.08	16.08	0.18	0.03	0.01	0.10	0.00	0.00	20.9
20	26	-0	-1781	0	0	0	-1472	--	--	16.08	16.08	0.18	0.02	0.01	0.11	0.00	0.00	20.9
37	26	-0	-1906	0	0	0	-1272	--	--	16.08	16.08	0.18	0.02	0.02	0.12	0.00	0.00	20.9
38	26	-0	-1505	0	0	0	-1545	--	--	16.08	16.08	0.18	0.03	0.01	0.09	0.00	0.00	20.9
39	26	-0	-1757	0	0	0	-1440	--	--	16.08	16.08	0.18	0.02	0.01	0.11	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	-1657	0	0	0	-1350	--	--	16.08	16.08	0.18	0.02	0.01	0.10	0.00	0.00	20.9
2	51	-0	-1323	0	0	0	-1015	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9

3	51	-0	-1299	0	0	0	-998	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
4	51	-0	-1251	0	0	0	-1079	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
5	51	-0	-1227	0	0	0	-1062	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
6	51	-0	-1326	0	0	0	-1057	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
7	51	-0	-1245	0	0	0	-1000	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
8	51	-0	-1305	0	0	0	-1077	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
9	51	-0	-1224	0	0	0	-1019	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
10	51	-0	-1323	0	0	0	-1015	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
11	51	-0	-1299	0	0	0	-998	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
12	51	-0	-1251	0	0	0	-1079	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
13	51	-0	-1227	0	0	0	-1062	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
14	51	-0	-1326	0	0	0	-1057	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
15	51	-0	-1245	0	0	0	-1000	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
16	51	-0	-1305	0	0	0	-1077	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
17	51	-0	-1224	0	0	0	-1019	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
18	51	-0	-1870	0	0	0	-1371	--	--	16.08	16.08	0.18	0.02	0.02	0.12	0.00	0.00	20.9
19	51	-0	-1629	0	0	0	-1535	--	--	16.08	16.08	0.18	0.03	0.01	0.10	0.00	0.00	20.9
20	51	-0	-1781	0	0	0	-1472	--	--	16.08	16.08	0.18	0.02	0.01	0.11	0.00	0.00	20.9
37	51	-0	-1906	0	0	0	-1272	--	--	16.08	16.08	0.18	0.02	0.02	0.12	0.00	0.00	20.9
38	51	-0	-1505	0	0	0	-1545	--	--	16.08	16.08	0.18	0.03	0.01	0.09	0.00	0.00	20.9
39	51	-0	-1757	0	0	0	-1440	--	--	16.08	16.08	0.18	0.02	0.01	0.11	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 131 NI 1273 NF 1272 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--												Fx,M	Bielle	V,Mx			
	cm		daN			daN*m				cmq						cmq/m		cm
1	0	-0	-914	0	0	0	-1453	--	--	16.08	16.08	0.18	0.02	0.01	0.06	0.00	0.00	20.9
2	0	-0	-752	0	0	0	-1102	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
3	0	-0	-736	0	0	0	-1083	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
4	0	-0	-671	0	0	0	-1152	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
5	0	-0	-655	0	0	0	-1133	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
6	0	-0	-743	0	0	0	-1143	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
7	0	-0	-688	0	0	0	-1077	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
8	0	-0	-719	0	0	0	-1158	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
9	0	-0	-664	0	0	0	-1092	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
10	0	-0	-752	0	0	0	-1102	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
11	0	-0	-736	0	0	0	-1083	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
12	0	-0	-671	0	0	0	-1152	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
13	0	-0	-655	0	0	0	-1133	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
14	0	-0	-743	0	0	0	-1143	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
15	0	-0	-688	0	0	0	-1077	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
16	0	-0	-719	0	0	0	-1158	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
17	0	-0	-664	0	0	0	-1092	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
18	0	-0	-1078	0	0	0	-1497	--	--	16.08	16.08	0.18	0.02	0.01	0.07	0.00	0.00	20.9
19	0	-0	-821	0	0	0	-1617	--	--	16.08	16.08	0.18	0.03	0.01	0.05	0.00	0.00	20.9
20	0	-0	-962	0	0	0	-1577	--	--	16.08	16.08	0.18	0.03	0.01	0.06	0.00	0.00	20.9
37	0	-0	-1145	0	0	0	-1411	--	--	16.08	16.08	0.18	0.02	0.01	0.07	0.00	0.00	20.9
38	0	-0	-717	0	0	0	-1612	--	--	16.08	16.08	0.18	0.03	0.01	0.04	0.00	0.00	20.9
39	0	-0	-952	0	0	0	-1545	--	--	16.08	16.08	0.18	0.03	0.01	0.06	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	-914	0	0	0	-1453	--	--	16.08	16.08	0.18	0.02	0.01	0.06	0.00	0.00	20.9
2	26	-0	-752	0	0	0	-1102	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
3	26	-0	-736	0	0	0	-1083	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
4	26	-0	-671	0	0	0	-1152	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
5	26	-0	-655	0	0	0	-1133	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
6	26	-0	-743	0	0	0	-1143	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
7	26	-0	-688	0	0	0	-1077	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
8	26	-0	-719	0	0	0	-1158	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
9	26	-0	-664	0	0	0	-1092	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
10	26	-0	-752	0	0	0	-1102	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
11	26	-0	-736	0	0	0	-1083	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
12	26	-0	-671	0	0	0	-1152	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
13	26	-0	-655	0	0	0	-1133	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
14	26	-0	-743	0	0	0	-1143	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
15	26	-0	-688	0	0	0	-1077	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
16	26	-0	-719	0	0	0	-1158	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
17	26	-0	-664	0	0	0	-1092	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
18	26	-0	-1078	0	0	0	-1497	--	--	16.08	16.08	0.18	0.02	0.01	0.07	0.00	0.00	20.9
19	26	-0	-821	0	0	0	-1617	--	--	16.08	16.08	0.18	0.03	0.01	0.05	0.00	0.00	20.9
20	26	-0	-962	0	0	0	-1577	--	--	16.08	16.08	0.18	0.03	0.01	0.06	0.00	0.00	20.9
37	26	-0	-1145	0	0	0	-1411	--	--	16.08	16.08	0.18	0.02	0.01	0.07	0.00	0.00	20.9
38	26	-0	-717	0	0	0	-1612	--	--	16.08	16.08	0.18	0.03	0.01	0.04	0.00	0.00	20.9
39	26	-0	-952	0	0	0	-1545	--	--	16.08	16.08	0.18	0.03	0.01	0.06	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	-914	0	0	0	-1453	--	--	16.08	16.08	0.18	0.02	0.01	0.06	0.00	0.00	20.9
2	51	-0	-752	0	0	0	-1102	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
3	51	-0	-736	0	0	0	-1083	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
4	51	-0	-671	0	0	0	-1152	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
5	51	-0	-655	0	0	0	-1133	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
6	51	-0	-743	0	0	0	-1143	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
7	51	-0	-688	0	0	0	-1077	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
8	51	-0	-719	0	0	0	-1158	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
9	51	-0	-664	0	0	0	-1092	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
10	51	-0	-752	0	0	0	-1102	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
11	51	-0	-736	0	0	0	-1083	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
12	51	-0	-671	0	0	0	-1152	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
13	51	-0	-655	0	0	0	-1133	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
14	51	-0	-743	0	0	0	-1143	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
15	51	-0	-688	0	0	0	-1077	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
16	51	-0	-719	0	0	0	-1158	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
17	51	-0	-664	0	0	0	-1092	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
18	51	-0	-1078	0	0	0	-1497	--	--	16.08	16.08	0.18	0.02	0.01	0.07	0.00	0.00	20.9
19	51	-0	-821	0	0	0	-1617	--	--	16.08	16.08	0.18	0.03	0.01	0.05	0.00	0.00	20.9
20	51	-0	-962	0	0	0	-1577	--	--	16.08	16.08	0.18	0.03	0.01	0.06	0.00	0.00	20.9
37	51	-0	-1145	0	0	0	-1411	--	--	16.08	16.08	0.18	0.02	0.01	0.07	0.00	0.00	20.9
38	51	-0	-717	0	0	0	-1612	--	--	16.08	16.08	0.18	0.03	0.01	0.04	0.00	0.00	20.9
39	51	-0	-952	0	0	0	-1545	--	--	16.08	16.08	0.18	0.03	0.01	0.06	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 132 NI 1272 NF 1310 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-289	0	0	0	-1420	--	--	16.08	16.08	0.18	0.02	0.00	0.02	0.00	0.00	20.9
2	0	-0	-268	0	0	0	-1085	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
3	0	-0	-258	0	0	0	-1065	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
4	0	-0	-186	0	0	0	-1120	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
5	0	-0	-176	0	0	0	-1100	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
6	0	-0	-251	0	0	0	-1121	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
7	0	-0	-218	0	0	0	-1053	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
8	0	-0	-227	0	0	0	-1132	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
9	0	-0	-193	0	0	0	-1063	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
10	0	-0	-268	0	0	0	-1085	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
11	0	-0	-258	0	0	0	-1065	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
12	0	-0	-186	0	0	0	-1120	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
13	0	-0	-176	0	0	0	-1100	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
14	0	-0	-251	0	0	0	-1121	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
15	0	-0	-218	0	0	0	-1053	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
16	0	-0	-227	0	0	0	-1132	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
17	0	-0	-193	0	0	0	-1063	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
18	0	-0	-401	0	0	0	-1477	--	--	16.08	16.08	0.18	0.02	0.00	0.03	0.00	0.00	20.9
19	0	-0	-148	0	0	0	-1552	--	--	16.08	16.08	0.18	0.03	0.00	0.01	0.00	0.00	20.9
20	0	-0	-270	0	0	0	-1532	--	--	16.08	16.08	0.18	0.03	0.00	0.02	0.00	0.00	20.9
37	0	-0	-490	0	0	0	-1411	--	--	16.08	16.08	0.18	0.02	0.00	0.03	0.00	0.00	20.9
38	0	-0	-68	0	0	0	-1535	--	--	16.08	16.08	0.18	0.03	0.00	0.00	0.00	0.00	20.9
39	0	-0	-273	0	0	0	-1502	--	--	16.08	16.08	0.18	0.02	0.00	0.02	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	26	-0	-289	0	0	0	-1420	--	--	16.08	16.08	0.18	0.02	0.00	0.02	0.00	0.00	20.9
2	26	-0	-268	0	0	0	-1085	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
3	26	-0	-258	0	0	0	-1065	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
4	26	-0	-186	0	0	0	-1120	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
5	26	-0	-176	0	0	0	-1100	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
6	26	-0	-251	0	0	0	-1121	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
7	26	-0	-218	0	0	0	-1053	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
8	26	-0	-227	0	0	0	-1132	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
9	26	-0	-193	0	0	0	-1063	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
10	26	-0	-268	0	0	0	-1085	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
11	26	-0	-258	0	0	0	-1065	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
12	26	-0	-186	0	0	0	-1120	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
13	26	-0	-176	0	0	0	-1100	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
14	26	-0	-251	0	0	0	-1121	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
15	26	-0	-218	0	0	0	-1053	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
16	26	-0	-227	0	0	0	-1132	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
17	26	-0	-193	0	0	0	-1063	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
18	26	-0	-401	0	0	0	-1477	--	--	16.08	16.08	0.18	0.02	0.00	0.03	0.00	0.00	20.9
19	26	-0	-148	0	0	0	-1552	--	--	16.08	16.08	0.18	0.03	0.00	0.01	0.00	0.00	20.9
20	26	-0	-270	0	0	0	-1532	--	--	16.08	16.08	0.18	0.03	0.00	0.02	0.00	0.00	20.9
37	26	-0	-490	0	0	0	-1411	--	--	16.08	16.08	0.18	0.02	0.00	0.03	0.00	0.00	20.9
38	26	-0	-68	0	0	0	-1535	--	--	16.08	16.08	0.18	0.03	0.00	0.00	0.00	0.00	20.9
39	26	-0	-273	0	0	0	-1502	--	--	16.08	16.08	0.18	0.02	0.00	0.02	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	51	-0	-289	0	0	0	-1420	--	--	16.08	16.08	0.18	0.02	0.00	0.02	0.00	0.00	20.9
2	51	-0	-268	0	0	0	-1085	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
3	51	-0	-258	0	0	0	-1065	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
4	51	-0	-186	0	0	0	-1120	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
5	51	-0	-176	0	0	0	-1100	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
6	51	-0	-251	0	0	0	-1121	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
7	51	-0	-218	0	0	0	-1053	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
8	51	-0	-227	0	0	0	-1132	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
9	51	-0	-193	0	0	0	-1063	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
10	51	-0	-268	0	0	0	-1085	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
11	51	-0	-258	0	0	0	-1065	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
12	51	-0	-186	0	0	0	-1120	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
13	51	-0	-176	0	0	0	-1100	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
14	51	-0	-251	0	0	0	-1121	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
15	51	-0	-218	0	0	0	-1053	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
16	51	-0	-227	0	0	0	-1132	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
17	51	-0	-193	0	0	0	-1063	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
18	51	-0	-401	0	0	0	-1477	--	--	16.08	16.08	0.18	0.02	0.00	0.03	0.00	0.00	20.9
19	51	-0	-148	0	0	0	-1552	--	--	16.08	16.08	0.18	0.03	0.00	0.01	0.00	0.00	20.9
20	51	-0	-270	0	0	0	-1532	--	--	16.08	16.08	0.18	0.03	0.00	0.02	0.00	0.00	20.9
37	51	-0	-490	0	0	0	-1411	--	--	16.08	16.08	0.18	0.02	0.00	0.03	0.00	0.00	20.9
38	51	-0	-68	0	0	0	-1535	--	--	16.08	16.08	0.18	0.03	0.00	0.00	0.00	0.00	20.9
39	51	-0	-273	0	0	0	-1502	--	--	16.08	16.08	0.18	0.02	0.00	0.02	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 133 NI 1310 NF 1309 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	283	0	0	0	-1422	--	--	16.08	16.08	0.18	0.02	0.00	0.02	0.00	0.00	20.9
2	0	-0	174	0	0	0	-1072	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
3	0	-0	178	0	0	0	-1054	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
4	0	-0	257	0	0	0	-1134	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
5	0	-0	262	0	0	0	-1116	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
6	0	-0	198	0	0	0	-1115	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
7	0	-0	212	0	0	0	-1054	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
8	0	-0	223	0	0	0	-1134	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
9	0	-0	237	0	0	0	-1073	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
10	0	-0	174	0	0	0	-1072	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9

11	0	-0	178	0	0	0	-1054	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
12	0	-0	257	0	0	0	-1134	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
13	0	-0	262	0	0	0	-1116	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
14	0	-0	198	0	0	0	-1115	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
15	0	-0	212	0	0	0	-1054	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
16	0	-0	223	0	0	0	-1134	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
17	0	-0	237	0	0	0	-1073	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
18	0	-0	219	0	0	0	-1451	--	--	16.08	16.08	0.18	0.02	0.00	0.01	0.00	0.00	20.9
19	0	-0	471	0	0	0	-1609	--	--	16.08	16.08	0.18	0.03	0.00	0.03	0.00	0.00	20.9
20	0	-0	363	0	0	0	-1551	--	--	16.08	16.08	0.18	0.03	0.00	0.02	0.00	0.00	20.9
37	0	-0	109	0	0	0	-1351	--	--	16.08	16.08	0.18	0.02	0.00	0.01	0.00	0.00	20.9
38	0	-0	528	0	0	0	-1615	--	--	16.08	16.08	0.18	0.03	0.00	0.03	0.00	0.00	20.9
39	0	-0	349	0	0	0	-1519	--	--	16.08	16.08	0.18	0.03	0.00	0.02	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	283	0	0	0	-1422	--	--	16.08	16.08	0.18	0.02	0.00	0.02	0.00	0.00	20.9
2	26	-0	174	0	0	0	-1072	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
3	26	-0	178	0	0	0	-1054	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
4	26	-0	257	0	0	0	-1134	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
5	26	-0	262	0	0	0	-1116	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
6	26	-0	198	0	0	0	-1115	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
7	26	-0	212	0	0	0	-1054	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
8	26	-0	223	0	0	0	-1134	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
9	26	-0	237	0	0	0	-1073	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
10	26	-0	174	0	0	0	-1072	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
11	26	-0	178	0	0	0	-1054	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
12	26	-0	257	0	0	0	-1134	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
13	26	-0	262	0	0	0	-1116	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
14	26	-0	198	0	0	0	-1115	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
15	26	-0	212	0	0	0	-1054	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
16	26	-0	223	0	0	0	-1134	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
17	26	-0	237	0	0	0	-1073	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
18	26	-0	219	0	0	0	-1451	--	--	16.08	16.08	0.18	0.02	0.00	0.01	0.00	0.00	20.9
19	26	-0	471	0	0	0	-1609	--	--	16.08	16.08	0.18	0.03	0.00	0.03	0.00	0.00	20.9
20	26	-0	363	0	0	0	-1551	--	--	16.08	16.08	0.18	0.03	0.00	0.02	0.00	0.00	20.9
37	26	-0	109	0	0	0	-1351	--	--	16.08	16.08	0.18	0.02	0.00	0.01	0.00	0.00	20.9
38	26	-0	528	0	0	0	-1615	--	--	16.08	16.08	0.18	0.03	0.00	0.03	0.00	0.00	20.9
39	26	-0	349	0	0	0	-1519	--	--	16.08	16.08	0.18	0.03	0.00	0.02	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	283	0	0	0	-1422	--	--	16.08	16.08	0.18	0.02	0.00	0.02	0.00	0.00	20.9
2	51	-0	174	0	0	0	-1072	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
3	51	-0	178	0	0	0	-1054	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
4	51	-0	257	0	0	0	-1134	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
5	51	-0	262	0	0	0	-1116	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
6	51	-0	198	0	0	0	-1115	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
7	51	-0	212	0	0	0	-1054	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
8	51	-0	223	0	0	0	-1134	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
9	51	-0	237	0	0	0	-1073	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
10	51	-0	174	0	0	0	-1072	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
11	51	-0	178	0	0	0	-1054	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
12	51	-0	257	0	0	0	-1134	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
13	51	-0	262	0	0	0	-1116	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
14	51	-0	198	0	0	0	-1115	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
15	51	-0	212	0	0	0	-1054	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
16	51	-0	223	0	0	0	-1134	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
17	51	-0	237	0	0	0	-1073	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
18	51	-0	219	0	0	0	-1451	--	--	16.08	16.08	0.18	0.02	0.00	0.01	0.00	0.00	20.9
19	51	-0	471	0	0	0	-1609	--	--	16.08	16.08	0.18	0.03	0.00	0.03	0.00	0.00	20.9
20	51	-0	363	0	0	0	-1551	--	--	16.08	16.08	0.18	0.03	0.00	0.02	0.00	0.00	20.9
37	51	-0	109	0	0	0	-1351	--	--	16.08	16.08	0.18	0.02	0.00	0.01	0.00	0.00	20.9
38	51	-0	528	0	0	0	-1615	--	--	16.08	16.08	0.18	0.03	0.00	0.03	0.00	0.00	20.9
39	51	-0	349	0	0	0	-1519	--	--	16.08	16.08	0.18	0.03	0.00	0.02	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 134 NI 1309 NF 1267 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	846	0	0	0	-1458	--	--	16.08	16.08	0.18	0.02	0.01	0.05	0.00	0.00	20.9
2	0	-0	608	0	0	0	-1108	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
3	0	-0	607	0	0	0	-1088	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
4	0	-0	694	0	0	0	-1155	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
5	0	-0	693	0	0	0	-1135	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
6	0	-0	639	0	0	0	-1147	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
7	0	-0	636	0	0	0	-1081	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
8	0	-0	665	0	0	0	-1162	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
9	0	-0	662	0	0	0	-1096	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
10	0	-0	608	0	0	0	-1108	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
11	0	-0	607	0	0	0	-1088	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
12	0	-0	694	0	0	0	-1155	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
13	0	-0	693	0	0	0	-1135	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
14	0	-0	639	0	0	0	-1147	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
15	0	-0	636	0	0	0	-1081	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
16	0	-0	665	0	0	0	-1162	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
17	0	-0	662	0	0	0	-1096	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
18	0	-0	828	0	0	0	-1506	--	--	16.08	16.08	0.18	0.02	0.01	0.05	0.00	0.00	20.9
19	0	-0	1082	0	0	0	-1618	--	--	16.08	16.08	0.18	0.03	0.01	0.07	0.00	0.00	20.9
20	0	-0	986	0	0	0	-1583	--	--	16.08	16.08	0.18	0.03	0.01	0.06	0.00	0.00	20.9
37	0	-0	695	0	0	0	-1422	--	--	16.08	16.08	0.18	0.02	0.01	0.04	0.00	0.00	20.9
38	0	-0	1119	0	0	0	-1610	--	--	16.08	16.08	0.18	0.03	0.01	0.07	0.00	0.00	20.9
39	0	-0	960	0	0	0	-1550	--	--	16.08	16.08	0.18	0.03	0.01	0.06	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	846	0	0	0	-1458	--	--	16.08	16.08	0.18	0.02	0.01	0.05	0.00	0.00	20.9
2	26	-0	608	0	0	0	-1108	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
3	26	-0	607	0	0	0	-1088	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
4	26	-0	694	0	0	0	-1155	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
5	26	-0	693	0	0	0	-1135	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
6	26	-0	639	0	0	0	-1147	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9

7	26	-0	636	0	0	0	-1081	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
8	26	-0	665	0	0	0	-1162	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
9	26	-0	662	0	0	0	-1096	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
10	26	-0	608	0	0	0	-1108	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
11	26	-0	607	0	0	0	-1088	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
12	26	-0	694	0	0	0	-1155	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
13	26	-0	693	0	0	0	-1135	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
14	26	-0	639	0	0	0	-1147	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
15	26	-0	636	0	0	0	-1081	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
16	26	-0	665	0	0	0	-1162	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
17	26	-0	662	0	0	0	-1096	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
18	26	-0	828	0	0	0	-1506	--	--	16.08	16.08	0.18	0.02	0.01	0.05	0.00	0.00	20.9
19	26	-0	1082	0	0	0	-1618	--	--	16.08	16.08	0.18	0.03	0.01	0.07	0.00	0.00	20.9
20	26	-0	986	0	0	0	-1583	--	--	16.08	16.08	0.18	0.03	0.01	0.06	0.00	0.00	20.9
37	26	-0	695	0	0	0	-1422	--	--	16.08	16.08	0.18	0.02	0.01	0.04	0.00	0.00	20.9
38	26	-0	1119	0	0	0	-1610	--	--	16.08	16.08	0.18	0.03	0.01	0.07	0.00	0.00	20.9
39	26	-0	960	0	0	0	-1550	--	--	16.08	16.08	0.18	0.03	0.01	0.06	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	846	0	0	0	-1458	--	--	16.08	16.08	0.18	0.02	0.01	0.05	0.00	0.00	20.9
2	51	-0	608	0	0	0	-1108	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
3	51	-0	607	0	0	0	-1088	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
4	51	-0	694	0	0	0	-1155	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
5	51	-0	693	0	0	0	-1135	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
6	51	-0	639	0	0	0	-1147	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
7	51	-0	636	0	0	0	-1081	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
8	51	-0	665	0	0	0	-1162	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
9	51	-0	662	0	0	0	-1096	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
10	51	-0	608	0	0	0	-1108	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
11	51	-0	607	0	0	0	-1088	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
12	51	-0	694	0	0	0	-1155	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
13	51	-0	693	0	0	0	-1135	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
14	51	-0	639	0	0	0	-1147	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
15	51	-0	636	0	0	0	-1081	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
16	51	-0	665	0	0	0	-1162	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
17	51	-0	662	0	0	0	-1096	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
18	51	-0	828	0	0	0	-1506	--	--	16.08	16.08	0.18	0.02	0.01	0.05	0.00	0.00	20.9
19	51	-0	1082	0	0	0	-1618	--	--	16.08	16.08	0.18	0.03	0.01	0.07	0.00	0.00	20.9
20	51	-0	986	0	0	0	-1583	--	--	16.08	16.08	0.18	0.03	0.01	0.06	0.00	0.00	20.9
37	51	-0	695	0	0	0	-1422	--	--	16.08	16.08	0.18	0.02	0.01	0.04	0.00	0.00	20.9
38	51	-0	1119	0	0	0	-1610	--	--	16.08	16.08	0.18	0.03	0.01	0.07	0.00	0.00	20.9
39	51	-0	960	0	0	0	-1550	--	--	16.08	16.08	0.18	0.03	0.01	0.06	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 135 NI 1267 NF 1298 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	1440	0	0	0	-1380	--	--	16.08	16.08	0.18	0.02	0.01	0.09	0.00	0.00	20.9
2	0	-0	1066	0	0	0	-1056	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
3	0	-0	1060	0	0	0	-1036	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
4	0	-0	1156	0	0	0	-1088	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
5	0	-0	1151	0	0	0	-1068	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
6	0	-0	1104	0	0	0	-1091	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
7	0	-0	1085	0	0	0	-1023	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
8	0	-0	1131	0	0	0	-1101	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
9	0	-0	1112	0	0	0	-1033	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
10	0	-0	1066	0	0	0	-1056	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
11	0	-0	1060	0	0	0	-1036	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
12	0	-0	1156	0	0	0	-1088	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
13	0	-0	1151	0	0	0	-1068	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
14	0	-0	1104	0	0	0	-1091	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
15	0	-0	1085	0	0	0	-1023	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
16	0	-0	1131	0	0	0	-1101	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
17	0	-0	1112	0	0	0	-1033	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
18	0	-0	1468	0	0	0	-1439	--	--	16.08	16.08	0.18	0.02	0.01	0.09	0.00	0.00	20.9
19	0	-0	1731	0	0	0	-1504	--	--	16.08	16.08	0.18	0.02	0.01	0.11	0.00	0.00	20.9
20	0	-0	1645	0	0	0	-1489	--	--	16.08	16.08	0.18	0.02	0.01	0.10	0.00	0.00	20.9
37	0	-0	1309	0	0	0	-1377	--	--	16.08	16.08	0.18	0.02	0.01	0.08	0.00	0.00	20.9
38	0	-0	1748	0	0	0	-1486	--	--	16.08	16.08	0.18	0.02	0.01	0.11	0.00	0.00	20.9
39	0	-0	1605	0	0	0	-1460	--	--	16.08	16.08	0.18	0.02	0.01	0.10	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	1440	0	0	0	-1380	--	--	16.08	16.08	0.18	0.02	0.01	0.09	0.00	0.00	20.9
2	26	-0	1066	0	0	0	-1056	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
3	26	-0	1060	0	0	0	-1036	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
4	26	-0	1156	0	0	0	-1088	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
5	26	-0	1151	0	0	0	-1068	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
6	26	-0	1104	0	0	0	-1091	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
7	26	-0	1085	0	0	0	-1023	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
8	26	-0	1131	0	0	0	-1101	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
9	26	-0	1112	0	0	0	-1033	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
10	26	-0	1066	0	0	0	-1056	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
11	26	-0	1060	0	0	0	-1036	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
12	26	-0	1156	0	0	0	-1088	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
13	26	-0	1151	0	0	0	-1068	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
14	26	-0	1104	0	0	0	-1091	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
15	26	-0	1085	0	0	0	-1023	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
16	26	-0	1131	0	0	0	-1101	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
17	26	-0	1112	0	0	0	-1033	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
18	26	-0	1468	0	0	0	-1439	--	--	16.08	16.08	0.18	0.02	0.01	0.09	0.00	0.00	20.9
19	26	-0	1731	0	0	0	-1504	--	--	16.08	16.08	0.18	0.02	0.01	0.11	0.00	0.00	20.9
20	26	-0	1645	0	0	0	-1489	--	--	16.08	16.08	0.18	0.02	0.01	0.10	0.00	0.00	20.9
37	26	-0	1309	0	0	0	-1377	--	--	16.08	16.08	0.18	0.02	0.01	0.08	0.00	0.00	20.9
38	26	-0	1748	0	0	0	-1486	--	--	16.08	16.08	0.18	0.02	0.01	0.11	0.00	0.00	20.9
39	26	-0	1605	0	0	0	-1460	--	--	16.08	16.08	0.18	0.02	0.01	0.10	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	1440	0	0	0	-1380	--	--	16.08	16.08	0.18	0.02	0.01	0.09	0.00	0.00	20.9
2	51	-0	1066	0	0	0	-1056	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9

3	51	-0	1060	0	0	0	-1036	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
4	51	-0	1156	0	0	0	-1088	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
5	51	-0	1151	0	0	0	-1068	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
6	51	-0	1104	0	0	0	-1091	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
7	51	-0	1085	0	0	0	-1023	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
8	51	-0	1131	0	0	0	-1101	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
9	51	-0	1112	0	0	0	-1033	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
10	51	-0	1066	0	0	0	-1056	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
11	51	-0	1060	0	0	0	-1036	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
12	51	-0	1156	0	0	0	-1088	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
13	51	-0	1151	0	0	0	-1068	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
14	51	-0	1104	0	0	0	-1091	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
15	51	-0	1085	0	0	0	-1023	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
16	51	-0	1131	0	0	0	-1101	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
17	51	-0	1112	0	0	0	-1033	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
18	51	-0	1468	0	0	0	-1439	--	--	16.08	16.08	0.18	0.02	0.01	0.09	0.00	0.00	20.9
19	51	-0	1731	0	0	0	-1504	--	--	16.08	16.08	0.18	0.02	0.01	0.11	0.00	0.00	20.9
20	51	-0	1645	0	0	0	-1489	--	--	16.08	16.08	0.18	0.02	0.01	0.10	0.00	0.00	20.9
37	51	-0	1309	0	0	0	-1377	--	--	16.08	16.08	0.18	0.02	0.01	0.08	0.00	0.00	20.9
38	51	-0	1748	0	0	0	-1486	--	--	16.08	16.08	0.18	0.02	0.01	0.11	0.00	0.00	20.9
39	51	-0	1605	0	0	0	-1460	--	--	16.08	16.08	0.18	0.02	0.01	0.10	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 136 NI 1298 NF 1275 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	2108	0	0	0	-1173	--	--	16.08	16.08	0.18	0.02	0.02	0.13	0.00	0.00	20.9
2	0	-0	1580	0	0	0	-905	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
3	0	-0	1569	0	0	0	-885	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
4	0	-0	1673	0	0	0	-920	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
5	0	-0	1663	0	0	0	-900	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
6	0	-0	1625	0	0	0	-933	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
7	0	-0	1590	0	0	0	-867	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
8	0	-0	1653	0	0	0	-938	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
9	0	-0	1618	0	0	0	-871	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
10	0	-0	1580	0	0	0	-905	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
11	0	-0	1569	0	0	0	-885	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
12	0	-0	1673	0	0	0	-920	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
13	0	-0	1663	0	0	0	-900	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
14	0	-0	1625	0	0	0	-933	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
15	0	-0	1590	0	0	0	-867	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
16	0	-0	1653	0	0	0	-938	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
17	0	-0	1618	0	0	0	-871	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
18	0	-0	2187	0	0	0	-1234	--	--	16.08	16.08	0.18	0.02	0.02	0.14	0.00	0.00	20.9
19	0	-0	2456	0	0	0	-1249	--	--	16.08	16.08	0.18	0.02	0.02	0.15	0.00	0.00	20.9
20	0	-0	2382	0	0	0	-1252	--	--	16.08	16.08	0.18	0.02	0.02	0.15	0.00	0.00	20.9
37	0	-0	2001	0	0	0	-1199	--	--	16.08	16.08	0.18	0.02	0.02	0.13	0.00	0.00	20.9
38	0	-0	2449	0	0	0	-1223	--	--	16.08	16.08	0.18	0.02	0.02	0.15	0.00	0.00	20.9
39	0	-0	2327	0	0	0	-1228	--	--	16.08	16.08	0.18	0.02	0.02	0.15	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	2108	0	0	0	-1173	--	--	16.08	16.08	0.18	0.02	0.02	0.13	0.00	0.00	20.9
2	26	-0	1580	0	0	0	-905	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
3	26	-0	1569	0	0	0	-885	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
4	26	-0	1673	0	0	0	-920	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
5	26	-0	1663	0	0	0	-900	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
6	26	-0	1625	0	0	0	-933	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
7	26	-0	1590	0	0	0	-867	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
8	26	-0	1653	0	0	0	-938	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
9	26	-0	1618	0	0	0	-871	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
10	26	-0	1580	0	0	0	-905	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
11	26	-0	1569	0	0	0	-885	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
12	26	-0	1673	0	0	0	-920	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
13	26	-0	1663	0	0	0	-900	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
14	26	-0	1625	0	0	0	-933	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
15	26	-0	1590	0	0	0	-867	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
16	26	-0	1653	0	0	0	-938	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
17	26	-0	1618	0	0	0	-871	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
18	26	-0	2187	0	0	0	-1234	--	--	16.08	16.08	0.18	0.02	0.02	0.14	0.00	0.00	20.9
19	26	-0	2456	0	0	0	-1249	--	--	16.08	16.08	0.18	0.02	0.02	0.15	0.00	0.00	20.9
20	26	-0	2382	0	0	0	-1252	--	--	16.08	16.08	0.18	0.02	0.02	0.15	0.00	0.00	20.9
37	26	-0	2001	0	0	0	-1199	--	--	16.08	16.08	0.18	0.02	0.02	0.13	0.00	0.00	20.9
38	26	-0	2449	0	0	0	-1223	--	--	16.08	16.08	0.18	0.02	0.02	0.15	0.00	0.00	20.9
39	26	-0	2327	0	0	0	-1228	--	--	16.08	16.08	0.18	0.02	0.02	0.15	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	2108	0	0	0	-1173	--	--	16.08	16.08	0.18	0.02	0.02	0.13	0.00	0.00	20.9
2	51	-0	1580	0	0	0	-905	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
3	51	-0	1569	0	0	0	-885	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
4	51	-0	1673	0	0	0	-920	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
5	51	-0	1663	0	0	0	-900	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
6	51	-0	1625	0	0	0	-933	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
7	51	-0	1590	0	0	0	-867	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
8	51	-0	1653	0	0	0	-938	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
9	51	-0	1618	0	0	0	-871	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
10	51	-0	1580	0	0	0	-905	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
11	51	-0	1569	0	0	0	-885	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
12	51	-0	1673	0	0	0	-920	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
13	51	-0	1663	0	0	0	-900	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
14	51	-0	1625	0	0	0	-933	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
15	51	-0	1590	0	0	0	-867	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
16	51	-0	1653	0	0	0	-938	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
17	51	-0	1618	0	0	0	-871	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
18	51	-0	2187	0	0	0	-1234	--	--	16.08	16.08	0.18	0.02	0.02	0.14	0.00	0.00	20.9
19	51	-0	2456	0	0	0	13	--	--	16.08	16.08	0.00	0.00	0.02	0.15	0.00	0.00	20.9
20	51	-0	2382	0	0	0	-1252	--	--	16.08	16.08	0.18	0.02	0.02	0.15	0.00	0.00	20.9
37	51	-0	2001	0	0	0	-1199	--	--	16.08	16.08	0.18	0.02	0.02	0.13	0.00	0.00	20.9
38	51	-0	2449	0	0	0	35	--	--	16.08	16.08	0.00	0.00	0.02	0.15	0.00	0.00	20.9
39	51	-0	2327	0	0	0	-1228	--	--	16.08	16.08	0.18	0.02	0.02	0.15	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 137 NI 1275 NF 1337 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	2457	0	0	0	-880	--	--	16.08	16.08	0.18	0.01	0.02	0.15	0.00	0.00	20.9
2	0	-0	1855	0	0	0	-690	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
3	0	-0	1840	0	0	0	-671	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
4	0	-0	1941	0	0	0	-683	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
5	0	-0	1926	0	0	0	-664	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
6	0	-0	1903	0	0	0	-709	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
7	0	-0	1852	0	0	0	-647	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
8	0	-0	1928	0	0	0	-707	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
9	0	-0	1878	0	0	0	-645	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
10	0	-0	1855	0	0	0	-690	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
11	0	-0	1840	0	0	0	-671	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
12	0	-0	1941	0	0	0	-683	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
13	0	-0	1926	0	0	0	-664	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
14	0	-0	1903	0	0	0	-709	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
15	0	-0	1852	0	0	0	-647	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
16	0	-0	1928	0	0	0	-707	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
17	0	-0	1878	0	0	0	-645	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
18	0	-0	2577	0	0	0	-941	--	--	16.08	16.08	0.18	0.02	0.02	0.16	0.00	0.00	20.9
19	0	-0	2825	0	0	0	-893	--	--	16.08	16.08	0.18	0.01	0.02	0.18	0.00	0.00	20.9
20	0	-0	2775	0	0	0	-919	--	--	16.08	16.08	0.18	0.02	0.02	0.17	0.00	0.00	20.9
37	0	-0	2385	0	0	0	-941	--	--	16.08	16.08	0.18	0.02	0.02	0.15	0.00	0.00	20.9
38	0	-0	2797	0	0	0	-861	--	--	16.08	16.08	0.18	0.01	0.02	0.18	0.00	0.00	20.9
39	0	-0	2714	0	0	0	-903	--	--	16.08	16.08	0.18	0.01	0.02	0.17	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	2457	0	0	0	-880	--	--	16.08	16.08	0.18	0.01	0.02	0.15	0.00	0.00	20.9
2	26	-0	1855	0	0	0	-690	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
3	26	-0	1840	0	0	0	-671	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
4	26	-0	1941	0	0	0	-683	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
5	26	-0	1926	0	0	0	-664	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
6	26	-0	1903	0	0	0	-709	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
7	26	-0	1852	0	0	0	-647	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
8	26	-0	1928	0	0	0	-707	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
9	26	-0	1878	0	0	0	-645	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
10	26	-0	1855	0	0	0	-690	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
11	26	-0	1840	0	0	0	-671	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
12	26	-0	1941	0	0	0	-683	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
13	26	-0	1926	0	0	0	-664	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
14	26	-0	1903	0	0	0	-709	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
15	26	-0	1852	0	0	0	-647	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
16	26	-0	1928	0	0	0	-707	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
17	26	-0	1878	0	0	0	-645	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
18	26	-0	2577	0	0	0	-941	--	--	16.08	16.08	0.18	0.02	0.02	0.16	0.00	0.00	20.9
19	26	-0	2825	0	0	0	-893	--	--	16.08	16.08	0.18	0.01	0.02	0.18	0.00	0.00	20.9
20	26	-0	2775	0	0	0	-919	--	--	16.08	16.08	0.18	0.02	0.02	0.17	0.00	0.00	20.9
37	26	-0	2385	0	0	0	-941	--	--	16.08	16.08	0.18	0.02	0.02	0.15	0.00	0.00	20.9
38	26	-0	2797	0	0	0	-861	--	--	16.08	16.08	0.18	0.01	0.02	0.18	0.00	0.00	20.9
39	26	-0	2714	0	0	0	-903	--	--	16.08	16.08	0.18	0.01	0.02	0.17	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	2457	0	0	0	382	--	--	16.08	16.08	0.00	0.01	0.02	0.15	0.00	0.00	20.9
2	51	-0	1855	0	0	0	263	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
3	51	-0	1840	0	0	0	274	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
4	51	-0	1941	0	0	0	314	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
5	51	-0	1926	0	0	0	325	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
6	51	-0	1903	0	0	0	268	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
7	51	-0	1852	0	0	0	305	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
8	51	-0	1928	0	0	0	284	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
9	51	-0	1878	0	0	0	320	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
10	51	-0	1855	0	0	0	263	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
11	51	-0	1840	0	0	0	274	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
12	51	-0	1941	0	0	0	314	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
13	51	-0	1926	0	0	0	325	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
14	51	-0	1903	0	0	0	268	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
15	51	-0	1852	0	0	0	305	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
16	51	-0	1928	0	0	0	284	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
17	51	-0	1878	0	0	0	320	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
18	51	-0	2577	0	0	0	383	--	--	16.08	16.08	0.00	0.01	0.02	0.16	0.00	0.00	20.9
19	51	-0	2825	0	0	0	558	--	--	16.08	16.08	0.00	0.01	0.02	0.18	0.00	0.00	20.9
20	51	-0	2775	0	0	0	507	--	--	16.08	16.08	0.00	0.01	0.02	0.17	0.00	0.00	20.9
37	51	-0	2385	0	0	0	284	--	--	16.08	16.08	0.00	0.00	0.02	0.15	0.00	0.00	20.9
38	51	-0	2797	0	0	0	576	--	--	16.08	16.08	0.00	0.01	0.02	0.18	0.00	0.00	20.9
39	51	-0	2714	0	0	0	491	--	--	16.08	16.08	0.00	0.01	0.02	0.17	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 138 NI 1337 NF 1277 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	1916	0	0	0	-368	--	--	16.08	16.08	0.18	0.01	0.02	0.12	0.00	0.00	20.9
2	0	-0	1425	0	0	0	-323	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
3	0	-0	1405	0	0	0	-307	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
4	0	-0	1542	0	0	0	-259	--	--	16.08	16.08	0.29	0.00	0.01	0.10	0.00	0.00	20.9
5	0	-0	1522	0	0	0	-243	--	--	16.08	16.08	0.29	0.00	0.01	0.10	0.00	0.00	20.9
6	0	-0	1489	0	0	0	-319	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
7	0	-0	1423	0	0	0	-267	--	--	16.08	16.08	0.29	0.00	0.01	0.09	0.00	0.00	20.9
8	0	-0	1524	0	0	0	-300	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
9	0	-0	1458	0	0	0	-247	--	--	16.08	16.08	0.29	0.00	0.01	0.09	0.00	0.00	20.9
10	0	-0	1425	0	0	0	-323	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9

11	0	-0	1405	0	0	0	-307	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
12	0	-0	1542	0	0	0	-259	--	--	16.08	16.08	0.29	0.00	0.01	0.10	0.00	0.00	20.9
13	0	-0	1522	0	0	0	-243	--	--	16.08	16.08	0.29	0.00	0.01	0.10	0.00	0.00	20.9
14	0	-0	1489	0	0	0	-319	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
15	0	-0	1423	0	0	0	-267	--	--	16.08	16.08	0.29	0.00	0.01	0.09	0.00	0.00	20.9
16	0	-0	1524	0	0	0	-300	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
17	0	-0	1458	0	0	0	-247	--	--	16.08	16.08	0.29	0.00	0.01	0.09	0.00	0.00	20.9
18	0	-0	1974	0	0	0	-459	--	--	16.08	16.08	0.18	0.01	0.02	0.12	0.00	0.00	20.9
19	0	-0	2314	0	0	0	-240	--	--	16.08	16.08	0.18	0.00	0.02	0.15	0.00	0.00	20.9
20	0	-0	2225	0	0	0	-338	--	--	16.08	16.08	0.18	0.01	0.02	0.14	0.00	0.00	20.9
37	0	-0	1759	0	0	0	-541	--	--	16.08	16.08	0.18	0.01	0.01	0.11	0.00	0.00	20.9
38	0	-0	2326	0	0	0	-175	--	--	16.08	16.08	0.18	0.00	0.02	0.15	0.00	0.00	20.9
39	0	-0	2178	0	0	0	-338	--	--	16.08	16.08	0.18	0.01	0.02	0.14	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	1916	0	0	0	2172	--	--	16.08	16.08	0.00	0.04	0.02	0.12	0.00	0.00	20.9
2	26	-0	1425	0	0	0	1566	--	--	16.08	16.08	0.10	0.03	0.01	0.09	0.00	0.00	20.9
3	26	-0	1405	0	0	0	1555	--	--	16.08	16.08	0.10	0.03	0.01	0.09	0.00	0.00	20.9
4	26	-0	1542	0	0	0	1785	--	--	16.08	16.08	0.10	0.03	0.01	0.10	0.00	0.00	20.9
5	26	-0	1522	0	0	0	1774	--	--	16.08	16.08	0.10	0.03	0.01	0.10	0.00	0.00	20.9
6	26	-0	1489	0	0	0	1655	--	--	16.08	16.08	0.10	0.03	0.01	0.09	0.00	0.00	20.9
7	26	-0	1423	0	0	0	1620	--	--	16.08	16.08	0.10	0.03	0.01	0.09	0.00	0.00	20.9
8	26	-0	1524	0	0	0	1721	--	--	16.08	16.08	0.10	0.03	0.01	0.10	0.00	0.00	20.9
9	26	-0	1458	0	0	0	1685	--	--	16.08	16.08	0.10	0.03	0.01	0.09	0.00	0.00	20.9
10	26	-0	1425	0	0	0	1566	--	--	16.08	16.08	0.10	0.03	0.01	0.09	0.00	0.00	20.9
11	26	-0	1405	0	0	0	1555	--	--	16.08	16.08	0.10	0.03	0.01	0.09	0.00	0.00	20.9
12	26	-0	1542	0	0	0	1785	--	--	16.08	16.08	0.10	0.03	0.01	0.10	0.00	0.00	20.9
13	26	-0	1522	0	0	0	1774	--	--	16.08	16.08	0.10	0.03	0.01	0.10	0.00	0.00	20.9
14	26	-0	1489	0	0	0	1655	--	--	16.08	16.08	0.10	0.03	0.01	0.09	0.00	0.00	20.9
15	26	-0	1423	0	0	0	1620	--	--	16.08	16.08	0.10	0.03	0.01	0.09	0.00	0.00	20.9
16	26	-0	1524	0	0	0	1721	--	--	16.08	16.08	0.10	0.03	0.01	0.10	0.00	0.00	20.9
17	26	-0	1458	0	0	0	1685	--	--	16.08	16.08	0.10	0.03	0.01	0.09	0.00	0.00	20.9
18	26	-0	1974	0	0	0	2157	--	--	16.08	16.08	0.00	0.04	0.02	0.12	0.00	0.00	20.9
19	26	-0	2314	0	0	0	2827	--	--	16.08	16.08	0.00	0.05	0.02	0.15	0.00	0.00	20.9
20	26	-0	2225	0	0	0	2612	--	--	16.08	16.08	0.00	0.04	0.02	0.14	0.00	0.00	20.9
37	26	-0	1759	0	0	0	-541	--	--	16.08	16.08	0.18	0.01	0.01	0.11	0.00	0.00	20.9
38	26	-0	2326	0	0	0	2908	--	--	16.08	16.08	0.00	0.05	0.02	0.15	0.00	0.00	20.9
39	26	-0	2178	0	0	0	2549	--	--	16.08	16.08	0.00	0.04	0.02	0.14	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	1916	0	0	0	616	--	--	16.08	16.08	0.00	0.01	0.02	0.12	0.00	0.00	20.9
2	51	-0	1425	0	0	0	409	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
3	51	-0	1405	0	0	0	414	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
4	51	-0	1542	0	0	0	533	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
5	51	-0	1522	0	0	0	538	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
6	51	-0	1489	0	0	0	446	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
7	51	-0	1423	0	0	0	464	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
8	51	-0	1524	0	0	0	483	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
9	51	-0	1458	0	0	0	501	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
10	51	-0	1425	0	0	0	409	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
11	51	-0	1405	0	0	0	414	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
12	51	-0	1542	0	0	0	533	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
13	51	-0	1522	0	0	0	538	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
14	51	-0	1489	0	0	0	446	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
15	51	-0	1423	0	0	0	464	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
16	51	-0	1524	0	0	0	483	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
17	51	-0	1458	0	0	0	501	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
18	51	-0	1974	0	0	0	555	--	--	16.08	16.08	0.00	0.01	0.02	0.12	0.00	0.00	20.9
19	51	-0	2314	0	0	0	948	--	--	16.08	16.08	0.00	0.02	0.02	0.15	0.00	0.00	20.9
20	51	-0	2225	0	0	0	805	--	--	16.08	16.08	0.00	0.01	0.02	0.14	0.00	0.00	20.9
37	51	-0	1759	0	0	0	363	--	--	16.08	16.08	0.00	0.01	0.01	0.11	0.00	0.00	20.9
38	51	-0	2326	0	0	0	1019	--	--	16.08	16.08	0.00	0.02	0.02	0.15	0.00	0.00	20.9
39	51	-0	2178	0	0	0	781	--	--	16.08	16.08	0.00	0.01	0.02	0.14	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 139 NI 1277 NF 1270 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm

1	0	-0	-1387	0	0	0	580	--	--	16.08	16.08	0.00	0.01	0.01	0.09	0.00	0.00	20.9
2	0	-0	-1141	0	0	0	521	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
3	0	-0	-1116	0	0	0	524	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
4	0	-0	-1017	0	0	0	369	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
5	0	-0	-993	0	0	0	371	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
6	0	-0	-1126	0	0	0	465	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
7	0	-0	-1044	0	0	0	473	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
8	0	-0	-1089	0	0	0	419	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
9	0	-0	-1007	0	0	0	428	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
10	0	-0	-1141	0	0	0	521	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
11	0	-0	-1116	0	0	0	524	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
12	0	-0	-1017	0	0	0	369	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
13	0	-0	-993	0	0	0	371	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
14	0	-0	-1126	0	0	0	465	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
15	0	-0	-1044	0	0	0	473	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
16	0	-0	-1089	0	0	0	419	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
17	0	-0	-1007	0	0	0	428	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
18	0	-0	-1752	0	0	0	924	--	--	16.08	16.08	0.00	0.02	0.01	0.11	0.00	0.00	20.9
19	0	-0	-1368	0	0	0	472	--	--	16.08	16.08	0.00	0.01	0.01	0.09	0.00	0.00	20.9
20	0	-0	-1585	0	0	0	749	--	--	16.08	16.08	0.00	0.01	0.01	0.10	0.00	0.00	20.9
37	0	-0	-1801	0	0	0	1020	--	--	16.08	16.08	0.00	0.02	0.01	0.11	0.00	0.00	20.9
38	0	-0	-1161	0	0	0	267	--	--	16.08	16.08	0.00	0.00	0.01	0.07	0.00	0.00	20.9
39	0	-0	-1522	0	0	0	728	--	--	16.08	16.08	0.00	0.01	0.01	0.10	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	-1387	0	0	0	580	--	--	16.08	16.08	0.00	0.01	0.01	0.09	0.00	0.00	20.9
2	26	-0	-1141	0	0	0	521	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
3	26	-0	-1116	0	0	0	524	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
4	26	-0	-1017	0	0	0	369	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
5	26	-0	-993	0	0	0	371	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
6	26	-0	-1126	0	0	0	465	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9

7	26	-0	-1044	0	0	0	473	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
8	26	-0	-1089	0	0	0	419	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
9	26	-0	-1007	0	0	0	428	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
10	26	-0	-1141	0	0	0	521	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
11	26	-0	-1116	0	0	0	524	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
12	26	-0	-1017	0	0	0	369	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
13	26	-0	-993	0	0	0	371	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
14	26	-0	-1126	0	0	0	465	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
15	26	-0	-1044	0	0	0	473	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
16	26	-0	-1089	0	0	0	419	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
17	26	-0	-1007	0	0	0	428	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
18	26	-0	-1752	0	0	0	924	--	--	16.08	16.08	0.00	0.02	0.01	0.11	0.00	0.00	20.9
19	26	-0	-1368	0	0	0	472	--	--	16.08	16.08	0.00	0.01	0.01	0.09	0.00	0.00	20.9
20	26	-0	-1585	0	0	0	749	--	--	16.08	16.08	0.00	0.01	0.01	0.10	0.00	0.00	20.9
37	26	-0	-1801	0	0	0	1020	--	--	16.08	16.08	0.00	0.02	0.01	0.11	0.00	0.00	20.9
38	26	-0	-1161	0	0	0	-329	--	--	16.08	16.08	0.18	0.01	0.01	0.07	0.00	0.00	20.9
39	26	-0	-1522	0	0	0	728	--	--	16.08	16.08	0.00	0.01	0.01	0.10	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	-1387	0	0	0	-132	--	--	16.08	16.08	0.18	0.00	0.01	0.09	0.00	0.00	20.9
2	51	-0	-1141	0	0	0	-65	--	--	16.08	16.08	0.29	0.00	0.01	0.07	0.00	0.00	20.9
3	51	-0	-1116	0	0	0	-50	--	--	16.08	16.08	0.29	0.00	0.01	0.07	0.00	0.00	20.9
4	51	-0	-1017	0	0	0	-154	--	--	16.08	16.08	0.29	0.00	0.01	0.06	0.00	0.00	20.9
5	51	-0	-993	0	0	0	-138	--	--	16.08	16.08	0.29	0.00	0.01	0.06	0.00	0.00	20.9
6	51	-0	-1126	0	0	0	-114	--	--	16.08	16.08	0.29	0.00	0.01	0.07	0.00	0.00	20.9
7	51	-0	-1044	0	0	0	-63	--	--	16.08	16.08	0.29	0.00	0.01	0.07	0.00	0.00	20.9
8	51	-0	-1089	0	0	0	-140	--	--	16.08	16.08	0.29	0.00	0.01	0.07	0.00	0.00	20.9
9	51	-0	-1007	0	0	0	-90	--	--	16.08	16.08	0.29	0.00	0.01	0.06	0.00	0.00	20.9
10	51	-0	-1141	0	0	0	-65	--	--	16.08	16.08	0.29	0.00	0.01	0.07	0.00	0.00	20.9
11	51	-0	-1116	0	0	0	-50	--	--	16.08	16.08	0.29	0.00	0.01	0.07	0.00	0.00	20.9
12	51	-0	-1017	0	0	0	-154	--	--	16.08	16.08	0.29	0.00	0.01	0.06	0.00	0.00	20.9
13	51	-0	-993	0	0	0	-138	--	--	16.08	16.08	0.29	0.00	0.01	0.06	0.00	0.00	20.9
14	51	-0	-1126	0	0	0	-114	--	--	16.08	16.08	0.29	0.00	0.01	0.07	0.00	0.00	20.9
15	51	-0	-1044	0	0	0	-63	--	--	16.08	16.08	0.29	0.00	0.01	0.07	0.00	0.00	20.9
16	51	-0	-1089	0	0	0	-140	--	--	16.08	16.08	0.29	0.00	0.01	0.07	0.00	0.00	20.9
17	51	-0	-1007	0	0	0	-90	--	--	16.08	16.08	0.29	0.00	0.01	0.06	0.00	0.00	20.9
18	51	-0	-1752	0	0	0	24	--	--	16.08	16.08	0.00	0.00	0.01	0.11	0.00	0.00	20.9
19	51	-0	-1368	0	0	0	-230	--	--	16.08	16.08	0.18	0.00	0.01	0.09	0.00	0.00	20.9
20	51	-0	-1585	0	0	0	-65	--	--	16.08	16.08	0.18	0.00	0.01	0.10	0.00	0.00	20.9
37	51	-0	-1801	0	0	0	95	--	--	16.08	16.08	0.00	0.00	0.01	0.11	0.00	0.00	20.9
38	51	-0	-1161	0	0	0	-329	--	--	16.08	16.08	0.18	0.01	0.01	0.07	0.00	0.00	20.9
39	51	-0	-1522	0	0	0	-54	--	--	16.08	16.08	0.18	0.00	0.01	0.10	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 140 NI 1270 NF 1306 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-1937	0	0	0	420	--	--	16.08	16.08	0.00	0.01	0.02	0.12	0.00	0.00	20.9
2	0	-0	-1548	0	0	0	357	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
3	0	-0	-1528	0	0	0	367	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
4	0	-0	-1452	0	0	0	279	--	--	16.08	16.08	0.10	0.00	0.01	0.09	0.00	0.00	20.9
5	0	-0	-1432	0	0	0	289	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
6	0	-0	-1537	0	0	0	318	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
7	0	-0	-1472	0	0	0	351	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
8	0	-0	-1508	0	0	0	295	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
9	0	-0	-1443	0	0	0	327	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
10	0	-0	-1548	0	0	0	357	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
11	0	-0	-1528	0	0	0	367	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
12	0	-0	-1452	0	0	0	279	--	--	16.08	16.08	0.10	0.00	0.01	0.09	0.00	0.00	20.9
13	0	-0	-1432	0	0	0	289	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
14	0	-0	-1537	0	0	0	318	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
15	0	-0	-1472	0	0	0	351	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
16	0	-0	-1508	0	0	0	295	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
17	0	-0	-1443	0	0	0	327	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
18	0	-0	-2273	0	0	0	618	--	--	16.08	16.08	0.00	0.01	0.02	0.14	0.00	0.00	20.9
19	0	-0	-1976	0	0	0	394	--	--	16.08	16.08	0.00	0.01	0.02	0.12	0.00	0.00	20.9
20	0	-0	-2142	0	0	0	547	--	--	16.08	16.08	0.00	0.01	0.02	0.13	0.00	0.00	20.9
37	0	-0	-2285	0	0	0	652	--	--	16.08	16.08	0.00	0.01	0.02	0.14	0.00	0.00	20.9
38	0	-0	-1789	0	0	0	279	--	--	16.08	16.08	0.00	0.00	0.01	0.11	0.00	0.00	20.9
39	0	-0	-2066	0	0	0	533	--	--	16.08	16.08	0.00	0.01	0.02	0.13	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	-1937	0	0	0	-575	--	--	16.08	16.08	0.18	0.01	0.02	0.12	0.00	0.00	20.9
2	26	-0	-1548	0	0	0	-438	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
3	26	-0	-1528	0	0	0	-418	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
4	26	-0	-1452	0	0	0	-467	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
5	26	-0	-1432	0	0	0	-447	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
6	26	-0	-1537	0	0	0	-471	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
7	26	-0	-1472	0	0	0	-405	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
8	26	-0	-1508	0	0	0	-480	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
9	26	-0	-1443	0	0	0	-414	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
10	26	-0	-1548	0	0	0	-438	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
11	26	-0	-1528	0	0	0	-418	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
12	26	-0	-1452	0	0	0	-467	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
13	26	-0	-1432	0	0	0	-447	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
14	26	-0	-1537	0	0	0	-471	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
15	26	-0	-1472	0	0	0	-405	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
16	26	-0	-1508	0	0	0	-480	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
17	26	-0	-1443	0	0	0	-414	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
18	26	-0	-2273	0	0	0	618	--	--	16.08	16.08	0.00	0.01	0.02	0.14	0.00	0.00	20.9
19	26	-0	-1976	0	0	0	-621	--	--	16.08	16.08	0.18	0.01	0.02	0.12	0.00	0.00	20.9
20	26	-0	-2142	0	0	0	-554	--	--	16.08	16.08	0.18	0.01	0.02	0.13	0.00	0.00	20.9
37	26	-0	-2285	0	0	0	652	--	--	16.08	16.08	0.00	0.01	0.02	0.14	0.00	0.00	20.9
38	26	-0	-1789	0	0	0	-640	--	--	16.08	16.08	0.18	0.01	0.01	0.11	0.00	0.00	20.9
39	26	-0	-2066	0	0	0	533	--	--	16.08	16.08	0.00	0.01	0.02	0.13	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	-1937	0	0	0	-575	--	--	16.08	16.08	0.18	0.01	0.02	0.12	0.00	0.00	20.9
2	51	-0	-1548	0	0	0	-438	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9

3	51	-0	-1528	0	0	0	-418	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
4	51	-0	-1452	0	0	0	-467	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
5	51	-0	-1432	0	0	0	-447	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
6	51	-0	-1537	0	0	0	-471	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
7	51	-0	-1472	0	0	0	-405	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
8	51	-0	-1508	0	0	0	-480	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
9	51	-0	-1443	0	0	0	-414	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
10	51	-0	-1548	0	0	0	-438	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
11	51	-0	-1528	0	0	0	-418	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
12	51	-0	-1452	0	0	0	-467	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
13	51	-0	-1432	0	0	0	-447	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
14	51	-0	-1537	0	0	0	-471	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
15	51	-0	-1472	0	0	0	-405	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
16	51	-0	-1508	0	0	0	-480	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
17	51	-0	-1443	0	0	0	-414	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
18	51	-0	-2273	0	0	0	-550	--	--	16.08	16.08	0.18	0.01	0.02	0.14	0.00	0.00	20.9
19	51	-0	-1976	0	0	0	-621	--	--	16.08	16.08	0.18	0.01	0.02	0.12	0.00	0.00	20.9
20	51	-0	-2142	0	0	0	-554	--	--	16.08	16.08	0.18	0.01	0.02	0.13	0.00	0.00	20.9
37	51	-0	-2285	0	0	0	-521	--	--	16.08	16.08	0.18	0.01	0.02	0.14	0.00	0.00	20.9
38	51	-0	-1789	0	0	0	-640	--	--	16.08	16.08	0.18	0.01	0.01	0.11	0.00	0.00	20.9
39	51	-0	-2066	0	0	0	-528	--	--	16.08	16.08	0.18	0.01	0.02	0.13	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 141 NI 1306 NF 1305 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-1628	0	0	0	53	--	--	16.08	16.08	0.00	0.00	0.01	0.10	0.00	0.00	20.9
2	0	-0	-1314	0	0	0	63	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
3	0	-0	-1298	0	0	0	77	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
4	0	-0	-1207	0	0	0	4	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
5	0	-0	-1192	0	0	0	18	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
6	0	-0	-1295	0	0	0	26	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
7	0	-0	-1242	0	0	0	73	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
8	0	-0	-1263	0	0	0	8	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
9	0	-0	-1211	0	0	0	55	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
10	0	-0	-1314	0	0	0	63	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
11	0	-0	-1298	0	0	0	77	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
12	0	-0	-1207	0	0	0	4	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
13	0	-0	-1192	0	0	0	18	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
14	0	-0	-1295	0	0	0	26	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
15	0	-0	-1242	0	0	0	73	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
16	0	-0	-1263	0	0	0	8	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
17	0	-0	-1211	0	0	0	55	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
18	0	-0	-1939	0	0	0	180	--	--	16.08	16.08	0.00	0.00	0.02	0.12	0.00	0.00	20.9
19	0	-0	-1615	0	0	0	16	--	--	16.08	16.08	0.00	0.00	0.01	0.10	0.00	0.00	20.9
20	0	-0	-1785	0	0	0	134	--	--	16.08	16.08	0.00	0.00	0.01	0.11	0.00	0.00	20.9
37	0	-0	-1977	0	0	0	213	--	--	16.08	16.08	0.00	0.00	0.02	0.12	0.00	0.00	20.9
38	0	-0	-1436	0	0	0	-798	--	--	16.08	16.08	0.18	0.01	0.01	0.09	0.00	0.00	20.9
39	0	-0	-1721	0	0	0	137	--	--	16.08	16.08	0.00	0.00	0.01	0.11	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	-1628	0	0	0	-784	--	--	16.08	16.08	0.18	0.01	0.01	0.10	0.00	0.00	20.9
2	26	-0	-1314	0	0	0	-612	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
3	26	-0	-1298	0	0	0	-589	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
4	26	-0	-1207	0	0	0	-616	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
5	26	-0	-1192	0	0	0	-594	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
6	26	-0	-1295	0	0	0	-639	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
7	26	-0	-1242	0	0	0	-565	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
8	26	-0	-1263	0	0	0	-640	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
9	26	-0	-1211	0	0	0	-567	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
10	26	-0	-1314	0	0	0	-612	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
11	26	-0	-1298	0	0	0	-589	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
12	26	-0	-1207	0	0	0	-616	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
13	26	-0	-1192	0	0	0	-594	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
14	26	-0	-1295	0	0	0	-639	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
15	26	-0	-1242	0	0	0	-565	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
16	26	-0	-1263	0	0	0	-640	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
17	26	-0	-1211	0	0	0	-567	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
18	26	-0	-1939	0	0	0	-816	--	--	16.08	16.08	0.18	0.01	0.02	0.12	0.00	0.00	20.9
19	26	-0	-1615	0	0	0	-813	--	--	16.08	16.08	0.18	0.01	0.01	0.10	0.00	0.00	20.9
20	26	-0	-1785	0	0	0	-783	--	--	16.08	16.08	0.18	0.01	0.01	0.11	0.00	0.00	20.9
37	26	-0	-1977	0	0	0	-802	--	--	16.08	16.08	0.18	0.01	0.02	0.12	0.00	0.00	20.9
38	26	-0	-1436	0	0	0	-798	--	--	16.08	16.08	0.18	0.01	0.01	0.09	0.00	0.00	20.9
39	26	-0	-1721	0	0	0	-747	--	--	16.08	16.08	0.18	0.01	0.01	0.11	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	-1628	0	0	0	-784	--	--	16.08	16.08	0.18	0.01	0.01	0.10	0.00	0.00	20.9
2	51	-0	-1314	0	0	0	-612	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
3	51	-0	-1298	0	0	0	-589	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
4	51	-0	-1207	0	0	0	-616	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
5	51	-0	-1192	0	0	0	-594	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
6	51	-0	-1295	0	0	0	-639	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
7	51	-0	-1242	0	0	0	-565	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
8	51	-0	-1263	0	0	0	-640	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
9	51	-0	-1211	0	0	0	-567	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
10	51	-0	-1314	0	0	0	-612	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
11	51	-0	-1298	0	0	0	-589	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
12	51	-0	-1207	0	0	0	-616	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
13	51	-0	-1192	0	0	0	-594	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
14	51	-0	-1295	0	0	0	-639	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
15	51	-0	-1242	0	0	0	-565	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
16	51	-0	-1263	0	0	0	-640	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
17	51	-0	-1211	0	0	0	-567	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
18	51	-0	-1939	0	0	0	-816	--	--	16.08	16.08	0.18	0.01	0.02	0.12	0.00	0.00	20.9
19	51	-0	-1615	0	0	0	-813	--	--	16.08	16.08	0.18	0.01	0.01	0.10	0.00	0.00	20.9
20	51	-0	-1785	0	0	0	-783	--	--	16.08	16.08	0.18	0.01	0.01	0.11	0.00	0.00	20.9
37	51	-0	-1977	0	0	0	-802	--	--	16.08	16.08	0.18	0.01	0.02	0.12	0.00	0.00	20.9
38	51	-0	-1436	0	0	0	-798	--	--	16.08	16.08	0.18	0.01	0.01	0.09	0.00	0.00	20.9
39	51	-0	-1721	0	0	0	-747	--	--	16.08	16.08	0.18	0.01	0.01	0.11	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 142 NI 1305 NF 1304 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-991	0	0	0	-914	--	--	16.08	16.08	0.18	0.02	0.01	0.06	0.00	0.00	20.9
2	0	-0	-821	0	0	0	-723	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
3	0	-0	-810	0	0	0	-699	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
4	0	-0	-715	0	0	0	-707	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
5	0	-0	-703	0	0	0	-683	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
6	0	-0	-797	0	0	0	-745	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
7	0	-0	-759	0	0	0	-666	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
8	0	-0	-765	0	0	0	-740	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
9	0	-0	-727	0	0	0	-661	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
10	0	-0	-821	0	0	0	-723	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
11	0	-0	-810	0	0	0	-699	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
12	0	-0	-715	0	0	0	-707	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
13	0	-0	-703	0	0	0	-683	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
14	0	-0	-797	0	0	0	-745	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
15	0	-0	-759	0	0	0	-666	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
16	0	-0	-765	0	0	0	-740	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
17	0	-0	-727	0	0	0	-661	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
18	0	-0	-1246	0	0	0	-989	--	--	16.08	16.08	0.18	0.02	0.01	0.08	0.00	0.00	20.9
19	0	-0	-922	0	0	0	-924	--	--	16.08	16.08	0.18	0.02	0.01	0.06	0.00	0.00	20.9
20	0	-0	-1080	0	0	0	-923	--	--	16.08	16.08	0.18	0.02	0.01	0.07	0.00	0.00	20.9
37	0	-0	-1310	0	0	0	-991	--	--	16.08	16.08	0.18	0.02	0.01	0.08	0.00	0.00	20.9
38	0	-0	-770	0	0	0	-883	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9
39	0	-0	-1034	0	0	0	-880	--	--	16.08	16.08	0.18	0.01	0.01	0.06	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	26	-0	-991	0	0	0	-914	--	--	16.08	16.08	0.18	0.02	0.01	0.06	0.00	0.00	20.9
2	26	-0	-821	0	0	0	-723	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
3	26	-0	-810	0	0	0	-699	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
4	26	-0	-715	0	0	0	-707	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
5	26	-0	-703	0	0	0	-683	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
6	26	-0	-797	0	0	0	-745	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
7	26	-0	-759	0	0	0	-666	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
8	26	-0	-765	0	0	0	-740	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
9	26	-0	-727	0	0	0	-661	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
10	26	-0	-821	0	0	0	-723	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
11	26	-0	-810	0	0	0	-699	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
12	26	-0	-715	0	0	0	-707	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
13	26	-0	-703	0	0	0	-683	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
14	26	-0	-797	0	0	0	-745	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
15	26	-0	-759	0	0	0	-666	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
16	26	-0	-765	0	0	0	-740	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
17	26	-0	-727	0	0	0	-661	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
18	26	-0	-1246	0	0	0	-989	--	--	16.08	16.08	0.18	0.02	0.01	0.08	0.00	0.00	20.9
19	26	-0	-922	0	0	0	-924	--	--	16.08	16.08	0.18	0.02	0.01	0.06	0.00	0.00	20.9
20	26	-0	-1080	0	0	0	-923	--	--	16.08	16.08	0.18	0.02	0.01	0.07	0.00	0.00	20.9
37	26	-0	-1310	0	0	0	-991	--	--	16.08	16.08	0.18	0.02	0.01	0.08	0.00	0.00	20.9
38	26	-0	-770	0	0	0	-883	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9
39	26	-0	-1034	0	0	0	-880	--	--	16.08	16.08	0.18	0.01	0.01	0.06	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	51	-0	-991	0	0	0	-914	--	--	16.08	16.08	0.18	0.02	0.01	0.06	0.00	0.00	20.9
2	51	-0	-821	0	0	0	-723	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
3	51	-0	-810	0	0	0	-699	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
4	51	-0	-715	0	0	0	-707	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
5	51	-0	-703	0	0	0	-683	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
6	51	-0	-797	0	0	0	-745	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
7	51	-0	-759	0	0	0	-666	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
8	51	-0	-765	0	0	0	-740	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
9	51	-0	-727	0	0	0	-661	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
10	51	-0	-821	0	0	0	-723	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
11	51	-0	-810	0	0	0	-699	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
12	51	-0	-715	0	0	0	-707	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
13	51	-0	-703	0	0	0	-683	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
14	51	-0	-797	0	0	0	-745	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
15	51	-0	-759	0	0	0	-666	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
16	51	-0	-765	0	0	0	-740	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
17	51	-0	-727	0	0	0	-661	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
18	51	-0	-1246	0	0	0	-989	--	--	16.08	16.08	0.18	0.02	0.01	0.08	0.00	0.00	20.9
19	51	-0	-922	0	0	0	-924	--	--	16.08	16.08	0.18	0.02	0.01	0.06	0.00	0.00	20.9
20	51	-0	-1080	0	0	0	-923	--	--	16.08	16.08	0.18	0.02	0.01	0.07	0.00	0.00	20.9
37	51	-0	-1310	0	0	0	-991	--	--	16.08	16.08	0.18	0.02	0.01	0.08	0.00	0.00	20.9
38	51	-0	-770	0	0	0	-883	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9
39	51	-0	-1034	0	0	0	-880	--	--	16.08	16.08	0.18	0.01	0.01	0.06	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 143 NI 1304 NF 1261 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-429	0	0	0	-922	--	--	16.08	16.08	0.18	0.02	0.00	0.03	0.00	0.00	20.9
2	0	-0	-387	0	0	0	-740	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
3	0	-0	-380	0	0	0	-715	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
4	0	-0	-281	0	0	0	-704	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
5	0	-0	-274	0	0	0	-680	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
6	0	-0	-358	0	0	0	-756	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
7	0	-0	-334	0	0	0	-675	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
8	0	-0	-327	0	0	0	-745	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
9	0	-0	-302	0	0	0	-664	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
10	0	-0	-387	0	0	0	-740	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9

11	0	-0	-380	0	0	0	-715	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
12	0	-0	-281	0	0	0	-704	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
13	0	-0	-274	0	0	0	-680	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
14	0	-0	-358	0	0	0	-756	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
15	0	-0	-334	0	0	0	-675	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
16	0	-0	-327	0	0	0	-745	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
17	0	-0	-302	0	0	0	-664	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
18	0	-0	-634	0	0	0	-1029	--	--	16.08	16.08	0.18	0.02	0.01	0.04	0.00	0.00	20.9
19	0	-0	-314	0	0	0	-905	--	--	16.08	16.08	0.18	0.01	0.00	0.02	0.00	0.00	20.9
20	0	-0	-460	0	0	0	-929	--	--	16.08	16.08	0.18	0.02	0.00	0.03	0.00	0.00	20.9
37	0	-0	-719	0	0	0	-1050	--	--	16.08	16.08	0.18	0.02	0.01	0.05	0.00	0.00	20.9
38	0	-0	-186	0	0	0	-842	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9
39	0	-0	-429	0	0	0	-883	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	-429	0	0	0	-922	--	--	16.08	16.08	0.18	0.02	0.00	0.03	0.00	0.00	20.9
2	26	-0	-387	0	0	0	-740	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
3	26	-0	-380	0	0	0	-715	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
4	26	-0	-281	0	0	0	-704	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
5	26	-0	-274	0	0	0	-680	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
6	26	-0	-358	0	0	0	-756	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
7	26	-0	-334	0	0	0	-675	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
8	26	-0	-327	0	0	0	-745	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
9	26	-0	-302	0	0	0	-664	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
10	26	-0	-387	0	0	0	-740	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
11	26	-0	-380	0	0	0	-715	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
12	26	-0	-281	0	0	0	-704	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
13	26	-0	-274	0	0	0	-680	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
14	26	-0	-358	0	0	0	-756	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
15	26	-0	-334	0	0	0	-675	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
16	26	-0	-327	0	0	0	-745	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
17	26	-0	-302	0	0	0	-664	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
18	26	-0	-634	0	0	0	-1029	--	--	16.08	16.08	0.18	0.02	0.01	0.04	0.00	0.00	20.9
19	26	-0	-314	0	0	0	-905	--	--	16.08	16.08	0.18	0.01	0.00	0.02	0.00	0.00	20.9
20	26	-0	-460	0	0	0	-929	--	--	16.08	16.08	0.18	0.02	0.00	0.03	0.00	0.00	20.9
37	26	-0	-719	0	0	0	-1050	--	--	16.08	16.08	0.18	0.02	0.01	0.05	0.00	0.00	20.9
38	26	-0	-186	0	0	0	-842	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9
39	26	-0	-429	0	0	0	-883	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	-429	0	0	0	-922	--	--	16.08	16.08	0.18	0.02	0.00	0.03	0.00	0.00	20.9
2	51	-0	-387	0	0	0	-740	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
3	51	-0	-380	0	0	0	-715	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
4	51	-0	-281	0	0	0	-704	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
5	51	-0	-274	0	0	0	-680	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
6	51	-0	-358	0	0	0	-756	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
7	51	-0	-334	0	0	0	-675	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
8	51	-0	-327	0	0	0	-745	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
9	51	-0	-302	0	0	0	-664	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
10	51	-0	-387	0	0	0	-740	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
11	51	-0	-380	0	0	0	-715	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
12	51	-0	-281	0	0	0	-704	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
13	51	-0	-274	0	0	0	-680	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
14	51	-0	-358	0	0	0	-756	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
15	51	-0	-334	0	0	0	-675	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
16	51	-0	-327	0	0	0	-745	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
17	51	-0	-302	0	0	0	-664	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
18	51	-0	-634	0	0	0	-1029	--	--	16.08	16.08	0.18	0.02	0.01	0.04	0.00	0.00	20.9
19	51	-0	-314	0	0	0	-905	--	--	16.08	16.08	0.18	0.01	0.00	0.02	0.00	0.00	20.9
20	51	-0	-460	0	0	0	-929	--	--	16.08	16.08	0.18	0.02	0.00	0.03	0.00	0.00	20.9
37	51	-0	-719	0	0	0	-1050	--	--	16.08	16.08	0.18	0.02	0.01	0.05	0.00	0.00	20.9
38	51	-0	-186	0	0	0	-842	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9
39	51	-0	-429	0	0	0	-883	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 144 NI 1261 NF 1260 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm

1	0	-0	90	0	0	0	-873	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9
2	0	-0	14	0	0	0	-683	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
3	0	-0	18	0	0	0	-660	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
4	0	-0	121	0	0	0	-682	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
5	0	-0	125	0	0	0	-660	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
6	0	-0	48	0	0	0	-709	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
7	0	-0	59	0	0	0	-634	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
8	0	-0	80	0	0	0	-709	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
9	0	-0	91	0	0	0	-634	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
10	0	-0	14	0	0	0	-683	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
11	0	-0	18	0	0	0	-660	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
12	0	-0	121	0	0	0	-682	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
13	0	-0	125	0	0	0	-660	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
14	0	-0	48	0	0	0	-709	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
15	0	-0	59	0	0	0	-634	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
16	0	-0	80	0	0	0	-709	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
17	0	-0	91	0	0	0	-634	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
18	0	-0	-72	0	0	0	-956	--	--	16.08	16.08	0.18	0.02	0.00	0.00	0.00	0.00	20.9
19	0	-0	251	0	0	0	-901	--	--	16.08	16.08	0.18	0.01	0.00	0.02	0.00	0.00	20.9
20	0	-0	114	0	0	0	-879	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9
37	0	-0	-179	0	0	0	-1000	--	--	16.08	16.08	0.18	0.02	0.00	0.01	0.00	0.00	20.9
38	0	-0	360	0	0	0	-877	--	--	16.08	16.08	0.18	0.01	0.00	0.02	0.00	0.00	20.9
39	0	-0	130	0	0	0	-840	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	90	0	0	0	-873	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9
2	26	-0	14	0	0	0	-683	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
3	26	-0	18	0	0	0	-660	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
4	26	-0	121	0	0	0	-682	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
5	26	-0	125	0	0	0	-660	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
6	26	-0	48	0	0	0	-709	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9

7	26	-0	59	0	0	0	-634	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
8	26	-0	80	0	0	0	-709	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
9	26	-0	91	0	0	0	-634	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
10	26	-0	14	0	0	0	-683	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
11	26	-0	18	0	0	0	-660	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
12	26	-0	121	0	0	0	-682	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
13	26	-0	125	0	0	0	-660	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
14	26	-0	48	0	0	0	-709	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
15	26	-0	59	0	0	0	-634	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
16	26	-0	80	0	0	0	-709	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
17	26	-0	91	0	0	0	-634	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
18	26	-0	-72	0	0	0	-956	--	--	16.08	16.08	0.18	0.02	0.00	0.00	0.00	0.00	20.9
19	26	-0	251	0	0	0	-901	--	--	16.08	16.08	0.18	0.01	0.00	0.02	0.00	0.00	20.9
20	26	-0	114	0	0	0	-879	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9
37	26	-0	-179	0	0	0	-1000	--	--	16.08	16.08	0.18	0.02	0.00	0.01	0.00	0.00	20.9
38	26	-0	360	0	0	0	-877	--	--	16.08	16.08	0.18	0.01	0.00	0.02	0.00	0.00	20.9
39	26	-0	130	0	0	0	-840	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	90	0	0	0	-873	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9
2	51	-0	14	0	0	0	-683	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
3	51	-0	18	0	0	0	-660	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
4	51	-0	121	0	0	0	-682	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
5	51	-0	125	0	0	0	-660	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
6	51	-0	48	0	0	0	-709	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
7	51	-0	59	0	0	0	-634	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
8	51	-0	80	0	0	0	-709	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
9	51	-0	91	0	0	0	-634	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
10	51	-0	14	0	0	0	-683	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
11	51	-0	18	0	0	0	-660	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
12	51	-0	121	0	0	0	-682	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
13	51	-0	125	0	0	0	-660	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
14	51	-0	48	0	0	0	-709	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
15	51	-0	59	0	0	0	-634	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
16	51	-0	80	0	0	0	-709	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
17	51	-0	91	0	0	0	-634	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
18	51	-0	-72	0	0	0	-956	--	--	16.08	16.08	0.18	0.02	0.00	0.00	0.00	0.00	20.9
19	51	-0	251	0	0	0	-901	--	--	16.08	16.08	0.18	0.01	0.00	0.02	0.00	0.00	20.9
20	51	-0	114	0	0	0	-879	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9
37	51	-0	-179	0	0	0	-1000	--	--	16.08	16.08	0.18	0.02	0.00	0.01	0.00	0.00	20.9
38	51	-0	360	0	0	0	-877	--	--	16.08	16.08	0.18	0.01	0.00	0.02	0.00	0.00	20.9
39	51	-0	130	0	0	0	-840	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 145 NI 1260 NF 1271 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	610	0	0	0	-938	--	--	16.08	16.08	0.18	0.02	0.01	0.04	0.00	0.00	20.9
2	0	-0	414	0	0	0	-743	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
3	0	-0	414	0	0	0	-719	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
4	0	-0	525	0	0	0	-724	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
5	0	-0	524	0	0	0	-700	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
6	0	-0	454	0	0	0	-764	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
7	0	-0	452	0	0	0	-685	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
8	0	-0	487	0	0	0	-758	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
9	0	-0	484	0	0	0	-679	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
10	0	-0	414	0	0	0	-743	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
11	0	-0	414	0	0	0	-719	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
12	0	-0	525	0	0	0	-724	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
13	0	-0	524	0	0	0	-700	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
14	0	-0	454	0	0	0	-764	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
15	0	-0	452	0	0	0	-685	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
16	0	-0	487	0	0	0	-758	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
17	0	-0	484	0	0	0	-679	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
18	0	-0	488	0	0	0	-1020	--	--	16.08	16.08	0.18	0.02	0.00	0.03	0.00	0.00	20.9
19	0	-0	820	0	0	0	-945	--	--	16.08	16.08	0.18	0.02	0.01	0.05	0.00	0.00	20.9
20	0	-0	686	0	0	0	-948	--	--	16.08	16.08	0.18	0.02	0.01	0.04	0.00	0.00	20.9
37	0	-0	357	0	0	0	-1024	--	--	16.08	16.08	0.18	0.02	0.00	0.02	0.00	0.00	20.9
38	0	-0	910	0	0	0	-898	--	--	16.08	16.08	0.18	0.01	0.01	0.06	0.00	0.00	20.9
39	0	-0	687	0	0	0	-904	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	610	0	0	0	-938	--	--	16.08	16.08	0.18	0.02	0.01	0.04	0.00	0.00	20.9
2	26	-0	414	0	0	0	-743	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
3	26	-0	414	0	0	0	-719	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
4	26	-0	525	0	0	0	-724	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
5	26	-0	524	0	0	0	-700	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
6	26	-0	454	0	0	0	-764	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
7	26	-0	452	0	0	0	-685	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
8	26	-0	487	0	0	0	-758	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
9	26	-0	484	0	0	0	-679	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
10	26	-0	414	0	0	0	-743	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
11	26	-0	414	0	0	0	-719	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
12	26	-0	525	0	0	0	-724	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
13	26	-0	524	0	0	0	-700	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
14	26	-0	454	0	0	0	-764	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
15	26	-0	452	0	0	0	-685	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
16	26	-0	487	0	0	0	-758	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
17	26	-0	484	0	0	0	-679	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
18	26	-0	488	0	0	0	-1020	--	--	16.08	16.08	0.18	0.02	0.00	0.03	0.00	0.00	20.9
19	26	-0	820	0	0	0	-945	--	--	16.08	16.08	0.18	0.02	0.01	0.05	0.00	0.00	20.9
20	26	-0	686	0	0	0	-948	--	--	16.08	16.08	0.18	0.02	0.01	0.04	0.00	0.00	20.9
37	26	-0	357	0	0	0	-1024	--	--	16.08	16.08	0.18	0.02	0.00	0.02	0.00	0.00	20.9
38	26	-0	910	0	0	0	-898	--	--	16.08	16.08	0.18	0.01	0.01	0.06	0.00	0.00	20.9
39	26	-0	687	0	0	0	-904	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	610	0	0	0	-938	--	--	16.08	16.08	0.18	0.02	0.01	0.04	0.00	0.00	20.9
2	51	-0	414	0	0	0	-743	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9

3	51	-0	414	0	0	0	-719	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
4	51	-0	525	0	0	0	-724	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
5	51	-0	524	0	0	0	-700	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
6	51	-0	454	0	0	0	-764	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
7	51	-0	452	0	0	0	-685	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
8	51	-0	487	0	0	0	-758	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
9	51	-0	484	0	0	0	-679	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
10	51	-0	414	0	0	0	-743	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
11	51	-0	414	0	0	0	-719	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
12	51	-0	525	0	0	0	-724	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
13	51	-0	524	0	0	0	-700	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
14	51	-0	454	0	0	0	-764	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
15	51	-0	452	0	0	0	-685	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
16	51	-0	487	0	0	0	-758	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
17	51	-0	484	0	0	0	-679	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
18	51	-0	488	0	0	0	-1020	--	--	16.08	16.08	0.18	0.02	0.00	0.03	0.00	0.00	20.9
19	51	-0	820	0	0	0	-945	--	--	16.08	16.08	0.18	0.02	0.01	0.05	0.00	0.00	20.9
20	51	-0	686	0	0	0	-948	--	--	16.08	16.08	0.18	0.02	0.01	0.04	0.00	0.00	20.9
37	51	-0	357	0	0	0	-1024	--	--	16.08	16.08	0.18	0.02	0.00	0.02	0.00	0.00	20.9
38	51	-0	910	0	0	0	-898	--	--	16.08	16.08	0.18	0.01	0.01	0.06	0.00	0.00	20.9
39	51	-0	687	0	0	0	-904	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 146 NI 1271 NF 1308 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	1172	0	0	0	-899	--	--	16.08	16.08	0.18	0.01	0.01	0.07	0.00	0.00	20.9
2	0	-0	847	0	0	0	-723	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
3	0	-0	842	0	0	0	-699	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
4	0	-0	961	0	0	0	-685	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
5	0	-0	956	0	0	0	-660	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
6	0	-0	893	0	0	0	-738	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
7	0	-0	876	0	0	0	-657	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
8	0	-0	927	0	0	0	-727	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
9	0	-0	910	0	0	0	-645	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
10	0	-0	847	0	0	0	-723	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
11	0	-0	842	0	0	0	-699	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
12	0	-0	961	0	0	0	-685	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
13	0	-0	956	0	0	0	-660	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
14	0	-0	893	0	0	0	-738	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
15	0	-0	876	0	0	0	-657	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
16	0	-0	927	0	0	0	-727	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
17	0	-0	910	0	0	0	-645	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
18	0	-0	1090	0	0	0	-1009	--	--	16.08	16.08	0.18	0.02	0.01	0.07	0.00	0.00	20.9
19	0	-0	1433	0	0	0	-875	--	--	16.08	16.08	0.18	0.01	0.01	0.09	0.00	0.00	20.9
20	0	-0	1302	0	0	0	-903	--	--	16.08	16.08	0.18	0.01	0.01	0.08	0.00	0.00	20.9
37	0	-0	933	0	0	0	-1034	--	--	16.08	16.08	0.18	0.02	0.01	0.06	0.00	0.00	20.9
38	0	-0	1506	0	0	0	-810	--	--	16.08	16.08	0.18	0.01	0.01	0.09	0.00	0.00	20.9
39	0	-0	1286	0	0	0	-857	--	--	16.08	16.08	0.18	0.01	0.01	0.08	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	1172	0	0	0	-899	--	--	16.08	16.08	0.18	0.01	0.01	0.07	0.00	0.00	20.9
2	26	-0	847	0	0	0	-723	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
3	26	-0	842	0	0	0	-699	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
4	26	-0	961	0	0	0	-685	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
5	26	-0	956	0	0	0	-660	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
6	26	-0	893	0	0	0	-738	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
7	26	-0	876	0	0	0	-657	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
8	26	-0	927	0	0	0	-727	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
9	26	-0	910	0	0	0	-645	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
10	26	-0	847	0	0	0	-723	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
11	26	-0	842	0	0	0	-699	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
12	26	-0	961	0	0	0	-685	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
13	26	-0	956	0	0	0	-660	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
14	26	-0	893	0	0	0	-738	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
15	26	-0	876	0	0	0	-657	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
16	26	-0	927	0	0	0	-727	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
17	26	-0	910	0	0	0	-645	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
18	26	-0	1090	0	0	0	-1009	--	--	16.08	16.08	0.18	0.02	0.01	0.07	0.00	0.00	20.9
19	26	-0	1433	0	0	0	-875	--	--	16.08	16.08	0.18	0.01	0.01	0.09	0.00	0.00	20.9
20	26	-0	1302	0	0	0	-903	--	--	16.08	16.08	0.18	0.01	0.01	0.08	0.00	0.00	20.9
37	26	-0	933	0	0	0	-1034	--	--	16.08	16.08	0.18	0.02	0.01	0.06	0.00	0.00	20.9
38	26	-0	1506	0	0	0	-810	--	--	16.08	16.08	0.18	0.01	0.01	0.09	0.00	0.00	20.9
39	26	-0	1286	0	0	0	-857	--	--	16.08	16.08	0.18	0.01	0.01	0.08	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	1172	0	0	0	-899	--	--	16.08	16.08	0.18	0.01	0.01	0.07	0.00	0.00	20.9
2	51	-0	847	0	0	0	-723	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
3	51	-0	842	0	0	0	-699	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
4	51	-0	961	0	0	0	-685	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
5	51	-0	956	0	0	0	-660	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
6	51	-0	893	0	0	0	-738	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
7	51	-0	876	0	0	0	-657	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
8	51	-0	927	0	0	0	-727	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
9	51	-0	910	0	0	0	-645	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
10	51	-0	847	0	0	0	-723	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
11	51	-0	842	0	0	0	-699	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
12	51	-0	961	0	0	0	-685	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
13	51	-0	956	0	0	0	-660	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
14	51	-0	893	0	0	0	-738	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
15	51	-0	876	0	0	0	-657	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
16	51	-0	927	0	0	0	-727	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
17	51	-0	910	0	0	0	-645	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
18	51	-0	1090	0	0	0	-1009	--	--	16.08	16.08	0.18	0.02	0.01	0.07	0.00	0.00	20.9
19	51	-0	1433	0	0	0	-875	--	--	16.08	16.08	0.18	0.01	0.01	0.09	0.00	0.00	20.9
20	51	-0	1302	0	0	0	-903	--	--	16.08	16.08	0.18	0.01	0.01	0.08	0.00	0.00	20.9
37	51	-0	933	0	0	0	-1034	--	--	16.08	16.08	0.18	0.02	0.01	0.06	0.00	0.00	20.9
38	51	-0	1506	0	0	0	-810	--	--	16.08	16.08	0.18	0.01	0.01	0.09	0.00	0.00	20.9
39	51	-0	1286	0	0	0	-857	--	--	16.08	16.08	0.18	0.01	0.01	0.08	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 147 NI 1308 NF 1307 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	1805	0	0	0	-741	--	--	16.08	16.08	0.18	0.01	0.01	0.11	0.00	0.00	20.9
2	0	-0	1338	0	0	0	-611	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
3	0	-0	1329	0	0	0	-587	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
4	0	-0	1448	0	0	0	-554	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
5	0	-0	1438	0	0	0	-529	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
6	0	-0	1388	0	0	0	-619	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
7	0	-0	1355	0	0	0	-538	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
8	0	-0	1421	0	0	0	-602	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
9	0	-0	1388	0	0	0	-521	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
10	0	-0	1338	0	0	0	-611	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
11	0	-0	1329	0	0	0	-587	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
12	0	-0	1448	0	0	0	-554	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
13	0	-0	1438	0	0	0	-529	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
14	0	-0	1388	0	0	0	-619	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
15	0	-0	1355	0	0	0	-538	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
16	0	-0	1421	0	0	0	-602	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
17	0	-0	1388	0	0	0	-521	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
18	0	-0	1778	0	0	0	-868	--	--	16.08	16.08	0.18	0.01	0.01	0.11	0.00	0.00	20.9
19	0	-0	2108	0	0	0	-678	--	--	16.08	16.08	0.18	0.01	0.02	0.13	0.00	0.00	20.9
20	0	-0	1992	0	0	0	-727	--	--	16.08	16.08	0.18	0.01	0.02	0.12	0.00	0.00	20.9
37	0	-0	1602	0	0	0	-917	--	--	16.08	16.08	0.18	0.02	0.01	0.10	0.00	0.00	20.9
38	0	-0	2152	0	0	0	-599	--	--	16.08	16.08	0.18	0.01	0.02	0.14	0.00	0.00	20.9
39	0	-0	1959	0	0	0	-681	--	--	16.08	16.08	0.18	0.01	0.02	0.12	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	1805	0	0	0	-741	--	--	16.08	16.08	0.18	0.01	0.01	0.11	0.00	0.00	20.9
2	26	-0	1338	0	0	0	-611	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
3	26	-0	1329	0	0	0	-587	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
4	26	-0	1448	0	0	0	-554	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
5	26	-0	1438	0	0	0	-529	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
6	26	-0	1388	0	0	0	-619	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
7	26	-0	1355	0	0	0	-538	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
8	26	-0	1421	0	0	0	-602	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
9	26	-0	1388	0	0	0	-521	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
10	26	-0	1338	0	0	0	-611	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
11	26	-0	1329	0	0	0	-587	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
12	26	-0	1448	0	0	0	-554	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
13	26	-0	1438	0	0	0	-529	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
14	26	-0	1388	0	0	0	-619	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
15	26	-0	1355	0	0	0	-538	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
16	26	-0	1421	0	0	0	-602	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
17	26	-0	1388	0	0	0	-521	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
18	26	-0	1778	0	0	0	-868	--	--	16.08	16.08	0.18	0.01	0.01	0.11	0.00	0.00	20.9
19	26	-0	2108	0	0	0	-678	--	--	16.08	16.08	0.18	0.01	0.02	0.13	0.00	0.00	20.9
20	26	-0	1992	0	0	0	-727	--	--	16.08	16.08	0.18	0.01	0.02	0.12	0.00	0.00	20.9
37	26	-0	1602	0	0	0	-917	--	--	16.08	16.08	0.18	0.02	0.01	0.10	0.00	0.00	20.9
38	26	-0	2152	0	0	0	-599	--	--	16.08	16.08	0.18	0.01	0.02	0.14	0.00	0.00	20.9
39	26	-0	1959	0	0	0	-681	--	--	16.08	16.08	0.18	0.01	0.02	0.12	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	1805	0	0	0	186	--	--	16.08	16.08	0.00	0.00	0.01	0.11	0.00	0.00	20.9
2	51	-0	1338	0	0	0	77	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
3	51	-0	1329	0	0	0	96	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
4	51	-0	1448	0	0	0	190	--	--	16.08	16.08	0.10	0.00	0.01	0.09	0.00	0.00	20.9
5	51	-0	1438	0	0	0	209	--	--	16.08	16.08	0.10	0.00	0.01	0.09	0.00	0.00	20.9
6	51	-0	1388	0	0	0	94	--	--	16.08	16.08	0.10	0.00	0.01	0.09	0.00	0.00	20.9
7	51	-0	1355	0	0	0	158	--	--	16.08	16.08	0.10	0.00	0.01	0.09	0.00	0.00	20.9
8	51	-0	1421	0	0	0	128	--	--	16.08	16.08	0.10	0.00	0.01	0.09	0.00	0.00	20.9
9	51	-0	1388	0	0	0	192	--	--	16.08	16.08	0.10	0.00	0.01	0.09	0.00	0.00	20.9
10	51	-0	1338	0	0	0	77	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
11	51	-0	1329	0	0	0	96	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
12	51	-0	1448	0	0	0	190	--	--	16.08	16.08	0.10	0.00	0.01	0.09	0.00	0.00	20.9
13	51	-0	1438	0	0	0	209	--	--	16.08	16.08	0.10	0.00	0.01	0.09	0.00	0.00	20.9
14	51	-0	1388	0	0	0	94	--	--	16.08	16.08	0.10	0.00	0.01	0.09	0.00	0.00	20.9
15	51	-0	1355	0	0	0	158	--	--	16.08	16.08	0.10	0.00	0.01	0.09	0.00	0.00	20.9
16	51	-0	1421	0	0	0	128	--	--	16.08	16.08	0.10	0.00	0.01	0.09	0.00	0.00	20.9
17	51	-0	1388	0	0	0	192	--	--	16.08	16.08	0.10	0.00	0.01	0.09	0.00	0.00	20.9
18	51	-0	1778	0	0	0	45	--	--	16.08	16.08	0.00	0.00	0.01	0.11	0.00	0.00	20.9
19	51	-0	2108	0	0	0	405	--	--	16.08	16.08	0.00	0.01	0.02	0.13	0.00	0.00	20.9
20	51	-0	1992	0	0	0	296	--	--	16.08	16.08	0.00	0.01	0.02	0.12	0.00	0.00	20.9
37	51	-0	1602	0	0	0	-917	--	--	16.08	16.08	0.18	0.02	0.01	0.10	0.00	0.00	20.9
38	51	-0	2152	0	0	0	506	--	--	16.08	16.08	0.00	0.01	0.02	0.14	0.00	0.00	20.9
39	51	-0	1959	0	0	0	325	--	--	16.08	16.08	0.00	0.01	0.02	0.12	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 148 NI 1307 NF 1276 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	2138	0	0	0	-500	--	--	16.08	16.08	0.18	0.01	0.02	0.13	0.00	0.00	20.9
2	0	-0	1615	0	0	0	-433	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
3	0	-0	1601	0	0	0	-410	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
4	0	-0	1689	0	0	0	-358	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
5	0	-0	1675	0	0	0	-335	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
6	0	-0	1657	0	0	0	-434	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
7	0	-0	1610	0	0	0	-357	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
8	0	-0	1679	0	0	0	-412	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
9	0	-0	1632	0	0	0	-334	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
10	0	-0	1615	0	0	0	-433	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9

11	0	-0	1601	0	0	0	-410	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
12	0	-0	1689	0	0	0	-358	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
13	0	-0	1675	0	0	0	-335	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
14	0	-0	1657	0	0	0	-434	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
15	0	-0	1610	0	0	0	-357	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
16	0	-0	1679	0	0	0	-412	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
17	0	-0	1632	0	0	0	-334	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
18	0	-0	2189	0	0	0	-636	--	--	16.08	16.08	0.18	0.01	0.02	0.14	0.00	0.00	20.9
19	0	-0	2415	0	0	0	-392	--	--	16.08	16.08	0.18	0.01	0.02	0.15	0.00	0.00	20.9
20	0	-0	2361	0	0	0	-459	--	--	16.08	16.08	0.18	0.01	0.02	0.15	0.00	0.00	20.9
37	0	-0	2034	0	0	0	-711	--	--	16.08	16.08	0.18	0.01	0.02	0.13	0.00	0.00	20.9
38	0	-0	2411	0	0	0	-304	--	--	16.08	16.08	0.18	0.01	0.02	0.15	0.00	0.00	20.9
39	0	-0	2321	0	0	0	-416	--	--	16.08	16.08	0.18	0.01	0.02	0.15	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	2138	0	0	0	2335	--	--	16.08	16.08	0.00	0.04	0.02	0.13	0.00	0.00	20.9
2	26	-0	1615	0	0	0	-433	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
3	26	-0	1601	0	0	0	1712	--	--	16.08	16.08	0.10	0.03	0.01	0.10	0.00	0.00	20.9
4	26	-0	1689	0	0	0	1880	--	--	16.08	16.08	0.10	0.03	0.01	0.11	0.00	0.00	20.9
5	26	-0	1675	0	0	0	1885	--	--	16.08	16.08	0.10	0.03	0.01	0.11	0.00	0.00	20.9
6	26	-0	1657	0	0	0	-434	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
7	26	-0	1610	0	0	0	1777	--	--	16.08	16.08	0.10	0.03	0.01	0.10	0.00	0.00	20.9
8	26	-0	1679	0	0	0	1814	--	--	16.08	16.08	0.10	0.03	0.01	0.11	0.00	0.00	20.9
9	26	-0	1632	0	0	0	1829	--	--	16.08	16.08	0.10	0.03	0.01	0.10	0.00	0.00	20.9
10	26	-0	1615	0	0	0	-433	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
11	26	-0	1601	0	0	0	1712	--	--	16.08	16.08	0.10	0.03	0.01	0.10	0.00	0.00	20.9
12	26	-0	1689	0	0	0	1880	--	--	16.08	16.08	0.10	0.03	0.01	0.11	0.00	0.00	20.9
13	26	-0	1675	0	0	0	1885	--	--	16.08	16.08	0.10	0.03	0.01	0.11	0.00	0.00	20.9
14	26	-0	1657	0	0	0	-434	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
15	26	-0	1610	0	0	0	1777	--	--	16.08	16.08	0.10	0.03	0.01	0.10	0.00	0.00	20.9
16	26	-0	1679	0	0	0	1814	--	--	16.08	16.08	0.10	0.03	0.01	0.11	0.00	0.00	20.9
17	26	-0	1632	0	0	0	1829	--	--	16.08	16.08	0.10	0.03	0.01	0.10	0.00	0.00	20.9
18	26	-0	2189	0	0	0	-636	--	--	16.08	16.08	0.18	0.01	0.02	0.14	0.00	0.00	20.9
19	26	-0	2415	0	0	0	2809	--	--	16.08	16.08	0.00	0.05	0.02	0.15	0.00	0.00	20.9
20	26	-0	2361	0	0	0	2671	--	--	16.08	16.08	0.00	0.05	0.02	0.15	0.00	0.00	20.9
37	26	-0	2034	0	0	0	-711	--	--	16.08	16.08	0.18	0.01	0.02	0.13	0.00	0.00	20.9
38	26	-0	2411	0	0	0	2892	--	--	16.08	16.08	0.00	0.05	0.02	0.15	0.00	0.00	20.9
39	26	-0	2321	0	0	0	2661	--	--	16.08	16.08	0.00	0.05	0.02	0.15	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	2138	0	0	0	599	--	--	16.08	16.08	0.00	0.01	0.02	0.13	0.00	0.00	20.9
2	51	-0	1615	0	0	0	396	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
3	51	-0	1601	0	0	0	412	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
4	51	-0	1689	0	0	0	509	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
5	51	-0	1675	0	0	0	525	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
6	51	-0	1657	0	0	0	417	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
7	51	-0	1610	0	0	0	470	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
8	51	-0	1679	0	0	0	451	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
9	51	-0	1632	0	0	0	504	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
10	51	-0	1615	0	0	0	396	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
11	51	-0	1601	0	0	0	412	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
12	51	-0	1689	0	0	0	509	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
13	51	-0	1675	0	0	0	525	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
14	51	-0	1657	0	0	0	417	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
15	51	-0	1610	0	0	0	470	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
16	51	-0	1679	0	0	0	451	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
17	51	-0	1632	0	0	0	504	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
18	51	-0	2189	0	0	0	489	--	--	16.08	16.08	0.00	0.01	0.02	0.14	0.00	0.00	20.9
19	51	-0	2415	0	0	0	849	--	--	16.08	16.08	0.00	0.01	0.02	0.15	0.00	0.00	20.9
20	51	-0	2361	0	0	0	754	--	--	16.08	16.08	0.00	0.01	0.02	0.15	0.00	0.00	20.9
37	51	-0	2034	0	0	0	334	--	--	16.08	16.08	0.00	0.01	0.02	0.13	0.00	0.00	20.9
38	51	-0	2411	0	0	0	934	--	--	16.08	16.08	0.00	0.02	0.02	0.15	0.00	0.00	20.9
39	51	-0	2321	0	0	0	776	--	--	16.08	16.08	0.00	0.01	0.02	0.15	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 149 NI 1276 NF 1278 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm

1	0	-0	1697	0	0	0	-16	--	--	16.08	16.08	0.18	0.00	0.01	0.11	0.00	0.00	20.9
2	0	-0	1278	0	0	0	-86	--	--	16.08	16.08	0.29	0.00	0.01	0.08	0.00	0.00	20.9
3	0	-0	1258	0	0	0	-66	--	--	16.08	16.08	0.29	0.00	0.01	0.08	0.00	0.00	20.9
4	0	-0	1353	0	0	0	41	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
5	0	-0	1334	0	0	0	61	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
6	0	-0	1327	0	0	0	-65	--	--	16.08	16.08	0.29	0.00	0.01	0.08	0.00	0.00	20.9
7	0	-0	1261	0	0	0	1	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
8	0	-0	1350	0	0	0	-27	--	--	16.08	16.08	0.29	0.00	0.01	0.08	0.00	0.00	20.9
9	0	-0	1284	0	0	0	39	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
10	0	-0	1278	0	0	0	-86	--	--	16.08	16.08	0.29	0.00	0.01	0.08	0.00	0.00	20.9
11	0	-0	1258	0	0	0	-66	--	--	16.08	16.08	0.29	0.00	0.01	0.08	0.00	0.00	20.9
12	0	-0	1353	0	0	0	41	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
13	0	-0	1334	0	0	0	61	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
14	0	-0	1327	0	0	0	-65	--	--	16.08	16.08	0.29	0.00	0.01	0.08	0.00	0.00	20.9
15	0	-0	1261	0	0	0	1	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
16	0	-0	1350	0	0	0	-27	--	--	16.08	16.08	0.29	0.00	0.01	0.08	0.00	0.00	20.9
17	0	-0	1284	0	0	0	39	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
18	0	-0	1734	0	0	0	-190	--	--	16.08	16.08	0.18	0.00	0.01	0.11	0.00	0.00	20.9
19	0	-0	1965	0	0	0	209	--	--	16.08	16.08	0.00	0.00	0.02	0.12	0.00	0.00	20.9
20	0	-0	1911	0	0	0	74	--	--	16.08	16.08	0.00	0.00	0.02	0.12	0.00	0.00	20.9
37	0	-0	1583	0	0	0	-336	--	--	16.08	16.08	0.18	0.01	0.01	0.10	0.00	0.00	20.9
38	0	-0	1968	0	0	0	330	--	--	16.08	16.08	0.00	0.01	0.02	0.12	0.00	0.00	20.9
39	0	-0	1877	0	0	0	105	--	--	16.08	16.08	0.00	0.00	0.02	0.12	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	1697	0	0	0	2233	--	--	16.08	16.08	0.00	0.04	0.01	0.11	0.00	0.00	20.9
2	26	-0	1278	0	0	0	1608	--	--	16.08	16.08	0.10	0.03	0.01	0.08	0.00	0.00	20.9
3	26	-0	1258	0	0	0	1602	--	--	16.08	16.08	0.10	0.03	0.01	0.08	0.00	0.00	20.9
4	26	-0	1353	0	0	0	1834	--	--	16.08	16.08	0.10	0.03	0.01	0.08	0.00	0.00	20.9
5	26	-0	1334	0	0	0	1829	--	--	16.08	16.08	0.10	0.03	0.01	0.08	0.00	0.00	20.9
6	26	-0	1327	0	0	0	1695	--	--	16.08	16.08	0.10	0.03	0.01	0.08	0.00	0.00	20.9

7	26	-0	1261	0	0	0	1673	--	--	16.08	16.08	0.10	0.03	0.01	0.08	0.00	0.00	20.9
8	26	-0	1350	0	0	0	1763	--	--	16.08	16.08	0.10	0.03	0.01	0.08	0.00	0.00	20.9
9	26	-0	1284	0	0	0	1741	--	--	16.08	16.08	0.10	0.03	0.01	0.08	0.00	0.00	20.9
10	26	-0	1278	0	0	0	1608	--	--	16.08	16.08	0.10	0.03	0.01	0.08	0.00	0.00	20.9
11	26	-0	1258	0	0	0	1602	--	--	16.08	16.08	0.10	0.03	0.01	0.08	0.00	0.00	20.9
12	26	-0	1353	0	0	0	1834	--	--	16.08	16.08	0.10	0.03	0.01	0.08	0.00	0.00	20.9
13	26	-0	1334	0	0	0	1829	--	--	16.08	16.08	0.10	0.03	0.01	0.08	0.00	0.00	20.9
14	26	-0	1327	0	0	0	1695	--	--	16.08	16.08	0.10	0.03	0.01	0.08	0.00	0.00	20.9
15	26	-0	1261	0	0	0	1673	--	--	16.08	16.08	0.10	0.03	0.01	0.08	0.00	0.00	20.9
16	26	-0	1350	0	0	0	1763	--	--	16.08	16.08	0.10	0.03	0.01	0.08	0.00	0.00	20.9
17	26	-0	1284	0	0	0	1741	--	--	16.08	16.08	0.10	0.03	0.01	0.08	0.00	0.00	20.9
18	26	-0	1734	0	0	0	2108	--	--	16.08	16.08	0.00	0.04	0.01	0.11	0.00	0.00	20.9
19	26	-0	1965	0	0	0	2814	--	--	16.08	16.08	0.00	0.05	0.02	0.12	0.00	0.00	20.9
20	26	-0	1911	0	0	0	2607	--	--	16.08	16.08	0.00	0.04	0.02	0.12	0.00	0.00	20.9
37	26	-0	1583	0	0	0	1763	--	--	16.08	16.08	0.00	0.03	0.01	0.10	0.00	0.00	20.9
38	26	-0	1968	0	0	0	2939	--	--	16.08	16.08	0.00	0.05	0.02	0.12	0.00	0.00	20.9
39	26	-0	1877	0	0	0	2593	--	--	16.08	16.08	0.00	0.04	0.02	0.12	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	1697	0	0	0	855	--	--	16.08	16.08	0.00	0.01	0.01	0.11	0.00	0.00	20.9
2	51	-0	1278	0	0	0	570	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
3	51	-0	1258	0	0	0	580	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
4	51	-0	1353	0	0	0	736	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
5	51	-0	1334	0	0	0	746	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
6	51	-0	1327	0	0	0	617	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
7	51	-0	1261	0	0	0	649	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
8	51	-0	1350	0	0	0	667	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
9	51	-0	1284	0	0	0	699	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
10	51	-0	1278	0	0	0	570	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
11	51	-0	1258	0	0	0	580	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
12	51	-0	1353	0	0	0	736	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
13	51	-0	1334	0	0	0	746	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
14	51	-0	1327	0	0	0	617	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
15	51	-0	1261	0	0	0	649	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
16	51	-0	1350	0	0	0	667	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
17	51	-0	1284	0	0	0	699	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
18	51	-0	1734	0	0	0	700	--	--	16.08	16.08	0.00	0.01	0.01	0.11	0.00	0.00	20.9
19	51	-0	1965	0	0	0	1218	--	--	16.08	16.08	0.00	0.02	0.02	0.12	0.00	0.00	20.9
20	51	-0	1911	0	0	0	1055	--	--	16.08	16.08	0.00	0.02	0.02	0.12	0.00	0.00	20.9
37	51	-0	1583	0	0	0	477	--	--	16.08	16.08	0.00	0.01	0.01	0.10	0.00	0.00	20.9
38	51	-0	1968	0	0	0	1341	--	--	16.08	16.08	0.00	0.02	0.02	0.12	0.00	0.00	20.9
39	51	-0	1877	0	0	0	1069	--	--	16.08	16.08	0.00	0.02	0.02	0.12	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 150 NI 1278 NF 1268 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-2314	0	0	0	934	--	--	16.08	16.08	0.00	0.02	0.02	0.15	0.00	0.00	20.9
2	0	-0	-1827	0	0	0	738	--	--	16.08	16.08	0.10	0.01	0.02	0.11	0.00	0.00	20.9
3	0	-0	-1794	0	0	0	745	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
4	0	-0	-1766	0	0	0	692	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
5	0	-0	-1733	0	0	0	700	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
6	0	-0	-1844	0	0	0	713	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
7	0	-0	-1734	0	0	0	738	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
8	0	-0	-1826	0	0	0	699	--	--	16.08	16.08	0.10	0.01	0.02	0.11	0.00	0.00	20.9
9	0	-0	-1716	0	0	0	724	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
10	0	-0	-1827	0	0	0	738	--	--	16.08	16.08	0.10	0.01	0.02	0.11	0.00	0.00	20.9
11	0	-0	-1794	0	0	0	745	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
12	0	-0	-1766	0	0	0	692	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
13	0	-0	-1733	0	0	0	700	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
14	0	-0	-1844	0	0	0	713	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
15	0	-0	-1734	0	0	0	738	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
16	0	-0	-1826	0	0	0	699	--	--	16.08	16.08	0.10	0.01	0.02	0.11	0.00	0.00	20.9
17	0	-0	-1716	0	0	0	724	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
18	0	-0	-2626	0	0	0	1099	--	--	16.08	16.08	0.00	0.02	0.02	0.16	0.00	0.00	20.9
19	0	-0	-2444	0	0	0	989	--	--	16.08	16.08	0.00	0.02	0.02	0.15	0.00	0.00	20.9
20	0	-0	-2540	0	0	0	1139	--	--	16.08	16.08	0.00	0.02	0.02	0.16	0.00	0.00	20.9
37	0	-0	-2584	0	0	0	1083	--	--	16.08	16.08	0.00	0.02	0.02	0.16	0.00	0.00	20.9
38	0	-0	-2282	0	0	0	900	--	--	16.08	16.08	0.00	0.02	0.02	0.14	0.00	0.00	20.9
39	0	-0	-2441	0	0	0	1149	--	--	16.08	16.08	0.00	0.02	0.02	0.15	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	-2314	0	0	0	934	--	--	16.08	16.08	0.00	0.02	0.02	0.15	0.00	0.00	20.9
2	26	-0	-1827	0	0	0	738	--	--	16.08	16.08	0.10	0.01	0.02	0.11	0.00	0.00	20.9
3	26	-0	-1794	0	0	0	745	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
4	26	-0	-1766	0	0	0	692	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
5	26	-0	-1733	0	0	0	700	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
6	26	-0	-1844	0	0	0	713	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
7	26	-0	-1734	0	0	0	738	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
8	26	-0	-1826	0	0	0	699	--	--	16.08	16.08	0.10	0.01	0.02	0.11	0.00	0.00	20.9
9	26	-0	-1716	0	0	0	724	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
10	26	-0	-1827	0	0	0	738	--	--	16.08	16.08	0.10	0.01	0.02	0.11	0.00	0.00	20.9
11	26	-0	-1794	0	0	0	745	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
12	26	-0	-1766	0	0	0	692	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
13	26	-0	-1733	0	0	0	700	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
14	26	-0	-1844	0	0	0	713	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
15	26	-0	-1734	0	0	0	738	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
16	26	-0	-1826	0	0	0	699	--	--	16.08	16.08	0.10	0.01	0.02	0.11	0.00	0.00	20.9
17	26	-0	-1716	0	0	0	724	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
18	26	-0	-2626	0	0	0	1099	--	--	16.08	16.08	0.00	0.02	0.02	0.16	0.00	0.00	20.9
19	26	-0	-2444	0	0	0	989	--	--	16.08	16.08	0.00	0.02	0.02	0.15	0.00	0.00	20.9
20	26	-0	-2540	0	0	0	1139	--	--	16.08	16.08	0.00	0.02	0.02	0.16	0.00	0.00	20.9
37	26	-0	-2584	0	0	0	1083	--	--	16.08	16.08	0.00	0.02	0.02	0.16	0.00	0.00	20.9
38	26	-0	-2282	0	0	0	900	--	--	16.08	16.08	0.00	0.02	0.02	0.14	0.00	0.00	20.9
39	26	-0	-2441	0	0	0	1149	--	--	16.08	16.08	0.00	0.02	0.02	0.15	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	-2314	0	0	0	-254	--	--	16.08	16.08	0.18	0.00	0.02	0.15	0.00	0.00	20.9
2	51	-0	-1827	0	0	0	-201	--	--	16.08	16.08	0.29	0.00	0.02	0.11	0.00	0.00	20.9

3	51	-0	-1794	0	0	0	-176	--	--	16.08	16.08	0.29	0.00	0.01	0.11	0.00	0.00	20.9
4	51	-0	-1766	0	0	0	-215	--	--	16.08	16.08	0.29	0.00	0.01	0.11	0.00	0.00	20.9
5	51	-0	-1733	0	0	0	-190	--	--	16.08	16.08	0.29	0.00	0.01	0.11	0.00	0.00	20.9
6	51	-0	-1844	0	0	0	-234	--	--	16.08	16.08	0.29	0.00	0.02	0.12	0.00	0.00	20.9
7	51	-0	-1734	0	0	0	-153	--	--	16.08	16.08	0.29	0.00	0.01	0.11	0.00	0.00	20.9
8	51	-0	-1826	0	0	0	-238	--	--	16.08	16.08	0.29	0.00	0.02	0.11	0.00	0.00	20.9
9	51	-0	-1716	0	0	0	-157	--	--	16.08	16.08	0.29	0.00	0.01	0.11	0.00	0.00	20.9
10	51	-0	-1827	0	0	0	-201	--	--	16.08	16.08	0.29	0.00	0.02	0.11	0.00	0.00	20.9
11	51	-0	-1794	0	0	0	-176	--	--	16.08	16.08	0.29	0.00	0.01	0.11	0.00	0.00	20.9
12	51	-0	-1766	0	0	0	-215	--	--	16.08	16.08	0.29	0.00	0.01	0.11	0.00	0.00	20.9
13	51	-0	-1733	0	0	0	-190	--	--	16.08	16.08	0.29	0.00	0.01	0.11	0.00	0.00	20.9
14	51	-0	-1844	0	0	0	-234	--	--	16.08	16.08	0.29	0.00	0.02	0.12	0.00	0.00	20.9
15	51	-0	-1734	0	0	0	-153	--	--	16.08	16.08	0.29	0.00	0.01	0.11	0.00	0.00	20.9
16	51	-0	-1826	0	0	0	-238	--	--	16.08	16.08	0.29	0.00	0.02	0.11	0.00	0.00	20.9
17	51	-0	-1716	0	0	0	-157	--	--	16.08	16.08	0.29	0.00	0.01	0.11	0.00	0.00	20.9
18	51	-0	-2626	0	0	0	-249	--	--	16.08	16.08	0.18	0.00	0.02	0.16	0.00	0.00	20.9
19	51	-0	-2444	0	0	0	-266	--	--	16.08	16.08	0.18	0.00	0.02	0.15	0.00	0.00	20.9
20	51	-0	-2540	0	0	0	-165	--	--	16.08	16.08	0.18	0.00	0.02	0.16	0.00	0.00	20.9
37	51	-0	-2584	0	0	0	-244	--	--	16.08	16.08	0.18	0.00	0.02	0.16	0.00	0.00	20.9
38	51	-0	-2282	0	0	0	-272	--	--	16.08	16.08	0.18	0.00	0.02	0.14	0.00	0.00	20.9
39	51	-0	-2441	0	0	0	-104	--	--	16.08	16.08	0.18	0.00	0.02	0.15	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 151 NI 1268 NF 1301 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--	----------			----------			----------					----------			----------		-----
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-2719	0	0	0	569	--	--	16.08	16.08	0.00	0.01	0.02	0.17	0.00	0.00	20.9
2	0	-0	-2132	0	0	0	427	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
3	0	-0	-2106	0	0	0	444	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
4	0	-0	-2077	0	0	0	432	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
5	0	-0	-2051	0	0	0	449	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
6	0	-0	-2142	0	0	0	410	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
7	0	-0	-2057	0	0	0	464	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
8	0	-0	-2126	0	0	0	412	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
9	0	-0	-2041	0	0	0	466	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
10	0	-0	-2132	0	0	0	427	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
11	0	-0	-2106	0	0	0	444	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
12	0	-0	-2077	0	0	0	432	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
13	0	-0	-2051	0	0	0	449	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
14	0	-0	-2142	0	0	0	410	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
15	0	-0	-2057	0	0	0	464	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
16	0	-0	-2126	0	0	0	412	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
17	0	-0	-2041	0	0	0	466	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
18	0	-0	-3024	0	0	0	616	--	--	16.08	16.08	0.00	0.01	0.02	0.19	0.00	0.00	20.9
19	0	-0	-2862	0	0	0	657	--	--	16.08	16.08	0.00	0.01	0.02	0.18	0.00	0.00	20.9
20	0	-0	-2954	0	0	0	728	--	--	16.08	16.08	0.00	0.01	0.02	0.19	0.00	0.00	20.9
37	0	-0	-2973	0	0	0	570	--	--	16.08	16.08	0.00	0.01	0.02	0.19	0.00	0.00	20.9
38	0	-0	-2703	0	0	0	637	--	--	16.08	16.08	0.00	0.01	0.02	0.17	0.00	0.00	20.9
39	0	-0	-2856	0	0	0	756	--	--	16.08	16.08	0.00	0.01	0.02	0.18	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	-2719	0	0	0	-827	--	--	16.08	16.08	0.18	0.01	0.02	0.17	0.00	0.00	20.9
2	26	-0	-2132	0	0	0	-668	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
3	26	-0	-2106	0	0	0	-638	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
4	26	-0	-2077	0	0	0	-634	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
5	26	-0	-2051	0	0	0	-605	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
6	26	-0	-2142	0	0	0	-690	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
7	26	-0	-2057	0	0	0	-592	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
8	26	-0	-2126	0	0	0	-680	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
9	26	-0	-2041	0	0	0	-582	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
10	26	-0	-2132	0	0	0	-668	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
11	26	-0	-2106	0	0	0	-638	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
12	26	-0	-2077	0	0	0	-634	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
13	26	-0	-2051	0	0	0	-605	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
14	26	-0	-2142	0	0	0	-690	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
15	26	-0	-2057	0	0	0	-592	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
16	26	-0	-2126	0	0	0	-680	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
17	26	-0	-2041	0	0	0	-582	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
18	26	-0	-3024	0	0	0	-937	--	--	16.08	16.08	0.18	0.02	0.02	0.19	0.00	0.00	20.9
19	26	-0	-2862	0	0	0	-814	--	--	16.08	16.08	0.18	0.01	0.02	0.18	0.00	0.00	20.9
20	26	-0	-2954	0	0	0	-790	--	--	16.08	16.08	0.18	0.01	0.02	0.19	0.00	0.00	20.9
37	26	-0	-2973	0	0	0	-957	--	--	16.08	16.08	0.18	0.02	0.02	0.19	0.00	0.00	20.9
38	26	-0	-2703	0	0	0	-751	--	--	16.08	16.08	0.18	0.01	0.02	0.17	0.00	0.00	20.9
39	26	-0	-2856	0	0	0	756	--	--	16.08	16.08	0.00	0.01	0.02	0.18	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	-2719	0	0	0	-827	--	--	16.08	16.08	0.18	0.01	0.02	0.17	0.00	0.00	20.9
2	51	-0	-2132	0	0	0	-668	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
3	51	-0	-2106	0	0	0	-638	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
4	51	-0	-2077	0	0	0	-634	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
5	51	-0	-2051	0	0	0	-605	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
6	51	-0	-2142	0	0	0	-690	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
7	51	-0	-2057	0	0	0	-592	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
8	51	-0	-2126	0	0	0	-680	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
9	51	-0	-2041	0	0	0	-582	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
10	51	-0	-2132	0	0	0	-668	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
11	51	-0	-2106	0	0	0	-638	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
12	51	-0	-2077	0	0	0	-634	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
13	51	-0	-2051	0	0	0	-605	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
14	51	-0	-2142	0	0	0	-690	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
15	51	-0	-2057	0	0	0	-592	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
16	51	-0	-2126	0	0	0	-680	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
17	51	-0	-2041	0	0	0	-582	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
18	51	-0	-3024	0	0	0	-937	--	--	16.08	16.08	0.18	0.02	0.02	0.19	0.00	0.00	20.9
19	51	-0	-2862	0	0	0	-814	--	--	16.08	16.08	0.18	0.01	0.02	0.18	0.00	0.00	20.9
20	51	-0	-2954	0	0	0	-790	--	--	16.08	16.08	0.18	0.01	0.02	0.19	0.00	0.00	20.9
37	51	-0	-2973	0	0	0	-957	--	--	16.08	16.08	0.18	0.02	0.02	0.19	0.00	0.00	20.9
38	51	-0	-2703	0	0	0	-751	--	--	16.08	16.08	0.18	0.01	0.02	0.17	0.00	0.00	20.9
39	51	-0	-2856	0	0	0	-711	--	--	16.08	16.08	0.18	0.01	0.02	0.18	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 152 NI 1301 NF 1300 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-2320	0	0	0	26	--	--	16.08	16.08	0.00	0.00	0.02	0.15	0.00	0.00	20.9
2	0	-0	-1838	0	0	0	8	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
3	0	-0	-1820	0	0	0	30	--	--	16.08	16.08	0.10	0.00	0.02	0.11	0.00	0.00	20.9
4	0	-0	-1748	0	0	0	9	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
5	0	-0	-1730	0	0	0	32	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
6	0	-0	-1828	0	0	0	-957	--	--	16.08	16.08	0.29	0.02	0.02	0.11	0.00	0.00	20.9
7	0	-0	-1768	0	0	0	58	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
8	0	-0	-1801	0	0	0	-943	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
9	0	-0	-1741	0	0	0	58	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
10	0	-0	-1838	0	0	0	8	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
11	0	-0	-1820	0	0	0	30	--	--	16.08	16.08	0.10	0.00	0.02	0.11	0.00	0.00	20.9
12	0	-0	-1748	0	0	0	9	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
13	0	-0	-1730	0	0	0	32	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
14	0	-0	-1828	0	0	0	-957	--	--	16.08	16.08	0.29	0.02	0.02	0.11	0.00	0.00	20.9
15	0	-0	-1768	0	0	0	58	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
16	0	-0	-1801	0	0	0	-943	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
17	0	-0	-1741	0	0	0	58	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
18	0	-0	-2635	0	0	0	28	--	--	16.08	16.08	0.00	0.00	0.02	0.17	0.00	0.00	20.9
19	0	-0	-2370	0	0	0	58	--	--	16.08	16.08	0.00	0.00	0.02	0.15	0.00	0.00	20.9
20	0	-0	-2522	0	0	0	136	--	--	16.08	16.08	0.00	0.00	0.02	0.16	0.00	0.00	20.9
37	0	-0	-2637	0	0	0	8	--	--	16.08	16.08	0.00	0.00	0.02	0.17	0.00	0.00	20.9
38	0	-0	-2195	0	0	0	57	--	--	16.08	16.08	0.00	0.00	0.02	0.14	0.00	0.00	20.9
39	0	-0	-2448	0	0	0	188	--	--	16.08	16.08	0.00	0.00	0.02	0.15	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	26	-0	-2320	0	0	0	-1166	--	--	16.08	16.08	0.18	0.02	0.02	0.15	0.00	0.00	20.9
2	26	-0	-1838	0	0	0	-936	--	--	16.08	16.08	0.29	0.02	0.02	0.12	0.00	0.00	20.9
3	26	-0	-1820	0	0	0	-904	--	--	16.08	16.08	0.29	0.02	0.02	0.11	0.00	0.00	20.9
4	26	-0	-1748	0	0	0	-889	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
5	26	-0	-1730	0	0	0	-857	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
6	26	-0	-1828	0	0	0	-957	--	--	16.08	16.08	0.29	0.02	0.02	0.11	0.00	0.00	20.9
7	26	-0	-1768	0	0	0	-850	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
8	26	-0	-1801	0	0	0	-943	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
9	26	-0	-1741	0	0	0	-836	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
10	26	-0	-1838	0	0	0	-936	--	--	16.08	16.08	0.29	0.02	0.02	0.12	0.00	0.00	20.9
11	26	-0	-1820	0	0	0	-904	--	--	16.08	16.08	0.29	0.02	0.02	0.11	0.00	0.00	20.9
12	26	-0	-1748	0	0	0	-889	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
13	26	-0	-1730	0	0	0	-857	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
14	26	-0	-1828	0	0	0	-957	--	--	16.08	16.08	0.29	0.02	0.02	0.11	0.00	0.00	20.9
15	26	-0	-1768	0	0	0	-850	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
16	26	-0	-1801	0	0	0	-943	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
17	26	-0	-1741	0	0	0	-836	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
18	26	-0	-2635	0	0	0	-1325	--	--	16.08	16.08	0.18	0.02	0.02	0.17	0.00	0.00	20.9
19	26	-0	-2370	0	0	0	-1159	--	--	16.08	16.08	0.18	0.02	0.02	0.15	0.00	0.00	20.9
20	26	-0	-2522	0	0	0	-1159	--	--	16.08	16.08	0.18	0.02	0.02	0.16	0.00	0.00	20.9
37	26	-0	-2637	0	0	0	-1346	--	--	16.08	16.08	0.18	0.02	0.02	0.17	0.00	0.00	20.9
38	26	-0	-2195	0	0	0	-1070	--	--	16.08	16.08	0.18	0.02	0.02	0.14	0.00	0.00	20.9
39	26	-0	-2448	0	0	0	-1070	--	--	16.08	16.08	0.18	0.02	0.02	0.15	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	51	-0	-2320	0	0	0	-1166	--	--	16.08	16.08	0.18	0.02	0.02	0.15	0.00	0.00	20.9
2	51	-0	-1838	0	0	0	-936	--	--	16.08	16.08	0.29	0.02	0.02	0.12	0.00	0.00	20.9
3	51	-0	-1820	0	0	0	-904	--	--	16.08	16.08	0.29	0.02	0.02	0.11	0.00	0.00	20.9
4	51	-0	-1748	0	0	0	-889	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
5	51	-0	-1730	0	0	0	-857	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
6	51	-0	-1828	0	0	0	-957	--	--	16.08	16.08	0.29	0.02	0.02	0.11	0.00	0.00	20.9
7	51	-0	-1768	0	0	0	-850	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
8	51	-0	-1801	0	0	0	-943	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
9	51	-0	-1741	0	0	0	-836	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
10	51	-0	-1838	0	0	0	-936	--	--	16.08	16.08	0.29	0.02	0.02	0.12	0.00	0.00	20.9
11	51	-0	-1820	0	0	0	-904	--	--	16.08	16.08	0.29	0.02	0.02	0.11	0.00	0.00	20.9
12	51	-0	-1748	0	0	0	-889	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
13	51	-0	-1730	0	0	0	-857	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
14	51	-0	-1828	0	0	0	-957	--	--	16.08	16.08	0.29	0.02	0.02	0.11	0.00	0.00	20.9
15	51	-0	-1768	0	0	0	-850	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
16	51	-0	-1801	0	0	0	-943	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
17	51	-0	-1741	0	0	0	-836	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
18	51	-0	-2635	0	0	0	-1325	--	--	16.08	16.08	0.18	0.02	0.02	0.17	0.00	0.00	20.9
19	51	-0	-2370	0	0	0	-1159	--	--	16.08	16.08	0.18	0.02	0.02	0.15	0.00	0.00	20.9
20	51	-0	-2522	0	0	0	-1159	--	--	16.08	16.08	0.18	0.02	0.02	0.16	0.00	0.00	20.9
37	51	-0	-2637	0	0	0	-1346	--	--	16.08	16.08	0.18	0.02	0.02	0.17	0.00	0.00	20.9
38	51	-0	-2195	0	0	0	-1070	--	--	16.08	16.08	0.18	0.02	0.02	0.14	0.00	0.00	20.9
39	51	-0	-2448	0	0	0	-1070	--	--	16.08	16.08	0.18	0.02	0.02	0.15	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 153 NI 1300 NF 1299 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-1645	0	0	0	-1407	--	--	16.08	16.08	0.18	0.02	0.01	0.10	0.00	0.00	20.9
2	0	-0	-1319	0	0	0	-1131	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
3	0	-0	-1308	0	0	0	-1098	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
4	0	-0	-1223	0	0	0	-1068	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
5	0	-0	-1213	0	0	0	-1035	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
6	0	-0	-1297	0	0	0	-1147	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
7	0	-0	-1263	0	0	0	-1037	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
8	0	-0	-1269	0	0	0	-1128	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
9	0	-0	-1234	0	0	0	-1018	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
10	0	-0	-1319	0	0	0	-1131	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9

11	0	-0	-1308	0	0	0	-1098	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
12	0	-0	-1223	0	0	0	-1068	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
13	0	-0	-1213	0	0	0	-1035	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
14	0	-0	-1297	0	0	0	-1147	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
15	0	-0	-1263	0	0	0	-1037	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
16	0	-0	-1269	0	0	0	-1128	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
17	0	-0	-1234	0	0	0	-1018	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
18	0	-0	-1919	0	0	0	-1609	--	--	16.08	16.08	0.18	0.03	0.02	0.12	0.00	0.00	20.9
19	0	-0	-1637	0	0	0	-1398	--	--	16.08	16.08	0.18	0.02	0.01	0.10	0.00	0.00	20.9
20	0	-0	-1802	0	0	0	-1425	--	--	16.08	16.08	0.18	0.02	0.01	0.11	0.00	0.00	20.9
37	0	-0	-1951	0	0	0	-1636	--	--	16.08	16.08	0.18	0.03	0.02	0.12	0.00	0.00	20.9
38	0	-0	-1480	0	0	0	-1284	--	--	16.08	16.08	0.18	0.02	0.01	0.09	0.00	0.00	20.9
39	0	-0	-1755	0	0	0	-1329	--	--	16.08	16.08	0.18	0.02	0.01	0.11	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	-1645	0	0	0	-1407	--	--	16.08	16.08	0.18	0.02	0.01	0.10	0.00	0.00	20.9
2	26	-0	-1319	0	0	0	-1131	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
3	26	-0	-1308	0	0	0	-1098	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
4	26	-0	-1223	0	0	0	-1068	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
5	26	-0	-1213	0	0	0	-1035	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
6	26	-0	-1297	0	0	0	-1147	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
7	26	-0	-1263	0	0	0	-1037	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
8	26	-0	-1269	0	0	0	-1128	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
9	26	-0	-1234	0	0	0	-1018	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
10	26	-0	-1319	0	0	0	-1131	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
11	26	-0	-1308	0	0	0	-1098	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
12	26	-0	-1223	0	0	0	-1068	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
13	26	-0	-1213	0	0	0	-1035	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
14	26	-0	-1297	0	0	0	-1147	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
15	26	-0	-1263	0	0	0	-1037	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
16	26	-0	-1269	0	0	0	-1128	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
17	26	-0	-1234	0	0	0	-1018	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
18	26	-0	-1919	0	0	0	-1609	--	--	16.08	16.08	0.18	0.03	0.02	0.12	0.00	0.00	20.9
19	26	-0	-1637	0	0	0	-1398	--	--	16.08	16.08	0.18	0.02	0.01	0.10	0.00	0.00	20.9
20	26	-0	-1802	0	0	0	-1425	--	--	16.08	16.08	0.18	0.02	0.01	0.11	0.00	0.00	20.9
37	26	-0	-1951	0	0	0	-1636	--	--	16.08	16.08	0.18	0.03	0.02	0.12	0.00	0.00	20.9
38	26	-0	-1480	0	0	0	-1284	--	--	16.08	16.08	0.18	0.02	0.01	0.09	0.00	0.00	20.9
39	26	-0	-1755	0	0	0	-1329	--	--	16.08	16.08	0.18	0.02	0.01	0.11	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	-1645	0	0	0	-1407	--	--	16.08	16.08	0.18	0.02	0.01	0.10	0.00	0.00	20.9
2	51	-0	-1319	0	0	0	-1131	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
3	51	-0	-1308	0	0	0	-1098	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
4	51	-0	-1223	0	0	0	-1068	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
5	51	-0	-1213	0	0	0	-1035	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
6	51	-0	-1297	0	0	0	-1147	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
7	51	-0	-1263	0	0	0	-1037	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
8	51	-0	-1269	0	0	0	-1128	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
9	51	-0	-1234	0	0	0	-1018	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
10	51	-0	-1319	0	0	0	-1131	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
11	51	-0	-1308	0	0	0	-1098	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
12	51	-0	-1223	0	0	0	-1068	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
13	51	-0	-1213	0	0	0	-1035	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
14	51	-0	-1297	0	0	0	-1147	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
15	51	-0	-1263	0	0	0	-1037	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
16	51	-0	-1269	0	0	0	-1128	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
17	51	-0	-1234	0	0	0	-1018	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
18	51	-0	-1919	0	0	0	-1609	--	--	16.08	16.08	0.18	0.03	0.02	0.12	0.00	0.00	20.9
19	51	-0	-1637	0	0	0	-1398	--	--	16.08	16.08	0.18	0.02	0.01	0.10	0.00	0.00	20.9
20	51	-0	-1802	0	0	0	-1425	--	--	16.08	16.08	0.18	0.02	0.01	0.11	0.00	0.00	20.9
37	51	-0	-1951	0	0	0	-1636	--	--	16.08	16.08	0.18	0.03	0.02	0.12	0.00	0.00	20.9
38	51	-0	-1480	0	0	0	-1284	--	--	16.08	16.08	0.18	0.02	0.01	0.09	0.00	0.00	20.9
39	51	-0	-1755	0	0	0	-1329	--	--	16.08	16.08	0.18	0.02	0.01	0.11	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 154 NI 1299 NF 1339 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm

1	0	-0	-1043	0	0	0	-1518	--	--	16.08	16.08	0.18	0.03	0.01	0.07	0.00	0.00	20.9
2	0	-0	-850	0	0	0	-1223	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
3	0	-0	-847	0	0	0	-1191	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
4	0	-0	-758	0	0	0	-1144	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
5	0	-0	-756	0	0	0	-1112	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
6	0	-0	-821	0	0	0	-1233	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
7	0	-0	-812	0	0	0	-1126	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
8	0	-0	-793	0	0	0	-1210	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
9	0	-0	-785	0	0	0	-1102	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
10	0	-0	-850	0	0	0	-1223	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
11	0	-0	-847	0	0	0	-1191	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
12	0	-0	-758	0	0	0	-1144	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
13	0	-0	-756	0	0	0	-1112	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
14	0	-0	-821	0	0	0	-1233	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
15	0	-0	-812	0	0	0	-1126	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
16	0	-0	-793	0	0	0	-1210	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
17	0	-0	-785	0	0	0	-1102	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
18	0	-0	-1268	0	0	0	-1754	--	--	16.08	16.08	0.18	0.03	0.01	0.08	0.00	0.00	20.9
19	0	-0	-998	0	0	0	-1495	--	--	16.08	16.08	0.18	0.02	0.01	0.06	0.00	0.00	20.9
20	0	-0	-1163	0	0	0	-1552	--	--	16.08	16.08	0.18	0.03	0.01	0.07	0.00	0.00	20.9
37	0	-0	-1316	0	0	0	-1792	--	--	16.08	16.08	0.18	0.03	0.01	0.08	0.00	0.00	20.9
38	0	-0	-867	0	0	0	-1361	--	--	16.08	16.08	0.18	0.02	0.01	0.05	0.00	0.00	20.9
39	0	-0	-1141	0	0	0	-1456	--	--	16.08	16.08	0.18	0.02	0.01	0.07	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	-1043	0	0	0	-1518	--	--	16.08	16.08	0.18	0.03	0.01	0.07	0.00	0.00	20.9
2	26	-0	-850	0	0	0	-1223	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
3	26	-0	-847	0	0	0	-1191	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
4	26	-0	-758	0	0	0	-1144	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
5	26	-0	-756	0	0	0	-1112	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
6	26	-0	-821	0	0	0	-1233	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9

7	26	-0	-812	0	0	0	-1126	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
8	26	-0	-793	0	0	0	-1210	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
9	26	-0	-785	0	0	0	-1102	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
10	26	-0	-850	0	0	0	-1223	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
11	26	-0	-847	0	0	0	-1191	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
12	26	-0	-758	0	0	0	-1144	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
13	26	-0	-756	0	0	0	-1112	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
14	26	-0	-821	0	0	0	-1233	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
15	26	-0	-812	0	0	0	-1126	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
16	26	-0	-793	0	0	0	-1210	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
17	26	-0	-785	0	0	0	-1102	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
18	26	-0	-1268	0	0	0	-1754	--	--	16.08	16.08	0.18	0.03	0.01	0.08	0.00	0.00	20.9
19	26	-0	-998	0	0	0	-1495	--	--	16.08	16.08	0.18	0.02	0.01	0.06	0.00	0.00	20.9
20	26	-0	-1163	0	0	0	-1552	--	--	16.08	16.08	0.18	0.03	0.01	0.07	0.00	0.00	20.9
37	26	-0	-1316	0	0	0	-1792	--	--	16.08	16.08	0.18	0.03	0.01	0.08	0.00	0.00	20.9
38	26	-0	-867	0	0	0	-1361	--	--	16.08	16.08	0.18	0.02	0.01	0.05	0.00	0.00	20.9
39	26	-0	-1141	0	0	0	-1456	--	--	16.08	16.08	0.18	0.02	0.01	0.07	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	-1043	0	0	0	-1518	--	--	16.08	16.08	0.18	0.03	0.01	0.07	0.00	0.00	20.9
2	51	-0	-850	0	0	0	-1223	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
3	51	-0	-847	0	0	0	-1191	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
4	51	-0	-758	0	0	0	-1144	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
5	51	-0	-756	0	0	0	-1112	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
6	51	-0	-821	0	0	0	-1233	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
7	51	-0	-812	0	0	0	-1126	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
8	51	-0	-793	0	0	0	-1210	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
9	51	-0	-785	0	0	0	-1102	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
10	51	-0	-850	0	0	0	-1223	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
11	51	-0	-847	0	0	0	-1191	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
12	51	-0	-758	0	0	0	-1144	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
13	51	-0	-756	0	0	0	-1112	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
14	51	-0	-821	0	0	0	-1233	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
15	51	-0	-812	0	0	0	-1126	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
16	51	-0	-793	0	0	0	-1210	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
17	51	-0	-785	0	0	0	-1102	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
18	51	-0	-1268	0	0	0	-1754	--	--	16.08	16.08	0.18	0.03	0.01	0.08	0.00	0.00	20.9
19	51	-0	-998	0	0	0	-1495	--	--	16.08	16.08	0.18	0.02	0.01	0.06	0.00	0.00	20.9
20	51	-0	-1163	0	0	0	-1552	--	--	16.08	16.08	0.18	0.03	0.01	0.07	0.00	0.00	20.9
37	51	-0	-1316	0	0	0	-1792	--	--	16.08	16.08	0.18	0.03	0.01	0.08	0.00	0.00	20.9
38	51	-0	-867	0	0	0	-1361	--	--	16.08	16.08	0.18	0.02	0.01	0.05	0.00	0.00	20.9
39	51	-0	-1141	0	0	0	-1456	--	--	16.08	16.08	0.18	0.02	0.01	0.07	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 155 NI 1339 NF 1338 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm

1	0	-0	-474	0	0	0	-1514	--	--	16.08	16.08	0.18	0.03	0.00	0.03	0.00	0.00	20.9
2	0	-0	-405	0	0	0	-1227	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
3	0	-0	-410	0	0	0	-1197	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
4	0	-0	-318	0	0	0	-1133	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
5	0	-0	-324	0	0	0	-1103	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
6	0	-0	-368	0	0	0	-1229	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
7	0	-0	-387	0	0	0	-1129	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
8	0	-0	-342	0	0	0	-1201	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
9	0	-0	-361	0	0	0	-1101	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
10	0	-0	-405	0	0	0	-1227	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
11	0	-0	-410	0	0	0	-1197	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
12	0	-0	-318	0	0	0	-1133	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
13	0	-0	-324	0	0	0	-1103	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
14	0	-0	-368	0	0	0	-1229	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
15	0	-0	-387	0	0	0	-1129	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
16	0	-0	-342	0	0	0	-1201	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
17	0	-0	-361	0	0	0	-1101	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
18	0	-0	-650	0	0	0	-1775	--	--	16.08	16.08	0.18	0.03	0.01	0.04	0.00	0.00	20.9
19	0	-0	-396	0	0	0	-1472	--	--	16.08	16.08	0.18	0.02	0.00	0.02	0.00	0.00	20.9
20	0	-0	-562	0	0	0	-1559	--	--	16.08	16.08	0.18	0.03	0.00	0.04	0.00	0.00	20.9
37	0	-0	-712	0	0	0	-1827	--	--	16.08	16.08	0.18	0.03	0.01	0.04	0.00	0.00	20.9
38	0	-0	-289	0	0	0	-1322	--	--	16.08	16.08	0.18	0.02	0.00	0.02	0.00	0.00	20.9
39	0	-0	-566	0	0	0	-1467	--	--	16.08	16.08	0.18	0.02	0.00	0.04	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	-474	0	0	0	-1514	--	--	16.08	16.08	0.18	0.03	0.00	0.03	0.00	0.00	20.9
2	26	-0	-405	0	0	0	-1227	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
3	26	-0	-410	0	0	0	-1197	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
4	26	-0	-318	0	0	0	-1133	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
5	26	-0	-324	0	0	0	-1103	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
6	26	-0	-368	0	0	0	-1229	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
7	26	-0	-387	0	0	0	-1129	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
8	26	-0	-342	0	0	0	-1201	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
9	26	-0	-361	0	0	0	-1101	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
10	26	-0	-405	0	0	0	-1227	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
11	26	-0	-410	0	0	0	-1197	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
12	26	-0	-318	0	0	0	-1133	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
13	26	-0	-324	0	0	0	-1103	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
14	26	-0	-368	0	0	0	-1229	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
15	26	-0	-387	0	0	0	-1129	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
16	26	-0	-342	0	0	0	-1201	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
17	26	-0	-361	0	0	0	-1101	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
18	26	-0	-650	0	0	0	-1775	--	--	16.08	16.08	0.18	0.03	0.01	0.04	0.00	0.00	20.9
19	26	-0	-396	0	0	0	-1472	--	--	16.08	16.08	0.18	0.02	0.00	0.02	0.00	0.00	20.9
20	26	-0	-562	0	0	0	-1559	--	--	16.08	16.08	0.18	0.03	0.00	0.04	0.00	0.00	20.9
37	26	-0	-712	0	0	0	-1827	--	--	16.08	16.08	0.18	0.03	0.01	0.04	0.00	0.00	20.9
38	26	-0	-289	0	0	0	-1322	--	--	16.08	16.08	0.18	0.02	0.00	0.02	0.00	0.00	20.9
39	26	-0	-566	0	0	0	-1467	--	--	16.08	16.08	0.18	0.02	0.00	0.04	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	-474	0	0	0	-1514	--	--	16.08	16.08	0.18	0.03	0.00	0.03	0.00	0.00	20.9
2	51	-0	-405	0	0	0	-1227	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9

3	51	-0	-410	0	0	0	-1197	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
4	51	-0	-318	0	0	0	-1133	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
5	51	-0	-324	0	0	0	-1103	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
6	51	-0	-368	0	0	0	-1229	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
7	51	-0	-387	0	0	0	-1129	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
8	51	-0	-342	0	0	0	-1201	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
9	51	-0	-361	0	0	0	-1101	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
10	51	-0	-405	0	0	0	-1227	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
11	51	-0	-410	0	0	0	-1197	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
12	51	-0	-318	0	0	0	-1133	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
13	51	-0	-324	0	0	0	-1103	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
14	51	-0	-368	0	0	0	-1229	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
15	51	-0	-387	0	0	0	-1129	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
16	51	-0	-342	0	0	0	-1201	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
17	51	-0	-361	0	0	0	-1101	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
18	51	-0	-650	0	0	0	-1775	--	--	16.08	16.08	0.18	0.03	0.01	0.04	0.00	0.00	20.9
19	51	-0	-396	0	0	0	-1472	--	--	16.08	16.08	0.18	0.02	0.00	0.02	0.00	0.00	20.9
20	51	-0	-562	0	0	0	-1559	--	--	16.08	16.08	0.18	0.03	0.00	0.04	0.00	0.00	20.9
37	51	-0	-712	0	0	0	-1827	--	--	16.08	16.08	0.18	0.03	0.01	0.04	0.00	0.00	20.9
38	51	-0	-289	0	0	0	-1322	--	--	16.08	16.08	0.18	0.02	0.00	0.02	0.00	0.00	20.9
39	51	-0	-566	0	0	0	-1467	--	--	16.08	16.08	0.18	0.02	0.00	0.04	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 156 NI 1338 NF 1269 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	105	0	0	0	-1449	--	--	16.08	16.08	0.18	0.02	0.00	0.01	0.00	0.00	20.9
2	0	-0	48	0	0	0	-1165	--	--	16.08	16.08	0.29	0.02	0.00	0.00	0.00	0.00	20.9
3	0	-0	32	0	0	0	-1132	--	--	16.08	16.08	0.29	0.02	0.00	0.00	0.00	0.00	20.9
4	0	-0	129	0	0	0	-1098	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
5	0	-0	113	0	0	0	-1065	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
6	0	-0	94	0	0	0	-1181	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
7	0	-0	43	0	0	0	-1069	--	--	16.08	16.08	0.29	0.02	0.00	0.00	0.00	0.00	20.9
8	0	-0	118	0	0	0	-1161	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
9	0	-0	67	0	0	0	-1049	--	--	16.08	16.08	0.29	0.02	0.00	0.00	0.00	0.00	20.9
10	0	-0	48	0	0	0	-1165	--	--	16.08	16.08	0.29	0.02	0.00	0.00	0.00	0.00	20.9
11	0	-0	32	0	0	0	-1132	--	--	16.08	16.08	0.29	0.02	0.00	0.00	0.00	0.00	20.9
12	0	-0	129	0	0	0	-1098	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
13	0	-0	113	0	0	0	-1065	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
14	0	-0	94	0	0	0	-1181	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
15	0	-0	43	0	0	0	-1069	--	--	16.08	16.08	0.29	0.02	0.00	0.00	0.00	0.00	20.9
16	0	-0	118	0	0	0	-1161	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
17	0	-0	67	0	0	0	-1049	--	--	16.08	16.08	0.29	0.02	0.00	0.00	0.00	0.00	20.9
18	0	-0	-23	0	0	0	-1671	--	--	16.08	16.08	0.18	0.03	0.00	0.00	0.00	0.00	20.9
19	0	-0	213	0	0	0	-1437	--	--	16.08	16.08	0.18	0.02	0.00	0.01	0.00	0.00	20.9
20	0	-0	43	0	0	0	-1468	--	--	16.08	16.08	0.18	0.02	0.00	0.00	0.00	0.00	20.9
37	0	-0	-99	0	0	0	-1740	--	--	16.08	16.08	0.18	0.03	0.00	0.01	0.00	0.00	20.9
38	0	-0	295	0	0	0	-1318	--	--	16.08	16.08	0.18	0.02	0.00	0.02	0.00	0.00	20.9
39	0	-0	11	0	0	0	-1371	--	--	16.08	16.08	0.18	0.02	0.00	0.00	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	105	0	0	0	-1449	--	--	16.08	16.08	0.18	0.02	0.00	0.01	0.00	0.00	20.9
2	26	-0	48	0	0	0	-1165	--	--	16.08	16.08	0.29	0.02	0.00	0.00	0.00	0.00	20.9
3	26	-0	32	0	0	0	-1132	--	--	16.08	16.08	0.29	0.02	0.00	0.00	0.00	0.00	20.9
4	26	-0	129	0	0	0	-1098	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
5	26	-0	113	0	0	0	-1065	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
6	26	-0	94	0	0	0	-1181	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
7	26	-0	43	0	0	0	-1069	--	--	16.08	16.08	0.29	0.02	0.00	0.00	0.00	0.00	20.9
8	26	-0	118	0	0	0	-1161	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
9	26	-0	67	0	0	0	-1049	--	--	16.08	16.08	0.29	0.02	0.00	0.00	0.00	0.00	20.9
10	26	-0	48	0	0	0	-1165	--	--	16.08	16.08	0.29	0.02	0.00	0.00	0.00	0.00	20.9
11	26	-0	32	0	0	0	-1132	--	--	16.08	16.08	0.29	0.02	0.00	0.00	0.00	0.00	20.9
12	26	-0	129	0	0	0	-1098	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
13	26	-0	113	0	0	0	-1065	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
14	26	-0	94	0	0	0	-1181	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
15	26	-0	43	0	0	0	-1069	--	--	16.08	16.08	0.29	0.02	0.00	0.00	0.00	0.00	20.9
16	26	-0	118	0	0	0	-1161	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
17	26	-0	67	0	0	0	-1049	--	--	16.08	16.08	0.29	0.02	0.00	0.00	0.00	0.00	20.9
18	26	-0	-23	0	0	0	-1671	--	--	16.08	16.08	0.18	0.03	0.00	0.00	0.00	0.00	20.9
19	26	-0	213	0	0	0	-1437	--	--	16.08	16.08	0.18	0.02	0.00	0.01	0.00	0.00	20.9
20	26	-0	43	0	0	0	-1468	--	--	16.08	16.08	0.18	0.02	0.00	0.00	0.00	0.00	20.9
37	26	-0	-99	0	0	0	-1740	--	--	16.08	16.08	0.18	0.03	0.00	0.01	0.00	0.00	20.9
38	26	-0	295	0	0	0	-1318	--	--	16.08	16.08	0.18	0.02	0.00	0.02	0.00	0.00	20.9
39	26	-0	11	0	0	0	-1371	--	--	16.08	16.08	0.18	0.02	0.00	0.00	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	105	0	0	0	-1449	--	--	16.08	16.08	0.18	0.02	0.00	0.01	0.00	0.00	20.9
2	51	-0	48	0	0	0	-1165	--	--	16.08	16.08	0.29	0.02	0.00	0.00	0.00	0.00	20.9
3	51	-0	32	0	0	0	-1132	--	--	16.08	16.08	0.29	0.02	0.00	0.00	0.00	0.00	20.9
4	51	-0	129	0	0	0	-1098	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
5	51	-0	113	0	0	0	-1065	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
6	51	-0	94	0	0	0	-1181	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
7	51	-0	43	0	0	0	-1069	--	--	16.08	16.08	0.29	0.02	0.00	0.00	0.00	0.00	20.9
8	51	-0	118	0	0	0	-1161	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
9	51	-0	67	0	0	0	-1049	--	--	16.08	16.08	0.29	0.02	0.00	0.00	0.00	0.00	20.9
10	51	-0	48	0	0	0	-1165	--	--	16.08	16.08	0.29	0.02	0.00	0.00	0.00	0.00	20.9
11	51	-0	32	0	0	0	-1132	--	--	16.08	16.08	0.29	0.02	0.00	0.00	0.00	0.00	20.9
12	51	-0	129	0	0	0	-1098	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
13	51	-0	113	0	0	0	-1065	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
14	51	-0	94	0	0	0	-1181	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
15	51	-0	43	0	0	0	-1069	--	--	16.08	16.08	0.29	0.02	0.00	0.00	0.00	0.00	20.9
16	51	-0	118	0	0	0	-1161	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
17	51	-0	67	0	0	0	-1049	--	--	16.08	16.08	0.29	0.02	0.00	0.00	0.00	0.00	20.9
18	51	-0	-23	0	0	0	-1671	--	--	16.08	16.08	0.18	0.03	0.00	0.00	0.00	0.00	20.9
19	51	-0	213	0	0	0	-1437	--	--	16.08	16.08	0.18	0.02	0.00	0.01	0.00	0.00	20.9
20	51	-0	43	0	0	0	-1468	--	--	16.08	16.08	0.18	0.02	0.00	0.00	0.00	0.00	20.9
37	51	-0	-99	0	0	0	-1740	--	--	16.08	16.08	0.18	0.03	0.00	0.01	0.00	0.00	20.9
38	51	-0	295	0	0	0	-1318	--	--	16.08	16.08	0.18	0.02	0.00	0.02	0.00	0.00	20.9
39	51	-0	11	0	0	0	-1371	--	--	16.08	16.08	0.18	0.02	0.00	0.00	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 157 NI 1269 NF 1303 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	732	0	0	0	-1518	--	--	16.08	16.08	0.18	0.03	0.01	0.05	0.00	0.00	20.9
2	0	-0	539	0	0	0	-1225	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
3	0	-0	512	0	0	0	-1193	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
4	0	-0	614	0	0	0	-1142	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
5	0	-0	587	0	0	0	-1110	--	--	16.08	16.08	0.29	0.02	0.00	0.04	0.00	0.00	20.9
6	0	-0	597	0	0	0	-1233	--	--	16.08	16.08	0.29	0.02	0.00	0.04	0.00	0.00	20.9
7	0	-0	507	0	0	0	-1126	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
8	0	-0	619	0	0	0	-1208	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
9	0	-0	529	0	0	0	-1102	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
10	0	-0	539	0	0	0	-1225	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
11	0	-0	512	0	0	0	-1193	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
12	0	-0	614	0	0	0	-1142	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
13	0	-0	587	0	0	0	-1110	--	--	16.08	16.08	0.29	0.02	0.00	0.04	0.00	0.00	20.9
14	0	-0	597	0	0	0	-1233	--	--	16.08	16.08	0.29	0.02	0.00	0.04	0.00	0.00	20.9
15	0	-0	507	0	0	0	-1126	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
16	0	-0	619	0	0	0	-1208	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
17	0	-0	529	0	0	0	-1102	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
18	0	-0	656	0	0	0	-1758	--	--	16.08	16.08	0.18	0.03	0.01	0.04	0.00	0.00	20.9
19	0	-0	873	0	0	0	-1489	--	--	16.08	16.08	0.18	0.02	0.01	0.05	0.00	0.00	20.9
20	0	-0	694	0	0	0	-1551	--	--	16.08	16.08	0.18	0.03	0.01	0.04	0.00	0.00	20.9
37	0	-0	566	0	0	0	-1800	--	--	16.08	16.08	0.18	0.03	0.00	0.04	0.00	0.00	20.9
38	0	-0	927	0	0	0	-1351	--	--	16.08	16.08	0.18	0.02	0.01	0.06	0.00	0.00	20.9
39	0	-0	628	0	0	0	-1455	--	--	16.08	16.08	0.18	0.02	0.01	0.04	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	26	-0	732	0	0	0	-1518	--	--	16.08	16.08	0.18	0.03	0.01	0.05	0.00	0.00	20.9
2	26	-0	539	0	0	0	-1225	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
3	26	-0	512	0	0	0	-1193	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
4	26	-0	614	0	0	0	-1142	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
5	26	-0	587	0	0	0	-1110	--	--	16.08	16.08	0.29	0.02	0.00	0.04	0.00	0.00	20.9
6	26	-0	597	0	0	0	-1233	--	--	16.08	16.08	0.29	0.02	0.00	0.04	0.00	0.00	20.9
7	26	-0	507	0	0	0	-1126	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
8	26	-0	619	0	0	0	-1208	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
9	26	-0	529	0	0	0	-1102	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
10	26	-0	539	0	0	0	-1225	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
11	26	-0	512	0	0	0	-1193	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
12	26	-0	614	0	0	0	-1142	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
13	26	-0	587	0	0	0	-1110	--	--	16.08	16.08	0.29	0.02	0.00	0.04	0.00	0.00	20.9
14	26	-0	597	0	0	0	-1233	--	--	16.08	16.08	0.29	0.02	0.00	0.04	0.00	0.00	20.9
15	26	-0	507	0	0	0	-1126	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
16	26	-0	619	0	0	0	-1208	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
17	26	-0	529	0	0	0	-1102	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
18	26	-0	656	0	0	0	-1758	--	--	16.08	16.08	0.18	0.03	0.01	0.04	0.00	0.00	20.9
19	26	-0	873	0	0	0	-1489	--	--	16.08	16.08	0.18	0.02	0.01	0.05	0.00	0.00	20.9
20	26	-0	694	0	0	0	-1551	--	--	16.08	16.08	0.18	0.03	0.01	0.04	0.00	0.00	20.9
37	26	-0	566	0	0	0	-1800	--	--	16.08	16.08	0.18	0.03	0.00	0.04	0.00	0.00	20.9
38	26	-0	927	0	0	0	-1351	--	--	16.08	16.08	0.18	0.02	0.01	0.06	0.00	0.00	20.9
39	26	-0	628	0	0	0	-1455	--	--	16.08	16.08	0.18	0.02	0.01	0.04	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	51	-0	732	0	0	0	-1518	--	--	16.08	16.08	0.18	0.03	0.01	0.05	0.00	0.00	20.9
2	51	-0	539	0	0	0	-1225	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
3	51	-0	512	0	0	0	-1193	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
4	51	-0	614	0	0	0	-1142	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
5	51	-0	587	0	0	0	-1110	--	--	16.08	16.08	0.29	0.02	0.00	0.04	0.00	0.00	20.9
6	51	-0	597	0	0	0	-1233	--	--	16.08	16.08	0.29	0.02	0.00	0.04	0.00	0.00	20.9
7	51	-0	507	0	0	0	-1126	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
8	51	-0	619	0	0	0	-1208	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
9	51	-0	529	0	0	0	-1102	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
10	51	-0	539	0	0	0	-1225	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
11	51	-0	512	0	0	0	-1193	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
12	51	-0	614	0	0	0	-1142	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
13	51	-0	587	0	0	0	-1110	--	--	16.08	16.08	0.29	0.02	0.00	0.04	0.00	0.00	20.9
14	51	-0	597	0	0	0	-1233	--	--	16.08	16.08	0.29	0.02	0.00	0.04	0.00	0.00	20.9
15	51	-0	507	0	0	0	-1126	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
16	51	-0	619	0	0	0	-1208	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
17	51	-0	529	0	0	0	-1102	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
18	51	-0	656	0	0	0	-1758	--	--	16.08	16.08	0.18	0.03	0.01	0.04	0.00	0.00	20.9
19	51	-0	873	0	0	0	-1489	--	--	16.08	16.08	0.18	0.02	0.01	0.05	0.00	0.00	20.9
20	51	-0	694	0	0	0	-1551	--	--	16.08	16.08	0.18	0.03	0.01	0.04	0.00	0.00	20.9
37	51	-0	566	0	0	0	-1800	--	--	16.08	16.08	0.18	0.03	0.00	0.04	0.00	0.00	20.9
38	51	-0	927	0	0	0	-1351	--	--	16.08	16.08	0.18	0.02	0.01	0.06	0.00	0.00	20.9
39	51	-0	628	0	0	0	-1455	--	--	16.08	16.08	0.18	0.02	0.01	0.04	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 158 NI 1303 NF 1302 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	1462	0	0	0	-1455	--	--	16.08	16.08	0.18	0.02	0.01	0.09	0.00	0.00	20.9
2	0	-0	1116	0	0	0	-1182	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
3	0	-0	1074	0	0	0	-1154	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
4	0	-0	1176	0	0	0	-1085	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
5	0	-0	1134	0	0	0	-1057	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
6	0	-0	1185	0	0	0	-1180	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
7	0	-0	1047	0	0	0	-1087	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
8	0	-0	1203	0	0	0	-1151	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
9	0	-0	1065	0	0	0	-1058	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
10	0	-0	1116	0	0	0	-1182	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9

11	0	-0	1074	0	0	0	-1154	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
12	0	-0	1176	0	0	0	-1085	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
13	0	-0	1134	0	0	0	-1057	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
14	0	-0	1185	0	0	0	-1180	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
15	0	-0	1047	0	0	0	-1087	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
16	0	-0	1203	0	0	0	-1151	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
17	0	-0	1065	0	0	0	-1058	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
18	0	-0	1453	0	0	0	-1716	--	--	16.08	16.08	0.18	0.03	0.01	0.09	0.00	0.00	20.9
19	0	-0	1628	0	0	0	-1403	--	--	16.08	16.08	0.18	0.02	0.01	0.10	0.00	0.00	20.9
20	0	-0	1443	0	0	0	-1499	--	--	16.08	16.08	0.18	0.02	0.01	0.09	0.00	0.00	20.9
37	0	-0	1355	0	0	0	-1773	--	--	16.08	16.08	0.18	0.03	0.01	0.09	0.00	0.00	20.9
38	0	-0	1646	0	0	0	-1252	--	--	16.08	16.08	0.18	0.02	0.01	0.10	0.00	0.00	20.9
39	0	-0	1339	0	0	0	-1411	--	--	16.08	16.08	0.18	0.02	0.01	0.08	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	1462	0	0	0	-1455	--	--	16.08	16.08	0.18	0.02	0.01	0.09	0.00	0.00	20.9
2	26	-0	1116	0	0	0	-1182	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
3	26	-0	1074	0	0	0	-1154	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
4	26	-0	1176	0	0	0	-1085	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
5	26	-0	1134	0	0	0	-1057	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
6	26	-0	1185	0	0	0	-1180	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
7	26	-0	1047	0	0	0	-1087	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
8	26	-0	1203	0	0	0	-1151	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
9	26	-0	1065	0	0	0	-1058	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
10	26	-0	1116	0	0	0	-1182	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
11	26	-0	1074	0	0	0	-1154	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
12	26	-0	1176	0	0	0	-1085	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
13	26	-0	1134	0	0	0	-1057	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
14	26	-0	1185	0	0	0	-1180	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
15	26	-0	1047	0	0	0	-1087	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
16	26	-0	1203	0	0	0	-1151	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
17	26	-0	1065	0	0	0	-1058	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
18	26	-0	1453	0	0	0	-1716	--	--	16.08	16.08	0.18	0.03	0.01	0.09	0.00	0.00	20.9
19	26	-0	1628	0	0	0	-1403	--	--	16.08	16.08	0.18	0.02	0.01	0.10	0.00	0.00	20.9
20	26	-0	1443	0	0	0	-1499	--	--	16.08	16.08	0.18	0.02	0.01	0.09	0.00	0.00	20.9
37	26	-0	1355	0	0	0	-1773	--	--	16.08	16.08	0.18	0.03	0.01	0.09	0.00	0.00	20.9
38	26	-0	1646	0	0	0	-1252	--	--	16.08	16.08	0.18	0.02	0.01	0.10	0.00	0.00	20.9
39	26	-0	1339	0	0	0	-1411	--	--	16.08	16.08	0.18	0.02	0.01	0.08	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	1462	0	0	0	-1455	--	--	16.08	16.08	0.18	0.02	0.01	0.09	0.00	0.00	20.9
2	51	-0	1116	0	0	0	-1182	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
3	51	-0	1074	0	0	0	-1154	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
4	51	-0	1176	0	0	0	-1085	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
5	51	-0	1134	0	0	0	-1057	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
6	51	-0	1185	0	0	0	-1180	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
7	51	-0	1047	0	0	0	-1087	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
8	51	-0	1203	0	0	0	-1151	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
9	51	-0	1065	0	0	0	-1058	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
10	51	-0	1116	0	0	0	-1182	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
11	51	-0	1074	0	0	0	-1154	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
12	51	-0	1176	0	0	0	-1085	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
13	51	-0	1134	0	0	0	-1057	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
14	51	-0	1185	0	0	0	-1180	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
15	51	-0	1047	0	0	0	-1087	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
16	51	-0	1203	0	0	0	-1151	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
17	51	-0	1065	0	0	0	-1058	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
18	51	-0	1453	0	0	0	-1716	--	--	16.08	16.08	0.18	0.03	0.01	0.09	0.00	0.00	20.9
19	51	-0	1628	0	0	0	-1403	--	--	16.08	16.08	0.18	0.02	0.01	0.10	0.00	0.00	20.9
20	51	-0	1443	0	0	0	-1499	--	--	16.08	16.08	0.18	0.02	0.01	0.09	0.00	0.00	20.9
37	51	-0	1355	0	0	0	-1773	--	--	16.08	16.08	0.18	0.03	0.01	0.09	0.00	0.00	20.9
38	51	-0	1646	0	0	0	-1252	--	--	16.08	16.08	0.18	0.02	0.01	0.10	0.00	0.00	20.9
39	51	-0	1339	0	0	0	-1411	--	--	16.08	16.08	0.18	0.02	0.01	0.08	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 159 NI 1302 NF 1340 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm

1	0	-0	2084	0	0	0	-1273	--	--	16.08	16.08	0.18	0.02	0.02	0.13	0.00	0.00	20.9
2	0	-0	1614	0	0	0	-1046	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
3	0	-0	1562	0	0	0	-1024	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
4	0	-0	1645	0	0	0	-935	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
5	0	-0	1592	0	0	0	-913	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
6	0	-0	1686	0	0	0	-1032	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
7	0	-0	1511	0	0	0	-960	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
8	0	-0	1695	0	0	0	-999	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
9	0	-0	1521	0	0	0	-927	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
10	0	-0	1614	0	0	0	-1046	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
11	0	-0	1562	0	0	0	-1024	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
12	0	-0	1645	0	0	0	-935	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
13	0	-0	1592	0	0	0	-913	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
14	0	-0	1686	0	0	0	-1032	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
15	0	-0	1511	0	0	0	-960	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
16	0	-0	1695	0	0	0	-999	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
17	0	-0	1521	0	0	0	-927	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
18	0	-0	2128	0	0	0	-1554	--	--	16.08	16.08	0.18	0.03	0.02	0.13	0.00	0.00	20.9
19	0	-0	2224	0	0	0	-1196	--	--	16.08	16.08	0.18	0.02	0.02	0.14	0.00	0.00	20.9
20	0	-0	2068	0	0	0	-1327	--	--	16.08	16.08	0.18	0.02	0.02	0.13	0.00	0.00	20.9
37	0	-0	2045	0	0	0	-1629	--	--	16.08	16.08	0.18	0.03	0.02	0.13	0.00	0.00	20.9
38	0	-0	2205	0	0	0	-1032	--	--	16.08	16.08	0.18	0.02	0.02	0.14	0.00	0.00	20.9
39	0	-0	1945	0	0	0	-1252	--	--	16.08	16.08	0.18	0.02	0.02	0.12	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	2084	0	0	0	-1273	--	--	16.08	16.08	0.18	0.02	0.02	0.13	0.00	0.00	20.9
2	26	-0	1614	0	0	0	-1046	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
3	26	-0	1562	0	0	0	-1024	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
4	26	-0	1645	0	0	0	-935	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
5	26	-0	1592	0	0	0	-913	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
6	26	-0	1686	0	0	0	-1032	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9

7	26	-0	1511	0	0	0	-960	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
8	26	-0	1695	0	0	0	-999	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
9	26	-0	1521	0	0	0	-927	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
10	26	-0	1614	0	0	0	-1046	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
11	26	-0	1562	0	0	0	-1024	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
12	26	-0	1645	0	0	0	-935	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
13	26	-0	1592	0	0	0	-913	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
14	26	-0	1686	0	0	0	-1032	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
15	26	-0	1511	0	0	0	-960	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
16	26	-0	1695	0	0	0	-999	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
17	26	-0	1521	0	0	0	-927	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
18	26	-0	2128	0	0	0	-1554	--	--	16.08	16.08	0.18	0.03	0.02	0.13	0.00	0.00	20.9
19	26	-0	2224	0	0	0	-1196	--	--	16.08	16.08	0.18	0.02	0.02	0.14	0.00	0.00	20.9
20	26	-0	2068	0	0	0	-1327	--	--	16.08	16.08	0.18	0.02	0.02	0.13	0.00	0.00	20.9
37	26	-0	2045	0	0	0	-1629	--	--	16.08	16.08	0.18	0.03	0.02	0.13	0.00	0.00	20.9
38	26	-0	2205	0	0	0	-1032	--	--	16.08	16.08	0.18	0.02	0.02	0.14	0.00	0.00	20.9
39	26	-0	1945	0	0	0	-1252	--	--	16.08	16.08	0.18	0.02	0.02	0.12	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	2084	0	0	0	-1273	--	--	16.08	16.08	0.18	0.02	0.02	0.13	0.00	0.00	20.9
2	51	-0	1614	0	0	0	-1046	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
3	51	-0	1562	0	0	0	-1024	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
4	51	-0	1645	0	0	0	-935	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
5	51	-0	1592	0	0	0	-913	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
6	51	-0	1686	0	0	0	-1032	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
7	51	-0	1511	0	0	0	-960	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
8	51	-0	1695	0	0	0	-999	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
9	51	-0	1521	0	0	0	-927	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
10	51	-0	1614	0	0	0	-1046	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
11	51	-0	1562	0	0	0	-1024	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
12	51	-0	1645	0	0	0	-935	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
13	51	-0	1592	0	0	0	-913	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
14	51	-0	1686	0	0	0	-1032	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
15	51	-0	1511	0	0	0	-960	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
16	51	-0	1695	0	0	0	-999	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
17	51	-0	1521	0	0	0	-927	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
18	51	-0	2128	0	0	0	-1554	--	--	16.08	16.08	0.18	0.03	0.02	0.13	0.00	0.00	20.9
19	51	-0	2224	0	0	0	-1196	--	--	16.08	16.08	0.18	0.02	0.02	0.14	0.00	0.00	20.9
20	51	-0	2068	0	0	0	-1327	--	--	16.08	16.08	0.18	0.02	0.02	0.13	0.00	0.00	20.9
37	51	-0	2045	0	0	0	-1629	--	--	16.08	16.08	0.18	0.03	0.02	0.13	0.00	0.00	20.9
38	51	-0	2205	0	0	0	100	--	--	16.08	16.08	0.00	0.00	0.02	0.14	0.00	0.00	20.9
39	51	-0	1945	0	0	0	-1252	--	--	16.08	16.08	0.18	0.02	0.02	0.12	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 160 NI 1340 NF 1808 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	2087	0	0	0	-901	--	--	16.08	16.08	0.18	0.01	0.02	0.13	0.00	0.00	20.9
2	0	-0	1600	0	0	0	-774	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
3	0	-0	1559	0	0	0	-765	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
4	0	-0	1653	0	0	0	-621	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
5	0	-0	1611	0	0	0	-611	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
6	0	-0	1667	0	0	0	-732	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
7	0	-0	1529	0	0	0	-700	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
8	0	-0	1683	0	0	0	-686	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
9	0	-0	1545	0	0	0	-654	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
10	0	-0	1600	0	0	0	-774	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
11	0	-0	1559	0	0	0	-765	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
12	0	-0	1653	0	0	0	-621	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
13	0	-0	1611	0	0	0	-611	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
14	0	-0	1667	0	0	0	-732	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
15	0	-0	1529	0	0	0	-700	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
16	0	-0	1683	0	0	0	-686	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
17	0	-0	1545	0	0	0	-654	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
18	0	-0	2015	0	0	0	-1239	--	--	16.08	16.08	0.18	0.02	0.02	0.13	0.00	0.00	20.9
19	0	-0	2195	0	0	0	-746	--	--	16.08	16.08	0.18	0.01	0.02	0.14	0.00	0.00	20.9
20	0	-0	2044	0	0	0	-968	--	--	16.08	16.08	0.18	0.02	0.02	0.13	0.00	0.00	20.9
37	0	-0	1927	0	0	0	-1366	--	--	16.08	16.08	0.18	0.02	0.02	0.12	0.00	0.00	20.9
38	0	-0	2227	0	0	0	-545	--	--	16.08	16.08	0.18	0.01	0.02	0.14	0.00	0.00	20.9
39	0	-0	1976	0	0	0	-915	--	--	16.08	16.08	0.18	0.02	0.02	0.12	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	2087	0	0	0	-901	--	--	16.08	16.08	0.18	0.01	0.02	0.13	0.00	0.00	20.9
2	26	-0	1600	0	0	0	-774	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
3	26	-0	1559	0	0	0	-765	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
4	26	-0	1653	0	0	0	-621	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
5	26	-0	1611	0	0	0	-611	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
6	26	-0	1667	0	0	0	-732	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
7	26	-0	1529	0	0	0	-700	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
8	26	-0	1683	0	0	0	-686	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
9	26	-0	1545	0	0	0	-654	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
10	26	-0	1600	0	0	0	-774	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
11	26	-0	1559	0	0	0	-765	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
12	26	-0	1653	0	0	0	-621	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
13	26	-0	1611	0	0	0	-611	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
14	26	-0	1667	0	0	0	-732	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
15	26	-0	1529	0	0	0	-700	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
16	26	-0	1683	0	0	0	-686	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
17	26	-0	1545	0	0	0	-654	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
18	26	-0	2015	0	0	0	-1239	--	--	16.08	16.08	0.18	0.02	0.02	0.13	0.00	0.00	20.9
19	26	-0	2195	0	0	0	-746	--	--	16.08	16.08	0.18	0.01	0.02	0.14	0.00	0.00	20.9
20	26	-0	2044	0	0	0	-968	--	--	16.08	16.08	0.18	0.02	0.02	0.13	0.00	0.00	20.9
37	26	-0	1927	0	0	0	-1366	--	--	16.08	16.08	0.18	0.02	0.02	0.12	0.00	0.00	20.9
38	26	-0	2227	0	0	0	2407	--	--	16.08	16.08	0.00	0.04	0.02	0.14	0.00	0.00	20.9
39	26	-0	1976	0	0	0	-915	--	--	16.08	16.08	0.18	0.02	0.02	0.12	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	51	-0	2087	0	0	0	171	--	--	16.08	16.08	0.00	0.00	0.02	0.13	0.00	0.00	20.9
2	51	-0	1600	0	0	0	47	--	--	16.08	16.08	0.10	0.00	0.01	0.10	0.00	0.00	20.9

3	51	-0	1559	0	0	0	36	--	--	16.08	16.08	0.10	0.00	0.01	0.10	0.00	0.00	20.9
4	51	-0	1653	0	0	0	228	--	--	16.08	16.08	0.10	0.00	0.01	0.10	0.00	0.00	20.9
5	51	-0	1611	0	0	0	216	--	--	16.08	16.08	0.10	0.00	0.01	0.10	0.00	0.00	20.9
6	51	-0	1667	0	0	0	124	--	--	16.08	16.08	0.10	0.00	0.01	0.10	0.00	0.00	20.9
7	51	-0	1529	0	0	0	85	--	--	16.08	16.08	0.10	0.00	0.01	0.10	0.00	0.00	20.9
8	51	-0	1683	0	0	0	179	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
9	51	-0	1545	0	0	0	139	--	--	16.08	16.08	0.10	0.00	0.01	0.10	0.00	0.00	20.9
10	51	-0	1600	0	0	0	47	--	--	16.08	16.08	0.10	0.00	0.01	0.10	0.00	0.00	20.9
11	51	-0	1559	0	0	0	36	--	--	16.08	16.08	0.10	0.00	0.01	0.10	0.00	0.00	20.9
12	51	-0	1653	0	0	0	228	--	--	16.08	16.08	0.10	0.00	0.01	0.10	0.00	0.00	20.9
13	51	-0	1611	0	0	0	216	--	--	16.08	16.08	0.10	0.00	0.01	0.10	0.00	0.00	20.9
14	51	-0	1667	0	0	0	124	--	--	16.08	16.08	0.10	0.00	0.01	0.10	0.00	0.00	20.9
15	51	-0	1529	0	0	0	85	--	--	16.08	16.08	0.10	0.00	0.01	0.10	0.00	0.00	20.9
16	51	-0	1683	0	0	0	179	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
17	51	-0	1545	0	0	0	139	--	--	16.08	16.08	0.10	0.00	0.01	0.10	0.00	0.00	20.9
18	51	-0	2015	0	0	0	-1239	--	--	16.08	16.08	0.18	0.02	0.02	0.13	0.00	0.00	20.9
19	51	-0	2195	0	0	0	381	--	--	16.08	16.08	0.00	0.01	0.02	0.14	0.00	0.00	20.9
20	51	-0	2044	0	0	0	82	--	--	16.08	16.08	0.00	0.00	0.02	0.13	0.00	0.00	20.9
37	51	-0	1927	0	0	0	-1366	--	--	16.08	16.08	0.18	0.02	0.02	0.12	0.00	0.00	20.9
38	51	-0	2227	0	0	0	599	--	--	16.08	16.08	0.00	0.01	0.02	0.14	0.00	0.00	20.9
39	51	-0	1976	0	0	0	99	--	--	16.08	16.08	0.00	0.00	0.02	0.12	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 161 NI 1678 NF 1679 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-503	0	0	0	-201	--	--	16.08	16.08	0.18	0.00	0.00	0.03	0.00	0.00	20.9
2	0	-0	-532	0	0	0	-213	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
3	0	-0	-523	0	0	0	-209	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
4	0	-0	-251	0	0	0	-101	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
5	0	-0	-243	0	0	0	-97	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
6	0	-0	-443	0	0	0	-177	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
7	0	-0	-415	0	0	0	-166	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
8	0	-0	-359	0	0	0	-144	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
9	0	-0	-331	0	0	0	-132	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
10	0	-0	-532	0	0	0	-213	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
11	0	-0	-523	0	0	0	-209	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
12	0	-0	-251	0	0	0	-101	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
13	0	-0	-243	0	0	0	-97	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
14	0	-0	-443	0	0	0	-177	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
15	0	-0	-415	0	0	0	-166	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
16	0	-0	-359	0	0	0	-144	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
17	0	-0	-331	0	0	0	-132	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
18	0	-0	-2265	0	0	0	-906	--	--	16.08	16.08	0.18	0.02	0.02	0.14	0.00	0.00	20.9
19	0	-0	-732	0	0	0	-293	--	--	16.08	16.08	0.18	0.00	0.01	0.05	0.00	0.00	20.9
20	0	-0	-1348	0	0	0	-539	--	--	16.08	16.08	0.18	0.01	0.01	0.08	0.00	0.00	20.9
37	0	-0	-2450	0	0	0	-980	--	--	16.08	16.08	0.18	0.02	0.02	0.15	0.00	0.00	20.9
38	0	-0	106	0	0	0	-113	--	--	16.08	16.08	0.18	0.00	0.00	0.01	0.00	0.00	20.9
39	0	-0	-921	0	0	0	-369	--	--	16.08	16.08	0.18	0.01	0.01	0.06	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	20	-0	-503	0	0	0	-201	--	--	16.08	16.08	0.18	0.00	0.00	0.03	0.00	0.00	20.9
2	20	-0	-532	0	0	0	-213	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
3	20	-0	-523	0	0	0	-209	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
4	20	-0	-251	0	0	0	-101	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
5	20	-0	-243	0	0	0	-97	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
6	20	-0	-443	0	0	0	-177	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
7	20	-0	-415	0	0	0	-166	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
8	20	-0	-359	0	0	0	-144	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
9	20	-0	-331	0	0	0	-132	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
10	20	-0	-532	0	0	0	-213	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
11	20	-0	-523	0	0	0	-209	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
12	20	-0	-251	0	0	0	-101	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
13	20	-0	-243	0	0	0	-97	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
14	20	-0	-443	0	0	0	-177	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
15	20	-0	-415	0	0	0	-166	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
16	20	-0	-359	0	0	0	-144	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
17	20	-0	-331	0	0	0	-132	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
18	20	-0	-2265	0	0	0	-906	--	--	16.08	16.08	0.18	0.02	0.02	0.14	0.00	0.00	20.9
19	20	-0	-732	0	0	0	-293	--	--	16.08	16.08	0.18	0.00	0.01	0.05	0.00	0.00	20.9
20	20	-0	-1348	0	0	0	-539	--	--	16.08	16.08	0.18	0.01	0.01	0.08	0.00	0.00	20.9
37	20	-0	-2450	0	0	0	-980	--	--	16.08	16.08	0.18	0.02	0.02	0.15	0.00	0.00	20.9
38	20	-0	106	0	0	0	134	--	--	16.08	16.08	0.00	0.00	0.00	0.01	0.00	0.00	20.9
39	20	-0	-921	0	0	0	-369	--	--	16.08	16.08	0.18	0.01	0.01	0.06	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	40	-0	-503	0	0	0	-201	--	--	16.08	16.08	0.18	0.00	0.00	0.03	0.00	0.00	20.9
2	40	-0	-532	0	0	0	-213	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
3	40	-0	-523	0	0	0	-209	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
4	40	-0	-251	0	0	0	-101	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
5	40	-0	-243	0	0	0	-97	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
6	40	-0	-443	0	0	0	-177	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
7	40	-0	-415	0	0	0	-166	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
8	40	-0	-359	0	0	0	-144	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
9	40	-0	-331	0	0	0	-132	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
10	40	-0	-532	0	0	0	-213	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
11	40	-0	-523	0	0	0	-209	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
12	40	-0	-251	0	0	0	-101	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
13	40	-0	-243	0	0	0	-97	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
14	40	-0	-443	0	0	0	-177	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
15	40	-0	-415	0	0	0	-166	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
16	40	-0	-359	0	0	0	-144	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
17	40	-0	-331	0	0	0	-132	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
18	40	-0	-2265	0	0	0	-906	--	--	16.08	16.08	0.18	0.02	0.02	0.14	0.00	0.00	20.9
19	40	-0	-732	0	0	0	-293	--	--	16.08	16.08	0.18	0.00	0.01	0.05	0.00	0.00	20.9
20	40	-0	-1348	0	0	0	-539	--	--	16.08	16.08	0.18	0.01	0.01	0.08	0.00	0.00	20.9
37	40	-0	-2450	0	0	0	-980	--	--	16.08	16.08	0.18	0.02	0.02	0.15	0.00	0.00	20.9
38	40	-0	106	0	0	0	42	--	--	16.08	16.08	0.00	0.00	0.00	0.01	0.00	0.00	20.9
39	40	-0	-921	0	0	0	-369	--	--	16.08	16.08	0.18	0.01	0.01	0.06	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 162 NI 1679 NF 1680 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-859	0	0	0	-631	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9
2	0	-0	-1039	0	0	0	-732	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
3	0	-0	-1018	0	0	0	-718	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
4	0	-0	-304	0	0	0	-252	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
5	0	-0	-282	0	0	0	-238	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
6	0	-0	-806	0	0	0	-581	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
7	0	-0	-736	0	0	0	-534	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
8	0	-0	-586	0	0	0	-437	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
9	0	-0	-515	0	0	0	-390	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
10	0	-0	-1039	0	0	0	-732	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
11	0	-0	-1018	0	0	0	-718	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
12	0	-0	-304	0	0	0	-252	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
13	0	-0	-282	0	0	0	-238	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
14	0	-0	-806	0	0	0	-581	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
15	0	-0	-736	0	0	0	-534	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
16	0	-0	-586	0	0	0	-437	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
17	0	-0	-515	0	0	0	-390	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
18	0	-0	-5422	0	0	0	-3617	--	--	16.08	16.08	0.18	0.06	0.04	0.34	0.00	0.00	20.9
19	0	-0	-1339	0	0	0	-962	--	--	16.08	16.08	0.18	0.02	0.01	0.08	0.00	0.00	20.9
20	0	-0	-3019	0	0	0	-2049	--	--	16.08	16.08	0.18	0.03	0.02	0.19	0.00	0.00	20.9
37	0	-0	-5955	0	0	0	-3957	--	--	16.08	16.08	0.18	0.07	0.05	0.37	0.00	0.00	20.9
38	0	-0	849	0	0	0	42	--	--	16.08	16.08	0.00	0.00	0.01	0.05	0.00	0.00	20.9
39	0	-0	-1951	0	0	0	-1344	--	--	16.08	16.08	0.18	0.02	0.02	0.12	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	25	-0	-859	0	0	0	-631	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9
2	25	-0	-1039	0	0	0	-732	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
3	25	-0	-1018	0	0	0	-718	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
4	25	-0	-304	0	0	0	-252	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
5	25	-0	-282	0	0	0	-238	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
6	25	-0	-806	0	0	0	-581	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
7	25	-0	-736	0	0	0	-534	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
8	25	-0	-586	0	0	0	-437	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
9	25	-0	-515	0	0	0	-390	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
10	25	-0	-1039	0	0	0	-732	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
11	25	-0	-1018	0	0	0	-718	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
12	25	-0	-304	0	0	0	-252	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
13	25	-0	-282	0	0	0	-238	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
14	25	-0	-806	0	0	0	-581	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
15	25	-0	-736	0	0	0	-534	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
16	25	-0	-586	0	0	0	-437	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
17	25	-0	-515	0	0	0	-390	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
18	25	-0	-5422	0	0	0	-3617	--	--	16.08	16.08	0.18	0.06	0.04	0.34	0.00	0.00	20.9
19	25	-0	-1339	0	0	0	-962	--	--	16.08	16.08	0.18	0.02	0.01	0.08	0.00	0.00	20.9
20	25	-0	-3019	0	0	0	-2049	--	--	16.08	16.08	0.18	0.03	0.02	0.19	0.00	0.00	20.9
37	25	-0	-5955	0	0	0	-3957	--	--	16.08	16.08	0.18	0.07	0.05	0.37	0.00	0.00	20.9
38	25	-0	849	0	0	0	1162	--	--	16.08	16.08	0.00	0.02	0.01	0.05	0.00	0.00	20.9
39	25	-0	-1951	0	0	0	-1344	--	--	16.08	16.08	0.18	0.02	0.02	0.12	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	50	-0	-859	0	0	0	-631	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9
2	50	-0	-1039	0	0	0	-732	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
3	50	-0	-1018	0	0	0	-718	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
4	50	-0	-304	0	0	0	-252	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
5	50	-0	-282	0	0	0	-238	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
6	50	-0	-806	0	0	0	-581	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
7	50	-0	-736	0	0	0	-534	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
8	50	-0	-586	0	0	0	-437	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
9	50	-0	-515	0	0	0	-390	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
10	50	-0	-1039	0	0	0	-732	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
11	50	-0	-1018	0	0	0	-718	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
12	50	-0	-304	0	0	0	-252	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
13	50	-0	-282	0	0	0	-238	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
14	50	-0	-806	0	0	0	-581	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
15	50	-0	-736	0	0	0	-534	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
16	50	-0	-586	0	0	0	-437	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
17	50	-0	-515	0	0	0	-390	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
18	50	-0	-5422	0	0	0	-3617	--	--	16.08	16.08	0.18	0.06	0.04	0.34	0.00	0.00	20.9
19	50	-0	-1339	0	0	0	-962	--	--	16.08	16.08	0.18	0.02	0.01	0.08	0.00	0.00	20.9
20	50	-0	-3019	0	0	0	-2049	--	--	16.08	16.08	0.18	0.03	0.02	0.19	0.00	0.00	20.9
37	50	-0	-5955	0	0	0	-3957	--	--	16.08	16.08	0.18	0.07	0.05	0.37	0.00	0.00	20.9
38	50	-0	849	0	0	0	467	--	--	16.08	16.08	0.00	0.01	0.01	0.05	0.00	0.00	20.9
39	50	-0	-1951	0	0	0	-1344	--	--	16.08	16.08	0.18	0.02	0.02	0.12	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 163 NI 1680 NF 1681 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-175	0	0	0	-718	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9
2	0	-0	-648	0	0	0	-1056	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
3	0	-0	-621	0	0	0	-1029	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
4	0	-0	352	0	0	0	-252	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
5	0	-0	379	0	0	0	-238	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
6	0	-0	-329	0	0	0	-745	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
7	0	-0	-240	0	0	0	-654	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
8	0	-0	-29	0	0	0	-451	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
9	0	-0	60	0	0	0	-390	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
10	0	-0	-648	0	0	0	-1056	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9

11	0	-0	-621	0	0	0	-1029	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
12	0	-0	352	0	0	0	-252	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
13	0	-0	379	0	0	0	-238	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
14	0	-0	-329	0	0	0	-745	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
15	0	-0	-240	0	0	0	-654	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
16	0	-0	-29	0	0	0	-451	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
17	0	-0	60	0	0	0	-390	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
18	0	-0	-6239	0	0	0	-6736	--	--	16.08	16.08	0.18	0.11	0.05	0.39	0.00	0.00	20.9
19	0	-0	-572	0	0	0	-1248	--	--	16.08	16.08	0.18	0.02	0.00	0.04	0.00	0.00	20.9
20	0	-0	-2986	0	0	0	-3542	--	--	16.08	16.08	0.18	0.06	0.02	0.19	0.00	0.00	20.9
37	0	-0	-7066	0	0	0	-7490	--	--	16.08	16.08	0.18	0.12	0.06	0.44	0.00	0.00	20.9
38	0	-0	2380	0	0	0	467	--	--	16.08	16.08	0.00	0.01	0.02	0.15	0.00	0.00	20.9
39	0	-0	-1645	0	0	0	-2166	--	--	16.08	16.08	0.18	0.04	0.01	0.10	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	25	-0	-175	0	0	0	-718	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9
2	25	-0	-648	0	0	0	-1056	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
3	25	-0	-621	0	0	0	-1029	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
4	25	-0	352	0	0	0	-252	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
5	25	-0	379	0	0	0	-238	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
6	25	-0	-329	0	0	0	-745	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
7	25	-0	-240	0	0	0	-654	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
8	25	-0	-29	0	0	0	-451	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
9	25	-0	60	0	0	0	-390	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
10	25	-0	-648	0	0	0	-1056	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
11	25	-0	-621	0	0	0	-1029	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
12	25	-0	352	0	0	0	-252	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
13	25	-0	379	0	0	0	-238	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
14	25	-0	-329	0	0	0	-745	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
15	25	-0	-240	0	0	0	-654	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
16	25	-0	-29	0	0	0	-451	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
17	25	-0	60	0	0	0	-390	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
18	25	-0	-6239	0	0	0	-6736	--	--	16.08	16.08	0.18	0.11	0.05	0.39	0.00	0.00	20.9
19	25	-0	-572	0	0	0	-1248	--	--	16.08	16.08	0.18	0.02	0.00	0.04	0.00	0.00	20.9
20	25	-0	-2986	0	0	0	-3542	--	--	16.08	16.08	0.18	0.06	0.02	0.19	0.00	0.00	20.9
37	25	-0	-7066	0	0	0	-7490	--	--	16.08	16.08	0.18	0.12	0.06	0.44	0.00	0.00	20.9
38	25	-0	2380	0	0	0	3606	--	--	16.08	16.08	0.00	0.06	0.02	0.15	0.00	0.00	20.9
39	25	-0	-1645	0	0	0	-2166	--	--	16.08	16.08	0.18	0.04	0.01	0.10	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	50	-0	-175	0	0	0	-718	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9
2	50	-0	-648	0	0	0	-1056	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
3	50	-0	-621	0	0	0	-1029	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
4	50	-0	352	0	0	0	-252	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
5	50	-0	379	0	0	0	-238	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
6	50	-0	-329	0	0	0	-745	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
7	50	-0	-240	0	0	0	-654	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
8	50	-0	-29	0	0	0	-451	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
9	50	-0	60	0	0	0	-390	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
10	50	-0	-648	0	0	0	-1056	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
11	50	-0	-621	0	0	0	-1029	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
12	50	-0	352	0	0	0	-252	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
13	50	-0	379	0	0	0	-238	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
14	50	-0	-329	0	0	0	-745	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
15	50	-0	-240	0	0	0	-654	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
16	50	-0	-29	0	0	0	-451	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
17	50	-0	60	0	0	0	-390	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
18	50	-0	-6239	0	0	0	-6736	--	--	16.08	16.08	0.18	0.11	0.05	0.39	0.00	0.00	20.9
19	50	-0	-572	0	0	0	-1248	--	--	16.08	16.08	0.18	0.02	0.00	0.04	0.00	0.00	20.9
20	50	-0	-2986	0	0	0	-3542	--	--	16.08	16.08	0.18	0.06	0.02	0.19	0.00	0.00	20.9
37	50	-0	-7066	0	0	0	-7490	--	--	16.08	16.08	0.18	0.12	0.06	0.44	0.00	0.00	20.9
38	50	-0	2380	0	0	0	1657	--	--	16.08	16.08	0.00	0.03	0.02	0.15	0.00	0.00	20.9
39	50	-0	-1645	0	0	0	-2166	--	--	16.08	16.08	0.18	0.04	0.01	0.10	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 164 NI 1681 NF 1682 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-8621	0	0	0	2235	--	--	16.08	16.08	0.00	0.04	0.07	0.54	0.00	0.00	20.9
2	0	-0	-6668	0	0	0	1700	--	--	16.08	16.08	0.10	0.03	0.05	0.42	0.00	0.00	20.9
3	0	-0	-6681	0	0	0	1666	--	--	16.08	16.08	0.10	0.03	0.06	0.42	0.00	0.00	20.9
4	0	-0	-6582	0	0	0	1772	--	--	16.08	16.08	0.10	0.03	0.05	0.41	0.00	0.00	20.9
5	0	-0	-6596	0	0	0	1738	--	--	16.08	16.08	0.10	0.03	0.05	0.41	0.00	0.00	20.9
6	0	-0	-6622	0	0	0	1765	--	--	16.08	16.08	0.10	0.03	0.05	0.42	0.00	0.00	20.9
7	0	-0	-6667	0	0	0	1651	--	--	16.08	16.08	0.10	0.03	0.05	0.42	0.00	0.00	20.9
8	0	-0	-6596	0	0	0	1787	--	--	16.08	16.08	0.10	0.03	0.05	0.41	0.00	0.00	20.9
9	0	-0	-6642	0	0	0	1673	--	--	16.08	16.08	0.10	0.03	0.05	0.42	0.00	0.00	20.9
10	0	-0	-6668	0	0	0	1700	--	--	16.08	16.08	0.10	0.03	0.05	0.42	0.00	0.00	20.9
11	0	-0	-6681	0	0	0	1666	--	--	16.08	16.08	0.10	0.03	0.06	0.42	0.00	0.00	20.9
12	0	-0	-6582	0	0	0	1772	--	--	16.08	16.08	0.10	0.03	0.05	0.41	0.00	0.00	20.9
13	0	-0	-6596	0	0	0	1738	--	--	16.08	16.08	0.10	0.03	0.05	0.41	0.00	0.00	20.9
14	0	-0	-6622	0	0	0	1765	--	--	16.08	16.08	0.10	0.03	0.05	0.42	0.00	0.00	20.9
15	0	-0	-6667	0	0	0	1651	--	--	16.08	16.08	0.10	0.03	0.05	0.42	0.00	0.00	20.9
16	0	-0	-6596	0	0	0	1787	--	--	16.08	16.08	0.10	0.03	0.05	0.41	0.00	0.00	20.9
17	0	-0	-6642	0	0	0	1673	--	--	16.08	16.08	0.10	0.03	0.05	0.42	0.00	0.00	20.9
18	0	-0	-10270	0	0	0	2922	--	--	16.08	16.08	0.00	0.05	0.08	0.64	0.00	0.00	20.9
19	0	-0	-11180	0	0	0	2850	--	--	16.08	16.08	0.00	0.05	0.09	0.70	0.00	0.00	20.9
20	0	-0	-10560	0	0	0	2671	--	--	16.08	16.08	0.00	0.05	0.09	0.66	0.00	0.00	20.9
37	0	-0	-9297	0	0	0	2735	--	--	16.08	16.08	0.00	0.05	0.08	0.58	0.00	0.00	20.9
38	0	-0	-10810	0	0	0	2614	--	--	16.08	16.08	0.00	0.04	0.09	0.68	0.00	0.00	20.9
39	0	-0	-9779	0	0	0	2316	--	--	16.08	16.08	0.00	0.04	0.08	0.61	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	10	-0	-8621	0	0	0	2235	--	--	16.08	16.08	0.00	0.04	0.07	0.54	0.00	0.00	20.9
2	10	-0	-6668	0	0	0	1700	--	--	16.08	16.08	0.10	0.03	0.05	0.42	0.00	0.00	20.9
3	10	-0	-6681	0	0	0	1666	--	--	16.08	16.08	0.10	0.03	0.06	0.42	0.00	0.00	20.9
4	10	-0	-6582	0	0	0	1772	--	--	16.08	16.08	0.10	0.03	0.05	0.41	0.00	0.00	20.9
5	10	-0	-6596	0	0	0	1738	--	--	16.08	16.08	0.10	0.03	0.05	0.41	0.00	0.00	20.9
6	10	-0	-6622	0	0	0	1765	--	--	16.08	16.08	0.10	0.03	0.05	0.42	0.00	0.00	20.9

7	10	-0	-6667	0	0	0	1651	--	--	16.08	16.08	0.10	0.03	0.05	0.42	0.00	0.00	20.9
8	10	-0	-6596	0	0	0	1787	--	--	16.08	16.08	0.10	0.03	0.05	0.41	0.00	0.00	20.9
9	10	-0	-6642	0	0	0	1673	--	--	16.08	16.08	0.10	0.03	0.05	0.42	0.00	0.00	20.9
10	10	-0	-6668	0	0	0	1700	--	--	16.08	16.08	0.10	0.03	0.05	0.42	0.00	0.00	20.9
11	10	-0	-6681	0	0	0	1666	--	--	16.08	16.08	0.10	0.03	0.06	0.42	0.00	0.00	20.9
12	10	-0	-6582	0	0	0	1772	--	--	16.08	16.08	0.10	0.03	0.05	0.41	0.00	0.00	20.9
13	10	-0	-6596	0	0	0	1738	--	--	16.08	16.08	0.10	0.03	0.05	0.41	0.00	0.00	20.9
14	10	-0	-6622	0	0	0	1765	--	--	16.08	16.08	0.10	0.03	0.05	0.42	0.00	0.00	20.9
15	10	-0	-6667	0	0	0	1651	--	--	16.08	16.08	0.10	0.03	0.05	0.42	0.00	0.00	20.9
16	10	-0	-6596	0	0	0	1787	--	--	16.08	16.08	0.10	0.03	0.05	0.41	0.00	0.00	20.9
17	10	-0	-6642	0	0	0	1673	--	--	16.08	16.08	0.10	0.03	0.05	0.42	0.00	0.00	20.9
18	10	-0	-10270	0	0	0	2922	--	--	16.08	16.08	0.00	0.05	0.08	0.64	0.00	0.00	20.9
19	10	-0	-11180	0	0	0	2850	--	--	16.08	16.08	0.00	0.05	0.09	0.70	0.00	0.00	20.9
20	10	-0	-10560	0	0	0	2671	--	--	16.08	16.08	0.00	0.05	0.09	0.66	0.00	0.00	20.9
37	10	-0	-9297	0	0	0	2735	--	--	16.08	16.08	0.00	0.05	0.08	0.58	0.00	0.00	20.9
38	10	-0	-10810	0	0	0	2614	--	--	16.08	16.08	0.00	0.04	0.09	0.68	0.00	0.00	20.9
39	10	-0	-9779	0	0	0	2316	--	--	16.08	16.08	0.00	0.04	0.08	0.61	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	20	-0	-8621	0	0	0	510	--	--	16.08	16.08	0.00	0.01	0.07	0.54	0.00	0.00	20.9
2	20	-0	-6668	0	0	0	366	--	--	16.08	16.08	0.10	0.01	0.05	0.42	0.00	0.00	20.9
3	20	-0	-6681	0	0	0	329	--	--	16.08	16.08	0.10	0.01	0.06	0.42	0.00	0.00	20.9
4	20	-0	-6582	0	0	0	456	--	--	16.08	16.08	0.10	0.01	0.05	0.41	0.00	0.00	20.9
5	20	-0	-6596	0	0	0	419	--	--	16.08	16.08	0.10	0.01	0.05	0.41	0.00	0.00	20.9
6	20	-0	-6622	0	0	0	441	--	--	16.08	16.08	0.10	0.01	0.05	0.42	0.00	0.00	20.9
7	20	-0	-6667	0	0	0	318	--	--	16.08	16.08	0.10	0.01	0.05	0.42	0.00	0.00	20.9
8	20	-0	-6596	0	0	0	467	--	--	16.08	16.08	0.10	0.01	0.05	0.41	0.00	0.00	20.9
9	20	-0	-6642	0	0	0	344	--	--	16.08	16.08	0.10	0.01	0.05	0.42	0.00	0.00	20.9
10	20	-0	-6668	0	0	0	366	--	--	16.08	16.08	0.10	0.01	0.05	0.42	0.00	0.00	20.9
11	20	-0	-6681	0	0	0	329	--	--	16.08	16.08	0.10	0.01	0.06	0.42	0.00	0.00	20.9
12	20	-0	-6582	0	0	0	456	--	--	16.08	16.08	0.10	0.01	0.05	0.41	0.00	0.00	20.9
13	20	-0	-6596	0	0	0	419	--	--	16.08	16.08	0.10	0.01	0.05	0.41	0.00	0.00	20.9
14	20	-0	-6622	0	0	0	441	--	--	16.08	16.08	0.10	0.01	0.05	0.42	0.00	0.00	20.9
15	20	-0	-6667	0	0	0	318	--	--	16.08	16.08	0.10	0.01	0.05	0.42	0.00	0.00	20.9
16	20	-0	-6596	0	0	0	467	--	--	16.08	16.08	0.10	0.01	0.05	0.41	0.00	0.00	20.9
17	20	-0	-6642	0	0	0	344	--	--	16.08	16.08	0.10	0.01	0.05	0.42	0.00	0.00	20.9
18	20	-0	-10270	0	0	0	868	--	--	16.08	16.08	0.00	0.01	0.08	0.64	0.00	0.00	20.9
19	20	-0	-11180	0	0	0	614	--	--	16.08	16.08	0.00	0.01	0.09	0.70	0.00	0.00	20.9
20	20	-0	-10560	0	0	0	559	--	--	16.08	16.08	0.00	0.01	0.09	0.66	0.00	0.00	20.9
37	20	-0	-9297	0	0	0	875	--	--	16.08	16.08	0.00	0.01	0.08	0.58	0.00	0.00	20.9
38	20	-0	-10810	0	0	0	452	--	--	16.08	16.08	0.00	0.01	0.09	0.68	0.00	0.00	20.9
39	20	-0	-9779	0	0	0	360	--	--	16.08	16.08	0.00	0.01	0.08	0.61	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 165 NI 1682 NF 1677 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm

1	0	-0	-525	0	0	0	105	--	--	16.08	16.08	0.00	0.00	0.00	0.03	0.00	0.00	20.9
2	0	-0	-422	0	0	0	85	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
3	0	-0	-420	0	0	0	84	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
4	0	-0	-387	0	0	0	77	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
5	0	-0	-385	0	0	0	77	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
6	0	-0	-412	0	0	0	82	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
7	0	-0	-406	0	0	0	81	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
8	0	-0	-402	0	0	0	80	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
9	0	-0	-395	0	0	0	79	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
10	0	-0	-422	0	0	0	85	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
11	0	-0	-420	0	0	0	84	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
12	0	-0	-387	0	0	0	77	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
13	0	-0	-385	0	0	0	77	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
14	0	-0	-412	0	0	0	82	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
15	0	-0	-406	0	0	0	81	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
16	0	-0	-402	0	0	0	80	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
17	0	-0	-395	0	0	0	79	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
18	0	-0	-812	0	0	0	162	--	--	16.08	16.08	0.00	0.00	0.01	0.05	0.00	0.00	20.9
19	0	-0	-673	0	0	0	135	--	--	16.08	16.08	0.00	0.00	0.01	0.04	0.00	0.00	20.9
20	0	-0	-690	0	0	0	138	--	--	16.08	16.08	0.00	0.00	0.01	0.04	0.00	0.00	20.9
37	0	-0	-788	0	0	0	158	--	--	16.08	16.08	0.00	0.00	0.01	0.05	0.00	0.00	20.9
38	0	-0	-556	0	0	0	111	--	--	16.08	16.08	0.00	0.00	0.00	0.03	0.00	0.00	20.9
39	0	-0	-584	0	0	0	117	--	--	16.08	16.08	0.00	0.00	0.00	0.04	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	10	-0	-525	0	0	0	105	--	--	16.08	16.08	0.00	0.00	0.00	0.03	0.00	0.00	20.9
2	10	-0	-422	0	0	0	85	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
3	10	-0	-420	0	0	0	84	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
4	10	-0	-387	0	0	0	77	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
5	10	-0	-385	0	0	0	77	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
6	10	-0	-412	0	0	0	82	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
7	10	-0	-406	0	0	0	81	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
8	10	-0	-402	0	0	0	80	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
9	10	-0	-395	0	0	0	79	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
10	10	-0	-422	0	0	0	85	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
11	10	-0	-420	0	0	0	84	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
12	10	-0	-387	0	0	0	77	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
13	10	-0	-385	0	0	0	77	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
14	10	-0	-412	0	0	0	82	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
15	10	-0	-406	0	0	0	81	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
16	10	-0	-402	0	0	0	80	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
17	10	-0	-395	0	0	0	79	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
18	10	-0	-812	0	0	0	162	--	--	16.08	16.08	0.00	0.00	0.01	0.05	0.00	0.00	20.9
19	10	-0	-673	0	0	0	135	--	--	16.08	16.08	0.00	0.00	0.01	0.04	0.00	0.00	20.9
20	10	-0	-690	0	0	0	138	--	--	16.08	16.08	0.00	0.00	0.01	0.04	0.00	0.00	20.9
37	10	-0	-788	0	0	0	158	--	--	16.08	16.08	0.00	0.00	0.01	0.05	0.00	0.00	20.9
38	10	-0	-556	0	0	0	111	--	--	16.08	16.08	0.00	0.00	0.00	0.03	0.00	0.00	20.9
39	10	-0	-584	0	0	0	117	--	--	16.08	16.08	0.00	0.00	0.00	0.04	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	20	-0	-525	0	0	0	-561	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9
2	20	-0	-422	0	0	0	-452	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9

3	20	-0	-420	0	0	0	-449	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
4	20	-0	-387	0	0	0	-414	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
5	20	-0	-385	0	0	0	-412	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
6	20	-0	-412	0	0	0	-441	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
7	20	-0	-406	0	0	0	-434	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
8	20	-0	-402	0	0	0	-430	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
9	20	-0	-395	0	0	0	-422	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
10	20	-0	-422	0	0	0	-452	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
11	20	-0	-420	0	0	0	-449	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
12	20	-0	-387	0	0	0	-414	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
13	20	-0	-385	0	0	0	-412	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
14	20	-0	-412	0	0	0	-441	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
15	20	-0	-406	0	0	0	-434	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
16	20	-0	-402	0	0	0	-430	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
17	20	-0	-395	0	0	0	-422	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
18	20	-0	-812	0	0	0	-868	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9
19	20	-0	-673	0	0	0	-719	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
20	20	-0	-690	0	0	0	-737	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
37	20	-0	-788	0	0	0	-842	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9
38	20	-0	-556	0	0	0	-594	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9
39	20	-0	-584	0	0	0	-624	--	--	16.08	16.08	0.18	0.01	0.00	0.04	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 166 NI 1566 NF 1565 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	730	0	0	0	-780	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9
2	0	-0	463	0	0	0	-495	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
3	0	-0	453	0	0	0	-484	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
4	0	-0	670	0	0	0	-716	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
5	0	-0	660	0	0	0	-705	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
6	0	-0	546	0	0	0	-584	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
7	0	-0	514	0	0	0	-550	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
8	0	-0	608	0	0	0	-650	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
9	0	-0	576	0	0	0	-616	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
10	0	-0	463	0	0	0	-495	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
11	0	-0	453	0	0	0	-484	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
12	0	-0	670	0	0	0	-716	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
13	0	-0	660	0	0	0	-705	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
14	0	-0	546	0	0	0	-584	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
15	0	-0	514	0	0	0	-550	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
16	0	-0	608	0	0	0	-650	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
17	0	-0	576	0	0	0	-616	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
18	0	-0	855	0	0	0	-914	--	--	16.08	16.08	0.18	0.02	0.01	0.05	0.00	0.00	20.9
19	0	-0	1915	0	0	0	-2047	--	--	16.08	16.08	0.18	0.03	0.02	0.12	0.00	0.00	20.9
20	0	-0	1238	0	0	0	-1323	--	--	16.08	16.08	0.18	0.02	0.01	0.08	0.00	0.00	20.9
37	0	-0	288	0	0	0	-308	--	--	16.08	16.08	0.18	0.01	0.00	0.02	0.00	0.00	20.9
38	0	-0	2055	0	0	0	-2196	--	--	16.08	16.08	0.18	0.04	0.02	0.13	0.00	0.00	20.9
39	0	-0	927	0	0	0	-991	--	--	16.08	16.08	0.18	0.02	0.01	0.06	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	25	-0	730	0	0	0	962	--	--	16.08	16.08	0.00	0.02	0.01	0.05	0.00	0.00	20.9
2	25	-0	463	0	0	0	611	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
3	25	-0	453	0	0	0	598	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
4	25	-0	670	0	0	0	883	--	--	16.08	16.08	0.10	0.02	0.01	0.04	0.00	0.00	20.9
5	25	-0	660	0	0	0	870	--	--	16.08	16.08	0.10	0.02	0.01	0.04	0.00	0.00	20.9
6	25	-0	546	0	0	0	721	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
7	25	-0	514	0	0	0	678	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
8	25	-0	608	0	0	0	802	--	--	16.08	16.08	0.10	0.01	0.01	0.04	0.00	0.00	20.9
9	25	-0	576	0	0	0	760	--	--	16.08	16.08	0.10	0.01	0.00	0.04	0.00	0.00	20.9
10	25	-0	463	0	0	0	611	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
11	25	-0	453	0	0	0	598	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
12	25	-0	670	0	0	0	883	--	--	16.08	16.08	0.10	0.02	0.01	0.04	0.00	0.00	20.9
13	25	-0	660	0	0	0	870	--	--	16.08	16.08	0.10	0.02	0.01	0.04	0.00	0.00	20.9
14	25	-0	546	0	0	0	721	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
15	25	-0	514	0	0	0	678	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
16	25	-0	608	0	0	0	802	--	--	16.08	16.08	0.10	0.01	0.01	0.04	0.00	0.00	20.9
17	25	-0	576	0	0	0	760	--	--	16.08	16.08	0.10	0.01	0.00	0.04	0.00	0.00	20.9
18	25	-0	855	0	0	0	1127	--	--	16.08	16.08	0.00	0.02	0.01	0.05	0.00	0.00	20.9
19	25	-0	1915	0	0	0	2525	--	--	16.08	16.08	0.00	0.04	0.02	0.12	0.00	0.00	20.9
20	25	-0	1238	0	0	0	1633	--	--	16.08	16.08	0.00	0.03	0.01	0.08	0.00	0.00	20.9
37	25	-0	288	0	0	0	380	--	--	16.08	16.08	0.00	0.01	0.00	0.02	0.00	0.00	20.9
38	25	-0	2055	0	0	0	2710	--	--	16.08	16.08	0.00	0.05	0.02	0.13	0.00	0.00	20.9
39	25	-0	927	0	0	0	1223	--	--	16.08	16.08	0.00	0.02	0.01	0.06	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	50	-0	730	0	0	0	365	--	--	16.08	16.08	0.00	0.01	0.01	0.05	0.00	0.00	20.9
2	50	-0	463	0	0	0	231	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
3	50	-0	453	0	0	0	227	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
4	50	-0	670	0	0	0	335	--	--	16.08	16.08	0.10	0.01	0.01	0.04	0.00	0.00	20.9
5	50	-0	660	0	0	0	330	--	--	16.08	16.08	0.10	0.01	0.01	0.04	0.00	0.00	20.9
6	50	-0	546	0	0	0	273	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
7	50	-0	514	0	0	0	257	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
8	50	-0	608	0	0	0	304	--	--	16.08	16.08	0.10	0.01	0.01	0.04	0.00	0.00	20.9
9	50	-0	576	0	0	0	288	--	--	16.08	16.08	0.10	0.01	0.00	0.04	0.00	0.00	20.9
10	50	-0	463	0	0	0	231	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
11	50	-0	453	0	0	0	227	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
12	50	-0	670	0	0	0	335	--	--	16.08	16.08	0.10	0.01	0.01	0.04	0.00	0.00	20.9
13	50	-0	660	0	0	0	330	--	--	16.08	16.08	0.10	0.01	0.01	0.04	0.00	0.00	20.9
14	50	-0	546	0	0	0	273	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
15	50	-0	514	0	0	0	257	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
16	50	-0	608	0	0	0	304	--	--	16.08	16.08	0.10	0.01	0.01	0.04	0.00	0.00	20.9
17	50	-0	576	0	0	0	288	--	--	16.08	16.08	0.10	0.01	0.00	0.04	0.00	0.00	20.9
18	50	-0	855	0	0	0	427	--	--	16.08	16.08	0.00	0.01	0.01	0.05	0.00	0.00	20.9
19	50	-0	1915	0	0	0	958	--	--	16.08	16.08	0.00	0.02	0.02	0.12	0.00	0.00	20.9
20	50	-0	1238	0	0	0	619	--	--	16.08	16.08	0.00	0.01	0.01	0.08	0.00	0.00	20.9
37	50	-0	288	0	0	0	144	--	--	16.08	16.08	0.00	0.00	0.00	0.02	0.00	0.00	20.9
38	50	-0	2055	0	0	0	1028	--	--	16.08	16.08	0.00	0.02	0.02	0.13	0.00	0.00	20.9
39	50	-0	927	0	0	0	464	--	--	16.08	16.08	0.00	0.01	0.01	0.06	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 167 NI 1565 NF 1564 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	2195	0	0	0	365	--	--	16.08	16.08	0.00	0.01	0.02	0.14	0.00	0.00	20.9
2	0	-0	1434	0	0	0	231	--	--	16.08	16.08	0.10	0.00	0.01	0.09	0.00	0.00	20.9
3	0	-0	1408	0	0	0	227	--	--	16.08	16.08	0.10	0.00	0.01	0.09	0.00	0.00	20.9
4	0	-0	1969	0	0	0	335	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
5	0	-0	1943	0	0	0	330	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
6	0	-0	1651	0	0	0	273	--	--	16.08	16.08	0.10	0.00	0.01	0.10	0.00	0.00	20.9
7	0	-0	1565	0	0	0	257	--	--	16.08	16.08	0.10	0.00	0.01	0.10	0.00	0.00	20.9
8	0	-0	1812	0	0	0	304	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
9	0	-0	1726	0	0	0	288	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
10	0	-0	1434	0	0	0	231	--	--	16.08	16.08	0.10	0.00	0.01	0.09	0.00	0.00	20.9
11	0	-0	1408	0	0	0	227	--	--	16.08	16.08	0.10	0.00	0.01	0.09	0.00	0.00	20.9
12	0	-0	1969	0	0	0	335	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
13	0	-0	1943	0	0	0	330	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
14	0	-0	1651	0	0	0	273	--	--	16.08	16.08	0.10	0.00	0.01	0.10	0.00	0.00	20.9
15	0	-0	1565	0	0	0	257	--	--	16.08	16.08	0.10	0.00	0.01	0.10	0.00	0.00	20.9
16	0	-0	1812	0	0	0	304	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
17	0	-0	1726	0	0	0	288	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
18	0	-0	2618	0	0	0	427	--	--	16.08	16.08	0.00	0.01	0.02	0.16	0.00	0.00	20.9
19	0	-0	5308	0	0	0	958	--	--	16.08	16.08	0.00	0.02	0.04	0.33	0.00	0.00	20.9
20	0	-0	3557	0	0	0	619	--	--	16.08	16.08	0.00	0.01	0.03	0.22	0.00	0.00	20.9
37	0	-0	1145	0	0	0	144	--	--	16.08	16.08	0.00	0.00	0.01	0.07	0.00	0.00	20.9
38	0	-0	5629	0	0	0	1028	--	--	16.08	16.08	0.00	0.02	0.05	0.35	0.00	0.00	20.9
39	0	-0	2711	0	0	0	464	--	--	16.08	16.08	0.00	0.01	0.02	0.17	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	25	-0	2195	0	0	0	3259	--	--	16.08	16.08	0.00	0.06	0.02	0.14	0.00	0.00	20.9
2	25	-0	1434	0	0	0	2123	--	--	16.08	16.08	0.10	0.04	0.01	0.09	0.00	0.00	20.9
3	25	-0	1408	0	0	0	2083	--	--	16.08	16.08	0.10	0.04	0.01	0.09	0.00	0.00	20.9
4	25	-0	1969	0	0	0	2931	--	--	16.08	16.08	0.10	0.05	0.02	0.12	0.00	0.00	20.9
5	25	-0	1943	0	0	0	2892	--	--	16.08	16.08	0.10	0.05	0.02	0.12	0.00	0.00	20.9
6	25	-0	1651	0	0	0	2451	--	--	16.08	16.08	0.10	0.04	0.01	0.10	0.00	0.00	20.9
7	25	-0	1565	0	0	0	2321	--	--	16.08	16.08	0.10	0.04	0.01	0.10	0.00	0.00	20.9
8	25	-0	1812	0	0	0	2694	--	--	16.08	16.08	0.10	0.05	0.01	0.11	0.00	0.00	20.9
9	25	-0	1726	0	0	0	2564	--	--	16.08	16.08	0.10	0.05	0.01	0.11	0.00	0.00	20.9
10	25	-0	1434	0	0	0	2123	--	--	16.08	16.08	0.10	0.04	0.01	0.09	0.00	0.00	20.9
11	25	-0	1408	0	0	0	2083	--	--	16.08	16.08	0.10	0.04	0.01	0.09	0.00	0.00	20.9
12	25	-0	1969	0	0	0	2931	--	--	16.08	16.08	0.10	0.05	0.02	0.12	0.00	0.00	20.9
13	25	-0	1943	0	0	0	2892	--	--	16.08	16.08	0.10	0.05	0.02	0.12	0.00	0.00	20.9
14	25	-0	1651	0	0	0	2451	--	--	16.08	16.08	0.10	0.04	0.01	0.10	0.00	0.00	20.9
15	25	-0	1565	0	0	0	2321	--	--	16.08	16.08	0.10	0.04	0.01	0.10	0.00	0.00	20.9
16	25	-0	1812	0	0	0	2694	--	--	16.08	16.08	0.10	0.05	0.01	0.11	0.00	0.00	20.9
17	25	-0	1726	0	0	0	2564	--	--	16.08	16.08	0.10	0.05	0.01	0.11	0.00	0.00	20.9
18	25	-0	2618	0	0	0	3880	--	--	16.08	16.08	0.00	0.07	0.02	0.16	0.00	0.00	20.9
19	25	-0	5308	0	0	0	7958	--	--	16.08	16.08	0.00	0.14	0.04	0.33	0.00	0.00	20.9
20	25	-0	3557	0	0	0	5310	--	--	16.08	16.08	0.00	0.09	0.03	0.22	0.00	0.00	20.9
37	25	-0	1145	0	0	0	1654	--	--	16.08	16.08	0.00	0.03	0.01	0.07	0.00	0.00	20.9
38	25	-0	5629	0	0	0	8451	--	--	16.08	16.08	0.00	0.14	0.05	0.35	0.00	0.00	20.9
39	25	-0	2711	0	0	0	4039	--	--	16.08	16.08	0.00	0.07	0.02	0.17	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	50	-0	2195	0	0	0	1462	--	--	16.08	16.08	0.00	0.02	0.02	0.14	0.00	0.00	20.9
2	50	-0	1434	0	0	0	948	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
3	50	-0	1408	0	0	0	931	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
4	50	-0	1969	0	0	0	1319	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
5	50	-0	1943	0	0	0	1301	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
6	50	-0	1651	0	0	0	1099	--	--	16.08	16.08	0.10	0.02	0.01	0.10	0.00	0.00	20.9
7	50	-0	1565	0	0	0	1040	--	--	16.08	16.08	0.10	0.02	0.01	0.10	0.00	0.00	20.9
8	50	-0	1812	0	0	0	1210	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
9	50	-0	1726	0	0	0	1151	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
10	50	-0	1434	0	0	0	948	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
11	50	-0	1408	0	0	0	931	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
12	50	-0	1969	0	0	0	1319	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
13	50	-0	1943	0	0	0	1301	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
14	50	-0	1651	0	0	0	1099	--	--	16.08	16.08	0.10	0.02	0.01	0.10	0.00	0.00	20.9
15	50	-0	1565	0	0	0	1040	--	--	16.08	16.08	0.10	0.02	0.01	0.10	0.00	0.00	20.9
16	50	-0	1812	0	0	0	1210	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
17	50	-0	1726	0	0	0	1151	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
18	50	-0	2618	0	0	0	1736	--	--	16.08	16.08	0.00	0.03	0.02	0.16	0.00	0.00	20.9
19	50	-0	5308	0	0	0	3612	--	--	16.08	16.08	0.00	0.06	0.04	0.33	0.00	0.00	20.9
20	50	-0	3557	0	0	0	2398	--	--	16.08	16.08	0.00	0.04	0.03	0.22	0.00	0.00	20.9
37	50	-0	1145	0	0	0	717	--	--	16.08	16.08	0.00	0.01	0.01	0.07	0.00	0.00	20.9
38	50	-0	5629	0	0	0	3842	--	--	16.08	16.08	0.00	0.07	0.05	0.35	0.00	0.00	20.9
39	50	-0	2711	0	0	0	1819	--	--	16.08	16.08	0.00	0.03	0.02	0.17	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 168 NI 1564 NF 1563 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	3667	0	0	0	1462	--	--	16.08	16.08	0.00	0.02	0.03	0.23	0.00	0.00	20.9
2	0	-0	2451	0	0	0	948	--	--	16.08	16.08	0.10	0.02	0.02	0.15	0.00	0.00	20.9
3	0	-0	2412	0	0	0	931	--	--	16.08	16.08	0.10	0.02	0.02	0.15	0.00	0.00	20.9
4	0	-0	3230	0	0	0	1319	--	--	16.08	16.08	0.10	0.02	0.03	0.20	0.00	0.00	20.9
5	0	-0	3191	0	0	0	1301	--	--	16.08	16.08	0.10	0.02	0.03	0.20	0.00	0.00	20.9
6	0	-0	2768	0	0	0	1099	--	--	16.08	16.08	0.10	0.02	0.02	0.17	0.00	0.00	20.9
7	0	-0	2639	0	0	0	1040	--	--	16.08	16.08	0.10	0.02	0.02	0.17	0.00	0.00	20.9
8	0	-0	3002	0	0	0	1210	--	--	16.08	16.08	0.10	0.02	0.02	0.19	0.00	0.00	20.9
9	0	-0	2873	0	0	0	1151	--	--	16.08	16.08	0.10	0.02	0.02	0.18	0.00	0.00	20.9
10	0	-0	2451	0	0	0	948	--	--	16.08	16.08	0.10	0.02	0.02	0.15	0.00	0.00	20.9

11	0	-0	2412	0	0	0	931	--	--	16.08	16.08	0.10	0.02	0.02	0.15	0.00	0.00	20.9
12	0	-0	3230	0	0	0	1319	--	--	16.08	16.08	0.10	0.02	0.03	0.20	0.00	0.00	20.9
13	0	-0	3191	0	0	0	1301	--	--	16.08	16.08	0.10	0.02	0.03	0.20	0.00	0.00	20.9
14	0	-0	2768	0	0	0	1099	--	--	16.08	16.08	0.10	0.02	0.02	0.17	0.00	0.00	20.9
15	0	-0	2639	0	0	0	1040	--	--	16.08	16.08	0.10	0.02	0.02	0.17	0.00	0.00	20.9
16	0	-0	3002	0	0	0	1210	--	--	16.08	16.08	0.10	0.02	0.02	0.19	0.00	0.00	20.9
17	0	-0	2873	0	0	0	1151	--	--	16.08	16.08	0.10	0.02	0.02	0.18	0.00	0.00	20.9
18	0	-0	4436	0	0	0	1736	--	--	16.08	16.08	0.00	0.03	0.04	0.28	0.00	0.00	20.9
19	0	-0	8266	0	0	0	3612	--	--	16.08	16.08	0.00	0.06	0.07	0.52	0.00	0.00	20.9
20	0	-0	5721	0	0	0	2398	--	--	16.08	16.08	0.00	0.04	0.05	0.36	0.00	0.00	20.9
37	0	-0	2286	0	0	0	717	--	--	16.08	16.08	0.00	0.01	0.02	0.14	0.00	0.00	20.9
38	0	-0	8670	0	0	0	3842	--	--	16.08	16.08	0.00	0.07	0.07	0.54	0.00	0.00	20.9
39	0	-0	4428	0	0	0	1819	--	--	16.08	16.08	0.00	0.03	0.04	0.28	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	25	-0	3667	0	0	0	6298	--	--	16.08	16.08	0.00	0.11	0.03	0.23	0.00	0.00	20.9
2	25	-0	2451	0	0	0	4181	--	--	16.08	16.08	0.10	0.07	0.02	0.15	0.00	0.00	20.9
3	25	-0	2412	0	0	0	4112	--	--	16.08	16.08	0.10	0.07	0.02	0.15	0.00	0.00	20.9
4	25	-0	3230	0	0	0	5579	--	--	16.08	16.08	0.10	0.10	0.03	0.20	0.00	0.00	20.9
5	25	-0	3191	0	0	0	5509	--	--	16.08	16.08	0.10	0.10	0.03	0.20	0.00	0.00	20.9
6	25	-0	2768	0	0	0	4749	--	--	16.08	16.08	0.10	0.08	0.02	0.17	0.00	0.00	20.9
7	25	-0	2639	0	0	0	4520	--	--	16.08	16.08	0.10	0.08	0.02	0.17	0.00	0.00	20.9
8	25	-0	3002	0	0	0	5169	--	--	16.08	16.08	0.10	0.09	0.02	0.19	0.00	0.00	20.9
9	25	-0	2873	0	0	0	4940	--	--	16.08	16.08	0.10	0.09	0.02	0.18	0.00	0.00	20.9
10	25	-0	2451	0	0	0	4181	--	--	16.08	16.08	0.10	0.07	0.02	0.15	0.00	0.00	20.9
11	25	-0	2412	0	0	0	4112	--	--	16.08	16.08	0.10	0.07	0.02	0.15	0.00	0.00	20.9
12	25	-0	3230	0	0	0	5579	--	--	16.08	16.08	0.10	0.10	0.03	0.20	0.00	0.00	20.9
13	25	-0	3191	0	0	0	5509	--	--	16.08	16.08	0.10	0.10	0.03	0.20	0.00	0.00	20.9
14	25	-0	2768	0	0	0	4749	--	--	16.08	16.08	0.10	0.08	0.02	0.17	0.00	0.00	20.9
15	25	-0	2639	0	0	0	4520	--	--	16.08	16.08	0.10	0.08	0.02	0.17	0.00	0.00	20.9
16	25	-0	3002	0	0	0	5169	--	--	16.08	16.08	0.10	0.09	0.02	0.19	0.00	0.00	20.9
17	25	-0	2873	0	0	0	4940	--	--	16.08	16.08	0.10	0.09	0.02	0.18	0.00	0.00	20.9
18	25	-0	4436	0	0	0	7586	--	--	16.08	16.08	0.00	0.13	0.04	0.28	0.00	0.00	20.9
19	25	-0	8266	0	0	0	14513	--	--	16.08	16.08	0.00	0.25	0.07	0.52	0.00	0.00	20.9
20	25	-0	5721	0	0	0	9942	--	--	16.08	16.08	0.00	0.17	0.05	0.36	0.00	0.00	20.9
37	25	-0	2286	0	0	0	3731	--	--	16.08	16.08	0.00	0.06	0.02	0.14	0.00	0.00	20.9
38	25	-0	8670	0	0	0	15276	--	--	16.08	16.08	0.00	0.26	0.07	0.54	0.00	0.00	20.9
39	25	-0	4428	0	0	0	7658	--	--	16.08	16.08	0.00	0.13	0.04	0.28	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	50	-0	3667	0	0	0	3296	--	--	16.08	16.08	0.00	0.06	0.03	0.23	0.00	0.00	20.9
2	50	-0	2451	0	0	0	2174	--	--	16.08	16.08	0.10	0.04	0.02	0.15	0.00	0.00	20.9
3	50	-0	2412	0	0	0	2137	--	--	16.08	16.08	0.10	0.04	0.02	0.15	0.00	0.00	20.9
4	50	-0	3230	0	0	0	2934	--	--	16.08	16.08	0.10	0.05	0.03	0.20	0.00	0.00	20.9
5	50	-0	3191	0	0	0	2897	--	--	16.08	16.08	0.10	0.05	0.03	0.20	0.00	0.00	20.9
6	50	-0	2768	0	0	0	2483	--	--	16.08	16.08	0.10	0.04	0.02	0.17	0.00	0.00	20.9
7	50	-0	2639	0	0	0	2359	--	--	16.08	16.08	0.10	0.04	0.02	0.17	0.00	0.00	20.9
8	50	-0	3002	0	0	0	2711	--	--	16.08	16.08	0.10	0.05	0.02	0.19	0.00	0.00	20.9
9	50	-0	2873	0	0	0	2588	--	--	16.08	16.08	0.10	0.05	0.02	0.18	0.00	0.00	20.9
10	50	-0	2451	0	0	0	2174	--	--	16.08	16.08	0.10	0.04	0.02	0.15	0.00	0.00	20.9
11	50	-0	2412	0	0	0	2137	--	--	16.08	16.08	0.10	0.04	0.02	0.15	0.00	0.00	20.9
12	50	-0	3230	0	0	0	2934	--	--	16.08	16.08	0.10	0.05	0.03	0.20	0.00	0.00	20.9
13	50	-0	3191	0	0	0	2897	--	--	16.08	16.08	0.10	0.05	0.03	0.20	0.00	0.00	20.9
14	50	-0	2768	0	0	0	2483	--	--	16.08	16.08	0.10	0.04	0.02	0.17	0.00	0.00	20.9
15	50	-0	2639	0	0	0	2359	--	--	16.08	16.08	0.10	0.04	0.02	0.17	0.00	0.00	20.9
16	50	-0	3002	0	0	0	2711	--	--	16.08	16.08	0.10	0.05	0.02	0.19	0.00	0.00	20.9
17	50	-0	2873	0	0	0	2588	--	--	16.08	16.08	0.10	0.05	0.02	0.18	0.00	0.00	20.9
18	50	-0	4436	0	0	0	3954	--	--	16.08	16.08	0.00	0.07	0.04	0.28	0.00	0.00	20.9
19	50	-0	8266	0	0	0	7745	--	--	16.08	16.08	0.00	0.13	0.07	0.52	0.00	0.00	20.9
20	50	-0	5721	0	0	0	5258	--	--	16.08	16.08	0.00	0.09	0.05	0.36	0.00	0.00	20.9
37	50	-0	2286	0	0	0	1859	--	--	16.08	16.08	0.00	0.03	0.02	0.14	0.00	0.00	20.9
38	50	-0	8670	0	0	0	8177	--	--	16.08	16.08	0.00	0.14	0.07	0.54	0.00	0.00	20.9
39	50	-0	4428	0	0	0	4033	--	--	16.08	16.08	0.00	0.07	0.04	0.28	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 169 NI 1563 NF 1562 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--	----------			----------			----------					----------			-----		-----
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	5143	0	0	0	3296	--	--	16.08	16.08	0.00	0.06	0.04	0.32	0.00	0.00	20.9
2	0	-0	3511	0	0	0	2174	--	--	16.08	16.08	0.10	0.04	0.03	0.22	0.00	0.00	20.9
3	0	-0	3463	0	0	0	2137	--	--	16.08	16.08	0.10	0.04	0.03	0.22	0.00	0.00	20.9
4	0	-0	4450	0	0	0	2934	--	--	16.08	16.08	0.10	0.05	0.04	0.28	0.00	0.00	20.9
5	0	-0	4401	0	0	0	2897	--	--	16.08	16.08	0.10	0.05	0.04	0.28	0.00	0.00	20.9
6	0	-0	3896	0	0	0	2483	--	--	16.08	16.08	0.10	0.04	0.03	0.24	0.00	0.00	20.9
7	0	-0	3735	0	0	0	2359	--	--	16.08	16.08	0.10	0.04	0.03	0.23	0.00	0.00	20.9
8	0	-0	4178	0	0	0	2711	--	--	16.08	16.08	0.10	0.05	0.03	0.26	0.00	0.00	20.9
9	0	-0	4016	0	0	0	2588	--	--	16.08	16.08	0.10	0.05	0.03	0.25	0.00	0.00	20.9
10	0	-0	3511	0	0	0	2174	--	--	16.08	16.08	0.10	0.04	0.03	0.22	0.00	0.00	20.9
11	0	-0	3463	0	0	0	2137	--	--	16.08	16.08	0.10	0.04	0.03	0.22	0.00	0.00	20.9
12	0	-0	4450	0	0	0	2934	--	--	16.08	16.08	0.10	0.05	0.04	0.28	0.00	0.00	20.9
13	0	-0	4401	0	0	0	2897	--	--	16.08	16.08	0.10	0.05	0.04	0.28	0.00	0.00	20.9
14	0	-0	3896	0	0	0	2483	--	--	16.08	16.08	0.10	0.04	0.03	0.24	0.00	0.00	20.9
15	0	-0	3735	0	0	0	2359	--	--	16.08	16.08	0.10	0.04	0.03	0.23	0.00	0.00	20.9
16	0	-0	4178	0	0	0	2711	--	--	16.08	16.08	0.10	0.05	0.03	0.26	0.00	0.00	20.9
17	0	-0	4016	0	0	0	2588	--	--	16.08	16.08	0.10	0.05	0.03	0.25	0.00	0.00	20.9
18	0	-0	6306	0	0	0	3954	--	--	16.08	16.08	0.00	0.07	0.05	0.40	0.00	0.00	20.9
19	0	-0	10780	0	0	0	7745	--	--	16.08	16.08	0.00	0.13	0.09	0.68	0.00	0.00	20.9
20	0	-0	7724	0	0	0	5258	--	--	16.08	16.08	0.00	0.09	0.06	0.48	0.00	0.00	20.9
37	0	-0	3709	0	0	0	1859	--	--	16.08	16.08	0.00	0.03	0.03	0.23	0.00	0.00	20.9
38	0	-0	11170	0	0	0	8177	--	--	16.08	16.08	0.00	0.14	0.09	0.70	0.00	0.00	20.9
39	0	-0	6072	0	0	0	4033	--	--	16.08	16.08	0.00	0.07	0.05	0.38	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	25	-0	5143	0	0	0	10079	--	--	16.08	16.08	0.00	0.17	0.04	0.32	0.00	0.00	20.9
2	25	-0	3511	0	0	0	6804	--	--	16.08	16.08	0.10	0.12	0.03	0.22	0.00	0.00	20.9
3	25	-0	3463	0	0	0	6704	--	--	16.08	16.08	0.10	0.12	0.03	0.22	0.00	0.00	20.9
4	25	-0	4450	0	0	0	8802	--	--	16.08	16.08	0.10	0.16	0.04	0.28	0.00	0.00	20.9
5	25	-0	4401	0	0	0	8701	--	--	16.08	16.08	0.10	0.15	0.04	0.28	0.00	0.00	20.9
6	25	-0	3896	0	0	0	7621	--	--	16.08	16.08	0.10	0.14	0.03	0.24	0.00	0.00	20.9

7	25	-0	3735	0	0	0	7285	--	--	16.08	16.08	0.10	0.13	0.03	0.23	0.00	0.00	20.9
8	25	-0	4178	0	0	0	8221	--	--	16.08	16.08	0.10	0.15	0.03	0.26	0.00	0.00	20.9
9	25	-0	4016	0	0	0	7884	--	--	16.08	16.08	0.10	0.14	0.03	0.25	0.00	0.00	20.9
10	25	-0	3511	0	0	0	6804	--	--	16.08	16.08	0.10	0.12	0.03	0.22	0.00	0.00	20.9
11	25	-0	3463	0	0	0	6704	--	--	16.08	16.08	0.10	0.12	0.03	0.22	0.00	0.00	20.9
12	25	-0	4450	0	0	0	8802	--	--	16.08	16.08	0.10	0.16	0.04	0.28	0.00	0.00	20.9
13	25	-0	4401	0	0	0	8701	--	--	16.08	16.08	0.10	0.15	0.04	0.28	0.00	0.00	20.9
14	25	-0	3896	0	0	0	7621	--	--	16.08	16.08	0.10	0.14	0.03	0.24	0.00	0.00	20.9
15	25	-0	3735	0	0	0	7285	--	--	16.08	16.08	0.10	0.13	0.03	0.23	0.00	0.00	20.9
16	25	-0	4178	0	0	0	8221	--	--	16.08	16.08	0.10	0.15	0.03	0.26	0.00	0.00	20.9
17	25	-0	4016	0	0	0	7884	--	--	16.08	16.08	0.10	0.14	0.03	0.25	0.00	0.00	20.9
18	25	-0	6306	0	0	0	12270	--	--	16.08	16.08	0.00	0.21	0.05	0.40	0.00	0.00	20.9
19	25	-0	10780	0	0	0	21964	--	--	16.08	16.08	0.00	0.37	0.09	0.68	0.00	0.00	20.9
20	25	-0	7724	0	0	0	15444	--	--	16.08	16.08	0.00	0.26	0.06	0.48	0.00	0.00	20.9
37	25	-0	3709	0	0	0	6750	--	--	16.08	16.08	0.00	0.12	0.03	0.23	0.00	0.00	20.9
38	25	-0	11170	0	0	0	22906	--	--	16.08	16.08	0.00	0.39	0.09	0.70	0.00	0.00	20.9
39	25	-0	6072	0	0	0	12040	--	--	16.08	16.08	0.00	0.21	0.05	0.38	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	50	-0	5143	0	0	0	5868	--	--	16.08	16.08	0.00	0.10	0.04	0.32	0.00	0.00	20.9
2	50	-0	3511	0	0	0	3929	--	--	16.08	16.08	0.10	0.07	0.03	0.22	0.00	0.00	20.9
3	50	-0	3463	0	0	0	3868	--	--	16.08	16.08	0.10	0.07	0.03	0.22	0.00	0.00	20.9
4	50	-0	4450	0	0	0	5159	--	--	16.08	16.08	0.10	0.09	0.04	0.28	0.00	0.00	20.9
5	50	-0	4401	0	0	0	5098	--	--	16.08	16.08	0.10	0.09	0.04	0.28	0.00	0.00	20.9
6	50	-0	3896	0	0	0	4431	--	--	16.08	16.08	0.10	0.08	0.03	0.24	0.00	0.00	20.9
7	50	-0	3735	0	0	0	4227	--	--	16.08	16.08	0.10	0.08	0.03	0.23	0.00	0.00	20.9
8	50	-0	4178	0	0	0	4800	--	--	16.08	16.08	0.10	0.09	0.03	0.26	0.00	0.00	20.9
9	50	-0	4016	0	0	0	4596	--	--	16.08	16.08	0.10	0.08	0.03	0.25	0.00	0.00	20.9
10	50	-0	3511	0	0	0	3929	--	--	16.08	16.08	0.10	0.07	0.03	0.22	0.00	0.00	20.9
11	50	-0	3463	0	0	0	3868	--	--	16.08	16.08	0.10	0.07	0.03	0.22	0.00	0.00	20.9
12	50	-0	4450	0	0	0	5159	--	--	16.08	16.08	0.10	0.09	0.04	0.28	0.00	0.00	20.9
13	50	-0	4401	0	0	0	5098	--	--	16.08	16.08	0.10	0.09	0.04	0.28	0.00	0.00	20.9
14	50	-0	3896	0	0	0	4431	--	--	16.08	16.08	0.10	0.08	0.03	0.24	0.00	0.00	20.9
15	50	-0	3735	0	0	0	4227	--	--	16.08	16.08	0.10	0.08	0.03	0.23	0.00	0.00	20.9
16	50	-0	4178	0	0	0	4800	--	--	16.08	16.08	0.10	0.09	0.03	0.26	0.00	0.00	20.9
17	50	-0	4016	0	0	0	4596	--	--	16.08	16.08	0.10	0.08	0.03	0.25	0.00	0.00	20.9
18	50	-0	6306	0	0	0	7107	--	--	16.08	16.08	0.00	0.12	0.05	0.40	0.00	0.00	20.9
19	50	-0	10780	0	0	0	13140	--	--	16.08	16.08	0.00	0.22	0.09	0.68	0.00	0.00	20.9
20	50	-0	7724	0	0	0	9120	--	--	16.08	16.08	0.00	0.16	0.06	0.48	0.00	0.00	20.9
37	50	-0	3709	0	0	0	3714	--	--	16.08	16.08	0.00	0.06	0.03	0.23	0.00	0.00	20.9
38	50	-0	11170	0	0	0	13760	--	--	16.08	16.08	0.00	0.23	0.09	0.70	0.00	0.00	20.9
39	50	-0	6072	0	0	0	7069	--	--	16.08	16.08	0.00	0.12	0.05	0.38	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 170 NI 1562 NF 1569 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	6760	0	0	0	5868	--	--	16.08	16.08	0.00	0.10	0.06	0.42	0.00	0.00	20.9
2	0	-0	4719	0	0	0	3929	--	--	16.08	16.08	0.10	0.07	0.04	0.30	0.00	0.00	20.9
3	0	-0	4664	0	0	0	3868	--	--	16.08	16.08	0.10	0.07	0.04	0.29	0.00	0.00	20.9
4	0	-0	5736	0	0	0	5159	--	--	16.08	16.08	0.10	0.09	0.05	0.36	0.00	0.00	20.9
5	0	-0	5680	0	0	0	5098	--	--	16.08	16.08	0.10	0.09	0.05	0.36	0.00	0.00	20.9
6	0	-0	5140	0	0	0	4431	--	--	16.08	16.08	0.10	0.08	0.04	0.32	0.00	0.00	20.9
7	0	-0	4955	0	0	0	4227	--	--	16.08	16.08	0.10	0.08	0.04	0.31	0.00	0.00	20.9
8	0	-0	5445	0	0	0	4800	--	--	16.08	16.08	0.10	0.09	0.04	0.34	0.00	0.00	20.9
9	0	-0	5260	0	0	0	4596	--	--	16.08	16.08	0.10	0.08	0.04	0.33	0.00	0.00	20.9
10	0	-0	4719	0	0	0	3929	--	--	16.08	16.08	0.10	0.07	0.04	0.30	0.00	0.00	20.9
11	0	-0	4664	0	0	0	3868	--	--	16.08	16.08	0.10	0.07	0.04	0.29	0.00	0.00	20.9
12	0	-0	5736	0	0	0	5159	--	--	16.08	16.08	0.10	0.09	0.05	0.36	0.00	0.00	20.9
13	0	-0	5680	0	0	0	5098	--	--	16.08	16.08	0.10	0.09	0.05	0.36	0.00	0.00	20.9
14	0	-0	5140	0	0	0	4431	--	--	16.08	16.08	0.10	0.08	0.04	0.32	0.00	0.00	20.9
15	0	-0	4955	0	0	0	4227	--	--	16.08	16.08	0.10	0.08	0.04	0.31	0.00	0.00	20.9
16	0	-0	5445	0	0	0	4800	--	--	16.08	16.08	0.10	0.09	0.04	0.34	0.00	0.00	20.9
17	0	-0	5260	0	0	0	4596	--	--	16.08	16.08	0.10	0.08	0.04	0.33	0.00	0.00	20.9
18	0	-0	8406	0	0	0	7107	--	--	16.08	16.08	0.00	0.12	0.07	0.53	0.00	0.00	20.9
19	0	-0	13030	0	0	0	13140	--	--	16.08	16.08	0.00	0.22	0.11	0.82	0.00	0.00	20.9
20	0	-0	9730	0	0	0	9120	--	--	16.08	16.08	0.00	0.16	0.08	0.61	0.00	0.00	20.9
37	0	-0	5580	0	0	0	3714	--	--	16.08	16.08	0.00	0.06	0.05	0.35	0.00	0.00	20.9
38	0	-0	13290	0	0	0	13760	--	--	16.08	16.08	0.00	0.23	0.11	0.83	0.00	0.00	20.9
39	0	-0	7788	0	0	0	7069	--	--	16.08	16.08	0.00	0.12	0.06	0.49	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	30	-0	6760	0	0	0	15120	--	--	16.08	16.08	0.00	0.26	0.06	0.42	0.00	0.00	20.9
2	30	-0	4719	0	0	0	10388	--	--	16.08	16.08	0.10	0.18	0.04	0.30	0.00	0.00	20.9
3	30	-0	4664	0	0	0	10252	--	--	16.08	16.08	0.10	0.18	0.04	0.29	0.00	0.00	20.9
4	30	-0	5736	0	0	0	13010	--	--	16.08	16.08	0.10	0.23	0.05	0.36	0.00	0.00	20.9
5	30	-0	5680	0	0	0	12873	--	--	16.08	16.08	0.10	0.23	0.05	0.36	0.00	0.00	20.9
6	30	-0	5140	0	0	0	11466	--	--	16.08	16.08	0.10	0.20	0.04	0.32	0.00	0.00	20.9
7	30	-0	4955	0	0	0	11009	--	--	16.08	16.08	0.10	0.20	0.04	0.31	0.00	0.00	20.9
8	30	-0	5445	0	0	0	12253	--	--	16.08	16.08	0.10	0.22	0.04	0.34	0.00	0.00	20.9
9	30	-0	5260	0	0	0	11796	--	--	16.08	16.08	0.10	0.21	0.04	0.33	0.00	0.00	20.9
10	30	-0	4719	0	0	0	10388	--	--	16.08	16.08	0.10	0.18	0.04	0.30	0.00	0.00	20.9
11	30	-0	4664	0	0	0	10252	--	--	16.08	16.08	0.10	0.18	0.04	0.29	0.00	0.00	20.9
12	30	-0	5736	0	0	0	13010	--	--	16.08	16.08	0.10	0.23	0.05	0.36	0.00	0.00	20.9
13	30	-0	5680	0	0	0	12873	--	--	16.08	16.08	0.10	0.23	0.05	0.36	0.00	0.00	20.9
14	30	-0	5140	0	0	0	11466	--	--	16.08	16.08	0.10	0.20	0.04	0.32	0.00	0.00	20.9
15	30	-0	4955	0	0	0	11009	--	--	16.08	16.08	0.10	0.20	0.04	0.31	0.00	0.00	20.9
16	30	-0	5445	0	0	0	12253	--	--	16.08	16.08	0.10	0.22	0.04	0.34	0.00	0.00	20.9
17	30	-0	5260	0	0	0	11796	--	--	16.08	16.08	0.10	0.21	0.04	0.33	0.00	0.00	20.9
18	30	-0	8406	0	0	0	18612	--	--	16.08	16.08	0.00	0.32	0.07	0.53	0.00	0.00	20.9
19	30	-0	13030	0	0	0	30971	--	--	16.08	16.08	0.00	0.53	0.11	0.82	0.00	0.00	20.9
20	30	-0	9730	0	0	0	22439	--	--	16.08	16.08	0.00	0.38	0.08	0.61	0.00	0.00	20.9
37	30	-0	5580	0	0	0	11352	--	--	16.08	16.08	0.00	0.19	0.05	0.35	0.00	0.00	20.9
38	30	-0	13290	0	0	0	31949	--	--	16.08	16.08	0.00	0.54	0.11	0.83	0.00	0.00	20.9
39	30	-0	7788	0	0	0	17728	--	--	16.08	16.08	0.00	0.30	0.06	0.49	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	60	-0	6760	0	0	0	9923	--	--	16.08	16.08	0.00	0.17	0.06	0.42	0.00	0.00	20.9
2	60	-0	4719	0	0	0	6761	--	--	16.08	16.08	0.10	0.12	0.04	0.30	0.00	0.00	20.9

3	60	-0	4664	0	0	0	6667	--	--	16.08	16.08	0.10	0.12	0.04	0.29	0.00	0.00	20.9
4	60	-0	5736	0	0	0	8600	--	--	16.08	16.08	0.10	0.15	0.05	0.36	0.00	0.00	20.9
5	60	-0	5680	0	0	0	8506	--	--	16.08	16.08	0.10	0.15	0.05	0.36	0.00	0.00	20.9
6	60	-0	5140	0	0	0	7515	--	--	16.08	16.08	0.10	0.13	0.04	0.32	0.00	0.00	20.9
7	60	-0	4955	0	0	0	7200	--	--	16.08	16.08	0.10	0.13	0.04	0.31	0.00	0.00	20.9
8	60	-0	5445	0	0	0	8067	--	--	16.08	16.08	0.10	0.14	0.04	0.34	0.00	0.00	20.9
9	60	-0	5260	0	0	0	7752	--	--	16.08	16.08	0.10	0.14	0.04	0.33	0.00	0.00	20.9
10	60	-0	4719	0	0	0	6761	--	--	16.08	16.08	0.10	0.12	0.04	0.30	0.00	0.00	20.9
11	60	-0	4664	0	0	0	6667	--	--	16.08	16.08	0.10	0.12	0.04	0.29	0.00	0.00	20.9
12	60	-0	5736	0	0	0	8600	--	--	16.08	16.08	0.10	0.15	0.05	0.36	0.00	0.00	20.9
13	60	-0	5680	0	0	0	8506	--	--	16.08	16.08	0.10	0.15	0.05	0.36	0.00	0.00	20.9
14	60	-0	5140	0	0	0	7515	--	--	16.08	16.08	0.10	0.13	0.04	0.32	0.00	0.00	20.9
15	60	-0	4955	0	0	0	7200	--	--	16.08	16.08	0.10	0.13	0.04	0.31	0.00	0.00	20.9
16	60	-0	5445	0	0	0	8067	--	--	16.08	16.08	0.10	0.14	0.04	0.34	0.00	0.00	20.9
17	60	-0	5260	0	0	0	7752	--	--	16.08	16.08	0.10	0.14	0.04	0.33	0.00	0.00	20.9
18	60	-0	8406	0	0	0	12150	--	--	16.08	16.08	0.00	0.21	0.07	0.53	0.00	0.00	20.9
19	60	-0	13030	0	0	0	20950	--	--	16.08	16.08	0.00	0.36	0.11	0.82	0.00	0.00	20.9
20	60	-0	9730	0	0	0	14960	--	--	16.08	16.08	0.00	0.26	0.08	0.61	0.00	0.00	20.9
37	60	-0	5580	0	0	0	7062	--	--	16.08	16.08	0.00	0.12	0.05	0.35	0.00	0.00	20.9
38	60	-0	13290	0	0	0	21730	--	--	16.08	16.08	0.00	0.37	0.11	0.83	0.00	0.00	20.9
39	60	-0	7788	0	0	0	11740	--	--	16.08	16.08	0.00	0.20	0.06	0.49	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 171 NI 1569 NF 1568 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	7155	0	0	0	7997	--	--	16.08	16.08	0.00	0.14	0.06	0.45	0.00	0.00	20.9
2	0	-0	5707	0	0	0	5488	--	--	16.08	16.08	0.10	0.10	0.05	0.36	0.00	0.00	20.9
3	0	-0	5740	0	0	0	5388	--	--	16.08	16.08	0.10	0.10	0.05	0.36	0.00	0.00	20.9
4	0	-0	5267	0	0	0	6915	--	--	16.08	16.08	0.10	0.12	0.04	0.33	0.00	0.00	20.9
5	0	-0	5300	0	0	0	6815	--	--	16.08	16.08	0.10	0.12	0.04	0.33	0.00	0.00	20.9
6	0	-0	5515	0	0	0	6104	--	--	16.08	16.08	0.10	0.11	0.05	0.35	0.00	0.00	20.9
7	0	-0	5624	0	0	0	5771	--	--	16.08	16.08	0.10	0.10	0.05	0.35	0.00	0.00	20.9
8	0	-0	5383	0	0	0	6532	--	--	16.08	16.08	0.10	0.12	0.04	0.34	0.00	0.00	20.9
9	0	-0	5492	0	0	0	6199	--	--	16.08	16.08	0.10	0.11	0.05	0.34	0.00	0.00	20.9
10	0	-0	5707	0	0	0	5488	--	--	16.08	16.08	0.10	0.10	0.05	0.36	0.00	0.00	20.9
11	0	-0	5740	0	0	0	5388	--	--	16.08	16.08	0.10	0.10	0.05	0.36	0.00	0.00	20.9
12	0	-0	5267	0	0	0	6915	--	--	16.08	16.08	0.10	0.12	0.04	0.33	0.00	0.00	20.9
13	0	-0	5300	0	0	0	6815	--	--	16.08	16.08	0.10	0.12	0.04	0.33	0.00	0.00	20.9
14	0	-0	5515	0	0	0	6104	--	--	16.08	16.08	0.10	0.11	0.05	0.35	0.00	0.00	20.9
15	0	-0	5624	0	0	0	5771	--	--	16.08	16.08	0.10	0.10	0.05	0.35	0.00	0.00	20.9
16	0	-0	5383	0	0	0	6532	--	--	16.08	16.08	0.10	0.12	0.04	0.34	0.00	0.00	20.9
17	0	-0	5492	0	0	0	6199	--	--	16.08	16.08	0.10	0.11	0.05	0.34	0.00	0.00	20.9
18	0	-0	10150	0	0	0	9613	--	--	16.08	16.08	0.00	0.16	0.08	0.64	0.00	0.00	20.9
19	0	-0	6095	0	0	0	17120	--	--	16.08	16.08	0.00	0.29	0.05	0.38	0.00	0.00	20.9
20	0	-0	8166	0	0	0	12020	--	--	16.08	16.08	0.00	0.20	0.07	0.51	0.00	0.00	20.9
37	0	-0	11200	0	0	0	5367	--	--	16.08	16.08	0.00	0.09	0.09	0.70	0.00	0.00	20.9
38	0	-0	4449	0	0	0	17870	--	--	16.08	16.08	0.00	0.30	0.04	0.28	0.00	0.00	20.9
39	0	-0	7900	0	0	0	9379	--	--	16.08	16.08	0.00	0.16	0.07	0.50	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	10	-0	7155	0	0	0	16359	--	--	16.08	16.08	0.00	0.28	0.06	0.45	0.00	0.00	20.9
2	10	-0	5707	0	0	0	12158	--	--	16.08	16.08	0.10	0.22	0.05	0.36	0.00	0.00	20.9
3	10	-0	5740	0	0	0	12097	--	--	16.08	16.08	0.10	0.21	0.05	0.36	0.00	0.00	20.9
4	10	-0	5267	0	0	0	13071	--	--	16.08	16.08	0.10	0.23	0.04	0.33	0.00	0.00	20.9
5	10	-0	5300	0	0	0	13009	--	--	16.08	16.08	0.10	0.23	0.04	0.33	0.00	0.00	20.9
6	10	-0	5515	0	0	0	12550	--	--	16.08	16.08	0.10	0.22	0.05	0.35	0.00	0.00	20.9
7	10	-0	5624	0	0	0	12344	--	--	16.08	16.08	0.10	0.22	0.05	0.35	0.00	0.00	20.9
8	10	-0	5383	0	0	0	12824	--	--	16.08	16.08	0.10	0.23	0.04	0.34	0.00	0.00	20.9
9	10	-0	5492	0	0	0	12618	--	--	16.08	16.08	0.10	0.22	0.05	0.34	0.00	0.00	20.9
10	10	-0	5707	0	0	0	12158	--	--	16.08	16.08	0.10	0.22	0.05	0.36	0.00	0.00	20.9
11	10	-0	5740	0	0	0	12097	--	--	16.08	16.08	0.10	0.21	0.05	0.36	0.00	0.00	20.9
12	10	-0	5267	0	0	0	13071	--	--	16.08	16.08	0.10	0.23	0.04	0.33	0.00	0.00	20.9
13	10	-0	5300	0	0	0	13009	--	--	16.08	16.08	0.10	0.23	0.04	0.33	0.00	0.00	20.9
14	10	-0	5515	0	0	0	12550	--	--	16.08	16.08	0.10	0.22	0.05	0.35	0.00	0.00	20.9
15	10	-0	5624	0	0	0	12344	--	--	16.08	16.08	0.10	0.22	0.05	0.35	0.00	0.00	20.9
16	10	-0	5383	0	0	0	12824	--	--	16.08	16.08	0.10	0.23	0.04	0.34	0.00	0.00	20.9
17	10	-0	5492	0	0	0	12618	--	--	16.08	16.08	0.10	0.22	0.05	0.34	0.00	0.00	20.9
18	10	-0	10150	0	0	0	21474	--	--	16.08	16.08	0.00	0.37	0.08	0.64	0.00	0.00	20.9
19	10	-0	6095	0	0	0	24239	--	--	16.08	16.08	0.00	0.41	0.05	0.38	0.00	0.00	20.9
20	10	-0	8166	0	0	0	21562	--	--	16.08	16.08	0.00	0.37	0.07	0.51	0.00	0.00	20.9
37	10	-0	11200	0	0	0	18458	--	--	16.08	16.08	0.00	0.31	0.09	0.70	0.00	0.00	20.9
38	10	-0	4449	0	0	0	23070	--	--	16.08	16.08	0.00	0.39	0.04	0.28	0.00	0.00	20.9
39	10	-0	7900	0	0	0	18613	--	--	16.08	16.08	0.00	0.32	0.07	0.50	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	20	-0	7155	0	0	0	9428	--	--	16.08	16.08	0.00	0.16	0.06	0.45	0.00	0.00	20.9
2	20	-0	5707	0	0	0	6630	--	--	16.08	16.08	0.10	0.12	0.05	0.36	0.00	0.00	20.9
3	20	-0	5740	0	0	0	6536	--	--	16.08	16.08	0.10	0.12	0.05	0.36	0.00	0.00	20.9
4	20	-0	5267	0	0	0	7968	--	--	16.08	16.08	0.10	0.14	0.04	0.33	0.00	0.00	20.9
5	20	-0	5300	0	0	0	7875	--	--	16.08	16.08	0.10	0.14	0.04	0.33	0.00	0.00	20.9
6	20	-0	5515	0	0	0	7207	--	--	16.08	16.08	0.10	0.13	0.05	0.35	0.00	0.00	20.9
7	20	-0	5624	0	0	0	6895	--	--	16.08	16.08	0.10	0.12	0.05	0.35	0.00	0.00	20.9
8	20	-0	5383	0	0	0	7609	--	--	16.08	16.08	0.10	0.14	0.04	0.34	0.00	0.00	20.9
9	20	-0	5492	0	0	0	7297	--	--	16.08	16.08	0.10	0.13	0.05	0.34	0.00	0.00	20.9
10	20	-0	5707	0	0	0	6630	--	--	16.08	16.08	0.10	0.12	0.05	0.36	0.00	0.00	20.9
11	20	-0	5740	0	0	0	6536	--	--	16.08	16.08	0.10	0.12	0.05	0.36	0.00	0.00	20.9
12	20	-0	5267	0	0	0	7968	--	--	16.08	16.08	0.10	0.14	0.04	0.33	0.00	0.00	20.9
13	20	-0	5300	0	0	0	7875	--	--	16.08	16.08	0.10	0.14	0.04	0.33	0.00	0.00	20.9
14	20	-0	5515	0	0	0	7207	--	--	16.08	16.08	0.10	0.13	0.05	0.35	0.00	0.00	20.9
15	20	-0	5624	0	0	0	6895	--	--	16.08	16.08	0.10	0.12	0.05	0.35	0.00	0.00	20.9
16	20	-0	5383	0	0	0	7609	--	--	16.08	16.08	0.10	0.14	0.04	0.34	0.00	0.00	20.9
17	20	-0	5492	0	0	0	7297	--	--	16.08	16.08	0.10	0.13	0.05	0.34	0.00	0.00	20.9
18	20	-0	10150	0	0	0	11640	--	--	16.08	16.08	0.00	0.20	0.08	0.64	0.00	0.00	20.9
19	20	-0	6095	0	0	0	18330	--	--	16.08	16.08	0.00	0.31	0.05	0.38	0.00	0.00	20.9
20	20	-0	8166	0	0	0	13650	--	--	16.08	16.08	0.00	0.23	0.07	0.51	0.00	0.00	20.9
37	20	-0	11200	0	0	0	7608	--	--	16.08	16.08	0.00	0.13	0.09	0.70	0.00	0.00	20.9
38	20	-0	4449	0	0	0	18760	--	--	16.08	16.08	0.00	0.32	0.04	0.28	0.00	0.00	20.9
39	20	-0	7900	0	0	0	10960	--	--	16.08	16.08	0.00	0.19	0.07	0.50	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 172 NI 1568 NF 1561 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-2858	0	0	0	2384	--	--	16.08	16.08	0.00	0.04	0.02	0.18	0.00	0.00	20.9
2	0	-0	-2482	0	0	0	2101	--	--	16.08	16.08	0.10	0.04	0.02	0.16	0.00	0.00	20.9
3	0	-0	-2498	0	0	0	2116	--	--	16.08	16.08	0.10	0.04	0.02	0.16	0.00	0.00	20.9
4	0	-0	-1899	0	0	0	1551	--	--	16.08	16.08	0.10	0.03	0.02	0.12	0.00	0.00	20.9
5	0	-0	-1914	0	0	0	1566	--	--	16.08	16.08	0.10	0.03	0.02	0.12	0.00	0.00	20.9
6	0	-0	-2260	0	0	0	1891	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
7	0	-0	-2311	0	0	0	1942	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
8	0	-0	-2085	0	0	0	1726	--	--	16.08	16.08	0.10	0.03	0.02	0.13	0.00	0.00	20.9
9	0	-0	-2136	0	0	0	1777	--	--	16.08	16.08	0.10	0.03	0.02	0.13	0.00	0.00	20.9
10	0	-0	-2482	0	0	0	2101	--	--	16.08	16.08	0.10	0.04	0.02	0.16	0.00	0.00	20.9
11	0	-0	-2498	0	0	0	2116	--	--	16.08	16.08	0.10	0.04	0.02	0.16	0.00	0.00	20.9
12	0	-0	-1899	0	0	0	1551	--	--	16.08	16.08	0.10	0.03	0.02	0.12	0.00	0.00	20.9
13	0	-0	-1914	0	0	0	1566	--	--	16.08	16.08	0.10	0.03	0.02	0.12	0.00	0.00	20.9
14	0	-0	-2260	0	0	0	1891	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
15	0	-0	-2311	0	0	0	1942	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
16	0	-0	-2085	0	0	0	1726	--	--	16.08	16.08	0.10	0.03	0.02	0.13	0.00	0.00	20.9
17	0	-0	-2136	0	0	0	1777	--	--	16.08	16.08	0.10	0.03	0.02	0.13	0.00	0.00	20.9
18	0	-0	-4107	0	0	0	3461	--	--	16.08	16.08	0.00	0.06	0.03	0.26	0.00	0.00	20.9
19	0	-0	-180	0	0	0	-272	--	--	16.08	16.08	0.18	0.00	0.00	0.01	0.00	0.00	20.9
20	0	-0	-2147	0	0	0	1668	--	--	16.08	16.08	0.00	0.03	0.02	0.13	0.00	0.00	20.9
37	0	-0	-5658	0	0	0	4926	--	--	16.08	16.08	0.00	0.08	0.05	0.35	0.00	0.00	20.9
38	0	-0	887	0	0	0	-1146	--	--	16.08	16.08	0.18	0.02	0.01	0.06	0.00	0.00	20.9
39	0	-0	-2390	0	0	0	1937	--	--	16.08	16.08	0.00	0.03	0.02	0.15	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	25	-0	-2858	0	0	0	2384	--	--	16.08	16.08	0.00	0.04	0.02	0.18	0.00	0.00	20.9
2	25	-0	-2482	0	0	0	2101	--	--	16.08	16.08	0.10	0.04	0.02	0.16	0.00	0.00	20.9
3	25	-0	-2498	0	0	0	2116	--	--	16.08	16.08	0.10	0.04	0.02	0.16	0.00	0.00	20.9
4	25	-0	-1899	0	0	0	1551	--	--	16.08	16.08	0.10	0.03	0.02	0.12	0.00	0.00	20.9
5	25	-0	-1914	0	0	0	1566	--	--	16.08	16.08	0.10	0.03	0.02	0.12	0.00	0.00	20.9
6	25	-0	-2260	0	0	0	1891	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
7	25	-0	-2311	0	0	0	1942	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
8	25	-0	-2085	0	0	0	1726	--	--	16.08	16.08	0.10	0.03	0.02	0.13	0.00	0.00	20.9
9	25	-0	-2136	0	0	0	1777	--	--	16.08	16.08	0.10	0.03	0.02	0.13	0.00	0.00	20.9
10	25	-0	-2482	0	0	0	2101	--	--	16.08	16.08	0.10	0.04	0.02	0.16	0.00	0.00	20.9
11	25	-0	-2498	0	0	0	2116	--	--	16.08	16.08	0.10	0.04	0.02	0.16	0.00	0.00	20.9
12	25	-0	-1899	0	0	0	1551	--	--	16.08	16.08	0.10	0.03	0.02	0.12	0.00	0.00	20.9
13	25	-0	-1914	0	0	0	1566	--	--	16.08	16.08	0.10	0.03	0.02	0.12	0.00	0.00	20.9
14	25	-0	-2260	0	0	0	1891	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
15	25	-0	-2311	0	0	0	1942	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
16	25	-0	-2085	0	0	0	1726	--	--	16.08	16.08	0.10	0.03	0.02	0.13	0.00	0.00	20.9
17	25	-0	-2136	0	0	0	1777	--	--	16.08	16.08	0.10	0.03	0.02	0.13	0.00	0.00	20.9
18	25	-0	-4107	0	0	0	3461	--	--	16.08	16.08	0.00	0.06	0.03	0.26	0.00	0.00	20.9
19	25	-0	-180	0	0	0	-272	--	--	16.08	16.08	0.18	0.00	0.00	0.01	0.00	0.00	20.9
20	25	-0	-2147	0	0	0	1668	--	--	16.08	16.08	0.00	0.03	0.02	0.13	0.00	0.00	20.9
37	25	-0	-5658	0	0	0	4926	--	--	16.08	16.08	0.00	0.08	0.05	0.35	0.00	0.00	20.9
38	25	-0	887	0	0	0	-1146	--	--	16.08	16.08	0.18	0.02	0.01	0.06	0.00	0.00	20.9
39	25	-0	-2390	0	0	0	1937	--	--	16.08	16.08	0.00	0.03	0.02	0.15	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	50	-0	-2858	0	0	0	955	--	--	16.08	16.08	0.00	0.02	0.02	0.18	0.00	0.00	20.9
2	50	-0	-2482	0	0	0	860	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
3	50	-0	-2498	0	0	0	867	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
4	50	-0	-1899	0	0	0	602	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
5	50	-0	-1914	0	0	0	609	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
6	50	-0	-2260	0	0	0	761	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
7	50	-0	-2311	0	0	0	786	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
8	50	-0	-2085	0	0	0	683	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
9	50	-0	-2136	0	0	0	708	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
10	50	-0	-2482	0	0	0	860	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
11	50	-0	-2498	0	0	0	867	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
12	50	-0	-1899	0	0	0	602	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
13	50	-0	-1914	0	0	0	609	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
14	50	-0	-2260	0	0	0	761	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
15	50	-0	-2311	0	0	0	786	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
16	50	-0	-2085	0	0	0	683	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
17	50	-0	-2136	0	0	0	708	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
18	50	-0	-4107	0	0	0	1407	--	--	16.08	16.08	0.00	0.02	0.03	0.26	0.00	0.00	20.9
19	50	-0	-180	0	0	0	-272	--	--	16.08	16.08	0.18	0.00	0.00	0.01	0.00	0.00	20.9
20	50	-0	-2147	0	0	0	594	--	--	16.08	16.08	0.00	0.01	0.02	0.13	0.00	0.00	20.9
37	50	-0	-5658	0	0	0	2097	--	--	16.08	16.08	0.00	0.04	0.05	0.35	0.00	0.00	20.9
38	50	-0	887	0	0	0	-1146	--	--	16.08	16.08	0.18	0.02	0.01	0.06	0.00	0.00	20.9
39	50	-0	-2390	0	0	0	742	--	--	16.08	16.08	0.00	0.01	0.02	0.15	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 173 NI 1561 NF 1560 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-1546	0	0	0	955	--	--	16.08	16.08	0.00	0.02	0.01	0.10	0.00	0.00	20.9
2	0	-0	-1384	0	0	0	860	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
3	0	-0	-1395	0	0	0	867	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
4	0	-0	-984	0	0	0	602	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
5	0	-0	-995	0	0	0	609	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
6	0	-0	-1230	0	0	0	761	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
7	0	-0	-1269	0	0	0	786	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
8	0	-0	-1110	0	0	0	683	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
9	0	-0	-1149	0	0	0	708	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
10	0	-0	-1384	0	0	0	860	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9

11	0	-0	-1395	0	0	0	867	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
12	0	-0	-984	0	0	0	602	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
13	0	-0	-995	0	0	0	609	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
14	0	-0	-1230	0	0	0	761	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
15	0	-0	-1269	0	0	0	786	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
16	0	-0	-1110	0	0	0	683	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
17	0	-0	-1149	0	0	0	708	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
18	0	-0	-2269	0	0	0	1407	--	--	16.08	16.08	0.00	0.02	0.02	0.14	0.00	0.00	20.9
19	0	-0	347	0	0	0	-272	--	--	16.08	16.08	0.18	0.00	0.00	0.02	0.00	0.00	20.9
20	0	-0	-998	0	0	0	594	--	--	16.08	16.08	0.00	0.01	0.01	0.06	0.00	0.00	20.9
37	0	-0	-3337	0	0	0	2097	--	--	16.08	16.08	0.00	0.04	0.03	0.21	0.00	0.00	20.9
38	0	-0	1022	0	0	0	-702	--	--	16.08	16.08	0.18	0.01	0.01	0.06	0.00	0.00	20.9
39	0	-0	-1218	0	0	0	742	--	--	16.08	16.08	0.00	0.01	0.01	0.08	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	25	-0	-1546	0	0	0	955	--	--	16.08	16.08	0.00	0.02	0.01	0.10	0.00	0.00	20.9
2	25	-0	-1384	0	0	0	860	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
3	25	-0	-1395	0	0	0	867	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
4	25	-0	-984	0	0	0	602	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
5	25	-0	-995	0	0	0	609	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
6	25	-0	-1230	0	0	0	761	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
7	25	-0	-1269	0	0	0	786	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
8	25	-0	-1110	0	0	0	683	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
9	25	-0	-1149	0	0	0	708	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
10	25	-0	-1384	0	0	0	860	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
11	25	-0	-1395	0	0	0	867	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
12	25	-0	-984	0	0	0	602	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
13	25	-0	-995	0	0	0	609	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
14	25	-0	-1230	0	0	0	761	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
15	25	-0	-1269	0	0	0	786	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
16	25	-0	-1110	0	0	0	683	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
17	25	-0	-1149	0	0	0	708	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
18	25	-0	-2269	0	0	0	1407	--	--	16.08	16.08	0.00	0.02	0.02	0.14	0.00	0.00	20.9
19	25	-0	347	0	0	0	-272	--	--	16.08	16.08	0.18	0.00	0.00	0.02	0.00	0.00	20.9
20	25	-0	-998	0	0	0	594	--	--	16.08	16.08	0.00	0.01	0.01	0.06	0.00	0.00	20.9
37	25	-0	-3337	0	0	0	2097	--	--	16.08	16.08	0.00	0.04	0.03	0.21	0.00	0.00	20.9
38	25	-0	1022	0	0	0	-702	--	--	16.08	16.08	0.18	0.01	0.01	0.06	0.00	0.00	20.9
39	25	-0	-1218	0	0	0	742	--	--	16.08	16.08	0.00	0.01	0.01	0.08	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	50	-0	-1546	0	0	0	182	--	--	16.08	16.08	0.00	0.00	0.01	0.10	0.00	0.00	20.9
2	50	-0	-1384	0	0	0	168	--	--	16.08	16.08	0.10	0.00	0.01	0.09	0.00	0.00	20.9
3	50	-0	-1395	0	0	0	170	--	--	16.08	16.08	0.10	0.00	0.01	0.09	0.00	0.00	20.9
4	50	-0	-984	0	0	0	110	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
5	50	-0	-995	0	0	0	112	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
6	50	-0	-1230	0	0	0	146	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
7	50	-0	-1269	0	0	0	152	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
8	50	-0	-1110	0	0	0	128	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
9	50	-0	-1149	0	0	0	134	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
10	50	-0	-1384	0	0	0	168	--	--	16.08	16.08	0.10	0.00	0.01	0.09	0.00	0.00	20.9
11	50	-0	-1395	0	0	0	170	--	--	16.08	16.08	0.10	0.00	0.01	0.09	0.00	0.00	20.9
12	50	-0	-984	0	0	0	110	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
13	50	-0	-995	0	0	0	112	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
14	50	-0	-1230	0	0	0	146	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
15	50	-0	-1269	0	0	0	152	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
16	50	-0	-1110	0	0	0	128	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
17	50	-0	-1149	0	0	0	134	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
18	50	-0	-2269	0	0	0	273	--	--	16.08	16.08	0.00	0.00	0.02	0.14	0.00	0.00	20.9
19	50	-0	347	0	0	0	-272	--	--	16.08	16.08	0.18	0.00	0.00	0.02	0.00	0.00	20.9
20	50	-0	-998	0	0	0	96	--	--	16.08	16.08	0.00	0.00	0.01	0.06	0.00	0.00	20.9
37	50	-0	-3337	0	0	0	428	--	--	16.08	16.08	0.00	0.01	0.03	0.21	0.00	0.00	20.9
38	50	-0	1022	0	0	0	-702	--	--	16.08	16.08	0.18	0.01	0.01	0.06	0.00	0.00	20.9
39	50	-0	-1218	0	0	0	133	--	--	16.08	16.08	0.00	0.00	0.01	0.08	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 174 NI 1560 NF 1567 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-454	0	0	0	182	--	--	16.08	16.08	0.00	0.00	0.00	0.03	0.00	0.00	20.9
2	0	-0	-420	0	0	0	168	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
3	0	-0	-424	0	0	0	170	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
4	0	-0	-275	0	0	0	110	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
5	0	-0	-279	0	0	0	112	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
6	0	-0	-364	0	0	0	146	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
7	0	-0	-379	0	0	0	152	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
8	0	-0	-320	0	0	0	128	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
9	0	-0	-335	0	0	0	134	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
10	0	-0	-420	0	0	0	168	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
11	0	-0	-424	0	0	0	170	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
12	0	-0	-275	0	0	0	110	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
13	0	-0	-279	0	0	0	112	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
14	0	-0	-364	0	0	0	146	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
15	0	-0	-379	0	0	0	152	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
16	0	-0	-320	0	0	0	128	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
17	0	-0	-335	0	0	0	134	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
18	0	-0	-682	0	0	0	273	--	--	16.08	16.08	0.00	0.00	0.01	0.04	0.00	0.00	20.9
19	0	-0	248	0	0	0	-99	--	--	16.08	16.08	0.18	0.00	0.00	0.02	0.00	0.00	20.9
20	0	-0	-239	0	0	0	96	--	--	16.08	16.08	0.00	0.00	0.00	0.02	0.00	0.00	20.9
37	0	-0	-1071	0	0	0	428	--	--	16.08	16.08	0.00	0.01	0.01	0.07	0.00	0.00	20.9
38	0	-0	478	0	0	0	-191	--	--	16.08	16.08	0.18	0.00	0.00	0.03	0.00	0.00	20.9
39	0	-0	-333	0	0	0	133	--	--	16.08	16.08	0.00	0.00	0.00	0.02	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	20	-0	-454	0	0	0	182	--	--	16.08	16.08	0.00	0.00	0.00	0.03	0.00	0.00	20.9
2	20	-0	-420	0	0	0	168	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
3	20	-0	-424	0	0	0	170	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
4	20	-0	-275	0	0	0	110	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
5	20	-0	-279	0	0	0	112	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
6	20	-0	-364	0	0	0	146	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9

7	20	-0	-379	0	0	0	152	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
8	20	-0	-320	0	0	0	128	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
9	20	-0	-335	0	0	0	134	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
10	20	-0	-420	0	0	0	168	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
11	20	-0	-424	0	0	0	170	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
12	20	-0	-275	0	0	0	110	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
13	20	-0	-279	0	0	0	112	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
14	20	-0	-364	0	0	0	146	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
15	20	-0	-379	0	0	0	152	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
16	20	-0	-320	0	0	0	128	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
17	20	-0	-335	0	0	0	134	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
18	20	-0	-682	0	0	0	273	--	--	16.08	16.08	0.00	0.00	0.01	0.04	0.00	0.00	20.9
19	20	-0	248	0	0	0	-99	--	--	16.08	16.08	0.18	0.00	0.00	0.02	0.00	0.00	20.9
20	20	-0	-239	0	0	0	96	--	--	16.08	16.08	0.00	0.00	0.00	0.02	0.00	0.00	20.9
37	20	-0	-1071	0	0	0	428	--	--	16.08	16.08	0.00	0.01	0.01	0.07	0.00	0.00	20.9
38	20	-0	478	0	0	0	-191	--	--	16.08	16.08	0.18	0.00	0.00	0.03	0.00	0.00	20.9
39	20	-0	-333	0	0	0	133	--	--	16.08	16.08	0.00	0.00	0.00	0.02	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	40	-0	-454	0	0	0	-486	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9
2	40	-0	-420	0	0	0	-449	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
3	40	-0	-424	0	0	0	-454	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
4	40	-0	-275	0	0	0	-294	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
5	40	-0	-279	0	0	0	-298	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
6	40	-0	-364	0	0	0	-389	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
7	40	-0	-379	0	0	0	-405	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
8	40	-0	-320	0	0	0	-342	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
9	40	-0	-335	0	0	0	-358	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
10	40	-0	-420	0	0	0	-449	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
11	40	-0	-424	0	0	0	-454	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
12	40	-0	-275	0	0	0	-294	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
13	40	-0	-279	0	0	0	-298	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
14	40	-0	-364	0	0	0	-389	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
15	40	-0	-379	0	0	0	-405	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
16	40	-0	-320	0	0	0	-342	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
17	40	-0	-335	0	0	0	-358	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
18	40	-0	-682	0	0	0	-729	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
19	40	-0	248	0	0	0	-99	--	--	16.08	16.08	0.18	0.00	0.00	0.02	0.00	0.00	20.9
20	40	-0	-239	0	0	0	-256	--	--	16.08	16.08	0.18	0.00	0.00	0.02	0.00	0.00	20.9
37	40	-0	-1071	0	0	0	-1145	--	--	16.08	16.08	0.18	0.02	0.01	0.07	0.00	0.00	20.9
38	40	-0	478	0	0	0	-191	--	--	16.08	16.08	0.18	0.00	0.00	0.03	0.00	0.00	20.9
39	40	-0	-333	0	0	0	-356	--	--	16.08	16.08	0.18	0.01	0.00	0.02	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 175 NI 1675 NF 824 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm

1	0	-0	-682	0	0	0	136	--	--	16.08	16.08	0.00	0.00	0.01	0.04	0.00	0.00	20.9
2	0	-0	-558	0	0	0	112	--	--	16.08	16.08	0.10	0.00	0.00	0.04	0.00	0.00	20.9
3	0	-0	-557	0	0	0	111	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
4	0	-0	-492	0	0	0	98	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
5	0	-0	-491	0	0	0	98	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
6	0	-0	-537	0	0	0	107	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
7	0	-0	-532	0	0	0	106	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
8	0	-0	-517	0	0	0	103	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
9	0	-0	-512	0	0	0	102	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
10	0	-0	-558	0	0	0	112	--	--	16.08	16.08	0.10	0.00	0.00	0.04	0.00	0.00	20.9
11	0	-0	-557	0	0	0	111	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
12	0	-0	-492	0	0	0	98	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
13	0	-0	-491	0	0	0	98	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
14	0	-0	-537	0	0	0	107	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
15	0	-0	-532	0	0	0	106	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
16	0	-0	-517	0	0	0	103	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
17	0	-0	-512	0	0	0	102	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
18	0	-0	-1163	0	0	0	233	--	--	16.08	16.08	0.00	0.00	0.01	0.07	0.00	0.00	20.9
19	0	-0	-898	0	0	0	180	--	--	16.08	16.08	0.00	0.00	0.01	0.06	0.00	0.00	20.9
20	0	-0	-970	0	0	0	194	--	--	16.08	16.08	0.00	0.00	0.01	0.06	0.00	0.00	20.9
37	0	-0	-1138	0	0	0	228	--	--	16.08	16.08	0.00	0.00	0.01	0.07	0.00	0.00	20.9
38	0	-0	-696	0	0	0	139	--	--	16.08	16.08	0.00	0.00	0.01	0.04	0.00	0.00	20.9
39	0	-0	-817	0	0	0	163	--	--	16.08	16.08	0.00	0.00	0.01	0.05	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	10	-0	-682	0	0	0	136	--	--	16.08	16.08	0.00	0.00	0.01	0.04	0.00	0.00	20.9
2	10	-0	-558	0	0	0	112	--	--	16.08	16.08	0.10	0.00	0.00	0.04	0.00	0.00	20.9
3	10	-0	-557	0	0	0	111	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
4	10	-0	-492	0	0	0	98	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
5	10	-0	-491	0	0	0	98	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
6	10	-0	-537	0	0	0	107	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
7	10	-0	-532	0	0	0	106	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
8	10	-0	-517	0	0	0	103	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
9	10	-0	-512	0	0	0	102	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
10	10	-0	-558	0	0	0	112	--	--	16.08	16.08	0.10	0.00	0.00	0.04	0.00	0.00	20.9
11	10	-0	-557	0	0	0	111	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
12	10	-0	-492	0	0	0	98	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
13	10	-0	-491	0	0	0	98	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
14	10	-0	-537	0	0	0	107	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
15	10	-0	-532	0	0	0	106	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
16	10	-0	-517	0	0	0	103	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
17	10	-0	-512	0	0	0	102	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
18	10	-0	-1163	0	0	0	233	--	--	16.08	16.08	0.00	0.00	0.01	0.07	0.00	0.00	20.9
19	10	-0	-898	0	0	0	180	--	--	16.08	16.08	0.00	0.00	0.01	0.06	0.00	0.00	20.9
20	10	-0	-970	0	0	0	194	--	--	16.08	16.08	0.00	0.00	0.01	0.06	0.00	0.00	20.9
37	10	-0	-1138	0	0	0	228	--	--	16.08	16.08	0.00	0.00	0.01	0.07	0.00	0.00	20.9
38	10	-0	-696	0	0	0	139	--	--	16.08	16.08	0.00	0.00	0.01	0.04	0.00	0.00	20.9
39	10	-0	-817	0	0	0	163	--	--	16.08	16.08	0.00	0.00	0.01	0.05	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	20	-0	-682	0	0	0	-729	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
2	20	-0	-558	0	0	0	-597	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9

3	20	-0	-557	0	0	0	-595	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
4	20	-0	-492	0	0	0	-526	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
5	20	-0	-491	0	0	0	-524	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
6	20	-0	-537	0	0	0	-574	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
7	20	-0	-532	0	0	0	-569	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
8	20	-0	-517	0	0	0	-553	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
9	20	-0	-512	0	0	0	-547	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
10	20	-0	-558	0	0	0	-597	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
11	20	-0	-557	0	0	0	-595	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
12	20	-0	-492	0	0	0	-526	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
13	20	-0	-491	0	0	0	-524	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
14	20	-0	-537	0	0	0	-574	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
15	20	-0	-532	0	0	0	-569	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
16	20	-0	-517	0	0	0	-553	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
17	20	-0	-512	0	0	0	-547	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
18	20	-0	-1163	0	0	0	-1243	--	--	16.08	16.08	0.18	0.02	0.01	0.07	0.00	0.00	20.9
19	20	-0	-898	0	0	0	-960	--	--	16.08	16.08	0.18	0.02	0.01	0.06	0.00	0.00	20.9
20	20	-0	-970	0	0	0	-1037	--	--	16.08	16.08	0.18	0.02	0.01	0.06	0.00	0.00	20.9
37	20	-0	-1138	0	0	0	-1216	--	--	16.08	16.08	0.18	0.02	0.01	0.07	0.00	0.00	20.9
38	20	-0	-696	0	0	0	-744	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
39	20	-0	-817	0	0	0	-873	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 176 NI 1672 NF 1675 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-8760	0	0	0	3134	--	--	16.08	16.08	0.00	0.05	0.07	0.55	0.00	0.00	20.9
2	0	-0	-6713	0	0	0	2524	--	--	16.08	16.08	0.10	0.04	0.06	0.42	0.00	0.00	20.9
3	0	-0	-6705	0	0	0	2540	--	--	16.08	16.08	0.10	0.05	0.06	0.42	0.00	0.00	20.9
4	0	-0	-6772	0	0	0	2282	--	--	16.08	16.08	0.10	0.04	0.06	0.42	0.00	0.00	20.9
5	0	-0	-6764	0	0	0	2298	--	--	16.08	16.08	0.10	0.04	0.06	0.42	0.00	0.00	20.9
6	0	-0	-6744	0	0	0	2421	--	--	16.08	16.08	0.10	0.04	0.06	0.42	0.00	0.00	20.9
7	0	-0	-6716	0	0	0	2474	--	--	16.08	16.08	0.10	0.04	0.06	0.42	0.00	0.00	20.9
8	0	-0	-6761	0	0	0	2348	--	--	16.08	16.08	0.10	0.04	0.06	0.42	0.00	0.00	20.9
9	0	-0	-6733	0	0	0	2401	--	--	16.08	16.08	0.10	0.04	0.06	0.42	0.00	0.00	20.9
10	0	-0	-6713	0	0	0	2524	--	--	16.08	16.08	0.10	0.04	0.06	0.42	0.00	0.00	20.9
11	0	-0	-6705	0	0	0	2540	--	--	16.08	16.08	0.10	0.05	0.06	0.42	0.00	0.00	20.9
12	0	-0	-6772	0	0	0	2282	--	--	16.08	16.08	0.10	0.04	0.06	0.42	0.00	0.00	20.9
13	0	-0	-6764	0	0	0	2298	--	--	16.08	16.08	0.10	0.04	0.06	0.42	0.00	0.00	20.9
14	0	-0	-6744	0	0	0	2421	--	--	16.08	16.08	0.10	0.04	0.06	0.42	0.00	0.00	20.9
15	0	-0	-6716	0	0	0	2474	--	--	16.08	16.08	0.10	0.04	0.06	0.42	0.00	0.00	20.9
16	0	-0	-6761	0	0	0	2348	--	--	16.08	16.08	0.10	0.04	0.06	0.42	0.00	0.00	20.9
17	0	-0	-6733	0	0	0	2401	--	--	16.08	16.08	0.10	0.04	0.06	0.42	0.00	0.00	20.9
18	0	-0	-10530	0	0	0	5065	--	--	16.08	16.08	0.00	0.09	0.09	0.66	0.00	0.00	20.9
19	0	-0	-11470	0	0	0	4221	--	--	16.08	16.08	0.00	0.07	0.09	0.72	0.00	0.00	20.9
20	0	-0	-10610	0	0	0	4466	--	--	16.08	16.08	0.00	0.08	0.09	0.67	0.00	0.00	20.9
37	0	-0	-9503	0	0	0	4857	--	--	16.08	16.08	0.00	0.08	0.08	0.60	0.00	0.00	20.9
38	0	-0	-11060	0	0	0	3451	--	--	16.08	16.08	0.00	0.06	0.09	0.69	0.00	0.00	20.9
39	0	-0	-9628	0	0	0	3859	--	--	16.08	16.08	0.00	0.07	0.08	0.60	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	10	-0	-8760	0	0	0	3134	--	--	16.08	16.08	0.00	0.05	0.07	0.55	0.00	0.00	20.9
2	10	-0	-6713	0	0	0	2524	--	--	16.08	16.08	0.10	0.04	0.06	0.42	0.00	0.00	20.9
3	10	-0	-6705	0	0	0	2540	--	--	16.08	16.08	0.10	0.05	0.06	0.42	0.00	0.00	20.9
4	10	-0	-6772	0	0	0	2282	--	--	16.08	16.08	0.10	0.04	0.06	0.42	0.00	0.00	20.9
5	10	-0	-6764	0	0	0	2298	--	--	16.08	16.08	0.10	0.04	0.06	0.42	0.00	0.00	20.9
6	10	-0	-6744	0	0	0	2421	--	--	16.08	16.08	0.10	0.04	0.06	0.42	0.00	0.00	20.9
7	10	-0	-6716	0	0	0	2474	--	--	16.08	16.08	0.10	0.04	0.06	0.42	0.00	0.00	20.9
8	10	-0	-6761	0	0	0	2348	--	--	16.08	16.08	0.10	0.04	0.06	0.42	0.00	0.00	20.9
9	10	-0	-6733	0	0	0	2401	--	--	16.08	16.08	0.10	0.04	0.06	0.42	0.00	0.00	20.9
10	10	-0	-6713	0	0	0	2524	--	--	16.08	16.08	0.10	0.04	0.06	0.42	0.00	0.00	20.9
11	10	-0	-6705	0	0	0	2540	--	--	16.08	16.08	0.10	0.05	0.06	0.42	0.00	0.00	20.9
12	10	-0	-6772	0	0	0	2282	--	--	16.08	16.08	0.10	0.04	0.06	0.42	0.00	0.00	20.9
13	10	-0	-6764	0	0	0	2298	--	--	16.08	16.08	0.10	0.04	0.06	0.42	0.00	0.00	20.9
14	10	-0	-6744	0	0	0	2421	--	--	16.08	16.08	0.10	0.04	0.06	0.42	0.00	0.00	20.9
15	10	-0	-6716	0	0	0	2474	--	--	16.08	16.08	0.10	0.04	0.06	0.42	0.00	0.00	20.9
16	10	-0	-6761	0	0	0	2348	--	--	16.08	16.08	0.10	0.04	0.06	0.42	0.00	0.00	20.9
17	10	-0	-6733	0	0	0	2401	--	--	16.08	16.08	0.10	0.04	0.06	0.42	0.00	0.00	20.9
18	10	-0	-10530	0	0	0	5065	--	--	16.08	16.08	0.00	0.09	0.09	0.66	0.00	0.00	20.9
19	10	-0	-11470	0	0	0	4221	--	--	16.08	16.08	0.00	0.07	0.09	0.72	0.00	0.00	20.9
20	10	-0	-10610	0	0	0	4466	--	--	16.08	16.08	0.00	0.08	0.09	0.67	0.00	0.00	20.9
37	10	-0	-9503	0	0	0	4857	--	--	16.08	16.08	0.00	0.08	0.08	0.60	0.00	0.00	20.9
38	10	-0	-11060	0	0	0	3451	--	--	16.08	16.08	0.00	0.06	0.09	0.69	0.00	0.00	20.9
39	10	-0	-9628	0	0	0	3859	--	--	16.08	16.08	0.00	0.07	0.08	0.60	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	20	-0	-8760	0	0	0	1382	--	--	16.08	16.08	0.00	0.02	0.07	0.55	0.00	0.00	20.9
2	20	-0	-6713	0	0	0	1181	--	--	16.08	16.08	0.10	0.02	0.06	0.42	0.00	0.00	20.9
3	20	-0	-6705	0	0	0	1199	--	--	16.08	16.08	0.10	0.02	0.06	0.42	0.00	0.00	20.9
4	20	-0	-6772	0	0	0	927	--	--	16.08	16.08	0.10	0.02	0.06	0.42	0.00	0.00	20.9
5	20	-0	-6764	0	0	0	945	--	--	16.08	16.08	0.10	0.02	0.06	0.42	0.00	0.00	20.9
6	20	-0	-6744	0	0	0	1072	--	--	16.08	16.08	0.10	0.02	0.06	0.42	0.00	0.00	20.9
7	20	-0	-6716	0	0	0	1131	--	--	16.08	16.08	0.10	0.02	0.06	0.42	0.00	0.00	20.9
8	20	-0	-6761	0	0	0	996	--	--	16.08	16.08	0.10	0.02	0.06	0.42	0.00	0.00	20.9
9	20	-0	-6733	0	0	0	1054	--	--	16.08	16.08	0.10	0.02	0.06	0.42	0.00	0.00	20.9
10	20	-0	-6713	0	0	0	1181	--	--	16.08	16.08	0.10	0.02	0.06	0.42	0.00	0.00	20.9
11	20	-0	-6705	0	0	0	1199	--	--	16.08	16.08	0.10	0.02	0.06	0.42	0.00	0.00	20.9
12	20	-0	-6772	0	0	0	927	--	--	16.08	16.08	0.10	0.02	0.06	0.42	0.00	0.00	20.9
13	20	-0	-6764	0	0	0	945	--	--	16.08	16.08	0.10	0.02	0.06	0.42	0.00	0.00	20.9
14	20	-0	-6744	0	0	0	1072	--	--	16.08	16.08	0.10	0.02	0.06	0.42	0.00	0.00	20.9
15	20	-0	-6716	0	0	0	1131	--	--	16.08	16.08	0.10	0.02	0.06	0.42	0.00	0.00	20.9
16	20	-0	-6761	0	0	0	996	--	--	16.08	16.08	0.10	0.02	0.06	0.42	0.00	0.00	20.9
17	20	-0	-6733	0	0	0	1054	--	--	16.08	16.08	0.10	0.02	0.06	0.42	0.00	0.00	20.9
18	20	-0	-10530	0	0	0	2958	--	--	16.08	16.08	0.00	0.05	0.09	0.66	0.00	0.00	20.9
19	20	-0	-11470	0	0	0	1927	--	--	16.08	16.08	0.00	0.03	0.09	0.72	0.00	0.00	20.9
20	20	-0	-10610	0	0	0	2344	--	--	16.08	16.08	0.00	0.04	0.09	0.67	0.00	0.00	20.9
37	20	-0	-9503	0	0	0	2957	--	--	16.08	16.08	0.00	0.05	0.08	0.60	0.00	0.00	20.9
38	20	-0	-11060	0	0	0	1238	--	--	16.08	16.08	0.00	0.02	0.09	0.69	0.00	0.00	20.9
39	20	-0	-9628	0	0	0	1933	--	--	16.08	16.08	0.00	0.03	0.08	0.60	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 177 NI 1669 NF 1672 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-3243	0	0	0	-3776	--	--	16.08	16.08	0.18	0.06	0.03	0.20	0.00	0.00	20.9
2	0	-0	-3476	0	0	0	-3865	--	--	16.08	16.08	0.29	0.07	0.03	0.22	0.00	0.00	20.9
3	0	-0	-3454	0	0	0	-3843	--	--	16.08	16.08	0.29	0.07	0.03	0.22	0.00	0.00	20.9
4	0	-0	-1535	0	0	0	-1966	--	--	16.08	16.08	0.29	0.03	0.01	0.10	0.00	0.00	20.9
5	0	-0	-1514	0	0	0	-1944	--	--	16.08	16.08	0.29	0.03	0.01	0.09	0.00	0.00	20.9
6	0	-0	-2822	0	0	0	-3225	--	--	16.08	16.08	0.29	0.06	0.02	0.18	0.00	0.00	20.9
7	0	-0	-2750	0	0	0	-3153	--	--	16.08	16.08	0.29	0.05	0.02	0.17	0.00	0.00	20.9
8	0	-0	-2239	0	0	0	-2656	--	--	16.08	16.08	0.29	0.05	0.02	0.14	0.00	0.00	20.9
9	0	-0	-2168	0	0	0	-2583	--	--	16.08	16.08	0.29	0.04	0.02	0.14	0.00	0.00	20.9
10	0	-0	-3476	0	0	0	-3865	--	--	16.08	16.08	0.29	0.07	0.03	0.22	0.00	0.00	20.9
11	0	-0	-3454	0	0	0	-3843	--	--	16.08	16.08	0.29	0.07	0.03	0.22	0.00	0.00	20.9
12	0	-0	-1535	0	0	0	-1966	--	--	16.08	16.08	0.29	0.03	0.01	0.10	0.00	0.00	20.9
13	0	-0	-1514	0	0	0	-1944	--	--	16.08	16.08	0.29	0.03	0.01	0.09	0.00	0.00	20.9
14	0	-0	-2822	0	0	0	-3225	--	--	16.08	16.08	0.29	0.06	0.02	0.18	0.00	0.00	20.9
15	0	-0	-2750	0	0	0	-3153	--	--	16.08	16.08	0.29	0.05	0.02	0.17	0.00	0.00	20.9
16	0	-0	-2239	0	0	0	-2656	--	--	16.08	16.08	0.29	0.05	0.02	0.14	0.00	0.00	20.9
17	0	-0	-2168	0	0	0	-2583	--	--	16.08	16.08	0.29	0.04	0.02	0.14	0.00	0.00	20.9
18	0	-0	-14210	0	0	0	-14620	--	--	16.08	16.08	0.18	0.24	0.12	0.89	0.00	0.00	20.9
19	0	-0	-4544	0	0	0	-5230	--	--	16.08	16.08	0.18	0.09	0.04	0.29	0.00	0.00	20.9
20	0	-0	-8476	0	0	0	-9012	--	--	16.08	16.08	0.18	0.15	0.07	0.53	0.00	0.00	20.9
37	0	-0	-15430	0	0	0	-15740	--	--	16.08	16.08	0.18	0.26	0.13	0.97	0.00	0.00	20.9
38	0	-0	690	0	0	0	-429	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
39	0	-0	-5863	0	0	0	-6387	--	--	16.08	16.08	0.18	0.11	0.05	0.37	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	25	-0	-3243	0	0	0	-3776	--	--	16.08	16.08	0.18	0.06	0.03	0.20	0.00	0.00	20.9
2	25	-0	-3476	0	0	0	-3865	--	--	16.08	16.08	0.29	0.07	0.03	0.22	0.00	0.00	20.9
3	25	-0	-3454	0	0	0	-3843	--	--	16.08	16.08	0.29	0.07	0.03	0.22	0.00	0.00	20.9
4	25	-0	-1535	0	0	0	-1966	--	--	16.08	16.08	0.29	0.03	0.01	0.10	0.00	0.00	20.9
5	25	-0	-1514	0	0	0	-1944	--	--	16.08	16.08	0.29	0.03	0.01	0.09	0.00	0.00	20.9
6	25	-0	-2822	0	0	0	-3225	--	--	16.08	16.08	0.29	0.06	0.02	0.18	0.00	0.00	20.9
7	25	-0	-2750	0	0	0	-3153	--	--	16.08	16.08	0.29	0.05	0.02	0.17	0.00	0.00	20.9
8	25	-0	-2239	0	0	0	-2656	--	--	16.08	16.08	0.29	0.05	0.02	0.14	0.00	0.00	20.9
9	25	-0	-2168	0	0	0	-2583	--	--	16.08	16.08	0.29	0.04	0.02	0.14	0.00	0.00	20.9
10	25	-0	-3476	0	0	0	-3865	--	--	16.08	16.08	0.29	0.07	0.03	0.22	0.00	0.00	20.9
11	25	-0	-3454	0	0	0	-3843	--	--	16.08	16.08	0.29	0.07	0.03	0.22	0.00	0.00	20.9
12	25	-0	-1535	0	0	0	-1966	--	--	16.08	16.08	0.29	0.03	0.01	0.10	0.00	0.00	20.9
13	25	-0	-1514	0	0	0	-1944	--	--	16.08	16.08	0.29	0.03	0.01	0.09	0.00	0.00	20.9
14	25	-0	-2822	0	0	0	-3225	--	--	16.08	16.08	0.29	0.06	0.02	0.18	0.00	0.00	20.9
15	25	-0	-2750	0	0	0	-3153	--	--	16.08	16.08	0.29	0.05	0.02	0.17	0.00	0.00	20.9
16	25	-0	-2239	0	0	0	-2656	--	--	16.08	16.08	0.29	0.05	0.02	0.14	0.00	0.00	20.9
17	25	-0	-2168	0	0	0	-2583	--	--	16.08	16.08	0.29	0.04	0.02	0.14	0.00	0.00	20.9
18	25	-0	-14210	0	0	0	-14620	--	--	16.08	16.08	0.18	0.24	0.12	0.89	0.00	0.00	20.9
19	25	-0	-4544	0	0	0	-5230	--	--	16.08	16.08	0.18	0.09	0.04	0.29	0.00	0.00	20.9
20	25	-0	-8476	0	0	0	-9012	--	--	16.08	16.08	0.18	0.15	0.07	0.53	0.00	0.00	20.9
37	25	-0	-15430	0	0	0	-15740	--	--	16.08	16.08	0.18	0.26	0.13	0.97	0.00	0.00	20.9
38	25	-0	690	0	0	0	-429	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
39	25	-0	-5863	0	0	0	-6387	--	--	16.08	16.08	0.18	0.11	0.05	0.37	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	50	-0	-3243	0	0	0	-3776	--	--	16.08	16.08	0.18	0.06	0.03	0.20	0.00	0.00	20.9
2	50	-0	-3476	0	0	0	-3865	--	--	16.08	16.08	0.29	0.07	0.03	0.22	0.00	0.00	20.9
3	50	-0	-3454	0	0	0	-3843	--	--	16.08	16.08	0.29	0.07	0.03	0.22	0.00	0.00	20.9
4	50	-0	-1535	0	0	0	-1966	--	--	16.08	16.08	0.29	0.03	0.01	0.10	0.00	0.00	20.9
5	50	-0	-1514	0	0	0	-1944	--	--	16.08	16.08	0.29	0.03	0.01	0.09	0.00	0.00	20.9
6	50	-0	-2822	0	0	0	-3225	--	--	16.08	16.08	0.29	0.06	0.02	0.18	0.00	0.00	20.9
7	50	-0	-2750	0	0	0	-3153	--	--	16.08	16.08	0.29	0.05	0.02	0.17	0.00	0.00	20.9
8	50	-0	-2239	0	0	0	-2656	--	--	16.08	16.08	0.29	0.05	0.02	0.14	0.00	0.00	20.9
9	50	-0	-2168	0	0	0	-2583	--	--	16.08	16.08	0.29	0.04	0.02	0.14	0.00	0.00	20.9
10	50	-0	-3476	0	0	0	-3865	--	--	16.08	16.08	0.29	0.07	0.03	0.22	0.00	0.00	20.9
11	50	-0	-3454	0	0	0	-3843	--	--	16.08	16.08	0.29	0.07	0.03	0.22	0.00	0.00	20.9
12	50	-0	-1535	0	0	0	-1966	--	--	16.08	16.08	0.29	0.03	0.01	0.10	0.00	0.00	20.9
13	50	-0	-1514	0	0	0	-1944	--	--	16.08	16.08	0.29	0.03	0.01	0.09	0.00	0.00	20.9
14	50	-0	-2822	0	0	0	-3225	--	--	16.08	16.08	0.29	0.06	0.02	0.18	0.00	0.00	20.9
15	50	-0	-2750	0	0	0	-3153	--	--	16.08	16.08	0.29	0.05	0.02	0.17	0.00	0.00	20.9
16	50	-0	-2239	0	0	0	-2656	--	--	16.08	16.08	0.29	0.05	0.02	0.14	0.00	0.00	20.9
17	50	-0	-2168	0	0	0	-2583	--	--	16.08	16.08	0.29	0.04	0.02	0.14	0.00	0.00	20.9
18	50	-0	-14210	0	0	0	-14620	--	--	16.08	16.08	0.18	0.24	0.12	0.89	0.00	0.00	20.9
19	50	-0	-4544	0	0	0	-5230	--	--	16.08	16.08	0.18	0.09	0.04	0.29	0.00	0.00	20.9
20	50	-0	-8476	0	0	0	-9012	--	--	16.08	16.08	0.18	0.15	0.07	0.53	0.00	0.00	20.9
37	50	-0	-15430	0	0	0	-15740	--	--	16.08	16.08	0.18	0.26	0.13	0.97	0.00	0.00	20.9
38	50	-0	690	0	0	0	-429	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
39	50	-0	-5863	0	0	0	-6387	--	--	16.08	16.08	0.18	0.11	0.05	0.37	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 178 NI 1666 NF 1669 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-3184	0	0	0	-2154	--	--	16.08	16.08	0.18	0.04	0.03	0.20	0.00	0.00	20.9
2	0	-0	-3170	0	0	0	-2127	--	--	16.08	16.08	0.29	0.04	0.03	0.20	0.00	0.00	20.9
3	0	-0	-3153	0	0	0	-2116	--	--	16.08	16.08	0.29	0.04	0.03	0.20	0.00	0.00	20.9
4	0	-0	-1746	0	0	0	-1198	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
5	0	-0	-1729	0	0	0	-1187	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
6	0	-0	-2691	0	0	0	-1815	--	--	16.08	16.08	0.29	0.03	0.02	0.17	0.00	0.00	20.9
7	0	-0	-2635	0	0	0	-1778	--	--	16.08	16.08	0.29	0.03	0.02	0.17	0.00	0.00	20.9
8	0	-0	-2264	0	0	0	-1536	--	--	16.08	16.08	0.29	0.03	0.02	0.14	0.00	0.00	20.9
9	0	-0	-2208	0	0	0	-1499	--	--	16.08	16.08	0.29	0.03	0.02	0.14	0.00	0.00	20.9
10	0	-0	-3170	0	0	0	-2127	--	--	16.08	16.08	0.29	0.04	0.03	0.20	0.00	0.00	20.9

11	0	-0	-3153	0	0	0	-2116	--	--	16.08	16.08	0.29	0.04	0.03	0.20	0.00	0.00	20.9
12	0	-0	-1746	0	0	0	-1198	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
13	0	-0	-1729	0	0	0	-1187	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
14	0	-0	-2691	0	0	0	-1815	--	--	16.08	16.08	0.29	0.03	0.02	0.17	0.00	0.00	20.9
15	0	-0	-2635	0	0	0	-1778	--	--	16.08	16.08	0.29	0.03	0.02	0.17	0.00	0.00	20.9
16	0	-0	-2264	0	0	0	-1536	--	--	16.08	16.08	0.29	0.03	0.02	0.14	0.00	0.00	20.9
17	0	-0	-2208	0	0	0	-1499	--	--	16.08	16.08	0.29	0.03	0.02	0.14	0.00	0.00	20.9
18	0	-0	-11390	0	0	0	-7517	--	--	16.08	16.08	0.18	0.12	0.09	0.71	0.00	0.00	20.9
19	0	-0	-4381	0	0	0	-2958	--	--	16.08	16.08	0.18	0.05	0.04	0.27	0.00	0.00	20.9
20	0	-0	-7180	0	0	0	-4774	--	--	16.08	16.08	0.18	0.08	0.06	0.45	0.00	0.00	20.9
37	0	-0	-12180	0	0	0	-8028	--	--	16.08	16.08	0.18	0.13	0.10	0.76	0.00	0.00	20.9
38	0	-0	-507	0	0	0	-429	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9
39	0	-0	-5171	0	0	0	-3456	--	--	16.08	16.08	0.18	0.06	0.04	0.32	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	25	-0	-3184	0	0	0	-2154	--	--	16.08	16.08	0.18	0.04	0.03	0.20	0.00	0.00	20.9
2	25	-0	-3170	0	0	0	-2127	--	--	16.08	16.08	0.29	0.04	0.03	0.20	0.00	0.00	20.9
3	25	-0	-3153	0	0	0	-2116	--	--	16.08	16.08	0.29	0.04	0.03	0.20	0.00	0.00	20.9
4	25	-0	-1746	0	0	0	-1198	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
5	25	-0	-1729	0	0	0	-1187	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
6	25	-0	-2691	0	0	0	-1815	--	--	16.08	16.08	0.29	0.03	0.02	0.17	0.00	0.00	20.9
7	25	-0	-2635	0	0	0	-1778	--	--	16.08	16.08	0.29	0.03	0.02	0.17	0.00	0.00	20.9
8	25	-0	-2264	0	0	0	-1536	--	--	16.08	16.08	0.29	0.03	0.02	0.14	0.00	0.00	20.9
9	25	-0	-2208	0	0	0	-1499	--	--	16.08	16.08	0.29	0.03	0.02	0.14	0.00	0.00	20.9
10	25	-0	-3170	0	0	0	-2127	--	--	16.08	16.08	0.29	0.04	0.03	0.20	0.00	0.00	20.9
11	25	-0	-3153	0	0	0	-2116	--	--	16.08	16.08	0.29	0.04	0.03	0.20	0.00	0.00	20.9
12	25	-0	-1746	0	0	0	-1198	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
13	25	-0	-1729	0	0	0	-1187	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
14	25	-0	-2691	0	0	0	-1815	--	--	16.08	16.08	0.29	0.03	0.02	0.17	0.00	0.00	20.9
15	25	-0	-2635	0	0	0	-1778	--	--	16.08	16.08	0.29	0.03	0.02	0.17	0.00	0.00	20.9
16	25	-0	-2264	0	0	0	-1536	--	--	16.08	16.08	0.29	0.03	0.02	0.14	0.00	0.00	20.9
17	25	-0	-2208	0	0	0	-1499	--	--	16.08	16.08	0.29	0.03	0.02	0.14	0.00	0.00	20.9
18	25	-0	-11390	0	0	0	-7517	--	--	16.08	16.08	0.18	0.12	0.09	0.71	0.00	0.00	20.9
19	25	-0	-4381	0	0	0	-2958	--	--	16.08	16.08	0.18	0.05	0.04	0.27	0.00	0.00	20.9
20	25	-0	-7180	0	0	0	-4774	--	--	16.08	16.08	0.18	0.08	0.06	0.45	0.00	0.00	20.9
37	25	-0	-12180	0	0	0	-8028	--	--	16.08	16.08	0.18	0.13	0.10	0.76	0.00	0.00	20.9
38	25	-0	-507	0	0	0	-429	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9
39	25	-0	-5171	0	0	0	-3456	--	--	16.08	16.08	0.18	0.06	0.04	0.32	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	50	-0	-3184	0	0	0	-2154	--	--	16.08	16.08	0.18	0.04	0.03	0.20	0.00	0.00	20.9
2	50	-0	-3170	0	0	0	-2127	--	--	16.08	16.08	0.29	0.04	0.03	0.20	0.00	0.00	20.9
3	50	-0	-3153	0	0	0	-2116	--	--	16.08	16.08	0.29	0.04	0.03	0.20	0.00	0.00	20.9
4	50	-0	-1746	0	0	0	-1198	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
5	50	-0	-1729	0	0	0	-1187	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
6	50	-0	-2691	0	0	0	-1815	--	--	16.08	16.08	0.29	0.03	0.02	0.17	0.00	0.00	20.9
7	50	-0	-2635	0	0	0	-1778	--	--	16.08	16.08	0.29	0.03	0.02	0.17	0.00	0.00	20.9
8	50	-0	-2264	0	0	0	-1536	--	--	16.08	16.08	0.29	0.03	0.02	0.14	0.00	0.00	20.9
9	50	-0	-2208	0	0	0	-1499	--	--	16.08	16.08	0.29	0.03	0.02	0.14	0.00	0.00	20.9
10	50	-0	-3170	0	0	0	-2127	--	--	16.08	16.08	0.29	0.04	0.03	0.20	0.00	0.00	20.9
11	50	-0	-3153	0	0	0	-2116	--	--	16.08	16.08	0.29	0.04	0.03	0.20	0.00	0.00	20.9
12	50	-0	-1746	0	0	0	-1198	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
13	50	-0	-1729	0	0	0	-1187	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
14	50	-0	-2691	0	0	0	-1815	--	--	16.08	16.08	0.29	0.03	0.02	0.17	0.00	0.00	20.9
15	50	-0	-2635	0	0	0	-1778	--	--	16.08	16.08	0.29	0.03	0.02	0.17	0.00	0.00	20.9
16	50	-0	-2264	0	0	0	-1536	--	--	16.08	16.08	0.29	0.03	0.02	0.14	0.00	0.00	20.9
17	50	-0	-2208	0	0	0	-1499	--	--	16.08	16.08	0.29	0.03	0.02	0.14	0.00	0.00	20.9
18	50	-0	-11390	0	0	0	-7517	--	--	16.08	16.08	0.18	0.12	0.09	0.71	0.00	0.00	20.9
19	50	-0	-4381	0	0	0	-2958	--	--	16.08	16.08	0.18	0.05	0.04	0.27	0.00	0.00	20.9
20	50	-0	-7180	0	0	0	-4774	--	--	16.08	16.08	0.18	0.08	0.06	0.45	0.00	0.00	20.9
37	50	-0	-12180	0	0	0	-8028	--	--	16.08	16.08	0.18	0.13	0.10	0.76	0.00	0.00	20.9
38	50	-0	-507	0	0	0	-429	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9
39	50	-0	-5171	0	0	0	-3456	--	--	16.08	16.08	0.18	0.06	0.04	0.32	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 179 NI 799 NF 1666 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-1405	0	0	0	-562	--	--	16.08	16.08	0.18	0.01	0.01	0.09	0.00	0.00	20.9
2	0	-0	-1355	0	0	0	-542	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
3	0	-0	-1348	0	0	0	-539	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
4	0	-0	-813	0	0	0	-325	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
5	0	-0	-807	0	0	0	-323	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
6	0	-0	-1173	0	0	0	-469	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
7	0	-0	-1151	0	0	0	-460	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
8	0	-0	-1011	0	0	0	-404	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
9	0	-0	-988	0	0	0	-395	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
10	0	-0	-1355	0	0	0	-542	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
11	0	-0	-1348	0	0	0	-539	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
12	0	-0	-813	0	0	0	-325	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
13	0	-0	-807	0	0	0	-323	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
14	0	-0	-1173	0	0	0	-469	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
15	0	-0	-1151	0	0	0	-460	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
16	0	-0	-1011	0	0	0	-404	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
17	0	-0	-988	0	0	0	-395	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
18	0	-0	-4560	0	0	0	-1824	--	--	16.08	16.08	0.18	0.03	0.04	0.29	0.00	0.00	20.9
19	0	-0	-1919	0	0	0	-768	--	--	16.08	16.08	0.18	0.01	0.02	0.12	0.00	0.00	20.9
20	0	-0	-2961	0	0	0	-1184	--	--	16.08	16.08	0.18	0.02	0.02	0.19	0.00	0.00	20.9
37	0	-0	-4840	0	0	0	-1936	--	--	16.08	16.08	0.18	0.03	0.04	0.30	0.00	0.00	20.9
38	0	-0	-438	0	0	0	-175	--	--	16.08	16.08	0.18	0.00	0.00	0.03	0.00	0.00	20.9
39	0	-0	-2176	0	0	0	-870	--	--	16.08	16.08	0.18	0.01	0.02	0.14	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	20	-0	-1405	0	0	0	-562	--	--	16.08	16.08	0.18	0.01	0.01	0.09	0.00	0.00	20.9
2	20	-0	-1355	0	0	0	-542	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
3	20	-0	-1348	0	0	0	-539	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
4	20	-0	-813	0	0	0	-325	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
5	20	-0	-807	0	0	0	-323	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
6	20	-0	-1173	0	0	0	-469	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9

7	20	-0	-1151	0	0	0	-460	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
8	20	-0	-1011	0	0	0	-404	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
9	20	-0	-988	0	0	0	-395	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
10	20	-0	-1355	0	0	0	-542	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
11	20	-0	-1348	0	0	0	-539	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
12	20	-0	-813	0	0	0	-325	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
13	20	-0	-807	0	0	0	-323	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
14	20	-0	-1173	0	0	0	-469	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
15	20	-0	-1151	0	0	0	-460	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
16	20	-0	-1011	0	0	0	-404	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
17	20	-0	-988	0	0	0	-395	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
18	20	-0	-4560	0	0	0	-1824	--	--	16.08	16.08	0.18	0.03	0.04	0.29	0.00	0.00	20.9
19	20	-0	-1919	0	0	0	-768	--	--	16.08	16.08	0.18	0.01	0.02	0.12	0.00	0.00	20.9
20	20	-0	-2961	0	0	0	-1184	--	--	16.08	16.08	0.18	0.02	0.02	0.19	0.00	0.00	20.9
37	20	-0	-4840	0	0	0	-1936	--	--	16.08	16.08	0.18	0.03	0.04	0.30	0.00	0.00	20.9
38	20	-0	-438	0	0	0	-175	--	--	16.08	16.08	0.18	0.00	0.00	0.03	0.00	0.00	20.9
39	20	-0	-2176	0	0	0	-870	--	--	16.08	16.08	0.18	0.01	0.02	0.14	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	40	-0	-1405	0	0	0	-562	--	--	16.08	16.08	0.18	0.01	0.01	0.09	0.00	0.00	20.9
2	40	-0	-1355	0	0	0	-542	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
3	40	-0	-1348	0	0	0	-539	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
4	40	-0	-813	0	0	0	-325	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
5	40	-0	-807	0	0	0	-323	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
6	40	-0	-1173	0	0	0	-469	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
7	40	-0	-1151	0	0	0	-460	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
8	40	-0	-1011	0	0	0	-404	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
9	40	-0	-988	0	0	0	-395	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
10	40	-0	-1355	0	0	0	-542	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
11	40	-0	-1348	0	0	0	-539	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
12	40	-0	-813	0	0	0	-325	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
13	40	-0	-807	0	0	0	-323	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
14	40	-0	-1173	0	0	0	-469	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
15	40	-0	-1151	0	0	0	-460	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
16	40	-0	-1011	0	0	0	-404	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
17	40	-0	-988	0	0	0	-395	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
18	40	-0	-4560	0	0	0	-1824	--	--	16.08	16.08	0.18	0.03	0.04	0.29	0.00	0.00	20.9
19	40	-0	-1919	0	0	0	-768	--	--	16.08	16.08	0.18	0.01	0.02	0.12	0.00	0.00	20.9
20	40	-0	-2961	0	0	0	-1184	--	--	16.08	16.08	0.18	0.02	0.02	0.19	0.00	0.00	20.9
37	40	-0	-4840	0	0	0	-1936	--	--	16.08	16.08	0.18	0.03	0.04	0.30	0.00	0.00	20.9
38	40	-0	-438	0	0	0	-175	--	--	16.08	16.08	0.18	0.00	0.00	0.03	0.00	0.00	20.9
39	40	-0	-2176	0	0	0	-870	--	--	16.08	16.08	0.18	0.01	0.02	0.14	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 180 NI 1571 NF 1559 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-251	0	0	0	100	--	--	16.08	16.08	0.00	0.00	0.00	0.02	0.00	0.00	20.9
2	0	-0	-333	0	0	0	133	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
3	0	-0	-335	0	0	0	134	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
4	0	-0	-51	0	0	0	20	--	--	16.08	16.08	0.10	0.00	0.00	0.00	0.00	0.00	20.9
5	0	-0	-53	0	0	0	21	--	--	16.08	16.08	0.10	0.00	0.00	0.00	0.00	0.00	20.9
6	0	-0	-233	0	0	0	93	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
7	0	-0	-238	0	0	0	95	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
8	0	-0	-148	0	0	0	59	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
9	0	-0	-154	0	0	0	62	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
10	0	-0	-333	0	0	0	133	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
11	0	-0	-335	0	0	0	134	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
12	0	-0	-51	0	0	0	20	--	--	16.08	16.08	0.10	0.00	0.00	0.00	0.00	0.00	20.9
13	0	-0	-53	0	0	0	21	--	--	16.08	16.08	0.10	0.00	0.00	0.00	0.00	0.00	20.9
14	0	-0	-233	0	0	0	93	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
15	0	-0	-238	0	0	0	95	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
16	0	-0	-148	0	0	0	59	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
17	0	-0	-154	0	0	0	62	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
18	0	-0	-448	0	0	0	179	--	--	16.08	16.08	0.00	0.00	0.00	0.03	0.00	0.00	20.9
19	0	-0	963	0	0	0	-385	--	--	16.08	16.08	0.18	0.01	0.01	0.06	0.00	0.00	20.9
20	0	-0	188	0	0	0	-75	--	--	16.08	16.08	0.18	0.00	0.00	0.01	0.00	0.00	20.9
37	0	-0	-1086	0	0	0	434	--	--	16.08	16.08	0.00	0.01	0.01	0.07	0.00	0.00	20.9
38	0	-0	1267	0	0	0	-507	--	--	16.08	16.08	0.18	0.01	0.01	0.08	0.00	0.00	20.9
39	0	-0	-25	0	0	0	10	--	--	16.08	16.08	0.00	0.00	0.00	0.00	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	20	-0	-251	0	0	0	100	--	--	16.08	16.08	0.00	0.00	0.00	0.02	0.00	0.00	20.9
2	20	-0	-333	0	0	0	133	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
3	20	-0	-335	0	0	0	134	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
4	20	-0	-51	0	0	0	20	--	--	16.08	16.08	0.10	0.00	0.00	0.00	0.00	0.00	20.9
5	20	-0	-53	0	0	0	21	--	--	16.08	16.08	0.10	0.00	0.00	0.00	0.00	0.00	20.9
6	20	-0	-233	0	0	0	93	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
7	20	-0	-238	0	0	0	95	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
8	20	-0	-148	0	0	0	59	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
9	20	-0	-154	0	0	0	62	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
10	20	-0	-333	0	0	0	133	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
11	20	-0	-335	0	0	0	134	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
12	20	-0	-51	0	0	0	20	--	--	16.08	16.08	0.10	0.00	0.00	0.00	0.00	0.00	20.9
13	20	-0	-53	0	0	0	21	--	--	16.08	16.08	0.10	0.00	0.00	0.00	0.00	0.00	20.9
14	20	-0	-233	0	0	0	93	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
15	20	-0	-238	0	0	0	95	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
16	20	-0	-148	0	0	0	59	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
17	20	-0	-154	0	0	0	62	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
18	20	-0	-448	0	0	0	179	--	--	16.08	16.08	0.00	0.00	0.00	0.03	0.00	0.00	20.9
19	20	-0	963	0	0	0	-385	--	--	16.08	16.08	0.18	0.01	0.01	0.06	0.00	0.00	20.9
20	20	-0	188	0	0	0	-75	--	--	16.08	16.08	0.18	0.00	0.00	0.01	0.00	0.00	20.9
37	20	-0	-1086	0	0	0	434	--	--	16.08	16.08	0.00	0.01	0.01	0.07	0.00	0.00	20.9
38	20	-0	1267	0	0	0	-507	--	--	16.08	16.08	0.18	0.01	0.01	0.08	0.00	0.00	20.9
39	20	-0	-25	0	0	0	10	--	--	16.08	16.08	0.00	0.00	0.00	0.00	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	40	-0	-251	0	0	0	-268	--	--	16.08	16.08	0.18	0.00	0.00	0.02	0.00	0.00	20.9
2	40	-0	-333	0	0	0	-356	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9

3	40	-0	-335	0	0	0	-358	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
4	40	-0	-51	0	0	0	-55	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
5	40	-0	-53	0	0	0	-57	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
6	40	-0	-233	0	0	0	-249	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
7	40	-0	-238	0	0	0	-255	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
8	40	-0	-148	0	0	0	-158	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
9	40	-0	-154	0	0	0	-164	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
10	40	-0	-333	0	0	0	-356	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
11	40	-0	-335	0	0	0	-358	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
12	40	-0	-51	0	0	0	-55	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
13	40	-0	-53	0	0	0	-57	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
14	40	-0	-233	0	0	0	-249	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
15	40	-0	-238	0	0	0	-255	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
16	40	-0	-148	0	0	0	-158	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
17	40	-0	-154	0	0	0	-164	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
18	40	-0	-448	0	0	0	-479	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9
19	40	-0	963	0	0	0	-385	--	--	16.08	16.08	0.18	0.01	0.01	0.06	0.00	0.00	20.9
20	40	-0	188	0	0	0	-75	--	--	16.08	16.08	0.18	0.00	0.00	0.01	0.00	0.00	20.9
37	40	-0	-1086	0	0	0	-1161	--	--	16.08	16.08	0.18	0.02	0.01	0.07	0.00	0.00	20.9
38	40	-0	1267	0	0	0	-507	--	--	16.08	16.08	0.18	0.01	0.01	0.08	0.00	0.00	20.9
39	40	-0	-25	0	0	0	-27	--	--	16.08	16.08	0.18	0.00	0.00	0.00	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 181 NI 1570 NF 1571 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-1031	0	0	0	616	--	--	16.08	16.08	0.00	0.01	0.01	0.06	0.00	0.00	20.9
2	0	-0	-1178	0	0	0	723	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
3	0	-0	-1183	0	0	0	726	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
4	0	-0	-403	0	0	0	222	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
5	0	-0	-408	0	0	0	225	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
6	0	-0	-902	0	0	0	544	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
7	0	-0	-917	0	0	0	554	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
8	0	-0	-669	0	0	0	394	--	--	16.08	16.08	0.10	0.01	0.01	0.04	0.00	0.00	20.9
9	0	-0	-685	0	0	0	404	--	--	16.08	16.08	0.10	0.01	0.01	0.04	0.00	0.00	20.9
10	0	-0	-1178	0	0	0	723	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
11	0	-0	-1183	0	0	0	726	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
12	0	-0	-403	0	0	0	222	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
13	0	-0	-408	0	0	0	225	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
14	0	-0	-902	0	0	0	544	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
15	0	-0	-917	0	0	0	554	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
16	0	-0	-669	0	0	0	394	--	--	16.08	16.08	0.10	0.01	0.01	0.04	0.00	0.00	20.9
17	0	-0	-685	0	0	0	404	--	--	16.08	16.08	0.10	0.01	0.01	0.04	0.00	0.00	20.9
18	0	-0	-1703	0	0	0	1031	--	--	16.08	16.08	0.00	0.02	0.01	0.11	0.00	0.00	20.9
19	0	-0	2253	0	0	0	-1512	--	--	16.08	16.08	0.18	0.03	0.02	0.14	0.00	0.00	20.9
20	0	-0	102	0	0	0	-127	--	--	16.08	16.08	0.18	0.00	0.00	0.01	0.00	0.00	20.9
37	0	-0	-3453	0	0	0	2161	--	--	16.08	16.08	0.00	0.04	0.03	0.22	0.00	0.00	20.9
38	0	-0	3141	0	0	0	-2077	--	--	16.08	16.08	0.18	0.03	0.03	0.20	0.00	0.00	20.9
39	0	-0	-443	0	0	0	231	--	--	16.08	16.08	0.00	0.00	0.00	0.03	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	25	-0	-1031	0	0	0	616	--	--	16.08	16.08	0.00	0.01	0.01	0.06	0.00	0.00	20.9
2	25	-0	-1178	0	0	0	723	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
3	25	-0	-1183	0	0	0	726	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
4	25	-0	-403	0	0	0	222	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
5	25	-0	-408	0	0	0	225	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
6	25	-0	-902	0	0	0	544	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
7	25	-0	-917	0	0	0	554	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
8	25	-0	-669	0	0	0	394	--	--	16.08	16.08	0.10	0.01	0.01	0.04	0.00	0.00	20.9
9	25	-0	-685	0	0	0	404	--	--	16.08	16.08	0.10	0.01	0.01	0.04	0.00	0.00	20.9
10	25	-0	-1178	0	0	0	723	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
11	25	-0	-1183	0	0	0	726	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
12	25	-0	-403	0	0	0	222	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
13	25	-0	-408	0	0	0	225	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
14	25	-0	-902	0	0	0	544	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
15	25	-0	-917	0	0	0	554	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
16	25	-0	-669	0	0	0	394	--	--	16.08	16.08	0.10	0.01	0.01	0.04	0.00	0.00	20.9
17	25	-0	-685	0	0	0	404	--	--	16.08	16.08	0.10	0.01	0.01	0.04	0.00	0.00	20.9
18	25	-0	-1703	0	0	0	1031	--	--	16.08	16.08	0.00	0.02	0.01	0.11	0.00	0.00	20.9
19	25	-0	2253	0	0	0	-1512	--	--	16.08	16.08	0.18	0.03	0.02	0.14	0.00	0.00	20.9
20	25	-0	102	0	0	0	-127	--	--	16.08	16.08	0.18	0.00	0.00	0.01	0.00	0.00	20.9
37	25	-0	-3453	0	0	0	2161	--	--	16.08	16.08	0.00	0.04	0.03	0.22	0.00	0.00	20.9
38	25	-0	3141	0	0	0	-2077	--	--	16.08	16.08	0.18	0.03	0.03	0.20	0.00	0.00	20.9
39	25	-0	-443	0	0	0	231	--	--	16.08	16.08	0.00	0.00	0.00	0.03	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	50	-0	-1031	0	0	0	100	--	--	16.08	16.08	0.00	0.00	0.01	0.06	0.00	0.00	20.9
2	50	-0	-1178	0	0	0	133	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
3	50	-0	-1183	0	0	0	134	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
4	50	-0	-403	0	0	0	20	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
5	50	-0	-408	0	0	0	21	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
6	50	-0	-902	0	0	0	93	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
7	50	-0	-917	0	0	0	95	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
8	50	-0	-669	0	0	0	59	--	--	16.08	16.08	0.10	0.00	0.01	0.04	0.00	0.00	20.9
9	50	-0	-685	0	0	0	62	--	--	16.08	16.08	0.10	0.00	0.01	0.04	0.00	0.00	20.9
10	50	-0	-1178	0	0	0	133	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
11	50	-0	-1183	0	0	0	134	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
12	50	-0	-403	0	0	0	20	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
13	50	-0	-408	0	0	0	21	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
14	50	-0	-902	0	0	0	93	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
15	50	-0	-917	0	0	0	95	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
16	50	-0	-669	0	0	0	59	--	--	16.08	16.08	0.10	0.00	0.01	0.04	0.00	0.00	20.9
17	50	-0	-685	0	0	0	62	--	--	16.08	16.08	0.10	0.00	0.01	0.04	0.00	0.00	20.9
18	50	-0	-1703	0	0	0	179	--	--	16.08	16.08	0.00	0.00	0.01	0.11	0.00	0.00	20.9
19	50	-0	2253	0	0	0	-1512	--	--	16.08	16.08	0.18	0.03	0.02	0.14	0.00	0.00	20.9
20	50	-0	102	0	0	0	-127	--	--	16.08	16.08	0.18	0.00	0.00	0.01	0.00	0.00	20.9
37	50	-0	-3453	0	0	0	434	--	--	16.08	16.08	0.00	0.01	0.03	0.22	0.00	0.00	20.9
38	50	-0	3141	0	0	0	-2077	--	--	16.08	16.08	0.18	0.03	0.03	0.20	0.00	0.00	20.9
39	50	-0	-443	0	0	0	10	--	--	16.08	16.08	0.00	0.00	0.00	0.03	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 182 NI 1557 NF 1570 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-2198	0	0	0	1715	--	--	16.08	16.08	0.00	0.03	0.02	0.14	0.00	0.00	20.9
2	0	-0	-2250	0	0	0	1848	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
3	0	-0	-2257	0	0	0	1854	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
4	0	-0	-1124	0	0	0	784	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
5	0	-0	-1131	0	0	0	791	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
6	0	-0	-1848	0	0	0	1468	--	--	16.08	16.08	0.10	0.03	0.02	0.12	0.00	0.00	20.9
7	0	-0	-1871	0	0	0	1489	--	--	16.08	16.08	0.10	0.03	0.02	0.12	0.00	0.00	20.9
8	0	-0	-1510	0	0	0	1149	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
9	0	-0	-1533	0	0	0	1170	--	--	16.08	16.08	0.10	0.02	0.01	0.10	0.00	0.00	20.9
10	0	-0	-2250	0	0	0	1848	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
11	0	-0	-2257	0	0	0	1854	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
12	0	-0	-1124	0	0	0	784	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
13	0	-0	-1131	0	0	0	791	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
14	0	-0	-1848	0	0	0	1468	--	--	16.08	16.08	0.10	0.03	0.02	0.12	0.00	0.00	20.9
15	0	-0	-1871	0	0	0	1489	--	--	16.08	16.08	0.10	0.03	0.02	0.12	0.00	0.00	20.9
16	0	-0	-1510	0	0	0	1149	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
17	0	-0	-1533	0	0	0	1170	--	--	16.08	16.08	0.10	0.02	0.01	0.10	0.00	0.00	20.9
18	0	-0	-3442	0	0	0	2752	--	--	16.08	16.08	0.00	0.05	0.03	0.22	0.00	0.00	20.9
19	0	-0	2467	0	0	0	-2745	--	--	16.08	16.08	0.18	0.05	0.02	0.15	0.00	0.00	20.9
20	0	-0	-701	0	0	0	224	--	--	16.08	16.08	0.00	0.00	0.01	0.04	0.00	0.00	20.9
37	0	-0	-5977	0	0	0	5149	--	--	16.08	16.08	0.00	0.09	0.05	0.37	0.00	0.00	20.9
38	0	-0	3871	0	0	0	-4012	--	--	16.08	16.08	0.18	0.07	0.03	0.24	0.00	0.00	20.9
39	0	-0	-1410	0	0	0	936	--	--	16.08	16.08	0.00	0.02	0.01	0.09	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	25	-0	-2198	0	0	0	1715	--	--	16.08	16.08	0.00	0.03	0.02	0.14	0.00	0.00	20.9
2	25	-0	-2250	0	0	0	1848	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
3	25	-0	-2257	0	0	0	1854	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
4	25	-0	-1124	0	0	0	784	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
5	25	-0	-1131	0	0	0	791	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
6	25	-0	-1848	0	0	0	1468	--	--	16.08	16.08	0.10	0.03	0.02	0.12	0.00	0.00	20.9
7	25	-0	-1871	0	0	0	1489	--	--	16.08	16.08	0.10	0.03	0.02	0.12	0.00	0.00	20.9
8	25	-0	-1510	0	0	0	1149	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
9	25	-0	-1533	0	0	0	1170	--	--	16.08	16.08	0.10	0.02	0.01	0.10	0.00	0.00	20.9
10	25	-0	-2250	0	0	0	1848	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
11	25	-0	-2257	0	0	0	1854	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
12	25	-0	-1124	0	0	0	784	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
13	25	-0	-1131	0	0	0	791	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
14	25	-0	-1848	0	0	0	1468	--	--	16.08	16.08	0.10	0.03	0.02	0.12	0.00	0.00	20.9
15	25	-0	-1871	0	0	0	1489	--	--	16.08	16.08	0.10	0.03	0.02	0.12	0.00	0.00	20.9
16	25	-0	-1510	0	0	0	1149	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
17	25	-0	-1533	0	0	0	1170	--	--	16.08	16.08	0.10	0.02	0.01	0.10	0.00	0.00	20.9
18	25	-0	-3442	0	0	0	2752	--	--	16.08	16.08	0.00	0.05	0.03	0.22	0.00	0.00	20.9
19	25	-0	2467	0	0	0	-2745	--	--	16.08	16.08	0.18	0.05	0.02	0.15	0.00	0.00	20.9
20	25	-0	-701	0	0	0	224	--	--	16.08	16.08	0.00	0.00	0.01	0.04	0.00	0.00	20.9
37	25	-0	-5977	0	0	0	5149	--	--	16.08	16.08	0.00	0.09	0.05	0.37	0.00	0.00	20.9
38	25	-0	3871	0	0	0	-4012	--	--	16.08	16.08	0.18	0.07	0.03	0.24	0.00	0.00	20.9
39	25	-0	-1410	0	0	0	936	--	--	16.08	16.08	0.00	0.02	0.01	0.09	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	50	-0	-2198	0	0	0	616	--	--	16.08	16.08	0.00	0.01	0.02	0.14	0.00	0.00	20.9
2	50	-0	-2250	0	0	0	723	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
3	50	-0	-2257	0	0	0	726	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
4	50	-0	-1124	0	0	0	222	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
5	50	-0	-1131	0	0	0	225	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
6	50	-0	-1848	0	0	0	544	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
7	50	-0	-1871	0	0	0	554	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
8	50	-0	-1510	0	0	0	394	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
9	50	-0	-1533	0	0	0	404	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
10	50	-0	-2250	0	0	0	723	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
11	50	-0	-2257	0	0	0	726	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
12	50	-0	-1124	0	0	0	222	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
13	50	-0	-1131	0	0	0	225	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
14	50	-0	-1848	0	0	0	544	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
15	50	-0	-1871	0	0	0	554	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
16	50	-0	-1510	0	0	0	394	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
17	50	-0	-1533	0	0	0	404	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
18	50	-0	-3442	0	0	0	1031	--	--	16.08	16.08	0.00	0.02	0.03	0.22	0.00	0.00	20.9
19	50	-0	2467	0	0	0	-2745	--	--	16.08	16.08	0.18	0.05	0.02	0.15	0.00	0.00	20.9
20	50	-0	-701	0	0	0	-127	--	--	16.08	16.08	0.18	0.00	0.01	0.04	0.00	0.00	20.9
37	50	-0	-5977	0	0	0	2161	--	--	16.08	16.08	0.00	0.04	0.05	0.37	0.00	0.00	20.9
38	50	-0	3871	0	0	0	-4012	--	--	16.08	16.08	0.18	0.07	0.03	0.24	0.00	0.00	20.9
39	50	-0	-1410	0	0	0	231	--	--	16.08	16.08	0.00	0.00	0.01	0.09	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 183 NI 1545 NF 1557 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	6315	0	0	0	12460	--	--	16.08	16.08	0.00	0.21	0.05	0.40	0.00	0.00	20.9
2	0	-0	5315	0	0	0	8055	--	--	16.08	16.08	0.10	0.14	0.04	0.33	0.00	0.00	20.9
3	0	-0	5319	0	0	0	8047	--	--	16.08	16.08	0.10	0.14	0.04	0.33	0.00	0.00	20.9
4	0	-0	4397	0	0	0	11130	--	--	16.08	16.08	0.10	0.20	0.04	0.28	0.00	0.00	20.9
5	0	-0	4401	0	0	0	11120	--	--	16.08	16.08	0.10	0.20	0.04	0.28	0.00	0.00	20.9
6	0	-0	4988	0	0	0	9141	--	--	16.08	16.08	0.10	0.16	0.04	0.31	0.00	0.00	20.9
7	0	-0	5003	0	0	0	9113	--	--	16.08	16.08	0.10	0.16	0.04	0.31	0.00	0.00	20.9
8	0	-0	4713	0	0	0	10060	--	--	16.08	16.08	0.10	0.18	0.04	0.30	0.00	0.00	20.9
9	0	-0	4727	0	0	0	10030	--	--	16.08	16.08	0.10	0.18	0.04	0.30	0.00	0.00	20.9
10	0	-0	5315	0	0	0	8055	--	--	16.08	16.08	0.10	0.14	0.04	0.33	0.00	0.00	20.9

11	0	-0	5319	0	0	0	8047	--	--	16.08	16.08	0.10	0.14	0.04	0.33	0.00	0.00	20.9
12	0	-0	4397	0	0	0	11130	--	--	16.08	16.08	0.10	0.20	0.04	0.28	0.00	0.00	20.9
13	0	-0	4401	0	0	0	11120	--	--	16.08	16.08	0.10	0.20	0.04	0.28	0.00	0.00	20.9
14	0	-0	4988	0	0	0	9141	--	--	16.08	16.08	0.10	0.16	0.04	0.31	0.00	0.00	20.9
15	0	-0	5003	0	0	0	9113	--	--	16.08	16.08	0.10	0.16	0.04	0.31	0.00	0.00	20.9
16	0	-0	4713	0	0	0	10060	--	--	16.08	16.08	0.10	0.18	0.04	0.30	0.00	0.00	20.9
17	0	-0	4727	0	0	0	10030	--	--	16.08	16.08	0.10	0.18	0.04	0.30	0.00	0.00	20.9
18	0	-0	9047	0	0	0	16190	--	--	16.08	16.08	0.00	0.28	0.07	0.57	0.00	0.00	20.9
19	0	-0	3996	0	0	0	27850	--	--	16.08	16.08	0.00	0.47	0.03	0.25	0.00	0.00	20.9
20	0	-0	6466	0	0	0	20540	--	--	16.08	16.08	0.00	0.35	0.05	0.41	0.00	0.00	20.9
37	0	-0	10680	0	0	0	9201	--	--	16.08	16.08	0.00	0.16	0.09	0.67	0.00	0.00	20.9
38	0	-0	2263	0	0	0	28630	--	--	16.08	16.08	0.00	0.49	0.02	0.14	0.00	0.00	20.9
39	0	-0	6378	0	0	0	16440	--	--	16.08	16.08	0.00	0.28	0.05	0.40	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	10	-0	6315	0	0	0	19844	--	--	16.08	16.08	0.00	0.34	0.05	0.40	0.00	0.00	20.9
2	10	-0	5315	0	0	0	14267	--	--	16.08	16.08	0.10	0.25	0.04	0.33	0.00	0.00	20.9
3	10	-0	5319	0	0	0	14264	--	--	16.08	16.08	0.10	0.25	0.04	0.33	0.00	0.00	20.9
4	10	-0	4397	0	0	0	16269	--	--	16.08	16.08	0.10	0.29	0.04	0.28	0.00	0.00	20.9
5	10	-0	4401	0	0	0	16264	--	--	16.08	16.08	0.10	0.29	0.04	0.28	0.00	0.00	20.9
6	10	-0	4988	0	0	0	14971	--	--	16.08	16.08	0.10	0.27	0.04	0.31	0.00	0.00	20.9
7	10	-0	5003	0	0	0	14958	--	--	16.08	16.08	0.10	0.27	0.04	0.31	0.00	0.00	20.9
8	10	-0	4713	0	0	0	15567	--	--	16.08	16.08	0.10	0.28	0.04	0.30	0.00	0.00	20.9
9	10	-0	4727	0	0	0	15557	--	--	16.08	16.08	0.10	0.28	0.04	0.30	0.00	0.00	20.9
10	10	-0	5315	0	0	0	14267	--	--	16.08	16.08	0.10	0.25	0.04	0.33	0.00	0.00	20.9
11	10	-0	5319	0	0	0	14264	--	--	16.08	16.08	0.10	0.25	0.04	0.33	0.00	0.00	20.9
12	10	-0	4397	0	0	0	16269	--	--	16.08	16.08	0.10	0.29	0.04	0.28	0.00	0.00	20.9
13	10	-0	4401	0	0	0	16264	--	--	16.08	16.08	0.10	0.29	0.04	0.28	0.00	0.00	20.9
14	10	-0	4988	0	0	0	14971	--	--	16.08	16.08	0.10	0.27	0.04	0.31	0.00	0.00	20.9
15	10	-0	5003	0	0	0	14958	--	--	16.08	16.08	0.10	0.27	0.04	0.31	0.00	0.00	20.9
16	10	-0	4713	0	0	0	15567	--	--	16.08	16.08	0.10	0.28	0.04	0.30	0.00	0.00	20.9
17	10	-0	4727	0	0	0	15557	--	--	16.08	16.08	0.10	0.28	0.04	0.30	0.00	0.00	20.9
18	10	-0	9047	0	0	0	26764	--	--	16.08	16.08	0.00	0.46	0.07	0.57	0.00	0.00	20.9
19	10	-0	3996	0	0	0	32521	--	--	16.08	16.08	0.00	0.55	0.03	0.25	0.00	0.00	20.9
20	10	-0	6466	0	0	0	28096	--	--	16.08	16.08	0.00	0.48	0.05	0.41	0.00	0.00	20.9
37	10	-0	10680	0	0	0	21685	--	--	16.08	16.08	0.00	0.37	0.09	0.67	0.00	0.00	20.9
38	10	-0	2263	0	0	0	31274	--	--	16.08	16.08	0.00	0.53	0.02	0.14	0.00	0.00	20.9
39	10	-0	6378	0	0	0	23896	--	--	16.08	16.08	0.00	0.41	0.05	0.40	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	20	-0	6315	0	0	0	13730	--	--	16.08	16.08	0.00	0.23	0.05	0.40	0.00	0.00	20.9
2	20	-0	5315	0	0	0	9118	--	--	16.08	16.08	0.10	0.16	0.04	0.33	0.00	0.00	20.9
3	20	-0	5319	0	0	0	9111	--	--	16.08	16.08	0.10	0.16	0.04	0.33	0.00	0.00	20.9
4	20	-0	4397	0	0	0	12010	--	--	16.08	16.08	0.10	0.21	0.04	0.28	0.00	0.00	20.9
5	20	-0	4401	0	0	0	12000	--	--	16.08	16.08	0.10	0.21	0.04	0.28	0.00	0.00	20.9
6	20	-0	4988	0	0	0	10140	--	--	16.08	16.08	0.10	0.18	0.04	0.31	0.00	0.00	20.9
7	20	-0	5003	0	0	0	10110	--	--	16.08	16.08	0.10	0.18	0.04	0.31	0.00	0.00	20.9
8	20	-0	4713	0	0	0	11000	--	--	16.08	16.08	0.10	0.20	0.04	0.30	0.00	0.00	20.9
9	20	-0	4727	0	0	0	10980	--	--	16.08	16.08	0.10	0.19	0.04	0.30	0.00	0.00	20.9
10	20	-0	5315	0	0	0	9118	--	--	16.08	16.08	0.10	0.16	0.04	0.33	0.00	0.00	20.9
11	20	-0	5319	0	0	0	9111	--	--	16.08	16.08	0.10	0.16	0.04	0.33	0.00	0.00	20.9
12	20	-0	4397	0	0	0	12010	--	--	16.08	16.08	0.10	0.21	0.04	0.28	0.00	0.00	20.9
13	20	-0	4401	0	0	0	12000	--	--	16.08	16.08	0.10	0.21	0.04	0.28	0.00	0.00	20.9
14	20	-0	4988	0	0	0	10140	--	--	16.08	16.08	0.10	0.18	0.04	0.31	0.00	0.00	20.9
15	20	-0	5003	0	0	0	10110	--	--	16.08	16.08	0.10	0.18	0.04	0.31	0.00	0.00	20.9
16	20	-0	4713	0	0	0	11000	--	--	16.08	16.08	0.10	0.20	0.04	0.30	0.00	0.00	20.9
17	20	-0	4727	0	0	0	10980	--	--	16.08	16.08	0.10	0.19	0.04	0.30	0.00	0.00	20.9
18	20	-0	9047	0	0	0	18000	--	--	16.08	16.08	0.00	0.31	0.07	0.57	0.00	0.00	20.9
19	20	-0	3996	0	0	0	28650	--	--	16.08	16.08	0.00	0.49	0.03	0.25	0.00	0.00	20.9
20	20	-0	6466	0	0	0	21830	--	--	16.08	16.08	0.00	0.37	0.05	0.41	0.00	0.00	20.9
37	20	-0	10680	0	0	0	11340	--	--	16.08	16.08	0.00	0.19	0.09	0.67	0.00	0.00	20.9
38	20	-0	2263	0	0	0	29080	--	--	16.08	16.08	0.00	0.50	0.02	0.14	0.00	0.00	20.9
39	20	-0	6378	0	0	0	17720	--	--	16.08	16.08	0.00	0.30	0.05	0.40	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 184 NI 1555 NF 1545 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	9682	0	0	0	9051	--	--	16.08	16.08	0.00	0.15	0.08	0.61	0.00	0.00	20.9
2	0	-0	6435	0	0	0	5745	--	--	16.08	16.08	0.10	0.10	0.05	0.40	0.00	0.00	20.9
3	0	-0	6419	0	0	0	5727	--	--	16.08	16.08	0.10	0.10	0.05	0.40	0.00	0.00	20.9
4	0	-0	8476	0	0	0	8198	--	--	16.08	16.08	0.10	0.15	0.07	0.53	0.00	0.00	20.9
5	0	-0	8460	0	0	0	8180	--	--	16.08	16.08	0.10	0.15	0.07	0.53	0.00	0.00	20.9
6	0	-0	7167	0	0	0	6625	--	--	16.08	16.08	0.10	0.12	0.06	0.45	0.00	0.00	20.9
7	0	-0	7115	0	0	0	6564	--	--	16.08	16.08	0.10	0.12	0.06	0.45	0.00	0.00	20.9
8	0	-0	7780	0	0	0	7361	--	--	16.08	16.08	0.10	0.13	0.06	0.49	0.00	0.00	20.9
9	0	-0	7727	0	0	0	7300	--	--	16.08	16.08	0.10	0.13	0.06	0.48	0.00	0.00	20.9
10	0	-0	6435	0	0	0	5745	--	--	16.08	16.08	0.10	0.10	0.05	0.40	0.00	0.00	20.9
11	0	-0	6419	0	0	0	5727	--	--	16.08	16.08	0.10	0.10	0.05	0.40	0.00	0.00	20.9
12	0	-0	8476	0	0	0	8198	--	--	16.08	16.08	0.10	0.15	0.07	0.53	0.00	0.00	20.9
13	0	-0	8460	0	0	0	8180	--	--	16.08	16.08	0.10	0.15	0.07	0.53	0.00	0.00	20.9
14	0	-0	7167	0	0	0	6625	--	--	16.08	16.08	0.10	0.12	0.06	0.45	0.00	0.00	20.9
15	0	-0	7115	0	0	0	6564	--	--	16.08	16.08	0.10	0.12	0.06	0.45	0.00	0.00	20.9
16	0	-0	7780	0	0	0	7361	--	--	16.08	16.08	0.10	0.13	0.06	0.49	0.00	0.00	20.9
17	0	-0	7727	0	0	0	7300	--	--	16.08	16.08	0.10	0.13	0.06	0.48	0.00	0.00	20.9
18	0	-0	12650	0	0	0	11630	--	--	16.08	16.08	0.00	0.20	0.10	0.79	0.00	0.00	20.9
19	0	-0	20200	0	0	0	21310	--	--	16.08	16.08	0.00	0.36	0.17	1.27	2.37	0.00	20.9
20	0	-0	15340	0	0	0	15290	--	--	16.08	16.08	0.00	0.26	0.13	0.96	0.00	0.00	20.9
37	0	-0	7945	0	0	0	5996	--	--	16.08	16.08	0.00	0.10	0.07	0.50	0.00	0.00	20.9
38	0	-0	20530	0	0	0	22120	--	--	16.08	16.08	0.00	0.38	0.17	1.29	2.41	0.00	20.9
39	0	-0	12420	0	0	0	12090	--	--	16.08	16.08	0.00	0.21	0.10	0.78	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	30	-0	9682	0	0	0	22303	--	--	16.08	16.08	0.00	0.38	0.08	0.61	0.00	0.00	20.9
2	30	-0	6435	0	0	0	14553	--	--	16.08	16.08	0.10	0.26	0.05	0.40	0.00	0.00	20.9
3	30	-0	6419	0	0	0	14513	--	--	16.08	16.08	0.10	0.26	0.05	0.40	0.00	0.00	20.9
4	30	-0	8476	0	0	0	19798	--	--	16.08	16.08	0.10	0.35	0.07	0.53	0.00	0.00	20.9
5	30	-0	8460	0	0	0	19762	--	--	16.08	16.08	0.10	0.35	0.07	0.53	0.00	0.00	20.9
6	30	-0	7167	0	0	0	16437	--	--	16.08	16.08	0.10	0.29	0.06	0.45	0.00	0.00	20.9

7	30	-0	7115	0	0	0	16301	--	--	16.08	16.08	0.10	0.29	0.06	0.45	0.00	0.00	20.9
8	30	-0	7780	0	0	0	18010	--	--	16.08	16.08	0.10	0.32	0.06	0.49	0.00	0.00	20.9
9	30	-0	7727	0	0	0	17878	--	--	16.08	16.08	0.10	0.32	0.06	0.48	0.00	0.00	20.9
10	30	-0	6435	0	0	0	14553	--	--	16.08	16.08	0.10	0.26	0.05	0.40	0.00	0.00	20.9
11	30	-0	6419	0	0	0	14513	--	--	16.08	16.08	0.10	0.26	0.05	0.40	0.00	0.00	20.9
12	30	-0	8476	0	0	0	19798	--	--	16.08	16.08	0.10	0.35	0.07	0.53	0.00	0.00	20.9
13	30	-0	8460	0	0	0	19762	--	--	16.08	16.08	0.10	0.35	0.07	0.53	0.00	0.00	20.9
14	30	-0	7167	0	0	0	16437	--	--	16.08	16.08	0.10	0.29	0.06	0.45	0.00	0.00	20.9
15	30	-0	7115	0	0	0	16301	--	--	16.08	16.08	0.10	0.29	0.06	0.45	0.00	0.00	20.9
16	30	-0	7780	0	0	0	18010	--	--	16.08	16.08	0.10	0.32	0.06	0.49	0.00	0.00	20.9
17	30	-0	7727	0	0	0	17878	--	--	16.08	16.08	0.10	0.32	0.06	0.48	0.00	0.00	20.9
18	30	-0	12650	0	0	0	28950	--	--	16.08	16.08	0.00	0.49	0.10	0.79	0.00	0.00	20.9
19	30	-0	20200	0	0	0	48959	--	--	16.08	16.08	0.00	0.83	0.17	1.17	2.37	0.00	20.9
20	30	-0	15340	0	0	0	36285	--	--	16.08	16.08	0.00	0.62	0.13	0.96	0.00	0.00	20.9
37	30	-0	7945	0	0	0	16869	--	--	16.08	16.08	0.00	0.29	0.07	0.50	0.00	0.00	20.9
38	30	-0	20530	0	0	0	50216	--	--	16.08	16.08	0.00	0.86	0.17	1.19	2.41	0.00	20.9
39	30	-0	12420	0	0	0	29089	--	--	16.08	16.08	0.00	0.50	0.10	0.78	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	60	-0	9682	0	0	0	14860	--	--	16.08	16.08	0.00	0.25	0.08	0.61	0.00	0.00	20.9
2	60	-0	6435	0	0	0	9606	--	--	16.08	16.08	0.10	0.17	0.05	0.40	0.00	0.00	20.9
3	60	-0	6419	0	0	0	9578	--	--	16.08	16.08	0.10	0.17	0.05	0.40	0.00	0.00	20.9
4	60	-0	8476	0	0	0	13280	--	--	16.08	16.08	0.10	0.24	0.07	0.53	0.00	0.00	20.9
5	60	-0	8460	0	0	0	13260	--	--	16.08	16.08	0.10	0.24	0.07	0.53	0.00	0.00	20.9
6	60	-0	7167	0	0	0	10930	--	--	16.08	16.08	0.10	0.19	0.06	0.45	0.00	0.00	20.9
7	60	-0	7115	0	0	0	10830	--	--	16.08	16.08	0.10	0.19	0.06	0.45	0.00	0.00	20.9
8	60	-0	7780	0	0	0	12030	--	--	16.08	16.08	0.10	0.21	0.06	0.49	0.00	0.00	20.9
9	60	-0	7727	0	0	0	11940	--	--	16.08	16.08	0.10	0.21	0.06	0.48	0.00	0.00	20.9
10	60	-0	6435	0	0	0	9606	--	--	16.08	16.08	0.10	0.17	0.05	0.40	0.00	0.00	20.9
11	60	-0	6419	0	0	0	9578	--	--	16.08	16.08	0.10	0.17	0.05	0.40	0.00	0.00	20.9
12	60	-0	8476	0	0	0	13280	--	--	16.08	16.08	0.10	0.24	0.07	0.53	0.00	0.00	20.9
13	60	-0	8460	0	0	0	13260	--	--	16.08	16.08	0.10	0.24	0.07	0.53	0.00	0.00	20.9
14	60	-0	7167	0	0	0	10930	--	--	16.08	16.08	0.10	0.19	0.06	0.45	0.00	0.00	20.9
15	60	-0	7115	0	0	0	10830	--	--	16.08	16.08	0.10	0.19	0.06	0.45	0.00	0.00	20.9
16	60	-0	7780	0	0	0	12030	--	--	16.08	16.08	0.10	0.21	0.06	0.49	0.00	0.00	20.9
17	60	-0	7727	0	0	0	11940	--	--	16.08	16.08	0.10	0.21	0.06	0.48	0.00	0.00	20.9
18	60	-0	12650	0	0	0	19230	--	--	16.08	16.08	0.00	0.33	0.10	0.79	0.00	0.00	20.9
19	60	-0	20200	0	0	0	33430	--	--	16.08	16.08	0.00	0.57	0.17	1.27	2.37	0.00	20.9
20	60	-0	15340	0	0	0	24490	--	--	16.08	16.08	0.00	0.42	0.13	0.96	0.00	0.00	20.9
37	60	-0	7945	0	0	0	10760	--	--	16.08	16.08	0.00	0.18	0.07	0.50	0.00	0.00	20.9
38	60	-0	20530	0	0	0	34430	--	--	16.08	16.08	0.00	0.59	0.17	1.29	2.41	0.00	20.9
39	60	-0	12420	0	0	0	19540	--	--	16.08	16.08	0.00	0.33	0.10	0.78	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 185 NI 1553 NF 1555 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm

1	0	-0	7674	0	0	0	5214	--	--	16.08	16.08	0.00	0.09	0.06	0.48	0.00	0.00	20.9
2	0	-0	4972	0	0	0	3259	--	--	16.08	16.08	0.10	0.06	0.04	0.31	0.00	0.00	20.9
3	0	-0	4958	0	0	0	3248	--	--	16.08	16.08	0.10	0.06	0.04	0.31	0.00	0.00	20.9
4	0	-0	6848	0	0	0	4774	--	--	16.08	16.08	0.10	0.08	0.06	0.43	0.00	0.00	20.9
5	0	-0	6834	0	0	0	4762	--	--	16.08	16.08	0.10	0.08	0.06	0.43	0.00	0.00	20.9
6	0	-0	5645	0	0	0	3802	--	--	16.08	16.08	0.10	0.07	0.05	0.35	0.00	0.00	20.9
7	0	-0	5598	0	0	0	3765	--	--	16.08	16.08	0.10	0.07	0.05	0.35	0.00	0.00	20.9
8	0	-0	6208	0	0	0	4257	--	--	16.08	16.08	0.10	0.08	0.05	0.39	0.00	0.00	20.9
9	0	-0	6161	0	0	0	4219	--	--	16.08	16.08	0.10	0.07	0.05	0.39	0.00	0.00	20.9
10	0	-0	4972	0	0	0	3259	--	--	16.08	16.08	0.10	0.06	0.04	0.31	0.00	0.00	20.9
11	0	-0	4958	0	0	0	3248	--	--	16.08	16.08	0.10	0.06	0.04	0.31	0.00	0.00	20.9
12	0	-0	6848	0	0	0	4774	--	--	16.08	16.08	0.10	0.08	0.06	0.43	0.00	0.00	20.9
13	0	-0	6834	0	0	0	4762	--	--	16.08	16.08	0.10	0.08	0.06	0.43	0.00	0.00	20.9
14	0	-0	5645	0	0	0	3802	--	--	16.08	16.08	0.10	0.07	0.05	0.35	0.00	0.00	20.9
15	0	-0	5598	0	0	0	3765	--	--	16.08	16.08	0.10	0.07	0.05	0.35	0.00	0.00	20.9
16	0	-0	6208	0	0	0	4257	--	--	16.08	16.08	0.10	0.08	0.05	0.39	0.00	0.00	20.9
17	0	-0	6161	0	0	0	4219	--	--	16.08	16.08	0.10	0.07	0.05	0.39	0.00	0.00	20.9
18	0	-0	9937	0	0	0	6666	--	--	16.08	16.08	0.00	0.11	0.08	0.62	0.00	0.00	20.9
19	0	-0	17160	0	0	0	12720	--	--	16.08	16.08	0.00	0.22	0.14	1.08	2.02	0.00	20.9
20	0	-0	12610	0	0	0	8986	--	--	16.08	16.08	0.00	0.15	0.10	0.79	0.00	0.00	20.9
37	0	-0	5618	0	0	0	3188	--	--	16.08	16.08	0.00	0.05	0.05	0.35	0.00	0.00	20.9
38	0	-0	17660	0	0	0	13290	--	--	16.08	16.08	0.00	0.23	0.15	1.11	2.07	0.00	20.9
39	0	-0	10070	0	0	0	7054	--	--	16.08	16.08	0.00	0.12	0.08	0.63	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	25	-0	7674	0	0	0	15334	--	--	16.08	16.08	0.00	0.26	0.06	0.48	0.00	0.00	20.9
2	25	-0	4972	0	0	0	9816	--	--	16.08	16.08	0.10	0.17	0.04	0.31	0.00	0.00	20.9
3	25	-0	4958	0	0	0	9786	--	--	16.08	16.08	0.10	0.17	0.04	0.31	0.00	0.00	20.9
4	25	-0	6848	0	0	0	13805	--	--	16.08	16.08	0.10	0.24	0.06	0.43	0.00	0.00	20.9
5	25	-0	6834	0	0	0	13775	--	--	16.08	16.08	0.10	0.24	0.06	0.43	0.00	0.00	20.9
6	25	-0	5645	0	0	0	11247	--	--	16.08	16.08	0.10	0.20	0.05	0.35	0.00	0.00	20.9
7	25	-0	5598	0	0	0	11147	--	--	16.08	16.08	0.10	0.20	0.05	0.35	0.00	0.00	20.9
8	25	-0	6208	0	0	0	12444	--	--	16.08	16.08	0.10	0.22	0.05	0.39	0.00	0.00	20.9
9	25	-0	6161	0	0	0	12344	--	--	16.08	16.08	0.10	0.22	0.05	0.39	0.00	0.00	20.9
10	25	-0	4972	0	0	0	9816	--	--	16.08	16.08	0.10	0.17	0.04	0.31	0.00	0.00	20.9
11	25	-0	4958	0	0	0	9786	--	--	16.08	16.08	0.10	0.17	0.04	0.31	0.00	0.00	20.9
12	25	-0	6848	0	0	0	13805	--	--	16.08	16.08	0.10	0.24	0.06	0.43	0.00	0.00	20.9
13	25	-0	6834	0	0	0	13775	--	--	16.08	16.08	0.10	0.24	0.06	0.43	0.00	0.00	20.9
14	25	-0	5645	0	0	0	11247	--	--	16.08	16.08	0.10	0.20	0.05	0.35	0.00	0.00	20.9
15	25	-0	5598	0	0	0	11147	--	--	16.08	16.08	0.10	0.20	0.05	0.35	0.00	0.00	20.9
16	25	-0	6208	0	0	0	12444	--	--	16.08	16.08	0.10	0.22	0.05	0.39	0.00	0.00	20.9
17	25	-0	6161	0	0	0	12344	--	--	16.08	16.08	0.10	0.22	0.05	0.39	0.00	0.00	20.9
18	25	-0	9937	0	0	0	19768	--	--	16.08	16.08	0.00	0.34	0.08	0.62	0.00	0.00	20.9
19	25	-0	17160	0	0	0	35355	--	--	16.08	16.08	0.00	0.60	0.14	1.08	2.02	0.00	20.9
20	25	-0	12610	0	0	0	25615	--	--	16.08	16.08	0.00	0.44	0.10	0.79	0.00	0.00	20.9
37	25	-0	5618	0	0	0	10596	--	--	16.08	16.08	0.00	0.18	0.05	0.35	0.00	0.00	20.9
38	25	-0	17660	0	0	0	36579	--	--	16.08	16.08	0.00	0.62	0.15	1.11	2.07	0.00	20.9
39	25	-0	10070	0	0	0	20334	--	--	16.08	16.08	0.00	0.35	0.08	0.63	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	50	-0	7674	0	0	0	9051	--	--	16.08	16.08	0.00	0.15	0.06	0.48	0.00	0.00	20.9
2	50	-0	4972	0	0	0	5745	--	--	16.08	16.08	0.10	0.10	0.04	0.31	0.00	0.00	20.9

3	50	-0	4958	0	0	0	5727	--	--	16.08	16.08	0.10	0.10	0.04	0.31	0.00	0.00	20.9
4	50	-0	6848	0	0	0	8198	--	--	16.08	16.08	0.10	0.15	0.06	0.43	0.00	0.00	20.9
5	50	-0	6834	0	0	0	8180	--	--	16.08	16.08	0.10	0.15	0.06	0.43	0.00	0.00	20.9
6	50	-0	5645	0	0	0	6625	--	--	16.08	16.08	0.10	0.12	0.05	0.35	0.00	0.00	20.9
7	50	-0	5598	0	0	0	6564	--	--	16.08	16.08	0.10	0.12	0.05	0.35	0.00	0.00	20.9
8	50	-0	6208	0	0	0	7361	--	--	16.08	16.08	0.10	0.13	0.05	0.39	0.00	0.00	20.9
9	50	-0	6161	0	0	0	7300	--	--	16.08	16.08	0.10	0.13	0.05	0.39	0.00	0.00	20.9
10	50	-0	4972	0	0	0	5745	--	--	16.08	16.08	0.10	0.10	0.04	0.31	0.00	0.00	20.9
11	50	-0	4958	0	0	0	5727	--	--	16.08	16.08	0.10	0.10	0.04	0.31	0.00	0.00	20.9
12	50	-0	6848	0	0	0	8198	--	--	16.08	16.08	0.10	0.15	0.06	0.43	0.00	0.00	20.9
13	50	-0	6834	0	0	0	8180	--	--	16.08	16.08	0.10	0.15	0.06	0.43	0.00	0.00	20.9
14	50	-0	5645	0	0	0	6625	--	--	16.08	16.08	0.10	0.12	0.05	0.35	0.00	0.00	20.9
15	50	-0	5598	0	0	0	6564	--	--	16.08	16.08	0.10	0.12	0.05	0.35	0.00	0.00	20.9
16	50	-0	6208	0	0	0	7361	--	--	16.08	16.08	0.10	0.13	0.05	0.39	0.00	0.00	20.9
17	50	-0	6161	0	0	0	7300	--	--	16.08	16.08	0.10	0.13	0.05	0.39	0.00	0.00	20.9
18	50	-0	9937	0	0	0	11630	--	--	16.08	16.08	0.00	0.20	0.08	0.62	0.00	0.00	20.9
19	50	-0	17160	0	0	0	21310	--	--	16.08	16.08	0.00	0.36	0.14	1.08	2.02	0.00	20.9
20	50	-0	12610	0	0	0	15290	--	--	16.08	16.08	0.00	0.26	0.10	0.79	0.00	0.00	20.9
37	50	-0	5618	0	0	0	5996	--	--	16.08	16.08	0.00	0.10	0.05	0.35	0.00	0.00	20.9
38	50	-0	17660	0	0	0	22120	--	--	16.08	16.08	0.00	0.38	0.15	1.11	2.07	0.00	20.9
39	50	-0	10070	0	0	0	12090	--	--	16.08	16.08	0.00	0.21	0.08	0.63	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 186 NI 1551 NF 1553 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	5677	0	0	0	2376	--	--	16.08	16.08	0.00	0.04	0.05	0.36	0.00	0.00	20.9
2	0	-0	3596	0	0	0	1461	--	--	16.08	16.08	0.10	0.03	0.03	0.23	0.00	0.00	20.9
3	0	-0	3584	0	0	0	1456	--	--	16.08	16.08	0.10	0.03	0.03	0.22	0.00	0.00	20.9
4	0	-0	5150	0	0	0	2199	--	--	16.08	16.08	0.10	0.04	0.04	0.32	0.00	0.00	20.9
5	0	-0	5138	0	0	0	2193	--	--	16.08	16.08	0.10	0.04	0.04	0.32	0.00	0.00	20.9
6	0	-0	4153	0	0	0	1726	--	--	16.08	16.08	0.10	0.03	0.03	0.26	0.00	0.00	20.9
7	0	-0	4114	0	0	0	1708	--	--	16.08	16.08	0.10	0.03	0.03	0.26	0.00	0.00	20.9
8	0	-0	4619	0	0	0	1947	--	--	16.08	16.08	0.10	0.03	0.04	0.29	0.00	0.00	20.9
9	0	-0	4581	0	0	0	1929	--	--	16.08	16.08	0.10	0.03	0.04	0.29	0.00	0.00	20.9
10	0	-0	3596	0	0	0	1461	--	--	16.08	16.08	0.10	0.03	0.03	0.23	0.00	0.00	20.9
11	0	-0	3584	0	0	0	1456	--	--	16.08	16.08	0.10	0.03	0.03	0.22	0.00	0.00	20.9
12	0	-0	5150	0	0	0	2199	--	--	16.08	16.08	0.10	0.04	0.04	0.32	0.00	0.00	20.9
13	0	-0	5138	0	0	0	2193	--	--	16.08	16.08	0.10	0.04	0.04	0.32	0.00	0.00	20.9
14	0	-0	4153	0	0	0	1726	--	--	16.08	16.08	0.10	0.03	0.03	0.26	0.00	0.00	20.9
15	0	-0	4114	0	0	0	1708	--	--	16.08	16.08	0.10	0.03	0.03	0.26	0.00	0.00	20.9
16	0	-0	4619	0	0	0	1947	--	--	16.08	16.08	0.10	0.03	0.04	0.29	0.00	0.00	20.9
17	0	-0	4581	0	0	0	1929	--	--	16.08	16.08	0.10	0.03	0.04	0.29	0.00	0.00	20.9
18	0	-0	7291	0	0	0	3020	--	--	16.08	16.08	0.00	0.05	0.06	0.46	0.00	0.00	20.9
19	0	-0	13430	0	0	0	6008	--	--	16.08	16.08	0.00	0.10	0.11	0.84	0.00	0.00	20.9
20	0	-0	9618	0	0	0	4177	--	--	16.08	16.08	0.00	0.07	0.08	0.60	0.00	0.00	20.9
37	0	-0	3720	0	0	0	1328	--	--	16.08	16.08	0.00	0.02	0.03	0.23	0.00	0.00	20.9
38	0	-0	13960	0	0	0	6308	--	--	16.08	16.08	0.00	0.11	0.12	0.88	0.00	0.00	20.9
39	0	-0	7596	0	0	0	3256	--	--	16.08	16.08	0.00	0.06	0.06	0.48	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	25	-0	5677	0	0	0	9862	--	--	16.08	16.08	0.00	0.17	0.05	0.36	0.00	0.00	20.9
2	25	-0	3596	0	0	0	6203	--	--	16.08	16.08	0.10	0.11	0.03	0.23	0.00	0.00	20.9
3	25	-0	3584	0	0	0	6182	--	--	16.08	16.08	0.10	0.11	0.03	0.22	0.00	0.00	20.9
4	25	-0	5150	0	0	0	8991	--	--	16.08	16.08	0.10	0.16	0.04	0.32	0.00	0.00	20.9
5	25	-0	5138	0	0	0	8969	--	--	16.08	16.08	0.10	0.16	0.04	0.32	0.00	0.00	20.9
6	25	-0	4153	0	0	0	7203	--	--	16.08	16.08	0.10	0.13	0.03	0.26	0.00	0.00	20.9
7	25	-0	4114	0	0	0	7133	--	--	16.08	16.08	0.10	0.13	0.03	0.26	0.00	0.00	20.9
8	25	-0	4619	0	0	0	8039	--	--	16.08	16.08	0.10	0.14	0.04	0.29	0.00	0.00	20.9
9	25	-0	4581	0	0	0	7970	--	--	16.08	16.08	0.10	0.14	0.04	0.29	0.00	0.00	20.9
10	25	-0	3596	0	0	0	6203	--	--	16.08	16.08	0.10	0.11	0.03	0.23	0.00	0.00	20.9
11	25	-0	3584	0	0	0	6182	--	--	16.08	16.08	0.10	0.11	0.03	0.22	0.00	0.00	20.9
12	25	-0	5150	0	0	0	8991	--	--	16.08	16.08	0.10	0.16	0.04	0.32	0.00	0.00	20.9
13	25	-0	5138	0	0	0	8969	--	--	16.08	16.08	0.10	0.16	0.04	0.32	0.00	0.00	20.9
14	25	-0	4153	0	0	0	7203	--	--	16.08	16.08	0.10	0.13	0.03	0.26	0.00	0.00	20.9
15	25	-0	4114	0	0	0	7133	--	--	16.08	16.08	0.10	0.13	0.03	0.26	0.00	0.00	20.9
16	25	-0	4619	0	0	0	8039	--	--	16.08	16.08	0.10	0.14	0.04	0.29	0.00	0.00	20.9
17	25	-0	4581	0	0	0	7970	--	--	16.08	16.08	0.10	0.14	0.04	0.29	0.00	0.00	20.9
18	25	-0	7291	0	0	0	12635	--	--	16.08	16.08	0.00	0.22	0.06	0.46	0.00	0.00	20.9
19	25	-0	13430	0	0	0	23717	--	--	16.08	16.08	0.00	0.40	0.11	0.84	0.00	0.00	20.9
20	25	-0	9618	0	0	0	16861	--	--	16.08	16.08	0.00	0.29	0.08	0.60	0.00	0.00	20.9
37	25	-0	3720	0	0	0	6234	--	--	16.08	16.08	0.00	0.11	0.03	0.23	0.00	0.00	20.9
38	25	-0	13960	0	0	0	24719	--	--	16.08	16.08	0.00	0.42	0.12	0.88	0.00	0.00	20.9
39	25	-0	7596	0	0	0	13273	--	--	16.08	16.08	0.00	0.23	0.06	0.48	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	50	-0	5677	0	0	0	5214	--	--	16.08	16.08	0.00	0.09	0.05	0.36	0.00	0.00	20.9
2	50	-0	3596	0	0	0	3259	--	--	16.08	16.08	0.10	0.06	0.03	0.23	0.00	0.00	20.9
3	50	-0	3584	0	0	0	3248	--	--	16.08	16.08	0.10	0.06	0.03	0.22	0.00	0.00	20.9
4	50	-0	5150	0	0	0	4774	--	--	16.08	16.08	0.10	0.08	0.04	0.32	0.00	0.00	20.9
5	50	-0	5138	0	0	0	4762	--	--	16.08	16.08	0.10	0.08	0.04	0.32	0.00	0.00	20.9
6	50	-0	4153	0	0	0	3802	--	--	16.08	16.08	0.10	0.07	0.03	0.26	0.00	0.00	20.9
7	50	-0	4114	0	0	0	3765	--	--	16.08	16.08	0.10	0.07	0.03	0.26	0.00	0.00	20.9
8	50	-0	4619	0	0	0	4257	--	--	16.08	16.08	0.10	0.08	0.04	0.29	0.00	0.00	20.9
9	50	-0	4581	0	0	0	4219	--	--	16.08	16.08	0.10	0.07	0.04	0.29	0.00	0.00	20.9
10	50	-0	3596	0	0	0	3259	--	--	16.08	16.08	0.10	0.06	0.03	0.23	0.00	0.00	20.9
11	50	-0	3584	0	0	0	3248	--	--	16.08	16.08	0.10	0.06	0.03	0.22	0.00	0.00	20.9
12	50	-0	5150	0	0	0	4774	--	--	16.08	16.08	0.10	0.08	0.04	0.32	0.00	0.00	20.9
13	50	-0	5138	0	0	0	4762	--	--	16.08	16.08	0.10	0.08	0.04	0.32	0.00	0.00	20.9
14	50	-0	4153	0	0	0	3802	--	--	16.08	16.08	0.10	0.07	0.03	0.26	0.00	0.00	20.9
15	50	-0	4114	0	0	0	3765	--	--	16.08	16.08	0.10	0.07	0.03	0.26	0.00	0.00	20.9
16	50	-0	4619	0	0	0	4257	--	--	16.08	16.08	0.10	0.08	0.04	0.29	0.00	0.00	20.9
17	50	-0	4581	0	0	0	4219	--	--	16.08	16.08	0.10	0.07	0.04	0.29	0.00	0.00	20.9
18	50	-0	7291	0	0	0	6666	--	--	16.08	16.08	0.00	0.11	0.06	0.46	0.00	0.00	20.9
19	50	-0	13430	0	0	0	12720	--	--	16.08	16.08	0.00	0.22	0.11	0.84	0.00	0.00	20.9
20	50	-0	9618	0	0	0	8986	--	--	16.08	16.08	0.00	0.15	0.08	0.60	0.00	0.00	20.9
37	50	-0	3720	0	0	0	3188	--	--	16.08	16.08	0.00	0.05	0.03	0.23	0.00	0.00	20.9
38	50	-0	13960	0	0	0	13290	--	--	16.08	16.08	0.00	0.23	0.12	0.88	0.00	0.00	20.9
39	50	-0	7596	0	0	0	7054	--	--	16.08	16.08	0.00	0.12	0.06	0.48	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 187 NI 1549 NF 1551 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	3526	0	0	0	613	--	--	16.08	16.08	0.00	0.01	0.03	0.22	0.00	0.00	20.9
2	0	-0	2184	0	0	0	370	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
3	0	-0	2176	0	0	0	368	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
4	0	-0	3248	0	0	0	575	--	--	16.08	16.08	0.10	0.01	0.03	0.20	0.00	0.00	20.9
5	0	-0	3240	0	0	0	573	--	--	16.08	16.08	0.10	0.01	0.03	0.20	0.00	0.00	20.9
6	0	-0	2565	0	0	0	443	--	--	16.08	16.08	0.10	0.01	0.02	0.16	0.00	0.00	20.9
7	0	-0	2539	0	0	0	438	--	--	16.08	16.08	0.10	0.01	0.02	0.16	0.00	0.00	20.9
8	0	-0	2885	0	0	0	505	--	--	16.08	16.08	0.10	0.01	0.02	0.18	0.00	0.00	20.9
9	0	-0	2859	0	0	0	500	--	--	16.08	16.08	0.10	0.01	0.02	0.18	0.00	0.00	20.9
10	0	-0	2184	0	0	0	370	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
11	0	-0	2176	0	0	0	368	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
12	0	-0	3248	0	0	0	575	--	--	16.08	16.08	0.10	0.01	0.03	0.20	0.00	0.00	20.9
13	0	-0	3240	0	0	0	573	--	--	16.08	16.08	0.10	0.01	0.03	0.20	0.00	0.00	20.9
14	0	-0	2565	0	0	0	443	--	--	16.08	16.08	0.10	0.01	0.02	0.16	0.00	0.00	20.9
15	0	-0	2539	0	0	0	438	--	--	16.08	16.08	0.10	0.01	0.02	0.16	0.00	0.00	20.9
16	0	-0	2885	0	0	0	505	--	--	16.08	16.08	0.10	0.01	0.02	0.18	0.00	0.00	20.9
17	0	-0	2859	0	0	0	500	--	--	16.08	16.08	0.10	0.01	0.02	0.18	0.00	0.00	20.9
18	0	-0	4493	0	0	0	774	--	--	16.08	16.08	0.00	0.01	0.04	0.28	0.00	0.00	20.9
19	0	-0	8784	0	0	0	1616	--	--	16.08	16.08	0.00	0.03	0.07	0.55	0.00	0.00	20.9
20	0	-0	6147	0	0	0	1103	--	--	16.08	16.08	0.00	0.02	0.05	0.39	0.00	0.00	20.9
37	0	-0	2049	0	0	0	304	--	--	16.08	16.08	0.00	0.01	0.02	0.13	0.00	0.00	20.9
38	0	-0	9202	0	0	0	1707	--	--	16.08	16.08	0.00	0.03	0.08	0.58	0.00	0.00	20.9
39	0	-0	4806	0	0	0	853	--	--	16.08	16.08	0.00	0.01	0.04	0.30	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	25	-0	3526	0	0	0	5263	--	--	16.08	16.08	0.00	0.09	0.03	0.22	0.00	0.00	20.9
2	25	-0	2184	0	0	0	3249	--	--	16.08	16.08	0.10	0.06	0.02	0.14	0.00	0.00	20.9
3	25	-0	2176	0	0	0	3238	--	--	16.08	16.08	0.10	0.06	0.02	0.14	0.00	0.00	20.9
4	25	-0	3248	0	0	0	4858	--	--	16.08	16.08	0.10	0.09	0.03	0.20	0.00	0.00	20.9
5	25	-0	3240	0	0	0	4846	--	--	16.08	16.08	0.10	0.09	0.03	0.20	0.00	0.00	20.9
6	25	-0	2565	0	0	0	3826	--	--	16.08	16.08	0.10	0.07	0.02	0.16	0.00	0.00	20.9
7	25	-0	2539	0	0	0	3787	--	--	16.08	16.08	0.10	0.07	0.02	0.16	0.00	0.00	20.9
8	25	-0	2885	0	0	0	4309	--	--	16.08	16.08	0.10	0.08	0.02	0.18	0.00	0.00	20.9
9	25	-0	2859	0	0	0	4270	--	--	16.08	16.08	0.10	0.08	0.02	0.18	0.00	0.00	20.9
10	25	-0	2184	0	0	0	3249	--	--	16.08	16.08	0.10	0.06	0.02	0.14	0.00	0.00	20.9
11	25	-0	2176	0	0	0	3238	--	--	16.08	16.08	0.10	0.06	0.02	0.14	0.00	0.00	20.9
12	25	-0	3248	0	0	0	4858	--	--	16.08	16.08	0.10	0.09	0.03	0.20	0.00	0.00	20.9
13	25	-0	3240	0	0	0	4846	--	--	16.08	16.08	0.10	0.09	0.03	0.20	0.00	0.00	20.9
14	25	-0	2565	0	0	0	3826	--	--	16.08	16.08	0.10	0.07	0.02	0.16	0.00	0.00	20.9
15	25	-0	2539	0	0	0	3787	--	--	16.08	16.08	0.10	0.07	0.02	0.16	0.00	0.00	20.9
16	25	-0	2885	0	0	0	4309	--	--	16.08	16.08	0.10	0.08	0.02	0.18	0.00	0.00	20.9
17	25	-0	2859	0	0	0	4270	--	--	16.08	16.08	0.10	0.08	0.02	0.18	0.00	0.00	20.9
18	25	-0	4493	0	0	0	6699	--	--	16.08	16.08	0.00	0.11	0.04	0.28	0.00	0.00	20.9
19	25	-0	8784	0	0	0	13200	--	--	16.08	16.08	0.00	0.23	0.07	0.55	0.00	0.00	20.9
20	25	-0	6147	0	0	0	9210	--	--	16.08	16.08	0.00	0.16	0.05	0.39	0.00	0.00	20.9
37	25	-0	2049	0	0	0	3006	--	--	16.08	16.08	0.00	0.05	0.02	0.13	0.00	0.00	20.9
38	25	-0	9202	0	0	0	13842	--	--	16.08	16.08	0.00	0.24	0.08	0.58	0.00	0.00	20.9
39	25	-0	4806	0	0	0	7191	--	--	16.08	16.08	0.00	0.12	0.04	0.30	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	50	-0	3526	0	0	0	2376	--	--	16.08	16.08	0.00	0.04	0.03	0.22	0.00	0.00	20.9
2	50	-0	2184	0	0	0	1461	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
3	50	-0	2176	0	0	0	1456	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
4	50	-0	3248	0	0	0	2199	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
5	50	-0	3240	0	0	0	2193	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
6	50	-0	2565	0	0	0	1726	--	--	16.08	16.08	0.10	0.03	0.02	0.16	0.00	0.00	20.9
7	50	-0	2539	0	0	0	1708	--	--	16.08	16.08	0.10	0.03	0.02	0.16	0.00	0.00	20.9
8	50	-0	2885	0	0	0	1947	--	--	16.08	16.08	0.10	0.03	0.02	0.18	0.00	0.00	20.9
9	50	-0	2859	0	0	0	1929	--	--	16.08	16.08	0.10	0.03	0.02	0.18	0.00	0.00	20.9
10	50	-0	2184	0	0	0	1461	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
11	50	-0	2176	0	0	0	1456	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
12	50	-0	3248	0	0	0	2199	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
13	50	-0	3240	0	0	0	2193	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
14	50	-0	2565	0	0	0	1726	--	--	16.08	16.08	0.10	0.03	0.02	0.16	0.00	0.00	20.9
15	50	-0	2539	0	0	0	1708	--	--	16.08	16.08	0.10	0.03	0.02	0.16	0.00	0.00	20.9
16	50	-0	2885	0	0	0	1947	--	--	16.08	16.08	0.10	0.03	0.02	0.18	0.00	0.00	20.9
17	50	-0	2859	0	0	0	1929	--	--	16.08	16.08	0.10	0.03	0.02	0.18	0.00	0.00	20.9
18	50	-0	4493	0	0	0	3020	--	--	16.08	16.08	0.00	0.05	0.04	0.28	0.00	0.00	20.9
19	50	-0	8784	0	0	0	6008	--	--	16.08	16.08	0.00	0.10	0.07	0.55	0.00	0.00	20.9
20	50	-0	6147	0	0	0	4177	--	--	16.08	16.08	0.00	0.07	0.05	0.39	0.00	0.00	20.9
37	50	-0	2049	0	0	0	1328	--	--	16.08	16.08	0.00	0.02	0.02	0.13	0.00	0.00	20.9
38	50	-0	9202	0	0	0	6308	--	--	16.08	16.08	0.00	0.11	0.08	0.58	0.00	0.00	20.9
39	50	-0	4806	0	0	0	3256	--	--	16.08	16.08	0.00	0.06	0.04	0.30	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 188 NI 1546 NF 1549 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	1226	0	0	0	-1310	--	--	16.08	16.08	0.18	0.02	0.01	0.08	0.00	0.00	20.9
2	0	-0	739	0	0	0	-790	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
3	0	-0	736	0	0	0	-787	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
4	0	-0	1149	0	0	0	-1228	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
5	0	-0	1146	0	0	0	-1225	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
6	0	-0	886	0	0	0	-947	--	--	16.08	16.08	0.29	0.02	0.01	0.06	0.00	0.00	20.9
7	0	-0	876	0	0	0	-937	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
8	0	-0	1009	0	0	0	-1078	--	--	16.08	16.08	0.29	0.02	0.01	0.06	0.00	0.00	20.9
9	0	-0	999	0	0	0	-1068	--	--	16.08	16.08	0.29	0.02	0.01	0.06	0.00	0.00	20.9
10	0	-0	739	0	0	0	-790	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9

11	0	-0	736	0	0	0	-787	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
12	0	-0	1149	0	0	0	-1228	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
13	0	-0	1146	0	0	0	-1225	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
14	0	-0	886	0	0	0	-947	--	--	16.08	16.08	0.29	0.02	0.01	0.06	0.00	0.00	20.9
15	0	-0	876	0	0	0	-937	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
16	0	-0	1009	0	0	0	-1078	--	--	16.08	16.08	0.29	0.02	0.01	0.06	0.00	0.00	20.9
17	0	-0	999	0	0	0	-1068	--	--	16.08	16.08	0.29	0.02	0.01	0.06	0.00	0.00	20.9
18	0	-0	1547	0	0	0	-1653	--	--	16.08	16.08	0.18	0.03	0.01	0.10	0.00	0.00	20.9
19	0	-0	3231	0	0	0	-3453	--	--	16.08	16.08	0.18	0.06	0.03	0.20	0.00	0.00	20.9
20	0	-0	2207	0	0	0	-2359	--	--	16.08	16.08	0.18	0.04	0.02	0.14	0.00	0.00	20.9
37	0	-0	607	0	0	0	-649	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
38	0	-0	3414	0	0	0	-3649	--	--	16.08	16.08	0.18	0.06	0.03	0.21	0.00	0.00	20.9
39	0	-0	1706	0	0	0	-1823	--	--	16.08	16.08	0.18	0.03	0.01	0.11	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	25	-0	1226	0	0	0	1617	--	--	16.08	16.08	0.00	0.03	0.01	0.08	0.00	0.00	20.9
2	25	-0	739	0	0	0	975	--	--	16.08	16.08	0.10	0.02	0.01	0.05	0.00	0.00	20.9
3	25	-0	736	0	0	0	971	--	--	16.08	16.08	0.10	0.02	0.01	0.05	0.00	0.00	20.9
4	25	-0	1149	0	0	0	1515	--	--	16.08	16.08	0.10	0.03	0.01	0.07	0.00	0.00	20.9
5	25	-0	1146	0	0	0	1511	--	--	16.08	16.08	0.10	0.03	0.01	0.07	0.00	0.00	20.9
6	25	-0	886	0	0	0	1169	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9
7	25	-0	876	0	0	0	1156	--	--	16.08	16.08	0.10	0.02	0.01	0.05	0.00	0.00	20.9
8	25	-0	1009	0	0	0	1331	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9
9	25	-0	999	0	0	0	1318	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9
10	25	-0	739	0	0	0	975	--	--	16.08	16.08	0.10	0.02	0.01	0.05	0.00	0.00	20.9
11	25	-0	736	0	0	0	971	--	--	16.08	16.08	0.10	0.02	0.01	0.05	0.00	0.00	20.9
12	25	-0	1149	0	0	0	1515	--	--	16.08	16.08	0.10	0.03	0.01	0.07	0.00	0.00	20.9
13	25	-0	1146	0	0	0	1511	--	--	16.08	16.08	0.10	0.03	0.01	0.07	0.00	0.00	20.9
14	25	-0	886	0	0	0	1169	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9
15	25	-0	876	0	0	0	1156	--	--	16.08	16.08	0.10	0.02	0.01	0.05	0.00	0.00	20.9
16	25	-0	1009	0	0	0	1331	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9
17	25	-0	999	0	0	0	1318	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9
18	25	-0	1547	0	0	0	2040	--	--	16.08	16.08	0.00	0.03	0.01	0.10	0.00	0.00	20.9
19	25	-0	3231	0	0	0	4261	--	--	16.08	16.08	0.00	0.07	0.03	0.20	0.00	0.00	20.9
20	25	-0	2207	0	0	0	2910	--	--	16.08	16.08	0.00	0.05	0.02	0.14	0.00	0.00	20.9
37	25	-0	607	0	0	0	801	--	--	16.08	16.08	0.00	0.01	0.01	0.04	0.00	0.00	20.9
38	25	-0	3414	0	0	0	4502	--	--	16.08	16.08	0.00	0.08	0.03	0.21	0.00	0.00	20.9
39	25	-0	1706	0	0	0	2250	--	--	16.08	16.08	0.00	0.04	0.01	0.11	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	50	-0	1226	0	0	0	613	--	--	16.08	16.08	0.00	0.01	0.01	0.08	0.00	0.00	20.9
2	50	-0	739	0	0	0	370	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
3	50	-0	736	0	0	0	368	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
4	50	-0	1149	0	0	0	575	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
5	50	-0	1146	0	0	0	573	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
6	50	-0	886	0	0	0	443	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
7	50	-0	876	0	0	0	438	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
8	50	-0	1009	0	0	0	505	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
9	50	-0	999	0	0	0	500	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
10	50	-0	739	0	0	0	370	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
11	50	-0	736	0	0	0	368	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
12	50	-0	1149	0	0	0	575	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
13	50	-0	1146	0	0	0	573	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
14	50	-0	886	0	0	0	443	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
15	50	-0	876	0	0	0	438	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
16	50	-0	1009	0	0	0	505	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
17	50	-0	999	0	0	0	500	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
18	50	-0	1547	0	0	0	774	--	--	16.08	16.08	0.00	0.01	0.01	0.10	0.00	0.00	20.9
19	50	-0	3231	0	0	0	1616	--	--	16.08	16.08	0.00	0.03	0.03	0.20	0.00	0.00	20.9
20	50	-0	2207	0	0	0	1103	--	--	16.08	16.08	0.00	0.02	0.02	0.14	0.00	0.00	20.9
37	50	-0	607	0	0	0	304	--	--	16.08	16.08	0.00	0.01	0.01	0.04	0.00	0.00	20.9
38	50	-0	3414	0	0	0	1707	--	--	16.08	16.08	0.00	0.03	0.03	0.21	0.00	0.00	20.9
39	50	-0	1706	0	0	0	853	--	--	16.08	16.08	0.00	0.01	0.01	0.11	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 189 NI 1668 NF 1676 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-724	0	0	0	145	--	--	16.08	16.08	0.00	0.00	0.01	0.05	0.00	0.00	20.9
2	0	-0	-597	0	0	0	119	--	--	16.08	16.08	0.10	0.00	0.00	0.04	0.00	0.00	20.9
3	0	-0	-596	0	0	0	119	--	--	16.08	16.08	0.10	0.00	0.00	0.04	0.00	0.00	20.9
4	0	-0	-518	0	0	0	104	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
5	0	-0	-517	0	0	0	103	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
6	0	-0	-571	0	0	0	114	--	--	16.08	16.08	0.10	0.00	0.00	0.04	0.00	0.00	20.9
7	0	-0	-566	0	0	0	113	--	--	16.08	16.08	0.10	0.00	0.00	0.04	0.00	0.00	20.9
8	0	-0	-547	0	0	0	110	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
9	0	-0	-543	0	0	0	109	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
10	0	-0	-597	0	0	0	119	--	--	16.08	16.08	0.10	0.00	0.00	0.04	0.00	0.00	20.9
11	0	-0	-596	0	0	0	119	--	--	16.08	16.08	0.10	0.00	0.00	0.04	0.00	0.00	20.9
12	0	-0	-518	0	0	0	104	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
13	0	-0	-517	0	0	0	103	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
14	0	-0	-571	0	0	0	114	--	--	16.08	16.08	0.10	0.00	0.00	0.04	0.00	0.00	20.9
15	0	-0	-566	0	0	0	113	--	--	16.08	16.08	0.10	0.00	0.00	0.04	0.00	0.00	20.9
16	0	-0	-547	0	0	0	110	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
17	0	-0	-543	0	0	0	109	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
18	0	-0	-1267	0	0	0	254	--	--	16.08	16.08	0.00	0.00	0.01	0.08	0.00	0.00	20.9
19	0	-0	-954	0	0	0	191	--	--	16.08	16.08	0.00	0.00	0.01	0.06	0.00	0.00	20.9
20	0	-0	-1050	0	0	0	210	--	--	16.08	16.08	0.00	0.00	0.01	0.07	0.00	0.00	20.9
37	0	-0	-1246	0	0	0	249	--	--	16.08	16.08	0.00	0.00	0.01	0.08	0.00	0.00	20.9
38	0	-0	-724	0	0	0	145	--	--	16.08	16.08	0.00	0.00	0.01	0.05	0.00	0.00	20.9
39	0	-0	-883	0	0	0	177	--	--	16.08	16.08	0.00	0.00	0.01	0.06	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	10	-0	-724	0	0	0	145	--	--	16.08	16.08	0.00	0.00	0.01	0.05	0.00	0.00	20.9
2	10	-0	-597	0	0	0	119	--	--	16.08	16.08	0.10	0.00	0.00	0.04	0.00	0.00	20.9
3	10	-0	-596	0	0	0	119	--	--	16.08	16.08	0.10	0.00	0.00	0.04	0.00	0.00	20.9
4	10	-0	-518	0	0	0	104	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
5	10	-0	-517	0	0	0	103	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
6	10	-0	-571	0	0	0	114	--	--	16.08	16.08	0.10	0.00	0.00	0.04	0.00	0.00	20.9

7	10	-0	-566	0	0	0	113	--	--	16.08	16.08	0.10	0.00	0.00	0.04	0.00	0.00	20.9
8	10	-0	-547	0	0	0	110	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
9	10	-0	-543	0	0	0	109	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
10	10	-0	-597	0	0	0	119	--	--	16.08	16.08	0.10	0.00	0.00	0.04	0.00	0.00	20.9
11	10	-0	-596	0	0	0	119	--	--	16.08	16.08	0.10	0.00	0.00	0.04	0.00	0.00	20.9
12	10	-0	-518	0	0	0	104	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
13	10	-0	-517	0	0	0	103	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
14	10	-0	-571	0	0	0	114	--	--	16.08	16.08	0.10	0.00	0.00	0.04	0.00	0.00	20.9
15	10	-0	-566	0	0	0	113	--	--	16.08	16.08	0.10	0.00	0.00	0.04	0.00	0.00	20.9
16	10	-0	-547	0	0	0	110	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
17	10	-0	-543	0	0	0	109	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
18	10	-0	-1267	0	0	0	254	--	--	16.08	16.08	0.00	0.00	0.01	0.08	0.00	0.00	20.9
19	10	-0	-954	0	0	0	191	--	--	16.08	16.08	0.00	0.00	0.01	0.06	0.00	0.00	20.9
20	10	-0	-1050	0	0	0	210	--	--	16.08	16.08	0.00	0.00	0.01	0.07	0.00	0.00	20.9
37	10	-0	-1246	0	0	0	249	--	--	16.08	16.08	0.00	0.00	0.01	0.08	0.00	0.00	20.9
38	10	-0	-724	0	0	0	145	--	--	16.08	16.08	0.00	0.00	0.01	0.05	0.00	0.00	20.9
39	10	-0	-883	0	0	0	177	--	--	16.08	16.08	0.00	0.00	0.01	0.06	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	20	-0	-724	0	0	0	-774	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9
2	20	-0	-597	0	0	0	-638	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
3	20	-0	-596	0	0	0	-636	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
4	20	-0	-518	0	0	0	-554	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
5	20	-0	-517	0	0	0	-552	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
6	20	-0	-571	0	0	0	-610	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
7	20	-0	-566	0	0	0	-605	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
8	20	-0	-547	0	0	0	-585	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
9	20	-0	-543	0	0	0	-580	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
10	20	-0	-597	0	0	0	-638	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
11	20	-0	-596	0	0	0	-636	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
12	20	-0	-518	0	0	0	-554	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
13	20	-0	-517	0	0	0	-552	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
14	20	-0	-571	0	0	0	-610	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
15	20	-0	-566	0	0	0	-605	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
16	20	-0	-547	0	0	0	-585	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
17	20	-0	-543	0	0	0	-580	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
18	20	-0	-1267	0	0	0	-1354	--	--	16.08	16.08	0.18	0.02	0.01	0.08	0.00	0.00	20.9
19	20	-0	-954	0	0	0	-1020	--	--	16.08	16.08	0.18	0.02	0.01	0.06	0.00	0.00	20.9
20	20	-0	-1050	0	0	0	-1122	--	--	16.08	16.08	0.18	0.02	0.01	0.07	0.00	0.00	20.9
37	20	-0	-1246	0	0	0	-1332	--	--	16.08	16.08	0.18	0.02	0.01	0.08	0.00	0.00	20.9
38	20	-0	-724	0	0	0	-774	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9
39	20	-0	-883	0	0	0	-944	--	--	16.08	16.08	0.18	0.02	0.01	0.06	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 190 NI 1670 NF 1668 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm

1	0	-0	-9019	0	0	0	3030	--	--	16.08	16.08	0.00	0.05	0.07	0.57	0.00	0.00	20.9
2	0	-0	-6931	0	0	0	2437	--	--	16.08	16.08	0.10	0.04	0.06	0.43	0.00	0.00	20.9
3	0	-0	-6940	0	0	0	2413	--	--	16.08	16.08	0.10	0.04	0.06	0.44	0.00	0.00	20.9
4	0	-0	-6936	0	0	0	2247	--	--	16.08	16.08	0.10	0.04	0.06	0.44	0.00	0.00	20.9
5	0	-0	-6944	0	0	0	2224	--	--	16.08	16.08	0.10	0.04	0.06	0.44	0.00	0.00	20.9
6	0	-0	-6923	0	0	0	2399	--	--	16.08	16.08	0.10	0.04	0.06	0.43	0.00	0.00	20.9
7	0	-0	-6951	0	0	0	2319	--	--	16.08	16.08	0.10	0.04	0.06	0.44	0.00	0.00	20.9
8	0	-0	-6924	0	0	0	2342	--	--	16.08	16.08	0.10	0.04	0.06	0.43	0.00	0.00	20.9
9	0	-0	-6953	0	0	0	2262	--	--	16.08	16.08	0.10	0.04	0.06	0.44	0.00	0.00	20.9
10	0	-0	-6931	0	0	0	2437	--	--	16.08	16.08	0.10	0.04	0.06	0.43	0.00	0.00	20.9
11	0	-0	-6940	0	0	0	2413	--	--	16.08	16.08	0.10	0.04	0.06	0.44	0.00	0.00	20.9
12	0	-0	-6936	0	0	0	2247	--	--	16.08	16.08	0.10	0.04	0.06	0.44	0.00	0.00	20.9
13	0	-0	-6944	0	0	0	2224	--	--	16.08	16.08	0.10	0.04	0.06	0.44	0.00	0.00	20.9
14	0	-0	-6923	0	0	0	2399	--	--	16.08	16.08	0.10	0.04	0.06	0.43	0.00	0.00	20.9
15	0	-0	-6951	0	0	0	2319	--	--	16.08	16.08	0.10	0.04	0.06	0.44	0.00	0.00	20.9
16	0	-0	-6924	0	0	0	2342	--	--	16.08	16.08	0.10	0.04	0.06	0.43	0.00	0.00	20.9
17	0	-0	-6953	0	0	0	2262	--	--	16.08	16.08	0.10	0.04	0.06	0.44	0.00	0.00	20.9
18	0	-0	-11130	0	0	0	4775	--	--	16.08	16.08	0.00	0.08	0.09	0.70	0.00	0.00	20.9
19	0	-0	-11790	0	0	0	4161	--	--	16.08	16.08	0.00	0.07	0.10	0.74	0.00	0.00	20.9
20	0	-0	-11100	0	0	0	4198	--	--	16.08	16.08	0.00	0.07	0.09	0.70	0.00	0.00	20.9
37	0	-0	-10120	0	0	0	4514	--	--	16.08	16.08	0.00	0.08	0.08	0.63	0.00	0.00	20.9
38	0	-0	-11230	0	0	0	3491	--	--	16.08	16.08	0.00	0.06	0.09	0.70	0.00	0.00	20.9
39	0	-0	-10080	0	0	0	3551	--	--	16.08	16.08	0.00	0.06	0.08	0.63	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	10	-0	-9019	0	0	0	3030	--	--	16.08	16.08	0.00	0.05	0.07	0.57	0.00	0.00	20.9
2	10	-0	-6931	0	0	0	2437	--	--	16.08	16.08	0.10	0.04	0.06	0.43	0.00	0.00	20.9
3	10	-0	-6940	0	0	0	2413	--	--	16.08	16.08	0.10	0.04	0.06	0.44	0.00	0.00	20.9
4	10	-0	-6936	0	0	0	2247	--	--	16.08	16.08	0.10	0.04	0.06	0.44	0.00	0.00	20.9
5	10	-0	-6944	0	0	0	2224	--	--	16.08	16.08	0.10	0.04	0.06	0.44	0.00	0.00	20.9
6	10	-0	-6923	0	0	0	2399	--	--	16.08	16.08	0.10	0.04	0.06	0.43	0.00	0.00	20.9
7	10	-0	-6951	0	0	0	2319	--	--	16.08	16.08	0.10	0.04	0.06	0.44	0.00	0.00	20.9
8	10	-0	-6924	0	0	0	2342	--	--	16.08	16.08	0.10	0.04	0.06	0.43	0.00	0.00	20.9
9	10	-0	-6953	0	0	0	2262	--	--	16.08	16.08	0.10	0.04	0.06	0.44	0.00	0.00	20.9
10	10	-0	-6931	0	0	0	2437	--	--	16.08	16.08	0.10	0.04	0.06	0.43	0.00	0.00	20.9
11	10	-0	-6940	0	0	0	2413	--	--	16.08	16.08	0.10	0.04	0.06	0.44	0.00	0.00	20.9
12	10	-0	-6936	0	0	0	2247	--	--	16.08	16.08	0.10	0.04	0.06	0.44	0.00	0.00	20.9
13	10	-0	-6944	0	0	0	2224	--	--	16.08	16.08	0.10	0.04	0.06	0.44	0.00	0.00	20.9
14	10	-0	-6923	0	0	0	2399	--	--	16.08	16.08	0.10	0.04	0.06	0.43	0.00	0.00	20.9
15	10	-0	-6951	0	0	0	2319	--	--	16.08	16.08	0.10	0.04	0.06	0.44	0.00	0.00	20.9
16	10	-0	-6924	0	0	0	2342	--	--	16.08	16.08	0.10	0.04	0.06	0.43	0.00	0.00	20.9
17	10	-0	-6953	0	0	0	2262	--	--	16.08	16.08	0.10	0.04	0.06	0.44	0.00	0.00	20.9
18	10	-0	-11130	0	0	0	4775	--	--	16.08	16.08	0.00	0.08	0.09	0.70	0.00	0.00	20.9
19	10	-0	-11790	0	0	0	4161	--	--	16.08	16.08	0.00	0.07	0.10	0.74	0.00	0.00	20.9
20	10	-0	-11100	0	0	0	4198	--	--	16.08	16.08	0.00	0.07	0.09	0.70	0.00	0.00	20.9
37	10	-0	-10120	0	0	0	4514	--	--	16.08	16.08	0.00	0.08	0.08	0.63	0.00	0.00	20.9
38	10	-0	-11230	0	0	0	3491	--	--	16.08	16.08	0.00	0.06	0.09	0.70	0.00	0.00	20.9
39	10	-0	-10080	0	0	0	3551	--	--	16.08	16.08	0.00	0.06	0.08	0.63	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	20	-0	-9019	0	0	0	1226	--	--	16.08	16.08	0.00	0.02	0.07	0.57	0.00	0.00	20.9
2	20	-0	-6931	0	0	0	1051	--	--	16.08	16.08	0.10	0.02	0.06	0.43	0.00	0.00	20.9

3	20	-0	-6940	0	0	0	1026	--	--	16.08	16.08	0.10	0.02	0.06	0.44	0.00	0.00	20.9
4	20	-0	-6936	0	0	0	860	--	--	16.08	16.08	0.10	0.02	0.06	0.44	0.00	0.00	20.9
5	20	-0	-6944	0	0	0	835	--	--	16.08	16.08	0.10	0.01	0.06	0.44	0.00	0.00	20.9
6	20	-0	-6923	0	0	0	1014	--	--	16.08	16.08	0.10	0.02	0.06	0.43	0.00	0.00	20.9
7	20	-0	-6951	0	0	0	929	--	--	16.08	16.08	0.10	0.02	0.06	0.44	0.00	0.00	20.9
8	20	-0	-6924	0	0	0	957	--	--	16.08	16.08	0.10	0.02	0.06	0.43	0.00	0.00	20.9
9	20	-0	-6953	0	0	0	872	--	--	16.08	16.08	0.10	0.02	0.06	0.44	0.00	0.00	20.9
10	20	-0	-6931	0	0	0	1051	--	--	16.08	16.08	0.10	0.02	0.06	0.43	0.00	0.00	20.9
11	20	-0	-6940	0	0	0	1026	--	--	16.08	16.08	0.10	0.02	0.06	0.44	0.00	0.00	20.9
12	20	-0	-6936	0	0	0	860	--	--	16.08	16.08	0.10	0.02	0.06	0.44	0.00	0.00	20.9
13	20	-0	-6944	0	0	0	835	--	--	16.08	16.08	0.10	0.01	0.06	0.44	0.00	0.00	20.9
14	20	-0	-6923	0	0	0	1014	--	--	16.08	16.08	0.10	0.02	0.06	0.43	0.00	0.00	20.9
15	20	-0	-6951	0	0	0	929	--	--	16.08	16.08	0.10	0.02	0.06	0.44	0.00	0.00	20.9
16	20	-0	-6924	0	0	0	957	--	--	16.08	16.08	0.10	0.02	0.06	0.43	0.00	0.00	20.9
17	20	-0	-6953	0	0	0	872	--	--	16.08	16.08	0.10	0.02	0.06	0.44	0.00	0.00	20.9
18	20	-0	-11130	0	0	0	2550	--	--	16.08	16.08	0.00	0.04	0.09	0.70	0.00	0.00	20.9
19	20	-0	-11790	0	0	0	1802	--	--	16.08	16.08	0.00	0.03	0.10	0.74	0.00	0.00	20.9
20	20	-0	-11100	0	0	0	1978	--	--	16.08	16.08	0.00	0.03	0.09	0.70	0.00	0.00	20.9
37	20	-0	-10120	0	0	0	2490	--	--	16.08	16.08	0.00	0.04	0.08	0.63	0.00	0.00	20.9
38	20	-0	-11230	0	0	0	1244	--	--	16.08	16.08	0.00	0.02	0.09	0.70	0.00	0.00	20.9
39	20	-0	-10080	0	0	0	1536	--	--	16.08	16.08	0.00	0.03	0.08	0.63	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 191 NI 1671 NF 1670 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-4178	0	0	0	-4701	--	--	16.08	16.08	0.18	0.08	0.03	0.26	0.00	0.00	20.9
2	0	-0	-4373	0	0	0	-4751	--	--	16.08	16.08	0.29	0.08	0.04	0.27	0.00	0.00	20.9
3	0	-0	-4338	0	0	0	-4717	--	--	16.08	16.08	0.29	0.08	0.04	0.27	0.00	0.00	20.9
4	0	-0	-2089	0	0	0	-2515	--	--	16.08	16.08	0.29	0.04	0.02	0.13	0.00	0.00	20.9
5	0	-0	-2055	0	0	0	-2481	--	--	16.08	16.08	0.29	0.04	0.02	0.13	0.00	0.00	20.9
6	0	-0	-3613	0	0	0	-4007	--	--	16.08	16.08	0.29	0.07	0.03	0.23	0.00	0.00	20.9
7	0	-0	-3499	0	0	0	-3895	--	--	16.08	16.08	0.29	0.07	0.03	0.22	0.00	0.00	20.9
8	0	-0	-2928	0	0	0	-3337	--	--	16.08	16.08	0.29	0.06	0.02	0.18	0.00	0.00	20.9
9	0	-0	-2814	0	0	0	-3224	--	--	16.08	16.08	0.29	0.06	0.02	0.18	0.00	0.00	20.9
10	0	-0	-4373	0	0	0	-4751	--	--	16.08	16.08	0.29	0.08	0.04	0.27	0.00	0.00	20.9
11	0	-0	-4338	0	0	0	-4717	--	--	16.08	16.08	0.29	0.08	0.04	0.27	0.00	0.00	20.9
12	0	-0	-2089	0	0	0	-2515	--	--	16.08	16.08	0.29	0.04	0.02	0.13	0.00	0.00	20.9
13	0	-0	-2055	0	0	0	-2481	--	--	16.08	16.08	0.29	0.04	0.02	0.13	0.00	0.00	20.9
14	0	-0	-3613	0	0	0	-4007	--	--	16.08	16.08	0.29	0.07	0.03	0.23	0.00	0.00	20.9
15	0	-0	-3499	0	0	0	-3895	--	--	16.08	16.08	0.29	0.07	0.03	0.22	0.00	0.00	20.9
16	0	-0	-2928	0	0	0	-3337	--	--	16.08	16.08	0.29	0.06	0.02	0.18	0.00	0.00	20.9
17	0	-0	-2814	0	0	0	-3224	--	--	16.08	16.08	0.29	0.06	0.02	0.18	0.00	0.00	20.9
18	0	-0	-16620	0	0	0	-17000	--	--	16.08	16.08	0.18	0.28	0.14	1.04	1.95	0.00	20.9
19	0	-0	-5673	0	0	0	-6353	--	--	16.08	16.08	0.18	0.11	0.05	0.36	0.00	0.00	20.9
20	0	-0	-10040	0	0	0	-10570	--	--	16.08	16.08	0.18	0.18	0.08	0.63	0.00	0.00	20.9
37	0	-0	-17990	0	0	0	-18270	--	--	16.08	16.08	0.18	0.30	0.15	1.13	2.11	0.00	20.9
38	0	-0	258	0	0	0	-649	--	--	16.08	16.08	0.18	0.01	0.00	0.02	0.00	0.00	20.9
39	0	-0	-7027	0	0	0	-7554	--	--	16.08	16.08	0.18	0.13	0.06	0.44	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	25	-0	-4178	0	0	0	-4701	--	--	16.08	16.08	0.18	0.08	0.03	0.26	0.00	0.00	20.9
2	25	-0	-4373	0	0	0	-4751	--	--	16.08	16.08	0.29	0.08	0.04	0.27	0.00	0.00	20.9
3	25	-0	-4338	0	0	0	-4717	--	--	16.08	16.08	0.29	0.08	0.04	0.27	0.00	0.00	20.9
4	25	-0	-2089	0	0	0	-2515	--	--	16.08	16.08	0.29	0.04	0.02	0.13	0.00	0.00	20.9
5	25	-0	-2055	0	0	0	-2481	--	--	16.08	16.08	0.29	0.04	0.02	0.13	0.00	0.00	20.9
6	25	-0	-3613	0	0	0	-4007	--	--	16.08	16.08	0.29	0.07	0.03	0.23	0.00	0.00	20.9
7	25	-0	-3499	0	0	0	-3895	--	--	16.08	16.08	0.29	0.07	0.03	0.22	0.00	0.00	20.9
8	25	-0	-2928	0	0	0	-3337	--	--	16.08	16.08	0.29	0.06	0.02	0.18	0.00	0.00	20.9
9	25	-0	-2814	0	0	0	-3224	--	--	16.08	16.08	0.29	0.06	0.02	0.18	0.00	0.00	20.9
10	25	-0	-4373	0	0	0	-4751	--	--	16.08	16.08	0.29	0.08	0.04	0.27	0.00	0.00	20.9
11	25	-0	-4338	0	0	0	-4717	--	--	16.08	16.08	0.29	0.08	0.04	0.27	0.00	0.00	20.9
12	25	-0	-2089	0	0	0	-2515	--	--	16.08	16.08	0.29	0.04	0.02	0.13	0.00	0.00	20.9
13	25	-0	-2055	0	0	0	-2481	--	--	16.08	16.08	0.29	0.04	0.02	0.13	0.00	0.00	20.9
14	25	-0	-3613	0	0	0	-4007	--	--	16.08	16.08	0.29	0.07	0.03	0.23	0.00	0.00	20.9
15	25	-0	-3499	0	0	0	-3895	--	--	16.08	16.08	0.29	0.07	0.03	0.22	0.00	0.00	20.9
16	25	-0	-2928	0	0	0	-3337	--	--	16.08	16.08	0.29	0.06	0.02	0.18	0.00	0.00	20.9
17	25	-0	-2814	0	0	0	-3224	--	--	16.08	16.08	0.29	0.06	0.02	0.18	0.00	0.00	20.9
18	25	-0	-16620	0	0	0	-17000	--	--	16.08	16.08	0.18	0.28	0.14	1.04	1.95	0.00	20.9
19	25	-0	-5673	0	0	0	-6353	--	--	16.08	16.08	0.18	0.11	0.05	0.36	0.00	0.00	20.9
20	25	-0	-10040	0	0	0	-10570	--	--	16.08	16.08	0.18	0.18	0.08	0.63	0.00	0.00	20.9
37	25	-0	-17990	0	0	0	-18270	--	--	16.08	16.08	0.18	0.30	0.15	1.13	2.11	0.00	20.9
38	25	-0	258	0	0	0	-649	--	--	16.08	16.08	0.18	0.01	0.00	0.02	0.00	0.00	20.9
39	25	-0	-7027	0	0	0	-7554	--	--	16.08	16.08	0.18	0.13	0.06	0.44	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	50	-0	-4178	0	0	0	-4701	--	--	16.08	16.08	0.18	0.08	0.03	0.26	0.00	0.00	20.9
2	50	-0	-4373	0	0	0	-4751	--	--	16.08	16.08	0.29	0.08	0.04	0.27	0.00	0.00	20.9
3	50	-0	-4338	0	0	0	-4717	--	--	16.08	16.08	0.29	0.08	0.04	0.27	0.00	0.00	20.9
4	50	-0	-2089	0	0	0	-2515	--	--	16.08	16.08	0.29	0.04	0.02	0.13	0.00	0.00	20.9
5	50	-0	-2055	0	0	0	-2481	--	--	16.08	16.08	0.29	0.04	0.02	0.13	0.00	0.00	20.9
6	50	-0	-3613	0	0	0	-4007	--	--	16.08	16.08	0.29	0.07	0.03	0.23	0.00	0.00	20.9
7	50	-0	-3499	0	0	0	-3895	--	--	16.08	16.08	0.29	0.07	0.03	0.22	0.00	0.00	20.9
8	50	-0	-2928	0	0	0	-3337	--	--	16.08	16.08	0.29	0.06	0.02	0.18	0.00	0.00	20.9
9	50	-0	-2814	0	0	0	-3224	--	--	16.08	16.08	0.29	0.06	0.02	0.18	0.00	0.00	20.9
10	50	-0	-4373	0	0	0	-4751	--	--	16.08	16.08	0.29	0.08	0.04	0.27	0.00	0.00	20.9
11	50	-0	-4338	0	0	0	-4717	--	--	16.08	16.08	0.29	0.08	0.04	0.27	0.00	0.00	20.9
12	50	-0	-2089	0	0	0	-2515	--	--	16.08	16.08	0.29	0.04	0.02	0.13	0.00	0.00	20.9
13	50	-0	-2055	0	0	0	-2481	--	--	16.08	16.08	0.29	0.04	0.02	0.13	0.00	0.00	20.9
14	50	-0	-3613	0	0	0	-4007	--	--	16.08	16.08	0.29	0.07	0.03	0.23	0.00	0.00	20.9
15	50	-0	-3499	0	0	0	-3895	--	--	16.08	16.08	0.29	0.07	0.03	0.22	0.00	0.00	20.9
16	50	-0	-2928	0	0	0	-3337	--	--	16.08	16.08	0.29	0.06	0.02	0.18	0.00	0.00	20.9
17	50	-0	-2814	0	0	0	-3224	--	--	16.08	16.08	0.29	0.06	0.02	0.18	0.00	0.00	20.9
18	50	-0	-16620	0	0	0	-17000	--	--	16.08	16.08	0.18	0.28	0.14	1.04	1.95	0.00	20.9
19	50	-0	-5673	0	0	0	-6353	--	--	16.08	16.08	0.18	0.11	0.05	0.36	0.00	0.00	20.9
20	50	-0	-10040	0	0	0	-10570	--	--	16.08	16.08	0.18	0.18	0.08	0.63	0.00	0.00	20.9
37	50	-0	-17990	0	0	0	-18270	--	--	16.08	16.08	0.18	0.30	0.15	1.13	2.11	0.00	20.9
38	50	-0	258	0	0	0	-649	--	--	16.08	16.08	0.18	0.01	0.00	0.02	0.00	0.00	20.9
39	50	-0	-7027	0	0	0	-7554	--	--	16.08	16.08	0.18	0.13	0.06	0.44	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 192 NI 1673 NF 1671 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-3884	0	0	0	-2612	--	--	16.08	16.08	0.18	0.04	0.03	0.24	0.00	0.00	20.9
2	0	-0	-3839	0	0	0	-2564	--	--	16.08	16.08	0.29	0.04	0.03	0.24	0.00	0.00	20.9
3	0	-0	-3814	0	0	0	-2548	--	--	16.08	16.08	0.29	0.04	0.03	0.24	0.00	0.00	20.9
4	0	-0	-2162	0	0	0	-1471	--	--	16.08	16.08	0.29	0.03	0.02	0.14	0.00	0.00	20.9
5	0	-0	-2136	0	0	0	-1454	--	--	16.08	16.08	0.29	0.03	0.02	0.13	0.00	0.00	20.9
6	0	-0	-3282	0	0	0	-2201	--	--	16.08	16.08	0.29	0.04	0.03	0.21	0.00	0.00	20.9
7	0	-0	-3197	0	0	0	-2145	--	--	16.08	16.08	0.29	0.04	0.03	0.20	0.00	0.00	20.9
8	0	-0	-2779	0	0	0	-1873	--	--	16.08	16.08	0.29	0.03	0.02	0.17	0.00	0.00	20.9
9	0	-0	-2694	0	0	0	-1817	--	--	16.08	16.08	0.29	0.03	0.02	0.17	0.00	0.00	20.9
10	0	-0	-3839	0	0	0	-2564	--	--	16.08	16.08	0.29	0.04	0.03	0.24	0.00	0.00	20.9
11	0	-0	-3814	0	0	0	-2548	--	--	16.08	16.08	0.29	0.04	0.03	0.24	0.00	0.00	20.9
12	0	-0	-2162	0	0	0	-1471	--	--	16.08	16.08	0.29	0.03	0.02	0.14	0.00	0.00	20.9
13	0	-0	-2136	0	0	0	-1454	--	--	16.08	16.08	0.29	0.03	0.02	0.13	0.00	0.00	20.9
14	0	-0	-3282	0	0	0	-2201	--	--	16.08	16.08	0.29	0.04	0.03	0.21	0.00	0.00	20.9
15	0	-0	-3197	0	0	0	-2145	--	--	16.08	16.08	0.29	0.04	0.03	0.20	0.00	0.00	20.9
16	0	-0	-2779	0	0	0	-1873	--	--	16.08	16.08	0.29	0.03	0.02	0.17	0.00	0.00	20.9
17	0	-0	-2694	0	0	0	-1817	--	--	16.08	16.08	0.29	0.03	0.02	0.17	0.00	0.00	20.9
18	0	-0	-13180	0	0	0	-8691	--	--	16.08	16.08	0.18	0.14	0.11	0.83	0.00	0.00	20.9
19	0	-0	-5234	0	0	0	-3517	--	--	16.08	16.08	0.18	0.06	0.04	0.33	0.00	0.00	20.9
20	0	-0	-8367	0	0	0	-5552	--	--	16.08	16.08	0.18	0.09	0.07	0.52	0.00	0.00	20.9
37	0	-0	-14090	0	0	0	-9273	--	--	16.08	16.08	0.18	0.15	0.12	0.88	0.00	0.00	20.9
38	0	-0	-842	0	0	0	-649	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9
39	0	-0	-6063	0	0	0	-4041	--	--	16.08	16.08	0.18	0.07	0.05	0.38	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	25	-0	-3884	0	0	0	-2612	--	--	16.08	16.08	0.18	0.04	0.03	0.24	0.00	0.00	20.9
2	25	-0	-3839	0	0	0	-2564	--	--	16.08	16.08	0.29	0.04	0.03	0.24	0.00	0.00	20.9
3	25	-0	-3814	0	0	0	-2548	--	--	16.08	16.08	0.29	0.04	0.03	0.24	0.00	0.00	20.9
4	25	-0	-2162	0	0	0	-1471	--	--	16.08	16.08	0.29	0.03	0.02	0.14	0.00	0.00	20.9
5	25	-0	-2136	0	0	0	-1454	--	--	16.08	16.08	0.29	0.03	0.02	0.13	0.00	0.00	20.9
6	25	-0	-3282	0	0	0	-2201	--	--	16.08	16.08	0.29	0.04	0.03	0.21	0.00	0.00	20.9
7	25	-0	-3197	0	0	0	-2145	--	--	16.08	16.08	0.29	0.04	0.03	0.20	0.00	0.00	20.9
8	25	-0	-2779	0	0	0	-1873	--	--	16.08	16.08	0.29	0.03	0.02	0.17	0.00	0.00	20.9
9	25	-0	-2694	0	0	0	-1817	--	--	16.08	16.08	0.29	0.03	0.02	0.17	0.00	0.00	20.9
10	25	-0	-3839	0	0	0	-2564	--	--	16.08	16.08	0.29	0.04	0.03	0.24	0.00	0.00	20.9
11	25	-0	-3814	0	0	0	-2548	--	--	16.08	16.08	0.29	0.04	0.03	0.24	0.00	0.00	20.9
12	25	-0	-2162	0	0	0	-1471	--	--	16.08	16.08	0.29	0.03	0.02	0.14	0.00	0.00	20.9
13	25	-0	-2136	0	0	0	-1454	--	--	16.08	16.08	0.29	0.03	0.02	0.13	0.00	0.00	20.9
14	25	-0	-3282	0	0	0	-2201	--	--	16.08	16.08	0.29	0.04	0.03	0.21	0.00	0.00	20.9
15	25	-0	-3197	0	0	0	-2145	--	--	16.08	16.08	0.29	0.04	0.03	0.20	0.00	0.00	20.9
16	25	-0	-2779	0	0	0	-1873	--	--	16.08	16.08	0.29	0.03	0.02	0.17	0.00	0.00	20.9
17	25	-0	-2694	0	0	0	-1817	--	--	16.08	16.08	0.29	0.03	0.02	0.17	0.00	0.00	20.9
18	25	-0	-13180	0	0	0	-8691	--	--	16.08	16.08	0.18	0.14	0.11	0.83	0.00	0.00	20.9
19	25	-0	-5234	0	0	0	-3517	--	--	16.08	16.08	0.18	0.06	0.04	0.33	0.00	0.00	20.9
20	25	-0	-8367	0	0	0	-5552	--	--	16.08	16.08	0.18	0.09	0.07	0.52	0.00	0.00	20.9
37	25	-0	-14090	0	0	0	-9273	--	--	16.08	16.08	0.18	0.15	0.12	0.88	0.00	0.00	20.9
38	25	-0	-842	0	0	0	-649	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9
39	25	-0	-6063	0	0	0	-4041	--	--	16.08	16.08	0.18	0.07	0.05	0.38	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	50	-0	-3884	0	0	0	-2612	--	--	16.08	16.08	0.18	0.04	0.03	0.24	0.00	0.00	20.9
2	50	-0	-3839	0	0	0	-2564	--	--	16.08	16.08	0.29	0.04	0.03	0.24	0.00	0.00	20.9
3	50	-0	-3814	0	0	0	-2548	--	--	16.08	16.08	0.29	0.04	0.03	0.24	0.00	0.00	20.9
4	50	-0	-2162	0	0	0	-1471	--	--	16.08	16.08	0.29	0.03	0.02	0.14	0.00	0.00	20.9
5	50	-0	-2136	0	0	0	-1454	--	--	16.08	16.08	0.29	0.03	0.02	0.13	0.00	0.00	20.9
6	50	-0	-3282	0	0	0	-2201	--	--	16.08	16.08	0.29	0.04	0.03	0.21	0.00	0.00	20.9
7	50	-0	-3197	0	0	0	-2145	--	--	16.08	16.08	0.29	0.04	0.03	0.20	0.00	0.00	20.9
8	50	-0	-2779	0	0	0	-1873	--	--	16.08	16.08	0.29	0.03	0.02	0.17	0.00	0.00	20.9
9	50	-0	-2694	0	0	0	-1817	--	--	16.08	16.08	0.29	0.03	0.02	0.17	0.00	0.00	20.9
10	50	-0	-3839	0	0	0	-2564	--	--	16.08	16.08	0.29	0.04	0.03	0.24	0.00	0.00	20.9
11	50	-0	-3814	0	0	0	-2548	--	--	16.08	16.08	0.29	0.04	0.03	0.24	0.00	0.00	20.9
12	50	-0	-2162	0	0	0	-1471	--	--	16.08	16.08	0.29	0.03	0.02	0.14	0.00	0.00	20.9
13	50	-0	-2136	0	0	0	-1454	--	--	16.08	16.08	0.29	0.03	0.02	0.13	0.00	0.00	20.9
14	50	-0	-3282	0	0	0	-2201	--	--	16.08	16.08	0.29	0.04	0.03	0.21	0.00	0.00	20.9
15	50	-0	-3197	0	0	0	-2145	--	--	16.08	16.08	0.29	0.04	0.03	0.20	0.00	0.00	20.9
16	50	-0	-2779	0	0	0	-1873	--	--	16.08	16.08	0.29	0.03	0.02	0.17	0.00	0.00	20.9
17	50	-0	-2694	0	0	0	-1817	--	--	16.08	16.08	0.29	0.03	0.02	0.17	0.00	0.00	20.9
18	50	-0	-13180	0	0	0	-8691	--	--	16.08	16.08	0.18	0.14	0.11	0.83	0.00	0.00	20.9
19	50	-0	-5234	0	0	0	-3517	--	--	16.08	16.08	0.18	0.06	0.04	0.33	0.00	0.00	20.9
20	50	-0	-8367	0	0	0	-5552	--	--	16.08	16.08	0.18	0.09	0.07	0.52	0.00	0.00	20.9
37	50	-0	-14090	0	0	0	-9273	--	--	16.08	16.08	0.18	0.15	0.12	0.88	0.00	0.00	20.9
38	50	-0	-842	0	0	0	-649	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9
39	50	-0	-6063	0	0	0	-4041	--	--	16.08	16.08	0.18	0.07	0.05	0.38	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 193 NI 1674 NF 1673 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-1674	0	0	0	-670	--	--	16.08	16.08	0.18	0.01	0.01	0.11	0.00	0.00	20.9
2	0	-0	-1612	0	0	0	-645	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
3	0	-0	-1602	0	0	0	-641	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
4	0	-0	-974	0	0	0	-390	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
5	0	-0	-964	0	0	0	-386	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
6	0	-0	-1400	0	0	0	-560	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
7	0	-0	-1367	0	0	0	-547	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
8	0	-0	-1209	0	0	0	-484	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
9	0	-0	-1176	0	0	0	-470	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
10	0	-0	-1612	0	0	0	-645	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9

11	0	-0	-1602	0	0	0	-641	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
12	0	-0	-974	0	0	0	-390	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
13	0	-0	-964	0	0	0	-386	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
14	0	-0	-1400	0	0	0	-560	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
15	0	-0	-1367	0	0	0	-547	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
16	0	-0	-1209	0	0	0	-484	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
17	0	-0	-1176	0	0	0	-470	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
18	0	-0	-5249	0	0	0	-2100	--	--	16.08	16.08	0.18	0.03	0.04	0.33	0.00	0.00	20.9
19	0	-0	-2249	0	0	0	-900	--	--	16.08	16.08	0.18	0.01	0.02	0.14	0.00	0.00	20.9
20	0	-0	-3421	0	0	0	-1368	--	--	16.08	16.08	0.18	0.02	0.03	0.21	0.00	0.00	20.9
37	0	-0	-5571	0	0	0	-2228	--	--	16.08	16.08	0.18	0.04	0.05	0.35	0.00	0.00	20.9
38	0	-0	-570	0	0	0	-228	--	--	16.08	16.08	0.18	0.00	0.00	0.04	0.00	0.00	20.9
39	0	-0	-2524	0	0	0	-1009	--	--	16.08	16.08	0.18	0.02	0.02	0.16	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	20	-0	-1674	0	0	0	-670	--	--	16.08	16.08	0.18	0.01	0.01	0.11	0.00	0.00	20.9
2	20	-0	-1612	0	0	0	-645	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
3	20	-0	-1602	0	0	0	-641	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
4	20	-0	-974	0	0	0	-390	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
5	20	-0	-964	0	0	0	-386	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
6	20	-0	-1400	0	0	0	-560	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
7	20	-0	-1367	0	0	0	-547	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
8	20	-0	-1209	0	0	0	-484	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
9	20	-0	-1176	0	0	0	-470	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
10	20	-0	-1612	0	0	0	-645	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
11	20	-0	-1602	0	0	0	-641	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
12	20	-0	-974	0	0	0	-390	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
13	20	-0	-964	0	0	0	-386	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
14	20	-0	-1400	0	0	0	-560	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
15	20	-0	-1367	0	0	0	-547	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
16	20	-0	-1209	0	0	0	-484	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
17	20	-0	-1176	0	0	0	-470	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
18	20	-0	-5249	0	0	0	-2100	--	--	16.08	16.08	0.18	0.03	0.04	0.33	0.00	0.00	20.9
19	20	-0	-2249	0	0	0	-900	--	--	16.08	16.08	0.18	0.01	0.02	0.14	0.00	0.00	20.9
20	20	-0	-3421	0	0	0	-1368	--	--	16.08	16.08	0.18	0.02	0.03	0.21	0.00	0.00	20.9
37	20	-0	-5571	0	0	0	-2228	--	--	16.08	16.08	0.18	0.04	0.05	0.35	0.00	0.00	20.9
38	20	-0	-570	0	0	0	-228	--	--	16.08	16.08	0.18	0.00	0.00	0.04	0.00	0.00	20.9
39	20	-0	-2524	0	0	0	-1009	--	--	16.08	16.08	0.18	0.02	0.02	0.16	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	40	-0	-1674	0	0	0	-670	--	--	16.08	16.08	0.18	0.01	0.01	0.11	0.00	0.00	20.9
2	40	-0	-1612	0	0	0	-645	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
3	40	-0	-1602	0	0	0	-641	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
4	40	-0	-974	0	0	0	-390	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
5	40	-0	-964	0	0	0	-386	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
6	40	-0	-1400	0	0	0	-560	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
7	40	-0	-1367	0	0	0	-547	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
8	40	-0	-1209	0	0	0	-484	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
9	40	-0	-1176	0	0	0	-470	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
10	40	-0	-1612	0	0	0	-645	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
11	40	-0	-1602	0	0	0	-641	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
12	40	-0	-974	0	0	0	-390	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
13	40	-0	-964	0	0	0	-386	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
14	40	-0	-1400	0	0	0	-560	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
15	40	-0	-1367	0	0	0	-547	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
16	40	-0	-1209	0	0	0	-484	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
17	40	-0	-1176	0	0	0	-470	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
18	40	-0	-5249	0	0	0	-2100	--	--	16.08	16.08	0.18	0.03	0.04	0.33	0.00	0.00	20.9
19	40	-0	-2249	0	0	0	-900	--	--	16.08	16.08	0.18	0.01	0.02	0.14	0.00	0.00	20.9
20	40	-0	-3421	0	0	0	-1368	--	--	16.08	16.08	0.18	0.02	0.03	0.21	0.00	0.00	20.9
37	40	-0	-5571	0	0	0	-2228	--	--	16.08	16.08	0.18	0.04	0.05	0.35	0.00	0.00	20.9
38	40	-0	-570	0	0	0	-228	--	--	16.08	16.08	0.18	0.00	0.00	0.04	0.00	0.00	20.9
39	40	-0	-2524	0	0	0	-1009	--	--	16.08	16.08	0.18	0.02	0.02	0.16	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 194 NI 1591 NF 1584 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm

1	0	-0	-156	0	0	0	62	--	--	16.08	16.08	0.00	0.00	0.00	0.01	0.00	0.00	20.9
2	0	-0	-286	0	0	0	115	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
3	0	-0	-289	0	0	0	116	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
4	0	-0	50	0	0	0	-20	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
5	0	-0	47	0	0	0	-19	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
6	0	-0	-165	0	0	0	66	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
7	0	-0	-175	0	0	0	70	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
8	0	-0	-64	0	0	0	26	--	--	16.08	16.08	0.10	0.00	0.00	0.00	0.00	0.00	20.9
9	0	-0	-75	0	0	0	30	--	--	16.08	16.08	0.10	0.00	0.00	0.00	0.00	0.00	20.9
10	0	-0	-286	0	0	0	115	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
11	0	-0	-289	0	0	0	116	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
12	0	-0	50	0	0	0	-20	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
13	0	-0	47	0	0	0	-19	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
14	0	-0	-165	0	0	0	66	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
15	0	-0	-175	0	0	0	70	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
16	0	-0	-64	0	0	0	26	--	--	16.08	16.08	0.10	0.00	0.00	0.00	0.00	0.00	20.9
17	0	-0	-75	0	0	0	30	--	--	16.08	16.08	0.10	0.00	0.00	0.00	0.00	0.00	20.9
18	0	-0	-331	0	0	0	132	--	--	16.08	16.08	0.00	0.00	0.00	0.02	0.00	0.00	20.9
19	0	-0	1232	0	0	0	-493	--	--	16.08	16.08	0.18	0.01	0.01	0.08	0.00	0.00	20.9
20	0	-0	354	0	0	0	-141	--	--	16.08	16.08	0.18	0.00	0.00	0.02	0.00	0.00	20.9
37	0	-0	-1051	0	0	0	421	--	--	16.08	16.08	0.00	0.01	0.01	0.07	0.00	0.00	20.9
38	0	-0	1554	0	0	0	-622	--	--	16.08	16.08	0.18	0.01	0.01	0.10	0.00	0.00	20.9
39	0	-0	90	0	0	0	-36	--	--	16.08	16.08	0.18	0.00	0.00	0.01	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	20	-0	-156	0	0	0	62	--	--	16.08	16.08	0.00	0.00	0.00	0.01	0.00	0.00	20.9
2	20	-0	-286	0	0	0	115	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
3	20	-0	-289	0	0	0	116	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
4	20	-0	50	0	0	0	-20	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
5	20	-0	47	0	0	0	-19	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
6	20	-0	-165	0	0	0	66	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9

7	20	-0	-175	0	0	0	70	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
8	20	-0	-64	0	0	0	26	--	--	16.08	16.08	0.10	0.00	0.00	0.00	0.00	0.00	20.9
9	20	-0	-75	0	0	0	30	--	--	16.08	16.08	0.10	0.00	0.00	0.00	0.00	0.00	20.9
10	20	-0	-286	0	0	0	115	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
11	20	-0	-289	0	0	0	116	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
12	20	-0	50	0	0	0	-20	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
13	20	-0	47	0	0	0	-19	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
14	20	-0	-165	0	0	0	66	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
15	20	-0	-175	0	0	0	70	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
16	20	-0	-64	0	0	0	26	--	--	16.08	16.08	0.10	0.00	0.00	0.00	0.00	0.00	20.9
17	20	-0	-75	0	0	0	30	--	--	16.08	16.08	0.10	0.00	0.00	0.00	0.00	0.00	20.9
18	20	-0	-331	0	0	0	132	--	--	16.08	16.08	0.00	0.00	0.00	0.02	0.00	0.00	20.9
19	20	-0	1232	0	0	0	-493	--	--	16.08	16.08	0.18	0.01	0.01	0.08	0.00	0.00	20.9
20	20	-0	354	0	0	0	-141	--	--	16.08	16.08	0.18	0.00	0.00	0.02	0.00	0.00	20.9
37	20	-0	-1051	0	0	0	421	--	--	16.08	16.08	0.00	0.01	0.01	0.07	0.00	0.00	20.9
38	20	-0	1554	0	0	0	-622	--	--	16.08	16.08	0.18	0.01	0.01	0.10	0.00	0.00	20.9
39	20	-0	90	0	0	0	-36	--	--	16.08	16.08	0.18	0.00	0.00	0.01	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	40	-0	-156	0	0	0	-166	--	--	16.08	16.08	0.18	0.00	0.00	0.01	0.00	0.00	20.9
2	40	-0	-286	0	0	0	-306	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
3	40	-0	-289	0	0	0	-309	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
4	40	-0	50	0	0	0	-20	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
5	40	-0	47	0	0	0	-19	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
6	40	-0	-165	0	0	0	-176	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
7	40	-0	-175	0	0	0	-187	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
8	40	-0	-64	0	0	0	-68	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
9	40	-0	-75	0	0	0	-80	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
10	40	-0	-286	0	0	0	-306	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
11	40	-0	-289	0	0	0	-309	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
12	40	-0	50	0	0	0	-20	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
13	40	-0	47	0	0	0	-19	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
14	40	-0	-165	0	0	0	-176	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
15	40	-0	-175	0	0	0	-187	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
16	40	-0	-64	0	0	0	-68	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
17	40	-0	-75	0	0	0	-80	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
18	40	-0	-331	0	0	0	-354	--	--	16.08	16.08	0.18	0.01	0.00	0.02	0.00	0.00	20.9
19	40	-0	1232	0	0	0	-493	--	--	16.08	16.08	0.18	0.01	0.01	0.08	0.00	0.00	20.9
20	40	-0	354	0	0	0	-141	--	--	16.08	16.08	0.18	0.00	0.00	0.02	0.00	0.00	20.9
37	40	-0	-1051	0	0	0	-1123	--	--	16.08	16.08	0.18	0.02	0.01	0.07	0.00	0.00	20.9
38	40	-0	1554	0	0	0	-622	--	--	16.08	16.08	0.18	0.01	0.01	0.10	0.00	0.00	20.9
39	40	-0	90	0	0	0	-36	--	--	16.08	16.08	0.18	0.00	0.00	0.01	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 195 NI 1590 NF 1591 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-770	0	0	0	447	--	--	16.08	16.08	0.00	0.01	0.01	0.05	0.00	0.00	20.9
2	0	-0	-1050	0	0	0	639	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
3	0	-0	-1058	0	0	0	645	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
4	0	-0	-127	0	0	0	43	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
5	0	-0	-135	0	0	0	49	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
6	0	-0	-717	0	0	0	424	--	--	16.08	16.08	0.10	0.01	0.01	0.04	0.00	0.00	20.9
7	0	-0	-745	0	0	0	443	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
8	0	-0	-440	0	0	0	246	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
9	0	-0	-468	0	0	0	264	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
10	0	-0	-1050	0	0	0	639	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
11	0	-0	-1058	0	0	0	645	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
12	0	-0	-127	0	0	0	43	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
13	0	-0	-135	0	0	0	49	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
14	0	-0	-717	0	0	0	424	--	--	16.08	16.08	0.10	0.01	0.01	0.04	0.00	0.00	20.9
15	0	-0	-745	0	0	0	443	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
16	0	-0	-440	0	0	0	246	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
17	0	-0	-468	0	0	0	264	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
18	0	-0	-1385	0	0	0	825	--	--	16.08	16.08	0.00	0.01	0.01	0.09	0.00	0.00	20.9
19	0	-0	2987	0	0	0	-1987	--	--	16.08	16.08	0.18	0.03	0.02	0.19	0.00	0.00	20.9
20	0	-0	550	0	0	0	-416	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9
37	0	-0	-3360	0	0	0	2101	--	--	16.08	16.08	0.00	0.04	0.03	0.21	0.00	0.00	20.9
38	0	-0	3928	0	0	0	-2586	--	--	16.08	16.08	0.18	0.04	0.03	0.25	0.00	0.00	20.9
39	0	-0	-135	0	0	0	31	--	--	16.08	16.08	0.00	0.00	0.00	0.01	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	25	-0	-770	0	0	0	447	--	--	16.08	16.08	0.00	0.01	0.01	0.05	0.00	0.00	20.9
2	25	-0	-1050	0	0	0	639	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
3	25	-0	-1058	0	0	0	645	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
4	25	-0	-127	0	0	0	43	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
5	25	-0	-135	0	0	0	49	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
6	25	-0	-717	0	0	0	424	--	--	16.08	16.08	0.10	0.01	0.01	0.04	0.00	0.00	20.9
7	25	-0	-745	0	0	0	443	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
8	25	-0	-440	0	0	0	246	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
9	25	-0	-468	0	0	0	264	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
10	25	-0	-1050	0	0	0	639	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
11	25	-0	-1058	0	0	0	645	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
12	25	-0	-127	0	0	0	43	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
13	25	-0	-135	0	0	0	49	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
14	25	-0	-717	0	0	0	424	--	--	16.08	16.08	0.10	0.01	0.01	0.04	0.00	0.00	20.9
15	25	-0	-745	0	0	0	443	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
16	25	-0	-440	0	0	0	246	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
17	25	-0	-468	0	0	0	264	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
18	25	-0	-1385	0	0	0	825	--	--	16.08	16.08	0.00	0.01	0.01	0.09	0.00	0.00	20.9
19	25	-0	2987	0	0	0	-1987	--	--	16.08	16.08	0.18	0.03	0.02	0.19	0.00	0.00	20.9
20	25	-0	550	0	0	0	-416	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9
37	25	-0	-3360	0	0	0	2101	--	--	16.08	16.08	0.00	0.04	0.03	0.21	0.00	0.00	20.9
38	25	-0	3928	0	0	0	-2586	--	--	16.08	16.08	0.18	0.04	0.03	0.25	0.00	0.00	20.9
39	25	-0	-135	0	0	0	-36	--	--	16.08	16.08	0.18	0.00	0.00	0.01	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	50	-0	-770	0	0	0	62	--	--	16.08	16.08	0.00	0.00	0.01	0.05	0.00	0.00	20.9
2	50	-0	-1050	0	0	0	115	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9

3	50	-0	-1058	0	0	0	116	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
4	50	-0	-127	0	0	0	-20	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
5	50	-0	-135	0	0	0	-19	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
6	50	-0	-717	0	0	0	66	--	--	16.08	16.08	0.10	0.00	0.01	0.04	0.00	0.00	20.9
7	50	-0	-745	0	0	0	70	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
8	50	-0	-440	0	0	0	26	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
9	50	-0	-468	0	0	0	30	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
10	50	-0	-1050	0	0	0	115	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
11	50	-0	-1058	0	0	0	116	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
12	50	-0	-127	0	0	0	-20	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
13	50	-0	-135	0	0	0	-19	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
14	50	-0	-717	0	0	0	66	--	--	16.08	16.08	0.10	0.00	0.01	0.04	0.00	0.00	20.9
15	50	-0	-745	0	0	0	70	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
16	50	-0	-440	0	0	0	26	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
17	50	-0	-468	0	0	0	30	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
18	50	-0	-1385	0	0	0	132	--	--	16.08	16.08	0.00	0.00	0.01	0.09	0.00	0.00	20.9
19	50	-0	2987	0	0	0	-1987	--	--	16.08	16.08	0.18	0.03	0.02	0.19	0.00	0.00	20.9
20	50	-0	550	0	0	0	-416	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9
37	50	-0	-3360	0	0	0	421	--	--	16.08	16.08	0.00	0.01	0.03	0.21	0.00	0.00	20.9
38	50	-0	3928	0	0	0	-2586	--	--	16.08	16.08	0.18	0.04	0.03	0.25	0.00	0.00	20.9
39	50	-0	-135	0	0	0	-36	--	--	16.08	16.08	0.18	0.00	0.00	0.01	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 196 NI 1583 NF 1590 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-1822	0	0	0	1358	--	--	16.08	16.08	0.00	0.02	0.02	0.11	0.00	0.00	20.9
2	0	-0	-2066	0	0	0	1673	--	--	16.08	16.08	0.10	0.03	0.02	0.13	0.00	0.00	20.9
3	0	-0	-2078	0	0	0	1684	--	--	16.08	16.08	0.10	0.03	0.02	0.13	0.00	0.00	20.9
4	0	-0	-724	0	0	0	406	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
5	0	-0	-736	0	0	0	417	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
6	0	-0	-1583	0	0	0	1216	--	--	16.08	16.08	0.10	0.02	0.01	0.10	0.00	0.00	20.9
7	0	-0	-1623	0	0	0	1254	--	--	16.08	16.08	0.10	0.02	0.01	0.10	0.00	0.00	20.9
8	0	-0	-1180	0	0	0	836	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
9	0	-0	-1220	0	0	0	874	--	--	16.08	16.08	0.10	0.02	0.01	0.08	0.00	0.00	20.9
10	0	-0	-2066	0	0	0	1673	--	--	16.08	16.08	0.10	0.03	0.02	0.13	0.00	0.00	20.9
11	0	-0	-2078	0	0	0	1684	--	--	16.08	16.08	0.10	0.03	0.02	0.13	0.00	0.00	20.9
12	0	-0	-724	0	0	0	406	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
13	0	-0	-736	0	0	0	417	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
14	0	-0	-1583	0	0	0	1216	--	--	16.08	16.08	0.10	0.02	0.01	0.10	0.00	0.00	20.9
15	0	-0	-1623	0	0	0	1254	--	--	16.08	16.08	0.10	0.02	0.01	0.10	0.00	0.00	20.9
16	0	-0	-1180	0	0	0	836	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
17	0	-0	-1220	0	0	0	874	--	--	16.08	16.08	0.10	0.02	0.01	0.08	0.00	0.00	20.9
18	0	-0	-2989	0	0	0	2320	--	--	16.08	16.08	0.00	0.04	0.02	0.19	0.00	0.00	20.9
19	0	-0	3527	0	0	0	-3750	--	--	16.08	16.08	0.18	0.06	0.03	0.22	0.00	0.00	20.9
20	0	-0	-66	0	0	0	-416	--	--	16.08	16.08	0.18	0.01	0.00	0.00	0.00	0.00	20.9
37	0	-0	-5851	0	0	0	5026	--	--	16.08	16.08	0.00	0.09	0.05	0.37	0.00	0.00	20.9
38	0	-0	5009	0	0	0	-5090	--	--	16.08	16.08	0.18	0.08	0.04	0.31	0.00	0.00	20.9
39	0	-0	-979	0	0	0	521	--	--	16.08	16.08	0.00	0.01	0.01	0.06	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	25	-0	-1822	0	0	0	1358	--	--	16.08	16.08	0.00	0.02	0.02	0.11	0.00	0.00	20.9
2	25	-0	-2066	0	0	0	1673	--	--	16.08	16.08	0.10	0.03	0.02	0.13	0.00	0.00	20.9
3	25	-0	-2078	0	0	0	1684	--	--	16.08	16.08	0.10	0.03	0.02	0.13	0.00	0.00	20.9
4	25	-0	-724	0	0	0	406	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
5	25	-0	-736	0	0	0	417	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
6	25	-0	-1583	0	0	0	1216	--	--	16.08	16.08	0.10	0.02	0.01	0.10	0.00	0.00	20.9
7	25	-0	-1623	0	0	0	1254	--	--	16.08	16.08	0.10	0.02	0.01	0.10	0.00	0.00	20.9
8	25	-0	-1180	0	0	0	836	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
9	25	-0	-1220	0	0	0	874	--	--	16.08	16.08	0.10	0.02	0.01	0.08	0.00	0.00	20.9
10	25	-0	-2066	0	0	0	1673	--	--	16.08	16.08	0.10	0.03	0.02	0.13	0.00	0.00	20.9
11	25	-0	-2078	0	0	0	1684	--	--	16.08	16.08	0.10	0.03	0.02	0.13	0.00	0.00	20.9
12	25	-0	-724	0	0	0	406	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
13	25	-0	-736	0	0	0	417	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
14	25	-0	-1583	0	0	0	1216	--	--	16.08	16.08	0.10	0.02	0.01	0.10	0.00	0.00	20.9
15	25	-0	-1623	0	0	0	1254	--	--	16.08	16.08	0.10	0.02	0.01	0.10	0.00	0.00	20.9
16	25	-0	-1180	0	0	0	836	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
17	25	-0	-1220	0	0	0	874	--	--	16.08	16.08	0.10	0.02	0.01	0.08	0.00	0.00	20.9
18	25	-0	-2989	0	0	0	2320	--	--	16.08	16.08	0.00	0.04	0.02	0.19	0.00	0.00	20.9
19	25	-0	3527	0	0	0	-3750	--	--	16.08	16.08	0.18	0.06	0.03	0.22	0.00	0.00	20.9
20	25	-0	-66	0	0	0	-416	--	--	16.08	16.08	0.18	0.01	0.00	0.00	0.00	0.00	20.9
37	25	-0	-5851	0	0	0	5026	--	--	16.08	16.08	0.00	0.09	0.05	0.37	0.00	0.00	20.9
38	25	-0	5009	0	0	0	-5090	--	--	16.08	16.08	0.18	0.08	0.04	0.31	0.00	0.00	20.9
39	25	-0	-979	0	0	0	521	--	--	16.08	16.08	0.00	0.01	0.01	0.06	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	50	-0	-1822	0	0	0	447	--	--	16.08	16.08	0.00	0.01	0.02	0.11	0.00	0.00	20.9
2	50	-0	-2066	0	0	0	639	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
3	50	-0	-2078	0	0	0	645	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
4	50	-0	-724	0	0	0	43	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
5	50	-0	-736	0	0	0	49	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
6	50	-0	-1583	0	0	0	424	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
7	50	-0	-1623	0	0	0	443	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
8	50	-0	-1180	0	0	0	246	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
9	50	-0	-1220	0	0	0	264	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
10	50	-0	-2066	0	0	0	639	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
11	50	-0	-2078	0	0	0	645	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
12	50	-0	-724	0	0	0	43	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
13	50	-0	-736	0	0	0	49	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
14	50	-0	-1583	0	0	0	424	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
15	50	-0	-1623	0	0	0	443	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
16	50	-0	-1180	0	0	0	246	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
17	50	-0	-1220	0	0	0	264	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
18	50	-0	-2989	0	0	0	825	--	--	16.08	16.08	0.00	0.01	0.02	0.19	0.00	0.00	20.9
19	50	-0	3527	0	0	0	-3750	--	--	16.08	16.08	0.18	0.06	0.03	0.22	0.00	0.00	20.9
20	50	-0	-66	0	0	0	-416	--	--	16.08	16.08	0.18	0.01	0.00	0.00	0.00	0.00	20.9
37	50	-0	-5851	0	0	0	2101	--	--	16.08	16.08	0.00	0.04	0.05	0.37	0.00	0.00	20.9
38	50	-0	5009	0	0	0	-5090	--	--	16.08	16.08	0.18	0.08	0.04	0.31	0.00	0.00	20.9
39	50	-0	-979	0	0	0	31	--	--	16.08	16.08	0.00	0.00	0.01	0.06	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 197 NI 1582 NF 1583 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	6121	0	0	0	13510	--	--	16.08	16.08	0.00	0.23	0.05	0.38	0.00	0.00	20.9
2	0	-0	5218	0	0	0	8640	--	--	16.08	16.08	0.10	0.15	0.04	0.33	0.00	0.00	20.9
3	0	-0	5231	0	0	0	8588	--	--	16.08	16.08	0.10	0.15	0.04	0.33	0.00	0.00	20.9
4	0	-0	4186	0	0	0	12200	--	--	16.08	16.08	0.10	0.22	0.03	0.26	0.00	0.00	20.9
5	0	-0	4199	0	0	0	12150	--	--	16.08	16.08	0.10	0.22	0.03	0.26	0.00	0.00	20.9
6	0	-0	4843	0	0	0	9946	--	--	16.08	16.08	0.10	0.18	0.04	0.30	0.00	0.00	20.9
7	0	-0	4884	0	0	0	9774	--	--	16.08	16.08	0.10	0.17	0.04	0.31	0.00	0.00	20.9
8	0	-0	4533	0	0	0	11010	--	--	16.08	16.08	0.10	0.20	0.04	0.28	0.00	0.00	20.9
9	0	-0	4574	0	0	0	10840	--	--	16.08	16.08	0.10	0.19	0.04	0.29	0.00	0.00	20.9
10	0	-0	5218	0	0	0	8640	--	--	16.08	16.08	0.10	0.15	0.04	0.33	0.00	0.00	20.9
11	0	-0	5231	0	0	0	8588	--	--	16.08	16.08	0.10	0.15	0.04	0.33	0.00	0.00	20.9
12	0	-0	4186	0	0	0	12200	--	--	16.08	16.08	0.10	0.22	0.03	0.26	0.00	0.00	20.9
13	0	-0	4199	0	0	0	12150	--	--	16.08	16.08	0.10	0.22	0.03	0.26	0.00	0.00	20.9
14	0	-0	4843	0	0	0	9946	--	--	16.08	16.08	0.10	0.18	0.04	0.30	0.00	0.00	20.9
15	0	-0	4884	0	0	0	9774	--	--	16.08	16.08	0.10	0.17	0.04	0.31	0.00	0.00	20.9
16	0	-0	4533	0	0	0	11010	--	--	16.08	16.08	0.10	0.20	0.04	0.28	0.00	0.00	20.9
17	0	-0	4574	0	0	0	10840	--	--	16.08	16.08	0.10	0.19	0.04	0.29	0.00	0.00	20.9
18	0	-0	8809	0	0	0	17650	--	--	16.08	16.08	0.00	0.30	0.07	0.55	0.00	0.00	20.9
19	0	-0	3499	0	0	0	30570	--	--	16.08	16.08	0.00	0.52	0.03	0.22	0.00	0.00	20.9
20	0	-0	6164	0	0	0	22390	--	--	16.08	16.08	0.00	0.38	0.05	0.39	0.00	0.00	20.9
37	0	-0	10580	0	0	0	9893	--	--	16.08	16.08	0.00	0.17	0.09	0.66	0.00	0.00	20.9
38	0	-0	1735	0	0	0	31440	--	--	16.08	16.08	0.00	0.54	0.01	0.11	0.00	0.00	20.9
39	0	-0	6176	0	0	0	17800	--	--	16.08	16.08	0.00	0.30	0.05	0.39	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	10	-0	6121	0	0	0	20667	--	--	16.08	16.08	0.00	0.35	0.05	0.38	0.00	0.00	20.9
2	10	-0	5218	0	0	0	14739	--	--	16.08	16.08	0.10	0.26	0.04	0.33	0.00	0.00	20.9
3	10	-0	5231	0	0	0	14702	--	--	16.08	16.08	0.10	0.26	0.04	0.33	0.00	0.00	20.9
4	10	-0	4186	0	0	0	17094	--	--	16.08	16.08	0.10	0.30	0.03	0.26	0.00	0.00	20.9
5	10	-0	4199	0	0	0	17058	--	--	16.08	16.08	0.10	0.30	0.03	0.26	0.00	0.00	20.9
6	10	-0	4843	0	0	0	15604	--	--	16.08	16.08	0.10	0.28	0.04	0.30	0.00	0.00	20.9
7	10	-0	4884	0	0	0	15482	--	--	16.08	16.08	0.10	0.27	0.04	0.31	0.00	0.00	20.9
8	10	-0	4533	0	0	0	16310	--	--	16.08	16.08	0.10	0.29	0.04	0.28	0.00	0.00	20.9
9	10	-0	4574	0	0	0	16188	--	--	16.08	16.08	0.10	0.29	0.04	0.29	0.00	0.00	20.9
10	10	-0	5218	0	0	0	14739	--	--	16.08	16.08	0.10	0.26	0.04	0.33	0.00	0.00	20.9
11	10	-0	5231	0	0	0	14702	--	--	16.08	16.08	0.10	0.26	0.04	0.33	0.00	0.00	20.9
12	10	-0	4186	0	0	0	17094	--	--	16.08	16.08	0.10	0.30	0.03	0.26	0.00	0.00	20.9
13	10	-0	4199	0	0	0	17058	--	--	16.08	16.08	0.10	0.30	0.03	0.26	0.00	0.00	20.9
14	10	-0	4843	0	0	0	15604	--	--	16.08	16.08	0.10	0.28	0.04	0.30	0.00	0.00	20.9
15	10	-0	4884	0	0	0	15482	--	--	16.08	16.08	0.10	0.27	0.04	0.31	0.00	0.00	20.9
16	10	-0	4533	0	0	0	16310	--	--	16.08	16.08	0.10	0.29	0.04	0.28	0.00	0.00	20.9
17	10	-0	4574	0	0	0	16188	--	--	16.08	16.08	0.10	0.29	0.04	0.29	0.00	0.00	20.9
18	10	-0	8809	0	0	0	27945	--	--	16.08	16.08	0.00	0.48	0.07	0.55	0.00	0.00	20.9
19	10	-0	3499	0	0	0	34660	--	--	16.08	16.08	0.00	0.59	0.03	0.22	0.00	0.00	20.9
20	10	-0	6164	0	0	0	29598	--	--	16.08	16.08	0.00	0.50	0.05	0.39	0.00	0.00	20.9
37	10	-0	10580	0	0	0	22259	--	--	16.08	16.08	0.00	0.38	0.09	0.66	0.00	0.00	20.9
38	10	-0	1735	0	0	0	33464	--	--	16.08	16.08	0.00	0.57	0.01	0.11	0.00	0.00	20.9
39	10	-0	6176	0	0	0	25021	--	--	16.08	16.08	0.00	0.43	0.05	0.39	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	20	-0	6121	0	0	0	14740	--	--	16.08	16.08	0.00	0.25	0.05	0.38	0.00	0.00	20.9
2	20	-0	5218	0	0	0	9684	--	--	16.08	16.08	0.10	0.17	0.04	0.33	0.00	0.00	20.9
3	20	-0	5231	0	0	0	9635	--	--	16.08	16.08	0.10	0.17	0.04	0.33	0.00	0.00	20.9
4	20	-0	4186	0	0	0	13040	--	--	16.08	16.08	0.10	0.23	0.03	0.26	0.00	0.00	20.9
5	20	-0	4199	0	0	0	12990	--	--	16.08	16.08	0.10	0.23	0.03	0.26	0.00	0.00	20.9
6	20	-0	4843	0	0	0	10910	--	--	16.08	16.08	0.10	0.19	0.04	0.30	0.00	0.00	20.9
7	20	-0	4884	0	0	0	10750	--	--	16.08	16.08	0.10	0.19	0.04	0.31	0.00	0.00	20.9
8	20	-0	4533	0	0	0	11920	--	--	16.08	16.08	0.10	0.21	0.04	0.28	0.00	0.00	20.9
9	20	-0	4574	0	0	0	11760	--	--	16.08	16.08	0.10	0.21	0.04	0.29	0.00	0.00	20.9
10	20	-0	5218	0	0	0	9684	--	--	16.08	16.08	0.10	0.17	0.04	0.33	0.00	0.00	20.9
11	20	-0	5231	0	0	0	9635	--	--	16.08	16.08	0.10	0.17	0.04	0.33	0.00	0.00	20.9
12	20	-0	4186	0	0	0	13040	--	--	16.08	16.08	0.10	0.23	0.03	0.26	0.00	0.00	20.9
13	20	-0	4199	0	0	0	12990	--	--	16.08	16.08	0.10	0.23	0.03	0.26	0.00	0.00	20.9
14	20	-0	4843	0	0	0	10910	--	--	16.08	16.08	0.10	0.19	0.04	0.30	0.00	0.00	20.9
15	20	-0	4884	0	0	0	10750	--	--	16.08	16.08	0.10	0.19	0.04	0.31	0.00	0.00	20.9
16	20	-0	4533	0	0	0	11920	--	--	16.08	16.08	0.10	0.21	0.04	0.28	0.00	0.00	20.9
17	20	-0	4574	0	0	0	11760	--	--	16.08	16.08	0.10	0.21	0.04	0.29	0.00	0.00	20.9
18	20	-0	8809	0	0	0	19410	--	--	16.08	16.08	0.00	0.33	0.07	0.55	0.00	0.00	20.9
19	20	-0	3499	0	0	0	31270	--	--	16.08	16.08	0.00	0.53	0.03	0.22	0.00	0.00	20.9
20	20	-0	6164	0	0	0	23630	--	--	16.08	16.08	0.00	0.40	0.05	0.39	0.00	0.00	20.9
37	20	-0	10580	0	0	0	12010	--	--	16.08	16.08	0.00	0.20	0.09	0.66	0.00	0.00	20.9
38	20	-0	1735	0	0	0	31780	--	--	16.08	16.08	0.00	0.54	0.01	0.11	0.00	0.00	20.9
39	20	-0	6176	0	0	0	19040	--	--	16.08	16.08	0.00	0.32	0.05	0.39	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 198 NI 1589 NF 1582 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	10430	0	0	0	9937	--	--	16.08	16.08	0.00	0.17	0.09	0.65	0.00	0.00	20.9
2	0	-0	6826	0	0	0	6205	--	--	16.08	16.08	0.10	0.11	0.06	0.43	0.00	0.00	20.9
3	0	-0	6798	0	0	0	6172	--	--	16.08	16.08	0.10	0.11	0.06	0.43	0.00	0.00	20.9
4	0	-0	9247	0	0	0	9116	--	--	16.08	16.08	0.10	0.16	0.08	0.58	0.00	0.00	20.9
5	0	-0	9219	0	0	0	9083	--	--	16.08	16.08	0.10	0.16	0.08	0.58	0.00	0.00	20.9
6	0	-0	7706	0	0	0	7261	--	--	16.08	16.08	0.10	0.13	0.06	0.48	0.00	0.00	20.9
7	0	-0	7613	0	0	0	7153	--	--	16.08	16.08	0.10	0.13	0.06	0.48	0.00	0.00	20.9
8	0	-0	8432	0	0	0	8135	--	--	16.08	16.08	0.10	0.14	0.07	0.53	0.00	0.00	20.9
9	0	-0	8339	0	0	0	8027	--	--	16.08	16.08	0.10	0.14	0.07	0.52	0.00	0.00	20.9
10	0	-0	6826	0	0	0	6205	--	--	16.08	16.08	0.10	0.11	0.06	0.43	0.00	0.00	20.9

11	0	-0	6798	0	0	0	6172	--	--	16.08	16.08	0.10	0.11	0.06	0.43	0.00	0.00	20.9
12	0	-0	9247	0	0	0	9116	--	--	16.08	16.08	0.10	0.16	0.08	0.58	0.00	0.00	20.9
13	0	-0	9219	0	0	0	9083	--	--	16.08	16.08	0.10	0.16	0.08	0.58	0.00	0.00	20.9
14	0	-0	7706	0	0	0	7261	--	--	16.08	16.08	0.10	0.13	0.06	0.48	0.00	0.00	20.9
15	0	-0	7613	0	0	0	7153	--	--	16.08	16.08	0.10	0.13	0.06	0.48	0.00	0.00	20.9
16	0	-0	8432	0	0	0	8135	--	--	16.08	16.08	0.10	0.14	0.07	0.53	0.00	0.00	20.9
17	0	-0	8339	0	0	0	8027	--	--	16.08	16.08	0.10	0.14	0.07	0.52	0.00	0.00	20.9
18	0	-0	13650	0	0	0	12800	--	--	16.08	16.08	0.00	0.22	0.11	0.86	0.00	0.00	20.9
19	0	-0	22280	0	0	0	23770	--	--	16.08	16.08	0.00	0.41	0.18	1.40	2.62	0.00	20.9
20	0	-0	16770	0	0	0	16960	--	--	16.08	16.08	0.00	0.29	0.14	1.05	1.97	0.00	20.9
37	0	-0	8327	0	0	0	6426	--	--	16.08	16.08	0.00	0.11	0.07	0.52	0.00	0.00	20.9
38	0	-0	22700	0	0	0	24710	--	--	16.08	16.08	0.00	0.42	0.19	1.42	2.67	0.00	20.9
39	0	-0	13520	0	0	0	13360	--	--	16.08	16.08	0.00	0.23	0.11	0.85	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	30	-0	10430	0	0	0	24211	--	--	16.08	16.08	0.00	0.41	0.09	0.65	0.00	0.00	20.9
2	30	-0	6826	0	0	0	15548	--	--	16.08	16.08	0.10	0.28	0.06	0.43	0.00	0.00	20.9
3	30	-0	6798	0	0	0	15476	--	--	16.08	16.08	0.10	0.27	0.06	0.43	0.00	0.00	20.9
4	30	-0	9247	0	0	0	21771	--	--	16.08	16.08	0.10	0.39	0.08	0.58	0.00	0.00	20.9
5	30	-0	9219	0	0	0	21699	--	--	16.08	16.08	0.10	0.39	0.08	0.58	0.00	0.00	20.9
6	30	-0	7706	0	0	0	17806	--	--	16.08	16.08	0.10	0.32	0.06	0.48	0.00	0.00	20.9
7	30	-0	7613	0	0	0	17573	--	--	16.08	16.08	0.10	0.31	0.06	0.48	0.00	0.00	20.9
8	30	-0	8432	0	0	0	19674	--	--	16.08	16.08	0.10	0.35	0.07	0.53	0.00	0.00	20.9
9	30	-0	8339	0	0	0	19441	--	--	16.08	16.08	0.10	0.34	0.07	0.52	0.00	0.00	20.9
10	30	-0	6826	0	0	0	15548	--	--	16.08	16.08	0.10	0.28	0.06	0.43	0.00	0.00	20.9
11	30	-0	6798	0	0	0	15476	--	--	16.08	16.08	0.10	0.27	0.06	0.43	0.00	0.00	20.9
12	30	-0	9247	0	0	0	21771	--	--	16.08	16.08	0.10	0.39	0.08	0.58	0.00	0.00	20.9
13	30	-0	9219	0	0	0	21699	--	--	16.08	16.08	0.10	0.39	0.08	0.58	0.00	0.00	20.9
14	30	-0	7706	0	0	0	17806	--	--	16.08	16.08	0.10	0.32	0.06	0.48	0.00	0.00	20.9
15	30	-0	7613	0	0	0	17573	--	--	16.08	16.08	0.10	0.31	0.06	0.48	0.00	0.00	20.9
16	30	-0	8432	0	0	0	19674	--	--	16.08	16.08	0.10	0.35	0.07	0.53	0.00	0.00	20.9
17	30	-0	8339	0	0	0	19441	--	--	16.08	16.08	0.10	0.34	0.07	0.52	0.00	0.00	20.9
18	30	-0	13650	0	0	0	31483	--	--	16.08	16.08	0.00	0.54	0.11	0.86	0.00	0.00	20.9
19	30	-0	22280	0	0	0	54262	--	--	16.08	16.08	0.00	0.93	0.18	1.23	2.62	0.00	20.9
20	30	-0	16770	0	0	0	39913	--	--	16.08	16.08	0.00	0.68	0.14	1.02	1.97	0.00	20.9
37	30	-0	8327	0	0	0	17822	--	--	16.08	16.08	0.00	0.30	0.07	0.52	0.00	0.00	20.9
38	30	-0	22700	0	0	0	55781	--	--	16.08	16.08	0.00	0.95	0.19	1.26	2.67	0.00	20.9
39	30	-0	13520	0	0	0	31864	--	--	16.08	16.08	0.00	0.54	0.11	0.85	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	60	-0	10430	0	0	0	16190	--	--	16.08	16.08	0.00	0.28	0.09	0.65	0.00	0.00	20.9
2	60	-0	6826	0	0	0	10300	--	--	16.08	16.08	0.10	0.18	0.06	0.43	0.00	0.00	20.9
3	60	-0	6798	0	0	0	10250	--	--	16.08	16.08	0.10	0.18	0.06	0.43	0.00	0.00	20.9
4	60	-0	9247	0	0	0	14660	--	--	16.08	16.08	0.10	0.26	0.08	0.58	0.00	0.00	20.9
5	60	-0	9219	0	0	0	14610	--	--	16.08	16.08	0.10	0.26	0.08	0.58	0.00	0.00	20.9
6	60	-0	7706	0	0	0	11880	--	--	16.08	16.08	0.10	0.21	0.06	0.48	0.00	0.00	20.9
7	60	-0	7613	0	0	0	11720	--	--	16.08	16.08	0.10	0.21	0.06	0.48	0.00	0.00	20.9
8	60	-0	8432	0	0	0	13190	--	--	16.08	16.08	0.10	0.23	0.07	0.53	0.00	0.00	20.9
9	60	-0	8339	0	0	0	13030	--	--	16.08	16.08	0.10	0.23	0.07	0.52	0.00	0.00	20.9
10	60	-0	6826	0	0	0	10300	--	--	16.08	16.08	0.10	0.18	0.06	0.43	0.00	0.00	20.9
11	60	-0	6798	0	0	0	10250	--	--	16.08	16.08	0.10	0.18	0.06	0.43	0.00	0.00	20.9
12	60	-0	9247	0	0	0	14660	--	--	16.08	16.08	0.10	0.26	0.08	0.58	0.00	0.00	20.9
13	60	-0	9219	0	0	0	14610	--	--	16.08	16.08	0.10	0.26	0.08	0.58	0.00	0.00	20.9
14	60	-0	7706	0	0	0	11880	--	--	16.08	16.08	0.10	0.21	0.06	0.48	0.00	0.00	20.9
15	60	-0	7613	0	0	0	11720	--	--	16.08	16.08	0.10	0.21	0.06	0.48	0.00	0.00	20.9
16	60	-0	8432	0	0	0	13190	--	--	16.08	16.08	0.10	0.23	0.07	0.53	0.00	0.00	20.9
17	60	-0	8339	0	0	0	13030	--	--	16.08	16.08	0.10	0.23	0.07	0.52	0.00	0.00	20.9
18	60	-0	13650	0	0	0	20990	--	--	16.08	16.08	0.00	0.36	0.11	0.86	0.00	0.00	20.9
19	60	-0	22280	0	0	0	37130	--	--	16.08	16.08	0.00	0.63	0.18	1.36	2.62	0.00	20.9
20	60	-0	16770	0	0	0	27020	--	--	16.08	16.08	0.00	0.46	0.14	1.05	1.97	0.00	20.9
37	60	-0	8327	0	0	0	11420	--	--	16.08	16.08	0.00	0.19	0.07	0.52	0.00	0.00	20.9
38	60	-0	22700	0	0	0	38330	--	--	16.08	16.08	0.00	0.65	0.19	1.38	2.67	0.00	20.9
39	60	-0	13520	0	0	0	21470	--	--	16.08	16.08	0.00	0.37	0.11	0.85	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 199 NI 1588 NF 1589 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm

1	0	-0	8355	0	0	0	5759	--	--	16.08	16.08	0.00	0.10	0.07	0.52	0.00	0.00	20.9
2	0	-0	5327	0	0	0	3541	--	--	16.08	16.08	0.10	0.06	0.04	0.33	0.00	0.00	20.9
3	0	-0	5301	0	0	0	3521	--	--	16.08	16.08	0.10	0.06	0.04	0.33	0.00	0.00	20.9
4	0	-0	7553	0	0	0	5339	--	--	16.08	16.08	0.10	0.09	0.06	0.47	0.00	0.00	20.9
5	0	-0	7528	0	0	0	5319	--	--	16.08	16.08	0.10	0.09	0.06	0.47	0.00	0.00	20.9
6	0	-0	6135	0	0	0	4194	--	--	16.08	16.08	0.10	0.07	0.05	0.38	0.00	0.00	20.9
7	0	-0	6051	0	0	0	4128	--	--	16.08	16.08	0.10	0.07	0.05	0.38	0.00	0.00	20.9
8	0	-0	6803	0	0	0	4733	--	--	16.08	16.08	0.10	0.08	0.06	0.43	0.00	0.00	20.9
9	0	-0	6719	0	0	0	4667	--	--	16.08	16.08	0.10	0.08	0.06	0.42	0.00	0.00	20.9
10	0	-0	5327	0	0	0	3541	--	--	16.08	16.08	0.10	0.06	0.04	0.33	0.00	0.00	20.9
11	0	-0	5301	0	0	0	3521	--	--	16.08	16.08	0.10	0.06	0.04	0.33	0.00	0.00	20.9
12	0	-0	7553	0	0	0	5339	--	--	16.08	16.08	0.10	0.09	0.06	0.47	0.00	0.00	20.9
13	0	-0	7528	0	0	0	5319	--	--	16.08	16.08	0.10	0.09	0.06	0.47	0.00	0.00	20.9
14	0	-0	6135	0	0	0	4194	--	--	16.08	16.08	0.10	0.07	0.05	0.38	0.00	0.00	20.9
15	0	-0	6051	0	0	0	4128	--	--	16.08	16.08	0.10	0.07	0.05	0.38	0.00	0.00	20.9
16	0	-0	6803	0	0	0	4733	--	--	16.08	16.08	0.10	0.08	0.06	0.43	0.00	0.00	20.9
17	0	-0	6719	0	0	0	4667	--	--	16.08	16.08	0.10	0.08	0.06	0.42	0.00	0.00	20.9
18	0	-0	10840	0	0	0	7380	--	--	16.08	16.08	0.00	0.13	0.09	0.68	0.00	0.00	20.9
19	0	-0	19060	0	0	0	14240	--	--	16.08	16.08	0.00	0.24	0.16	1.20	2.24	0.00	20.9
20	0	-0	13900	0	0	0	10010	--	--	16.08	16.08	0.00	0.17	0.11	0.87	0.00	0.00	20.9
37	0	-0	5955	0	0	0	3449	--	--	16.08	16.08	0.00	0.06	0.05	0.37	0.00	0.00	20.9
38	0	-0	19650	0	0	0	14880	--	--	16.08	16.08	0.00	0.25	0.16	1.23	2.31	0.00	20.9
39	0	-0	11060	0	0	0	7829	--	--	16.08	16.08	0.00	0.13	0.09	0.69	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	25	-0	8355	0	0	0	16777	--	--	16.08	16.08	0.00	0.29	0.07	0.52	0.00	0.00	20.9
2	25	-0	5327	0	0	0	10566	--	--	16.08	16.08	0.10	0.19	0.04	0.33	0.00	0.00	20.9
3	25	-0	5301	0	0	0	10512	--	--	16.08	16.08	0.10	0.19	0.04	0.33	0.00	0.00	20.9
4	25	-0	7553	0	0	0	15300	--	--	16.08	16.08	0.10	0.27	0.06	0.47	0.00	0.00	20.9
5	25	-0	7528	0	0	0	15247	--	--	16.08	16.08	0.10	0.27	0.06	0.47	0.00	0.00	20.9
6	25	-0	6135	0	0	0	12284	--	--	16.08	16.08	0.10	0.22	0.05	0.38	0.00	0.00	20.9

7	25	-0	6051	0	0	0	12108	--	--	16.08	16.08	0.10	0.21	0.05	0.38	0.00	0.00	20.9
8	25	-0	6803	0	0	0	13705	--	--	16.08	16.08	0.10	0.24	0.06	0.43	0.00	0.00	20.9
9	25	-0	6719	0	0	0	13528	--	--	16.08	16.08	0.10	0.24	0.06	0.42	0.00	0.00	20.9
10	25	-0	5327	0	0	0	10566	--	--	16.08	16.08	0.10	0.19	0.04	0.33	0.00	0.00	20.9
11	25	-0	5301	0	0	0	10512	--	--	16.08	16.08	0.10	0.19	0.04	0.33	0.00	0.00	20.9
12	25	-0	7553	0	0	0	15300	--	--	16.08	16.08	0.10	0.27	0.06	0.47	0.00	0.00	20.9
13	25	-0	7528	0	0	0	15247	--	--	16.08	16.08	0.10	0.27	0.06	0.47	0.00	0.00	20.9
14	25	-0	6135	0	0	0	12284	--	--	16.08	16.08	0.10	0.22	0.05	0.38	0.00	0.00	20.9
15	25	-0	6051	0	0	0	12108	--	--	16.08	16.08	0.10	0.21	0.05	0.38	0.00	0.00	20.9
16	25	-0	6803	0	0	0	13705	--	--	16.08	16.08	0.10	0.24	0.06	0.43	0.00	0.00	20.9
17	25	-0	6719	0	0	0	13528	--	--	16.08	16.08	0.10	0.24	0.06	0.42	0.00	0.00	20.9
18	25	-0	10840	0	0	0	21675	--	--	16.08	16.08	0.00	0.37	0.09	0.68	0.00	0.00	20.9
19	25	-0	19060	0	0	0	39375	--	--	16.08	16.08	0.00	0.67	0.16	1.16	2.24	0.00	20.9
20	25	-0	13900	0	0	0	28341	--	--	16.08	16.08	0.00	0.48	0.11	0.87	0.00	0.00	20.9
37	25	-0	5955	0	0	0	11302	--	--	16.08	16.08	0.00	0.19	0.05	0.37	0.00	0.00	20.9
38	25	-0	19650	0	0	0	40796	--	--	16.08	16.08	0.00	0.70	0.16	1.20	2.31	0.00	20.9
39	25	-0	11060	0	0	0	22415	--	--	16.08	16.08	0.00	0.38	0.09	0.69	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	50	-0	8355	0	0	0	9937	--	--	16.08	16.08	0.00	0.17	0.07	0.52	0.00	0.00	20.9
2	50	-0	5327	0	0	0	6205	--	--	16.08	16.08	0.10	0.11	0.04	0.33	0.00	0.00	20.9
3	50	-0	5301	0	0	0	6172	--	--	16.08	16.08	0.10	0.11	0.04	0.33	0.00	0.00	20.9
4	50	-0	7553	0	0	0	9116	--	--	16.08	16.08	0.10	0.16	0.06	0.47	0.00	0.00	20.9
5	50	-0	7528	0	0	0	9083	--	--	16.08	16.08	0.10	0.16	0.06	0.47	0.00	0.00	20.9
6	50	-0	6135	0	0	0	7261	--	--	16.08	16.08	0.10	0.13	0.05	0.38	0.00	0.00	20.9
7	50	-0	6051	0	0	0	7153	--	--	16.08	16.08	0.10	0.13	0.05	0.38	0.00	0.00	20.9
8	50	-0	6803	0	0	0	8135	--	--	16.08	16.08	0.10	0.14	0.06	0.43	0.00	0.00	20.9
9	50	-0	6719	0	0	0	8027	--	--	16.08	16.08	0.10	0.14	0.06	0.42	0.00	0.00	20.9
10	50	-0	5327	0	0	0	6205	--	--	16.08	16.08	0.10	0.11	0.04	0.33	0.00	0.00	20.9
11	50	-0	5301	0	0	0	6172	--	--	16.08	16.08	0.10	0.11	0.04	0.33	0.00	0.00	20.9
12	50	-0	7553	0	0	0	9116	--	--	16.08	16.08	0.10	0.16	0.06	0.47	0.00	0.00	20.9
13	50	-0	7528	0	0	0	9083	--	--	16.08	16.08	0.10	0.16	0.06	0.47	0.00	0.00	20.9
14	50	-0	6135	0	0	0	7261	--	--	16.08	16.08	0.10	0.13	0.05	0.38	0.00	0.00	20.9
15	50	-0	6051	0	0	0	7153	--	--	16.08	16.08	0.10	0.13	0.05	0.38	0.00	0.00	20.9
16	50	-0	6803	0	0	0	8135	--	--	16.08	16.08	0.10	0.14	0.06	0.43	0.00	0.00	20.9
17	50	-0	6719	0	0	0	8027	--	--	16.08	16.08	0.10	0.14	0.06	0.42	0.00	0.00	20.9
18	50	-0	10840	0	0	0	12800	--	--	16.08	16.08	0.00	0.22	0.09	0.68	0.00	0.00	20.9
19	50	-0	19060	0	0	0	23770	--	--	16.08	16.08	0.00	0.41	0.16	1.20	2.24	0.00	20.9
20	50	-0	13900	0	0	0	16960	--	--	16.08	16.08	0.00	0.29	0.11	0.87	0.00	0.00	20.9
37	50	-0	5955	0	0	0	6426	--	--	16.08	16.08	0.00	0.11	0.05	0.37	0.00	0.00	20.9
38	50	-0	19650	0	0	0	24710	--	--	16.08	16.08	0.00	0.42	0.16	1.23	2.31	0.00	20.9
39	50	-0	11060	0	0	0	13360	--	--	16.08	16.08	0.00	0.23	0.09	0.69	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 200 NI 1587 NF 1588 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	6238	0	0	0	2640	--	--	16.08	16.08	0.00	0.05	0.05	0.39	0.00	0.00	20.9
2	0	-0	3886	0	0	0	1598	--	--	16.08	16.08	0.10	0.03	0.03	0.24	0.00	0.00	20.9
3	0	-0	3866	0	0	0	1589	--	--	16.08	16.08	0.10	0.03	0.03	0.24	0.00	0.00	20.9
4	0	-0	5731	0	0	0	2474	--	--	16.08	16.08	0.10	0.04	0.05	0.36	0.00	0.00	20.9
5	0	-0	5711	0	0	0	2464	--	--	16.08	16.08	0.10	0.04	0.05	0.36	0.00	0.00	20.9
6	0	-0	4556	0	0	0	1916	--	--	16.08	16.08	0.10	0.03	0.04	0.29	0.00	0.00	20.9
7	0	-0	4488	0	0	0	1884	--	--	16.08	16.08	0.10	0.03	0.04	0.28	0.00	0.00	20.9
8	0	-0	5109	0	0	0	2178	--	--	16.08	16.08	0.10	0.04	0.04	0.32	0.00	0.00	20.9
9	0	-0	5041	0	0	0	2146	--	--	16.08	16.08	0.10	0.04	0.04	0.32	0.00	0.00	20.9
10	0	-0	3886	0	0	0	1598	--	--	16.08	16.08	0.10	0.03	0.03	0.24	0.00	0.00	20.9
11	0	-0	3866	0	0	0	1589	--	--	16.08	16.08	0.10	0.03	0.03	0.24	0.00	0.00	20.9
12	0	-0	5731	0	0	0	2474	--	--	16.08	16.08	0.10	0.04	0.05	0.36	0.00	0.00	20.9
13	0	-0	5711	0	0	0	2464	--	--	16.08	16.08	0.10	0.04	0.05	0.36	0.00	0.00	20.9
14	0	-0	4556	0	0	0	1916	--	--	16.08	16.08	0.10	0.03	0.04	0.29	0.00	0.00	20.9
15	0	-0	4488	0	0	0	1884	--	--	16.08	16.08	0.10	0.03	0.04	0.28	0.00	0.00	20.9
16	0	-0	5109	0	0	0	2178	--	--	16.08	16.08	0.10	0.04	0.04	0.32	0.00	0.00	20.9
17	0	-0	5041	0	0	0	2146	--	--	16.08	16.08	0.10	0.04	0.04	0.32	0.00	0.00	20.9
18	0	-0	8028	0	0	0	3366	--	--	16.08	16.08	0.00	0.06	0.07	0.50	0.00	0.00	20.9
19	0	-0	14990	0	0	0	6745	--	--	16.08	16.08	0.00	0.11	0.12	0.94	0.00	0.00	20.9
20	0	-0	10670	0	0	0	4671	--	--	16.08	16.08	0.00	0.08	0.09	0.67	0.00	0.00	20.9
37	0	-0	3991	0	0	0	1453	--	--	16.08	16.08	0.00	0.02	0.03	0.25	0.00	0.00	20.9
38	0	-0	15600	0	0	0	7085	--	--	16.08	16.08	0.00	0.12	0.13	0.98	0.00	0.00	20.9
39	0	-0	8399	0	0	0	3629	--	--	16.08	16.08	0.00	0.06	0.07	0.53	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	25	-0	6238	0	0	0	10866	--	--	16.08	16.08	0.00	0.19	0.05	0.39	0.00	0.00	20.9
2	25	-0	3886	0	0	0	6723	--	--	16.08	16.08	0.10	0.12	0.03	0.24	0.00	0.00	20.9
3	25	-0	3866	0	0	0	6687	--	--	16.08	16.08	0.10	0.12	0.03	0.24	0.00	0.00	20.9
4	25	-0	5731	0	0	0	10032	--	--	16.08	16.08	0.10	0.18	0.05	0.36	0.00	0.00	20.9
5	25	-0	5711	0	0	0	9995	--	--	16.08	16.08	0.10	0.18	0.05	0.36	0.00	0.00	20.9
6	25	-0	4556	0	0	0	7924	--	--	16.08	16.08	0.10	0.14	0.04	0.29	0.00	0.00	20.9
7	25	-0	4488	0	0	0	7803	--	--	16.08	16.08	0.10	0.14	0.04	0.28	0.00	0.00	20.9
8	25	-0	5109	0	0	0	8916	--	--	16.08	16.08	0.10	0.16	0.04	0.32	0.00	0.00	20.9
9	25	-0	5041	0	0	0	8794	--	--	16.08	16.08	0.10	0.16	0.04	0.32	0.00	0.00	20.9
10	25	-0	3886	0	0	0	6723	--	--	16.08	16.08	0.10	0.12	0.03	0.24	0.00	0.00	20.9
11	25	-0	3866	0	0	0	6687	--	--	16.08	16.08	0.10	0.12	0.03	0.24	0.00	0.00	20.9
12	25	-0	5731	0	0	0	10032	--	--	16.08	16.08	0.10	0.18	0.05	0.36	0.00	0.00	20.9
13	25	-0	5711	0	0	0	9995	--	--	16.08	16.08	0.10	0.18	0.05	0.36	0.00	0.00	20.9
14	25	-0	4556	0	0	0	7924	--	--	16.08	16.08	0.10	0.14	0.04	0.29	0.00	0.00	20.9
15	25	-0	4488	0	0	0	7803	--	--	16.08	16.08	0.10	0.14	0.04	0.28	0.00	0.00	20.9
16	25	-0	5109	0	0	0	8916	--	--	16.08	16.08	0.10	0.16	0.04	0.32	0.00	0.00	20.9
17	25	-0	5041	0	0	0	8794	--	--	16.08	16.08	0.10	0.16	0.04	0.32	0.00	0.00	20.9
18	25	-0	8028	0	0	0	13953	--	--	16.08	16.08	0.00	0.24	0.07	0.50	0.00	0.00	20.9
19	25	-0	14990	0	0	0	26513	--	--	16.08	16.08	0.00	0.45	0.12	0.94	0.00	0.00	20.9
20	25	-0	10670	0	0	0	18744	--	--	16.08	16.08	0.00	0.32	0.09	0.67	0.00	0.00	20.9
37	25	-0	3991	0	0	0	6716	--	--	16.08	16.08	0.00	0.11	0.03	0.25	0.00	0.00	20.9
38	25	-0	15600	0	0	0	27655	--	--	16.08	16.08	0.00	0.47	0.13	0.98	0.00	0.00	20.9
39	25	-0	8399	0	0	0	14705	--	--	16.08	16.08	0.00	0.25	0.07	0.53	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	50	-0	6238	0	0	0	5759	--	--	16.08	16.08	0.00	0.10	0.05	0.39	0.00	0.00	20.9
2	50	-0	3886	0	0	0	3541	--	--	16.08	16.08	0.10	0.06	0.03	0.24	0.00	0.00	20.9

3	50	-0	3866	0	0	0	3521	--	--	16.08	16.08	0.10	0.06	0.03	0.24	0.00	0.00	20.9
4	50	-0	5731	0	0	0	5339	--	--	16.08	16.08	0.10	0.09	0.05	0.36	0.00	0.00	20.9
5	50	-0	5711	0	0	0	5319	--	--	16.08	16.08	0.10	0.09	0.05	0.36	0.00	0.00	20.9
6	50	-0	4556	0	0	0	4194	--	--	16.08	16.08	0.10	0.07	0.04	0.29	0.00	0.00	20.9
7	50	-0	4488	0	0	0	4128	--	--	16.08	16.08	0.10	0.07	0.04	0.28	0.00	0.00	20.9
8	50	-0	5109	0	0	0	4733	--	--	16.08	16.08	0.10	0.08	0.04	0.32	0.00	0.00	20.9
9	50	-0	5041	0	0	0	4667	--	--	16.08	16.08	0.10	0.08	0.04	0.32	0.00	0.00	20.9
10	50	-0	3886	0	0	0	3541	--	--	16.08	16.08	0.10	0.06	0.03	0.24	0.00	0.00	20.9
11	50	-0	3866	0	0	0	3521	--	--	16.08	16.08	0.10	0.06	0.03	0.24	0.00	0.00	20.9
12	50	-0	5731	0	0	0	5339	--	--	16.08	16.08	0.10	0.09	0.05	0.36	0.00	0.00	20.9
13	50	-0	5711	0	0	0	5319	--	--	16.08	16.08	0.10	0.09	0.05	0.36	0.00	0.00	20.9
14	50	-0	4556	0	0	0	4194	--	--	16.08	16.08	0.10	0.07	0.04	0.29	0.00	0.00	20.9
15	50	-0	4488	0	0	0	4128	--	--	16.08	16.08	0.10	0.07	0.04	0.28	0.00	0.00	20.9
16	50	-0	5109	0	0	0	4733	--	--	16.08	16.08	0.10	0.08	0.04	0.32	0.00	0.00	20.9
17	50	-0	5041	0	0	0	4667	--	--	16.08	16.08	0.10	0.08	0.04	0.32	0.00	0.00	20.9
18	50	-0	8028	0	0	0	7380	--	--	16.08	16.08	0.00	0.13	0.07	0.50	0.00	0.00	20.9
19	50	-0	14990	0	0	0	14240	--	--	16.08	16.08	0.00	0.24	0.12	0.94	0.00	0.00	20.9
20	50	-0	10670	0	0	0	10010	--	--	16.08	16.08	0.00	0.17	0.09	0.67	0.00	0.00	20.9
37	50	-0	3991	0	0	0	3449	--	--	16.08	16.08	0.00	0.06	0.03	0.25	0.00	0.00	20.9
38	50	-0	15600	0	0	0	14880	--	--	16.08	16.08	0.00	0.25	0.13	0.98	0.00	0.00	20.9
39	50	-0	8399	0	0	0	7829	--	--	16.08	16.08	0.00	0.13	0.07	0.53	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 201 NI 1586 NF 1587 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	3908	0	0	0	686	--	--	16.08	16.08	0.00	0.01	0.03	0.25	0.00	0.00	20.9
2	0	-0	2381	0	0	0	407	--	--	16.08	16.08	0.10	0.01	0.02	0.15	0.00	0.00	20.9
3	0	-0	2367	0	0	0	405	--	--	16.08	16.08	0.10	0.01	0.02	0.15	0.00	0.00	20.9
4	0	-0	3645	0	0	0	651	--	--	16.08	16.08	0.10	0.01	0.03	0.23	0.00	0.00	20.9
5	0	-0	3631	0	0	0	648	--	--	16.08	16.08	0.10	0.01	0.03	0.23	0.00	0.00	20.9
6	0	-0	2840	0	0	0	496	--	--	16.08	16.08	0.10	0.01	0.02	0.18	0.00	0.00	20.9
7	0	-0	2794	0	0	0	487	--	--	16.08	16.08	0.10	0.01	0.02	0.18	0.00	0.00	20.9
8	0	-0	3219	0	0	0	569	--	--	16.08	16.08	0.10	0.01	0.03	0.20	0.00	0.00	20.9
9	0	-0	3173	0	0	0	560	--	--	16.08	16.08	0.10	0.01	0.03	0.20	0.00	0.00	20.9
10	0	-0	2381	0	0	0	407	--	--	16.08	16.08	0.10	0.01	0.02	0.15	0.00	0.00	20.9
11	0	-0	2367	0	0	0	405	--	--	16.08	16.08	0.10	0.01	0.02	0.15	0.00	0.00	20.9
12	0	-0	3645	0	0	0	651	--	--	16.08	16.08	0.10	0.01	0.03	0.23	0.00	0.00	20.9
13	0	-0	3631	0	0	0	648	--	--	16.08	16.08	0.10	0.01	0.03	0.23	0.00	0.00	20.9
14	0	-0	2840	0	0	0	496	--	--	16.08	16.08	0.10	0.01	0.02	0.18	0.00	0.00	20.9
15	0	-0	2794	0	0	0	487	--	--	16.08	16.08	0.10	0.01	0.02	0.18	0.00	0.00	20.9
16	0	-0	3219	0	0	0	569	--	--	16.08	16.08	0.10	0.01	0.03	0.20	0.00	0.00	20.9
17	0	-0	3173	0	0	0	560	--	--	16.08	16.08	0.10	0.01	0.03	0.20	0.00	0.00	20.9
18	0	-0	4993	0	0	0	869	--	--	16.08	16.08	0.00	0.01	0.04	0.31	0.00	0.00	20.9
19	0	-0	9849	0	0	0	1820	--	--	16.08	16.08	0.00	0.03	0.08	0.62	0.00	0.00	20.9
20	0	-0	6863	0	0	0	1240	--	--	16.08	16.08	0.00	0.02	0.06	0.43	0.00	0.00	20.9
37	0	-0	2231	0	0	0	338	--	--	16.08	16.08	0.00	0.01	0.02	0.14	0.00	0.00	20.9
38	0	-0	10320	0	0	0	1923	--	--	16.08	16.08	0.00	0.03	0.09	0.65	0.00	0.00	20.9
39	0	-0	5347	0	0	0	956	--	--	16.08	16.08	0.00	0.02	0.04	0.34	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	25	-0	3908	0	0	0	5840	--	--	16.08	16.08	0.00	0.10	0.03	0.25	0.00	0.00	20.9
2	25	-0	2381	0	0	0	3547	--	--	16.08	16.08	0.10	0.06	0.02	0.15	0.00	0.00	20.9
3	25	-0	2367	0	0	0	3527	--	--	16.08	16.08	0.10	0.06	0.02	0.15	0.00	0.00	20.9
4	25	-0	3645	0	0	0	5458	--	--	16.08	16.08	0.10	0.10	0.03	0.23	0.00	0.00	20.9
5	25	-0	3631	0	0	0	5437	--	--	16.08	16.08	0.10	0.10	0.03	0.23	0.00	0.00	20.9
6	25	-0	2840	0	0	0	4241	--	--	16.08	16.08	0.10	0.08	0.02	0.18	0.00	0.00	20.9
7	25	-0	2794	0	0	0	4172	--	--	16.08	16.08	0.10	0.07	0.02	0.18	0.00	0.00	20.9
8	25	-0	3219	0	0	0	4814	--	--	16.08	16.08	0.10	0.09	0.03	0.20	0.00	0.00	20.9
9	25	-0	3173	0	0	0	4744	--	--	16.08	16.08	0.10	0.08	0.03	0.20	0.00	0.00	20.9
10	25	-0	2381	0	0	0	3547	--	--	16.08	16.08	0.10	0.06	0.02	0.15	0.00	0.00	20.9
11	25	-0	2367	0	0	0	3527	--	--	16.08	16.08	0.10	0.06	0.02	0.15	0.00	0.00	20.9
12	25	-0	3645	0	0	0	5458	--	--	16.08	16.08	0.10	0.10	0.03	0.23	0.00	0.00	20.9
13	25	-0	3631	0	0	0	5437	--	--	16.08	16.08	0.10	0.10	0.03	0.23	0.00	0.00	20.9
14	25	-0	2840	0	0	0	4241	--	--	16.08	16.08	0.10	0.08	0.02	0.18	0.00	0.00	20.9
15	25	-0	2794	0	0	0	4172	--	--	16.08	16.08	0.10	0.07	0.02	0.18	0.00	0.00	20.9
16	25	-0	3219	0	0	0	4814	--	--	16.08	16.08	0.10	0.09	0.03	0.20	0.00	0.00	20.9
17	25	-0	3173	0	0	0	4744	--	--	16.08	16.08	0.10	0.08	0.03	0.20	0.00	0.00	20.9
18	25	-0	4993	0	0	0	7454	--	--	16.08	16.08	0.00	0.13	0.04	0.31	0.00	0.00	20.9
19	25	-0	9849	0	0	0	14809	--	--	16.08	16.08	0.00	0.25	0.08	0.62	0.00	0.00	20.9
20	25	-0	6863	0	0	0	10290	--	--	16.08	16.08	0.00	0.18	0.06	0.43	0.00	0.00	20.9
37	25	-0	2231	0	0	0	3280	--	--	16.08	16.08	0.00	0.06	0.02	0.14	0.00	0.00	20.9
38	25	-0	10320	0	0	0	15534	--	--	16.08	16.08	0.00	0.26	0.09	0.65	0.00	0.00	20.9
39	25	-0	5347	0	0	0	8007	--	--	16.08	16.08	0.00	0.14	0.04	0.34	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	50	-0	3908	0	0	0	2640	--	--	16.08	16.08	0.00	0.05	0.03	0.25	0.00	0.00	20.9
2	50	-0	2381	0	0	0	1598	--	--	16.08	16.08	0.10	0.03	0.02	0.15	0.00	0.00	20.9
3	50	-0	2367	0	0	0	1589	--	--	16.08	16.08	0.10	0.03	0.02	0.15	0.00	0.00	20.9
4	50	-0	3645	0	0	0	2474	--	--	16.08	16.08	0.10	0.04	0.03	0.23	0.00	0.00	20.9
5	50	-0	3631	0	0	0	2464	--	--	16.08	16.08	0.10	0.04	0.03	0.23	0.00	0.00	20.9
6	50	-0	2840	0	0	0	1916	--	--	16.08	16.08	0.10	0.03	0.02	0.18	0.00	0.00	20.9
7	50	-0	2794	0	0	0	1884	--	--	16.08	16.08	0.10	0.03	0.02	0.18	0.00	0.00	20.9
8	50	-0	3219	0	0	0	2178	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
9	50	-0	3173	0	0	0	2146	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
10	50	-0	2381	0	0	0	1598	--	--	16.08	16.08	0.10	0.03	0.02	0.15	0.00	0.00	20.9
11	50	-0	2367	0	0	0	1589	--	--	16.08	16.08	0.10	0.03	0.02	0.15	0.00	0.00	20.9
12	50	-0	3645	0	0	0	2474	--	--	16.08	16.08	0.10	0.04	0.03	0.23	0.00	0.00	20.9
13	50	-0	3631	0	0	0	2464	--	--	16.08	16.08	0.10	0.04	0.03	0.23	0.00	0.00	20.9
14	50	-0	2840	0	0	0	1916	--	--	16.08	16.08	0.10	0.03	0.02	0.18	0.00	0.00	20.9
15	50	-0	2794	0	0	0	1884	--	--	16.08	16.08	0.10	0.03	0.02	0.18	0.00	0.00	20.9
16	50	-0	3219	0	0	0	2178	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
17	50	-0	3173	0	0	0	2146	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
18	50	-0	4993	0	0	0	3366	--	--	16.08	16.08	0.00	0.06	0.04	0.31	0.00	0.00	20.9
19	50	-0	9849	0	0	0	6745	--	--	16.08	16.08	0.00	0.11	0.08	0.62	0.00	0.00	20.9
20	50	-0	6863	0	0	0	4671	--	--	16.08	16.08	0.00	0.08	0.06	0.43	0.00	0.00	20.9
37	50	-0	2231	0	0	0	1453	--	--	16.08	16.08	0.00	0.02	0.02	0.14	0.00	0.00	20.9
38	50	-0	10320	0	0	0	7085	--	--	16.08	16.08	0.00	0.12	0.09	0.65	0.00	0.00	20.9
39	50	-0	5347	0	0	0	3629	--	--	16.08	16.08	0.00	0.06	0.04	0.34	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 202 NI 1585 NF 1586 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	1372	0	0	0	-1466	--	--	16.08	16.08	0.18	0.02	0.01	0.09	0.00	0.00	20.9
2	0	-0	815	0	0	0	-871	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
3	0	-0	810	0	0	0	-865	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
4	0	-0	1302	0	0	0	-1392	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
5	0	-0	1297	0	0	0	-1386	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
6	0	-0	992	0	0	0	-1060	--	--	16.08	16.08	0.29	0.02	0.01	0.06	0.00	0.00	20.9
7	0	-0	974	0	0	0	-1041	--	--	16.08	16.08	0.29	0.02	0.01	0.06	0.00	0.00	20.9
8	0	-0	1138	0	0	0	-1216	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
9	0	-0	1120	0	0	0	-1197	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
10	0	-0	815	0	0	0	-871	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
11	0	-0	810	0	0	0	-865	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
12	0	-0	1302	0	0	0	-1392	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
13	0	-0	1297	0	0	0	-1386	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
14	0	-0	992	0	0	0	-1060	--	--	16.08	16.08	0.29	0.02	0.01	0.06	0.00	0.00	20.9
15	0	-0	974	0	0	0	-1041	--	--	16.08	16.08	0.29	0.02	0.01	0.06	0.00	0.00	20.9
16	0	-0	1138	0	0	0	-1216	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
17	0	-0	1120	0	0	0	-1197	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
18	0	-0	1738	0	0	0	-1857	--	--	16.08	16.08	0.18	0.03	0.01	0.11	0.00	0.00	20.9
19	0	-0	3640	0	0	0	-3890	--	--	16.08	16.08	0.18	0.06	0.03	0.23	0.00	0.00	20.9
20	0	-0	2480	0	0	0	-2650	--	--	16.08	16.08	0.18	0.04	0.02	0.16	0.00	0.00	20.9
37	0	-0	676	0	0	0	-722	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
38	0	-0	3845	0	0	0	-4109	--	--	16.08	16.08	0.18	0.07	0.03	0.24	0.00	0.00	20.9
39	0	-0	1911	0	0	0	-2042	--	--	16.08	16.08	0.18	0.03	0.02	0.12	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	25	-0	1372	0	0	0	1809	--	--	16.08	16.08	0.00	0.03	0.01	0.09	0.00	0.00	20.9
2	25	-0	815	0	0	0	1075	--	--	16.08	16.08	0.10	0.02	0.01	0.05	0.00	0.00	20.9
3	25	-0	810	0	0	0	1068	--	--	16.08	16.08	0.10	0.02	0.01	0.05	0.00	0.00	20.9
4	25	-0	1302	0	0	0	1717	--	--	16.08	16.08	0.10	0.03	0.01	0.08	0.00	0.00	20.9
5	25	-0	1297	0	0	0	1710	--	--	16.08	16.08	0.10	0.03	0.01	0.08	0.00	0.00	20.9
6	25	-0	992	0	0	0	1308	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9
7	25	-0	974	0	0	0	1284	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9
8	25	-0	1138	0	0	0	1501	--	--	16.08	16.08	0.10	0.03	0.01	0.07	0.00	0.00	20.9
9	25	-0	1120	0	0	0	1477	--	--	16.08	16.08	0.10	0.03	0.01	0.07	0.00	0.00	20.9
10	25	-0	815	0	0	0	1075	--	--	16.08	16.08	0.10	0.02	0.01	0.05	0.00	0.00	20.9
11	25	-0	810	0	0	0	1068	--	--	16.08	16.08	0.10	0.02	0.01	0.05	0.00	0.00	20.9
12	25	-0	1302	0	0	0	1717	--	--	16.08	16.08	0.10	0.03	0.01	0.08	0.00	0.00	20.9
13	25	-0	1297	0	0	0	1710	--	--	16.08	16.08	0.10	0.03	0.01	0.08	0.00	0.00	20.9
14	25	-0	992	0	0	0	1308	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9
15	25	-0	974	0	0	0	1284	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9
16	25	-0	1138	0	0	0	1501	--	--	16.08	16.08	0.10	0.03	0.01	0.07	0.00	0.00	20.9
17	25	-0	1120	0	0	0	1477	--	--	16.08	16.08	0.10	0.03	0.01	0.07	0.00	0.00	20.9
18	25	-0	1738	0	0	0	2292	--	--	16.08	16.08	0.00	0.04	0.01	0.11	0.00	0.00	20.9
19	25	-0	3640	0	0	0	4800	--	--	16.08	16.08	0.00	0.08	0.03	0.23	0.00	0.00	20.9
20	25	-0	2480	0	0	0	3270	--	--	16.08	16.08	0.00	0.06	0.02	0.16	0.00	0.00	20.9
37	25	-0	676	0	0	0	891	--	--	16.08	16.08	0.00	0.02	0.01	0.04	0.00	0.00	20.9
38	25	-0	3845	0	0	0	5071	--	--	16.08	16.08	0.00	0.09	0.03	0.24	0.00	0.00	20.9
39	25	-0	1911	0	0	0	2520	--	--	16.08	16.08	0.00	0.04	0.02	0.12	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	50	-0	1372	0	0	0	686	--	--	16.08	16.08	0.00	0.01	0.01	0.09	0.00	0.00	20.9
2	50	-0	815	0	0	0	407	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
3	50	-0	810	0	0	0	405	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
4	50	-0	1302	0	0	0	651	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
5	50	-0	1297	0	0	0	648	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
6	50	-0	992	0	0	0	496	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
7	50	-0	974	0	0	0	487	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
8	50	-0	1138	0	0	0	569	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
9	50	-0	1120	0	0	0	560	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
10	50	-0	815	0	0	0	407	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
11	50	-0	810	0	0	0	405	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
12	50	-0	1302	0	0	0	651	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
13	50	-0	1297	0	0	0	648	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
14	50	-0	992	0	0	0	496	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
15	50	-0	974	0	0	0	487	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
16	50	-0	1138	0	0	0	569	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
17	50	-0	1120	0	0	0	560	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
18	50	-0	1738	0	0	0	869	--	--	16.08	16.08	0.00	0.01	0.01	0.11	0.00	0.00	20.9
19	50	-0	3640	0	0	0	1820	--	--	16.08	16.08	0.00	0.03	0.03	0.23	0.00	0.00	20.9
20	50	-0	2480	0	0	0	1240	--	--	16.08	16.08	0.00	0.02	0.02	0.16	0.00	0.00	20.9
37	50	-0	676	0	0	0	338	--	--	16.08	16.08	0.00	0.01	0.01	0.04	0.00	0.00	20.9
38	50	-0	3845	0	0	0	1923	--	--	16.08	16.08	0.00	0.03	0.03	0.24	0.00	0.00	20.9
39	50	-0	1911	0	0	0	956	--	--	16.08	16.08	0.00	0.02	0.02	0.12	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 203 NI 1685 NF 1690 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-664	0	0	0	133	--	--	16.08	16.08	0.00	0.00	0.01	0.04	0.00	0.00	20.9
2	0	-0	-546	0	0	0	109	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
3	0	-0	-547	0	0	0	109	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
4	0	-0	-475	0	0	0	95	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
5	0	-0	-475	0	0	0	95	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
6	0	-0	-521	0	0	0	104	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
7	0	-0	-522	0	0	0	104	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
8	0	-0	-500	0	0	0	100	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
9	0	-0	-500	0	0	0	100	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
10	0	-0	-546	0	0	0	109	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9

11	0	-0	-547	0	0	0	109	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
12	0	-0	-475	0	0	0	95	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
13	0	-0	-475	0	0	0	95	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
14	0	-0	-521	0	0	0	104	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
15	0	-0	-522	0	0	0	104	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
16	0	-0	-500	0	0	0	100	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
17	0	-0	-500	0	0	0	100	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
18	0	-0	-1131	0	0	0	226	--	--	16.08	16.08	0.00	0.00	0.01	0.07	0.00	0.00	20.9
19	0	-0	-858	0	0	0	172	--	--	16.08	16.08	0.00	0.00	0.01	0.05	0.00	0.00	20.9
20	0	-0	-946	0	0	0	189	--	--	16.08	16.08	0.00	0.00	0.01	0.06	0.00	0.00	20.9
37	0	-0	-1115	0	0	0	223	--	--	16.08	16.08	0.00	0.00	0.01	0.07	0.00	0.00	20.9
38	0	-0	-660	0	0	0	132	--	--	16.08	16.08	0.00	0.00	0.01	0.04	0.00	0.00	20.9
39	0	-0	-806	0	0	0	161	--	--	16.08	16.08	0.00	0.00	0.01	0.05	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	10	-0	-664	0	0	0	133	--	--	16.08	16.08	0.00	0.00	0.01	0.04	0.00	0.00	20.9
2	10	-0	-546	0	0	0	109	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
3	10	-0	-547	0	0	0	109	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
4	10	-0	-475	0	0	0	95	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
5	10	-0	-475	0	0	0	95	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
6	10	-0	-521	0	0	0	104	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
7	10	-0	-522	0	0	0	104	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
8	10	-0	-500	0	0	0	100	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
9	10	-0	-500	0	0	0	100	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
10	10	-0	-546	0	0	0	109	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
11	10	-0	-547	0	0	0	109	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
12	10	-0	-475	0	0	0	95	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
13	10	-0	-475	0	0	0	95	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
14	10	-0	-521	0	0	0	104	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
15	10	-0	-522	0	0	0	104	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
16	10	-0	-500	0	0	0	100	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
17	10	-0	-500	0	0	0	100	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
18	10	-0	-1131	0	0	0	226	--	--	16.08	16.08	0.00	0.00	0.01	0.07	0.00	0.00	20.9
19	10	-0	-858	0	0	0	172	--	--	16.08	16.08	0.00	0.00	0.01	0.05	0.00	0.00	20.9
20	10	-0	-946	0	0	0	189	--	--	16.08	16.08	0.00	0.00	0.01	0.06	0.00	0.00	20.9
37	10	-0	-1115	0	0	0	223	--	--	16.08	16.08	0.00	0.00	0.01	0.07	0.00	0.00	20.9
38	10	-0	-660	0	0	0	132	--	--	16.08	16.08	0.00	0.00	0.01	0.04	0.00	0.00	20.9
39	10	-0	-806	0	0	0	161	--	--	16.08	16.08	0.00	0.00	0.01	0.05	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	20	-0	-664	0	0	0	-709	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
2	20	-0	-546	0	0	0	-584	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
3	20	-0	-547	0	0	0	-584	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
4	20	-0	-475	0	0	0	-507	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
5	20	-0	-475	0	0	0	-507	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
6	20	-0	-521	0	0	0	-557	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
7	20	-0	-522	0	0	0	-558	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
8	20	-0	-500	0	0	0	-534	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
9	20	-0	-500	0	0	0	-535	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
10	20	-0	-546	0	0	0	-584	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
11	20	-0	-547	0	0	0	-584	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
12	20	-0	-475	0	0	0	-507	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
13	20	-0	-475	0	0	0	-507	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
14	20	-0	-521	0	0	0	-557	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
15	20	-0	-522	0	0	0	-558	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
16	20	-0	-500	0	0	0	-534	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
17	20	-0	-500	0	0	0	-535	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
18	20	-0	-1131	0	0	0	-1209	--	--	16.08	16.08	0.18	0.02	0.01	0.07	0.00	0.00	20.9
19	20	-0	-858	0	0	0	-917	--	--	16.08	16.08	0.18	0.02	0.01	0.05	0.00	0.00	20.9
20	20	-0	-946	0	0	0	-1011	--	--	16.08	16.08	0.18	0.02	0.01	0.06	0.00	0.00	20.9
37	20	-0	-1115	0	0	0	-1192	--	--	16.08	16.08	0.18	0.02	0.01	0.07	0.00	0.00	20.9
38	20	-0	-660	0	0	0	-705	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
39	20	-0	-806	0	0	0	-862	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 204 NI 1686 NF 1685 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-8612	0	0	0	3228	--	--	16.08	16.08	0.00	0.06	0.07	0.54	0.00	0.00	20.9
2	0	-0	-6556	0	0	0	2646	--	--	16.08	16.08	0.10	0.05	0.05	0.41	0.00	0.00	20.9
3	0	-0	-6550	0	0	0	2653	--	--	16.08	16.08	0.10	0.05	0.05	0.41	0.00	0.00	20.9
4	0	-0	-6699	0	0	0	2314	--	--	16.08	16.08	0.10	0.04	0.06	0.42	0.00	0.00	20.9
5	0	-0	-6693	0	0	0	2321	--	--	16.08	16.08	0.10	0.04	0.06	0.42	0.00	0.00	20.9
6	0	-0	-6614	0	0	0	2522	--	--	16.08	16.08	0.10	0.04	0.05	0.41	0.00	0.00	20.9
7	0	-0	-6593	0	0	0	2545	--	--	16.08	16.08	0.10	0.05	0.05	0.41	0.00	0.00	20.9
8	0	-0	-6656	0	0	0	2422	--	--	16.08	16.08	0.10	0.04	0.05	0.42	0.00	0.00	20.9
9	0	-0	-6636	0	0	0	2445	--	--	16.08	16.08	0.10	0.04	0.05	0.42	0.00	0.00	20.9
10	0	-0	-6556	0	0	0	2646	--	--	16.08	16.08	0.10	0.05	0.05	0.41	0.00	0.00	20.9
11	0	-0	-6550	0	0	0	2653	--	--	16.08	16.08	0.10	0.05	0.05	0.41	0.00	0.00	20.9
12	0	-0	-6699	0	0	0	2314	--	--	16.08	16.08	0.10	0.04	0.06	0.42	0.00	0.00	20.9
13	0	-0	-6693	0	0	0	2321	--	--	16.08	16.08	0.10	0.04	0.06	0.42	0.00	0.00	20.9
14	0	-0	-6614	0	0	0	2522	--	--	16.08	16.08	0.10	0.04	0.05	0.41	0.00	0.00	20.9
15	0	-0	-6593	0	0	0	2545	--	--	16.08	16.08	0.10	0.05	0.05	0.41	0.00	0.00	20.9
16	0	-0	-6656	0	0	0	2422	--	--	16.08	16.08	0.10	0.04	0.05	0.42	0.00	0.00	20.9
17	0	-0	-6636	0	0	0	2445	--	--	16.08	16.08	0.10	0.04	0.05	0.42	0.00	0.00	20.9
18	0	-0	-9874	0	0	0	5563	--	--	16.08	16.08	0.00	0.09	0.08	0.62	0.00	0.00	20.9
19	0	-0	-11250	0	0	0	4314	--	--	16.08	16.08	0.00	0.07	0.09	0.71	0.00	0.00	20.9
20	0	-0	-10240	0	0	0	4699	--	--	16.08	16.08	0.00	0.08	0.08	0.64	0.00	0.00	20.9
37	0	-0	-8791	0	0	0	5425	--	--	16.08	16.08	0.00	0.09	0.07	0.55	0.00	0.00	20.9
38	0	-0	-11080	0	0	0	3343	--	--	16.08	16.08	0.00	0.06	0.09	0.70	0.00	0.00	20.9
39	0	-0	-9409	0	0	0	3985	--	--	16.08	16.08	0.00	0.07	0.08	0.59	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	10	-0	-8612	0	0	0	3228	--	--	16.08	16.08	0.00	0.06	0.07	0.54	0.00	0.00	20.9
2	10	-0	-6556	0	0	0	2646	--	--	16.08	16.08	0.10	0.05	0.05	0.41	0.00	0.00	20.9
3	10	-0	-6550	0	0	0	2653	--	--	16.08	16.08	0.10	0.05	0.05	0.41	0.00	0.00	20.9
4	10	-0	-6699	0	0	0	2314	--	--	16.08	16.08	0.10	0.04	0.06	0.42	0.00	0.00	20.9
5	10	-0	-6693	0	0	0	2321	--	--	16.08	16.08	0.10	0.04	0.06	0.42	0.00	0.00	20.9
6	10	-0	-6614	0	0	0	2522	--	--	16.08	16.08	0.10	0.04	0.05	0.41	0.00	0.00	20.9

7	10	-0	-6593	0	0	0	2545	--	--	16.08	16.08	0.10	0.05	0.05	0.41	0.00	0.00	20.9
8	10	-0	-6656	0	0	0	2422	--	--	16.08	16.08	0.10	0.04	0.05	0.42	0.00	0.00	20.9
9	10	-0	-6636	0	0	0	2445	--	--	16.08	16.08	0.10	0.04	0.05	0.42	0.00	0.00	20.9
10	10	-0	-6556	0	0	0	2646	--	--	16.08	16.08	0.10	0.05	0.05	0.41	0.00	0.00	20.9
11	10	-0	-6550	0	0	0	2653	--	--	16.08	16.08	0.10	0.05	0.05	0.41	0.00	0.00	20.9
12	10	-0	-6699	0	0	0	2314	--	--	16.08	16.08	0.10	0.04	0.06	0.42	0.00	0.00	20.9
13	10	-0	-6693	0	0	0	2321	--	--	16.08	16.08	0.10	0.04	0.06	0.42	0.00	0.00	20.9
14	10	-0	-6614	0	0	0	2522	--	--	16.08	16.08	0.10	0.04	0.05	0.41	0.00	0.00	20.9
15	10	-0	-6593	0	0	0	2545	--	--	16.08	16.08	0.10	0.05	0.05	0.41	0.00	0.00	20.9
16	10	-0	-6656	0	0	0	2422	--	--	16.08	16.08	0.10	0.04	0.05	0.42	0.00	0.00	20.9
17	10	-0	-6636	0	0	0	2445	--	--	16.08	16.08	0.10	0.04	0.05	0.42	0.00	0.00	20.9
18	10	-0	-9874	0	0	0	5563	--	--	16.08	16.08	0.00	0.09	0.08	0.62	0.00	0.00	20.9
19	10	-0	-11250	0	0	0	4314	--	--	16.08	16.08	0.00	0.07	0.09	0.71	0.00	0.00	20.9
20	10	-0	-10240	0	0	0	4699	--	--	16.08	16.08	0.00	0.08	0.08	0.64	0.00	0.00	20.9
37	10	-0	-8791	0	0	0	5425	--	--	16.08	16.08	0.00	0.09	0.07	0.55	0.00	0.00	20.9
38	10	-0	-11080	0	0	0	3343	--	--	16.08	16.08	0.00	0.06	0.09	0.70	0.00	0.00	20.9
39	10	-0	-9409	0	0	0	3985	--	--	16.08	16.08	0.00	0.07	0.08	0.59	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	20	-0	-8612	0	0	0	1506	--	--	16.08	16.08	0.00	0.03	0.07	0.54	0.00	0.00	20.9
2	20	-0	-6556	0	0	0	1335	--	--	16.08	16.08	0.10	0.02	0.05	0.41	0.00	0.00	20.9
3	20	-0	-6550	0	0	0	1343	--	--	16.08	16.08	0.10	0.02	0.05	0.41	0.00	0.00	20.9
4	20	-0	-6699	0	0	0	974	--	--	16.08	16.08	0.10	0.02	0.06	0.42	0.00	0.00	20.9
5	20	-0	-6693	0	0	0	982	--	--	16.08	16.08	0.10	0.02	0.06	0.42	0.00	0.00	20.9
6	20	-0	-6614	0	0	0	1199	--	--	16.08	16.08	0.10	0.02	0.05	0.41	0.00	0.00	20.9
7	20	-0	-6593	0	0	0	1226	--	--	16.08	16.08	0.10	0.02	0.05	0.41	0.00	0.00	20.9
8	20	-0	-6656	0	0	0	1091	--	--	16.08	16.08	0.10	0.02	0.05	0.42	0.00	0.00	20.9
9	20	-0	-6636	0	0	0	1118	--	--	16.08	16.08	0.10	0.02	0.05	0.42	0.00	0.00	20.9
10	20	-0	-6556	0	0	0	1335	--	--	16.08	16.08	0.10	0.02	0.05	0.41	0.00	0.00	20.9
11	20	-0	-6550	0	0	0	1343	--	--	16.08	16.08	0.10	0.02	0.05	0.41	0.00	0.00	20.9
12	20	-0	-6699	0	0	0	974	--	--	16.08	16.08	0.10	0.02	0.06	0.42	0.00	0.00	20.9
13	20	-0	-6693	0	0	0	982	--	--	16.08	16.08	0.10	0.02	0.06	0.42	0.00	0.00	20.9
14	20	-0	-6614	0	0	0	1199	--	--	16.08	16.08	0.10	0.02	0.05	0.41	0.00	0.00	20.9
15	20	-0	-6593	0	0	0	1226	--	--	16.08	16.08	0.10	0.02	0.05	0.41	0.00	0.00	20.9
16	20	-0	-6656	0	0	0	1091	--	--	16.08	16.08	0.10	0.02	0.05	0.42	0.00	0.00	20.9
17	20	-0	-6636	0	0	0	1118	--	--	16.08	16.08	0.10	0.02	0.05	0.42	0.00	0.00	20.9
18	20	-0	-9874	0	0	0	3588	--	--	16.08	16.08	0.00	0.06	0.08	0.62	0.00	0.00	20.9
19	20	-0	-11250	0	0	0	2064	--	--	16.08	16.08	0.00	0.04	0.09	0.71	0.00	0.00	20.9
20	20	-0	-10240	0	0	0	2650	--	--	16.08	16.08	0.00	0.05	0.08	0.64	0.00	0.00	20.9
37	20	-0	-8791	0	0	0	3666	--	--	16.08	16.08	0.00	0.06	0.07	0.55	0.00	0.00	20.9
38	20	-0	-11080	0	0	0	1126	--	--	16.08	16.08	0.00	0.02	0.09	0.70	0.00	0.00	20.9
39	20	-0	-9409	0	0	0	2103	--	--	16.08	16.08	0.00	0.04	0.08	0.59	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 205 NI 1687 NF 1686 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-2890	0	0	0	-3424	--	--	16.08	16.08	0.18	0.06	0.02	0.18	0.00	0.00	20.9
2	0	-0	-3265	0	0	0	-3653	--	--	16.08	16.08	0.29	0.06	0.03	0.20	0.00	0.00	20.9
3	0	-0	-3250	0	0	0	-3640	--	--	16.08	16.08	0.29	0.06	0.03	0.20	0.00	0.00	20.9
4	0	-0	-1196	0	0	0	-1628	--	--	16.08	16.08	0.29	0.03	0.01	0.08	0.00	0.00	20.9
5	0	-0	-1181	0	0	0	-1614	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
6	0	-0	-2558	0	0	0	-2961	--	--	16.08	16.08	0.29	0.05	0.02	0.16	0.00	0.00	20.9
7	0	-0	-2509	0	0	0	-2915	--	--	16.08	16.08	0.29	0.05	0.02	0.16	0.00	0.00	20.9
8	0	-0	-1938	0	0	0	-2353	--	--	16.08	16.08	0.29	0.04	0.02	0.12	0.00	0.00	20.9
9	0	-0	-1888	0	0	0	-2307	--	--	16.08	16.08	0.29	0.04	0.02	0.12	0.00	0.00	20.9
10	0	-0	-3265	0	0	0	-3653	--	--	16.08	16.08	0.29	0.06	0.03	0.20	0.00	0.00	20.9
11	0	-0	-3250	0	0	0	-3640	--	--	16.08	16.08	0.29	0.06	0.03	0.20	0.00	0.00	20.9
12	0	-0	-1196	0	0	0	-1628	--	--	16.08	16.08	0.29	0.03	0.01	0.08	0.00	0.00	20.9
13	0	-0	-1181	0	0	0	-1614	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
14	0	-0	-2558	0	0	0	-2961	--	--	16.08	16.08	0.29	0.05	0.02	0.16	0.00	0.00	20.9
15	0	-0	-2509	0	0	0	-2915	--	--	16.08	16.08	0.29	0.05	0.02	0.16	0.00	0.00	20.9
16	0	-0	-1938	0	0	0	-2353	--	--	16.08	16.08	0.29	0.04	0.02	0.12	0.00	0.00	20.9
17	0	-0	-1888	0	0	0	-2307	--	--	16.08	16.08	0.29	0.04	0.02	0.12	0.00	0.00	20.9
18	0	-0	-13520	0	0	0	-13940	--	--	16.08	16.08	0.18	0.23	0.11	0.85	0.00	0.00	20.9
19	0	-0	-3714	0	0	0	-4405	--	--	16.08	16.08	0.18	0.07	0.03	0.23	0.00	0.00	20.9
20	0	-0	-7746	0	0	0	-8298	--	--	16.08	16.08	0.18	0.14	0.06	0.49	0.00	0.00	20.9
37	0	-0	-14920	0	0	0	-15230	--	--	16.08	16.08	0.18	0.25	0.12	0.94	0.00	0.00	20.9
38	0	-0	1435	0	0	0	-60	--	--	16.08	16.08	0.18	0.00	0.01	0.09	0.00	0.00	20.9
39	0	-0	-5285	0	0	0	-5832	--	--	16.08	16.08	0.18	0.10	0.04	0.33	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	25	-0	-2890	0	0	0	-3424	--	--	16.08	16.08	0.18	0.06	0.02	0.18	0.00	0.00	20.9
2	25	-0	-3265	0	0	0	-3653	--	--	16.08	16.08	0.29	0.06	0.03	0.20	0.00	0.00	20.9
3	25	-0	-3250	0	0	0	-3640	--	--	16.08	16.08	0.29	0.06	0.03	0.20	0.00	0.00	20.9
4	25	-0	-1196	0	0	0	-1628	--	--	16.08	16.08	0.29	0.03	0.01	0.08	0.00	0.00	20.9
5	25	-0	-1181	0	0	0	-1614	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
6	25	-0	-2558	0	0	0	-2961	--	--	16.08	16.08	0.29	0.05	0.02	0.16	0.00	0.00	20.9
7	25	-0	-2509	0	0	0	-2915	--	--	16.08	16.08	0.29	0.05	0.02	0.16	0.00	0.00	20.9
8	25	-0	-1938	0	0	0	-2353	--	--	16.08	16.08	0.29	0.04	0.02	0.12	0.00	0.00	20.9
9	25	-0	-1888	0	0	0	-2307	--	--	16.08	16.08	0.29	0.04	0.02	0.12	0.00	0.00	20.9
10	25	-0	-3265	0	0	0	-3653	--	--	16.08	16.08	0.29	0.06	0.03	0.20	0.00	0.00	20.9
11	25	-0	-3250	0	0	0	-3640	--	--	16.08	16.08	0.29	0.06	0.03	0.20	0.00	0.00	20.9
12	25	-0	-1196	0	0	0	-1628	--	--	16.08	16.08	0.29	0.03	0.01	0.08	0.00	0.00	20.9
13	25	-0	-1181	0	0	0	-1614	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
14	25	-0	-2558	0	0	0	-2961	--	--	16.08	16.08	0.29	0.05	0.02	0.16	0.00	0.00	20.9
15	25	-0	-2509	0	0	0	-2915	--	--	16.08	16.08	0.29	0.05	0.02	0.16	0.00	0.00	20.9
16	25	-0	-1938	0	0	0	-2353	--	--	16.08	16.08	0.29	0.04	0.02	0.12	0.00	0.00	20.9
17	25	-0	-1888	0	0	0	-2307	--	--	16.08	16.08	0.29	0.04	0.02	0.12	0.00	0.00	20.9
18	25	-0	-13520	0	0	0	-13940	--	--	16.08	16.08	0.18	0.23	0.11	0.85	0.00	0.00	20.9
19	25	-0	-3714	0	0	0	-4405	--	--	16.08	16.08	0.18	0.07	0.03	0.23	0.00	0.00	20.9
20	25	-0	-7746	0	0	0	-8298	--	--	16.08	16.08	0.18	0.14	0.06	0.49	0.00	0.00	20.9
37	25	-0	-14920	0	0	0	-15230	--	--	16.08	16.08	0.18	0.25	0.12	0.94	0.00	0.00	20.9
38	25	-0	1435	0	0	0	1832	--	--	16.08	16.08	0.00	0.03	0.01	0.09	0.00	0.00	20.9
39	25	-0	-5285	0	0	0	-5832	--	--	16.08	16.08	0.18	0.10	0.04	0.33	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	50	-0	-2890	0	0	0	-3424	--	--	16.08	16.08	0.18	0.06	0.02	0.18	0.00	0.00	20.9
2	50	-0	-3265	0	0	0	-3653	--	--	16.08	16.08	0.29	0.06	0.03	0.20	0.00	0.00	20.9

3	50	-0	-3250	0	0	0	-3640	--	--	16.08	16.08	0.29	0.06	0.03	0.20	0.00	0.00	20.9
4	50	-0	-1196	0	0	0	-1628	--	--	16.08	16.08	0.29	0.03	0.01	0.08	0.00	0.00	20.9
5	50	-0	-1181	0	0	0	-1614	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
6	50	-0	-2558	0	0	0	-2961	--	--	16.08	16.08	0.29	0.05	0.02	0.16	0.00	0.00	20.9
7	50	-0	-2509	0	0	0	-2915	--	--	16.08	16.08	0.29	0.05	0.02	0.16	0.00	0.00	20.9
8	50	-0	-1938	0	0	0	-2353	--	--	16.08	16.08	0.29	0.04	0.02	0.12	0.00	0.00	20.9
9	50	-0	-1888	0	0	0	-2307	--	--	16.08	16.08	0.29	0.04	0.02	0.12	0.00	0.00	20.9
10	50	-0	-3265	0	0	0	-3653	--	--	16.08	16.08	0.29	0.06	0.03	0.20	0.00	0.00	20.9
11	50	-0	-3250	0	0	0	-3640	--	--	16.08	16.08	0.29	0.06	0.03	0.20	0.00	0.00	20.9
12	50	-0	-1196	0	0	0	-1628	--	--	16.08	16.08	0.29	0.03	0.01	0.08	0.00	0.00	20.9
13	50	-0	-1181	0	0	0	-1614	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
14	50	-0	-2558	0	0	0	-2961	--	--	16.08	16.08	0.29	0.05	0.02	0.16	0.00	0.00	20.9
15	50	-0	-2509	0	0	0	-2915	--	--	16.08	16.08	0.29	0.05	0.02	0.16	0.00	0.00	20.9
16	50	-0	-1938	0	0	0	-2353	--	--	16.08	16.08	0.29	0.04	0.02	0.12	0.00	0.00	20.9
17	50	-0	-1888	0	0	0	-2307	--	--	16.08	16.08	0.29	0.04	0.02	0.12	0.00	0.00	20.9
18	50	-0	-13520	0	0	0	-13940	--	--	16.08	16.08	0.18	0.23	0.11	0.85	0.00	0.00	20.9
19	50	-0	-3714	0	0	0	-4405	--	--	16.08	16.08	0.18	0.07	0.03	0.23	0.00	0.00	20.9
20	50	-0	-7746	0	0	0	-8298	--	--	16.08	16.08	0.18	0.14	0.06	0.49	0.00	0.00	20.9
37	50	-0	-14920	0	0	0	-15230	--	--	16.08	16.08	0.18	0.25	0.12	0.94	0.00	0.00	20.9
38	50	-0	1435	0	0	0	657	--	--	16.08	16.08	0.00	0.01	0.01	0.09	0.00	0.00	20.9
39	50	-0	-5285	0	0	0	-5832	--	--	16.08	16.08	0.18	0.10	0.04	0.33	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 206 NI 1688 NF 1687 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-2917	0	0	0	-1979	--	--	16.08	16.08	0.18	0.03	0.02	0.18	0.00	0.00	20.9
2	0	-0	-3009	0	0	0	-2021	--	--	16.08	16.08	0.29	0.04	0.02	0.19	0.00	0.00	20.9
3	0	-0	-2999	0	0	0	-2015	--	--	16.08	16.08	0.29	0.03	0.02	0.19	0.00	0.00	20.9
4	0	-0	-1489	0	0	0	-1030	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
5	0	-0	-1479	0	0	0	-1023	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
6	0	-0	-2488	0	0	0	-1681	--	--	16.08	16.08	0.29	0.03	0.02	0.16	0.00	0.00	20.9
7	0	-0	-2455	0	0	0	-1660	--	--	16.08	16.08	0.29	0.03	0.02	0.15	0.00	0.00	20.9
8	0	-0	-2032	0	0	0	-1384	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
9	0	-0	-1999	0	0	0	-1363	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
10	0	-0	-3009	0	0	0	-2021	--	--	16.08	16.08	0.29	0.04	0.02	0.19	0.00	0.00	20.9
11	0	-0	-2999	0	0	0	-2015	--	--	16.08	16.08	0.29	0.03	0.02	0.19	0.00	0.00	20.9
12	0	-0	-1489	0	0	0	-1030	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
13	0	-0	-1479	0	0	0	-1023	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
14	0	-0	-2488	0	0	0	-1681	--	--	16.08	16.08	0.29	0.03	0.02	0.16	0.00	0.00	20.9
15	0	-0	-2455	0	0	0	-1660	--	--	16.08	16.08	0.29	0.03	0.02	0.15	0.00	0.00	20.9
16	0	-0	-2032	0	0	0	-1384	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
17	0	-0	-1999	0	0	0	-1363	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
18	0	-0	-10870	0	0	0	-7178	--	--	16.08	16.08	0.18	0.12	0.09	0.68	0.00	0.00	20.9
19	0	-0	-3755	0	0	0	-2548	--	--	16.08	16.08	0.18	0.04	0.03	0.24	0.00	0.00	20.9
20	0	-0	-6644	0	0	0	-4425	--	--	16.08	16.08	0.18	0.07	0.05	0.42	0.00	0.00	20.9
37	0	-0	-11800	0	0	0	-7777	--	--	16.08	16.08	0.18	0.13	0.10	0.74	0.00	0.00	20.9
38	0	-0	55	0	0	0	-88	--	--	16.08	16.08	0.18	0.00	0.00	0.00	0.00	0.00	20.9
39	0	-0	-4760	0	0	0	-3189	--	--	16.08	16.08	0.18	0.05	0.04	0.30	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	25	-0	-2917	0	0	0	-1979	--	--	16.08	16.08	0.18	0.03	0.02	0.18	0.00	0.00	20.9
2	25	-0	-3009	0	0	0	-2021	--	--	16.08	16.08	0.29	0.04	0.02	0.19	0.00	0.00	20.9
3	25	-0	-2999	0	0	0	-2015	--	--	16.08	16.08	0.29	0.03	0.02	0.19	0.00	0.00	20.9
4	25	-0	-1489	0	0	0	-1030	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
5	25	-0	-1479	0	0	0	-1023	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
6	25	-0	-2488	0	0	0	-1681	--	--	16.08	16.08	0.29	0.03	0.02	0.16	0.00	0.00	20.9
7	25	-0	-2455	0	0	0	-1660	--	--	16.08	16.08	0.29	0.03	0.02	0.15	0.00	0.00	20.9
8	25	-0	-2032	0	0	0	-1384	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
9	25	-0	-1999	0	0	0	-1363	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
10	25	-0	-3009	0	0	0	-2021	--	--	16.08	16.08	0.29	0.04	0.02	0.19	0.00	0.00	20.9
11	25	-0	-2999	0	0	0	-2015	--	--	16.08	16.08	0.29	0.03	0.02	0.19	0.00	0.00	20.9
12	25	-0	-1489	0	0	0	-1030	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
13	25	-0	-1479	0	0	0	-1023	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
14	25	-0	-2488	0	0	0	-1681	--	--	16.08	16.08	0.29	0.03	0.02	0.16	0.00	0.00	20.9
15	25	-0	-2455	0	0	0	-1660	--	--	16.08	16.08	0.29	0.03	0.02	0.15	0.00	0.00	20.9
16	25	-0	-2032	0	0	0	-1384	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
17	25	-0	-1999	0	0	0	-1363	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
18	25	-0	-10870	0	0	0	-7178	--	--	16.08	16.08	0.18	0.12	0.09	0.68	0.00	0.00	20.9
19	25	-0	-3755	0	0	0	-2548	--	--	16.08	16.08	0.18	0.04	0.03	0.24	0.00	0.00	20.9
20	25	-0	-6644	0	0	0	-4425	--	--	16.08	16.08	0.18	0.07	0.05	0.42	0.00	0.00	20.9
37	25	-0	-11800	0	0	0	-7777	--	--	16.08	16.08	0.18	0.13	0.10	0.74	0.00	0.00	20.9
38	25	-0	55	0	0	0	-88	--	--	16.08	16.08	0.18	0.00	0.00	0.00	0.00	0.00	20.9
39	25	-0	-4760	0	0	0	-3189	--	--	16.08	16.08	0.18	0.05	0.04	0.30	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	50	-0	-2917	0	0	0	-1979	--	--	16.08	16.08	0.18	0.03	0.02	0.18	0.00	0.00	20.9
2	50	-0	-3009	0	0	0	-2021	--	--	16.08	16.08	0.29	0.04	0.02	0.19	0.00	0.00	20.9
3	50	-0	-2999	0	0	0	-2015	--	--	16.08	16.08	0.29	0.03	0.02	0.19	0.00	0.00	20.9
4	50	-0	-1489	0	0	0	-1030	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
5	50	-0	-1479	0	0	0	-1023	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
6	50	-0	-2488	0	0	0	-1681	--	--	16.08	16.08	0.29	0.03	0.02	0.16	0.00	0.00	20.9
7	50	-0	-2455	0	0	0	-1660	--	--	16.08	16.08	0.29	0.03	0.02	0.15	0.00	0.00	20.9
8	50	-0	-2032	0	0	0	-1384	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
9	50	-0	-1999	0	0	0	-1363	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
10	50	-0	-3009	0	0	0	-2021	--	--	16.08	16.08	0.29	0.04	0.02	0.19	0.00	0.00	20.9
11	50	-0	-2999	0	0	0	-2015	--	--	16.08	16.08	0.29	0.03	0.02	0.19	0.00	0.00	20.9
12	50	-0	-1489	0	0	0	-1030	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
13	50	-0	-1479	0	0	0	-1023	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
14	50	-0	-2488	0	0	0	-1681	--	--	16.08	16.08	0.29	0.03	0.02	0.16	0.00	0.00	20.9
15	50	-0	-2455	0	0	0	-1660	--	--	16.08	16.08	0.29	0.03	0.02	0.15	0.00	0.00	20.9
16	50	-0	-2032	0	0	0	-1384	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
17	50	-0	-1999	0	0	0	-1363	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
18	50	-0	-10870	0	0	0	-7178	--	--	16.08	16.08	0.18	0.12	0.09	0.68	0.00	0.00	20.9
19	50	-0	-3755	0	0	0	-2548	--	--	16.08	16.08	0.18	0.04	0.03	0.24	0.00	0.00	20.9
20	50	-0	-6644	0	0	0	-4425	--	--	16.08	16.08	0.18	0.07	0.05	0.42	0.00	0.00	20.9
37	50	-0	-11800	0	0	0	-7777	--	--	16.08	16.08	0.18	0.13	0.10	0.74	0.00	0.00	20.9
38	50	-0	55	0	0	0	-88	--	--	16.08	16.08	0.18	0.00	0.00	0.00	0.00	0.00	20.9
39	50	-0	-4760	0	0	0	-3189	--	--	16.08	16.08	0.18	0.05	0.04	0.30	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 207 NI 1689 NF 1688 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-1301	0	0	0	-520	--	--	16.08	16.08	0.18	0.01	0.01	0.08	0.00	0.00	20.9
2	0	-0	-1292	0	0	0	-517	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
3	0	-0	-1288	0	0	0	-515	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
4	0	-0	-714	0	0	0	-286	--	--	16.08	16.08	0.29	0.00	0.01	0.04	0.00	0.00	20.9
5	0	-0	-710	0	0	0	-284	--	--	16.08	16.08	0.29	0.00	0.01	0.04	0.00	0.00	20.9
6	0	-0	-1094	0	0	0	-437	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
7	0	-0	-1082	0	0	0	-433	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
8	0	-0	-920	0	0	0	-368	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
9	0	-0	-908	0	0	0	-363	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
10	0	-0	-1292	0	0	0	-517	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
11	0	-0	-1288	0	0	0	-515	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
12	0	-0	-714	0	0	0	-286	--	--	16.08	16.08	0.29	0.00	0.01	0.04	0.00	0.00	20.9
13	0	-0	-710	0	0	0	-284	--	--	16.08	16.08	0.29	0.00	0.01	0.04	0.00	0.00	20.9
14	0	-0	-1094	0	0	0	-437	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
15	0	-0	-1082	0	0	0	-433	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
16	0	-0	-920	0	0	0	-368	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
17	0	-0	-908	0	0	0	-363	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
18	0	-0	-4359	0	0	0	-1744	--	--	16.08	16.08	0.18	0.03	0.04	0.27	0.00	0.00	20.9
19	0	-0	-1677	0	0	0	-671	--	--	16.08	16.08	0.18	0.01	0.01	0.11	0.00	0.00	20.9
20	0	-0	-2758	0	0	0	-1103	--	--	16.08	16.08	0.18	0.02	0.02	0.17	0.00	0.00	20.9
37	0	-0	-4692	0	0	0	-1877	--	--	16.08	16.08	0.18	0.03	0.04	0.29	0.00	0.00	20.9
38	0	-0	-220	0	0	0	-88	--	--	16.08	16.08	0.18	0.00	0.00	0.01	0.00	0.00	20.9
39	0	-0	-2023	0	0	0	-809	--	--	16.08	16.08	0.18	0.01	0.02	0.13	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	20	-0	-1301	0	0	0	-520	--	--	16.08	16.08	0.18	0.01	0.01	0.08	0.00	0.00	20.9
2	20	-0	-1292	0	0	0	-517	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
3	20	-0	-1288	0	0	0	-515	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
4	20	-0	-714	0	0	0	-286	--	--	16.08	16.08	0.29	0.00	0.01	0.04	0.00	0.00	20.9
5	20	-0	-710	0	0	0	-284	--	--	16.08	16.08	0.29	0.00	0.01	0.04	0.00	0.00	20.9
6	20	-0	-1094	0	0	0	-437	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
7	20	-0	-1082	0	0	0	-433	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
8	20	-0	-920	0	0	0	-368	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
9	20	-0	-908	0	0	0	-363	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
10	20	-0	-1292	0	0	0	-517	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
11	20	-0	-1288	0	0	0	-515	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
12	20	-0	-714	0	0	0	-286	--	--	16.08	16.08	0.29	0.00	0.01	0.04	0.00	0.00	20.9
13	20	-0	-710	0	0	0	-284	--	--	16.08	16.08	0.29	0.00	0.01	0.04	0.00	0.00	20.9
14	20	-0	-1094	0	0	0	-437	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
15	20	-0	-1082	0	0	0	-433	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
16	20	-0	-920	0	0	0	-368	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
17	20	-0	-908	0	0	0	-363	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
18	20	-0	-4359	0	0	0	-1744	--	--	16.08	16.08	0.18	0.03	0.04	0.27	0.00	0.00	20.9
19	20	-0	-1677	0	0	0	-671	--	--	16.08	16.08	0.18	0.01	0.01	0.11	0.00	0.00	20.9
20	20	-0	-2758	0	0	0	-1103	--	--	16.08	16.08	0.18	0.02	0.02	0.17	0.00	0.00	20.9
37	20	-0	-4692	0	0	0	-1877	--	--	16.08	16.08	0.18	0.03	0.04	0.29	0.00	0.00	20.9
38	20	-0	-220	0	0	0	-88	--	--	16.08	16.08	0.18	0.00	0.00	0.01	0.00	0.00	20.9
39	20	-0	-2023	0	0	0	-809	--	--	16.08	16.08	0.18	0.01	0.02	0.13	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	40	-0	-1301	0	0	0	-520	--	--	16.08	16.08	0.18	0.01	0.01	0.08	0.00	0.00	20.9
2	40	-0	-1292	0	0	0	-517	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
3	40	-0	-1288	0	0	0	-515	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
4	40	-0	-714	0	0	0	-286	--	--	16.08	16.08	0.29	0.00	0.01	0.04	0.00	0.00	20.9
5	40	-0	-710	0	0	0	-284	--	--	16.08	16.08	0.29	0.00	0.01	0.04	0.00	0.00	20.9
6	40	-0	-1094	0	0	0	-437	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
7	40	-0	-1082	0	0	0	-433	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
8	40	-0	-920	0	0	0	-368	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
9	40	-0	-908	0	0	0	-363	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
10	40	-0	-1292	0	0	0	-517	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
11	40	-0	-1288	0	0	0	-515	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
12	40	-0	-714	0	0	0	-286	--	--	16.08	16.08	0.29	0.00	0.01	0.04	0.00	0.00	20.9
13	40	-0	-710	0	0	0	-284	--	--	16.08	16.08	0.29	0.00	0.01	0.04	0.00	0.00	20.9
14	40	-0	-1094	0	0	0	-437	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
15	40	-0	-1082	0	0	0	-433	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
16	40	-0	-920	0	0	0	-368	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
17	40	-0	-908	0	0	0	-363	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
18	40	-0	-4359	0	0	0	-1744	--	--	16.08	16.08	0.18	0.03	0.04	0.27	0.00	0.00	20.9
19	40	-0	-1677	0	0	0	-671	--	--	16.08	16.08	0.18	0.01	0.01	0.11	0.00	0.00	20.9
20	40	-0	-2758	0	0	0	-1103	--	--	16.08	16.08	0.18	0.02	0.02	0.17	0.00	0.00	20.9
37	40	-0	-4692	0	0	0	-1877	--	--	16.08	16.08	0.18	0.03	0.04	0.29	0.00	0.00	20.9
38	40	-0	-220	0	0	0	-88	--	--	16.08	16.08	0.18	0.00	0.00	0.01	0.00	0.00	20.9
39	40	-0	-2023	0	0	0	-809	--	--	16.08	16.08	0.18	0.01	0.02	0.13	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 208 NI 1611 NF 1604 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-235	0	0	0	94	--	--	16.08	16.08	0.00	0.00	0.00	0.01	0.00	0.00	20.9
2	0	-0	-343	0	0	0	137	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
3	0	-0	-343	0	0	0	137	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
4	0	-0	-19	0	0	0	7	--	--	16.08	16.08	0.10	0.00	0.00	0.00	0.00	0.00	20.9
5	0	-0	-19	0	0	0	8	--	--	16.08	16.08	0.10	0.00	0.00	0.00	0.00	0.00	20.9
6	0	-0	-229	0	0	0	92	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
7	0	-0	-230	0	0	0	92	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
8	0	-0	-132	0	0	0	53	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
9	0	-0	-132	0	0	0	53	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
10	0	-0	-343	0	0	0	137	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9

11	0	-0	-343	0	0	0	137	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
12	0	-0	-19	0	0	0	7	--	--	16.08	16.08	0.10	0.00	0.00	0.00	0.00	0.00	20.9
13	0	-0	-19	0	0	0	8	--	--	16.08	16.08	0.10	0.00	0.00	0.00	0.00	0.00	20.9
14	0	-0	-229	0	0	0	92	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
15	0	-0	-230	0	0	0	92	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
16	0	-0	-132	0	0	0	53	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
17	0	-0	-132	0	0	0	53	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
18	0	-0	-475	0	0	0	190	--	--	16.08	16.08	0.00	0.00	0.00	0.03	0.00	0.00	20.9
19	0	-0	1046	0	0	0	-419	--	--	16.08	16.08	0.18	0.01	0.01	0.07	0.00	0.00	20.9
20	0	-0	208	0	0	0	-83	--	--	16.08	16.08	0.18	0.00	0.00	0.01	0.00	0.00	20.9
37	0	-0	-1153	0	0	0	461	--	--	16.08	16.08	0.00	0.01	0.01	0.07	0.00	0.00	20.9
38	0	-0	1382	0	0	0	-553	--	--	16.08	16.08	0.18	0.01	0.01	0.09	0.00	0.00	20.9
39	0	-0	-15	0	0	0	6	--	--	16.08	16.08	0.00	0.00	0.00	0.00	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	20	-0	-235	0	0	0	94	--	--	16.08	16.08	0.00	0.00	0.00	0.01	0.00	0.00	20.9
2	20	-0	-343	0	0	0	137	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
3	20	-0	-343	0	0	0	137	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
4	20	-0	-19	0	0	0	7	--	--	16.08	16.08	0.10	0.00	0.00	0.00	0.00	0.00	20.9
5	20	-0	-19	0	0	0	8	--	--	16.08	16.08	0.10	0.00	0.00	0.00	0.00	0.00	20.9
6	20	-0	-229	0	0	0	92	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
7	20	-0	-230	0	0	0	92	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
8	20	-0	-132	0	0	0	53	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
9	20	-0	-132	0	0	0	53	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
10	20	-0	-343	0	0	0	137	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
11	20	-0	-343	0	0	0	137	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
12	20	-0	-19	0	0	0	7	--	--	16.08	16.08	0.10	0.00	0.00	0.00	0.00	0.00	20.9
13	20	-0	-19	0	0	0	8	--	--	16.08	16.08	0.10	0.00	0.00	0.00	0.00	0.00	20.9
14	20	-0	-229	0	0	0	92	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
15	20	-0	-230	0	0	0	92	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
16	20	-0	-132	0	0	0	53	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
17	20	-0	-132	0	0	0	53	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
18	20	-0	-475	0	0	0	190	--	--	16.08	16.08	0.00	0.00	0.00	0.03	0.00	0.00	20.9
19	20	-0	1046	0	0	0	-419	--	--	16.08	16.08	0.18	0.01	0.01	0.07	0.00	0.00	20.9
20	20	-0	208	0	0	0	-83	--	--	16.08	16.08	0.18	0.00	0.00	0.01	0.00	0.00	20.9
37	20	-0	-1153	0	0	0	461	--	--	16.08	16.08	0.00	0.01	0.01	0.07	0.00	0.00	20.9
38	20	-0	1382	0	0	0	-553	--	--	16.08	16.08	0.18	0.01	0.01	0.09	0.00	0.00	20.9
39	20	-0	-15	0	0	0	6	--	--	16.08	16.08	0.00	0.00	0.00	0.00	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	40	-0	-235	0	0	0	-251	--	--	16.08	16.08	0.18	0.00	0.00	0.01	0.00	0.00	20.9
2	40	-0	-343	0	0	0	-366	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
3	40	-0	-343	0	0	0	-367	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
4	40	-0	-19	0	0	0	-20	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
5	40	-0	-19	0	0	0	-20	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
6	40	-0	-229	0	0	0	-245	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
7	40	-0	-230	0	0	0	-245	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
8	40	-0	-132	0	0	0	-141	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
9	40	-0	-132	0	0	0	-142	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
10	40	-0	-343	0	0	0	-366	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
11	40	-0	-343	0	0	0	-367	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
12	40	-0	-19	0	0	0	-20	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
13	40	-0	-19	0	0	0	-20	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
14	40	-0	-229	0	0	0	-245	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
15	40	-0	-230	0	0	0	-245	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
16	40	-0	-132	0	0	0	-141	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
17	40	-0	-132	0	0	0	-142	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
18	40	-0	-475	0	0	0	-507	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9
19	40	-0	1046	0	0	0	-419	--	--	16.08	16.08	0.18	0.01	0.01	0.07	0.00	0.00	20.9
20	40	-0	208	0	0	0	-83	--	--	16.08	16.08	0.18	0.00	0.00	0.01	0.00	0.00	20.9
37	40	-0	-1153	0	0	0	-1232	--	--	16.08	16.08	0.18	0.02	0.01	0.07	0.00	0.00	20.9
38	40	-0	1382	0	0	0	-553	--	--	16.08	16.08	0.18	0.01	0.01	0.09	0.00	0.00	20.9
39	40	-0	-15	0	0	0	-16	--	--	16.08	16.08	0.18	0.00	0.00	0.00	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 209 NI 1610 NF 1611 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm

1	0	-0	-981	0	0	0	584	--	--	16.08	16.08	0.00	0.01	0.01	0.06	0.00	0.00	20.9
2	0	-0	-1200	0	0	0	737	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
3	0	-0	-1201	0	0	0	738	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
4	0	-0	-308	0	0	0	161	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
5	0	-0	-309	0	0	0	162	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
6	0	-0	-887	0	0	0	535	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
7	0	-0	-889	0	0	0	537	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
8	0	-0	-619	0	0	0	362	--	--	16.08	16.08	0.10	0.01	0.01	0.04	0.00	0.00	20.9
9	0	-0	-622	0	0	0	364	--	--	16.08	16.08	0.10	0.01	0.01	0.04	0.00	0.00	20.9
10	0	-0	-1200	0	0	0	737	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
11	0	-0	-1201	0	0	0	738	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
12	0	-0	-308	0	0	0	161	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
13	0	-0	-309	0	0	0	162	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
14	0	-0	-887	0	0	0	535	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
15	0	-0	-889	0	0	0	537	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
16	0	-0	-619	0	0	0	362	--	--	16.08	16.08	0.10	0.01	0.01	0.04	0.00	0.00	20.9
17	0	-0	-622	0	0	0	364	--	--	16.08	16.08	0.10	0.01	0.01	0.04	0.00	0.00	20.9
18	0	-0	-1769	0	0	0	1075	--	--	16.08	16.08	0.00	0.02	0.01	0.11	0.00	0.00	20.9
19	0	-0	2491	0	0	0	-1664	--	--	16.08	16.08	0.18	0.03	0.02	0.16	0.00	0.00	20.9
20	0	-0	161	0	0	0	-164	--	--	16.08	16.08	0.18	0.00	0.00	0.01	0.00	0.00	20.9
37	0	-0	-3632	0	0	0	2277	--	--	16.08	16.08	0.00	0.04	0.03	0.23	0.00	0.00	20.9
38	0	-0	3468	0	0	0	-2287	--	--	16.08	16.08	0.18	0.04	0.03	0.22	0.00	0.00	20.9
39	0	-0	-414	0	0	0	213	--	--	16.08	16.08	0.00	0.00	0.00	0.03	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	25	-0	-981	0	0	0	584	--	--	16.08	16.08	0.00	0.01	0.01	0.06	0.00	0.00	20.9
2	25	-0	-1200	0	0	0	737	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
3	25	-0	-1201	0	0	0	738	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
4	25	-0	-308	0	0	0	161	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
5	25	-0	-309	0	0	0	162	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
6	25	-0	-887	0	0	0	535	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9

7	25	-0	-889	0	0	0	537	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
8	25	-0	-619	0	0	0	362	--	--	16.08	16.08	0.10	0.01	0.01	0.04	0.00	0.00	20.9
9	25	-0	-622	0	0	0	364	--	--	16.08	16.08	0.10	0.01	0.01	0.04	0.00	0.00	20.9
10	25	-0	-1200	0	0	0	737	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
11	25	-0	-1201	0	0	0	738	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
12	25	-0	-308	0	0	0	161	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
13	25	-0	-309	0	0	0	162	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
14	25	-0	-887	0	0	0	535	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
15	25	-0	-889	0	0	0	537	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
16	25	-0	-619	0	0	0	362	--	--	16.08	16.08	0.10	0.01	0.01	0.04	0.00	0.00	20.9
17	25	-0	-622	0	0	0	364	--	--	16.08	16.08	0.10	0.01	0.01	0.04	0.00	0.00	20.9
18	25	-0	-1769	0	0	0	1075	--	--	16.08	16.08	0.00	0.02	0.01	0.11	0.00	0.00	20.9
19	25	-0	2491	0	0	0	-1664	--	--	16.08	16.08	0.18	0.03	0.02	0.16	0.00	0.00	20.9
20	25	-0	161	0	0	0	-164	--	--	16.08	16.08	0.18	0.00	0.00	0.01	0.00	0.00	20.9
37	25	-0	-3632	0	0	0	2277	--	--	16.08	16.08	0.00	0.04	0.03	0.23	0.00	0.00	20.9
38	25	-0	3468	0	0	0	-2287	--	--	16.08	16.08	0.18	0.04	0.03	0.22	0.00	0.00	20.9
39	25	-0	-414	0	0	0	213	--	--	16.08	16.08	0.00	0.00	0.00	0.03	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	50	-0	-981	0	0	0	94	--	--	16.08	16.08	0.00	0.00	0.01	0.06	0.00	0.00	20.9
2	50	-0	-1200	0	0	0	137	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
3	50	-0	-1201	0	0	0	137	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
4	50	-0	-308	0	0	0	7	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
5	50	-0	-309	0	0	0	8	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
6	50	-0	-887	0	0	0	92	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
7	50	-0	-889	0	0	0	92	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
8	50	-0	-619	0	0	0	53	--	--	16.08	16.08	0.10	0.00	0.01	0.04	0.00	0.00	20.9
9	50	-0	-622	0	0	0	53	--	--	16.08	16.08	0.10	0.00	0.01	0.04	0.00	0.00	20.9
10	50	-0	-1200	0	0	0	137	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
11	50	-0	-1201	0	0	0	137	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
12	50	-0	-308	0	0	0	7	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
13	50	-0	-309	0	0	0	8	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
14	50	-0	-887	0	0	0	92	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
15	50	-0	-889	0	0	0	92	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
16	50	-0	-619	0	0	0	53	--	--	16.08	16.08	0.10	0.00	0.01	0.04	0.00	0.00	20.9
17	50	-0	-622	0	0	0	53	--	--	16.08	16.08	0.10	0.00	0.01	0.04	0.00	0.00	20.9
18	50	-0	-1769	0	0	0	190	--	--	16.08	16.08	0.00	0.00	0.01	0.11	0.00	0.00	20.9
19	50	-0	2491	0	0	0	-1664	--	--	16.08	16.08	0.18	0.03	0.02	0.16	0.00	0.00	20.9
20	50	-0	161	0	0	0	-164	--	--	16.08	16.08	0.18	0.00	0.00	0.01	0.00	0.00	20.9
37	50	-0	-3632	0	0	0	461	--	--	16.08	16.08	0.00	0.01	0.03	0.23	0.00	0.00	20.9
38	50	-0	3468	0	0	0	-2287	--	--	16.08	16.08	0.18	0.04	0.03	0.22	0.00	0.00	20.9
39	50	-0	-414	0	0	0	6	--	--	16.08	16.08	0.00	0.00	0.00	0.03	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 210 NI 1603 NF 1610 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-2111	0	0	0	1640	--	--	16.08	16.08	0.00	0.03	0.02	0.13	0.00	0.00	20.9
2	0	-0	-2273	0	0	0	1874	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
3	0	-0	-2274	0	0	0	1875	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
4	0	-0	-974	0	0	0	648	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
5	0	-0	-976	0	0	0	650	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
6	0	-0	-1816	0	0	0	1443	--	--	16.08	16.08	0.10	0.03	0.01	0.11	0.00	0.00	20.9
7	0	-0	-1822	0	0	0	1447	--	--	16.08	16.08	0.10	0.03	0.02	0.11	0.00	0.00	20.9
8	0	-0	-1426	0	0	0	1076	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
9	0	-0	-1432	0	0	0	1080	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
10	0	-0	-2273	0	0	0	1874	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
11	0	-0	-2274	0	0	0	1875	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
12	0	-0	-974	0	0	0	648	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
13	0	-0	-976	0	0	0	650	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
14	0	-0	-1816	0	0	0	1443	--	--	16.08	16.08	0.10	0.03	0.01	0.11	0.00	0.00	20.9
15	0	-0	-1822	0	0	0	1447	--	--	16.08	16.08	0.10	0.03	0.02	0.11	0.00	0.00	20.9
16	0	-0	-1426	0	0	0	1076	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
17	0	-0	-1432	0	0	0	1080	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
18	0	-0	-3524	0	0	0	2837	--	--	16.08	16.08	0.00	0.05	0.03	0.22	0.00	0.00	20.9
19	0	-0	2832	0	0	0	-3080	--	--	16.08	16.08	0.18	0.05	0.02	0.18	0.00	0.00	20.9
20	0	-0	-609	0	0	0	140	--	--	16.08	16.08	0.00	0.00	0.01	0.04	0.00	0.00	20.9
37	0	-0	-6227	0	0	0	5391	--	--	16.08	16.08	0.00	0.09	0.05	0.39	0.00	0.00	20.9
38	0	-0	4366	0	0	0	-4470	--	--	16.08	16.08	0.18	0.07	0.04	0.27	0.00	0.00	20.9
39	0	-0	-1368	0	0	0	897	--	--	16.08	16.08	0.00	0.02	0.01	0.09	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	25	-0	-2111	0	0	0	1640	--	--	16.08	16.08	0.00	0.03	0.02	0.13	0.00	0.00	20.9
2	25	-0	-2273	0	0	0	1874	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
3	25	-0	-2274	0	0	0	1875	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
4	25	-0	-974	0	0	0	648	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
5	25	-0	-976	0	0	0	650	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
6	25	-0	-1816	0	0	0	1443	--	--	16.08	16.08	0.10	0.03	0.01	0.11	0.00	0.00	20.9
7	25	-0	-1822	0	0	0	1447	--	--	16.08	16.08	0.10	0.03	0.02	0.11	0.00	0.00	20.9
8	25	-0	-1426	0	0	0	1076	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
9	25	-0	-1432	0	0	0	1080	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
10	25	-0	-2273	0	0	0	1874	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
11	25	-0	-2274	0	0	0	1875	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
12	25	-0	-974	0	0	0	648	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
13	25	-0	-976	0	0	0	650	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
14	25	-0	-1816	0	0	0	1443	--	--	16.08	16.08	0.10	0.03	0.01	0.11	0.00	0.00	20.9
15	25	-0	-1822	0	0	0	1447	--	--	16.08	16.08	0.10	0.03	0.02	0.11	0.00	0.00	20.9
16	25	-0	-1426	0	0	0	1076	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
17	25	-0	-1432	0	0	0	1080	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
18	25	-0	-3524	0	0	0	2837	--	--	16.08	16.08	0.00	0.05	0.03	0.22	0.00	0.00	20.9
19	25	-0	2832	0	0	0	-3080	--	--	16.08	16.08	0.18	0.05	0.02	0.18	0.00	0.00	20.9
20	25	-0	-609	0	0	0	-164	--	--	16.08	16.08	0.18	0.00	0.01	0.04	0.00	0.00	20.9
37	25	-0	-6227	0	0	0	5391	--	--	16.08	16.08	0.00	0.09	0.05	0.39	0.00	0.00	20.9
38	25	-0	4366	0	0	0	-4470	--	--	16.08	16.08	0.18	0.07	0.04	0.27	0.00	0.00	20.9
39	25	-0	-1368	0	0	0	897	--	--	16.08	16.08	0.00	0.02	0.01	0.09	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	50	-0	-2111	0	0	0	584	--	--	16.08	16.08	0.00	0.01	0.02	0.13	0.00	0.00	20.9
2	50	-0	-2273	0	0	0	737	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9

3	50	-0	-2274	0	0	0	738	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
4	50	-0	-974	0	0	0	161	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
5	50	-0	-976	0	0	0	162	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
6	50	-0	-1816	0	0	0	535	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
7	50	-0	-1822	0	0	0	537	--	--	16.08	16.08	0.10	0.01	0.02	0.11	0.00	0.00	20.9
8	50	-0	-1426	0	0	0	362	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
9	50	-0	-1432	0	0	0	364	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
10	50	-0	-2273	0	0	0	737	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
11	50	-0	-2274	0	0	0	738	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
12	50	-0	-974	0	0	0	161	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
13	50	-0	-976	0	0	0	162	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
14	50	-0	-1816	0	0	0	535	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
15	50	-0	-1822	0	0	0	537	--	--	16.08	16.08	0.10	0.01	0.02	0.11	0.00	0.00	20.9
16	50	-0	-1426	0	0	0	362	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
17	50	-0	-1432	0	0	0	364	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
18	50	-0	-3524	0	0	0	1075	--	--	16.08	16.08	0.00	0.02	0.03	0.22	0.00	0.00	20.9
19	50	-0	2832	0	0	0	-3080	--	--	16.08	16.08	0.18	0.05	0.02	0.18	0.00	0.00	20.9
20	50	-0	-609	0	0	0	-164	--	--	16.08	16.08	0.18	0.00	0.01	0.04	0.00	0.00	20.9
37	50	-0	-6227	0	0	0	2277	--	--	16.08	16.08	0.00	0.04	0.05	0.39	0.00	0.00	20.9
38	50	-0	4366	0	0	0	-4470	--	--	16.08	16.08	0.18	0.07	0.04	0.27	0.00	0.00	20.9
39	50	-0	-1368	0	0	0	213	--	--	16.08	16.08	0.00	0.00	0.01	0.09	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 211 NI 1602 NF 1603 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	6297	0	0	0	12350	--	--	16.08	16.08	0.00	0.21	0.05	0.40	0.00	0.00	20.9
2	0	-0	5345	0	0	0	7784	--	--	16.08	16.08	0.10	0.14	0.04	0.34	0.00	0.00	20.9
3	0	-0	5344	0	0	0	7795	--	--	16.08	16.08	0.10	0.14	0.04	0.34	0.00	0.00	20.9
4	0	-0	4344	0	0	0	11200	--	--	16.08	16.08	0.10	0.20	0.04	0.27	0.00	0.00	20.9
5	0	-0	4343	0	0	0	11210	--	--	16.08	16.08	0.10	0.20	0.04	0.27	0.00	0.00	20.9
6	0	-0	4996	0	0	0	8966	--	--	16.08	16.08	0.10	0.16	0.04	0.31	0.00	0.00	20.9
7	0	-0	4992	0	0	0	9005	--	--	16.08	16.08	0.10	0.16	0.04	0.31	0.00	0.00	20.9
8	0	-0	4696	0	0	0	9991	--	--	16.08	16.08	0.10	0.18	0.04	0.29	0.00	0.00	20.9
9	0	-0	4692	0	0	0	10030	--	--	16.08	16.08	0.10	0.18	0.04	0.29	0.00	0.00	20.9
10	0	-0	5345	0	0	0	7784	--	--	16.08	16.08	0.10	0.14	0.04	0.34	0.00	0.00	20.9
11	0	-0	5344	0	0	0	7795	--	--	16.08	16.08	0.10	0.14	0.04	0.34	0.00	0.00	20.9
12	0	-0	4344	0	0	0	11200	--	--	16.08	16.08	0.10	0.20	0.04	0.27	0.00	0.00	20.9
13	0	-0	4343	0	0	0	11210	--	--	16.08	16.08	0.10	0.20	0.04	0.27	0.00	0.00	20.9
14	0	-0	4996	0	0	0	8966	--	--	16.08	16.08	0.10	0.16	0.04	0.31	0.00	0.00	20.9
15	0	-0	4992	0	0	0	9005	--	--	16.08	16.08	0.10	0.16	0.04	0.31	0.00	0.00	20.9
16	0	-0	4696	0	0	0	9991	--	--	16.08	16.08	0.10	0.18	0.04	0.29	0.00	0.00	20.9
17	0	-0	4692	0	0	0	10030	--	--	16.08	16.08	0.10	0.18	0.04	0.29	0.00	0.00	20.9
18	0	-0	9106	0	0	0	15660	--	--	16.08	16.08	0.00	0.27	0.08	0.57	0.00	0.00	20.9
19	0	-0	3830	0	0	0	28230	--	--	16.08	16.08	0.00	0.48	0.03	0.24	0.00	0.00	20.9
20	0	-0	6425	0	0	0	20520	--	--	16.08	16.08	0.00	0.35	0.05	0.40	0.00	0.00	20.9
37	0	-0	10830	0	0	0	8346	--	--	16.08	16.08	0.00	0.14	0.09	0.68	0.00	0.00	20.9
38	0	-0	2033	0	0	0	29300	--	--	16.08	16.08	0.00	0.50	0.02	0.13	0.00	0.00	20.9
39	0	-0	6357	0	0	0	16460	--	--	16.08	16.08	0.00	0.28	0.05	0.40	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	10	-0	6297	0	0	0	19710	--	--	16.08	16.08	0.00	0.34	0.05	0.40	0.00	0.00	20.9
2	10	-0	5345	0	0	0	14031	--	--	16.08	16.08	0.10	0.25	0.04	0.34	0.00	0.00	20.9
3	10	-0	5344	0	0	0	14041	--	--	16.08	16.08	0.10	0.25	0.04	0.34	0.00	0.00	20.9
4	10	-0	4344	0	0	0	16278	--	--	16.08	16.08	0.10	0.29	0.04	0.27	0.00	0.00	20.9
5	10	-0	4343	0	0	0	16287	--	--	16.08	16.08	0.10	0.29	0.04	0.27	0.00	0.00	20.9
6	10	-0	4996	0	0	0	14805	--	--	16.08	16.08	0.10	0.26	0.04	0.31	0.00	0.00	20.9
7	10	-0	4992	0	0	0	14838	--	--	16.08	16.08	0.10	0.26	0.04	0.31	0.00	0.00	20.9
8	10	-0	4696	0	0	0	15479	--	--	16.08	16.08	0.10	0.27	0.04	0.29	0.00	0.00	20.9
9	10	-0	4692	0	0	0	15515	--	--	16.08	16.08	0.10	0.28	0.04	0.29	0.00	0.00	20.9
10	10	-0	5345	0	0	0	14031	--	--	16.08	16.08	0.10	0.25	0.04	0.34	0.00	0.00	20.9
11	10	-0	5344	0	0	0	14041	--	--	16.08	16.08	0.10	0.25	0.04	0.34	0.00	0.00	20.9
12	10	-0	4344	0	0	0	16278	--	--	16.08	16.08	0.10	0.29	0.04	0.27	0.00	0.00	20.9
13	10	-0	4343	0	0	0	16287	--	--	16.08	16.08	0.10	0.29	0.04	0.27	0.00	0.00	20.9
14	10	-0	4996	0	0	0	14805	--	--	16.08	16.08	0.10	0.26	0.04	0.31	0.00	0.00	20.9
15	10	-0	4992	0	0	0	14838	--	--	16.08	16.08	0.10	0.26	0.04	0.31	0.00	0.00	20.9
16	10	-0	4696	0	0	0	15479	--	--	16.08	16.08	0.10	0.27	0.04	0.29	0.00	0.00	20.9
17	10	-0	4692	0	0	0	15515	--	--	16.08	16.08	0.10	0.28	0.04	0.29	0.00	0.00	20.9
18	10	-0	9106	0	0	0	26302	--	--	16.08	16.08	0.00	0.45	0.08	0.57	0.00	0.00	20.9
19	10	-0	3830	0	0	0	32703	--	--	16.08	16.08	0.00	0.56	0.03	0.24	0.00	0.00	20.9
20	10	-0	6425	0	0	0	28032	--	--	16.08	16.08	0.00	0.48	0.05	0.40	0.00	0.00	20.9
37	10	-0	10830	0	0	0	21003	--	--	16.08	16.08	0.00	0.36	0.09	0.68	0.00	0.00	20.9
38	10	-0	2033	0	0	0	31673	--	--	16.08	16.08	0.00	0.54	0.02	0.13	0.00	0.00	20.9
39	10	-0	6357	0	0	0	23889	--	--	16.08	16.08	0.00	0.41	0.05	0.40	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	20	-0	6297	0	0	0	13610	--	--	16.08	16.08	0.00	0.23	0.05	0.40	0.00	0.00	20.9
2	20	-0	5345	0	0	0	8853	--	--	16.08	16.08	0.10	0.16	0.04	0.34	0.00	0.00	20.9
3	20	-0	5344	0	0	0	8864	--	--	16.08	16.08	0.10	0.16	0.04	0.34	0.00	0.00	20.9
4	20	-0	4344	0	0	0	12070	--	--	16.08	16.08	0.10	0.21	0.04	0.27	0.00	0.00	20.9
5	20	-0	4343	0	0	0	12080	--	--	16.08	16.08	0.10	0.21	0.04	0.27	0.00	0.00	20.9
6	20	-0	4996	0	0	0	9965	--	--	16.08	16.08	0.10	0.18	0.04	0.31	0.00	0.00	20.9
7	20	-0	4992	0	0	0	10000	--	--	16.08	16.08	0.10	0.18	0.04	0.31	0.00	0.00	20.9
8	20	-0	4696	0	0	0	10930	--	--	16.08	16.08	0.10	0.19	0.04	0.29	0.00	0.00	20.9
9	20	-0	4692	0	0	0	10970	--	--	16.08	16.08	0.10	0.19	0.04	0.29	0.00	0.00	20.9
10	20	-0	5345	0	0	0	8853	--	--	16.08	16.08	0.10	0.16	0.04	0.34	0.00	0.00	20.9
11	20	-0	5344	0	0	0	8864	--	--	16.08	16.08	0.10	0.16	0.04	0.34	0.00	0.00	20.9
12	20	-0	4344	0	0	0	12070	--	--	16.08	16.08	0.10	0.21	0.04	0.27	0.00	0.00	20.9
13	20	-0	4343	0	0	0	12080	--	--	16.08	16.08	0.10	0.21	0.04	0.27	0.00	0.00	20.9
14	20	-0	4996	0	0	0	9965	--	--	16.08	16.08	0.10	0.18	0.04	0.31	0.00	0.00	20.9
15	20	-0	4992	0	0	0	10000	--	--	16.08	16.08	0.10	0.18	0.04	0.31	0.00	0.00	20.9
16	20	-0	4696	0	0	0	10930	--	--	16.08	16.08	0.10	0.19	0.04	0.29	0.00	0.00	20.9
17	20	-0	4692	0	0	0	10970	--	--	16.08	16.08	0.10	0.19	0.04	0.29	0.00	0.00	20.9
18	20	-0	9106	0	0	0	17480	--	--	16.08	16.08	0.00	0.30	0.08	0.57	0.00	0.00	20.9
19	20	-0	3830	0	0	0	28990	--	--	16.08	16.08	0.00	0.49	0.03	0.24	0.00	0.00	20.9
20	20	-0	6425	0	0	0	21810	--	--	16.08	16.08	0.00	0.37	0.05	0.40	0.00	0.00	20.9
37	20	-0	10830	0	0	0	10510	--	--	16.08	16.08	0.00	0.18	0.09	0.68	0.00	0.00	20.9
38	20	-0	2033	0	0	0	29700	--	--	16.08	16.08	0.00	0.51	0.02	0.13	0.00	0.00	20.9
39	20	-0	6357	0	0	0	17730	--	--	16.08	16.08	0.00	0.30	0.05	0.40	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 212 NI 1609 NF 1602 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	9587	0	0	0	8985	--	--	16.08	16.08	0.00	0.15	0.08	0.60	0.00	0.00	20.9
2	0	-0	6222	0	0	0	5522	--	--	16.08	16.08	0.10	0.10	0.05	0.39	0.00	0.00	20.9
3	0	-0	6231	0	0	0	5530	--	--	16.08	16.08	0.10	0.10	0.05	0.39	0.00	0.00	20.9
4	0	-0	8519	0	0	0	8293	--	--	16.08	16.08	0.10	0.15	0.07	0.53	0.00	0.00	20.9
5	0	-0	8528	0	0	0	8301	--	--	16.08	16.08	0.10	0.15	0.07	0.53	0.00	0.00	20.9
6	0	-0	7016	0	0	0	6482	--	--	16.08	16.08	0.10	0.12	0.06	0.44	0.00	0.00	20.9
7	0	-0	7045	0	0	0	6510	--	--	16.08	16.08	0.10	0.12	0.06	0.44	0.00	0.00	20.9
8	0	-0	7705	0	0	0	7314	--	--	16.08	16.08	0.10	0.13	0.06	0.48	0.00	0.00	20.9
9	0	-0	7734	0	0	0	7341	--	--	16.08	16.08	0.10	0.13	0.06	0.49	0.00	0.00	20.9
10	0	-0	6222	0	0	0	5522	--	--	16.08	16.08	0.10	0.10	0.05	0.39	0.00	0.00	20.9
11	0	-0	6231	0	0	0	5530	--	--	16.08	16.08	0.10	0.10	0.05	0.39	0.00	0.00	20.9
12	0	-0	8519	0	0	0	8293	--	--	16.08	16.08	0.10	0.15	0.07	0.53	0.00	0.00	20.9
13	0	-0	8528	0	0	0	8301	--	--	16.08	16.08	0.10	0.15	0.07	0.53	0.00	0.00	20.9
14	0	-0	7016	0	0	0	6482	--	--	16.08	16.08	0.10	0.12	0.06	0.44	0.00	0.00	20.9
15	0	-0	7045	0	0	0	6510	--	--	16.08	16.08	0.10	0.12	0.06	0.44	0.00	0.00	20.9
16	0	-0	7705	0	0	0	7314	--	--	16.08	16.08	0.10	0.13	0.06	0.48	0.00	0.00	20.9
17	0	-0	7734	0	0	0	7341	--	--	16.08	16.08	0.10	0.13	0.06	0.49	0.00	0.00	20.9
18	0	-0	12250	0	0	0	11190	--	--	16.08	16.08	0.00	0.19	0.10	0.77	0.00	0.00	20.9
19	0	-0	20490	0	0	0	21720	--	--	16.08	16.08	0.00	0.37	0.17	1.29	2.41	0.00	20.9
20	0	-0	15360	0	0	0	15350	--	--	16.08	16.08	0.00	0.26	0.13	0.96	0.00	0.00	20.9
37	0	-0	7297	0	0	0	5254	--	--	16.08	16.08	0.00	0.09	0.06	0.46	0.00	0.00	20.9
38	0	-0	21030	0	0	0	22790	--	--	16.08	16.08	0.00	0.39	0.17	1.32	2.47	0.00	20.9
39	0	-0	12490	0	0	0	12180	--	--	16.08	16.08	0.00	0.21	0.10	0.78	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	30	-0	9587	0	0	0	22109	--	--	16.08	16.08	0.00	0.38	0.08	0.60	0.00	0.00	20.9
2	30	-0	6222	0	0	0	14038	--	--	16.08	16.08	0.10	0.25	0.05	0.39	0.00	0.00	20.9
3	30	-0	6231	0	0	0	14058	--	--	16.08	16.08	0.10	0.25	0.05	0.39	0.00	0.00	20.9
4	30	-0	8519	0	0	0	19951	--	--	16.08	16.08	0.10	0.35	0.07	0.53	0.00	0.00	20.9
5	30	-0	8528	0	0	0	19975	--	--	16.08	16.08	0.10	0.35	0.07	0.53	0.00	0.00	20.9
6	30	-0	7016	0	0	0	16084	--	--	16.08	16.08	0.10	0.29	0.06	0.44	0.00	0.00	20.9
7	30	-0	7045	0	0	0	16154	--	--	16.08	16.08	0.10	0.29	0.06	0.44	0.00	0.00	20.9
8	30	-0	7705	0	0	0	17862	--	--	16.08	16.08	0.10	0.32	0.06	0.48	0.00	0.00	20.9
9	30	-0	7734	0	0	0	17926	--	--	16.08	16.08	0.10	0.32	0.06	0.49	0.00	0.00	20.9
10	30	-0	6222	0	0	0	14038	--	--	16.08	16.08	0.10	0.25	0.05	0.39	0.00	0.00	20.9
11	30	-0	6231	0	0	0	14058	--	--	16.08	16.08	0.10	0.25	0.05	0.39	0.00	0.00	20.9
12	30	-0	8519	0	0	0	19951	--	--	16.08	16.08	0.10	0.35	0.07	0.53	0.00	0.00	20.9
13	30	-0	8528	0	0	0	19975	--	--	16.08	16.08	0.10	0.35	0.07	0.53	0.00	0.00	20.9
14	30	-0	7016	0	0	0	16084	--	--	16.08	16.08	0.10	0.29	0.06	0.44	0.00	0.00	20.9
15	30	-0	7045	0	0	0	16154	--	--	16.08	16.08	0.10	0.29	0.06	0.44	0.00	0.00	20.9
16	30	-0	7705	0	0	0	17862	--	--	16.08	16.08	0.10	0.32	0.06	0.48	0.00	0.00	20.9
17	30	-0	7734	0	0	0	17926	--	--	16.08	16.08	0.10	0.32	0.06	0.49	0.00	0.00	20.9
18	30	-0	12250	0	0	0	27957	--	--	16.08	16.08	0.00	0.48	0.10	0.77	0.00	0.00	20.9
19	30	-0	20490	0	0	0	49764	--	--	16.08	16.08	0.00	0.85	0.17	1.19	2.41	0.00	20.9
20	30	-0	15360	0	0	0	36376	--	--	16.08	16.08	0.00	0.62	0.13	0.96	0.00	0.00	20.9
37	30	-0	7297	0	0	0	15242	--	--	16.08	16.08	0.00	0.26	0.06	0.46	0.00	0.00	20.9
38	30	-0	21030	0	0	0	51576	--	--	16.08	16.08	0.00	0.88	0.17	1.17	2.47	0.00	20.9
39	30	-0	12490	0	0	0	29279	--	--	16.08	16.08	0.00	0.50	0.10	0.78	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	60	-0	9587	0	0	0	14740	--	--	16.08	16.08	0.00	0.25	0.08	0.60	0.00	0.00	20.9
2	60	-0	6222	0	0	0	9255	--	--	16.08	16.08	0.10	0.16	0.05	0.39	0.00	0.00	20.9
3	60	-0	6231	0	0	0	9268	--	--	16.08	16.08	0.10	0.16	0.05	0.39	0.00	0.00	20.9
4	60	-0	8519	0	0	0	13400	--	--	16.08	16.08	0.10	0.24	0.07	0.53	0.00	0.00	20.9
5	60	-0	8528	0	0	0	13420	--	--	16.08	16.08	0.10	0.24	0.07	0.53	0.00	0.00	20.9
6	60	-0	7016	0	0	0	10690	--	--	16.08	16.08	0.10	0.19	0.06	0.44	0.00	0.00	20.9
7	60	-0	7045	0	0	0	10740	--	--	16.08	16.08	0.10	0.19	0.06	0.44	0.00	0.00	20.9
8	60	-0	7705	0	0	0	11940	--	--	16.08	16.08	0.10	0.21	0.06	0.48	0.00	0.00	20.9
9	60	-0	7734	0	0	0	11980	--	--	16.08	16.08	0.10	0.21	0.06	0.49	0.00	0.00	20.9
10	60	-0	6222	0	0	0	9255	--	--	16.08	16.08	0.10	0.16	0.05	0.39	0.00	0.00	20.9
11	60	-0	6231	0	0	0	9268	--	--	16.08	16.08	0.10	0.16	0.05	0.39	0.00	0.00	20.9
12	60	-0	8519	0	0	0	13400	--	--	16.08	16.08	0.10	0.24	0.07	0.53	0.00	0.00	20.9
13	60	-0	8528	0	0	0	13420	--	--	16.08	16.08	0.10	0.24	0.07	0.53	0.00	0.00	20.9
14	60	-0	7016	0	0	0	10690	--	--	16.08	16.08	0.10	0.19	0.06	0.44	0.00	0.00	20.9
15	60	-0	7045	0	0	0	10740	--	--	16.08	16.08	0.10	0.19	0.06	0.44	0.00	0.00	20.9
16	60	-0	7705	0	0	0	11940	--	--	16.08	16.08	0.10	0.21	0.06	0.48	0.00	0.00	20.9
17	60	-0	7734	0	0	0	11980	--	--	16.08	16.08	0.10	0.21	0.06	0.49	0.00	0.00	20.9
18	60	-0	12250	0	0	0	18540	--	--	16.08	16.08	0.00	0.32	0.10	0.77	0.00	0.00	20.9
19	60	-0	20490	0	0	0	34010	--	--	16.08	16.08	0.00	0.58	0.17	1.29	2.41	0.00	20.9
20	60	-0	15360	0	0	0	24570	--	--	16.08	16.08	0.00	0.42	0.13	0.96	0.00	0.00	20.9
37	60	-0	7297	0	0	0	9632	--	--	16.08	16.08	0.00	0.16	0.06	0.46	0.00	0.00	20.9
38	60	-0	21030	0	0	0	35410	--	--	16.08	16.08	0.00	0.60	0.17	1.32	2.47	0.00	20.9
39	60	-0	12490	0	0	0	19680	--	--	16.08	16.08	0.00	0.34	0.10	0.78	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 213 NI 1608 NF 1609 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	7610	0	0	0	5180	--	--	16.08	16.08	0.00	0.09	0.06	0.48	0.00	0.00	20.9
2	0	-0	4792	0	0	0	3126	--	--	16.08	16.08	0.10	0.06	0.04	0.30	0.00	0.00	20.9
3	0	-0	4799	0	0	0	3131	--	--	16.08	16.08	0.10	0.06	0.04	0.30	0.00	0.00	20.9
4	0	-0	6909	0	0	0	4839	--	--	16.08	16.08	0.10	0.09	0.06	0.43	0.00	0.00	20.9
5	0	-0	6916	0	0	0	4844	--	--	16.08	16.08	0.10	0.09	0.06	0.43	0.00	0.00	20.9
6	0	-0	5525	0	0	0	3720	--	--	16.08	16.08	0.10	0.07	0.05	0.35	0.00	0.00	20.9
7	0	-0	5548	0	0	0	3736	--	--	16.08	16.08	0.10	0.07	0.05	0.35	0.00	0.00	20.9
8	0	-0	6160	0	0	0	4234	--	--	16.08	16.08	0.10	0.08	0.05	0.39	0.00	0.00	20.9
9	0	-0	6183	0	0	0	4250	--	--	16.08	16.08	0.10	0.08	0.05	0.39	0.00	0.00	20.9
10	0	-0	4792	0	0	0	3126	--	--	16.08	16.08	0.10	0.06	0.04	0.30	0.00	0.00	20.9

11	0	-0	4799	0	0	0	3131	--	--	16.08	16.08	0.10	0.06	0.04	0.30	0.00	0.00	20.9
12	0	-0	6909	0	0	0	4839	--	--	16.08	16.08	0.10	0.09	0.06	0.43	0.00	0.00	20.9
13	0	-0	6916	0	0	0	4844	--	--	16.08	16.08	0.10	0.09	0.06	0.43	0.00	0.00	20.9
14	0	-0	5525	0	0	0	3720	--	--	16.08	16.08	0.10	0.07	0.05	0.35	0.00	0.00	20.9
15	0	-0	5548	0	0	0	3736	--	--	16.08	16.08	0.10	0.07	0.05	0.35	0.00	0.00	20.9
16	0	-0	6160	0	0	0	4234	--	--	16.08	16.08	0.10	0.08	0.05	0.39	0.00	0.00	20.9
17	0	-0	6183	0	0	0	4250	--	--	16.08	16.08	0.10	0.08	0.05	0.39	0.00	0.00	20.9
18	0	-0	9585	0	0	0	6400	--	--	16.08	16.08	0.00	0.11	0.08	0.60	0.00	0.00	20.9
19	0	-0	17460	0	0	0	12990	--	--	16.08	16.08	0.00	0.22	0.14	1.10	2.05	0.00	20.9
20	0	-0	12650	0	0	0	9026	--	--	16.08	16.08	0.00	0.15	0.10	0.79	0.00	0.00	20.9
37	0	-0	5039	0	0	0	2735	--	--	16.08	16.08	0.00	0.05	0.04	0.32	0.00	0.00	20.9
38	0	-0	18160	0	0	0	13720	--	--	16.08	16.08	0.00	0.23	0.15	1.14	2.13	0.00	20.9
39	0	-0	10140	0	0	0	7112	--	--	16.08	16.08	0.00	0.12	0.08	0.64	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	25	-0	7610	0	0	0	15216	--	--	16.08	16.08	0.00	0.26	0.06	0.48	0.00	0.00	20.9
2	25	-0	4792	0	0	0	9445	--	--	16.08	16.08	0.10	0.17	0.04	0.30	0.00	0.00	20.9
3	25	-0	4799	0	0	0	9459	--	--	16.08	16.08	0.10	0.17	0.04	0.30	0.00	0.00	20.9
4	25	-0	6909	0	0	0	13950	--	--	16.08	16.08	0.10	0.25	0.06	0.43	0.00	0.00	20.9
5	25	-0	6916	0	0	0	13964	--	--	16.08	16.08	0.10	0.25	0.06	0.43	0.00	0.00	20.9
6	25	-0	5525	0	0	0	11006	--	--	16.08	16.08	0.10	0.20	0.05	0.35	0.00	0.00	20.9
7	25	-0	5548	0	0	0	11052	--	--	16.08	16.08	0.10	0.20	0.05	0.35	0.00	0.00	20.9
8	25	-0	6160	0	0	0	12357	--	--	16.08	16.08	0.10	0.22	0.05	0.39	0.00	0.00	20.9
9	25	-0	6183	0	0	0	12404	--	--	16.08	16.08	0.10	0.22	0.05	0.39	0.00	0.00	20.9
10	25	-0	4792	0	0	0	9445	--	--	16.08	16.08	0.10	0.17	0.04	0.30	0.00	0.00	20.9
11	25	-0	4799	0	0	0	9459	--	--	16.08	16.08	0.10	0.17	0.04	0.30	0.00	0.00	20.9
12	25	-0	6909	0	0	0	13950	--	--	16.08	16.08	0.10	0.25	0.06	0.43	0.00	0.00	20.9
13	25	-0	6916	0	0	0	13964	--	--	16.08	16.08	0.10	0.25	0.06	0.43	0.00	0.00	20.9
14	25	-0	5525	0	0	0	11006	--	--	16.08	16.08	0.10	0.20	0.05	0.35	0.00	0.00	20.9
15	25	-0	5548	0	0	0	11052	--	--	16.08	16.08	0.10	0.20	0.05	0.35	0.00	0.00	20.9
16	25	-0	6160	0	0	0	12357	--	--	16.08	16.08	0.10	0.22	0.05	0.39	0.00	0.00	20.9
17	25	-0	6183	0	0	0	12404	--	--	16.08	16.08	0.10	0.22	0.05	0.39	0.00	0.00	20.9
18	25	-0	9585	0	0	0	19039	--	--	16.08	16.08	0.00	0.32	0.08	0.60	0.00	0.00	20.9
19	25	-0	17460	0	0	0	36015	--	--	16.08	16.08	0.00	0.61	0.14	1.10	2.05	0.00	20.9
20	25	-0	12650	0	0	0	25708	--	--	16.08	16.08	0.00	0.44	0.10	0.79	0.00	0.00	20.9
37	25	-0	5039	0	0	0	9380	--	--	16.08	16.08	0.00	0.16	0.04	0.32	0.00	0.00	20.9
38	25	-0	18160	0	0	0	37664	--	--	16.08	16.08	0.00	0.64	0.15	1.11	2.13	0.00	20.9
39	25	-0	10140	0	0	0	20483	--	--	16.08	16.08	0.00	0.35	0.08	0.64	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	50	-0	7610	0	0	0	8985	--	--	16.08	16.08	0.00	0.15	0.06	0.48	0.00	0.00	20.9
2	50	-0	4792	0	0	0	5522	--	--	16.08	16.08	0.10	0.10	0.04	0.30	0.00	0.00	20.9
3	50	-0	4799	0	0	0	5530	--	--	16.08	16.08	0.10	0.10	0.04	0.30	0.00	0.00	20.9
4	50	-0	6909	0	0	0	8293	--	--	16.08	16.08	0.10	0.15	0.06	0.43	0.00	0.00	20.9
5	50	-0	6916	0	0	0	8301	--	--	16.08	16.08	0.10	0.15	0.06	0.43	0.00	0.00	20.9
6	50	-0	5525	0	0	0	6482	--	--	16.08	16.08	0.10	0.12	0.05	0.35	0.00	0.00	20.9
7	50	-0	5548	0	0	0	6510	--	--	16.08	16.08	0.10	0.12	0.05	0.35	0.00	0.00	20.9
8	50	-0	6160	0	0	0	7314	--	--	16.08	16.08	0.10	0.13	0.05	0.39	0.00	0.00	20.9
9	50	-0	6183	0	0	0	7341	--	--	16.08	16.08	0.10	0.13	0.05	0.39	0.00	0.00	20.9
10	50	-0	4792	0	0	0	5522	--	--	16.08	16.08	0.10	0.10	0.04	0.30	0.00	0.00	20.9
11	50	-0	4799	0	0	0	5530	--	--	16.08	16.08	0.10	0.10	0.04	0.30	0.00	0.00	20.9
12	50	-0	6909	0	0	0	8293	--	--	16.08	16.08	0.10	0.15	0.06	0.43	0.00	0.00	20.9
13	50	-0	6916	0	0	0	8301	--	--	16.08	16.08	0.10	0.15	0.06	0.43	0.00	0.00	20.9
14	50	-0	5525	0	0	0	6482	--	--	16.08	16.08	0.10	0.12	0.05	0.35	0.00	0.00	20.9
15	50	-0	5548	0	0	0	6510	--	--	16.08	16.08	0.10	0.12	0.05	0.35	0.00	0.00	20.9
16	50	-0	6160	0	0	0	7314	--	--	16.08	16.08	0.10	0.13	0.05	0.39	0.00	0.00	20.9
17	50	-0	6183	0	0	0	7341	--	--	16.08	16.08	0.10	0.13	0.05	0.39	0.00	0.00	20.9
18	50	-0	9585	0	0	0	11190	--	--	16.08	16.08	0.00	0.19	0.08	0.60	0.00	0.00	20.9
19	50	-0	17460	0	0	0	21720	--	--	16.08	16.08	0.00	0.37	0.14	1.10	2.05	0.00	20.9
20	50	-0	12650	0	0	0	15350	--	--	16.08	16.08	0.00	0.26	0.10	0.79	0.00	0.00	20.9
37	50	-0	5039	0	0	0	5254	--	--	16.08	16.08	0.00	0.09	0.04	0.32	0.00	0.00	20.9
38	50	-0	18160	0	0	0	22790	--	--	16.08	16.08	0.00	0.39	0.15	1.14	2.13	0.00	20.9
39	50	-0	10140	0	0	0	12180	--	--	16.08	16.08	0.00	0.21	0.08	0.64	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 214 NI 1607 NF 1608 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	5636	0	0	0	2362	--	--	16.08	16.08	0.00	0.04	0.05	0.35	0.00	0.00	20.9
2	0	-0	3455	0	0	0	1399	--	--	16.08	16.08	0.10	0.02	0.03	0.22	0.00	0.00	20.9
3	0	-0	3460	0	0	0	1401	--	--	16.08	16.08	0.10	0.02	0.03	0.22	0.00	0.00	20.9
4	0	-0	5211	0	0	0	2233	--	--	16.08	16.08	0.10	0.04	0.04	0.33	0.00	0.00	20.9
5	0	-0	5216	0	0	0	2235	--	--	16.08	16.08	0.10	0.04	0.04	0.33	0.00	0.00	20.9
6	0	-0	4064	0	0	0	1688	--	--	16.08	16.08	0.10	0.03	0.03	0.25	0.00	0.00	20.9
7	0	-0	4081	0	0	0	1695	--	--	16.08	16.08	0.10	0.03	0.03	0.26	0.00	0.00	20.9
8	0	-0	4591	0	0	0	1939	--	--	16.08	16.08	0.10	0.03	0.04	0.29	0.00	0.00	20.9
9	0	-0	4608	0	0	0	1946	--	--	16.08	16.08	0.10	0.03	0.04	0.29	0.00	0.00	20.9
10	0	-0	3455	0	0	0	1399	--	--	16.08	16.08	0.10	0.02	0.03	0.22	0.00	0.00	20.9
11	0	-0	3460	0	0	0	1401	--	--	16.08	16.08	0.10	0.02	0.03	0.22	0.00	0.00	20.9
12	0	-0	5211	0	0	0	2233	--	--	16.08	16.08	0.10	0.04	0.04	0.33	0.00	0.00	20.9
13	0	-0	5216	0	0	0	2235	--	--	16.08	16.08	0.10	0.04	0.04	0.33	0.00	0.00	20.9
14	0	-0	4064	0	0	0	1688	--	--	16.08	16.08	0.10	0.03	0.03	0.25	0.00	0.00	20.9
15	0	-0	4081	0	0	0	1695	--	--	16.08	16.08	0.10	0.03	0.03	0.26	0.00	0.00	20.9
16	0	-0	4591	0	0	0	1939	--	--	16.08	16.08	0.10	0.03	0.04	0.29	0.00	0.00	20.9
17	0	-0	4608	0	0	0	1946	--	--	16.08	16.08	0.10	0.03	0.04	0.29	0.00	0.00	20.9
18	0	-0	7012	0	0	0	2894	--	--	16.08	16.08	0.00	0.05	0.06	0.44	0.00	0.00	20.9
19	0	-0	13700	0	0	0	6141	--	--	16.08	16.08	0.00	0.10	0.11	0.86	0.00	0.00	20.9
20	0	-0	9656	0	0	0	4198	--	--	16.08	16.08	0.00	0.07	0.08	0.61	0.00	0.00	20.9
37	0	-0	3250	0	0	0	1110	--	--	16.08	16.08	0.00	0.02	0.03	0.20	0.00	0.00	20.9
38	0	-0	14390	0	0	0	6522	--	--	16.08	16.08	0.00	0.11	0.12	0.90	0.00	0.00	20.9
39	0	-0	7656	0	0	0	3284	--	--	16.08	16.08	0.00	0.06	0.06	0.48	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	25	-0	5636	0	0	0	9794	--	--	16.08	16.08	0.00	0.17	0.05	0.35	0.00	0.00	20.9
2	25	-0	3455	0	0	0	5955	--	--	16.08	16.08	0.10	0.11	0.03	0.22	0.00	0.00	20.9
3	25	-0	3460	0	0	0	5964	--	--	16.08	16.08	0.10	0.11	0.03	0.22	0.00	0.00	20.9
4	25	-0	5211	0	0	0	9105	--	--	16.08	16.08	0.10	0.16	0.04	0.33	0.00	0.00	20.9
5	25	-0	5216	0	0	0	9114	--	--	16.08	16.08	0.10	0.16	0.04	0.33	0.00	0.00	20.9
6	25	-0	4064	0	0	0	7047	--	--	16.08	16.08	0.10	0.13	0.03	0.25	0.00	0.00	20.9

7	25	-0	4081	0	0	0	7077	--	--	16.08	16.08	0.10	0.13	0.03	0.26	0.00	0.00	20.9
8	25	-0	4591	0	0	0	7993	--	--	16.08	16.08	0.10	0.14	0.04	0.29	0.00	0.00	20.9
9	25	-0	4608	0	0	0	8023	--	--	16.08	16.08	0.10	0.14	0.04	0.29	0.00	0.00	20.9
10	25	-0	3455	0	0	0	5955	--	--	16.08	16.08	0.10	0.11	0.03	0.22	0.00	0.00	20.9
11	25	-0	3460	0	0	0	5964	--	--	16.08	16.08	0.10	0.11	0.03	0.22	0.00	0.00	20.9
12	25	-0	5211	0	0	0	9105	--	--	16.08	16.08	0.10	0.16	0.04	0.33	0.00	0.00	20.9
13	25	-0	5216	0	0	0	9114	--	--	16.08	16.08	0.10	0.16	0.04	0.33	0.00	0.00	20.9
14	25	-0	4064	0	0	0	7047	--	--	16.08	16.08	0.10	0.13	0.03	0.25	0.00	0.00	20.9
15	25	-0	4081	0	0	0	7077	--	--	16.08	16.08	0.10	0.13	0.03	0.26	0.00	0.00	20.9
16	25	-0	4591	0	0	0	7993	--	--	16.08	16.08	0.10	0.14	0.04	0.29	0.00	0.00	20.9
17	25	-0	4608	0	0	0	8023	--	--	16.08	16.08	0.10	0.14	0.04	0.29	0.00	0.00	20.9
18	25	-0	7012	0	0	0	12141	--	--	16.08	16.08	0.00	0.21	0.06	0.44	0.00	0.00	20.9
19	25	-0	13700	0	0	0	24207	--	--	16.08	16.08	0.00	0.41	0.11	0.86	0.00	0.00	20.9
20	25	-0	9656	0	0	0	16932	--	--	16.08	16.08	0.00	0.29	0.08	0.61	0.00	0.00	20.9
37	25	-0	3250	0	0	0	5396	--	--	16.08	16.08	0.00	0.09	0.03	0.20	0.00	0.00	20.9
38	25	-0	14390	0	0	0	25500	--	--	16.08	16.08	0.00	0.43	0.12	0.90	0.00	0.00	20.9
39	25	-0	7656	0	0	0	13380	--	--	16.08	16.08	0.00	0.23	0.06	0.48	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	50	-0	5636	0	0	0	5180	--	--	16.08	16.08	0.00	0.09	0.05	0.35	0.00	0.00	20.9
2	50	-0	3455	0	0	0	3126	--	--	16.08	16.08	0.10	0.06	0.03	0.22	0.00	0.00	20.9
3	50	-0	3460	0	0	0	3131	--	--	16.08	16.08	0.10	0.06	0.03	0.22	0.00	0.00	20.9
4	50	-0	5211	0	0	0	4839	--	--	16.08	16.08	0.10	0.09	0.04	0.33	0.00	0.00	20.9
5	50	-0	5216	0	0	0	4844	--	--	16.08	16.08	0.10	0.09	0.04	0.33	0.00	0.00	20.9
6	50	-0	4064	0	0	0	3720	--	--	16.08	16.08	0.10	0.07	0.03	0.25	0.00	0.00	20.9
7	50	-0	4081	0	0	0	3736	--	--	16.08	16.08	0.10	0.07	0.03	0.26	0.00	0.00	20.9
8	50	-0	4591	0	0	0	4234	--	--	16.08	16.08	0.10	0.08	0.04	0.29	0.00	0.00	20.9
9	50	-0	4608	0	0	0	4250	--	--	16.08	16.08	0.10	0.08	0.04	0.29	0.00	0.00	20.9
10	50	-0	3455	0	0	0	3126	--	--	16.08	16.08	0.10	0.06	0.03	0.22	0.00	0.00	20.9
11	50	-0	3460	0	0	0	3131	--	--	16.08	16.08	0.10	0.06	0.03	0.22	0.00	0.00	20.9
12	50	-0	5211	0	0	0	4839	--	--	16.08	16.08	0.10	0.09	0.04	0.33	0.00	0.00	20.9
13	50	-0	5216	0	0	0	4844	--	--	16.08	16.08	0.10	0.09	0.04	0.33	0.00	0.00	20.9
14	50	-0	4064	0	0	0	3720	--	--	16.08	16.08	0.10	0.07	0.03	0.25	0.00	0.00	20.9
15	50	-0	4081	0	0	0	3736	--	--	16.08	16.08	0.10	0.07	0.03	0.26	0.00	0.00	20.9
16	50	-0	4591	0	0	0	4234	--	--	16.08	16.08	0.10	0.08	0.04	0.29	0.00	0.00	20.9
17	50	-0	4608	0	0	0	4250	--	--	16.08	16.08	0.10	0.08	0.04	0.29	0.00	0.00	20.9
18	50	-0	7012	0	0	0	6400	--	--	16.08	16.08	0.00	0.11	0.06	0.44	0.00	0.00	20.9
19	50	-0	13700	0	0	0	12990	--	--	16.08	16.08	0.00	0.22	0.11	0.86	0.00	0.00	20.9
20	50	-0	9656	0	0	0	9026	--	--	16.08	16.08	0.00	0.15	0.08	0.61	0.00	0.00	20.9
37	50	-0	3250	0	0	0	2735	--	--	16.08	16.08	0.00	0.05	0.03	0.20	0.00	0.00	20.9
38	50	-0	14390	0	0	0	13720	--	--	16.08	16.08	0.00	0.23	0.12	0.90	0.00	0.00	20.9
39	50	-0	7656	0	0	0	7112	--	--	16.08	16.08	0.00	0.12	0.06	0.48	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 215 NI 1606 NF 1607 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	3504	0	0	0	610	--	--	16.08	16.08	0.00	0.01	0.03	0.22	0.00	0.00	20.9
2	0	-0	2092	0	0	0	353	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
3	0	-0	2095	0	0	0	353	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
4	0	-0	3297	0	0	0	585	--	--	16.08	16.08	0.10	0.01	0.03	0.21	0.00	0.00	20.9
5	0	-0	3300	0	0	0	586	--	--	16.08	16.08	0.10	0.01	0.03	0.21	0.00	0.00	20.9
6	0	-0	2510	0	0	0	433	--	--	16.08	16.08	0.10	0.01	0.02	0.16	0.00	0.00	20.9
7	0	-0	2520	0	0	0	435	--	--	16.08	16.08	0.10	0.01	0.02	0.16	0.00	0.00	20.9
8	0	-0	2871	0	0	0	503	--	--	16.08	16.08	0.10	0.01	0.02	0.18	0.00	0.00	20.9
9	0	-0	2882	0	0	0	505	--	--	16.08	16.08	0.10	0.01	0.02	0.18	0.00	0.00	20.9
10	0	-0	2092	0	0	0	353	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
11	0	-0	2095	0	0	0	353	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
12	0	-0	3297	0	0	0	585	--	--	16.08	16.08	0.10	0.01	0.03	0.21	0.00	0.00	20.9
13	0	-0	3300	0	0	0	586	--	--	16.08	16.08	0.10	0.01	0.03	0.21	0.00	0.00	20.9
14	0	-0	2510	0	0	0	433	--	--	16.08	16.08	0.10	0.01	0.02	0.16	0.00	0.00	20.9
15	0	-0	2520	0	0	0	435	--	--	16.08	16.08	0.10	0.01	0.02	0.16	0.00	0.00	20.9
16	0	-0	2871	0	0	0	503	--	--	16.08	16.08	0.10	0.01	0.02	0.18	0.00	0.00	20.9
17	0	-0	2882	0	0	0	505	--	--	16.08	16.08	0.10	0.01	0.02	0.18	0.00	0.00	20.9
18	0	-0	4308	0	0	0	740	--	--	16.08	16.08	0.00	0.01	0.04	0.27	0.00	0.00	20.9
19	0	-0	8974	0	0	0	1654	--	--	16.08	16.08	0.00	0.03	0.07	0.56	0.00	0.00	20.9
20	0	-0	6177	0	0	0	1110	--	--	16.08	16.08	0.00	0.02	0.05	0.39	0.00	0.00	20.9
37	0	-0	1732	0	0	0	243	--	--	16.08	16.08	0.00	0.00	0.01	0.11	0.00	0.00	20.9
38	0	-0	9508	0	0	0	1768	--	--	16.08	16.08	0.00	0.03	0.08	0.60	0.00	0.00	20.9
39	0	-0	4846	0	0	0	861	--	--	16.08	16.08	0.00	0.01	0.04	0.30	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	25	-0	3504	0	0	0	5231	--	--	16.08	16.08	0.00	0.09	0.03	0.22	0.00	0.00	20.9
2	25	-0	2092	0	0	0	3112	--	--	16.08	16.08	0.10	0.06	0.02	0.13	0.00	0.00	20.9
3	25	-0	2095	0	0	0	3116	--	--	16.08	16.08	0.10	0.06	0.02	0.13	0.00	0.00	20.9
4	25	-0	3297	0	0	0	4933	--	--	16.08	16.08	0.10	0.09	0.03	0.21	0.00	0.00	20.9
5	25	-0	3300	0	0	0	4937	--	--	16.08	16.08	0.10	0.09	0.03	0.21	0.00	0.00	20.9
6	25	-0	2510	0	0	0	3743	--	--	16.08	16.08	0.10	0.07	0.02	0.16	0.00	0.00	20.9
7	25	-0	2520	0	0	0	3758	--	--	16.08	16.08	0.10	0.07	0.02	0.16	0.00	0.00	20.9
8	25	-0	2871	0	0	0	4289	--	--	16.08	16.08	0.10	0.08	0.02	0.18	0.00	0.00	20.9
9	25	-0	2882	0	0	0	4306	--	--	16.08	16.08	0.10	0.08	0.02	0.18	0.00	0.00	20.9
10	25	-0	2092	0	0	0	3112	--	--	16.08	16.08	0.10	0.06	0.02	0.13	0.00	0.00	20.9
11	25	-0	2095	0	0	0	3116	--	--	16.08	16.08	0.10	0.06	0.02	0.13	0.00	0.00	20.9
12	25	-0	3297	0	0	0	4933	--	--	16.08	16.08	0.10	0.09	0.03	0.21	0.00	0.00	20.9
13	25	-0	3300	0	0	0	4937	--	--	16.08	16.08	0.10	0.09	0.03	0.21	0.00	0.00	20.9
14	25	-0	2510	0	0	0	3743	--	--	16.08	16.08	0.10	0.07	0.02	0.16	0.00	0.00	20.9
15	25	-0	2520	0	0	0	3758	--	--	16.08	16.08	0.10	0.07	0.02	0.16	0.00	0.00	20.9
16	25	-0	2871	0	0	0	4289	--	--	16.08	16.08	0.10	0.08	0.02	0.18	0.00	0.00	20.9
17	25	-0	2882	0	0	0	4306	--	--	16.08	16.08	0.10	0.08	0.02	0.18	0.00	0.00	20.9
18	25	-0	4308	0	0	0	6421	--	--	16.08	16.08	0.00	0.11	0.04	0.27	0.00	0.00	20.9
19	25	-0	8974	0	0	0	13488	--	--	16.08	16.08	0.00	0.23	0.07	0.56	0.00	0.00	20.9
20	25	-0	6177	0	0	0	9256	--	--	16.08	16.08	0.00	0.16	0.05	0.39	0.00	0.00	20.9
37	25	-0	1732	0	0	0	2528	--	--	16.08	16.08	0.00	0.04	0.01	0.11	0.00	0.00	20.9
38	25	-0	9508	0	0	0	14307	--	--	16.08	16.08	0.00	0.24	0.08	0.60	0.00	0.00	20.9
39	25	-0	4846	0	0	0	7252	--	--	16.08	16.08	0.00	0.12	0.04	0.30	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	50	-0	3504	0	0	0	2362	--	--	16.08	16.08	0.00	0.04	0.03	0.22	0.00	0.00	20.9
2	50	-0	2092	0	0	0	1399	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9

3	50	-0	2095	0	0	0	1401	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
4	50	-0	3297	0	0	0	2233	--	--	16.08	16.08	0.10	0.04	0.03	0.21	0.00	0.00	20.9
5	50	-0	3300	0	0	0	2235	--	--	16.08	16.08	0.10	0.04	0.03	0.21	0.00	0.00	20.9
6	50	-0	2510	0	0	0	1688	--	--	16.08	16.08	0.10	0.03	0.02	0.16	0.00	0.00	20.9
7	50	-0	2520	0	0	0	1695	--	--	16.08	16.08	0.10	0.03	0.02	0.16	0.00	0.00	20.9
8	50	-0	2871	0	0	0	1939	--	--	16.08	16.08	0.10	0.03	0.02	0.18	0.00	0.00	20.9
9	50	-0	2882	0	0	0	1946	--	--	16.08	16.08	0.10	0.03	0.02	0.18	0.00	0.00	20.9
10	50	-0	2092	0	0	0	1399	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
11	50	-0	2095	0	0	0	1401	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
12	50	-0	3297	0	0	0	2233	--	--	16.08	16.08	0.10	0.04	0.03	0.21	0.00	0.00	20.9
13	50	-0	3300	0	0	0	2235	--	--	16.08	16.08	0.10	0.04	0.03	0.21	0.00	0.00	20.9
14	50	-0	2510	0	0	0	1688	--	--	16.08	16.08	0.10	0.03	0.02	0.16	0.00	0.00	20.9
15	50	-0	2520	0	0	0	1695	--	--	16.08	16.08	0.10	0.03	0.02	0.16	0.00	0.00	20.9
16	50	-0	2871	0	0	0	1939	--	--	16.08	16.08	0.10	0.03	0.02	0.18	0.00	0.00	20.9
17	50	-0	2882	0	0	0	1946	--	--	16.08	16.08	0.10	0.03	0.02	0.18	0.00	0.00	20.9
18	50	-0	4308	0	0	0	2894	--	--	16.08	16.08	0.00	0.05	0.04	0.27	0.00	0.00	20.9
19	50	-0	8974	0	0	0	6141	--	--	16.08	16.08	0.00	0.10	0.07	0.56	0.00	0.00	20.9
20	50	-0	6177	0	0	0	4198	--	--	16.08	16.08	0.00	0.07	0.05	0.39	0.00	0.00	20.9
37	50	-0	1732	0	0	0	1110	--	--	16.08	16.08	0.00	0.02	0.01	0.11	0.00	0.00	20.9
38	50	-0	9508	0	0	0	6522	--	--	16.08	16.08	0.00	0.11	0.08	0.60	0.00	0.00	20.9
39	50	-0	4846	0	0	0	3284	--	--	16.08	16.08	0.00	0.06	0.04	0.30	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 216 NI 1605 NF 1606 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	1220	0	0	0	-1304	--	--	16.08	16.08	0.18	0.02	0.01	0.08	0.00	0.00	20.9
2	0	-0	706	0	0	0	-754	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
3	0	-0	707	0	0	0	-755	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
4	0	-0	1170	0	0	0	-1250	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
5	0	-0	1171	0	0	0	-1252	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
6	0	-0	867	0	0	0	-926	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
7	0	-0	871	0	0	0	-930	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
8	0	-0	1006	0	0	0	-1075	--	--	16.08	16.08	0.29	0.02	0.01	0.06	0.00	0.00	20.9
9	0	-0	1010	0	0	0	-1079	--	--	16.08	16.08	0.29	0.02	0.01	0.06	0.00	0.00	20.9
10	0	-0	706	0	0	0	-754	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
11	0	-0	707	0	0	0	-755	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
12	0	-0	1170	0	0	0	-1250	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
13	0	-0	1171	0	0	0	-1252	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
14	0	-0	867	0	0	0	-926	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
15	0	-0	871	0	0	0	-930	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
16	0	-0	1006	0	0	0	-1075	--	--	16.08	16.08	0.29	0.02	0.01	0.06	0.00	0.00	20.9
17	0	-0	1010	0	0	0	-1079	--	--	16.08	16.08	0.29	0.02	0.01	0.06	0.00	0.00	20.9
18	0	-0	1479	0	0	0	-1581	--	--	16.08	16.08	0.18	0.03	0.01	0.09	0.00	0.00	20.9
19	0	-0	3308	0	0	0	-3535	--	--	16.08	16.08	0.18	0.06	0.03	0.21	0.00	0.00	20.9
20	0	-0	2220	0	0	0	-2373	--	--	16.08	16.08	0.18	0.04	0.02	0.14	0.00	0.00	20.9
37	0	-0	487	0	0	0	-521	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9
38	0	-0	3535	0	0	0	-3778	--	--	16.08	16.08	0.18	0.06	0.03	0.22	0.00	0.00	20.9
39	0	-0	1722	0	0	0	-1840	--	--	16.08	16.08	0.18	0.03	0.01	0.11	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	25	-0	1220	0	0	0	1609	--	--	16.08	16.08	0.00	0.03	0.01	0.08	0.00	0.00	20.9
2	25	-0	706	0	0	0	930	--	--	16.08	16.08	0.10	0.02	0.01	0.04	0.00	0.00	20.9
3	25	-0	707	0	0	0	932	--	--	16.08	16.08	0.10	0.02	0.01	0.04	0.00	0.00	20.9
4	25	-0	1170	0	0	0	1543	--	--	16.08	16.08	0.10	0.03	0.01	0.07	0.00	0.00	20.9
5	25	-0	1171	0	0	0	1544	--	--	16.08	16.08	0.10	0.03	0.01	0.07	0.00	0.00	20.9
6	25	-0	867	0	0	0	1143	--	--	16.08	16.08	0.10	0.02	0.01	0.05	0.00	0.00	20.9
7	25	-0	871	0	0	0	1148	--	--	16.08	16.08	0.10	0.02	0.01	0.05	0.00	0.00	20.9
8	25	-0	1006	0	0	0	1327	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9
9	25	-0	1010	0	0	0	1332	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9
10	25	-0	706	0	0	0	930	--	--	16.08	16.08	0.10	0.02	0.01	0.04	0.00	0.00	20.9
11	25	-0	707	0	0	0	932	--	--	16.08	16.08	0.10	0.02	0.01	0.04	0.00	0.00	20.9
12	25	-0	1170	0	0	0	1543	--	--	16.08	16.08	0.10	0.03	0.01	0.07	0.00	0.00	20.9
13	25	-0	1171	0	0	0	1544	--	--	16.08	16.08	0.10	0.03	0.01	0.07	0.00	0.00	20.9
14	25	-0	867	0	0	0	1143	--	--	16.08	16.08	0.10	0.02	0.01	0.05	0.00	0.00	20.9
15	25	-0	871	0	0	0	1148	--	--	16.08	16.08	0.10	0.02	0.01	0.05	0.00	0.00	20.9
16	25	-0	1006	0	0	0	1327	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9
17	25	-0	1010	0	0	0	1332	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9
18	25	-0	1479	0	0	0	1950	--	--	16.08	16.08	0.00	0.03	0.01	0.09	0.00	0.00	20.9
19	25	-0	3308	0	0	0	4362	--	--	16.08	16.08	0.00	0.07	0.03	0.21	0.00	0.00	20.9
20	25	-0	2220	0	0	0	2928	--	--	16.08	16.08	0.00	0.05	0.02	0.14	0.00	0.00	20.9
37	25	-0	487	0	0	0	642	--	--	16.08	16.08	0.00	0.01	0.00	0.03	0.00	0.00	20.9
38	25	-0	3535	0	0	0	4662	--	--	16.08	16.08	0.00	0.08	0.03	0.22	0.00	0.00	20.9
39	25	-0	1722	0	0	0	2271	--	--	16.08	16.08	0.00	0.04	0.01	0.11	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	50	-0	1220	0	0	0	610	--	--	16.08	16.08	0.00	0.01	0.01	0.08	0.00	0.00	20.9
2	50	-0	706	0	0	0	353	--	--	16.08	16.08	0.10	0.01	0.01	0.04	0.00	0.00	20.9
3	50	-0	707	0	0	0	353	--	--	16.08	16.08	0.10	0.01	0.01	0.04	0.00	0.00	20.9
4	50	-0	1170	0	0	0	585	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
5	50	-0	1171	0	0	0	586	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
6	50	-0	867	0	0	0	433	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
7	50	-0	871	0	0	0	435	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
8	50	-0	1006	0	0	0	503	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
9	50	-0	1010	0	0	0	505	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
10	50	-0	706	0	0	0	353	--	--	16.08	16.08	0.10	0.01	0.01	0.04	0.00	0.00	20.9
11	50	-0	707	0	0	0	353	--	--	16.08	16.08	0.10	0.01	0.01	0.04	0.00	0.00	20.9
12	50	-0	1170	0	0	0	585	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
13	50	-0	1171	0	0	0	586	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
14	50	-0	867	0	0	0	433	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
15	50	-0	871	0	0	0	435	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
16	50	-0	1006	0	0	0	503	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
17	50	-0	1010	0	0	0	505	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
18	50	-0	1479	0	0	0	740	--	--	16.08	16.08	0.00	0.01	0.01	0.09	0.00	0.00	20.9
19	50	-0	3308	0	0	0	1654	--	--	16.08	16.08	0.00	0.03	0.03	0.21	0.00	0.00	20.9
20	50	-0	2220	0	0	0	1110	--	--	16.08	16.08	0.00	0.02	0.02	0.14	0.00	0.00	20.9
37	50	-0	487	0	0	0	243	--	--	16.08	16.08	0.00	0.00	0.00	0.03	0.00	0.00	20.9
38	50	-0	3535	0	0	0	1768	--	--	16.08	16.08	0.00	0.03	0.03	0.22	0.00	0.00	20.9
39	50	-0	1722	0	0	0	861	--	--	16.08	16.08	0.00	0.01	0.01	0.11	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 217 NI 1693 NF 1698 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-533	0	0	0	107	--	--	16.08	16.08	0.00	0.00	0.00	0.03	0.00	0.00	20.9
2	0	-0	-435	0	0	0	87	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
3	0	-0	-437	0	0	0	87	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
4	0	-0	-383	0	0	0	77	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
5	0	-0	-384	0	0	0	77	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
6	0	-0	-415	0	0	0	83	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
7	0	-0	-421	0	0	0	84	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
8	0	-0	-399	0	0	0	80	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
9	0	-0	-405	0	0	0	81	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
10	0	-0	-435	0	0	0	87	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
11	0	-0	-437	0	0	0	87	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
12	0	-0	-383	0	0	0	77	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
13	0	-0	-384	0	0	0	77	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
14	0	-0	-415	0	0	0	83	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
15	0	-0	-421	0	0	0	84	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
16	0	-0	-399	0	0	0	80	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
17	0	-0	-405	0	0	0	81	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
18	0	-0	-806	0	0	0	161	--	--	16.08	16.08	0.00	0.00	0.01	0.05	0.00	0.00	20.9
19	0	-0	-632	0	0	0	126	--	--	16.08	16.08	0.00	0.00	0.01	0.04	0.00	0.00	20.9
20	0	-0	-696	0	0	0	139	--	--	16.08	16.08	0.00	0.00	0.01	0.04	0.00	0.00	20.9
37	0	-0	-803	0	0	0	161	--	--	16.08	16.08	0.00	0.00	0.01	0.05	0.00	0.00	20.9
38	0	-0	-513	0	0	0	103	--	--	16.08	16.08	0.00	0.00	0.00	0.03	0.00	0.00	20.9
39	0	-0	-620	0	0	0	124	--	--	16.08	16.08	0.00	0.00	0.01	0.04	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	10	-0	-533	0	0	0	107	--	--	16.08	16.08	0.00	0.00	0.00	0.03	0.00	0.00	20.9
2	10	-0	-435	0	0	0	87	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
3	10	-0	-437	0	0	0	87	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
4	10	-0	-383	0	0	0	77	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
5	10	-0	-384	0	0	0	77	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
6	10	-0	-415	0	0	0	83	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
7	10	-0	-421	0	0	0	84	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
8	10	-0	-399	0	0	0	80	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
9	10	-0	-405	0	0	0	81	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
10	10	-0	-435	0	0	0	87	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
11	10	-0	-437	0	0	0	87	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
12	10	-0	-383	0	0	0	77	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
13	10	-0	-384	0	0	0	77	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
14	10	-0	-415	0	0	0	83	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
15	10	-0	-421	0	0	0	84	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
16	10	-0	-399	0	0	0	80	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
17	10	-0	-405	0	0	0	81	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
18	10	-0	-806	0	0	0	161	--	--	16.08	16.08	0.00	0.00	0.01	0.05	0.00	0.00	20.9
19	10	-0	-632	0	0	0	126	--	--	16.08	16.08	0.00	0.00	0.01	0.04	0.00	0.00	20.9
20	10	-0	-696	0	0	0	139	--	--	16.08	16.08	0.00	0.00	0.01	0.04	0.00	0.00	20.9
37	10	-0	-803	0	0	0	161	--	--	16.08	16.08	0.00	0.00	0.01	0.05	0.00	0.00	20.9
38	10	-0	-513	0	0	0	103	--	--	16.08	16.08	0.00	0.00	0.00	0.03	0.00	0.00	20.9
39	10	-0	-620	0	0	0	124	--	--	16.08	16.08	0.00	0.00	0.01	0.04	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	20	-0	-533	0	0	0	-569	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9
2	20	-0	-435	0	0	0	-465	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
3	20	-0	-437	0	0	0	-467	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
4	20	-0	-383	0	0	0	-409	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
5	20	-0	-384	0	0	0	-411	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
6	20	-0	-415	0	0	0	-443	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
7	20	-0	-421	0	0	0	-450	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
8	20	-0	-399	0	0	0	-426	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
9	20	-0	-405	0	0	0	-433	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
10	20	-0	-435	0	0	0	-465	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
11	20	-0	-437	0	0	0	-467	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
12	20	-0	-383	0	0	0	-409	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
13	20	-0	-384	0	0	0	-411	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
14	20	-0	-415	0	0	0	-443	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
15	20	-0	-421	0	0	0	-450	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
16	20	-0	-399	0	0	0	-426	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
17	20	-0	-405	0	0	0	-433	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
18	20	-0	-806	0	0	0	-862	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9
19	20	-0	-632	0	0	0	-676	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
20	20	-0	-696	0	0	0	-744	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
37	20	-0	-803	0	0	0	-858	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9
38	20	-0	-513	0	0	0	-549	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9
39	20	-0	-620	0	0	0	-663	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 218 NI 1694 NF 1693 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-7519	0	0	0	1921	--	--	16.08	16.08	0.00	0.03	0.06	0.47	0.00	0.00	20.9
2	0	-0	-5516	0	0	0	1638	--	--	16.08	16.08	0.10	0.03	0.05	0.35	0.00	0.00	20.9
3	0	-0	-5528	0	0	0	1674	--	--	16.08	16.08	0.10	0.03	0.05	0.35	0.00	0.00	20.9
4	0	-0	-6039	0	0	0	1281	--	--	16.08	16.08	0.10	0.02	0.05	0.38	0.00	0.00	20.9
5	0	-0	-6051	0	0	0	1317	--	--	16.08	16.08	0.10	0.02	0.05	0.38	0.00	0.00	20.9
6	0	-0	-5685	0	0	0	1471	--	--	16.08	16.08	0.10	0.03	0.05	0.36	0.00	0.00	20.9
7	0	-0	-5726	0	0	0	1591	--	--	16.08	16.08	0.10	0.03	0.05	0.36	0.00	0.00	20.9
8	0	-0	-5842	0	0	0	1364	--	--	16.08	16.08	0.10	0.02	0.05	0.37	0.00	0.00	20.9
9	0	-0	-5883	0	0	0	1484	--	--	16.08	16.08	0.10	0.03	0.05	0.37	0.00	0.00	20.9
10	0	-0	-5516	0	0	0	1638	--	--	16.08	16.08	0.10	0.03	0.05	0.35	0.00	0.00	20.9

11	0	-0	-5528	0	0	0	1674	--	--	16.08	16.08	0.10	0.03	0.05	0.35	0.00	0.00	20.9
12	0	-0	-6039	0	0	0	1281	--	--	16.08	16.08	0.10	0.02	0.05	0.38	0.00	0.00	20.9
13	0	-0	-6051	0	0	0	1317	--	--	16.08	16.08	0.10	0.02	0.05	0.38	0.00	0.00	20.9
14	0	-0	-5685	0	0	0	1471	--	--	16.08	16.08	0.10	0.03	0.05	0.36	0.00	0.00	20.9
15	0	-0	-5726	0	0	0	1591	--	--	16.08	16.08	0.10	0.03	0.05	0.36	0.00	0.00	20.9
16	0	-0	-5842	0	0	0	1364	--	--	16.08	16.08	0.10	0.02	0.05	0.37	0.00	0.00	20.9
17	0	-0	-5883	0	0	0	1484	--	--	16.08	16.08	0.10	0.03	0.05	0.37	0.00	0.00	20.9
18	0	-0	-7190	0	0	0	3374	--	--	16.08	16.08	0.00	0.06	0.06	0.45	0.00	0.00	20.9
19	0	-0	-10350	0	0	0	1885	--	--	16.08	16.08	0.00	0.03	0.09	0.65	0.00	0.00	20.9
20	0	-0	-8620	0	0	0	2611	--	--	16.08	16.08	0.00	0.04	0.07	0.54	0.00	0.00	20.9
37	0	-0	-5745	0	0	0	3639	--	--	16.08	16.08	0.00	0.06	0.05	0.36	0.00	0.00	20.9
38	0	-0	-11010	0	0	0	1157	--	--	16.08	16.08	0.00	0.02	0.09	0.69	0.00	0.00	20.9
39	0	-0	-8128	0	0	0	2367	--	--	16.08	16.08	0.00	0.04	0.07	0.51	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	10	-0	-7519	0	0	0	1921	--	--	16.08	16.08	0.00	0.03	0.06	0.47	0.00	0.00	20.9
2	10	-0	-5516	0	0	0	1638	--	--	16.08	16.08	0.10	0.03	0.05	0.35	0.00	0.00	20.9
3	10	-0	-5528	0	0	0	1674	--	--	16.08	16.08	0.10	0.03	0.05	0.35	0.00	0.00	20.9
4	10	-0	-6039	0	0	0	1281	--	--	16.08	16.08	0.10	0.02	0.05	0.38	0.00	0.00	20.9
5	10	-0	-6051	0	0	0	1317	--	--	16.08	16.08	0.10	0.02	0.05	0.38	0.00	0.00	20.9
6	10	-0	-5685	0	0	0	1471	--	--	16.08	16.08	0.10	0.03	0.05	0.36	0.00	0.00	20.9
7	10	-0	-5726	0	0	0	1591	--	--	16.08	16.08	0.10	0.03	0.05	0.36	0.00	0.00	20.9
8	10	-0	-5842	0	0	0	1364	--	--	16.08	16.08	0.10	0.02	0.05	0.37	0.00	0.00	20.9
9	10	-0	-5883	0	0	0	1484	--	--	16.08	16.08	0.10	0.03	0.05	0.37	0.00	0.00	20.9
10	10	-0	-5516	0	0	0	1638	--	--	16.08	16.08	0.10	0.03	0.05	0.35	0.00	0.00	20.9
11	10	-0	-5528	0	0	0	1674	--	--	16.08	16.08	0.10	0.03	0.05	0.35	0.00	0.00	20.9
12	10	-0	-6039	0	0	0	1281	--	--	16.08	16.08	0.10	0.02	0.05	0.38	0.00	0.00	20.9
13	10	-0	-6051	0	0	0	1317	--	--	16.08	16.08	0.10	0.02	0.05	0.38	0.00	0.00	20.9
14	10	-0	-5685	0	0	0	1471	--	--	16.08	16.08	0.10	0.03	0.05	0.36	0.00	0.00	20.9
15	10	-0	-5726	0	0	0	1591	--	--	16.08	16.08	0.10	0.03	0.05	0.36	0.00	0.00	20.9
16	10	-0	-5842	0	0	0	1364	--	--	16.08	16.08	0.10	0.02	0.05	0.37	0.00	0.00	20.9
17	10	-0	-5883	0	0	0	1484	--	--	16.08	16.08	0.10	0.03	0.05	0.37	0.00	0.00	20.9
18	10	-0	-7190	0	0	0	3374	--	--	16.08	16.08	0.00	0.06	0.06	0.45	0.00	0.00	20.9
19	10	-0	-10350	0	0	0	1885	--	--	16.08	16.08	0.00	0.03	0.09	0.65	0.00	0.00	20.9
20	10	-0	-8620	0	0	0	2611	--	--	16.08	16.08	0.00	0.04	0.07	0.54	0.00	0.00	20.9
37	10	-0	-5745	0	0	0	3639	--	--	16.08	16.08	0.00	0.06	0.05	0.36	0.00	0.00	20.9
38	10	-0	-11010	0	0	0	1157	--	--	16.08	16.08	0.00	0.02	0.09	0.69	0.00	0.00	20.9
39	10	-0	-8128	0	0	0	2367	--	--	16.08	16.08	0.00	0.04	0.07	0.51	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	20	-0	-7519	0	0	0	417	--	--	16.08	16.08	0.00	0.01	0.06	0.47	0.00	0.00	20.9
2	20	-0	-5516	0	0	0	535	--	--	16.08	16.08	0.10	0.01	0.05	0.35	0.00	0.00	20.9
3	20	-0	-5528	0	0	0	568	--	--	16.08	16.08	0.10	0.01	0.05	0.35	0.00	0.00	20.9
4	20	-0	-6039	0	0	0	74	--	--	16.08	16.08	0.10	0.00	0.05	0.38	0.00	0.00	20.9
5	20	-0	-6051	0	0	0	107	--	--	16.08	16.08	0.10	0.00	0.05	0.38	0.00	0.00	20.9
6	20	-0	-5685	0	0	0	334	--	--	16.08	16.08	0.10	0.01	0.05	0.36	0.00	0.00	20.9
7	20	-0	-5726	0	0	0	446	--	--	16.08	16.08	0.10	0.01	0.05	0.36	0.00	0.00	20.9
8	20	-0	-5842	0	0	0	196	--	--	16.08	16.08	0.10	0.00	0.05	0.37	0.00	0.00	20.9
9	20	-0	-5883	0	0	0	307	--	--	16.08	16.08	0.10	0.01	0.05	0.37	0.00	0.00	20.9
10	20	-0	-5516	0	0	0	535	--	--	16.08	16.08	0.10	0.01	0.05	0.35	0.00	0.00	20.9
11	20	-0	-5528	0	0	0	568	--	--	16.08	16.08	0.10	0.01	0.05	0.35	0.00	0.00	20.9
12	20	-0	-6039	0	0	0	74	--	--	16.08	16.08	0.10	0.00	0.05	0.38	0.00	0.00	20.9
13	20	-0	-6051	0	0	0	107	--	--	16.08	16.08	0.10	0.00	0.05	0.38	0.00	0.00	20.9
14	20	-0	-5685	0	0	0	334	--	--	16.08	16.08	0.10	0.01	0.05	0.36	0.00	0.00	20.9
15	20	-0	-5726	0	0	0	446	--	--	16.08	16.08	0.10	0.01	0.05	0.36	0.00	0.00	20.9
16	20	-0	-5842	0	0	0	196	--	--	16.08	16.08	0.10	0.00	0.05	0.37	0.00	0.00	20.9
17	20	-0	-5883	0	0	0	307	--	--	16.08	16.08	0.10	0.01	0.05	0.37	0.00	0.00	20.9
18	20	-0	-7190	0	0	0	1936	--	--	16.08	16.08	0.00	0.03	0.06	0.45	0.00	0.00	20.9
19	20	-0	-10350	0	0	0	-185	--	--	16.08	16.08	0.18	0.00	0.09	0.65	0.00	0.00	20.9
20	20	-0	-8620	0	0	0	887	--	--	16.08	16.08	0.00	0.02	0.07	0.54	0.00	0.00	20.9
37	20	-0	-5745	0	0	0	2490	--	--	16.08	16.08	0.00	0.04	0.05	0.36	0.00	0.00	20.9
38	20	-0	-11010	0	0	0	-1045	--	--	16.08	16.08	0.18	0.02	0.09	0.69	0.00	0.00	20.9
39	20	-0	-8128	0	0	0	741	--	--	16.08	16.08	0.00	0.01	0.07	0.51	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 219 NI 1695 NF 1694 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	1193	0	0	0	-33	--	--	16.08	16.08	0.18	0.00	0.01	0.07	0.00	0.00	20.9
2	0	-0	434	0	0	0	-266	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
3	0	-0	440	0	0	0	-265	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
4	0	-0	1395	0	0	0	214	--	--	16.08	16.08	0.10	0.00	0.01	0.09	0.00	0.00	20.9
5	0	-0	1401	0	0	0	215	--	--	16.08	16.08	0.10	0.00	0.01	0.09	0.00	0.00	20.9
6	0	-0	762	0	0	0	-99	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
7	0	-0	784	0	0	0	-96	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
8	0	-0	1051	0	0	0	45	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
9	0	-0	1073	0	0	0	48	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
10	0	-0	434	0	0	0	-266	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
11	0	-0	440	0	0	0	-265	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
12	0	-0	1395	0	0	0	214	--	--	16.08	16.08	0.10	0.00	0.01	0.09	0.00	0.00	20.9
13	0	-0	1401	0	0	0	215	--	--	16.08	16.08	0.10	0.00	0.01	0.09	0.00	0.00	20.9
14	0	-0	762	0	0	0	-99	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
15	0	-0	784	0	0	0	-96	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
16	0	-0	1051	0	0	0	45	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
17	0	-0	1073	0	0	0	48	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
18	0	-0	-3171	0	0	0	-3837	--	--	16.08	16.08	0.18	0.06	0.03	0.20	0.00	0.00	20.9
19	0	-0	1629	0	0	0	54	--	--	16.08	16.08	0.00	0.00	0.01	0.10	0.00	0.00	20.9
20	0	-0	-472	0	0	0	-1178	--	--	16.08	16.08	0.18	0.02	0.00	0.03	0.00	0.00	20.9
37	0	-0	-4128	0	0	0	-4737	--	--	16.08	16.08	0.18	0.08	0.03	0.26	0.00	0.00	20.9
38	0	-0	3870	0	0	0	1172	--	--	16.08	16.08	0.00	0.02	0.03	0.24	0.00	0.00	20.9
39	0	-0	369	0	0	0	-490	--	--	16.08	16.08	0.18	0.01	0.00	0.02	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	25	-0	1193	0	0	0	1540	--	--	16.08	16.08	0.00	0.03	0.01	0.07	0.00	0.00	20.9
2	25	-0	434	0	0	0	-266	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
3	25	-0	440	0	0	0	-265	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
4	25	-0	1395	0	0	0	2054	--	--	16.08	16.08	0.10	0.04	0.01	0.09	0.00	0.00	20.9
5	25	-0	1401	0	0	0	2063	--	--	16.08	16.08	0.10	0.04	0.01	0.09	0.00	0.00	20.9
6	25	-0	762	0	0	0	906	--	--	16.08	16.08	0.10	0.02	0.01	0.05	0.00	0.00	20.9

7	25	-0	784	0	0	0	938	--	--	16.08	16.08	0.10	0.02	0.01	0.05	0.00	0.00	20.9
8	25	-0	1051	0	0	0	1431	--	--	16.08	16.08	0.10	0.03	0.01	0.07	0.00	0.00	20.9
9	25	-0	1073	0	0	0	1463	--	--	16.08	16.08	0.10	0.03	0.01	0.07	0.00	0.00	20.9
10	25	-0	434	0	0	0	-266	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
11	25	-0	440	0	0	0	-265	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
12	25	-0	1395	0	0	0	2054	--	--	16.08	16.08	0.10	0.04	0.01	0.09	0.00	0.00	20.9
13	25	-0	1401	0	0	0	2063	--	--	16.08	16.08	0.10	0.04	0.01	0.09	0.00	0.00	20.9
14	25	-0	762	0	0	0	906	--	--	16.08	16.08	0.10	0.02	0.01	0.05	0.00	0.00	20.9
15	25	-0	784	0	0	0	938	--	--	16.08	16.08	0.10	0.02	0.01	0.05	0.00	0.00	20.9
16	25	-0	1051	0	0	0	1431	--	--	16.08	16.08	0.10	0.03	0.01	0.07	0.00	0.00	20.9
17	25	-0	1073	0	0	0	1463	--	--	16.08	16.08	0.10	0.03	0.01	0.07	0.00	0.00	20.9
18	25	-0	-3171	0	0	0	-3837	--	--	16.08	16.08	0.18	0.06	0.03	0.20	0.00	0.00	20.9
19	25	-0	1629	0	0	0	2203	--	--	16.08	16.08	0.00	0.04	0.01	0.10	0.00	0.00	20.9
20	25	-0	-472	0	0	0	-1178	--	--	16.08	16.08	0.18	0.02	0.00	0.03	0.00	0.00	20.9
37	25	-0	-4128	0	0	0	-4737	--	--	16.08	16.08	0.18	0.08	0.03	0.26	0.00	0.00	20.9
38	25	-0	3870	0	0	0	6276	--	--	16.08	16.08	0.00	0.11	0.03	0.24	0.00	0.00	20.9
39	25	-0	369	0	0	0	-490	--	--	16.08	16.08	0.18	0.01	0.00	0.02	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	50	-0	1193	0	0	0	563	--	--	16.08	16.08	0.00	0.01	0.01	0.07	0.00	0.00	20.9
2	50	-0	434	0	0	0	-266	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
3	50	-0	440	0	0	0	-265	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
4	50	-0	1395	0	0	0	911	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
5	50	-0	1401	0	0	0	916	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
6	50	-0	762	0	0	0	282	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
7	50	-0	784	0	0	0	296	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
8	50	-0	1051	0	0	0	570	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
9	50	-0	1073	0	0	0	584	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
10	50	-0	434	0	0	0	-266	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
11	50	-0	440	0	0	0	-265	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
12	50	-0	1395	0	0	0	911	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
13	50	-0	1401	0	0	0	916	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
14	50	-0	762	0	0	0	282	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
15	50	-0	784	0	0	0	296	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
16	50	-0	1051	0	0	0	570	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
17	50	-0	1073	0	0	0	584	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
18	50	-0	-3171	0	0	0	-3837	--	--	16.08	16.08	0.18	0.06	0.03	0.20	0.00	0.00	20.9
19	50	-0	1629	0	0	0	869	--	--	16.08	16.08	0.00	0.01	0.01	0.10	0.00	0.00	20.9
20	50	-0	-472	0	0	0	-1178	--	--	16.08	16.08	0.18	0.02	0.00	0.03	0.00	0.00	20.9
37	50	-0	-4128	0	0	0	-4737	--	--	16.08	16.08	0.18	0.08	0.03	0.26	0.00	0.00	20.9
38	50	-0	3870	0	0	0	3107	--	--	16.08	16.08	0.00	0.05	0.03	0.24	0.00	0.00	20.9
39	50	-0	369	0	0	0	-490	--	--	16.08	16.08	0.18	0.01	0.00	0.02	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 220 NI 1696 NF 1695 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	69	0	0	0	-68	--	--	16.08	16.08	0.18	0.00	0.00	0.00	0.00	0.00	20.9
2	0	-0	-314	0	0	0	-266	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
3	0	-0	-312	0	0	0	-265	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
4	0	-0	418	0	0	0	5	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
5	0	-0	420	0	0	0	5	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
6	0	-0	-60	0	0	0	-99	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
7	0	-0	-54	0	0	0	-96	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
8	0	-0	160	0	0	0	-35	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
9	0	-0	166	0	0	0	-35	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
10	0	-0	-314	0	0	0	-266	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
11	0	-0	-312	0	0	0	-265	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
12	0	-0	418	0	0	0	5	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
13	0	-0	420	0	0	0	5	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
14	0	-0	-60	0	0	0	-99	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
15	0	-0	-54	0	0	0	-96	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
16	0	-0	160	0	0	0	-35	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
17	0	-0	166	0	0	0	-35	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
18	0	-0	-3308	0	0	0	-2252	--	--	16.08	16.08	0.18	0.04	0.03	0.21	0.00	0.00	20.9
19	0	-0	227	0	0	0	-59	--	--	16.08	16.08	0.18	0.00	0.00	0.01	0.00	0.00	20.9
20	0	-0	-1303	0	0	0	-942	--	--	16.08	16.08	0.18	0.02	0.01	0.08	0.00	0.00	20.9
37	0	-0	-3960	0	0	0	-2672	--	--	16.08	16.08	0.18	0.04	0.03	0.25	0.00	0.00	20.9
38	0	-0	1932	0	0	0	206	--	--	16.08	16.08	0.00	0.00	0.02	0.12	0.00	0.00	20.9
39	0	-0	-619	0	0	0	-490	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	25	-0	69	0	0	0	-68	--	--	16.08	16.08	0.18	0.00	0.00	0.00	0.00	0.00	20.9
2	25	-0	-314	0	0	0	-266	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
3	25	-0	-312	0	0	0	-265	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
4	25	-0	418	0	0	0	556	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
5	25	-0	420	0	0	0	559	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
6	25	-0	-60	0	0	0	-99	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
7	25	-0	-54	0	0	0	-96	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
8	25	-0	160	0	0	0	175	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
9	25	-0	166	0	0	0	184	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
10	25	-0	-314	0	0	0	-266	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
11	25	-0	-312	0	0	0	-265	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
12	25	-0	418	0	0	0	556	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
13	25	-0	420	0	0	0	559	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
14	25	-0	-60	0	0	0	-99	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
15	25	-0	-54	0	0	0	-96	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
16	25	-0	160	0	0	0	175	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
17	25	-0	166	0	0	0	184	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
18	25	-0	-3308	0	0	0	-2252	--	--	16.08	16.08	0.18	0.04	0.03	0.21	0.00	0.00	20.9
19	25	-0	227	0	0	0	-59	--	--	16.08	16.08	0.18	0.00	0.00	0.01	0.00	0.00	20.9
20	25	-0	-1303	0	0	0	-942	--	--	16.08	16.08	0.18	0.02	0.01	0.08	0.00	0.00	20.9
37	25	-0	-3960	0	0	0	-2672	--	--	16.08	16.08	0.18	0.04	0.03	0.25	0.00	0.00	20.9
38	25	-0	1932	0	0	0	2754	--	--	16.08	16.08	0.00	0.05	0.02	0.12	0.00	0.00	20.9
39	25	-0	-619	0	0	0	-490	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	50	-0	69	0	0	0	-68	--	--	16.08	16.08	0.18	0.00	0.00	0.00	0.00	0.00	20.9
2	50	-0	-314	0	0	0	-266	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9

3	50	-0	-312	0	0	0	-265	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
4	50	-0	418	0	0	0	214	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
5	50	-0	420	0	0	0	215	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
6	50	-0	-60	0	0	0	-99	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
7	50	-0	-54	0	0	0	-96	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
8	50	-0	160	0	0	0	45	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
9	50	-0	166	0	0	0	48	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
10	50	-0	-314	0	0	0	-266	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
11	50	-0	-312	0	0	0	-265	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
12	50	-0	418	0	0	0	214	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
13	50	-0	420	0	0	0	215	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
14	50	-0	-60	0	0	0	-99	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
15	50	-0	-54	0	0	0	-96	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
16	50	-0	160	0	0	0	45	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
17	50	-0	166	0	0	0	48	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
18	50	-0	-3308	0	0	0	-2252	--	--	16.08	16.08	0.18	0.04	0.03	0.21	0.00	0.00	20.9
19	50	-0	227	0	0	0	54	--	--	16.08	16.08	0.00	0.00	0.00	0.01	0.00	0.00	20.9
20	50	-0	-1303	0	0	0	-942	--	--	16.08	16.08	0.18	0.02	0.01	0.08	0.00	0.00	20.9
37	50	-0	-3960	0	0	0	-2672	--	--	16.08	16.08	0.18	0.04	0.03	0.25	0.00	0.00	20.9
38	50	-0	1932	0	0	0	1172	--	--	16.08	16.08	0.00	0.02	0.02	0.12	0.00	0.00	20.9
39	50	-0	-619	0	0	0	-490	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 221 NI 1697 NF 1696 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--												Fx,M	Bielle	V,Mx			
	cm		daN			daN*m				cmq						cmq/m		cm
1	0	-0	-169	0	0	0	-68	--	--	16.08	16.08	0.18	0.00	0.00	0.01	0.00	0.00	20.9
2	0	-0	-273	0	0	0	-109	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
3	0	-0	-273	0	0	0	-109	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
4	0	-0	12	0	0	0	-13	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
5	0	-0	12	0	0	0	-13	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
6	0	-0	-173	0	0	0	-69	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
7	0	-0	-173	0	0	0	-69	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
8	0	-0	-87	0	0	0	-35	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
9	0	-0	-87	0	0	0	-35	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
10	0	-0	-273	0	0	0	-109	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
11	0	-0	-273	0	0	0	-109	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
12	0	-0	12	0	0	0	-13	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
13	0	-0	12	0	0	0	-13	--	--	16.08	16.08	0.29	0.00	0.00	0.00	0.00	0.00	20.9
14	0	-0	-173	0	0	0	-69	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
15	0	-0	-173	0	0	0	-69	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
16	0	-0	-87	0	0	0	-35	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
17	0	-0	-87	0	0	0	-35	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
18	0	-0	-1495	0	0	0	-598	--	--	16.08	16.08	0.18	0.01	0.01	0.09	0.00	0.00	20.9
19	0	-0	-148	0	0	0	-59	--	--	16.08	16.08	0.18	0.00	0.00	0.01	0.00	0.00	20.9
20	0	-0	-727	0	0	0	-291	--	--	16.08	16.08	0.18	0.00	0.01	0.05	0.00	0.00	20.9
37	0	-0	-1731	0	0	0	-692	--	--	16.08	16.08	0.18	0.01	0.01	0.11	0.00	0.00	20.9
38	0	-0	514	0	0	0	-550	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9
39	0	-0	-451	0	0	0	-180	--	--	16.08	16.08	0.18	0.00	0.00	0.03	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	20	-0	-169	0	0	0	-68	--	--	16.08	16.08	0.18	0.00	0.00	0.01	0.00	0.00	20.9
2	20	-0	-273	0	0	0	-109	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
3	20	-0	-273	0	0	0	-109	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
4	20	-0	12	0	0	0	16	--	--	16.08	16.08	0.10	0.00	0.00	0.00	0.00	0.00	20.9
5	20	-0	12	0	0	0	16	--	--	16.08	16.08	0.10	0.00	0.00	0.00	0.00	0.00	20.9
6	20	-0	-173	0	0	0	-69	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
7	20	-0	-173	0	0	0	-69	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
8	20	-0	-87	0	0	0	-35	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
9	20	-0	-87	0	0	0	-35	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
10	20	-0	-273	0	0	0	-109	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
11	20	-0	-273	0	0	0	-109	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
12	20	-0	12	0	0	0	16	--	--	16.08	16.08	0.10	0.00	0.00	0.00	0.00	0.00	20.9
13	20	-0	12	0	0	0	16	--	--	16.08	16.08	0.10	0.00	0.00	0.00	0.00	0.00	20.9
14	20	-0	-173	0	0	0	-69	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
15	20	-0	-173	0	0	0	-69	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
16	20	-0	-87	0	0	0	-35	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
17	20	-0	-87	0	0	0	-35	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
18	20	-0	-1495	0	0	0	-598	--	--	16.08	16.08	0.18	0.01	0.01	0.09	0.00	0.00	20.9
19	20	-0	-148	0	0	0	-59	--	--	16.08	16.08	0.18	0.00	0.00	0.01	0.00	0.00	20.9
20	20	-0	-727	0	0	0	-291	--	--	16.08	16.08	0.18	0.00	0.01	0.05	0.00	0.00	20.9
37	20	-0	-1731	0	0	0	-692	--	--	16.08	16.08	0.18	0.01	0.01	0.11	0.00	0.00	20.9
38	20	-0	514	0	0	0	653	--	--	16.08	16.08	0.00	0.01	0.00	0.03	0.00	0.00	20.9
39	20	-0	-451	0	0	0	-180	--	--	16.08	16.08	0.18	0.00	0.00	0.03	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	40	-0	-169	0	0	0	-68	--	--	16.08	16.08	0.18	0.00	0.00	0.01	0.00	0.00	20.9
2	40	-0	-273	0	0	0	-109	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
3	40	-0	-273	0	0	0	-109	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
4	40	-0	12	0	0	0	5	--	--	16.08	16.08	0.10	0.00	0.00	0.00	0.00	0.00	20.9
5	40	-0	12	0	0	0	5	--	--	16.08	16.08	0.10	0.00	0.00	0.00	0.00	0.00	20.9
6	40	-0	-173	0	0	0	-69	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
7	40	-0	-173	0	0	0	-69	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
8	40	-0	-87	0	0	0	-35	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
9	40	-0	-87	0	0	0	-35	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
10	40	-0	-273	0	0	0	-109	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
11	40	-0	-273	0	0	0	-109	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
12	40	-0	12	0	0	0	5	--	--	16.08	16.08	0.10	0.00	0.00	0.00	0.00	0.00	20.9
13	40	-0	12	0	0	0	5	--	--	16.08	16.08	0.10	0.00	0.00	0.00	0.00	0.00	20.9
14	40	-0	-173	0	0	0	-69	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
15	40	-0	-173	0	0	0	-69	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
16	40	-0	-87	0	0	0	-35	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
17	40	-0	-87	0	0	0	-35	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
18	40	-0	-1495	0	0	0	-598	--	--	16.08	16.08	0.18	0.01	0.01	0.09	0.00	0.00	20.9
19	40	-0	-148	0	0	0	-59	--	--	16.08	16.08	0.18	0.00	0.00	0.01	0.00	0.00	20.9
20	40	-0	-727	0	0	0	-291	--	--	16.08	16.08	0.18	0.00	0.01	0.05	0.00	0.00	20.9
37	40	-0	-1731	0	0	0	-692	--	--	16.08	16.08	0.18	0.01	0.01	0.11	0.00	0.00	20.9
38	40	-0	514	0	0	0	206	--	--	16.08	16.08	0.00	0.00	0.00	0.03	0.00	0.00	20.9
39	40	-0	-451	0	0	0	-180	--	--	16.08	16.08	0.18	0.00	0.00	0.03	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 222 NI 1631 NF 1624 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-472	0	0	0	189	--	--	16.08	16.08	0.00	0.00	0.00	0.03	0.00	0.00	20.9
2	0	-0	-477	0	0	0	191	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
3	0	-0	-474	0	0	0	190	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
4	0	-0	-252	0	0	0	101	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
5	0	-0	-249	0	0	0	100	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
6	0	-0	-402	0	0	0	161	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
7	0	-0	-392	0	0	0	157	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
8	0	-0	-335	0	0	0	134	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
9	0	-0	-324	0	0	0	130	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
10	0	-0	-477	0	0	0	191	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
11	0	-0	-474	0	0	0	190	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
12	0	-0	-252	0	0	0	101	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
13	0	-0	-249	0	0	0	100	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
14	0	-0	-402	0	0	0	161	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
15	0	-0	-392	0	0	0	157	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
16	0	-0	-335	0	0	0	134	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
17	0	-0	-324	0	0	0	130	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
18	0	-0	-798	0	0	0	319	--	--	16.08	16.08	0.00	0.01	0.01	0.05	0.00	0.00	20.9
19	0	-0	355	0	0	0	-142	--	--	16.08	16.08	0.18	0.00	0.00	0.02	0.00	0.00	20.9
20	0	-0	-251	0	0	0	100	--	--	16.08	16.08	0.00	0.00	0.00	0.02	0.00	0.00	20.9
37	0	-0	-1266	0	0	0	506	--	--	16.08	16.08	0.00	0.01	0.01	0.08	0.00	0.00	20.9
38	0	-0	656	0	0	0	-262	--	--	16.08	16.08	0.18	0.00	0.01	0.04	0.00	0.00	20.9
39	0	-0	-353	0	0	0	141	--	--	16.08	16.08	0.00	0.00	0.00	0.02	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	20	-0	-472	0	0	0	189	--	--	16.08	16.08	0.00	0.00	0.00	0.03	0.00	0.00	20.9
2	20	-0	-477	0	0	0	191	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
3	20	-0	-474	0	0	0	190	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
4	20	-0	-252	0	0	0	101	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
5	20	-0	-249	0	0	0	100	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
6	20	-0	-402	0	0	0	161	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
7	20	-0	-392	0	0	0	157	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
8	20	-0	-335	0	0	0	134	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
9	20	-0	-324	0	0	0	130	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
10	20	-0	-477	0	0	0	191	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
11	20	-0	-474	0	0	0	190	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
12	20	-0	-252	0	0	0	101	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
13	20	-0	-249	0	0	0	100	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
14	20	-0	-402	0	0	0	161	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
15	20	-0	-392	0	0	0	157	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
16	20	-0	-335	0	0	0	134	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
17	20	-0	-324	0	0	0	130	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
18	20	-0	-798	0	0	0	319	--	--	16.08	16.08	0.00	0.01	0.01	0.05	0.00	0.00	20.9
19	20	-0	355	0	0	0	-142	--	--	16.08	16.08	0.18	0.00	0.00	0.02	0.00	0.00	20.9
20	20	-0	-251	0	0	0	100	--	--	16.08	16.08	0.00	0.00	0.00	0.02	0.00	0.00	20.9
37	20	-0	-1266	0	0	0	506	--	--	16.08	16.08	0.00	0.01	0.01	0.08	0.00	0.00	20.9
38	20	-0	656	0	0	0	-262	--	--	16.08	16.08	0.18	0.00	0.01	0.04	0.00	0.00	20.9
39	20	-0	-353	0	0	0	141	--	--	16.08	16.08	0.00	0.00	0.00	0.02	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	40	-0	-472	0	0	0	-505	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9
2	40	-0	-477	0	0	0	-510	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
3	40	-0	-474	0	0	0	-507	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
4	40	-0	-252	0	0	0	-270	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
5	40	-0	-249	0	0	0	-267	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
6	40	-0	-402	0	0	0	-430	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
7	40	-0	-392	0	0	0	-419	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
8	40	-0	-335	0	0	0	-358	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
9	40	-0	-324	0	0	0	-347	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
10	40	-0	-477	0	0	0	-510	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
11	40	-0	-474	0	0	0	-507	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
12	40	-0	-252	0	0	0	-270	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
13	40	-0	-249	0	0	0	-267	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
14	40	-0	-402	0	0	0	-430	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
15	40	-0	-392	0	0	0	-419	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
16	40	-0	-335	0	0	0	-358	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
17	40	-0	-324	0	0	0	-347	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
18	40	-0	-798	0	0	0	-853	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9
19	40	-0	355	0	0	0	-142	--	--	16.08	16.08	0.18	0.00	0.00	0.02	0.00	0.00	20.9
20	40	-0	-251	0	0	0	-268	--	--	16.08	16.08	0.18	0.00	0.00	0.02	0.00	0.00	20.9
37	40	-0	-1266	0	0	0	-1353	--	--	16.08	16.08	0.18	0.02	0.01	0.08	0.00	0.00	20.9
38	40	-0	656	0	0	0	-262	--	--	16.08	16.08	0.18	0.00	0.01	0.04	0.00	0.00	20.9
39	40	-0	-353	0	0	0	-377	--	--	16.08	16.08	0.18	0.01	0.00	0.02	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 223 NI 1630 NF 1631 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-1610	0	0	0	994	--	--	16.08	16.08	0.00	0.02	0.01	0.10	0.00	0.00	20.9
2	0	-0	-1550	0	0	0	966	--	--	16.08	16.08	0.10	0.02	0.01	0.10	0.00	0.00	20.9
3	0	-0	-1542	0	0	0	961	--	--	16.08	16.08	0.10	0.02	0.01	0.10	0.00	0.00	20.9
4	0	-0	-936	0	0	0	569	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
5	0	-0	-928	0	0	0	564	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
6	0	-0	-1344	0	0	0	833	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
7	0	-0	-1318	0	0	0	816	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
8	0	-0	-1160	0	0	0	714	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
9	0	-0	-1134	0	0	0	697	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
10	0	-0	-1550	0	0	0	966	--	--	16.08	16.08	0.10	0.02	0.01	0.10	0.00	0.00	20.9

11	0	-0	-1542	0	0	0	961	--	--	16.08	16.08	0.10	0.02	0.01	0.10	0.00	0.00	20.9
12	0	-0	-936	0	0	0	569	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
13	0	-0	-928	0	0	0	564	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
14	0	-0	-1344	0	0	0	833	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
15	0	-0	-1318	0	0	0	816	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
16	0	-0	-1160	0	0	0	714	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
17	0	-0	-1134	0	0	0	697	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
18	0	-0	-2606	0	0	0	1622	--	--	16.08	16.08	0.00	0.03	0.02	0.16	0.00	0.00	20.9
19	0	-0	618	0	0	0	-451	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
20	0	-0	-1064	0	0	0	632	--	--	16.08	16.08	0.00	0.01	0.01	0.07	0.00	0.00	20.9
37	0	-0	-3886	0	0	0	2450	--	--	16.08	16.08	0.00	0.04	0.03	0.24	0.00	0.00	20.9
38	0	-0	1487	0	0	0	-1006	--	--	16.08	16.08	0.18	0.02	0.01	0.09	0.00	0.00	20.9
39	0	-0	-1315	0	0	0	799	--	--	16.08	16.08	0.00	0.01	0.01	0.08	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	25	-0	-1610	0	0	0	994	--	--	16.08	16.08	0.00	0.02	0.01	0.10	0.00	0.00	20.9
2	25	-0	-1550	0	0	0	966	--	--	16.08	16.08	0.10	0.02	0.01	0.10	0.00	0.00	20.9
3	25	-0	-1542	0	0	0	961	--	--	16.08	16.08	0.10	0.02	0.01	0.10	0.00	0.00	20.9
4	25	-0	-936	0	0	0	569	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
5	25	-0	-928	0	0	0	564	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
6	25	-0	-1344	0	0	0	833	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
7	25	-0	-1318	0	0	0	816	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
8	25	-0	-1160	0	0	0	714	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
9	25	-0	-1134	0	0	0	697	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
10	25	-0	-1550	0	0	0	966	--	--	16.08	16.08	0.10	0.02	0.01	0.10	0.00	0.00	20.9
11	25	-0	-1542	0	0	0	961	--	--	16.08	16.08	0.10	0.02	0.01	0.10	0.00	0.00	20.9
12	25	-0	-936	0	0	0	569	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
13	25	-0	-928	0	0	0	564	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
14	25	-0	-1344	0	0	0	833	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
15	25	-0	-1318	0	0	0	816	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
16	25	-0	-1160	0	0	0	714	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
17	25	-0	-1134	0	0	0	697	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
18	25	-0	-2606	0	0	0	1622	--	--	16.08	16.08	0.00	0.03	0.02	0.16	0.00	0.00	20.9
19	25	-0	618	0	0	0	-451	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
20	25	-0	-1064	0	0	0	632	--	--	16.08	16.08	0.00	0.01	0.01	0.07	0.00	0.00	20.9
37	25	-0	-3886	0	0	0	2450	--	--	16.08	16.08	0.00	0.04	0.03	0.24	0.00	0.00	20.9
38	25	-0	1487	0	0	0	-1006	--	--	16.08	16.08	0.18	0.02	0.01	0.09	0.00	0.00	20.9
39	25	-0	-1315	0	0	0	799	--	--	16.08	16.08	0.00	0.01	0.01	0.08	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	50	-0	-1610	0	0	0	189	--	--	16.08	16.08	0.00	0.00	0.01	0.10	0.00	0.00	20.9
2	50	-0	-1550	0	0	0	191	--	--	16.08	16.08	0.10	0.00	0.01	0.10	0.00	0.00	20.9
3	50	-0	-1542	0	0	0	190	--	--	16.08	16.08	0.10	0.00	0.01	0.10	0.00	0.00	20.9
4	50	-0	-936	0	0	0	101	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
5	50	-0	-928	0	0	0	100	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
6	50	-0	-1344	0	0	0	161	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
7	50	-0	-1318	0	0	0	157	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
8	50	-0	-1160	0	0	0	134	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
9	50	-0	-1134	0	0	0	130	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
10	50	-0	-1550	0	0	0	191	--	--	16.08	16.08	0.10	0.00	0.01	0.10	0.00	0.00	20.9
11	50	-0	-1542	0	0	0	190	--	--	16.08	16.08	0.10	0.00	0.01	0.10	0.00	0.00	20.9
12	50	-0	-936	0	0	0	101	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
13	50	-0	-928	0	0	0	100	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
14	50	-0	-1344	0	0	0	161	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
15	50	-0	-1318	0	0	0	157	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
16	50	-0	-1160	0	0	0	134	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
17	50	-0	-1134	0	0	0	130	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
18	50	-0	-2606	0	0	0	319	--	--	16.08	16.08	0.00	0.01	0.02	0.16	0.00	0.00	20.9
19	50	-0	618	0	0	0	-451	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
20	50	-0	-1064	0	0	0	100	--	--	16.08	16.08	0.00	0.00	0.01	0.07	0.00	0.00	20.9
37	50	-0	-3886	0	0	0	506	--	--	16.08	16.08	0.00	0.01	0.03	0.24	0.00	0.00	20.9
38	50	-0	1487	0	0	0	-1006	--	--	16.08	16.08	0.18	0.02	0.01	0.09	0.00	0.00	20.9
39	50	-0	-1315	0	0	0	141	--	--	16.08	16.08	0.00	0.00	0.01	0.08	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 224 NI 1623 NF 1630 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-2982	0	0	0	2485	--	--	16.08	16.08	0.00	0.04	0.02	0.19	0.00	0.00	20.9
2	0	-0	-2742	0	0	0	2337	--	--	16.08	16.08	0.10	0.04	0.02	0.17	0.00	0.00	20.9
3	0	-0	-2732	0	0	0	2326	--	--	16.08	16.08	0.10	0.04	0.02	0.17	0.00	0.00	20.9
4	0	-0	-1856	0	0	0	1497	--	--	16.08	16.08	0.10	0.03	0.02	0.12	0.00	0.00	20.9
5	0	-0	-1846	0	0	0	1487	--	--	16.08	16.08	0.10	0.03	0.02	0.12	0.00	0.00	20.9
6	0	-0	-2444	0	0	0	2055	--	--	16.08	16.08	0.10	0.04	0.02	0.15	0.00	0.00	20.9
7	0	-0	-2409	0	0	0	2020	--	--	16.08	16.08	0.10	0.04	0.02	0.15	0.00	0.00	20.9
8	0	-0	-2179	0	0	0	1803	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
9	0	-0	-2143	0	0	0	1768	--	--	16.08	16.08	0.10	0.03	0.02	0.13	0.00	0.00	20.9
10	0	-0	-2742	0	0	0	2337	--	--	16.08	16.08	0.10	0.04	0.02	0.17	0.00	0.00	20.9
11	0	-0	-2732	0	0	0	2326	--	--	16.08	16.08	0.10	0.04	0.02	0.17	0.00	0.00	20.9
12	0	-0	-1856	0	0	0	1497	--	--	16.08	16.08	0.10	0.03	0.02	0.12	0.00	0.00	20.9
13	0	-0	-1846	0	0	0	1487	--	--	16.08	16.08	0.10	0.03	0.02	0.12	0.00	0.00	20.9
14	0	-0	-2444	0	0	0	2055	--	--	16.08	16.08	0.10	0.04	0.02	0.15	0.00	0.00	20.9
15	0	-0	-2409	0	0	0	2020	--	--	16.08	16.08	0.10	0.04	0.02	0.15	0.00	0.00	20.9
16	0	-0	-2179	0	0	0	1803	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
17	0	-0	-2143	0	0	0	1768	--	--	16.08	16.08	0.10	0.03	0.02	0.13	0.00	0.00	20.9
18	0	-0	-4635	0	0	0	3940	--	--	16.08	16.08	0.00	0.07	0.04	0.29	0.00	0.00	20.9
19	0	-0	165	0	0	0	-533	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9
20	0	-0	-2314	0	0	0	1789	--	--	16.08	16.08	0.00	0.03	0.02	0.15	0.00	0.00	20.9
37	0	-0	-6486	0	0	0	5693	--	--	16.08	16.08	0.00	0.10	0.05	0.41	0.00	0.00	20.9
38	0	-0	1513	0	0	0	-1762	--	--	16.08	16.08	0.18	0.03	0.01	0.09	0.00	0.00	20.9
39	0	-0	-2618	0	0	0	2108	--	--	16.08	16.08	0.00	0.04	0.02	0.16	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	25	-0	-2982	0	0	0	2485	--	--	16.08	16.08	0.00	0.04	0.02	0.19	0.00	0.00	20.9
2	25	-0	-2742	0	0	0	2337	--	--	16.08	16.08	0.10	0.04	0.02	0.17	0.00	0.00	20.9
3	25	-0	-2732	0	0	0	2326	--	--	16.08	16.08	0.10	0.04	0.02	0.17	0.00	0.00	20.9
4	25	-0	-1856	0	0	0	1497	--	--	16.08	16.08	0.10	0.03	0.02	0.12	0.00	0.00	20.9
5	25	-0	-1846	0	0	0	1487	--	--	16.08	16.08	0.10	0.03	0.02	0.12	0.00	0.00	20.9
6	25	-0	-2444	0	0	0	2055	--	--	16.08	16.08	0.10	0.04	0.02	0.15	0.00	0.00	20.9

7	25	-0	-2409	0	0	0	2020	--	--	16.08	16.08	0.10	0.04	0.02	0.15	0.00	0.00	20.9
8	25	-0	-2179	0	0	0	1803	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
9	25	-0	-2143	0	0	0	1768	--	--	16.08	16.08	0.10	0.03	0.02	0.13	0.00	0.00	20.9
10	25	-0	-2742	0	0	0	2337	--	--	16.08	16.08	0.10	0.04	0.02	0.17	0.00	0.00	20.9
11	25	-0	-2732	0	0	0	2326	--	--	16.08	16.08	0.10	0.04	0.02	0.17	0.00	0.00	20.9
12	25	-0	-1856	0	0	0	1497	--	--	16.08	16.08	0.10	0.03	0.02	0.12	0.00	0.00	20.9
13	25	-0	-1846	0	0	0	1487	--	--	16.08	16.08	0.10	0.03	0.02	0.12	0.00	0.00	20.9
14	25	-0	-2444	0	0	0	2055	--	--	16.08	16.08	0.10	0.04	0.02	0.15	0.00	0.00	20.9
15	25	-0	-2409	0	0	0	2020	--	--	16.08	16.08	0.10	0.04	0.02	0.15	0.00	0.00	20.9
16	25	-0	-2179	0	0	0	1803	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
17	25	-0	-2143	0	0	0	1768	--	--	16.08	16.08	0.10	0.03	0.02	0.13	0.00	0.00	20.9
18	25	-0	-4635	0	0	0	3940	--	--	16.08	16.08	0.00	0.07	0.04	0.29	0.00	0.00	20.9
19	25	-0	165	0	0	0	-533	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9
20	25	-0	-2314	0	0	0	1789	--	--	16.08	16.08	0.00	0.03	0.02	0.15	0.00	0.00	20.9
37	25	-0	-6486	0	0	0	5693	--	--	16.08	16.08	0.00	0.10	0.05	0.41	0.00	0.00	20.9
38	25	-0	1513	0	0	0	-1762	--	--	16.08	16.08	0.18	0.03	0.01	0.09	0.00	0.00	20.9
39	25	-0	-2618	0	0	0	2108	--	--	16.08	16.08	0.00	0.04	0.02	0.16	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	50	-0	-2982	0	0	0	994	--	--	16.08	16.08	0.00	0.02	0.02	0.19	0.00	0.00	20.9
2	50	-0	-2742	0	0	0	966	--	--	16.08	16.08	0.10	0.02	0.02	0.17	0.00	0.00	20.9
3	50	-0	-2732	0	0	0	961	--	--	16.08	16.08	0.10	0.02	0.02	0.17	0.00	0.00	20.9
4	50	-0	-1856	0	0	0	569	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
5	50	-0	-1846	0	0	0	564	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
6	50	-0	-2444	0	0	0	833	--	--	16.08	16.08	0.10	0.01	0.02	0.15	0.00	0.00	20.9
7	50	-0	-2409	0	0	0	816	--	--	16.08	16.08	0.10	0.01	0.02	0.15	0.00	0.00	20.9
8	50	-0	-2179	0	0	0	714	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
9	50	-0	-2143	0	0	0	697	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
10	50	-0	-2742	0	0	0	966	--	--	16.08	16.08	0.10	0.02	0.02	0.17	0.00	0.00	20.9
11	50	-0	-2732	0	0	0	961	--	--	16.08	16.08	0.10	0.02	0.02	0.17	0.00	0.00	20.9
12	50	-0	-1856	0	0	0	569	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
13	50	-0	-1846	0	0	0	564	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
14	50	-0	-2444	0	0	0	833	--	--	16.08	16.08	0.10	0.01	0.02	0.15	0.00	0.00	20.9
15	50	-0	-2409	0	0	0	816	--	--	16.08	16.08	0.10	0.01	0.02	0.15	0.00	0.00	20.9
16	50	-0	-2179	0	0	0	714	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
17	50	-0	-2143	0	0	0	697	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
18	50	-0	-4635	0	0	0	1622	--	--	16.08	16.08	0.00	0.03	0.04	0.29	0.00	0.00	20.9
19	50	-0	165	0	0	0	-533	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9
20	50	-0	-2314	0	0	0	632	--	--	16.08	16.08	0.00	0.01	0.02	0.15	0.00	0.00	20.9
37	50	-0	-6486	0	0	0	2450	--	--	16.08	16.08	0.00	0.04	0.05	0.41	0.00	0.00	20.9
38	50	-0	1513	0	0	0	-1762	--	--	16.08	16.08	0.18	0.03	0.01	0.09	0.00	0.00	20.9
39	50	-0	-2618	0	0	0	799	--	--	16.08	16.08	0.00	0.01	0.02	0.16	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 225 NI 1622 NF 1623 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	7369	0	0	0	8356	--	--	16.08	16.08	0.00	0.14	0.06	0.46	0.00	0.00	20.9
2	0	-0	6125	0	0	0	5043	--	--	16.08	16.08	0.10	0.09	0.05	0.38	0.00	0.00	20.9
3	0	-0	6111	0	0	0	5115	--	--	16.08	16.08	0.10	0.09	0.05	0.38	0.00	0.00	20.9
4	0	-0	5226	0	0	0	7741	--	--	16.08	16.08	0.10	0.14	0.04	0.33	0.00	0.00	20.9
5	0	-0	5211	0	0	0	7813	--	--	16.08	16.08	0.10	0.14	0.04	0.33	0.00	0.00	20.9
6	0	-0	5827	0	0	0	5903	--	--	16.08	16.08	0.10	0.10	0.05	0.37	0.00	0.00	20.9
7	0	-0	5779	0	0	0	6144	--	--	16.08	16.08	0.10	0.11	0.05	0.36	0.00	0.00	20.9
8	0	-0	5557	0	0	0	6712	--	--	16.08	16.08	0.10	0.12	0.05	0.35	0.00	0.00	20.9
9	0	-0	5509	0	0	0	6953	--	--	16.08	16.08	0.10	0.12	0.05	0.35	0.00	0.00	20.9
10	0	-0	6125	0	0	0	5043	--	--	16.08	16.08	0.10	0.09	0.05	0.38	0.00	0.00	20.9
11	0	-0	6111	0	0	0	5115	--	--	16.08	16.08	0.10	0.09	0.05	0.38	0.00	0.00	20.9
12	0	-0	5226	0	0	0	7741	--	--	16.08	16.08	0.10	0.14	0.04	0.33	0.00	0.00	20.9
13	0	-0	5211	0	0	0	7813	--	--	16.08	16.08	0.10	0.14	0.04	0.33	0.00	0.00	20.9
14	0	-0	5827	0	0	0	5903	--	--	16.08	16.08	0.10	0.10	0.05	0.37	0.00	0.00	20.9
15	0	-0	5779	0	0	0	6144	--	--	16.08	16.08	0.10	0.11	0.05	0.36	0.00	0.00	20.9
16	0	-0	5557	0	0	0	6712	--	--	16.08	16.08	0.10	0.12	0.05	0.35	0.00	0.00	20.9
17	0	-0	5509	0	0	0	6953	--	--	16.08	16.08	0.10	0.12	0.05	0.35	0.00	0.00	20.9
18	0	-0	11020	0	0	0	8686	--	--	16.08	16.08	0.00	0.15	0.09	0.69	0.00	0.00	20.9
19	0	-0	5602	0	0	0	19590	--	--	16.08	16.08	0.00	0.33	0.05	0.35	0.00	0.00	20.9
20	0	-0	8138	0	0	0	13420	--	--	16.08	16.08	0.00	0.23	0.07	0.51	0.00	0.00	20.9
37	0	-0	12540	0	0	0	3168	--	--	16.08	16.08	0.00	0.05	0.10	0.79	0.00	0.00	20.9
38	0	-0	3508	0	0	0	21350	--	--	16.08	16.08	0.00	0.36	0.03	0.22	0.00	0.00	20.9
39	0	-0	7734	0	0	0	11060	--	--	16.08	16.08	0.00	0.19	0.06	0.49	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	10	-0	7369	0	0	0	16969	--	--	16.08	16.08	0.00	0.29	0.06	0.46	0.00	0.00	20.9
2	10	-0	6125	0	0	0	12202	--	--	16.08	16.08	0.10	0.22	0.05	0.38	0.00	0.00	20.9
3	10	-0	6111	0	0	0	12258	--	--	16.08	16.08	0.10	0.22	0.05	0.38	0.00	0.00	20.9
4	10	-0	5226	0	0	0	13849	--	--	16.08	16.08	0.10	0.25	0.04	0.33	0.00	0.00	20.9
5	10	-0	5211	0	0	0	13903	--	--	16.08	16.08	0.10	0.25	0.04	0.33	0.00	0.00	20.9
6	10	-0	5827	0	0	0	12713	--	--	16.08	16.08	0.10	0.23	0.05	0.37	0.00	0.00	20.9
7	10	-0	5779	0	0	0	12898	--	--	16.08	16.08	0.10	0.23	0.05	0.36	0.00	0.00	20.9
8	10	-0	5557	0	0	0	13207	--	--	16.08	16.08	0.10	0.23	0.05	0.35	0.00	0.00	20.9
9	10	-0	5509	0	0	0	13392	--	--	16.08	16.08	0.10	0.24	0.05	0.35	0.00	0.00	20.9
10	10	-0	6125	0	0	0	12202	--	--	16.08	16.08	0.10	0.22	0.05	0.38	0.00	0.00	20.9
11	10	-0	6111	0	0	0	12258	--	--	16.08	16.08	0.10	0.22	0.05	0.38	0.00	0.00	20.9
12	10	-0	5226	0	0	0	13849	--	--	16.08	16.08	0.10	0.25	0.04	0.33	0.00	0.00	20.9
13	10	-0	5211	0	0	0	13903	--	--	16.08	16.08	0.10	0.25	0.04	0.33	0.00	0.00	20.9
14	10	-0	5827	0	0	0	12713	--	--	16.08	16.08	0.10	0.23	0.05	0.37	0.00	0.00	20.9
15	10	-0	5779	0	0	0	12898	--	--	16.08	16.08	0.10	0.23	0.05	0.36	0.00	0.00	20.9
16	10	-0	5557	0	0	0	13207	--	--	16.08	16.08	0.10	0.23	0.05	0.35	0.00	0.00	20.9
17	10	-0	5509	0	0	0	13392	--	--	16.08	16.08	0.10	0.24	0.05	0.35	0.00	0.00	20.9
18	10	-0	11020	0	0	0	21566	--	--	16.08	16.08	0.00	0.37	0.09	0.69	0.00	0.00	20.9
19	10	-0	5602	0	0	0	26137	--	--	16.08	16.08	0.00	0.45	0.05	0.35	0.00	0.00	20.9
20	10	-0	8138	0	0	0	22932	--	--	16.08	16.08	0.00	0.39	0.07	0.51	0.00	0.00	20.9
37	10	-0	12540	0	0	0	17824	--	--	16.08	16.08	0.00	0.30	0.10	0.79	0.00	0.00	20.9
38	10	-0	3508	0	0	0	25449	--	--	16.08	16.08	0.00	0.43	0.03	0.22	0.00	0.00	20.9
39	10	-0	7734	0	0	0	20096	--	--	16.08	16.08	0.00	0.34	0.06	0.49	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	20	-0	7369	0	0	0	9830	--	--	16.08	16.08	0.00	0.17	0.06	0.46	0.00	0.00	20.9
2	20	-0	6125	0	0	0	6268	--	--	16.08	16.08	0.10	0.11	0.05	0.38	0.00	0.00	20.9

3	20	-0	6111	0	0	0	6338	--	--	16.08	16.08	0.10	0.11	0.05	0.38	0.00	0.00	20.9
4	20	-0	5226	0	0	0	8786	--	--	16.08	16.08	0.10	0.16	0.04	0.33	0.00	0.00	20.9
5	20	-0	5211	0	0	0	8855	--	--	16.08	16.08	0.10	0.16	0.04	0.33	0.00	0.00	20.9
6	20	-0	5827	0	0	0	7068	--	--	16.08	16.08	0.10	0.13	0.05	0.37	0.00	0.00	20.9
7	20	-0	5779	0	0	0	7300	--	--	16.08	16.08	0.10	0.13	0.05	0.36	0.00	0.00	20.9
8	20	-0	5557	0	0	0	7823	--	--	16.08	16.08	0.10	0.14	0.05	0.35	0.00	0.00	20.9
9	20	-0	5509	0	0	0	8055	--	--	16.08	16.08	0.10	0.14	0.05	0.35	0.00	0.00	20.9
10	20	-0	6125	0	0	0	6268	--	--	16.08	16.08	0.10	0.11	0.05	0.38	0.00	0.00	20.9
11	20	-0	6111	0	0	0	6338	--	--	16.08	16.08	0.10	0.11	0.05	0.38	0.00	0.00	20.9
12	20	-0	5226	0	0	0	8786	--	--	16.08	16.08	0.10	0.16	0.04	0.33	0.00	0.00	20.9
13	20	-0	5211	0	0	0	8855	--	--	16.08	16.08	0.10	0.16	0.04	0.33	0.00	0.00	20.9
14	20	-0	5827	0	0	0	7068	--	--	16.08	16.08	0.10	0.13	0.05	0.37	0.00	0.00	20.9
15	20	-0	5779	0	0	0	7300	--	--	16.08	16.08	0.10	0.13	0.05	0.36	0.00	0.00	20.9
16	20	-0	5557	0	0	0	7823	--	--	16.08	16.08	0.10	0.14	0.05	0.35	0.00	0.00	20.9
17	20	-0	5509	0	0	0	8055	--	--	16.08	16.08	0.10	0.14	0.05	0.35	0.00	0.00	20.9
18	20	-0	11020	0	0	0	10890	--	--	16.08	16.08	0.00	0.19	0.09	0.69	0.00	0.00	20.9
19	20	-0	5602	0	0	0	20710	--	--	16.08	16.08	0.00	0.35	0.05	0.35	0.00	0.00	20.9
20	20	-0	8138	0	0	0	15050	--	--	16.08	16.08	0.00	0.26	0.07	0.51	0.00	0.00	20.9
37	20	-0	12540	0	0	0	5676	--	--	16.08	16.08	0.00	0.10	0.10	0.79	0.00	0.00	20.9
38	20	-0	3508	0	0	0	22050	--	--	16.08	16.08	0.00	0.38	0.03	0.22	0.00	0.00	20.9
39	20	-0	7734	0	0	0	12600	--	--	16.08	16.08	0.00	0.21	0.06	0.49	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 226 NI 1629 NF 1622 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	7153	0	0	0	6223	--	--	16.08	16.08	0.00	0.11	0.06	0.45	0.00	0.00	20.9
2	0	-0	4625	0	0	0	3746	--	--	16.08	16.08	0.10	0.07	0.04	0.29	0.00	0.00	20.9
3	0	-0	4662	0	0	0	3787	--	--	16.08	16.08	0.10	0.07	0.04	0.29	0.00	0.00	20.9
4	0	-0	6342	0	0	0	5787	--	--	16.08	16.08	0.10	0.10	0.05	0.40	0.00	0.00	20.9
5	0	-0	6379	0	0	0	5828	--	--	16.08	16.08	0.10	0.10	0.05	0.40	0.00	0.00	20.9
6	0	-0	5183	0	0	0	4412	--	--	16.08	16.08	0.10	0.08	0.04	0.33	0.00	0.00	20.9
7	0	-0	5306	0	0	0	4549	--	--	16.08	16.08	0.10	0.08	0.04	0.33	0.00	0.00	20.9
8	0	-0	5698	0	0	0	5025	--	--	16.08	16.08	0.10	0.09	0.05	0.36	0.00	0.00	20.9
9	0	-0	5821	0	0	0	5161	--	--	16.08	16.08	0.10	0.09	0.05	0.37	0.00	0.00	20.9
10	0	-0	4625	0	0	0	3746	--	--	16.08	16.08	0.10	0.07	0.04	0.29	0.00	0.00	20.9
11	0	-0	4662	0	0	0	3787	--	--	16.08	16.08	0.10	0.07	0.04	0.29	0.00	0.00	20.9
12	0	-0	6342	0	0	0	5787	--	--	16.08	16.08	0.10	0.10	0.05	0.40	0.00	0.00	20.9
13	0	-0	6379	0	0	0	5828	--	--	16.08	16.08	0.10	0.10	0.05	0.40	0.00	0.00	20.9
14	0	-0	5183	0	0	0	4412	--	--	16.08	16.08	0.10	0.08	0.04	0.33	0.00	0.00	20.9
15	0	-0	5306	0	0	0	4549	--	--	16.08	16.08	0.10	0.08	0.04	0.33	0.00	0.00	20.9
16	0	-0	5698	0	0	0	5025	--	--	16.08	16.08	0.10	0.09	0.05	0.36	0.00	0.00	20.9
17	0	-0	5821	0	0	0	5161	--	--	16.08	16.08	0.10	0.09	0.05	0.37	0.00	0.00	20.9
18	0	-0	8188	0	0	0	6707	--	--	16.08	16.08	0.00	0.11	0.07	0.51	0.00	0.00	20.9
19	0	-0	14610	0	0	0	14850	--	--	16.08	16.08	0.00	0.25	0.12	0.92	0.00	0.00	20.9
20	0	-0	10830	0	0	0	10180	--	--	16.08	16.08	0.00	0.17	0.09	0.68	0.00	0.00	20.9
37	0	-0	4671	0	0	0	2511	--	--	16.08	16.08	0.00	0.04	0.04	0.29	0.00	0.00	20.9
38	0	-0	15370	0	0	0	16080	--	--	16.08	16.08	0.00	0.27	0.13	0.96	0.00	0.00	20.9
39	0	-0	9077	0	0	0	8297	--	--	16.08	16.08	0.00	0.14	0.07	0.57	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	30	-0	7153	0	0	0	16011	--	--	16.08	16.08	0.00	0.27	0.06	0.45	0.00	0.00	20.9
2	30	-0	4625	0	0	0	10076	--	--	16.08	16.08	0.10	0.18	0.04	0.29	0.00	0.00	20.9
3	30	-0	4662	0	0	0	10168	--	--	16.08	16.08	0.10	0.18	0.04	0.29	0.00	0.00	20.9
4	30	-0	6342	0	0	0	14468	--	--	16.08	16.08	0.10	0.26	0.05	0.40	0.00	0.00	20.9
5	30	-0	6379	0	0	0	14559	--	--	16.08	16.08	0.10	0.26	0.05	0.40	0.00	0.00	20.9
6	30	-0	5183	0	0	0	11506	--	--	16.08	16.08	0.10	0.20	0.04	0.33	0.00	0.00	20.9
7	30	-0	5306	0	0	0	11812	--	--	16.08	16.08	0.10	0.21	0.04	0.33	0.00	0.00	20.9
8	30	-0	5698	0	0	0	12824	--	--	16.08	16.08	0.10	0.23	0.05	0.36	0.00	0.00	20.9
9	30	-0	5821	0	0	0	13129	--	--	16.08	16.08	0.10	0.23	0.05	0.37	0.00	0.00	20.9
10	30	-0	4625	0	0	0	10076	--	--	16.08	16.08	0.10	0.18	0.04	0.29	0.00	0.00	20.9
11	30	-0	4662	0	0	0	10168	--	--	16.08	16.08	0.10	0.18	0.04	0.29	0.00	0.00	20.9
12	30	-0	6342	0	0	0	14468	--	--	16.08	16.08	0.10	0.26	0.05	0.40	0.00	0.00	20.9
13	30	-0	6379	0	0	0	14559	--	--	16.08	16.08	0.10	0.26	0.05	0.40	0.00	0.00	20.9
14	30	-0	5183	0	0	0	11506	--	--	16.08	16.08	0.10	0.20	0.04	0.33	0.00	0.00	20.9
15	30	-0	5306	0	0	0	11812	--	--	16.08	16.08	0.10	0.21	0.04	0.33	0.00	0.00	20.9
16	30	-0	5698	0	0	0	12824	--	--	16.08	16.08	0.10	0.23	0.05	0.36	0.00	0.00	20.9
17	30	-0	5821	0	0	0	13129	--	--	16.08	16.08	0.10	0.23	0.05	0.37	0.00	0.00	20.9
18	30	-0	8188	0	0	0	17914	--	--	16.08	16.08	0.00	0.31	0.07	0.51	0.00	0.00	20.9
19	30	-0	14610	0	0	0	34844	--	--	16.08	16.08	0.00	0.59	0.12	0.92	0.00	0.00	20.9
20	30	-0	10830	0	0	0	25005	--	--	16.08	16.08	0.00	0.43	0.09	0.68	0.00	0.00	20.9
37	30	-0	4671	0	0	0	8905	--	--	16.08	16.08	0.00	0.15	0.04	0.29	0.00	0.00	20.9
38	30	-0	15370	0	0	0	37117	--	--	16.08	16.08	0.00	0.63	0.13	0.94	0.00	0.00	20.9
39	30	-0	9077	0	0	0	20720	--	--	16.08	16.08	0.00	0.35	0.07	0.57	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	60	-0	7153	0	0	0	10510	--	--	16.08	16.08	0.00	0.18	0.06	0.45	0.00	0.00	20.9
2	60	-0	4625	0	0	0	6521	--	--	16.08	16.08	0.10	0.12	0.04	0.29	0.00	0.00	20.9
3	60	-0	4662	0	0	0	6584	--	--	16.08	16.08	0.10	0.12	0.04	0.29	0.00	0.00	20.9
4	60	-0	6342	0	0	0	9592	--	--	16.08	16.08	0.10	0.17	0.05	0.40	0.00	0.00	20.9
5	60	-0	6379	0	0	0	9655	--	--	16.08	16.08	0.10	0.17	0.05	0.40	0.00	0.00	20.9
6	60	-0	5183	0	0	0	7522	--	--	16.08	16.08	0.10	0.13	0.04	0.33	0.00	0.00	20.9
7	60	-0	5306	0	0	0	7733	--	--	16.08	16.08	0.10	0.14	0.04	0.33	0.00	0.00	20.9
8	60	-0	5698	0	0	0	8444	--	--	16.08	16.08	0.10	0.15	0.05	0.36	0.00	0.00	20.9
9	60	-0	5821	0	0	0	8654	--	--	16.08	16.08	0.10	0.15	0.05	0.37	0.00	0.00	20.9
10	60	-0	4625	0	0	0	6521	--	--	16.08	16.08	0.10	0.12	0.04	0.29	0.00	0.00	20.9
11	60	-0	4662	0	0	0	6584	--	--	16.08	16.08	0.10	0.12	0.04	0.29	0.00	0.00	20.9
12	60	-0	6342	0	0	0	9592	--	--	16.08	16.08	0.10	0.17	0.05	0.40	0.00	0.00	20.9
13	60	-0	6379	0	0	0	9655	--	--	16.08	16.08	0.10	0.17	0.05	0.40	0.00	0.00	20.9
14	60	-0	5183	0	0	0	7522	--	--	16.08	16.08	0.10	0.13	0.04	0.33	0.00	0.00	20.9
15	60	-0	5306	0	0	0	7733	--	--	16.08	16.08	0.10	0.14	0.04	0.33	0.00	0.00	20.9
16	60	-0	5698	0	0	0	8444	--	--	16.08	16.08	0.10	0.15	0.05	0.36	0.00	0.00	20.9
17	60	-0	5821	0	0	0	8654	--	--	16.08	16.08	0.10	0.15	0.05	0.37	0.00	0.00	20.9
18	60	-0	8188	0	0	0	11620	--	--	16.08	16.08	0.00	0.20	0.07	0.51	0.00	0.00	20.9
19	60	-0	14610	0	0	0	23610	--	--	16.08	16.08	0.00	0.40	0.12	0.92	0.00	0.00	20.9
20	60	-0	10830	0	0	0	16680	--	--	16.08	16.08	0.00	0.28	0.09	0.68	0.00	0.00	20.9
37	60	-0	4671	0	0	0	5314	--	--	16.08	16.08	0.00	0.09	0.04	0.29	0.00	0.00	20.9
38	60	-0	15370	0	0	0	25300	--	--	16.08	16.08	0.00	0.43	0.13	0.96	0.00	0.00	20.9
39	60	-0	9077	0	0	0	13740	--	--	16.08	16.08	0.00	0.23	0.07	0.57	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 227 NI 1628 NF 1629 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	5449	0	0	0	3498	--	--	16.08	16.08	0.00	0.06	0.04	0.34	0.00	0.00	20.9
2	0	-0	3391	0	0	0	2050	--	--	16.08	16.08	0.10	0.04	0.03	0.21	0.00	0.00	20.9
3	0	-0	3424	0	0	0	2075	--	--	16.08	16.08	0.10	0.04	0.03	0.21	0.00	0.00	20.9
4	0	-0	4960	0	0	0	3307	--	--	16.08	16.08	0.10	0.06	0.04	0.31	0.00	0.00	20.9
5	0	-0	4992	0	0	0	3332	--	--	16.08	16.08	0.10	0.06	0.04	0.31	0.00	0.00	20.9
6	0	-0	3902	0	0	0	2461	--	--	16.08	16.08	0.10	0.04	0.03	0.24	0.00	0.00	20.9
7	0	-0	4010	0	0	0	2544	--	--	16.08	16.08	0.10	0.05	0.03	0.25	0.00	0.00	20.9
8	0	-0	4373	0	0	0	2838	--	--	16.08	16.08	0.10	0.05	0.04	0.27	0.00	0.00	20.9
9	0	-0	4481	0	0	0	2921	--	--	16.08	16.08	0.10	0.05	0.04	0.28	0.00	0.00	20.9
10	0	-0	3391	0	0	0	2050	--	--	16.08	16.08	0.10	0.04	0.03	0.21	0.00	0.00	20.9
11	0	-0	3424	0	0	0	2075	--	--	16.08	16.08	0.10	0.04	0.03	0.21	0.00	0.00	20.9
12	0	-0	4960	0	0	0	3307	--	--	16.08	16.08	0.10	0.06	0.04	0.31	0.00	0.00	20.9
13	0	-0	4992	0	0	0	3332	--	--	16.08	16.08	0.10	0.06	0.04	0.31	0.00	0.00	20.9
14	0	-0	3902	0	0	0	2461	--	--	16.08	16.08	0.10	0.04	0.03	0.24	0.00	0.00	20.9
15	0	-0	4010	0	0	0	2544	--	--	16.08	16.08	0.10	0.05	0.03	0.25	0.00	0.00	20.9
16	0	-0	4373	0	0	0	2838	--	--	16.08	16.08	0.10	0.05	0.04	0.27	0.00	0.00	20.9
17	0	-0	4481	0	0	0	2921	--	--	16.08	16.08	0.10	0.05	0.04	0.28	0.00	0.00	20.9
18	0	-0	6040	0	0	0	3687	--	--	16.08	16.08	0.00	0.06	0.05	0.38	0.00	0.00	20.9
19	0	-0	12140	0	0	0	8776	--	--	16.08	16.08	0.00	0.15	0.10	0.76	0.00	0.00	20.9
20	0	-0	8611	0	0	0	5873	--	--	16.08	16.08	0.00	0.10	0.07	0.54	0.00	0.00	20.9
37	0	-0	2821	0	0	0	1101	--	--	16.08	16.08	0.00	0.02	0.02	0.18	0.00	0.00	20.9
38	0	-0	12990	0	0	0	9583	--	--	16.08	16.08	0.00	0.16	0.11	0.81	0.00	0.00	20.9
39	0	-0	7105	0	0	0	4744	--	--	16.08	16.08	0.00	0.08	0.06	0.45	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	25	-0	5449	0	0	0	10684	--	--	16.08	16.08	0.00	0.18	0.04	0.34	0.00	0.00	20.9
2	25	-0	3391	0	0	0	6522	--	--	16.08	16.08	0.10	0.12	0.03	0.21	0.00	0.00	20.9
3	25	-0	3424	0	0	0	6590	--	--	16.08	16.08	0.10	0.12	0.03	0.21	0.00	0.00	20.9
4	25	-0	4960	0	0	0	9848	--	--	16.08	16.08	0.10	0.17	0.04	0.31	0.00	0.00	20.9
5	25	-0	4992	0	0	0	9915	--	--	16.08	16.08	0.10	0.18	0.04	0.31	0.00	0.00	20.9
6	25	-0	3902	0	0	0	7607	--	--	16.08	16.08	0.10	0.13	0.03	0.24	0.00	0.00	20.9
7	25	-0	4010	0	0	0	7832	--	--	16.08	16.08	0.10	0.14	0.03	0.25	0.00	0.00	20.9
8	25	-0	4373	0	0	0	8605	--	--	16.08	16.08	0.10	0.15	0.04	0.27	0.00	0.00	20.9
9	25	-0	4481	0	0	0	8830	--	--	16.08	16.08	0.10	0.16	0.04	0.28	0.00	0.00	20.9
10	25	-0	3391	0	0	0	6522	--	--	16.08	16.08	0.10	0.12	0.03	0.21	0.00	0.00	20.9
11	25	-0	3424	0	0	0	6590	--	--	16.08	16.08	0.10	0.12	0.03	0.21	0.00	0.00	20.9
12	25	-0	4960	0	0	0	9848	--	--	16.08	16.08	0.10	0.17	0.04	0.31	0.00	0.00	20.9
13	25	-0	4992	0	0	0	9915	--	--	16.08	16.08	0.10	0.18	0.04	0.31	0.00	0.00	20.9
14	25	-0	3902	0	0	0	7607	--	--	16.08	16.08	0.10	0.13	0.03	0.24	0.00	0.00	20.9
15	25	-0	4010	0	0	0	7832	--	--	16.08	16.08	0.10	0.14	0.03	0.25	0.00	0.00	20.9
16	25	-0	4373	0	0	0	8605	--	--	16.08	16.08	0.10	0.15	0.04	0.27	0.00	0.00	20.9
17	25	-0	4481	0	0	0	8830	--	--	16.08	16.08	0.10	0.16	0.04	0.28	0.00	0.00	20.9
18	25	-0	6040	0	0	0	11652	--	--	16.08	16.08	0.00	0.20	0.05	0.38	0.00	0.00	20.9
19	25	-0	12140	0	0	0	24788	--	--	16.08	16.08	0.00	0.42	0.10	0.76	0.00	0.00	20.9
20	25	-0	8611	0	0	0	17230	--	--	16.08	16.08	0.00	0.29	0.07	0.54	0.00	0.00	20.9
37	25	-0	2821	0	0	0	4821	--	--	16.08	16.08	0.00	0.08	0.02	0.18	0.00	0.00	20.9
38	25	-0	12990	0	0	0	26715	--	--	16.08	16.08	0.00	0.46	0.11	0.81	0.00	0.00	20.9
39	25	-0	7105	0	0	0	14114	--	--	16.08	16.08	0.00	0.24	0.06	0.45	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	50	-0	5449	0	0	0	6223	--	--	16.08	16.08	0.00	0.11	0.04	0.34	0.00	0.00	20.9
2	50	-0	3391	0	0	0	3746	--	--	16.08	16.08	0.10	0.07	0.03	0.21	0.00	0.00	20.9
3	50	-0	3424	0	0	0	3787	--	--	16.08	16.08	0.10	0.07	0.03	0.21	0.00	0.00	20.9
4	50	-0	4960	0	0	0	5787	--	--	16.08	16.08	0.10	0.10	0.04	0.31	0.00	0.00	20.9
5	50	-0	4992	0	0	0	5828	--	--	16.08	16.08	0.10	0.10	0.04	0.31	0.00	0.00	20.9
6	50	-0	3902	0	0	0	4412	--	--	16.08	16.08	0.10	0.08	0.03	0.24	0.00	0.00	20.9
7	50	-0	4010	0	0	0	4549	--	--	16.08	16.08	0.10	0.08	0.03	0.25	0.00	0.00	20.9
8	50	-0	4373	0	0	0	5025	--	--	16.08	16.08	0.10	0.09	0.04	0.27	0.00	0.00	20.9
9	50	-0	4481	0	0	0	5161	--	--	16.08	16.08	0.10	0.09	0.04	0.28	0.00	0.00	20.9
10	50	-0	3391	0	0	0	3746	--	--	16.08	16.08	0.10	0.07	0.03	0.21	0.00	0.00	20.9
11	50	-0	3424	0	0	0	3787	--	--	16.08	16.08	0.10	0.07	0.03	0.21	0.00	0.00	20.9
12	50	-0	4960	0	0	0	5787	--	--	16.08	16.08	0.10	0.10	0.04	0.31	0.00	0.00	20.9
13	50	-0	4992	0	0	0	5828	--	--	16.08	16.08	0.10	0.10	0.04	0.31	0.00	0.00	20.9
14	50	-0	3902	0	0	0	4412	--	--	16.08	16.08	0.10	0.08	0.03	0.24	0.00	0.00	20.9
15	50	-0	4010	0	0	0	4549	--	--	16.08	16.08	0.10	0.08	0.03	0.25	0.00	0.00	20.9
16	50	-0	4373	0	0	0	5025	--	--	16.08	16.08	0.10	0.09	0.04	0.27	0.00	0.00	20.9
17	50	-0	4481	0	0	0	5161	--	--	16.08	16.08	0.10	0.09	0.04	0.28	0.00	0.00	20.9
18	50	-0	6040	0	0	0	6707	--	--	16.08	16.08	0.00	0.11	0.05	0.38	0.00	0.00	20.9
19	50	-0	12140	0	0	0	14850	--	--	16.08	16.08	0.00	0.25	0.10	0.76	0.00	0.00	20.9
20	50	-0	8611	0	0	0	10180	--	--	16.08	16.08	0.00	0.17	0.07	0.54	0.00	0.00	20.9
37	50	-0	2821	0	0	0	2511	--	--	16.08	16.08	0.00	0.04	0.02	0.18	0.00	0.00	20.9
38	50	-0	12990	0	0	0	16080	--	--	16.08	16.08	0.00	0.27	0.11	0.81	0.00	0.00	20.9
39	50	-0	7105	0	0	0	8297	--	--	16.08	16.08	0.00	0.14	0.06	0.45	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 228 NI 1627 NF 1628 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	3890	0	0	0	1554	--	--	16.08	16.08	0.00	0.03	0.03	0.24	0.00	0.00	20.9
2	0	-0	2332	0	0	0	884	--	--	16.08	16.08	0.10	0.02	0.02	0.15	0.00	0.00	20.9
3	0	-0	2358	0	0	0	896	--	--	16.08	16.08	0.10	0.02	0.02	0.15	0.00	0.00	20.9
4	0	-0	3626	0	0	0	1495	--	--	16.08	16.08	0.10	0.03	0.03	0.23	0.00	0.00	20.9
5	0	-0	3652	0	0	0	1506	--	--	16.08	16.08	0.10	0.03	0.03	0.23	0.00	0.00	20.9
6	0	-0	2755	0	0	0	1084	--	--	16.08	16.08	0.10	0.02	0.02	0.17	0.00	0.00	20.9
7	0	-0	2841	0	0	0	1123	--	--	16.08	16.08	0.10	0.02	0.02	0.18	0.00	0.00	20.9
8	0	-0	3143	0	0	0	1267	--	--	16.08	16.08	0.10	0.02	0.03	0.20	0.00	0.00	20.9
9	0	-0	3229	0	0	0	1306	--	--	16.08	16.08	0.10	0.02	0.03	0.20	0.00	0.00	20.9
10	0	-0	2332	0	0	0	884	--	--	16.08	16.08	0.10	0.02	0.02	0.15	0.00	0.00	20.9

11	0	-0	2358	0	0	0	896	--	--	16.08	16.08	0.10	0.02	0.02	0.15	0.00	0.00	20.9
12	0	-0	3626	0	0	0	1495	--	--	16.08	16.08	0.10	0.03	0.03	0.23	0.00	0.00	20.9
13	0	-0	3652	0	0	0	1506	--	--	16.08	16.08	0.10	0.03	0.03	0.23	0.00	0.00	20.9
14	0	-0	2755	0	0	0	1084	--	--	16.08	16.08	0.10	0.02	0.02	0.17	0.00	0.00	20.9
15	0	-0	2841	0	0	0	1123	--	--	16.08	16.08	0.10	0.02	0.02	0.18	0.00	0.00	20.9
16	0	-0	3143	0	0	0	1267	--	--	16.08	16.08	0.10	0.02	0.03	0.20	0.00	0.00	20.9
17	0	-0	3229	0	0	0	1306	--	--	16.08	16.08	0.10	0.02	0.03	0.20	0.00	0.00	20.9
18	0	-0	4179	0	0	0	1598	--	--	16.08	16.08	0.00	0.03	0.03	0.26	0.00	0.00	20.9
19	0	-0	9347	0	0	0	4102	--	--	16.08	16.08	0.00	0.07	0.08	0.59	0.00	0.00	20.9
20	0	-0	6386	0	0	0	2680	--	--	16.08	16.08	0.00	0.05	0.05	0.40	0.00	0.00	20.9
37	0	-0	1521	0	0	0	340	--	--	16.08	16.08	0.00	0.01	0.01	0.10	0.00	0.00	20.9
38	0	-0	10130	0	0	0	4515	--	--	16.08	16.08	0.00	0.08	0.08	0.64	0.00	0.00	20.9
39	0	-0	5198	0	0	0	2145	--	--	16.08	16.08	0.00	0.04	0.04	0.33	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	25	-0	3890	0	0	0	6683	--	--	16.08	16.08	0.00	0.11	0.03	0.24	0.00	0.00	20.9
2	25	-0	2332	0	0	0	3959	--	--	16.08	16.08	0.10	0.07	0.02	0.15	0.00	0.00	20.9
3	25	-0	2358	0	0	0	4005	--	--	16.08	16.08	0.10	0.07	0.02	0.15	0.00	0.00	20.9
4	25	-0	3626	0	0	0	6276	--	--	16.08	16.08	0.10	0.11	0.03	0.23	0.00	0.00	20.9
5	25	-0	3652	0	0	0	6322	--	--	16.08	16.08	0.10	0.11	0.03	0.23	0.00	0.00	20.9
6	25	-0	2755	0	0	0	4717	--	--	16.08	16.08	0.10	0.08	0.02	0.17	0.00	0.00	20.9
7	25	-0	2841	0	0	0	4870	--	--	16.08	16.08	0.10	0.09	0.02	0.18	0.00	0.00	20.9
8	25	-0	3143	0	0	0	5412	--	--	16.08	16.08	0.10	0.10	0.03	0.20	0.00	0.00	20.9
9	25	-0	3229	0	0	0	5564	--	--	16.08	16.08	0.10	0.10	0.03	0.20	0.00	0.00	20.9
10	25	-0	2332	0	0	0	3959	--	--	16.08	16.08	0.10	0.07	0.02	0.15	0.00	0.00	20.9
11	25	-0	2358	0	0	0	4005	--	--	16.08	16.08	0.10	0.07	0.02	0.15	0.00	0.00	20.9
12	25	-0	3626	0	0	0	6276	--	--	16.08	16.08	0.10	0.11	0.03	0.23	0.00	0.00	20.9
13	25	-0	3652	0	0	0	6322	--	--	16.08	16.08	0.10	0.11	0.03	0.23	0.00	0.00	20.9
14	25	-0	2755	0	0	0	4717	--	--	16.08	16.08	0.10	0.08	0.02	0.17	0.00	0.00	20.9
15	25	-0	2841	0	0	0	4870	--	--	16.08	16.08	0.10	0.09	0.02	0.18	0.00	0.00	20.9
16	25	-0	3143	0	0	0	5412	--	--	16.08	16.08	0.10	0.10	0.03	0.20	0.00	0.00	20.9
17	25	-0	3229	0	0	0	5564	--	--	16.08	16.08	0.10	0.10	0.03	0.20	0.00	0.00	20.9
18	25	-0	4179	0	0	0	7109	--	--	16.08	16.08	0.00	0.12	0.03	0.26	0.00	0.00	20.9
19	25	-0	9347	0	0	0	16429	--	--	16.08	16.08	0.00	0.28	0.08	0.59	0.00	0.00	20.9
20	25	-0	6386	0	0	0	11102	--	--	16.08	16.08	0.00	0.19	0.05	0.40	0.00	0.00	20.9
37	25	-0	1521	0	0	0	2346	--	--	16.08	16.08	0.00	0.04	0.01	0.10	0.00	0.00	20.9
38	25	-0	10130	0	0	0	17875	--	--	16.08	16.08	0.00	0.30	0.08	0.64	0.00	0.00	20.9
39	25	-0	5198	0	0	0	9000	--	--	16.08	16.08	0.00	0.15	0.04	0.33	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	50	-0	3890	0	0	0	3498	--	--	16.08	16.08	0.00	0.06	0.03	0.24	0.00	0.00	20.9
2	50	-0	2332	0	0	0	2050	--	--	16.08	16.08	0.10	0.04	0.02	0.15	0.00	0.00	20.9
3	50	-0	2358	0	0	0	2075	--	--	16.08	16.08	0.10	0.04	0.02	0.15	0.00	0.00	20.9
4	50	-0	3626	0	0	0	3307	--	--	16.08	16.08	0.10	0.06	0.03	0.23	0.00	0.00	20.9
5	50	-0	3652	0	0	0	3332	--	--	16.08	16.08	0.10	0.06	0.03	0.23	0.00	0.00	20.9
6	50	-0	2755	0	0	0	2461	--	--	16.08	16.08	0.10	0.04	0.02	0.17	0.00	0.00	20.9
7	50	-0	2841	0	0	0	2544	--	--	16.08	16.08	0.10	0.05	0.02	0.18	0.00	0.00	20.9
8	50	-0	3143	0	0	0	2838	--	--	16.08	16.08	0.10	0.05	0.03	0.20	0.00	0.00	20.9
9	50	-0	3229	0	0	0	2921	--	--	16.08	16.08	0.10	0.05	0.03	0.20	0.00	0.00	20.9
10	50	-0	2332	0	0	0	2050	--	--	16.08	16.08	0.10	0.04	0.02	0.15	0.00	0.00	20.9
11	50	-0	2358	0	0	0	2075	--	--	16.08	16.08	0.10	0.04	0.02	0.15	0.00	0.00	20.9
12	50	-0	3626	0	0	0	3307	--	--	16.08	16.08	0.10	0.06	0.03	0.23	0.00	0.00	20.9
13	50	-0	3652	0	0	0	3332	--	--	16.08	16.08	0.10	0.06	0.03	0.23	0.00	0.00	20.9
14	50	-0	2755	0	0	0	2461	--	--	16.08	16.08	0.10	0.04	0.02	0.17	0.00	0.00	20.9
15	50	-0	2841	0	0	0	2544	--	--	16.08	16.08	0.10	0.05	0.02	0.18	0.00	0.00	20.9
16	50	-0	3143	0	0	0	2838	--	--	16.08	16.08	0.10	0.05	0.03	0.20	0.00	0.00	20.9
17	50	-0	3229	0	0	0	2921	--	--	16.08	16.08	0.10	0.05	0.03	0.20	0.00	0.00	20.9
18	50	-0	4179	0	0	0	3687	--	--	16.08	16.08	0.00	0.06	0.03	0.26	0.00	0.00	20.9
19	50	-0	9347	0	0	0	8776	--	--	16.08	16.08	0.00	0.15	0.08	0.59	0.00	0.00	20.9
20	50	-0	6386	0	0	0	5873	--	--	16.08	16.08	0.00	0.10	0.05	0.40	0.00	0.00	20.9
37	50	-0	1521	0	0	0	1101	--	--	16.08	16.08	0.00	0.02	0.01	0.10	0.00	0.00	20.9
38	50	-0	10130	0	0	0	9583	--	--	16.08	16.08	0.00	0.16	0.08	0.64	0.00	0.00	20.9
39	50	-0	5198	0	0	0	4744	--	--	16.08	16.08	0.00	0.08	0.04	0.33	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 229 NI 1626 NF 1627 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	2331	0	0	0	388	--	--	16.08	16.08	0.00	0.01	0.02	0.15	0.00	0.00	20.9
2	0	-0	1343	0	0	0	212	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
3	0	-0	1360	0	0	0	215	--	--	16.08	16.08	0.10	0.00	0.01	0.09	0.00	0.00	20.9
4	0	-0	2226	0	0	0	382	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
5	0	-0	2243	0	0	0	385	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
6	0	-0	1632	0	0	0	268	--	--	16.08	16.08	0.10	0.00	0.01	0.10	0.00	0.00	20.9
7	0	-0	1689	0	0	0	278	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
8	0	-0	1897	0	0	0	319	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
9	0	-0	1954	0	0	0	329	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
10	0	-0	1343	0	0	0	212	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
11	0	-0	1360	0	0	0	215	--	--	16.08	16.08	0.10	0.00	0.01	0.09	0.00	0.00	20.9
12	0	-0	2226	0	0	0	382	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
13	0	-0	2243	0	0	0	385	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
14	0	-0	1632	0	0	0	268	--	--	16.08	16.08	0.10	0.00	0.01	0.10	0.00	0.00	20.9
15	0	-0	1689	0	0	0	278	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
16	0	-0	1897	0	0	0	319	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
17	0	-0	1954	0	0	0	329	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
18	0	-0	2423	0	0	0	386	--	--	16.08	16.08	0.00	0.01	0.02	0.15	0.00	0.00	20.9
19	0	-0	6023	0	0	0	1091	--	--	16.08	16.08	0.00	0.02	0.05	0.38	0.00	0.00	20.9
20	0	-0	3975	0	0	0	693	--	--	16.08	16.08	0.00	0.01	0.03	0.25	0.00	0.00	20.9
37	0	-0	606	0	0	0	37	--	--	16.08	16.08	0.00	0.00	0.00	0.04	0.00	0.00	20.9
38	0	-0	6607	0	0	0	1211	--	--	16.08	16.08	0.00	0.02	0.05	0.41	0.00	0.00	20.9
39	0	-0	3194	0	0	0	548	--	--	16.08	16.08	0.00	0.01	0.03	0.20	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	25	-0	2331	0	0	0	3462	--	--	16.08	16.08	0.00	0.06	0.02	0.15	0.00	0.00	20.9
2	25	-0	1343	0	0	0	1983	--	--	16.08	16.08	0.10	0.04	0.01	0.08	0.00	0.00	20.9
3	25	-0	1360	0	0	0	2009	--	--	16.08	16.08	0.10	0.04	0.01	0.09	0.00	0.00	20.9
4	25	-0	2226	0	0	0	3317	--	--	16.08	16.08	0.10	0.06	0.02	0.14	0.00	0.00	20.9
5	25	-0	2243	0	0	0	3343	--	--	16.08	16.08	0.10	0.06	0.02	0.14	0.00	0.00	20.9
6	25	-0	1632	0	0	0	2420	--	--	16.08	16.08	0.10	0.04	0.01	0.10	0.00	0.00	20.9

7	25	-0	1689	0	0	0	2506	--	--	16.08	16.08	0.10	0.04	0.01	0.11	0.00	0.00	20.9
8	25	-0	1897	0	0	0	2820	--	--	16.08	16.08	0.10	0.05	0.02	0.12	0.00	0.00	20.9
9	25	-0	1954	0	0	0	2906	--	--	16.08	16.08	0.10	0.05	0.02	0.12	0.00	0.00	20.9
10	25	-0	1343	0	0	0	1983	--	--	16.08	16.08	0.10	0.04	0.01	0.08	0.00	0.00	20.9
11	25	-0	1360	0	0	0	2009	--	--	16.08	16.08	0.10	0.04	0.01	0.09	0.00	0.00	20.9
12	25	-0	2226	0	0	0	3317	--	--	16.08	16.08	0.10	0.06	0.02	0.14	0.00	0.00	20.9
13	25	-0	2243	0	0	0	3343	--	--	16.08	16.08	0.10	0.06	0.02	0.14	0.00	0.00	20.9
14	25	-0	1632	0	0	0	2420	--	--	16.08	16.08	0.10	0.04	0.01	0.10	0.00	0.00	20.9
15	25	-0	1689	0	0	0	2506	--	--	16.08	16.08	0.10	0.04	0.01	0.11	0.00	0.00	20.9
16	25	-0	1897	0	0	0	2820	--	--	16.08	16.08	0.10	0.05	0.02	0.12	0.00	0.00	20.9
17	25	-0	1954	0	0	0	2906	--	--	16.08	16.08	0.10	0.05	0.02	0.12	0.00	0.00	20.9
18	25	-0	2423	0	0	0	3582	--	--	16.08	16.08	0.00	0.06	0.02	0.15	0.00	0.00	20.9
19	25	-0	6023	0	0	0	9034	--	--	16.08	16.08	0.00	0.15	0.05	0.38	0.00	0.00	20.9
20	25	-0	3975	0	0	0	5935	--	--	16.08	16.08	0.00	0.10	0.03	0.25	0.00	0.00	20.9
37	25	-0	606	0	0	0	837	--	--	16.08	16.08	0.00	0.01	0.00	0.04	0.00	0.00	20.9
38	25	-0	6607	0	0	0	9924	--	--	16.08	16.08	0.00	0.17	0.05	0.41	0.00	0.00	20.9
39	25	-0	3194	0	0	0	4760	--	--	16.08	16.08	0.00	0.08	0.03	0.20	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	50	-0	2331	0	0	0	1554	--	--	16.08	16.08	0.00	0.03	0.02	0.15	0.00	0.00	20.9
2	50	-0	1343	0	0	0	884	--	--	16.08	16.08	0.10	0.02	0.01	0.08	0.00	0.00	20.9
3	50	-0	1360	0	0	0	896	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
4	50	-0	2226	0	0	0	1495	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
5	50	-0	2243	0	0	0	1506	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
6	50	-0	1632	0	0	0	1084	--	--	16.08	16.08	0.10	0.02	0.01	0.10	0.00	0.00	20.9
7	50	-0	1689	0	0	0	1123	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
8	50	-0	1897	0	0	0	1267	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
9	50	-0	1954	0	0	0	1306	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
10	50	-0	1343	0	0	0	884	--	--	16.08	16.08	0.10	0.02	0.01	0.08	0.00	0.00	20.9
11	50	-0	1360	0	0	0	896	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
12	50	-0	2226	0	0	0	1495	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
13	50	-0	2243	0	0	0	1506	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
14	50	-0	1632	0	0	0	1084	--	--	16.08	16.08	0.10	0.02	0.01	0.10	0.00	0.00	20.9
15	50	-0	1689	0	0	0	1123	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
16	50	-0	1897	0	0	0	1267	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
17	50	-0	1954	0	0	0	1306	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
18	50	-0	2423	0	0	0	1598	--	--	16.08	16.08	0.00	0.03	0.02	0.15	0.00	0.00	20.9
19	50	-0	6023	0	0	0	4102	--	--	16.08	16.08	0.00	0.07	0.05	0.38	0.00	0.00	20.9
20	50	-0	3975	0	0	0	2680	--	--	16.08	16.08	0.00	0.05	0.03	0.25	0.00	0.00	20.9
37	50	-0	606	0	0	0	340	--	--	16.08	16.08	0.00	0.01	0.00	0.04	0.00	0.00	20.9
38	50	-0	6607	0	0	0	4515	--	--	16.08	16.08	0.00	0.08	0.05	0.41	0.00	0.00	20.9
39	50	-0	3194	0	0	0	2145	--	--	16.08	16.08	0.00	0.04	0.03	0.20	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 230 NI 1625 NF 1626 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	776	0	0	0	-830	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9
2	0	-0	424	0	0	0	-454	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
3	0	-0	431	0	0	0	-460	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
4	0	-0	763	0	0	0	-816	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
5	0	-0	770	0	0	0	-823	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
6	0	-0	536	0	0	0	-572	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
7	0	-0	557	0	0	0	-595	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
8	0	-0	637	0	0	0	-681	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
9	0	-0	659	0	0	0	-704	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
10	0	-0	424	0	0	0	-454	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
11	0	-0	431	0	0	0	-460	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
12	0	-0	763	0	0	0	-816	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
13	0	-0	770	0	0	0	-823	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
14	0	-0	536	0	0	0	-572	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
15	0	-0	557	0	0	0	-595	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
16	0	-0	637	0	0	0	-681	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
17	0	-0	659	0	0	0	-704	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
18	0	-0	773	0	0	0	-826	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9
19	0	-0	2182	0	0	0	-2332	--	--	16.08	16.08	0.18	0.04	0.02	0.14	0.00	0.00	20.9
20	0	-0	1386	0	0	0	-1481	--	--	16.08	16.08	0.18	0.02	0.01	0.09	0.00	0.00	20.9
37	0	-0	74	0	0	0	-80	--	--	16.08	16.08	0.18	0.00	0.00	0.00	0.00	0.00	20.9
38	0	-0	2423	0	0	0	-2590	--	--	16.08	16.08	0.18	0.04	0.02	0.15	0.00	0.00	20.9
39	0	-0	1096	0	0	0	-1171	--	--	16.08	16.08	0.18	0.02	0.01	0.07	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	25	-0	776	0	0	0	1024	--	--	16.08	16.08	0.00	0.02	0.01	0.05	0.00	0.00	20.9
2	25	-0	424	0	0	0	560	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
3	25	-0	431	0	0	0	568	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
4	25	-0	763	0	0	0	1007	--	--	16.08	16.08	0.10	0.02	0.01	0.05	0.00	0.00	20.9
5	25	-0	770	0	0	0	1015	--	--	16.08	16.08	0.10	0.02	0.01	0.05	0.00	0.00	20.9
6	25	-0	536	0	0	0	706	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
7	25	-0	557	0	0	0	735	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
8	25	-0	637	0	0	0	840	--	--	16.08	16.08	0.10	0.01	0.01	0.04	0.00	0.00	20.9
9	25	-0	659	0	0	0	869	--	--	16.08	16.08	0.10	0.02	0.01	0.04	0.00	0.00	20.9
10	25	-0	424	0	0	0	560	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
11	25	-0	431	0	0	0	568	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
12	25	-0	763	0	0	0	1007	--	--	16.08	16.08	0.10	0.02	0.01	0.05	0.00	0.00	20.9
13	25	-0	770	0	0	0	1015	--	--	16.08	16.08	0.10	0.02	0.01	0.05	0.00	0.00	20.9
14	25	-0	536	0	0	0	706	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
15	25	-0	557	0	0	0	735	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
16	25	-0	637	0	0	0	840	--	--	16.08	16.08	0.10	0.01	0.01	0.04	0.00	0.00	20.9
17	25	-0	659	0	0	0	869	--	--	16.08	16.08	0.10	0.02	0.01	0.04	0.00	0.00	20.9
18	25	-0	773	0	0	0	1019	--	--	16.08	16.08	0.00	0.02	0.01	0.05	0.00	0.00	20.9
19	25	-0	2182	0	0	0	2878	--	--	16.08	16.08	0.00	0.05	0.02	0.14	0.00	0.00	20.9
20	25	-0	1386	0	0	0	1828	--	--	16.08	16.08	0.00	0.03	0.01	0.09	0.00	0.00	20.9
37	25	-0	74	0	0	0	98	--	--	16.08	16.08	0.00	0.00	0.00	0.00	0.00	0.00	20.9
38	25	-0	2423	0	0	0	3195	--	--	16.08	16.08	0.00	0.05	0.02	0.15	0.00	0.00	20.9
39	25	-0	1096	0	0	0	1445	--	--	16.08	16.08	0.00	0.02	0.01	0.07	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	50	-0	776	0	0	0	388	--	--	16.08	16.08	0.00	0.01	0.01	0.05	0.00	0.00	20.9
2	50	-0	424	0	0	0	212	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9

3	50	-0	431	0	0	0	215	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
4	50	-0	763	0	0	0	382	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
5	50	-0	770	0	0	0	385	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
6	50	-0	536	0	0	0	268	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
7	50	-0	557	0	0	0	278	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
8	50	-0	637	0	0	0	319	--	--	16.08	16.08	0.10	0.01	0.01	0.04	0.00	0.00	20.9
9	50	-0	659	0	0	0	329	--	--	16.08	16.08	0.10	0.01	0.01	0.04	0.00	0.00	20.9
10	50	-0	424	0	0	0	212	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
11	50	-0	431	0	0	0	215	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
12	50	-0	763	0	0	0	382	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
13	50	-0	770	0	0	0	385	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
14	50	-0	536	0	0	0	268	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
15	50	-0	557	0	0	0	278	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
16	50	-0	637	0	0	0	319	--	--	16.08	16.08	0.10	0.01	0.01	0.04	0.00	0.00	20.9
17	50	-0	659	0	0	0	329	--	--	16.08	16.08	0.10	0.01	0.01	0.04	0.00	0.00	20.9
18	50	-0	773	0	0	0	386	--	--	16.08	16.08	0.00	0.01	0.01	0.05	0.00	0.00	20.9
19	50	-0	2182	0	0	0	1091	--	--	16.08	16.08	0.00	0.02	0.02	0.14	0.00	0.00	20.9
20	50	-0	1386	0	0	0	693	--	--	16.08	16.08	0.00	0.01	0.01	0.09	0.00	0.00	20.9
37	50	-0	74	0	0	0	37	--	--	16.08	16.08	0.00	0.00	0.00	0.00	0.00	0.00	20.9
38	50	-0	2423	0	0	0	1211	--	--	16.08	16.08	0.00	0.02	0.02	0.15	0.00	0.00	20.9
39	50	-0	1096	0	0	0	548	--	--	16.08	16.08	0.00	0.01	0.01	0.07	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

Delta Ingegneria srl
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Lavoro: **D2403a** Intestazione lavoro: **Palestra Campobello**
Elemento: **TRAVE DI FONDAZIONE** Gruppo: **2** Tabella: **Tabella fondazioni**
Descrizione: **Fondazione dir Y**
Rck: **350.00** daN/cm^2 fyk: **4580.0** daN/cm^2 Copriferro: **5.0** cm
Verifica in ottemperanza alle NTC2018
Per le combinazioni sismiche la capacità è valutata in campo elastico o sostanzialmente elastico (§7.2.5,7.4.1 NTC2018)
Diametro staffe: **10** mm Numero braccia: **2**

ASTA NUM. 1 NI 1757 NF 1642 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	1115	0	0	0	-314	--	--	16.08	16.08	0.18	0.01	0.01	0.07	0.00	0.00	20.9
2	0	-0	797	0	0	0	-266	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
3	0	-0	714	0	0	0	-258	--	--	16.08	16.08	0.29	0.00	0.01	0.04	0.00	0.00	20.9
4	0	-0	1002	0	0	0	-225	--	--	16.08	16.08	0.29	0.00	0.01	0.06	0.00	0.00	20.9
5	0	-0	919	0	0	0	-217	--	--	16.08	16.08	0.29	0.00	0.01	0.06	0.00	0.00	20.9
6	0	-0	965	0	0	0	-262	--	--	16.08	16.08	0.29	0.00	0.01	0.06	0.00	0.00	20.9
7	0	-0	690	0	0	0	-234	--	--	16.08	16.08	0.29	0.00	0.01	0.04	0.00	0.00	20.9
8	0	-0	1026	0	0	0	-250	--	--	16.08	16.08	0.29	0.00	0.01	0.06	0.00	0.00	20.9
9	0	-0	751	0	0	0	-221	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
10	0	-0	797	0	0	0	-266	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
11	0	-0	714	0	0	0	-258	--	--	16.08	16.08	0.29	0.00	0.01	0.04	0.00	0.00	20.9
12	0	-0	1002	0	0	0	-225	--	--	16.08	16.08	0.29	0.00	0.01	0.06	0.00	0.00	20.9
13	0	-0	919	0	0	0	-217	--	--	16.08	16.08	0.29	0.00	0.01	0.06	0.00	0.00	20.9
14	0	-0	965	0	0	0	-262	--	--	16.08	16.08	0.29	0.00	0.01	0.06	0.00	0.00	20.9
15	0	-0	690	0	0	0	-234	--	--	16.08	16.08	0.29	0.00	0.01	0.04	0.00	0.00	20.9
16	0	-0	1026	0	0	0	-250	--	--	16.08	16.08	0.29	0.00	0.01	0.06	0.00	0.00	20.9
17	0	-0	751	0	0	0	-221	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
18	0	-0	1278	0	0	0	-488	--	--	16.08	16.08	0.18	0.01	0.01	0.08	0.00	0.00	20.9
19	0	-0	1791	0	0	0	-212	--	--	16.08	16.08	0.18	0.00	0.01	0.11	0.00	0.00	20.9
20	0	-0	1311	0	0	0	-361	--	--	16.08	16.08	0.18	0.01	0.01	0.08	0.00	0.00	20.9
37	0	-0	970	0	0	0	-567	--	--	16.08	16.08	0.18	0.01	0.01	0.06	0.00	0.00	20.9
38	0	-0	1825	0	0	0	-108	--	--	16.08	16.08	0.18	0.00	0.02	0.11	0.00	0.00	20.9
39	0	-0	1026	0	0	0	-356	--	--	16.08	16.08	0.18	0.01	0.01	0.06	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	27	-0	1115	0	0	0	-314	--	--	16.08	16.08	0.18	0.01	0.01	0.07	0.00	0.00	20.9
2	27	-0	797	0	0	0	-266	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
3	27	-0	714	0	0	0	-258	--	--	16.08	16.08	0.29	0.00	0.01	0.04	0.00	0.00	20.9
4	27	-0	1002	0	0	0	1119	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9
5	27	-0	919	0	0	0	1016	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9
6	27	-0	965	0	0	0	1032	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9
7	27	-0	690	0	0	0	-234	--	--	16.08	16.08	0.29	0.00	0.01	0.04	0.00	0.00	20.9
8	27	-0	1026	0	0	0	1127	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9
9	27	-0	751	0	0	0	-221	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
10	27	-0	797	0	0	0	-266	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
11	27	-0	714	0	0	0	-258	--	--	16.08	16.08	0.29	0.00	0.01	0.04	0.00	0.00	20.9
12	27	-0	1002	0	0	0	1119	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9
13	27	-0	919	0	0	0	1016	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9
14	27	-0	965	0	0	0	1032	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9
15	27	-0	690	0	0	0	-234	--	--	16.08	16.08	0.29	0.00	0.01	0.04	0.00	0.00	20.9
16	27	-0	1026	0	0	0	1127	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9
17	27	-0	751	0	0	0	-221	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
18	27	-0	1278	0	0	0	-488	--	--	16.08	16.08	0.18	0.01	0.01	0.08	0.00	0.00	20.9
19	27	-0	1791	0	0	0	2191	--	--	16.08	16.08	0.00	0.04	0.01	0.11	0.00	0.00	20.9
20	27	-0	1311	0	0	0	-361	--	--	16.08	16.08	0.18	0.01	0.01	0.08	0.00	0.00	20.9
37	27	-0	970	0	0	0	-567	--	--	16.08	16.08	0.18	0.01	0.01	0.06	0.00	0.00	20.9
38	27	-0	1825	0	0	0	2340	--	--	16.08	16.08	0.00	0.04	0.02	0.11	0.00	0.00	20.9
39	27	-0	1026	0	0	0	-356	--	--	16.08	16.08	0.18	0.01	0.01	0.06	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	55	-0	1115	0	0	0	294	--	--	16.08	16.08	0.00	0.01	0.01	0.07	0.00	0.00	20.9
2	55	-0	797	0	0	0	168	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
3	55	-0	714	0	0	0	132	--	--	16.08	16.08	0.10	0.00	0.01	0.04	0.00	0.00	20.9
4	55	-0	1002	0	0	0	321	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
5	55	-0	919	0	0	0	284	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
6	55	-0	965	0	0	0	264	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
7	55	-0	690	0	0	0	142	--	--	16.08	16.08	0.10	0.00	0.01	0.04	0.00	0.00	20.9
8	55	-0	1026	0	0	0	310	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
9	55	-0	751	0	0	0	188	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
10	55	-0	797	0	0	0	168	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
11	55	-0	714	0	0	0	132	--	--	16.08	16.08	0.10	0.00	0.01	0.04	0.00	0.00	20.9
12	55	-0	1002	0	0	0	321	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
13	55	-0	919	0	0	0	284	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
14	55	-0	965	0	0	0	264	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
15	55	-0	690	0	0	0	142	--	--	16.08	16.08	0.10	0.00	0.01	0.04	0.00	0.00	20.9
16	55	-0	1026	0	0	0	310	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
17	55	-0	751	0	0	0	188	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
18	55	-0	1278	0	0	0	210	--	--	16.08	16.08	0.00	0.00	0.01	0.08	0.00	0.00	20.9
19	55	-0	1791	0	0	0	765	--	--	16.08	16.08	0.00	0.01	0.01	0.11	0.00	0.00	20.9
20	55	-0	1311	0	0	0	354	--	--	16.08	16.08	0.00	0.01	0.01	0.08	0.00	0.00	20.9
37	55	-0	970	0	0	0	-567	--	--	16.08	16.08	0.18	0.01	0.01	0.06	0.00	0.00	20.9
38	55	-0	1825	0	0	0	888	--	--	16.08	16.08	0.00	0.02	0.02	0.11	0.00	0.00	20.9
39	55	-0	1026	0	0	0	203	--	--	16.08	16.08	0.00	0.00	0.01	0.06	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 2 NI 1748 NF 1757 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	2299	0	0	0	-921	--	--	16.08	16.08	0.18	0.02	0.02	0.14	0.00	0.00	20.9
2	0	-0	1613	0	0	0	-679	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
3	0	-0	1548	0	0	0	-654	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
4	0	-0	1988	0	0	0	-762	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
5	0	-0	1923	0	0	0	-738	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
6	0	-0	1820	0	0	0	-736	--	--	16.08	16.08	0.29	0.01	0.02	0.11	0.00	0.00	20.9
7	0	-0	1604	0	0	0	-655	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
8	0	-0	1932	0	0	0	-762	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
9	0	-0	1716	0	0	0	-681	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
10	0	-0	1613	0	0	0	-679	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
11	0	-0	1548	0	0	0	-654	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
12	0	-0	1988	0	0	0	-762	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
13	0	-0	1923	0	0	0	-738	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
14	0	-0	1820	0	0	0	-736	--	--	16.08	16.08	0.29	0.01	0.02	0.11	0.00	0.00	20.9
15	0	-0	1604	0	0	0	-655	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
16	0	-0	1932	0	0	0	-762	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
17	0	-0	1716	0	0	0	-681	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
18	0	-0	2346	0	0	0	-1076	--	--	16.08	16.08	0.18	0.02	0.02	0.15	0.00	0.00	20.9
19	0	-0	3211	0	0	0	-1151	--	--	16.08	16.08	0.18	0.02	0.03	0.20	0.00	0.00	20.9
20	0	-0	2574	0	0	0	-1071	--	--	16.08	16.08	0.18	0.02	0.02	0.16	0.00	0.00	20.9
37	0	-0	1901	0	0	0	-988	--	--	16.08	16.08	0.18	0.02	0.02	0.12	0.00	0.00	20.9
38	0	-0	3342	0	0	0	-1112	--	--	16.08	16.08	0.18	0.02	0.03	0.21	0.00	0.00	20.9
39	0	-0	2280	0	0	0	-979	--	--	16.08	16.08	0.18	0.02	0.02	0.14	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	27	-0	2299	0	0	0	-921	--	--	16.08	16.08	0.18	0.02	0.02	0.14	0.00	0.00	20.9
2	27	-0	1613	0	0	0	-679	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
3	27	-0	1548	0	0	0	-654	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
4	27	-0	1988	0	0	0	-762	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
5	27	-0	1923	0	0	0	-738	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
6	27	-0	1820	0	0	0	-736	--	--	16.08	16.08	0.29	0.01	0.02	0.11	0.00	0.00	20.9
7	27	-0	1604	0	0	0	-655	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
8	27	-0	1932	0	0	0	-762	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
9	27	-0	1716	0	0	0	-681	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
10	27	-0	1613	0	0	0	-679	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
11	27	-0	1548	0	0	0	-654	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
12	27	-0	1988	0	0	0	-762	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
13	27	-0	1923	0	0	0	-738	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
14	27	-0	1820	0	0	0	-736	--	--	16.08	16.08	0.29	0.01	0.02	0.11	0.00	0.00	20.9
15	27	-0	1604	0	0	0	-655	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
16	27	-0	1932	0	0	0	-762	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
17	27	-0	1716	0	0	0	-681	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
18	27	-0	2346	0	0	0	-1076	--	--	16.08	16.08	0.18	0.02	0.02	0.15	0.00	0.00	20.9
19	27	-0	3211	0	0	0	-1151	--	--	16.08	16.08	0.18	0.02	0.03	0.20	0.00	0.00	20.9
20	27	-0	2574	0	0	0	-1071	--	--	16.08	16.08	0.18	0.02	0.02	0.16	0.00	0.00	20.9
37	27	-0	1901	0	0	0	-988	--	--	16.08	16.08	0.18	0.02	0.02	0.12	0.00	0.00	20.9
38	27	-0	3342	0	0	0	-1112	--	--	16.08	16.08	0.18	0.02	0.03	0.21	0.00	0.00	20.9
39	27	-0	2280	0	0	0	-979	--	--	16.08	16.08	0.18	0.02	0.02	0.14	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	55	-0	2299	0	0	0	333	--	--	16.08	16.08	0.00	0.01	0.02	0.14	0.00	0.00	20.9
2	55	-0	1613	0	0	0	201	--	--	16.08	16.08	0.10	0.00	0.01	0.10	0.00	0.00	20.9
3	55	-0	1548	0	0	0	190	--	--	16.08	16.08	0.10	0.00	0.01	0.10	0.00	0.00	20.9
4	55	-0	1988	0	0	0	322	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
5	55	-0	1923	0	0	0	311	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
6	55	-0	1820	0	0	0	256	--	--	16.08	16.08	0.10	0.00	0.02	0.11	0.00	0.00	20.9
7	55	-0	1604	0	0	0	219	--	--	16.08	16.08	0.10	0.00	0.01	0.10	0.00	0.00	20.9
8	55	-0	1932	0	0	0	292	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
9	55	-0	1716	0	0	0	256	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
10	55	-0	1613	0	0	0	201	--	--	16.08	16.08	0.10	0.00	0.01	0.10	0.00	0.00	20.9
11	55	-0	1548	0	0	0	190	--	--	16.08	16.08	0.10	0.00	0.01	0.10	0.00	0.00	20.9
12	55	-0	1988	0	0	0	322	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
13	55	-0	1923	0	0	0	311	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
14	55	-0	1820	0	0	0	256	--	--	16.08	16.08	0.10	0.00	0.02	0.11	0.00	0.00	20.9
15	55	-0	1604	0	0	0	219	--	--	16.08	16.08	0.10	0.00	0.01	0.10	0.00	0.00	20.9
16	55	-0	1932	0	0	0	292	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
17	55	-0	1716	0	0	0	256	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
18	55	-0	2346	0	0	0	203	--	--	16.08	16.08	0.00	0.00	0.02	0.15	0.00	0.00	20.9
19	55	-0	3211	0	0	0	600	--	--	16.08	16.08	0.00	0.01	0.03	0.20	0.00	0.00	20.9
20	55	-0	2574	0	0	0	333	--	--	16.08	16.08	0.00	0.01	0.02	0.16	0.00	0.00	20.9
37	55	-0	1901	0	0	0	49	--	--	16.08	16.08	0.00	0.00	0.02	0.12	0.00	0.00	20.9
38	55	-0	3342	0	0	0	711	--	--	16.08	16.08	0.00	0.01	0.03	0.21	0.00	0.00	20.9
39	55	-0	2280	0	0	0	265	--	--	16.08	16.08	0.00	0.00	0.02	0.14	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 3 NI 1749 NF 1748 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	1531	0	0	0	-1205	--	--	16.08	16.08	0.18	0.02	0.01	0.10	0.00	0.00	20.9
2	0	-0	1023	0	0	0	-873	--	--	16.08	16.08	0.29	0.02	0.01	0.06	0.00	0.00	20.9
3	0	-0	1019	0	0	0	-836	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
4	0	-0	1337	0	0	0	-1017	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
5	0	-0	1333	0	0	0	-981	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
6	0	-0	1138	0	0	0	-967	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
7	0	-0	1124	0	0	0	-844	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
8	0	-0	1232	0	0	0	-1010	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
9	0	-0	1218	0	0	0	-887	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
10	0	-0	1023	0	0	0	-873	--	--	16.08	16.08	0.29	0.02	0.01	0.06	0.00	0.00	20.9
11	0	-0	1019	0	0	0	-836	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
12	0	-0	1337	0	0	0	-1017	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
13	0	-0	1333	0	0	0	-981	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
14	0	-0	1138	0	0	0	-967	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
15	0	-0	1124	0	0	0	-844	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
16	0	-0	1232	0	0	0	-1010	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9

17	0	-0	1218	0	0	0	-887	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
18	0	-0	1352	0	0	0	-1339	--	--	16.08	16.08	0.18	0.02	0.01	0.08	0.00	0.00	20.9
19	0	-0	2189	0	0	0	-1584	--	--	16.08	16.08	0.18	0.03	0.02	0.14	0.00	0.00	20.9
20	0	-0	1711	0	0	0	-1384	--	--	16.08	16.08	0.18	0.02	0.01	0.11	0.00	0.00	20.9
37	0	-0	994	0	0	0	-1172	--	--	16.08	16.08	0.18	0.02	0.01	0.06	0.00	0.00	20.9
38	0	-0	2389	0	0	0	-1581	--	--	16.08	16.08	0.18	0.03	0.02	0.15	0.00	0.00	20.9
39	0	-0	1593	0	0	0	-1248	--	--	16.08	16.08	0.18	0.02	0.01	0.10	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	1531	0	0	0	-1205	--	--	16.08	16.08	0.18	0.02	0.01	0.10	0.00	0.00	20.9
2	27	-0	1023	0	0	0	-873	--	--	16.08	16.08	0.29	0.02	0.01	0.06	0.00	0.00	20.9
3	27	-0	1019	0	0	0	-836	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
4	27	-0	1337	0	0	0	-1017	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
5	27	-0	1333	0	0	0	-981	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
6	27	-0	1138	0	0	0	-967	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
7	27	-0	1124	0	0	0	-844	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
8	27	-0	1232	0	0	0	-1010	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
9	27	-0	1218	0	0	0	-887	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
10	27	-0	1023	0	0	0	-873	--	--	16.08	16.08	0.29	0.02	0.01	0.06	0.00	0.00	20.9
11	27	-0	1019	0	0	0	-836	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
12	27	-0	1337	0	0	0	-1017	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
13	27	-0	1333	0	0	0	-981	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
14	27	-0	1138	0	0	0	-967	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
15	27	-0	1124	0	0	0	-844	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
16	27	-0	1232	0	0	0	-1010	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
17	27	-0	1218	0	0	0	-887	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
18	27	-0	1352	0	0	0	-1339	--	--	16.08	16.08	0.18	0.02	0.01	0.08	0.00	0.00	20.9
19	27	-0	2189	0	0	0	-1584	--	--	16.08	16.08	0.18	0.03	0.02	0.14	0.00	0.00	20.9
20	27	-0	1711	0	0	0	-1384	--	--	16.08	16.08	0.18	0.02	0.01	0.11	0.00	0.00	20.9
37	27	-0	994	0	0	0	-1172	--	--	16.08	16.08	0.18	0.02	0.01	0.06	0.00	0.00	20.9
38	27	-0	2389	0	0	0	-1581	--	--	16.08	16.08	0.18	0.03	0.02	0.15	0.00	0.00	20.9
39	27	-0	1593	0	0	0	-1248	--	--	16.08	16.08	0.18	0.02	0.01	0.10	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	1531	0	0	0	-1205	--	--	16.08	16.08	0.18	0.02	0.01	0.10	0.00	0.00	20.9
2	55	-0	1023	0	0	0	-873	--	--	16.08	16.08	0.29	0.02	0.01	0.06	0.00	0.00	20.9
3	55	-0	1019	0	0	0	-836	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
4	55	-0	1337	0	0	0	-1017	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
5	55	-0	1333	0	0	0	-981	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
6	55	-0	1138	0	0	0	-967	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
7	55	-0	1124	0	0	0	-844	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
8	55	-0	1232	0	0	0	-1010	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
9	55	-0	1218	0	0	0	-887	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
10	55	-0	1023	0	0	0	-873	--	--	16.08	16.08	0.29	0.02	0.01	0.06	0.00	0.00	20.9
11	55	-0	1019	0	0	0	-836	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
12	55	-0	1337	0	0	0	-1017	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
13	55	-0	1333	0	0	0	-981	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
14	55	-0	1138	0	0	0	-967	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
15	55	-0	1124	0	0	0	-844	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
16	55	-0	1232	0	0	0	-1010	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
17	55	-0	1218	0	0	0	-887	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
18	55	-0	1352	0	0	0	-1339	--	--	16.08	16.08	0.18	0.02	0.01	0.08	0.00	0.00	20.9
19	55	-0	2189	0	0	0	-1584	--	--	16.08	16.08	0.18	0.03	0.02	0.14	0.00	0.00	20.9
20	55	-0	1711	0	0	0	-1384	--	--	16.08	16.08	0.18	0.02	0.01	0.11	0.00	0.00	20.9
37	55	-0	994	0	0	0	-1172	--	--	16.08	16.08	0.18	0.02	0.01	0.06	0.00	0.00	20.9
38	55	-0	2389	0	0	0	-1581	--	--	16.08	16.08	0.18	0.03	0.02	0.15	0.00	0.00	20.9
39	55	-0	1593	0	0	0	-1248	--	--	16.08	16.08	0.18	0.02	0.01	0.10	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 4 NI 1742 NF 1749 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	592	0	0	0	-1310	--	--	16.08	16.08	0.18	0.02	0.00	0.04	0.00	0.00	20.9
2	0	-0	335	0	0	0	-932	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
3	0	-0	355	0	0	0	-895	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
4	0	-0	556	0	0	0	-1120	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
5	0	-0	576	0	0	0	-1082	--	--	16.08	16.08	0.29	0.02	0.00	0.04	0.00	0.00	20.9
6	0	-0	390	0	0	0	-1042	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
7	0	-0	454	0	0	0	-917	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
8	0	-0	457	0	0	0	-1098	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
9	0	-0	521	0	0	0	-973	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
10	0	-0	335	0	0	0	-932	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
11	0	-0	355	0	0	0	-895	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
12	0	-0	556	0	0	0	-1120	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
13	0	-0	576	0	0	0	-1082	--	--	16.08	16.08	0.29	0.02	0.00	0.04	0.00	0.00	20.9
14	0	-0	390	0	0	0	-1042	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
15	0	-0	454	0	0	0	-917	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
16	0	-0	457	0	0	0	-1098	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
17	0	-0	521	0	0	0	-973	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
18	0	-0	252	0	0	0	-1373	--	--	16.08	16.08	0.18	0.02	0.00	0.02	0.00	0.00	20.9
19	0	-0	985	0	0	0	-1771	--	--	16.08	16.08	0.18	0.03	0.01	0.06	0.00	0.00	20.9
20	0	-0	636	0	0	0	-1491	--	--	16.08	16.08	0.18	0.02	0.01	0.04	0.00	0.00	20.9
37	0	-0	-3	0	0	0	-1155	--	--	16.08	16.08	0.18	0.02	0.00	0.00	0.00	0.00	20.9
38	0	-0	1219	0	0	0	-1817	--	--	16.08	16.08	0.18	0.03	0.01	0.08	0.00	0.00	20.9
39	0	-0	638	0	0	0	-1350	--	--	16.08	16.08	0.18	0.02	0.01	0.04	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	592	0	0	0	-1310	--	--	16.08	16.08	0.18	0.02	0.00	0.04	0.00	0.00	20.9
2	27	-0	335	0	0	0	-932	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
3	27	-0	355	0	0	0	-895	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
4	27	-0	556	0	0	0	-1120	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
5	27	-0	576	0	0	0	-1082	--	--	16.08	16.08	0.29	0.02	0.00	0.04	0.00	0.00	20.9
6	27	-0	390	0	0	0	-1042	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
7	27	-0	454	0	0	0	-917	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
8	27	-0	457	0	0	0	-1098	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
9	27	-0	521	0	0	0	-973	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
10	27	-0	335	0	0	0	-932	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
11	27	-0	355	0	0	0	-895	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
12	27	-0	556	0	0	0	-1120	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9

13	27	-0	576	0	0	0	-1082	--	--	16.08	16.08	0.29	0.02	0.00	0.04	0.00	0.00	20.9
14	27	-0	390	0	0	0	-1042	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
15	27	-0	454	0	0	0	-917	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
16	27	-0	457	0	0	0	-1098	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
17	27	-0	521	0	0	0	-973	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
18	27	-0	252	0	0	0	-1373	--	--	16.08	16.08	0.18	0.02	0.00	0.02	0.00	0.00	20.9
19	27	-0	985	0	0	0	-1771	--	--	16.08	16.08	0.18	0.03	0.01	0.06	0.00	0.00	20.9
20	27	-0	636	0	0	0	-1491	--	--	16.08	16.08	0.18	0.02	0.01	0.04	0.00	0.00	20.9
37	27	-0	-3	0	0	0	-1155	--	--	16.08	16.08	0.18	0.02	0.00	0.00	0.00	0.00	20.9
38	27	-0	1219	0	0	0	-1817	--	--	16.08	16.08	0.18	0.03	0.01	0.08	0.00	0.00	20.9
39	27	-0	638	0	0	0	-1350	--	--	16.08	16.08	0.18	0.02	0.01	0.04	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	592	0	0	0	-1310	--	--	16.08	16.08	0.18	0.02	0.00	0.04	0.00	0.00	20.9
2	55	-0	335	0	0	0	-932	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
3	55	-0	355	0	0	0	-895	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
4	55	-0	556	0	0	0	-1120	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
5	55	-0	576	0	0	0	-1082	--	--	16.08	16.08	0.29	0.02	0.00	0.04	0.00	0.00	20.9
6	55	-0	390	0	0	0	-1042	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
7	55	-0	454	0	0	0	-917	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
8	55	-0	457	0	0	0	-1098	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
9	55	-0	521	0	0	0	-973	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
10	55	-0	335	0	0	0	-932	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
11	55	-0	355	0	0	0	-895	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
12	55	-0	556	0	0	0	-1120	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
13	55	-0	576	0	0	0	-1082	--	--	16.08	16.08	0.29	0.02	0.00	0.04	0.00	0.00	20.9
14	55	-0	390	0	0	0	-1042	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
15	55	-0	454	0	0	0	-917	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
16	55	-0	457	0	0	0	-1098	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
17	55	-0	521	0	0	0	-973	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
18	55	-0	252	0	0	0	-1373	--	--	16.08	16.08	0.18	0.02	0.00	0.02	0.00	0.00	20.9
19	55	-0	985	0	0	0	-1771	--	--	16.08	16.08	0.18	0.03	0.01	0.06	0.00	0.00	20.9
20	55	-0	636	0	0	0	-1491	--	--	16.08	16.08	0.18	0.02	0.01	0.04	0.00	0.00	20.9
37	55	-0	-3	0	0	0	-1155	--	--	16.08	16.08	0.18	0.02	0.00	0.00	0.00	0.00	20.9
38	55	-0	1219	0	0	0	-1817	--	--	16.08	16.08	0.18	0.03	0.01	0.08	0.00	0.00	20.9
39	55	-0	638	0	0	0	-1350	--	--	16.08	16.08	0.18	0.02	0.01	0.04	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 5 NI 1755 NF 1742 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-83	0	0	0	-1266	--	--	16.08	16.08	0.18	0.02	0.00	0.01	0.00	0.00	20.9
2	0	-0	-160	0	0	0	-936	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
3	0	-0	-135	0	0	0	-889	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
4	0	-0	7	0	0	0	-1063	--	--	16.08	16.08	0.29	0.02	0.00	0.00	0.00	0.00	20.9
5	0	-0	32	0	0	0	-1030	--	--	16.08	16.08	0.29	0.02	0.00	0.00	0.00	0.00	20.9
6	0	-0	-132	0	0	0	-1034	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
7	0	-0	-46	0	0	0	-877	--	--	16.08	16.08	0.29	0.02	0.00	0.00	0.00	0.00	20.9
8	0	-0	-82	0	0	0	-1071	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
9	0	-0	4	0	0	0	-917	--	--	16.08	16.08	0.29	0.02	0.00	0.00	0.00	0.00	20.9
10	0	-0	-160	0	0	0	-936	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
11	0	-0	-135	0	0	0	-889	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
12	0	-0	7	0	0	0	-1063	--	--	16.08	16.08	0.29	0.02	0.00	0.00	0.00	0.00	20.9
13	0	-0	32	0	0	0	-1030	--	--	16.08	16.08	0.29	0.02	0.00	0.00	0.00	0.00	20.9
14	0	-0	-132	0	0	0	-1034	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
15	0	-0	-46	0	0	0	-877	--	--	16.08	16.08	0.29	0.02	0.00	0.00	0.00	0.00	20.9
16	0	-0	-82	0	0	0	-1071	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
17	0	-0	4	0	0	0	-917	--	--	16.08	16.08	0.29	0.02	0.00	0.00	0.00	0.00	20.9
18	0	-0	-569	0	0	0	-1484	--	--	16.08	16.08	0.18	0.02	0.00	0.04	0.00	0.00	20.9
19	0	-0	155	0	0	0	-1715	--	--	16.08	16.08	0.18	0.03	0.00	0.01	0.00	0.00	20.9
20	0	-0	-152	0	0	0	-1459	--	--	16.08	16.08	0.18	0.02	0.00	0.01	0.00	0.00	20.9
37	0	-0	-773	0	0	0	-1340	--	--	16.08	16.08	0.18	0.02	0.01	0.05	0.00	0.00	20.9
38	0	-0	435	0	0	0	-1821	--	--	16.08	16.08	0.18	0.03	0.00	0.03	0.00	0.00	20.9
39	0	-0	-77	0	0	0	-1298	--	--	16.08	16.08	0.18	0.02	0.00	0.00	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-83	0	0	0	-1266	--	--	16.08	16.08	0.18	0.02	0.00	0.01	0.00	0.00	20.9
2	27	-0	-160	0	0	0	-936	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
3	27	-0	-135	0	0	0	-889	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
4	27	-0	7	0	0	0	-1063	--	--	16.08	16.08	0.29	0.02	0.00	0.00	0.00	0.00	20.9
5	27	-0	32	0	0	0	-1030	--	--	16.08	16.08	0.29	0.02	0.00	0.00	0.00	0.00	20.9
6	27	-0	-132	0	0	0	-1034	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
7	27	-0	-46	0	0	0	-877	--	--	16.08	16.08	0.29	0.02	0.00	0.00	0.00	0.00	20.9
8	27	-0	-82	0	0	0	-1071	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
9	27	-0	4	0	0	0	-917	--	--	16.08	16.08	0.29	0.02	0.00	0.00	0.00	0.00	20.9
10	27	-0	-160	0	0	0	-936	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
11	27	-0	-135	0	0	0	-889	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
12	27	-0	7	0	0	0	-1063	--	--	16.08	16.08	0.29	0.02	0.00	0.00	0.00	0.00	20.9
13	27	-0	32	0	0	0	-1030	--	--	16.08	16.08	0.29	0.02	0.00	0.00	0.00	0.00	20.9
14	27	-0	-132	0	0	0	-1034	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
15	27	-0	-46	0	0	0	-877	--	--	16.08	16.08	0.29	0.02	0.00	0.00	0.00	0.00	20.9
16	27	-0	-82	0	0	0	-1071	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
17	27	-0	4	0	0	0	-917	--	--	16.08	16.08	0.29	0.02	0.00	0.00	0.00	0.00	20.9
18	27	-0	-569	0	0	0	-1484	--	--	16.08	16.08	0.18	0.02	0.00	0.04	0.00	0.00	20.9
19	27	-0	155	0	0	0	-1715	--	--	16.08	16.08	0.18	0.03	0.00	0.01	0.00	0.00	20.9
20	27	-0	-152	0	0	0	-1459	--	--	16.08	16.08	0.18	0.02	0.00	0.01	0.00	0.00	20.9
37	27	-0	-773	0	0	0	-1340	--	--	16.08	16.08	0.18	0.02	0.01	0.05	0.00	0.00	20.9
38	27	-0	435	0	0	0	-1821	--	--	16.08	16.08	0.18	0.03	0.00	0.03	0.00	0.00	20.9
39	27	-0	-77	0	0	0	-1298	--	--	16.08	16.08	0.18	0.02	0.00	0.00	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	-83	0	0	0	-1266	--	--	16.08	16.08	0.18	0.02	0.00	0.01	0.00	0.00	20.9
2	55	-0	-160	0	0	0	-936	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
3	55	-0	-135	0	0	0	-889	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
4	55	-0	7	0	0	0	-1063	--	--	16.08	16.08	0.29	0.02	0.00	0.00	0.00	0.00	20.9
5	55	-0	32	0	0	0	-1030	--	--	16.08	16.08	0.29	0.02	0.00	0.00	0.00	0.00	20.9
6	55	-0	-132	0	0	0	-1034	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
7	55	-0	-46	0	0	0	-877	--	--	16.08	16.08	0.29	0.02	0.00	0.00	0.00	0.00	20.9
8	55	-0	-82	0	0	0	-1071	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9

9	55	-0	4	0	0	0	-917	--	--	16.08	16.08	0.29	0.02	0.00	0.00	0.00	0.00	20.9
10	55	-0	-160	0	0	0	-936	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
11	55	-0	-135	0	0	0	-889	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
12	55	-0	7	0	0	0	-1063	--	--	16.08	16.08	0.29	0.02	0.00	0.00	0.00	0.00	20.9
13	55	-0	32	0	0	0	-1030	--	--	16.08	16.08	0.29	0.02	0.00	0.00	0.00	0.00	20.9
14	55	-0	-132	0	0	0	-1034	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
15	55	-0	-46	0	0	0	-877	--	--	16.08	16.08	0.29	0.02	0.00	0.00	0.00	0.00	20.9
16	55	-0	-82	0	0	0	-1071	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
17	55	-0	4	0	0	0	-917	--	--	16.08	16.08	0.29	0.02	0.00	0.00	0.00	0.00	20.9
18	55	-0	-569	0	0	0	-1484	--	--	16.08	16.08	0.18	0.02	0.00	0.04	0.00	0.00	20.9
19	55	-0	155	0	0	0	-1715	--	--	16.08	16.08	0.18	0.03	0.00	0.01	0.00	0.00	20.9
20	55	-0	-152	0	0	0	-1459	--	--	16.08	16.08	0.18	0.02	0.00	0.01	0.00	0.00	20.9
37	55	-0	-773	0	0	0	-1340	--	--	16.08	16.08	0.18	0.02	0.01	0.05	0.00	0.00	20.9
38	55	-0	435	0	0	0	-1821	--	--	16.08	16.08	0.18	0.03	0.00	0.03	0.00	0.00	20.9
39	55	-0	-77	0	0	0	-1298	--	--	16.08	16.08	0.18	0.02	0.00	0.00	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 6 NI 1756 NF 1755 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-675	0	0	0	-1365	--	--	16.08	16.08	0.18	0.02	0.01	0.04	0.00	0.00	20.9
2	0	-0	-602	0	0	0	-991	--	--	16.08	16.08	0.29	0.02	0.00	0.04	0.00	0.00	20.9
3	0	-0	-573	0	0	0	-948	--	--	16.08	16.08	0.29	0.02	0.00	0.04	0.00	0.00	20.9
4	0	-0	-466	0	0	0	-1151	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
5	0	-0	-437	0	0	0	-1109	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
6	0	-0	-588	0	0	0	-1097	--	--	16.08	16.08	0.29	0.02	0.00	0.04	0.00	0.00	20.9
7	0	-0	-492	0	0	0	-954	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
8	0	-0	-547	0	0	0	-1145	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
9	0	-0	-451	0	0	0	-1003	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
10	0	-0	-602	0	0	0	-991	--	--	16.08	16.08	0.29	0.02	0.00	0.04	0.00	0.00	20.9
11	0	-0	-573	0	0	0	-948	--	--	16.08	16.08	0.29	0.02	0.00	0.04	0.00	0.00	20.9
12	0	-0	-466	0	0	0	-1151	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
13	0	-0	-437	0	0	0	-1109	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
14	0	-0	-588	0	0	0	-1097	--	--	16.08	16.08	0.29	0.02	0.00	0.04	0.00	0.00	20.9
15	0	-0	-492	0	0	0	-954	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
16	0	-0	-547	0	0	0	-1145	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
17	0	-0	-451	0	0	0	-1003	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
18	0	-0	-1330	0	0	0	-1524	--	--	16.08	16.08	0.18	0.03	0.01	0.08	0.00	0.00	20.9
19	0	-0	-542	0	0	0	-1792	--	--	16.08	16.08	0.18	0.03	0.00	0.03	0.00	0.00	20.9
20	0	-0	-852	0	0	0	-1564	--	--	16.08	16.08	0.18	0.03	0.01	0.05	0.00	0.00	20.9
37	0	-0	-1510	0	0	0	-1339	--	--	16.08	16.08	0.18	0.02	0.01	0.09	0.00	0.00	20.9
38	0	-0	-197	0	0	0	-1785	--	--	16.08	16.08	0.18	0.03	0.00	0.01	0.00	0.00	20.9
39	0	-0	-714	0	0	0	-1405	--	--	16.08	16.08	0.18	0.02	0.01	0.04	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-675	0	0	0	-1365	--	--	16.08	16.08	0.18	0.02	0.01	0.04	0.00	0.00	20.9
2	27	-0	-602	0	0	0	-991	--	--	16.08	16.08	0.29	0.02	0.00	0.04	0.00	0.00	20.9
3	27	-0	-573	0	0	0	-948	--	--	16.08	16.08	0.29	0.02	0.00	0.04	0.00	0.00	20.9
4	27	-0	-466	0	0	0	-1151	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
5	27	-0	-437	0	0	0	-1109	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
6	27	-0	-588	0	0	0	-1097	--	--	16.08	16.08	0.29	0.02	0.00	0.04	0.00	0.00	20.9
7	27	-0	-492	0	0	0	-954	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
8	27	-0	-547	0	0	0	-1145	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
9	27	-0	-451	0	0	0	-1003	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
10	27	-0	-602	0	0	0	-991	--	--	16.08	16.08	0.29	0.02	0.00	0.04	0.00	0.00	20.9
11	27	-0	-573	0	0	0	-948	--	--	16.08	16.08	0.29	0.02	0.00	0.04	0.00	0.00	20.9
12	27	-0	-466	0	0	0	-1151	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
13	27	-0	-437	0	0	0	-1109	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
14	27	-0	-588	0	0	0	-1097	--	--	16.08	16.08	0.29	0.02	0.00	0.04	0.00	0.00	20.9
15	27	-0	-492	0	0	0	-954	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
16	27	-0	-547	0	0	0	-1145	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
17	27	-0	-451	0	0	0	-1003	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
18	27	-0	-1330	0	0	0	-1524	--	--	16.08	16.08	0.18	0.03	0.01	0.08	0.00	0.00	20.9
19	27	-0	-542	0	0	0	-1792	--	--	16.08	16.08	0.18	0.03	0.00	0.03	0.00	0.00	20.9
20	27	-0	-852	0	0	0	-1564	--	--	16.08	16.08	0.18	0.03	0.01	0.05	0.00	0.00	20.9
37	27	-0	-1510	0	0	0	-1339	--	--	16.08	16.08	0.18	0.02	0.01	0.09	0.00	0.00	20.9
38	27	-0	-197	0	0	0	-1785	--	--	16.08	16.08	0.18	0.03	0.00	0.01	0.00	0.00	20.9
39	27	-0	-714	0	0	0	-1405	--	--	16.08	16.08	0.18	0.02	0.01	0.04	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	-675	0	0	0	-1365	--	--	16.08	16.08	0.18	0.02	0.01	0.04	0.00	0.00	20.9
2	55	-0	-602	0	0	0	-991	--	--	16.08	16.08	0.29	0.02	0.00	0.04	0.00	0.00	20.9
3	55	-0	-573	0	0	0	-948	--	--	16.08	16.08	0.29	0.02	0.00	0.04	0.00	0.00	20.9
4	55	-0	-466	0	0	0	-1151	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
5	55	-0	-437	0	0	0	-1109	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
6	55	-0	-588	0	0	0	-1097	--	--	16.08	16.08	0.29	0.02	0.00	0.04	0.00	0.00	20.9
7	55	-0	-492	0	0	0	-954	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
8	55	-0	-547	0	0	0	-1145	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
9	55	-0	-451	0	0	0	-1003	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
10	55	-0	-602	0	0	0	-991	--	--	16.08	16.08	0.29	0.02	0.00	0.04	0.00	0.00	20.9
11	55	-0	-573	0	0	0	-948	--	--	16.08	16.08	0.29	0.02	0.00	0.04	0.00	0.00	20.9
12	55	-0	-466	0	0	0	-1151	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
13	55	-0	-437	0	0	0	-1109	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
14	55	-0	-588	0	0	0	-1097	--	--	16.08	16.08	0.29	0.02	0.00	0.04	0.00	0.00	20.9
15	55	-0	-492	0	0	0	-954	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
16	55	-0	-547	0	0	0	-1145	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
17	55	-0	-451	0	0	0	-1003	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
18	55	-0	-1330	0	0	0	-1524	--	--	16.08	16.08	0.18	0.03	0.01	0.08	0.00	0.00	20.9
19	55	-0	-542	0	0	0	-1792	--	--	16.08	16.08	0.18	0.03	0.00	0.03	0.00	0.00	20.9
20	55	-0	-852	0	0	0	-1564	--	--	16.08	16.08	0.18	0.03	0.01	0.05	0.00	0.00	20.9
37	55	-0	-1510	0	0	0	-1339	--	--	16.08	16.08	0.18	0.02	0.01	0.09	0.00	0.00	20.9
38	55	-0	-197	0	0	0	-1785	--	--	16.08	16.08	0.18	0.03	0.00	0.01	0.00	0.00	20.9
39	55	-0	-714	0	0	0	-1405	--	--	16.08	16.08	0.18	0.02	0.01	0.04	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 7 NI 1745 NF 1756 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle V,Mx	cmq/m		cm
1	0	-0	-1287	0	0	0	-1328	--	--	16.08	16.08	0.18	0.02	0.01 0.08	0.00	0.00	20.9
2	0	-0	-1061	0	0	0	-947	--	--	16.08	16.08	0.29	0.02	0.01 0.07	0.00	0.00	20.9
3	0	-0	-1030	0	0	0	-910	--	--	16.08	16.08	0.29	0.02	0.01 0.06	0.00	0.00	20.9
4	0	-0	-949	0	0	0	-1133	--	--	16.08	16.08	0.29	0.02	0.01 0.06	0.00	0.00	20.9
5	0	-0	-918	0	0	0	-1095	--	--	16.08	16.08	0.29	0.02	0.01 0.06	0.00	0.00	20.9
6	0	-0	-1058	0	0	0	-1056	--	--	16.08	16.08	0.29	0.02	0.01 0.07	0.00	0.00	20.9
7	0	-0	-955	0	0	0	-931	--	--	16.08	16.08	0.29	0.02	0.01 0.06	0.00	0.00	20.9
8	0	-0	-1024	0	0	0	-1112	--	--	16.08	16.08	0.29	0.02	0.01 0.06	0.00	0.00	20.9
9	0	-0	-922	0	0	0	-986	--	--	16.08	16.08	0.29	0.02	0.01 0.06	0.00	0.00	20.9
10	0	-0	-1061	0	0	0	-947	--	--	16.08	16.08	0.29	0.02	0.01 0.07	0.00	0.00	20.9
11	0	-0	-1030	0	0	0	-910	--	--	16.08	16.08	0.29	0.02	0.01 0.06	0.00	0.00	20.9
12	0	-0	-949	0	0	0	-1133	--	--	16.08	16.08	0.29	0.02	0.01 0.06	0.00	0.00	20.9
13	0	-0	-918	0	0	0	-1095	--	--	16.08	16.08	0.29	0.02	0.01 0.06	0.00	0.00	20.9
14	0	-0	-1058	0	0	0	-1056	--	--	16.08	16.08	0.29	0.02	0.01 0.07	0.00	0.00	20.9
15	0	-0	-955	0	0	0	-931	--	--	16.08	16.08	0.29	0.02	0.01 0.06	0.00	0.00	20.9
16	0	-0	-1024	0	0	0	-1112	--	--	16.08	16.08	0.29	0.02	0.01 0.06	0.00	0.00	20.9
17	0	-0	-922	0	0	0	-986	--	--	16.08	16.08	0.29	0.02	0.01 0.06	0.00	0.00	20.9
18	0	-0	-2148	0	0	0	-1399	--	--	16.08	16.08	0.18	0.02	0.02 0.13	0.00	0.00	20.9
19	0	-0	-1260	0	0	0	-1781	--	--	16.08	16.08	0.18	0.03	0.01 0.08	0.00	0.00	20.9
20	0	-0	-1590	0	0	0	-1508	--	--	16.08	16.08	0.18	0.02	0.01 0.10	0.00	0.00	20.9
37	0	-0	-2311	0	0	0	76	--	--	16.08	16.08	0.00	0.00	0.02 0.14	0.00	0.00	20.9
38	0	-0	-831	0	0	0	-1822	--	--	16.08	16.08	0.18	0.03	0.01 0.05	0.00	0.00	20.9
39	0	-0	-1382	0	0	0	-1367	--	--	16.08	16.08	0.18	0.02	0.01 0.09	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle V,Mx	cmq/m		cm
1	27	-0	-1287	0	0	0	-1328	--	--	16.08	16.08	0.18	0.02	0.01 0.08	0.00	0.00	20.9
2	27	-0	-1061	0	0	0	-947	--	--	16.08	16.08	0.29	0.02	0.01 0.07	0.00	0.00	20.9
3	27	-0	-1030	0	0	0	-910	--	--	16.08	16.08	0.29	0.02	0.01 0.06	0.00	0.00	20.9
4	27	-0	-949	0	0	0	-1133	--	--	16.08	16.08	0.29	0.02	0.01 0.06	0.00	0.00	20.9
5	27	-0	-918	0	0	0	-1095	--	--	16.08	16.08	0.29	0.02	0.01 0.06	0.00	0.00	20.9
6	27	-0	-1058	0	0	0	-1056	--	--	16.08	16.08	0.29	0.02	0.01 0.07	0.00	0.00	20.9
7	27	-0	-955	0	0	0	-931	--	--	16.08	16.08	0.29	0.02	0.01 0.06	0.00	0.00	20.9
8	27	-0	-1024	0	0	0	-1112	--	--	16.08	16.08	0.29	0.02	0.01 0.06	0.00	0.00	20.9
9	27	-0	-922	0	0	0	-986	--	--	16.08	16.08	0.29	0.02	0.01 0.06	0.00	0.00	20.9
10	27	-0	-1061	0	0	0	-947	--	--	16.08	16.08	0.29	0.02	0.01 0.07	0.00	0.00	20.9
11	27	-0	-1030	0	0	0	-910	--	--	16.08	16.08	0.29	0.02	0.01 0.06	0.00	0.00	20.9
12	27	-0	-949	0	0	0	-1133	--	--	16.08	16.08	0.29	0.02	0.01 0.06	0.00	0.00	20.9
13	27	-0	-918	0	0	0	-1095	--	--	16.08	16.08	0.29	0.02	0.01 0.06	0.00	0.00	20.9
14	27	-0	-1058	0	0	0	-1056	--	--	16.08	16.08	0.29	0.02	0.01 0.07	0.00	0.00	20.9
15	27	-0	-955	0	0	0	-931	--	--	16.08	16.08	0.29	0.02	0.01 0.06	0.00	0.00	20.9
16	27	-0	-1024	0	0	0	-1112	--	--	16.08	16.08	0.29	0.02	0.01 0.06	0.00	0.00	20.9
17	27	-0	-922	0	0	0	-986	--	--	16.08	16.08	0.29	0.02	0.01 0.06	0.00	0.00	20.9
18	27	-0	-2148	0	0	0	-1399	--	--	16.08	16.08	0.18	0.02	0.02 0.13	0.00	0.00	20.9
19	27	-0	-1260	0	0	0	-1781	--	--	16.08	16.08	0.18	0.03	0.01 0.08	0.00	0.00	20.9
20	27	-0	-1590	0	0	0	-1508	--	--	16.08	16.08	0.18	0.02	0.01 0.10	0.00	0.00	20.9
37	27	-0	-2311	0	0	0	-1184	--	--	16.08	16.08	0.18	0.02	0.02 0.14	0.00	0.00	20.9
38	27	-0	-831	0	0	0	-1822	--	--	16.08	16.08	0.18	0.03	0.01 0.05	0.00	0.00	20.9
39	27	-0	-1382	0	0	0	-1367	--	--	16.08	16.08	0.18	0.02	0.01 0.09	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle V,Mx	cmq/m		cm
1	55	-0	-1287	0	0	0	-1328	--	--	16.08	16.08	0.18	0.02	0.01 0.08	0.00	0.00	20.9
2	55	-0	-1061	0	0	0	-947	--	--	16.08	16.08	0.29	0.02	0.01 0.07	0.00	0.00	20.9
3	55	-0	-1030	0	0	0	-910	--	--	16.08	16.08	0.29	0.02	0.01 0.06	0.00	0.00	20.9
4	55	-0	-949	0	0	0	-1133	--	--	16.08	16.08	0.29	0.02	0.01 0.06	0.00	0.00	20.9
5	55	-0	-918	0	0	0	-1095	--	--	16.08	16.08	0.29	0.02	0.01 0.06	0.00	0.00	20.9
6	55	-0	-1058	0	0	0	-1056	--	--	16.08	16.08	0.29	0.02	0.01 0.07	0.00	0.00	20.9
7	55	-0	-955	0	0	0	-931	--	--	16.08	16.08	0.29	0.02	0.01 0.06	0.00	0.00	20.9
8	55	-0	-1024	0	0	0	-1112	--	--	16.08	16.08	0.29	0.02	0.01 0.06	0.00	0.00	20.9
9	55	-0	-922	0	0	0	-986	--	--	16.08	16.08	0.29	0.02	0.01 0.06	0.00	0.00	20.9
10	55	-0	-1061	0	0	0	-947	--	--	16.08	16.08	0.29	0.02	0.01 0.07	0.00	0.00	20.9
11	55	-0	-1030	0	0	0	-910	--	--	16.08	16.08	0.29	0.02	0.01 0.06	0.00	0.00	20.9
12	55	-0	-949	0	0	0	-1133	--	--	16.08	16.08	0.29	0.02	0.01 0.06	0.00	0.00	20.9
13	55	-0	-918	0	0	0	-1095	--	--	16.08	16.08	0.29	0.02	0.01 0.06	0.00	0.00	20.9
14	55	-0	-1058	0	0	0	-1056	--	--	16.08	16.08	0.29	0.02	0.01 0.07	0.00	0.00	20.9
15	55	-0	-955	0	0	0	-931	--	--	16.08	16.08	0.29	0.02	0.01 0.06	0.00	0.00	20.9
16	55	-0	-1024	0	0	0	-1112	--	--	16.08	16.08	0.29	0.02	0.01 0.06	0.00	0.00	20.9
17	55	-0	-922	0	0	0	-986	--	--	16.08	16.08	0.29	0.02	0.01 0.06	0.00	0.00	20.9
18	55	-0	-2148	0	0	0	-1399	--	--	16.08	16.08	0.18	0.02	0.02 0.13	0.00	0.00	20.9
19	55	-0	-1260	0	0	0	-1781	--	--	16.08	16.08	0.18	0.03	0.01 0.08	0.00	0.00	20.9
20	55	-0	-1590	0	0	0	-1508	--	--	16.08	16.08	0.18	0.02	0.01 0.10	0.00	0.00	20.9
37	55	-0	-2311	0	0	0	-1184	--	--	16.08	16.08	0.18	0.02	0.02 0.14	0.00	0.00	20.9
38	55	-0	-831	0	0	0	-1822	--	--	16.08	16.08	0.18	0.03	0.01 0.05	0.00	0.00	20.9
39	55	-0	-1382	0	0	0	-1367	--	--	16.08	16.08	0.18	0.02	0.01 0.09	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 8 NI 1746 NF 1745 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle V,Mx	cmq/m		cm
1	0	-0	-2024	0	0	0	-1144	--	--	16.08	16.08	0.18	0.02	0.02 0.13	0.00	0.00	20.9
2	0	-0	-1610	0	0	0	82	--	--	16.08	16.08	0.10	0.00	0.01 0.10	0.00	0.00	20.9
3	0	-0	-1580	0	0	0	98	--	--	16.08	16.08	0.10	0.00	0.01 0.10	0.00	0.00	20.9
4	0	-0	-1534	0	0	0	-995	--	--	16.08	16.08	0.29	0.02	0.01 0.10	0.00	0.00	20.9
5	0	-0	-1504	0	0	0	-963	--	--	16.08	16.08	0.29	0.02	0.01 0.09	0.00	0.00	20.9
6	0	-0	-1620	0	0	0	-904	--	--	16.08	16.08	0.29	0.02	0.01 0.10	0.00	0.00	20.9
7	0	-0	-1517	0	0	0	32	--	--	16.08	16.08	0.10	0.00	0.01 0.10	0.00	0.00	20.9
8	0	-0	-1597	0	0	0	-964	--	--	16.08	16.08	0.29	0.02	0.01 0.10	0.00	0.00	20.9
9	0	-0	-1495	0	0	0	-855	--	--	16.08	16.08	0.29	0.01	0.01 0.09	0.00	0.00	20.9
10	0	-0	-1610	0	0	0	82	--	--	16.08	16.08	0.10	0.00	0.01 0.10	0.00	0.00	20.9
11	0	-0	-1580	0	0	0	98	--	--	16.08	16.08	0.10	0.00	0.01 0.10	0.00	0.00	20.9
12	0	-0	-1534	0	0	0	-995	--	--	16.08	16.08	0.29	0.02	0.01 0.10	0.00	0.00	20.9
13	0	-0	-1504	0	0	0	-963	--	--	16.08	16.08	0.29	0.02	0.01 0.09	0.00	0.00	20.9
14	0	-0	-1620	0	0	0	-904	--	--	16.08	16.08	0.29	0.02	0.01 0.10	0.00	0.00	20.9
15	0	-0	-1517	0	0	0	32	--	--	16.08	16.08	0.10	0.00	0.01 0.10	0.00	0.00	20.9
16	0	-0	-1597	0	0	0	-964	--	--	16.08	16.08	0.29	0.02	0.01 0.10	0.00	0.00	20.9

17	0	-0	-1495	0	0	0	-855	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
18	0	-0	-3153	0	0	0	637	--	--	16.08	16.08	0.00	0.01	0.03	0.20	0.00	0.00	20.9
19	0	-0	-2183	0	0	0	-1576	--	--	16.08	16.08	0.18	0.03	0.02	0.14	0.00	0.00	20.9
20	0	-0	-2518	0	0	0	107	--	--	16.08	16.08	0.00	0.00	0.02	0.16	0.00	0.00	20.9
37	0	-0	-3271	0	0	0	928	--	--	16.08	16.08	0.00	0.02	0.03	0.21	0.00	0.00	20.9
38	0	-0	-1654	0	0	0	-1678	--	--	16.08	16.08	0.18	0.03	0.01	0.10	0.00	0.00	20.9
39	0	-0	-2214	0	0	0	45	--	--	16.08	16.08	0.00	0.00	0.02	0.14	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-2024	0	0	0	-1144	--	--	16.08	16.08	0.18	0.02	0.02	0.13	0.00	0.00	20.9
2	27	-0	-1610	0	0	0	-796	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
3	27	-0	-1580	0	0	0	-764	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
4	27	-0	-1534	0	0	0	-995	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
5	27	-0	-1504	0	0	0	-963	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
6	27	-0	-1620	0	0	0	-904	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
7	27	-0	-1517	0	0	0	-796	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
8	27	-0	-1597	0	0	0	-964	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
9	27	-0	-1495	0	0	0	-855	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
10	27	-0	-1610	0	0	0	-796	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
11	27	-0	-1580	0	0	0	-764	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
12	27	-0	-1534	0	0	0	-995	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
13	27	-0	-1504	0	0	0	-963	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
14	27	-0	-1620	0	0	0	-904	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
15	27	-0	-1517	0	0	0	-796	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
16	27	-0	-1597	0	0	0	-964	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
17	27	-0	-1495	0	0	0	-855	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
18	27	-0	-3153	0	0	0	-1083	--	--	16.08	16.08	0.18	0.02	0.03	0.20	0.00	0.00	20.9
19	27	-0	-2183	0	0	0	-1576	--	--	16.08	16.08	0.18	0.03	0.02	0.14	0.00	0.00	20.9
20	27	-0	-2518	0	0	0	-1267	--	--	16.08	16.08	0.18	0.02	0.02	0.16	0.00	0.00	20.9
37	27	-0	-3271	0	0	0	928	--	--	16.08	16.08	0.00	0.02	0.03	0.21	0.00	0.00	20.9
38	27	-0	-1654	0	0	0	-1678	--	--	16.08	16.08	0.18	0.03	0.01	0.10	0.00	0.00	20.9
39	27	-0	-2214	0	0	0	-1163	--	--	16.08	16.08	0.18	0.02	0.02	0.14	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	-2024	0	0	0	-1144	--	--	16.08	16.08	0.18	0.02	0.02	0.13	0.00	0.00	20.9
2	55	-0	-1610	0	0	0	-796	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
3	55	-0	-1580	0	0	0	-764	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
4	55	-0	-1534	0	0	0	-995	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
5	55	-0	-1504	0	0	0	-963	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
6	55	-0	-1620	0	0	0	-904	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
7	55	-0	-1517	0	0	0	-796	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
8	55	-0	-1597	0	0	0	-964	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
9	55	-0	-1495	0	0	0	-855	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
10	55	-0	-1610	0	0	0	-796	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
11	55	-0	-1580	0	0	0	-764	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
12	55	-0	-1534	0	0	0	-995	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
13	55	-0	-1504	0	0	0	-963	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
14	55	-0	-1620	0	0	0	-904	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
15	55	-0	-1517	0	0	0	-796	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
16	55	-0	-1597	0	0	0	-964	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
17	55	-0	-1495	0	0	0	-855	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
18	55	-0	-3153	0	0	0	-1083	--	--	16.08	16.08	0.18	0.02	0.03	0.20	0.00	0.00	20.9
19	55	-0	-2183	0	0	0	-1576	--	--	16.08	16.08	0.18	0.03	0.02	0.14	0.00	0.00	20.9
20	55	-0	-2518	0	0	0	-1267	--	--	16.08	16.08	0.18	0.02	0.02	0.16	0.00	0.00	20.9
37	55	-0	-3271	0	0	0	-856	--	--	16.08	16.08	0.18	0.01	0.03	0.21	0.00	0.00	20.9
38	55	-0	-1654	0	0	0	-1678	--	--	16.08	16.08	0.18	0.03	0.01	0.10	0.00	0.00	20.9
39	55	-0	-2214	0	0	0	-1163	--	--	16.08	16.08	0.18	0.02	0.02	0.14	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 9 NI 1747 NF 1746 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-3011	0	0	0	891	--	--	16.08	16.08	0.00	0.02	0.02	0.19	0.00	0.00	20.9
2	0	-0	-2326	0	0	0	772	--	--	16.08	16.08	0.10	0.01	0.02	0.15	0.00	0.00	20.9
3	0	-0	-2306	0	0	0	790	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
4	0	-0	-2327	0	0	0	581	--	--	16.08	16.08	0.10	0.01	0.02	0.15	0.00	0.00	20.9
5	0	-0	-2307	0	0	0	600	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
6	0	-0	-2350	0	0	0	683	--	--	16.08	16.08	0.10	0.01	0.02	0.15	0.00	0.00	20.9
7	0	-0	-2282	0	0	0	745	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
8	0	-0	-2351	0	0	0	626	--	--	16.08	16.08	0.10	0.01	0.02	0.15	0.00	0.00	20.9
9	0	-0	-2283	0	0	0	688	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
10	0	-0	-2326	0	0	0	772	--	--	16.08	16.08	0.10	0.01	0.02	0.15	0.00	0.00	20.9
11	0	-0	-2306	0	0	0	790	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
12	0	-0	-2327	0	0	0	581	--	--	16.08	16.08	0.10	0.01	0.02	0.15	0.00	0.00	20.9
13	0	-0	-2307	0	0	0	600	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
14	0	-0	-2350	0	0	0	683	--	--	16.08	16.08	0.10	0.01	0.02	0.15	0.00	0.00	20.9
15	0	-0	-2282	0	0	0	745	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
16	0	-0	-2351	0	0	0	626	--	--	16.08	16.08	0.10	0.01	0.02	0.15	0.00	0.00	20.9
17	0	-0	-2283	0	0	0	688	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
18	0	-0	-4499	0	0	0	1962	--	--	16.08	16.08	0.00	0.03	0.04	0.28	0.00	0.00	20.9
19	0	-0	-3543	0	0	0	861	--	--	16.08	16.08	0.00	0.01	0.03	0.22	0.00	0.00	20.9
20	0	-0	-3842	0	0	0	1351	--	--	16.08	16.08	0.00	0.02	0.03	0.24	0.00	0.00	20.9
37	0	-0	-4495	0	0	0	2166	--	--	16.08	16.08	0.00	0.04	0.04	0.28	0.00	0.00	20.9
38	0	-0	-2902	0	0	0	330	--	--	16.08	16.08	0.00	0.01	0.02	0.18	0.00	0.00	20.9
39	0	-0	-3400	0	0	0	1147	--	--	16.08	16.08	0.00	0.02	0.03	0.21	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-3011	0	0	0	891	--	--	16.08	16.08	0.00	0.02	0.02	0.19	0.00	0.00	20.9
2	27	-0	-2326	0	0	0	772	--	--	16.08	16.08	0.10	0.01	0.02	0.15	0.00	0.00	20.9
3	27	-0	-2306	0	0	0	790	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
4	27	-0	-2327	0	0	0	-689	--	--	16.08	16.08	0.29	0.01	0.02	0.15	0.00	0.00	20.9
5	27	-0	-2307	0	0	0	-659	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
6	27	-0	-2350	0	0	0	683	--	--	16.08	16.08	0.10	0.01	0.02	0.15	0.00	0.00	20.9
7	27	-0	-2282	0	0	0	745	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
8	27	-0	-2351	0	0	0	-656	--	--	16.08	16.08	0.29	0.01	0.02	0.15	0.00	0.00	20.9
9	27	-0	-2283	0	0	0	688	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
10	27	-0	-2326	0	0	0	772	--	--	16.08	16.08	0.10	0.01	0.02	0.15	0.00	0.00	20.9
11	27	-0	-2306	0	0	0	790	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
12	27	-0	-2327	0	0	0	-689	--	--	16.08	16.08	0.29	0.01	0.02	0.15	0.00	0.00	20.9

13	27	-0	-2307	0	0	0	-659	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
14	27	-0	-2350	0	0	0	683	--	--	16.08	16.08	0.10	0.01	0.02	0.15	0.00	0.00	20.9
15	27	-0	-2282	0	0	0	745	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
16	27	-0	-2351	0	0	0	-656	--	--	16.08	16.08	0.29	0.01	0.02	0.15	0.00	0.00	20.9
17	27	-0	-2283	0	0	0	688	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
18	27	-0	-4499	0	0	0	1962	--	--	16.08	16.08	0.00	0.03	0.04	0.28	0.00	0.00	20.9
19	27	-0	-3543	0	0	0	-1072	--	--	16.08	16.08	0.18	0.02	0.03	0.22	0.00	0.00	20.9
20	27	-0	-3842	0	0	0	1351	--	--	16.08	16.08	0.00	0.02	0.03	0.24	0.00	0.00	20.9
37	27	-0	-4495	0	0	0	2166	--	--	16.08	16.08	0.00	0.04	0.04	0.28	0.00	0.00	20.9
38	27	-0	-2902	0	0	0	-1253	--	--	16.08	16.08	0.18	0.02	0.02	0.18	0.00	0.00	20.9
39	27	-0	-3400	0	0	0	1147	--	--	16.08	16.08	0.00	0.02	0.03	0.21	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	-3011	0	0	0	-752	--	--	16.08	16.08	0.18	0.01	0.02	0.19	0.00	0.00	20.9
2	55	-0	-2326	0	0	0	-497	--	--	16.08	16.08	0.29	0.01	0.02	0.15	0.00	0.00	20.9
3	55	-0	-2306	0	0	0	-467	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
4	55	-0	-2327	0	0	0	-689	--	--	16.08	16.08	0.29	0.01	0.02	0.15	0.00	0.00	20.9
5	55	-0	-2307	0	0	0	-659	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
6	55	-0	-2350	0	0	0	-599	--	--	16.08	16.08	0.29	0.01	0.02	0.15	0.00	0.00	20.9
7	55	-0	-2282	0	0	0	-500	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
8	55	-0	-2351	0	0	0	-656	--	--	16.08	16.08	0.29	0.01	0.02	0.15	0.00	0.00	20.9
9	55	-0	-2283	0	0	0	-557	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
10	55	-0	-2326	0	0	0	-497	--	--	16.08	16.08	0.29	0.01	0.02	0.15	0.00	0.00	20.9
11	55	-0	-2306	0	0	0	-467	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
12	55	-0	-2327	0	0	0	-689	--	--	16.08	16.08	0.29	0.01	0.02	0.15	0.00	0.00	20.9
13	55	-0	-2307	0	0	0	-659	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
14	55	-0	-2350	0	0	0	-599	--	--	16.08	16.08	0.29	0.01	0.02	0.15	0.00	0.00	20.9
15	55	-0	-2282	0	0	0	-500	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
16	55	-0	-2351	0	0	0	-656	--	--	16.08	16.08	0.29	0.01	0.02	0.15	0.00	0.00	20.9
17	55	-0	-2283	0	0	0	-557	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
18	55	-0	-4499	0	0	0	-492	--	--	16.08	16.08	0.18	0.01	0.04	0.28	0.00	0.00	20.9
19	55	-0	-3543	0	0	0	-1072	--	--	16.08	16.08	0.18	0.02	0.03	0.22	0.00	0.00	20.9
20	55	-0	-3842	0	0	0	-745	--	--	16.08	16.08	0.18	0.01	0.03	0.24	0.00	0.00	20.9
37	55	-0	-4495	0	0	0	-286	--	--	16.08	16.08	0.18	0.00	0.04	0.28	0.00	0.00	20.9
38	55	-0	-2902	0	0	0	-1253	--	--	16.08	16.08	0.18	0.02	0.02	0.18	0.00	0.00	20.9
39	55	-0	-3400	0	0	0	-707	--	--	16.08	16.08	0.18	0.01	0.03	0.21	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 10 NI 1741 NF 1747 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-2886	0	0	0	1276	--	--	16.08	16.08	0.00	0.02	0.02	0.18	0.00	0.00	20.9
2	0	-0	-2293	0	0	0	1110	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
3	0	-0	-2303	0	0	0	1147	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
4	0	-0	-2138	0	0	0	816	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
5	0	-0	-2148	0	0	0	853	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
6	0	-0	-2227	0	0	0	964	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
7	0	-0	-2260	0	0	0	1087	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
8	0	-0	-2181	0	0	0	876	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
9	0	-0	-2214	0	0	0	999	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
10	0	-0	-2293	0	0	0	1110	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
11	0	-0	-2303	0	0	0	1147	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
12	0	-0	-2138	0	0	0	816	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
13	0	-0	-2148	0	0	0	853	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
14	0	-0	-2227	0	0	0	964	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
15	0	-0	-2260	0	0	0	1087	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
16	0	-0	-2181	0	0	0	876	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
17	0	-0	-2214	0	0	0	999	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
18	0	-0	-4419	0	0	0	2605	--	--	16.08	16.08	0.00	0.04	0.04	0.28	0.00	0.00	20.9
19	0	-0	-2781	0	0	0	918	--	--	16.08	16.08	0.00	0.02	0.02	0.17	0.00	0.00	20.9
20	0	-0	-3549	0	0	0	1762	--	--	16.08	16.08	0.00	0.03	0.03	0.22	0.00	0.00	20.9
37	0	-0	-4739	0	0	0	3016	--	--	16.08	16.08	0.00	0.05	0.04	0.30	0.00	0.00	20.9
38	0	-0	-2010	0	0	0	205	--	--	16.08	16.08	0.00	0.00	0.02	0.13	0.00	0.00	20.9
39	0	-0	-3289	0	0	0	1612	--	--	16.08	16.08	0.00	0.03	0.03	0.21	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-2886	0	0	0	1276	--	--	16.08	16.08	0.00	0.02	0.02	0.18	0.00	0.00	20.9
2	27	-0	-2293	0	0	0	1110	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
3	27	-0	-2303	0	0	0	1147	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
4	27	-0	-2138	0	0	0	816	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
5	27	-0	-2148	0	0	0	853	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
6	27	-0	-2227	0	0	0	964	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
7	27	-0	-2260	0	0	0	1087	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
8	27	-0	-2181	0	0	0	876	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
9	27	-0	-2214	0	0	0	999	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
10	27	-0	-2293	0	0	0	1110	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
11	27	-0	-2303	0	0	0	1147	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
12	27	-0	-2138	0	0	0	816	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
13	27	-0	-2148	0	0	0	853	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
14	27	-0	-2227	0	0	0	964	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
15	27	-0	-2260	0	0	0	1087	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
16	27	-0	-2181	0	0	0	876	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
17	27	-0	-2214	0	0	0	999	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
18	27	-0	-4419	0	0	0	2605	--	--	16.08	16.08	0.00	0.04	0.04	0.28	0.00	0.00	20.9
19	27	-0	-2781	0	0	0	918	--	--	16.08	16.08	0.00	0.02	0.02	0.17	0.00	0.00	20.9
20	27	-0	-3549	0	0	0	1762	--	--	16.08	16.08	0.00	0.03	0.03	0.22	0.00	0.00	20.9
37	27	-0	-4739	0	0	0	3016	--	--	16.08	16.08	0.00	0.05	0.04	0.30	0.00	0.00	20.9
38	27	-0	-2010	0	0	0	-891	--	--	16.08	16.08	0.18	0.01	0.02	0.13	0.00	0.00	20.9
39	27	-0	-3289	0	0	0	1612	--	--	16.08	16.08	0.00	0.03	0.03	0.21	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	-2886	0	0	0	-298	--	--	16.08	16.08	0.18	0.00	0.02	0.18	0.00	0.00	20.9
2	55	-0	-2293	0	0	0	-140	--	--	16.08	16.08	0.29	0.00	0.02	0.14	0.00	0.00	20.9
3	55	-0	-2303	0	0	0	-109	--	--	16.08	16.08	0.29	0.00	0.02	0.14	0.00	0.00	20.9
4	55	-0	-2138	0	0	0	-350	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
5	55	-0	-2148	0	0	0	-319	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
6	55	-0	-2227	0	0	0	-250	--	--	16.08	16.08	0.29	0.00	0.02	0.14	0.00	0.00	20.9
7	55	-0	-2260	0	0	0	-146	--	--	16.08	16.08	0.29	0.00	0.02	0.14	0.00	0.00	20.9
8	55	-0	-2181	0	0	0	-313	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9

9	55	-0	-2214	0	0	0	-209	--	--	16.08	16.08	0.29	0.00	0.02	0.14	0.00	0.00	20.9
10	55	-0	-2293	0	0	0	-140	--	--	16.08	16.08	0.29	0.00	0.02	0.14	0.00	0.00	20.9
11	55	-0	-2303	0	0	0	-109	--	--	16.08	16.08	0.29	0.00	0.02	0.14	0.00	0.00	20.9
12	55	-0	-2138	0	0	0	-350	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
13	55	-0	-2148	0	0	0	-319	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
14	55	-0	-2227	0	0	0	-250	--	--	16.08	16.08	0.29	0.00	0.02	0.14	0.00	0.00	20.9
15	55	-0	-2260	0	0	0	-146	--	--	16.08	16.08	0.29	0.00	0.02	0.14	0.00	0.00	20.9
16	55	-0	-2181	0	0	0	-313	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
17	55	-0	-2214	0	0	0	-209	--	--	16.08	16.08	0.29	0.00	0.02	0.14	0.00	0.00	20.9
18	55	-0	-4419	0	0	0	195	--	--	16.08	16.08	0.00	0.00	0.04	0.28	0.00	0.00	20.9
19	55	-0	-2781	0	0	0	-599	--	--	16.08	16.08	0.18	0.01	0.02	0.17	0.00	0.00	20.9
20	55	-0	-3549	0	0	0	-173	--	--	16.08	16.08	0.18	0.00	0.03	0.22	0.00	0.00	20.9
37	55	-0	-4739	0	0	0	431	--	--	16.08	16.08	0.00	0.01	0.04	0.30	0.00	0.00	20.9
38	55	-0	-2010	0	0	0	-891	--	--	16.08	16.08	0.18	0.01	0.02	0.13	0.00	0.00	20.9
39	55	-0	-3289	0	0	0	-182	--	--	16.08	16.08	0.18	0.00	0.03	0.21	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 11 NI 1622 NF 1741 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	1229	0	0	0	-412	--	--	16.08	16.08	0.18	0.01	0.01	0.08	0.00	0.00	20.9
2	0	-0	322	0	0	0	140	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
3	0	-0	321	0	0	0	164	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
4	0	-0	1570	0	0	0	-798	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
5	0	-0	1569	0	0	0	-774	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
6	0	-0	759	0	0	0	-216	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
7	0	-0	758	0	0	0	-136	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
8	0	-0	1134	0	0	0	-498	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
9	0	-0	1132	0	0	0	-418	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
10	0	-0	322	0	0	0	140	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
11	0	-0	321	0	0	0	164	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
12	0	-0	1570	0	0	0	-798	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
13	0	-0	1569	0	0	0	-774	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
14	0	-0	759	0	0	0	-216	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
15	0	-0	758	0	0	0	-136	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
16	0	-0	1134	0	0	0	-498	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
17	0	-0	1132	0	0	0	-418	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
18	0	-0	589	0	0	0	770	--	--	16.08	16.08	0.00	0.01	0.00	0.04	0.00	0.00	20.9
19	0	-0	5979	0	0	0	-3379	--	--	16.08	16.08	0.18	0.06	0.05	0.38	0.00	0.00	20.9
20	0	-0	2927	0	0	0	-1116	--	--	16.08	16.08	0.18	0.02	0.02	0.18	0.00	0.00	20.9
37	0	-0	-1882	0	0	0	2451	--	--	16.08	16.08	0.00	0.04	0.02	0.12	0.00	0.00	20.9
38	0	-0	7103	0	0	0	-4463	--	--	16.08	16.08	0.18	0.07	0.06	0.45	0.00	0.00	20.9
39	0	-0	2016	0	0	0	-693	--	--	16.08	16.08	0.18	0.01	0.02	0.13	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	1229	0	0	0	-412	--	--	16.08	16.08	0.18	0.01	0.01	0.08	0.00	0.00	20.9
2	27	-0	322	0	0	0	571	--	--	16.08	16.08	0.10	0.01	0.00	0.02	0.00	0.00	20.9
3	27	-0	321	0	0	0	595	--	--	16.08	16.08	0.10	0.01	0.00	0.02	0.00	0.00	20.9
4	27	-0	1570	0	0	0	-798	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
5	27	-0	1569	0	0	0	-774	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
6	27	-0	759	0	0	0	-216	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
7	27	-0	758	0	0	0	880	--	--	16.08	16.08	0.10	0.02	0.01	0.05	0.00	0.00	20.9
8	27	-0	1134	0	0	0	-498	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
9	27	-0	1132	0	0	0	-418	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
10	27	-0	322	0	0	0	571	--	--	16.08	16.08	0.10	0.01	0.00	0.02	0.00	0.00	20.9
11	27	-0	321	0	0	0	595	--	--	16.08	16.08	0.10	0.01	0.00	0.02	0.00	0.00	20.9
12	27	-0	1570	0	0	0	-798	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
13	27	-0	1569	0	0	0	-774	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
14	27	-0	759	0	0	0	-216	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
15	27	-0	758	0	0	0	880	--	--	16.08	16.08	0.10	0.02	0.01	0.05	0.00	0.00	20.9
16	27	-0	1134	0	0	0	-498	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
17	27	-0	1132	0	0	0	-418	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
18	27	-0	589	0	0	0	1560	--	--	16.08	16.08	0.00	0.03	0.00	0.04	0.00	0.00	20.9
19	27	-0	5979	0	0	0	-3379	--	--	16.08	16.08	0.18	0.06	0.05	0.38	0.00	0.00	20.9
20	27	-0	2927	0	0	0	-1116	--	--	16.08	16.08	0.18	0.02	0.02	0.18	0.00	0.00	20.9
37	27	-0	-1882	0	0	0	2451	--	--	16.08	16.08	0.00	0.04	0.02	0.12	0.00	0.00	20.9
38	27	-0	7103	0	0	0	-4463	--	--	16.08	16.08	0.18	0.07	0.06	0.45	0.00	0.00	20.9
39	27	-0	2016	0	0	0	-693	--	--	16.08	16.08	0.18	0.01	0.02	0.13	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	1229	0	0	0	259	--	--	16.08	16.08	0.00	0.00	0.01	0.08	0.00	0.00	20.9
2	55	-0	322	0	0	0	315	--	--	16.08	16.08	0.10	0.01	0.00	0.02	0.00	0.00	20.9
3	55	-0	321	0	0	0	339	--	--	16.08	16.08	0.10	0.01	0.00	0.02	0.00	0.00	20.9
4	55	-0	1570	0	0	0	59	--	--	16.08	16.08	0.10	0.00	0.01	0.10	0.00	0.00	20.9
5	55	-0	1569	0	0	0	82	--	--	16.08	16.08	0.10	0.00	0.01	0.10	0.00	0.00	20.9
6	55	-0	759	0	0	0	198	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
7	55	-0	758	0	0	0	277	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
8	55	-0	1134	0	0	0	121	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
9	55	-0	1132	0	0	0	200	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
10	55	-0	322	0	0	0	315	--	--	16.08	16.08	0.10	0.01	0.00	0.02	0.00	0.00	20.9
11	55	-0	321	0	0	0	339	--	--	16.08	16.08	0.10	0.01	0.00	0.02	0.00	0.00	20.9
12	55	-0	1570	0	0	0	59	--	--	16.08	16.08	0.10	0.00	0.01	0.10	0.00	0.00	20.9
13	55	-0	1569	0	0	0	82	--	--	16.08	16.08	0.10	0.00	0.01	0.10	0.00	0.00	20.9
14	55	-0	759	0	0	0	198	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
15	55	-0	758	0	0	0	277	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
16	55	-0	1134	0	0	0	121	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
17	55	-0	1132	0	0	0	200	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
18	55	-0	589	0	0	0	1091	--	--	16.08	16.08	0.00	0.02	0.00	0.04	0.00	0.00	20.9
19	55	-0	5979	0	0	0	-3379	--	--	16.08	16.08	0.18	0.06	0.05	0.38	0.00	0.00	20.9
20	55	-0	2927	0	0	0	481	--	--	16.08	16.08	0.00	0.01	0.02	0.18	0.00	0.00	20.9
37	55	-0	-1882	0	0	0	1424	--	--	16.08	16.08	0.00	0.02	0.02	0.12	0.00	0.00	20.9
38	55	-0	7103	0	0	0	-4463	--	--	16.08	16.08	0.18	0.07	0.06	0.45	0.00	0.00	20.9
39	55	-0	2016	0	0	0	407	--	--	16.08	16.08	0.00	0.01	0.02	0.13	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 12 NI 1760 NF 1622 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-1399	0	0	0	598	--	--	16.08	16.08	0.00	0.01	0.01	0.09	0.00	0.00	20.9
2	0	-0	-407	0	0	0	514	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
3	0	-0	-461	0	0	0	552	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
4	0	-0	-1691	0	0	0	369	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
5	0	-0	-1745	0	0	0	407	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
6	0	-0	-793	0	0	0	420	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
7	0	-0	-974	0	0	0	544	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
8	0	-0	-1178	0	0	0	376	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
9	0	-0	-1359	0	0	0	501	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
10	0	-0	-407	0	0	0	514	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
11	0	-0	-461	0	0	0	552	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
12	0	-0	-1691	0	0	0	369	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
13	0	-0	-1745	0	0	0	407	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
14	0	-0	-793	0	0	0	420	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
15	0	-0	-974	0	0	0	544	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
16	0	-0	-1178	0	0	0	376	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
17	0	-0	-1359	0	0	0	501	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
18	0	-0	-419	0	0	0	1421	--	--	16.08	16.08	0.00	0.02	0.00	0.03	0.00	0.00	20.9
19	0	-0	-5837	0	0	0	599	--	--	16.08	16.08	0.00	0.01	0.05	0.37	0.00	0.00	20.9
20	0	-0	-3019	0	0	0	1035	--	--	16.08	16.08	0.00	0.02	0.02	0.19	0.00	0.00	20.9
37	0	-0	1956	0	0	0	1565	--	--	16.08	16.08	0.00	0.03	0.02	0.12	0.00	0.00	20.9
38	0	-0	-7074	0	0	0	195	--	--	16.08	16.08	0.00	0.00	0.06	0.44	0.00	0.00	20.9
39	0	-0	-2378	0	0	0	922	--	--	16.08	16.08	0.00	0.02	0.02	0.15	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-1399	0	0	0	598	--	--	16.08	16.08	0.00	0.01	0.01	0.09	0.00	0.00	20.9
2	27	-0	-407	0	0	0	514	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
3	27	-0	-461	0	0	0	552	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
4	27	-0	-1691	0	0	0	-553	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
5	27	-0	-1745	0	0	0	-546	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
6	27	-0	-793	0	0	0	420	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
7	27	-0	-974	0	0	0	544	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
8	27	-0	-1178	0	0	0	376	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
9	27	-0	-1359	0	0	0	501	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
10	27	-0	-407	0	0	0	514	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
11	27	-0	-461	0	0	0	552	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
12	27	-0	-1691	0	0	0	-553	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
13	27	-0	-1745	0	0	0	-546	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
14	27	-0	-793	0	0	0	420	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
15	27	-0	-974	0	0	0	544	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
16	27	-0	-1178	0	0	0	376	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
17	27	-0	-1359	0	0	0	501	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
18	27	-0	-419	0	0	0	1421	--	--	16.08	16.08	0.00	0.02	0.00	0.03	0.00	0.00	20.9
19	27	-0	-5837	0	0	0	-2585	--	--	16.08	16.08	0.18	0.04	0.05	0.37	0.00	0.00	20.9
20	27	-0	-3019	0	0	0	1035	--	--	16.08	16.08	0.00	0.02	0.02	0.19	0.00	0.00	20.9
37	27	-0	1956	0	0	0	4189	--	--	16.08	16.08	0.00	0.07	0.02	0.12	0.00	0.00	20.9
38	27	-0	-7074	0	0	0	-3664	--	--	16.08	16.08	0.18	0.06	0.06	0.44	0.00	0.00	20.9
39	27	-0	-2378	0	0	0	922	--	--	16.08	16.08	0.00	0.02	0.02	0.15	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	-1399	0	0	0	-165	--	--	16.08	16.08	0.18	0.00	0.01	0.09	0.00	0.00	20.9
2	55	-0	-407	0	0	0	292	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
3	55	-0	-461	0	0	0	300	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
4	55	-0	-1691	0	0	0	-553	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
5	55	-0	-1745	0	0	0	-546	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
6	55	-0	-793	0	0	0	-13	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
7	55	-0	-974	0	0	0	13	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
8	55	-0	-1178	0	0	0	-266	--	--	16.08	16.08	0.29	0.00	0.01	0.07	0.00	0.00	20.9
9	55	-0	-1359	0	0	0	-241	--	--	16.08	16.08	0.29	0.00	0.01	0.09	0.00	0.00	20.9
10	55	-0	-407	0	0	0	292	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
11	55	-0	-461	0	0	0	300	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
12	55	-0	-1691	0	0	0	-553	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
13	55	-0	-1745	0	0	0	-546	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
14	55	-0	-793	0	0	0	-13	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
15	55	-0	-974	0	0	0	13	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
16	55	-0	-1178	0	0	0	-266	--	--	16.08	16.08	0.29	0.00	0.01	0.07	0.00	0.00	20.9
17	55	-0	-1359	0	0	0	-241	--	--	16.08	16.08	0.29	0.00	0.01	0.09	0.00	0.00	20.9
18	55	-0	-419	0	0	0	1193	--	--	16.08	16.08	0.00	0.02	0.00	0.03	0.00	0.00	20.9
19	55	-0	-5837	0	0	0	-2585	--	--	16.08	16.08	0.18	0.04	0.05	0.37	0.00	0.00	20.9
20	55	-0	-3019	0	0	0	-612	--	--	16.08	16.08	0.18	0.01	0.02	0.19	0.00	0.00	20.9
37	55	-0	1956	0	0	0	2633	--	--	16.08	16.08	0.00	0.04	0.02	0.12	0.00	0.00	20.9
38	55	-0	-7074	0	0	0	-3664	--	--	16.08	16.08	0.18	0.06	0.06	0.44	0.00	0.00	20.9
39	55	-0	-2378	0	0	0	-375	--	--	16.08	16.08	0.18	0.01	0.02	0.15	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 13 NI 1753 NF 1760 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	2435	0	0	0	80	--	--	16.08	16.08	0.00	0.00	0.02	0.15	0.00	0.00	20.9
2	0	-0	2000	0	0	0	104	--	--	16.08	16.08	0.10	0.00	0.02	0.13	0.00	0.00	20.9
3	0	-0	2005	0	0	0	130	--	--	16.08	16.08	0.10	0.00	0.02	0.13	0.00	0.00	20.9
4	0	-0	1741	0	0	0	-7	--	--	16.08	16.08	0.29	0.00	0.01	0.11	0.00	0.00	20.9
5	0	-0	1747	0	0	0	19	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
6	0	-0	1903	0	0	0	36	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
7	0	-0	1921	0	0	0	121	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
8	0	-0	1825	0	0	0	2	--	--	16.08	16.08	0.10	0.00	0.02	0.11	0.00	0.00	20.9
9	0	-0	1844	0	0	0	87	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
10	0	-0	2000	0	0	0	104	--	--	16.08	16.08	0.10	0.00	0.02	0.13	0.00	0.00	20.9
11	0	-0	2005	0	0	0	130	--	--	16.08	16.08	0.10	0.00	0.02	0.13	0.00	0.00	20.9
12	0	-0	1741	0	0	0	-7	--	--	16.08	16.08	0.29	0.00	0.01	0.11	0.00	0.00	20.9
13	0	-0	1747	0	0	0	19	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
14	0	-0	1903	0	0	0	36	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
15	0	-0	1921	0	0	0	121	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
16	0	-0	1825	0	0	0	2	--	--	16.08	16.08	0.10	0.00	0.02	0.11	0.00	0.00	20.9

17	0	-0	1844	0	0	0	87	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
18	0	-0	4120	0	0	0	550	--	--	16.08	16.08	0.00	0.01	0.03	0.26	0.00	0.00	20.9
19	0	-0	2190	0	0	0	69	--	--	16.08	16.08	0.00	0.00	0.02	0.14	0.00	0.00	20.9
20	0	-0	3044	0	0	0	332	--	--	16.08	16.08	0.00	0.01	0.03	0.19	0.00	0.00	20.9
37	0	-0	4537	0	0	0	638	--	--	16.08	16.08	0.00	0.01	0.04	0.28	0.00	0.00	20.9
38	0	-0	1321	0	0	0	-163	--	--	16.08	16.08	0.18	0.00	0.01	0.08	0.00	0.00	20.9
39	0	-0	2744	0	0	0	275	--	--	16.08	16.08	0.00	0.00	0.02	0.17	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	2435	0	0	0	3346	--	--	16.08	16.08	0.00	0.06	0.02	0.15	0.00	0.00	20.9
2	27	-0	2000	0	0	0	2787	--	--	16.08	16.08	0.10	0.05	0.02	0.13	0.00	0.00	20.9
3	27	-0	2005	0	0	0	2820	--	--	16.08	16.08	0.10	0.05	0.02	0.13	0.00	0.00	20.9
4	27	-0	1741	0	0	0	2329	--	--	16.08	16.08	0.10	0.04	0.01	0.11	0.00	0.00	20.9
5	27	-0	1747	0	0	0	2362	--	--	16.08	16.08	0.10	0.04	0.01	0.11	0.00	0.00	20.9
6	27	-0	1903	0	0	0	2589	--	--	16.08	16.08	0.10	0.05	0.02	0.12	0.00	0.00	20.9
7	27	-0	1921	0	0	0	2698	--	--	16.08	16.08	0.10	0.05	0.02	0.12	0.00	0.00	20.9
8	27	-0	1825	0	0	0	2451	--	--	16.08	16.08	0.10	0.04	0.02	0.11	0.00	0.00	20.9
9	27	-0	1844	0	0	0	2561	--	--	16.08	16.08	0.10	0.05	0.02	0.12	0.00	0.00	20.9
10	27	-0	2000	0	0	0	2787	--	--	16.08	16.08	0.10	0.05	0.02	0.13	0.00	0.00	20.9
11	27	-0	2005	0	0	0	2820	--	--	16.08	16.08	0.10	0.05	0.02	0.13	0.00	0.00	20.9
12	27	-0	1741	0	0	0	2329	--	--	16.08	16.08	0.10	0.04	0.01	0.11	0.00	0.00	20.9
13	27	-0	1747	0	0	0	2362	--	--	16.08	16.08	0.10	0.04	0.01	0.11	0.00	0.00	20.9
14	27	-0	1903	0	0	0	2589	--	--	16.08	16.08	0.10	0.05	0.02	0.12	0.00	0.00	20.9
15	27	-0	1921	0	0	0	2698	--	--	16.08	16.08	0.10	0.05	0.02	0.12	0.00	0.00	20.9
16	27	-0	1825	0	0	0	2451	--	--	16.08	16.08	0.10	0.04	0.02	0.11	0.00	0.00	20.9
17	27	-0	1844	0	0	0	2561	--	--	16.08	16.08	0.10	0.05	0.02	0.12	0.00	0.00	20.9
18	27	-0	4120	0	0	0	6077	--	--	16.08	16.08	0.00	0.10	0.03	0.26	0.00	0.00	20.9
19	27	-0	2190	0	0	0	3007	--	--	16.08	16.08	0.00	0.05	0.02	0.14	0.00	0.00	20.9
20	27	-0	3044	0	0	0	4415	--	--	16.08	16.08	0.00	0.08	0.03	0.19	0.00	0.00	20.9
37	27	-0	4537	0	0	0	6724	--	--	16.08	16.08	0.00	0.11	0.04	0.28	0.00	0.00	20.9
38	27	-0	1321	0	0	0	1609	--	--	16.08	16.08	0.00	0.03	0.01	0.08	0.00	0.00	20.9
39	27	-0	2744	0	0	0	3956	--	--	16.08	16.08	0.00	0.07	0.02	0.17	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	2435	0	0	0	1408	--	--	16.08	16.08	0.00	0.02	0.02	0.15	0.00	0.00	20.9
2	55	-0	2000	0	0	0	1195	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
3	55	-0	2005	0	0	0	1224	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
4	55	-0	1741	0	0	0	943	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
5	55	-0	1747	0	0	0	971	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
6	55	-0	1903	0	0	0	1074	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
7	55	-0	1921	0	0	0	1169	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
8	55	-0	1825	0	0	0	998	--	--	16.08	16.08	0.10	0.02	0.02	0.11	0.00	0.00	20.9
9	55	-0	1844	0	0	0	1093	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
10	55	-0	2000	0	0	0	1195	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
11	55	-0	2005	0	0	0	1224	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
12	55	-0	1741	0	0	0	943	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
13	55	-0	1747	0	0	0	971	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
14	55	-0	1903	0	0	0	1074	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
15	55	-0	1921	0	0	0	1169	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
16	55	-0	1825	0	0	0	998	--	--	16.08	16.08	0.10	0.02	0.02	0.11	0.00	0.00	20.9
17	55	-0	1844	0	0	0	1093	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
18	55	-0	4120	0	0	0	2797	--	--	16.08	16.08	0.00	0.05	0.03	0.26	0.00	0.00	20.9
19	55	-0	2190	0	0	0	1264	--	--	16.08	16.08	0.00	0.02	0.02	0.14	0.00	0.00	20.9
20	55	-0	3044	0	0	0	1992	--	--	16.08	16.08	0.00	0.03	0.03	0.19	0.00	0.00	20.9
37	55	-0	4537	0	0	0	3112	--	--	16.08	16.08	0.00	0.05	0.04	0.28	0.00	0.00	20.9
38	55	-0	1321	0	0	0	557	--	--	16.08	16.08	0.00	0.01	0.01	0.08	0.00	0.00	20.9
39	55	-0	2744	0	0	0	1771	--	--	16.08	16.08	0.00	0.03	0.02	0.17	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 14 NI 1754 NF 1753 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	2411	0	0	0	-293	--	--	16.08	16.08	0.18	0.00	0.02	0.15	0.00	0.00	20.9
2	0	-0	1876	0	0	0	-195	--	--	16.08	16.08	0.29	0.00	0.02	0.12	0.00	0.00	20.9
3	0	-0	1921	0	0	0	-171	--	--	16.08	16.08	0.29	0.00	0.02	0.12	0.00	0.00	20.9
4	0	-0	1788	0	0	0	-280	--	--	16.08	16.08	0.29	0.00	0.01	0.11	0.00	0.00	20.9
5	0	-0	1833	0	0	0	-256	--	--	16.08	16.08	0.29	0.00	0.02	0.11	0.00	0.00	20.9
6	0	-0	1794	0	0	0	-253	--	--	16.08	16.08	0.29	0.00	0.01	0.11	0.00	0.00	20.9
7	0	-0	1942	0	0	0	-173	--	--	16.08	16.08	0.29	0.00	0.02	0.12	0.00	0.00	20.9
8	0	-0	1767	0	0	0	-278	--	--	16.08	16.08	0.29	0.00	0.01	0.11	0.00	0.00	20.9
9	0	-0	1916	0	0	0	-198	--	--	16.08	16.08	0.29	0.00	0.02	0.12	0.00	0.00	20.9
10	0	-0	1876	0	0	0	-195	--	--	16.08	16.08	0.29	0.00	0.02	0.12	0.00	0.00	20.9
11	0	-0	1921	0	0	0	-171	--	--	16.08	16.08	0.29	0.00	0.02	0.12	0.00	0.00	20.9
12	0	-0	1788	0	0	0	-280	--	--	16.08	16.08	0.29	0.00	0.01	0.11	0.00	0.00	20.9
13	0	-0	1833	0	0	0	-256	--	--	16.08	16.08	0.29	0.00	0.02	0.11	0.00	0.00	20.9
14	0	-0	1794	0	0	0	-253	--	--	16.08	16.08	0.29	0.00	0.01	0.11	0.00	0.00	20.9
15	0	-0	1942	0	0	0	-173	--	--	16.08	16.08	0.29	0.00	0.02	0.12	0.00	0.00	20.9
16	0	-0	1767	0	0	0	-278	--	--	16.08	16.08	0.29	0.00	0.01	0.11	0.00	0.00	20.9
17	0	-0	1916	0	0	0	-198	--	--	16.08	16.08	0.29	0.00	0.02	0.12	0.00	0.00	20.9
18	0	-0	3888	0	0	0	-67	--	--	16.08	16.08	0.18	0.00	0.03	0.24	0.00	0.00	20.9
19	0	-0	2709	0	0	0	-325	--	--	16.08	16.08	0.18	0.01	0.02	0.17	0.00	0.00	20.9
20	0	-0	3269	0	0	0	-155	--	--	16.08	16.08	0.18	0.00	0.03	0.21	0.00	0.00	20.9
37	0	-0	3998	0	0	0	-11	--	--	16.08	16.08	0.18	0.00	0.03	0.25	0.00	0.00	20.9
38	0	-0	2035	0	0	0	-441	--	--	16.08	16.08	0.18	0.01	0.02	0.13	0.00	0.00	20.9
39	0	-0	2968	0	0	0	-159	--	--	16.08	16.08	0.18	0.00	0.02	0.19	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	2411	0	0	0	2941	--	--	16.08	16.08	0.00	0.05	0.02	0.15	0.00	0.00	20.9
2	27	-0	1876	0	0	0	2321	--	--	16.08	16.08	0.10	0.04	0.02	0.12	0.00	0.00	20.9
3	27	-0	1921	0	0	0	2406	--	--	16.08	16.08	0.10	0.04	0.02	0.12	0.00	0.00	20.9
4	27	-0	1788	0	0	0	2119	--	--	16.08	16.08	0.10	0.04	0.01	0.11	0.00	0.00	20.9
5	27	-0	1833	0	0	0	2203	--	--	16.08	16.08	0.10	0.04	0.02	0.11	0.00	0.00	20.9
6	27	-0	1794	0	0	0	2154	--	--	16.08	16.08	0.10	0.04	0.01	0.11	0.00	0.00	20.9
7	27	-0	1942	0	0	0	2432	--	--	16.08	16.08	0.10	0.04	0.02	0.12	0.00	0.00	20.9
8	27	-0	1767	0	0	0	2093	--	--	16.08	16.08	0.10	0.04	0.01	0.11	0.00	0.00	20.9
9	27	-0	1916	0	0	0	2372	--	--	16.08	16.08	0.10	0.04	0.02	0.12	0.00	0.00	20.9
10	27	-0	1876	0	0	0	2321	--	--	16.08	16.08	0.10	0.04	0.02	0.12	0.00	0.00	20.9
11	27	-0	1921	0	0	0	2406	--	--	16.08	16.08	0.10	0.04	0.02	0.12	0.00	0.00	20.9
12	27	-0	1788	0	0	0	2119	--	--	16.08	16.08	0.10	0.04	0.01	0.11	0.00	0.00	20.9

13	27	-0	1833	0	0	0	2203	--	--	16.08	16.08	0.10	0.04	0.02	0.11	0.00	0.00	20.9
14	27	-0	1794	0	0	0	2154	--	--	16.08	16.08	0.10	0.04	0.01	0.11	0.00	0.00	20.9
15	27	-0	1942	0	0	0	2432	--	--	16.08	16.08	0.10	0.04	0.02	0.12	0.00	0.00	20.9
16	27	-0	1767	0	0	0	2093	--	--	16.08	16.08	0.10	0.04	0.01	0.11	0.00	0.00	20.9
17	27	-0	1916	0	0	0	2372	--	--	16.08	16.08	0.10	0.04	0.02	0.12	0.00	0.00	20.9
18	27	-0	3888	0	0	0	5149	--	--	16.08	16.08	0.00	0.09	0.03	0.24	0.00	0.00	20.9
19	27	-0	2709	0	0	0	3309	--	--	16.08	16.08	0.00	0.06	0.02	0.17	0.00	0.00	20.9
20	27	-0	3269	0	0	0	4230	--	--	16.08	16.08	0.00	0.07	0.03	0.21	0.00	0.00	20.9
37	27	-0	3998	0	0	0	5352	--	--	16.08	16.08	0.00	0.09	0.03	0.25	0.00	0.00	20.9
38	27	-0	2035	0	0	0	2289	--	--	16.08	16.08	0.00	0.04	0.02	0.13	0.00	0.00	20.9
39	27	-0	2968	0	0	0	3823	--	--	16.08	16.08	0.00	0.07	0.02	0.19	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	2411	0	0	0	1022	--	--	16.08	16.08	0.00	0.02	0.02	0.15	0.00	0.00	20.9
2	55	-0	1876	0	0	0	828	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
3	55	-0	1921	0	0	0	876	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
4	55	-0	1788	0	0	0	696	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
5	55	-0	1833	0	0	0	744	--	--	16.08	16.08	0.10	0.01	0.02	0.11	0.00	0.00	20.9
6	55	-0	1794	0	0	0	726	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
7	55	-0	1942	0	0	0	886	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
8	55	-0	1767	0	0	0	686	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
9	55	-0	1916	0	0	0	847	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
10	55	-0	1876	0	0	0	828	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
11	55	-0	1921	0	0	0	876	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
12	55	-0	1788	0	0	0	696	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
13	55	-0	1833	0	0	0	744	--	--	16.08	16.08	0.10	0.01	0.02	0.11	0.00	0.00	20.9
14	55	-0	1794	0	0	0	726	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
15	55	-0	1942	0	0	0	886	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
16	55	-0	1767	0	0	0	686	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
17	55	-0	1916	0	0	0	847	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
18	55	-0	3888	0	0	0	2054	--	--	16.08	16.08	0.00	0.04	0.03	0.24	0.00	0.00	20.9
19	55	-0	2709	0	0	0	1153	--	--	16.08	16.08	0.00	0.02	0.02	0.17	0.00	0.00	20.9
20	55	-0	3269	0	0	0	1628	--	--	16.08	16.08	0.00	0.03	0.03	0.21	0.00	0.00	20.9
37	55	-0	3998	0	0	0	2170	--	--	16.08	16.08	0.00	0.04	0.03	0.25	0.00	0.00	20.9
38	55	-0	2035	0	0	0	669	--	--	16.08	16.08	0.00	0.01	0.02	0.13	0.00	0.00	20.9
39	55	-0	2968	0	0	0	1460	--	--	16.08	16.08	0.00	0.02	0.02	0.19	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 15 NI 1744 NF 1754 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm

1	0	-0	1359	0	0	0	-570	--	--	16.08	16.08	0.18	0.01	0.01	0.09	0.00	0.00	20.9
2	0	-0	1092	0	0	0	-404	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
3	0	-0	1140	0	0	0	-388	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
4	0	-0	952	0	0	0	-490	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
5	0	-0	999	0	0	0	-474	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
6	0	-0	987	0	0	0	-453	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
7	0	-0	1146	0	0	0	-399	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
8	0	-0	945	0	0	0	-479	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
9	0	-0	1104	0	0	0	-424	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
10	0	-0	1092	0	0	0	-404	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
11	0	-0	1140	0	0	0	-388	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
12	0	-0	952	0	0	0	-490	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
13	0	-0	999	0	0	0	-474	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
14	0	-0	987	0	0	0	-453	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
15	0	-0	1146	0	0	0	-399	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
16	0	-0	945	0	0	0	-479	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
17	0	-0	1104	0	0	0	-424	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
18	0	-0	2358	0	0	0	-514	--	--	16.08	16.08	0.18	0.01	0.02	0.15	0.00	0.00	20.9
19	0	-0	1286	0	0	0	-694	--	--	16.08	16.08	0.18	0.01	0.01	0.08	0.00	0.00	20.9
20	0	-0	1869	0	0	0	-562	--	--	16.08	16.08	0.18	0.01	0.02	0.12	0.00	0.00	20.9
37	0	-0	2570	0	0	0	-442	--	--	16.08	16.08	0.18	0.01	0.02	0.16	0.00	0.00	20.9
38	0	-0	783	0	0	0	-743	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9
39	0	-0	1756	0	0	0	-522	--	--	16.08	16.08	0.18	0.01	0.01	0.11	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	1359	0	0	0	-570	--	--	16.08	16.08	0.18	0.01	0.01	0.09	0.00	0.00	20.9
2	27	-0	1092	0	0	0	-404	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
3	27	-0	1140	0	0	0	-388	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
4	27	-0	952	0	0	0	-490	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
5	27	-0	999	0	0	0	-474	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
6	27	-0	987	0	0	0	-453	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
7	27	-0	1146	0	0	0	-399	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
8	27	-0	945	0	0	0	-479	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
9	27	-0	1104	0	0	0	-424	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
10	27	-0	1092	0	0	0	-404	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
11	27	-0	1140	0	0	0	-388	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
12	27	-0	952	0	0	0	-490	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
13	27	-0	999	0	0	0	-474	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
14	27	-0	987	0	0	0	-453	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
15	27	-0	1146	0	0	0	-399	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
16	27	-0	945	0	0	0	-479	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
17	27	-0	1104	0	0	0	-424	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
18	27	-0	2358	0	0	0	2649	--	--	16.08	16.08	0.00	0.05	0.02	0.15	0.00	0.00	20.9
19	27	-0	1286	0	0	0	-694	--	--	16.08	16.08	0.18	0.01	0.01	0.08	0.00	0.00	20.9
20	27	-0	1869	0	0	0	-562	--	--	16.08	16.08	0.18	0.01	0.02	0.12	0.00	0.00	20.9
37	27	-0	2570	0	0	0	3005	--	--	16.08	16.08	0.00	0.05	0.02	0.16	0.00	0.00	20.9
38	27	-0	783	0	0	0	-743	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9
39	27	-0	1756	0	0	0	-522	--	--	16.08	16.08	0.18	0.01	0.01	0.11	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	1359	0	0	0	171	--	--	16.08	16.08	0.00	0.00	0.01	0.09	0.00	0.00	20.9
2	55	-0	1092	0	0	0	192	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
3	55	-0	1140	0	0	0	234	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
4	55	-0	952	0	0	0	29	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
5	55	-0	999	0	0	0	71	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
6	55	-0	987	0	0	0	85	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
7	55	-0	1146	0	0	0	227	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
8	55	-0	945	0	0	0	36	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9

9	55	-0	1104	0	0	0	178	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
10	55	-0	1092	0	0	0	192	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
11	55	-0	1140	0	0	0	234	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
12	55	-0	952	0	0	0	29	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
13	55	-0	999	0	0	0	71	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
14	55	-0	987	0	0	0	85	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
15	55	-0	1146	0	0	0	227	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
16	55	-0	945	0	0	0	36	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
17	55	-0	1104	0	0	0	178	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
18	55	-0	2358	0	0	0	772	--	--	16.08	16.08	0.00	0.01	0.02	0.15	0.00	0.00	20.9
19	55	-0	1286	0	0	0	7	--	--	16.08	16.08	0.00	0.00	0.01	0.08	0.00	0.00	20.9
20	55	-0	1869	0	0	0	458	--	--	16.08	16.08	0.00	0.01	0.02	0.12	0.00	0.00	20.9
37	55	-0	2570	0	0	0	959	--	--	16.08	16.08	0.00	0.02	0.02	0.16	0.00	0.00	20.9
38	55	-0	783	0	0	0	-743	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9
39	55	-0	1756	0	0	0	435	--	--	16.08	16.08	0.00	0.01	0.01	0.11	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 16 NI 1758 NF 1744 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	587	0	0	0	-623	--	--	16.08	16.08	0.18	0.01	0.00	0.04	0.00	0.00	20.9
2	0	-0	497	0	0	0	-445	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
3	0	-0	542	0	0	0	-437	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
4	0	-0	361	0	0	0	-521	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
5	0	-0	407	0	0	0	-513	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
6	0	-0	397	0	0	0	-481	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
7	0	-0	548	0	0	0	-454	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
8	0	-0	356	0	0	0	-504	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
9	0	-0	507	0	0	0	-477	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
10	0	-0	497	0	0	0	-445	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
11	0	-0	542	0	0	0	-437	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
12	0	-0	361	0	0	0	-521	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
13	0	-0	407	0	0	0	-513	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
14	0	-0	397	0	0	0	-481	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
15	0	-0	548	0	0	0	-454	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
16	0	-0	356	0	0	0	-504	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
17	0	-0	507	0	0	0	-477	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
18	0	-0	1194	0	0	0	-634	--	--	16.08	16.08	0.18	0.01	0.01	0.07	0.00	0.00	20.9
19	0	-0	392	0	0	0	-754	--	--	16.08	16.08	0.18	0.01	0.00	0.02	0.00	0.00	20.9
20	0	-0	875	0	0	0	-667	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9
37	0	-0	1397	0	0	0	-571	--	--	16.08	16.08	0.18	0.01	0.01	0.09	0.00	0.00	20.9
38	0	-0	62	0	0	0	-770	--	--	16.08	16.08	0.18	0.01	0.00	0.00	0.00	0.00	20.9
39	0	-0	867	0	0	0	-626	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	587	0	0	0	-623	--	--	16.08	16.08	0.18	0.01	0.00	0.04	0.00	0.00	20.9
2	27	-0	497	0	0	0	-445	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
3	27	-0	542	0	0	0	-437	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
4	27	-0	361	0	0	0	-521	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
5	27	-0	407	0	0	0	-513	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
6	27	-0	397	0	0	0	-481	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
7	27	-0	548	0	0	0	-454	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
8	27	-0	356	0	0	0	-504	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
9	27	-0	507	0	0	0	-477	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
10	27	-0	497	0	0	0	-445	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
11	27	-0	542	0	0	0	-437	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
12	27	-0	361	0	0	0	-521	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
13	27	-0	407	0	0	0	-513	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
14	27	-0	397	0	0	0	-481	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
15	27	-0	548	0	0	0	-454	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
16	27	-0	356	0	0	0	-504	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
17	27	-0	507	0	0	0	-477	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
18	27	-0	1194	0	0	0	-634	--	--	16.08	16.08	0.18	0.01	0.01	0.07	0.00	0.00	20.9
19	27	-0	392	0	0	0	-754	--	--	16.08	16.08	0.18	0.01	0.00	0.02	0.00	0.00	20.9
20	27	-0	875	0	0	0	-667	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9
37	27	-0	1397	0	0	0	-571	--	--	16.08	16.08	0.18	0.01	0.01	0.09	0.00	0.00	20.9
38	27	-0	62	0	0	0	-770	--	--	16.08	16.08	0.18	0.01	0.00	0.00	0.00	0.00	20.9
39	27	-0	867	0	0	0	-626	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	587	0	0	0	-623	--	--	16.08	16.08	0.18	0.01	0.00	0.04	0.00	0.00	20.9
2	55	-0	497	0	0	0	-445	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
3	55	-0	542	0	0	0	-437	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
4	55	-0	361	0	0	0	-521	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
5	55	-0	407	0	0	0	-513	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
6	55	-0	397	0	0	0	-481	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
7	55	-0	548	0	0	0	-454	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
8	55	-0	356	0	0	0	-504	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
9	55	-0	507	0	0	0	-477	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
10	55	-0	497	0	0	0	-445	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
11	55	-0	542	0	0	0	-437	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
12	55	-0	361	0	0	0	-521	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
13	55	-0	407	0	0	0	-513	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
14	55	-0	397	0	0	0	-481	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
15	55	-0	548	0	0	0	-454	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
16	55	-0	356	0	0	0	-504	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
17	55	-0	507	0	0	0	-477	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
18	55	-0	1194	0	0	0	17	--	--	16.08	16.08	0.00	0.00	0.01	0.07	0.00	0.00	20.9
19	55	-0	392	0	0	0	-754	--	--	16.08	16.08	0.18	0.01	0.00	0.02	0.00	0.00	20.9
20	55	-0	875	0	0	0	-667	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9
37	55	-0	1397	0	0	0	191	--	--	16.08	16.08	0.00	0.00	0.01	0.09	0.00	0.00	20.9
38	55	-0	62	0	0	0	-770	--	--	16.08	16.08	0.18	0.01	0.00	0.00	0.00	0.00	20.9
39	55	-0	867	0	0	0	-626	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 17 NI 1759 NF 1758 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-57	0	0	0	-546	--	--	16.08	16.08	0.18	0.01	0.00	0.00	0.00	0.00	20.9
2	0	-0	-13	0	0	0	-371	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
3	0	-0	30	0	0	0	-364	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
4	0	-0	-118	0	0	0	-493	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
5	0	-0	-75	0	0	0	-469	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
6	0	-0	-101	0	0	0	-441	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
7	0	-0	44	0	0	0	-386	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
8	0	-0	-132	0	0	0	-478	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
9	0	-0	12	0	0	0	-406	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
10	0	-0	-13	0	0	0	-371	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
11	0	-0	30	0	0	0	-364	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
12	0	-0	-118	0	0	0	-493	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
13	0	-0	-75	0	0	0	-469	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
14	0	-0	-101	0	0	0	-441	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
15	0	-0	44	0	0	0	-386	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
16	0	-0	-132	0	0	0	-478	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
17	0	-0	12	0	0	0	-406	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
18	0	-0	188	0	0	0	-514	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9
19	0	-0	-260	0	0	0	-762	--	--	16.08	16.08	0.18	0.01	0.00	0.02	0.00	0.00	20.9
20	0	-0	71	0	0	0	-564	--	--	16.08	16.08	0.18	0.01	0.00	0.00	0.00	0.00	20.9
37	0	-0	332	0	0	0	-461	--	--	16.08	16.08	0.18	0.01	0.00	0.02	0.00	0.00	20.9
38	0	-0	-415	0	0	0	-865	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9
39	0	-0	138	0	0	0	-545	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-57	0	0	0	-546	--	--	16.08	16.08	0.18	0.01	0.00	0.00	0.00	0.00	20.9
2	27	-0	-13	0	0	0	-371	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
3	27	-0	30	0	0	0	-364	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
4	27	-0	-118	0	0	0	-493	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
5	27	-0	-75	0	0	0	-469	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
6	27	-0	-101	0	0	0	-441	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
7	27	-0	44	0	0	0	-386	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
8	27	-0	-132	0	0	0	-478	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
9	27	-0	12	0	0	0	-406	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
10	27	-0	-13	0	0	0	-371	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
11	27	-0	30	0	0	0	-364	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
12	27	-0	-118	0	0	0	-493	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
13	27	-0	-75	0	0	0	-469	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
14	27	-0	-101	0	0	0	-441	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
15	27	-0	44	0	0	0	-386	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
16	27	-0	-132	0	0	0	-478	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
17	27	-0	12	0	0	0	-406	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
18	27	-0	188	0	0	0	-514	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9
19	27	-0	-260	0	0	0	-762	--	--	16.08	16.08	0.18	0.01	0.00	0.02	0.00	0.00	20.9
20	27	-0	71	0	0	0	-564	--	--	16.08	16.08	0.18	0.01	0.00	0.00	0.00	0.00	20.9
37	27	-0	332	0	0	0	-461	--	--	16.08	16.08	0.18	0.01	0.00	0.02	0.00	0.00	20.9
38	27	-0	-415	0	0	0	-865	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9
39	27	-0	138	0	0	0	-545	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	-57	0	0	0	-546	--	--	16.08	16.08	0.18	0.01	0.00	0.00	0.00	0.00	20.9
2	55	-0	-13	0	0	0	-371	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
3	55	-0	30	0	0	0	-364	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
4	55	-0	-118	0	0	0	-493	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
5	55	-0	-75	0	0	0	-469	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
6	55	-0	-101	0	0	0	-441	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
7	55	-0	44	0	0	0	-386	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
8	55	-0	-132	0	0	0	-478	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
9	55	-0	12	0	0	0	-406	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
10	55	-0	-13	0	0	0	-371	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
11	55	-0	30	0	0	0	-364	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
12	55	-0	-118	0	0	0	-493	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
13	55	-0	-75	0	0	0	-469	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
14	55	-0	-101	0	0	0	-441	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
15	55	-0	44	0	0	0	-386	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
16	55	-0	-132	0	0	0	-478	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
17	55	-0	12	0	0	0	-406	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
18	55	-0	188	0	0	0	-514	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9
19	55	-0	-260	0	0	0	-762	--	--	16.08	16.08	0.18	0.01	0.00	0.02	0.00	0.00	20.9
20	55	-0	71	0	0	0	-564	--	--	16.08	16.08	0.18	0.01	0.00	0.00	0.00	0.00	20.9
37	55	-0	332	0	0	0	-461	--	--	16.08	16.08	0.18	0.01	0.00	0.02	0.00	0.00	20.9
38	55	-0	-415	0	0	0	-865	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9
39	55	-0	138	0	0	0	-545	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 18 NI 1750 NF 1759 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-714	0	0	0	-629	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
2	0	-0	-534	0	0	0	-446	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
3	0	-0	-492	0	0	0	-430	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
4	0	-0	-608	0	0	0	-538	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
5	0	-0	-565	0	0	0	-522	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
6	0	-0	-609	0	0	0	-496	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
7	0	-0	-468	0	0	0	-445	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
8	0	-0	-631	0	0	0	-523	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
9	0	-0	-490	0	0	0	-472	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
10	0	-0	-534	0	0	0	-446	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
11	0	-0	-492	0	0	0	-430	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
12	0	-0	-608	0	0	0	-538	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
13	0	-0	-565	0	0	0	-522	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
14	0	-0	-609	0	0	0	-496	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
15	0	-0	-468	0	0	0	-445	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
16	0	-0	-631	0	0	0	-523	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9

17	0	-0	-490	0	0	0	-472	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
18	0	-0	-843	0	0	0	-598	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9
19	0	-0	-934	0	0	0	-788	--	--	16.08	16.08	0.18	0.01	0.01	0.06	0.00	0.00	20.9
20	0	-0	-752	0	0	0	-649	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9
37	0	-0	-756	0	0	0	-513	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9
38	0	-0	-907	0	0	0	-831	--	--	16.08	16.08	0.18	0.01	0.01	0.06	0.00	0.00	20.9
39	0	-0	-605	0	0	0	-598	--	--	16.08	16.08	0.18	0.01	0.00	0.04	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-714	0	0	0	-629	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
2	27	-0	-534	0	0	0	-446	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
3	27	-0	-492	0	0	0	-430	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
4	27	-0	-608	0	0	0	-538	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
5	27	-0	-565	0	0	0	-522	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
6	27	-0	-609	0	0	0	-496	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
7	27	-0	-468	0	0	0	-445	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
8	27	-0	-631	0	0	0	-523	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
9	27	-0	-490	0	0	0	-472	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
10	27	-0	-534	0	0	0	-446	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
11	27	-0	-492	0	0	0	-430	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
12	27	-0	-608	0	0	0	-538	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
13	27	-0	-565	0	0	0	-522	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
14	27	-0	-609	0	0	0	-496	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
15	27	-0	-468	0	0	0	-445	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
16	27	-0	-631	0	0	0	-523	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
17	27	-0	-490	0	0	0	-472	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
18	27	-0	-843	0	0	0	-598	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9
19	27	-0	-934	0	0	0	-788	--	--	16.08	16.08	0.18	0.01	0.01	0.06	0.00	0.00	20.9
20	27	-0	-752	0	0	0	-649	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9
37	27	-0	-756	0	0	0	-513	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9
38	27	-0	-907	0	0	0	-831	--	--	16.08	16.08	0.18	0.01	0.01	0.06	0.00	0.00	20.9
39	27	-0	-605	0	0	0	-598	--	--	16.08	16.08	0.18	0.01	0.00	0.04	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	-714	0	0	0	-629	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
2	55	-0	-534	0	0	0	-446	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
3	55	-0	-492	0	0	0	-430	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
4	55	-0	-608	0	0	0	-538	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
5	55	-0	-565	0	0	0	-522	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
6	55	-0	-609	0	0	0	-496	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
7	55	-0	-468	0	0	0	-445	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
8	55	-0	-631	0	0	0	-523	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
9	55	-0	-490	0	0	0	-472	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
10	55	-0	-534	0	0	0	-446	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
11	55	-0	-492	0	0	0	-430	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
12	55	-0	-608	0	0	0	-538	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
13	55	-0	-565	0	0	0	-522	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
14	55	-0	-609	0	0	0	-496	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
15	55	-0	-468	0	0	0	-445	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
16	55	-0	-631	0	0	0	-523	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
17	55	-0	-490	0	0	0	-472	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
18	55	-0	-843	0	0	0	-598	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9
19	55	-0	-934	0	0	0	-788	--	--	16.08	16.08	0.18	0.01	0.01	0.06	0.00	0.00	20.9
20	55	-0	-752	0	0	0	-649	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9
37	55	-0	-756	0	0	0	-513	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9
38	55	-0	-907	0	0	0	-831	--	--	16.08	16.08	0.18	0.01	0.01	0.06	0.00	0.00	20.9
39	55	-0	-605	0	0	0	-598	--	--	16.08	16.08	0.18	0.01	0.00	0.04	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 19 NI 1751 NF 1750 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-1535	0	0	0	293	--	--	16.08	16.08	0.00	0.00	0.01	0.10	0.00	0.00	20.9
2	0	-0	-1166	0	0	0	243	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
3	0	-0	-1125	0	0	0	228	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
4	0	-0	-1236	0	0	0	222	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
5	0	-0	-1196	0	0	0	207	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
6	0	-0	-1238	0	0	0	253	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
7	0	-0	-1102	0	0	0	204	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
8	0	-0	-1259	0	0	0	247	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
9	0	-0	-1123	0	0	0	197	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
10	0	-0	-1166	0	0	0	243	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
11	0	-0	-1125	0	0	0	228	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
12	0	-0	-1236	0	0	0	222	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
13	0	-0	-1196	0	0	0	207	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
14	0	-0	-1238	0	0	0	253	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
15	0	-0	-1102	0	0	0	204	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
16	0	-0	-1259	0	0	0	247	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
17	0	-0	-1123	0	0	0	197	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
18	0	-0	-2104	0	0	0	617	--	--	16.08	16.08	0.00	0.01	0.02	0.13	0.00	0.00	20.9
19	0	-0	-1910	0	0	0	438	--	--	16.08	16.08	0.00	0.01	0.02	0.12	0.00	0.00	20.9
20	0	-0	-1828	0	0	0	448	--	--	16.08	16.08	0.00	0.01	0.02	0.11	0.00	0.00	20.9
37	0	-0	-2017	0	0	0	602	--	--	16.08	16.08	0.00	0.01	0.02	0.13	0.00	0.00	20.9
38	0	-0	-1693	0	0	0	304	--	--	16.08	16.08	0.00	0.01	0.01	0.11	0.00	0.00	20.9
39	0	-0	-1557	0	0	0	319	--	--	16.08	16.08	0.00	0.01	0.01	0.10	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-1535	0	0	0	-544	--	--	16.08	16.08	0.18	0.01	0.01	0.10	0.00	0.00	20.9
2	27	-0	-1166	0	0	0	-393	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
3	27	-0	-1125	0	0	0	-385	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
4	27	-0	-1236	0	0	0	-452	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
5	27	-0	-1196	0	0	0	-445	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
6	27	-0	-1238	0	0	0	-422	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
7	27	-0	-1102	0	0	0	-398	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
8	27	-0	-1259	0	0	0	-440	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
9	27	-0	-1123	0	0	0	-415	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
10	27	-0	-1166	0	0	0	-393	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
11	27	-0	-1125	0	0	0	-385	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
12	27	-0	-1236	0	0	0	-452	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9

13	27	-0	-1196	0	0	0	-445	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
14	27	-0	-1238	0	0	0	-422	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
15	27	-0	-1102	0	0	0	-398	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
16	27	-0	-1259	0	0	0	-440	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
17	27	-0	-1123	0	0	0	-415	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
18	27	-0	-2104	0	0	0	617	--	--	16.08	16.08	0.00	0.01	0.02	0.13	0.00	0.00	20.9
19	27	-0	-1910	0	0	0	-603	--	--	16.08	16.08	0.18	0.01	0.02	0.12	0.00	0.00	20.9
20	27	-0	-1828	0	0	0	-549	--	--	16.08	16.08	0.18	0.01	0.02	0.11	0.00	0.00	20.9
37	27	-0	-2017	0	0	0	602	--	--	16.08	16.08	0.00	0.01	0.02	0.13	0.00	0.00	20.9
38	27	-0	-1693	0	0	0	-620	--	--	16.08	16.08	0.18	0.01	0.01	0.11	0.00	0.00	20.9
39	27	-0	-1557	0	0	0	-530	--	--	16.08	16.08	0.18	0.01	0.01	0.10	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	-1535	0	0	0	-544	--	--	16.08	16.08	0.18	0.01	0.01	0.10	0.00	0.00	20.9
2	55	-0	-1166	0	0	0	-393	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
3	55	-0	-1125	0	0	0	-385	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
4	55	-0	-1236	0	0	0	-452	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
5	55	-0	-1196	0	0	0	-445	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
6	55	-0	-1238	0	0	0	-422	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
7	55	-0	-1102	0	0	0	-398	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
8	55	-0	-1259	0	0	0	-440	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
9	55	-0	-1123	0	0	0	-415	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
10	55	-0	-1166	0	0	0	-393	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
11	55	-0	-1125	0	0	0	-385	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
12	55	-0	-1236	0	0	0	-452	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
13	55	-0	-1196	0	0	0	-445	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
14	55	-0	-1238	0	0	0	-422	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
15	55	-0	-1102	0	0	0	-398	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
16	55	-0	-1259	0	0	0	-440	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
17	55	-0	-1123	0	0	0	-415	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
18	55	-0	-2104	0	0	0	-530	--	--	16.08	16.08	0.18	0.01	0.02	0.13	0.00	0.00	20.9
19	55	-0	-1910	0	0	0	-603	--	--	16.08	16.08	0.18	0.01	0.02	0.12	0.00	0.00	20.9
20	55	-0	-1828	0	0	0	-549	--	--	16.08	16.08	0.18	0.01	0.02	0.11	0.00	0.00	20.9
37	55	-0	-2017	0	0	0	-498	--	--	16.08	16.08	0.18	0.01	0.02	0.13	0.00	0.00	20.9
38	55	-0	-1693	0	0	0	-620	--	--	16.08	16.08	0.18	0.01	0.01	0.11	0.00	0.00	20.9
39	55	-0	-1557	0	0	0	-530	--	--	16.08	16.08	0.18	0.01	0.01	0.10	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 20 NI 1752 NF 1751 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-2692	0	0	0	1256	--	--	16.08	16.08	0.00	0.02	0.02	0.17	0.00	0.00	20.9
2	0	-0	-2020	0	0	0	943	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
3	0	-0	-1989	0	0	0	927	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
4	0	-0	-2153	0	0	0	1004	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
5	0	-0	-2122	0	0	0	989	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
6	0	-0	-2103	0	0	0	982	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
7	0	-0	-1999	0	0	0	931	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
8	0	-0	-2143	0	0	0	1000	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
9	0	-0	-2039	0	0	0	950	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
10	0	-0	-2020	0	0	0	943	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
11	0	-0	-1989	0	0	0	927	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
12	0	-0	-2153	0	0	0	1004	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
13	0	-0	-2122	0	0	0	989	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
14	0	-0	-2103	0	0	0	982	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
15	0	-0	-1999	0	0	0	931	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
16	0	-0	-2143	0	0	0	1000	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
17	0	-0	-2039	0	0	0	950	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
18	0	-0	-3837	0	0	0	1995	--	--	16.08	16.08	0.00	0.03	0.03	0.24	0.00	0.00	20.9
19	0	-0	-3527	0	0	0	1862	--	--	16.08	16.08	0.00	0.03	0.03	0.22	0.00	0.00	20.9
20	0	-0	-3449	0	0	0	1781	--	--	16.08	16.08	0.00	0.03	0.03	0.22	0.00	0.00	20.9
37	0	-0	-3622	0	0	0	1823	--	--	16.08	16.08	0.00	0.03	0.03	0.23	0.00	0.00	20.9
38	0	-0	-3106	0	0	0	1601	--	--	16.08	16.08	0.00	0.03	0.03	0.19	0.00	0.00	20.9
39	0	-0	-2976	0	0	0	1467	--	--	16.08	16.08	0.00	0.03	0.02	0.19	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-2692	0	0	0	1256	--	--	16.08	16.08	0.00	0.02	0.02	0.17	0.00	0.00	20.9
2	27	-0	-2020	0	0	0	943	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
3	27	-0	-1989	0	0	0	927	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
4	27	-0	-2153	0	0	0	1004	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
5	27	-0	-2122	0	0	0	989	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
6	27	-0	-2103	0	0	0	982	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
7	27	-0	-1999	0	0	0	931	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
8	27	-0	-2143	0	0	0	1000	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
9	27	-0	-2039	0	0	0	950	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
10	27	-0	-2020	0	0	0	943	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
11	27	-0	-1989	0	0	0	927	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
12	27	-0	-2153	0	0	0	1004	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
13	27	-0	-2122	0	0	0	989	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
14	27	-0	-2103	0	0	0	982	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
15	27	-0	-1999	0	0	0	931	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
16	27	-0	-2143	0	0	0	1000	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
17	27	-0	-2039	0	0	0	950	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
18	27	-0	-3837	0	0	0	1995	--	--	16.08	16.08	0.00	0.03	0.03	0.24	0.00	0.00	20.9
19	27	-0	-3527	0	0	0	1862	--	--	16.08	16.08	0.00	0.03	0.03	0.22	0.00	0.00	20.9
20	27	-0	-3449	0	0	0	1781	--	--	16.08	16.08	0.00	0.03	0.03	0.22	0.00	0.00	20.9
37	27	-0	-3622	0	0	0	1823	--	--	16.08	16.08	0.00	0.03	0.03	0.23	0.00	0.00	20.9
38	27	-0	-3106	0	0	0	1601	--	--	16.08	16.08	0.00	0.03	0.03	0.19	0.00	0.00	20.9
39	27	-0	-2976	0	0	0	1467	--	--	16.08	16.08	0.00	0.03	0.02	0.19	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	-2692	0	0	0	-213	--	--	16.08	16.08	0.18	0.00	0.02	0.17	0.00	0.00	20.9
2	55	-0	-2020	0	0	0	-159	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
3	55	-0	-1989	0	0	0	-158	--	--	16.08	16.08	0.29	0.00	0.02	0.12	0.00	0.00	20.9
4	55	-0	-2153	0	0	0	-170	--	--	16.08	16.08	0.29	0.00	0.02	0.14	0.00	0.00	20.9
5	55	-0	-2122	0	0	0	-168	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
6	55	-0	-2103	0	0	0	-165	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
7	55	-0	-1999	0	0	0	-159	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
8	55	-0	-2143	0	0	0	-168	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9

9	55	-0	-2039	0	0	0	-162	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
10	55	-0	-2020	0	0	0	-159	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
11	55	-0	-1989	0	0	0	-158	--	--	16.08	16.08	0.29	0.00	0.02	0.12	0.00	0.00	20.9
12	55	-0	-2153	0	0	0	-170	--	--	16.08	16.08	0.29	0.00	0.02	0.14	0.00	0.00	20.9
13	55	-0	-2122	0	0	0	-168	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
14	55	-0	-2103	0	0	0	-165	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
15	55	-0	-1999	0	0	0	-159	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
16	55	-0	-2143	0	0	0	-168	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
17	55	-0	-2039	0	0	0	-162	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
18	55	-0	-3837	0	0	0	-98	--	--	16.08	16.08	0.18	0.00	0.03	0.24	0.00	0.00	20.9
19	55	-0	-3527	0	0	0	-63	--	--	16.08	16.08	0.18	0.00	0.03	0.22	0.00	0.00	20.9
20	55	-0	-3449	0	0	0	-100	--	--	16.08	16.08	0.18	0.00	0.03	0.22	0.00	0.00	20.9
37	55	-0	-3622	0	0	0	-152	--	--	16.08	16.08	0.18	0.00	0.03	0.23	0.00	0.00	20.9
38	55	-0	-3106	0	0	0	-94	--	--	16.08	16.08	0.18	0.00	0.03	0.19	0.00	0.00	20.9
39	55	-0	-2976	0	0	0	-156	--	--	16.08	16.08	0.18	0.00	0.02	0.19	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 21 NI 1743 NF 1752 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-2385	0	0	0	1455	--	--	16.08	16.08	0.00	0.02	0.02	0.15	0.00	0.00	20.9
2	0	-0	-1884	0	0	0	1147	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
3	0	-0	-1890	0	0	0	1152	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
4	0	-0	-1779	0	0	0	1087	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
5	0	-0	-1785	0	0	0	1092	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
6	0	-0	-1841	0	0	0	1119	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
7	0	-0	-1860	0	0	0	1137	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
8	0	-0	-1809	0	0	0	1102	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
9	0	-0	-1829	0	0	0	1119	--	--	16.08	16.08	0.10	0.02	0.02	0.11	0.00	0.00	20.9
10	0	-0	-1884	0	0	0	1147	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
11	0	-0	-1890	0	0	0	1152	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
12	0	-0	-1779	0	0	0	1087	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
13	0	-0	-1785	0	0	0	1092	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
14	0	-0	-1841	0	0	0	1119	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
15	0	-0	-1860	0	0	0	1137	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
16	0	-0	-1809	0	0	0	1102	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
17	0	-0	-1829	0	0	0	1119	--	--	16.08	16.08	0.10	0.02	0.02	0.11	0.00	0.00	20.9
18	0	-0	-3524	0	0	0	2328	--	--	16.08	16.08	0.00	0.04	0.03	0.22	0.00	0.00	20.9
19	0	-0	-2260	0	0	0	1606	--	--	16.08	16.08	0.00	0.03	0.02	0.14	0.00	0.00	20.9
20	0	-0	-2834	0	0	0	1901	--	--	16.08	16.08	0.00	0.03	0.02	0.18	0.00	0.00	20.9
37	0	-0	-3785	0	0	0	2406	--	--	16.08	16.08	0.00	0.04	0.03	0.24	0.00	0.00	20.9
38	0	-0	-1679	0	0	0	1203	--	--	16.08	16.08	0.00	0.02	0.01	0.11	0.00	0.00	20.9
39	0	-0	-2636	0	0	0	1695	--	--	16.08	16.08	0.00	0.03	0.02	0.17	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-2385	0	0	0	1455	--	--	16.08	16.08	0.00	0.02	0.02	0.15	0.00	0.00	20.9
2	27	-0	-1884	0	0	0	1147	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
3	27	-0	-1890	0	0	0	1152	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
4	27	-0	-1779	0	0	0	1087	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
5	27	-0	-1785	0	0	0	1092	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
6	27	-0	-1841	0	0	0	1119	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
7	27	-0	-1860	0	0	0	1137	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
8	27	-0	-1809	0	0	0	1102	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
9	27	-0	-1829	0	0	0	1119	--	--	16.08	16.08	0.10	0.02	0.02	0.11	0.00	0.00	20.9
10	27	-0	-1884	0	0	0	1147	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
11	27	-0	-1890	0	0	0	1152	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
12	27	-0	-1779	0	0	0	1087	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
13	27	-0	-1785	0	0	0	1092	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
14	27	-0	-1841	0	0	0	1119	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
15	27	-0	-1860	0	0	0	1137	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
16	27	-0	-1809	0	0	0	1102	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
17	27	-0	-1829	0	0	0	1119	--	--	16.08	16.08	0.10	0.02	0.02	0.11	0.00	0.00	20.9
18	27	-0	-3524	0	0	0	2328	--	--	16.08	16.08	0.00	0.04	0.03	0.22	0.00	0.00	20.9
19	27	-0	-2260	0	0	0	1606	--	--	16.08	16.08	0.00	0.03	0.02	0.14	0.00	0.00	20.9
20	27	-0	-2834	0	0	0	1901	--	--	16.08	16.08	0.00	0.03	0.02	0.18	0.00	0.00	20.9
37	27	-0	-3785	0	0	0	2406	--	--	16.08	16.08	0.00	0.04	0.03	0.24	0.00	0.00	20.9
38	27	-0	-1679	0	0	0	1203	--	--	16.08	16.08	0.00	0.02	0.01	0.11	0.00	0.00	20.9
39	27	-0	-2636	0	0	0	1695	--	--	16.08	16.08	0.00	0.03	0.02	0.17	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	-2385	0	0	0	154	--	--	16.08	16.08	0.00	0.00	0.02	0.15	0.00	0.00	20.9
2	55	-0	-1884	0	0	0	119	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
3	55	-0	-1890	0	0	0	121	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
4	55	-0	-1779	0	0	0	117	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
5	55	-0	-1785	0	0	0	119	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
6	55	-0	-1841	0	0	0	116	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
7	55	-0	-1860	0	0	0	122	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
8	55	-0	-1809	0	0	0	115	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
9	55	-0	-1829	0	0	0	122	--	--	16.08	16.08	0.10	0.00	0.02	0.11	0.00	0.00	20.9
10	55	-0	-1884	0	0	0	119	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
11	55	-0	-1890	0	0	0	121	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
12	55	-0	-1779	0	0	0	117	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
13	55	-0	-1785	0	0	0	119	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
14	55	-0	-1841	0	0	0	116	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
15	55	-0	-1860	0	0	0	122	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
16	55	-0	-1809	0	0	0	115	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
17	55	-0	-1829	0	0	0	122	--	--	16.08	16.08	0.10	0.00	0.02	0.11	0.00	0.00	20.9
18	55	-0	-3524	0	0	0	406	--	--	16.08	16.08	0.00	0.01	0.03	0.22	0.00	0.00	20.9
19	55	-0	-2260	0	0	0	373	--	--	16.08	16.08	0.00	0.01	0.02	0.14	0.00	0.00	20.9
20	55	-0	-2834	0	0	0	356	--	--	16.08	16.08	0.00	0.01	0.02	0.18	0.00	0.00	20.9
37	55	-0	-3785	0	0	0	341	--	--	16.08	16.08	0.00	0.01	0.03	0.24	0.00	0.00	20.9
38	55	-0	-1679	0	0	0	287	--	--	16.08	16.08	0.00	0.00	0.01	0.11	0.00	0.00	20.9
39	55	-0	-2636	0	0	0	257	--	--	16.08	16.08	0.00	0.00	0.02	0.17	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 22 NI 1602 NF 1743 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle V,Mx	cmq/m		cm
1	0	-0	3277	0	0	0	-1152	--	--	16.08	16.08	0.18	0.02	0.03 0.21	0.00	0.00	20.9
2	0	-0	1774	0	0	0	-464	--	--	16.08	16.08	0.29	0.01	0.01 0.11	0.00	0.00	20.9
3	0	-0	1742	0	0	0	-454	--	--	16.08	16.08	0.29	0.01	0.01 0.11	0.00	0.00	20.9
4	0	-0	3299	0	0	0	-1319	--	--	16.08	16.08	0.29	0.02	0.03 0.21	0.00	0.00	20.9
5	0	-0	3267	0	0	0	-1309	--	--	16.08	16.08	0.29	0.02	0.03 0.20	0.00	0.00	20.9
6	0	-0	2344	0	0	0	-775	--	--	16.08	16.08	0.29	0.01	0.02 0.15	0.00	0.00	20.9
7	0	-0	2239	0	0	0	-742	--	--	16.08	16.08	0.29	0.01	0.02 0.14	0.00	0.00	20.9
8	0	-0	2802	0	0	0	-1031	--	--	16.08	16.08	0.29	0.02	0.02 0.18	0.00	0.00	20.9
9	0	-0	2697	0	0	0	-998	--	--	16.08	16.08	0.29	0.02	0.02 0.17	0.00	0.00	20.9
10	0	-0	1774	0	0	0	-464	--	--	16.08	16.08	0.29	0.01	0.01 0.11	0.00	0.00	20.9
11	0	-0	1742	0	0	0	-454	--	--	16.08	16.08	0.29	0.01	0.01 0.11	0.00	0.00	20.9
12	0	-0	3299	0	0	0	-1319	--	--	16.08	16.08	0.29	0.02	0.03 0.21	0.00	0.00	20.9
13	0	-0	3267	0	0	0	-1309	--	--	16.08	16.08	0.29	0.02	0.03 0.20	0.00	0.00	20.9
14	0	-0	2344	0	0	0	-775	--	--	16.08	16.08	0.29	0.01	0.02 0.15	0.00	0.00	20.9
15	0	-0	2239	0	0	0	-742	--	--	16.08	16.08	0.29	0.01	0.02 0.14	0.00	0.00	20.9
16	0	-0	2802	0	0	0	-1031	--	--	16.08	16.08	0.29	0.02	0.02 0.18	0.00	0.00	20.9
17	0	-0	2697	0	0	0	-998	--	--	16.08	16.08	0.29	0.02	0.02 0.17	0.00	0.00	20.9
18	0	-0	4098	0	0	0	-1094	--	--	16.08	16.08	0.18	0.02	0.03 0.26	0.00	0.00	20.9
19	0	-0	9915	0	0	0	-4584	--	--	16.08	16.08	0.18	0.08	0.08 0.62	0.00	0.00	20.9
20	0	-0	6351	0	0	0	-2558	--	--	16.08	16.08	0.18	0.04	0.05 0.40	0.00	0.00	20.9
37	0	-0	943	0	0	0	622	--	--	16.08	16.08	0.00	0.01	0.01 0.06	0.00	0.00	20.9
38	0	-0	10640	0	0	0	-5195	--	--	16.08	16.08	0.18	0.09	0.09 0.67	0.00	0.00	20.9
39	0	-0	4697	0	0	0	-1818	--	--	16.08	16.08	0.18	0.03	0.04 0.29	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	3277	0	0	0	-1152	--	--	16.08	16.08	0.18	0.02	0.03 0.21	0.00	0.00	20.9
2	27	-0	1774	0	0	0	1916	--	--	16.08	16.08	0.10	0.03	0.01 0.11	0.00	0.00	20.9
3	27	-0	1742	0	0	0	1883	--	--	16.08	16.08	0.10	0.03	0.01 0.11	0.00	0.00	20.9
4	27	-0	3299	0	0	0	-1319	--	--	16.08	16.08	0.29	0.02	0.03 0.21	0.00	0.00	20.9
5	27	-0	3267	0	0	0	-1309	--	--	16.08	16.08	0.29	0.02	0.03 0.20	0.00	0.00	20.9
6	27	-0	2344	0	0	0	-775	--	--	16.08	16.08	0.29	0.01	0.02 0.15	0.00	0.00	20.9
7	27	-0	2239	0	0	0	-742	--	--	16.08	16.08	0.29	0.01	0.02 0.14	0.00	0.00	20.9
8	27	-0	2802	0	0	0	-1031	--	--	16.08	16.08	0.29	0.02	0.02 0.18	0.00	0.00	20.9
9	27	-0	2697	0	0	0	-998	--	--	16.08	16.08	0.29	0.02	0.02 0.17	0.00	0.00	20.9
10	27	-0	1774	0	0	0	1916	--	--	16.08	16.08	0.10	0.03	0.01 0.11	0.00	0.00	20.9
11	27	-0	1742	0	0	0	1883	--	--	16.08	16.08	0.10	0.03	0.01 0.11	0.00	0.00	20.9
12	27	-0	3299	0	0	0	-1319	--	--	16.08	16.08	0.29	0.02	0.03 0.21	0.00	0.00	20.9
13	27	-0	3267	0	0	0	-1309	--	--	16.08	16.08	0.29	0.02	0.03 0.20	0.00	0.00	20.9
14	27	-0	2344	0	0	0	-775	--	--	16.08	16.08	0.29	0.01	0.02 0.15	0.00	0.00	20.9
15	27	-0	2239	0	0	0	-742	--	--	16.08	16.08	0.29	0.01	0.02 0.14	0.00	0.00	20.9
16	27	-0	2802	0	0	0	-1031	--	--	16.08	16.08	0.29	0.02	0.02 0.18	0.00	0.00	20.9
17	27	-0	2697	0	0	0	-998	--	--	16.08	16.08	0.29	0.02	0.02 0.17	0.00	0.00	20.9
18	27	-0	4098	0	0	0	4404	--	--	16.08	16.08	0.00	0.08	0.03 0.26	0.00	0.00	20.9
19	27	-0	9915	0	0	0	-4584	--	--	16.08	16.08	0.18	0.08	0.08 0.62	0.00	0.00	20.9
20	27	-0	6351	0	0	0	-2558	--	--	16.08	16.08	0.18	0.04	0.05 0.40	0.00	0.00	20.9
37	27	-0	943	0	0	0	1886	--	--	16.08	16.08	0.00	0.03	0.01 0.06	0.00	0.00	20.9
38	27	-0	10640	0	0	0	-5195	--	--	16.08	16.08	0.18	0.09	0.09 0.67	0.00	0.00	20.9
39	27	-0	4697	0	0	0	-1818	--	--	16.08	16.08	0.18	0.03	0.04 0.29	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	3277	0	0	0	635	--	--	16.08	16.08	0.00	0.01	0.03 0.21	0.00	0.00	20.9
2	55	-0	1774	0	0	0	504	--	--	16.08	16.08	0.10	0.01	0.01 0.11	0.00	0.00	20.9
3	55	-0	1742	0	0	0	497	--	--	16.08	16.08	0.10	0.01	0.01 0.11	0.00	0.00	20.9
4	55	-0	3299	0	0	0	480	--	--	16.08	16.08	0.10	0.01	0.03 0.21	0.00	0.00	20.9
5	55	-0	3267	0	0	0	473	--	--	16.08	16.08	0.10	0.01	0.03 0.20	0.00	0.00	20.9
6	55	-0	2344	0	0	0	504	--	--	16.08	16.08	0.10	0.01	0.02 0.15	0.00	0.00	20.9
7	55	-0	2239	0	0	0	480	--	--	16.08	16.08	0.10	0.01	0.02 0.14	0.00	0.00	20.9
8	55	-0	2802	0	0	0	497	--	--	16.08	16.08	0.10	0.01	0.02 0.18	0.00	0.00	20.9
9	55	-0	2697	0	0	0	473	--	--	16.08	16.08	0.10	0.01	0.02 0.17	0.00	0.00	20.9
10	55	-0	1774	0	0	0	504	--	--	16.08	16.08	0.10	0.01	0.01 0.11	0.00	0.00	20.9
11	55	-0	1742	0	0	0	497	--	--	16.08	16.08	0.10	0.01	0.01 0.11	0.00	0.00	20.9
12	55	-0	3299	0	0	0	480	--	--	16.08	16.08	0.10	0.01	0.03 0.21	0.00	0.00	20.9
13	55	-0	3267	0	0	0	473	--	--	16.08	16.08	0.10	0.01	0.03 0.20	0.00	0.00	20.9
14	55	-0	2344	0	0	0	504	--	--	16.08	16.08	0.10	0.01	0.02 0.15	0.00	0.00	20.9
15	55	-0	2239	0	0	0	480	--	--	16.08	16.08	0.10	0.01	0.02 0.14	0.00	0.00	20.9
16	55	-0	2802	0	0	0	497	--	--	16.08	16.08	0.10	0.01	0.02 0.18	0.00	0.00	20.9
17	55	-0	2697	0	0	0	473	--	--	16.08	16.08	0.10	0.01	0.02 0.17	0.00	0.00	20.9
18	55	-0	4098	0	0	0	1142	--	--	16.08	16.08	0.00	0.02	0.03 0.26	0.00	0.00	20.9
19	55	-0	9915	0	0	0	825	--	--	16.08	16.08	0.00	0.01	0.08 0.62	0.00	0.00	20.9
20	55	-0	6351	0	0	0	907	--	--	16.08	16.08	0.00	0.02	0.05 0.40	0.00	0.00	20.9
37	55	-0	943	0	0	0	1136	--	--	16.08	16.08	0.00	0.02	0.01 0.06	0.00	0.00	20.9
38	55	-0	10640	0	0	0	608	--	--	16.08	16.08	0.00	0.01	0.09 0.67	0.00	0.00	20.9
39	55	-0	4697	0	0	0	744	--	--	16.08	16.08	0.00	0.01	0.04 0.29	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 23 NI 1740 NF 1602 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle V,Mx	cmq/m		cm
1	0	-0	-2925	0	0	0	655	--	--	16.08	16.08	0.00	0.01	0.02 0.18	0.00	0.00	20.9
2	0	-0	-1425	0	0	0	475	--	--	16.08	16.08	0.10	0.01	0.01 0.09	0.00	0.00	20.9
3	0	-0	-1469	0	0	0	484	--	--	16.08	16.08	0.10	0.01	0.01 0.09	0.00	0.00	20.9
4	0	-0	-3030	0	0	0	523	--	--	16.08	16.08	0.10	0.01	0.02 0.19	0.00	0.00	20.9
5	0	-0	-3074	0	0	0	533	--	--	16.08	16.08	0.10	0.01	0.03 0.19	0.00	0.00	20.9
6	0	-0	-1936	0	0	0	481	--	--	16.08	16.08	0.10	0.01	0.02 0.12	0.00	0.00	20.9
7	0	-0	-2082	0	0	0	512	--	--	16.08	16.08	0.10	0.01	0.02 0.13	0.00	0.00	20.9
8	0	-0	-2418	0	0	0	495	--	--	16.08	16.08	0.10	0.01	0.02 0.15	0.00	0.00	20.9
9	0	-0	-2563	0	0	0	527	--	--	16.08	16.08	0.10	0.01	0.02 0.16	0.00	0.00	20.9
10	0	-0	-1425	0	0	0	475	--	--	16.08	16.08	0.10	0.01	0.01 0.09	0.00	0.00	20.9
11	0	-0	-1469	0	0	0	484	--	--	16.08	16.08	0.10	0.01	0.01 0.09	0.00	0.00	20.9
12	0	-0	-3030	0	0	0	523	--	--	16.08	16.08	0.10	0.01	0.02 0.19	0.00	0.00	20.9
13	0	-0	-3074	0	0	0	533	--	--	16.08	16.08	0.10	0.01	0.03 0.19	0.00	0.00	20.9
14	0	-0	-1936	0	0	0	481	--	--	16.08	16.08	0.10	0.01	0.02 0.12	0.00	0.00	20.9
15	0	-0	-2082	0	0	0	512	--	--	16.08	16.08	0.10	0.01	0.02 0.13	0.00	0.00	20.9
16	0	-0	-2418	0	0	0	495	--	--	16.08	16.08	0.10	0.01	0.02 0.15	0.00	0.00	20.9

17	0	-0	-2563	0	0	0	527	--	--	16.08	16.08	0.10	0.01	0.02	0.16	0.00	0.00	20.9
18	0	-0	-3156	0	0	0	1021	--	--	16.08	16.08	0.00	0.02	0.03	0.20	0.00	0.00	20.9
19	0	-0	-9439	0	0	0	1018	--	--	16.08	16.08	0.00	0.02	0.08	0.59	0.00	0.00	20.9
20	0	-0	-5922	0	0	0	995	--	--	16.08	16.08	0.00	0.02	0.05	0.37	0.00	0.00	20.9
37	0	-0	40	0	0	0	904	--	--	16.08	16.08	0.00	0.02	0.00	0.00	0.00	0.00	20.9
38	0	-0	-10430	0	0	0	900	--	--	16.08	16.08	0.00	0.02	0.09	0.65	0.00	0.00	20.9
39	0	-0	-4569	0	0	0	862	--	--	16.08	16.08	0.00	0.01	0.04	0.29	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-2925	0	0	0	-940	--	--	16.08	16.08	0.18	0.02	0.02	0.18	0.00	0.00	20.9
2	27	-0	-1425	0	0	0	475	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
3	27	-0	-1469	0	0	0	484	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
4	27	-0	-3030	0	0	0	-1130	--	--	16.08	16.08	0.29	0.02	0.02	0.19	0.00	0.00	20.9
5	27	-0	-3074	0	0	0	-1144	--	--	16.08	16.08	0.29	0.02	0.03	0.19	0.00	0.00	20.9
6	27	-0	-1936	0	0	0	-575	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
7	27	-0	-2082	0	0	0	-623	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
8	27	-0	-2418	0	0	0	-823	--	--	16.08	16.08	0.29	0.01	0.02	0.15	0.00	0.00	20.9
9	27	-0	-2563	0	0	0	-872	--	--	16.08	16.08	0.29	0.02	0.02	0.16	0.00	0.00	20.9
10	27	-0	-1425	0	0	0	475	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
11	27	-0	-1469	0	0	0	484	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
12	27	-0	-3030	0	0	0	-1130	--	--	16.08	16.08	0.29	0.02	0.02	0.19	0.00	0.00	20.9
13	27	-0	-3074	0	0	0	-1144	--	--	16.08	16.08	0.29	0.02	0.03	0.19	0.00	0.00	20.9
14	27	-0	-1936	0	0	0	-575	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
15	27	-0	-2082	0	0	0	-623	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
16	27	-0	-2418	0	0	0	-823	--	--	16.08	16.08	0.29	0.01	0.02	0.15	0.00	0.00	20.9
17	27	-0	-2563	0	0	0	-872	--	--	16.08	16.08	0.29	0.02	0.02	0.16	0.00	0.00	20.9
18	27	-0	-3156	0	0	0	1021	--	--	16.08	16.08	0.00	0.02	0.03	0.20	0.00	0.00	20.9
19	27	-0	-9439	0	0	0	-4131	--	--	16.08	16.08	0.18	0.07	0.08	0.59	0.00	0.00	20.9
20	27	-0	-5922	0	0	0	-2235	--	--	16.08	16.08	0.18	0.04	0.05	0.37	0.00	0.00	20.9
37	27	-0	40	0	0	0	958	--	--	16.08	16.08	0.00	0.02	0.00	0.00	0.00	0.00	20.9
38	27	-0	-10430	0	0	0	-4790	--	--	16.08	16.08	0.18	0.08	0.09	0.65	0.00	0.00	20.9
39	27	-0	-4569	0	0	0	-1631	--	--	16.08	16.08	0.18	0.03	0.04	0.29	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	-2925	0	0	0	-940	--	--	16.08	16.08	0.18	0.02	0.02	0.18	0.00	0.00	20.9
2	55	-0	-1425	0	0	0	-302	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
3	55	-0	-1469	0	0	0	-317	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
4	55	-0	-3030	0	0	0	-1130	--	--	16.08	16.08	0.29	0.02	0.02	0.19	0.00	0.00	20.9
5	55	-0	-3074	0	0	0	-1144	--	--	16.08	16.08	0.29	0.02	0.03	0.19	0.00	0.00	20.9
6	55	-0	-1936	0	0	0	-575	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
7	55	-0	-2082	0	0	0	-623	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
8	55	-0	-2418	0	0	0	-823	--	--	16.08	16.08	0.29	0.01	0.02	0.15	0.00	0.00	20.9
9	55	-0	-2563	0	0	0	-872	--	--	16.08	16.08	0.29	0.02	0.02	0.16	0.00	0.00	20.9
10	55	-0	-1425	0	0	0	-302	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
11	55	-0	-1469	0	0	0	-317	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
12	55	-0	-3030	0	0	0	-1130	--	--	16.08	16.08	0.29	0.02	0.02	0.19	0.00	0.00	20.9
13	55	-0	-3074	0	0	0	-1144	--	--	16.08	16.08	0.29	0.02	0.03	0.19	0.00	0.00	20.9
14	55	-0	-1936	0	0	0	-575	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
15	55	-0	-2082	0	0	0	-623	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
16	55	-0	-2418	0	0	0	-823	--	--	16.08	16.08	0.29	0.01	0.02	0.15	0.00	0.00	20.9
17	55	-0	-2563	0	0	0	-872	--	--	16.08	16.08	0.29	0.02	0.02	0.16	0.00	0.00	20.9
18	55	-0	-3156	0	0	0	-701	--	--	16.08	16.08	0.18	0.01	0.03	0.20	0.00	0.00	20.9
19	55	-0	-9439	0	0	0	-4131	--	--	16.08	16.08	0.18	0.07	0.08	0.59	0.00	0.00	20.9
20	55	-0	-5922	0	0	0	-2235	--	--	16.08	16.08	0.18	0.04	0.05	0.37	0.00	0.00	20.9
37	55	-0	40	0	0	0	926	--	--	16.08	16.08	0.00	0.02	0.00	0.00	0.00	0.00	20.9
38	55	-0	-10430	0	0	0	-4790	--	--	16.08	16.08	0.18	0.08	0.09	0.65	0.00	0.00	20.9
39	55	-0	-4569	0	0	0	-1631	--	--	16.08	16.08	0.18	0.03	0.04	0.29	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 24 NI 1736 NF 1740 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	2532	0	0	0	141	--	--	16.08	16.08	0.00	0.00	0.02	0.16	0.00	0.00	20.9
2	0	-0	2064	0	0	0	68	--	--	16.08	16.08	0.10	0.00	0.02	0.13	0.00	0.00	20.9
3	0	-0	2052	0	0	0	70	--	--	16.08	16.08	0.10	0.00	0.02	0.13	0.00	0.00	20.9
4	0	-0	1844	0	0	0	147	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
5	0	-0	1832	0	0	0	149	--	--	16.08	16.08	0.10	0.00	0.02	0.11	0.00	0.00	20.9
6	0	-0	2000	0	0	0	94	--	--	16.08	16.08	0.10	0.00	0.02	0.13	0.00	0.00	20.9
7	0	-0	1961	0	0	0	99	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
8	0	-0	1934	0	0	0	118	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
9	0	-0	1895	0	0	0	123	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
10	0	-0	2064	0	0	0	68	--	--	16.08	16.08	0.10	0.00	0.02	0.13	0.00	0.00	20.9
11	0	-0	2052	0	0	0	70	--	--	16.08	16.08	0.10	0.00	0.02	0.13	0.00	0.00	20.9
12	0	-0	1844	0	0	0	147	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
13	0	-0	1832	0	0	0	149	--	--	16.08	16.08	0.10	0.00	0.02	0.11	0.00	0.00	20.9
14	0	-0	2000	0	0	0	94	--	--	16.08	16.08	0.10	0.00	0.02	0.13	0.00	0.00	20.9
15	0	-0	1961	0	0	0	99	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
16	0	-0	1934	0	0	0	118	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
17	0	-0	1895	0	0	0	123	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
18	0	-0	4117	0	0	0	184	--	--	16.08	16.08	0.00	0.00	0.03	0.26	0.00	0.00	20.9
19	0	-0	2289	0	0	0	522	--	--	16.08	16.08	0.00	0.01	0.02	0.14	0.00	0.00	20.9
20	0	-0	3056	0	0	0	333	--	--	16.08	16.08	0.00	0.01	0.03	0.19	0.00	0.00	20.9
37	0	-0	4516	0	0	0	3	--	--	16.08	16.08	0.00	0.00	0.04	0.28	0.00	0.00	20.9
38	0	-0	1468	0	0	0	565	--	--	16.08	16.08	0.00	0.01	0.01	0.09	0.00	0.00	20.9
39	0	-0	2746	0	0	0	250	--	--	16.08	16.08	0.00	0.00	0.02	0.17	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	2532	0	0	0	3538	--	--	16.08	16.08	0.00	0.06	0.02	0.16	0.00	0.00	20.9
2	27	-0	2064	0	0	0	2837	--	--	16.08	16.08	0.10	0.05	0.02	0.13	0.00	0.00	20.9
3	27	-0	2052	0	0	0	2823	--	--	16.08	16.08	0.10	0.05	0.02	0.13	0.00	0.00	20.9
4	27	-0	1844	0	0	0	2621	--	--	16.08	16.08	0.10	0.05	0.02	0.12	0.00	0.00	20.9
5	27	-0	1832	0	0	0	2606	--	--	16.08	16.08	0.10	0.05	0.02	0.11	0.00	0.00	20.9
6	27	-0	2000	0	0	0	2777	--	--	16.08	16.08	0.10	0.05	0.02	0.13	0.00	0.00	20.9
7	27	-0	1961	0	0	0	2730	--	--	16.08	16.08	0.10	0.05	0.02	0.12	0.00	0.00	20.9
8	27	-0	1934	0	0	0	2712	--	--	16.08	16.08	0.10	0.05	0.02	0.12	0.00	0.00	20.9
9	27	-0	1895	0	0	0	2665	--	--	16.08	16.08	0.10	0.05	0.02	0.12	0.00	0.00	20.9
10	27	-0	2064	0	0	0	2837	--	--	16.08	16.08	0.10	0.05	0.02	0.13	0.00	0.00	20.9
11	27	-0	2052	0	0	0	2823	--	--	16.08	16.08	0.10	0.05	0.02	0.13	0.00	0.00	20.9
12	27	-0	1844	0	0	0	2621	--	--	16.08	16.08	0.10	0.05	0.02	0.12	0.00	0.00	20.9

13	27	-0	1832	0	0	0	2606	--	--	16.08	16.08	0.10	0.05	0.02	0.11	0.00	0.00	20.9
14	27	-0	2000	0	0	0	2777	--	--	16.08	16.08	0.10	0.05	0.02	0.13	0.00	0.00	20.9
15	27	-0	1961	0	0	0	2730	--	--	16.08	16.08	0.10	0.05	0.02	0.12	0.00	0.00	20.9
16	27	-0	1934	0	0	0	2712	--	--	16.08	16.08	0.10	0.05	0.02	0.12	0.00	0.00	20.9
17	27	-0	1895	0	0	0	2665	--	--	16.08	16.08	0.10	0.05	0.02	0.12	0.00	0.00	20.9
18	27	-0	4117	0	0	0	5707	--	--	16.08	16.08	0.00	0.10	0.03	0.26	0.00	0.00	20.9
19	27	-0	2289	0	0	0	3592	--	--	16.08	16.08	0.00	0.06	0.02	0.14	0.00	0.00	20.9
20	27	-0	3056	0	0	0	4432	--	--	16.08	16.08	0.00	0.08	0.03	0.19	0.00	0.00	20.9
37	27	-0	4516	0	0	0	6060	--	--	16.08	16.08	0.00	0.10	0.04	0.28	0.00	0.00	20.9
38	27	-0	1468	0	0	0	2535	--	--	16.08	16.08	0.00	0.04	0.01	0.09	0.00	0.00	20.9
39	27	-0	2746	0	0	0	3934	--	--	16.08	16.08	0.00	0.07	0.02	0.17	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	2532	0	0	0	1522	--	--	16.08	16.08	0.00	0.03	0.02	0.16	0.00	0.00	20.9
2	55	-0	2064	0	0	0	1194	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
3	55	-0	2052	0	0	0	1189	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
4	55	-0	1844	0	0	0	1153	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
5	55	-0	1832	0	0	0	1148	--	--	16.08	16.08	0.10	0.02	0.02	0.11	0.00	0.00	20.9
6	55	-0	2000	0	0	0	1185	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
7	55	-0	1961	0	0	0	1169	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
8	55	-0	1934	0	0	0	1173	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
9	55	-0	1895	0	0	0	1157	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
10	55	-0	2064	0	0	0	1194	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
11	55	-0	2052	0	0	0	1189	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
12	55	-0	1844	0	0	0	1153	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
13	55	-0	1832	0	0	0	1148	--	--	16.08	16.08	0.10	0.02	0.02	0.11	0.00	0.00	20.9
14	55	-0	2000	0	0	0	1185	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
15	55	-0	1961	0	0	0	1169	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
16	55	-0	1934	0	0	0	1173	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
17	55	-0	1895	0	0	0	1157	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
18	55	-0	4117	0	0	0	2430	--	--	16.08	16.08	0.00	0.04	0.03	0.26	0.00	0.00	20.9
19	55	-0	2289	0	0	0	1770	--	--	16.08	16.08	0.00	0.03	0.02	0.14	0.00	0.00	20.9
20	55	-0	3056	0	0	0	1999	--	--	16.08	16.08	0.00	0.03	0.03	0.19	0.00	0.00	20.9
37	55	-0	4516	0	0	0	2465	--	--	16.08	16.08	0.00	0.04	0.04	0.28	0.00	0.00	20.9
38	55	-0	1468	0	0	0	1366	--	--	16.08	16.08	0.00	0.02	0.01	0.09	0.00	0.00	20.9
39	55	-0	2746	0	0	0	1748	--	--	16.08	16.08	0.00	0.03	0.02	0.17	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 25 NI 1737 NF 1736 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	2722	0	0	0	-255	--	--	16.08	16.08	0.18	0.00	0.02	0.17	0.00	0.00	20.9
2	0	-0	2078	0	0	0	-242	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
3	0	-0	2103	0	0	0	-239	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
4	0	-0	2085	0	0	0	-153	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
5	0	-0	2110	0	0	0	-150	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
6	0	-0	2051	0	0	0	-215	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
7	0	-0	2134	0	0	0	-204	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
8	0	-0	2053	0	0	0	-188	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
9	0	-0	2137	0	0	0	-177	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
10	0	-0	2078	0	0	0	-242	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
11	0	-0	2103	0	0	0	-239	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
12	0	-0	2085	0	0	0	-153	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
13	0	-0	2110	0	0	0	-150	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
14	0	-0	2051	0	0	0	-215	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
15	0	-0	2134	0	0	0	-204	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
16	0	-0	2053	0	0	0	-188	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
17	0	-0	2137	0	0	0	-177	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
18	0	-0	4229	0	0	0	-429	--	--	16.08	16.08	0.18	0.01	0.03	0.27	0.00	0.00	20.9
19	0	-0	3329	0	0	0	72	--	--	16.08	16.08	0.00	0.00	0.03	0.21	0.00	0.00	20.9
20	0	-0	3676	0	0	0	-171	--	--	16.08	16.08	0.18	0.00	0.03	0.23	0.00	0.00	20.9
37	0	-0	4191	0	0	0	-622	--	--	16.08	16.08	0.18	0.01	0.03	0.26	0.00	0.00	20.9
38	0	-0	2692	0	0	0	213	--	--	16.08	16.08	0.00	0.00	0.02	0.17	0.00	0.00	20.9
39	0	-0	3269	0	0	0	-191	--	--	16.08	16.08	0.18	0.00	0.03	0.21	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	2722	0	0	0	3397	--	--	16.08	16.08	0.00	0.06	0.02	0.17	0.00	0.00	20.9
2	27	-0	2078	0	0	0	2545	--	--	16.08	16.08	0.10	0.05	0.02	0.13	0.00	0.00	20.9
3	27	-0	2103	0	0	0	2582	--	--	16.08	16.08	0.10	0.05	0.02	0.13	0.00	0.00	20.9
4	27	-0	2085	0	0	0	2644	--	--	16.08	16.08	0.10	0.05	0.02	0.13	0.00	0.00	20.9
5	27	-0	2110	0	0	0	2681	--	--	16.08	16.08	0.10	0.05	0.02	0.13	0.00	0.00	20.9
6	27	-0	2051	0	0	0	2536	--	--	16.08	16.08	0.10	0.05	0.02	0.13	0.00	0.00	20.9
7	27	-0	2134	0	0	0	2659	--	--	16.08	16.08	0.10	0.05	0.02	0.13	0.00	0.00	20.9
8	27	-0	2053	0	0	0	2566	--	--	16.08	16.08	0.10	0.05	0.02	0.13	0.00	0.00	20.9
9	27	-0	2137	0	0	0	2690	--	--	16.08	16.08	0.10	0.05	0.02	0.13	0.00	0.00	20.9
10	27	-0	2078	0	0	0	2545	--	--	16.08	16.08	0.10	0.05	0.02	0.13	0.00	0.00	20.9
11	27	-0	2103	0	0	0	2582	--	--	16.08	16.08	0.10	0.05	0.02	0.13	0.00	0.00	20.9
12	27	-0	2085	0	0	0	2644	--	--	16.08	16.08	0.10	0.05	0.02	0.13	0.00	0.00	20.9
13	27	-0	2110	0	0	0	2681	--	--	16.08	16.08	0.10	0.05	0.02	0.13	0.00	0.00	20.9
14	27	-0	2051	0	0	0	2536	--	--	16.08	16.08	0.10	0.05	0.02	0.13	0.00	0.00	20.9
15	27	-0	2134	0	0	0	2659	--	--	16.08	16.08	0.10	0.05	0.02	0.13	0.00	0.00	20.9
16	27	-0	2053	0	0	0	2566	--	--	16.08	16.08	0.10	0.05	0.02	0.13	0.00	0.00	20.9
17	27	-0	2137	0	0	0	2690	--	--	16.08	16.08	0.10	0.05	0.02	0.13	0.00	0.00	20.9
18	27	-0	4229	0	0	0	5244	--	--	16.08	16.08	0.00	0.09	0.03	0.27	0.00	0.00	20.9
19	27	-0	3329	0	0	0	4538	--	--	16.08	16.08	0.00	0.08	0.03	0.21	0.00	0.00	20.9
20	27	-0	3676	0	0	0	4760	--	--	16.08	16.08	0.00	0.08	0.03	0.23	0.00	0.00	20.9
37	27	-0	4191	0	0	0	5000	--	--	16.08	16.08	0.00	0.09	0.03	0.26	0.00	0.00	20.9
38	27	-0	2692	0	0	0	3825	--	--	16.08	16.08	0.00	0.07	0.02	0.17	0.00	0.00	20.9
39	27	-0	3269	0	0	0	4194	--	--	16.08	16.08	0.00	0.07	0.03	0.21	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	2722	0	0	0	1230	--	--	16.08	16.08	0.00	0.02	0.02	0.17	0.00	0.00	20.9
2	55	-0	2078	0	0	0	891	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
3	55	-0	2103	0	0	0	908	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
4	55	-0	2085	0	0	0	985	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
5	55	-0	2110	0	0	0	1002	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
6	55	-0	2051	0	0	0	904	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
7	55	-0	2134	0	0	0	961	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
8	55	-0	2053	0	0	0	932	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9

9	55	-0	2137	0	0	0	989	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
10	55	-0	2078	0	0	0	891	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
11	55	-0	2103	0	0	0	908	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
12	55	-0	2085	0	0	0	985	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
13	55	-0	2110	0	0	0	1002	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
14	55	-0	2051	0	0	0	904	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
15	55	-0	2134	0	0	0	961	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
16	55	-0	2053	0	0	0	932	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
17	55	-0	2137	0	0	0	989	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
18	55	-0	4229	0	0	0	1878	--	--	16.08	16.08	0.00	0.03	0.03	0.27	0.00	0.00	20.9
19	55	-0	3329	0	0	0	1888	--	--	16.08	16.08	0.00	0.03	0.03	0.21	0.00	0.00	20.9
20	55	-0	3676	0	0	0	1834	--	--	16.08	16.08	0.00	0.03	0.03	0.23	0.00	0.00	20.9
37	55	-0	4191	0	0	0	1664	--	--	16.08	16.08	0.00	0.03	0.03	0.26	0.00	0.00	20.9
38	55	-0	2692	0	0	0	1682	--	--	16.08	16.08	0.00	0.03	0.02	0.17	0.00	0.00	20.9
39	55	-0	3269	0	0	0	1592	--	--	16.08	16.08	0.00	0.03	0.03	0.21	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 26 NI 1732 NF 1737 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	1523	0	0	0	-592	--	--	16.08	16.08	0.18	0.01	0.01	0.10	0.00	0.00	20.9
2	0	-0	1184	0	0	0	-486	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
3	0	-0	1217	0	0	0	-487	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
4	0	-0	1127	0	0	0	-424	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
5	0	-0	1159	0	0	0	-424	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
6	0	-0	1126	0	0	0	-464	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
7	0	-0	1234	0	0	0	-465	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
8	0	-0	1109	0	0	0	-445	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
9	0	-0	1217	0	0	0	-446	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
10	0	-0	1184	0	0	0	-486	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
11	0	-0	1217	0	0	0	-487	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
12	0	-0	1127	0	0	0	-424	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
13	0	-0	1159	0	0	0	-424	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
14	0	-0	1126	0	0	0	-464	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
15	0	-0	1234	0	0	0	-465	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
16	0	-0	1109	0	0	0	-445	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
17	0	-0	1217	0	0	0	-446	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
18	0	-0	2425	0	0	0	-934	--	--	16.08	16.08	0.18	0.02	0.02	0.15	0.00	0.00	20.9
19	0	-0	1639	0	0	0	-437	--	--	16.08	16.08	0.18	0.01	0.01	0.10	0.00	0.00	20.9
20	0	-0	2034	0	0	0	-661	--	--	16.08	16.08	0.18	0.01	0.02	0.13	0.00	0.00	20.9
37	0	-0	2526	0	0	0	-1071	--	--	16.08	16.08	0.18	0.02	0.02	0.16	0.00	0.00	20.9
38	0	-0	1215	0	0	0	-242	--	--	16.08	16.08	0.18	0.00	0.01	0.08	0.00	0.00	20.9
39	0	-0	1873	0	0	0	-615	--	--	16.08	16.08	0.18	0.01	0.02	0.12	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	1523	0	0	0	-592	--	--	16.08	16.08	0.18	0.01	0.01	0.10	0.00	0.00	20.9
2	27	-0	1184	0	0	0	-486	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
3	27	-0	1217	0	0	0	-487	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
4	27	-0	1127	0	0	0	-424	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
5	27	-0	1159	0	0	0	-424	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
6	27	-0	1126	0	0	0	-464	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
7	27	-0	1234	0	0	0	-465	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
8	27	-0	1109	0	0	0	-445	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
9	27	-0	1217	0	0	0	-446	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
10	27	-0	1184	0	0	0	-486	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
11	27	-0	1217	0	0	0	-487	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
12	27	-0	1127	0	0	0	-424	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
13	27	-0	1159	0	0	0	-424	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
14	27	-0	1126	0	0	0	-464	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
15	27	-0	1234	0	0	0	-465	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
16	27	-0	1109	0	0	0	-445	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
17	27	-0	1217	0	0	0	-446	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
18	27	-0	2425	0	0	0	-934	--	--	16.08	16.08	0.18	0.02	0.02	0.15	0.00	0.00	20.9
19	27	-0	1639	0	0	0	1762	--	--	16.08	16.08	0.00	0.03	0.01	0.10	0.00	0.00	20.9
20	27	-0	2034	0	0	0	-661	--	--	16.08	16.08	0.18	0.01	0.02	0.13	0.00	0.00	20.9
37	27	-0	2526	0	0	0	-1071	--	--	16.08	16.08	0.18	0.02	0.02	0.16	0.00	0.00	20.9
38	27	-0	1215	0	0	0	1388	--	--	16.08	16.08	0.00	0.02	0.01	0.08	0.00	0.00	20.9
39	27	-0	1873	0	0	0	-615	--	--	16.08	16.08	0.18	0.01	0.02	0.12	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	1523	0	0	0	239	--	--	16.08	16.08	0.00	0.00	0.01	0.10	0.00	0.00	20.9
2	55	-0	1184	0	0	0	160	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
3	55	-0	1217	0	0	0	177	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
4	55	-0	1127	0	0	0	191	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
5	55	-0	1159	0	0	0	208	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
6	55	-0	1126	0	0	0	151	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
7	55	-0	1234	0	0	0	208	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
8	55	-0	1109	0	0	0	160	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
9	55	-0	1217	0	0	0	217	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
10	55	-0	1184	0	0	0	160	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
11	55	-0	1217	0	0	0	177	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
12	55	-0	1127	0	0	0	191	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
13	55	-0	1159	0	0	0	208	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
14	55	-0	1126	0	0	0	151	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
15	55	-0	1234	0	0	0	208	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
16	55	-0	1109	0	0	0	160	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
17	55	-0	1217	0	0	0	217	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
18	55	-0	2425	0	0	0	388	--	--	16.08	16.08	0.00	0.01	0.02	0.15	0.00	0.00	20.9
19	55	-0	1639	0	0	0	457	--	--	16.08	16.08	0.00	0.01	0.01	0.10	0.00	0.00	20.9
20	55	-0	2034	0	0	0	448	--	--	16.08	16.08	0.00	0.01	0.02	0.13	0.00	0.00	20.9
37	55	-0	2526	0	0	0	307	--	--	16.08	16.08	0.00	0.01	0.02	0.16	0.00	0.00	20.9
38	55	-0	1215	0	0	0	421	--	--	16.08	16.08	0.00	0.01	0.01	0.08	0.00	0.00	20.9
39	55	-0	1873	0	0	0	407	--	--	16.08	16.08	0.00	0.01	0.02	0.12	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 27 NI 1738 NF 1732 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	687	0	0	0	-672	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
2	0	-0	538	0	0	0	-540	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
3	0	-0	570	0	0	0	-546	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
4	0	-0	486	0	0	0	-487	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
5	0	-0	518	0	0	0	-493	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
6	0	-0	483	0	0	0	-514	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
7	0	-0	589	0	0	0	-535	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
8	0	-0	467	0	0	0	-498	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
9	0	-0	574	0	0	0	-519	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
10	0	-0	538	0	0	0	-540	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
11	0	-0	570	0	0	0	-546	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
12	0	-0	486	0	0	0	-487	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
13	0	-0	518	0	0	0	-493	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
14	0	-0	483	0	0	0	-514	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
15	0	-0	589	0	0	0	-535	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
16	0	-0	467	0	0	0	-498	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
17	0	-0	574	0	0	0	-519	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
18	0	-0	1135	0	0	0	-1057	--	--	16.08	16.08	0.18	0.02	0.01	0.07	0.00	0.00	20.9
19	0	-0	648	0	0	0	-573	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
20	0	-0	939	0	0	0	-797	--	--	16.08	16.08	0.18	0.01	0.01	0.06	0.00	0.00	20.9
37	0	-0	1233	0	0	0	-1173	--	--	16.08	16.08	0.18	0.02	0.01	0.08	0.00	0.00	20.9
38	0	-0	422	0	0	0	-367	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9
39	0	-0	906	0	0	0	-740	--	--	16.08	16.08	0.18	0.01	0.01	0.06	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	687	0	0	0	-672	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
2	27	-0	538	0	0	0	-540	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
3	27	-0	570	0	0	0	-546	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
4	27	-0	486	0	0	0	-487	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
5	27	-0	518	0	0	0	-493	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
6	27	-0	483	0	0	0	-514	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
7	27	-0	589	0	0	0	-535	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
8	27	-0	467	0	0	0	-498	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
9	27	-0	574	0	0	0	-519	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
10	27	-0	538	0	0	0	-540	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
11	27	-0	570	0	0	0	-546	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
12	27	-0	486	0	0	0	-487	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
13	27	-0	518	0	0	0	-493	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
14	27	-0	483	0	0	0	-514	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
15	27	-0	589	0	0	0	-535	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
16	27	-0	467	0	0	0	-498	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
17	27	-0	574	0	0	0	-519	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
18	27	-0	1135	0	0	0	-1057	--	--	16.08	16.08	0.18	0.02	0.01	0.07	0.00	0.00	20.9
19	27	-0	648	0	0	0	-573	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
20	27	-0	939	0	0	0	-797	--	--	16.08	16.08	0.18	0.01	0.01	0.06	0.00	0.00	20.9
37	27	-0	1233	0	0	0	-1173	--	--	16.08	16.08	0.18	0.02	0.01	0.08	0.00	0.00	20.9
38	27	-0	422	0	0	0	-367	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9
39	27	-0	906	0	0	0	-740	--	--	16.08	16.08	0.18	0.01	0.01	0.06	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	687	0	0	0	-672	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
2	55	-0	538	0	0	0	-540	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
3	55	-0	570	0	0	0	-546	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
4	55	-0	486	0	0	0	-487	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
5	55	-0	518	0	0	0	-493	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
6	55	-0	483	0	0	0	-514	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
7	55	-0	589	0	0	0	-535	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
8	55	-0	467	0	0	0	-498	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
9	55	-0	574	0	0	0	-519	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
10	55	-0	538	0	0	0	-540	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
11	55	-0	570	0	0	0	-546	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
12	55	-0	486	0	0	0	-487	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
13	55	-0	518	0	0	0	-493	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
14	55	-0	483	0	0	0	-514	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
15	55	-0	589	0	0	0	-535	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
16	55	-0	467	0	0	0	-498	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
17	55	-0	574	0	0	0	-519	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
18	55	-0	1135	0	0	0	-1057	--	--	16.08	16.08	0.18	0.02	0.01	0.07	0.00	0.00	20.9
19	55	-0	648	0	0	0	-573	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
20	55	-0	939	0	0	0	-797	--	--	16.08	16.08	0.18	0.01	0.01	0.06	0.00	0.00	20.9
37	55	-0	1233	0	0	0	-1173	--	--	16.08	16.08	0.18	0.02	0.01	0.08	0.00	0.00	20.9
38	55	-0	422	0	0	0	-367	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9
39	55	-0	906	0	0	0	-740	--	--	16.08	16.08	0.18	0.01	0.01	0.06	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 28 NI 1739 NF 1738 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	14	0	0	0	-578	--	--	16.08	16.08	0.18	0.01	0.00	0.00	0.00	0.00	20.9
2	0	-0	4	0	0	0	-461	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
3	0	-0	35	0	0	0	-473	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
4	0	-0	-13	0	0	0	-423	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
5	0	-0	18	0	0	0	-428	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
6	0	-0	-39	0	0	0	-452	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
7	0	-0	66	0	0	0	-471	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
8	0	-0	-44	0	0	0	-441	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
9	0	-0	61	0	0	0	-458	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
10	0	-0	4	0	0	0	-461	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
11	0	-0	35	0	0	0	-473	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
12	0	-0	-13	0	0	0	-423	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
13	0	-0	18	0	0	0	-428	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
14	0	-0	-39	0	0	0	-452	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
15	0	-0	66	0	0	0	-471	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
16	0	-0	-44	0	0	0	-441	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9

17	0	-0	61	0	0	0	-458	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
18	0	-0	75	0	0	0	-914	--	--	16.08	16.08	0.18	0.02	0.00	0.00	0.00	0.00	20.9
19	0	-0	-28	0	0	0	-506	--	--	16.08	16.08	0.18	0.01	0.00	0.00	0.00	0.00	20.9
20	0	-0	100	0	0	0	-702	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9
37	0	-0	108	0	0	0	-1016	--	--	16.08	16.08	0.18	0.02	0.00	0.01	0.00	0.00	20.9
38	0	-0	-65	0	0	0	-346	--	--	16.08	16.08	0.18	0.01	0.00	0.00	0.00	0.00	20.9
39	0	-0	148	0	0	0	-662	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	14	0	0	0	-578	--	--	16.08	16.08	0.18	0.01	0.00	0.00	0.00	0.00	20.9
2	27	-0	4	0	0	0	-461	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
3	27	-0	35	0	0	0	-473	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
4	27	-0	-13	0	0	0	-423	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
5	27	-0	18	0	0	0	-428	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
6	27	-0	-39	0	0	0	-452	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
7	27	-0	66	0	0	0	-471	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
8	27	-0	-44	0	0	0	-441	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
9	27	-0	61	0	0	0	-458	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
10	27	-0	4	0	0	0	-461	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
11	27	-0	35	0	0	0	-473	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
12	27	-0	-13	0	0	0	-423	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
13	27	-0	18	0	0	0	-428	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
14	27	-0	-39	0	0	0	-452	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
15	27	-0	66	0	0	0	-471	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
16	27	-0	-44	0	0	0	-441	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
17	27	-0	61	0	0	0	-458	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
18	27	-0	75	0	0	0	-914	--	--	16.08	16.08	0.18	0.02	0.00	0.00	0.00	0.00	20.9
19	27	-0	-28	0	0	0	-506	--	--	16.08	16.08	0.18	0.01	0.00	0.00	0.00	0.00	20.9
20	27	-0	100	0	0	0	-702	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9
37	27	-0	108	0	0	0	-1016	--	--	16.08	16.08	0.18	0.02	0.00	0.01	0.00	0.00	20.9
38	27	-0	-65	0	0	0	-346	--	--	16.08	16.08	0.18	0.01	0.00	0.00	0.00	0.00	20.9
39	27	-0	148	0	0	0	-662	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	14	0	0	0	-578	--	--	16.08	16.08	0.18	0.01	0.00	0.00	0.00	0.00	20.9
2	55	-0	4	0	0	0	-461	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
3	55	-0	35	0	0	0	-473	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
4	55	-0	-13	0	0	0	-423	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
5	55	-0	18	0	0	0	-428	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
6	55	-0	-39	0	0	0	-452	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
7	55	-0	66	0	0	0	-471	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
8	55	-0	-44	0	0	0	-441	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
9	55	-0	61	0	0	0	-458	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
10	55	-0	4	0	0	0	-461	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
11	55	-0	35	0	0	0	-473	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
12	55	-0	-13	0	0	0	-423	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
13	55	-0	18	0	0	0	-428	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
14	55	-0	-39	0	0	0	-452	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
15	55	-0	66	0	0	0	-471	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
16	55	-0	-44	0	0	0	-441	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
17	55	-0	61	0	0	0	-458	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
18	55	-0	75	0	0	0	-914	--	--	16.08	16.08	0.18	0.02	0.00	0.00	0.00	0.00	20.9
19	55	-0	-28	0	0	0	-506	--	--	16.08	16.08	0.18	0.01	0.00	0.00	0.00	0.00	20.9
20	55	-0	100	0	0	0	-702	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9
37	55	-0	108	0	0	0	-1016	--	--	16.08	16.08	0.18	0.02	0.00	0.01	0.00	0.00	20.9
38	55	-0	-65	0	0	0	-346	--	--	16.08	16.08	0.18	0.01	0.00	0.00	0.00	0.00	20.9
39	55	-0	148	0	0	0	-662	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 29 NI 1733 NF 1739 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-662	0	0	0	-668	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
2	0	-0	-534	0	0	0	-539	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
3	0	-0	-502	0	0	0	-540	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
4	0	-0	-515	0	0	0	-488	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
5	0	-0	-484	0	0	0	-489	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
6	0	-0	-565	0	0	0	-520	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
7	0	-0	-459	0	0	0	-523	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
8	0	-0	-559	0	0	0	-505	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
9	0	-0	-453	0	0	0	-508	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
10	0	-0	-534	0	0	0	-539	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
11	0	-0	-502	0	0	0	-540	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
12	0	-0	-515	0	0	0	-488	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
13	0	-0	-484	0	0	0	-489	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
14	0	-0	-565	0	0	0	-520	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
15	0	-0	-459	0	0	0	-523	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
16	0	-0	-559	0	0	0	-505	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
17	0	-0	-453	0	0	0	-508	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
18	0	-0	-991	0	0	0	-1041	--	--	16.08	16.08	0.18	0.02	0.01	0.06	0.00	0.00	20.9
19	0	-0	-711	0	0	0	-575	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
20	0	-0	-743	0	0	0	-778	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9
37	0	-0	-1023	0	0	0	-1153	--	--	16.08	16.08	0.18	0.02	0.01	0.06	0.00	0.00	20.9
38	0	-0	-557	0	0	0	-376	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9
39	0	-0	-611	0	0	0	-714	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-662	0	0	0	-668	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
2	27	-0	-534	0	0	0	-539	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
3	27	-0	-502	0	0	0	-540	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
4	27	-0	-515	0	0	0	-488	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
5	27	-0	-484	0	0	0	-489	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
6	27	-0	-565	0	0	0	-520	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
7	27	-0	-459	0	0	0	-523	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
8	27	-0	-559	0	0	0	-505	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
9	27	-0	-453	0	0	0	-508	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
10	27	-0	-534	0	0	0	-539	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
11	27	-0	-502	0	0	0	-540	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
12	27	-0	-515	0	0	0	-488	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9

13	27	-0	-484	0	0	0	-489	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
14	27	-0	-565	0	0	0	-520	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
15	27	-0	-459	0	0	0	-523	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
16	27	-0	-559	0	0	0	-505	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
17	27	-0	-453	0	0	0	-508	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
18	27	-0	-991	0	0	0	-1041	--	--	16.08	16.08	0.18	0.02	0.01	0.06	0.00	0.00	20.9
19	27	-0	-711	0	0	0	-575	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
20	27	-0	-743	0	0	0	-778	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9
37	27	-0	-1023	0	0	0	-1153	--	--	16.08	16.08	0.18	0.02	0.01	0.06	0.00	0.00	20.9
38	27	-0	-557	0	0	0	-376	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9
39	27	-0	-611	0	0	0	-714	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	-662	0	0	0	-668	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
2	55	-0	-534	0	0	0	-539	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
3	55	-0	-502	0	0	0	-540	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
4	55	-0	-515	0	0	0	-488	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
5	55	-0	-484	0	0	0	-489	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
6	55	-0	-565	0	0	0	-520	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
7	55	-0	-459	0	0	0	-523	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
8	55	-0	-559	0	0	0	-505	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
9	55	-0	-453	0	0	0	-508	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
10	55	-0	-534	0	0	0	-539	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
11	55	-0	-502	0	0	0	-540	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
12	55	-0	-515	0	0	0	-488	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
13	55	-0	-484	0	0	0	-489	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
14	55	-0	-565	0	0	0	-520	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
15	55	-0	-459	0	0	0	-523	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
16	55	-0	-559	0	0	0	-505	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
17	55	-0	-453	0	0	0	-508	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
18	55	-0	-991	0	0	0	-1041	--	--	16.08	16.08	0.18	0.02	0.01	0.06	0.00	0.00	20.9
19	55	-0	-711	0	0	0	-575	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
20	55	-0	-743	0	0	0	-778	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9
37	55	-0	-1023	0	0	0	-1153	--	--	16.08	16.08	0.18	0.02	0.01	0.06	0.00	0.00	20.9
38	55	-0	-557	0	0	0	-376	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9
39	55	-0	-611	0	0	0	-714	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 30 NI 1734 NF 1733 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--	--	--	--	--	--	--	--	--	--	--		--	--	--	--	--	--
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-1512	0	0	0	234	--	--	16.08	16.08	0.00	0.00	0.01	0.09	0.00	0.00	20.9
2	0	-0	-1191	0	0	0	165	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
3	0	-0	-1158	0	0	0	141	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
4	0	-0	-1168	0	0	0	219	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
5	0	-0	-1135	0	0	0	194	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
6	0	-0	-1220	0	0	0	213	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
7	0	-0	-1112	0	0	0	131	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
8	0	-0	-1213	0	0	0	229	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
9	0	-0	-1106	0	0	0	147	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
10	0	-0	-1191	0	0	0	165	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
11	0	-0	-1158	0	0	0	141	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
12	0	-0	-1168	0	0	0	219	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
13	0	-0	-1135	0	0	0	194	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
14	0	-0	-1220	0	0	0	213	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
15	0	-0	-1112	0	0	0	131	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
16	0	-0	-1213	0	0	0	229	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
17	0	-0	-1106	0	0	0	147	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
18	0	-0	-2302	0	0	0	314	--	--	16.08	16.08	0.00	0.01	0.02	0.14	0.00	0.00	20.9
19	0	-0	-1724	0	0	0	517	--	--	16.08	16.08	0.00	0.01	0.01	0.11	0.00	0.00	20.9
20	0	-0	-1856	0	0	0	338	--	--	16.08	16.08	0.00	0.01	0.02	0.12	0.00	0.00	20.9
37	0	-0	-2334	0	0	0	187	--	--	16.08	16.08	0.00	0.00	0.02	0.15	0.00	0.00	20.9
38	0	-0	-1372	0	0	0	525	--	--	16.08	16.08	0.00	0.01	0.01	0.09	0.00	0.00	20.9
39	0	-0	-1592	0	0	0	228	--	--	16.08	16.08	0.00	0.00	0.01	0.10	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-1512	0	0	0	-591	--	--	16.08	16.08	0.18	0.01	0.01	0.09	0.00	0.00	20.9
2	27	-0	-1191	0	0	0	-484	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
3	27	-0	-1158	0	0	0	-491	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
4	27	-0	-1168	0	0	0	-418	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
5	27	-0	-1135	0	0	0	-425	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
6	27	-0	-1220	0	0	0	-453	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
7	27	-0	-1112	0	0	0	-476	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
8	27	-0	-1213	0	0	0	-433	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
9	27	-0	-1106	0	0	0	-456	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
10	27	-0	-1191	0	0	0	-484	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
11	27	-0	-1158	0	0	0	-491	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
12	27	-0	-1168	0	0	0	-418	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
13	27	-0	-1135	0	0	0	-425	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
14	27	-0	-1220	0	0	0	-453	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
15	27	-0	-1112	0	0	0	-476	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
16	27	-0	-1213	0	0	0	-433	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
17	27	-0	-1106	0	0	0	-456	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
18	27	-0	-2302	0	0	0	-942	--	--	16.08	16.08	0.18	0.02	0.02	0.14	0.00	0.00	20.9
19	27	-0	-1724	0	0	0	517	--	--	16.08	16.08	0.00	0.01	0.01	0.11	0.00	0.00	20.9
20	27	-0	-1856	0	0	0	-674	--	--	16.08	16.08	0.18	0.01	0.02	0.12	0.00	0.00	20.9
37	27	-0	-2334	0	0	0	-1086	--	--	16.08	16.08	0.18	0.02	0.02	0.15	0.00	0.00	20.9
38	27	-0	-1372	0	0	0	525	--	--	16.08	16.08	0.00	0.01	0.01	0.09	0.00	0.00	20.9
39	27	-0	-1592	0	0	0	-640	--	--	16.08	16.08	0.18	0.01	0.01	0.10	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	-1512	0	0	0	-591	--	--	16.08	16.08	0.18	0.01	0.01	0.09	0.00	0.00	20.9
2	55	-0	-1191	0	0	0	-484	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
3	55	-0	-1158	0	0	0	-491	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
4	55	-0	-1168	0	0	0	-418	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
5	55	-0	-1135	0	0	0	-425	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
6	55	-0	-1220	0	0	0	-453	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
7	55	-0	-1112	0	0	0	-476	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
8	55	-0	-1213	0	0	0	-433	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9

9	55	-0	-1106	0	0	0	-456	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
10	55	-0	-1191	0	0	0	-484	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
11	55	-0	-1158	0	0	0	-491	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
12	55	-0	-1168	0	0	0	-418	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
13	55	-0	-1135	0	0	0	-425	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
14	55	-0	-1220	0	0	0	-453	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
15	55	-0	-1112	0	0	0	-476	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
16	55	-0	-1213	0	0	0	-433	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
17	55	-0	-1106	0	0	0	-456	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
18	55	-0	-2302	0	0	0	-942	--	--	16.08	16.08	0.18	0.02	0.02	0.14	0.00	0.00	20.9
19	55	-0	-1724	0	0	0	-424	--	--	16.08	16.08	0.18	0.01	0.01	0.11	0.00	0.00	20.9
20	55	-0	-1856	0	0	0	-674	--	--	16.08	16.08	0.18	0.01	0.02	0.12	0.00	0.00	20.9
37	55	-0	-2334	0	0	0	-1086	--	--	16.08	16.08	0.18	0.02	0.02	0.15	0.00	0.00	20.9
38	55	-0	-1372	0	0	0	-223	--	--	16.08	16.08	0.18	0.00	0.01	0.09	0.00	0.00	20.9
39	55	-0	-1592	0	0	0	-640	--	--	16.08	16.08	0.18	0.01	0.01	0.10	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 31 NI 1735 NF 1734 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-2727	0	0	0	1234	--	--	16.08	16.08	0.00	0.02	0.02	0.17	0.00	0.00	20.9
2	0	-0	-2089	0	0	0	901	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
3	0	-0	-2063	0	0	0	875	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
4	0	-0	-2133	0	0	0	1024	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
5	0	-0	-2107	0	0	0	998	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
6	0	-0	-2135	0	0	0	974	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
7	0	-0	-2048	0	0	0	888	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
8	0	-0	-2148	0	0	0	1011	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
9	0	-0	-2061	0	0	0	925	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
10	0	-0	-2089	0	0	0	901	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
11	0	-0	-2063	0	0	0	875	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
12	0	-0	-2133	0	0	0	1024	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
13	0	-0	-2107	0	0	0	998	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
14	0	-0	-2135	0	0	0	974	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
15	0	-0	-2048	0	0	0	888	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
16	0	-0	-2148	0	0	0	1011	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
17	0	-0	-2061	0	0	0	925	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
18	0	-0	-4132	0	0	0	1800	--	--	16.08	16.08	0.00	0.03	0.03	0.26	0.00	0.00	20.9
19	0	-0	-3441	0	0	0	1983	--	--	16.08	16.08	0.00	0.03	0.03	0.22	0.00	0.00	20.9
20	0	-0	-3564	0	0	0	1743	--	--	16.08	16.08	0.00	0.03	0.03	0.22	0.00	0.00	20.9
37	0	-0	-4022	0	0	0	1527	--	--	16.08	16.08	0.00	0.03	0.03	0.25	0.00	0.00	20.9
38	0	-0	-2871	0	0	0	1832	--	--	16.08	16.08	0.00	0.03	0.02	0.18	0.00	0.00	20.9
39	0	-0	-3076	0	0	0	1431	--	--	16.08	16.08	0.00	0.02	0.03	0.19	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-2727	0	0	0	1234	--	--	16.08	16.08	0.00	0.02	0.02	0.17	0.00	0.00	20.9
2	27	-0	-2089	0	0	0	901	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
3	27	-0	-2063	0	0	0	875	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
4	27	-0	-2133	0	0	0	1024	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
5	27	-0	-2107	0	0	0	998	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
6	27	-0	-2135	0	0	0	974	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
7	27	-0	-2048	0	0	0	888	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
8	27	-0	-2148	0	0	0	1011	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
9	27	-0	-2061	0	0	0	925	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
10	27	-0	-2089	0	0	0	901	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
11	27	-0	-2063	0	0	0	875	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
12	27	-0	-2133	0	0	0	1024	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
13	27	-0	-2107	0	0	0	998	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
14	27	-0	-2135	0	0	0	974	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
15	27	-0	-2048	0	0	0	888	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
16	27	-0	-2148	0	0	0	1011	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
17	27	-0	-2061	0	0	0	925	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
18	27	-0	-4132	0	0	0	1800	--	--	16.08	16.08	0.00	0.03	0.03	0.26	0.00	0.00	20.9
19	27	-0	-3441	0	0	0	1983	--	--	16.08	16.08	0.00	0.03	0.03	0.22	0.00	0.00	20.9
20	27	-0	-3564	0	0	0	1743	--	--	16.08	16.08	0.00	0.03	0.03	0.22	0.00	0.00	20.9
37	27	-0	-4022	0	0	0	1527	--	--	16.08	16.08	0.00	0.03	0.03	0.25	0.00	0.00	20.9
38	27	-0	-2871	0	0	0	1832	--	--	16.08	16.08	0.00	0.03	0.02	0.18	0.00	0.00	20.9
39	27	-0	-3076	0	0	0	1431	--	--	16.08	16.08	0.00	0.02	0.03	0.19	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	-2727	0	0	0	-254	--	--	16.08	16.08	0.18	0.00	0.02	0.17	0.00	0.00	20.9
2	55	-0	-2089	0	0	0	-239	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
3	55	-0	-2063	0	0	0	-250	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
4	55	-0	-2133	0	0	0	-140	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
5	55	-0	-2107	0	0	0	-151	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
6	55	-0	-2135	0	0	0	-191	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
7	55	-0	-2048	0	0	0	-229	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
8	55	-0	-2148	0	0	0	-161	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
9	55	-0	-2061	0	0	0	-199	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
10	55	-0	-2089	0	0	0	-239	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
11	55	-0	-2063	0	0	0	-250	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
12	55	-0	-2133	0	0	0	-140	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
13	55	-0	-2107	0	0	0	-151	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
14	55	-0	-2135	0	0	0	-191	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
15	55	-0	-2048	0	0	0	-229	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
16	55	-0	-2148	0	0	0	-161	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
17	55	-0	-2061	0	0	0	-199	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
18	55	-0	-4132	0	0	0	-454	--	--	16.08	16.08	0.18	0.01	0.03	0.26	0.00	0.00	20.9
19	55	-0	-3441	0	0	0	106	--	--	16.08	16.08	0.00	0.00	0.03	0.22	0.00	0.00	20.9
20	55	-0	-3564	0	0	0	-201	--	--	16.08	16.08	0.18	0.00	0.03	0.22	0.00	0.00	20.9
37	55	-0	-4022	0	0	0	-668	--	--	16.08	16.08	0.18	0.01	0.03	0.25	0.00	0.00	20.9
38	55	-0	-2871	0	0	0	266	--	--	16.08	16.08	0.00	0.00	0.02	0.18	0.00	0.00	20.9
39	55	-0	-3076	0	0	0	-247	--	--	16.08	16.08	0.18	0.00	0.03	0.19	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 32 NI 1731 NF 1735 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice resistenza			aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-2394	0	0	0	1424	--	--	16.08	16.08	0.00	0.02	0.02	0.15	0.00	0.00	20.9
2	0	-0	-1932	0	0	0	1103	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
3	0	-0	-1946	0	0	0	1101	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
4	0	-0	-1737	0	0	0	1090	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
5	0	-0	-1751	0	0	0	1087	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
6	0	-0	-1848	0	0	0	1101	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
7	0	-0	-1894	0	0	0	1094	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
8	0	-0	-1789	0	0	0	1097	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
9	0	-0	-1835	0	0	0	1089	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
10	0	-0	-1932	0	0	0	1103	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
11	0	-0	-1946	0	0	0	1101	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
12	0	-0	-1737	0	0	0	1090	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
13	0	-0	-1751	0	0	0	1087	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
14	0	-0	-1848	0	0	0	1101	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
15	0	-0	-1894	0	0	0	1094	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
16	0	-0	-1789	0	0	0	1097	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
17	0	-0	-1835	0	0	0	1089	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
18	0	-0	-3759	0	0	0	2151	--	--	16.08	16.08	0.00	0.04	0.03	0.24	0.00	0.00	20.9
19	0	-0	-2110	0	0	0	1678	--	--	16.08	16.08	0.00	0.03	0.02	0.13	0.00	0.00	20.9
20	0	-0	-2906	0	0	0	1861	--	--	16.08	16.08	0.00	0.03	0.02	0.18	0.00	0.00	20.9
37	0	-0	-4140	0	0	0	2152	--	--	16.08	16.08	0.00	0.04	0.03	0.26	0.00	0.00	20.9
38	0	-0	-1391	0	0	0	1364	--	--	16.08	16.08	0.00	0.02	0.01	0.09	0.00	0.00	20.9
39	0	-0	-2716	0	0	0	1668	--	--	16.08	16.08	0.00	0.03	0.02	0.17	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice resistenza			aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	27	-0	-2394	0	0	0	1424	--	--	16.08	16.08	0.00	0.02	0.02	0.15	0.00	0.00	20.9
2	27	-0	-1932	0	0	0	1103	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
3	27	-0	-1946	0	0	0	1101	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
4	27	-0	-1737	0	0	0	1090	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
5	27	-0	-1751	0	0	0	1087	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
6	27	-0	-1848	0	0	0	1101	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
7	27	-0	-1894	0	0	0	1094	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
8	27	-0	-1789	0	0	0	1097	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
9	27	-0	-1835	0	0	0	1089	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
10	27	-0	-1932	0	0	0	1103	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
11	27	-0	-1946	0	0	0	1101	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
12	27	-0	-1737	0	0	0	1090	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
13	27	-0	-1751	0	0	0	1087	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
14	27	-0	-1848	0	0	0	1101	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
15	27	-0	-1894	0	0	0	1094	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
16	27	-0	-1789	0	0	0	1097	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
17	27	-0	-1835	0	0	0	1089	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
18	27	-0	-3759	0	0	0	2151	--	--	16.08	16.08	0.00	0.04	0.03	0.24	0.00	0.00	20.9
19	27	-0	-2110	0	0	0	1678	--	--	16.08	16.08	0.00	0.03	0.02	0.13	0.00	0.00	20.9
20	27	-0	-2906	0	0	0	1861	--	--	16.08	16.08	0.00	0.03	0.02	0.18	0.00	0.00	20.9
37	27	-0	-4140	0	0	0	2152	--	--	16.08	16.08	0.00	0.04	0.03	0.26	0.00	0.00	20.9
38	27	-0	-1391	0	0	0	1364	--	--	16.08	16.08	0.00	0.02	0.01	0.09	0.00	0.00	20.9
39	27	-0	-2716	0	0	0	1668	--	--	16.08	16.08	0.00	0.03	0.02	0.17	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice resistenza			aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	55	-0	-2394	0	0	0	118	--	--	16.08	16.08	0.00	0.00	0.02	0.15	0.00	0.00	20.9
2	55	-0	-1932	0	0	0	50	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
3	55	-0	-1946	0	0	0	40	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
4	55	-0	-1737	0	0	0	142	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
5	55	-0	-1751	0	0	0	132	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
6	55	-0	-1848	0	0	0	93	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
7	55	-0	-1894	0	0	0	61	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
8	55	-0	-1789	0	0	0	121	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
9	55	-0	-1835	0	0	0	89	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
10	55	-0	-1932	0	0	0	50	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
11	55	-0	-1946	0	0	0	40	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
12	55	-0	-1737	0	0	0	142	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
13	55	-0	-1751	0	0	0	132	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
14	55	-0	-1848	0	0	0	93	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
15	55	-0	-1894	0	0	0	61	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
16	55	-0	-1789	0	0	0	121	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
17	55	-0	-1835	0	0	0	89	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
18	55	-0	-3759	0	0	0	100	--	--	16.08	16.08	0.00	0.00	0.03	0.24	0.00	0.00	20.9
19	55	-0	-2110	0	0	0	528	--	--	16.08	16.08	0.00	0.01	0.02	0.13	0.00	0.00	20.9
20	55	-0	-2906	0	0	0	276	--	--	16.08	16.08	0.00	0.00	0.02	0.18	0.00	0.00	20.9
37	55	-0	-4140	0	0	0	-106	--	--	16.08	16.08	0.18	0.00	0.03	0.26	0.00	0.00	20.9
38	55	-0	-1391	0	0	0	606	--	--	16.08	16.08	0.00	0.01	0.01	0.09	0.00	0.00	20.9
39	55	-0	-2716	0	0	0	187	--	--	16.08	16.08	0.00	0.00	0.02	0.17	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 33 NI 1582 NF 1731 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice resistenza			aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	3633	0	0	0	-1374	--	--	16.08	16.08	0.18	0.02	0.03	0.23	0.00	0.00	20.9
2	0	-0	2011	0	0	0	-650	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
3	0	-0	1946	0	0	0	-633	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
4	0	-0	3644	0	0	0	-1481	--	--	16.08	16.08	0.29	0.03	0.03	0.23	0.00	0.00	20.9
5	0	-0	3579	0	0	0	-1464	--	--	16.08	16.08	0.29	0.03	0.03	0.22	0.00	0.00	20.9
6	0	-0	2658	0	0	0	-961	--	--	16.08	16.08	0.29	0.02	0.02	0.17	0.00	0.00	20.9
7	0	-0	2441	0	0	0	-904	--	--	16.08	16.08	0.29	0.02	0.02	0.15	0.00	0.00	20.9
8	0	-0	3149	0	0	0	-1210	--	--	16.08	16.08	0.29	0.02	0.03	0.20	0.00	0.00	20.9
9	0	-0	2931	0	0	0	-1154	--	--	16.08	16.08	0.29	0.02	0.02	0.18	0.00	0.00	20.9
10	0	-0	2011	0	0	0	-650	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
11	0	-0	1946	0	0	0	-633	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
12	0	-0	3644	0	0	0	-1481	--	--	16.08	16.08	0.29	0.03	0.03	0.23	0.00	0.00	20.9
13	0	-0	3579	0	0	0	-1464	--	--	16.08	16.08	0.29	0.03	0.03	0.22	0.00	0.00	20.9
14	0	-0	2658	0	0	0	-961	--	--	16.08	16.08	0.29	0.02	0.02	0.17	0.00	0.00	20.9
15	0	-0	2441	0	0	0	-904	--	--	16.08	16.08	0.29	0.02	0.02	0.15	0.00	0.00	20.9
16	0	-0	3149	0	0	0	-1210	--	--	16.08	16.08	0.29	0.02	0.03	0.20	0.00	0.00	20.9

17	0	-0	2931	0	0	0	-1154	--	--	16.08	16.08	0.29	0.02	0.02	0.18	0.00	0.00	20.9
18	0	-0	4530	0	0	0	-1584	--	--	16.08	16.08	0.18	0.03	0.04	0.28	0.00	0.00	20.9
19	0	-0	10770	0	0	0	-4893	--	--	16.08	16.08	0.18	0.08	0.09	0.68	0.00	0.00	20.9
20	0	-0	6853	0	0	0	-2886	--	--	16.08	16.08	0.18	0.05	0.06	0.43	0.00	0.00	20.9
37	0	-0	1139	0	0	0	129	--	--	16.08	16.08	0.00	0.00	0.01	0.07	0.00	0.00	20.9
38	0	-0	11540	0	0	0	-5387	--	--	16.08	16.08	0.18	0.09	0.10	0.72	0.00	0.00	20.9
39	0	-0	5012	0	0	0	-2041	--	--	16.08	16.08	0.18	0.03	0.04	0.31	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	3633	0	0	0	-1374	--	--	16.08	16.08	0.18	0.02	0.03	0.23	0.00	0.00	20.9
2	27	-0	2011	0	0	0	-650	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
3	27	-0	1946	0	0	0	-633	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
4	27	-0	3644	0	0	0	-1481	--	--	16.08	16.08	0.29	0.03	0.03	0.23	0.00	0.00	20.9
5	27	-0	3579	0	0	0	-1464	--	--	16.08	16.08	0.29	0.03	0.03	0.22	0.00	0.00	20.9
6	27	-0	2658	0	0	0	-961	--	--	16.08	16.08	0.29	0.02	0.02	0.17	0.00	0.00	20.9
7	27	-0	2441	0	0	0	-904	--	--	16.08	16.08	0.29	0.02	0.02	0.15	0.00	0.00	20.9
8	27	-0	3149	0	0	0	-1210	--	--	16.08	16.08	0.29	0.02	0.03	0.20	0.00	0.00	20.9
9	27	-0	2931	0	0	0	-1154	--	--	16.08	16.08	0.29	0.02	0.02	0.18	0.00	0.00	20.9
10	27	-0	2011	0	0	0	-650	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
11	27	-0	1946	0	0	0	-633	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
12	27	-0	3644	0	0	0	-1481	--	--	16.08	16.08	0.29	0.03	0.03	0.23	0.00	0.00	20.9
13	27	-0	3579	0	0	0	-1464	--	--	16.08	16.08	0.29	0.03	0.03	0.22	0.00	0.00	20.9
14	27	-0	2658	0	0	0	-961	--	--	16.08	16.08	0.29	0.02	0.02	0.17	0.00	0.00	20.9
15	27	-0	2441	0	0	0	-904	--	--	16.08	16.08	0.29	0.02	0.02	0.15	0.00	0.00	20.9
16	27	-0	3149	0	0	0	-1210	--	--	16.08	16.08	0.29	0.02	0.03	0.20	0.00	0.00	20.9
17	27	-0	2931	0	0	0	-1154	--	--	16.08	16.08	0.29	0.02	0.02	0.18	0.00	0.00	20.9
18	27	-0	4530	0	0	0	-1584	--	--	16.08	16.08	0.18	0.03	0.04	0.28	0.00	0.00	20.9
19	27	-0	10770	0	0	0	-4893	--	--	16.08	16.08	0.18	0.08	0.09	0.68	0.00	0.00	20.9
20	27	-0	6853	0	0	0	-2886	--	--	16.08	16.08	0.18	0.05	0.06	0.43	0.00	0.00	20.9
37	27	-0	1139	0	0	0	1657	--	--	16.08	16.08	0.00	0.03	0.01	0.07	0.00	0.00	20.9
38	27	-0	11540	0	0	0	-5387	--	--	16.08	16.08	0.18	0.09	0.10	0.72	0.00	0.00	20.9
39	27	-0	5012	0	0	0	-2041	--	--	16.08	16.08	0.18	0.03	0.04	0.31	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	3633	0	0	0	608	--	--	16.08	16.08	0.00	0.01	0.03	0.23	0.00	0.00	20.9
2	55	-0	2011	0	0	0	447	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
3	55	-0	1946	0	0	0	428	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
4	55	-0	3644	0	0	0	507	--	--	16.08	16.08	0.10	0.01	0.03	0.23	0.00	0.00	20.9
5	55	-0	3579	0	0	0	488	--	--	16.08	16.08	0.10	0.01	0.03	0.22	0.00	0.00	20.9
6	55	-0	2658	0	0	0	490	--	--	16.08	16.08	0.10	0.01	0.02	0.17	0.00	0.00	20.9
7	55	-0	2441	0	0	0	428	--	--	16.08	16.08	0.10	0.01	0.02	0.15	0.00	0.00	20.9
8	55	-0	3149	0	0	0	508	--	--	16.08	16.08	0.10	0.01	0.03	0.20	0.00	0.00	20.9
9	55	-0	2931	0	0	0	446	--	--	16.08	16.08	0.10	0.01	0.02	0.18	0.00	0.00	20.9
10	55	-0	2011	0	0	0	447	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
11	55	-0	1946	0	0	0	428	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
12	55	-0	3644	0	0	0	507	--	--	16.08	16.08	0.10	0.01	0.03	0.23	0.00	0.00	20.9
13	55	-0	3579	0	0	0	488	--	--	16.08	16.08	0.10	0.01	0.03	0.22	0.00	0.00	20.9
14	55	-0	2658	0	0	0	490	--	--	16.08	16.08	0.10	0.01	0.02	0.17	0.00	0.00	20.9
15	55	-0	2441	0	0	0	428	--	--	16.08	16.08	0.10	0.01	0.02	0.15	0.00	0.00	20.9
16	55	-0	3149	0	0	0	508	--	--	16.08	16.08	0.10	0.01	0.03	0.20	0.00	0.00	20.9
17	55	-0	2931	0	0	0	446	--	--	16.08	16.08	0.10	0.01	0.02	0.18	0.00	0.00	20.9
18	55	-0	4530	0	0	0	887	--	--	16.08	16.08	0.00	0.02	0.04	0.28	0.00	0.00	20.9
19	55	-0	10770	0	0	0	981	--	--	16.08	16.08	0.00	0.02	0.09	0.68	0.00	0.00	20.9
20	55	-0	6853	0	0	0	853	--	--	16.08	16.08	0.00	0.01	0.06	0.43	0.00	0.00	20.9
37	55	-0	1139	0	0	0	750	--	--	16.08	16.08	0.00	0.01	0.01	0.07	0.00	0.00	20.9
38	55	-0	11540	0	0	0	907	--	--	16.08	16.08	0.00	0.02	0.10	0.72	0.00	0.00	20.9
39	55	-0	5012	0	0	0	693	--	--	16.08	16.08	0.00	0.01	0.04	0.31	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 34 NI 1730 NF 1582 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-3614	0	0	0	609	--	--	16.08	16.08	0.00	0.01	0.03	0.23	0.00	0.00	20.9
2	0	-0	-1940	0	0	0	437	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
3	0	-0	-1965	0	0	0	445	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
4	0	-0	-3595	0	0	0	491	--	--	16.08	16.08	0.10	0.01	0.03	0.23	0.00	0.00	20.9
5	0	-0	-3620	0	0	0	500	--	--	16.08	16.08	0.10	0.01	0.03	0.23	0.00	0.00	20.9
6	0	-0	-2490	0	0	0	446	--	--	16.08	16.08	0.10	0.01	0.02	0.16	0.00	0.00	20.9
7	0	-0	-2573	0	0	0	474	--	--	16.08	16.08	0.10	0.01	0.02	0.16	0.00	0.00	20.9
8	0	-0	-2986	0	0	0	463	--	--	16.08	16.08	0.10	0.01	0.02	0.19	0.00	0.00	20.9
9	0	-0	-3070	0	0	0	490	--	--	16.08	16.08	0.10	0.01	0.03	0.19	0.00	0.00	20.9
10	0	-0	-1940	0	0	0	437	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
11	0	-0	-1965	0	0	0	445	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
12	0	-0	-3595	0	0	0	491	--	--	16.08	16.08	0.10	0.01	0.03	0.23	0.00	0.00	20.9
13	0	-0	-3620	0	0	0	500	--	--	16.08	16.08	0.10	0.01	0.03	0.23	0.00	0.00	20.9
14	0	-0	-2490	0	0	0	446	--	--	16.08	16.08	0.10	0.01	0.02	0.16	0.00	0.00	20.9
15	0	-0	-2573	0	0	0	474	--	--	16.08	16.08	0.10	0.01	0.02	0.16	0.00	0.00	20.9
16	0	-0	-2986	0	0	0	463	--	--	16.08	16.08	0.10	0.01	0.02	0.19	0.00	0.00	20.9
17	0	-0	-3070	0	0	0	490	--	--	16.08	16.08	0.10	0.01	0.03	0.19	0.00	0.00	20.9
18	0	-0	-4449	0	0	0	888	--	--	16.08	16.08	0.00	0.02	0.04	0.28	0.00	0.00	20.9
19	0	-0	-10730	0	0	0	961	--	--	16.08	16.08	0.00	0.02	0.09	0.67	0.00	0.00	20.9
20	0	-0	-7101	0	0	0	940	--	--	16.08	16.08	0.00	0.02	0.06	0.45	0.00	0.00	20.9
37	0	-0	-1059	0	0	0	762	--	--	16.08	16.08	0.00	0.01	0.01	0.07	0.00	0.00	20.9
38	0	-0	-11520	0	0	0	883	--	--	16.08	16.08	0.00	0.02	0.09	0.72	0.00	0.00	20.9
39	0	-0	-5480	0	0	0	848	--	--	16.08	16.08	0.00	0.01	0.05	0.34	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-3614	0	0	0	-1363	--	--	16.08	16.08	0.18	0.02	0.03	0.23	0.00	0.00	20.9
2	27	-0	-1940	0	0	0	-621	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
3	27	-0	-1965	0	0	0	-627	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
4	27	-0	-3595	0	0	0	-1470	--	--	16.08	16.08	0.29	0.03	0.03	0.23	0.00	0.00	20.9
5	27	-0	-3620	0	0	0	-1475	--	--	16.08	16.08	0.29	0.03	0.03	0.23	0.00	0.00	20.9
6	27	-0	-2490	0	0	0	-912	--	--	16.08	16.08	0.29	0.02	0.02	0.16	0.00	0.00	20.9
7	27	-0	-2573	0	0	0	-930	--	--	16.08	16.08	0.29	0.02	0.02	0.16	0.00	0.00	20.9
8	27	-0	-2986	0	0	0	-1166	--	--	16.08	16.08	0.29	0.02	0.02	0.19	0.00	0.00	20.9
9	27	-0	-3070	0	0	0	-1184	--	--	16.08	16.08	0.29	0.02	0.03	0.19	0.00	0.00	20.9
10	27	-0	-1940	0	0	0	-621	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
11	27	-0	-1965	0	0	0	-627	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
12	27	-0	-3595	0	0	0	-1470	--	--	16.08	16.08	0.29	0.03	0.03	0.23	0.00	0.00	20.9

13	27	-0	-3620	0	0	0	-1475	--	--	16.08	16.08	0.29	0.03	0.03	0.23	0.00	0.00	20.9
14	27	-0	-2490	0	0	0	-912	--	--	16.08	16.08	0.29	0.02	0.02	0.16	0.00	0.00	20.9
15	27	-0	-2573	0	0	0	-930	--	--	16.08	16.08	0.29	0.02	0.02	0.16	0.00	0.00	20.9
16	27	-0	-2986	0	0	0	-1166	--	--	16.08	16.08	0.29	0.02	0.02	0.19	0.00	0.00	20.9
17	27	-0	-3070	0	0	0	-1184	--	--	16.08	16.08	0.29	0.02	0.03	0.19	0.00	0.00	20.9
18	27	-0	-4449	0	0	0	-1538	--	--	16.08	16.08	0.18	0.03	0.04	0.28	0.00	0.00	20.9
19	27	-0	-10730	0	0	0	-4891	--	--	16.08	16.08	0.18	0.08	0.09	0.67	0.00	0.00	20.9
20	27	-0	-7101	0	0	0	-2934	--	--	16.08	16.08	0.18	0.05	0.06	0.45	0.00	0.00	20.9
37	27	-0	-1059	0	0	0	762	--	--	16.08	16.08	0.00	0.01	0.01	0.07	0.00	0.00	20.9
38	27	-0	-11520	0	0	0	-5403	--	--	16.08	16.08	0.18	0.09	0.09	0.72	0.00	0.00	20.9
39	27	-0	-5480	0	0	0	-2141	--	--	16.08	16.08	0.18	0.04	0.05	0.34	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	-3614	0	0	0	-1363	--	--	16.08	16.08	0.18	0.02	0.03	0.23	0.00	0.00	20.9
2	55	-0	-1940	0	0	0	-621	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
3	55	-0	-1965	0	0	0	-627	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
4	55	-0	-3595	0	0	0	-1470	--	--	16.08	16.08	0.29	0.03	0.03	0.23	0.00	0.00	20.9
5	55	-0	-3620	0	0	0	-1475	--	--	16.08	16.08	0.29	0.03	0.03	0.23	0.00	0.00	20.9
6	55	-0	-2490	0	0	0	-912	--	--	16.08	16.08	0.29	0.02	0.02	0.16	0.00	0.00	20.9
7	55	-0	-2573	0	0	0	-930	--	--	16.08	16.08	0.29	0.02	0.02	0.16	0.00	0.00	20.9
8	55	-0	-2986	0	0	0	-1166	--	--	16.08	16.08	0.29	0.02	0.02	0.19	0.00	0.00	20.9
9	55	-0	-3070	0	0	0	-1184	--	--	16.08	16.08	0.29	0.02	0.03	0.19	0.00	0.00	20.9
10	55	-0	-1940	0	0	0	-621	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
11	55	-0	-1965	0	0	0	-627	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
12	55	-0	-3595	0	0	0	-1470	--	--	16.08	16.08	0.29	0.03	0.03	0.23	0.00	0.00	20.9
13	55	-0	-3620	0	0	0	-1475	--	--	16.08	16.08	0.29	0.03	0.03	0.23	0.00	0.00	20.9
14	55	-0	-2490	0	0	0	-912	--	--	16.08	16.08	0.29	0.02	0.02	0.16	0.00	0.00	20.9
15	55	-0	-2573	0	0	0	-930	--	--	16.08	16.08	0.29	0.02	0.02	0.16	0.00	0.00	20.9
16	55	-0	-2986	0	0	0	-1166	--	--	16.08	16.08	0.29	0.02	0.02	0.19	0.00	0.00	20.9
17	55	-0	-3070	0	0	0	-1184	--	--	16.08	16.08	0.29	0.02	0.03	0.19	0.00	0.00	20.9
18	55	-0	-4449	0	0	0	-1538	--	--	16.08	16.08	0.18	0.03	0.04	0.28	0.00	0.00	20.9
19	55	-0	-10730	0	0	0	-4891	--	--	16.08	16.08	0.18	0.08	0.09	0.67	0.00	0.00	20.9
20	55	-0	-7101	0	0	0	-2934	--	--	16.08	16.08	0.18	0.05	0.06	0.45	0.00	0.00	20.9
37	55	-0	-1059	0	0	0	184	--	--	16.08	16.08	0.00	0.00	0.01	0.07	0.00	0.00	20.9
38	55	-0	-11520	0	0	0	-5403	--	--	16.08	16.08	0.18	0.09	0.09	0.72	0.00	0.00	20.9
39	55	-0	-5480	0	0	0	-2141	--	--	16.08	16.08	0.18	0.04	0.05	0.34	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 35 NI 1726 NF 1730 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	2367	0	0	0	141	--	--	16.08	16.08	0.00	0.00	0.02	0.15	0.00	0.00	20.9
2	0	-0	1934	0	0	0	61	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
3	0	-0	1913	0	0	0	63	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
4	0	-0	1728	0	0	0	154	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
5	0	-0	1707	0	0	0	156	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
6	0	-0	1887	0	0	0	92	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
7	0	-0	1815	0	0	0	97	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
8	0	-0	1826	0	0	0	119	--	--	16.08	16.08	0.10	0.00	0.02	0.11	0.00	0.00	20.9
9	0	-0	1754	0	0	0	125	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
10	0	-0	1934	0	0	0	61	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
11	0	-0	1913	0	0	0	63	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
12	0	-0	1728	0	0	0	154	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
13	0	-0	1707	0	0	0	156	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
14	0	-0	1887	0	0	0	92	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
15	0	-0	1815	0	0	0	97	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
16	0	-0	1826	0	0	0	119	--	--	16.08	16.08	0.10	0.00	0.02	0.11	0.00	0.00	20.9
17	0	-0	1754	0	0	0	125	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
18	0	-0	3741	0	0	0	133	--	--	16.08	16.08	0.00	0.00	0.03	0.23	0.00	0.00	20.9
19	0	-0	2077	0	0	0	553	--	--	16.08	16.08	0.00	0.01	0.02	0.13	0.00	0.00	20.9
20	0	-0	2739	0	0	0	361	--	--	16.08	16.08	0.00	0.01	0.02	0.17	0.00	0.00	20.9
37	0	-0	4125	0	0	0	-73	--	--	16.08	16.08	0.18	0.00	0.03	0.26	0.00	0.00	20.9
38	0	-0	1352	0	0	0	627	--	--	16.08	16.08	0.00	0.01	0.01	0.08	0.00	0.00	20.9
39	0	-0	2457	0	0	0	307	--	--	16.08	16.08	0.00	0.01	0.02	0.15	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	2367	0	0	0	3316	--	--	16.08	16.08	0.00	0.06	0.02	0.15	0.00	0.00	20.9
2	27	-0	1934	0	0	0	2656	--	--	16.08	16.08	0.10	0.05	0.02	0.12	0.00	0.00	20.9
3	27	-0	1913	0	0	0	2629	--	--	16.08	16.08	0.10	0.05	0.02	0.12	0.00	0.00	20.9
4	27	-0	1728	0	0	0	2472	--	--	16.08	16.08	0.10	0.04	0.01	0.11	0.00	0.00	20.9
5	27	-0	1707	0	0	0	2446	--	--	16.08	16.08	0.10	0.04	0.01	0.11	0.00	0.00	20.9
6	27	-0	1887	0	0	0	2623	--	--	16.08	16.08	0.10	0.05	0.02	0.12	0.00	0.00	20.9
7	27	-0	1815	0	0	0	2533	--	--	16.08	16.08	0.10	0.04	0.01	0.11	0.00	0.00	20.9
8	27	-0	1826	0	0	0	2569	--	--	16.08	16.08	0.10	0.05	0.02	0.11	0.00	0.00	20.9
9	27	-0	1754	0	0	0	2478	--	--	16.08	16.08	0.10	0.04	0.01	0.11	0.00	0.00	20.9
10	27	-0	1934	0	0	0	2656	--	--	16.08	16.08	0.10	0.05	0.02	0.12	0.00	0.00	20.9
11	27	-0	1913	0	0	0	2629	--	--	16.08	16.08	0.10	0.05	0.02	0.12	0.00	0.00	20.9
12	27	-0	1728	0	0	0	2472	--	--	16.08	16.08	0.10	0.04	0.01	0.11	0.00	0.00	20.9
13	27	-0	1707	0	0	0	2446	--	--	16.08	16.08	0.10	0.04	0.01	0.11	0.00	0.00	20.9
14	27	-0	1887	0	0	0	2623	--	--	16.08	16.08	0.10	0.05	0.02	0.12	0.00	0.00	20.9
15	27	-0	1815	0	0	0	2533	--	--	16.08	16.08	0.10	0.04	0.01	0.11	0.00	0.00	20.9
16	27	-0	1826	0	0	0	2569	--	--	16.08	16.08	0.10	0.05	0.02	0.11	0.00	0.00	20.9
17	27	-0	1754	0	0	0	2478	--	--	16.08	16.08	0.10	0.04	0.01	0.11	0.00	0.00	20.9
18	27	-0	3741	0	0	0	5152	--	--	16.08	16.08	0.00	0.09	0.03	0.23	0.00	0.00	20.9
19	27	-0	2077	0	0	0	3339	--	--	16.08	16.08	0.00	0.06	0.02	0.13	0.00	0.00	20.9
20	27	-0	2739	0	0	0	4035	--	--	16.08	16.08	0.00	0.07	0.02	0.17	0.00	0.00	20.9
37	27	-0	4125	0	0	0	5461	--	--	16.08	16.08	0.00	0.09	0.03	0.26	0.00	0.00	20.9
38	27	-0	1352	0	0	0	2440	--	--	16.08	16.08	0.00	0.04	0.01	0.08	0.00	0.00	20.9
39	27	-0	2457	0	0	0	3602	--	--	16.08	16.08	0.00	0.06	0.02	0.15	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	2367	0	0	0	1432	--	--	16.08	16.08	0.00	0.02	0.02	0.15	0.00	0.00	20.9
2	55	-0	1934	0	0	0	1116	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
3	55	-0	1913	0	0	0	1106	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
4	55	-0	1728	0	0	0	1097	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
5	55	-0	1707	0	0	0	1087	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
6	55	-0	1887	0	0	0	1121	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
7	55	-0	1815	0	0	0	1088	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
8	55	-0	1826	0	0	0	1115	--	--	16.08	16.08	0.10	0.02	0.02	0.11	0.00	0.00	20.9

9	55	-0	1754	0	0	0	1082	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
10	55	-0	1934	0	0	0	1116	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
11	55	-0	1913	0	0	0	1106	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
12	55	-0	1728	0	0	0	1097	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
13	55	-0	1707	0	0	0	1087	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
14	55	-0	1887	0	0	0	1121	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
15	55	-0	1815	0	0	0	1088	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
16	55	-0	1826	0	0	0	1115	--	--	16.08	16.08	0.10	0.02	0.02	0.11	0.00	0.00	20.9
17	55	-0	1754	0	0	0	1082	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
18	55	-0	3741	0	0	0	2174	--	--	16.08	16.08	0.00	0.04	0.03	0.23	0.00	0.00	20.9
19	55	-0	2077	0	0	0	1686	--	--	16.08	16.08	0.00	0.03	0.02	0.13	0.00	0.00	20.9
20	55	-0	2739	0	0	0	1855	--	--	16.08	16.08	0.00	0.03	0.02	0.17	0.00	0.00	20.9
37	55	-0	4125	0	0	0	2177	--	--	16.08	16.08	0.00	0.04	0.03	0.26	0.00	0.00	20.9
38	55	-0	1352	0	0	0	1364	--	--	16.08	16.08	0.00	0.02	0.01	0.08	0.00	0.00	20.9
39	55	-0	2457	0	0	0	1646	--	--	16.08	16.08	0.00	0.03	0.02	0.15	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 36 NI 1727 NF 1726 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	2634	0	0	0	-224	--	--	16.08	16.08	0.18	0.00	0.02	0.17	0.00	0.00	20.9
2	0	-0	2005	0	0	0	-226	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
3	0	-0	2017	0	0	0	-221	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
4	0	-0	2035	0	0	0	-123	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
5	0	-0	2046	0	0	0	-118	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
6	0	-0	2002	0	0	0	-196	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
7	0	-0	2041	0	0	0	-178	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
8	0	-0	2011	0	0	0	-166	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
9	0	-0	2050	0	0	0	-148	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
10	0	-0	2005	0	0	0	-226	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
11	0	-0	2017	0	0	0	-221	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
12	0	-0	2035	0	0	0	-123	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
13	0	-0	2046	0	0	0	-118	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
14	0	-0	2002	0	0	0	-196	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
15	0	-0	2041	0	0	0	-178	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
16	0	-0	2011	0	0	0	-166	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
17	0	-0	2050	0	0	0	-148	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
18	0	-0	3992	0	0	0	-415	--	--	16.08	16.08	0.18	0.01	0.03	0.25	0.00	0.00	20.9
19	0	-0	3278	0	0	0	143	--	--	16.08	16.08	0.00	0.00	0.03	0.21	0.00	0.00	20.9
20	0	-0	3498	0	0	0	-86	--	--	16.08	16.08	0.18	0.00	0.03	0.22	0.00	0.00	20.9
37	0	-0	3909	0	0	0	-631	--	--	16.08	16.08	0.18	0.01	0.03	0.25	0.00	0.00	20.9
38	0	-0	2720	0	0	0	299	--	--	16.08	16.08	0.00	0.01	0.02	0.17	0.00	0.00	20.9
39	0	-0	3086	0	0	0	-83	--	--	16.08	16.08	0.18	0.00	0.03	0.19	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	2634	0	0	0	3310	--	--	16.08	16.08	0.00	0.06	0.02	0.17	0.00	0.00	20.9
2	27	-0	2005	0	0	0	2464	--	--	16.08	16.08	0.10	0.04	0.02	0.13	0.00	0.00	20.9
3	27	-0	2017	0	0	0	2485	--	--	16.08	16.08	0.10	0.04	0.02	0.13	0.00	0.00	20.9
4	27	-0	2035	0	0	0	2606	--	--	16.08	16.08	0.10	0.05	0.02	0.13	0.00	0.00	20.9
5	27	-0	2046	0	0	0	2627	--	--	16.08	16.08	0.10	0.05	0.02	0.13	0.00	0.00	20.9
6	27	-0	2002	0	0	0	2489	--	--	16.08	16.08	0.10	0.04	0.02	0.13	0.00	0.00	20.9
7	27	-0	2041	0	0	0	2560	--	--	16.08	16.08	0.10	0.05	0.02	0.13	0.00	0.00	20.9
8	27	-0	2011	0	0	0	2532	--	--	16.08	16.08	0.10	0.04	0.02	0.13	0.00	0.00	20.9
9	27	-0	2050	0	0	0	2602	--	--	16.08	16.08	0.10	0.05	0.02	0.13	0.00	0.00	20.9
10	27	-0	2005	0	0	0	2464	--	--	16.08	16.08	0.10	0.04	0.02	0.13	0.00	0.00	20.9
11	27	-0	2017	0	0	0	2485	--	--	16.08	16.08	0.10	0.04	0.02	0.13	0.00	0.00	20.9
12	27	-0	2035	0	0	0	2606	--	--	16.08	16.08	0.10	0.05	0.02	0.13	0.00	0.00	20.9
13	27	-0	2046	0	0	0	2627	--	--	16.08	16.08	0.10	0.05	0.02	0.13	0.00	0.00	20.9
14	27	-0	2002	0	0	0	2489	--	--	16.08	16.08	0.10	0.04	0.02	0.13	0.00	0.00	20.9
15	27	-0	2041	0	0	0	2560	--	--	16.08	16.08	0.10	0.05	0.02	0.13	0.00	0.00	20.9
16	27	-0	2011	0	0	0	2532	--	--	16.08	16.08	0.10	0.04	0.02	0.13	0.00	0.00	20.9
17	27	-0	2050	0	0	0	2602	--	--	16.08	16.08	0.10	0.05	0.02	0.13	0.00	0.00	20.9
18	27	-0	3992	0	0	0	4940	--	--	16.08	16.08	0.00	0.08	0.03	0.25	0.00	0.00	20.9
19	27	-0	3278	0	0	0	4540	--	--	16.08	16.08	0.00	0.08	0.03	0.21	0.00	0.00	20.9
20	27	-0	3498	0	0	0	4606	--	--	16.08	16.08	0.00	0.08	0.03	0.22	0.00	0.00	20.9
37	27	-0	3909	0	0	0	4613	--	--	16.08	16.08	0.00	0.08	0.03	0.25	0.00	0.00	20.9
38	27	-0	2720	0	0	0	3948	--	--	16.08	16.08	0.00	0.07	0.02	0.17	0.00	0.00	20.9
39	27	-0	3086	0	0	0	4057	--	--	16.08	16.08	0.00	0.07	0.03	0.19	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	2634	0	0	0	1213	--	--	16.08	16.08	0.00	0.02	0.02	0.17	0.00	0.00	20.9
2	55	-0	2005	0	0	0	868	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
3	55	-0	2017	0	0	0	879	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
4	55	-0	2035	0	0	0	986	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
5	55	-0	2046	0	0	0	998	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
6	55	-0	2002	0	0	0	896	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
7	55	-0	2041	0	0	0	935	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
8	55	-0	2011	0	0	0	931	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
9	55	-0	2050	0	0	0	970	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
10	55	-0	2005	0	0	0	868	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
11	55	-0	2017	0	0	0	879	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
12	55	-0	2035	0	0	0	986	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
13	55	-0	2046	0	0	0	998	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
14	55	-0	2002	0	0	0	896	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
15	55	-0	2041	0	0	0	935	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
16	55	-0	2011	0	0	0	931	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
17	55	-0	2050	0	0	0	970	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
18	55	-0	3992	0	0	0	1763	--	--	16.08	16.08	0.00	0.03	0.03	0.25	0.00	0.00	20.9
19	55	-0	3278	0	0	0	1931	--	--	16.08	16.08	0.00	0.03	0.03	0.21	0.00	0.00	20.9
20	55	-0	3498	0	0	0	1822	--	--	16.08	16.08	0.00	0.03	0.03	0.22	0.00	0.00	20.9
37	55	-0	3909	0	0	0	1502	--	--	16.08	16.08	0.00	0.03	0.03	0.25	0.00	0.00	20.9
38	55	-0	2720	0	0	0	1783	--	--	16.08	16.08	0.00	0.03	0.02	0.17	0.00	0.00	20.9
39	55	-0	3086	0	0	0	1600	--	--	16.08	16.08	0.00	0.03	0.03	0.19	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 37 NI 1722 NF 1727 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m			cm
1	0	-0	1397	0	0	0	-542	--	--	16.08	16.08	0.18	0.01	0.01	0.09	0.00	0.00	20.9
2	0	-0	1084	0	0	0	-456	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
3	0	-0	1105	0	0	0	-452	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
4	0	-0	1044	0	0	0	-382	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
5	0	-0	1066	0	0	0	-378	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
6	0	-0	1044	0	0	0	-435	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
7	0	-0	1117	0	0	0	-421	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
8	0	-0	1033	0	0	0	-413	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
9	0	-0	1105	0	0	0	-399	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
10	0	-0	1084	0	0	0	-456	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
11	0	-0	1105	0	0	0	-452	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
12	0	-0	1044	0	0	0	-382	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
13	0	-0	1066	0	0	0	-378	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
14	0	-0	1044	0	0	0	-435	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
15	0	-0	1117	0	0	0	-421	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
16	0	-0	1033	0	0	0	-413	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
17	0	-0	1105	0	0	0	-399	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
18	0	-0	2129	0	0	0	-877	--	--	16.08	16.08	0.18	0.01	0.02	0.13	0.00	0.00	20.9
19	0	-0	1524	0	0	0	-355	--	--	16.08	16.08	0.18	0.01	0.01	0.10	0.00	0.00	20.9
20	0	-0	1806	0	0	0	-543	--	--	16.08	16.08	0.18	0.01	0.01	0.11	0.00	0.00	20.9
37	0	-0	2195	0	0	0	-1029	--	--	16.08	16.08	0.18	0.02	0.02	0.14	0.00	0.00	20.9
38	0	-0	1186	0	0	0	-158	--	--	16.08	16.08	0.18	0.00	0.01	0.07	0.00	0.00	20.9
39	0	-0	1657	0	0	0	-472	--	--	16.08	16.08	0.18	0.01	0.01	0.10	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	1397	0	0	0	-542	--	--	16.08	16.08	0.18	0.01	0.01	0.09	0.00	0.00	20.9
2	27	-0	1084	0	0	0	-456	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
3	27	-0	1105	0	0	0	-452	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
4	27	-0	1044	0	0	0	-382	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
5	27	-0	1066	0	0	0	-378	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
6	27	-0	1044	0	0	0	-435	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
7	27	-0	1117	0	0	0	-421	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
8	27	-0	1033	0	0	0	-413	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
9	27	-0	1105	0	0	0	-399	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
10	27	-0	1084	0	0	0	-456	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
11	27	-0	1105	0	0	0	-452	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
12	27	-0	1044	0	0	0	-382	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
13	27	-0	1066	0	0	0	-378	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
14	27	-0	1044	0	0	0	-435	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
15	27	-0	1117	0	0	0	-421	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
16	27	-0	1033	0	0	0	-413	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
17	27	-0	1105	0	0	0	-399	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
18	27	-0	2129	0	0	0	-877	--	--	16.08	16.08	0.18	0.01	0.02	0.13	0.00	0.00	20.9
19	27	-0	1524	0	0	0	1690	--	--	16.08	16.08	0.00	0.03	0.01	0.10	0.00	0.00	20.9
20	27	-0	1806	0	0	0	-543	--	--	16.08	16.08	0.18	0.01	0.01	0.11	0.00	0.00	20.9
37	27	-0	2195	0	0	0	-1029	--	--	16.08	16.08	0.18	0.02	0.02	0.14	0.00	0.00	20.9
38	27	-0	1186	0	0	0	1433	--	--	16.08	16.08	0.00	0.02	0.01	0.07	0.00	0.00	20.9
39	27	-0	1657	0	0	0	-472	--	--	16.08	16.08	0.18	0.01	0.01	0.10	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	1397	0	0	0	220	--	--	16.08	16.08	0.00	0.00	0.01	0.09	0.00	0.00	20.9
2	55	-0	1084	0	0	0	135	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
3	55	-0	1105	0	0	0	151	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
4	55	-0	1044	0	0	0	187	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
5	55	-0	1066	0	0	0	203	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
6	55	-0	1044	0	0	0	135	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
7	55	-0	1117	0	0	0	188	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
8	55	-0	1033	0	0	0	150	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
9	55	-0	1105	0	0	0	204	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
10	55	-0	1084	0	0	0	135	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
11	55	-0	1105	0	0	0	151	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
12	55	-0	1044	0	0	0	187	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
13	55	-0	1066	0	0	0	203	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
14	55	-0	1044	0	0	0	135	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
15	55	-0	1117	0	0	0	188	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
16	55	-0	1033	0	0	0	150	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
17	55	-0	1105	0	0	0	204	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
18	55	-0	2129	0	0	0	284	--	--	16.08	16.08	0.00	0.00	0.02	0.13	0.00	0.00	20.9
19	55	-0	1524	0	0	0	477	--	--	16.08	16.08	0.00	0.01	0.01	0.10	0.00	0.00	20.9
20	55	-0	1806	0	0	0	443	--	--	16.08	16.08	0.00	0.01	0.01	0.11	0.00	0.00	20.9
37	55	-0	2195	0	0	0	168	--	--	16.08	16.08	0.00	0.00	0.02	0.14	0.00	0.00	20.9
38	55	-0	1186	0	0	0	488	--	--	16.08	16.08	0.00	0.01	0.01	0.07	0.00	0.00	20.9
39	55	-0	1657	0	0	0	432	--	--	16.08	16.08	0.00	0.01	0.01	0.10	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 38 NI 1728 NF 1722 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m			cm
1	0	-0	538	0	0	0	-595	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9
2	0	-0	422	0	0	0	-489	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
3	0	-0	444	0	0	0	-489	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
4	0	-0	384	0	0	0	-427	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
5	0	-0	406	0	0	0	-427	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
6	0	-0	382	0	0	0	-468	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
7	0	-0	457	0	0	0	-467	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
8	0	-0	371	0	0	0	-449	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
9	0	-0	446	0	0	0	-448	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
10	0	-0	422	0	0	0	-489	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
11	0	-0	444	0	0	0	-489	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
12	0	-0	384	0	0	0	-427	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
13	0	-0	406	0	0	0	-427	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
14	0	-0	382	0	0	0	-468	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
15	0	-0	457	0	0	0	-467	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
16	0	-0	371	0	0	0	-449	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9

17	0	-0	446	0	0	0	-448	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
18	0	-0	809	0	0	0	-942	--	--	16.08	16.08	0.18	0.02	0.01	0.05	0.00	0.00	20.9
19	0	-0	494	0	0	0	-464	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9
20	0	-0	684	0	0	0	-633	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
37	0	-0	879	0	0	0	-1068	--	--	16.08	16.08	0.18	0.02	0.01	0.06	0.00	0.00	20.9
38	0	-0	354	0	0	0	-271	--	--	16.08	16.08	0.18	0.00	0.00	0.02	0.00	0.00	20.9
39	0	-0	669	0	0	0	-553	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	538	0	0	0	-595	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9
2	27	-0	422	0	0	0	-489	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
3	27	-0	444	0	0	0	-489	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
4	27	-0	384	0	0	0	-427	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
5	27	-0	406	0	0	0	-427	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
6	27	-0	382	0	0	0	-468	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
7	27	-0	457	0	0	0	-467	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
8	27	-0	371	0	0	0	-449	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
9	27	-0	446	0	0	0	-448	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
10	27	-0	422	0	0	0	-489	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
11	27	-0	444	0	0	0	-489	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
12	27	-0	384	0	0	0	-427	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
13	27	-0	406	0	0	0	-427	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
14	27	-0	382	0	0	0	-468	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
15	27	-0	457	0	0	0	-467	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
16	27	-0	371	0	0	0	-449	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
17	27	-0	446	0	0	0	-448	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
18	27	-0	809	0	0	0	-942	--	--	16.08	16.08	0.18	0.02	0.01	0.05	0.00	0.00	20.9
19	27	-0	494	0	0	0	-464	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9
20	27	-0	684	0	0	0	-633	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
37	27	-0	879	0	0	0	-1068	--	--	16.08	16.08	0.18	0.02	0.01	0.06	0.00	0.00	20.9
38	27	-0	354	0	0	0	-271	--	--	16.08	16.08	0.18	0.00	0.00	0.02	0.00	0.00	20.9
39	27	-0	669	0	0	0	-553	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	538	0	0	0	-595	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9
2	55	-0	422	0	0	0	-489	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
3	55	-0	444	0	0	0	-489	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
4	55	-0	384	0	0	0	-427	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
5	55	-0	406	0	0	0	-427	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
6	55	-0	382	0	0	0	-468	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
7	55	-0	457	0	0	0	-467	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
8	55	-0	371	0	0	0	-449	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
9	55	-0	446	0	0	0	-448	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
10	55	-0	422	0	0	0	-489	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
11	55	-0	444	0	0	0	-489	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
12	55	-0	384	0	0	0	-427	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
13	55	-0	406	0	0	0	-427	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
14	55	-0	382	0	0	0	-468	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
15	55	-0	457	0	0	0	-467	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
16	55	-0	371	0	0	0	-449	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
17	55	-0	446	0	0	0	-448	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
18	55	-0	809	0	0	0	-942	--	--	16.08	16.08	0.18	0.02	0.01	0.05	0.00	0.00	20.9
19	55	-0	494	0	0	0	-464	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9
20	55	-0	684	0	0	0	-633	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
37	55	-0	879	0	0	0	-1068	--	--	16.08	16.08	0.18	0.02	0.01	0.06	0.00	0.00	20.9
38	55	-0	354	0	0	0	-271	--	--	16.08	16.08	0.18	0.00	0.00	0.02	0.00	0.00	20.9
39	55	-0	669	0	0	0	-553	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 39 NI 1729 NF 1728 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm

1	0	-0	-149	0	0	0	-551	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9
2	0	-0	-122	0	0	0	-453	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
3	0	-0	-100	0	0	0	-444	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
4	0	-0	-129	0	0	0	-404	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
5	0	-0	-107	0	0	0	-395	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
6	0	-0	-150	0	0	0	-445	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
7	0	-0	-76	0	0	0	-418	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
8	0	-0	-153	0	0	0	-430	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
9	0	-0	-78	0	0	0	-403	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
10	0	-0	-122	0	0	0	-453	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
11	0	-0	-100	0	0	0	-444	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
12	0	-0	-129	0	0	0	-404	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
13	0	-0	-107	0	0	0	-395	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
14	0	-0	-150	0	0	0	-445	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
15	0	-0	-76	0	0	0	-418	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
16	0	-0	-153	0	0	0	-430	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
17	0	-0	-78	0	0	0	-403	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
18	0	-0	-266	0	0	0	-881	--	--	16.08	16.08	0.18	0.01	0.00	0.02	0.00	0.00	20.9
19	0	-0	-209	0	0	0	-460	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9
20	0	-0	-172	0	0	0	-581	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9
37	0	-0	-256	0	0	0	-984	--	--	16.08	16.08	0.18	0.02	0.00	0.02	0.00	0.00	20.9
38	0	-0	-160	0	0	0	-283	--	--	16.08	16.08	0.18	0.00	0.00	0.01	0.00	0.00	20.9
39	0	-0	-100	0	0	0	-484	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-149	0	0	0	-551	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9
2	27	-0	-122	0	0	0	-453	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
3	27	-0	-100	0	0	0	-444	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
4	27	-0	-129	0	0	0	-404	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
5	27	-0	-107	0	0	0	-395	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
6	27	-0	-150	0	0	0	-445	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
7	27	-0	-76	0	0	0	-418	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
8	27	-0	-153	0	0	0	-430	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
9	27	-0	-78	0	0	0	-403	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
10	27	-0	-122	0	0	0	-453	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
11	27	-0	-100	0	0	0	-444	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
12	27	-0	-129	0	0	0	-404	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9

13	27	-0	-107	0	0	0	-395	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
14	27	-0	-150	0	0	0	-445	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
15	27	-0	-76	0	0	0	-418	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
16	27	-0	-153	0	0	0	-430	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
17	27	-0	-78	0	0	0	-403	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
18	27	-0	-266	0	0	0	-881	--	--	16.08	16.08	0.18	0.01	0.00	0.02	0.00	0.00	20.9
19	27	-0	-209	0	0	0	-460	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9
20	27	-0	-172	0	0	0	-581	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9
37	27	-0	-256	0	0	0	-984	--	--	16.08	16.08	0.18	0.02	0.00	0.02	0.00	0.00	20.9
38	27	-0	-160	0	0	0	-283	--	--	16.08	16.08	0.18	0.00	0.00	0.01	0.00	0.00	20.9
39	27	-0	-100	0	0	0	-484	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	-149	0	0	0	-551	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9
2	55	-0	-122	0	0	0	-453	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
3	55	-0	-100	0	0	0	-444	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
4	55	-0	-129	0	0	0	-404	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
5	55	-0	-107	0	0	0	-395	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
6	55	-0	-150	0	0	0	-445	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
7	55	-0	-76	0	0	0	-418	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
8	55	-0	-153	0	0	0	-430	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
9	55	-0	-78	0	0	0	-403	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
10	55	-0	-122	0	0	0	-453	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
11	55	-0	-100	0	0	0	-444	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
12	55	-0	-129	0	0	0	-404	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
13	55	-0	-107	0	0	0	-395	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
14	55	-0	-150	0	0	0	-445	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
15	55	-0	-76	0	0	0	-418	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
16	55	-0	-153	0	0	0	-430	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
17	55	-0	-78	0	0	0	-403	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
18	55	-0	-266	0	0	0	-881	--	--	16.08	16.08	0.18	0.01	0.00	0.02	0.00	0.00	20.9
19	55	-0	-209	0	0	0	-460	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9
20	55	-0	-172	0	0	0	-581	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9
37	55	-0	-256	0	0	0	-984	--	--	16.08	16.08	0.18	0.02	0.00	0.02	0.00	0.00	20.9
38	55	-0	-160	0	0	0	-283	--	--	16.08	16.08	0.18	0.00	0.00	0.01	0.00	0.00	20.9
39	55	-0	-100	0	0	0	-484	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 40 NI 1723 NF 1729 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-835	0	0	0	-622	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9
2	0	-0	-665	0	0	0	-511	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
3	0	-0	-643	0	0	0	-507	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
4	0	-0	-642	0	0	0	-451	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
5	0	-0	-619	0	0	0	-447	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
6	0	-0	-683	0	0	0	-494	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
7	0	-0	-608	0	0	0	-481	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
8	0	-0	-676	0	0	0	-476	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
9	0	-0	-601	0	0	0	-463	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
10	0	-0	-665	0	0	0	-511	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
11	0	-0	-643	0	0	0	-507	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
12	0	-0	-642	0	0	0	-451	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
13	0	-0	-619	0	0	0	-447	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
14	0	-0	-683	0	0	0	-494	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
15	0	-0	-608	0	0	0	-481	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
16	0	-0	-676	0	0	0	-476	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
17	0	-0	-601	0	0	0	-463	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
18	0	-0	-1340	0	0	0	-990	--	--	16.08	16.08	0.18	0.02	0.01	0.08	0.00	0.00	20.9
19	0	-0	-910	0	0	0	-503	--	--	16.08	16.08	0.18	0.01	0.01	0.06	0.00	0.00	20.9
20	0	-0	-1025	0	0	0	-665	--	--	16.08	16.08	0.18	0.01	0.01	0.06	0.00	0.00	20.9
37	0	-0	-1390	0	0	0	-1113	--	--	16.08	16.08	0.18	0.02	0.01	0.09	0.00	0.00	20.9
38	0	-0	-673	0	0	0	65	--	--	16.08	16.08	0.00	0.00	0.01	0.04	0.00	0.00	20.9
39	0	-0	-865	0	0	0	-572	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-835	0	0	0	-622	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9
2	27	-0	-665	0	0	0	-511	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
3	27	-0	-643	0	0	0	-507	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
4	27	-0	-642	0	0	0	-451	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
5	27	-0	-619	0	0	0	-447	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
6	27	-0	-683	0	0	0	-494	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
7	27	-0	-608	0	0	0	-481	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
8	27	-0	-676	0	0	0	-476	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
9	27	-0	-601	0	0	0	-463	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
10	27	-0	-665	0	0	0	-511	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
11	27	-0	-643	0	0	0	-507	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
12	27	-0	-642	0	0	0	-451	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
13	27	-0	-619	0	0	0	-447	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
14	27	-0	-683	0	0	0	-494	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
15	27	-0	-608	0	0	0	-481	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
16	27	-0	-676	0	0	0	-476	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
17	27	-0	-601	0	0	0	-463	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
18	27	-0	-1340	0	0	0	-990	--	--	16.08	16.08	0.18	0.02	0.01	0.08	0.00	0.00	20.9
19	27	-0	-910	0	0	0	-503	--	--	16.08	16.08	0.18	0.01	0.01	0.06	0.00	0.00	20.9
20	27	-0	-1025	0	0	0	-665	--	--	16.08	16.08	0.18	0.01	0.01	0.06	0.00	0.00	20.9
37	27	-0	-1390	0	0	0	-1113	--	--	16.08	16.08	0.18	0.02	0.01	0.09	0.00	0.00	20.9
38	27	-0	-673	0	0	0	-303	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
39	27	-0	-865	0	0	0	-572	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	-835	0	0	0	-622	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9
2	55	-0	-665	0	0	0	-511	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
3	55	-0	-643	0	0	0	-507	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
4	55	-0	-642	0	0	0	-451	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
5	55	-0	-619	0	0	0	-447	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
6	55	-0	-683	0	0	0	-494	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
7	55	-0	-608	0	0	0	-481	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
8	55	-0	-676	0	0	0	-476	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9

9	55	-0	-601	0	0	0	-463	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
10	55	-0	-665	0	0	0	-511	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
11	55	-0	-643	0	0	0	-507	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
12	55	-0	-642	0	0	0	-451	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
13	55	-0	-619	0	0	0	-447	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
14	55	-0	-683	0	0	0	-494	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
15	55	-0	-608	0	0	0	-481	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
16	55	-0	-676	0	0	0	-476	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
17	55	-0	-601	0	0	0	-463	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
18	55	-0	-1340	0	0	0	-990	--	--	16.08	16.08	0.18	0.02	0.01	0.08	0.00	0.00	20.9
19	55	-0	-910	0	0	0	-503	--	--	16.08	16.08	0.18	0.01	0.01	0.06	0.00	0.00	20.9
20	55	-0	-1025	0	0	0	-665	--	--	16.08	16.08	0.18	0.01	0.01	0.06	0.00	0.00	20.9
37	55	-0	-1390	0	0	0	-1113	--	--	16.08	16.08	0.18	0.02	0.01	0.09	0.00	0.00	20.9
38	55	-0	-673	0	0	0	-303	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
39	55	-0	-865	0	0	0	-572	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 41 NI 1724 NF 1723 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-1688	0	0	0	403	--	--	16.08	16.08	0.00	0.01	0.01	0.11	0.00	0.00	20.9
2	0	-0	-1322	0	0	0	287	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
3	0	-0	-1300	0	0	0	275	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
4	0	-0	-1297	0	0	0	345	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
5	0	-0	-1275	0	0	0	333	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
6	0	-0	-1339	0	0	0	321	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
7	0	-0	-1265	0	0	0	281	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
8	0	-0	-1331	0	0	0	339	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
9	0	-0	-1258	0	0	0	299	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
10	0	-0	-1322	0	0	0	287	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
11	0	-0	-1300	0	0	0	275	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
12	0	-0	-1297	0	0	0	345	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
13	0	-0	-1275	0	0	0	333	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
14	0	-0	-1339	0	0	0	321	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
15	0	-0	-1265	0	0	0	281	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
16	0	-0	-1331	0	0	0	339	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
17	0	-0	-1258	0	0	0	299	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
18	0	-0	-2648	0	0	0	614	--	--	16.08	16.08	0.00	0.01	0.02	0.17	0.00	0.00	20.9
19	0	-0	-1925	0	0	0	724	--	--	16.08	16.08	0.00	0.01	0.02	0.12	0.00	0.00	20.9
20	0	-0	-2136	0	0	0	650	--	--	16.08	16.08	0.00	0.01	0.02	0.13	0.00	0.00	20.9
37	0	-0	-2697	0	0	0	490	--	--	16.08	16.08	0.00	0.01	0.02	0.17	0.00	0.00	20.9
38	0	-0	-1492	0	0	0	675	--	--	16.08	16.08	0.00	0.01	0.01	0.09	0.00	0.00	20.9
39	0	-0	-1844	0	0	0	550	--	--	16.08	16.08	0.00	0.01	0.02	0.12	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-1688	0	0	0	-518	--	--	16.08	16.08	0.18	0.01	0.01	0.11	0.00	0.00	20.9
2	27	-0	-1322	0	0	0	-434	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
3	27	-0	-1300	0	0	0	-434	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
4	27	-0	-1297	0	0	0	-362	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
5	27	-0	-1275	0	0	0	-362	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
6	27	-0	-1339	0	0	0	-409	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
7	27	-0	-1265	0	0	0	-409	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
8	27	-0	-1331	0	0	0	-387	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
9	27	-0	-1258	0	0	0	-387	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
10	27	-0	-1322	0	0	0	-434	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
11	27	-0	-1300	0	0	0	-434	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
12	27	-0	-1297	0	0	0	-362	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
13	27	-0	-1275	0	0	0	-362	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
14	27	-0	-1339	0	0	0	-409	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
15	27	-0	-1265	0	0	0	-409	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
16	27	-0	-1331	0	0	0	-387	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
17	27	-0	-1258	0	0	0	-387	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
18	27	-0	-2648	0	0	0	-831	--	--	16.08	16.08	0.18	0.01	0.02	0.17	0.00	0.00	20.9
19	27	-0	-1925	0	0	0	724	--	--	16.08	16.08	0.00	0.01	0.02	0.12	0.00	0.00	20.9
20	27	-0	-2136	0	0	0	650	--	--	16.08	16.08	0.00	0.01	0.02	0.13	0.00	0.00	20.9
37	27	-0	-2697	0	0	0	-981	--	--	16.08	16.08	0.18	0.02	0.02	0.17	0.00	0.00	20.9
38	27	-0	-1492	0	0	0	675	--	--	16.08	16.08	0.00	0.01	0.01	0.09	0.00	0.00	20.9
39	27	-0	-1844	0	0	0	550	--	--	16.08	16.08	0.00	0.01	0.02	0.12	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	-1688	0	0	0	-518	--	--	16.08	16.08	0.18	0.01	0.01	0.11	0.00	0.00	20.9
2	55	-0	-1322	0	0	0	-434	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
3	55	-0	-1300	0	0	0	-434	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
4	55	-0	-1297	0	0	0	-362	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
5	55	-0	-1275	0	0	0	-362	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
6	55	-0	-1339	0	0	0	-409	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
7	55	-0	-1265	0	0	0	-409	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
8	55	-0	-1331	0	0	0	-387	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
9	55	-0	-1258	0	0	0	-387	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
10	55	-0	-1322	0	0	0	-434	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
11	55	-0	-1300	0	0	0	-434	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
12	55	-0	-1297	0	0	0	-362	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
13	55	-0	-1275	0	0	0	-362	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
14	55	-0	-1339	0	0	0	-409	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
15	55	-0	-1265	0	0	0	-409	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
16	55	-0	-1331	0	0	0	-387	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
17	55	-0	-1258	0	0	0	-387	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
18	55	-0	-2648	0	0	0	-831	--	--	16.08	16.08	0.18	0.01	0.02	0.17	0.00	0.00	20.9
19	55	-0	-1925	0	0	0	-325	--	--	16.08	16.08	0.18	0.01	0.02	0.12	0.00	0.00	20.9
20	55	-0	-2136	0	0	0	-515	--	--	16.08	16.08	0.18	0.01	0.02	0.13	0.00	0.00	20.9
37	55	-0	-2697	0	0	0	-981	--	--	16.08	16.08	0.18	0.02	0.02	0.17	0.00	0.00	20.9
38	55	-0	-1492	0	0	0	-139	--	--	16.08	16.08	0.18	0.00	0.01	0.09	0.00	0.00	20.9
39	55	-0	-1844	0	0	0	-455	--	--	16.08	16.08	0.18	0.01	0.02	0.12	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 42 NI 1725 NF 1724 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-2894	0	0	0	1423	--	--	16.08	16.08	0.00	0.02	0.02	0.18	0.00	0.00	20.9
2	0	-0	-2214	0	0	0	1038	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
3	0	-0	-2201	0	0	0	1030	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
4	0	-0	-2252	0	0	0	1160	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
5	0	-0	-2239	0	0	0	1151	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
6	0	-0	-2243	0	0	0	1092	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
7	0	-0	-2199	0	0	0	1062	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
8	0	-0	-2254	0	0	0	1128	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
9	0	-0	-2210	0	0	0	1098	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
10	0	-0	-2214	0	0	0	1038	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
11	0	-0	-2201	0	0	0	1030	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
12	0	-0	-2252	0	0	0	1160	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
13	0	-0	-2239	0	0	0	1151	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
14	0	-0	-2243	0	0	0	1092	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
15	0	-0	-2199	0	0	0	1062	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
16	0	-0	-2254	0	0	0	1128	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
17	0	-0	-2210	0	0	0	1098	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
18	0	-0	-4456	0	0	0	2142	--	--	16.08	16.08	0.00	0.04	0.04	0.28	0.00	0.00	20.9
19	0	-0	-3614	0	0	0	2194	--	--	16.08	16.08	0.00	0.04	0.03	0.23	0.00	0.00	20.9
20	0	-0	-3824	0	0	0	2086	--	--	16.08	16.08	0.00	0.04	0.03	0.24	0.00	0.00	20.9
37	0	-0	-4371	0	0	0	1884	--	--	16.08	16.08	0.00	0.03	0.04	0.27	0.00	0.00	20.9
38	0	-0	-2967	0	0	0	1970	--	--	16.08	16.08	0.00	0.03	0.02	0.19	0.00	0.00	20.9
39	0	-0	-3318	0	0	0	1791	--	--	16.08	16.08	0.00	0.03	0.03	0.21	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-2894	0	0	0	1423	--	--	16.08	16.08	0.00	0.02	0.02	0.18	0.00	0.00	20.9
2	27	-0	-2214	0	0	0	1038	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
3	27	-0	-2201	0	0	0	1030	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
4	27	-0	-2252	0	0	0	1160	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
5	27	-0	-2239	0	0	0	1151	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
6	27	-0	-2243	0	0	0	1092	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
7	27	-0	-2199	0	0	0	1062	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
8	27	-0	-2254	0	0	0	1128	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
9	27	-0	-2210	0	0	0	1098	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
10	27	-0	-2214	0	0	0	1038	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
11	27	-0	-2201	0	0	0	1030	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
12	27	-0	-2252	0	0	0	1160	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
13	27	-0	-2239	0	0	0	1151	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
14	27	-0	-2243	0	0	0	1092	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
15	27	-0	-2199	0	0	0	1062	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
16	27	-0	-2254	0	0	0	1128	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
17	27	-0	-2210	0	0	0	1098	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
18	27	-0	-4456	0	0	0	2142	--	--	16.08	16.08	0.00	0.04	0.04	0.28	0.00	0.00	20.9
19	27	-0	-3614	0	0	0	2194	--	--	16.08	16.08	0.00	0.04	0.03	0.23	0.00	0.00	20.9
20	27	-0	-3824	0	0	0	2086	--	--	16.08	16.08	0.00	0.04	0.03	0.24	0.00	0.00	20.9
37	27	-0	-4371	0	0	0	1884	--	--	16.08	16.08	0.00	0.03	0.04	0.27	0.00	0.00	20.9
38	27	-0	-2967	0	0	0	1970	--	--	16.08	16.08	0.00	0.03	0.02	0.19	0.00	0.00	20.9
39	27	-0	-3318	0	0	0	1791	--	--	16.08	16.08	0.00	0.03	0.03	0.21	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	-2894	0	0	0	-156	--	--	16.08	16.08	0.18	0.00	0.02	0.18	0.00	0.00	20.9
2	55	-0	-2214	0	0	0	-169	--	--	16.08	16.08	0.29	0.00	0.02	0.14	0.00	0.00	20.9
3	55	-0	-2201	0	0	0	-171	--	--	16.08	16.08	0.29	0.00	0.02	0.14	0.00	0.00	20.9
4	55	-0	-2252	0	0	0	-68	--	--	16.08	16.08	0.29	0.00	0.02	0.14	0.00	0.00	20.9
5	55	-0	-2239	0	0	0	-70	--	--	16.08	16.08	0.29	0.00	0.02	0.14	0.00	0.00	20.9
6	55	-0	-2243	0	0	0	-132	--	--	16.08	16.08	0.29	0.00	0.02	0.14	0.00	0.00	20.9
7	55	-0	-2199	0	0	0	-138	--	--	16.08	16.08	0.29	0.00	0.02	0.14	0.00	0.00	20.9
8	55	-0	-2254	0	0	0	-101	--	--	16.08	16.08	0.29	0.00	0.02	0.14	0.00	0.00	20.9
9	55	-0	-2210	0	0	0	-107	--	--	16.08	16.08	0.29	0.00	0.02	0.14	0.00	0.00	20.9
10	55	-0	-2214	0	0	0	-169	--	--	16.08	16.08	0.29	0.00	0.02	0.14	0.00	0.00	20.9
11	55	-0	-2201	0	0	0	-171	--	--	16.08	16.08	0.29	0.00	0.02	0.14	0.00	0.00	20.9
12	55	-0	-2252	0	0	0	-68	--	--	16.08	16.08	0.29	0.00	0.02	0.14	0.00	0.00	20.9
13	55	-0	-2239	0	0	0	-70	--	--	16.08	16.08	0.29	0.00	0.02	0.14	0.00	0.00	20.9
14	55	-0	-2243	0	0	0	-132	--	--	16.08	16.08	0.29	0.00	0.02	0.14	0.00	0.00	20.9
15	55	-0	-2199	0	0	0	-138	--	--	16.08	16.08	0.29	0.00	0.02	0.14	0.00	0.00	20.9
16	55	-0	-2254	0	0	0	-101	--	--	16.08	16.08	0.29	0.00	0.02	0.14	0.00	0.00	20.9
17	55	-0	-2210	0	0	0	-107	--	--	16.08	16.08	0.29	0.00	0.02	0.14	0.00	0.00	20.9
18	55	-0	-4456	0	0	0	-289	--	--	16.08	16.08	0.18	0.00	0.04	0.28	0.00	0.00	20.9
19	55	-0	-3614	0	0	0	222	--	--	16.08	16.08	0.00	0.00	0.03	0.23	0.00	0.00	20.9
20	55	-0	-3824	0	0	0	-0	--	--	16.08	16.08	0.18	0.00	0.03	0.24	0.00	0.00	20.9
37	55	-0	-4371	0	0	0	-500	--	--	16.08	16.08	0.18	0.01	0.04	0.27	0.00	0.00	20.9
38	55	-0	-2967	0	0	0	352	--	--	16.08	16.08	0.00	0.01	0.02	0.19	0.00	0.00	20.9
39	55	-0	-3318	0	0	0	-19	--	--	16.08	16.08	0.18	0.00	0.03	0.21	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 43 NI 1721 NF 1725 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-2656	0	0	0	1706	--	--	16.08	16.08	0.00	0.03	0.02	0.17	0.00	0.00	20.9
2	0	-0	-2112	0	0	0	1300	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
3	0	-0	-2136	0	0	0	1315	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
4	0	-0	-1950	0	0	0	1309	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
5	0	-0	-1974	0	0	0	1324	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
6	0	-0	-2027	0	0	0	1286	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
7	0	-0	-2107	0	0	0	1336	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
8	0	-0	-1979	0	0	0	1288	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
9	0	-0	-2059	0	0	0	1339	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
10	0	-0	-2112	0	0	0	1300	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
11	0	-0	-2136	0	0	0	1315	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
12	0	-0	-1950	0	0	0	1309	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
13	0	-0	-1974	0	0	0	1324	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
14	0	-0	-2027	0	0	0	1286	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
15	0	-0	-2107	0	0	0	1336	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
16	0	-0	-1979	0	0	0	1288	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9

17	0	-0	-2059	0	0	0	1339	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
18	0	-0	-4211	0	0	0	2637	--	--	16.08	16.08	0.00	0.04	0.03	0.26	0.00	0.00	20.9
19	0	-0	-2511	0	0	0	2071	--	--	16.08	16.08	0.00	0.04	0.02	0.16	0.00	0.00	20.9
20	0	-0	-3327	0	0	0	2362	--	--	16.08	16.08	0.00	0.04	0.03	0.21	0.00	0.00	20.9
37	0	-0	-4555	0	0	0	2618	--	--	16.08	16.08	0.00	0.04	0.04	0.29	0.00	0.00	20.9
38	0	-0	-1721	0	0	0	1674	--	--	16.08	16.08	0.00	0.03	0.01	0.11	0.00	0.00	20.9
39	0	-0	-3081	0	0	0	2159	--	--	16.08	16.08	0.00	0.04	0.03	0.19	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-2656	0	0	0	1706	--	--	16.08	16.08	0.00	0.03	0.02	0.17	0.00	0.00	20.9
2	27	-0	-2112	0	0	0	1300	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
3	27	-0	-2136	0	0	0	1315	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
4	27	-0	-1950	0	0	0	1309	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
5	27	-0	-1974	0	0	0	1324	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
6	27	-0	-2027	0	0	0	1286	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
7	27	-0	-2107	0	0	0	1336	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
8	27	-0	-1979	0	0	0	1288	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
9	27	-0	-2059	0	0	0	1339	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
10	27	-0	-2112	0	0	0	1300	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
11	27	-0	-2136	0	0	0	1315	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
12	27	-0	-1950	0	0	0	1309	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
13	27	-0	-1974	0	0	0	1324	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
14	27	-0	-2027	0	0	0	1286	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
15	27	-0	-2107	0	0	0	1336	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
16	27	-0	-1979	0	0	0	1288	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
17	27	-0	-2059	0	0	0	1339	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
18	27	-0	-4211	0	0	0	2637	--	--	16.08	16.08	0.00	0.04	0.03	0.26	0.00	0.00	20.9
19	27	-0	-2511	0	0	0	2071	--	--	16.08	16.08	0.00	0.04	0.02	0.16	0.00	0.00	20.9
20	27	-0	-3327	0	0	0	2362	--	--	16.08	16.08	0.00	0.04	0.03	0.21	0.00	0.00	20.9
37	27	-0	-4555	0	0	0	2618	--	--	16.08	16.08	0.00	0.04	0.04	0.29	0.00	0.00	20.9
38	27	-0	-1721	0	0	0	1674	--	--	16.08	16.08	0.00	0.03	0.01	0.11	0.00	0.00	20.9
39	27	-0	-3081	0	0	0	2159	--	--	16.08	16.08	0.00	0.04	0.03	0.19	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	-2656	0	0	0	257	--	--	16.08	16.08	0.00	0.00	0.02	0.17	0.00	0.00	20.9
2	55	-0	-2112	0	0	0	148	--	--	16.08	16.08	0.10	0.00	0.02	0.13	0.00	0.00	20.9
3	55	-0	-2136	0	0	0	150	--	--	16.08	16.08	0.10	0.00	0.02	0.13	0.00	0.00	20.9
4	55	-0	-1950	0	0	0	246	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
5	55	-0	-1974	0	0	0	248	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
6	55	-0	-2027	0	0	0	180	--	--	16.08	16.08	0.10	0.00	0.02	0.13	0.00	0.00	20.9
7	55	-0	-2107	0	0	0	187	--	--	16.08	16.08	0.10	0.00	0.02	0.13	0.00	0.00	20.9
8	55	-0	-1979	0	0	0	209	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
9	55	-0	-2059	0	0	0	216	--	--	16.08	16.08	0.10	0.00	0.02	0.13	0.00	0.00	20.9
10	55	-0	-2112	0	0	0	148	--	--	16.08	16.08	0.10	0.00	0.02	0.13	0.00	0.00	20.9
11	55	-0	-2136	0	0	0	150	--	--	16.08	16.08	0.10	0.00	0.02	0.13	0.00	0.00	20.9
12	55	-0	-1950	0	0	0	246	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
13	55	-0	-1974	0	0	0	248	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
14	55	-0	-2027	0	0	0	180	--	--	16.08	16.08	0.10	0.00	0.02	0.13	0.00	0.00	20.9
15	55	-0	-2107	0	0	0	187	--	--	16.08	16.08	0.10	0.00	0.02	0.13	0.00	0.00	20.9
16	55	-0	-1979	0	0	0	209	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
17	55	-0	-2059	0	0	0	216	--	--	16.08	16.08	0.10	0.00	0.02	0.13	0.00	0.00	20.9
18	55	-0	-4211	0	0	0	340	--	--	16.08	16.08	0.00	0.01	0.03	0.26	0.00	0.00	20.9
19	55	-0	-2511	0	0	0	701	--	--	16.08	16.08	0.00	0.01	0.02	0.16	0.00	0.00	20.9
20	55	-0	-3327	0	0	0	547	--	--	16.08	16.08	0.00	0.01	0.03	0.21	0.00	0.00	20.9
37	55	-0	-4555	0	0	0	133	--	--	16.08	16.08	0.00	0.00	0.04	0.29	0.00	0.00	20.9
38	55	-0	-1721	0	0	0	736	--	--	16.08	16.08	0.00	0.01	0.01	0.11	0.00	0.00	20.9
39	55	-0	-3081	0	0	0	479	--	--	16.08	16.08	0.00	0.01	0.03	0.19	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 44 NI 1545 NF 1721 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	2864	0	0	0	-761	--	--	16.08	16.08	0.18	0.01	0.02	0.18	0.00	0.00	20.9
2	0	-0	1535	0	0	0	-259	--	--	16.08	16.08	0.29	0.00	0.01	0.10	0.00	0.00	20.9
3	0	-0	1486	0	0	0	-236	--	--	16.08	16.08	0.29	0.00	0.01	0.09	0.00	0.00	20.9
4	0	-0	2920	0	0	0	-934	--	--	16.08	16.08	0.29	0.02	0.02	0.18	0.00	0.00	20.9
5	0	-0	2871	0	0	0	-911	--	--	16.08	16.08	0.29	0.02	0.02	0.18	0.00	0.00	20.9
6	0	-0	2077	0	0	0	-523	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
7	0	-0	1913	0	0	0	-445	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
8	0	-0	2493	0	0	0	-725	--	--	16.08	16.08	0.29	0.01	0.02	0.16	0.00	0.00	20.9
9	0	-0	2329	0	0	0	-648	--	--	16.08	16.08	0.29	0.01	0.02	0.15	0.00	0.00	20.9
10	0	-0	1535	0	0	0	-259	--	--	16.08	16.08	0.29	0.00	0.01	0.10	0.00	0.00	20.9
11	0	-0	1486	0	0	0	-236	--	--	16.08	16.08	0.29	0.00	0.01	0.09	0.00	0.00	20.9
12	0	-0	2920	0	0	0	-934	--	--	16.08	16.08	0.29	0.02	0.02	0.18	0.00	0.00	20.9
13	0	-0	2871	0	0	0	-911	--	--	16.08	16.08	0.29	0.02	0.02	0.18	0.00	0.00	20.9
14	0	-0	2077	0	0	0	-523	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
15	0	-0	1913	0	0	0	-445	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
16	0	-0	2493	0	0	0	-725	--	--	16.08	16.08	0.29	0.01	0.02	0.16	0.00	0.00	20.9
17	0	-0	2329	0	0	0	-648	--	--	16.08	16.08	0.29	0.01	0.02	0.15	0.00	0.00	20.9
18	0	-0	3361	0	0	0	-619	--	--	16.08	16.08	0.18	0.01	0.03	0.21	0.00	0.00	20.9
19	0	-0	9092	0	0	0	-3692	--	--	16.08	16.08	0.18	0.06	0.07	0.57	0.00	0.00	20.9
20	0	-0	5575	0	0	0	-1815	--	--	16.08	16.08	0.18	0.03	0.05	0.35	0.00	0.00	20.9
37	0	-0	352	0	0	0	862	--	--	16.08	16.08	0.00	0.01	0.00	0.02	0.00	0.00	20.9
38	0	-0	9904	0	0	0	-4259	--	--	16.08	16.08	0.18	0.07	0.08	0.62	0.00	0.00	20.9
39	0	-0	4042	0	0	0	-1131	--	--	16.08	16.08	0.18	0.02	0.03	0.25	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	2864	0	0	0	3081	--	--	16.08	16.08	0.00	0.05	0.02	0.18	0.00	0.00	20.9
2	27	-0	1535	0	0	0	1800	--	--	16.08	16.08	0.10	0.03	0.01	0.10	0.00	0.00	20.9
3	27	-0	1486	0	0	0	1758	--	--	16.08	16.08	0.10	0.03	0.01	0.09	0.00	0.00	20.9
4	27	-0	2920	0	0	0	-934	--	--	16.08	16.08	0.29	0.02	0.02	0.18	0.00	0.00	20.9
5	27	-0	2871	0	0	0	-911	--	--	16.08	16.08	0.29	0.02	0.02	0.18	0.00	0.00	20.9
6	27	-0	2077	0	0	0	2264	--	--	16.08	16.08	0.10	0.04	0.02	0.13	0.00	0.00	20.9
7	27	-0	1913	0	0	0	2121	--	--	16.08	16.08	0.10	0.04	0.02	0.12	0.00	0.00	20.9
8	27	-0	2493	0	0	0	-725	--	--	16.08	16.08	0.29	0.01	0.02	0.16	0.00	0.00	20.9
9	27	-0	2329	0	0	0	-648	--	--	16.08	16.08	0.29	0.01	0.02	0.15	0.00	0.00	20.9
10	27	-0	1535	0	0	0	1800	--	--	16.08	16.08	0.10	0.03	0.01	0.10	0.00	0.00	20.9
11	27	-0	1486	0	0	0	1758	--	--	16.08	16.08	0.10	0.03	0.01	0.09	0.00	0.00	20.9
12	27	-0	2920	0	0	0	-934	--	--	16.08	16.08	0.29	0.02	0.02	0.18	0.00	0.00	20.9

13	27	-0	2871	0	0	0	-911	--	--	16.08	16.08	0.29	0.02	0.02	0.18	0.00	0.00	20.9
14	27	-0	2077	0	0	0	2264	--	--	16.08	16.08	0.10	0.04	0.02	0.13	0.00	0.00	20.9
15	27	-0	1913	0	0	0	2121	--	--	16.08	16.08	0.10	0.04	0.02	0.12	0.00	0.00	20.9
16	27	-0	2493	0	0	0	-725	--	--	16.08	16.08	0.29	0.01	0.02	0.16	0.00	0.00	20.9
17	27	-0	2329	0	0	0	-648	--	--	16.08	16.08	0.29	0.01	0.02	0.15	0.00	0.00	20.9
18	27	-0	3361	0	0	0	3890	--	--	16.08	16.08	0.00	0.07	0.03	0.21	0.00	0.00	20.9
19	27	-0	9092	0	0	0	-3692	--	--	16.08	16.08	0.18	0.06	0.07	0.57	0.00	0.00	20.9
20	27	-0	5575	0	0	0	-1815	--	--	16.08	16.08	0.18	0.03	0.05	0.35	0.00	0.00	20.9
37	27	-0	352	0	0	0	1334	--	--	16.08	16.08	0.00	0.02	0.00	0.02	0.00	0.00	20.9
38	27	-0	9904	0	0	0	-4259	--	--	16.08	16.08	0.18	0.07	0.08	0.62	0.00	0.00	20.9
39	27	-0	4042	0	0	0	-1131	--	--	16.08	16.08	0.18	0.02	0.03	0.25	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	2864	0	0	0	801	--	--	16.08	16.08	0.00	0.01	0.02	0.18	0.00	0.00	20.9
2	55	-0	1535	0	0	0	578	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
3	55	-0	1486	0	0	0	575	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
4	55	-0	2920	0	0	0	658	--	--	16.08	16.08	0.10	0.01	0.02	0.18	0.00	0.00	20.9
5	55	-0	2871	0	0	0	655	--	--	16.08	16.08	0.10	0.01	0.02	0.18	0.00	0.00	20.9
6	55	-0	2077	0	0	0	610	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
7	55	-0	1913	0	0	0	599	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
8	55	-0	2493	0	0	0	634	--	--	16.08	16.08	0.10	0.01	0.02	0.16	0.00	0.00	20.9
9	55	-0	2329	0	0	0	623	--	--	16.08	16.08	0.10	0.01	0.02	0.15	0.00	0.00	20.9
10	55	-0	1535	0	0	0	578	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
11	55	-0	1486	0	0	0	575	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
12	55	-0	2920	0	0	0	658	--	--	16.08	16.08	0.10	0.01	0.02	0.18	0.00	0.00	20.9
13	55	-0	2871	0	0	0	655	--	--	16.08	16.08	0.10	0.01	0.02	0.18	0.00	0.00	20.9
14	55	-0	2077	0	0	0	610	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
15	55	-0	1913	0	0	0	599	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
16	55	-0	2493	0	0	0	634	--	--	16.08	16.08	0.10	0.01	0.02	0.16	0.00	0.00	20.9
17	55	-0	2329	0	0	0	623	--	--	16.08	16.08	0.10	0.01	0.02	0.15	0.00	0.00	20.9
18	55	-0	3361	0	0	0	1214	--	--	16.08	16.08	0.00	0.02	0.03	0.21	0.00	0.00	20.9
19	55	-0	9092	0	0	0	1268	--	--	16.08	16.08	0.00	0.02	0.07	0.57	0.00	0.00	20.9
20	55	-0	5575	0	0	0	1227	--	--	16.08	16.08	0.00	0.02	0.05	0.35	0.00	0.00	20.9
37	55	-0	352	0	0	0	1054	--	--	16.08	16.08	0.00	0.02	0.00	0.02	0.00	0.00	20.9
38	55	-0	9904	0	0	0	1144	--	--	16.08	16.08	0.00	0.02	0.08	0.62	0.00	0.00	20.9
39	55	-0	4042	0	0	0	1074	--	--	16.08	16.08	0.00	0.02	0.03	0.25	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 45 NI 1720 NF 1545 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-3474	0	0	0	894	--	--	16.08	16.08	0.00	0.02	0.03	0.22	0.00	0.00	20.9
2	0	-0	-1938	0	0	0	668	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
3	0	-0	-1967	0	0	0	686	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
4	0	-0	-3377	0	0	0	690	--	--	16.08	16.08	0.10	0.01	0.03	0.21	0.00	0.00	20.9
5	0	-0	-3407	0	0	0	708	--	--	16.08	16.08	0.10	0.01	0.03	0.21	0.00	0.00	20.9
6	0	-0	-2408	0	0	0	654	--	--	16.08	16.08	0.10	0.01	0.02	0.15	0.00	0.00	20.9
7	0	-0	-2505	0	0	0	715	--	--	16.08	16.08	0.10	0.01	0.02	0.16	0.00	0.00	20.9
8	0	-0	-2839	0	0	0	661	--	--	16.08	16.08	0.10	0.01	0.02	0.18	0.00	0.00	20.9
9	0	-0	-2937	0	0	0	722	--	--	16.08	16.08	0.10	0.01	0.02	0.18	0.00	0.00	20.9
10	0	-0	-1938	0	0	0	668	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
11	0	-0	-1967	0	0	0	686	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
12	0	-0	-3377	0	0	0	690	--	--	16.08	16.08	0.10	0.01	0.03	0.21	0.00	0.00	20.9
13	0	-0	-3407	0	0	0	708	--	--	16.08	16.08	0.10	0.01	0.03	0.21	0.00	0.00	20.9
14	0	-0	-2408	0	0	0	654	--	--	16.08	16.08	0.10	0.01	0.02	0.15	0.00	0.00	20.9
15	0	-0	-2505	0	0	0	715	--	--	16.08	16.08	0.10	0.01	0.02	0.16	0.00	0.00	20.9
16	0	-0	-2839	0	0	0	661	--	--	16.08	16.08	0.10	0.01	0.02	0.18	0.00	0.00	20.9
17	0	-0	-2937	0	0	0	722	--	--	16.08	16.08	0.10	0.01	0.02	0.18	0.00	0.00	20.9
18	0	-0	-4403	0	0	0	1438	--	--	16.08	16.08	0.00	0.02	0.04	0.28	0.00	0.00	20.9
19	0	-0	-9934	0	0	0	1178	--	--	16.08	16.08	0.00	0.02	0.08	0.62	0.00	0.00	20.9
20	0	-0	-6669	0	0	0	1349	--	--	16.08	16.08	0.00	0.02	0.05	0.42	0.00	0.00	20.9
37	0	-0	-1352	0	0	0	1390	--	--	16.08	16.08	0.00	0.02	0.01	0.08	0.00	0.00	20.9
38	0	-0	-10570	0	0	0	957	--	--	16.08	16.08	0.00	0.02	0.09	0.66	0.00	0.00	20.9
39	0	-0	-5130	0	0	0	1243	--	--	16.08	16.08	0.00	0.02	0.04	0.32	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-3474	0	0	0	-1001	--	--	16.08	16.08	0.18	0.02	0.03	0.22	0.00	0.00	20.9
2	27	-0	-1938	0	0	0	668	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
3	27	-0	-1967	0	0	0	686	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
4	27	-0	-3377	0	0	0	-1153	--	--	16.08	16.08	0.29	0.02	0.03	0.21	0.00	0.00	20.9
5	27	-0	-3407	0	0	0	-1150	--	--	16.08	16.08	0.29	0.02	0.03	0.21	0.00	0.00	20.9
6	27	-0	-2408	0	0	0	-659	--	--	16.08	16.08	0.29	0.01	0.02	0.15	0.00	0.00	20.9
7	27	-0	-2505	0	0	0	715	--	--	16.08	16.08	0.10	0.01	0.02	0.16	0.00	0.00	20.9
8	27	-0	-2839	0	0	0	-888	--	--	16.08	16.08	0.29	0.02	0.02	0.18	0.00	0.00	20.9
9	27	-0	-2937	0	0	0	-881	--	--	16.08	16.08	0.29	0.02	0.02	0.18	0.00	0.00	20.9
10	27	-0	-1938	0	0	0	668	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
11	27	-0	-1967	0	0	0	686	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
12	27	-0	-3377	0	0	0	-1153	--	--	16.08	16.08	0.29	0.02	0.03	0.21	0.00	0.00	20.9
13	27	-0	-3407	0	0	0	-1150	--	--	16.08	16.08	0.29	0.02	0.03	0.21	0.00	0.00	20.9
14	27	-0	-2408	0	0	0	-659	--	--	16.08	16.08	0.29	0.01	0.02	0.15	0.00	0.00	20.9
15	27	-0	-2505	0	0	0	715	--	--	16.08	16.08	0.10	0.01	0.02	0.16	0.00	0.00	20.9
16	27	-0	-2839	0	0	0	-888	--	--	16.08	16.08	0.29	0.02	0.02	0.18	0.00	0.00	20.9
17	27	-0	-2937	0	0	0	-881	--	--	16.08	16.08	0.29	0.02	0.02	0.18	0.00	0.00	20.9
18	27	-0	-4403	0	0	0	1438	--	--	16.08	16.08	0.00	0.02	0.04	0.28	0.00	0.00	20.9
19	27	-0	-9934	0	0	0	-4241	--	--	16.08	16.08	0.18	0.07	0.08	0.62	0.00	0.00	20.9
20	27	-0	-6669	0	0	0	-2289	--	--	16.08	16.08	0.18	0.04	0.05	0.42	0.00	0.00	20.9
37	27	-0	-1352	0	0	0	1390	--	--	16.08	16.08	0.00	0.02	0.01	0.08	0.00	0.00	20.9
38	27	-0	-10570	0	0	0	-4810	--	--	16.08	16.08	0.18	0.08	0.09	0.66	0.00	0.00	20.9
39	27	-0	-5130	0	0	0	-1555	--	--	16.08	16.08	0.18	0.03	0.04	0.32	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	-3474	0	0	0	-1001	--	--	16.08	16.08	0.18	0.02	0.03	0.22	0.00	0.00	20.9
2	55	-0	-1938	0	0	0	-390	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
3	55	-0	-1967	0	0	0	-387	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
4	55	-0	-3377	0	0	0	-1153	--	--	16.08	16.08	0.29	0.02	0.03	0.21	0.00	0.00	20.9
5	55	-0	-3407	0	0	0	-1150	--	--	16.08	16.08	0.29	0.02	0.03	0.21	0.00	0.00	20.9
6	55	-0	-2408	0	0	0	-659	--	--	16.08	16.08	0.29	0.01	0.02	0.15	0.00	0.00	20.9
7	55	-0	-2505	0	0	0	-652	--	--	16.08	16.08	0.29	0.01	0.02	0.16	0.00	0.00	20.9
8	55	-0	-2839	0	0	0	-888	--	--	16.08	16.08	0.29	0.02	0.02	0.18	0.00	0.00	20.9

9	55	-0	-2937	0	0	0	-881	--	--	16.08	16.08	0.29	0.02	0.02	0.18	0.00	0.00	20.9
10	55	-0	-1938	0	0	0	-390	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
11	55	-0	-1967	0	0	0	-387	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
12	55	-0	-3377	0	0	0	-1153	--	--	16.08	16.08	0.29	0.02	0.03	0.21	0.00	0.00	20.9
13	55	-0	-3407	0	0	0	-1150	--	--	16.08	16.08	0.29	0.02	0.03	0.21	0.00	0.00	20.9
14	55	-0	-2408	0	0	0	-659	--	--	16.08	16.08	0.29	0.01	0.02	0.15	0.00	0.00	20.9
15	55	-0	-2505	0	0	0	-652	--	--	16.08	16.08	0.29	0.01	0.02	0.16	0.00	0.00	20.9
16	55	-0	-2839	0	0	0	-888	--	--	16.08	16.08	0.29	0.02	0.02	0.18	0.00	0.00	20.9
17	55	-0	-2937	0	0	0	-881	--	--	16.08	16.08	0.29	0.02	0.02	0.18	0.00	0.00	20.9
18	55	-0	-4403	0	0	0	-964	--	--	16.08	16.08	0.18	0.02	0.04	0.28	0.00	0.00	20.9
19	55	-0	-9934	0	0	0	-4241	--	--	16.08	16.08	0.18	0.07	0.08	0.62	0.00	0.00	20.9
20	55	-0	-6669	0	0	0	-2289	--	--	16.08	16.08	0.18	0.04	0.05	0.42	0.00	0.00	20.9
37	55	-0	-1352	0	0	0	653	--	--	16.08	16.08	0.00	0.01	0.01	0.08	0.00	0.00	20.9
38	55	-0	-10570	0	0	0	-4810	--	--	16.08	16.08	0.18	0.08	0.09	0.66	0.00	0.00	20.9
39	55	-0	-5130	0	0	0	-1555	--	--	16.08	16.08	0.18	0.03	0.04	0.32	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 46 NI 1716 NF 1720 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	2181	0	0	0	467	--	--	16.08	16.08	0.00	0.01	0.02	0.14	0.00	0.00	20.9
2	0	-0	1751	0	0	0	328	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
3	0	-0	1752	0	0	0	334	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
4	0	-0	1604	0	0	0	384	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
5	0	-0	1605	0	0	0	390	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
6	0	-0	1698	0	0	0	340	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
7	0	-0	1702	0	0	0	361	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
8	0	-0	1654	0	0	0	357	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
9	0	-0	1658	0	0	0	378	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
10	0	-0	1751	0	0	0	328	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
11	0	-0	1752	0	0	0	334	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
12	0	-0	1604	0	0	0	384	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
13	0	-0	1605	0	0	0	390	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
14	0	-0	1698	0	0	0	340	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
15	0	-0	1702	0	0	0	361	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
16	0	-0	1654	0	0	0	357	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
17	0	-0	1658	0	0	0	378	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
18	0	-0	3336	0	0	0	764	--	--	16.08	16.08	0.00	0.01	0.03	0.21	0.00	0.00	20.9
19	0	-0	2021	0	0	0	810	--	--	16.08	16.08	0.00	0.01	0.02	0.13	0.00	0.00	20.9
20	0	-0	2654	0	0	0	794	--	--	16.08	16.08	0.00	0.01	0.02	0.17	0.00	0.00	20.9
37	0	-0	3620	0	0	0	643	--	--	16.08	16.08	0.00	0.01	0.03	0.23	0.00	0.00	20.9
38	0	-0	1428	0	0	0	720	--	--	16.08	16.08	0.00	0.01	0.01	0.09	0.00	0.00	20.9
39	0	-0	2483	0	0	0	695	--	--	16.08	16.08	0.00	0.01	0.02	0.16	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	2181	0	0	0	3392	--	--	16.08	16.08	0.00	0.06	0.02	0.14	0.00	0.00	20.9
2	27	-0	1751	0	0	0	2677	--	--	16.08	16.08	0.10	0.05	0.01	0.11	0.00	0.00	20.9
3	27	-0	1752	0	0	0	2685	--	--	16.08	16.08	0.10	0.05	0.01	0.11	0.00	0.00	20.9
4	27	-0	1604	0	0	0	2535	--	--	16.08	16.08	0.10	0.04	0.01	0.10	0.00	0.00	20.9
5	27	-0	1605	0	0	0	2543	--	--	16.08	16.08	0.10	0.05	0.01	0.10	0.00	0.00	20.9
6	27	-0	1698	0	0	0	2618	--	--	16.08	16.08	0.10	0.05	0.01	0.11	0.00	0.00	20.9
7	27	-0	1702	0	0	0	2644	--	--	16.08	16.08	0.10	0.05	0.01	0.11	0.00	0.00	20.9
8	27	-0	1654	0	0	0	2576	--	--	16.08	16.08	0.10	0.05	0.01	0.10	0.00	0.00	20.9
9	27	-0	1658	0	0	0	2602	--	--	16.08	16.08	0.10	0.05	0.01	0.10	0.00	0.00	20.9
10	27	-0	1751	0	0	0	2677	--	--	16.08	16.08	0.10	0.05	0.01	0.11	0.00	0.00	20.9
11	27	-0	1752	0	0	0	2685	--	--	16.08	16.08	0.10	0.05	0.01	0.11	0.00	0.00	20.9
12	27	-0	1604	0	0	0	2535	--	--	16.08	16.08	0.10	0.04	0.01	0.10	0.00	0.00	20.9
13	27	-0	1605	0	0	0	2543	--	--	16.08	16.08	0.10	0.05	0.01	0.10	0.00	0.00	20.9
14	27	-0	1698	0	0	0	2618	--	--	16.08	16.08	0.10	0.05	0.01	0.11	0.00	0.00	20.9
15	27	-0	1702	0	0	0	2644	--	--	16.08	16.08	0.10	0.05	0.01	0.11	0.00	0.00	20.9
16	27	-0	1654	0	0	0	2576	--	--	16.08	16.08	0.10	0.05	0.01	0.10	0.00	0.00	20.9
17	27	-0	1658	0	0	0	2602	--	--	16.08	16.08	0.10	0.05	0.01	0.10	0.00	0.00	20.9
18	27	-0	3336	0	0	0	5239	--	--	16.08	16.08	0.00	0.09	0.03	0.21	0.00	0.00	20.9
19	27	-0	2021	0	0	0	3521	--	--	16.08	16.08	0.00	0.06	0.02	0.13	0.00	0.00	20.9
20	27	-0	2654	0	0	0	4355	--	--	16.08	16.08	0.00	0.07	0.02	0.17	0.00	0.00	20.9
37	27	-0	3620	0	0	0	5499	--	--	16.08	16.08	0.00	0.09	0.03	0.23	0.00	0.00	20.9
38	27	-0	1428	0	0	0	2636	--	--	16.08	16.08	0.00	0.04	0.01	0.09	0.00	0.00	20.9
39	27	-0	2483	0	0	0	4026	--	--	16.08	16.08	0.00	0.07	0.02	0.16	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	2181	0	0	0	1656	--	--	16.08	16.08	0.00	0.03	0.02	0.14	0.00	0.00	20.9
2	55	-0	1751	0	0	0	1283	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
3	55	-0	1752	0	0	0	1290	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
4	55	-0	1604	0	0	0	1258	--	--	16.08	16.08	0.10	0.02	0.01	0.10	0.00	0.00	20.9
5	55	-0	1605	0	0	0	1265	--	--	16.08	16.08	0.10	0.02	0.01	0.10	0.00	0.00	20.9
6	55	-0	1698	0	0	0	1266	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
7	55	-0	1702	0	0	0	1289	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
8	55	-0	1654	0	0	0	1259	--	--	16.08	16.08	0.10	0.02	0.01	0.10	0.00	0.00	20.9
9	55	-0	1658	0	0	0	1282	--	--	16.08	16.08	0.10	0.02	0.01	0.10	0.00	0.00	20.9
10	55	-0	1751	0	0	0	1283	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
11	55	-0	1752	0	0	0	1290	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
12	55	-0	1604	0	0	0	1258	--	--	16.08	16.08	0.10	0.02	0.01	0.10	0.00	0.00	20.9
13	55	-0	1605	0	0	0	1265	--	--	16.08	16.08	0.10	0.02	0.01	0.10	0.00	0.00	20.9
14	55	-0	1698	0	0	0	1266	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
15	55	-0	1702	0	0	0	1289	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
16	55	-0	1654	0	0	0	1259	--	--	16.08	16.08	0.10	0.02	0.01	0.10	0.00	0.00	20.9
17	55	-0	1658	0	0	0	1282	--	--	16.08	16.08	0.10	0.02	0.01	0.10	0.00	0.00	20.9
18	55	-0	3336	0	0	0	2583	--	--	16.08	16.08	0.00	0.04	0.03	0.21	0.00	0.00	20.9
19	55	-0	2021	0	0	0	1912	--	--	16.08	16.08	0.00	0.03	0.02	0.13	0.00	0.00	20.9
20	55	-0	2654	0	0	0	2242	--	--	16.08	16.08	0.00	0.04	0.02	0.17	0.00	0.00	20.9
37	55	-0	3620	0	0	0	2617	--	--	16.08	16.08	0.00	0.04	0.03	0.23	0.00	0.00	20.9
38	55	-0	1428	0	0	0	1499	--	--	16.08	16.08	0.00	0.03	0.01	0.09	0.00	0.00	20.9
39	55	-0	2483	0	0	0	2049	--	--	16.08	16.08	0.00	0.03	0.02	0.16	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 47 NI 1717 NF 1716 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice resistenza			aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	2419	0	0	0	144	--	--	16.08	16.08	0.00	0.00	0.02	0.15	0.00	0.00	20.9
2	0	-0	1809	0	0	0	78	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
3	0	-0	1848	0	0	0	83	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
4	0	-0	1873	0	0	0	138	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
5	0	-0	1912	0	0	0	143	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
6	0	-0	1786	0	0	0	92	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
7	0	-0	1916	0	0	0	110	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
8	0	-0	1805	0	0	0	111	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
9	0	-0	1935	0	0	0	129	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
10	0	-0	1809	0	0	0	78	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
11	0	-0	1848	0	0	0	83	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
12	0	-0	1873	0	0	0	138	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
13	0	-0	1912	0	0	0	143	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
14	0	-0	1786	0	0	0	92	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
15	0	-0	1916	0	0	0	110	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
16	0	-0	1805	0	0	0	111	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
17	0	-0	1935	0	0	0	129	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
18	0	-0	3553	0	0	0	297	--	--	16.08	16.08	0.00	0.01	0.03	0.22	0.00	0.00	20.9
19	0	-0	3122	0	0	0	434	--	--	16.08	16.08	0.00	0.01	0.03	0.20	0.00	0.00	20.9
20	0	-0	3386	0	0	0	371	--	--	16.08	16.08	0.00	0.01	0.03	0.21	0.00	0.00	20.9
37	0	-0	3405	0	0	0	177	--	--	16.08	16.08	0.00	0.00	0.03	0.21	0.00	0.00	20.9
38	0	-0	2686	0	0	0	405	--	--	16.08	16.08	0.00	0.01	0.02	0.17	0.00	0.00	20.9
39	0	-0	3126	0	0	0	301	--	--	16.08	16.08	0.00	0.01	0.03	0.20	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice resistenza			aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	27	-0	2419	0	0	0	3389	--	--	16.08	16.08	0.00	0.06	0.02	0.15	0.00	0.00	20.9
2	27	-0	1809	0	0	0	2504	--	--	16.08	16.08	0.10	0.04	0.01	0.11	0.00	0.00	20.9
3	27	-0	1848	0	0	0	2562	--	--	16.08	16.08	0.10	0.05	0.02	0.12	0.00	0.00	20.9
4	27	-0	1873	0	0	0	2651	--	--	16.08	16.08	0.10	0.05	0.02	0.12	0.00	0.00	20.9
5	27	-0	1912	0	0	0	2708	--	--	16.08	16.08	0.10	0.05	0.02	0.12	0.00	0.00	20.9
6	27	-0	1786	0	0	0	2488	--	--	16.08	16.08	0.10	0.04	0.01	0.11	0.00	0.00	20.9
7	27	-0	1916	0	0	0	2681	--	--	16.08	16.08	0.10	0.05	0.02	0.12	0.00	0.00	20.9
8	27	-0	1805	0	0	0	2532	--	--	16.08	16.08	0.10	0.04	0.01	0.11	0.00	0.00	20.9
9	27	-0	1935	0	0	0	2724	--	--	16.08	16.08	0.10	0.05	0.02	0.12	0.00	0.00	20.9
10	27	-0	1809	0	0	0	2504	--	--	16.08	16.08	0.10	0.04	0.01	0.11	0.00	0.00	20.9
11	27	-0	1848	0	0	0	2562	--	--	16.08	16.08	0.10	0.05	0.02	0.12	0.00	0.00	20.9
12	27	-0	1873	0	0	0	2651	--	--	16.08	16.08	0.10	0.05	0.02	0.12	0.00	0.00	20.9
13	27	-0	1912	0	0	0	2708	--	--	16.08	16.08	0.10	0.05	0.02	0.12	0.00	0.00	20.9
14	27	-0	1786	0	0	0	2488	--	--	16.08	16.08	0.10	0.04	0.01	0.11	0.00	0.00	20.9
15	27	-0	1916	0	0	0	2681	--	--	16.08	16.08	0.10	0.05	0.02	0.12	0.00	0.00	20.9
16	27	-0	1805	0	0	0	2532	--	--	16.08	16.08	0.10	0.04	0.01	0.11	0.00	0.00	20.9
17	27	-0	1935	0	0	0	2724	--	--	16.08	16.08	0.10	0.05	0.02	0.12	0.00	0.00	20.9
18	27	-0	3553	0	0	0	5063	--	--	16.08	16.08	0.00	0.09	0.03	0.22	0.00	0.00	20.9
19	27	-0	3122	0	0	0	4622	--	--	16.08	16.08	0.00	0.08	0.03	0.20	0.00	0.00	20.9
20	27	-0	3386	0	0	0	4913	--	--	16.08	16.08	0.00	0.08	0.03	0.21	0.00	0.00	20.9
37	27	-0	3405	0	0	0	4745	--	--	16.08	16.08	0.00	0.08	0.03	0.21	0.00	0.00	20.9
38	27	-0	2686	0	0	0	4008	--	--	16.08	16.08	0.00	0.07	0.02	0.17	0.00	0.00	20.9
39	27	-0	3126	0	0	0	4494	--	--	16.08	16.08	0.00	0.08	0.03	0.20	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice resistenza			aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	55	-0	2419	0	0	0	1463	--	--	16.08	16.08	0.00	0.02	0.02	0.15	0.00	0.00	20.9
2	55	-0	1809	0	0	0	1064	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
3	55	-0	1848	0	0	0	1091	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
4	55	-0	1873	0	0	0	1160	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
5	55	-0	1912	0	0	0	1186	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
6	55	-0	1786	0	0	0	1066	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
7	55	-0	1916	0	0	0	1156	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
8	55	-0	1805	0	0	0	1095	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
9	55	-0	1935	0	0	0	1184	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
10	55	-0	1809	0	0	0	1064	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
11	55	-0	1848	0	0	0	1091	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
12	55	-0	1873	0	0	0	1160	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
13	55	-0	1912	0	0	0	1186	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
14	55	-0	1786	0	0	0	1066	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
15	55	-0	1916	0	0	0	1156	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
16	55	-0	1805	0	0	0	1095	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
17	55	-0	1935	0	0	0	1184	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
18	55	-0	3553	0	0	0	2235	--	--	16.08	16.08	0.00	0.04	0.03	0.22	0.00	0.00	20.9
19	55	-0	3122	0	0	0	2137	--	--	16.08	16.08	0.00	0.04	0.03	0.20	0.00	0.00	20.9
20	55	-0	3386	0	0	0	2218	--	--	16.08	16.08	0.00	0.04	0.03	0.21	0.00	0.00	20.9
37	55	-0	3405	0	0	0	2034	--	--	16.08	16.08	0.00	0.03	0.03	0.21	0.00	0.00	20.9
38	55	-0	2686	0	0	0	1870	--	--	16.08	16.08	0.00	0.03	0.02	0.17	0.00	0.00	20.9
39	55	-0	3126	0	0	0	2006	--	--	16.08	16.08	0.00	0.03	0.03	0.20	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 48 NI 1712 NF 1717 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice resistenza			aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	1229	0	0	0	-132	--	--	16.08	16.08	0.18	0.00	0.01	0.08	0.00	0.00	20.9
2	0	-0	920	0	0	0	-115	--	--	16.08	16.08	0.29	0.00	0.01	0.06	0.00	0.00	20.9
3	0	-0	967	0	0	0	-117	--	--	16.08	16.08	0.29	0.00	0.01	0.06	0.00	0.00	20.9
4	0	-0	923	0	0	0	-86	--	--	16.08	16.08	0.29	0.00	0.01	0.06	0.00	0.00	20.9
5	0	-0	970	0	0	0	-87	--	--	16.08	16.08	0.29	0.00	0.01	0.06	0.00	0.00	20.9
6	0	-0	866	0	0	0	-103	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
7	0	-0	1023	0	0	0	-108	--	--	16.08	16.08	0.29	0.00	0.01	0.06	0.00	0.00	20.9
8	0	-0	867	0	0	0	-94	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
9	0	-0	1024	0	0	0	-99	--	--	16.08	16.08	0.29	0.00	0.01	0.06	0.00	0.00	20.9
10	0	-0	920	0	0	0	-115	--	--	16.08	16.08	0.29	0.00	0.01	0.06	0.00	0.00	20.9
11	0	-0	967	0	0	0	-117	--	--	16.08	16.08	0.29	0.00	0.01	0.06	0.00	0.00	20.9
12	0	-0	923	0	0	0	-86	--	--	16.08	16.08	0.29	0.00	0.01	0.06	0.00	0.00	20.9
13	0	-0	970	0	0	0	-87	--	--	16.08	16.08	0.29	0.00	0.01	0.06	0.00	0.00	20.9
14	0	-0	866	0	0	0	-103	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
15	0	-0	1023	0	0	0	-108	--	--	16.08	16.08	0.29	0.00	0.01	0.06	0.00	0.00	20.9
16	0	-0	867	0	0	0	-94	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9

17	0	-0	1024	0	0	0	-99	--	--	16.08	16.08	0.29	0.00	0.01	0.06	0.00	0.00	20.9
18	0	-0	1768	0	0	0	-82	--	--	16.08	16.08	0.18	0.00	0.01	0.11	0.00	0.00	20.9
19	0	-0	1457	0	0	0	-19	--	--	16.08	16.08	0.18	0.00	0.01	0.09	0.00	0.00	20.9
20	0	-0	1786	0	0	0	-63	--	--	16.08	16.08	0.18	0.00	0.01	0.11	0.00	0.00	20.9
37	0	-0	1751	0	0	0	-133	--	--	16.08	16.08	0.18	0.00	0.01	0.11	0.00	0.00	20.9
38	0	-0	1233	0	0	0	-27	--	--	16.08	16.08	0.18	0.00	0.01	0.08	0.00	0.00	20.9
39	0	-0	1781	0	0	0	-101	--	--	16.08	16.08	0.18	0.00	0.01	0.11	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	1229	0	0	0	1517	--	--	16.08	16.08	0.00	0.03	0.01	0.08	0.00	0.00	20.9
2	27	-0	920	0	0	0	1119	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9
3	27	-0	967	0	0	0	1181	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9
4	27	-0	923	0	0	0	1152	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9
5	27	-0	970	0	0	0	1214	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9
6	27	-0	866	0	0	0	1058	--	--	16.08	16.08	0.10	0.02	0.01	0.05	0.00	0.00	20.9
7	27	-0	1023	0	0	0	1264	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9
8	27	-0	867	0	0	0	1068	--	--	16.08	16.08	0.10	0.02	0.01	0.05	0.00	0.00	20.9
9	27	-0	1024	0	0	0	1274	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9
10	27	-0	920	0	0	0	1119	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9
11	27	-0	967	0	0	0	1181	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9
12	27	-0	923	0	0	0	1152	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9
13	27	-0	970	0	0	0	1214	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9
14	27	-0	866	0	0	0	1058	--	--	16.08	16.08	0.10	0.02	0.01	0.05	0.00	0.00	20.9
15	27	-0	1023	0	0	0	1264	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9
16	27	-0	867	0	0	0	1068	--	--	16.08	16.08	0.10	0.02	0.01	0.05	0.00	0.00	20.9
17	27	-0	1024	0	0	0	1274	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9
18	27	-0	1768	0	0	0	2289	--	--	16.08	16.08	0.00	0.04	0.01	0.11	0.00	0.00	20.9
19	27	-0	1457	0	0	0	1935	--	--	16.08	16.08	0.00	0.03	0.01	0.09	0.00	0.00	20.9
20	27	-0	1786	0	0	0	2333	--	--	16.08	16.08	0.00	0.04	0.01	0.11	0.00	0.00	20.9
37	27	-0	1751	0	0	0	2216	--	--	16.08	16.08	0.00	0.04	0.01	0.11	0.00	0.00	20.9
38	27	-0	1233	0	0	0	1627	--	--	16.08	16.08	0.00	0.03	0.01	0.08	0.00	0.00	20.9
39	27	-0	1781	0	0	0	2288	--	--	16.08	16.08	0.00	0.04	0.01	0.11	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	1229	0	0	0	538	--	--	16.08	16.08	0.00	0.01	0.01	0.08	0.00	0.00	20.9
2	55	-0	920	0	0	0	386	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
3	55	-0	967	0	0	0	411	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
4	55	-0	923	0	0	0	418	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
5	55	-0	970	0	0	0	442	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
6	55	-0	866	0	0	0	369	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
7	55	-0	1023	0	0	0	450	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
8	55	-0	867	0	0	0	378	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
9	55	-0	1024	0	0	0	459	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
10	55	-0	920	0	0	0	386	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
11	55	-0	967	0	0	0	411	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
12	55	-0	923	0	0	0	418	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
13	55	-0	970	0	0	0	442	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
14	55	-0	866	0	0	0	369	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
15	55	-0	1023	0	0	0	450	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
16	55	-0	867	0	0	0	378	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
17	55	-0	1024	0	0	0	459	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
18	55	-0	1768	0	0	0	882	--	--	16.08	16.08	0.00	0.02	0.01	0.11	0.00	0.00	20.9
19	55	-0	1457	0	0	0	776	--	--	16.08	16.08	0.00	0.01	0.01	0.09	0.00	0.00	20.9
20	55	-0	1786	0	0	0	911	--	--	16.08	16.08	0.00	0.02	0.01	0.11	0.00	0.00	20.9
37	55	-0	1751	0	0	0	822	--	--	16.08	16.08	0.00	0.01	0.01	0.11	0.00	0.00	20.9
38	55	-0	1233	0	0	0	646	--	--	16.08	16.08	0.00	0.01	0.01	0.08	0.00	0.00	20.9
39	55	-0	1781	0	0	0	870	--	--	16.08	16.08	0.00	0.01	0.01	0.11	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 49 NI 1718 NF 1712 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm

1	0	-0	392	0	0	0	-154	--	--	16.08	16.08	0.18	0.00	0.00	0.02	0.00	0.00	20.9
2	0	-0	277	0	0	0	-120	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
3	0	-0	325	0	0	0	-130	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
4	0	-0	278	0	0	0	-106	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
5	0	-0	326	0	0	0	-117	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
6	0	-0	222	0	0	0	-103	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
7	0	-0	381	0	0	0	-138	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
8	0	-0	222	0	0	0	-99	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
9	0	-0	382	0	0	0	-134	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
10	0	-0	277	0	0	0	-120	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
11	0	-0	325	0	0	0	-130	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
12	0	-0	278	0	0	0	-106	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
13	0	-0	326	0	0	0	-117	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
14	0	-0	222	0	0	0	-103	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
15	0	-0	381	0	0	0	-138	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
16	0	-0	222	0	0	0	-99	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
17	0	-0	382	0	0	0	-134	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
18	0	-0	494	0	0	0	-86	--	--	16.08	16.08	0.18	0.00	0.00	0.03	0.00	0.00	20.9
19	0	-0	455	0	0	0	-108	--	--	16.08	16.08	0.18	0.00	0.00	0.03	0.00	0.00	20.9
20	0	-0	715	0	0	0	-156	--	--	16.08	16.08	0.18	0.00	0.01	0.04	0.00	0.00	20.9
37	0	-0	484	0	0	0	-100	--	--	16.08	16.08	0.18	0.00	0.00	0.03	0.00	0.00	20.9
38	0	-0	418	0	0	0	-137	--	--	16.08	16.08	0.18	0.00	0.00	0.03	0.00	0.00	20.9
39	0	-0	851	0	0	0	-217	--	--	16.08	16.08	0.18	0.00	0.01	0.05	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	392	0	0	0	-154	--	--	16.08	16.08	0.18	0.00	0.00	0.02	0.00	0.00	20.9
2	27	-0	277	0	0	0	-120	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
3	27	-0	325	0	0	0	-130	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
4	27	-0	278	0	0	0	-106	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
5	27	-0	326	0	0	0	-117	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
6	27	-0	222	0	0	0	-103	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
7	27	-0	381	0	0	0	-138	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
8	27	-0	222	0	0	0	-99	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
9	27	-0	382	0	0	0	-134	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
10	27	-0	277	0	0	0	-120	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
11	27	-0	325	0	0	0	-130	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
12	27	-0	278	0	0	0	-106	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9

13	27	-0	326	0	0	0	-117	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
14	27	-0	222	0	0	0	-103	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
15	27	-0	381	0	0	0	-138	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
16	27	-0	222	0	0	0	-99	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
17	27	-0	382	0	0	0	-134	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
18	27	-0	494	0	0	0	578	--	--	16.08	16.08	0.00	0.01	0.00	0.03	0.00	0.00	20.9
19	27	-0	455	0	0	0	502	--	--	16.08	16.08	0.00	0.01	0.00	0.03	0.00	0.00	20.9
20	27	-0	715	0	0	0	803	--	--	16.08	16.08	0.00	0.01	0.01	0.04	0.00	0.00	20.9
37	27	-0	484	0	0	0	549	--	--	16.08	16.08	0.00	0.01	0.00	0.03	0.00	0.00	20.9
38	27	-0	418	0	0	0	-137	--	--	16.08	16.08	0.18	0.00	0.00	0.03	0.00	0.00	20.9
39	27	-0	851	0	0	0	925	--	--	16.08	16.08	0.00	0.02	0.01	0.05	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	392	0	0	0	60	--	--	16.08	16.08	0.00	0.00	0.00	0.02	0.00	0.00	20.9
2	55	-0	277	0	0	0	31	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
3	55	-0	325	0	0	0	47	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
4	55	-0	278	0	0	0	45	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
5	55	-0	326	0	0	0	61	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
6	55	-0	222	0	0	0	18	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
7	55	-0	381	0	0	0	70	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
8	55	-0	222	0	0	0	22	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
9	55	-0	382	0	0	0	74	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
10	55	-0	277	0	0	0	31	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
11	55	-0	325	0	0	0	47	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
12	55	-0	278	0	0	0	45	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
13	55	-0	326	0	0	0	61	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
14	55	-0	222	0	0	0	18	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
15	55	-0	381	0	0	0	70	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
16	55	-0	222	0	0	0	22	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
17	55	-0	382	0	0	0	74	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
18	55	-0	494	0	0	0	184	--	--	16.08	16.08	0.00	0.00	0.00	0.03	0.00	0.00	20.9
19	55	-0	455	0	0	0	140	--	--	16.08	16.08	0.00	0.00	0.00	0.03	0.00	0.00	20.9
20	55	-0	715	0	0	0	234	--	--	16.08	16.08	0.00	0.00	0.01	0.04	0.00	0.00	20.9
37	55	-0	484	0	0	0	164	--	--	16.08	16.08	0.00	0.00	0.00	0.03	0.00	0.00	20.9
38	55	-0	418	0	0	0	91	--	--	16.08	16.08	0.00	0.00	0.00	0.03	0.00	0.00	20.9
39	55	-0	851	0	0	0	247	--	--	16.08	16.08	0.00	0.00	0.01	0.05	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 50 NI 1719 NF 1718 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--	--	--	--	--	--	--	--	--	--	--		--	--	--	--	--	--
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-275	0	0	0	-157	--	--	16.08	16.08	0.18	0.00	0.00	0.02	0.00	0.00	20.9
2	0	-0	-248	0	0	0	4	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
3	0	-0	-199	0	0	0	-124	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
4	0	-0	-224	0	0	0	5	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
5	0	-0	-176	0	0	0	-110	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
6	0	-0	-296	0	0	0	27	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
7	0	-0	-135	0	0	0	-112	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
8	0	-0	-289	0	0	0	28	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
9	0	-0	-128	0	0	0	-107	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
10	0	-0	-248	0	0	0	4	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
11	0	-0	-199	0	0	0	-124	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
12	0	-0	-224	0	0	0	5	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
13	0	-0	-176	0	0	0	-110	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
14	0	-0	-296	0	0	0	27	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
15	0	-0	-135	0	0	0	-112	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
16	0	-0	-289	0	0	0	28	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
17	0	-0	-128	0	0	0	-107	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
18	0	-0	-537	0	0	0	166	--	--	16.08	16.08	0.00	0.00	0.00	0.03	0.00	0.00	20.9
19	0	-0	-242	0	0	0	18	--	--	16.08	16.08	0.00	0.00	0.00	0.02	0.00	0.00	20.9
20	0	-0	-96	0	0	0	-82	--	--	16.08	16.08	0.18	0.00	0.00	0.01	0.00	0.00	20.9
37	0	-0	-597	0	0	0	181	--	--	16.08	16.08	0.00	0.00	0.00	0.04	0.00	0.00	20.9
38	0	-0	-105	0	0	0	-124	--	--	16.08	16.08	0.18	0.00	0.00	0.01	0.00	0.00	20.9
39	0	-0	139	0	0	0	-146	--	--	16.08	16.08	0.18	0.00	0.00	0.01	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-275	0	0	0	-157	--	--	16.08	16.08	0.18	0.00	0.00	0.02	0.00	0.00	20.9
2	27	-0	-248	0	0	0	-131	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
3	27	-0	-199	0	0	0	-124	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
4	27	-0	-224	0	0	0	-117	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
5	27	-0	-176	0	0	0	-110	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
6	27	-0	-296	0	0	0	-134	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
7	27	-0	-135	0	0	0	-112	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
8	27	-0	-289	0	0	0	-130	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
9	27	-0	-128	0	0	0	-107	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
10	27	-0	-248	0	0	0	-131	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
11	27	-0	-199	0	0	0	-124	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
12	27	-0	-224	0	0	0	-117	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
13	27	-0	-176	0	0	0	-110	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
14	27	-0	-296	0	0	0	-134	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
15	27	-0	-135	0	0	0	-112	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
16	27	-0	-289	0	0	0	-130	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
17	27	-0	-128	0	0	0	-107	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
18	27	-0	-537	0	0	0	166	--	--	16.08	16.08	0.00	0.00	0.00	0.03	0.00	0.00	20.9
19	27	-0	-242	0	0	0	-114	--	--	16.08	16.08	0.18	0.00	0.00	0.02	0.00	0.00	20.9
20	27	-0	-96	0	0	0	-82	--	--	16.08	16.08	0.18	0.00	0.00	0.01	0.00	0.00	20.9
37	27	-0	-597	0	0	0	181	--	--	16.08	16.08	0.00	0.00	0.00	0.04	0.00	0.00	20.9
38	27	-0	-105	0	0	0	-124	--	--	16.08	16.08	0.18	0.00	0.00	0.01	0.00	0.00	20.9
39	27	-0	139	0	0	0	-146	--	--	16.08	16.08	0.18	0.00	0.00	0.01	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	-275	0	0	0	-157	--	--	16.08	16.08	0.18	0.00	0.00	0.02	0.00	0.00	20.9
2	55	-0	-248	0	0	0	-131	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
3	55	-0	-199	0	0	0	-124	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
4	55	-0	-224	0	0	0	-117	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
5	55	-0	-176	0	0	0	-110	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
6	55	-0	-296	0	0	0	-134	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
7	55	-0	-135	0	0	0	-112	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
8	55	-0	-289	0	0	0	-130	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9

9	55	-0	-128	0	0	0	-107	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
10	55	-0	-248	0	0	0	-131	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
11	55	-0	-199	0	0	0	-124	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
12	55	-0	-224	0	0	0	-117	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
13	55	-0	-176	0	0	0	-110	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
14	55	-0	-296	0	0	0	-134	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
15	55	-0	-135	0	0	0	-112	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
16	55	-0	-289	0	0	0	-130	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
17	55	-0	-128	0	0	0	-107	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
18	55	-0	-537	0	0	0	-127	--	--	16.08	16.08	0.18	0.00	0.00	0.03	0.00	0.00	20.9
19	55	-0	-242	0	0	0	-114	--	--	16.08	16.08	0.18	0.00	0.00	0.02	0.00	0.00	20.9
20	55	-0	-96	0	0	0	-82	--	--	16.08	16.08	0.18	0.00	0.00	0.01	0.00	0.00	20.9
37	55	-0	-597	0	0	0	-145	--	--	16.08	16.08	0.18	0.00	0.00	0.04	0.00	0.00	20.9
38	55	-0	-105	0	0	0	-124	--	--	16.08	16.08	0.18	0.00	0.00	0.01	0.00	0.00	20.9
39	55	-0	139	0	0	0	-146	--	--	16.08	16.08	0.18	0.00	0.00	0.01	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 51 NI 1713 NF 1719 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-925	0	0	0	302	--	--	16.08	16.08	0.00	0.01	0.01	0.06	0.00	0.00	20.9
2	0	-0	-761	0	0	0	252	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
3	0	-0	-711	0	0	0	223	--	--	16.08	16.08	0.10	0.00	0.01	0.04	0.00	0.00	20.9
4	0	-0	-712	0	0	0	241	--	--	16.08	16.08	0.10	0.00	0.01	0.04	0.00	0.00	20.9
5	0	-0	-662	0	0	0	212	--	--	16.08	16.08	0.10	0.00	0.01	0.04	0.00	0.00	20.9
6	0	-0	-802	0	0	0	283	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
7	0	-0	-636	0	0	0	185	--	--	16.08	16.08	0.10	0.00	0.01	0.04	0.00	0.00	20.9
8	0	-0	-787	0	0	0	279	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
9	0	-0	-621	0	0	0	181	--	--	16.08	16.08	0.10	0.00	0.01	0.04	0.00	0.00	20.9
10	0	-0	-761	0	0	0	252	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
11	0	-0	-711	0	0	0	223	--	--	16.08	16.08	0.10	0.00	0.01	0.04	0.00	0.00	20.9
12	0	-0	-712	0	0	0	241	--	--	16.08	16.08	0.10	0.00	0.01	0.04	0.00	0.00	20.9
13	0	-0	-662	0	0	0	212	--	--	16.08	16.08	0.10	0.00	0.01	0.04	0.00	0.00	20.9
14	0	-0	-802	0	0	0	283	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
15	0	-0	-636	0	0	0	185	--	--	16.08	16.08	0.10	0.00	0.01	0.04	0.00	0.00	20.9
16	0	-0	-787	0	0	0	279	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
17	0	-0	-621	0	0	0	181	--	--	16.08	16.08	0.10	0.00	0.01	0.04	0.00	0.00	20.9
18	0	-0	-1539	0	0	0	660	--	--	16.08	16.08	0.00	0.01	0.01	0.10	0.00	0.00	20.9
19	0	-0	-908	0	0	0	337	--	--	16.08	16.08	0.00	0.01	0.01	0.06	0.00	0.00	20.9
20	0	-0	-872	0	0	0	300	--	--	16.08	16.08	0.00	0.01	0.01	0.05	0.00	0.00	20.9
37	0	-0	-1652	0	0	0	701	--	--	16.08	16.08	0.00	0.01	0.01	0.10	0.00	0.00	20.9
38	0	-0	-601	0	0	0	162	--	--	16.08	16.08	0.00	0.00	0.00	0.04	0.00	0.00	20.9
39	0	-0	-541	0	0	0	100	--	--	16.08	16.08	0.00	0.00	0.00	0.03	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-925	0	0	0	302	--	--	16.08	16.08	0.00	0.01	0.01	0.06	0.00	0.00	20.9
2	27	-0	-761	0	0	0	252	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
3	27	-0	-711	0	0	0	223	--	--	16.08	16.08	0.10	0.00	0.01	0.04	0.00	0.00	20.9
4	27	-0	-712	0	0	0	241	--	--	16.08	16.08	0.10	0.00	0.01	0.04	0.00	0.00	20.9
5	27	-0	-662	0	0	0	212	--	--	16.08	16.08	0.10	0.00	0.01	0.04	0.00	0.00	20.9
6	27	-0	-802	0	0	0	283	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
7	27	-0	-636	0	0	0	185	--	--	16.08	16.08	0.10	0.00	0.01	0.04	0.00	0.00	20.9
8	27	-0	-787	0	0	0	279	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
9	27	-0	-621	0	0	0	181	--	--	16.08	16.08	0.10	0.00	0.01	0.04	0.00	0.00	20.9
10	27	-0	-761	0	0	0	252	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
11	27	-0	-711	0	0	0	223	--	--	16.08	16.08	0.10	0.00	0.01	0.04	0.00	0.00	20.9
12	27	-0	-712	0	0	0	241	--	--	16.08	16.08	0.10	0.00	0.01	0.04	0.00	0.00	20.9
13	27	-0	-662	0	0	0	212	--	--	16.08	16.08	0.10	0.00	0.01	0.04	0.00	0.00	20.9
14	27	-0	-802	0	0	0	283	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
15	27	-0	-636	0	0	0	185	--	--	16.08	16.08	0.10	0.00	0.01	0.04	0.00	0.00	20.9
16	27	-0	-787	0	0	0	279	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
17	27	-0	-621	0	0	0	181	--	--	16.08	16.08	0.10	0.00	0.01	0.04	0.00	0.00	20.9
18	27	-0	-1539	0	0	0	660	--	--	16.08	16.08	0.00	0.01	0.01	0.10	0.00	0.00	20.9
19	27	-0	-908	0	0	0	337	--	--	16.08	16.08	0.00	0.01	0.01	0.06	0.00	0.00	20.9
20	27	-0	-872	0	0	0	300	--	--	16.08	16.08	0.00	0.01	0.01	0.05	0.00	0.00	20.9
37	27	-0	-1652	0	0	0	701	--	--	16.08	16.08	0.00	0.01	0.01	0.10	0.00	0.00	20.9
38	27	-0	-601	0	0	0	-166	--	--	16.08	16.08	0.18	0.00	0.00	0.04	0.00	0.00	20.9
39	27	-0	-541	0	0	0	-195	--	--	16.08	16.08	0.18	0.00	0.00	0.03	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	-925	0	0	0	-203	--	--	16.08	16.08	0.18	0.00	0.01	0.06	0.00	0.00	20.9
2	55	-0	-761	0	0	0	-163	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
3	55	-0	-711	0	0	0	-165	--	--	16.08	16.08	0.29	0.00	0.01	0.04	0.00	0.00	20.9
4	55	-0	-712	0	0	0	-147	--	--	16.08	16.08	0.29	0.00	0.01	0.04	0.00	0.00	20.9
5	55	-0	-662	0	0	0	-150	--	--	16.08	16.08	0.29	0.00	0.01	0.04	0.00	0.00	20.9
6	55	-0	-802	0	0	0	-155	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
7	55	-0	-636	0	0	0	-162	--	--	16.08	16.08	0.29	0.00	0.01	0.04	0.00	0.00	20.9
8	55	-0	-787	0	0	0	-150	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
9	55	-0	-621	0	0	0	-158	--	--	16.08	16.08	0.29	0.00	0.01	0.04	0.00	0.00	20.9
10	55	-0	-761	0	0	0	-163	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
11	55	-0	-711	0	0	0	-165	--	--	16.08	16.08	0.29	0.00	0.01	0.04	0.00	0.00	20.9
12	55	-0	-712	0	0	0	-147	--	--	16.08	16.08	0.29	0.00	0.01	0.04	0.00	0.00	20.9
13	55	-0	-662	0	0	0	-150	--	--	16.08	16.08	0.29	0.00	0.01	0.04	0.00	0.00	20.9
14	55	-0	-802	0	0	0	-155	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
15	55	-0	-636	0	0	0	-162	--	--	16.08	16.08	0.29	0.00	0.01	0.04	0.00	0.00	20.9
16	55	-0	-787	0	0	0	-150	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
17	55	-0	-621	0	0	0	-158	--	--	16.08	16.08	0.29	0.00	0.01	0.04	0.00	0.00	20.9
18	55	-0	-1539	0	0	0	-179	--	--	16.08	16.08	0.18	0.00	0.01	0.10	0.00	0.00	20.9
19	55	-0	-908	0	0	0	-159	--	--	16.08	16.08	0.18	0.00	0.01	0.06	0.00	0.00	20.9
20	55	-0	-872	0	0	0	-176	--	--	16.08	16.08	0.18	0.00	0.01	0.05	0.00	0.00	20.9
37	55	-0	-1652	0	0	0	-200	--	--	16.08	16.08	0.18	0.00	0.01	0.10	0.00	0.00	20.9
38	55	-0	-601	0	0	0	-166	--	--	16.08	16.08	0.18	0.00	0.00	0.04	0.00	0.00	20.9
39	55	-0	-541	0	0	0	-195	--	--	16.08	16.08	0.18	0.00	0.00	0.03	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 52 NI 1714 NF 1713 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-1693	0	0	0	836	--	--	16.08	16.08	0.00	0.01	0.01	0.11	0.00	0.00	20.9
2	0	-0	-1358	0	0	0	671	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
3	0	-0	-1306	0	0	0	632	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
4	0	-0	-1298	0	0	0	654	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
5	0	-0	-1246	0	0	0	615	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
6	0	-0	-1398	0	0	0	712	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
7	0	-0	-1225	0	0	0	579	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
8	0	-0	-1380	0	0	0	707	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
9	0	-0	-1207	0	0	0	574	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
10	0	-0	-1358	0	0	0	671	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
11	0	-0	-1306	0	0	0	632	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
12	0	-0	-1298	0	0	0	654	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
13	0	-0	-1246	0	0	0	615	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
14	0	-0	-1398	0	0	0	712	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
15	0	-0	-1225	0	0	0	579	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
16	0	-0	-1380	0	0	0	707	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
17	0	-0	-1207	0	0	0	574	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
18	0	-0	-2700	0	0	0	1485	--	--	16.08	16.08	0.00	0.03	0.02	0.17	0.00	0.00	20.9
19	0	-0	-1785	0	0	0	962	--	--	16.08	16.08	0.00	0.02	0.01	0.11	0.00	0.00	20.9
20	0	-0	-1820	0	0	0	927	--	--	16.08	16.08	0.00	0.02	0.02	0.11	0.00	0.00	20.9
37	0	-0	-2828	0	0	0	1531	--	--	16.08	16.08	0.00	0.03	0.02	0.18	0.00	0.00	20.9
38	0	-0	-1303	0	0	0	659	--	--	16.08	16.08	0.00	0.01	0.01	0.08	0.00	0.00	20.9
39	0	-0	-1362	0	0	0	600	--	--	16.08	16.08	0.00	0.01	0.01	0.09	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-1693	0	0	0	836	--	--	16.08	16.08	0.00	0.01	0.01	0.11	0.00	0.00	20.9
2	27	-0	-1358	0	0	0	671	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
3	27	-0	-1306	0	0	0	632	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
4	27	-0	-1298	0	0	0	654	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
5	27	-0	-1246	0	0	0	615	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
6	27	-0	-1398	0	0	0	712	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
7	27	-0	-1225	0	0	0	579	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
8	27	-0	-1380	0	0	0	707	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
9	27	-0	-1207	0	0	0	574	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
10	27	-0	-1358	0	0	0	671	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
11	27	-0	-1306	0	0	0	632	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
12	27	-0	-1298	0	0	0	654	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
13	27	-0	-1246	0	0	0	615	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
14	27	-0	-1398	0	0	0	712	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
15	27	-0	-1225	0	0	0	579	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
16	27	-0	-1380	0	0	0	707	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
17	27	-0	-1207	0	0	0	574	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
18	27	-0	-2700	0	0	0	1485	--	--	16.08	16.08	0.00	0.03	0.02	0.17	0.00	0.00	20.9
19	27	-0	-1785	0	0	0	962	--	--	16.08	16.08	0.00	0.02	0.01	0.11	0.00	0.00	20.9
20	27	-0	-1820	0	0	0	927	--	--	16.08	16.08	0.00	0.02	0.02	0.11	0.00	0.00	20.9
37	27	-0	-2828	0	0	0	1531	--	--	16.08	16.08	0.00	0.03	0.02	0.18	0.00	0.00	20.9
38	27	-0	-1303	0	0	0	659	--	--	16.08	16.08	0.00	0.01	0.01	0.08	0.00	0.00	20.9
39	27	-0	-1362	0	0	0	600	--	--	16.08	16.08	0.00	0.01	0.01	0.09	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	-1693	0	0	0	-88	--	--	16.08	16.08	0.18	0.00	0.01	0.11	0.00	0.00	20.9
2	55	-0	-1358	0	0	0	-70	--	--	16.08	16.08	0.29	0.00	0.01	0.09	0.00	0.00	20.9
3	55	-0	-1306	0	0	0	-81	--	--	16.08	16.08	0.29	0.00	0.01	0.08	0.00	0.00	20.9
4	55	-0	-1298	0	0	0	-54	--	--	16.08	16.08	0.29	0.00	0.01	0.08	0.00	0.00	20.9
5	55	-0	-1246	0	0	0	-65	--	--	16.08	16.08	0.29	0.00	0.01	0.08	0.00	0.00	20.9
6	55	-0	-1398	0	0	0	-51	--	--	16.08	16.08	0.29	0.00	0.01	0.09	0.00	0.00	20.9
7	55	-0	-1225	0	0	0	-89	--	--	16.08	16.08	0.29	0.00	0.01	0.08	0.00	0.00	20.9
8	55	-0	-1380	0	0	0	-46	--	--	16.08	16.08	0.29	0.00	0.01	0.09	0.00	0.00	20.9
9	55	-0	-1207	0	0	0	-84	--	--	16.08	16.08	0.29	0.00	0.01	0.08	0.00	0.00	20.9
10	55	-0	-1358	0	0	0	-70	--	--	16.08	16.08	0.29	0.00	0.01	0.09	0.00	0.00	20.9
11	55	-0	-1306	0	0	0	-81	--	--	16.08	16.08	0.29	0.00	0.01	0.08	0.00	0.00	20.9
12	55	-0	-1298	0	0	0	-54	--	--	16.08	16.08	0.29	0.00	0.01	0.08	0.00	0.00	20.9
13	55	-0	-1246	0	0	0	-65	--	--	16.08	16.08	0.29	0.00	0.01	0.08	0.00	0.00	20.9
14	55	-0	-1398	0	0	0	-51	--	--	16.08	16.08	0.29	0.00	0.01	0.09	0.00	0.00	20.9
15	55	-0	-1225	0	0	0	-89	--	--	16.08	16.08	0.29	0.00	0.01	0.08	0.00	0.00	20.9
16	55	-0	-1380	0	0	0	-46	--	--	16.08	16.08	0.29	0.00	0.01	0.09	0.00	0.00	20.9
17	55	-0	-1207	0	0	0	-84	--	--	16.08	16.08	0.29	0.00	0.01	0.08	0.00	0.00	20.9
18	55	-0	-2700	0	0	0	12	--	--	16.08	16.08	0.00	0.00	0.02	0.17	0.00	0.00	20.9
19	55	-0	-1785	0	0	0	-12	--	--	16.08	16.08	0.18	0.00	0.01	0.11	0.00	0.00	20.9
20	55	-0	-1820	0	0	0	-66	--	--	16.08	16.08	0.18	0.00	0.02	0.11	0.00	0.00	20.9
37	55	-0	-2828	0	0	0	-12	--	--	16.08	16.08	0.18	0.00	0.02	0.18	0.00	0.00	20.9
38	55	-0	-1303	0	0	0	-51	--	--	16.08	16.08	0.18	0.00	0.01	0.08	0.00	0.00	20.9
39	55	-0	-1362	0	0	0	-142	--	--	16.08	16.08	0.18	0.00	0.01	0.09	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 53 NI 1715 NF 1714 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-2726	0	0	0	1739	--	--	16.08	16.08	0.00	0.03	0.02	0.17	0.00	0.00	20.9
2	0	-0	-2141	0	0	0	1360	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
3	0	-0	-2093	0	0	0	1314	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
4	0	-0	-2101	0	0	0	1360	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
5	0	-0	-2053	0	0	0	1315	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
6	0	-0	-2183	0	0	0	1413	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
7	0	-0	-2023	0	0	0	1261	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
8	0	-0	-2171	0	0	0	1413	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
9	0	-0	-2011	0	0	0	1261	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
10	0	-0	-2141	0	0	0	1360	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
11	0	-0	-2093	0	0	0	1314	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
12	0	-0	-2101	0	0	0	1360	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
13	0	-0	-2053	0	0	0	1315	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
14	0	-0	-2183	0	0	0	1413	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
15	0	-0	-2023	0	0	0	1261	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
16	0	-0	-2171	0	0	0	1413	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9

17	0	-0	-2011	0	0	0	1261	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
18	0	-0	-4230	0	0	0	2842	--	--	16.08	16.08	0.00	0.05	0.03	0.27	0.00	0.00	20.9
19	0	-0	-3122	0	0	0	2132	--	--	16.08	16.08	0.00	0.04	0.03	0.20	0.00	0.00	20.9
20	0	-0	-3181	0	0	0	2079	--	--	16.08	16.08	0.00	0.04	0.03	0.20	0.00	0.00	20.9
37	0	-0	-4294	0	0	0	2834	--	--	16.08	16.08	0.00	0.05	0.04	0.27	0.00	0.00	20.9
38	0	-0	-2447	0	0	0	1652	--	--	16.08	16.08	0.00	0.03	0.02	0.15	0.00	0.00	20.9
39	0	-0	-2546	0	0	0	1562	--	--	16.08	16.08	0.00	0.03	0.02	0.16	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-2726	0	0	0	1739	--	--	16.08	16.08	0.00	0.03	0.02	0.17	0.00	0.00	20.9
2	27	-0	-2141	0	0	0	1360	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
3	27	-0	-2093	0	0	0	1314	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
4	27	-0	-2101	0	0	0	1360	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
5	27	-0	-2053	0	0	0	1315	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
6	27	-0	-2183	0	0	0	1413	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
7	27	-0	-2023	0	0	0	1261	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
8	27	-0	-2171	0	0	0	1413	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
9	27	-0	-2011	0	0	0	1261	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
10	27	-0	-2141	0	0	0	1360	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
11	27	-0	-2093	0	0	0	1314	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
12	27	-0	-2101	0	0	0	1360	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
13	27	-0	-2053	0	0	0	1315	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
14	27	-0	-2183	0	0	0	1413	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
15	27	-0	-2023	0	0	0	1261	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
16	27	-0	-2171	0	0	0	1413	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
17	27	-0	-2011	0	0	0	1261	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
18	27	-0	-4230	0	0	0	2842	--	--	16.08	16.08	0.00	0.05	0.03	0.27	0.00	0.00	20.9
19	27	-0	-3122	0	0	0	2132	--	--	16.08	16.08	0.00	0.04	0.03	0.20	0.00	0.00	20.9
20	27	-0	-3181	0	0	0	2079	--	--	16.08	16.08	0.00	0.04	0.03	0.20	0.00	0.00	20.9
37	27	-0	-4294	0	0	0	2834	--	--	16.08	16.08	0.00	0.05	0.04	0.27	0.00	0.00	20.9
38	27	-0	-2447	0	0	0	1652	--	--	16.08	16.08	0.00	0.03	0.02	0.15	0.00	0.00	20.9
39	27	-0	-2546	0	0	0	1562	--	--	16.08	16.08	0.00	0.03	0.02	0.16	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	-2726	0	0	0	251	--	--	16.08	16.08	0.00	0.00	0.02	0.17	0.00	0.00	20.9
2	55	-0	-2141	0	0	0	192	--	--	16.08	16.08	0.10	0.00	0.02	0.13	0.00	0.00	20.9
3	55	-0	-2093	0	0	0	173	--	--	16.08	16.08	0.10	0.00	0.02	0.13	0.00	0.00	20.9
4	55	-0	-2101	0	0	0	214	--	--	16.08	16.08	0.10	0.00	0.02	0.13	0.00	0.00	20.9
5	55	-0	-2053	0	0	0	195	--	--	16.08	16.08	0.10	0.00	0.02	0.13	0.00	0.00	20.9
6	55	-0	-2183	0	0	0	223	--	--	16.08	16.08	0.10	0.00	0.02	0.14	0.00	0.00	20.9
7	55	-0	-2023	0	0	0	158	--	--	16.08	16.08	0.10	0.00	0.02	0.13	0.00	0.00	20.9
8	55	-0	-2171	0	0	0	229	--	--	16.08	16.08	0.10	0.00	0.02	0.14	0.00	0.00	20.9
9	55	-0	-2011	0	0	0	164	--	--	16.08	16.08	0.10	0.00	0.02	0.13	0.00	0.00	20.9
10	55	-0	-2141	0	0	0	192	--	--	16.08	16.08	0.10	0.00	0.02	0.13	0.00	0.00	20.9
11	55	-0	-2093	0	0	0	173	--	--	16.08	16.08	0.10	0.00	0.02	0.13	0.00	0.00	20.9
12	55	-0	-2101	0	0	0	214	--	--	16.08	16.08	0.10	0.00	0.02	0.13	0.00	0.00	20.9
13	55	-0	-2053	0	0	0	195	--	--	16.08	16.08	0.10	0.00	0.02	0.13	0.00	0.00	20.9
14	55	-0	-2183	0	0	0	223	--	--	16.08	16.08	0.10	0.00	0.02	0.14	0.00	0.00	20.9
15	55	-0	-2023	0	0	0	158	--	--	16.08	16.08	0.10	0.00	0.02	0.13	0.00	0.00	20.9
16	55	-0	-2171	0	0	0	229	--	--	16.08	16.08	0.10	0.00	0.02	0.14	0.00	0.00	20.9
17	55	-0	-2011	0	0	0	164	--	--	16.08	16.08	0.10	0.00	0.02	0.13	0.00	0.00	20.9
18	55	-0	-4230	0	0	0	534	--	--	16.08	16.08	0.00	0.01	0.03	0.27	0.00	0.00	20.9
19	55	-0	-3122	0	0	0	430	--	--	16.08	16.08	0.00	0.01	0.03	0.20	0.00	0.00	20.9
20	55	-0	-3181	0	0	0	344	--	--	16.08	16.08	0.00	0.01	0.03	0.20	0.00	0.00	20.9
37	55	-0	-4294	0	0	0	491	--	--	16.08	16.08	0.00	0.01	0.04	0.27	0.00	0.00	20.9
38	55	-0	-2447	0	0	0	317	--	--	16.08	16.08	0.00	0.01	0.02	0.15	0.00	0.00	20.9
39	55	-0	-2546	0	0	0	174	--	--	16.08	16.08	0.00	0.00	0.02	0.16	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 54 NI 1711 NF 1715 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-2734	0	0	0	2176	--	--	16.08	16.08	0.00	0.04	0.02	0.17	0.00	0.00	20.9
2	0	-0	-2170	0	0	0	1714	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
3	0	-0	-2165	0	0	0	1690	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
4	0	-0	-2042	0	0	0	1657	--	--	16.08	16.08	0.10	0.03	0.02	0.13	0.00	0.00	20.9
5	0	-0	-2037	0	0	0	1633	--	--	16.08	16.08	0.10	0.03	0.02	0.13	0.00	0.00	20.9
6	0	-0	-2132	0	0	0	1722	--	--	16.08	16.08	0.10	0.03	0.02	0.13	0.00	0.00	20.9
7	0	-0	-2114	0	0	0	1643	--	--	16.08	16.08	0.10	0.03	0.02	0.13	0.00	0.00	20.9
8	0	-0	-2093	0	0	0	1705	--	--	16.08	16.08	0.10	0.03	0.02	0.13	0.00	0.00	20.9
9	0	-0	-2075	0	0	0	1626	--	--	16.08	16.08	0.10	0.03	0.02	0.13	0.00	0.00	20.9
10	0	-0	-2170	0	0	0	1714	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
11	0	-0	-2165	0	0	0	1690	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
12	0	-0	-2042	0	0	0	1657	--	--	16.08	16.08	0.10	0.03	0.02	0.13	0.00	0.00	20.9
13	0	-0	-2037	0	0	0	1633	--	--	16.08	16.08	0.10	0.03	0.02	0.13	0.00	0.00	20.9
14	0	-0	-2132	0	0	0	1722	--	--	16.08	16.08	0.10	0.03	0.02	0.13	0.00	0.00	20.9
15	0	-0	-2114	0	0	0	1643	--	--	16.08	16.08	0.10	0.03	0.02	0.13	0.00	0.00	20.9
16	0	-0	-2093	0	0	0	1705	--	--	16.08	16.08	0.10	0.03	0.02	0.13	0.00	0.00	20.9
17	0	-0	-2075	0	0	0	1626	--	--	16.08	16.08	0.10	0.03	0.02	0.13	0.00	0.00	20.9
18	0	-0	-4333	0	0	0	3567	--	--	16.08	16.08	0.00	0.06	0.04	0.27	0.00	0.00	20.9
19	0	-0	-2674	0	0	0	2368	--	--	16.08	16.08	0.00	0.04	0.02	0.17	0.00	0.00	20.9
20	0	-0	-3146	0	0	0	2584	--	--	16.08	16.08	0.00	0.04	0.03	0.20	0.00	0.00	20.9
37	0	-0	-4641	0	0	0	3710	--	--	16.08	16.08	0.00	0.06	0.04	0.29	0.00	0.00	20.9
38	0	-0	-1875	0	0	0	1711	--	--	16.08	16.08	0.00	0.03	0.02	0.12	0.00	0.00	20.9
39	0	-0	-2663	0	0	0	2071	--	--	16.08	16.08	0.00	0.04	0.02	0.17	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-2734	0	0	0	2176	--	--	16.08	16.08	0.00	0.04	0.02	0.17	0.00	0.00	20.9
2	27	-0	-2170	0	0	0	1714	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
3	27	-0	-2165	0	0	0	1690	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
4	27	-0	-2042	0	0	0	1657	--	--	16.08	16.08	0.10	0.03	0.02	0.13	0.00	0.00	20.9
5	27	-0	-2037	0	0	0	1633	--	--	16.08	16.08	0.10	0.03	0.02	0.13	0.00	0.00	20.9
6	27	-0	-2132	0	0	0	1722	--	--	16.08	16.08	0.10	0.03	0.02	0.13	0.00	0.00	20.9
7	27	-0	-2114	0	0	0	1643	--	--	16.08	16.08	0.10	0.03	0.02	0.13	0.00	0.00	20.9
8	27	-0	-2093	0	0	0	1705	--	--	16.08	16.08	0.10	0.03	0.02	0.13	0.00	0.00	20.9
9	27	-0	-2075	0	0	0	1626	--	--	16.08	16.08	0.10	0.03	0.02	0.13	0.00	0.00	20.9
10	27	-0	-2170	0	0	0	1714	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
11	27	-0	-2165	0	0	0	1690	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
12	27	-0	-2042	0	0	0	1657	--	--	16.08	16.08	0.10	0.03	0.02	0.13	0.00	0.00	20.9

13	27	-0	-2037	0	0	0	1633	--	--	16.08	16.08	0.10	0.03	0.02	0.13	0.00	0.00	20.9
14	27	-0	-2132	0	0	0	1722	--	--	16.08	16.08	0.10	0.03	0.02	0.13	0.00	0.00	20.9
15	27	-0	-2114	0	0	0	1643	--	--	16.08	16.08	0.10	0.03	0.02	0.13	0.00	0.00	20.9
16	27	-0	-2093	0	0	0	1705	--	--	16.08	16.08	0.10	0.03	0.02	0.13	0.00	0.00	20.9
17	27	-0	-2075	0	0	0	1626	--	--	16.08	16.08	0.10	0.03	0.02	0.13	0.00	0.00	20.9
18	27	-0	-4333	0	0	0	3567	--	--	16.08	16.08	0.00	0.06	0.04	0.27	0.00	0.00	20.9
19	27	-0	-2674	0	0	0	2368	--	--	16.08	16.08	0.00	0.04	0.02	0.17	0.00	0.00	20.9
20	27	-0	-3146	0	0	0	2584	--	--	16.08	16.08	0.00	0.04	0.03	0.20	0.00	0.00	20.9
37	27	-0	-4641	0	0	0	3710	--	--	16.08	16.08	0.00	0.06	0.04	0.29	0.00	0.00	20.9
38	27	-0	-1875	0	0	0	1711	--	--	16.08	16.08	0.00	0.03	0.02	0.12	0.00	0.00	20.9
39	27	-0	-2663	0	0	0	2071	--	--	16.08	16.08	0.00	0.04	0.02	0.17	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	-2734	0	0	0	684	--	--	16.08	16.08	0.00	0.01	0.02	0.17	0.00	0.00	20.9
2	55	-0	-2170	0	0	0	530	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
3	55	-0	-2165	0	0	0	509	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
4	55	-0	-2042	0	0	0	543	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
5	55	-0	-2037	0	0	0	522	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
6	55	-0	-2132	0	0	0	559	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
7	55	-0	-2114	0	0	0	490	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
8	55	-0	-2093	0	0	0	563	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
9	55	-0	-2075	0	0	0	494	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
10	55	-0	-2170	0	0	0	530	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
11	55	-0	-2165	0	0	0	509	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
12	55	-0	-2042	0	0	0	543	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
13	55	-0	-2037	0	0	0	522	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
14	55	-0	-2132	0	0	0	559	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
15	55	-0	-2114	0	0	0	490	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
16	55	-0	-2093	0	0	0	563	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
17	55	-0	-2075	0	0	0	494	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
18	55	-0	-4333	0	0	0	1204	--	--	16.08	16.08	0.00	0.02	0.04	0.27	0.00	0.00	20.9
19	55	-0	-2674	0	0	0	910	--	--	16.08	16.08	0.00	0.02	0.02	0.17	0.00	0.00	20.9
20	55	-0	-3146	0	0	0	868	--	--	16.08	16.08	0.00	0.01	0.03	0.20	0.00	0.00	20.9
37	55	-0	-4641	0	0	0	1178	--	--	16.08	16.08	0.00	0.02	0.04	0.29	0.00	0.00	20.9
38	55	-0	-1875	0	0	0	688	--	--	16.08	16.08	0.00	0.01	0.02	0.12	0.00	0.00	20.9
39	55	-0	-2663	0	0	0	619	--	--	16.08	16.08	0.00	0.01	0.02	0.17	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 55 NI 1569 NF 1711 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	1015	0	0	0	715	--	--	16.08	16.08	0.00	0.01	0.01	0.06	0.00	0.00	20.9
2	0	-0	492	0	0	0	722	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
3	0	-0	431	0	0	0	724	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
4	0	-0	1130	0	0	0	375	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
5	0	-0	1069	0	0	0	377	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
6	0	-0	787	0	0	0	599	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
7	0	-0	583	0	0	0	604	--	--	16.08	16.08	0.10	0.01	0.00	0.04	0.00	0.00	20.9
8	0	-0	978	0	0	0	495	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
9	0	-0	775	0	0	0	501	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
10	0	-0	492	0	0	0	722	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
11	0	-0	431	0	0	0	724	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
12	0	-0	1130	0	0	0	375	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
13	0	-0	1069	0	0	0	377	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
14	0	-0	787	0	0	0	599	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
15	0	-0	583	0	0	0	604	--	--	16.08	16.08	0.10	0.01	0.00	0.04	0.00	0.00	20.9
16	0	-0	978	0	0	0	495	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
17	0	-0	775	0	0	0	501	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
18	0	-0	665	0	0	0	1774	--	--	16.08	16.08	0.00	0.03	0.01	0.04	0.00	0.00	20.9
19	0	-0	4439	0	0	0	-873	--	--	16.08	16.08	0.18	0.01	0.04	0.28	0.00	0.00	20.9
20	0	-0	2382	0	0	0	286	--	--	16.08	16.08	0.00	0.00	0.02	0.15	0.00	0.00	20.9
37	0	-0	-1095	0	0	0	2742	--	--	16.08	16.08	0.00	0.05	0.01	0.07	0.00	0.00	20.9
38	0	-0	5193	0	0	0	-1668	--	--	16.08	16.08	0.18	0.03	0.04	0.33	0.00	0.00	20.9
39	0	-0	1765	0	0	0	262	--	--	16.08	16.08	0.00	0.00	0.01	0.11	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	1015	0	0	0	2076	--	--	16.08	16.08	0.00	0.04	0.01	0.06	0.00	0.00	20.9
2	27	-0	492	0	0	0	1383	--	--	16.08	16.08	0.10	0.02	0.00	0.03	0.00	0.00	20.9
3	27	-0	431	0	0	0	1303	--	--	16.08	16.08	0.10	0.02	0.00	0.03	0.00	0.00	20.9
4	27	-0	1130	0	0	0	1891	--	--	16.08	16.08	0.10	0.03	0.01	0.07	0.00	0.00	20.9
5	27	-0	1069	0	0	0	1811	--	--	16.08	16.08	0.10	0.03	0.01	0.07	0.00	0.00	20.9
6	27	-0	787	0	0	0	1654	--	--	16.08	16.08	0.10	0.03	0.01	0.05	0.00	0.00	20.9
7	27	-0	583	0	0	0	1387	--	--	16.08	16.08	0.10	0.02	0.00	0.04	0.00	0.00	20.9
8	27	-0	978	0	0	0	1808	--	--	16.08	16.08	0.10	0.03	0.01	0.06	0.00	0.00	20.9
9	27	-0	775	0	0	0	1540	--	--	16.08	16.08	0.10	0.03	0.01	0.05	0.00	0.00	20.9
10	27	-0	492	0	0	0	1383	--	--	16.08	16.08	0.10	0.02	0.00	0.03	0.00	0.00	20.9
11	27	-0	431	0	0	0	1303	--	--	16.08	16.08	0.10	0.02	0.00	0.03	0.00	0.00	20.9
12	27	-0	1130	0	0	0	1891	--	--	16.08	16.08	0.10	0.03	0.01	0.07	0.00	0.00	20.9
13	27	-0	1069	0	0	0	1811	--	--	16.08	16.08	0.10	0.03	0.01	0.07	0.00	0.00	20.9
14	27	-0	787	0	0	0	1654	--	--	16.08	16.08	0.10	0.03	0.01	0.05	0.00	0.00	20.9
15	27	-0	583	0	0	0	1387	--	--	16.08	16.08	0.10	0.02	0.00	0.04	0.00	0.00	20.9
16	27	-0	978	0	0	0	1808	--	--	16.08	16.08	0.10	0.03	0.01	0.06	0.00	0.00	20.9
17	27	-0	775	0	0	0	1540	--	--	16.08	16.08	0.10	0.03	0.01	0.05	0.00	0.00	20.9
18	27	-0	665	0	0	0	2667	--	--	16.08	16.08	0.00	0.05	0.01	0.04	0.00	0.00	20.9
19	27	-0	4439	0	0	0	5082	--	--	16.08	16.08	0.00	0.09	0.04	0.28	0.00	0.00	20.9
20	27	-0	2382	0	0	0	3481	--	--	16.08	16.08	0.00	0.06	0.02	0.15	0.00	0.00	20.9
37	27	-0	-1095	0	0	0	2742	--	--	16.08	16.08	0.00	0.05	0.01	0.07	0.00	0.00	20.9
38	27	-0	5193	0	0	0	-1668	--	--	16.08	16.08	0.18	0.03	0.04	0.33	0.00	0.00	20.9
39	27	-0	1765	0	0	0	2629	--	--	16.08	16.08	0.00	0.04	0.01	0.11	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	1015	0	0	0	1268	--	--	16.08	16.08	0.00	0.02	0.01	0.06	0.00	0.00	20.9
2	55	-0	492	0	0	0	991	--	--	16.08	16.08	0.10	0.02	0.00	0.03	0.00	0.00	20.9
3	55	-0	431	0	0	0	959	--	--	16.08	16.08	0.10	0.02	0.00	0.03	0.00	0.00	20.9
4	55	-0	1130	0	0	0	992	--	--	16.08	16.08	0.10	0.02	0.01	0.07	0.00	0.00	20.9
5	55	-0	1069	0	0	0	960	--	--	16.08	16.08	0.10	0.02	0.01	0.07	0.00	0.00	20.9
6	55	-0	787	0	0	0	1028	--	--	16.08	16.08	0.10	0.02	0.01	0.05	0.00	0.00	20.9
7	55	-0	583	0	0	0	923	--	--	16.08	16.08	0.10	0.02	0.00	0.04	0.00	0.00	20.9
8	55	-0	978	0	0	0	1029	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9

9	55	-0	775	0	0	0	923	--	--	16.08	16.08	0.10	0.02	0.01	0.05	0.00	0.00	20.9
10	55	-0	492	0	0	0	991	--	--	16.08	16.08	0.10	0.02	0.00	0.03	0.00	0.00	20.9
11	55	-0	431	0	0	0	959	--	--	16.08	16.08	0.10	0.02	0.00	0.03	0.00	0.00	20.9
12	55	-0	1130	0	0	0	992	--	--	16.08	16.08	0.10	0.02	0.01	0.07	0.00	0.00	20.9
13	55	-0	1069	0	0	0	960	--	--	16.08	16.08	0.10	0.02	0.01	0.07	0.00	0.00	20.9
14	55	-0	787	0	0	0	1028	--	--	16.08	16.08	0.10	0.02	0.01	0.05	0.00	0.00	20.9
15	55	-0	583	0	0	0	923	--	--	16.08	16.08	0.10	0.02	0.00	0.04	0.00	0.00	20.9
16	55	-0	978	0	0	0	1029	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9
17	55	-0	775	0	0	0	923	--	--	16.08	16.08	0.10	0.02	0.01	0.05	0.00	0.00	20.9
18	55	-0	665	0	0	0	2137	--	--	16.08	16.08	0.00	0.04	0.01	0.04	0.00	0.00	20.9
19	55	-0	4439	0	0	0	1549	--	--	16.08	16.08	0.00	0.03	0.04	0.28	0.00	0.00	20.9
20	55	-0	2382	0	0	0	1585	--	--	16.08	16.08	0.00	0.03	0.02	0.15	0.00	0.00	20.9
37	55	-0	-1095	0	0	0	2145	--	--	16.08	16.08	0.00	0.04	0.01	0.07	0.00	0.00	20.9
38	55	-0	5193	0	0	0	1164	--	--	16.08	16.08	0.00	0.02	0.04	0.33	0.00	0.00	20.9
39	55	-0	1765	0	0	0	1224	--	--	16.08	16.08	0.00	0.02	0.01	0.11	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 56 NI 1710 NF 1569 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-1297	0	0	0	1112	--	--	16.08	16.08	0.00	0.02	0.01	0.08	0.00	0.00	20.9
2	0	-0	-644	0	0	0	910	--	--	16.08	16.08	0.10	0.02	0.01	0.04	0.00	0.00	20.9
3	0	-0	-613	0	0	0	879	--	--	16.08	16.08	0.10	0.02	0.01	0.04	0.00	0.00	20.9
4	0	-0	-1383	0	0	0	832	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
5	0	-0	-1352	0	0	0	801	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
6	0	-0	-938	0	0	0	919	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9
7	0	-0	-836	0	0	0	815	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
8	0	-0	-1160	0	0	0	895	--	--	16.08	16.08	0.10	0.02	0.01	0.07	0.00	0.00	20.9
9	0	-0	-1058	0	0	0	792	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
10	0	-0	-644	0	0	0	910	--	--	16.08	16.08	0.10	0.02	0.01	0.04	0.00	0.00	20.9
11	0	-0	-613	0	0	0	879	--	--	16.08	16.08	0.10	0.02	0.01	0.04	0.00	0.00	20.9
12	0	-0	-1383	0	0	0	832	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
13	0	-0	-1352	0	0	0	801	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
14	0	-0	-938	0	0	0	919	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9
15	0	-0	-836	0	0	0	815	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
16	0	-0	-1160	0	0	0	895	--	--	16.08	16.08	0.10	0.02	0.01	0.07	0.00	0.00	20.9
17	0	-0	-1058	0	0	0	792	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
18	0	-0	-1225	0	0	0	2005	--	--	16.08	16.08	0.00	0.03	0.01	0.08	0.00	0.00	20.9
19	0	-0	-5162	0	0	0	1051	--	--	16.08	16.08	0.00	0.02	0.04	0.32	0.00	0.00	20.9
20	0	-0	-2136	0	0	0	891	--	--	16.08	16.08	0.00	0.02	0.02	0.13	0.00	0.00	20.9
37	0	-0	710	0	0	0	2186	--	--	16.08	16.08	0.00	0.04	0.01	0.04	0.00	0.00	20.9
38	0	-0	-5851	0	0	0	595	--	--	16.08	16.08	0.00	0.01	0.05	0.37	0.00	0.00	20.9
39	0	-0	-808	0	0	0	329	--	--	16.08	16.08	0.00	0.01	0.01	0.05	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-1297	0	0	0	1112	--	--	16.08	16.08	0.00	0.02	0.01	0.08	0.00	0.00	20.9
2	27	-0	-644	0	0	0	910	--	--	16.08	16.08	0.10	0.02	0.01	0.04	0.00	0.00	20.9
3	27	-0	-613	0	0	0	879	--	--	16.08	16.08	0.10	0.02	0.01	0.04	0.00	0.00	20.9
4	27	-0	-1383	0	0	0	832	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
5	27	-0	-1352	0	0	0	801	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
6	27	-0	-938	0	0	0	919	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9
7	27	-0	-836	0	0	0	815	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
8	27	-0	-1160	0	0	0	895	--	--	16.08	16.08	0.10	0.02	0.01	0.07	0.00	0.00	20.9
9	27	-0	-1058	0	0	0	792	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
10	27	-0	-644	0	0	0	910	--	--	16.08	16.08	0.10	0.02	0.01	0.04	0.00	0.00	20.9
11	27	-0	-613	0	0	0	879	--	--	16.08	16.08	0.10	0.02	0.01	0.04	0.00	0.00	20.9
12	27	-0	-1383	0	0	0	832	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
13	27	-0	-1352	0	0	0	801	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
14	27	-0	-938	0	0	0	919	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9
15	27	-0	-836	0	0	0	815	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
16	27	-0	-1160	0	0	0	895	--	--	16.08	16.08	0.10	0.02	0.01	0.07	0.00	0.00	20.9
17	27	-0	-1058	0	0	0	792	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
18	27	-0	-1225	0	0	0	2005	--	--	16.08	16.08	0.00	0.03	0.01	0.08	0.00	0.00	20.9
19	27	-0	-5162	0	0	0	-1765	--	--	16.08	16.08	0.18	0.03	0.04	0.32	0.00	0.00	20.9
20	27	-0	-2136	0	0	0	891	--	--	16.08	16.08	0.00	0.02	0.02	0.13	0.00	0.00	20.9
37	27	-0	710	0	0	0	3139	--	--	16.08	16.08	0.00	0.05	0.01	0.04	0.00	0.00	20.9
38	27	-0	-5851	0	0	0	-2597	--	--	16.08	16.08	0.18	0.04	0.05	0.37	0.00	0.00	20.9
39	27	-0	-808	0	0	0	329	--	--	16.08	16.08	0.00	0.01	0.01	0.05	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	-1297	0	0	0	404	--	--	16.08	16.08	0.00	0.01	0.01	0.08	0.00	0.00	20.9
2	55	-0	-644	0	0	0	559	--	--	16.08	16.08	0.10	0.01	0.01	0.04	0.00	0.00	20.9
3	55	-0	-613	0	0	0	544	--	--	16.08	16.08	0.10	0.01	0.01	0.04	0.00	0.00	20.9
4	55	-0	-1383	0	0	0	78	--	--	16.08	16.08	0.10	0.00	0.01	0.09	0.00	0.00	20.9
5	55	-0	-1352	0	0	0	63	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
6	55	-0	-938	0	0	0	407	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
7	55	-0	-836	0	0	0	359	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
8	55	-0	-1160	0	0	0	263	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
9	55	-0	-1058	0	0	0	215	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
10	55	-0	-644	0	0	0	559	--	--	16.08	16.08	0.10	0.01	0.01	0.04	0.00	0.00	20.9
11	55	-0	-613	0	0	0	544	--	--	16.08	16.08	0.10	0.01	0.01	0.04	0.00	0.00	20.9
12	55	-0	-1383	0	0	0	78	--	--	16.08	16.08	0.10	0.00	0.01	0.09	0.00	0.00	20.9
13	55	-0	-1352	0	0	0	63	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
14	55	-0	-938	0	0	0	407	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
15	55	-0	-836	0	0	0	359	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
16	55	-0	-1160	0	0	0	263	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
17	55	-0	-1058	0	0	0	215	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
18	55	-0	-1225	0	0	0	1337	--	--	16.08	16.08	0.00	0.02	0.01	0.08	0.00	0.00	20.9
19	55	-0	-5162	0	0	0	-1765	--	--	16.08	16.08	0.18	0.03	0.04	0.32	0.00	0.00	20.9
20	55	-0	-2136	0	0	0	-274	--	--	16.08	16.08	0.18	0.00	0.02	0.13	0.00	0.00	20.9
37	55	-0	710	0	0	0	2573	--	--	16.08	16.08	0.00	0.04	0.01	0.04	0.00	0.00	20.9
38	55	-0	-5851	0	0	0	-2597	--	--	16.08	16.08	0.18	0.04	0.05	0.37	0.00	0.00	20.9
39	55	-0	-808	0	0	0	-112	--	--	16.08	16.08	0.18	0.00	0.01	0.05	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 57 NI 1706 NF 1710 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	2766	0	0	0	563	--	--	16.08	16.08	0.00	0.01	0.02	0.17	0.00	0.00	20.9
2	0	-0	2181	0	0	0	475	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
3	0	-0	2202	0	0	0	430	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
4	0	-0	2053	0	0	0	437	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
5	0	-0	2074	0	0	0	392	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
6	0	-0	2113	0	0	0	514	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
7	0	-0	2181	0	0	0	364	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
8	0	-0	2074	0	0	0	503	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
9	0	-0	2143	0	0	0	352	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
10	0	-0	2181	0	0	0	475	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
11	0	-0	2202	0	0	0	430	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
12	0	-0	2053	0	0	0	437	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
13	0	-0	2074	0	0	0	392	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
14	0	-0	2113	0	0	0	514	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
15	0	-0	2181	0	0	0	364	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
16	0	-0	2074	0	0	0	503	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
17	0	-0	2143	0	0	0	352	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
18	0	-0	4224	0	0	0	1134	--	--	16.08	16.08	0.00	0.02	0.03	0.26	0.00	0.00	20.9
19	0	-0	2702	0	0	0	580	--	--	16.08	16.08	0.00	0.01	0.02	0.17	0.00	0.00	20.9
20	0	-0	4131	0	0	0	64	--	--	16.08	16.08	0.00	0.00	0.03	0.26	0.00	0.00	20.9
37	0	-0	4512	0	0	0	1219	--	--	16.08	16.08	0.00	0.02	0.04	0.28	0.00	0.00	20.9
38	0	-0	1976	0	0	0	295	--	--	16.08	16.08	0.00	0.01	0.02	0.12	0.00	0.00	20.9
39	0	-0	4357	0	0	0	-565	--	--	16.08	16.08	0.18	0.01	0.04	0.27	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	2766	0	0	0	4274	--	--	16.08	16.08	0.00	0.07	0.02	0.17	0.00	0.00	20.9
2	27	-0	2181	0	0	0	3401	--	--	16.08	16.08	0.10	0.06	0.02	0.14	0.00	0.00	20.9
3	27	-0	2202	0	0	0	3384	--	--	16.08	16.08	0.10	0.06	0.02	0.14	0.00	0.00	20.9
4	27	-0	2053	0	0	0	3191	--	--	16.08	16.08	0.10	0.06	0.02	0.13	0.00	0.00	20.9
5	27	-0	2074	0	0	0	3174	--	--	16.08	16.08	0.10	0.06	0.02	0.13	0.00	0.00	20.9
6	27	-0	2113	0	0	0	3348	--	--	16.08	16.08	0.10	0.06	0.02	0.13	0.00	0.00	20.9
7	27	-0	2181	0	0	0	3289	--	--	16.08	16.08	0.10	0.06	0.02	0.14	0.00	0.00	20.9
8	27	-0	2074	0	0	0	3285	--	--	16.08	16.08	0.10	0.06	0.02	0.13	0.00	0.00	20.9
9	27	-0	2143	0	0	0	3227	--	--	16.08	16.08	0.10	0.06	0.02	0.13	0.00	0.00	20.9
10	27	-0	2181	0	0	0	3401	--	--	16.08	16.08	0.10	0.06	0.02	0.14	0.00	0.00	20.9
11	27	-0	2202	0	0	0	3384	--	--	16.08	16.08	0.10	0.06	0.02	0.14	0.00	0.00	20.9
12	27	-0	2053	0	0	0	3191	--	--	16.08	16.08	0.10	0.06	0.02	0.13	0.00	0.00	20.9
13	27	-0	2074	0	0	0	3174	--	--	16.08	16.08	0.10	0.06	0.02	0.13	0.00	0.00	20.9
14	27	-0	2113	0	0	0	3348	--	--	16.08	16.08	0.10	0.06	0.02	0.13	0.00	0.00	20.9
15	27	-0	2181	0	0	0	3289	--	--	16.08	16.08	0.10	0.06	0.02	0.14	0.00	0.00	20.9
16	27	-0	2074	0	0	0	3285	--	--	16.08	16.08	0.10	0.06	0.02	0.13	0.00	0.00	20.9
17	27	-0	2143	0	0	0	3227	--	--	16.08	16.08	0.10	0.06	0.02	0.13	0.00	0.00	20.9
18	27	-0	4224	0	0	0	6800	--	--	16.08	16.08	0.00	0.12	0.03	0.26	0.00	0.00	20.9
19	27	-0	2702	0	0	0	4205	--	--	16.08	16.08	0.00	0.07	0.02	0.17	0.00	0.00	20.9
20	27	-0	4131	0	0	0	5605	--	--	16.08	16.08	0.00	0.10	0.03	0.26	0.00	0.00	20.9
37	27	-0	4512	0	0	0	7272	--	--	16.08	16.08	0.00	0.12	0.04	0.28	0.00	0.00	20.9
38	27	-0	1976	0	0	0	2946	--	--	16.08	16.08	0.00	0.05	0.02	0.12	0.00	0.00	20.9
39	27	-0	4357	0	0	0	5280	--	--	16.08	16.08	0.00	0.09	0.04	0.27	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	2766	0	0	0	2072	--	--	16.08	16.08	0.00	0.04	0.02	0.17	0.00	0.00	20.9
2	55	-0	2181	0	0	0	1665	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
3	55	-0	2202	0	0	0	1631	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
4	55	-0	2053	0	0	0	1557	--	--	16.08	16.08	0.10	0.03	0.02	0.13	0.00	0.00	20.9
5	55	-0	2074	0	0	0	1523	--	--	16.08	16.08	0.10	0.03	0.02	0.13	0.00	0.00	20.9
6	55	-0	2113	0	0	0	1666	--	--	16.08	16.08	0.10	0.03	0.02	0.13	0.00	0.00	20.9
7	55	-0	2181	0	0	0	1553	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
8	55	-0	2074	0	0	0	1634	--	--	16.08	16.08	0.10	0.03	0.02	0.13	0.00	0.00	20.9
9	55	-0	2143	0	0	0	1521	--	--	16.08	16.08	0.10	0.03	0.02	0.13	0.00	0.00	20.9
10	55	-0	2181	0	0	0	1665	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
11	55	-0	2202	0	0	0	1631	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
12	55	-0	2053	0	0	0	1557	--	--	16.08	16.08	0.10	0.03	0.02	0.13	0.00	0.00	20.9
13	55	-0	2074	0	0	0	1523	--	--	16.08	16.08	0.10	0.03	0.02	0.13	0.00	0.00	20.9
14	55	-0	2113	0	0	0	1666	--	--	16.08	16.08	0.10	0.03	0.02	0.13	0.00	0.00	20.9
15	55	-0	2181	0	0	0	1553	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
16	55	-0	2074	0	0	0	1634	--	--	16.08	16.08	0.10	0.03	0.02	0.13	0.00	0.00	20.9
17	55	-0	2143	0	0	0	1521	--	--	16.08	16.08	0.10	0.03	0.02	0.13	0.00	0.00	20.9
18	55	-0	4224	0	0	0	3438	--	--	16.08	16.08	0.00	0.06	0.03	0.26	0.00	0.00	20.9
19	55	-0	2702	0	0	0	2054	--	--	16.08	16.08	0.00	0.04	0.02	0.17	0.00	0.00	20.9
20	55	-0	4131	0	0	0	2317	--	--	16.08	16.08	0.00	0.04	0.03	0.26	0.00	0.00	20.9
37	55	-0	4512	0	0	0	3681	--	--	16.08	16.08	0.00	0.06	0.04	0.28	0.00	0.00	20.9
38	55	-0	1976	0	0	0	1373	--	--	16.08	16.08	0.00	0.02	0.02	0.12	0.00	0.00	20.9
39	55	-0	4357	0	0	0	1812	--	--	16.08	16.08	0.00	0.03	0.04	0.27	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 58 NI 1707 NF 1706 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	2939	0	0	0	109	--	--	16.08	16.08	0.00	0.00	0.02	0.18	0.00	0.00	20.9
2	0	-0	2247	0	0	0	120	--	--	16.08	16.08	0.10	0.00	0.02	0.14	0.00	0.00	20.9
3	0	-0	2302	0	0	0	71	--	--	16.08	16.08	0.10	0.00	0.02	0.14	0.00	0.00	20.9
4	0	-0	2220	0	0	0	97	--	--	16.08	16.08	0.10	0.00	0.02	0.14	0.00	0.00	20.9
5	0	-0	2275	0	0	0	48	--	--	16.08	16.08	0.10	0.00	0.02	0.14	0.00	0.00	20.9
6	0	-0	2174	0	0	0	170	--	--	16.08	16.08	0.10	0.00	0.02	0.14	0.00	0.00	20.9
7	0	-0	2356	0	0	0	5	--	--	16.08	16.08	0.10	0.00	0.02	0.15	0.00	0.00	20.9
8	0	-0	2166	0	0	0	163	--	--	16.08	16.08	0.10	0.00	0.02	0.14	0.00	0.00	20.9
9	0	-0	2348	0	0	0	-2	--	--	16.08	16.08	0.29	0.00	0.02	0.15	0.00	0.00	20.9
10	0	-0	2247	0	0	0	120	--	--	16.08	16.08	0.10	0.00	0.02	0.14	0.00	0.00	20.9
11	0	-0	2302	0	0	0	71	--	--	16.08	16.08	0.10	0.00	0.02	0.14	0.00	0.00	20.9
12	0	-0	2220	0	0	0	97	--	--	16.08	16.08	0.10	0.00	0.02	0.14	0.00	0.00	20.9
13	0	-0	2275	0	0	0	48	--	--	16.08	16.08	0.10	0.00	0.02	0.14	0.00	0.00	20.9
14	0	-0	2174	0	0	0	170	--	--	16.08	16.08	0.10	0.00	0.02	0.14	0.00	0.00	20.9
15	0	-0	2356	0	0	0	5	--	--	16.08	16.08	0.10	0.00	0.02	0.15	0.00	0.00	20.9
16	0	-0	2166	0	0	0	163	--	--	16.08	16.08	0.10	0.00	0.02	0.14	0.00	0.00	20.9

17	0	-0	2348	0	0	0	-2	--	--	16.08	16.08	0.29	0.00	0.02	0.15	0.00	0.00	20.9
18	0	-0	4419	0	0	0	451	--	--	16.08	16.08	0.00	0.01	0.04	0.28	0.00	0.00	20.9
19	0	-0	3382	0	0	0	99	--	--	16.08	16.08	0.00	0.00	0.03	0.21	0.00	0.00	20.9
20	0	-0	4681	0	0	0	-658	--	--	16.08	16.08	0.18	0.01	0.04	0.29	0.00	0.00	20.9
37	0	-0	4458	0	0	0	509	--	--	16.08	16.08	0.00	0.01	0.04	0.28	0.00	0.00	20.9
38	0	-0	2731	0	0	0	-78	--	--	16.08	16.08	0.18	0.00	0.02	0.17	0.00	0.00	20.9
39	0	-0	4896	0	0	0	-1338	--	--	16.08	16.08	0.18	0.02	0.04	0.31	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	2939	0	0	0	4052	--	--	16.08	16.08	0.00	0.07	0.02	0.18	0.00	0.00	20.9
2	27	-0	2247	0	0	0	3135	--	--	16.08	16.08	0.10	0.06	0.02	0.14	0.00	0.00	20.9
3	27	-0	2302	0	0	0	3159	--	--	16.08	16.08	0.10	0.06	0.02	0.14	0.00	0.00	20.9
4	27	-0	2220	0	0	0	3075	--	--	16.08	16.08	0.10	0.05	0.02	0.14	0.00	0.00	20.9
5	27	-0	2275	0	0	0	3100	--	--	16.08	16.08	0.10	0.06	0.02	0.14	0.00	0.00	20.9
6	27	-0	2174	0	0	0	3086	--	--	16.08	16.08	0.10	0.05	0.02	0.14	0.00	0.00	20.9
7	27	-0	2356	0	0	0	3166	--	--	16.08	16.08	0.10	0.06	0.02	0.15	0.00	0.00	20.9
8	27	-0	2166	0	0	0	3069	--	--	16.08	16.08	0.10	0.05	0.02	0.14	0.00	0.00	20.9
9	27	-0	2348	0	0	0	3148	--	--	16.08	16.08	0.10	0.06	0.02	0.15	0.00	0.00	20.9
10	27	-0	2247	0	0	0	3135	--	--	16.08	16.08	0.10	0.06	0.02	0.14	0.00	0.00	20.9
11	27	-0	2302	0	0	0	3159	--	--	16.08	16.08	0.10	0.06	0.02	0.14	0.00	0.00	20.9
12	27	-0	2220	0	0	0	3075	--	--	16.08	16.08	0.10	0.05	0.02	0.14	0.00	0.00	20.9
13	27	-0	2275	0	0	0	3100	--	--	16.08	16.08	0.10	0.06	0.02	0.14	0.00	0.00	20.9
14	27	-0	2174	0	0	0	3086	--	--	16.08	16.08	0.10	0.05	0.02	0.14	0.00	0.00	20.9
15	27	-0	2356	0	0	0	3166	--	--	16.08	16.08	0.10	0.06	0.02	0.15	0.00	0.00	20.9
16	27	-0	2166	0	0	0	3069	--	--	16.08	16.08	0.10	0.05	0.02	0.14	0.00	0.00	20.9
17	27	-0	2348	0	0	0	3148	--	--	16.08	16.08	0.10	0.06	0.02	0.15	0.00	0.00	20.9
18	27	-0	4419	0	0	0	6379	--	--	16.08	16.08	0.00	0.11	0.04	0.28	0.00	0.00	20.9
19	27	-0	3382	0	0	0	4635	--	--	16.08	16.08	0.00	0.08	0.03	0.21	0.00	0.00	20.9
20	27	-0	4681	0	0	0	5622	--	--	16.08	16.08	0.00	0.10	0.04	0.29	0.00	0.00	20.9
37	27	-0	4458	0	0	0	6490	--	--	16.08	16.08	0.00	0.11	0.04	0.28	0.00	0.00	20.9
38	27	-0	2731	0	0	0	3586	--	--	16.08	16.08	0.00	0.06	0.02	0.17	0.00	0.00	20.9
39	27	-0	4896	0	0	0	-1338	--	--	16.08	16.08	0.18	0.02	0.04	0.31	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	2939	0	0	0	1713	--	--	16.08	16.08	0.00	0.03	0.02	0.18	0.00	0.00	20.9
2	55	-0	2247	0	0	0	1346	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
3	55	-0	2302	0	0	0	1327	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
4	55	-0	2220	0	0	0	1308	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
5	55	-0	2275	0	0	0	1289	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
6	55	-0	2174	0	0	0	1356	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
7	55	-0	2356	0	0	0	1290	--	--	16.08	16.08	0.10	0.02	0.02	0.15	0.00	0.00	20.9
8	55	-0	2166	0	0	0	1345	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
9	55	-0	2348	0	0	0	1279	--	--	16.08	16.08	0.10	0.02	0.02	0.15	0.00	0.00	20.9
10	55	-0	2247	0	0	0	1346	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
11	55	-0	2302	0	0	0	1327	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
12	55	-0	2220	0	0	0	1308	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
13	55	-0	2275	0	0	0	1289	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
14	55	-0	2174	0	0	0	1356	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
15	55	-0	2356	0	0	0	1290	--	--	16.08	16.08	0.10	0.02	0.02	0.15	0.00	0.00	20.9
16	55	-0	2166	0	0	0	1345	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
17	55	-0	2348	0	0	0	1279	--	--	16.08	16.08	0.10	0.02	0.02	0.15	0.00	0.00	20.9
18	55	-0	4419	0	0	0	2861	--	--	16.08	16.08	0.00	0.05	0.04	0.28	0.00	0.00	20.9
19	55	-0	3382	0	0	0	1943	--	--	16.08	16.08	0.00	0.03	0.03	0.21	0.00	0.00	20.9
20	55	-0	4681	0	0	0	1896	--	--	16.08	16.08	0.00	0.03	0.04	0.29	0.00	0.00	20.9
37	55	-0	4458	0	0	0	2941	--	--	16.08	16.08	0.00	0.05	0.04	0.28	0.00	0.00	20.9
38	55	-0	2731	0	0	0	1412	--	--	16.08	16.08	0.00	0.02	0.02	0.17	0.00	0.00	20.9
39	55	-0	4896	0	0	0	1332	--	--	16.08	16.08	0.00	0.02	0.04	0.31	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 59 NI 1702 NF 1707 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm

1	0	-0	2056	0	0	0	-302	--	--	16.08	16.08	0.18	0.01	0.02	0.13	0.00	0.00	20.9
2	0	-0	1573	0	0	0	-190	--	--	16.08	16.08	0.29	0.00	0.01	0.10	0.00	0.00	20.9
3	0	-0	1640	0	0	0	-249	--	--	16.08	16.08	0.29	0.00	0.01	0.10	0.00	0.00	20.9
4	0	-0	1524	0	0	0	-216	--	--	16.08	16.08	0.29	0.00	0.01	0.10	0.00	0.00	20.9
5	0	-0	1591	0	0	0	-275	--	--	16.08	16.08	0.29	0.00	0.01	0.10	0.00	0.00	20.9
6	0	-0	1478	0	0	0	-130	--	--	16.08	16.08	0.29	0.00	0.01	0.09	0.00	0.00	20.9
7	0	-0	1701	0	0	0	-327	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
8	0	-0	1463	0	0	0	-138	--	--	16.08	16.08	0.29	0.00	0.01	0.09	0.00	0.00	20.9
9	0	-0	1686	0	0	0	-335	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
10	0	-0	1573	0	0	0	-190	--	--	16.08	16.08	0.29	0.00	0.01	0.10	0.00	0.00	20.9
11	0	-0	1640	0	0	0	-249	--	--	16.08	16.08	0.29	0.00	0.01	0.10	0.00	0.00	20.9
12	0	-0	1524	0	0	0	-216	--	--	16.08	16.08	0.29	0.00	0.01	0.10	0.00	0.00	20.9
13	0	-0	1591	0	0	0	-275	--	--	16.08	16.08	0.29	0.00	0.01	0.10	0.00	0.00	20.9
14	0	-0	1478	0	0	0	-130	--	--	16.08	16.08	0.29	0.00	0.01	0.09	0.00	0.00	20.9
15	0	-0	1701	0	0	0	-327	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
16	0	-0	1463	0	0	0	-138	--	--	16.08	16.08	0.29	0.00	0.01	0.09	0.00	0.00	20.9
17	0	-0	1686	0	0	0	-335	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
18	0	-0	3155	0	0	0	-170	--	--	16.08	16.08	0.18	0.00	0.03	0.20	0.00	0.00	20.9
19	0	-0	2220	0	0	0	-413	--	--	16.08	16.08	0.18	0.01	0.02	0.14	0.00	0.00	20.9
20	0	-0	3595	0	0	0	-1386	--	--	16.08	16.08	0.18	0.02	0.03	0.23	0.00	0.00	20.9
37	0	-0	3266	0	0	0	-98	--	--	16.08	16.08	0.18	0.00	0.03	0.20	0.00	0.00	20.9
38	0	-0	1708	0	0	0	-504	--	--	16.08	16.08	0.18	0.01	0.01	0.11	0.00	0.00	20.9
39	0	-0	3999	0	0	0	-2125	--	--	16.08	16.08	0.18	0.04	0.03	0.25	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	2056	0	0	0	2456	--	--	16.08	16.08	0.00	0.04	0.02	0.13	0.00	0.00	20.9
2	27	-0	1573	0	0	0	1920	--	--	16.08	16.08	0.10	0.03	0.01	0.10	0.00	0.00	20.9
3	27	-0	1640	0	0	0	1951	--	--	16.08	16.08	0.10	0.03	0.01	0.10	0.00	0.00	20.9
4	27	-0	1524	0	0	0	1828	--	--	16.08	16.08	0.10	0.03	0.01	0.10	0.00	0.00	20.9
5	27	-0	1591	0	0	0	1859	--	--	16.08	16.08	0.10	0.03	0.01	0.10	0.00	0.00	20.9
6	27	-0	1478	0	0	0	1852	--	--	16.08	16.08	0.10	0.03	0.01	0.09	0.00	0.00	20.9
7	27	-0	1701	0	0	0	1955	--	--	16.08	16.08	0.10	0.03	0.01	0.11	0.00	0.00	20.9
8	27	-0	1463	0	0	0	1824	--	--	16.08	16.08	0.10	0.03	0.01	0.09	0.00	0.00	20.9
9	27	-0	1686	0	0	0	1927	--	--	16.08	16.08	0.10	0.03	0.01	0.11	0.00	0.00	20.9
10	27	-0	1573	0	0	0	1920	--	--	16.08	16.08	0.10	0.03	0.01	0.10	0.00	0.00	20.9
11	27	-0	1640	0	0	0	1951	--	--	16.08	16.08	0.10	0.03	0.01	0.10	0.00	0.00	20.9
12	27	-0	1524	0	0	0	1828	--	--	16.08	16.08	0.10	0.03	0.01	0.10	0.00	0.00	20.9

13	27	-0	1591	0	0	0	1859	--	--	16.08	16.08	0.10	0.03	0.01	0.10	0.00	0.00	20.9
14	27	-0	1478	0	0	0	1852	--	--	16.08	16.08	0.10	0.03	0.01	0.09	0.00	0.00	20.9
15	27	-0	1701	0	0	0	1955	--	--	16.08	16.08	0.10	0.03	0.01	0.11	0.00	0.00	20.9
16	27	-0	1463	0	0	0	1824	--	--	16.08	16.08	0.10	0.03	0.01	0.09	0.00	0.00	20.9
17	27	-0	1686	0	0	0	1927	--	--	16.08	16.08	0.10	0.03	0.01	0.11	0.00	0.00	20.9
18	27	-0	3155	0	0	0	4062	--	--	16.08	16.08	0.00	0.07	0.03	0.20	0.00	0.00	20.9
19	27	-0	2220	0	0	0	2565	--	--	16.08	16.08	0.00	0.04	0.02	0.14	0.00	0.00	20.9
20	27	-0	3595	0	0	0	-1386	--	--	16.08	16.08	0.18	0.02	0.03	0.23	0.00	0.00	20.9
37	27	-0	3266	0	0	0	4283	--	--	16.08	16.08	0.00	0.07	0.03	0.20	0.00	0.00	20.9
38	27	-0	1708	0	0	0	-504	--	--	16.08	16.08	0.18	0.01	0.01	0.11	0.00	0.00	20.9
39	27	-0	3999	0	0	0	-2125	--	--	16.08	16.08	0.18	0.04	0.03	0.25	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	2056	0	0	0	819	--	--	16.08	16.08	0.00	0.01	0.02	0.13	0.00	0.00	20.9
2	55	-0	1573	0	0	0	668	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
3	55	-0	1640	0	0	0	645	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
4	55	-0	1524	0	0	0	615	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
5	55	-0	1591	0	0	0	593	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
6	55	-0	1478	0	0	0	676	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
7	55	-0	1701	0	0	0	601	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
8	55	-0	1463	0	0	0	660	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
9	55	-0	1686	0	0	0	585	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
10	55	-0	1573	0	0	0	668	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
11	55	-0	1640	0	0	0	645	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
12	55	-0	1524	0	0	0	615	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
13	55	-0	1591	0	0	0	593	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
14	55	-0	1478	0	0	0	676	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
15	55	-0	1701	0	0	0	601	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
16	55	-0	1463	0	0	0	660	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
17	55	-0	1686	0	0	0	585	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
18	55	-0	3155	0	0	0	1551	--	--	16.08	16.08	0.00	0.03	0.03	0.20	0.00	0.00	20.9
19	55	-0	2220	0	0	0	797	--	--	16.08	16.08	0.00	0.01	0.02	0.14	0.00	0.00	20.9
20	55	-0	3595	0	0	0	575	--	--	16.08	16.08	0.00	0.01	0.03	0.23	0.00	0.00	20.9
37	55	-0	3266	0	0	0	1683	--	--	16.08	16.08	0.00	0.03	0.03	0.20	0.00	0.00	20.9
38	55	-0	1708	0	0	0	428	--	--	16.08	16.08	0.00	0.01	0.01	0.11	0.00	0.00	20.9
39	55	-0	3999	0	0	0	57	--	--	16.08	16.08	0.00	0.00	0.03	0.25	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 60 NI 1708 NF 1702 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	1445	0	0	0	-534	--	--	16.08	16.08	0.18	0.01	0.01	0.09	0.00	0.00	20.9
2	0	-0	1103	0	0	0	-363	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
3	0	-0	1171	0	0	0	-435	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
4	0	-0	1052	0	0	0	-386	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
5	0	-0	1121	0	0	0	-458	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
6	0	-0	1006	0	0	0	-288	--	--	16.08	16.08	0.29	0.00	0.01	0.06	0.00	0.00	20.9
7	0	-0	1233	0	0	0	-526	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
8	0	-0	990	0	0	0	-295	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
9	0	-0	1218	0	0	0	-533	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
10	0	-0	1103	0	0	0	-363	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
11	0	-0	1171	0	0	0	-435	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
12	0	-0	1052	0	0	0	-386	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
13	0	-0	1121	0	0	0	-458	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
14	0	-0	1006	0	0	0	-288	--	--	16.08	16.08	0.29	0.00	0.01	0.06	0.00	0.00	20.9
15	0	-0	1233	0	0	0	-526	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
16	0	-0	990	0	0	0	-295	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
17	0	-0	1218	0	0	0	-533	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
18	0	-0	2288	0	0	0	-539	--	--	16.08	16.08	0.18	0.01	0.02	0.14	0.00	0.00	20.9
19	0	-0	1491	0	0	0	-679	--	--	16.08	16.08	0.18	0.01	0.01	0.09	0.00	0.00	20.9
20	0	-0	2866	0	0	0	-1891	--	--	16.08	16.08	0.18	0.03	0.02	0.18	0.00	0.00	20.9
37	0	-0	2412	0	0	0	-474	--	--	16.08	16.08	0.18	0.01	0.02	0.15	0.00	0.00	20.9
38	0	-0	1084	0	0	0	-708	--	--	16.08	16.08	0.18	0.01	0.01	0.07	0.00	0.00	20.9
39	0	-0	3375	0	0	0	-2728	--	--	16.08	16.08	0.18	0.05	0.03	0.21	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	1445	0	0	0	-534	--	--	16.08	16.08	0.18	0.01	0.01	0.09	0.00	0.00	20.9
2	27	-0	1103	0	0	0	-363	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
3	27	-0	1171	0	0	0	-435	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
4	27	-0	1052	0	0	0	-386	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
5	27	-0	1121	0	0	0	-458	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
6	27	-0	1006	0	0	0	-288	--	--	16.08	16.08	0.29	0.00	0.01	0.06	0.00	0.00	20.9
7	27	-0	1233	0	0	0	-526	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
8	27	-0	990	0	0	0	-295	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
9	27	-0	1218	0	0	0	-533	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
10	27	-0	1103	0	0	0	-363	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
11	27	-0	1171	0	0	0	-435	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
12	27	-0	1052	0	0	0	-386	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
13	27	-0	1121	0	0	0	-458	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
14	27	-0	1006	0	0	0	-288	--	--	16.08	16.08	0.29	0.00	0.01	0.06	0.00	0.00	20.9
15	27	-0	1233	0	0	0	-526	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
16	27	-0	990	0	0	0	-295	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
17	27	-0	1218	0	0	0	-533	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
18	27	-0	2288	0	0	0	2531	--	--	16.08	16.08	0.00	0.04	0.02	0.14	0.00	0.00	20.9
19	27	-0	1491	0	0	0	-679	--	--	16.08	16.08	0.18	0.01	0.01	0.09	0.00	0.00	20.9
20	27	-0	2866	0	0	0	-1891	--	--	16.08	16.08	0.18	0.03	0.02	0.18	0.00	0.00	20.9
37	27	-0	2412	0	0	0	2762	--	--	16.08	16.08	0.00	0.05	0.02	0.15	0.00	0.00	20.9
38	27	-0	1084	0	0	0	-708	--	--	16.08	16.08	0.18	0.01	0.01	0.07	0.00	0.00	20.9
39	27	-0	3375	0	0	0	-2728	--	--	16.08	16.08	0.18	0.05	0.03	0.21	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	1445	0	0	0	255	--	--	16.08	16.08	0.00	0.00	0.01	0.09	0.00	0.00	20.9
2	55	-0	1103	0	0	0	238	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
3	55	-0	1171	0	0	0	204	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
4	55	-0	1052	0	0	0	188	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
5	55	-0	1121	0	0	0	153	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
6	55	-0	1006	0	0	0	260	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
7	55	-0	1233	0	0	0	147	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
8	55	-0	990	0	0	0	245	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9

9	55	-0	1218	0	0	0	132	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
10	55	-0	1103	0	0	0	238	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
11	55	-0	1171	0	0	0	204	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
12	55	-0	1052	0	0	0	188	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
13	55	-0	1121	0	0	0	153	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
14	55	-0	1006	0	0	0	260	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
15	55	-0	1233	0	0	0	147	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
16	55	-0	990	0	0	0	245	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
17	55	-0	1218	0	0	0	132	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
18	55	-0	2288	0	0	0	709	--	--	16.08	16.08	0.00	0.01	0.02	0.14	0.00	0.00	20.9
19	55	-0	1491	0	0	0	134	--	--	16.08	16.08	0.00	0.00	0.01	0.09	0.00	0.00	20.9
20	55	-0	2866	0	0	0	-1891	--	--	16.08	16.08	0.18	0.03	0.02	0.18	0.00	0.00	20.9
37	55	-0	2412	0	0	0	842	--	--	16.08	16.08	0.00	0.01	0.02	0.15	0.00	0.00	20.9
38	55	-0	1084	0	0	0	-708	--	--	16.08	16.08	0.18	0.01	0.01	0.07	0.00	0.00	20.9
39	55	-0	3375	0	0	0	-2728	--	--	16.08	16.08	0.18	0.05	0.03	0.21	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 61 NI 1709 NF 1708 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	987	0	0	0	-653	--	--	16.08	16.08	0.18	0.01	0.01	0.06	0.00	0.00	20.9
2	0	-0	748	0	0	0	-452	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
3	0	-0	816	0	0	0	-536	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
4	0	-0	702	0	0	0	-469	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
5	0	-0	770	0	0	0	-553	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
6	0	-0	653	0	0	0	-360	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
7	0	-0	879	0	0	0	-640	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
8	0	-0	639	0	0	0	-365	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
9	0	-0	866	0	0	0	-645	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
10	0	-0	748	0	0	0	-452	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
11	0	-0	816	0	0	0	-536	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
12	0	-0	702	0	0	0	-469	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
13	0	-0	770	0	0	0	-553	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
14	0	-0	653	0	0	0	-360	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
15	0	-0	879	0	0	0	-640	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
16	0	-0	639	0	0	0	-365	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
17	0	-0	866	0	0	0	-645	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
18	0	-0	1649	0	0	0	-754	--	--	16.08	16.08	0.18	0.01	0.01	0.10	0.00	0.00	20.9
19	0	-0	987	0	0	0	-804	--	--	16.08	16.08	0.18	0.01	0.01	0.06	0.00	0.00	20.9
20	0	-0	2344	0	0	0	-2263	--	--	16.08	16.08	0.18	0.04	0.02	0.15	0.00	0.00	20.9
37	0	-0	1763	0	0	0	-703	--	--	16.08	16.08	0.18	0.01	0.01	0.11	0.00	0.00	20.9
38	0	-0	660	0	0	0	-786	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
39	0	-0	2921	0	0	0	-3218	--	--	16.08	16.08	0.18	0.05	0.02	0.18	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	987	0	0	0	-653	--	--	16.08	16.08	0.18	0.01	0.01	0.06	0.00	0.00	20.9
2	27	-0	748	0	0	0	-452	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
3	27	-0	816	0	0	0	-536	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
4	27	-0	702	0	0	0	-469	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
5	27	-0	770	0	0	0	-553	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
6	27	-0	653	0	0	0	-360	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
7	27	-0	879	0	0	0	-640	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
8	27	-0	639	0	0	0	-365	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
9	27	-0	866	0	0	0	-645	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
10	27	-0	748	0	0	0	-452	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
11	27	-0	816	0	0	0	-536	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
12	27	-0	702	0	0	0	-469	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
13	27	-0	770	0	0	0	-553	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
14	27	-0	653	0	0	0	-360	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
15	27	-0	879	0	0	0	-640	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
16	27	-0	639	0	0	0	-365	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
17	27	-0	866	0	0	0	-645	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
18	27	-0	1649	0	0	0	-754	--	--	16.08	16.08	0.18	0.01	0.01	0.10	0.00	0.00	20.9
19	27	-0	987	0	0	0	-804	--	--	16.08	16.08	0.18	0.01	0.01	0.06	0.00	0.00	20.9
20	27	-0	2344	0	0	0	-2263	--	--	16.08	16.08	0.18	0.04	0.02	0.15	0.00	0.00	20.9
37	27	-0	1763	0	0	0	-703	--	--	16.08	16.08	0.18	0.01	0.01	0.11	0.00	0.00	20.9
38	27	-0	660	0	0	0	-786	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
39	27	-0	2921	0	0	0	-3218	--	--	16.08	16.08	0.18	0.05	0.02	0.18	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	987	0	0	0	-653	--	--	16.08	16.08	0.18	0.01	0.01	0.06	0.00	0.00	20.9
2	55	-0	748	0	0	0	-452	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
3	55	-0	816	0	0	0	-536	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
4	55	-0	702	0	0	0	-469	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
5	55	-0	770	0	0	0	-553	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
6	55	-0	653	0	0	0	-360	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
7	55	-0	879	0	0	0	-640	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
8	55	-0	639	0	0	0	-365	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
9	55	-0	866	0	0	0	-645	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
10	55	-0	748	0	0	0	-452	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
11	55	-0	816	0	0	0	-536	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
12	55	-0	702	0	0	0	-469	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
13	55	-0	770	0	0	0	-553	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
14	55	-0	653	0	0	0	-360	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
15	55	-0	879	0	0	0	-640	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
16	55	-0	639	0	0	0	-365	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
17	55	-0	866	0	0	0	-645	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
18	55	-0	1649	0	0	0	145	--	--	16.08	16.08	0.00	0.00	0.01	0.10	0.00	0.00	20.9
19	55	-0	987	0	0	0	-804	--	--	16.08	16.08	0.18	0.01	0.01	0.06	0.00	0.00	20.9
20	55	-0	2344	0	0	0	-2263	--	--	16.08	16.08	0.18	0.04	0.02	0.15	0.00	0.00	20.9
37	55	-0	1763	0	0	0	258	--	--	16.08	16.08	0.00	0.00	0.01	0.11	0.00	0.00	20.9
38	55	-0	660	0	0	0	-786	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
39	55	-0	2921	0	0	0	-3218	--	--	16.08	16.08	0.18	0.05	0.02	0.18	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 62 NI 1703 NF 1709 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	593	0	0	0	-692	--	--	16.08	16.08	0.18	0.01	0.00	0.04	0.00	0.00	20.9
2	0	-0	444	0	0	0	-479	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
3	0	-0	511	0	0	0	-575	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
4	0	-0	402	0	0	0	-489	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
5	0	-0	469	0	0	0	-586	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
6	0	-0	351	0	0	0	-369	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
7	0	-0	575	0	0	0	-692	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
8	0	-0	338	0	0	0	-373	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
9	0	-0	562	0	0	0	-695	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
10	0	-0	444	0	0	0	-479	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
11	0	-0	511	0	0	0	-575	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
12	0	-0	402	0	0	0	-489	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
13	0	-0	469	0	0	0	-586	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
14	0	-0	351	0	0	0	-369	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
15	0	-0	575	0	0	0	-692	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
16	0	-0	338	0	0	0	-373	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
17	0	-0	562	0	0	0	-695	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
18	0	-0	1120	0	0	0	-866	--	--	16.08	16.08	0.18	0.01	0.01	0.07	0.00	0.00	20.9
19	0	-0	564	0	0	0	-834	--	--	16.08	16.08	0.18	0.01	0.00	0.04	0.00	0.00	20.9
20	0	-0	1912	0	0	0	-2550	--	--	16.08	16.08	0.18	0.04	0.02	0.12	0.00	0.00	20.9
37	0	-0	1223	0	0	0	-831	--	--	16.08	16.08	0.18	0.01	0.01	0.08	0.00	0.00	20.9
38	0	-0	297	0	0	0	-777	--	--	16.08	16.08	0.18	0.01	0.00	0.02	0.00	0.00	20.9
39	0	-0	2545	0	0	0	-3638	--	--	16.08	16.08	0.18	0.06	0.02	0.16	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	593	0	0	0	-692	--	--	16.08	16.08	0.18	0.01	0.00	0.04	0.00	0.00	20.9
2	27	-0	444	0	0	0	-479	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
3	27	-0	511	0	0	0	-575	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
4	27	-0	402	0	0	0	-489	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
5	27	-0	469	0	0	0	-586	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
6	27	-0	351	0	0	0	-369	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
7	27	-0	575	0	0	0	-692	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
8	27	-0	338	0	0	0	-373	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
9	27	-0	562	0	0	0	-695	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
10	27	-0	444	0	0	0	-479	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
11	27	-0	511	0	0	0	-575	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
12	27	-0	402	0	0	0	-489	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
13	27	-0	469	0	0	0	-586	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
14	27	-0	351	0	0	0	-369	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
15	27	-0	575	0	0	0	-692	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
16	27	-0	338	0	0	0	-373	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
17	27	-0	562	0	0	0	-695	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
18	27	-0	1120	0	0	0	-866	--	--	16.08	16.08	0.18	0.01	0.01	0.07	0.00	0.00	20.9
19	27	-0	564	0	0	0	-834	--	--	16.08	16.08	0.18	0.01	0.00	0.04	0.00	0.00	20.9
20	27	-0	1912	0	0	0	-2550	--	--	16.08	16.08	0.18	0.04	0.02	0.12	0.00	0.00	20.9
37	27	-0	1223	0	0	0	-831	--	--	16.08	16.08	0.18	0.01	0.01	0.08	0.00	0.00	20.9
38	27	-0	297	0	0	0	-777	--	--	16.08	16.08	0.18	0.01	0.00	0.02	0.00	0.00	20.9
39	27	-0	2545	0	0	0	-3638	--	--	16.08	16.08	0.18	0.06	0.02	0.16	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	593	0	0	0	-692	--	--	16.08	16.08	0.18	0.01	0.00	0.04	0.00	0.00	20.9
2	55	-0	444	0	0	0	-479	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
3	55	-0	511	0	0	0	-575	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
4	55	-0	402	0	0	0	-489	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
5	55	-0	469	0	0	0	-586	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
6	55	-0	351	0	0	0	-369	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
7	55	-0	575	0	0	0	-692	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
8	55	-0	338	0	0	0	-373	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
9	55	-0	562	0	0	0	-695	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
10	55	-0	444	0	0	0	-479	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
11	55	-0	511	0	0	0	-575	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
12	55	-0	402	0	0	0	-489	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
13	55	-0	469	0	0	0	-586	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
14	55	-0	351	0	0	0	-369	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
15	55	-0	575	0	0	0	-692	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
16	55	-0	338	0	0	0	-373	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
17	55	-0	562	0	0	0	-695	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
18	55	-0	1120	0	0	0	-866	--	--	16.08	16.08	0.18	0.01	0.01	0.07	0.00	0.00	20.9
19	55	-0	564	0	0	0	-834	--	--	16.08	16.08	0.18	0.01	0.00	0.04	0.00	0.00	20.9
20	55	-0	1912	0	0	0	-2550	--	--	16.08	16.08	0.18	0.04	0.02	0.12	0.00	0.00	20.9
37	55	-0	1223	0	0	0	-831	--	--	16.08	16.08	0.18	0.01	0.01	0.08	0.00	0.00	20.9
38	55	-0	297	0	0	0	-777	--	--	16.08	16.08	0.18	0.01	0.00	0.02	0.00	0.00	20.9
39	55	-0	2545	0	0	0	-3638	--	--	16.08	16.08	0.18	0.06	0.02	0.16	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 63 NI 1704 NF 1703 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	219	0	0	0	-654	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9
2	0	-0	157	0	0	0	-448	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
3	0	-0	222	0	0	0	-557	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
4	0	-0	114	0	0	0	-450	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
5	0	-0	180	0	0	0	-559	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
6	0	-0	65	0	0	0	-321	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
7	0	-0	284	0	0	0	-685	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
8	0	-0	52	0	0	0	-322	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
9	0	-0	271	0	0	0	-685	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
10	0	-0	157	0	0	0	-448	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
11	0	-0	222	0	0	0	-557	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
12	0	-0	114	0	0	0	-450	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
13	0	-0	180	0	0	0	-559	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
14	0	-0	65	0	0	0	-321	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
15	0	-0	284	0	0	0	-685	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
16	0	-0	52	0	0	0	-322	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9

17	0	-0	271	0	0	0	-685	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
18	0	-0	646	0	0	0	-892	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
19	0	-0	153	0	0	0	-778	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9
20	0	-0	1545	0	0	0	-2793	--	--	16.08	16.08	0.18	0.05	0.01	0.10	0.00	0.00	20.9
37	0	-0	749	0	0	0	-876	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9
38	0	-0	-73	0	0	0	-726	--	--	16.08	16.08	0.18	0.01	0.00	0.00	0.00	0.00	20.9
39	0	-0	2247	0	0	0	-4044	--	--	16.08	16.08	0.18	0.07	0.02	0.14	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	219	0	0	0	-654	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9
2	27	-0	157	0	0	0	-448	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
3	27	-0	222	0	0	0	-557	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
4	27	-0	114	0	0	0	-450	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
5	27	-0	180	0	0	0	-559	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
6	27	-0	65	0	0	0	-321	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
7	27	-0	284	0	0	0	-685	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
8	27	-0	52	0	0	0	-322	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
9	27	-0	271	0	0	0	-685	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
10	27	-0	157	0	0	0	-448	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
11	27	-0	222	0	0	0	-557	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
12	27	-0	114	0	0	0	-450	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
13	27	-0	180	0	0	0	-559	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
14	27	-0	65	0	0	0	-321	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
15	27	-0	284	0	0	0	-685	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
16	27	-0	52	0	0	0	-322	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
17	27	-0	271	0	0	0	-685	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
18	27	-0	646	0	0	0	-892	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
19	27	-0	153	0	0	0	-778	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9
20	27	-0	1545	0	0	0	-2793	--	--	16.08	16.08	0.18	0.05	0.01	0.10	0.00	0.00	20.9
37	27	-0	749	0	0	0	-876	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9
38	27	-0	-73	0	0	0	-726	--	--	16.08	16.08	0.18	0.01	0.00	0.00	0.00	0.00	20.9
39	27	-0	2247	0	0	0	-4044	--	--	16.08	16.08	0.18	0.07	0.02	0.14	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	219	0	0	0	-654	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9
2	55	-0	157	0	0	0	-448	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
3	55	-0	222	0	0	0	-557	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
4	55	-0	114	0	0	0	-450	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
5	55	-0	180	0	0	0	-559	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
6	55	-0	65	0	0	0	-321	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
7	55	-0	284	0	0	0	-685	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
8	55	-0	52	0	0	0	-322	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
9	55	-0	271	0	0	0	-685	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
10	55	-0	157	0	0	0	-448	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
11	55	-0	222	0	0	0	-557	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
12	55	-0	114	0	0	0	-450	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
13	55	-0	180	0	0	0	-559	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
14	55	-0	65	0	0	0	-321	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
15	55	-0	284	0	0	0	-685	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
16	55	-0	52	0	0	0	-322	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
17	55	-0	271	0	0	0	-685	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
18	55	-0	646	0	0	0	-892	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
19	55	-0	153	0	0	0	-778	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9
20	55	-0	1545	0	0	0	-2793	--	--	16.08	16.08	0.18	0.05	0.01	0.10	0.00	0.00	20.9
37	55	-0	749	0	0	0	-876	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9
38	55	-0	-73	0	0	0	-726	--	--	16.08	16.08	0.18	0.01	0.00	0.00	0.00	0.00	20.9
39	55	-0	2247	0	0	0	-4044	--	--	16.08	16.08	0.18	0.07	0.02	0.14	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 64 NI 1705 NF 1704 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm

1	0	-0	-192	0	0	0	-611	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9
2	0	-0	-151	0	0	0	-419	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
3	0	-0	-95	0	0	0	-504	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
4	0	-0	-200	0	0	0	-436	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
5	0	-0	-144	0	0	0	-521	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
6	0	-0	-234	0	0	0	-326	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
7	0	-0	-47	0	0	0	-609	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
8	0	-0	-248	0	0	0	-331	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
9	0	-0	-62	0	0	0	-614	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
10	0	-0	-151	0	0	0	-419	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
11	0	-0	-95	0	0	0	-504	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
12	0	-0	-200	0	0	0	-436	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
13	0	-0	-144	0	0	0	-521	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
14	0	-0	-234	0	0	0	-326	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
15	0	-0	-47	0	0	0	-609	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
16	0	-0	-248	0	0	0	-331	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
17	0	-0	-62	0	0	0	-614	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
18	0	-0	183	0	0	0	-814	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9
19	0	-0	-294	0	0	0	-766	--	--	16.08	16.08	0.18	0.01	0.00	0.02	0.00	0.00	20.9
20	0	-0	1268	0	0	0	-3041	--	--	16.08	16.08	0.18	0.05	0.01	0.08	0.00	0.00	20.9
37	0	-0	292	0	0	0	-820	--	--	16.08	16.08	0.18	0.01	0.00	0.02	0.00	0.00	20.9
38	0	-0	-503	0	0	0	-747	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9
39	0	-0	2101	0	0	0	-4531	--	--	16.08	16.08	0.18	0.08	0.02	0.13	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-192	0	0	0	-611	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9
2	27	-0	-151	0	0	0	-419	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
3	27	-0	-95	0	0	0	-504	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
4	27	-0	-200	0	0	0	-436	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
5	27	-0	-144	0	0	0	-521	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
6	27	-0	-234	0	0	0	-326	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
7	27	-0	-47	0	0	0	-609	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
8	27	-0	-248	0	0	0	-331	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
9	27	-0	-62	0	0	0	-614	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
10	27	-0	-151	0	0	0	-419	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
11	27	-0	-95	0	0	0	-504	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
12	27	-0	-200	0	0	0	-436	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9

13	27	-0	-144	0	0	0	-521	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
14	27	-0	-234	0	0	0	-326	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
15	27	-0	-47	0	0	0	-609	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
16	27	-0	-248	0	0	0	-331	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
17	27	-0	-62	0	0	0	-614	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
18	27	-0	183	0	0	0	-814	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9
19	27	-0	-294	0	0	0	-766	--	--	16.08	16.08	0.18	0.01	0.00	0.02	0.00	0.00	20.9
20	27	-0	1268	0	0	0	-3041	--	--	16.08	16.08	0.18	0.05	0.01	0.08	0.00	0.00	20.9
37	27	-0	292	0	0	0	-820	--	--	16.08	16.08	0.18	0.01	0.00	0.02	0.00	0.00	20.9
38	27	-0	-503	0	0	0	-747	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9
39	27	-0	2101	0	0	0	-4531	--	--	16.08	16.08	0.18	0.08	0.02	0.13	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	-192	0	0	0	-611	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9
2	55	-0	-151	0	0	0	-419	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
3	55	-0	-95	0	0	0	-504	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
4	55	-0	-200	0	0	0	-436	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
5	55	-0	-144	0	0	0	-521	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
6	55	-0	-234	0	0	0	-326	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
7	55	-0	-47	0	0	0	-609	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
8	55	-0	-248	0	0	0	-331	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
9	55	-0	-62	0	0	0	-614	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
10	55	-0	-151	0	0	0	-419	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
11	55	-0	-95	0	0	0	-504	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
12	55	-0	-200	0	0	0	-436	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
13	55	-0	-144	0	0	0	-521	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
14	55	-0	-234	0	0	0	-326	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
15	55	-0	-47	0	0	0	-609	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
16	55	-0	-248	0	0	0	-331	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
17	55	-0	-62	0	0	0	-614	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
18	55	-0	183	0	0	0	-814	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9
19	55	-0	-294	0	0	0	-766	--	--	16.08	16.08	0.18	0.01	0.00	0.02	0.00	0.00	20.9
20	55	-0	1268	0	0	0	-3041	--	--	16.08	16.08	0.18	0.05	0.01	0.08	0.00	0.00	20.9
37	55	-0	292	0	0	0	-820	--	--	16.08	16.08	0.18	0.01	0.00	0.02	0.00	0.00	20.9
38	55	-0	-503	0	0	0	-747	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9
39	55	-0	2101	0	0	0	-4531	--	--	16.08	16.08	0.18	0.08	0.02	0.13	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 65 NI 1701 NF 1705 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--	--	--	--	--	--	--	--	--	--	--		--	--	--	--	--	--
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-662	0	0	0	-583	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
2	0	-0	-489	0	0	0	-400	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
3	0	-0	-469	0	0	0	-492	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
4	0	-0	-550	0	0	0	-405	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
5	0	-0	-530	0	0	0	-498	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
6	0	-0	-533	0	0	0	-294	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
7	0	-0	-467	0	0	0	-602	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
8	0	-0	-552	0	0	0	6	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
9	0	-0	-485	0	0	0	-604	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
10	0	-0	-489	0	0	0	-400	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
11	0	-0	-469	0	0	0	-492	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
12	0	-0	-550	0	0	0	-405	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
13	0	-0	-530	0	0	0	-498	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
14	0	-0	-533	0	0	0	-294	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
15	0	-0	-467	0	0	0	-602	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
16	0	-0	-552	0	0	0	6	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
17	0	-0	-485	0	0	0	-604	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
18	0	-0	-318	0	0	0	-781	--	--	16.08	16.08	0.18	0.01	0.00	0.02	0.00	0.00	20.9
19	0	-0	-790	0	0	0	-726	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9
20	0	-0	1111	0	0	0	-3387	--	--	16.08	16.08	0.18	0.06	0.01	0.07	0.00	0.00	20.9
37	0	-0	-203	0	0	0	-749	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9
38	0	-0	-990	0	0	0	-658	--	--	16.08	16.08	0.18	0.01	0.01	0.06	0.00	0.00	20.9
39	0	-0	2179	0	0	0	-5272	--	--	16.08	16.08	0.18	0.09	0.02	0.14	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-662	0	0	0	-583	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
2	27	-0	-489	0	0	0	-400	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
3	27	-0	-469	0	0	0	-492	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
4	27	-0	-550	0	0	0	-405	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
5	27	-0	-530	0	0	0	-498	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
6	27	-0	-533	0	0	0	-294	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
7	27	-0	-467	0	0	0	-602	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
8	27	-0	-552	0	0	0	-295	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
9	27	-0	-485	0	0	0	-604	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
10	27	-0	-489	0	0	0	-400	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
11	27	-0	-469	0	0	0	-492	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
12	27	-0	-550	0	0	0	-405	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
13	27	-0	-530	0	0	0	-498	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
14	27	-0	-533	0	0	0	-294	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
15	27	-0	-467	0	0	0	-602	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
16	27	-0	-552	0	0	0	-295	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
17	27	-0	-485	0	0	0	-604	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
18	27	-0	-318	0	0	0	-781	--	--	16.08	16.08	0.18	0.01	0.00	0.02	0.00	0.00	20.9
19	27	-0	-790	0	0	0	-726	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9
20	27	-0	1111	0	0	0	-3387	--	--	16.08	16.08	0.18	0.06	0.01	0.07	0.00	0.00	20.9
37	27	-0	-203	0	0	0	-749	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9
38	27	-0	-990	0	0	0	-658	--	--	16.08	16.08	0.18	0.01	0.01	0.06	0.00	0.00	20.9
39	27	-0	2179	0	0	0	-5272	--	--	16.08	16.08	0.18	0.09	0.02	0.14	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	-662	0	0	0	-583	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
2	55	-0	-489	0	0	0	-400	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
3	55	-0	-469	0	0	0	-492	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
4	55	-0	-550	0	0	0	-405	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
5	55	-0	-530	0	0	0	-498	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
6	55	-0	-533	0	0	0	-294	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
7	55	-0	-467	0	0	0	-602	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
8	55	-0	-552	0	0	0	-295	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9

9	55	-0	-485	0	0	0	-604	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
10	55	-0	-489	0	0	0	-400	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
11	55	-0	-469	0	0	0	-492	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
12	55	-0	-550	0	0	0	-405	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
13	55	-0	-530	0	0	0	-498	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
14	55	-0	-533	0	0	0	-294	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
15	55	-0	-467	0	0	0	-602	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
16	55	-0	-552	0	0	0	-295	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
17	55	-0	-485	0	0	0	-604	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
18	55	-0	-318	0	0	0	-781	--	--	16.08	16.08	0.18	0.01	0.00	0.02	0.00	0.00	20.9
19	55	-0	-790	0	0	0	-726	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9
20	55	-0	1111	0	0	0	-3387	--	--	16.08	16.08	0.18	0.06	0.01	0.07	0.00	0.00	20.9
37	55	-0	-203	0	0	0	-749	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9
38	55	-0	-990	0	0	0	-658	--	--	16.08	16.08	0.18	0.01	0.01	0.06	0.00	0.00	20.9
39	55	-0	2179	0	0	0	-5272	--	--	16.08	16.08	0.18	0.09	0.02	0.14	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 66 NI 1541 NF 1701 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-923	0	0	0	59	--	--	16.08	16.08	0.00	0.00	0.01	0.06	0.00	0.00	20.9
2	0	-0	-666	0	0	0	68	--	--	16.08	16.08	0.10	0.00	0.01	0.04	0.00	0.00	20.9
3	0	-0	-653	0	0	0	-413	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
4	0	-0	-766	0	0	0	148	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
5	0	-0	-754	0	0	0	22	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
6	0	-0	-716	0	0	0	243	--	--	16.08	16.08	0.10	0.00	0.01	0.04	0.00	0.00	20.9
7	0	-0	-673	0	0	0	-543	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
8	0	-0	-746	0	0	0	266	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
9	0	-0	-704	0	0	0	-536	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
10	0	-0	-666	0	0	0	68	--	--	16.08	16.08	0.10	0.00	0.01	0.04	0.00	0.00	20.9
11	0	-0	-653	0	0	0	-413	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
12	0	-0	-766	0	0	0	148	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
13	0	-0	-754	0	0	0	22	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
14	0	-0	-716	0	0	0	243	--	--	16.08	16.08	0.10	0.00	0.01	0.04	0.00	0.00	20.9
15	0	-0	-673	0	0	0	-543	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
16	0	-0	-746	0	0	0	266	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
17	0	-0	-704	0	0	0	-536	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
18	0	-0	-633	0	0	0	-787	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
19	0	-0	-1198	0	0	0	146	--	--	16.08	16.08	0.00	0.00	0.01	0.08	0.00	0.00	20.9
20	0	-0	1269	0	0	0	-4286	--	--	16.08	16.08	0.18	0.07	0.01	0.08	0.00	0.00	20.9
37	0	-0	-454	0	0	0	-818	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9
38	0	-0	-1396	0	0	0	408	--	--	16.08	16.08	0.00	0.01	0.01	0.09	0.00	0.00	20.9
39	0	-0	2716	0	0	0	-6977	--	--	16.08	16.08	0.18	0.12	0.02	0.17	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-923	0	0	0	-445	--	--	16.08	16.08	0.18	0.01	0.01	0.06	0.00	0.00	20.9
2	27	-0	-666	0	0	0	-295	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
3	27	-0	-653	0	0	0	-413	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
4	27	-0	-766	0	0	0	-271	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
5	27	-0	-754	0	0	0	-389	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
6	27	-0	-716	0	0	0	243	--	--	16.08	16.08	0.10	0.00	0.01	0.04	0.00	0.00	20.9
7	27	-0	-673	0	0	0	-543	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
8	27	-0	-746	0	0	0	266	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
9	27	-0	-704	0	0	0	-536	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
10	27	-0	-666	0	0	0	-295	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
11	27	-0	-653	0	0	0	-413	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
12	27	-0	-766	0	0	0	-271	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
13	27	-0	-754	0	0	0	-389	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
14	27	-0	-716	0	0	0	243	--	--	16.08	16.08	0.10	0.00	0.01	0.04	0.00	0.00	20.9
15	27	-0	-673	0	0	0	-543	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
16	27	-0	-746	0	0	0	266	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
17	27	-0	-704	0	0	0	-536	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
18	27	-0	-633	0	0	0	-787	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
19	27	-0	-1198	0	0	0	-508	--	--	16.08	16.08	0.18	0.01	0.01	0.08	0.00	0.00	20.9
20	27	-0	1269	0	0	0	-4286	--	--	16.08	16.08	0.18	0.07	0.01	0.08	0.00	0.00	20.9
37	27	-0	-454	0	0	0	-818	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9
38	27	-0	-1396	0	0	0	408	--	--	16.08	16.08	0.00	0.01	0.01	0.09	0.00	0.00	20.9
39	27	-0	2716	0	0	0	-6977	--	--	16.08	16.08	0.18	0.12	0.02	0.17	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	-923	0	0	0	-445	--	--	16.08	16.08	0.18	0.01	0.01	0.06	0.00	0.00	20.9
2	55	-0	-666	0	0	0	-295	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
3	55	-0	-653	0	0	0	-413	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
4	55	-0	-766	0	0	0	-271	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
5	55	-0	-754	0	0	0	-389	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
6	55	-0	-716	0	0	0	-148	--	--	16.08	16.08	0.29	0.00	0.01	0.04	0.00	0.00	20.9
7	55	-0	-673	0	0	0	-543	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
8	55	-0	-746	0	0	0	-141	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
9	55	-0	-704	0	0	0	-536	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
10	55	-0	-666	0	0	0	-295	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
11	55	-0	-653	0	0	0	-413	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
12	55	-0	-766	0	0	0	-271	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
13	55	-0	-754	0	0	0	-389	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
14	55	-0	-716	0	0	0	-148	--	--	16.08	16.08	0.29	0.00	0.01	0.04	0.00	0.00	20.9
15	55	-0	-673	0	0	0	-543	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
16	55	-0	-746	0	0	0	-141	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
17	55	-0	-704	0	0	0	-536	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
18	55	-0	-633	0	0	0	-787	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
19	55	-0	-1198	0	0	0	-508	--	--	16.08	16.08	0.18	0.01	0.01	0.08	0.00	0.00	20.9
20	55	-0	1269	0	0	0	-4286	--	--	16.08	16.08	0.18	0.07	0.01	0.08	0.00	0.00	20.9
37	55	-0	-454	0	0	0	-818	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9
38	55	-0	-1396	0	0	0	-353	--	--	16.08	16.08	0.18	0.01	0.01	0.09	0.00	0.00	20.9
39	55	-0	2716	0	0	0	-6977	--	--	16.08	16.08	0.18	0.12	0.02	0.17	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 67 NI 1314 NF 1279 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle V,Mx	cmq/m		cm
1	0	-0	910	0	0	0	-228	--	--	16.08	16.08	0.18	0.00	0.01 0.06	0.00	0.00	20.9
2	0	-0	684	0	0	0	-177	--	--	16.08	16.08	0.29	0.00	0.01 0.04	0.00	0.00	20.9
3	0	-0	656	0	0	0	-174	--	--	16.08	16.08	0.29	0.00	0.01 0.04	0.00	0.00	20.9
4	0	-0	744	0	0	0	-177	--	--	16.08	16.08	0.29	0.00	0.01 0.05	0.00	0.00	20.9
5	0	-0	716	0	0	0	-174	--	--	16.08	16.08	0.29	0.00	0.01 0.04	0.00	0.00	20.9
6	0	-0	737	0	0	0	-181	--	--	16.08	16.08	0.29	0.00	0.01 0.05	0.00	0.00	20.9
7	0	-0	645	0	0	0	-170	--	--	16.08	16.08	0.29	0.00	0.01 0.04	0.00	0.00	20.9
8	0	-0	755	0	0	0	-181	--	--	16.08	16.08	0.29	0.00	0.01 0.05	0.00	0.00	20.9
9	0	-0	663	0	0	0	-170	--	--	16.08	16.08	0.29	0.00	0.01 0.04	0.00	0.00	20.9
10	0	-0	684	0	0	0	-177	--	--	16.08	16.08	0.29	0.00	0.01 0.04	0.00	0.00	20.9
11	0	-0	656	0	0	0	-174	--	--	16.08	16.08	0.29	0.00	0.01 0.04	0.00	0.00	20.9
12	0	-0	744	0	0	0	-177	--	--	16.08	16.08	0.29	0.00	0.01 0.05	0.00	0.00	20.9
13	0	-0	716	0	0	0	-174	--	--	16.08	16.08	0.29	0.00	0.01 0.04	0.00	0.00	20.9
14	0	-0	737	0	0	0	-181	--	--	16.08	16.08	0.29	0.00	0.01 0.05	0.00	0.00	20.9
15	0	-0	645	0	0	0	-170	--	--	16.08	16.08	0.29	0.00	0.01 0.04	0.00	0.00	20.9
16	0	-0	755	0	0	0	-181	--	--	16.08	16.08	0.29	0.00	0.01 0.05	0.00	0.00	20.9
17	0	-0	663	0	0	0	-170	--	--	16.08	16.08	0.29	0.00	0.01 0.04	0.00	0.00	20.9
18	0	-0	938	0	0	0	-231	--	--	16.08	16.08	0.18	0.00	0.01 0.06	0.00	0.00	20.9
19	0	-0	1055	0	0	0	-221	--	--	16.08	16.08	0.18	0.00	0.01 0.07	0.00	0.00	20.9
20	0	-0	1059	0	0	0	-251	--	--	16.08	16.08	0.18	0.00	0.01 0.07	0.00	0.00	20.9
37	0	-0	864	0	0	0	-236	--	--	16.08	16.08	0.18	0.00	0.01 0.05	0.00	0.00	20.9
38	0	-0	1060	0	0	0	-220	--	--	16.08	16.08	0.18	0.00	0.01 0.07	0.00	0.00	20.9
39	0	-0	1067	0	0	0	-270	--	--	16.08	16.08	0.18	0.00	0.01 0.07	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	910	0	0	0	988	--	--	16.08	16.08	0.00	0.02	0.01 0.06	0.00	0.00	20.9
2	27	-0	684	0	0	0	737	--	--	16.08	16.08	0.10	0.01	0.01 0.04	0.00	0.00	20.9
3	27	-0	656	0	0	0	703	--	--	16.08	16.08	0.10	0.01	0.01 0.04	0.00	0.00	20.9
4	27	-0	744	0	0	0	817	--	--	16.08	16.08	0.10	0.01	0.01 0.05	0.00	0.00	20.9
5	27	-0	716	0	0	0	784	--	--	16.08	16.08	0.10	0.01	0.01 0.04	0.00	0.00	20.9
6	27	-0	737	0	0	0	804	--	--	16.08	16.08	0.10	0.01	0.01 0.05	0.00	0.00	20.9
7	27	-0	645	0	0	0	693	--	--	16.08	16.08	0.10	0.01	0.01 0.04	0.00	0.00	20.9
8	27	-0	755	0	0	0	828	--	--	16.08	16.08	0.10	0.01	0.01 0.05	0.00	0.00	20.9
9	27	-0	663	0	0	0	717	--	--	16.08	16.08	0.10	0.01	0.01 0.04	0.00	0.00	20.9
10	27	-0	684	0	0	0	737	--	--	16.08	16.08	0.10	0.01	0.01 0.04	0.00	0.00	20.9
11	27	-0	656	0	0	0	703	--	--	16.08	16.08	0.10	0.01	0.01 0.04	0.00	0.00	20.9
12	27	-0	744	0	0	0	817	--	--	16.08	16.08	0.10	0.01	0.01 0.05	0.00	0.00	20.9
13	27	-0	716	0	0	0	784	--	--	16.08	16.08	0.10	0.01	0.01 0.04	0.00	0.00	20.9
14	27	-0	737	0	0	0	804	--	--	16.08	16.08	0.10	0.01	0.01 0.05	0.00	0.00	20.9
15	27	-0	645	0	0	0	693	--	--	16.08	16.08	0.10	0.01	0.01 0.04	0.00	0.00	20.9
16	27	-0	755	0	0	0	828	--	--	16.08	16.08	0.10	0.01	0.01 0.05	0.00	0.00	20.9
17	27	-0	663	0	0	0	717	--	--	16.08	16.08	0.10	0.01	0.01 0.04	0.00	0.00	20.9
18	27	-0	938	0	0	0	1022	--	--	16.08	16.08	0.00	0.02	0.01 0.06	0.00	0.00	20.9
19	27	-0	1055	0	0	0	1189	--	--	16.08	16.08	0.00	0.02	0.01 0.07	0.00	0.00	20.9
20	27	-0	1059	0	0	0	1165	--	--	16.08	16.08	0.00	0.02	0.01 0.07	0.00	0.00	20.9
37	27	-0	864	0	0	0	-236	--	--	16.08	16.08	0.18	0.00	0.01 0.05	0.00	0.00	20.9
38	27	-0	1060	0	0	0	1196	--	--	16.08	16.08	0.00	0.02	0.01 0.07	0.00	0.00	20.9
39	27	-0	1067	0	0	0	1156	--	--	16.08	16.08	0.00	0.02	0.01 0.07	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	54	-0	910	0	0	0	260	--	--	16.08	16.08	0.00	0.00	0.01 0.06	0.00	0.00	20.9
2	54	-0	684	0	0	0	189	--	--	16.08	16.08	0.10	0.00	0.01 0.04	0.00	0.00	20.9
3	54	-0	656	0	0	0	178	--	--	16.08	16.08	0.10	0.00	0.01 0.04	0.00	0.00	20.9
4	54	-0	744	0	0	0	221	--	--	16.08	16.08	0.10	0.00	0.01 0.05	0.00	0.00	20.9
5	54	-0	716	0	0	0	210	--	--	16.08	16.08	0.10	0.00	0.01 0.04	0.00	0.00	20.9
6	54	-0	737	0	0	0	214	--	--	16.08	16.08	0.10	0.00	0.01 0.05	0.00	0.00	20.9
7	54	-0	645	0	0	0	176	--	--	16.08	16.08	0.10	0.00	0.01 0.04	0.00	0.00	20.9
8	54	-0	755	0	0	0	223	--	--	16.08	16.08	0.10	0.00	0.01 0.05	0.00	0.00	20.9
9	54	-0	663	0	0	0	186	--	--	16.08	16.08	0.10	0.00	0.01 0.04	0.00	0.00	20.9
10	54	-0	684	0	0	0	189	--	--	16.08	16.08	0.10	0.00	0.01 0.04	0.00	0.00	20.9
11	54	-0	656	0	0	0	178	--	--	16.08	16.08	0.10	0.00	0.01 0.04	0.00	0.00	20.9
12	54	-0	744	0	0	0	221	--	--	16.08	16.08	0.10	0.00	0.01 0.05	0.00	0.00	20.9
13	54	-0	716	0	0	0	210	--	--	16.08	16.08	0.10	0.00	0.01 0.04	0.00	0.00	20.9
14	54	-0	737	0	0	0	214	--	--	16.08	16.08	0.10	0.00	0.01 0.05	0.00	0.00	20.9
15	54	-0	645	0	0	0	176	--	--	16.08	16.08	0.10	0.00	0.01 0.04	0.00	0.00	20.9
16	54	-0	755	0	0	0	223	--	--	16.08	16.08	0.10	0.00	0.01 0.05	0.00	0.00	20.9
17	54	-0	663	0	0	0	186	--	--	16.08	16.08	0.10	0.00	0.01 0.04	0.00	0.00	20.9
18	54	-0	938	0	0	0	272	--	--	16.08	16.08	0.00	0.00	0.01 0.06	0.00	0.00	20.9
19	54	-0	1055	0	0	0	344	--	--	16.08	16.08	0.00	0.01	0.01 0.07	0.00	0.00	20.9
20	54	-0	1059	0	0	0	316	--	--	16.08	16.08	0.00	0.01	0.01 0.07	0.00	0.00	20.9
37	54	-0	864	0	0	0	227	--	--	16.08	16.08	0.00	0.00	0.01 0.05	0.00	0.00	20.9
38	54	-0	1060	0	0	0	347	--	--	16.08	16.08	0.00	0.01	0.01 0.07	0.00	0.00	20.9
39	54	-0	1067	0	0	0	302	--	--	16.08	16.08	0.00	0.01	0.01 0.07	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 68 NI 1282 NF 1314 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle V,Mx	cmq/m		cm
1	0	-0	588	0	0	0	-354	--	--	16.08	16.08	0.18	0.01	0.00 0.04	0.00	0.00	20.9
2	0	-0	421	0	0	0	-263	--	--	16.08	16.08	0.29	0.00	0.00 0.03	0.00	0.00	20.9
3	0	-0	415	0	0	0	-258	--	--	16.08	16.08	0.29	0.00	0.00 0.03	0.00	0.00	20.9
4	0	-0	490	0	0	0	-286	--	--	16.08	16.08	0.29	0.00	0.00 0.03	0.00	0.00	20.9
5	0	-0	484	0	0	0	-281	--	--	16.08	16.08	0.29	0.00	0.00 0.03	0.00	0.00	20.9
6	0	-0	451	0	0	0	-276	--	--	16.08	16.08	0.29	0.00	0.00 0.03	0.00	0.00	20.9
7	0	-0	433	0	0	0	-261	--	--	16.08	16.08	0.29	0.00	0.00 0.03	0.00	0.00	20.9
8	0	-0	472	0	0	0	-283	--	--	16.08	16.08	0.29	0.00	0.00 0.03	0.00	0.00	20.9
9	0	-0	453	0	0	0	-268	--	--	16.08	16.08	0.29	0.00	0.00 0.03	0.00	0.00	20.9
10	0	-0	421	0	0	0	-263	--	--	16.08	16.08	0.29	0.00	0.00 0.03	0.00	0.00	20.9
11	0	-0	415	0	0	0	-258	--	--	16.08	16.08	0.29	0.00	0.00 0.03	0.00	0.00	20.9
12	0	-0	490	0	0	0	-286	--	--	16.08	16.08	0.29	0.00	0.00 0.03	0.00	0.00	20.9
13	0	-0	484	0	0	0	-281	--	--	16.08	16.08	0.29	0.00	0.00 0.03	0.00	0.00	20.9
14	0	-0	451	0	0	0	-276	--	--	16.08	16.08	0.29	0.00	0.00 0.03	0.00	0.00	20.9
15	0	-0	433	0	0	0	-261	--	--	16.08	16.08	0.29	0.00	0.00 0.03	0.00	0.00	20.9
16	0	-0	472	0	0	0	-283	--	--	16.08	16.08	0.29	0.00	0.00 0.03	0.00	0.00	20.9

17	0	-0	453	0	0	0	-268	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
18	0	-0	522	0	0	0	-334	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9
19	0	-0	702	0	0	0	-387	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
20	0	-0	639	0	0	0	-389	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
37	0	-0	452	0	0	0	-314	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9
38	0	-0	752	0	0	0	-404	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9
39	0	-0	646	0	0	0	-406	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	588	0	0	0	-354	--	--	16.08	16.08	0.18	0.01	0.00	0.04	0.00	0.00	20.9
2	27	-0	421	0	0	0	-263	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
3	27	-0	415	0	0	0	-258	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
4	27	-0	490	0	0	0	-286	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
5	27	-0	484	0	0	0	-281	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
6	27	-0	451	0	0	0	-276	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
7	27	-0	433	0	0	0	-261	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
8	27	-0	472	0	0	0	-283	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
9	27	-0	453	0	0	0	-268	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
10	27	-0	421	0	0	0	-263	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
11	27	-0	415	0	0	0	-258	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
12	27	-0	490	0	0	0	-286	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
13	27	-0	484	0	0	0	-281	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
14	27	-0	451	0	0	0	-276	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
15	27	-0	433	0	0	0	-261	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
16	27	-0	472	0	0	0	-283	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
17	27	-0	453	0	0	0	-268	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
18	27	-0	522	0	0	0	-334	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9
19	27	-0	702	0	0	0	-387	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
20	27	-0	639	0	0	0	-389	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
37	27	-0	452	0	0	0	-314	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9
38	27	-0	752	0	0	0	-404	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9
39	27	-0	646	0	0	0	-406	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	54	-0	588	0	0	0	-354	--	--	16.08	16.08	0.18	0.01	0.00	0.04	0.00	0.00	20.9
2	54	-0	421	0	0	0	-263	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
3	54	-0	415	0	0	0	-258	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
4	54	-0	490	0	0	0	-286	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
5	54	-0	484	0	0	0	-281	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
6	54	-0	451	0	0	0	-276	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
7	54	-0	433	0	0	0	-261	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
8	54	-0	472	0	0	0	-283	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
9	54	-0	453	0	0	0	-268	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
10	54	-0	421	0	0	0	-263	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
11	54	-0	415	0	0	0	-258	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
12	54	-0	490	0	0	0	-286	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
13	54	-0	484	0	0	0	-281	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
14	54	-0	451	0	0	0	-276	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
15	54	-0	433	0	0	0	-261	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
16	54	-0	472	0	0	0	-283	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
17	54	-0	453	0	0	0	-268	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
18	54	-0	522	0	0	0	-334	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9
19	54	-0	702	0	0	0	-387	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
20	54	-0	639	0	0	0	-389	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
37	54	-0	452	0	0	0	-314	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9
38	54	-0	752	0	0	0	-404	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9
39	54	-0	646	0	0	0	-406	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 69 NI 1312 NF 1282 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm

1	0	-0	-380	0	0	0	-434	--	--	16.08	16.08	0.18	0.01	0.00	0.02	0.00	0.00	20.9
2	0	-0	-348	0	0	0	-347	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
3	0	-0	-318	0	0	0	-327	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
4	0	-0	-268	0	0	0	-341	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
5	0	-0	-237	0	0	0	-320	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
6	0	-0	-355	0	0	0	-369	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
7	0	-0	-254	0	0	0	-301	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
8	0	-0	-331	0	0	0	-367	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
9	0	-0	-230	0	0	0	-299	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
10	0	-0	-348	0	0	0	-347	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
11	0	-0	-318	0	0	0	-327	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
12	0	-0	-268	0	0	0	-341	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
13	0	-0	-237	0	0	0	-320	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
14	0	-0	-355	0	0	0	-369	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
15	0	-0	-254	0	0	0	-301	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
16	0	-0	-331	0	0	0	-367	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
17	0	-0	-230	0	0	0	-299	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
18	0	-0	-612	0	0	0	-507	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
19	0	-0	-334	0	0	0	-450	--	--	16.08	16.08	0.18	0.01	0.00	0.02	0.00	0.00	20.9
20	0	-0	-510	0	0	0	-529	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9
37	0	-0	-666	0	0	0	-510	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
38	0	-0	-204	0	0	0	-414	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9
39	0	-0	-497	0	0	0	-546	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-380	0	0	0	-434	--	--	16.08	16.08	0.18	0.01	0.00	0.02	0.00	0.00	20.9
2	27	-0	-348	0	0	0	-347	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
3	27	-0	-318	0	0	0	-327	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
4	27	-0	-268	0	0	0	-341	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
5	27	-0	-237	0	0	0	-320	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
6	27	-0	-355	0	0	0	-369	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
7	27	-0	-254	0	0	0	-301	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
8	27	-0	-331	0	0	0	-367	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
9	27	-0	-230	0	0	0	-299	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
10	27	-0	-348	0	0	0	-347	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
11	27	-0	-318	0	0	0	-327	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
12	27	-0	-268	0	0	0	-341	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9

13	27	-0	-237	0	0	0	-320	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
14	27	-0	-355	0	0	0	-369	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
15	27	-0	-254	0	0	0	-301	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
16	27	-0	-331	0	0	0	-367	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
17	27	-0	-230	0	0	0	-299	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
18	27	-0	-612	0	0	0	-507	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
19	27	-0	-334	0	0	0	-450	--	--	16.08	16.08	0.18	0.01	0.00	0.02	0.00	0.00	20.9
20	27	-0	-510	0	0	0	-529	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9
37	27	-0	-666	0	0	0	-510	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
38	27	-0	-204	0	0	0	-414	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9
39	27	-0	-497	0	0	0	-546	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	54	-0	-380	0	0	0	-434	--	--	16.08	16.08	0.18	0.01	0.00	0.02	0.00	0.00	20.9
2	54	-0	-348	0	0	0	-347	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
3	54	-0	-318	0	0	0	-327	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
4	54	-0	-268	0	0	0	-341	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
5	54	-0	-237	0	0	0	-320	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
6	54	-0	-355	0	0	0	-369	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
7	54	-0	-254	0	0	0	-301	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
8	54	-0	-331	0	0	0	-367	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
9	54	-0	-230	0	0	0	-299	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
10	54	-0	-348	0	0	0	-347	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
11	54	-0	-318	0	0	0	-327	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
12	54	-0	-268	0	0	0	-341	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
13	54	-0	-237	0	0	0	-320	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
14	54	-0	-355	0	0	0	-369	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
15	54	-0	-254	0	0	0	-301	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
16	54	-0	-331	0	0	0	-367	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
17	54	-0	-230	0	0	0	-299	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
18	54	-0	-612	0	0	0	-507	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
19	54	-0	-334	0	0	0	-450	--	--	16.08	16.08	0.18	0.01	0.00	0.02	0.00	0.00	20.9
20	54	-0	-510	0	0	0	-529	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9
37	54	-0	-666	0	0	0	-510	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
38	54	-0	-204	0	0	0	-414	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9
39	54	-0	-497	0	0	0	-546	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 70 NI 1313 NF 1312 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-1339	0	0	0	123	--	--	16.08	16.08	0.00	0.00	0.01	0.08	0.00	0.00	20.9
2	0	-0	-1093	0	0	0	121	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
3	0	-0	-1048	0	0	0	119	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
4	0	-0	-1012	0	0	0	70	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
5	0	-0	-967	0	0	0	68	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
6	0	-0	-1117	0	0	0	106	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
7	0	-0	-967	0	0	0	98	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
8	0	-0	-1093	0	0	0	91	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
9	0	-0	-943	0	0	0	83	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
10	0	-0	-1093	0	0	0	121	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
11	0	-0	-1048	0	0	0	119	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
12	0	-0	-1012	0	0	0	70	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
13	0	-0	-967	0	0	0	68	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
14	0	-0	-1117	0	0	0	106	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
15	0	-0	-967	0	0	0	98	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
16	0	-0	-1093	0	0	0	91	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
17	0	-0	-943	0	0	0	83	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
18	0	-0	-1672	0	0	0	238	--	--	16.08	16.08	0.00	0.00	0.01	0.10	0.00	0.00	20.9
19	0	-0	-1362	0	0	0	94	--	--	16.08	16.08	0.00	0.00	0.01	0.09	0.00	0.00	20.9
20	0	-0	-1578	0	0	0	143	--	--	16.08	16.08	0.00	0.00	0.01	0.10	0.00	0.00	20.9
37	0	-0	-1700	0	0	0	266	--	--	16.08	16.08	0.00	0.00	0.01	0.11	0.00	0.00	20.9
38	0	-0	-1185	0	0	0	25	--	--	16.08	16.08	0.00	0.00	0.01	0.07	0.00	0.00	20.9
39	0	-0	-1544	0	0	0	107	--	--	16.08	16.08	0.00	0.00	0.01	0.10	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-1339	0	0	0	-594	--	--	16.08	16.08	0.18	0.01	0.01	0.08	0.00	0.00	20.9
2	27	-0	-1093	0	0	0	-464	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
3	27	-0	-1048	0	0	0	-443	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
4	27	-0	-1012	0	0	0	-472	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
5	27	-0	-967	0	0	0	-450	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
6	27	-0	-1117	0	0	0	-492	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
7	27	-0	-967	0	0	0	-420	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
8	27	-0	-1093	0	0	0	-495	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
9	27	-0	-943	0	0	0	-422	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
10	27	-0	-1093	0	0	0	-464	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
11	27	-0	-1048	0	0	0	-443	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
12	27	-0	-1012	0	0	0	-472	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
13	27	-0	-967	0	0	0	-450	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
14	27	-0	-1117	0	0	0	-492	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
15	27	-0	-967	0	0	0	-420	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
16	27	-0	-1093	0	0	0	-495	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
17	27	-0	-943	0	0	0	-422	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
18	27	-0	-1672	0	0	0	-657	--	--	16.08	16.08	0.18	0.01	0.01	0.10	0.00	0.00	20.9
19	27	-0	-1362	0	0	0	-636	--	--	16.08	16.08	0.18	0.01	0.01	0.09	0.00	0.00	20.9
20	27	-0	-1578	0	0	0	-702	--	--	16.08	16.08	0.18	0.01	0.01	0.10	0.00	0.00	20.9
37	27	-0	-1700	0	0	0	-645	--	--	16.08	16.08	0.18	0.01	0.01	0.11	0.00	0.00	20.9
38	27	-0	-1185	0	0	0	-610	--	--	16.08	16.08	0.18	0.01	0.01	0.07	0.00	0.00	20.9
39	27	-0	-1544	0	0	0	-720	--	--	16.08	16.08	0.18	0.01	0.01	0.10	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	54	-0	-1339	0	0	0	-594	--	--	16.08	16.08	0.18	0.01	0.01	0.08	0.00	0.00	20.9
2	54	-0	-1093	0	0	0	-464	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
3	54	-0	-1048	0	0	0	-443	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
4	54	-0	-1012	0	0	0	-472	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
5	54	-0	-967	0	0	0	-450	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
6	54	-0	-1117	0	0	0	-492	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
7	54	-0	-967	0	0	0	-420	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
8	54	-0	-1093	0	0	0	-495	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9

9	54	-0	-943	0	0	0	-422	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
10	54	-0	-1093	0	0	0	-464	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
11	54	-0	-1048	0	0	0	-443	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
12	54	-0	-1012	0	0	0	-472	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
13	54	-0	-967	0	0	0	-450	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
14	54	-0	-1117	0	0	0	-492	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
15	54	-0	-967	0	0	0	-420	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
16	54	-0	-1093	0	0	0	-495	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
17	54	-0	-943	0	0	0	-422	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
18	54	-0	-1672	0	0	0	-657	--	--	16.08	16.08	0.18	0.01	0.01	0.10	0.00	0.00	20.9
19	54	-0	-1362	0	0	0	-636	--	--	16.08	16.08	0.18	0.01	0.01	0.09	0.00	0.00	20.9
20	54	-0	-1578	0	0	0	-702	--	--	16.08	16.08	0.18	0.01	0.01	0.10	0.00	0.00	20.9
37	54	-0	-1700	0	0	0	-645	--	--	16.08	16.08	0.18	0.01	0.01	0.11	0.00	0.00	20.9
38	54	-0	-1185	0	0	0	-610	--	--	16.08	16.08	0.18	0.01	0.01	0.07	0.00	0.00	20.9
39	54	-0	-1544	0	0	0	-720	--	--	16.08	16.08	0.18	0.01	0.01	0.10	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 71 NI 1280 NF 1313 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-2249	0	0	0	730	--	--	16.08	16.08	0.00	0.01	0.02	0.14	0.00	0.00	20.9
2	0	-0	-1791	0	0	0	597	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
3	0	-0	-1746	0	0	0	590	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
4	0	-0	-1714	0	0	0	534	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
5	0	-0	-1669	0	0	0	526	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
6	0	-0	-1817	0	0	0	583	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
7	0	-0	-1666	0	0	0	559	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
8	0	-0	-1794	0	0	0	564	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
9	0	-0	-1643	0	0	0	540	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
10	0	-0	-1791	0	0	0	597	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
11	0	-0	-1746	0	0	0	590	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
12	0	-0	-1714	0	0	0	534	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
13	0	-0	-1669	0	0	0	526	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
14	0	-0	-1817	0	0	0	583	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
15	0	-0	-1666	0	0	0	559	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
16	0	-0	-1794	0	0	0	564	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
17	0	-0	-1643	0	0	0	540	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
18	0	-0	-2648	0	0	0	924	--	--	16.08	16.08	0.00	0.02	0.02	0.17	0.00	0.00	20.9
19	0	-0	-2337	0	0	0	732	--	--	16.08	16.08	0.00	0.01	0.02	0.15	0.00	0.00	20.9
20	0	-0	-2550	0	0	0	809	--	--	16.08	16.08	0.00	0.01	0.02	0.16	0.00	0.00	20.9
37	0	-0	-2647	0	0	0	943	--	--	16.08	16.08	0.00	0.02	0.02	0.17	0.00	0.00	20.9
38	0	-0	-2129	0	0	0	623	--	--	16.08	16.08	0.00	0.01	0.02	0.13	0.00	0.00	20.9
39	0	-0	-2484	0	0	0	751	--	--	16.08	16.08	0.00	0.01	0.02	0.16	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-2249	0	0	0	730	--	--	16.08	16.08	0.00	0.01	0.02	0.14	0.00	0.00	20.9
2	27	-0	-1791	0	0	0	597	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
3	27	-0	-1746	0	0	0	590	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
4	27	-0	-1714	0	0	0	534	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
5	27	-0	-1669	0	0	0	526	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
6	27	-0	-1817	0	0	0	583	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
7	27	-0	-1666	0	0	0	559	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
8	27	-0	-1794	0	0	0	564	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
9	27	-0	-1643	0	0	0	540	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
10	27	-0	-1791	0	0	0	597	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
11	27	-0	-1746	0	0	0	590	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
12	27	-0	-1714	0	0	0	534	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
13	27	-0	-1669	0	0	0	526	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
14	27	-0	-1817	0	0	0	583	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
15	27	-0	-1666	0	0	0	559	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
16	27	-0	-1794	0	0	0	564	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
17	27	-0	-1643	0	0	0	540	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
18	27	-0	-2648	0	0	0	924	--	--	16.08	16.08	0.00	0.02	0.02	0.17	0.00	0.00	20.9
19	27	-0	-2337	0	0	0	732	--	--	16.08	16.08	0.00	0.01	0.02	0.15	0.00	0.00	20.9
20	27	-0	-2550	0	0	0	809	--	--	16.08	16.08	0.00	0.01	0.02	0.16	0.00	0.00	20.9
37	27	-0	-2647	0	0	0	943	--	--	16.08	16.08	0.00	0.02	0.02	0.17	0.00	0.00	20.9
38	27	-0	-2129	0	0	0	623	--	--	16.08	16.08	0.00	0.01	0.02	0.13	0.00	0.00	20.9
39	27	-0	-2484	0	0	0	751	--	--	16.08	16.08	0.00	0.01	0.02	0.16	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	54	-0	-2249	0	0	0	-475	--	--	16.08	16.08	0.18	0.01	0.02	0.14	0.00	0.00	20.9
2	54	-0	-1791	0	0	0	-363	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
3	54	-0	-1746	0	0	0	-346	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
4	54	-0	-1714	0	0	0	-384	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
5	54	-0	-1669	0	0	0	-367	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
6	54	-0	-1817	0	0	0	-390	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
7	54	-0	-1666	0	0	0	-334	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
8	54	-0	-1794	0	0	0	-397	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
9	54	-0	-1643	0	0	0	-340	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
10	54	-0	-1791	0	0	0	-363	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
11	54	-0	-1746	0	0	0	-346	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
12	54	-0	-1714	0	0	0	-384	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
13	54	-0	-1669	0	0	0	-367	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
14	54	-0	-1817	0	0	0	-390	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
15	54	-0	-1666	0	0	0	-334	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
16	54	-0	-1794	0	0	0	-397	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
17	54	-0	-1643	0	0	0	-340	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
18	54	-0	-2648	0	0	0	-494	--	--	16.08	16.08	0.18	0.01	0.02	0.17	0.00	0.00	20.9
19	54	-0	-2337	0	0	0	-520	--	--	16.08	16.08	0.18	0.01	0.02	0.15	0.00	0.00	20.9
20	54	-0	-2550	0	0	0	-557	--	--	16.08	16.08	0.18	0.01	0.02	0.16	0.00	0.00	20.9
37	54	-0	-2647	0	0	0	-475	--	--	16.08	16.08	0.18	0.01	0.02	0.17	0.00	0.00	20.9
38	54	-0	-2129	0	0	0	-518	--	--	16.08	16.08	0.18	0.01	0.02	0.13	0.00	0.00	20.9
39	54	-0	-2484	0	0	0	-579	--	--	16.08	16.08	0.18	0.01	0.02	0.16	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 72 NI 1281 NF 1280 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-2887	0	0	0	1360	--	--	16.08	16.08	0.00	0.02	0.02	0.18	0.00	0.00	20.9
2	0	-0	-2262	0	0	0	1078	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
3	0	-0	-2242	0	0	0	1082	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
4	0	-0	-2199	0	0	0	1011	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
5	0	-0	-2179	0	0	0	1015	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
6	0	-0	-2265	0	0	0	1050	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
7	0	-0	-2195	0	0	0	1063	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
8	0	-0	-2246	0	0	0	1030	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
9	0	-0	-2176	0	0	0	1043	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
10	0	-0	-2262	0	0	0	1078	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
11	0	-0	-2242	0	0	0	1082	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
12	0	-0	-2199	0	0	0	1011	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
13	0	-0	-2179	0	0	0	1015	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
14	0	-0	-2265	0	0	0	1050	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
15	0	-0	-2195	0	0	0	1063	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
16	0	-0	-2246	0	0	0	1030	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
17	0	-0	-2176	0	0	0	1043	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
18	0	-0	-3266	0	0	0	1589	--	--	16.08	16.08	0.00	0.03	0.03	0.20	0.00	0.00	20.9
19	0	-0	-3023	0	0	0	1399	--	--	16.08	16.08	0.00	0.02	0.02	0.19	0.00	0.00	20.9
20	0	-0	-3165	0	0	0	1457	--	--	16.08	16.08	0.00	0.02	0.03	0.20	0.00	0.00	20.9
37	0	-0	-3232	0	0	0	1588	--	--	16.08	16.08	0.00	0.03	0.03	0.20	0.00	0.00	20.9
38	0	-0	-2828	0	0	0	1272	--	--	16.08	16.08	0.00	0.02	0.02	0.18	0.00	0.00	20.9
39	0	-0	-3064	0	0	0	1368	--	--	16.08	16.08	0.00	0.02	0.03	0.19	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-2887	0	0	0	1360	--	--	16.08	16.08	0.00	0.02	0.02	0.18	0.00	0.00	20.9
2	27	-0	-2262	0	0	0	1078	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
3	27	-0	-2242	0	0	0	1082	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
4	27	-0	-2199	0	0	0	1011	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
5	27	-0	-2179	0	0	0	1015	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
6	27	-0	-2265	0	0	0	1050	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
7	27	-0	-2195	0	0	0	1063	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
8	27	-0	-2246	0	0	0	1030	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
9	27	-0	-2176	0	0	0	1043	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
10	27	-0	-2262	0	0	0	1078	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
11	27	-0	-2242	0	0	0	1082	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
12	27	-0	-2199	0	0	0	1011	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
13	27	-0	-2179	0	0	0	1015	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
14	27	-0	-2265	0	0	0	1050	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
15	27	-0	-2195	0	0	0	1063	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
16	27	-0	-2246	0	0	0	1030	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
17	27	-0	-2176	0	0	0	1043	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
18	27	-0	-3266	0	0	0	1589	--	--	16.08	16.08	0.00	0.03	0.03	0.20	0.00	0.00	20.9
19	27	-0	-3023	0	0	0	1399	--	--	16.08	16.08	0.00	0.02	0.02	0.19	0.00	0.00	20.9
20	27	-0	-3165	0	0	0	1457	--	--	16.08	16.08	0.00	0.02	0.03	0.20	0.00	0.00	20.9
37	27	-0	-3232	0	0	0	1588	--	--	16.08	16.08	0.00	0.03	0.03	0.20	0.00	0.00	20.9
38	27	-0	-2828	0	0	0	1272	--	--	16.08	16.08	0.00	0.02	0.02	0.18	0.00	0.00	20.9
39	27	-0	-3064	0	0	0	1368	--	--	16.08	16.08	0.00	0.02	0.03	0.19	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	54	-0	-2887	0	0	0	-186	--	--	16.08	16.08	0.18	0.00	0.02	0.18	0.00	0.00	20.9
2	54	-0	-2262	0	0	0	-134	--	--	16.08	16.08	0.29	0.00	0.02	0.14	0.00	0.00	20.9
3	54	-0	-2242	0	0	0	-119	--	--	16.08	16.08	0.29	0.00	0.02	0.14	0.00	0.00	20.9
4	54	-0	-2199	0	0	0	-167	--	--	16.08	16.08	0.29	0.00	0.02	0.14	0.00	0.00	20.9
5	54	-0	-2179	0	0	0	-152	--	--	16.08	16.08	0.29	0.00	0.02	0.14	0.00	0.00	20.9
6	54	-0	-2265	0	0	0	-163	--	--	16.08	16.08	0.29	0.00	0.02	0.14	0.00	0.00	20.9
7	54	-0	-2195	0	0	0	-113	--	--	16.08	16.08	0.29	0.00	0.02	0.14	0.00	0.00	20.9
8	54	-0	-2246	0	0	0	-173	--	--	16.08	16.08	0.29	0.00	0.02	0.14	0.00	0.00	20.9
9	54	-0	-2176	0	0	0	-123	--	--	16.08	16.08	0.29	0.00	0.02	0.14	0.00	0.00	20.9
10	54	-0	-2262	0	0	0	-134	--	--	16.08	16.08	0.29	0.00	0.02	0.14	0.00	0.00	20.9
11	54	-0	-2242	0	0	0	-119	--	--	16.08	16.08	0.29	0.00	0.02	0.14	0.00	0.00	20.9
12	54	-0	-2199	0	0	0	-167	--	--	16.08	16.08	0.29	0.00	0.02	0.14	0.00	0.00	20.9
13	54	-0	-2179	0	0	0	-152	--	--	16.08	16.08	0.29	0.00	0.02	0.14	0.00	0.00	20.9
14	54	-0	-2265	0	0	0	-163	--	--	16.08	16.08	0.29	0.00	0.02	0.14	0.00	0.00	20.9
15	54	-0	-2195	0	0	0	-113	--	--	16.08	16.08	0.29	0.00	0.02	0.14	0.00	0.00	20.9
16	54	-0	-2246	0	0	0	-173	--	--	16.08	16.08	0.29	0.00	0.02	0.14	0.00	0.00	20.9
17	54	-0	-2176	0	0	0	-123	--	--	16.08	16.08	0.29	0.00	0.02	0.14	0.00	0.00	20.9
18	54	-0	-3266	0	0	0	-161	--	--	16.08	16.08	0.18	0.00	0.03	0.20	0.00	0.00	20.9
19	54	-0	-3023	0	0	0	-221	--	--	16.08	16.08	0.18	0.00	0.02	0.19	0.00	0.00	20.9
20	54	-0	-3165	0	0	0	-239	--	--	16.08	16.08	0.18	0.00	0.03	0.20	0.00	0.00	20.9
37	54	-0	-3232	0	0	0	-143	--	--	16.08	16.08	0.18	0.00	0.03	0.20	0.00	0.00	20.9
38	54	-0	-2828	0	0	0	-243	--	--	16.08	16.08	0.18	0.00	0.02	0.18	0.00	0.00	20.9
39	54	-0	-3064	0	0	0	-273	--	--	16.08	16.08	0.18	0.00	0.03	0.19	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 73 NI 1321 NF 1281 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-2879	0	0	0	1977	--	--	16.08	16.08	0.00	0.03	0.02	0.18	0.00	0.00	20.9
2	0	-0	-2241	0	0	0	1554	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
3	0	-0	-2241	0	0	0	1562	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
4	0	-0	-2187	0	0	0	1479	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
5	0	-0	-2188	0	0	0	1487	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
6	0	-0	-2221	0	0	0	1519	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
7	0	-0	-2223	0	0	0	1545	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
8	0	-0	-2205	0	0	0	1496	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
9	0	-0	-2207	0	0	0	1522	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
10	0	-0	-2241	0	0	0	1554	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
11	0	-0	-2241	0	0	0	1562	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
12	0	-0	-2187	0	0	0	1479	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
13	0	-0	-2188	0	0	0	1487	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
14	0	-0	-2221	0	0	0	1519	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
15	0	-0	-2223	0	0	0	1545	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
16	0	-0	-2205	0	0	0	1496	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9

17	0	-0	-2207	0	0	0	1522	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
18	0	-0	-3203	0	0	0	2262	--	--	16.08	16.08	0.00	0.04	0.03	0.20	0.00	0.00	20.9
19	0	-0	-3003	0	0	0	2039	--	--	16.08	16.08	0.00	0.03	0.02	0.19	0.00	0.00	20.9
20	0	-0	-3103	0	0	0	2111	--	--	16.08	16.08	0.00	0.04	0.03	0.19	0.00	0.00	20.9
37	0	-0	-3168	0	0	0	2254	--	--	16.08	16.08	0.00	0.04	0.03	0.20	0.00	0.00	20.9
38	0	-0	-2836	0	0	0	1883	--	--	16.08	16.08	0.00	0.03	0.02	0.18	0.00	0.00	20.9
39	0	-0	-3002	0	0	0	2002	--	--	16.08	16.08	0.00	0.03	0.02	0.19	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-2879	0	0	0	1977	--	--	16.08	16.08	0.00	0.03	0.02	0.18	0.00	0.00	20.9
2	27	-0	-2241	0	0	0	1554	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
3	27	-0	-2241	0	0	0	1562	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
4	27	-0	-2187	0	0	0	1479	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
5	27	-0	-2188	0	0	0	1487	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
6	27	-0	-2221	0	0	0	1519	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
7	27	-0	-2223	0	0	0	1545	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
8	27	-0	-2205	0	0	0	1496	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
9	27	-0	-2207	0	0	0	1522	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
10	27	-0	-2241	0	0	0	1554	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
11	27	-0	-2241	0	0	0	1562	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
12	27	-0	-2187	0	0	0	1479	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
13	27	-0	-2188	0	0	0	1487	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
14	27	-0	-2221	0	0	0	1519	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
15	27	-0	-2223	0	0	0	1545	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
16	27	-0	-2205	0	0	0	1496	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
17	27	-0	-2207	0	0	0	1522	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
18	27	-0	-3203	0	0	0	2262	--	--	16.08	16.08	0.00	0.04	0.03	0.20	0.00	0.00	20.9
19	27	-0	-3003	0	0	0	2039	--	--	16.08	16.08	0.00	0.03	0.02	0.19	0.00	0.00	20.9
20	27	-0	-3103	0	0	0	2111	--	--	16.08	16.08	0.00	0.04	0.03	0.19	0.00	0.00	20.9
37	27	-0	-3168	0	0	0	2254	--	--	16.08	16.08	0.00	0.04	0.03	0.20	0.00	0.00	20.9
38	27	-0	-2836	0	0	0	1883	--	--	16.08	16.08	0.00	0.03	0.02	0.18	0.00	0.00	20.9
39	27	-0	-3002	0	0	0	2002	--	--	16.08	16.08	0.00	0.03	0.02	0.19	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	54	-0	-2879	0	0	0	434	--	--	16.08	16.08	0.00	0.01	0.02	0.18	0.00	0.00	20.9
2	54	-0	-2241	0	0	0	354	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
3	54	-0	-2241	0	0	0	361	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
4	54	-0	-2187	0	0	0	307	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
5	54	-0	-2188	0	0	0	315	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
6	54	-0	-2221	0	0	0	329	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
7	54	-0	-2223	0	0	0	354	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
8	54	-0	-2205	0	0	0	315	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
9	54	-0	-2207	0	0	0	340	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
10	54	-0	-2241	0	0	0	354	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
11	54	-0	-2241	0	0	0	361	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
12	54	-0	-2187	0	0	0	307	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
13	54	-0	-2188	0	0	0	315	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
14	54	-0	-2221	0	0	0	329	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
15	54	-0	-2223	0	0	0	354	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
16	54	-0	-2205	0	0	0	315	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
17	54	-0	-2207	0	0	0	340	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
18	54	-0	-3203	0	0	0	546	--	--	16.08	16.08	0.00	0.01	0.03	0.20	0.00	0.00	20.9
19	54	-0	-3003	0	0	0	430	--	--	16.08	16.08	0.00	0.01	0.02	0.19	0.00	0.00	20.9
20	54	-0	-3103	0	0	0	448	--	--	16.08	16.08	0.00	0.01	0.03	0.19	0.00	0.00	20.9
37	54	-0	-3168	0	0	0	557	--	--	16.08	16.08	0.00	0.01	0.03	0.20	0.00	0.00	20.9
38	54	-0	-2836	0	0	0	363	--	--	16.08	16.08	0.00	0.01	0.02	0.18	0.00	0.00	20.9
39	54	-0	-3002	0	0	0	394	--	--	16.08	16.08	0.00	0.01	0.02	0.19	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 74 NI 1311 NF 1320 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm

1	0	-0	1843	0	0	0	368	--	--	16.08	16.08	0.00	0.01	0.02	0.12	0.00	0.00	20.9
2	0	-0	1382	0	0	0	335	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
3	0	-0	1378	0	0	0	339	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
4	0	-0	1458	0	0	0	228	--	--	16.08	16.08	0.10	0.00	0.01	0.09	0.00	0.00	20.9
5	0	-0	1453	0	0	0	232	--	--	16.08	16.08	0.10	0.00	0.01	0.09	0.00	0.00	20.9
6	0	-0	1414	0	0	0	293	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
7	0	-0	1399	0	0	0	306	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
8	0	-0	1437	0	0	0	261	--	--	16.08	16.08	0.10	0.00	0.01	0.09	0.00	0.00	20.9
9	0	-0	1421	0	0	0	274	--	--	16.08	16.08	0.10	0.00	0.01	0.09	0.00	0.00	20.9
10	0	-0	1382	0	0	0	335	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
11	0	-0	1378	0	0	0	339	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
12	0	-0	1458	0	0	0	228	--	--	16.08	16.08	0.10	0.00	0.01	0.09	0.00	0.00	20.9
13	0	-0	1453	0	0	0	232	--	--	16.08	16.08	0.10	0.00	0.01	0.09	0.00	0.00	20.9
14	0	-0	1414	0	0	0	293	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
15	0	-0	1399	0	0	0	306	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
16	0	-0	1437	0	0	0	261	--	--	16.08	16.08	0.10	0.00	0.01	0.09	0.00	0.00	20.9
17	0	-0	1421	0	0	0	274	--	--	16.08	16.08	0.10	0.00	0.01	0.09	0.00	0.00	20.9
18	0	-0	1805	0	0	0	619	--	--	16.08	16.08	0.00	0.01	0.01	0.11	0.00	0.00	20.9
19	0	-0	2102	0	0	0	268	--	--	16.08	16.08	0.00	0.00	0.02	0.13	0.00	0.00	20.9
20	0	-0	1874	0	0	0	455	--	--	16.08	16.08	0.00	0.01	0.02	0.12	0.00	0.00	20.9
37	0	-0	1638	0	0	0	708	--	--	16.08	16.08	0.00	0.01	0.01	0.10	0.00	0.00	20.9
38	0	-0	2133	0	0	0	123	--	--	16.08	16.08	0.00	0.00	0.02	0.13	0.00	0.00	20.9
39	0	-0	1754	0	0	0	436	--	--	16.08	16.08	0.00	0.01	0.01	0.11	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	1843	0	0	0	2831	--	--	16.08	16.08	0.00	0.05	0.02	0.12	0.00	0.00	20.9
2	27	-0	1382	0	0	0	2182	--	--	16.08	16.08	0.10	0.04	0.01	0.09	0.00	0.00	20.9
3	27	-0	1378	0	0	0	2181	--	--	16.08	16.08	0.10	0.04	0.01	0.09	0.00	0.00	20.9
4	27	-0	1458	0	0	0	2177	--	--	16.08	16.08	0.10	0.04	0.01	0.09	0.00	0.00	20.9
5	27	-0	1453	0	0	0	2174	--	--	16.08	16.08	0.10	0.04	0.01	0.09	0.00	0.00	20.9
6	27	-0	1414	0	0	0	2183	--	--	16.08	16.08	0.10	0.04	0.01	0.09	0.00	0.00	20.9
7	27	-0	1399	0	0	0	2176	--	--	16.08	16.08	0.10	0.04	0.01	0.09	0.00	0.00	20.9
8	27	-0	1437	0	0	0	2181	--	--	16.08	16.08	0.10	0.04	0.01	0.09	0.00	0.00	20.9
9	27	-0	1421	0	0	0	2173	--	--	16.08	16.08	0.10	0.04	0.01	0.09	0.00	0.00	20.9
10	27	-0	1382	0	0	0	2182	--	--	16.08	16.08	0.10	0.04	0.01	0.09	0.00	0.00	20.9
11	27	-0	1378	0	0	0	2181	--	--	16.08	16.08	0.10	0.04	0.01	0.09	0.00	0.00	20.9
12	27	-0	1458	0	0	0	2177	--	--	16.08	16.08	0.10	0.04	0.01	0.09	0.00	0.00	20.9

13	27	-0	1453	0	0	0	2174	--	--	16.08	16.08	0.10	0.04	0.01	0.09	0.00	0.00	20.9
14	27	-0	1414	0	0	0	2183	--	--	16.08	16.08	0.10	0.04	0.01	0.09	0.00	0.00	20.9
15	27	-0	1399	0	0	0	2176	--	--	16.08	16.08	0.10	0.04	0.01	0.09	0.00	0.00	20.9
16	27	-0	1437	0	0	0	2181	--	--	16.08	16.08	0.10	0.04	0.01	0.09	0.00	0.00	20.9
17	27	-0	1421	0	0	0	2173	--	--	16.08	16.08	0.10	0.04	0.01	0.09	0.00	0.00	20.9
18	27	-0	1805	0	0	0	3031	--	--	16.08	16.08	0.00	0.05	0.01	0.11	0.00	0.00	20.9
19	27	-0	2102	0	0	0	3077	--	--	16.08	16.08	0.00	0.05	0.02	0.13	0.00	0.00	20.9
20	27	-0	1874	0	0	0	2961	--	--	16.08	16.08	0.00	0.05	0.02	0.12	0.00	0.00	20.9
37	27	-0	1638	0	0	0	2898	--	--	16.08	16.08	0.00	0.05	0.01	0.10	0.00	0.00	20.9
38	27	-0	2133	0	0	0	2974	--	--	16.08	16.08	0.00	0.05	0.02	0.13	0.00	0.00	20.9
39	27	-0	1754	0	0	0	2780	--	--	16.08	16.08	0.00	0.05	0.01	0.11	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	54	-0	1843	0	0	0	1355	--	--	16.08	16.08	0.00	0.02	0.02	0.12	0.00	0.00	20.9
2	54	-0	1382	0	0	0	1075	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
3	54	-0	1378	0	0	0	1077	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
4	54	-0	1458	0	0	0	1009	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
5	54	-0	1453	0	0	0	1010	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
6	54	-0	1414	0	0	0	1050	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
7	54	-0	1399	0	0	0	1055	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
8	54	-0	1437	0	0	0	1030	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
9	54	-0	1421	0	0	0	1035	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
10	54	-0	1382	0	0	0	1075	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
11	54	-0	1378	0	0	0	1077	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
12	54	-0	1458	0	0	0	1009	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
13	54	-0	1453	0	0	0	1010	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
14	54	-0	1414	0	0	0	1050	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
15	54	-0	1399	0	0	0	1055	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
16	54	-0	1437	0	0	0	1030	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
17	54	-0	1421	0	0	0	1035	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
18	54	-0	1805	0	0	0	1586	--	--	16.08	16.08	0.00	0.03	0.01	0.11	0.00	0.00	20.9
19	54	-0	2102	0	0	0	1393	--	--	16.08	16.08	0.00	0.02	0.02	0.13	0.00	0.00	20.9
20	54	-0	1874	0	0	0	1460	--	--	16.08	16.08	0.00	0.02	0.02	0.12	0.00	0.00	20.9
37	54	-0	1638	0	0	0	1586	--	--	16.08	16.08	0.00	0.03	0.01	0.10	0.00	0.00	20.9
38	54	-0	2133	0	0	0	1265	--	--	16.08	16.08	0.00	0.02	0.02	0.13	0.00	0.00	20.9
39	54	-0	1754	0	0	0	1376	--	--	16.08	16.08	0.00	0.02	0.01	0.11	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 75 NI 1318 NF 1311 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	1104	0	0	0	312	--	--	16.08	16.08	0.00	0.01	0.01	0.07	0.00	0.00	20.9
2	0	-0	785	0	0	0	302	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
3	0	-0	811	0	0	0	306	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
4	0	-0	887	0	0	0	175	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
5	0	-0	913	0	0	0	179	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
6	0	-0	790	0	0	0	253	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
7	0	-0	877	0	0	0	266	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
8	0	-0	821	0	0	0	214	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
9	0	-0	908	0	0	0	228	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
10	0	-0	785	0	0	0	302	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
11	0	-0	811	0	0	0	306	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
12	0	-0	887	0	0	0	175	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
13	0	-0	913	0	0	0	179	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
14	0	-0	790	0	0	0	253	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
15	0	-0	877	0	0	0	266	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
16	0	-0	821	0	0	0	214	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
17	0	-0	908	0	0	0	228	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
18	0	-0	891	0	0	0	610	--	--	16.08	16.08	0.00	0.01	0.01	0.06	0.00	0.00	20.9
19	0	-0	1345	0	0	0	172	--	--	16.08	16.08	0.00	0.00	0.01	0.08	0.00	0.00	20.9
20	0	-0	1002	0	0	0	415	--	--	16.08	16.08	0.00	0.01	0.01	0.06	0.00	0.00	20.9
37	0	-0	705	0	0	0	731	--	--	16.08	16.08	0.00	0.01	0.01	0.04	0.00	0.00	20.9
38	0	-0	1462	0	0	0	2	--	--	16.08	16.08	0.00	0.00	0.01	0.09	0.00	0.00	20.9
39	0	-0	890	0	0	0	406	--	--	16.08	16.08	0.00	0.01	0.01	0.06	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	1104	0	0	0	1788	--	--	16.08	16.08	0.00	0.03	0.01	0.07	0.00	0.00	20.9
2	27	-0	785	0	0	0	1351	--	--	16.08	16.08	0.10	0.02	0.01	0.05	0.00	0.00	20.9
3	27	-0	811	0	0	0	1390	--	--	16.08	16.08	0.10	0.02	0.01	0.05	0.00	0.00	20.9
4	27	-0	887	0	0	0	1360	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9
5	27	-0	913	0	0	0	1399	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9
6	27	-0	790	0	0	0	1309	--	--	16.08	16.08	0.10	0.02	0.01	0.05	0.00	0.00	20.9
7	27	-0	877	0	0	0	1439	--	--	16.08	16.08	0.10	0.03	0.01	0.06	0.00	0.00	20.9
8	27	-0	821	0	0	0	1311	--	--	16.08	16.08	0.10	0.02	0.01	0.05	0.00	0.00	20.9
9	27	-0	908	0	0	0	1441	--	--	16.08	16.08	0.10	0.03	0.01	0.06	0.00	0.00	20.9
10	27	-0	785	0	0	0	1351	--	--	16.08	16.08	0.10	0.02	0.01	0.05	0.00	0.00	20.9
11	27	-0	811	0	0	0	1390	--	--	16.08	16.08	0.10	0.02	0.01	0.05	0.00	0.00	20.9
12	27	-0	887	0	0	0	1360	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9
13	27	-0	913	0	0	0	1399	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9
14	27	-0	790	0	0	0	1309	--	--	16.08	16.08	0.10	0.02	0.01	0.05	0.00	0.00	20.9
15	27	-0	877	0	0	0	1439	--	--	16.08	16.08	0.10	0.03	0.01	0.06	0.00	0.00	20.9
16	27	-0	821	0	0	0	1311	--	--	16.08	16.08	0.10	0.02	0.01	0.05	0.00	0.00	20.9
17	27	-0	908	0	0	0	1441	--	--	16.08	16.08	0.10	0.03	0.01	0.06	0.00	0.00	20.9
18	27	-0	891	0	0	0	1801	--	--	16.08	16.08	0.00	0.03	0.01	0.06	0.00	0.00	20.9
19	27	-0	1345	0	0	0	1970	--	--	16.08	16.08	0.00	0.03	0.01	0.08	0.00	0.00	20.9
20	27	-0	1002	0	0	0	1754	--	--	16.08	16.08	0.00	0.03	0.01	0.06	0.00	0.00	20.9
37	27	-0	705	0	0	0	1674	--	--	16.08	16.08	0.00	0.03	0.01	0.04	0.00	0.00	20.9
38	27	-0	1462	0	0	0	1956	--	--	16.08	16.08	0.00	0.03	0.01	0.09	0.00	0.00	20.9
39	27	-0	890	0	0	0	1596	--	--	16.08	16.08	0.00	0.03	0.01	0.06	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	54	-0	1104	0	0	0	904	--	--	16.08	16.08	0.00	0.02	0.01	0.07	0.00	0.00	20.9
2	54	-0	785	0	0	0	723	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
3	54	-0	811	0	0	0	741	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
4	54	-0	887	0	0	0	650	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
5	54	-0	913	0	0	0	668	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
6	54	-0	790	0	0	0	676	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
7	54	-0	877	0	0	0	736	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
8	54	-0	821	0	0	0	654	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9

9	54	-0	908	0	0	0	714	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
10	54	-0	785	0	0	0	723	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
11	54	-0	811	0	0	0	741	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
12	54	-0	887	0	0	0	650	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
13	54	-0	913	0	0	0	668	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
14	54	-0	790	0	0	0	676	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
15	54	-0	877	0	0	0	736	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
16	54	-0	821	0	0	0	654	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
17	54	-0	908	0	0	0	714	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
18	54	-0	891	0	0	0	1087	--	--	16.08	16.08	0.00	0.02	0.01	0.06	0.00	0.00	20.9
19	54	-0	1345	0	0	0	893	--	--	16.08	16.08	0.00	0.02	0.01	0.08	0.00	0.00	20.9
20	54	-0	1002	0	0	0	952	--	--	16.08	16.08	0.00	0.02	0.01	0.06	0.00	0.00	20.9
37	54	-0	705	0	0	0	1109	--	--	16.08	16.08	0.00	0.02	0.01	0.04	0.00	0.00	20.9
38	54	-0	1462	0	0	0	785	--	--	16.08	16.08	0.00	0.01	0.01	0.09	0.00	0.00	20.9
39	54	-0	890	0	0	0	883	--	--	16.08	16.08	0.00	0.02	0.01	0.06	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 76 NI 1319 NF 1318 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-8	0	0	0	548	--	--	16.08	16.08	0.00	0.01	0.00	0.00	0.00	0.00	20.9
2	0	-0	-91	0	0	0	505	--	--	16.08	16.08	0.10	0.01	0.00	0.01	0.00	0.00	20.9
3	0	-0	-55	0	0	0	503	--	--	16.08	16.08	0.10	0.01	0.00	0.00	0.00	0.00	20.9
4	0	-0	42	0	0	0	340	--	--	16.08	16.08	0.10	0.01	0.00	0.00	0.00	0.00	20.9
5	0	-0	78	0	0	0	338	--	--	16.08	16.08	0.10	0.01	0.00	0.00	0.00	0.00	20.9
6	0	-0	-88	0	0	0	449	--	--	16.08	16.08	0.10	0.01	0.00	0.01	0.00	0.00	20.9
7	0	-0	35	0	0	0	443	--	--	16.08	16.08	0.10	0.01	0.00	0.00	0.00	0.00	20.9
8	0	-0	-48	0	0	0	400	--	--	16.08	16.08	0.10	0.01	0.00	0.00	0.00	0.00	20.9
9	0	-0	75	0	0	0	394	--	--	16.08	16.08	0.10	0.01	0.00	0.00	0.00	0.00	20.9
10	0	-0	-91	0	0	0	505	--	--	16.08	16.08	0.10	0.01	0.00	0.01	0.00	0.00	20.9
11	0	-0	-55	0	0	0	503	--	--	16.08	16.08	0.10	0.01	0.00	0.00	0.00	0.00	20.9
12	0	-0	42	0	0	0	340	--	--	16.08	16.08	0.10	0.01	0.00	0.00	0.00	0.00	20.9
13	0	-0	78	0	0	0	338	--	--	16.08	16.08	0.10	0.01	0.00	0.00	0.00	0.00	20.9
14	0	-0	-88	0	0	0	449	--	--	16.08	16.08	0.10	0.01	0.00	0.01	0.00	0.00	20.9
15	0	-0	35	0	0	0	443	--	--	16.08	16.08	0.10	0.01	0.00	0.00	0.00	0.00	20.9
16	0	-0	-48	0	0	0	400	--	--	16.08	16.08	0.10	0.01	0.00	0.00	0.00	0.00	20.9
17	0	-0	75	0	0	0	394	--	--	16.08	16.08	0.10	0.01	0.00	0.00	0.00	0.00	20.9
18	0	-0	-408	0	0	0	969	--	--	16.08	16.08	0.00	0.02	0.00	0.03	0.00	0.00	20.9
19	0	-0	204	0	0	0	364	--	--	16.08	16.08	0.00	0.01	0.00	0.01	0.00	0.00	20.9
20	0	-0	-208	0	0	0	698	--	--	16.08	16.08	0.00	0.01	0.00	0.01	0.00	0.00	20.9
37	0	-0	-606	0	0	0	1137	--	--	16.08	16.08	0.00	0.02	0.00	0.04	0.00	0.00	20.9
38	0	-0	414	0	0	0	129	--	--	16.08	16.08	0.00	0.00	0.00	0.03	0.00	0.00	20.9
39	0	-0	-274	0	0	0	686	--	--	16.08	16.08	0.00	0.01	0.00	0.02	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-8	0	0	0	548	--	--	16.08	16.08	0.00	0.01	0.00	0.00	0.00	0.00	20.9
2	27	-0	-91	0	0	0	505	--	--	16.08	16.08	0.10	0.01	0.00	0.01	0.00	0.00	20.9
3	27	-0	-55	0	0	0	503	--	--	16.08	16.08	0.10	0.01	0.00	0.00	0.00	0.00	20.9
4	27	-0	42	0	0	0	395	--	--	16.08	16.08	0.10	0.01	0.00	0.00	0.00	0.00	20.9
5	27	-0	78	0	0	0	443	--	--	16.08	16.08	0.10	0.01	0.00	0.00	0.00	0.00	20.9
6	27	-0	-88	0	0	0	449	--	--	16.08	16.08	0.10	0.01	0.00	0.01	0.00	0.00	20.9
7	27	-0	35	0	0	0	490	--	--	16.08	16.08	0.10	0.01	0.00	0.00	0.00	0.00	20.9
8	27	-0	-48	0	0	0	400	--	--	16.08	16.08	0.10	0.01	0.00	0.00	0.00	0.00	20.9
9	27	-0	75	0	0	0	494	--	--	16.08	16.08	0.10	0.01	0.00	0.00	0.00	0.00	20.9
10	27	-0	-91	0	0	0	505	--	--	16.08	16.08	0.10	0.01	0.00	0.01	0.00	0.00	20.9
11	27	-0	-55	0	0	0	503	--	--	16.08	16.08	0.10	0.01	0.00	0.00	0.00	0.00	20.9
12	27	-0	42	0	0	0	395	--	--	16.08	16.08	0.10	0.01	0.00	0.00	0.00	0.00	20.9
13	27	-0	78	0	0	0	443	--	--	16.08	16.08	0.10	0.01	0.00	0.00	0.00	0.00	20.9
14	27	-0	-88	0	0	0	449	--	--	16.08	16.08	0.10	0.01	0.00	0.01	0.00	0.00	20.9
15	27	-0	35	0	0	0	490	--	--	16.08	16.08	0.10	0.01	0.00	0.00	0.00	0.00	20.9
16	27	-0	-48	0	0	0	400	--	--	16.08	16.08	0.10	0.01	0.00	0.00	0.00	0.00	20.9
17	27	-0	75	0	0	0	494	--	--	16.08	16.08	0.10	0.01	0.00	0.00	0.00	0.00	20.9
18	27	-0	-408	0	0	0	969	--	--	16.08	16.08	0.00	0.02	0.00	0.03	0.00	0.00	20.9
19	27	-0	204	0	0	0	637	--	--	16.08	16.08	0.00	0.01	0.00	0.01	0.00	0.00	20.9
20	27	-0	-208	0	0	0	698	--	--	16.08	16.08	0.00	0.01	0.00	0.01	0.00	0.00	20.9
37	27	-0	-606	0	0	0	1137	--	--	16.08	16.08	0.00	0.02	0.00	0.04	0.00	0.00	20.9
38	27	-0	414	0	0	0	683	--	--	16.08	16.08	0.00	0.01	0.00	0.03	0.00	0.00	20.9
39	27	-0	-274	0	0	0	686	--	--	16.08	16.08	0.00	0.01	0.00	0.02	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	54	-0	-8	0	0	0	543	--	--	16.08	16.08	0.00	0.01	0.00	0.00	0.00	0.00	20.9
2	54	-0	-91	0	0	0	456	--	--	16.08	16.08	0.10	0.01	0.00	0.01	0.00	0.00	20.9
3	54	-0	-55	0	0	0	474	--	--	16.08	16.08	0.10	0.01	0.00	0.00	0.00	0.00	20.9
4	54	-0	42	0	0	0	362	--	--	16.08	16.08	0.10	0.01	0.00	0.00	0.00	0.00	20.9
5	54	-0	78	0	0	0	380	--	--	16.08	16.08	0.10	0.01	0.00	0.00	0.00	0.00	20.9
6	54	-0	-88	0	0	0	402	--	--	16.08	16.08	0.10	0.01	0.00	0.01	0.00	0.00	20.9
7	54	-0	35	0	0	0	462	--	--	16.08	16.08	0.10	0.01	0.00	0.00	0.00	0.00	20.9
8	54	-0	-48	0	0	0	374	--	--	16.08	16.08	0.10	0.01	0.00	0.00	0.00	0.00	20.9
9	54	-0	75	0	0	0	434	--	--	16.08	16.08	0.10	0.01	0.00	0.00	0.00	0.00	20.9
10	54	-0	-91	0	0	0	456	--	--	16.08	16.08	0.10	0.01	0.00	0.01	0.00	0.00	20.9
11	54	-0	-55	0	0	0	474	--	--	16.08	16.08	0.10	0.01	0.00	0.00	0.00	0.00	20.9
12	54	-0	42	0	0	0	362	--	--	16.08	16.08	0.10	0.01	0.00	0.00	0.00	0.00	20.9
13	54	-0	78	0	0	0	380	--	--	16.08	16.08	0.10	0.01	0.00	0.00	0.00	0.00	20.9
14	54	-0	-88	0	0	0	402	--	--	16.08	16.08	0.10	0.01	0.00	0.01	0.00	0.00	20.9
15	54	-0	35	0	0	0	462	--	--	16.08	16.08	0.10	0.01	0.00	0.00	0.00	0.00	20.9
16	54	-0	-48	0	0	0	374	--	--	16.08	16.08	0.10	0.01	0.00	0.00	0.00	0.00	20.9
17	54	-0	75	0	0	0	434	--	--	16.08	16.08	0.10	0.01	0.00	0.00	0.00	0.00	20.9
18	54	-0	-408	0	0	0	750	--	--	16.08	16.08	0.00	0.01	0.00	0.03	0.00	0.00	20.9
19	54	-0	204	0	0	0	473	--	--	16.08	16.08	0.00	0.01	0.00	0.01	0.00	0.00	20.9
20	54	-0	-208	0	0	0	586	--	--	16.08	16.08	0.00	0.01	0.00	0.01	0.00	0.00	20.9
37	54	-0	-606	0	0	0	813	--	--	16.08	16.08	0.00	0.01	0.00	0.04	0.00	0.00	20.9
38	54	-0	414	0	0	0	351	--	--	16.08	16.08	0.00	0.01	0.00	0.03	0.00	0.00	20.9
39	54	-0	-274	0	0	0	540	--	--	16.08	16.08	0.00	0.01	0.00	0.02	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 77 NI 1285 NF 1319 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-1505	0	0	0	1384	--	--	16.08	16.08	0.00	0.02	0.01	0.09	0.00	0.00	20.9
2	0	-0	-1281	0	0	0	1193	--	--	16.08	16.08	0.10	0.02	0.01	0.08	0.00	0.00	20.9
3	0	-0	-1239	0	0	0	1181	--	--	16.08	16.08	0.10	0.02	0.01	0.08	0.00	0.00	20.9
4	0	-0	-1077	0	0	0	947	--	--	16.08	16.08	0.10	0.02	0.01	0.07	0.00	0.00	20.9
5	0	-0	-1034	0	0	0	936	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9
6	0	-0	-1259	0	0	0	1121	--	--	16.08	16.08	0.10	0.02	0.01	0.08	0.00	0.00	20.9
7	0	-0	-1118	0	0	0	1082	--	--	16.08	16.08	0.10	0.02	0.01	0.07	0.00	0.00	20.9
8	0	-0	-1198	0	0	0	1047	--	--	16.08	16.08	0.10	0.02	0.01	0.08	0.00	0.00	20.9
9	0	-0	-1057	0	0	0	1008	--	--	16.08	16.08	0.10	0.02	0.01	0.07	0.00	0.00	20.9
10	0	-0	-1281	0	0	0	1193	--	--	16.08	16.08	0.10	0.02	0.01	0.08	0.00	0.00	20.9
11	0	-0	-1239	0	0	0	1181	--	--	16.08	16.08	0.10	0.02	0.01	0.08	0.00	0.00	20.9
12	0	-0	-1077	0	0	0	947	--	--	16.08	16.08	0.10	0.02	0.01	0.07	0.00	0.00	20.9
13	0	-0	-1034	0	0	0	936	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9
14	0	-0	-1259	0	0	0	1121	--	--	16.08	16.08	0.10	0.02	0.01	0.08	0.00	0.00	20.9
15	0	-0	-1118	0	0	0	1082	--	--	16.08	16.08	0.10	0.02	0.01	0.07	0.00	0.00	20.9
16	0	-0	-1198	0	0	0	1047	--	--	16.08	16.08	0.10	0.02	0.01	0.08	0.00	0.00	20.9
17	0	-0	-1057	0	0	0	1008	--	--	16.08	16.08	0.10	0.02	0.01	0.07	0.00	0.00	20.9
18	0	-0	-2221	0	0	0	2094	--	--	16.08	16.08	0.00	0.04	0.02	0.14	0.00	0.00	20.9
19	0	-0	-1300	0	0	0	1147	--	--	16.08	16.08	0.00	0.02	0.01	0.08	0.00	0.00	20.9
20	0	-0	-1797	0	0	0	1618	--	--	16.08	16.08	0.00	0.03	0.01	0.11	0.00	0.00	20.9
37	0	-0	-2465	0	0	0	2342	--	--	16.08	16.08	0.00	0.04	0.02	0.15	0.00	0.00	20.9
38	0	-0	-930	0	0	0	763	--	--	16.08	16.08	0.00	0.01	0.01	0.06	0.00	0.00	20.9
39	0	-0	-1759	0	0	0	1549	--	--	16.08	16.08	0.00	0.03	0.01	0.11	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	27	-0	-1505	0	0	0	1384	--	--	16.08	16.08	0.00	0.02	0.01	0.09	0.00	0.00	20.9
2	27	-0	-1281	0	0	0	1193	--	--	16.08	16.08	0.10	0.02	0.01	0.08	0.00	0.00	20.9
3	27	-0	-1239	0	0	0	1181	--	--	16.08	16.08	0.10	0.02	0.01	0.08	0.00	0.00	20.9
4	27	-0	-1077	0	0	0	947	--	--	16.08	16.08	0.10	0.02	0.01	0.07	0.00	0.00	20.9
5	27	-0	-1034	0	0	0	936	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9
6	27	-0	-1259	0	0	0	1121	--	--	16.08	16.08	0.10	0.02	0.01	0.08	0.00	0.00	20.9
7	27	-0	-1118	0	0	0	1082	--	--	16.08	16.08	0.10	0.02	0.01	0.07	0.00	0.00	20.9
8	27	-0	-1198	0	0	0	1047	--	--	16.08	16.08	0.10	0.02	0.01	0.08	0.00	0.00	20.9
9	27	-0	-1057	0	0	0	1008	--	--	16.08	16.08	0.10	0.02	0.01	0.07	0.00	0.00	20.9
10	27	-0	-1281	0	0	0	1193	--	--	16.08	16.08	0.10	0.02	0.01	0.08	0.00	0.00	20.9
11	27	-0	-1239	0	0	0	1181	--	--	16.08	16.08	0.10	0.02	0.01	0.08	0.00	0.00	20.9
12	27	-0	-1077	0	0	0	947	--	--	16.08	16.08	0.10	0.02	0.01	0.07	0.00	0.00	20.9
13	27	-0	-1034	0	0	0	936	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9
14	27	-0	-1259	0	0	0	1121	--	--	16.08	16.08	0.10	0.02	0.01	0.08	0.00	0.00	20.9
15	27	-0	-1118	0	0	0	1082	--	--	16.08	16.08	0.10	0.02	0.01	0.07	0.00	0.00	20.9
16	27	-0	-1198	0	0	0	1047	--	--	16.08	16.08	0.10	0.02	0.01	0.08	0.00	0.00	20.9
17	27	-0	-1057	0	0	0	1008	--	--	16.08	16.08	0.10	0.02	0.01	0.07	0.00	0.00	20.9
18	27	-0	-2221	0	0	0	2094	--	--	16.08	16.08	0.00	0.04	0.02	0.14	0.00	0.00	20.9
19	27	-0	-1300	0	0	0	1147	--	--	16.08	16.08	0.00	0.02	0.01	0.08	0.00	0.00	20.9
20	27	-0	-1797	0	0	0	1618	--	--	16.08	16.08	0.00	0.03	0.01	0.11	0.00	0.00	20.9
37	27	-0	-2465	0	0	0	2342	--	--	16.08	16.08	0.00	0.04	0.02	0.15	0.00	0.00	20.9
38	27	-0	-930	0	0	0	763	--	--	16.08	16.08	0.00	0.01	0.01	0.06	0.00	0.00	20.9
39	27	-0	-1759	0	0	0	1549	--	--	16.08	16.08	0.00	0.03	0.01	0.11	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	54	-0	-1505	0	0	0	577	--	--	16.08	16.08	0.00	0.01	0.01	0.09	0.00	0.00	20.9
2	54	-0	-1281	0	0	0	507	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
3	54	-0	-1239	0	0	0	518	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
4	54	-0	-1077	0	0	0	371	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
5	54	-0	-1034	0	0	0	381	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
6	54	-0	-1259	0	0	0	447	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
7	54	-0	-1118	0	0	0	483	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
8	54	-0	-1198	0	0	0	406	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
9	54	-0	-1057	0	0	0	442	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
10	54	-0	-1281	0	0	0	507	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
11	54	-0	-1239	0	0	0	518	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
12	54	-0	-1077	0	0	0	371	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
13	54	-0	-1034	0	0	0	381	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
14	54	-0	-1259	0	0	0	447	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
15	54	-0	-1118	0	0	0	483	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
16	54	-0	-1198	0	0	0	406	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
17	54	-0	-1057	0	0	0	442	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
18	54	-0	-2221	0	0	0	904	--	--	16.08	16.08	0.00	0.02	0.02	0.14	0.00	0.00	20.9
19	54	-0	-1300	0	0	0	451	--	--	16.08	16.08	0.00	0.01	0.01	0.08	0.00	0.00	20.9
20	54	-0	-1797	0	0	0	655	--	--	16.08	16.08	0.00	0.01	0.01	0.11	0.00	0.00	20.9
37	54	-0	-2465	0	0	0	1021	--	--	16.08	16.08	0.00	0.02	0.02	0.15	0.00	0.00	20.9
38	54	-0	-930	0	0	0	265	--	--	16.08	16.08	0.00	0.00	0.01	0.06	0.00	0.00	20.9
39	54	-0	-1759	0	0	0	606	--	--	16.08	16.08	0.00	0.01	0.01	0.11	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 78 NI 1286 NF 1285 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-3011	0	0	0	2660	--	--	16.08	16.08	0.00	0.05	0.02	0.19	0.00	0.00	20.9
2	0	-0	-2494	0	0	0	2249	--	--	16.08	16.08	0.10	0.04	0.02	0.16	0.00	0.00	20.9
3	0	-0	-2443	0	0	0	2221	--	--	16.08	16.08	0.10	0.04	0.02	0.15	0.00	0.00	20.9
4	0	-0	-2189	0	0	0	1871	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
5	0	-0	-2139	0	0	0	1844	--	--	16.08	16.08	0.10	0.03	0.02	0.13	0.00	0.00	20.9
6	0	-0	-2446	0	0	0	2149	--	--	16.08	16.08	0.10	0.04	0.02	0.15	0.00	0.00	20.9
7	0	-0	-2277	0	0	0	2057	--	--	16.08	16.08	0.10	0.04	0.02	0.14	0.00	0.00	20.9
8	0	-0	-2355	0	0	0	2035	--	--	16.08	16.08	0.10	0.04	0.02	0.15	0.00	0.00	20.9
9	0	-0	-2186	0	0	0	1944	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
10	0	-0	-2494	0	0	0	2249	--	--	16.08	16.08	0.10	0.04	0.02	0.16	0.00	0.00	20.9
11	0	-0	-2443	0	0	0	2221	--	--	16.08	16.08	0.10	0.04	0.02	0.15	0.00	0.00	20.9
12	0	-0	-2189	0	0	0	1871	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
13	0	-0	-2139	0	0	0	1844	--	--	16.08	16.08	0.10	0.03	0.02	0.13	0.00	0.00	20.9
14	0	-0	-2446	0	0	0	2149	--	--	16.08	16.08	0.10	0.04	0.02	0.15	0.00	0.00	20.9
15	0	-0	-2277	0	0	0	2057	--	--	16.08	16.08	0.10	0.04	0.02	0.14	0.00	0.00	20.9
16	0	-0	-2355	0	0	0	2035	--	--	16.08	16.08	0.10	0.04	0.02	0.15	0.00	0.00	20.9

17	0	-0	-2186	0	0	0	1944	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
18	0	-0	-4194	0	0	0	3884	--	--	16.08	16.08	0.00	0.07	0.03	0.26	0.00	0.00	20.9
19	0	-0	-2830	0	0	0	2374	--	--	16.08	16.08	0.00	0.04	0.02	0.18	0.00	0.00	20.9
20	0	-0	-3360	0	0	0	2987	--	--	16.08	16.08	0.00	0.05	0.03	0.21	0.00	0.00	20.9
37	0	-0	-4505	0	0	0	4249	--	--	16.08	16.08	0.00	0.07	0.04	0.28	0.00	0.00	20.9
38	0	-0	-2231	0	0	0	1731	--	--	16.08	16.08	0.00	0.03	0.02	0.14	0.00	0.00	20.9
39	0	-0	-3115	0	0	0	2753	--	--	16.08	16.08	0.00	0.05	0.03	0.20	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-3011	0	0	0	2660	--	--	16.08	16.08	0.00	0.05	0.02	0.19	0.00	0.00	20.9
2	27	-0	-2494	0	0	0	2249	--	--	16.08	16.08	0.10	0.04	0.02	0.16	0.00	0.00	20.9
3	27	-0	-2443	0	0	0	2221	--	--	16.08	16.08	0.10	0.04	0.02	0.15	0.00	0.00	20.9
4	27	-0	-2189	0	0	0	1871	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
5	27	-0	-2139	0	0	0	1844	--	--	16.08	16.08	0.10	0.03	0.02	0.13	0.00	0.00	20.9
6	27	-0	-2446	0	0	0	2149	--	--	16.08	16.08	0.10	0.04	0.02	0.15	0.00	0.00	20.9
7	27	-0	-2277	0	0	0	2057	--	--	16.08	16.08	0.10	0.04	0.02	0.14	0.00	0.00	20.9
8	27	-0	-2355	0	0	0	2035	--	--	16.08	16.08	0.10	0.04	0.02	0.15	0.00	0.00	20.9
9	27	-0	-2186	0	0	0	1944	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
10	27	-0	-2494	0	0	0	2249	--	--	16.08	16.08	0.10	0.04	0.02	0.16	0.00	0.00	20.9
11	27	-0	-2443	0	0	0	2221	--	--	16.08	16.08	0.10	0.04	0.02	0.15	0.00	0.00	20.9
12	27	-0	-2189	0	0	0	1871	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
13	27	-0	-2139	0	0	0	1844	--	--	16.08	16.08	0.10	0.03	0.02	0.13	0.00	0.00	20.9
14	27	-0	-2446	0	0	0	2149	--	--	16.08	16.08	0.10	0.04	0.02	0.15	0.00	0.00	20.9
15	27	-0	-2277	0	0	0	2057	--	--	16.08	16.08	0.10	0.04	0.02	0.14	0.00	0.00	20.9
16	27	-0	-2355	0	0	0	2035	--	--	16.08	16.08	0.10	0.04	0.02	0.15	0.00	0.00	20.9
17	27	-0	-2186	0	0	0	1944	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
18	27	-0	-4194	0	0	0	3884	--	--	16.08	16.08	0.00	0.07	0.03	0.26	0.00	0.00	20.9
19	27	-0	-2830	0	0	0	2374	--	--	16.08	16.08	0.00	0.04	0.02	0.18	0.00	0.00	20.9
20	27	-0	-3360	0	0	0	2987	--	--	16.08	16.08	0.00	0.05	0.03	0.21	0.00	0.00	20.9
37	27	-0	-4505	0	0	0	4249	--	--	16.08	16.08	0.00	0.07	0.04	0.28	0.00	0.00	20.9
38	27	-0	-2231	0	0	0	1731	--	--	16.08	16.08	0.00	0.03	0.02	0.14	0.00	0.00	20.9
39	27	-0	-3115	0	0	0	2753	--	--	16.08	16.08	0.00	0.05	0.03	0.20	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	54	-0	-3011	0	0	0	1047	--	--	16.08	16.08	0.00	0.02	0.02	0.19	0.00	0.00	20.9
2	54	-0	-2494	0	0	0	913	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
3	54	-0	-2443	0	0	0	912	--	--	16.08	16.08	0.10	0.02	0.02	0.15	0.00	0.00	20.9
4	54	-0	-2189	0	0	0	698	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
5	54	-0	-2139	0	0	0	698	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
6	54	-0	-2446	0	0	0	838	--	--	16.08	16.08	0.10	0.01	0.02	0.15	0.00	0.00	20.9
7	54	-0	-2277	0	0	0	837	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
8	54	-0	-2355	0	0	0	774	--	--	16.08	16.08	0.10	0.01	0.02	0.15	0.00	0.00	20.9
9	54	-0	-2186	0	0	0	773	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
10	54	-0	-2494	0	0	0	913	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
11	54	-0	-2443	0	0	0	912	--	--	16.08	16.08	0.10	0.02	0.02	0.15	0.00	0.00	20.9
12	54	-0	-2189	0	0	0	698	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
13	54	-0	-2139	0	0	0	698	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
14	54	-0	-2446	0	0	0	838	--	--	16.08	16.08	0.10	0.01	0.02	0.15	0.00	0.00	20.9
15	54	-0	-2277	0	0	0	837	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
16	54	-0	-2355	0	0	0	774	--	--	16.08	16.08	0.10	0.01	0.02	0.15	0.00	0.00	20.9
17	54	-0	-2186	0	0	0	773	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
18	54	-0	-4194	0	0	0	1638	--	--	16.08	16.08	0.00	0.03	0.03	0.26	0.00	0.00	20.9
19	54	-0	-2830	0	0	0	858	--	--	16.08	16.08	0.00	0.01	0.02	0.18	0.00	0.00	20.9
20	54	-0	-3360	0	0	0	1187	--	--	16.08	16.08	0.00	0.02	0.03	0.21	0.00	0.00	20.9
37	54	-0	-4505	0	0	0	1836	--	--	16.08	16.08	0.00	0.03	0.04	0.28	0.00	0.00	20.9
38	54	-0	-2231	0	0	0	536	--	--	16.08	16.08	0.00	0.01	0.02	0.14	0.00	0.00	20.9
39	54	-0	-3115	0	0	0	1085	--	--	16.08	16.08	0.00	0.02	0.03	0.20	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 79 NI 1845 NF 1286 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-2080	0	0	0	3472	--	--	16.08	16.08	0.00	0.06	0.02	0.13	0.00	0.00	20.9
2	0	-0	-1742	0	0	0	2948	--	--	16.08	16.08	0.10	0.05	0.01	0.11	0.00	0.00	20.9
3	0	-0	-1675	0	0	0	2891	--	--	16.08	16.08	0.10	0.05	0.01	0.11	0.00	0.00	20.9
4	0	-0	-1524	0	0	0	2451	--	--	16.08	16.08	0.10	0.04	0.01	0.10	0.00	0.00	20.9
5	0	-0	-1458	0	0	0	2394	--	--	16.08	16.08	0.10	0.04	0.01	0.09	0.00	0.00	20.9
6	0	-0	-1743	0	0	0	2841	--	--	16.08	16.08	0.10	0.05	0.01	0.11	0.00	0.00	20.9
7	0	-0	-1522	0	0	0	2650	--	--	16.08	16.08	0.10	0.05	0.01	0.10	0.00	0.00	20.9
8	0	-0	-1678	0	0	0	2692	--	--	16.08	16.08	0.10	0.05	0.01	0.11	0.00	0.00	20.9
9	0	-0	-1456	0	0	0	2501	--	--	16.08	16.08	0.10	0.04	0.01	0.09	0.00	0.00	20.9
10	0	-0	-1742	0	0	0	2948	--	--	16.08	16.08	0.10	0.05	0.01	0.11	0.00	0.00	20.9
11	0	-0	-1675	0	0	0	2891	--	--	16.08	16.08	0.10	0.05	0.01	0.11	0.00	0.00	20.9
12	0	-0	-1524	0	0	0	2451	--	--	16.08	16.08	0.10	0.04	0.01	0.10	0.00	0.00	20.9
13	0	-0	-1458	0	0	0	2394	--	--	16.08	16.08	0.10	0.04	0.01	0.09	0.00	0.00	20.9
14	0	-0	-1743	0	0	0	2841	--	--	16.08	16.08	0.10	0.05	0.01	0.11	0.00	0.00	20.9
15	0	-0	-1522	0	0	0	2650	--	--	16.08	16.08	0.10	0.05	0.01	0.10	0.00	0.00	20.9
16	0	-0	-1678	0	0	0	2692	--	--	16.08	16.08	0.10	0.05	0.01	0.11	0.00	0.00	20.9
17	0	-0	-1456	0	0	0	2501	--	--	16.08	16.08	0.10	0.04	0.01	0.09	0.00	0.00	20.9
18	0	-0	-3278	0	0	0	5287	--	--	16.08	16.08	0.00	0.09	0.03	0.21	0.00	0.00	20.9
19	0	-0	-2088	0	0	0	3175	--	--	16.08	16.08	0.00	0.05	0.02	0.13	0.00	0.00	20.9
20	0	-0	-2403	0	0	0	3937	--	--	16.08	16.08	0.00	0.07	0.02	0.15	0.00	0.00	20.9
37	0	-0	-3499	0	0	0	5766	--	--	16.08	16.08	0.00	0.10	0.03	0.22	0.00	0.00	20.9
38	0	-0	-1516	0	0	0	2245	--	--	16.08	16.08	0.00	0.04	0.01	0.10	0.00	0.00	20.9
39	0	-0	-2040	0	0	0	3516	--	--	16.08	16.08	0.00	0.06	0.02	0.13	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-2080	0	0	0	3472	--	--	16.08	16.08	0.00	0.06	0.02	0.13	0.00	0.00	20.9
2	27	-0	-1742	0	0	0	2948	--	--	16.08	16.08	0.10	0.05	0.01	0.11	0.00	0.00	20.9
3	27	-0	-1675	0	0	0	2891	--	--	16.08	16.08	0.10	0.05	0.01	0.11	0.00	0.00	20.9
4	27	-0	-1524	0	0	0	2451	--	--	16.08	16.08	0.10	0.04	0.01	0.10	0.00	0.00	20.9
5	27	-0	-1458	0	0	0	2394	--	--	16.08	16.08	0.10	0.04	0.01	0.09	0.00	0.00	20.9
6	27	-0	-1743	0	0	0	2841	--	--	16.08	16.08	0.10	0.05	0.01	0.11	0.00	0.00	20.9
7	27	-0	-1522	0	0	0	2650	--	--	16.08	16.08	0.10	0.05	0.01	0.10	0.00	0.00	20.9
8	27	-0	-1678	0	0	0	2692	--	--	16.08	16.08	0.10	0.05	0.01	0.11	0.00	0.00	20.9
9	27	-0	-1456	0	0	0	2501	--	--	16.08	16.08	0.10	0.04	0.01	0.09	0.00	0.00	20.9
10	27	-0	-1742	0	0	0	2948	--	--	16.08	16.08	0.10	0.05	0.01	0.11	0.00	0.00	20.9
11	27	-0	-1675	0	0	0	2891	--	--	16.08	16.08	0.10	0.05	0.01	0.11	0.00	0.00	20.9
12	27	-0	-1524	0	0	0	2451	--	--	16.08	16.08	0.10	0.04	0.01	0.10	0.00	0.00	20.9

13	27	-0	-1458	0	0	0	2394	--	--	16.08	16.08	0.10	0.04	0.01	0.09	0.00	0.00	20.9
14	27	-0	-1743	0	0	0	2841	--	--	16.08	16.08	0.10	0.05	0.01	0.11	0.00	0.00	20.9
15	27	-0	-1522	0	0	0	2650	--	--	16.08	16.08	0.10	0.05	0.01	0.10	0.00	0.00	20.9
16	27	-0	-1678	0	0	0	2692	--	--	16.08	16.08	0.10	0.05	0.01	0.11	0.00	0.00	20.9
17	27	-0	-1456	0	0	0	2501	--	--	16.08	16.08	0.10	0.04	0.01	0.09	0.00	0.00	20.9
18	27	-0	-3278	0	0	0	5287	--	--	16.08	16.08	0.00	0.09	0.03	0.21	0.00	0.00	20.9
19	27	-0	-2088	0	0	0	3175	--	--	16.08	16.08	0.00	0.05	0.02	0.13	0.00	0.00	20.9
20	27	-0	-2403	0	0	0	3937	--	--	16.08	16.08	0.00	0.07	0.02	0.15	0.00	0.00	20.9
37	27	-0	-3499	0	0	0	5766	--	--	16.08	16.08	0.00	0.10	0.03	0.22	0.00	0.00	20.9
38	27	-0	-1516	0	0	0	2245	--	--	16.08	16.08	0.00	0.04	0.01	0.10	0.00	0.00	20.9
39	27	-0	-2040	0	0	0	3516	--	--	16.08	16.08	0.00	0.06	0.02	0.13	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	54	-0	-2080	0	0	0	2358	--	--	16.08	16.08	0.00	0.04	0.02	0.13	0.00	0.00	20.9
2	54	-0	-1742	0	0	0	2015	--	--	16.08	16.08	0.10	0.04	0.01	0.11	0.00	0.00	20.9
3	54	-0	-1675	0	0	0	1993	--	--	16.08	16.08	0.10	0.04	0.01	0.11	0.00	0.00	20.9
4	54	-0	-1524	0	0	0	1635	--	--	16.08	16.08	0.10	0.03	0.01	0.10	0.00	0.00	20.9
5	54	-0	-1458	0	0	0	1613	--	--	16.08	16.08	0.10	0.03	0.01	0.09	0.00	0.00	20.9
6	54	-0	-1743	0	0	0	1907	--	--	16.08	16.08	0.10	0.03	0.01	0.11	0.00	0.00	20.9
7	54	-0	-1522	0	0	0	1835	--	--	16.08	16.08	0.10	0.03	0.01	0.10	0.00	0.00	20.9
8	54	-0	-1678	0	0	0	1793	--	--	16.08	16.08	0.10	0.03	0.01	0.11	0.00	0.00	20.9
9	54	-0	-1456	0	0	0	1721	--	--	16.08	16.08	0.10	0.03	0.01	0.09	0.00	0.00	20.9
10	54	-0	-1742	0	0	0	2015	--	--	16.08	16.08	0.10	0.04	0.01	0.11	0.00	0.00	20.9
11	54	-0	-1675	0	0	0	1993	--	--	16.08	16.08	0.10	0.04	0.01	0.11	0.00	0.00	20.9
12	54	-0	-1524	0	0	0	1635	--	--	16.08	16.08	0.10	0.03	0.01	0.10	0.00	0.00	20.9
13	54	-0	-1458	0	0	0	1613	--	--	16.08	16.08	0.10	0.03	0.01	0.09	0.00	0.00	20.9
14	54	-0	-1743	0	0	0	1907	--	--	16.08	16.08	0.10	0.03	0.01	0.11	0.00	0.00	20.9
15	54	-0	-1522	0	0	0	1835	--	--	16.08	16.08	0.10	0.03	0.01	0.10	0.00	0.00	20.9
16	54	-0	-1678	0	0	0	1793	--	--	16.08	16.08	0.10	0.03	0.01	0.11	0.00	0.00	20.9
17	54	-0	-1456	0	0	0	1721	--	--	16.08	16.08	0.10	0.03	0.01	0.09	0.00	0.00	20.9
18	54	-0	-3278	0	0	0	3531	--	--	16.08	16.08	0.00	0.06	0.03	0.21	0.00	0.00	20.9
19	54	-0	-2088	0	0	0	2056	--	--	16.08	16.08	0.00	0.04	0.02	0.13	0.00	0.00	20.9
20	54	-0	-2403	0	0	0	2650	--	--	16.08	16.08	0.00	0.05	0.02	0.15	0.00	0.00	20.9
37	54	-0	-3499	0	0	0	3892	--	--	16.08	16.08	0.00	0.07	0.03	0.22	0.00	0.00	20.9
38	54	-0	-1516	0	0	0	1433	--	--	16.08	16.08	0.00	0.02	0.01	0.10	0.00	0.00	20.9
39	54	-0	-2040	0	0	0	2423	--	--	16.08	16.08	0.00	0.04	0.02	0.13	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 80 NI 1317 NF 1845 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	6591	0	0	0	3451	--	--	16.08	16.08	0.00	0.06	0.05	0.41	0.00	0.00	20.9
2	0	-0	5264	0	0	0	3188	--	--	16.08	16.08	0.10	0.06	0.04	0.33	0.00	0.00	20.9
3	0	-0	5269	0	0	0	3079	--	--	16.08	16.08	0.10	0.05	0.04	0.33	0.00	0.00	20.9
4	0	-0	4871	0	0	0	2230	--	--	16.08	16.08	0.10	0.04	0.04	0.31	0.00	0.00	20.9
5	0	-0	4876	0	0	0	2122	--	--	16.08	16.08	0.10	0.04	0.04	0.31	0.00	0.00	20.9
6	0	-0	5120	0	0	0	2979	--	--	16.08	16.08	0.10	0.05	0.04	0.32	0.00	0.00	20.9
7	0	-0	5138	0	0	0	2618	--	--	16.08	16.08	0.10	0.05	0.04	0.32	0.00	0.00	20.9
8	0	-0	5002	0	0	0	2692	--	--	16.08	16.08	0.10	0.05	0.04	0.31	0.00	0.00	20.9
9	0	-0	5020	0	0	0	2330	--	--	16.08	16.08	0.10	0.04	0.04	0.31	0.00	0.00	20.9
10	0	-0	5264	0	0	0	3188	--	--	16.08	16.08	0.10	0.06	0.04	0.33	0.00	0.00	20.9
11	0	-0	5269	0	0	0	3079	--	--	16.08	16.08	0.10	0.05	0.04	0.33	0.00	0.00	20.9
12	0	-0	4871	0	0	0	2230	--	--	16.08	16.08	0.10	0.04	0.04	0.31	0.00	0.00	20.9
13	0	-0	4876	0	0	0	2122	--	--	16.08	16.08	0.10	0.04	0.04	0.31	0.00	0.00	20.9
14	0	-0	5120	0	0	0	2979	--	--	16.08	16.08	0.10	0.05	0.04	0.32	0.00	0.00	20.9
15	0	-0	5138	0	0	0	2618	--	--	16.08	16.08	0.10	0.05	0.04	0.32	0.00	0.00	20.9
16	0	-0	5002	0	0	0	2692	--	--	16.08	16.08	0.10	0.05	0.04	0.31	0.00	0.00	20.9
17	0	-0	5020	0	0	0	2330	--	--	16.08	16.08	0.10	0.04	0.04	0.31	0.00	0.00	20.9
18	0	-0	8125	0	0	0	6561	--	--	16.08	16.08	0.00	0.11	0.07	0.51	0.00	0.00	20.9
19	0	-0	6403	0	0	0	2708	--	--	16.08	16.08	0.00	0.05	0.05	0.40	0.00	0.00	20.9
20	0	-0	7001	0	0	0	4301	--	--	16.08	16.08	0.00	0.07	0.06	0.44	0.00	0.00	20.9
37	0	-0	8483	0	0	0	7500	--	--	16.08	16.08	0.00	0.13	0.07	0.53	0.00	0.00	20.9
38	0	-0	5613	0	0	0	1078	--	--	16.08	16.08	0.00	0.02	0.05	0.35	0.00	0.00	20.9
39	0	-0	6609	0	0	0	3734	--	--	16.08	16.08	0.00	0.06	0.05	0.41	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	6591	0	0	0	12198	--	--	16.08	16.08	0.00	0.21	0.05	0.41	0.00	0.00	20.9
2	26	-0	5264	0	0	0	10174	--	--	16.08	16.08	0.10	0.18	0.04	0.33	0.00	0.00	20.9
3	26	-0	5269	0	0	0	10072	--	--	16.08	16.08	0.10	0.18	0.04	0.33	0.00	0.00	20.9
4	26	-0	4871	0	0	0	8694	--	--	16.08	16.08	0.10	0.15	0.04	0.31	0.00	0.00	20.9
5	26	-0	4876	0	0	0	8593	--	--	16.08	16.08	0.10	0.15	0.04	0.31	0.00	0.00	20.9
6	26	-0	5120	0	0	0	9774	--	--	16.08	16.08	0.10	0.17	0.04	0.32	0.00	0.00	20.9
7	26	-0	5138	0	0	0	9437	--	--	16.08	16.08	0.10	0.17	0.04	0.32	0.00	0.00	20.9
8	26	-0	5002	0	0	0	9330	--	--	16.08	16.08	0.10	0.17	0.04	0.31	0.00	0.00	20.9
9	26	-0	5020	0	0	0	8992	--	--	16.08	16.08	0.10	0.16	0.04	0.31	0.00	0.00	20.9
10	26	-0	5264	0	0	0	10174	--	--	16.08	16.08	0.10	0.18	0.04	0.33	0.00	0.00	20.9
11	26	-0	5269	0	0	0	10072	--	--	16.08	16.08	0.10	0.18	0.04	0.33	0.00	0.00	20.9
12	26	-0	4871	0	0	0	8694	--	--	16.08	16.08	0.10	0.15	0.04	0.31	0.00	0.00	20.9
13	26	-0	4876	0	0	0	8593	--	--	16.08	16.08	0.10	0.15	0.04	0.31	0.00	0.00	20.9
14	26	-0	5120	0	0	0	9774	--	--	16.08	16.08	0.10	0.17	0.04	0.32	0.00	0.00	20.9
15	26	-0	5138	0	0	0	9437	--	--	16.08	16.08	0.10	0.17	0.04	0.32	0.00	0.00	20.9
16	26	-0	5002	0	0	0	9330	--	--	16.08	16.08	0.10	0.17	0.04	0.31	0.00	0.00	20.9
17	26	-0	5020	0	0	0	8992	--	--	16.08	16.08	0.10	0.16	0.04	0.31	0.00	0.00	20.9
18	26	-0	8125	0	0	0	17344	--	--	16.08	16.08	0.00	0.30	0.07	0.51	0.00	0.00	20.9
19	26	-0	6403	0	0	0	11205	--	--	16.08	16.08	0.00	0.19	0.05	0.40	0.00	0.00	20.9
20	26	-0	7001	0	0	0	13592	--	--	16.08	16.08	0.00	0.23	0.06	0.44	0.00	0.00	20.9
37	26	-0	8483	0	0	0	18756	--	--	16.08	16.08	0.00	0.32	0.07	0.53	0.00	0.00	20.9
38	26	-0	5613	0	0	0	8527	--	--	16.08	16.08	0.00	0.15	0.05	0.35	0.00	0.00	20.9
39	26	-0	6609	0	0	0	12505	--	--	16.08	16.08	0.00	0.21	0.05	0.41	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	52	-0	6591	0	0	0	6857	--	--	16.08	16.08	0.00	0.12	0.05	0.41	0.00	0.00	20.9
2	52	-0	5264	0	0	0	5908	--	--	16.08	16.08	0.10	0.10	0.04	0.33	0.00	0.00	20.9
3	52	-0	5269	0	0	0	5802	--	--	16.08	16.08	0.10	0.10	0.04	0.33	0.00	0.00	20.9
4	52	-0	4871	0	0	0	4747	--	--	16.08	16.08	0.10	0.08	0.04	0.31	0.00	0.00	20.9
5	52	-0	4876	0	0	0	4641	--	--	16.08	16.08	0.10	0.08	0.04	0.31	0.00	0.00	20.9
6	52	-0	5120	0	0	0	5625	--	--	16.08	16.08	0.10	0.10	0.04	0.32	0.00	0.00	20.9
7	52	-0	5138	0	0	0	5273	--	--	16.08	16.08	0.10	0.09	0.04	0.32	0.00	0.00	20.9
8	52	-0	5002	0	0	0	5276	--	--	16.08	16.08	0.10	0.09	0.04	0.31	0.00	0.00	20.9

9	52	-0	5020	0	0	0	4924	--	--	16.08	16.08	0.10	0.09	0.04	0.31	0.00	0.00	20.9
10	52	-0	5264	0	0	0	5908	--	--	16.08	16.08	0.10	0.10	0.04	0.33	0.00	0.00	20.9
11	52	-0	5269	0	0	0	5802	--	--	16.08	16.08	0.10	0.10	0.04	0.33	0.00	0.00	20.9
12	52	-0	4871	0	0	0	4747	--	--	16.08	16.08	0.10	0.08	0.04	0.31	0.00	0.00	20.9
13	52	-0	4876	0	0	0	4641	--	--	16.08	16.08	0.10	0.08	0.04	0.31	0.00	0.00	20.9
14	52	-0	5120	0	0	0	5625	--	--	16.08	16.08	0.10	0.10	0.04	0.32	0.00	0.00	20.9
15	52	-0	5138	0	0	0	5273	--	--	16.08	16.08	0.10	0.09	0.04	0.32	0.00	0.00	20.9
16	52	-0	5002	0	0	0	5276	--	--	16.08	16.08	0.10	0.09	0.04	0.31	0.00	0.00	20.9
17	52	-0	5020	0	0	0	4924	--	--	16.08	16.08	0.10	0.09	0.04	0.31	0.00	0.00	20.9
18	52	-0	8125	0	0	0	10760	--	--	16.08	16.08	0.00	0.18	0.07	0.51	0.00	0.00	20.9
19	52	-0	6403	0	0	0	6016	--	--	16.08	16.08	0.00	0.10	0.05	0.40	0.00	0.00	20.9
20	52	-0	7001	0	0	0	7919	--	--	16.08	16.08	0.00	0.14	0.06	0.44	0.00	0.00	20.9
37	52	-0	8483	0	0	0	11880	--	--	16.08	16.08	0.00	0.20	0.07	0.53	0.00	0.00	20.9
38	52	-0	5613	0	0	0	3978	--	--	16.08	16.08	0.00	0.07	0.05	0.35	0.00	0.00	20.9
39	52	-0	6609	0	0	0	7149	--	--	16.08	16.08	0.00	0.12	0.05	0.41	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 81 NI 1284 NF 1317 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	4811	0	0	0	966	--	--	16.08	16.08	0.00	0.02	0.04	0.30	0.00	0.00	20.9
2	0	-0	3895	0	0	0	1176	--	--	16.08	16.08	0.10	0.02	0.03	0.24	0.00	0.00	20.9
3	0	-0	3899	0	0	0	1065	--	--	16.08	16.08	0.10	0.02	0.03	0.24	0.00	0.00	20.9
4	0	-0	3502	0	0	0	421	--	--	16.08	16.08	0.10	0.01	0.03	0.22	0.00	0.00	20.9
5	0	-0	3506	0	0	0	311	--	--	16.08	16.08	0.10	0.01	0.03	0.22	0.00	0.00	20.9
6	0	-0	3753	0	0	0	1040	--	--	16.08	16.08	0.10	0.02	0.03	0.24	0.00	0.00	20.9
7	0	-0	3766	0	0	0	672	--	--	16.08	16.08	0.10	0.01	0.03	0.24	0.00	0.00	20.9
8	0	-0	3635	0	0	0	814	--	--	16.08	16.08	0.10	0.01	0.03	0.23	0.00	0.00	20.9
9	0	-0	3648	0	0	0	446	--	--	16.08	16.08	0.10	0.01	0.03	0.23	0.00	0.00	20.9
10	0	-0	3895	0	0	0	1176	--	--	16.08	16.08	0.10	0.02	0.03	0.24	0.00	0.00	20.9
11	0	-0	3899	0	0	0	1065	--	--	16.08	16.08	0.10	0.02	0.03	0.24	0.00	0.00	20.9
12	0	-0	3502	0	0	0	421	--	--	16.08	16.08	0.10	0.01	0.03	0.22	0.00	0.00	20.9
13	0	-0	3506	0	0	0	311	--	--	16.08	16.08	0.10	0.01	0.03	0.22	0.00	0.00	20.9
14	0	-0	3753	0	0	0	1040	--	--	16.08	16.08	0.10	0.02	0.03	0.24	0.00	0.00	20.9
15	0	-0	3766	0	0	0	672	--	--	16.08	16.08	0.10	0.01	0.03	0.24	0.00	0.00	20.9
16	0	-0	3635	0	0	0	814	--	--	16.08	16.08	0.10	0.01	0.03	0.23	0.00	0.00	20.9
17	0	-0	3648	0	0	0	446	--	--	16.08	16.08	0.10	0.01	0.03	0.23	0.00	0.00	20.9
18	0	-0	6215	0	0	0	3350	--	--	16.08	16.08	0.00	0.06	0.05	0.39	0.00	0.00	20.9
19	0	-0	4563	0	0	0	350	--	--	16.08	16.08	0.00	0.01	0.04	0.29	0.00	0.00	20.9
20	0	-0	5152	0	0	0	1640	--	--	16.08	16.08	0.00	0.03	0.04	0.32	0.00	0.00	20.9
37	0	-0	6585	0	0	0	4098	--	--	16.08	16.08	0.00	0.07	0.05	0.41	0.00	0.00	20.9
38	0	-0	3831	0	0	0	-901	--	--	16.08	16.08	0.18	0.01	0.03	0.24	0.00	0.00	20.9
39	0	-0	4813	0	0	0	1248	--	--	16.08	16.08	0.00	0.02	0.04	0.30	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	4811	0	0	0	7350	--	--	16.08	16.08	0.00	0.13	0.04	0.30	0.00	0.00	20.9
2	26	-0	3895	0	0	0	6345	--	--	16.08	16.08	0.10	0.11	0.03	0.24	0.00	0.00	20.9
3	26	-0	3899	0	0	0	6239	--	--	16.08	16.08	0.10	0.11	0.03	0.24	0.00	0.00	20.9
4	26	-0	3502	0	0	0	5068	--	--	16.08	16.08	0.10	0.09	0.03	0.22	0.00	0.00	20.9
5	26	-0	3506	0	0	0	4963	--	--	16.08	16.08	0.10	0.09	0.03	0.22	0.00	0.00	20.9
6	26	-0	3753	0	0	0	6021	--	--	16.08	16.08	0.10	0.11	0.03	0.24	0.00	0.00	20.9
7	26	-0	3766	0	0	0	5670	--	--	16.08	16.08	0.10	0.10	0.03	0.24	0.00	0.00	20.9
8	26	-0	3635	0	0	0	5638	--	--	16.08	16.08	0.10	0.10	0.03	0.23	0.00	0.00	20.9
9	26	-0	3648	0	0	0	5287	--	--	16.08	16.08	0.10	0.09	0.03	0.23	0.00	0.00	20.9
10	26	-0	3895	0	0	0	6345	--	--	16.08	16.08	0.10	0.11	0.03	0.24	0.00	0.00	20.9
11	26	-0	3899	0	0	0	6239	--	--	16.08	16.08	0.10	0.11	0.03	0.24	0.00	0.00	20.9
12	26	-0	3502	0	0	0	5068	--	--	16.08	16.08	0.10	0.09	0.03	0.22	0.00	0.00	20.9
13	26	-0	3506	0	0	0	4963	--	--	16.08	16.08	0.10	0.09	0.03	0.22	0.00	0.00	20.9
14	26	-0	3753	0	0	0	6021	--	--	16.08	16.08	0.10	0.11	0.03	0.24	0.00	0.00	20.9
15	26	-0	3766	0	0	0	5670	--	--	16.08	16.08	0.10	0.10	0.03	0.24	0.00	0.00	20.9
16	26	-0	3635	0	0	0	5638	--	--	16.08	16.08	0.10	0.10	0.03	0.23	0.00	0.00	20.9
17	26	-0	3648	0	0	0	5287	--	--	16.08	16.08	0.10	0.09	0.03	0.23	0.00	0.00	20.9
18	26	-0	6215	0	0	0	11598	--	--	16.08	16.08	0.00	0.20	0.05	0.39	0.00	0.00	20.9
19	26	-0	4563	0	0	0	6406	--	--	16.08	16.08	0.00	0.11	0.04	0.29	0.00	0.00	20.9
20	26	-0	5152	0	0	0	8477	--	--	16.08	16.08	0.00	0.14	0.04	0.32	0.00	0.00	20.9
37	26	-0	6585	0	0	0	12837	--	--	16.08	16.08	0.00	0.22	0.05	0.41	0.00	0.00	20.9
38	26	-0	3831	0	0	0	4183	--	--	16.08	16.08	0.00	0.07	0.03	0.24	0.00	0.00	20.9
39	26	-0	4813	0	0	0	7635	--	--	16.08	16.08	0.00	0.13	0.04	0.30	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	52	-0	4811	0	0	0	3451	--	--	16.08	16.08	0.00	0.06	0.04	0.30	0.00	0.00	20.9
2	52	-0	3895	0	0	0	3188	--	--	16.08	16.08	0.10	0.06	0.03	0.24	0.00	0.00	20.9
3	52	-0	3899	0	0	0	3079	--	--	16.08	16.08	0.10	0.05	0.03	0.24	0.00	0.00	20.9
4	52	-0	3502	0	0	0	2230	--	--	16.08	16.08	0.10	0.04	0.03	0.22	0.00	0.00	20.9
5	52	-0	3506	0	0	0	2122	--	--	16.08	16.08	0.10	0.04	0.03	0.22	0.00	0.00	20.9
6	52	-0	3753	0	0	0	2979	--	--	16.08	16.08	0.10	0.05	0.03	0.24	0.00	0.00	20.9
7	52	-0	3766	0	0	0	2618	--	--	16.08	16.08	0.10	0.05	0.03	0.24	0.00	0.00	20.9
8	52	-0	3635	0	0	0	2692	--	--	16.08	16.08	0.10	0.05	0.03	0.23	0.00	0.00	20.9
9	52	-0	3648	0	0	0	2330	--	--	16.08	16.08	0.10	0.04	0.03	0.23	0.00	0.00	20.9
10	52	-0	3895	0	0	0	3188	--	--	16.08	16.08	0.10	0.06	0.03	0.24	0.00	0.00	20.9
11	52	-0	3899	0	0	0	3079	--	--	16.08	16.08	0.10	0.05	0.03	0.24	0.00	0.00	20.9
12	52	-0	3502	0	0	0	2230	--	--	16.08	16.08	0.10	0.04	0.03	0.22	0.00	0.00	20.9
13	52	-0	3506	0	0	0	2122	--	--	16.08	16.08	0.10	0.04	0.03	0.22	0.00	0.00	20.9
14	52	-0	3753	0	0	0	2979	--	--	16.08	16.08	0.10	0.05	0.03	0.24	0.00	0.00	20.9
15	52	-0	3766	0	0	0	2618	--	--	16.08	16.08	0.10	0.05	0.03	0.24	0.00	0.00	20.9
16	52	-0	3635	0	0	0	2692	--	--	16.08	16.08	0.10	0.05	0.03	0.23	0.00	0.00	20.9
17	52	-0	3648	0	0	0	2330	--	--	16.08	16.08	0.10	0.04	0.03	0.23	0.00	0.00	20.9
18	52	-0	6215	0	0	0	6561	--	--	16.08	16.08	0.00	0.11	0.05	0.39	0.00	0.00	20.9
19	52	-0	4563	0	0	0	2708	--	--	16.08	16.08	0.00	0.05	0.04	0.29	0.00	0.00	20.9
20	52	-0	5152	0	0	0	4301	--	--	16.08	16.08	0.00	0.07	0.04	0.32	0.00	0.00	20.9
37	52	-0	6585	0	0	0	7500	--	--	16.08	16.08	0.00	0.13	0.05	0.41	0.00	0.00	20.9
38	52	-0	3831	0	0	0	1078	--	--	16.08	16.08	0.00	0.02	0.03	0.24	0.00	0.00	20.9
39	52	-0	4813	0	0	0	3734	--	--	16.08	16.08	0.00	0.06	0.04	0.30	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 82 NI 1315 NF 1284 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	3109	0	0	0	-640	--	--	16.08	16.08	0.18	0.01	0.03	0.20	0.00	0.00	20.9
2	0	-0	2594	0	0	0	-165	--	--	16.08	16.08	0.29	0.00	0.02	0.16	0.00	0.00	20.9
3	0	-0	2594	0	0	0	-275	--	--	16.08	16.08	0.29	0.00	0.02	0.16	0.00	0.00	20.9
4	0	-0	2189	0	0	0	-710	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
5	0	-0	2189	0	0	0	-820	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
6	0	-0	2452	0	0	0	-226	--	--	16.08	16.08	0.29	0.00	0.02	0.15	0.00	0.00	20.9
7	0	-0	2453	0	0	0	-595	--	--	16.08	16.08	0.29	0.01	0.02	0.15	0.00	0.00	20.9
8	0	-0	2330	0	0	0	-390	--	--	16.08	16.08	0.29	0.01	0.02	0.15	0.00	0.00	20.9
9	0	-0	2331	0	0	0	-759	--	--	16.08	16.08	0.29	0.01	0.02	0.15	0.00	0.00	20.9
10	0	-0	2594	0	0	0	-165	--	--	16.08	16.08	0.29	0.00	0.02	0.16	0.00	0.00	20.9
11	0	-0	2594	0	0	0	-275	--	--	16.08	16.08	0.29	0.00	0.02	0.16	0.00	0.00	20.9
12	0	-0	2189	0	0	0	-710	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
13	0	-0	2189	0	0	0	-820	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
14	0	-0	2452	0	0	0	-226	--	--	16.08	16.08	0.29	0.00	0.02	0.15	0.00	0.00	20.9
15	0	-0	2453	0	0	0	-595	--	--	16.08	16.08	0.29	0.01	0.02	0.15	0.00	0.00	20.9
16	0	-0	2330	0	0	0	-390	--	--	16.08	16.08	0.29	0.01	0.02	0.15	0.00	0.00	20.9
17	0	-0	2331	0	0	0	-759	--	--	16.08	16.08	0.29	0.01	0.02	0.15	0.00	0.00	20.9
18	0	-0	4424	0	0	0	1064	--	--	16.08	16.08	0.00	0.02	0.04	0.28	0.00	0.00	20.9
19	0	-0	2794	0	0	0	-1093	--	--	16.08	16.08	0.18	0.02	0.02	0.18	0.00	0.00	20.9
20	0	-0	3398	0	0	0	-116	--	--	16.08	16.08	0.18	0.00	0.03	0.21	0.00	0.00	20.9
37	0	-0	4817	0	0	0	1610	--	--	16.08	16.08	0.00	0.03	0.04	0.30	0.00	0.00	20.9
38	0	-0	2099	0	0	0	-1986	--	--	16.08	16.08	0.18	0.03	0.02	0.13	0.00	0.00	20.9
39	0	-0	3105	0	0	0	-357	--	--	16.08	16.08	0.18	0.01	0.03	0.19	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	3109	0	0	0	3486	--	--	16.08	16.08	0.00	0.06	0.03	0.20	0.00	0.00	20.9
2	26	-0	2594	0	0	0	3278	--	--	16.08	16.08	0.10	0.06	0.02	0.16	0.00	0.00	20.9
3	26	-0	2594	0	0	0	3167	--	--	16.08	16.08	0.10	0.06	0.02	0.16	0.00	0.00	20.9
4	26	-0	2189	0	0	0	-710	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
5	26	-0	2189	0	0	0	-820	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
6	26	-0	2452	0	0	0	3027	--	--	16.08	16.08	0.10	0.05	0.02	0.15	0.00	0.00	20.9
7	26	-0	2453	0	0	0	2660	--	--	16.08	16.08	0.10	0.05	0.02	0.15	0.00	0.00	20.9
8	26	-0	2330	0	0	0	2702	--	--	16.08	16.08	0.10	0.05	0.02	0.15	0.00	0.00	20.9
9	26	-0	2331	0	0	0	-759	--	--	16.08	16.08	0.29	0.01	0.02	0.15	0.00	0.00	20.9
10	26	-0	2594	0	0	0	3278	--	--	16.08	16.08	0.10	0.06	0.02	0.16	0.00	0.00	20.9
11	26	-0	2594	0	0	0	3167	--	--	16.08	16.08	0.10	0.06	0.02	0.16	0.00	0.00	20.9
12	26	-0	2189	0	0	0	-710	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
13	26	-0	2189	0	0	0	-820	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
14	26	-0	2452	0	0	0	3027	--	--	16.08	16.08	0.10	0.05	0.02	0.15	0.00	0.00	20.9
15	26	-0	2453	0	0	0	2660	--	--	16.08	16.08	0.10	0.05	0.02	0.15	0.00	0.00	20.9
16	26	-0	2330	0	0	0	2702	--	--	16.08	16.08	0.10	0.05	0.02	0.15	0.00	0.00	20.9
17	26	-0	2331	0	0	0	-759	--	--	16.08	16.08	0.29	0.01	0.02	0.15	0.00	0.00	20.9
18	26	-0	4424	0	0	0	6935	--	--	16.08	16.08	0.00	0.12	0.04	0.28	0.00	0.00	20.9
19	26	-0	2794	0	0	0	-1093	--	--	16.08	16.08	0.18	0.02	0.02	0.18	0.00	0.00	20.9
20	26	-0	3398	0	0	0	4394	--	--	16.08	16.08	0.00	0.07	0.03	0.21	0.00	0.00	20.9
37	26	-0	4817	0	0	0	8002	--	--	16.08	16.08	0.00	0.14	0.04	0.30	0.00	0.00	20.9
38	26	-0	2099	0	0	0	-1986	--	--	16.08	16.08	0.18	0.03	0.02	0.13	0.00	0.00	20.9
39	26	-0	3105	0	0	0	3764	--	--	16.08	16.08	0.00	0.06	0.03	0.19	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	52	-0	3109	0	0	0	966	--	--	16.08	16.08	0.00	0.02	0.03	0.20	0.00	0.00	20.9
2	52	-0	2594	0	0	0	1176	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
3	52	-0	2594	0	0	0	1065	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
4	52	-0	2189	0	0	0	421	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
5	52	-0	2189	0	0	0	311	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
6	52	-0	2452	0	0	0	1040	--	--	16.08	16.08	0.10	0.02	0.02	0.15	0.00	0.00	20.9
7	52	-0	2453	0	0	0	672	--	--	16.08	16.08	0.10	0.01	0.02	0.15	0.00	0.00	20.9
8	52	-0	2330	0	0	0	814	--	--	16.08	16.08	0.10	0.01	0.02	0.15	0.00	0.00	20.9
9	52	-0	2331	0	0	0	446	--	--	16.08	16.08	0.10	0.01	0.02	0.15	0.00	0.00	20.9
10	52	-0	2594	0	0	0	1176	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
11	52	-0	2594	0	0	0	1065	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
12	52	-0	2189	0	0	0	421	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
13	52	-0	2189	0	0	0	311	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
14	52	-0	2452	0	0	0	1040	--	--	16.08	16.08	0.10	0.02	0.02	0.15	0.00	0.00	20.9
15	52	-0	2453	0	0	0	672	--	--	16.08	16.08	0.10	0.01	0.02	0.15	0.00	0.00	20.9
16	52	-0	2330	0	0	0	814	--	--	16.08	16.08	0.10	0.01	0.02	0.15	0.00	0.00	20.9
17	52	-0	2331	0	0	0	446	--	--	16.08	16.08	0.10	0.01	0.02	0.15	0.00	0.00	20.9
18	52	-0	4424	0	0	0	3350	--	--	16.08	16.08	0.00	0.06	0.04	0.28	0.00	0.00	20.9
19	52	-0	2794	0	0	0	350	--	--	16.08	16.08	0.00	0.01	0.02	0.18	0.00	0.00	20.9
20	52	-0	3398	0	0	0	1640	--	--	16.08	16.08	0.00	0.03	0.03	0.21	0.00	0.00	20.9
37	52	-0	4817	0	0	0	4098	--	--	16.08	16.08	0.00	0.07	0.04	0.30	0.00	0.00	20.9
38	52	-0	2099	0	0	0	-1986	--	--	16.08	16.08	0.18	0.03	0.02	0.13	0.00	0.00	20.9
39	52	-0	3105	0	0	0	1248	--	--	16.08	16.08	0.00	0.02	0.03	0.19	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 83 NI 1316 NF 1315 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	1487	0	0	0	-1409	--	--	16.08	16.08	0.18	0.02	0.01	0.09	0.00	0.00	20.9
2	0	-0	1364	0	0	0	-869	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
3	0	-0	1358	0	0	0	-977	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
4	0	-0	929	0	0	0	-1190	--	--	16.08	16.08	0.29	0.02	0.01	0.06	0.00	0.00	20.9
5	0	-0	924	0	0	0	-1298	--	--	16.08	16.08	0.29	0.02	0.01	0.06	0.00	0.00	20.9
6	0	-0	1218	0	0	0	-856	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
7	0	-0	1199	0	0	0	-1215	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
8	0	-0	1088	0	0	0	-952	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
9	0	-0	1069	0	0	0	-1311	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
10	0	-0	1364	0	0	0	-869	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
11	0	-0	1358	0	0	0	-977	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
12	0	-0	929	0	0	0	-1190	--	--	16.08	16.08	0.29	0.02	0.01	0.06	0.00	0.00	20.9
13	0	-0	924	0	0	0	-1298	--	--	16.08	16.08	0.29	0.02	0.01	0.06	0.00	0.00	20.9
14	0	-0	1218	0	0	0	-856	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
15	0	-0	1199	0	0	0	-1215	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
16	0	-0	1088	0	0	0	-952	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9

17	0	-0	1069	0	0	0	-1311	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
18	0	-0	2765	0	0	0	-365	--	--	16.08	16.08	0.18	0.01	0.02	0.17	0.00	0.00	20.9
19	0	-0	1094	0	0	0	-1658	--	--	16.08	16.08	0.18	0.03	0.01	0.07	0.00	0.00	20.9
20	0	-0	1741	0	0	0	-1016	--	--	16.08	16.08	0.18	0.02	0.01	0.11	0.00	0.00	20.9
37	0	-0	3194	0	0	0	-40	--	--	16.08	16.08	0.18	0.00	0.03	0.20	0.00	0.00	20.9
38	0	-0	408	0	0	0	-2197	--	--	16.08	16.08	0.18	0.04	0.00	0.03	0.00	0.00	20.9
39	0	-0	1487	0	0	0	-1125	--	--	16.08	16.08	0.18	0.02	0.01	0.09	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	1487	0	0	0	-1409	--	--	16.08	16.08	0.18	0.02	0.01	0.09	0.00	0.00	20.9
2	26	-0	1364	0	0	0	-869	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
3	26	-0	1358	0	0	0	-977	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
4	26	-0	929	0	0	0	-1190	--	--	16.08	16.08	0.29	0.02	0.01	0.06	0.00	0.00	20.9
5	26	-0	924	0	0	0	-1298	--	--	16.08	16.08	0.29	0.02	0.01	0.06	0.00	0.00	20.9
6	26	-0	1218	0	0	0	-856	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
7	26	-0	1199	0	0	0	-1215	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
8	26	-0	1088	0	0	0	-952	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
9	26	-0	1069	0	0	0	-1311	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
10	26	-0	1364	0	0	0	-869	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
11	26	-0	1358	0	0	0	-977	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
12	26	-0	929	0	0	0	-1190	--	--	16.08	16.08	0.29	0.02	0.01	0.06	0.00	0.00	20.9
13	26	-0	924	0	0	0	-1298	--	--	16.08	16.08	0.29	0.02	0.01	0.06	0.00	0.00	20.9
14	26	-0	1218	0	0	0	-856	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
15	26	-0	1199	0	0	0	-1215	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
16	26	-0	1088	0	0	0	-952	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
17	26	-0	1069	0	0	0	-1311	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
18	26	-0	2765	0	0	0	3305	--	--	16.08	16.08	0.00	0.06	0.02	0.17	0.00	0.00	20.9
19	26	-0	1094	0	0	0	-1658	--	--	16.08	16.08	0.18	0.03	0.01	0.07	0.00	0.00	20.9
20	26	-0	1741	0	0	0	-1016	--	--	16.08	16.08	0.18	0.02	0.01	0.11	0.00	0.00	20.9
37	26	-0	3194	0	0	0	4198	--	--	16.08	16.08	0.00	0.07	0.03	0.20	0.00	0.00	20.9
38	26	-0	408	0	0	0	-2197	--	--	16.08	16.08	0.18	0.04	0.00	0.03	0.00	0.00	20.9
39	26	-0	1487	0	0	0	-1125	--	--	16.08	16.08	0.18	0.02	0.01	0.09	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	52	-0	1487	0	0	0	-1409	--	--	16.08	16.08	0.18	0.02	0.01	0.09	0.00	0.00	20.9
2	52	-0	1364	0	0	0	-869	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
3	52	-0	1358	0	0	0	-977	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
4	52	-0	929	0	0	0	-1190	--	--	16.08	16.08	0.29	0.02	0.01	0.06	0.00	0.00	20.9
5	52	-0	924	0	0	0	-1298	--	--	16.08	16.08	0.29	0.02	0.01	0.06	0.00	0.00	20.9
6	52	-0	1218	0	0	0	-856	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
7	52	-0	1199	0	0	0	-1215	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
8	52	-0	1088	0	0	0	-952	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
9	52	-0	1069	0	0	0	-1311	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
10	52	-0	1364	0	0	0	-869	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
11	52	-0	1358	0	0	0	-977	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
12	52	-0	929	0	0	0	-1190	--	--	16.08	16.08	0.29	0.02	0.01	0.06	0.00	0.00	20.9
13	52	-0	924	0	0	0	-1298	--	--	16.08	16.08	0.29	0.02	0.01	0.06	0.00	0.00	20.9
14	52	-0	1218	0	0	0	-856	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
15	52	-0	1199	0	0	0	-1215	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
16	52	-0	1088	0	0	0	-952	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
17	52	-0	1069	0	0	0	-1311	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
18	52	-0	2765	0	0	0	1064	--	--	16.08	16.08	0.00	0.02	0.02	0.17	0.00	0.00	20.9
19	52	-0	1094	0	0	0	-1658	--	--	16.08	16.08	0.18	0.03	0.01	0.07	0.00	0.00	20.9
20	52	-0	1741	0	0	0	-1016	--	--	16.08	16.08	0.18	0.02	0.01	0.11	0.00	0.00	20.9
37	52	-0	3194	0	0	0	1610	--	--	16.08	16.08	0.00	0.03	0.03	0.20	0.00	0.00	20.9
38	52	-0	408	0	0	0	-2197	--	--	16.08	16.08	0.18	0.04	0.00	0.03	0.00	0.00	20.9
39	52	-0	1487	0	0	0	-1125	--	--	16.08	16.08	0.18	0.02	0.01	0.09	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 84 NI 1283 NF 1316 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-63	0	0	0	-1409	--	--	16.08	16.08	0.18	0.02	0.00	0.00	0.00	0.00	20.9
2	0	-0	200	0	0	0	-973	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
3	0	-0	185	0	0	0	-1073	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
4	0	-0	-282	0	0	0	-1190	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
5	0	-0	-297	0	0	0	-1298	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
6	0	-0	48	0	0	0	-881	--	--	16.08	16.08	0.29	0.02	0.00	0.00	0.00	0.00	20.9
7	0	-0	-1	0	0	0	-1215	--	--	16.08	16.08	0.29	0.02	0.00	0.00	0.00	0.00	20.9
8	0	-0	-96	0	0	0	-952	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
9	0	-0	-146	0	0	0	-1311	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
10	0	-0	200	0	0	0	-973	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
11	0	-0	185	0	0	0	-1073	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
12	0	-0	-282	0	0	0	-1190	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
13	0	-0	-297	0	0	0	-1298	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
14	0	-0	48	0	0	0	-881	--	--	16.08	16.08	0.29	0.02	0.00	0.00	0.00	0.00	20.9
15	0	-0	-1	0	0	0	-1215	--	--	16.08	16.08	0.29	0.02	0.00	0.00	0.00	0.00	20.9
16	0	-0	-96	0	0	0	-952	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
17	0	-0	-146	0	0	0	-1311	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
18	0	-0	1238	0	0	0	-1004	--	--	16.08	16.08	0.18	0.02	0.01	0.08	0.00	0.00	20.9
19	0	-0	-545	0	0	0	-1658	--	--	16.08	16.08	0.18	0.03	0.00	0.03	0.00	0.00	20.9
20	0	-0	179	0	0	0	-1108	--	--	16.08	16.08	0.18	0.02	0.00	0.01	0.00	0.00	20.9
37	0	-0	1719	0	0	0	-928	--	--	16.08	16.08	0.18	0.02	0.01	0.11	0.00	0.00	20.9
38	0	-0	-1253	0	0	0	-2197	--	--	16.08	16.08	0.18	0.04	0.01	0.08	0.00	0.00	20.9
39	0	-0	-47	0	0	0	-1125	--	--	16.08	16.08	0.18	0.02	0.00	0.00	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	-63	0	0	0	-1409	--	--	16.08	16.08	0.18	0.02	0.00	0.00	0.00	0.00	20.9
2	26	-0	200	0	0	0	-973	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
3	26	-0	185	0	0	0	-1073	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
4	26	-0	-282	0	0	0	-1190	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
5	26	-0	-297	0	0	0	-1298	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
6	26	-0	48	0	0	0	-881	--	--	16.08	16.08	0.29	0.02	0.00	0.00	0.00	0.00	20.9
7	26	-0	-1	0	0	0	-1215	--	--	16.08	16.08	0.29	0.02	0.00	0.00	0.00	0.00	20.9
8	26	-0	-96	0	0	0	-952	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
9	26	-0	-146	0	0	0	-1311	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
10	26	-0	200	0	0	0	-973	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
11	26	-0	185	0	0	0	-1073	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
12	26	-0	-282	0	0	0	-1190	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9

13	26	-0	-297	0	0	0	-1298	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
14	26	-0	48	0	0	0	-881	--	--	16.08	16.08	0.29	0.02	0.00	0.00	0.00	0.00	20.9
15	26	-0	-1	0	0	0	-1215	--	--	16.08	16.08	0.29	0.02	0.00	0.00	0.00	0.00	20.9
16	26	-0	-96	0	0	0	-952	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
17	26	-0	-146	0	0	0	-1311	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
18	26	-0	1238	0	0	0	-1004	--	--	16.08	16.08	0.18	0.02	0.01	0.08	0.00	0.00	20.9
19	26	-0	-545	0	0	0	-1658	--	--	16.08	16.08	0.18	0.03	0.00	0.03	0.00	0.00	20.9
20	26	-0	179	0	0	0	-1108	--	--	16.08	16.08	0.18	0.02	0.00	0.01	0.00	0.00	20.9
37	26	-0	1719	0	0	0	-928	--	--	16.08	16.08	0.18	0.02	0.01	0.11	0.00	0.00	20.9
38	26	-0	-1253	0	0	0	-2197	--	--	16.08	16.08	0.18	0.04	0.01	0.08	0.00	0.00	20.9
39	26	-0	-47	0	0	0	-1125	--	--	16.08	16.08	0.18	0.02	0.00	0.00	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	52	-0	-63	0	0	0	-1409	--	--	16.08	16.08	0.18	0.02	0.00	0.00	0.00	0.00	20.9
2	52	-0	200	0	0	0	-973	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
3	52	-0	185	0	0	0	-1073	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
4	52	-0	-282	0	0	0	-1190	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
5	52	-0	-297	0	0	0	-1298	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
6	52	-0	48	0	0	0	-881	--	--	16.08	16.08	0.29	0.02	0.00	0.00	0.00	0.00	20.9
7	52	-0	-1	0	0	0	-1215	--	--	16.08	16.08	0.29	0.02	0.00	0.00	0.00	0.00	20.9
8	52	-0	-96	0	0	0	-952	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
9	52	-0	-146	0	0	0	-1311	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
10	52	-0	200	0	0	0	-973	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
11	52	-0	185	0	0	0	-1073	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
12	52	-0	-282	0	0	0	-1190	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
13	52	-0	-297	0	0	0	-1298	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
14	52	-0	48	0	0	0	-881	--	--	16.08	16.08	0.29	0.02	0.00	0.00	0.00	0.00	20.9
15	52	-0	-1	0	0	0	-1215	--	--	16.08	16.08	0.29	0.02	0.00	0.00	0.00	0.00	20.9
16	52	-0	-96	0	0	0	-952	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
17	52	-0	-146	0	0	0	-1311	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
18	52	-0	1238	0	0	0	-1004	--	--	16.08	16.08	0.18	0.02	0.01	0.08	0.00	0.00	20.9
19	52	-0	-545	0	0	0	-1658	--	--	16.08	16.08	0.18	0.03	0.00	0.03	0.00	0.00	20.9
20	52	-0	179	0	0	0	-1108	--	--	16.08	16.08	0.18	0.02	0.00	0.01	0.00	0.00	20.9
37	52	-0	1719	0	0	0	-928	--	--	16.08	16.08	0.18	0.02	0.01	0.11	0.00	0.00	20.9
38	52	-0	-1253	0	0	0	-2197	--	--	16.08	16.08	0.18	0.04	0.01	0.08	0.00	0.00	20.9
39	52	-0	-47	0	0	0	-1125	--	--	16.08	16.08	0.18	0.02	0.00	0.00	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 85 NI 1265 NF 1283 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm

1	0	-0	-1551	0	0	0	-1376	--	--	16.08	16.08	0.18	0.02	0.01	0.10	0.00	0.00	20.9
2	0	-0	-904	0	0	0	-973	--	--	16.08	16.08	0.29	0.02	0.01	0.06	0.00	0.00	20.9
3	0	-0	-931	0	0	0	-1073	--	--	16.08	16.08	0.29	0.02	0.01	0.06	0.00	0.00	20.9
4	0	-0	-1455	0	0	0	-1044	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
5	0	-0	-1482	0	0	0	-1144	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
6	0	-0	-1065	0	0	0	-881	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
7	0	-0	-1156	0	0	0	-1214	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
8	0	-0	-1230	0	0	0	-902	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
9	0	-0	-1321	0	0	0	-1236	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
10	0	-0	-904	0	0	0	-973	--	--	16.08	16.08	0.29	0.02	0.01	0.06	0.00	0.00	20.9
11	0	-0	-931	0	0	0	-1073	--	--	16.08	16.08	0.29	0.02	0.01	0.06	0.00	0.00	20.9
12	0	-0	-1455	0	0	0	-1044	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
13	0	-0	-1482	0	0	0	-1144	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
14	0	-0	-1065	0	0	0	-881	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
15	0	-0	-1156	0	0	0	-1214	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
16	0	-0	-1230	0	0	0	-902	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
17	0	-0	-1321	0	0	0	-1236	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
18	0	-0	-162	0	0	0	-1004	--	--	16.08	16.08	0.18	0.02	0.00	0.01	0.00	0.00	20.9
19	0	-0	-2136	0	0	0	-1377	--	--	16.08	16.08	0.18	0.02	0.02	0.13	0.00	0.00	20.9
20	0	-0	-1299	0	0	0	-1108	--	--	16.08	16.08	0.18	0.02	0.01	0.08	0.00	0.00	20.9
37	0	-0	390	0	0	0	-1130	--	--	16.08	16.08	0.18	0.02	0.00	0.02	0.00	0.00	20.9
38	0	-0	-2901	0	0	0	-1549	--	--	16.08	16.08	0.18	0.03	0.02	0.18	0.00	0.00	20.9
39	0	-0	-1505	0	0	0	-1101	--	--	16.08	16.08	0.18	0.02	0.01	0.09	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	-1551	0	0	0	-1376	--	--	16.08	16.08	0.18	0.02	0.01	0.10	0.00	0.00	20.9
2	26	-0	-904	0	0	0	-973	--	--	16.08	16.08	0.29	0.02	0.01	0.06	0.00	0.00	20.9
3	26	-0	-931	0	0	0	-1073	--	--	16.08	16.08	0.29	0.02	0.01	0.06	0.00	0.00	20.9
4	26	-0	-1455	0	0	0	-1044	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
5	26	-0	-1482	0	0	0	-1144	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
6	26	-0	-1065	0	0	0	-881	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
7	26	-0	-1156	0	0	0	-1214	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
8	26	-0	-1230	0	0	0	-902	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
9	26	-0	-1321	0	0	0	-1236	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
10	26	-0	-904	0	0	0	-973	--	--	16.08	16.08	0.29	0.02	0.01	0.06	0.00	0.00	20.9
11	26	-0	-931	0	0	0	-1073	--	--	16.08	16.08	0.29	0.02	0.01	0.06	0.00	0.00	20.9
12	26	-0	-1455	0	0	0	-1044	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
13	26	-0	-1482	0	0	0	-1144	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
14	26	-0	-1065	0	0	0	-881	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
15	26	-0	-1156	0	0	0	-1214	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
16	26	-0	-1230	0	0	0	-902	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
17	26	-0	-1321	0	0	0	-1236	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
18	26	-0	-162	0	0	0	-1004	--	--	16.08	16.08	0.18	0.02	0.00	0.01	0.00	0.00	20.9
19	26	-0	-2136	0	0	0	-1377	--	--	16.08	16.08	0.18	0.02	0.02	0.13	0.00	0.00	20.9
20	26	-0	-1299	0	0	0	-1108	--	--	16.08	16.08	0.18	0.02	0.01	0.08	0.00	0.00	20.9
37	26	-0	390	0	0	0	-1130	--	--	16.08	16.08	0.18	0.02	0.00	0.02	0.00	0.00	20.9
38	26	-0	-2901	0	0	0	-1549	--	--	16.08	16.08	0.18	0.03	0.02	0.18	0.00	0.00	20.9
39	26	-0	-1505	0	0	0	-1101	--	--	16.08	16.08	0.18	0.02	0.01	0.09	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	52	-0	-1551	0	0	0	-1376	--	--	16.08	16.08	0.18	0.02	0.01	0.10	0.00	0.00	20.9
2	52	-0	-904	0	0	0	-973	--	--	16.08	16.08	0.29	0.02	0.01	0.06	0.00	0.00	20.9
3	52	-0	-931	0	0	0	-1073	--	--	16.08	16.08	0.29	0.02	0.01	0.06	0.00	0.00	20.9
4	52	-0	-1455	0	0	0	-1044	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
5	52	-0	-1482	0	0	0	-1144	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
6	52	-0	-1065	0	0	0	-881	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
7	52	-0	-1156	0	0	0	-1214	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
8	52	-0	-1230	0	0	0	-902	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9

9	52	-0	-1321	0	0	0	-1236	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
10	52	-0	-904	0	0	0	-973	--	--	16.08	16.08	0.29	0.02	0.01	0.06	0.00	0.00	20.9
11	52	-0	-931	0	0	0	-1073	--	--	16.08	16.08	0.29	0.02	0.01	0.06	0.00	0.00	20.9
12	52	-0	-1455	0	0	0	-1044	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
13	52	-0	-1482	0	0	0	-1144	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
14	52	-0	-1065	0	0	0	-881	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
15	52	-0	-1156	0	0	0	-1214	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
16	52	-0	-1230	0	0	0	-902	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
17	52	-0	-1321	0	0	0	-1236	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
18	52	-0	-162	0	0	0	-1004	--	--	16.08	16.08	0.18	0.02	0.00	0.01	0.00	0.00	20.9
19	52	-0	-2136	0	0	0	-1377	--	--	16.08	16.08	0.18	0.02	0.02	0.13	0.00	0.00	20.9
20	52	-0	-1299	0	0	0	-1108	--	--	16.08	16.08	0.18	0.02	0.01	0.08	0.00	0.00	20.9
37	52	-0	390	0	0	0	-1130	--	--	16.08	16.08	0.18	0.02	0.00	0.02	0.00	0.00	20.9
38	52	-0	-2901	0	0	0	-1549	--	--	16.08	16.08	0.18	0.03	0.02	0.18	0.00	0.00	20.9
39	52	-0	-1505	0	0	0	-1101	--	--	16.08	16.08	0.18	0.02	0.01	0.09	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 86 NI 1901 NF 1277 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	1351	0	0	0	-4136	--	--	16.08	16.08	0.18	0.07	0.01	0.08	0.00	0.00	20.9
2	0	-0	1007	0	0	0	-3218	--	--	16.08	16.08	0.29	0.06	0.01	0.06	0.00	0.00	20.9
3	0	-0	1064	0	0	0	-3105	--	--	16.08	16.08	0.29	0.05	0.01	0.07	0.00	0.00	20.9
4	0	-0	1015	0	0	0	-3258	--	--	16.08	16.08	0.29	0.06	0.01	0.06	0.00	0.00	20.9
5	0	-0	1072	0	0	0	-3145	--	--	16.08	16.08	0.29	0.05	0.01	0.07	0.00	0.00	20.9
6	0	-0	944	0	0	0	-3364	--	--	16.08	16.08	0.29	0.06	0.01	0.06	0.00	0.00	20.9
7	0	-0	1133	0	0	0	-2987	--	--	16.08	16.08	0.29	0.05	0.01	0.07	0.00	0.00	20.9
8	0	-0	946	0	0	0	-3376	--	--	16.08	16.08	0.29	0.06	0.01	0.06	0.00	0.00	20.9
9	0	-0	1136	0	0	0	-2999	--	--	16.08	16.08	0.29	0.05	0.01	0.07	0.00	0.00	20.9
10	0	-0	1007	0	0	0	-3218	--	--	16.08	16.08	0.29	0.06	0.01	0.06	0.00	0.00	20.9
11	0	-0	1064	0	0	0	-3105	--	--	16.08	16.08	0.29	0.05	0.01	0.07	0.00	0.00	20.9
12	0	-0	1015	0	0	0	-3258	--	--	16.08	16.08	0.29	0.06	0.01	0.06	0.00	0.00	20.9
13	0	-0	1072	0	0	0	-3145	--	--	16.08	16.08	0.29	0.05	0.01	0.07	0.00	0.00	20.9
14	0	-0	944	0	0	0	-3364	--	--	16.08	16.08	0.29	0.06	0.01	0.06	0.00	0.00	20.9
15	0	-0	1133	0	0	0	-2987	--	--	16.08	16.08	0.29	0.05	0.01	0.07	0.00	0.00	20.9
16	0	-0	946	0	0	0	-3376	--	--	16.08	16.08	0.29	0.06	0.01	0.06	0.00	0.00	20.9
17	0	-0	1136	0	0	0	-2999	--	--	16.08	16.08	0.29	0.05	0.01	0.07	0.00	0.00	20.9
18	0	-0	1111	0	0	0	-4903	--	--	16.08	16.08	0.18	0.08	0.01	0.07	0.00	0.00	20.9
19	0	-0	1158	0	0	0	-4890	--	--	16.08	16.08	0.18	0.08	0.01	0.07	0.00	0.00	20.9
20	0	-0	1016	0	0	0	-5194	--	--	16.08	16.08	0.18	0.09	0.01	0.06	0.00	0.00	20.9
37	0	-0	1182	0	0	0	-4607	--	--	16.08	16.08	0.18	0.08	0.01	0.07	0.00	0.00	20.9
38	0	-0	1260	0	0	0	-4585	--	--	16.08	16.08	0.18	0.08	0.01	0.08	0.00	0.00	20.9
39	0	-0	1024	0	0	0	-5091	--	--	16.08	16.08	0.18	0.08	0.01	0.06	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	1351	0	0	0	-4136	--	--	16.08	16.08	0.18	0.07	0.01	0.08	0.00	0.00	20.9
2	27	-0	1007	0	0	0	-3218	--	--	16.08	16.08	0.29	0.06	0.01	0.06	0.00	0.00	20.9
3	27	-0	1064	0	0	0	-3105	--	--	16.08	16.08	0.29	0.05	0.01	0.07	0.00	0.00	20.9
4	27	-0	1015	0	0	0	-3258	--	--	16.08	16.08	0.29	0.06	0.01	0.06	0.00	0.00	20.9
5	27	-0	1072	0	0	0	-3145	--	--	16.08	16.08	0.29	0.05	0.01	0.07	0.00	0.00	20.9
6	27	-0	944	0	0	0	-3364	--	--	16.08	16.08	0.29	0.06	0.01	0.06	0.00	0.00	20.9
7	27	-0	1133	0	0	0	-2987	--	--	16.08	16.08	0.29	0.05	0.01	0.07	0.00	0.00	20.9
8	27	-0	946	0	0	0	-3376	--	--	16.08	16.08	0.29	0.06	0.01	0.06	0.00	0.00	20.9
9	27	-0	1136	0	0	0	-2999	--	--	16.08	16.08	0.29	0.05	0.01	0.07	0.00	0.00	20.9
10	27	-0	1007	0	0	0	-3218	--	--	16.08	16.08	0.29	0.06	0.01	0.06	0.00	0.00	20.9
11	27	-0	1064	0	0	0	-3105	--	--	16.08	16.08	0.29	0.05	0.01	0.07	0.00	0.00	20.9
12	27	-0	1015	0	0	0	-3258	--	--	16.08	16.08	0.29	0.06	0.01	0.06	0.00	0.00	20.9
13	27	-0	1072	0	0	0	-3145	--	--	16.08	16.08	0.29	0.05	0.01	0.07	0.00	0.00	20.9
14	27	-0	944	0	0	0	-3364	--	--	16.08	16.08	0.29	0.06	0.01	0.06	0.00	0.00	20.9
15	27	-0	1133	0	0	0	-2987	--	--	16.08	16.08	0.29	0.05	0.01	0.07	0.00	0.00	20.9
16	27	-0	946	0	0	0	-3376	--	--	16.08	16.08	0.29	0.06	0.01	0.06	0.00	0.00	20.9
17	27	-0	1136	0	0	0	-2999	--	--	16.08	16.08	0.29	0.05	0.01	0.07	0.00	0.00	20.9
18	27	-0	1111	0	0	0	-4903	--	--	16.08	16.08	0.18	0.08	0.01	0.07	0.00	0.00	20.9
19	27	-0	1158	0	0	0	-4890	--	--	16.08	16.08	0.18	0.08	0.01	0.07	0.00	0.00	20.9
20	27	-0	1016	0	0	0	-5194	--	--	16.08	16.08	0.18	0.09	0.01	0.06	0.00	0.00	20.9
37	27	-0	1182	0	0	0	-4607	--	--	16.08	16.08	0.18	0.08	0.01	0.07	0.00	0.00	20.9
38	27	-0	1260	0	0	0	-4585	--	--	16.08	16.08	0.18	0.08	0.01	0.08	0.00	0.00	20.9
39	27	-0	1024	0	0	0	-5091	--	--	16.08	16.08	0.18	0.08	0.01	0.06	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	54	-0	1351	0	0	0	-4136	--	--	16.08	16.08	0.18	0.07	0.01	0.08	0.00	0.00	20.9
2	54	-0	1007	0	0	0	-3218	--	--	16.08	16.08	0.29	0.06	0.01	0.06	0.00	0.00	20.9
3	54	-0	1064	0	0	0	-3105	--	--	16.08	16.08	0.29	0.05	0.01	0.07	0.00	0.00	20.9
4	54	-0	1015	0	0	0	-3258	--	--	16.08	16.08	0.29	0.06	0.01	0.06	0.00	0.00	20.9
5	54	-0	1072	0	0	0	-3145	--	--	16.08	16.08	0.29	0.05	0.01	0.07	0.00	0.00	20.9
6	54	-0	944	0	0	0	-3364	--	--	16.08	16.08	0.29	0.06	0.01	0.06	0.00	0.00	20.9
7	54	-0	1133	0	0	0	-2987	--	--	16.08	16.08	0.29	0.05	0.01	0.07	0.00	0.00	20.9
8	54	-0	946	0	0	0	-3376	--	--	16.08	16.08	0.29	0.06	0.01	0.06	0.00	0.00	20.9
9	54	-0	1136	0	0	0	-2999	--	--	16.08	16.08	0.29	0.05	0.01	0.07	0.00	0.00	20.9
10	54	-0	1007	0	0	0	-3218	--	--	16.08	16.08	0.29	0.06	0.01	0.06	0.00	0.00	20.9
11	54	-0	1064	0	0	0	-3105	--	--	16.08	16.08	0.29	0.05	0.01	0.07	0.00	0.00	20.9
12	54	-0	1015	0	0	0	-3258	--	--	16.08	16.08	0.29	0.06	0.01	0.06	0.00	0.00	20.9
13	54	-0	1072	0	0	0	-3145	--	--	16.08	16.08	0.29	0.05	0.01	0.07	0.00	0.00	20.9
14	54	-0	944	0	0	0	-3364	--	--	16.08	16.08	0.29	0.06	0.01	0.06	0.00	0.00	20.9
15	54	-0	1133	0	0	0	-2987	--	--	16.08	16.08	0.29	0.05	0.01	0.07	0.00	0.00	20.9
16	54	-0	946	0	0	0	-3376	--	--	16.08	16.08	0.29	0.06	0.01	0.06	0.00	0.00	20.9
17	54	-0	1136	0	0	0	-2999	--	--	16.08	16.08	0.29	0.05	0.01	0.07	0.00	0.00	20.9
18	54	-0	1111	0	0	0	-4903	--	--	16.08	16.08	0.18	0.08	0.01	0.07	0.00	0.00	20.9
19	54	-0	1158	0	0	0	-4890	--	--	16.08	16.08	0.18	0.08	0.01	0.07	0.00	0.00	20.9
20	54	-0	1016	0	0	0	-5194	--	--	16.08	16.08	0.18	0.09	0.01	0.06	0.00	0.00	20.9
37	54	-0	1182	0	0	0	-4607	--	--	16.08	16.08	0.18	0.08	0.01	0.07	0.00	0.00	20.9
38	54	-0	1260	0	0	0	-4585	--	--	16.08	16.08	0.18	0.08	0.01	0.08	0.00	0.00	20.9
39	54	-0	1024	0	0	0	-5091	--	--	16.08	16.08	0.18	0.08	0.01	0.06	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 87 NI 1893 NF 1901 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice resistenza			aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-253	0	0	0	-4136	--	--	16.08	16.08	0.18	0.07	0.00	0.02	0.00	0.00	20.9
2	0	-0	-229	0	0	0	-3218	--	--	16.08	16.08	0.29	0.06	0.00	0.01	0.00	0.00	20.9
3	0	-0	-165	0	0	0	-3105	--	--	16.08	16.08	0.29	0.05	0.00	0.01	0.00	0.00	20.9
4	0	-0	-224	0	0	0	-3258	--	--	16.08	16.08	0.29	0.06	0.00	0.01	0.00	0.00	20.9
5	0	-0	-161	0	0	0	-3145	--	--	16.08	16.08	0.29	0.05	0.00	0.01	0.00	0.00	20.9
6	0	-0	-302	0	0	0	-3364	--	--	16.08	16.08	0.29	0.06	0.00	0.02	0.00	0.00	20.9
7	0	-0	-89	0	0	0	-2987	--	--	16.08	16.08	0.29	0.05	0.00	0.01	0.00	0.00	20.9
8	0	-0	-301	0	0	0	-3376	--	--	16.08	16.08	0.29	0.06	0.00	0.02	0.00	0.00	20.9
9	0	-0	-88	0	0	0	-2999	--	--	16.08	16.08	0.29	0.05	0.00	0.01	0.00	0.00	20.9
10	0	-0	-229	0	0	0	-3218	--	--	16.08	16.08	0.29	0.06	0.00	0.01	0.00	0.00	20.9
11	0	-0	-165	0	0	0	-3105	--	--	16.08	16.08	0.29	0.05	0.00	0.01	0.00	0.00	20.9
12	0	-0	-224	0	0	0	-3258	--	--	16.08	16.08	0.29	0.06	0.00	0.01	0.00	0.00	20.9
13	0	-0	-161	0	0	0	-3145	--	--	16.08	16.08	0.29	0.05	0.00	0.01	0.00	0.00	20.9
14	0	-0	-302	0	0	0	-3364	--	--	16.08	16.08	0.29	0.06	0.00	0.02	0.00	0.00	20.9
15	0	-0	-89	0	0	0	-2987	--	--	16.08	16.08	0.29	0.05	0.00	0.01	0.00	0.00	20.9
16	0	-0	-301	0	0	0	-3376	--	--	16.08	16.08	0.29	0.06	0.00	0.02	0.00	0.00	20.9
17	0	-0	-88	0	0	0	-2999	--	--	16.08	16.08	0.29	0.05	0.00	0.01	0.00	0.00	20.9
18	0	-0	-598	0	0	0	-4903	--	--	16.08	16.08	0.18	0.08	0.00	0.04	0.00	0.00	20.9
19	0	-0	-554	0	0	0	-4890	--	--	16.08	16.08	0.18	0.08	0.00	0.03	0.00	0.00	20.9
20	0	-0	-710	0	0	0	-5194	--	--	16.08	16.08	0.18	0.09	0.01	0.04	0.00	0.00	20.9
37	0	-0	-477	0	0	0	-4607	--	--	16.08	16.08	0.18	0.08	0.00	0.03	0.00	0.00	20.9
38	0	-0	-405	0	0	0	-4585	--	--	16.08	16.08	0.18	0.08	0.00	0.03	0.00	0.00	20.9
39	0	-0	-664	0	0	0	-5091	--	--	16.08	16.08	0.18	0.08	0.01	0.04	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice resistenza			aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	27	-0	-253	0	0	0	-4136	--	--	16.08	16.08	0.18	0.07	0.00	0.02	0.00	0.00	20.9
2	27	-0	-229	0	0	0	-3218	--	--	16.08	16.08	0.29	0.06	0.00	0.01	0.00	0.00	20.9
3	27	-0	-165	0	0	0	-3105	--	--	16.08	16.08	0.29	0.05	0.00	0.01	0.00	0.00	20.9
4	27	-0	-224	0	0	0	-3258	--	--	16.08	16.08	0.29	0.06	0.00	0.01	0.00	0.00	20.9
5	27	-0	-161	0	0	0	-3145	--	--	16.08	16.08	0.29	0.05	0.00	0.01	0.00	0.00	20.9
6	27	-0	-302	0	0	0	-3364	--	--	16.08	16.08	0.29	0.06	0.00	0.02	0.00	0.00	20.9
7	27	-0	-89	0	0	0	-2987	--	--	16.08	16.08	0.29	0.05	0.00	0.01	0.00	0.00	20.9
8	27	-0	-301	0	0	0	-3376	--	--	16.08	16.08	0.29	0.06	0.00	0.02	0.00	0.00	20.9
9	27	-0	-88	0	0	0	-2999	--	--	16.08	16.08	0.29	0.05	0.00	0.01	0.00	0.00	20.9
10	27	-0	-229	0	0	0	-3218	--	--	16.08	16.08	0.29	0.06	0.00	0.01	0.00	0.00	20.9
11	27	-0	-165	0	0	0	-3105	--	--	16.08	16.08	0.29	0.05	0.00	0.01	0.00	0.00	20.9
12	27	-0	-224	0	0	0	-3258	--	--	16.08	16.08	0.29	0.06	0.00	0.01	0.00	0.00	20.9
13	27	-0	-161	0	0	0	-3145	--	--	16.08	16.08	0.29	0.05	0.00	0.01	0.00	0.00	20.9
14	27	-0	-302	0	0	0	-3364	--	--	16.08	16.08	0.29	0.06	0.00	0.02	0.00	0.00	20.9
15	27	-0	-89	0	0	0	-2987	--	--	16.08	16.08	0.29	0.05	0.00	0.01	0.00	0.00	20.9
16	27	-0	-301	0	0	0	-3376	--	--	16.08	16.08	0.29	0.06	0.00	0.02	0.00	0.00	20.9
17	27	-0	-88	0	0	0	-2999	--	--	16.08	16.08	0.29	0.05	0.00	0.01	0.00	0.00	20.9
18	27	-0	-598	0	0	0	-4903	--	--	16.08	16.08	0.18	0.08	0.00	0.04	0.00	0.00	20.9
19	27	-0	-554	0	0	0	-4890	--	--	16.08	16.08	0.18	0.08	0.00	0.03	0.00	0.00	20.9
20	27	-0	-710	0	0	0	-5194	--	--	16.08	16.08	0.18	0.09	0.01	0.04	0.00	0.00	20.9
37	27	-0	-477	0	0	0	-4607	--	--	16.08	16.08	0.18	0.08	0.00	0.03	0.00	0.00	20.9
38	27	-0	-405	0	0	0	-4585	--	--	16.08	16.08	0.18	0.08	0.00	0.03	0.00	0.00	20.9
39	27	-0	-664	0	0	0	-5091	--	--	16.08	16.08	0.18	0.08	0.01	0.04	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice resistenza			aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	54	-0	-253	0	0	0	-4136	--	--	16.08	16.08	0.18	0.07	0.00	0.02	0.00	0.00	20.9
2	54	-0	-229	0	0	0	-3218	--	--	16.08	16.08	0.29	0.06	0.00	0.01	0.00	0.00	20.9
3	54	-0	-165	0	0	0	-3105	--	--	16.08	16.08	0.29	0.05	0.00	0.01	0.00	0.00	20.9
4	54	-0	-224	0	0	0	-3258	--	--	16.08	16.08	0.29	0.06	0.00	0.01	0.00	0.00	20.9
5	54	-0	-161	0	0	0	-3145	--	--	16.08	16.08	0.29	0.05	0.00	0.01	0.00	0.00	20.9
6	54	-0	-302	0	0	0	-3364	--	--	16.08	16.08	0.29	0.06	0.00	0.02	0.00	0.00	20.9
7	54	-0	-89	0	0	0	-2987	--	--	16.08	16.08	0.29	0.05	0.00	0.01	0.00	0.00	20.9
8	54	-0	-301	0	0	0	-3376	--	--	16.08	16.08	0.29	0.06	0.00	0.02	0.00	0.00	20.9
9	54	-0	-88	0	0	0	-2999	--	--	16.08	16.08	0.29	0.05	0.00	0.01	0.00	0.00	20.9
10	54	-0	-229	0	0	0	-3218	--	--	16.08	16.08	0.29	0.06	0.00	0.01	0.00	0.00	20.9
11	54	-0	-165	0	0	0	-3105	--	--	16.08	16.08	0.29	0.05	0.00	0.01	0.00	0.00	20.9
12	54	-0	-224	0	0	0	-3258	--	--	16.08	16.08	0.29	0.06	0.00	0.01	0.00	0.00	20.9
13	54	-0	-161	0	0	0	-3145	--	--	16.08	16.08	0.29	0.05	0.00	0.01	0.00	0.00	20.9
14	54	-0	-302	0	0	0	-3364	--	--	16.08	16.08	0.29	0.06	0.00	0.02	0.00	0.00	20.9
15	54	-0	-89	0	0	0	-2987	--	--	16.08	16.08	0.29	0.05	0.00	0.01	0.00	0.00	20.9
16	54	-0	-301	0	0	0	-3376	--	--	16.08	16.08	0.29	0.06	0.00	0.02	0.00	0.00	20.9
17	54	-0	-88	0	0	0	-2999	--	--	16.08	16.08	0.29	0.05	0.00	0.01	0.00	0.00	20.9
18	54	-0	-598	0	0	0	-4903	--	--	16.08	16.08	0.18	0.08	0.00	0.04	0.00	0.00	20.9
19	54	-0	-554	0	0	0	-4890	--	--	16.08	16.08	0.18	0.08	0.00	0.03	0.00	0.00	20.9
20	54	-0	-710	0	0	0	-5194	--	--	16.08	16.08	0.18	0.09	0.01	0.04	0.00	0.00	20.9
37	54	-0	-477	0	0	0	-4607	--	--	16.08	16.08	0.18	0.08	0.00	0.03	0.00	0.00	20.9
38	54	-0	-405	0	0	0	-4585	--	--	16.08	16.08	0.18	0.08	0.00	0.03	0.00	0.00	20.9
39	54	-0	-664	0	0	0	-5091	--	--	16.08	16.08	0.18	0.08	0.01	0.04	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 88 NI 1899 NF 1893 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice resistenza			aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-1950	0	0	0	-4000	--	--	16.08	16.08	0.18	0.07	0.02	0.12	0.00	0.00	20.9
2	0	-0	-1535	0	0	0	-3095	--	--	16.08	16.08	0.29	0.05	0.01	0.10	0.00	0.00	20.9
3	0	-0	-1465	0	0	0	-3016	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
4	0	-0	-1535	0	0	0	-3138	--	--	16.08	16.08	0.29	0.05	0.01	0.10	0.00	0.00	20.9
5	0	-0	-1465	0	0	0	-3059	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
6	0	-0	-1617	0	0	0	-3202	--	--	16.08	16.08	0.29	0.06	0.01	0.10	0.00	0.00	20.9
7	0	-0	-1383	0	0	0	-2939	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
8	0	-0	-1617	0	0	0	-3215	--	--	16.08	16.08	0.29	0.06	0.01	0.10	0.00	0.00	20.9
9	0	-0	-1383	0	0	0	-2952	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
10	0	-0	-1535	0	0	0	-3095	--	--	16.08	16.08	0.29	0.05	0.01	0.10	0.00	0.00	20.9
11	0	-0	-1465	0	0	0	-3016	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
12	0	-0	-1535	0	0	0	-3138	--	--	16.08	16.08	0.29	0.05	0.01	0.10	0.00	0.00	20.9
13	0	-0	-1465	0	0	0	-3059	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
14	0	-0	-1617	0	0	0	-3202	--	--	16.08	16.08	0.29	0.06	0.01	0.10	0.00	0.00	20.9
15	0	-0	-1383	0	0	0	-2939	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
16	0	-0	-1617	0	0	0	-3215	--	--	16.08	16.08	0.29	0.06	0.01	0.10	0.00	0.00	20.9

17	0	-0	-1383	0	0	0	-2952	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
18	0	-0	-2419	0	0	0	-4583	--	--	16.08	16.08	0.18	0.08	0.02	0.15	0.00	0.00	20.9
19	0	-0	-2377	0	0	0	-4593	--	--	16.08	16.08	0.18	0.08	0.02	0.15	0.00	0.00	20.9
20	0	-0	-2540	0	0	0	-4813	--	--	16.08	16.08	0.18	0.08	0.02	0.16	0.00	0.00	20.9
37	0	-0	-2241	0	0	0	-4352	--	--	16.08	16.08	0.18	0.07	0.02	0.14	0.00	0.00	20.9
38	0	-0	-2171	0	0	0	-4368	--	--	16.08	16.08	0.18	0.07	0.02	0.14	0.00	0.00	20.9
39	0	-0	-2442	0	0	0	-4735	--	--	16.08	16.08	0.18	0.08	0.02	0.15	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-1950	0	0	0	-4000	--	--	16.08	16.08	0.18	0.07	0.02	0.12	0.00	0.00	20.9
2	27	-0	-1535	0	0	0	-3095	--	--	16.08	16.08	0.29	0.05	0.01	0.10	0.00	0.00	20.9
3	27	-0	-1465	0	0	0	-3016	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
4	27	-0	-1535	0	0	0	-3138	--	--	16.08	16.08	0.29	0.05	0.01	0.10	0.00	0.00	20.9
5	27	-0	-1465	0	0	0	-3059	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
6	27	-0	-1617	0	0	0	-3202	--	--	16.08	16.08	0.29	0.06	0.01	0.10	0.00	0.00	20.9
7	27	-0	-1383	0	0	0	-2939	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
8	27	-0	-1617	0	0	0	-3215	--	--	16.08	16.08	0.29	0.06	0.01	0.10	0.00	0.00	20.9
9	27	-0	-1383	0	0	0	-2952	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
10	27	-0	-1535	0	0	0	-3095	--	--	16.08	16.08	0.29	0.05	0.01	0.10	0.00	0.00	20.9
11	27	-0	-1465	0	0	0	-3016	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
12	27	-0	-1535	0	0	0	-3138	--	--	16.08	16.08	0.29	0.05	0.01	0.10	0.00	0.00	20.9
13	27	-0	-1465	0	0	0	-3059	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
14	27	-0	-1617	0	0	0	-3202	--	--	16.08	16.08	0.29	0.06	0.01	0.10	0.00	0.00	20.9
15	27	-0	-1383	0	0	0	-2939	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
16	27	-0	-1617	0	0	0	-3215	--	--	16.08	16.08	0.29	0.06	0.01	0.10	0.00	0.00	20.9
17	27	-0	-1383	0	0	0	-2952	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
18	27	-0	-2419	0	0	0	-4583	--	--	16.08	16.08	0.18	0.08	0.02	0.15	0.00	0.00	20.9
19	27	-0	-2377	0	0	0	-4593	--	--	16.08	16.08	0.18	0.08	0.02	0.15	0.00	0.00	20.9
20	27	-0	-2540	0	0	0	-4813	--	--	16.08	16.08	0.18	0.08	0.02	0.16	0.00	0.00	20.9
37	27	-0	-2241	0	0	0	-4352	--	--	16.08	16.08	0.18	0.07	0.02	0.14	0.00	0.00	20.9
38	27	-0	-2171	0	0	0	-4368	--	--	16.08	16.08	0.18	0.07	0.02	0.14	0.00	0.00	20.9
39	27	-0	-2442	0	0	0	-4735	--	--	16.08	16.08	0.18	0.08	0.02	0.15	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	54	-0	-1950	0	0	0	-4000	--	--	16.08	16.08	0.18	0.07	0.02	0.12	0.00	0.00	20.9
2	54	-0	-1535	0	0	0	-3095	--	--	16.08	16.08	0.29	0.05	0.01	0.10	0.00	0.00	20.9
3	54	-0	-1465	0	0	0	-3016	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
4	54	-0	-1535	0	0	0	-3138	--	--	16.08	16.08	0.29	0.05	0.01	0.10	0.00	0.00	20.9
5	54	-0	-1465	0	0	0	-3059	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
6	54	-0	-1617	0	0	0	-3202	--	--	16.08	16.08	0.29	0.06	0.01	0.10	0.00	0.00	20.9
7	54	-0	-1383	0	0	0	-2939	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
8	54	-0	-1617	0	0	0	-3215	--	--	16.08	16.08	0.29	0.06	0.01	0.10	0.00	0.00	20.9
9	54	-0	-1383	0	0	0	-2952	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
10	54	-0	-1535	0	0	0	-3095	--	--	16.08	16.08	0.29	0.05	0.01	0.10	0.00	0.00	20.9
11	54	-0	-1465	0	0	0	-3016	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
12	54	-0	-1535	0	0	0	-3138	--	--	16.08	16.08	0.29	0.05	0.01	0.10	0.00	0.00	20.9
13	54	-0	-1465	0	0	0	-3059	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
14	54	-0	-1617	0	0	0	-3202	--	--	16.08	16.08	0.29	0.06	0.01	0.10	0.00	0.00	20.9
15	54	-0	-1383	0	0	0	-2939	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
16	54	-0	-1617	0	0	0	-3215	--	--	16.08	16.08	0.29	0.06	0.01	0.10	0.00	0.00	20.9
17	54	-0	-1383	0	0	0	-2952	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
18	54	-0	-2419	0	0	0	-4583	--	--	16.08	16.08	0.18	0.08	0.02	0.15	0.00	0.00	20.9
19	54	-0	-2377	0	0	0	-4593	--	--	16.08	16.08	0.18	0.08	0.02	0.15	0.00	0.00	20.9
20	54	-0	-2540	0	0	0	-4813	--	--	16.08	16.08	0.18	0.08	0.02	0.16	0.00	0.00	20.9
37	54	-0	-2241	0	0	0	-4352	--	--	16.08	16.08	0.18	0.07	0.02	0.14	0.00	0.00	20.9
38	54	-0	-2171	0	0	0	-4368	--	--	16.08	16.08	0.18	0.07	0.02	0.14	0.00	0.00	20.9
39	54	-0	-2442	0	0	0	-4735	--	--	16.08	16.08	0.18	0.08	0.02	0.15	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 89 NI 1900 NF 1899 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-3763	0	0	0	-2955	--	--	16.08	16.08	0.18	0.05	0.03	0.24	0.00	0.00	20.9
2	0	-0	-2931	0	0	0	-2272	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
3	0	-0	-2854	0	0	0	-2231	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
4	0	-0	-2936	0	0	0	-2315	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
5	0	-0	-2859	0	0	0	-2274	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
6	0	-0	-3022	0	0	0	-2335	--	--	16.08	16.08	0.29	0.04	0.02	0.19	0.00	0.00	20.9
7	0	-0	-2766	0	0	0	-2198	--	--	16.08	16.08	0.29	0.04	0.02	0.17	0.00	0.00	20.9
8	0	-0	-3023	0	0	0	-2348	--	--	16.08	16.08	0.29	0.04	0.02	0.19	0.00	0.00	20.9
9	0	-0	-2768	0	0	0	-2211	--	--	16.08	16.08	0.29	0.04	0.02	0.17	0.00	0.00	20.9
10	0	-0	-2931	0	0	0	-2272	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
11	0	-0	-2854	0	0	0	-2231	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
12	0	-0	-2936	0	0	0	-2315	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
13	0	-0	-2859	0	0	0	-2274	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
14	0	-0	-3022	0	0	0	-2335	--	--	16.08	16.08	0.29	0.04	0.02	0.19	0.00	0.00	20.9
15	0	-0	-2766	0	0	0	-2198	--	--	16.08	16.08	0.29	0.04	0.02	0.17	0.00	0.00	20.9
16	0	-0	-3023	0	0	0	-2348	--	--	16.08	16.08	0.29	0.04	0.02	0.19	0.00	0.00	20.9
17	0	-0	-2768	0	0	0	-2211	--	--	16.08	16.08	0.29	0.04	0.02	0.17	0.00	0.00	20.9
18	0	-0	-4379	0	0	0	-3287	--	--	16.08	16.08	0.18	0.05	0.04	0.27	0.00	0.00	20.9
19	0	-0	-4338	0	0	0	-3320	--	--	16.08	16.08	0.18	0.06	0.04	0.27	0.00	0.00	20.9
20	0	-0	-4503	0	0	0	-3453	--	--	16.08	16.08	0.18	0.06	0.04	0.28	0.00	0.00	20.9
37	0	-0	-4135	0	0	0	-3151	--	--	16.08	16.08	0.18	0.05	0.03	0.26	0.00	0.00	20.9
38	0	-0	-4067	0	0	0	-3205	--	--	16.08	16.08	0.18	0.05	0.03	0.26	0.00	0.00	20.9
39	0	-0	-4340	0	0	0	-3427	--	--	16.08	16.08	0.18	0.06	0.04	0.27	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-3763	0	0	0	-2955	--	--	16.08	16.08	0.18	0.05	0.03	0.24	0.00	0.00	20.9
2	27	-0	-2931	0	0	0	-2272	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
3	27	-0	-2854	0	0	0	-2231	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
4	27	-0	-2936	0	0	0	-2315	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
5	27	-0	-2859	0	0	0	-2274	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
6	27	-0	-3022	0	0	0	-2335	--	--	16.08	16.08	0.29	0.04	0.02	0.19	0.00	0.00	20.9
7	27	-0	-2766	0	0	0	-2198	--	--	16.08	16.08	0.29	0.04	0.02	0.17	0.00	0.00	20.9
8	27	-0	-3023	0	0	0	-2348	--	--	16.08	16.08	0.29	0.04	0.02	0.19	0.00	0.00	20.9
9	27	-0	-2768	0	0	0	-2211	--	--	16.08	16.08	0.29	0.04	0.02	0.17	0.00	0.00	20.9
10	27	-0	-2931	0	0	0	-2272	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
11	27	-0	-2854	0	0	0	-2231	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
12	27	-0	-2936	0	0	0	-2315	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9

13	27	-0	-2859	0	0	0	-2274	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
14	27	-0	-3022	0	0	0	-2335	--	--	16.08	16.08	0.29	0.04	0.02	0.19	0.00	0.00	20.9
15	27	-0	-2766	0	0	0	-2198	--	--	16.08	16.08	0.29	0.04	0.02	0.17	0.00	0.00	20.9
16	27	-0	-3023	0	0	0	-2348	--	--	16.08	16.08	0.29	0.04	0.02	0.19	0.00	0.00	20.9
17	27	-0	-2768	0	0	0	-2211	--	--	16.08	16.08	0.29	0.04	0.02	0.17	0.00	0.00	20.9
18	27	-0	-4379	0	0	0	-3287	--	--	16.08	16.08	0.18	0.05	0.04	0.27	0.00	0.00	20.9
19	27	-0	-4338	0	0	0	-3320	--	--	16.08	16.08	0.18	0.06	0.04	0.27	0.00	0.00	20.9
20	27	-0	-4503	0	0	0	-3453	--	--	16.08	16.08	0.18	0.06	0.04	0.28	0.00	0.00	20.9
37	27	-0	-4135	0	0	0	-3151	--	--	16.08	16.08	0.18	0.05	0.03	0.26	0.00	0.00	20.9
38	27	-0	-4067	0	0	0	-3205	--	--	16.08	16.08	0.18	0.05	0.03	0.26	0.00	0.00	20.9
39	27	-0	-4340	0	0	0	-3427	--	--	16.08	16.08	0.18	0.06	0.04	0.27	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	54	-0	-3763	0	0	0	-2955	--	--	16.08	16.08	0.18	0.05	0.03	0.24	0.00	0.00	20.9
2	54	-0	-2931	0	0	0	-2272	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
3	54	-0	-2854	0	0	0	-2231	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
4	54	-0	-2936	0	0	0	-2315	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
5	54	-0	-2859	0	0	0	-2274	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
6	54	-0	-3022	0	0	0	-2335	--	--	16.08	16.08	0.29	0.04	0.02	0.19	0.00	0.00	20.9
7	54	-0	-2766	0	0	0	-2198	--	--	16.08	16.08	0.29	0.04	0.02	0.17	0.00	0.00	20.9
8	54	-0	-3023	0	0	0	-2348	--	--	16.08	16.08	0.29	0.04	0.02	0.19	0.00	0.00	20.9
9	54	-0	-2768	0	0	0	-2211	--	--	16.08	16.08	0.29	0.04	0.02	0.17	0.00	0.00	20.9
10	54	-0	-2931	0	0	0	-2272	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
11	54	-0	-2854	0	0	0	-2231	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
12	54	-0	-2936	0	0	0	-2315	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
13	54	-0	-2859	0	0	0	-2274	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
14	54	-0	-3022	0	0	0	-2335	--	--	16.08	16.08	0.29	0.04	0.02	0.19	0.00	0.00	20.9
15	54	-0	-2766	0	0	0	-2198	--	--	16.08	16.08	0.29	0.04	0.02	0.17	0.00	0.00	20.9
16	54	-0	-3023	0	0	0	-2348	--	--	16.08	16.08	0.29	0.04	0.02	0.19	0.00	0.00	20.9
17	54	-0	-2768	0	0	0	-2211	--	--	16.08	16.08	0.29	0.04	0.02	0.17	0.00	0.00	20.9
18	54	-0	-4379	0	0	0	-3287	--	--	16.08	16.08	0.18	0.05	0.04	0.27	0.00	0.00	20.9
19	54	-0	-4338	0	0	0	-3320	--	--	16.08	16.08	0.18	0.06	0.04	0.27	0.00	0.00	20.9
20	54	-0	-4503	0	0	0	-3453	--	--	16.08	16.08	0.18	0.06	0.04	0.28	0.00	0.00	20.9
37	54	-0	-4135	0	0	0	-3151	--	--	16.08	16.08	0.18	0.05	0.03	0.26	0.00	0.00	20.9
38	54	-0	-4067	0	0	0	-3205	--	--	16.08	16.08	0.18	0.05	0.03	0.26	0.00	0.00	20.9
39	54	-0	-4340	0	0	0	-3427	--	--	16.08	16.08	0.18	0.06	0.04	0.27	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 90 NI 1891 NF 1900 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--	--	--	--	--	--	--	--	--	--	--		--	--	--	--	--	--
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-5713	0	0	0	2121	--	--	16.08	16.08	0.00	0.04	0.05	0.36	0.00	0.00	20.9
2	0	-0	-4430	0	0	0	1671	--	--	16.08	16.08	0.10	0.03	0.04	0.28	0.00	0.00	20.9
3	0	-0	-4347	0	0	0	1626	--	--	16.08	16.08	0.10	0.03	0.04	0.27	0.00	0.00	20.9
4	0	-0	-4442	0	0	0	1637	--	--	16.08	16.08	0.10	0.03	0.04	0.28	0.00	0.00	20.9
5	0	-0	-4359	0	0	0	1592	--	--	16.08	16.08	0.10	0.03	0.04	0.27	0.00	0.00	20.9
6	0	-0	-4532	0	0	0	1711	--	--	16.08	16.08	0.10	0.03	0.04	0.28	0.00	0.00	20.9
7	0	-0	-4254	0	0	0	1562	--	--	16.08	16.08	0.10	0.03	0.04	0.27	0.00	0.00	20.9
8	0	-0	-4535	0	0	0	1701	--	--	16.08	16.08	0.10	0.03	0.04	0.28	0.00	0.00	20.9
9	0	-0	-4257	0	0	0	1552	--	--	16.08	16.08	0.10	0.03	0.04	0.27	0.00	0.00	20.9
10	0	-0	-4430	0	0	0	1671	--	--	16.08	16.08	0.10	0.03	0.04	0.28	0.00	0.00	20.9
11	0	-0	-4347	0	0	0	1626	--	--	16.08	16.08	0.10	0.03	0.04	0.27	0.00	0.00	20.9
12	0	-0	-4442	0	0	0	1637	--	--	16.08	16.08	0.10	0.03	0.04	0.28	0.00	0.00	20.9
13	0	-0	-4359	0	0	0	1592	--	--	16.08	16.08	0.10	0.03	0.04	0.27	0.00	0.00	20.9
14	0	-0	-4532	0	0	0	1711	--	--	16.08	16.08	0.10	0.03	0.04	0.28	0.00	0.00	20.9
15	0	-0	-4254	0	0	0	1562	--	--	16.08	16.08	0.10	0.03	0.04	0.27	0.00	0.00	20.9
16	0	-0	-4535	0	0	0	1701	--	--	16.08	16.08	0.10	0.03	0.04	0.28	0.00	0.00	20.9
17	0	-0	-4257	0	0	0	1552	--	--	16.08	16.08	0.10	0.03	0.04	0.27	0.00	0.00	20.9
18	0	-0	-6503	0	0	0	2543	--	--	16.08	16.08	0.00	0.04	0.05	0.41	0.00	0.00	20.9
19	0	-0	-6461	0	0	0	2466	--	--	16.08	16.08	0.00	0.04	0.05	0.41	0.00	0.00	20.9
20	0	-0	-6622	0	0	0	2507	--	--	16.08	16.08	0.00	0.04	0.05	0.42	0.00	0.00	20.9
37	0	-0	-6181	0	0	0	2376	--	--	16.08	16.08	0.00	0.04	0.05	0.39	0.00	0.00	20.9
38	0	-0	-6112	0	0	0	2248	--	--	16.08	16.08	0.00	0.04	0.05	0.38	0.00	0.00	20.9
39	0	-0	-6381	0	0	0	2317	--	--	16.08	16.08	0.00	0.04	0.05	0.40	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-5713	0	0	0	2121	--	--	16.08	16.08	0.00	0.04	0.05	0.36	0.00	0.00	20.9
2	27	-0	-4430	0	0	0	1671	--	--	16.08	16.08	0.10	0.03	0.04	0.28	0.00	0.00	20.9
3	27	-0	-4347	0	0	0	1626	--	--	16.08	16.08	0.10	0.03	0.04	0.27	0.00	0.00	20.9
4	27	-0	-4442	0	0	0	1637	--	--	16.08	16.08	0.10	0.03	0.04	0.28	0.00	0.00	20.9
5	27	-0	-4359	0	0	0	1592	--	--	16.08	16.08	0.10	0.03	0.04	0.27	0.00	0.00	20.9
6	27	-0	-4532	0	0	0	1711	--	--	16.08	16.08	0.10	0.03	0.04	0.28	0.00	0.00	20.9
7	27	-0	-4254	0	0	0	1562	--	--	16.08	16.08	0.10	0.03	0.04	0.27	0.00	0.00	20.9
8	27	-0	-4535	0	0	0	1701	--	--	16.08	16.08	0.10	0.03	0.04	0.28	0.00	0.00	20.9
9	27	-0	-4257	0	0	0	1552	--	--	16.08	16.08	0.10	0.03	0.04	0.27	0.00	0.00	20.9
10	27	-0	-4430	0	0	0	1671	--	--	16.08	16.08	0.10	0.03	0.04	0.28	0.00	0.00	20.9
11	27	-0	-4347	0	0	0	1626	--	--	16.08	16.08	0.10	0.03	0.04	0.27	0.00	0.00	20.9
12	27	-0	-4442	0	0	0	1637	--	--	16.08	16.08	0.10	0.03	0.04	0.28	0.00	0.00	20.9
13	27	-0	-4359	0	0	0	1592	--	--	16.08	16.08	0.10	0.03	0.04	0.27	0.00	0.00	20.9
14	27	-0	-4532	0	0	0	1711	--	--	16.08	16.08	0.10	0.03	0.04	0.28	0.00	0.00	20.9
15	27	-0	-4254	0	0	0	1562	--	--	16.08	16.08	0.10	0.03	0.04	0.27	0.00	0.00	20.9
16	27	-0	-4535	0	0	0	1701	--	--	16.08	16.08	0.10	0.03	0.04	0.28	0.00	0.00	20.9
17	27	-0	-4257	0	0	0	1552	--	--	16.08	16.08	0.10	0.03	0.04	0.27	0.00	0.00	20.9
18	27	-0	-6503	0	0	0	2543	--	--	16.08	16.08	0.00	0.04	0.05	0.41	0.00	0.00	20.9
19	27	-0	-6461	0	0	0	2466	--	--	16.08	16.08	0.00	0.04	0.05	0.41	0.00	0.00	20.9
20	27	-0	-6622	0	0	0	2507	--	--	16.08	16.08	0.00	0.04	0.05	0.42	0.00	0.00	20.9
37	27	-0	-6181	0	0	0	2376	--	--	16.08	16.08	0.00	0.04	0.05	0.39	0.00	0.00	20.9
38	27	-0	-6112	0	0	0	2248	--	--	16.08	16.08	0.00	0.04	0.05	0.38	0.00	0.00	20.9
39	27	-0	-6381	0	0	0	2317	--	--	16.08	16.08	0.00	0.04	0.05	0.40	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	54	-0	-5713	0	0	0	-939	--	--	16.08	16.08	0.18	0.02	0.05	0.36	0.00	0.00	20.9
2	54	-0	-4430	0	0	0	-702	--	--	16.08	16.08	0.29	0.01	0.04	0.28	0.00	0.00	20.9
3	54	-0	-4347	0	0	0	-702	--	--	16.08	16.08	0.29	0.01	0.04	0.27	0.00	0.00	20.9
4	54	-0	-4442	0	0	0	-743	--	--	16.08	16.08	0.29	0.01	0.04	0.28	0.00	0.00	20.9
5	54	-0	-4359	0	0	0	-743	--	--	16.08	16.08	0.29	0.01	0.04	0.27	0.00	0.00	20.9
6	54	-0	-4532	0	0	0	-716	--	--	16.08	16.08	0.29	0.01	0.04	0.28	0.00	0.00	20.9
7	54	-0	-4254	0	0	0	-716	--	--	16.08	16.08	0.29	0.01	0.04	0.27	0.00	0.00	20.9
8	54	-0	-4535	0	0	0	-728	--	--	16.08	16.08	0.29	0.01	0.04	0.28	0.00	0.00	20.9

9	54	-0	-4257	0	0	0	-729	--	--	16.08	16.08	0.29	0.01	0.04	0.27	0.00	0.00	20.9
10	54	-0	-4430	0	0	0	-702	--	--	16.08	16.08	0.29	0.01	0.04	0.28	0.00	0.00	20.9
11	54	-0	-4347	0	0	0	-702	--	--	16.08	16.08	0.29	0.01	0.04	0.27	0.00	0.00	20.9
12	54	-0	-4442	0	0	0	-743	--	--	16.08	16.08	0.29	0.01	0.04	0.28	0.00	0.00	20.9
13	54	-0	-4359	0	0	0	-743	--	--	16.08	16.08	0.29	0.01	0.04	0.27	0.00	0.00	20.9
14	54	-0	-4532	0	0	0	-716	--	--	16.08	16.08	0.29	0.01	0.04	0.28	0.00	0.00	20.9
15	54	-0	-4254	0	0	0	-716	--	--	16.08	16.08	0.29	0.01	0.04	0.27	0.00	0.00	20.9
16	54	-0	-4535	0	0	0	-728	--	--	16.08	16.08	0.29	0.01	0.04	0.28	0.00	0.00	20.9
17	54	-0	-4257	0	0	0	-729	--	--	16.08	16.08	0.29	0.01	0.04	0.27	0.00	0.00	20.9
18	54	-0	-6503	0	0	0	-941	--	--	16.08	16.08	0.18	0.02	0.05	0.41	0.00	0.00	20.9
19	54	-0	-6461	0	0	0	-995	--	--	16.08	16.08	0.18	0.02	0.05	0.41	0.00	0.00	20.9
20	54	-0	-6622	0	0	0	-1040	--	--	16.08	16.08	0.18	0.02	0.05	0.42	0.00	0.00	20.9
37	54	-0	-6181	0	0	0	-936	--	--	16.08	16.08	0.18	0.02	0.05	0.39	0.00	0.00	20.9
38	54	-0	-6112	0	0	0	-1026	--	--	16.08	16.08	0.18	0.02	0.05	0.38	0.00	0.00	20.9
39	54	-0	-6381	0	0	0	-1102	--	--	16.08	16.08	0.18	0.02	0.05	0.40	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 91 NI 1892 NF 1891 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-7809	0	0	0	6304	--	--	16.08	16.08	0.00	0.11	0.06	0.49	0.00	0.00	20.9
2	0	-0	-6042	0	0	0	4908	--	--	16.08	16.08	0.10	0.09	0.05	0.38	0.00	0.00	20.9
3	0	-0	-5952	0	0	0	4815	--	--	16.08	16.08	0.10	0.09	0.05	0.37	0.00	0.00	20.9
4	0	-0	-6062	0	0	0	4884	--	--	16.08	16.08	0.10	0.09	0.05	0.38	0.00	0.00	20.9
5	0	-0	-5972	0	0	0	4791	--	--	16.08	16.08	0.10	0.09	0.05	0.37	0.00	0.00	20.9
6	0	-0	-6154	0	0	0	5008	--	--	16.08	16.08	0.10	0.09	0.05	0.39	0.00	0.00	20.9
7	0	-0	-5854	0	0	0	4698	--	--	16.08	16.08	0.10	0.08	0.05	0.37	0.00	0.00	20.9
8	0	-0	-6160	0	0	0	5001	--	--	16.08	16.08	0.10	0.09	0.05	0.39	0.00	0.00	20.9
9	0	-0	-5860	0	0	0	4691	--	--	16.08	16.08	0.10	0.08	0.05	0.37	0.00	0.00	20.9
10	0	-0	-6042	0	0	0	4908	--	--	16.08	16.08	0.10	0.09	0.05	0.38	0.00	0.00	20.9
11	0	-0	-5952	0	0	0	4815	--	--	16.08	16.08	0.10	0.09	0.05	0.37	0.00	0.00	20.9
12	0	-0	-6062	0	0	0	4884	--	--	16.08	16.08	0.10	0.09	0.05	0.38	0.00	0.00	20.9
13	0	-0	-5972	0	0	0	4791	--	--	16.08	16.08	0.10	0.09	0.05	0.37	0.00	0.00	20.9
14	0	-0	-6154	0	0	0	5008	--	--	16.08	16.08	0.10	0.09	0.05	0.39	0.00	0.00	20.9
15	0	-0	-5854	0	0	0	4698	--	--	16.08	16.08	0.10	0.08	0.05	0.37	0.00	0.00	20.9
16	0	-0	-6160	0	0	0	5001	--	--	16.08	16.08	0.10	0.09	0.05	0.39	0.00	0.00	20.9
17	0	-0	-5860	0	0	0	4691	--	--	16.08	16.08	0.10	0.08	0.05	0.37	0.00	0.00	20.9
18	0	-0	-8798	0	0	0	7256	--	--	16.08	16.08	0.00	0.12	0.07	0.55	0.00	0.00	20.9
19	0	-0	-8756	0	0	0	7157	--	--	16.08	16.08	0.00	0.12	0.07	0.55	0.00	0.00	20.9
20	0	-0	-8909	0	0	0	7280	--	--	16.08	16.08	0.00	0.12	0.07	0.56	0.00	0.00	20.9
37	0	-0	-8390	0	0	0	6870	--	--	16.08	16.08	0.00	0.12	0.07	0.53	0.00	0.00	20.9
38	0	-0	-8319	0	0	0	6704	--	--	16.08	16.08	0.00	0.11	0.07	0.52	0.00	0.00	20.9
39	0	-0	-8575	0	0	0	6910	--	--	16.08	16.08	0.00	0.12	0.07	0.54	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-7809	0	0	0	6304	--	--	16.08	16.08	0.00	0.11	0.06	0.49	0.00	0.00	20.9
2	27	-0	-6042	0	0	0	4908	--	--	16.08	16.08	0.10	0.09	0.05	0.38	0.00	0.00	20.9
3	27	-0	-5952	0	0	0	4815	--	--	16.08	16.08	0.10	0.09	0.05	0.37	0.00	0.00	20.9
4	27	-0	-6062	0	0	0	4884	--	--	16.08	16.08	0.10	0.09	0.05	0.38	0.00	0.00	20.9
5	27	-0	-5972	0	0	0	4791	--	--	16.08	16.08	0.10	0.09	0.05	0.37	0.00	0.00	20.9
6	27	-0	-6154	0	0	0	5008	--	--	16.08	16.08	0.10	0.09	0.05	0.39	0.00	0.00	20.9
7	27	-0	-5854	0	0	0	4698	--	--	16.08	16.08	0.10	0.08	0.05	0.37	0.00	0.00	20.9
8	27	-0	-6160	0	0	0	5001	--	--	16.08	16.08	0.10	0.09	0.05	0.39	0.00	0.00	20.9
9	27	-0	-5860	0	0	0	4691	--	--	16.08	16.08	0.10	0.08	0.05	0.37	0.00	0.00	20.9
10	27	-0	-6042	0	0	0	4908	--	--	16.08	16.08	0.10	0.09	0.05	0.38	0.00	0.00	20.9
11	27	-0	-5952	0	0	0	4815	--	--	16.08	16.08	0.10	0.09	0.05	0.37	0.00	0.00	20.9
12	27	-0	-6062	0	0	0	4884	--	--	16.08	16.08	0.10	0.09	0.05	0.38	0.00	0.00	20.9
13	27	-0	-5972	0	0	0	4791	--	--	16.08	16.08	0.10	0.09	0.05	0.37	0.00	0.00	20.9
14	27	-0	-6154	0	0	0	5008	--	--	16.08	16.08	0.10	0.09	0.05	0.39	0.00	0.00	20.9
15	27	-0	-5854	0	0	0	4698	--	--	16.08	16.08	0.10	0.08	0.05	0.37	0.00	0.00	20.9
16	27	-0	-6160	0	0	0	5001	--	--	16.08	16.08	0.10	0.09	0.05	0.39	0.00	0.00	20.9
17	27	-0	-5860	0	0	0	4691	--	--	16.08	16.08	0.10	0.08	0.05	0.37	0.00	0.00	20.9
18	27	-0	-8798	0	0	0	7256	--	--	16.08	16.08	0.00	0.12	0.07	0.55	0.00	0.00	20.9
19	27	-0	-8756	0	0	0	7157	--	--	16.08	16.08	0.00	0.12	0.07	0.55	0.00	0.00	20.9
20	27	-0	-8909	0	0	0	7280	--	--	16.08	16.08	0.00	0.12	0.07	0.56	0.00	0.00	20.9
37	27	-0	-8390	0	0	0	6870	--	--	16.08	16.08	0.00	0.12	0.07	0.53	0.00	0.00	20.9
38	27	-0	-8319	0	0	0	6704	--	--	16.08	16.08	0.00	0.11	0.07	0.52	0.00	0.00	20.9
39	27	-0	-8575	0	0	0	6910	--	--	16.08	16.08	0.00	0.12	0.07	0.54	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	54	-0	-7809	0	0	0	2121	--	--	16.08	16.08	0.00	0.04	0.06	0.49	0.00	0.00	20.9
2	54	-0	-6042	0	0	0	1671	--	--	16.08	16.08	0.10	0.03	0.05	0.38	0.00	0.00	20.9
3	54	-0	-5952	0	0	0	1626	--	--	16.08	16.08	0.10	0.03	0.05	0.37	0.00	0.00	20.9
4	54	-0	-6062	0	0	0	1637	--	--	16.08	16.08	0.10	0.03	0.05	0.38	0.00	0.00	20.9
5	54	-0	-5972	0	0	0	1592	--	--	16.08	16.08	0.10	0.03	0.05	0.37	0.00	0.00	20.9
6	54	-0	-6154	0	0	0	1711	--	--	16.08	16.08	0.10	0.03	0.05	0.39	0.00	0.00	20.9
7	54	-0	-5854	0	0	0	1562	--	--	16.08	16.08	0.10	0.03	0.05	0.37	0.00	0.00	20.9
8	54	-0	-6160	0	0	0	1701	--	--	16.08	16.08	0.10	0.03	0.05	0.39	0.00	0.00	20.9
9	54	-0	-5860	0	0	0	1552	--	--	16.08	16.08	0.10	0.03	0.05	0.37	0.00	0.00	20.9
10	54	-0	-6042	0	0	0	1671	--	--	16.08	16.08	0.10	0.03	0.05	0.38	0.00	0.00	20.9
11	54	-0	-5952	0	0	0	1626	--	--	16.08	16.08	0.10	0.03	0.05	0.37	0.00	0.00	20.9
12	54	-0	-6062	0	0	0	1637	--	--	16.08	16.08	0.10	0.03	0.05	0.38	0.00	0.00	20.9
13	54	-0	-5972	0	0	0	1592	--	--	16.08	16.08	0.10	0.03	0.05	0.37	0.00	0.00	20.9
14	54	-0	-6154	0	0	0	1711	--	--	16.08	16.08	0.10	0.03	0.05	0.39	0.00	0.00	20.9
15	54	-0	-5854	0	0	0	1562	--	--	16.08	16.08	0.10	0.03	0.05	0.37	0.00	0.00	20.9
16	54	-0	-6160	0	0	0	1701	--	--	16.08	16.08	0.10	0.03	0.05	0.39	0.00	0.00	20.9
17	54	-0	-5860	0	0	0	1552	--	--	16.08	16.08	0.10	0.03	0.05	0.37	0.00	0.00	20.9
18	54	-0	-8798	0	0	0	2543	--	--	16.08	16.08	0.00	0.04	0.07	0.55	0.00	0.00	20.9
19	54	-0	-8756	0	0	0	2466	--	--	16.08	16.08	0.00	0.04	0.07	0.55	0.00	0.00	20.9
20	54	-0	-8909	0	0	0	2507	--	--	16.08	16.08	0.00	0.04	0.07	0.56	0.00	0.00	20.9
37	54	-0	-8390	0	0	0	2376	--	--	16.08	16.08	0.00	0.04	0.07	0.53	0.00	0.00	20.9
38	54	-0	-8319	0	0	0	2248	--	--	16.08	16.08	0.00	0.04	0.07	0.52	0.00	0.00	20.9
39	54	-0	-8575	0	0	0	2317	--	--	16.08	16.08	0.00	0.04	0.07	0.54	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 92 NI 1908 NF 1892 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m			cm
1	0	-0	-10050	0	0	0	11690	--	--	16.08	16.08	0.00	0.20	0.08	0.63	0.00	0.00	20.9
2	0	-0	-7761	0	0	0	9065	--	--	16.08	16.08	0.10	0.16	0.06	0.49	0.00	0.00	20.9
3	0	-0	-7664	0	0	0	8920	--	--	16.08	16.08	0.10	0.16	0.06	0.48	0.00	0.00	20.9
4	0	-0	-7791	0	0	0	9058	--	--	16.08	16.08	0.10	0.16	0.06	0.49	0.00	0.00	20.9
5	0	-0	-7694	0	0	0	8913	--	--	16.08	16.08	0.10	0.16	0.06	0.48	0.00	0.00	20.9
6	0	-0	-7884	0	0	0	9232	--	--	16.08	16.08	0.10	0.16	0.06	0.49	0.00	0.00	20.9
7	0	-0	-7561	0	0	0	8749	--	--	16.08	16.08	0.10	0.16	0.06	0.47	0.00	0.00	20.9
8	0	-0	-7893	0	0	0	9229	--	--	16.08	16.08	0.10	0.16	0.07	0.50	0.00	0.00	20.9
9	0	-0	-7570	0	0	0	8746	--	--	16.08	16.08	0.10	0.16	0.06	0.47	0.00	0.00	20.9
10	0	-0	-7761	0	0	0	9065	--	--	16.08	16.08	0.10	0.16	0.06	0.49	0.00	0.00	20.9
11	0	-0	-7664	0	0	0	8920	--	--	16.08	16.08	0.10	0.16	0.06	0.48	0.00	0.00	20.9
12	0	-0	-7791	0	0	0	9058	--	--	16.08	16.08	0.10	0.16	0.06	0.49	0.00	0.00	20.9
13	0	-0	-7694	0	0	0	8913	--	--	16.08	16.08	0.10	0.16	0.06	0.48	0.00	0.00	20.9
14	0	-0	-7884	0	0	0	9232	--	--	16.08	16.08	0.10	0.16	0.06	0.49	0.00	0.00	20.9
15	0	-0	-7561	0	0	0	8749	--	--	16.08	16.08	0.10	0.16	0.06	0.47	0.00	0.00	20.9
16	0	-0	-7893	0	0	0	9229	--	--	16.08	16.08	0.10	0.16	0.07	0.50	0.00	0.00	20.9
17	0	-0	-7570	0	0	0	8746	--	--	16.08	16.08	0.10	0.16	0.06	0.47	0.00	0.00	20.9
18	0	-0	-11260	0	0	0	13290	--	--	16.08	16.08	0.00	0.23	0.09	0.71	0.00	0.00	20.9
19	0	-0	-11210	0	0	0	13160	--	--	16.08	16.08	0.00	0.22	0.09	0.70	0.00	0.00	20.9
20	0	-0	-11360	0	0	0	13360	--	--	16.08	16.08	0.00	0.23	0.09	0.71	0.00	0.00	20.9
37	0	-0	-10750	0	0	0	12630	--	--	16.08	16.08	0.00	0.22	0.09	0.67	0.00	0.00	20.9
38	0	-0	-10680	0	0	0	12430	--	--	16.08	16.08	0.00	0.21	0.09	0.67	0.00	0.00	20.9
39	0	-0	-10920	0	0	0	12760	--	--	16.08	16.08	0.00	0.22	0.09	0.69	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-10050	0	0	0	11690	--	--	16.08	16.08	0.00	0.20	0.08	0.63	0.00	0.00	20.9
2	27	-0	-7761	0	0	0	9065	--	--	16.08	16.08	0.10	0.16	0.06	0.49	0.00	0.00	20.9
3	27	-0	-7664	0	0	0	8920	--	--	16.08	16.08	0.10	0.16	0.06	0.48	0.00	0.00	20.9
4	27	-0	-7791	0	0	0	9058	--	--	16.08	16.08	0.10	0.16	0.06	0.49	0.00	0.00	20.9
5	27	-0	-7694	0	0	0	8913	--	--	16.08	16.08	0.10	0.16	0.06	0.48	0.00	0.00	20.9
6	27	-0	-7884	0	0	0	9232	--	--	16.08	16.08	0.10	0.16	0.06	0.49	0.00	0.00	20.9
7	27	-0	-7561	0	0	0	8749	--	--	16.08	16.08	0.10	0.16	0.06	0.47	0.00	0.00	20.9
8	27	-0	-7893	0	0	0	9229	--	--	16.08	16.08	0.10	0.16	0.07	0.50	0.00	0.00	20.9
9	27	-0	-7570	0	0	0	8746	--	--	16.08	16.08	0.10	0.16	0.06	0.47	0.00	0.00	20.9
10	27	-0	-7761	0	0	0	9065	--	--	16.08	16.08	0.10	0.16	0.06	0.49	0.00	0.00	20.9
11	27	-0	-7664	0	0	0	8920	--	--	16.08	16.08	0.10	0.16	0.06	0.48	0.00	0.00	20.9
12	27	-0	-7791	0	0	0	9058	--	--	16.08	16.08	0.10	0.16	0.06	0.49	0.00	0.00	20.9
13	27	-0	-7694	0	0	0	8913	--	--	16.08	16.08	0.10	0.16	0.06	0.48	0.00	0.00	20.9
14	27	-0	-7884	0	0	0	9232	--	--	16.08	16.08	0.10	0.16	0.06	0.49	0.00	0.00	20.9
15	27	-0	-7561	0	0	0	8749	--	--	16.08	16.08	0.10	0.16	0.06	0.47	0.00	0.00	20.9
16	27	-0	-7893	0	0	0	9229	--	--	16.08	16.08	0.10	0.16	0.07	0.50	0.00	0.00	20.9
17	27	-0	-7570	0	0	0	8746	--	--	16.08	16.08	0.10	0.16	0.06	0.47	0.00	0.00	20.9
18	27	-0	-11260	0	0	0	13290	--	--	16.08	16.08	0.00	0.23	0.09	0.71	0.00	0.00	20.9
19	27	-0	-11210	0	0	0	13160	--	--	16.08	16.08	0.00	0.22	0.09	0.70	0.00	0.00	20.9
20	27	-0	-11360	0	0	0	13360	--	--	16.08	16.08	0.00	0.23	0.09	0.71	0.00	0.00	20.9
37	27	-0	-10750	0	0	0	12630	--	--	16.08	16.08	0.00	0.22	0.09	0.67	0.00	0.00	20.9
38	27	-0	-10680	0	0	0	12430	--	--	16.08	16.08	0.00	0.21	0.09	0.67	0.00	0.00	20.9
39	27	-0	-10920	0	0	0	12760	--	--	16.08	16.08	0.00	0.22	0.09	0.69	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	54	-0	-10050	0	0	0	6304	--	--	16.08	16.08	0.00	0.11	0.08	0.63	0.00	0.00	20.9
2	54	-0	-7761	0	0	0	4908	--	--	16.08	16.08	0.10	0.09	0.06	0.49	0.00	0.00	20.9
3	54	-0	-7664	0	0	0	4815	--	--	16.08	16.08	0.10	0.09	0.06	0.48	0.00	0.00	20.9
4	54	-0	-7791	0	0	0	4884	--	--	16.08	16.08	0.10	0.09	0.06	0.49	0.00	0.00	20.9
5	54	-0	-7694	0	0	0	4791	--	--	16.08	16.08	0.10	0.09	0.06	0.48	0.00	0.00	20.9
6	54	-0	-7884	0	0	0	5008	--	--	16.08	16.08	0.10	0.09	0.06	0.49	0.00	0.00	20.9
7	54	-0	-7561	0	0	0	4698	--	--	16.08	16.08	0.10	0.08	0.06	0.47	0.00	0.00	20.9
8	54	-0	-7893	0	0	0	5001	--	--	16.08	16.08	0.10	0.09	0.07	0.50	0.00	0.00	20.9
9	54	-0	-7570	0	0	0	4691	--	--	16.08	16.08	0.10	0.08	0.06	0.47	0.00	0.00	20.9
10	54	-0	-7761	0	0	0	4908	--	--	16.08	16.08	0.10	0.09	0.06	0.49	0.00	0.00	20.9
11	54	-0	-7664	0	0	0	4815	--	--	16.08	16.08	0.10	0.09	0.06	0.48	0.00	0.00	20.9
12	54	-0	-7791	0	0	0	4884	--	--	16.08	16.08	0.10	0.09	0.06	0.49	0.00	0.00	20.9
13	54	-0	-7694	0	0	0	4791	--	--	16.08	16.08	0.10	0.09	0.06	0.48	0.00	0.00	20.9
14	54	-0	-7884	0	0	0	5008	--	--	16.08	16.08	0.10	0.09	0.06	0.49	0.00	0.00	20.9
15	54	-0	-7561	0	0	0	4698	--	--	16.08	16.08	0.10	0.08	0.06	0.47	0.00	0.00	20.9
16	54	-0	-7893	0	0	0	5001	--	--	16.08	16.08	0.10	0.09	0.07	0.50	0.00	0.00	20.9
17	54	-0	-7570	0	0	0	4691	--	--	16.08	16.08	0.10	0.08	0.06	0.47	0.00	0.00	20.9
18	54	-0	-11260	0	0	0	7256	--	--	16.08	16.08	0.00	0.12	0.09	0.71	0.00	0.00	20.9
19	54	-0	-11210	0	0	0	7157	--	--	16.08	16.08	0.00	0.12	0.09	0.70	0.00	0.00	20.9
20	54	-0	-11360	0	0	0	7280	--	--	16.08	16.08	0.00	0.12	0.09	0.71	0.00	0.00	20.9
37	54	-0	-10750	0	0	0	6870	--	--	16.08	16.08	0.00	0.12	0.09	0.67	0.00	0.00	20.9
38	54	-0	-10680	0	0	0	6704	--	--	16.08	16.08	0.00	0.11	0.09	0.67	0.00	0.00	20.9
39	54	-0	-10920	0	0	0	6910	--	--	16.08	16.08	0.00	0.12	0.09	0.69	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 93 NI 1904 NF 1908 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m			cm
1	0	-0	7609	0	0	0	6451	--	--	16.08	16.08	0.00	0.11	0.06	0.48	0.00	0.00	20.9
2	0	-0	5855	0	0	0	4947	--	--	16.08	16.08	0.10	0.09	0.05	0.37	0.00	0.00	20.9
3	0	-0	5878	0	0	0	4997	--	--	16.08	16.08	0.10	0.09	0.05	0.37	0.00	0.00	20.9
4	0	-0	5829	0	0	0	4927	--	--	16.08	16.08	0.10	0.09	0.05	0.37	0.00	0.00	20.9
5	0	-0	5851	0	0	0	4977	--	--	16.08	16.08	0.10	0.09	0.05	0.37	0.00	0.00	20.9
6	0	-0	5820	0	0	0	4881	--	--	16.08	16.08	0.10	0.09	0.05	0.37	0.00	0.00	20.9
7	0	-0	5895	0	0	0	5049	--	--	16.08	16.08	0.10	0.09	0.05	0.37	0.00	0.00	20.9
8	0	-0	5812	0	0	0	4875	--	--	16.08	16.08	0.10	0.09	0.05	0.36	0.00	0.00	20.9
9	0	-0	5887	0	0	0	5043	--	--	16.08	16.08	0.10	0.09	0.05	0.37	0.00	0.00	20.9
10	0	-0	5855	0	0	0	4947	--	--	16.08	16.08	0.10	0.09	0.05	0.37	0.00	0.00	20.9
11	0	-0	5878	0	0	0	4997	--	--	16.08	16.08	0.10	0.09	0.05	0.37	0.00	0.00	20.9
12	0	-0	5829	0	0	0	4927	--	--	16.08	16.08	0.10	0.09	0.05	0.37	0.00	0.00	20.9
13	0	-0	5851	0	0	0	4977	--	--	16.08	16.08	0.10	0.09	0.05	0.37	0.00	0.00	20.9
14	0	-0	5820	0	0	0	4881	--	--	16.08	16.08	0.10	0.09	0.05	0.37	0.00	0.00	20.9
15	0	-0	5895	0	0	0	5049	--	--	16.08	16.08	0.10	0.09	0.05	0.37	0.00	0.00	20.9
16	0	-0	5812	0	0	0	4875	--	--	16.08	16.08	0.10	0.09	0.05	0.36	0.00	0.00	20.9

17	0	-0	5887	0	0	0	5043	--	--	16.08	16.08	0.10	0.09	0.05	0.37	0.00	0.00	20.9
18	0	-0	8064	0	0	0	6906	--	--	16.08	16.08	0.00	0.12	0.07	0.51	0.00	0.00	20.9
19	0	-0	8064	0	0	0	6938	--	--	16.08	16.08	0.00	0.12	0.07	0.51	0.00	0.00	20.9
20	0	-0	7851	0	0	0	6655	--	--	16.08	16.08	0.00	0.11	0.06	0.49	0.00	0.00	20.9
37	0	-0	7793	0	0	0	6608	--	--	16.08	16.08	0.00	0.11	0.06	0.49	0.00	0.00	20.9
38	0	-0	7793	0	0	0	6662	--	--	16.08	16.08	0.00	0.11	0.06	0.49	0.00	0.00	20.9
39	0	-0	7437	0	0	0	6190	--	--	16.08	16.08	0.00	0.11	0.06	0.47	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	7609	0	0	0	16623	--	--	16.08	16.08	0.00	0.28	0.06	0.48	0.00	0.00	20.9
2	27	-0	5855	0	0	0	12773	--	--	16.08	16.08	0.10	0.23	0.05	0.37	0.00	0.00	20.9
3	27	-0	5878	0	0	0	12854	--	--	16.08	16.08	0.10	0.23	0.05	0.37	0.00	0.00	20.9
4	27	-0	5829	0	0	0	12718	--	--	16.08	16.08	0.10	0.23	0.05	0.37	0.00	0.00	20.9
5	27	-0	5851	0	0	0	12798	--	--	16.08	16.08	0.10	0.23	0.05	0.37	0.00	0.00	20.9
6	27	-0	5820	0	0	0	12660	--	--	16.08	16.08	0.10	0.22	0.05	0.37	0.00	0.00	20.9
7	27	-0	5895	0	0	0	12928	--	--	16.08	16.08	0.10	0.23	0.05	0.37	0.00	0.00	20.9
8	27	-0	5812	0	0	0	12644	--	--	16.08	16.08	0.10	0.22	0.05	0.36	0.00	0.00	20.9
9	27	-0	5887	0	0	0	12912	--	--	16.08	16.08	0.10	0.23	0.05	0.37	0.00	0.00	20.9
10	27	-0	5855	0	0	0	12773	--	--	16.08	16.08	0.10	0.23	0.05	0.37	0.00	0.00	20.9
11	27	-0	5878	0	0	0	12854	--	--	16.08	16.08	0.10	0.23	0.05	0.37	0.00	0.00	20.9
12	27	-0	5829	0	0	0	12718	--	--	16.08	16.08	0.10	0.23	0.05	0.37	0.00	0.00	20.9
13	27	-0	5851	0	0	0	12798	--	--	16.08	16.08	0.10	0.23	0.05	0.37	0.00	0.00	20.9
14	27	-0	5820	0	0	0	12660	--	--	16.08	16.08	0.10	0.22	0.05	0.37	0.00	0.00	20.9
15	27	-0	5895	0	0	0	12928	--	--	16.08	16.08	0.10	0.23	0.05	0.37	0.00	0.00	20.9
16	27	-0	5812	0	0	0	12644	--	--	16.08	16.08	0.10	0.22	0.05	0.36	0.00	0.00	20.9
17	27	-0	5887	0	0	0	12912	--	--	16.08	16.08	0.10	0.23	0.05	0.37	0.00	0.00	20.9
18	27	-0	8064	0	0	0	17686	--	--	16.08	16.08	0.00	0.30	0.07	0.51	0.00	0.00	20.9
19	27	-0	8064	0	0	0	17717	--	--	16.08	16.08	0.00	0.30	0.07	0.51	0.00	0.00	20.9
20	27	-0	7851	0	0	0	17148	--	--	16.08	16.08	0.00	0.29	0.06	0.49	0.00	0.00	20.9
37	27	-0	7793	0	0	0	17023	--	--	16.08	16.08	0.00	0.29	0.06	0.49	0.00	0.00	20.9
38	27	-0	7793	0	0	0	17080	--	--	16.08	16.08	0.00	0.29	0.06	0.49	0.00	0.00	20.9
39	27	-0	7437	0	0	0	16128	--	--	16.08	16.08	0.00	0.27	0.06	0.47	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	54	-0	7609	0	0	0	10530	--	--	16.08	16.08	0.00	0.18	0.06	0.48	0.00	0.00	20.9
2	54	-0	5855	0	0	0	8084	--	--	16.08	16.08	0.10	0.14	0.05	0.37	0.00	0.00	20.9
3	54	-0	5878	0	0	0	8146	--	--	16.08	16.08	0.10	0.14	0.05	0.37	0.00	0.00	20.9
4	54	-0	5829	0	0	0	8050	--	--	16.08	16.08	0.10	0.14	0.05	0.37	0.00	0.00	20.9
5	54	-0	5851	0	0	0	8112	--	--	16.08	16.08	0.10	0.14	0.05	0.37	0.00	0.00	20.9
6	54	-0	5820	0	0	0	7999	--	--	16.08	16.08	0.10	0.14	0.05	0.37	0.00	0.00	20.9
7	54	-0	5895	0	0	0	8207	--	--	16.08	16.08	0.10	0.15	0.05	0.37	0.00	0.00	20.9
8	54	-0	5812	0	0	0	7989	--	--	16.08	16.08	0.10	0.14	0.05	0.36	0.00	0.00	20.9
9	54	-0	5887	0	0	0	8197	--	--	16.08	16.08	0.10	0.15	0.05	0.37	0.00	0.00	20.9
10	54	-0	5855	0	0	0	8084	--	--	16.08	16.08	0.10	0.14	0.05	0.37	0.00	0.00	20.9
11	54	-0	5878	0	0	0	8146	--	--	16.08	16.08	0.10	0.14	0.05	0.37	0.00	0.00	20.9
12	54	-0	5829	0	0	0	8050	--	--	16.08	16.08	0.10	0.14	0.05	0.37	0.00	0.00	20.9
13	54	-0	5851	0	0	0	8112	--	--	16.08	16.08	0.10	0.14	0.05	0.37	0.00	0.00	20.9
14	54	-0	5820	0	0	0	7999	--	--	16.08	16.08	0.10	0.14	0.05	0.37	0.00	0.00	20.9
15	54	-0	5895	0	0	0	8207	--	--	16.08	16.08	0.10	0.15	0.05	0.37	0.00	0.00	20.9
16	54	-0	5812	0	0	0	7989	--	--	16.08	16.08	0.10	0.14	0.05	0.36	0.00	0.00	20.9
17	54	-0	5887	0	0	0	8197	--	--	16.08	16.08	0.10	0.15	0.05	0.37	0.00	0.00	20.9
18	54	-0	8064	0	0	0	11230	--	--	16.08	16.08	0.00	0.19	0.07	0.51	0.00	0.00	20.9
19	54	-0	8064	0	0	0	11260	--	--	16.08	16.08	0.00	0.19	0.07	0.51	0.00	0.00	20.9
20	54	-0	7851	0	0	0	10860	--	--	16.08	16.08	0.00	0.19	0.06	0.49	0.00	0.00	20.9
37	54	-0	7793	0	0	0	10780	--	--	16.08	16.08	0.00	0.18	0.06	0.49	0.00	0.00	20.9
38	54	-0	7793	0	0	0	10840	--	--	16.08	16.08	0.00	0.18	0.06	0.49	0.00	0.00	20.9
39	54	-0	7437	0	0	0	10170	--	--	16.08	16.08	0.00	0.17	0.06	0.47	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 94 NI 1896 NF 1904 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm

1	0	-0	5248	0	0	0	3639	--	--	16.08	16.08	0.00	0.06	0.04	0.33	0.00	0.00	20.9
2	0	-0	4043	0	0	0	2781	--	--	16.08	16.08	0.10	0.05	0.03	0.25	0.00	0.00	20.9
3	0	-0	4071	0	0	0	2816	--	--	16.08	16.08	0.10	0.05	0.03	0.26	0.00	0.00	20.9
4	0	-0	4003	0	0	0	2782	--	--	16.08	16.08	0.10	0.05	0.03	0.25	0.00	0.00	20.9
5	0	-0	4031	0	0	0	2818	--	--	16.08	16.08	0.10	0.05	0.03	0.25	0.00	0.00	20.9
6	0	-0	3997	0	0	0	2740	--	--	16.08	16.08	0.10	0.05	0.03	0.25	0.00	0.00	20.9
7	0	-0	4090	0	0	0	2858	--	--	16.08	16.08	0.10	0.05	0.03	0.26	0.00	0.00	20.9
8	0	-0	3985	0	0	0	2741	--	--	16.08	16.08	0.10	0.05	0.03	0.25	0.00	0.00	20.9
9	0	-0	4078	0	0	0	2859	--	--	16.08	16.08	0.10	0.05	0.03	0.26	0.00	0.00	20.9
10	0	-0	4043	0	0	0	2781	--	--	16.08	16.08	0.10	0.05	0.03	0.25	0.00	0.00	20.9
11	0	-0	4071	0	0	0	2816	--	--	16.08	16.08	0.10	0.05	0.03	0.26	0.00	0.00	20.9
12	0	-0	4003	0	0	0	2782	--	--	16.08	16.08	0.10	0.05	0.03	0.25	0.00	0.00	20.9
13	0	-0	4031	0	0	0	2818	--	--	16.08	16.08	0.10	0.05	0.03	0.25	0.00	0.00	20.9
14	0	-0	3997	0	0	0	2740	--	--	16.08	16.08	0.10	0.05	0.03	0.25	0.00	0.00	20.9
15	0	-0	4090	0	0	0	2858	--	--	16.08	16.08	0.10	0.05	0.03	0.26	0.00	0.00	20.9
16	0	-0	3985	0	0	0	2741	--	--	16.08	16.08	0.10	0.05	0.03	0.25	0.00	0.00	20.9
17	0	-0	4078	0	0	0	2859	--	--	16.08	16.08	0.10	0.05	0.03	0.26	0.00	0.00	20.9
18	0	-0	5449	0	0	0	3987	--	--	16.08	16.08	0.00	0.07	0.04	0.34	0.00	0.00	20.9
19	0	-0	5450	0	0	0	4018	--	--	16.08	16.08	0.00	0.07	0.04	0.34	0.00	0.00	20.9
20	0	-0	5259	0	0	0	3838	--	--	16.08	16.08	0.00	0.07	0.04	0.33	0.00	0.00	20.9
37	0	-0	5285	0	0	0	3776	--	--	16.08	16.08	0.00	0.06	0.04	0.33	0.00	0.00	20.9
38	0	-0	5287	0	0	0	3829	--	--	16.08	16.08	0.00	0.07	0.04	0.33	0.00	0.00	20.9
39	0	-0	4969	0	0	0	3528	--	--	16.08	16.08	0.00	0.06	0.04	0.31	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	5248	0	0	0	10654	--	--	16.08	16.08	0.00	0.18	0.04	0.33	0.00	0.00	20.9
2	27	-0	4043	0	0	0	8185	--	--	16.08	16.08	0.10	0.15	0.03	0.25	0.00	0.00	20.9
3	27	-0	4071	0	0	0	8257	--	--	16.08	16.08	0.10	0.15	0.03	0.26	0.00	0.00	20.9
4	27	-0	4003	0	0	0	8133	--	--	16.08	16.08	0.10	0.14	0.03	0.25	0.00	0.00	20.9
5	27	-0	4031	0	0	0	8206	--	--	16.08	16.08	0.10	0.15	0.03	0.25	0.00	0.00	20.9
6	27	-0	3997	0	0	0	8082	--	--	16.08	16.08	0.10	0.14	0.03	0.25	0.00	0.00	20.9
7	27	-0	4090	0	0	0	8325	--	--	16.08	16.08	0.10	0.15	0.03	0.26	0.00	0.00	20.9
8	27	-0	3985	0	0	0	8067	--	--	16.08	16.08	0.10	0.14	0.03	0.25	0.00	0.00	20.9
9	27	-0	4078	0	0	0	8309	--	--	16.08	16.08	0.10	0.15	0.03	0.26	0.00	0.00	20.9
10	27	-0	4043	0	0	0	8185	--	--	16.08	16.08	0.10	0.15	0.03	0.25	0.00	0.00	20.9
11	27	-0	4071	0	0	0	8257	--	--	16.08	16.08	0.10	0.15	0.03	0.26	0.00	0.00	20.9
12	27	-0	4003	0	0	0	8133	--	--	16.08	16.08	0.10	0.14	0.03	0.25	0.00	0.00	20.9

13	27	-0	4031	0	0	0	8206	--	--	16.08	16.08	0.10	0.15	0.03	0.25	0.00	0.00	20.9
14	27	-0	3997	0	0	0	8082	--	--	16.08	16.08	0.10	0.14	0.03	0.25	0.00	0.00	20.9
15	27	-0	4090	0	0	0	8325	--	--	16.08	16.08	0.10	0.15	0.03	0.26	0.00	0.00	20.9
16	27	-0	3985	0	0	0	8067	--	--	16.08	16.08	0.10	0.14	0.03	0.25	0.00	0.00	20.9
17	27	-0	4078	0	0	0	8309	--	--	16.08	16.08	0.10	0.15	0.03	0.26	0.00	0.00	20.9
18	27	-0	5449	0	0	0	11270	--	--	16.08	16.08	0.00	0.19	0.04	0.34	0.00	0.00	20.9
19	27	-0	5450	0	0	0	11303	--	--	16.08	16.08	0.00	0.19	0.04	0.34	0.00	0.00	20.9
20	27	-0	5259	0	0	0	10867	--	--	16.08	16.08	0.00	0.19	0.04	0.33	0.00	0.00	20.9
37	27	-0	5285	0	0	0	10840	--	--	16.08	16.08	0.00	0.18	0.04	0.33	0.00	0.00	20.9
38	27	-0	5287	0	0	0	10896	--	--	16.08	16.08	0.00	0.19	0.04	0.33	0.00	0.00	20.9
39	27	-0	4969	0	0	0	10170	--	--	16.08	16.08	0.00	0.17	0.04	0.31	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	54	-0	5248	0	0	0	6451	--	--	16.08	16.08	0.00	0.11	0.04	0.33	0.00	0.00	20.9
2	54	-0	4043	0	0	0	4947	--	--	16.08	16.08	0.10	0.09	0.03	0.25	0.00	0.00	20.9
3	54	-0	4071	0	0	0	4997	--	--	16.08	16.08	0.10	0.09	0.03	0.26	0.00	0.00	20.9
4	54	-0	4003	0	0	0	4927	--	--	16.08	16.08	0.10	0.09	0.03	0.25	0.00	0.00	20.9
5	54	-0	4031	0	0	0	4977	--	--	16.08	16.08	0.10	0.09	0.03	0.25	0.00	0.00	20.9
6	54	-0	3997	0	0	0	4881	--	--	16.08	16.08	0.10	0.09	0.03	0.25	0.00	0.00	20.9
7	54	-0	4090	0	0	0	5049	--	--	16.08	16.08	0.10	0.09	0.03	0.26	0.00	0.00	20.9
8	54	-0	3985	0	0	0	4875	--	--	16.08	16.08	0.10	0.09	0.03	0.25	0.00	0.00	20.9
9	54	-0	4078	0	0	0	5043	--	--	16.08	16.08	0.10	0.09	0.03	0.26	0.00	0.00	20.9
10	54	-0	4043	0	0	0	4947	--	--	16.08	16.08	0.10	0.09	0.03	0.25	0.00	0.00	20.9
11	54	-0	4071	0	0	0	4997	--	--	16.08	16.08	0.10	0.09	0.03	0.26	0.00	0.00	20.9
12	54	-0	4003	0	0	0	4927	--	--	16.08	16.08	0.10	0.09	0.03	0.25	0.00	0.00	20.9
13	54	-0	4031	0	0	0	4977	--	--	16.08	16.08	0.10	0.09	0.03	0.25	0.00	0.00	20.9
14	54	-0	3997	0	0	0	4881	--	--	16.08	16.08	0.10	0.09	0.03	0.25	0.00	0.00	20.9
15	54	-0	4090	0	0	0	5049	--	--	16.08	16.08	0.10	0.09	0.03	0.26	0.00	0.00	20.9
16	54	-0	3985	0	0	0	4875	--	--	16.08	16.08	0.10	0.09	0.03	0.25	0.00	0.00	20.9
17	54	-0	4078	0	0	0	5043	--	--	16.08	16.08	0.10	0.09	0.03	0.26	0.00	0.00	20.9
18	54	-0	5449	0	0	0	6906	--	--	16.08	16.08	0.00	0.12	0.04	0.34	0.00	0.00	20.9
19	54	-0	5450	0	0	0	6938	--	--	16.08	16.08	0.00	0.12	0.04	0.34	0.00	0.00	20.9
20	54	-0	5259	0	0	0	6655	--	--	16.08	16.08	0.00	0.11	0.04	0.33	0.00	0.00	20.9
37	54	-0	5285	0	0	0	6608	--	--	16.08	16.08	0.00	0.11	0.04	0.33	0.00	0.00	20.9
38	54	-0	5287	0	0	0	6662	--	--	16.08	16.08	0.00	0.11	0.04	0.33	0.00	0.00	20.9
39	54	-0	4969	0	0	0	6190	--	--	16.08	16.08	0.00	0.11	0.04	0.31	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 95 NI 1902 NF 1896 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	2904	0	0	0	2084	--	--	16.08	16.08	0.00	0.04	0.02	0.18	0.00	0.00	20.9
2	0	-0	2245	0	0	0	1578	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
3	0	-0	2278	0	0	0	1596	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
4	0	-0	2190	0	0	0	1610	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
5	0	-0	2222	0	0	0	1627	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
6	0	-0	2188	0	0	0	1568	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
7	0	-0	2297	0	0	0	1628	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
8	0	-0	2171	0	0	0	1578	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
9	0	-0	2280	0	0	0	1637	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
10	0	-0	2245	0	0	0	1578	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
11	0	-0	2278	0	0	0	1596	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
12	0	-0	2190	0	0	0	1610	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
13	0	-0	2222	0	0	0	1627	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
14	0	-0	2188	0	0	0	1568	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
15	0	-0	2297	0	0	0	1628	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
16	0	-0	2171	0	0	0	1578	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
17	0	-0	2280	0	0	0	1637	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
18	0	-0	2842	0	0	0	2464	--	--	16.08	16.08	0.00	0.04	0.02	0.18	0.00	0.00	20.9
19	0	-0	2844	0	0	0	2495	--	--	16.08	16.08	0.00	0.04	0.02	0.18	0.00	0.00	20.9
20	0	-0	2679	0	0	0	2402	--	--	16.08	16.08	0.00	0.04	0.02	0.17	0.00	0.00	20.9
37	0	-0	2788	0	0	0	2283	--	--	16.08	16.08	0.00	0.04	0.02	0.17	0.00	0.00	20.9
38	0	-0	2791	0	0	0	2334	--	--	16.08	16.08	0.00	0.04	0.02	0.18	0.00	0.00	20.9
39	0	-0	2516	0	0	0	2180	--	--	16.08	16.08	0.00	0.04	0.02	0.16	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	2904	0	0	0	5965	--	--	16.08	16.08	0.00	0.10	0.02	0.18	0.00	0.00	20.9
2	27	-0	2245	0	0	0	4579	--	--	16.08	16.08	0.10	0.08	0.02	0.14	0.00	0.00	20.9
3	27	-0	2278	0	0	0	4641	--	--	16.08	16.08	0.10	0.08	0.02	0.14	0.00	0.00	20.9
4	27	-0	2190	0	0	0	4537	--	--	16.08	16.08	0.10	0.08	0.02	0.14	0.00	0.00	20.9
5	27	-0	2222	0	0	0	4597	--	--	16.08	16.08	0.10	0.08	0.02	0.14	0.00	0.00	20.9
6	27	-0	2188	0	0	0	4492	--	--	16.08	16.08	0.10	0.08	0.02	0.14	0.00	0.00	20.9
7	27	-0	2297	0	0	0	4698	--	--	16.08	16.08	0.10	0.08	0.02	0.14	0.00	0.00	20.9
8	27	-0	2171	0	0	0	4480	--	--	16.08	16.08	0.10	0.08	0.02	0.14	0.00	0.00	20.9
9	27	-0	2280	0	0	0	4685	--	--	16.08	16.08	0.10	0.08	0.02	0.14	0.00	0.00	20.9
10	27	-0	2245	0	0	0	4579	--	--	16.08	16.08	0.10	0.08	0.02	0.14	0.00	0.00	20.9
11	27	-0	2278	0	0	0	4641	--	--	16.08	16.08	0.10	0.08	0.02	0.14	0.00	0.00	20.9
12	27	-0	2190	0	0	0	4537	--	--	16.08	16.08	0.10	0.08	0.02	0.14	0.00	0.00	20.9
13	27	-0	2222	0	0	0	4597	--	--	16.08	16.08	0.10	0.08	0.02	0.14	0.00	0.00	20.9
14	27	-0	2188	0	0	0	4492	--	--	16.08	16.08	0.10	0.08	0.02	0.14	0.00	0.00	20.9
15	27	-0	2297	0	0	0	4698	--	--	16.08	16.08	0.10	0.08	0.02	0.14	0.00	0.00	20.9
16	27	-0	2171	0	0	0	4480	--	--	16.08	16.08	0.10	0.08	0.02	0.14	0.00	0.00	20.9
17	27	-0	2280	0	0	0	4685	--	--	16.08	16.08	0.10	0.08	0.02	0.14	0.00	0.00	20.9
18	27	-0	2842	0	0	0	6263	--	--	16.08	16.08	0.00	0.11	0.02	0.18	0.00	0.00	20.9
19	27	-0	2844	0	0	0	6296	--	--	16.08	16.08	0.00	0.11	0.02	0.18	0.00	0.00	20.9
20	27	-0	2679	0	0	0	5983	--	--	16.08	16.08	0.00	0.10	0.02	0.17	0.00	0.00	20.9
37	27	-0	2788	0	0	0	6009	--	--	16.08	16.08	0.00	0.10	0.02	0.17	0.00	0.00	20.9
38	27	-0	2791	0	0	0	6064	--	--	16.08	16.08	0.00	0.10	0.02	0.18	0.00	0.00	20.9
39	27	-0	2516	0	0	0	5543	--	--	16.08	16.08	0.00	0.09	0.02	0.16	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	54	-0	2904	0	0	0	3639	--	--	16.08	16.08	0.00	0.06	0.02	0.18	0.00	0.00	20.9
2	54	-0	2245	0	0	0	2781	--	--	16.08	16.08	0.10	0.05	0.02	0.14	0.00	0.00	20.9
3	54	-0	2278	0	0	0	2816	--	--	16.08	16.08	0.10	0.05	0.02	0.14	0.00	0.00	20.9
4	54	-0	2190	0	0	0	2782	--	--	16.08	16.08	0.10	0.05	0.02	0.14	0.00	0.00	20.9
5	54	-0	2222	0	0	0	2818	--	--	16.08	16.08	0.10	0.05	0.02	0.14	0.00	0.00	20.9
6	54	-0	2188	0	0	0	2740	--	--	16.08	16.08	0.10	0.05	0.02	0.14	0.00	0.00	20.9
7	54	-0	2297	0	0	0	2858	--	--	16.08	16.08	0.10	0.05	0.02	0.14	0.00	0.00	20.9
8	54	-0	2171	0	0	0	2741	--	--	16.08	16.08	0.10	0.05	0.02	0.14	0.00	0.00	20.9

9	54	-0	2280	0	0	0	2859	--	--	16.08	16.08	0.10	0.05	0.02	0.14	0.00	0.00	20.9
10	54	-0	2245	0	0	0	2781	--	--	16.08	16.08	0.10	0.05	0.02	0.14	0.00	0.00	20.9
11	54	-0	2278	0	0	0	2816	--	--	16.08	16.08	0.10	0.05	0.02	0.14	0.00	0.00	20.9
12	54	-0	2190	0	0	0	2782	--	--	16.08	16.08	0.10	0.05	0.02	0.14	0.00	0.00	20.9
13	54	-0	2222	0	0	0	2818	--	--	16.08	16.08	0.10	0.05	0.02	0.14	0.00	0.00	20.9
14	54	-0	2188	0	0	0	2740	--	--	16.08	16.08	0.10	0.05	0.02	0.14	0.00	0.00	20.9
15	54	-0	2297	0	0	0	2858	--	--	16.08	16.08	0.10	0.05	0.02	0.14	0.00	0.00	20.9
16	54	-0	2171	0	0	0	2741	--	--	16.08	16.08	0.10	0.05	0.02	0.14	0.00	0.00	20.9
17	54	-0	2280	0	0	0	2859	--	--	16.08	16.08	0.10	0.05	0.02	0.14	0.00	0.00	20.9
18	54	-0	2842	0	0	0	3987	--	--	16.08	16.08	0.00	0.07	0.02	0.18	0.00	0.00	20.9
19	54	-0	2844	0	0	0	4018	--	--	16.08	16.08	0.00	0.07	0.02	0.18	0.00	0.00	20.9
20	54	-0	2679	0	0	0	3838	--	--	16.08	16.08	0.00	0.07	0.02	0.17	0.00	0.00	20.9
37	54	-0	2788	0	0	0	3776	--	--	16.08	16.08	0.00	0.06	0.02	0.17	0.00	0.00	20.9
38	54	-0	2791	0	0	0	3829	--	--	16.08	16.08	0.00	0.07	0.02	0.18	0.00	0.00	20.9
39	54	-0	2516	0	0	0	3528	--	--	16.08	16.08	0.00	0.06	0.02	0.16	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 96 NI 1903 NF 1902 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	589	0	0	0	1768	--	--	16.08	16.08	0.00	0.03	0.00	0.04	0.00	0.00	20.9
2	0	-0	472	0	0	0	1326	--	--	16.08	16.08	0.10	0.02	0.00	0.03	0.00	0.00	20.9
3	0	-0	509	0	0	0	1324	--	--	16.08	16.08	0.10	0.02	0.00	0.03	0.00	0.00	20.9
4	0	-0	398	0	0	0	1396	--	--	16.08	16.08	0.10	0.02	0.00	0.02	0.00	0.00	20.9
5	0	-0	435	0	0	0	1394	--	--	16.08	16.08	0.10	0.02	0.00	0.03	0.00	0.00	20.9
6	0	-0	402	0	0	0	1353	--	--	16.08	16.08	0.10	0.02	0.00	0.03	0.00	0.00	20.9
7	0	-0	526	0	0	0	1346	--	--	16.08	16.08	0.10	0.02	0.00	0.03	0.00	0.00	20.9
8	0	-0	380	0	0	0	1374	--	--	16.08	16.08	0.10	0.02	0.00	0.02	0.00	0.00	20.9
9	0	-0	504	0	0	0	1367	--	--	16.08	16.08	0.10	0.02	0.00	0.03	0.00	0.00	20.9
10	0	-0	472	0	0	0	1326	--	--	16.08	16.08	0.10	0.02	0.00	0.03	0.00	0.00	20.9
11	0	-0	509	0	0	0	1324	--	--	16.08	16.08	0.10	0.02	0.00	0.03	0.00	0.00	20.9
12	0	-0	398	0	0	0	1396	--	--	16.08	16.08	0.10	0.02	0.00	0.02	0.00	0.00	20.9
13	0	-0	435	0	0	0	1394	--	--	16.08	16.08	0.10	0.02	0.00	0.03	0.00	0.00	20.9
14	0	-0	402	0	0	0	1353	--	--	16.08	16.08	0.10	0.02	0.00	0.03	0.00	0.00	20.9
15	0	-0	526	0	0	0	1346	--	--	16.08	16.08	0.10	0.02	0.00	0.03	0.00	0.00	20.9
16	0	-0	380	0	0	0	1374	--	--	16.08	16.08	0.10	0.02	0.00	0.02	0.00	0.00	20.9
17	0	-0	504	0	0	0	1367	--	--	16.08	16.08	0.10	0.02	0.00	0.03	0.00	0.00	20.9
18	0	-0	258	0	0	0	2326	--	--	16.08	16.08	0.00	0.04	0.00	0.02	0.00	0.00	20.9
19	0	-0	261	0	0	0	2355	--	--	16.08	16.08	0.00	0.04	0.00	0.02	0.00	0.00	20.9
20	0	-0	124	0	0	0	2336	--	--	16.08	16.08	0.00	0.04	0.00	0.01	0.00	0.00	20.9
37	0	-0	314	0	0	0	2115	--	--	16.08	16.08	0.00	0.04	0.00	0.02	0.00	0.00	20.9
38	0	-0	319	0	0	0	2163	--	--	16.08	16.08	0.00	0.04	0.00	0.02	0.00	0.00	20.9
39	0	-0	90	0	0	0	2132	--	--	16.08	16.08	0.00	0.04	0.00	0.01	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	589	0	0	0	2556	--	--	16.08	16.08	0.00	0.04	0.00	0.04	0.00	0.00	20.9
2	27	-0	472	0	0	0	1956	--	--	16.08	16.08	0.10	0.03	0.00	0.03	0.00	0.00	20.9
3	27	-0	509	0	0	0	2004	--	--	16.08	16.08	0.10	0.04	0.00	0.03	0.00	0.00	20.9
4	27	-0	398	0	0	0	1928	--	--	16.08	16.08	0.10	0.03	0.00	0.02	0.00	0.00	20.9
5	27	-0	435	0	0	0	1975	--	--	16.08	16.08	0.10	0.04	0.00	0.03	0.00	0.00	20.9
6	27	-0	402	0	0	0	1891	--	--	16.08	16.08	0.10	0.03	0.00	0.03	0.00	0.00	20.9
7	27	-0	526	0	0	0	2049	--	--	16.08	16.08	0.10	0.04	0.00	0.03	0.00	0.00	20.9
8	27	-0	380	0	0	0	1882	--	--	16.08	16.08	0.10	0.03	0.00	0.02	0.00	0.00	20.9
9	27	-0	504	0	0	0	2041	--	--	16.08	16.08	0.10	0.04	0.00	0.03	0.00	0.00	20.9
10	27	-0	472	0	0	0	1956	--	--	16.08	16.08	0.10	0.03	0.00	0.03	0.00	0.00	20.9
11	27	-0	509	0	0	0	2004	--	--	16.08	16.08	0.10	0.04	0.00	0.03	0.00	0.00	20.9
12	27	-0	398	0	0	0	1928	--	--	16.08	16.08	0.10	0.03	0.00	0.02	0.00	0.00	20.9
13	27	-0	435	0	0	0	1975	--	--	16.08	16.08	0.10	0.04	0.00	0.03	0.00	0.00	20.9
14	27	-0	402	0	0	0	1891	--	--	16.08	16.08	0.10	0.03	0.00	0.03	0.00	0.00	20.9
15	27	-0	526	0	0	0	2049	--	--	16.08	16.08	0.10	0.04	0.00	0.03	0.00	0.00	20.9
16	27	-0	380	0	0	0	1882	--	--	16.08	16.08	0.10	0.03	0.00	0.02	0.00	0.00	20.9
17	27	-0	504	0	0	0	2041	--	--	16.08	16.08	0.10	0.04	0.00	0.03	0.00	0.00	20.9
18	27	-0	258	0	0	0	2671	--	--	16.08	16.08	0.00	0.05	0.00	0.02	0.00	0.00	20.9
19	27	-0	261	0	0	0	2704	--	--	16.08	16.08	0.00	0.05	0.00	0.02	0.00	0.00	20.9
20	27	-0	124	0	0	0	2502	--	--	16.08	16.08	0.00	0.04	0.00	0.01	0.00	0.00	20.9
37	27	-0	314	0	0	0	2535	--	--	16.08	16.08	0.00	0.04	0.00	0.02	0.00	0.00	20.9
38	27	-0	319	0	0	0	2589	--	--	16.08	16.08	0.00	0.04	0.00	0.02	0.00	0.00	20.9
39	27	-0	90	0	0	0	2253	--	--	16.08	16.08	0.00	0.04	0.00	0.01	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	54	-0	589	0	0	0	2084	--	--	16.08	16.08	0.00	0.04	0.00	0.04	0.00	0.00	20.9
2	54	-0	472	0	0	0	1578	--	--	16.08	16.08	0.10	0.03	0.00	0.03	0.00	0.00	20.9
3	54	-0	509	0	0	0	1596	--	--	16.08	16.08	0.10	0.03	0.00	0.03	0.00	0.00	20.9
4	54	-0	398	0	0	0	1610	--	--	16.08	16.08	0.10	0.03	0.00	0.02	0.00	0.00	20.9
5	54	-0	435	0	0	0	1627	--	--	16.08	16.08	0.10	0.03	0.00	0.03	0.00	0.00	20.9
6	54	-0	402	0	0	0	1568	--	--	16.08	16.08	0.10	0.03	0.00	0.03	0.00	0.00	20.9
7	54	-0	526	0	0	0	1628	--	--	16.08	16.08	0.10	0.03	0.00	0.03	0.00	0.00	20.9
8	54	-0	380	0	0	0	1578	--	--	16.08	16.08	0.10	0.03	0.00	0.02	0.00	0.00	20.9
9	54	-0	504	0	0	0	1637	--	--	16.08	16.08	0.10	0.03	0.00	0.03	0.00	0.00	20.9
10	54	-0	472	0	0	0	1578	--	--	16.08	16.08	0.10	0.03	0.00	0.03	0.00	0.00	20.9
11	54	-0	509	0	0	0	1596	--	--	16.08	16.08	0.10	0.03	0.00	0.03	0.00	0.00	20.9
12	54	-0	398	0	0	0	1610	--	--	16.08	16.08	0.10	0.03	0.00	0.02	0.00	0.00	20.9
13	54	-0	435	0	0	0	1627	--	--	16.08	16.08	0.10	0.03	0.00	0.03	0.00	0.00	20.9
14	54	-0	402	0	0	0	1568	--	--	16.08	16.08	0.10	0.03	0.00	0.03	0.00	0.00	20.9
15	54	-0	526	0	0	0	1628	--	--	16.08	16.08	0.10	0.03	0.00	0.03	0.00	0.00	20.9
16	54	-0	380	0	0	0	1578	--	--	16.08	16.08	0.10	0.03	0.00	0.02	0.00	0.00	20.9
17	54	-0	504	0	0	0	1637	--	--	16.08	16.08	0.10	0.03	0.00	0.03	0.00	0.00	20.9
18	54	-0	258	0	0	0	2464	--	--	16.08	16.08	0.00	0.04	0.00	0.02	0.00	0.00	20.9
19	54	-0	261	0	0	0	2495	--	--	16.08	16.08	0.00	0.04	0.00	0.02	0.00	0.00	20.9
20	54	-0	124	0	0	0	2402	--	--	16.08	16.08	0.00	0.04	0.00	0.01	0.00	0.00	20.9
37	54	-0	314	0	0	0	2283	--	--	16.08	16.08	0.00	0.04	0.00	0.02	0.00	0.00	20.9
38	54	-0	319	0	0	0	2334	--	--	16.08	16.08	0.00	0.04	0.00	0.02	0.00	0.00	20.9
39	54	-0	90	0	0	0	2180	--	--	16.08	16.08	0.00	0.04	0.00	0.01	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 97 NI 1894 NF 1903 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-1691	0	0	0	2674	--	--	16.08	16.08	0.00	0.05	0.01	0.11	0.00	0.00	20.9
2	0	-0	-1274	0	0	0	2008	--	--	16.08	16.08	0.10	0.04	0.01	0.08	0.00	0.00	20.9
3	0	-0	-1233	0	0	0	1984	--	--	16.08	16.08	0.10	0.04	0.01	0.08	0.00	0.00	20.9
4	0	-0	-1368	0	0	0	2129	--	--	16.08	16.08	0.10	0.04	0.01	0.09	0.00	0.00	20.9
5	0	-0	-1327	0	0	0	2105	--	--	16.08	16.08	0.10	0.04	0.01	0.08	0.00	0.00	20.9
6	0	-0	-1355	0	0	0	2079	--	--	16.08	16.08	0.10	0.04	0.01	0.09	0.00	0.00	20.9
7	0	-0	-1218	0	0	0	1998	--	--	16.08	16.08	0.10	0.04	0.01	0.08	0.00	0.00	20.9
8	0	-0	-1383	0	0	0	2115	--	--	16.08	16.08	0.10	0.04	0.01	0.09	0.00	0.00	20.9
9	0	-0	-1246	0	0	0	2035	--	--	16.08	16.08	0.10	0.04	0.01	0.08	0.00	0.00	20.9
10	0	-0	-1274	0	0	0	2008	--	--	16.08	16.08	0.10	0.04	0.01	0.08	0.00	0.00	20.9
11	0	-0	-1233	0	0	0	1984	--	--	16.08	16.08	0.10	0.04	0.01	0.08	0.00	0.00	20.9
12	0	-0	-1368	0	0	0	2129	--	--	16.08	16.08	0.10	0.04	0.01	0.09	0.00	0.00	20.9
13	0	-0	-1327	0	0	0	2105	--	--	16.08	16.08	0.10	0.04	0.01	0.08	0.00	0.00	20.9
14	0	-0	-1355	0	0	0	2079	--	--	16.08	16.08	0.10	0.04	0.01	0.09	0.00	0.00	20.9
15	0	-0	-1218	0	0	0	1998	--	--	16.08	16.08	0.10	0.04	0.01	0.08	0.00	0.00	20.9
16	0	-0	-1383	0	0	0	2115	--	--	16.08	16.08	0.10	0.04	0.01	0.09	0.00	0.00	20.9
17	0	-0	-1246	0	0	0	2035	--	--	16.08	16.08	0.10	0.04	0.01	0.08	0.00	0.00	20.9
18	0	-0	-2296	0	0	0	3556	--	--	16.08	16.08	0.00	0.06	0.02	0.14	0.00	0.00	20.9
19	0	-0	-2293	0	0	0	3583	--	--	16.08	16.08	0.00	0.06	0.02	0.14	0.00	0.00	20.9
20	0	-0	-2400	0	0	0	3621	--	--	16.08	16.08	0.00	0.06	0.02	0.15	0.00	0.00	20.9
37	0	-0	-2130	0	0	0	3256	--	--	16.08	16.08	0.00	0.06	0.02	0.13	0.00	0.00	20.9
38	0	-0	-2124	0	0	0	3301	--	--	16.08	16.08	0.00	0.06	0.02	0.13	0.00	0.00	20.9
39	0	-0	-2302	0	0	0	3365	--	--	16.08	16.08	0.00	0.06	0.02	0.14	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-1691	0	0	0	2674	--	--	16.08	16.08	0.00	0.05	0.01	0.11	0.00	0.00	20.9
2	27	-0	-1274	0	0	0	2008	--	--	16.08	16.08	0.10	0.04	0.01	0.08	0.00	0.00	20.9
3	27	-0	-1233	0	0	0	1984	--	--	16.08	16.08	0.10	0.04	0.01	0.08	0.00	0.00	20.9
4	27	-0	-1368	0	0	0	2129	--	--	16.08	16.08	0.10	0.04	0.01	0.09	0.00	0.00	20.9
5	27	-0	-1327	0	0	0	2105	--	--	16.08	16.08	0.10	0.04	0.01	0.08	0.00	0.00	20.9
6	27	-0	-1355	0	0	0	2079	--	--	16.08	16.08	0.10	0.04	0.01	0.09	0.00	0.00	20.9
7	27	-0	-1218	0	0	0	1998	--	--	16.08	16.08	0.10	0.04	0.01	0.08	0.00	0.00	20.9
8	27	-0	-1383	0	0	0	2115	--	--	16.08	16.08	0.10	0.04	0.01	0.09	0.00	0.00	20.9
9	27	-0	-1246	0	0	0	2035	--	--	16.08	16.08	0.10	0.04	0.01	0.08	0.00	0.00	20.9
10	27	-0	-1274	0	0	0	2008	--	--	16.08	16.08	0.10	0.04	0.01	0.08	0.00	0.00	20.9
11	27	-0	-1233	0	0	0	1984	--	--	16.08	16.08	0.10	0.04	0.01	0.08	0.00	0.00	20.9
12	27	-0	-1368	0	0	0	2129	--	--	16.08	16.08	0.10	0.04	0.01	0.09	0.00	0.00	20.9
13	27	-0	-1327	0	0	0	2105	--	--	16.08	16.08	0.10	0.04	0.01	0.08	0.00	0.00	20.9
14	27	-0	-1355	0	0	0	2079	--	--	16.08	16.08	0.10	0.04	0.01	0.09	0.00	0.00	20.9
15	27	-0	-1218	0	0	0	1998	--	--	16.08	16.08	0.10	0.04	0.01	0.08	0.00	0.00	20.9
16	27	-0	-1383	0	0	0	2115	--	--	16.08	16.08	0.10	0.04	0.01	0.09	0.00	0.00	20.9
17	27	-0	-1246	0	0	0	2035	--	--	16.08	16.08	0.10	0.04	0.01	0.08	0.00	0.00	20.9
18	27	-0	-2296	0	0	0	3556	--	--	16.08	16.08	0.00	0.06	0.02	0.14	0.00	0.00	20.9
19	27	-0	-2293	0	0	0	3583	--	--	16.08	16.08	0.00	0.06	0.02	0.14	0.00	0.00	20.9
20	27	-0	-2400	0	0	0	3621	--	--	16.08	16.08	0.00	0.06	0.02	0.15	0.00	0.00	20.9
37	27	-0	-2130	0	0	0	3256	--	--	16.08	16.08	0.00	0.06	0.02	0.13	0.00	0.00	20.9
38	27	-0	-2124	0	0	0	3301	--	--	16.08	16.08	0.00	0.06	0.02	0.13	0.00	0.00	20.9
39	27	-0	-2302	0	0	0	3365	--	--	16.08	16.08	0.00	0.06	0.02	0.14	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	54	-0	-1691	0	0	0	1768	--	--	16.08	16.08	0.00	0.03	0.01	0.11	0.00	0.00	20.9
2	54	-0	-1274	0	0	0	1326	--	--	16.08	16.08	0.10	0.02	0.01	0.08	0.00	0.00	20.9
3	54	-0	-1233	0	0	0	1324	--	--	16.08	16.08	0.10	0.02	0.01	0.08	0.00	0.00	20.9
4	54	-0	-1368	0	0	0	1396	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
5	54	-0	-1327	0	0	0	1394	--	--	16.08	16.08	0.10	0.02	0.01	0.08	0.00	0.00	20.9
6	54	-0	-1355	0	0	0	1353	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
7	54	-0	-1218	0	0	0	1346	--	--	16.08	16.08	0.10	0.02	0.01	0.08	0.00	0.00	20.9
8	54	-0	-1383	0	0	0	1374	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
9	54	-0	-1246	0	0	0	1367	--	--	16.08	16.08	0.10	0.02	0.01	0.08	0.00	0.00	20.9
10	54	-0	-1274	0	0	0	1326	--	--	16.08	16.08	0.10	0.02	0.01	0.08	0.00	0.00	20.9
11	54	-0	-1233	0	0	0	1324	--	--	16.08	16.08	0.10	0.02	0.01	0.08	0.00	0.00	20.9
12	54	-0	-1368	0	0	0	1396	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
13	54	-0	-1327	0	0	0	1394	--	--	16.08	16.08	0.10	0.02	0.01	0.08	0.00	0.00	20.9
14	54	-0	-1355	0	0	0	1353	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
15	54	-0	-1218	0	0	0	1346	--	--	16.08	16.08	0.10	0.02	0.01	0.08	0.00	0.00	20.9
16	54	-0	-1383	0	0	0	1374	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
17	54	-0	-1246	0	0	0	1367	--	--	16.08	16.08	0.10	0.02	0.01	0.08	0.00	0.00	20.9
18	54	-0	-2296	0	0	0	2326	--	--	16.08	16.08	0.00	0.04	0.02	0.14	0.00	0.00	20.9
19	54	-0	-2293	0	0	0	2355	--	--	16.08	16.08	0.00	0.04	0.02	0.14	0.00	0.00	20.9
20	54	-0	-2400	0	0	0	2336	--	--	16.08	16.08	0.00	0.04	0.02	0.15	0.00	0.00	20.9
37	54	-0	-2130	0	0	0	2115	--	--	16.08	16.08	0.00	0.04	0.02	0.13	0.00	0.00	20.9
38	54	-0	-2124	0	0	0	2163	--	--	16.08	16.08	0.00	0.04	0.02	0.13	0.00	0.00	20.9
39	54	-0	-2302	0	0	0	2132	--	--	16.08	16.08	0.00	0.04	0.02	0.14	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 98 NI 1895 NF 1894 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-3932	0	0	0	4780	--	--	16.08	16.08	0.00	0.08	0.03	0.25	0.00	0.00	20.9
2	0	-0	-2990	0	0	0	3610	--	--	16.08	16.08	0.10	0.06	0.02	0.19	0.00	0.00	20.9
3	0	-0	-2945	0	0	0	3562	--	--	16.08	16.08	0.10	0.06	0.02	0.18	0.00	0.00	20.9
4	0	-0	-3105	0	0	0	3793	--	--	16.08	16.08	0.10	0.07	0.03	0.19	0.00	0.00	20.9
5	0	-0	-3060	0	0	0	3744	--	--	16.08	16.08	0.10	0.07	0.03	0.19	0.00	0.00	20.9
6	0	-0	-3083	0	0	0	3730	--	--	16.08	16.08	0.10	0.07	0.03	0.19	0.00	0.00	20.9
7	0	-0	-2933	0	0	0	3569	--	--	16.08	16.08	0.10	0.06	0.02	0.18	0.00	0.00	20.9
8	0	-0	-3117	0	0	0	3785	--	--	16.08	16.08	0.10	0.07	0.03	0.20	0.00	0.00	20.9
9	0	-0	-2967	0	0	0	3624	--	--	16.08	16.08	0.10	0.06	0.02	0.19	0.00	0.00	20.9
10	0	-0	-2990	0	0	0	3610	--	--	16.08	16.08	0.10	0.06	0.02	0.19	0.00	0.00	20.9
11	0	-0	-2945	0	0	0	3562	--	--	16.08	16.08	0.10	0.06	0.02	0.18	0.00	0.00	20.9
12	0	-0	-3105	0	0	0	3793	--	--	16.08	16.08	0.10	0.07	0.03	0.19	0.00	0.00	20.9
13	0	-0	-3060	0	0	0	3744	--	--	16.08	16.08	0.10	0.07	0.03	0.19	0.00	0.00	20.9
14	0	-0	-3083	0	0	0	3730	--	--	16.08	16.08	0.10	0.07	0.03	0.19	0.00	0.00	20.9
15	0	-0	-2933	0	0	0	3569	--	--	16.08	16.08	0.10	0.06	0.02	0.18	0.00	0.00	20.9
16	0	-0	-3117	0	0	0	3785	--	--	16.08	16.08	0.10	0.07	0.03	0.20	0.00	0.00	20.9

17	0	-0	-2967	0	0	0	3624	--	--	16.08	16.08	0.10	0.06	0.02	0.19	0.00	0.00	20.9
18	0	-0	-4816	0	0	0	6136	--	--	16.08	16.08	0.00	0.10	0.04	0.30	0.00	0.00	20.9
19	0	-0	-4811	0	0	0	6160	--	--	16.08	16.08	0.00	0.11	0.04	0.30	0.00	0.00	20.9
20	0	-0	-4886	0	0	0	6239	--	--	16.08	16.08	0.00	0.11	0.04	0.31	0.00	0.00	20.9
37	0	-0	-4540	0	0	0	5688	--	--	16.08	16.08	0.00	0.10	0.04	0.28	0.00	0.00	20.9
38	0	-0	-4532	0	0	0	5728	--	--	16.08	16.08	0.00	0.10	0.04	0.28	0.00	0.00	20.9
39	0	-0	-4657	0	0	0	5860	--	--	16.08	16.08	0.00	0.10	0.04	0.29	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-3932	0	0	0	4780	--	--	16.08	16.08	0.00	0.08	0.03	0.25	0.00	0.00	20.9
2	27	-0	-2990	0	0	0	3610	--	--	16.08	16.08	0.10	0.06	0.02	0.19	0.00	0.00	20.9
3	27	-0	-2945	0	0	0	3562	--	--	16.08	16.08	0.10	0.06	0.02	0.18	0.00	0.00	20.9
4	27	-0	-3105	0	0	0	3793	--	--	16.08	16.08	0.10	0.07	0.03	0.19	0.00	0.00	20.9
5	27	-0	-3060	0	0	0	3744	--	--	16.08	16.08	0.10	0.07	0.03	0.19	0.00	0.00	20.9
6	27	-0	-3083	0	0	0	3730	--	--	16.08	16.08	0.10	0.07	0.03	0.19	0.00	0.00	20.9
7	27	-0	-2933	0	0	0	3569	--	--	16.08	16.08	0.10	0.06	0.02	0.18	0.00	0.00	20.9
8	27	-0	-3117	0	0	0	3785	--	--	16.08	16.08	0.10	0.07	0.03	0.20	0.00	0.00	20.9
9	27	-0	-2967	0	0	0	3624	--	--	16.08	16.08	0.10	0.06	0.02	0.19	0.00	0.00	20.9
10	27	-0	-2990	0	0	0	3610	--	--	16.08	16.08	0.10	0.06	0.02	0.19	0.00	0.00	20.9
11	27	-0	-2945	0	0	0	3562	--	--	16.08	16.08	0.10	0.06	0.02	0.18	0.00	0.00	20.9
12	27	-0	-3105	0	0	0	3793	--	--	16.08	16.08	0.10	0.07	0.03	0.19	0.00	0.00	20.9
13	27	-0	-3060	0	0	0	3744	--	--	16.08	16.08	0.10	0.07	0.03	0.19	0.00	0.00	20.9
14	27	-0	-3083	0	0	0	3730	--	--	16.08	16.08	0.10	0.07	0.03	0.19	0.00	0.00	20.9
15	27	-0	-2933	0	0	0	3569	--	--	16.08	16.08	0.10	0.06	0.02	0.18	0.00	0.00	20.9
16	27	-0	-3117	0	0	0	3785	--	--	16.08	16.08	0.10	0.07	0.03	0.20	0.00	0.00	20.9
17	27	-0	-2967	0	0	0	3624	--	--	16.08	16.08	0.10	0.06	0.02	0.19	0.00	0.00	20.9
18	27	-0	-4816	0	0	0	6136	--	--	16.08	16.08	0.00	0.10	0.04	0.30	0.00	0.00	20.9
19	27	-0	-4811	0	0	0	6160	--	--	16.08	16.08	0.00	0.11	0.04	0.30	0.00	0.00	20.9
20	27	-0	-4886	0	0	0	6239	--	--	16.08	16.08	0.00	0.11	0.04	0.31	0.00	0.00	20.9
37	27	-0	-4540	0	0	0	5688	--	--	16.08	16.08	0.00	0.10	0.04	0.28	0.00	0.00	20.9
38	27	-0	-4532	0	0	0	5728	--	--	16.08	16.08	0.00	0.10	0.04	0.28	0.00	0.00	20.9
39	27	-0	-4657	0	0	0	5860	--	--	16.08	16.08	0.00	0.10	0.04	0.29	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	54	-0	-3932	0	0	0	2674	--	--	16.08	16.08	0.00	0.05	0.03	0.25	0.00	0.00	20.9
2	54	-0	-2990	0	0	0	2008	--	--	16.08	16.08	0.10	0.04	0.02	0.19	0.00	0.00	20.9
3	54	-0	-2945	0	0	0	1984	--	--	16.08	16.08	0.10	0.04	0.02	0.18	0.00	0.00	20.9
4	54	-0	-3105	0	0	0	2129	--	--	16.08	16.08	0.10	0.04	0.03	0.19	0.00	0.00	20.9
5	54	-0	-3060	0	0	0	2105	--	--	16.08	16.08	0.10	0.04	0.03	0.19	0.00	0.00	20.9
6	54	-0	-3083	0	0	0	2079	--	--	16.08	16.08	0.10	0.04	0.03	0.19	0.00	0.00	20.9
7	54	-0	-2933	0	0	0	1998	--	--	16.08	16.08	0.10	0.04	0.02	0.18	0.00	0.00	20.9
8	54	-0	-3117	0	0	0	2115	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
9	54	-0	-2967	0	0	0	2035	--	--	16.08	16.08	0.10	0.04	0.02	0.19	0.00	0.00	20.9
10	54	-0	-2990	0	0	0	2008	--	--	16.08	16.08	0.10	0.04	0.02	0.19	0.00	0.00	20.9
11	54	-0	-2945	0	0	0	1984	--	--	16.08	16.08	0.10	0.04	0.02	0.18	0.00	0.00	20.9
12	54	-0	-3105	0	0	0	2129	--	--	16.08	16.08	0.10	0.04	0.03	0.19	0.00	0.00	20.9
13	54	-0	-3060	0	0	0	2105	--	--	16.08	16.08	0.10	0.04	0.03	0.19	0.00	0.00	20.9
14	54	-0	-3083	0	0	0	2079	--	--	16.08	16.08	0.10	0.04	0.03	0.19	0.00	0.00	20.9
15	54	-0	-2933	0	0	0	1998	--	--	16.08	16.08	0.10	0.04	0.02	0.18	0.00	0.00	20.9
16	54	-0	-3117	0	0	0	2115	--	--	16.08	16.08	0.10	0.04	0.03	0.20	0.00	0.00	20.9
17	54	-0	-2967	0	0	0	2035	--	--	16.08	16.08	0.10	0.04	0.02	0.19	0.00	0.00	20.9
18	54	-0	-4816	0	0	0	3556	--	--	16.08	16.08	0.00	0.06	0.04	0.30	0.00	0.00	20.9
19	54	-0	-4811	0	0	0	3583	--	--	16.08	16.08	0.00	0.06	0.04	0.30	0.00	0.00	20.9
20	54	-0	-4886	0	0	0	3621	--	--	16.08	16.08	0.00	0.06	0.04	0.31	0.00	0.00	20.9
37	54	-0	-4540	0	0	0	3256	--	--	16.08	16.08	0.00	0.06	0.04	0.28	0.00	0.00	20.9
38	54	-0	-4532	0	0	0	3301	--	--	16.08	16.08	0.00	0.06	0.04	0.28	0.00	0.00	20.9
39	54	-0	-4657	0	0	0	3365	--	--	16.08	16.08	0.00	0.06	0.04	0.29	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 99 NI 1844 NF 1895 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-6127	0	0	0	8063	--	--	16.08	16.08	0.00	0.14	0.05	0.38	0.00	0.00	20.9
2	0	-0	-4668	0	0	0	6111	--	--	16.08	16.08	0.10	0.11	0.04	0.29	0.00	0.00	20.9
3	0	-0	-4620	0	0	0	6037	--	--	16.08	16.08	0.10	0.11	0.04	0.29	0.00	0.00	20.9
4	0	-0	-4806	0	0	0	6367	--	--	16.08	16.08	0.10	0.11	0.04	0.30	0.00	0.00	20.9
5	0	-0	-4758	0	0	0	6293	--	--	16.08	16.08	0.10	0.11	0.04	0.30	0.00	0.00	20.9
6	0	-0	-4773	0	0	0	6287	--	--	16.08	16.08	0.10	0.11	0.04	0.30	0.00	0.00	20.9
7	0	-0	-4612	0	0	0	6040	--	--	16.08	16.08	0.10	0.11	0.04	0.29	0.00	0.00	20.9
8	0	-0	-4814	0	0	0	6364	--	--	16.08	16.08	0.10	0.11	0.04	0.30	0.00	0.00	20.9
9	0	-0	-4653	0	0	0	6117	--	--	16.08	16.08	0.10	0.11	0.04	0.29	0.00	0.00	20.9
10	0	-0	-4668	0	0	0	6111	--	--	16.08	16.08	0.10	0.11	0.04	0.29	0.00	0.00	20.9
11	0	-0	-4620	0	0	0	6037	--	--	16.08	16.08	0.10	0.11	0.04	0.29	0.00	0.00	20.9
12	0	-0	-4806	0	0	0	6367	--	--	16.08	16.08	0.10	0.11	0.04	0.30	0.00	0.00	20.9
13	0	-0	-4758	0	0	0	6293	--	--	16.08	16.08	0.10	0.11	0.04	0.30	0.00	0.00	20.9
14	0	-0	-4773	0	0	0	6287	--	--	16.08	16.08	0.10	0.11	0.04	0.30	0.00	0.00	20.9
15	0	-0	-4612	0	0	0	6040	--	--	16.08	16.08	0.10	0.11	0.04	0.29	0.00	0.00	20.9
16	0	-0	-4814	0	0	0	6364	--	--	16.08	16.08	0.10	0.11	0.04	0.30	0.00	0.00	20.9
17	0	-0	-4653	0	0	0	6117	--	--	16.08	16.08	0.10	0.11	0.04	0.29	0.00	0.00	20.9
18	0	-0	-7289	0	0	0	10040	--	--	16.08	16.08	0.00	0.17	0.06	0.46	0.00	0.00	20.9
19	0	-0	-7282	0	0	0	10060	--	--	16.08	16.08	0.00	0.17	0.06	0.46	0.00	0.00	20.9
20	0	-0	-7323	0	0	0	10160	--	--	16.08	16.08	0.00	0.17	0.06	0.46	0.00	0.00	20.9
37	0	-0	-6904	0	0	0	9386	--	--	16.08	16.08	0.00	0.16	0.06	0.43	0.00	0.00	20.9
38	0	-0	-6894	0	0	0	9421	--	--	16.08	16.08	0.00	0.16	0.06	0.43	0.00	0.00	20.9
39	0	-0	-6961	0	0	0	9589	--	--	16.08	16.08	0.00	0.16	0.06	0.44	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-6127	0	0	0	8063	--	--	16.08	16.08	0.00	0.14	0.05	0.38	0.00	0.00	20.9
2	27	-0	-4668	0	0	0	6111	--	--	16.08	16.08	0.10	0.11	0.04	0.29	0.00	0.00	20.9
3	27	-0	-4620	0	0	0	6037	--	--	16.08	16.08	0.10	0.11	0.04	0.29	0.00	0.00	20.9
4	27	-0	-4806	0	0	0	6367	--	--	16.08	16.08	0.10	0.11	0.04	0.30	0.00	0.00	20.9
5	27	-0	-4758	0	0	0	6293	--	--	16.08	16.08	0.10	0.11	0.04	0.30	0.00	0.00	20.9
6	27	-0	-4773	0	0	0	6287	--	--	16.08	16.08	0.10	0.11	0.04	0.30	0.00	0.00	20.9
7	27	-0	-4612	0	0	0	6040	--	--	16.08	16.08	0.10	0.11	0.04	0.29	0.00	0.00	20.9
8	27	-0	-4814	0	0	0	6364	--	--	16.08	16.08	0.10	0.11	0.04	0.30	0.00	0.00	20.9
9	27	-0	-4653	0	0	0	6117	--	--	16.08	16.08	0.10	0.11	0.04	0.29	0.00	0.00	20.9
10	27	-0	-4668	0	0	0	6111	--	--	16.08	16.08	0.10	0.11	0.04	0.29	0.00	0.00	20.9
11	27	-0	-4620	0	0	0	6037	--	--	16.08	16.08	0.10	0.11	0.04	0.29	0.00	0.00	20.9
12	27	-0	-4806	0	0	0	6367	--	--	16.08	16.08	0.10	0.11	0.04	0.30	0.00	0.00	20.9

13	27	-0	-4758	0	0	0	6293	--	--	16.08	16.08	0.10	0.11	0.04	0.30	0.00	0.00	20.9
14	27	-0	-4773	0	0	0	6287	--	--	16.08	16.08	0.10	0.11	0.04	0.30	0.00	0.00	20.9
15	27	-0	-4612	0	0	0	6040	--	--	16.08	16.08	0.10	0.11	0.04	0.29	0.00	0.00	20.9
16	27	-0	-4814	0	0	0	6364	--	--	16.08	16.08	0.10	0.11	0.04	0.30	0.00	0.00	20.9
17	27	-0	-4653	0	0	0	6117	--	--	16.08	16.08	0.10	0.11	0.04	0.29	0.00	0.00	20.9
18	27	-0	-7289	0	0	0	10040	--	--	16.08	16.08	0.00	0.17	0.06	0.46	0.00	0.00	20.9
19	27	-0	-7282	0	0	0	10060	--	--	16.08	16.08	0.00	0.17	0.06	0.46	0.00	0.00	20.9
20	27	-0	-7323	0	0	0	10160	--	--	16.08	16.08	0.00	0.17	0.06	0.46	0.00	0.00	20.9
37	27	-0	-6904	0	0	0	9386	--	--	16.08	16.08	0.00	0.16	0.06	0.43	0.00	0.00	20.9
38	27	-0	-6894	0	0	0	9421	--	--	16.08	16.08	0.00	0.16	0.06	0.43	0.00	0.00	20.9
39	27	-0	-6961	0	0	0	9589	--	--	16.08	16.08	0.00	0.16	0.06	0.44	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	54	-0	-6127	0	0	0	4780	--	--	16.08	16.08	0.00	0.08	0.05	0.38	0.00	0.00	20.9
2	54	-0	-4668	0	0	0	3610	--	--	16.08	16.08	0.10	0.06	0.04	0.29	0.00	0.00	20.9
3	54	-0	-4620	0	0	0	3562	--	--	16.08	16.08	0.10	0.06	0.04	0.29	0.00	0.00	20.9
4	54	-0	-4806	0	0	0	3793	--	--	16.08	16.08	0.10	0.07	0.04	0.30	0.00	0.00	20.9
5	54	-0	-4758	0	0	0	3744	--	--	16.08	16.08	0.10	0.07	0.04	0.30	0.00	0.00	20.9
6	54	-0	-4773	0	0	0	3730	--	--	16.08	16.08	0.10	0.07	0.04	0.30	0.00	0.00	20.9
7	54	-0	-4612	0	0	0	3569	--	--	16.08	16.08	0.10	0.06	0.04	0.29	0.00	0.00	20.9
8	54	-0	-4814	0	0	0	3785	--	--	16.08	16.08	0.10	0.07	0.04	0.30	0.00	0.00	20.9
9	54	-0	-4653	0	0	0	3624	--	--	16.08	16.08	0.10	0.06	0.04	0.29	0.00	0.00	20.9
10	54	-0	-4668	0	0	0	3610	--	--	16.08	16.08	0.10	0.06	0.04	0.29	0.00	0.00	20.9
11	54	-0	-4620	0	0	0	3562	--	--	16.08	16.08	0.10	0.06	0.04	0.29	0.00	0.00	20.9
12	54	-0	-4806	0	0	0	3793	--	--	16.08	16.08	0.10	0.07	0.04	0.30	0.00	0.00	20.9
13	54	-0	-4758	0	0	0	3744	--	--	16.08	16.08	0.10	0.07	0.04	0.30	0.00	0.00	20.9
14	54	-0	-4773	0	0	0	3730	--	--	16.08	16.08	0.10	0.07	0.04	0.30	0.00	0.00	20.9
15	54	-0	-4612	0	0	0	3569	--	--	16.08	16.08	0.10	0.06	0.04	0.29	0.00	0.00	20.9
16	54	-0	-4814	0	0	0	3785	--	--	16.08	16.08	0.10	0.07	0.04	0.30	0.00	0.00	20.9
17	54	-0	-4653	0	0	0	3624	--	--	16.08	16.08	0.10	0.06	0.04	0.29	0.00	0.00	20.9
18	54	-0	-7289	0	0	0	6136	--	--	16.08	16.08	0.00	0.10	0.06	0.46	0.00	0.00	20.9
19	54	-0	-7282	0	0	0	6160	--	--	16.08	16.08	0.00	0.11	0.06	0.46	0.00	0.00	20.9
20	54	-0	-7323	0	0	0	6239	--	--	16.08	16.08	0.00	0.11	0.06	0.46	0.00	0.00	20.9
37	54	-0	-6904	0	0	0	5688	--	--	16.08	16.08	0.00	0.10	0.06	0.43	0.00	0.00	20.9
38	54	-0	-6894	0	0	0	5728	--	--	16.08	16.08	0.00	0.10	0.06	0.43	0.00	0.00	20.9
39	54	-0	-6961	0	0	0	5860	--	--	16.08	16.08	0.00	0.10	0.06	0.44	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 100 NI 1907 NF 1844 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--	--	--	--	--	--	--	--	--	--	--		--	--	--	--	--	--
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	8168	0	0	0	5724	--	--	16.08	16.08	0.00	0.10	0.07	0.51	0.00	0.00	20.9
2	0	-0	6182	0	0	0	4340	--	--	16.08	16.08	0.10	0.08	0.05	0.39	0.00	0.00	20.9
3	0	-0	6186	0	0	0	4248	--	--	16.08	16.08	0.10	0.08	0.05	0.39	0.00	0.00	20.9
4	0	-0	6380	0	0	0	4557	--	--	16.08	16.08	0.10	0.08	0.05	0.40	0.00	0.00	20.9
5	0	-0	6383	0	0	0	4465	--	--	16.08	16.08	0.10	0.08	0.05	0.40	0.00	0.00	20.9
6	0	-0	6247	0	0	0	4523	--	--	16.08	16.08	0.10	0.08	0.05	0.39	0.00	0.00	20.9
7	0	-0	6260	0	0	0	4217	--	--	16.08	16.08	0.10	0.07	0.05	0.39	0.00	0.00	20.9
8	0	-0	6306	0	0	0	4588	--	--	16.08	16.08	0.10	0.08	0.05	0.40	0.00	0.00	20.9
9	0	-0	6319	0	0	0	4282	--	--	16.08	16.08	0.10	0.08	0.05	0.40	0.00	0.00	20.9
10	0	-0	6182	0	0	0	4340	--	--	16.08	16.08	0.10	0.08	0.05	0.39	0.00	0.00	20.9
11	0	-0	6186	0	0	0	4248	--	--	16.08	16.08	0.10	0.08	0.05	0.39	0.00	0.00	20.9
12	0	-0	6380	0	0	0	4557	--	--	16.08	16.08	0.10	0.08	0.05	0.40	0.00	0.00	20.9
13	0	-0	6383	0	0	0	4465	--	--	16.08	16.08	0.10	0.08	0.05	0.40	0.00	0.00	20.9
14	0	-0	6247	0	0	0	4523	--	--	16.08	16.08	0.10	0.08	0.05	0.39	0.00	0.00	20.9
15	0	-0	6260	0	0	0	4217	--	--	16.08	16.08	0.10	0.07	0.05	0.39	0.00	0.00	20.9
16	0	-0	6306	0	0	0	4588	--	--	16.08	16.08	0.10	0.08	0.05	0.40	0.00	0.00	20.9
17	0	-0	6319	0	0	0	4282	--	--	16.08	16.08	0.10	0.08	0.05	0.40	0.00	0.00	20.9
18	0	-0	9285	0	0	0	7204	--	--	16.08	16.08	0.00	0.12	0.08	0.58	0.00	0.00	20.9
19	0	-0	9493	0	0	0	7282	--	--	16.08	16.08	0.00	0.12	0.08	0.60	0.00	0.00	20.9
20	0	-0	8999	0	0	0	6777	--	--	16.08	16.08	0.00	0.12	0.07	0.56	0.00	0.00	20.9
37	0	-0	8766	0	0	0	6678	--	--	16.08	16.08	0.00	0.11	0.07	0.55	0.00	0.00	20.9
38	0	-0	9113	0	0	0	6808	--	--	16.08	16.08	0.00	0.12	0.08	0.57	0.00	0.00	20.9
39	0	-0	8289	0	0	0	5967	--	--	16.08	16.08	0.00	0.10	0.07	0.52	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	8168	0	0	0	16564	--	--	16.08	16.08	0.00	0.28	0.07	0.51	0.00	0.00	20.9
2	26	-0	6182	0	0	0	12545	--	--	16.08	16.08	0.10	0.22	0.05	0.39	0.00	0.00	20.9
3	26	-0	6186	0	0	0	12458	--	--	16.08	16.08	0.10	0.22	0.05	0.39	0.00	0.00	20.9
4	26	-0	6380	0	0	0	13024	--	--	16.08	16.08	0.10	0.23	0.05	0.40	0.00	0.00	20.9
5	26	-0	6383	0	0	0	12936	--	--	16.08	16.08	0.10	0.23	0.05	0.40	0.00	0.00	20.9
6	26	-0	6247	0	0	0	12813	--	--	16.08	16.08	0.10	0.23	0.05	0.39	0.00	0.00	20.9
7	26	-0	6260	0	0	0	12524	--	--	16.08	16.08	0.10	0.22	0.05	0.39	0.00	0.00	20.9
8	26	-0	6306	0	0	0	12957	--	--	16.08	16.08	0.10	0.23	0.05	0.40	0.00	0.00	20.9
9	26	-0	6319	0	0	0	12668	--	--	16.08	16.08	0.10	0.22	0.05	0.40	0.00	0.00	20.9
10	26	-0	6182	0	0	0	12545	--	--	16.08	16.08	0.10	0.22	0.05	0.39	0.00	0.00	20.9
11	26	-0	6186	0	0	0	12458	--	--	16.08	16.08	0.10	0.22	0.05	0.39	0.00	0.00	20.9
12	26	-0	6380	0	0	0	13024	--	--	16.08	16.08	0.10	0.23	0.05	0.40	0.00	0.00	20.9
13	26	-0	6383	0	0	0	12936	--	--	16.08	16.08	0.10	0.23	0.05	0.40	0.00	0.00	20.9
14	26	-0	6247	0	0	0	12813	--	--	16.08	16.08	0.10	0.23	0.05	0.39	0.00	0.00	20.9
15	26	-0	6260	0	0	0	12524	--	--	16.08	16.08	0.10	0.22	0.05	0.39	0.00	0.00	20.9
16	26	-0	6306	0	0	0	12957	--	--	16.08	16.08	0.10	0.23	0.05	0.40	0.00	0.00	20.9
17	26	-0	6319	0	0	0	12668	--	--	16.08	16.08	0.10	0.22	0.05	0.40	0.00	0.00	20.9
18	26	-0	9285	0	0	0	19525	--	--	16.08	16.08	0.00	0.33	0.08	0.58	0.00	0.00	20.9
19	26	-0	9493	0	0	0	19882	--	--	16.08	16.08	0.00	0.34	0.08	0.60	0.00	0.00	20.9
20	26	-0	8999	0	0	0	18721	--	--	16.08	16.08	0.00	0.32	0.07	0.56	0.00	0.00	20.9
37	26	-0	8766	0	0	0	18313	--	--	16.08	16.08	0.00	0.31	0.07	0.55	0.00	0.00	20.9
38	26	-0	9113	0	0	0	18904	--	--	16.08	16.08	0.00	0.32	0.08	0.57	0.00	0.00	20.9
39	26	-0	8289	0	0	0	16967	--	--	16.08	16.08	0.00	0.29	0.07	0.52	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	52	-0	8168	0	0	0	9944	--	--	16.08	16.08	0.00	0.17	0.07	0.51	0.00	0.00	20.9
2	52	-0	6182	0	0	0	7535	--	--	16.08	16.08	0.10	0.13	0.05	0.39	0.00	0.00	20.9
3	52	-0	6186	0	0	0	7445	--	--	16.08	16.08	0.10	0.13	0.05	0.39	0.00	0.00	20.9
4	52	-0	6380	0	0	0	7853	--	--	16.08	16.08	0.10	0.14	0.05	0.40	0.00	0.00	20.9
5	52	-0	6383	0	0	0	7763	--	--	16.08	16.08	0.10	0.14	0.05	0.40	0.00	0.00	20.9
6	52	-0	6247	0	0	0	7751	--	--	16.08	16.08	0.10	0.14	0.05	0.39	0.00	0.00	20.9
7	52	-0	6260	0	0	0	7451	--	--	16.08	16.08	0.10	0.13	0.05	0.39	0.00	0.00	20.9
8	52	-0	6306	0	0	0	7847	--	--	16.08	16.08	0.10	0.14	0.05	0.40	0.00	0.00	20.9

9	52	-0	6319	0	0	0	7547	--	--	16.08	16.08	0.10	0.13	0.05	0.40	0.00	0.00	20.9
10	52	-0	6182	0	0	0	7535	--	--	16.08	16.08	0.10	0.13	0.05	0.39	0.00	0.00	20.9
11	52	-0	6186	0	0	0	7445	--	--	16.08	16.08	0.10	0.13	0.05	0.39	0.00	0.00	20.9
12	52	-0	6380	0	0	0	7853	--	--	16.08	16.08	0.10	0.14	0.05	0.40	0.00	0.00	20.9
13	52	-0	6383	0	0	0	7763	--	--	16.08	16.08	0.10	0.14	0.05	0.40	0.00	0.00	20.9
14	52	-0	6247	0	0	0	7751	--	--	16.08	16.08	0.10	0.14	0.05	0.39	0.00	0.00	20.9
15	52	-0	6260	0	0	0	7451	--	--	16.08	16.08	0.10	0.13	0.05	0.39	0.00	0.00	20.9
16	52	-0	6306	0	0	0	7847	--	--	16.08	16.08	0.10	0.14	0.05	0.40	0.00	0.00	20.9
17	52	-0	6319	0	0	0	7547	--	--	16.08	16.08	0.10	0.13	0.05	0.40	0.00	0.00	20.9
18	52	-0	9285	0	0	0	12000	--	--	16.08	16.08	0.00	0.20	0.08	0.58	0.00	0.00	20.9
19	52	-0	9493	0	0	0	12190	--	--	16.08	16.08	0.00	0.21	0.08	0.60	0.00	0.00	20.9
20	52	-0	8999	0	0	0	11430	--	--	16.08	16.08	0.00	0.19	0.07	0.56	0.00	0.00	20.9
37	52	-0	8766	0	0	0	11210	--	--	16.08	16.08	0.00	0.19	0.07	0.55	0.00	0.00	20.9
38	52	-0	9113	0	0	0	11520	--	--	16.08	16.08	0.00	0.20	0.08	0.57	0.00	0.00	20.9
39	52	-0	8289	0	0	0	10250	--	--	16.08	16.08	0.00	0.17	0.07	0.52	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 101 NI 1898 NF 1907 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	6253	0	0	0	2493	--	--	16.08	16.08	0.00	0.04	0.05	0.39	0.00	0.00	20.9
2	0	-0	4718	0	0	0	1903	--	--	16.08	16.08	0.10	0.03	0.04	0.30	0.00	0.00	20.9
3	0	-0	4724	0	0	0	1808	--	--	16.08	16.08	0.10	0.03	0.04	0.30	0.00	0.00	20.9
4	0	-0	4896	0	0	0	2028	--	--	16.08	16.08	0.10	0.04	0.04	0.31	0.00	0.00	20.9
5	0	-0	4901	0	0	0	1933	--	--	16.08	16.08	0.10	0.03	0.04	0.31	0.00	0.00	20.9
6	0	-0	4774	0	0	0	2057	--	--	16.08	16.08	0.10	0.04	0.04	0.30	0.00	0.00	20.9
7	0	-0	4792	0	0	0	1742	--	--	16.08	16.08	0.10	0.03	0.04	0.30	0.00	0.00	20.9
8	0	-0	4827	0	0	0	2094	--	--	16.08	16.08	0.10	0.04	0.04	0.30	0.00	0.00	20.9
9	0	-0	4845	0	0	0	1779	--	--	16.08	16.08	0.10	0.03	0.04	0.30	0.00	0.00	20.9
10	0	-0	4718	0	0	0	1903	--	--	16.08	16.08	0.10	0.03	0.04	0.30	0.00	0.00	20.9
11	0	-0	4724	0	0	0	1808	--	--	16.08	16.08	0.10	0.03	0.04	0.30	0.00	0.00	20.9
12	0	-0	4896	0	0	0	2028	--	--	16.08	16.08	0.10	0.04	0.04	0.31	0.00	0.00	20.9
13	0	-0	4901	0	0	0	1933	--	--	16.08	16.08	0.10	0.03	0.04	0.31	0.00	0.00	20.9
14	0	-0	4774	0	0	0	2057	--	--	16.08	16.08	0.10	0.04	0.04	0.30	0.00	0.00	20.9
15	0	-0	4792	0	0	0	1742	--	--	16.08	16.08	0.10	0.03	0.04	0.30	0.00	0.00	20.9
16	0	-0	4827	0	0	0	2094	--	--	16.08	16.08	0.10	0.04	0.04	0.30	0.00	0.00	20.9
17	0	-0	4845	0	0	0	1779	--	--	16.08	16.08	0.10	0.03	0.04	0.30	0.00	0.00	20.9
18	0	-0	7130	0	0	0	3520	--	--	16.08	16.08	0.00	0.06	0.06	0.45	0.00	0.00	20.9
19	0	-0	7342	0	0	0	3489	--	--	16.08	16.08	0.00	0.06	0.06	0.46	0.00	0.00	20.9
20	0	-0	6883	0	0	0	3221	--	--	16.08	16.08	0.00	0.05	0.06	0.43	0.00	0.00	20.9
37	0	-0	6702	0	0	0	3216	--	--	16.08	16.08	0.00	0.05	0.06	0.42	0.00	0.00	20.9
38	0	-0	7055	0	0	0	3164	--	--	16.08	16.08	0.00	0.05	0.06	0.44	0.00	0.00	20.9
39	0	-0	6290	0	0	0	2717	--	--	16.08	16.08	0.00	0.05	0.05	0.39	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	6253	0	0	0	10791	--	--	16.08	16.08	0.00	0.18	0.05	0.39	0.00	0.00	20.9
2	26	-0	4718	0	0	0	8164	--	--	16.08	16.08	0.10	0.14	0.04	0.30	0.00	0.00	20.9
3	26	-0	4724	0	0	0	8077	--	--	16.08	16.08	0.10	0.14	0.04	0.30	0.00	0.00	20.9
4	26	-0	4896	0	0	0	8525	--	--	16.08	16.08	0.10	0.15	0.04	0.31	0.00	0.00	20.9
5	26	-0	4901	0	0	0	8437	--	--	16.08	16.08	0.10	0.15	0.04	0.31	0.00	0.00	20.9
6	26	-0	4774	0	0	0	8392	--	--	16.08	16.08	0.10	0.15	0.04	0.30	0.00	0.00	20.9
7	26	-0	4792	0	0	0	8101	--	--	16.08	16.08	0.10	0.14	0.04	0.30	0.00	0.00	20.9
8	26	-0	4827	0	0	0	8500	--	--	16.08	16.08	0.10	0.15	0.04	0.30	0.00	0.00	20.9
9	26	-0	4845	0	0	0	8209	--	--	16.08	16.08	0.10	0.15	0.04	0.30	0.00	0.00	20.9
10	26	-0	4718	0	0	0	8164	--	--	16.08	16.08	0.10	0.14	0.04	0.30	0.00	0.00	20.9
11	26	-0	4724	0	0	0	8077	--	--	16.08	16.08	0.10	0.14	0.04	0.30	0.00	0.00	20.9
12	26	-0	4896	0	0	0	8525	--	--	16.08	16.08	0.10	0.15	0.04	0.31	0.00	0.00	20.9
13	26	-0	4901	0	0	0	8437	--	--	16.08	16.08	0.10	0.15	0.04	0.31	0.00	0.00	20.9
14	26	-0	4774	0	0	0	8392	--	--	16.08	16.08	0.10	0.15	0.04	0.30	0.00	0.00	20.9
15	26	-0	4792	0	0	0	8101	--	--	16.08	16.08	0.10	0.14	0.04	0.30	0.00	0.00	20.9
16	26	-0	4827	0	0	0	8500	--	--	16.08	16.08	0.10	0.15	0.04	0.30	0.00	0.00	20.9
17	26	-0	4845	0	0	0	8209	--	--	16.08	16.08	0.10	0.15	0.04	0.30	0.00	0.00	20.9
18	26	-0	7130	0	0	0	12982	--	--	16.08	16.08	0.00	0.22	0.06	0.45	0.00	0.00	20.9
19	26	-0	7342	0	0	0	13232	--	--	16.08	16.08	0.00	0.23	0.06	0.46	0.00	0.00	20.9
20	26	-0	6883	0	0	0	12355	--	--	16.08	16.08	0.00	0.21	0.06	0.43	0.00	0.00	20.9
37	26	-0	6702	0	0	0	12110	--	--	16.08	16.08	0.00	0.21	0.06	0.42	0.00	0.00	20.9
38	26	-0	7055	0	0	0	12526	--	--	16.08	16.08	0.00	0.21	0.06	0.44	0.00	0.00	20.9
39	26	-0	6290	0	0	0	11064	--	--	16.08	16.08	0.00	0.19	0.05	0.39	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	52	-0	6253	0	0	0	5724	--	--	16.08	16.08	0.00	0.10	0.05	0.39	0.00	0.00	20.9
2	52	-0	4718	0	0	0	4340	--	--	16.08	16.08	0.10	0.08	0.04	0.30	0.00	0.00	20.9
3	52	-0	4724	0	0	0	4248	--	--	16.08	16.08	0.10	0.08	0.04	0.30	0.00	0.00	20.9
4	52	-0	4896	0	0	0	4557	--	--	16.08	16.08	0.10	0.08	0.04	0.31	0.00	0.00	20.9
5	52	-0	4901	0	0	0	4465	--	--	16.08	16.08	0.10	0.08	0.04	0.31	0.00	0.00	20.9
6	52	-0	4774	0	0	0	4523	--	--	16.08	16.08	0.10	0.08	0.04	0.30	0.00	0.00	20.9
7	52	-0	4792	0	0	0	4217	--	--	16.08	16.08	0.10	0.07	0.04	0.30	0.00	0.00	20.9
8	52	-0	4827	0	0	0	4588	--	--	16.08	16.08	0.10	0.08	0.04	0.30	0.00	0.00	20.9
9	52	-0	4845	0	0	0	4282	--	--	16.08	16.08	0.10	0.08	0.04	0.30	0.00	0.00	20.9
10	52	-0	4718	0	0	0	4340	--	--	16.08	16.08	0.10	0.08	0.04	0.30	0.00	0.00	20.9
11	52	-0	4724	0	0	0	4248	--	--	16.08	16.08	0.10	0.08	0.04	0.30	0.00	0.00	20.9
12	52	-0	4896	0	0	0	4557	--	--	16.08	16.08	0.10	0.08	0.04	0.31	0.00	0.00	20.9
13	52	-0	4901	0	0	0	4465	--	--	16.08	16.08	0.10	0.08	0.04	0.31	0.00	0.00	20.9
14	52	-0	4774	0	0	0	4523	--	--	16.08	16.08	0.10	0.08	0.04	0.30	0.00	0.00	20.9
15	52	-0	4792	0	0	0	4217	--	--	16.08	16.08	0.10	0.07	0.04	0.30	0.00	0.00	20.9
16	52	-0	4827	0	0	0	4588	--	--	16.08	16.08	0.10	0.08	0.04	0.30	0.00	0.00	20.9
17	52	-0	4845	0	0	0	4282	--	--	16.08	16.08	0.10	0.08	0.04	0.30	0.00	0.00	20.9
18	52	-0	7130	0	0	0	7204	--	--	16.08	16.08	0.00	0.12	0.06	0.45	0.00	0.00	20.9
19	52	-0	7342	0	0	0	7282	--	--	16.08	16.08	0.00	0.12	0.06	0.46	0.00	0.00	20.9
20	52	-0	6883	0	0	0	6777	--	--	16.08	16.08	0.00	0.12	0.06	0.43	0.00	0.00	20.9
37	52	-0	6702	0	0	0	6678	--	--	16.08	16.08	0.00	0.11	0.06	0.42	0.00	0.00	20.9
38	52	-0	7055	0	0	0	6808	--	--	16.08	16.08	0.00	0.12	0.06	0.44	0.00	0.00	20.9
39	52	-0	6290	0	0	0	5967	--	--	16.08	16.08	0.00	0.10	0.05	0.39	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 102 NI 1905 NF 1898 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	4498	0	0	0	169	--	--	16.08	16.08	0.00	0.00	0.04	0.28	0.00	0.00	20.9
2	0	-0	3377	0	0	0	158	--	--	16.08	16.08	0.10	0.00	0.03	0.21	0.00	0.00	20.9
3	0	-0	3382	0	0	0	60	--	--	16.08	16.08	0.10	0.00	0.03	0.21	0.00	0.00	20.9
4	0	-0	3537	0	0	0	200	--	--	16.08	16.08	0.10	0.00	0.03	0.22	0.00	0.00	20.9
5	0	-0	3543	0	0	0	103	--	--	16.08	16.08	0.10	0.00	0.03	0.22	0.00	0.00	20.9
6	0	-0	3427	0	0	0	286	--	--	16.08	16.08	0.10	0.01	0.03	0.21	0.00	0.00	20.9
7	0	-0	3445	0	0	0	-38	--	--	16.08	16.08	0.29	0.00	0.03	0.22	0.00	0.00	20.9
8	0	-0	3475	0	0	0	299	--	--	16.08	16.08	0.10	0.01	0.03	0.22	0.00	0.00	20.9
9	0	-0	3493	0	0	0	-26	--	--	16.08	16.08	0.29	0.00	0.03	0.22	0.00	0.00	20.9
10	0	-0	3377	0	0	0	158	--	--	16.08	16.08	0.10	0.00	0.03	0.21	0.00	0.00	20.9
11	0	-0	3382	0	0	0	60	--	--	16.08	16.08	0.10	0.00	0.03	0.21	0.00	0.00	20.9
12	0	-0	3537	0	0	0	200	--	--	16.08	16.08	0.10	0.00	0.03	0.22	0.00	0.00	20.9
13	0	-0	3543	0	0	0	103	--	--	16.08	16.08	0.10	0.00	0.03	0.22	0.00	0.00	20.9
14	0	-0	3427	0	0	0	286	--	--	16.08	16.08	0.10	0.01	0.03	0.21	0.00	0.00	20.9
15	0	-0	3445	0	0	0	-38	--	--	16.08	16.08	0.29	0.00	0.03	0.22	0.00	0.00	20.9
16	0	-0	3475	0	0	0	299	--	--	16.08	16.08	0.10	0.01	0.03	0.22	0.00	0.00	20.9
17	0	-0	3493	0	0	0	-26	--	--	16.08	16.08	0.29	0.00	0.03	0.22	0.00	0.00	20.9
18	0	-0	5163	0	0	0	853	--	--	16.08	16.08	0.00	0.01	0.04	0.32	0.00	0.00	20.9
19	0	-0	5380	0	0	0	710	--	--	16.08	16.08	0.00	0.01	0.04	0.34	0.00	0.00	20.9
20	0	-0	4954	0	0	0	661	--	--	16.08	16.08	0.00	0.01	0.04	0.31	0.00	0.00	20.9
37	0	-0	4815	0	0	0	728	--	--	16.08	16.08	0.00	0.01	0.04	0.30	0.00	0.00	20.9
38	0	-0	5176	0	0	0	489	--	--	16.08	16.08	0.00	0.01	0.04	0.32	0.00	0.00	20.9
39	0	-0	4467	0	0	0	409	--	--	16.08	16.08	0.00	0.01	0.04	0.28	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	26	-0	4498	0	0	0	6138	--	--	16.08	16.08	0.00	0.10	0.04	0.28	0.00	0.00	20.9
2	26	-0	3377	0	0	0	4640	--	--	16.08	16.08	0.10	0.08	0.03	0.21	0.00	0.00	20.9
3	26	-0	3382	0	0	0	4549	--	--	16.08	16.08	0.10	0.08	0.03	0.21	0.00	0.00	20.9
4	26	-0	3537	0	0	0	4894	--	--	16.08	16.08	0.10	0.09	0.03	0.22	0.00	0.00	20.9
5	26	-0	3543	0	0	0	4804	--	--	16.08	16.08	0.10	0.09	0.03	0.22	0.00	0.00	20.9
6	26	-0	3427	0	0	0	4834	--	--	16.08	16.08	0.10	0.09	0.03	0.21	0.00	0.00	20.9
7	26	-0	3445	0	0	0	4534	--	--	16.08	16.08	0.10	0.08	0.03	0.22	0.00	0.00	20.9
8	26	-0	3475	0	0	0	4910	--	--	16.08	16.08	0.10	0.09	0.03	0.22	0.00	0.00	20.9
9	26	-0	3493	0	0	0	4610	--	--	16.08	16.08	0.10	0.08	0.03	0.22	0.00	0.00	20.9
10	26	-0	3377	0	0	0	4640	--	--	16.08	16.08	0.10	0.08	0.03	0.21	0.00	0.00	20.9
11	26	-0	3382	0	0	0	4549	--	--	16.08	16.08	0.10	0.08	0.03	0.21	0.00	0.00	20.9
12	26	-0	3537	0	0	0	4894	--	--	16.08	16.08	0.10	0.09	0.03	0.22	0.00	0.00	20.9
13	26	-0	3543	0	0	0	4804	--	--	16.08	16.08	0.10	0.09	0.03	0.22	0.00	0.00	20.9
14	26	-0	3427	0	0	0	4834	--	--	16.08	16.08	0.10	0.09	0.03	0.21	0.00	0.00	20.9
15	26	-0	3445	0	0	0	4534	--	--	16.08	16.08	0.10	0.08	0.03	0.22	0.00	0.00	20.9
16	26	-0	3475	0	0	0	4910	--	--	16.08	16.08	0.10	0.09	0.03	0.22	0.00	0.00	20.9
17	26	-0	3493	0	0	0	4610	--	--	16.08	16.08	0.10	0.08	0.03	0.22	0.00	0.00	20.9
18	26	-0	5163	0	0	0	7704	--	--	16.08	16.08	0.00	0.13	0.04	0.32	0.00	0.00	20.9
19	26	-0	5380	0	0	0	7849	--	--	16.08	16.08	0.00	0.13	0.04	0.34	0.00	0.00	20.9
20	26	-0	4954	0	0	0	7236	--	--	16.08	16.08	0.00	0.12	0.04	0.31	0.00	0.00	20.9
37	26	-0	4815	0	0	0	7118	--	--	16.08	16.08	0.00	0.12	0.04	0.30	0.00	0.00	20.9
38	26	-0	5176	0	0	0	7358	--	--	16.08	16.08	0.00	0.13	0.04	0.32	0.00	0.00	20.9
39	26	-0	4467	0	0	0	6337	--	--	16.08	16.08	0.00	0.11	0.04	0.28	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	52	-0	4498	0	0	0	2493	--	--	16.08	16.08	0.00	0.04	0.04	0.28	0.00	0.00	20.9
2	52	-0	3377	0	0	0	1903	--	--	16.08	16.08	0.10	0.03	0.03	0.21	0.00	0.00	20.9
3	52	-0	3382	0	0	0	1808	--	--	16.08	16.08	0.10	0.03	0.03	0.21	0.00	0.00	20.9
4	52	-0	3537	0	0	0	2028	--	--	16.08	16.08	0.10	0.04	0.03	0.22	0.00	0.00	20.9
5	52	-0	3543	0	0	0	1933	--	--	16.08	16.08	0.10	0.03	0.03	0.22	0.00	0.00	20.9
6	52	-0	3427	0	0	0	2057	--	--	16.08	16.08	0.10	0.04	0.03	0.21	0.00	0.00	20.9
7	52	-0	3445	0	0	0	1742	--	--	16.08	16.08	0.10	0.03	0.03	0.22	0.00	0.00	20.9
8	52	-0	3475	0	0	0	2094	--	--	16.08	16.08	0.10	0.04	0.03	0.22	0.00	0.00	20.9
9	52	-0	3493	0	0	0	1779	--	--	16.08	16.08	0.10	0.03	0.03	0.22	0.00	0.00	20.9
10	52	-0	3377	0	0	0	1903	--	--	16.08	16.08	0.10	0.03	0.03	0.21	0.00	0.00	20.9
11	52	-0	3382	0	0	0	1808	--	--	16.08	16.08	0.10	0.03	0.03	0.21	0.00	0.00	20.9
12	52	-0	3537	0	0	0	2028	--	--	16.08	16.08	0.10	0.04	0.03	0.22	0.00	0.00	20.9
13	52	-0	3543	0	0	0	1933	--	--	16.08	16.08	0.10	0.03	0.03	0.22	0.00	0.00	20.9
14	52	-0	3427	0	0	0	2057	--	--	16.08	16.08	0.10	0.04	0.03	0.21	0.00	0.00	20.9
15	52	-0	3445	0	0	0	1742	--	--	16.08	16.08	0.10	0.03	0.03	0.22	0.00	0.00	20.9
16	52	-0	3475	0	0	0	2094	--	--	16.08	16.08	0.10	0.04	0.03	0.22	0.00	0.00	20.9
17	52	-0	3493	0	0	0	1779	--	--	16.08	16.08	0.10	0.03	0.03	0.22	0.00	0.00	20.9
18	52	-0	5163	0	0	0	3520	--	--	16.08	16.08	0.00	0.06	0.04	0.32	0.00	0.00	20.9
19	52	-0	5380	0	0	0	3489	--	--	16.08	16.08	0.00	0.06	0.04	0.34	0.00	0.00	20.9
20	52	-0	4954	0	0	0	3221	--	--	16.08	16.08	0.00	0.05	0.04	0.31	0.00	0.00	20.9
37	52	-0	4815	0	0	0	3216	--	--	16.08	16.08	0.00	0.05	0.04	0.30	0.00	0.00	20.9
38	52	-0	5176	0	0	0	3164	--	--	16.08	16.08	0.00	0.05	0.04	0.32	0.00	0.00	20.9
39	52	-0	4467	0	0	0	2717	--	--	16.08	16.08	0.00	0.05	0.04	0.28	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 103 NI 1906 NF 1905 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	2911	0	0	0	-1335	--	--	16.08	16.08	0.18	0.02	0.02	0.18	0.00	0.00	20.9
2	0	-0	2164	0	0	0	-960	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
3	0	-0	2168	0	0	0	-1060	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
4	0	-0	2311	0	0	0	-994	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
5	0	-0	2314	0	0	0	-1093	--	--	16.08	16.08	0.29	0.02	0.02	0.15	0.00	0.00	20.9
6	0	-0	2212	0	0	0	-857	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
7	0	-0	2223	0	0	0	-1187	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
8	0	-0	2256	0	0	0	-867	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
9	0	-0	2267	0	0	0	-1197	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
10	0	-0	2164	0	0	0	-960	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
11	0	-0	2168	0	0	0	-1060	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
12	0	-0	2311	0	0	0	-994	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
13	0	-0	2314	0	0	0	-1093	--	--	16.08	16.08	0.29	0.02	0.02	0.15	0.00	0.00	20.9
14	0	-0	2212	0	0	0	-857	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
15	0	-0	2223	0	0	0	-1187	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
16	0	-0	2256	0	0	0	-867	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9

17	0	-0	2267	0	0	0	-1197	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
18	0	-0	3395	0	0	0	-902	--	--	16.08	16.08	0.18	0.01	0.03	0.21	0.00	0.00	20.9
19	0	-0	3619	0	0	0	-1160	--	--	16.08	16.08	0.18	0.02	0.03	0.23	0.00	0.00	20.9
20	0	-0	3224	0	0	0	-1004	--	--	16.08	16.08	0.18	0.02	0.03	0.20	0.00	0.00	20.9
37	0	-0	3115	0	0	0	-882	--	--	16.08	16.08	0.18	0.01	0.03	0.20	0.00	0.00	20.9
38	0	-0	3487	0	0	0	-1313	--	--	16.08	16.08	0.18	0.02	0.03	0.22	0.00	0.00	20.9
39	0	-0	2828	0	0	0	-1053	--	--	16.08	16.08	0.18	0.02	0.02	0.18	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	2911	0	0	0	-1335	--	--	16.08	16.08	0.18	0.02	0.02	0.18	0.00	0.00	20.9
2	26	-0	2164	0	0	0	-960	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
3	26	-0	2168	0	0	0	-1060	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
4	26	-0	2311	0	0	0	-994	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
5	26	-0	2314	0	0	0	-1093	--	--	16.08	16.08	0.29	0.02	0.02	0.15	0.00	0.00	20.9
6	26	-0	2212	0	0	0	-857	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
7	26	-0	2223	0	0	0	-1187	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
8	26	-0	2256	0	0	0	-867	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
9	26	-0	2267	0	0	0	-1197	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
10	26	-0	2164	0	0	0	-960	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
11	26	-0	2168	0	0	0	-1060	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
12	26	-0	2311	0	0	0	-994	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
13	26	-0	2314	0	0	0	-1093	--	--	16.08	16.08	0.29	0.02	0.02	0.15	0.00	0.00	20.9
14	26	-0	2212	0	0	0	-857	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
15	26	-0	2223	0	0	0	-1187	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
16	26	-0	2256	0	0	0	-867	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
17	26	-0	2267	0	0	0	-1197	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
18	26	-0	3395	0	0	0	-902	--	--	16.08	16.08	0.18	0.01	0.03	0.21	0.00	0.00	20.9
19	26	-0	3619	0	0	0	-1160	--	--	16.08	16.08	0.18	0.02	0.03	0.23	0.00	0.00	20.9
20	26	-0	3224	0	0	0	-1004	--	--	16.08	16.08	0.18	0.02	0.03	0.20	0.00	0.00	20.9
37	26	-0	3115	0	0	0	-882	--	--	16.08	16.08	0.18	0.01	0.03	0.20	0.00	0.00	20.9
38	26	-0	3487	0	0	0	-1313	--	--	16.08	16.08	0.18	0.02	0.03	0.22	0.00	0.00	20.9
39	26	-0	2828	0	0	0	-1053	--	--	16.08	16.08	0.18	0.02	0.02	0.18	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	52	-0	2911	0	0	0	169	--	--	16.08	16.08	0.00	0.00	0.02	0.18	0.00	0.00	20.9
2	52	-0	2164	0	0	0	158	--	--	16.08	16.08	0.10	0.00	0.02	0.14	0.00	0.00	20.9
3	52	-0	2168	0	0	0	60	--	--	16.08	16.08	0.10	0.00	0.02	0.14	0.00	0.00	20.9
4	52	-0	2311	0	0	0	200	--	--	16.08	16.08	0.10	0.00	0.02	0.14	0.00	0.00	20.9
5	52	-0	2314	0	0	0	103	--	--	16.08	16.08	0.10	0.00	0.02	0.15	0.00	0.00	20.9
6	52	-0	2212	0	0	0	286	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
7	52	-0	2223	0	0	0	-1187	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
8	52	-0	2256	0	0	0	299	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
9	52	-0	2267	0	0	0	-1197	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
10	52	-0	2164	0	0	0	158	--	--	16.08	16.08	0.10	0.00	0.02	0.14	0.00	0.00	20.9
11	52	-0	2168	0	0	0	60	--	--	16.08	16.08	0.10	0.00	0.02	0.14	0.00	0.00	20.9
12	52	-0	2311	0	0	0	200	--	--	16.08	16.08	0.10	0.00	0.02	0.14	0.00	0.00	20.9
13	52	-0	2314	0	0	0	103	--	--	16.08	16.08	0.10	0.00	0.02	0.15	0.00	0.00	20.9
14	52	-0	2212	0	0	0	286	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
15	52	-0	2223	0	0	0	-1187	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
16	52	-0	2256	0	0	0	299	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
17	52	-0	2267	0	0	0	-1197	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
18	52	-0	3395	0	0	0	853	--	--	16.08	16.08	0.00	0.01	0.03	0.21	0.00	0.00	20.9
19	52	-0	3619	0	0	0	710	--	--	16.08	16.08	0.00	0.01	0.03	0.23	0.00	0.00	20.9
20	52	-0	3224	0	0	0	661	--	--	16.08	16.08	0.00	0.01	0.03	0.20	0.00	0.00	20.9
37	52	-0	3115	0	0	0	728	--	--	16.08	16.08	0.00	0.01	0.03	0.20	0.00	0.00	20.9
38	52	-0	3487	0	0	0	489	--	--	16.08	16.08	0.00	0.01	0.03	0.22	0.00	0.00	20.9
39	52	-0	2828	0	0	0	409	--	--	16.08	16.08	0.00	0.01	0.02	0.18	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 104 NI 1897 NF 1906 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	1489	0	0	0	-2104	--	--	16.08	16.08	0.18	0.03	0.01	0.09	0.00	0.00	20.9
2	0	-0	1077	0	0	0	-1517	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
3	0	-0	1076	0	0	0	-1615	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
4	0	-0	1214	0	0	0	-1621	--	--	16.08	16.08	0.29	0.03	0.01	0.08	0.00	0.00	20.9
5	0	-0	1213	0	0	0	-1720	--	--	16.08	16.08	0.29	0.03	0.01	0.08	0.00	0.00	20.9
6	0	-0	1126	0	0	0	-1438	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
7	0	-0	1123	0	0	0	-1767	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
8	0	-0	1167	0	0	0	-1470	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
9	0	-0	1164	0	0	0	-1798	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
10	0	-0	1077	0	0	0	-1517	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
11	0	-0	1076	0	0	0	-1615	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
12	0	-0	1214	0	0	0	-1621	--	--	16.08	16.08	0.29	0.03	0.01	0.08	0.00	0.00	20.9
13	0	-0	1213	0	0	0	-1720	--	--	16.08	16.08	0.29	0.03	0.01	0.08	0.00	0.00	20.9
14	0	-0	1126	0	0	0	-1438	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
15	0	-0	1123	0	0	0	-1767	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
16	0	-0	1167	0	0	0	-1470	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
17	0	-0	1164	0	0	0	-1798	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
18	0	-0	1828	0	0	0	-1846	--	--	16.08	16.08	0.18	0.03	0.02	0.11	0.00	0.00	20.9
19	0	-0	2059	0	0	0	-2224	--	--	16.08	16.08	0.18	0.04	0.02	0.13	0.00	0.00	20.9
20	0	-0	1690	0	0	0	-1877	--	--	16.08	16.08	0.18	0.03	0.01	0.11	0.00	0.00	20.9
37	0	-0	1601	0	0	0	-1709	--	--	16.08	16.08	0.18	0.03	0.01	0.10	0.00	0.00	20.9
38	0	-0	1986	0	0	0	-2339	--	--	16.08	16.08	0.18	0.04	0.02	0.12	0.00	0.00	20.9
39	0	-0	1371	0	0	0	-1761	--	--	16.08	16.08	0.18	0.03	0.01	0.09	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	1489	0	0	0	-2104	--	--	16.08	16.08	0.18	0.03	0.01	0.09	0.00	0.00	20.9
2	26	-0	1077	0	0	0	-1517	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
3	26	-0	1076	0	0	0	-1615	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
4	26	-0	1214	0	0	0	-1621	--	--	16.08	16.08	0.29	0.03	0.01	0.08	0.00	0.00	20.9
5	26	-0	1213	0	0	0	-1720	--	--	16.08	16.08	0.29	0.03	0.01	0.08	0.00	0.00	20.9
6	26	-0	1126	0	0	0	-1438	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
7	26	-0	1123	0	0	0	-1767	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
8	26	-0	1167	0	0	0	-1470	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
9	26	-0	1164	0	0	0	-1798	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
10	26	-0	1077	0	0	0	-1517	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
11	26	-0	1076	0	0	0	-1615	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
12	26	-0	1214	0	0	0	-1621	--	--	16.08	16.08	0.29	0.03	0.01	0.08	0.00	0.00	20.9

13	26	-0	1213	0	0	0	-1720	--	--	16.08	16.08	0.29	0.03	0.01	0.08	0.00	0.00	20.9
14	26	-0	1126	0	0	0	-1438	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
15	26	-0	1123	0	0	0	-1767	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
16	26	-0	1167	0	0	0	-1470	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
17	26	-0	1164	0	0	0	-1798	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
18	26	-0	1828	0	0	0	-1846	--	--	16.08	16.08	0.18	0.03	0.02	0.11	0.00	0.00	20.9
19	26	-0	2059	0	0	0	-2224	--	--	16.08	16.08	0.18	0.04	0.02	0.13	0.00	0.00	20.9
20	26	-0	1690	0	0	0	-1877	--	--	16.08	16.08	0.18	0.03	0.01	0.11	0.00	0.00	20.9
37	26	-0	1601	0	0	0	-1709	--	--	16.08	16.08	0.18	0.03	0.01	0.10	0.00	0.00	20.9
38	26	-0	1986	0	0	0	-2339	--	--	16.08	16.08	0.18	0.04	0.02	0.12	0.00	0.00	20.9
39	26	-0	1371	0	0	0	-1761	--	--	16.08	16.08	0.18	0.03	0.01	0.09	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	52	-0	1489	0	0	0	-2104	--	--	16.08	16.08	0.18	0.03	0.01	0.09	0.00	0.00	20.9
2	52	-0	1077	0	0	0	-1517	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
3	52	-0	1076	0	0	0	-1615	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
4	52	-0	1214	0	0	0	-1621	--	--	16.08	16.08	0.29	0.03	0.01	0.08	0.00	0.00	20.9
5	52	-0	1213	0	0	0	-1720	--	--	16.08	16.08	0.29	0.03	0.01	0.08	0.00	0.00	20.9
6	52	-0	1126	0	0	0	-1438	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
7	52	-0	1123	0	0	0	-1767	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
8	52	-0	1167	0	0	0	-1470	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
9	52	-0	1164	0	0	0	-1798	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
10	52	-0	1077	0	0	0	-1517	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
11	52	-0	1076	0	0	0	-1615	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
12	52	-0	1214	0	0	0	-1621	--	--	16.08	16.08	0.29	0.03	0.01	0.08	0.00	0.00	20.9
13	52	-0	1213	0	0	0	-1720	--	--	16.08	16.08	0.29	0.03	0.01	0.08	0.00	0.00	20.9
14	52	-0	1126	0	0	0	-1438	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
15	52	-0	1123	0	0	0	-1767	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
16	52	-0	1167	0	0	0	-1470	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
17	52	-0	1164	0	0	0	-1798	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
18	52	-0	1828	0	0	0	-1846	--	--	16.08	16.08	0.18	0.03	0.02	0.11	0.00	0.00	20.9
19	52	-0	2059	0	0	0	-2224	--	--	16.08	16.08	0.18	0.04	0.02	0.13	0.00	0.00	20.9
20	52	-0	1690	0	0	0	-1877	--	--	16.08	16.08	0.18	0.03	0.01	0.11	0.00	0.00	20.9
37	52	-0	1601	0	0	0	-1709	--	--	16.08	16.08	0.18	0.03	0.01	0.10	0.00	0.00	20.9
38	52	-0	1986	0	0	0	-2339	--	--	16.08	16.08	0.18	0.04	0.02	0.12	0.00	0.00	20.9
39	52	-0	1371	0	0	0	-1761	--	--	16.08	16.08	0.18	0.03	0.01	0.09	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 105 NI 1258 NF 1897 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	222	0	0	0	-2218	--	--	16.08	16.08	0.18	0.04	0.00	0.01	0.00	0.00	20.9
2	0	-0	110	0	0	0	-1574	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
3	0	-0	101	0	0	0	-1668	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
4	0	-0	240	0	0	0	-1745	--	--	16.08	16.08	0.29	0.03	0.00	0.02	0.00	0.00	20.9
5	0	-0	231	0	0	0	-1839	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
6	0	-0	165	0	0	0	-1524	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
7	0	-0	137	0	0	0	-1838	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
8	0	-0	204	0	0	0	-1575	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
9	0	-0	176	0	0	0	-1889	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
10	0	-0	110	0	0	0	-1574	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
11	0	-0	101	0	0	0	-1668	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
12	0	-0	240	0	0	0	-1745	--	--	16.08	16.08	0.29	0.03	0.00	0.02	0.00	0.00	20.9
13	0	-0	231	0	0	0	-1839	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
14	0	-0	165	0	0	0	-1524	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
15	0	-0	137	0	0	0	-1838	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
16	0	-0	204	0	0	0	-1575	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
17	0	-0	176	0	0	0	-1889	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
18	0	-0	451	0	0	0	-2079	--	--	16.08	16.08	0.18	0.03	0.00	0.03	0.00	0.00	20.9
19	0	-0	690	0	0	0	-2580	--	--	16.08	16.08	0.18	0.04	0.01	0.04	0.00	0.00	20.9
20	0	-0	344	0	0	0	-2055	--	--	16.08	16.08	0.18	0.03	0.00	0.02	0.00	0.00	20.9
37	0	-0	266	0	0	0	-1846	--	--	16.08	16.08	0.18	0.03	0.00	0.02	0.00	0.00	20.9
38	0	-0	664	0	0	0	-2682	--	--	16.08	16.08	0.18	0.04	0.01	0.04	0.00	0.00	20.9
39	0	-0	88	0	0	0	-1806	--	--	16.08	16.08	0.18	0.03	0.00	0.01	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	222	0	0	0	-2218	--	--	16.08	16.08	0.18	0.04	0.00	0.01	0.00	0.00	20.9
2	26	-0	110	0	0	0	-1574	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
3	26	-0	101	0	0	0	-1668	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
4	26	-0	240	0	0	0	-1745	--	--	16.08	16.08	0.29	0.03	0.00	0.02	0.00	0.00	20.9
5	26	-0	231	0	0	0	-1839	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
6	26	-0	165	0	0	0	-1524	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
7	26	-0	137	0	0	0	-1838	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
8	26	-0	204	0	0	0	-1575	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
9	26	-0	176	0	0	0	-1889	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
10	26	-0	110	0	0	0	-1574	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
11	26	-0	101	0	0	0	-1668	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
12	26	-0	240	0	0	0	-1745	--	--	16.08	16.08	0.29	0.03	0.00	0.02	0.00	0.00	20.9
13	26	-0	231	0	0	0	-1839	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
14	26	-0	165	0	0	0	-1524	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
15	26	-0	137	0	0	0	-1838	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
16	26	-0	204	0	0	0	-1575	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
17	26	-0	176	0	0	0	-1889	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
18	26	-0	451	0	0	0	-2079	--	--	16.08	16.08	0.18	0.03	0.00	0.03	0.00	0.00	20.9
19	26	-0	690	0	0	0	-2580	--	--	16.08	16.08	0.18	0.04	0.01	0.04	0.00	0.00	20.9
20	26	-0	344	0	0	0	-2055	--	--	16.08	16.08	0.18	0.03	0.00	0.02	0.00	0.00	20.9
37	26	-0	266	0	0	0	-1846	--	--	16.08	16.08	0.18	0.03	0.00	0.02	0.00	0.00	20.9
38	26	-0	664	0	0	0	-2682	--	--	16.08	16.08	0.18	0.04	0.01	0.04	0.00	0.00	20.9
39	26	-0	88	0	0	0	-1806	--	--	16.08	16.08	0.18	0.03	0.00	0.01	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	52	-0	222	0	0	0	-2218	--	--	16.08	16.08	0.18	0.04	0.00	0.01	0.00	0.00	20.9
2	52	-0	110	0	0	0	-1574	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
3	52	-0	101	0	0	0	-1668	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
4	52	-0	240	0	0	0	-1745	--	--	16.08	16.08	0.29	0.03	0.00	0.02	0.00	0.00	20.9
5	52	-0	231	0	0	0	-1839	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
6	52	-0	165	0	0	0	-1524	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
7	52	-0	137	0	0	0	-1838	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
8	52	-0	204	0	0	0	-1575	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9

9	52	-0	176	0	0	0	-1889	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
10	52	-0	110	0	0	0	-1574	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
11	52	-0	101	0	0	0	-1668	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
12	52	-0	240	0	0	0	-1745	--	--	16.08	16.08	0.29	0.03	0.00	0.02	0.00	0.00	20.9
13	52	-0	231	0	0	0	-1839	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
14	52	-0	165	0	0	0	-1524	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
15	52	-0	137	0	0	0	-1838	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
16	52	-0	204	0	0	0	-1575	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
17	52	-0	176	0	0	0	-1889	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
18	52	-0	451	0	0	0	-2079	--	--	16.08	16.08	0.18	0.03	0.00	0.03	0.00	0.00	20.9
19	52	-0	690	0	0	0	-2580	--	--	16.08	16.08	0.18	0.04	0.01	0.04	0.00	0.00	20.9
20	52	-0	344	0	0	0	-2055	--	--	16.08	16.08	0.18	0.03	0.00	0.02	0.00	0.00	20.9
37	52	-0	266	0	0	0	-1846	--	--	16.08	16.08	0.18	0.03	0.00	0.02	0.00	0.00	20.9
38	52	-0	664	0	0	0	-2682	--	--	16.08	16.08	0.18	0.04	0.01	0.04	0.00	0.00	20.9
39	52	-0	88	0	0	0	-1806	--	--	16.08	16.08	0.18	0.03	0.00	0.01	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 106 NI 1970 NF 1278 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	1504	0	0	0	-3808	--	--	16.08	16.08	0.18	0.06	0.01	0.09	0.00	0.00	20.9
2	0	-0	1134	0	0	0	-2950	--	--	16.08	16.08	0.29	0.05	0.01	0.07	0.00	0.00	20.9
3	0	-0	1199	0	0	0	-2804	--	--	16.08	16.08	0.29	0.05	0.01	0.08	0.00	0.00	20.9
4	0	-0	1115	0	0	0	-3054	--	--	16.08	16.08	0.29	0.05	0.01	0.07	0.00	0.00	20.9
5	0	-0	1180	0	0	0	-2908	--	--	16.08	16.08	0.29	0.05	0.01	0.07	0.00	0.00	20.9
6	0	-0	1051	0	0	0	-3156	--	--	16.08	16.08	0.29	0.05	0.01	0.07	0.00	0.00	20.9
7	0	-0	1268	0	0	0	-2670	--	--	16.08	16.08	0.29	0.05	0.01	0.08	0.00	0.00	20.9
8	0	-0	1046	0	0	0	-3187	--	--	16.08	16.08	0.29	0.06	0.01	0.07	0.00	0.00	20.9
9	0	-0	1262	0	0	0	-2702	--	--	16.08	16.08	0.29	0.05	0.01	0.08	0.00	0.00	20.9
10	0	-0	1134	0	0	0	-2950	--	--	16.08	16.08	0.29	0.05	0.01	0.07	0.00	0.00	20.9
11	0	-0	1199	0	0	0	-2804	--	--	16.08	16.08	0.29	0.05	0.01	0.08	0.00	0.00	20.9
12	0	-0	1115	0	0	0	-3054	--	--	16.08	16.08	0.29	0.05	0.01	0.07	0.00	0.00	20.9
13	0	-0	1180	0	0	0	-2908	--	--	16.08	16.08	0.29	0.05	0.01	0.07	0.00	0.00	20.9
14	0	-0	1051	0	0	0	-3156	--	--	16.08	16.08	0.29	0.05	0.01	0.07	0.00	0.00	20.9
15	0	-0	1268	0	0	0	-2670	--	--	16.08	16.08	0.29	0.05	0.01	0.08	0.00	0.00	20.9
16	0	-0	1046	0	0	0	-3187	--	--	16.08	16.08	0.29	0.06	0.01	0.07	0.00	0.00	20.9
17	0	-0	1262	0	0	0	-2702	--	--	16.08	16.08	0.29	0.05	0.01	0.08	0.00	0.00	20.9
18	0	-0	1378	0	0	0	-4136	--	--	16.08	16.08	0.18	0.07	0.01	0.09	0.00	0.00	20.9
19	0	-0	1318	0	0	0	-4510	--	--	16.08	16.08	0.18	0.07	0.01	0.08	0.00	0.00	20.9
20	0	-0	1274	0	0	0	-4501	--	--	16.08	16.08	0.18	0.07	0.01	0.08	0.00	0.00	20.9
37	0	-0	1464	0	0	0	-3792	--	--	16.08	16.08	0.18	0.06	0.01	0.09	0.00	0.00	20.9
38	0	-0	1364	0	0	0	-4414	--	--	16.08	16.08	0.18	0.07	0.01	0.09	0.00	0.00	20.9
39	0	-0	1290	0	0	0	-4401	--	--	16.08	16.08	0.18	0.07	0.01	0.08	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	1504	0	0	0	-3808	--	--	16.08	16.08	0.18	0.06	0.01	0.09	0.00	0.00	20.9
2	27	-0	1134	0	0	0	-2950	--	--	16.08	16.08	0.29	0.05	0.01	0.07	0.00	0.00	20.9
3	27	-0	1199	0	0	0	-2804	--	--	16.08	16.08	0.29	0.05	0.01	0.08	0.00	0.00	20.9
4	27	-0	1115	0	0	0	-3054	--	--	16.08	16.08	0.29	0.05	0.01	0.07	0.00	0.00	20.9
5	27	-0	1180	0	0	0	-2908	--	--	16.08	16.08	0.29	0.05	0.01	0.07	0.00	0.00	20.9
6	27	-0	1051	0	0	0	-3156	--	--	16.08	16.08	0.29	0.05	0.01	0.07	0.00	0.00	20.9
7	27	-0	1268	0	0	0	-2670	--	--	16.08	16.08	0.29	0.05	0.01	0.08	0.00	0.00	20.9
8	27	-0	1046	0	0	0	-3187	--	--	16.08	16.08	0.29	0.06	0.01	0.07	0.00	0.00	20.9
9	27	-0	1262	0	0	0	-2702	--	--	16.08	16.08	0.29	0.05	0.01	0.08	0.00	0.00	20.9
10	27	-0	1134	0	0	0	-2950	--	--	16.08	16.08	0.29	0.05	0.01	0.07	0.00	0.00	20.9
11	27	-0	1199	0	0	0	-2804	--	--	16.08	16.08	0.29	0.05	0.01	0.08	0.00	0.00	20.9
12	27	-0	1115	0	0	0	-3054	--	--	16.08	16.08	0.29	0.05	0.01	0.07	0.00	0.00	20.9
13	27	-0	1180	0	0	0	-2908	--	--	16.08	16.08	0.29	0.05	0.01	0.07	0.00	0.00	20.9
14	27	-0	1051	0	0	0	-3156	--	--	16.08	16.08	0.29	0.05	0.01	0.07	0.00	0.00	20.9
15	27	-0	1268	0	0	0	-2670	--	--	16.08	16.08	0.29	0.05	0.01	0.08	0.00	0.00	20.9
16	27	-0	1046	0	0	0	-3187	--	--	16.08	16.08	0.29	0.06	0.01	0.07	0.00	0.00	20.9
17	27	-0	1262	0	0	0	-2702	--	--	16.08	16.08	0.29	0.05	0.01	0.08	0.00	0.00	20.9
18	27	-0	1378	0	0	0	-4136	--	--	16.08	16.08	0.18	0.07	0.01	0.09	0.00	0.00	20.9
19	27	-0	1318	0	0	0	-4510	--	--	16.08	16.08	0.18	0.07	0.01	0.08	0.00	0.00	20.9
20	27	-0	1274	0	0	0	-4501	--	--	16.08	16.08	0.18	0.07	0.01	0.08	0.00	0.00	20.9
37	27	-0	1464	0	0	0	-3792	--	--	16.08	16.08	0.18	0.06	0.01	0.09	0.00	0.00	20.9
38	27	-0	1364	0	0	0	-4414	--	--	16.08	16.08	0.18	0.07	0.01	0.09	0.00	0.00	20.9
39	27	-0	1290	0	0	0	-4401	--	--	16.08	16.08	0.18	0.07	0.01	0.08	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	54	-0	1504	0	0	0	-3808	--	--	16.08	16.08	0.18	0.06	0.01	0.09	0.00	0.00	20.9
2	54	-0	1134	0	0	0	-2950	--	--	16.08	16.08	0.29	0.05	0.01	0.07	0.00	0.00	20.9
3	54	-0	1199	0	0	0	-2804	--	--	16.08	16.08	0.29	0.05	0.01	0.08	0.00	0.00	20.9
4	54	-0	1115	0	0	0	-3054	--	--	16.08	16.08	0.29	0.05	0.01	0.07	0.00	0.00	20.9
5	54	-0	1180	0	0	0	-2908	--	--	16.08	16.08	0.29	0.05	0.01	0.07	0.00	0.00	20.9
6	54	-0	1051	0	0	0	-3156	--	--	16.08	16.08	0.29	0.05	0.01	0.07	0.00	0.00	20.9
7	54	-0	1268	0	0	0	-2670	--	--	16.08	16.08	0.29	0.05	0.01	0.08	0.00	0.00	20.9
8	54	-0	1046	0	0	0	-3187	--	--	16.08	16.08	0.29	0.06	0.01	0.07	0.00	0.00	20.9
9	54	-0	1262	0	0	0	-2702	--	--	16.08	16.08	0.29	0.05	0.01	0.08	0.00	0.00	20.9
10	54	-0	1134	0	0	0	-2950	--	--	16.08	16.08	0.29	0.05	0.01	0.07	0.00	0.00	20.9
11	54	-0	1199	0	0	0	-2804	--	--	16.08	16.08	0.29	0.05	0.01	0.08	0.00	0.00	20.9
12	54	-0	1115	0	0	0	-3054	--	--	16.08	16.08	0.29	0.05	0.01	0.07	0.00	0.00	20.9
13	54	-0	1180	0	0	0	-2908	--	--	16.08	16.08	0.29	0.05	0.01	0.07	0.00	0.00	20.9
14	54	-0	1051	0	0	0	-3156	--	--	16.08	16.08	0.29	0.05	0.01	0.07	0.00	0.00	20.9
15	54	-0	1268	0	0	0	-2670	--	--	16.08	16.08	0.29	0.05	0.01	0.08	0.00	0.00	20.9
16	54	-0	1046	0	0	0	-3187	--	--	16.08	16.08	0.29	0.06	0.01	0.07	0.00	0.00	20.9
17	54	-0	1262	0	0	0	-2702	--	--	16.08	16.08	0.29	0.05	0.01	0.08	0.00	0.00	20.9
18	54	-0	1378	0	0	0	-4136	--	--	16.08	16.08	0.18	0.07	0.01	0.09	0.00	0.00	20.9
19	54	-0	1318	0	0	0	-4510	--	--	16.08	16.08	0.18	0.07	0.01	0.08	0.00	0.00	20.9
20	54	-0	1274	0	0	0	-4501	--	--	16.08	16.08	0.18	0.07	0.01	0.08	0.00	0.00	20.9
37	54	-0	1464	0	0	0	-3792	--	--	16.08	16.08	0.18	0.06	0.01	0.09	0.00	0.00	20.9
38	54	-0	1364	0	0	0	-4414	--	--	16.08	16.08	0.18	0.07	0.01	0.09	0.00	0.00	20.9
39	54	-0	1290	0	0	0	-4401	--	--	16.08	16.08	0.18	0.07	0.01	0.08	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 107 NI 1962 NF 1970 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-111	0	0	0	-3808	--	--	16.08	16.08	0.18	0.06	0.00	0.01	0.00	0.00	20.9
2	0	-0	-112	0	0	0	-2950	--	--	16.08	16.08	0.29	0.05	0.00	0.01	0.00	0.00	20.9
3	0	-0	-38	0	0	0	-2804	--	--	16.08	16.08	0.29	0.05	0.00	0.00	0.00	0.00	20.9
4	0	-0	-132	0	0	0	-3054	--	--	16.08	16.08	0.29	0.05	0.00	0.01	0.00	0.00	20.9
5	0	-0	-58	0	0	0	-2908	--	--	16.08	16.08	0.29	0.05	0.00	0.00	0.00	0.00	20.9
6	0	-0	-205	0	0	0	-3156	--	--	16.08	16.08	0.29	0.05	0.00	0.01	0.00	0.00	20.9
7	0	-0	41	0	0	0	-2692	--	--	16.08	16.08	0.29	0.05	0.00	0.00	0.00	0.00	20.9
8	0	-0	-211	0	0	0	-3187	--	--	16.08	16.08	0.29	0.06	0.00	0.01	0.00	0.00	20.9
9	0	-0	35	0	0	0	-2721	--	--	16.08	16.08	0.29	0.05	0.00	0.00	0.00	0.00	20.9
10	0	-0	-112	0	0	0	-2950	--	--	16.08	16.08	0.29	0.05	0.00	0.01	0.00	0.00	20.9
11	0	-0	-38	0	0	0	-2804	--	--	16.08	16.08	0.29	0.05	0.00	0.00	0.00	0.00	20.9
12	0	-0	-132	0	0	0	-3054	--	--	16.08	16.08	0.29	0.05	0.00	0.01	0.00	0.00	20.9
13	0	-0	-58	0	0	0	-2908	--	--	16.08	16.08	0.29	0.05	0.00	0.00	0.00	0.00	20.9
14	0	-0	-205	0	0	0	-3156	--	--	16.08	16.08	0.29	0.05	0.00	0.01	0.00	0.00	20.9
15	0	-0	41	0	0	0	-2692	--	--	16.08	16.08	0.29	0.05	0.00	0.00	0.00	0.00	20.9
16	0	-0	-211	0	0	0	-3187	--	--	16.08	16.08	0.29	0.06	0.00	0.01	0.00	0.00	20.9
17	0	-0	35	0	0	0	-2721	--	--	16.08	16.08	0.29	0.05	0.00	0.00	0.00	0.00	20.9
18	0	-0	-330	0	0	0	-4136	--	--	16.08	16.08	0.18	0.07	0.00	0.02	0.00	0.00	20.9
19	0	-0	-395	0	0	0	-4510	--	--	16.08	16.08	0.18	0.07	0.00	0.02	0.00	0.00	20.9
20	0	-0	-436	0	0	0	-4501	--	--	16.08	16.08	0.18	0.07	0.00	0.03	0.00	0.00	20.9
37	0	-0	-197	0	0	0	-3792	--	--	16.08	16.08	0.18	0.06	0.00	0.01	0.00	0.00	20.9
38	0	-0	-305	0	0	0	-4414	--	--	16.08	16.08	0.18	0.07	0.00	0.02	0.00	0.00	20.9
39	0	-0	-374	0	0	0	-4401	--	--	16.08	16.08	0.18	0.07	0.00	0.02	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-111	0	0	0	-3808	--	--	16.08	16.08	0.18	0.06	0.00	0.01	0.00	0.00	20.9
2	27	-0	-112	0	0	0	-2950	--	--	16.08	16.08	0.29	0.05	0.00	0.01	0.00	0.00	20.9
3	27	-0	-38	0	0	0	-2804	--	--	16.08	16.08	0.29	0.05	0.00	0.00	0.00	0.00	20.9
4	27	-0	-132	0	0	0	-3054	--	--	16.08	16.08	0.29	0.05	0.00	0.01	0.00	0.00	20.9
5	27	-0	-58	0	0	0	-2908	--	--	16.08	16.08	0.29	0.05	0.00	0.00	0.00	0.00	20.9
6	27	-0	-205	0	0	0	-3156	--	--	16.08	16.08	0.29	0.05	0.00	0.01	0.00	0.00	20.9
7	27	-0	41	0	0	0	-2692	--	--	16.08	16.08	0.29	0.05	0.00	0.00	0.00	0.00	20.9
8	27	-0	-211	0	0	0	-3187	--	--	16.08	16.08	0.29	0.06	0.00	0.01	0.00	0.00	20.9
9	27	-0	35	0	0	0	-2721	--	--	16.08	16.08	0.29	0.05	0.00	0.00	0.00	0.00	20.9
10	27	-0	-112	0	0	0	-2950	--	--	16.08	16.08	0.29	0.05	0.00	0.01	0.00	0.00	20.9
11	27	-0	-38	0	0	0	-2804	--	--	16.08	16.08	0.29	0.05	0.00	0.00	0.00	0.00	20.9
12	27	-0	-132	0	0	0	-3054	--	--	16.08	16.08	0.29	0.05	0.00	0.01	0.00	0.00	20.9
13	27	-0	-58	0	0	0	-2908	--	--	16.08	16.08	0.29	0.05	0.00	0.00	0.00	0.00	20.9
14	27	-0	-205	0	0	0	-3156	--	--	16.08	16.08	0.29	0.05	0.00	0.01	0.00	0.00	20.9
15	27	-0	41	0	0	0	-2692	--	--	16.08	16.08	0.29	0.05	0.00	0.00	0.00	0.00	20.9
16	27	-0	-211	0	0	0	-3187	--	--	16.08	16.08	0.29	0.06	0.00	0.01	0.00	0.00	20.9
17	27	-0	35	0	0	0	-2721	--	--	16.08	16.08	0.29	0.05	0.00	0.00	0.00	0.00	20.9
18	27	-0	-330	0	0	0	-4136	--	--	16.08	16.08	0.18	0.07	0.00	0.02	0.00	0.00	20.9
19	27	-0	-395	0	0	0	-4510	--	--	16.08	16.08	0.18	0.07	0.00	0.02	0.00	0.00	20.9
20	27	-0	-436	0	0	0	-4501	--	--	16.08	16.08	0.18	0.07	0.00	0.03	0.00	0.00	20.9
37	27	-0	-197	0	0	0	-3792	--	--	16.08	16.08	0.18	0.06	0.00	0.01	0.00	0.00	20.9
38	27	-0	-305	0	0	0	-4414	--	--	16.08	16.08	0.18	0.07	0.00	0.02	0.00	0.00	20.9
39	27	-0	-374	0	0	0	-4401	--	--	16.08	16.08	0.18	0.07	0.00	0.02	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	54	-0	-111	0	0	0	-3808	--	--	16.08	16.08	0.18	0.06	0.00	0.01	0.00	0.00	20.9
2	54	-0	-112	0	0	0	-2950	--	--	16.08	16.08	0.29	0.05	0.00	0.01	0.00	0.00	20.9
3	54	-0	-38	0	0	0	-2804	--	--	16.08	16.08	0.29	0.05	0.00	0.00	0.00	0.00	20.9
4	54	-0	-132	0	0	0	-3054	--	--	16.08	16.08	0.29	0.05	0.00	0.01	0.00	0.00	20.9
5	54	-0	-58	0	0	0	-2908	--	--	16.08	16.08	0.29	0.05	0.00	0.00	0.00	0.00	20.9
6	54	-0	-205	0	0	0	-3156	--	--	16.08	16.08	0.29	0.05	0.00	0.01	0.00	0.00	20.9
7	54	-0	41	0	0	0	-2692	--	--	16.08	16.08	0.29	0.05	0.00	0.00	0.00	0.00	20.9
8	54	-0	-211	0	0	0	-3187	--	--	16.08	16.08	0.29	0.06	0.00	0.01	0.00	0.00	20.9
9	54	-0	35	0	0	0	-2721	--	--	16.08	16.08	0.29	0.05	0.00	0.00	0.00	0.00	20.9
10	54	-0	-112	0	0	0	-2950	--	--	16.08	16.08	0.29	0.05	0.00	0.01	0.00	0.00	20.9
11	54	-0	-38	0	0	0	-2804	--	--	16.08	16.08	0.29	0.05	0.00	0.00	0.00	0.00	20.9
12	54	-0	-132	0	0	0	-3054	--	--	16.08	16.08	0.29	0.05	0.00	0.01	0.00	0.00	20.9
13	54	-0	-58	0	0	0	-2908	--	--	16.08	16.08	0.29	0.05	0.00	0.00	0.00	0.00	20.9
14	54	-0	-205	0	0	0	-3156	--	--	16.08	16.08	0.29	0.05	0.00	0.01	0.00	0.00	20.9
15	54	-0	41	0	0	0	-2692	--	--	16.08	16.08	0.29	0.05	0.00	0.00	0.00	0.00	20.9
16	54	-0	-211	0	0	0	-3187	--	--	16.08	16.08	0.29	0.06	0.00	0.01	0.00	0.00	20.9
17	54	-0	35	0	0	0	-2721	--	--	16.08	16.08	0.29	0.05	0.00	0.00	0.00	0.00	20.9
18	54	-0	-330	0	0	0	-4136	--	--	16.08	16.08	0.18	0.07	0.00	0.02	0.00	0.00	20.9
19	54	-0	-395	0	0	0	-4510	--	--	16.08	16.08	0.18	0.07	0.00	0.02	0.00	0.00	20.9
20	54	-0	-436	0	0	0	-4501	--	--	16.08	16.08	0.18	0.07	0.00	0.03	0.00	0.00	20.9
37	54	-0	-197	0	0	0	-3792	--	--	16.08	16.08	0.18	0.06	0.00	0.01	0.00	0.00	20.9
38	54	-0	-305	0	0	0	-4414	--	--	16.08	16.08	0.18	0.07	0.00	0.02	0.00	0.00	20.9
39	54	-0	-374	0	0	0	-4401	--	--	16.08	16.08	0.18	0.07	0.00	0.02	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 108 NI 1968 NF 1962 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-1804	0	0	0	-3748	--	--	16.08	16.08	0.18	0.06	0.01	0.11	0.00	0.00	20.9
2	0	-0	-1418	0	0	0	-2889	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
3	0	-0	-1337	0	0	0	-2783	--	--	16.08	16.08	0.29	0.05	0.01	0.08	0.00	0.00	20.9
4	0	-0	-1439	0	0	0	-2983	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
5	0	-0	-1358	0	0	0	-2877	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
6	0	-0	-1521	0	0	0	-3046	--	--	16.08	16.08	0.29	0.05	0.01	0.10	0.00	0.00	20.9
7	0	-0	-1249	0	0	0	-2692	--	--	16.08	16.08	0.29	0.05	0.01	0.08	0.00	0.00	20.9
8	0	-0	-1527	0	0	0	-3074	--	--	16.08	16.08	0.29	0.05	0.01	0.10	0.00	0.00	20.9
9	0	-0	-1255	0	0	0	-2721	--	--	16.08	16.08	0.29	0.05	0.01	0.08	0.00	0.00	20.9
10	0	-0	-1418	0	0	0	-2889	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
11	0	-0	-1337	0	0	0	-2783	--	--	16.08	16.08	0.29	0.05	0.01	0.08	0.00	0.00	20.9
12	0	-0	-1439	0	0	0	-2983	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
13	0	-0	-1358	0	0	0	-2877	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
14	0	-0	-1521	0	0	0	-3046	--	--	16.08	16.08	0.29	0.05	0.01	0.10	0.00	0.00	20.9
15	0	-0	-1249	0	0	0	-2692	--	--	16.08	16.08	0.29	0.05	0.01	0.08	0.00	0.00	20.9
16	0	-0	-1527	0	0	0	-3074	--	--	16.08	16.08	0.29	0.05	0.01	0.10	0.00	0.00	20.9

17	0	-0	-1255	0	0	0	-2721	--	--	16.08	16.08	0.29	0.05	0.01	0.08	0.00	0.00	20.9
18	0	-0	-2135	0	0	0	-3959	--	--	16.08	16.08	0.18	0.07	0.02	0.13	0.00	0.00	20.9
19	0	-0	-2206	0	0	0	-4298	--	--	16.08	16.08	0.18	0.07	0.02	0.14	0.00	0.00	20.9
20	0	-0	-2239	0	0	0	-4268	--	--	16.08	16.08	0.18	0.07	0.02	0.14	0.00	0.00	20.9
37	0	-0	-1947	0	0	0	-3687	--	--	16.08	16.08	0.18	0.06	0.02	0.12	0.00	0.00	20.9
38	0	-0	-2065	0	0	0	-4251	--	--	16.08	16.08	0.18	0.07	0.02	0.13	0.00	0.00	20.9
39	0	-0	-2120	0	0	0	-4201	--	--	16.08	16.08	0.18	0.07	0.02	0.13	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-1804	0	0	0	-3748	--	--	16.08	16.08	0.18	0.06	0.01	0.11	0.00	0.00	20.9
2	27	-0	-1418	0	0	0	-2889	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
3	27	-0	-1337	0	0	0	-2783	--	--	16.08	16.08	0.29	0.05	0.01	0.08	0.00	0.00	20.9
4	27	-0	-1439	0	0	0	-2983	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
5	27	-0	-1358	0	0	0	-2877	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
6	27	-0	-1521	0	0	0	-3046	--	--	16.08	16.08	0.29	0.05	0.01	0.10	0.00	0.00	20.9
7	27	-0	-1249	0	0	0	-2692	--	--	16.08	16.08	0.29	0.05	0.01	0.08	0.00	0.00	20.9
8	27	-0	-1527	0	0	0	-3074	--	--	16.08	16.08	0.29	0.05	0.01	0.10	0.00	0.00	20.9
9	27	-0	-1255	0	0	0	-2721	--	--	16.08	16.08	0.29	0.05	0.01	0.08	0.00	0.00	20.9
10	27	-0	-1418	0	0	0	-2889	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
11	27	-0	-1337	0	0	0	-2783	--	--	16.08	16.08	0.29	0.05	0.01	0.08	0.00	0.00	20.9
12	27	-0	-1439	0	0	0	-2983	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
13	27	-0	-1358	0	0	0	-2877	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
14	27	-0	-1521	0	0	0	-3046	--	--	16.08	16.08	0.29	0.05	0.01	0.10	0.00	0.00	20.9
15	27	-0	-1249	0	0	0	-2692	--	--	16.08	16.08	0.29	0.05	0.01	0.08	0.00	0.00	20.9
16	27	-0	-1527	0	0	0	-3074	--	--	16.08	16.08	0.29	0.05	0.01	0.10	0.00	0.00	20.9
17	27	-0	-1255	0	0	0	-2721	--	--	16.08	16.08	0.29	0.05	0.01	0.08	0.00	0.00	20.9
18	27	-0	-2135	0	0	0	-3959	--	--	16.08	16.08	0.18	0.07	0.02	0.13	0.00	0.00	20.9
19	27	-0	-2206	0	0	0	-4298	--	--	16.08	16.08	0.18	0.07	0.02	0.14	0.00	0.00	20.9
20	27	-0	-2239	0	0	0	-4268	--	--	16.08	16.08	0.18	0.07	0.02	0.14	0.00	0.00	20.9
37	27	-0	-1947	0	0	0	-3687	--	--	16.08	16.08	0.18	0.06	0.02	0.12	0.00	0.00	20.9
38	27	-0	-2065	0	0	0	-4251	--	--	16.08	16.08	0.18	0.07	0.02	0.13	0.00	0.00	20.9
39	27	-0	-2120	0	0	0	-4201	--	--	16.08	16.08	0.18	0.07	0.02	0.13	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	54	-0	-1804	0	0	0	-3748	--	--	16.08	16.08	0.18	0.06	0.01	0.11	0.00	0.00	20.9
2	54	-0	-1418	0	0	0	-2889	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
3	54	-0	-1337	0	0	0	-2783	--	--	16.08	16.08	0.29	0.05	0.01	0.08	0.00	0.00	20.9
4	54	-0	-1439	0	0	0	-2983	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
5	54	-0	-1358	0	0	0	-2877	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
6	54	-0	-1521	0	0	0	-3046	--	--	16.08	16.08	0.29	0.05	0.01	0.10	0.00	0.00	20.9
7	54	-0	-1249	0	0	0	-2692	--	--	16.08	16.08	0.29	0.05	0.01	0.08	0.00	0.00	20.9
8	54	-0	-1527	0	0	0	-3074	--	--	16.08	16.08	0.29	0.05	0.01	0.10	0.00	0.00	20.9
9	54	-0	-1255	0	0	0	-2721	--	--	16.08	16.08	0.29	0.05	0.01	0.08	0.00	0.00	20.9
10	54	-0	-1418	0	0	0	-2889	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
11	54	-0	-1337	0	0	0	-2783	--	--	16.08	16.08	0.29	0.05	0.01	0.08	0.00	0.00	20.9
12	54	-0	-1439	0	0	0	-2983	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
13	54	-0	-1358	0	0	0	-2877	--	--	16.08	16.08	0.29	0.05	0.01	0.09	0.00	0.00	20.9
14	54	-0	-1521	0	0	0	-3046	--	--	16.08	16.08	0.29	0.05	0.01	0.10	0.00	0.00	20.9
15	54	-0	-1249	0	0	0	-2692	--	--	16.08	16.08	0.29	0.05	0.01	0.08	0.00	0.00	20.9
16	54	-0	-1527	0	0	0	-3074	--	--	16.08	16.08	0.29	0.05	0.01	0.10	0.00	0.00	20.9
17	54	-0	-1255	0	0	0	-2721	--	--	16.08	16.08	0.29	0.05	0.01	0.08	0.00	0.00	20.9
18	54	-0	-2135	0	0	0	-3959	--	--	16.08	16.08	0.18	0.07	0.02	0.13	0.00	0.00	20.9
19	54	-0	-2206	0	0	0	-4298	--	--	16.08	16.08	0.18	0.07	0.02	0.14	0.00	0.00	20.9
20	54	-0	-2239	0	0	0	-4268	--	--	16.08	16.08	0.18	0.07	0.02	0.14	0.00	0.00	20.9
37	54	-0	-1947	0	0	0	-3687	--	--	16.08	16.08	0.18	0.06	0.02	0.12	0.00	0.00	20.9
38	54	-0	-2065	0	0	0	-4251	--	--	16.08	16.08	0.18	0.07	0.02	0.13	0.00	0.00	20.9
39	54	-0	-2120	0	0	0	-4201	--	--	16.08	16.08	0.18	0.07	0.02	0.13	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 109 NI 1969 NF 1968 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-3601	0	0	0	-2782	--	--	16.08	16.08	0.18	0.05	0.03	0.23	0.00	0.00	20.9
2	0	-0	-2803	0	0	0	-2130	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
3	0	-0	-2714	0	0	0	-2067	--	--	16.08	16.08	0.29	0.04	0.02	0.17	0.00	0.00	20.9
4	0	-0	-2826	0	0	0	-2212	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
5	0	-0	-2737	0	0	0	-2150	--	--	16.08	16.08	0.29	0.04	0.02	0.17	0.00	0.00	20.9
6	0	-0	-2914	0	0	0	-2231	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
7	0	-0	-2619	0	0	0	-2023	--	--	16.08	16.08	0.29	0.04	0.02	0.16	0.00	0.00	20.9
8	0	-0	-2921	0	0	0	-2256	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
9	0	-0	-2625	0	0	0	-2048	--	--	16.08	16.08	0.29	0.04	0.02	0.16	0.00	0.00	20.9
10	0	-0	-2803	0	0	0	-2130	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
11	0	-0	-2714	0	0	0	-2067	--	--	16.08	16.08	0.29	0.04	0.02	0.17	0.00	0.00	20.9
12	0	-0	-2826	0	0	0	-2212	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
13	0	-0	-2737	0	0	0	-2150	--	--	16.08	16.08	0.29	0.04	0.02	0.17	0.00	0.00	20.9
14	0	-0	-2914	0	0	0	-2231	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
15	0	-0	-2619	0	0	0	-2023	--	--	16.08	16.08	0.29	0.04	0.02	0.16	0.00	0.00	20.9
16	0	-0	-2921	0	0	0	-2256	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
17	0	-0	-2625	0	0	0	-2048	--	--	16.08	16.08	0.29	0.04	0.02	0.16	0.00	0.00	20.9
18	0	-0	-4061	0	0	0	-2815	--	--	16.08	16.08	0.18	0.05	0.03	0.25	0.00	0.00	20.9
19	0	-0	-4141	0	0	0	-3116	--	--	16.08	16.08	0.18	0.05	0.03	0.26	0.00	0.00	20.9
20	0	-0	-4161	0	0	0	-3068	--	--	16.08	16.08	0.18	0.05	0.03	0.26	0.00	0.00	20.9
37	0	-0	-3808	0	0	0	-2643	--	--	16.08	16.08	0.18	0.04	0.03	0.24	0.00	0.00	20.9
38	0	-0	-3942	0	0	0	-3145	--	--	16.08	16.08	0.18	0.05	0.03	0.25	0.00	0.00	20.9
39	0	-0	-3974	0	0	0	-3065	--	--	16.08	16.08	0.18	0.05	0.03	0.25	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-3601	0	0	0	-2782	--	--	16.08	16.08	0.18	0.05	0.03	0.23	0.00	0.00	20.9
2	27	-0	-2803	0	0	0	-2130	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
3	27	-0	-2714	0	0	0	-2067	--	--	16.08	16.08	0.29	0.04	0.02	0.17	0.00	0.00	20.9
4	27	-0	-2826	0	0	0	-2212	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
5	27	-0	-2737	0	0	0	-2150	--	--	16.08	16.08	0.29	0.04	0.02	0.17	0.00	0.00	20.9
6	27	-0	-2914	0	0	0	-2231	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
7	27	-0	-2619	0	0	0	-2023	--	--	16.08	16.08	0.29	0.04	0.02	0.16	0.00	0.00	20.9
8	27	-0	-2921	0	0	0	-2256	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
9	27	-0	-2625	0	0	0	-2048	--	--	16.08	16.08	0.29	0.04	0.02	0.16	0.00	0.00	20.9
10	27	-0	-2803	0	0	0	-2130	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
11	27	-0	-2714	0	0	0	-2067	--	--	16.08	16.08	0.29	0.04	0.02	0.17	0.00	0.00	20.9
12	27	-0	-2826	0	0	0	-2212	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9

13	27	-0	-2737	0	0	0	-2150	--	--	16.08	16.08	0.29	0.04	0.02	0.17	0.00	0.00	20.9
14	27	-0	-2914	0	0	0	-2231	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
15	27	-0	-2619	0	0	0	-2023	--	--	16.08	16.08	0.29	0.04	0.02	0.16	0.00	0.00	20.9
16	27	-0	-2921	0	0	0	-2256	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
17	27	-0	-2625	0	0	0	-2048	--	--	16.08	16.08	0.29	0.04	0.02	0.16	0.00	0.00	20.9
18	27	-0	-4061	0	0	0	-2815	--	--	16.08	16.08	0.18	0.05	0.03	0.25	0.00	0.00	20.9
19	27	-0	-4141	0	0	0	-3116	--	--	16.08	16.08	0.18	0.05	0.03	0.26	0.00	0.00	20.9
20	27	-0	-4161	0	0	0	-3068	--	--	16.08	16.08	0.18	0.05	0.03	0.26	0.00	0.00	20.9
37	27	-0	-3808	0	0	0	-2643	--	--	16.08	16.08	0.18	0.04	0.03	0.24	0.00	0.00	20.9
38	27	-0	-3942	0	0	0	-3145	--	--	16.08	16.08	0.18	0.05	0.03	0.25	0.00	0.00	20.9
39	27	-0	-3974	0	0	0	-3065	--	--	16.08	16.08	0.18	0.05	0.03	0.25	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	54	-0	-3601	0	0	0	-2782	--	--	16.08	16.08	0.18	0.05	0.03	0.23	0.00	0.00	20.9
2	54	-0	-2803	0	0	0	-2130	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
3	54	-0	-2714	0	0	0	-2067	--	--	16.08	16.08	0.29	0.04	0.02	0.17	0.00	0.00	20.9
4	54	-0	-2826	0	0	0	-2212	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
5	54	-0	-2737	0	0	0	-2150	--	--	16.08	16.08	0.29	0.04	0.02	0.17	0.00	0.00	20.9
6	54	-0	-2914	0	0	0	-2231	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
7	54	-0	-2619	0	0	0	-2023	--	--	16.08	16.08	0.29	0.04	0.02	0.16	0.00	0.00	20.9
8	54	-0	-2921	0	0	0	-2256	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
9	54	-0	-2625	0	0	0	-2048	--	--	16.08	16.08	0.29	0.04	0.02	0.16	0.00	0.00	20.9
10	54	-0	-2803	0	0	0	-2130	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
11	54	-0	-2714	0	0	0	-2067	--	--	16.08	16.08	0.29	0.04	0.02	0.17	0.00	0.00	20.9
12	54	-0	-2826	0	0	0	-2212	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
13	54	-0	-2737	0	0	0	-2150	--	--	16.08	16.08	0.29	0.04	0.02	0.17	0.00	0.00	20.9
14	54	-0	-2914	0	0	0	-2231	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
15	54	-0	-2619	0	0	0	-2023	--	--	16.08	16.08	0.29	0.04	0.02	0.16	0.00	0.00	20.9
16	54	-0	-2921	0	0	0	-2256	--	--	16.08	16.08	0.29	0.04	0.02	0.18	0.00	0.00	20.9
17	54	-0	-2625	0	0	0	-2048	--	--	16.08	16.08	0.29	0.04	0.02	0.16	0.00	0.00	20.9
18	54	-0	-4061	0	0	0	-2815	--	--	16.08	16.08	0.18	0.05	0.03	0.25	0.00	0.00	20.9
19	54	-0	-4141	0	0	0	-3116	--	--	16.08	16.08	0.18	0.05	0.03	0.26	0.00	0.00	20.9
20	54	-0	-4161	0	0	0	-3068	--	--	16.08	16.08	0.18	0.05	0.03	0.26	0.00	0.00	20.9
37	54	-0	-3808	0	0	0	-2643	--	--	16.08	16.08	0.18	0.04	0.03	0.24	0.00	0.00	20.9
38	54	-0	-3942	0	0	0	-3145	--	--	16.08	16.08	0.18	0.05	0.03	0.25	0.00	0.00	20.9
39	54	-0	-3974	0	0	0	-3065	--	--	16.08	16.08	0.18	0.05	0.03	0.25	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 110 NI 1960 NF 1969 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--	--	--		--	--	--	--	--	--	--		--	--	--	--	--	--
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-5519	0	0	0	2104	--	--	16.08	16.08	0.00	0.04	0.05	0.35	0.00	0.00	20.9
2	0	-0	-4280	0	0	0	1665	--	--	16.08	16.08	0.10	0.03	0.04	0.27	0.00	0.00	20.9
3	0	-0	-4185	0	0	0	1629	--	--	16.08	16.08	0.10	0.03	0.03	0.26	0.00	0.00	20.9
4	0	-0	-4306	0	0	0	1608	--	--	16.08	16.08	0.10	0.03	0.04	0.27	0.00	0.00	20.9
5	0	-0	-4211	0	0	0	1572	--	--	16.08	16.08	0.10	0.03	0.03	0.26	0.00	0.00	20.9
6	0	-0	-4401	0	0	0	1688	--	--	16.08	16.08	0.10	0.03	0.04	0.28	0.00	0.00	20.9
7	0	-0	-4083	0	0	0	1567	--	--	16.08	16.08	0.10	0.03	0.03	0.26	0.00	0.00	20.9
8	0	-0	-4409	0	0	0	1671	--	--	16.08	16.08	0.10	0.03	0.04	0.28	0.00	0.00	20.9
9	0	-0	-4090	0	0	0	1550	--	--	16.08	16.08	0.10	0.03	0.03	0.26	0.00	0.00	20.9
10	0	-0	-4280	0	0	0	1665	--	--	16.08	16.08	0.10	0.03	0.04	0.27	0.00	0.00	20.9
11	0	-0	-4185	0	0	0	1629	--	--	16.08	16.08	0.10	0.03	0.03	0.26	0.00	0.00	20.9
12	0	-0	-4306	0	0	0	1608	--	--	16.08	16.08	0.10	0.03	0.04	0.27	0.00	0.00	20.9
13	0	-0	-4211	0	0	0	1572	--	--	16.08	16.08	0.10	0.03	0.03	0.26	0.00	0.00	20.9
14	0	-0	-4401	0	0	0	1688	--	--	16.08	16.08	0.10	0.03	0.04	0.28	0.00	0.00	20.9
15	0	-0	-4083	0	0	0	1567	--	--	16.08	16.08	0.10	0.03	0.03	0.26	0.00	0.00	20.9
16	0	-0	-4409	0	0	0	1671	--	--	16.08	16.08	0.10	0.03	0.04	0.28	0.00	0.00	20.9
17	0	-0	-4090	0	0	0	1550	--	--	16.08	16.08	0.10	0.03	0.03	0.26	0.00	0.00	20.9
18	0	-0	-6128	0	0	0	2644	--	--	16.08	16.08	0.00	0.05	0.05	0.38	0.00	0.00	20.9
19	0	-0	-6222	0	0	0	2436	--	--	16.08	16.08	0.00	0.04	0.05	0.39	0.00	0.00	20.9
20	0	-0	-6223	0	0	0	2495	--	--	16.08	16.08	0.00	0.04	0.05	0.39	0.00	0.00	20.9
37	0	-0	-5800	0	0	0	2504	--	--	16.08	16.08	0.00	0.04	0.05	0.36	0.00	0.00	20.9
38	0	-0	-5956	0	0	0	2158	--	--	16.08	16.08	0.00	0.04	0.05	0.37	0.00	0.00	20.9
39	0	-0	-5958	0	0	0	2256	--	--	16.08	16.08	0.00	0.04	0.05	0.37	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-5519	0	0	0	2104	--	--	16.08	16.08	0.00	0.04	0.05	0.35	0.00	0.00	20.9
2	27	-0	-4280	0	0	0	1665	--	--	16.08	16.08	0.10	0.03	0.04	0.27	0.00	0.00	20.9
3	27	-0	-4185	0	0	0	1629	--	--	16.08	16.08	0.10	0.03	0.03	0.26	0.00	0.00	20.9
4	27	-0	-4306	0	0	0	1608	--	--	16.08	16.08	0.10	0.03	0.04	0.27	0.00	0.00	20.9
5	27	-0	-4211	0	0	0	1572	--	--	16.08	16.08	0.10	0.03	0.03	0.26	0.00	0.00	20.9
6	27	-0	-4401	0	0	0	1688	--	--	16.08	16.08	0.10	0.03	0.04	0.28	0.00	0.00	20.9
7	27	-0	-4083	0	0	0	1567	--	--	16.08	16.08	0.10	0.03	0.03	0.26	0.00	0.00	20.9
8	27	-0	-4409	0	0	0	1671	--	--	16.08	16.08	0.10	0.03	0.04	0.28	0.00	0.00	20.9
9	27	-0	-4090	0	0	0	1550	--	--	16.08	16.08	0.10	0.03	0.03	0.26	0.00	0.00	20.9
10	27	-0	-4280	0	0	0	1665	--	--	16.08	16.08	0.10	0.03	0.04	0.27	0.00	0.00	20.9
11	27	-0	-4185	0	0	0	1629	--	--	16.08	16.08	0.10	0.03	0.03	0.26	0.00	0.00	20.9
12	27	-0	-4306	0	0	0	1608	--	--	16.08	16.08	0.10	0.03	0.04	0.27	0.00	0.00	20.9
13	27	-0	-4211	0	0	0	1572	--	--	16.08	16.08	0.10	0.03	0.03	0.26	0.00	0.00	20.9
14	27	-0	-4401	0	0	0	1688	--	--	16.08	16.08	0.10	0.03	0.04	0.28	0.00	0.00	20.9
15	27	-0	-4083	0	0	0	1567	--	--	16.08	16.08	0.10	0.03	0.03	0.26	0.00	0.00	20.9
16	27	-0	-4409	0	0	0	1671	--	--	16.08	16.08	0.10	0.03	0.04	0.28	0.00	0.00	20.9
17	27	-0	-4090	0	0	0	1550	--	--	16.08	16.08	0.10	0.03	0.03	0.26	0.00	0.00	20.9
18	27	-0	-6128	0	0	0	2644	--	--	16.08	16.08	0.00	0.05	0.05	0.38	0.00	0.00	20.9
19	27	-0	-6222	0	0	0	2436	--	--	16.08	16.08	0.00	0.04	0.05	0.39	0.00	0.00	20.9
20	27	-0	-6223	0	0	0	2495	--	--	16.08	16.08	0.00	0.04	0.05	0.39	0.00	0.00	20.9
37	27	-0	-5800	0	0	0	2504	--	--	16.08	16.08	0.00	0.04	0.05	0.36	0.00	0.00	20.9
38	27	-0	-5956	0	0	0	2158	--	--	16.08	16.08	0.00	0.04	0.05	0.37	0.00	0.00	20.9
39	27	-0	-5958	0	0	0	2256	--	--	16.08	16.08	0.00	0.04	0.05	0.37	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	54	-0	-5519	0	0	0	-852	--	--	16.08	16.08	0.18	0.01	0.05	0.35	0.00	0.00	20.9
2	54	-0	-4280	0	0	0	-628	--	--	16.08	16.08	0.29	0.01	0.04	0.27	0.00	0.00	20.9
3	54	-0	-4185	0	0	0	-613	--	--	16.08	16.08	0.29	0.01	0.03	0.26	0.00	0.00	20.9
4	54	-0	-4306	0	0	0	-698	--	--	16.08	16.08	0.29	0.01	0.04	0.27	0.00	0.00	20.9
5	54	-0	-4211	0	0	0	-684	--	--	16.08	16.08	0.29	0.01	0.03	0.26	0.00	0.00	20.9
6	54	-0	-4401	0	0	0	-670	--	--	16.08	16.08	0.29	0.01	0.04	0.28	0.00	0.00	20.9
7	54	-0	-4083	0	0	0	-620	--	--	16.08	16.08	0.29	0.01	0.03	0.26	0.00	0.00	20.9
8	54	-0	-4409	0	0	0	-691	--	--	16.08	16.08	0.29	0.01	0.04	0.28	0.00	0.00	20.9

9	54	-0	-4090	0	0	0	-642	--	--	16.08	16.08	0.29	0.01	0.03	0.26	0.00	0.00	20.9
10	54	-0	-4280	0	0	0	-628	--	--	16.08	16.08	0.29	0.01	0.04	0.27	0.00	0.00	20.9
11	54	-0	-4185	0	0	0	-613	--	--	16.08	16.08	0.29	0.01	0.03	0.26	0.00	0.00	20.9
12	54	-0	-4306	0	0	0	-698	--	--	16.08	16.08	0.29	0.01	0.04	0.27	0.00	0.00	20.9
13	54	-0	-4211	0	0	0	-684	--	--	16.08	16.08	0.29	0.01	0.03	0.26	0.00	0.00	20.9
14	54	-0	-4401	0	0	0	-670	--	--	16.08	16.08	0.29	0.01	0.04	0.28	0.00	0.00	20.9
15	54	-0	-4083	0	0	0	-620	--	--	16.08	16.08	0.29	0.01	0.03	0.26	0.00	0.00	20.9
16	54	-0	-4409	0	0	0	-691	--	--	16.08	16.08	0.29	0.01	0.04	0.28	0.00	0.00	20.9
17	54	-0	-4090	0	0	0	-642	--	--	16.08	16.08	0.29	0.01	0.03	0.26	0.00	0.00	20.9
18	54	-0	-6128	0	0	0	-639	--	--	16.08	16.08	0.18	0.01	0.05	0.38	0.00	0.00	20.9
19	54	-0	-6222	0	0	0	-897	--	--	16.08	16.08	0.18	0.01	0.05	0.39	0.00	0.00	20.9
20	54	-0	-6223	0	0	0	-839	--	--	16.08	16.08	0.18	0.01	0.05	0.39	0.00	0.00	20.9
37	54	-0	-5800	0	0	0	-603	--	--	16.08	16.08	0.18	0.01	0.05	0.36	0.00	0.00	20.9
38	54	-0	-5956	0	0	0	-1033	--	--	16.08	16.08	0.18	0.02	0.05	0.37	0.00	0.00	20.9
39	54	-0	-5958	0	0	0	-936	--	--	16.08	16.08	0.18	0.02	0.05	0.37	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 111 NI 1961 NF 1960 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-7569	0	0	0	6159	--	--	16.08	16.08	0.00	0.11	0.06	0.47	0.00	0.00	20.9
2	0	-0	-5858	0	0	0	4803	--	--	16.08	16.08	0.10	0.09	0.05	0.37	0.00	0.00	20.9
3	0	-0	-5756	0	0	0	4712	--	--	16.08	16.08	0.10	0.08	0.05	0.36	0.00	0.00	20.9
4	0	-0	-5888	0	0	0	4763	--	--	16.08	16.08	0.10	0.08	0.05	0.37	0.00	0.00	20.9
5	0	-0	-5786	0	0	0	4672	--	--	16.08	16.08	0.10	0.08	0.05	0.36	0.00	0.00	20.9
6	0	-0	-5988	0	0	0	4895	--	--	16.08	16.08	0.10	0.09	0.05	0.38	0.00	0.00	20.9
7	0	-0	-5647	0	0	0	4592	--	--	16.08	16.08	0.10	0.08	0.05	0.35	0.00	0.00	20.9
8	0	-0	-5997	0	0	0	4883	--	--	16.08	16.08	0.10	0.09	0.05	0.38	0.00	0.00	20.9
9	0	-0	-5656	0	0	0	4580	--	--	16.08	16.08	0.10	0.08	0.05	0.35	0.00	0.00	20.9
10	0	-0	-5858	0	0	0	4803	--	--	16.08	16.08	0.10	0.09	0.05	0.37	0.00	0.00	20.9
11	0	-0	-5756	0	0	0	4712	--	--	16.08	16.08	0.10	0.08	0.05	0.36	0.00	0.00	20.9
12	0	-0	-5888	0	0	0	4763	--	--	16.08	16.08	0.10	0.08	0.05	0.37	0.00	0.00	20.9
13	0	-0	-5786	0	0	0	4672	--	--	16.08	16.08	0.10	0.08	0.05	0.36	0.00	0.00	20.9
14	0	-0	-5988	0	0	0	4895	--	--	16.08	16.08	0.10	0.09	0.05	0.38	0.00	0.00	20.9
15	0	-0	-5647	0	0	0	4592	--	--	16.08	16.08	0.10	0.08	0.05	0.35	0.00	0.00	20.9
16	0	-0	-5997	0	0	0	4883	--	--	16.08	16.08	0.10	0.09	0.05	0.38	0.00	0.00	20.9
17	0	-0	-5656	0	0	0	4580	--	--	16.08	16.08	0.10	0.08	0.05	0.35	0.00	0.00	20.9
18	0	-0	-8344	0	0	0	7114	--	--	16.08	16.08	0.00	0.12	0.07	0.52	0.00	0.00	20.9
19	0	-0	-8458	0	0	0	6967	--	--	16.08	16.08	0.00	0.12	0.07	0.53	0.00	0.00	20.9
20	0	-0	-8435	0	0	0	7013	--	--	16.08	16.08	0.00	0.12	0.07	0.53	0.00	0.00	20.9
37	0	-0	-7929	0	0	0	6752	--	--	16.08	16.08	0.00	0.12	0.07	0.50	0.00	0.00	20.9
38	0	-0	-8119	0	0	0	6507	--	--	16.08	16.08	0.00	0.11	0.07	0.51	0.00	0.00	20.9
39	0	-0	-8081	0	0	0	6585	--	--	16.08	16.08	0.00	0.11	0.07	0.51	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-7569	0	0	0	6159	--	--	16.08	16.08	0.00	0.11	0.06	0.47	0.00	0.00	20.9
2	27	-0	-5858	0	0	0	4803	--	--	16.08	16.08	0.10	0.09	0.05	0.37	0.00	0.00	20.9
3	27	-0	-5756	0	0	0	4712	--	--	16.08	16.08	0.10	0.08	0.05	0.36	0.00	0.00	20.9
4	27	-0	-5888	0	0	0	4763	--	--	16.08	16.08	0.10	0.08	0.05	0.37	0.00	0.00	20.9
5	27	-0	-5786	0	0	0	4672	--	--	16.08	16.08	0.10	0.08	0.05	0.36	0.00	0.00	20.9
6	27	-0	-5988	0	0	0	4895	--	--	16.08	16.08	0.10	0.09	0.05	0.38	0.00	0.00	20.9
7	27	-0	-5647	0	0	0	4592	--	--	16.08	16.08	0.10	0.08	0.05	0.35	0.00	0.00	20.9
8	27	-0	-5997	0	0	0	4883	--	--	16.08	16.08	0.10	0.09	0.05	0.38	0.00	0.00	20.9
9	27	-0	-5656	0	0	0	4580	--	--	16.08	16.08	0.10	0.08	0.05	0.35	0.00	0.00	20.9
10	27	-0	-5858	0	0	0	4803	--	--	16.08	16.08	0.10	0.09	0.05	0.37	0.00	0.00	20.9
11	27	-0	-5756	0	0	0	4712	--	--	16.08	16.08	0.10	0.08	0.05	0.36	0.00	0.00	20.9
12	27	-0	-5888	0	0	0	4763	--	--	16.08	16.08	0.10	0.08	0.05	0.37	0.00	0.00	20.9
13	27	-0	-5786	0	0	0	4672	--	--	16.08	16.08	0.10	0.08	0.05	0.36	0.00	0.00	20.9
14	27	-0	-5988	0	0	0	4895	--	--	16.08	16.08	0.10	0.09	0.05	0.38	0.00	0.00	20.9
15	27	-0	-5647	0	0	0	4592	--	--	16.08	16.08	0.10	0.08	0.05	0.35	0.00	0.00	20.9
16	27	-0	-5997	0	0	0	4883	--	--	16.08	16.08	0.10	0.09	0.05	0.38	0.00	0.00	20.9
17	27	-0	-5656	0	0	0	4580	--	--	16.08	16.08	0.10	0.08	0.05	0.35	0.00	0.00	20.9
18	27	-0	-8344	0	0	0	7114	--	--	16.08	16.08	0.00	0.12	0.07	0.52	0.00	0.00	20.9
19	27	-0	-8458	0	0	0	6967	--	--	16.08	16.08	0.00	0.12	0.07	0.53	0.00	0.00	20.9
20	27	-0	-8435	0	0	0	7013	--	--	16.08	16.08	0.00	0.12	0.07	0.53	0.00	0.00	20.9
37	27	-0	-7929	0	0	0	6752	--	--	16.08	16.08	0.00	0.12	0.07	0.50	0.00	0.00	20.9
38	27	-0	-8119	0	0	0	6507	--	--	16.08	16.08	0.00	0.11	0.07	0.51	0.00	0.00	20.9
39	27	-0	-8081	0	0	0	6585	--	--	16.08	16.08	0.00	0.11	0.07	0.51	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	54	-0	-7569	0	0	0	2104	--	--	16.08	16.08	0.00	0.04	0.06	0.47	0.00	0.00	20.9
2	54	-0	-5858	0	0	0	1665	--	--	16.08	16.08	0.10	0.03	0.05	0.37	0.00	0.00	20.9
3	54	-0	-5756	0	0	0	1629	--	--	16.08	16.08	0.10	0.03	0.05	0.36	0.00	0.00	20.9
4	54	-0	-5888	0	0	0	1608	--	--	16.08	16.08	0.10	0.03	0.05	0.37	0.00	0.00	20.9
5	54	-0	-5786	0	0	0	1572	--	--	16.08	16.08	0.10	0.03	0.05	0.36	0.00	0.00	20.9
6	54	-0	-5988	0	0	0	1688	--	--	16.08	16.08	0.10	0.03	0.05	0.38	0.00	0.00	20.9
7	54	-0	-5647	0	0	0	1567	--	--	16.08	16.08	0.10	0.03	0.05	0.35	0.00	0.00	20.9
8	54	-0	-5997	0	0	0	1671	--	--	16.08	16.08	0.10	0.03	0.05	0.38	0.00	0.00	20.9
9	54	-0	-5656	0	0	0	1550	--	--	16.08	16.08	0.10	0.03	0.05	0.35	0.00	0.00	20.9
10	54	-0	-5858	0	0	0	1665	--	--	16.08	16.08	0.10	0.03	0.05	0.37	0.00	0.00	20.9
11	54	-0	-5756	0	0	0	1629	--	--	16.08	16.08	0.10	0.03	0.05	0.36	0.00	0.00	20.9
12	54	-0	-5888	0	0	0	1608	--	--	16.08	16.08	0.10	0.03	0.05	0.37	0.00	0.00	20.9
13	54	-0	-5786	0	0	0	1572	--	--	16.08	16.08	0.10	0.03	0.05	0.36	0.00	0.00	20.9
14	54	-0	-5988	0	0	0	1688	--	--	16.08	16.08	0.10	0.03	0.05	0.38	0.00	0.00	20.9
15	54	-0	-5647	0	0	0	1567	--	--	16.08	16.08	0.10	0.03	0.05	0.35	0.00	0.00	20.9
16	54	-0	-5997	0	0	0	1671	--	--	16.08	16.08	0.10	0.03	0.05	0.38	0.00	0.00	20.9
17	54	-0	-5656	0	0	0	1550	--	--	16.08	16.08	0.10	0.03	0.05	0.35	0.00	0.00	20.9
18	54	-0	-8344	0	0	0	2644	--	--	16.08	16.08	0.00	0.05	0.07	0.52	0.00	0.00	20.9
19	54	-0	-8458	0	0	0	2436	--	--	16.08	16.08	0.00	0.04	0.07	0.53	0.00	0.00	20.9
20	54	-0	-8435	0	0	0	2495	--	--	16.08	16.08	0.00	0.04	0.07	0.53	0.00	0.00	20.9
37	54	-0	-7929	0	0	0	2504	--	--	16.08	16.08	0.00	0.04	0.07	0.50	0.00	0.00	20.9
38	54	-0	-8119	0	0	0	2158	--	--	16.08	16.08	0.00	0.04	0.07	0.51	0.00	0.00	20.9
39	54	-0	-8081	0	0	0	2256	--	--	16.08	16.08	0.00	0.04	0.07	0.51	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 112 NI 1977 NF 1961 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-9743	0	0	0	11380	--	--	16.08	16.08	0.00	0.19	0.08	0.61	0.00	0.00	20.9
2	0	-0	-7531	0	0	0	8838	--	--	16.08	16.08	0.10	0.16	0.06	0.47	0.00	0.00	20.9
3	0	-0	-7423	0	0	0	8689	--	--	16.08	16.08	0.10	0.15	0.06	0.47	0.00	0.00	20.9
4	0	-0	-7567	0	0	0	8816	--	--	16.08	16.08	0.10	0.16	0.06	0.47	0.00	0.00	20.9
5	0	-0	-7459	0	0	0	8667	--	--	16.08	16.08	0.10	0.15	0.06	0.47	0.00	0.00	20.9
6	0	-0	-7670	0	0	0	9004	--	--	16.08	16.08	0.10	0.16	0.06	0.48	0.00	0.00	20.9
7	0	-0	-7309	0	0	0	8507	--	--	16.08	16.08	0.10	0.15	0.06	0.46	0.00	0.00	20.9
8	0	-0	-7681	0	0	0	8998	--	--	16.08	16.08	0.10	0.16	0.06	0.48	0.00	0.00	20.9
9	0	-0	-7320	0	0	0	8501	--	--	16.08	16.08	0.10	0.15	0.06	0.46	0.00	0.00	20.9
10	0	-0	-7531	0	0	0	8838	--	--	16.08	16.08	0.10	0.16	0.06	0.47	0.00	0.00	20.9
11	0	-0	-7423	0	0	0	8689	--	--	16.08	16.08	0.10	0.15	0.06	0.47	0.00	0.00	20.9
12	0	-0	-7567	0	0	0	8816	--	--	16.08	16.08	0.10	0.16	0.06	0.47	0.00	0.00	20.9
13	0	-0	-7459	0	0	0	8667	--	--	16.08	16.08	0.10	0.15	0.06	0.47	0.00	0.00	20.9
14	0	-0	-7670	0	0	0	9004	--	--	16.08	16.08	0.10	0.16	0.06	0.48	0.00	0.00	20.9
15	0	-0	-7309	0	0	0	8507	--	--	16.08	16.08	0.10	0.15	0.06	0.46	0.00	0.00	20.9
16	0	-0	-7681	0	0	0	8998	--	--	16.08	16.08	0.10	0.16	0.06	0.48	0.00	0.00	20.9
17	0	-0	-7320	0	0	0	8501	--	--	16.08	16.08	0.10	0.15	0.06	0.46	0.00	0.00	20.9
18	0	-0	-10700	0	0	0	12850	--	--	16.08	16.08	0.00	0.22	0.09	0.67	0.00	0.00	20.9
19	0	-0	-10840	0	0	0	12770	--	--	16.08	16.08	0.00	0.22	0.09	0.68	0.00	0.00	20.9
20	0	-0	-10790	0	0	0	12790	--	--	16.08	16.08	0.00	0.22	0.09	0.68	0.00	0.00	20.9
37	0	-0	-10190	0	0	0	12210	--	--	16.08	16.08	0.00	0.21	0.08	0.64	0.00	0.00	20.9
38	0	-0	-10420	0	0	0	12090	--	--	16.08	16.08	0.00	0.21	0.09	0.65	0.00	0.00	20.9
39	0	-0	-10340	0	0	0	12120	--	--	16.08	16.08	0.00	0.21	0.09	0.65	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-9743	0	0	0	11380	--	--	16.08	16.08	0.00	0.19	0.08	0.61	0.00	0.00	20.9
2	27	-0	-7531	0	0	0	8838	--	--	16.08	16.08	0.10	0.16	0.06	0.47	0.00	0.00	20.9
3	27	-0	-7423	0	0	0	8689	--	--	16.08	16.08	0.10	0.15	0.06	0.47	0.00	0.00	20.9
4	27	-0	-7567	0	0	0	8816	--	--	16.08	16.08	0.10	0.16	0.06	0.47	0.00	0.00	20.9
5	27	-0	-7459	0	0	0	8667	--	--	16.08	16.08	0.10	0.15	0.06	0.47	0.00	0.00	20.9
6	27	-0	-7670	0	0	0	9004	--	--	16.08	16.08	0.10	0.16	0.06	0.48	0.00	0.00	20.9
7	27	-0	-7309	0	0	0	8507	--	--	16.08	16.08	0.10	0.15	0.06	0.46	0.00	0.00	20.9
8	27	-0	-7681	0	0	0	8998	--	--	16.08	16.08	0.10	0.16	0.06	0.48	0.00	0.00	20.9
9	27	-0	-7320	0	0	0	8501	--	--	16.08	16.08	0.10	0.15	0.06	0.46	0.00	0.00	20.9
10	27	-0	-7531	0	0	0	8838	--	--	16.08	16.08	0.10	0.16	0.06	0.47	0.00	0.00	20.9
11	27	-0	-7423	0	0	0	8689	--	--	16.08	16.08	0.10	0.15	0.06	0.47	0.00	0.00	20.9
12	27	-0	-7567	0	0	0	8816	--	--	16.08	16.08	0.10	0.16	0.06	0.47	0.00	0.00	20.9
13	27	-0	-7459	0	0	0	8667	--	--	16.08	16.08	0.10	0.15	0.06	0.47	0.00	0.00	20.9
14	27	-0	-7670	0	0	0	9004	--	--	16.08	16.08	0.10	0.16	0.06	0.48	0.00	0.00	20.9
15	27	-0	-7309	0	0	0	8507	--	--	16.08	16.08	0.10	0.15	0.06	0.46	0.00	0.00	20.9
16	27	-0	-7681	0	0	0	8998	--	--	16.08	16.08	0.10	0.16	0.06	0.48	0.00	0.00	20.9
17	27	-0	-7320	0	0	0	8501	--	--	16.08	16.08	0.10	0.15	0.06	0.46	0.00	0.00	20.9
18	27	-0	-10700	0	0	0	12850	--	--	16.08	16.08	0.00	0.22	0.09	0.67	0.00	0.00	20.9
19	27	-0	-10840	0	0	0	12770	--	--	16.08	16.08	0.00	0.22	0.09	0.68	0.00	0.00	20.9
20	27	-0	-10790	0	0	0	12790	--	--	16.08	16.08	0.00	0.22	0.09	0.68	0.00	0.00	20.9
37	27	-0	-10190	0	0	0	12210	--	--	16.08	16.08	0.00	0.21	0.08	0.64	0.00	0.00	20.9
38	27	-0	-10420	0	0	0	12090	--	--	16.08	16.08	0.00	0.21	0.09	0.65	0.00	0.00	20.9
39	27	-0	-10340	0	0	0	12120	--	--	16.08	16.08	0.00	0.21	0.09	0.65	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	54	-0	-9743	0	0	0	6159	--	--	16.08	16.08	0.00	0.11	0.08	0.61	0.00	0.00	20.9
2	54	-0	-7531	0	0	0	4803	--	--	16.08	16.08	0.10	0.09	0.06	0.47	0.00	0.00	20.9
3	54	-0	-7423	0	0	0	4712	--	--	16.08	16.08	0.10	0.08	0.06	0.47	0.00	0.00	20.9
4	54	-0	-7567	0	0	0	4763	--	--	16.08	16.08	0.10	0.08	0.06	0.47	0.00	0.00	20.9
5	54	-0	-7459	0	0	0	4672	--	--	16.08	16.08	0.10	0.08	0.06	0.47	0.00	0.00	20.9
6	54	-0	-7670	0	0	0	4895	--	--	16.08	16.08	0.10	0.09	0.06	0.48	0.00	0.00	20.9
7	54	-0	-7309	0	0	0	4592	--	--	16.08	16.08	0.10	0.08	0.06	0.46	0.00	0.00	20.9
8	54	-0	-7681	0	0	0	4883	--	--	16.08	16.08	0.10	0.09	0.06	0.48	0.00	0.00	20.9
9	54	-0	-7320	0	0	0	4580	--	--	16.08	16.08	0.10	0.08	0.06	0.46	0.00	0.00	20.9
10	54	-0	-7531	0	0	0	4803	--	--	16.08	16.08	0.10	0.09	0.06	0.47	0.00	0.00	20.9
11	54	-0	-7423	0	0	0	4712	--	--	16.08	16.08	0.10	0.08	0.06	0.47	0.00	0.00	20.9
12	54	-0	-7567	0	0	0	4763	--	--	16.08	16.08	0.10	0.08	0.06	0.47	0.00	0.00	20.9
13	54	-0	-7459	0	0	0	4672	--	--	16.08	16.08	0.10	0.08	0.06	0.47	0.00	0.00	20.9
14	54	-0	-7670	0	0	0	4895	--	--	16.08	16.08	0.10	0.09	0.06	0.48	0.00	0.00	20.9
15	54	-0	-7309	0	0	0	4592	--	--	16.08	16.08	0.10	0.08	0.06	0.46	0.00	0.00	20.9
16	54	-0	-7681	0	0	0	4883	--	--	16.08	16.08	0.10	0.09	0.06	0.48	0.00	0.00	20.9
17	54	-0	-7320	0	0	0	4580	--	--	16.08	16.08	0.10	0.08	0.06	0.46	0.00	0.00	20.9
18	54	-0	-10700	0	0	0	7114	--	--	16.08	16.08	0.00	0.12	0.09	0.67	0.00	0.00	20.9
19	54	-0	-10840	0	0	0	6967	--	--	16.08	16.08	0.00	0.12	0.09	0.68	0.00	0.00	20.9
20	54	-0	-10790	0	0	0	7013	--	--	16.08	16.08	0.00	0.12	0.09	0.68	0.00	0.00	20.9
37	54	-0	-10190	0	0	0	6752	--	--	16.08	16.08	0.00	0.12	0.08	0.64	0.00	0.00	20.9
38	54	-0	-10420	0	0	0	6507	--	--	16.08	16.08	0.00	0.11	0.09	0.65	0.00	0.00	20.9
39	54	-0	-10340	0	0	0	6585	--	--	16.08	16.08	0.00	0.11	0.09	0.65	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 113 NI 1973 NF 1977 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	7775	0	0	0	6630	--	--	16.08	16.08	0.00	0.11	0.06	0.49	0.00	0.00	20.9
2	0	-0	5977	0	0	0	5113	--	--	16.08	16.08	0.10	0.09	0.05	0.37	0.00	0.00	20.9
3	0	-0	6012	0	0	0	5185	--	--	16.08	16.08	0.10	0.09	0.05	0.38	0.00	0.00	20.9
4	0	-0	5949	0	0	0	5015	--	--	16.08	16.08	0.10	0.09	0.05	0.37	0.00	0.00	20.9
5	0	-0	5984	0	0	0	5087	--	--	16.08	16.08	0.10	0.09	0.05	0.38	0.00	0.00	20.9
6	0	-0	5927	0	0	0	4995	--	--	16.08	16.08	0.10	0.09	0.05	0.37	0.00	0.00	20.9
7	0	-0	6043	0	0	0	5235	--	--	16.08	16.08	0.10	0.09	0.05	0.38	0.00	0.00	20.9
8	0	-0	5919	0	0	0	4966	--	--	16.08	16.08	0.10	0.09	0.05	0.37	0.00	0.00	20.9
9	0	-0	6034	0	0	0	5205	--	--	16.08	16.08	0.10	0.09	0.05	0.38	0.00	0.00	20.9
10	0	-0	5977	0	0	0	5113	--	--	16.08	16.08	0.10	0.09	0.05	0.37	0.00	0.00	20.9
11	0	-0	6012	0	0	0	5185	--	--	16.08	16.08	0.10	0.09	0.05	0.38	0.00	0.00	20.9
12	0	-0	5949	0	0	0	5015	--	--	16.08	16.08	0.10	0.09	0.05	0.37	0.00	0.00	20.9
13	0	-0	5984	0	0	0	5087	--	--	16.08	16.08	0.10	0.09	0.05	0.38	0.00	0.00	20.9
14	0	-0	5927	0	0	0	4995	--	--	16.08	16.08	0.10	0.09	0.05	0.37	0.00	0.00	20.9
15	0	-0	6043	0	0	0	5235	--	--	16.08	16.08	0.10	0.09	0.05	0.38	0.00	0.00	20.9
16	0	-0	5919	0	0	0	4966	--	--	16.08	16.08	0.10	0.09	0.05	0.37	0.00	0.00	20.9

17	0	-0	6034	0	0	0	5205	--	--	16.08	16.08	0.10	0.09	0.05	0.38	0.00	0.00	20.9
18	0	-0	8405	0	0	0	7573	--	--	16.08	16.08	0.00	0.13	0.07	0.53	0.00	0.00	20.9
19	0	-0	8307	0	0	0	7164	--	--	16.08	16.08	0.00	0.12	0.07	0.52	0.00	0.00	20.9
20	0	-0	8206	0	0	0	7205	--	--	16.08	16.08	0.00	0.12	0.07	0.51	0.00	0.00	20.9
37	0	-0	8125	0	0	0	7336	--	--	16.08	16.08	0.00	0.13	0.07	0.51	0.00	0.00	20.9
38	0	-0	7962	0	0	0	6655	--	--	16.08	16.08	0.00	0.11	0.07	0.50	0.00	0.00	20.9
39	0	-0	7793	0	0	0	6722	--	--	16.08	16.08	0.00	0.11	0.06	0.49	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	7775	0	0	0	17025	--	--	16.08	16.08	0.00	0.29	0.06	0.49	0.00	0.00	20.9
2	27	-0	5977	0	0	0	13102	--	--	16.08	16.08	0.10	0.23	0.05	0.37	0.00	0.00	20.9
3	27	-0	6012	0	0	0	13221	--	--	16.08	16.08	0.10	0.23	0.05	0.38	0.00	0.00	20.9
4	27	-0	5949	0	0	0	12966	--	--	16.08	16.08	0.10	0.23	0.05	0.37	0.00	0.00	20.9
5	27	-0	5984	0	0	0	13085	--	--	16.08	16.08	0.10	0.23	0.05	0.38	0.00	0.00	20.9
6	27	-0	5927	0	0	0	12917	--	--	16.08	16.08	0.10	0.23	0.05	0.37	0.00	0.00	20.9
7	27	-0	6043	0	0	0	13312	--	--	16.08	16.08	0.10	0.24	0.05	0.38	0.00	0.00	20.9
8	27	-0	5919	0	0	0	12877	--	--	16.08	16.08	0.10	0.23	0.05	0.37	0.00	0.00	20.9
9	27	-0	6034	0	0	0	13270	--	--	16.08	16.08	0.10	0.24	0.05	0.38	0.00	0.00	20.9
10	27	-0	5977	0	0	0	13102	--	--	16.08	16.08	0.10	0.23	0.05	0.37	0.00	0.00	20.9
11	27	-0	6012	0	0	0	13221	--	--	16.08	16.08	0.10	0.23	0.05	0.38	0.00	0.00	20.9
12	27	-0	5949	0	0	0	12966	--	--	16.08	16.08	0.10	0.23	0.05	0.37	0.00	0.00	20.9
13	27	-0	5984	0	0	0	13085	--	--	16.08	16.08	0.10	0.23	0.05	0.38	0.00	0.00	20.9
14	27	-0	5927	0	0	0	12917	--	--	16.08	16.08	0.10	0.23	0.05	0.37	0.00	0.00	20.9
15	27	-0	6043	0	0	0	13312	--	--	16.08	16.08	0.10	0.24	0.05	0.38	0.00	0.00	20.9
16	27	-0	5919	0	0	0	12877	--	--	16.08	16.08	0.10	0.23	0.05	0.37	0.00	0.00	20.9
17	27	-0	6034	0	0	0	13270	--	--	16.08	16.08	0.10	0.24	0.05	0.38	0.00	0.00	20.9
18	27	-0	8405	0	0	0	18804	--	--	16.08	16.08	0.00	0.32	0.07	0.53	0.00	0.00	20.9
19	27	-0	8307	0	0	0	18265	--	--	16.08	16.08	0.00	0.31	0.07	0.52	0.00	0.00	20.9
20	27	-0	8206	0	0	0	18173	--	--	16.08	16.08	0.00	0.31	0.07	0.51	0.00	0.00	20.9
37	27	-0	8125	0	0	0	18197	--	--	16.08	16.08	0.00	0.31	0.07	0.51	0.00	0.00	20.9
38	27	-0	7962	0	0	0	17297	--	--	16.08	16.08	0.00	0.29	0.07	0.50	0.00	0.00	20.9
39	27	-0	7793	0	0	0	17140	--	--	16.08	16.08	0.00	0.29	0.06	0.49	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	54	-0	7775	0	0	0	10800	--	--	16.08	16.08	0.00	0.18	0.06	0.49	0.00	0.00	20.9
2	54	-0	5977	0	0	0	8315	--	--	16.08	16.08	0.10	0.15	0.05	0.37	0.00	0.00	20.9
3	54	-0	6012	0	0	0	8406	--	--	16.08	16.08	0.10	0.15	0.05	0.38	0.00	0.00	20.9
4	54	-0	5949	0	0	0	8202	--	--	16.08	16.08	0.10	0.15	0.05	0.37	0.00	0.00	20.9
5	54	-0	5984	0	0	0	8293	--	--	16.08	16.08	0.10	0.15	0.05	0.38	0.00	0.00	20.9
6	54	-0	5927	0	0	0	8170	--	--	16.08	16.08	0.10	0.14	0.05	0.37	0.00	0.00	20.9
7	54	-0	6043	0	0	0	8472	--	--	16.08	16.08	0.10	0.15	0.05	0.38	0.00	0.00	20.9
8	54	-0	5919	0	0	0	8136	--	--	16.08	16.08	0.10	0.14	0.05	0.37	0.00	0.00	20.9
9	54	-0	6034	0	0	0	8438	--	--	16.08	16.08	0.10	0.15	0.05	0.38	0.00	0.00	20.9
10	54	-0	5977	0	0	0	8315	--	--	16.08	16.08	0.10	0.15	0.05	0.37	0.00	0.00	20.9
11	54	-0	6012	0	0	0	8406	--	--	16.08	16.08	0.10	0.15	0.05	0.38	0.00	0.00	20.9
12	54	-0	5949	0	0	0	8202	--	--	16.08	16.08	0.10	0.15	0.05	0.37	0.00	0.00	20.9
13	54	-0	5984	0	0	0	8293	--	--	16.08	16.08	0.10	0.15	0.05	0.38	0.00	0.00	20.9
14	54	-0	5927	0	0	0	8170	--	--	16.08	16.08	0.10	0.14	0.05	0.37	0.00	0.00	20.9
15	54	-0	6043	0	0	0	8472	--	--	16.08	16.08	0.10	0.15	0.05	0.38	0.00	0.00	20.9
16	54	-0	5919	0	0	0	8136	--	--	16.08	16.08	0.10	0.14	0.05	0.37	0.00	0.00	20.9
17	54	-0	6034	0	0	0	8438	--	--	16.08	16.08	0.10	0.15	0.05	0.38	0.00	0.00	20.9
18	54	-0	8405	0	0	0	12070	--	--	16.08	16.08	0.00	0.21	0.07	0.53	0.00	0.00	20.9
19	54	-0	8307	0	0	0	11610	--	--	16.08	16.08	0.00	0.20	0.07	0.52	0.00	0.00	20.9
20	54	-0	8206	0	0	0	11600	--	--	16.08	16.08	0.00	0.20	0.07	0.51	0.00	0.00	20.9
37	54	-0	8125	0	0	0	11690	--	--	16.08	16.08	0.00	0.20	0.07	0.51	0.00	0.00	20.9
38	54	-0	7962	0	0	0	10920	--	--	16.08	16.08	0.00	0.19	0.07	0.50	0.00	0.00	20.9
39	54	-0	7793	0	0	0	10900	--	--	16.08	16.08	0.00	0.19	0.06	0.49	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 114 NI 1965 NF 1973 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	5505	0	0	0	3681	--	--	16.08	16.08	0.00	0.06	0.05	0.35	0.00	0.00	20.9
2	0	-0	4234	0	0	0	2845	--	--	16.08	16.08	0.10	0.05	0.03	0.27	0.00	0.00	20.9
3	0	-0	4273	0	0	0	2896	--	--	16.08	16.08	0.10	0.05	0.04	0.27	0.00	0.00	20.9
4	0	-0	4196	0	0	0	2767	--	--	16.08	16.08	0.10	0.05	0.03	0.26	0.00	0.00	20.9
5	0	-0	4235	0	0	0	2819	--	--	16.08	16.08	0.10	0.05	0.03	0.27	0.00	0.00	20.9
6	0	-0	4175	0	0	0	2758	--	--	16.08	16.08	0.10	0.05	0.03	0.26	0.00	0.00	20.9
7	0	-0	4305	0	0	0	2928	--	--	16.08	16.08	0.10	0.05	0.04	0.27	0.00	0.00	20.9
8	0	-0	4164	0	0	0	2735	--	--	16.08	16.08	0.10	0.05	0.03	0.26	0.00	0.00	20.9
9	0	-0	4294	0	0	0	2905	--	--	16.08	16.08	0.10	0.05	0.04	0.27	0.00	0.00	20.9
10	0	-0	4234	0	0	0	2845	--	--	16.08	16.08	0.10	0.05	0.03	0.27	0.00	0.00	20.9
11	0	-0	4273	0	0	0	2896	--	--	16.08	16.08	0.10	0.05	0.04	0.27	0.00	0.00	20.9
12	0	-0	4196	0	0	0	2767	--	--	16.08	16.08	0.10	0.05	0.03	0.26	0.00	0.00	20.9
13	0	-0	4235	0	0	0	2819	--	--	16.08	16.08	0.10	0.05	0.03	0.27	0.00	0.00	20.9
14	0	-0	4175	0	0	0	2758	--	--	16.08	16.08	0.10	0.05	0.03	0.26	0.00	0.00	20.9
15	0	-0	4305	0	0	0	2928	--	--	16.08	16.08	0.10	0.05	0.04	0.27	0.00	0.00	20.9
16	0	-0	4164	0	0	0	2735	--	--	16.08	16.08	0.10	0.05	0.03	0.26	0.00	0.00	20.9
17	0	-0	4294	0	0	0	2905	--	--	16.08	16.08	0.10	0.05	0.04	0.27	0.00	0.00	20.9
18	0	-0	5942	0	0	0	4390	--	--	16.08	16.08	0.00	0.07	0.05	0.37	0.00	0.00	20.9
19	0	-0	5799	0	0	0	4058	--	--	16.08	16.08	0.00	0.07	0.05	0.36	0.00	0.00	20.9
20	0	-0	5741	0	0	0	4129	--	--	16.08	16.08	0.00	0.07	0.05	0.36	0.00	0.00	20.9
37	0	-0	5772	0	0	0	4243	--	--	16.08	16.08	0.00	0.07	0.05	0.36	0.00	0.00	20.9
38	0	-0	5533	0	0	0	3691	--	--	16.08	16.08	0.00	0.06	0.05	0.35	0.00	0.00	20.9
39	0	-0	5437	0	0	0	3810	--	--	16.08	16.08	0.00	0.06	0.04	0.34	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	5505	0	0	0	11039	--	--	16.08	16.08	0.00	0.19	0.05	0.35	0.00	0.00	20.9
2	27	-0	4234	0	0	0	8504	--	--	16.08	16.08	0.10	0.15	0.03	0.27	0.00	0.00	20.9
3	27	-0	4273	0	0	0	8607	--	--	16.08	16.08	0.10	0.15	0.04	0.27	0.00	0.00	20.9
4	27	-0	4196	0	0	0	8375	--	--	16.08	16.08	0.10	0.15	0.03	0.26	0.00	0.00	20.9
5	27	-0	4235	0	0	0	8479	--	--	16.08	16.08	0.10	0.15	0.03	0.27	0.00	0.00	20.9
6	27	-0	4175	0	0	0	8339	--	--	16.08	16.08	0.10	0.15	0.03	0.26	0.00	0.00	20.9
7	27	-0	4305	0	0	0	8682	--	--	16.08	16.08	0.10	0.15	0.04	0.27	0.00	0.00	20.9
8	27	-0	4164	0	0	0	8301	--	--	16.08	16.08	0.10	0.15	0.03	0.26	0.00	0.00	20.9
9	27	-0	4294	0	0	0	8644	--	--	16.08	16.08	0.10	0.15	0.04	0.27	0.00	0.00	20.9
10	27	-0	4234	0	0	0	8504	--	--	16.08	16.08	0.10	0.15	0.03	0.27	0.00	0.00	20.9
11	27	-0	4273	0	0	0	8607	--	--	16.08	16.08	0.10	0.15	0.04	0.27	0.00	0.00	20.9
12	27	-0	4196	0	0	0	8375	--	--	16.08	16.08	0.10	0.15	0.03	0.26	0.00	0.00	20.9

13	27	-0	4235	0	0	0	8479	--	--	16.08	16.08	0.10	0.15	0.03	0.27	0.00	0.00	20.9
14	27	-0	4175	0	0	0	8339	--	--	16.08	16.08	0.10	0.15	0.03	0.26	0.00	0.00	20.9
15	27	-0	4305	0	0	0	8682	--	--	16.08	16.08	0.10	0.15	0.04	0.27	0.00	0.00	20.9
16	27	-0	4164	0	0	0	8301	--	--	16.08	16.08	0.10	0.15	0.03	0.26	0.00	0.00	20.9
17	27	-0	4294	0	0	0	8644	--	--	16.08	16.08	0.10	0.15	0.04	0.27	0.00	0.00	20.9
18	27	-0	5942	0	0	0	12332	--	--	16.08	16.08	0.00	0.21	0.05	0.37	0.00	0.00	20.9
19	27	-0	5799	0	0	0	11809	--	--	16.08	16.08	0.00	0.20	0.05	0.36	0.00	0.00	20.9
20	27	-0	5741	0	0	0	11803	--	--	16.08	16.08	0.00	0.20	0.05	0.36	0.00	0.00	20.9
37	27	-0	5772	0	0	0	11958	--	--	16.08	16.08	0.00	0.20	0.05	0.36	0.00	0.00	20.9
38	27	-0	5533	0	0	0	11086	--	--	16.08	16.08	0.00	0.19	0.05	0.35	0.00	0.00	20.9
39	27	-0	5437	0	0	0	11077	--	--	16.08	16.08	0.00	0.19	0.04	0.34	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	54	-0	5505	0	0	0	6630	--	--	16.08	16.08	0.00	0.11	0.05	0.35	0.00	0.00	20.9
2	54	-0	4234	0	0	0	5113	--	--	16.08	16.08	0.10	0.09	0.03	0.27	0.00	0.00	20.9
3	54	-0	4273	0	0	0	5185	--	--	16.08	16.08	0.10	0.09	0.04	0.27	0.00	0.00	20.9
4	54	-0	4196	0	0	0	5015	--	--	16.08	16.08	0.10	0.09	0.03	0.26	0.00	0.00	20.9
5	54	-0	4235	0	0	0	5087	--	--	16.08	16.08	0.10	0.09	0.03	0.27	0.00	0.00	20.9
6	54	-0	4175	0	0	0	4995	--	--	16.08	16.08	0.10	0.09	0.03	0.26	0.00	0.00	20.9
7	54	-0	4305	0	0	0	5235	--	--	16.08	16.08	0.10	0.09	0.04	0.27	0.00	0.00	20.9
8	54	-0	4164	0	0	0	4966	--	--	16.08	16.08	0.10	0.09	0.03	0.26	0.00	0.00	20.9
9	54	-0	4294	0	0	0	5205	--	--	16.08	16.08	0.10	0.09	0.04	0.27	0.00	0.00	20.9
10	54	-0	4234	0	0	0	5113	--	--	16.08	16.08	0.10	0.09	0.03	0.27	0.00	0.00	20.9
11	54	-0	4273	0	0	0	5185	--	--	16.08	16.08	0.10	0.09	0.04	0.27	0.00	0.00	20.9
12	54	-0	4196	0	0	0	5015	--	--	16.08	16.08	0.10	0.09	0.03	0.26	0.00	0.00	20.9
13	54	-0	4235	0	0	0	5087	--	--	16.08	16.08	0.10	0.09	0.03	0.27	0.00	0.00	20.9
14	54	-0	4175	0	0	0	4995	--	--	16.08	16.08	0.10	0.09	0.03	0.26	0.00	0.00	20.9
15	54	-0	4305	0	0	0	5235	--	--	16.08	16.08	0.10	0.09	0.04	0.27	0.00	0.00	20.9
16	54	-0	4164	0	0	0	4966	--	--	16.08	16.08	0.10	0.09	0.03	0.26	0.00	0.00	20.9
17	54	-0	4294	0	0	0	5205	--	--	16.08	16.08	0.10	0.09	0.04	0.27	0.00	0.00	20.9
18	54	-0	5942	0	0	0	7573	--	--	16.08	16.08	0.00	0.13	0.05	0.37	0.00	0.00	20.9
19	54	-0	5799	0	0	0	7164	--	--	16.08	16.08	0.00	0.12	0.05	0.36	0.00	0.00	20.9
20	54	-0	5741	0	0	0	7205	--	--	16.08	16.08	0.00	0.12	0.05	0.36	0.00	0.00	20.9
37	54	-0	5772	0	0	0	7336	--	--	16.08	16.08	0.00	0.13	0.05	0.36	0.00	0.00	20.9
38	54	-0	5533	0	0	0	6655	--	--	16.08	16.08	0.00	0.11	0.05	0.35	0.00	0.00	20.9
39	54	-0	5437	0	0	0	6722	--	--	16.08	16.08	0.00	0.11	0.04	0.34	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 115 NI 1971 NF 1965 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	3266	0	0	0	1932	--	--	16.08	16.08	0.00	0.03	0.03	0.20	0.00	0.00	20.9
2	0	-0	2517	0	0	0	1497	--	--	16.08	16.08	0.10	0.03	0.02	0.16	0.00	0.00	20.9
3	0	-0	2559	0	0	0	1525	--	--	16.08	16.08	0.10	0.03	0.02	0.16	0.00	0.00	20.9
4	0	-0	2465	0	0	0	1447	--	--	16.08	16.08	0.10	0.03	0.02	0.15	0.00	0.00	20.9
5	0	-0	2508	0	0	0	1475	--	--	16.08	16.08	0.10	0.03	0.02	0.16	0.00	0.00	20.9
6	0	-0	2449	0	0	0	1446	--	--	16.08	16.08	0.10	0.03	0.02	0.15	0.00	0.00	20.9
7	0	-0	2591	0	0	0	1540	--	--	16.08	16.08	0.10	0.03	0.02	0.16	0.00	0.00	20.9
8	0	-0	2434	0	0	0	1431	--	--	16.08	16.08	0.10	0.03	0.02	0.15	0.00	0.00	20.9
9	0	-0	2575	0	0	0	1526	--	--	16.08	16.08	0.10	0.03	0.02	0.16	0.00	0.00	20.9
10	0	-0	2517	0	0	0	1497	--	--	16.08	16.08	0.10	0.03	0.02	0.16	0.00	0.00	20.9
11	0	-0	2559	0	0	0	1525	--	--	16.08	16.08	0.10	0.03	0.02	0.16	0.00	0.00	20.9
12	0	-0	2465	0	0	0	1447	--	--	16.08	16.08	0.10	0.03	0.02	0.15	0.00	0.00	20.9
13	0	-0	2508	0	0	0	1475	--	--	16.08	16.08	0.10	0.03	0.02	0.16	0.00	0.00	20.9
14	0	-0	2449	0	0	0	1446	--	--	16.08	16.08	0.10	0.03	0.02	0.15	0.00	0.00	20.9
15	0	-0	2591	0	0	0	1540	--	--	16.08	16.08	0.10	0.03	0.02	0.16	0.00	0.00	20.9
16	0	-0	2434	0	0	0	1431	--	--	16.08	16.08	0.10	0.03	0.02	0.15	0.00	0.00	20.9
17	0	-0	2575	0	0	0	1526	--	--	16.08	16.08	0.10	0.03	0.02	0.16	0.00	0.00	20.9
18	0	-0	3515	0	0	0	2507	--	--	16.08	16.08	0.00	0.04	0.03	0.22	0.00	0.00	20.9
19	0	-0	3315	0	0	0	2282	--	--	16.08	16.08	0.00	0.04	0.03	0.21	0.00	0.00	20.9
20	0	-0	3306	0	0	0	2358	--	--	16.08	16.08	0.00	0.04	0.03	0.21	0.00	0.00	20.9
37	0	-0	3458	0	0	0	2391	--	--	16.08	16.08	0.00	0.04	0.03	0.22	0.00	0.00	20.9
38	0	-0	3125	0	0	0	2017	--	--	16.08	16.08	0.00	0.03	0.03	0.20	0.00	0.00	20.9
39	0	-0	3110	0	0	0	2144	--	--	16.08	16.08	0.00	0.04	0.03	0.20	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	3266	0	0	0	6297	--	--	16.08	16.08	0.00	0.11	0.03	0.20	0.00	0.00	20.9
2	27	-0	2517	0	0	0	4861	--	--	16.08	16.08	0.10	0.09	0.02	0.16	0.00	0.00	20.9
3	27	-0	2559	0	0	0	4945	--	--	16.08	16.08	0.10	0.09	0.02	0.16	0.00	0.00	20.9
4	27	-0	2465	0	0	0	4741	--	--	16.08	16.08	0.10	0.08	0.02	0.15	0.00	0.00	20.9
5	27	-0	2508	0	0	0	4827	--	--	16.08	16.08	0.10	0.09	0.02	0.16	0.00	0.00	20.9
6	27	-0	2449	0	0	0	4719	--	--	16.08	16.08	0.10	0.08	0.02	0.15	0.00	0.00	20.9
7	27	-0	2591	0	0	0	5003	--	--	16.08	16.08	0.10	0.09	0.02	0.16	0.00	0.00	20.9
8	27	-0	2434	0	0	0	4684	--	--	16.08	16.08	0.10	0.08	0.02	0.15	0.00	0.00	20.9
9	27	-0	2575	0	0	0	4968	--	--	16.08	16.08	0.10	0.09	0.02	0.16	0.00	0.00	20.9
10	27	-0	2517	0	0	0	4861	--	--	16.08	16.08	0.10	0.09	0.02	0.16	0.00	0.00	20.9
11	27	-0	2559	0	0	0	4945	--	--	16.08	16.08	0.10	0.09	0.02	0.16	0.00	0.00	20.9
12	27	-0	2465	0	0	0	4741	--	--	16.08	16.08	0.10	0.08	0.02	0.15	0.00	0.00	20.9
13	27	-0	2508	0	0	0	4827	--	--	16.08	16.08	0.10	0.09	0.02	0.16	0.00	0.00	20.9
14	27	-0	2449	0	0	0	4719	--	--	16.08	16.08	0.10	0.08	0.02	0.15	0.00	0.00	20.9
15	27	-0	2591	0	0	0	5003	--	--	16.08	16.08	0.10	0.09	0.02	0.16	0.00	0.00	20.9
16	27	-0	2434	0	0	0	4684	--	--	16.08	16.08	0.10	0.08	0.02	0.15	0.00	0.00	20.9
17	27	-0	2575	0	0	0	4968	--	--	16.08	16.08	0.10	0.09	0.02	0.16	0.00	0.00	20.9
18	27	-0	3515	0	0	0	7205	--	--	16.08	16.08	0.00	0.12	0.03	0.22	0.00	0.00	20.9
19	27	-0	3315	0	0	0	6713	--	--	16.08	16.08	0.00	0.11	0.03	0.21	0.00	0.00	20.9
20	27	-0	3306	0	0	0	6777	--	--	16.08	16.08	0.00	0.12	0.03	0.21	0.00	0.00	20.9
37	27	-0	3458	0	0	0	7013	--	--	16.08	16.08	0.00	0.12	0.03	0.22	0.00	0.00	20.9
38	27	-0	3125	0	0	0	6194	--	--	16.08	16.08	0.00	0.11	0.03	0.20	0.00	0.00	20.9
39	27	-0	3110	0	0	0	6301	--	--	16.08	16.08	0.00	0.11	0.03	0.20	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	54	-0	3266	0	0	0	3681	--	--	16.08	16.08	0.00	0.06	0.03	0.20	0.00	0.00	20.9
2	54	-0	2517	0	0	0	2845	--	--	16.08	16.08	0.10	0.05	0.02	0.16	0.00	0.00	20.9
3	54	-0	2559	0	0	0	2896	--	--	16.08	16.08	0.10	0.05	0.02	0.16	0.00	0.00	20.9
4	54	-0	2465	0	0	0	2767	--	--	16.08	16.08	0.10	0.05	0.02	0.15	0.00	0.00	20.9
5	54	-0	2508	0	0	0	2819	--	--	16.08	16.08	0.10	0.05	0.02	0.16	0.00	0.00	20.9
6	54	-0	2449	0	0	0	2758	--	--	16.08	16.08	0.10	0.05	0.02	0.15	0.00	0.00	20.9
7	54	-0	2591	0	0	0	2928	--	--	16.08	16.08	0.10	0.05	0.02	0.16	0.00	0.00	20.9
8	54	-0	2434	0	0	0	2735	--	--	16.08	16.08	0.10	0.05	0.02	0.15	0.00	0.00	20.9

9	54	-0	2575	0	0	0	2905	--	--	16.08	16.08	0.10	0.05	0.02	0.16	0.00	0.00	20.9
10	54	-0	2517	0	0	0	2845	--	--	16.08	16.08	0.10	0.05	0.02	0.16	0.00	0.00	20.9
11	54	-0	2559	0	0	0	2896	--	--	16.08	16.08	0.10	0.05	0.02	0.16	0.00	0.00	20.9
12	54	-0	2465	0	0	0	2767	--	--	16.08	16.08	0.10	0.05	0.02	0.15	0.00	0.00	20.9
13	54	-0	2508	0	0	0	2819	--	--	16.08	16.08	0.10	0.05	0.02	0.16	0.00	0.00	20.9
14	54	-0	2449	0	0	0	2758	--	--	16.08	16.08	0.10	0.05	0.02	0.15	0.00	0.00	20.9
15	54	-0	2591	0	0	0	2928	--	--	16.08	16.08	0.10	0.05	0.02	0.16	0.00	0.00	20.9
16	54	-0	2434	0	0	0	2735	--	--	16.08	16.08	0.10	0.05	0.02	0.15	0.00	0.00	20.9
17	54	-0	2575	0	0	0	2905	--	--	16.08	16.08	0.10	0.05	0.02	0.16	0.00	0.00	20.9
18	54	-0	3515	0	0	0	4390	--	--	16.08	16.08	0.00	0.07	0.03	0.22	0.00	0.00	20.9
19	54	-0	3315	0	0	0	4058	--	--	16.08	16.08	0.00	0.07	0.03	0.21	0.00	0.00	20.9
20	54	-0	3306	0	0	0	4129	--	--	16.08	16.08	0.00	0.07	0.03	0.21	0.00	0.00	20.9
37	54	-0	3458	0	0	0	4243	--	--	16.08	16.08	0.00	0.07	0.03	0.22	0.00	0.00	20.9
38	54	-0	3125	0	0	0	3691	--	--	16.08	16.08	0.00	0.06	0.03	0.20	0.00	0.00	20.9
39	54	-0	3110	0	0	0	3810	--	--	16.08	16.08	0.00	0.06	0.03	0.20	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 116 NI 1972 NF 1971 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	1073	0	0	0	1357	--	--	16.08	16.08	0.00	0.02	0.01	0.07	0.00	0.00	20.9
2	0	-0	837	0	0	0	1048	--	--	16.08	16.08	0.10	0.02	0.01	0.05	0.00	0.00	20.9
3	0	-0	882	0	0	0	1052	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9
4	0	-0	769	0	0	0	1035	--	--	16.08	16.08	0.10	0.02	0.01	0.05	0.00	0.00	20.9
5	0	-0	814	0	0	0	1039	--	--	16.08	16.08	0.10	0.02	0.01	0.05	0.00	0.00	20.9
6	0	-0	760	0	0	0	1039	--	--	16.08	16.08	0.10	0.02	0.01	0.05	0.00	0.00	20.9
7	0	-0	911	0	0	0	1052	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9
8	0	-0	740	0	0	0	1035	--	--	16.08	16.08	0.10	0.02	0.01	0.05	0.00	0.00	20.9
9	0	-0	891	0	0	0	1048	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9
10	0	-0	837	0	0	0	1048	--	--	16.08	16.08	0.10	0.02	0.01	0.05	0.00	0.00	20.9
11	0	-0	882	0	0	0	1052	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9
12	0	-0	769	0	0	0	1035	--	--	16.08	16.08	0.10	0.02	0.01	0.05	0.00	0.00	20.9
13	0	-0	814	0	0	0	1039	--	--	16.08	16.08	0.10	0.02	0.01	0.05	0.00	0.00	20.9
14	0	-0	760	0	0	0	1039	--	--	16.08	16.08	0.10	0.02	0.01	0.05	0.00	0.00	20.9
15	0	-0	911	0	0	0	1052	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9
16	0	-0	740	0	0	0	1035	--	--	16.08	16.08	0.10	0.02	0.01	0.05	0.00	0.00	20.9
17	0	-0	891	0	0	0	1048	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9
18	0	-0	1142	0	0	0	1895	--	--	16.08	16.08	0.00	0.03	0.01	0.07	0.00	0.00	20.9
19	0	-0	871	0	0	0	1815	--	--	16.08	16.08	0.00	0.03	0.01	0.05	0.00	0.00	20.9
20	0	-0	919	0	0	0	1866	--	--	16.08	16.08	0.00	0.03	0.01	0.06	0.00	0.00	20.9
37	0	-0	1201	0	0	0	1748	--	--	16.08	16.08	0.00	0.03	0.01	0.08	0.00	0.00	20.9
38	0	-0	750	0	0	0	1615	--	--	16.08	16.08	0.00	0.03	0.01	0.05	0.00	0.00	20.9
39	0	-0	829	0	0	0	1700	--	--	16.08	16.08	0.00	0.03	0.01	0.05	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	1073	0	0	0	2791	--	--	16.08	16.08	0.00	0.05	0.01	0.07	0.00	0.00	20.9
2	27	-0	837	0	0	0	2167	--	--	16.08	16.08	0.10	0.04	0.01	0.05	0.00	0.00	20.9
3	27	-0	882	0	0	0	2231	--	--	16.08	16.08	0.10	0.04	0.01	0.06	0.00	0.00	20.9
4	27	-0	769	0	0	0	2063	--	--	16.08	16.08	0.10	0.04	0.01	0.05	0.00	0.00	20.9
5	27	-0	814	0	0	0	2127	--	--	16.08	16.08	0.10	0.04	0.01	0.05	0.00	0.00	20.9
6	27	-0	760	0	0	0	2055	--	--	16.08	16.08	0.10	0.04	0.01	0.05	0.00	0.00	20.9
7	27	-0	911	0	0	0	2270	--	--	16.08	16.08	0.10	0.04	0.01	0.06	0.00	0.00	20.9
8	27	-0	740	0	0	0	2023	--	--	16.08	16.08	0.10	0.04	0.01	0.05	0.00	0.00	20.9
9	27	-0	891	0	0	0	2239	--	--	16.08	16.08	0.10	0.04	0.01	0.06	0.00	0.00	20.9
10	27	-0	837	0	0	0	2167	--	--	16.08	16.08	0.10	0.04	0.01	0.05	0.00	0.00	20.9
11	27	-0	882	0	0	0	2231	--	--	16.08	16.08	0.10	0.04	0.01	0.06	0.00	0.00	20.9
12	27	-0	769	0	0	0	2063	--	--	16.08	16.08	0.10	0.04	0.01	0.05	0.00	0.00	20.9
13	27	-0	814	0	0	0	2127	--	--	16.08	16.08	0.10	0.04	0.01	0.05	0.00	0.00	20.9
14	27	-0	760	0	0	0	2055	--	--	16.08	16.08	0.10	0.04	0.01	0.05	0.00	0.00	20.9
15	27	-0	911	0	0	0	2270	--	--	16.08	16.08	0.10	0.04	0.01	0.06	0.00	0.00	20.9
16	27	-0	740	0	0	0	2023	--	--	16.08	16.08	0.10	0.04	0.01	0.05	0.00	0.00	20.9
17	27	-0	891	0	0	0	2239	--	--	16.08	16.08	0.10	0.04	0.01	0.06	0.00	0.00	20.9
18	27	-0	1142	0	0	0	3422	--	--	16.08	16.08	0.00	0.06	0.01	0.07	0.00	0.00	20.9
19	27	-0	871	0	0	0	2980	--	--	16.08	16.08	0.00	0.05	0.01	0.05	0.00	0.00	20.9
20	27	-0	919	0	0	0	3094	--	--	16.08	16.08	0.00	0.05	0.01	0.06	0.00	0.00	20.9
37	27	-0	1201	0	0	0	3353	--	--	16.08	16.08	0.00	0.06	0.01	0.08	0.00	0.00	20.9
38	27	-0	750	0	0	0	2617	--	--	16.08	16.08	0.00	0.04	0.01	0.05	0.00	0.00	20.9
39	27	-0	829	0	0	0	2808	--	--	16.08	16.08	0.00	0.05	0.01	0.05	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	54	-0	1073	0	0	0	1932	--	--	16.08	16.08	0.00	0.03	0.01	0.07	0.00	0.00	20.9
2	54	-0	837	0	0	0	1497	--	--	16.08	16.08	0.10	0.03	0.01	0.05	0.00	0.00	20.9
3	54	-0	882	0	0	0	1525	--	--	16.08	16.08	0.10	0.03	0.01	0.06	0.00	0.00	20.9
4	54	-0	769	0	0	0	1447	--	--	16.08	16.08	0.10	0.03	0.01	0.05	0.00	0.00	20.9
5	54	-0	814	0	0	0	1475	--	--	16.08	16.08	0.10	0.03	0.01	0.05	0.00	0.00	20.9
6	54	-0	760	0	0	0	1446	--	--	16.08	16.08	0.10	0.03	0.01	0.05	0.00	0.00	20.9
7	54	-0	911	0	0	0	1540	--	--	16.08	16.08	0.10	0.03	0.01	0.06	0.00	0.00	20.9
8	54	-0	740	0	0	0	1431	--	--	16.08	16.08	0.10	0.03	0.01	0.05	0.00	0.00	20.9
9	54	-0	891	0	0	0	1526	--	--	16.08	16.08	0.10	0.03	0.01	0.06	0.00	0.00	20.9
10	54	-0	837	0	0	0	1497	--	--	16.08	16.08	0.10	0.03	0.01	0.05	0.00	0.00	20.9
11	54	-0	882	0	0	0	1525	--	--	16.08	16.08	0.10	0.03	0.01	0.06	0.00	0.00	20.9
12	54	-0	769	0	0	0	1447	--	--	16.08	16.08	0.10	0.03	0.01	0.05	0.00	0.00	20.9
13	54	-0	814	0	0	0	1475	--	--	16.08	16.08	0.10	0.03	0.01	0.05	0.00	0.00	20.9
14	54	-0	760	0	0	0	1446	--	--	16.08	16.08	0.10	0.03	0.01	0.05	0.00	0.00	20.9
15	54	-0	911	0	0	0	1540	--	--	16.08	16.08	0.10	0.03	0.01	0.06	0.00	0.00	20.9
16	54	-0	740	0	0	0	1431	--	--	16.08	16.08	0.10	0.03	0.01	0.05	0.00	0.00	20.9
17	54	-0	891	0	0	0	1526	--	--	16.08	16.08	0.10	0.03	0.01	0.06	0.00	0.00	20.9
18	54	-0	1142	0	0	0	2507	--	--	16.08	16.08	0.00	0.04	0.01	0.07	0.00	0.00	20.9
19	54	-0	871	0	0	0	2282	--	--	16.08	16.08	0.00	0.04	0.01	0.05	0.00	0.00	20.9
20	54	-0	919	0	0	0	2358	--	--	16.08	16.08	0.00	0.04	0.01	0.06	0.00	0.00	20.9
37	54	-0	1201	0	0	0	2391	--	--	16.08	16.08	0.00	0.04	0.01	0.08	0.00	0.00	20.9
38	54	-0	750	0	0	0	2017	--	--	16.08	16.08	0.00	0.03	0.01	0.05	0.00	0.00	20.9
39	54	-0	829	0	0	0	2144	--	--	16.08	16.08	0.00	0.04	0.01	0.05	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 117 NI 1963 NF 1972 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice resistenza			aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-1070	0	0	0	1930	--	--	16.08	16.08	0.00	0.03	0.01	0.07	0.00	0.00	20.9
2	0	-0	-803	0	0	0	1478	--	--	16.08	16.08	0.10	0.03	0.01	0.05	0.00	0.00	20.9
3	0	-0	-755	0	0	0	1456	--	--	16.08	16.08	0.10	0.03	0.01	0.05	0.00	0.00	20.9
4	0	-0	-891	0	0	0	1512	--	--	16.08	16.08	0.10	0.03	0.01	0.06	0.00	0.00	20.9
5	0	-0	-843	0	0	0	1490	--	--	16.08	16.08	0.10	0.03	0.01	0.05	0.00	0.00	20.9
6	0	-0	-890	0	0	0	1516	--	--	16.08	16.08	0.10	0.03	0.01	0.06	0.00	0.00	20.9
7	0	-0	-729	0	0	0	1443	--	--	16.08	16.08	0.10	0.03	0.01	0.05	0.00	0.00	20.9
8	0	-0	-916	0	0	0	1526	--	--	16.08	16.08	0.10	0.03	0.01	0.06	0.00	0.00	20.9
9	0	-0	-756	0	0	0	1453	--	--	16.08	16.08	0.10	0.03	0.01	0.05	0.00	0.00	20.9
10	0	-0	-803	0	0	0	1478	--	--	16.08	16.08	0.10	0.03	0.01	0.05	0.00	0.00	20.9
11	0	-0	-755	0	0	0	1456	--	--	16.08	16.08	0.10	0.03	0.01	0.05	0.00	0.00	20.9
12	0	-0	-891	0	0	0	1512	--	--	16.08	16.08	0.10	0.03	0.01	0.06	0.00	0.00	20.9
13	0	-0	-843	0	0	0	1490	--	--	16.08	16.08	0.10	0.03	0.01	0.05	0.00	0.00	20.9
14	0	-0	-890	0	0	0	1516	--	--	16.08	16.08	0.10	0.03	0.01	0.06	0.00	0.00	20.9
15	0	-0	-729	0	0	0	1443	--	--	16.08	16.08	0.10	0.03	0.01	0.05	0.00	0.00	20.9
16	0	-0	-916	0	0	0	1526	--	--	16.08	16.08	0.10	0.03	0.01	0.06	0.00	0.00	20.9
17	0	-0	-756	0	0	0	1453	--	--	16.08	16.08	0.10	0.03	0.01	0.05	0.00	0.00	20.9
18	0	-0	-1171	0	0	0	2522	--	--	16.08	16.08	0.00	0.04	0.01	0.07	0.00	0.00	20.9
19	0	-0	-1527	0	0	0	2633	--	--	16.08	16.08	0.00	0.04	0.01	0.10	0.00	0.00	20.9
20	0	-0	-1416	0	0	0	2624	--	--	16.08	16.08	0.00	0.04	0.01	0.09	0.00	0.00	20.9
37	0	-0	-994	0	0	0	2280	--	--	16.08	16.08	0.00	0.04	0.01	0.06	0.00	0.00	20.9
38	0	-0	-1587	0	0	0	2465	--	--	16.08	16.08	0.00	0.04	0.01	0.10	0.00	0.00	20.9
39	0	-0	-1402	0	0	0	2451	--	--	16.08	16.08	0.00	0.04	0.01	0.09	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-1070	0	0	0	1930	--	--	16.08	16.08	0.00	0.03	0.01	0.07	0.00	0.00	20.9
2	27	-0	-803	0	0	0	1478	--	--	16.08	16.08	0.10	0.03	0.01	0.05	0.00	0.00	20.9
3	27	-0	-755	0	0	0	1456	--	--	16.08	16.08	0.10	0.03	0.01	0.05	0.00	0.00	20.9
4	27	-0	-891	0	0	0	1512	--	--	16.08	16.08	0.10	0.03	0.01	0.06	0.00	0.00	20.9
5	27	-0	-843	0	0	0	1490	--	--	16.08	16.08	0.10	0.03	0.01	0.05	0.00	0.00	20.9
6	27	-0	-890	0	0	0	1516	--	--	16.08	16.08	0.10	0.03	0.01	0.06	0.00	0.00	20.9
7	27	-0	-729	0	0	0	1443	--	--	16.08	16.08	0.10	0.03	0.01	0.05	0.00	0.00	20.9
8	27	-0	-916	0	0	0	1526	--	--	16.08	16.08	0.10	0.03	0.01	0.06	0.00	0.00	20.9
9	27	-0	-756	0	0	0	1453	--	--	16.08	16.08	0.10	0.03	0.01	0.05	0.00	0.00	20.9
10	27	-0	-803	0	0	0	1478	--	--	16.08	16.08	0.10	0.03	0.01	0.05	0.00	0.00	20.9
11	27	-0	-755	0	0	0	1456	--	--	16.08	16.08	0.10	0.03	0.01	0.05	0.00	0.00	20.9
12	27	-0	-891	0	0	0	1512	--	--	16.08	16.08	0.10	0.03	0.01	0.06	0.00	0.00	20.9
13	27	-0	-843	0	0	0	1490	--	--	16.08	16.08	0.10	0.03	0.01	0.05	0.00	0.00	20.9
14	27	-0	-890	0	0	0	1516	--	--	16.08	16.08	0.10	0.03	0.01	0.06	0.00	0.00	20.9
15	27	-0	-729	0	0	0	1443	--	--	16.08	16.08	0.10	0.03	0.01	0.05	0.00	0.00	20.9
16	27	-0	-916	0	0	0	1526	--	--	16.08	16.08	0.10	0.03	0.01	0.06	0.00	0.00	20.9
17	27	-0	-756	0	0	0	1453	--	--	16.08	16.08	0.10	0.03	0.01	0.05	0.00	0.00	20.9
18	27	-0	-1171	0	0	0	2522	--	--	16.08	16.08	0.00	0.04	0.01	0.07	0.00	0.00	20.9
19	27	-0	-1527	0	0	0	2633	--	--	16.08	16.08	0.00	0.04	0.01	0.10	0.00	0.00	20.9
20	27	-0	-1416	0	0	0	2624	--	--	16.08	16.08	0.00	0.04	0.01	0.09	0.00	0.00	20.9
37	27	-0	-994	0	0	0	2280	--	--	16.08	16.08	0.00	0.04	0.01	0.06	0.00	0.00	20.9
38	27	-0	-1587	0	0	0	2465	--	--	16.08	16.08	0.00	0.04	0.01	0.10	0.00	0.00	20.9
39	27	-0	-1402	0	0	0	2451	--	--	16.08	16.08	0.00	0.04	0.01	0.09	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	54	-0	-1070	0	0	0	1357	--	--	16.08	16.08	0.00	0.02	0.01	0.07	0.00	0.00	20.9
2	54	-0	-803	0	0	0	1048	--	--	16.08	16.08	0.10	0.02	0.01	0.05	0.00	0.00	20.9
3	54	-0	-755	0	0	0	1052	--	--	16.08	16.08	0.10	0.02	0.01	0.05	0.00	0.00	20.9
4	54	-0	-891	0	0	0	1035	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9
5	54	-0	-843	0	0	0	1039	--	--	16.08	16.08	0.10	0.02	0.01	0.05	0.00	0.00	20.9
6	54	-0	-890	0	0	0	1039	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9
7	54	-0	-729	0	0	0	1052	--	--	16.08	16.08	0.10	0.02	0.01	0.05	0.00	0.00	20.9
8	54	-0	-916	0	0	0	1035	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9
9	54	-0	-756	0	0	0	1048	--	--	16.08	16.08	0.10	0.02	0.01	0.05	0.00	0.00	20.9
10	54	-0	-803	0	0	0	1048	--	--	16.08	16.08	0.10	0.02	0.01	0.05	0.00	0.00	20.9
11	54	-0	-755	0	0	0	1052	--	--	16.08	16.08	0.10	0.02	0.01	0.05	0.00	0.00	20.9
12	54	-0	-891	0	0	0	1035	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9
13	54	-0	-843	0	0	0	1039	--	--	16.08	16.08	0.10	0.02	0.01	0.05	0.00	0.00	20.9
14	54	-0	-890	0	0	0	1039	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9
15	54	-0	-729	0	0	0	1052	--	--	16.08	16.08	0.10	0.02	0.01	0.05	0.00	0.00	20.9
16	54	-0	-916	0	0	0	1035	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9
17	54	-0	-756	0	0	0	1048	--	--	16.08	16.08	0.10	0.02	0.01	0.05	0.00	0.00	20.9
18	54	-0	-1171	0	0	0	1895	--	--	16.08	16.08	0.00	0.03	0.01	0.07	0.00	0.00	20.9
19	54	-0	-1527	0	0	0	1815	--	--	16.08	16.08	0.00	0.03	0.01	0.10	0.00	0.00	20.9
20	54	-0	-1416	0	0	0	1866	--	--	16.08	16.08	0.00	0.03	0.01	0.09	0.00	0.00	20.9
37	54	-0	-994	0	0	0	1748	--	--	16.08	16.08	0.00	0.03	0.01	0.06	0.00	0.00	20.9
38	54	-0	-1587	0	0	0	1615	--	--	16.08	16.08	0.00	0.03	0.01	0.10	0.00	0.00	20.9
39	54	-0	-1402	0	0	0	1700	--	--	16.08	16.08	0.00	0.03	0.01	0.09	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 118 NI 1964 NF 1963 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice resistenza			aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-3161	0	0	0	3623	--	--	16.08	16.08	0.00	0.06	0.03	0.20	0.00	0.00	20.9
2	0	-0	-2400	0	0	0	2764	--	--	16.08	16.08	0.10	0.05	0.02	0.15	0.00	0.00	20.9
3	0	-0	-2350	0	0	0	2715	--	--	16.08	16.08	0.10	0.05	0.02	0.15	0.00	0.00	20.9
4	0	-0	-2513	0	0	0	2858	--	--	16.08	16.08	0.10	0.05	0.02	0.16	0.00	0.00	20.9
5	0	-0	-2462	0	0	0	2809	--	--	16.08	16.08	0.10	0.05	0.02	0.15	0.00	0.00	20.9
6	0	-0	-2499	0	0	0	2854	--	--	16.08	16.08	0.10	0.05	0.02	0.16	0.00	0.00	20.9
7	0	-0	-2330	0	0	0	2691	--	--	16.08	16.08	0.10	0.05	0.02	0.15	0.00	0.00	20.9
8	0	-0	-2532	0	0	0	2882	--	--	16.08	16.08	0.10	0.05	0.02	0.16	0.00	0.00	20.9
9	0	-0	-2364	0	0	0	2719	--	--	16.08	16.08	0.10	0.05	0.02	0.15	0.00	0.00	20.9
10	0	-0	-2400	0	0	0	2764	--	--	16.08	16.08	0.10	0.05	0.02	0.15	0.00	0.00	20.9
11	0	-0	-2350	0	0	0	2715	--	--	16.08	16.08	0.10	0.05	0.02	0.15	0.00	0.00	20.9
12	0	-0	-2513	0	0	0	2858	--	--	16.08	16.08	0.10	0.05	0.02	0.16	0.00	0.00	20.9
13	0	-0	-2462	0	0	0	2809	--	--	16.08	16.08	0.10	0.05	0.02	0.15	0.00	0.00	20.9
14	0	-0	-2499	0	0	0	2854	--	--	16.08	16.08	0.10	0.05	0.02	0.16	0.00	0.00	20.9
15	0	-0	-2330	0	0	0	2691	--	--	16.08	16.08	0.10	0.05	0.02	0.15	0.00	0.00	20.9
16	0	-0	-2532	0	0	0	2882	--	--	16.08	16.08	0.10	0.05	0.02	0.16	0.00	0.00	20.9

17	0	-0	-2364	0	0	0	2719	--	--	16.08	16.08	0.10	0.05	0.02	0.15	0.00	0.00	20.9
18	0	-0	-3419	0	0	0	4354	--	--	16.08	16.08	0.00	0.07	0.03	0.21	0.00	0.00	20.9
19	0	-0	-3876	0	0	0	4709	--	--	16.08	16.08	0.00	0.08	0.03	0.24	0.00	0.00	20.9
20	0	-0	-3693	0	0	0	4603	--	--	16.08	16.08	0.00	0.08	0.03	0.23	0.00	0.00	20.9
37	0	-0	-3122	0	0	0	3953	--	--	16.08	16.08	0.00	0.07	0.03	0.20	0.00	0.00	20.9
38	0	-0	-3884	0	0	0	4546	--	--	16.08	16.08	0.00	0.08	0.03	0.24	0.00	0.00	20.9
39	0	-0	-3579	0	0	0	4368	--	--	16.08	16.08	0.00	0.07	0.03	0.22	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-3161	0	0	0	3623	--	--	16.08	16.08	0.00	0.06	0.03	0.20	0.00	0.00	20.9
2	27	-0	-2400	0	0	0	2764	--	--	16.08	16.08	0.10	0.05	0.02	0.15	0.00	0.00	20.9
3	27	-0	-2350	0	0	0	2715	--	--	16.08	16.08	0.10	0.05	0.02	0.15	0.00	0.00	20.9
4	27	-0	-2513	0	0	0	2858	--	--	16.08	16.08	0.10	0.05	0.02	0.16	0.00	0.00	20.9
5	27	-0	-2462	0	0	0	2809	--	--	16.08	16.08	0.10	0.05	0.02	0.15	0.00	0.00	20.9
6	27	-0	-2499	0	0	0	2854	--	--	16.08	16.08	0.10	0.05	0.02	0.16	0.00	0.00	20.9
7	27	-0	-2330	0	0	0	2691	--	--	16.08	16.08	0.10	0.05	0.02	0.15	0.00	0.00	20.9
8	27	-0	-2532	0	0	0	2882	--	--	16.08	16.08	0.10	0.05	0.02	0.16	0.00	0.00	20.9
9	27	-0	-2364	0	0	0	2719	--	--	16.08	16.08	0.10	0.05	0.02	0.15	0.00	0.00	20.9
10	27	-0	-2400	0	0	0	2764	--	--	16.08	16.08	0.10	0.05	0.02	0.15	0.00	0.00	20.9
11	27	-0	-2350	0	0	0	2715	--	--	16.08	16.08	0.10	0.05	0.02	0.15	0.00	0.00	20.9
12	27	-0	-2513	0	0	0	2858	--	--	16.08	16.08	0.10	0.05	0.02	0.16	0.00	0.00	20.9
13	27	-0	-2462	0	0	0	2809	--	--	16.08	16.08	0.10	0.05	0.02	0.15	0.00	0.00	20.9
14	27	-0	-2499	0	0	0	2854	--	--	16.08	16.08	0.10	0.05	0.02	0.16	0.00	0.00	20.9
15	27	-0	-2330	0	0	0	2691	--	--	16.08	16.08	0.10	0.05	0.02	0.15	0.00	0.00	20.9
16	27	-0	-2532	0	0	0	2882	--	--	16.08	16.08	0.10	0.05	0.02	0.16	0.00	0.00	20.9
17	27	-0	-2364	0	0	0	2719	--	--	16.08	16.08	0.10	0.05	0.02	0.15	0.00	0.00	20.9
18	27	-0	-3419	0	0	0	4354	--	--	16.08	16.08	0.00	0.07	0.03	0.21	0.00	0.00	20.9
19	27	-0	-3876	0	0	0	4709	--	--	16.08	16.08	0.00	0.08	0.03	0.24	0.00	0.00	20.9
20	27	-0	-3693	0	0	0	4603	--	--	16.08	16.08	0.00	0.08	0.03	0.23	0.00	0.00	20.9
37	27	-0	-3122	0	0	0	3953	--	--	16.08	16.08	0.00	0.07	0.03	0.20	0.00	0.00	20.9
38	27	-0	-3884	0	0	0	4546	--	--	16.08	16.08	0.00	0.08	0.03	0.24	0.00	0.00	20.9
39	27	-0	-3579	0	0	0	4368	--	--	16.08	16.08	0.00	0.07	0.03	0.22	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	54	-0	-3161	0	0	0	1930	--	--	16.08	16.08	0.00	0.03	0.03	0.20	0.00	0.00	20.9
2	54	-0	-2400	0	0	0	1478	--	--	16.08	16.08	0.10	0.03	0.02	0.15	0.00	0.00	20.9
3	54	-0	-2350	0	0	0	1456	--	--	16.08	16.08	0.10	0.03	0.02	0.15	0.00	0.00	20.9
4	54	-0	-2513	0	0	0	1512	--	--	16.08	16.08	0.10	0.03	0.02	0.16	0.00	0.00	20.9
5	54	-0	-2462	0	0	0	1490	--	--	16.08	16.08	0.10	0.03	0.02	0.15	0.00	0.00	20.9
6	54	-0	-2499	0	0	0	1516	--	--	16.08	16.08	0.10	0.03	0.02	0.16	0.00	0.00	20.9
7	54	-0	-2330	0	0	0	1443	--	--	16.08	16.08	0.10	0.03	0.02	0.15	0.00	0.00	20.9
8	54	-0	-2532	0	0	0	1526	--	--	16.08	16.08	0.10	0.03	0.02	0.16	0.00	0.00	20.9
9	54	-0	-2364	0	0	0	1453	--	--	16.08	16.08	0.10	0.03	0.02	0.15	0.00	0.00	20.9
10	54	-0	-2400	0	0	0	1478	--	--	16.08	16.08	0.10	0.03	0.02	0.15	0.00	0.00	20.9
11	54	-0	-2350	0	0	0	1456	--	--	16.08	16.08	0.10	0.03	0.02	0.15	0.00	0.00	20.9
12	54	-0	-2513	0	0	0	1512	--	--	16.08	16.08	0.10	0.03	0.02	0.16	0.00	0.00	20.9
13	54	-0	-2462	0	0	0	1490	--	--	16.08	16.08	0.10	0.03	0.02	0.15	0.00	0.00	20.9
14	54	-0	-2499	0	0	0	1516	--	--	16.08	16.08	0.10	0.03	0.02	0.16	0.00	0.00	20.9
15	54	-0	-2330	0	0	0	1443	--	--	16.08	16.08	0.10	0.03	0.02	0.15	0.00	0.00	20.9
16	54	-0	-2532	0	0	0	1526	--	--	16.08	16.08	0.10	0.03	0.02	0.16	0.00	0.00	20.9
17	54	-0	-2364	0	0	0	1453	--	--	16.08	16.08	0.10	0.03	0.02	0.15	0.00	0.00	20.9
18	54	-0	-3419	0	0	0	2522	--	--	16.08	16.08	0.00	0.04	0.03	0.21	0.00	0.00	20.9
19	54	-0	-3876	0	0	0	2633	--	--	16.08	16.08	0.00	0.04	0.03	0.24	0.00	0.00	20.9
20	54	-0	-3693	0	0	0	2624	--	--	16.08	16.08	0.00	0.04	0.03	0.23	0.00	0.00	20.9
37	54	-0	-3122	0	0	0	2280	--	--	16.08	16.08	0.00	0.04	0.03	0.20	0.00	0.00	20.9
38	54	-0	-3884	0	0	0	2465	--	--	16.08	16.08	0.00	0.04	0.03	0.24	0.00	0.00	20.9
39	54	-0	-3579	0	0	0	2451	--	--	16.08	16.08	0.00	0.04	0.03	0.22	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 119 NI 1843 NF 1964 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-5195	0	0	0	6406	--	--	16.08	16.08	0.00	0.11	0.04	0.33	0.00	0.00	20.9
2	0	-0	-3952	0	0	0	4881	--	--	16.08	16.08	0.10	0.09	0.03	0.25	0.00	0.00	20.9
3	0	-0	-3900	0	0	0	4805	--	--	16.08	16.08	0.10	0.09	0.03	0.24	0.00	0.00	20.9
4	0	-0	-4092	0	0	0	5050	--	--	16.08	16.08	0.10	0.09	0.03	0.26	0.00	0.00	20.9
5	0	-0	-4039	0	0	0	4973	--	--	16.08	16.08	0.10	0.09	0.03	0.25	0.00	0.00	20.9
6	0	-0	-4062	0	0	0	5030	--	--	16.08	16.08	0.10	0.09	0.03	0.25	0.00	0.00	20.9
7	0	-0	-3888	0	0	0	4774	--	--	16.08	16.08	0.10	0.08	0.03	0.24	0.00	0.00	20.9
8	0	-0	-4104	0	0	0	5081	--	--	16.08	16.08	0.10	0.09	0.03	0.26	0.00	0.00	20.9
9	0	-0	-3929	0	0	0	4824	--	--	16.08	16.08	0.10	0.09	0.03	0.25	0.00	0.00	20.9
10	0	-0	-3952	0	0	0	4881	--	--	16.08	16.08	0.10	0.09	0.03	0.25	0.00	0.00	20.9
11	0	-0	-3900	0	0	0	4805	--	--	16.08	16.08	0.10	0.09	0.03	0.24	0.00	0.00	20.9
12	0	-0	-4092	0	0	0	5050	--	--	16.08	16.08	0.10	0.09	0.03	0.26	0.00	0.00	20.9
13	0	-0	-4039	0	0	0	4973	--	--	16.08	16.08	0.10	0.09	0.03	0.25	0.00	0.00	20.9
14	0	-0	-4062	0	0	0	5030	--	--	16.08	16.08	0.10	0.09	0.03	0.25	0.00	0.00	20.9
15	0	-0	-3888	0	0	0	4774	--	--	16.08	16.08	0.10	0.08	0.03	0.24	0.00	0.00	20.9
16	0	-0	-4104	0	0	0	5081	--	--	16.08	16.08	0.10	0.09	0.03	0.26	0.00	0.00	20.9
17	0	-0	-3929	0	0	0	4824	--	--	16.08	16.08	0.10	0.09	0.03	0.25	0.00	0.00	20.9
18	0	-0	-5595	0	0	0	7351	--	--	16.08	16.08	0.00	0.13	0.05	0.35	0.00	0.00	20.9
19	0	-0	-6168	0	0	0	8014	--	--	16.08	16.08	0.00	0.14	0.05	0.39	0.00	0.00	20.9
20	0	-0	-5906	0	0	0	7767	--	--	16.08	16.08	0.00	0.13	0.05	0.37	0.00	0.00	20.9
37	0	-0	-5177	0	0	0	6726	--	--	16.08	16.08	0.00	0.11	0.04	0.32	0.00	0.00	20.9
38	0	-0	-6132	0	0	0	7831	--	--	16.08	16.08	0.00	0.13	0.05	0.38	0.00	0.00	20.9
39	0	-0	-5695	0	0	0	7419	--	--	16.08	16.08	0.00	0.13	0.05	0.36	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-5195	0	0	0	6406	--	--	16.08	16.08	0.00	0.11	0.04	0.33	0.00	0.00	20.9
2	27	-0	-3952	0	0	0	4881	--	--	16.08	16.08	0.10	0.09	0.03	0.25	0.00	0.00	20.9
3	27	-0	-3900	0	0	0	4805	--	--	16.08	16.08	0.10	0.09	0.03	0.24	0.00	0.00	20.9
4	27	-0	-4092	0	0	0	5050	--	--	16.08	16.08	0.10	0.09	0.03	0.26	0.00	0.00	20.9
5	27	-0	-4039	0	0	0	4973	--	--	16.08	16.08	0.10	0.09	0.03	0.25	0.00	0.00	20.9
6	27	-0	-4062	0	0	0	5030	--	--	16.08	16.08	0.10	0.09	0.03	0.25	0.00	0.00	20.9
7	27	-0	-3888	0	0	0	4774	--	--	16.08	16.08	0.10	0.08	0.03	0.24	0.00	0.00	20.9
8	27	-0	-4104	0	0	0	5081	--	--	16.08	16.08	0.10	0.09	0.03	0.26	0.00	0.00	20.9
9	27	-0	-3929	0	0	0	4824	--	--	16.08	16.08	0.10	0.09	0.03	0.25	0.00	0.00	20.9
10	27	-0	-3952	0	0	0	4881	--	--	16.08	16.08	0.10	0.09	0.03	0.25	0.00	0.00	20.9
11	27	-0	-3900	0	0	0	4805	--	--	16.08	16.08	0.10	0.09	0.03	0.24	0.00	0.00	20.9
12	27	-0	-4092	0	0	0	5050	--	--	16.08	16.08	0.10	0.09	0.03	0.26	0.00	0.00	20.9

13	27	-0	-4039	0	0	0	4973	--	--	16.08	16.08	0.10	0.09	0.03	0.25	0.00	0.00	20.9
14	27	-0	-4062	0	0	0	5030	--	--	16.08	16.08	0.10	0.09	0.03	0.25	0.00	0.00	20.9
15	27	-0	-3888	0	0	0	4774	--	--	16.08	16.08	0.10	0.08	0.03	0.24	0.00	0.00	20.9
16	27	-0	-4104	0	0	0	5081	--	--	16.08	16.08	0.10	0.09	0.03	0.26	0.00	0.00	20.9
17	27	-0	-3929	0	0	0	4824	--	--	16.08	16.08	0.10	0.09	0.03	0.25	0.00	0.00	20.9
18	27	-0	-5595	0	0	0	7351	--	--	16.08	16.08	0.00	0.13	0.05	0.35	0.00	0.00	20.9
19	27	-0	-6168	0	0	0	8014	--	--	16.08	16.08	0.00	0.14	0.05	0.39	0.00	0.00	20.9
20	27	-0	-5906	0	0	0	7767	--	--	16.08	16.08	0.00	0.13	0.05	0.37	0.00	0.00	20.9
37	27	-0	-5177	0	0	0	6726	--	--	16.08	16.08	0.00	0.11	0.04	0.32	0.00	0.00	20.9
38	27	-0	-6132	0	0	0	7831	--	--	16.08	16.08	0.00	0.13	0.05	0.38	0.00	0.00	20.9
39	27	-0	-5695	0	0	0	7419	--	--	16.08	16.08	0.00	0.13	0.05	0.36	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	54	-0	-5195	0	0	0	3623	--	--	16.08	16.08	0.00	0.06	0.04	0.33	0.00	0.00	20.9
2	54	-0	-3952	0	0	0	2764	--	--	16.08	16.08	0.10	0.05	0.03	0.25	0.00	0.00	20.9
3	54	-0	-3900	0	0	0	2715	--	--	16.08	16.08	0.10	0.05	0.03	0.24	0.00	0.00	20.9
4	54	-0	-4092	0	0	0	2858	--	--	16.08	16.08	0.10	0.05	0.03	0.26	0.00	0.00	20.9
5	54	-0	-4039	0	0	0	2809	--	--	16.08	16.08	0.10	0.05	0.03	0.25	0.00	0.00	20.9
6	54	-0	-4062	0	0	0	2854	--	--	16.08	16.08	0.10	0.05	0.03	0.25	0.00	0.00	20.9
7	54	-0	-3888	0	0	0	2691	--	--	16.08	16.08	0.10	0.05	0.03	0.24	0.00	0.00	20.9
8	54	-0	-4104	0	0	0	2882	--	--	16.08	16.08	0.10	0.05	0.03	0.26	0.00	0.00	20.9
9	54	-0	-3929	0	0	0	2719	--	--	16.08	16.08	0.10	0.05	0.03	0.25	0.00	0.00	20.9
10	54	-0	-3952	0	0	0	2764	--	--	16.08	16.08	0.10	0.05	0.03	0.25	0.00	0.00	20.9
11	54	-0	-3900	0	0	0	2715	--	--	16.08	16.08	0.10	0.05	0.03	0.24	0.00	0.00	20.9
12	54	-0	-4092	0	0	0	2858	--	--	16.08	16.08	0.10	0.05	0.03	0.26	0.00	0.00	20.9
13	54	-0	-4039	0	0	0	2809	--	--	16.08	16.08	0.10	0.05	0.03	0.25	0.00	0.00	20.9
14	54	-0	-4062	0	0	0	2854	--	--	16.08	16.08	0.10	0.05	0.03	0.25	0.00	0.00	20.9
15	54	-0	-3888	0	0	0	2691	--	--	16.08	16.08	0.10	0.05	0.03	0.24	0.00	0.00	20.9
16	54	-0	-4104	0	0	0	2882	--	--	16.08	16.08	0.10	0.05	0.03	0.26	0.00	0.00	20.9
17	54	-0	-3929	0	0	0	2719	--	--	16.08	16.08	0.10	0.05	0.03	0.25	0.00	0.00	20.9
18	54	-0	-5595	0	0	0	4354	--	--	16.08	16.08	0.00	0.07	0.05	0.35	0.00	0.00	20.9
19	54	-0	-6168	0	0	0	4709	--	--	16.08	16.08	0.00	0.08	0.05	0.39	0.00	0.00	20.9
20	54	-0	-5906	0	0	0	4603	--	--	16.08	16.08	0.00	0.08	0.05	0.37	0.00	0.00	20.9
37	54	-0	-5177	0	0	0	3953	--	--	16.08	16.08	0.00	0.07	0.04	0.32	0.00	0.00	20.9
38	54	-0	-6132	0	0	0	4546	--	--	16.08	16.08	0.00	0.08	0.05	0.38	0.00	0.00	20.9
39	54	-0	-5695	0	0	0	4368	--	--	16.08	16.08	0.00	0.07	0.05	0.36	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 120 NI 1976 NF 1843 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	7577	0	0	0	5045	--	--	16.08	16.08	0.00	0.09	0.06	0.48	0.00	0.00	20.9
2	0	-0	5786	0	0	0	3926	--	--	16.08	16.08	0.10	0.07	0.05	0.36	0.00	0.00	20.9
3	0	-0	5802	0	0	0	3853	--	--	16.08	16.08	0.10	0.07	0.05	0.36	0.00	0.00	20.9
4	0	-0	5855	0	0	0	3908	--	--	16.08	16.08	0.10	0.07	0.05	0.37	0.00	0.00	20.9
5	0	-0	5871	0	0	0	3836	--	--	16.08	16.08	0.10	0.07	0.05	0.37	0.00	0.00	20.9
6	0	-0	5790	0	0	0	4005	--	--	16.08	16.08	0.10	0.07	0.05	0.36	0.00	0.00	20.9
7	0	-0	5846	0	0	0	3762	--	--	16.08	16.08	0.10	0.07	0.05	0.37	0.00	0.00	20.9
8	0	-0	5811	0	0	0	3999	--	--	16.08	16.08	0.10	0.07	0.05	0.36	0.00	0.00	20.9
9	0	-0	5867	0	0	0	3757	--	--	16.08	16.08	0.10	0.07	0.05	0.37	0.00	0.00	20.9
10	0	-0	5786	0	0	0	3926	--	--	16.08	16.08	0.10	0.07	0.05	0.36	0.00	0.00	20.9
11	0	-0	5802	0	0	0	3853	--	--	16.08	16.08	0.10	0.07	0.05	0.36	0.00	0.00	20.9
12	0	-0	5855	0	0	0	3908	--	--	16.08	16.08	0.10	0.07	0.05	0.37	0.00	0.00	20.9
13	0	-0	5871	0	0	0	3836	--	--	16.08	16.08	0.10	0.07	0.05	0.37	0.00	0.00	20.9
14	0	-0	5790	0	0	0	4005	--	--	16.08	16.08	0.10	0.07	0.05	0.36	0.00	0.00	20.9
15	0	-0	5846	0	0	0	3762	--	--	16.08	16.08	0.10	0.07	0.05	0.37	0.00	0.00	20.9
16	0	-0	5811	0	0	0	3999	--	--	16.08	16.08	0.10	0.07	0.05	0.36	0.00	0.00	20.9
17	0	-0	5867	0	0	0	3757	--	--	16.08	16.08	0.10	0.07	0.05	0.37	0.00	0.00	20.9
18	0	-0	8528	0	0	0	6522	--	--	16.08	16.08	0.00	0.11	0.07	0.53	0.00	0.00	20.9
19	0	-0	8846	0	0	0	6459	--	--	16.08	16.08	0.00	0.11	0.07	0.55	0.00	0.00	20.9
20	0	-0	8410	0	0	0	6084	--	--	16.08	16.08	0.00	0.10	0.07	0.53	0.00	0.00	20.9
37	0	-0	8017	0	0	0	6074	--	--	16.08	16.08	0.00	0.10	0.07	0.50	0.00	0.00	20.9
38	0	-0	8547	0	0	0	5970	--	--	16.08	16.08	0.00	0.10	0.07	0.54	0.00	0.00	20.9
39	0	-0	7820	0	0	0	5344	--	--	16.08	16.08	0.00	0.09	0.06	0.49	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	7577	0	0	0	15100	--	--	16.08	16.08	0.00	0.26	0.06	0.48	0.00	0.00	20.9
2	26	-0	5786	0	0	0	11604	--	--	16.08	16.08	0.10	0.21	0.05	0.36	0.00	0.00	20.9
3	26	-0	5802	0	0	0	11553	--	--	16.08	16.08	0.10	0.21	0.05	0.36	0.00	0.00	20.9
4	26	-0	5855	0	0	0	11678	--	--	16.08	16.08	0.10	0.21	0.05	0.37	0.00	0.00	20.9
5	26	-0	5871	0	0	0	11627	--	--	16.08	16.08	0.10	0.21	0.05	0.37	0.00	0.00	20.9
6	26	-0	5790	0	0	0	11689	--	--	16.08	16.08	0.10	0.21	0.05	0.36	0.00	0.00	20.9
7	26	-0	5846	0	0	0	11520	--	--	16.08	16.08	0.10	0.20	0.05	0.37	0.00	0.00	20.9
8	26	-0	5811	0	0	0	11711	--	--	16.08	16.08	0.10	0.21	0.05	0.36	0.00	0.00	20.9
9	26	-0	5867	0	0	0	11543	--	--	16.08	16.08	0.10	0.20	0.05	0.37	0.00	0.00	20.9
10	26	-0	5786	0	0	0	11604	--	--	16.08	16.08	0.10	0.21	0.05	0.36	0.00	0.00	20.9
11	26	-0	5802	0	0	0	11553	--	--	16.08	16.08	0.10	0.21	0.05	0.36	0.00	0.00	20.9
12	26	-0	5855	0	0	0	11678	--	--	16.08	16.08	0.10	0.21	0.05	0.37	0.00	0.00	20.9
13	26	-0	5871	0	0	0	11627	--	--	16.08	16.08	0.10	0.21	0.05	0.37	0.00	0.00	20.9
14	26	-0	5790	0	0	0	11689	--	--	16.08	16.08	0.10	0.21	0.05	0.36	0.00	0.00	20.9
15	26	-0	5846	0	0	0	11520	--	--	16.08	16.08	0.10	0.20	0.05	0.37	0.00	0.00	20.9
16	26	-0	5811	0	0	0	11711	--	--	16.08	16.08	0.10	0.21	0.05	0.36	0.00	0.00	20.9
17	26	-0	5867	0	0	0	11543	--	--	16.08	16.08	0.10	0.20	0.05	0.37	0.00	0.00	20.9
18	26	-0	8528	0	0	0	17840	--	--	16.08	16.08	0.00	0.30	0.07	0.53	0.00	0.00	20.9
19	26	-0	8846	0	0	0	18199	--	--	16.08	16.08	0.00	0.31	0.07	0.55	0.00	0.00	20.9
20	26	-0	8410	0	0	0	17245	--	--	16.08	16.08	0.00	0.29	0.07	0.53	0.00	0.00	20.9
37	26	-0	8017	0	0	0	16715	--	--	16.08	16.08	0.00	0.28	0.07	0.50	0.00	0.00	20.9
38	26	-0	8547	0	0	0	17315	--	--	16.08	16.08	0.00	0.30	0.07	0.54	0.00	0.00	20.9
39	26	-0	7820	0	0	0	15722	--	--	16.08	16.08	0.00	0.27	0.06	0.49	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	52	-0	7577	0	0	0	8960	--	--	16.08	16.08	0.00	0.15	0.06	0.48	0.00	0.00	20.9
2	52	-0	5786	0	0	0	6915	--	--	16.08	16.08	0.10	0.12	0.05	0.36	0.00	0.00	20.9
3	52	-0	5802	0	0	0	6851	--	--	16.08	16.08	0.10	0.12	0.05	0.36	0.00	0.00	20.9
4	52	-0	5855	0	0	0	6933	--	--	16.08	16.08	0.10	0.12	0.05	0.37	0.00	0.00	20.9
5	52	-0	5871	0	0	0	6869	--	--	16.08	16.08	0.10	0.12	0.05	0.37	0.00	0.00	20.9
6	52	-0	5790	0	0	0	6997	--	--	16.08	16.08	0.10	0.12	0.05	0.36	0.00	0.00	20.9
7	52	-0	5846	0	0	0	6783	--	--	16.08	16.08	0.10	0.12	0.05	0.37	0.00	0.00	20.9
8	52	-0	5811	0	0	0	7002	--	--	16.08	16.08	0.10	0.12	0.05	0.36	0.00	0.00	20.9

9	52	-0	5867	0	0	0	6788	--	--	16.08	16.08	0.10	0.12	0.05	0.37	0.00	0.00	20.9
10	52	-0	5786	0	0	0	6915	--	--	16.08	16.08	0.10	0.12	0.05	0.36	0.00	0.00	20.9
11	52	-0	5802	0	0	0	6851	--	--	16.08	16.08	0.10	0.12	0.05	0.36	0.00	0.00	20.9
12	52	-0	5855	0	0	0	6933	--	--	16.08	16.08	0.10	0.12	0.05	0.37	0.00	0.00	20.9
13	52	-0	5871	0	0	0	6869	--	--	16.08	16.08	0.10	0.12	0.05	0.37	0.00	0.00	20.9
14	52	-0	5790	0	0	0	6997	--	--	16.08	16.08	0.10	0.12	0.05	0.36	0.00	0.00	20.9
15	52	-0	5846	0	0	0	6783	--	--	16.08	16.08	0.10	0.12	0.05	0.37	0.00	0.00	20.9
16	52	-0	5811	0	0	0	7002	--	--	16.08	16.08	0.10	0.12	0.05	0.36	0.00	0.00	20.9
17	52	-0	5867	0	0	0	6788	--	--	16.08	16.08	0.10	0.12	0.05	0.37	0.00	0.00	20.9
18	52	-0	8528	0	0	0	10930	--	--	16.08	16.08	0.00	0.19	0.07	0.53	0.00	0.00	20.9
19	52	-0	8846	0	0	0	11030	--	--	16.08	16.08	0.00	0.19	0.07	0.55	0.00	0.00	20.9
20	52	-0	8410	0	0	0	10430	--	--	16.08	16.08	0.00	0.18	0.07	0.53	0.00	0.00	20.9
37	52	-0	8017	0	0	0	10220	--	--	16.08	16.08	0.00	0.17	0.07	0.50	0.00	0.00	20.9
38	52	-0	8547	0	0	0	10390	--	--	16.08	16.08	0.00	0.18	0.07	0.54	0.00	0.00	20.9
39	52	-0	7820	0	0	0	9384	--	--	16.08	16.08	0.00	0.16	0.06	0.49	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 121 NI 1967 NF 1976 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice resistenza			aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	5816	0	0	0	2041	--	--	16.08	16.08	0.00	0.03	0.05	0.36	0.00	0.00	20.9
2	0	-0	4446	0	0	0	1629	--	--	16.08	16.08	0.10	0.03	0.04	0.28	0.00	0.00	20.9
3	0	-0	4463	0	0	0	1548	--	--	16.08	16.08	0.10	0.03	0.04	0.28	0.00	0.00	20.9
4	0	-0	4484	0	0	0	1592	--	--	16.08	16.08	0.10	0.03	0.04	0.28	0.00	0.00	20.9
5	0	-0	4501	0	0	0	1511	--	--	16.08	16.08	0.10	0.03	0.04	0.28	0.00	0.00	20.9
6	0	-0	4440	0	0	0	1711	--	--	16.08	16.08	0.10	0.03	0.04	0.28	0.00	0.00	20.9
7	0	-0	4496	0	0	0	1440	--	--	16.08	16.08	0.10	0.03	0.04	0.28	0.00	0.00	20.9
8	0	-0	4451	0	0	0	1700	--	--	16.08	16.08	0.10	0.03	0.04	0.28	0.00	0.00	20.9
9	0	-0	4507	0	0	0	1428	--	--	16.08	16.08	0.10	0.03	0.04	0.28	0.00	0.00	20.9
10	0	-0	4446	0	0	0	1629	--	--	16.08	16.08	0.10	0.03	0.04	0.28	0.00	0.00	20.9
11	0	-0	4463	0	0	0	1548	--	--	16.08	16.08	0.10	0.03	0.04	0.28	0.00	0.00	20.9
12	0	-0	4484	0	0	0	1592	--	--	16.08	16.08	0.10	0.03	0.04	0.28	0.00	0.00	20.9
13	0	-0	4501	0	0	0	1511	--	--	16.08	16.08	0.10	0.03	0.04	0.28	0.00	0.00	20.9
14	0	-0	4440	0	0	0	1711	--	--	16.08	16.08	0.10	0.03	0.04	0.28	0.00	0.00	20.9
15	0	-0	4496	0	0	0	1440	--	--	16.08	16.08	0.10	0.03	0.04	0.28	0.00	0.00	20.9
16	0	-0	4451	0	0	0	1700	--	--	16.08	16.08	0.10	0.03	0.04	0.28	0.00	0.00	20.9
17	0	-0	4507	0	0	0	1428	--	--	16.08	16.08	0.10	0.03	0.04	0.28	0.00	0.00	20.9
18	0	-0	6675	0	0	0	3073	--	--	16.08	16.08	0.00	0.05	0.06	0.42	0.00	0.00	20.9
19	0	-0	6860	0	0	0	2915	--	--	16.08	16.08	0.00	0.05	0.06	0.43	0.00	0.00	20.9
20	0	-0	6511	0	0	0	2720	--	--	16.08	16.08	0.00	0.05	0.05	0.41	0.00	0.00	20.9
37	0	-0	6274	0	0	0	2833	--	--	16.08	16.08	0.00	0.05	0.05	0.39	0.00	0.00	20.9
38	0	-0	6581	0	0	0	2570	--	--	16.08	16.08	0.00	0.04	0.05	0.41	0.00	0.00	20.9
39	0	-0	5999	0	0	0	2245	--	--	16.08	16.08	0.00	0.04	0.05	0.38	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	5816	0	0	0	9759	--	--	16.08	16.08	0.00	0.17	0.05	0.36	0.00	0.00	20.9
2	26	-0	4446	0	0	0	7529	--	--	16.08	16.08	0.10	0.13	0.04	0.28	0.00	0.00	20.9
3	26	-0	4463	0	0	0	7470	--	--	16.08	16.08	0.10	0.13	0.04	0.28	0.00	0.00	20.9
4	26	-0	4484	0	0	0	7542	--	--	16.08	16.08	0.10	0.13	0.04	0.28	0.00	0.00	20.9
5	26	-0	4501	0	0	0	7484	--	--	16.08	16.08	0.10	0.13	0.04	0.28	0.00	0.00	20.9
6	26	-0	4440	0	0	0	7603	--	--	16.08	16.08	0.10	0.13	0.04	0.28	0.00	0.00	20.9
7	26	-0	4496	0	0	0	7406	--	--	16.08	16.08	0.10	0.13	0.04	0.28	0.00	0.00	20.9
8	26	-0	4451	0	0	0	7607	--	--	16.08	16.08	0.10	0.13	0.04	0.28	0.00	0.00	20.9
9	26	-0	4507	0	0	0	7409	--	--	16.08	16.08	0.10	0.13	0.04	0.28	0.00	0.00	20.9
10	26	-0	4446	0	0	0	7529	--	--	16.08	16.08	0.10	0.13	0.04	0.28	0.00	0.00	20.9
11	26	-0	4463	0	0	0	7470	--	--	16.08	16.08	0.10	0.13	0.04	0.28	0.00	0.00	20.9
12	26	-0	4484	0	0	0	7542	--	--	16.08	16.08	0.10	0.13	0.04	0.28	0.00	0.00	20.9
13	26	-0	4501	0	0	0	7484	--	--	16.08	16.08	0.10	0.13	0.04	0.28	0.00	0.00	20.9
14	26	-0	4440	0	0	0	7603	--	--	16.08	16.08	0.10	0.13	0.04	0.28	0.00	0.00	20.9
15	26	-0	4496	0	0	0	7406	--	--	16.08	16.08	0.10	0.13	0.04	0.28	0.00	0.00	20.9
16	26	-0	4451	0	0	0	7607	--	--	16.08	16.08	0.10	0.13	0.04	0.28	0.00	0.00	20.9
17	26	-0	4507	0	0	0	7409	--	--	16.08	16.08	0.10	0.13	0.04	0.28	0.00	0.00	20.9
18	26	-0	6675	0	0	0	11931	--	--	16.08	16.08	0.00	0.20	0.06	0.42	0.00	0.00	20.9
19	26	-0	6860	0	0	0	12019	--	--	16.08	16.08	0.00	0.20	0.06	0.43	0.00	0.00	20.9
20	26	-0	6511	0	0	0	11361	--	--	16.08	16.08	0.00	0.19	0.05	0.41	0.00	0.00	20.9
37	26	-0	6274	0	0	0	11159	--	--	16.08	16.08	0.00	0.19	0.05	0.39	0.00	0.00	20.9
38	26	-0	6581	0	0	0	11303	--	--	16.08	16.08	0.00	0.19	0.05	0.41	0.00	0.00	20.9
39	26	-0	5999	0	0	0	10206	--	--	16.08	16.08	0.00	0.17	0.05	0.38	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	52	-0	5816	0	0	0	5045	--	--	16.08	16.08	0.00	0.09	0.05	0.36	0.00	0.00	20.9
2	52	-0	4446	0	0	0	3926	--	--	16.08	16.08	0.10	0.07	0.04	0.28	0.00	0.00	20.9
3	52	-0	4463	0	0	0	3853	--	--	16.08	16.08	0.10	0.07	0.04	0.28	0.00	0.00	20.9
4	52	-0	4484	0	0	0	3908	--	--	16.08	16.08	0.10	0.07	0.04	0.28	0.00	0.00	20.9
5	52	-0	4501	0	0	0	3836	--	--	16.08	16.08	0.10	0.07	0.04	0.28	0.00	0.00	20.9
6	52	-0	4440	0	0	0	4005	--	--	16.08	16.08	0.10	0.07	0.04	0.28	0.00	0.00	20.9
7	52	-0	4496	0	0	0	3762	--	--	16.08	16.08	0.10	0.07	0.04	0.28	0.00	0.00	20.9
8	52	-0	4451	0	0	0	3999	--	--	16.08	16.08	0.10	0.07	0.04	0.28	0.00	0.00	20.9
9	52	-0	4507	0	0	0	3757	--	--	16.08	16.08	0.10	0.07	0.04	0.28	0.00	0.00	20.9
10	52	-0	4446	0	0	0	3926	--	--	16.08	16.08	0.10	0.07	0.04	0.28	0.00	0.00	20.9
11	52	-0	4463	0	0	0	3853	--	--	16.08	16.08	0.10	0.07	0.04	0.28	0.00	0.00	20.9
12	52	-0	4484	0	0	0	3908	--	--	16.08	16.08	0.10	0.07	0.04	0.28	0.00	0.00	20.9
13	52	-0	4501	0	0	0	3836	--	--	16.08	16.08	0.10	0.07	0.04	0.28	0.00	0.00	20.9
14	52	-0	4440	0	0	0	4005	--	--	16.08	16.08	0.10	0.07	0.04	0.28	0.00	0.00	20.9
15	52	-0	4496	0	0	0	3762	--	--	16.08	16.08	0.10	0.07	0.04	0.28	0.00	0.00	20.9
16	52	-0	4451	0	0	0	3999	--	--	16.08	16.08	0.10	0.07	0.04	0.28	0.00	0.00	20.9
17	52	-0	4507	0	0	0	3757	--	--	16.08	16.08	0.10	0.07	0.04	0.28	0.00	0.00	20.9
18	52	-0	6675	0	0	0	6522	--	--	16.08	16.08	0.00	0.11	0.06	0.42	0.00	0.00	20.9
19	52	-0	6860	0	0	0	6459	--	--	16.08	16.08	0.00	0.11	0.06	0.43	0.00	0.00	20.9
20	52	-0	6511	0	0	0	6084	--	--	16.08	16.08	0.00	0.10	0.05	0.41	0.00	0.00	20.9
37	52	-0	6274	0	0	0	6074	--	--	16.08	16.08	0.00	0.10	0.05	0.39	0.00	0.00	20.9
38	52	-0	6581	0	0	0	5970	--	--	16.08	16.08	0.00	0.10	0.05	0.41	0.00	0.00	20.9
39	52	-0	5999	0	0	0	5344	--	--	16.08	16.08	0.00	0.09	0.05	0.38	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 122 NI 1974 NF 1967 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice resistenza			aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	4206	0	0	0	-132	--	--	16.08	16.08	0.18	0.00	0.03	0.26	0.00	0.00	20.9
2	0	-0	3225	0	0	0	-38	--	--	16.08	16.08	0.29	0.00	0.03	0.20	0.00	0.00	20.9
3	0	-0	3241	0	0	0	-127	--	--	16.08	16.08	0.29	0.00	0.03	0.20	0.00	0.00	20.9
4	0	-0	3229	0	0	0	-77	--	--	16.08	16.08	0.29	0.00	0.03	0.20	0.00	0.00	20.9
5	0	-0	3245	0	0	0	-166	--	--	16.08	16.08	0.29	0.00	0.03	0.20	0.00	0.00	20.9
6	0	-0	3208	0	0	0	53	--	--	16.08	16.08	0.10	0.00	0.03	0.20	0.00	0.00	20.9
7	0	-0	3261	0	0	0	-245	--	--	16.08	16.08	0.29	0.00	0.03	0.20	0.00	0.00	20.9
8	0	-0	3210	0	0	0	42	--	--	16.08	16.08	0.10	0.00	0.03	0.20	0.00	0.00	20.9
9	0	-0	3262	0	0	0	-257	--	--	16.08	16.08	0.29	0.00	0.03	0.20	0.00	0.00	20.9
10	0	-0	3225	0	0	0	-38	--	--	16.08	16.08	0.29	0.00	0.03	0.20	0.00	0.00	20.9
11	0	-0	3241	0	0	0	-127	--	--	16.08	16.08	0.29	0.00	0.03	0.20	0.00	0.00	20.9
12	0	-0	3229	0	0	0	-77	--	--	16.08	16.08	0.29	0.00	0.03	0.20	0.00	0.00	20.9
13	0	-0	3245	0	0	0	-166	--	--	16.08	16.08	0.29	0.00	0.03	0.20	0.00	0.00	20.9
14	0	-0	3208	0	0	0	53	--	--	16.08	16.08	0.10	0.00	0.03	0.20	0.00	0.00	20.9
15	0	-0	3261	0	0	0	-245	--	--	16.08	16.08	0.29	0.00	0.03	0.20	0.00	0.00	20.9
16	0	-0	3210	0	0	0	42	--	--	16.08	16.08	0.10	0.00	0.03	0.20	0.00	0.00	20.9
17	0	-0	3262	0	0	0	-257	--	--	16.08	16.08	0.29	0.00	0.03	0.20	0.00	0.00	20.9
18	0	-0	5009	0	0	0	485	--	--	16.08	16.08	0.00	0.01	0.04	0.31	0.00	0.00	20.9
19	0	-0	5050	0	0	0	306	--	--	16.08	16.08	0.00	0.01	0.04	0.32	0.00	0.00	20.9
20	0	-0	4790	0	0	0	245	--	--	16.08	16.08	0.00	0.00	0.04	0.30	0.00	0.00	20.9
37	0	-0	4709	0	0	0	400	--	--	16.08	16.08	0.00	0.01	0.04	0.30	0.00	0.00	20.9
38	0	-0	4778	0	0	0	101	--	--	16.08	16.08	0.00	0.00	0.04	0.30	0.00	0.00	20.9
39	0	-0	4344	0	0	0	-0	--	--	16.08	16.08	0.18	0.00	0.04	0.27	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice resistenza			aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	26	-0	4206	0	0	0	5450	--	--	16.08	16.08	0.00	0.09	0.03	0.26	0.00	0.00	20.9
2	26	-0	3225	0	0	0	4242	--	--	16.08	16.08	0.10	0.08	0.03	0.20	0.00	0.00	20.9
3	26	-0	3241	0	0	0	4174	--	--	16.08	16.08	0.10	0.07	0.03	0.20	0.00	0.00	20.9
4	26	-0	3229	0	0	0	4209	--	--	16.08	16.08	0.10	0.07	0.03	0.20	0.00	0.00	20.9
5	26	-0	3245	0	0	0	4141	--	--	16.08	16.08	0.10	0.07	0.03	0.20	0.00	0.00	20.9
6	26	-0	3208	0	0	0	4311	--	--	16.08	16.08	0.10	0.08	0.03	0.20	0.00	0.00	20.9
7	26	-0	3261	0	0	0	4083	--	--	16.08	16.08	0.10	0.07	0.03	0.20	0.00	0.00	20.9
8	26	-0	3210	0	0	0	4301	--	--	16.08	16.08	0.10	0.08	0.03	0.20	0.00	0.00	20.9
9	26	-0	3262	0	0	0	4072	--	--	16.08	16.08	0.10	0.07	0.03	0.20	0.00	0.00	20.9
10	26	-0	3225	0	0	0	4242	--	--	16.08	16.08	0.10	0.08	0.03	0.20	0.00	0.00	20.9
11	26	-0	3241	0	0	0	4174	--	--	16.08	16.08	0.10	0.07	0.03	0.20	0.00	0.00	20.9
12	26	-0	3229	0	0	0	4209	--	--	16.08	16.08	0.10	0.07	0.03	0.20	0.00	0.00	20.9
13	26	-0	3245	0	0	0	4141	--	--	16.08	16.08	0.10	0.07	0.03	0.20	0.00	0.00	20.9
14	26	-0	3208	0	0	0	4311	--	--	16.08	16.08	0.10	0.08	0.03	0.20	0.00	0.00	20.9
15	26	-0	3261	0	0	0	4083	--	--	16.08	16.08	0.10	0.07	0.03	0.20	0.00	0.00	20.9
16	26	-0	3210	0	0	0	4301	--	--	16.08	16.08	0.10	0.08	0.03	0.20	0.00	0.00	20.9
17	26	-0	3262	0	0	0	4072	--	--	16.08	16.08	0.10	0.07	0.03	0.20	0.00	0.00	20.9
18	26	-0	5009	0	0	0	7132	--	--	16.08	16.08	0.00	0.12	0.04	0.31	0.00	0.00	20.9
19	26	-0	5050	0	0	0	7008	--	--	16.08	16.08	0.00	0.12	0.04	0.32	0.00	0.00	20.9
20	26	-0	4790	0	0	0	6602	--	--	16.08	16.08	0.00	0.11	0.04	0.30	0.00	0.00	20.9
37	26	-0	4709	0	0	0	6649	--	--	16.08	16.08	0.00	0.11	0.04	0.30	0.00	0.00	20.9
38	26	-0	4778	0	0	0	6442	--	--	16.08	16.08	0.00	0.11	0.04	0.30	0.00	0.00	20.9
39	26	-0	4344	0	0	0	5765	--	--	16.08	16.08	0.00	0.10	0.04	0.27	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice resistenza			aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	52	-0	4206	0	0	0	2041	--	--	16.08	16.08	0.00	0.03	0.03	0.26	0.00	0.00	20.9
2	52	-0	3225	0	0	0	1629	--	--	16.08	16.08	0.10	0.03	0.03	0.20	0.00	0.00	20.9
3	52	-0	3241	0	0	0	1548	--	--	16.08	16.08	0.10	0.03	0.03	0.20	0.00	0.00	20.9
4	52	-0	3229	0	0	0	1592	--	--	16.08	16.08	0.10	0.03	0.03	0.20	0.00	0.00	20.9
5	52	-0	3245	0	0	0	1511	--	--	16.08	16.08	0.10	0.03	0.03	0.20	0.00	0.00	20.9
6	52	-0	3208	0	0	0	1711	--	--	16.08	16.08	0.10	0.03	0.03	0.20	0.00	0.00	20.9
7	52	-0	3261	0	0	0	1440	--	--	16.08	16.08	0.10	0.03	0.03	0.20	0.00	0.00	20.9
8	52	-0	3210	0	0	0	1700	--	--	16.08	16.08	0.10	0.03	0.03	0.20	0.00	0.00	20.9
9	52	-0	3262	0	0	0	1428	--	--	16.08	16.08	0.10	0.03	0.03	0.20	0.00	0.00	20.9
10	52	-0	3225	0	0	0	1629	--	--	16.08	16.08	0.10	0.03	0.03	0.20	0.00	0.00	20.9
11	52	-0	3241	0	0	0	1548	--	--	16.08	16.08	0.10	0.03	0.03	0.20	0.00	0.00	20.9
12	52	-0	3229	0	0	0	1592	--	--	16.08	16.08	0.10	0.03	0.03	0.20	0.00	0.00	20.9
13	52	-0	3245	0	0	0	1511	--	--	16.08	16.08	0.10	0.03	0.03	0.20	0.00	0.00	20.9
14	52	-0	3208	0	0	0	1711	--	--	16.08	16.08	0.10	0.03	0.03	0.20	0.00	0.00	20.9
15	52	-0	3261	0	0	0	1440	--	--	16.08	16.08	0.10	0.03	0.03	0.20	0.00	0.00	20.9
16	52	-0	3210	0	0	0	1700	--	--	16.08	16.08	0.10	0.03	0.03	0.20	0.00	0.00	20.9
17	52	-0	3262	0	0	0	1428	--	--	16.08	16.08	0.10	0.03	0.03	0.20	0.00	0.00	20.9
18	52	-0	5009	0	0	0	3073	--	--	16.08	16.08	0.00	0.05	0.04	0.31	0.00	0.00	20.9
19	52	-0	5050	0	0	0	2915	--	--	16.08	16.08	0.00	0.05	0.04	0.32	0.00	0.00	20.9
20	52	-0	4790	0	0	0	2720	--	--	16.08	16.08	0.00	0.05	0.04	0.30	0.00	0.00	20.9
37	52	-0	4709	0	0	0	2833	--	--	16.08	16.08	0.00	0.05	0.04	0.30	0.00	0.00	20.9
38	52	-0	4778	0	0	0	2570	--	--	16.08	16.08	0.00	0.04	0.04	0.30	0.00	0.00	20.9
39	52	-0	4344	0	0	0	2245	--	--	16.08	16.08	0.00	0.04	0.04	0.27	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 123 NI 1975 NF 1974 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice resistenza			aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	2753	0	0	0	-1555	--	--	16.08	16.08	0.18	0.03	0.02	0.17	0.00	0.00	20.9
2	0	-0	2128	0	0	0	-1137	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
3	0	-0	2140	0	0	0	-1233	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
4	0	-0	2095	0	0	0	-1159	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
5	0	-0	2108	0	0	0	-1255	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
6	0	-0	2101	0	0	0	-1033	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
7	0	-0	2144	0	0	0	-1353	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
8	0	-0	2092	0	0	0	-1039	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
9	0	-0	2134	0	0	0	-1359	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
10	0	-0	2128	0	0	0	-1137	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
11	0	-0	2140	0	0	0	-1233	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
12	0	-0	2095	0	0	0	-1159	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
13	0	-0	2108	0	0	0	-1255	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
14	0	-0	2101	0	0	0	-1033	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
15	0	-0	2144	0	0	0	-1353	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
16	0	-0	2092	0	0	0	-1039	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9

17	0	-0	2134	0	0	0	-1359	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
18	0	-0	3538	0	0	0	-1343	--	--	16.08	16.08	0.18	0.02	0.03	0.22	0.00	0.00	20.9
19	0	-0	3426	0	0	0	-1464	--	--	16.08	16.08	0.18	0.02	0.03	0.21	0.00	0.00	20.9
20	0	-0	3256	0	0	0	-1437	--	--	16.08	16.08	0.18	0.02	0.03	0.20	0.00	0.00	20.9
37	0	-0	3332	0	0	0	-1322	--	--	16.08	16.08	0.18	0.02	0.03	0.21	0.00	0.00	20.9
38	0	-0	3144	0	0	0	-1524	--	--	16.08	16.08	0.18	0.03	0.03	0.20	0.00	0.00	20.9
39	0	-0	2862	0	0	0	-1479	--	--	16.08	16.08	0.18	0.02	0.02	0.18	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	2753	0	0	0	-1555	--	--	16.08	16.08	0.18	0.03	0.02	0.17	0.00	0.00	20.9
2	26	-0	2128	0	0	0	-1137	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
3	26	-0	2140	0	0	0	-1233	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
4	26	-0	2095	0	0	0	-1159	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
5	26	-0	2108	0	0	0	-1255	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
6	26	-0	2101	0	0	0	-1033	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
7	26	-0	2144	0	0	0	-1353	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
8	26	-0	2092	0	0	0	-1039	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
9	26	-0	2134	0	0	0	-1359	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
10	26	-0	2128	0	0	0	-1137	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
11	26	-0	2140	0	0	0	-1233	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
12	26	-0	2095	0	0	0	-1159	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
13	26	-0	2108	0	0	0	-1255	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
14	26	-0	2101	0	0	0	-1033	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
15	26	-0	2144	0	0	0	-1353	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
16	26	-0	2092	0	0	0	-1039	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
17	26	-0	2134	0	0	0	-1359	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
18	26	-0	3538	0	0	0	-1343	--	--	16.08	16.08	0.18	0.02	0.03	0.22	0.00	0.00	20.9
19	26	-0	3426	0	0	0	-1464	--	--	16.08	16.08	0.18	0.02	0.03	0.21	0.00	0.00	20.9
20	26	-0	3256	0	0	0	-1437	--	--	16.08	16.08	0.18	0.02	0.03	0.20	0.00	0.00	20.9
37	26	-0	3332	0	0	0	-1322	--	--	16.08	16.08	0.18	0.02	0.03	0.21	0.00	0.00	20.9
38	26	-0	3144	0	0	0	-1524	--	--	16.08	16.08	0.18	0.03	0.03	0.20	0.00	0.00	20.9
39	26	-0	2862	0	0	0	-1479	--	--	16.08	16.08	0.18	0.02	0.02	0.18	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	52	-0	2753	0	0	0	-1555	--	--	16.08	16.08	0.18	0.03	0.02	0.17	0.00	0.00	20.9
2	52	-0	2128	0	0	0	-1137	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
3	52	-0	2140	0	0	0	-1233	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
4	52	-0	2095	0	0	0	-1159	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
5	52	-0	2108	0	0	0	-1255	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
6	52	-0	2101	0	0	0	53	--	--	16.08	16.08	0.10	0.00	0.02	0.13	0.00	0.00	20.9
7	52	-0	2144	0	0	0	-1353	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
8	52	-0	2092	0	0	0	42	--	--	16.08	16.08	0.10	0.00	0.02	0.13	0.00	0.00	20.9
9	52	-0	2134	0	0	0	-1359	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
10	52	-0	2128	0	0	0	-1137	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
11	52	-0	2140	0	0	0	-1233	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
12	52	-0	2095	0	0	0	-1159	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
13	52	-0	2108	0	0	0	-1255	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
14	52	-0	2101	0	0	0	53	--	--	16.08	16.08	0.10	0.00	0.02	0.13	0.00	0.00	20.9
15	52	-0	2144	0	0	0	-1353	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
16	52	-0	2092	0	0	0	42	--	--	16.08	16.08	0.10	0.00	0.02	0.13	0.00	0.00	20.9
17	52	-0	2134	0	0	0	-1359	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
18	52	-0	3538	0	0	0	485	--	--	16.08	16.08	0.00	0.01	0.03	0.22	0.00	0.00	20.9
19	52	-0	3426	0	0	0	306	--	--	16.08	16.08	0.00	0.01	0.03	0.21	0.00	0.00	20.9
20	52	-0	3256	0	0	0	245	--	--	16.08	16.08	0.00	0.00	0.03	0.20	0.00	0.00	20.9
37	52	-0	3332	0	0	0	400	--	--	16.08	16.08	0.00	0.01	0.03	0.21	0.00	0.00	20.9
38	52	-0	3144	0	0	0	101	--	--	16.08	16.08	0.00	0.00	0.03	0.20	0.00	0.00	20.9
39	52	-0	2862	0	0	0	-1479	--	--	16.08	16.08	0.18	0.02	0.02	0.18	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 124 NI 1966 NF 1975 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	1454	0	0	0	-2306	--	--	16.08	16.08	0.18	0.04	0.01	0.09	0.00	0.00	20.9
2	0	-0	1150	0	0	0	-1731	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
3	0	-0	1157	0	0	0	-1831	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
4	0	-0	1079	0	0	0	-1716	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
5	0	-0	1086	0	0	0	-1816	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
6	0	-0	1116	0	0	0	-1609	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
7	0	-0	1141	0	0	0	-1942	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
8	0	-0	1095	0	0	0	-1605	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
9	0	-0	1120	0	0	0	-1938	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
10	0	-0	1150	0	0	0	-1731	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
11	0	-0	1157	0	0	0	-1831	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
12	0	-0	1079	0	0	0	-1716	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
13	0	-0	1086	0	0	0	-1816	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
14	0	-0	1116	0	0	0	-1609	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
15	0	-0	1141	0	0	0	-1942	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
16	0	-0	1095	0	0	0	-1605	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
17	0	-0	1120	0	0	0	-1938	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
18	0	-0	2263	0	0	0	-2512	--	--	16.08	16.08	0.18	0.04	0.02	0.14	0.00	0.00	20.9
19	0	-0	1985	0	0	0	-2490	--	--	16.08	16.08	0.18	0.04	0.02	0.12	0.00	0.00	20.9
20	0	-0	1907	0	0	0	-2422	--	--	16.08	16.08	0.18	0.04	0.02	0.12	0.00	0.00	20.9
37	0	-0	2140	0	0	0	-2428	--	--	16.08	16.08	0.18	0.04	0.02	0.13	0.00	0.00	20.9
38	0	-0	1677	0	0	0	-2390	--	--	16.08	16.08	0.18	0.04	0.01	0.11	0.00	0.00	20.9
39	0	-0	1547	0	0	0	-2278	--	--	16.08	16.08	0.18	0.04	0.01	0.10	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	1454	0	0	0	-2306	--	--	16.08	16.08	0.18	0.04	0.01	0.09	0.00	0.00	20.9
2	26	-0	1150	0	0	0	-1731	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
3	26	-0	1157	0	0	0	-1831	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
4	26	-0	1079	0	0	0	-1716	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
5	26	-0	1086	0	0	0	-1816	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
6	26	-0	1116	0	0	0	-1609	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
7	26	-0	1141	0	0	0	-1942	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
8	26	-0	1095	0	0	0	-1605	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
9	26	-0	1120	0	0	0	-1938	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
10	26	-0	1150	0	0	0	-1731	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
11	26	-0	1157	0	0	0	-1831	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
12	26	-0	1079	0	0	0	-1716	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9

13	26	-0	1086	0	0	0	-1816	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
14	26	-0	1116	0	0	0	-1609	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
15	26	-0	1141	0	0	0	-1942	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
16	26	-0	1095	0	0	0	-1605	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
17	26	-0	1120	0	0	0	-1938	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
18	26	-0	2263	0	0	0	-2512	--	--	16.08	16.08	0.18	0.04	0.02	0.14	0.00	0.00	20.9
19	26	-0	1985	0	0	0	-2490	--	--	16.08	16.08	0.18	0.04	0.02	0.12	0.00	0.00	20.9
20	26	-0	1907	0	0	0	-2422	--	--	16.08	16.08	0.18	0.04	0.02	0.12	0.00	0.00	20.9
37	26	-0	2140	0	0	0	-2428	--	--	16.08	16.08	0.18	0.04	0.02	0.13	0.00	0.00	20.9
38	26	-0	1677	0	0	0	-2390	--	--	16.08	16.08	0.18	0.04	0.01	0.11	0.00	0.00	20.9
39	26	-0	1547	0	0	0	-2278	--	--	16.08	16.08	0.18	0.04	0.01	0.10	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	52	-0	1454	0	0	0	-2306	--	--	16.08	16.08	0.18	0.04	0.01	0.09	0.00	0.00	20.9
2	52	-0	1150	0	0	0	-1731	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
3	52	-0	1157	0	0	0	-1831	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
4	52	-0	1079	0	0	0	-1716	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
5	52	-0	1086	0	0	0	-1816	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
6	52	-0	1116	0	0	0	-1609	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
7	52	-0	1141	0	0	0	-1942	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
8	52	-0	1095	0	0	0	-1605	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
9	52	-0	1120	0	0	0	-1938	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
10	52	-0	1150	0	0	0	-1731	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
11	52	-0	1157	0	0	0	-1831	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
12	52	-0	1079	0	0	0	-1716	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
13	52	-0	1086	0	0	0	-1816	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
14	52	-0	1116	0	0	0	-1609	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
15	52	-0	1141	0	0	0	-1942	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
16	52	-0	1095	0	0	0	-1605	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
17	52	-0	1120	0	0	0	-1938	--	--	16.08	16.08	0.29	0.03	0.01	0.07	0.00	0.00	20.9
18	52	-0	2263	0	0	0	-2512	--	--	16.08	16.08	0.18	0.04	0.02	0.14	0.00	0.00	20.9
19	52	-0	1985	0	0	0	-2490	--	--	16.08	16.08	0.18	0.04	0.02	0.12	0.00	0.00	20.9
20	52	-0	1907	0	0	0	-2422	--	--	16.08	16.08	0.18	0.04	0.02	0.12	0.00	0.00	20.9
37	52	-0	2140	0	0	0	-2428	--	--	16.08	16.08	0.18	0.04	0.02	0.13	0.00	0.00	20.9
38	52	-0	1677	0	0	0	-2390	--	--	16.08	16.08	0.18	0.04	0.01	0.11	0.00	0.00	20.9
39	52	-0	1547	0	0	0	-2278	--	--	16.08	16.08	0.18	0.04	0.01	0.10	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 125 NI 1257 NF 1966 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	297	0	0	0	-2459	--	--	16.08	16.08	0.18	0.04	0.00	0.02	0.00	0.00	20.9
2	0	-0	285	0	0	0	-1878	--	--	16.08	16.08	0.29	0.03	0.00	0.02	0.00	0.00	20.9
3	0	-0	285	0	0	0	-1978	--	--	16.08	16.08	0.29	0.03	0.00	0.02	0.00	0.00	20.9
4	0	-0	172	0	0	0	-1806	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
5	0	-0	172	0	0	0	-1905	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
6	0	-0	246	0	0	0	-1736	--	--	16.08	16.08	0.29	0.03	0.00	0.02	0.00	0.00	20.9
7	0	-0	245	0	0	0	-2069	--	--	16.08	16.08	0.29	0.04	0.00	0.02	0.00	0.00	20.9
8	0	-0	212	0	0	0	-1715	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
9	0	-0	211	0	0	0	-2047	--	--	16.08	16.08	0.29	0.04	0.00	0.01	0.00	0.00	20.9
10	0	-0	285	0	0	0	-1878	--	--	16.08	16.08	0.29	0.03	0.00	0.02	0.00	0.00	20.9
11	0	-0	285	0	0	0	-1978	--	--	16.08	16.08	0.29	0.03	0.00	0.02	0.00	0.00	20.9
12	0	-0	172	0	0	0	-1806	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
13	0	-0	172	0	0	0	-1905	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
14	0	-0	246	0	0	0	-1736	--	--	16.08	16.08	0.29	0.03	0.00	0.02	0.00	0.00	20.9
15	0	-0	245	0	0	0	-2069	--	--	16.08	16.08	0.29	0.04	0.00	0.02	0.00	0.00	20.9
16	0	-0	212	0	0	0	-1715	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
17	0	-0	211	0	0	0	-2047	--	--	16.08	16.08	0.29	0.04	0.00	0.01	0.00	0.00	20.9
18	0	-0	1174	0	0	0	-3119	--	--	16.08	16.08	0.18	0.05	0.01	0.07	0.00	0.00	20.9
19	0	-0	718	0	0	0	-2860	--	--	16.08	16.08	0.18	0.05	0.01	0.05	0.00	0.00	20.9
20	0	-0	733	0	0	0	-2801	--	--	16.08	16.08	0.18	0.05	0.01	0.05	0.00	0.00	20.9
37	0	-0	1126	0	0	0	-3010	--	--	16.08	16.08	0.18	0.05	0.01	0.07	0.00	0.00	20.9
38	0	-0	366	0	0	0	-2579	--	--	16.08	16.08	0.18	0.04	0.00	0.02	0.00	0.00	20.9
39	0	-0	392	0	0	0	-2480	--	--	16.08	16.08	0.18	0.04	0.00	0.02	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	297	0	0	0	-2459	--	--	16.08	16.08	0.18	0.04	0.00	0.02	0.00	0.00	20.9
2	26	-0	285	0	0	0	-1878	--	--	16.08	16.08	0.29	0.03	0.00	0.02	0.00	0.00	20.9
3	26	-0	285	0	0	0	-1978	--	--	16.08	16.08	0.29	0.03	0.00	0.02	0.00	0.00	20.9
4	26	-0	172	0	0	0	-1806	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
5	26	-0	172	0	0	0	-1905	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
6	26	-0	246	0	0	0	-1736	--	--	16.08	16.08	0.29	0.03	0.00	0.02	0.00	0.00	20.9
7	26	-0	245	0	0	0	-2069	--	--	16.08	16.08	0.29	0.04	0.00	0.02	0.00	0.00	20.9
8	26	-0	212	0	0	0	-1715	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
9	26	-0	211	0	0	0	-2047	--	--	16.08	16.08	0.29	0.04	0.00	0.01	0.00	0.00	20.9
10	26	-0	285	0	0	0	-1878	--	--	16.08	16.08	0.29	0.03	0.00	0.02	0.00	0.00	20.9
11	26	-0	285	0	0	0	-1978	--	--	16.08	16.08	0.29	0.03	0.00	0.02	0.00	0.00	20.9
12	26	-0	172	0	0	0	-1806	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
13	26	-0	172	0	0	0	-1905	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
14	26	-0	246	0	0	0	-1736	--	--	16.08	16.08	0.29	0.03	0.00	0.02	0.00	0.00	20.9
15	26	-0	245	0	0	0	-2069	--	--	16.08	16.08	0.29	0.04	0.00	0.02	0.00	0.00	20.9
16	26	-0	212	0	0	0	-1715	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
17	26	-0	211	0	0	0	-2047	--	--	16.08	16.08	0.29	0.04	0.00	0.01	0.00	0.00	20.9
18	26	-0	1174	0	0	0	-3119	--	--	16.08	16.08	0.18	0.05	0.01	0.07	0.00	0.00	20.9
19	26	-0	718	0	0	0	-2860	--	--	16.08	16.08	0.18	0.05	0.01	0.05	0.00	0.00	20.9
20	26	-0	733	0	0	0	-2801	--	--	16.08	16.08	0.18	0.05	0.01	0.05	0.00	0.00	20.9
37	26	-0	1126	0	0	0	-3010	--	--	16.08	16.08	0.18	0.05	0.01	0.07	0.00	0.00	20.9
38	26	-0	366	0	0	0	-2579	--	--	16.08	16.08	0.18	0.04	0.00	0.02	0.00	0.00	20.9
39	26	-0	392	0	0	0	-2480	--	--	16.08	16.08	0.18	0.04	0.00	0.02	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	52	-0	297	0	0	0	-2459	--	--	16.08	16.08	0.18	0.04	0.00	0.02	0.00	0.00	20.9
2	52	-0	285	0	0	0	-1878	--	--	16.08	16.08	0.29	0.03	0.00	0.02	0.00	0.00	20.9
3	52	-0	285	0	0	0	-1978	--	--	16.08	16.08	0.29	0.03	0.00	0.02	0.00	0.00	20.9
4	52	-0	172	0	0	0	-1806	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
5	52	-0	172	0	0	0	-1905	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
6	52	-0	246	0	0	0	-1736	--	--	16.08	16.08	0.29	0.03	0.00	0.02	0.00	0.00	20.9
7	52	-0	245	0	0	0	-2069	--	--	16.08	16.08	0.29	0.04	0.00	0.02	0.00	0.00	20.9
8	52	-0	212	0	0	0	-1715	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9

9	52	-0	211	0	0	0	-2047	--	--	16.08	16.08	0.29	0.04	0.00	0.01	0.00	0.00	20.9
10	52	-0	285	0	0	0	-1878	--	--	16.08	16.08	0.29	0.03	0.00	0.02	0.00	0.00	20.9
11	52	-0	285	0	0	0	-1978	--	--	16.08	16.08	0.29	0.03	0.00	0.02	0.00	0.00	20.9
12	52	-0	172	0	0	0	-1806	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
13	52	-0	172	0	0	0	-1905	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
14	52	-0	246	0	0	0	-1736	--	--	16.08	16.08	0.29	0.03	0.00	0.02	0.00	0.00	20.9
15	52	-0	245	0	0	0	-2069	--	--	16.08	16.08	0.29	0.04	0.00	0.02	0.00	0.00	20.9
16	52	-0	212	0	0	0	-1715	--	--	16.08	16.08	0.29	0.03	0.00	0.01	0.00	0.00	20.9
17	52	-0	211	0	0	0	-2047	--	--	16.08	16.08	0.29	0.04	0.00	0.01	0.00	0.00	20.9
18	52	-0	1174	0	0	0	-3119	--	--	16.08	16.08	0.18	0.05	0.01	0.07	0.00	0.00	20.9
19	52	-0	718	0	0	0	-2860	--	--	16.08	16.08	0.18	0.05	0.01	0.05	0.00	0.00	20.9
20	52	-0	733	0	0	0	-2801	--	--	16.08	16.08	0.18	0.05	0.01	0.05	0.00	0.00	20.9
37	52	-0	1126	0	0	0	-3010	--	--	16.08	16.08	0.18	0.05	0.01	0.07	0.00	0.00	20.9
38	52	-0	366	0	0	0	-2579	--	--	16.08	16.08	0.18	0.04	0.00	0.02	0.00	0.00	20.9
39	52	-0	392	0	0	0	-2480	--	--	16.08	16.08	0.18	0.04	0.00	0.02	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 126 NI 1807 NF 1808 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	1534	0	0	0	-395	--	--	16.08	16.08	0.18	0.01	0.01	0.10	0.00	0.00	20.9
2	0	-0	1286	0	0	0	-328	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
3	0	-0	1196	0	0	0	-316	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
4	0	-0	1164	0	0	0	-292	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
5	0	-0	1074	0	0	0	-279	--	--	16.08	16.08	0.29	0.00	0.01	0.07	0.00	0.00	20.9
6	0	-0	1348	0	0	0	-329	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
7	0	-0	1048	0	0	0	-289	--	--	16.08	16.08	0.29	0.00	0.01	0.07	0.00	0.00	20.9
8	0	-0	1312	0	0	0	-319	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
9	0	-0	1011	0	0	0	-278	--	--	16.08	16.08	0.29	0.00	0.01	0.06	0.00	0.00	20.9
10	0	-0	1286	0	0	0	-328	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
11	0	-0	1196	0	0	0	-316	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
12	0	-0	1164	0	0	0	-292	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
13	0	-0	1074	0	0	0	-279	--	--	16.08	16.08	0.29	0.00	0.01	0.07	0.00	0.00	20.9
14	0	-0	1348	0	0	0	-329	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
15	0	-0	1048	0	0	0	-289	--	--	16.08	16.08	0.29	0.00	0.01	0.07	0.00	0.00	20.9
16	0	-0	1312	0	0	0	-319	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
17	0	-0	1011	0	0	0	-278	--	--	16.08	16.08	0.29	0.00	0.01	0.06	0.00	0.00	20.9
18	0	-0	2168	0	0	0	-527	--	--	16.08	16.08	0.18	0.01	0.02	0.14	0.00	0.00	20.9
19	0	-0	1748	0	0	0	-427	--	--	16.08	16.08	0.18	0.01	0.01	0.11	0.00	0.00	20.9
20	0	-0	1665	0	0	0	-464	--	--	16.08	16.08	0.18	0.01	0.01	0.10	0.00	0.00	20.9
37	0	-0	2163	0	0	0	-535	--	--	16.08	16.08	0.18	0.01	0.02	0.14	0.00	0.00	20.9
38	0	-0	1463	0	0	0	-367	--	--	16.08	16.08	0.18	0.01	0.01	0.09	0.00	0.00	20.9
39	0	-0	1325	0	0	0	-428	--	--	16.08	16.08	0.18	0.01	0.01	0.08	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	1534	0	0	0	1656	--	--	16.08	16.08	0.00	0.03	0.01	0.10	0.00	0.00	20.9
2	27	-0	1286	0	0	0	1391	--	--	16.08	16.08	0.10	0.02	0.01	0.08	0.00	0.00	20.9
3	27	-0	1196	0	0	0	1283	--	--	16.08	16.08	0.10	0.02	0.01	0.08	0.00	0.00	20.9
4	27	-0	1164	0	0	0	1264	--	--	16.08	16.08	0.10	0.02	0.01	0.07	0.00	0.00	20.9
5	27	-0	1074	0	0	0	1156	--	--	16.08	16.08	0.10	0.02	0.01	0.07	0.00	0.00	20.9
6	27	-0	1348	0	0	0	1472	--	--	16.08	16.08	0.10	0.03	0.01	0.08	0.00	0.00	20.9
7	27	-0	1048	0	0	0	-289	--	--	16.08	16.08	0.29	0.00	0.01	0.07	0.00	0.00	20.9
8	27	-0	1312	0	0	0	1435	--	--	16.08	16.08	0.10	0.03	0.01	0.08	0.00	0.00	20.9
9	27	-0	1011	0	0	0	-278	--	--	16.08	16.08	0.29	0.00	0.01	0.06	0.00	0.00	20.9
10	27	-0	1286	0	0	0	1391	--	--	16.08	16.08	0.10	0.02	0.01	0.08	0.00	0.00	20.9
11	27	-0	1196	0	0	0	1283	--	--	16.08	16.08	0.10	0.02	0.01	0.08	0.00	0.00	20.9
12	27	-0	1164	0	0	0	1264	--	--	16.08	16.08	0.10	0.02	0.01	0.07	0.00	0.00	20.9
13	27	-0	1074	0	0	0	1156	--	--	16.08	16.08	0.10	0.02	0.01	0.07	0.00	0.00	20.9
14	27	-0	1348	0	0	0	1472	--	--	16.08	16.08	0.10	0.03	0.01	0.08	0.00	0.00	20.9
15	27	-0	1048	0	0	0	-289	--	--	16.08	16.08	0.29	0.00	0.01	0.07	0.00	0.00	20.9
16	27	-0	1312	0	0	0	1435	--	--	16.08	16.08	0.10	0.03	0.01	0.08	0.00	0.00	20.9
17	27	-0	1011	0	0	0	-278	--	--	16.08	16.08	0.29	0.00	0.01	0.06	0.00	0.00	20.9
18	27	-0	2168	0	0	0	2370	--	--	16.08	16.08	0.00	0.04	0.02	0.14	0.00	0.00	20.9
19	27	-0	1748	0	0	0	1910	--	--	16.08	16.08	0.00	0.03	0.01	0.11	0.00	0.00	20.9
20	27	-0	1665	0	0	0	-464	--	--	16.08	16.08	0.18	0.01	0.01	0.10	0.00	0.00	20.9
37	27	-0	2163	0	0	0	2356	--	--	16.08	16.08	0.00	0.04	0.02	0.14	0.00	0.00	20.9
38	27	-0	1463	0	0	0	1589	--	--	16.08	16.08	0.00	0.03	0.01	0.09	0.00	0.00	20.9
39	27	-0	1325	0	0	0	-428	--	--	16.08	16.08	0.18	0.01	0.01	0.08	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	54	-0	1534	0	0	0	427	--	--	16.08	16.08	0.00	0.01	0.01	0.10	0.00	0.00	20.9
2	54	-0	1286	0	0	0	361	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
3	54	-0	1196	0	0	0	325	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
4	54	-0	1164	0	0	0	332	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
5	54	-0	1074	0	0	0	296	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
6	54	-0	1348	0	0	0	393	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
7	54	-0	1048	0	0	0	273	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
8	54	-0	1312	0	0	0	384	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
9	54	-0	1011	0	0	0	264	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
10	54	-0	1286	0	0	0	361	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
11	54	-0	1196	0	0	0	325	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
12	54	-0	1164	0	0	0	332	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
13	54	-0	1074	0	0	0	296	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
14	54	-0	1348	0	0	0	393	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
15	54	-0	1048	0	0	0	273	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
16	54	-0	1312	0	0	0	384	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
17	54	-0	1011	0	0	0	264	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
18	54	-0	2168	0	0	0	634	--	--	16.08	16.08	0.00	0.01	0.02	0.14	0.00	0.00	20.9
19	54	-0	1748	0	0	0	510	--	--	16.08	16.08	0.00	0.01	0.01	0.11	0.00	0.00	20.9
20	54	-0	1665	0	0	0	428	--	--	16.08	16.08	0.00	0.01	0.01	0.10	0.00	0.00	20.9
37	54	-0	2163	0	0	0	624	--	--	16.08	16.08	0.00	0.01	0.02	0.14	0.00	0.00	20.9
38	54	-0	1463	0	0	0	417	--	--	16.08	16.08	0.00	0.01	0.01	0.09	0.00	0.00	20.9
39	54	-0	1325	0	0	0	281	--	--	16.08	16.08	0.00	0.00	0.01	0.08	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 127 NI 1804 NF 1807 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	1093	0	0	0	-645	--	--	16.08	16.08	0.18	0.01	0.01	0.07	0.00	0.00	20.9
2	0	-0	909	0	0	0	-538	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
3	0	-0	865	0	0	0	-516	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
4	0	-0	816	0	0	0	-476	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
5	0	-0	772	0	0	0	-453	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
6	0	-0	927	0	0	0	-543	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
7	0	-0	782	0	0	0	-467	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
8	0	-0	899	0	0	0	-525	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
9	0	-0	754	0	0	0	-448	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
10	0	-0	909	0	0	0	-538	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
11	0	-0	865	0	0	0	-516	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
12	0	-0	816	0	0	0	-476	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
13	0	-0	772	0	0	0	-453	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
14	0	-0	927	0	0	0	-543	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
15	0	-0	782	0	0	0	-467	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
16	0	-0	899	0	0	0	-525	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
17	0	-0	754	0	0	0	-448	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
18	0	-0	1547	0	0	0	-896	--	--	16.08	16.08	0.18	0.01	0.01	0.10	0.00	0.00	20.9
19	0	-0	1235	0	0	0	-705	--	--	16.08	16.08	0.18	0.01	0.01	0.08	0.00	0.00	20.9
20	0	-0	1227	0	0	0	-742	--	--	16.08	16.08	0.18	0.01	0.01	0.08	0.00	0.00	20.9
37	0	-0	1553	0	0	0	-908	--	--	16.08	16.08	0.18	0.02	0.01	0.10	0.00	0.00	20.9
38	0	-0	1032	0	0	0	-591	--	--	16.08	16.08	0.18	0.01	0.01	0.06	0.00	0.00	20.9
39	0	-0	1018	0	0	0	-652	--	--	16.08	16.08	0.18	0.01	0.01	0.06	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	1093	0	0	0	-645	--	--	16.08	16.08	0.18	0.01	0.01	0.07	0.00	0.00	20.9
2	27	-0	909	0	0	0	-538	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
3	27	-0	865	0	0	0	-516	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
4	27	-0	816	0	0	0	-476	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
5	27	-0	772	0	0	0	-453	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
6	27	-0	927	0	0	0	-543	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
7	27	-0	782	0	0	0	-467	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
8	27	-0	899	0	0	0	-525	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
9	27	-0	754	0	0	0	-448	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
10	27	-0	909	0	0	0	-538	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
11	27	-0	865	0	0	0	-516	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
12	27	-0	816	0	0	0	-476	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
13	27	-0	772	0	0	0	-453	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
14	27	-0	927	0	0	0	-543	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
15	27	-0	782	0	0	0	-467	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
16	27	-0	899	0	0	0	-525	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
17	27	-0	754	0	0	0	-448	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
18	27	-0	1547	0	0	0	-896	--	--	16.08	16.08	0.18	0.01	0.01	0.10	0.00	0.00	20.9
19	27	-0	1235	0	0	0	-705	--	--	16.08	16.08	0.18	0.01	0.01	0.08	0.00	0.00	20.9
20	27	-0	1227	0	0	0	-742	--	--	16.08	16.08	0.18	0.01	0.01	0.08	0.00	0.00	20.9
37	27	-0	1553	0	0	0	-908	--	--	16.08	16.08	0.18	0.02	0.01	0.10	0.00	0.00	20.9
38	27	-0	1032	0	0	0	-591	--	--	16.08	16.08	0.18	0.01	0.01	0.06	0.00	0.00	20.9
39	27	-0	1018	0	0	0	-652	--	--	16.08	16.08	0.18	0.01	0.01	0.06	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	54	-0	1093	0	0	0	-645	--	--	16.08	16.08	0.18	0.01	0.01	0.07	0.00	0.00	20.9
2	54	-0	909	0	0	0	-538	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
3	54	-0	865	0	0	0	-516	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
4	54	-0	816	0	0	0	-476	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
5	54	-0	772	0	0	0	-453	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
6	54	-0	927	0	0	0	-543	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
7	54	-0	782	0	0	0	-467	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
8	54	-0	899	0	0	0	-525	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
9	54	-0	754	0	0	0	-448	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
10	54	-0	909	0	0	0	-538	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
11	54	-0	865	0	0	0	-516	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
12	54	-0	816	0	0	0	-476	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
13	54	-0	772	0	0	0	-453	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
14	54	-0	927	0	0	0	-543	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
15	54	-0	782	0	0	0	-467	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
16	54	-0	899	0	0	0	-525	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
17	54	-0	754	0	0	0	-448	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
18	54	-0	1547	0	0	0	-896	--	--	16.08	16.08	0.18	0.01	0.01	0.10	0.00	0.00	20.9
19	54	-0	1235	0	0	0	-705	--	--	16.08	16.08	0.18	0.01	0.01	0.08	0.00	0.00	20.9
20	54	-0	1227	0	0	0	-742	--	--	16.08	16.08	0.18	0.01	0.01	0.08	0.00	0.00	20.9
37	54	-0	1553	0	0	0	-908	--	--	16.08	16.08	0.18	0.02	0.01	0.10	0.00	0.00	20.9
38	54	-0	1032	0	0	0	-591	--	--	16.08	16.08	0.18	0.01	0.01	0.06	0.00	0.00	20.9
39	54	-0	1018	0	0	0	-652	--	--	16.08	16.08	0.18	0.01	0.01	0.06	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 128 NI 1805 NF 1804 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-55	0	0	0	-645	--	--	16.08	16.08	0.18	0.01	0.00	0.00	0.00	0.00	20.9
2	0	-0	-39	0	0	0	-546	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
3	0	-0	-4	0	0	0	-498	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
4	0	-0	-80	0	0	0	-495	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
5	0	-0	-45	0	0	0	-447	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
6	0	-0	-94	0	0	0	-584	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
7	0	-0	22	0	0	0	-436	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
8	0	-0	-106	0	0	0	-569	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
9	0	-0	9	0	0	0	-414	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
10	0	-0	-39	0	0	0	-546	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
11	0	-0	-4	0	0	0	-498	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
12	0	-0	-80	0	0	0	-495	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
13	0	-0	-45	0	0	0	-447	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
14	0	-0	-94	0	0	0	-584	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
15	0	-0	22	0	0	0	-436	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
16	0	-0	-106	0	0	0	-569	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9

17	0	-0	9	0	0	0	-414	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
18	0	-0	77	0	0	0	-933	--	--	16.08	16.08	0.18	0.02	0.00	0.00	0.00	0.00	20.9
19	0	-0	-56	0	0	0	-731	--	--	16.08	16.08	0.18	0.01	0.00	0.00	0.00	0.00	20.9
20	0	-0	55	0	0	0	-729	--	--	16.08	16.08	0.18	0.01	0.00	0.00	0.00	0.00	20.9
37	0	-0	110	0	0	0	-947	--	--	16.08	16.08	0.18	0.02	0.00	0.01	0.00	0.00	20.9
38	0	-0	-111	0	0	0	-620	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9
39	0	-0	73	0	0	0	-606	--	--	16.08	16.08	0.18	0.01	0.00	0.00	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-55	0	0	0	-645	--	--	16.08	16.08	0.18	0.01	0.00	0.00	0.00	0.00	20.9
2	27	-0	-39	0	0	0	-546	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
3	27	-0	-4	0	0	0	-498	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
4	27	-0	-80	0	0	0	-495	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
5	27	-0	-45	0	0	0	-447	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
6	27	-0	-94	0	0	0	-584	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
7	27	-0	22	0	0	0	-436	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
8	27	-0	-106	0	0	0	-569	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
9	27	-0	9	0	0	0	-414	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
10	27	-0	-39	0	0	0	-546	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
11	27	-0	-4	0	0	0	-498	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
12	27	-0	-80	0	0	0	-495	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
13	27	-0	-45	0	0	0	-447	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
14	27	-0	-94	0	0	0	-584	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
15	27	-0	22	0	0	0	-436	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
16	27	-0	-106	0	0	0	-569	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
17	27	-0	9	0	0	0	-414	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
18	27	-0	77	0	0	0	-933	--	--	16.08	16.08	0.18	0.02	0.00	0.00	0.00	0.00	20.9
19	27	-0	-56	0	0	0	-731	--	--	16.08	16.08	0.18	0.01	0.00	0.00	0.00	0.00	20.9
20	27	-0	55	0	0	0	-729	--	--	16.08	16.08	0.18	0.01	0.00	0.00	0.00	0.00	20.9
37	27	-0	110	0	0	0	-947	--	--	16.08	16.08	0.18	0.02	0.00	0.01	0.00	0.00	20.9
38	27	-0	-111	0	0	0	-620	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9
39	27	-0	73	0	0	0	-606	--	--	16.08	16.08	0.18	0.01	0.00	0.00	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	54	-0	-55	0	0	0	-645	--	--	16.08	16.08	0.18	0.01	0.00	0.00	0.00	0.00	20.9
2	54	-0	-39	0	0	0	-546	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
3	54	-0	-4	0	0	0	-498	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
4	54	-0	-80	0	0	0	-495	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
5	54	-0	-45	0	0	0	-447	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
6	54	-0	-94	0	0	0	-584	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
7	54	-0	22	0	0	0	-436	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
8	54	-0	-106	0	0	0	-569	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
9	54	-0	9	0	0	0	-414	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
10	54	-0	-39	0	0	0	-546	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
11	54	-0	-4	0	0	0	-498	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
12	54	-0	-80	0	0	0	-495	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
13	54	-0	-45	0	0	0	-447	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
14	54	-0	-94	0	0	0	-584	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
15	54	-0	22	0	0	0	-436	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
16	54	-0	-106	0	0	0	-569	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
17	54	-0	9	0	0	0	-414	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
18	54	-0	77	0	0	0	-933	--	--	16.08	16.08	0.18	0.02	0.00	0.00	0.00	0.00	20.9
19	54	-0	-56	0	0	0	-731	--	--	16.08	16.08	0.18	0.01	0.00	0.00	0.00	0.00	20.9
20	54	-0	55	0	0	0	-729	--	--	16.08	16.08	0.18	0.01	0.00	0.00	0.00	0.00	20.9
37	54	-0	110	0	0	0	-947	--	--	16.08	16.08	0.18	0.02	0.00	0.01	0.00	0.00	20.9
38	54	-0	-111	0	0	0	-620	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9
39	54	-0	73	0	0	0	-606	--	--	16.08	16.08	0.18	0.01	0.00	0.00	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 129 NI 1806 NF 1805 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm

1	0	-0	-1093	0	0	0	-906	--	--	16.08	16.08	0.18	0.02	0.01	0.07	0.00	0.00	20.9
2	0	-0	-874	0	0	0	-761	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
3	0	-0	-809	0	0	0	-704	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
4	0	-0	-872	0	0	0	-689	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
5	0	-0	-807	0	0	0	-632	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
6	0	-0	-950	0	0	0	-802	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
7	0	-0	-732	0	0	0	-613	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
8	0	-0	-949	0	0	0	-780	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
9	0	-0	-732	0	0	0	-591	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
10	0	-0	-874	0	0	0	-761	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
11	0	-0	-809	0	0	0	-704	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
12	0	-0	-872	0	0	0	-689	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
13	0	-0	-807	0	0	0	-632	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
14	0	-0	-950	0	0	0	-802	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
15	0	-0	-732	0	0	0	-613	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
16	0	-0	-949	0	0	0	-780	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
17	0	-0	-732	0	0	0	-591	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
18	0	-0	-1151	0	0	0	-1249	--	--	16.08	16.08	0.18	0.02	0.01	0.07	0.00	0.00	20.9
19	0	-0	-1153	0	0	0	-1019	--	--	16.08	16.08	0.18	0.02	0.01	0.07	0.00	0.00	20.9
20	0	-0	-1028	0	0	0	-988	--	--	16.08	16.08	0.18	0.02	0.01	0.06	0.00	0.00	20.9
37	0	-0	-1110	0	0	0	-1247	--	--	16.08	16.08	0.18	0.02	0.01	0.07	0.00	0.00	20.9
38	0	-0	-1114	0	0	0	-863	--	--	16.08	16.08	0.18	0.01	0.01	0.07	0.00	0.00	20.9
39	0	-0	-906	0	0	0	-813	--	--	16.08	16.08	0.18	0.01	0.01	0.06	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-1093	0	0	0	-906	--	--	16.08	16.08	0.18	0.02	0.01	0.07	0.00	0.00	20.9
2	27	-0	-874	0	0	0	-761	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
3	27	-0	-809	0	0	0	-704	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
4	27	-0	-872	0	0	0	-689	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
5	27	-0	-807	0	0	0	-632	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
6	27	-0	-950	0	0	0	-802	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
7	27	-0	-732	0	0	0	-613	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
8	27	-0	-949	0	0	0	-780	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
9	27	-0	-732	0	0	0	-591	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
10	27	-0	-874	0	0	0	-761	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
11	27	-0	-809	0	0	0	-704	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
12	27	-0	-872	0	0	0	-689	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9

13	27	-0	-807	0	0	0	-632	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
14	27	-0	-950	0	0	0	-802	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
15	27	-0	-732	0	0	0	-613	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
16	27	-0	-949	0	0	0	-780	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
17	27	-0	-732	0	0	0	-591	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
18	27	-0	-1151	0	0	0	-1249	--	--	16.08	16.08	0.18	0.02	0.01	0.07	0.00	0.00	20.9
19	27	-0	-1153	0	0	0	-1019	--	--	16.08	16.08	0.18	0.02	0.01	0.07	0.00	0.00	20.9
20	27	-0	-1028	0	0	0	-988	--	--	16.08	16.08	0.18	0.02	0.01	0.06	0.00	0.00	20.9
37	27	-0	-1110	0	0	0	-1247	--	--	16.08	16.08	0.18	0.02	0.01	0.07	0.00	0.00	20.9
38	27	-0	-1114	0	0	0	-863	--	--	16.08	16.08	0.18	0.01	0.01	0.07	0.00	0.00	20.9
39	27	-0	-906	0	0	0	-813	--	--	16.08	16.08	0.18	0.01	0.01	0.06	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	54	-0	-1093	0	0	0	-906	--	--	16.08	16.08	0.18	0.02	0.01	0.07	0.00	0.00	20.9
2	54	-0	-874	0	0	0	-761	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
3	54	-0	-809	0	0	0	-704	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
4	54	-0	-872	0	0	0	-689	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
5	54	-0	-807	0	0	0	-632	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
6	54	-0	-950	0	0	0	-802	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
7	54	-0	-732	0	0	0	-613	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
8	54	-0	-949	0	0	0	-780	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
9	54	-0	-732	0	0	0	-591	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
10	54	-0	-874	0	0	0	-761	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
11	54	-0	-809	0	0	0	-704	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
12	54	-0	-872	0	0	0	-689	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
13	54	-0	-807	0	0	0	-632	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
14	54	-0	-950	0	0	0	-802	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
15	54	-0	-732	0	0	0	-613	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
16	54	-0	-949	0	0	0	-780	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
17	54	-0	-732	0	0	0	-591	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
18	54	-0	-1151	0	0	0	-1249	--	--	16.08	16.08	0.18	0.02	0.01	0.07	0.00	0.00	20.9
19	54	-0	-1153	0	0	0	-1019	--	--	16.08	16.08	0.18	0.02	0.01	0.07	0.00	0.00	20.9
20	54	-0	-1028	0	0	0	-988	--	--	16.08	16.08	0.18	0.02	0.01	0.06	0.00	0.00	20.9
37	54	-0	-1110	0	0	0	-1247	--	--	16.08	16.08	0.18	0.02	0.01	0.07	0.00	0.00	20.9
38	54	-0	-1114	0	0	0	-863	--	--	16.08	16.08	0.18	0.01	0.01	0.07	0.00	0.00	20.9
39	54	-0	-906	0	0	0	-813	--	--	16.08	16.08	0.18	0.01	0.01	0.06	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 130 NI 1802 NF 1806 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-2025	0	0	0	233	--	--	16.08	16.08	0.00	0.00	0.02	0.13	0.00	0.00	20.9
2	0	-0	-1609	0	0	0	140	--	--	16.08	16.08	0.10	0.00	0.01	0.10	0.00	0.00	20.9
3	0	-0	-1543	0	0	0	157	--	--	16.08	16.08	0.10	0.00	0.01	0.10	0.00	0.00	20.9
4	0	-0	-1572	0	0	0	202	--	--	16.08	16.08	0.10	0.00	0.01	0.10	0.00	0.00	20.9
5	0	-0	-1506	0	0	0	219	--	--	16.08	16.08	0.10	0.00	0.01	0.09	0.00	0.00	20.9
6	0	-0	-1672	0	0	0	142	--	--	16.08	16.08	0.10	0.00	0.01	0.10	0.00	0.00	20.9
7	0	-0	-1454	0	0	0	198	--	--	16.08	16.08	0.10	0.00	0.01	0.09	0.00	0.00	20.9
8	0	-0	-1661	0	0	0	161	--	--	16.08	16.08	0.10	0.00	0.01	0.10	0.00	0.00	20.9
9	0	-0	-1443	0	0	0	217	--	--	16.08	16.08	0.10	0.00	0.01	0.09	0.00	0.00	20.9
10	0	-0	-1609	0	0	0	140	--	--	16.08	16.08	0.10	0.00	0.01	0.10	0.00	0.00	20.9
11	0	-0	-1543	0	0	0	157	--	--	16.08	16.08	0.10	0.00	0.01	0.10	0.00	0.00	20.9
12	0	-0	-1572	0	0	0	202	--	--	16.08	16.08	0.10	0.00	0.01	0.10	0.00	0.00	20.9
13	0	-0	-1506	0	0	0	219	--	--	16.08	16.08	0.10	0.00	0.01	0.09	0.00	0.00	20.9
14	0	-0	-1672	0	0	0	142	--	--	16.08	16.08	0.10	0.00	0.01	0.10	0.00	0.00	20.9
15	0	-0	-1454	0	0	0	198	--	--	16.08	16.08	0.10	0.00	0.01	0.09	0.00	0.00	20.9
16	0	-0	-1661	0	0	0	161	--	--	16.08	16.08	0.10	0.00	0.01	0.10	0.00	0.00	20.9
17	0	-0	-1443	0	0	0	217	--	--	16.08	16.08	0.10	0.00	0.01	0.09	0.00	0.00	20.9
18	0	-0	-2187	0	0	0	-1225	--	--	16.08	16.08	0.18	0.02	0.02	0.14	0.00	0.00	20.9
19	0	-0	-2096	0	0	0	159	--	--	16.08	16.08	0.00	0.00	0.02	0.13	0.00	0.00	20.9
20	0	-0	-2019	0	0	0	129	--	--	16.08	16.08	0.00	0.00	0.02	0.13	0.00	0.00	20.9
37	0	-0	-2149	0	0	0	-1231	--	--	16.08	16.08	0.18	0.02	0.02	0.13	0.00	0.00	20.9
38	0	-0	-1997	0	0	0	274	--	--	16.08	16.08	0.00	0.00	0.02	0.13	0.00	0.00	20.9
39	0	-0	-1869	0	0	0	223	--	--	16.08	16.08	0.00	0.00	0.02	0.12	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-2025	0	0	0	-851	--	--	16.08	16.08	0.18	0.01	0.02	0.13	0.00	0.00	20.9
2	27	-0	-1609	0	0	0	-722	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
3	27	-0	-1543	0	0	0	-670	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
4	27	-0	-1572	0	0	0	-639	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
5	27	-0	-1506	0	0	0	-588	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
6	27	-0	-1672	0	0	0	-753	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
7	27	-0	-1454	0	0	0	-581	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
8	27	-0	-1661	0	0	0	-729	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
9	27	-0	-1443	0	0	0	-556	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
10	27	-0	-1609	0	0	0	-722	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
11	27	-0	-1543	0	0	0	-670	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
12	27	-0	-1572	0	0	0	-639	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
13	27	-0	-1506	0	0	0	-588	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
14	27	-0	-1672	0	0	0	-753	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
15	27	-0	-1454	0	0	0	-581	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
16	27	-0	-1661	0	0	0	-729	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
17	27	-0	-1443	0	0	0	-556	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
18	27	-0	-2187	0	0	0	-1225	--	--	16.08	16.08	0.18	0.02	0.02	0.14	0.00	0.00	20.9
19	27	-0	-2096	0	0	0	-963	--	--	16.08	16.08	0.18	0.02	0.02	0.13	0.00	0.00	20.9
20	27	-0	-2019	0	0	0	-953	--	--	16.08	16.08	0.18	0.02	0.02	0.13	0.00	0.00	20.9
37	27	-0	-2149	0	0	0	-1231	--	--	16.08	16.08	0.18	0.02	0.02	0.13	0.00	0.00	20.9
38	27	-0	-1997	0	0	0	-796	--	--	16.08	16.08	0.18	0.01	0.02	0.13	0.00	0.00	20.9
39	27	-0	-1869	0	0	0	-778	--	--	16.08	16.08	0.18	0.01	0.02	0.12	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	54	-0	-2025	0	0	0	-851	--	--	16.08	16.08	0.18	0.01	0.02	0.13	0.00	0.00	20.9
2	54	-0	-1609	0	0	0	-722	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
3	54	-0	-1543	0	0	0	-670	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
4	54	-0	-1572	0	0	0	-639	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
5	54	-0	-1506	0	0	0	-588	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
6	54	-0	-1672	0	0	0	-753	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
7	54	-0	-1454	0	0	0	-581	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
8	54	-0	-1661	0	0	0	-729	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9

9	54	-0	-1443	0	0	0	-556	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
10	54	-0	-1609	0	0	0	-722	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
11	54	-0	-1543	0	0	0	-670	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
12	54	-0	-1572	0	0	0	-639	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
13	54	-0	-1506	0	0	0	-588	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
14	54	-0	-1672	0	0	0	-753	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
15	54	-0	-1454	0	0	0	-581	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
16	54	-0	-1661	0	0	0	-729	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
17	54	-0	-1443	0	0	0	-556	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
18	54	-0	-2187	0	0	0	-1225	--	--	16.08	16.08	0.18	0.02	0.02	0.14	0.00	0.00	20.9
19	54	-0	-2096	0	0	0	-963	--	--	16.08	16.08	0.18	0.02	0.02	0.13	0.00	0.00	20.9
20	54	-0	-2019	0	0	0	-953	--	--	16.08	16.08	0.18	0.02	0.02	0.13	0.00	0.00	20.9
37	54	-0	-2149	0	0	0	-1231	--	--	16.08	16.08	0.18	0.02	0.02	0.13	0.00	0.00	20.9
38	54	-0	-1997	0	0	0	-796	--	--	16.08	16.08	0.18	0.01	0.02	0.13	0.00	0.00	20.9
39	54	-0	-1869	0	0	0	-778	--	--	16.08	16.08	0.18	0.01	0.02	0.12	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 131 NI 1803 NF 1802 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-2570	0	0	0	735	--	--	16.08	16.08	0.00	0.01	0.02	0.16	0.00	0.00	20.9
2	0	-0	-2019	0	0	0	519	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
3	0	-0	-1995	0	0	0	556	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
4	0	-0	-1959	0	0	0	574	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
5	0	-0	-1935	0	0	0	612	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
6	0	-0	-2026	0	0	0	494	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
7	0	-0	-1946	0	0	0	620	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
8	0	-0	-2008	0	0	0	511	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
9	0	-0	-1928	0	0	0	636	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
10	0	-0	-2019	0	0	0	519	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
11	0	-0	-1995	0	0	0	556	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
12	0	-0	-1959	0	0	0	574	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
13	0	-0	-1935	0	0	0	612	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
14	0	-0	-2026	0	0	0	494	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
15	0	-0	-1946	0	0	0	620	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
16	0	-0	-2008	0	0	0	511	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
17	0	-0	-1928	0	0	0	636	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
18	0	-0	-2700	0	0	0	404	--	--	16.08	16.08	0.00	0.01	0.02	0.17	0.00	0.00	20.9
19	0	-0	-2567	0	0	0	615	--	--	16.08	16.08	0.00	0.01	0.02	0.16	0.00	0.00	20.9
20	0	-0	-2620	0	0	0	650	--	--	16.08	16.08	0.00	0.01	0.02	0.16	0.00	0.00	20.9
37	0	-0	-2687	0	0	0	385	--	--	16.08	16.08	0.00	0.01	0.02	0.17	0.00	0.00	20.9
38	0	-0	-2466	0	0	0	736	--	--	16.08	16.08	0.00	0.01	0.02	0.15	0.00	0.00	20.9
39	0	-0	-2555	0	0	0	795	--	--	16.08	16.08	0.00	0.01	0.02	0.16	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-2570	0	0	0	735	--	--	16.08	16.08	0.00	0.01	0.02	0.16	0.00	0.00	20.9
2	27	-0	-2019	0	0	0	-563	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
3	27	-0	-1995	0	0	0	556	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
4	27	-0	-1959	0	0	0	574	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
5	27	-0	-1935	0	0	0	612	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
6	27	-0	-2026	0	0	0	-591	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
7	27	-0	-1946	0	0	0	620	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
8	27	-0	-2008	0	0	0	-565	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
9	27	-0	-1928	0	0	0	636	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
10	27	-0	-2019	0	0	0	-563	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
11	27	-0	-1995	0	0	0	556	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
12	27	-0	-1959	0	0	0	574	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
13	27	-0	-1935	0	0	0	612	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
14	27	-0	-2026	0	0	0	-591	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
15	27	-0	-1946	0	0	0	620	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
16	27	-0	-2008	0	0	0	-565	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
17	27	-0	-1928	0	0	0	636	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
18	27	-0	-2700	0	0	0	-1042	--	--	16.08	16.08	0.18	0.02	0.02	0.17	0.00	0.00	20.9
19	27	-0	-2567	0	0	0	-760	--	--	16.08	16.08	0.18	0.01	0.02	0.16	0.00	0.00	20.9
20	27	-0	-2620	0	0	0	-754	--	--	16.08	16.08	0.18	0.01	0.02	0.16	0.00	0.00	20.9
37	27	-0	-2687	0	0	0	-1055	--	--	16.08	16.08	0.18	0.02	0.02	0.17	0.00	0.00	20.9
38	27	-0	-2466	0	0	0	736	--	--	16.08	16.08	0.00	0.01	0.02	0.15	0.00	0.00	20.9
39	27	-0	-2555	0	0	0	795	--	--	16.08	16.08	0.00	0.01	0.02	0.16	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	54	-0	-2570	0	0	0	-642	--	--	16.08	16.08	0.18	0.01	0.02	0.16	0.00	0.00	20.9
2	54	-0	-2019	0	0	0	-563	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
3	54	-0	-1995	0	0	0	-513	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
4	54	-0	-1959	0	0	0	-475	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
5	54	-0	-1935	0	0	0	-425	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
6	54	-0	-2026	0	0	0	-591	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
7	54	-0	-1946	0	0	0	-423	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
8	54	-0	-2008	0	0	0	-565	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
9	54	-0	-1928	0	0	0	-397	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
10	54	-0	-2019	0	0	0	-563	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
11	54	-0	-1995	0	0	0	-513	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
12	54	-0	-1959	0	0	0	-475	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
13	54	-0	-1935	0	0	0	-425	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
14	54	-0	-2026	0	0	0	-591	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
15	54	-0	-1946	0	0	0	-423	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
16	54	-0	-2008	0	0	0	-565	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
17	54	-0	-1928	0	0	0	-397	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
18	54	-0	-2700	0	0	0	-1042	--	--	16.08	16.08	0.18	0.02	0.02	0.17	0.00	0.00	20.9
19	54	-0	-2567	0	0	0	-760	--	--	16.08	16.08	0.18	0.01	0.02	0.16	0.00	0.00	20.9
20	54	-0	-2620	0	0	0	-754	--	--	16.08	16.08	0.18	0.01	0.02	0.16	0.00	0.00	20.9
37	54	-0	-2687	0	0	0	-1055	--	--	16.08	16.08	0.18	0.02	0.02	0.17	0.00	0.00	20.9
38	54	-0	-2466	0	0	0	-585	--	--	16.08	16.08	0.18	0.01	0.02	0.15	0.00	0.00	20.9
39	54	-0	-2555	0	0	0	-574	--	--	16.08	16.08	0.18	0.01	0.02	0.16	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 132 NI 1798 NF 1803 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice resistenza			aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-2444	0	0	0	1225	--	--	16.08	16.08	0.00	0.02	0.02	0.15	0.00	0.00	20.9
2	0	-0	-1928	0	0	0	908	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
3	0	-0	-1931	0	0	0	949	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
4	0	-0	-1828	0	0	0	935	--	--	16.08	16.08	0.10	0.02	0.02	0.11	0.00	0.00	20.9
5	0	-0	-1832	0	0	0	976	--	--	16.08	16.08	0.10	0.02	0.02	0.11	0.00	0.00	20.9
6	0	-0	-1889	0	0	0	870	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
7	0	-0	-1901	0	0	0	1006	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
8	0	-0	-1859	0	0	0	878	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
9	0	-0	-1871	0	0	0	1014	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
10	0	-0	-1928	0	0	0	908	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
11	0	-0	-1931	0	0	0	949	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
12	0	-0	-1828	0	0	0	935	--	--	16.08	16.08	0.10	0.02	0.02	0.11	0.00	0.00	20.9
13	0	-0	-1832	0	0	0	976	--	--	16.08	16.08	0.10	0.02	0.02	0.11	0.00	0.00	20.9
14	0	-0	-1889	0	0	0	870	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
15	0	-0	-1901	0	0	0	1006	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
16	0	-0	-1859	0	0	0	878	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
17	0	-0	-1871	0	0	0	1014	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
18	0	-0	-2554	0	0	0	921	--	--	16.08	16.08	0.00	0.02	0.02	0.16	0.00	0.00	20.9
19	0	-0	-2331	0	0	0	1065	--	--	16.08	16.08	0.00	0.02	0.02	0.15	0.00	0.00	20.9
20	0	-0	-2500	0	0	0	1151	--	--	16.08	16.08	0.00	0.02	0.02	0.16	0.00	0.00	20.9
37	0	-0	-2597	0	0	0	921	--	--	16.08	16.08	0.00	0.02	0.02	0.16	0.00	0.00	20.9
38	0	-0	-2225	0	0	0	1161	--	--	16.08	16.08	0.00	0.02	0.02	0.14	0.00	0.00	20.9
39	0	-0	-2506	0	0	0	1304	--	--	16.08	16.08	0.00	0.02	0.02	0.16	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-2444	0	0	0	1225	--	--	16.08	16.08	0.00	0.02	0.02	0.15	0.00	0.00	20.9
2	27	-0	-1928	0	0	0	908	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
3	27	-0	-1931	0	0	0	949	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
4	27	-0	-1828	0	0	0	935	--	--	16.08	16.08	0.10	0.02	0.02	0.11	0.00	0.00	20.9
5	27	-0	-1832	0	0	0	976	--	--	16.08	16.08	0.10	0.02	0.02	0.11	0.00	0.00	20.9
6	27	-0	-1889	0	0	0	870	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
7	27	-0	-1901	0	0	0	1006	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
8	27	-0	-1859	0	0	0	878	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
9	27	-0	-1871	0	0	0	1014	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
10	27	-0	-1928	0	0	0	908	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
11	27	-0	-1931	0	0	0	949	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
12	27	-0	-1828	0	0	0	935	--	--	16.08	16.08	0.10	0.02	0.02	0.11	0.00	0.00	20.9
13	27	-0	-1832	0	0	0	976	--	--	16.08	16.08	0.10	0.02	0.02	0.11	0.00	0.00	20.9
14	27	-0	-1889	0	0	0	870	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
15	27	-0	-1901	0	0	0	1006	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
16	27	-0	-1859	0	0	0	878	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
17	27	-0	-1871	0	0	0	1014	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
18	27	-0	-2554	0	0	0	921	--	--	16.08	16.08	0.00	0.02	0.02	0.16	0.00	0.00	20.9
19	27	-0	-2331	0	0	0	1065	--	--	16.08	16.08	0.00	0.02	0.02	0.15	0.00	0.00	20.9
20	27	-0	-2500	0	0	0	1151	--	--	16.08	16.08	0.00	0.02	0.02	0.16	0.00	0.00	20.9
37	27	-0	-2597	0	0	0	921	--	--	16.08	16.08	0.00	0.02	0.02	0.16	0.00	0.00	20.9
38	27	-0	-2225	0	0	0	1161	--	--	16.08	16.08	0.00	0.02	0.02	0.14	0.00	0.00	20.9
39	27	-0	-2506	0	0	0	1304	--	--	16.08	16.08	0.00	0.02	0.02	0.16	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	54	-0	-2444	0	0	0	-84	--	--	16.08	16.08	0.18	0.00	0.02	0.15	0.00	0.00	20.9
2	54	-0	-1928	0	0	0	-124	--	--	16.08	16.08	0.29	0.00	0.02	0.12	0.00	0.00	20.9
3	54	-0	-1931	0	0	0	-86	--	--	16.08	16.08	0.29	0.00	0.02	0.12	0.00	0.00	20.9
4	54	-0	-1828	0	0	0	-44	--	--	16.08	16.08	0.29	0.00	0.02	0.11	0.00	0.00	20.9
5	54	-0	-1832	0	0	0	-6	--	--	16.08	16.08	0.29	0.00	0.02	0.11	0.00	0.00	20.9
6	54	-0	-1889	0	0	0	-142	--	--	16.08	16.08	0.29	0.00	0.02	0.12	0.00	0.00	20.9
7	54	-0	-1901	0	0	0	-12	--	--	16.08	16.08	0.29	0.00	0.02	0.12	0.00	0.00	20.9
8	54	-0	-1859	0	0	0	-118	--	--	16.08	16.08	0.29	0.00	0.02	0.12	0.00	0.00	20.9
9	54	-0	-1871	0	0	0	12	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
10	54	-0	-1928	0	0	0	-124	--	--	16.08	16.08	0.29	0.00	0.02	0.12	0.00	0.00	20.9
11	54	-0	-1931	0	0	0	-86	--	--	16.08	16.08	0.29	0.00	0.02	0.12	0.00	0.00	20.9
12	54	-0	-1828	0	0	0	-44	--	--	16.08	16.08	0.29	0.00	0.02	0.11	0.00	0.00	20.9
13	54	-0	-1832	0	0	0	-6	--	--	16.08	16.08	0.29	0.00	0.02	0.11	0.00	0.00	20.9
14	54	-0	-1889	0	0	0	-142	--	--	16.08	16.08	0.29	0.00	0.02	0.12	0.00	0.00	20.9
15	54	-0	-1901	0	0	0	-12	--	--	16.08	16.08	0.29	0.00	0.02	0.12	0.00	0.00	20.9
16	54	-0	-1859	0	0	0	-118	--	--	16.08	16.08	0.29	0.00	0.02	0.12	0.00	0.00	20.9
17	54	-0	-1871	0	0	0	12	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
18	54	-0	-2554	0	0	0	-447	--	--	16.08	16.08	0.18	0.01	0.02	0.16	0.00	0.00	20.9
19	54	-0	-2331	0	0	0	-184	--	--	16.08	16.08	0.18	0.00	0.02	0.15	0.00	0.00	20.9
20	54	-0	-2500	0	0	0	-188	--	--	16.08	16.08	0.18	0.00	0.02	0.16	0.00	0.00	20.9
37	54	-0	-2597	0	0	0	-470	--	--	16.08	16.08	0.18	0.01	0.02	0.16	0.00	0.00	20.9
38	54	-0	-2225	0	0	0	-31	--	--	16.08	16.08	0.18	0.00	0.02	0.14	0.00	0.00	20.9
39	54	-0	-2506	0	0	0	-38	--	--	16.08	16.08	0.18	0.00	0.02	0.16	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 133 NI 1789 NF 1798 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice resistenza			aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	1593	0	0	0	231	--	--	16.08	16.08	0.00	0.00	0.01	0.10	0.00	0.00	20.9
2	0	-0	1164	0	0	0	164	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
3	0	-0	1158	0	0	0	191	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
4	0	-0	1293	0	0	0	165	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
5	0	-0	1287	0	0	0	192	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
6	0	-0	1216	0	0	0	133	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
7	0	-0	1196	0	0	0	222	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
8	0	-0	1255	0	0	0	133	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
9	0	-0	1235	0	0	0	223	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
10	0	-0	1164	0	0	0	164	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
11	0	-0	1158	0	0	0	191	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
12	0	-0	1293	0	0	0	165	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
13	0	-0	1287	0	0	0	192	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
14	0	-0	1216	0	0	0	133	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
15	0	-0	1196	0	0	0	222	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
16	0	-0	1255	0	0	0	133	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9

17	0	-0	1235	0	0	0	223	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
18	0	-0	1729	0	0	0	-94	--	--	16.08	16.08	0.18	0.00	0.01	0.11	0.00	0.00	20.9
19	0	-0	2030	0	0	0	-21	--	--	16.08	16.08	0.18	0.00	0.02	0.13	0.00	0.00	20.9
20	0	-0	1819	0	0	0	68	--	--	16.08	16.08	0.00	0.00	0.01	0.11	0.00	0.00	20.9
37	0	-0	1519	0	0	0	-40	--	--	16.08	16.08	0.18	0.00	0.01	0.10	0.00	0.00	20.9
38	0	-0	2021	0	0	0	81	--	--	16.08	16.08	0.00	0.00	0.02	0.13	0.00	0.00	20.9
39	0	-0	1670	0	0	0	230	--	--	16.08	16.08	0.00	0.00	0.01	0.10	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	1593	0	0	0	2361	--	--	16.08	16.08	0.00	0.04	0.01	0.10	0.00	0.00	20.9
2	27	-0	1164	0	0	0	1720	--	--	16.08	16.08	0.10	0.03	0.01	0.07	0.00	0.00	20.9
3	27	-0	1158	0	0	0	1739	--	--	16.08	16.08	0.10	0.03	0.01	0.07	0.00	0.00	20.9
4	27	-0	1293	0	0	0	1893	--	--	16.08	16.08	0.10	0.03	0.01	0.08	0.00	0.00	20.9
5	27	-0	1287	0	0	0	1912	--	--	16.08	16.08	0.10	0.03	0.01	0.08	0.00	0.00	20.9
6	27	-0	1216	0	0	0	1758	--	--	16.08	16.08	0.10	0.03	0.01	0.08	0.00	0.00	20.9
7	27	-0	1196	0	0	0	1821	--	--	16.08	16.08	0.10	0.03	0.01	0.08	0.00	0.00	20.9
8	27	-0	1255	0	0	0	1811	--	--	16.08	16.08	0.10	0.03	0.01	0.08	0.00	0.00	20.9
9	27	-0	1235	0	0	0	1873	--	--	16.08	16.08	0.10	0.03	0.01	0.08	0.00	0.00	20.9
10	27	-0	1164	0	0	0	1720	--	--	16.08	16.08	0.10	0.03	0.01	0.07	0.00	0.00	20.9
11	27	-0	1158	0	0	0	1739	--	--	16.08	16.08	0.10	0.03	0.01	0.07	0.00	0.00	20.9
12	27	-0	1293	0	0	0	1893	--	--	16.08	16.08	0.10	0.03	0.01	0.08	0.00	0.00	20.9
13	27	-0	1287	0	0	0	1912	--	--	16.08	16.08	0.10	0.03	0.01	0.08	0.00	0.00	20.9
14	27	-0	1216	0	0	0	1758	--	--	16.08	16.08	0.10	0.03	0.01	0.08	0.00	0.00	20.9
15	27	-0	1196	0	0	0	1821	--	--	16.08	16.08	0.10	0.03	0.01	0.08	0.00	0.00	20.9
16	27	-0	1255	0	0	0	1811	--	--	16.08	16.08	0.10	0.03	0.01	0.08	0.00	0.00	20.9
17	27	-0	1235	0	0	0	1873	--	--	16.08	16.08	0.10	0.03	0.01	0.08	0.00	0.00	20.9
18	27	-0	1729	0	0	0	2217	--	--	16.08	16.08	0.00	0.04	0.01	0.11	0.00	0.00	20.9
19	27	-0	2030	0	0	0	2692	--	--	16.08	16.08	0.00	0.05	0.02	0.13	0.00	0.00	20.9
20	27	-0	1819	0	0	0	2500	--	--	16.08	16.08	0.00	0.04	0.01	0.11	0.00	0.00	20.9
37	27	-0	1519	0	0	0	1990	--	--	16.08	16.08	0.00	0.03	0.01	0.10	0.00	0.00	20.9
38	27	-0	2021	0	0	0	2782	--	--	16.08	16.08	0.00	0.05	0.02	0.13	0.00	0.00	20.9
39	27	-0	1670	0	0	0	2463	--	--	16.08	16.08	0.00	0.04	0.01	0.10	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	54	-0	1593	0	0	0	1085	--	--	16.08	16.08	0.00	0.02	0.01	0.10	0.00	0.00	20.9
2	54	-0	1164	0	0	0	787	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
3	54	-0	1158	0	0	0	811	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
4	54	-0	1293	0	0	0	858	--	--	16.08	16.08	0.10	0.02	0.01	0.08	0.00	0.00	20.9
5	54	-0	1287	0	0	0	881	--	--	16.08	16.08	0.10	0.02	0.01	0.08	0.00	0.00	20.9
6	54	-0	1216	0	0	0	784	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
7	54	-0	1196	0	0	0	863	--	--	16.08	16.08	0.10	0.02	0.01	0.08	0.00	0.00	20.9
8	54	-0	1255	0	0	0	806	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
9	54	-0	1235	0	0	0	884	--	--	16.08	16.08	0.10	0.02	0.01	0.08	0.00	0.00	20.9
10	54	-0	1164	0	0	0	787	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
11	54	-0	1158	0	0	0	811	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
12	54	-0	1293	0	0	0	858	--	--	16.08	16.08	0.10	0.02	0.01	0.08	0.00	0.00	20.9
13	54	-0	1287	0	0	0	881	--	--	16.08	16.08	0.10	0.02	0.01	0.08	0.00	0.00	20.9
14	54	-0	1216	0	0	0	784	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
15	54	-0	1196	0	0	0	863	--	--	16.08	16.08	0.10	0.02	0.01	0.08	0.00	0.00	20.9
16	54	-0	1255	0	0	0	806	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
17	54	-0	1235	0	0	0	884	--	--	16.08	16.08	0.10	0.02	0.01	0.08	0.00	0.00	20.9
18	54	-0	1729	0	0	0	832	--	--	16.08	16.08	0.00	0.01	0.01	0.11	0.00	0.00	20.9
19	54	-0	2030	0	0	0	1066	--	--	16.08	16.08	0.00	0.02	0.02	0.13	0.00	0.00	20.9
20	54	-0	1819	0	0	0	1043	--	--	16.08	16.08	0.00	0.02	0.01	0.11	0.00	0.00	20.9
37	54	-0	1519	0	0	0	774	--	--	16.08	16.08	0.00	0.01	0.01	0.10	0.00	0.00	20.9
38	54	-0	2021	0	0	0	1164	--	--	16.08	16.08	0.00	0.02	0.02	0.13	0.00	0.00	20.9
39	54	-0	1670	0	0	0	1125	--	--	16.08	16.08	0.00	0.02	0.01	0.10	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 134 NI 1777 NF 1789 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	1497	0	0	0	-63	--	--	16.08	16.08	0.18	0.00	0.01	0.09	0.00	0.00	20.9
2	0	-0	1031	0	0	0	-28	--	--	16.08	16.08	0.29	0.00	0.01	0.06	0.00	0.00	20.9
3	0	-0	1065	0	0	0	-17	--	--	16.08	16.08	0.29	0.00	0.01	0.07	0.00	0.00	20.9
4	0	-0	1237	0	0	0	-80	--	--	16.08	16.08	0.29	0.00	0.01	0.08	0.00	0.00	20.9
5	0	-0	1272	0	0	0	-69	--	--	16.08	16.08	0.29	0.00	0.01	0.08	0.00	0.00	20.9
6	0	-0	1062	0	0	0	-60	--	--	16.08	16.08	0.29	0.00	0.01	0.07	0.00	0.00	20.9
7	0	-0	1178	0	0	0	-22	--	--	16.08	16.08	0.29	0.00	0.01	0.07	0.00	0.00	20.9
8	0	-0	1124	0	0	0	-75	--	--	16.08	16.08	0.29	0.00	0.01	0.07	0.00	0.00	20.9
9	0	-0	1240	0	0	0	-37	--	--	16.08	16.08	0.29	0.00	0.01	0.08	0.00	0.00	20.9
10	0	-0	1031	0	0	0	-28	--	--	16.08	16.08	0.29	0.00	0.01	0.06	0.00	0.00	20.9
11	0	-0	1065	0	0	0	-17	--	--	16.08	16.08	0.29	0.00	0.01	0.07	0.00	0.00	20.9
12	0	-0	1237	0	0	0	-80	--	--	16.08	16.08	0.29	0.00	0.01	0.08	0.00	0.00	20.9
13	0	-0	1272	0	0	0	-69	--	--	16.08	16.08	0.29	0.00	0.01	0.08	0.00	0.00	20.9
14	0	-0	1062	0	0	0	-60	--	--	16.08	16.08	0.29	0.00	0.01	0.07	0.00	0.00	20.9
15	0	-0	1178	0	0	0	-22	--	--	16.08	16.08	0.29	0.00	0.01	0.07	0.00	0.00	20.9
16	0	-0	1124	0	0	0	-75	--	--	16.08	16.08	0.29	0.00	0.01	0.07	0.00	0.00	20.9
17	0	-0	1240	0	0	0	-37	--	--	16.08	16.08	0.29	0.00	0.01	0.08	0.00	0.00	20.9
18	0	-0	1388	0	0	0	-327	--	--	16.08	16.08	0.18	0.01	0.01	0.09	0.00	0.00	20.9
19	0	-0	1914	0	0	0	-394	--	--	16.08	16.08	0.18	0.01	0.02	0.12	0.00	0.00	20.9
20	0	-0	1707	0	0	0	-269	--	--	16.08	16.08	0.18	0.00	0.01	0.11	0.00	0.00	20.9
37	0	-0	1142	0	0	0	-219	--	--	16.08	16.08	0.18	0.00	0.01	0.07	0.00	0.00	20.9
38	0	-0	2018	0	0	0	-331	--	--	16.08	16.08	0.18	0.01	0.02	0.13	0.00	0.00	20.9
39	0	-0	1673	0	0	0	-122	--	--	16.08	16.08	0.18	0.00	0.01	0.10	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	1497	0	0	0	1938	--	--	16.08	16.08	0.00	0.03	0.01	0.09	0.00	0.00	20.9
2	27	-0	1031	0	0	0	1350	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9
3	27	-0	1065	0	0	0	1407	--	--	16.08	16.08	0.10	0.02	0.01	0.07	0.00	0.00	20.9
4	27	-0	1237	0	0	0	1573	--	--	16.08	16.08	0.10	0.03	0.01	0.08	0.00	0.00	20.9
5	27	-0	1272	0	0	0	1631	--	--	16.08	16.08	0.10	0.03	0.01	0.08	0.00	0.00	20.9
6	27	-0	1062	0	0	0	1360	--	--	16.08	16.08	0.10	0.02	0.01	0.07	0.00	0.00	20.9
7	27	-0	1178	0	0	0	1553	--	--	16.08	16.08	0.10	0.03	0.01	0.07	0.00	0.00	20.9
8	27	-0	1124	0	0	0	1427	--	--	16.08	16.08	0.10	0.03	0.01	0.07	0.00	0.00	20.9
9	27	-0	1240	0	0	0	1620	--	--	16.08	16.08	0.10	0.03	0.01	0.08	0.00	0.00	20.9
10	27	-0	1031	0	0	0	1350	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9
11	27	-0	1065	0	0	0	1407	--	--	16.08	16.08	0.10	0.02	0.01	0.07	0.00	0.00	20.9
12	27	-0	1237	0	0	0	1573	--	--	16.08	16.08	0.10	0.03	0.01	0.08	0.00	0.00	20.9

13	27	-0	1272	0	0	0	1631	--	--	16.08	16.08	0.10	0.03	0.01	0.08	0.00	0.00	20.9
14	27	-0	1062	0	0	0	1360	--	--	16.08	16.08	0.10	0.02	0.01	0.07	0.00	0.00	20.9
15	27	-0	1178	0	0	0	1553	--	--	16.08	16.08	0.10	0.03	0.01	0.07	0.00	0.00	20.9
16	27	-0	1124	0	0	0	1427	--	--	16.08	16.08	0.10	0.03	0.01	0.07	0.00	0.00	20.9
17	27	-0	1240	0	0	0	1620	--	--	16.08	16.08	0.10	0.03	0.01	0.08	0.00	0.00	20.9
18	27	-0	1388	0	0	0	1528	--	--	16.08	16.08	0.00	0.03	0.01	0.09	0.00	0.00	20.9
19	27	-0	1914	0	0	0	2164	--	--	16.08	16.08	0.00	0.04	0.02	0.12	0.00	0.00	20.9
20	27	-0	1707	0	0	0	2013	--	--	16.08	16.08	0.00	0.03	0.01	0.11	0.00	0.00	20.9
37	27	-0	1142	0	0	0	1307	--	--	16.08	16.08	0.00	0.02	0.01	0.07	0.00	0.00	20.9
38	27	-0	2018	0	0	0	2366	--	--	16.08	16.08	0.00	0.04	0.02	0.13	0.00	0.00	20.9
39	27	-0	1673	0	0	0	2114	--	--	16.08	16.08	0.00	0.04	0.01	0.10	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	54	-0	1497	0	0	0	738	--	--	16.08	16.08	0.00	0.01	0.01	0.09	0.00	0.00	20.9
2	54	-0	1031	0	0	0	524	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
3	54	-0	1065	0	0	0	554	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
4	54	-0	1237	0	0	0	582	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
5	54	-0	1272	0	0	0	612	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
6	54	-0	1062	0	0	0	509	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
7	54	-0	1178	0	0	0	609	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
8	54	-0	1124	0	0	0	527	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
9	54	-0	1240	0	0	0	627	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
10	54	-0	1031	0	0	0	524	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
11	54	-0	1065	0	0	0	554	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
12	54	-0	1237	0	0	0	582	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
13	54	-0	1272	0	0	0	612	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
14	54	-0	1062	0	0	0	509	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
15	54	-0	1178	0	0	0	609	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
16	54	-0	1124	0	0	0	527	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
17	54	-0	1240	0	0	0	627	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
18	54	-0	1388	0	0	0	416	--	--	16.08	16.08	0.00	0.01	0.01	0.09	0.00	0.00	20.9
19	54	-0	1914	0	0	0	631	--	--	16.08	16.08	0.00	0.01	0.02	0.12	0.00	0.00	20.9
20	54	-0	1707	0	0	0	645	--	--	16.08	16.08	0.00	0.01	0.01	0.11	0.00	0.00	20.9
37	54	-0	1142	0	0	0	393	--	--	16.08	16.08	0.00	0.01	0.01	0.07	0.00	0.00	20.9
38	54	-0	2018	0	0	0	750	--	--	16.08	16.08	0.00	0.01	0.02	0.13	0.00	0.00	20.9
39	54	-0	1673	0	0	0	774	--	--	16.08	16.08	0.00	0.01	0.01	0.10	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 135 NI 1787 NF 1777 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--	--	--	--	--	--	--	--	--	--	--		--	--	--	--	--	--
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	576	0	0	0	-37	--	--	16.08	16.08	0.18	0.00	0.00	0.04	0.00	0.00	20.9
2	0	-0	249	0	0	0	28	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
3	0	-0	339	0	0	0	31	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
4	0	-0	548	0	0	0	-89	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
5	0	-0	638	0	0	0	-85	--	--	16.08	16.08	0.29	0.00	0.01	0.04	0.00	0.00	20.9
6	0	-0	248	0	0	0	-17	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
7	0	-0	548	0	0	0	-6	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
8	0	-0	338	0	0	0	-51	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
9	0	-0	638	0	0	0	-41	--	--	16.08	16.08	0.29	0.00	0.01	0.04	0.00	0.00	20.9
10	0	-0	249	0	0	0	28	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
11	0	-0	339	0	0	0	31	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
12	0	-0	548	0	0	0	-89	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
13	0	-0	638	0	0	0	-85	--	--	16.08	16.08	0.29	0.00	0.01	0.04	0.00	0.00	20.9
14	0	-0	248	0	0	0	-17	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
15	0	-0	548	0	0	0	-6	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
16	0	-0	338	0	0	0	-51	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
17	0	-0	638	0	0	0	-41	--	--	16.08	16.08	0.29	0.00	0.01	0.04	0.00	0.00	20.9
18	0	-0	103	0	0	0	-208	--	--	16.08	16.08	0.18	0.00	0.00	0.01	0.00	0.00	20.9
19	0	-0	895	0	0	0	-440	--	--	16.08	16.08	0.18	0.01	0.01	0.06	0.00	0.00	20.9
20	0	-0	708	0	0	0	-250	--	--	16.08	16.08	0.18	0.00	0.01	0.04	0.00	0.00	20.9
37	0	-0	-152	0	0	0	-128	--	--	16.08	16.08	0.18	0.00	0.00	0.01	0.00	0.00	20.9
38	0	-0	1168	0	0	0	-434	--	--	16.08	16.08	0.18	0.01	0.01	0.07	0.00	0.00	20.9
39	0	-0	857	0	0	0	-117	--	--	16.08	16.08	0.18	0.00	0.01	0.05	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	576	0	0	0	733	--	--	16.08	16.08	0.00	0.01	0.00	0.04	0.00	0.00	20.9
2	27	-0	249	0	0	0	360	--	--	16.08	16.08	0.10	0.01	0.00	0.02	0.00	0.00	20.9
3	27	-0	339	0	0	0	484	--	--	16.08	16.08	0.10	0.01	0.00	0.02	0.00	0.00	20.9
4	27	-0	548	0	0	0	643	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
5	27	-0	638	0	0	0	767	--	--	16.08	16.08	0.10	0.01	0.01	0.04	0.00	0.00	20.9
6	27	-0	248	0	0	0	316	--	--	16.08	16.08	0.10	0.01	0.00	0.02	0.00	0.00	20.9
7	27	-0	548	0	0	0	727	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
8	27	-0	338	0	0	0	400	--	--	16.08	16.08	0.10	0.01	0.00	0.02	0.00	0.00	20.9
9	27	-0	638	0	0	0	812	--	--	16.08	16.08	0.10	0.01	0.01	0.04	0.00	0.00	20.9
10	27	-0	249	0	0	0	360	--	--	16.08	16.08	0.10	0.01	0.00	0.02	0.00	0.00	20.9
11	27	-0	339	0	0	0	484	--	--	16.08	16.08	0.10	0.01	0.00	0.02	0.00	0.00	20.9
12	27	-0	548	0	0	0	643	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
13	27	-0	638	0	0	0	767	--	--	16.08	16.08	0.10	0.01	0.01	0.04	0.00	0.00	20.9
14	27	-0	248	0	0	0	316	--	--	16.08	16.08	0.10	0.01	0.00	0.02	0.00	0.00	20.9
15	27	-0	548	0	0	0	727	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
16	27	-0	338	0	0	0	400	--	--	16.08	16.08	0.10	0.01	0.00	0.02	0.00	0.00	20.9
17	27	-0	638	0	0	0	812	--	--	16.08	16.08	0.10	0.01	0.01	0.04	0.00	0.00	20.9
18	27	-0	103	0	0	0	-208	--	--	16.08	16.08	0.18	0.00	0.00	0.01	0.00	0.00	20.9
19	27	-0	895	0	0	0	-440	--	--	16.08	16.08	0.18	0.01	0.01	0.06	0.00	0.00	20.9
20	27	-0	708	0	0	0	-250	--	--	16.08	16.08	0.18	0.00	0.01	0.04	0.00	0.00	20.9
37	27	-0	-152	0	0	0	-128	--	--	16.08	16.08	0.18	0.00	0.00	0.01	0.00	0.00	20.9
38	27	-0	1168	0	0	0	-434	--	--	16.08	16.08	0.18	0.01	0.01	0.07	0.00	0.00	20.9
39	27	-0	857	0	0	0	1028	--	--	16.08	16.08	0.00	0.02	0.01	0.05	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	54	-0	576	0	0	0	271	--	--	16.08	16.08	0.00	0.00	0.00	0.04	0.00	0.00	20.9
2	54	-0	249	0	0	0	161	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
3	54	-0	339	0	0	0	212	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
4	54	-0	548	0	0	0	205	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
5	54	-0	638	0	0	0	256	--	--	16.08	16.08	0.10	0.00	0.01	0.04	0.00	0.00	20.9
6	54	-0	248	0	0	0	117	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
7	54	-0	548	0	0	0	287	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
8	54	-0	338	0	0	0	130	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9

9	54	-0	638	0	0	0	301	--	--	16.08	16.08	0.10	0.01	0.01	0.04	0.00	0.00	20.9
10	54	-0	249	0	0	0	161	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
11	54	-0	339	0	0	0	212	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
12	54	-0	548	0	0	0	205	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
13	54	-0	638	0	0	0	256	--	--	16.08	16.08	0.10	0.00	0.01	0.04	0.00	0.00	20.9
14	54	-0	248	0	0	0	117	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
15	54	-0	548	0	0	0	287	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
16	54	-0	338	0	0	0	130	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
17	54	-0	638	0	0	0	301	--	--	16.08	16.08	0.10	0.01	0.01	0.04	0.00	0.00	20.9
18	54	-0	103	0	0	0	-208	--	--	16.08	16.08	0.18	0.00	0.00	0.01	0.00	0.00	20.9
19	54	-0	895	0	0	0	39	--	--	16.08	16.08	0.00	0.00	0.01	0.06	0.00	0.00	20.9
20	54	-0	708	0	0	0	129	--	--	16.08	16.08	0.00	0.00	0.01	0.04	0.00	0.00	20.9
37	54	-0	-152	0	0	0	-128	--	--	16.08	16.08	0.18	0.00	0.00	0.01	0.00	0.00	20.9
38	54	-0	1168	0	0	0	192	--	--	16.08	16.08	0.00	0.00	0.01	0.07	0.00	0.00	20.9
39	54	-0	857	0	0	0	342	--	--	16.08	16.08	0.00	0.01	0.01	0.05	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 136 NI 1788 NF 1787 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-583	0	0	0	240	--	--	16.08	16.08	0.00	0.00	0.00	0.04	0.00	0.00	20.9
2	0	-0	-697	0	0	0	294	--	--	16.08	16.08	0.10	0.01	0.01	0.04	0.00	0.00	20.9
3	0	-0	-590	0	0	0	280	--	--	16.08	16.08	0.10	0.00	0.00	0.04	0.00	0.00	20.9
4	0	-0	-307	0	0	0	89	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
5	0	-0	-200	0	0	0	75	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
6	0	-0	-685	0	0	0	239	--	--	16.08	16.08	0.10	0.00	0.01	0.04	0.00	0.00	20.9
7	0	-0	-329	0	0	0	192	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
8	0	-0	-568	0	0	0	177	--	--	16.08	16.08	0.10	0.00	0.00	0.04	0.00	0.00	20.9
9	0	-0	-212	0	0	0	130	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
10	0	-0	-697	0	0	0	294	--	--	16.08	16.08	0.10	0.01	0.01	0.04	0.00	0.00	20.9
11	0	-0	-590	0	0	0	280	--	--	16.08	16.08	0.10	0.00	0.00	0.04	0.00	0.00	20.9
12	0	-0	-307	0	0	0	89	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
13	0	-0	-200	0	0	0	75	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
14	0	-0	-685	0	0	0	239	--	--	16.08	16.08	0.10	0.00	0.01	0.04	0.00	0.00	20.9
15	0	-0	-329	0	0	0	192	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
16	0	-0	-568	0	0	0	177	--	--	16.08	16.08	0.10	0.00	0.00	0.04	0.00	0.00	20.9
17	0	-0	-212	0	0	0	130	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
18	0	-0	-1353	0	0	0	248	--	--	16.08	16.08	0.00	0.00	0.01	0.08	0.00	0.00	20.9
19	0	-0	-321	0	0	0	-387	--	--	16.08	16.08	0.18	0.01	0.00	0.02	0.00	0.00	20.9
20	0	-0	-574	0	0	0	46	--	--	16.08	16.08	0.00	0.00	0.00	0.04	0.00	0.00	20.9
37	0	-0	-1621	0	0	0	465	--	--	16.08	16.08	0.00	0.01	0.01	0.10	0.00	0.00	20.9
38	0	-0	99	0	0	0	-306	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9
39	0	-0	-322	0	0	0	129	--	--	16.08	16.08	0.00	0.00	0.00	0.02	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-583	0	0	0	240	--	--	16.08	16.08	0.00	0.00	0.00	0.04	0.00	0.00	20.9
2	27	-0	-697	0	0	0	294	--	--	16.08	16.08	0.10	0.01	0.01	0.04	0.00	0.00	20.9
3	27	-0	-590	0	0	0	280	--	--	16.08	16.08	0.10	0.00	0.00	0.04	0.00	0.00	20.9
4	27	-0	-307	0	0	0	89	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
5	27	-0	-200	0	0	0	75	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
6	27	-0	-685	0	0	0	239	--	--	16.08	16.08	0.10	0.00	0.01	0.04	0.00	0.00	20.9
7	27	-0	-329	0	0	0	192	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
8	27	-0	-568	0	0	0	177	--	--	16.08	16.08	0.10	0.00	0.00	0.04	0.00	0.00	20.9
9	27	-0	-212	0	0	0	130	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
10	27	-0	-697	0	0	0	294	--	--	16.08	16.08	0.10	0.01	0.01	0.04	0.00	0.00	20.9
11	27	-0	-590	0	0	0	280	--	--	16.08	16.08	0.10	0.00	0.00	0.04	0.00	0.00	20.9
12	27	-0	-307	0	0	0	89	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
13	27	-0	-200	0	0	0	75	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
14	27	-0	-685	0	0	0	239	--	--	16.08	16.08	0.10	0.00	0.01	0.04	0.00	0.00	20.9
15	27	-0	-329	0	0	0	192	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
16	27	-0	-568	0	0	0	177	--	--	16.08	16.08	0.10	0.00	0.00	0.04	0.00	0.00	20.9
17	27	-0	-212	0	0	0	130	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
18	27	-0	-1353	0	0	0	-477	--	--	16.08	16.08	0.18	0.01	0.01	0.08	0.00	0.00	20.9
19	27	-0	-321	0	0	0	-387	--	--	16.08	16.08	0.18	0.01	0.00	0.02	0.00	0.00	20.9
20	27	-0	-574	0	0	0	-261	--	--	16.08	16.08	0.18	0.00	0.00	0.04	0.00	0.00	20.9
37	27	-0	-1621	0	0	0	465	--	--	16.08	16.08	0.00	0.01	0.01	0.10	0.00	0.00	20.9
38	27	-0	99	0	0	0	-306	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9
39	27	-0	-322	0	0	0	129	--	--	16.08	16.08	0.00	0.00	0.00	0.02	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	54	-0	-583	0	0	0	-73	--	--	16.08	16.08	0.18	0.00	0.00	0.04	0.00	0.00	20.9
2	54	-0	-697	0	0	0	-79	--	--	16.08	16.08	0.29	0.00	0.01	0.04	0.00	0.00	20.9
3	54	-0	-590	0	0	0	-36	--	--	16.08	16.08	0.29	0.00	0.00	0.04	0.00	0.00	20.9
4	54	-0	-307	0	0	0	-76	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
5	54	-0	-200	0	0	0	-33	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
6	54	-0	-685	0	0	0	-128	--	--	16.08	16.08	0.29	0.00	0.01	0.04	0.00	0.00	20.9
7	54	-0	-329	0	0	0	15	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
8	54	-0	-568	0	0	0	-127	--	--	16.08	16.08	0.29	0.00	0.00	0.04	0.00	0.00	20.9
9	54	-0	-212	0	0	0	16	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
10	54	-0	-697	0	0	0	-79	--	--	16.08	16.08	0.29	0.00	0.01	0.04	0.00	0.00	20.9
11	54	-0	-590	0	0	0	-36	--	--	16.08	16.08	0.29	0.00	0.00	0.04	0.00	0.00	20.9
12	54	-0	-307	0	0	0	-76	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
13	54	-0	-200	0	0	0	-33	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
14	54	-0	-685	0	0	0	-128	--	--	16.08	16.08	0.29	0.00	0.01	0.04	0.00	0.00	20.9
15	54	-0	-329	0	0	0	15	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
16	54	-0	-568	0	0	0	-127	--	--	16.08	16.08	0.29	0.00	0.00	0.04	0.00	0.00	20.9
17	54	-0	-212	0	0	0	16	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
18	54	-0	-1353	0	0	0	-477	--	--	16.08	16.08	0.18	0.01	0.01	0.08	0.00	0.00	20.9
19	54	-0	-321	0	0	0	-387	--	--	16.08	16.08	0.18	0.01	0.00	0.02	0.00	0.00	20.9
20	54	-0	-574	0	0	0	-261	--	--	16.08	16.08	0.18	0.00	0.00	0.04	0.00	0.00	20.9
37	54	-0	-1621	0	0	0	-403	--	--	16.08	16.08	0.18	0.01	0.01	0.10	0.00	0.00	20.9
38	54	-0	99	0	0	0	-306	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9
39	54	-0	-322	0	0	0	-43	--	--	16.08	16.08	0.18	0.00	0.00	0.02	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 137 NI 1775 NF 1788 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m			cm
1	0	-0	-1787	0	0	0	864	--	--	16.08	16.08	0.00	0.01	0.01	0.11	0.00	0.00	20.9
2	0	-0	-1675	0	0	0	842	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
3	0	-0	-1572	0	0	0	813	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
4	0	-0	-1178	0	0	0	516	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
5	0	-0	-1075	0	0	0	487	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
6	0	-0	-1621	0	0	0	761	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
7	0	-0	-1278	0	0	0	666	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
8	0	-0	-1472	0	0	0	663	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
9	0	-0	-1129	0	0	0	568	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
10	0	-0	-1675	0	0	0	842	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
11	0	-0	-1572	0	0	0	813	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
12	0	-0	-1178	0	0	0	516	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
13	0	-0	-1075	0	0	0	487	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
14	0	-0	-1621	0	0	0	761	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
15	0	-0	-1278	0	0	0	666	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
16	0	-0	-1472	0	0	0	663	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
17	0	-0	-1129	0	0	0	568	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
18	0	-0	-2840	0	0	0	1124	--	--	16.08	16.08	0.00	0.02	0.02	0.18	0.00	0.00	20.9
19	0	-0	-1543	0	0	0	358	--	--	16.08	16.08	0.00	0.01	0.01	0.10	0.00	0.00	20.9
20	0	-0	-1919	0	0	0	727	--	--	16.08	16.08	0.00	0.01	0.02	0.12	0.00	0.00	20.9
37	0	-0	-3138	0	0	0	1408	--	--	16.08	16.08	0.00	0.02	0.03	0.20	0.00	0.00	20.9
38	0	-0	-977	0	0	0	130	--	--	16.08	16.08	0.00	0.00	0.01	0.06	0.00	0.00	20.9
39	0	-0	-1603	0	0	0	745	--	--	16.08	16.08	0.00	0.01	0.01	0.10	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m			cm
1	27	-0	-1787	0	0	0	864	--	--	16.08	16.08	0.00	0.01	0.01	0.11	0.00	0.00	20.9
2	27	-0	-1675	0	0	0	842	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
3	27	-0	-1572	0	0	0	813	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
4	27	-0	-1178	0	0	0	516	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
5	27	-0	-1075	0	0	0	487	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
6	27	-0	-1621	0	0	0	761	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
7	27	-0	-1278	0	0	0	666	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
8	27	-0	-1472	0	0	0	663	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
9	27	-0	-1129	0	0	0	568	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
10	27	-0	-1675	0	0	0	842	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
11	27	-0	-1572	0	0	0	813	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
12	27	-0	-1178	0	0	0	516	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
13	27	-0	-1075	0	0	0	487	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
14	27	-0	-1621	0	0	0	761	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
15	27	-0	-1278	0	0	0	666	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
16	27	-0	-1472	0	0	0	663	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
17	27	-0	-1129	0	0	0	568	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
18	27	-0	-2840	0	0	0	1124	--	--	16.08	16.08	0.00	0.02	0.02	0.18	0.00	0.00	20.9
19	27	-0	-1543	0	0	0	-469	--	--	16.08	16.08	0.18	0.01	0.01	0.10	0.00	0.00	20.9
20	27	-0	-1919	0	0	0	727	--	--	16.08	16.08	0.00	0.01	0.02	0.12	0.00	0.00	20.9
37	27	-0	-3138	0	0	0	1408	--	--	16.08	16.08	0.00	0.02	0.03	0.20	0.00	0.00	20.9
38	27	-0	-977	0	0	0	-393	--	--	16.08	16.08	0.18	0.01	0.01	0.06	0.00	0.00	20.9
39	27	-0	-1603	0	0	0	745	--	--	16.08	16.08	0.00	0.01	0.01	0.10	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m			cm
1	54	-0	-1787	0	0	0	-93	--	--	16.08	16.08	0.18	0.00	0.01	0.11	0.00	0.00	20.9
2	54	-0	-1675	0	0	0	-55	--	--	16.08	16.08	0.29	0.00	0.01	0.11	0.00	0.00	20.9
3	54	-0	-1572	0	0	0	-28	--	--	16.08	16.08	0.29	0.00	0.01	0.10	0.00	0.00	20.9
4	54	-0	-1178	0	0	0	-115	--	--	16.08	16.08	0.29	0.00	0.01	0.07	0.00	0.00	20.9
5	54	-0	-1075	0	0	0	-89	--	--	16.08	16.08	0.29	0.00	0.01	0.07	0.00	0.00	20.9
6	54	-0	-1621	0	0	0	-108	--	--	16.08	16.08	0.29	0.00	0.01	0.10	0.00	0.00	20.9
7	54	-0	-1278	0	0	0	-18	--	--	16.08	16.08	0.29	0.00	0.01	0.08	0.00	0.00	20.9
8	54	-0	-1472	0	0	0	-126	--	--	16.08	16.08	0.29	0.00	0.01	0.09	0.00	0.00	20.9
9	54	-0	-1129	0	0	0	-36	--	--	16.08	16.08	0.29	0.00	0.01	0.07	0.00	0.00	20.9
10	54	-0	-1675	0	0	0	-55	--	--	16.08	16.08	0.29	0.00	0.01	0.11	0.00	0.00	20.9
11	54	-0	-1572	0	0	0	-28	--	--	16.08	16.08	0.29	0.00	0.01	0.10	0.00	0.00	20.9
12	54	-0	-1178	0	0	0	-115	--	--	16.08	16.08	0.29	0.00	0.01	0.07	0.00	0.00	20.9
13	54	-0	-1075	0	0	0	-89	--	--	16.08	16.08	0.29	0.00	0.01	0.07	0.00	0.00	20.9
14	54	-0	-1621	0	0	0	-108	--	--	16.08	16.08	0.29	0.00	0.01	0.10	0.00	0.00	20.9
15	54	-0	-1278	0	0	0	-18	--	--	16.08	16.08	0.29	0.00	0.01	0.08	0.00	0.00	20.9
16	54	-0	-1472	0	0	0	-126	--	--	16.08	16.08	0.29	0.00	0.01	0.09	0.00	0.00	20.9
17	54	-0	-1129	0	0	0	-36	--	--	16.08	16.08	0.29	0.00	0.01	0.07	0.00	0.00	20.9
18	54	-0	-2840	0	0	0	-397	--	--	16.08	16.08	0.18	0.01	0.02	0.18	0.00	0.00	20.9
19	54	-0	-1543	0	0	0	-469	--	--	16.08	16.08	0.18	0.01	0.01	0.10	0.00	0.00	20.9
20	54	-0	-1919	0	0	0	-301	--	--	16.08	16.08	0.18	0.00	0.02	0.12	0.00	0.00	20.9
37	54	-0	-3138	0	0	0	-273	--	--	16.08	16.08	0.18	0.00	0.03	0.20	0.00	0.00	20.9
38	54	-0	-977	0	0	0	-393	--	--	16.08	16.08	0.18	0.01	0.01	0.06	0.00	0.00	20.9
39	54	-0	-1603	0	0	0	-114	--	--	16.08	16.08	0.18	0.00	0.01	0.10	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 138 NI 1776 NF 1775 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m			cm
1	0	-0	-2380	0	0	0	1334	--	--	16.08	16.08	0.00	0.02	0.02	0.15	0.00	0.00	20.9
2	0	-0	-2138	0	0	0	1251	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
3	0	-0	-2077	0	0	0	1234	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
4	0	-0	-1585	0	0	0	818	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
5	0	-0	-1524	0	0	0	802	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
6	0	-0	-2015	0	0	0	1119	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
7	0	-0	-1812	0	0	0	1064	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
8	0	-0	-1850	0	0	0	989	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
9	0	-0	-1646	0	0	0	934	--	--	16.08	16.08	0.10	0.02	0.01	0.10	0.00	0.00	20.9
10	0	-0	-2138	0	0	0	1251	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
11	0	-0	-2077	0	0	0	1234	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
12	0	-0	-1585	0	0	0	818	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
13	0	-0	-1524	0	0	0	802	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
14	0	-0	-2015	0	0	0	1119	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
15	0	-0	-1812	0	0	0	1064	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
16	0	-0	-1850	0	0	0	989	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9

17	0	-0	-1646	0	0	0	934	--	--	16.08	16.08	0.10	0.02	0.01	0.10	0.00	0.00	20.9
18	0	-0	-3508	0	0	0	1762	--	--	16.08	16.08	0.00	0.03	0.03	0.22	0.00	0.00	20.9
19	0	-0	-2069	0	0	0	723	--	--	16.08	16.08	0.00	0.01	0.02	0.13	0.00	0.00	20.9
20	0	-0	-2597	0	0	0	1242	--	--	16.08	16.08	0.00	0.02	0.02	0.16	0.00	0.00	20.9
37	0	-0	-3847	0	0	0	2124	--	--	16.08	16.08	0.00	0.04	0.03	0.24	0.00	0.00	20.9
38	0	-0	-1447	0	0	0	391	--	--	16.08	16.08	0.00	0.01	0.01	0.09	0.00	0.00	20.9
39	0	-0	-2328	0	0	0	1257	--	--	16.08	16.08	0.00	0.02	0.02	0.15	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-2380	0	0	0	1334	--	--	16.08	16.08	0.00	0.02	0.02	0.15	0.00	0.00	20.9
2	27	-0	-2138	0	0	0	1251	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
3	27	-0	-2077	0	0	0	1234	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
4	27	-0	-1585	0	0	0	818	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
5	27	-0	-1524	0	0	0	802	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
6	27	-0	-2015	0	0	0	1119	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
7	27	-0	-1812	0	0	0	1064	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
8	27	-0	-1850	0	0	0	989	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
9	27	-0	-1646	0	0	0	934	--	--	16.08	16.08	0.10	0.02	0.01	0.10	0.00	0.00	20.9
10	27	-0	-2138	0	0	0	1251	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
11	27	-0	-2077	0	0	0	1234	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
12	27	-0	-1585	0	0	0	818	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
13	27	-0	-1524	0	0	0	802	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
14	27	-0	-2015	0	0	0	1119	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
15	27	-0	-1812	0	0	0	1064	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
16	27	-0	-1850	0	0	0	989	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
17	27	-0	-1646	0	0	0	934	--	--	16.08	16.08	0.10	0.02	0.01	0.10	0.00	0.00	20.9
18	27	-0	-3508	0	0	0	1762	--	--	16.08	16.08	0.00	0.03	0.03	0.22	0.00	0.00	20.9
19	27	-0	-2069	0	0	0	723	--	--	16.08	16.08	0.00	0.01	0.02	0.13	0.00	0.00	20.9
20	27	-0	-2597	0	0	0	1242	--	--	16.08	16.08	0.00	0.02	0.02	0.16	0.00	0.00	20.9
37	27	-0	-3847	0	0	0	2124	--	--	16.08	16.08	0.00	0.04	0.03	0.24	0.00	0.00	20.9
38	27	-0	-1447	0	0	0	391	--	--	16.08	16.08	0.00	0.01	0.01	0.09	0.00	0.00	20.9
39	27	-0	-2328	0	0	0	1257	--	--	16.08	16.08	0.00	0.02	0.02	0.15	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	54	-0	-2380	0	0	0	59	--	--	16.08	16.08	0.00	0.00	0.02	0.15	0.00	0.00	20.9
2	54	-0	-2138	0	0	0	106	--	--	16.08	16.08	0.10	0.00	0.02	0.13	0.00	0.00	20.9
3	54	-0	-2077	0	0	0	122	--	--	16.08	16.08	0.10	0.00	0.02	0.13	0.00	0.00	20.9
4	54	-0	-1585	0	0	0	-31	--	--	16.08	16.08	0.29	0.00	0.01	0.10	0.00	0.00	20.9
5	54	-0	-1524	0	0	0	-15	--	--	16.08	16.08	0.29	0.00	0.01	0.10	0.00	0.00	20.9
6	54	-0	-2015	0	0	0	39	--	--	16.08	16.08	0.10	0.00	0.02	0.13	0.00	0.00	20.9
7	54	-0	-1812	0	0	0	93	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
8	54	-0	-1850	0	0	0	-2	--	--	16.08	16.08	0.29	0.00	0.02	0.12	0.00	0.00	20.9
9	54	-0	-1646	0	0	0	52	--	--	16.08	16.08	0.10	0.00	0.01	0.10	0.00	0.00	20.9
10	54	-0	-2138	0	0	0	106	--	--	16.08	16.08	0.10	0.00	0.02	0.13	0.00	0.00	20.9
11	54	-0	-2077	0	0	0	122	--	--	16.08	16.08	0.10	0.00	0.02	0.13	0.00	0.00	20.9
12	54	-0	-1585	0	0	0	-31	--	--	16.08	16.08	0.29	0.00	0.01	0.10	0.00	0.00	20.9
13	54	-0	-1524	0	0	0	-15	--	--	16.08	16.08	0.29	0.00	0.01	0.10	0.00	0.00	20.9
14	54	-0	-2015	0	0	0	39	--	--	16.08	16.08	0.10	0.00	0.02	0.13	0.00	0.00	20.9
15	54	-0	-1812	0	0	0	93	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
16	54	-0	-1850	0	0	0	-2	--	--	16.08	16.08	0.29	0.00	0.02	0.12	0.00	0.00	20.9
17	54	-0	-1646	0	0	0	52	--	--	16.08	16.08	0.10	0.00	0.01	0.10	0.00	0.00	20.9
18	54	-0	-3508	0	0	0	-117	--	--	16.08	16.08	0.18	0.00	0.03	0.22	0.00	0.00	20.9
19	54	-0	-2069	0	0	0	-386	--	--	16.08	16.08	0.18	0.01	0.02	0.13	0.00	0.00	20.9
20	54	-0	-2597	0	0	0	-149	--	--	16.08	16.08	0.18	0.00	0.02	0.16	0.00	0.00	20.9
37	54	-0	-3847	0	0	0	63	--	--	16.08	16.08	0.00	0.00	0.03	0.24	0.00	0.00	20.9
38	54	-0	-1447	0	0	0	-384	--	--	16.08	16.08	0.18	0.01	0.01	0.09	0.00	0.00	20.9
39	54	-0	-2328	0	0	0	10	--	--	16.08	16.08	0.00	0.00	0.02	0.15	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 139 NI 1799 NF 1776 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm

1	0	-0	-1231	0	0	0	1287	--	--	16.08	16.08	0.00	0.02	0.01	0.08	0.00	0.00	20.9
2	0	-0	-1188	0	0	0	1254	--	--	16.08	16.08	0.10	0.02	0.01	0.07	0.00	0.00	20.9
3	0	-0	-1169	0	0	0	1239	--	--	16.08	16.08	0.10	0.02	0.01	0.07	0.00	0.00	20.9
4	0	-0	-724	0	0	0	741	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
5	0	-0	-706	0	0	0	727	--	--	16.08	16.08	0.10	0.01	0.01	0.04	0.00	0.00	20.9
6	0	-0	-1047	0	0	0	1092	--	--	16.08	16.08	0.10	0.02	0.01	0.07	0.00	0.00	20.9
7	0	-0	-985	0	0	0	1043	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9
8	0	-0	-908	0	0	0	938	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9
9	0	-0	-846	0	0	0	889	--	--	16.08	16.08	0.10	0.02	0.01	0.05	0.00	0.00	20.9
10	0	-0	-1188	0	0	0	1254	--	--	16.08	16.08	0.10	0.02	0.01	0.07	0.00	0.00	20.9
11	0	-0	-1169	0	0	0	1239	--	--	16.08	16.08	0.10	0.02	0.01	0.07	0.00	0.00	20.9
12	0	-0	-724	0	0	0	741	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
13	0	-0	-706	0	0	0	727	--	--	16.08	16.08	0.10	0.01	0.01	0.04	0.00	0.00	20.9
14	0	-0	-1047	0	0	0	1092	--	--	16.08	16.08	0.10	0.02	0.01	0.07	0.00	0.00	20.9
15	0	-0	-985	0	0	0	1043	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9
16	0	-0	-908	0	0	0	938	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9
17	0	-0	-846	0	0	0	889	--	--	16.08	16.08	0.10	0.02	0.01	0.05	0.00	0.00	20.9
18	0	-0	-2143	0	0	0	1881	--	--	16.08	16.08	0.00	0.03	0.02	0.13	0.00	0.00	20.9
19	0	-0	-812	0	0	0	570	--	--	16.08	16.08	0.00	0.01	0.01	0.05	0.00	0.00	20.9
20	0	-0	-1387	0	0	0	1218	--	--	16.08	16.08	0.00	0.02	0.01	0.09	0.00	0.00	20.9
37	0	-0	-2503	0	0	0	2324	--	--	16.08	16.08	0.00	0.04	0.02	0.16	0.00	0.00	20.9
38	0	-0	-285	0	0	0	140	--	--	16.08	16.08	0.00	0.00	0.00	0.02	0.00	0.00	20.9
39	0	-0	-1243	0	0	0	1219	--	--	16.08	16.08	0.00	0.02	0.01	0.08	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-1231	0	0	0	1287	--	--	16.08	16.08	0.00	0.02	0.01	0.08	0.00	0.00	20.9
2	27	-0	-1188	0	0	0	1254	--	--	16.08	16.08	0.10	0.02	0.01	0.07	0.00	0.00	20.9
3	27	-0	-1169	0	0	0	1239	--	--	16.08	16.08	0.10	0.02	0.01	0.07	0.00	0.00	20.9
4	27	-0	-724	0	0	0	741	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
5	27	-0	-706	0	0	0	727	--	--	16.08	16.08	0.10	0.01	0.01	0.04	0.00	0.00	20.9
6	27	-0	-1047	0	0	0	1092	--	--	16.08	16.08	0.10	0.02	0.01	0.07	0.00	0.00	20.9
7	27	-0	-985	0	0	0	1043	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9
8	27	-0	-908	0	0	0	938	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9
9	27	-0	-846	0	0	0	889	--	--	16.08	16.08	0.10	0.02	0.01	0.05	0.00	0.00	20.9
10	27	-0	-1188	0	0	0	1254	--	--	16.08	16.08	0.10	0.02	0.01	0.07	0.00	0.00	20.9
11	27	-0	-1169	0	0	0	1239	--	--	16.08	16.08	0.10	0.02	0.01	0.07	0.00	0.00	20.9
12	27	-0	-724	0	0	0	741	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9

13	27	-0	-706	0	0	0	727	--	--	16.08	16.08	0.10	0.01	0.01	0.04	0.00	0.00	20.9
14	27	-0	-1047	0	0	0	1092	--	--	16.08	16.08	0.10	0.02	0.01	0.07	0.00	0.00	20.9
15	27	-0	-985	0	0	0	1043	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9
16	27	-0	-908	0	0	0	938	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9
17	27	-0	-846	0	0	0	889	--	--	16.08	16.08	0.10	0.02	0.01	0.05	0.00	0.00	20.9
18	27	-0	-2143	0	0	0	1881	--	--	16.08	16.08	0.00	0.03	0.02	0.13	0.00	0.00	20.9
19	27	-0	-812	0	0	0	570	--	--	16.08	16.08	0.00	0.01	0.01	0.05	0.00	0.00	20.9
20	27	-0	-1387	0	0	0	1218	--	--	16.08	16.08	0.00	0.02	0.01	0.09	0.00	0.00	20.9
37	27	-0	-2503	0	0	0	2324	--	--	16.08	16.08	0.00	0.04	0.02	0.16	0.00	0.00	20.9
38	27	-0	-285	0	0	0	140	--	--	16.08	16.08	0.00	0.00	0.00	0.02	0.00	0.00	20.9
39	27	-0	-1243	0	0	0	1219	--	--	16.08	16.08	0.00	0.02	0.01	0.08	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	54	-0	-1231	0	0	0	628	--	--	16.08	16.08	0.00	0.01	0.01	0.08	0.00	0.00	20.9
2	54	-0	-1188	0	0	0	617	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
3	54	-0	-1169	0	0	0	613	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
4	54	-0	-724	0	0	0	354	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
5	54	-0	-706	0	0	0	349	--	--	16.08	16.08	0.10	0.01	0.01	0.04	0.00	0.00	20.9
6	54	-0	-1047	0	0	0	531	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
7	54	-0	-985	0	0	0	515	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
8	54	-0	-908	0	0	0	451	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
9	54	-0	-846	0	0	0	436	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
10	54	-0	-1188	0	0	0	617	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
11	54	-0	-1169	0	0	0	613	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
12	54	-0	-724	0	0	0	354	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
13	54	-0	-706	0	0	0	349	--	--	16.08	16.08	0.10	0.01	0.01	0.04	0.00	0.00	20.9
14	54	-0	-1047	0	0	0	531	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
15	54	-0	-985	0	0	0	515	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
16	54	-0	-908	0	0	0	451	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
17	54	-0	-846	0	0	0	436	--	--	16.08	16.08	0.10	0.01	0.01	0.05	0.00	0.00	20.9
18	54	-0	-2143	0	0	0	733	--	--	16.08	16.08	0.00	0.01	0.02	0.13	0.00	0.00	20.9
19	54	-0	-812	0	0	0	135	--	--	16.08	16.08	0.00	0.00	0.01	0.05	0.00	0.00	20.9
20	54	-0	-1387	0	0	0	475	--	--	16.08	16.08	0.00	0.01	0.01	0.09	0.00	0.00	20.9
37	54	-0	-2503	0	0	0	983	--	--	16.08	16.08	0.00	0.02	0.02	0.16	0.00	0.00	20.9
38	54	-0	-285	0	0	0	-13	--	--	16.08	16.08	0.18	0.00	0.00	0.02	0.00	0.00	20.9
39	54	-0	-1243	0	0	0	553	--	--	16.08	16.08	0.00	0.01	0.01	0.08	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 140 NI 1792 NF 1799 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--	--	--	--	--	--	--	--	--	--	--		--	--	--	--	--	--
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	1440	0	0	0	252	--	--	16.08	16.08	0.00	0.00	0.01	0.09	0.00	0.00	20.9
2	0	-0	1248	0	0	0	358	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
3	0	-0	1210	0	0	0	344	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
4	0	-0	1005	0	0	0	43	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
5	0	-0	968	0	0	0	29	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
6	0	-0	1206	0	0	0	264	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
7	0	-0	1082	0	0	0	218	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
8	0	-0	1133	0	0	0	170	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
9	0	-0	1009	0	0	0	123	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
10	0	-0	1248	0	0	0	358	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
11	0	-0	1210	0	0	0	344	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
12	0	-0	1005	0	0	0	43	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
13	0	-0	968	0	0	0	29	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
14	0	-0	1206	0	0	0	264	--	--	16.08	16.08	0.10	0.00	0.01	0.08	0.00	0.00	20.9
15	0	-0	1082	0	0	0	218	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
16	0	-0	1133	0	0	0	170	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
17	0	-0	1009	0	0	0	123	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
18	0	-0	1848	0	0	0	398	--	--	16.08	16.08	0.00	0.01	0.02	0.12	0.00	0.00	20.9
19	0	-0	1438	0	0	0	-431	--	--	16.08	16.08	0.18	0.01	0.01	0.09	0.00	0.00	20.9
20	0	-0	1556	0	0	0	-17	--	--	16.08	16.08	0.18	0.00	0.01	0.10	0.00	0.00	20.9
37	0	-0	1907	0	0	0	755	--	--	16.08	16.08	0.00	0.01	0.02	0.12	0.00	0.00	20.9
38	0	-0	1224	0	0	0	-628	--	--	16.08	16.08	0.18	0.01	0.01	0.08	0.00	0.00	20.9
39	0	-0	1421	0	0	0	63	--	--	16.08	16.08	0.00	0.00	0.01	0.09	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	1440	0	0	0	2163	--	--	16.08	16.08	0.00	0.04	0.01	0.09	0.00	0.00	20.9
2	26	-0	1248	0	0	0	2014	--	--	16.08	16.08	0.10	0.04	0.01	0.08	0.00	0.00	20.9
3	26	-0	1210	0	0	0	1950	--	--	16.08	16.08	0.10	0.03	0.01	0.08	0.00	0.00	20.9
4	26	-0	1005	0	0	0	1377	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9
5	26	-0	968	0	0	0	1314	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9
6	26	-0	1206	0	0	0	1865	--	--	16.08	16.08	0.10	0.03	0.01	0.08	0.00	0.00	20.9
7	26	-0	1082	0	0	0	1654	--	--	16.08	16.08	0.10	0.03	0.01	0.07	0.00	0.00	20.9
8	26	-0	1133	0	0	0	1674	--	--	16.08	16.08	0.10	0.03	0.01	0.07	0.00	0.00	20.9
9	26	-0	1009	0	0	0	1462	--	--	16.08	16.08	0.10	0.03	0.01	0.06	0.00	0.00	20.9
10	26	-0	1248	0	0	0	2014	--	--	16.08	16.08	0.10	0.04	0.01	0.08	0.00	0.00	20.9
11	26	-0	1210	0	0	0	1950	--	--	16.08	16.08	0.10	0.03	0.01	0.08	0.00	0.00	20.9
12	26	-0	1005	0	0	0	1377	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9
13	26	-0	968	0	0	0	1314	--	--	16.08	16.08	0.10	0.02	0.01	0.06	0.00	0.00	20.9
14	26	-0	1206	0	0	0	1865	--	--	16.08	16.08	0.10	0.03	0.01	0.08	0.00	0.00	20.9
15	26	-0	1082	0	0	0	1654	--	--	16.08	16.08	0.10	0.03	0.01	0.07	0.00	0.00	20.9
16	26	-0	1133	0	0	0	1674	--	--	16.08	16.08	0.10	0.03	0.01	0.07	0.00	0.00	20.9
17	26	-0	1009	0	0	0	1462	--	--	16.08	16.08	0.10	0.03	0.01	0.06	0.00	0.00	20.9
18	26	-0	1848	0	0	0	2851	--	--	16.08	16.08	0.00	0.05	0.02	0.12	0.00	0.00	20.9
19	26	-0	1438	0	0	0	-431	--	--	16.08	16.08	0.18	0.01	0.01	0.09	0.00	0.00	20.9
20	26	-0	1556	0	0	0	2048	--	--	16.08	16.08	0.00	0.03	0.01	0.10	0.00	0.00	20.9
37	26	-0	1907	0	0	0	3286	--	--	16.08	16.08	0.00	0.06	0.02	0.12	0.00	0.00	20.9
38	26	-0	1224	0	0	0	-628	--	--	16.08	16.08	0.18	0.01	0.01	0.08	0.00	0.00	20.9
39	26	-0	1421	0	0	0	1949	--	--	16.08	16.08	0.00	0.03	0.01	0.09	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	52	-0	1440	0	0	0	996	--	--	16.08	16.08	0.00	0.02	0.01	0.09	0.00	0.00	20.9
2	52	-0	1248	0	0	0	1003	--	--	16.08	16.08	0.10	0.02	0.01	0.08	0.00	0.00	20.9
3	52	-0	1210	0	0	0	970	--	--	16.08	16.08	0.10	0.02	0.01	0.08	0.00	0.00	20.9
4	52	-0	1005	0	0	0	563	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
5	52	-0	968	0	0	0	529	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
6	52	-0	1206	0	0	0	888	--	--	16.08	16.08	0.10	0.02	0.01	0.08	0.00	0.00	20.9
7	52	-0	1082	0	0	0	777	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
8	52	-0	1133	0	0	0	756	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9

9	52	-0	1009	0	0	0	645	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
10	52	-0	1248	0	0	0	1003	--	--	16.08	16.08	0.10	0.02	0.01	0.08	0.00	0.00	20.9
11	52	-0	1210	0	0	0	970	--	--	16.08	16.08	0.10	0.02	0.01	0.08	0.00	0.00	20.9
12	52	-0	1005	0	0	0	563	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
13	52	-0	968	0	0	0	529	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
14	52	-0	1206	0	0	0	888	--	--	16.08	16.08	0.10	0.02	0.01	0.08	0.00	0.00	20.9
15	52	-0	1082	0	0	0	777	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
16	52	-0	1133	0	0	0	756	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
17	52	-0	1009	0	0	0	645	--	--	16.08	16.08	0.10	0.01	0.01	0.06	0.00	0.00	20.9
18	52	-0	1848	0	0	0	1353	--	--	16.08	16.08	0.00	0.02	0.02	0.12	0.00	0.00	20.9
19	52	-0	1438	0	0	0	311	--	--	16.08	16.08	0.00	0.01	0.01	0.09	0.00	0.00	20.9
20	52	-0	1556	0	0	0	787	--	--	16.08	16.08	0.00	0.01	0.01	0.10	0.00	0.00	20.9
37	52	-0	1907	0	0	0	1740	--	--	16.08	16.08	0.00	0.03	0.02	0.12	0.00	0.00	20.9
38	52	-0	1224	0	0	0	4	--	--	16.08	16.08	0.00	0.00	0.01	0.08	0.00	0.00	20.9
39	52	-0	1421	0	0	0	797	--	--	16.08	16.08	0.00	0.01	0.01	0.09	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 141 NI 1779 NF 1792 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	2606	0	0	0	-225	--	--	16.08	16.08	0.18	0.00	0.02	0.16	0.00	0.00	20.9
2	0	-0	2180	0	0	0	-43	--	--	16.08	16.08	0.29	0.00	0.02	0.14	0.00	0.00	20.9
3	0	-0	2157	0	0	0	-58	--	--	16.08	16.08	0.29	0.00	0.02	0.14	0.00	0.00	20.9
4	0	-0	1853	0	0	0	-288	--	--	16.08	16.08	0.29	0.00	0.02	0.12	0.00	0.00	20.9
5	0	-0	1830	0	0	0	-303	--	--	16.08	16.08	0.29	0.01	0.02	0.11	0.00	0.00	20.9
6	0	-0	2093	0	0	0	-111	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
7	0	-0	2015	0	0	0	-161	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
8	0	-0	1995	0	0	0	-185	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
9	0	-0	1917	0	0	0	-234	--	--	16.08	16.08	0.29	0.00	0.02	0.12	0.00	0.00	20.9
10	0	-0	2180	0	0	0	-43	--	--	16.08	16.08	0.29	0.00	0.02	0.14	0.00	0.00	20.9
11	0	-0	2157	0	0	0	-58	--	--	16.08	16.08	0.29	0.00	0.02	0.14	0.00	0.00	20.9
12	0	-0	1853	0	0	0	-288	--	--	16.08	16.08	0.29	0.00	0.02	0.12	0.00	0.00	20.9
13	0	-0	1830	0	0	0	-303	--	--	16.08	16.08	0.29	0.01	0.02	0.11	0.00	0.00	20.9
14	0	-0	2093	0	0	0	-111	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
15	0	-0	2015	0	0	0	-161	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
16	0	-0	1995	0	0	0	-185	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
17	0	-0	1917	0	0	0	-234	--	--	16.08	16.08	0.29	0.00	0.02	0.12	0.00	0.00	20.9
18	0	-0	3074	0	0	0	-133	--	--	16.08	16.08	0.18	0.00	0.03	0.19	0.00	0.00	20.9
19	0	-0	2587	0	0	0	-867	--	--	16.08	16.08	0.18	0.01	0.02	0.16	0.00	0.00	20.9
20	0	-0	2763	0	0	0	-504	--	--	16.08	16.08	0.18	0.01	0.02	0.17	0.00	0.00	20.9
37	0	-0	3144	0	0	0	198	--	--	16.08	16.08	0.00	0.00	0.03	0.20	0.00	0.00	20.9
38	0	-0	2333	0	0	0	-1026	--	--	16.08	16.08	0.18	0.02	0.02	0.15	0.00	0.00	20.9
39	0	-0	2626	0	0	0	-420	--	--	16.08	16.08	0.18	0.01	0.02	0.16	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	2606	0	0	0	3234	--	--	16.08	16.08	0.00	0.06	0.02	0.16	0.00	0.00	20.9
2	26	-0	2180	0	0	0	2851	--	--	16.08	16.08	0.10	0.05	0.02	0.14	0.00	0.00	20.9
3	26	-0	2157	0	0	0	2805	--	--	16.08	16.08	0.10	0.05	0.02	0.14	0.00	0.00	20.9
4	26	-0	1853	0	0	0	2171	--	--	16.08	16.08	0.10	0.04	0.02	0.12	0.00	0.00	20.9
5	26	-0	1830	0	0	0	2126	--	--	16.08	16.08	0.10	0.04	0.02	0.11	0.00	0.00	20.9
6	26	-0	2093	0	0	0	2666	--	--	16.08	16.08	0.10	0.05	0.02	0.13	0.00	0.00	20.9
7	26	-0	2015	0	0	0	2513	--	--	16.08	16.08	0.10	0.04	0.02	0.13	0.00	0.00	20.9
8	26	-0	1995	0	0	0	2463	--	--	16.08	16.08	0.10	0.04	0.02	0.13	0.00	0.00	20.9
9	26	-0	1917	0	0	0	2310	--	--	16.08	16.08	0.10	0.04	0.02	0.12	0.00	0.00	20.9
10	26	-0	2180	0	0	0	2851	--	--	16.08	16.08	0.10	0.05	0.02	0.14	0.00	0.00	20.9
11	26	-0	2157	0	0	0	2805	--	--	16.08	16.08	0.10	0.05	0.02	0.14	0.00	0.00	20.9
12	26	-0	1853	0	0	0	2171	--	--	16.08	16.08	0.10	0.04	0.02	0.12	0.00	0.00	20.9
13	26	-0	1830	0	0	0	2126	--	--	16.08	16.08	0.10	0.04	0.02	0.11	0.00	0.00	20.9
14	26	-0	2093	0	0	0	2666	--	--	16.08	16.08	0.10	0.05	0.02	0.13	0.00	0.00	20.9
15	26	-0	2015	0	0	0	2513	--	--	16.08	16.08	0.10	0.04	0.02	0.13	0.00	0.00	20.9
16	26	-0	1995	0	0	0	2463	--	--	16.08	16.08	0.10	0.04	0.02	0.13	0.00	0.00	20.9
17	26	-0	1917	0	0	0	2310	--	--	16.08	16.08	0.10	0.04	0.02	0.12	0.00	0.00	20.9
18	26	-0	3074	0	0	0	3946	--	--	16.08	16.08	0.00	0.07	0.03	0.19	0.00	0.00	20.9
19	26	-0	2587	0	0	0	-867	--	--	16.08	16.08	0.18	0.01	0.02	0.16	0.00	0.00	20.9
20	26	-0	2763	0	0	0	3163	--	--	16.08	16.08	0.00	0.05	0.02	0.17	0.00	0.00	20.9
37	26	-0	3144	0	0	0	4370	--	--	16.08	16.08	0.00	0.07	0.03	0.20	0.00	0.00	20.9
38	26	-0	2333	0	0	0	-1026	--	--	16.08	16.08	0.18	0.02	0.02	0.15	0.00	0.00	20.9
39	26	-0	2626	0	0	0	3065	--	--	16.08	16.08	0.00	0.05	0.02	0.16	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	52	-0	2606	0	0	0	1122	--	--	16.08	16.08	0.00	0.02	0.02	0.16	0.00	0.00	20.9
2	52	-0	2180	0	0	0	1084	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
3	52	-0	2157	0	0	0	1057	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
4	52	-0	1853	0	0	0	669	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
5	52	-0	1830	0	0	0	642	--	--	16.08	16.08	0.10	0.01	0.02	0.11	0.00	0.00	20.9
6	52	-0	2093	0	0	0	970	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
7	52	-0	2015	0	0	0	880	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
8	52	-0	1995	0	0	0	846	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
9	52	-0	1917	0	0	0	756	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
10	52	-0	2180	0	0	0	1084	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
11	52	-0	2157	0	0	0	1057	--	--	16.08	16.08	0.10	0.02	0.02	0.14	0.00	0.00	20.9
12	52	-0	1853	0	0	0	669	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
13	52	-0	1830	0	0	0	642	--	--	16.08	16.08	0.10	0.01	0.02	0.11	0.00	0.00	20.9
14	52	-0	2093	0	0	0	970	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
15	52	-0	2015	0	0	0	880	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
16	52	-0	1995	0	0	0	846	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
17	52	-0	1917	0	0	0	756	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
18	52	-0	3074	0	0	0	1455	--	--	16.08	16.08	0.00	0.02	0.03	0.19	0.00	0.00	20.9
19	52	-0	2587	0	0	0	469	--	--	16.08	16.08	0.00	0.01	0.02	0.16	0.00	0.00	20.9
20	52	-0	2763	0	0	0	924	--	--	16.08	16.08	0.00	0.02	0.02	0.17	0.00	0.00	20.9
37	52	-0	3144	0	0	0	1822	--	--	16.08	16.08	0.00	0.03	0.03	0.20	0.00	0.00	20.9
38	52	-0	2333	0	0	0	180	--	--	16.08	16.08	0.00	0.00	0.02	0.15	0.00	0.00	20.9
39	52	-0	2626	0	0	0	937	--	--	16.08	16.08	0.00	0.02	0.02	0.16	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 142 NI 1790 NF 1779 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	1945	0	0	0	-380	--	--	16.08	16.08	0.18	0.01	0.02	0.12	0.00	0.00	20.9
2	0	-0	1613	0	0	0	-180	--	--	16.08	16.08	0.29	0.00	0.01	0.10	0.00	0.00	20.9
3	0	-0	1631	0	0	0	-189	--	--	16.08	16.08	0.29	0.00	0.01	0.10	0.00	0.00	20.9
4	0	-0	1362	0	0	0	-396	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
5	0	-0	1379	0	0	0	-405	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
6	0	-0	1505	0	0	0	-244	--	--	16.08	16.08	0.29	0.00	0.01	0.09	0.00	0.00	20.9
7	0	-0	1563	0	0	0	-276	--	--	16.08	16.08	0.29	0.00	0.01	0.10	0.00	0.00	20.9
8	0	-0	1430	0	0	0	-309	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
9	0	-0	1487	0	0	0	-341	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
10	0	-0	1613	0	0	0	-180	--	--	16.08	16.08	0.29	0.00	0.01	0.10	0.00	0.00	20.9
11	0	-0	1631	0	0	0	-189	--	--	16.08	16.08	0.29	0.00	0.01	0.10	0.00	0.00	20.9
12	0	-0	1362	0	0	0	-396	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
13	0	-0	1379	0	0	0	-405	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
14	0	-0	1505	0	0	0	-244	--	--	16.08	16.08	0.29	0.00	0.01	0.09	0.00	0.00	20.9
15	0	-0	1563	0	0	0	-276	--	--	16.08	16.08	0.29	0.00	0.01	0.10	0.00	0.00	20.9
16	0	-0	1430	0	0	0	-309	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
17	0	-0	1487	0	0	0	-341	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
18	0	-0	2021	0	0	0	-266	--	--	16.08	16.08	0.18	0.00	0.02	0.13	0.00	0.00	20.9
19	0	-0	1785	0	0	0	-998	--	--	16.08	16.08	0.18	0.02	0.01	0.11	0.00	0.00	20.9
20	0	-0	1946	0	0	0	-629	--	--	16.08	16.08	0.18	0.01	0.02	0.12	0.00	0.00	20.9
37	0	-0	2096	0	0	0	58	--	--	16.08	16.08	0.00	0.00	0.02	0.13	0.00	0.00	20.9
38	0	-0	1703	0	0	0	-1162	--	--	16.08	16.08	0.18	0.02	0.01	0.11	0.00	0.00	20.9
39	0	-0	1969	0	0	0	-547	--	--	16.08	16.08	0.18	0.01	0.02	0.12	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	1945	0	0	0	2201	--	--	16.08	16.08	0.00	0.04	0.02	0.12	0.00	0.00	20.9
2	26	-0	1613	0	0	0	1961	--	--	16.08	16.08	0.10	0.03	0.01	0.10	0.00	0.00	20.9
3	26	-0	1631	0	0	0	1975	--	--	16.08	16.08	0.10	0.04	0.01	0.10	0.00	0.00	20.9
4	26	-0	1362	0	0	0	-396	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
5	26	-0	1379	0	0	0	-405	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
6	26	-0	1505	0	0	0	1753	--	--	16.08	16.08	0.10	0.03	0.01	0.09	0.00	0.00	20.9
7	26	-0	1563	0	0	0	1798	--	--	16.08	16.08	0.10	0.03	0.01	0.10	0.00	0.00	20.9
8	26	-0	1430	0	0	0	1588	--	--	16.08	16.08	0.10	0.03	0.01	0.09	0.00	0.00	20.9
9	26	-0	1487	0	0	0	1633	--	--	16.08	16.08	0.10	0.03	0.01	0.09	0.00	0.00	20.9
10	26	-0	1613	0	0	0	1961	--	--	16.08	16.08	0.10	0.03	0.01	0.10	0.00	0.00	20.9
11	26	-0	1631	0	0	0	1975	--	--	16.08	16.08	0.10	0.04	0.01	0.10	0.00	0.00	20.9
12	26	-0	1362	0	0	0	-396	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
13	26	-0	1379	0	0	0	-405	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
14	26	-0	1505	0	0	0	1753	--	--	16.08	16.08	0.10	0.03	0.01	0.09	0.00	0.00	20.9
15	26	-0	1563	0	0	0	1798	--	--	16.08	16.08	0.10	0.03	0.01	0.10	0.00	0.00	20.9
16	26	-0	1430	0	0	0	1588	--	--	16.08	16.08	0.10	0.03	0.01	0.09	0.00	0.00	20.9
17	26	-0	1487	0	0	0	1633	--	--	16.08	16.08	0.10	0.03	0.01	0.09	0.00	0.00	20.9
18	26	-0	2021	0	0	0	2416	--	--	16.08	16.08	0.00	0.04	0.02	0.13	0.00	0.00	20.9
19	26	-0	1785	0	0	0	-998	--	--	16.08	16.08	0.18	0.02	0.01	0.11	0.00	0.00	20.9
20	26	-0	1946	0	0	0	-629	--	--	16.08	16.08	0.18	0.01	0.02	0.12	0.00	0.00	20.9
37	26	-0	2096	0	0	0	2840	--	--	16.08	16.08	0.00	0.05	0.02	0.13	0.00	0.00	20.9
38	26	-0	1703	0	0	0	-1162	--	--	16.08	16.08	0.18	0.02	0.01	0.11	0.00	0.00	20.9
39	26	-0	1969	0	0	0	-547	--	--	16.08	16.08	0.18	0.01	0.02	0.12	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	52	-0	1945	0	0	0	625	--	--	16.08	16.08	0.00	0.01	0.02	0.12	0.00	0.00	20.9
2	52	-0	1613	0	0	0	654	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
3	52	-0	1631	0	0	0	654	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
4	52	-0	1362	0	0	0	308	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
5	52	-0	1379	0	0	0	307	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
6	52	-0	1505	0	0	0	533	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
7	52	-0	1563	0	0	0	532	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
8	52	-0	1430	0	0	0	430	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
9	52	-0	1487	0	0	0	428	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
10	52	-0	1613	0	0	0	654	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
11	52	-0	1631	0	0	0	654	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
12	52	-0	1362	0	0	0	308	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
13	52	-0	1379	0	0	0	307	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
14	52	-0	1505	0	0	0	533	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
15	52	-0	1563	0	0	0	532	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
16	52	-0	1430	0	0	0	430	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
17	52	-0	1487	0	0	0	428	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
18	52	-0	2021	0	0	0	778	--	--	16.08	16.08	0.00	0.01	0.02	0.13	0.00	0.00	20.9
19	52	-0	1785	0	0	0	-998	--	--	16.08	16.08	0.18	0.02	0.01	0.11	0.00	0.00	20.9
20	52	-0	1946	0	0	0	376	--	--	16.08	16.08	0.00	0.01	0.02	0.12	0.00	0.00	20.9
37	52	-0	2096	0	0	0	1141	--	--	16.08	16.08	0.00	0.02	0.02	0.13	0.00	0.00	20.9
38	52	-0	1703	0	0	0	-1162	--	--	16.08	16.08	0.18	0.02	0.01	0.11	0.00	0.00	20.9
39	52	-0	1969	0	0	0	471	--	--	16.08	16.08	0.00	0.01	0.02	0.12	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 143 NI 1791 NF 1790 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	662	0	0	0	-342	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
2	0	-0	558	0	0	0	-157	--	--	16.08	16.08	0.29	0.00	0.00	0.04	0.00	0.00	20.9
3	0	-0	579	0	0	0	-160	--	--	16.08	16.08	0.29	0.00	0.00	0.04	0.00	0.00	20.9
4	0	-0	439	0	0	0	-365	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
5	0	-0	460	0	0	0	-369	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
6	0	-0	492	0	0	0	-226	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
7	0	-0	562	0	0	0	-237	--	--	16.08	16.08	0.29	0.00	0.00	0.04	0.00	0.00	20.9
8	0	-0	456	0	0	0	-289	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
9	0	-0	526	0	0	0	-300	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
10	0	-0	558	0	0	0	-157	--	--	16.08	16.08	0.29	0.00	0.00	0.04	0.00	0.00	20.9
11	0	-0	579	0	0	0	-160	--	--	16.08	16.08	0.29	0.00	0.00	0.04	0.00	0.00	20.9
12	0	-0	439	0	0	0	-365	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
13	0	-0	460	0	0	0	-369	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
14	0	-0	492	0	0	0	-226	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
15	0	-0	562	0	0	0	-237	--	--	16.08	16.08	0.29	0.00	0.00	0.04	0.00	0.00	20.9
16	0	-0	456	0	0	0	-289	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9

17	0	-0	526	0	0	0	-300	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
18	0	-0	306	0	0	0	-134	--	--	16.08	16.08	0.18	0.00	0.00	0.02	0.00	0.00	20.9
19	0	-0	419	0	0	0	-925	--	--	16.08	16.08	0.18	0.02	0.00	0.03	0.00	0.00	20.9
20	0	-0	440	0	0	0	-520	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9
37	0	-0	355	0	0	0	190	--	--	16.08	16.08	0.00	0.00	0.00	0.02	0.00	0.00	20.9
38	0	-0	542	0	0	0	-1128	--	--	16.08	16.08	0.18	0.02	0.00	0.03	0.00	0.00	20.9
39	0	-0	578	0	0	0	-453	--	--	16.08	16.08	0.18	0.01	0.00	0.04	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	662	0	0	0	-342	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
2	26	-0	558	0	0	0	-157	--	--	16.08	16.08	0.29	0.00	0.00	0.04	0.00	0.00	20.9
3	26	-0	579	0	0	0	-160	--	--	16.08	16.08	0.29	0.00	0.00	0.04	0.00	0.00	20.9
4	26	-0	439	0	0	0	-365	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
5	26	-0	460	0	0	0	-369	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
6	26	-0	492	0	0	0	-226	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
7	26	-0	562	0	0	0	-237	--	--	16.08	16.08	0.29	0.00	0.00	0.04	0.00	0.00	20.9
8	26	-0	456	0	0	0	-289	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
9	26	-0	526	0	0	0	-300	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
10	26	-0	558	0	0	0	-157	--	--	16.08	16.08	0.29	0.00	0.00	0.04	0.00	0.00	20.9
11	26	-0	579	0	0	0	-160	--	--	16.08	16.08	0.29	0.00	0.00	0.04	0.00	0.00	20.9
12	26	-0	439	0	0	0	-365	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
13	26	-0	460	0	0	0	-369	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
14	26	-0	492	0	0	0	-226	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
15	26	-0	562	0	0	0	-237	--	--	16.08	16.08	0.29	0.00	0.00	0.04	0.00	0.00	20.9
16	26	-0	456	0	0	0	-289	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
17	26	-0	526	0	0	0	-300	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
18	26	-0	306	0	0	0	-134	--	--	16.08	16.08	0.18	0.00	0.00	0.02	0.00	0.00	20.9
19	26	-0	419	0	0	0	-925	--	--	16.08	16.08	0.18	0.02	0.00	0.03	0.00	0.00	20.9
20	26	-0	440	0	0	0	-520	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9
37	26	-0	355	0	0	0	661	--	--	16.08	16.08	0.00	0.01	0.00	0.02	0.00	0.00	20.9
38	26	-0	542	0	0	0	-1128	--	--	16.08	16.08	0.18	0.02	0.00	0.03	0.00	0.00	20.9
39	26	-0	578	0	0	0	-453	--	--	16.08	16.08	0.18	0.01	0.00	0.04	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	52	-0	662	0	0	0	0	--	--	16.08	16.08	0.00	0.00	0.01	0.04	0.00	0.00	20.9
2	52	-0	558	0	0	0	132	--	--	16.08	16.08	0.10	0.00	0.00	0.04	0.00	0.00	20.9
3	52	-0	579	0	0	0	139	--	--	16.08	16.08	0.10	0.00	0.00	0.04	0.00	0.00	20.9
4	52	-0	439	0	0	0	-365	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
5	52	-0	460	0	0	0	-369	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
6	52	-0	492	0	0	0	28	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
7	52	-0	562	0	0	0	53	--	--	16.08	16.08	0.10	0.00	0.00	0.04	0.00	0.00	20.9
8	52	-0	456	0	0	0	-289	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
9	52	-0	526	0	0	0	-300	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
10	52	-0	558	0	0	0	132	--	--	16.08	16.08	0.10	0.00	0.00	0.04	0.00	0.00	20.9
11	52	-0	579	0	0	0	139	--	--	16.08	16.08	0.10	0.00	0.00	0.04	0.00	0.00	20.9
12	52	-0	439	0	0	0	-365	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
13	52	-0	460	0	0	0	-369	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
14	52	-0	492	0	0	0	28	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
15	52	-0	562	0	0	0	53	--	--	16.08	16.08	0.10	0.00	0.00	0.04	0.00	0.00	20.9
16	52	-0	456	0	0	0	-289	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
17	52	-0	526	0	0	0	-300	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
18	52	-0	306	0	0	0	24	--	--	16.08	16.08	0.00	0.00	0.00	0.02	0.00	0.00	20.9
19	52	-0	419	0	0	0	-925	--	--	16.08	16.08	0.18	0.02	0.00	0.03	0.00	0.00	20.9
20	52	-0	440	0	0	0	-520	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9
37	52	-0	355	0	0	0	373	--	--	16.08	16.08	0.00	0.01	0.00	0.02	0.00	0.00	20.9
38	52	-0	542	0	0	0	-1128	--	--	16.08	16.08	0.18	0.02	0.00	0.03	0.00	0.00	20.9
39	52	-0	578	0	0	0	-453	--	--	16.08	16.08	0.18	0.01	0.00	0.04	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 144 NI 1778 NF 1791 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm

1	0	-0	-250	0	0	0	-329	--	--	16.08	16.08	0.18	0.01	0.00	0.02	0.00	0.00	20.9
2	0	-0	-182	0	0	0	-145	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
3	0	-0	-198	0	0	0	-133	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
4	0	-0	-188	0	0	0	-373	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
5	0	-0	-203	0	0	0	-362	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
6	0	-0	-165	0	0	0	-238	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
7	0	-0	-218	0	0	0	-200	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
8	0	-0	-167	0	0	0	-307	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
9	0	-0	-220	0	0	0	-268	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
10	0	-0	-182	0	0	0	-145	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
11	0	-0	-198	0	0	0	-133	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
12	0	-0	-188	0	0	0	-373	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
13	0	-0	-203	0	0	0	-362	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
14	0	-0	-165	0	0	0	-238	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
15	0	-0	-218	0	0	0	-200	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
16	0	-0	-167	0	0	0	-307	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
17	0	-0	-220	0	0	0	-268	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
18	0	-0	-895	0	0	0	136	--	--	16.08	16.08	0.00	0.00	0.01	0.06	0.00	0.00	20.9
19	0	-0	-488	0	0	0	-1029	--	--	16.08	16.08	0.18	0.02	0.00	0.03	0.00	0.00	20.9
20	0	-0	-680	0	0	0	-616	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
37	0	-0	-892	0	0	0	479	--	--	16.08	16.08	0.00	0.01	0.01	0.06	0.00	0.00	20.9
38	0	-0	-215	0	0	0	-1154	--	--	16.08	16.08	0.18	0.02	0.00	0.01	0.00	0.00	20.9
39	0	-0	-535	0	0	0	-465	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	-250	0	0	0	-329	--	--	16.08	16.08	0.18	0.01	0.00	0.02	0.00	0.00	20.9
2	26	-0	-182	0	0	0	-145	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
3	26	-0	-198	0	0	0	-133	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
4	26	-0	-188	0	0	0	-373	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
5	26	-0	-203	0	0	0	-362	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
6	26	-0	-165	0	0	0	-238	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
7	26	-0	-218	0	0	0	-200	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
8	26	-0	-167	0	0	0	-307	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
9	26	-0	-220	0	0	0	-268	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
10	26	-0	-182	0	0	0	-145	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
11	26	-0	-198	0	0	0	-133	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
12	26	-0	-188	0	0	0	-373	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9

13	26	-0	-203	0	0	0	-362	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
14	26	-0	-165	0	0	0	-238	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
15	26	-0	-218	0	0	0	-200	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
16	26	-0	-167	0	0	0	-307	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
17	26	-0	-220	0	0	0	-268	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
18	26	-0	-895	0	0	0	-326	--	--	16.08	16.08	0.18	0.01	0.01	0.06	0.00	0.00	20.9
19	26	-0	-488	0	0	0	-1029	--	--	16.08	16.08	0.18	0.02	0.00	0.03	0.00	0.00	20.9
20	26	-0	-680	0	0	0	-616	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
37	26	-0	-892	0	0	0	479	--	--	16.08	16.08	0.00	0.01	0.01	0.06	0.00	0.00	20.9
38	26	-0	-215	0	0	0	-1154	--	--	16.08	16.08	0.18	0.02	0.00	0.01	0.00	0.00	20.9
39	26	-0	-535	0	0	0	-465	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	52	-0	-250	0	0	0	-329	--	--	16.08	16.08	0.18	0.01	0.00	0.02	0.00	0.00	20.9
2	52	-0	-182	0	0	0	-145	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
3	52	-0	-198	0	0	0	-133	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
4	52	-0	-188	0	0	0	-373	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
5	52	-0	-203	0	0	0	-362	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
6	52	-0	-165	0	0	0	-238	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
7	52	-0	-218	0	0	0	-200	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
8	52	-0	-167	0	0	0	-307	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
9	52	-0	-220	0	0	0	-268	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
10	52	-0	-182	0	0	0	-145	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
11	52	-0	-198	0	0	0	-133	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
12	52	-0	-188	0	0	0	-373	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
13	52	-0	-203	0	0	0	-362	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
14	52	-0	-165	0	0	0	-238	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
15	52	-0	-218	0	0	0	-200	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
16	52	-0	-167	0	0	0	-307	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
17	52	-0	-220	0	0	0	-268	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
18	52	-0	-895	0	0	0	-326	--	--	16.08	16.08	0.18	0.01	0.01	0.06	0.00	0.00	20.9
19	52	-0	-488	0	0	0	-1029	--	--	16.08	16.08	0.18	0.02	0.00	0.03	0.00	0.00	20.9
20	52	-0	-680	0	0	0	-616	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
37	52	-0	-892	0	0	0	18	--	--	16.08	16.08	0.00	0.00	0.01	0.06	0.00	0.00	20.9
38	52	-0	-215	0	0	0	-1154	--	--	16.08	16.08	0.18	0.02	0.00	0.01	0.00	0.00	20.9
39	52	-0	-535	0	0	0	-465	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 145 NI 1800 NF 1778 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-422	0	0	0	-314	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9
2	0	-0	-355	0	0	0	53	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
3	0	-0	-394	0	0	0	78	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
4	0	-0	-255	0	0	0	-357	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
5	0	-0	-294	0	0	0	-351	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
6	0	-0	-275	0	0	0	-216	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
7	0	-0	-404	0	0	0	11	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
8	0	-0	-244	0	0	0	-284	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
9	0	-0	-374	0	0	0	-266	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
10	0	-0	-355	0	0	0	53	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
11	0	-0	-394	0	0	0	78	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
12	0	-0	-255	0	0	0	-357	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
13	0	-0	-294	0	0	0	-351	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
14	0	-0	-275	0	0	0	-216	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
15	0	-0	-404	0	0	0	11	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
16	0	-0	-244	0	0	0	-284	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
17	0	-0	-374	0	0	0	-266	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
18	0	-0	-1444	0	0	0	604	--	--	16.08	16.08	0.00	0.01	0.01	0.09	0.00	0.00	20.9
19	0	-0	-688	0	0	0	-948	--	--	16.08	16.08	0.18	0.02	0.01	0.04	0.00	0.00	20.9
20	0	-0	-1079	0	0	0	50	--	--	16.08	16.08	0.00	0.00	0.01	0.07	0.00	0.00	20.9
37	0	-0	-1491	0	0	0	971	--	--	16.08	16.08	0.00	0.02	0.01	0.09	0.00	0.00	20.9
38	0	-0	-232	0	0	0	-1145	--	--	16.08	16.08	0.18	0.02	0.00	0.01	0.00	0.00	20.9
39	0	-0	-884	0	0	0	47	--	--	16.08	16.08	0.00	0.00	0.01	0.06	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	26	-0	-422	0	0	0	-314	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9
2	26	-0	-355	0	0	0	-131	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
3	26	-0	-394	0	0	0	-126	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
4	26	-0	-255	0	0	0	-357	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
5	26	-0	-294	0	0	0	-351	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
6	26	-0	-275	0	0	0	-216	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
7	26	-0	-404	0	0	0	-198	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
8	26	-0	-244	0	0	0	-284	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
9	26	-0	-374	0	0	0	-266	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
10	26	-0	-355	0	0	0	-131	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
11	26	-0	-394	0	0	0	-126	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
12	26	-0	-255	0	0	0	-357	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
13	26	-0	-294	0	0	0	-351	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
14	26	-0	-275	0	0	0	-216	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
15	26	-0	-404	0	0	0	-198	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
16	26	-0	-244	0	0	0	-284	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
17	26	-0	-374	0	0	0	-266	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
18	26	-0	-1444	0	0	0	604	--	--	16.08	16.08	0.00	0.01	0.01	0.09	0.00	0.00	20.9
19	26	-0	-688	0	0	0	-948	--	--	16.08	16.08	0.18	0.02	0.01	0.04	0.00	0.00	20.9
20	26	-0	-1079	0	0	0	-508	--	--	16.08	16.08	0.18	0.01	0.01	0.07	0.00	0.00	20.9
37	26	-0	-1491	0	0	0	971	--	--	16.08	16.08	0.00	0.02	0.01	0.09	0.00	0.00	20.9
38	26	-0	-232	0	0	0	-1145	--	--	16.08	16.08	0.18	0.02	0.00	0.01	0.00	0.00	20.9
39	26	-0	-884	0	0	0	-410	--	--	16.08	16.08	0.18	0.01	0.01	0.06	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	52	-0	-422	0	0	0	-314	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9
2	52	-0	-355	0	0	0	-131	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
3	52	-0	-394	0	0	0	-126	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
4	52	-0	-255	0	0	0	-357	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
5	52	-0	-294	0	0	0	-351	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
6	52	-0	-275	0	0	0	-216	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
7	52	-0	-404	0	0	0	-198	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
8	52	-0	-244	0	0	0	-284	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9

9	52	-0	-374	0	0	0	-266	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
10	52	-0	-355	0	0	0	-131	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
11	52	-0	-394	0	0	0	-126	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
12	52	-0	-255	0	0	0	-357	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
13	52	-0	-294	0	0	0	-351	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
14	52	-0	-275	0	0	0	-216	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
15	52	-0	-404	0	0	0	-198	--	--	16.08	16.08	0.29	0.00	0.00	0.03	0.00	0.00	20.9
16	52	-0	-244	0	0	0	-284	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
17	52	-0	-374	0	0	0	-266	--	--	16.08	16.08	0.29	0.00	0.00	0.02	0.00	0.00	20.9
18	52	-0	-1444	0	0	0	-141	--	--	16.08	16.08	0.18	0.00	0.01	0.09	0.00	0.00	20.9
19	52	-0	-688	0	0	0	-948	--	--	16.08	16.08	0.18	0.02	0.01	0.04	0.00	0.00	20.9
20	52	-0	-1079	0	0	0	-508	--	--	16.08	16.08	0.18	0.01	0.01	0.07	0.00	0.00	20.9
37	52	-0	-1491	0	0	0	200	--	--	16.08	16.08	0.00	0.00	0.01	0.09	0.00	0.00	20.9
38	52	-0	-232	0	0	0	-1145	--	--	16.08	16.08	0.18	0.02	0.00	0.01	0.00	0.00	20.9
39	52	-0	-884	0	0	0	-410	--	--	16.08	16.08	0.18	0.01	0.01	0.06	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 146 NI 1795 NF 1800 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-402	0	0	0	-696	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9
2	0	-0	-27	0	0	0	-357	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
3	0	-0	-74	0	0	0	-356	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
4	0	-0	-545	0	0	0	-714	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
5	0	-0	-592	0	0	0	-713	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
6	0	-0	-154	0	0	0	-483	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
7	0	-0	-309	0	0	0	-481	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
8	0	-0	-310	0	0	0	-590	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
9	0	-0	-465	0	0	0	-588	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
10	0	-0	-27	0	0	0	-357	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
11	0	-0	-74	0	0	0	-356	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
12	0	-0	-545	0	0	0	-714	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
13	0	-0	-592	0	0	0	-713	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
14	0	-0	-154	0	0	0	-483	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
15	0	-0	-309	0	0	0	-481	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
16	0	-0	-310	0	0	0	-590	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
17	0	-0	-465	0	0	0	-588	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
18	0	-0	640	0	0	0	-476	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
19	0	-0	-1483	0	0	0	-1617	--	--	16.08	16.08	0.18	0.03	0.01	0.09	0.00	0.00	20.9
20	0	-0	-532	0	0	0	-892	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9
37	0	-0	1340	0	0	0	-269	--	--	16.08	16.08	0.18	0.00	0.01	0.08	0.00	0.00	20.9
38	0	-0	-2199	0	0	0	-2040	--	--	16.08	16.08	0.18	0.03	0.02	0.14	0.00	0.00	20.9
39	0	-0	-613	0	0	0	-831	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	24	-0	-402	0	0	0	-696	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9
2	24	-0	-27	0	0	0	-357	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
3	24	-0	-74	0	0	0	-356	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
4	24	-0	-545	0	0	0	-714	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
5	24	-0	-592	0	0	0	-713	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
6	24	-0	-154	0	0	0	-483	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
7	24	-0	-309	0	0	0	-481	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
8	24	-0	-310	0	0	0	-590	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
9	24	-0	-465	0	0	0	-588	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
10	24	-0	-27	0	0	0	-357	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
11	24	-0	-74	0	0	0	-356	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
12	24	-0	-545	0	0	0	-714	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
13	24	-0	-592	0	0	0	-713	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
14	24	-0	-154	0	0	0	-483	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
15	24	-0	-309	0	0	0	-481	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
16	24	-0	-310	0	0	0	-590	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
17	24	-0	-465	0	0	0	-588	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
18	24	-0	640	0	0	0	-476	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
19	24	-0	-1483	0	0	0	-1617	--	--	16.08	16.08	0.18	0.03	0.01	0.09	0.00	0.00	20.9
20	24	-0	-532	0	0	0	-892	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9
37	24	-0	1340	0	0	0	1487	--	--	16.08	16.08	0.00	0.03	0.01	0.08	0.00	0.00	20.9
38	24	-0	-2199	0	0	0	-2040	--	--	16.08	16.08	0.18	0.03	0.02	0.14	0.00	0.00	20.9
39	24	-0	-613	0	0	0	-831	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	48	-0	-402	0	0	0	-696	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9
2	48	-0	-27	0	0	0	-357	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
3	48	-0	-74	0	0	0	-356	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
4	48	-0	-545	0	0	0	-714	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
5	48	-0	-592	0	0	0	-713	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
6	48	-0	-154	0	0	0	-483	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
7	48	-0	-309	0	0	0	-481	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
8	48	-0	-310	0	0	0	-590	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
9	48	-0	-465	0	0	0	-588	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
10	48	-0	-27	0	0	0	-357	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
11	48	-0	-74	0	0	0	-356	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
12	48	-0	-545	0	0	0	-714	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
13	48	-0	-592	0	0	0	-713	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
14	48	-0	-154	0	0	0	-483	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
15	48	-0	-309	0	0	0	-481	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
16	48	-0	-310	0	0	0	-590	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
17	48	-0	-465	0	0	0	-588	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
18	48	-0	640	0	0	0	-476	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9
19	48	-0	-1483	0	0	0	-1617	--	--	16.08	16.08	0.18	0.03	0.01	0.09	0.00	0.00	20.9
20	48	-0	-532	0	0	0	-892	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9
37	48	-0	1340	0	0	0	378	--	--	16.08	16.08	0.00	0.01	0.01	0.08	0.00	0.00	20.9
38	48	-0	-2199	0	0	0	-2040	--	--	16.08	16.08	0.18	0.03	0.02	0.14	0.00	0.00	20.9
39	48	-0	-613	0	0	0	-831	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 147 NI 1781 NF 1795 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-415	0	0	0	-464	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9
2	0	-0	-98	0	0	0	-244	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
3	0	-0	-128	0	0	0	-239	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
4	0	-0	-511	0	0	0	-475	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
5	0	-0	-541	0	0	0	-469	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
6	0	-0	-208	0	0	0	-332	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
7	0	-0	-307	0	0	0	-313	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
8	0	-0	-332	0	0	0	-401	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
9	0	-0	-431	0	0	0	-382	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
10	0	-0	-98	0	0	0	-244	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
11	0	-0	-128	0	0	0	-239	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
12	0	-0	-511	0	0	0	-475	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
13	0	-0	-541	0	0	0	-469	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
14	0	-0	-208	0	0	0	-332	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
15	0	-0	-307	0	0	0	-313	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
16	0	-0	-332	0	0	0	-401	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
17	0	-0	-431	0	0	0	-382	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
18	0	-0	154	0	0	0	-273	--	--	16.08	16.08	0.18	0.00	0.00	0.01	0.00	0.00	20.9
19	0	-0	-1598	0	0	0	-1132	--	--	16.08	16.08	0.18	0.02	0.01	0.10	0.00	0.00	20.9
20	0	-0	-748	0	0	0	-647	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9
37	0	-0	821	0	0	0	-218	--	--	16.08	16.08	0.18	0.00	0.01	0.05	0.00	0.00	20.9
38	0	-0	-2099	0	0	0	-1379	--	--	16.08	16.08	0.18	0.02	0.02	0.13	0.00	0.00	20.9
39	0	-0	-682	0	0	0	-570	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	24	-0	-415	0	0	0	-464	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9
2	24	-0	-98	0	0	0	-244	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
3	24	-0	-128	0	0	0	-239	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
4	24	-0	-511	0	0	0	-475	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
5	24	-0	-541	0	0	0	-469	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
6	24	-0	-208	0	0	0	-332	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
7	24	-0	-307	0	0	0	-313	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
8	24	-0	-332	0	0	0	-401	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
9	24	-0	-431	0	0	0	-382	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
10	24	-0	-98	0	0	0	-244	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
11	24	-0	-128	0	0	0	-239	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
12	24	-0	-511	0	0	0	-475	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
13	24	-0	-541	0	0	0	-469	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
14	24	-0	-208	0	0	0	-332	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
15	24	-0	-307	0	0	0	-313	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
16	24	-0	-332	0	0	0	-401	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
17	24	-0	-431	0	0	0	-382	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
18	24	-0	154	0	0	0	-273	--	--	16.08	16.08	0.18	0.00	0.00	0.01	0.00	0.00	20.9
19	24	-0	-1598	0	0	0	-1132	--	--	16.08	16.08	0.18	0.02	0.01	0.10	0.00	0.00	20.9
20	24	-0	-748	0	0	0	-647	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9
37	24	-0	821	0	0	0	-218	--	--	16.08	16.08	0.18	0.00	0.01	0.05	0.00	0.00	20.9
38	24	-0	-2099	0	0	0	-1379	--	--	16.08	16.08	0.18	0.02	0.02	0.13	0.00	0.00	20.9
39	24	-0	-682	0	0	0	-570	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	48	-0	-415	0	0	0	-464	--	--	16.08	16.08	0.18	0.01	0.00	0.03	0.00	0.00	20.9
2	48	-0	-98	0	0	0	-244	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
3	48	-0	-128	0	0	0	-239	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
4	48	-0	-511	0	0	0	-475	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
5	48	-0	-541	0	0	0	-469	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
6	48	-0	-208	0	0	0	-332	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
7	48	-0	-307	0	0	0	-313	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
8	48	-0	-332	0	0	0	-401	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
9	48	-0	-431	0	0	0	-382	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
10	48	-0	-98	0	0	0	-244	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
11	48	-0	-128	0	0	0	-239	--	--	16.08	16.08	0.29	0.00	0.00	0.01	0.00	0.00	20.9
12	48	-0	-511	0	0	0	-475	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
13	48	-0	-541	0	0	0	-469	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
14	48	-0	-208	0	0	0	-332	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
15	48	-0	-307	0	0	0	-313	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
16	48	-0	-332	0	0	0	-401	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
17	48	-0	-431	0	0	0	-382	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
18	48	-0	154	0	0	0	-273	--	--	16.08	16.08	0.18	0.00	0.00	0.01	0.00	0.00	20.9
19	48	-0	-1598	0	0	0	-1132	--	--	16.08	16.08	0.18	0.02	0.01	0.10	0.00	0.00	20.9
20	48	-0	-748	0	0	0	-647	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9
37	48	-0	821	0	0	0	178	--	--	16.08	16.08	0.00	0.00	0.01	0.05	0.00	0.00	20.9
38	48	-0	-2099	0	0	0	-1379	--	--	16.08	16.08	0.18	0.02	0.02	0.13	0.00	0.00	20.9
39	48	-0	-682	0	0	0	-570	--	--	16.08	16.08	0.18	0.01	0.01	0.04	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 148 NI 1793 NF 1781 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-1233	0	0	0	175	--	--	16.08	16.08	0.00	0.00	0.01	0.08	0.00	0.00	20.9
2	0	-0	-794	0	0	0	119	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
3	0	-0	-791	0	0	0	148	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
4	0	-0	-1105	0	0	0	122	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
5	0	-0	-1102	0	0	0	150	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
6	0	-0	-906	0	0	0	87	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
7	0	-0	-897	0	0	0	182	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
8	0	-0	-1000	0	0	0	88	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
9	0	-0	-990	0	0	0	183	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
10	0	-0	-794	0	0	0	119	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
11	0	-0	-791	0	0	0	148	--	--	16.08	16.08	0.10	0.00	0.01	0.05	0.00	0.00	20.9
12	0	-0	-1105	0	0	0	122	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
13	0	-0	-1102	0	0	0	150	--	--	16.08	16.08	0.10	0.00	0.01	0.07	0.00	0.00	20.9
14	0	-0	-906	0	0	0	87	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
15	0	-0	-897	0	0	0	182	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
16	0	-0	-1000	0	0	0	88	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9

17	0	-0	-990	0	0	0	183	--	--	16.08	16.08	0.10	0.00	0.01	0.06	0.00	0.00	20.9
18	0	-0	-1229	0	0	0	237	--	--	16.08	16.08	0.00	0.00	0.01	0.08	0.00	0.00	20.9
19	0	-0	-2676	0	0	0	353	--	--	16.08	16.08	0.00	0.01	0.02	0.17	0.00	0.00	20.9
20	0	-0	-1846	0	0	0	322	--	--	16.08	16.08	0.00	0.01	0.02	0.12	0.00	0.00	20.9
37	0	-0	-530	0	0	0	169	--	--	16.08	16.08	0.00	0.00	0.00	0.03	0.00	0.00	20.9
38	0	-0	-2943	0	0	0	363	--	--	16.08	16.08	0.00	0.01	0.02	0.18	0.00	0.00	20.9
39	0	-0	-1558	0	0	0	311	--	--	16.08	16.08	0.00	0.01	0.01	0.10	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	24	-0	-1233	0	0	0	-420	--	--	16.08	16.08	0.18	0.01	0.01	0.08	0.00	0.00	20.9
2	24	-0	-794	0	0	0	-264	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
3	24	-0	-791	0	0	0	-234	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
4	24	-0	-1105	0	0	0	-412	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
5	24	-0	-1102	0	0	0	-382	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
6	24	-0	-906	0	0	0	-351	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
7	24	-0	-897	0	0	0	-251	--	--	16.08	16.08	0.29	0.00	0.01	0.06	0.00	0.00	20.9
8	24	-0	-1000	0	0	0	-396	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
9	24	-0	-990	0	0	0	-296	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
10	24	-0	-794	0	0	0	-264	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
11	24	-0	-791	0	0	0	-234	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
12	24	-0	-1105	0	0	0	-412	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
13	24	-0	-1102	0	0	0	-382	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
14	24	-0	-906	0	0	0	-351	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
15	24	-0	-897	0	0	0	-251	--	--	16.08	16.08	0.29	0.00	0.01	0.06	0.00	0.00	20.9
16	24	-0	-1000	0	0	0	-396	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
17	24	-0	-990	0	0	0	-296	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
18	24	-0	-1229	0	0	0	-357	--	--	16.08	16.08	0.18	0.01	0.01	0.08	0.00	0.00	20.9
19	24	-0	-2676	0	0	0	-940	--	--	16.08	16.08	0.18	0.02	0.02	0.17	0.00	0.00	20.9
20	24	-0	-1846	0	0	0	-570	--	--	16.08	16.08	0.18	0.01	0.02	0.12	0.00	0.00	20.9
37	24	-0	-530	0	0	0	169	--	--	16.08	16.08	0.00	0.00	0.00	0.03	0.00	0.00	20.9
38	24	-0	-2943	0	0	0	-1059	--	--	16.08	16.08	0.18	0.02	0.02	0.18	0.00	0.00	20.9
39	24	-0	-1558	0	0	0	-442	--	--	16.08	16.08	0.18	0.01	0.01	0.10	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	48	-0	-1233	0	0	0	-420	--	--	16.08	16.08	0.18	0.01	0.01	0.08	0.00	0.00	20.9
2	48	-0	-794	0	0	0	-264	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
3	48	-0	-791	0	0	0	-234	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
4	48	-0	-1105	0	0	0	-412	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
5	48	-0	-1102	0	0	0	-382	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
6	48	-0	-906	0	0	0	-351	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
7	48	-0	-897	0	0	0	-251	--	--	16.08	16.08	0.29	0.00	0.01	0.06	0.00	0.00	20.9
8	48	-0	-1000	0	0	0	-396	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
9	48	-0	-990	0	0	0	-296	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
10	48	-0	-794	0	0	0	-264	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
11	48	-0	-791	0	0	0	-234	--	--	16.08	16.08	0.29	0.00	0.01	0.05	0.00	0.00	20.9
12	48	-0	-1105	0	0	0	-412	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
13	48	-0	-1102	0	0	0	-382	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
14	48	-0	-906	0	0	0	-351	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
15	48	-0	-897	0	0	0	-251	--	--	16.08	16.08	0.29	0.00	0.01	0.06	0.00	0.00	20.9
16	48	-0	-1000	0	0	0	-396	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
17	48	-0	-990	0	0	0	-296	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
18	48	-0	-1229	0	0	0	-357	--	--	16.08	16.08	0.18	0.01	0.01	0.08	0.00	0.00	20.9
19	48	-0	-2676	0	0	0	-940	--	--	16.08	16.08	0.18	0.02	0.02	0.17	0.00	0.00	20.9
20	48	-0	-1846	0	0	0	-570	--	--	16.08	16.08	0.18	0.01	0.02	0.12	0.00	0.00	20.9
37	48	-0	-530	0	0	0	-87	--	--	16.08	16.08	0.18	0.00	0.00	0.03	0.00	0.00	20.9
38	48	-0	-2943	0	0	0	-1059	--	--	16.08	16.08	0.18	0.02	0.02	0.18	0.00	0.00	20.9
39	48	-0	-1558	0	0	0	-442	--	--	16.08	16.08	0.18	0.01	0.01	0.10	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 149 NI 1794 NF 1793 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-2356	0	0	0	792	--	--	16.08	16.08	0.00	0.01	0.02	0.15	0.00	0.00	20.9
2	0	-0	-1713	0	0	0	583	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
3	0	-0	-1714	0	0	0	624	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
4	0	-0	-1911	0	0	0	594	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
5	0	-0	-1912	0	0	0	634	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
6	0	-0	-1781	0	0	0	540	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
7	0	-0	-1785	0	0	0	674	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
8	0	-0	-1840	0	0	0	543	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
9	0	-0	-1844	0	0	0	678	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
10	0	-0	-1713	0	0	0	583	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
11	0	-0	-1714	0	0	0	624	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
12	0	-0	-1911	0	0	0	594	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
13	0	-0	-1912	0	0	0	634	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
14	0	-0	-1781	0	0	0	540	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
15	0	-0	-1785	0	0	0	674	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
16	0	-0	-1840	0	0	0	543	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
17	0	-0	-1844	0	0	0	678	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
18	0	-0	-2866	0	0	0	1024	--	--	16.08	16.08	0.00	0.02	0.02	0.18	0.00	0.00	20.9
19	0	-0	-4018	0	0	0	1284	--	--	16.08	16.08	0.00	0.02	0.03	0.25	0.00	0.00	20.9
20	0	-0	-3297	0	0	0	1177	--	--	16.08	16.08	0.00	0.02	0.03	0.21	0.00	0.00	20.9
37	0	-0	-2145	0	0	0	832	--	--	16.08	16.08	0.00	0.01	0.02	0.13	0.00	0.00	20.9
38	0	-0	-4066	0	0	0	1266	--	--	16.08	16.08	0.00	0.02	0.03	0.26	0.00	0.00	20.9
39	0	-0	-2865	0	0	0	1088	--	--	16.08	16.08	0.00	0.02	0.02	0.18	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	24	-0	-2356	0	0	0	792	--	--	16.08	16.08	0.00	0.01	0.02	0.15	0.00	0.00	20.9
2	24	-0	-1713	0	0	0	583	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
3	24	-0	-1714	0	0	0	624	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
4	24	-0	-1911	0	0	0	594	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
5	24	-0	-1912	0	0	0	634	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
6	24	-0	-1781	0	0	0	540	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
7	24	-0	-1785	0	0	0	674	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
8	24	-0	-1840	0	0	0	543	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
9	24	-0	-1844	0	0	0	678	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
10	24	-0	-1713	0	0	0	583	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
11	24	-0	-1714	0	0	0	624	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
12	24	-0	-1911	0	0	0	594	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9

13	24	-0	-1912	0	0	0	634	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
14	24	-0	-1781	0	0	0	540	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
15	24	-0	-1785	0	0	0	674	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
16	24	-0	-1840	0	0	0	543	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
17	24	-0	-1844	0	0	0	678	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
18	24	-0	-2866	0	0	0	1024	--	--	16.08	16.08	0.00	0.02	0.02	0.18	0.00	0.00	20.9
19	24	-0	-4018	0	0	0	1284	--	--	16.08	16.08	0.00	0.02	0.03	0.25	0.00	0.00	20.9
20	24	-0	-3297	0	0	0	1177	--	--	16.08	16.08	0.00	0.02	0.03	0.21	0.00	0.00	20.9
37	24	-0	-2145	0	0	0	832	--	--	16.08	16.08	0.00	0.01	0.02	0.13	0.00	0.00	20.9
38	24	-0	-4066	0	0	0	1266	--	--	16.08	16.08	0.00	0.02	0.03	0.26	0.00	0.00	20.9
39	24	-0	-2865	0	0	0	1088	--	--	16.08	16.08	0.00	0.02	0.02	0.18	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	48	-0	-2356	0	0	0	-347	--	--	16.08	16.08	0.18	0.01	0.02	0.15	0.00	0.00	20.9
2	48	-0	-1713	0	0	0	-244	--	--	16.08	16.08	0.29	0.00	0.01	0.11	0.00	0.00	20.9
3	48	-0	-1714	0	0	0	-205	--	--	16.08	16.08	0.29	0.00	0.01	0.11	0.00	0.00	20.9
4	48	-0	-1911	0	0	0	-329	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
5	48	-0	-1912	0	0	0	-290	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
6	48	-0	-1781	0	0	0	-320	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
7	48	-0	-1785	0	0	0	-188	--	--	16.08	16.08	0.29	0.00	0.01	0.11	0.00	0.00	20.9
8	48	-0	-1840	0	0	0	-346	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
9	48	-0	-1844	0	0	0	-214	--	--	16.08	16.08	0.29	0.00	0.02	0.12	0.00	0.00	20.9
10	48	-0	-1713	0	0	0	-244	--	--	16.08	16.08	0.29	0.00	0.01	0.11	0.00	0.00	20.9
11	48	-0	-1714	0	0	0	-205	--	--	16.08	16.08	0.29	0.00	0.01	0.11	0.00	0.00	20.9
12	48	-0	-1911	0	0	0	-329	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
13	48	-0	-1912	0	0	0	-290	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
14	48	-0	-1781	0	0	0	-320	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
15	48	-0	-1785	0	0	0	-188	--	--	16.08	16.08	0.29	0.00	0.01	0.11	0.00	0.00	20.9
16	48	-0	-1840	0	0	0	-346	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
17	48	-0	-1844	0	0	0	-214	--	--	16.08	16.08	0.29	0.00	0.02	0.12	0.00	0.00	20.9
18	48	-0	-2866	0	0	0	-361	--	--	16.08	16.08	0.18	0.01	0.02	0.18	0.00	0.00	20.9
19	48	-0	-4018	0	0	0	-658	--	--	16.08	16.08	0.18	0.01	0.03	0.25	0.00	0.00	20.9
20	48	-0	-3297	0	0	0	-416	--	--	16.08	16.08	0.18	0.01	0.03	0.21	0.00	0.00	20.9
37	48	-0	-2145	0	0	0	-205	--	--	16.08	16.08	0.18	0.00	0.02	0.13	0.00	0.00	20.9
38	48	-0	-4066	0	0	0	-699	--	--	16.08	16.08	0.18	0.01	0.03	0.26	0.00	0.00	20.9
39	48	-0	-2865	0	0	0	-297	--	--	16.08	16.08	0.18	0.00	0.02	0.18	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 150 NI 1780 NF 1794 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-2494	0	0	0	1038	--	--	16.08	16.08	0.00	0.02	0.02	0.16	0.00	0.00	20.9
2	0	-0	-1777	0	0	0	713	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
3	0	-0	-1806	0	0	0	772	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
4	0	-0	-2032	0	0	0	825	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
5	0	-0	-2060	0	0	0	884	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
6	0	-0	-1833	0	0	0	683	--	--	16.08	16.08	0.10	0.01	0.02	0.11	0.00	0.00	20.9
7	0	-0	-1928	0	0	0	881	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
8	0	-0	-1910	0	0	0	717	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
9	0	-0	-2004	0	0	0	914	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
10	0	-0	-1777	0	0	0	713	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
11	0	-0	-1806	0	0	0	772	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
12	0	-0	-2032	0	0	0	825	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
13	0	-0	-2060	0	0	0	884	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
14	0	-0	-1833	0	0	0	683	--	--	16.08	16.08	0.10	0.01	0.02	0.11	0.00	0.00	20.9
15	0	-0	-1928	0	0	0	881	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
16	0	-0	-1910	0	0	0	717	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
17	0	-0	-2004	0	0	0	914	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
18	0	-0	-2586	0	0	0	941	--	--	16.08	16.08	0.00	0.02	0.02	0.16	0.00	0.00	20.9
19	0	-0	-4057	0	0	0	1706	--	--	16.08	16.08	0.00	0.03	0.03	0.25	0.00	0.00	20.9
20	0	-0	-3290	0	0	0	1412	--	--	16.08	16.08	0.00	0.02	0.03	0.21	0.00	0.00	20.9
37	0	-0	-1842	0	0	0	608	--	--	16.08	16.08	0.00	0.01	0.02	0.12	0.00	0.00	20.9
38	0	-0	-4293	0	0	0	1883	--	--	16.08	16.08	0.00	0.03	0.04	0.27	0.00	0.00	20.9
39	0	-0	-3015	0	0	0	1393	--	--	16.08	16.08	0.00	0.02	0.02	0.19	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	24	-0	-2494	0	0	0	1038	--	--	16.08	16.08	0.00	0.02	0.02	0.16	0.00	0.00	20.9
2	24	-0	-1777	0	0	0	713	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
3	24	-0	-1806	0	0	0	772	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
4	24	-0	-2032	0	0	0	825	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
5	24	-0	-2060	0	0	0	884	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
6	24	-0	-1833	0	0	0	683	--	--	16.08	16.08	0.10	0.01	0.02	0.11	0.00	0.00	20.9
7	24	-0	-1928	0	0	0	881	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
8	24	-0	-1910	0	0	0	717	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
9	24	-0	-2004	0	0	0	914	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
10	24	-0	-1777	0	0	0	713	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
11	24	-0	-1806	0	0	0	772	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
12	24	-0	-2032	0	0	0	825	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
13	24	-0	-2060	0	0	0	884	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
14	24	-0	-1833	0	0	0	683	--	--	16.08	16.08	0.10	0.01	0.02	0.11	0.00	0.00	20.9
15	24	-0	-1928	0	0	0	881	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
16	24	-0	-1910	0	0	0	717	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
17	24	-0	-2004	0	0	0	914	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
18	24	-0	-2586	0	0	0	941	--	--	16.08	16.08	0.00	0.02	0.02	0.16	0.00	0.00	20.9
19	24	-0	-4057	0	0	0	1706	--	--	16.08	16.08	0.00	0.03	0.03	0.25	0.00	0.00	20.9
20	24	-0	-3290	0	0	0	1412	--	--	16.08	16.08	0.00	0.02	0.03	0.21	0.00	0.00	20.9
37	24	-0	-1842	0	0	0	608	--	--	16.08	16.08	0.00	0.01	0.02	0.12	0.00	0.00	20.9
38	24	-0	-4293	0	0	0	1883	--	--	16.08	16.08	0.00	0.03	0.04	0.27	0.00	0.00	20.9
39	24	-0	-3015	0	0	0	1393	--	--	16.08	16.08	0.00	0.02	0.02	0.19	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	48	-0	-2494	0	0	0	-168	--	--	16.08	16.08	0.18	0.00	0.02	0.16	0.00	0.00	20.9
2	48	-0	-1777	0	0	0	-146	--	--	16.08	16.08	0.29	0.00	0.01	0.11	0.00	0.00	20.9
3	48	-0	-1806	0	0	0	-100	--	--	16.08	16.08	0.29	0.00	0.01	0.11	0.00	0.00	20.9
4	48	-0	-2032	0	0	0	-157	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
5	48	-0	-2060	0	0	0	-112	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
6	48	-0	-1833	0	0	0	-203	--	--	16.08	16.08	0.29	0.00	0.02	0.11	0.00	0.00	20.9
7	48	-0	-1928	0	0	0	-51	--	--	16.08	16.08	0.29	0.00	0.02	0.12	0.00	0.00	20.9
8	48	-0	-1910	0	0	0	-207	--	--	16.08	16.08	0.29	0.00	0.02	0.12	0.00	0.00	20.9

9	48	-0	-2004	0	0	0	-55	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
10	48	-0	-1777	0	0	0	-146	--	--	16.08	16.08	0.29	0.00	0.01	0.11	0.00	0.00	20.9
11	48	-0	-1806	0	0	0	-100	--	--	16.08	16.08	0.29	0.00	0.01	0.11	0.00	0.00	20.9
12	48	-0	-2032	0	0	0	-157	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
13	48	-0	-2060	0	0	0	-112	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
14	48	-0	-1833	0	0	0	-203	--	--	16.08	16.08	0.29	0.00	0.02	0.11	0.00	0.00	20.9
15	48	-0	-1928	0	0	0	-51	--	--	16.08	16.08	0.29	0.00	0.02	0.12	0.00	0.00	20.9
16	48	-0	-1910	0	0	0	-207	--	--	16.08	16.08	0.29	0.00	0.02	0.12	0.00	0.00	20.9
17	48	-0	-2004	0	0	0	-55	--	--	16.08	16.08	0.29	0.00	0.02	0.13	0.00	0.00	20.9
18	48	-0	-2586	0	0	0	-309	--	--	16.08	16.08	0.18	0.01	0.02	0.16	0.00	0.00	20.9
19	48	-0	-4057	0	0	0	-255	--	--	16.08	16.08	0.18	0.00	0.03	0.25	0.00	0.00	20.9
20	48	-0	-3290	0	0	0	-178	--	--	16.08	16.08	0.18	0.00	0.03	0.21	0.00	0.00	20.9
37	48	-0	-1842	0	0	0	-282	--	--	16.08	16.08	0.18	0.00	0.02	0.12	0.00	0.00	20.9
38	48	-0	-4293	0	0	0	-192	--	--	16.08	16.08	0.18	0.00	0.04	0.27	0.00	0.00	20.9
39	48	-0	-3015	0	0	0	-64	--	--	16.08	16.08	0.18	0.00	0.02	0.19	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 151 NI 1693 NF 1780 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-356	0	0	0	430	--	--	16.08	16.08	0.00	0.01	0.00	0.02	0.00	0.00	20.9
2	0	-0	135	0	0	0	86	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
3	0	-0	117	0	0	0	136	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
4	0	-0	-664	0	0	0	525	--	--	16.08	16.08	0.10	0.01	0.01	0.04	0.00	0.00	20.9
5	0	-0	-683	0	0	0	576	--	--	16.08	16.08	0.10	0.01	0.01	0.04	0.00	0.00	20.9
6	0	-0	-123	0	0	0	180	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
7	0	-0	-184	0	0	0	349	--	--	16.08	16.08	0.10	0.01	0.00	0.01	0.00	0.00	20.9
8	0	-0	-363	0	0	0	312	--	--	16.08	16.08	0.10	0.01	0.00	0.02	0.00	0.00	20.9
9	0	-0	-424	0	0	0	481	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
10	0	-0	135	0	0	0	86	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
11	0	-0	117	0	0	0	136	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
12	0	-0	-664	0	0	0	525	--	--	16.08	16.08	0.10	0.01	0.01	0.04	0.00	0.00	20.9
13	0	-0	-683	0	0	0	576	--	--	16.08	16.08	0.10	0.01	0.01	0.04	0.00	0.00	20.9
14	0	-0	-123	0	0	0	180	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
15	0	-0	-184	0	0	0	349	--	--	16.08	16.08	0.10	0.01	0.00	0.01	0.00	0.00	20.9
16	0	-0	-363	0	0	0	312	--	--	16.08	16.08	0.10	0.01	0.00	0.02	0.00	0.00	20.9
17	0	-0	-424	0	0	0	481	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
18	0	-0	2357	0	0	0	-1087	--	--	16.08	16.08	0.18	0.02	0.02	0.15	0.00	0.00	20.9
19	0	-0	-1267	0	0	0	1077	--	--	16.08	16.08	0.00	0.02	0.01	0.08	0.00	0.00	20.9
20	0	-0	343	0	0	0	172	--	--	16.08	16.08	0.00	0.00	0.00	0.02	0.00	0.00	20.9
37	0	-0	3259	0	0	0	-1650	--	--	16.08	16.08	0.18	0.03	0.03	0.20	0.00	0.00	20.9
38	0	-0	-2782	0	0	0	1958	--	--	16.08	16.08	0.00	0.03	0.02	0.17	0.00	0.00	20.9
39	0	-0	-98	0	0	0	448	--	--	16.08	16.08	0.00	0.01	0.00	0.01	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	24	-0	-356	0	0	0	430	--	--	16.08	16.08	0.00	0.01	0.00	0.02	0.00	0.00	20.9
2	24	-0	135	0	0	0	263	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
3	24	-0	117	0	0	0	290	--	--	16.08	16.08	0.10	0.01	0.00	0.01	0.00	0.00	20.9
4	24	-0	-664	0	0	0	525	--	--	16.08	16.08	0.10	0.01	0.01	0.04	0.00	0.00	20.9
5	24	-0	-683	0	0	0	576	--	--	16.08	16.08	0.10	0.01	0.01	0.04	0.00	0.00	20.9
6	24	-0	-123	0	0	0	180	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
7	24	-0	-184	0	0	0	349	--	--	16.08	16.08	0.10	0.01	0.00	0.01	0.00	0.00	20.9
8	24	-0	-363	0	0	0	312	--	--	16.08	16.08	0.10	0.01	0.00	0.02	0.00	0.00	20.9
9	24	-0	-424	0	0	0	481	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
10	24	-0	135	0	0	0	263	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
11	24	-0	117	0	0	0	290	--	--	16.08	16.08	0.10	0.01	0.00	0.01	0.00	0.00	20.9
12	24	-0	-664	0	0	0	525	--	--	16.08	16.08	0.10	0.01	0.01	0.04	0.00	0.00	20.9
13	24	-0	-683	0	0	0	576	--	--	16.08	16.08	0.10	0.01	0.01	0.04	0.00	0.00	20.9
14	24	-0	-123	0	0	0	180	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
15	24	-0	-184	0	0	0	349	--	--	16.08	16.08	0.10	0.01	0.00	0.01	0.00	0.00	20.9
16	24	-0	-363	0	0	0	312	--	--	16.08	16.08	0.10	0.01	0.00	0.02	0.00	0.00	20.9
17	24	-0	-424	0	0	0	481	--	--	16.08	16.08	0.10	0.01	0.00	0.03	0.00	0.00	20.9
18	24	-0	2357	0	0	0	-1087	--	--	16.08	16.08	0.18	0.02	0.02	0.15	0.00	0.00	20.9
19	24	-0	-1267	0	0	0	1077	--	--	16.08	16.08	0.00	0.02	0.01	0.08	0.00	0.00	20.9
20	24	-0	343	0	0	0	622	--	--	16.08	16.08	0.00	0.01	0.00	0.02	0.00	0.00	20.9
37	24	-0	3259	0	0	0	-1650	--	--	16.08	16.08	0.18	0.03	0.03	0.20	0.00	0.00	20.9
38	24	-0	-2782	0	0	0	1958	--	--	16.08	16.08	0.00	0.03	0.02	0.17	0.00	0.00	20.9
39	24	-0	-98	0	0	0	448	--	--	16.08	16.08	0.00	0.01	0.00	0.01	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	48	-0	-356	0	0	0	258	--	--	16.08	16.08	0.00	0.00	0.00	0.02	0.00	0.00	20.9
2	48	-0	135	0	0	0	151	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
3	48	-0	117	0	0	0	193	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
4	48	-0	-664	0	0	0	204	--	--	16.08	16.08	0.10	0.00	0.01	0.04	0.00	0.00	20.9
5	48	-0	-683	0	0	0	246	--	--	16.08	16.08	0.10	0.00	0.01	0.04	0.00	0.00	20.9
6	48	-0	-123	0	0	0	121	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
7	48	-0	-184	0	0	0	260	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
8	48	-0	-363	0	0	0	137	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
9	48	-0	-424	0	0	0	276	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
10	48	-0	135	0	0	0	151	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
11	48	-0	117	0	0	0	193	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
12	48	-0	-664	0	0	0	204	--	--	16.08	16.08	0.10	0.00	0.01	0.04	0.00	0.00	20.9
13	48	-0	-683	0	0	0	246	--	--	16.08	16.08	0.10	0.00	0.01	0.04	0.00	0.00	20.9
14	48	-0	-123	0	0	0	121	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
15	48	-0	-184	0	0	0	260	--	--	16.08	16.08	0.10	0.00	0.00	0.01	0.00	0.00	20.9
16	48	-0	-363	0	0	0	137	--	--	16.08	16.08	0.10	0.00	0.00	0.02	0.00	0.00	20.9
17	48	-0	-424	0	0	0	276	--	--	16.08	16.08	0.10	0.00	0.00	0.03	0.00	0.00	20.9
18	48	-0	2357	0	0	0	52	--	--	16.08	16.08	0.00	0.00	0.02	0.15	0.00	0.00	20.9
19	48	-0	-1267	0	0	0	465	--	--	16.08	16.08	0.00	0.01	0.01	0.08	0.00	0.00	20.9
20	48	-0	343	0	0	0	338	--	--	16.08	16.08	0.00	0.01	0.00	0.02	0.00	0.00	20.9
37	48	-0	3259	0	0	0	-1650	--	--	16.08	16.08	0.18	0.03	0.03	0.20	0.00	0.00	20.9
38	48	-0	-2782	0	0	0	613	--	--	16.08	16.08	0.00	0.01	0.02	0.17	0.00	0.00	20.9
39	48	-0	-98	0	0	0	401	--	--	16.08	16.08	0.00	0.01	0.00	0.01	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 152 NI 1801 NF 1693 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	3313	0	0	0	104	--	--	16.08	16.08	0.00	0.00	0.03	0.21	0.00	0.00	20.9
2	0	-0	2561	0	0	0	25	--	--	16.08	16.08	0.10	0.00	0.02	0.16	0.00	0.00	20.9
3	0	-0	2541	0	0	0	75	--	--	16.08	16.08	0.10	0.00	0.02	0.16	0.00	0.00	20.9
4	0	-0	2556	0	0	0	86	--	--	16.08	16.08	0.10	0.00	0.02	0.16	0.00	0.00	20.9
5	0	-0	2536	0	0	0	135	--	--	16.08	16.08	0.10	0.00	0.02	0.16	0.00	0.00	20.9
6	0	-0	2582	0	0	0	-11	--	--	16.08	16.08	0.29	0.00	0.02	0.16	0.00	0.00	20.9
7	0	-0	2517	0	0	0	154	--	--	16.08	16.08	0.10	0.00	0.02	0.16	0.00	0.00	20.9
8	0	-0	2580	0	0	0	7	--	--	16.08	16.08	0.10	0.00	0.02	0.16	0.00	0.00	20.9
9	0	-0	2515	0	0	0	172	--	--	16.08	16.08	0.10	0.00	0.02	0.16	0.00	0.00	20.9
10	0	-0	2561	0	0	0	25	--	--	16.08	16.08	0.10	0.00	0.02	0.16	0.00	0.00	20.9
11	0	-0	2541	0	0	0	75	--	--	16.08	16.08	0.10	0.00	0.02	0.16	0.00	0.00	20.9
12	0	-0	2556	0	0	0	86	--	--	16.08	16.08	0.10	0.00	0.02	0.16	0.00	0.00	20.9
13	0	-0	2536	0	0	0	135	--	--	16.08	16.08	0.10	0.00	0.02	0.16	0.00	0.00	20.9
14	0	-0	2582	0	0	0	-11	--	--	16.08	16.08	0.29	0.00	0.02	0.16	0.00	0.00	20.9
15	0	-0	2517	0	0	0	154	--	--	16.08	16.08	0.10	0.00	0.02	0.16	0.00	0.00	20.9
16	0	-0	2580	0	0	0	7	--	--	16.08	16.08	0.10	0.00	0.02	0.16	0.00	0.00	20.9
17	0	-0	2515	0	0	0	172	--	--	16.08	16.08	0.10	0.00	0.02	0.16	0.00	0.00	20.9
18	0	-0	4223	0	0	0	251	--	--	16.08	16.08	0.00	0.00	0.03	0.26	0.00	0.00	20.9
19	0	-0	4489	0	0	0	555	--	--	16.08	16.08	0.00	0.01	0.04	0.28	0.00	0.00	20.9
20	0	-0	4135	0	0	0	472	--	--	16.08	16.08	0.00	0.01	0.03	0.26	0.00	0.00	20.9
37	0	-0	3798	0	0	0	66	--	--	16.08	16.08	0.00	0.00	0.03	0.24	0.00	0.00	20.9
38	0	-0	4241	0	0	0	573	--	--	16.08	16.08	0.00	0.01	0.03	0.27	0.00	0.00	20.9
39	0	-0	3653	0	0	0	433	--	--	16.08	16.08	0.00	0.01	0.03	0.23	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	3313	0	0	0	4549	--	--	16.08	16.08	0.00	0.08	0.03	0.21	0.00	0.00	20.9
2	27	-0	2561	0	0	0	3461	--	--	16.08	16.08	0.10	0.06	0.02	0.16	0.00	0.00	20.9
3	27	-0	2541	0	0	0	3484	--	--	16.08	16.08	0.10	0.06	0.02	0.16	0.00	0.00	20.9
4	27	-0	2556	0	0	0	3515	--	--	16.08	16.08	0.10	0.06	0.02	0.16	0.00	0.00	20.9
5	27	-0	2536	0	0	0	3537	--	--	16.08	16.08	0.10	0.06	0.02	0.16	0.00	0.00	20.9
6	27	-0	2582	0	0	0	3452	--	--	16.08	16.08	0.10	0.06	0.02	0.16	0.00	0.00	20.9
7	27	-0	2517	0	0	0	3530	--	--	16.08	16.08	0.10	0.06	0.02	0.16	0.00	0.00	20.9
8	27	-0	2580	0	0	0	3468	--	--	16.08	16.08	0.10	0.06	0.02	0.16	0.00	0.00	20.9
9	27	-0	2515	0	0	0	3546	--	--	16.08	16.08	0.10	0.06	0.02	0.16	0.00	0.00	20.9
10	27	-0	2561	0	0	0	3461	--	--	16.08	16.08	0.10	0.06	0.02	0.16	0.00	0.00	20.9
11	27	-0	2541	0	0	0	3484	--	--	16.08	16.08	0.10	0.06	0.02	0.16	0.00	0.00	20.9
12	27	-0	2556	0	0	0	3515	--	--	16.08	16.08	0.10	0.06	0.02	0.16	0.00	0.00	20.9
13	27	-0	2536	0	0	0	3537	--	--	16.08	16.08	0.10	0.06	0.02	0.16	0.00	0.00	20.9
14	27	-0	2582	0	0	0	3452	--	--	16.08	16.08	0.10	0.06	0.02	0.16	0.00	0.00	20.9
15	27	-0	2517	0	0	0	3530	--	--	16.08	16.08	0.10	0.06	0.02	0.16	0.00	0.00	20.9
16	27	-0	2580	0	0	0	3468	--	--	16.08	16.08	0.10	0.06	0.02	0.16	0.00	0.00	20.9
17	27	-0	2515	0	0	0	3546	--	--	16.08	16.08	0.10	0.06	0.02	0.16	0.00	0.00	20.9
18	27	-0	4223	0	0	0	5917	--	--	16.08	16.08	0.00	0.10	0.03	0.26	0.00	0.00	20.9
19	27	-0	4489	0	0	0	6577	--	--	16.08	16.08	0.00	0.11	0.04	0.28	0.00	0.00	20.9
20	27	-0	4135	0	0	0	6019	--	--	16.08	16.08	0.00	0.10	0.03	0.26	0.00	0.00	20.9
37	27	-0	3798	0	0	0	5161	--	--	16.08	16.08	0.00	0.09	0.03	0.24	0.00	0.00	20.9
38	27	-0	4241	0	0	0	6262	--	--	16.08	16.08	0.00	0.11	0.03	0.27	0.00	0.00	20.9
39	27	-0	3653	0	0	0	5333	--	--	16.08	16.08	0.00	0.09	0.03	0.23	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	3313	0	0	0	1912	--	--	16.08	16.08	0.00	0.03	0.03	0.21	0.00	0.00	20.9
2	55	-0	2561	0	0	0	1422	--	--	16.08	16.08	0.10	0.03	0.02	0.16	0.00	0.00	20.9
3	55	-0	2541	0	0	0	1461	--	--	16.08	16.08	0.10	0.03	0.02	0.16	0.00	0.00	20.9
4	55	-0	2556	0	0	0	1480	--	--	16.08	16.08	0.10	0.03	0.02	0.16	0.00	0.00	20.9
5	55	-0	2536	0	0	0	1519	--	--	16.08	16.08	0.10	0.03	0.02	0.16	0.00	0.00	20.9
6	55	-0	2582	0	0	0	1397	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
7	55	-0	2517	0	0	0	1526	--	--	16.08	16.08	0.10	0.03	0.02	0.16	0.00	0.00	20.9
8	55	-0	2580	0	0	0	1415	--	--	16.08	16.08	0.10	0.03	0.02	0.16	0.00	0.00	20.9
9	55	-0	2515	0	0	0	1544	--	--	16.08	16.08	0.10	0.03	0.02	0.16	0.00	0.00	20.9
10	55	-0	2561	0	0	0	1422	--	--	16.08	16.08	0.10	0.03	0.02	0.16	0.00	0.00	20.9
11	55	-0	2541	0	0	0	1461	--	--	16.08	16.08	0.10	0.03	0.02	0.16	0.00	0.00	20.9
12	55	-0	2556	0	0	0	1480	--	--	16.08	16.08	0.10	0.03	0.02	0.16	0.00	0.00	20.9
13	55	-0	2536	0	0	0	1519	--	--	16.08	16.08	0.10	0.03	0.02	0.16	0.00	0.00	20.9
14	55	-0	2582	0	0	0	1397	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
15	55	-0	2517	0	0	0	1526	--	--	16.08	16.08	0.10	0.03	0.02	0.16	0.00	0.00	20.9
16	55	-0	2580	0	0	0	1415	--	--	16.08	16.08	0.10	0.03	0.02	0.16	0.00	0.00	20.9
17	55	-0	2515	0	0	0	1544	--	--	16.08	16.08	0.10	0.03	0.02	0.16	0.00	0.00	20.9
18	55	-0	4223	0	0	0	2555	--	--	16.08	16.08	0.00	0.04	0.03	0.26	0.00	0.00	20.9
19	55	-0	4489	0	0	0	3004	--	--	16.08	16.08	0.00	0.05	0.04	0.28	0.00	0.00	20.9
20	55	-0	4135	0	0	0	2727	--	--	16.08	16.08	0.00	0.05	0.03	0.26	0.00	0.00	20.9
37	55	-0	3798	0	0	0	2137	--	--	16.08	16.08	0.00	0.04	0.03	0.24	0.00	0.00	20.9
38	55	-0	4241	0	0	0	2886	--	--	16.08	16.08	0.00	0.05	0.03	0.27	0.00	0.00	20.9
39	55	-0	3653	0	0	0	2425	--	--	16.08	16.08	0.00	0.04	0.03	0.23	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 153 NI 1785 NF 1801 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	4154	0	0	0	-782	--	--	16.08	16.08	0.18	0.01	0.03	0.26	0.00	0.00	20.9
2	0	-0	3322	0	0	0	-691	--	--	16.08	16.08	0.29	0.01	0.03	0.21	0.00	0.00	20.9
3	0	-0	3352	0	0	0	-657	--	--	16.08	16.08	0.29	0.01	0.03	0.21	0.00	0.00	20.9
4	0	-0	3038	0	0	0	-546	--	--	16.08	16.08	0.29	0.01	0.03	0.19	0.00	0.00	20.9
5	0	-0	3069	0	0	0	-513	--	--	16.08	16.08	0.29	0.01	0.03	0.19	0.00	0.00	20.9
6	0	-0	3187	0	0	0	-679	--	--	16.08	16.08	0.29	0.01	0.03	0.20	0.00	0.00	20.9
7	0	-0	3288	0	0	0	-568	--	--	16.08	16.08	0.29	0.01	0.03	0.21	0.00	0.00	20.9
8	0	-0	3102	0	0	0	-635	--	--	16.08	16.08	0.29	0.01	0.03	0.19	0.00	0.00	20.9
9	0	-0	3203	0	0	0	-525	--	--	16.08	16.08	0.29	0.01	0.03	0.20	0.00	0.00	20.9
10	0	-0	3322	0	0	0	-691	--	--	16.08	16.08	0.29	0.01	0.03	0.21	0.00	0.00	20.9
11	0	-0	3352	0	0	0	-657	--	--	16.08	16.08	0.29	0.01	0.03	0.21	0.00	0.00	20.9
12	0	-0	3038	0	0	0	-546	--	--	16.08	16.08	0.29	0.01	0.03	0.19	0.00	0.00	20.9
13	0	-0	3069	0	0	0	-513	--	--	16.08	16.08	0.29	0.01	0.03	0.19	0.00	0.00	20.9
14	0	-0	3187	0	0	0	-679	--	--	16.08	16.08	0.29	0.01	0.03	0.20	0.00	0.00	20.9
15	0	-0	3288	0	0	0	-568	--	--	16.08	16.08	0.29	0.01	0.03	0.21	0.00	0.00	20.9
16	0	-0	3102	0	0	0	-635	--	--	16.08	16.08	0.29	0.01	0.03	0.19	0.00	0.00	20.9

17	0	-0	3203	0	0	0	-525	--	--	16.08	16.08	0.29	0.01	0.03	0.20	0.00	0.00	20.9
18	0	-0	6109	0	0	0	-1192	--	--	16.08	16.08	0.18	0.02	0.05	0.38	0.00	0.00	20.9
19	0	-0	5462	0	0	0	-639	--	--	16.08	16.08	0.18	0.01	0.05	0.34	0.00	0.00	20.9
20	0	-0	5610	0	0	0	-824	--	--	16.08	16.08	0.18	0.01	0.05	0.35	0.00	0.00	20.9
37	0	-0	5800	0	0	0	-1321	--	--	16.08	16.08	0.18	0.02	0.05	0.36	0.00	0.00	20.9
38	0	-0	4720	0	0	0	-400	--	--	16.08	16.08	0.18	0.01	0.04	0.30	0.00	0.00	20.9
39	0	-0	4968	0	0	0	-708	--	--	16.08	16.08	0.18	0.01	0.04	0.31	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	4154	0	0	0	4790	--	--	16.08	16.08	0.00	0.08	0.03	0.26	0.00	0.00	20.9
2	27	-0	3322	0	0	0	3766	--	--	16.08	16.08	0.10	0.07	0.03	0.21	0.00	0.00	20.9
3	27	-0	3352	0	0	0	3839	--	--	16.08	16.08	0.10	0.07	0.03	0.21	0.00	0.00	20.9
4	27	-0	3038	0	0	0	3529	--	--	16.08	16.08	0.10	0.06	0.03	0.19	0.00	0.00	20.9
5	27	-0	3069	0	0	0	3604	--	--	16.08	16.08	0.10	0.06	0.03	0.19	0.00	0.00	20.9
6	27	-0	3187	0	0	0	3597	--	--	16.08	16.08	0.10	0.06	0.03	0.20	0.00	0.00	20.9
7	27	-0	3288	0	0	0	3843	--	--	16.08	16.08	0.10	0.07	0.03	0.21	0.00	0.00	20.9
8	27	-0	3102	0	0	0	3526	--	--	16.08	16.08	0.10	0.06	0.03	0.19	0.00	0.00	20.9
9	27	-0	3203	0	0	0	3772	--	--	16.08	16.08	0.10	0.07	0.03	0.20	0.00	0.00	20.9
10	27	-0	3322	0	0	0	3766	--	--	16.08	16.08	0.10	0.07	0.03	0.21	0.00	0.00	20.9
11	27	-0	3352	0	0	0	3839	--	--	16.08	16.08	0.10	0.07	0.03	0.21	0.00	0.00	20.9
12	27	-0	3038	0	0	0	3529	--	--	16.08	16.08	0.10	0.06	0.03	0.19	0.00	0.00	20.9
13	27	-0	3069	0	0	0	3604	--	--	16.08	16.08	0.10	0.06	0.03	0.19	0.00	0.00	20.9
14	27	-0	3187	0	0	0	3597	--	--	16.08	16.08	0.10	0.06	0.03	0.20	0.00	0.00	20.9
15	27	-0	3288	0	0	0	3843	--	--	16.08	16.08	0.10	0.07	0.03	0.21	0.00	0.00	20.9
16	27	-0	3102	0	0	0	3526	--	--	16.08	16.08	0.10	0.06	0.03	0.19	0.00	0.00	20.9
17	27	-0	3203	0	0	0	3772	--	--	16.08	16.08	0.10	0.07	0.03	0.20	0.00	0.00	20.9
18	27	-0	6109	0	0	0	7003	--	--	16.08	16.08	0.00	0.12	0.05	0.38	0.00	0.00	20.9
19	27	-0	5462	0	0	0	6688	--	--	16.08	16.08	0.00	0.11	0.05	0.34	0.00	0.00	20.9
20	27	-0	5610	0	0	0	6702	--	--	16.08	16.08	0.00	0.11	0.05	0.35	0.00	0.00	20.9
37	27	-0	5800	0	0	0	6459	--	--	16.08	16.08	0.00	0.11	0.05	0.36	0.00	0.00	20.9
38	27	-0	4720	0	0	0	5932	--	--	16.08	16.08	0.00	0.10	0.04	0.30	0.00	0.00	20.9
39	27	-0	4968	0	0	0	5956	--	--	16.08	16.08	0.00	0.10	0.04	0.31	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	4154	0	0	0	1483	--	--	16.08	16.08	0.00	0.03	0.03	0.26	0.00	0.00	20.9
2	55	-0	3322	0	0	0	1121	--	--	16.08	16.08	0.10	0.02	0.03	0.21	0.00	0.00	20.9
3	55	-0	3352	0	0	0	1171	--	--	16.08	16.08	0.10	0.02	0.03	0.21	0.00	0.00	20.9
4	55	-0	3038	0	0	0	1111	--	--	16.08	16.08	0.10	0.02	0.03	0.19	0.00	0.00	20.9
5	55	-0	3069	0	0	0	1161	--	--	16.08	16.08	0.10	0.02	0.03	0.19	0.00	0.00	20.9
6	55	-0	3187	0	0	0	1060	--	--	16.08	16.08	0.10	0.02	0.03	0.20	0.00	0.00	20.9
7	55	-0	3288	0	0	0	1225	--	--	16.08	16.08	0.10	0.02	0.03	0.21	0.00	0.00	20.9
8	55	-0	3102	0	0	0	1057	--	--	16.08	16.08	0.10	0.02	0.03	0.19	0.00	0.00	20.9
9	55	-0	3203	0	0	0	1222	--	--	16.08	16.08	0.10	0.02	0.03	0.20	0.00	0.00	20.9
10	55	-0	3322	0	0	0	1121	--	--	16.08	16.08	0.10	0.02	0.03	0.21	0.00	0.00	20.9
11	55	-0	3352	0	0	0	1171	--	--	16.08	16.08	0.10	0.02	0.03	0.21	0.00	0.00	20.9
12	55	-0	3038	0	0	0	1111	--	--	16.08	16.08	0.10	0.02	0.03	0.19	0.00	0.00	20.9
13	55	-0	3069	0	0	0	1161	--	--	16.08	16.08	0.10	0.02	0.03	0.19	0.00	0.00	20.9
14	55	-0	3187	0	0	0	1060	--	--	16.08	16.08	0.10	0.02	0.03	0.20	0.00	0.00	20.9
15	55	-0	3288	0	0	0	1225	--	--	16.08	16.08	0.10	0.02	0.03	0.21	0.00	0.00	20.9
16	55	-0	3102	0	0	0	1057	--	--	16.08	16.08	0.10	0.02	0.03	0.19	0.00	0.00	20.9
17	55	-0	3203	0	0	0	1222	--	--	16.08	16.08	0.10	0.02	0.03	0.20	0.00	0.00	20.9
18	55	-0	6109	0	0	0	2140	--	--	16.08	16.08	0.00	0.04	0.05	0.38	0.00	0.00	20.9
19	55	-0	5462	0	0	0	2340	--	--	16.08	16.08	0.00	0.04	0.05	0.34	0.00	0.00	20.9
20	55	-0	5610	0	0	0	2236	--	--	16.08	16.08	0.00	0.04	0.05	0.35	0.00	0.00	20.9
37	55	-0	5800	0	0	0	1842	--	--	16.08	16.08	0.00	0.03	0.05	0.36	0.00	0.00	20.9
38	55	-0	4720	0	0	0	2175	--	--	16.08	16.08	0.00	0.04	0.04	0.30	0.00	0.00	20.9
39	55	-0	4968	0	0	0	2001	--	--	16.08	16.08	0.00	0.03	0.04	0.31	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 154 NI 1786 NF 1785 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	3212	0	0	0	-1282	--	--	16.08	16.08	0.18	0.02	0.03	0.20	0.00	0.00	20.9
2	0	-0	2562	0	0	0	-1086	--	--	16.08	16.08	0.29	0.02	0.02	0.16	0.00	0.00	20.9
3	0	-0	2625	0	0	0	-1058	--	--	16.08	16.08	0.29	0.02	0.02	0.16	0.00	0.00	20.9
4	0	-0	2317	0	0	0	-914	--	--	16.08	16.08	0.29	0.02	0.02	0.15	0.00	0.00	20.9
5	0	-0	2380	0	0	0	-886	--	--	16.08	16.08	0.29	0.02	0.02	0.15	0.00	0.00	20.9
6	0	-0	2403	0	0	0	-1059	--	--	16.08	16.08	0.29	0.02	0.02	0.15	0.00	0.00	20.9
7	0	-0	2613	0	0	0	-965	--	--	16.08	16.08	0.29	0.02	0.02	0.16	0.00	0.00	20.9
8	0	-0	2329	0	0	0	-1007	--	--	16.08	16.08	0.29	0.02	0.02	0.15	0.00	0.00	20.9
9	0	-0	2539	0	0	0	-913	--	--	16.08	16.08	0.29	0.02	0.02	0.16	0.00	0.00	20.9
10	0	-0	2562	0	0	0	-1086	--	--	16.08	16.08	0.29	0.02	0.02	0.16	0.00	0.00	20.9
11	0	-0	2625	0	0	0	-1058	--	--	16.08	16.08	0.29	0.02	0.02	0.16	0.00	0.00	20.9
12	0	-0	2317	0	0	0	-914	--	--	16.08	16.08	0.29	0.02	0.02	0.15	0.00	0.00	20.9
13	0	-0	2380	0	0	0	-886	--	--	16.08	16.08	0.29	0.02	0.02	0.15	0.00	0.00	20.9
14	0	-0	2403	0	0	0	-1059	--	--	16.08	16.08	0.29	0.02	0.02	0.15	0.00	0.00	20.9
15	0	-0	2613	0	0	0	-965	--	--	16.08	16.08	0.29	0.02	0.02	0.16	0.00	0.00	20.9
16	0	-0	2329	0	0	0	-1007	--	--	16.08	16.08	0.29	0.02	0.02	0.15	0.00	0.00	20.9
17	0	-0	2539	0	0	0	-913	--	--	16.08	16.08	0.29	0.02	0.02	0.16	0.00	0.00	20.9
18	0	-0	4724	0	0	0	-1925	--	--	16.08	16.08	0.18	0.03	0.04	0.30	0.00	0.00	20.9
19	0	-0	4193	0	0	0	-1316	--	--	16.08	16.08	0.18	0.02	0.03	0.26	0.00	0.00	20.9
20	0	-0	4428	0	0	0	-1510	--	--	16.08	16.08	0.18	0.03	0.04	0.28	0.00	0.00	20.9
37	0	-0	4501	0	0	0	-2008	--	--	16.08	16.08	0.18	0.03	0.04	0.28	0.00	0.00	20.9
38	0	-0	3616	0	0	0	-992	--	--	16.08	16.08	0.18	0.02	0.03	0.23	0.00	0.00	20.9
39	0	-0	4008	0	0	0	-1316	--	--	16.08	16.08	0.18	0.02	0.03	0.25	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	3212	0	0	0	-1282	--	--	16.08	16.08	0.18	0.02	0.03	0.20	0.00	0.00	20.9
2	27	-0	2562	0	0	0	-1086	--	--	16.08	16.08	0.29	0.02	0.02	0.16	0.00	0.00	20.9
3	27	-0	2625	0	0	0	-1058	--	--	16.08	16.08	0.29	0.02	0.02	0.16	0.00	0.00	20.9
4	27	-0	2317	0	0	0	-914	--	--	16.08	16.08	0.29	0.02	0.02	0.15	0.00	0.00	20.9
5	27	-0	2380	0	0	0	-886	--	--	16.08	16.08	0.29	0.02	0.02	0.15	0.00	0.00	20.9
6	27	-0	2403	0	0	0	-1059	--	--	16.08	16.08	0.29	0.02	0.02	0.15	0.00	0.00	20.9
7	27	-0	2613	0	0	0	-965	--	--	16.08	16.08	0.29	0.02	0.02	0.16	0.00	0.00	20.9
8	27	-0	2329	0	0	0	-1007	--	--	16.08	16.08	0.29	0.02	0.02	0.15	0.00	0.00	20.9
9	27	-0	2539	0	0	0	-913	--	--	16.08	16.08	0.29	0.02	0.02	0.16	0.00	0.00	20.9
10	27	-0	2562	0	0	0	-1086	--	--	16.08	16.08	0.29	0.02	0.02	0.16	0.00	0.00	20.9
11	27	-0	2625	0	0	0	-1058	--	--	16.08	16.08	0.29	0.02	0.02	0.16	0.00	0.00	20.9
12	27	-0	2317	0	0	0	-914	--	--	16.08	16.08	0.29	0.02	0.02	0.15	0.00	0.00	20.9

13	27	-0	2380	0	0	0	-886	--	--	16.08	16.08	0.29	0.02	0.02	0.15	0.00	0.00	20.9
14	27	-0	2403	0	0	0	-1059	--	--	16.08	16.08	0.29	0.02	0.02	0.15	0.00	0.00	20.9
15	27	-0	2613	0	0	0	-965	--	--	16.08	16.08	0.29	0.02	0.02	0.16	0.00	0.00	20.9
16	27	-0	2329	0	0	0	-1007	--	--	16.08	16.08	0.29	0.02	0.02	0.15	0.00	0.00	20.9
17	27	-0	2539	0	0	0	-913	--	--	16.08	16.08	0.29	0.02	0.02	0.16	0.00	0.00	20.9
18	27	-0	4724	0	0	0	-1925	--	--	16.08	16.08	0.18	0.03	0.04	0.30	0.00	0.00	20.9
19	27	-0	4193	0	0	0	-1316	--	--	16.08	16.08	0.18	0.02	0.03	0.26	0.00	0.00	20.9
20	27	-0	4428	0	0	0	-1510	--	--	16.08	16.08	0.18	0.03	0.04	0.28	0.00	0.00	20.9
37	27	-0	4501	0	0	0	-2008	--	--	16.08	16.08	0.18	0.03	0.04	0.28	0.00	0.00	20.9
38	27	-0	3616	0	0	0	-992	--	--	16.08	16.08	0.18	0.02	0.03	0.23	0.00	0.00	20.9
39	27	-0	4008	0	0	0	-1316	--	--	16.08	16.08	0.18	0.02	0.03	0.25	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	3212	0	0	0	471	--	--	16.08	16.08	0.00	0.01	0.03	0.20	0.00	0.00	20.9
2	55	-0	2562	0	0	0	312	--	--	16.08	16.08	0.10	0.01	0.02	0.16	0.00	0.00	20.9
3	55	-0	2625	0	0	0	374	--	--	16.08	16.08	0.10	0.01	0.02	0.16	0.00	0.00	20.9
4	55	-0	2317	0	0	0	350	--	--	16.08	16.08	0.10	0.01	0.02	0.15	0.00	0.00	20.9
5	55	-0	2380	0	0	0	412	--	--	16.08	16.08	0.10	0.01	0.02	0.15	0.00	0.00	20.9
6	55	-0	2403	0	0	0	252	--	--	16.08	16.08	0.10	0.00	0.02	0.15	0.00	0.00	20.9
7	55	-0	2613	0	0	0	460	--	--	16.08	16.08	0.10	0.01	0.02	0.16	0.00	0.00	20.9
8	55	-0	2329	0	0	0	264	--	--	16.08	16.08	0.10	0.00	0.02	0.15	0.00	0.00	20.9
9	55	-0	2539	0	0	0	472	--	--	16.08	16.08	0.10	0.01	0.02	0.16	0.00	0.00	20.9
10	55	-0	2562	0	0	0	312	--	--	16.08	16.08	0.10	0.01	0.02	0.16	0.00	0.00	20.9
11	55	-0	2625	0	0	0	374	--	--	16.08	16.08	0.10	0.01	0.02	0.16	0.00	0.00	20.9
12	55	-0	2317	0	0	0	350	--	--	16.08	16.08	0.10	0.01	0.02	0.15	0.00	0.00	20.9
13	55	-0	2380	0	0	0	412	--	--	16.08	16.08	0.10	0.01	0.02	0.15	0.00	0.00	20.9
14	55	-0	2403	0	0	0	252	--	--	16.08	16.08	0.10	0.00	0.02	0.15	0.00	0.00	20.9
15	55	-0	2613	0	0	0	460	--	--	16.08	16.08	0.10	0.01	0.02	0.16	0.00	0.00	20.9
16	55	-0	2329	0	0	0	264	--	--	16.08	16.08	0.10	0.00	0.02	0.15	0.00	0.00	20.9
17	55	-0	2539	0	0	0	472	--	--	16.08	16.08	0.10	0.01	0.02	0.16	0.00	0.00	20.9
18	55	-0	4724	0	0	0	651	--	--	16.08	16.08	0.00	0.01	0.04	0.30	0.00	0.00	20.9
19	55	-0	4193	0	0	0	971	--	--	16.08	16.08	0.00	0.02	0.03	0.26	0.00	0.00	20.9
20	55	-0	4428	0	0	0	906	--	--	16.08	16.08	0.00	0.02	0.04	0.28	0.00	0.00	20.9
37	55	-0	4501	0	0	0	448	--	--	16.08	16.08	0.00	0.01	0.04	0.28	0.00	0.00	20.9
38	55	-0	3616	0	0	0	980	--	--	16.08	16.08	0.00	0.02	0.03	0.23	0.00	0.00	20.9
39	55	-0	4008	0	0	0	871	--	--	16.08	16.08	0.00	0.01	0.03	0.25	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 155 NI 1774 NF 1786 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	1756	0	0	0	-1527	--	--	16.08	16.08	0.18	0.03	0.01	0.11	0.00	0.00	20.9
2	0	-0	1369	0	0	0	-1280	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
3	0	-0	1431	0	0	0	-1261	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
4	0	-0	1270	0	0	0	-1088	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
5	0	-0	1332	0	0	0	-1070	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
6	0	-0	1262	0	0	0	-1234	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
7	0	-0	1469	0	0	0	-1173	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
8	0	-0	1232	0	0	0	-1177	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
9	0	-0	1439	0	0	0	-1116	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
10	0	-0	1369	0	0	0	-1280	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
11	0	-0	1431	0	0	0	-1261	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
12	0	-0	1270	0	0	0	-1088	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
13	0	-0	1332	0	0	0	-1070	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
14	0	-0	1262	0	0	0	-1234	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
15	0	-0	1469	0	0	0	-1173	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
16	0	-0	1232	0	0	0	-1177	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
17	0	-0	1439	0	0	0	-1116	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
18	0	-0	2378	0	0	0	-2287	--	--	16.08	16.08	0.18	0.04	0.02	0.15	0.00	0.00	20.9
19	0	-0	2296	0	0	0	-1646	--	--	16.08	16.08	0.18	0.03	0.02	0.14	0.00	0.00	20.9
20	0	-0	2405	0	0	0	-1865	--	--	16.08	16.08	0.18	0.03	0.02	0.15	0.00	0.00	20.9
37	0	-0	2221	0	0	0	-2349	--	--	16.08	16.08	0.18	0.04	0.02	0.14	0.00	0.00	20.9
38	0	-0	2086	0	0	0	-1280	--	--	16.08	16.08	0.18	0.02	0.02	0.13	0.00	0.00	20.9
39	0	-0	2267	0	0	0	-1646	--	--	16.08	16.08	0.18	0.03	0.02	0.14	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	1756	0	0	0	-1527	--	--	16.08	16.08	0.18	0.03	0.01	0.11	0.00	0.00	20.9
2	27	-0	1369	0	0	0	-1280	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
3	27	-0	1431	0	0	0	-1261	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
4	27	-0	1270	0	0	0	-1088	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
5	27	-0	1332	0	0	0	-1070	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
6	27	-0	1262	0	0	0	-1234	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
7	27	-0	1469	0	0	0	-1173	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
8	27	-0	1232	0	0	0	-1177	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
9	27	-0	1439	0	0	0	-1116	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
10	27	-0	1369	0	0	0	-1280	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
11	27	-0	1431	0	0	0	-1261	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
12	27	-0	1270	0	0	0	-1088	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
13	27	-0	1332	0	0	0	-1070	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
14	27	-0	1262	0	0	0	-1234	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
15	27	-0	1469	0	0	0	-1173	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
16	27	-0	1232	0	0	0	-1177	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
17	27	-0	1439	0	0	0	-1116	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
18	27	-0	2378	0	0	0	-2287	--	--	16.08	16.08	0.18	0.04	0.02	0.15	0.00	0.00	20.9
19	27	-0	2296	0	0	0	-1646	--	--	16.08	16.08	0.18	0.03	0.02	0.14	0.00	0.00	20.9
20	27	-0	2405	0	0	0	-1865	--	--	16.08	16.08	0.18	0.03	0.02	0.15	0.00	0.00	20.9
37	27	-0	2221	0	0	0	-2349	--	--	16.08	16.08	0.18	0.04	0.02	0.14	0.00	0.00	20.9
38	27	-0	2086	0	0	0	-1280	--	--	16.08	16.08	0.18	0.02	0.02	0.13	0.00	0.00	20.9
39	27	-0	2267	0	0	0	-1646	--	--	16.08	16.08	0.18	0.03	0.02	0.14	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	1756	0	0	0	-1527	--	--	16.08	16.08	0.18	0.03	0.01	0.11	0.00	0.00	20.9
2	55	-0	1369	0	0	0	-1280	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
3	55	-0	1431	0	0	0	-1261	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
4	55	-0	1270	0	0	0	-1088	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
5	55	-0	1332	0	0	0	-1070	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
6	55	-0	1262	0	0	0	-1234	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
7	55	-0	1469	0	0	0	-1173	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
8	55	-0	1232	0	0	0	-1177	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9

9	55	-0	1439	0	0	0	-1116	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
10	55	-0	1369	0	0	0	-1280	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
11	55	-0	1431	0	0	0	-1261	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
12	55	-0	1270	0	0	0	-1088	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
13	55	-0	1332	0	0	0	-1070	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
14	55	-0	1262	0	0	0	-1234	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
15	55	-0	1469	0	0	0	-1173	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
16	55	-0	1232	0	0	0	-1177	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
17	55	-0	1439	0	0	0	-1116	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
18	55	-0	2378	0	0	0	-2287	--	--	16.08	16.08	0.18	0.04	0.02	0.15	0.00	0.00	20.9
19	55	-0	2296	0	0	0	-1646	--	--	16.08	16.08	0.18	0.03	0.02	0.14	0.00	0.00	20.9
20	55	-0	2405	0	0	0	-1865	--	--	16.08	16.08	0.18	0.03	0.02	0.15	0.00	0.00	20.9
37	55	-0	2221	0	0	0	-2349	--	--	16.08	16.08	0.18	0.04	0.02	0.14	0.00	0.00	20.9
38	55	-0	2086	0	0	0	-1280	--	--	16.08	16.08	0.18	0.02	0.02	0.13	0.00	0.00	20.9
39	55	-0	2267	0	0	0	-1646	--	--	16.08	16.08	0.18	0.03	0.02	0.14	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 156 NI 1796 NF 1774 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	540	0	0	0	-1474	--	--	16.08	16.08	0.18	0.02	0.00	0.03	0.00	0.00	20.9
2	0	-0	384	0	0	0	-1228	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
3	0	-0	440	0	0	0	-1220	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
4	0	-0	390	0	0	0	-1048	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
5	0	-0	447	0	0	0	-1039	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
6	0	-0	320	0	0	0	-1175	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
7	0	-0	509	0	0	0	-1147	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
8	0	-0	322	0	0	0	-1121	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
9	0	-0	511	0	0	0	-1093	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
10	0	-0	384	0	0	0	-1228	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
11	0	-0	440	0	0	0	-1220	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
12	0	-0	390	0	0	0	-1048	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
13	0	-0	447	0	0	0	-1039	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
14	0	-0	320	0	0	0	-1175	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
15	0	-0	509	0	0	0	-1147	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
16	0	-0	322	0	0	0	-1121	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
17	0	-0	511	0	0	0	-1093	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
18	0	-0	494	0	0	0	-2163	--	--	16.08	16.08	0.18	0.04	0.00	0.03	0.00	0.00	20.9
19	0	-0	711	0	0	0	-1581	--	--	16.08	16.08	0.18	0.03	0.01	0.04	0.00	0.00	20.9
20	0	-0	735	0	0	0	-1802	--	--	16.08	16.08	0.18	0.03	0.01	0.05	0.00	0.00	20.9
37	0	-0	407	0	0	0	-2219	--	--	16.08	16.08	0.18	0.04	0.00	0.03	0.00	0.00	20.9
38	0	-0	768	0	0	0	-1249	--	--	16.08	16.08	0.18	0.02	0.01	0.05	0.00	0.00	20.9
39	0	-0	807	0	0	0	-1617	--	--	16.08	16.08	0.18	0.03	0.01	0.05	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	540	0	0	0	-1474	--	--	16.08	16.08	0.18	0.02	0.00	0.03	0.00	0.00	20.9
2	27	-0	384	0	0	0	-1228	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
3	27	-0	440	0	0	0	-1220	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
4	27	-0	390	0	0	0	-1048	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
5	27	-0	447	0	0	0	-1039	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
6	27	-0	320	0	0	0	-1175	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
7	27	-0	509	0	0	0	-1147	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
8	27	-0	322	0	0	0	-1121	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
9	27	-0	511	0	0	0	-1093	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
10	27	-0	384	0	0	0	-1228	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
11	27	-0	440	0	0	0	-1220	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
12	27	-0	390	0	0	0	-1048	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
13	27	-0	447	0	0	0	-1039	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
14	27	-0	320	0	0	0	-1175	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
15	27	-0	509	0	0	0	-1147	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
16	27	-0	322	0	0	0	-1121	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
17	27	-0	511	0	0	0	-1093	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
18	27	-0	494	0	0	0	-2163	--	--	16.08	16.08	0.18	0.04	0.00	0.03	0.00	0.00	20.9
19	27	-0	711	0	0	0	-1581	--	--	16.08	16.08	0.18	0.03	0.01	0.04	0.00	0.00	20.9
20	27	-0	735	0	0	0	-1802	--	--	16.08	16.08	0.18	0.03	0.01	0.05	0.00	0.00	20.9
37	27	-0	407	0	0	0	-2219	--	--	16.08	16.08	0.18	0.04	0.00	0.03	0.00	0.00	20.9
38	27	-0	768	0	0	0	-1249	--	--	16.08	16.08	0.18	0.02	0.01	0.05	0.00	0.00	20.9
39	27	-0	807	0	0	0	-1617	--	--	16.08	16.08	0.18	0.03	0.01	0.05	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	540	0	0	0	-1474	--	--	16.08	16.08	0.18	0.02	0.00	0.03	0.00	0.00	20.9
2	55	-0	384	0	0	0	-1228	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
3	55	-0	440	0	0	0	-1220	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
4	55	-0	390	0	0	0	-1048	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
5	55	-0	447	0	0	0	-1039	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
6	55	-0	320	0	0	0	-1175	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
7	55	-0	509	0	0	0	-1147	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
8	55	-0	322	0	0	0	-1121	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
9	55	-0	511	0	0	0	-1093	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
10	55	-0	384	0	0	0	-1228	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
11	55	-0	440	0	0	0	-1220	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
12	55	-0	390	0	0	0	-1048	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
13	55	-0	447	0	0	0	-1039	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
14	55	-0	320	0	0	0	-1175	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
15	55	-0	509	0	0	0	-1147	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
16	55	-0	322	0	0	0	-1121	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
17	55	-0	511	0	0	0	-1093	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
18	55	-0	494	0	0	0	-2163	--	--	16.08	16.08	0.18	0.04	0.00	0.03	0.00	0.00	20.9
19	55	-0	711	0	0	0	-1581	--	--	16.08	16.08	0.18	0.03	0.01	0.04	0.00	0.00	20.9
20	55	-0	735	0	0	0	-1802	--	--	16.08	16.08	0.18	0.03	0.01	0.05	0.00	0.00	20.9
37	55	-0	407	0	0	0	-2219	--	--	16.08	16.08	0.18	0.04	0.00	0.03	0.00	0.00	20.9
38	55	-0	768	0	0	0	-1249	--	--	16.08	16.08	0.18	0.02	0.01	0.05	0.00	0.00	20.9
39	55	-0	807	0	0	0	-1617	--	--	16.08	16.08	0.18	0.03	0.01	0.05	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 157 NI 1797 NF 1796 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle V,Mx	cmq/m		cm
1	0	-0	-588	0	0	0	-1497	--	--	16.08	16.08	0.18	0.02	0.00 0.04	0.00	0.00	20.9
2	0	-0	-526	0	0	0	-1266	--	--	16.08	16.08	0.29	0.02	0.00 0.03	0.00	0.00	20.9
3	0	-0	-474	0	0	0	-1238	--	--	16.08	16.08	0.29	0.02	0.00 0.03	0.00	0.00	20.9
4	0	-0	-430	0	0	0	-1065	--	--	16.08	16.08	0.29	0.02	0.00 0.03	0.00	0.00	20.9
5	0	-0	-378	0	0	0	-1037	--	--	16.08	16.08	0.29	0.02	0.00 0.02	0.00	0.00	20.9
6	0	-0	-553	0	0	0	-1228	--	--	16.08	16.08	0.29	0.02	0.00 0.03	0.00	0.00	20.9
7	0	-0	-379	0	0	0	-1136	--	--	16.08	16.08	0.29	0.02	0.00 0.02	0.00	0.00	20.9
8	0	-0	-525	0	0	0	-1168	--	--	16.08	16.08	0.29	0.02	0.00 0.03	0.00	0.00	20.9
9	0	-0	-350	0	0	0	-1076	--	--	16.08	16.08	0.29	0.02	0.00 0.02	0.00	0.00	20.9
10	0	-0	-526	0	0	0	-1266	--	--	16.08	16.08	0.29	0.02	0.00 0.03	0.00	0.00	20.9
11	0	-0	-474	0	0	0	-1238	--	--	16.08	16.08	0.29	0.02	0.00 0.03	0.00	0.00	20.9
12	0	-0	-430	0	0	0	-1065	--	--	16.08	16.08	0.29	0.02	0.00 0.03	0.00	0.00	20.9
13	0	-0	-378	0	0	0	-1037	--	--	16.08	16.08	0.29	0.02	0.00 0.02	0.00	0.00	20.9
14	0	-0	-553	0	0	0	-1228	--	--	16.08	16.08	0.29	0.02	0.00 0.03	0.00	0.00	20.9
15	0	-0	-379	0	0	0	-1136	--	--	16.08	16.08	0.29	0.02	0.00 0.02	0.00	0.00	20.9
16	0	-0	-525	0	0	0	-1168	--	--	16.08	16.08	0.29	0.02	0.00 0.03	0.00	0.00	20.9
17	0	-0	-350	0	0	0	-1076	--	--	16.08	16.08	0.29	0.02	0.00 0.02	0.00	0.00	20.9
18	0	-0	-1229	0	0	0	-2322	--	--	16.08	16.08	0.18	0.04	0.01 0.08	0.00	0.00	20.9
19	0	-0	-772	0	0	0	-1612	--	--	16.08	16.08	0.18	0.03	0.01 0.05	0.00	0.00	20.9
20	0	-0	-808	0	0	0	-1838	--	--	16.08	16.08	0.18	0.03	0.01 0.05	0.00	0.00	20.9
37	0	-0	-1243	0	0	0	-2396	--	--	16.08	16.08	0.18	0.04	0.01 0.08	0.00	0.00	20.9
38	0	-0	-480	0	0	0	-1213	--	--	16.08	16.08	0.18	0.02	0.00 0.03	0.00	0.00	20.9
39	0	-0	-541	0	0	0	-1589	--	--	16.08	16.08	0.18	0.03	0.00 0.03	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-588	0	0	0	-1497	--	--	16.08	16.08	0.18	0.02	0.00 0.04	0.00	0.00	20.9
2	27	-0	-526	0	0	0	-1266	--	--	16.08	16.08	0.29	0.02	0.00 0.03	0.00	0.00	20.9
3	27	-0	-474	0	0	0	-1238	--	--	16.08	16.08	0.29	0.02	0.00 0.03	0.00	0.00	20.9
4	27	-0	-430	0	0	0	-1065	--	--	16.08	16.08	0.29	0.02	0.00 0.03	0.00	0.00	20.9
5	27	-0	-378	0	0	0	-1037	--	--	16.08	16.08	0.29	0.02	0.00 0.02	0.00	0.00	20.9
6	27	-0	-553	0	0	0	-1228	--	--	16.08	16.08	0.29	0.02	0.00 0.03	0.00	0.00	20.9
7	27	-0	-379	0	0	0	-1136	--	--	16.08	16.08	0.29	0.02	0.00 0.02	0.00	0.00	20.9
8	27	-0	-525	0	0	0	-1168	--	--	16.08	16.08	0.29	0.02	0.00 0.03	0.00	0.00	20.9
9	27	-0	-350	0	0	0	-1076	--	--	16.08	16.08	0.29	0.02	0.00 0.02	0.00	0.00	20.9
10	27	-0	-526	0	0	0	-1266	--	--	16.08	16.08	0.29	0.02	0.00 0.03	0.00	0.00	20.9
11	27	-0	-474	0	0	0	-1238	--	--	16.08	16.08	0.29	0.02	0.00 0.03	0.00	0.00	20.9
12	27	-0	-430	0	0	0	-1065	--	--	16.08	16.08	0.29	0.02	0.00 0.03	0.00	0.00	20.9
13	27	-0	-378	0	0	0	-1037	--	--	16.08	16.08	0.29	0.02	0.00 0.02	0.00	0.00	20.9
14	27	-0	-553	0	0	0	-1228	--	--	16.08	16.08	0.29	0.02	0.00 0.03	0.00	0.00	20.9
15	27	-0	-379	0	0	0	-1136	--	--	16.08	16.08	0.29	0.02	0.00 0.02	0.00	0.00	20.9
16	27	-0	-525	0	0	0	-1168	--	--	16.08	16.08	0.29	0.02	0.00 0.03	0.00	0.00	20.9
17	27	-0	-350	0	0	0	-1076	--	--	16.08	16.08	0.29	0.02	0.00 0.02	0.00	0.00	20.9
18	27	-0	-1229	0	0	0	-2322	--	--	16.08	16.08	0.18	0.04	0.01 0.08	0.00	0.00	20.9
19	27	-0	-772	0	0	0	-1612	--	--	16.08	16.08	0.18	0.03	0.01 0.05	0.00	0.00	20.9
20	27	-0	-808	0	0	0	-1838	--	--	16.08	16.08	0.18	0.03	0.01 0.05	0.00	0.00	20.9
37	27	-0	-1243	0	0	0	-2396	--	--	16.08	16.08	0.18	0.04	0.01 0.08	0.00	0.00	20.9
38	27	-0	-480	0	0	0	-1213	--	--	16.08	16.08	0.18	0.02	0.00 0.03	0.00	0.00	20.9
39	27	-0	-541	0	0	0	-1589	--	--	16.08	16.08	0.18	0.03	0.00 0.03	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	-588	0	0	0	-1497	--	--	16.08	16.08	0.18	0.02	0.00 0.04	0.00	0.00	20.9
2	55	-0	-526	0	0	0	-1266	--	--	16.08	16.08	0.29	0.02	0.00 0.03	0.00	0.00	20.9
3	55	-0	-474	0	0	0	-1238	--	--	16.08	16.08	0.29	0.02	0.00 0.03	0.00	0.00	20.9
4	55	-0	-430	0	0	0	-1065	--	--	16.08	16.08	0.29	0.02	0.00 0.03	0.00	0.00	20.9
5	55	-0	-378	0	0	0	-1037	--	--	16.08	16.08	0.29	0.02	0.00 0.02	0.00	0.00	20.9
6	55	-0	-553	0	0	0	-1228	--	--	16.08	16.08	0.29	0.02	0.00 0.03	0.00	0.00	20.9
7	55	-0	-379	0	0	0	-1136	--	--	16.08	16.08	0.29	0.02	0.00 0.02	0.00	0.00	20.9
8	55	-0	-525	0	0	0	-1168	--	--	16.08	16.08	0.29	0.02	0.00 0.03	0.00	0.00	20.9
9	55	-0	-350	0	0	0	-1076	--	--	16.08	16.08	0.29	0.02	0.00 0.02	0.00	0.00	20.9
10	55	-0	-526	0	0	0	-1266	--	--	16.08	16.08	0.29	0.02	0.00 0.03	0.00	0.00	20.9
11	55	-0	-474	0	0	0	-1238	--	--	16.08	16.08	0.29	0.02	0.00 0.03	0.00	0.00	20.9
12	55	-0	-430	0	0	0	-1065	--	--	16.08	16.08	0.29	0.02	0.00 0.03	0.00	0.00	20.9
13	55	-0	-378	0	0	0	-1037	--	--	16.08	16.08	0.29	0.02	0.00 0.02	0.00	0.00	20.9
14	55	-0	-553	0	0	0	-1228	--	--	16.08	16.08	0.29	0.02	0.00 0.03	0.00	0.00	20.9
15	55	-0	-379	0	0	0	-1136	--	--	16.08	16.08	0.29	0.02	0.00 0.02	0.00	0.00	20.9
16	55	-0	-525	0	0	0	-1168	--	--	16.08	16.08	0.29	0.02	0.00 0.03	0.00	0.00	20.9
17	55	-0	-350	0	0	0	-1076	--	--	16.08	16.08	0.29	0.02	0.00 0.02	0.00	0.00	20.9
18	55	-0	-1229	0	0	0	-2322	--	--	16.08	16.08	0.18	0.04	0.01 0.08	0.00	0.00	20.9
19	55	-0	-772	0	0	0	-1612	--	--	16.08	16.08	0.18	0.03	0.01 0.05	0.00	0.00	20.9
20	55	-0	-808	0	0	0	-1838	--	--	16.08	16.08	0.18	0.03	0.01 0.05	0.00	0.00	20.9
37	55	-0	-1243	0	0	0	-2396	--	--	16.08	16.08	0.18	0.04	0.01 0.08	0.00	0.00	20.9
38	55	-0	-480	0	0	0	-1213	--	--	16.08	16.08	0.18	0.02	0.00 0.03	0.00	0.00	20.9
39	55	-0	-541	0	0	0	-1589	--	--	16.08	16.08	0.18	0.03	0.00 0.03	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 158 NI 1782 NF 1797 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle V,Mx	cmq/m		cm
1	0	-0	-1744	0	0	0	-1577	--	--	16.08	16.08	0.18	0.03	0.01 0.11	0.00	0.00	20.9
2	0	-0	-1459	0	0	0	-1320	--	--	16.08	16.08	0.29	0.02	0.01 0.09	0.00	0.00	20.9
3	0	-0	-1410	0	0	0	-1303	--	--	16.08	16.08	0.29	0.02	0.01 0.09	0.00	0.00	20.9
4	0	-0	-1273	0	0	0	-1123	--	--	16.08	16.08	0.29	0.02	0.01 0.08	0.00	0.00	20.9
5	0	-0	-1224	0	0	0	-1106	--	--	16.08	16.08	0.29	0.02	0.01 0.08	0.00	0.00	20.9
6	0	-0	-1451	0	0	0	-1271	--	--	16.08	16.08	0.29	0.02	0.01 0.09	0.00	0.00	20.9
7	0	-0	-1287	0	0	0	-1214	--	--	16.08	16.08	0.29	0.02	0.01 0.08	0.00	0.00	20.9
8	0	-0	-1395	0	0	0	-1212	--	--	16.08	16.08	0.29	0.02	0.01 0.09	0.00	0.00	20.9
9	0	-0	-1232	0	0	0	-1155	--	--	16.08	16.08	0.29	0.02	0.01 0.08	0.00	0.00	20.9
10	0	-0	-1459	0	0	0	-1320	--	--	16.08	16.08	0.29	0.02	0.01 0.09	0.00	0.00	20.9
11	0	-0	-1410	0	0	0	-1303	--	--	16.08	16.08	0.29	0.02	0.01 0.09	0.00	0.00	20.9
12	0	-0	-1273	0	0	0	-1123	--	--	16.08	16.08	0.29	0.02	0.01 0.08	0.00	0.00	20.9
13	0	-0	-1224	0	0	0	-1106	--	--	16.08	16.08	0.29	0.02	0.01 0.08	0.00	0.00	20.9
14	0	-0	-1451	0	0	0	-1271	--	--	16.08	16.08	0.29	0.02	0.01 0.09	0.00	0.00	20.9
15	0	-0	-1287	0	0	0	-1214	--	--	16.08	16.08	0.29	0.02	0.01 0.08	0.00	0.00	20.9
16	0	-0	-1395	0	0	0	-1212	--	--	16.08	16.08	0.29	0.02	0.01 0.09	0.00	0.00	20.9

17	0	-0	-1232	0	0	0	-1155	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
18	0	-0	-3015	0	0	0	-2380	--	--	16.08	16.08	0.18	0.04	0.02	0.19	0.00	0.00	20.9
19	0	-0	-2308	0	0	0	-1720	--	--	16.08	16.08	0.18	0.03	0.02	0.14	0.00	0.00	20.9
20	0	-0	-2402	0	0	0	-1946	--	--	16.08	16.08	0.18	0.03	0.02	0.15	0.00	0.00	20.9
37	0	-0	-2948	0	0	0	-2438	--	--	16.08	16.08	0.18	0.04	0.02	0.18	0.00	0.00	20.9
38	0	-0	-1770	0	0	0	-1336	--	--	16.08	16.08	0.18	0.02	0.01	0.11	0.00	0.00	20.9
39	0	-0	-1926	0	0	0	-1714	--	--	16.08	16.08	0.18	0.03	0.02	0.12	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-1744	0	0	0	-1577	--	--	16.08	16.08	0.18	0.03	0.01	0.11	0.00	0.00	20.9
2	27	-0	-1459	0	0	0	-1320	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
3	27	-0	-1410	0	0	0	-1303	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
4	27	-0	-1273	0	0	0	-1123	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
5	27	-0	-1224	0	0	0	-1106	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
6	27	-0	-1451	0	0	0	-1271	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
7	27	-0	-1287	0	0	0	-1214	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
8	27	-0	-1395	0	0	0	-1212	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
9	27	-0	-1232	0	0	0	-1155	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
10	27	-0	-1459	0	0	0	-1320	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
11	27	-0	-1410	0	0	0	-1303	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
12	27	-0	-1273	0	0	0	-1123	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
13	27	-0	-1224	0	0	0	-1106	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
14	27	-0	-1451	0	0	0	-1271	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
15	27	-0	-1287	0	0	0	-1214	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
16	27	-0	-1395	0	0	0	-1212	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
17	27	-0	-1232	0	0	0	-1155	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
18	27	-0	-3015	0	0	0	-2380	--	--	16.08	16.08	0.18	0.04	0.02	0.19	0.00	0.00	20.9
19	27	-0	-2308	0	0	0	-1720	--	--	16.08	16.08	0.18	0.03	0.02	0.14	0.00	0.00	20.9
20	27	-0	-2402	0	0	0	-1946	--	--	16.08	16.08	0.18	0.03	0.02	0.15	0.00	0.00	20.9
37	27	-0	-2948	0	0	0	-2438	--	--	16.08	16.08	0.18	0.04	0.02	0.18	0.00	0.00	20.9
38	27	-0	-1770	0	0	0	-1336	--	--	16.08	16.08	0.18	0.02	0.01	0.11	0.00	0.00	20.9
39	27	-0	-1926	0	0	0	-1714	--	--	16.08	16.08	0.18	0.03	0.02	0.12	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	-1744	0	0	0	-1577	--	--	16.08	16.08	0.18	0.03	0.01	0.11	0.00	0.00	20.9
2	55	-0	-1459	0	0	0	-1320	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
3	55	-0	-1410	0	0	0	-1303	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
4	55	-0	-1273	0	0	0	-1123	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
5	55	-0	-1224	0	0	0	-1106	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
6	55	-0	-1451	0	0	0	-1271	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
7	55	-0	-1287	0	0	0	-1214	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
8	55	-0	-1395	0	0	0	-1212	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
9	55	-0	-1232	0	0	0	-1155	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
10	55	-0	-1459	0	0	0	-1320	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
11	55	-0	-1410	0	0	0	-1303	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
12	55	-0	-1273	0	0	0	-1123	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
13	55	-0	-1224	0	0	0	-1106	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
14	55	-0	-1451	0	0	0	-1271	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
15	55	-0	-1287	0	0	0	-1214	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
16	55	-0	-1395	0	0	0	-1212	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
17	55	-0	-1232	0	0	0	-1155	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
18	55	-0	-3015	0	0	0	-2380	--	--	16.08	16.08	0.18	0.04	0.02	0.19	0.00	0.00	20.9
19	55	-0	-2308	0	0	0	-1720	--	--	16.08	16.08	0.18	0.03	0.02	0.14	0.00	0.00	20.9
20	55	-0	-2402	0	0	0	-1946	--	--	16.08	16.08	0.18	0.03	0.02	0.15	0.00	0.00	20.9
37	55	-0	-2948	0	0	0	-2438	--	--	16.08	16.08	0.18	0.04	0.02	0.18	0.00	0.00	20.9
38	55	-0	-1770	0	0	0	-1336	--	--	16.08	16.08	0.18	0.02	0.01	0.11	0.00	0.00	20.9
39	55	-0	-1926	0	0	0	-1714	--	--	16.08	16.08	0.18	0.03	0.02	0.12	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 159 NI 1783 NF 1782 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-3044	0	0	0	251	--	--	16.08	16.08	0.00	0.00	0.03	0.19	0.00	0.00	20.9
2	0	-0	-2512	0	0	0	197	--	--	16.08	16.08	0.10	0.00	0.02	0.16	0.00	0.00	20.9
3	0	-0	-2466	0	0	0	179	--	--	16.08	16.08	0.10	0.00	0.02	0.15	0.00	0.00	20.9
4	0	-0	-2218	0	0	0	208	--	--	16.08	16.08	0.10	0.00	0.02	0.14	0.00	0.00	20.9
5	0	-0	-2172	0	0	0	190	--	--	16.08	16.08	0.10	0.00	0.02	0.14	0.00	0.00	20.9
6	0	-0	-2463	0	0	0	221	--	--	16.08	16.08	0.10	0.00	0.02	0.15	0.00	0.00	20.9
7	0	-0	-2309	0	0	0	163	--	--	16.08	16.08	0.10	0.00	0.02	0.14	0.00	0.00	20.9
8	0	-0	-2374	0	0	0	224	--	--	16.08	16.08	0.10	0.00	0.02	0.15	0.00	0.00	20.9
9	0	-0	-2221	0	0	0	166	--	--	16.08	16.08	0.10	0.00	0.02	0.14	0.00	0.00	20.9
10	0	-0	-2512	0	0	0	197	--	--	16.08	16.08	0.10	0.00	0.02	0.16	0.00	0.00	20.9
11	0	-0	-2466	0	0	0	179	--	--	16.08	16.08	0.10	0.00	0.02	0.15	0.00	0.00	20.9
12	0	-0	-2218	0	0	0	208	--	--	16.08	16.08	0.10	0.00	0.02	0.14	0.00	0.00	20.9
13	0	-0	-2172	0	0	0	190	--	--	16.08	16.08	0.10	0.00	0.02	0.14	0.00	0.00	20.9
14	0	-0	-2463	0	0	0	221	--	--	16.08	16.08	0.10	0.00	0.02	0.15	0.00	0.00	20.9
15	0	-0	-2309	0	0	0	163	--	--	16.08	16.08	0.10	0.00	0.02	0.14	0.00	0.00	20.9
16	0	-0	-2374	0	0	0	224	--	--	16.08	16.08	0.10	0.00	0.02	0.15	0.00	0.00	20.9
17	0	-0	-2221	0	0	0	166	--	--	16.08	16.08	0.10	0.00	0.02	0.14	0.00	0.00	20.9
18	0	-0	-5075	0	0	0	718	--	--	16.08	16.08	0.00	0.01	0.04	0.32	0.00	0.00	20.9
19	0	-0	-4052	0	0	0	710	--	--	16.08	16.08	0.00	0.01	0.03	0.25	0.00	0.00	20.9
20	0	-0	-4221	0	0	0	591	--	--	16.08	16.08	0.00	0.01	0.03	0.26	0.00	0.00	20.9
37	0	-0	-4918	0	0	0	576	--	--	16.08	16.08	0.00	0.01	0.04	0.31	0.00	0.00	20.9
38	0	-0	-3213	0	0	0	564	--	--	16.08	16.08	0.00	0.01	0.03	0.20	0.00	0.00	20.9
39	0	-0	-3495	0	0	0	366	--	--	16.08	16.08	0.00	0.01	0.03	0.22	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-3044	0	0	0	-1409	--	--	16.08	16.08	0.18	0.02	0.03	0.19	0.00	0.00	20.9
2	27	-0	-2512	0	0	0	-1173	--	--	16.08	16.08	0.29	0.02	0.02	0.16	0.00	0.00	20.9
3	27	-0	-2466	0	0	0	-1165	--	--	16.08	16.08	0.29	0.02	0.02	0.15	0.00	0.00	20.9
4	27	-0	-2218	0	0	0	-1002	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
5	27	-0	-2172	0	0	0	-994	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
6	27	-0	-2463	0	0	0	-1122	--	--	16.08	16.08	0.29	0.02	0.02	0.15	0.00	0.00	20.9
7	27	-0	-2309	0	0	0	-1096	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
8	27	-0	-2374	0	0	0	-1071	--	--	16.08	16.08	0.29	0.02	0.02	0.15	0.00	0.00	20.9
9	27	-0	-2221	0	0	0	-1045	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
10	27	-0	-2512	0	0	0	-1173	--	--	16.08	16.08	0.29	0.02	0.02	0.16	0.00	0.00	20.9
11	27	-0	-2466	0	0	0	-1165	--	--	16.08	16.08	0.29	0.02	0.02	0.15	0.00	0.00	20.9
12	27	-0	-2218	0	0	0	-1002	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9

13	27	-0	-2172	0	0	0	-994	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
14	27	-0	-2463	0	0	0	-1122	--	--	16.08	16.08	0.29	0.02	0.02	0.15	0.00	0.00	20.9
15	27	-0	-2309	0	0	0	-1096	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
16	27	-0	-2374	0	0	0	-1071	--	--	16.08	16.08	0.29	0.02	0.02	0.15	0.00	0.00	20.9
17	27	-0	-2221	0	0	0	-1045	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
18	27	-0	-5075	0	0	0	-2050	--	--	16.08	16.08	0.18	0.03	0.04	0.32	0.00	0.00	20.9
19	27	-0	-4052	0	0	0	-1500	--	--	16.08	16.08	0.18	0.02	0.03	0.25	0.00	0.00	20.9
20	27	-0	-4221	0	0	0	-1711	--	--	16.08	16.08	0.18	0.03	0.03	0.26	0.00	0.00	20.9
37	27	-0	-4918	0	0	0	-2106	--	--	16.08	16.08	0.18	0.03	0.04	0.31	0.00	0.00	20.9
38	27	-0	-3213	0	0	0	-1189	--	--	16.08	16.08	0.18	0.02	0.03	0.20	0.00	0.00	20.9
39	27	-0	-3495	0	0	0	-1541	--	--	16.08	16.08	0.18	0.03	0.03	0.22	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	-3044	0	0	0	-1409	--	--	16.08	16.08	0.18	0.02	0.03	0.19	0.00	0.00	20.9
2	55	-0	-2512	0	0	0	-1173	--	--	16.08	16.08	0.29	0.02	0.02	0.16	0.00	0.00	20.9
3	55	-0	-2466	0	0	0	-1165	--	--	16.08	16.08	0.29	0.02	0.02	0.15	0.00	0.00	20.9
4	55	-0	-2218	0	0	0	-1002	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
5	55	-0	-2172	0	0	0	-994	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
6	55	-0	-2463	0	0	0	-1122	--	--	16.08	16.08	0.29	0.02	0.02	0.15	0.00	0.00	20.9
7	55	-0	-2309	0	0	0	-1096	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
8	55	-0	-2374	0	0	0	-1071	--	--	16.08	16.08	0.29	0.02	0.02	0.15	0.00	0.00	20.9
9	55	-0	-2221	0	0	0	-1045	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
10	55	-0	-2512	0	0	0	-1173	--	--	16.08	16.08	0.29	0.02	0.02	0.16	0.00	0.00	20.9
11	55	-0	-2466	0	0	0	-1165	--	--	16.08	16.08	0.29	0.02	0.02	0.15	0.00	0.00	20.9
12	55	-0	-2218	0	0	0	-1002	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
13	55	-0	-2172	0	0	0	-994	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
14	55	-0	-2463	0	0	0	-1122	--	--	16.08	16.08	0.29	0.02	0.02	0.15	0.00	0.00	20.9
15	55	-0	-2309	0	0	0	-1096	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
16	55	-0	-2374	0	0	0	-1071	--	--	16.08	16.08	0.29	0.02	0.02	0.15	0.00	0.00	20.9
17	55	-0	-2221	0	0	0	-1045	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
18	55	-0	-5075	0	0	0	-2050	--	--	16.08	16.08	0.18	0.03	0.04	0.32	0.00	0.00	20.9
19	55	-0	-4052	0	0	0	-1500	--	--	16.08	16.08	0.18	0.02	0.03	0.25	0.00	0.00	20.9
20	55	-0	-4221	0	0	0	-1711	--	--	16.08	16.08	0.18	0.03	0.03	0.26	0.00	0.00	20.9
37	55	-0	-4918	0	0	0	-2106	--	--	16.08	16.08	0.18	0.03	0.04	0.31	0.00	0.00	20.9
38	55	-0	-3213	0	0	0	-1189	--	--	16.08	16.08	0.18	0.02	0.03	0.20	0.00	0.00	20.9
39	55	-0	-3495	0	0	0	-1541	--	--	16.08	16.08	0.18	0.03	0.03	0.22	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 160 NI 1784 NF 1783 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--	--	--	--	--	--	--	--	--	--	--		--	--	--	--	--	--
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-4622	0	0	0	1595	--	--	16.08	16.08	0.00	0.03	0.04	0.29	0.00	0.00	20.9
2	0	-0	-3795	0	0	0	1300	--	--	16.08	16.08	0.10	0.02	0.03	0.24	0.00	0.00	20.9
3	0	-0	-3760	0	0	0	1281	--	--	16.08	16.08	0.10	0.02	0.03	0.24	0.00	0.00	20.9
4	0	-0	-3351	0	0	0	1173	--	--	16.08	16.08	0.10	0.02	0.03	0.21	0.00	0.00	20.9
5	0	-0	-3315	0	0	0	1154	--	--	16.08	16.08	0.10	0.02	0.03	0.21	0.00	0.00	20.9
6	0	-0	-3681	0	0	0	1277	--	--	16.08	16.08	0.10	0.02	0.03	0.23	0.00	0.00	20.9
7	0	-0	-3562	0	0	0	1215	--	--	16.08	16.08	0.10	0.02	0.03	0.22	0.00	0.00	20.9
8	0	-0	-3548	0	0	0	1239	--	--	16.08	16.08	0.10	0.02	0.03	0.22	0.00	0.00	20.9
9	0	-0	-3429	0	0	0	1177	--	--	16.08	16.08	0.10	0.02	0.03	0.22	0.00	0.00	20.9
10	0	-0	-3795	0	0	0	1300	--	--	16.08	16.08	0.10	0.02	0.03	0.24	0.00	0.00	20.9
11	0	-0	-3760	0	0	0	1281	--	--	16.08	16.08	0.10	0.02	0.03	0.24	0.00	0.00	20.9
12	0	-0	-3351	0	0	0	1173	--	--	16.08	16.08	0.10	0.02	0.03	0.21	0.00	0.00	20.9
13	0	-0	-3315	0	0	0	1154	--	--	16.08	16.08	0.10	0.02	0.03	0.21	0.00	0.00	20.9
14	0	-0	-3681	0	0	0	1277	--	--	16.08	16.08	0.10	0.02	0.03	0.23	0.00	0.00	20.9
15	0	-0	-3562	0	0	0	1215	--	--	16.08	16.08	0.10	0.02	0.03	0.22	0.00	0.00	20.9
16	0	-0	-3548	0	0	0	1239	--	--	16.08	16.08	0.10	0.02	0.03	0.22	0.00	0.00	20.9
17	0	-0	-3429	0	0	0	1177	--	--	16.08	16.08	0.10	0.02	0.03	0.22	0.00	0.00	20.9
18	0	-0	-7661	0	0	0	2972	--	--	16.08	16.08	0.00	0.05	0.06	0.48	0.00	0.00	20.9
19	0	-0	-6178	0	0	0	2512	--	--	16.08	16.08	0.00	0.04	0.05	0.39	0.00	0.00	20.9
20	0	-0	-6489	0	0	0	2515	--	--	16.08	16.08	0.00	0.04	0.05	0.41	0.00	0.00	20.9
37	0	-0	-7406	0	0	0	2759	--	--	16.08	16.08	0.00	0.05	0.06	0.46	0.00	0.00	20.9
38	0	-0	-4934	0	0	0	1991	--	--	16.08	16.08	0.00	0.03	0.04	0.31	0.00	0.00	20.9
39	0	-0	-5452	0	0	0	1997	--	--	16.08	16.08	0.00	0.03	0.04	0.34	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-4622	0	0	0	1595	--	--	16.08	16.08	0.00	0.03	0.04	0.29	0.00	0.00	20.9
2	27	-0	-3795	0	0	0	1300	--	--	16.08	16.08	0.10	0.02	0.03	0.24	0.00	0.00	20.9
3	27	-0	-3760	0	0	0	1281	--	--	16.08	16.08	0.10	0.02	0.03	0.24	0.00	0.00	20.9
4	27	-0	-3351	0	0	0	1173	--	--	16.08	16.08	0.10	0.02	0.03	0.21	0.00	0.00	20.9
5	27	-0	-3315	0	0	0	1154	--	--	16.08	16.08	0.10	0.02	0.03	0.21	0.00	0.00	20.9
6	27	-0	-3681	0	0	0	1277	--	--	16.08	16.08	0.10	0.02	0.03	0.23	0.00	0.00	20.9
7	27	-0	-3562	0	0	0	1215	--	--	16.08	16.08	0.10	0.02	0.03	0.22	0.00	0.00	20.9
8	27	-0	-3548	0	0	0	1239	--	--	16.08	16.08	0.10	0.02	0.03	0.22	0.00	0.00	20.9
9	27	-0	-3429	0	0	0	1177	--	--	16.08	16.08	0.10	0.02	0.03	0.22	0.00	0.00	20.9
10	27	-0	-3795	0	0	0	1300	--	--	16.08	16.08	0.10	0.02	0.03	0.24	0.00	0.00	20.9
11	27	-0	-3760	0	0	0	1281	--	--	16.08	16.08	0.10	0.02	0.03	0.24	0.00	0.00	20.9
12	27	-0	-3351	0	0	0	1173	--	--	16.08	16.08	0.10	0.02	0.03	0.21	0.00	0.00	20.9
13	27	-0	-3315	0	0	0	1154	--	--	16.08	16.08	0.10	0.02	0.03	0.21	0.00	0.00	20.9
14	27	-0	-3681	0	0	0	1277	--	--	16.08	16.08	0.10	0.02	0.03	0.23	0.00	0.00	20.9
15	27	-0	-3562	0	0	0	1215	--	--	16.08	16.08	0.10	0.02	0.03	0.22	0.00	0.00	20.9
16	27	-0	-3548	0	0	0	1239	--	--	16.08	16.08	0.10	0.02	0.03	0.22	0.00	0.00	20.9
17	27	-0	-3429	0	0	0	1177	--	--	16.08	16.08	0.10	0.02	0.03	0.22	0.00	0.00	20.9
18	27	-0	-7661	0	0	0	2972	--	--	16.08	16.08	0.00	0.05	0.06	0.48	0.00	0.00	20.9
19	27	-0	-6178	0	0	0	2512	--	--	16.08	16.08	0.00	0.04	0.05	0.39	0.00	0.00	20.9
20	27	-0	-6489	0	0	0	2515	--	--	16.08	16.08	0.00	0.04	0.05	0.41	0.00	0.00	20.9
37	27	-0	-7406	0	0	0	2759	--	--	16.08	16.08	0.00	0.05	0.06	0.46	0.00	0.00	20.9
38	27	-0	-4934	0	0	0	1991	--	--	16.08	16.08	0.00	0.03	0.04	0.31	0.00	0.00	20.9
39	27	-0	-5452	0	0	0	1997	--	--	16.08	16.08	0.00	0.03	0.04	0.34	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	-4622	0	0	0	-926	--	--	16.08	16.08	0.18	0.02	0.04	0.29	0.00	0.00	20.9
2	55	-0	-3795	0	0	0	-771	--	--	16.08	16.08	0.29	0.01	0.03	0.24	0.00	0.00	20.9
3	55	-0	-3760	0	0	0	-770	--	--	16.08	16.08	0.29	0.01	0.03	0.24	0.00	0.00	20.9
4	55	-0	-3351	0	0	0	-655	--	--	16.08	16.08	0.29	0.01	0.03	0.21	0.00	0.00	20.9
5	55	-0	-3315	0	0	0	-654	--	--	16.08	16.08	0.29	0.01	0.03	0.21	0.00	0.00	20.9
6	55	-0	-3681	0	0	0	-731	--	--	16.08	16.08	0.29	0.01	0.03	0.23	0.00	0.00	20.9
7	55	-0	-3562	0	0	0	-729	--	--	16.08	16.08	0.29	0.01	0.03	0.22	0.00	0.00	20.9
8	55	-0	-3548	0	0	0	-697	--	--	16.08	16.08	0.29	0.01	0.03	0.22	0.00	0.00	20.9

9	55	-0	-3429	0	0	0	-694	--	--	16.08	16.08	0.29	0.01	0.03	0.22	0.00	0.00	20.9
10	55	-0	-3795	0	0	0	-771	--	--	16.08	16.08	0.29	0.01	0.03	0.24	0.00	0.00	20.9
11	55	-0	-3760	0	0	0	-770	--	--	16.08	16.08	0.29	0.01	0.03	0.24	0.00	0.00	20.9
12	55	-0	-3351	0	0	0	-655	--	--	16.08	16.08	0.29	0.01	0.03	0.21	0.00	0.00	20.9
13	55	-0	-3315	0	0	0	-654	--	--	16.08	16.08	0.29	0.01	0.03	0.21	0.00	0.00	20.9
14	55	-0	-3681	0	0	0	-731	--	--	16.08	16.08	0.29	0.01	0.03	0.23	0.00	0.00	20.9
15	55	-0	-3562	0	0	0	-729	--	--	16.08	16.08	0.29	0.01	0.03	0.22	0.00	0.00	20.9
16	55	-0	-3548	0	0	0	-697	--	--	16.08	16.08	0.29	0.01	0.03	0.22	0.00	0.00	20.9
17	55	-0	-3429	0	0	0	-694	--	--	16.08	16.08	0.29	0.01	0.03	0.22	0.00	0.00	20.9
18	55	-0	-7661	0	0	0	-1207	--	--	16.08	16.08	0.18	0.02	0.06	0.48	0.00	0.00	20.9
19	55	-0	-6178	0	0	0	-859	--	--	16.08	16.08	0.18	0.01	0.05	0.39	0.00	0.00	20.9
20	55	-0	-6489	0	0	0	-1024	--	--	16.08	16.08	0.18	0.02	0.05	0.41	0.00	0.00	20.9
37	55	-0	-7406	0	0	0	-1281	--	--	16.08	16.08	0.18	0.02	0.06	0.46	0.00	0.00	20.9
38	55	-0	-4934	0	0	0	-700	--	--	16.08	16.08	0.18	0.01	0.04	0.31	0.00	0.00	20.9
39	55	-0	-5452	0	0	0	-977	--	--	16.08	16.08	0.18	0.02	0.04	0.34	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 161 NI 1773 NF 1784 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-5059	0	0	0	2483	--	--	16.08	16.08	0.00	0.04	0.04	0.32	0.00	0.00	20.9
2	0	-0	-4101	0	0	0	1994	--	--	16.08	16.08	0.10	0.04	0.03	0.26	0.00	0.00	20.9
3	0	-0	-4103	0	0	0	1995	--	--	16.08	16.08	0.10	0.04	0.03	0.26	0.00	0.00	20.9
4	0	-0	-3680	0	0	0	1825	--	--	16.08	16.08	0.10	0.03	0.03	0.23	0.00	0.00	20.9
5	0	-0	-3681	0	0	0	1826	--	--	16.08	16.08	0.10	0.03	0.03	0.23	0.00	0.00	20.9
6	0	-0	-3953	0	0	0	1935	--	--	16.08	16.08	0.10	0.03	0.03	0.25	0.00	0.00	20.9
7	0	-0	-3956	0	0	0	1936	--	--	16.08	16.08	0.10	0.03	0.03	0.25	0.00	0.00	20.9
8	0	-0	-3826	0	0	0	1884	--	--	16.08	16.08	0.10	0.03	0.03	0.24	0.00	0.00	20.9
9	0	-0	-3830	0	0	0	1885	--	--	16.08	16.08	0.10	0.03	0.03	0.24	0.00	0.00	20.9
10	0	-0	-4101	0	0	0	1994	--	--	16.08	16.08	0.10	0.04	0.03	0.26	0.00	0.00	20.9
11	0	-0	-4103	0	0	0	1995	--	--	16.08	16.08	0.10	0.04	0.03	0.26	0.00	0.00	20.9
12	0	-0	-3680	0	0	0	1825	--	--	16.08	16.08	0.10	0.03	0.03	0.23	0.00	0.00	20.9
13	0	-0	-3681	0	0	0	1826	--	--	16.08	16.08	0.10	0.03	0.03	0.23	0.00	0.00	20.9
14	0	-0	-3953	0	0	0	1935	--	--	16.08	16.08	0.10	0.03	0.03	0.25	0.00	0.00	20.9
15	0	-0	-3956	0	0	0	1936	--	--	16.08	16.08	0.10	0.03	0.03	0.25	0.00	0.00	20.9
16	0	-0	-3826	0	0	0	1884	--	--	16.08	16.08	0.10	0.03	0.03	0.24	0.00	0.00	20.9
17	0	-0	-3830	0	0	0	1885	--	--	16.08	16.08	0.10	0.03	0.03	0.24	0.00	0.00	20.9
18	0	-0	-7998	0	0	0	4179	--	--	16.08	16.08	0.00	0.07	0.07	0.50	0.00	0.00	20.9
19	0	-0	-6698	0	0	0	3646	--	--	16.08	16.08	0.00	0.06	0.06	0.42	0.00	0.00	20.9
20	0	-0	-7019	0	0	0	3697	--	--	16.08	16.08	0.00	0.06	0.06	0.44	0.00	0.00	20.9
37	0	-0	-7685	0	0	0	3899	--	--	16.08	16.08	0.00	0.07	0.06	0.48	0.00	0.00	20.9
38	0	-0	-5519	0	0	0	3009	--	--	16.08	16.08	0.00	0.05	0.05	0.35	0.00	0.00	20.9
39	0	-0	-6053	0	0	0	3095	--	--	16.08	16.08	0.00	0.05	0.05	0.38	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-5059	0	0	0	2483	--	--	16.08	16.08	0.00	0.04	0.04	0.32	0.00	0.00	20.9
2	27	-0	-4101	0	0	0	1994	--	--	16.08	16.08	0.10	0.04	0.03	0.26	0.00	0.00	20.9
3	27	-0	-4103	0	0	0	1995	--	--	16.08	16.08	0.10	0.04	0.03	0.26	0.00	0.00	20.9
4	27	-0	-3680	0	0	0	1825	--	--	16.08	16.08	0.10	0.03	0.03	0.23	0.00	0.00	20.9
5	27	-0	-3681	0	0	0	1826	--	--	16.08	16.08	0.10	0.03	0.03	0.23	0.00	0.00	20.9
6	27	-0	-3953	0	0	0	1935	--	--	16.08	16.08	0.10	0.03	0.03	0.25	0.00	0.00	20.9
7	27	-0	-3956	0	0	0	1936	--	--	16.08	16.08	0.10	0.03	0.03	0.25	0.00	0.00	20.9
8	27	-0	-3826	0	0	0	1884	--	--	16.08	16.08	0.10	0.03	0.03	0.24	0.00	0.00	20.9
9	27	-0	-3830	0	0	0	1885	--	--	16.08	16.08	0.10	0.03	0.03	0.24	0.00	0.00	20.9
10	27	-0	-4101	0	0	0	1994	--	--	16.08	16.08	0.10	0.04	0.03	0.26	0.00	0.00	20.9
11	27	-0	-4103	0	0	0	1995	--	--	16.08	16.08	0.10	0.04	0.03	0.26	0.00	0.00	20.9
12	27	-0	-3680	0	0	0	1825	--	--	16.08	16.08	0.10	0.03	0.03	0.23	0.00	0.00	20.9
13	27	-0	-3681	0	0	0	1826	--	--	16.08	16.08	0.10	0.03	0.03	0.23	0.00	0.00	20.9
14	27	-0	-3953	0	0	0	1935	--	--	16.08	16.08	0.10	0.03	0.03	0.25	0.00	0.00	20.9
15	27	-0	-3956	0	0	0	1936	--	--	16.08	16.08	0.10	0.03	0.03	0.25	0.00	0.00	20.9
16	27	-0	-3826	0	0	0	1884	--	--	16.08	16.08	0.10	0.03	0.03	0.24	0.00	0.00	20.9
17	27	-0	-3830	0	0	0	1885	--	--	16.08	16.08	0.10	0.03	0.03	0.24	0.00	0.00	20.9
18	27	-0	-7998	0	0	0	4179	--	--	16.08	16.08	0.00	0.07	0.07	0.50	0.00	0.00	20.9
19	27	-0	-6698	0	0	0	3646	--	--	16.08	16.08	0.00	0.06	0.06	0.42	0.00	0.00	20.9
20	27	-0	-7019	0	0	0	3697	--	--	16.08	16.08	0.00	0.06	0.06	0.44	0.00	0.00	20.9
37	27	-0	-7685	0	0	0	3899	--	--	16.08	16.08	0.00	0.07	0.06	0.48	0.00	0.00	20.9
38	27	-0	-5519	0	0	0	3009	--	--	16.08	16.08	0.00	0.05	0.05	0.35	0.00	0.00	20.9
39	27	-0	-6053	0	0	0	3095	--	--	16.08	16.08	0.00	0.05	0.05	0.38	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	-5059	0	0	0	-276	--	--	16.08	16.08	0.18	0.00	0.04	0.32	0.00	0.00	20.9
2	55	-0	-4101	0	0	0	-243	--	--	16.08	16.08	0.29	0.00	0.03	0.26	0.00	0.00	20.9
3	55	-0	-4103	0	0	0	-243	--	--	16.08	16.08	0.29	0.00	0.03	0.26	0.00	0.00	20.9
4	55	-0	-3680	0	0	0	-182	--	--	16.08	16.08	0.29	0.00	0.03	0.23	0.00	0.00	20.9
5	55	-0	-3681	0	0	0	-182	--	--	16.08	16.08	0.29	0.00	0.03	0.23	0.00	0.00	20.9
6	55	-0	-3953	0	0	0	-221	--	--	16.08	16.08	0.29	0.00	0.03	0.25	0.00	0.00	20.9
7	55	-0	-3956	0	0	0	-222	--	--	16.08	16.08	0.29	0.00	0.03	0.25	0.00	0.00	20.9
8	55	-0	-3826	0	0	0	-203	--	--	16.08	16.08	0.29	0.00	0.03	0.24	0.00	0.00	20.9
9	55	-0	-3830	0	0	0	-204	--	--	16.08	16.08	0.29	0.00	0.03	0.24	0.00	0.00	20.9
10	55	-0	-4101	0	0	0	-243	--	--	16.08	16.08	0.29	0.00	0.03	0.26	0.00	0.00	20.9
11	55	-0	-4103	0	0	0	-243	--	--	16.08	16.08	0.29	0.00	0.03	0.26	0.00	0.00	20.9
12	55	-0	-3680	0	0	0	-182	--	--	16.08	16.08	0.29	0.00	0.03	0.23	0.00	0.00	20.9
13	55	-0	-3681	0	0	0	-182	--	--	16.08	16.08	0.29	0.00	0.03	0.23	0.00	0.00	20.9
14	55	-0	-3953	0	0	0	-221	--	--	16.08	16.08	0.29	0.00	0.03	0.25	0.00	0.00	20.9
15	55	-0	-3956	0	0	0	-222	--	--	16.08	16.08	0.29	0.00	0.03	0.25	0.00	0.00	20.9
16	55	-0	-3826	0	0	0	-203	--	--	16.08	16.08	0.29	0.00	0.03	0.24	0.00	0.00	20.9
17	55	-0	-3830	0	0	0	-204	--	--	16.08	16.08	0.29	0.00	0.03	0.24	0.00	0.00	20.9
18	55	-0	-7998	0	0	0	-183	--	--	16.08	16.08	0.18	0.00	0.07	0.50	0.00	0.00	20.9
19	55	-0	-6698	0	0	0	-8	--	--	16.08	16.08	0.18	0.00	0.06	0.42	0.00	0.00	20.9
20	55	-0	-7019	0	0	0	-130	--	--	16.08	16.08	0.18	0.00	0.06	0.44	0.00	0.00	20.9
37	55	-0	-7685	0	0	0	-293	--	--	16.08	16.08	0.18	0.00	0.06	0.48	0.00	0.00	20.9
38	55	-0	-5519	0	0	0	-1	--	--	16.08	16.08	0.18	0.00	0.05	0.35	0.00	0.00	20.9
39	55	-0	-6053	0	0	0	-206	--	--	16.08	16.08	0.18	0.00	0.05	0.38	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 162 NI 1685 NF 1773 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-1702	0	0	0	1694	--	--	16.08	16.08	0.00	0.03	0.01	0.11	0.00	0.00	20.9
2	0	-0	-1171	0	0	0	1245	--	--	16.08	16.08	0.10	0.02	0.01	0.07	0.00	0.00	20.9
3	0	-0	-1202	0	0	0	1252	--	--	16.08	16.08	0.10	0.02	0.01	0.08	0.00	0.00	20.9
4	0	-0	-1417	0	0	0	1354	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
5	0	-0	-1448	0	0	0	1362	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
6	0	-0	-1221	0	0	0	1275	--	--	16.08	16.08	0.10	0.02	0.01	0.08	0.00	0.00	20.9
7	0	-0	-1324	0	0	0	1299	--	--	16.08	16.08	0.10	0.02	0.01	0.08	0.00	0.00	20.9
8	0	-0	-1295	0	0	0	1308	--	--	16.08	16.08	0.10	0.02	0.01	0.08	0.00	0.00	20.9
9	0	-0	-1398	0	0	0	1332	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
10	0	-0	-1171	0	0	0	1245	--	--	16.08	16.08	0.10	0.02	0.01	0.07	0.00	0.00	20.9
11	0	-0	-1202	0	0	0	1252	--	--	16.08	16.08	0.10	0.02	0.01	0.08	0.00	0.00	20.9
12	0	-0	-1417	0	0	0	1354	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
13	0	-0	-1448	0	0	0	1362	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
14	0	-0	-1221	0	0	0	1275	--	--	16.08	16.08	0.10	0.02	0.01	0.08	0.00	0.00	20.9
15	0	-0	-1324	0	0	0	1299	--	--	16.08	16.08	0.10	0.02	0.01	0.08	0.00	0.00	20.9
16	0	-0	-1295	0	0	0	1308	--	--	16.08	16.08	0.10	0.02	0.01	0.08	0.00	0.00	20.9
17	0	-0	-1398	0	0	0	1332	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
18	0	-0	-641	0	0	0	1825	--	--	16.08	16.08	0.00	0.03	0.01	0.04	0.00	0.00	20.9
19	0	-0	-1981	0	0	0	2476	--	--	16.08	16.08	0.00	0.04	0.02	0.12	0.00	0.00	20.9
20	0	-0	-1462	0	0	0	2100	--	--	16.08	16.08	0.00	0.04	0.01	0.09	0.00	0.00	20.9
37	0	-0	-322	0	0	0	1467	--	--	16.08	16.08	0.00	0.03	0.00	0.02	0.00	0.00	20.9
38	0	-0	-2556	0	0	0	2552	--	--	16.08	16.08	0.00	0.04	0.02	0.16	0.00	0.00	20.9
39	0	-0	-1690	0	0	0	1925	--	--	16.08	16.08	0.00	0.03	0.01	0.11	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	27	-0	-1702	0	0	0	1694	--	--	16.08	16.08	0.00	0.03	0.01	0.11	0.00	0.00	20.9
2	27	-0	-1171	0	0	0	1245	--	--	16.08	16.08	0.10	0.02	0.01	0.07	0.00	0.00	20.9
3	27	-0	-1202	0	0	0	1252	--	--	16.08	16.08	0.10	0.02	0.01	0.08	0.00	0.00	20.9
4	27	-0	-1417	0	0	0	1354	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
5	27	-0	-1448	0	0	0	1362	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
6	27	-0	-1221	0	0	0	1275	--	--	16.08	16.08	0.10	0.02	0.01	0.08	0.00	0.00	20.9
7	27	-0	-1324	0	0	0	1299	--	--	16.08	16.08	0.10	0.02	0.01	0.08	0.00	0.00	20.9
8	27	-0	-1295	0	0	0	1308	--	--	16.08	16.08	0.10	0.02	0.01	0.08	0.00	0.00	20.9
9	27	-0	-1398	0	0	0	1332	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
10	27	-0	-1171	0	0	0	1245	--	--	16.08	16.08	0.10	0.02	0.01	0.07	0.00	0.00	20.9
11	27	-0	-1202	0	0	0	1252	--	--	16.08	16.08	0.10	0.02	0.01	0.08	0.00	0.00	20.9
12	27	-0	-1417	0	0	0	1354	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
13	27	-0	-1448	0	0	0	1362	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
14	27	-0	-1221	0	0	0	1275	--	--	16.08	16.08	0.10	0.02	0.01	0.08	0.00	0.00	20.9
15	27	-0	-1324	0	0	0	1299	--	--	16.08	16.08	0.10	0.02	0.01	0.08	0.00	0.00	20.9
16	27	-0	-1295	0	0	0	1308	--	--	16.08	16.08	0.10	0.02	0.01	0.08	0.00	0.00	20.9
17	27	-0	-1398	0	0	0	1332	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
18	27	-0	-641	0	0	0	1825	--	--	16.08	16.08	0.00	0.03	0.01	0.04	0.00	0.00	20.9
19	27	-0	-1981	0	0	0	2476	--	--	16.08	16.08	0.00	0.04	0.02	0.12	0.00	0.00	20.9
20	27	-0	-1462	0	0	0	2100	--	--	16.08	16.08	0.00	0.04	0.01	0.09	0.00	0.00	20.9
37	27	-0	-322	0	0	0	1467	--	--	16.08	16.08	0.00	0.03	0.00	0.02	0.00	0.00	20.9
38	27	-0	-2556	0	0	0	2552	--	--	16.08	16.08	0.00	0.04	0.02	0.16	0.00	0.00	20.9
39	27	-0	-1690	0	0	0	1925	--	--	16.08	16.08	0.00	0.03	0.01	0.11	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	55	-0	-1702	0	0	0	766	--	--	16.08	16.08	0.00	0.01	0.01	0.11	0.00	0.00	20.9
2	55	-0	-1171	0	0	0	606	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
3	55	-0	-1202	0	0	0	597	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
4	55	-0	-1417	0	0	0	581	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
5	55	-0	-1448	0	0	0	572	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
6	55	-0	-1221	0	0	0	609	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
7	55	-0	-1324	0	0	0	577	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
8	55	-0	-1295	0	0	0	601	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
9	55	-0	-1398	0	0	0	569	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
10	55	-0	-1171	0	0	0	606	--	--	16.08	16.08	0.10	0.01	0.01	0.07	0.00	0.00	20.9
11	55	-0	-1202	0	0	0	597	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
12	55	-0	-1417	0	0	0	581	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
13	55	-0	-1448	0	0	0	572	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
14	55	-0	-1221	0	0	0	609	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
15	55	-0	-1324	0	0	0	577	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
16	55	-0	-1295	0	0	0	601	--	--	16.08	16.08	0.10	0.01	0.01	0.08	0.00	0.00	20.9
17	55	-0	-1398	0	0	0	569	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
18	55	-0	-641	0	0	0	1475	--	--	16.08	16.08	0.00	0.03	0.01	0.04	0.00	0.00	20.9
19	55	-0	-1981	0	0	0	1395	--	--	16.08	16.08	0.00	0.02	0.02	0.12	0.00	0.00	20.9
20	55	-0	-1462	0	0	0	1303	--	--	16.08	16.08	0.00	0.02	0.01	0.09	0.00	0.00	20.9
37	55	-0	-322	0	0	0	1291	--	--	16.08	16.08	0.00	0.02	0.00	0.02	0.00	0.00	20.9
38	55	-0	-2556	0	0	0	1157	--	--	16.08	16.08	0.00	0.02	0.02	0.16	0.00	0.00	20.9
39	55	-0	-1690	0	0	0	1003	--	--	16.08	16.08	0.00	0.02	0.01	0.11	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 163 NI 1772 NF 1685 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	2393	0	0	0	1074	--	--	16.08	16.08	0.00	0.02	0.02	0.15	0.00	0.00	20.9
2	0	-0	1761	0	0	0	884	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
3	0	-0	1720	0	0	0	887	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
4	0	-0	1961	0	0	0	765	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
5	0	-0	1921	0	0	0	768	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
6	0	-0	1878	0	0	0	839	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
7	0	-0	1744	0	0	0	848	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
8	0	-0	1938	0	0	0	804	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
9	0	-0	1804	0	0	0	813	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
10	0	-0	1761	0	0	0	884	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
11	0	-0	1720	0	0	0	887	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
12	0	-0	1961	0	0	0	765	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
13	0	-0	1921	0	0	0	768	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
14	0	-0	1878	0	0	0	839	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
15	0	-0	1744	0	0	0	848	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
16	0	-0	1938	0	0	0	804	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9

17	0	-0	1804	0	0	0	813	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
18	0	-0	2440	0	0	0	2166	--	--	16.08	16.08	0.00	0.04	0.02	0.15	0.00	0.00	20.9
19	0	-0	3427	0	0	0	1683	--	--	16.08	16.08	0.00	0.03	0.03	0.21	0.00	0.00	20.9
20	0	-0	2726	0	0	0	1810	--	--	16.08	16.08	0.00	0.03	0.02	0.17	0.00	0.00	20.9
37	0	-0	1942	0	0	0	2053	--	--	16.08	16.08	0.00	0.04	0.02	0.12	0.00	0.00	20.9
38	0	-0	3588	0	0	0	1249	--	--	16.08	16.08	0.00	0.02	0.03	0.23	0.00	0.00	20.9
39	0	-0	2420	0	0	0	1461	--	--	16.08	16.08	0.00	0.02	0.02	0.15	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	2393	0	0	0	4284	--	--	16.08	16.08	0.00	0.07	0.02	0.15	0.00	0.00	20.9
2	27	-0	1761	0	0	0	3247	--	--	16.08	16.08	0.10	0.06	0.01	0.11	0.00	0.00	20.9
3	27	-0	1720	0	0	0	3194	--	--	16.08	16.08	0.10	0.06	0.01	0.11	0.00	0.00	20.9
4	27	-0	1961	0	0	0	3396	--	--	16.08	16.08	0.10	0.06	0.02	0.12	0.00	0.00	20.9
5	27	-0	1921	0	0	0	3345	--	--	16.08	16.08	0.10	0.06	0.02	0.12	0.00	0.00	20.9
6	27	-0	1878	0	0	0	3359	--	--	16.08	16.08	0.10	0.06	0.02	0.12	0.00	0.00	20.9
7	27	-0	1744	0	0	0	3188	--	--	16.08	16.08	0.10	0.06	0.01	0.11	0.00	0.00	20.9
8	27	-0	1938	0	0	0	3404	--	--	16.08	16.08	0.10	0.06	0.02	0.12	0.00	0.00	20.9
9	27	-0	1804	0	0	0	3233	--	--	16.08	16.08	0.10	0.06	0.01	0.11	0.00	0.00	20.9
10	27	-0	1761	0	0	0	3247	--	--	16.08	16.08	0.10	0.06	0.01	0.11	0.00	0.00	20.9
11	27	-0	1720	0	0	0	3194	--	--	16.08	16.08	0.10	0.06	0.01	0.11	0.00	0.00	20.9
12	27	-0	1961	0	0	0	3396	--	--	16.08	16.08	0.10	0.06	0.02	0.12	0.00	0.00	20.9
13	27	-0	1921	0	0	0	3345	--	--	16.08	16.08	0.10	0.06	0.02	0.12	0.00	0.00	20.9
14	27	-0	1878	0	0	0	3359	--	--	16.08	16.08	0.10	0.06	0.02	0.12	0.00	0.00	20.9
15	27	-0	1744	0	0	0	3188	--	--	16.08	16.08	0.10	0.06	0.01	0.11	0.00	0.00	20.9
16	27	-0	1938	0	0	0	3404	--	--	16.08	16.08	0.10	0.06	0.02	0.12	0.00	0.00	20.9
17	27	-0	1804	0	0	0	3233	--	--	16.08	16.08	0.10	0.06	0.01	0.11	0.00	0.00	20.9
18	27	-0	2440	0	0	0	5439	--	--	16.08	16.08	0.00	0.09	0.02	0.15	0.00	0.00	20.9
19	27	-0	3427	0	0	0	6281	--	--	16.08	16.08	0.00	0.11	0.03	0.21	0.00	0.00	20.9
20	27	-0	2726	0	0	0	5467	--	--	16.08	16.08	0.00	0.09	0.02	0.17	0.00	0.00	20.9
37	27	-0	1942	0	0	0	4658	--	--	16.08	16.08	0.00	0.08	0.02	0.12	0.00	0.00	20.9
38	27	-0	3588	0	0	0	6062	--	--	16.08	16.08	0.00	0.10	0.03	0.23	0.00	0.00	20.9
39	27	-0	2420	0	0	0	4707	--	--	16.08	16.08	0.00	0.08	0.02	0.15	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	2393	0	0	0	2379	--	--	16.08	16.08	0.00	0.04	0.02	0.15	0.00	0.00	20.9
2	55	-0	1761	0	0	0	1845	--	--	16.08	16.08	0.10	0.03	0.01	0.11	0.00	0.00	20.9
3	55	-0	1720	0	0	0	1825	--	--	16.08	16.08	0.10	0.03	0.01	0.11	0.00	0.00	20.9
4	55	-0	1961	0	0	0	1835	--	--	16.08	16.08	0.10	0.03	0.02	0.12	0.00	0.00	20.9
5	55	-0	1921	0	0	0	1816	--	--	16.08	16.08	0.10	0.03	0.02	0.12	0.00	0.00	20.9
6	55	-0	1878	0	0	0	1864	--	--	16.08	16.08	0.10	0.03	0.02	0.12	0.00	0.00	20.9
7	55	-0	1744	0	0	0	1799	--	--	16.08	16.08	0.10	0.03	0.01	0.11	0.00	0.00	20.9
8	55	-0	1938	0	0	0	1861	--	--	16.08	16.08	0.10	0.03	0.02	0.12	0.00	0.00	20.9
9	55	-0	1804	0	0	0	1797	--	--	16.08	16.08	0.10	0.03	0.01	0.11	0.00	0.00	20.9
10	55	-0	1761	0	0	0	1845	--	--	16.08	16.08	0.10	0.03	0.01	0.11	0.00	0.00	20.9
11	55	-0	1720	0	0	0	1825	--	--	16.08	16.08	0.10	0.03	0.01	0.11	0.00	0.00	20.9
12	55	-0	1961	0	0	0	1835	--	--	16.08	16.08	0.10	0.03	0.02	0.12	0.00	0.00	20.9
13	55	-0	1921	0	0	0	1816	--	--	16.08	16.08	0.10	0.03	0.02	0.12	0.00	0.00	20.9
14	55	-0	1878	0	0	0	1864	--	--	16.08	16.08	0.10	0.03	0.02	0.12	0.00	0.00	20.9
15	55	-0	1744	0	0	0	1799	--	--	16.08	16.08	0.10	0.03	0.01	0.11	0.00	0.00	20.9
16	55	-0	1938	0	0	0	1861	--	--	16.08	16.08	0.10	0.03	0.02	0.12	0.00	0.00	20.9
17	55	-0	1804	0	0	0	1797	--	--	16.08	16.08	0.10	0.03	0.01	0.11	0.00	0.00	20.9
18	55	-0	2440	0	0	0	3496	--	--	16.08	16.08	0.00	0.06	0.02	0.15	0.00	0.00	20.9
19	55	-0	3427	0	0	0	3553	--	--	16.08	16.08	0.00	0.06	0.03	0.21	0.00	0.00	20.9
20	55	-0	2726	0	0	0	3298	--	--	16.08	16.08	0.00	0.06	0.02	0.17	0.00	0.00	20.9
37	55	-0	1942	0	0	0	3112	--	--	16.08	16.08	0.00	0.05	0.02	0.12	0.00	0.00	20.9
38	55	-0	3588	0	0	0	3206	--	--	16.08	16.08	0.00	0.05	0.03	0.23	0.00	0.00	20.9
39	55	-0	2420	0	0	0	2781	--	--	16.08	16.08	0.00	0.05	0.02	0.15	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 164 NI 1768 NF 1772 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	5071	0	0	0	-59	--	--	16.08	16.08	0.18	0.00	0.04	0.32	0.00	0.00	20.9
2	0	-0	4086	0	0	0	-36	--	--	16.08	16.08	0.29	0.00	0.03	0.26	0.00	0.00	20.9
3	0	-0	4074	0	0	0	-40	--	--	16.08	16.08	0.29	0.00	0.03	0.26	0.00	0.00	20.9
4	0	-0	3728	0	0	0	-51	--	--	16.08	16.08	0.29	0.00	0.03	0.23	0.00	0.00	20.9
5	0	-0	3715	0	0	0	-55	--	--	16.08	16.08	0.29	0.00	0.03	0.23	0.00	0.00	20.9
6	0	-0	3976	0	0	0	-37	--	--	16.08	16.08	0.29	0.00	0.03	0.25	0.00	0.00	20.9
7	0	-0	3933	0	0	0	-50	--	--	16.08	16.08	0.29	0.00	0.03	0.25	0.00	0.00	20.9
8	0	-0	3868	0	0	0	-41	--	--	16.08	16.08	0.29	0.00	0.03	0.24	0.00	0.00	20.9
9	0	-0	3826	0	0	0	-54	--	--	16.08	16.08	0.29	0.00	0.03	0.24	0.00	0.00	20.9
10	0	-0	4086	0	0	0	-36	--	--	16.08	16.08	0.29	0.00	0.03	0.26	0.00	0.00	20.9
11	0	-0	4074	0	0	0	-40	--	--	16.08	16.08	0.29	0.00	0.03	0.26	0.00	0.00	20.9
12	0	-0	3728	0	0	0	-51	--	--	16.08	16.08	0.29	0.00	0.03	0.23	0.00	0.00	20.9
13	0	-0	3715	0	0	0	-55	--	--	16.08	16.08	0.29	0.00	0.03	0.23	0.00	0.00	20.9
14	0	-0	3976	0	0	0	-37	--	--	16.08	16.08	0.29	0.00	0.03	0.25	0.00	0.00	20.9
15	0	-0	3933	0	0	0	-50	--	--	16.08	16.08	0.29	0.00	0.03	0.25	0.00	0.00	20.9
16	0	-0	3868	0	0	0	-41	--	--	16.08	16.08	0.29	0.00	0.03	0.24	0.00	0.00	20.9
17	0	-0	3826	0	0	0	-54	--	--	16.08	16.08	0.29	0.00	0.03	0.24	0.00	0.00	20.9
18	0	-0	8176	0	0	0	250	--	--	16.08	16.08	0.00	0.00	0.07	0.51	0.00	0.00	20.9
19	0	-0	7084	0	0	0	110	--	--	16.08	16.08	0.00	0.00	0.06	0.44	0.00	0.00	20.9
20	0	-0	7199	0	0	0	142	--	--	16.08	16.08	0.00	0.00	0.06	0.45	0.00	0.00	20.9
37	0	-0	7714	0	0	0	222	--	--	16.08	16.08	0.00	0.00	0.06	0.48	0.00	0.00	20.9
38	0	-0	5894	0	0	0	-12	--	--	16.08	16.08	0.18	0.00	0.05	0.37	0.00	0.00	20.9
39	0	-0	6085	0	0	0	41	--	--	16.08	16.08	0.00	0.00	0.05	0.38	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	5071	0	0	0	6744	--	--	16.08	16.08	0.00	0.11	0.04	0.32	0.00	0.00	20.9
2	27	-0	4086	0	0	0	5446	--	--	16.08	16.08	0.10	0.10	0.03	0.26	0.00	0.00	20.9
3	27	-0	4074	0	0	0	5425	--	--	16.08	16.08	0.10	0.10	0.03	0.26	0.00	0.00	20.9
4	27	-0	3728	0	0	0	4950	--	--	16.08	16.08	0.10	0.09	0.03	0.23	0.00	0.00	20.9
5	27	-0	3715	0	0	0	4928	--	--	16.08	16.08	0.10	0.09	0.03	0.23	0.00	0.00	20.9
6	27	-0	3976	0	0	0	5297	--	--	16.08	16.08	0.10	0.09	0.03	0.25	0.00	0.00	20.9
7	27	-0	3933	0	0	0	5227	--	--	16.08	16.08	0.10	0.09	0.03	0.25	0.00	0.00	20.9
8	27	-0	3868	0	0	0	5148	--	--	16.08	16.08	0.10	0.09	0.03	0.24	0.00	0.00	20.9
9	27	-0	3826	0	0	0	5078	--	--	16.08	16.08	0.10	0.09	0.03	0.24	0.00	0.00	20.9
10	27	-0	4086	0	0	0	5446	--	--	16.08	16.08	0.10	0.10	0.03	0.26	0.00	0.00	20.9
11	27	-0	4074	0	0	0	5425	--	--	16.08	16.08	0.10	0.10	0.03	0.26	0.00	0.00	20.9
12	27	-0	3728	0	0	0	4950	--	--	16.08	16.08	0.10	0.09	0.03	0.23	0.00	0.00	20.9

13	27	-0	3715	0	0	0	4928	--	--	16.08	16.08	0.10	0.09	0.03	0.23	0.00	0.00	20.9
14	27	-0	3976	0	0	0	5297	--	--	16.08	16.08	0.10	0.09	0.03	0.25	0.00	0.00	20.9
15	27	-0	3933	0	0	0	5227	--	--	16.08	16.08	0.10	0.09	0.03	0.25	0.00	0.00	20.9
16	27	-0	3868	0	0	0	5148	--	--	16.08	16.08	0.10	0.09	0.03	0.24	0.00	0.00	20.9
17	27	-0	3826	0	0	0	5078	--	--	16.08	16.08	0.10	0.09	0.03	0.24	0.00	0.00	20.9
18	27	-0	8176	0	0	0	11218	--	--	16.08	16.08	0.00	0.19	0.07	0.51	0.00	0.00	20.9
19	27	-0	7084	0	0	0	9613	--	--	16.08	16.08	0.00	0.16	0.06	0.44	0.00	0.00	20.9
20	27	-0	7199	0	0	0	9799	--	--	16.08	16.08	0.00	0.17	0.06	0.45	0.00	0.00	20.9
37	27	-0	7714	0	0	0	10570	--	--	16.08	16.08	0.00	0.18	0.06	0.48	0.00	0.00	20.9
38	27	-0	5894	0	0	0	7894	--	--	16.08	16.08	0.00	0.13	0.05	0.37	0.00	0.00	20.9
39	27	-0	6085	0	0	0	8204	--	--	16.08	16.08	0.00	0.14	0.05	0.38	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	5071	0	0	0	2707	--	--	16.08	16.08	0.00	0.05	0.04	0.32	0.00	0.00	20.9
2	55	-0	4086	0	0	0	2193	--	--	16.08	16.08	0.10	0.04	0.03	0.26	0.00	0.00	20.9
3	55	-0	4074	0	0	0	2182	--	--	16.08	16.08	0.10	0.04	0.03	0.26	0.00	0.00	20.9
4	55	-0	3728	0	0	0	1982	--	--	16.08	16.08	0.10	0.04	0.03	0.23	0.00	0.00	20.9
5	55	-0	3715	0	0	0	1971	--	--	16.08	16.08	0.10	0.03	0.03	0.23	0.00	0.00	20.9
6	55	-0	3976	0	0	0	2132	--	--	16.08	16.08	0.10	0.04	0.03	0.25	0.00	0.00	20.9
7	55	-0	3933	0	0	0	2096	--	--	16.08	16.08	0.10	0.04	0.03	0.25	0.00	0.00	20.9
8	55	-0	3868	0	0	0	2069	--	--	16.08	16.08	0.10	0.04	0.03	0.24	0.00	0.00	20.9
9	55	-0	3826	0	0	0	2032	--	--	16.08	16.08	0.10	0.04	0.03	0.24	0.00	0.00	20.9
10	55	-0	4086	0	0	0	2193	--	--	16.08	16.08	0.10	0.04	0.03	0.26	0.00	0.00	20.9
11	55	-0	4074	0	0	0	2182	--	--	16.08	16.08	0.10	0.04	0.03	0.26	0.00	0.00	20.9
12	55	-0	3728	0	0	0	1982	--	--	16.08	16.08	0.10	0.04	0.03	0.23	0.00	0.00	20.9
13	55	-0	3715	0	0	0	1971	--	--	16.08	16.08	0.10	0.03	0.03	0.23	0.00	0.00	20.9
14	55	-0	3976	0	0	0	2132	--	--	16.08	16.08	0.10	0.04	0.03	0.25	0.00	0.00	20.9
15	55	-0	3933	0	0	0	2096	--	--	16.08	16.08	0.10	0.04	0.03	0.25	0.00	0.00	20.9
16	55	-0	3868	0	0	0	2069	--	--	16.08	16.08	0.10	0.04	0.03	0.24	0.00	0.00	20.9
17	55	-0	3826	0	0	0	2032	--	--	16.08	16.08	0.10	0.04	0.03	0.24	0.00	0.00	20.9
18	55	-0	8176	0	0	0	4709	--	--	16.08	16.08	0.00	0.08	0.07	0.51	0.00	0.00	20.9
19	55	-0	7084	0	0	0	3974	--	--	16.08	16.08	0.00	0.07	0.06	0.44	0.00	0.00	20.9
20	55	-0	7199	0	0	0	4068	--	--	16.08	16.08	0.00	0.07	0.06	0.45	0.00	0.00	20.9
37	55	-0	7714	0	0	0	4429	--	--	16.08	16.08	0.00	0.08	0.06	0.48	0.00	0.00	20.9
38	55	-0	5894	0	0	0	3202	--	--	16.08	16.08	0.00	0.05	0.05	0.37	0.00	0.00	20.9
39	55	-0	6085	0	0	0	3360	--	--	16.08	16.08	0.00	0.06	0.05	0.38	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 165 NI 1769 NF 1768 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	4295	0	0	0	-711	--	--	16.08	16.08	0.18	0.01	0.04	0.27	0.00	0.00	20.9
2	0	-0	3467	0	0	0	-561	--	--	16.08	16.08	0.29	0.01	0.03	0.22	0.00	0.00	20.9
3	0	-0	3489	0	0	0	-563	--	--	16.08	16.08	0.29	0.01	0.03	0.22	0.00	0.00	20.9
4	0	-0	3118	0	0	0	-531	--	--	16.08	16.08	0.29	0.01	0.03	0.20	0.00	0.00	20.9
5	0	-0	3140	0	0	0	-533	--	--	16.08	16.08	0.29	0.01	0.03	0.20	0.00	0.00	20.9
6	0	-0	3320	0	0	0	-549	--	--	16.08	16.08	0.29	0.01	0.03	0.21	0.00	0.00	20.9
7	0	-0	3392	0	0	0	-555	--	--	16.08	16.08	0.29	0.01	0.03	0.21	0.00	0.00	20.9
8	0	-0	3215	0	0	0	-540	--	--	16.08	16.08	0.29	0.01	0.03	0.20	0.00	0.00	20.9
9	0	-0	3288	0	0	0	-546	--	--	16.08	16.08	0.29	0.01	0.03	0.21	0.00	0.00	20.9
10	0	-0	3467	0	0	0	-561	--	--	16.08	16.08	0.29	0.01	0.03	0.22	0.00	0.00	20.9
11	0	-0	3489	0	0	0	-563	--	--	16.08	16.08	0.29	0.01	0.03	0.22	0.00	0.00	20.9
12	0	-0	3118	0	0	0	-531	--	--	16.08	16.08	0.29	0.01	0.03	0.20	0.00	0.00	20.9
13	0	-0	3140	0	0	0	-533	--	--	16.08	16.08	0.29	0.01	0.03	0.20	0.00	0.00	20.9
14	0	-0	3320	0	0	0	-549	--	--	16.08	16.08	0.29	0.01	0.03	0.21	0.00	0.00	20.9
15	0	-0	3392	0	0	0	-555	--	--	16.08	16.08	0.29	0.01	0.03	0.21	0.00	0.00	20.9
16	0	-0	3215	0	0	0	-540	--	--	16.08	16.08	0.29	0.01	0.03	0.20	0.00	0.00	20.9
17	0	-0	3288	0	0	0	-546	--	--	16.08	16.08	0.29	0.01	0.03	0.21	0.00	0.00	20.9
18	0	-0	7065	0	0	0	-810	--	--	16.08	16.08	0.18	0.01	0.06	0.44	0.00	0.00	20.9
19	0	-0	5992	0	0	0	-805	--	--	16.08	16.08	0.18	0.01	0.05	0.38	0.00	0.00	20.9
20	0	-0	6240	0	0	0	-787	--	--	16.08	16.08	0.18	0.01	0.05	0.39	0.00	0.00	20.9
37	0	-0	6701	0	0	0	-778	--	--	16.08	16.08	0.18	0.01	0.06	0.42	0.00	0.00	20.9
38	0	-0	4914	0	0	0	-771	--	--	16.08	16.08	0.18	0.01	0.04	0.31	0.00	0.00	20.9
39	0	-0	5327	0	0	0	-740	--	--	16.08	16.08	0.18	0.01	0.04	0.33	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	4295	0	0	0	5051	--	--	16.08	16.08	0.00	0.09	0.04	0.27	0.00	0.00	20.9
2	27	-0	3467	0	0	0	4090	--	--	16.08	16.08	0.10	0.07	0.03	0.22	0.00	0.00	20.9
3	27	-0	3489	0	0	0	4117	--	--	16.08	16.08	0.10	0.07	0.03	0.22	0.00	0.00	20.9
4	27	-0	3118	0	0	0	3652	--	--	16.08	16.08	0.10	0.06	0.03	0.20	0.00	0.00	20.9
5	27	-0	3140	0	0	0	3679	--	--	16.08	16.08	0.10	0.07	0.03	0.20	0.00	0.00	20.9
6	27	-0	3320	0	0	0	3905	--	--	16.08	16.08	0.10	0.07	0.03	0.21	0.00	0.00	20.9
7	27	-0	3392	0	0	0	3996	--	--	16.08	16.08	0.10	0.07	0.03	0.21	0.00	0.00	20.9
8	27	-0	3215	0	0	0	3773	--	--	16.08	16.08	0.10	0.07	0.03	0.20	0.00	0.00	20.9
9	27	-0	3288	0	0	0	3865	--	--	16.08	16.08	0.10	0.07	0.03	0.21	0.00	0.00	20.9
10	27	-0	3467	0	0	0	4090	--	--	16.08	16.08	0.10	0.07	0.03	0.22	0.00	0.00	20.9
11	27	-0	3489	0	0	0	4117	--	--	16.08	16.08	0.10	0.07	0.03	0.22	0.00	0.00	20.9
12	27	-0	3118	0	0	0	3652	--	--	16.08	16.08	0.10	0.06	0.03	0.20	0.00	0.00	20.9
13	27	-0	3140	0	0	0	3679	--	--	16.08	16.08	0.10	0.07	0.03	0.20	0.00	0.00	20.9
14	27	-0	3320	0	0	0	3905	--	--	16.08	16.08	0.10	0.07	0.03	0.21	0.00	0.00	20.9
15	27	-0	3392	0	0	0	3996	--	--	16.08	16.08	0.10	0.07	0.03	0.21	0.00	0.00	20.9
16	27	-0	3215	0	0	0	3773	--	--	16.08	16.08	0.10	0.07	0.03	0.20	0.00	0.00	20.9
17	27	-0	3288	0	0	0	3865	--	--	16.08	16.08	0.10	0.07	0.03	0.21	0.00	0.00	20.9
18	27	-0	7065	0	0	0	8668	--	--	16.08	16.08	0.00	0.15	0.06	0.44	0.00	0.00	20.9
19	27	-0	5992	0	0	0	7233	--	--	16.08	16.08	0.00	0.12	0.05	0.38	0.00	0.00	20.9
20	27	-0	6240	0	0	0	7584	--	--	16.08	16.08	0.00	0.13	0.05	0.39	0.00	0.00	20.9
37	27	-0	6701	0	0	0	8211	--	--	16.08	16.08	0.00	0.14	0.06	0.42	0.00	0.00	20.9
38	27	-0	4914	0	0	0	5822	--	--	16.08	16.08	0.00	0.10	0.04	0.31	0.00	0.00	20.9
39	27	-0	5327	0	0	0	6406	--	--	16.08	16.08	0.00	0.11	0.04	0.33	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	4295	0	0	0	1632	--	--	16.08	16.08	0.00	0.03	0.04	0.27	0.00	0.00	20.9
2	55	-0	3467	0	0	0	1330	--	--	16.08	16.08	0.10	0.02	0.03	0.22	0.00	0.00	20.9
3	55	-0	3489	0	0	0	1340	--	--	16.08	16.08	0.10	0.02	0.03	0.22	0.00	0.00	20.9
4	55	-0	3118	0	0	0	1170	--	--	16.08	16.08	0.10	0.02	0.03	0.20	0.00	0.00	20.9
5	55	-0	3140	0	0	0	1180	--	--	16.08	16.08	0.10	0.02	0.03	0.20	0.00	0.00	20.9
6	55	-0	3320	0	0	0	1262	--	--	16.08	16.08	0.10	0.02	0.03	0.21	0.00	0.00	20.9
7	55	-0	3392	0	0	0	1296	--	--	16.08	16.08	0.10	0.02	0.03	0.21	0.00	0.00	20.9
8	55	-0	3215	0	0	0	1214	--	--	16.08	16.08	0.10	0.02	0.03	0.20	0.00	0.00	20.9

9	55	-0	3288	0	0	0	1248	--	--	16.08	16.08	0.10	0.02	0.03	0.21	0.00	0.00	20.9
10	55	-0	3467	0	0	0	1330	--	--	16.08	16.08	0.10	0.02	0.03	0.22	0.00	0.00	20.9
11	55	-0	3489	0	0	0	1340	--	--	16.08	16.08	0.10	0.02	0.03	0.22	0.00	0.00	20.9
12	55	-0	3118	0	0	0	1170	--	--	16.08	16.08	0.10	0.02	0.03	0.20	0.00	0.00	20.9
13	55	-0	3140	0	0	0	1180	--	--	16.08	16.08	0.10	0.02	0.03	0.20	0.00	0.00	20.9
14	55	-0	3320	0	0	0	1262	--	--	16.08	16.08	0.10	0.02	0.03	0.21	0.00	0.00	20.9
15	55	-0	3392	0	0	0	1296	--	--	16.08	16.08	0.10	0.02	0.03	0.21	0.00	0.00	20.9
16	55	-0	3215	0	0	0	1214	--	--	16.08	16.08	0.10	0.02	0.03	0.20	0.00	0.00	20.9
17	55	-0	3288	0	0	0	1248	--	--	16.08	16.08	0.10	0.02	0.03	0.21	0.00	0.00	20.9
18	55	-0	7065	0	0	0	3044	--	--	16.08	16.08	0.00	0.05	0.06	0.44	0.00	0.00	20.9
19	55	-0	5992	0	0	0	2464	--	--	16.08	16.08	0.00	0.04	0.05	0.38	0.00	0.00	20.9
20	55	-0	6240	0	0	0	2617	--	--	16.08	16.08	0.00	0.04	0.05	0.39	0.00	0.00	20.9
37	55	-0	6701	0	0	0	2877	--	--	16.08	16.08	0.00	0.05	0.06	0.42	0.00	0.00	20.9
38	55	-0	4914	0	0	0	1910	--	--	16.08	16.08	0.00	0.03	0.04	0.31	0.00	0.00	20.9
39	55	-0	5327	0	0	0	2166	--	--	16.08	16.08	0.00	0.04	0.04	0.33	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 166 NI 1764 NF 1769 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	2540	0	0	0	-1115	--	--	16.08	16.08	0.18	0.02	0.02	0.16	0.00	0.00	20.9
2	0	-0	2028	0	0	0	-889	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
3	0	-0	2058	0	0	0	-894	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
4	0	-0	1849	0	0	0	-821	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
5	0	-0	1879	0	0	0	-827	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
6	0	-0	1931	0	0	0	-859	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
7	0	-0	2030	0	0	0	-876	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
8	0	-0	1877	0	0	0	-839	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
9	0	-0	1976	0	0	0	-856	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
10	0	-0	2028	0	0	0	-889	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
11	0	-0	2058	0	0	0	-894	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
12	0	-0	1849	0	0	0	-821	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
13	0	-0	1879	0	0	0	-827	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
14	0	-0	1931	0	0	0	-859	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
15	0	-0	2030	0	0	0	-876	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
16	0	-0	1877	0	0	0	-839	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
17	0	-0	1976	0	0	0	-856	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
18	0	-0	4069	0	0	0	-1502	--	--	16.08	16.08	0.18	0.02	0.03	0.26	0.00	0.00	20.9
19	0	-0	3568	0	0	0	-1378	--	--	16.08	16.08	0.18	0.02	0.03	0.22	0.00	0.00	20.9
20	0	-0	3694	0	0	0	-1392	--	--	16.08	16.08	0.18	0.02	0.03	0.23	0.00	0.00	20.9
37	0	-0	3825	0	0	0	-1436	--	--	16.08	16.08	0.18	0.02	0.03	0.24	0.00	0.00	20.9
38	0	-0	2990	0	0	0	-1230	--	--	16.08	16.08	0.18	0.02	0.02	0.19	0.00	0.00	20.9
39	0	-0	3200	0	0	0	-1253	--	--	16.08	16.08	0.18	0.02	0.03	0.20	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	2540	0	0	0	-1115	--	--	16.08	16.08	0.18	0.02	0.02	0.16	0.00	0.00	20.9
2	27	-0	2028	0	0	0	-889	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
3	27	-0	2058	0	0	0	-894	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
4	27	-0	1849	0	0	0	-821	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
5	27	-0	1879	0	0	0	-827	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
6	27	-0	1931	0	0	0	-859	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
7	27	-0	2030	0	0	0	-876	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
8	27	-0	1877	0	0	0	-839	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
9	27	-0	1976	0	0	0	-856	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
10	27	-0	2028	0	0	0	-889	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
11	27	-0	2058	0	0	0	-894	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
12	27	-0	1849	0	0	0	-821	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
13	27	-0	1879	0	0	0	-827	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
14	27	-0	1931	0	0	0	-859	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
15	27	-0	2030	0	0	0	-876	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
16	27	-0	1877	0	0	0	-839	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
17	27	-0	1976	0	0	0	-856	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
18	27	-0	4069	0	0	0	-1502	--	--	16.08	16.08	0.18	0.02	0.03	0.26	0.00	0.00	20.9
19	27	-0	3568	0	0	0	-1378	--	--	16.08	16.08	0.18	0.02	0.03	0.22	0.00	0.00	20.9
20	27	-0	3694	0	0	0	-1392	--	--	16.08	16.08	0.18	0.02	0.03	0.23	0.00	0.00	20.9
37	27	-0	3825	0	0	0	-1436	--	--	16.08	16.08	0.18	0.02	0.03	0.24	0.00	0.00	20.9
38	27	-0	2990	0	0	0	-1230	--	--	16.08	16.08	0.18	0.02	0.02	0.19	0.00	0.00	20.9
39	27	-0	3200	0	0	0	-1253	--	--	16.08	16.08	0.18	0.02	0.03	0.20	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	2540	0	0	0	270	--	--	16.08	16.08	0.00	0.00	0.02	0.16	0.00	0.00	20.9
2	55	-0	2028	0	0	0	218	--	--	16.08	16.08	0.10	0.00	0.02	0.13	0.00	0.00	20.9
3	55	-0	2058	0	0	0	229	--	--	16.08	16.08	0.10	0.00	0.02	0.13	0.00	0.00	20.9
4	55	-0	1849	0	0	0	187	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
5	55	-0	1879	0	0	0	198	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
6	55	-0	1931	0	0	0	194	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
7	55	-0	2030	0	0	0	231	--	--	16.08	16.08	0.10	0.00	0.02	0.13	0.00	0.00	20.9
8	55	-0	1877	0	0	0	185	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
9	55	-0	1976	0	0	0	222	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
10	55	-0	2028	0	0	0	218	--	--	16.08	16.08	0.10	0.00	0.02	0.13	0.00	0.00	20.9
11	55	-0	2058	0	0	0	229	--	--	16.08	16.08	0.10	0.00	0.02	0.13	0.00	0.00	20.9
12	55	-0	1849	0	0	0	187	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
13	55	-0	1879	0	0	0	198	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
14	55	-0	1931	0	0	0	194	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
15	55	-0	2030	0	0	0	231	--	--	16.08	16.08	0.10	0.00	0.02	0.13	0.00	0.00	20.9
16	55	-0	1877	0	0	0	185	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
17	55	-0	1976	0	0	0	222	--	--	16.08	16.08	0.10	0.00	0.02	0.12	0.00	0.00	20.9
18	55	-0	4069	0	0	0	717	--	--	16.08	16.08	0.00	0.01	0.03	0.26	0.00	0.00	20.9
19	55	-0	3568	0	0	0	567	--	--	16.08	16.08	0.00	0.01	0.03	0.22	0.00	0.00	20.9
20	55	-0	3694	0	0	0	623	--	--	16.08	16.08	0.00	0.01	0.03	0.23	0.00	0.00	20.9
37	55	-0	3825	0	0	0	650	--	--	16.08	16.08	0.00	0.01	0.03	0.24	0.00	0.00	20.9
38	55	-0	2990	0	0	0	400	--	--	16.08	16.08	0.00	0.01	0.02	0.19	0.00	0.00	20.9
39	55	-0	3200	0	0	0	492	--	--	16.08	16.08	0.00	0.01	0.03	0.20	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 167 NI 1770 NF 1764 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle V,Mx		cmq/m	cm
1	0	-0	1113	0	0	0	-1157	--	--	16.08	16.08	0.18	0.02	0.01 0.07	0.00	0.00	20.9
2	0	-0	870	0	0	0	-919	--	--	16.08	16.08	0.29	0.02	0.01 0.05	0.00	0.00	20.9
3	0	-0	900	0	0	0	-930	--	--	16.08	16.08	0.29	0.02	0.01 0.06	0.00	0.00	20.9
4	0	-0	812	0	0	0	-850	--	--	16.08	16.08	0.29	0.01	0.01 0.05	0.00	0.00	20.9
5	0	-0	842	0	0	0	-860	--	--	16.08	16.08	0.29	0.01	0.01 0.05	0.00	0.00	20.9
6	0	-0	814	0	0	0	-882	--	--	16.08	16.08	0.29	0.02	0.01 0.05	0.00	0.00	20.9
7	0	-0	915	0	0	0	-918	--	--	16.08	16.08	0.29	0.02	0.01 0.06	0.00	0.00	20.9
8	0	-0	797	0	0	0	-862	--	--	16.08	16.08	0.29	0.01	0.01 0.05	0.00	0.00	20.9
9	0	-0	898	0	0	0	-897	--	--	16.08	16.08	0.29	0.02	0.01 0.06	0.00	0.00	20.9
10	0	-0	870	0	0	0	-919	--	--	16.08	16.08	0.29	0.02	0.01 0.05	0.00	0.00	20.9
11	0	-0	900	0	0	0	-930	--	--	16.08	16.08	0.29	0.02	0.01 0.06	0.00	0.00	20.9
12	0	-0	812	0	0	0	-850	--	--	16.08	16.08	0.29	0.01	0.01 0.05	0.00	0.00	20.9
13	0	-0	842	0	0	0	-860	--	--	16.08	16.08	0.29	0.01	0.01 0.05	0.00	0.00	20.9
14	0	-0	814	0	0	0	-882	--	--	16.08	16.08	0.29	0.02	0.01 0.05	0.00	0.00	20.9
15	0	-0	915	0	0	0	-918	--	--	16.08	16.08	0.29	0.02	0.01 0.06	0.00	0.00	20.9
16	0	-0	797	0	0	0	-862	--	--	16.08	16.08	0.29	0.01	0.01 0.05	0.00	0.00	20.9
17	0	-0	898	0	0	0	-897	--	--	16.08	16.08	0.29	0.02	0.01 0.06	0.00	0.00	20.9
18	0	-0	1719	0	0	0	-1572	--	--	16.08	16.08	0.18	0.03	0.01 0.11	0.00	0.00	20.9
19	0	-0	1606	0	0	0	-1451	--	--	16.08	16.08	0.18	0.02	0.01 0.10	0.00	0.00	20.9
20	0	-0	1648	0	0	0	-1471	--	--	16.08	16.08	0.18	0.02	0.01 0.10	0.00	0.00	20.9
37	0	-0	1582	0	0	0	-1497	--	--	16.08	16.08	0.18	0.02	0.01 0.10	0.00	0.00	20.9
38	0	-0	1393	0	0	0	-1294	--	--	16.08	16.08	0.18	0.02	0.01 0.09	0.00	0.00	20.9
39	0	-0	1463	0	0	0	-1328	--	--	16.08	16.08	0.18	0.02	0.01 0.09	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle V,Mx		cmq/m	cm
1	27	-0	1113	0	0	0	-1157	--	--	16.08	16.08	0.18	0.02	0.01 0.07	0.00	0.00	20.9
2	27	-0	870	0	0	0	-919	--	--	16.08	16.08	0.29	0.02	0.01 0.05	0.00	0.00	20.9
3	27	-0	900	0	0	0	-930	--	--	16.08	16.08	0.29	0.02	0.01 0.06	0.00	0.00	20.9
4	27	-0	812	0	0	0	-850	--	--	16.08	16.08	0.29	0.01	0.01 0.05	0.00	0.00	20.9
5	27	-0	842	0	0	0	-860	--	--	16.08	16.08	0.29	0.01	0.01 0.05	0.00	0.00	20.9
6	27	-0	814	0	0	0	-882	--	--	16.08	16.08	0.29	0.02	0.01 0.05	0.00	0.00	20.9
7	27	-0	915	0	0	0	-918	--	--	16.08	16.08	0.29	0.02	0.01 0.06	0.00	0.00	20.9
8	27	-0	797	0	0	0	-862	--	--	16.08	16.08	0.29	0.01	0.01 0.05	0.00	0.00	20.9
9	27	-0	898	0	0	0	-897	--	--	16.08	16.08	0.29	0.02	0.01 0.06	0.00	0.00	20.9
10	27	-0	870	0	0	0	-919	--	--	16.08	16.08	0.29	0.02	0.01 0.05	0.00	0.00	20.9
11	27	-0	900	0	0	0	-930	--	--	16.08	16.08	0.29	0.02	0.01 0.06	0.00	0.00	20.9
12	27	-0	812	0	0	0	-850	--	--	16.08	16.08	0.29	0.01	0.01 0.05	0.00	0.00	20.9
13	27	-0	842	0	0	0	-860	--	--	16.08	16.08	0.29	0.01	0.01 0.05	0.00	0.00	20.9
14	27	-0	814	0	0	0	-882	--	--	16.08	16.08	0.29	0.02	0.01 0.05	0.00	0.00	20.9
15	27	-0	915	0	0	0	-918	--	--	16.08	16.08	0.29	0.02	0.01 0.06	0.00	0.00	20.9
16	27	-0	797	0	0	0	-862	--	--	16.08	16.08	0.29	0.01	0.01 0.05	0.00	0.00	20.9
17	27	-0	898	0	0	0	-897	--	--	16.08	16.08	0.29	0.02	0.01 0.06	0.00	0.00	20.9
18	27	-0	1719	0	0	0	-1572	--	--	16.08	16.08	0.18	0.03	0.01 0.11	0.00	0.00	20.9
19	27	-0	1606	0	0	0	-1451	--	--	16.08	16.08	0.18	0.02	0.01 0.10	0.00	0.00	20.9
20	27	-0	1648	0	0	0	-1471	--	--	16.08	16.08	0.18	0.02	0.01 0.10	0.00	0.00	20.9
37	27	-0	1582	0	0	0	-1497	--	--	16.08	16.08	0.18	0.02	0.01 0.10	0.00	0.00	20.9
38	27	-0	1393	0	0	0	-1294	--	--	16.08	16.08	0.18	0.02	0.01 0.09	0.00	0.00	20.9
39	27	-0	1463	0	0	0	-1328	--	--	16.08	16.08	0.18	0.02	0.01 0.09	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle V,Mx		cmq/m	cm
1	55	-0	1113	0	0	0	-1157	--	--	16.08	16.08	0.18	0.02	0.01 0.07	0.00	0.00	20.9
2	55	-0	870	0	0	0	-919	--	--	16.08	16.08	0.29	0.02	0.01 0.05	0.00	0.00	20.9
3	55	-0	900	0	0	0	-930	--	--	16.08	16.08	0.29	0.02	0.01 0.06	0.00	0.00	20.9
4	55	-0	812	0	0	0	-850	--	--	16.08	16.08	0.29	0.01	0.01 0.05	0.00	0.00	20.9
5	55	-0	842	0	0	0	-860	--	--	16.08	16.08	0.29	0.01	0.01 0.05	0.00	0.00	20.9
6	55	-0	814	0	0	0	-882	--	--	16.08	16.08	0.29	0.02	0.01 0.05	0.00	0.00	20.9
7	55	-0	915	0	0	0	-918	--	--	16.08	16.08	0.29	0.02	0.01 0.06	0.00	0.00	20.9
8	55	-0	797	0	0	0	-862	--	--	16.08	16.08	0.29	0.01	0.01 0.05	0.00	0.00	20.9
9	55	-0	898	0	0	0	-897	--	--	16.08	16.08	0.29	0.02	0.01 0.06	0.00	0.00	20.9
10	55	-0	870	0	0	0	-919	--	--	16.08	16.08	0.29	0.02	0.01 0.05	0.00	0.00	20.9
11	55	-0	900	0	0	0	-930	--	--	16.08	16.08	0.29	0.02	0.01 0.06	0.00	0.00	20.9
12	55	-0	812	0	0	0	-850	--	--	16.08	16.08	0.29	0.01	0.01 0.05	0.00	0.00	20.9
13	55	-0	842	0	0	0	-860	--	--	16.08	16.08	0.29	0.01	0.01 0.05	0.00	0.00	20.9
14	55	-0	814	0	0	0	-882	--	--	16.08	16.08	0.29	0.02	0.01 0.05	0.00	0.00	20.9
15	55	-0	915	0	0	0	-918	--	--	16.08	16.08	0.29	0.02	0.01 0.06	0.00	0.00	20.9
16	55	-0	797	0	0	0	-862	--	--	16.08	16.08	0.29	0.01	0.01 0.05	0.00	0.00	20.9
17	55	-0	898	0	0	0	-897	--	--	16.08	16.08	0.29	0.02	0.01 0.06	0.00	0.00	20.9
18	55	-0	1719	0	0	0	-1572	--	--	16.08	16.08	0.18	0.03	0.01 0.11	0.00	0.00	20.9
19	55	-0	1606	0	0	0	-1451	--	--	16.08	16.08	0.18	0.02	0.01 0.10	0.00	0.00	20.9
20	55	-0	1648	0	0	0	-1471	--	--	16.08	16.08	0.18	0.02	0.01 0.10	0.00	0.00	20.9
37	55	-0	1582	0	0	0	-1497	--	--	16.08	16.08	0.18	0.02	0.01 0.10	0.00	0.00	20.9
38	55	-0	1393	0	0	0	-1294	--	--	16.08	16.08	0.18	0.02	0.01 0.09	0.00	0.00	20.9
39	55	-0	1463	0	0	0	-1328	--	--	16.08	16.08	0.18	0.02	0.01 0.09	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 168 NI 1771 NF 1770 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle V,Mx		cmq/m	cm
1	0	-0	-178	0	0	0	-1010	--	--	16.08	16.08	0.18	0.02	0.00 0.01	0.00	0.00	20.9
2	0	-0	-173	0	0	0	-812	--	--	16.08	16.08	0.29	0.01	0.00 0.01	0.00	0.00	20.9
3	0	-0	-142	0	0	0	-812	--	--	16.08	16.08	0.29	0.01	0.00 0.01	0.00	0.00	20.9
4	0	-0	-131	0	0	0	-743	--	--	16.08	16.08	0.29	0.01	0.00 0.01	0.00	0.00	20.9
5	0	-0	-100	0	0	0	-743	--	--	16.08	16.08	0.29	0.01	0.00 0.01	0.00	0.00	20.9
6	0	-0	-195	0	0	0	-788	--	--	16.08	16.08	0.29	0.01	0.00 0.01	0.00	0.00	20.9
7	0	-0	-92	0	0	0	-787	--	--	16.08	16.08	0.29	0.01	0.00 0.01	0.00	0.00	20.9
8	0	-0	-182	0	0	0	-767	--	--	16.08	16.08	0.29	0.01	0.00 0.01	0.00	0.00	20.9
9	0	-0	-79	0	0	0	-766	--	--	16.08	16.08	0.29	0.01	0.00 0.00	0.00	0.00	20.9
10	0	-0	-173	0	0	0	-812	--	--	16.08	16.08	0.29	0.01	0.00 0.01	0.00	0.00	20.9
11	0	-0	-142	0	0	0	-812	--	--	16.08	16.08	0.29	0.01	0.00 0.01	0.00	0.00	20.9
12	0	-0	-131	0	0	0	-743	--	--	16.08	16.08	0.29	0.01	0.00 0.01	0.00	0.00	20.9
13	0	-0	-100	0	0	0	-743	--	--	16.08	16.08	0.29	0.01	0.00 0.01	0.00	0.00	20.9
14	0	-0	-195	0	0	0	-788	--	--	16.08	16.08	0.29	0.01	0.00 0.01	0.00	0.00	20.9
15	0	-0	-92	0	0	0	-787	--	--	16.08	16.08	0.29	0.01	0.00 0.01	0.00	0.00	20.9
16	0	-0	-182	0	0	0	-767	--	--	16.08	16.08	0.29	0.01	0.00 0.01	0.00	0.00	20.9

17	0	-0	-79	0	0	0	-766	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
18	0	-0	-373	0	0	0	-1371	--	--	16.08	16.08	0.18	0.02	0.00	0.02	0.00	0.00	20.9
19	0	-0	-170	0	0	0	-1223	--	--	16.08	16.08	0.18	0.02	0.00	0.01	0.00	0.00	20.9
20	0	-0	-189	0	0	0	-1242	--	--	16.08	16.08	0.18	0.02	0.00	0.01	0.00	0.00	20.9
37	0	-0	-407	0	0	0	-1326	--	--	16.08	16.08	0.18	0.02	0.00	0.03	0.00	0.00	20.9
38	0	-0	-70	0	0	0	-1079	--	--	16.08	16.08	0.18	0.02	0.00	0.00	0.00	0.00	20.9
39	0	-0	-101	0	0	0	-1111	--	--	16.08	16.08	0.18	0.02	0.00	0.01	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-178	0	0	0	-1010	--	--	16.08	16.08	0.18	0.02	0.00	0.01	0.00	0.00	20.9
2	27	-0	-173	0	0	0	-812	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
3	27	-0	-142	0	0	0	-812	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
4	27	-0	-131	0	0	0	-743	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
5	27	-0	-100	0	0	0	-743	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
6	27	-0	-195	0	0	0	-788	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
7	27	-0	-92	0	0	0	-787	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
8	27	-0	-182	0	0	0	-767	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
9	27	-0	-79	0	0	0	-766	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
10	27	-0	-173	0	0	0	-812	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
11	27	-0	-142	0	0	0	-812	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
12	27	-0	-131	0	0	0	-743	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
13	27	-0	-100	0	0	0	-743	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
14	27	-0	-195	0	0	0	-788	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
15	27	-0	-92	0	0	0	-787	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
16	27	-0	-182	0	0	0	-767	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
17	27	-0	-79	0	0	0	-766	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
18	27	-0	-373	0	0	0	-1371	--	--	16.08	16.08	0.18	0.02	0.00	0.02	0.00	0.00	20.9
19	27	-0	-170	0	0	0	-1223	--	--	16.08	16.08	0.18	0.02	0.00	0.01	0.00	0.00	20.9
20	27	-0	-189	0	0	0	-1242	--	--	16.08	16.08	0.18	0.02	0.00	0.01	0.00	0.00	20.9
37	27	-0	-407	0	0	0	-1326	--	--	16.08	16.08	0.18	0.02	0.00	0.03	0.00	0.00	20.9
38	27	-0	-70	0	0	0	-1079	--	--	16.08	16.08	0.18	0.02	0.00	0.00	0.00	0.00	20.9
39	27	-0	-101	0	0	0	-1111	--	--	16.08	16.08	0.18	0.02	0.00	0.01	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	-178	0	0	0	-1010	--	--	16.08	16.08	0.18	0.02	0.00	0.01	0.00	0.00	20.9
2	55	-0	-173	0	0	0	-812	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
3	55	-0	-142	0	0	0	-812	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
4	55	-0	-131	0	0	0	-743	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
5	55	-0	-100	0	0	0	-743	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
6	55	-0	-195	0	0	0	-788	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
7	55	-0	-92	0	0	0	-787	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
8	55	-0	-182	0	0	0	-767	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
9	55	-0	-79	0	0	0	-766	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
10	55	-0	-173	0	0	0	-812	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
11	55	-0	-142	0	0	0	-812	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
12	55	-0	-131	0	0	0	-743	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
13	55	-0	-100	0	0	0	-743	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
14	55	-0	-195	0	0	0	-788	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
15	55	-0	-92	0	0	0	-787	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
16	55	-0	-182	0	0	0	-767	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
17	55	-0	-79	0	0	0	-766	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
18	55	-0	-373	0	0	0	-1371	--	--	16.08	16.08	0.18	0.02	0.00	0.02	0.00	0.00	20.9
19	55	-0	-170	0	0	0	-1223	--	--	16.08	16.08	0.18	0.02	0.00	0.01	0.00	0.00	20.9
20	55	-0	-189	0	0	0	-1242	--	--	16.08	16.08	0.18	0.02	0.00	0.01	0.00	0.00	20.9
37	55	-0	-407	0	0	0	-1326	--	--	16.08	16.08	0.18	0.02	0.00	0.03	0.00	0.00	20.9
38	55	-0	-70	0	0	0	-1079	--	--	16.08	16.08	0.18	0.02	0.00	0.00	0.00	0.00	20.9
39	55	-0	-101	0	0	0	-1111	--	--	16.08	16.08	0.18	0.02	0.00	0.01	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 169 NI 1765 NF 1771 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-1479	0	0	0	-1191	--	--	16.08	16.08	0.18	0.02	0.01	0.09	0.00	0.00	20.9
2	0	-0	-1226	0	0	0	-952	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
3	0	-0	-1193	0	0	0	-957	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
4	0	-0	-1082	0	0	0	-875	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
5	0	-0	-1050	0	0	0	-880	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
6	0	-0	-1213	0	0	0	-918	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
7	0	-0	-1106	0	0	0	-936	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
8	0	-0	-1170	0	0	0	-895	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
9	0	-0	-1063	0	0	0	-913	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
10	0	-0	-1226	0	0	0	-952	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
11	0	-0	-1193	0	0	0	-957	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
12	0	-0	-1082	0	0	0	-875	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
13	0	-0	-1050	0	0	0	-880	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
14	0	-0	-1213	0	0	0	-918	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
15	0	-0	-1106	0	0	0	-936	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
16	0	-0	-1170	0	0	0	-895	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
17	0	-0	-1063	0	0	0	-913	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
18	0	-0	-2487	0	0	0	-1644	--	--	16.08	16.08	0.18	0.03	0.02	0.16	0.00	0.00	20.9
19	0	-0	-1965	0	0	0	-1485	--	--	16.08	16.08	0.18	0.02	0.02	0.12	0.00	0.00	20.9
20	0	-0	-2042	0	0	0	-1510	--	--	16.08	16.08	0.18	0.03	0.02	0.13	0.00	0.00	20.9
37	0	-0	-2416	0	0	0	-1575	--	--	16.08	16.08	0.18	0.03	0.02	0.15	0.00	0.00	20.9
38	0	-0	-1546	0	0	0	-1309	--	--	16.08	16.08	0.18	0.02	0.01	0.10	0.00	0.00	20.9
39	0	-0	-1676	0	0	0	-1351	--	--	16.08	16.08	0.18	0.02	0.01	0.11	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-1479	0	0	0	-1191	--	--	16.08	16.08	0.18	0.02	0.01	0.09	0.00	0.00	20.9
2	27	-0	-1226	0	0	0	-952	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
3	27	-0	-1193	0	0	0	-957	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
4	27	-0	-1082	0	0	0	-875	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
5	27	-0	-1050	0	0	0	-880	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
6	27	-0	-1213	0	0	0	-918	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
7	27	-0	-1106	0	0	0	-936	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
8	27	-0	-1170	0	0	0	-895	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
9	27	-0	-1063	0	0	0	-913	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
10	27	-0	-1226	0	0	0	-952	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
11	27	-0	-1193	0	0	0	-957	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
12	27	-0	-1082	0	0	0	-875	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9

13	27	-0	-1050	0	0	0	-880	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
14	27	-0	-1213	0	0	0	-918	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
15	27	-0	-1106	0	0	0	-936	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
16	27	-0	-1170	0	0	0	-895	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
17	27	-0	-1063	0	0	0	-913	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
18	27	-0	-2487	0	0	0	-1644	--	--	16.08	16.08	0.18	0.03	0.02	0.16	0.00	0.00	20.9
19	27	-0	-1965	0	0	0	-1485	--	--	16.08	16.08	0.18	0.02	0.02	0.12	0.00	0.00	20.9
20	27	-0	-2042	0	0	0	-1510	--	--	16.08	16.08	0.18	0.03	0.02	0.13	0.00	0.00	20.9
37	27	-0	-2416	0	0	0	-1575	--	--	16.08	16.08	0.18	0.03	0.02	0.15	0.00	0.00	20.9
38	27	-0	-1546	0	0	0	-1309	--	--	16.08	16.08	0.18	0.02	0.01	0.10	0.00	0.00	20.9
39	27	-0	-1676	0	0	0	-1351	--	--	16.08	16.08	0.18	0.02	0.01	0.11	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	-1479	0	0	0	-1191	--	--	16.08	16.08	0.18	0.02	0.01	0.09	0.00	0.00	20.9
2	55	-0	-1226	0	0	0	-952	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
3	55	-0	-1193	0	0	0	-957	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
4	55	-0	-1082	0	0	0	-875	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
5	55	-0	-1050	0	0	0	-880	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
6	55	-0	-1213	0	0	0	-918	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
7	55	-0	-1106	0	0	0	-936	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
8	55	-0	-1170	0	0	0	-895	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
9	55	-0	-1063	0	0	0	-913	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
10	55	-0	-1226	0	0	0	-952	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
11	55	-0	-1193	0	0	0	-957	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
12	55	-0	-1082	0	0	0	-875	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
13	55	-0	-1050	0	0	0	-880	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
14	55	-0	-1213	0	0	0	-918	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
15	55	-0	-1106	0	0	0	-936	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
16	55	-0	-1170	0	0	0	-895	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
17	55	-0	-1063	0	0	0	-913	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
18	55	-0	-2487	0	0	0	-1644	--	--	16.08	16.08	0.18	0.03	0.02	0.16	0.00	0.00	20.9
19	55	-0	-1965	0	0	0	-1485	--	--	16.08	16.08	0.18	0.02	0.02	0.12	0.00	0.00	20.9
20	55	-0	-2042	0	0	0	-1510	--	--	16.08	16.08	0.18	0.03	0.02	0.13	0.00	0.00	20.9
37	55	-0	-2416	0	0	0	-1575	--	--	16.08	16.08	0.18	0.03	0.02	0.15	0.00	0.00	20.9
38	55	-0	-1546	0	0	0	-1309	--	--	16.08	16.08	0.18	0.02	0.01	0.10	0.00	0.00	20.9
39	55	-0	-1676	0	0	0	-1351	--	--	16.08	16.08	0.18	0.02	0.01	0.11	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 170 NI 1766 NF 1765 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-2932	0	0	0	510	--	--	16.08	16.08	0.00	0.01	0.02	0.18	0.00	0.00	20.9
2	0	-0	-2404	0	0	0	449	--	--	16.08	16.08	0.10	0.01	0.02	0.15	0.00	0.00	20.9
3	0	-0	-2370	0	0	0	419	--	--	16.08	16.08	0.10	0.01	0.02	0.15	0.00	0.00	20.9
4	0	-0	-2140	0	0	0	365	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
5	0	-0	-2106	0	0	0	335	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
6	0	-0	-2352	0	0	0	455	--	--	16.08	16.08	0.10	0.01	0.02	0.15	0.00	0.00	20.9
7	0	-0	-2237	0	0	0	354	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
8	0	-0	-2273	0	0	0	430	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
9	0	-0	-2158	0	0	0	329	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
10	0	-0	-2404	0	0	0	449	--	--	16.08	16.08	0.10	0.01	0.02	0.15	0.00	0.00	20.9
11	0	-0	-2370	0	0	0	419	--	--	16.08	16.08	0.10	0.01	0.02	0.15	0.00	0.00	20.9
12	0	-0	-2140	0	0	0	365	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
13	0	-0	-2106	0	0	0	335	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
14	0	-0	-2352	0	0	0	455	--	--	16.08	16.08	0.10	0.01	0.02	0.15	0.00	0.00	20.9
15	0	-0	-2237	0	0	0	354	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
16	0	-0	-2273	0	0	0	430	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
17	0	-0	-2158	0	0	0	329	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
18	0	-0	-4886	0	0	0	1214	--	--	16.08	16.08	0.00	0.02	0.04	0.31	0.00	0.00	20.9
19	0	-0	-3970	0	0	0	806	--	--	16.08	16.08	0.00	0.01	0.03	0.25	0.00	0.00	20.9
20	0	-0	-4128	0	0	0	880	--	--	16.08	16.08	0.00	0.02	0.03	0.26	0.00	0.00	20.9
37	0	-0	-4704	0	0	0	1187	--	--	16.08	16.08	0.00	0.02	0.04	0.30	0.00	0.00	20.9
38	0	-0	-3177	0	0	0	507	--	--	16.08	16.08	0.00	0.01	0.03	0.20	0.00	0.00	20.9
39	0	-0	-3441	0	0	0	630	--	--	16.08	16.08	0.00	0.01	0.03	0.22	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-2932	0	0	0	-1089	--	--	16.08	16.08	0.18	0.02	0.02	0.18	0.00	0.00	20.9
2	27	-0	-2404	0	0	0	-863	--	--	16.08	16.08	0.29	0.01	0.02	0.15	0.00	0.00	20.9
3	27	-0	-2370	0	0	0	-874	--	--	16.08	16.08	0.29	0.02	0.02	0.15	0.00	0.00	20.9
4	27	-0	-2140	0	0	0	-802	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
5	27	-0	-2106	0	0	0	-813	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
6	27	-0	-2352	0	0	0	-828	--	--	16.08	16.08	0.29	0.01	0.02	0.15	0.00	0.00	20.9
7	27	-0	-2237	0	0	0	-866	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
8	27	-0	-2273	0	0	0	-810	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
9	27	-0	-2158	0	0	0	-848	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
10	27	-0	-2404	0	0	0	-863	--	--	16.08	16.08	0.29	0.01	0.02	0.15	0.00	0.00	20.9
11	27	-0	-2370	0	0	0	-874	--	--	16.08	16.08	0.29	0.02	0.02	0.15	0.00	0.00	20.9
12	27	-0	-2140	0	0	0	-802	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
13	27	-0	-2106	0	0	0	-813	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
14	27	-0	-2352	0	0	0	-828	--	--	16.08	16.08	0.29	0.01	0.02	0.15	0.00	0.00	20.9
15	27	-0	-2237	0	0	0	-866	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
16	27	-0	-2273	0	0	0	-810	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
17	27	-0	-2158	0	0	0	-848	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
18	27	-0	-4886	0	0	0	-1451	--	--	16.08	16.08	0.18	0.02	0.04	0.31	0.00	0.00	20.9
19	27	-0	-3970	0	0	0	-1359	--	--	16.08	16.08	0.18	0.02	0.03	0.25	0.00	0.00	20.9
20	27	-0	-4128	0	0	0	-1372	--	--	16.08	16.08	0.18	0.02	0.03	0.26	0.00	0.00	20.9
37	27	-0	-4704	0	0	0	-1378	--	--	16.08	16.08	0.18	0.02	0.04	0.30	0.00	0.00	20.9
38	27	-0	-3177	0	0	0	-1225	--	--	16.08	16.08	0.18	0.02	0.03	0.20	0.00	0.00	20.9
39	27	-0	-3441	0	0	0	-1246	--	--	16.08	16.08	0.18	0.02	0.03	0.22	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	-2932	0	0	0	-1089	--	--	16.08	16.08	0.18	0.02	0.02	0.18	0.00	0.00	20.9
2	55	-0	-2404	0	0	0	-863	--	--	16.08	16.08	0.29	0.01	0.02	0.15	0.00	0.00	20.9
3	55	-0	-2370	0	0	0	-874	--	--	16.08	16.08	0.29	0.02	0.02	0.15	0.00	0.00	20.9
4	55	-0	-2140	0	0	0	-802	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
5	55	-0	-2106	0	0	0	-813	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
6	55	-0	-2352	0	0	0	-828	--	--	16.08	16.08	0.29	0.01	0.02	0.15	0.00	0.00	20.9
7	55	-0	-2237	0	0	0	-866	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
8	55	-0	-2273	0	0	0	-810	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9

9	55	-0	-2158	0	0	0	-848	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
10	55	-0	-2404	0	0	0	-863	--	--	16.08	16.08	0.29	0.01	0.02	0.15	0.00	0.00	20.9
11	55	-0	-2370	0	0	0	-874	--	--	16.08	16.08	0.29	0.02	0.02	0.15	0.00	0.00	20.9
12	55	-0	-2140	0	0	0	-802	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
13	55	-0	-2106	0	0	0	-813	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
14	55	-0	-2352	0	0	0	-828	--	--	16.08	16.08	0.29	0.01	0.02	0.15	0.00	0.00	20.9
15	55	-0	-2237	0	0	0	-866	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
16	55	-0	-2273	0	0	0	-810	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
17	55	-0	-2158	0	0	0	-848	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
18	55	-0	-4886	0	0	0	-1451	--	--	16.08	16.08	0.18	0.02	0.04	0.31	0.00	0.00	20.9
19	55	-0	-3970	0	0	0	-1359	--	--	16.08	16.08	0.18	0.02	0.03	0.25	0.00	0.00	20.9
20	55	-0	-4128	0	0	0	-1372	--	--	16.08	16.08	0.18	0.02	0.03	0.26	0.00	0.00	20.9
37	55	-0	-4704	0	0	0	-1378	--	--	16.08	16.08	0.18	0.02	0.04	0.30	0.00	0.00	20.9
38	55	-0	-3177	0	0	0	-1225	--	--	16.08	16.08	0.18	0.02	0.03	0.20	0.00	0.00	20.9
39	55	-0	-3441	0	0	0	-1246	--	--	16.08	16.08	0.18	0.02	0.03	0.22	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 171 NI 1767 NF 1766 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-4692	0	0	0	1926	--	--	16.08	16.08	0.00	0.03	0.04	0.29	0.00	0.00	20.9
2	0	-0	-3840	0	0	0	1611	--	--	16.08	16.08	0.10	0.03	0.03	0.24	0.00	0.00	20.9
3	0	-0	-3809	0	0	0	1578	--	--	16.08	16.08	0.10	0.03	0.03	0.24	0.00	0.00	20.9
4	0	-0	-3409	0	0	0	1386	--	--	16.08	16.08	0.10	0.02	0.03	0.21	0.00	0.00	20.9
5	0	-0	-3378	0	0	0	1353	--	--	16.08	16.08	0.10	0.02	0.03	0.21	0.00	0.00	20.9
6	0	-0	-3725	0	0	0	1570	--	--	16.08	16.08	0.10	0.03	0.03	0.23	0.00	0.00	20.9
7	0	-0	-3622	0	0	0	1461	--	--	16.08	16.08	0.10	0.03	0.03	0.23	0.00	0.00	20.9
8	0	-0	-3596	0	0	0	1503	--	--	16.08	16.08	0.10	0.03	0.03	0.23	0.00	0.00	20.9
9	0	-0	-3493	0	0	0	1394	--	--	16.08	16.08	0.10	0.02	0.03	0.22	0.00	0.00	20.9
10	0	-0	-3840	0	0	0	1611	--	--	16.08	16.08	0.10	0.03	0.03	0.24	0.00	0.00	20.9
11	0	-0	-3809	0	0	0	1578	--	--	16.08	16.08	0.10	0.03	0.03	0.24	0.00	0.00	20.9
12	0	-0	-3409	0	0	0	1386	--	--	16.08	16.08	0.10	0.02	0.03	0.21	0.00	0.00	20.9
13	0	-0	-3378	0	0	0	1353	--	--	16.08	16.08	0.10	0.02	0.03	0.21	0.00	0.00	20.9
14	0	-0	-3725	0	0	0	1570	--	--	16.08	16.08	0.10	0.03	0.03	0.23	0.00	0.00	20.9
15	0	-0	-3622	0	0	0	1461	--	--	16.08	16.08	0.10	0.03	0.03	0.23	0.00	0.00	20.9
16	0	-0	-3596	0	0	0	1503	--	--	16.08	16.08	0.10	0.03	0.03	0.23	0.00	0.00	20.9
17	0	-0	-3493	0	0	0	1394	--	--	16.08	16.08	0.10	0.02	0.03	0.22	0.00	0.00	20.9
18	0	-0	-7877	0	0	0	3642	--	--	16.08	16.08	0.00	0.06	0.06	0.49	0.00	0.00	20.9
19	0	-0	-6404	0	0	0	2751	--	--	16.08	16.08	0.00	0.05	0.05	0.40	0.00	0.00	20.9
20	0	-0	-6712	0	0	0	2950	--	--	16.08	16.08	0.00	0.05	0.06	0.42	0.00	0.00	20.9
37	0	-0	-7571	0	0	0	3526	--	--	16.08	16.08	0.00	0.06	0.06	0.47	0.00	0.00	20.9
38	0	-0	-5117	0	0	0	2041	--	--	16.08	16.08	0.00	0.03	0.04	0.32	0.00	0.00	20.9
39	0	-0	-5630	0	0	0	2372	--	--	16.08	16.08	0.00	0.04	0.05	0.35	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-4692	0	0	0	1926	--	--	16.08	16.08	0.00	0.03	0.04	0.29	0.00	0.00	20.9
2	27	-0	-3840	0	0	0	1611	--	--	16.08	16.08	0.10	0.03	0.03	0.24	0.00	0.00	20.9
3	27	-0	-3809	0	0	0	1578	--	--	16.08	16.08	0.10	0.03	0.03	0.24	0.00	0.00	20.9
4	27	-0	-3409	0	0	0	1386	--	--	16.08	16.08	0.10	0.02	0.03	0.21	0.00	0.00	20.9
5	27	-0	-3378	0	0	0	1353	--	--	16.08	16.08	0.10	0.02	0.03	0.21	0.00	0.00	20.9
6	27	-0	-3725	0	0	0	1570	--	--	16.08	16.08	0.10	0.03	0.03	0.23	0.00	0.00	20.9
7	27	-0	-3622	0	0	0	1461	--	--	16.08	16.08	0.10	0.03	0.03	0.23	0.00	0.00	20.9
8	27	-0	-3596	0	0	0	1503	--	--	16.08	16.08	0.10	0.03	0.03	0.23	0.00	0.00	20.9
9	27	-0	-3493	0	0	0	1394	--	--	16.08	16.08	0.10	0.02	0.03	0.22	0.00	0.00	20.9
10	27	-0	-3840	0	0	0	1611	--	--	16.08	16.08	0.10	0.03	0.03	0.24	0.00	0.00	20.9
11	27	-0	-3809	0	0	0	1578	--	--	16.08	16.08	0.10	0.03	0.03	0.24	0.00	0.00	20.9
12	27	-0	-3409	0	0	0	1386	--	--	16.08	16.08	0.10	0.02	0.03	0.21	0.00	0.00	20.9
13	27	-0	-3378	0	0	0	1353	--	--	16.08	16.08	0.10	0.02	0.03	0.21	0.00	0.00	20.9
14	27	-0	-3725	0	0	0	1570	--	--	16.08	16.08	0.10	0.03	0.03	0.23	0.00	0.00	20.9
15	27	-0	-3622	0	0	0	1461	--	--	16.08	16.08	0.10	0.03	0.03	0.23	0.00	0.00	20.9
16	27	-0	-3596	0	0	0	1503	--	--	16.08	16.08	0.10	0.03	0.03	0.23	0.00	0.00	20.9
17	27	-0	-3493	0	0	0	1394	--	--	16.08	16.08	0.10	0.02	0.03	0.22	0.00	0.00	20.9
18	27	-0	-7877	0	0	0	3642	--	--	16.08	16.08	0.00	0.06	0.06	0.49	0.00	0.00	20.9
19	27	-0	-6404	0	0	0	2751	--	--	16.08	16.08	0.00	0.05	0.05	0.40	0.00	0.00	20.9
20	27	-0	-6712	0	0	0	2950	--	--	16.08	16.08	0.00	0.05	0.06	0.42	0.00	0.00	20.9
37	27	-0	-7571	0	0	0	3526	--	--	16.08	16.08	0.00	0.06	0.06	0.47	0.00	0.00	20.9
38	27	-0	-5117	0	0	0	2041	--	--	16.08	16.08	0.00	0.03	0.04	0.32	0.00	0.00	20.9
39	27	-0	-5630	0	0	0	2372	--	--	16.08	16.08	0.00	0.04	0.05	0.35	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	-4692	0	0	0	-633	--	--	16.08	16.08	0.18	0.01	0.04	0.29	0.00	0.00	20.9
2	55	-0	-3840	0	0	0	-484	--	--	16.08	16.08	0.29	0.01	0.03	0.24	0.00	0.00	20.9
3	55	-0	-3809	0	0	0	-500	--	--	16.08	16.08	0.29	0.01	0.03	0.24	0.00	0.00	20.9
4	55	-0	-3409	0	0	0	-473	--	--	16.08	16.08	0.29	0.01	0.03	0.21	0.00	0.00	20.9
5	55	-0	-3378	0	0	0	-490	--	--	16.08	16.08	0.29	0.01	0.03	0.21	0.00	0.00	20.9
6	55	-0	-3725	0	0	0	-462	--	--	16.08	16.08	0.29	0.01	0.03	0.23	0.00	0.00	20.9
7	55	-0	-3622	0	0	0	-515	--	--	16.08	16.08	0.29	0.01	0.03	0.23	0.00	0.00	20.9
8	55	-0	-3596	0	0	0	-458	--	--	16.08	16.08	0.29	0.01	0.03	0.23	0.00	0.00	20.9
9	55	-0	-3493	0	0	0	-512	--	--	16.08	16.08	0.29	0.01	0.03	0.22	0.00	0.00	20.9
10	55	-0	-3840	0	0	0	-484	--	--	16.08	16.08	0.29	0.01	0.03	0.24	0.00	0.00	20.9
11	55	-0	-3809	0	0	0	-500	--	--	16.08	16.08	0.29	0.01	0.03	0.24	0.00	0.00	20.9
12	55	-0	-3409	0	0	0	-473	--	--	16.08	16.08	0.29	0.01	0.03	0.21	0.00	0.00	20.9
13	55	-0	-3378	0	0	0	-490	--	--	16.08	16.08	0.29	0.01	0.03	0.21	0.00	0.00	20.9
14	55	-0	-3725	0	0	0	-462	--	--	16.08	16.08	0.29	0.01	0.03	0.23	0.00	0.00	20.9
15	55	-0	-3622	0	0	0	-515	--	--	16.08	16.08	0.29	0.01	0.03	0.23	0.00	0.00	20.9
16	55	-0	-3596	0	0	0	-458	--	--	16.08	16.08	0.29	0.01	0.03	0.23	0.00	0.00	20.9
17	55	-0	-3493	0	0	0	-512	--	--	16.08	16.08	0.29	0.01	0.03	0.22	0.00	0.00	20.9
18	55	-0	-7877	0	0	0	-654	--	--	16.08	16.08	0.18	0.01	0.06	0.49	0.00	0.00	20.9
19	55	-0	-6404	0	0	0	-743	--	--	16.08	16.08	0.18	0.01	0.05	0.40	0.00	0.00	20.9
20	55	-0	-6712	0	0	0	-712	--	--	16.08	16.08	0.18	0.01	0.06	0.42	0.00	0.00	20.9
37	55	-0	-7571	0	0	0	-603	--	--	16.08	16.08	0.18	0.01	0.06	0.47	0.00	0.00	20.9
38	55	-0	-5117	0	0	0	-751	--	--	16.08	16.08	0.18	0.01	0.04	0.32	0.00	0.00	20.9
39	55	-0	-5630	0	0	0	-699	--	--	16.08	16.08	0.18	0.01	0.05	0.35	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 172 NI 1763 NF 1767 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice resistenza			aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-5287	0	0	0	2917	--	--	16.08	16.08	0.00	0.05	0.04	0.33	0.00	0.00	20.9
2	0	-0	-4282	0	0	0	2393	--	--	16.08	16.08	0.10	0.04	0.04	0.27	0.00	0.00	20.9
3	0	-0	-4288	0	0	0	2381	--	--	16.08	16.08	0.10	0.04	0.04	0.27	0.00	0.00	20.9
4	0	-0	-3845	0	0	0	2108	--	--	16.08	16.08	0.10	0.04	0.03	0.24	0.00	0.00	20.9
5	0	-0	-3851	0	0	0	2096	--	--	16.08	16.08	0.10	0.04	0.03	0.24	0.00	0.00	20.9
6	0	-0	-4123	0	0	0	2307	--	--	16.08	16.08	0.10	0.04	0.03	0.26	0.00	0.00	20.9
7	0	-0	-4142	0	0	0	2267	--	--	16.08	16.08	0.10	0.04	0.03	0.26	0.00	0.00	20.9
8	0	-0	-3991	0	0	0	2221	--	--	16.08	16.08	0.10	0.04	0.03	0.25	0.00	0.00	20.9
9	0	-0	-4011	0	0	0	2181	--	--	16.08	16.08	0.10	0.04	0.03	0.25	0.00	0.00	20.9
10	0	-0	-4282	0	0	0	2393	--	--	16.08	16.08	0.10	0.04	0.04	0.27	0.00	0.00	20.9
11	0	-0	-4288	0	0	0	2381	--	--	16.08	16.08	0.10	0.04	0.04	0.27	0.00	0.00	20.9
12	0	-0	-3845	0	0	0	2108	--	--	16.08	16.08	0.10	0.04	0.03	0.24	0.00	0.00	20.9
13	0	-0	-3851	0	0	0	2096	--	--	16.08	16.08	0.10	0.04	0.03	0.24	0.00	0.00	20.9
14	0	-0	-4123	0	0	0	2307	--	--	16.08	16.08	0.10	0.04	0.03	0.26	0.00	0.00	20.9
15	0	-0	-4142	0	0	0	2267	--	--	16.08	16.08	0.10	0.04	0.03	0.26	0.00	0.00	20.9
16	0	-0	-3991	0	0	0	2221	--	--	16.08	16.08	0.10	0.04	0.03	0.25	0.00	0.00	20.9
17	0	-0	-4011	0	0	0	2181	--	--	16.08	16.08	0.10	0.04	0.03	0.25	0.00	0.00	20.9
18	0	-0	-8603	0	0	0	5121	--	--	16.08	16.08	0.00	0.09	0.07	0.54	0.00	0.00	20.9
19	0	-0	-7173	0	0	0	4062	--	--	16.08	16.08	0.00	0.07	0.06	0.45	0.00	0.00	20.9
20	0	-0	-7542	0	0	0	4348	--	--	16.08	16.08	0.00	0.07	0.06	0.47	0.00	0.00	20.9
37	0	-0	-8236	0	0	0	4930	--	--	16.08	16.08	0.00	0.08	0.07	0.52	0.00	0.00	20.9
38	0	-0	-5851	0	0	0	3166	--	--	16.08	16.08	0.00	0.05	0.05	0.37	0.00	0.00	20.9
39	0	-0	-6466	0	0	0	3643	--	--	16.08	16.08	0.00	0.06	0.05	0.41	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-5287	0	0	0	2917	--	--	16.08	16.08	0.00	0.05	0.04	0.33	0.00	0.00	20.9
2	27	-0	-4282	0	0	0	2393	--	--	16.08	16.08	0.10	0.04	0.04	0.27	0.00	0.00	20.9
3	27	-0	-4288	0	0	0	2381	--	--	16.08	16.08	0.10	0.04	0.04	0.27	0.00	0.00	20.9
4	27	-0	-3845	0	0	0	2108	--	--	16.08	16.08	0.10	0.04	0.03	0.24	0.00	0.00	20.9
5	27	-0	-3851	0	0	0	2096	--	--	16.08	16.08	0.10	0.04	0.03	0.24	0.00	0.00	20.9
6	27	-0	-4123	0	0	0	2307	--	--	16.08	16.08	0.10	0.04	0.03	0.26	0.00	0.00	20.9
7	27	-0	-4142	0	0	0	2267	--	--	16.08	16.08	0.10	0.04	0.03	0.26	0.00	0.00	20.9
8	27	-0	-3991	0	0	0	2221	--	--	16.08	16.08	0.10	0.04	0.03	0.25	0.00	0.00	20.9
9	27	-0	-4011	0	0	0	2181	--	--	16.08	16.08	0.10	0.04	0.03	0.25	0.00	0.00	20.9
10	27	-0	-4282	0	0	0	2393	--	--	16.08	16.08	0.10	0.04	0.04	0.27	0.00	0.00	20.9
11	27	-0	-4288	0	0	0	2381	--	--	16.08	16.08	0.10	0.04	0.04	0.27	0.00	0.00	20.9
12	27	-0	-3845	0	0	0	2108	--	--	16.08	16.08	0.10	0.04	0.03	0.24	0.00	0.00	20.9
13	27	-0	-3851	0	0	0	2096	--	--	16.08	16.08	0.10	0.04	0.03	0.24	0.00	0.00	20.9
14	27	-0	-4123	0	0	0	2307	--	--	16.08	16.08	0.10	0.04	0.03	0.26	0.00	0.00	20.9
15	27	-0	-4142	0	0	0	2267	--	--	16.08	16.08	0.10	0.04	0.03	0.26	0.00	0.00	20.9
16	27	-0	-3991	0	0	0	2221	--	--	16.08	16.08	0.10	0.04	0.03	0.25	0.00	0.00	20.9
17	27	-0	-4011	0	0	0	2181	--	--	16.08	16.08	0.10	0.04	0.03	0.25	0.00	0.00	20.9
18	27	-0	-8603	0	0	0	5121	--	--	16.08	16.08	0.00	0.09	0.07	0.54	0.00	0.00	20.9
19	27	-0	-7173	0	0	0	4062	--	--	16.08	16.08	0.00	0.07	0.06	0.45	0.00	0.00	20.9
20	27	-0	-7542	0	0	0	4348	--	--	16.08	16.08	0.00	0.07	0.06	0.47	0.00	0.00	20.9
37	27	-0	-8236	0	0	0	4930	--	--	16.08	16.08	0.00	0.08	0.07	0.52	0.00	0.00	20.9
38	27	-0	-5851	0	0	0	3166	--	--	16.08	16.08	0.00	0.05	0.05	0.37	0.00	0.00	20.9
39	27	-0	-6466	0	0	0	3643	--	--	16.08	16.08	0.00	0.06	0.05	0.41	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	-5287	0	0	0	34	--	--	16.08	16.08	0.00	0.00	0.04	0.33	0.00	0.00	20.9
2	55	-0	-4282	0	0	0	57	--	--	16.08	16.08	0.10	0.00	0.04	0.27	0.00	0.00	20.9
3	55	-0	-4288	0	0	0	42	--	--	16.08	16.08	0.10	0.00	0.04	0.27	0.00	0.00	20.9
4	55	-0	-3845	0	0	0	11	--	--	16.08	16.08	0.10	0.00	0.03	0.24	0.00	0.00	20.9
5	55	-0	-3851	0	0	0	-5	--	--	16.08	16.08	0.29	0.00	0.03	0.24	0.00	0.00	20.9
6	55	-0	-4123	0	0	0	59	--	--	16.08	16.08	0.10	0.00	0.03	0.26	0.00	0.00	20.9
7	55	-0	-4142	0	0	0	8	--	--	16.08	16.08	0.10	0.00	0.03	0.26	0.00	0.00	20.9
8	55	-0	-3991	0	0	0	45	--	--	16.08	16.08	0.10	0.00	0.03	0.25	0.00	0.00	20.9
9	55	-0	-4011	0	0	0	-6	--	--	16.08	16.08	0.29	0.00	0.03	0.25	0.00	0.00	20.9
10	55	-0	-4282	0	0	0	57	--	--	16.08	16.08	0.10	0.00	0.04	0.27	0.00	0.00	20.9
11	55	-0	-4288	0	0	0	42	--	--	16.08	16.08	0.10	0.00	0.04	0.27	0.00	0.00	20.9
12	55	-0	-3845	0	0	0	11	--	--	16.08	16.08	0.10	0.00	0.03	0.24	0.00	0.00	20.9
13	55	-0	-3851	0	0	0	-5	--	--	16.08	16.08	0.29	0.00	0.03	0.24	0.00	0.00	20.9
14	55	-0	-4123	0	0	0	59	--	--	16.08	16.08	0.10	0.00	0.03	0.26	0.00	0.00	20.9
15	55	-0	-4142	0	0	0	8	--	--	16.08	16.08	0.10	0.00	0.03	0.26	0.00	0.00	20.9
16	55	-0	-3991	0	0	0	45	--	--	16.08	16.08	0.10	0.00	0.03	0.25	0.00	0.00	20.9
17	55	-0	-4011	0	0	0	-6	--	--	16.08	16.08	0.29	0.00	0.03	0.25	0.00	0.00	20.9
18	55	-0	-8603	0	0	0	428	--	--	16.08	16.08	0.00	0.01	0.07	0.54	0.00	0.00	20.9
19	55	-0	-7173	0	0	0	150	--	--	16.08	16.08	0.00	0.00	0.06	0.45	0.00	0.00	20.9
20	55	-0	-7542	0	0	0	235	--	--	16.08	16.08	0.00	0.00	0.06	0.47	0.00	0.00	20.9
37	55	-0	-8236	0	0	0	438	--	--	16.08	16.08	0.00	0.01	0.07	0.52	0.00	0.00	20.9
38	55	-0	-5851	0	0	0	-26	--	--	16.08	16.08	0.18	0.00	0.05	0.37	0.00	0.00	20.9
39	55	-0	-6466	0	0	0	116	--	--	16.08	16.08	0.00	0.00	0.05	0.41	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 173 NI 1668 NF 1763 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice resistenza			aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-2055	0	0	0	2298	--	--	16.08	16.08	0.00	0.04	0.02	0.13	0.00	0.00	20.9
2	0	-0	-1486	0	0	0	1803	--	--	16.08	16.08	0.10	0.03	0.01	0.09	0.00	0.00	20.9
3	0	-0	-1540	0	0	0	1808	--	--	16.08	16.08	0.10	0.03	0.01	0.10	0.00	0.00	20.9
4	0	-0	-1621	0	0	0	1727	--	--	16.08	16.08	0.10	0.03	0.01	0.10	0.00	0.00	20.9
5	0	-0	-1676	0	0	0	1731	--	--	16.08	16.08	0.10	0.03	0.01	0.11	0.00	0.00	20.9
6	0	-0	-1470	0	0	0	1772	--	--	16.08	16.08	0.10	0.03	0.01	0.09	0.00	0.00	20.9
7	0	-0	-1652	0	0	0	1786	--	--	16.08	16.08	0.10	0.03	0.01	0.10	0.00	0.00	20.9
8	0	-0	-1510	0	0	0	1749	--	--	16.08	16.08	0.10	0.03	0.01	0.09	0.00	0.00	20.9
9	0	-0	-1692	0	0	0	1763	--	--	16.08	16.08	0.10	0.03	0.01	0.11	0.00	0.00	20.9
10	0	-0	-1486	0	0	0	1803	--	--	16.08	16.08	0.10	0.03	0.01	0.09	0.00	0.00	20.9
11	0	-0	-1540	0	0	0	1808	--	--	16.08	16.08	0.10	0.03	0.01	0.10	0.00	0.00	20.9
12	0	-0	-1621	0	0	0	1727	--	--	16.08	16.08	0.10	0.03	0.01	0.10	0.00	0.00	20.9
13	0	-0	-1676	0	0	0	1731	--	--	16.08	16.08	0.10	0.03	0.01	0.11	0.00	0.00	20.9
14	0	-0	-1470	0	0	0	1772	--	--	16.08	16.08	0.10	0.03	0.01	0.09	0.00	0.00	20.9
15	0	-0	-1652	0	0	0	1786	--	--	16.08	16.08	0.10	0.03	0.01	0.10	0.00	0.00	20.9
16	0	-0	-1510	0	0	0	1749	--	--	16.08	16.08	0.10	0.03	0.01	0.09	0.00	0.00	20.9

17	0	-0	-1692	0	0	0	1763	--	--	16.08	16.08	0.10	0.03	0.01	0.11	0.00	0.00	20.9
18	0	-0	-1725	0	0	0	3283	--	--	16.08	16.08	0.00	0.06	0.01	0.11	0.00	0.00	20.9
19	0	-0	-2557	0	0	0	3112	--	--	16.08	16.08	0.00	0.05	0.02	0.16	0.00	0.00	20.9
20	0	-0	-2298	0	0	0	3114	--	--	16.08	16.08	0.00	0.05	0.02	0.14	0.00	0.00	20.9
37	0	-0	-1424	0	0	0	3050	--	--	16.08	16.08	0.00	0.05	0.01	0.09	0.00	0.00	20.9
38	0	-0	-2810	0	0	0	2764	--	--	16.08	16.08	0.00	0.05	0.02	0.18	0.00	0.00	20.9
39	0	-0	-2377	0	0	0	2768	--	--	16.08	16.08	0.00	0.05	0.02	0.15	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-2055	0	0	0	2298	--	--	16.08	16.08	0.00	0.04	0.02	0.13	0.00	0.00	20.9
2	27	-0	-1486	0	0	0	1803	--	--	16.08	16.08	0.10	0.03	0.01	0.09	0.00	0.00	20.9
3	27	-0	-1540	0	0	0	1808	--	--	16.08	16.08	0.10	0.03	0.01	0.10	0.00	0.00	20.9
4	27	-0	-1621	0	0	0	1727	--	--	16.08	16.08	0.10	0.03	0.01	0.10	0.00	0.00	20.9
5	27	-0	-1676	0	0	0	1731	--	--	16.08	16.08	0.10	0.03	0.01	0.11	0.00	0.00	20.9
6	27	-0	-1470	0	0	0	1772	--	--	16.08	16.08	0.10	0.03	0.01	0.09	0.00	0.00	20.9
7	27	-0	-1652	0	0	0	1786	--	--	16.08	16.08	0.10	0.03	0.01	0.10	0.00	0.00	20.9
8	27	-0	-1510	0	0	0	1749	--	--	16.08	16.08	0.10	0.03	0.01	0.09	0.00	0.00	20.9
9	27	-0	-1692	0	0	0	1763	--	--	16.08	16.08	0.10	0.03	0.01	0.11	0.00	0.00	20.9
10	27	-0	-1486	0	0	0	1803	--	--	16.08	16.08	0.10	0.03	0.01	0.09	0.00	0.00	20.9
11	27	-0	-1540	0	0	0	1808	--	--	16.08	16.08	0.10	0.03	0.01	0.10	0.00	0.00	20.9
12	27	-0	-1621	0	0	0	1727	--	--	16.08	16.08	0.10	0.03	0.01	0.10	0.00	0.00	20.9
13	27	-0	-1676	0	0	0	1731	--	--	16.08	16.08	0.10	0.03	0.01	0.11	0.00	0.00	20.9
14	27	-0	-1470	0	0	0	1772	--	--	16.08	16.08	0.10	0.03	0.01	0.09	0.00	0.00	20.9
15	27	-0	-1652	0	0	0	1786	--	--	16.08	16.08	0.10	0.03	0.01	0.10	0.00	0.00	20.9
16	27	-0	-1510	0	0	0	1749	--	--	16.08	16.08	0.10	0.03	0.01	0.09	0.00	0.00	20.9
17	27	-0	-1692	0	0	0	1763	--	--	16.08	16.08	0.10	0.03	0.01	0.11	0.00	0.00	20.9
18	27	-0	-1725	0	0	0	3283	--	--	16.08	16.08	0.00	0.06	0.01	0.11	0.00	0.00	20.9
19	27	-0	-2557	0	0	0	3112	--	--	16.08	16.08	0.00	0.05	0.02	0.16	0.00	0.00	20.9
20	27	-0	-2298	0	0	0	3114	--	--	16.08	16.08	0.00	0.05	0.02	0.14	0.00	0.00	20.9
37	27	-0	-1424	0	0	0	3050	--	--	16.08	16.08	0.00	0.05	0.01	0.09	0.00	0.00	20.9
38	27	-0	-2810	0	0	0	2764	--	--	16.08	16.08	0.00	0.05	0.02	0.18	0.00	0.00	20.9
39	27	-0	-2377	0	0	0	2768	--	--	16.08	16.08	0.00	0.05	0.02	0.15	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	-2055	0	0	0	1177	--	--	16.08	16.08	0.00	0.02	0.02	0.13	0.00	0.00	20.9
2	55	-0	-1486	0	0	0	993	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
3	55	-0	-1540	0	0	0	967	--	--	16.08	16.08	0.10	0.02	0.01	0.10	0.00	0.00	20.9
4	55	-0	-1621	0	0	0	843	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
5	55	-0	-1676	0	0	0	817	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
6	55	-0	-1470	0	0	0	970	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
7	55	-0	-1652	0	0	0	885	--	--	16.08	16.08	0.10	0.02	0.01	0.10	0.00	0.00	20.9
8	55	-0	-1510	0	0	0	925	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
9	55	-0	-1692	0	0	0	840	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
10	55	-0	-1486	0	0	0	993	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
11	55	-0	-1540	0	0	0	967	--	--	16.08	16.08	0.10	0.02	0.01	0.10	0.00	0.00	20.9
12	55	-0	-1621	0	0	0	843	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
13	55	-0	-1676	0	0	0	817	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
14	55	-0	-1470	0	0	0	970	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
15	55	-0	-1652	0	0	0	885	--	--	16.08	16.08	0.10	0.02	0.01	0.10	0.00	0.00	20.9
16	55	-0	-1510	0	0	0	925	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
17	55	-0	-1692	0	0	0	840	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
18	55	-0	-1725	0	0	0	2342	--	--	16.08	16.08	0.00	0.04	0.01	0.11	0.00	0.00	20.9
19	55	-0	-2557	0	0	0	1717	--	--	16.08	16.08	0.00	0.03	0.02	0.16	0.00	0.00	20.9
20	55	-0	-2298	0	0	0	1860	--	--	16.08	16.08	0.00	0.03	0.02	0.14	0.00	0.00	20.9
37	55	-0	-1424	0	0	0	2273	--	--	16.08	16.08	0.00	0.04	0.01	0.09	0.00	0.00	20.9
38	55	-0	-2810	0	0	0	1231	--	--	16.08	16.08	0.00	0.02	0.02	0.18	0.00	0.00	20.9
39	55	-0	-2377	0	0	0	1471	--	--	16.08	16.08	0.00	0.03	0.02	0.15	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 174 NI 1657 NF 1668 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm

1	0	-0	2148	0	0	0	1203	--	--	16.08	16.08	0.00	0.02	0.02	0.13	0.00	0.00	20.9
2	0	-0	1571	0	0	0	1005	--	--	16.08	16.08	0.10	0.02	0.01	0.10	0.00	0.00	20.9
3	0	-0	1532	0	0	0	1007	--	--	16.08	16.08	0.10	0.02	0.01	0.10	0.00	0.00	20.9
4	0	-0	1772	0	0	0	843	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
5	0	-0	1733	0	0	0	845	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
6	0	-0	1687	0	0	0	946	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
7	0	-0	1556	0	0	0	953	--	--	16.08	16.08	0.10	0.02	0.01	0.10	0.00	0.00	20.9
8	0	-0	1748	0	0	0	897	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
9	0	-0	1617	0	0	0	904	--	--	16.08	16.08	0.10	0.02	0.01	0.10	0.00	0.00	20.9
10	0	-0	1571	0	0	0	1005	--	--	16.08	16.08	0.10	0.02	0.01	0.10	0.00	0.00	20.9
11	0	-0	1532	0	0	0	1007	--	--	16.08	16.08	0.10	0.02	0.01	0.10	0.00	0.00	20.9
12	0	-0	1772	0	0	0	843	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
13	0	-0	1733	0	0	0	845	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
14	0	-0	1687	0	0	0	946	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
15	0	-0	1556	0	0	0	953	--	--	16.08	16.08	0.10	0.02	0.01	0.10	0.00	0.00	20.9
16	0	-0	1748	0	0	0	897	--	--	16.08	16.08	0.10	0.02	0.01	0.11	0.00	0.00	20.9
17	0	-0	1617	0	0	0	904	--	--	16.08	16.08	0.10	0.02	0.01	0.10	0.00	0.00	20.9
18	0	-0	1948	0	0	0	2372	--	--	16.08	16.08	0.00	0.04	0.02	0.12	0.00	0.00	20.9
19	0	-0	2906	0	0	0	1710	--	--	16.08	16.08	0.00	0.03	0.02	0.18	0.00	0.00	20.9
20	0	-0	2237	0	0	0	1973	--	--	16.08	16.08	0.00	0.03	0.02	0.14	0.00	0.00	20.9
37	0	-0	1542	0	0	0	2319	--	--	16.08	16.08	0.00	0.04	0.01	0.10	0.00	0.00	20.9
38	0	-0	3139	0	0	0	1217	--	--	16.08	16.08	0.00	0.02	0.03	0.20	0.00	0.00	20.9
39	0	-0	2024	0	0	0	1655	--	--	16.08	16.08	0.00	0.03	0.02	0.13	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	2148	0	0	0	4084	--	--	16.08	16.08	0.00	0.07	0.02	0.13	0.00	0.00	20.9
2	27	-0	1571	0	0	0	3113	--	--	16.08	16.08	0.10	0.06	0.01	0.10	0.00	0.00	20.9
3	27	-0	1532	0	0	0	3062	--	--	16.08	16.08	0.10	0.05	0.01	0.10	0.00	0.00	20.9
4	27	-0	1772	0	0	0	3220	--	--	16.08	16.08	0.10	0.06	0.01	0.11	0.00	0.00	20.9
5	27	-0	1733	0	0	0	3170	--	--	16.08	16.08	0.10	0.06	0.01	0.11	0.00	0.00	20.9
6	27	-0	1687	0	0	0	3209	--	--	16.08	16.08	0.10	0.06	0.01	0.11	0.00	0.00	20.9
7	27	-0	1556	0	0	0	3040	--	--	16.08	16.08	0.10	0.05	0.01	0.10	0.00	0.00	20.9
8	27	-0	1748	0	0	0	3242	--	--	16.08	16.08	0.10	0.06	0.01	0.11	0.00	0.00	20.9
9	27	-0	1617	0	0	0	3073	--	--	16.08	16.08	0.10	0.05	0.01	0.10	0.00	0.00	20.9
10	27	-0	1571	0	0	0	3113	--	--	16.08	16.08	0.10	0.06	0.01	0.10	0.00	0.00	20.9
11	27	-0	1532	0	0	0	3062	--	--	16.08	16.08	0.10	0.05	0.01	0.10	0.00	0.00	20.9
12	27	-0	1772	0	0	0	3220	--	--	16.08	16.08	0.10	0.06	0.01	0.11	0.00	0.00	20.9

13	27	-0	1733	0	0	0	3170	--	--	16.08	16.08	0.10	0.06	0.01	0.11	0.00	0.00	20.9
14	27	-0	1687	0	0	0	3209	--	--	16.08	16.08	0.10	0.06	0.01	0.11	0.00	0.00	20.9
15	27	-0	1556	0	0	0	3040	--	--	16.08	16.08	0.10	0.05	0.01	0.10	0.00	0.00	20.9
16	27	-0	1748	0	0	0	3242	--	--	16.08	16.08	0.10	0.06	0.01	0.11	0.00	0.00	20.9
17	27	-0	1617	0	0	0	3073	--	--	16.08	16.08	0.10	0.05	0.01	0.10	0.00	0.00	20.9
18	27	-0	1948	0	0	0	4985	--	--	16.08	16.08	0.00	0.08	0.02	0.12	0.00	0.00	20.9
19	27	-0	2906	0	0	0	5608	--	--	16.08	16.08	0.00	0.10	0.02	0.18	0.00	0.00	20.9
20	27	-0	2237	0	0	0	4974	--	--	16.08	16.08	0.00	0.08	0.02	0.14	0.00	0.00	20.9
37	27	-0	1542	0	0	0	4388	--	--	16.08	16.08	0.00	0.07	0.01	0.10	0.00	0.00	20.9
38	27	-0	3139	0	0	0	5428	--	--	16.08	16.08	0.00	0.09	0.03	0.20	0.00	0.00	20.9
39	27	-0	2024	0	0	0	4370	--	--	16.08	16.08	0.00	0.07	0.02	0.13	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	2148	0	0	0	2374	--	--	16.08	16.08	0.00	0.04	0.02	0.13	0.00	0.00	20.9
2	55	-0	1571	0	0	0	1862	--	--	16.08	16.08	0.10	0.03	0.01	0.10	0.00	0.00	20.9
3	55	-0	1532	0	0	0	1843	--	--	16.08	16.08	0.10	0.03	0.01	0.10	0.00	0.00	20.9
4	55	-0	1772	0	0	0	1810	--	--	16.08	16.08	0.10	0.03	0.01	0.11	0.00	0.00	20.9
5	55	-0	1733	0	0	0	1791	--	--	16.08	16.08	0.10	0.03	0.01	0.11	0.00	0.00	20.9
6	55	-0	1687	0	0	0	1866	--	--	16.08	16.08	0.10	0.03	0.01	0.11	0.00	0.00	20.9
7	55	-0	1556	0	0	0	1802	--	--	16.08	16.08	0.10	0.03	0.01	0.10	0.00	0.00	20.9
8	55	-0	1748	0	0	0	1851	--	--	16.08	16.08	0.10	0.03	0.01	0.11	0.00	0.00	20.9
9	55	-0	1617	0	0	0	1786	--	--	16.08	16.08	0.10	0.03	0.01	0.10	0.00	0.00	20.9
10	55	-0	1571	0	0	0	1862	--	--	16.08	16.08	0.10	0.03	0.01	0.10	0.00	0.00	20.9
11	55	-0	1532	0	0	0	1843	--	--	16.08	16.08	0.10	0.03	0.01	0.10	0.00	0.00	20.9
12	55	-0	1772	0	0	0	1810	--	--	16.08	16.08	0.10	0.03	0.01	0.11	0.00	0.00	20.9
13	55	-0	1733	0	0	0	1791	--	--	16.08	16.08	0.10	0.03	0.01	0.11	0.00	0.00	20.9
14	55	-0	1687	0	0	0	1866	--	--	16.08	16.08	0.10	0.03	0.01	0.11	0.00	0.00	20.9
15	55	-0	1556	0	0	0	1802	--	--	16.08	16.08	0.10	0.03	0.01	0.10	0.00	0.00	20.9
16	55	-0	1748	0	0	0	1851	--	--	16.08	16.08	0.10	0.03	0.01	0.11	0.00	0.00	20.9
17	55	-0	1617	0	0	0	1786	--	--	16.08	16.08	0.10	0.03	0.01	0.10	0.00	0.00	20.9
18	55	-0	1948	0	0	0	3434	--	--	16.08	16.08	0.00	0.06	0.02	0.12	0.00	0.00	20.9
19	55	-0	2906	0	0	0	3295	--	--	16.08	16.08	0.00	0.06	0.02	0.18	0.00	0.00	20.9
20	55	-0	2237	0	0	0	3194	--	--	16.08	16.08	0.00	0.05	0.02	0.14	0.00	0.00	20.9
37	55	-0	1542	0	0	0	3160	--	--	16.08	16.08	0.00	0.05	0.01	0.10	0.00	0.00	20.9
38	55	-0	3139	0	0	0	2929	--	--	16.08	16.08	0.00	0.05	0.03	0.20	0.00	0.00	20.9
39	55	-0	2024	0	0	0	2759	--	--	16.08	16.08	0.00	0.05	0.02	0.13	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 175 NI 1615 NF 1657 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm

1	0	-0	5242	0	0	0	92	--	--	16.08	16.08	0.00	0.00	0.04	0.33	0.00	0.00	20.9
2	0	-0	4244	0	0	0	106	--	--	16.08	16.08	0.10	0.00	0.03	0.27	0.00	0.00	20.9
3	0	-0	4209	0	0	0	105	--	--	16.08	16.08	0.10	0.00	0.03	0.26	0.00	0.00	20.9
4	0	-0	3856	0	0	0	37	--	--	16.08	16.08	0.10	0.00	0.03	0.24	0.00	0.00	20.9
5	0	-0	3821	0	0	0	36	--	--	16.08	16.08	0.10	0.00	0.03	0.24	0.00	0.00	20.9
6	0	-0	4149	0	0	0	83	--	--	16.08	16.08	0.10	0.00	0.03	0.26	0.00	0.00	20.9
7	0	-0	4032	0	0	0	79	--	--	16.08	16.08	0.10	0.00	0.03	0.25	0.00	0.00	20.9
8	0	-0	4032	0	0	0	63	--	--	16.08	16.08	0.10	0.00	0.03	0.25	0.00	0.00	20.9
9	0	-0	3916	0	0	0	59	--	--	16.08	16.08	0.10	0.00	0.03	0.25	0.00	0.00	20.9
10	0	-0	4244	0	0	0	106	--	--	16.08	16.08	0.10	0.00	0.03	0.27	0.00	0.00	20.9
11	0	-0	4209	0	0	0	105	--	--	16.08	16.08	0.10	0.00	0.03	0.26	0.00	0.00	20.9
12	0	-0	3856	0	0	0	37	--	--	16.08	16.08	0.10	0.00	0.03	0.24	0.00	0.00	20.9
13	0	-0	3821	0	0	0	36	--	--	16.08	16.08	0.10	0.00	0.03	0.24	0.00	0.00	20.9
14	0	-0	4149	0	0	0	83	--	--	16.08	16.08	0.10	0.00	0.03	0.26	0.00	0.00	20.9
15	0	-0	4032	0	0	0	79	--	--	16.08	16.08	0.10	0.00	0.03	0.25	0.00	0.00	20.9
16	0	-0	4032	0	0	0	63	--	--	16.08	16.08	0.10	0.00	0.03	0.25	0.00	0.00	20.9
17	0	-0	3916	0	0	0	59	--	--	16.08	16.08	0.10	0.00	0.03	0.25	0.00	0.00	20.9
18	0	-0	8551	0	0	0	522	--	--	16.08	16.08	0.00	0.01	0.07	0.54	0.00	0.00	20.9
19	0	-0	7252	0	0	0	172	--	--	16.08	16.08	0.00	0.00	0.06	0.45	0.00	0.00	20.9
20	0	-0	7388	0	0	0	359	--	--	16.08	16.08	0.00	0.01	0.06	0.46	0.00	0.00	20.9
37	0	-0	8122	0	0	0	555	--	--	16.08	16.08	0.00	0.01	0.07	0.51	0.00	0.00	20.9
38	0	-0	5957	0	0	0	-28	--	--	16.08	16.08	0.18	0.00	0.05	0.37	0.00	0.00	20.9
39	0	-0	6183	0	0	0	284	--	--	16.08	16.08	0.00	0.00	0.05	0.39	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	5242	0	0	0	7124	--	--	16.08	16.08	0.00	0.12	0.04	0.33	0.00	0.00	20.9
2	27	-0	4244	0	0	0	5799	--	--	16.08	16.08	0.10	0.10	0.03	0.27	0.00	0.00	20.9
3	27	-0	4209	0	0	0	5751	--	--	16.08	16.08	0.10	0.10	0.03	0.26	0.00	0.00	20.9
4	27	-0	3856	0	0	0	5210	--	--	16.08	16.08	0.10	0.09	0.03	0.24	0.00	0.00	20.9
5	27	-0	3821	0	0	0	5162	--	--	16.08	16.08	0.10	0.09	0.03	0.24	0.00	0.00	20.9
6	27	-0	4149	0	0	0	5649	--	--	16.08	16.08	0.10	0.10	0.03	0.26	0.00	0.00	20.9
7	27	-0	4032	0	0	0	5488	--	--	16.08	16.08	0.10	0.10	0.03	0.25	0.00	0.00	20.9
8	27	-0	4032	0	0	0	5471	--	--	16.08	16.08	0.10	0.10	0.03	0.25	0.00	0.00	20.9
9	27	-0	3916	0	0	0	5312	--	--	16.08	16.08	0.10	0.09	0.03	0.25	0.00	0.00	20.9
10	27	-0	4244	0	0	0	5799	--	--	16.08	16.08	0.10	0.10	0.03	0.27	0.00	0.00	20.9
11	27	-0	4209	0	0	0	5751	--	--	16.08	16.08	0.10	0.10	0.03	0.26	0.00	0.00	20.9
12	27	-0	3856	0	0	0	5210	--	--	16.08	16.08	0.10	0.09	0.03	0.24	0.00	0.00	20.9
13	27	-0	3821	0	0	0	5162	--	--	16.08	16.08	0.10	0.09	0.03	0.24	0.00	0.00	20.9
14	27	-0	4149	0	0	0	5649	--	--	16.08	16.08	0.10	0.10	0.03	0.26	0.00	0.00	20.9
15	27	-0	4032	0	0	0	5488	--	--	16.08	16.08	0.10	0.10	0.03	0.25	0.00	0.00	20.9
16	27	-0	4032	0	0	0	5471	--	--	16.08	16.08	0.10	0.10	0.03	0.25	0.00	0.00	20.9
17	27	-0	3916	0	0	0	5312	--	--	16.08	16.08	0.10	0.09	0.03	0.25	0.00	0.00	20.9
18	27	-0	8551	0	0	0	11993	--	--	16.08	16.08	0.00	0.20	0.07	0.54	0.00	0.00	20.9
19	27	-0	7252	0	0	0	9901	--	--	16.08	16.08	0.00	0.17	0.06	0.45	0.00	0.00	20.9
20	27	-0	7388	0	0	0	10270	--	--	16.08	16.08	0.00	0.18	0.06	0.46	0.00	0.00	20.9
37	27	-0	8122	0	0	0	11450	--	--	16.08	16.08	0.00	0.20	0.07	0.51	0.00	0.00	20.9
38	27	-0	5957	0	0	0	7963	--	--	16.08	16.08	0.00	0.14	0.05	0.37	0.00	0.00	20.9
39	27	-0	6183	0	0	0	8578	--	--	16.08	16.08	0.00	0.15	0.05	0.39	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	5242	0	0	0	2951	--	--	16.08	16.08	0.00	0.05	0.04	0.33	0.00	0.00	20.9
2	55	-0	4244	0	0	0	2421	--	--	16.08	16.08	0.10	0.04	0.03	0.27	0.00	0.00	20.9
3	55	-0	4209	0	0	0	2400	--	--	16.08	16.08	0.10	0.04	0.03	0.26	0.00	0.00	20.9
4	55	-0	3856	0	0	0	2140	--	--	16.08	16.08	0.10	0.04	0.03	0.24	0.00	0.00	20.9
5	55	-0	3821	0	0	0	2120	--	--	16.08	16.08	0.10	0.04	0.03	0.24	0.00	0.00	20.9
6	55	-0	4149	0	0	0	2346	--	--	16.08	16.08	0.10	0.04	0.03	0.26	0.00	0.00	20.9
7	55	-0	4032	0	0	0	2279	--	--	16.08	16.08	0.10	0.04	0.03	0.25	0.00	0.00	20.9
8	55	-0	4032	0	0	0	2262	--	--	16.08	16.08	0.10	0.04	0.03	0.25	0.00	0.00	20.9

9	55	-0	3916	0	0	0	2195	--	--	16.08	16.08	0.10	0.04	0.03	0.25	0.00	0.00	20.9
10	55	-0	4244	0	0	0	2421	--	--	16.08	16.08	0.10	0.04	0.03	0.27	0.00	0.00	20.9
11	55	-0	4209	0	0	0	2400	--	--	16.08	16.08	0.10	0.04	0.03	0.26	0.00	0.00	20.9
12	55	-0	3856	0	0	0	2140	--	--	16.08	16.08	0.10	0.04	0.03	0.24	0.00	0.00	20.9
13	55	-0	3821	0	0	0	2120	--	--	16.08	16.08	0.10	0.04	0.03	0.24	0.00	0.00	20.9
14	55	-0	4149	0	0	0	2346	--	--	16.08	16.08	0.10	0.04	0.03	0.26	0.00	0.00	20.9
15	55	-0	4032	0	0	0	2279	--	--	16.08	16.08	0.10	0.04	0.03	0.25	0.00	0.00	20.9
16	55	-0	4032	0	0	0	2262	--	--	16.08	16.08	0.10	0.04	0.03	0.25	0.00	0.00	20.9
17	55	-0	3916	0	0	0	2195	--	--	16.08	16.08	0.10	0.04	0.03	0.25	0.00	0.00	20.9
18	55	-0	8551	0	0	0	5186	--	--	16.08	16.08	0.00	0.09	0.07	0.54	0.00	0.00	20.9
19	55	-0	7252	0	0	0	4128	--	--	16.08	16.08	0.00	0.07	0.06	0.45	0.00	0.00	20.9
20	55	-0	7388	0	0	0	4389	--	--	16.08	16.08	0.00	0.07	0.06	0.46	0.00	0.00	20.9
37	55	-0	8122	0	0	0	4985	--	--	16.08	16.08	0.00	0.08	0.07	0.51	0.00	0.00	20.9
38	55	-0	5957	0	0	0	3221	--	--	16.08	16.08	0.00	0.05	0.05	0.37	0.00	0.00	20.9
39	55	-0	6183	0	0	0	3656	--	--	16.08	16.08	0.00	0.06	0.05	0.39	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 176 NI 1616 NF 1615 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	4503	0	0	0	-564	--	--	16.08	16.08	0.18	0.01	0.04	0.28	0.00	0.00	20.9
2	0	-0	3658	0	0	0	-425	--	--	16.08	16.08	0.29	0.01	0.03	0.23	0.00	0.00	20.9
3	0	-0	3657	0	0	0	-421	--	--	16.08	16.08	0.29	0.01	0.03	0.23	0.00	0.00	20.9
4	0	-0	3272	0	0	0	-446	--	--	16.08	16.08	0.29	0.01	0.03	0.21	0.00	0.00	20.9
5	0	-0	3271	0	0	0	-442	--	--	16.08	16.08	0.29	0.01	0.03	0.21	0.00	0.00	20.9
6	0	-0	3524	0	0	0	-437	--	--	16.08	16.08	0.29	0.01	0.03	0.22	0.00	0.00	20.9
7	0	-0	3520	0	0	0	-423	--	--	16.08	16.08	0.29	0.01	0.03	0.22	0.00	0.00	20.9
8	0	-0	3408	0	0	0	-444	--	--	16.08	16.08	0.29	0.01	0.03	0.21	0.00	0.00	20.9
9	0	-0	3404	0	0	0	-430	--	--	16.08	16.08	0.29	0.01	0.03	0.21	0.00	0.00	20.9
10	0	-0	3658	0	0	0	-425	--	--	16.08	16.08	0.29	0.01	0.03	0.23	0.00	0.00	20.9
11	0	-0	3657	0	0	0	-421	--	--	16.08	16.08	0.29	0.01	0.03	0.23	0.00	0.00	20.9
12	0	-0	3272	0	0	0	-446	--	--	16.08	16.08	0.29	0.01	0.03	0.21	0.00	0.00	20.9
13	0	-0	3271	0	0	0	-442	--	--	16.08	16.08	0.29	0.01	0.03	0.21	0.00	0.00	20.9
14	0	-0	3524	0	0	0	-437	--	--	16.08	16.08	0.29	0.01	0.03	0.22	0.00	0.00	20.9
15	0	-0	3520	0	0	0	-423	--	--	16.08	16.08	0.29	0.01	0.03	0.22	0.00	0.00	20.9
16	0	-0	3408	0	0	0	-444	--	--	16.08	16.08	0.29	0.01	0.03	0.21	0.00	0.00	20.9
17	0	-0	3404	0	0	0	-430	--	--	16.08	16.08	0.29	0.01	0.03	0.21	0.00	0.00	20.9
18	0	-0	7530	0	0	0	-546	--	--	16.08	16.08	0.18	0.01	0.06	0.47	0.00	0.00	20.9
19	0	-0	6224	0	0	0	-731	--	--	16.08	16.08	0.18	0.01	0.05	0.39	0.00	0.00	20.9
20	0	-0	6507	0	0	0	-558	--	--	16.08	16.08	0.18	0.01	0.05	0.41	0.00	0.00	20.9
37	0	-0	7196	0	0	0	-461	--	--	16.08	16.08	0.18	0.01	0.06	0.45	0.00	0.00	20.9
38	0	-0	5019	0	0	0	-769	--	--	16.08	16.08	0.18	0.01	0.04	0.31	0.00	0.00	20.9
39	0	-0	5491	0	0	0	-482	--	--	16.08	16.08	0.18	0.01	0.05	0.34	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	4503	0	0	0	5477	--	--	16.08	16.08	0.00	0.09	0.04	0.28	0.00	0.00	20.9
2	27	-0	3658	0	0	0	4482	--	--	16.08	16.08	0.10	0.08	0.03	0.23	0.00	0.00	20.9
3	27	-0	3657	0	0	0	4485	--	--	16.08	16.08	0.10	0.08	0.03	0.23	0.00	0.00	20.9
4	27	-0	3272	0	0	0	3943	--	--	16.08	16.08	0.10	0.07	0.03	0.21	0.00	0.00	20.9
5	27	-0	3271	0	0	0	3946	--	--	16.08	16.08	0.10	0.07	0.03	0.21	0.00	0.00	20.9
6	27	-0	3524	0	0	0	4290	--	--	16.08	16.08	0.10	0.08	0.03	0.22	0.00	0.00	20.9
7	27	-0	3520	0	0	0	4299	--	--	16.08	16.08	0.10	0.08	0.03	0.22	0.00	0.00	20.9
8	27	-0	3408	0	0	0	4128	--	--	16.08	16.08	0.10	0.07	0.03	0.21	0.00	0.00	20.9
9	27	-0	3404	0	0	0	4137	--	--	16.08	16.08	0.10	0.07	0.03	0.21	0.00	0.00	20.9
10	27	-0	3658	0	0	0	4482	--	--	16.08	16.08	0.10	0.08	0.03	0.23	0.00	0.00	20.9
11	27	-0	3657	0	0	0	4485	--	--	16.08	16.08	0.10	0.08	0.03	0.23	0.00	0.00	20.9
12	27	-0	3272	0	0	0	3943	--	--	16.08	16.08	0.10	0.07	0.03	0.21	0.00	0.00	20.9
13	27	-0	3271	0	0	0	3946	--	--	16.08	16.08	0.10	0.07	0.03	0.21	0.00	0.00	20.9
14	27	-0	3524	0	0	0	4290	--	--	16.08	16.08	0.10	0.08	0.03	0.22	0.00	0.00	20.9
15	27	-0	3520	0	0	0	4299	--	--	16.08	16.08	0.10	0.08	0.03	0.22	0.00	0.00	20.9
16	27	-0	3408	0	0	0	4128	--	--	16.08	16.08	0.10	0.07	0.03	0.21	0.00	0.00	20.9
17	27	-0	3404	0	0	0	4137	--	--	16.08	16.08	0.10	0.07	0.03	0.21	0.00	0.00	20.9
18	27	-0	7530	0	0	0	9556	--	--	16.08	16.08	0.00	0.16	0.06	0.47	0.00	0.00	20.9
19	27	-0	6224	0	0	0	7618	--	--	16.08	16.08	0.00	0.13	0.05	0.39	0.00	0.00	20.9
20	27	-0	6507	0	0	0	8171	--	--	16.08	16.08	0.00	0.14	0.05	0.41	0.00	0.00	20.9
37	27	-0	7196	0	0	0	9192	--	--	16.08	16.08	0.00	0.16	0.06	0.45	0.00	0.00	20.9
38	27	-0	5019	0	0	0	5964	--	--	16.08	16.08	0.00	0.10	0.04	0.31	0.00	0.00	20.9
39	27	-0	5491	0	0	0	6884	--	--	16.08	16.08	0.00	0.12	0.05	0.34	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	4503	0	0	0	1893	--	--	16.08	16.08	0.00	0.03	0.04	0.28	0.00	0.00	20.9
2	55	-0	3658	0	0	0	1570	--	--	16.08	16.08	0.10	0.03	0.03	0.23	0.00	0.00	20.9
3	55	-0	3657	0	0	0	1574	--	--	16.08	16.08	0.10	0.03	0.03	0.23	0.00	0.00	20.9
4	55	-0	3272	0	0	0	1339	--	--	16.08	16.08	0.10	0.02	0.03	0.21	0.00	0.00	20.9
5	55	-0	3271	0	0	0	1342	--	--	16.08	16.08	0.10	0.02	0.03	0.21	0.00	0.00	20.9
6	55	-0	3524	0	0	0	1485	--	--	16.08	16.08	0.10	0.03	0.03	0.22	0.00	0.00	20.9
7	55	-0	3520	0	0	0	1497	--	--	16.08	16.08	0.10	0.03	0.03	0.22	0.00	0.00	20.9
8	55	-0	3408	0	0	0	1415	--	--	16.08	16.08	0.10	0.03	0.03	0.21	0.00	0.00	20.9
9	55	-0	3404	0	0	0	1428	--	--	16.08	16.08	0.10	0.03	0.03	0.21	0.00	0.00	20.9
10	55	-0	3658	0	0	0	1570	--	--	16.08	16.08	0.10	0.03	0.03	0.23	0.00	0.00	20.9
11	55	-0	3657	0	0	0	1574	--	--	16.08	16.08	0.10	0.03	0.03	0.23	0.00	0.00	20.9
12	55	-0	3272	0	0	0	1339	--	--	16.08	16.08	0.10	0.02	0.03	0.21	0.00	0.00	20.9
13	55	-0	3271	0	0	0	1342	--	--	16.08	16.08	0.10	0.02	0.03	0.21	0.00	0.00	20.9
14	55	-0	3524	0	0	0	1485	--	--	16.08	16.08	0.10	0.03	0.03	0.22	0.00	0.00	20.9
15	55	-0	3520	0	0	0	1497	--	--	16.08	16.08	0.10	0.03	0.03	0.22	0.00	0.00	20.9
16	55	-0	3408	0	0	0	1415	--	--	16.08	16.08	0.10	0.03	0.03	0.21	0.00	0.00	20.9
17	55	-0	3404	0	0	0	1428	--	--	16.08	16.08	0.10	0.03	0.03	0.21	0.00	0.00	20.9
18	55	-0	7530	0	0	0	3562	--	--	16.08	16.08	0.00	0.06	0.06	0.47	0.00	0.00	20.9
19	55	-0	6224	0	0	0	2664	--	--	16.08	16.08	0.00	0.05	0.05	0.39	0.00	0.00	20.9
20	55	-0	6507	0	0	0	2991	--	--	16.08	16.08	0.00	0.05	0.05	0.41	0.00	0.00	20.9
37	55	-0	7196	0	0	0	3464	--	--	16.08	16.08	0.00	0.06	0.06	0.45	0.00	0.00	20.9
38	55	-0	5019	0	0	0	1969	--	--	16.08	16.08	0.00	0.03	0.04	0.31	0.00	0.00	20.9
39	55	-0	5491	0	0	0	2513	--	--	16.08	16.08	0.00	0.04	0.05	0.34	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 177 NI 1574 NF 1616 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice resistenza			aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	2699	0	0	0	-983	--	--	16.08	16.08	0.18	0.02	0.02	0.17	0.00	0.00	20.9
2	0	-0	2181	0	0	0	-769	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
3	0	-0	2193	0	0	0	-765	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
4	0	-0	1959	0	0	0	-748	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
5	0	-0	1971	0	0	0	-744	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
6	0	-0	2090	0	0	0	-767	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
7	0	-0	2128	0	0	0	-752	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
8	0	-0	2024	0	0	0	-761	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
9	0	-0	2061	0	0	0	-746	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
10	0	-0	2181	0	0	0	-769	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
11	0	-0	2193	0	0	0	-765	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
12	0	-0	1959	0	0	0	-748	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
13	0	-0	1971	0	0	0	-744	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
14	0	-0	2090	0	0	0	-767	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
15	0	-0	2128	0	0	0	-752	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
16	0	-0	2024	0	0	0	-761	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
17	0	-0	2061	0	0	0	-746	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
18	0	-0	4453	0	0	0	-1276	--	--	16.08	16.08	0.18	0.02	0.04	0.28	0.00	0.00	20.9
19	0	-0	3709	0	0	0	-1311	--	--	16.08	16.08	0.18	0.02	0.03	0.23	0.00	0.00	20.9
20	0	-0	3894	0	0	0	-1176	--	--	16.08	16.08	0.18	0.02	0.03	0.24	0.00	0.00	20.9
37	0	-0	4253	0	0	0	-1165	--	--	16.08	16.08	0.18	0.02	0.04	0.27	0.00	0.00	20.9
38	0	-0	3013	0	0	0	-1223	--	--	16.08	16.08	0.18	0.02	0.02	0.19	0.00	0.00	20.9
39	0	-0	3322	0	0	0	-998	--	--	16.08	16.08	0.18	0.02	0.03	0.21	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	2699	0	0	0	-983	--	--	16.08	16.08	0.18	0.02	0.02	0.17	0.00	0.00	20.9
2	27	-0	2181	0	0	0	-769	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
3	27	-0	2193	0	0	0	-765	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
4	27	-0	1959	0	0	0	-748	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
5	27	-0	1971	0	0	0	-744	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
6	27	-0	2090	0	0	0	-767	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
7	27	-0	2128	0	0	0	-752	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
8	27	-0	2024	0	0	0	-761	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
9	27	-0	2061	0	0	0	-746	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
10	27	-0	2181	0	0	0	-769	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
11	27	-0	2193	0	0	0	-765	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
12	27	-0	1959	0	0	0	-748	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
13	27	-0	1971	0	0	0	-744	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
14	27	-0	2090	0	0	0	-767	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
15	27	-0	2128	0	0	0	-752	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
16	27	-0	2024	0	0	0	-761	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
17	27	-0	2061	0	0	0	-746	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
18	27	-0	4453	0	0	0	-1276	--	--	16.08	16.08	0.18	0.02	0.04	0.28	0.00	0.00	20.9
19	27	-0	3709	0	0	0	-1311	--	--	16.08	16.08	0.18	0.02	0.03	0.23	0.00	0.00	20.9
20	27	-0	3894	0	0	0	-1176	--	--	16.08	16.08	0.18	0.02	0.03	0.24	0.00	0.00	20.9
37	27	-0	4253	0	0	0	-1165	--	--	16.08	16.08	0.18	0.02	0.04	0.27	0.00	0.00	20.9
38	27	-0	3013	0	0	0	-1223	--	--	16.08	16.08	0.18	0.02	0.02	0.19	0.00	0.00	20.9
39	27	-0	3322	0	0	0	-998	--	--	16.08	16.08	0.18	0.02	0.03	0.21	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	2699	0	0	0	488	--	--	16.08	16.08	0.00	0.01	0.02	0.17	0.00	0.00	20.9
2	55	-0	2181	0	0	0	421	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
3	55	-0	2193	0	0	0	431	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
4	55	-0	1959	0	0	0	320	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
5	55	-0	1971	0	0	0	331	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
6	55	-0	2090	0	0	0	373	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
7	55	-0	2128	0	0	0	409	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
8	55	-0	2024	0	0	0	343	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
9	55	-0	2061	0	0	0	378	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
10	55	-0	2181	0	0	0	421	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
11	55	-0	2193	0	0	0	431	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
12	55	-0	1959	0	0	0	320	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
13	55	-0	1971	0	0	0	331	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
14	55	-0	2090	0	0	0	373	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
15	55	-0	2128	0	0	0	409	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
16	55	-0	2024	0	0	0	343	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
17	55	-0	2061	0	0	0	378	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
18	55	-0	4453	0	0	0	1152	--	--	16.08	16.08	0.00	0.02	0.04	0.28	0.00	0.00	20.9
19	55	-0	3709	0	0	0	711	--	--	16.08	16.08	0.00	0.01	0.03	0.23	0.00	0.00	20.9
20	55	-0	3894	0	0	0	948	--	--	16.08	16.08	0.00	0.02	0.03	0.24	0.00	0.00	20.9
37	55	-0	4253	0	0	0	1155	--	--	16.08	16.08	0.00	0.02	0.04	0.27	0.00	0.00	20.9
38	55	-0	3013	0	0	0	420	--	--	16.08	16.08	0.00	0.01	0.02	0.19	0.00	0.00	20.9
39	55	-0	3322	0	0	0	814	--	--	16.08	16.08	0.00	0.01	0.03	0.21	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 178 NI 1655 NF 1574 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice resistenza			aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	1229	0	0	0	-1037	--	--	16.08	16.08	0.18	0.02	0.01	0.08	0.00	0.00	20.9
2	0	-0	990	0	0	0	-813	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
3	0	-0	1004	0	0	0	-812	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
4	0	-0	886	0	0	0	-784	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
5	0	-0	901	0	0	0	-782	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
6	0	-0	936	0	0	0	-805	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
7	0	-0	985	0	0	0	-799	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
8	0	-0	906	0	0	0	-796	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
9	0	-0	954	0	0	0	-790	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
10	0	-0	990	0	0	0	-813	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
11	0	-0	1004	0	0	0	-812	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
12	0	-0	886	0	0	0	-784	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
13	0	-0	901	0	0	0	-782	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
14	0	-0	936	0	0	0	-805	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
15	0	-0	985	0	0	0	-799	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
16	0	-0	906	0	0	0	-796	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9

17	0	-0	954	0	0	0	-790	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
18	0	-0	2023	0	0	0	-1381	--	--	16.08	16.08	0.18	0.02	0.02	0.13	0.00	0.00	20.9
19	0	-0	1673	0	0	0	-1381	--	--	16.08	16.08	0.18	0.02	0.01	0.10	0.00	0.00	20.9
20	0	-0	1786	0	0	0	-1265	--	--	16.08	16.08	0.18	0.02	0.01	0.11	0.00	0.00	20.9
37	0	-0	1940	0	0	0	-1271	--	--	16.08	16.08	0.18	0.02	0.02	0.12	0.00	0.00	20.9
38	0	-0	1356	0	0	0	-1271	--	--	16.08	16.08	0.18	0.02	0.01	0.09	0.00	0.00	20.9
39	0	-0	1544	0	0	0	-1076	--	--	16.08	16.08	0.18	0.02	0.01	0.10	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	1229	0	0	0	-1037	--	--	16.08	16.08	0.18	0.02	0.01	0.08	0.00	0.00	20.9
2	27	-0	990	0	0	0	-813	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
3	27	-0	1004	0	0	0	-812	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
4	27	-0	886	0	0	0	-784	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
5	27	-0	901	0	0	0	-782	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
6	27	-0	936	0	0	0	-805	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
7	27	-0	985	0	0	0	-799	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
8	27	-0	906	0	0	0	-796	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
9	27	-0	954	0	0	0	-790	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
10	27	-0	990	0	0	0	-813	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
11	27	-0	1004	0	0	0	-812	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
12	27	-0	886	0	0	0	-784	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
13	27	-0	901	0	0	0	-782	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
14	27	-0	936	0	0	0	-805	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
15	27	-0	985	0	0	0	-799	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
16	27	-0	906	0	0	0	-796	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
17	27	-0	954	0	0	0	-790	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
18	27	-0	2023	0	0	0	-1381	--	--	16.08	16.08	0.18	0.02	0.02	0.13	0.00	0.00	20.9
19	27	-0	1673	0	0	0	-1381	--	--	16.08	16.08	0.18	0.02	0.01	0.10	0.00	0.00	20.9
20	27	-0	1786	0	0	0	-1265	--	--	16.08	16.08	0.18	0.02	0.01	0.11	0.00	0.00	20.9
37	27	-0	1940	0	0	0	-1271	--	--	16.08	16.08	0.18	0.02	0.02	0.12	0.00	0.00	20.9
38	27	-0	1356	0	0	0	-1271	--	--	16.08	16.08	0.18	0.02	0.01	0.09	0.00	0.00	20.9
39	27	-0	1544	0	0	0	-1076	--	--	16.08	16.08	0.18	0.02	0.01	0.10	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	1229	0	0	0	-1037	--	--	16.08	16.08	0.18	0.02	0.01	0.08	0.00	0.00	20.9
2	55	-0	990	0	0	0	-813	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
3	55	-0	1004	0	0	0	-812	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
4	55	-0	886	0	0	0	-784	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
5	55	-0	901	0	0	0	-782	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
6	55	-0	936	0	0	0	-805	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
7	55	-0	985	0	0	0	-799	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
8	55	-0	906	0	0	0	-796	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
9	55	-0	954	0	0	0	-790	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
10	55	-0	990	0	0	0	-813	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
11	55	-0	1004	0	0	0	-812	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
12	55	-0	886	0	0	0	-784	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
13	55	-0	901	0	0	0	-782	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
14	55	-0	936	0	0	0	-805	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
15	55	-0	985	0	0	0	-799	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
16	55	-0	906	0	0	0	-796	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
17	55	-0	954	0	0	0	-790	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
18	55	-0	2023	0	0	0	-1381	--	--	16.08	16.08	0.18	0.02	0.02	0.13	0.00	0.00	20.9
19	55	-0	1673	0	0	0	-1381	--	--	16.08	16.08	0.18	0.02	0.01	0.10	0.00	0.00	20.9
20	55	-0	1786	0	0	0	-1265	--	--	16.08	16.08	0.18	0.02	0.01	0.11	0.00	0.00	20.9
37	55	-0	1940	0	0	0	-1271	--	--	16.08	16.08	0.18	0.02	0.02	0.12	0.00	0.00	20.9
38	55	-0	1356	0	0	0	-1271	--	--	16.08	16.08	0.18	0.02	0.01	0.09	0.00	0.00	20.9
39	55	-0	1544	0	0	0	-1076	--	--	16.08	16.08	0.18	0.02	0.01	0.10	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 179 NI 1656 NF 1655 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-91	0	0	0	-853	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9
2	0	-0	-77	0	0	0	-666	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
3	0	-0	-60	0	0	0	-659	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
4	0	-0	-81	0	0	0	-653	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
5	0	-0	-64	0	0	0	-646	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
6	0	-0	-98	0	0	0	-670	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
7	0	-0	-42	0	0	0	-646	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
8	0	-0	-99	0	0	0	-666	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
9	0	-0	-43	0	0	0	-642	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
10	0	-0	-77	0	0	0	-666	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
11	0	-0	-60	0	0	0	-659	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
12	0	-0	-81	0	0	0	-653	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
13	0	-0	-64	0	0	0	-646	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
14	0	-0	-98	0	0	0	-670	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
15	0	-0	-42	0	0	0	-646	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
16	0	-0	-99	0	0	0	-666	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
17	0	-0	-43	0	0	0	-642	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
18	0	-0	-122	0	0	0	-1077	--	--	16.08	16.08	0.18	0.02	0.00	0.01	0.00	0.00	20.9
19	0	-0	-153	0	0	0	-1137	--	--	16.08	16.08	0.18	0.02	0.00	0.01	0.00	0.00	20.9
20	0	-0	-91	0	0	0	-991	--	--	16.08	16.08	0.18	0.02	0.00	0.01	0.00	0.00	20.9
37	0	-0	-96	0	0	0	-975	--	--	16.08	16.08	0.18	0.02	0.00	0.01	0.00	0.00	20.9
38	0	-0	-148	0	0	0	-1075	--	--	16.08	16.08	0.18	0.02	0.00	0.01	0.00	0.00	20.9
39	0	-0	-44	0	0	0	-832	--	--	16.08	16.08	0.18	0.01	0.00	0.00	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-91	0	0	0	-853	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9
2	27	-0	-77	0	0	0	-666	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
3	27	-0	-60	0	0	0	-659	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
4	27	-0	-81	0	0	0	-653	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
5	27	-0	-64	0	0	0	-646	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
6	27	-0	-98	0	0	0	-670	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
7	27	-0	-42	0	0	0	-646	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
8	27	-0	-99	0	0	0	-666	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
9	27	-0	-43	0	0	0	-642	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
10	27	-0	-77	0	0	0	-666	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
11	27	-0	-60	0	0	0	-659	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
12	27	-0	-81	0	0	0	-653	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9

13	27	-0	-64	0	0	0	-646	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
14	27	-0	-98	0	0	0	-670	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
15	27	-0	-42	0	0	0	-646	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
16	27	-0	-99	0	0	0	-666	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
17	27	-0	-43	0	0	0	-642	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
18	27	-0	-122	0	0	0	-1077	--	--	16.08	16.08	0.18	0.02	0.00	0.01	0.00	0.00	20.9
19	27	-0	-153	0	0	0	-1137	--	--	16.08	16.08	0.18	0.02	0.00	0.01	0.00	0.00	20.9
20	27	-0	-91	0	0	0	-991	--	--	16.08	16.08	0.18	0.02	0.00	0.01	0.00	0.00	20.9
37	27	-0	-96	0	0	0	-975	--	--	16.08	16.08	0.18	0.02	0.00	0.01	0.00	0.00	20.9
38	27	-0	-148	0	0	0	-1075	--	--	16.08	16.08	0.18	0.02	0.00	0.01	0.00	0.00	20.9
39	27	-0	-44	0	0	0	-832	--	--	16.08	16.08	0.18	0.01	0.00	0.00	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	-91	0	0	0	-853	--	--	16.08	16.08	0.18	0.01	0.00	0.01	0.00	0.00	20.9
2	55	-0	-77	0	0	0	-666	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
3	55	-0	-60	0	0	0	-659	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
4	55	-0	-81	0	0	0	-653	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
5	55	-0	-64	0	0	0	-646	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
6	55	-0	-98	0	0	0	-670	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
7	55	-0	-42	0	0	0	-646	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
8	55	-0	-99	0	0	0	-666	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
9	55	-0	-43	0	0	0	-642	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
10	55	-0	-77	0	0	0	-666	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
11	55	-0	-60	0	0	0	-659	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
12	55	-0	-81	0	0	0	-653	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
13	55	-0	-64	0	0	0	-646	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
14	55	-0	-98	0	0	0	-670	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
15	55	-0	-42	0	0	0	-646	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
16	55	-0	-99	0	0	0	-666	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
17	55	-0	-43	0	0	0	-642	--	--	16.08	16.08	0.29	0.01	0.00	0.00	0.00	0.00	20.9
18	55	-0	-122	0	0	0	-1077	--	--	16.08	16.08	0.18	0.02	0.00	0.01	0.00	0.00	20.9
19	55	-0	-153	0	0	0	-1137	--	--	16.08	16.08	0.18	0.02	0.00	0.01	0.00	0.00	20.9
20	55	-0	-91	0	0	0	-991	--	--	16.08	16.08	0.18	0.02	0.00	0.01	0.00	0.00	20.9
37	55	-0	-96	0	0	0	-975	--	--	16.08	16.08	0.18	0.02	0.00	0.01	0.00	0.00	20.9
38	55	-0	-148	0	0	0	-1075	--	--	16.08	16.08	0.18	0.02	0.00	0.01	0.00	0.00	20.9
39	55	-0	-44	0	0	0	-832	--	--	16.08	16.08	0.18	0.01	0.00	0.00	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 180 NI 1597 NF 1656 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-1406	0	0	0	-1050	--	--	16.08	16.08	0.18	0.02	0.01	0.09	0.00	0.00	20.9
2	0	-0	-1138	0	0	0	-824	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
3	0	-0	-1119	0	0	0	-819	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
4	0	-0	-1044	0	0	0	-796	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
5	0	-0	-1025	0	0	0	-791	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
6	0	-0	-1128	0	0	0	-819	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
7	0	-0	-1063	0	0	0	-804	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
8	0	-0	-1099	0	0	0	-811	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
9	0	-0	-1035	0	0	0	-796	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
10	0	-0	-1138	0	0	0	-824	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
11	0	-0	-1119	0	0	0	-819	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
12	0	-0	-1044	0	0	0	-796	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
13	0	-0	-1025	0	0	0	-791	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
14	0	-0	-1128	0	0	0	-819	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
15	0	-0	-1063	0	0	0	-804	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
16	0	-0	-1099	0	0	0	-811	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
17	0	-0	-1035	0	0	0	-796	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
18	0	-0	-2252	0	0	0	-1396	--	--	16.08	16.08	0.18	0.02	0.02	0.14	0.00	0.00	20.9
19	0	-0	-1971	0	0	0	-1404	--	--	16.08	16.08	0.18	0.02	0.02	0.12	0.00	0.00	20.9
20	0	-0	-1955	0	0	0	-1275	--	--	16.08	16.08	0.18	0.02	0.02	0.12	0.00	0.00	20.9
37	0	-0	-2117	0	0	0	-1280	--	--	16.08	16.08	0.18	0.02	0.02	0.13	0.00	0.00	20.9
38	0	-0	-1648	0	0	0	-1294	--	--	16.08	16.08	0.18	0.02	0.01	0.10	0.00	0.00	20.9
39	0	-0	-1622	0	0	0	-1080	--	--	16.08	16.08	0.18	0.02	0.01	0.10	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-1406	0	0	0	-1050	--	--	16.08	16.08	0.18	0.02	0.01	0.09	0.00	0.00	20.9
2	27	-0	-1138	0	0	0	-824	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
3	27	-0	-1119	0	0	0	-819	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
4	27	-0	-1044	0	0	0	-796	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
5	27	-0	-1025	0	0	0	-791	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
6	27	-0	-1128	0	0	0	-819	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
7	27	-0	-1063	0	0	0	-804	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
8	27	-0	-1099	0	0	0	-811	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
9	27	-0	-1035	0	0	0	-796	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
10	27	-0	-1138	0	0	0	-824	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
11	27	-0	-1119	0	0	0	-819	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
12	27	-0	-1044	0	0	0	-796	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
13	27	-0	-1025	0	0	0	-791	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
14	27	-0	-1128	0	0	0	-819	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
15	27	-0	-1063	0	0	0	-804	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
16	27	-0	-1099	0	0	0	-811	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
17	27	-0	-1035	0	0	0	-796	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
18	27	-0	-2252	0	0	0	-1396	--	--	16.08	16.08	0.18	0.02	0.02	0.14	0.00	0.00	20.9
19	27	-0	-1971	0	0	0	-1404	--	--	16.08	16.08	0.18	0.02	0.02	0.12	0.00	0.00	20.9
20	27	-0	-1955	0	0	0	-1275	--	--	16.08	16.08	0.18	0.02	0.02	0.12	0.00	0.00	20.9
37	27	-0	-2117	0	0	0	-1280	--	--	16.08	16.08	0.18	0.02	0.02	0.13	0.00	0.00	20.9
38	27	-0	-1648	0	0	0	-1294	--	--	16.08	16.08	0.18	0.02	0.01	0.10	0.00	0.00	20.9
39	27	-0	-1622	0	0	0	-1080	--	--	16.08	16.08	0.18	0.02	0.01	0.10	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	-1406	0	0	0	-1050	--	--	16.08	16.08	0.18	0.02	0.01	0.09	0.00	0.00	20.9
2	55	-0	-1138	0	0	0	-824	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
3	55	-0	-1119	0	0	0	-819	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
4	55	-0	-1044	0	0	0	-796	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
5	55	-0	-1025	0	0	0	-791	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
6	55	-0	-1128	0	0	0	-819	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
7	55	-0	-1063	0	0	0	-804	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
8	55	-0	-1099	0	0	0	-811	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9

9	55	-0	-1035	0	0	0	-796	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
10	55	-0	-1138	0	0	0	-824	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
11	55	-0	-1119	0	0	0	-819	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
12	55	-0	-1044	0	0	0	-796	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
13	55	-0	-1025	0	0	0	-791	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
14	55	-0	-1128	0	0	0	-819	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
15	55	-0	-1063	0	0	0	-804	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
16	55	-0	-1099	0	0	0	-811	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
17	55	-0	-1035	0	0	0	-796	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
18	55	-0	-2252	0	0	0	-1396	--	--	16.08	16.08	0.18	0.02	0.02	0.14	0.00	0.00	20.9
19	55	-0	-1971	0	0	0	-1404	--	--	16.08	16.08	0.18	0.02	0.02	0.12	0.00	0.00	20.9
20	55	-0	-1955	0	0	0	-1275	--	--	16.08	16.08	0.18	0.02	0.02	0.12	0.00	0.00	20.9
37	55	-0	-2117	0	0	0	-1280	--	--	16.08	16.08	0.18	0.02	0.02	0.13	0.00	0.00	20.9
38	55	-0	-1648	0	0	0	-1294	--	--	16.08	16.08	0.18	0.02	0.01	0.10	0.00	0.00	20.9
39	55	-0	-1622	0	0	0	-1080	--	--	16.08	16.08	0.18	0.02	0.01	0.10	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 181 NI 1598 NF 1597 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-2859	0	0	0	601	--	--	16.08	16.08	0.00	0.01	0.02	0.18	0.00	0.00	20.9
2	0	-0	-2315	0	0	0	514	--	--	16.08	16.08	0.10	0.01	0.02	0.15	0.00	0.00	20.9
3	0	-0	-2293	0	0	0	504	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
4	0	-0	-2106	0	0	0	420	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
5	0	-0	-2084	0	0	0	410	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
6	0	-0	-2267	0	0	0	493	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
7	0	-0	-2195	0	0	0	460	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
8	0	-0	-2204	0	0	0	465	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
9	0	-0	-2132	0	0	0	431	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
10	0	-0	-2315	0	0	0	514	--	--	16.08	16.08	0.10	0.01	0.02	0.15	0.00	0.00	20.9
11	0	-0	-2293	0	0	0	504	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
12	0	-0	-2106	0	0	0	420	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
13	0	-0	-2084	0	0	0	410	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
14	0	-0	-2267	0	0	0	493	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
15	0	-0	-2195	0	0	0	460	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
16	0	-0	-2204	0	0	0	465	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
17	0	-0	-2132	0	0	0	431	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
18	0	-0	-4642	0	0	0	1296	--	--	16.08	16.08	0.00	0.02	0.04	0.29	0.00	0.00	20.9
19	0	-0	-3982	0	0	0	900	--	--	16.08	16.08	0.00	0.02	0.03	0.25	0.00	0.00	20.9
20	0	-0	-4034	0	0	0	1056	--	--	16.08	16.08	0.00	0.02	0.03	0.25	0.00	0.00	20.9
37	0	-0	-4391	0	0	0	1266	--	--	16.08	16.08	0.00	0.02	0.04	0.28	0.00	0.00	20.9
38	0	-0	-3291	0	0	0	605	--	--	16.08	16.08	0.00	0.01	0.03	0.21	0.00	0.00	20.9
39	0	-0	-3376	0	0	0	866	--	--	16.08	16.08	0.00	0.01	0.03	0.21	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-2859	0	0	0	-959	--	--	16.08	16.08	0.18	0.02	0.02	0.18	0.00	0.00	20.9
2	27	-0	-2315	0	0	0	-748	--	--	16.08	16.08	0.29	0.01	0.02	0.15	0.00	0.00	20.9
3	27	-0	-2293	0	0	0	-746	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
4	27	-0	-2106	0	0	0	-729	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
5	27	-0	-2084	0	0	0	-727	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
6	27	-0	-2267	0	0	0	-743	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
7	27	-0	-2195	0	0	0	-738	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
8	27	-0	-2204	0	0	0	-737	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
9	27	-0	-2132	0	0	0	-732	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
10	27	-0	-2315	0	0	0	-748	--	--	16.08	16.08	0.29	0.01	0.02	0.15	0.00	0.00	20.9
11	27	-0	-2293	0	0	0	-746	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
12	27	-0	-2106	0	0	0	-729	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
13	27	-0	-2084	0	0	0	-727	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
14	27	-0	-2267	0	0	0	-743	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
15	27	-0	-2195	0	0	0	-738	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
16	27	-0	-2204	0	0	0	-737	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
17	27	-0	-2132	0	0	0	-732	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
18	27	-0	-4642	0	0	0	1296	--	--	16.08	16.08	0.00	0.02	0.04	0.29	0.00	0.00	20.9
19	27	-0	-3982	0	0	0	-1272	--	--	16.08	16.08	0.18	0.02	0.03	0.25	0.00	0.00	20.9
20	27	-0	-4034	0	0	0	-1144	--	--	16.08	16.08	0.18	0.02	0.03	0.25	0.00	0.00	20.9
37	27	-0	-4391	0	0	0	1266	--	--	16.08	16.08	0.00	0.02	0.04	0.28	0.00	0.00	20.9
38	27	-0	-3291	0	0	0	-1190	--	--	16.08	16.08	0.18	0.02	0.03	0.21	0.00	0.00	20.9
39	27	-0	-3376	0	0	0	-975	--	--	16.08	16.08	0.18	0.02	0.03	0.21	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	-2859	0	0	0	-959	--	--	16.08	16.08	0.18	0.02	0.02	0.18	0.00	0.00	20.9
2	55	-0	-2315	0	0	0	-748	--	--	16.08	16.08	0.29	0.01	0.02	0.15	0.00	0.00	20.9
3	55	-0	-2293	0	0	0	-746	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
4	55	-0	-2106	0	0	0	-729	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
5	55	-0	-2084	0	0	0	-727	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
6	55	-0	-2267	0	0	0	-743	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
7	55	-0	-2195	0	0	0	-738	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
8	55	-0	-2204	0	0	0	-737	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
9	55	-0	-2132	0	0	0	-732	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
10	55	-0	-2315	0	0	0	-748	--	--	16.08	16.08	0.29	0.01	0.02	0.15	0.00	0.00	20.9
11	55	-0	-2293	0	0	0	-746	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
12	55	-0	-2106	0	0	0	-729	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
13	55	-0	-2084	0	0	0	-727	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
14	55	-0	-2267	0	0	0	-743	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
15	55	-0	-2195	0	0	0	-738	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
16	55	-0	-2204	0	0	0	-737	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
17	55	-0	-2132	0	0	0	-732	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
18	55	-0	-4642	0	0	0	-1236	--	--	16.08	16.08	0.18	0.02	0.04	0.29	0.00	0.00	20.9
19	55	-0	-3982	0	0	0	-1272	--	--	16.08	16.08	0.18	0.02	0.03	0.25	0.00	0.00	20.9
20	55	-0	-4034	0	0	0	-1144	--	--	16.08	16.08	0.18	0.02	0.03	0.25	0.00	0.00	20.9
37	55	-0	-4391	0	0	0	-1129	--	--	16.08	16.08	0.18	0.02	0.04	0.28	0.00	0.00	20.9
38	55	-0	-3291	0	0	0	-1190	--	--	16.08	16.08	0.18	0.02	0.03	0.21	0.00	0.00	20.9
39	55	-0	-3376	0	0	0	-975	--	--	16.08	16.08	0.18	0.02	0.03	0.21	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 182 NI 1614 NF 1598 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-4622	0	0	0	2015	--	--	16.08	16.08	0.00	0.03	0.04	0.29	0.00	0.00	20.9
2	0	-0	-3748	0	0	0	1667	--	--	16.08	16.08	0.10	0.03	0.03	0.24	0.00	0.00	20.9
3	0	-0	-3733	0	0	0	1659	--	--	16.08	16.08	0.10	0.03	0.03	0.23	0.00	0.00	20.9
4	0	-0	-3377	0	0	0	1441	--	--	16.08	16.08	0.10	0.03	0.03	0.21	0.00	0.00	20.9
5	0	-0	-3362	0	0	0	1433	--	--	16.08	16.08	0.10	0.03	0.03	0.21	0.00	0.00	20.9
6	0	-0	-3636	0	0	0	1597	--	--	16.08	16.08	0.10	0.03	0.03	0.23	0.00	0.00	20.9
7	0	-0	-3585	0	0	0	1570	--	--	16.08	16.08	0.10	0.03	0.03	0.22	0.00	0.00	20.9
8	0	-0	-3525	0	0	0	1530	--	--	16.08	16.08	0.10	0.03	0.03	0.22	0.00	0.00	20.9
9	0	-0	-3474	0	0	0	1503	--	--	16.08	16.08	0.10	0.03	0.03	0.22	0.00	0.00	20.9
10	0	-0	-3748	0	0	0	1667	--	--	16.08	16.08	0.10	0.03	0.03	0.24	0.00	0.00	20.9
11	0	-0	-3733	0	0	0	1659	--	--	16.08	16.08	0.10	0.03	0.03	0.23	0.00	0.00	20.9
12	0	-0	-3377	0	0	0	1441	--	--	16.08	16.08	0.10	0.03	0.03	0.21	0.00	0.00	20.9
13	0	-0	-3362	0	0	0	1433	--	--	16.08	16.08	0.10	0.03	0.03	0.21	0.00	0.00	20.9
14	0	-0	-3636	0	0	0	1597	--	--	16.08	16.08	0.10	0.03	0.03	0.23	0.00	0.00	20.9
15	0	-0	-3585	0	0	0	1570	--	--	16.08	16.08	0.10	0.03	0.03	0.22	0.00	0.00	20.9
16	0	-0	-3525	0	0	0	1530	--	--	16.08	16.08	0.10	0.03	0.03	0.22	0.00	0.00	20.9
17	0	-0	-3474	0	0	0	1503	--	--	16.08	16.08	0.10	0.03	0.03	0.22	0.00	0.00	20.9
18	0	-0	-7625	0	0	0	3699	--	--	16.08	16.08	0.00	0.06	0.06	0.48	0.00	0.00	20.9
19	0	-0	-6422	0	0	0	2862	--	--	16.08	16.08	0.00	0.05	0.05	0.40	0.00	0.00	20.9
20	0	-0	-6618	0	0	0	3131	--	--	16.08	16.08	0.00	0.05	0.05	0.42	0.00	0.00	20.9
37	0	-0	-7247	0	0	0	3566	--	--	16.08	16.08	0.00	0.06	0.06	0.45	0.00	0.00	20.9
38	0	-0	-5241	0	0	0	2171	--	--	16.08	16.08	0.00	0.04	0.04	0.33	0.00	0.00	20.9
39	0	-0	-5568	0	0	0	2619	--	--	16.08	16.08	0.00	0.04	0.05	0.35	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-4622	0	0	0	2015	--	--	16.08	16.08	0.00	0.03	0.04	0.29	0.00	0.00	20.9
2	27	-0	-3748	0	0	0	1667	--	--	16.08	16.08	0.10	0.03	0.03	0.24	0.00	0.00	20.9
3	27	-0	-3733	0	0	0	1659	--	--	16.08	16.08	0.10	0.03	0.03	0.23	0.00	0.00	20.9
4	27	-0	-3377	0	0	0	1441	--	--	16.08	16.08	0.10	0.03	0.03	0.21	0.00	0.00	20.9
5	27	-0	-3362	0	0	0	1433	--	--	16.08	16.08	0.10	0.03	0.03	0.21	0.00	0.00	20.9
6	27	-0	-3636	0	0	0	1597	--	--	16.08	16.08	0.10	0.03	0.03	0.23	0.00	0.00	20.9
7	27	-0	-3585	0	0	0	1570	--	--	16.08	16.08	0.10	0.03	0.03	0.22	0.00	0.00	20.9
8	27	-0	-3525	0	0	0	1530	--	--	16.08	16.08	0.10	0.03	0.03	0.22	0.00	0.00	20.9
9	27	-0	-3474	0	0	0	1503	--	--	16.08	16.08	0.10	0.03	0.03	0.22	0.00	0.00	20.9
10	27	-0	-3748	0	0	0	1667	--	--	16.08	16.08	0.10	0.03	0.03	0.24	0.00	0.00	20.9
11	27	-0	-3733	0	0	0	1659	--	--	16.08	16.08	0.10	0.03	0.03	0.23	0.00	0.00	20.9
12	27	-0	-3377	0	0	0	1441	--	--	16.08	16.08	0.10	0.03	0.03	0.21	0.00	0.00	20.9
13	27	-0	-3362	0	0	0	1433	--	--	16.08	16.08	0.10	0.03	0.03	0.21	0.00	0.00	20.9
14	27	-0	-3636	0	0	0	1597	--	--	16.08	16.08	0.10	0.03	0.03	0.23	0.00	0.00	20.9
15	27	-0	-3585	0	0	0	1570	--	--	16.08	16.08	0.10	0.03	0.03	0.22	0.00	0.00	20.9
16	27	-0	-3525	0	0	0	1530	--	--	16.08	16.08	0.10	0.03	0.03	0.22	0.00	0.00	20.9
17	27	-0	-3474	0	0	0	1503	--	--	16.08	16.08	0.10	0.03	0.03	0.22	0.00	0.00	20.9
18	27	-0	-7625	0	0	0	3699	--	--	16.08	16.08	0.00	0.06	0.06	0.48	0.00	0.00	20.9
19	27	-0	-6422	0	0	0	2862	--	--	16.08	16.08	0.00	0.05	0.05	0.40	0.00	0.00	20.9
20	27	-0	-6618	0	0	0	3131	--	--	16.08	16.08	0.00	0.05	0.05	0.42	0.00	0.00	20.9
37	27	-0	-7247	0	0	0	3566	--	--	16.08	16.08	0.00	0.06	0.06	0.45	0.00	0.00	20.9
38	27	-0	-5241	0	0	0	2171	--	--	16.08	16.08	0.00	0.04	0.04	0.33	0.00	0.00	20.9
39	27	-0	-5568	0	0	0	2619	--	--	16.08	16.08	0.00	0.04	0.05	0.35	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	-4622	0	0	0	-506	--	--	16.08	16.08	0.18	0.01	0.04	0.29	0.00	0.00	20.9
2	55	-0	-3748	0	0	0	-378	--	--	16.08	16.08	0.29	0.01	0.03	0.24	0.00	0.00	20.9
3	55	-0	-3733	0	0	0	-377	--	--	16.08	16.08	0.29	0.01	0.03	0.23	0.00	0.00	20.9
4	55	-0	-3377	0	0	0	-401	--	--	16.08	16.08	0.29	0.01	0.03	0.21	0.00	0.00	20.9
5	55	-0	-3362	0	0	0	-401	--	--	16.08	16.08	0.29	0.01	0.03	0.21	0.00	0.00	20.9
6	55	-0	-3636	0	0	0	-386	--	--	16.08	16.08	0.29	0.01	0.03	0.23	0.00	0.00	20.9
7	55	-0	-3585	0	0	0	-385	--	--	16.08	16.08	0.29	0.01	0.03	0.22	0.00	0.00	20.9
8	55	-0	-3525	0	0	0	-393	--	--	16.08	16.08	0.29	0.01	0.03	0.22	0.00	0.00	20.9
9	55	-0	-3474	0	0	0	-392	--	--	16.08	16.08	0.29	0.01	0.03	0.22	0.00	0.00	20.9
10	55	-0	-3748	0	0	0	-378	--	--	16.08	16.08	0.29	0.01	0.03	0.24	0.00	0.00	20.9
11	55	-0	-3733	0	0	0	-377	--	--	16.08	16.08	0.29	0.01	0.03	0.23	0.00	0.00	20.9
12	55	-0	-3377	0	0	0	-401	--	--	16.08	16.08	0.29	0.01	0.03	0.21	0.00	0.00	20.9
13	55	-0	-3362	0	0	0	-401	--	--	16.08	16.08	0.29	0.01	0.03	0.21	0.00	0.00	20.9
14	55	-0	-3636	0	0	0	-386	--	--	16.08	16.08	0.29	0.01	0.03	0.23	0.00	0.00	20.9
15	55	-0	-3585	0	0	0	-385	--	--	16.08	16.08	0.29	0.01	0.03	0.22	0.00	0.00	20.9
16	55	-0	-3525	0	0	0	-393	--	--	16.08	16.08	0.29	0.01	0.03	0.22	0.00	0.00	20.9
17	55	-0	-3474	0	0	0	-392	--	--	16.08	16.08	0.29	0.01	0.03	0.22	0.00	0.00	20.9
18	55	-0	-7625	0	0	0	-460	--	--	16.08	16.08	0.18	0.01	0.06	0.48	0.00	0.00	20.9
19	55	-0	-6422	0	0	0	-641	--	--	16.08	16.08	0.18	0.01	0.05	0.40	0.00	0.00	20.9
20	55	-0	-6618	0	0	0	-479	--	--	16.08	16.08	0.18	0.01	0.05	0.42	0.00	0.00	20.9
37	55	-0	-7247	0	0	0	-387	--	--	16.08	16.08	0.18	0.01	0.06	0.45	0.00	0.00	20.9
38	55	-0	-5241	0	0	0	-688	--	--	16.08	16.08	0.18	0.01	0.04	0.33	0.00	0.00	20.9
39	55	-0	-5568	0	0	0	-418	--	--	16.08	16.08	0.18	0.01	0.05	0.35	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 183 NI 1554 NF 1614 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-5301	0	0	0	3071	--	--	16.08	16.08	0.00	0.05	0.04	0.33	0.00	0.00	20.9
2	0	-0	-4266	0	0	0	2501	--	--	16.08	16.08	0.10	0.04	0.04	0.27	0.00	0.00	20.9
3	0	-0	-4283	0	0	0	2514	--	--	16.08	16.08	0.10	0.04	0.04	0.27	0.00	0.00	20.9
4	0	-0	-3873	0	0	0	2211	--	--	16.08	16.08	0.10	0.04	0.03	0.24	0.00	0.00	20.9
5	0	-0	-3890	0	0	0	2224	--	--	16.08	16.08	0.10	0.04	0.03	0.24	0.00	0.00	20.9
6	0	-0	-4108	0	0	0	2384	--	--	16.08	16.08	0.10	0.04	0.03	0.26	0.00	0.00	20.9
7	0	-0	-4165	0	0	0	2428	--	--	16.08	16.08	0.10	0.04	0.03	0.26	0.00	0.00	20.9
8	0	-0	-3991	0	0	0	2297	--	--	16.08	16.08	0.10	0.04	0.03	0.25	0.00	0.00	20.9
9	0	-0	-4048	0	0	0	2341	--	--	16.08	16.08	0.10	0.04	0.03	0.25	0.00	0.00	20.9
10	0	-0	-4266	0	0	0	2501	--	--	16.08	16.08	0.10	0.04	0.04	0.27	0.00	0.00	20.9
11	0	-0	-4283	0	0	0	2514	--	--	16.08	16.08	0.10	0.04	0.04	0.27	0.00	0.00	20.9
12	0	-0	-3873	0	0	0	2211	--	--	16.08	16.08	0.10	0.04	0.03	0.24	0.00	0.00	20.9
13	0	-0	-3890	0	0	0	2224	--	--	16.08	16.08	0.10	0.04	0.03	0.24	0.00	0.00	20.9
14	0	-0	-4108	0	0	0	2384	--	--	16.08	16.08	0.10	0.04	0.03	0.26	0.00	0.00	20.9
15	0	-0	-4165	0	0	0	2428	--	--	16.08	16.08	0.10	0.04	0.03	0.26	0.00	0.00	20.9
16	0	-0	-3991	0	0	0	2297	--	--	16.08	16.08	0.10	0.04	0.03	0.25	0.00	0.00	20.9

17	0	-0	-4048	0	0	0	2341	--	--	16.08	16.08	0.10	0.04	0.03	0.25	0.00	0.00	20.9
18	0	-0	-8539	0	0	0	5310	--	--	16.08	16.08	0.00	0.09	0.07	0.54	0.00	0.00	20.9
19	0	-0	-7313	0	0	0	4288	--	--	16.08	16.08	0.00	0.07	0.06	0.46	0.00	0.00	20.9
20	0	-0	-7581	0	0	0	4645	--	--	16.08	16.08	0.00	0.08	0.06	0.48	0.00	0.00	20.9
37	0	-0	-8097	0	0	0	5089	--	--	16.08	16.08	0.00	0.09	0.07	0.51	0.00	0.00	20.9
38	0	-0	-6054	0	0	0	3386	--	--	16.08	16.08	0.00	0.06	0.05	0.38	0.00	0.00	20.9
39	0	-0	-6501	0	0	0	3981	--	--	16.08	16.08	0.00	0.07	0.05	0.41	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-5301	0	0	0	3071	--	--	16.08	16.08	0.00	0.05	0.04	0.33	0.00	0.00	20.9
2	27	-0	-4266	0	0	0	2501	--	--	16.08	16.08	0.10	0.04	0.04	0.27	0.00	0.00	20.9
3	27	-0	-4283	0	0	0	2514	--	--	16.08	16.08	0.10	0.04	0.04	0.27	0.00	0.00	20.9
4	27	-0	-3873	0	0	0	2211	--	--	16.08	16.08	0.10	0.04	0.03	0.24	0.00	0.00	20.9
5	27	-0	-3890	0	0	0	2224	--	--	16.08	16.08	0.10	0.04	0.03	0.24	0.00	0.00	20.9
6	27	-0	-4108	0	0	0	2384	--	--	16.08	16.08	0.10	0.04	0.03	0.26	0.00	0.00	20.9
7	27	-0	-4165	0	0	0	2428	--	--	16.08	16.08	0.10	0.04	0.03	0.26	0.00	0.00	20.9
8	27	-0	-3991	0	0	0	2297	--	--	16.08	16.08	0.10	0.04	0.03	0.25	0.00	0.00	20.9
9	27	-0	-4048	0	0	0	2341	--	--	16.08	16.08	0.10	0.04	0.03	0.25	0.00	0.00	20.9
10	27	-0	-4266	0	0	0	2501	--	--	16.08	16.08	0.10	0.04	0.04	0.27	0.00	0.00	20.9
11	27	-0	-4283	0	0	0	2514	--	--	16.08	16.08	0.10	0.04	0.04	0.27	0.00	0.00	20.9
12	27	-0	-3873	0	0	0	2211	--	--	16.08	16.08	0.10	0.04	0.03	0.24	0.00	0.00	20.9
13	27	-0	-3890	0	0	0	2224	--	--	16.08	16.08	0.10	0.04	0.03	0.24	0.00	0.00	20.9
14	27	-0	-4108	0	0	0	2384	--	--	16.08	16.08	0.10	0.04	0.03	0.26	0.00	0.00	20.9
15	27	-0	-4165	0	0	0	2428	--	--	16.08	16.08	0.10	0.04	0.03	0.26	0.00	0.00	20.9
16	27	-0	-3991	0	0	0	2297	--	--	16.08	16.08	0.10	0.04	0.03	0.25	0.00	0.00	20.9
17	27	-0	-4048	0	0	0	2341	--	--	16.08	16.08	0.10	0.04	0.03	0.25	0.00	0.00	20.9
18	27	-0	-8539	0	0	0	5310	--	--	16.08	16.08	0.00	0.09	0.07	0.54	0.00	0.00	20.9
19	27	-0	-7313	0	0	0	4288	--	--	16.08	16.08	0.00	0.07	0.06	0.46	0.00	0.00	20.9
20	27	-0	-7581	0	0	0	4645	--	--	16.08	16.08	0.00	0.08	0.06	0.48	0.00	0.00	20.9
37	27	-0	-8097	0	0	0	5089	--	--	16.08	16.08	0.00	0.09	0.07	0.51	0.00	0.00	20.9
38	27	-0	-6054	0	0	0	3386	--	--	16.08	16.08	0.00	0.06	0.05	0.38	0.00	0.00	20.9
39	27	-0	-6501	0	0	0	3981	--	--	16.08	16.08	0.00	0.07	0.05	0.41	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	-5301	0	0	0	180	--	--	16.08	16.08	0.00	0.00	0.04	0.33	0.00	0.00	20.9
2	55	-0	-4266	0	0	0	174	--	--	16.08	16.08	0.10	0.00	0.04	0.27	0.00	0.00	20.9
3	55	-0	-4283	0	0	0	178	--	--	16.08	16.08	0.10	0.00	0.04	0.27	0.00	0.00	20.9
4	55	-0	-3873	0	0	0	98	--	--	16.08	16.08	0.10	0.00	0.03	0.24	0.00	0.00	20.9
5	55	-0	-3890	0	0	0	102	--	--	16.08	16.08	0.10	0.00	0.03	0.24	0.00	0.00	20.9
6	55	-0	-4108	0	0	0	143	--	--	16.08	16.08	0.10	0.00	0.03	0.26	0.00	0.00	20.9
7	55	-0	-4165	0	0	0	156	--	--	16.08	16.08	0.10	0.00	0.03	0.26	0.00	0.00	20.9
8	55	-0	-3991	0	0	0	120	--	--	16.08	16.08	0.10	0.00	0.03	0.25	0.00	0.00	20.9
9	55	-0	-4048	0	0	0	133	--	--	16.08	16.08	0.10	0.00	0.03	0.25	0.00	0.00	20.9
10	55	-0	-4266	0	0	0	174	--	--	16.08	16.08	0.10	0.00	0.04	0.27	0.00	0.00	20.9
11	55	-0	-4283	0	0	0	178	--	--	16.08	16.08	0.10	0.00	0.04	0.27	0.00	0.00	20.9
12	55	-0	-3873	0	0	0	98	--	--	16.08	16.08	0.10	0.00	0.03	0.24	0.00	0.00	20.9
13	55	-0	-3890	0	0	0	102	--	--	16.08	16.08	0.10	0.00	0.03	0.24	0.00	0.00	20.9
14	55	-0	-4108	0	0	0	143	--	--	16.08	16.08	0.10	0.00	0.03	0.26	0.00	0.00	20.9
15	55	-0	-4165	0	0	0	156	--	--	16.08	16.08	0.10	0.00	0.03	0.26	0.00	0.00	20.9
16	55	-0	-3991	0	0	0	120	--	--	16.08	16.08	0.10	0.00	0.03	0.25	0.00	0.00	20.9
17	55	-0	-4048	0	0	0	133	--	--	16.08	16.08	0.10	0.00	0.03	0.25	0.00	0.00	20.9
18	55	-0	-8539	0	0	0	653	--	--	16.08	16.08	0.00	0.01	0.07	0.54	0.00	0.00	20.9
19	55	-0	-7313	0	0	0	299	--	--	16.08	16.08	0.00	0.01	0.06	0.46	0.00	0.00	20.9
20	55	-0	-7581	0	0	0	510	--	--	16.08	16.08	0.00	0.01	0.06	0.48	0.00	0.00	20.9
37	55	-0	-8097	0	0	0	673	--	--	16.08	16.08	0.00	0.01	0.07	0.51	0.00	0.00	20.9
38	55	-0	-6054	0	0	0	84	--	--	16.08	16.08	0.00	0.00	0.05	0.38	0.00	0.00	20.9
39	55	-0	-6501	0	0	0	436	--	--	16.08	16.08	0.00	0.01	0.05	0.41	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 184 NI 1675 NF 1554 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-2474	0	0	0	2720	--	--	16.08	16.08	0.00	0.05	0.02	0.16	0.00	0.00	20.9
2	0	-0	-1844	0	0	0	2154	--	--	16.08	16.08	0.10	0.04	0.02	0.12	0.00	0.00	20.9
3	0	-0	-1879	0	0	0	2170	--	--	16.08	16.08	0.10	0.04	0.02	0.12	0.00	0.00	20.9
4	0	-0	-1927	0	0	0	2014	--	--	16.08	16.08	0.10	0.04	0.02	0.12	0.00	0.00	20.9
5	0	-0	-1962	0	0	0	2030	--	--	16.08	16.08	0.10	0.04	0.02	0.12	0.00	0.00	20.9
6	0	-0	-1833	0	0	0	2086	--	--	16.08	16.08	0.10	0.04	0.02	0.11	0.00	0.00	20.9
7	0	-0	-1948	0	0	0	2140	--	--	16.08	16.08	0.10	0.04	0.02	0.12	0.00	0.00	20.9
8	0	-0	-1858	0	0	0	2044	--	--	16.08	16.08	0.10	0.04	0.02	0.12	0.00	0.00	20.9
9	0	-0	-1973	0	0	0	2098	--	--	16.08	16.08	0.10	0.04	0.02	0.12	0.00	0.00	20.9
10	0	-0	-1844	0	0	0	2154	--	--	16.08	16.08	0.10	0.04	0.02	0.12	0.00	0.00	20.9
11	0	-0	-1879	0	0	0	2170	--	--	16.08	16.08	0.10	0.04	0.02	0.12	0.00	0.00	20.9
12	0	-0	-1927	0	0	0	2014	--	--	16.08	16.08	0.10	0.04	0.02	0.12	0.00	0.00	20.9
13	0	-0	-1962	0	0	0	2030	--	--	16.08	16.08	0.10	0.04	0.02	0.12	0.00	0.00	20.9
14	0	-0	-1833	0	0	0	2086	--	--	16.08	16.08	0.10	0.04	0.02	0.11	0.00	0.00	20.9
15	0	-0	-1948	0	0	0	2140	--	--	16.08	16.08	0.10	0.04	0.02	0.12	0.00	0.00	20.9
16	0	-0	-1858	0	0	0	2044	--	--	16.08	16.08	0.10	0.04	0.02	0.12	0.00	0.00	20.9
17	0	-0	-1973	0	0	0	2098	--	--	16.08	16.08	0.10	0.04	0.02	0.12	0.00	0.00	20.9
18	0	-0	-2632	0	0	0	4108	--	--	16.08	16.08	0.00	0.07	0.02	0.17	0.00	0.00	20.9
19	0	-0	-3281	0	0	0	3741	--	--	16.08	16.08	0.00	0.06	0.03	0.21	0.00	0.00	20.9
20	0	-0	-2965	0	0	0	3850	--	--	16.08	16.08	0.00	0.07	0.02	0.19	0.00	0.00	20.9
37	0	-0	-2263	0	0	0	3841	--	--	16.08	16.08	0.00	0.07	0.02	0.14	0.00	0.00	20.9
38	0	-0	-3346	0	0	0	3228	--	--	16.08	16.08	0.00	0.06	0.03	0.21	0.00	0.00	20.9
39	0	-0	-2818	0	0	0	3411	--	--	16.08	16.08	0.00	0.06	0.02	0.18	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-2474	0	0	0	2720	--	--	16.08	16.08	0.00	0.05	0.02	0.16	0.00	0.00	20.9
2	27	-0	-1844	0	0	0	2154	--	--	16.08	16.08	0.10	0.04	0.02	0.12	0.00	0.00	20.9
3	27	-0	-1879	0	0	0	2170	--	--	16.08	16.08	0.10	0.04	0.02	0.12	0.00	0.00	20.9
4	27	-0	-1927	0	0	0	2014	--	--	16.08	16.08	0.10	0.04	0.02	0.12	0.00	0.00	20.9
5	27	-0	-1962	0	0	0	2030	--	--	16.08	16.08	0.10	0.04	0.02	0.12	0.00	0.00	20.9
6	27	-0	-1833	0	0	0	2086	--	--	16.08	16.08	0.10	0.04	0.02	0.11	0.00	0.00	20.9
7	27	-0	-1948	0	0	0	2140	--	--	16.08	16.08	0.10	0.04	0.02	0.12	0.00	0.00	20.9
8	27	-0	-1858	0	0	0	2044	--	--	16.08	16.08	0.10	0.04	0.02	0.12	0.00	0.00	20.9
9	27	-0	-1973	0	0	0	2098	--	--	16.08	16.08	0.10	0.04	0.02	0.12	0.00	0.00	20.9
10	27	-0	-1844	0	0	0	2154	--	--	16.08	16.08	0.10	0.04	0.02	0.12	0.00	0.00	20.9
11	27	-0	-1879	0	0	0	2170	--	--	16.08	16.08	0.10	0.04	0.02	0.12	0.00	0.00	20.9
12	27	-0	-1927	0	0	0	2014	--	--	16.08	16.08	0.10	0.04	0.02	0.12	0.00	0.00	20.9

13	27	-0	-1962	0	0	0	2030	--	--	16.08	16.08	0.10	0.04	0.02	0.12	0.00	0.00	20.9
14	27	-0	-1833	0	0	0	2086	--	--	16.08	16.08	0.10	0.04	0.02	0.11	0.00	0.00	20.9
15	27	-0	-1948	0	0	0	2140	--	--	16.08	16.08	0.10	0.04	0.02	0.12	0.00	0.00	20.9
16	27	-0	-1858	0	0	0	2044	--	--	16.08	16.08	0.10	0.04	0.02	0.12	0.00	0.00	20.9
17	27	-0	-1973	0	0	0	2098	--	--	16.08	16.08	0.10	0.04	0.02	0.12	0.00	0.00	20.9
18	27	-0	-2632	0	0	0	4108	--	--	16.08	16.08	0.00	0.07	0.02	0.17	0.00	0.00	20.9
19	27	-0	-3281	0	0	0	3741	--	--	16.08	16.08	0.00	0.06	0.03	0.21	0.00	0.00	20.9
20	27	-0	-2965	0	0	0	3850	--	--	16.08	16.08	0.00	0.07	0.02	0.19	0.00	0.00	20.9
37	27	-0	-2263	0	0	0	3841	--	--	16.08	16.08	0.00	0.07	0.02	0.14	0.00	0.00	20.9
38	27	-0	-3346	0	0	0	3228	--	--	16.08	16.08	0.00	0.06	0.03	0.21	0.00	0.00	20.9
39	27	-0	-2818	0	0	0	3411	--	--	16.08	16.08	0.00	0.06	0.02	0.18	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	-2474	0	0	0	1370	--	--	16.08	16.08	0.00	0.02	0.02	0.16	0.00	0.00	20.9
2	55	-0	-1844	0	0	0	1148	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
3	55	-0	-1879	0	0	0	1145	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
4	55	-0	-1927	0	0	0	963	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
5	55	-0	-1962	0	0	0	960	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
6	55	-0	-1833	0	0	0	1086	--	--	16.08	16.08	0.10	0.02	0.02	0.11	0.00	0.00	20.9
7	55	-0	-1948	0	0	0	1077	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
8	55	-0	-1858	0	0	0	1031	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
9	55	-0	-1973	0	0	0	1022	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
10	55	-0	-1844	0	0	0	1148	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
11	55	-0	-1879	0	0	0	1145	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
12	55	-0	-1927	0	0	0	963	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
13	55	-0	-1962	0	0	0	960	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
14	55	-0	-1833	0	0	0	1086	--	--	16.08	16.08	0.10	0.02	0.02	0.11	0.00	0.00	20.9
15	55	-0	-1948	0	0	0	1077	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
16	55	-0	-1858	0	0	0	1031	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
17	55	-0	-1973	0	0	0	1022	--	--	16.08	16.08	0.10	0.02	0.02	0.12	0.00	0.00	20.9
18	55	-0	-2632	0	0	0	2673	--	--	16.08	16.08	0.00	0.05	0.02	0.17	0.00	0.00	20.9
19	55	-0	-3281	0	0	0	1951	--	--	16.08	16.08	0.00	0.03	0.03	0.21	0.00	0.00	20.9
20	55	-0	-2965	0	0	0	2233	--	--	16.08	16.08	0.00	0.04	0.02	0.19	0.00	0.00	20.9
37	55	-0	-2263	0	0	0	2606	--	--	16.08	16.08	0.00	0.04	0.02	0.14	0.00	0.00	20.9
38	55	-0	-3346	0	0	0	1403	--	--	16.08	16.08	0.00	0.02	0.03	0.21	0.00	0.00	20.9
39	55	-0	-2818	0	0	0	1873	--	--	16.08	16.08	0.00	0.03	0.02	0.18	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 185 NI 1762 NF 1675 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	1676	0	0	0	1221	--	--	16.08	16.08	0.00	0.02	0.01	0.11	0.00	0.00	20.9
2	0	-0	1180	0	0	0	986	--	--	16.08	16.08	0.10	0.02	0.01	0.07	0.00	0.00	20.9
3	0	-0	1145	0	0	0	1003	--	--	16.08	16.08	0.10	0.02	0.01	0.07	0.00	0.00	20.9
4	0	-0	1433	0	0	0	876	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
5	0	-0	1399	0	0	0	892	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
6	0	-0	1308	0	0	0	928	--	--	16.08	16.08	0.10	0.02	0.01	0.08	0.00	0.00	20.9
7	0	-0	1194	0	0	0	983	--	--	16.08	16.08	0.10	0.02	0.01	0.07	0.00	0.00	20.9
8	0	-0	1384	0	0	0	895	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
9	0	-0	1270	0	0	0	950	--	--	16.08	16.08	0.10	0.02	0.01	0.08	0.00	0.00	20.9
10	0	-0	1180	0	0	0	986	--	--	16.08	16.08	0.10	0.02	0.01	0.07	0.00	0.00	20.9
11	0	-0	1145	0	0	0	1003	--	--	16.08	16.08	0.10	0.02	0.01	0.07	0.00	0.00	20.9
12	0	-0	1433	0	0	0	876	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
13	0	-0	1399	0	0	0	892	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
14	0	-0	1308	0	0	0	928	--	--	16.08	16.08	0.10	0.02	0.01	0.08	0.00	0.00	20.9
15	0	-0	1194	0	0	0	983	--	--	16.08	16.08	0.10	0.02	0.01	0.07	0.00	0.00	20.9
16	0	-0	1384	0	0	0	895	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
17	0	-0	1270	0	0	0	950	--	--	16.08	16.08	0.10	0.02	0.01	0.08	0.00	0.00	20.9
18	0	-0	951	0	0	0	2171	--	--	16.08	16.08	0.00	0.04	0.01	0.06	0.00	0.00	20.9
19	0	-0	2145	0	0	0	1796	--	--	16.08	16.08	0.00	0.03	0.02	0.13	0.00	0.00	20.9
20	0	-0	1489	0	0	0	1966	--	--	16.08	16.08	0.00	0.03	0.01	0.09	0.00	0.00	20.9
37	0	-0	599	0	0	0	2048	--	--	16.08	16.08	0.00	0.03	0.00	0.04	0.00	0.00	20.9
38	0	-0	2588	0	0	0	1423	--	--	16.08	16.08	0.00	0.02	0.02	0.16	0.00	0.00	20.9
39	0	-0	1495	0	0	0	1705	--	--	16.08	16.08	0.00	0.03	0.01	0.09	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	1676	0	0	0	3469	--	--	16.08	16.08	0.00	0.06	0.01	0.11	0.00	0.00	20.9
2	27	-0	1180	0	0	0	2569	--	--	16.08	16.08	0.10	0.05	0.01	0.07	0.00	0.00	20.9
3	27	-0	1145	0	0	0	2539	--	--	16.08	16.08	0.10	0.05	0.01	0.07	0.00	0.00	20.9
4	27	-0	1433	0	0	0	2798	--	--	16.08	16.08	0.10	0.05	0.01	0.09	0.00	0.00	20.9
5	27	-0	1399	0	0	0	2769	--	--	16.08	16.08	0.10	0.05	0.01	0.09	0.00	0.00	20.9
6	27	-0	1308	0	0	0	2683	--	--	16.08	16.08	0.10	0.05	0.01	0.08	0.00	0.00	20.9
7	27	-0	1194	0	0	0	2585	--	--	16.08	16.08	0.10	0.05	0.01	0.07	0.00	0.00	20.9
8	27	-0	1384	0	0	0	2752	--	--	16.08	16.08	0.10	0.05	0.01	0.09	0.00	0.00	20.9
9	27	-0	1270	0	0	0	2654	--	--	16.08	16.08	0.10	0.05	0.01	0.08	0.00	0.00	20.9
10	27	-0	1180	0	0	0	2569	--	--	16.08	16.08	0.10	0.05	0.01	0.07	0.00	0.00	20.9
11	27	-0	1145	0	0	0	2539	--	--	16.08	16.08	0.10	0.05	0.01	0.07	0.00	0.00	20.9
12	27	-0	1433	0	0	0	2798	--	--	16.08	16.08	0.10	0.05	0.01	0.09	0.00	0.00	20.9
13	27	-0	1399	0	0	0	2769	--	--	16.08	16.08	0.10	0.05	0.01	0.09	0.00	0.00	20.9
14	27	-0	1308	0	0	0	2683	--	--	16.08	16.08	0.10	0.05	0.01	0.08	0.00	0.00	20.9
15	27	-0	1194	0	0	0	2585	--	--	16.08	16.08	0.10	0.05	0.01	0.07	0.00	0.00	20.9
16	27	-0	1384	0	0	0	2752	--	--	16.08	16.08	0.10	0.05	0.01	0.09	0.00	0.00	20.9
17	27	-0	1270	0	0	0	2654	--	--	16.08	16.08	0.10	0.05	0.01	0.08	0.00	0.00	20.9
18	27	-0	951	0	0	0	3447	--	--	16.08	16.08	0.00	0.06	0.01	0.06	0.00	0.00	20.9
19	27	-0	2145	0	0	0	4673	--	--	16.08	16.08	0.00	0.08	0.02	0.13	0.00	0.00	20.9
20	27	-0	1489	0	0	0	3963	--	--	16.08	16.08	0.00	0.07	0.01	0.09	0.00	0.00	20.9
37	27	-0	599	0	0	0	2851	--	--	16.08	16.08	0.00	0.05	0.00	0.04	0.00	0.00	20.9
38	27	-0	2588	0	0	0	4895	--	--	16.08	16.08	0.00	0.08	0.02	0.16	0.00	0.00	20.9
39	27	-0	1495	0	0	0	3711	--	--	16.08	16.08	0.00	0.06	0.01	0.09	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	1676	0	0	0	2135	--	--	16.08	16.08	0.00	0.04	0.01	0.11	0.00	0.00	20.9
2	55	-0	1180	0	0	0	1630	--	--	16.08	16.08	0.10	0.03	0.01	0.07	0.00	0.00	20.9
3	55	-0	1145	0	0	0	1628	--	--	16.08	16.08	0.10	0.03	0.01	0.07	0.00	0.00	20.9
4	55	-0	1433	0	0	0	1657	--	--	16.08	16.08	0.10	0.03	0.01	0.09	0.00	0.00	20.9
5	55	-0	1399	0	0	0	1655	--	--	16.08	16.08	0.10	0.03	0.01	0.09	0.00	0.00	20.9
6	55	-0	1308	0	0	0	1642	--	--	16.08	16.08	0.10	0.03	0.01	0.08	0.00	0.00	20.9
7	55	-0	1194	0	0	0	1634	--	--	16.08	16.08	0.10	0.03	0.01	0.07	0.00	0.00	20.9
8	55	-0	1384	0	0	0	1650	--	--	16.08	16.08	0.10	0.03	0.01	0.09	0.00	0.00	20.9

9	55	-0	1270	0	0	0	1643	--	--	16.08	16.08	0.10	0.03	0.01	0.08	0.00	0.00	20.9
10	55	-0	1180	0	0	0	1630	--	--	16.08	16.08	0.10	0.03	0.01	0.07	0.00	0.00	20.9
11	55	-0	1145	0	0	0	1628	--	--	16.08	16.08	0.10	0.03	0.01	0.07	0.00	0.00	20.9
12	55	-0	1433	0	0	0	1657	--	--	16.08	16.08	0.10	0.03	0.01	0.09	0.00	0.00	20.9
13	55	-0	1399	0	0	0	1655	--	--	16.08	16.08	0.10	0.03	0.01	0.09	0.00	0.00	20.9
14	55	-0	1308	0	0	0	1642	--	--	16.08	16.08	0.10	0.03	0.01	0.08	0.00	0.00	20.9
15	55	-0	1194	0	0	0	1634	--	--	16.08	16.08	0.10	0.03	0.01	0.07	0.00	0.00	20.9
16	55	-0	1384	0	0	0	1650	--	--	16.08	16.08	0.10	0.03	0.01	0.09	0.00	0.00	20.9
17	55	-0	1270	0	0	0	1643	--	--	16.08	16.08	0.10	0.03	0.01	0.08	0.00	0.00	20.9
18	55	-0	951	0	0	0	2690	--	--	16.08	16.08	0.00	0.05	0.01	0.06	0.00	0.00	20.9
19	55	-0	2145	0	0	0	2966	--	--	16.08	16.08	0.00	0.05	0.02	0.13	0.00	0.00	20.9
20	55	-0	1489	0	0	0	2778	--	--	16.08	16.08	0.00	0.05	0.01	0.09	0.00	0.00	20.9
37	55	-0	599	0	0	0	2375	--	--	16.08	16.08	0.00	0.04	0.00	0.04	0.00	0.00	20.9
38	55	-0	2588	0	0	0	2835	--	--	16.08	16.08	0.00	0.05	0.02	0.16	0.00	0.00	20.9
39	55	-0	1495	0	0	0	2521	--	--	16.08	16.08	0.00	0.04	0.01	0.09	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 186 NI 1635 NF 1762 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	4959	0	0	0	211	--	--	16.08	16.08	0.00	0.00	0.04	0.31	0.00	0.00	20.9
2	0	-0	3999	0	0	0	177	--	--	16.08	16.08	0.10	0.00	0.03	0.25	0.00	0.00	20.9
3	0	-0	4000	0	0	0	182	--	--	16.08	16.08	0.10	0.00	0.03	0.25	0.00	0.00	20.9
4	0	-0	3629	0	0	0	142	--	--	16.08	16.08	0.10	0.00	0.03	0.23	0.00	0.00	20.9
5	0	-0	3630	0	0	0	147	--	--	16.08	16.08	0.10	0.00	0.03	0.23	0.00	0.00	20.9
6	0	-0	3869	0	0	0	160	--	--	16.08	16.08	0.10	0.00	0.03	0.24	0.00	0.00	20.9
7	0	-0	3871	0	0	0	175	--	--	16.08	16.08	0.10	0.00	0.03	0.24	0.00	0.00	20.9
8	0	-0	3758	0	0	0	149	--	--	16.08	16.08	0.10	0.00	0.03	0.24	0.00	0.00	20.9
9	0	-0	3760	0	0	0	165	--	--	16.08	16.08	0.10	0.00	0.03	0.24	0.00	0.00	20.9
10	0	-0	3999	0	0	0	177	--	--	16.08	16.08	0.10	0.00	0.03	0.25	0.00	0.00	20.9
11	0	-0	4000	0	0	0	182	--	--	16.08	16.08	0.10	0.00	0.03	0.25	0.00	0.00	20.9
12	0	-0	3629	0	0	0	142	--	--	16.08	16.08	0.10	0.00	0.03	0.23	0.00	0.00	20.9
13	0	-0	3630	0	0	0	147	--	--	16.08	16.08	0.10	0.00	0.03	0.23	0.00	0.00	20.9
14	0	-0	3869	0	0	0	160	--	--	16.08	16.08	0.10	0.00	0.03	0.24	0.00	0.00	20.9
15	0	-0	3871	0	0	0	175	--	--	16.08	16.08	0.10	0.00	0.03	0.24	0.00	0.00	20.9
16	0	-0	3758	0	0	0	149	--	--	16.08	16.08	0.10	0.00	0.03	0.24	0.00	0.00	20.9
17	0	-0	3760	0	0	0	165	--	--	16.08	16.08	0.10	0.00	0.03	0.24	0.00	0.00	20.9
18	0	-0	7989	0	0	0	550	--	--	16.08	16.08	0.00	0.01	0.07	0.50	0.00	0.00	20.9
19	0	-0	6746	0	0	0	415	--	--	16.08	16.08	0.00	0.01	0.06	0.42	0.00	0.00	20.9
20	0	-0	7070	0	0	0	489	--	--	16.08	16.08	0.00	0.01	0.06	0.44	0.00	0.00	20.9
37	0	-0	7622	0	0	0	507	--	--	16.08	16.08	0.00	0.01	0.06	0.48	0.00	0.00	20.9
38	0	-0	5551	0	0	0	281	--	--	16.08	16.08	0.00	0.00	0.05	0.35	0.00	0.00	20.9
39	0	-0	6091	0	0	0	404	--	--	16.08	16.08	0.00	0.01	0.05	0.38	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	4959	0	0	0	6863	--	--	16.08	16.08	0.00	0.12	0.04	0.31	0.00	0.00	20.9
2	27	-0	3999	0	0	0	5542	--	--	16.08	16.08	0.10	0.10	0.03	0.25	0.00	0.00	20.9
3	27	-0	4000	0	0	0	5548	--	--	16.08	16.08	0.10	0.10	0.03	0.25	0.00	0.00	20.9
4	27	-0	3629	0	0	0	5010	--	--	16.08	16.08	0.10	0.09	0.03	0.23	0.00	0.00	20.9
5	27	-0	3630	0	0	0	5017	--	--	16.08	16.08	0.10	0.09	0.03	0.23	0.00	0.00	20.9
6	27	-0	3869	0	0	0	5350	--	--	16.08	16.08	0.10	0.09	0.03	0.24	0.00	0.00	20.9
7	27	-0	3871	0	0	0	5368	--	--	16.08	16.08	0.10	0.10	0.03	0.24	0.00	0.00	20.9
8	27	-0	3758	0	0	0	5190	--	--	16.08	16.08	0.10	0.09	0.03	0.24	0.00	0.00	20.9
9	27	-0	3760	0	0	0	5208	--	--	16.08	16.08	0.10	0.09	0.03	0.24	0.00	0.00	20.9
10	27	-0	3999	0	0	0	5542	--	--	16.08	16.08	0.10	0.10	0.03	0.25	0.00	0.00	20.9
11	27	-0	4000	0	0	0	5548	--	--	16.08	16.08	0.10	0.10	0.03	0.25	0.00	0.00	20.9
12	27	-0	3629	0	0	0	5010	--	--	16.08	16.08	0.10	0.09	0.03	0.23	0.00	0.00	20.9
13	27	-0	3630	0	0	0	5017	--	--	16.08	16.08	0.10	0.09	0.03	0.23	0.00	0.00	20.9
14	27	-0	3869	0	0	0	5350	--	--	16.08	16.08	0.10	0.09	0.03	0.24	0.00	0.00	20.9
15	27	-0	3871	0	0	0	5368	--	--	16.08	16.08	0.10	0.10	0.03	0.24	0.00	0.00	20.9
16	27	-0	3758	0	0	0	5190	--	--	16.08	16.08	0.10	0.09	0.03	0.24	0.00	0.00	20.9
17	27	-0	3760	0	0	0	5208	--	--	16.08	16.08	0.10	0.09	0.03	0.24	0.00	0.00	20.9
18	27	-0	7989	0	0	0	11267	--	--	16.08	16.08	0.00	0.19	0.07	0.50	0.00	0.00	20.9
19	27	-0	6746	0	0	0	9464	--	--	16.08	16.08	0.00	0.16	0.06	0.42	0.00	0.00	20.9
20	27	-0	7070	0	0	0	9973	--	--	16.08	16.08	0.00	0.17	0.06	0.44	0.00	0.00	20.9
37	27	-0	7622	0	0	0	10731	--	--	16.08	16.08	0.00	0.18	0.06	0.48	0.00	0.00	20.9
38	27	-0	5551	0	0	0	7727	--	--	16.08	16.08	0.00	0.13	0.05	0.35	0.00	0.00	20.9
39	27	-0	6091	0	0	0	8575	--	--	16.08	16.08	0.00	0.15	0.05	0.38	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	4959	0	0	0	2915	--	--	16.08	16.08	0.00	0.05	0.04	0.31	0.00	0.00	20.9
2	55	-0	3999	0	0	0	2359	--	--	16.08	16.08	0.10	0.04	0.03	0.25	0.00	0.00	20.9
3	55	-0	4000	0	0	0	2364	--	--	16.08	16.08	0.10	0.04	0.03	0.25	0.00	0.00	20.9
4	55	-0	3629	0	0	0	2121	--	--	16.08	16.08	0.10	0.04	0.03	0.23	0.00	0.00	20.9
5	55	-0	3630	0	0	0	2127	--	--	16.08	16.08	0.10	0.04	0.03	0.23	0.00	0.00	20.9
6	55	-0	3869	0	0	0	2270	--	--	16.08	16.08	0.10	0.04	0.03	0.24	0.00	0.00	20.9
7	55	-0	3871	0	0	0	2287	--	--	16.08	16.08	0.10	0.04	0.03	0.24	0.00	0.00	20.9
8	55	-0	3758	0	0	0	2198	--	--	16.08	16.08	0.10	0.04	0.03	0.24	0.00	0.00	20.9
9	55	-0	3760	0	0	0	2215	--	--	16.08	16.08	0.10	0.04	0.03	0.24	0.00	0.00	20.9
10	55	-0	3999	0	0	0	2359	--	--	16.08	16.08	0.10	0.04	0.03	0.25	0.00	0.00	20.9
11	55	-0	4000	0	0	0	2364	--	--	16.08	16.08	0.10	0.04	0.03	0.25	0.00	0.00	20.9
12	55	-0	3629	0	0	0	2121	--	--	16.08	16.08	0.10	0.04	0.03	0.23	0.00	0.00	20.9
13	55	-0	3630	0	0	0	2127	--	--	16.08	16.08	0.10	0.04	0.03	0.23	0.00	0.00	20.9
14	55	-0	3869	0	0	0	2270	--	--	16.08	16.08	0.10	0.04	0.03	0.24	0.00	0.00	20.9
15	55	-0	3871	0	0	0	2287	--	--	16.08	16.08	0.10	0.04	0.03	0.24	0.00	0.00	20.9
16	55	-0	3758	0	0	0	2198	--	--	16.08	16.08	0.10	0.04	0.03	0.24	0.00	0.00	20.9
17	55	-0	3760	0	0	0	2215	--	--	16.08	16.08	0.10	0.04	0.03	0.24	0.00	0.00	20.9
18	55	-0	7989	0	0	0	4907	--	--	16.08	16.08	0.00	0.08	0.07	0.50	0.00	0.00	20.9
19	55	-0	6746	0	0	0	4094	--	--	16.08	16.08	0.00	0.07	0.06	0.42	0.00	0.00	20.9
20	55	-0	7070	0	0	0	4345	--	--	16.08	16.08	0.00	0.07	0.06	0.44	0.00	0.00	20.9
37	55	-0	7622	0	0	0	4664	--	--	16.08	16.08	0.00	0.08	0.06	0.48	0.00	0.00	20.9
38	55	-0	5551	0	0	0	3308	--	--	16.08	16.08	0.00	0.06	0.05	0.35	0.00	0.00	20.9
39	55	-0	6091	0	0	0	3726	--	--	16.08	16.08	0.00	0.06	0.05	0.38	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 187 NI 1636 NF 1635 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	4390	0	0	0	-413	--	--	16.08	16.08	0.18	0.01	0.04	0.28	0.00	0.00	20.9
2	0	-0	3558	0	0	0	-326	--	--	16.08	16.08	0.29	0.01	0.03	0.22	0.00	0.00	20.9
3	0	-0	3598	0	0	0	-323	--	--	16.08	16.08	0.29	0.01	0.03	0.23	0.00	0.00	20.9
4	0	-0	3155	0	0	0	-313	--	--	16.08	16.08	0.29	0.01	0.03	0.20	0.00	0.00	20.9
5	0	-0	3195	0	0	0	-310	--	--	16.08	16.08	0.29	0.01	0.03	0.20	0.00	0.00	20.9
6	0	-0	3370	0	0	0	-325	--	--	16.08	16.08	0.29	0.01	0.03	0.21	0.00	0.00	20.9
7	0	-0	3505	0	0	0	-315	--	--	16.08	16.08	0.29	0.01	0.03	0.22	0.00	0.00	20.9
8	0	-0	3249	0	0	0	-321	--	--	16.08	16.08	0.29	0.01	0.03	0.20	0.00	0.00	20.9
9	0	-0	3384	0	0	0	-311	--	--	16.08	16.08	0.29	0.01	0.03	0.21	0.00	0.00	20.9
10	0	-0	3558	0	0	0	-326	--	--	16.08	16.08	0.29	0.01	0.03	0.22	0.00	0.00	20.9
11	0	-0	3598	0	0	0	-323	--	--	16.08	16.08	0.29	0.01	0.03	0.23	0.00	0.00	20.9
12	0	-0	3155	0	0	0	-313	--	--	16.08	16.08	0.29	0.01	0.03	0.20	0.00	0.00	20.9
13	0	-0	3195	0	0	0	-310	--	--	16.08	16.08	0.29	0.01	0.03	0.20	0.00	0.00	20.9
14	0	-0	3370	0	0	0	-325	--	--	16.08	16.08	0.29	0.01	0.03	0.21	0.00	0.00	20.9
15	0	-0	3505	0	0	0	-315	--	--	16.08	16.08	0.29	0.01	0.03	0.22	0.00	0.00	20.9
16	0	-0	3249	0	0	0	-321	--	--	16.08	16.08	0.29	0.01	0.03	0.20	0.00	0.00	20.9
17	0	-0	3384	0	0	0	-311	--	--	16.08	16.08	0.29	0.01	0.03	0.21	0.00	0.00	20.9
18	0	-0	7355	0	0	0	-460	--	--	16.08	16.08	0.18	0.01	0.06	0.46	0.00	0.00	20.9
19	0	-0	5954	0	0	0	-425	--	--	16.08	16.08	0.18	0.01	0.05	0.37	0.00	0.00	20.9
20	0	-0	6525	0	0	0	-414	--	--	16.08	16.08	0.18	0.01	0.05	0.41	0.00	0.00	20.9
37	0	-0	7087	0	0	0	-464	--	--	16.08	16.08	0.18	0.01	0.06	0.44	0.00	0.00	20.9
38	0	-0	4753	0	0	0	-404	--	--	16.08	16.08	0.18	0.01	0.04	0.30	0.00	0.00	20.9
39	0	-0	5704	0	0	0	-387	--	--	16.08	16.08	0.18	0.01	0.05	0.36	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	4390	0	0	0	5476	--	--	16.08	16.08	0.00	0.09	0.04	0.28	0.00	0.00	20.9
2	27	-0	3558	0	0	0	4447	--	--	16.08	16.08	0.10	0.08	0.03	0.22	0.00	0.00	20.9
3	27	-0	3598	0	0	0	4504	--	--	16.08	16.08	0.10	0.08	0.03	0.23	0.00	0.00	20.9
4	27	-0	3155	0	0	0	3920	--	--	16.08	16.08	0.10	0.07	0.03	0.20	0.00	0.00	20.9
5	27	-0	3195	0	0	0	3976	--	--	16.08	16.08	0.10	0.07	0.03	0.20	0.00	0.00	20.9
6	27	-0	3370	0	0	0	4196	--	--	16.08	16.08	0.10	0.07	0.03	0.21	0.00	0.00	20.9
7	27	-0	3505	0	0	0	4387	--	--	16.08	16.08	0.10	0.08	0.03	0.22	0.00	0.00	20.9
8	27	-0	3249	0	0	0	4038	--	--	16.08	16.08	0.10	0.07	0.03	0.20	0.00	0.00	20.9
9	27	-0	3384	0	0	0	4228	--	--	16.08	16.08	0.10	0.08	0.03	0.21	0.00	0.00	20.9
10	27	-0	3558	0	0	0	4447	--	--	16.08	16.08	0.10	0.08	0.03	0.22	0.00	0.00	20.9
11	27	-0	3598	0	0	0	4504	--	--	16.08	16.08	0.10	0.08	0.03	0.23	0.00	0.00	20.9
12	27	-0	3155	0	0	0	3920	--	--	16.08	16.08	0.10	0.07	0.03	0.20	0.00	0.00	20.9
13	27	-0	3195	0	0	0	3976	--	--	16.08	16.08	0.10	0.07	0.03	0.20	0.00	0.00	20.9
14	27	-0	3370	0	0	0	4196	--	--	16.08	16.08	0.10	0.07	0.03	0.21	0.00	0.00	20.9
15	27	-0	3505	0	0	0	4387	--	--	16.08	16.08	0.10	0.08	0.03	0.22	0.00	0.00	20.9
16	27	-0	3249	0	0	0	4038	--	--	16.08	16.08	0.10	0.07	0.03	0.20	0.00	0.00	20.9
17	27	-0	3384	0	0	0	4228	--	--	16.08	16.08	0.10	0.08	0.03	0.21	0.00	0.00	20.9
18	27	-0	7355	0	0	0	9406	--	--	16.08	16.08	0.00	0.16	0.06	0.46	0.00	0.00	20.9
19	27	-0	5954	0	0	0	7562	--	--	16.08	16.08	0.00	0.13	0.05	0.37	0.00	0.00	20.9
20	27	-0	6525	0	0	0	8339	--	--	16.08	16.08	0.00	0.14	0.05	0.41	0.00	0.00	20.9
37	27	-0	7087	0	0	0	9043	--	--	16.08	16.08	0.00	0.15	0.06	0.44	0.00	0.00	20.9
38	27	-0	4753	0	0	0	5972	--	--	16.08	16.08	0.00	0.10	0.04	0.30	0.00	0.00	20.9
39	27	-0	5704	0	0	0	7265	--	--	16.08	16.08	0.00	0.12	0.05	0.36	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	4390	0	0	0	1981	--	--	16.08	16.08	0.00	0.03	0.04	0.28	0.00	0.00	20.9
2	55	-0	3558	0	0	0	1615	--	--	16.08	16.08	0.10	0.03	0.03	0.22	0.00	0.00	20.9
3	55	-0	3598	0	0	0	1640	--	--	16.08	16.08	0.10	0.03	0.03	0.23	0.00	0.00	20.9
4	55	-0	3155	0	0	0	1408	--	--	16.08	16.08	0.10	0.02	0.03	0.20	0.00	0.00	20.9
5	55	-0	3195	0	0	0	1433	--	--	16.08	16.08	0.10	0.03	0.03	0.20	0.00	0.00	20.9
6	55	-0	3370	0	0	0	1513	--	--	16.08	16.08	0.10	0.03	0.03	0.21	0.00	0.00	20.9
7	55	-0	3505	0	0	0	1597	--	--	16.08	16.08	0.10	0.03	0.03	0.22	0.00	0.00	20.9
8	55	-0	3249	0	0	0	1451	--	--	16.08	16.08	0.10	0.03	0.03	0.20	0.00	0.00	20.9
9	55	-0	3384	0	0	0	1535	--	--	16.08	16.08	0.10	0.03	0.03	0.21	0.00	0.00	20.9
10	55	-0	3558	0	0	0	1615	--	--	16.08	16.08	0.10	0.03	0.03	0.22	0.00	0.00	20.9
11	55	-0	3598	0	0	0	1640	--	--	16.08	16.08	0.10	0.03	0.03	0.23	0.00	0.00	20.9
12	55	-0	3155	0	0	0	1408	--	--	16.08	16.08	0.10	0.02	0.03	0.20	0.00	0.00	20.9
13	55	-0	3195	0	0	0	1433	--	--	16.08	16.08	0.10	0.03	0.03	0.20	0.00	0.00	20.9
14	55	-0	3370	0	0	0	1513	--	--	16.08	16.08	0.10	0.03	0.03	0.21	0.00	0.00	20.9
15	55	-0	3505	0	0	0	1597	--	--	16.08	16.08	0.10	0.03	0.03	0.22	0.00	0.00	20.9
16	55	-0	3249	0	0	0	1451	--	--	16.08	16.08	0.10	0.03	0.03	0.20	0.00	0.00	20.9
17	55	-0	3384	0	0	0	1535	--	--	16.08	16.08	0.10	0.03	0.03	0.21	0.00	0.00	20.9
18	55	-0	7355	0	0	0	3551	--	--	16.08	16.08	0.00	0.06	0.06	0.46	0.00	0.00	20.9
19	55	-0	5954	0	0	0	2823	--	--	16.08	16.08	0.00	0.05	0.05	0.37	0.00	0.00	20.9
20	55	-0	6525	0	0	0	3145	--	--	16.08	16.08	0.00	0.05	0.05	0.41	0.00	0.00	20.9
37	55	-0	7087	0	0	0	3402	--	--	16.08	16.08	0.00	0.06	0.06	0.44	0.00	0.00	20.9
38	55	-0	4753	0	0	0	2189	--	--	16.08	16.08	0.00	0.04	0.04	0.30	0.00	0.00	20.9
39	55	-0	5704	0	0	0	2725	--	--	16.08	16.08	0.00	0.05	0.05	0.36	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 188 NI 1576 NF 1636 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	2755	0	0	0	-847	--	--	16.08	16.08	0.18	0.01	0.02	0.17	0.00	0.00	20.9
2	0	-0	2232	0	0	0	-681	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
3	0	-0	2283	0	0	0	-687	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
4	0	-0	1955	0	0	0	-616	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
5	0	-0	2006	0	0	0	-621	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
6	0	-0	2075	0	0	0	-652	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
7	0	-0	2246	0	0	0	-670	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
8	0	-0	1992	0	0	0	-632	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
9	0	-0	2163	0	0	0	-651	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
10	0	-0	2232	0	0	0	-681	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
11	0	-0	2283	0	0	0	-687	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
12	0	-0	1955	0	0	0	-616	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
13	0	-0	2006	0	0	0	-621	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
14	0	-0	2075	0	0	0	-652	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
15	0	-0	2246	0	0	0	-670	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
16	0	-0	1992	0	0	0	-632	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9

17	0	-0	2163	0	0	0	-651	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
18	0	-0	4671	0	0	0	-1238	--	--	16.08	16.08	0.18	0.02	0.04	0.29	0.00	0.00	20.9
19	0	-0	3682	0	0	0	-1005	--	--	16.08	16.08	0.18	0.02	0.03	0.23	0.00	0.00	20.9
20	0	-0	4225	0	0	0	-1104	--	--	16.08	16.08	0.18	0.02	0.03	0.27	0.00	0.00	20.9
37	0	-0	4539	0	0	0	-1227	--	--	16.08	16.08	0.18	0.02	0.04	0.28	0.00	0.00	20.9
38	0	-0	2892	0	0	0	-839	--	--	16.08	16.08	0.18	0.01	0.02	0.18	0.00	0.00	20.9
39	0	-0	3796	0	0	0	-1005	--	--	16.08	16.08	0.18	0.02	0.03	0.24	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	2755	0	0	0	-847	--	--	16.08	16.08	0.18	0.01	0.02	0.17	0.00	0.00	20.9
2	27	-0	2232	0	0	0	-681	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
3	27	-0	2283	0	0	0	-687	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
4	27	-0	1955	0	0	0	-616	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
5	27	-0	2006	0	0	0	-621	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
6	27	-0	2075	0	0	0	-652	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
7	27	-0	2246	0	0	0	-670	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
8	27	-0	1992	0	0	0	-632	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
9	27	-0	2163	0	0	0	-651	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
10	27	-0	2232	0	0	0	-681	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
11	27	-0	2283	0	0	0	-687	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
12	27	-0	1955	0	0	0	-616	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
13	27	-0	2006	0	0	0	-621	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
14	27	-0	2075	0	0	0	-652	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
15	27	-0	2246	0	0	0	-670	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
16	27	-0	1992	0	0	0	-632	--	--	16.08	16.08	0.29	0.01	0.02	0.12	0.00	0.00	20.9
17	27	-0	2163	0	0	0	-651	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
18	27	-0	4671	0	0	0	5028	--	--	16.08	16.08	0.00	0.09	0.04	0.29	0.00	0.00	20.9
19	27	-0	3682	0	0	0	-1005	--	--	16.08	16.08	0.18	0.02	0.03	0.23	0.00	0.00	20.9
20	27	-0	4225	0	0	0	4563	--	--	16.08	16.08	0.00	0.08	0.03	0.27	0.00	0.00	20.9
37	27	-0	4539	0	0	0	4862	--	--	16.08	16.08	0.00	0.08	0.04	0.28	0.00	0.00	20.9
38	27	-0	2892	0	0	0	-839	--	--	16.08	16.08	0.18	0.01	0.02	0.18	0.00	0.00	20.9
39	27	-0	3796	0	0	0	4087	--	--	16.08	16.08	0.00	0.07	0.03	0.24	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	2755	0	0	0	656	--	--	16.08	16.08	0.00	0.01	0.02	0.17	0.00	0.00	20.9
2	55	-0	2232	0	0	0	536	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
3	55	-0	2283	0	0	0	558	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
4	55	-0	1955	0	0	0	451	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
5	55	-0	2006	0	0	0	473	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
6	55	-0	2075	0	0	0	480	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
7	55	-0	2246	0	0	0	555	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
8	55	-0	1992	0	0	0	454	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
9	55	-0	2163	0	0	0	529	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
10	55	-0	2232	0	0	0	536	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
11	55	-0	2283	0	0	0	558	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
12	55	-0	1955	0	0	0	451	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
13	55	-0	2006	0	0	0	473	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
14	55	-0	2075	0	0	0	480	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
15	55	-0	2246	0	0	0	555	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
16	55	-0	1992	0	0	0	454	--	--	16.08	16.08	0.10	0.01	0.02	0.12	0.00	0.00	20.9
17	55	-0	2163	0	0	0	529	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
18	55	-0	4671	0	0	0	1310	--	--	16.08	16.08	0.00	0.02	0.04	0.29	0.00	0.00	20.9
19	55	-0	3682	0	0	0	1003	--	--	16.08	16.08	0.00	0.02	0.03	0.23	0.00	0.00	20.9
20	55	-0	4225	0	0	0	1200	--	--	16.08	16.08	0.00	0.02	0.03	0.27	0.00	0.00	20.9
37	55	-0	4539	0	0	0	1249	--	--	16.08	16.08	0.00	0.02	0.04	0.28	0.00	0.00	20.9
38	55	-0	2892	0	0	0	738	--	--	16.08	16.08	0.00	0.01	0.02	0.18	0.00	0.00	20.9
39	55	-0	3796	0	0	0	1066	--	--	16.08	16.08	0.00	0.02	0.03	0.24	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 189 NI 1658 NF 1576 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	1433	0	0	0	-955	--	--	16.08	16.08	0.18	0.02	0.01	0.09	0.00	0.00	20.9
2	0	-0	1169	0	0	0	-773	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
3	0	-0	1224	0	0	0	-789	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
4	0	-0	981	0	0	0	-680	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
5	0	-0	1035	0	0	0	-696	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
6	0	-0	1040	0	0	0	-722	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
7	0	-0	1221	0	0	0	-775	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
8	0	-0	983	0	0	0	-693	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
9	0	-0	1165	0	0	0	-747	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
10	0	-0	1169	0	0	0	-773	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
11	0	-0	1224	0	0	0	-789	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
12	0	-0	981	0	0	0	-680	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
13	0	-0	1035	0	0	0	-696	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
14	0	-0	1040	0	0	0	-722	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
15	0	-0	1221	0	0	0	-775	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
16	0	-0	983	0	0	0	-693	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
17	0	-0	1165	0	0	0	-747	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
18	0	-0	2580	0	0	0	-1483	--	--	16.08	16.08	0.18	0.02	0.02	0.16	0.00	0.00	20.9
19	0	-0	1859	0	0	0	-1133	--	--	16.08	16.08	0.18	0.02	0.02	0.12	0.00	0.00	20.9
20	0	-0	2396	0	0	0	-1339	--	--	16.08	16.08	0.18	0.02	0.02	0.15	0.00	0.00	20.9
37	0	-0	2565	0	0	0	-1486	--	--	16.08	16.08	0.18	0.02	0.02	0.16	0.00	0.00	20.9
38	0	-0	1364	0	0	0	-903	--	--	16.08	16.08	0.18	0.01	0.01	0.09	0.00	0.00	20.9
39	0	-0	2258	0	0	0	-1246	--	--	16.08	16.08	0.18	0.02	0.02	0.14	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	1433	0	0	0	-955	--	--	16.08	16.08	0.18	0.02	0.01	0.09	0.00	0.00	20.9
2	27	-0	1169	0	0	0	-773	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
3	27	-0	1224	0	0	0	-789	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
4	27	-0	981	0	0	0	-680	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
5	27	-0	1035	0	0	0	-696	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
6	27	-0	1040	0	0	0	-722	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
7	27	-0	1221	0	0	0	-775	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
8	27	-0	983	0	0	0	-693	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
9	27	-0	1165	0	0	0	-747	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
10	27	-0	1169	0	0	0	-773	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
11	27	-0	1224	0	0	0	-789	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
12	27	-0	981	0	0	0	-680	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9

13	27	-0	1035	0	0	0	-696	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
14	27	-0	1040	0	0	0	-722	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
15	27	-0	1221	0	0	0	-775	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
16	27	-0	983	0	0	0	-693	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
17	27	-0	1165	0	0	0	-747	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
18	27	-0	2580	0	0	0	-1483	--	--	16.08	16.08	0.18	0.02	0.02	0.16	0.00	0.00	20.9
19	27	-0	1859	0	0	0	-1133	--	--	16.08	16.08	0.18	0.02	0.02	0.12	0.00	0.00	20.9
20	27	-0	2396	0	0	0	-1339	--	--	16.08	16.08	0.18	0.02	0.02	0.15	0.00	0.00	20.9
37	27	-0	2565	0	0	0	-1486	--	--	16.08	16.08	0.18	0.02	0.02	0.16	0.00	0.00	20.9
38	27	-0	1364	0	0	0	-903	--	--	16.08	16.08	0.18	0.01	0.01	0.09	0.00	0.00	20.9
39	27	-0	2258	0	0	0	-1246	--	--	16.08	16.08	0.18	0.02	0.02	0.14	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	1433	0	0	0	-955	--	--	16.08	16.08	0.18	0.02	0.01	0.09	0.00	0.00	20.9
2	55	-0	1169	0	0	0	-773	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
3	55	-0	1224	0	0	0	-789	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
4	55	-0	981	0	0	0	-680	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
5	55	-0	1035	0	0	0	-696	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
6	55	-0	1040	0	0	0	-722	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
7	55	-0	1221	0	0	0	-775	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
8	55	-0	983	0	0	0	-693	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
9	55	-0	1165	0	0	0	-747	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
10	55	-0	1169	0	0	0	-773	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
11	55	-0	1224	0	0	0	-789	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
12	55	-0	981	0	0	0	-680	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
13	55	-0	1035	0	0	0	-696	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
14	55	-0	1040	0	0	0	-722	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
15	55	-0	1221	0	0	0	-775	--	--	16.08	16.08	0.29	0.01	0.01	0.08	0.00	0.00	20.9
16	55	-0	983	0	0	0	-693	--	--	16.08	16.08	0.29	0.01	0.01	0.06	0.00	0.00	20.9
17	55	-0	1165	0	0	0	-747	--	--	16.08	16.08	0.29	0.01	0.01	0.07	0.00	0.00	20.9
18	55	-0	2580	0	0	0	-1483	--	--	16.08	16.08	0.18	0.02	0.02	0.16	0.00	0.00	20.9
19	55	-0	1859	0	0	0	-1133	--	--	16.08	16.08	0.18	0.02	0.02	0.12	0.00	0.00	20.9
20	55	-0	2396	0	0	0	-1339	--	--	16.08	16.08	0.18	0.02	0.02	0.15	0.00	0.00	20.9
37	55	-0	2565	0	0	0	-1486	--	--	16.08	16.08	0.18	0.02	0.02	0.16	0.00	0.00	20.9
38	55	-0	1364	0	0	0	-903	--	--	16.08	16.08	0.18	0.01	0.01	0.09	0.00	0.00	20.9
39	55	-0	2258	0	0	0	-1246	--	--	16.08	16.08	0.18	0.02	0.02	0.14	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 190 NI 1761 NF 1658 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	267	0	0	0	-812	--	--	16.08	16.08	0.18	0.01	0.00	0.02	0.00	0.00	20.9
2	0	-0	236	0	0	0	-664	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
3	0	-0	294	0	0	0	-691	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
4	0	-0	117	0	0	0	-558	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
5	0	-0	175	0	0	0	-586	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
6	0	-0	127	0	0	0	-594	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
7	0	-0	320	0	0	0	-687	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
8	0	-0	91	0	0	0	-563	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
9	0	-0	284	0	0	0	-655	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
10	0	-0	236	0	0	0	-664	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
11	0	-0	294	0	0	0	-691	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
12	0	-0	117	0	0	0	-558	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
13	0	-0	175	0	0	0	-586	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
14	0	-0	127	0	0	0	-594	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
15	0	-0	320	0	0	0	-687	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
16	0	-0	91	0	0	0	-563	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
17	0	-0	284	0	0	0	-655	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
18	0	-0	779	0	0	0	-1336	--	--	16.08	16.08	0.18	0.02	0.01	0.05	0.00	0.00	20.9
19	0	-0	256	0	0	0	-917	--	--	16.08	16.08	0.18	0.02	0.00	0.02	0.00	0.00	20.9
20	0	-0	810	0	0	0	-1231	--	--	16.08	16.08	0.18	0.02	0.01	0.05	0.00	0.00	20.9
37	0	-0	872	0	0	0	-1374	--	--	16.08	16.08	0.18	0.02	0.01	0.05	0.00	0.00	20.9
38	0	-0	1	0	0	0	-676	--	--	16.08	16.08	0.18	0.01	0.00	0.00	0.00	0.00	20.9
39	0	-0	923	0	0	0	-1201	--	--	16.08	16.08	0.18	0.02	0.01	0.06	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	267	0	0	0	-812	--	--	16.08	16.08	0.18	0.01	0.00	0.02	0.00	0.00	20.9
2	27	-0	236	0	0	0	-664	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
3	27	-0	294	0	0	0	-691	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
4	27	-0	117	0	0	0	-558	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
5	27	-0	175	0	0	0	-586	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
6	27	-0	127	0	0	0	-594	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
7	27	-0	320	0	0	0	-687	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
8	27	-0	91	0	0	0	-563	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
9	27	-0	284	0	0	0	-655	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
10	27	-0	236	0	0	0	-664	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
11	27	-0	294	0	0	0	-691	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
12	27	-0	117	0	0	0	-558	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
13	27	-0	175	0	0	0	-586	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
14	27	-0	127	0	0	0	-594	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
15	27	-0	320	0	0	0	-687	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
16	27	-0	91	0	0	0	-563	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
17	27	-0	284	0	0	0	-655	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
18	27	-0	779	0	0	0	-1336	--	--	16.08	16.08	0.18	0.02	0.01	0.05	0.00	0.00	20.9
19	27	-0	256	0	0	0	-917	--	--	16.08	16.08	0.18	0.02	0.00	0.02	0.00	0.00	20.9
20	27	-0	810	0	0	0	-1231	--	--	16.08	16.08	0.18	0.02	0.01	0.05	0.00	0.00	20.9
37	27	-0	872	0	0	0	-1374	--	--	16.08	16.08	0.18	0.02	0.01	0.05	0.00	0.00	20.9
38	27	-0	1	0	0	0	-676	--	--	16.08	16.08	0.18	0.01	0.00	0.00	0.00	0.00	20.9
39	27	-0	923	0	0	0	-1201	--	--	16.08	16.08	0.18	0.02	0.01	0.06	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	267	0	0	0	-812	--	--	16.08	16.08	0.18	0.01	0.00	0.02	0.00	0.00	20.9
2	55	-0	236	0	0	0	-664	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
3	55	-0	294	0	0	0	-691	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
4	55	-0	117	0	0	0	-558	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
5	55	-0	175	0	0	0	-586	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
6	55	-0	127	0	0	0	-594	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
7	55	-0	320	0	0	0	-687	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
8	55	-0	91	0	0	0	-563	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9

9	55	-0	284	0	0	0	-655	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
10	55	-0	236	0	0	0	-664	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
11	55	-0	294	0	0	0	-691	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
12	55	-0	117	0	0	0	-558	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
13	55	-0	175	0	0	0	-586	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
14	55	-0	127	0	0	0	-594	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
15	55	-0	320	0	0	0	-687	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
16	55	-0	91	0	0	0	-563	--	--	16.08	16.08	0.29	0.01	0.00	0.01	0.00	0.00	20.9
17	55	-0	284	0	0	0	-655	--	--	16.08	16.08	0.29	0.01	0.00	0.02	0.00	0.00	20.9
18	55	-0	779	0	0	0	-1336	--	--	16.08	16.08	0.18	0.02	0.01	0.05	0.00	0.00	20.9
19	55	-0	256	0	0	0	-917	--	--	16.08	16.08	0.18	0.02	0.00	0.02	0.00	0.00	20.9
20	55	-0	810	0	0	0	-1231	--	--	16.08	16.08	0.18	0.02	0.01	0.05	0.00	0.00	20.9
37	55	-0	872	0	0	0	-1374	--	--	16.08	16.08	0.18	0.02	0.01	0.05	0.00	0.00	20.9
38	55	-0	1	0	0	0	-676	--	--	16.08	16.08	0.18	0.01	0.00	0.00	0.00	0.00	20.9
39	55	-0	923	0	0	0	-1201	--	--	16.08	16.08	0.18	0.02	0.01	0.06	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 191 NI 1617 NF 1761 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice		resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m			cm
1	0	-0	-866	0	0	0	-901	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00		20.9
2	0	-0	-670	0	0	0	-726	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00		20.9
3	0	-0	-607	0	0	0	-733	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00		20.9
4	0	-0	-726	0	0	0	-654	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00		20.9
5	0	-0	-664	0	0	0	-660	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00		20.9
6	0	-0	-762	0	0	0	-694	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00		20.9
7	0	-0	-554	0	0	0	-715	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00		20.9
8	0	-0	-779	0	0	0	-672	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00		20.9
9	0	-0	-571	0	0	0	-693	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00		20.9
10	0	-0	-670	0	0	0	-726	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00		20.9
11	0	-0	-607	0	0	0	-733	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00		20.9
12	0	-0	-726	0	0	0	-654	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00		20.9
13	0	-0	-664	0	0	0	-660	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00		20.9
14	0	-0	-762	0	0	0	-694	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00		20.9
15	0	-0	-554	0	0	0	-715	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00		20.9
16	0	-0	-779	0	0	0	-672	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00		20.9
17	0	-0	-571	0	0	0	-693	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00		20.9
18	0	-0	-949	0	0	0	-1335	--	--	16.08	16.08	0.18	0.02	0.01	0.06	0.00	0.00		20.9
19	0	-0	-1299	0	0	0	-1077	--	--	16.08	16.08	0.18	0.02	0.01	0.08	0.00	0.00		20.9
20	0	-0	-714	0	0	0	-1187	--	--	16.08	16.08	0.18	0.02	0.01	0.04	0.00	0.00		20.9
37	0	-0	-750	0	0	0	-1323	--	--	16.08	16.08	0.18	0.02	0.01	0.05	0.00	0.00		20.9
38	0	-0	-1332	0	0	0	-894	--	--	16.08	16.08	0.18	0.01	0.01	0.08	0.00	0.00		20.9
39	0	-0	-358	0	0	0	-1076	--	--	16.08	16.08	0.18	0.02	0.00	0.02	0.00	0.00		20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-866	0	0	0	-901	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9
2	27	-0	-670	0	0	0	-726	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
3	27	-0	-607	0	0	0	-733	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
4	27	-0	-726	0	0	0	-654	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
5	27	-0	-664	0	0	0	-660	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
6	27	-0	-762	0	0	0	-694	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
7	27	-0	-554	0	0	0	-715	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
8	27	-0	-779	0	0	0	-672	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
9	27	-0	-571	0	0	0	-693	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
10	27	-0	-670	0	0	0	-726	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
11	27	-0	-607	0	0	0	-733	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
12	27	-0	-726	0	0	0	-654	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
13	27	-0	-664	0	0	0	-660	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
14	27	-0	-762	0	0	0	-694	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
15	27	-0	-554	0	0	0	-715	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
16	27	-0	-779	0	0	0	-672	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
17	27	-0	-571	0	0	0	-693	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
18	27	-0	-949	0	0	0	-1335	--	--	16.08	16.08	0.18	0.02	0.01	0.06	0.00	0.00	20.9
19	27	-0	-1299	0	0	0	-1077	--	--	16.08	16.08	0.18	0.02	0.01	0.08	0.00	0.00	20.9
20	27	-0	-714	0	0	0	-1187	--	--	16.08	16.08	0.18	0.02	0.01	0.04	0.00	0.00	20.9
37	27	-0	-750	0	0	0	-1323	--	--	16.08	16.08	0.18	0.02	0.01	0.05	0.00	0.00	20.9
38	27	-0	-1332	0	0	0	-894	--	--	16.08	16.08	0.18	0.01	0.01	0.08	0.00	0.00	20.9
39	27	-0	-358	0	0	0	-1076	--	--	16.08	16.08	0.18	0.02	0.00	0.02	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	-866	0	0	0	-901	--	--	16.08	16.08	0.18	0.01	0.01	0.05	0.00	0.00	20.9
2	55	-0	-670	0	0	0	-726	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
3	55	-0	-607	0	0	0	-733	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
4	55	-0	-726	0	0	0	-654	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
5	55	-0	-664	0	0	0	-660	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
6	55	-0	-762	0	0	0	-694	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
7	55	-0	-554	0	0	0	-715	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
8	55	-0	-779	0	0	0	-672	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
9	55	-0	-571	0	0	0	-693	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
10	55	-0	-670	0	0	0	-726	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
11	55	-0	-607	0	0	0	-733	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
12	55	-0	-726	0	0	0	-654	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
13	55	-0	-664	0	0	0	-660	--	--	16.08	16.08	0.29	0.01	0.01	0.04	0.00	0.00	20.9
14	55	-0	-762	0	0	0	-694	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
15	55	-0	-554	0	0	0	-715	--	--	16.08	16.08	0.29	0.01	0.00	0.03	0.00	0.00	20.9
16	55	-0	-779	0	0	0	-672	--	--	16.08	16.08	0.29	0.01	0.01	0.05	0.00	0.00	20.9
17	55	-0	-571	0	0	0	-693	--	--	16.08	16.08	0.29	0.01	0.00	0.04	0.00	0.00	20.9
18	55	-0	-949	0	0	0	-1335	--	--	16.08	16.08	0.18	0.02	0.01	0.06	0.00	0.00	20.9
19	55	-0	-1299	0	0	0	-1077	--	--	16.08	16.08	0.18	0.02	0.01	0.08	0.00	0.00	20.9
20	55	-0	-714	0	0	0	-1187	--	--	16.08	16.08	0.18	0.02	0.01	0.04	0.00	0.00	20.9
37	55	-0	-750	0	0	0	-1323	--	--	16.08	16.08	0.18	0.02	0.01	0.05	0.00	0.00	20.9
38	55	-0	-1332	0	0	0	-894	--	--	16.08	16.08	0.18	0.01	0.01	0.08	0.00	0.00	20.9
39	55	-0	-358	0	0	0	-1076	--	--	16.08	16.08	0.18	0.02	0.00	0.02	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 192 NI 1618 NF 1617 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice resistenza			aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-2087	0	0	0	252	--	--	16.08	16.08	0.00	0.00	0.02	0.13	0.00	0.00	20.9
2	0	-0	-1645	0	0	0	179	--	--	16.08	16.08	0.10	0.00	0.01	0.10	0.00	0.00	20.9
3	0	-0	-1577	0	0	0	125	--	--	16.08	16.08	0.10	0.00	0.01	0.10	0.00	0.00	20.9
4	0	-0	-1634	0	0	0	263	--	--	16.08	16.08	0.10	0.00	0.01	0.10	0.00	0.00	20.9
5	0	-0	-1566	0	0	0	209	--	--	16.08	16.08	0.10	0.00	0.01	0.10	0.00	0.00	20.9
6	0	-0	-1720	0	0	0	272	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
7	0	-0	-1494	0	0	0	91	--	--	16.08	16.08	0.10	0.00	0.01	0.09	0.00	0.00	20.9
8	0	-0	-1716	0	0	0	297	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
9	0	-0	-1491	0	0	0	116	--	--	16.08	16.08	0.10	0.00	0.01	0.09	0.00	0.00	20.9
10	0	-0	-1645	0	0	0	179	--	--	16.08	16.08	0.10	0.00	0.01	0.10	0.00	0.00	20.9
11	0	-0	-1577	0	0	0	125	--	--	16.08	16.08	0.10	0.00	0.01	0.10	0.00	0.00	20.9
12	0	-0	-1634	0	0	0	263	--	--	16.08	16.08	0.10	0.00	0.01	0.10	0.00	0.00	20.9
13	0	-0	-1566	0	0	0	209	--	--	16.08	16.08	0.10	0.00	0.01	0.10	0.00	0.00	20.9
14	0	-0	-1720	0	0	0	272	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
15	0	-0	-1494	0	0	0	91	--	--	16.08	16.08	0.10	0.00	0.01	0.09	0.00	0.00	20.9
16	0	-0	-1716	0	0	0	297	--	--	16.08	16.08	0.10	0.01	0.01	0.11	0.00	0.00	20.9
17	0	-0	-1491	0	0	0	116	--	--	16.08	16.08	0.10	0.00	0.01	0.09	0.00	0.00	20.9
18	0	-0	-2817	0	0	0	167	--	--	16.08	16.08	0.00	0.00	0.02	0.18	0.00	0.00	20.9
19	0	-0	-2971	0	0	0	586	--	--	16.08	16.08	0.00	0.01	0.02	0.19	0.00	0.00	20.9
20	0	-0	-2358	0	0	0	45	--	--	16.08	16.08	0.00	0.00	0.02	0.15	0.00	0.00	20.9
37	0	-0	-2504	0	0	0	-1380	--	--	16.08	16.08	0.18	0.02	0.02	0.16	0.00	0.00	20.9
38	0	-0	-2761	0	0	0	685	--	--	16.08	16.08	0.00	0.01	0.02	0.17	0.00	0.00	20.9
39	0	-0	-1739	0	0	0	-1166	--	--	16.08	16.08	0.18	0.02	0.01	0.11	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-2087	0	0	0	-886	--	--	16.08	16.08	0.18	0.01	0.02	0.13	0.00	0.00	20.9
2	27	-0	-1645	0	0	0	-718	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
3	27	-0	-1577	0	0	0	-735	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
4	27	-0	-1634	0	0	0	-628	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
5	27	-0	-1566	0	0	0	-645	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
6	27	-0	-1720	0	0	0	-666	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
7	27	-0	-1494	0	0	0	-724	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
8	27	-0	-1716	0	0	0	-639	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
9	27	-0	-1491	0	0	0	-697	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
10	27	-0	-1645	0	0	0	-718	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
11	27	-0	-1577	0	0	0	-735	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
12	27	-0	-1634	0	0	0	-628	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
13	27	-0	-1566	0	0	0	-645	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
14	27	-0	-1720	0	0	0	-666	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
15	27	-0	-1494	0	0	0	-724	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
16	27	-0	-1716	0	0	0	-639	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
17	27	-0	-1491	0	0	0	-697	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
18	27	-0	-2817	0	0	0	-1370	--	--	16.08	16.08	0.18	0.02	0.02	0.18	0.00	0.00	20.9
19	27	-0	-2971	0	0	0	-1035	--	--	16.08	16.08	0.18	0.02	0.02	0.19	0.00	0.00	20.9
20	27	-0	-2358	0	0	0	-1242	--	--	16.08	16.08	0.18	0.02	0.02	0.15	0.00	0.00	20.9
37	27	-0	-2504	0	0	0	-1380	--	--	16.08	16.08	0.18	0.02	0.02	0.16	0.00	0.00	20.9
38	27	-0	-2761	0	0	0	-821	--	--	16.08	16.08	0.18	0.01	0.02	0.17	0.00	0.00	20.9
39	27	-0	-1739	0	0	0	-1166	--	--	16.08	16.08	0.18	0.02	0.01	0.11	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	-2087	0	0	0	-886	--	--	16.08	16.08	0.18	0.01	0.02	0.13	0.00	0.00	20.9
2	55	-0	-1645	0	0	0	-718	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
3	55	-0	-1577	0	0	0	-735	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
4	55	-0	-1634	0	0	0	-628	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
5	55	-0	-1566	0	0	0	-645	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
6	55	-0	-1720	0	0	0	-666	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
7	55	-0	-1494	0	0	0	-724	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
8	55	-0	-1716	0	0	0	-639	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
9	55	-0	-1491	0	0	0	-697	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
10	55	-0	-1645	0	0	0	-718	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
11	55	-0	-1577	0	0	0	-735	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
12	55	-0	-1634	0	0	0	-628	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
13	55	-0	-1566	0	0	0	-645	--	--	16.08	16.08	0.29	0.01	0.01	0.10	0.00	0.00	20.9
14	55	-0	-1720	0	0	0	-666	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
15	55	-0	-1494	0	0	0	-724	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
16	55	-0	-1716	0	0	0	-639	--	--	16.08	16.08	0.29	0.01	0.01	0.11	0.00	0.00	20.9
17	55	-0	-1491	0	0	0	-697	--	--	16.08	16.08	0.29	0.01	0.01	0.09	0.00	0.00	20.9
18	55	-0	-2817	0	0	0	-1370	--	--	16.08	16.08	0.18	0.02	0.02	0.18	0.00	0.00	20.9
19	55	-0	-2971	0	0	0	-1035	--	--	16.08	16.08	0.18	0.02	0.02	0.19	0.00	0.00	20.9
20	55	-0	-2358	0	0	0	-1242	--	--	16.08	16.08	0.18	0.02	0.02	0.15	0.00	0.00	20.9
37	55	-0	-2504	0	0	0	-1380	--	--	16.08	16.08	0.18	0.02	0.02	0.16	0.00	0.00	20.9
38	55	-0	-2761	0	0	0	-821	--	--	16.08	16.08	0.18	0.01	0.02	0.17	0.00	0.00	20.9
39	55	-0	-1739	0	0	0	-1166	--	--	16.08	16.08	0.18	0.02	0.01	0.11	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 193 NI 1634 NF 1618 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice resistenza			aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-3526	0	0	0	1355	--	--	16.08	16.08	0.00	0.02	0.03	0.22	0.00	0.00	20.9
2	0	-0	-2795	0	0	0	1057	--	--	16.08	16.08	0.10	0.02	0.02	0.18	0.00	0.00	20.9
3	0	-0	-2727	0	0	0	992	--	--	16.08	16.08	0.10	0.02	0.02	0.17	0.00	0.00	20.9
4	0	-0	-2697	0	0	0	1092	--	--	16.08	16.08	0.10	0.02	0.02	0.17	0.00	0.00	20.9
5	0	-0	-2630	0	0	0	1027	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
6	0	-0	-2839	0	0	0	1145	--	--	16.08	16.08	0.10	0.02	0.02	0.18	0.00	0.00	20.9
7	0	-0	-2615	0	0	0	929	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
8	0	-0	-2810	0	0	0	1155	--	--	16.08	16.08	0.10	0.02	0.02	0.18	0.00	0.00	20.9
9	0	-0	-2586	0	0	0	940	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
10	0	-0	-2795	0	0	0	1057	--	--	16.08	16.08	0.10	0.02	0.02	0.18	0.00	0.00	20.9
11	0	-0	-2727	0	0	0	992	--	--	16.08	16.08	0.10	0.02	0.02	0.17	0.00	0.00	20.9
12	0	-0	-2697	0	0	0	1092	--	--	16.08	16.08	0.10	0.02	0.02	0.17	0.00	0.00	20.9
13	0	-0	-2630	0	0	0	1027	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
14	0	-0	-2839	0	0	0	1145	--	--	16.08	16.08	0.10	0.02	0.02	0.18	0.00	0.00	20.9
15	0	-0	-2615	0	0	0	929	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
16	0	-0	-2810	0	0	0	1155	--	--	16.08	16.08	0.10	0.02	0.02	0.18	0.00	0.00	20.9

17	0	-0	-2586	0	0	0	940	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
18	0	-0	-5055	0	0	0	1828	--	--	16.08	16.08	0.00	0.03	0.04	0.32	0.00	0.00	20.9
19	0	-0	-4946	0	0	0	2123	--	--	16.08	16.08	0.00	0.04	0.04	0.31	0.00	0.00	20.9
20	0	-0	-4342	0	0	0	1495	--	--	16.08	16.08	0.00	0.03	0.04	0.27	0.00	0.00	20.9
37	0	-0	-4614	0	0	0	1527	--	--	16.08	16.08	0.00	0.03	0.04	0.29	0.00	0.00	20.9
38	0	-0	-4432	0	0	0	2019	--	--	16.08	16.08	0.00	0.03	0.04	0.28	0.00	0.00	20.9
39	0	-0	-3424	0	0	0	973	--	--	16.08	16.08	0.00	0.02	0.03	0.21	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-3526	0	0	0	1355	--	--	16.08	16.08	0.00	0.02	0.03	0.22	0.00	0.00	20.9
2	27	-0	-2795	0	0	0	1057	--	--	16.08	16.08	0.10	0.02	0.02	0.18	0.00	0.00	20.9
3	27	-0	-2727	0	0	0	992	--	--	16.08	16.08	0.10	0.02	0.02	0.17	0.00	0.00	20.9
4	27	-0	-2697	0	0	0	1092	--	--	16.08	16.08	0.10	0.02	0.02	0.17	0.00	0.00	20.9
5	27	-0	-2630	0	0	0	1027	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
6	27	-0	-2839	0	0	0	1145	--	--	16.08	16.08	0.10	0.02	0.02	0.18	0.00	0.00	20.9
7	27	-0	-2615	0	0	0	929	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
8	27	-0	-2810	0	0	0	1155	--	--	16.08	16.08	0.10	0.02	0.02	0.18	0.00	0.00	20.9
9	27	-0	-2586	0	0	0	940	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
10	27	-0	-2795	0	0	0	1057	--	--	16.08	16.08	0.10	0.02	0.02	0.18	0.00	0.00	20.9
11	27	-0	-2727	0	0	0	992	--	--	16.08	16.08	0.10	0.02	0.02	0.17	0.00	0.00	20.9
12	27	-0	-2697	0	0	0	1092	--	--	16.08	16.08	0.10	0.02	0.02	0.17	0.00	0.00	20.9
13	27	-0	-2630	0	0	0	1027	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
14	27	-0	-2839	0	0	0	1145	--	--	16.08	16.08	0.10	0.02	0.02	0.18	0.00	0.00	20.9
15	27	-0	-2615	0	0	0	929	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
16	27	-0	-2810	0	0	0	1155	--	--	16.08	16.08	0.10	0.02	0.02	0.18	0.00	0.00	20.9
17	27	-0	-2586	0	0	0	940	--	--	16.08	16.08	0.10	0.02	0.02	0.16	0.00	0.00	20.9
18	27	-0	-5055	0	0	0	1828	--	--	16.08	16.08	0.00	0.03	0.04	0.32	0.00	0.00	20.9
19	27	-0	-4946	0	0	0	2123	--	--	16.08	16.08	0.00	0.04	0.04	0.31	0.00	0.00	20.9
20	27	-0	-4342	0	0	0	1495	--	--	16.08	16.08	0.00	0.03	0.04	0.27	0.00	0.00	20.9
37	27	-0	-4614	0	0	0	1527	--	--	16.08	16.08	0.00	0.03	0.04	0.29	0.00	0.00	20.9
38	27	-0	-4432	0	0	0	2019	--	--	16.08	16.08	0.00	0.03	0.04	0.28	0.00	0.00	20.9
39	27	-0	-3424	0	0	0	973	--	--	16.08	16.08	0.00	0.02	0.03	0.21	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	-3526	0	0	0	-568	--	--	16.08	16.08	0.18	0.01	0.03	0.22	0.00	0.00	20.9
2	55	-0	-2795	0	0	0	-467	--	--	16.08	16.08	0.29	0.01	0.02	0.18	0.00	0.00	20.9
3	55	-0	-2727	0	0	0	-495	--	--	16.08	16.08	0.29	0.01	0.02	0.17	0.00	0.00	20.9
4	55	-0	-2697	0	0	0	-379	--	--	16.08	16.08	0.29	0.01	0.02	0.17	0.00	0.00	20.9
5	55	-0	-2630	0	0	0	-407	--	--	16.08	16.08	0.29	0.01	0.02	0.16	0.00	0.00	20.9
6	55	-0	-2839	0	0	0	-404	--	--	16.08	16.08	0.29	0.01	0.02	0.18	0.00	0.00	20.9
7	55	-0	-2615	0	0	0	-497	--	--	16.08	16.08	0.29	0.01	0.02	0.16	0.00	0.00	20.9
8	55	-0	-2810	0	0	0	-377	--	--	16.08	16.08	0.29	0.01	0.02	0.18	0.00	0.00	20.9
9	55	-0	-2586	0	0	0	-471	--	--	16.08	16.08	0.29	0.01	0.02	0.16	0.00	0.00	20.9
10	55	-0	-2795	0	0	0	-467	--	--	16.08	16.08	0.29	0.01	0.02	0.18	0.00	0.00	20.9
11	55	-0	-2727	0	0	0	-495	--	--	16.08	16.08	0.29	0.01	0.02	0.17	0.00	0.00	20.9
12	55	-0	-2697	0	0	0	-379	--	--	16.08	16.08	0.29	0.01	0.02	0.17	0.00	0.00	20.9
13	55	-0	-2630	0	0	0	-407	--	--	16.08	16.08	0.29	0.01	0.02	0.16	0.00	0.00	20.9
14	55	-0	-2839	0	0	0	-404	--	--	16.08	16.08	0.29	0.01	0.02	0.18	0.00	0.00	20.9
15	55	-0	-2615	0	0	0	-497	--	--	16.08	16.08	0.29	0.01	0.02	0.16	0.00	0.00	20.9
16	55	-0	-2810	0	0	0	-377	--	--	16.08	16.08	0.29	0.01	0.02	0.18	0.00	0.00	20.9
17	55	-0	-2586	0	0	0	-471	--	--	16.08	16.08	0.29	0.01	0.02	0.16	0.00	0.00	20.9
18	55	-0	-5055	0	0	0	-930	--	--	16.08	16.08	0.18	0.02	0.04	0.32	0.00	0.00	20.9
19	55	-0	-4946	0	0	0	-575	--	--	16.08	16.08	0.18	0.01	0.04	0.31	0.00	0.00	20.9
20	55	-0	-4342	0	0	0	-873	--	--	16.08	16.08	0.18	0.01	0.04	0.27	0.00	0.00	20.9
37	55	-0	-4614	0	0	0	-989	--	--	16.08	16.08	0.18	0.02	0.04	0.29	0.00	0.00	20.9
38	55	-0	-4432	0	0	0	-398	--	--	16.08	16.08	0.18	0.01	0.04	0.28	0.00	0.00	20.9
39	55	-0	-3424	0	0	0	-895	--	--	16.08	16.08	0.18	0.01	0.03	0.21	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 194 NI 1575 NF 1634 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-4251	0	0	0	2307	--	--	16.08	16.08	0.00	0.04	0.04	0.27	0.00	0.00	20.9
2	0	-0	-3360	0	0	0	1805	--	--	16.08	16.08	0.10	0.03	0.03	0.21	0.00	0.00	20.9
3	0	-0	-3328	0	0	0	1754	--	--	16.08	16.08	0.10	0.03	0.03	0.21	0.00	0.00	20.9
4	0	-0	-3212	0	0	0	1795	--	--	16.08	16.08	0.10	0.03	0.03	0.20	0.00	0.00	20.9
5	0	-0	-3180	0	0	0	1745	--	--	16.08	16.08	0.10	0.03	0.03	0.20	0.00	0.00	20.9
6	0	-0	-3346	0	0	0	1861	--	--	16.08	16.08	0.10	0.03	0.03	0.21	0.00	0.00	20.9
7	0	-0	-3239	0	0	0	1692	--	--	16.08	16.08	0.10	0.03	0.03	0.20	0.00	0.00	20.9
8	0	-0	-3301	0	0	0	1858	--	--	16.08	16.08	0.10	0.03	0.03	0.21	0.00	0.00	20.9
9	0	-0	-3194	0	0	0	1689	--	--	16.08	16.08	0.10	0.03	0.03	0.20	0.00	0.00	20.9
10	0	-0	-3360	0	0	0	1805	--	--	16.08	16.08	0.10	0.03	0.03	0.21	0.00	0.00	20.9
11	0	-0	-3328	0	0	0	1754	--	--	16.08	16.08	0.10	0.03	0.03	0.21	0.00	0.00	20.9
12	0	-0	-3212	0	0	0	1795	--	--	16.08	16.08	0.10	0.03	0.03	0.20	0.00	0.00	20.9
13	0	-0	-3180	0	0	0	1745	--	--	16.08	16.08	0.10	0.03	0.03	0.20	0.00	0.00	20.9
14	0	-0	-3346	0	0	0	1861	--	--	16.08	16.08	0.10	0.03	0.03	0.21	0.00	0.00	20.9
15	0	-0	-3239	0	0	0	1692	--	--	16.08	16.08	0.10	0.03	0.03	0.20	0.00	0.00	20.9
16	0	-0	-3301	0	0	0	1858	--	--	16.08	16.08	0.10	0.03	0.03	0.21	0.00	0.00	20.9
17	0	-0	-3194	0	0	0	1689	--	--	16.08	16.08	0.10	0.03	0.03	0.20	0.00	0.00	20.9
18	0	-0	-6123	0	0	0	3205	--	--	16.08	16.08	0.00	0.05	0.05	0.38	0.00	0.00	20.9
19	0	-0	-5897	0	0	0	3417	--	--	16.08	16.08	0.00	0.06	0.05	0.37	0.00	0.00	20.9
20	0	-0	-5385	0	0	0	2769	--	--	16.08	16.08	0.00	0.05	0.04	0.34	0.00	0.00	20.9
37	0	-0	-5630	0	0	0	2809	--	--	16.08	16.08	0.00	0.05	0.05	0.35	0.00	0.00	20.9
38	0	-0	-5252	0	0	0	3162	--	--	16.08	16.08	0.00	0.05	0.04	0.33	0.00	0.00	20.9
39	0	-0	-4400	0	0	0	2082	--	--	16.08	16.08	0.00	0.04	0.04	0.28	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-4251	0	0	0	2307	--	--	16.08	16.08	0.00	0.04	0.04	0.27	0.00	0.00	20.9
2	27	-0	-3360	0	0	0	1805	--	--	16.08	16.08	0.10	0.03	0.03	0.21	0.00	0.00	20.9
3	27	-0	-3328	0	0	0	1754	--	--	16.08	16.08	0.10	0.03	0.03	0.21	0.00	0.00	20.9
4	27	-0	-3212	0	0	0	1795	--	--	16.08	16.08	0.10	0.03	0.03	0.20	0.00	0.00	20.9
5	27	-0	-3180	0	0	0	1745	--	--	16.08	16.08	0.10	0.03	0.03	0.20	0.00	0.00	20.9
6	27	-0	-3346	0	0	0	1861	--	--	16.08	16.08	0.10	0.03	0.03	0.21	0.00	0.00	20.9
7	27	-0	-3239	0	0	0	1692	--	--	16.08	16.08	0.10	0.03	0.03	0.20	0.00	0.00	20.9
8	27	-0	-3301	0	0	0	1858	--	--	16.08	16.08	0.10	0.03	0.03	0.21	0.00	0.00	20.9
9	27	-0	-3194	0	0	0	1689	--	--	16.08	16.08	0.10	0.03	0.03	0.20	0.00	0.00	20.9
10	27	-0	-3360	0	0	0	1805	--	--	16.08	16.08	0.10	0.03	0.03	0.21	0.00	0.00	20.9
11	27	-0	-3328	0	0	0	1754	--	--	16.08	16.08	0.10	0.03	0.03	0.21	0.00	0.00	20.9
12	27	-0	-3212	0	0	0	1795	--	--	16.08	16.08	0.10	0.03	0.03	0.20	0.00	0.00	20.9

13	27	-0	-3180	0	0	0	1745	--	--	16.08	16.08	0.10	0.03	0.03	0.20	0.00	0.00	20.9
14	27	-0	-3346	0	0	0	1861	--	--	16.08	16.08	0.10	0.03	0.03	0.21	0.00	0.00	20.9
15	27	-0	-3239	0	0	0	1692	--	--	16.08	16.08	0.10	0.03	0.03	0.20	0.00	0.00	20.9
16	27	-0	-3301	0	0	0	1858	--	--	16.08	16.08	0.10	0.03	0.03	0.21	0.00	0.00	20.9
17	27	-0	-3194	0	0	0	1689	--	--	16.08	16.08	0.10	0.03	0.03	0.20	0.00	0.00	20.9
18	27	-0	-6123	0	0	0	3205	--	--	16.08	16.08	0.00	0.05	0.05	0.38	0.00	0.00	20.9
19	27	-0	-5897	0	0	0	3417	--	--	16.08	16.08	0.00	0.06	0.05	0.37	0.00	0.00	20.9
20	27	-0	-5385	0	0	0	2769	--	--	16.08	16.08	0.00	0.05	0.04	0.34	0.00	0.00	20.9
37	27	-0	-5630	0	0	0	2809	--	--	16.08	16.08	0.00	0.05	0.05	0.35	0.00	0.00	20.9
38	27	-0	-5252	0	0	0	3162	--	--	16.08	16.08	0.00	0.05	0.04	0.33	0.00	0.00	20.9
39	27	-0	-4400	0	0	0	2082	--	--	16.08	16.08	0.00	0.04	0.04	0.28	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	-4251	0	0	0	-12	--	--	16.08	16.08	0.18	0.00	0.04	0.27	0.00	0.00	20.9
2	55	-0	-3360	0	0	0	-28	--	--	16.08	16.08	0.29	0.00	0.03	0.21	0.00	0.00	20.9
3	55	-0	-3328	0	0	0	-61	--	--	16.08	16.08	0.29	0.00	0.03	0.21	0.00	0.00	20.9
4	55	-0	-3212	0	0	0	44	--	--	16.08	16.08	0.10	0.00	0.03	0.20	0.00	0.00	20.9
5	55	-0	-3180	0	0	0	10	--	--	16.08	16.08	0.10	0.00	0.03	0.20	0.00	0.00	20.9
6	55	-0	-3346	0	0	0	36	--	--	16.08	16.08	0.10	0.00	0.03	0.21	0.00	0.00	20.9
7	55	-0	-3239	0	0	0	-75	--	--	16.08	16.08	0.29	0.00	0.03	0.20	0.00	0.00	20.9
8	55	-0	-3301	0	0	0	57	--	--	16.08	16.08	0.10	0.00	0.03	0.21	0.00	0.00	20.9
9	55	-0	-3194	0	0	0	-54	--	--	16.08	16.08	0.29	0.00	0.03	0.20	0.00	0.00	20.9
10	55	-0	-3360	0	0	0	-28	--	--	16.08	16.08	0.29	0.00	0.03	0.21	0.00	0.00	20.9
11	55	-0	-3328	0	0	0	-61	--	--	16.08	16.08	0.29	0.00	0.03	0.21	0.00	0.00	20.9
12	55	-0	-3212	0	0	0	44	--	--	16.08	16.08	0.10	0.00	0.03	0.20	0.00	0.00	20.9
13	55	-0	-3180	0	0	0	10	--	--	16.08	16.08	0.10	0.00	0.03	0.20	0.00	0.00	20.9
14	55	-0	-3346	0	0	0	36	--	--	16.08	16.08	0.10	0.00	0.03	0.21	0.00	0.00	20.9
15	55	-0	-3239	0	0	0	-75	--	--	16.08	16.08	0.29	0.00	0.03	0.20	0.00	0.00	20.9
16	55	-0	-3301	0	0	0	57	--	--	16.08	16.08	0.10	0.00	0.03	0.21	0.00	0.00	20.9
17	55	-0	-3194	0	0	0	-54	--	--	16.08	16.08	0.29	0.00	0.03	0.20	0.00	0.00	20.9
18	55	-0	-6123	0	0	0	-135	--	--	16.08	16.08	0.18	0.00	0.05	0.38	0.00	0.00	20.9
19	55	-0	-5897	0	0	0	201	--	--	16.08	16.08	0.00	0.00	0.05	0.37	0.00	0.00	20.9
20	55	-0	-5385	0	0	0	-168	--	--	16.08	16.08	0.18	0.00	0.04	0.34	0.00	0.00	20.9
37	55	-0	-5630	0	0	0	-262	--	--	16.08	16.08	0.18	0.00	0.05	0.35	0.00	0.00	20.9
38	55	-0	-5252	0	0	0	297	--	--	16.08	16.08	0.00	0.01	0.04	0.33	0.00	0.00	20.9
39	55	-0	-4400	0	0	0	-318	--	--	16.08	16.08	0.18	0.01	0.04	0.28	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 195 NI 1682 NF 1575 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-2791	0	0	0	2516	--	--	16.08	16.08	0.00	0.04	0.02	0.18	0.00	0.00	20.9
2	0	-0	-2189	0	0	0	1975	--	--	16.08	16.08	0.10	0.04	0.02	0.14	0.00	0.00	20.9
3	0	-0	-2206	0	0	0	1934	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
4	0	-0	-2088	0	0	0	1936	--	--	16.08	16.08	0.10	0.03	0.02	0.13	0.00	0.00	20.9
5	0	-0	-2105	0	0	0	1896	--	--	16.08	16.08	0.10	0.03	0.02	0.13	0.00	0.00	20.9
6	0	-0	-2134	0	0	0	2009	--	--	16.08	16.08	0.10	0.04	0.02	0.13	0.00	0.00	20.9
7	0	-0	-2191	0	0	0	1874	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
8	0	-0	-2104	0	0	0	1997	--	--	16.08	16.08	0.10	0.04	0.02	0.13	0.00	0.00	20.9
9	0	-0	-2160	0	0	0	1862	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
10	0	-0	-2189	0	0	0	1975	--	--	16.08	16.08	0.10	0.04	0.02	0.14	0.00	0.00	20.9
11	0	-0	-2206	0	0	0	1934	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
12	0	-0	-2088	0	0	0	1936	--	--	16.08	16.08	0.10	0.03	0.02	0.13	0.00	0.00	20.9
13	0	-0	-2105	0	0	0	1896	--	--	16.08	16.08	0.10	0.03	0.02	0.13	0.00	0.00	20.9
14	0	-0	-2134	0	0	0	2009	--	--	16.08	16.08	0.10	0.04	0.02	0.13	0.00	0.00	20.9
15	0	-0	-2191	0	0	0	1874	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
16	0	-0	-2104	0	0	0	1997	--	--	16.08	16.08	0.10	0.04	0.02	0.13	0.00	0.00	20.9
17	0	-0	-2160	0	0	0	1862	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
18	0	-0	-3689	0	0	0	3439	--	--	16.08	16.08	0.00	0.06	0.03	0.23	0.00	0.00	20.9
19	0	-0	-3768	0	0	0	3657	--	--	16.08	16.08	0.00	0.06	0.03	0.24	0.00	0.00	20.9
20	0	-0	-3295	0	0	0	2973	--	--	16.08	16.08	0.00	0.05	0.03	0.21	0.00	0.00	20.9
37	0	-0	-3362	0	0	0	3033	--	--	16.08	16.08	0.00	0.05	0.03	0.21	0.00	0.00	20.9
38	0	-0	-3494	0	0	0	3396	--	--	16.08	16.08	0.00	0.06	0.03	0.22	0.00	0.00	20.9
39	0	-0	-2705	0	0	0	2255	--	--	16.08	16.08	0.00	0.04	0.02	0.17	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-2791	0	0	0	2516	--	--	16.08	16.08	0.00	0.04	0.02	0.18	0.00	0.00	20.9
2	27	-0	-2189	0	0	0	1975	--	--	16.08	16.08	0.10	0.04	0.02	0.14	0.00	0.00	20.9
3	27	-0	-2206	0	0	0	1934	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
4	27	-0	-2088	0	0	0	1936	--	--	16.08	16.08	0.10	0.03	0.02	0.13	0.00	0.00	20.9
5	27	-0	-2105	0	0	0	1896	--	--	16.08	16.08	0.10	0.03	0.02	0.13	0.00	0.00	20.9
6	27	-0	-2134	0	0	0	2009	--	--	16.08	16.08	0.10	0.04	0.02	0.13	0.00	0.00	20.9
7	27	-0	-2191	0	0	0	1874	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
8	27	-0	-2104	0	0	0	1997	--	--	16.08	16.08	0.10	0.04	0.02	0.13	0.00	0.00	20.9
9	27	-0	-2160	0	0	0	1862	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
10	27	-0	-2189	0	0	0	1975	--	--	16.08	16.08	0.10	0.04	0.02	0.14	0.00	0.00	20.9
11	27	-0	-2206	0	0	0	1934	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
12	27	-0	-2088	0	0	0	1936	--	--	16.08	16.08	0.10	0.03	0.02	0.13	0.00	0.00	20.9
13	27	-0	-2105	0	0	0	1896	--	--	16.08	16.08	0.10	0.03	0.02	0.13	0.00	0.00	20.9
14	27	-0	-2134	0	0	0	2009	--	--	16.08	16.08	0.10	0.04	0.02	0.13	0.00	0.00	20.9
15	27	-0	-2191	0	0	0	1874	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
16	27	-0	-2104	0	0	0	1997	--	--	16.08	16.08	0.10	0.04	0.02	0.13	0.00	0.00	20.9
17	27	-0	-2160	0	0	0	1862	--	--	16.08	16.08	0.10	0.03	0.02	0.14	0.00	0.00	20.9
18	27	-0	-3689	0	0	0	3439	--	--	16.08	16.08	0.00	0.06	0.03	0.23	0.00	0.00	20.9
19	27	-0	-3768	0	0	0	3657	--	--	16.08	16.08	0.00	0.06	0.03	0.24	0.00	0.00	20.9
20	27	-0	-3295	0	0	0	2973	--	--	16.08	16.08	0.00	0.05	0.03	0.21	0.00	0.00	20.9
37	27	-0	-3362	0	0	0	3033	--	--	16.08	16.08	0.00	0.05	0.03	0.21	0.00	0.00	20.9
38	27	-0	-3494	0	0	0	3396	--	--	16.08	16.08	0.00	0.06	0.03	0.22	0.00	0.00	20.9
39	27	-0	-2705	0	0	0	2255	--	--	16.08	16.08	0.00	0.04	0.02	0.17	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	-2791	0	0	0	994	--	--	16.08	16.08	0.00	0.02	0.02	0.18	0.00	0.00	20.9
2	55	-0	-2189	0	0	0	781	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
3	55	-0	-2206	0	0	0	731	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
4	55	-0	-2088	0	0	0	798	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
5	55	-0	-2105	0	0	0	748	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
6	55	-0	-2134	0	0	0	844	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
7	55	-0	-2191	0	0	0	679	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
8	55	-0	-2104	0	0	0	849	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9

9	55	-0	-2160	0	0	0	684	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
10	55	-0	-2189	0	0	0	781	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
11	55	-0	-2206	0	0	0	731	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
12	55	-0	-2088	0	0	0	798	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
13	55	-0	-2105	0	0	0	748	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
14	55	-0	-2134	0	0	0	844	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
15	55	-0	-2191	0	0	0	679	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
16	55	-0	-2104	0	0	0	849	--	--	16.08	16.08	0.10	0.02	0.02	0.13	0.00	0.00	20.9
17	55	-0	-2160	0	0	0	684	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
18	55	-0	-3689	0	0	0	1427	--	--	16.08	16.08	0.00	0.02	0.03	0.23	0.00	0.00	20.9
19	55	-0	-3768	0	0	0	1601	--	--	16.08	16.08	0.00	0.03	0.03	0.24	0.00	0.00	20.9
20	55	-0	-3295	0	0	0	1175	--	--	16.08	16.08	0.00	0.02	0.03	0.21	0.00	0.00	20.9
37	55	-0	-3362	0	0	0	1200	--	--	16.08	16.08	0.00	0.02	0.03	0.21	0.00	0.00	20.9
38	55	-0	-3494	0	0	0	1490	--	--	16.08	16.08	0.00	0.03	0.03	0.22	0.00	0.00	20.9
39	55	-0	-2705	0	0	0	780	--	--	16.08	16.08	0.00	0.01	0.02	0.17	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 196 NI 1654 NF 1682 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	2036	0	0	0	425	--	--	16.08	16.08	0.00	0.01	0.02	0.13	0.00	0.00	20.9
2	0	-0	1478	0	0	0	293	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
3	0	-0	1487	0	0	0	240	--	--	16.08	16.08	0.10	0.00	0.01	0.09	0.00	0.00	20.9
4	0	-0	1646	0	0	0	415	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
5	0	-0	1655	0	0	0	361	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
6	0	-0	1527	0	0	0	397	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
7	0	-0	1556	0	0	0	220	--	--	16.08	16.08	0.10	0.00	0.01	0.10	0.00	0.00	20.9
8	0	-0	1577	0	0	0	434	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
9	0	-0	1606	0	0	0	257	--	--	16.08	16.08	0.10	0.00	0.01	0.10	0.00	0.00	20.9
10	0	-0	1478	0	0	0	293	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
11	0	-0	1487	0	0	0	240	--	--	16.08	16.08	0.10	0.00	0.01	0.09	0.00	0.00	20.9
12	0	-0	1646	0	0	0	415	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
13	0	-0	1655	0	0	0	361	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
14	0	-0	1527	0	0	0	397	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
15	0	-0	1556	0	0	0	220	--	--	16.08	16.08	0.10	0.00	0.01	0.10	0.00	0.00	20.9
16	0	-0	1577	0	0	0	434	--	--	16.08	16.08	0.10	0.01	0.01	0.10	0.00	0.00	20.9
17	0	-0	1606	0	0	0	257	--	--	16.08	16.08	0.10	0.00	0.01	0.10	0.00	0.00	20.9
18	0	-0	1347	0	0	0	238	--	--	16.08	16.08	0.00	0.00	0.01	0.08	0.00	0.00	20.9
19	0	-0	2589	0	0	0	899	--	--	16.08	16.08	0.00	0.02	0.02	0.16	0.00	0.00	20.9
20	0	-0	2574	0	0	0	-124	--	--	16.08	16.08	0.18	0.00	0.02	0.16	0.00	0.00	20.9
37	0	-0	962	0	0	0	-29	--	--	16.08	16.08	0.18	0.00	0.01	0.06	0.00	0.00	20.9
38	0	-0	3031	0	0	0	1072	--	--	16.08	16.08	0.00	0.02	0.02	0.19	0.00	0.00	20.9
39	0	-0	3007	0	0	0	-632	--	--	16.08	16.08	0.18	0.01	0.02	0.19	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	2036	0	0	0	3157	--	--	16.08	16.08	0.00	0.05	0.02	0.13	0.00	0.00	20.9
2	27	-0	1478	0	0	0	2276	--	--	16.08	16.08	0.10	0.04	0.01	0.09	0.00	0.00	20.9
3	27	-0	1487	0	0	0	2235	--	--	16.08	16.08	0.10	0.04	0.01	0.09	0.00	0.00	20.9
4	27	-0	1646	0	0	0	2622	--	--	16.08	16.08	0.10	0.05	0.01	0.10	0.00	0.00	20.9
5	27	-0	1655	0	0	0	2581	--	--	16.08	16.08	0.10	0.05	0.01	0.10	0.00	0.00	20.9
6	27	-0	1527	0	0	0	2446	--	--	16.08	16.08	0.10	0.04	0.01	0.10	0.00	0.00	20.9
7	27	-0	1556	0	0	0	2308	--	--	16.08	16.08	0.10	0.04	0.01	0.10	0.00	0.00	20.9
8	27	-0	1577	0	0	0	2549	--	--	16.08	16.08	0.10	0.05	0.01	0.10	0.00	0.00	20.9
9	27	-0	1606	0	0	0	2411	--	--	16.08	16.08	0.10	0.04	0.01	0.10	0.00	0.00	20.9
10	27	-0	1478	0	0	0	2276	--	--	16.08	16.08	0.10	0.04	0.01	0.09	0.00	0.00	20.9
11	27	-0	1487	0	0	0	2235	--	--	16.08	16.08	0.10	0.04	0.01	0.09	0.00	0.00	20.9
12	27	-0	1646	0	0	0	2622	--	--	16.08	16.08	0.10	0.05	0.01	0.10	0.00	0.00	20.9
13	27	-0	1655	0	0	0	2581	--	--	16.08	16.08	0.10	0.05	0.01	0.10	0.00	0.00	20.9
14	27	-0	1527	0	0	0	2446	--	--	16.08	16.08	0.10	0.04	0.01	0.10	0.00	0.00	20.9
15	27	-0	1556	0	0	0	2308	--	--	16.08	16.08	0.10	0.04	0.01	0.10	0.00	0.00	20.9
16	27	-0	1577	0	0	0	2549	--	--	16.08	16.08	0.10	0.05	0.01	0.10	0.00	0.00	20.9
17	27	-0	1606	0	0	0	2411	--	--	16.08	16.08	0.10	0.04	0.01	0.10	0.00	0.00	20.9
18	27	-0	1347	0	0	0	2045	--	--	16.08	16.08	0.00	0.03	0.01	0.08	0.00	0.00	20.9
19	27	-0	2589	0	0	0	4372	--	--	16.08	16.08	0.00	0.07	0.02	0.16	0.00	0.00	20.9
20	27	-0	2574	0	0	0	3329	--	--	16.08	16.08	0.00	0.06	0.02	0.16	0.00	0.00	20.9
37	27	-0	962	0	0	0	1261	--	--	16.08	16.08	0.00	0.02	0.01	0.06	0.00	0.00	20.9
38	27	-0	3031	0	0	0	5138	--	--	16.08	16.08	0.00	0.09	0.02	0.19	0.00	0.00	20.9
39	27	-0	3007	0	0	0	3402	--	--	16.08	16.08	0.00	0.06	0.02	0.19	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	2036	0	0	0	1536	--	--	16.08	16.08	0.00	0.03	0.02	0.13	0.00	0.00	20.9
2	55	-0	1478	0	0	0	1099	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
3	55	-0	1487	0	0	0	1051	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
4	55	-0	1646	0	0	0	1312	--	--	16.08	16.08	0.10	0.02	0.01	0.10	0.00	0.00	20.9
5	55	-0	1655	0	0	0	1264	--	--	16.08	16.08	0.10	0.02	0.01	0.10	0.00	0.00	20.9
6	55	-0	1527	0	0	0	1230	--	--	16.08	16.08	0.10	0.02	0.01	0.10	0.00	0.00	20.9
7	55	-0	1556	0	0	0	1069	--	--	16.08	16.08	0.10	0.02	0.01	0.10	0.00	0.00	20.9
8	55	-0	1577	0	0	0	1294	--	--	16.08	16.08	0.10	0.02	0.01	0.10	0.00	0.00	20.9
9	55	-0	1606	0	0	0	1133	--	--	16.08	16.08	0.10	0.02	0.01	0.10	0.00	0.00	20.9
10	55	-0	1478	0	0	0	1099	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
11	55	-0	1487	0	0	0	1051	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
12	55	-0	1646	0	0	0	1312	--	--	16.08	16.08	0.10	0.02	0.01	0.10	0.00	0.00	20.9
13	55	-0	1655	0	0	0	1264	--	--	16.08	16.08	0.10	0.02	0.01	0.10	0.00	0.00	20.9
14	55	-0	1527	0	0	0	1230	--	--	16.08	16.08	0.10	0.02	0.01	0.10	0.00	0.00	20.9
15	55	-0	1556	0	0	0	1069	--	--	16.08	16.08	0.10	0.02	0.01	0.10	0.00	0.00	20.9
16	55	-0	1577	0	0	0	1294	--	--	16.08	16.08	0.10	0.02	0.01	0.10	0.00	0.00	20.9
17	55	-0	1606	0	0	0	1133	--	--	16.08	16.08	0.10	0.02	0.01	0.10	0.00	0.00	20.9
18	55	-0	1347	0	0	0	973	--	--	16.08	16.08	0.00	0.02	0.01	0.08	0.00	0.00	20.9
19	55	-0	2589	0	0	0	2311	--	--	16.08	16.08	0.00	0.04	0.02	0.16	0.00	0.00	20.9
20	55	-0	2574	0	0	0	1280	--	--	16.08	16.08	0.00	0.02	0.02	0.16	0.00	0.00	20.9
37	55	-0	962	0	0	0	495	--	--	16.08	16.08	0.00	0.01	0.01	0.06	0.00	0.00	20.9
38	55	-0	3031	0	0	0	2725	--	--	16.08	16.08	0.00	0.05	0.02	0.19	0.00	0.00	20.9
39	55	-0	3007	0	0	0	1008	--	--	16.08	16.08	0.00	0.02	0.02	0.19	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 197 NI 1595 NF 1654 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	4376	0	0	0	-395	--	--	16.08	16.08	0.18	0.01	0.04	0.27	0.00	0.00	20.9
2	0	-0	3409	0	0	0	-332	--	--	16.08	16.08	0.29	0.01	0.03	0.21	0.00	0.00	20.9
3	0	-0	3415	0	0	0	-395	--	--	16.08	16.08	0.29	0.01	0.03	0.21	0.00	0.00	20.9
4	0	-0	3318	0	0	0	-212	--	--	16.08	16.08	0.29	0.00	0.03	0.21	0.00	0.00	20.9
5	0	-0	3324	0	0	0	-275	--	--	16.08	16.08	0.29	0.00	0.03	0.21	0.00	0.00	20.9
6	0	-0	3370	0	0	0	-216	--	--	16.08	16.08	0.29	0.00	0.03	0.21	0.00	0.00	20.9
7	0	-0	3390	0	0	0	-427	--	--	16.08	16.08	0.29	0.01	0.03	0.21	0.00	0.00	20.9
8	0	-0	3342	0	0	0	-180	--	--	16.08	16.08	0.29	0.00	0.03	0.21	0.00	0.00	20.9
9	0	-0	3363	0	0	0	-391	--	--	16.08	16.08	0.29	0.01	0.03	0.21	0.00	0.00	20.9
10	0	-0	3409	0	0	0	-332	--	--	16.08	16.08	0.29	0.01	0.03	0.21	0.00	0.00	20.9
11	0	-0	3415	0	0	0	-395	--	--	16.08	16.08	0.29	0.01	0.03	0.21	0.00	0.00	20.9
12	0	-0	3318	0	0	0	-212	--	--	16.08	16.08	0.29	0.00	0.03	0.21	0.00	0.00	20.9
13	0	-0	3324	0	0	0	-275	--	--	16.08	16.08	0.29	0.00	0.03	0.21	0.00	0.00	20.9
14	0	-0	3370	0	0	0	-216	--	--	16.08	16.08	0.29	0.00	0.03	0.21	0.00	0.00	20.9
15	0	-0	3390	0	0	0	-427	--	--	16.08	16.08	0.29	0.01	0.03	0.21	0.00	0.00	20.9
16	0	-0	3342	0	0	0	-180	--	--	16.08	16.08	0.29	0.00	0.03	0.21	0.00	0.00	20.9
17	0	-0	3363	0	0	0	-391	--	--	16.08	16.08	0.29	0.01	0.03	0.21	0.00	0.00	20.9
18	0	-0	5886	0	0	0	-773	--	--	16.08	16.08	0.18	0.01	0.05	0.37	0.00	0.00	20.9
19	0	-0	5914	0	0	0	-224	--	--	16.08	16.08	0.18	0.00	0.05	0.37	0.00	0.00	20.9
20	0	-0	6354	0	0	0	-1305	--	--	16.08	16.08	0.18	0.02	0.05	0.40	0.00	0.00	20.9
37	0	-0	5385	0	0	0	-924	--	--	16.08	16.08	0.18	0.02	0.04	0.34	0.00	0.00	20.9
38	0	-0	5432	0	0	0	-9	--	--	16.08	16.08	0.18	0.00	0.04	0.34	0.00	0.00	20.9
39	0	-0	6165	0	0	0	-1811	--	--	16.08	16.08	0.18	0.03	0.05	0.39	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	4376	0	0	0	5475	--	--	16.08	16.08	0.00	0.09	0.04	0.27	0.00	0.00	20.9
2	27	-0	3409	0	0	0	4241	--	--	16.08	16.08	0.10	0.08	0.03	0.21	0.00	0.00	20.9
3	27	-0	3415	0	0	0	4186	--	--	16.08	16.08	0.10	0.07	0.03	0.21	0.00	0.00	20.9
4	27	-0	3318	0	0	0	4239	--	--	16.08	16.08	0.10	0.08	0.03	0.21	0.00	0.00	20.9
5	27	-0	3324	0	0	0	4184	--	--	16.08	16.08	0.10	0.07	0.03	0.21	0.00	0.00	20.9
6	27	-0	3370	0	0	0	4304	--	--	16.08	16.08	0.10	0.08	0.03	0.21	0.00	0.00	20.9
7	27	-0	3390	0	0	0	4121	--	--	16.08	16.08	0.10	0.07	0.03	0.21	0.00	0.00	20.9
8	27	-0	3342	0	0	0	4303	--	--	16.08	16.08	0.10	0.08	0.03	0.21	0.00	0.00	20.9
9	27	-0	3363	0	0	0	4121	--	--	16.08	16.08	0.10	0.07	0.03	0.21	0.00	0.00	20.9
10	27	-0	3409	0	0	0	4241	--	--	16.08	16.08	0.10	0.08	0.03	0.21	0.00	0.00	20.9
11	27	-0	3415	0	0	0	4186	--	--	16.08	16.08	0.10	0.07	0.03	0.21	0.00	0.00	20.9
12	27	-0	3318	0	0	0	4239	--	--	16.08	16.08	0.10	0.08	0.03	0.21	0.00	0.00	20.9
13	27	-0	3324	0	0	0	4184	--	--	16.08	16.08	0.10	0.07	0.03	0.21	0.00	0.00	20.9
14	27	-0	3370	0	0	0	4304	--	--	16.08	16.08	0.10	0.08	0.03	0.21	0.00	0.00	20.9
15	27	-0	3390	0	0	0	4121	--	--	16.08	16.08	0.10	0.07	0.03	0.21	0.00	0.00	20.9
16	27	-0	3342	0	0	0	4303	--	--	16.08	16.08	0.10	0.08	0.03	0.21	0.00	0.00	20.9
17	27	-0	3363	0	0	0	4121	--	--	16.08	16.08	0.10	0.07	0.03	0.21	0.00	0.00	20.9
18	27	-0	5886	0	0	0	7123	--	--	16.08	16.08	0.00	0.12	0.05	0.37	0.00	0.00	20.9
19	27	-0	5914	0	0	0	7709	--	--	16.08	16.08	0.00	0.13	0.05	0.37	0.00	0.00	20.9
20	27	-0	6354	0	0	0	7218	--	--	16.08	16.08	0.00	0.12	0.05	0.40	0.00	0.00	20.9
37	27	-0	5385	0	0	0	6300	--	--	16.08	16.08	0.00	0.11	0.04	0.34	0.00	0.00	20.9
38	27	-0	5432	0	0	0	7278	--	--	16.08	16.08	0.00	0.12	0.04	0.34	0.00	0.00	20.9
39	27	-0	6165	0	0	0	-1811	--	--	16.08	16.08	0.18	0.03	0.05	0.39	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	4376	0	0	0	1992	--	--	16.08	16.08	0.00	0.03	0.04	0.27	0.00	0.00	20.9
2	55	-0	3409	0	0	0	1527	--	--	16.08	16.08	0.10	0.03	0.03	0.21	0.00	0.00	20.9
3	55	-0	3415	0	0	0	1467	--	--	16.08	16.08	0.10	0.03	0.03	0.21	0.00	0.00	20.9
4	55	-0	3318	0	0	0	1598	--	--	16.08	16.08	0.10	0.03	0.03	0.21	0.00	0.00	20.9
5	55	-0	3324	0	0	0	1538	--	--	16.08	16.08	0.10	0.03	0.03	0.21	0.00	0.00	20.9
6	55	-0	3370	0	0	0	1622	--	--	16.08	16.08	0.10	0.03	0.03	0.21	0.00	0.00	20.9
7	55	-0	3390	0	0	0	1422	--	--	16.08	16.08	0.10	0.03	0.03	0.21	0.00	0.00	20.9
8	55	-0	3342	0	0	0	1643	--	--	16.08	16.08	0.10	0.03	0.03	0.21	0.00	0.00	20.9
9	55	-0	3363	0	0	0	1444	--	--	16.08	16.08	0.10	0.03	0.03	0.21	0.00	0.00	20.9
10	55	-0	3409	0	0	0	1527	--	--	16.08	16.08	0.10	0.03	0.03	0.21	0.00	0.00	20.9
11	55	-0	3415	0	0	0	1467	--	--	16.08	16.08	0.10	0.03	0.03	0.21	0.00	0.00	20.9
12	55	-0	3318	0	0	0	1598	--	--	16.08	16.08	0.10	0.03	0.03	0.21	0.00	0.00	20.9
13	55	-0	3324	0	0	0	1538	--	--	16.08	16.08	0.10	0.03	0.03	0.21	0.00	0.00	20.9
14	55	-0	3370	0	0	0	1622	--	--	16.08	16.08	0.10	0.03	0.03	0.21	0.00	0.00	20.9
15	55	-0	3390	0	0	0	1422	--	--	16.08	16.08	0.10	0.03	0.03	0.21	0.00	0.00	20.9
16	55	-0	3342	0	0	0	1643	--	--	16.08	16.08	0.10	0.03	0.03	0.21	0.00	0.00	20.9
17	55	-0	3363	0	0	0	1444	--	--	16.08	16.08	0.10	0.03	0.03	0.21	0.00	0.00	20.9
18	55	-0	5886	0	0	0	2437	--	--	16.08	16.08	0.00	0.04	0.05	0.37	0.00	0.00	20.9
19	55	-0	5914	0	0	0	3001	--	--	16.08	16.08	0.00	0.05	0.05	0.37	0.00	0.00	20.9
20	55	-0	6354	0	0	0	2160	--	--	16.08	16.08	0.00	0.04	0.05	0.40	0.00	0.00	20.9
37	55	-0	5385	0	0	0	2014	--	--	16.08	16.08	0.00	0.03	0.04	0.34	0.00	0.00	20.9
38	55	-0	5432	0	0	0	2954	--	--	16.08	16.08	0.00	0.05	0.04	0.34	0.00	0.00	20.9
39	55	-0	6165	0	0	0	1552	--	--	16.08	16.08	0.00	0.03	0.05	0.39	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 198 NI 1596 NF 1595 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	3966	0	0	0	-981	--	--	16.08	16.08	0.18	0.02	0.03	0.25	0.00	0.00	20.9
2	0	-0	3083	0	0	0	-783	--	--	16.08	16.08	0.29	0.01	0.03	0.19	0.00	0.00	20.9
3	0	-0	3123	0	0	0	-849	--	--	16.08	16.08	0.29	0.01	0.03	0.20	0.00	0.00	20.9
4	0	-0	2978	0	0	0	-660	--	--	16.08	16.08	0.29	0.01	0.02	0.19	0.00	0.00	20.9
5	0	-0	3018	0	0	0	-726	--	--	16.08	16.08	0.29	0.01	0.02	0.19	0.00	0.00	20.9
6	0	-0	2999	0	0	0	-664	--	--	16.08	16.08	0.29	0.01	0.02	0.19	0.00	0.00	20.9
7	0	-0	3133	0	0	0	-882	--	--	16.08	16.08	0.29	0.02	0.03	0.20	0.00	0.00	20.9
8	0	-0	2968	0	0	0	-627	--	--	16.08	16.08	0.29	0.01	0.02	0.19	0.00	0.00	20.9
9	0	-0	3102	0	0	0	-846	--	--	16.08	16.08	0.29	0.01	0.03	0.19	0.00	0.00	20.9
10	0	-0	3083	0	0	0	-783	--	--	16.08	16.08	0.29	0.01	0.03	0.19	0.00	0.00	20.9
11	0	-0	3123	0	0	0	-849	--	--	16.08	16.08	0.29	0.01	0.03	0.20	0.00	0.00	20.9
12	0	-0	2978	0	0	0	-660	--	--	16.08	16.08	0.29	0.01	0.02	0.19	0.00	0.00	20.9
13	0	-0	3018	0	0	0	-726	--	--	16.08	16.08	0.29	0.01	0.02	0.19	0.00	0.00	20.9
14	0	-0	2999	0	0	0	-664	--	--	16.08	16.08	0.29	0.01	0.02	0.19	0.00	0.00	20.9
15	0	-0	3133	0	0	0	-882	--	--	16.08	16.08	0.29	0.02	0.03	0.20	0.00	0.00	20.9
16	0	-0	2968	0	0	0	-627	--	--	16.08	16.08	0.29	0.01	0.02	0.19	0.00	0.00	20.9

17	0	-0	3102	0	0	0	-846	--	--	16.08	16.08	0.29	0.01	0.03	0.19	0.00	0.00	20.9
18	0	-0	5469	0	0	0	-1521	--	--	16.08	16.08	0.18	0.03	0.05	0.34	0.00	0.00	20.9
19	0	-0	5397	0	0	0	-1021	--	--	16.08	16.08	0.18	0.02	0.04	0.34	0.00	0.00	20.9
20	0	-0	6059	0	0	0	-2195	--	--	16.08	16.08	0.18	0.04	0.05	0.38	0.00	0.00	20.9
37	0	-0	5020	0	0	0	-1595	--	--	16.08	16.08	0.18	0.03	0.04	0.31	0.00	0.00	20.9
38	0	-0	4900	0	0	0	-761	--	--	16.08	16.08	0.18	0.01	0.04	0.31	0.00	0.00	20.9
39	0	-0	6004	0	0	0	-2719	--	--	16.08	16.08	0.18	0.05	0.05	0.38	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	3966	0	0	0	4339	--	--	16.08	16.08	0.00	0.07	0.03	0.25	0.00	0.00	20.9
2	27	-0	3083	0	0	0	3353	--	--	16.08	16.08	0.10	0.06	0.03	0.19	0.00	0.00	20.9
3	27	-0	3123	0	0	0	3341	--	--	16.08	16.08	0.10	0.06	0.03	0.20	0.00	0.00	20.9
4	27	-0	2978	0	0	0	3334	--	--	16.08	16.08	0.10	0.06	0.02	0.19	0.00	0.00	20.9
5	27	-0	3018	0	0	0	3323	--	--	16.08	16.08	0.10	0.06	0.02	0.19	0.00	0.00	20.9
6	27	-0	2999	0	0	0	3360	--	--	16.08	16.08	0.10	0.06	0.02	0.19	0.00	0.00	20.9
7	27	-0	3133	0	0	0	-882	--	--	16.08	16.08	0.29	0.02	0.03	0.20	0.00	0.00	20.9
8	27	-0	2968	0	0	0	3355	--	--	16.08	16.08	0.10	0.06	0.02	0.19	0.00	0.00	20.9
9	27	-0	3102	0	0	0	3316	--	--	16.08	16.08	0.10	0.06	0.03	0.19	0.00	0.00	20.9
10	27	-0	3083	0	0	0	3353	--	--	16.08	16.08	0.10	0.06	0.03	0.19	0.00	0.00	20.9
11	27	-0	3123	0	0	0	3341	--	--	16.08	16.08	0.10	0.06	0.03	0.20	0.00	0.00	20.9
12	27	-0	2978	0	0	0	3334	--	--	16.08	16.08	0.10	0.06	0.02	0.19	0.00	0.00	20.9
13	27	-0	3018	0	0	0	3323	--	--	16.08	16.08	0.10	0.06	0.02	0.19	0.00	0.00	20.9
14	27	-0	2999	0	0	0	3360	--	--	16.08	16.08	0.10	0.06	0.02	0.19	0.00	0.00	20.9
15	27	-0	3133	0	0	0	-882	--	--	16.08	16.08	0.29	0.02	0.03	0.20	0.00	0.00	20.9
16	27	-0	2968	0	0	0	3355	--	--	16.08	16.08	0.10	0.06	0.02	0.19	0.00	0.00	20.9
17	27	-0	3102	0	0	0	3316	--	--	16.08	16.08	0.10	0.06	0.03	0.19	0.00	0.00	20.9
18	27	-0	5469	0	0	0	-1521	--	--	16.08	16.08	0.18	0.03	0.05	0.34	0.00	0.00	20.9
19	27	-0	5397	0	0	0	6219	--	--	16.08	16.08	0.00	0.11	0.04	0.34	0.00	0.00	20.9
20	27	-0	6059	0	0	0	-2195	--	--	16.08	16.08	0.18	0.04	0.05	0.38	0.00	0.00	20.9
37	27	-0	5020	0	0	0	-1595	--	--	16.08	16.08	0.18	0.03	0.04	0.31	0.00	0.00	20.9
38	27	-0	4900	0	0	0	5812	--	--	16.08	16.08	0.00	0.10	0.04	0.31	0.00	0.00	20.9
39	27	-0	6004	0	0	0	-2719	--	--	16.08	16.08	0.18	0.05	0.05	0.38	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	3966	0	0	0	1182	--	--	16.08	16.08	0.00	0.02	0.03	0.25	0.00	0.00	20.9
2	55	-0	3083	0	0	0	898	--	--	16.08	16.08	0.10	0.02	0.03	0.19	0.00	0.00	20.9
3	55	-0	3123	0	0	0	855	--	--	16.08	16.08	0.10	0.02	0.03	0.20	0.00	0.00	20.9
4	55	-0	2978	0	0	0	964	--	--	16.08	16.08	0.10	0.02	0.02	0.19	0.00	0.00	20.9
5	55	-0	3018	0	0	0	920	--	--	16.08	16.08	0.10	0.02	0.02	0.19	0.00	0.00	20.9
6	55	-0	2999	0	0	0	972	--	--	16.08	16.08	0.10	0.02	0.02	0.19	0.00	0.00	20.9
7	55	-0	3133	0	0	0	826	--	--	16.08	16.08	0.10	0.01	0.03	0.20	0.00	0.00	20.9
8	55	-0	2968	0	0	0	992	--	--	16.08	16.08	0.10	0.02	0.02	0.19	0.00	0.00	20.9
9	55	-0	3102	0	0	0	846	--	--	16.08	16.08	0.10	0.02	0.03	0.19	0.00	0.00	20.9
10	55	-0	3083	0	0	0	898	--	--	16.08	16.08	0.10	0.02	0.03	0.19	0.00	0.00	20.9
11	55	-0	3123	0	0	0	855	--	--	16.08	16.08	0.10	0.02	0.03	0.20	0.00	0.00	20.9
12	55	-0	2978	0	0	0	964	--	--	16.08	16.08	0.10	0.02	0.02	0.19	0.00	0.00	20.9
13	55	-0	3018	0	0	0	920	--	--	16.08	16.08	0.10	0.02	0.02	0.19	0.00	0.00	20.9
14	55	-0	2999	0	0	0	972	--	--	16.08	16.08	0.10	0.02	0.02	0.19	0.00	0.00	20.9
15	55	-0	3133	0	0	0	826	--	--	16.08	16.08	0.10	0.01	0.03	0.20	0.00	0.00	20.9
16	55	-0	2968	0	0	0	992	--	--	16.08	16.08	0.10	0.02	0.02	0.19	0.00	0.00	20.9
17	55	-0	3102	0	0	0	846	--	--	16.08	16.08	0.10	0.02	0.03	0.19	0.00	0.00	20.9
18	55	-0	5469	0	0	0	1462	--	--	16.08	16.08	0.00	0.02	0.05	0.34	0.00	0.00	20.9
19	55	-0	5397	0	0	0	1923	--	--	16.08	16.08	0.00	0.03	0.04	0.34	0.00	0.00	20.9
20	55	-0	6059	0	0	0	1110	--	--	16.08	16.08	0.00	0.02	0.05	0.38	0.00	0.00	20.9
37	55	-0	5020	0	0	0	1143	--	--	16.08	16.08	0.00	0.02	0.04	0.31	0.00	0.00	20.9
38	55	-0	4900	0	0	0	1911	--	--	16.08	16.08	0.00	0.03	0.04	0.31	0.00	0.00	20.9
39	55	-0	6004	0	0	0	555	--	--	16.08	16.08	0.00	0.01	0.05	0.38	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 199 NI 1552 NF 1596 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	2796	0	0	0	-1428	--	--	16.08	16.08	0.18	0.02	0.02	0.18	0.00	0.00	20.9
2	0	-0	2153	0	0	0	-1126	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
3	0	-0	2206	0	0	0	-1199	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
4	0	-0	2095	0	0	0	-998	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
5	0	-0	2148	0	0	0	-1071	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
6	0	-0	2071	0	0	0	-995	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
7	0	-0	2247	0	0	0	-1239	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
8	0	-0	2054	0	0	0	-957	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
9	0	-0	2230	0	0	0	-1201	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
10	0	-0	2153	0	0	0	-1126	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
11	0	-0	2206	0	0	0	-1199	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
12	0	-0	2095	0	0	0	-998	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
13	0	-0	2148	0	0	0	-1071	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
14	0	-0	2071	0	0	0	-995	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
15	0	-0	2247	0	0	0	-1239	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
16	0	-0	2054	0	0	0	-957	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
17	0	-0	2230	0	0	0	-1201	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
18	0	-0	3778	0	0	0	-2122	--	--	16.08	16.08	0.18	0.04	0.03	0.24	0.00	0.00	20.9
19	0	-0	3824	0	0	0	-1642	--	--	16.08	16.08	0.18	0.03	0.03	0.24	0.00	0.00	20.9
20	0	-0	4573	0	0	0	-2955	--	--	16.08	16.08	0.18	0.05	0.04	0.29	0.00	0.00	20.9
37	0	-0	3439	0	0	0	-2137	--	--	16.08	16.08	0.18	0.04	0.03	0.22	0.00	0.00	20.9
38	0	-0	3516	0	0	0	-1336	--	--	16.08	16.08	0.18	0.02	0.03	0.22	0.00	0.00	20.9
39	0	-0	4765	0	0	0	-3526	--	--	16.08	16.08	0.18	0.06	0.04	0.30	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	2796	0	0	0	-1428	--	--	16.08	16.08	0.18	0.02	0.02	0.18	0.00	0.00	20.9
2	27	-0	2153	0	0	0	-1126	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
3	27	-0	2206	0	0	0	-1199	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
4	27	-0	2095	0	0	0	-998	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
5	27	-0	2148	0	0	0	-1071	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
6	27	-0	2071	0	0	0	-995	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
7	27	-0	2247	0	0	0	-1239	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
8	27	-0	2054	0	0	0	-957	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
9	27	-0	2230	0	0	0	-1201	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
10	27	-0	2153	0	0	0	-1126	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
11	27	-0	2206	0	0	0	-1199	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
12	27	-0	2095	0	0	0	-998	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9

13	27	-0	2148	0	0	0	-1071	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
14	27	-0	2071	0	0	0	-995	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
15	27	-0	2247	0	0	0	-1239	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
16	27	-0	2054	0	0	0	-957	--	--	16.08	16.08	0.29	0.02	0.02	0.13	0.00	0.00	20.9
17	27	-0	2230	0	0	0	-1201	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
18	27	-0	3778	0	0	0	-2122	--	--	16.08	16.08	0.18	0.04	0.03	0.24	0.00	0.00	20.9
19	27	-0	3824	0	0	0	-1642	--	--	16.08	16.08	0.18	0.03	0.03	0.24	0.00	0.00	20.9
20	27	-0	4573	0	0	0	-2955	--	--	16.08	16.08	0.18	0.05	0.04	0.29	0.00	0.00	20.9
37	27	-0	3439	0	0	0	-2137	--	--	16.08	16.08	0.18	0.04	0.03	0.22	0.00	0.00	20.9
38	27	-0	3516	0	0	0	-1336	--	--	16.08	16.08	0.18	0.02	0.03	0.22	0.00	0.00	20.9
39	27	-0	4765	0	0	0	-3526	--	--	16.08	16.08	0.18	0.06	0.04	0.30	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	2796	0	0	0	97	--	--	16.08	16.08	0.00	0.00	0.02	0.18	0.00	0.00	20.9
2	55	-0	2153	0	0	0	49	--	--	16.08	16.08	0.10	0.00	0.02	0.14	0.00	0.00	20.9
3	55	-0	2206	0	0	0	4	--	--	16.08	16.08	0.10	0.00	0.02	0.14	0.00	0.00	20.9
4	55	-0	2095	0	0	0	145	--	--	16.08	16.08	0.10	0.00	0.02	0.13	0.00	0.00	20.9
5	55	-0	2148	0	0	0	101	--	--	16.08	16.08	0.10	0.00	0.02	0.13	0.00	0.00	20.9
6	55	-0	2071	0	0	0	134	--	--	16.08	16.08	0.10	0.00	0.02	0.13	0.00	0.00	20.9
7	55	-0	2247	0	0	0	-1239	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
8	55	-0	2054	0	0	0	163	--	--	16.08	16.08	0.10	0.00	0.02	0.13	0.00	0.00	20.9
9	55	-0	2230	0	0	0	15	--	--	16.08	16.08	0.10	0.00	0.02	0.14	0.00	0.00	20.9
10	55	-0	2153	0	0	0	49	--	--	16.08	16.08	0.10	0.00	0.02	0.14	0.00	0.00	20.9
11	55	-0	2206	0	0	0	4	--	--	16.08	16.08	0.10	0.00	0.02	0.14	0.00	0.00	20.9
12	55	-0	2095	0	0	0	145	--	--	16.08	16.08	0.10	0.00	0.02	0.13	0.00	0.00	20.9
13	55	-0	2148	0	0	0	101	--	--	16.08	16.08	0.10	0.00	0.02	0.13	0.00	0.00	20.9
14	55	-0	2071	0	0	0	134	--	--	16.08	16.08	0.10	0.00	0.02	0.13	0.00	0.00	20.9
15	55	-0	2247	0	0	0	-1239	--	--	16.08	16.08	0.29	0.02	0.02	0.14	0.00	0.00	20.9
16	55	-0	2054	0	0	0	163	--	--	16.08	16.08	0.10	0.00	0.02	0.13	0.00	0.00	20.9
17	55	-0	2230	0	0	0	15	--	--	16.08	16.08	0.10	0.00	0.02	0.14	0.00	0.00	20.9
18	55	-0	3778	0	0	0	-2122	--	--	16.08	16.08	0.18	0.04	0.03	0.24	0.00	0.00	20.9
19	55	-0	3824	0	0	0	444	--	--	16.08	16.08	0.00	0.01	0.03	0.24	0.00	0.00	20.9
20	55	-0	4573	0	0	0	-2955	--	--	16.08	16.08	0.18	0.05	0.04	0.29	0.00	0.00	20.9
37	55	-0	3439	0	0	0	-2137	--	--	16.08	16.08	0.18	0.04	0.03	0.22	0.00	0.00	20.9
38	55	-0	3516	0	0	0	582	--	--	16.08	16.08	0.00	0.01	0.03	0.22	0.00	0.00	20.9
39	55	-0	4765	0	0	0	-3526	--	--	16.08	16.08	0.18	0.06	0.04	0.30	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 200 NI 1637 NF 1552 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	1835	0	0	0	-1648	--	--	16.08	16.08	0.18	0.03	0.02	0.12	0.00	0.00	20.9
2	0	-0	1392	0	0	0	-1288	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
3	0	-0	1447	0	0	0	-1372	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
4	0	-0	1376	0	0	0	-1163	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
5	0	-0	1431	0	0	0	-1247	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
6	0	-0	1322	0	0	0	-1147	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
7	0	-0	1506	0	0	0	-1425	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
8	0	-0	1317	0	0	0	-1110	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
9	0	-0	1501	0	0	0	-1388	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
10	0	-0	1392	0	0	0	-1288	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
11	0	-0	1447	0	0	0	-1372	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
12	0	-0	1376	0	0	0	-1163	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
13	0	-0	1431	0	0	0	-1247	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
14	0	-0	1322	0	0	0	-1147	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
15	0	-0	1506	0	0	0	-1425	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
16	0	-0	1317	0	0	0	-1110	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
17	0	-0	1501	0	0	0	-1388	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
18	0	-0	2413	0	0	0	-2399	--	--	16.08	16.08	0.18	0.04	0.02	0.15	0.00	0.00	20.9
19	0	-0	2561	0	0	0	-1961	--	--	16.08	16.08	0.18	0.03	0.02	0.16	0.00	0.00	20.9
20	0	-0	3355	0	0	0	-3430	--	--	16.08	16.08	0.18	0.06	0.03	0.21	0.00	0.00	20.9
37	0	-0	2154	0	0	0	-2375	--	--	16.08	16.08	0.18	0.04	0.02	0.14	0.00	0.00	20.9
38	0	-0	2400	0	0	0	-1644	--	--	16.08	16.08	0.18	0.03	0.02	0.15	0.00	0.00	20.9
39	0	-0	3725	0	0	0	-4093	--	--	16.08	16.08	0.18	0.07	0.03	0.23	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	1835	0	0	0	-1648	--	--	16.08	16.08	0.18	0.03	0.02	0.12	0.00	0.00	20.9
2	27	-0	1392	0	0	0	-1288	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
3	27	-0	1447	0	0	0	-1372	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
4	27	-0	1376	0	0	0	-1163	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
5	27	-0	1431	0	0	0	-1247	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
6	27	-0	1322	0	0	0	-1147	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
7	27	-0	1506	0	0	0	-1425	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
8	27	-0	1317	0	0	0	-1110	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
9	27	-0	1501	0	0	0	-1388	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
10	27	-0	1392	0	0	0	-1288	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
11	27	-0	1447	0	0	0	-1372	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
12	27	-0	1376	0	0	0	-1163	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
13	27	-0	1431	0	0	0	-1247	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
14	27	-0	1322	0	0	0	-1147	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
15	27	-0	1506	0	0	0	-1425	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
16	27	-0	1317	0	0	0	-1110	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
17	27	-0	1501	0	0	0	-1388	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
18	27	-0	2413	0	0	0	-2399	--	--	16.08	16.08	0.18	0.04	0.02	0.15	0.00	0.00	20.9
19	27	-0	2561	0	0	0	-1961	--	--	16.08	16.08	0.18	0.03	0.02	0.16	0.00	0.00	20.9
20	27	-0	3355	0	0	0	-3430	--	--	16.08	16.08	0.18	0.06	0.03	0.21	0.00	0.00	20.9
37	27	-0	2154	0	0	0	-2375	--	--	16.08	16.08	0.18	0.04	0.02	0.14	0.00	0.00	20.9
38	27	-0	2400	0	0	0	-1644	--	--	16.08	16.08	0.18	0.03	0.02	0.15	0.00	0.00	20.9
39	27	-0	3725	0	0	0	-4093	--	--	16.08	16.08	0.18	0.07	0.03	0.23	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	1835	0	0	0	-1648	--	--	16.08	16.08	0.18	0.03	0.02	0.12	0.00	0.00	20.9
2	55	-0	1392	0	0	0	-1288	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
3	55	-0	1447	0	0	0	-1372	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
4	55	-0	1376	0	0	0	-1163	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
5	55	-0	1431	0	0	0	-1247	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
6	55	-0	1322	0	0	0	-1147	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
7	55	-0	1506	0	0	0	-1425	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
8	55	-0	1317	0	0	0	-1110	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9

9	55	-0	1501	0	0	0	-1388	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
10	55	-0	1392	0	0	0	-1288	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
11	55	-0	1447	0	0	0	-1372	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
12	55	-0	1376	0	0	0	-1163	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
13	55	-0	1431	0	0	0	-1247	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
14	55	-0	1322	0	0	0	-1147	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
15	55	-0	1506	0	0	0	-1425	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
16	55	-0	1317	0	0	0	-1110	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
17	55	-0	1501	0	0	0	-1388	--	--	16.08	16.08	0.29	0.02	0.01	0.09	0.00	0.00	20.9
18	55	-0	2413	0	0	0	-2399	--	--	16.08	16.08	0.18	0.04	0.02	0.15	0.00	0.00	20.9
19	55	-0	2561	0	0	0	-1961	--	--	16.08	16.08	0.18	0.03	0.02	0.16	0.00	0.00	20.9
20	55	-0	3355	0	0	0	-3430	--	--	16.08	16.08	0.18	0.06	0.03	0.21	0.00	0.00	20.9
37	55	-0	2154	0	0	0	-2375	--	--	16.08	16.08	0.18	0.04	0.02	0.14	0.00	0.00	20.9
38	55	-0	2400	0	0	0	-1644	--	--	16.08	16.08	0.18	0.03	0.02	0.15	0.00	0.00	20.9
39	55	-0	3725	0	0	0	-4093	--	--	16.08	16.08	0.18	0.07	0.03	0.23	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 201 NI 1638 NF 1637 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	994	0	0	0	-1694	--	--	16.08	16.08	0.18	0.03	0.01	0.06	0.00	0.00	20.9
2	0	-0	726	0	0	0	-1313	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
3	0	-0	782	0	0	0	-1407	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
4	0	-0	748	0	0	0	-1199	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
5	0	-0	803	0	0	0	-1293	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
6	0	-0	669	0	0	0	-1164	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
7	0	-0	854	0	0	0	-1477	--	--	16.08	16.08	0.29	0.03	0.01	0.05	0.00	0.00	20.9
8	0	-0	676	0	0	0	-1129	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
9	0	-0	860	0	0	0	-1443	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
10	0	-0	726	0	0	0	-1313	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
11	0	-0	782	0	0	0	-1407	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
12	0	-0	748	0	0	0	-1199	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
13	0	-0	803	0	0	0	-1293	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
14	0	-0	669	0	0	0	-1164	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
15	0	-0	854	0	0	0	-1477	--	--	16.08	16.08	0.29	0.03	0.01	0.05	0.00	0.00	20.9
16	0	-0	676	0	0	0	-1129	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
17	0	-0	860	0	0	0	-1443	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
18	0	-0	1231	0	0	0	-2434	--	--	16.08	16.08	0.18	0.04	0.01	0.08	0.00	0.00	20.9
19	0	-0	1473	0	0	0	-2056	--	--	16.08	16.08	0.18	0.03	0.01	0.09	0.00	0.00	20.9
20	0	-0	2299	0	0	0	-3688	--	--	16.08	16.08	0.18	0.06	0.02	0.14	0.00	0.00	20.9
37	0	-0	1036	0	0	0	-2383	--	--	16.08	16.08	0.18	0.04	0.01	0.06	0.00	0.00	20.9
38	0	-0	1439	0	0	0	-1754	--	--	16.08	16.08	0.18	0.03	0.01	0.09	0.00	0.00	20.9
39	0	-0	2815	0	0	0	-4474	--	--	16.08	16.08	0.18	0.07	0.02	0.18	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	994	0	0	0	-1694	--	--	16.08	16.08	0.18	0.03	0.01	0.06	0.00	0.00	20.9
2	27	-0	726	0	0	0	-1313	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
3	27	-0	782	0	0	0	-1407	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
4	27	-0	748	0	0	0	-1199	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
5	27	-0	803	0	0	0	-1293	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
6	27	-0	669	0	0	0	-1164	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
7	27	-0	854	0	0	0	-1477	--	--	16.08	16.08	0.29	0.03	0.01	0.05	0.00	0.00	20.9
8	27	-0	676	0	0	0	-1129	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
9	27	-0	860	0	0	0	-1443	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
10	27	-0	726	0	0	0	-1313	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
11	27	-0	782	0	0	0	-1407	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
12	27	-0	748	0	0	0	-1199	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
13	27	-0	803	0	0	0	-1293	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
14	27	-0	669	0	0	0	-1164	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
15	27	-0	854	0	0	0	-1477	--	--	16.08	16.08	0.29	0.03	0.01	0.05	0.00	0.00	20.9
16	27	-0	676	0	0	0	-1129	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
17	27	-0	860	0	0	0	-1443	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
18	27	-0	1231	0	0	0	-2434	--	--	16.08	16.08	0.18	0.04	0.01	0.08	0.00	0.00	20.9
19	27	-0	1473	0	0	0	-2056	--	--	16.08	16.08	0.18	0.03	0.01	0.09	0.00	0.00	20.9
20	27	-0	2299	0	0	0	-3688	--	--	16.08	16.08	0.18	0.06	0.02	0.14	0.00	0.00	20.9
37	27	-0	1036	0	0	0	-2383	--	--	16.08	16.08	0.18	0.04	0.01	0.06	0.00	0.00	20.9
38	27	-0	1439	0	0	0	-1754	--	--	16.08	16.08	0.18	0.03	0.01	0.09	0.00	0.00	20.9
39	27	-0	2815	0	0	0	-4474	--	--	16.08	16.08	0.18	0.07	0.02	0.18	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	994	0	0	0	-1694	--	--	16.08	16.08	0.18	0.03	0.01	0.06	0.00	0.00	20.9
2	55	-0	726	0	0	0	-1313	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
3	55	-0	782	0	0	0	-1407	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
4	55	-0	748	0	0	0	-1199	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
5	55	-0	803	0	0	0	-1293	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
6	55	-0	669	0	0	0	-1164	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
7	55	-0	854	0	0	0	-1477	--	--	16.08	16.08	0.29	0.03	0.01	0.05	0.00	0.00	20.9
8	55	-0	676	0	0	0	-1129	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
9	55	-0	860	0	0	0	-1443	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
10	55	-0	726	0	0	0	-1313	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
11	55	-0	782	0	0	0	-1407	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
12	55	-0	748	0	0	0	-1199	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
13	55	-0	803	0	0	0	-1293	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
14	55	-0	669	0	0	0	-1164	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
15	55	-0	854	0	0	0	-1477	--	--	16.08	16.08	0.29	0.03	0.01	0.05	0.00	0.00	20.9
16	55	-0	676	0	0	0	-1129	--	--	16.08	16.08	0.29	0.02	0.01	0.04	0.00	0.00	20.9
17	55	-0	860	0	0	0	-1443	--	--	16.08	16.08	0.29	0.02	0.01	0.05	0.00	0.00	20.9
18	55	-0	1231	0	0	0	-2434	--	--	16.08	16.08	0.18	0.04	0.01	0.08	0.00	0.00	20.9
19	55	-0	1473	0	0	0	-2056	--	--	16.08	16.08	0.18	0.03	0.01	0.09	0.00	0.00	20.9
20	55	-0	2299	0	0	0	-3688	--	--	16.08	16.08	0.18	0.06	0.02	0.14	0.00	0.00	20.9
37	55	-0	1036	0	0	0	-2383	--	--	16.08	16.08	0.18	0.04	0.01	0.06	0.00	0.00	20.9
38	55	-0	1439	0	0	0	-1754	--	--	16.08	16.08	0.18	0.03	0.01	0.09	0.00	0.00	20.9
39	55	-0	2815	0	0	0	-4474	--	--	16.08	16.08	0.18	0.07	0.02	0.18	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 202 NI 1577 NF 1638 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice resistenza			aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	204	0	0	0	-1585	--	--	16.08	16.08	0.18	0.03	0.00	0.01	0.00	0.00	20.9
2	0	-0	101	0	0	0	-1215	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
3	0	-0	155	0	0	0	-1320	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
4	0	-0	159	0	0	0	-1119	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
5	0	-0	213	0	0	0	-1223	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
6	0	-0	58	0	0	0	-1060	--	--	16.08	16.08	0.29	0.02	0.00	0.00	0.00	0.00	20.9
7	0	-0	239	0	0	0	-1408	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
8	0	-0	75	0	0	0	-1031	--	--	16.08	16.08	0.29	0.02	0.00	0.00	0.00	0.00	20.9
9	0	-0	256	0	0	0	-1379	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
10	0	-0	101	0	0	0	-1215	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
11	0	-0	155	0	0	0	-1320	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
12	0	-0	159	0	0	0	-1119	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
13	0	-0	213	0	0	0	-1223	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
14	0	-0	58	0	0	0	-1060	--	--	16.08	16.08	0.29	0.02	0.00	0.00	0.00	0.00	20.9
15	0	-0	239	0	0	0	-1408	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
16	0	-0	75	0	0	0	-1031	--	--	16.08	16.08	0.29	0.02	0.00	0.00	0.00	0.00	20.9
17	0	-0	256	0	0	0	-1379	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
18	0	-0	135	0	0	0	-2253	--	--	16.08	16.08	0.18	0.04	0.00	0.01	0.00	0.00	20.9
19	0	-0	471	0	0	0	-1957	--	--	16.08	16.08	0.18	0.03	0.00	0.03	0.00	0.00	20.9
20	0	-0	1319	0	0	0	-3758	--	--	16.08	16.08	0.18	0.06	0.01	0.08	0.00	0.00	20.9
37	0	-0	-8	0	0	0	-2191	--	--	16.08	16.08	0.18	0.04	0.00	0.00	0.00	0.00	20.9
38	0	-0	552	0	0	0	-1691	--	--	16.08	16.08	0.18	0.03	0.00	0.03	0.00	0.00	20.9
39	0	-0	1965	0	0	0	-4694	--	--	16.08	16.08	0.18	0.08	0.02	0.12	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	204	0	0	0	-1585	--	--	16.08	16.08	0.18	0.03	0.00	0.01	0.00	0.00	20.9
2	27	-0	101	0	0	0	-1215	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
3	27	-0	155	0	0	0	-1320	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
4	27	-0	159	0	0	0	-1119	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
5	27	-0	213	0	0	0	-1223	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
6	27	-0	58	0	0	0	-1060	--	--	16.08	16.08	0.29	0.02	0.00	0.00	0.00	0.00	20.9
7	27	-0	239	0	0	0	-1408	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
8	27	-0	75	0	0	0	-1031	--	--	16.08	16.08	0.29	0.02	0.00	0.00	0.00	0.00	20.9
9	27	-0	256	0	0	0	-1379	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
10	27	-0	101	0	0	0	-1215	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
11	27	-0	155	0	0	0	-1320	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
12	27	-0	159	0	0	0	-1119	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
13	27	-0	213	0	0	0	-1223	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
14	27	-0	58	0	0	0	-1060	--	--	16.08	16.08	0.29	0.02	0.00	0.00	0.00	0.00	20.9
15	27	-0	239	0	0	0	-1408	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
16	27	-0	75	0	0	0	-1031	--	--	16.08	16.08	0.29	0.02	0.00	0.00	0.00	0.00	20.9
17	27	-0	256	0	0	0	-1379	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
18	27	-0	135	0	0	0	-2253	--	--	16.08	16.08	0.18	0.04	0.00	0.01	0.00	0.00	20.9
19	27	-0	471	0	0	0	-1957	--	--	16.08	16.08	0.18	0.03	0.00	0.03	0.00	0.00	20.9
20	27	-0	1319	0	0	0	-3758	--	--	16.08	16.08	0.18	0.06	0.01	0.08	0.00	0.00	20.9
37	27	-0	-8	0	0	0	-2191	--	--	16.08	16.08	0.18	0.04	0.00	0.00	0.00	0.00	20.9
38	27	-0	552	0	0	0	-1691	--	--	16.08	16.08	0.18	0.03	0.00	0.03	0.00	0.00	20.9
39	27	-0	1965	0	0	0	-4694	--	--	16.08	16.08	0.18	0.08	0.02	0.12	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	204	0	0	0	-1585	--	--	16.08	16.08	0.18	0.03	0.00	0.01	0.00	0.00	20.9
2	55	-0	101	0	0	0	-1215	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
3	55	-0	155	0	0	0	-1320	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
4	55	-0	159	0	0	0	-1119	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
5	55	-0	213	0	0	0	-1223	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
6	55	-0	58	0	0	0	-1060	--	--	16.08	16.08	0.29	0.02	0.00	0.00	0.00	0.00	20.9
7	55	-0	239	0	0	0	-1408	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
8	55	-0	75	0	0	0	-1031	--	--	16.08	16.08	0.29	0.02	0.00	0.00	0.00	0.00	20.9
9	55	-0	256	0	0	0	-1379	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
10	55	-0	101	0	0	0	-1215	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
11	55	-0	155	0	0	0	-1320	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
12	55	-0	159	0	0	0	-1119	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
13	55	-0	213	0	0	0	-1223	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
14	55	-0	58	0	0	0	-1060	--	--	16.08	16.08	0.29	0.02	0.00	0.00	0.00	0.00	20.9
15	55	-0	239	0	0	0	-1408	--	--	16.08	16.08	0.29	0.02	0.00	0.01	0.00	0.00	20.9
16	55	-0	75	0	0	0	-1031	--	--	16.08	16.08	0.29	0.02	0.00	0.00	0.00	0.00	20.9
17	55	-0	256	0	0	0	-1379	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
18	55	-0	135	0	0	0	-2253	--	--	16.08	16.08	0.18	0.04	0.00	0.01	0.00	0.00	20.9
19	55	-0	471	0	0	0	-1957	--	--	16.08	16.08	0.18	0.03	0.00	0.03	0.00	0.00	20.9
20	55	-0	1319	0	0	0	-3758	--	--	16.08	16.08	0.18	0.06	0.01	0.08	0.00	0.00	20.9
37	55	-0	-8	0	0	0	-2191	--	--	16.08	16.08	0.18	0.04	0.00	0.00	0.00	0.00	20.9
38	55	-0	552	0	0	0	-1691	--	--	16.08	16.08	0.18	0.03	0.00	0.03	0.00	0.00	20.9
39	55	-0	1965	0	0	0	-4694	--	--	16.08	16.08	0.18	0.08	0.02	0.12	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 203 NI 1578 NF 1577 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice resistenza			aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx	cmq/m		cm
1	0	-0	-589	0	0	0	-1632	--	--	16.08	16.08	0.18	0.03	0.00	0.04	0.00	0.00	20.9
2	0	-0	-527	0	0	0	-1274	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
3	0	-0	-475	0	0	0	-1360	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
4	0	-0	-430	0	0	0	-1151	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
5	0	-0	-379	0	0	0	-1237	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
6	0	-0	-554	0	0	0	-1132	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
7	0	-0	-381	0	0	0	-1416	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
8	0	-0	-525	0	0	0	-1095	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
9	0	-0	-352	0	0	0	-1380	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
10	0	-0	-527	0	0	0	-1274	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
11	0	-0	-475	0	0	0	-1360	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
12	0	-0	-430	0	0	0	-1151	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
13	0	-0	-379	0	0	0	-1237	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
14	0	-0	-554	0	0	0	-1132	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
15	0	-0	-381	0	0	0	-1416	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
16	0	-0	-525	0	0	0	-1095	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9

17	0	-0	-352	0	0	0	-1380	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
18	0	-0	-951	0	0	0	-2370	--	--	16.08	16.08	0.18	0.04	0.01	0.06	0.00	0.00	20.9
19	0	-0	-510	0	0	0	-1940	--	--	16.08	16.08	0.18	0.03	0.00	0.03	0.00	0.00	20.9
20	0	-0	374	0	0	0	-3660	--	--	16.08	16.08	0.18	0.06	0.00	0.02	0.00	0.00	20.9
37	0	-0	-1052	0	0	0	-2347	--	--	16.08	16.08	0.18	0.04	0.01	0.07	0.00	0.00	20.9
38	0	-0	-317	0	0	0	-1629	--	--	16.08	16.08	0.18	0.03	0.00	0.02	0.00	0.00	20.9
39	0	-0	1157	0	0	0	-4786	--	--	16.08	16.08	0.18	0.08	0.01	0.07	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-589	0	0	0	-1632	--	--	16.08	16.08	0.18	0.03	0.00	0.04	0.00	0.00	20.9
2	27	-0	-527	0	0	0	-1274	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
3	27	-0	-475	0	0	0	-1360	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
4	27	-0	-430	0	0	0	-1151	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
5	27	-0	-379	0	0	0	-1237	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
6	27	-0	-554	0	0	0	-1132	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
7	27	-0	-381	0	0	0	-1416	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
8	27	-0	-525	0	0	0	-1095	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
9	27	-0	-352	0	0	0	-1380	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
10	27	-0	-527	0	0	0	-1274	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
11	27	-0	-475	0	0	0	-1360	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
12	27	-0	-430	0	0	0	-1151	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
13	27	-0	-379	0	0	0	-1237	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
14	27	-0	-554	0	0	0	-1132	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
15	27	-0	-381	0	0	0	-1416	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
16	27	-0	-525	0	0	0	-1095	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
17	27	-0	-352	0	0	0	-1380	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
18	27	-0	-951	0	0	0	-2370	--	--	16.08	16.08	0.18	0.04	0.01	0.06	0.00	0.00	20.9
19	27	-0	-510	0	0	0	-1940	--	--	16.08	16.08	0.18	0.03	0.00	0.03	0.00	0.00	20.9
20	27	-0	374	0	0	0	-3660	--	--	16.08	16.08	0.18	0.06	0.00	0.02	0.00	0.00	20.9
37	27	-0	-1052	0	0	0	-2347	--	--	16.08	16.08	0.18	0.04	0.01	0.07	0.00	0.00	20.9
38	27	-0	-317	0	0	0	-1629	--	--	16.08	16.08	0.18	0.03	0.00	0.02	0.00	0.00	20.9
39	27	-0	1157	0	0	0	-4786	--	--	16.08	16.08	0.18	0.08	0.01	0.07	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	-589	0	0	0	-1632	--	--	16.08	16.08	0.18	0.03	0.00	0.04	0.00	0.00	20.9
2	55	-0	-527	0	0	0	-1274	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
3	55	-0	-475	0	0	0	-1360	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
4	55	-0	-430	0	0	0	-1151	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
5	55	-0	-379	0	0	0	-1237	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
6	55	-0	-554	0	0	0	-1132	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
7	55	-0	-381	0	0	0	-1416	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
8	55	-0	-525	0	0	0	-1095	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
9	55	-0	-352	0	0	0	-1380	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
10	55	-0	-527	0	0	0	-1274	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
11	55	-0	-475	0	0	0	-1360	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
12	55	-0	-430	0	0	0	-1151	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
13	55	-0	-379	0	0	0	-1237	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
14	55	-0	-554	0	0	0	-1132	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
15	55	-0	-381	0	0	0	-1416	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
16	55	-0	-525	0	0	0	-1095	--	--	16.08	16.08	0.29	0.02	0.00	0.03	0.00	0.00	20.9
17	55	-0	-352	0	0	0	-1380	--	--	16.08	16.08	0.29	0.02	0.00	0.02	0.00	0.00	20.9
18	55	-0	-951	0	0	0	-2370	--	--	16.08	16.08	0.18	0.04	0.01	0.06	0.00	0.00	20.9
19	55	-0	-510	0	0	0	-1940	--	--	16.08	16.08	0.18	0.03	0.00	0.03	0.00	0.00	20.9
20	55	-0	374	0	0	0	-3660	--	--	16.08	16.08	0.18	0.06	0.00	0.02	0.00	0.00	20.9
37	55	-0	-1052	0	0	0	-2347	--	--	16.08	16.08	0.18	0.04	0.01	0.07	0.00	0.00	20.9
38	55	-0	-317	0	0	0	-1629	--	--	16.08	16.08	0.18	0.03	0.00	0.02	0.00	0.00	20.9
39	55	-0	1157	0	0	0	-4786	--	--	16.08	16.08	0.18	0.08	0.01	0.07	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 204 NI 1594 NF 1578 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--																	
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm

1	0	-0	-1456	0	0	0	-1613	--	--	16.08	16.08	0.18	0.03	0.01	0.09	0.00	0.00	20.9
2	0	-0	-1211	0	0	0	-1247	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
3	0	-0	-1171	0	0	0	-1342	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
4	0	-0	-1069	0	0	0	-1139	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
5	0	-0	-1029	0	0	0	-1234	--	--	16.08	16.08	0.29	0.02	0.01	0.06	0.00	0.00	20.9
6	0	-0	-1208	0	0	0	-1099	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
7	0	-0	-1075	0	0	0	-1414	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
8	0	-0	-1165	0	0	0	-1067	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
9	0	-0	-1033	0	0	0	-1382	--	--	16.08	16.08	0.29	0.02	0.01	0.06	0.00	0.00	20.9
10	0	-0	-1211	0	0	0	-1247	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
11	0	-0	-1171	0	0	0	-1342	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
12	0	-0	-1069	0	0	0	-1139	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
13	0	-0	-1029	0	0	0	-1234	--	--	16.08	16.08	0.29	0.02	0.01	0.06	0.00	0.00	20.9
14	0	-0	-1208	0	0	0	-1099	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
15	0	-0	-1075	0	0	0	-1414	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
16	0	-0	-1165	0	0	0	-1067	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
17	0	-0	-1033	0	0	0	-1382	--	--	16.08	16.08	0.29	0.02	0.01	0.06	0.00	0.00	20.9
18	0	-0	-2108	0	0	0	-2319	--	--	16.08	16.08	0.18	0.04	0.02	0.13	0.00	0.00	20.9
19	0	-0	-1536	0	0	0	-1965	--	--	16.08	16.08	0.18	0.03	0.01	0.10	0.00	0.00	20.9
20	0	-0	-544	0	0	0	-3700	--	--	16.08	16.08	0.18	0.06	0.00	0.03	0.00	0.00	20.9
37	0	-0	-2181	0	0	0	-2268	--	--	16.08	16.08	0.18	0.04	0.02	0.14	0.00	0.00	20.9
38	0	-0	-1227	0	0	0	-1678	--	--	16.08	16.08	0.18	0.03	0.01	0.08	0.00	0.00	20.9
39	0	-0	426	0	0	0	-4801	--	--	16.08	16.08	0.18	0.08	0.00	0.03	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-1456	0	0	0	-1613	--	--	16.08	16.08	0.18	0.03	0.01	0.09	0.00	0.00	20.9
2	27	-0	-1211	0	0	0	-1247	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
3	27	-0	-1171	0	0	0	-1342	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
4	27	-0	-1069	0	0	0	-1139	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
5	27	-0	-1029	0	0	0	-1234	--	--	16.08	16.08	0.29	0.02	0.01	0.06	0.00	0.00	20.9
6	27	-0	-1208	0	0	0	-1099	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
7	27	-0	-1075	0	0	0	-1414	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
8	27	-0	-1165	0	0	0	-1067	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
9	27	-0	-1033	0	0	0	-1382	--	--	16.08	16.08	0.29	0.02	0.01	0.06	0.00	0.00	20.9
10	27	-0	-1211	0	0	0	-1247	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
11	27	-0	-1171	0	0	0	-1342	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
12	27	-0	-1069	0	0	0	-1139	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9

13	27	-0	-1029	0	0	0	-1234	--	--	16.08	16.08	0.29	0.02	0.01	0.06	0.00	0.00	20.9
14	27	-0	-1208	0	0	0	-1099	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
15	27	-0	-1075	0	0	0	-1414	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
16	27	-0	-1165	0	0	0	-1067	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
17	27	-0	-1033	0	0	0	-1382	--	--	16.08	16.08	0.29	0.02	0.01	0.06	0.00	0.00	20.9
18	27	-0	-2108	0	0	0	-2319	--	--	16.08	16.08	0.18	0.04	0.02	0.13	0.00	0.00	20.9
19	27	-0	-1536	0	0	0	-1965	--	--	16.08	16.08	0.18	0.03	0.01	0.10	0.00	0.00	20.9
20	27	-0	-544	0	0	0	-3700	--	--	16.08	16.08	0.18	0.06	0.00	0.03	0.00	0.00	20.9
37	27	-0	-2181	0	0	0	-2268	--	--	16.08	16.08	0.18	0.04	0.02	0.14	0.00	0.00	20.9
38	27	-0	-1227	0	0	0	-1678	--	--	16.08	16.08	0.18	0.03	0.01	0.08	0.00	0.00	20.9
39	27	-0	426	0	0	0	-4801	--	--	16.08	16.08	0.18	0.08	0.00	0.03	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	-1456	0	0	0	-1613	--	--	16.08	16.08	0.18	0.03	0.01	0.09	0.00	0.00	20.9
2	55	-0	-1211	0	0	0	-1247	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
3	55	-0	-1171	0	0	0	-1342	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
4	55	-0	-1069	0	0	0	-1139	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
5	55	-0	-1029	0	0	0	-1234	--	--	16.08	16.08	0.29	0.02	0.01	0.06	0.00	0.00	20.9
6	55	-0	-1208	0	0	0	-1099	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
7	55	-0	-1075	0	0	0	-1414	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
8	55	-0	-1165	0	0	0	-1067	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
9	55	-0	-1033	0	0	0	-1382	--	--	16.08	16.08	0.29	0.02	0.01	0.06	0.00	0.00	20.9
10	55	-0	-1211	0	0	0	-1247	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
11	55	-0	-1171	0	0	0	-1342	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
12	55	-0	-1069	0	0	0	-1139	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
13	55	-0	-1029	0	0	0	-1234	--	--	16.08	16.08	0.29	0.02	0.01	0.06	0.00	0.00	20.9
14	55	-0	-1208	0	0	0	-1099	--	--	16.08	16.08	0.29	0.02	0.01	0.08	0.00	0.00	20.9
15	55	-0	-1075	0	0	0	-1414	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
16	55	-0	-1165	0	0	0	-1067	--	--	16.08	16.08	0.29	0.02	0.01	0.07	0.00	0.00	20.9
17	55	-0	-1033	0	0	0	-1382	--	--	16.08	16.08	0.29	0.02	0.01	0.06	0.00	0.00	20.9
18	55	-0	-2108	0	0	0	-2319	--	--	16.08	16.08	0.18	0.04	0.02	0.13	0.00	0.00	20.9
19	55	-0	-1536	0	0	0	-1965	--	--	16.08	16.08	0.18	0.03	0.01	0.10	0.00	0.00	20.9
20	55	-0	-544	0	0	0	-3700	--	--	16.08	16.08	0.18	0.06	0.00	0.03	0.00	0.00	20.9
37	55	-0	-2181	0	0	0	-2268	--	--	16.08	16.08	0.18	0.04	0.02	0.14	0.00	0.00	20.9
38	55	-0	-1227	0	0	0	-1678	--	--	16.08	16.08	0.18	0.03	0.01	0.08	0.00	0.00	20.9
39	55	-0	426	0	0	0	-4801	--	--	16.08	16.08	0.18	0.08	0.00	0.03	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 205 NI 1550 NF 1594 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-2296	0	0	0	-1403	--	--	16.08	16.08	0.18	0.02	0.02	0.14	0.00	0.00	20.9
2	0	-0	-1867	0	0	0	-1069	--	--	16.08	16.08	0.29	0.02	0.02	0.12	0.00	0.00	20.9
3	0	-0	-1865	0	0	0	-1168	--	--	16.08	16.08	0.29	0.02	0.02	0.12	0.00	0.00	20.9
4	0	-0	-1667	0	0	0	-991	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
5	0	-0	-1665	0	0	0	-1089	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
6	0	-0	-1799	0	0	0	55	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
7	0	-0	-1793	0	0	0	-1255	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
8	0	-0	-1740	0	0	0	46	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
9	0	-0	-1733	0	0	0	-1232	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
10	0	-0	-1867	0	0	0	-1069	--	--	16.08	16.08	0.29	0.02	0.02	0.12	0.00	0.00	20.9
11	0	-0	-1865	0	0	0	-1168	--	--	16.08	16.08	0.29	0.02	0.02	0.12	0.00	0.00	20.9
12	0	-0	-1667	0	0	0	-991	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
13	0	-0	-1665	0	0	0	-1089	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
14	0	-0	-1799	0	0	0	55	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
15	0	-0	-1793	0	0	0	-1255	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
16	0	-0	-1740	0	0	0	46	--	--	16.08	16.08	0.10	0.00	0.01	0.11	0.00	0.00	20.9
17	0	-0	-1733	0	0	0	-1232	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
18	0	-0	-3220	0	0	0	-2005	--	--	16.08	16.08	0.18	0.03	0.03	0.20	0.00	0.00	20.9
19	0	-0	-2474	0	0	0	-1776	--	--	16.08	16.08	0.18	0.03	0.02	0.16	0.00	0.00	20.9
20	0	-0	-1259	0	0	0	-3835	--	--	16.08	16.08	0.18	0.06	0.01	0.08	0.00	0.00	20.9
37	0	-0	-3291	0	0	0	-1925	--	--	16.08	16.08	0.18	0.03	0.03	0.21	0.00	0.00	20.9
38	0	-0	-2049	0	0	0	-1544	--	--	16.08	16.08	0.18	0.03	0.02	0.13	0.00	0.00	20.9
39	0	-0	-23	0	0	0	-4975	--	--	16.08	16.08	0.18	0.08	0.00	0.00	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-2296	0	0	0	-1403	--	--	16.08	16.08	0.18	0.02	0.02	0.14	0.00	0.00	20.9
2	27	-0	-1867	0	0	0	-1069	--	--	16.08	16.08	0.29	0.02	0.02	0.12	0.00	0.00	20.9
3	27	-0	-1865	0	0	0	-1168	--	--	16.08	16.08	0.29	0.02	0.02	0.12	0.00	0.00	20.9
4	27	-0	-1667	0	0	0	-991	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
5	27	-0	-1665	0	0	0	-1089	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
6	27	-0	-1799	0	0	0	-927	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
7	27	-0	-1793	0	0	0	-1255	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
8	27	-0	-1740	0	0	0	-903	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
9	27	-0	-1733	0	0	0	-1232	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
10	27	-0	-1867	0	0	0	-1069	--	--	16.08	16.08	0.29	0.02	0.02	0.12	0.00	0.00	20.9
11	27	-0	-1865	0	0	0	-1168	--	--	16.08	16.08	0.29	0.02	0.02	0.12	0.00	0.00	20.9
12	27	-0	-1667	0	0	0	-991	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
13	27	-0	-1665	0	0	0	-1089	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
14	27	-0	-1799	0	0	0	-927	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
15	27	-0	-1793	0	0	0	-1255	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
16	27	-0	-1740	0	0	0	-903	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
17	27	-0	-1733	0	0	0	-1232	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
18	27	-0	-3220	0	0	0	-2005	--	--	16.08	16.08	0.18	0.03	0.03	0.20	0.00	0.00	20.9
19	27	-0	-2474	0	0	0	-1776	--	--	16.08	16.08	0.18	0.03	0.02	0.16	0.00	0.00	20.9
20	27	-0	-1259	0	0	0	-3835	--	--	16.08	16.08	0.18	0.06	0.01	0.08	0.00	0.00	20.9
37	27	-0	-3291	0	0	0	-1925	--	--	16.08	16.08	0.18	0.03	0.03	0.21	0.00	0.00	20.9
38	27	-0	-2049	0	0	0	-1544	--	--	16.08	16.08	0.18	0.03	0.02	0.13	0.00	0.00	20.9
39	27	-0	-23	0	0	0	-4975	--	--	16.08	16.08	0.18	0.08	0.00	0.00	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	-2296	0	0	0	-1403	--	--	16.08	16.08	0.18	0.02	0.02	0.14	0.00	0.00	20.9
2	55	-0	-1867	0	0	0	-1069	--	--	16.08	16.08	0.29	0.02	0.02	0.12	0.00	0.00	20.9
3	55	-0	-1865	0	0	0	-1168	--	--	16.08	16.08	0.29	0.02	0.02	0.12	0.00	0.00	20.9
4	55	-0	-1667	0	0	0	-991	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
5	55	-0	-1665	0	0	0	-1089	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
6	55	-0	-1799	0	0	0	-927	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
7	55	-0	-1793	0	0	0	-1255	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
8	55	-0	-1740	0	0	0	-903	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9

9	55	-0	-1733	0	0	0	-1232	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
10	55	-0	-1867	0	0	0	-1069	--	--	16.08	16.08	0.29	0.02	0.02	0.12	0.00	0.00	20.9
11	55	-0	-1865	0	0	0	-1168	--	--	16.08	16.08	0.29	0.02	0.02	0.12	0.00	0.00	20.9
12	55	-0	-1667	0	0	0	-991	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
13	55	-0	-1665	0	0	0	-1089	--	--	16.08	16.08	0.29	0.02	0.01	0.10	0.00	0.00	20.9
14	55	-0	-1799	0	0	0	-927	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
15	55	-0	-1793	0	0	0	-1255	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
16	55	-0	-1740	0	0	0	-903	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
17	55	-0	-1733	0	0	0	-1232	--	--	16.08	16.08	0.29	0.02	0.01	0.11	0.00	0.00	20.9
18	55	-0	-3220	0	0	0	-2005	--	--	16.08	16.08	0.18	0.03	0.03	0.20	0.00	0.00	20.9
19	55	-0	-2474	0	0	0	-1776	--	--	16.08	16.08	0.18	0.03	0.02	0.16	0.00	0.00	20.9
20	55	-0	-1259	0	0	0	-3835	--	--	16.08	16.08	0.18	0.06	0.01	0.08	0.00	0.00	20.9
37	55	-0	-3291	0	0	0	-1925	--	--	16.08	16.08	0.18	0.03	0.03	0.21	0.00	0.00	20.9
38	55	-0	-2049	0	0	0	-1544	--	--	16.08	16.08	0.18	0.03	0.02	0.13	0.00	0.00	20.9
39	55	-0	-23	0	0	0	-4975	--	--	16.08	16.08	0.18	0.08	0.00	0.00	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 206 NI 1538 NF 1550 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm		daN			daN*m				cmq			Fx,M	Bielle	V,Mx		cmq/m	cm
1	0	-0	-2855	0	0	0	726	--	--	16.08	16.08	0.00	0.01	0.02	0.18	0.00	0.00	20.9
2	0	-0	-2333	0	0	0	686	--	--	16.08	16.08	0.10	0.01	0.02	0.15	0.00	0.00	20.9
3	0	-0	-2343	0	0	0	576	--	--	16.08	16.08	0.10	0.01	0.02	0.15	0.00	0.00	20.9
4	0	-0	-2049	0	0	0	541	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
5	0	-0	-2060	0	0	0	431	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
6	0	-0	-2222	0	0	0	763	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
7	0	-0	-2256	0	0	0	397	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
8	0	-0	-2137	0	0	0	720	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
9	0	-0	-2171	0	0	0	354	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
10	0	-0	-2333	0	0	0	686	--	--	16.08	16.08	0.10	0.01	0.02	0.15	0.00	0.00	20.9
11	0	-0	-2343	0	0	0	576	--	--	16.08	16.08	0.10	0.01	0.02	0.15	0.00	0.00	20.9
12	0	-0	-2049	0	0	0	541	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
13	0	-0	-2060	0	0	0	431	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
14	0	-0	-2222	0	0	0	763	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
15	0	-0	-2256	0	0	0	397	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
16	0	-0	-2137	0	0	0	720	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
17	0	-0	-2171	0	0	0	354	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
18	0	-0	-4249	0	0	0	1197	--	--	16.08	16.08	0.00	0.02	0.04	0.27	0.00	0.00	20.9
19	0	-0	-3147	0	0	0	532	--	--	16.08	16.08	0.00	0.01	0.03	0.20	0.00	0.00	20.9
20	0	-0	-1650	0	0	0	-3916	--	--	16.08	16.08	0.18	0.06	0.01	0.10	0.00	0.00	20.9
37	0	-0	-4344	0	0	0	1372	--	--	16.08	16.08	0.00	0.02	0.04	0.27	0.00	0.00	20.9
38	0	-0	-2507	0	0	0	264	--	--	16.08	16.08	0.00	0.00	0.02	0.16	0.00	0.00	20.9
39	0	-0	-12	0	0	0	-5657	--	--	16.08	16.08	0.18	0.09	0.00	0.00	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	-2855	0	0	0	-831	--	--	16.08	16.08	0.18	0.01	0.02	0.18	0.00	0.00	20.9
2	27	-0	-2333	0	0	0	686	--	--	16.08	16.08	0.10	0.01	0.02	0.15	0.00	0.00	20.9
3	27	-0	-2343	0	0	0	-702	--	--	16.08	16.08	0.29	0.01	0.02	0.15	0.00	0.00	20.9
4	27	-0	-2049	0	0	0	-577	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
5	27	-0	-2060	0	0	0	-692	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
6	27	-0	-2222	0	0	0	763	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
7	27	-0	-2256	0	0	0	-833	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
8	27	-0	-2137	0	0	0	720	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
9	27	-0	-2171	0	0	0	-830	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
10	27	-0	-2333	0	0	0	686	--	--	16.08	16.08	0.10	0.01	0.02	0.15	0.00	0.00	20.9
11	27	-0	-2343	0	0	0	-702	--	--	16.08	16.08	0.29	0.01	0.02	0.15	0.00	0.00	20.9
12	27	-0	-2049	0	0	0	-577	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
13	27	-0	-2060	0	0	0	-692	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
14	27	-0	-2222	0	0	0	763	--	--	16.08	16.08	0.10	0.01	0.02	0.14	0.00	0.00	20.9
15	27	-0	-2256	0	0	0	-833	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
16	27	-0	-2137	0	0	0	720	--	--	16.08	16.08	0.10	0.01	0.02	0.13	0.00	0.00	20.9
17	27	-0	-2171	0	0	0	-830	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
18	27	-0	-4249	0	0	0	1197	--	--	16.08	16.08	0.00	0.02	0.04	0.27	0.00	0.00	20.9
19	27	-0	-3147	0	0	0	-1185	--	--	16.08	16.08	0.18	0.02	0.03	0.20	0.00	0.00	20.9
20	27	-0	-1650	0	0	0	-3916	--	--	16.08	16.08	0.18	0.06	0.01	0.10	0.00	0.00	20.9
37	27	-0	-4344	0	0	0	1372	--	--	16.08	16.08	0.00	0.02	0.04	0.27	0.00	0.00	20.9
38	27	-0	-2507	0	0	0	-1104	--	--	16.08	16.08	0.18	0.02	0.02	0.16	0.00	0.00	20.9
39	27	-0	-12	0	0	0	-5657	--	--	16.08	16.08	0.18	0.09	0.00	0.00	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	55	-0	-2855	0	0	0	-831	--	--	16.08	16.08	0.18	0.01	0.02	0.18	0.00	0.00	20.9
2	55	-0	-2333	0	0	0	-587	--	--	16.08	16.08	0.29	0.01	0.02	0.15	0.00	0.00	20.9
3	55	-0	-2343	0	0	0	-702	--	--	16.08	16.08	0.29	0.01	0.02	0.15	0.00	0.00	20.9
4	55	-0	-2049	0	0	0	-577	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
5	55	-0	-2060	0	0	0	-692	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
6	55	-0	-2222	0	0	0	-448	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
7	55	-0	-2256	0	0	0	-833	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
8	55	-0	-2137	0	0	0	-446	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
9	55	-0	-2171	0	0	0	-830	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
10	55	-0	-2333	0	0	0	-587	--	--	16.08	16.08	0.29	0.01	0.02	0.15	0.00	0.00	20.9
11	55	-0	-2343	0	0	0	-702	--	--	16.08	16.08	0.29	0.01	0.02	0.15	0.00	0.00	20.9
12	55	-0	-2049	0	0	0	-577	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
13	55	-0	-2060	0	0	0	-692	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
14	55	-0	-2222	0	0	0	-448	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
15	55	-0	-2256	0	0	0	-833	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
16	55	-0	-2137	0	0	0	-446	--	--	16.08	16.08	0.29	0.01	0.02	0.13	0.00	0.00	20.9
17	55	-0	-2171	0	0	0	-830	--	--	16.08	16.08	0.29	0.01	0.02	0.14	0.00	0.00	20.9
18	55	-0	-4249	0	0	0	-1121	--	--	16.08	16.08	0.18	0.02	0.04	0.27	0.00	0.00	20.9
19	55	-0	-3147	0	0	0	-1185	--	--	16.08	16.08	0.18	0.02	0.03	0.20	0.00	0.00	20.9
20	55	-0	-1650	0	0	0	-3916	--	--	16.08	16.08	0.18	0.06	0.01	0.10	0.00	0.00	20.9
37	55	-0	-4344	0	0	0	-998	--	--	16.08	16.08	0.18	0.02	0.04	0.27	0.00	0.00	20.9
38	55	-0	-2507	0	0	0	-1104	--	--	16.08	16.08	0.18	0.02	0.02	0.16	0.00	0.00	20.9
39	55	-0	-12	0	0	0	-5657	--	--	16.08	16.08	0.18	0.09	0.00	0.00	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

ASTA NUM. 207 NI 1320 NF 1321 SEZ. Tr B= 1.500 H= 1.000 b= 0.500 h= 0.300 (trave di fondazione)

armatura base = 4 X 2.01 per le armature aggiuntive consultare il tabulato

NC	x	Fx	Fy	Fz	Mx	My	Mz	APOST	AANT	AINF	ASUP	x/d	Indice	resistenza		aswta	aswto	PASSO
	cm	daN			daN*m			cmq					Fx,M	Bielle	V,Mx	cmq/m			cm
1	0	-0	1863	0	0	0	764	--	--	16.08	16.08	0.00	0.01	0.02	0.12	0.00	0.00	20.9
2	0	-0	1415	0	0	0	630	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
3	0	-0	1390	0	0	0	635	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
4	0	-0	1476	0	0	0	541	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
5	0	-0	1451	0	0	0	546	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
6	0	-0	1466	0	0	0	592	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
7	0	-0	1382	0	0	0	611	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
8	0	-0	1484	0	0	0	565	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
9	0	-0	1401	0	0	0	584	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
10	0	-0	1415	0	0	0	630	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
11	0	-0	1390	0	0	0	635	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
12	0	-0	1476	0	0	0	541	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
13	0	-0	1451	0	0	0	546	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
14	0	-0	1466	0	0	0	592	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
15	0	-0	1382	0	0	0	611	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
16	0	-0	1484	0	0	0	565	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
17	0	-0	1401	0	0	0	584	--	--	16.08	16.08	0.10	0.01	0.01	0.09	0.00	0.00	20.9
18	0	-0	1897	0	0	0	996	--	--	16.08	16.08	0.00	0.02	0.02	0.12	0.00	0.00	20.9
19	0	-0	2094	0	0	0	723	--	--	16.08	16.08	0.00	0.01	0.02	0.13	0.00	0.00	20.9
20	0	-0	1953	0	0	0	850	--	--	16.08	16.08	0.00	0.01	0.02	0.12	0.00	0.00	20.9
37	0	-0	1762	0	0	0	1046	--	--	16.08	16.08	0.00	0.02	0.01	0.11	0.00	0.00	20.9
38	0	-0	2090	0	0	0	590	--	--	16.08	16.08	0.00	0.01	0.02	0.13	0.00	0.00	20.9
39	0	-0	1856	0	0	0	801	--	--	16.08	16.08	0.00	0.01	0.02	0.12	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	27	-0	1863	0	0	0	3254	--	--	16.08	16.08	0.00	0.06	0.02	0.12	0.00	0.00	20.9
2	27	-0	1415	0	0	0	2521	--	--	16.08	16.08	0.10	0.04	0.01	0.09	0.00	0.00	20.9
3	27	-0	1390	0	0	0	2493	--	--	16.08	16.08	0.10	0.04	0.01	0.09	0.00	0.00	20.9
4	27	-0	1476	0	0	0	2513	--	--	16.08	16.08	0.10	0.04	0.01	0.09	0.00	0.00	20.9
5	27	-0	1451	0	0	0	2486	--	--	16.08	16.08	0.10	0.04	0.01	0.09	0.00	0.00	20.9
6	27	-0	1466	0	0	0	2551	--	--	16.08	16.08	0.10	0.05	0.01	0.09	0.00	0.00	20.9
7	27	-0	1382	0	0	0	2458	--	--	16.08	16.08	0.10	0.04	0.01	0.09	0.00	0.00	20.9
8	27	-0	1484	0	0	0	2549	--	--	16.08	16.08	0.10	0.05	0.01	0.09	0.00	0.00	20.9
9	27	-0	1401	0	0	0	2457	--	--	16.08	16.08	0.10	0.04	0.01	0.09	0.00	0.00	20.9
10	27	-0	1415	0	0	0	2521	--	--	16.08	16.08	0.10	0.04	0.01	0.09	0.00	0.00	20.9
11	27	-0	1390	0	0	0	2493	--	--	16.08	16.08	0.10	0.04	0.01	0.09	0.00	0.00	20.9
12	27	-0	1476	0	0	0	2513	--	--	16.08	16.08	0.10	0.04	0.01	0.09	0.00	0.00	20.9
13	27	-0	1451	0	0	0	2486	--	--	16.08	16.08	0.10	0.04	0.01	0.09	0.00	0.00	20.9
14	27	-0	1466	0	0	0	2551	--	--	16.08	16.08	0.10	0.05	0.01	0.09	0.00	0.00	20.9
15	27	-0	1382	0	0	0	2458	--	--	16.08	16.08	0.10	0.04	0.01	0.09	0.00	0.00	20.9
16	27	-0	1484	0	0	0	2549	--	--	16.08	16.08	0.10	0.05	0.01	0.09	0.00	0.00	20.9
17	27	-0	1401	0	0	0	2457	--	--	16.08	16.08	0.10	0.04	0.01	0.09	0.00	0.00	20.9
18	27	-0	1897	0	0	0	3532	--	--	16.08	16.08	0.00	0.06	0.02	0.12	0.00	0.00	20.9
19	27	-0	2094	0	0	0	3521	--	--	16.08	16.08	0.00	0.06	0.02	0.13	0.00	0.00	20.9
20	27	-0	1953	0	0	0	3460	--	--	16.08	16.08	0.00	0.06	0.02	0.12	0.00	0.00	20.9
37	27	-0	1762	0	0	0	3401	--	--	16.08	16.08	0.00	0.06	0.01	0.11	0.00	0.00	20.9
38	27	-0	2090	0	0	0	3384	--	--	16.08	16.08	0.00	0.06	0.02	0.13	0.00	0.00	20.9
39	27	-0	1856	0	0	0	3282	--	--	16.08	16.08	0.00	0.06	0.02	0.12	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

1	54	-0	1863	0	0	0	1762	--	--	16.08	16.08	0.00	0.03	0.02	0.12	0.00	0.00	20.9
2	54	-0	1415	0	0	0	1388	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
3	54	-0	1390	0	0	0	1380	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
4	54	-0	1476	0	0	0	1331	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
5	54	-0	1451	0	0	0	1324	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
6	54	-0	1466	0	0	0	1377	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
7	54	-0	1382	0	0	0	1351	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
8	54	-0	1484	0	0	0	1360	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
9	54	-0	1401	0	0	0	1335	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
10	54	-0	1415	0	0	0	1388	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
11	54	-0	1390	0	0	0	1380	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
12	54	-0	1476	0	0	0	1331	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
13	54	-0	1451	0	0	0	1324	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
14	54	-0	1466	0	0	0	1377	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
15	54	-0	1382	0	0	0	1351	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
16	54	-0	1484	0	0	0	1360	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
17	54	-0	1401	0	0	0	1335	--	--	16.08	16.08	0.10	0.02	0.01	0.09	0.00	0.00	20.9
18	54	-0	1897	0	0	0	2012	--	--	16.08	16.08	0.00	0.03	0.02	0.12	0.00	0.00	20.9
19	54	-0	2094	0	0	0	1844	--	--	16.08	16.08	0.00	0.03	0.02	0.13	0.00	0.00	20.9
20	54	-0	1953	0	0	0	1896	--	--	16.08	16.08	0.00	0.03	0.02	0.12	0.00	0.00	20.9
37	54	-0	1762	0	0	0	1990	--	--	16.08	16.08	0.00	0.03	0.01	0.11	0.00	0.00	20.9
38	54	-0	2090	0	0	0	1710	--	--	16.08	16.08	0.00	0.03	0.02	0.13	0.00	0.00	20.9
39	54	-0	1856	0	0	0	1795	--	--	16.08	16.08	0.00	0.03	0.02	0.12	0.00	0.00	20.9

apost= -- aant= -- ainf= 12.06 asup= 12.06 (e arm. base= 4 X 2.01) staffe= 2 d 10 / 20.9

STAMPA SINTETICA (stampa degli elementi con massimo IR a presso-tenso-flessione (Fx, M), IR bielle (taglio))

FONDAZIONI

Gruppo	El.	NC	x	Fx, M	Bielle	Note
			--	-----	------	
			cm	IR	IR	
1	198	38	30	0.95	--	
1	198	38	0	--	0.19	